



CN.240/2 Miniature soldering iron 15 watt 240 volts, fitted with nickel plated 3/32" bit and packed in transparent display box. Also available for 220 volts. Price £1.70

CN.240 Miniature soldering iron 15 watt 240 volts, fitted with iron coated 3/32" bit. Up to 18 interchangeable spare bits obtainable. This iron can also be supplied for 220, 110, 50 or 24 volts. Price £1.70

G.240 Miniature soldering iron 18 watt 240 volts extensively used by H.M. Forces. Suitable for high speed soldering and fitted with iron coated 3/32" bit. Also available for 220 volts. Spare bits 1/8", 3/16" and $\frac{1}{4}$ " are obtainable. Price £1.83.



CCN.240 New model 15 watt 240 volts miniature soldering iron with ceramic shaft to ensure perfect insulation (4,000 v A.C.). Will solder live transistors in perfect safety; fitted with 3/32" iron coated bit. Spare bits 1/8" 3/16" and ¼" available. Can also be supplied for 220 volts. Price £1.80

CCN.240/7 The same soldering iron fitted with our new 7-star high efficiency bit for very high speed soldering The Imple- coated bits are iron, nickel and chromium plated, Price £1.95



E.240 20 watt 240 volts soldering iron fitted with %'' iron coated bit. Spare bits 3/32", 1/8" and 3/16" available. Can also be supplied for 220 and 110 volts. Price £1.80.

ES.240 25 watt 240 volts soldering iron fitted with 1/8'' iron coated bit. Spare bits 3/32'', 3/16'' and 3/8'' available. Can also be supplied for 220 and 110 volts. **Price £1.83**



SK.1 SOLDERING KIT

The kit contains a 15 watt 240 volts soldering iron

fitted with a 3/16" bit, nickel plated spare bits of 5/32" and 3/32", a reel of solder, heat sink,

Price £2.75 cleaning pad, stand and booklet "How to Solder". Also available for 220 volts



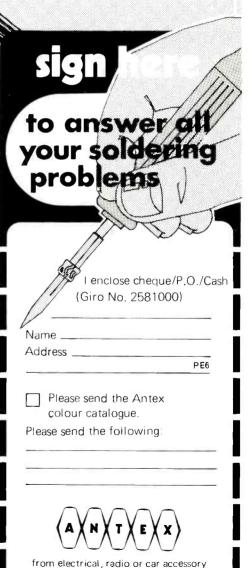
SK. 2 SOLDERING KIT

This kit contains a 15 watt 240 volts soldering iron fitted with a 3/16" bit, nickel plated spare bits of 5/32" and 3/32", a reel of solder, Heat Sink, 1 amp fuse and booklet "How to Solder"



MES. 12

A battery operated 12 volts 25 watt soldering iron complete with 15' lead, two crocodile clips for connection to car battery and a booklet "How to Solder" packed in a strong plastic wallet. **Price £1.95.**

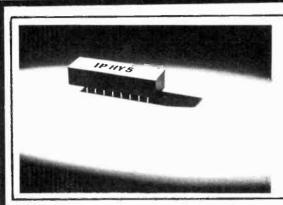


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HY40 IS POWER AMP PERFECTION

Lets face it — an immediate success, the HY40 is here to stay.

HY40 means Hybrid Power, power neatly locked away inside an Intregrated Circuit. Power the modern way, simply mount

only five additional components on a printed circuit board (all of which are supplied with the HY40). Power not only for Hi-Fi, power for Groups, for public address, for industry, power for all.

HY40 is HI-FI POWER ILP are POWER PROUD

In addition to the P.C. board and manual supplied with the HY40 we now include the five remaining components, at minimal cost, needed to complete the assembly of a High Performance Power Amplifier.

By merely combining two HY40s with a Stereo Preamplifier (2 x HY5) and simple Power Supply (PSU45), premium quality stereo may be obtained for a very modest outlay.

The free manual supplied with the HY40 gives clear, easy build instructions for Power Supply; volume, bass, treble and balance controls, together with inputs for Ceramic and Magnetic Pick-ups, Tape, Tuner and Auxiliary functions.

Internally the HY40 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER British Rating 40 WATTS PEAK, 20 watts RMS continuous.

LOAD IMPEDANCE 4-16 ohms
INPUT IMPEDANCE 22Kohms at
1Khz

INPUT SENSITIVITY 300 mV for maximum output.

VOLTAGE GAIN 30db at 1KHz. FREQUENCY RESPONSE 5Hz-60KHz ± 1db.

TOTAL DISTORTION less than 1% (typical 0.1%) at all output powers.

SUPPLY VOLTAGE ± 22.5 volts D.C.

SUPPLY CURRENT 0.8 amps maximum.

PRICE: including comprehensive manual, P.C. Board and FIVE EXTRA COMPONENTS:
MONO £4-40 STEREO £8-80 all post free.

A WORLDS FIRST TO JOIN THE WORLDS BEST

The HY5 is a unique and revolutionary concept in High-Fidelity pre-amplifiers. Thanks to the latest techniques, all feedback and equalization networks are, for the first time, combined into an integrated pre-amplifier circuit.

Simply by adding volume, treble, bass potentiometers and only three stabilizing capacitors, which are supplied, your HY5 is complete and ready for use.

The HY5 provides equalization for almost every conceivable input. This years developments in equalization technique enables precise correction for both output voltage and frequency response for any crystal or ceramic cartridge. Yet another feature of the HY5 is its inbuilt stabilization circuit, allowing it to be run off any unregulated power amplifier supply.

The HY5 contains a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo preamplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY40 and PSU45 forms a completely integrated system.

INPUTS

Magnetic Pick-up (within ±1db R1AA curve) 2mV. Tape Replay (external components to suit head). 4mV. Microphone (flat) 10mV. Ceramic Pick-up (equalized and

compensatable) 20 – 2000mV variable.

Tuner (flat) 250mV. Auxiliary 1 250mV. Auxiliary 2 2-20mV

OUTPUTS

Main Pre-amp output 500mV. Direct tape output 120mV.

ACTIVE TONE CONTROLS Treble +12db. Bass +12db.

INTERNAL STABILIZATION Enables the HY5 to share an unregulated supply with the Power Amplifier.

SUPPLY VOLTAGE 15-25 volt.

SUPPLY CURRENT

OVERLOAD CAPABILITY better than 28db on most sensitive input infinite on tuner and auxl.

OUTPUT NOISE VOLTAGE 0.5mV.

PRICE Mono £3-60

Stereo £7-20

POWER SUPPLY PSU45



The PSU45 is specifically designed to supply, simultaneously, your HY40 (in mono or stereo format) and one or two HY5s.

Spec.

PSU45 ± 22.5 volts, 2 amps simultaneously.

PRICE: £4-50 including Postage and Packing

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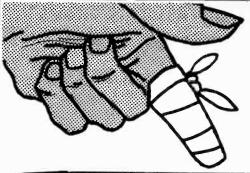
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ACI07 ACI13	15p AFI 15 20p AFI 16	17p BC140	35p BCY31 35p BCY32	22p BF272 25p BF273	80p EC403 30p GET880	15p ORP60 27p ORP61	40p 2N930 40p 2N1131	25p 2N2904A 20p 2N2905	30p 2N3706 25p 2N3707	13p
ACI15	23p AFI17	17p BC142	45p BCY33	17p BF274	30p MAT100	15p 5T140	12n 2N 1 132	22p 2N2905A	30p 2N3708 25p 2N3709	
AC125 AC126	17p AFI18 17p AFI24	30p BC143 21p BC145	40p BCY34 45p BCY70	20p BF308 17p BF309	35p MAT 101 37p MAT 120	17p 5T141 15p TI543	17p 2N1302 40p 2N1303	17p 2N2906 17p 2N2906A	25p 2N3709 27p 2N3710	
AC 127	17p AF125	20p BC 47	17p BCY71	30p BF316	75p MAT121	17p UT46	27n 2N I 304	20p 2N2907	25p 2N3711	
AC128	17p AF126	20p BC148	12p BCY72	15p BFW10	55p MPF102	43p V405A	25p 2N 1305 45p 2N 1306	20p 2N2907A 22p 2N2923	30p 2N3B19 13p 2N3B20	
ACI4IK ACI42K	17p AF127 17p AF139	20p BC149 33p BC150	17p 8CZ11	20p BFX29 85p BFX84	27p MPF105 20p OC19	43p V410A 30p 2G301	19n 2N 1307	22p 2N2924	13p 2N3903	
ACIST	15p AF178	50p BC151	20p BD123	85p BFX85	27p OC20	50p 2G302	19n 2N 1308	27p 2N2925	13p 2N3904	
ACI54	15p AF179	50p BC152	17p BD124 27p BD131	75p BFX86	22p OC22 25p OC23	30p 2G303 33p 2G304	19p 2N 1309 20p 2N 1613	27p 2N2926 17p (G)	2N3905 12p 2N3906	
AC155 AC156	17p AF180	50p BC153 50p BC154	30p 8D132	80p BFX87 80p BFX88	22p OC24	45p 2G306	35p 2N 1711	20p 2N 2926 (Y	() IIp 2N4058	15p
AC157	17p AF186	45p BCIS7	20p BDY20	£1 BFY50	20p OC25	25p 2G308	35p 2N 1889	35p 2N2926	2N4059 2N4060	
AC165 AC166	17p AF239 17p AFZII	37p BC158 37p BC159	17p BF115 20p BF117	22p BFY51 45p BFY52	20p OC26 20p OC28	25p 2G309 40p 2G339	35p 2N 1890 17p 2N 1893	45p (O) 37p 2N3010	10p 2N4060 80p 2N4061	
AC167	20p AFZ12	45p BC167	13p BF118	60p BFY53	17p OC29	40p 2G339A	15p 2N2160	60p 2N3011	20p 2N4062	I2p
ACI68	20p AL102	85p BC168	13p BF119	70p BSX19	15p OC35	33p 2G344	15p 2N2147 15p 2N2148	75p 2N3053 60p 2N3054	20p 2N5172 50p 2N5459	
AC169 AC176	14p AL103 23p ASY26	85p BC169 25p BC170	13p BF152 12p BF153	35p B5 X20 35p BS Y25	15p OC36 15p OC41	40p 2G345 20p 2G371	13p 2N2192	30p 2N 3055	63p 25034	75p
ACI77	20p ASY27	30p BC171	13p BF154	35p BSY26	15p OC42	22p 2G371B	10p 2N2193	30p 2N3391	17p 2S301	50p
AC187	30p ASY28	25p BC172	13p 8F1S7	45p BSY27	15p OC44 15p OC45	15p 2G374 12p 2G377	17p 2N2194 27p 2N2217	27p 2N3391A 20p 2N3392	20p 25302A 17p 25302	45p 45p
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ACY41	18p 8C115	30p BC207	11p 8F183	30p C441	27p OC170	15p 2N706	7 D			
ACY44	35p BC116	35p BC209 35p BC209	IIp BF184	25p C442 30p C444	35p OC171 37p OC200	15p 2N706A 25p 2N708	8p AA119 12p AA120	8p BYZII 8p BYZI2	32p OA81 30p OA85	7р 7р
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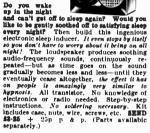


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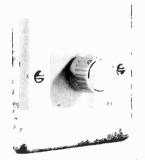
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The DIMMASWITCH is an attractive and efficjent dimmer unit which fits in place of the normal light switch and is connected up in exactly the same way. The ivory mounting plate of the DIMMASWITCH matches modern electric fittings. Two models are available, with the bright chrome knob controlling up to 300 w or 600 w of all lights except fluorescents at mains voltages from 200-250 v. 50Hz. The DIMMASWITCH has built-in radio interference suppression:

600 Watt - £3-20. Kit Form £2-70 300 Watt-£2.70, Kit Form £2.20 All plus 10p post and packing. Please send C.W.O. to:-

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WEST LONDON DIRECT SUPPLIES (PE/1)
169 KENSINGTON HIGH STREET, LONDON, W.8

EAK BARGAINS STEREO 30 PLUS amplifier (cased)

Power output (both channels sinewave driven): 15 watts r.m.s. each channel into 8 ohm loud-speakers. Music power output 20 watts r.m.s. each channel into 8 ohm loudspeakers. Total harmonic distortion 0:1% for all power Total harmonic distortion 0.1% for all power levels up to 10 watts r.m.s. each channel at IKHz into 8 ohm loudspeakers. Crosstalk: Between left and right channels —50dB up to IKHz and —30dB at 10KHz. Dimensions: 13in (W) × 4\frac{3}{2}in (H) × 9\frac{3}{2}in (D).

LIST PRICE PRICE £45.00 C&P £62-50

STEREO 70 amplifier (cased)

Power output (both channels sinewave driven): watts r.m.s. each channel into 8 ohm loudspeakers. Total harmonic distortion: 0.1% for all power levels up to 25 watts r.m.s. each channel at IKHz into 8 ohm loudspeakers. Crosstalk: Between left and right channels —50dB up to IKHz and —30dB at 10KHz. Dimensions: 13in (W) × 4½in (H) × 9½in (D).

LIST PRICE LASKY'S £55.00

LEAK TEAK CASES

Teak case for Stereo 30 or Stereo 70, please state which is required.

LIST PRICE LASKY'S £2.75 PRICE £7.37

Teak case for Stereofetic tuner only.

LIST PRICE LASKY'S £2.50 PRICE

Double case to hold Stereo 30 or Stereo 70 and Stereofetic tuner.

ASKY'S £4.95 C & P 35_p LIST PRICE £10:37 PRICE



LEAK TRUSPEED

Superh helt drive turntable system complete with arm, plinth and cover and Shure cartridge.

LASKY'S £47.50 C&P £69.50

SINCLAIR PHASE LOCK LOOP STEREO TUNER



Incorporates varican diodes. printed circuit, coils, squelch circuit I.C. Decoder, etc., supplied completely built and

tested and ready to be mounted into any cabinet you choose. It may be used with any High Fidelity Amplifier.

LIST PRICE £25.00

LASKY'S £16.95

NIVICO MCA-V7E 4-CHANNEL AMPLIFIER



The MCA-V7E can be used as a true 4-channel integrated amplifier from discreet 4-channel source using four speakers or have synthesised -channel sound using only two speakers MCA-V7E can also be used as a conventional stereo amplifier with two speakers only. Output $4 \times 12.5 W$ or $2 \times 25 W$.

LIST PRICE LASKY'S £69.50 C&P

BELTEK C5700 8 TRACK

Stereo car

Player
Accepts all standard pre-recorded
8 track stereo cartridges. Features include automatic



and chrome trim.

BELTEK C5700 complete with mounting brackets and 8 trackpre-recorded demonstration cartridge

C & P 25p each £19.75

£24.95

Beltek SP24 speakers match the C5700 and other Beltek car units in performance and finish. Size: 7½in(M) × 4½in rear, 2½in front (H). Complete with leads. £5.95 Pair

BELTEK FM TUNING ADAPTOR

Matches the C5700, the ideal car stereo system. LASKY'S £18.95 C&P 25p PRICE

BELTEK CM88 MINI MODEL

Ultra mini model with repeat mechanism. ASKY'S £23.95 C&P 25p

PRICE

BELTEK CF03F CAR STEREO

Cartridge player and FM car radio combined. LASKY'S £47.50 C& P 25p

BELTEK C1600 De-Luxe 8 TRACK RECORDER De-Luxe 8 track stereo recorder deck styled to

suit any home surroundings. LASKY'S £55.00 C& P 25p PRICE

AKAI SCOOP! (C & P 75p on all Tape Decks.)

AKAI 4000D List Price £96-38 AKAI 1720L Lasky's Price £61-50

List Price £89-91 Lasky's Price £58-95 AKAI X1800SD List Price £167-50 Lasky's Price £111-50

AKAI X200D List Price £162-53 Lasky's Price £106-50 2 CSS-8 Speakers List Price £25:00

Lasky's Price £15.00 C & P 50p 2 ADM 10/8 mics. Suitable for use on all Akai tape recorders. List Price £11-90 Lasky's Price £7-50, C & P 15p.



C & P 15p each



CONTROL Fitted with bass, treble, vol. and

balance controls. All wires fitted for connecting. Size 9in × 1½in × 1in. £2-25. EP-9001 PRE-AMP. Input imp. PU 2.2M, tuner IM. Sensitivity PU 320mV, tuner 140mV. Treble and bass control range — 14dB to + 14dB Treble at 16KHz, bass at 60Hz. Size 4in × 5in × 1in. £2.4 Med.

Treble at 16KHz, bass at 60Hz. Size $4\text{in} \times 5\text{in} \times 1\text{in}$, £2.40. EP 9000 AMP. Output 4W per channel into 12 ohms. Output imp. 12–15 ohms or 8 ohms with series resistors. Freq. resp. 50Hz–16KHz. Size $3\frac{1}{2}\text{in} \times 4\text{in} \times 1\frac{1}{2}\text{in}$. £2.25. EP 9002 POWER SUPPLY. Use with control, EP9001 and $2 \times \text{EP9000 For } 220/250V$ mains. £3.50

€3.50.

DIGITAL CLOCK SCOOP

EXCLUSIVELY FROM LASKY



FROM LASKY'S
The clock measures 4½ W × ½ H

× 3½ D (overall
from front of
drum to back of switch). SPEC: 210/240V a.c. 50Hz
operation; switch rating 250V, 3A. Complete with
instructions. H UNDREDS OF APPLICATIONS
COMPLETE WITH KNOBS. FEATURES: INSTRUCTIONS. HUNDREDS OF APPLICATIONS
COMPLETE WITH KNOBS. FEATURES:
MAINS OPERATION @ 12-HOUR ALARM
AUTO "SLEEP" SWITCH @ HOURS,
MINUTES AND SECONDS READ-OFF
FORWARD AND BACKWARD TIME
ADJUSTMENT @ SILENT OPERATION
SHOCK AND VIBRATION PROOF
BUILT IN ALARM BUZZER LASKY'S £6.50

SPECIAL QUOTES FOR QUANTITIES **BSR TD8S**



List Price £24:20

LASKY'S £17.95



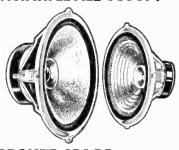
BARGAIN SCOOP

PYE S.W. CAR RADIO CONVERTER High quality transistorised and

High quality transistorised and ultra compact Shortwave Converter for use with any suitable MW(AM) Car Radio. Self powered for use on 12V positive or negative earth systems. The model 2649 is simply connected to the radio via the aerial socket and provides shortwave covering in 6 push button selected band spread ranges (13, 16, 19, 25, 31, 41, 49, 60 & 90 M) combined with the normal radio tuning to give full cover from 3:2MHz-21-75 MHz. On/off switch and by-pass switch for normal MV radio use. Complete with mounting bracket fitting and alignment instructions. Black hammer crackle finished case—size: 6(W) × I₂(H) × 3₂(D) in. C & P 20p.
Made to sell at Approx. £20-00 LASKY'S

LASKY'S £8.75 C&P20p

FANTASTIC VALUE WHARFEDALE SCOOP!



BRONZE 8RS/DD 8in, 15 ohms

LIST PRICE

LASKY'S £2.95 C&P

TWO FOR £5.75

SUPER IORS/DD 10in, 15 ohms

LIST PRICE £13-50

LASKY'S £6.50

TWO FOR £12-50



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Vhere can I get exclusive

TAPE DECK, MODEL CS-2000D

hi fi system is complete without one hook it up to any ROC or other good quality amplifier, and the results are fantastic! The CS-2000D records and plays back. A big feature is its easy-to-use piano-key controls. Easy-to-get-at mic inputs are on

top, line inputs and outputs at the rear Dual-channel recording level meter. Pog-up cassette ejection. Stereo/Mono button, Tape counter, Pause control. Tape speed 1% ips (4 75 cms). Frequency response 100-10,000 Hz and flutter better than 0.3%. Rewind time better than 60 sec with C60 cassette. Engineered throughout to the highest electrical and mechanical standards, Size 16" wide, 41," high and 8" deep. Walnut cabinet with saling

tornial Price £65 00 aluminium trims REALISTIC 30 WATT STEREO AMPLIFIER MODEL SA-500
A superb hi-fi amplifier with all the fea-

connecting leads

hetnew year evillor seni

f46-00. Saving over £10-00 on the normal retail value. Up-to-the-minute stider controls for bass and trebl volume and balance controls. Headphone socket on front panel Push-button input controls — magnetic phono (high/low) tuner, aux, mono, monitor Loudness push-button control for perfect sound at low output levels. Left and right push-button on/off switches for speakers. Noise filtering and tape monitoring facilities. Two auxiliary AC outlets. Frequency response 20

for under

1 dh at full nower, 15 watts rms per channel. Walnut cabinet with in aluminum trims, Inputs: phono 2-5mV and 5mV RIAA, tuner/aux 250mV. Hum and noise phono - 50db, tuner/aux - 65db, How's that for a specification!

Size 14," wide, 3," high, 10," deep

OLSON RA-310 AM/FM/MPX STEREO TUNER

POPULAR HI FI

This ROC Tuner is especially designed to match the Dison AM-395 Stereo Amplifier In price and value, as well as it's good look-

ing design! But of course it's also deal for use with any other amplifier. The RA-310 costs £10-00 less than the normal retail value, and yet it is a highly sophisticated unit, incorporating the latest solid state techniques. Operation is drift free for sup-reme station-holding capability. You can connect this Tuner to a stereo

amplifier, to a tape deck or a tape recorder. And of course H covers all the stations in the AM and FM bands, FM: 87-108 MHz, AM: 525-1605 kHz, lites: FM, 3µV; AM, 250µV. Stereo separation 30dB at 1kHz, image rejection 60dB, Size: 11 % "wide, 4" high, 71" deep.

REALISTIC SA-100B 6-WATT

Here's fabulous, exciting value in miniature! This high quality stereo amplifier measures only 9" wide - 3" high - 52" deep. And yet it has sepa-

tate ganged volume, balance and tone con-trols. Plus speaker in/out, mono/stereo, phono uner and power on/off slide switches. The ends are piled walnut, with match

ing enamelled metal top. The front panel is satin aluminium and walnut-brown enamel. Frequency response is 50 to 10,000 Hz - 3dB. Dutput 3 watts r.m.s. per channel into 8 ohms. Inputs are 100mV for both phono and tuner

STEREO TUNER

Here's another unit that gives vou fabulous value in miniature 1 Designed specifically to match the Realistic SA-100B in both annearance, size and perform

the TM-100 is superb value-for-money. It gives you the full FM AM ranges – FM, 88-108 MHz; AM, 535-1605 kHz. Sensitivities A FM 5µV. AM 250µV. Image rejection 50dB

> OLSON AM-395 40-WATT STERED AMPLIFIER An ideal unit for your new

stereo separate system. It is more than £10:00 below the normal retail price! Making the AM-395 one of Britain's best hi-fi

buys. It takes in signals from magnetic or ceramic pick-ups, tuners (see Olson RA-310) and tape decks. And it's got outputs for taping and for headphones. There are separate bass and treble controls, separate Left and Right channel volume controls. And a loudness switch for boosting the bass and treble notes when listening at low output levels. Frequency response: 20-20.004 hz 3 d8. Output: 20 watts m.s. per channel into 8 ohms. Inputs: magnetic phono 3 Om V RIAA, crystal phono 100mV; tape 100mV; tuner 160mV. Size 11 & wide, 4* high, 73* deep. The specification reads well—sounds even better!

FM-AM RECEIVER SYSTEM, MODEL 12-694 Brilliantly designed tuner/amplifier with two matching speakers. All three units in beautifully finished walnut cabinets with smart

Including
An increasing the design of the de

appearance matches the excellence of the specification

STERFO CARTRIDGE TAPE DECK, MODEL RP-1000ST

popular Lear-Jet type recording unit is the heart of fantastic RP-1000ST, which has full record and playback facilities. Automatic track change with manual over ride. Press to start button. Stereo headphone and Left and Right. Mic sockets on front panel. Dual recording level meter, and Left and Right volume controls. Built-in pre-amp. Tape speed 33 ips (9:5 cms). Frequency response playback 30-10,000 Hz: recording/playback 30-8,000 Hz Line output: fully variable 0-500mV. The RP-1000ST in-corporates all the features you'd expect in a top quality Cartridge Tape Orck. Size 16" wide, 4" high, 9" deep. Including connecting leads

£31.20

8-TRACK HOME STEREO CARTRIDGE PLAYER With this unit, you can play any standard 8-track cartridge

on the market — at a fraction of the normal retail value!
It gives you a total of 5 watts of power, to feed into two 8-ohm speakers. The frequency response is 50 to 10,000 Hz, giving you a fine tonal quality that can't be bettered at anything near this price. The E1 has separate tone balance and volume controls, giving you complete free-dom to select the sound you want to hear. Tape speed is 31 ips, and wow and flutter are both less than 0.3%. Size

R. 446 3-WAY MATCHED SPEAKERS

R.446 3-WAY MATCHED SPEAKERS
These will do justice to your amplifier – and to your pocket. At only £17-80 a pair, they are real value-for-money. pocket, Atomy 17-00 a pair, incy are lear value; 10-indiger, Each cabinet is heavily lagged and teak finished. They handle 16 watts rms (8 watts rms each). Each loudspeaker contains a large dual cone base unit, plus a separate tweeter, frequency range. 40 to 19,000 Hz. Size 14⁻⁷ high.

OLSON AM-357 4-WATT STEREO AMPLIFIER 🍳 Here's marvellous value for someone just starting to set them selves up in audio! At only £9.00 you get a fine amplifier in a

scratch resistant metal cabinet, with a smart brushed aluminu front panel. It incorporates separate tone and volume controls for each channel. Inputs are provided for turntable (ceramic car-tridge), tuner and tape deck or recorder. Frequency response: 70-20,000 Hz = 3d8. Output: 2 watts r.m.s. per channel into 8 ohms. Inputs: phono 80mV; tuner/aux 80mV. Size 8" wide, 2;" high

Headphone socket on front panel for easy access. Single tuning knob for FM and AM.

Built-in aerials, facilities for external FM aerial. Illiminated dial. Stereo broadcast indicator
light. Each speaker has 6] "bass and 3" treble units. Output: 9 watts r.m.s. per channel into
8 ohms. Frequency responses: 30 to 20,000 Hz. FM: frequency range 80-108 MHz, sensitivity 2.5µV,
stereo separation 3008, image rejection 40db.

