

Why take the risk?

of damage to expensive transistors and integrated circuits, when soldering?

Use Antex low-leakage soldering irons



220-240 Volts or Model X25

The leakage current of the NEW X25 is only a few microamps and cannot harm the most delicate equipment even when soldered "live" Tested at 1500v. A.C. This 25 watt iron with it's truly remarkable heat-capacity will easily "out-solder" any conventionally made 40 and 60 watt soldering irons, due to its unique construction advantages. Fitted long-life iron-coated bit 1/8" 2 other bits available 3/32" and 3/16".

Totally enclosed element in ceramic and steel shaft Bits do not "freeze" and can easily be removed

PRICE: £1.75 (rec. retail)

Suitable for production work and as a general purpose iron

Model CCN 220 volts or 240 volts

The 15 watt miniature model CCN. also has negligible leakage. Test voltage 4000v. A.C. Totally enclosed element in ceramic shaft. Fitted long-life iron-coated bit 3/32"

> 4 other bits available 1/8", 3/16" 1/4" and 1/16"

PRICE: £1.80 (rec. retail)

OR Fitted with triple-coated, (iron, nickel and Chromium) bit 1/8"

PRICE: f1 95 (rec. retail)

with 3/16" bit, 2 spare bits 5/32" and 3/32", heat sink, solder, stand

and "How to Solder" booklet.

A SELECTION OF OTHER SOLDERING EQUIPMENT.



MODEL CN

Miniature 15 watt soldering iron fitted 3/32" ironcoated bit. Many other bits available from 1/16" to 3/16". Voltages 240, 220, 110, 50 or 24

PRICE: £1.70 (rec. retail)

MODEL CN2

Miniature 15 watt soldering iron fitted with nickel plated bit 3/32". Voltages 240 or 220. PRICE. £1.70 (rec. retail)

18 Watt miniature iron, fitted with long life iron-

coated bit 3/32". Voltages 240, 220 or 110.

PRICE. £1.83 (rec. retail)



MODEL SK.2 KIT contains 15 Watt

miniature iron fitted with 3/16" bit, 2 spare bits 5/32" and 3/32"

heat sink, solder and booklet"How to Solder

PRICE £2.75



PRICE £2.40 (Rec. retail)

MES.KIT Battery-operated 12v, 25 watt iron fitted with 15' lead and 2 heavy clips

for connection to car battery. Packed in strong plastic wallet with booklet "How to Solder." PRICE £1.95

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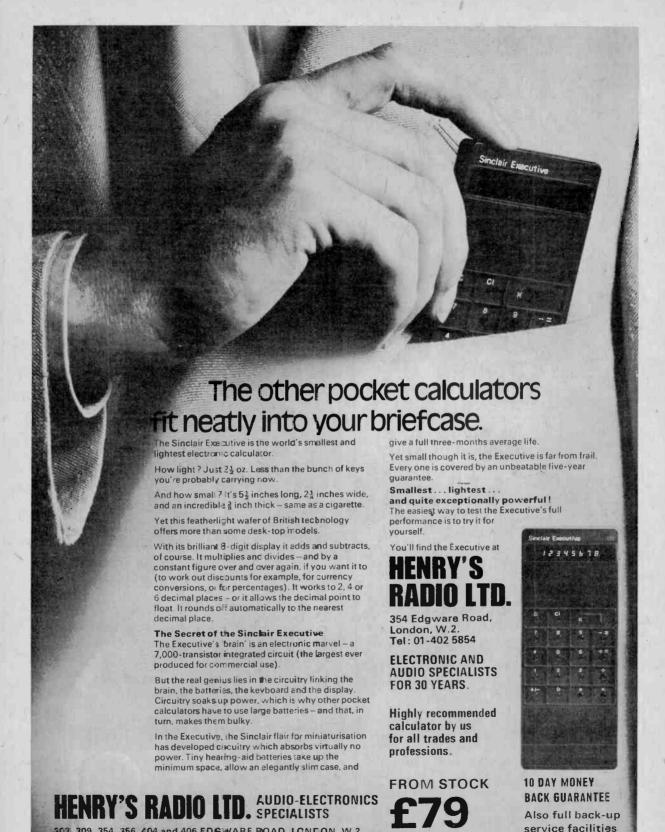
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B.D.2 Press button speed change turntable

features a special version of the

Now, a new development on the well established Connoisseur BD2 belt drive turntable press button speed change.

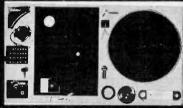
> This new development is exciting news for the enthusiast and comes as part of an integrated turntable and pickup arm assembly which also

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The B.D.1 well known for its superb performance and quality two speed working through a flexible belt drive system is now available in kit form. Construction is simplicity itself with no soldering required. Now it's so easy to own the best.

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Also single jaw model £3.37 (22p P. & P.)

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No batteries—no wires. Just plug in the mains for instant two-way, loud and clear communication. On/off switch and volume control with lock system. Price 212-40. P. & P. 55p extra.



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STEREO 30 plus Amp. LASKY'S £39.75 (Cased), LIST PRICE £62-50 PRICE

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Teak or Walnut case for Stereofetic tuner only. LASKY'S £2.50 LIST PRICE

Double case to hold Stereo 30 or Stereo 70 and Stereofetic tuner in Teak or Walnut.

LIST PRICE

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LEAK TRUSPEED

2-speed 45 and 33½ rpm belt drive turntable complete with plinth, cover and Shure cartridge.

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SINCLAIR PHASE LOCK LOOP STEREO FM TUNER



Incorporates varican diodes, printed cir-cuit, coils, squelch circuit I.C. Decoder, etc., supplied com-pletely built and tested and ready to

be mounted into any cabinet you choose. It may be used with any High Fidelity Amplifier. Power requirements 25/30V DC.

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BSR TAPE DECK SCOOP



BSR TD2

FANTASTIC VALUE, ONLY Lasky's can offer you a tape deck at such an amazing price. The BSR TD2 tape deck operates by a simple reliable mechanism using the minimum of controls.

With & track mono heads. Incorporates fast wind and fast rewind, records at 3½ ips, giving up to 3 hrs playing time, takes up to 5½in. spools. Size 13in. × 8½in. front to rear, 2½in. below plate, 1½in. above plate.

ALSO SUITABLE FOR USE AS A TAPE TRANSPORTER

LASKY'S £8.95 PRICE

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BELTEK C5700 8 TRACK

Stereo car Player Accepts all stand-ard pre-recorded 8 track stereo car-tridges. Features



tridges. Features include automatic head cleaner, channel select and channel repeat push buttons, slider type volume and tone controls, channel balance. Output 5 watts per channel, frequency response 50Hz-10kHz. Output imp. 4 ohms, size 4{(W) x | 1½(H) x 64(D) in. Operates on 12V DC negative earth. Beautifully styled with black ivory and chrome trim. negative earth. and chrome trim.

BELTEK C5700 complete with mounting brackets and 8 track pre-recorded demonstration cartridge.

£19.75 C&P30p

BELTEK R5310 FM TUNING ADAPTOR Matches the C5700, the ideal car stereo system.

LASKY'S PRICE £18.95 C&P 25p

Add £3.75 to any BELTEK car player for pair of FANTAVOX KS701 car speakers.



AKAI TAPE RECORDER SCOOP !

(C & P 75p on all Tape Decks,)

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AKAI X200D List Price £157-93 ... 2 CSS-8 Speakers

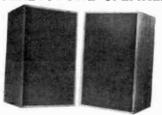
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2 ADM 11/8 mics. Suitable for use on all Akai tape recorders. List Price £11-90. Lasky's Price (pair) £7-50. C & P 15p.

FANTASTIC VALUE WHARFEDALE SCOOP 10" BRONZE C/S

10 in. cloth surround 15 ohms. LASKY'S £2.45 C& F

STEREOSOUND SPEAKERS



speaker system with teak veneer finish. Imp. 8 ohms. Max. Power 12W. Size 14½ (H) x 9 (W) x 7½ (D) in. LASKY'S PRICE (PAIR) £15.75 C&P25p

LEAK SPEAKERS

50 Speakers (pair) £38.95 C & P £48.95 £2.50 £68.75

DIGITAL CLOCK

EXCLUSIVELY FROM LASKY'S



FROM LASKY'S
The clock measures 5½ (W) x 2½ (H) x3* (D) (overall from front of
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8 TRACK STEREO
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The TD8S is suitable for use with most modern stereo amplifiers and delivers

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Power requirements: 210/250V AC, SOHz, Frequency response: 50Hz-10KHz, 4 pole dynamically balanced synchronous motor. Black and woodgrain plastic cabinet. Size: 8½(W) > 3½(H) > 10½ (D) in.

List Price £24-20

LASKY'S £17.95

Garrard Record Players



SP25 Mk. III Deck Only

4 speed Automatic Single Player

Lasky's price £11.50

Garrard SL9SB Deck
Add £9-00 for Garrard Base and Cover
Garrard AP76 deck only
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complete with stereo cartridge
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SP 25 Package

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SHURE M44E Cartridge
Lasky's Base and Cover Total List Price

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DECK ONLY 50p. PLINTH & COVER ONLY 25p. DECK WITH PLINTH AND COVER 75p.

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The exclusive Duo loudspeaker systems are incomparable for quality within their price range. Large speakers in extremely substantial cabinets. There's a choi the Duo II's for the smaller room or the big Duo III's for real bass response. There's a choice of **SPEAKERS**

Duo Type II Size approx. 17in. \times 10 \sharp in. \times 6 \sharp in. Drive unit I3in. \times 8in. with parasitic tweeter. Max power 10 watts, ohms. Simulated Teak cabinet.

£14 pair + £3 p & p.

£77-00 Total

PRICES: SYSTEM 2

Available complete for £69 + £4 p & p

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Total Available complete for only £52

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£22.00 +90p p&p £14'00 +£2 p&p

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MUSIC MAKERS



UNISOUND FOR THE NET

Amplifier is based on the famous Mullard Unilex system, Garrard 2025TC turntable complete with stereo ceramic cartridge, teak simulated plinth and tinted acrylic cover. Plus the big 13in. X 8in. EMI Twin-cone speakers ready for mounting in their elegant cabinets, which simply need screwing and glueing together. All glue and screws supplied. Easy to follow step-by-step instructions guide you quickly and effortlessly to taking the

wraps off truly realistic stereo sound.

#735 complete plus £7-80 p. & p. Diamond Stylus £1-25 extra.

Power output: 4 watts per channel into 8 ohms. Inputs: 120 mV (for ceramic cartridges). Stereo headphones with adaptor £4.00.

UNISOUND MODULES ONLY £6.95

UNISOUND MODULES ONLY 66-95
If you prefer, you can buy the three modules—pre-amplifier power supply/dual power amplifier, and control panel—by themselves for only 66-95, P. 8. P. 50p extra.

No soldering, just simply screw together with screwdriver supplied. Their overall specification is the same as shown for the complete Unisound console, using the high efficient I.C. monolithic power chips to ensure very low distortion at all power levels, correct operation in all ambient temperatures, full power over the audio spectrum.



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A'NATURAL' ONLY FROM THE TOURIST PB CAR RADIO KIT

Apart from the output stage, which is an integrated circuit, the only other electronic components that need soldering are some capacitors, resistors, etc. The kit includes a pre-built RF tuner unit, and fully modulised IF stages which are pre-aligned before despatch. As well as electronic components, this kit also contains 2 diamond-spun aluminium knobs, elegant matching front panel, dial, washers, screws and wire.

The Tourist PB is suitable for 12 volt working on both negative and positive earth vehicles. It covers the full medium and long wave bands. Four push-buttons for medium wave, one for long wave. It is permeability tuned and sturdily constructed. Output is a full 2-5 watts into an 8 ohm speaker. But the Tourist PB will operate into any loud-speaker from 8 to 15 ohms. Power consumption is less than 1 amp.

The Tourist PB can be mounted in any standard size dash panel and it has an illuminated tuning scale for easy reading at night. Chassis size is: 7in wide, 2in. high and 4 % in.

tuning scale for easy reading at night. Chassis size is: 7in wide, 2in. high and 41 in.

deep (excluding front panel, etc.).
★ Circuit diagram and comprehensive instructions 50p, free with parts.
★ Fully retractable lockable car aerial £1.25 post paid.
PRICE ONLY £7+p&p50p
8 ohm speaker with baffle and fixing strips £1.50 + 25p p&p, post free if brought with the kit.

If you can solder on printed circuit board, you can build this pushbutton car radio kit. It's simplejust follow the stepby- step instructions.







★ 5 Electronically Mixed Inputs. ★ 3 Individual Mixing Controls. ★ Separate bass and treble controls common to all 5 inputs. * Mixer employing F.E.T. (Field Effect Transistor). * Solid State Circuitry. * Attractive Styling.

INPUTS:—I. Crystal Mic. or Guitar 9mV. 2. Moving coil Mic. or Guitar 8mV. Inputs 3, 4 & 5 are suitable for a wide range of medium output equipment (Gram., Tuner, Monitor, Organ, etc.). All 250mV sensitivity.

CONTROLS:—3 Volume controls. Bass control range: 13dB @ 60Hz. Treble control range: ± 12dB @ 15KHz. Separate ON/OFF Switch. Neon indicator. POWER OUTPUT:—12 Watts R.M.S. into 3 to 4 ohms speaker. SIGNAL NOISE:—Better than —60dB on inputs 3, 4 and 5 & —50dB on 1 & 2. SUPPLY:—220-250 A.C. Mains. SIZE:—12\frac{1}{2}in. ×

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temperatures up to 5,000°F. Light
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AC142 AC142K AC151 AC154 AC156 AC156 AC167	0·14 0·17 0·15 0·20 0·20 0·20 0·24	AF139 AF178 AF179 AF180 AF181 AF186 AF239	0 · 28 0 · 30 0 · 50 0 · 50 0 · 50 0 · 45 0 · 45 0 · 37	BC168 BC169 BC170 BC171 BC172 BC173 BC174 BC176	0·12 0·12 0·12 0·14 0·14 0·14 0·14	BD187 BD188 BD189 BD190 BD195 BD196 BD197 BD198	0.70 0.75 0.75 0.85 0.85 0.90 0.90	BF271 BF272 BF273 BF274 BFW10 BFX29 BFX84 BFX85	0·30 0·80 0·35 0·35 0·60 0·27 0·22 0·30	0C44 0C45 0C70 0C71 0C72 0C74 0C75 0C76	0·15 0·12 0·10 0·10 0·14 0·14 0·15 0·15	2N404 2N404A 2N524 2N527 2N598 2N599 2N696 2N697	0·20 0·28 0·42 0·49 0·42 0·45 0·12 0·13	2N2904 0 · 17 2N2904A 0 · 21 2N2905 0 · 21 2N2905 A · 21 2N2906 0 · 15 2N2906 0 · 16 2N2907 0 · 20 2N2907 A 0 · 22	2N3702 0·10 2N3703 0·10	2N5172 2N5457 2N5458 2N5459 2B301 2B302A	0·17 0·18 0·32 0·82 0·40 0·50 0·42
AC165 AC166 AC167 AC168 AC169 AC176 AC177 AC178	0 · 20 0 · 20 0 · 20 0 · 24 0 · 14 0 · 20 0 · 24 0 · 28	AL102 AL103 A8Y26 A8Y27 A8Y28 A8Y29 A8Y50 A8Y51	0 · 65 0 · 65 0 · 25 0 · 30 0 · 25 0 · 25 0 · 25	BC177 BC178 BC179 BC180 BC181 BC182 BC182L	0·19 0·19 0·19 0·24 0·24 0·10 0·10	BD199 BD200 BD205 BD206 BD207 BD208 BDY20	0.95 0.95 0.80 0.80 0.95 0.95	BFX86 BFX87 BFX88 BFY50 BFY51 BFY52 BFY53	0 · 22 0 · 24 0 · 22 0 · 20 0 · 20 0 · 20 0 · 17	OC77 OC81 OC81D OC82 OC82D OC83 OC84	0 · 25 0 · 15 0 · 15 0 · 15 0 · 15 0 · 20 0 · 20	2N698 2N699 2N706 2N706A 2N708 2N711 2N717	0 · 24 0 · 35 0 · 08 0 · 09 0 · 12 0 · 30 0 · 35	2N2925 0·14 2N2924 0·14 2N2925 0·14 2N2926 (G) 0·12 2N2926 (Y) 0·11	2N3705 0 · 10 2N3706 0 · 09 2N3707 0 · 11 2N3708 0 · 07 2N3709 0 · 09 2N3710 0 · 09 2N3711 0 · 09	28302 28303 28304 28305 28306 28307 28321 28322	0 · 42 0 · 55 0 · 70 0 · 84 0 · 84 0 · 84 0 · 56 0 · 42
AC179 AC180 AC180 K AC181 AC181 K AC187 AC187 K	0 28 0 17 0 20 0 17 0 20 0 20 0 22 0 22	ASY51 ASY52 ASY54 ASY56 ASY56 ASY57 ASY58 ASZ21	0·25 0·25 0·25 0·25 0·25 0·25 0·25 0·25	BC183 BC183L BC184 BC184L BC186 BC187 BC207 BC208	0 · 10 0 · 12 0 · 12 0 · 28 0 · 28 0 · 11 0 · 11	BF115 BF117 BF118 BF119 BF121 BF123 BF125 BF127	0 · 24 0 · 45 0 · 70 0 · 70 0 · 45 0 · 50 0 · 45	BPX25 BSX19 BSX20 BSY25 BSY26 BBY27 BSY28 BSY29	0 · 85 0 · 15 0 · 15 0 · 15 0 · 15 0 · 15 0 · 15	OC139 OC140 OC169 OC170 OC171 OC200 OC201 OC202	0 · 20 0 · 25 0 · 25 0 · 25 0 · 25 0 · 25 0 · 28	2N718 2N718A 2N726 2N727 2N743 2N744 2N914 2N918	0·24 0·50 0·28 0·28 0·20 0·20	2N2926 (O) 0·10 2N2926 (R) 0·10 2N2926 (B) 0·10 2N3010 0·70	2N3819 0.28 2N3820 0.50 2N3821 0.35 2N3823 0.28 2N3903 0.28 2N3904 0.30 2N3905 0.28	28322A 28323 28324 28325 28326 28327 28701	0·48 0·56 0·70 0·70 0·70 0·70 0·48
AC188 AC188K ACY17 ACY18 ACY19 ACY20 ACY21	0·22 0·20 0·25 0·20 0·20 0·20 0·20	BC107 BC108 BC109 BC113 BC114 BC115 BC116	0 · 09 0 · 09 0 · 10 0 · 10 0 · 15 0 · 15 0 · 15	BC209 BC212L BC213L BC214L BC225 BC226 BCY30	0·12 0·11 0·11 0·14 0·25 0·35 0·24	BF152 BF153 BF154 BF155 BF156 BF157 BF158	0 · 55 0 · 45 0 · 45 0 · 70 0 · 48 0 · 55	BSY38 BSY39 BSY40 BSY41 BSY95 BSY95A Bul05	0 · 18 0 · 18 0 · 28 0 · 28 0 · 12	OC202 OC203 OC204 OC205 OC309 P346A P397 OCP71	0 25 0 25 0 35 0 40 0 20 0 42 0 48	2N929 2N930 2N1131 2N1132 2N1302 2N1303	0·30 0·21 0·21 0·20 0·22 0·14 0·14	AA119 0.08	2N3906 0 · 27 2N4058 0 · 12 DES AND RECTI BY133 0 · 21	OA10	0·40 0·45
ACY22 ACY27 ACY28 ACY29 ACY30 ACY31 ACY34 ACY35	0 16 0 18 0 19 0 35 0 28 0 28 0 21	BC117 BC118 BC119 BC120 BC125 BC126 BC132 BC134	0·15 0·10 0·30 0·80 0·12 0·18 0·12 0·18	BCY31 BCY32 BCY33 BCY34 BCY70 BCY71 BCY72 BCZ10	0 26 0 30 0 22 0 25 0 14 0 18 0 14 0 20	BF159 BF160 BF162 BF163 BF164 BF165 BF167 BF173	0 · 60 0 · 40 0 · 40 0 · 40 0 · 40 0 · 40 0 · 22 0 · 22	C111E C400 C407 C424 C425 C426 C428 C441	0·50 0·30 0·25 0·20 0·50 0·35 0·20 0·35	OCP/1 ORP12 ORP60 ORP61 ST140 ST141 TIS43 UT46 2G301	0 · 43 0 · 40 0 · 40 0 · 12 0 · 17 0 · 30 0 · 27 0 · 09	2N1304 2N1305 2N1306 2N1307 2N1308 2N1309 2N1613 2N1711 2N1889	0·17 0·21 0·21 0·23 0·23 0·20 0·20 0·32	AA120 0.08 AA129 0.08 AAY30 0.09 AA713 0.10 BA100 0.10 BA116 0.21 BA126 0.22 BA148 0.12 BA154 0.12	BY164 0.50 BYX38/30 0.42 BYZ10 0.35 BYZ11 0.30 BYZ12 0.30 BYZ13 0.25 BYZ16 0.40 BYZ17 0.40	OA47 OA70 OA79 OA81 OA85 OA90 OA91 OA95 OA200	0.07 0.07 0.07 0.07 0.09 0.08 0.08 0.07
ACY36 ACY40 ACY41 ACY44 AD130 AD140 AD142 AD143 AD143 AD161	0·28 0·17 0·18 0·35 0·38 0·48 0·38 0·38 0·38	BC135 BC136 BC137 BC139 BC140 BC141 BC142 BC143 BC145 BC147	0·12 0·15 0·15 0·40 0·80 0·30 0·30 0·30 0·45 0·10	BCZ11 BCZ12 BD121 BD123 BD124 BD131 BD132 BD133 BD135 BD136	0·25 0·25 0·60 0·65 0·60 0·50 0·65 0·65 0·65	BF176 BF177 BF178 BF179 BF180 BF181 BF182 BF183 BF184 BF185	0 · 35 0 · 36 0 · 30 0 · 30 0 · 30 0 · 30 0 · 40 0 · 40 0 · 25 0 · 30	C442 C444 C450 MAT100 MAT121 MAT121 MPF102 MPF104 MPF105	0·30 0·35 0·22 0·19 0·20 0·19 0·20 0·42 0·87 0·37	2G302 2G303 2G304 2G306 2G308 2G309 2G339 2G339 2G339 2G344 2G345	0·19 0·19 0·24 0·40 0·35 0·35 0·20 0·16 0·18	2N1890 2N1893 2N2147 2N2146 2N2160 2N2192 2N2193 2N2194 2N2217 2N2218	0 · 45 0 · 37 0 · 72 0 · 57 0 · 60 0 · 35 0 · 35 0 · 22 0 · 20	BA155 0-14 BA156 0-13 BY100 0-15 BY101 0-12 BY105 0-17 BY114 0-12 BY126 0-14 BY127 0-15 BY128 0-15 BY130 0-16	BYZ18 0.35 BYZ19 0.28 CG62 (Eg) OA91 0.05 CG651 (Eq) OA70- OA79 0.06 OA5 0.35 OA58L 0.21	OA200 8D10 8D19 IN34 IN34A IN914 IN916 IN414B	0.07 0.05 0.05 0.07 0.07 0.06 0.06 0.06

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SN7403	17 0 35 0 32 17 0 35 0 32 15 0 43 0 42 10 0 39 0 38 10 0 15 1 10 17 0 84 0 58 10 21 15 21 17 0 86 0 85 10 21 05 0 95 10 0 95 0 90 10 23 50 23 40 12 0 81 0 30 12 0 81 0 30 12 0 81 0 30 12 0 85 25 \$5 00
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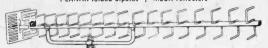
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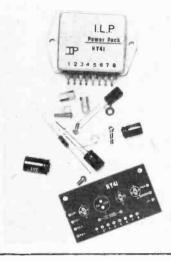
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THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in with this important improvement the nt 41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry.

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts

R M.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.
INPUT IMPEDANCE: 30K ohms at 1KHz.

VOLTAGE GAIN: 30db at 1KHz

TOTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%)

FREQUENCY RESPONSE: 5Hz-50KHz ± 1db. SUPPLY VOLTAGE: + 22.5volts D.C. SUPPLY CURRENT: Q,8 amps maximum.

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P.:-MONO: £4.90 STEREO: £9.80

UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of

volume, treble and bass potentiometers it is ready for use.

Internally the HY5 provides equalization for almost every conceivable input, the

desired function is achieved by use of a multi-way switch or by direct interconnection.

Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from 16–25 Volts and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

Magnetic Pick-up (within ±1db RIAA curve) 2mV. 47K Ω Tape Replay (external components to suit head). 4mV. 47KΩ

Microphone (flat) 10mV. 47KΩ

Ceramic Pick-up (equalized and compensatable) 20–2000mV. variable.

Tuner (flat) 250mV. 100K Ω Auxiliary 1 250mV. 47K Ω Auxiliary 2 2-20mV. 100K Ω

Main Pre-amp output 500mV. Direct tape output 120mV.

ACTIVE TONE CONTROLS (Bexendall) Treble + 12db. Bass + 12db.

INTERNAL STABILIZATION

Enables the HY5 to share an unregulated supply with the Power Amplifier.

SUPPLY VOLTAGE 16-25 volts

PRICE: MONO: £3.60 SUPPLY CURRENT

6mA approx. OVERLOAD CAPABILITY

better than 26db on most sensitive input infinite on tuner and auxl.

OUTPUT NOISE VOLTAGE: 0.5mV.

STEREO: £7.20



POWER SUPPLY PSU45

The versatile P.S.U.45 is designed to supply your HY41's +HY5's in stereo or mono format.

Specification

Input: 200-240 Volts. Output: ± 22.5 Volts at 2 amps. Overall Dimensions: L. 7"; D. 3.8"; H. 3.1"

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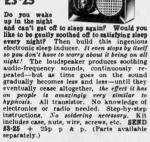
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20,000 Hz \pm 1 db at full power. 15 watts rms per channel. Walnut cabinet with satin aluminium trims. Inputs: phono 2-5mV and 5mV RIAA; tuner/aux 250mV. Hum and noise: phono - 50db; tuner/aux - 65db. How's that for a specification! Size 14½" wide, 3½" high, 10½" deep



OLSON RA-310 AM/FM/MPX

This ROC Tuner is especially de signed to match the Olson AM-395 Stereo Amplifier. In price and value, as well as it's good looking design! But of course it's also ideal for use with any other amplifier. The RA-310 costs £10-00 less than

to use with any other ampriler. The mary to costs from the standing the horizontal retail value, and yet it is a highly sophisticated unit, incorporation in the standing the latest solid state techniques. Deparation is drift free for suprementation-holding capability. You can connect this Tumer to a stereor mental retained to the standing to a tape deck or a tape recorder. And of course it covers all the stations in the AM and FM bands. FM 87-105 MHz; AM 255-1056 KHz.
FM Sensitivites: FM, 3.UV: AM, 250,UV. Stereo separation 30dB at 1kHz, image rejection.

60dB. Size: 11 4 " wide, 4" high, 71" deep



REALISTIC SA-100B 6-WATT STEREO AMPLIFIER

Here's fabulous, exciting value in miniature!' This high quality stereo amplifier measures only 9 "wide \times 3" high × 5%" deep. And yet it has sepa-rate ganged volume, balance and tone con-

trols. Plus speaker in/lour, mono/stereo, phono/ tuner and power on/olf slide switches. The ends are olled walnut, with match-ing enamelled metal top. The front panel is satin aluminium and walnut-brown enamel, Frequency response is 50 to 10,000 Hz \pm 3dB. Dutput 3 waits r.m.s. per channel into 8 ohms. Inputs are 100mV for both phono and tuner.

