

## ADCOLA Soldering Instruments add to your efficiency

 THE NEW 'INVADER' ADCOLA L. 646for Factory Bench
Line Assembly
A precision instrument--supplied with standard $3 / 16^{\prime \prime}(4.75 \mathrm{~mm}$ ) diameter, detachable copper chisel-face bit ${ }^{*}$
Standard temp. $360^{\circ} \mathrm{c}$ at 23 watts.
Special temps. from 250 "c$410^{\circ} \mathrm{C}$.
*Additional Stock Bits
(illustrated) available
COPPER


Don't take chances. We don't.
All our ADCOLA Soldering Instruments are of impeccable quality. You can depend on ADCOLA day after day. That's why they're so popular. You get consistent good service... reliability . . . from our famous thermally controlled ADCOLA Element and the tough steel construction of this ideal production tool.


*
Write for price list and catalogue


COMPONENTS MUST BE CLEARED

Transistor Radio Cases: 25p each. Size $9 \frac{1}{2}^{\prime \prime} \times 6 \frac{1}{2}^{\circ} \times 3 \frac{1}{2}^{\circ}$. Post 15 p . Speakers: 35p. 2 $\frac{1}{2}{ }^{\prime \prime} 8 \%$. Brand new. Post 15P. VHF/FM Tuners: 95p. 88-108 megs takes EEC85 valve (extra). BSR R/P
new, 200250 V tors: 95p. Brand Precision Tape Motors: El-95. 200/250V. Famous German manufacturer. Post 20p.
Transistor Gang Condensers: 20p. Miniature AM. Post free. Modern Gang Condensers: 30p.
AM/FM or AM only 20p. POst 10 p AM/FM or AM only 20p. Post 10 p Transistors 15p each, Post free.
ACI26, ACI28, AFII4 AFII7 AC126, OC45,OC71, OC81, OC81D. Valve ELL80 50p. Only stock in the country.
500500 K each. Post 5p. D SW DISW I meg./l00 KO 100 K 2. $500 / 500 \mathrm{~K} \Omega$. SISW 500 . 5/SW 625 ment fitting. Post 20p

Knobs: 100,000 to clear. Brand New. 100 assorted radio and ty knobs. 50p. Post 25p. Radios 6398 Transistor LW/ Personal 6 Transistor MW Post 15p.

TV TUBES REBUILT GUARANTEED 2 YEARS


14" £3.95: 17" \& 19" £5.95: $21^{\prime \prime} 623^{n} £ 6.45$
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Brand new $44^{\prime \prime}$ wide $\times 16^{\prime \prime}$ deep $\times 18^{\prime \prime}$ high with legs. A superb piece Brand new 44 wide $\times 16$ deep $\times I L E$ STOCKS LAST,

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## PHOTOELECTRIC KIT

 transistor, Latching Relay, :2 Transistors, B Diodew, Resistors, fiain ('untrol, Terminal Block, Elegant Case, Acrews, etc. In fact eweything vou hetil to buike a Ateadr-Ligh modulated-light weration.


## INVISIBLE BEAM OPTICAL KIT

Everything needed (except plyworl) for building: 1 Luxisible-bean Projector and I Photocell Receiver (as illustrated). Nuitable for all Photoelectric Burglar Alarms, Counters, Door Openers, ete.
CONTENTS: 2 lenses, $\mathfrak{2}$ mirrors, $: 4 \%$-legrew woolen blochs, fiffa-led filter, projector lamp holder, building plans, ete. Price $£ 1 \cdot 25$. Pontage and Pack. 10p (J.K.). Commonwealth: Surface Mail 20p; Air Mail j0p.

## LONG RANGE INVISIBLE BEAM OPTICAL KIT

CONTENTS: As above. Twice the range of standard kit. Larger Lensen, Filter, etc Price 21.85. Postage antl Pack. 1.jp ( $\left.{ }^{\top} . \mathrm{K}.\right)$. ('ommonwealth: Surface Mail 20 p ; A Mai 21 .

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Versatile Invisibte-beam, Relay-less, Stealy-light Photo-Switelh, Burglar Alarm, Door Opener, Conter,
Hesistors, Screvs, Full Size Plans, lansintur, 3 Transistors, Chassis, Plastic C'ase Resistors, Bcrens, etc. Ftilsize Plans, Instructions, Data Sheet " 10 Atranced Photn Price £1.25. Pos
JUNIOR OPTICAL KIT
CONTENTS: 2 Lenses, Infra-red Filter, Lamphoder, Bracket, Ilans, etc. Fiverything (except plywoal) to buid 1 miniature invisible bean projector and photocell receiver Price 75p. Post and Pack 10 petric Kit.

YORK ELECTRICS Mail Order Dept. 335 BATTERSEA PARK ROAD, LONDON, S.W. 11 Send S.A.E. for full details, a brief description of all kits atd Projects

## IP IL.P. (Electronics) Ltd



## HY40 <br> POWER AMP

Lets face it - an immediate success, the HY 40 is here to stay. HY40 means Hybrid Power, power neatly locked away inside an Intregrated Circuit. Power the modern way, simply mount only five additional components on a printed circuit board (all of which are supplied with the HY40). Power not only for $\mathrm{Hi}-\mathrm{Fi}$, power for Groups, for public address, for industry, power for all.
HY40 is HI-FI POWER ILP are POWER PROUD
In addition to the P.C. board and manual supplied with the HY40 we now include the five remaining components, at minimal cost, needed to complete the assembly of a High Performance Power Amplifier
By merely combining two HY40s with a Stereo Preamplifier (2 $\times$ HY5) and simple Power Supply (PSU45), premium quality stereo may be obtained for a very modest outlay.
The free manual supplied with the HY40 gives clear, easy build instructions for Power Supply: volume, bass, treble and balance controls, together with inputs for Ceramic and Magnetic Pick-ups, Tape, Tuner and Auxiliary functions.
Internally the HY40 is based on conventional and proven circuit techniques developed over recent years.


OUTPUT POWER British Rating 40 WATTS PEAK, 20 watts RMS continuous.
LOAD IMPEDANCE 4-16 ohms INPUT IMPEDANCE 22Kohms at 1 Khz.
INPUT SENSITIVITY 300 mV for maximum output.
VOLTAGE GAIN 30 db at 1 KHz . FREQUENCY RESPONSE $5 \mathrm{~Hz}_{2}$ $60 \mathrm{KHz}+1 \mathrm{db}$.
TOTAL DISTORTION less than $1 \%$ (typical $0.1 \%$ ) at all output powers.
SUPPLY VOLTAGE $\pm 22.5$ volts D.C.
SUPPLY CURRENT 0.8 amps maximum.
PRICE: including comprehensive manual, P.C. Board and FIVE EXTRA COMPONENTS:
MONO £4-40 STEREO £8-80 all post free.

A WORLDS FIRST TO JOIN THE WORLDS BEST

The HY5 is a unique and revolutionary concept in HighFidelity pre-amplifiers. Thanks to the latest techniques, all feedback and equalization networks are, for the first time, combined into an integrated pre-amplifier circuit.

Simply by adding volume, treble, bass potentiometers and only three stabilizing capacitors, which are supplied, your HY5 is complete and ready for use.

The HY5 provides equal ization for almost every conceivable input. This years developments in equalization technique enables precise correction for both output voltage and frequency response for any crystal or ceramic cartridge. Yet ano ther feature of the HY5 is its inbuilt stabilization circuit, allowing it to be run off any unregulated power amplifier supply.

The HY5 contains a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo preamplifier.

Specifically and critically designed to meet exacting $\mathrm{Hi}-\mathrm{Fi}$ standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY40 and PSU45 forms a completely integrated system.

## INPUTS

Magnetic Pick-up (within $\pm 1 \mathrm{db}$ RIAA curve) 2 mV
Tape Replay (external components to suit head). 4 mV Microphone (flat) 10 mV
Ceramic Pick-up lequalized and compensatable) $20-2000 \mathrm{mV}$ variable.
Tuner (flat) 250 mV
Auxiliary 1250 mV .
Auxiliary $22-20 \mathrm{mV}$
OUTPUTS
Main Pre-amp output 500 mV . Direct tape output 120 mV .
ACTIVE TONE CONTROLS
Treble +12 db
Bass $\mp 12 \mathrm{db}$.
INTERNAL STABILIZATION Enables the HY5 to share an ynregulated supply with the Power Amplifier.
SUPPLY VOLTAGE
15-25 volt.
SÚPPLY CURRENT
20 mA approx.
OVERLOAD CAPABILITY
better than 30 db on most sensitive input infinite on tuner and auxl. OUTPUT NOISE VOLTAGE

$$
0.5 \mathrm{mv} .
$$

0.5 mV .

PRICE
Mono $£ 3-60$ Stereo $£ 7$-20


The PSU45 is specifically designed to supply, simul taneously, your HY40 (in mono or stereo format) and one or two HY5s.

Spec.
PSU45 $\pm 22.5$ volts, 2 amps simultaneously.

PRICE: $£ 4-50$ including Postage and Packing

## The Iargest selection

NEW LOW PRICE TESTED S.C.R.'s PIV

| PIV | T0-5 | T0.66 | $7 A$ TO66 | 10A | 164 $\mathrm{TO}-48$ |  | $\begin{array}{r} 30 \mathrm{~A} \\ \mathrm{TO} 0-48 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 m | ${ }^{28}$ | ${ }^{20} 8$ | $2_{0}$ | 19 |  | ${ }^{2} 1$ |
| 30 |  | . 25 |  |  |  |  | 1.15 |
| 100 | 0.25 | 0.73 | 0.58 | 0.68 | ${ }_{0.75}^{0.68}$ | 78 | 1.40 |
| 200 | 0.35 | 0.37 | 0.57 | 0.81 | 0.75 |  | 1.6 |
| 400 | 0.43 | 0.47 | 0.67 | 0.78 | 0.93 |  | 1.7 |
| 600 | 0.58 | 0.57 | 0.77 | 0.97 | 1.25 | 25 |  |
| 800 | 0.68 | 0.70 | 0.90 | 1.20 | 1.50 |  | 4.00 |
| SIL. RECTS. TESTED |  |  |  |  |  |  |  |
| PIV | 300 m A | A 750 mA 1 A |  | 1.ja 3A 10A |  |  | 30 A |
|  | ${ }^{2} \mathrm{p}$ | ${ }^{20}$ | 25 |  |  |  |  |
|  | 0.04 | 0.05 | 0.05 | 0.07 |  | 0.21 |  |
| 100 | 0.04 | 0.08 | 0.05 | 0.18 | 0.16 | 0.23 | 3 |
| 200 | 0.05 | 0.09 | 0.08 | 0.14 | 0.20 | 0.24 |  |
| 400 | 0.08 | 0.13 | 0.07 | 0.20 | 0.87 | 0.37 | 7 |
| 600 | 0.07 | 0.18 | 0.10 | 0.23 | 0.84 | 0.4 |  |
| 800 | 0.10 | 0.17 | 0.13 | 0.25 | 0.87 | 0.55 |  |
| 1000 | 0.11 | 0.25 | 0.15 | 0.30 | 0.46 |  |  |
| 1200 |  | 0.33 |  | 0.33 | 0.57 | 76 |  |
| triacs |  |  |  | LUCAS SILICON RECTIFIERS |  |  |  |
| vbo | M 2 A | $\begin{array}{r} 6 A \\ \text { TO-66 } T \end{array}$ | $10 \mathrm{~A}$ |  |  |  |  |
|  | T0.1 |  |  |  |  |  | type. 21.10 each. |
|  | \% | 20 | 2p |  |  |  |  |
| 100 | . 50 | 0.69 | 1.00 |  | diacs |  |  |
| 200 | 0.70 | 0.90 | 1.25 | FOH | USE |  |  |
| 00 | 0.80 | 1.00 | . 60 | R100 |  |  | 7 p |