AM: frequency range 530-1605 kHz, sensitivity 100µV.
Stres: speakers 8 wide. 12 "high and 9] "deep. And their sophisticated

25-WATT 3-WAY CRYSLER 'LIVING AUDIO' SPEAKER CE-56 This high quality speak

er has its own built-in 3-way sound response switch giving you the ideal frequency response for hi-fi, natural or mood music listening. Its beautiful, heavy, oiled walnut-cabinet

incorporates two separate speaker units an 8 mid-range with 2" concentric tweeter. Power handling capacity: 25 watts r.m.s into 8 ohms. Overall frequency response: 35-20,000 Hz. Cabinet size: $10\frac{1}{2}$ " $7\frac{1}{2}$ " $8\frac{3}{4}$ ". Exp right for matching the most modern decor

PALACE AM/FM/MPX STEREO TUNER AMPLIFIER SSA-16

his is one of the inwest priced stero tuner amplifiers on the market. It revers the full range of both AM and FM broadcast frequencies. And when you're switched to FM, an indicator lights up when a stereo signal is received — that's the time to switch to 'Stereo'! The SSA-16 has all the facilities you'd expect to find on tuners costing twice as much — separate volome, bass, treble, balance and tuning controls. Selector switch for tape, phono, AM, FM, stereo. Jack socket on front panel for stereo headphones. Frequency range: FM 88-108 MHz. AM 535-1605 kHz. Frequency response: 50-10.000 Hz. + 3dB. Power output: 4 watts total music power into two 8 ohm speakers, Size: 15" wide, 4½" high. 8" deep.

ROC 7-WATT STEREO AMPLIFIER CHASSIS SK-317 This exclusive R O C Sterep self-contained, and it costs f2-25 less than the normal i tail value! The SK-317 is a really compact unit measuring only $5\frac{1}{2}$ wide, 11

high and 62" deep. It contains its own mains power supply, and has a ganged tone control and separate volume controls for each channel. Specification: frequency response 40-17,000 Hz - 3dB; output 3-5 watts music power per channel into 8 ohms; input, phono, 600mV; signal-to-noise, ratio better than 45dR.

£15.10 OLSDN AM-372 16-WATT STEREO AMPLIFIER 🕰

ere's a really good amplifier at a really down-to-earth price less than the normal retail value! Just look at what the AM-372 will do you - reproduce signals from ceramic or crystal cartridges, AM and for you – reproduce signals from ceramic or crystal tailings. In minimals Mt uners, and lape recorders. And it gives you outputs for two sets of speakers, headphones and tape recorders. Frequency response is 30 to 20,000 Hz + 3d8.0 utput 8 watts rims per channel music power into 8 to 10 ohm speakers. Phono input 200mV. Tuner input 200mV Size: 121 wide 31 high, 71 deep.



units at lowest prices?"

TOP VALUE . TOP QUALITY ACCESSORIES THAT EVERY HI-FI ENTHUSIAST NEEDS TO COMPLETE HIS SYSTEM



and jack plug. Frequency range 30-15,000 Hz. mpedance 8 ohms per channel. ROC PRICE £2 95

EAGLE SE-30 STERED HEADPHONE

(B) This model is for the more discriminating listener. For a start the frequency range ex tends from 30 to 16,000 Hz. And you an adjust the volume of each earpiece inde pendently. There's also a mono/stereo switch For maximum comfort, the ear cushions are covered in soft leathers. ROC PRICE £7-05



TEC HR-007 HEAD-PHONE RADIO

When you want to listen to the radio all by yourself Then this will solve the problem. Separate volume and tuning controls with

EAGLE

easy-to-use knobs. Frequency range is 535 to 1605 kHz medium wave band Maximum output is 300 mW Normal Price £9-45 ROC PRICE £5-80



PLAYER, CS.8 Drive to the sound of music – with this fabulous 8-Track Cartridge Player. It gives you superb tone and power fill the car with stereo sound, Ideal for use with R.151 or R.152 speakers. Com-plete with all mounting accessories. For negative earth electrical systems only. Output: 2.5 watts per channel. Frequency range: 70-10,000 Hz. Wow and flutter: less than 0:3%. Tape speed: 3:5 cm/sec. Channel selector: automatic with manual over-ride. Mounting dimensions: $5\frac{3\pi}{2}$ × $5\frac{\pi}{2}$ × $2\frac{\pi}{4}$ ROC PRICE £27-20

WATTS RECORD CLEANERS The original "Dust Bug" Automatic Record Cleaner keeps your records clean as

they play. £1-20 Watts Disc Preener. Keeps new records like new for perfect record reproduction. 35p

307 TRANSISTOR --IZEO STEREO PRE-AMPLIFIER

PRE-AMPLIFIER
Now your amplifier
that could only reproduce
ceramic or crystal pick-up cartridges, can accept signals from moving-magnet cart-ridges! The R.307 steps up signals from between 5-20mV to 200-800 mV. Input: 5-20mV. Equalisation: RIAA. Dutput: 200-800mV flat, Frequency range: 20-22,000 Hz Dimensions: 32" - 12" - 2-2". Supply 240 VAC ROC PRICE £4 92

15-FOOT STEREO HEADPHONE EXTENSION CORD R.362
Fitted with heavy duty
3-circuit stereo plug at

one end and a matching stereo socket at the other ROC PRICE £1.30 STEREO HEADPHDNE "Y" ADAPTOR R 361 Enables you to use two sets of stereo headphones from a single socket. Fitted with male plug and two female sockets. ROC PRICE £1 30

kind within its price range. Buy them separately or at the same time as the



PHONE JUNCTION BOX

If you want easy, fingertip control of headphones and loudspeakers, here's the idea solution to the problem. All you do is connect it to your speakers and amplifier, plug in your headphones—and you're ready to take over! At the lick of a slide switch, you can have headphones alone, or speakers alone, or both together suitable for use with amplifiers rated up to 20 watts. Size: 2 1 7 3 1 7 7 1 64



ROCPRICE £1 50 R.151 STERFO

CAR SPEAKERS Smart black, tough, plastic cases, each containing a high flux 110mm diameter speaker unit. Just what you need to go with the CS.8 Cartridge Player or any other car stereo system.

cable. Dimensions: $6\frac{1}{12}$ = $5\frac{1}{12}$ = $3\frac{1}{12}$. Impedance: 8 ohms per speaker. Rating, 5 watts max per speaker, ROC PRICE £3 72



speakers match the CS.8 Cartridge Player or any other car stereo system. Fitted with high flux 110mm diameter speaker unit, and over three yards of connecting cable. Dimensions: $6\frac{11}{100}$ 6±5" - 3½", Impedance: 8 ohms per speaker. Rating: 5 waits max. per speaker. ROC PRICE£4 96



you'll find it hard to beat.

0.7 mil diamond stylus. Dut-put: SmV per channel. Frequency range: 30-18,000 Hz. Channel balance: ± 1.5d8. Channel separation: 20dB. Recommended stylus pressure: 2-4 grams. Compliance: 9×10-6 cm/dyne. ROC PRICE £4-75

EAGLE LC.07 STEREO CARTRIDGE





MATCHED STEREO LOUD SPEAKERS Here's real value

stereo speakers! Each unit comes complete with 10-foot lead and phono plug, and look really smart. Power handling per speaker: 4 watts rms. 8 watts peak. Frequency range: 40-16,000 Hz. Flux density: 8,500 gauss Impedance: 8 ohms. Dimensions: 9" high, 5½" wide, 4½" deep. RDC PRICE £9 50 pair

OFFERED AT EVEN LOWER PRICES! **EXCLUSIVE TO ROC**



A-3000 36-WATT SOLID STATE STERED AMPLIFIER The A-3000 looks as good as it sounds Giving you a big performance this superb audio amplifier has a full range of facilities on the front and rear panels. On the front all the controls you're ever likely to need plus a headphone socket. On the rear signal inputs, speaker outputs and a line

fuse for circuit protection.

Specifications: 18 watts rms per channel into 8 ohms. Frequency response 20-35,000 into 8 ohms, Frequency response 20-05,000 Hz (± 2db) Inputs Magnetic, Ceramic, Tuner, Tape, Aux, Tape Play, Size; 345mm × 300mm × 130mm, Normal Price £30-70. ROC PRICE £28-00

000

speaker terminals.

R.200 20.WATT AM/EM/MPX STEREO TIINER

AMPLIFIER What more could a hi-fi enthusiast

want! The R-200 gives you top quality reproduction

of both AM and FM programmes, including all the stereo broadcasts now available on FM. And you

have built-in facilities for recording your favourite programmes on an external tape recorder. The front

panel is carefully designed, with the latest slider controls for bass, treble, volume and balance. Alongside the dial are a meter for accurate tuning and a stereo indicator lamp that automatically hights

up when you're tuned in to a stereo signal. Dozens of other brilliant facilities including main and remote

speaker terminals.

Specifications. 10 watts rms per channel into 8 ohms. Frequency response: 25-40,000 Hz (20b) inputs: Magnetic, Ceramic, Tape, Aux. Tape Play.

Size: 388mm > 267mm > 106mm. Normal Price.

SAQ-501 50-WATT SOLID STATE STERED AMPLIFIER A really powerful unit with all the facilities you need for home entertainment

inputs for magnetic cartridge. tape, radio tuner and auxiliary Controls for bass, treble balance and volume. Head phone socket on the front panel for easy access. Loudness switch. Rumble and scratch filters.

Specifications: 25 watts rms per channel into 8 ohms. Inputs Magnetic, Tuner, Tape/Aux, Tape 20-20,000 Hz (= 1db), Size: 333mm

102mm 285mm. Normal



A - 5000 60 - WATT STATE

STEREO AMPLIFIER

With the A-5000, you're in the big-sound class — 30 watts rms per channel into 8 ohms! The circuit is all-silicon-transistor, giving you top quality sound and a mere 0.2% distortion at 25 walts output. And optimum stereo input balance is derived from the use of an IC (integrated circuit). There's no need to worry about overload or short-circuiting the output - the A-5000 has built-in protection. Specifications: 30 watts rms per channel into 8 ohms. Frequency response 15-40,000 Hz (± 2db) Inputs Magnetic, Tuner, Tape/Aux, Tape Play. (± 2db) Inputs Magnetic, Tuner, Tape/Aux, Normal Price E43:40. ROC PRICE E34:00

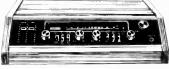


R-150 12-WATT AM/FM/MPX STERED TUNER AMPLIFIER You couldn't get better value-for-money in Stereo Tuner Amplifiers anywhere! Just look at all the facilities the R-150 gives you — bass, trebte, balance, volume, switchable AFC for drift-less reception on FM, socket for headphones on the front panel. A tuning meter, Stereo indicator, Tape output, so that you can record your favourite programmes. To name but a few, AM section covers the medium waveband —

535-1605 kHz, and the FM band 88-108 MHz.
Specifications: 6 watts rms per channel into 8 ohms.
Frequency response: 40-20,000 Hz (: 2db) Inputs:
Magnetic, Ceramic, Aux. Size: 107mm = 385mm | 263mm. Normal Price £38-30. ROC PRICE £29-90



CASSETTE OECK Precision engineered for trouble-free performance, this Stereo Cassette Deck has a fantastic range of facilities, making it a real value-for-money unit. Left and right level meters for recording, the latest slider controls for record level, switchable playback noise filter, aux/mic switch, mic input sockets, piano-key controls for record, rewind, play, fast-forward, and stop/eject, Index counter with reset button. Specifications: Frequency response: 35-12,000 Hz. Wow and flutter less than 0-25% Inputs: Mike, Aux. Din Socket, Size: 345mm . 100mm Normal Price £39-50 ROC PRICE £34 00



MR-15 AM/FM/MPX STEREO TUNER AMPLIFIER Here's a beautifully styled AM/FM Stereo Tuner Amplifier Featuring FET (Field Effect Transistor) front end FM tuner, and dual-channel IC equalizer for perfect balance, the MR-15 incorporates professional style vertical sliding controls for bass and treble. All the input/output facilities you need. Covers FM 88-108 MHz. AM 535-1605 kHz. Dutput 16 watts rms per channel into 8 ohms, Inputs Magnetic, Tape, Aux.
Tape Play, Size: 467mm 458mm 130mm, Normal Price
E67-60, RDC PRICE £54-00

1. JORY Esq. 193 EDGWARE RD, LONDON, W2 1ET.01-723 6211

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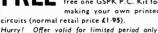
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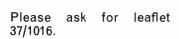


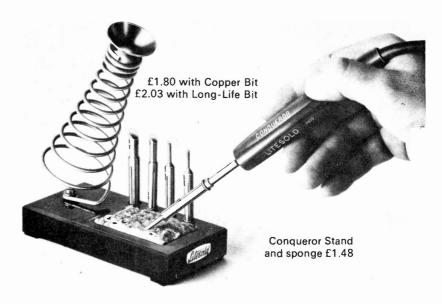
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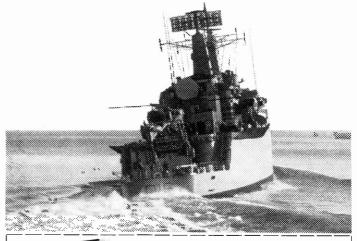
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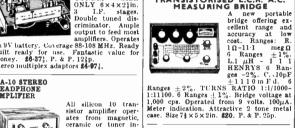


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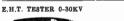
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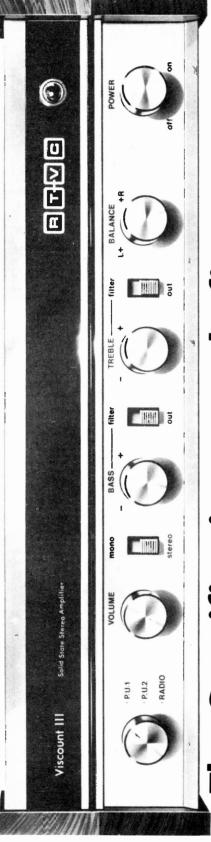
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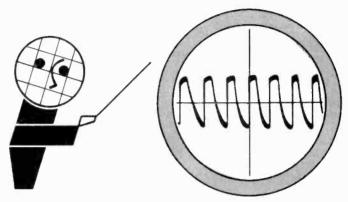




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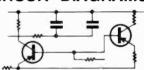
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VOL. 8 No. 6 June

PRACTICAL ECTRONIC

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BACK TO SCHOOL

r will seem remarkable to many that an industry closely identified with advanced communications and precision control of changing conditions should be unable to organise its own input of technical manpower efficiently. And yet there really does exist a serious mis-match between the educational policies pursued in the schools and technical colleges, and the electronics industry's present and future manpower needs. This unhappy fact is acknowledged in a report entitled The Electronics Industry and the Schools issued by the National Economic Development Office last March.

The Report states that greater opportunities than ever before will arise in the future for graduates, technician engineers, and technicians, especially in industries that have not previously employed electronics personnel on any large scale. However, the Report warns against too much emphasis upon graduate entry into industry while there is a real danger of deficiency in the supply of technician engineers and technicians. It is recruitment of the latter categories that should receive special attention. This point was endorsed at the IEETE Conference held at Sheffield last March, where the view was expressed that an ordinary degree for technician engineer status should be introduced.

Coming back to the NEDO Report, we read: "The proper progression of a potential technician's education and training requires a greater degree of vocational awareness and flexibility on the part of both pupils and teachers than is commonly present in schools now." The Report stresses the need for more people with a scientific and engineering background to remedy the shortage in the teaching profession. Perhaps the remedy is to be found in courses such as that planned by Edge Hill College of Education, Ormskirk, Lancs, and recently brought to our attention. Entitled Science and People this new course aims to provide "an alternative route into teaching, not only for sixth formers, but also for suitably qualified men and women who may find their present industrial occupations unsuitable or insecure.

We think this kind of feedback is much to be desired. An infusion into the schools of persons with practical industrial experience of electronics will help remove those barriers that apparently still separate some academics from practising technicians and engineers.

THIS MONTH

CONSTRUCTIONAL PROJECTS VERSATILE LIGHT EFFECTS 464 UNIT

P.E. GEMINI STEREO TUNER 483 TWO-TWENTY MINUTE TIMER 494 510 CHARGER POWER UNIT

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IGHTING effects units previously described in PRACTICAL ELECTRONICS have been primarily designed to be driven from a sound source. The audio signal has been divided, by filtering into a number of frequency bands, each of which is converted to provide an amplitude sensitive switching current to fire a thyristor or triac.

In this article the author has devised a means for frequency modulating the single channel sound source with a square wave, so that the louder the signal, the faster the flashing rate, or strobing effect.

THREE MODES

The unit described here is capable of driving filament lamps, of total power not exceeding 750 watts in three modes; these are strobe, sound-strobe and sound only. The last two modes are synchronised with sound by a feed

from a record player or similar sound source. The unit is suitable for use at parties and as a light show with discotheques or groups.

The author has built several thyristor light units and with them has often had difficulties with the thyristor driver stage "locking on" and it is understood that this is a moderately common fault. Several methods for curing this condition have been tried but were not considered by the author to be good long term solutions.

It was considered necessary at the outset, therefore, to design a reliable and effective driver and pivot the rest of the design around this. The resultant design (showed in the block diagram Fig. 1) has worked well in practice and on occasion has operated continuously for as long as ten hours without mishap. Indeed it has not yet been possible for the author to coax the prototype driver transistors into being more than luke-warm.

SOUND MODE

In the sound mode, the brightness of the lights connected to the output is controlled by the volume of the sound fed to the unit from a record player or similar system, at loudspeaker level via the input jack on the front panel.

STROBE MODE

When operating in the strobe mode the connected lights flash on and off at a rate which may be set by the panel SPEED control. The range of adjustment is not great but sufficient for some interesting effects to be produced.

SOUND-STROBE

When set to operate on sound-strobe, the unit combines the two above functions to provide a stroboscopic effect whose flashing speed is controlled by the volume of the sound arriving at the input socket, i.e. the louder the sound the faster the flash rate. The switching is carried out by a key switch; only the basic functions being shown in Fig. 1.

CIRCUIT DESCRIPTION

In all modes the thyristor is connected to mains neutral input as is shown in Fig. 2. It is at all times driven by the driver TR13 and TR14 on board 2. This driver fulfils the basic switch-on requirements of a thyristor, which is that the gate should be fed with a small positive potential, relative to the cathode, from a current limited source. The brightness control adjusts the limiting and so adjusts the brightness.

To effect sound control of the lights, the sound connected to the input jack is amplified and isolated on board one, then fed via the function switch (contacts B, C, F, E) and the light level control VR5 to TR12.

To produce a stroboscopic effect from the lights it is necessary to feed the thyristor driver with an audio signal pulsed at the flash rate required. This audio signal (of the order of 1.5kHz) is provided from the multivibrator TR8 and TR9. This signal is then gated by TR10 and its impedance at the output of the gate (C12) is lowered by the emitter follower TR11.

The signal at C13 is then routed via the function switch (contacts G, H) to VR4 on board 2. In the sound function the output at pin 2-5 is switched to signal earth, via switch contact I to stop leakage. The required amount of drive, set by VR4, is fed to the driver selector contacts (D, E, F) on the function switch. The gate TR10 is driven from TR7, the strobe multivibrator, via switch contacts J and K.

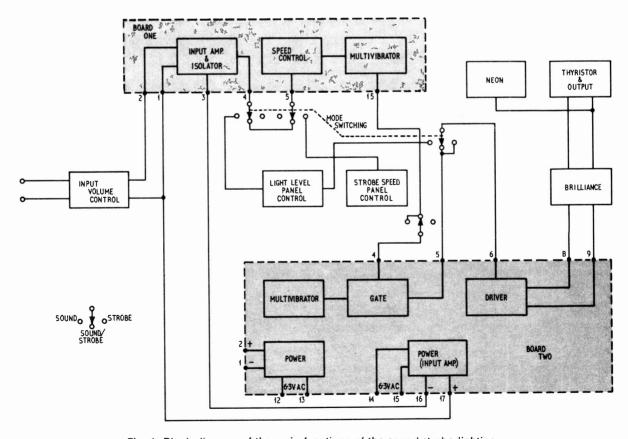


Fig. 1. Block diagram of the main functions of the sound-strobe lighting effects unit. Numbers correspond to terminations shown in Fig. 2

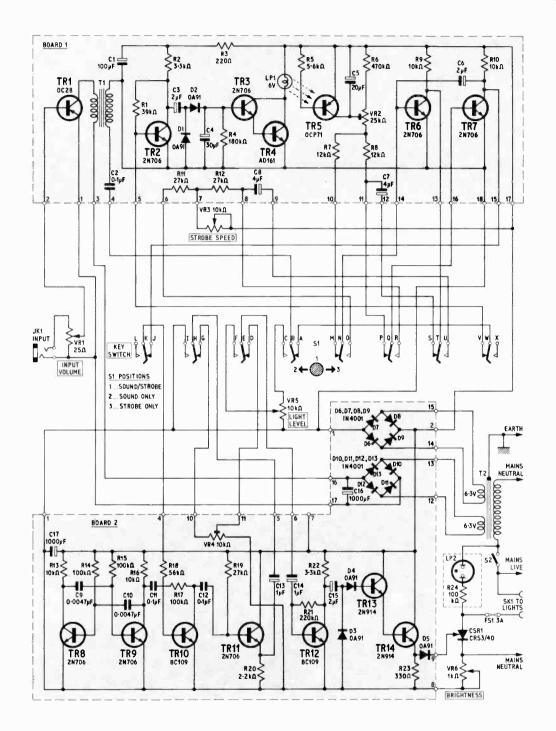


Fig. 2. Complete circuit of the effects control unit as built on two assembly boards, with the switch contacts in the centre. Movement of the keyswitch dolly in one direction (2) operates only contacts A to L. Movement in the opposite direction (3) operates only contacts M to X. The contacts are drawn as with the dolly in the centre position

The function switch selects with contacts M, N, O; P, Q, R; S, T, U, the relevant time-constant networks. The timing capacitor C6 is common to both strobe and sound-strobe function. The network for the strobe function is completed by R11, R12, C8 and the front panel "speed" control, VR3.

PHOTOTRANSISTOR

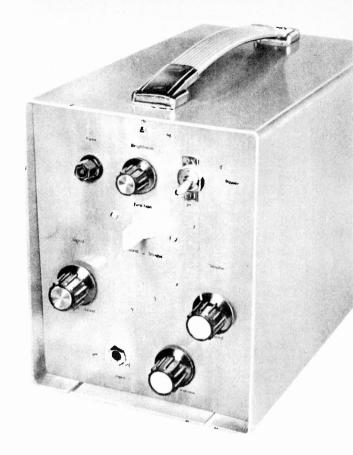
When in the sound-strobe position the function switch selects R7, R8 and C7. This network is completed as a d.c. path to the positive supply line by the phototransistor TR5 assisted by VR2 and R6. Because of this configuration, the speed of the multivibrator in the sound-strobe function may be controlled by the light emitted by the bulb LP1, which in turn is controlled through TR2, TR3, TR4, and the input amplifier by the sound supplied through the input jack.

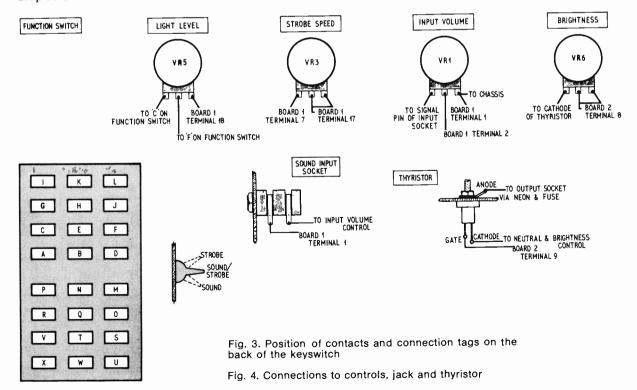
The preset potentiometer VR2 enables adjustment to be made of the amount of speed change the lamp/phototransistor gives. This configuration looks perhaps a little complicated but was considered after a trial of other methods to give the best compromise

between ease of operation and economy.

The wiring for the mains input, fuse, neon, thyristor, and transformer is shown bottom right of Fig. 2, and particular attention should be paid to the neon connections which give the neon two functions. When the on/off switch is closed, the neon functions as an output monitor and follows the output to facilitate easy setting up of the controls when the controlled lights are at a distance.

With the mains switch "off" the neon will only light when a continuous path exists from the neon resistor through the fuse and connected lights to the live mains connection. This is because the neon takes very little current and so there is little voltage drop across either the transformer or the resistor R24.





COMPONENTS . . .

BOARD ONE

Resistors							
R1	$39k\Omega$	R5	5-6kΩ	R9	$10k\Omega$		
R2	3-3kΩ	R6	470k Ω	R10	$10k\Omega$		
R3	220Ω	R7	12k Ω	R11	$27k\Omega$		
R4	180k Ω	R8	12kΩ	R12	$\textbf{27} k\Omega$		
ΑII	$\pm 10\%$. \pm	W car	rbon				

Potentiometer

VR2 $25k\Omega$ linear preset (skeleton type)

Capacitors

C1 100μF e	elect, 12V	C5	20μF elect, 10V
C2 0·1μF p	olyester		2μF elect, 6V
C3 2μF ele	ct. 12V		4μF elect, 12V
C4 30μF el	ect. 12V		4μF elect, 12V

Transformer

T1 Miniature push pull output transformer (e.g. type T/T7 or similar)

Transistors

TR1	OC28	TR3	2N706	TR6	2N706
TR2	2N706	TR4	AD161	TR7	2N706
TDE	0.0074	7 . 1 . 4 . 4			

TR5 OCP71 (phototransistor)

Diodes Lamp

D1, D2 OA91 (2 off) LP1 6V 40mA

Miscellaneous

S.r.b.p. wiring board 0.1in matrix or printed wiring board

BOARD TWO

Resistors

169191019					
R13 $10k\Omega$	R17	100k Ω	R21	220ks	
R14 100kΩ	R18	$56k\Omega$	R22	3-3kΩ	
R15 100kΩ	R19	27kΩ	R23	330Ω	
R16 $10k\Omega$	R20	2·2kΩ			
All ±10%, ¼W carbon					

Potentiometer

VR4 $10k\Omega$ linear preset (skeleton type)

Canacitors

apac	itors		
C9	0·0047µF	C14	1μF elect. 12V
C10	0·0047µF		2μF elect, 12V
C11	0·1μF		1,000µF elect. 12V
C12	0·1μ F		1,000μF elect. 12V
C13	1μF elect. 12V		,,

Transistors

	.0.3				
	2N706	TR11	2N706	TR13	2N914
TR9	2N706	TR12	BC109	TR14	2N914
TR10	BC109		_ • • • • •		

Diodes

D3, D4, D5	O A 91	(3	off)
D6 to D9	1 N4001	(4	off)
D10 to D13	1N4001	(4	off)

Miscellaneous

S.r.b.p. wiring board 0.1in matrix or printed wiring board

OTHER COMPONENTS

Potentiometers

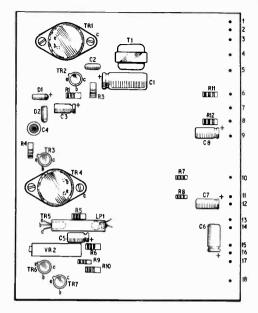
VR1 25Ω (input volume) VR5 $10k\Omega$ (light level) VR3 $10k\Omega$ (strobe speed) VR6 $1k\Omega$ (brightness)

Transformer

T2 Mains transformer. Two secondary windings, each 6.3V 0.1A or more

Thyristor

CSR1 400V 3A or higher. Type CRS3/40



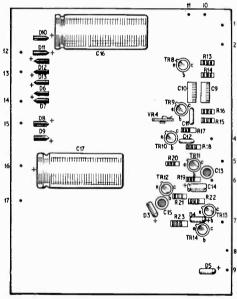


Fig. 5. Suggested positions only of components on two separate boards as on the author's unit

Switch

- S1 Keyswitch, P.O. type, three-position locking, 2×4 poles
- S2 Single-pole on-off toggle switch

Sockets

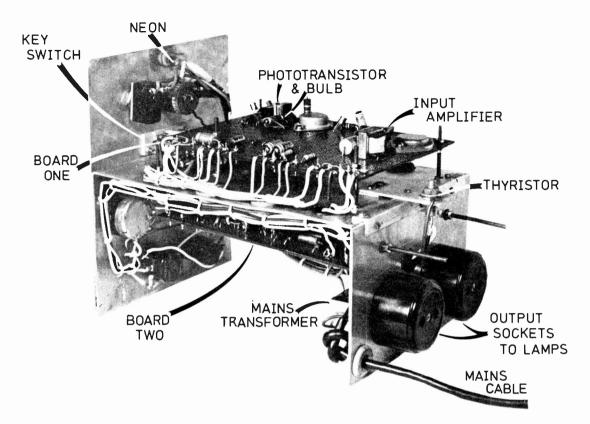
- JK1 Input jack SK1 Two pin,
- SK1 Two pin, 5A socket for lights, or two 2A sockets

Miscellaneous

Case and chassis to choice to suit board assembly LP2 Lamp assembly, mains neon with $100 k\Omega$ ballast resistor (R24)

FS1 Fuse 3A

Mains cable and light fittings to choice



This property of the circuit gives an easy check on the lights and the wiring to them and also on the fuse, for if any of them are defective the neon will remain unlit.