MAGNETIC CARTRIDGE For tabulous reproduc-tion at a very low price. you'll find it hard to beat 0-7 mild diamond stylus. Dut-put: 6mV per channel. Frequency range 30-18,000 Hz. Channel balance: ±1-5d8 Channel separation: 20dB. Recommended stylus pressure: 2-4 grams. Compliance: 9×10-6 cm/dyne, ROC PRICE £4-75 EAGLE LC.07 STEREO MOVING-MAGNET

Here's your opportunily to own a transcription cartridge for the price of a ceramic! Is specially designed to match top quality tone arms, and to get the very best from your hi-fi amplifier. 0-7 mil diamond stylus. Output: 7mV per channel, Frequency range: 20-21,000 Hz. Channel balance: ±1dB. Channel separation: 28dB. Compliance: 12×10-6 cm/dyne RDC PRICE £6-37

> OLSON AM-395 40-WATT STEREO

An ideal unit for your new stereo separate system. It is more than £10.00 below the normal retail price 1 Making the AM-395 one of Britain's best hi-fi

buys. It takes in signals from magnetic or ceramic pick-ups tuners (see Dison RA-310) and tape decks. And it's got outputs for taping and for headphones. There are separate bass and treble controls, separate Left and Right channel volume

and treble controls, separate Left and Right channel volume controls. And a loudness switch for boosting the bass and treble notes when listening at low output levels. Frequency response: 20-20,000 Hz ± 3dB. Output: 20 watts r.m.s. per channel into 8 ohms. Inputs: magnetic phone 3 °0mW RIAA, crystal phono 100mV; tape 160mV; tuner 160mV. Size 11+2" wide, 4" high, 7½" deep. The specification reads well - sounds even better!



SOLID STATE STEREO AMPLIFIER
The A-3000 looks as good as it sounds! Giving you a big performance this superb audio amplifier has a full range of facilities on the front and rear panels. On the front all the controls you're ever likely to need plus a headphone socket. On the rear signal inputs, speaker outputs and a line fuse for circuit protection. Specifications: 18 watts rms per channel

Specifications: 10 Watts link per challed into 8 ohms. Frequency response 20-35,000 Hz (± 2db) Inputs Magnetic. Ceramic. Tuner. Tape. Aux. Tape Play. Size: 345mm × 300mm × 130mm.

RECORD CLEANERS The original "Dust Bug" Automatic Record Cleaner keeps your records clean as they play. £1:16 Watts Disc Preener, Keeps new records like nev

for perfect record reproduction, 35p

R 307 TRANSISTOR-PRE-AMPLIFIER

Now your amplifier that could only reproduce that could only reproduce ceramic or crystal pick-up cartridges, can accept signals from moving-magnet cart-ridges! The R.307 steps up signals from between 5-20mV to 200-800 mV. Input 5-20mV. Equalisation: BIAA. Output 200-800mV flat. Frequency range: 20-22,000 Hz. Dimensions: 31"×11"×27 Supply: 240 VAC. RUC PRICE £4-92

15-FOOT STEREO HEADPHONE EXTENSION CORD R.362
Fitted with heavy duty
one end and a matching stereo plug at
the other. ROC PRICE £1-30 EXTENSION CORD R.362

STEREO HEADPHONE "Y" ADAPTOR stereo headphones from a single socket. Fitted with male plug and two female sockets. BOC PRICE £1-30



R.446 3-WAY MATCHED SPEAKERS
These will do justice to your amplifier — and to your pocket. At only £16-40 a pair, they are real value-for-money, Each cabinet is heavily lagged and teak finished. They handle 16 watts rms (8 watts rms each). Each loudspeaker contains a large dual cone base unit, plus a separate tweeter, Frequency range: 40 to 19,000 Hz. Size 14" high.

N. JORY Esq. 193 EDGWARE RD, LONDON, W2 1ET.01-723 6211

CALLERS WELCOME 9-6 MON TO SAT. LATE NIGHT THURSDAY 7 PM



OLSON AM-357 4-WATT STERED AMPLIFIER Here's marvellous value for someone just starting to set themselves up in audio! At only £10-50, you get a fine amplifier in a scratch resistant metal cabinet, with a smart brushed aluminium front panel. It incorporates separate tone, and volume controls for each channel. Inputs are provided for turntable (ceramic cartridge), tuner and tape deck or recorder. Frequency response: 70-20,000 Hz ± 3dB. Output: 2 watts r.m.s. per channel into 8 phms. Inputs: phono 80mV; tunar/aux 80mV. Size 8" wide, 2\frac{1}{2}" high,

Q 25-WATT 3-WAY CRYSLER LIVING AUDIO SPEAKER CE-56

This high quality speak er has its own built-in 3-way sound response switch, giving you the ideal frequency response for hi-fi, natural or mood music listening. Its beautiful, heavy, oiled welnut cabinet incorporates two separate speaker units an 8" woofer, and a 5"

mid-range with 2" concentric tweeter. Power handling capacity: 25 watts r.m.s into 8 ohms. Overall frequency res ponse: 35-20,000 Hz. Cabinet size: $10\frac{1}{2}^{\circ} \times 7\frac{1}{2}^{\circ} \times 8\frac{3}{4}^{\circ}$. Exactly right for matching the most modern decor.



PALACE AM/FM/MPX STERED TUNER AMPLIFIER SSA-16 This is one of the lowest priced stero tuner amplifiers on the market. It covers the full range of both AM and FM broadcast frequencies. And when you're switched to FM, an indicator lights up when a stereo signal is received - that's the time to itch to 'Stereo' 1 The SSA-16 has all the facilities you'd exswitch to "Stereo" I The SSA-16 has all the facilities you'd expect to find on lunars costing twice as much – separate valueme, bass, treble, balance and tuning controls. Selector switch for tape, phono, AM, FM, stereo, Jack socket on front panel for stereo headphones. Frequency range: FM 88-108 MHz, AM 535-1605 kHz. Frequency response: 50-10,000 Hz \pm 3d8. Power output: 4 warts total must power into two 8 ohm speakers. Size: 16% wide, $4\frac{1}{4}\%$ high, 8% deep.

ROC 7-WATT STEREO AMPLIFIER CHASSIS SK-317 R D C Stereo completely self-contained, and it costs £2-25 less than the normal re tail value! T SK-317 is a really compact unit measuring only 51" wide, 13" high and 6½" deep. It contains its own mains power supply, and has a ganged volume control and separate treble controls for each channel. Specification: frequency response 40-17 000 Hz \pm 3dB; output 3-5 watts music power per channel into 8 ohms; input, phono. 600mV; signal-to-noise



ratio betterthan 45dB

DLSON AM-372 16-WATT STEREO AMPLIFIER R Here's a really good amplifier at a really down-to-earth price — nearly £7 less than the normal retail value! Just look at what the AM-372 will do for you — reproduce signals from ceramic or crystal cartridges. AM and FM tuners, and tape recorders. And it gives you outputs for two sets of speakers, headphones and tape recorders. Frequency response is 30 to 20,000 M2 ± 3dB, Output 8 watts r.m.s. per channel music power into 8 ohm speakers. Phono input 200mV. Tuner input 200mV. Size: 121" wide, 31" high, 71" deep.

> Return-of-post mail order service. Orders over £10 post free (UK only). Add 25p for p & p to orders under £10. HP terms available for callers

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Plays 12", 10" or 7" records.
Auto or Manual. A high
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reliability with 12 months'
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Size 13½ × 11½in. Above motor board 31in. below motor board 21in.



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RCS DE-LUXE 3 WATT AMPLIFIER. Ready made, tested. Printed circuit. 3 watts output. Tone and volume controls. Complete with output valve and rectifier, two knobs, and high performance loudspeaker. Double wound fully isolated mains transformer. A.C. mains 200/250V. Response 50-12,000 cps. Sensitivity 300mV.

GARRARD DISCO DECK

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sizes of records. 4
pole beavy duty
motor. 9in. steel
turntable. Plug in
head complete with
stereo/mono cartridge. Adjustable stylus pressure. Autostop. Brown and Cream finish. AC mains 110/240v.
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Above motor board 3in., below motor board 2in.
Ideal for Home Hi-Pi or Discotheque.

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16/450V	15p	1000/50V	47p		331
32/450V	20p	8+8/450V	18p		
25/25V	10p	8+18/450V	20p		50r
50/50V	10p	16+18/450V	25p	32+32+32/350V	431
100/25V	10p	32+32/350V	25p	100+50+50/350V	481

1, 2, 4, 5, 8, 16, 25, 30, 50, 100, 200mF 15V 10p.
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2000mF 6V 25p; 25V 42p; 50V 57p
2000mF 6V 25p; 25V 42p; 50V 57p
2500mF 50V 82p, 3290mF 25V 47p, 50V 65p,
5000mF 8V 25p 12V 42p; 25V 75p
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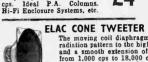
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3 ohm, 2 jin, 3 in, 5 × 3 in.
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	0.1	0.15
Size	matrix	matrix
2∮in × 3∄in	22p	16p
2∔in × 5in	24p	25p
3∄in × 3∄in	24p	25p /
3∄in × 5in	27p	29p
17in × 21in	75p	57 p
17in × 3∄in	£I	7.96
Pins-either	size: packe	t of 36, 18p
	orner President	

IμF	450V	19p	1,000µF	25 V	27 p
2μF	500V	20p	1,000µF	50V	39p
4µF	350V	14p	2,000µF	25V	36p
8µF	450V	16p	2,000µF	50V	53p
16µF	450V	17p	2,500µF	25V	45p
25µF	25V	7p	2,500µF	50 V	60p
25µF	50 V	8р	3,000µF	25V	48p
32µF	450V	24p	5,000µF	25V	55p
50µF	50 V	10p	5,000µF	50V	98p
100µF	25V	10p	8–8µF	450 V	18p
100μF	50V	10p	8-16µF	450 V	20p
250µF	25V	12p	16-16µF	450V	27p
250µF	50 V	17 p	16-32μF	450V	63p
500µF	25V	18p	32–32µF	450V	49p
500µF	50V	25p	50-50μF	350V	38p

MINIATURE ELECTROLYTICS

IμF	63V	6р	47µF	16V	7p
2.2µF	63V	6р	47µF	25V	6p
3 JuF	63 V	6р	68µF	16V	6p
1.7µF	63V	6р	100µF	107	6p
8µF	40V	7p	220µF	16V	7р
10µF	25 V	6p	330µF	16V	Пp
10µF	64V	7p	470µF	100	lip
16µF	40V	7 p	1,000µF	16V	l9p
30µF	15V	7p	1,500µF	16V	23p

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systems, giving 7½V, stabilised
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Carbon Al 5%, high-stability, El2 values. ‡W, lp; W, ip; IW, 4p; 2W, 6p Wire-wound 5W, 10p; 10W, 12p

*LOUDSPEAKERS

 $\begin{array}{l} \textbf{LOUDSPEAKERS} \\ 7: \textbf{IN} \times 4: \textbf{IN}, \ 3\Omega - \ell \cdot 1 \cdot 12, \ 8\Omega - \ell \cdot 1 \cdot 12, \\ 15\Omega - \ell \cdot 1 \cdot 40. \\ 15\Omega - \ell \cdot 1 \cdot 40. \\ 15\Omega - \ell \cdot 1 \cdot 40. \\ 15\Omega - \ell \cdot 1 \cdot 70. \\ 15\Omega - \ell \cdot 1 \cdot 70. \\ 15\Omega - \ell \cdot 2 \cdot 12. \\ 15\Omega - \ell \cdot 2 \cdot 12. \\ 15\Omega - \ell \cdot 2 \cdot 12. \\ 15\Omega - \ell \cdot 2 \cdot 10. \\$

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Car aerial
Co-axial
D.I.N. 2 pin (speaker)
D.I.N. 3 pin
D.I.N. 4 pin
D.I.N. 5 pin. 180°
D.I.N. 5 pin, 240°
D.I.N. 6 pin
Jack, 2+mm unscreened
Jack, 24mm screened
Jack, 31mm unscreened
Jack, 34mm screened
Jack, in unscreened
Jack, Jin screened
Jack, stereo, unscreened
Jack, stereo, screened
Phono, plastic top
Phono, plated metal
Phono, fitted 4 ft lead
Wander, red or black
Banana Amm. rad or black

LINE SOCKETS

Car aerial
Co-axial
D.I.N. 2 pin (speaker)
D.I.N. 3 pin
D.I.N. 5 pin, 180°
D.I.N. 5 pin, 240°
Jack, 3½mm
Jack, ½in screened
Jack, stereo, screened
Phono, plated metal

D	SUCKEIS	
	Car aerial	8p
b	Co-axial, surface	8p
<u></u>	Co-axial, flush	9p
n		10p
۲ ۲	D.I.N. 3 pin	9 _p
2	D.I.N. 5 pin, 180°	9p
_	D.I.N. 5 pin, 240°	9 p
μ	Jack, 2½mm	ιóρ
	Jack, 25mm	ίορ
Р		15p
р		17p
p	Jack, stereo, switched	24p
P P P P	Phono, single	5 p
D	Phono, 2 on a strip	7 p
	Phono, 3 on a strip	9 p
p P	Phono, 4 on a strip	10p
p	Wander, single, red or black	5p
p	Wander, twin strip	7 p
		6p
P	Banana 4mm red, or black	Sμ

CARACITORS

					F0011	C 124	
CAPA	CITO	RS		0·0027µF 0·003µF	500∨ 500∨	S/M Cer.	15p 5p
2-2pF	500 V	S/M	71p	0.0033µF	125V	P.5.	6p
3 3pF	500V	S/M	7 1 P	0.0033µF	500V	Poly.	6р
5pF	500V	5/M	7 ½ p	0.0033µF	1,000V	MDC	6р
10pF	125V 500V	P.S. S/M	5p 7∮p	0·0036μF 0·0047μF	500V 125V	5/M P.S.	15p 9p
10pF - 15pF	1250	P.S.	5p	0.0047µF	500V	Poly.	6p
15pF	500V	Cer.	4p	0.0047µF	500V	S/M	20p
18pF	500V	S/M	71p	0.0047µF	1,000V	MDC	6р
22pF	125V	P.S.	5p 7{p	0.005µF	100V	Mylar	3p
22pF 25pF	500V 500V	S/M S/M	7 i P	0.005µF 0.0068µF	500V 125V	Cer.	5p 101p
27pF	500 V	Čer.	4p	0.0068µF	500V	P.S. S/M	30p
33pF	125V	P.S.	5p	0.0068µF	500V	Poly.	6р
33pF	500 V	S/M	7 p 7 p	0.0082µF	125V	P.S. 5/M	101p
39pF	500V	S/M P.S.	7 j p	0·0082μF 0·01μF	500∨ 18∨	Disc	30p 4p
47pF 47pF	500 V	Cer.	5p 4p	0.01μF	125V	P.S.	101p
50pF	500 V	S/M	71n	0 01µF	160V	Poly.	4p
56pF	500V	S/M	7 j p	0.01µF	250V	M.F.	3 p
68pF	125V	P.S. S/M	7 p 5p 7 p	0·01μF 0·01μF	400 ∨ 500 ∨	Poly. Cer.	3p 5p
68pF 75pF	500V 500V	S/M	710	0.01µF	500V	S/M	30p
82pF	500V	S/M	7 p	0.01µF	600V	MDC	/p
100pF	125∨	P.S.	5p	0.01µF	1,000V	MDC	9p
100pF	500∨ 500∨	S/M Cer.	71p 5p	0·015μF 0·015μF	160V	Poly. Poly.	3p 3p
100pF 120pF	500 V	S/M	7 i P	0.02µF	1007	Mylar	3p
150pF	125V	P.S.	5p	0.022µF	187	Disc	5p
150pF	500V	P.S. S/M	5p 7∮p	0 022µF	250V	M.F.	3p
150pF	500V	Cer.	5р 7 1 р	0·022µF 0·022µF	400∨ 600∨	Poly. MDC	3p 71p
180pF 200pF	500∨ 500∨	S/M S/M	7 P	0·022μF	1,0000	MDC	9p
220pF	125V	P.S.	5p	0.033µF	250V	M.F.	4p
220pF	500V	Cer.	5p	0.033µF	400V	Poly.	4p
250pF	500 V	S/M	8p 5p	0·047μF 0·047μF	12V 160V	Disc Poly.	6p 3p
270pF 300pF	500V	Cer S/M	8p	0·047μF	250V	M.F.	3p
330pF	125V	P.S.	5p	0 047 μF	400V	Poly.	4p
330pF	500V	S/M	8р	0.047µF	600 V	MDC	8p
390pF	500V	5/M	8p	0 047μF	1,000V 30V	MDC Disc	I0p
470pF 470pF	125∨ 750∨	P.5. Disc	5p 5p	0·1μF 0·1μF	250	M.F.	6p 4p
500pF	500V	S/M	8p	0·1µF	400 V	Poly.	5 n
560pF	500V	5/M	8p	0-1 uF	600V	Poly. MDC MDC	10p
680pF	125V	P.S.	6р	0 IμF	1,000V 250V	MDC M.F.	13p 5p
680pF 820pF	500V 500V	5/M 5/M	8p	0·15μF 0·22μF	160V	Poly.	6p
0.001µF	1007	Mylar	3p	0.22µF	250V	M.F.	5p
0.001µF	125V	P.S.	6р	0.22µF	400V	Foil	I On
0.001µF	400V	Poly.	3р	0 22µF	1,000V	MDC M.F.	I5p
0·001μF 0·001μF	500V	S/M Cer.	10p 5p	0·33μF 0·47μF	250V 250V	M.F.	8p
0.001µF	1,000	MDC	6р	0.47µF	400 V	Foil	15p
0 0015µF	400V	Poly.	3 p	0·47µF	1,000V	MDC	20p
0.0015µF	500V	S/M	10p	I-0μF	250V	M.F.	15p
0.0015µF 0.0018µF	500V	Cer. S/M	5p	Note:			
0.002µF	100V	Mylar	3p	5/M = si	lver mic	1% to	ıl.
0.002 µF	500 V	Cer.	5p	P.S. = p	olystyren	e 21%	tol.
0.0022µF	125V 500V	P.5. S/M	6p 10p	M F -	a.c. ratir dullard n	nin foil	V .
0·0022μF 0·0022μF	1,000	MDC	6р		eramic.		
	.,						

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ZTX213 12p	ZTX384 16p	ZSI2I 9p	ZS276 23p	KS100A 17p
ZTX214 13p	ZTX450 15p	ZS122 IIp	ZS278 33p	KS110A 17p
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ZTX303 12p	ZTX502 15p	ZS141 39p	KSO33A 17p	KS180A 17p

GEMINI AMPLIFIER

V =1					
Set of Main Amp. semiconductors (stered	o)				£5-60
Set of Pre-amp. semiconductors (stereo)					£1-55
Set of Power Supply semiconductors					£2-15
Main amp, printed circuit board					£1-45
Pre-amp, printed circuit board			2		£1.95
Power Supply printed circuit board				14.14	€0-60
(P.C.B.'s are glass fibre and are roller tinn	ed ar	nd drille	ed)		4
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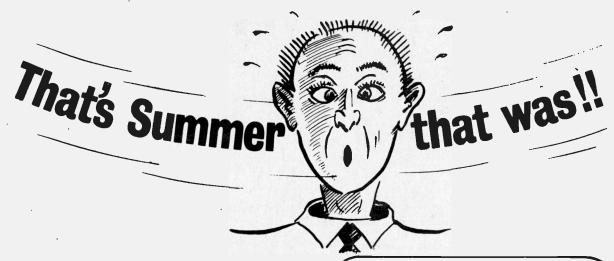


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Summer was so late arriving this year that it nearly slipped by without our noticing it! Already we are tucking the lawn mower in for its winter hibernation, and once again "the nights are drawing in" HOORAY!—that means we can really get cracking on those electronic projects that have been buzzing around at the back of our minds.

The first step is to get the components lined up. And the best way to do that? Simple—get a copy of the Home Radio Components Catalogue. Then we can quickly and clearly see what we need and how much it costs. We'll know too that either by sending an order or by calling in at the Mitcham shop, we can get just what we want "off the shelf". The catalogue costs 70p, including post and packing, or 50p over the counter. Every copy contains 10 vouchers, totalling a value of 50p when used as instructed—so you can soon get back the cost of the catalogue. Over 8,000 items are listed, over 1,500 of them illustrated, and free supplements are supplied regularly to keep you up to date.

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VOL. 8 No. 10 October 1972

PRACTICAL ELECTRONICS

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PROBLEMS OF PROGRESS

The pace of technical progress has become so accelerated that many interesting developments and techniques, especially in the field of integrated circuits, hardly see the light of day before their demise is threatened by yet another new development. Innovation leap-frogs innovation, and consequently valuable and thought-provoking devices become redundant long before they have been fully exploited. This poses problems to industrial users of such components, and despite crystal-ball gazing and shrewd planning ahead, many equipment makers have been caught out by this explosive state of the art.

The break-through in small calculator designs based on the single-chip i.c. is an outstanding case at this particular time. Commercial desk calculators costing in the region of £250 have been replaced overnight by new instruments selling at one third the price. Business people who purchased their calculator last year must be wringing their hands and wishing they had waited until the spring of '72. But it is easy to be wise after the event.

The same problem, although on a smaller scale, affects a magazine such as ours, catering for the private constructor. Does one sit back neglecting contemporary and readily available devices, just waiting for the "ultimate" one to turn up? For example, to have knowledge of impending changes in i.c. design that are likely to revolutionise the commercial calculator in the near future is one thing; it is quite a different thing, though, to predict with any certainty if and when these new l.s.i. chips will be made available to private individuals—and if so at what cost.

In such circumstances the P.E. Digi-Cal desk calculator was commissioned. The abundance of cheap TTL devices seemed to justify such a project being presented to the private constructor. The total cost of material for this project made it a most favourable proposition in view of the then prevailing cost of a comparable commercial instrument. However, between the completion of this design and the publication of the first article, the big break-through in cheap commercial calculators occurred.

Though "priced out of the market" the Digi-Cal remains a unique and valuable contribution to the record of design information published expressly for the benefit of private constructors and electronics enthusiasts. As an education exercise, the real worth of this project cannot be denied. Certainly it offers the technically inquisitive far more than the mere assembly of any commercial kit can possibly provide.

F.E.B.

THIS MONTH

CONSTRUCTIONAL PROJECTS

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SPECIAL DATA SHEET

I.C. LEAD-OUT IDENTICHART

We apologise for any slight loss of quality of print in this month's issue. Supplies of the normal paper were not available due to the Docks Dispute.

Our November issue will be published on Friday, October 13

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Practical Electronics, Fleetway House, Farringdon St., London, E.C.4. Phone: Editorial 01-634 4452; Advertisements 01-634 4202

Most of the cheaper intercoms on the market at the present time have a low output which can be very distorted. In order to overcome these difficulties it was decided to build a battery powered intercom using an integrated circuit chosen from the General Electric range of audio amplifiers.

The i.c. chosen was the PA234 which has a quoted output of just under one watt when working from an 18V supply with a typical distortion of three per cent. A preamplifier is needed to drive this i.c. and a simple, one transistor, common base type is used.

Even though the basic system described here is only a simple master/slave one it is very easy to extend it to master/master or master and two or more slaves, with or without call facilities; the necessary alterations for these additions are given at the end.

As no commercial cases could be found which looked right, it was decided to build these as well.

CIRCUIT OPERATION

The amplifier circuit diagram is shown in Fig. 1. It will be seen that TR1 is connected in the common base mode which is relatively rare.

In this configuration the signal is applied to the emitter producing the advantages of low input impedance—of the order of approximately 50 ohms, and a high output impedance, thus making it ideally suited to its purpose.

The microphone/speaker is a 25 ohm loudspeaker and this is easily matched to the preamplifier stage, another advantage being that this configuration prevents inductive pickup from TV sound. Whilst experimenting with the prototype a standard high gain common emitter preamplifier was used and the TV pickup drowned all other signals.

The purpose of CI is to filter out any TV or other radiated interference; the final version gives

no mains hum even though the cables run alongside mains leads for some distance.

The biasing for TR1 is provided by R1, R2 and C2 which ensures that the base is near earth potential as far as alternating signals are concerned. R3 serves a dual purpose in that it reduces the supply of 18V down to 9V for the preamplifier and in conjunction with C3 decouples the two stages preventing any feedback via the supply.

Potentiometer VR1 is a volume control and should be adjusted to give the best output. The signal is then fed via C4 and R4 to the input terminal, pin 3, of the i.c. The ratio of R5 to R6 is determined from the manufacturer's data sheet and controls the correct biasing of the i.c., whilst the gain is determined by the ratio R5 to R4.

The output is stabilised against oscillation by the capacitor C5, and C7 further stabilises the arrangement.

The circuit for the call oscillator is given in Fig. 2 and it will be seen that it is a conventional multivibrator working at about 1kHz. Other frequencies can be selected by varying R8, R9 and C8, C9.

The power supplies are two PP6 batteries connected in series to give 18 volts.

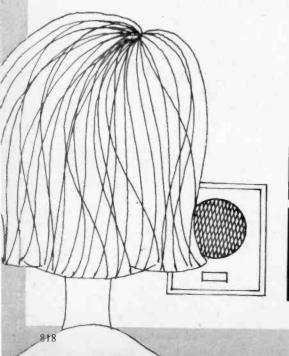
MASTER/SLAVE SWITCHING

Fig. 3 shows a simple master/slave set up. S1 is a miniature lever key switch having four sets of changeover contacts on each side. This switch is wired so that when the key is in the central position the master loudspeaker is in the listen mode. If now S2 is operated then power is applied to the amplifier and the slave can talk to the master.

Should the master wish to call the slave then pushing the key one way the oscillator which provides the calling tone and the amplifier are both powered and the output is fed to the slave speaker.

Pushing the key the other way switches the slave to the listen position thus enabling the master station to speak. This arrangement of switching ensures that privacy is enjoyed by the slave station—the master can not easily listen in, though, if desired, by mounting S2 at the master end one can control all functions from the one position.

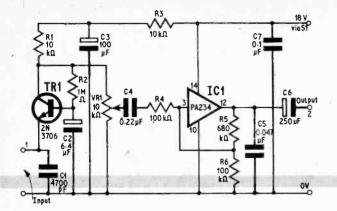
The wiring of the switch is shown in Fig. 7.



INTERCOM

Practical Electronics Oc

October 1972



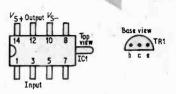


Fig. 1. Circuit diagram of the main amplifier

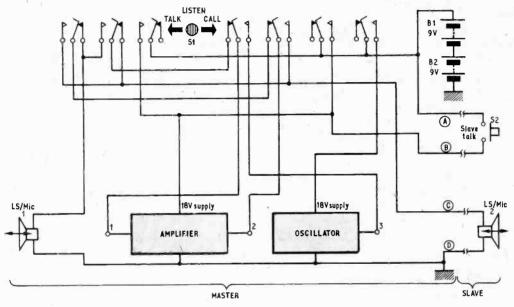


Fig. 3. Diagram showing the switching arrangement for a simple master/slave laystem. Only four wires connect the master to the slave (labelled A, B, C, D). Switch S2 and loudspeaker LS/MIC2 are in the slave

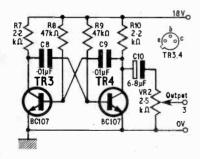
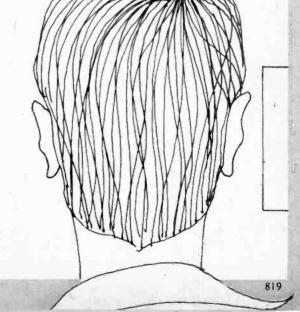


Fig. 2. Circuit diagram of the call oscillator

By R. A. PENFOLD



COMPONENTS ...