2A POTTED BRIDGE RECTIFIERS 200V 50p

| UNIJURCTION <br> UT4. Eqvt. 2N2646, <br> Eqvi. TIS43, BEN3000 <br> 27p each, $25-99$ 25p <br> 100 UP 20p. |
| :---: |
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AF239 PNP GERM AF239 PNP GERM, BIRTORA. RF MIXER © OSC. UP TO 900 PLACEMENT FOR AF139-AF186 \& $100^{\circ}$ OF OTHER USES IN VHF OUR GPECLAL esch, $25-99$ 840 each $100+80 \mathrm{p}$ each.

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## 2N 381 <br> 2N 3820

## CADMIUM CELLS

ORP12 48p
ORP60, ORP6140p each

## PHOTO TRANS

COMT Type. 48 D

8IL. G.P. DIODES 8 P | 300 mW |  |
| :--- | :--- |
| 40 PIV (Min.) | $100 \ldots$ |
| 100.50 |  |
| 1.50 |  | 40PIV (Min.)

Bub-Min.
500 Full Tested $1,000 \ldots 9.00$ Ideal for Organ Builders.

D1aDl silicon Unilateral switch sop each.
A Bilicon Planar, monolithic integrated circuit having thyriator electrical characteristics, but with an anode gate and a built-In "Zener" dlode between gate and cathode. Full data and application circuite avallable on request.

ADI61
AD $1622_{P N P}$ MATCHED COMPLE MATCHED COMPLE-
MENTARY PAIRG MENTARY PAIRS
OF GERM. POWER TRANBIBTORA. For mains driven out and Radio recelvers. OUR LOWEST PRICE OF 68p PER PAIR

2N3055 118 WATT SIL OUR PRICE 68 EACL

FULL RANGE OF ZETER DIODES VOLTAGE RANGE 2-887. 400 mF (D0.7 Case) 13p ea. 13w (TopHat) 18 p ea. 10 W (80-10 Stud) $25 p$ ea. All fully tested $5 \%$ tol. and
marked.
State voltage required.

BRAND MEW TEXAS GERM. TRAMBISTOR Coded and Guaranteed Pak No. $\begin{array}{llll}\text { T2 } & 8 & 2 G 374 & 0 C 75 \\ \text { T3 } & 8 & 2 G 3744 \mathrm{~A} & 0 \mathrm{OC81D}\end{array}$ $\begin{array}{llll}\text { T3 } & 8 & 2 G 3744 A & \text { OC81D } \\ \text { T4 } & 8 & \text { 2G381A } & \text { OC81 } \\ \text { T5 } & 8 & 2 G 382 T & \text { OC82 }\end{array}$ $\begin{array}{llll}\text { T6 } & 82 \mathrm{GG3} 2 \mathrm{~T} & 0 \mathrm{OC} 24 \\ \text { T7 } & 82 \mathrm{G} 345 \mathrm{~A} & \text { OC44 } \\ \text { OC45 }\end{array}$
 T10 82G417 AF117

## 2N2060 NPI SIL. DUAL

 TRANS. CODE D1699 TEXAS. Our price 25 p oach.120 VCB BIXIE DRIVER TRATSIETOR. gim B8X21 \& C407, 2N1893 FULLY TESTED AND CODED ND120. 1-2 17 p each. TO-5 N.P.N 25 up 15p each
Sil. trans. auitable for P.E. Organ. Metal To-1 Eqvit. ZTX.
Any Qty.

## EX-EQUPMENT AF117 Trandard afll 7 transistors. Large cat heade type. Lead real value at 15 for 50 p .

## KING OF THE PAKS

## SUPER PAKS

## NEW BI-PAK UNTESTED SEMICONDUCTORS



U20 12"1-5.Amp ailicon rectifters Top-Hat up to 1,000 PIV . U21 30 A.F. germanium alloy trangistors 2G 300 series \& OC71 U23 30 Madt's like MAT series PNP trannigtors U24 20 Germanium 1-Amp rectiffers GJM up to 300 FIV. U2̄ 25 300Mc/s NPN sllicon transistors 2N708, 138Y27. U26 30 Fast swltching silicon diodes like IN914 micro-min

$$
\begin{aligned}
& \text { Experimenters' assortment of integrated circuits } \\
& \text { Gates, Afip-flops, registers, etc., } 8 \text { assorted pleces . }
\end{aligned}
$$

$$
10 \text { 1-Amp SCR's TO-5 can up to } 600 \text { PIV CRs } 1 / 2 \overline{5}-600
$$

$$
15 \text { Plastle case } 1 \text { amp ailicon rectiflers IN } 4000 \text { series }
$$ 30 8il. PNP alloy trana. TO-5 BCY26, 28302/4 25 8il. planar trans. PNP TO-18 2N2906 $2 \overline{5}$ Sil. planar NPN trans. TO-5 BFY50/51/52 30 811. alloy trans. 80-2 PNP, OC200 28322 20 Fast switching sil. trans. NPN, $400 \mathrm{Mc} / \mathrm{s} 2 \mathrm{~N} 3011$ 30 RF germ. PNP trans. $2 \mathrm{~N} 1303 / \overline{5}$ TO-5 10 Dual trans. 6 lead TO-5 2N20f0

$$
25 \mathrm{RF} \text { germ. trans. TO-1 OC45 NKT72. }
$$

## 30200 m A sub-min. Sill Hodes

Snicon planar tramsion NPN sim. BSY9JA
d) silicon rectiflers Top-Hat 750 mA up to 1.000 V

20 Mixed volta 1 watt Zener diodes.

$$
20 \text { Sil. Planar N PN trans. low noise amp } 2 \text { N } 3707
$$

$$
25 \text { Zener diodes } 400 \mathrm{~mW} \text { D07 case mlxed volts, } 3-18
$$

## U42 10 VHF gern. PNP trans. TO-1 NKT667 AF117

Code Nos. mentloned above are given as a guide to the ty
the Pak. The devices thenselves are normally unmarked

## GENERAL PURPOSE GERM. PNP <br> \section*{POWER TRANSISTORS}

Coded GP100. BRAND NEW TO-3 CASE. PO\&8. REPLACEMENTS FOR:-OC25-28-20-30-35-36. NKT REPLACEMENTS FOR:-403-404-405-406-430-451-452-453. TI3027-3028, $2 N 250 \mathrm{~A}, 2 \mathrm{~N} 45 \mathrm{BA}-457 \mathrm{~A}-438 \mathrm{~A}, 2 \mathrm{~N} 511 \mathrm{~A}$ \& $\mathrm{B} .2 \mathrm{C} 220-$ 222, ETC.
gPECIFICATION
VCBO 80 V VCEO 50 V IC 10A PT. 30 WATTS Hfe 30-170.
PRICE

$$
\begin{array}{ccc}
1-24 & 2 j-99 & 100 \mathrm{up} \\
43 \mathrm{p} \text { each } & 40 \mathrm{p} \text { each } & 36 \mathrm{p} \text { each }
\end{array}
$$

## GENERAL PURPOSE SILICON NPN

 POWER TRANSISTORSCoded GP300, BRAND NEW TO-3 CASE. POB8IBLE REPLACEMENT FOR:-2N3055, BDY20, BDY11 BPECIFICATION
VCBO 100 V , VCEO 60Y, IC 15AMPS. PT. 115 WATTR Hie 20-100. FTI MHZ
PRICE $\underset{\text { B6p each }}{1-24}$
50-99
100 up

## GENERAL PURPOSE NPN SILICON SWITCRMG TRANS.

 GEYR B8Y27/98/95A. All usable devices no open or short circuits. ALAO AVAILABLE in PNP Sini. to 2 N 2906 , BCY 70 . When ordering please state preference NPN or PNP$$
\begin{array}{cccccc} 
& & \text { lp } & 100 & \text { For } & 1.75 \\
20 & \text { For } & 0.50 & 500 & \text { For } & 7.50 \\
50 & \text { For } & 1.00 & 1000 & \text { For } & 18.00 \\
\hline
\end{array}
$$

## COMPONENT PAKS <br> ENT

## MIXED

 ELECTRONIC COMPONENTSExceptionally good value (no rubbish)
Resistors, capacitors, pots, electrolytles and colls plus many other useful ltems. Approxi mately 3lbs in weight

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Plus our satisfaction or
money back gharantee.

| SILICON PHOTO TRAN- | BTL MICROLOGIC CRRCUIT8 |
| :---: | :---: |
| gIstor. To-18 Lens end. | Price et |
| NPN Sim. to BP $\times 25$ and P21. | Epozy T0-5 case 1-24 20-99 100 up |
| BRAND NEW. Fuil data | uL900 Bufer 35p 88p |
| avallable. Fully guarariteed. | gate Dual 2i/p 35p 28p 27p |
|  | uL923 J-K flp-flop 50p 470 46p |
| Qts. $\quad 1-2425-99100 \mathrm{up}$ | Data and Circuits Booklet for I.C's |
| Price each 45p 40p 35p | Price 7p. | -