CONSTRUCTION

Mechanical construction, it is felt, is rather at the discretion of the constructor. The author used a spare instrument case as shown in the photographs and the chassis and the front panel were made from sheet aluminium. The case was approximately 7in by $5\frac{3}{4}$ in by $9\frac{1}{2}$ in and the unit fitted into it well. The circuitry was built up on two perforated s.r.b.p. matrix boards which were approximately $4\frac{1}{2}$ in by $5\frac{3}{4}$ in, but any suitable printed wiring board can be adopted. It is possible to build the circuitry for both board one and board two on one s.r.b.p. or fibreglass board as small as $3\frac{1}{2}$ in by 9in using a printed circuit or ready made printed wiring board.

The main concern in the layout and positioning of components is that none of the more sensitive circuits on the boards should be mounted or wired in close proximity to any large signal components or wiring. Care should be taken, for example, when mounting the power transformer and thyristor circuit and wiring them to the rest of the circuit. It is advisable to tie all wires into cable forms and then route these out of the way of the boards.

The function switch specified is a G.P.O. type keyswitch and has 24 contacts, 22 of which are used. Care should be taken with this component because any mistakes made are difficult to rectify because of the close proximity of the contacts.

In the author's unit the thyristor was mounted on a piece of glass fibre board. This was then rigidly mounted on the chassis. It should be remembered when siting this component that the anode is at the mains line potential and is therefore somewhat dangerous. Do not allow contact between the thyristor and any other metallic conductor other than the intended connecting wires.

CONCLUSION

Since its completion this unit has worked quite satisfactorily. It was found, however, that one or two minutes are needed after switch on, for the auto speed circuit to settle down. When switched on the idle speed tends to race slightly but this effect disappears after about one minute. This was not found to be too objectionable.

One thing the described design does lack is a large dynamic range. The unit has to be readjusted after a quiet record for use with a loud one. This was not felt to be too objectionable but a compressor or a.v.c. would help to overcome this.

This month's cover picture was photographed in the "Bird's Nest" pub in the Kings Road, Chelsea, London.

INDEX

An Index for Volume Seven (January 1971 to December 1971) is now available price 10p inclusive of postage.

BIN DERS

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FOURTH UK SATELLITE

The fourth U.K. satellite Ariel 4 weighing 222lbs carried five experiments relating to an integrated experiment. There is on board an experiment contributed from America and was the first to go into orbit aboard a U.K. satellite. The satellite orbit is inclined at 83 degrees at a height of approximately 340 miles.

The main purpose of the mission is the exploration of the Earth's upper ionosphere and the relationship and interaction of this area with charged particles, plasma and electromagnetic waves. There is also equipment for studying the special noise which appears in the radio spectrum in these regions.

The American experiment relates to study of the spectrum of electrons and protons from 5.0eV and 50.000eV. This experiment is under the direction of Prof. L. A. Frank of the University of Iowa.

The other experiments are cooperative between Jodrell Bank under Prof. F. G. Smith and the space research station at Slough under R. Dalziel. These experiments use two 20ft extending aerials whose length can be controlled from Earth. The object is to study radio waves set up by the Cerenkov radiations from particle streams impinging on plasma in the magnetosphere and the ionosphere. These radiations are detected by a swept frequency receiver which operates from 0.75 to 4.0MHz and a receiver with a fixed frequency of 2.0MHz.

The VLF (very low frequency) and ELF (extra low frequency) radiations in the ionosphere caused by the instability of energetic particles, are detected by very sensitive receivers, each covering a very

wide band, and fed from an aerial system slung between the satellite paddles which carry the solar power cells. Correlation of the satellite data is between Sheffield University under Prof. T. R. Kaiser with an earth based station and another installation at Halley Bay.

Finally, their is an experiment for the study of electron density and temperature which is vital to an understanding of the structure of the magnetosphere and the electrical conductivity. This is gauged by grids at the end of booms which are fixed to opposing power cell paddles.

Due to mutual interference of experiments, arrangements are available for switching off individual units to remove this hazard.

In addition to the main experiments there is a small package receiver which will count thunderstorms and their distribution.

UHURU SATELLITE

The Uhuru satellite is providing a great deal of important data. This is particularly the case with the X-ray experiments. There is an extended region of such activity in the Coma cluster of galaxies. It contains some 800 galaxies, with a powerful radio source over a wide area and central X-ray source.

There is a weak magnetic field extending through the cluster with a strength of about 100 nanogauss. The high energy electrons that traverse the field generate electromagnetic waves in the radio range. At the same time collisions between photon and electrons give rise to X-rays.

To the question: How did this weak magnetic field appear, the researchers who have measured it. G. Perola and M. Reinhardt, suggest that it may be a relic of the primeval field that once filled the Universe. A requirement of such a suggestion is that a hot gas permeates the cluster and holds these field lines. Cosmopologists have always required a certain minimum amount of matter to hold a field and in this case the amount stated is enough to satisfy them.

There is, however, an alternative possibility. If very old radio sources have decayed and left a skeleton field, an appreciable amount of gas will be needed to support it. There are other clusters, Hercules and Proteus for example, which possess X-ray and radio sources and, if it is a fact that clusters all have this type of field, its origin is of the utmost importance to cosmologists.

THE VELA PULSAR

For some time the X-ray counterpart of the Vela pulsar has been sought by theoretical astronomers. They have made a number of abortive attempts to detect X-rays and astronomers will be relieved that this pulsar does, as it should with the short period of 89 milliseconds, emit X-rays. There are some puzzling difficulties still and it may be that there are more than one family of pulsars.

JUPITER HAS DEUTERIUM

Infra-red spectrometer measurements have revealed that deuterium in the form of deuterated methane (CH₃D) is present on the planet Jupiter. It is probably the first time that this isotope has been found outside the earth and there is evidence that this spectroscopic line appears in the spectrum of Jupiter as a whole.

The low density of the planet suggests it must consist for the most part of a mixture of hydrogen and methane. What the proportion of the deuterium is to the hydrogen is difficult to determine at this stage.

EARTH RESOURCES SATELLITE

The satellite to be launched to study the earth's resources will add enormously to the survey abilities available to investigators of the environment and ecology. The ability of the return beam vidicon camera and the multispectral scanner owes much to the successful Nimbus operations.

Multispectral techniques, with a coverage beyond that of the unaided human eye, can show detail which cannot be achieved in any other way. It is possible to distinguish between fields of oats, sorgham, wheat and maize. It can be shown that diseased crops and healthy crops have a different appearance not easily detectable at close hand.

Using the scanner each type of crop has a different spectral "signature". It will also be possible to chart the movement of fish and monitor pollution worldwide. To list the benefits would occupy a good deal of space if dealt with in detail

However, the importance of this activity is so great that it is justifiable to recount some specific items. Direct benefits are the detection of forest fires and the advent of locust storms; observations of ice movements, winter and monsoon conditions in India and Japan. The study of the hydrologic cycle in the Santa River basin in Peru, snow surveys in Norway to assess spring flooding; soil erosion in Guatemala.

More than 50 scientists from all over the world will be cooperating in this venture.

The data from this satellite will be freely available to all nations.

ALPHA NUMERIC DISPLAYS

Part By R.W.Coles



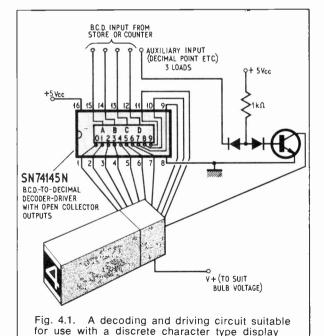
Decoding & Driving circuits for filament displays

IN LAST month's article some of the various incandescent filament displays were described. The discrete character and bar matrix type displays require different circuits for decoding the binary coded decimal (B.C.D.) into a form suitable to drive the display devices. This month some of these circuits are discussed, in particular those using the now widely available TTL integrated circuits.

DISCRETE CHARACTER DISPLAYS

The first type of display described in Part 3 last month was the discrete character type, where a separate circuit, i.e. an individual bulb, is used for each character.

A suitable decoding and driving circuit for this type of display is shown in Fig. 4.1. The input to the decoder is in the form of binary coded decimal and in order to drive the display this must be decoded into a one out of ten output.



This can be achieved using the SN74145N integrated circuit. This has ten outputs, only one of which will be conducting at a time. Thus only the bulb corresponding to the decimal equivalent of the B.C.D. input will be illuminated.

If the display device has a decimal point then a separate circuit of discrete components will be necessary. Any transistor which will withstand the current and voltage rating of the lamp is suitable.

DECODING/DRIVING CIRCUITS FOR MATRIX DISPLAYS

There is one fundamental difference between matrix and discrete character displays: the former requires a switching system which encodes the basic number or letter information into a series of on/off responses for each part of the matrix, whereas the latter uses the number or letter information directly to energise the correct character.

If the original information is in some other coded form (specifically Binary Coded Decimal, B.C.D.) then this information must first be decoded to decimal before being re-encoded in the form to drive the matrix. Only the decoder is required for the discrete type.

This decoding/encoding makes the logic of a seven segment "decoder/driver" i.e. quite complex, as can be seen from the gate diagram of the SN7447 device, which is part of the TTL Medium Scale Integration (M.S.I.) family, and which is shown in Fig. 4.2.

This complexity need be of no concern however, since the widespread use of seven segment indicators has brought the price of the 7447 down to a very low value in recent months, making it very competitive on a "decoder plus indicator" cost comparison with cold cathode tubes.

THE SN7447 INTEGRATED CIRCUIT

This decoder is typical of a variety of types available, and is suitable for directly driving the "Atron" and similar indicators, its ouputs sinking 20mA at up to 15 volts (the 7446 is selected for use up to 30 volts).

The inputs to this decoder must be in B.C.D. form, and thus only the numerals 0 to 9 are catered for; the "invalid" binary codes of 10 to 14 do produce a display, but it is meaningless. In addition to the four

B.C.D. inputs and the seven segment drive outputs, a number of other useful facilities have been provided.

The "lamp test" input can be grounded through a gate or switch to force all the segments to "on", thus showing up any open circuit filaments, a handy, and simply arranged facility.

The other input and output are the "Ripple Blanking Input" (R.B.I.) and the "Ripple Blanking Output, or Blanking Input" (R.B.O.). These two lines

OUTPUTS INPUTS 8 BLANKING ORIPPLE BLANKING OUTPUT LAMP TEST RIPPLE BLANKING

Fig. 4.2. The internal logic of the SN7447 integrated circuit. The SN7446 has the same internal logic but the output drivers can handle higher voltage

are used to achieve the leading or trailing edge ripple suppression of insignificant zeros in multi-digit displays, giving a much easier to read number.

In addition the R.B.O. can be used as an input to blank the display, a feature which is often employed to vary the brightness by switching the indicator on and off at high speed, the mark-space ratio of this on/off waveform altering the effective intensity.

ZERO SUPPRESSION

Ripple blanking itself was introduced when dealing with the 74141 decoder/Nixie tube combination in Part 2, and it is a neat little trick to prevent the display of meaningless zeros in long numbers, e.g. a six digit display system with a central decimal point would display 2.8 like this without ripple blanking:

002.800

but with ripple blanking the display would appear like this:

2.8

an obvious improvement!

The 74141 system required some quite complex gating external to the decoder to achieve ripple blanking, but with the 7447 seven segment decoder this gating is inside the device, only wire being required to make it work in a large display.

Just how easily a sophisticated six digit display can be made is demonstrated in Fig. 4.3. Here six Atrons are driven by six 7447s, and the display incorporates lamp-test, intensity control, and leading and trailing edge ripple blanking. Only one 5V supply is required, and the whole thing can be made very small, an excellent choice for a counter or voltmeter.

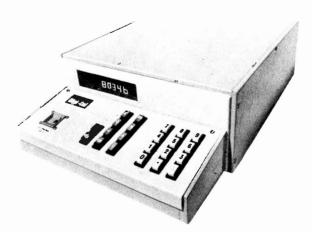
The ripple blanking is not connected for the two digits on either side of the decimal point; this improves readability and ensures that all numbers are displayed as we would write them, e.g. 0.005 will be displayed as:

0.005

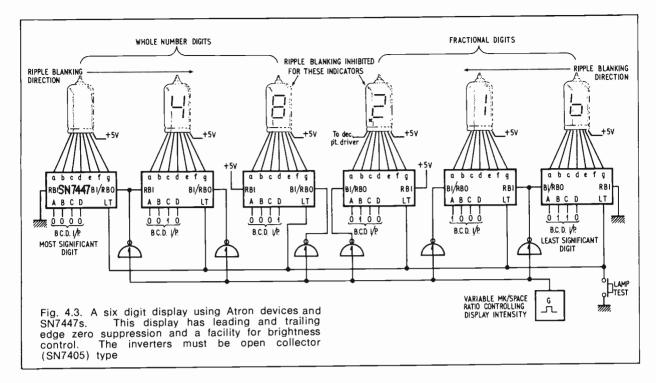
rather than as:

.005

as it would be with all decades connected for blanking.



Eight seven-segment filament indicators are used in the P.E. Digital electronic calculator to be seen next month



The intensity control scheme uses an open collector inverter package (SN7405) as the driver to each decoder. This is necessary (rather than a common wire to all decoders) because the R.B.O. is "wired-or" connected with the intensity modulation. "Wired-or" logic was described in *Making the Most of Logic IC's*, but those who have not come across this article, just remember that an open collector buffer is necessary to use this facility.

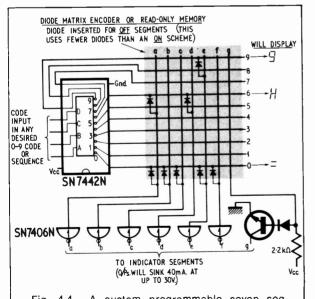


Fig. 4.4. A custom programmable seven segment decoder/driver. By suitably placed diodes, the seven segment display can be made to give characters not normally available from i.c. decoder/drivers

OTHER DECODERS

When discussing formats in Part 1 it was stated that a variety of letters and symbols, as well as the numerals, could be displayed on the seven segment design, but the 7447 does not help at all, being intended only to give 0 to 9, so what can be done to include these other character options? The answer is a "do-it-yourself" custom decoder, which is not as complicated as may be expected, and gives a high degree of flexibility.

A scheme to achieve this is shown in Fig. 4.4, where two i.c.s and a number of diodes are arranged in the form of a "Read Only Memory" (R.O.M.) which is programmed by the constructor to give any desired character out for any particular input, simply by wiring in diodes.

The R.O.M. is really a decoder/encoder combination, but it is easier to visualise when described as a R.O.M.

In this circuit a 7442 is used to generate the ten separate outputs for any of the possible B.C.D. inputs, and the particular output which is "addressed" by the input code then "reads" the particular set of diodes to produce the required on/off output arrangement. This is inverted and buffered by a hex power-driver i.c. (with one extra transistor to make the number up to the required seven) which drives the indicator directly.

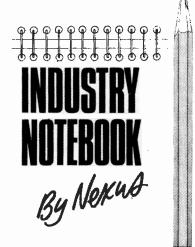
Only three examples of possible coding are shown, diodes being inserted in the matrix wherever an "off" segment is required. If a 74154 (four to 16 line) decoder is used instead of the 7442, then the complete number set can be programmed along with up to six letters or symbols, handy for those special applications encountered occasionally.

Next month: Light Emitting Diode (L.E.D.)
Displays

OUTLOOK FAIR

The first of the great trade barometers, the annual Paris Electronic Components Exhibition, while not exactly forecasting sunshine ahead was nonetheless far less gloomy than last year's event. The tone was set by the French themselves who reported a fortnight before the opening that the professional equipment sector of the French industry showed a 25 per cent growth in 1971 and an order book indicating that exports would be up by no less than 50 per cent.

Prior to the show I had been to Toulouse to visit the Motorola semiconductor plant and my personal impression was that the worst was over and while nobody was foolish enough to start counting their chickens there was a feeling of renewed buoyancy.



The impression was reinforced when I arrived at the Porte de Versailles exhibition centre in Paris where 1,000 exhibitors from 25 countries had set up shop. At the turn of the year it was feared that only a handful of British companies would be exhibiting following last year's depressing show. In the event the turnout was creditable, a number of companies having come in at the last moment.

Factors influencing comers included Britain's imminent entry to the Common Market, hopes (which were later justified) of a businessman's Budget in March. and the realisation that there was a perceptible but quite genuine upturn of trade in the UK and therefore they could afford, perhaps, to appear in Paris after all.

Any exhibitor will tell you that the Paris Salon is about the costliest exercise in the year's publicity

promotional budget—even with the financial support of the Department of Trade and Industry. But many companies still say, whatever the expense, that Paris is a "must". Plessey, in fact, used Paris as the key show of the year and balanced the books by ignoring the IEA at Olympia. I am told, however, that Plessey will be back at Olympia for the 1973 London Components show

British instrument manufacturers made a brave show either on their own stands or those of their agents. New instruments using LED's for readout were shown by Marconi Instruments and Solartron. New counters were shown by Advance Electronics, and SE Laboratories exhibited a 150MHz counter-timer with eight-decade readout. Other British companies in the instrument field were G. and E. Bradley (low cost counters), Farnell Instruments (RF signal generators), and Wayne Kerr (automatic test equipment).

Although Paris attracted about 100 fewer exhibitors this year it remains a brilliant, if tiring, exhibition. Now, having counted the cost, the salesmen are sweating it out hoping that the optimism engendered by a brisk enquiry rate will be justified in terms of orders.

YOU KNOW IT MAKES SENSE

I have long held the view that the advance of technology during past decade has outpaced the applications. That before a new development had been exploited there was always something to take its place and that development engineers almost automatically specified the newer-and generally more expensive as well as less proven-device to its predecessor.

In Britain we discovered the virtue of using the devil-you-know some little while back, a good example being the electronics in the Nimrod maritime reconnaissance aircraft which, while recognised as being among the most (if not the most) advanced in the world from the operational viewpoint, was put together largely from off-the-shelf equipment. Clever systems engineering gave us a quick and cost-effective solution to anti-submarine warfare. Even the Nimrod airframe is a modified Comet.

Now, I note that our cousins in the U.S. are feeling the financial pinch and following our lead. New contracts are specifying that current state-of-the-art components will be used as far as possible rather than exotic third or fourth generation devices still on the drawing board. This, of course, is a sad letdown for the back-room boys who have made a rich living out of inventing better and better devices which not only cost a lot more but don't always live up to expectations.

So worried are the Americans about escalating R and D costs in the defence field that an even worse fate is in store and one that would have been unthinkable in the U.S. five years ago. It is actually suggested that Uncle Sam should purchase ready-made defence systems from Europe. In fact the proposal is more than a suggestion and the British Rapier surface-to-air missile system is just one of the items now being evaluated and, one hopes, that is high on the U.S. Department of Defence shopping list.

This raises new hopes for the future of the British Clansman military communication system for which Racal Electronics recently announced the first production orders worth £11 million, divided £6 million for the British Army and £5 million for the Iranian Army. When I asked Racal Chairman and Managing Director, Ernie Harrison, if he thought there was much chance of it being specified for the U.S. Army he was not too optimistic. Nonetheless, Clansman is a production reality and is recognised as the best in the world after many vears of development, while the Americans are only now putting out tenders for a Clansman-like equipment.

The Americans are coming round to the idea that there is no profit in re-inventing the wheel or, for that matter, Clansman. They should think again before spending millions on duplication of other people's efforts.

HUMBLE PIE

Those who thought GEC were out of the semiconductor business for good, following last year's losses in the low-cost volume market and the subsequent closing of the Witham and Glenrothes plants, may yet have to eat humble pie. The custom-built business, based at Wembley, is gearing up towards a throughput of 2 million devices a year and products will include bipolars, MOS and thick-film hybrids. Full use will be made of the expertise of the famous Hirst Research Centre plus computeraided design (CAD) and advanced production processes including ion implantation.

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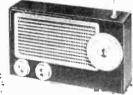
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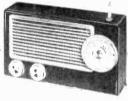
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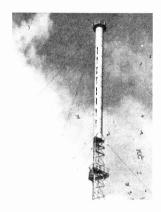


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Stereo Reception

By M. G. Foster, C.Eng., M.I.E.E.

THE FIRST BBC experimental stereophonic transmissions were broadcast from the Old Vic, in London, in 1926 using two medium-wave transmitters. In those days the medium wave band was not so congested, the power of transmitters was less and radio reception was possible using comparatively simple equipment.

By the late 1930s the position had radically altered and consideration was being given to ways of providing interference-free domestic radio services. In the event, however, it was not until after the

war that any real progress became possible.

MEDIUM WAVE LIMITATIONS

By this time the number of medium wave channels available to the BBC had become insufficient, and their quality inadequate, for the satisfactory national distribution of three programmes.

Fading, increasing interference from powerful foreign stations and the necessity for synchronized working were severely limiting the range of existing stations, mainly as a consequence of the unsatisfactory working of the Copenhagen Wavelength Plan in Europe.

To overcome these difficulties the BBC put forward a plan to establish a v.h.f. broadcasting service within the band allocated for sound broadcasting in the European Region. The BBC plan was subjected to a long series of practical tests both as regards its feasibility and in respect of the system of modulation to be used.

As nothing in this world is perfect it was only to be expected that snags existed, and among these the most noticeable from the listener's viewpoint were likely to be receiver hiss and impulsive interference such as that produced by motor car ignition systems.

ADVANTAGES OF F.M.

One result of the tests was that frequency modulation was adopted for the v.h.f. service because its use resulted in a considerable reduction in both these forms of noise and interference. It was also decided to use horizontal polarization throughout.

Propagation conditions in the v.h.f. band differ considerably from those in the medium and low frequency bands. Signal strength decreases rapidly with distance from the transmitter and terrain contours exert a greater influence on signals between transmitter and receiver; hills cast partial "shadows", similar to optical shadows.

Fading may occur at times owing to changes in weather conditions, reflections from aircraft, and similar causes depending on the distance from the transmitter

It is not possible to give as precise an estimate of the service area of a v.h.f. station as it is for one operating on medium waves. Listeners living in particularly unfavourable positions within a nominally "first class" service area may obtain only second class results, whereas those in geographically favourable locations outside such an area may still get a first class service.

Two other matters which could cause deterioration in reception are interference from stations operating on the same frequency, and interference from those

on closely adjacent frequencies.

The first can be reduced to negligible proportions by carefully siting transmitters using the same frequencies so as to provide the greatest possible geographical separation between them. The second can be mitigated by similar action but is also to some extent dependent on receiver design.

F.M. RECEIVERS

Two essential requirements for a good v.h.f. f.m. broadcast receiver are (a) that it should be provided with a limiter able to operate efficiently at the minimum field strength for which the receiver is designed, and (b) that oscillator drift should be reduced to reasonable limits. This latter point is inherent in the design of any v.h.f. receiver, but, with modern circuitry and sometimes the application of automatic frequency control it can be achieved without undue difficulty.

The first requirement is of the greatest importance because, unless the limiter does become fully operative the principal advantage of f.m., that of noise

suppression, is partially or wholly lost.

EXPERIMENTAL STEREO BROADCASTS

The v.h.f. broadcasts by the BBC passed out of the experimental stage and became a service, from the Wrotham station in Kent, in 1955. Within a year or two, however, stereophony was reaching, and interesting, a much wider audience through the medium of stereo recordings and reproducing equipment and a demand for stereophonic radio programmes began to assert itself.

A series of experimental transmissions using the pilot tone system was inaugurated by the BBC from Wrotham in 1962. These continued at intervals until. on 30 July 1966, the then Postmaster General authorised the BBC to introduce a limited stereo service using this system, which had been agreed as the stereo broadcasting system for the U.S.A.

and certain other European countries.

This system permits the stereo signal to be broadcast on a single v.h.f. channel without any significant increase in bandwidth and provides a satisfactory mono signal for listeners using existing v.h.f. receivers. It also offers a stereo service comparable with if not better than that obtainable from good stereo gramophone records.

ENCODING OF STEREO SIGNALS

Fig. 1 shows diagrammatically the distribution of the signals in the transmitted spectrum, including the 19kHz pilot tone.

The left plus right (L + R) section provides for mono reception by any f.m. receiver and, suitably combined with the left minus right (L - R) sidebands and the pilot tone in a multiplex decoder, the

three signals provide a stereo output.

To achieve this modulation the left and right signals from the microphones- or the appropriate outputs from a stereo microphone--are connected to a matrixing network from which two new outputs, the L + R and the L - R, are derived. The whole chain is shown in diagrammatic form in Fig. 2. The L + R is the equivalent of the mono signal but, as only a single transmitter is to be used, the L - R signal has also to be conveyed without its causing any interference to the reception of the mono signal.

The L + R signal normally has a frequency range of about 30Hz to 15kHz and, although the audio frequency spectrum may be considered to extend outside this range, receiver design precludes the reproduction of other frequencies. The L + R signal is therefore used to modulate the transmitter in a

conventional manner.

To handle the remaining information which must be sent simultaneously, a very stable 19kHz oscillator is used to generate the pilot tone which is used as additional modulation for the transmitter for ultimate recovery and processing in the receiver.