AMPLIFIER BOARD

Resistors

R1 10kO

R2 $1M\Omega$

R3 10kΩ R4 100kΩ

 $680k\Omega$ R5

R6 100kΩ

All ±10%, &W carbon

Potentiometer

VR1 $10k\Omega$ log.

Capacitors

C1 4,700pF

C2 6.4μF 25V elect. C3 100μF 25V elect. C4 0.22μF

C5 0.047µF

C6 250μF 30V elect. C7 0·1μF

Semiconductors

TR1 2N3706

IC1 PA234 (General Electric)

Speakers

LS/MIC1, LS/MIC2 22Ω 3in (2 off)

Switches

S1 Miniature lever Keyswitch, 4 pole changeover in each position

S2 Push on, release off push button

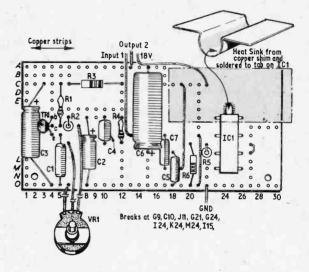


Fig. 4. Layout of the components on the amplifier board. The copper heatsink is carefully soldered to the i.c. tab

COMPONENT ASSEMBLY

The components are mounted on 0-lin pitch Veroboard as shown in Fig. 4 and Fig. 5, and special care is needed to ensure that no solder bridges are formed between adjacent strips. No real trouble should be encountered in the construction providing the diagrams showing the layout are followed carefully and that all breaks are made.

When soldering the i.c. in position do not leave the iron in place for too long. The i.c. needs a heat sink of at least I sq in and this can be made from an offcut of phosphor bronze draught strip though any copper or tin sheet will do. This heat sink, which should be bent so that it does not touch other components, is soldered directly onto the tab attached to the i.c.—take great care not to bend this tab too much or else it will break off and render the i.c. useless.

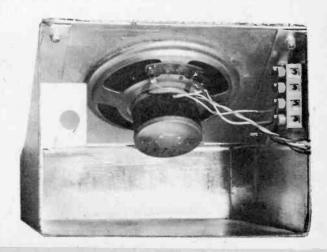
CASE CONSTRUCTION

The case for the master station was made from 20 gauge aluminium sheet. Fig. 6 gives the various details of sizes and cuts to be made.

A number of home constructors are put off making their own cases by the thought that it is too difficult and that the finished job will look "home made". Provided that the aluminium is marked out accurately and carefully before any cuts or bends are made no difficulty should be encountered.

When all the various bits have been cut out an Abra-file can be used to cut the hole for the loudspeaker and key switch. The exact size of these will depend on the actual components obtained. The holes for fixing the key switch should be drilled at the same time.

The inside of the master box is seen here with the components removed from their positions. brackets which hold the potentiometer and the call oscillator board can be seen fixed to the inside



COMPONENTS . . .

connecting wire

Breaks at 810, C10, D11, E12, F11, **OSCILLATOR BOARD** B Acopper strips Resistors R7 2.2kΩ C10 R8 $47k\Omega$ 0 0 R9 $47k\Omega$ 0 0 R10 $2.2k\Omega$ All $\pm 10\%$, $\frac{1}{4}W$ carbon 0 R10 0 0 Potentiometer R9 VR2 2.5kΩ miniature skeleton preset o o Capacitors C8 0.01μF C9 0.01μF 10 0 11 0 C10 6.8 F 35V elect. 12 o 13 **Transistors** TR3, TR4 BC107 or similar 14 15 Miscellaneous 16 B1, B2 9V battery (2 off) 0:1in matrix Veroboard (see text for sizes) 17 0 Aluminium for cases Terminal block, copper for heatsink, four way

Fig. 5. Layout of the components on the call

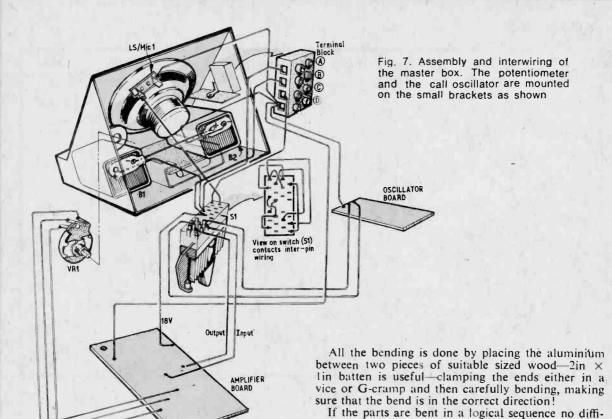
N.B. Oscillator and VR1 Brackets bonded to Sides of Case

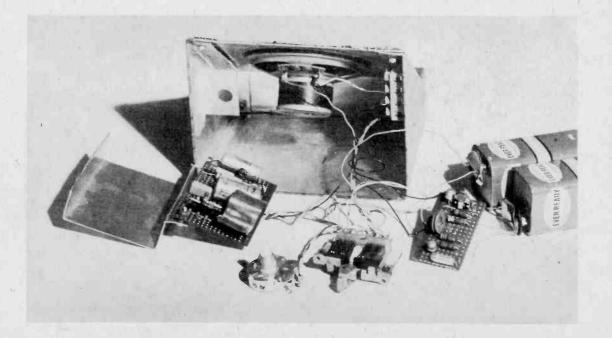
oscillator board

Fig. 6. Construction of the case for the master. 20 s.w.g. alluminium should be used and cut and bent to the sizes shown

Nellete made to suit 153 and 36 in respectively

Signature 17 in 164 in 164





culty will be encountered with the overlaps. When both pieces are completed offer them up together and hold in place whilst you drill suitable holes for holding them together; self tapping screws or pop rivets are ideal. Then cover the sloping front with speaker cloth and the rest with Fablon or similar.

ASSEMBLY OF THE UNIT

When fitting the switch it is necessary to wire it

up first and then fit it in position.

Any offcuts left can be used to make the bracket for VR1 which is glued in position using Evostick or Araldite. Other pieces can be used to make the circuit board support. The terminal block is also glued to the inside of the case on the opposite side to VR1 as shown in Fig. 7.

The case for the slave station can be purchased, adapted from an available tin or constructed from aluminium. It should be covered in the same way

as the master station.

The amplifier circuit board should then be

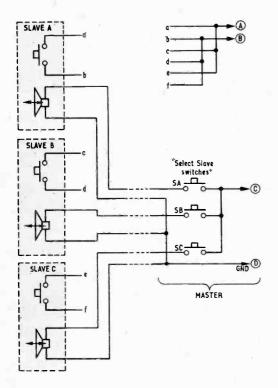


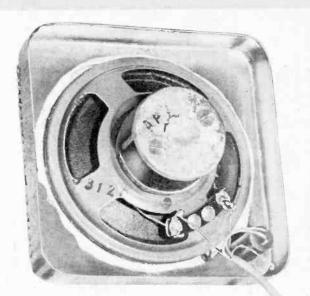
Fig. 8. Switching arrangement to give multiple slave operation, though none of the slaves has a call facility. The "select slave" switches are push buttons mounted on the master box

mounted on the bracket shown using insulating washers to ensure that the Veroboard strip is not shorted. The call oscillator can be mounted on its bracket which is then glued to the inside of the case behind the terminal block; to aid adjustment it helps if the preset on this board is easily accessible.

TESTING THE FINISHED UNIT

Before commencing testing ensure that all components are in the correct position, that their values and polarities are as in the diagram and also that you have made all the breaks. Trace all wires to see that they do go to the right terminals and most important that no solder bridges are present.

When you are completely satisfied connect the external speaker and plug the batteries in. It helps

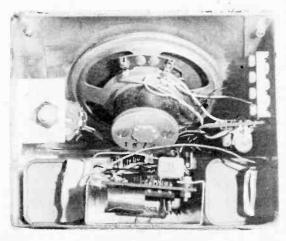


The internal construction of the slave showing the speaker and the push button in place

if a working transistor radio is placed near the slave station, when the switch is pushed one way you should hear the radio—adjust VRI to give the best results. If testing is carried out with the stations too close together, feedback will occur giving an almighty how!

Should you have no helper available you can short the two terminals taking power to the slave button at the master terminal block, this will be the same as pressing the "talk" button at the slave. Should there be a lot of distortion occurring when the slave talk button is pressed and the only cure is to reduce the volume you can try decoupling the two power lines going to the slave with a capacitor—say 50/F—connected across the appropriate terminals at the station end. When the lever key is pushed towards "call" the tone should sound in the slave speaker. The volume and quality can be adjusted to some extent by altering the value of the preset on the oscillator board.

continued on page 839



Completed master unit



GRAVITATIONAL WAVES

Some time ago details of an experiment to detect gravitational waves by radio was described. This experiment, which was originally suggested by Dr John Jelley, made some stir when the results were reported in *Nature*. There were two series of the experiments but the results were negative. There were certain difficulties mainly due to the high level of noise on the frequency of operation.

The original paper on gravitational waves was put forward by Joseph Weber in 1969. He claimed at that time that he detected these waves as coming from the centre of

the Galaxy. The possibility of these waves was predicted by Einstein in 1916 but nothing much was attempted in the way of investigation. The principle which underlies the theory is that gravitational waves are a form of radiation which affects mass. Small displacements of mass are caused by the radiation setting up a definite vibration. If they, are in line with the radiation the masses do not move with respect to each

Professor Weber's experiment was made with two huge aluminium cylinders deep down in the earth. Though Weber is satisfied that his results are positive, and indicate quite definitely that these waves come from the galactic centre, not all the scientific community accepts this.

SOURCE CONFIRMED

It is, therefore quite a move forward when independent experimenters confirm the source of the waves. Three physicists from Israel have published some work on their experiments and it seems to be a big step forward in this field. They are using the earth itself as the detector. Its great mass is much more sensitive than arrays of discs or cylinders.

If these waves are in fact coming from a specific point in the galaxy, then using the earth as a detector, all those points in line with the waves would vibrate the earth. Since the earth revolves on its axis this particular point on the earth would show a peak of activity twice in a sidereal day.

This effect will occur every 11hr 58min and has been detected by Dr Sadeh of Tel Aviv and Dr A. Ben-Menahem of the Weizmann Institute. They have set up a seis-mometer in the fairly noise free area on the Gulf of Agaba.

The team set out to discover if pulsars were the cause of the gravistars and revolve very rapidly. Since it is unlikely that they are completely homogeneous, there will be angular moments which will show as a variation of the gravitational effect. In other words there will be a certain frequency of change which could be detected.

FIRST EVIDENCE

The first evidence that this was right thinking came in 1971. The Israeli physicists found that there was a peak in the recording which corresponded to a periodicity of 0.53-0.60 seconds. Moreover, as each day passed the event came a little earlier in time. This was a clear indication that the origin of this event was outside the earth.

The twice a day response con-

firmed that the position of the source was at a celestial longitude of Right Ascension 11hr 33min. This position corresponded to the pulsar known as CP 1133.

As a check on this the team have examined the radio period of the pulsar and find that their events are in agreement. According to the present model of the pulsar, the radio pulses occur once with each revolution of the star. Gravity waves however would be emitted twice every revolution. Measure-ments confirmed that the seismometer events did occur at twice the rate of the radio pulses from CP 1133. The actual period of the gravitational waves is 0.594 seconds.

It would seem that there is a chance for confirmation of Weber's untiring efforts in this field. Certainly the benefits to astrophysics will be very great.

EARLY LINK-UP

It would seem possible that the planned space link-up exercises between America and Russia will be undertaken earlier than was pre-viously expected. While the main

exercise remains set for 1975 between a Soyus and Apollo vehicle, it is possible that a Salyut orbital station might be used.

The problems that have to be solved are many. Not the least of these is that of communications. The languages are different, the mode of procedures between the crews and ground will have to be rationalised to name two aspects.

There is also the problem of the airlock system. The Apollo atmosphere is nearly pure oxygen, at a pressure of 5lbs per square inch, while the Russians use a mixture of nitrogen and oxygen at the normal atmospheric pressure of sea level.

LUNA-20

Some new evidence about the lunar rock formation has been brought back by Luna-20, the automatic probe sent by the USSR to collect samples from the Moon.

The samples came from the highland area between the Mare Crisium and the Mare Fecunditatis. The soil in this region is much lighter and contains fragments of minerals and crystalline rocks. It is rich in aluminium, calcium and magnesium oxide and the surfaces are well preserved. The iron and titanium content is less than that brought back from the actual maria by Luna-16.

Altogether some 70 elements have been detected in the lunar soil by Soviet scientists. They are particularly interested in the nature of the lunar iron.

It seems that the lunar iron is even more rust proof than the meteoritic iron, and attempts are being made to simulate lunar conditions on earth with the possible benefits to industry. Already some success has resulted from the sublimation of iron from basalts which have been heated to a high temperature in a vacuum.

MYSTERY MOON

There are some rather puzzling features about Titan, Saturn's largest moon. Theoretically the gases should have boiled off, since this body has a low escape velocity.

The present low density atmosphere of molecular hydrogen and methane, from which the gases must be escaping quite rapidly into space, must have come into being long after the solar system was formed. This means that there must be a constant replenishing probably by evaporation and gassing from the solid surface.

Measurements made by L. Tafton of the McDonald Observatory suggest that there is some other major constituent in the atmosphere. It also seems probable that methane is present in the solid as well as in the gaseous state.



A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

This is YOUR page and any idea published will be awarded payment according to its merits.

TTL EQUIVALENCE GATE

Γ	A	8	output
same	0	0	0
different	1	0	
different	0	1	0
same	T		0

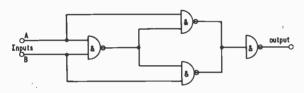


Fig. 1. TTL equivalence gate and truth table

HAVE built and tested an equivalence gate for use in TTL circuitry, see Fig. 1. It uses one inexpensive integrated circuit package, type SN7400, a quadruple 2-input NAND gate.

If the inputs A, B are the same, the output goes low ("0" in positive logic). If the inputs are different the output goes high ("1" in positive logic), see truth table in Fig. 1.

S. L. Thompson, Rainham.

VARIABLE ATTACK AND DECAY

Any audio circuit which produces a simulation of an instrument has not only to copy the frequency and waveform produced by the instrument but also has to emulate the general shape of the envelope, because the sound produced from any instrument, when it is played, does not immediately attain full volume but is a gradual build up. It also dies away slowly afterwards. It is in this respect that most simple electronic devices are inaccurate, as they produce an envelope with virtually no rise or decay time.

The circuit shown in Fig. 1 will produce a note with a rise and decay time variable between two limits. With the values given the note produced is

approximately 830Hz,

The first stage TR1 and TR2 are in the normal multivibrator configuration and the waveform which should be obtained from point A is shown in Fig. 2. Transistor TR3 is an overdriven amplifier to produce a good square wave and Fig. 3 shows the waveform that should be obtained at the output, point B. Transistor TR4 acts as an attenuator and is controlled by C3, VR1 and VR2 connected to its base.

The output from the circuit is taken from TR4 collector (R_L) , and if a resistive load is used its value should be $5.6 \mathrm{k}\Omega$, but other loads can be used to give different tones. An inductive load gives a sawtooth waveform and has a peculiar metallic tone. Other loads, such as capacitive, could be tried.

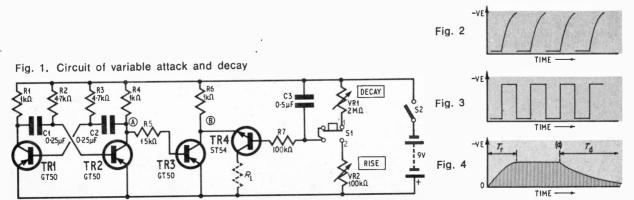
The envelope produced is shown in Fig. 4; t_r is the rise time, which will occur if S1 is pressed at time 0. Potentiometer VR2 gives a rise time variable between 0-50 milliseconds. The decay time $t_{\rm d}$ is controlled by VR1 and starts at point (a) in Fig. 4 and can be varied between 0-200 milliseconds.

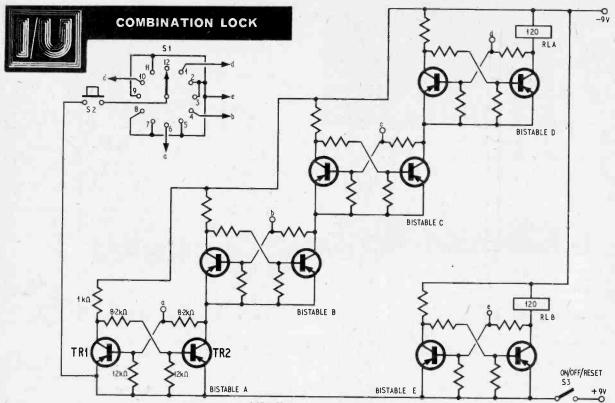
The output should be attenuated before (if desired)

it is amplified as it is in the region of 7V.

Switch \$1 should be of the push-on, release-off type with position 1 normally closed and position 2 normally open. The switch should be the break-before-make type because if the rise and decay time were both set at 0, the battery could be shorted out.

N. R. Adams, Colehill, Dorset.





BISTABLES B,C, D&E. COMPONENTS AS A

"HE circuit shown above is a 4-digit combination lock, against which the chances of finding the correct sequence of operation is 1 in 19,958,400, which is about 0.000 000 05, making it quite hard to pick!

Fundamentally, it consists of a four stage binary computer, the fifth stage being the alarm flip-flop which is only activated when the wrong digits are dialled. Each flip-flop, when switched, provides the power supply for the proceeding flip-flop and so on up the chain until the relay is activated, and thus driving the lock mechanism.

The flip-flops of the computer are simple bistables, i.e. it has two stable states. When one transistor is conducting the other one is not. The non-conducting transistor is made to conduct by applying a pulse to the base of conducting transistor.

In the combination lock this is accomplished by shorting the base of the first transistor of each stage to the positive line. When the power supply to a flip-flop is switched on, one transistor will always conduct first. This must be the first in each stage (due to inequalities in the circuit).

Operation of the combination lock is quite simple. The first number is dialled in this case number 6, and the pushbutton switch S2 is pressed momentarily switching on bistable A. The second number is dialled and the procedure is repeated. This procedure is repeated with the last two numbers till the lock is operated.

Resetting of the bistable is accomplished by disconnecting the power supply and then reconnecting

> G. E. Kaparnick. Swindon, Wilts.

Anyone who can supply the undermentioned communicate directly with the reader.

November 1968

Mr. E. J. Holt, Serenje Secondary School, P.O. Serenje, Central Province, Zambia.

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Mr. H. Anderson, Verites, Charterhouse, Godalming. **April 1972**

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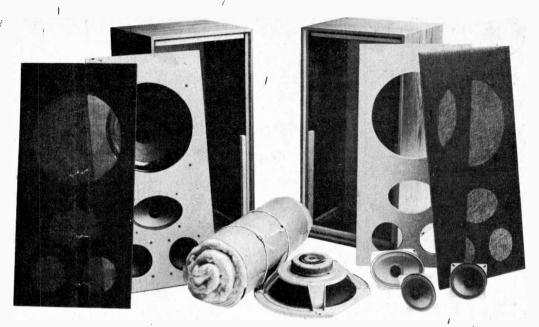
June, July, September 1970 and April 1971

Mr. S. T. Bartley, 41 Braemar Road, London, E13 8EH.

September, November 1970, February 1971, February 1972 Mr. C. P. Newton, Broadmead House, Broadmead Road, Send,

Woking, Surrey.

January, February 1969, January, April 1970, January 1972 Mr. M. B. Firth, Pine Cottage, Pontardulais Road, Gorseinon, Swansea, Glam.



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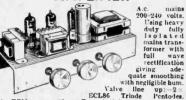


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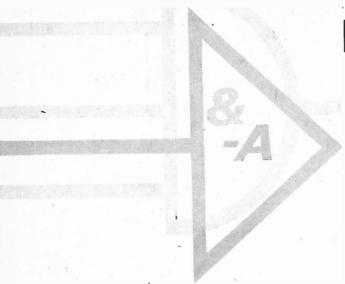
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Designing with

Integrated circuits

BY A.FOORD

A new series designed to help the experimenter to use I.C.s in practical applications. The circuits provided are not intended as definitive designs, but rather as a basis on which to experiment further.

1 The 741 as an ASTABLE

THERE are literally thousands of different integrated circuits on the market, and it would take every page of every issue of the magazine to make any impression in reviewing the complete field. Integrated circuits can be divided into two very broad categories, those intended for general applications and those designed with a specific function in mind.

The state of the art is such that many integrated circuits are so complex as to prohibit experimentation. Those for TV signal processing, for example, cannot adequately be used unless we are prepared to rewire a TV! Where appropriate such i.c.s usually appear in constructional articles.

In general research and development a selection of TTL and a few linear circuits allows much "routine" work to be achieved quickly. Manufacturers short form catalogues show where to go for "state-of-the-art" circuits if they become necessary.

Rather than extract up to the minute information from data sheets and application notes, we hope to show how the "standard" integrated circuits can be used in many cases. We will place the emphasis on designing circuits using integrated circuits and not necessarily on reviewing a different one each month. We feel that this is more useful for the reader who wishes to experiment because he will often be able to use the same integrated circuit more than once.

Readers requiring further details of individual i.c.s and their performance, are recommended to consult manufacturers' data sheets.

OPERATIONAL AMPLIFIERS

The first generation of linear integrated circuits were the μ A702 and 709 operational amplifiers and the 710

comparator. Both the 702 and 709 have their own disadvantages. The 702 has the limited input voltage range of +1.5V to -6V and can "latch up" if this is exceeded. It can however be used for many feedback applications from d.c. to 30MHz.

The 709 is an improvement on the 702's performance by providing a higher input impedance, a large input common mode range of ± 10 V and a high output swing. It has its own characteristics (cross-over distortion, for example) and is not short-circuit proof. It can be used for high performance applications from d.c. to 5MHz or so.

Both the 702 and 709 require several external components to provide frequency compensation so that they are stable under closed loop conditions, and do not become unstable when overall feedback is applied. This compensation can be chosen to obtain the best bandwidth for a given closed loop gain.

The first of the "second generation" of integrated circuits was the μ A741 which overcomes many of the disadvantages of the 702 and 709 series. It is very suitable for general work where a wide bandwidth and a fast slew rate are not required.

This month we introduce the 741C amplifier and will use it again later in the series. Although it is convenient for demonstration purposes its bandwidth restricts its use and the 702 or 709 circuits can be used, within their limitations, when we wish to work outside the frequency limit of the 741.

The 702, 709, 741 integrated circuits are available, under slightly different numbers, from many manufacturers. (Some guidance on these numbers can be seen in the table on the P.E. I.C. Identichart in this issue.)

THE 741C OPERATIONAL AMPLIFIER

The 741C is a high performance operational amplifier intended for a wide range of analogue applications from d.c. to 1MHz. Its high common mode range and absence of "latch up" make it ideal for a voltage follower.

It requires no external components for frequency compensation and is stable under closed loop conditions including unity gain and integrator applications. It is protected against an indefinite short circuit to ground or to either supply rail. The input offset voltage is typically 2mV and this may be nulled by a simple circuit.

Its connections are shown in the diagrams for the various package outlines. Typical parameters are shown in the Table 1.1. Versions without the "C" suffix have slightly improved parameters, such as working temperature range.

LOW FREQUENCY MULTIVIBRATOR

To start the series, let us look at the 741 wired in an astable multivibrator configuration. Although not necessarily the best application for the 741, it does illustrate how very simple the external circuitry of an i.c. can be to provide a useful application.

Fig. 1.1 shows a basic astable multivibrator suitable for generating a fixed frequency square wave for test purposes. It has a negative feedback loop from the output to the inverting input via R3 and a positive feedback loop from the output to the non-inverting input via R1 and R2. The circuit changes state regeneratively each time the two inputs are at the same potential.

If we assume that the circuit is operating and that the output has just switched to $+V_0$ (the positive saturated output level) then the voltage V_1 at the non-inverting input (marked +) will depend on R1 and R2. The voltage V_2 at the inverting input (marked -) will be rising exponentally towards $+V_0$ from an initial negative value.

Let constant
$$k = \frac{R_1}{R_1 + R_2}$$
 Initially $V_1 = + k V_0$
 $V_2 = - k V_0$

When V_2 reaches V_1 the amplifier will change state with the output switching to $-V_0$, V_1 switching to $-kV_0$, while V_2 now falls exponentally towards $-V_0$ from its initial value of $+kV_0$. When V_2 reaches V_1 (which is now $-kV_0$) the circuit changes state again and the cycle repeats.

Table 1.1: Typical Characteristics of the 741C

Table III. Typical Characteristi	cs of the 141C
Large signal open loop gain	100dB
Input resistance	1 Megohm
Differential input offset voltage	2mV
Differential input offset current	30n A
Input voltage range	±13V
Maximum output voltage swing	±13V
Common mode rejection ratio	90dB
Input bias current	200nA
Output resistance	75 ohms
Supply voltages	±15V
Slew rate at unity gain	0·5V/μs

GLOSSARY

ANALOGUE COMPUTING Computing system where continuous signals represent mechanical (or other) parameters.

COMMON MODE REJECTION RATIO

A common mode input is one applied to both inputs of an operational amplifier. In theory this should produce no output, since only the difference between the inputs is amplified. The CMRR is a measure of this rejection to a common input signal, and should be large.

COMPARATOR An amplifier designed for comparing two inputs and giving a 0 or 1 output. Usually the output is compatible with logic levels.

DIFFERENTIAL INPUT An input applied between two terminals, neither of which is at earth potential.

DIFFERENTIAL INPUT RATING The maximum differential input which may be applied between the two terminals.

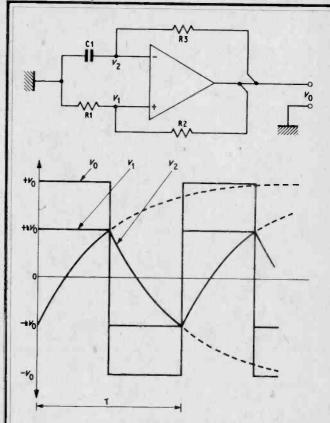


Fig. 1.1. The basic astable multivibrator using a 741

DIGITAL COMPUTING Computing system where two valued signals represent mechanical (or other) parameters.

FREQUENCY COMPENSATION The compensation required in feedback amplifiers to ensure stability and prevent unwanted oscillations.

INPUT COMMON MODE RANGE The maximum input which can be applied to either input without causing damage or abnormal operation.

INPUT OFFSET CURRENT The difference in input bias current requirements for the two inputs.

INPUT OFFSET VOLTAGE That voltage which must be applied between the input terminals to obtain a zero output voltage.

INTEGRATED CIRCUIT An electronic device containing several elements, active or passive, which perform all or part of a circuit function.

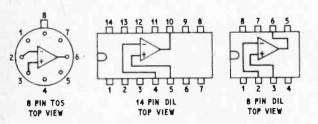
LATCH UP The switching of an electronic circuit to an unintended mode by improper voltage application.

OFFSET ERRORS Errors produced by input offset voltage and input offset current.

OPEN LOOP GAIN The gain of an amplifier before negative feedback is applied.

OPERATIONAL AMPLIFIER Originally a direct coupled high performance amplifier used in analogue computing to perform mathematical operations (summation, scaling, subtraction, integration, etc.). Today a low frequency packaged amplifier (about d.c. to 1MHz)

SLEW RATE The maximum rate of change of the output voltage for large signals. Usually in $V/\mu s$.