Q1 20 Red spot trans. PNP AF
Q2 16 White spot R.F. trans. PN P
4 OC77 type trans. 4 Matched trans. OC44/4デ/81/8iD
4 Matched trans.
0 C 75 transiatore
4 AC128 trans. PNP high gain
4 AC126 trans. PNP
oc81 type trans.
2 ACl27/128 comp. pairs PNP/NPN
3 AF116 type trans.
3 AF117 type trans.
3 OC171 H.F. type trans.
5 2N2926 sil. epoxy trang. .....
2 GET880 low notse gerni. trans
2 GET880 low notse gerni.
3 NPN 1 ST141 \& 2 GT140
4 Madt's 2 MAT 100 \& 2 M 4 Madt's 2 MAT 100 \& 2 MAT 120
3 Madt's 2 MAT 101 \& 1 MAT 121 4 OC44 germ. trans. A.F.
$3 \mathrm{AC127} \mathrm{NPN}$ germ. trans.
20 NKT trans. A.F. R.F. coded 10 OA202 sil, diodes sub-nin. 8 OA81 dlodes
6 IN914 sil. diodes 75 PIV 75 mA 8 OA95 germ. diodes sub-min. IN69 10A B00PIV sil. rects. I845R Sil. pouer rects. BYZ13 $1 \times 2 N 698$ Sil. switec trans. 2 N706 NPN Q31 6 sil. switch trans. 2N708 NPN Q3. 3 PNP sil. trans. $2 \times 2 \mathrm{~N} 1131$ 3 gil. NPN trans. 2 N 1711 7 Sil. NPN trans. 2N2369, 200 MHZ Q35 $\quad 3$ §II. PNP TO-5 $2 \times 2 \mathrm{~N} 2904$ Q36 7 2N 3646 TO-18 plastic 300 ME 2 Q37 3 NPN 20053 NPN sil. trans. 7 PNP trans. $4 \times 2$ N $3703,3 \times 2$ N3702 7 NPN trans. $4 \times 2 \mathrm{~N} 3704,3 \times 2 \mathrm{~N} 3705$ 7 NPN amp. $4 \times 2 N 3707,3 \times 3 N 3708$. 3 Plastle NPN TO-18 2N 3904 6 NPN trans. 2N515:
7 BC107 NPN trans. $10.3 \times 1 \mathrm{CCl} 109$ 3 BC113 NPN TO-18 trans.
3 BC115 NPN TO. 5 trans.
6 NPN high gain $3 \times$ BC167. $3 \times$ BCl 68 4 BCY70 NPN trans. TO-18 4 NPN trans. $2 \times$ BFY51, $2 \times$ 7 BSY 95 A N PN trans. 300 MH 2

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| $0 \mathrm{CO}^{2}$ | 80p | OC29 | 40p |
| $0 \mathrm{C2} 2$ | 80 p | 0035 | 88 p |
| OC23 | 33p | OC36 | 40 p |
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| OC26 | 250 | AD142 | 40 p |
| OCus | 400 | AD149 | 48D |

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$\begin{array}{llll}\text { T80 } 14 \text { pintype } & 30 p & 27 p & 25 p \\ \text { T80 } 16 \text { pintype } & 85 p & 32 p & 30 p\end{array}$

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74 series T.T.L. I.C's

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$\mathrm{BP91}=7401$ BP92 $=7492$ BP92 $=7492$ BP94 $=7494$ $\mathrm{BP94}=7494$
$\mathrm{BP95}=7495$
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$\mathrm{BPIO5}=7410$;
BP107 $=74107$ BP110 = 74110 $8 P 111=74111$ BP118 = 74118 BP119 = 74119 BP121 $=74121$
BP141 BP141 $=74141$ BP150 $=74150$ BP151 $=74150$ BP151
BP153
$=74153$
7415 BP154 = 74104 BP155 = 74150 BP15 $6=74156$ BP160 $=74160$ BP161 $=74161$ BP190 $=74190$ BP191 $=74191$
$\mathrm{BP192}=7419 \mathrm{y}$ BP193 $=74193$

| BP196 |  |
| ---: | :--- |
| BP197 | $=74196$ |
| 107 |  | BP197 $=74197$ BP198 $=\mathbf{7 4 1 9 8}$ BP199 $=7419$

Quad 2 -input NAND ga
Quad 2 -input pos. (with opent pas. NAND gate auad 2 -input plector output) quad +i-input pos. NAND gates (with open collector output) Hex Invertera
Hex Inverter (with open-collector Triple 3-itu
Triple 3-input pos. NAND gate
Dual 4-input pos. NAND gates
8 -input pos. NAND gates
Dual 4 -input pos. NAND huffera
BCD to decimal nixie driver
BCD to decimal tecoder ( $4-10$ linea. 1 of 10 )
BCD-to-seven-segment decoder/driver BCD-seven-segment decoter/driver (15V outputs)
BCD-to-seven-segment decoder/driver
Expandable dual ipandable dual "-input and-orIMal 2-win
gatea 2 -input and-or-incert quad o-input expandable and-or -wide 2 -input and-or-invert gates Dual 4 -input expander Single-phase J-K flp-flop and Mave J-K fip-Hop nal Master Jla Quad latch
Dual J-K with pre-set and clear lated full addera
6-bit read/write menory
bit binary full adders Quad full adder
Quad 2-Input excluasic NOR gaten BCD decade counter
Divide-by-twelve counter 4-bit binary counters
Dual entry 4 -hit shift register 4-bit up-down ahilt register -bit parallel in parallel out thiftregister
-bit bistable latchen
single J-K tlip-flop equivalent 9000 series
ingle $J$-K fip floy equivalent 900 I Dual Ma
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sync. up-down decade counter dock lines) up-down counter (tow clock mes) Pre-setable 50 MHz binary counter -bit parallel L-R shift register 8-bit parallel access shift register

Price and aty. price: $\begin{array}{ll}1-24 & 25-99 \\ 100\end{array}$ $\begin{array}{lll}\text { sp } & \text { ip } & \text { Ip } \\ 0.15 & 0.14 & 0.18\end{array}$ $\begin{array}{lll}0.16 & 0.14 & 0.12 \\ 0.15 & 0.14 & 0.12\end{array}$

| 0.15 | 0.14 | 0.12 |
| :--- | :--- | :--- |

$0.16 \quad 0.14$
0.18
0.18
0

## $0.89 \quad 0.28$

$\begin{array}{ll}15 & 0.14\end{array}$

$$
\begin{array}{lll}
0.15 & 0.14 & 0.12 \\
0.67 & 0.64 & 0.58
\end{array}
$$


$\begin{array}{ll}0.97 & 0.94\end{array}$


$$
\begin{array}{lll}
0.16 & 0.14 & 0.18
\end{array}
$$

$\begin{array}{ccc}0.18 & 0.14 & 0.12 \\ 0.15 & 0.14 & 0.12\end{array}$
$\begin{array}{lll}0.15 & 0.14 & 0.12 \\ 0.89 & 0.28 & 0.24 \\ 0.89 & 0.28 & 0.94\end{array}$
$\begin{array}{lll}0.29 & 0.28 & 0.24 \\ 0.87 & 0.35 & 0.82 \\ 0.37 & 0.85 & 0.89\end{array}$
$\begin{array}{lll}0.47 & 0.48 & 0.48 \\ 0.43 & 0.40 & 0.38 \\ 0.07 & 0.48\end{array}$
$\begin{array}{lll}0.87 & 0.84 & 0.88 \\ 0.87 & 0.94 & 0.88 \\ 0.97 & 0.94 & 0.88\end{array}$
$\begin{array}{lll}1.10 & 1.05 & 0.88 \\ 0.32 & 0.30 & 0.86\end{array}$
$\begin{array}{lll}0.32 & 0.30 & 0.88 \\ 0.67 & 0.64 & 0.58 \\ 0.87 & 0.84 & 0.88\end{array}$

$\begin{array}{lll}0.87 & 0.84 & 0.58 \\ 0.67 & 0.64 & 0.88 \\ 0.67 & 0.64 & 0.68\end{array}$ | 0.58 |
| :--- |
| 0.58 |
| 0.88 |

$\begin{array}{lll}0.77 & 0.74 & 0.68 \\ 0.77 & 0.74 & 0.68\end{array}$
$\begin{array}{lll}0.77 & 0.74 & 0.88 \\ 1.76 & 1.65 & 1.65\end{array}$
$\begin{array}{lll}0.97 & 9.94 & 0.88\end{array}$
$\begin{array}{lll}0.97 & 0.94 & 0.88 \\ 0.40 & 0.38 & 0.86 \\ 0.56 & 0.69 & 0.50\end{array}$
$\begin{array}{lll}0.55 & 0.68 & 0.50 \\ 1.25 & 1.15 & 1.00 \\ 1.00 & 0.85 & 0.80\end{array}$
$\begin{array}{lll}1.00 & 0.85 & 0.80 \\ 1.35 & 1.25 & 1.10 \\ 0.67 & 0.64 & 0.58 \\ 0.87 & 0.64 & 0.58\end{array}$
$\begin{array}{lll}0.87 & 0.64 & 0.58 \\ 1.60 & 1.40 & 0.58 \\ & 1.30\end{array}$
$\begin{array}{lll}1.60 & 1.40 & 1.30 \\ 1.60 & 1.70 & 1.60\end{array}$
$\begin{array}{lll}1.00 & 1.70 & 1.60 \\ 1.80 & 0.96 & 0.90 \\ 1.80 & 1.70 & 0.95\end{array}$
$\begin{array}{lll}1.80 & 1.70 & 1.80 \\ 1.40 & 1.30 & 1.80\end{array}$
0.80
1.80
1.20
1.20
$\begin{array}{lll}1.40 & 1.80 & 1.80 \\ 1.80 & 1.70 & 1.60 \\ 1.80 & 1.70 & 1.80 \\ 8.50 & 3.25 & 3.60\end{array}$
$\begin{array}{lll}3-50 \\ 2.10 & 8.25 & 8.00\end{array}$
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| $10.0 \mu \mathrm{~F}$ | 1.5 volts | 2.7 HF | 50 | volts | 12 | $\mu F$ | 35 | volts |
|  |  | $3 \mu \mathrm{~F}$ | 12 | volts. | 12 | $\mu F$ | 50 | volts |
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$2 \times$ Duo Type II speakers $£ 14+£ 2$ P.\&P. Garrard SP25 Mk. III with MAG. cartridge, plinth and cover


SYSTEM 2
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$2 \times$ Duo Type II speakers $£ 14+£ 2$ P.\&P.
Garrard SP25 Mk. III with CER. diamond cartridge, plinth and cover $\quad £ 21+£ 1.50$ P.\&P.

Total $£ 52$
Avallable complete for only $£ 49+£ 3.50$
P.\&P.

SPEAKERS Duo Type II
Size approx. 17in $\times 10 \frac{3}{4} \mathrm{in} \times 6 \frac{3}{4} \mathrm{in}$. Drive unit 13 in $\times 8$ in with parasitic tweeter. Max. power 10W, 3 ohms. Simulated Teak cabinet. £14 pair + £2 P. \& P. Duo Type III Size approx. $23 \frac{1}{2}$ in $\times 11 \frac{1}{2}$ in $\times 9 \frac{1}{2}$ in. Drive unit $13 \frac{1}{2}$ in $\times 8 \frac{1}{4}$ in with H.F. speaker. Max. power 20 W at 3 ohms. Frequency range 20 Hz to 20 kHz . Teak veneer cabinet. $£ 32$ pair $+£ 3 P . \& P$.