A second output from the oscillator is frequencydoubled to produce a 38kHz r.f. carrier. This, together with the L - R signal, is fed to a suppressed-carrier modulator in which sidebands are generated whilst the actual carrier is suppressed. The two sidebands obtained by this method provide the third source of modulation for the transmitter.

THE STEREO RECEIVER

At the receiver these well spaced signals will permit a mono set to reproduce only the L + R, or audio signal, shown on the left in Fig. 1, thus providing the mono programme. In a stereo receiver, however, one of two alternative types of decoder is present.

In the sum and difference type, shown in the diagram Fig. 3, the received f.m. signal is fed to three filters. The first, being tuned to pass only audio frequencies, rejects all but the L + R signal. The second accepts only frequencies above 23kHz and thus rejects the L + R signal and the 19kHz pilot tone, but passes the L - R sidebands.

The final filter, being sharply tuned to 19kHz,

rejects all but the pilot tone. The pilot tone is passed through a frequency doubler whose output is fed, together with the L - R sideband signals into a demodulator at the output of which the L - Rsignal is recovered.

The L - R and L + R signals then pass into a matrix network from which the original L and R signals are reproduced. This decoding system is, in essence, a reversal of the transmitting arrangements but it suffers from the disadvantage that each of the filters delays the signal by a different amount thus necessitating the inclusion of phase-correcting networks to re-establish the correct phase relationship between them prior to reproduction. This entails added complication and cost.

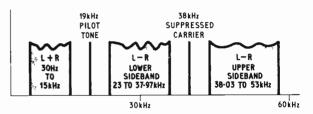


Fig. 1. Diagram showing the various components of the modulation of an f.m. stereo transmission. The signal bands are spaced for clarity; their positions on the frequency scale are only approximate

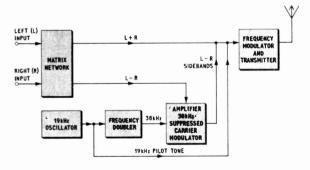


Fig. 2. Block diagram showing the method of modulating an f.m. transmitter with a multiplex stereo signal

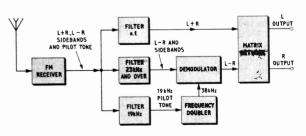


Fig. 3. Block diagram of a sum and difference type stereo decoder

SWITCHING DECODER

The second type of decoder, the switching decoder, was developed to overcome the disadvantage inherent in the sum and difference type. It is shown in schematic form in Fig. 4.

The 19kHz pilot tone is again extracted using a suitable filter and is frequency doubled as before to produce the 38kHz sub-carrier. This is fed to two demodulator units in which it is used as a switching signal to direct the entire output alternately to the left- or right-hand channel.

The v.h.f. transmissions certainly provide the best quality reception of sound radio available in the U.K. Interference from foreign stations is virtually eliminated and the f.m. system provides a much wider frequency range than is possible on the a.m. services on medium wave. Radio 3 also offers the stereo service over a wide area of the country as shown in Fig. 5.

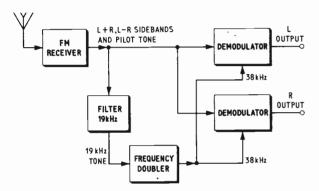


Fig. 4. Block diagram of a switching type stereo decoder

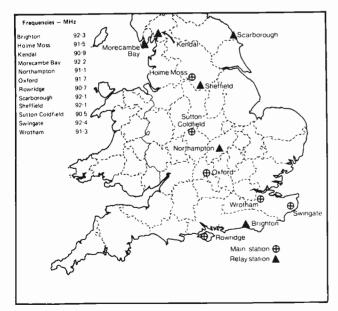


Fig. 5. The present area served by Radio 3 stereophonic transmissions. Good stereo reception should be obtainable over most of the area indicated by the unshaded part of the map, but the receiving aerial requirements are far more critical than those for monophonic reception

V.H.F. AERIALS

If, however, full advantage is to be taken of the improved reception which the service offers it is essential that a suitable aerial be used.

V.h.f. aerials are directional and thus the signal strength received depends upon the position of the aerial in relation to the direction of the transmitter. Freedom from interference and noise in a v.h.f. receiver depends partly on the strength of signal delivered to the receiver which, in turn, is dependent on the aerial.

The better the aerial the better the reception and the greater the freedom from noise.

This is particularly important when stereo programmes are being broadcast, as the slight reduction in the mono service area due to the fact that a small proportion—9 per cent to be exact—of the permissible deviation available for the f.m. transmitter is used to carry the 19kHz pilot tone; also some of the programme is carried in the supersonic part of the spectrum around 38kHz.

The only effect this is likely to have on a mono receiver is to make it slightly more susceptible to background noise, particularly motor car ignition noise if the receiver is located near a busy road. Tests have shown, however, that in nearly every case where such degradation was perceptible, it could be cured by the use of a more efficient aerial.

STEREO SIGNAL TO NOISE RATIO

A situation similar to that described above also exists when a stereo receiver is used, but there is an additional, inherent, reason for some worsening of the signal to noise ratio. The mono receiver is concerned purely with noise occurring within the frequency range 30Hz to 15kHz, whereas the stereo receiver must receive frequencies up to 53kHz, and thus any additional noise in this part of the spectrum, together with any intermodulation products falling within the audible range, will cause some degradation of the reproduced sound.

Some amelioration of these undesirable features can be achieved by suitable decoder design but, once again, practical experience has shown that very considerable improvement in the stereo reception at a given location is almost always possible by using a more efficient aerial to provide a higher input to the receiver.

From the foregoing it will be seen that, given a satisfactory receiver and a reasonable signal strength probably the most important single factor affecting v.h.f. reception in either mono or stereo is the use of a really efficient aerial to deliver the signal to the set. So important does the BBC consider the question of aerials that it has produced a leaflet entitled V.H.F. Receiving Aerials which can be obtained on request.

ADJACENT CHANNEL INTERFERENCE

In certain areas there is also the question of adjacent channel interference to be considered when receiving a stereo broadcast. Such interference can be caused by stations separated in some cases by only 200kHz. Under these circumstances the fifth harmonic of the 38kHz sub-carrier—190kHz—produces a difference frequency of 10kHz which is carrying both amplitude and frequency modulation.

This in turn gives rise to whistles or warbles, often referred to as "birdies". The insertion of a low pass

filter between the discriminator and decoder to remove the 190kHz component prevents this undesirable effect. The filter should be designed to pass only those frequencies below about 70kHz.

23KHZ PILOT TONE

On page 311 of the April 1972 issue it is stated that the BBC "have the unfortunate habit of putting a 23kHz pilot tone on top of mono programmes" and it may be of some interest to outline the reason for this tone.

Continuity monitoring of frequency-modulated transmissions over radio paths is the purpose of this low-level pilot tone. Originally the frequency used was 20kHz but, with the introduction of the stereo service, it was changed to 23kHz to prevent any mis-switching of stereo receivers.

The tone is injected into the audio system at a transmitting station at a level of -30 dB with reference to zero level and produces approximately 4.5kHZ deviation at the transmitter output.

At the receiving station it is detected by a receiver, filtered out and used to start up or close down transmitters, or to change from one programme source to another.

If the tone is to be used on the next radio path it is removed from the programme by a low-pass filter and tone from a local oscillator substituted prior to re-transmission. Some systems rely on detecting the main station carrier to start or close down relay transmitters. These, however, suffer from the disadvantage that it is possible for noise to produce sufficient output from the receiver after the main station has shut down for the relay to remain switched on.

LISTENING TO STEREO

For best stereophonic listening the two loudspeakers should ideally be spaced 6 to 12 feet apart and the listener should sit at a point which is equidistant from them and preferably not closer to them than their distance apart.

The programme announcements will usually be made from a central position and the receiver should be adjusted using the balance control, if fitted, so that the speaker's voice appears to come from a point midway between the loudspeakers.

The acoustics of the listening room will affect the results and different listening and loudspeaker positions should be tried to obtain the best result.

SERVICE AREA

At present the stereophonic transmissions are available to listeners within the service areas of the BBC's v.h.f. transmitting stations at Wrotham, Rowridge, Sutton Coldfield, Holme Moss and Swingate and of the following relay stations: Brighton, Oxford, Northampton, Sheffield, Scarborough, Morecambe Bay and Kendal, and the approximate area of the U.K. in which they can be received is shown in Fig. 5.

Stereophonic programmes are available in these areas on v.h.f. Radio 3 and are marked in Radio Times by a special "S" symbol. The emphasis is mainly on music, because this type of programme derives the greatest benefit from stereophonic reproduction.

Equipment is being installed to enable the number of stereophonic programmes in Radio 3 to be

increased. The BBC would like to extend stereophony throughout the country and to more than one of the radio services and it is hoped that the necessary finance can soon be found to bring this worthwhile improvement to the listener. In the meantime it is planning to expand its stereo service considerably during the next few years. The extension beyond the present Radio 3 service will take place in three phases.

EXTENSION OF STEREO SERVICE

First the installation of stereo origination facilities for Radio 2 (with Radio 1) and Radio 4. This has called for a major re-equipment programme involving modifications to the continuity suites and central control equipment in London as well as a considerable increase throughout the United Kingdom in the number of tape machines, gramophone desks, studios and outside broadcast units equipped for stereo.

This phase is already in progress, and it is expected that it will be possible to originate a major proportion of stereo programmes on Radio 2 by the end of 1972, and also to make possible the transmission of some stereo programmes on Radio 4. Further increases in stereo capability will continue during the succeeding years.

PULSE CODE MODULATION

The second phase concerns the extension of Radio 2 and Radio 4 stereo to those transmitters already radiating Radio 3 in stereo. For this a new system of super high frequency (s.h.f.) radio links is planned, using pulse code modulation (PCM).

The PCM system to be used on the s.h.f. radio links has been developed by the BBC. It will carry ten audio circuits. Each stereo programme will use two circuits, for the L and R channels, and the stereo coding will be carried out at each main transmitting station.

The PCM system will provide improved quality in respect of both audio bandwidth and signal-tonoise ratio, from which mono as well as stereo listeners will benefit. It thus forms part of the BBC's plan to improve still further the quality of its v.h.f. transmissions throughout the country.

It is expected that the three-network service, which involves the construction of several new radio link sites on the main route, will be available in the London area and the Midlands by the end of 1972 and in the North of England during 1973. Rowridge, serving central southern England, will be included in this phase and a full stereo service from Belmont, serving Lincolnshire, will follow the extension to the North of England.

THIRD PHASE

The third phase of the plan is the extension of the three network stereo service northwards to Central Scotland and westwards to the Bristol Channel area. The Post Office Corporation and the BBC are working towards this phase which it is expected will start in 1974.

ACKNOWLEDGEMENT

The author wishes to thank the Director of Engineering BBC for permission to publish this article.

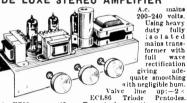
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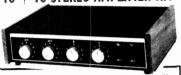
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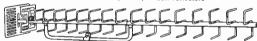
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bread. (14) Radio Control Tone Receiver. (15) Transistor P/P Amplifier. (16) Intercom. (17) 1-valve Amplifier. (18) Reliable Burglar Alarm. (19) Light-Seeking Animal,
Guided Missile. (20) Perpetual Motion Machine. (21) Metal Detector. (22) Transistor
Tester. (23) Human Body Radiation Detector. (24) Many/Woman Discriminator.
(25) Signal Injector. (26) Pocket Transeciver (Licence required). (27) Constant
Volume intercom. (28) Remote Control of Models by Induction. (29) Inductive-Loop
Transmitter. (30) Pocket Triple Reflex Radio. (31) Wristwatch Transmitter (Wire-less
Microphone. (32) Rain Alarm. (33) Ultrasonic Switch/Alarm. (34) Stereo Preamplifier. (35) Quality Stereo Push-Pull Amplifier. (18) Light-Beam Telephone
"Photophone" (37) Light-Beam Transmitter. (38) Silent TV Sound Adaptor. (39)
Ultrasonic Transmitter. (40) Thyristor Drill Speed Controller. Plus 10 Photoelectric
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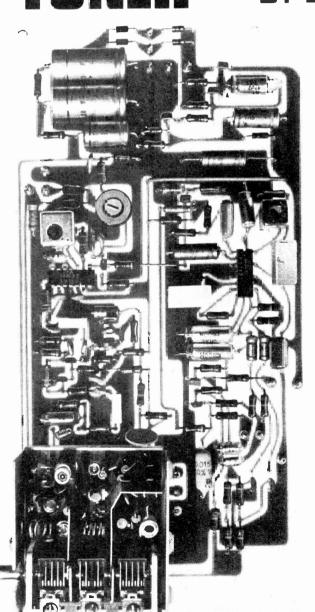
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Send a S.A.E. for full details and a brief description of all kits and Projects.

PEGEMIN

STERED TIMES

PART THREE BY D.S.GIBBS & I.M.SHAW



This is the final article describing the printed circuit board assembly, cord drive, and setting up procedure.

COILS

Coil L2 is available as a ready made unit, but L1 has to be specially wound by the constructor on a Neosid NS/E3 former. Wind 17 turns of 30 s.w.g. enamelled wire neatly on to this former and solder the ends to the pins shown in Fig. 21. The winding should be secured with a smear of polystyrene model cement or a single layer of coloured adhesive tape, to ensure that the tuning of the coil remains stable.

Now apply a little polystyrene cement to the bottom of the coil former and slip the ferrite sleeve over the coil. Then apply a dab of polystyrene cement to the top of the coil former and push on the polythene clamp ring. Leave for 30 minutes to dry and then screw in the ferrite core until the top of the core just protrudes from the top of the coil former. Finally, carefully solder the 47pF tuning capacitor (C16) in place.

It is very important to handle the ferrite coil former for L1 with great care, as it is very fragile, and any damage could alter the properties of the

complete assembly.

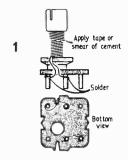
PRINTED CIRCUIT BOARD

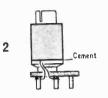
Most of the components are mounted on a single glass fibre printed circuit board. The conductor pattern of this is shown in Fig. 22 and the component layout in Fig. 23. If you do not purchase a ready drilled p.c.b. you will need a No. 60 drill for component and i.c. leads; a No. 46 drill for the turret tags. Solder the tags to the copper before any of the components are inserted.

The wiring of the board is self-explanatory but the following sequence is preferable, and will minimise the risk of damage to the integrated circuits and

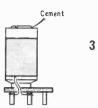
the tuner head.

Insert and solder all the resistors except R14, and then all the capacitors. Mount the two coils. The semiconductor devices can now be inserted, but before doing so make sure that the soldering iron is earthed and that the circuit board is completely "floating" above earth (for example, placed on an insulated table top).





- 1. Carefully wind on 17 turns of 30 s.w.g. enamelled wire and solder to the pins shown. Secure the winding with a smear of polystyrene cement or a single layer of adhesive tape. Handle the former very carefully or it will break
- 2. Apply a little polystyrene cement to the bottom of the coil former and slip the ferrite sleeve over the coil
- Apply a dab of polystyrene cement to the top of the coil former and push on the polythene clamp ring. Leave for 30 minutes to dry
- 4. Screw in the ferrite core until it just protrudes from the top of the coil former. Use a trimming tool, a screwdriver may break the core. Carefully solder the tuning capacitor in place as shown
- 5. Insert in the printed circuit board, together with the screening can



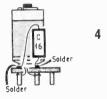


Fig. 21. Construction of L1

Fig. 22. The printed circuit board, copper side (full size)

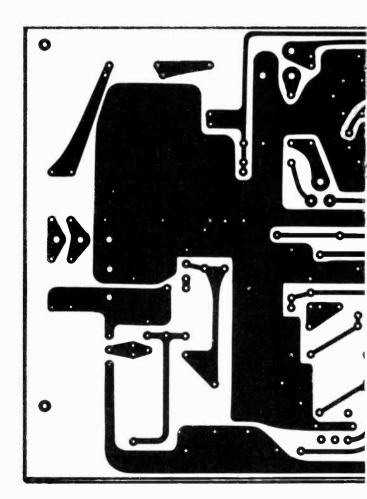
Fig. 23 (top right). The components assembled on the printed circuit board

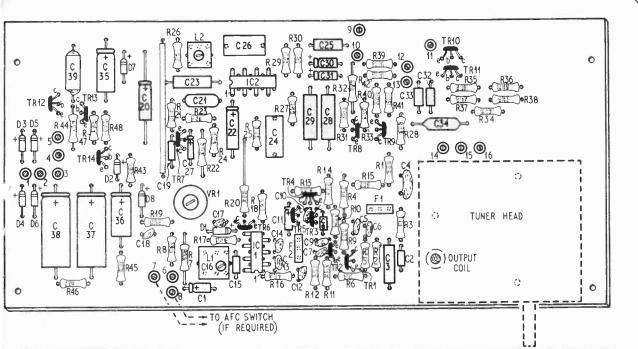
FURTHER NOTES

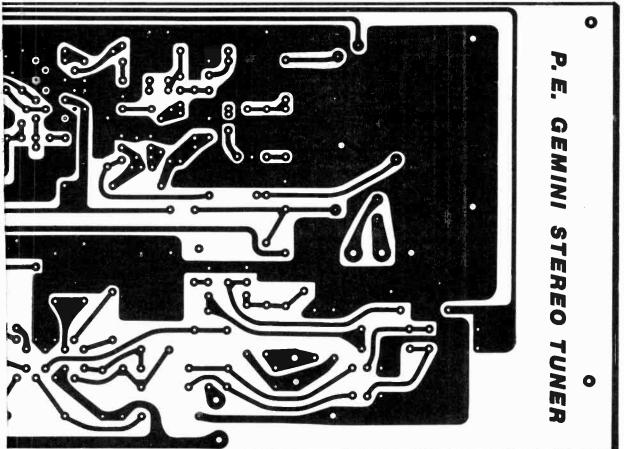
Some readers have informed us that they have had cases of the ZTX550 (TR12) blowing up.

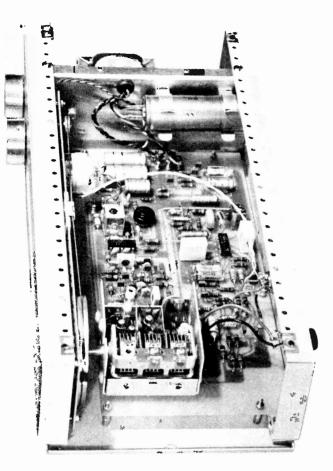
The authors have investigated this and have been unable to duplicate the fault, even when operating the power supply at a considerable overload. As the ZTX550 is worked within its ratings they can only assume that these cases were due to "rogue" devices, but TR12 does run hot and constructors who would like an additional safeguard can fit a heat dissipating clip if they wish. Suitable types are the I.E.R.C. type RUR67B1U or the Redpoint type 92DC.

In Fig. 14, the dimension from the left-hand end of the panel to hole A for the pilot lamp should be $2\frac{\pi}{4}$ in.









Semiconductor devices can easily be damaged by high voltage transients from unearthed soldering irons, and a damaged CA3090Q will cost you over three pounds to replace. Heat shunts are not necessary with silicon semiconductors provided the joint is made quickly with a clean hot iron.

An iron of 15 or 25 watts with a small bit (less than ¼in diameter) is preferable, and 22 s.w.g. cored solder should be used. Take great care not to allow solder "bridges" between adjacent tracks on the printed circuit board.

Finally, mount the tuner head and solder the pins that protrude from the underside and pass through holes in the board.

WIRING UP

The mains transformer and C40 are mounted on the small chassis plate shown in Fig. 20 last month. The mains switch is mounted on the front panel and the transient suppressor capacitor C41 should be wired directly on the switch terminals that are connected to the transformer. Sleeve the leads of this capacitor to prevent the possibility of a short circuit to the case. Mount the fuse holder, mains socket, aerial socket, and audio output socket on the back panel.

The printed circuit board is supported on five ½in spacers, and it is advisable to place a thin insulated washer over the top of the centre spacer because of the closeness of one of the copper tracks. In some cases it may be necessary to increase or decrease the height of the p.c.b. slightly to ensure that the tuning

drum fits inside the front panel without touching the top or the bottom. The top of the tuning drum should be approximately level with the top of the inner front panel.

There is very little wiring to do; this is shown in Fig. 24. If you are using a 75 ohm aerial the braid of the coax feeder should be connected to tag 16 and the inner to either tag 14 or tag 15 (it doesn't matter which). For a 300 ohm balanced feeder connect to tags 14 and 15; tag 16 is not used. The wiring shown in Fig. 24 is for the usual 75 ohm arrangement.

CORD DRIVE

Make a loop of nylon or similar drive cord approximately 25 inches total length and thread it around the drum, pulleys, and tuning drive as shown in Fig. 16 last month. Wrap two turns around the small drive shaft. It will probably be necessary to experiment with the length of the drive cord to obtain a satisfactory tension. If the cord is too slack remove it and shorten it slightly, or if it is too tight try a slightly longer loop.

Now turn the tuning knob so that the vanes of the tuning capacitor are fully interleaved. Slip the pointer over the front panel, slide it up to the 88MHz mark on the scale, and fasten to the cord. Make sure that the drive works smoothly over the whole length of the scale. If it slips the cord may be too slack, or there may be oil on the drive shaft. If everything is satisfactory the pointer can be secured with a blob of adhesive.

SETTING UP THE R.F. CIRCUITS

Before switching on check the board and the wiring carefully for errors, particularly the power supply. It is a good idea to complete the power supplies and test these before the integrated circuits or the tuner head are wired into circuit. Both power supplies should give between 11:2 and 12:5 volts

supplies should give between 11·2 and 12·5 volts.

Initially, resistor R14 should be left out or one end disconnected, so that the tuner head and the i.f. amplifier do not operate. Set VR1 to it's midposition, and if necessary adjust the mechanical zero of the tuning meter. Now switch on and adjust VR1 to bring the tuning meter back to zero. Switch off, disconnect the tuner from the mains, and solder R14 in place.

Temporarily short out the a.f.c. by connecting a link between tags 7 and 8, or if you have fitted an a.f.c. switch put it in the "out" position. Connect the tuner to an audio amplifier and the aerial socket to a suitable dipole aerial. Now switch on and tune the receiver through the f.m. band. It should be possible to find a station, although it will probably be badly distorted at this stage. As you tune through the station the background noise will fall and then will start rising again. Tune for minimum noise (pay no attention to the signal at this point as minimum noise may well coincide with minimum signal), or alternatively try to set the tuning midway between the two points where the noise becomes perceptible, as shown in Fig. 25. Now insert a trimming tool into the core of L1 and adjust it to bring the tuning meter back to zero. The reproduction should now be virtually noiseless and undistorted. Check that the tuning meter swings approximately equal amounts either side of zero as you tune through the station, and if not make a slight

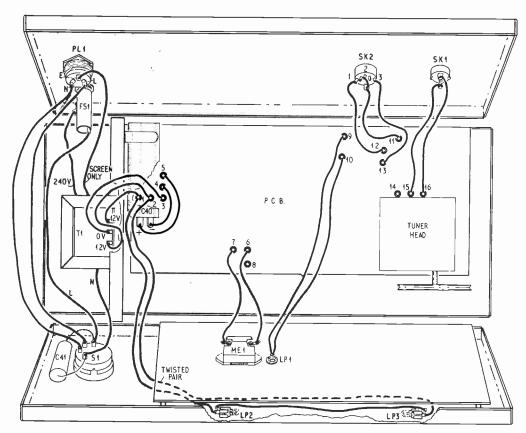
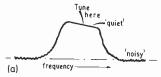


Fig. 24. Connections from the printed circuit board turret tags to components mounted on the case



1. When you first switch on, the response of the discriminator as you tune through a station will probably be like this. Try to tune to the centre of the quiet band. This may well coincide with minimum signal



Adjust the core of L1 to bring the tuning meter back to zero. Use a trimming tool, a screwdriver will break the core.

If your tuning was not quite accurate to start with the response may look like this



3. Tune through the station and check that the tuning meter swings approximately equal amounts either side of zero. If not, make a slight readjustment to L1

Fig. 25. Adjustment of L1

readjustment to L1. Finally, adjust the output coil of the tuner head for minimum background noise. This is best done on a stereo transmission. This adjustment is only required to take up the tolerance of the external tuning capacitors (C2 and C3) and it should not be necessary to tune the core more than about one turn either way. Use a hexagonal nylon trimming tool of the correct size as a screwdriver will break the core and may damage the coil as well. ON NO ACCOUNT MUST ANY OTHER ADJUSTMENTS BE MADE TO THE TUNER HEAD.

Disconnect from the mains and remove the short on the a.f.c.

ALTERNATIVE METHOD

If you live in a strong signal area and have a test meter of 10,000 ohm/volt or more there is a more simple and accurate method of adjustment as follows:

After adjusting VR1 as described earlier, short out the a.f.c. and solder R14 back in place. Connect an audio amplifier and an aerial. Connect the test meter, on the 10V range, to the collector of TR5 and tune in to a station.

Normally the collector voltage of TR5 will be about 0.2V, but when a strong signal is being received it rises. Adjust the tuning for maximum reading on the voltmeter, and adjust the output coil of the tuner head for maximum. Then, without altering the tuning, adjust the core of L1 to bring the tuning meter back to zero.

BBC STEREO TEST TRANSMISSION

Test No.	Time (approx	Left Channel (A)	Right Channel (B)
1	23.42	250Hz at zero level	440Hz at zero level
2	23.44	900Hz at +7dB	900Hz at +7dB antiphase to left channel
3	23.48	900Hz at +7dB	900Hz at +7dB in phase with left channel
4	23.49	900Hz at +-7dB	No modulation
5	23.50	No modulation	900Hz at +7dB
6	23.51.20	Tone sequence at —4dB. 60Hz, 900Hz 5kHz, 10kHz. Repeated	No modulation
7	23.52.20	No modulation	Tone sequence as at 23.51.20
8	23.53.30 23.55	No modulation Monophonic transr	No modulation mission

Note: If programme material extends beyond 23.42, test transmission begins two minutes after close. To facilitate channel identification and adjustment of channel crosstalk, 250Hz is transmitted in the left channel only from about four minutes after the end of Radio 3 until 23.55.

Zero reference level corresponds to 40 per cent of maximum modulation applied to either stereo channel before pre-emphasis.

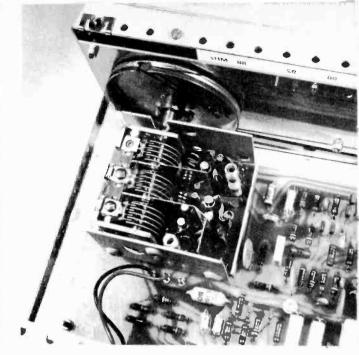
The prime purpose of the above test transmissions is described on the BBC leaflet mentioned in the text of this article.

STEREO DECODER

Screw the core of L2 fully down and tune in to a stereo transmission. The pilot indicator lamp should light; if it does not screw the core of L2 up slightly until the lamp comes on. Make sure that the lamp does not light on a mono programme, due to the stereo decoder locking on to the 23kHz signal which the BBC sometimes transmit.