Basic connections (looking at top) of inputs and output for the 741. For details of other connections, see the I.C. Lead-out Identichart

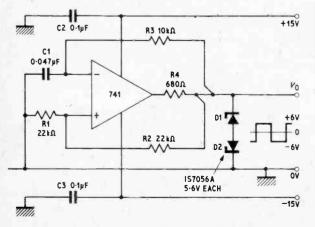


Fig. 1.2. A practical circuit for 1kHz operation

PERIOD OF OSCILLATION

If we assume that the inputs of the amplifier draw no current and that the positive and negative saturation levels are equal, then the period of oscillation is given by:

$$\tau = 2C_1R_3 \log_e \frac{(1+k)}{(1-k)}$$

For R₁ equal to R₂, this becomes $\tau = 2.2C_1R_2$ secs.

Although there is no need to do so, it is convenient to make R_3 equal to the parallel combination of R1 and R2 to minimise offset errors. The maximum allowable value for k depends on the differential input rating of the amplifier. For the 741, values for k of up to 0.9 are suitable. For a 709 with \pm 12V supplies a k of 0.2 would be used.

PRACTICAL CIRCUIT

A practical circuit for a nominal 1kHz operation is shown in Fig. 1.2. The Zener diodes clip the output level at \pm 6V to aid slew rate slightly. The measured frequency was 844Hz. This is 13 per cent lower than the nominal value, probably due to the 20 per cent tolerance of the capacitor.

Rise and fall times were 10µs, equivalent to a bandwidth of 35kHz. Although this is noticeable for a 1kHz square wave, it is still good enough for simple audio testing to illustrate the effects of tone controls, instability and ringing, or filters. For higher frequencies a 709 can be used with a value of 0·2 for k.

At frequencies lower than 1kHz, or if slightly longer rise and fall times can be tolerated, the Zener diodes may be removed and R4 shorted out, so that the circuit relies on the symmetrical limiting characteristics of the amplifier.

Part 2 Next month: Introduction to basic logic gates

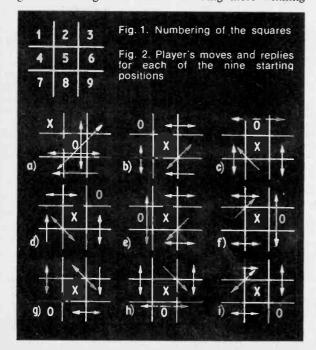


A novel entertainment for parties and fêtes

Noughts and crosses is a simple but fascinating game whose rules can be understood even by young children. Two players alternately place noughts and crosses in a three by three grid in an attempt to obtain a complete line of their own symbol either diagonally, horizontally or vertically.

With this machine the player is given the advantage of starting first and makes his play by using a pen to "write" a nought on to a colourful illuminated screen. The computer instantly replies by displaying a cross. Two anti-cheat devices are included to foil baffled players.

Most of the 945 different games that can be played against the computer will be drawn or lost, but in two per cent of the games the player can get three noughts in a line. Finding these winning



games is not easy and presents an interesting problem in logic for the player. Schoolchildren will play for hours trying to find one or more ways of beating the computer.

ANALYSIS OF THE GAME

The object of the game is to obtain a row (horizontally, vertically or diagonally) of three noughts, while preventing the computer from obtaining a row of three crosses.

In the usual game using pencil and paper the first player has a choice of nine places, his opponent then has a choice of eight places, and so on. Thus there are $9\times8\times7\times6\times5\times4\times3\times2\times1=362,880$ ways of filling the places. Though not all of these represent interesting games, the number is too large for a simple computer and so must be reduced.

This is done by allowing the player any choice of position, but limiting the machine to just one reply. The total is then $9 \times 1 \times 7 \times 1 \times 5 \times 1 \times 3 \times 1 = 945$ possible games, a number which allows simplified circuitry but still provides variety of play.

For further analysis of the game the squares are numbered 1 to 9 as in Fig. 1.

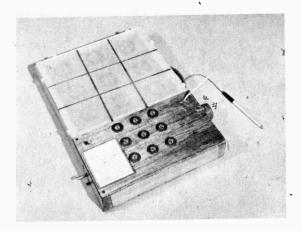
Square 5 is the most important because it controls four of the eight possible rows of three. Squares 1, 3, 7 and 9 each control three rows. Least important are squares 2, 4, 6 and 8 because each can only block two rows.

TACTICS OF THE MACHINE

The first basic principle of play is that if the player's first move is in one of squares 1, 2, 3, 4, 6, 7, 8 or 9, then the computer's best reply is square 5. If the player's first move is square 5, then the computer's reply should be either 1, 3, 7 or 9, but in practice it is made to be always square 1.

The player's first move determines the computer's reply for each successive move in that game. These moves and the corresponding replies are shown in Fig. 2(a) to (i).

Consider Fig. 2(a). The player has started with square 5 and the computer has replied with square 1.



The completed prototype showing the general appearance of the unit with the "how to play" notice in position

The double-headed arrows indicate reversible positions; for example if the player plays square 2 the computer answers with square 8 (to block the row), while if the player plays square 8, the computer replies with square 2 (to block the row).

This illustrates the second design principle: when the player fills in a second "0" in any line, the com-

puter should block the line with an "X".

It will be seen in Fig.2(a) that one of the arrows is single-headed indicating an irreversible play. If the player plays square 9 the reply is square 7, whereas if square 7 is played the reply is not square 9, but square 3.

This illustrates the third principle: if the player is just about to start a line of "0"s, the computer should reply with a second "X" in a line so as to

force the player on to the defensive.

If these three principles are followed in the usual pencil and paper game then the player cannot lose.

Possible moves and replies for the eight other starting positions can be followed by reference to Figs. 2(b) to (i).

INPUT UNIT

The player makes each move by touching the pen to one of nine lin diameter brass washers (corresponding to the nine squares). Each washer is connected to the gates of two thyristors (SCRs).

When a washer is touched, one of these thyristors switches on a lamp indicating the player's "0", and the other thyristor, by means of the memory store,

switches on the computer's reply "X".

Once on, the thyristors will stay on until the power supply is interrupted. Thus the use of thyristors has the important advantage that once a move is made, it cannot be changed either accidentally or deliberately. If toggle switches were used instead, players could cheat by flicking the switches to find the best move at each stage.

Fig. 3 shows the circuit diagram for these thyristors and Fig. 4 shows how they may be mounted on a piece of Veroboard. Eighteen 50 p.i.v. 1A SCRs were used in the prototype, but thyristors with other ratings may be used providing they are all of the

same type to ensure that the lamps light equally brightly.

Also needed for the input unit is the pen and a resistor which may be fitted inside the pen. The resistor should be the highest value that will give reliable triggering of the thyristors. A 150 ohm

W resistor was suitable in the prototype.

The pen is a plastic ballpoint of the kind that unscrews in the middle and has a retracting button at the top end. With the ink tube and button removed, flexible cable may be led in at the top hole, knotted, and soldered to the resistor which in turn is soldered to a thick wire which is then soldered or glued with "Araldite" epoxy resin, so as to protrude through the lower hole as in Fig. 5.

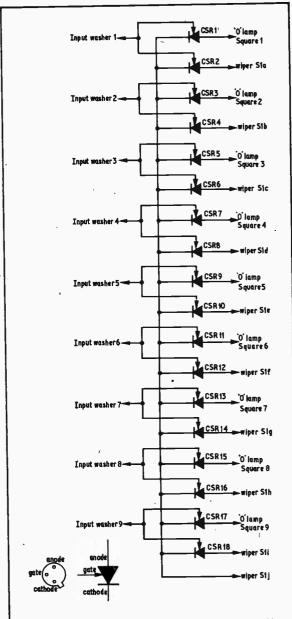


Fig. 3. Circuit diagram of the input unit. The thyristors can be any 50V, 1A type

COMPONENTS . . .

Resistor

R1 150 Ω ¹/₄W carbon (see text)

Thyristors

CSR1-CSR18 Any 50V 1A type (18 off)

Switches

S1 10 pole 10 way wafer switch (1 wafer must be a break-before-make type)

S2 Push-to-break push button switch

Lamps and holders

LP1-LP18 M.E.S. lamps and holders (for voltage ratings see text) (18 off)

Miscellaneous

1in dia. brass washers (9 off), ballpoint pen, large knob, mirror clips (6 off), two pieces of glass or Perspex, plywood or hardboard, 2in×1in softwood, red and green cellophane or cinemoid, tracing paper, Araldite (for details of these materials see text), $5in \times 1\frac{1}{4}in$ 0.15in matrix Veroboard

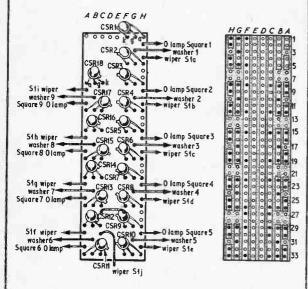


Fig. 4. Layout of the thyristors on the Veroboard panel

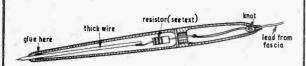
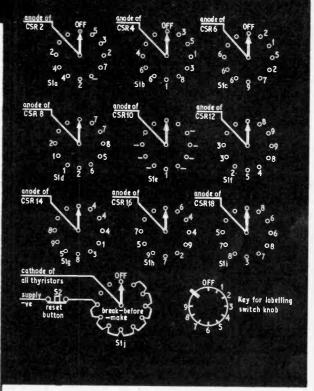


Fig. 5. Internal construction of the "pen"



MEMORY SWITCH

The memory switch consists of a 10 pole 10 way wafer switch. One way is used as an "off" position and the other nine positions of the switch are used to set the initial play number (i.e. select the required programme).

Nine of the wafers are used to route current to the correct lamps and the tenth wafer forms another anti-cheat device. This tenth wafer must be "break-before-make" type. This ensures that if a player tries to cheat by turning to a different programme part way through a game, the power supply to the thyristors is cut off momentarily and the display unit is wiped clean.

Fig. 6 shows the ten wafers. Wafers S1a to S1i must be wired together by reference to the numbers shown round each wafer in Fig. 6. All the contacts marked "1" must be wired together (for connection later to the "X" lamp in square 1 of the display unit). Similarly all the contacts marked "2" are wired together (for connection later to the "X" lamp in square 2 of the display unit), and so on. Great care should be taken at this stage to ensure correct wiring.

All except one of the contacts of wafer S1j are wired together, as shown in Fig. 6.

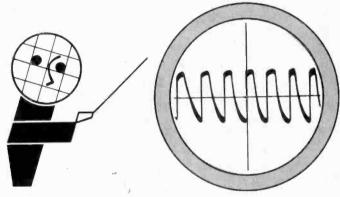
OUTPUT DISPLAY UNIT

This consists basically of 18 m.e.s. lamps in lampholders under a translucent screen. Nine lamps (green) are used to indicate the "0"s and the other nine (red) to indicate the "X"s using filters as described later.

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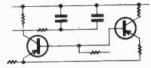
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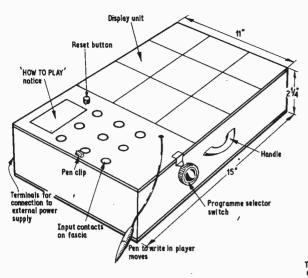


Fig. 7. General layout and dimensions of the complete unit (above)

Fig. 8. Construction of the cabinet and display unit (right)

Fig. 9. Arrangement of the "0" and "X" filters under the tracing paper (bottom right)

CONSTRUCTION OF CABINET AND DISPLAY UNIT

Fig. 7 shows the general layout. Fig. 8 shows the fascia and glass panels removed.

The dimensions are not critical except that the cabinet must be deep enough (at least 2½in) to take the wafer switch with all its wiring.

The lamp compartments should be as small as possible to give a bright display while ensuring that there is enough room to unscrew and replace lamps.

If a compartment is needed for HP2 cells (see "Power Supply" section below) then a maximum size of 11in × 15in overall may be used. If an external power supply is to be used then 8in × 15in will give a better, brighter display.

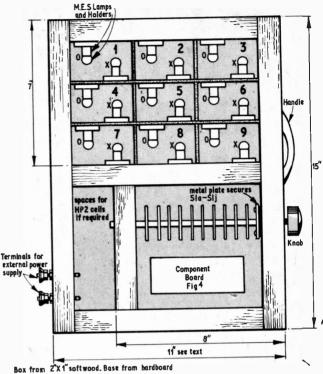
The cabinet may be made by glueing and pinning four pieces of $2in \times 1in$ softwood to each other and to a rectangular ($11in \times 15in$) hardboard base, see Fig 8.

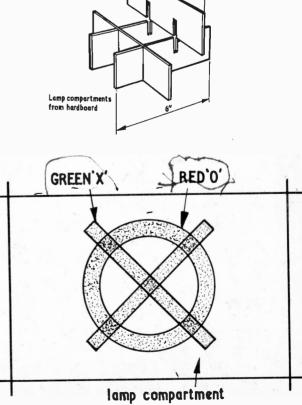
Four slotted partitions for the lamp compartments can be cut as shown, the m.e.s. lampholders screwed in position and the partitions slotted together and held in position by a 9in crosspiece.

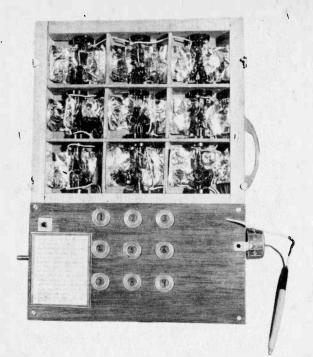
A metal plate, drilled to take the fixing bolt of the wafer switch can be screwed in position as shown. A short piece of softwood may be necessary to steady the end of the switch shaft if a battery compartment is required. Terminals or a power lead may be fitted for connection to an external power supply.

NOUGHTS AND CROSSES

The nine "0" lamps are each wrapped in one or more layers of green cellophane and the nine "X"







lamps are similarly wrapped in red cellophane or cinemoid. (Cellophane is obtainable from artists' supply shops and cinemoid, used in stage lighting, is obtainable from large electrical lighting shops.)

The lamp compartments are covered by two sheets of glass or Perspex which sandwich a sheet of tracing paper between them. Also sandwiched (under the tracing paper) are nine large red "0"s and nine large green "X"s cut out of cellophane, one of each over each lamp compartment (see Fig. 9). Thus when a green "0" lamp lights, it illuminates that square with green light except where the red "0" shape absorbs the green light and so appears as a black "0". Similarly when a red "X" lamp lights, a red square with a black "X" appears.

The cellophane or cinemoid should be chosen so that when a red and a green piece are overlapped and held to the light, it should appear as dark as possible without the individual colours being too dense for the lamps. In the prototype it was found that six layers of pale green cellophane and one layer of primary-red cinemoid were most suitable.

The brightness of the display is improved by fitting reflectors of aluminium kitchen foil behind the lamps, taking care not to cause a short circuit between the lampholder terminals.

The two sheets of glass may be held in place by mirror clips.

FASCIA PANEL

The fascia is cut from ¼in or ⅓in plywood or hardboard. Nine holes are drilled under the positions of the nine brass lin washers (see Fig. 7). Leads are soldered to the washers, passed through the holes and the washers are glued in position using "Araldite" epoxy resin. They should be numbered 1 to 9 as in Fig. 1.

The "push-to-break" reset switch is fixed to the fascia. A hole is also drilled for the lead to the pen. The wood may be finished with varnish or stain. A carrying handle, and a pen clip may be added.

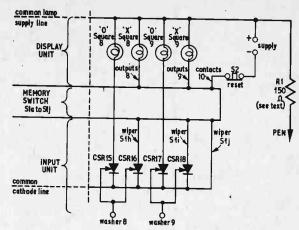


Fig. 10. Part of the complete circuit to show the method of interwiring the display, memory and input units

A large 12-faced plastic knob is needed for the wafer switch. The knob should be marked from 1 to 9 plus an "off" position corresponding to the switch positions shown in Fig. 6. A small metal pointer may be fixed to the fascia to facilitate reading the knob.

INTERWIRING OF THE UNITS

Fig. 10 shows part of the complete circuit.

One side of all the lamps is connected to the positive terminal using thick wire and a circuit similar to a ring main to keep the resistance to a minimum.

The pen lead is also connected to the positive terminal.

The negative terminal is connected through the reset switch to all the contacts on the tenth wafer, using thick wire.

The wiper of the tenth wafer is connected to the common cathode lines on the Veroboard (Fig. 4) again using thick wire.

The lead from washer 1 is connected to the gates of thyristors CSR1 and CSR2 (Fig. 4 and 10) and similarly with the leads from the other eight washers. Heat shunts should be used to protect the thyristors while soldering.

The anode of thyristor CSR2 is connected to the wiper of wafer S1a (see Figs. 4 and 10). The anodes of the eight other even numbered thyristors are similarly connected. If possible colour coded wire shoul be used here.

A lead from all the switch contacts marked 1 in Fig. 8 is connected to lamp 1 "X" (i.e. the red lamp in square 1). Similarly all the contacts marked 2 are wired to lamp 2 "X" and so on.

Finally each of the anodes of the "0" thyristors is wired to the corresponding green "0" lamp (Fig. 4).

POWER SUPPLY

This must be capable of lighting up to nine lamps in parallel, with least reduction in brightness.

Lead-acid accumulators or a tapping off a car battery or Nife alkaline cells give a bright display and can be re-charged.

Table 1: POWER SUPPLIES AND LAMPS

1	POWER SUPPLY	LAMPS
	1 lead-acid accumulator (2.2V)	1-25V, 0-25A
	2 lead-acid accumulators (4.4V)	0·3A
	3 lead-acid accumulators (6.6V)	5·5V, 0·3A or 6V, 0·3A
	2 NiFe cells (2·4V)	1.25V, 0.25A
	4 HP2 dry cells (2 pairs in parallel) (3V)	1.25V, 0.25A
	Mains driven d.c. power pack	bulb to suit voltage (allow 1 V drop across thyristors)

Table 2: "TRUTH TABLE" FOR CHECKING

SWITCH	٧	VAS	HE		PEN		D V	VIT	Н
	1	2	3	4	-5	6	7	8	9
1	5	3	2	7	wert;	8	4	6	8
2	3	5	1	7	-	9	4	4	6
3	2	1	- 5	8	-	9	4	4	6
4	7	3	2	5	_	8	1	9	8
5	_	8	7	6	1	4	3	2	7
6	2	1	9	2	_	5	8	7	3
7	4	6	6	1	-	2	5	9	8
8	4	6	6	1	_	3	9	- 5	7
9	2	4	6	2	_	3	8	7	5

Table 1 shows which lamps to use depending on the available power supply. If more powerful lamps are used, make sure that the thyristors can carry the necessary current.

If a power-pack is used, it must have a low internal resistance and be capable of delivering enough current for nine lamps.

High power U2 dry cells can be used, but have a limited life and the display will not be very bright.

TESTING

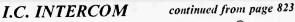
Table 2 shows the "truth table" for checking the computer's replies. For example with the switch set to position 1, if the pen is touched to washer 1 the green lamp in square 1 and the red lamp in square 5 should light. If the pen is then touched to washer 2, the green lamp in square 2 and the red lamp in square 3 should light. In this way the circuit should be carefully and methodically tested for each switch position, using the reset button where necessary.

METHOD OF PLAY

The player decides at the beginning of a game which position he will play initially and then moves the memory switch to indicate that position. This switch must be left in that position for the rest of the game. The player then uses the pen to write in his initial play and carries on with the rest of the game.

A notice suitable for fixing to the fascia near the reset button is shown in the photographs. The aim of the game should be given as "to get three noughts in a line".

It is left to the constructor to find the 18 winning games.



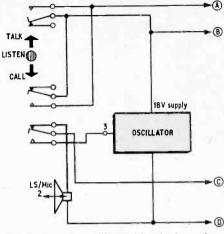


Fig. 9. A call oscillator identical to the one in the master can be used to give the slave a call facility. The switch is a miniature lever switch as used in the master. The letters to the right show how the modified slave is connected to the master

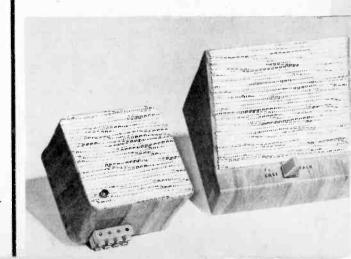
MODIFICATIONS TO THE BASIC SYSTEM

The basic system can easily be extended by connecting slaves in parallel. Fig. 8 shows a typical set up with three slaves none of which have call facilities to the master; in this case it is the master station which has to initiate any communication by pressing the relevant button. If it is wished to give the slave a call facility then Fig. 9 shows the arrangement and this can easily be wired in if the master/slave set up is sufficient.

If any of the configurations using two or more slaves are built then the cases may have to be redesigned. For example, if it is decided to build the master/two slaves with call facilities then the slaves will have to have a case large enough to accommodate the speaker, the call oscillator and the lever key whilst the master will need to be enlarged so that the multi-button switch and the indicator lights can be fitted.

Depending on what loudspeaker is finally used will dictate the method of fixing; the easiest is to glue them to the case making the hole a little smaller than the speaker.

The completed intercom





PART 2

POWER SUPPLY...

PRE-AMPLIFIER...

TREMOLO...

ELECTRONIC PIANO

By A. J. Boothman B.Sc.

To achieve a logical building sequence the order of construction presented will be the power supply unit, pre-amplifier and tremolo unit, main amplifier and pitch printed circuit boards. The mounting of the keyboard and other assembly details will round off the series.

To assist in lining up the p.c.b.s the power unit and amplifier are used as test gear, hence the order of construction.

POWER SUPPLY CIRCUIT

The circuit of the power supply is shown in Fig. 2.1 and is based on well established design principles. A transformer using the 20 volt secondary tap produces an open circuit voltage of approximately 30 volts across a large reservoir capacitor, and this reduces to about 26 volts at 2 amps. Two 6.8 volt Zener diodes connected in series act as the reference voltage with which a portion of the output voltage at the emitter of a ZT3055 is compared. Any error is amplified and fed to the output transistor, thus regulating the output voltage. Capacitor C4 produces a slow rise in output voltage at switch on, whilst C3 and R3 give high negative feedback of any ripple voltage which might be developed at at the output.

The output voltage range of the supply is 16-21 volts, controlled by VR1, and the maximum output

current is 2 amps. Worst case dissipation in the output transistor TR3 is 18W with 700mW in the driver transistor TR2. Two Zener diodes are used rather than one high voltage type in order to reduce the power requirement in one package. TR1 and each Zener diode have maximum power dissipation levels of approximately 75mW.

The earth connector allows the earth to the piano circuits to be disconnected in the event of any instabilities which might occur when the piano is connected to a self earthed external amplifier.

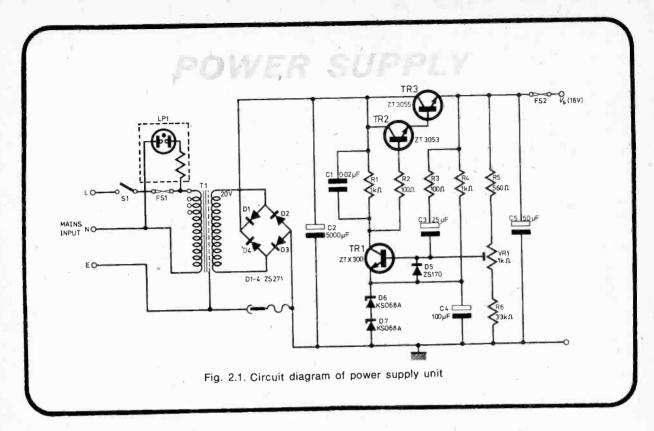
P.S.U. ASSEMBLY

The small components for the power supply unit are mounted on a simple printed circuit an etching and drilling pattern for which is given in Fig. 2.2.

With the p.c.b. completed and terminal pins inserted first the pre-set potentiometer is mounted, then the resistors, diodes, transistors, capacitors and finally the a.c. input terminal strip as in Fig. 2.3.

The two regulator transistors are mounted on a heatsink and the assembly completed using the transformer for mounting the board. The large capacitors, heatsink and transformer are mounted on a baseboard as seen in the photograph.

After assembly the power supply can be checked for correct operation by measurement of voltage at



a number of points. The voltage across the 5000 µF capacitor (two 2,500 µF capacitors, connected in parallel, were used in the prototype) on no load should be approximately 29 volts with a voltage on load of 25V at 1.5A. The emitter voltage of TR1 is 13 volts, with 18.5 volts at the collector for an output voltage of 17 volts.

The voltage on the slider of the preset potentiometer is 14 volts. This component should be of high quality as severe damage could be caused by a faulty condition. After experiencing some difficulties with cheap skeleton potentiometers the author decided to use a multi-turn linear track potentiometer which is probably at the other extreme on cost.

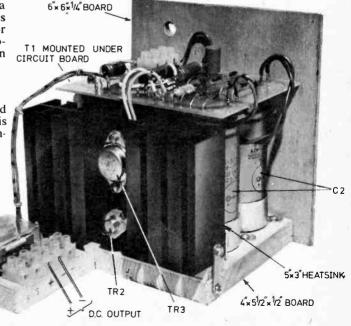
PRE-AMPLIFIER CIRCUIT

The pre-amplifier circuit is shown in Fig. 2.4 and consists of three stages. The input impedance is very low, and allows an unscreened signal interconnection between the pitch boards.

FS1/FS2

Perspective view of power supply module

It is essential that the amplifier should be able to handle a wide range of signals, since the peak level for one note is approximately 80mV peak-to-peak on maximum attack. The maximum input signal which can be presented at the input is approx. 2.6 volts peak-to-peak which represents 32 notes in the maximum attack position.



OWER SUPPLY BOARD

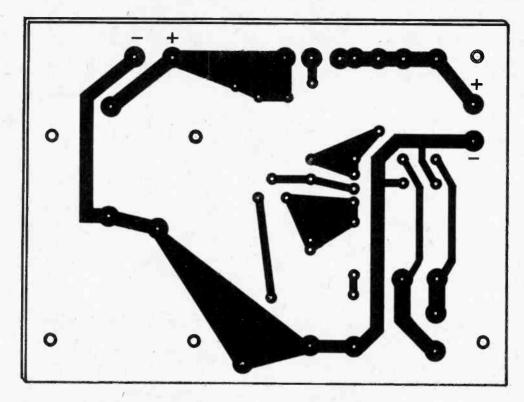


Fig. 2.2. Etching and drilling details for p.s.u. printed circuit board (full size)

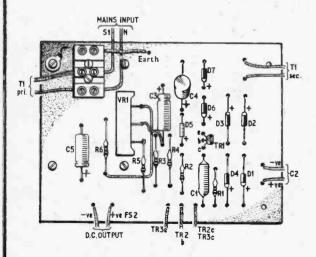


Fig. 2.3. Component assembly on p.s.u. printed circuit board

COMPONENTS . . .

POWER SUPPLY UNIT

Resistors

R1 $1k\Omega$ R4 $1k\Omega$ R2 100Ω R5 560Ω R3 100Ω R6 3.3kΩ All 5% 1W carbon

Potentiometer

 $VR1 1k\Omega$ preset

Capacitors

C1 $0.02\mu\text{F}$ polyester 125V C4 $100\mu\text{F}$ elect. 15V C2 5,000μF elect. 35V C5 50µF elect. 25V C3 25µF elect. 15V

Diodes

D1-D4 ZS271 (Ferranti) 4 off

ZS170 (Ferranti) D6-D7 K5068A (Ferranti) 6-8V 400mW Zener (2 off)

Transistors

D5

TR1 ZTX 300 Ferranti TR3 ZT 3055 Ferranti TR2 ZT 3053 Ferranti

Transformer

T1 Mains transformer, Douglas type MT3AT

Miscellaneous

FS1 - 200mA fuse, FS2 - 1.5A fuse, S1 - 1.Main toggle switch, heatsink, LP1 - Mains neon

The output from the first stage is fed via a resistor network to a compound emitter follower containing two transistors (TR5, TR6). The design of this portion of the circuit is determined by the condition required for the tremolo effect. The tremolo circuit, which is described later, acts as a shunt modulator by presenting a variable impedance across VR2, so giving a variable degree of attenuation of the signal between the first and second stages.