## SPECIFICATION R100/101

14 watts per channel into 3 to 4 ohms. Total distartion@10W@ $@ \mathrm{kHz} 0.1 \%$. P.U.1 (for ceramic cartridges) 150 mV into 3 Meg. P.U. 2 (for magnetic cartridges) 4 mV @ 1 kHz into 47 K equalised within $\pm 1 \mathrm{~dB}$ R.I.A.A. Radio 150 mV into 220K. (Sensitivities given at full power.) Tape out facilities; headphone socket, power out 250 mW per channel. Tone controls and filter characteristics. Bass: +12 dB to $-17 \mathrm{~dB} @ 60 \mathrm{~Hz}$. Bass filter: 6 dB per octave cut. Treble control: treble +12 dB to -12 dB @ 15 kHz . Treble filter: 12 dB per octave. Signal to noise ratio: (all controls at max.) R101-P.U.1. and radio65 dB . P.U.2-58dB. R100 same as R101 but P.U. 2 (for crystal cartridges) 450 mV into 3 Meg. Cross talk better than -35dB on all inputs. Overload characteristics better than 26 dB on all inputs. Size approx. $13 \frac{\mathrm{z}}{2} \times 9 \mathrm{in} \times 3 \mathrm{i} \mathrm{in}$.

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| 1RS | ．28 | 30 Cl | ． 28 | DY87 | 2.5 | EL500 | ． 81 | PcL82 | ． 38 | BC80 | 32 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 185 | ． 22 | 30 C 15 | －58 | D 8802 | ． 35 | EM80 | 41 | YCL83 | ． 58 | TAF42 | ． 61 |
| 1T4 | －16 | 30 Cl 17 | ． 78 | EABC80 | ． 32 | E381 | 41 | PCL8 | ． 34 | － $\mathrm{CL}^{1} 1$ | 58 |
| 38. | － 28 | 30018 | ． 61 | EAF42 | ． 50 | EM84 | ． 32 | PCL85 | ． 40 | CBr＇80 | ． 34 |
| $3 \vee 4$ | .37 | 30 Fs | ． 70 | EB41 | ． 40 | EM87 | ． 36 | ${ }^{\text {P}} \mathrm{CL}^{\text {c }} 86$ | 40 | U1．F89 | ． 82 |
| ¢U4G | ． 26 | 30FLL 1 | ． 61 | EB91 | ． 11 | とうご | 38 | PCL88 | ． 85 | CCC84 | .33 |
| 5 V 4 G | ． 35 | $30 \mathrm{HLL2}$ | ． 70 | Efl 33 | 40 | EY86 | ． 49 | PCL800 | ． 75 | ［CCPs | ． 85 |
| SY3GT | ． 28 | 30 FLI 4 | －68 | $\mathrm{FBC4}$ | ． 54 | EZ40 | 43 | PENA4 | ． 77 | ［＇CF80 | 33 |
| 52.46 | ． 35 | 30 LJ | ． 29 | EBC90 | ． 22 | EZ41 | 43 | PEN36C | C 70 | ＇Cll 42 | －62 |
| 6／30L？ | ． 58 | 30 L 15 | － 59 | EBFRO | ． 32 | EZ80 | ． 22 | PFL， 200 | ． 58 | UCH81 | ． 32 |
| 6．aL5 | ． 11 | $30 \mathrm{LI} \%$ | ． 71 | ERF89 | ． 28 | E281 | .23 | PL36 | ． 48 | ${ }^{\text {CTL }} 82$ | ． 34 |
| 6.4 M 6 | ． 13 | 30P4 | ． 65 | 3CC81 | ． 17 | （：Z30 | $\cdot 35$ | PL81 | － 45 | UCL83 | ． 65 |
| $6.4 Q 5$ | － 22 | 30 P 12 | ． 72 | ECC83 | ． 20 | CZ32 | 40 | PL81A | ． 48 | UF41 | ． 86 |
| 6 ATt | ． 20 | 30P19 | ． 65 | ECC8．3 | ． 35 | 923． | ． 48 | PL8：2 | －31 | U F89 | － 30 |
| 6av6 | －20 | 30 PL 1 | $\cdot 63$ | ECC85 | ． 28 | KT41 | ． 77 | PL83 | .33 | ［1L4］ | ． 57 |
| 68AG | － 20 | 30 PL 13 | ． 75 | EC＇C904 | ． 56 | KT61 | ． 55 | P＇L84 | $\cdot 30$ | ${ }^{1} \mathrm{~L}$ L4 | 11.00 |
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| 6 BJ 6 | ． 41 | $301 \cdot 15$ | ． 80 | ECP82 | ． 28 | L N 319 | ． 63 | PL504 | －64 | UM84 | 28 |
| ${ }^{15} \mathrm{BW} 7$ | ． 52 | 35L6GT | ． 45 | E（1H3） | ． 30 | IN 329 | ． 72 | PM84 | .35 | （－14） | 42 |
| 6CD6C 2 | 11.07 | 35 W 4 | ． 25 | EC＇H42 | ． 81 | IN 339 | ． 83 | PX25 | 81.00 | ǓY85 | ． 28 |
| 6 Fl 4 | ． 42 | 35 ZsGT | ． 25 | $\mathrm{BC}^{\text {ch81 }}$ | ． 29 | Ni78 | ． 87 | PY 32 | 65 | VP4B | 77 |
| $6 \mathrm{fr}^{2} 23$ | －68 | 807 | ． 45 | ECHB3 | ． 40 | P61 | ． 48 | PY33 | ． 55 | 777 | ． 22 |
| $4{ }^{6} 25$ | ． 57 | $60+3$ | ． 62 | ECH84 | ． 36 | PABC80 | ． 34 | PY81 | ． 27 | Transt | rs |
| 6K：C | ． 12 | $\mathrm{AC/VP2}^{\text {c }}$ | ． 77 | ECL 80 | ． 30 | PC86 | ． 47 | P 882 | ． 25 | AC107 | $\cdot 17$ |
| 6 K 8 G | $\cdot 17$ | B349 | ． 65 | ECL8＊ | ． 31 | PC88 | ． 47 | PY83 | ． 28 | AC127 | 18 |
| BQ7G | 27 | 13729 | ． 62 | ECL86 | ． 36 | ${ }^{\text {PC96 }}$ | 42 | PY88 | ． 33 | AD146 | 87 |
| 68N70T | ． 30 | CCH35 | －67 | EP39 | ． 38 | PC97 | ． 38 | PY800 | $\cdot 34$ | AF115 | ． 20 |
| 6 6\％b： | ． 23 | C「31 | ． 30 | EF41 | ． 60 | PC900 | ． 38 | PY801 | ． 34 | AF118 | － 20 |
| 6ybut | ． 31 | DAF＇Yl | ． 22 | EF80 | ． 23 | 1＇CC84 | ． 29 | R19 | $\cdot 30$ | AF117 | －20 |
| $6 \mathrm{X4}$ | － 23 | DAF96 | ． 36 | EF＇85 | ． 28 | PCC85 | ． 27 | R20 | ． 58 | AF118 | ． 48 |
| 6x50\％ | ． 28 | DF33 | ． 38 | E188 | ． 81 | PCC88 | －42 | U25 | ． 66 | AF125 | ． 17 |
| 7 BT | － 33 | D +91 | ． 16 | EF89 | ． 28 | PCC89 | ． 48 | ［126 | ． 58 | AF127 | ． 17 |
| 101913 | .58 | 1）＋96 | .36 | EF91 | ． 13 | PCC189 | ． 48 | U47 | ． 85 | OC26 | ． 25 |
| $12.4 T 7$ | $\cdot 17$ | $19 \mathrm{H77}$ | 20 | Et99 | ． 65 | PCC805 | ． 58 | U49 | ． 58 | $0 \mathrm{OC4} 4$ | $\cdot 12$ |
| 124156 | ． 20 | Dh32 | ． 33 | Eド183 | ． 28 | PCF80 | ． 28 | 1350 | ． 28 | OC45 | ． 12 |
| $12 \mathrm{AU7}$ | ． 20 | DK91 | ． 28 | EF184 | .31 | PCP82 | ． 31 | U52 | .31 | $0 \mathrm{C7} 1$ | ． 12 |
| $1 \because 1 \times 7$ | $\cdot 22$ | DK93 | －38 | EH90 | $\cdot 37$ | PCF8 ${ }^{\text {a }}$ | ． 45 | 178 | ． 24 | OC\％ 2 | ． 12 |
| $19 \mathrm{BLi6}$ C | ． 87 | DK¢6 | ． 38 | ELis3 | .55 | PCP800 | ． 48 | －191 | ． 59 | OC75 | ． 12 |
| \％6F\％ | ． 67 | DL35 | ． 40 | EL／34 | .45 | PCF801 | ． 30 | ［1193 | ． 42 | OC81 | ． 12 |
| 2013 | ． 80 | DLay | ． 28 | EL4 1 | ． 54 | PCF80\％ | ． 44 | प1251 | ． 88 | OC81 ${ }^{\text {d }}$ | ． 12 |
| 2014 | ． 92 | DL94 | .87 | E1．84 | ． 23 | PCF805 | ． 61 | U301 | ． 38 | OC8 2 | $\cdot 12$ |
| $2{ }^{5} \mathrm{~L} 6 \mathrm{GT}$ | ． 20 | D1．96 | ． 38 | EL40 | ． 26 | PCF80＇ | ． 58 | U329 | ． 86 | OC82D | ． 12 |
| 25 C 4 FT | － 67 | DY80 | ． 25 | EL95 | ． 33 | PCF808 | 68 | U801 | ． 88 | OC170 | ． 22 |