The exact tuning of L2 is not critical since once the phase lock loop locks, the coil is pulled into tune by the reactance circuit. However, best results can be obtained by adjusting the coil on the test tones which are transmitted by the BBC every Wednesday and Saturday night after 11.30 p.m. Details of these tones are given on information sheet 1605 issued by the BBC Engineering Information Department, Broadcasting House, London WIA IAA.

The core in L2 should be adjusted to give maximum separation, i.e. minimum signal in the right-hand channel when only the left-hand channel is being transmitted, and vice versa. You might have to make more than one attempt at doing this as no announcements are made between the various test tones transmitted and it is very easy to get lost. This completes the setting up of the tuner.



MONO TUNERS

Constructors who do not require stereo operation can build a mono version of the tuner as follows:

1. Omit all the parts associated with the stereo decoder, including R21 to R42, C21 to C34 and TR7 to TR11. Leave C20 in circuit.

2. Increase C19 to $0.01\mu\text{F}$ and take the output from point X to the output socket via a capacitor of $0.22\mu\text{F}$. The load resistance presented by the amplifier should be 47 kilohms or greater.

AERIAL

In strong signal areas the tuner will probably perform adequately from a short piece of wire connected to the aerial socket, but for best results, particularly from stereo transmissions, a dipole aerial of correct dimensions for the area of reception should be mounted as high up as possible. The signal-to-noise ratio of stereo programmes is always worse than mono programmes because of the increase in bandwidth from 15kHz for mono to 53kHz for stereo. Also there is a slight drop in signal level on stereo. In order to achieve the best possible stereo results, the need for a good aerial system cannot be over-emphasised.

ACKNOWLEDGEMENT

We are grateful to Ferranti Limited for permission to publish this article.







The central apparatus room at the Churches Television Centre



The latest Ampex Video Tape Recorder, type



Churches TV Centre goes Colour

N AN AGE when congregations are slowly dwindling away even the Church has to look to the mass media as a fast and efficient method of spread-

ing the message.

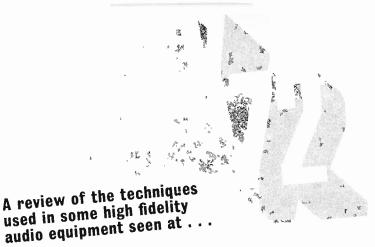
The Churches Television Centre has been established since 1959 and has three main aims: to train people on both sides of the camera; to produce material for religious education; and to carry out research into the problems of communication. The centre is financed by a Trust Fund created by the late Lord Rank.

The Centre has a fully equipped closed circuit studio at Bushey near Watford, and with its latest planned changeover to colour, at an estimated cost of nearly a quarter of a million pounds, it is expected to become the most up to date closed circuit system in the world.

The new colour equipment includes the advanced Marconi Mark VIII Automatic colour cameras (seen undergoing tests, bottom left). With automatic lineup and colour balance achieved within three minutes of switch on, as compared with the normal half hour, they are claimed to attain new standards in both performance and operational simplicity.

This system together with the latest Ampex Video Tape Recorder (upper left) will enable the Churches TV Centre to produce programmes of a quality suitable for any of the major broadcasting authorities.

Marconi Mark VIII colour cameras under test



By M. A. COLWELL

ow valuable are technical specifications to the buyer of hi fi equipment. "Vital!" you might say, and we would be inclined to agree with you. But does this mean that all other considerations go by the board in the potential buyers' assessment.

If one stops to think about this, one will then realise that perhaps these other considerations (for example, aesthetic appearance, personal auditory opinion, suitability for the intended auditorium) have a very important place in equipment choice.

Listening to recorded music over a period of time often spurs the listener to make auditory comparisons due, no less, to a wide variety of recording qualities. Is there something wrong with the recording, or is it the equipment? Such a perplexing problem is very real to the chap who has, by this time, joined the bands of hyper-sensitive critics looking for ways to cure that undesirable feature of his musical pleasures.

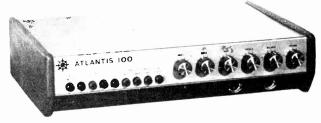
TRIP TO SONEX

Picture this chap for a moment embarking on his first trip to Sonex (such as held recently at the Skyway Hotel, London Airport); rows of small rooms, on four floors—most of which are emitting recorded sound in two or perhaps four channel stereo. Where does our perplexed friend start—with a catalogue? 'Fraid not! This is one exhibition that does not seem to believe in such necessities.

We could not even find the programme of seminar titles and times, until someone in the Press office made enquiries for us. We could not find many photos; we really had to hunt the whole four floors for the latest in audio equipment techniques.

But where was all that four-channel stuff we were promised would sweep the market (that was a couple of years ago). Still in the hands of the Japanese? like Sansui and JVC. Where is that British sense of innovation; still riding the stiff upper lip perhaps! Oh well! perhaps next year, or the year after?

Helme Atlantis 100 55 watt amplifier



CYBERNETIC HI FI

Going back to our friend with a desire to find out what he is missing, the best start is, believe it or not, the end of the chain, the loudspeaker, or sometimes referred to as "the weakest link".

However, some of the modern loudspeaker systems offer improvements over several five-year-old predecessors and if you are anxious to cut on size without loss of quality, we suggest you try to arrange a listen-in to "Servo-Sound Cybernetic Hi Fi". Don't be fooled by the fancy title; you should be truly surprised by the results.

These are small speakers (approximately 11 in \times 10¼ in \times 7in) that reproduce church organ music, bass guitars, full orchestras, as good as several others six or more times the size. The secret is in the feedback technique that the makers use in conjunction with the built-in power amplifiers.

The "cybernetic circuit" senses the motion of the speaker diaphragm, compares this with the original signal, and corrects the drive signal to balance the speaker output. The significant feature is the suppression of undesirable cabinet resonances, typical of such a size.

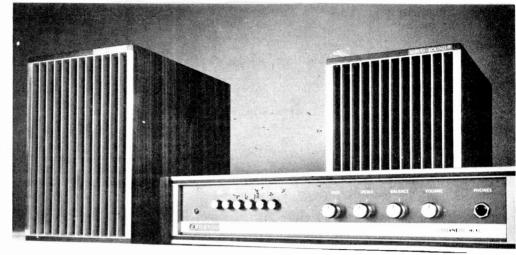
The price quoted for the unit, which includes the 15 watt (r.m.s.) amplifier is £55. A more robust version with ceiling or wall mounting cradle, for public address or discotheque work is offered for £64. Further details of these and stereo mixers, attenuators, and pre-amplifier control units are available from Sono-Sound, 5 Queen Street, London, EC4N ISU.

SPEAKERS

BBC monitors are the currently accepted standard by which to assess speaker performance, following the extensive trials carried out over the past few years. Incorporated in these are, among others, the rolled p.v.c. cone suspension pioneered by that fast growing firm KEF.

Now that KEF have successfully established themselves as quality manufacturers, they have breathed new life into the smaller bookshelf styles with the Coda (£18.75 each plus purchase tax) and the Cantor (£22.25 each plus purchase tax), both of which are available as matched pairs.

The Coda is intended to handle up to 15 watts r.m.s. (plenty for a domestic room) with a B110 15cm bass/mid-range unit and a T27 tweeter. System resonance is quoted as 60Hz. The Cantor, rated at 20W r.m.s. uses a B200 20cm bass unit and T27 tweeter; system resonance 70Hz. Both units will sit on a shelf 6in deep.



Servo-Sound Cybernetic Hi Fi speaker system and preamplifier

The company responsible for the original BBC monitor, IMF Products, of High Wycombe, exhibited at Sonex and created considerable interest with an add-on system of speaker units. For those whose speakers lack the clean resonance-tamed low frequency response, IMF are offering a £50 bass only speaker which comprises a transmission line system folded to take on the appearance of a 33in × 22in × 20in coffee table. Omni-directional radiation is achieved by the downward facing drive unit, and it is claimed that 17Hz can be reproduced. (Wonder what size organ pipe this would be.)

Also recommended are the "Studio" range of speakers from £61.95 to £73 plus purchase tax. Although somewhat expensive they are an excellent range and come from Spendor Audio Systems Ltd, of Redhill, Surrey. Main constituents are an 8in woofer of their own make, coupled with tweeters from Rola Celestion and ITT.

If you see the name Yamaha in connection with speakers, don't associate them with the noise of motor cycles. The Japanese certainly do come up with some unusual ideas, not the least being the Yamaha NS (for Natural Sound—what else?) range coded JA-6001, JA-5002, and many more.

The slim-line cone is of unusual shape, perhaps best described as a combination of semi-elliptical and small round (or those for guitars, more trapezoidal). Presumably this is a combination of woofer and tweeter on one chassis and one cone. For the added manufacturing complication and perhaps non-linear cone excursions, I personally fail to see any advantage over separate units. These types vary considerably in price and are imported by Jonathon Fallowfield Ltd, 60 St John Street, London, E.C.1.

TV SOUND THROUGH HI FI

It is worth noting that for addicts who crave to feed television sound signals through their hi fi systems, Rola Celestion are offering the Telefi ED10. This is one of those precious boxes claimed to get round the problems of live television chassis. This unit picks up the radiated 6MHz f.m. sound field from u.h.f. 625-line receivers only and converts in the normal way to an audio signal ready to feed into the "tuner", "aux", or "phono" input of the amplifier.

No electrical connection is made to the television receiver; only a pick-up transducer is mounted on the cabinet close to the i.f. strip. Rola Celestion are acting as distributors for the manufacturers Dinosaur Electronics Ltd of Windsor.

SUPER AMPLIFICATION

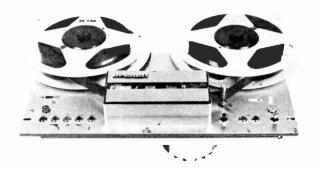
Since some of the foregoing indicate continuing improvements in loudspeaker design, the same cannot always be said for amplifiers. The standard of reproduction from a few is now approaching the ultimate possible with currently available components. It is all the more surprising therefore that several manufacturers do not seem to have the resources to improve their amplifiers measurably.

One well-known quality brand was in evidence in most of the non-amplifier demonstrations and in one room alone three were being used side by side. Have the rest accepted defeat?

There is very little to report on this subject but if you have the chance, listen-in to the Helme Atlantis 100 from P. F. & A. R. Helme Ltd of Harrogate. If you can detect -70dB noise at something like 55 watts r.m.s. into 8 ohms or 0·1 per cent distortion at 50 watts r.m.s., then you may not like this amplifier, but you would probably go a long way to find better figures than these quoted from the specification for such power output.

This brings us back to earlier comments; this amplifier has what is termed "Dynamic Matching Control". There are l.f. and h.f. controls which are set up during listening tests to an optimum to suit the listener's interpretation of how the loudspeakers are performing.

We gather that this is a kind of manual version of the Servo-Sound idea already described, in that speaker cabinet resonances can be damped by judicious settings of the controls. The idea is primarily to make up for deficiencies inherent in small bookshelf systems. The suggested retail price is quoted as £119.



Brenell Type 19 professional 1in tape deck

FRONT END

Now for the front end, and it is a pity that f.m. tuners were not as evident as they should be. Would this be due to difficult f.m. reception conditions so close to the moving aircraft at Heathrow, or lack of interest in a market that should grow after expansion of stereo broadcasting later this year.

So we are left with tape and disc, the former showing the boom in cassette cartridge systems with Dolby B incorporated. The success of chromium dioxide tapes added to Dolby makes tape recording and reproductions at 12 in per second an excellent proposition for acceptable quality music reproduction.

BASF introduced a combined radio/cassette recorder, the CC9300 priced at £67.97. With such a small size the cassette will undoubtedly be widely considered for incorporating with other equipment in one package, providing a very versatile system for domestic sales.

TAPE RECORDERS

Mention the words tape recorder and Philips are bound to be somewhere nearby. The interesting point about this organisation is diversity. Their products range from good value low price cassette machine that will go in a coat pocket, to professionally engineered studio transcriptors for broadcasting. Their latest is a three-motor, three-speed stereo machine and built-in 10 watt stereo amplifier, with illuminated tip-touch buttons allowing remote control boxes to be used.

The electronics has mixing, monitoring, multiplay and echo facilities, all demanded these days by the progressive musician who records at home or in a studio. This recorder, coded N4418, is offered at £189.75 including purchase tax, but if you want quality it is worth paying the price.

Brenell Engineering Co. seem to be on their own in supplying tape transport systems (to the general public) that can be applied to tailor-made self-constructed tape amplifiers. Brenell make a wide variety of decks and complete recorders.

They now produce a rugged tape deck Type 19 for industry that uses a Papst hystresis synchronous motor and two spool motor. Two speeds are available, $3\frac{3}{4}$ and $7\frac{1}{2}$ in per second, and the solenoid



Goldring G101 record deck with G850 pick-up

operated mechanics confirms the principles of older transcription machines, that use these for reliability.

However, for domestic applications, Brenell cater for less expensive tastes without neglecting quality, for example, the Mk 6 Deck at £62.04 and the Mk 610 at £79.60 including purchase tax. Bogen heads are available as optional extras for the Type 19, while the Mk 6 and 610 will accept a wide variety of heads at extra cost.

FOUR CHANNEL DISC

Turning for a moment to four-channel matters, it was a welcome sight to see the new RCA compatible discrete CD-4 disc record which will become available in May. RCA have been working with JVC and National Panasonic to produce this disc specially for four-channel equipment, and at the same sort of price as a top grade two-channel stereo disc. They are also willing to offer their expertise to other disc manufacturers to produce these recordings. Is this the kind of boost that the British want after Japan has already a choice of 65 CD-4 recordings?

LOW PRICE RECORD DECK

On the two-channel front, Goldring now produce the GL85, which was described in our Audio Fair report, and a newcomer, the G101, which is also belt driven and uses a magnetic cartridge—the G850. The aim of this new model is to offer Goldring quality at an economic price. At £24 plus purchase tax, including plinth and cover, this model is certainly good value.

PURCHASE TAX

Finally a note concerning prices; those quoted here were correct to the best of our knowledge at the time of going to press. Where purchase tax is not quoted, a reasonable estimate only would be to add about 17 per cent of the recommended retail prices.

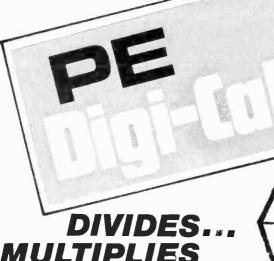
As purchase tax is based on manufacturers' trade prices, it is always wise to confirm the correct figures from them. Recent budget changes in purchase tax rates could in some cases mean "no change" where it is not applicable, or about 25 per cent of trade prices where reductions become effective.

The next date for your diary is October 23 to 28, the Audio Fair in the large Grand Hall, Olympia, London.



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Entries of up to six digits may be made, and the answers are given in up to eight digits. Calculations are carried out just as

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ALSO— THE CALLERCORD

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DIGITAL ELECTRONIC ORGAN SYSTEMS

A look at the more up-to-date methods of organ design

in the JULY issue of

PRACTICAL

ELECTRONICS

ON SALE JUNE 9



By R. Verrill B.Sc.

This simple electronic timer can be used for any operation where it is required to switch on an apparatus for a length of time and then automatically switch off. Alternatively, it can be used to switch on the apparatus automatically after the preset time, and remain on until switched off manually.

CIRCUIT DESCRIPTION

The circuit diagram of the timer is shown in Fig. 1. Here, when the mains switch S2 is turned on, the bridge rectifier (D1-D4) supplies the circuit with about 35V d.c. smoothed by the capacitor C1. The 250µF capacitor C2 is charged up to this voltage via the resistors R1 and R2. Some of the charging current flows through the base of the pnp transistor TR1 so that this remains on for a few seconds after closing S2 until C2 has become charged.

During the time that TR1 is on, capacitor C3 is charged up to the line voltage via TR1, R4 and the diode D5. As soon as TR1 goes off, the voltage on C3 starts to fall slowly because of the small current being leaked away by TR2. This transistor acts as a constant current source because its base is at a fixed potential and there is resistance in the emitter lead whose value is determined by the position of S1. The value of the emitter current is approximately equal to the emitter voltage divided by the emitter resistance. A fine control over the discharge current is obtained by adjustment of VR1 which alters the base voltage of TR2.

The Schmitt trigger circuit, comprising TR3, TR4, operates when the voltage on C3 has fallen to about 2 volts. TR3 then starts to turn off and TR4 starts to turn on. Current through the resistor R20 biases the emitter of TR3 positive thus turning TR3 further

COMPONENTS . . .

Resis	stors		
R1	22k Ω	R18	4.7M.
R2	10k Ω	R19	100k €
R3	4-7k Ω	R20	6-8k Ω
R4	1k Ω	R21	56k Ω
R5	390k Ω	R22	56k Ω
R6	15k Ω	R23	10k Ω
R7-	-R17 5-6k Ω (11 off)	R24	390 Ω
	10% , $\frac{1}{2}$ W carbon		

Potentiometer

VR1 22k Ω carbon linear

Transistors

TR1 ZTX503 (Ferranti)

TR2-TR5 ZTX107 (Ferranti) (4 off)

Diodes

D1-D4 ZS170 (Ferranti) (4 off)

D5-D7 ZS120 (Ferranti) (3 off)

Switches

S1 Double-pole, mains toggle switch

S2 Single-pole 11-way wafer switch

Relay

RLA 2-pole 2-way 26V 700 Ω, STC4189 GD (Henry's Radio)

Transformer

T1 Mains transformer, secondary 25V 0.5A Douglas MT102AT (Henry's Radio)

Miscellaneous

Diecast box $8\frac{3}{4}$ in \times $5\frac{3}{4}$ in \times $3\frac{5}{32}$ in, Veroboard $3\cdot4$ in \times $5\frac{1}{2}$ in $0\cdot1$ in matrix, FS1-100mA fuse and holder, SK1-six pin plug and socket (Bulgin).

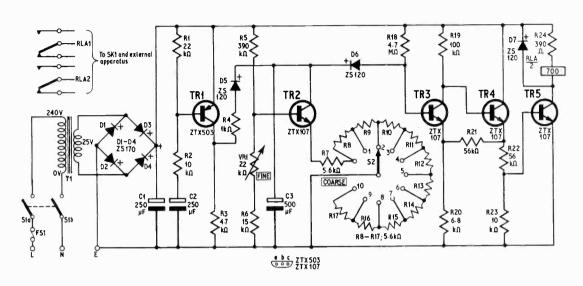


Fig. 1. Circuit diagram of process timer

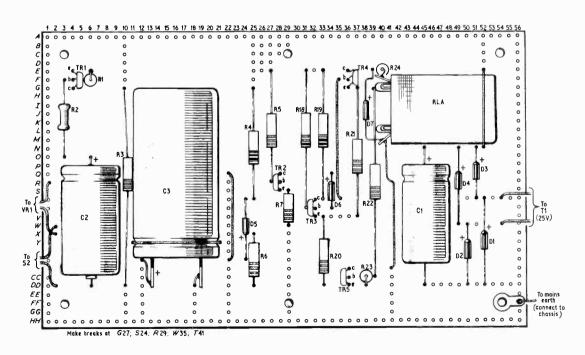
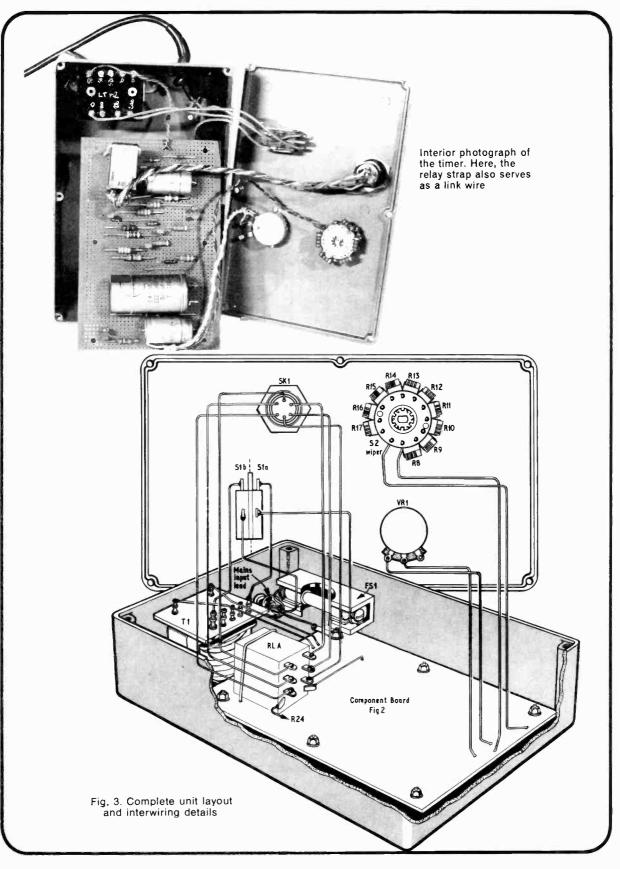


Fig. 2. Component mounting and wiring details of Veroboard sub-assembly



off. Regenerative feedback occurs so that TR3 is turned completely off and TR4 is turned on supplying current through R22 to the base of TR5 which operates the relay. The appropriate relay contacts are used to turn on or off the external apparatus as required.

CALCULATING THE PERIOD

The actual length of the timed period can be calculated as follows. The time taken for the voltage on a capacitor of C farads to fall by a voltage V volts when a constant current of I amperes is drawn from the capacitor is CV/I seconds.

The voltage at the base of TR2 is

$$\frac{35(VR1 + R6)}{VR1 + R5 + R6}$$

which works out at about $2\cdot 2V$ with VR1 wiper in the mid-position. Since the case/emitter drop is $0\cdot 7V$ the voltage at TR2 emitter is $(2\cdot 2-0\cdot 7)$ which is $1\cdot 5V$. If S2 is set for maximum resistance $(61\cdot 6k\Omega)$ the emitter current

$$I_e = \frac{1.5}{61.6 \times 10^3} = 24 \mu A$$

In the expression CV/I we can now substitute:— $C = 500 \mu F$

V = 33 volts (the voltage dropped from 35V to 2V) $1 = 27\mu A$

Therefore

period (CV/I) =
$$\frac{33 \times 500 \times 10^{-6}}{24 \times 10^{-6}}$$
 = 690 s

If VR1 had been set to zero resistance, the period would work out as 25 minutes, 40 seconds.

CHOICE OF CAPACITOR

Some readers may be of the opinion that the use of electrolytic capacitors in timing circuits should be avoided. This is true in some circuits especially where very accurately timed periods are required. The objection to using electrolytics arises mainly from their high internal leakage currents. For example, the type of capacitor used in this timer has a leakage of up to 1mA when used at its maximum working voltage of 64V. Since the discharge current in the circuit can be as low as 10 μ A we would require the leakage current to be less than 1 μ A and to change by less than 0·1 μ A to give any degree of stability to the timed period. In practice the degree of stability obtained is at least as good as this when a capacitor of the type specified is used.

LOW LEAKAGE

When a voltage is supplied to an electrolytic capacitor, besides the current required to give the capacitive charge, a forming current flows through the electrolyte until an insulating layer is formed of sufficient strength to withstand the voltage. If the voltage is then reduced, the insulating layer is more than sufficient to withstand the voltage now present so the forming current is no longer required and the leakage current is extremely small.

In the timer circuit, after the initial charge, the voltage on the capacitor is reduced at a constant rate, so the above conditions for low leakage are ideally satisfied.

CONSTRUCTION

All of the small circuit components are mounted on a 5½ in × 3½ in 0·1 in matrix Veroboard as in Fig. 2. Since, with this type of circuit, layout is not particularly critical, other forms of assembly can be made

In Fig. 3 the timer is shown completely assembled. When wiring up SK1 to the relay use different coloured sleeving, so that the switches of the relay can be identified.

SETTING UP

Before any setting up is done the circuit wiring should be thoroughly checked. If this checks out with Fig. 3 set the "Coarse" switch to position "1" and the "Fine" control (VR1) to a minimum. Switch on and you should find the relay changes over after a period of about two minutes.

Exact time multiples can be set up on S1 if VR1 is set for a 130 second delay. This has the effect of multiplying each of the "Coarse" range switch positions by a factor of 2. This means that position "1" will produce a delay of two minutes, position "2" four minutes and so on, up to 20 minutes at position "10". The error on each range will be about 10 seconds which is the time taken for C2 to be charged initially.

Repeated checks of timing periods produced an error of 10 seconds on the 20 minute range and proportionately less for shorter times.

RELAY CONTACT RATING

The relay specified has a contact rating of 2A but the actual load can be doubled if the switch contact pairs are used in parallel.

BACK TO SCHOOL

continued from page 463

Finally, a domestic note which is not entirely out of place here. A magazine such as PRACTICAL ELECTRONICS finds itself in a unique position in that while catering for the interests of private individuals it becomes to some extent a bridge between the educational establishments and the industry. This is because we are in regular contact with both sides and receive contributions from members of both the teaching and the engineering professions. We do not claim to be an educational journal in the formal sense, and are flattered and delighted that so many of the teaching profession do turn to PRACTICAL ELECTRONICS for instruction in applied modern electronics. We feel confident that they will be able to rely on this service equally in the future.

As to some recent critical comment aired in these pages, we wonder what teacher would like to be judged and outrightly condemned simply on one single lecture, delivered when Sir was perhaps somewhat under par?

F.E.B.

PATENTS BEVIEW...

THUNDERSTORM WARNING

By a quaint coincidence the waterproofing patent mentioned last month was published only one week later than British Patent 1 248 300 from Nitro Nobel AB of Sweden. The Nobel specification is concerned with a thunderstorm warning system.

Not surprisingly Nitro Nobel are concerned mostly with predicting thunderstorms for the benefit of those working with explosives, but the invention will probably find

much wider interest.

It is customary in thunderstorm warning systems to detect both the quasistatic electric field, which occurs between the electric charge of a thundercloud and earth, and the pulses of longwave electromagnetic radiations that are transmitted from lightning discharges. The signals are usually detected in two threshold steps; alert and alarm, which can be audible and/or visual warning.

The radiation pulses are detected by an aerial wire, often of considerable length and the obvious problem is that this aerial is likely to be struck by lightning. Another problem is that the device may mistake local machine spark discharges for lightning flashes.

The Nobel invention relies on an electronic logic system which ensures that the alarm is triggered by radio frequency radiation pulses only if these pulses are repeated within a predetermined time interval, or combined with simultaneous pulses in another (for example, spectral) range. The alarm can be triggered by a quasistatic electric field of above a threshold intensity. The alarm will also be triggered if the electric field alone rises to a predetermined high level.

Nobel suggest a field detector formed from a capacitor and a rotatable diaphragm positioned in front of the capacitor and operating in accordance with the so-called field mill principle. The detector can be of relatively small size and the diaphragm actually housed inside an antenna for longwave radio pulses. It is claimed that this arrangement is unlikely to attract a lightning strike.