Output from the emitter follower is again at low impedance and the nominal attenuation (tremolo off)

for the second stage is a factor of two. Thus the overall voltage gain to the output of the emitter follower is approximately 1.5.

LEVEL CONTROL SETTINGS

The second stage is followed by the two level determining elements, the first being the foot soft pedal control, whilst the second is the keyboard level control. The latter item consists of a five position switch with fixed resistors giving stepped attenuation levels.

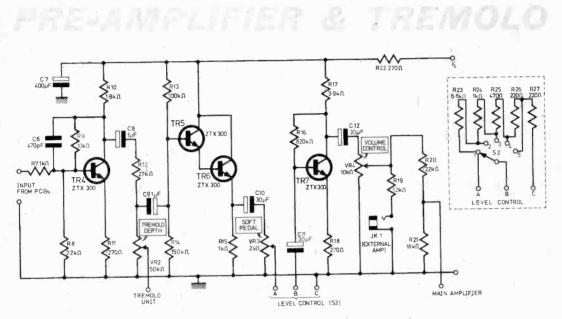


Fig. 2.4. Circuit diagram of pre-amplifier

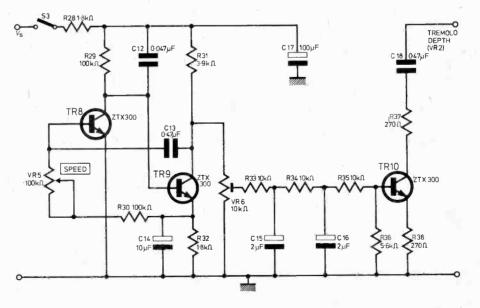


Fig. 2.5. Circuit diagram of tremolo unit, S3 is the keyboard on/off control switch

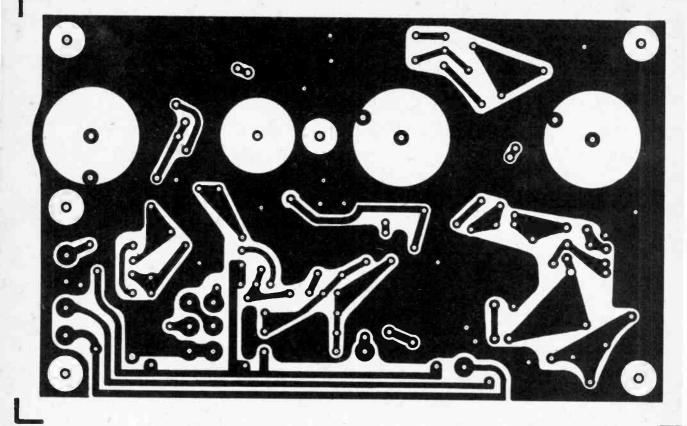


Fig. 2.6. Etching and drilling details for pre-amplifier and tremolo printed circuit board (full size). The white circles for JK1, VR2, VR4 and VR5 should be only $\frac{3}{6}$ in diameter

COMPONENTS . . .

PRE-AMPLIFIER		TREMOLO UNIT
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	/ off)	Resistors R28 1.8k Ω R34 10k Ω R29 100k Ω R35 10k Ω R30 100k Ω R36 5.6k Ω R31 3.9k Ω R37 270 Ω R32 1.8k Ω R38 270 Ω R33 10k Ω All resistors $\pm 5\% \frac{1}{3}$ W carbon Capacitors C12 0.047μF polyester 125V C13 0.47μF polyester 125V C14 10μF elect. 15V C15 2μF elect. 15V C16 2μF elect. 15V C17 100μF elect. 25V C18 0.47μF polyester 160V
Transistors TR4-TR7 ZTX300 (Ferra	anti) (4 off)	Transistors TR8-TR10 ZTX 300 (Ferranti) (3 off)
$\begin{array}{lll} \text{VR2} & 50 \text{k} \Omega \text{ carbon lin.} \\ \text{VR3} & 2 \text{k} \Omega \text{ carbon log.} \\ \text{VR4} & 10 \text{k} \Omega \text{ carbon log.} \\ \end{array}$		Potentiometers VR5 100k carbon lin. VR6 10k Ω preset
Miscellaneous S2—5-way single pole r JKI—Standard jack socke	otary switch	Switch S3—On/off switch

Normal setting is position 2 which gives the nominal output, on maximum master volume, for a five note input. Position 1 gives the nominal output when a single note is played and is only for special single note solo effects.

Positions 3, 4 and 5 give quick operation attenuated levels as required. In position 2 the attenuation between stages two and three is a factor of

five.

The single transistor third stage has a gain of approximately ten, and again has a high dynamic range, such that the maximum output swing capa-

bility is 8V peak-to-peak.

Overall pre-amplifier voltage gain with the level control in position 2 totals a factor of three, and is followed by a master volume control which feeds the external amplifier jack socket, and a fixed attenuation network prior to the main internal amplifier.

TREMOLO CIRCUIT

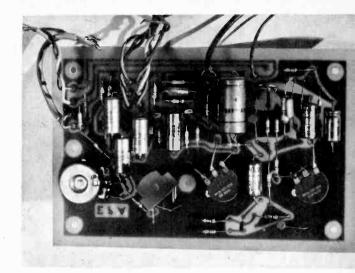
The tremolo circuit is shown in Fig. 2.5. and consists of a multivibrator (TR8, TR9) supplying a square wave output across a preset potentiometer in the range of 5-10Hz. The output from the preset feeds two low pass filters to give a ramp waveform at the base of TR10.

Preset adjustment ensures that the transistor operates from the off condition and provides maximum voltage change at the collector. In turn the degree of voltage swing is controlled by VR2 when

applied to the pre-amplifier.

PRE-AMPLIFIER AND TREMOLO ASSEMBLY

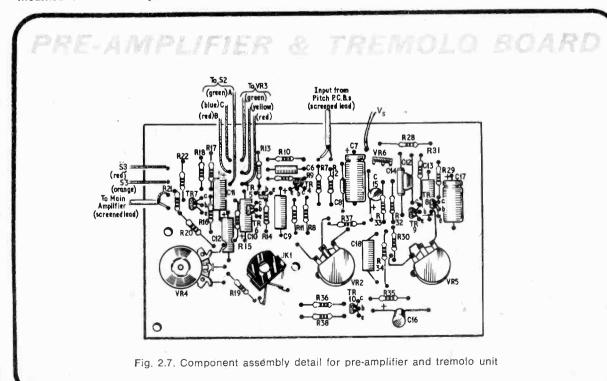
circuits are The pre-amplifier and tremolo mounted on the same printed circuit board, which



Photograph of the completed pre-amplifier and tremolo board

also acts as the panel to hold the external amplifier output socket, the master volume control, and the tremolo rate and depth controls.

Figs. 2.6 and 2.7 give details of the printed circuit board and component assembly. As before all holes should first be checked against the diagrams, and any missed holes should be drilled before proceeding. This may be particularly necessary in the case of the potentiometer peg location holes which will vary in position for different types and sizes of potentiometer.



Next the terminal pins should be fitted, followed by the potentiometers, jack socket, and preset potentiometer. Fit the resistors, transistors and capacitors in that order, and finally wire the potentiometers and output socket.

MAIN AMPLIFIER

The circuit of the main amplifier is shown in Fig. 2.8 and is based on the Sinclair integrated circuit type IC-12.

The amplifier is intended as a low power unit to drive the two small internal loudspeakers, or the headphones. Whilst the power is adequate for home use in a small or medium size room, an external amplifier is recommended for any serious use of the instrument outside the domestic circle.

The circuit within the package is fully explained in the Sinclair booklet which is supplied with the unit. If you should purchase a unit which includes the earlier simple two page leaflet the booklet can be obtained by writing to Sinclair Radionics Limited.

COMPONENT CHANGES

A printed circuit card is supplied with each unit and the photograph shows the assembled unit. Some of the component values have been changed from those suggested by Sinclair for the average application. The components affected are marked with an asterisk in Fig. 2.8 and the associated components list.

C19 $(0.5\mu F)$ has been chosen for the input coupling capacitor since, as explained later, the input impedance has been reduced such that bass response could suffer if this capacitor were 'not increased. C20 $(0.01 \mu F)$ has been used to provide a small amount of treble cut as a form of tone shaping on the internal amplifier setting. C25 (400 µF) prevents any possible instabilities due to the length of the supply lines.

MAXIMUM BASS

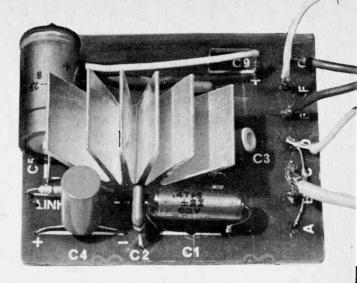
To provide maximum bass response a 1,000μF coupling capacitor (C27) is connected at the output. Due to the large size of this capacitor it has been removed from the p.c.b. as supplied by Sinclair. It will also be noted that the connection of this capacitor within the circuit has been removed from the ground side of the speakers and inserted on the live side. This prevents the possible shorting out of C27 to earth by the insertion of a jack plug into the headphone socket where the jack plug is connected to some other equipment which is earthed.

This rearrangement means, that is is necessary to connect a wire link across the connections intended for C27, thus making pin F an earth point.

The input impedance is reduced by the choice of R39 which minimises pick-up between the preamplifier board and main amplifier. R41 (470 Ω) is used to hold the amplifier gain at 60. This gives an input sensitivity of approximately 200mV peak-topeak for a 3 watt output into 6 ohms.

Sinclair Radionics state that it is very important that the i.e. only be used mounted on the printed circuit board which is supplied with it. Due to the very high gain of the device, the slightest coupling between output and input can cause trouble in the way of distortion and instability.

Next month: Pitch Board



Proprietary board assembly for the main amplifier

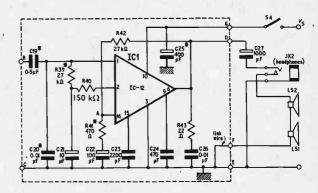


Fig. 2.8. Circuit diagram of main amplifier

COMPONENTS .

MAIN AMPLIFIER

Resistors

R39* 27k Ω

R40 150k Ω

R41* 470 Ω

 $\begin{array}{ccc} \text{R42} & 27 \text{k} \ \Omega \\ \text{R43} & 22 \ \Omega \end{array}$

All resistors ±5% ½W carbon

Capacitors

C19* 0.5µF polyester 125V

C20* 0.01µF polyester 125V

C21 10µF elect. 15V

C22 100μF elect. 15V

C23 2,200pF polyester 125V

C24 470pF polyester 125V

C25* 400µF elect. 25V

C26 0.01 µF polyester 125V

C27 1,000 µF elect. 15V

Integrated Circuit

-Super IC-12 with printed circuit board. (Sinclair Radionics Ltd.).

JK2—Jack socket to match headphones LS1-LS2 3 Ω elliptical loudspeakers 8in \times 2½in.

S4-On/off switch



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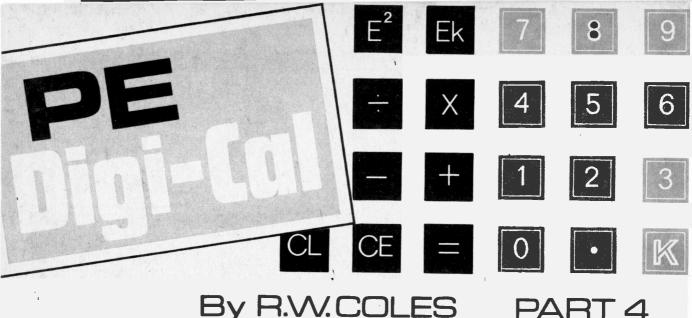
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KEYBOARD LOGIC AND HARDWARE

SATISFACTORY functioning of the keyboard is vital for correct calculator operation and to make things as easy as possible for the user, a great deal of thoughtful design has been carried out as regards key-top labels, keyboard layouts, the required function of each of the keys, and compensation for possible "finger-trouble"! The author's solutions to these problems are embodied in the Digi-Cal keyboard, but should any constructor wish to alter either the physical layout or the logic there is plenty of scope for modifications to produce a "custom" design.

KEYBOARD DEFINITION

The keyboard circuitry can be split up into a number of independent or interlocking sub-circuits, and each of these performs a different function, corresponding to one of the following list of keyboard requirements:

1. Convert figure key depressions into a four bit B.C.D. code and generate a single coincident clock pulse to enter the B.C.D. data into the (separate) entry register.

2. Convert arithmetic key depressions into a static two bit code suitable for use by the programme and arithmetic sections.

3. Record the number of decimal places in each figure entry and control the final alignment of the number so that it has the correct number of decimal places as entered on the thumb-wheel switch.

4. Produce a three bit code representing the number of decimal places to be displayed, dependent upon whether entries or answers are being read out.

5. Generate a single pulse to start the programme when the EQUALS key is pressed.

6. Switch on the overflow lamp when an OVER-FLOW input is received from the arithmetic section.

BLOCK DIAGRAM

The circuit of the keyboard panel can be subdivided into a number of relatively straightforward logic groups.

Fig. 4.1 shows these groups laid out in the form of a functional block diagram and it is best to understand the keyboard using this diagram before studying the full circuit in detail.

In the block diagram the circuit has been simplified as far as possible and the symbol consisting of a switch in a box with an arrowed input is used to represent gating functions which control the switched path, the arrow showing the input which has control.

ARITHMETIC KEYS

Starting at the top of the diagram, the four main arithmetic keys are fed to an encoding circuit which generates a unique binary code for each depression. This code is "staticised" in two latch flip-flops so that the code remains on the output wires until overridden by a future (different) arithmetic selection.

The E^2 key is in parallel with the "MULTIPLY" key since squaring is simply a modified multiplication sequence; a separate E^2 output is also produced to modify the programme.

The narrow START pulse required by the programme is generated by a monostable triggered by the EQUALS key, and this monostable is also used to start the second half of the multiply and divide sequences on command from the arithmetic section.

NUMERAL KEYS

The number keys are encoded to their B.C.D. equivalent in a diode matrix, the outputs of which are also staticised by four flip-flops so as to present a steady logic output during the clock pulse which enters the data into the entry register, the data in the latches remaining until either a different number key is pressed, or the EQUALS key is pressed in which

KEYBOARD LOGIC

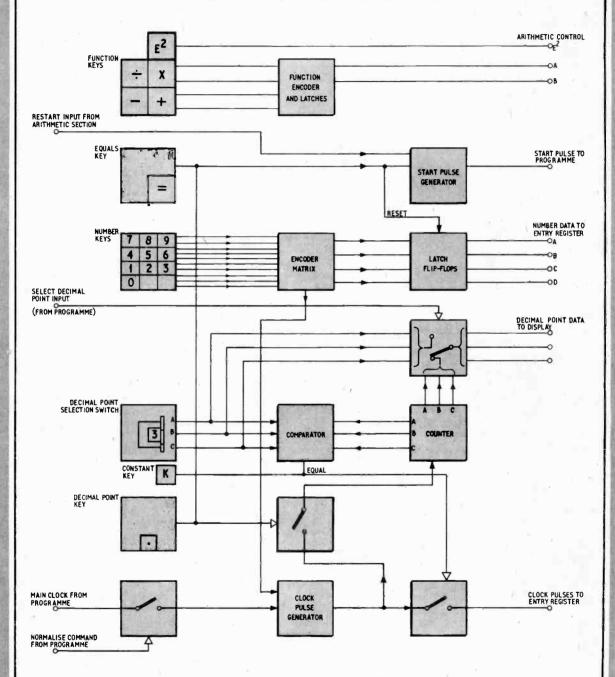
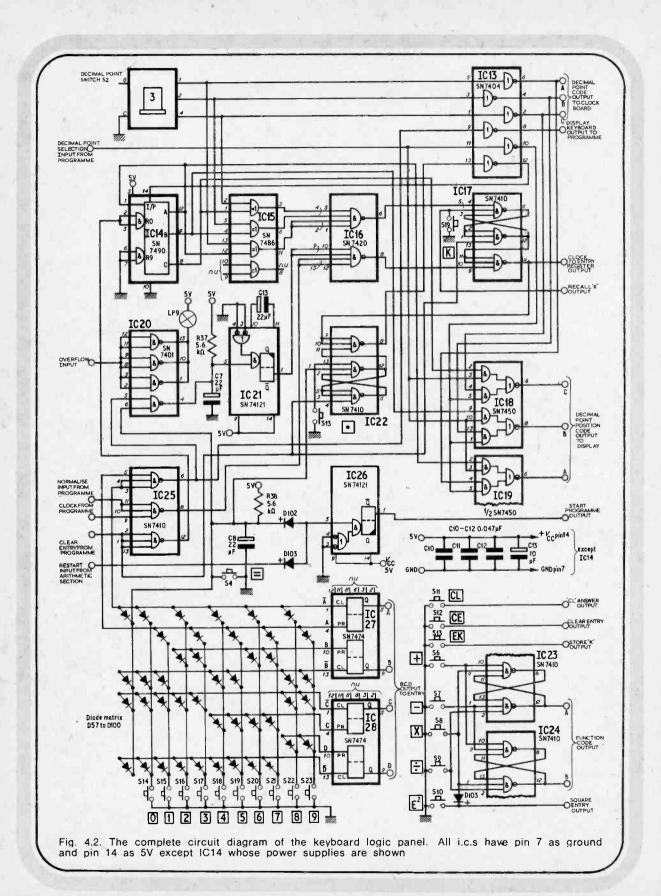
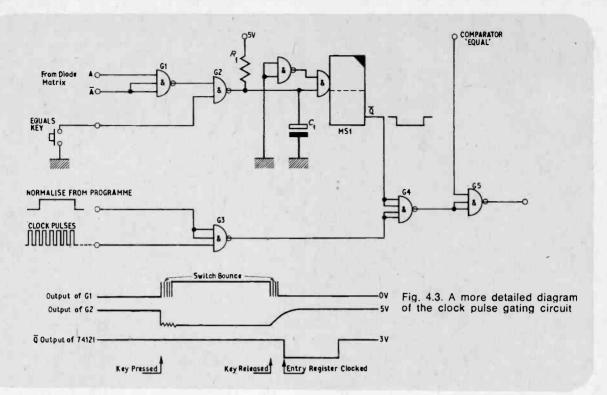


Fig. 4.1. Simplified block diagram of the keyboard logic. The symbol of a switch in a box with an arrowed input represents a group of logic gates, the arrow being the input which has control





case the latches are cleared. An output is also generated from the matrix whenever any key is pressed, and this signal is used to trigger the clock pulse generator, but more of this later.

DECIMAL POINT POSITIONING

If the decimal point key is pressed during an entry then a latch is set which in turn opens a gate to allow any subsequent clock pulses through to a counter. This counter counts the clock pulses after the point entry and gives an output which is compared with the setting of the decimal point thumbwheel in a comparator circuit.

When the correct number of decimal places have been entered the comparator registers the equality and shuts off the clock pulses from the clock pulse generator. It is this mechanism which prevents entry of too many decimal places in any figure entry.

If the number entered has too few decimal places then when the programme is started a NORMALISE command from the programme allows the main calculator clock pulses through to the clock generator in the keyboard, and the entry register data is rapidly shifted along until the comparator again registers equality then shuts off the clock.

This process ensures that all numbers can be entered without regard to the position of the point, normalisation being automatically carried out by the calculator itself.

OTHER FUNCTIONS

There are two additions to the clocking circuit to allow for special conditions. The EQUALS key is allowed to close the path connecting the clock pulses to the counter, this being done to cater for the occasions when only whole numbers are entered, the decimal point being unused.

Also, the RECALL CONSTANT (κ) key is allowed to shut off the clock path to the entry register so as to inhibit normalisation, this being necessary because the constant in store is correctly aligned to start with.

The three bit output of the thumbwheel switch is used to define decimal point position when the answer to a calculation is being displayed, and the three bit output of the counter is used to define it when an entry is being displayed. Switching between the two sources is carried out by a gating arrangement controlled primarily by the programme.

Any keys not shown on the simplified diagram have no associated logic circuitry and are passed out to the rest of Digi-Cal as switch closures to earth.

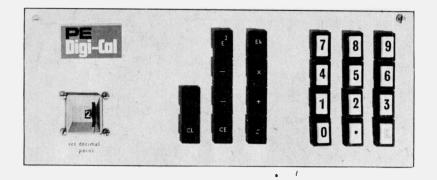
The full circuit of the keyboard is given in Fig. 4.2, and with the knowledge of its operation gained from the simplified diagram it should be possible to pick out the various logic groups previously discussed. One particular group may still be a little difficult to trace out, and that is the clock generation and gating.

To see this circuit in a clearer light it has been redrawn in Fig. 4.3 in an integrated way, and because this section is so important we can go through it step by step.

CLOCK CIRCUIT

The clocking is initiated by detecting any output from the diode matrix which is an indication of a key depression. Because the normally high A, B, C, and D outputs of the matrix will always have either their true or their complement output active (i.e. low) for any one of the ten relevant key depressions a detection circuit can be made by "ORing" together the true and complement version of any one of them.

In Fig. 4.3 G1 performs the detection by using the two "A" outputs from the matrix. The "logic 1"



The upper side of the keyboard showing the arrangement of the switches in the slots

output from G1 is applied to G2 which is an open collector gate with R_1 and C_1 in its collector circuit to give a slow "0" to "1" transition. The other input to G2 is an inhibiting input from the EQUALS key which prevents a clock pulse being generated by the latch reset when the EQUALS key is pressed.

The output of G1 is shown for a typical key depression and as you can see it carries with it a faithful (though inverted) representation of the switch bounce which is a feature of all mechanical s'witch operations, and which must be removed before the signal is used to trigger the monostable.

The output of G2 is "cleaned-up" by R₁ and C₁ to give the output pulse shown, and the slow transition after the key is released is used to activate the level sensitive trigger input of the SN74121. The fairly long negative going pulse from the monostable is "ORed" with the possible output of G3 and fed out to the entry register via G5 which is controlled by an inhibitory input from the COMPARATOR EQUAL latch. Gate G3 is used to control the main clock input used during the normalising cycle, being enabled by a long pulse from the programme.

DIODE MATRIX

The diode matrix used to encode the figure keys into their binary equivalent is so named because of its physical construction, the logic it performs being simply that of eight multi-input or gates, the number of inputs to each gate being set by the number of diodes connected to its output line.

In the circuit diagram the eight horizontal lines represent the gate outputs, the requisite inputs being made by the diode links to the eleven vertical lines

from the number keys and the reset line.

The matrix is built using the same technique as was employed for the display matrix (Part 3) with a small piece of Veroboard providing the vertical output lines to the latches and the key inputs being wired to the horizontal strips on the mother board.

Remember that it is necessary to make guide funnels on the blank side of the small piece of Veroboard to ease the location of the diodes prewired to the mother board, and most important, the cathode end of the diodes should be mounted next to the mother board.

The outputs from the matrix drive the PRESET and CLEAR inputs of the four latch bistables, which do not use their D inputs or CLOCK inputs in this application (IC27, IC28).

The use of SN7474 flip-flops in this position is a bit extravagant, since a couple of SN7400s cross coupled to form four latches would work just as

well and can be incorporated if desired, the more versatile SN7474s being used in the prototype toallow for possible future modification to enter data automatically from a source such as a tape reader.

FUNCTION CODER

Unlike the number coder and latches, the function coder and latches do not need a separate set of coding gates, the latches being built from SN7410 three input NAND gates, ICs 23 and 24, and the two inputs to each gate left after making the latch coupling are sufficient to provide the gating required to encode the arithmetic keys.

The E^2 key is coded in the same way as MULTIPLY and a diode D103 is used to facilitate this.

EQUALS KEY

Pressing the EQUALS key is the signal to start the selected arithmetic programme, and as may be expected, when it is pressed several things happen at once.

The earth appearing on the EQUALS line:

(a) resets the number latches via the matrix;

(b) inhibits the generation of a clock pulse which would normally result from the previous reset (see G2, Fig. 4.3);

(c) sets the decimal point latch IC22 to allow subsequent clock pulses through to the counter (this latch may have already been set by operation of the

DECIMAL POINT key during figure entry).

When the key is released and the earth disappears the resulting positive going signal on the line is "debounced" and used to trigger the START PROGRAMME monostable IC26 via a simple diode gate D101, D102. The output from the monostable is a very narrow pulse which is used to initiate the programme sequence. The diode gate is required so that the programme can also trigger the monostable to generate a "RESTART" pulse required in some arithmetic sequences.

DECIMAL POINT NORMALISATION

When the decimal point latch is set clock pulses are allowed through to the SN7490 decade counter IC14, which in effect counts the number of figures after the point in a number entry. The contents of this counter are continually compared with the decimal point switch output so as to detect a state of equality.

The thumbwheel switch output is already in a binary code though of an inverted form so that a logic "1" is represented by an earth connection and

COMPONENTS...

KEYBOARD PANEL

Resistors

R37, R38 5.6k Ω $\pm 10\%$ carbon

Integrated Circuits

IC13 SN7404 IC14 SN7490 IC15 SN7486 IC16 SN7420
IC15 SN7486 IC16 SN7420
IC16 SN7420
IC17 SN7410
IC18, IC19 SN7450 (or SN7451) (2 off)
IC20 SN7401
IC21 SN74121
IC22, 23, 24, 25 SN7410 (4 off)
IC26 SN74121
IC27, IC28 SN7474 (2 off)

Diodes

D57-D103 West Hyde type "red" (47 off)

Capacitors

C7, C9 $22\mu\text{F}$ 15V elect. (2 off) C8, C13 $10\mu\text{F}$ 15V elect. (2 off) C10, C11, C12 $0.047\mu\text{F}$ (3 off)

Switches

S2 Birch Stolec EB10N 1248 and a pair of end plates
S3-S23 On/off push button (Bulgin type MP22, white 12 off, black 9 off)

Lamp and holder

LP9 6V 40mA lamp and holder (Bulgin type D22)

Miscellaneous

9.5in×3.3in 0.1in matrix Veroboard

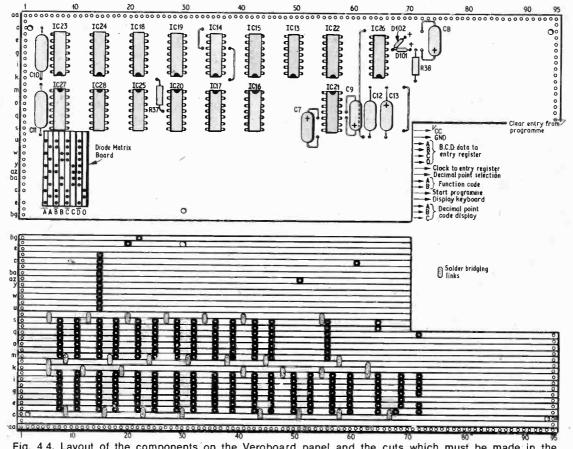
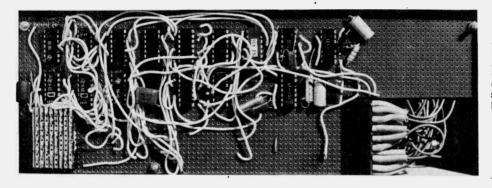


Fig. 4.4. Layout of the components on the Veroboard panel and the cuts which must be made in the copper strips. The links shown are for the power supply lines only and can either be made above or below the board. The black dots on the "diode matrix" board show the positions of the diodes which are arranged with the cathodes towards the main panel



A photograph of the keyboard logic panel in the prototype. The edge connector is an optional extra as wires can be soldered directly to the board

logic "0" by an open circuit. This suits our purpose admirably since the SN7486 used as a comparator, IC15, gives a "1" from each of its gates when its inputs are exactly opposite.