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|  | 0.05 | ${ }^{263301}$ | 0.13 | with PL 509 and PY500 ralves. As removed fromcolour receivers at |  |  |  |
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| ${ }^{\text {BSY }}$ 85 | 0.57 | ${ }^{\circ} \mathrm{C} 23$ | 0.50 0.30 | OC7l ork 72 Fully rested |  |  |  |
| ${ }^{\text {BSY26 }}$ | -0.13 | OC25 | 0.25 0.25 |  |  |  |  |
| BSY28 | 0.13 | ${ }^{\circ} \mathrm{C} 26$ | 0.25 |  | 25 | 20 | 15 |
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| - 8 BY95 | - 0.15 | OC36 | ${ }_{0.37}$ |  | 15 | 12 | 10 |
| $\mathrm{OC}_{4}$ | 0.13 | ${ }^{\text {ADI }} 149$ | 0.30 |  | 3 | 3 | 2 |
| $00^{0} 4$ | 0.13 | ${ }_{25034}$ | 1.25 0.25 | ${ }^{1}$ Watt Zener Diodes 75 | s |  |  |
| ${ }^{\circ} \mathrm{C} 71$ | ${ }_{0}^{0.13}$ | 2N3055 | 0.63 | 10 Watt Żener Diodes 51 |  |  |  |
| $\bigcirc \mathrm{OCl}^{\text {C }}$ | 0.17 | Diodes |  | Micro Switches, S/P, C/O |  |  |  |
| OC810 | 0.13 0.13 | AAY42 | 0.10 |  | 20 | 17 | 15 15 |
| ${ }^{\circ} \mathrm{C}$ C3 | 0.30 | OA79 | 0.10 0.09 | ${ }^{\text {a }}$ Amp. Bridge Rect. 25v. ${ }^{\text {a }}$ |  | 22 | 20 |
| - ${ }^{\circ} \mathrm{Cl139}$ | 0.13 0.17 | OAB14 | 0.09 0.07 |  |  |  |  |
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| W |  | MARKED UNTESTED | PAKS |
| :---: | :---: | :---: | :---: |
| B66 | 150 | Germanium Diodes Min. glass type | 50p |
| 883 | 200 | Trans. manufacturers' rejects all types NPN, PNP, Sit. and Germ. | 50p |
| 384 | 100 | Silicon Diodes DO-7 glass equiv. to OA200, OA202 | 50p |
| B86 | 50 | Sil. Diodes sub. min. IN914 and IN916 types | $50 p$ |
| B88 | 50 | Sil. Trans, NPN, PNP, equir to OC200/1. 2N706A, B5Y95A, etc. | $50 p$ |
| B60 | 10 | 7 Watt Zener Diodes Mixed Voltages | 50p |
| H6 | 40 | 250 mW . Zener Diodes DO-7 Min. Glass Type | 50p |
| H10 | 25 | Mixed volts, $1 \frac{1}{2}$ watt Zeners. Top hat type | 50p |
| HII | 30 | MAT Series " alloy "pnp Transistors | $50 p$ |
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| :---: | :---: | :---: | :---: |
| B2 | 4 |  | 50p |
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| म9 | 2 | Ocp7l Light Sensitive | 50p |
| H12 | 50 | NKTIS5.259 Ger.m. diodes. | 50p |
| H/8 | 10 | OC7I/75 uncoded black glass type PNP Germ. | 50p |
| H19 | 10 | - ${ }^{\text {OCB } / 1 / 810 ~ u n c o d e d ~ w h i t e ~}$ | 50p |
|  | 20 |  | 50p |
| H29 | 20 |  | 50p |

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Prim. 200/240V a.c. OMT4/1. One tapped sec, 5-20-30-$40-60 \mathrm{~V}$ giving $5-10-15-20-25-30-40-45-65-60,10-0-$ $10,20-0-20 ; 30-0-30 \mathrm{~V}$ a.c., 1A, 82.25 ; OMT4/2 ditto, 2A. 85 . 5 ; OMT5/1 one tapped sec, $40-50-60-80-90-$ $100-110 \mathrm{~V}$ a.c., 1A, $88 \cdot 45$. Duo 12 V 4A-12V 4A $28 \cdot 60$;
Duo $0-10-20-25 \mathrm{~V} \cdot 2 \mathrm{~A}-0-10-20-25 \mathrm{~V}$ LOW VOLTAGE TRANSFORMERS
Prim. 200/240V a.c., $6 \cdot 3 \mathrm{~V}, 1-5 \mathrm{~A}, 85 \mathrm{p}$; 3A, $2 \mathrm{~A} \cdot 18$; 6 A CT, 21-80; $12 \mathrm{~V}, 1 \cdot 5 \mathrm{~A}, 21 \cdot 18 ; 3 \mathrm{~A}$ CT, $21 \cdot 80 ; 6 \mathrm{~A}$ CT, 28.70 ; $18 \mathrm{~V}, 1.5 \mathrm{~A}$ CT, 21.80 ; $94 \mathrm{~V}, 1.5 \mathrm{~A}$ (T, 21.80 ; 3 A CT 52.70; 5A, $88.75 ; 8 \mathrm{~A}, 26 ; 12 \mathrm{~A}, 19 ; 40 \mathrm{~V}, 3 \mathrm{~A}$ CT, 83.45 . WDDGET RECTIFIER TRANEFORMERS
For FW rect., size $11 \times 2 \times 1 / \mathrm{in}$, Prim. $200 / 240 \mathrm{~V}$ a.c. output, PPT1 9-0-9V, 0.3A, PPT2 12-0-12V, 0.25A, PPT3 20-0-20V, 0.15A, $21 \cdot 20$ each; ditto, aize $2 \times 2 t$ $\times 1$ in MTV1 9-0-9V, 1A, 98p; MTV2 12-0-12V. IA, MTV3 20-0-20V, $0.75 \mathrm{~A}, 51.80$ each.
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(KT66, etc.), $84.05 ; 60 \mathrm{~W}, 3 \mathrm{k} \Omega$, A-A 28.75 : 100 W 3t $\Omega, A-A$, EL 34 (KT88, etc.) $211 \cdot 40$ with and to 400 W . LOUDSPEAKERS, EI-EI, P.A., GUITAR, ETC. New boxed famous make, 25 W , $46 \cdot 60$; 35 W a 7.20 $50 \mathrm{~W}, 20.45 ; 100 \mathrm{~W}, 110.00$ : E.M.I. $131 \times 81 \mathrm{n}$, 10 W , 3, 8 and 15 ohms, 2.25 ; fitted two tweeter Hi-Fi, 3 , 8 and 15 ohms, $84 ; 3^{\wedge}, 3$ ohms: $31{ }^{n}, 3$ or 15 ohms: $5^{\prime \prime} 3^{3}, 15$ or 25 ohms $90 \mathrm{p} .7^{*} \times 4^{\prime \prime}, 3$ ohms, $21 \cdot 10$.
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ideal for dark room light or for plastic case 80 peach． 3 heat model 400
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Three position switching to sult changes in the weather Bwitch up for full heater（2p \(\mathbf{k}\) W），switch down for half heat（1 \(\mathrm{k} W\) ），switch central
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\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline No．of & \(\underline{2}\) & 3 & 4 & \％ & 6 & 8 & 9 & 10 & 12 \\
\hline Poler & way & way & way & way & way & way & way & way & way \\
\hline 1 pole & 40 p & 100 & 400 & 400 & 400 & 40 D & 407 & 400 & 40 p \\
\hline 2 poles & 40 p & 40 p & 40 D & 400 & 400 & 400 & 40D & 70 D & 700 \\
\hline 3 poles & 40p & 40p & 40 p & 400 & 700 & 70 p & 70 p & 95\％ & 95p． \\
\hline 4 poles & 400 & 40p & 400 & 700 & 709 & 709 & 70 p & 21.80 & 21．20 \\
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\hline 7 poles & 70 p & 700 & 700 & 95 p & 81．20 & 21.20 & \＄1．20 & 21.95 & \＄1．95 \\
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\hline 9 poles & 70 p & 70 p & 95p & 95p & 81.45 & 21.45 & \＄1．45 & 22.45 & 88.45 \\
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\section*{HIGH ACCURACY THERMOSTAT} Uses differential comparator I．C．with thermister a probe．Designer claims tempersture control to power pack es－50．

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VOL. 7 No. 11 \\ November
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RETROSPECT AND PROSPECT

SEVEN years is a long time in electronics . . . Practical Electronics first appeared on the scene in mid October 1964. The very next day (!) Sir Alec Douglas-Home conceded victory to Mr. Harold Wilson. Shortly afterwards the Ministry of Technology was set up, intended by the incoming administration to be the symbol of a new technological era, and the British electronics industry received assurances of determined government backing in their battle with foreign competitors. At this time, valve manufacturers continued to face the future stoically despite the formidable progress of the transistor, but P.E. put its money on solid state from the word go.

Seven years on . . . the thermionic valve has all but conceded victory to the semi-conductor, and prepares to make its final stand in the high power region. On the other hand the transistor, after enjoying a few delightfully expansive years of near total sovereignity. is itself alerted to a serious threat from nearer home as that more recent offspring of solid state technology, the IC, makes its bid to take over the strategic small signal areas from its discrete brethen.

In the meanwhile . . . the government has changed once again and MinTech, child of that now demised white-hot technological revolution, is demolished and replaced by the no-nonsense, businesslike-if prosaic sounding-Department of Trade and Industry. Our semiconductor manufacturers, now "freed" after several years of cossetting at the taxpayers expense, bravely face the cold, hard outside world-as true exponents of private enterprise should-without a murmur (save perhaps, just a little one).

On the home constructor front developments proceed apace. It's an ill wind . . . IC manufacturers pour many thousands of their excess production onto the amateur market. Private designers and constructors get bigger ideas as the devices get smaller. Miniaturisation and yet expansion seems the order of the day.

Today . . . the outlook is, indeed, promising. Yet how does one magazine such as ours cope with the inordinate demands arising from the increasing popularity of amateur electronics as a hobby? For, considering the various types of individuals already involved, or likely to become so any moment now, it is obvious that technical knowledge, practical skills, and areas of special interest and involvement range enormously.
continued on page 938

\section*{CONSTRUCTIONAL PROIECTS}

RHYTHMETRON 890
WAR GAMES COMPUTER 902
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Our December issue will be published on
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Many circuits for simple electronic metronomes have been published but almost all of these have employed a multivibrator with one output coupled directly to a small high resistance loudspeaker. The resultant sound is a click, usually not very loud and bearing little resemblance to the more resonant beat produced by a mechanical metronome.

Unless an amplifier is included the loudness from a multivibrator and loudspeaker is not normally sufficient to make itself clearly audible above modern amplified musical instruments like the electronic organ or indeed above the sound produced by a small orchestra or choir.

The signal output from the generator described in this article is more than sufficient to drive almost any amplifier but as the sound it produces has no bass content quite a loud sound will be obtained even with a \(3 W\) amplifier and relatively small speaker, certainly sufficient for practice with a domestic electronic organ or piano and probably enough for school music classes.

\section*{DRUM BRUSH RHYTHM}

In addition to beat notes the generator will produce a steady drum brush effect with variable attack and decay so it also becomes a very simple rhythm unit. The tempo is continuously variable over the usual music range of about 40 to 250 beats per minute and to assist constructors a cut-out calibration scale is included with beats per minute marks and approximate settings for tempo variations between largo (very slow) and presto (very fast).