In Fig. 1 Nobel show how a detector system is connected to a logic unit by shielded cable. The detector system is earthed and

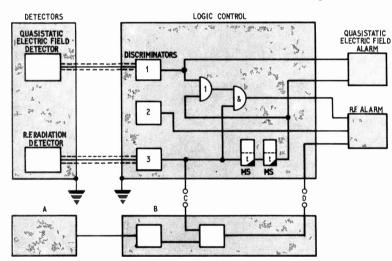
includes the two component detectors for electric field and electromagnetic radiation emission. The former provides a signal proportional to the intensity of the quasistatic electric field. example, a sinusoidal voltage of 200Hz. This signal is fed to two amplitude discriminators 1 and 2 having different threshold values. Discriminator 1 output is connected to the electric field warning circuit so as to activate it all the time that the quasielectric field is higher than a selected base threshold. This discriminator also feeds one input of an OR circuit.

is set by the trailing edge of the output of the first monostable.

An output signal from the second monostable is connected to the electric field warning circuit and to the second input of the OR circuit. The output of the OR circuit is connected to the second input of the AND circuit. The output from the latter AND circuit triggers the r.f. alarm, so that it is sounded if a signal pulse is transmitted from discriminator 3 during the time period in which D1 discriminator is producing a signal pulses from discriminator 3 occur

BP 1 248 300

Fig. 1



An output signal from discriminator 2 triggers the alarm circuit which holds "on" when activated.

When a lightning strike occurs, the r.f. radiation detector sends pulses to discriminator 3 which а discriminating corresponding to a normal flash of lightning at a distance of 10 to 15 kilometres. A radiation pulse exceeding this provides a signal pulse from discriminator 3 which is connected to the first input of an AND circuit, and to a timing circuit composed of two monostable multivibrators in series. One monostable is set by the pulse from discriminator 3 and the other

within a predetermined time interval. This distinguishes between one single pulse and a pulse train.

Pulses having a large spacing in time, in all probability, do not emanate from a thunderstorm. The actual time period gating must be suited to the geographical location in which the device is to be used.

The system described in this patent may be supplemented by other detectors. Supplementary optical detectors, discriminators, and AND gates can be linked into the system at A, B, C and D. More details are given in the patent specification.

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2N 2646	Sil. UJT	Oscillator, SCR driver	47p
2N296A	NPN	Small sig. amp	11p
2N3055	NPN	High power	50p
2N3702	PNP	Low power	10p
2N 3704	NPN	Low power	10p
AC126	Ger, PNP	Small sig./driver	23p
AC128	PNP	Low power	20p
AD149	PNP	High power	58p
AC176	NPN	Low power	16p
*AD161	NPN	Med. power	33p
*AD162	PNP	Med. power	36p
BC108	80. N PN	Small Signal	11p
BC109	NPN	Low noise	12p
BC168	NPN	Small signai	10p
BC169	NPN	Low noise	11p
BF194	NPN	RF amp.	14p
BFY51	NPN	Med. current	20p
OA90	Ger. diode	RF detector	6р
OA91	100	General	5 p
8D1		ilicon Rectifier I amp	10p
WO2	s	ilicon bridge 1 amp	30p
*Matched pa	air AD161/AD162		60p
	(Sil. = Silicon.	Ger. = Germanium)	

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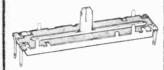
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Code	Power	Tolerance	Range in ohms	Values		10 to 99 see note be	
C	1/20W	5%	82-220K	E12	9	8	7
č	1/8W	5%	4-7-470K	E24	1	0.8	0.7
C	1/4W	10%	4·7-10M	E12	1	0.8	0.7
Č	1/2W	5%	4:7-10M	E24	1.2	1	0.9
Ċ	1 W	5%	4-7-10M	E12	2.5	-1	1.9
MO	1/2W	2%	10-1M	E24	4	3.5	3
WW	1 W	1000	0.22 - 3.9	E12	7	7	6
		$\pm 1/20 \Omega$					
M,M	3 W	5%	12~10K	E12	7	7	6
WW	7 W	5.90	19~10K	E12	9	43	8

Codes: C = carbon film high stability low noise

MO = metal oxide Electrosil TR5 ultra low noise

WW = wire wound Plessey

values: B12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24; as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 72, and their decades. Prices are in peace each for same obnic value and placer rating. NOT mixed values. (Ignore frations of 1p on total value of resistor order.)

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100/10, 22/35, 47/35, 10/25, 22/10, 47/10, 47/25, 100/10, 22/35, 9 ach. 10/63, 22/35, 47/35, 100/16, 100/25, 220/6, 220/10, 220/16, 470/3, 6p each.

4703., opeach. 4763, 100/35, 470/10, 7p each; 100/50, 220/35, 9p each; 100/68, 470/25, 100/10, 10p each; 220/63, 470/35, 100/016, 14p each; 1000/25, 16p each; 470/63, 1000/35, 19p each; 2000/200, 29p each; 1000/63, 2200/35, 470/618, 35p each.

Tantalum and other capacitors, etc., see latest 1972 catalogue—issue No. 6.

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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded payment according to its merits.

RADIO ALARM

AVING constructed the *Digital Clock* described in the December 1970 issue, I required an additional circuit to enable a transistor radio to be switched on at the same time as the alarm.

A thyristor was tried initially, but the holding current was greater than that drawn by the radio, so that after the ten-minute period that the alarm circuit input is active (i.e. pin 3, IC18 is high), the circuit would turn off (assuming the alarm had been turned off).

The circuit eventually devised is based on an emitter-coupled bistable and is given in Fig. 1.

With the alarm inactive, TR4 is on and TR5 is off. The voltage at the collector of TR4 is just above zero, and hence insufficient to cause the Darlington pair TR1, TR2 to switch on. When the alarm circuit is active, pin 3 of IC18 goes high (point B on the diagram) and TR3 is switched on, grounding the base of TR4. The bistable switches states (TR4 off and TR5 on) and the voltage at TR4 collector rises and the Darlington pair switch on (TR1 hard on).

So far as the radio is concerned, the circuit (Fig. 1) may be considered as a switch and should be connected into one of the battery leads. However, since transistors are used, the "switch" is voltage sensitive, and point "A" must be positive with respect to the circuit earth rail (the other pole of the switch), see Fig. 2a. Alternatively, the circuit may be inserted into the negative lead, if more convenient, but again, care must be taken to ensure that point "A" remains positive, Fig. 2b.

With a 6V battery in the radio, the leakage current through the circuit when "off" is less than $10\mu A$. It should be noted, however, that there is 0.6V dropped across the power transistor so a slight drop in radio volume will be noted.

This circuit may only be used with a battery powered radio and under no circumstances should a mains operated radio be used.

To retain the portability of a battery operated radio a jack plug socket mounted in the case of the radio and wire as shown in Fig. 3 can be used. The socket should be the type used for an earphone accessory.

R. C. Stone, Hampton, Middx.

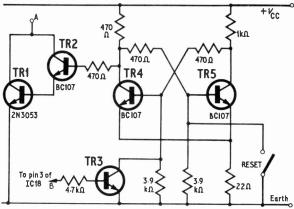
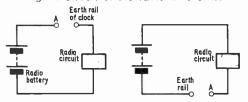


Fig. 1. Circuit of the radio time switch



Figs. 2. Method of connecting different polarity radios to the clock, for point A positive (left); point A negative (right)

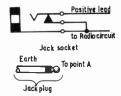


Fig. 3. Wiring of the break jack and plug

PHOTOMETER FOR ECOLOGICAL STUDIES

THE details in Fig. 1, show a simple photometer which was built in order to investigate variations in light intensity beneath various types of vegetation. It is simple to construct and use, and robust enough for field study work.

The basic element of the instrument is two photovoltaic Selenium cells. They consist of circular plates about 6cm in diameter and 2mm in thickness. They are capable of giving a considerable deflection on a milliameter when under full daylight illumination.

The cells are set in a piece of plywood, which has one surface chiselled out to hold them firmly. Below the cells a similarly shaped piece of aluminium foil is inserted so as to give a good electrical contact in the circuit.

A thicker though smaller sheet of foil is applied to the upper surface of the photosensitive plates, big enough to make electrical contact but not covering any appreciable part of the photo-electric surface. It is important that the two sheets of foil do not make contact with each other. To prevent this happening, a small piece of plastics is inserted between them. The entire assembly is then sandwiched by a plate of Perspex, with terminals to the upper and lower aluminium sheets.

Using a standard light source the instrument could be calibrated absolutely. Without such a source, however, a relative calibration is still possible, i.e. the non-linear response of the cell can be determined.

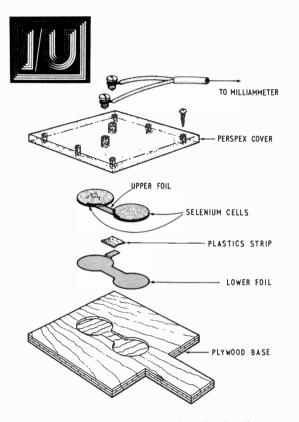


Fig. 1. Constructional details of a simple photometer

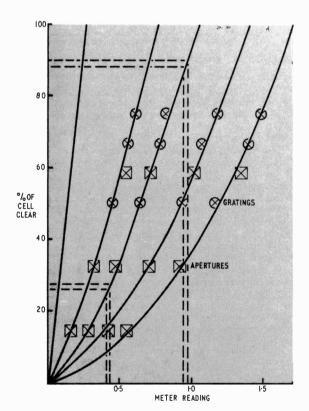


Fig. 2. Calibration graph for the photometer

Two methods were tried. The first utilised the inverse square law (placing the cell at different distances from a light source). In practice, this did not prove very successful, and instead the following method was devised.

A set of apertures and gratings were constructed out of black paper, transmitting 75%, 66.6%, 50%, of the total light. These apertures were fixed, in turn, with adhesive to the Perspex cover. Starting with the full cell area, a light source is moved to a position which gave a realistic reading on the milliameter. Then, without changing this distance, one of the apertures or gratings is placed over the Perspex cover and the current recorded.

Recalibration, with the apertures moved slightly so as to cover different parts of the cell surface, will give more accurate results. These are in Fig. 2.

Using the latter, relative transmissions of the different types of foliage can be determined. For example, the following results were obtained on an overcast October day (instrument held horizontally for all readings).

Open sky reading	Under foliage
0.96	0.44
0.98	0.42

Taking the 1.06 calibration curve, a 0.96 meter reading is equivalent to 88 per cent transmission, and 0.44 reading to 27 per cent transmission.

We therefore, obtain a relative transmission of:

 $27/88 \times 100 = 30.7$ per cent.

Similarly, the second pair of results give about 27.5 per cent relative transmission.

E. D. Dale, Worsley, Lancs.

POINTS ARISING

SEMICONDUCTOR LEADOUT IDENTICHART May The outline diagram for the 2N3702 to 2N3711 types should be diagram number 59a not 35a. On diagram 22a, reverse the b and e connections.

TAPE SPEED CONTROL (Ingenuity Unlimited April 1972)

Page 299, Fig. 3. Transistors TR7 and TR8 should be OC81 and OC35 types respectively.

P.E. SCORPIO IGNITION SYSTEM (November and December 1971)

Some constructors have had difficulty with using certain makes of 2N3055 in the "Scorpio" ignition system. What happens is that the circuit oscillates normally (at about 2kHz) until the output of the inverter is shorted, when the inverter goes into a high frequency mode at around 200kHz and remains in this mode when the short is removed.

This arises because 2N3055 transistors are made by a very large number of manufacturers and there are large variations in characteristics such as f_t between different makes. Only minimum or average values are normally quoted on the data sheet.

This trouble does not occur with the specified Ferranti 2N3055, or with RCA devices. It has occurred with Fairchild 2N3055's and may also occur with Motorola devices due to their high $f_{\rm t}$.



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30	200	9	8	12·0 × 10·3 × 10·0	4.39	52
62	250	12	4	9·5 × 12·7 × 11·4	5.80	67
55	350	15	0	14·0 × 10·8 × 12·4	7.77	82
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500	12	8	14:0 × 10:2 × 1	1.4			5.78	67
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86	6.0	5	12	10.2 >	8.9 >	8.3	units	do not	in-	3.07	52
146	8.0	6	4	8.9 ×	10.2 ×	102	clude	rectifie	rs	3.49	52
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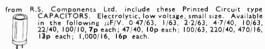
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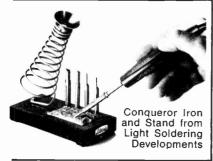
To help rationalize the profusion of plug and socket connecting configurations in the continental Din range, Parry Electronic Developments have introduced a PD Din connector that can be easily assembled in either 2-pin, 3-pin or 5-pin stereo configurations.

These connectors do not require soldering but use small terminal tags which are crimped, at one end, to the required wire and then have a pin inserted in a sprung triangular section at the other end. The pins are placed in any required arrangement on a centre bush, placed in one half of the outer casing and then the two halves are snapped together to form the complete connector.

Details of other connectors in the series and addresses of nearest stockists can be obtained from Parry Electronic Developments Ltd., 28 Greville Street, London ECI.

A miniature 2-pin plug and socket, useful for extension leads, is now being marketed by Senate Engineering.

A feature of the plug and socket



is that it is rated at 25A and has a claimed contact resistance of less than 1-4 milliohms. Again, leads are connected without the use of solder or screws.

Typical applications could be for automobile, caravan and boat electrics and emergency supplies. There are also many low current low voltage applications, such as control circuits and loudspeaker extensions where advantage can be taken of the low contact resistance.

The recommended retail price is 25p and further information is available from Senate Engineering Ltd., 77 Cotes Road, Barrow-in-Soar, Loughborough, Leicestershire.

SOLDERING IRON AND STAND

Available as a set or individual items Light Soldering Developments recently announced a new soldering iron and stand.

Called the Conqueror, the iron is available with five different slipon tip sizes from 16 in to 4 in. Ideal for transistor and i.e. work the iron is available for operating voltages of 12, 24, 115, 220 and 240V. A feature of the stand is the arrangement for mounting four spare bits on the base. The iron stand base is made from heatproof Bakelite and contains a wiping sponge for keeping iron tips clean.

The spring guard is claimed to give complete protection from burns and prevent damage to the iron if knocked. A flared steel ferrule at the narrow end of the spring gives easy location of the iron.

The price of the Conqueror is £1.80 with standard copper bits, or £2.03 with a long-life bit. The cost of the stand is £1.48. Further details and stockists can be obtained from Light Soldering Developments, 28 Sydenham Road, Croydon CR9 2LL.

SOUND SYSTEMS

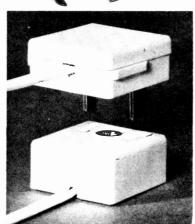
For people who prefer to purchase and choose their own turntable, cartridges, speakers, and design enclosures we can recommend the System 12 from **Bi-Kits**.

The kit consists of a pre-wired pre-amplifier, two integrated circuit power amplifiers, power supply

MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.





Miniature 25A Plug and Socket made by Senate Engineering

module and two 8in diameter twin cone speakers. The kit also contains all the necessary connecting wire, silver anodised front panel and control knobs.

The power amplifier modules use an SGS integrated circuit which they claim gives an output of 6 watts r.m.s. per channel. The frequency response of the system is claimed to be 20Hz to 50kHz.

Kits are available, price £13.95 plus 35p postage and packing, from Bi-Kits, 63a High Street, Ware, Herts.

The System 12 can be heard at the new **Bi-Pak's** Components Supermarket at 18 Baldock Street, Ware, Herts.

A new stereo system is now available from Servicon Dynamics Ltd. The amplifier moves away from conventional amplifier techniques and incorporates integrated operational amplifiers as the pre-amplifier tone control and driver stages. The output stages, which are transformerless and d.c. coupled, use complementary silicon transistors connected in a common emitter mode.

Total distortion is claimed to be 0.09 per cent at 15W per channel at



System 12 Kit marketed by Bi-Kits

1kHz and the cross talk -60dB at 1kHz with tone control flat and 15 watts/zero watts per channel loading.

The amplifier is mounted in a teak finish cabinet with a Perspex/teak lid which can be kept in place with records playing. The deck is the latest Garrard SP25 Mk. III with a ceramic cartridge KS41C-CDS as standard; a magnetic cartridge can be supplied as an extra.

The output is 30 watts r.m.s. per channel into 7.5 ohms with a frequency response of 30Hz to 29kHz (+ dR)

(± dB).

The system is sold as a package with two teak finish speaker cabinets each containing an 8in l.f. speaker and 4in tweeter with crossover capacitor. Power output 15 watts r.m.s. at 15 ohms per channel. Frequency 30Hz to 20kHz. A 50 watt system can be supplied as an alternative.

The system is offered at £89.00 for the 30 watt system; the amplifier and deck complete, without spakers, is £70.35. Further details available from Servicon Dynamics Ltd., 186/190 Cirencester Road, Charlton Kings, Cheltenham, Glos.

report from AUSTRALIA

BY J.M.WALDIE

In this new series of "Reports from down-under", the aim will be to cover three broad aspects of Australian electronics: home construction, industrial development, and the local hi-fi scene. It is felt that readers of P.E. intending to migrate to this side of the world would naturally be interested to know if their hobby is perpetuated here, and what form it takes; at the same time it is possible to make useful comparisons between here and the U.K. On the industrial front, items will be selected of interest to both hemispheres, since P.E. enjoys a relatively large readership in Australia.

MAGAZINES

Considering the population here, which may be considered to consist of approximately one and a half times that of Greater London spread over an area the size of America, and also in view of the fact that it is essentially an "outdoor" society, the interest in electronics as a hobby is remarkably widespread. Naturally this is concentrated in the five major cities of Australia, and particularly in Sydney and Melbourne.

This industry is served by two local magazines; all the English magazines, of which P.E. is the most popular, are also available at most newsagents.

Both local magazines, however, do not restrict themselves to home constructional projects. They both examine, in some detail, new commercial products in the hi-fi field and both conduct record reviews.

HOME CONSTRUCTION

A major difference is the fact that published projects are designed in the magazines' own laboratories. As a consequence, commercial units built here are frequently based on designs available to the public which contrasts sharply with the situation in the U.K. and in America where d.i.y. hi-fi projects appear to follow industrial trends. This rather trends. unusual situation offers two important advantages to the home constructor. Firstly, he can build units equal in performance to some local commercial systems and, secondly, the designs presented follow in logical sequence in terms of facilities and improved performance.

What service is offered to the constructor in terms of components, tools and so on? Visitors and should not Australian equivalents to the Edg-ware and Tottenham Court Roads, although small pockets of suppliers do exist. A glance through the local magazines indicate that Sydney possesses twelve kit/component shops; Melbourne has half that number. Only two or three of these advertise themselves as being strictly mail-order. Constructors should note, however, that, unlike the U.K., the great majority of importers and manufacturers will sell direct to individuals. The writer has not bought components in four years from a kit-shop, but rather from "trade-sales" counters in wholesale

PROJECTS

Readers and intending visitors should not delude themselves into thinking that Australia is simply a place where kangaroos leap down the main streets, and where the bathwater goes down in the opposite direction. Industrially and technically it is well advanced; although f.m. radio and colour television are not yet with us, plans are well advanced for their introduction. The sophistication is amply reflected in the standard and selection of home construction projects. There exists a greater penetration of components American origin than in the U.K., which has lead to a relatively early introduction of such devices as fieldeffect transistors, triacs and i.c.s into d.i.y. projects; circuits based on triacs, for example, appeared in 1968.

The projects themselves are basically similar to those in P.E. with possibly a greater emphasis on "outdoor" systems such as water-level alarms for home pools and protective and ancilliary circuits for cars. Mercifully, an all-electronic barbeque has yet to emerge. It seems, too, that there does not appear to be much interest in sophisticated toys and war-games.

This summarises the situation here regarding d.i.y. electronics in

Australia and those contemplating a temporary or permanent move need not have any fears regarding the ability to continue their hobby.

COMPUTERISED BETTING SHOPS

One interesting excursion of electronics into traditional areas has been the introduction in Sydney of computerised betting shops. These, in all states, are Government run; they are known as the TAB (Totaliser Agency Board), and provided £1 million profit last year in N.S.W. Bets can be placed not only on horse and greyhound racing, but also on trotting, a form of equine harassment not known in the U.K. The volume of punting is such that an expected 10,000 bets per minute will be placed by 1978.

It was decided to use an IBM 360/44 computer to handle this volume and was installed some 12 months ago. It is supported by AWA (Amalgamated Wireless Australia) branch selling terminals, STC branch printers and PMG telex in country areas. Cut-over of telephone betting from manual to computer has now been completed; the system of transmitting full collation figures to headquarters from the branches is more than half-way complete and 15 of the 380 existing branches_converted to machine vending. These are now being converted at the rate of four per week.

UP TO THE "OFF"

The computer checks the validity of each bet, runners and "scratchings" until the "off", the credit standing of the telephone punter and the validity of a winning claim and the amount. The timing is such that a bet placed two seconds after the race is due to close will be rejected.

Tradition dies hard. The cold impersonality of the new system, according to veteran punters, is no substitute for the excitement which occurred in 1964, for example, when crowds queueing outside two TAB branches had to be controlled by police because the windows had closed before all the punters had laid their wagers.

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AAY42	10p	BD115 76p BD123 86p	OC16 50p OC20 85p OC22 50p	2N1303 18p	
AAZ13	10p 15p 10p 10p	BD124 80p	OC20 859 OC22 509 OC23 609 OC24 609 OC25 409	2N1304 22p	
AAZ15	10p 10p	BD131 769 BD132 809	OC23 609 OC24 609	2N1306 25p	
AC107	850	BDYII	OC25 409	271301 EUD	
AAZ15 AAZ17 AC107 AC126 AC127 AC127Z AC128 AC176 AC187 AC188 ACV17	80p 25p	#1-50 BDY17	0020 200	2N1308 25p 2N1309 25p	
AC127Z	50p	81-50	OC29 809	1 9 N 16 13 90m	
AC128	20p	BDY38 659 BDY60	OC36 80m	2N2147 75p 2N2160 60p 2N2217 25p 2N2218 20p	
AC187	25p 25p	\$1.00		2N2217 25p	
ACT 188	800	BF115 25p	OC43 50p OC44 15p OC45 18p	I 2N2218A	
AC188 ACY17 ACY18 ACY19 ACY20 ACY21 ACY22 ACY39 ACY40 ACY41 ACY44 AD140	25p 25p	BF154 20p	OC45 18p OC70 18p	25p 2N2219 20p	
ACY20	20p	BF159 859 BF180 85p	OC71 18p	2N2219A	
ACY21	20p 10p	BF194 15m	OC75 250	2N2220 25p	
ACY39	55p 20p	DE105 15n	OC72 809 OC75 25p OC76 25p OC77 40p	2N2220 25p 2N2221 20p	
ACY40	150	BF196 15p BF197 15p	OC81 209 OC81D 209		
ACY44	25n	BFX13 25p BFX29 25p	OC81D 20p	2 N 2222 20p	
AD149	50p	BFX30 25p	OC81Z 40p OC83 25p	2N2222A 25p	
AD161	35p	BFX84 25p BFX85 80p	OC84 25p OC139 25p	2N2369 15p 2N2369A	
AD162 AF114 AF115	35p 25p	BFX86 25p	OC140 40p OC141 60p	150	
AF116	25p	BFX87 25p BFX88 20p	OC170 25a	2N2646 40p 2N2904 20p 2N2904A	
	20p	BFY18 25p	OC81 20y OC81D 20y OC81Z 40y OC83 25y OC84 25y OC139 25y OC140 40y OC141 60y OC170 25y OC171 30y OC190 40y	2N2904A	
AF118 AF124	25p	BFY50 20p BFY51 20p	OC200 40p OC201 75p	2N 2905 25n	
AF117 AF118 AF124 AF125 AF126 AF127 AF139 AF180 AF181	20p 20p	BYX13 259 BYX13 259 BYX30 259 BYX84 259 BYX85 259 BYX86 259 BYX86 259 BYX87 259 BYX87 259 BYX87 259 BYX97	IOC202 80m	2N 2905 A 25p	
AF127	90-	BFY90 65p	OC206 95p OCP71 97p	2N2906 20p 2N2906A	
AF139 AF180	30p	B8X20 15p B8X21 20p	ORP60 40n	9.5n	
AF185 AF186 AF239	45p 50p 40p	BSY27 15p BST95A 12p	RT140 15m	2N2907 28p	
AF185 AF186	50p	BSY95 12p	TIPONA SO-	2N2907A 25p	
AF239	4000	BU 105 42 25	TIP30A 80p TIP31A 80p TIP32A 70p		
ABY26 ABY27 ABY28 ABY29	20p 80p	BY126 12p	TIP31A 80p TIP32A 70p	2N2926 10p 2N3011 20p	
A8 Y 28	25p	BY124 15p	TIP33A	2N3053 20p 2N3054 50p	
A8Z21	25p 80p 55p 15p	BYZ10 85p	TIP34A	2N2926 10p 2N2926 10p 2N3011 20p 2N3053 20p 2N3055 75p 2N3055 75p	
BA100 BA102	80b	R8T95A.12, B8T95A.12, B8T95A.12, B8T95A.12, B8T95A.12, B710B.12, B7124.15, B710B.12, B7124.15, B7121B.12, B7121B.12, B7121B.12, B7121B.12, B7121B.12, B7121B.12, B7121B.12, B7121B.12, B7121B.12, B712B.12, B7	#1:50 T1843 40p	2N3525	
BA110	25p	BYZ13 25p	T1850 12p	2N3614 65p	
BA115 BAX13	7p 5p	GET102 85p	T1851 10p T1852 10p	2N3702 10p 2N3703 10p	
BAX16	7p	GET103 25p	T1860 18p	2N3704 12p 2N3705 10p	
BAY38	5p 7p 7p 15p 10p	GET113 25p	TIR69 95n	12N3707 12n	
BC107 BC108	10p 10p	GET114 20p	V405A 25p VR525 35p	2N3708 10p 2N3714	
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BC116 BC116A BC117 BC118	20n	GM378A 55p MAT101 25p MAT121 25p MC724P 60p	ZTX300 12p	2N 3771	
BC116A	25p 20p 20p	MAT101 25p MAT121 25p MC724P 60p	ZTX301 15p ZTX302 20p	2N3772	
BC118 BC119	20p 30p	MC724P 60p MJ420 80p	ZTX 303 20p ZTX 304 25p	2N3773	
BC119 BC134 BC135 BC136 BC137 BC138 BC147	20n	MJ421 80p	ZTX500 15p	42.85	
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BC137	20p 20p	MJ2901	ZTX503 17p ZTX504 40p	2N3819 86p	
BC147	12p 10p	M.I.E.340 50m	ZTX531 26p	2N3823 50p	
BC147 BC148 BC149 BC153 BC154 BC167 BC169 BC169C	10p 12p			2N3824 95p 2N3903 20p	
BC153	20 ₀	MJE371 80p MJE520 75p MJE521 70p	IN4148 7n	1 27 3900 Ear 1	
BC154 BC167	20p 15p	MJ E2955	I844 7p I8921 7p	2N4058 12p 2N4061 12p 2N4062 12p	
BC169 BC1690	12p	#1·10 MJE3055	18921 7p 18922 8p 20301 25p	ON 4000 10-	
BC189C BC177 BC178 BC179 BC182L BC183L	20m	75p	2G302 80p	2N4290 12p	
BC178	20p 20p	MP8A06 25p MP8A56 20p	201303 35p 2N404 20p 2N696 15p	2N4871 85p 2N5457 80p	
BC182L	10p 10p	MP8A56 20p MP8A70 15p MP8U06 50p	2N696 15p 2N697 15p	2N5458 85p 2N5459 40p	
BC184L	12p		2N698 80p	140250 50n I	
BC212L	12p 12p	NKT214 20p NKT216 85p NKT403 75p NKT404 65p	2N706 10p 2N706A 12p	40360 40p 40361 40p	
BC214L	15p	NKT403 75p	2N708 15p	40362 50p	
BCY31	85p 40p		2N930 20p 2N987 40p	40543 65 p	
BCY32 BCY33	60p 80p	OA10 25p	2N987 40p 2N1131 25p 2N1132 25p	40543 65p 40594 £1:05 40595 £1:05	
BCY34	85 p	OA47 10p OA70 10p	2N1302 18p	40636 #1:10	
BC183L BC184L BC212L BC213L BC214L BCY30 BCY31 BCY32 BCY33 BCY34 BCY38	45p	OA10 25p OA47 10p OA70 10p OA79 10p OA81 8p	Full transistor		
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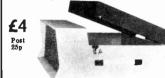
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NEWS BRIEFS

SOLID-STATE FYE

SMALL research model of a black-and-white camera A small research model of a black-and-white camera employing a solid-state "eye" that could make possible future TV cameras as small as a wristwatch was demonstrated recently by RCA.