By comparing the true counter outputs with the complement switch outputs a comparator is formed which gives three "1" outputs when the count equals the switch setting. These three ones are used to enable a gate IC16, which in turn sets a latch, IC17, the output of which forms the input to G5 of Fig. 4.5 and serves to shut off the supply of clock pulses to the/entry register.

DISPLAY CONNECTIONS

The position of the decimal point in the display can be governed either by the contents of the counter, IC14, or by the thumbwheel switch setting depending on a command from the programme.

Switching between these two sources is carried out by the AND OR INVERT gates IC18 and IC19, but note that for this purpose the outputs from the thumb-wheel switch are inverted by IC13, to make them compatible with the counter outputs. The selected point data is fed to the display via a three line bus.

OVERFLOW INDICATION

If an OVERFLOW condition is detected during an arithmetic operation a "1" input on the OVERFLOW line drives three SN7401, IC20, gates in parallel to switch on the panel indicator bulb. The correct procedure is then to use the CLEAR key to erase all data and then re-enter the problem in a rescaled form. It is necessary to parallel connect three gates for this job because of the current requirements of the bulb.

PROGRAMME RESET

To return the keyboard to its correct state for a further calculation it is necessary to rest the DECIMAL POINT and EQUALS latches and the decimal point position counter. This is carried out by a CLEAR ENTRY command from the programme which, as its name implies, also clears the contents of the entry register.

CONSTRUCTION

The layout of the Veroboard panel is shown in Fig. 4.4, the panel itself being cut to size from a West Hyde type 122 board.

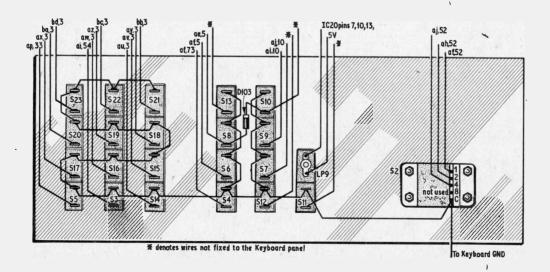


Fig. 4.5. The switches are wired as shown. All wires except those with an asterisk go to the panel shown in Fig. 4.4

The finished panel will be mounted upside down under the keyboard proper, affixed to the recessed wooden blocks either by means of wood screws, or, as in the prototype, by captive 6B.A. bolts cemented into the blocks with Araldite.

Needless to say, it is advisable to make all the board fixing arrangements before commencing the

wiring.

Wiring up is carried out as before with thin single core wire, using terminal pins where necessary to increase the wire handling capacity of a particular pad.

Off board wiring is achieved with thin flexible stranded wire left long enough that the board can be easily removed for access, but not too long that

stray pick-up could become a problem.

An edge connector was used to carry some of the off-board wiring in the prototype to help with development, this would not be necessary, or even advantageous to any significant extent with later versions, due to the very large number of interconnections required in all.

The switches are wired up as shown in Fig. 4.5.

TESTING

As with the display board last month it is advisable to wire up the keyboard logic a section at a time, testing each block before proceeding. In this way small mistakes can be easily discovered and dealt with before they become buried in several different circuit blocks.

Almost all the logic can be tested at the wiring stage without undue complication, outputs being monitored with a multimeter or by connecting them temporarily to the display board input if desired. If the latter course is chosen remember that the display board requires an inverted B.C.D. input, which while easily accommodating the decimal point outputs and function code outputs, will require temporary connection to the \overline{Q} rather than the Q outputs of the figure latches for correct display.

The clock pulse output is long enough to be detected on a meter which is an advantage for tests of this type, the EQUALS triggered START pulse is however far too short to be detected in this way but fortunately this part of the circuit is quite simple

and can be left unchecked at this stage.

Next month: Entry Register (constant store, entry register and multiplexer)

POINTS ARISING

SQUARE WAVE GENERATOR (Sept. 1972)

In the lower half of Fig. 6, the connections for the switch should read as follows reading from top to bottom:

(a) Top group is S1b numbered 1,2,3,W,4; (b) Bottom group is S1a numbered 4,3,2,1;

(c) S1b wiper should read S1a wiper.

NEWS BRIEFS

TECHNICAL INFORMATION SERVICE

NEW technical information service, aimed at giving A new technical antomaton as too, and firms, corporate bodies, instructors, students, and others engaged in educational work, advice on correct electrical installation practice according to I.E.E. "Regulations" has been established by the National Inspection Council for Electrical Installation Contracting.

The service is confined to technical matters and excludes advice on commercial or trading aspects, industrial or labour relations, and information relating to

manufacturers' products.

The aim is to promote a high standard of installation and maintenance safety of electrical wiring and appliances. The subscription fee is £3.50 per year to cover the services offered. Further information is available from the Council at Trafalgar Buildings, 1 Charing Cross Road, London SW1A 2DT.

NEW POCKET CALCULATOR

WHAT is claimed to be the world's smallest electronic calculator has just been announced by the British company Sinclair Radionics Ltd. At only just over $\frac{1}{2}$ in thick and $5\frac{1}{2}$ in \times 2 in this can really claim to be

a pocket sized calculator.

Known as the Sinclair Executive this calculator embodies many new techniques. Firstly the single MOS chip which forms the calculator consumes a mere 20 mW of power making it possible to run the whole machine from three mercury cells of the type used in hearing aids. This is made possible by switching off the i.c. completely between clock pulses relying on the capacitance of the MOS elements to store the information. Secondly the clock rate is reduced when the calculator is not performing a calculation so as to conserve power.

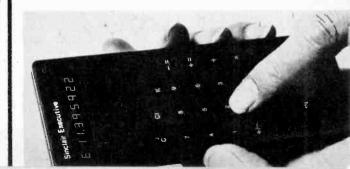
The battery voltage is just sufficient to drive the display thus eliminating the usual dropper resistors

which consume power.

The keyboard was specially developed for the calculator being only 4mm in depth. The contacts are gold plated and the keys are arranged so that it is virtually impossible to touch two at the same time.

The L.E.D. display has a capacity of eight digits. The calculator can perform all the usual arithmetic functions as well as automatic squaring, reciprocals and can operate in either fixed or floating decimal point mode. It also has a memory for calculations with a predetermined factor.

Although, at £79 this calculator is not the cheapest on the market, it must pose quite a threat to the present Japanese domination of the calculator field.



report from AUSTRALIA

BY J.M.WALDIE

In this report, the main theme will be the audio scene, which again should be of interest to intending

migrants and visitors.

Audiophiles here have a very large range of components from which to choose; it is likely that the range encountered in the average store will be greater than in a similar situation in the U.K. The possession of a respectable audio system, at least in the large cities, appears to be the rule rather than the exception, despite the "outdoor life" philosophy of the average Australian.

LOCAL PRODUCTS

The number of companies producing audio systems is relatively small. There are about six brands of Australian-made amplifiers (including Leak and Philips); only two very simple belt-driven turntables are produced here; I understand that there are only two locally produced reel-to-reel recorders and only one cassette system. There are, of course, several brands of "mid-Fi" modular grams and radiograms, including such brands as Kreisler (division of Philips); AWA (Amalgamated Wireless Australia), Thorn, Pye and HMV.

IMPORT TRADE

However, there is sufficient industry to warrant relatively high import surcharges—designed to protect local manufacturers (which, in some areas, are non-existant). Despite this, Japanese equipment dominates the retail trade, followed by British, German, Scandinavian and —to an increasing degree — American audio components.

For example, of the 30,000 reel-toreel mains-operated recorders and decks imported in 1970-71, 26,000 came from Japan. Some \$A 2 million worth (F.O.B. values) of amplifiers also arrived in the same period, of which well over half also came from Japan, and approximately one-quarter (in terms of value) from the U.K.

The British, however, have the lion's share of the turntable market: of the 200,000 units imported in the year ending June 1971, 176,000 came from the U.K. This is largely due to the practice of installing Garrard and BSR decks in mass-produced "unitaudio" systems.

There is a very wide range of loud-speakers—both imported and homegrown—available, and the Australian audiophile has a bewildering selection from which to choose. There are three locally-made brands of any consequence, and some very presentable designs have been issued. Japanese cabinets again dominate the imported systems. It is in this area that the Americans have been active, promoting the more expensive brands such as JBL, A.R., Marantz and Advent.

QUADRAPHONY

Largely due to the Japanese dominance in Australia in the audio field (Japan is one of Australia's largest customers for ore and coal; consequently the trade relations between the companies are maintained at a very close level), the current interest among audiophiles is the idea of 4-channel sound.

The battle between proponents for the CD-4 discrete system of quadraphonic disc reproduction (JVC/National/RCA) and the various matrix methods for obtaining more or less the same result (dominated by Sony's SQ system), is now in full swing.

Records produced by both methods are now available; the record manufacturers appear to be taking sides but showing apparent preference for the matrix method. It has been announced, for example, that EMI, with CBS, have opted for the Sony SQ system, but the decision to market SQ records will depend on demand. This demand will presumably originate from new owners of SQ equipment, but who would buy such equipment without a guaranteed source of quadraphonic records?

This chicken-and-egg situation is likely to delay still further the final decision. On the other side of the fence, aurally speaking, RCA have announced. in America, eventually all records issued by that particular stable will be "in discrete" quadraphony, a move that must be followed not only here but worldwide. And to confuse matters even more, according to local sources of information, A&M records are being matrixed to the Sansui QS method (not necessarily compatible with Sony's SQ) and two big German companies, Polydor and Deutsche Grammophon, are opting for a discrete system not necessarily similar to JVC/Nivico. Record manufacturers I spoke to locally all indicated that the outlook was in such confusion that nobody really knows what is happening next.

ORIENTAL CUSTOM

Australian audiophiles may have an extensive selection of audio equipment available but they don't grow on trees. For English equipment, the list retail price is likely to be double that in the U.K. For example, a Garrard Zero 100 deck has a list price here of \$A 269 (about £120) which compares with the U.K. list price of £54. On the other hand, the difference in price of Japanese equipment is very much less; a Sansui SD 5000 deck is listed here at \$A 756 (£345) which compares to £328 in the U.K.

This, of course, explains to some extent why Japanese equipment is so popular. However, we not only import oriental equipment but, to some extent, their methods of selling; it is usual to "haggle" over prices and the published list prices are something of a myth. Moreover, it is always possible to "trade-in" an article, which might not even be electrical.

COLOUR TELEVISION

It was recently announced that Australia will "go colour" in March 1975. The system to be adopted will be the 625-line PAL format and all four Sydney stations (1 national, 3 commercial) are in the process of preparing their studios and transmitting equipment.

The manufacturers, however, are treating the news with some trepidation; on the one hand, it could be regarded as a shot in the arm for the electronics industry, but a real concern is being expressed regarding imported receivers which, at the current import rates, could possibly be landed and sold at prices below those expected for locally-produced sets.

The matter will be discussed with the Tariff Board, who decide the magnitude of import duties applicable to any imports. And there are a number of critics who feel that, at an anticipated price of £500 for a 25in set, the sales to Australians, who for the most part regard television as a distraction rather than as a necessary part of life, may just not warrant the large initial outlay.

NEXT MONTH



A SURVEY OF THE COMMERCIAL SCENE

NORGANS

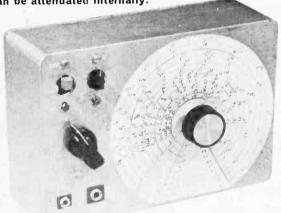
DEFFECTS UNITS # SYNTHESISERS

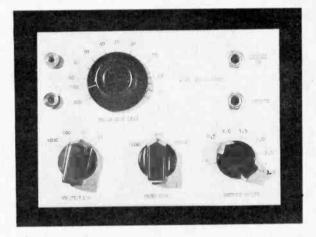
GUITARS

A.F. SIGNAL **GENERATOR**

For checking and measuring the characteristics of audio equipment, including frequency response, distortion, power output, signal to noise ratio, and dynamic range, one of the most important aids is an a.f. signal generator.

This instrument provides a sine wave output in the frequency range 19Hz to 200kHz in four bands. Square wave pulses from 19Hz to 20kHz are also available. Maximum output is just over 1V r.m.s. and can be attenuated internally.





SIMPLE C-R BRIDGE

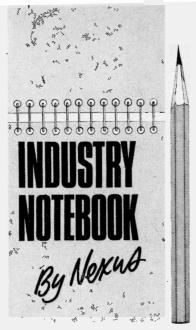
Ever had the frustration of finding a capacitor or resistor whose only fault is that the marked value is indecipherable? Now your problems can be over with this simple C-R Bridge.

Values of resistor or capacitors can be determined simply by turning a pointer until the signal from an audio generator is reduced to a minimum.

There is no meter so the unit is inexpensive and robust. The components are readily available and the instrument is easy to construct.

ACTICAL

NOVEMBER ISSUE ON SALE OCTOBER 13



VALUE ON THE BRIDGE

There was a bumper gathering of 300 delegates at the I.E.E. conference on Advances in Marine Navigational Aids. They came from all over the world to hear and discuss 55 papers.

It was a heady occasion embracing just about every navigation technique all the way from visual aids (the earliest known lighthouse was at Alexandria about 265 B.C.) to such twentieth century exotica as "System of location of balloons, ships or buoys by means of a low-orbiting satellite".

For the student of marine electronics the occasion was fascination itself. For the practical mariner, expected to foot the bill for equipment as well as understand and evaluate all the rival and complementary systems available, it was more like a nightmare.

The Chief Marine Superintendent of the B.P. Tanker Company Ltd., Mr R. Maybourn, put his finger on the shipowner's problem in his paper "Cost benefit and related factors—a shipowner's point of view". A navigation outfit for a modern tanker has an installed cost of almost £45,000 using fairly conventional equipment. Using some of the sophisticated systems described at the conference could result in a doubling of the cost with only dubious advantages.

EXOTIC IDEAS

Mr Maybourn criticised the electronics industry for developing expensive and exotic ideas without adequate reference to the shipowners, and which are not clearly related to adequately defined problems or needs. He suggested that we often seem to have the solution first and the problem becomes one of finding a need to which to match it

On computerised anti-collision systems, he wondered whether the problem had been adequately identified or even if the current problem is being solved. He referred to the computer as something which mesmerises the electronics engineer "itching to use its spare capacity in much the same way as an idle hand does a work study practitioner".

What Mr Maybourn asked of the industry was for far more reliability in existing equipment, and some element of standard design in equipment in regard to dimensions, methods of fitting and presentation of data which, he said, was chaotic and certainly would not be tolerated in the aircraft industry.

This point of view deserves some sympathy but should be examined in an historical perspective. Most of the exciting new concepts such as satellite navigation and the v.l.f. Omega system have their origin in military developments as, indeed, did marine radar and Decca Navigator before them. These last two items are now accepted as standard fit and comparatively inexpensive aids. What Mr Maybourn and the shipping industry are getting is the best of both worlds.

HIGH RELIABILITY

If the electronics industry demonstrated anything at all at the Conference it was that today's technology is available with high reliability and at a bargain price, while tomorrow's technology is being seriously considered and will be available in due course to merchant shipping at a fair price.

Timing is terribly important. The Marconi "Predictor" anti-collision radar system has been available for four years, yet less than a dozen have been sold. It was, and is, a brilliant example of electronic engineering and necessarily expensive. Decca Radar brought out a simple anti-collision radar with limited capability about the same time at about half the price and have sold some 700 equipments. It was what the shipowner wanted at a price he could afford. But the outlook for "Predictor" remains bright and Marconi still expect it to do well. It was only the timing that was seriously adrift.

TOUGH COMPETITION

On the other hand, you don't need to invent new technology to invent new systems. I was at the inauguration of the Southampton Harbour Radar system, said to be the finest in Europe if not in the whole world. I searched in vain for completely new technology in both the operations room and the equipment areas. Decca Radar, the prime contractors, hád done a wonderful systems engineering job

using off-the-shelf equipment freely available on the open market.

I was also at the unveiling of a new marine radar display concept introduced by Kelvin Hughes and reviewed at the Conference by marine consultant Captain J. P. Stewart. The system uses television techniques and is a notable advance, yet the only device in anv way unusual for a radar is a light-sensitive "image retaining panel". This panel has been commercially available for ten years but nobody had apparently thought of using it in a radar application until Kelvin Hughes originated the idea.

What is worrying the marine electronics industry is an unrealistic pricing policy. Competition is so severe that few companies are making sufficient money to support future civil (as distinct from naval) R and D at a reasonable level.

TXE2 TAKES TO THE ROAD

The Post Office is always fair game for the knockers and I have knocked away in my time with the best of 'em. SDS Components Ltd, the Portsmouth-based component distributors have gone one step further than knocking by abandoning postal delivery and employing Securicor to make all deliveries.

But the Post Office is not all that bad, although you might still think so when out driving and you get stuck behind one of the eighty or so 27ft long trailers now being built to house mobile electronic telephone exchanges. Each of these will house a Plessey TXE2 equipment and will be on the move to a site where 1,000 would-be telephone subscribers can stop biting their nails with frustration and get hooked into the network.

The Post Office already has 250 mobile exchanges of conventional types but these can only handle 400 lines each. The TXE2 electronic exchange in two trailers can handle 1,000 and a dual installation housed in three trailers will serve 2,000 subscribers.

Deliveries commence next Mav and the investment by the Post Office is £3 million. At least they are trying to keep pace with a demand that seems insatiable.

GOONHILLY 3

I was sorry to see that the 10th anniversary of the Post Office satellite station at Goonhilly Downs passed with so little notice. The occasion was marked by the inauguration of Goonhilly 3 making the station the busiest satellite terminal in Europe.

It seems more than ten years since we were all startled by Telstar 1 and Relay before Early Bird, the first of the Intelsat satellites, really got going with a full commercial service.

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ROAMER EIGHT

Mk. I

NOW WITH VARIABLE TONE CONTRÓL

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BUILDING COSTS 26.98 (OVERSEAS P. A. P. 4.1)

ROAMER SEVEN Mk. IV

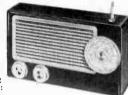
TUNABLE
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SW1, SW2, SW3
AND TRAWLER
BAND. Extra
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Luxembourg, etc. Built-in ferrite rod aerial for MW
and LW. Retractable 4 section 24in chrome plated
telescopic aerial for SW. Socket for car aerial. Powerful push-pull output. 7 transistors and 2 diodes,
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Volume/on/off, tuning and wave change controls.
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P.P. & INS. 41p.

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SIX



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TRAWLER
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TUNING OF LUXEMBOURG, ETC. Sensitive ferrite
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speaker. 8 stages—6 transistors and 2 diodes including
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POCKET FIVE



3 TUNABLE WAVE-BANDS: MW, LW, TRAWLER BAND WITH EXTENDED

WITH EXTENDED MW BAND FOR EASIER TUNING OF LUXEMBOURG, ETC. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving coil speaker. Attractive black and gold case. Size 5jin x 1in X 3jin. Easy build plans and parts price list 10p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

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BAND, 7 stage—5 transistors and 2 dioles, ferrite
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TRAW LE R
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BC108 BC109 BC169 BF194 BF274 BFY50 BSY25 BSY26 BSY27 BSY28 BSY29 BSY29	0.10 0.12 0.15 0.20 0.13 0.13 0.13	Power Transistors OC20 OC23 OC25 OC26 OC28 OC35 OC36 AD149 AUY10 25034	0.40 0.25 0.25 0.30 0.25 0.37 0.35
OC41 OC44 OC45 OC71 OC72 OC81 OC81 OC83 OC139 OC140	0-15 0-13 0-10 0-10 0-13 0-13 0-18 0-13	2N3055 Diodes. AAY42 OA95 OA79 OA81 OA95 IN914	0.40 0.10 0.07 0.07 0.07 0.07

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A CROSS HATCH GENERATOR FOR £3.50 111

YES, a complete kit of parts including Printed Circuit Board. A four position switch gives X-hatch, Dots, Vertical or Horizontal lines. Integrated Circuit design for easy construction and reliability. This is a project in the September edition of Practical Television.

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PATENTS BEVIEW...

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BP 1 267 194

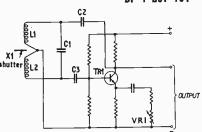


Fig. 1

British Patent 1 267 194 from Rotameter Manufacturing Co Ltd describes a simple but probably very effective circuit for sensing and registering very small physical movements of objects.

movements of objects.

The basic circuit is shown in Fig. 1 and relies on a Hartley oscillator with two magnetically coupled inductors L1, L2, a bridging capacitor C1 and d.c. blocking capacitors C2, C3. The variable resistor VR1 controls, along with the mutual inductance of inductors L1, L2, the amplitude of the circuit oscillations. The frequency of the oscillations depends upon the values chosen for the inductors L1, L2 and capacitor C1.

A small shutter X1, formed from non-magnetic but electrically conductive material (e.g. copper, brass, etc), is movable into and out of a small gap which is left between the magnetically coupled ends of the inductors L1, L2.

If the object whose movement is to be sensed is mechanically coupled to the shutter, then any movement, however slight, will cause a change in the amplitude of oscillation. This change may in some cases be reasonably linear

some cases be reasonably linear.
By amplifying TR1 output a direct dial readout can be obtained or, alternatively, the amplified output can be fed to a "pot coil" electromagnet arranged to apply a restoring force to the object which has moved. This restoring force will tend to move everything back to the original or null position, i.e. seek equilibrium in this state.

Component values are suggested which will detect and register a 0-025mm movement with a transistor output change of 200 millivolts.

ELECTRONIC SPEEDOMETER

In conventional electronic speedometers there is sometimes a problem in raising sufficient control voltage to not only display the speed, but also record the maximum speed obtained. Mechanical systems can introduce an inaccuracy of around 15 per cent which can be hopeless when the engine speeds are in the order of 10,000 r.p.m.

Porsche KG now claim (BP 1 254 486) a form of electronic speedometer which should be free from such problems. In Fig. 1 Porsche show how pulses derived from the ignition coil (at a frequency directly proportional to the engine speed) are shaped, integrated by the filter circuit and fed via the servo amplifier to a reversible servo motor. This motor drives the speedometer pointer through gearing to provide a direct readout indication of speed.

The car battery voltage is fed to the stabiliser to give a stabilised output voltage which is fed to the shaper and is also tapped by the servo motor to provide a feedback voltage to the servo amplifier. The servo motor also drives a maximum speed indicator through a ratchet which can be released for zeroing by a spring loaded button.

If it is thought wise, and safe, to provide an automatic switch-off for the engine, e.g., to avoid stripping the car gears, the speed voltage signal at the filter can be compared by the critical speed circuit with a predetermined limiting value to operate an ignition interrupter switch.

Instead of sensing pulses derived from the ignition coil, an

independent inductor associated with the engine shaft can be used to produce the necessary pulses.

PATENT ACTIVITY IN THE OPTICAL FIBRE FIELD

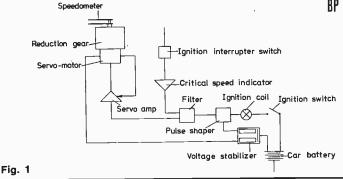
At least two different uses for light fibres in motor cars have now been patented by Joseph Lucas (Industries) Ltd.

In the first patent, published a few months ago (BP 1258395) Lucas described and claimed as novel the use of a light fibre with one end set in the door frame and the other behind a dashboard warning indicator. The door itself carries a mirror which is arranged so that light is reflected from a lamp into the doorframe end of the fibre only when the door is closed. Light thus emerges from the other end of the fibre to illuminate the dashboard indicator when the door is safe.

In their more recent patent (BP 1 264 325) Lucas claim as novel, the use of fibres extending variously from all the crucial car driving lights (headlights, sidelights, etc.) to various dashboard instruments. Thus any unlit instrument on the dashboard is a failsafe signal of an extinguished driving light.

The above patents are only reported briefly, because they are technically simple. But in view of recent published correspondence on this topic they may be interesting references for anyone working in the field. Incidentally, it should be borne in mind that although the patents have only recently been published, they were applied for several years ago.

BP 1 254 486



MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

FIRE ALARM KIT

The new fire regulations require all properties which provide overnight accommodation for more than a six people to be fitted with an acceptable fire alarm system. To meet this need Ramick Security Services have developed a new "Fire Alarm Kit" complete with instruction and wiring diagram to enable the handyman or an electrician to install a system for the smaller size hotel or boarding house.

The kit costs £30 complete and comprises a Control Unit; Heatswitch; Preswitch; Testswitch and a 12V d.c. 4in gong alarm bell.

The control unit operates from the mains a.c. supply but the voltage to the sensors is only 12V d.c. A battery is incorporated in the unit together with an automatic change-over circuit so that in the event of a mains failure the installation remains operative and changes back to a.c. supply when reconnected.

Whenever the alarm bell rings it

Whenever the alarm bell rings it continues until the control unit is reset manually. The control unit is contained in a pressed steel case, suitable for wall mounting, and has a mains indicator light and an on/off switch on the front panel.

The Heatswitch is a bi-metallic switch with a combined rate of rise and fixed temperature automatic fire detector to B.S. 3116. The contacts close when the temperature reaches 135°F (57°C) or if there

is an unusally rapid increase in temperature. The unit can be mounted in any position and provides coverage of approximately 500 square feet per heatswitch.

The Preswitch is a push button unit with a cast aluminium front plate and can be supplied for surface mounting or flush mounting Breaking the glass front operates the button which activates the alarm.

The Testswitch has a manually biased push button and indicator light complete with housing and is designed for fitting at the end of the twin wire circuit connecting the sensors to the control unit. When the switch is operated the indicator light is energised (and remains energised until the control unit is reset) and the control circuit, external wiring and alarm bell is checked.

Further details can be obtained from Ramick Security Services, The Lodge, Randalls Road, Leatherhead, Surrey.

PRINTED CIRCUIT BOARDS

Sometime ago we mentioned a versatile printed circuit board called Nippiboard marketed by NIP Electronics.

Although these boards have proved very successful, from the response of users they seem to suffer from two limitations. These limitations are that the boards are not pre-drilled and, more important, do not take integrated circuits.

Now, NIP Electronics have introduced a new range of boards called "NIP-E-Boards." These boards are available pre-drilled and are suitable for transistor circuits, integrated circuit designs or a combination of both.

The integrated circuit range of boards were designed in order to cater for the vast expansion of component manufacture in standar-dised DIL packages, such as relays, readout devices, as well as integrated circuits and transistor arrays.

All boards are made from s.r.b.p. or glass fibre and are available predrilled or undrilled according to choice. The designs of the boards are such that they will all accept edge connectors; a range of card handles, stand-off mounting pillars, and edge connectors is also available.

Further details and prices of the NIP-E-System can be obtained from NIP Electronics, P.O. Box 11, St. Albans, Herts.

POCKET METER

Readers should find the TS-60R Multimeter from West Hyde Developments an excellent purchase.

This pocket multimeter makes no pretentions to be up to professional standard but still covers most ranges needed for checking out the majority of circuits published in this magazine.

The meter movement is a $1000\Omega/V$ type and the ranges covered are: a.c. voltages 0-15V, 0-150V, 0-1000V; d.c. voltages 0-15V, 0-150V, 0-1000V; d.c. current lmA, 150mA; resistance $100k\Omega$. A feature of the meter is the "printed circuit" rotary switch.

The meter costs only £2 and in the event of a meter breakdown it is probably cheaper to throw it away and buy a replacement, where as with the more expensive counterpart it would cost more to repair than the purchase price of the TS-60R.

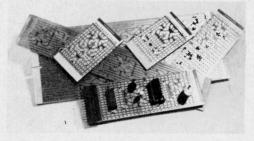
Further details of the TS-60R multimeter can be obtained from West Hyde Dèvelopments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middlesex.