The generator does not produce accented beats is this requires complex counting circuitry but as the beats are steady it is quite easy to play against them in three-four, two-four or four-four time, or multiples, depending on the setting of the tempo control. As the drum brush attack and decay can be controlled, the "voicing" can be set to produce a fast attack and short decay for fast tempi and soft attack and slow decaly for slow tempi such as the slow waltz.


\section*{THE CIRCUIT}

The generator can be operated from batteries or a small mains power supply. It consumes only 2 mA so it would run economically from two 9 V batteries in series. The circuit given in Fig. 1 shows the complete generator with a battery supply. An alternative mains operated power unit is given in Fig. 2.

The first stage consists of a multivibrator. TR 1 and TR2 are pnp transistors with emitters connected to the +18 V rail. The tempo is controlled by VR1.

The output from TR2 collector provides a positive going pulse which is coupled via C4 to the "beat" voicer TR3. This transistor is an npn type and is connected as a phase shift oscillator biased to cut-off. The positive pulse from C4 instantly drives TR3 on but the short time constant provided by C4/R5 allows the pulse voltage to decay quickly. The output from TR3 is, therefore, a short but gradually decaying burst of oscillation of about \(1,500 \mathrm{~Hz}\). The sound is a resonant tapping not unlike that of a clave and closely resembling the sound of a mechanical metronome.

\section*{THE DRUM BRUSH VOICER}

The output from TR2 is also fed to R15 and the diode D2 which together with the attack/decay network VR2, R16, C11, C12 and VR3 provides a positive pulse with variable rise and decay time. This pulse, from C11, drives the drum brush amplifier TR4.

The white noise for the drum brush voicing is obtained from the special Zener diode D1. It must be emphasised that any "noisy" Zener may fail to produce the required amount of white noise which must be at least 50 to 100 mV r.m.s. in level. The ZIJ Zener diode specified will produce in excess of 100 mV of noise and can be obtained from Semitron Limited, Cricklade, Wiltshire, price 40 p including packing and postage.

The outputs from the beat voicer (TR3) and the drum brush voicer (TR4) are taken to S1 which enables selection of either voice. The "mute" switch

S3 is optional but it is a worthwhile addition as it will enable the user to leave the generator running but stop and start the signals as required.

\section*{THE POWER SUPPLY}

The alternative mains power supply of Fig. 2 requires a transformer with a secondary delivering between 12 and 18 V . The current consumption required by the generator is small but the line voltage must be adjusted on load to 18 V , hence the resistor R23 in the power supply may need to be larger depending on the transformer secondary voltage. If the transformer specified is used it can be mounted on a piece of Veroboard together with the rectifier and the reservoir capacitor C16 and R23 omitted as shown in Fig. 3. If two 9 V batteries are used they can be retained within the generator case by suitable clips.

\section*{CONSTRUCTION}

In the prototype the generator was constructed on two boards as shown in Figs. 4 and 5. Board I




Fig. I. Circuit diagram of the Rhythmetron

Resistors
\begin{tabular}{llllll} 
Res & & \\
RI & \(12 \mathrm{k} \Omega\) & R9 & \(22 \mathrm{k} \Omega\) & R 17 & \(10 \mathrm{k} \Omega\) \\
R2 & \(120 \mathrm{k} \Omega\) & R10 & \(15 \mathrm{k} \Omega\) & R18 & \(100 \mathrm{k} \Omega\) \\
R3 & \(27 \mathrm{k} \Omega\) & R11 & \(2.2 \mathrm{k} \Omega\) & R19 & \(2.2 \mathrm{k} \Omega\) \\
R4 & \(12 \mathrm{k} \Omega\) & R12 & \(68 \mathrm{k} \Omega\) & R20 & \(10 \mathrm{k} \Omega\) \\
R5 & \(150 \mathrm{k} \Omega\) & R13 & \(100 \mathrm{k} \Omega\) & R21 & \(150 \mathrm{k} \Omega\) \\
R6 & \(390 \mathrm{k} \Omega\) & R14 & \(68 \mathrm{k} \Omega\) & R22 & \(68 \mathrm{k} \Omega\) \\
R7 & \(68 \mathrm{k} \Omega\) & R15 & \(1.2 \mathrm{M} \Omega\) & R23 & \(470 \Omega\) (see text) \\
R8 & \(22 \mathrm{k} \Omega\) & R16 & \(680 \Omega\) & & \\
All \(10 \% \frac{1}{2}\) watt carbon & &
\end{tabular}

Potentiometers

VRI IM \(\Omega\) log. carbon
VR2 lok \(\Omega\) linear carbon

VR3 500k \(\Omega\) linear carbon

Capacitors
\begin{tabular}{|c|c|c|c|}
\hline Cl & 1,000 F elect. 25 V & C9 & \(0.1 \mu \mathrm{~F}\) polyester \\
\hline C2 & \(2 \mu \mathrm{~F}\) elect. 15 V & Cl0 & \(0.02 \mu \mathrm{~F}\) polyester \\
\hline C3 & \(2 \mu \mathrm{~F}\) elect. 15 V & ClI & \(4 \mu \mathrm{~F}\) elect. 15 V \\
\hline C4 & \(0.1 \mu \mathrm{~F}\) polyester & Cl 2 & \(10 \mu \mathrm{~F}\) elect. 15 V \\
\hline C5 & 2,200 pF polystyrene & C13 & 6,800 pF polystyrene \\
\hline C6 & 2,200 pF polystyrene & Cl 4 & \(2.5 \mu \mathrm{~F}\) elect. 15 V \\
\hline C7 & 2,200 pF polystyrene & C15 & \(0.22 \mu \mathrm{~F}\) polyester \\
\hline C8 & 500 pF polystyrene & Cl 6 & 1,000 F elect. 25 V \\
\hline
\end{tabular}

C9 \(0.1 \mu \mathrm{~F}\) polyester
ClO \(0.02 \mu \mathrm{~F}\) polyester
CII \(4 \mu \mathrm{~F}\) elect. 15 V
\(\mathrm{Cl} 210 \mu \mathrm{~F}\) elect. 15 V
Cl3 6,800pF polystyrene
0.22 F ply

C16 1,000 \({ }^{\mathrm{F}}\) elect. 25 V

\section*{Transistors}

TR1, TR2 NKT214 or OC45 (2 off)
TR3, TR4 BCIO9 (2 off)

Diodes
DI ZIJ Zener (see text)
D2 OABI
D3-D6 Bridge rectifier LTII9

\section*{Switches}

SI S.P.D.T. slide switch
S2 Single pole on/off switch
S3 Single pole on/off (see text)

\section*{Miscellaneous}

TI-12-0-12V 50 mA Eagle transformer type MRI2 Universal chassis 8 in \(\times 6\) in \(\times 4 \mathrm{in}\). BYI-BY2 \(9 V\) batteries ( 2 off). JKI Standard jack socket.


Fig. 2. Circuit diagram of the mains power supply unit


Fig. 3. Component assembly and wiring details for power supply board


Fig. 4. Component assembly and wiring details for tempo generator and beat voicer circuits


Fig. 5 (right). Component assembly and wiring details for drum brush voicer circuit


Tempo generator and beat voicer board



Fig. 7. Tempo calibration scale which can be cut out and pasted on the front panel
carries the multivibrator and beat voicer (TR3) and Board 2 contains the white noise generator and drum brush voicer (TR4).

The prototype was built into a case approximately 8 in \(\times 6\) in \(\times 4 i n\). Board interwiring and the layout of the front panel components is given in Fig. 6.

Note that VR1, which is a \(\log\) potentiometer, is wired so that tempo increases with anti-clockwise rotation. This arrangement was found to provide a more linear calibration for the beats per minute scale. The scale is reproduced in Fig. 7 and can be cut out and used with the specified tempo potentiometer VR1.

\section*{OSCILLOGRAMS AND VOICE VARIATIONS}

To check the correct circuit functioning the oscillograms in Fig. 1 should be found by monitoring at the letter reference points. Of course, depending on the time base speed of the oscilloscope used, there may be some departure from these shapes.

Some adjustment can be made to the voicing. For example, the pitch of the metronome beat can be raised or lowered slightly by slightly changing the value of R 8 .

The drum brush voicing can be made sharper by omitting C13 and connecting a 200 pF mica capacitor between the collector and base of TR4. The variable controls VR2 and VR3 will provide a more than sufficient range of attack and decay requirements.

Ir is nearly 100 years since Bell demonstrated the first working telephone at Philadelphia. It was the culmination of many experiments with sound waves in search of a method by which deaf children might be taught to speak, and was the practical application of an idea by Charles G. Page in 1837 that electric current might carry sound.

The receiver used was a simple device enabling variations in electric current to produce magnetic attractions of related strength and frequency to a metal disc. The resulting piston-like vibrations of the disc modulated the air pressure between the disc and the ear of the person listening and produced intelligible sound, but it was necessary to place the earphone against the ear to hear the sounds clearly.

Further sound amplification was obtained by adding a megaphone-shaped horn to an appropriately modified earphone so that several people could hear the sound at the same time, and thus the earphone was turned into a loudspeaker. Alas, the sound it produced was far from a faithful reproduction of the original, and engineers were challenged with the task of improving the sound reproduced in order to satisfy the needs of the rapidly developing electric gramophone, talking pictures and wireless receiver.

\section*{MOVING COIL SPEAKERS}

The horn speaker was gradually replaced by a reed-driven cone speaker which could be mounted inside the same cabinet that would contain the radio receiver or gramophone. Still the quality left much to be desired and the moving iron type of drive unit was eventually superseded by the moving coil system very similar to that being used today.
In its early stages the magnetism of the moving coil speaker was provided by a large coil energised by the h.t. current of the receiver amplifier. This was necessary because at that time permanent magnet material was not very efficient and proved too expensive for the popular speakers.

Advances in both magnet steel and later the development of ferrite ceramics has resulted in the replacement of the energised magnet by the now total use of permanent magnets. These are applied in two basic ways, the screened magnet system Fig. 1 and the unscreened magnet system Fig. 2.

The screened magnet type of loudspeaker is particularly useful in transistor portables and similar equipment, where the loudspeaker is in close


Fig. I. Cutaway view of shielded magnet


Fig. 2. Cutaway view of unshielded ceramic magnet
proximity to components such as coils and aerials with ferrite cores, which would be affected in performance by stray magnetism. Fortunately, this problem does not exist with speakers housed in separate enclosures, so unscreened ceramic magnet systems are commonly used in these types with a saving in cost over equivalent steel magnet types.