The camera's imaging sensor is a silicon integrated circuit in contrast to the vacuum tubes of conventional

TV systems.

The camera's integrated circuit "eye" consists of 32 rows of photo-sensitive elements, with 44 elements in each row. When an image strikes the array, an electrical charge proportional to the light intensity is produced in each element. The rows are read out very rapidly in sequence to produce a black-and-white television-type picture.

A model of the camera, developed at RCA Laboratories in Princeton, America, has been delivered for evaluation to the Air Force Avionics Laboratory in Ohio, which sponsored research on the system.

LASAR DRILLS FOR DIAMONDS

M INUTE flaws and other imperfections in diamond gemstones can now be removed by use of a laser developed by the Raytheon Company of America.

In a series of experiments on natural diamonds, light energy from the laser was focused to extremely small areas and tiny holes "drilled" to the imperfections. The imperfections are then removed by a variety of methods

and the small-diameter holes cleaned.

The holes pierced by the laser are about two-thousandths of an inch in diameter—about the diameter of a human hair. These holes are not generally visible without magnification, and because of their small diameters, they do not change the stone's natural reflec-

SPACEWATCH

The International Telecommunication Union has made a proposal that a satellite communications system should be set up to provide aid following natural

disasters such as earthquakes and floods.

The ITU proposes the setting up of an organization in Geneva from where the coverage using two geo-stationary satellites over the Equator would be worldwide. Communications links required with this scheme include walkie-talkie radios, medium distance multichannel voice links and a mobile earth station. All this equipment would be air transportable with self-contained power sources.

DOLBY SOUND IN THE CINEMA

R ANK Audio Visual Ltd., in agreement with Dolby Laboratories, are now making Dolby noise reduction units available to cinemas on a rental basis. The new unit (Model 364) is a modification of the now well known Dolby "A" system. This reduces noise levels by boosting low level signals at all stages of recording until playback when they are reduced to their original level.

Cinema film sound is usually read from an optical track which is characteristically noisy, grain and dirt being the main offenders. The h.f. range of cinema sound is thus severely limited. By reducing noise the h.f. response can be greatly improved, for instance by using

a better quality speaker system.

The full potential of the playback unit will not be realised until Dolbied films are available, but Rank demonstrations have shown that in use with existing films the 364 unit gives a healthy though not dramatic improvement. At only £2.74 per week, many cinema owners should soon be taking advantage of this chance to improve the weak link in the film projection system.



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charger-



BY C.MARSHALL

An inexpensive 9V supply and Deac battery charger combined

F you use your transistor portable at home, this power supply unit will be a worthwhile investment. It will replace a 9V battery, the most common of supply voltages, by simply connecting the radio battery terminals to the output of the unit. Although this is a constant current device the power available is more than adequate for the majority of good quality transistor radios.

A built in bonus is the facility for charging nickel cadmium or Deac batteries. As any user of secondary cells knows, regular charging is the only way to get the best out of these.

DROPPING THE VOLTAGE

The circuit of Fig. 1 is unusual in that the normal mains voltage dropping transformer is missing, in this a capacitor (C1 or C2) is used to fulfil this function. One of the great advantages of using a reactance whether it be capacitive or inductive, is the fact that very little power is consumed although a voltage is dropped and a current passed.

For the capacitors used the reactance presented to the mains input is $1/(2\pi fC)$ ohms. This is, of course, an idealised figure since the capacitor diode bridge and load have resistance so the formula should be modified to $Z = \sqrt{(X_c^2 + R^2)}$ where X_c is the reactance and R the total circuit resistance. If comparative measurements were made it would be found that the reactance figure would be far in excess of the resistance figure so that we can say that the circuit is constant current device, the value being dependent on the series capacitance as the load presented plays little part in modifying the total impedance.

CROSSING THE BRIDGE

With the mains voltage applied and dropped it only remains for it to be rectified and smoothed. In this circuit the diodes D1-D4 afford rectification and the capacitor C3, smoothing. By rectification is meant the conversion of a.c. to d.c. However, when there is conversion there is normally some ripple present, so the capacitor C3 attempts to smooth this before it is passed on to the load.

ZENER PROTECTION

The diode D5 has the unique function of deciding the output voltage. In the condition of no load, the

COMPONENTS . . .

Resistors

R1 680kΩ ±watt carbon

Capacitors

C1 0.68µF 400V

C2 0.33µF 400V

C3 5,000µF elect. 25V

Diodes

D1-D4 1S100 or any silicon diodes of 50 p.i.v. and current capacity greater than 100mA D5 ZS9-1 Zener (see text)

Switches

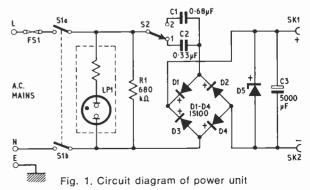
S1 Double-pole mains on/off toggleS2 Single-pole, double throw

LP1 Mains neon, FS1-500mA fuse, $2in \times 1\frac{1}{2}in$ Veroboard 0.15in matrix

voltage at the output would approach that of mains potential which could be dangerous. With the Zener diode D5 in circuit the voltage will drop to 9:1V. Obviously any low voltage diodes would be destroyed without this protective influence, so the diode serves as protection to the bridge and to supplying an output voltage on load of about 9V.

BATTERY CHARGING

Up to now we have only dealt with the unit in its power supply role at 9V. As a flexible secondary cell



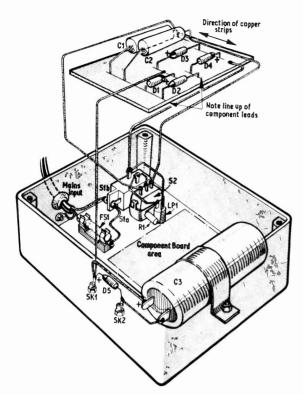


Fig. 2. Veroboard layout and interwiring details of power unit

charger there are a number of other points to be considered.

When charging a nickel cadmium cell it should be remembered that the charging current should not exceed the 10 hour rate. By this is meant that for a 200mAH cell, the charge current should be 200/10 = 20mA and at 225mAH, the current is 225/10 = 22.5mA.

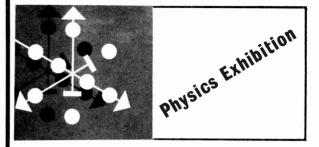
To recharge a totally discharged battery the total charge time should be the charging rate times 1.4. For example, if current is being replaced at the 10 hour rate the total time for recharge would be $10 \times 1.4 = 14$ hours.

With the circuit shown, in position 1 of the function switch S2, the unit will provide 25mA with Zener protection, for up to five Deac cells. This follows since the maximum charging voltage per cell is 1.5V, so that in the circuit given the output voltage will be around 9V with the cells disconnected. With a battery connected this will start to charge and the Zener diode will be cut off.

While the Zener diode will prove adequate for charging up to five cells, two ZS9·1 diodes connected in series should be used for six to ten cells, that is, for charging a 9 to 15V battery.

UNIT ASSEMBLY

The small components are assembled on a $2 \text{in} \times 1\frac{1}{2} \text{in}$ piece of 0.15 in matrix Veroboard, as in Fig. 2. Also given here are the complete interwiring details for the unit. The actual box dimensions for the prototype was $6 \text{in} \times 4 \text{in} \times 1\frac{1}{2} \text{in}$ but since any rearrangement of the components will not adversely affect performance, other housings can be tried.



The poor level of participation at this year's, the fifty-sixth, Physics Exhibition, was particularly evident by the large area of unused floor space in the Great Hall of Alexandra Palace. Earlier this year (March 13-16) this showcase of scientific instruments and apparatus seems to have been a sufferer of the same economic exigencies that have been denuding commercial exhibitions, particularly on the electronic scene.

With a reduction of nearly fifty per cent of last year's exhibitor count, the translation of the venue and amalgamation with another exhibition would seem inevitable. This, in fact, is what will happen next year when this will combine under the joint title of Labex and Physics Exhibition and be held at Earls Court. This Mecca will no doubt assure the future viability of this high quality scientific exhibition, but for me its "Ally-Pally" situation seemed in tune with its not too commercial, academic tenor.

This year the special features included exhibits arranged by the Electronics, Optical and Spectroscopy Group, to mark the occasion of the 1971 Nobel Prizes for both physics and chemistry to Professor Gabor for his developments of holography and Dr Herzberg for his work on the electronic structure and geometrics of molecules.

With man's desire for faster travel comes an awareness of the limitations of the existing systems. Conventional steel wheel-on-rail suspensions are limited to about 200 m.p.h. In overcoming this barrier two avenues have been explored; air suspension (hovercraft) and magnetic levitation (linear motors). While the former is commercially viable and a 250 m.p.h. tracked hovercraft will soon be starting test trials in this country, the linear motor has not yet enjoyed the same emergence.

The Department of Engineering at the University of Warwick demonstrated a linear motor model using superconducting magnets for the suspension and guidance of high speed vehicles with a conducting track.

In the same vein, a fascinating exhibit on the Decca Radar stand was a piezo-electric transducer in disc form made to act as a linear motor when subjected to ultrasonic vibrations at its resonant frequency. When excited this disc propelled itself silently along an inclined surface at speeds which were infinitely controllable up to 10cm/s: Possible research applications for this are tape and chart recorder drives and conveyor belts.

Ultrasonics also have applications in medicine as was shown by the Medical Research Council. The exhibit demonstrated that instantaneous blood velocity in the human aorta could be measured by Doppler analysis without involving the patient in chest surgery so enabling a quick assessment of heart pumping action.

A recent development from Mullard is a channel image intensifier which is fitted to the front of a television camera and can provide a gain of up to a hundred thousand so enabling the camera to produce bright clear pictures even in starlight.

Other Mullard exhibits included a fruit machine and a digital clock both specially devised for their educational service.

It is this sort of diversity that makes the Physics Exhibition so appealing and we can only hope that in its move to Central London that it manages to retain its particular identity.

REGULOUTE— A SELECTION FROM OUR POSTBAG

Correspondents wishing to have a reply must enclose a stamped addressed envelope. We regret we are unable to guarantee a reply on matters not relating to articles published in the magazine. Technical queries cannot be dealt with on the telephone.

Wrong formula

Sir—I have been teaching Physics, not pure Nuffield but with a slant that way, for only 10 years, but I share Mr. Cozens' concern, see "Paradoxical Stage" April Readout.

Perhaps he will be glad to know that the Association for Science Education, the Institute of Physics, and the numerous "new Maths" authorities are also aware and worried. The incompetence of pupils trained by some of the experimental methods is very obvious, and Mr. Cozens is quite right in saying that Physics teachers have to do their own traditional Maths teaching.

At an earlier stage, a colleague of mine who teaches both trad and modern Maths finds he has to teach 14 year olds that, say, 418 on a scale lies between 410 and 420. And at a higher level, some University entrance authorities are less than happy about the mathematical incompetence of many applicants who hold Maths and Physics Highers and A levels.

Incidentally, it's probably a traditional printer's error, but Mr. Cozens has the Wheatstone Bridge formula wrong. And very few pupils with a modern Physics Higher would know what a Wheatstone Bridge is, although they would know what to do with a collection of gates and a 5V supply.

It's sad that the same blind concern with change and trendiness affects the attitudes of some modern teachers to things like not hurting other people's feelings unless you really want to (manners), and sometimes getting on with something when you want to do something else (discipline). Luckily, most of these educational experiments are rethought before too much harm has been done.

W. H. Jarvis, M.A., A.Inst.P., Perthshire, Scotland.

I hope Mr. Jarvis is right in saying that educational experiments are usually put right before too much harm is done, but I am afraid I do not share his optimism, I think that this particular experiment with the "New Maths" should be left until the student has safely passed C.S.E. or G.C.E. in traditional maths.

About my error in the Wheatstone Bridge formula Mr. Jarvis is right. I will try to make it clear.

When the bridge is balanced

 $\frac{R1}{\overline{R2}} = \frac{R3}{R4}$

If RI is unknown resistance and R2 is the standard known resistance then

 $R1 = \frac{R3}{R\bar{4}} \times$

G. A. Cozens.

Better performance

Sir—As your Ferranti boys' Scorpio ignition looked the most sophisticated circuit yet published I purchased a set of components and assembled it for my Rover 2000 SC. The result is a distinctly brighter performance.

From the photograph enclosed you will notice that I have transposed the transformer and circuit connector block to suit the Rover. I have also clamped down the two large discharge capacitors by means of a hard Dural bridge-piece and a stainless steel rod screwed 6B.A. This rod passes through a clearance hole in the circuit board and is secured to the case by a couple of nuts. This is a more secure fixing than anchoring to the board which could distort in time and allow the

clamp to loosen.

Recently I went with a stop-watch
to my favourite testing stretch of
level road (there are six miles of
it) and got the following results.

Top gear: 30-50m.p.h. 11-4 secs. Scorpio 10-0 secs.

Top gear: 50-70m.p.h, 14-8 secs. Scorpio 11-2 secs.

3rd gear: 30-50m.p.h. 7.5 secs. Scorpio 7.0 secs.

3rd gear: 50-70m.p.h. 9.7 secs. Scorpio 8.6 secs.

The above results with brand new contact points, once they were burnt down a bit the discrepancy would be greater as I had previously found that after about 4,000 miles the engine got rough over 5,000 revs due to erratic ignition timing with the points pitted.

Please convey my congratulations to Messrs. Gibbs and Shaw.

G. A. Turner, Airdrie, Lanarkshire.

Mumbo-jumbo

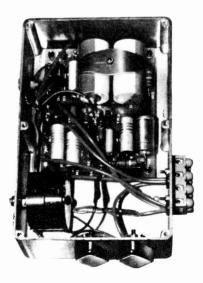
Sir—I resumed buying P.E. last December especially for the articles on "Logical Radio Control" and like Mr. W. G. Jones, (Letters, March issue), I found the whole thing almost unintelligible. I should like to make it clear that I have worked as a technician for a number of years in various types of laboratories and am used to unravelling the intricacies of strange systems

This is England, I am English and your magazine prints articles in English for me to understand. Of course Electronics has its own slice of language to be understood, but surely all the bits of electronic language have to be joined by clear, simple English. If you like, try printing your magazine using only an Electronic Dictionary and see how far you get!

Needless to say, I have not built any of the radio control circuits described (?) in the articles and feel disappointed about them. No doubt if I built them up just as shown and connected them all together it would all work, but I wouldn't know why and would have learnt nothing—and what if something went wrong? I was going to complain before now but let it slide until I read your Editorial in the April issue in which you seem to be defending the type of bad technical writing under discussion; your attitude being that it is our fault if we don't understand the mumbo-jumbo.

If your motives are good 1 can only assume that you don't realise how difficult it is to be a teacher and pass on information in a clear manner. If on the other hand, your intentions are less honourable 1 suppose it is in order to maintain some sort of superior position by withholding information.

C. F. Hughes, Bedford.



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BC 147	120	ST141	15p
BC148	12p	UT46	23p 35p
BC149	12p	2N696	15p
BC 157	15p	2N706A	12p
BC157 BC158	I4p	2N2926G	140
BC 159	14p	2N2926Y	13p
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BF178	32p	2N3055	72p
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2N4058

2N5459

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MISCELLANEOUS ITEMS
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Valve and Transistor Data book, 9th edition, 75p
Transistor equivalent book, BP1, 40p

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ELEC	TRO	LYTIC	cs		
1 µF 2 µF 4 µF 8 µF 16 µF 25 µF 50 µF 100 µF 250 µF 250 µF 500 µF	450V 500V 350V 450V 450V 50V 25V 50V 25V 50V 25V 50V	19p 20p 14p 16p 17p 8p 24p 10p 10p 12p 17p 17p 18p 25p	1,000µF 1,000µF 2,000µF 2,000µF 2,500µF 3,000µF 5,000µF 8=8µF 8=16µF 16-16µF 16-32µF 16-32µF	25 V 50 V 25 V 50 V 25 V 50 V 25 V 25 V 450 V 450 V 450 V	27p 39p 36p 53p 45p 60p 48p 55p 98p 18p 20p 27p 63p 49p
			50-50μF	350V	38p

MINIATURE ELECTROLYTICS

lμF	25 V	10µF	64V	
5µF	64V	16μ F	40V	
4µF	40V	25µF	25V	7
5μF	64V	30µF	157	40
8µF	15V	50µF	157	
8µF	40 V	100µF	15V	
Ι Oμ F	157			_

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3∄in × 3∄in	24p	25p
3∦in × 5in	27p	29 _D
l7in × 2 <u></u> ŧin	75p	57 p
l7in × 3∄in	£I	75 _D
Pins—both	sizes; packet of	36, 18p

ALUMINIUM BOXES with lids

anu	screws			
Туре	Length	Width	Depth	Price
GB7*	2∄in	5±in	1 tin	38p
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GB9*	4in	2∄in	1-in	38 _P
GB10*	4in	5≟in	l∮in	44p
GBII	4in	2∳īn	Žin	38p
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GB13	6in	4in	2in	52p
GB14	7in	5in	2½in	63p
GB15	8in	6in	3in	g18
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•	These sizes f			rds

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For Philips and similar cassette recorders. PUI2 Power unit for connection to 12V + or — E car electrical systems, giving 7½V, stabilised output. £3 •25

PP75 Mains power supply, output £1.95 71V d.c.
Both units are complete with cable and 5 pin D.I.N. plug

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B.A.F. wadding, 18in wide, 1in thick. The ideal lining for speaker enclosures. 25p per

LOW-OHM RESISTORS

2½ watt wire-wound, 1Ω , 1.8Ω , 2.7Ω , 3.3Ω , 3.9Ω , 4.7Ω , 5.6Ω , 6.8Ω , 8.2Ω

CAPA	CITO	RS		0.0027µF 0.003µF	500 V	S/M	15p
2-2pF	500 V	S/M	7 i p	0.003£F	1257	Cer. P.S.	5p 6p
3-3pF	500 V	\$/M	7 p	0.0033µF	500 V	Poly.	6p
5pF	500V	S/M	7 p	0.0033µF	1,000V	MDC	6p
10pF	125V	P.S.	5p	0.0036µF	500V	S/M	15p
10pF	500∨	S/M	71p	0.0047µF	125V	P.S.	9p
15pF	1257	P.S.	5p	0.0047µF	500 V	Poly.	6р
15pF	500V	Cer.	4p	0.0047µF	500V	S/M	20p
18 _P F	500V	S/M P.S.	7 1 P	0.0047µF	1,000V	MDC	6p
22pF	125V	P.S.	5p	0 005µF	1007	Mylar	3р
22pF	500V	S/M	7 1 p	0.005µF	500V	Cer.	5p 10}p
25pF	500V	S/M	7 ip	0 0068μF	125V	P.S.	10 3 p
27pF 33pF	500 V 125 V	Cer. P.S.	4p	0.0068µF	500V	S/M	30p
33pF	500V	S/M	_5p	0 0068µF	500V	Poly.	6р
39pF	500 V	S/M	71P 71P	0.0082µF	125V 500V	P.5. S/M	IQ}P
47pF	125	P.S.	′5P	0·0082μF 0·01μF	187	Disc	30p 4p
47pF	500 V	Cer.	4p	0.01µF	1257	P.5.	101P
50pF	500V	S/M	7 i P	0.01µF	160V	Poly.	4p
56 pF	500V	S/M	7 i p	0.01 µF	250V	M.F.	3p
68pF	125V	P.S.	5 n	0.01µF	400V	Poly.	3p
68pF	500V	S/M	7 t p	001µF	500V	Cer.	5p
75pF	500∨	S/M	7 P 7 P 7 P	0-01µF	500V	S/M	30 p
82pF	500∨	S/M	7 i p	0 01 µF	600 V	MDC MDC	7p
100pF	125V	P.S.	20	0.0111F	1,000V	MDC	9p
100pF	500V	S/M	7 jp	0 015µF	160V	Poly.	3р
100pF	500V	Cer.	_5p	0.015µF	400 V	Poly.	3р
120pF	500V	S/M	7 ½ p 5 p	0.02µF	100V	Mylar	3p
150pF 150pF	125V 500V	P.S. S/M	3ρ 7∮ρ	0 022μF	187	Disc	5p
150pF	500 V	Cer.	/ <u>1</u> P	0·022μF 0·022μF	250∨ 400∨	M.F.	3p
180pF	500 V	S/M	5p 71p	0.022µF	600V	Poly. MDC	3p 7 1 p
200pF	500 V	S/M	7 p	0.022µF	1,000	MDC	9p
220pF	125 V	P.S.	5p	0.033µF	250V	M.F.	4p
220pF 250pF	500V	Cer.	5ρ	0.033µF	400 V	Poly.	4p
250pF	500 V	S/M	8р	0.04711F	127	Disc	6р
270pF	500 ∨	Сег.	5p	0.047µF	160V	Poly.	3p
300pF	500∨	S/M	8р	0.047 _{/1} F	250V	M.F.	3р
330pF	125V	P.S.	5p	0 047µF	400 V	Poly.	4p
330pF 390pF	500∨ 500∨	S/M	8р	0.047µF	600V	MDC	.8p
470pF	1257	S/M P.S.	8p 5p	0·047μF 0·1μF	1,000∨ 30∨	MDC Disc	100
470pF	750V	Disc	5p	0.1µF	250V	M.F.	бр 4р
500pF	500V	S/M	8p	0.1µF	400V	Poly.	5p
560pF	500V	S/M	8р	0-1 µF	600V	MDC	10p
680pF	125V	P.S.	6р	0·1 µF	1,000∨	MDC	13p
680pF	500V	S/M	8р	0 15μF	250V	M.F.	5p
820pF	500∨	S/M	8ρ	0-22µF	160V	Poly.	6р
0.001µF	100V	Mylar	Зp	0.22µF	250V	M.F.	5p
0.001μF 0.001μF	125V	P.S.	6p	0.22µF	400V	Foil	10p
0.001µF	400∨ 500∨	Poly. \$/M	3p 10p	0·22μF 0·33μF	1,000V 250V	MDC M.F.	15p
0.001µF	500 V	Cer.	5p	0·47μF	250V	Foil	8p 8p
0.001µF	1,000V	MDC	6p	0.47µF	400V	Foil	15p
0.0015µF	400V	Poly.	3 p	0.47µF	1.000 V	MDC	20p
0.0015µF	500V	S/M	10p	1-0µF	250V	M.F.	15p
0 0015/2F	500V	Cer.	5p				
0.0018µF	500V	S/M	10p	Note:			
0·002μF 0·002μF	100V 500V	Mylar	3p	5/M = \$1	lver micz olystyren	1 % to	l.
0.0022µF	1257	Cer. P.S.	5p 6p	F.3. = pc	a.c. ratin	a = 300	TOI.
0.0022µF	500V	S/M	10p	M.F.=N	a.c. ratin 1uliard n	in foil	
0.0022µF	1,000V	MDC	6ρ	Cer. = c	eramic.		
			-				

PLUGS

L L U U U
Car aerial
Co-axial
D.I.N. 2 pin (speaker)
D.I.N. 3 pin
D.I.N. 4 pin
D.I.N. 5 pin, 180°
D.I.N. 5 pin, 240°
D.I.N. 6 pin
Jack, 2½mm unscreened
Jack, 2½mm screened
Jack, 3½mm unscreened
Jack, 34mm screened
Jack, ‡in unscreened
Jack, ‡in screened
Jack, stereo, unscreened
Jack, stereo, screened
Phono, plastic top
Phono, plated metal
Phono, fitted 4 ft lead
Wander, red or black
Banana 4mm, red or black

LINE SOCKETS

Car aerial
Co-axial
D.1.N. 2 pin (speaker)
D.I.N. 3 pin
D.I.N. 5 pin, 180°
D.I.N. 5 pin, 240° Jack, 3½mm Jack, ½in screened Jack, stereo, screened Phono, plated metal



SOCKETS

Co-axial, surface	8p
Co-axial, flush	8p
D.I.N. 2 pin (speaker)	10p
D.I.N. 3 pin	90
D.I.N. 5 pin, 180°	9p
D.I.N. 5 pin, 240°	9 _D
Jack, 2+mm	10p
Jack, 34mm	10p
Jack, £in unswitched	15p
Jack, in switched	17p
Jack, stereo, switched	240
Phono, single	50
Phono, 2 on a strip	7p
Phono, 3 on a strip	90
Phono, 4 on a strip	100
Wander, single, red or black	
Wander, twin strip	7p
Banana 4mm red, or black	60

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8р

Sinclair Project 60



Project 605

The easy way to buy and build Project 60



Project 605 is one pack containing: one PZ5, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free £29.95

All you need for a superb 30 watt high fidelity stereo amplifier.

Sinclair Radionics Ltd, London Road, St. Ives, Huntingdonshire PE17 4HJ, Tel: St. Ives 64311



Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

Project 60 modules are more versatile - using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all - price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair quarantee of reliability and satisfaction.

System	The Units to use	together with	£4.48	
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc		
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P U volume control etc.	£9.45	
12 W. RMS continuous sine wave stereo amp-for average needs	2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag P U , F,M Tuner, etc	£23.90	
25 W. RMS continuous sine wave stereo amp using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90	
80 W (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60 W. RMS into 8 ohms)	2 x Z.50s, Stereo 60 PZ.8, mains transformer	As above	£34.88	
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43	

Practical Electronics June 1972

Project 60 Stereo F.M. Tuner

Built and tested. Post free.