Whilst on meters, a comprehensive range of Avometer spare parts is always held in stock by Instrument Services and they are able to offer a rapid Avometer repair and recalibration service.

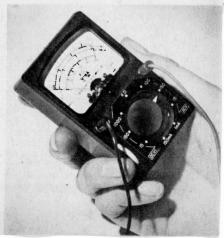
Complete refurbishing to "as new" is claimed to take approximately seven days. The company also offers a similar service to users of G.E.C. "Selectest" and "Minitest" instruments.

Further information of the meter repair service can be obtained from Instrument Services Company (London) Ltd., 208 Maybank Road, London E18.





(above) NIP-E-Boards from NIP Electronics (left) Ramick Fire Alarm Kit (right) TS-60R Multimeter from West Hyde



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REGULOTTE— A SELECTION FROM OUR POSTBAG

Correspondents wishing to have a reply must enclose a stamped addressed envelope. We regret we are unable to guarantee a reply on matters not relating to articles published in the magazine. Technical queries cannot be dealt with on the telephone.

Strong objection

Sir—I object strongly to the article Digi-Cal. Whilst I can understand people building their own electric organ or colour TV, I am sure nobody with any sense will build this machine at £110. These calculators can be purchased from about £60. Further to this, the cost of a simple counter with Nixie tube readout is approx. £5 per unit, i.e. with a six digit readout this section is approx. £30. Careful design should therefore give a complete calculator for £60. Still not worth making.

As a "Practical" magazine the very least I would expect is for articles to be practical propositions.

G. A. Bobker, Unsworth, Bury, Lancs. far too involved to be explained to "mere amateurs".

It does seem to be true that calculators are going the way of medium-wave transistor pocket radios, where the vast quantities which can be sold reduce prices to a level where amateur designs are difficult to justify on economic grounds, and to those readers who want a cheap calculator to use immediately without knowing what makes it tick, I can thoroughly recommend the new ready made machines available from retailers at low cost.

For those of us who also want to know what's ooing on inside, I hope Digi-Cal will help. After all, now that single-chip organs, f.m. tuners, and even computers are with us, it may be our last chance.

—R. W. Coles.

I' am sorry to hear that Mr Bobker objects so strongly to the Digi-Cal series, and though in the light of the latest developments in the field of m.o.s. technology I can sympathise with his comments on price differential, his letter does point to one very important advantage of these current articles.

The logic operations involved in any calculator are necessarily com-plex, and the new "single-chip" are valuable simply devices because the complex logic has been "wired-up" entirely by the i.c. manufacturer. Mr Bobker's concept of a calculator made from SN7490's and Nixies shows, I am afraid, a lamentable grasp of the way machines of this type operate, and since he himself is active in the circuit design field he could learn a tremendous amount about logic in general and calculating circuits in particular by following the Digi-Cal series. I am sure many readers will be glad of the chance to delve into this interesting and relevant field of electronics before the rapid march of technology reduces us all to mindless "wirer-uppers" of a circuit which can be built in half an hour but which is

What is the point?

Sir — Over the years 1 have successfully constructed many of the circuits published in P.E. The amount of enjoyment derived from assembling these projects has been twofold. Firstly, the satisfaction of building something with one's hands and seeing it working and secondly, knowing you have saved quite a bit doing it.

Therefore when you announced the P.E. Digi-Cal, which is the sort of project right up my street, I could hardly wait for the August issue to get cracking. Imagine my dismay at seeing the total cost as being approx. £110 when one can buy a ready built article to the same specification for £43·25.

Even if your design had cost the same I would have built it for the satisfaction to be obtained, but I cannot see anyone wanting to construct Digi-Cal with such a price difference. So really, what is the point of publishing a design like that.

This is my only criticism so far of an otherwise excellent magazine which I have taken since it first came out.

Brian Harrison, Settle, Yorks.

Beyond reason

Sir—I have been reading PRACTICAL ELECTRONICS since its inception in November 1964 and on average consider about 50 per cent of the constructional projects of interest to me (not that that figure relates to the quantity constructed!). But aren't we getting a little above ourselves with the introduction of a project to build an electronic calculator?

Now I am not one to decry the technical capabilities of your readers (quite the opposite) but what astounds me is the cost. Your author quotes a bulk component cost £110 yet one can buy an equally sophisticated machine (with all the trimmings like leading zero suppression, floating DP, constant key, etc.) for £56 and no extras like replacing over-soldered transistors or mis-wired ic's!

My point, to which I laboriously come, is what is the function of the constructional feature? I think it should be a medium through which constructors can promulgate their brainchildren so that readers can build a piece of equipment which is impossible to buy either because it is prohibitively expensive or because no manufacturer's specification matches that of the constructors. The intrinsic pleasure of building is enhanced when one notices that there are still pennies in the pocket.

Come on P.E. Continue to disseminate the superb features that you do but let us keep our exuberant competition with the pros within the bounds of reason.

J. E. Barrett, London, S.W.6

We recognise and understand the bewilderment caused to some readers because of the relatively high cost of building the P.E. Digi-Cal. This very creditable project provides a dramatic illustration of the far-reaching effects of rapid and stupendous advances in technology. See Editorial Comment, page 817.

Advance information

Sir—Could you please inform me if it is possible to purchase a full copy of PRACTICAL ELECTRONICS,

TION FROM OUR POSTBAG

Digi-Cal drawings and layout diagrams in advance, so that our apprentices may build as a project this very interesting and useful unit.

. We would also like to know if it is possible to extend the readout to ten digits without more complex

circuitry.

The advance purchase of the drawings, etc. will in no way effect our desire for obtaining further copies of Practical Electronics every month. As the Instructor in this Apprentice School I advocate all our electrical apprentices to get this magazine as it is so useful to them. For myself I have every copy since November 1964 having read ninety per cent of their contents (in-cluding—"Pleased to meet you") and all these have been bound into books year by year.

> G. Bolsover, Apprentice School, Perkins Engines Co., Peterborough.

This is not an uncommon request, but we must explain that it is just not possible to supply either individuals or organisations with full details of constructional projects prior to publication in the magazine. The division of the text for all major projects is carefully planned and the various parts of such articles presented in the most logical sequence to permit the construction work to proceed steadily, month by month.

Regarding your second point, e existing design cannot be the existing design cannot be readily modified to accommodate the extra i.c.'s and other com-ponents required to increase the

readout as suggested.

P.E. Scorpio ignition system

Sir—l have installed the P.E. Scorpio ignition system in a car to which I had previously fitted an impulse tachometer.

The instrument is a "Smiths" for which the fitting instructions refer to models 1T4, IT4C and 1T6, I have connected it into the lead from the coil to capacitors C6/C7 (tag 5) as suggested in Readout, March issue.

Some of your readers may be interested to know that this appears

to work satisfactorily.

H. R. M. Foster, Beverley, Yorks.

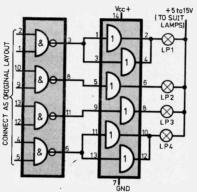
Logic identifier

Sir-With reference to Mr T. P. Schofield's "Logic Semiconductor Identifier" in the July issue.

Mr Schofield recommends the use of 7440's as lamp driving logic. Although these have a normalised fan-out of 30, I would recommend the use of 7407's. The latter are hex. buffer/drivers, capable of sinking 40mA per buffer, and their cost per package is less than the average price of one 2N1305 of which four are required in the equipment as designed.

Fig. I shows the use of a 7407 device in the circuit.

P. Lockerby, Nelson, Lancs.



7407 Fig. 1. Suggested circuit for a logic identifier. Note two pairs of buffers are paralleled solely to save tying unused inputs with resistors

Live wire

Sir-Mr W. A. Rawcliffe (the exceptional caravanner-July Readout) seems to have forgotten that PRACTICAL ELECTRONICS readers pride themselves in their ingenuity.

Having reached the same conclusion as W. A. R. that some indication was required that the flasher bulbs had not gone open circuit, I very simply wound 300 turns of 24 gauge plastic covered wire (about 30 feet) on to an old P.O. 3000 relay former and wired it in series with the extra "live" lead he talks about.

This gives ample magnetism to operate the relay and through it contacts an additional pilot lamp on the dashboard while at the same time having a resistance of less than ½12, drops less than 1 volt in doing so-thus not affecting the brightness of the flasher bulb by any noticeable amount.

This system could also be easily adapted for brake light if anyone should so decide and slightly less turns on the former would indicate when only one brake light has gone open circuit!!

H. G. Hearn, Sussex.

Be specific

· Sir-I have been reading PRAC-TICAL ELECTRONICS for two years now, and find it difficult to obtain many of the parts specified in your constructional projects. This applies particularly to transistors, as a lot of your work is done around "Ferranti" transistors, which I cannot find at reasonable prices in Australia. Equivalents lists are a great help, as most of the transistors I want are either not listed, or have a CV equivalent only, or a type which is itself out of production, or otherwise unavailable here.

I think that the publication of the characteristics of the transistors used, specifying any necessary parameters, e.g. power dissipation, maximum and minimum beta, and so on, and then go on to give one or two examples. Perhaps when "or similar" appears, you might like to put a few "or similars".

This practice is not confined to transistors, so please don't specify a specific component, just its characteristics and tolerances on those characteristics.

A. Wright, New South Wales, Australia.

Wigan radio club

Sir-I would be obliged if you could find space in P.E. to publicise the forthcoming formation of the Wigan and District Amateur Radio Society.

A temporary committee has been set up and I would like to hear from prospective members.

V. T. Brooks, 8, Sutherland Road, Worsley Mesnes, Wigan, Lancs.

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2N3055		11		0.65	BC108			12
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2N3704				0.10	BC177		. 0.	
2N3819	-			0.25	BC184L		. 0.	
2N4286				0.15	BC212L.		. 0	
2N4289			10.10	0.15	BD130	2.7		65
2N4443				0.88	BD131			77
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40362			-	0-45	BY164			45
40432				1.60	MJ481			20
40512				1.79	MJ491			35
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AD142				0-50	OC35	11	0-	63
AD149				0.68	82CN1			12
- AD161		110		0.42				09
AD162				0.40	TO3 Transist			
AD102				0 10	200 114113130		,	

RESISTORS 10%—5%—2%

Code	Power	Tolerance	Range in ohms	Values		10 to 99 see note bel	
C	1/20W	5%	82-220K	E12	9	8	7
C	1/8W	5%	4-7-470K	E24	1	0.8	0.7
č	1/4W	10%	4·7-10M	E12	1	0.8	0.7
С С С	1/2W	5%	4·7-10M	E24	1.2	1	0.9
C	1W	5%	4-7-10M	E12	2.5	2	1.9
MO	1/2W	2%	10-1 M	E24	4	3	2 net
ww	1W	10%	0.22 3.9	E12	7	7	6
		$\pm 1/20 \Omega$					
ww	3W	5%	1-10K	E12	7	7	6
ww	7 W	5%	1-10K	E12	9	9	8

Codes: C = carbon film high stability low noise
MO = metal oxide Electrosil TR5 ultra low noise
WW = wire wound Plessey

values:
E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 72, 91 and their decades. Prices are in pence each for same ohmic value and power rating, NOT mixed values. (Ignore fractions of 1p on total value of resistor order.)

Minitron DIGITAL INDICATOR

TYPE 3015F Seven seg-

TYPE 3015F Seven segment indicator compatible with standard logic modules and power supplies. Figs. 0-9 from well illuminated filament segments to give character of 9mm height plus decimal point. Power requirement 8mA from 5V d.c. per segment. A limited number of alphabetical symbols also available. In 16 lead D1L case

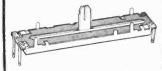
Suitable BCD decoder driver type FLL121T nett #1-36

D1L Socket; 16 lead 30p. No. 3015G showing + or - and fig. 1 and decimal point £2.

PRECISION COMPONENTS

Resistors by Rivlin, 0·1% to 0·01%, £1 to £2. Capacitors by MFD, 0·1 \(\mu \) F to 22 \(\mu \)F, 70p to £3·50. Prices and delivery times on request.

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Robust construction, smooth silent action. In values from $4k7\Omega$ to $1M\Omega$, linear or log. 26p each. Escutcheon, light grey, 10p.

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Many others in stock up to 10 patterns.

PUBLICATIONS

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	INTEGRA	E	U CI	KCUIIS	are nett	1.
	FLH101 (7400)		20p	FLJ121	(7473)	46p
	FLH201 (7401)		20p	FLJ141	(7474)	45p
	FLH191 (7402)		20p	FLJ151		45p
	FLH291 (7403)		20p	FLJ131	(7476)	45p
	FLH211 (7404)		25p	FLH221	(7480)	68p
	FLH271 (7405)		25p	FLH281		87p
	FLH381 (7408)		25p	FLH241		1.32
	FLH391 (7409)		25p	FLH341	(7486)	3 3 p
	FLH111 (7410)		20p	FLJ161	(7490)	80p
	FLH351 (7413)		35p	FLJ221	(7491A) .	1.28
	FLH 121 (7420)		20p	FLJ171	(7492)	85p
	FLH181 (7430)		20p	FLJ181	i i	809
	FLH141 (7440)		24p			1.13
	FLL101 (7414)		1.22	FLJ231	(7494)	87p
	FLH281 (7442)		1.16	FLJ191	(7495)	1.48
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	FLH371 (7444)		1.45	FLJ301		48p
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	FLH161 (7451)		20p	FLJ271 FLK 101	(74107)	48p
	PLH171 (7453)		20p		(74190)	1.80
l.	FLH181 (7454)		20p	FLJ201	(74191)	1.80
ľ	FLY101 (7466)		20p	FLJ211 FLJ241	(74191)	1.74
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DUAL CONCENTRIC in any combination of P.20 values, 60p; with switch, 72p. Knobs, pair 24p.

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As designed by P. J. Baxandali and originally described in "Wireless World". Complete kit inc. spkr., equaliser and special cabinet kit $48 \ln \times 10^{10} \times 10^{10}$ cut to size. 10 watt $80 \times 10^{10} \times 10^{10} \times 10^{10}$ cut $80 \times 10^{10} \times 10^{10} \times 10^{10}$

Speaker unit and equaliser kit, net. Post free £4.81.
Pack flat cabinet assembly (all cut to shape), natural teak
finish with instructions, £9 net. Part cost carr. in U.K. 60p.

SIEMENS THYRISTORS 0.8A-400V, 56p. 600V, 70 3A-400V, 60p. 600V, 88p.

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Small high quality, type PR linear only: 100 \(\Omega\$, 220 \(\Omega\$.

470 \(\Omega\$, \(\Omega\$) K, 2K2, 4K7, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M2, 5M, 10M \(\Omega\$). Vertical or horizontal mounting, 5p each.

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70 watt power amp module kit, £12-60 net. Power supply kit, £6-50 net.

Q.E.D. HIGH QUALITY AMPLIFIER SYSTEMS. Built to your personal specifications. Enquiries invited. Please quote PE.7.

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250V up to 0·1µF: 100V/0·1µF and above. 0·01, 0·012, 0·015, 0·018, 0·022, 0·027, 0·033, 0·047, 0·056,

0:068, 0:082, 0:1, 0:12, 0:15, 4p each, 0.18, 0.22, 5p each.

0.27, 0.33, 6p; 0.39, 7p; 0.47, 8p; 0.56, 10p; 0.68, 11p; 1µF, 13p.

ELECTROLYTIC CAPACITORS

[Values in $\mu E/V$] 0·47/100, 1/100, 2·2/63, 4·7/35, 10/25, 22/16, 47/10, 47/25, 0.47/100, 17/100, 22/36, 47/35, 10/25, 22/10, 47/10, 47/25, 100/10, 220/3, 7p each. 10/63, 22/35, 47/35, 100/16, 100/25, 220/6, 220/10, 220/16, 470/3, 7p each.

4:0/3. /p each. 47/50, 47/63, 100/35, 220/16, 8p each; 100/50, 220/35, 10p each; 100/63, 470/25, 1000/10, 12p each; 220/63, 470/35, 1000/16, 17p each; 1000/25, 20p each; 470/63, 1000/35, 23p each; 2200/25, 36p each; 1000/63, 2200/35, 4700/16, 40p each.

Tantalum and other capacitors, etc., see latest 1972 catalogue—issue No. 6.

1972 ELECTROVALUE CATALOGUE (No. 6)

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ELECTROVALUE LTD .- AN INDEPENDENT COMPANY SINCE ITS ESTABLISHMENT IN 1965

Sinclair Project 60

Stereo 60



Built and tested post free £9.98

pre-amplifier/control unit

The versatility of Project 60 high-fidelity modules is well demonstrated in this excellent unit. It provides the facilities essential to good stereo and will enhance the quality of any system it is used with, whether Project 60 or any any other top line power amplifiers. Compact, yet robustly constructed, the unit is easily panel mounted and will operate satisfactorily from 18 to 35 volts supply. Silicon epitaxial transistors are used throughout to achieve a very high signal to noise ratio with excellent separation between channels. Distortion at maximum output is barely 0.02% with magnetic p.u. input. Accurate equalisation is provided for all inputs, which are selected by push buttons. For maximum effectiveness, the Sinclair A.F.U. is recommended for use with the Stereo 60 pre-amp/control unit. A comprehensive manual supplied with Project 60 modules makes installing and connecting easy and ensures best possible results from your system.

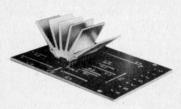
SPECIFICATIONS

Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV correct to R.I.A.A. curve ±1dB. 20 to 25,000 Hz. Ceramic p.u. – up to 3mV: Aux – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB.

Tone controls: TREBLE ± 12 to -12dB at 10KHz; BASS ± 12 to -12dB at 100Hz. Front panel: brushed aluminium with black knobs and controls.

Size: $66 \times 40 \times 207$ mm.

Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-ficonstructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up. F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 tranmake possible. It is the equivalent of a 22 tranmake possible.

sistor circuit contained within a 16 lead DLL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). 6-80. Frequency Response: 5Hz to 100KHz±1dB. Total Harmonic Distortion: Less than 1%. (Typical 0-1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90dB (1,000,000,000) times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size: 22×45×28mm including pins and heatsink...

Manual available separately 15p post free,

With FREE printed circuit board and 40 page manual.

£2.98 Post free

Project 605



The easy way to buy and build Project 60

Project 605 is one pack containing: one PZ5, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free £29.95

Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder.



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the world's most advanced high fidelity modules

Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual. 2.30 £4.48 2.50 £5.48

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8 Ω) and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications). -- Power Outputs:

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts Z.50 40 watts R.M.S. into 3 ohms using 50 volts: 30 watts R.M.S. into 8 ohms using 50 volts.

Frequency response: 30 to 300,000Hz±1dB. Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 8 Ω). For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57mm.





Project 60 Stereo F.M. Tuner

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108MHz. Sensitivity: 7μV for lock-in over full deviation. Squelch level: Typically 20μV. Signal to noise ratio: >65dB. Audio frequency response: 10Hz – 15KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2μV. Cross talk: 40dB. Output voltage: 2 x 150mV R.M.S. maximum Operating voltage: 25-30VDC. Indicators: Stereo on; tuning. Size: 93 x 40 x 207mm.



Built and tested. Post free.



£25

A.F.U. High & Low Pass Filter Unit

For use between Stereo 60 unit and two Z.30s or Z.50s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. There are two filter sections – rumble (high pass) and scratch (low pass). H.F. cut-off (—3dB) variable from 28KHz to 5KHz. L.F. cut-off (—3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) 0.02% at rated output. Operating voltage from 15 to 35V. Current 3mA. Size: 66 x 40 x 90mm.

Built, tested and guaranteed.

£5.98



Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply

Z.30

Z.30, PZ.5

60; PZ.5

Typical Project 60 applications

System

player

Simple battery

Mains powered record

12W, RMS continuous

sine wave stereo amp. for

record player

together with	Units cost
Crystal P.U., 12V battery volume control, etc.	£4.48
Crystal or ceramic P.U. volume control, etc.	£9.45
Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90

£26.90

PZ.5 30 volts unstabilised £4.98 PZ.6 35 volts stabilised PZ.8 45 volts stabilised (less mains transformer) PZ.8 mains transformer

average needs 25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers

2 x Z.30s, Stereo 60: PZ.6

2 x Z.30s, Stereo

The Units to use

Tuner, Tape Deck, etc.

£34.88

continuous sine wave de luxe stereo amplifier. (60W. Indoor P.A.

80W. (3 ohms) RMS

2 x Z.50s, Stereo 60: PZ.8, mains transformer

£19.43 Z.50, PZ.8, mains Mic., quitar, speakers, etc., controls

High quality ceramic or magnetic P.U., F.M.

transformer F.M. Stereo Tuner (£25) & A.F.U. (£5.98) may be added as required.







Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, you money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sincleir Radionics Ltd.

Sinciar regionics cto.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

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THE "PUP"

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2G304 2G271 2N697 2N744	20p 10p 12p 17p	2N3053 2N3134 2N3135 2N3702	30p 20p	ASY32 ASY76 ASZ20 BC107	20p 20p 30p	BCZ10 BCZ11A BF194 BF200	20p 30p 14p 30p	NKT221 OC28 OC45 OC71	25p 45p 10p
2N1303 2N1305	15p 20p	2N3707 2N4036	12p	BC108 BC109	10p	BFY51 BFY52	16p 20p	OC74 OC139	20p 25p
2N1309 2N1596	25p €1	2S002 2S323	50p	BC148 BC187	10p	BFX87 BFX88	25p 20p	OC200 OC201	25p 50p
2N1613 2N1711	15p 24p	25324 AC128	£1-20	BCY30 BCY32	35p 45p	BPX25 GET525	30p	V30/30P	30p
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ISKRA RESISTORS & Carbon film low noise all values ip each ON/OFF TO GGLE SWITCH IDP GRELCO 5-WAY SCREW CONNECTOR 13p 2 POLE SW STANDARD JACK SOCKETS 9p KNOBS. I in dia. screw fix. Grey. black 9p black 9p Black 9p RED PUSH BUTTON SWITCH SP. ROUND hole fix 10p