Advances in knowledge of electronic sound reproduction and manufacturing techniques, and a steady improvement in the characteristics of materials used

\section*{, LOUDSPEAKERS}

\section*{By \\ H. E. BARNES}
(E.M.I. Sound Products Ltd.)
has resulted in the modern speaker having improved frequency response, efficiency and power output. The most popular loudspeaker unit uses the moving coil system of drive and the explanations which follow apply to this particular type.

Before dealing with the technical details of units and completed loudspeaker systems in enclosures, a general appreciation might prove useful, particularly to newcomers to hi fi.

\section*{OPERATING PRINCIPLES}

The diagram Fig. 3 shows the important details of a moving coil speaker unit. It consists of a rigid frame or chassis, the front edge of which has a flange for fixing the chassis to the baffle board of an enclosure. At the rear of the chassis is the magnet system, which generates magnetic field in a circular gap formed between the centre pole and the front plate of the system, this plate being firmly attached to the chassis.

The diaphragm used to generate the sound waves is usually cone shaped, although it may be dome shaped in some high frequency speaker units. It is fixed at its outer edge to a flexible section of material which in turn is fixed to the flange of the chassis.
The inner portion of the cone or diaphragm is attached to a lightweight tube upon which a coil of copper or aluminium wire is wound. A circular flexible suspension diaphragm keeps the coil clear of the magnet system parts by centring the coil around the pole. The combination of the front and rear suspensions enables the cone and coil to move backwards and forwards under control.

The ends of the coil are attached to flexible connecting leads to which the amplifier is ultimately connected. The output signal from the audio amplifier comprises a complex series of alternating currents which pass through the speaker coil (or speech coil


Fig. 3. Section through a moving coil loudspeaker


Fig. 4. How piston oction of the cone creates sound pressure waves


An early direct radiator loudspeaker by Celestion


Popular small Plessey 3 in loudspeaker frequently used as inexpensive tweeters or as pocket radio speakers
as it is also called), driving it and the cone to and fro in a similar complex series of vibrations.

Since the cone is in contact with air, its vibrations are transmitted in the form of pressure waves to the listeners" ears, Fig. 4. The type of sound one hears depends upon the nature of the pressure waves. The purpose of the whole audio reproducing system is ultimately to regenerate sounds of a loudness and quality as closely resembling the original as possible.

In the case of bass frequencies, the air is displaced at comparatively low speeds. To obtain the required loudness, a much greater amount of air has to be moved per cone movement than at higher frequencies. Without a baffle board around the speaker orifice, air movement at the front of the cone would interfere with that at the back. The neatest form of baffle is usually that shaped into a box and is most effective when it is a sealed box, so that no air movement from the front of the cone can interfere with that at the back of the cone.

\section*{FREQUENCY RESPONSE}

Sounds audible to a good human ear range from approximately 30 Hz to 20 kHz and loudspeaker units can vary considerably in the way they produce this sound spectrum, mainly due to the characteristics of the materials used in speaker manufacture. Some units are designed primarily to reproduce their best at the bass end of the audible range, say, up to 500 Hz . There are mid-range units designed to cover


Fig. 5a. Impedance characteristic of a typical single speaker of wide range compared on the same scale with Fig. 5 b below


Fig. 5b. Impedance characteristic of a typical complete three-speaker system. Crossover frequencies are shown by the slight humps at approximately \(\mathbf{2 5 0 H z}\) and \(\mathbf{2 k H z}\)

500 Hz to 5 kHz for example, and high frequency units complete the audio range from 5 kHz to 20 kHz . There are also units which cover wider frequency ranges in each classification. It is possible to have a loudspeaker with one unit which has a limited range from, say, 100 Hz to 10 kHz or two complementary types of unit, with a crossover frequency network, covering from, say, 50 Hz to 15 kHz . Three types of units, with two crossover frequency networks, could cover a wide range from, say, 40 Hz to 20 kHz .

The crossover frequency networks are usually specified by the manufacturer to suit the frequency responses of the individual speaker units. The frequency of crossover is chosen so that the response of one unit is cut as the next one is introduced to give a smooth overall response.

\section*{IMPEDANCE}

The electrical resistance provided by the speech coil to the applied alternating drive current is the impedance, which is measured in ohms. Because it is the result of coil resistance and the effect of induced voltage in the coil when it vibrates, it is not constant in value over the frequency range of the speaker.

At the lower end of the frequency range of any particular unit, the moving system reaches a point of resonance where the amplitude of vibration is easily maintained for comparatively little input energy. This can produce a point of higher impedance than normal. Similarly, towards the upper end of the frequency range of the unit, the impedance can tend to rise (Fig. 5). The manufacturer generally quotes a nominal value which is usually 400 Hz for a bass unit. This is not necessarily the lowest value but normally the difference is small enough to be ignored.

\section*{MAGNET STRENGTH}

The performance of a speaker for sensitivity and overall frequency response depends a lot upon the power of the magnet system, because the current in the coil reacts with the magnetic field to produce the mechanical vibrations of the cone.
Speakers have various sizes of coil from about \(\frac{1}{2}\) in up to 3 in diameter depending upon their function in the system and the amount of acoustic power they have to produce. In general the larger the total lines of force (larger magnet), the more likely the speaker is to have a superior performance.

\section*{FUNDAMENTAL RESONANCE}

All speaker units have a fundamental resonance. This is of particular importance in the case of the bass speakers because it has a direct bearing upon the bass response of the loudspeaker in an enclosure.

One should select a speaker unit whose bass resonance is as low as possible so that the final resonance in the enclosure is also kept low, otherwise the sound will lack bass quality.

The aim should be to produce a completed speaker with a bass resonance below 100 Hz , and this can normally be achieved in infinite baffle enclosures with units which have a fundamental free air resonance of 35 Hz or less.


EMI 215 system incorporating a \(14 \mathrm{in} \times\) in elliptical bass unit, two 5 in mid-range units, a moulded chassis high frequency unit, and crossover network

\section*{EFFICIENCY}

Efficiency is the relationship between electrical power input to the loudspeaker and its sound power output in equivalent units. For example, a 10 watt power input into a speaker having 10 per cent efficiency will result in one tenth of the input power leaving the speaker as acoustic power-in this case, 1 watt.
Loudspeaker manufacturers rarely quote efficiency figures but as a general rule a unit with a large magnet can have an efficiency of 5 per cent for an 8 -inch round unit and about 10 per cent for a 12 -inch round unit. Bear in mind, however, that this figure is for total radiated sound power from the unit. When it is fitted into an enclosure only about a half of this power is radiated; the other half is ausorbed in the enclosure. The efficiency, therefore, of the complete speaker is half that of the unit in free air.


Fig. 6. Electrical input required for a speaker of 5 per cent efficiency related to room volume and sound intensity within

\section*{POWER RATING}

The loudspeaker is usually rated in terms of the amplifier which can be used to drive it. If the amplifier is rated at 15 watts r.m.s. maximum at, say, \(0 \cdot 1\) per cent total harmonic distortion at 4 ohms impedance, then the loudspeaker will need to have a nominal impedance of 4 ohms and a rating of 15 watts r.m.s. at least. It is not wise to use a loudspeaker with a lower watts rating than the amplifier (each channel in the case of stereo) otherwise the life of the speaker may be reduced.
Many studies have been made by acoustic engineers which have resulted in a relationship being established between power input to a speaker and the loudness of the sound it produces in an average furnished room of known dimensions. This is called acoustic intensity, which is the effect of air pressure waves at the point it is measured. Units are measured in decibels (dB) where 0 dB represents the reference intensity level equivalent to \(10^{-16}\) watts per square centimetre.
It has been established that an intensity level of 100 dB is extremely loud \(f f f\) in musical terms.
90 dB is very loud, off in musical terms. 80 dB is loud, \(f\) in musical terms.

\section*{POWER DRIVE REQUIREMENT}

The results of the studies have concluded with a mathematical relationship between room volume and acoustic intensity, so that if we know the efficiency of a loudspeaker we can obtain a close approximation to the input power required. For the data (Fig. 6 ), an efficiency of 5 per cent for the loudspeaker unit in free air is assumed. The reader can make proportional adjustment to suit. If he has a speaker with 10 per cent efficiency, the input power for a given loudness will be halved.

Remember that the data give the power requirements for one loudspeaker. When stereo is used, theoretically the total power required will be shared equally between the two speakers and amplifier channels. In practice a degree of uneven sound absorption occurs, and it is recommended that each channel is rated at 50 per cent more than the theoretical amount to avoid overload on either channel when the loudness of the channels is corrected by the balance control.

Taking an example, a room with a volume of 100 cubic metres will require a total input power of 10 watts to give a level of 100 dB intensity. If you have a stereo system, each channel will then be rated at \(7 \frac{1}{2}\) watts r.m.s. If you double the power available you will raise the maximum level to 103 dB which does not look much on this scale, and the increase in loudness is just noticeable. Having attained this level of loudness it would cost more money to obtain any marked increase than would be worthwhile.

\section*{LOUDSPEAKER ENCLOSURES}

If you intend to construct a loudspeaker enclosure with speaker units of your own choice it would be wisest to build an infinite baffle type, which is free from tuning problems. Vented cabinets can give low bass frequency response but unless one is prepared to experiment it is easy to spoil the quality of the bass response.
The principle of the infinite baffle enclosure is to seal the speaker units in a rigid walled box so


Cutaway view of a Tannoy folded horn enclosure used with a I5in dual concentric unit

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Response:
Impedance:
Crossover:
Treble:
Mid:
Bass:
Finish:
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44 Watts (D45.500)
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4 to 8 ohms
\(500 \& 5,000 \mathrm{~Hz}\)
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\title{
Music
} at mivnight

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A fairly recent innovation in extending bass response down to 30 Hz is achieved by using an auxiliary bass radiator (right) of similar dimensions to the mid range unit. In this Celestion system (Ditton 15) the ABR is a rigid diaphragm with a linear air suspension capable of large excursions. It is pressure driven by the rear radiation from the adjacent 8 in bass unit


Very good results are obtained by padding a small enclosure with plastics foam as shown in this photograph of the Ditton 10. Notice the rolled neoprene suspension on the cone of the larger unit to give optimum excursion capability


Elliptical speaker ( \(\left.13 \frac{1}{2} \times 8 \frac{1}{4} \mathrm{in}\right)\) with parasitic concentric tweeter - E.M.I. type 150


Elliptical speaker with coaxially mounted \(3 \frac{1}{4}\) in h.f. unit and crossover unit - E.M.I. type 350

that the minimum of "rear-of-cone" radiation occurs to interfere with the "front-of-cone" radiation.
Loudspeaker manufacturers give guidance on enclosure volumes suitable for their units which will give the best results and they often quote examples of enclosure construction. As a general rule, the enclosure walls should be as rigid as possible, and internally lined with absorbent material such as glass wool or acoustic wadding, to prevent reflections of sound back through the speaker cone. All joints of the enclosure and points of entry should be sealed and care should be taken to make sure the speaker units are also sealed to the baffle board.