The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range; 87.5 to 108 MHz. Capture ratio: 1.5dB. Sensitivity: 7 µV for lock-in over full deviation. Squelch level: 20 µV. Signal to noise ratio: > 65dB. Audio frequency response: 10 Hz – 15 KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2 µV. Cross talk: 40dB. Output voltage: 2 x 150mV R.M.S. Operating voltage: 25-30 VDC.

Indicators: Stereo on ; tuning. Size: 93 x 40 x 207mm.

Stereo 60 Pre-amp/control unit

Built, tested and guaranteed.

£9.98



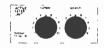
Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS—Input sensitivities: Radio — up to 3mV, Mag. p.u. 3mV: correct to R.I.A.A curve ±1dB:20 to 25,000 Hz, Ceramic p.u. — up to 3mV: Aux — up'to 3mV, Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE + 12 to —12dB at100Hz. Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm.

A.F.U. High & Low Pass Filter Unit

Built tested and guaranteed.

£5.98



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages—rumble (high pass) and scratch (low pass). Supply voltage = 15 to 35V. Current – 3mA. H.F. cut-off (—3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) 0.02% at rated output. Size: 66 x 40 x 90 mm.

Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual, 2.30 £4.48 2.50 £5.48



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8 $_{\Omega}$) and all lower outputs. Whether you

use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z.50 units are interchangeable

Power Outputs
Z.30 15 watts R.M.S. into 8 ohms using 35 volts.
20 watts R.M.S. into 3 ohms using 30 volts.
Z.50 40 watts R.M.S. into 3 ohms using 40 volts:
30 watts R.M.S. into 8 ohms using 50 0volts.
Frequency response: 30 to 300.000Hz ± 1dB.

ble with Z.30s in all applications).

Oistortion: 0.02% into 8 ohms.

Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 8Ω)
For speakers from 3 to 15 ohms impedance.

Size: 14 x 80 x 57 mm.

Power Supply Units





Designed special for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ 6 where a stabilised supply is essential.

PZ.5 30 volts unstabilised £4.98 PZ.6 35 volts stabilised £7.98 PZ.8 45 volts stabilised (less mains transformer) £7.98 PZ.8 mains transformer £5.98

Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at Once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost.



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Please send	Name
	Address
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VALVE MAIL ORDER CO. BLACKWOOD HALL

16a WELLFIELD ROAD, LONDON SW16 2BS SPECIAL EXPRESS MAIL ORDER SERVICE

Express postage Ip per transistor, over ten post free

	dn.		40		4		4		4-
1N21	₫p 0-17	AC126	£p 0-20 0-25	BF173	£p 0-25	GJ4M	£p 0-88	OC43 OC44 OC44M OC45	₫p 0-40
1N23 1N85	0.20	AC126 AC127	0.25	BE191	0.85	GJ5M	0-25	OC44	0.11
1N85	A-88	AC128	0.20	BF184	0.20	GJ7M	0.87	OC44M	0.17
1 N 2 5 3 1 N 2 5 6	0.50 0.50	AC187 AC188	0.25 0.25	BF185 BF194	0-20 0-17	HG1005 HS100A	0.50 0.20	OC45 OC45M	0·12 0·18
1N645	0.25	ACY17 ACY18 ACY19 ACY20 ACY21	0.80	BF195	0.15	MAT100	0.25	OC46	0.27
1N725A	0.20	ACY18	0.25	BF196	0.15	MAT101	0.30	OC57	0.60
1N914	0.07	ACY19	0.25	BF197	0.15	MAT120 MAT121	0.25	OC58	0-60
1N4007 -18021	0-20 0-20	ACY20	0.20 0.20	BFS61 BFS98	0.28 0.28	MAT121 MJE520	0.80	OC59 OC66	0-85 0-50
18113	0.15	ACY22	0.10	BFX 12	0.20	MJE2955	0.87	OC70	0.12
18130	0.18	ACY22 ACY27	0.25 0.17	BFX12 BFX13	0.25	MJE3055	0.87	OC71	0.12
18131	0.18	ACY28	0.17	BFX 29	0.25	NKT128 NKT129	0-85 0-80	OC72 OC73	0.20
18202	0.28	ACY39	0.50 0.15	BFX30	0.25	NKT129	0.80 0.25	OC73	0-80
2G240 2G301	0.20	ACV41	0.18	BFX29 BFX30 BFX35 BFX63	0.50	NKT211	0.25	OC74 OC7δ	0.25
2G302	1.97 0.20 0.82	ACY27 ACY28 ACY39 ACY40 ACY41 ACY44 AD140	0.25 0.50 0.50	BFX84 BFX85 BFX86	0.25	NKT129 NKT211 NKT213 NKT214 NKT216 NKT217 NKT218 NKT219 NKT229	0.15	0C76 0C77 0C78	0.25
2G306	0-80 0-82	AD140	0.50	BFX85	0.30	NKT216	0.87	OC77	0.40
2G371	0-22	VDIAG	0.50	BFX86	0.25	NKT217	0.85 1.13	0078	0·20 0·22
2G381 2G414	0.80	AD161 AD162	0-87 0-87	BFX87 BFX88	0.25 0.20	NKT219	0.88	OC79 OC81	0.20
2G417	0.22	AF106	0.80	BFY10	1.00	NKT222 NKT224	0.20	OC81D	0.20
2N214	0.48	AF114	0.25	BFY11	1.25	NKT224	0.22	OC81M	0.20
2N247	0.25 0.50	AF115 AF116	0.25	BFY17 BYF18	0.25	NKT251	0.24	OC81DM OC81Z	0.18
2N250 2N404	0.20	AF117	0-25 0-25	BFY19	0.25	NK 12/1	0-25 0-25	OC82	0-40 0-25
2N697	0.15	AF118	0.62	BEV24	0.45	NKT273	0.15	OC82D	0.20
2N698 2N706	0·15 0·40 0·10	AF119	0.20	BFY44 BFY50	1.00	NKT274	0.20	OC83 OC84	0.25
2N706	0.10	AF124	0.25	BFY50	0.22	NKT275	0.25	OC84	0-25
2N706A 2N708	0·12 0·15	AF125 AF126	0.20	BFY51 BFY52	0.20	NKT277	0-20 0 -25	OC114 OC122	0-88 0-60
2N709	0.68	AF127	0·17 0·17	BFY53	0.17	NKT301	0.40	OC123	0.65
2N711	0.87	AF139	0.80	BFY53 BFY64	0.42	NKT224 NKT251 NKT271 NKT272 NKT273 NKT274 NKT277 NKT277 NKT278 NKT301 NKT301 NKT304	0-40 0-75 0-75	OC139	0.25
2N987	0.58	AF178	0.55	DESTOR	0.65	NKT403 NKT404	0.75	OC140	0.85
2N1090	0-80 0-88	AF179 AF180	0-65 0-52	BSX27 BSX60 BSX76 BSY26 BSY27	0.50	NKT404	0.65	OC141 OC169	0-80 0-20
2N1091 2N1131	0.25	AF181	0.42	BSX 76	0.16	NKT678 NKT713	0-30 0-25	OC170	0.25
2N 1132	0.25	AF186 AFY19	0.40	BSY26	0·18 0·17	NKT773 NKT777	0.25	OC171 OC200	0.80
2N1302	0.18	AFY19	1.12		0.17	NKT777	0.88	OC200	0.40
2N1303	0·18 0·22	AFZ11	0.80 1.00	BS Y 51	0.50 0.12	O78B	0-38 0-20	OC201 OC202	0-70 0-80
2N1304 2N1305	0.22	AFZIZ	0.25	BSY95A BSY95	0.12	OA5 OA6	0.12	OC202 OC203	0.40
2N1306	0.25	A8Y27	0.82	BT102/50		0A47	0.10	OC204	0.40
2N 1307	0.25	A8Y28	0.25		0.75	OA70	0-10	OC205 OC206	0.75
2N1308	0-25 0-25	AFY19 AFZ11 AFZ12 A8Y26 A8Y27 A8Y28 A8Y29	0.80	BTY42 BTY79/10	0.92	OA71	0.10	OC206	0-90
2N1309 2N1420	0.09	ASY36 ASY50	0-25 0-17	BTY79/10	00 K	OA73 OA74	0·10 0·10 0·10 0·10	00207	0.90
2N1507	0.00	A8Y51	0.40	BTY79/40		0A79	0.10	OC470	0.80
2N 1526	0.38	ASY53	0.20		1.25	0A81	0.08	OC200 OC207 OC460 OC470 OCP71	0.75 0.90 0.90 0.20 0.80 0.97
2N1909	2.25 0.75	A8Y55	0-20 0-25	BY100	0.15	OA85	0·12 0·15	ORP12 ORP60	0-50 0-40
2N2147 2N2148	0.60	ASY62 ASY86	0.88	BY126	0-15	OA86 OA90	0.08	ORP61	0.42
2N2160	0.60	ASZ21	0.42	BY127	0.17	OA91	0.07	819T	0.80
2N2218	0.20	A8Z23	0.75 0.98	BY182 BY213	0-85 0-25	OA95	0.07	SAC40	0.25
2N2219 2N2287	0.20 1.08	AUY10 AU101	1.50	BY Z10	0.85	OA200 OA202	0.07 0.10	SFT308 ST722	0-88 0-88
2N 2297	0.20	BC107 BC108	0·10 0·10	BYZ11	0.32	OA210	0.25	ST7231	0.68
2N2369A	0.15	BC108	0.10	BYZ12	0.80	OA211	0.30	8X68	0-20
2N2444 2N2613	1.99 0.28	BC109 BC113	0-10 0-15	BYZ13	0.25	OAZ200 OAZ201	0.55 0.50	8X631	0-80
2N2646	0.45	BC115	0.20	BYZ15	1.00	0 4 7 2 0 2	0.42	8 X 640	0-40 0-50 0-55
2N2712	0.25	BC115 BC116	0.25	BYZ16	0.62	OAZ203	0.42	8X 641	0.55
2N 2784	0.50	BC116A	0-80 0-25	BYZ88C3	V3	OAZ202 OAZ203 OAZ204 OAZ205	0.80	8X 642	0.60
2N2846 2N2848	0.75	BC118	0.25 0.20	C114	0.15	OAZ205 OAZ206	0.42	8T722 8T7231 8X68 8X631 8X635 8X640 8X641 8X642 8X644 8X644 8X644	0-75 0-75
2N2904	0.20	BC121 BC122	0.20	CR81/03	0-85 0-25	OAZ200	0.47		0.50
2N2904A	0.25	BC125 BC126	0.68	CR81/05 CR81/40	0-47 2-50	OAZ208	0.82	V30/201P	0.75
2N 2906 2N 2907	0.20	BC126	0.65	CS4B	2.50	OAZ209	0.82	V60/201	0.50
2N2907 2N2924	0.28 0.28	BC140 BC147	0.55 0.15	CS10B DD000	3-18 0-15	OAZ200 OAZ207 OAZ208 OAZ209 OAZ210 OAZ211	0.32 0.32	V60/201P	0·75 0·10
2N2925	0·15 0·10	BC148 BC149 BC157 BC158 BC160	0.13	DDoog	0.15	OAZ222	0.45	X A101 X A102 X A151	0.18
2N2926	0.10	BC149	0.15	DD006	0.18	OAZ223	0.45	XA151	0.15
2N3054	0.50 0.75 0.10	BC157	0·15 0·12	DD006 DD007 DD008 GD3	0-40 0-88	OAZ224	0.45 0.22	XA152	0.15
2N3055 2N3702	0.10	BC158	0.12	0D3	0.88	OAZ241	0.22	XA161	0.25
2N3705 2N3706	0.10	BC169	0.13	GD4	0.06	OAZ244	0.22	XA162	0-25
2N3706	0.09	BCY31	0.85	GD5	0.88	OAZ211 OAZ222 OAZ223 OAZ224 OAZ241 OAZ242 OAZ244 OAZ246 OAZ290 OC16	0.23	XB101	0.48
2N 3707	0·12 0·10	BCY32	0-55	GD8	0-25 0-05	OAZ290	0.38	XB102	0-10
2N3709 2N3710	0.10		0.25	GD12 GET102	0.80	OCIGT	0.50 0.88	XB103 XB113	0.25
2N3711	0.10	BCY33 BCY34 BCY39 BCY40 BCY42 BCY70 BCY71 BCZ10 BCZ11	0-30	GET103	0-22	OC16T OC19 OC20 OC22 OC23	0.37	XB113 XB121	0·12 0·48
2N3819	0.85	BCY38	0.40	GET113 GET114	0.20	OC20	0-85	ZR24	0.68
2N3820 2N3823	0-60 0-75	BCY39	1.00 0.50	GET114 GET115	0-15 0-45	0022	0-50 0-60	Z8170	0.10
2N3823 2N5027	0.68	BCY42	0.25	GET116	0.50	OC23	0.80	Z8271	0.18
2N5088	0.88 1.00	BCY70	0.15	GET120 GET872	0.25	0C24 0C25	0.37	ZT21	0.25
28005	1.00	BCY71	0.20	GET872	0.80	OC26	0.25	ZT43	0.25
28178 28301	0-40	BCZ10	0.85 0.50	GET875	0.25 0.87	OC28	0.60	ZTX 107	0.15
28301	0.75	BD121	0.65	GET881	0.25	OC29	0.60	ZTX108	0.12
28501	0.87	BD123	0.80	GET875 GET880 GET881 GET882	0.25	OC30	0.40	ZTX 300	0.12
28703	0.62	BD124	0.75	G ICTARS	0.25 0.08	OC35	0.50	ZTX304	0.25
AA129 AAZ12	0-20 0-80	BDY11 BF115	1.62 0.25	GEX44 GEX45/1 GEX941	0.08	OC36		GG 37 F 66	0.16
AAZ13	0.12	BF117	0.50	GEX941	0.15	OC41	0.80 0.80	ZTX503	0.17
AC107	0.87	BF167	0.25	GJ3M	0.25	OC42	0.80	ZTX531	0.25

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Precision made — as used in record decks and tape recorders—ideal also for fan, blower, te. New and recorders—Meal also for extractor fan, blower, heaters, etc. New and perfect. Snip at **50p**. Postage 15p for first one, then 5p for each one ordered.



TELEPHONE HAND SET Ex-G.P.O. Perfect order. 50p each + 20p p. & p.

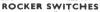


12 VOLT IL AM

This comprises double-wound 230/240V mains transformer with full wave rectifier and 2000 m/f/d smoothing. Price \$1.50, plus 20p post and packing.

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New Light Dimmer. This uses the latest technique from America, a self-triggering device known as the thermo tab and has enabled us to produce a really reliable dimmer at a remarkably low price—namely \$2.50 cach or 10 for \$22.50.





each. 10 for \$1.35.

Amplifier Case. Teak veneer on \$\frac{3}{2}\$ in ply, modern appearance and design. Size—front 13\text{in} \times \text{plane} \times \text{plane} \text

tions in box with commit entry. Frie 22-00 each plus 20p post and insurance and Brown - For van lighting or camping, etc. Will light a 2ft 20 watt standard fluorescent tube from a 12V car battery, current approx. 2A. Very well made unit using die cast chassis. Size 11 in × 2in × 1 in. Frice 25-50 complete with lamp holders and tube

clips.
Flex Cable Snip. 3 core heavy circular T.R.S. waterproof flex, ideal for running down the garden to pool or shed. 1-5mm cores (5 amp) 100 yard coils \$4.25 plus carriage 75p up to 200 miles. \$1.50—500 miles.

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bed, or chair. Outfit com
prises microphone with call
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master inter-com. Simply
plugs together. Originally
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Double Leaf Contact.

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MULLARD 1.F. MODULE
This is a fully screened intermediate frequency module
for amplification and detection of f.m. signals at
19.7M Hz amd a.m. signals at 470k Hz. The first stage
is used as an if, amplifier for f.m. and a self-oscillage
naiver for a.m. operation, in conjunction with an
external oscillator coil. 75p each; 10 for 28.75; 100
for 282.50. With connection dig.



COMPUTER TAPE



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ERGOTROL UNITS
These units made by the Mullard Group are for operating and controlling d.c. Motors and equipment from A.C. mains.
Thyristors are used and these supply a variable d.c. resulting in motor speed control and operating efficiency far superior to most other methods.
The units are contained in wall mounting cabinets with front control panel on which are fuses—push buttons for on/off and the variable thyristor firing control.
4 models are available—all are brand new in makers cases:

4 models are available—all are braild lew in makers cases: Model 2410 for up to 5 amps 217-50 Model 2411 for up to 10 amps 227-50 Model 2415 for up to 80 amps 295-00 Note: 2415 is a floor mounting 3 phase unit.



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CENTRIFIGAL FAN
Mains operated, turbo-blower type. Pressed
steel Housing contains motor and aluminium
impeller. Motor is 1/10th hg giving considerable
air flow but virtually no noise. Approx. dimensions 10½ in wide by 12 india. Outlet into trunking
10½ in × 4½ in. 24-95 + £1.

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THE AMPLIFIER
SENSATION OF THE YEAR
You will be amazed at the
fullness of reproduction and at

fullness of reproduction and at the added qualities your records or tuner will reproduce. Built into metal chassis ready for monunting on plinth this amplifier circuit with an output power of 6W R.M.S. split over the two channels. The amplifier'is ideal for use with normal pick-ups and tuners, it has a double wound mains transformer and ganged volume and tone controls—also switching for Mono to Stereo, tuner of pick-up. UNREPEATABLE PRICE is \$650 plus 209. Mono to Stereo, tuner or pick-up. UNREPEATABLE PRICE is \$6-50 plus 20p post and insurance. Simulated Teak cabinet ready for mounting amplifier \$1-50 (postage free when ordered with chassis).

P.E. GEMINI

Dual purpose twin 30W stereo amplifier for exceptional performance. Complete kit of parts \$45 or reprint of data and parts list 25p.





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Uses 4 transistors, and has an output of 500mW into 8 ohms speakers. Input suitable for crystal mic. or pick-up. 9V battery operated. Size 2in long 14in wide lin high.
SPECIAL SNIP PRICE 60p each. 10 for \$5.

CAPACITOR DISCHARGE CAR IGNITION



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Easiest way to fault find—traces signal from serial to speaker—when signal stops you've found the fault. Use it on Radio, TV amplifier, anything—complete kit comprises two special transistors and all parts including probe tube and crystal earpiece. \$22—twin stethoset instead of earpiece 75p extra—post and ins. 20p.



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Model 772—small but powerful lin pull—approx. size 1
i x 1 in 160p.

Model 400/1 lin pull. 8ize 2
i x 2 x 1 lin 75p.

Model TTIO 1 lin pull. 8ize 3
i x 2 i x 2 in 50 plus 20p
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MAINS RELAY BARGAIN Special this month are some single, double and treble pole changeover double and treole pole changeover relays. Contacts rated at 15 amps. Operating coil wound for 240 V. A.C. Good British Make. Unused. Size approx. 1 in × 1 ln. Open construction. Single pole 25p each 10 for 22-25 Treble pole 35p each 10 for 23-15



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Electronically changes speed from approximately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all control. Kit includes all parts, case, everything and full instructions. 21-50 plus 13p post and insurance. Made up model also available, 22-25 plus 13p post and p.



\$24.

Ditto as above but for printed circuit 5p each. 10 for 45p, 100 for 24-25.

Sub Miniature Slide Switch. DPDT 19mm (Jin approx.) between fixing centres. 12p each or 10 for £1-06.



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MINIATURE WAFER SWITCHES

WAFER SWITCHES
2 pole, 2 way—4 pole, 2 way—
3 pole, 3 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole
6 way—1 pole, 12 way. All at 309 each. 21.80 for ten, your assortment.



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Almost zero resistant in sunlight increases to 10 K Ohms in dark or dull light, epoxy. Rated at 500 MW, wire ended. 48p with circuit. Also ORP12 light cell 45p.

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for portable, car radio
or transmitter. Chrome plated
-six sections, extends from 7i to
47in. Hole in bottom for 5B.A. serve
p. KNUCKLED MODEL FOR F.M. 38p.

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2in square full vision for flush mounting. Moving iron instrument. Ideal for charger, Price 43p each. 10 for \$2.90.





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Cleans the air at the rate of
10,000 cubic ft. per hour.
Suitable for kitchens, bathrooms, factories, changing
rooms, etc., it's so quiet it can
hardly be heard. Compact, 5;
casing with 5;
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5A changeover contacts, 9p each. £1 doz. 15 amp Model 10p each or £1-05 doz.

10p each or \$1.05 doz.

Dry Film Lubricant. In aerosol can for easy application and for putting lubricant into places where the normal oil can cannot reach. Home and everyday uses. We have purchased a large quantity of these from the Liquidator and are able to offer them to you at about half of the original list price. 30p per (80z.) can or 12 cans for \$25 post paid. The lubricant is I.C.I. fluon L169.



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PCH101 FCH101 FCH101 FOH221 FOH221 FOH201 FCJ101 FCJ101 FCJ101 FCJ201 FCX101 FCX101 FCX101 FCX102 FXX102 FX	2 p 0 87 1 1 05 1 1 22 1 1 50 1 1 22 1 1 50 2 7 1 1 20 1 1 50 1 2 7 1 1 20 1 1 1 20 1 1 2 1 1 2 1 1 2 1 1 2 1 2	TH9014P PRE-AMP DATA 8H MULLA LINEA TA A241 242 283 300 310 320 350 435 521 522 530 700 700 TAD100 TAD100 TAD100 TAD100 TAD100 TAD100	#1.50 EETS #0.124 ARD 130.124 4.00 0.70 0.80 2.00 1.30 0.65 2.10 0.65 2.10 0.67 1.13 4.95 2.60 3.50 0.97 1.197 1.97 1.97 1.97	3 watt Audio Amplii Data 8heets 10p eac RCA Type	Type 1-24 25-99 Sp 2p CA3033A 4-28 8-80 CA3035 1-28 1-10 CA3035 1-128 1-10 CA3036 1-128 1-10 CA3036 1-128 1-10 CA3037 1-28 1-12 CA3038 2-58 2-25 CA3038 2-58 2-25 CA3038 3-40 8-08 CA304 1-09 0-97 CA304 1-20 1-07 CA304 1-09 0-07 CA304 1-00 0-07 CA305 1-08 1-08 1-07 CA305 1-08 1-08 1-07 CA305 1-08 1-08 1-08 1-08 1-08 1-08 1-08 1-08
PCH101 FCH101 FCH101 FOH121 FOH201 FOH201 FCY101 FCY101 FCY101 GENERA ELECTRIC PA299 PA246 PA206 SIEMENS TAA435 SGS TAA661B £1 TAA621 £2 All TTL IC' Or quantity or quantity	2 p 0.87 1 1.05 1.32 1 1.55 1.32 1 1.55 1.55 1.05 1.05 1.05 1.05 1.05 1.	TH9014P PRE-AMP DATA 8H MULLA LINEA TAA24I 242 283 300 310 320 350 435 521 522 520 670 700 770 TAA101 TAD100 TAD110 TAA76	#1.50 EETS #0.124 ARD 130.124 4.00 0.70 0.80 2.00 1.30 0.65 2.10 0.65 2.10 0.67 1.13 4.95 2.60 3.50 0.97 1.197 1.97 1.97 1.97	3 watt Audio Amplii Data 8heets 10p eac RCA Type 1-24 25-99	Type 1-24 25-99 Sp 2p CA3033A 4-26 3-80 CA3035 1-28 1-10 CA3035 1-128 1-10 CA3035 1-128 1-10 CA3035 1-128 1-10 CA3037 1-25 1-25 CA3037 2-55 2-25 CA3038 2-55 2-25 CA3038 2-55 2-25 CA3038 1-10 1-10 1-10 CA3041
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PA299 PA246 PA266 SIEMENS TAA151 TAA455 SGS TAA661B \$1 TAA452 All TTL ICO for quantity of 10 PR TO	2 p 0.87; 1.06; 1.32; 1.50; 1.	TH9014P PRE-AMP DATA 8H MULLA LINEA TAA241 242 263 300 310 320 350 485 521 522 530 7700 811 TAB101 TAD100 TAD100 TAD100 ders, 40.68 ders, 40.20 ders, 40.20 ders, 40.20	#1-50 EETS #0-124 RP	3 watt Audio Amplii Data Sheets 10p eac RCA Type	Type 1-24 25-99
PA239 PA246 PA246 PA266	2 p 0.87; 1.06; 1.10; 1.22; 1.50; 1.	TH9014P PRE-AMP DATA 8H MULLA LINEA TAA241 242 263 300 310 320 350 435 521 522 530 770 7700 811 TAB101 TAA71 TBA65 be mixed to to. ders, £0.20 ders, £0.25	#1-50 EETS #0-124 RP 39 1-30 4-00 0-70 0-85 2-10 0-73 0-87 1-97 1	3 watt Audio Amplii Data Sheets 10p eac RCA Type	Type 1-24 25-99
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PCH101 FCH101 FCH101 FOH121 FOH201 FOH201 FOH201 FCJ101 FC	\$\frac{8}{1.82} \\ \frac{1.82}{1.82} \\ \frac{1.82}	TH9014P PRE-AMP DATA 8H MULLA LINEA TAA24I 242 283 293 300 310 320 350 435 521 522 530 670 700 700 TAD110 TAD100 TAD110 TAD110 TAD110 TAA76 TBA65 be mixed to ta. ders. 40.26 ders. 40.26 ders. 40.83 6.C. Holders. C. Holders.	#1-50 EETS #0-124 RP 1-30	3 watt Audio Amplii Data 8heets 10p eac RCA Type	Type 1-24 25-99
PCH101 FCH101 FCH101 FOH121 FOH201 FOH201 FOH201 FCJ101 FC	2 p 0.87; 1.06; 1.32; 1.50; 1.	TH9014P PRE-AMP DATA 8H MULLA LINEA TAA24I 242 283 293 300 310 320 350 435 521 522 530 670 700 700 TAD110 TAD100 TAD110 TAD110 TAD110 TAA76 TBA65 be mixed to ta. ders. 40.26 ders. 40.26 ders. 40.83 6.C. Holders. C. Holders.	#1-50 EETS #0-124 RP	3 watt Audio Amplii Data 8heets 10p eac RCA Type	Type 1-24 25-99

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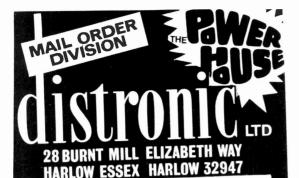
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١	T4 8 2G381T OC81		
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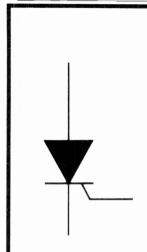
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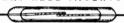
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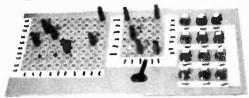
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