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NEW LOW PRICES LARGEST RANGE **FULLY GUARANTEED BRAND NEW**

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2N2219 2N2369	0-20 0-15	BCY32	0.55	GEX 45/	1 0.10	OC70 OC71	0-12 0-12	7428	0.50
2N2369A 2N2444	1.99	BCY33	0.25	GEX941	0.15	OC72	0.20	7430 7432	0.20
2N2613	0.28	BCY34 BCY38 BCY39 BCY40 BCY42	0.40	GJ3M GJ4M	0.25	0C72 0C73 0C74 0C75	0.80	7433	0.70
2N2646 2N2904	0.45	BCY39	1.00 0.50	GJ5M GJ5M	0.25	OC75	0.25	7437 7438	0-85 0-85
2N2904 A 2N2906 2N2907	0.25	BCY42	0.25	GJ7M HG1005	0-87 0-50 0-20	0C76 0C77	0.25	7440	0.20
2N2906 2N2907	0.20	BCY70 BCY71	0·15 0·20	H8100A	0.20 0.25	OC78 OC79	0.20	7441AN 7442	0-75 0-75
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2G308 30p 2N3566 22p 28303 60p BC122 2G309 30p 2N3566 22p 28303 60p BC125 2G371 15p 2N3568 25p 28304 75p BC126	20p BFX37 30p NKT238 25p 15p BFX44 37p NKT240 27p 20p BFX68 67p NKT241 27p	CA3011 75p FJH161 70p SN7446 100p CA3012 88p FJH171 25p SN7447 135p CA3013 105p FJH181 25p SN7448 195p	1R5 40p 30C17 90p EM84 35p 1R5 40p 30C17 90p EM85 100p 185 30p 30C18 80p EM87 70p 1T4 25p 30F5 85p EY51 40p
2G374 20p 2N3569 25p 28501 32p BC134 20p 2N3670 125p 28502 35p BC136 2N368A 48p 2N3572 97p 28503 27p BC136 2N404 20p 2N3605 27p 3N83 40p BC137	12p BFX84 25p NKT242 20p 12p BFX85 30p NKT243 62p 15p BFX86 25p NKT244 17p 15p BFX87 25p NKT245 20p	CA3014 124p FJH221 25p 8N7450 20p CA3018 84p FJH231 25p 8N7451 20p CA3018A FJH241 25p 8N7453 20p	1U4 30p 30FL1 75p EY86 40p 1U5 60p 30FL12 120p EY87 42p 2D21 35p 30FL14 95p EZ40 55p
2N696 15p 2N3606 27p 3N128 70p BC138 2N697 15p 2N3607 22p 3N140 77p BC140 2N698 25p 2N3638 18p 3N141 72p BC141	20p BFX88 20p NKT261 20p 35p BFX89 62p NKT262 30p 35p BFX93A 70p NKT264 20p	110p FJH251 25p SN7454 20p CA3019 84p FJJ101 50p SN7460 20p CA3020 126p FJJ111 50p SN7472 30p CA3020A FJJ121 60p SN7473 40p	3Q4 50p 30L15 85p EZ41 50p 384 35p 30L17 80p EZ80 27p 3V4 48p 30P12 80p EZ81 29p 5R4 75p 30P19 85p GZ32 48p
2N699 30p 2N3638A 20p 3N142 55p BC147 2N706 10p 2N3641 18p 3N143 67p BC148 2N706A 12p 2N3642 18p 3N152 87p BC149 2N708 15p 2N3643 20p 40050 55p BC152	10p BFY11 42p NKT271 20p 10p BFY18 25p NKT262 20p 12p BFY19 25p NKT274 20p 17p BFY21 42p NKT273 20p	CA3021 156p FJJ131 60p 8N7474 40p CA3021 156p FJJ141 125p 8N7475 45p CA3022 130p FJJ181 75p 8N7476 45p	5U4 85p 30PL1 75p GZ34 60p 5V4 45p 30PL13 93p KT66 205p 5Y3 40p 30PL14 90p KT88 200p
2N709 62p 2N3644 25p 40250 50p BC153 2N718 25p 2N3645 25p 40251 32p BC154 2N718A 30p 2N3691 15p 40309 32p BC157	20p BFY24 45p NKT278 25p 20p BFY29 40p NKT281 27p 15p BFY30 40p NKT401 87p	CA3026 100p FJJ211 125p 8N7486 33p CA3028A 74p FJJ251 125p 8N7490 87p CA3028B FJL101 125p 8N7492 87p	5Z4G 40p 35L6 50p MU14 75p 6/30L2 88p 35W4 35p PABC80 40p 6AC7 40p 35Z4 35p PC86 60p 6AG7 40p 35Z5 50p PC88 60p
2N727 30p 2N3693 15p 40311 35p BC159 2N914 17p 2N3694 18p 40312 47p BC160 2N916 17p 2N3702 10p 40314 37p BC167	11p BFY41 50p NKT402 90p 12p BFY43 62p NKT403 75p 35p BFY50 20p NKT404 55p 11p BFY51 20p NKT405 75p	105p FJY101 25p 8N7493 87p CA3029 87p IC12 180p 8N7495 87p CA3029A L900 40p 8N7496 87p 185p L914 40p 8N74107 52p	6AK5 35p 50B5 50p PC97 45p 6AK6 60p 50C5 50p PC900 48p 6AL5 20p 80 55p PCC84 40p
2N918 30p 2N3703 10p 40315 37p BC168B 2N929 22p 2N3704 11p 40316 47p BC168C 2N930 20p 2N3705 10p 40317 37p BC169B 2N987 40p 2N3706 9p 40319 55p BC169C	10p BFY52 20p NKT406 82p 11p BFY53 15p NKT451 62p 11p BFY56A 57p NKT452 62p	CA3030 137p L923 40p 8N74153 CA3035 122p LM380 £1 22p 135p CA3036 72p MC724P 60p 8N74154	6AM6 30p 88A2 50p PCC85 40p 6AQ5 38p 807 50p PCC89 55p 6AS6 40p 1625 50p PCC89 50p 6AT6 35p 5763 70p PCC189 55p
2N1090 22p 2N3707 11p 40320 47p BC170 2N1091 22p 2N3708 7p 40323 32p BC171 2N1131 25p 2N3709 9p 40324 47p BC172	12p BFY77 57p NKT713 20p 15p BFY90 65p NKT717 42p 15p BSX19 17p NKT734 27p	CA3039 82p MC780P 2477 8N74160 200p CA3041 109p MC788P 146p 180p CA3042 109p MC790P 124p 8N74161 CA3043 137p MC792P 66p 280p	6AU6 25p 6146 160p PCF80 30p 6AV6 30p AZ31 55p PCF82 34p 6BA6 25p CY31 35p PCF84 60p
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2N1305 22p 2N3715 123p 40348 52p BC182 2N1306 25p 2N3716 130p 40360 40p BC1821 2N1307 25p 2N3773 240p 40361 40p BC183	10p B8X28 32p OC19 37p 10p B8X60 82p OC20 75p 9p B8X61 62p OC22 50p	CA3047 137p MC1304P 225p CA3048 204p 225p 58774192 CA3049 160p MC1305P 58774192 CA3050 186p 386p 88774193	6BR7 90p DK91 40p PCP805 80p 6BR8 70p DK92 55p PCF806 70p 6BW6 85p DK96 50p PCF808 75p 6BW7 80p DL92 35p PCL82 35p
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2N1631 35p 2N3854 27p 40408 52p BC187 2N1632 30p 2N3854 27p 40409 55p BC212L 2N1637 30p 2N3855 27p 40410 62p BC213L 2N1638 27p 2N3855 30p 40412 BC213L	27p B8Y25 15p OC28 60p 12p B8Y26 17p OC29 60p 12p B8Y27 15p OC35 50p	CA3055 240p 461p TAA243 150p CA3059 165p MC1709CG TAA263 75p CA3064 120p 90 TAA293 97p PCH101 85 MFC4000P TAA300 175p	6CL6 50p DY86 32p PCL86 45p 6CW4 65p DY87 33p PFL200 65p 6F1 62p E88CC 100p PL36 55p 6F6G 35p E180F 100p PL81 50p
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2N1893 37p 2N3859 27p 40603 50p BCY33 2N2147 72p 2N3859A 32p AC107 30p BCY34 2N2160 57p 2N3860 30p AC126 20p BCY38	50p B8Y37 25p OC45 25p B8Y38 20p OC46 30p B8Y39 22p OC70 15p 40p B8Y39 50p OC71 12p	FCH141 105p SN7402 20p TAA435 147p FCH151 105p SN7403 20p TAA521 132p FCH171 105p SN7404 20p TAA522 360p FCH181 105p SN7405 20p TAA523 495p	6F23 85p EBC81 30p PL504 80p 6H6 17p EBF80 40p PY32 55p 6J4 50p EBF83 40p PY33 63p
2N2193 40p 2N3866 150p AC127 24p BCY39 2N2193A 42p 2N3877 40p AC128 20p BCY40 2N2194 27p 2N3877A 40p AC151 18p BCY41 2N2194A 30p 2N3900 37p AC152 22p BCY42	60p B8Y51 32p OC72 12p 50p B8Y52 32p OC73 30p 15p B8Y53 37p OC74 30p	FCH191 105p 8N7406 80p TAA811 445p FCH201 130p 8N7408 20p TAB101 97p FCH211 130p 8N7409 20p TAD100 150p	6J5 25p EBF89 32p PY80 40p 6J5GT 30p EBL21 60p PY81 30p 6J6 20p EC86 60p PY82 35p 6J7 45p EC88 60p PY83 38p
2N2217 25p 2N3900A 40p AC154 22p 8CY43 2N2218 20p 2N3901 97p AC176 20p 8CY54 2N2219 20p 2N3903 20p AC187 20p BCY58	15p B8Y56 90p OC76 22p 32p B8Y79 45p OC77 30p 22p B8Y90 57p OC78 20p	FCH221 130p SN7410 20p TAD110 150p FCH231 150p SN7411 23p SL403D 150p FCJ101 160p SN7412 48p SL702C 147p FCJ111 150p SN7413 30p UA702A 280p	6K8G/ 40p ECC40 65p PY88 40p 6L6GT 45p ECC84 30p PY800 40p 6LD20 50p ECC85 40p PY801 50p 6Q7 40p ECC88 40p U25 80p
2N2221 25p 2N3905 30p ACY17 27p BCY60 2N2222 20p 2N3906 25p ACY18 24p BCY70 2N2222A 25p 2N4058 12p ACY19 24p BCY71	22p B8Y95A 12p OC81 20p C424 15p OC81 20p 15p 450 15p OC82 25p 20p ET102 30p OC821 15p	FCJ121 275p 8N7416 84p UA702C 77p FCJ131 275p 8N7417 84p UA703C 137p FCJ141 525p 8N7420 20p UA709C 45p FCJ201 100p 8N7423 51p UA710C 125p	68A7 40p ECF80 35p U26 80p 68G7 40p ECF82 35p U50 40p 68J7 40p ECF86 65p U52 35p
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2N2410 42p 2N4244 47p ACY39 47p BCZ11 2N2483 27p 2N4248 15p ACY40 20p BD112 2N2484 32p 2N4249 15p ACY41 15p BD116	40p GET873 12p OC170 25p 50p GET880 30p OC171 30p 112p GET887 20p OC200 40p	BRIDGE 50PIV 4A 40P RECTIFIERS 100PIV 4A 40P 100PIV 4A	6U4 65p ECH83 45p U801 180p 6V6G 25p ECL80 45p UABC80 40p 6V6GT 32p ECL82 35p UAF42 55p 6X4 35p ECL83 70p UBC41 50p
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2N2712 25p 2N4287 17p AF109 45p BDY20	80p GET898 22p OC205 75p 125p MAT101 25p OC206 95p 105p MAT101 25p OC207 75p 125p MAT120 25p OC207 42p	50PIV 2A 50p 100PIV 6A 55p 100PIV 2A 50p 200PIV 6A 65p 200PIV 2A 55p 400PIV 6A 75p	10F1 75p EF40 50p UCC84 49p 10F13 60p EF41 65p UCC85 40p 10F14 110p EF42 70p UCF80 55p UCH21 60p 12AT6 30p EF80 25p UCH21 60p
2N2714 30p 2N4289 17p AF115 25p BDY62 2N2904 20p 2N4290 12p AF116 25p BF115 2N2904A 25p 2N4291 15p AF117 20p BF117	25p MAT121 25p ORP12 50p 25p MJ400 107p ORP60 40p 40p MJ420 80p ORP61 42p	SILICON RECTIFIERS MINIATURE WIRE ENDED PLASTIC	12AT7 30p EF85 35p UCH42 70p 12AU7 30p EF86 30p UCH81 40p 12AX7 30p EF89 28p UCL82 35p 12AV6 40p EF91 30p UCL83 60p
2N2905A 20p 2N4294 17p AF121 30p BF154 2N2906 20p 2N4303 47p AF124 22p BF158 2N2906A 25p 2N4964 15p AF125 19p BF159	28p MJ421 80p P346A 22p 20p MJ430 102p ST140 15p 15p MJ440 95p ST141 20p 85p MJ480 97p T1834 32p	SERIES IN PL CL 1 AMP 1-5 AMP 3 AMP 4001 50PIV 7p 8p 19p 4002 100PIV 7p 9p 260	12BA6 40p EF92 35p UF41 60p 12BE6 40p EF183 35p UF80 35p 12BH7 45p EF184 35p UF85 40p
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2N2926G 20p N5030 42p AF179 45p BF177 2N2926O 30 2N5172 12p AF180 50p BF178	30p MJE370 80p TIS47 11p 25p MJE371 80p TIS48 12p 30p MJE520 60p TIS49 12p	4007 1000PlV 15p 18p 30p 50+ less 10 % 100+ less 20 % SILICON RECTIFIERS	20P1 50p EL81 55p VR105/3038p 20P4 110p EL84 25p VR150/3035p
2N2926Y 10p DN5174 58p AF181 406 BF180 2N3011 30p DN5175 58p AF186 58 BF180 2N3014 50p DN5176 45p AF239 30p BF181 2N3053 15p Nx5282A 30p AF279 77 BF182 2N3054 45 AF286 47p BF184	35p MJE521 70p T1850 12p 32p MPF102 42p T1851 10p 30p MPF103 35p T1852 11p 20p MPF104 37p T1853 22p	STUD MOUNTING 6A 10A 17.5A 35A 100P1V 45p 50p £1.22	20P5 120p EL85 43p Add 12p in 2 25L6 50p EL91 35p for postage DIODES & RECTIFIERS 1N34A 10p BA154 12p GJ7M 37p
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TE 1018 DE-LUXE MONO HIGH IMPE-DANCE HEADSET Rensitive, soft earpads, adjustable headband. Magnetic, impedance 2,600 ohms. 21.97, P. & P. 15p.



MP7 MIXER PREAMPLIFIER

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5 microphone inputs each with
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facilities. Battery operated. 9½ × 5 × 3 ×
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1021 STEREO LISTENING STATION For balancing and gain selection of loudspeakers with additional facility.

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MCA. 220 AUTOMATIC VOLTAGE STABILISER Input 88-125 VAC, Output 120 VAC or 176-250V Input output 240 VAC. 200 VA output 240 VAC, 200 V rating, £11.97. Carr. 50p.





230 VOLT A.C. 50 CYCLES RELAYS

Brand New. 3 sets of changeover contacts at 5 amp rating. 50p each. P. & P. 10p (100 lots £40). Quantities avail-

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The first tuner in the world to use the phase lock loop principle—as used for receiving signals from space craft because of its vastly improved signal to noise ratio. Provides fantastic results even in difficult areas. Tuning range 87-5 to 108MHz. Automatic stereo indicator. Sensitivity: 2µV. AFC range ± 200KHz. Signal to noise ratio: 65dB. Output voltage 2x 150nhV. Operating voltage 25-30V D.C. Size: 93 × 40 × 207mm. The first tuner in the world to use the phase REC, LIST PRICE 425.

OUR PRICE £15.75 P. & P. Unrepeatable offer—buy now and save over \$9.

U4212 MULTIMETER

U4312 MULTIMETER
Extremely sturdy instrument for general electrical use. 667 o.p.v.
09.31.57.590/60/150/300/
600/900 VDC and 75mV.
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0/200 G/SK/30K Ω.
Accuracy DC 1%, AC 1.5%.
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4 Bands covering 550KHz-30MHz B.F.O. Built in Speaker 220/240V a.c. Brand new with instructions. \$15.75. Carr. 37‡p.



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PRACTICAL ELECTRONICS "SCORPIO" **ELECTRONIC IGNITION** SYSTEM .



This Capacitor-Discharge Electronic Ignition system was described in the November and December issues of Practical Electronics. It is suitable for incorporating in any 12V ignition system in cars, boats, gockarts, etc., of either pos. or neg. earth and up to six cylinders, the original coil, plugs, points and contact-breaker capacitor fixted in the wehicle are used. No extra or special components are required. Helps to promote easier starting (even under sub-zero conditions), improved acceleration, better high-speed performance, quicker engine warm-up and improved fuel economy. Eliminates excessive contact-breaker point burning and the need to adjust point and spark-plug gaps with precision.

and the need to adjust point and spark-plug gaps with precision.
Construction of the unit can easily be completed in an evening and installation should take no longer than half an hour. A complete complement of components is supplied with each kit together with ready-drilled roller-tinned professional quality fibre-glass printed-circuit board, custom-wound transformer and fully-machined die-cast case. All components are available separately. Case size 7±in × 4±in × 2in approx. Complete assembly and wiring manual 25p, refundable on purchase of kit. Price: £10-50 plus 50p P. & P. S.A.E. with all enquiries.

PSYCHODELIC LIGHTING. UNIT Mk. 3



This unit represents a natural progression from our phenomenally successful Mk. I and 2 Units. As before the drive voltage is and 2 Units, As before the drive voltage is derived directly from the amplifier output or across the speakers. The unit converts the audio frequency signals into a three-coloured light display; the colour depend-ing on the frequency of the signal and the intensity on the loudness of the audio

The unit is constructed on professional fibre-glass printed-circuit board material and uses latest full-wave triac circuitry. There is a master-level control, together There is a master-level control, together with independent sensitivity controls for each channel. The original minimum ambient light level controls have been redesigned permitting their use as faders; allowing dimming from max. to zero at the turn of a knob. R.F.I. suppression is now incorporated as standard as well as provision for D.J. "Pulse-Flash" controls. The choice of two inputs enables operation from both high and low power amplifiers. Max. power I-5kW per channel at 240V a.c. channel at 240V a.c.

Complete assembly built and tested. Size 9in × 7in × 3in. Price £25 carr. paid. S.A.E. with all

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AUTO TRANSFORMERS
0-110-200-2200 a.c. up or down fully shrouded fitted insulated terminal blocks. 30W £1-35; 50W £1-35; 50W £1-36; 75W £2-16; 100W £2-56; 150W £3-15; 200W £3-26; 300W £5-26; 300W £5-26; 500W £7-36; 600W £8-25; 7,000W £12-75; 1,500W £18; 2,000W £24-75; 0,000W £32-75; 1,500W £18; 2,000W £24-75; 0,000W £34; 0,000W £

1 × ½ × ½ in ½oz, with transparent cover, 2 C.O. in 9; 15; 20 or 30V d.c. 50p each. BULK TAPE ERASERS

BULK TAPE ERASERS Instant erasure, tape spools and cassettes, demagnetizes tape heads, a.c. 200/250V, £2.40 plus 24 P. & P. PERINTED CIRCUIT EXCHING AITS Complete outift; solutions and equipment to make your own P.C. boards instructions, £1.40, P. & P. 21p. Extra p.c. Boards 8 × 6in, 15p each. TAPE RECORDER MOTORS

A variety of uses, Blowers, Fans, etc., new. 230/250V a.c. 50p each.

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Paper: 0-01/2kV 124p; 0-1/1kV 124p; 0-22/1kV 25p;
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4/500V 25p, Electrolytics: 100 + 200/270V 40p; 100 +
4/500V 25p, Electrolytics: 100 + 200/270V 40p; 100 +
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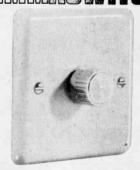
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The DIMMASWITCH is an attractive and efficient dimmer unit which fits in place of the normal light switch and is connected up in exactly the same way. The white mounting plate of the DIMMASWITCH matches modern electric fittings. Two models are available, with the bright chrome knob controlling up to 300 w or 600 w of all lights except fluorescents at mains voltages from 200-250 v, 50Hz. The DIMMASWITCH has built-in radio interference suppression:

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Electronically hanges speed from approximately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. 21-50 plus 13p post and insurance. Made up model also avail-able, 22-25 plus 13p post and p.

MAINS OPERATED CONTACTOR

220/240V. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 21 × 2 × 2 \$1.50 each. 10 for \$18.50



NEED A SPECIAL SWITCH?



Double Leaf Contact. Very slight pressure closes both contacts. 6p each, 60p doz. Plastic pushrod suitable for operating, 5p each, 45p doz.

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5 amp changeover contacts, 9p each. £1 doz. 15 amp Model 10p each or £1.05 doz.





MINIATURE

WAFER SWITCHES

2 pole, 2 way—4 pole, 2 way—
3 pole, 3 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole
6 way—1 pole, 12 way, All at 200 each, \$1.80 for ten, your assortment.

WATERPROOF HEATING
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26 yards length 70W. Self-regulating temperature
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IS AMP ELECTRICAL **PROGRAMMER**



Have radio playing and kettle boiling as you awake, switch on lights to ward off onlights intruders, has warm house to com

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Complete Kit (except wooden
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SNAP ACTION SLIDE SWITCH

Rated 5a. 240v. Made by Arrow. Type fitted in the handles of electric drills, vacuums, etc. 5p each, 10 for 45p.



For digital, instruments counters, timers, clocks, etc. Hi-vac XN. 3, Price \$1.45 each. 10 for £13. 12 WAY SUB-MINIATURE

7-0076 copper cores each core P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16ln. thick. Price 80p per yard.



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Almost zero resistant in sub-light increases to 10 K Ohms in dark or dull light, epoxy resin sealed. Size approx. In dia. by Jin thick. Rated at 500 MW, wire ended. 48p with circuit. Also ORP12 light cell 45p.

Miniature Tubes. These are approx. jin. diameter and need miniature bi-pin end connectors. 3 sizes available: 9in 6 watt, 2in 8 watt, 2in. 13 watt. Ali are 55p each. Less 10% on 10 or more.

A.C. Mains Buxzer. These are open constructions intended for fitting into instruments, etc. Size approx. 1\frac{1}{2}\text{in}, hlgh \times \text{lin}, deep \times \frac{1}{2}\text{in}, wide. approx. 11in, high x each; 10 for £2.25.

Watt Mains Transformer. As fitted into any day duty power pack—this has tapped primary rimary screen and four 10V secondaries—these may be loaded to a maximum of 250 wat a.c. output. Voltage available 10-20-30 and 40V, also 20-0-20 and 10-0-10V. This transformer weighs 7½ b. Price \$3 plus 45p post.

Panel Mounting Changeover Switch. With ce off position. Rated at 5 amp d.c. These switch and and an acc. 15p each; Page 185.

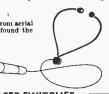


GOOD COMPANION

We can now offer these again in modular version using Muliard A.F. and I.F. Modules and Radiomobile Permeability Tuner. Should not take more than an evening to make. Cabinet size approx. 11in wide x 8in. high X 3in deep. Complete assembly instructions—24-75 plus 25p deep. Compost and lns.

RADIO STETHOSCOPE RADIO SIE I HOSCOPE Essiest way to fault find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio, TV amplifier, anything—com-plete kit comprises two special transistors and all parts inclu-

ding probe tube and crystal earpiece. \$2-twin stethoearpiece. 22—twin ste set instead of earpiece extra—post and ins. 20p.



STANDARD WAFER SWITCHES

Standard size 11 wafer-silver-plated 5-amp contact standard \$" spindle 2" long -with locking washer and nut

			·	P.		0				
	No. of Poles		3 way		5 way					12 way
	1 pole	40p	40p	40p	40p	40p	40p	40p	40p	40p
1	2 poles	40p	40p	40p	40p	40p	40p	40p	70p	70p
	3 poles	40p	40p	40p	40p	70p	70p	70p	95p	95p
	4 poles	40p	40p	40p	70p	70p	70p	70p	£1-20	£1-20
	5 poles	40p	40p	70p	70p	95p	95p	95p	£1-45	£1-45
	6 poles	40p	70p	70p	70p	95p	95p	95 p	£1.70	£1.70
ď	7 poles	70p	70p	70p	95p	£1-20	£1.20	£1-20		£1-95
	8 poles	70p	70p	70p	95p	£1-20	£1.20	£1.20		£2-20
	9 poles	70p	70p	95p	95p	21-45	21-45		42-45	£2·45
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	12 poles	70p	95p	95 p	£1-20	£1.70	£1.70	£1.70	£8-20	£8-20

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THYRISTOR LIGHT DIMMER

For any lamp up to lkW. Mounted on switch plate to fit in place of standard switch. Virtually no radio interference Price \$2.50, plus 20p post and insurance.



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REPEATIRG TIME SWITCH. 1 or 2 on/offs per.

24 hours. Repeats until reprogrammed. 8 witches up to 15 amp. 8 witching time completely adjustable through 24 hours Precision made with 24-hour dial. Miniature—will fit into 2in, cube. Mains operated clock but switch may be isolated for switching battery sets, Ideal for: shop window lighting, anti-thief devices, central heating control and many other automatic processes. Price with instructions \$2 each plus 20p post and insurance.



MULLARD AUDIO AMPLIFIER MODULE

Uses 4 transistors, and has an output of 500mW into ohms speakers. Input suitable for crystal mic. or pick-up. 9V battery operated. Size 2in long x 11in wide x lin high. SPECIAL SNIP PRICE 65p each. 10 for \$5.90.



HORSTMANN "TIME & SET" SWITCH
(A 30 Amp Switch.) Just the thing if you want to come home to a warm house without it costing you a fortune. You can delay the switch on time of your electric fires, etc., you to 14 hours from setting time or you can use the switch to give a boost on period of up to 3 hours. Equally suitable to control processing. Regular price probably around £5. Special only price £1.50. Post and ins. 23p.



HONEYWELL THERMOSTAT

HONEYWELL THERMOSTAT
Made by Honeywell for normal air temperatures
40-80°F (5-25°C). This is a precision instrument
with a differential which can be adjusted to better than
1.5°F. A mercury switch breaks on temp. rise—the
switch is operated by a colled bi-metal element and adjustable heater is incorporated for heat anticipation.
Elegantly styled and encased in an ivory plastic case
with clear plastic windows, thermometer above and
switch setting scale below—size approx. 3-8 in × 3-2 in
× 1-4 in deep—can be mounted on conduit box or
directly on wall. Price \$1.25 each or ten for \$11.25.



ZPM MODULATION MOTOR

Could also be used to open ventilators, doors, valve, damper, etc. particularly suitable for remote control. Made by Satchwell. Essentially a reversible geared motor fitted with internal limit switches to stop it at the end of its travel. Size approx. 6in. x 6 in. x 5 jin. and weighing approx. 9 lb. This is extremely powerful and would lift a heavy door or open a long line of ventilators. To operate this motor you put the 50 cycle supply through a changeover switch. For instance a thermostat with changeover contacts could automatically regulate the temperature in a growing house, chicken hatchery, etc. An indicator on the motor graduated 0-10 shows the state of open or close. Also internally fitted is a variable resistor, wires from this to a voit meter would give a remote indication of the open or close position. A very expensive motor if both direct from Satchwell, our price complete with step down Transformer is \$15.

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A parcel of Integrated circuits made by the famous Plessey Company. A oncein-a-lifetime offer of Micro electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect, first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP amplifiers. The 6th is a monolithic NPN matched pair. Regular price of parcel well over 25. Full circuit details of the IC's are included and in addition you will receive a list of many different IC's available at bargain prices 25p upwards with circuits and technical data of each. Complete parcel only \$1 post paid. DON'T MISS THIS TERRIFIC BARGAIN.

MULLARD I.F. MODULE

This is a fully scene dintermediate frequency module for amplification and detection of f.m. signals at 10.7MHz and a.m. signals at 470kHz. The first stage is used as an i.f. amplifier for f.m. and a self-oscillating mixer for a.m. operation, in conjunction with an external oscillator coil. 85p each; 10 for 27-85. With connection dig.



EDUCATIONAL KITS with pictorial instructions all



THIS BALANCE KIT FREE educa-Japanese made these are ex-cellent value for not expect to be

money. We do not expect to be able to repeat the softer once stocks are sold. Brief description of each kit is given below and with 3 kits or more we give FREE an accurate 11 piece balance kit. Frice of kits 409 each post paid. Special price for all 7 kits 25.69 with free balance kit. KA2 Lens Kit. Eleven parts, including candle, one concave lens, one convex lens, stage and slif frame, etc. Watch light rays bend as they pass through different lenses.

KA3 Water Pump Kit. Thirteen parts. Top of pump is transparent so that operating parts may be observed. Small parts are brightly coloured to be seen easily while working. Three types of pump may be made: Lift pump. Force Pump and Force Pump with reservoir and nozzle.

KA4 Busser Kit. Eleven parts. Transparent covers allow the operation of buzer to be seen. Illustrates and teaches how electromagnetism with an automatic switch results in an operating buzzer.

KA5—2-Pole. including enamel wire armsture.

MAS 2-Pole, including enamel wire, armature and pole piece, etc. Motor operates from 11 volt battery. Illustrates and teaches how electro-

and pose piece, etc. motol operaces from 17 to battery. Illustrates and teaches how electromagnetism operates a motor.

KA7 Electro-Magnet Kit. Fifteen parts, includes compass. Makes two electro-magnets one with one layer of wire and one with several layers or wire. Ficks up tacks, nails and any small parks showing how magnetism works.

small parts showing how magnetism works.

KAS Current and Resistance Kit. Twenty-nine
parts, including bench and light bulb. Conduct
interesting and educational projects to learn the
application of 'O'HMS LAW' and see the difference in current and resistance with different
types and lengths of wire.

KAS Bell Kit. Eight parts, including bell and
push button switch. Build a complete electric
bell and see how the hanimer is triggered to make
the bell ring.

KA10 Morse Key Busser and Bell Kit. 25 part
kit easy to construct, simple to operate.

4 Watt Amplifier Module. Made by Mullard Ref. No. EF9000. Part of the Uniter system. This has an output of 4 watt speech and music into a 12-16 ohm speaker. A powerful amplifier with a thousand uses—completely encased. Size approx.

thousand uses—completely encased. Size approx. 3½in. x ½in. x 1½in. Screw down input and output terminals. Price £.45 each; 10 for £13-06. Pre-Amplifier Module. 2 channel for Stereo. Input sensitivity 320mv. Part of the Mullard Unilex system and completely encased. Size in. x 4in. x 4in. Serew down input and output terminals. Price £1-80 each; 10 for £15-20. Stereo Power Module. Mullard Ref. No. EP9002. Rated at 12V 8VA. This has 2 separate outputs ceiminate cross talk. Again part of the Mullard Unilex system but suitable for many other purposes. Completely encased with screw down input and output terminals. Size 3½in. x 2½in. x 2½in. approx. Price £2-80 plus 20p post; 10 for £20-70. Heavy Duty Mains Power Pack. Output voitage

approx. Price 22-20 plus 20 p post, is the see 70.

Heavy Duty Mains Power Pack. Output voltage adjustable from 16-40V in steps—maximum load 250W—that is from 6 amp at 40V to 15 amp at 15V. This really is a high power heavy duty unit with dozens of workshop uses. Output voltage adjustment is very quick—simply interchange push on leads. Silicon rectifiers and smoothing by 3,000mF. Price 25-75 plus 659 post. Coloured Fluorescent Tubes. Unless otherwise stated all tubes are standard diameter and have

stated all tubes are standard diameter and have normal bi-pin ends.

18in. 15 watt, pink, green, gold/yellow, blue, red.

2tt 20 watt, red, radar red.

2tt 30 watt, peach and red.

3tt 30 watt, peach.

4tt 40 watt, rose.

5tt 80 watt, radar red, radar blue.

5tt 80 watt, radar red, radar blue, green, peach.

Lip to 3tt 409 each; 4tt 50p each; 5tt 60p each.

All leas 10% on 10 or more.

Flex Connecting Wire. Various colours P.V.C.

insulated.

Very thim—70076 pink pink, pluy, 100yd coils 50p.

Very thim—70076 pink pink, pluy, 100yd coils 50p. Very thin-7/0076 pink only, 100yd coils 50p

ach n—14/0076 black, white, red, violet, 100vd

eacn.
Thin—14/0076 black, white, red, coils 609 each.
Medium Thick—23/0076 black, red, violet and pink, 100yd coils 709 each: 500 yards 53.
Heavy—40/0076 red/brown, 100yd coils 21-50

neasy—a0/10016 real/1010km, 10090 coins 21/90 each.

Extra Heavy—70/0076 yellow, black and yellow/
red, 5009d coils £10 each; 100 yd coils, blue, black, £2-50 each.

Very Heavy—110/0076 1009d coils, blue, £3 each.

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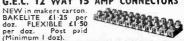
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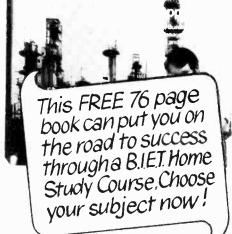
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