\section*{MULTI UNITS}

Should your loudspeaker contain a combination of units, place the mid-frequency and high-frequency units off centre in unequal amounts to reduce effects of reflection from the enclosure edges. The mounting of the high frequency unit is usually quite critical and unless you have special equipment for response testing, it is difficult to obtain an optimum result. However, if you mount the unit on the front surface of the baffle board this will be better usually than if it is sunk in a tunnel of baffle board thickness (i.e. on the rear surface of the baffle board).

Make sure all leads are correctly connected and internal components are unable to produce buzzing sounds by vibrating. Keep them completely clear of the speaker units and clamp them firmly to adjacent surfaces, preferably with felt or foam rubber mounting cushions.

There is no mystery around the efficiency of loudspeaker systems; having understood basic principles and peculiarities in certain operating conditions, a great deal of common sense and help from published books will help the reader devise a system to suit his needs.

THis last part shows how a "fire" is indicated and offers some ideas on how added "realism" can be effected by producing suitable battle sounds. Operational tactics are also given.

\section*{STAGE SEVEN一FIRE}

One third of the positions of the Ledex switch will pass current to Panel D (Fig. 17). The leading edge of this current is shaped by the differentiator circuit C30, R120 and passed to a ten second timing circuit. One has already been given (Fig. 10) and here is another. The shaped pulse switches a bistable formed by TR25 and TR26. The result is a slow charge of C31. The trigger formed by TR27 and TR28 finally fires, switching the bistable off again. While the bistable was on it primed the lamp driver TR29 and TR30 and also delivered a charge to the magazine storage capacitors through D13 and R129.
In play, some of the damage indications will be accompanied by a fire indication. The player can do nothing about the fire but watch and wait. If he is lucky, the lamp will go out in ten seconds with nothing untoward happening. If he is unlucky, the charge on his magazine storage capacitor will reach the critical value and the magazine lamp will glow, putting him out of the game.

\section*{SOUND EFFECTS}

Because of the belief that many constructors will want to add sound effects, the writer has spent some time experimenting with circuitry to do this. Various conclusions emerge. First, it would be annoying for sound to be emitted all the time. An on-off switch might serve, but the easiest method would be for sound to be emitted only during dialling. Secondly, hum and noise, oscillation and warble are not unacceptable in the war situation, if suitably filtered or chopped, so nothing elaborate is called for.

Taking off through a \(0.1 \mu \mathrm{~F}\) capacitor at the point (f) indicated in Fig. 3 is satisfactory only at heavier calibre settings, when the sound is like a heavy machine gun. At lighter calibres a buzz is emitted, as would be expected from the higher frequency. Such noises are of course intermittent as the pulse contacts on the dial open and close and do give some indication of hits scored. Figure 18 is given for those who might like to experiment further.
Taking off from point (k) (Fig. 12) gives an indication of damage pulses. As such it is useful, but again, not very realistic.
Examining the back of a telephone dial reveals a third pair of contacts that, like the ones that motivate the Ledex, close when dialling commences. If sound effects are desired the best method is a simple multivibrator giving good voltage swing and of appropriate frequency feeding directly into a permanent magnet loudspeaker and keyed from the dial (Fig. 19).

\section*{PLAYING TABLE}

For a full treatment of the subject the reader is referred to any of the books on war games, particularly "Naval War Games" by Featherstone (Stanley Paul, London, 1969). Here we can give only a sufficient outline. The first requirement is a playing board as large as possible and preferably marked in inch squares. Several sheets of card would do, or even a roll of ceiling paper.
If desired, shallows, rocks, islands and coastlines are marked in. Minefields might also be "laid" by each side and their position not divulged to the opponent. A token for each ship is required, clearly numbered. Simple card shapes will suffice, although for many it could be the beginning of a collection of any of the excellent little models available.



Fig. 17a. Fire indicating circuit on Panel "D"


Fig. I7b. Layout of Panel D and cuts in the copper strips

\section*{COMPONENTS . . .}

STAGE SEVEN (Panel "D" Fig, I7)
Resistors
\begin{tabular}{ll}
\(R e\) \\
\(R 120\) & \(4.7 \mathrm{k} \Omega\) \\
\(R 121\) & \(10 \mathrm{k} \Omega\) \\
\(R 122\) & \(12 \mathrm{k} \Omega\) \\
\(R 123\) & \(2.2 \mathrm{k} \Omega\) \\
\(R 124\) & \(150 \Omega\) \\
\(R 125\) & \(10 \mathrm{k} \Omega\) \\
\(R 126\) & \(10 \mathrm{k} \Omega\) \\
\(R 127\) & \(12 \mathrm{k} \Omega\) \\
\(R 128\) & \(2.2 \mathrm{k} \Omega\) \\
\(R 129\) & \(330 \mathrm{k} \Omega\) \\
\(R 130\) & \(150 \mathrm{k} \Omega\) \\
\(R 131\) & \(2.2 \mathrm{k} \Omega\) \\
\(R 132\) & \(47 \mathrm{k} \Omega\) \\
\(R 133\) & \(47 \mathrm{k} \Omega\) \\
\(R 134\) & \(1 \mathrm{k} \Omega\) \\
\(R 135\) & \(2 \mathrm{k} \Omega\) \\
\(R 136\) & \(10 \mathrm{k} \Omega\) \\
\(R 137\) & \(47 \mathrm{k} \Omega\) \\
\(R 138\) & \(180 \Omega\) \\
& \(1 W\)
\end{tabular}

All \(\pm 10 \%\), \(\frac{1}{4}\) W carbon except R138

\section*{Capacitors}

C30 0.1 \(\mu \mathrm{F}\) 125V
C31 \(50 \mu \mathrm{~F}\) elect. 25 V

\section*{Semiconductors}

TR25 to TR30 OC7I or similar pnp germanium
DI3 OA8I or any small germanium diode
Miscellaneous
Veroboard \(0 \cdot 15\) in matrix \(\sin \times 1 \frac{1}{4}\) in with copper strips


Fig. 18a. Experimental sound effects amplifier


Fig. 18b. Layout of experimental amplifier boards and cuts in the copper strips


Fig. 19. Using an astable multivibrator switched into use by dial contact in the common chassis line

\section*{COMPONENTS}

STAGE EIGHT (Experimental sound effects amplifier)
Resistors
\begin{tabular}{ll}
\(R 139\) & \(330 \mathrm{k} \Omega\) \\
\(R 140\) & \(4.7 \Omega\) \\
\(R 141\) & \(1 \mathrm{k} \Omega\) \\
\(R 142\) & \(330 \mathrm{k} \Omega\) \\
R143 & \(3.3 \mathrm{k} \Omega\) \\
R144 & \(22 \mathrm{k} \Omega\) \\
R145 & \(330 \Omega\) (for 35 ohm \(L S\) )
\end{tabular}

Capacitors
C32 0.1 \(\mu \mathrm{F} \quad 125 \mathrm{~V}\)
C33 \(100 \mu \mathrm{~F}\) elect. 25 V
C34 \(0.1 \mu \mathrm{~F} \quad 125 \mathrm{~V}\)
C35 \(4 \mu \mathrm{~F}\) elect. 25 V
Semiconductors
\(\begin{array}{ll}\text { TR31 } & \text { OC44 } \\ \text { TR32 } & \text { OC8ID } \\ \text { TR33 } & \text { OC81 }\end{array}\)
Miscellaneous
LSI Small 35-40 ohm loudspeaker
Veroboard 0.15 in matrix \(\operatorname{Sin} \times 1 \frac{1}{4}\) in with copper strips

Note: The lamps 6 and 7 should be "Double chance" and lamps 8 and 11 should be "Single chance", and not as indicated on page 816, October issue.

On page 810, half way through "STAGE FOURPANEL B", should read "Capacitor C11 blocks d.c. and leaves only pulses swinging about zero volts . . ."

\section*{SCORE CARDS}

Finally a score card for each ship is needed upon which is marked full details of armament, torpedo tubes, aircraft carried and thickness of belt armour. Sreed is also marked, scaled down to inches per move at full speed, and turning circle, expressed as a 45 degree turn every so many squares. Examples are given in Table 1.

On the reverse side of the card a sketch plan of the ship is made, clearly showing the position and sweep of all turrets and torpedo tubes. When the card is complete it may be covered with clear adhesive tape or sheet and used over and over for many years. Details as required may be obtained from any public library.

Table I: NAVAL FLEET MANCEUVRABILITY
\begin{tabular}{|c|c|c|c|}
\hline Size & Name & Speed (in/move) & Turning distance (for \(45^{\circ}\) ) \\
\hline \multirow[t]{4}{*}{Battleship Carrier Cruiser Destroyer} & \multirow[t]{4}{*}{Vanguard Eagle Essex Ajax} & 3 in & 4 in \\
\hline & & 4 in & 3 in \\
\hline & & 5 in & 3 in \\
\hline & & 7 in & 2 in \\
\hline \multirow[t]{2}{*}{Submarine} & \multirow[t]{2}{*}{Neptune} & \(\left\{\begin{array}{l}\text { surface } \\ 4 i n \\ \text { submerged }\end{array}\right.\) & 2 in \\
\hline & & 2 in & 2 in \\
\hline M.T.B. & T107 & 8 in & lin \\
\hline
\end{tabular}

When all is ready, tokens are placed on the board and play begins. Dice are rolled to determine the state of the sea and the visibility. The dice reading is transferred directly to the computer, and agreement reached as to how of ten this shall be done. Usually they are rolled for every ten moves. Both cancel switches are put in the cancel position and S11 (target number) slowly rotated all the way round, ensuring that all storage capacitors are completely discharged. A coin is tossed, the winner deciding whether to go first or last. Player A moves; player B moves; player A fires; player B fires. Damage is recorded and the coin tossed again. Play continues until one ship or the other is sunk.

\section*{USING THE COMPUTER}

When either player fires, the computer is set up as follows:

Target number corresponds to the number of the token and so must be carefully chosen at the outset.

Target speed is a direct reading in inches and is the speed the vessel is actually supposed to be going (which might be less than its possible maximum).

Armour thickness is taken from the score card and is a direct transfer in inches, as indicated by the knob.

Target size: twelve types of ship are given and the nearest in size to the target is registered.

The angle subtended is the angle the target ship makes to the line of fire; 90 degrees is broadside on, while 180 degrees is bow or stern on; 45 degrees is provided as a halfway condition. There is no need to get a protractor out; simply set the control to the nearest position. Range is directly read in inches and is quickly counted along the inch squares.

Firing ship's speed is also the actual speed indicated by movement in inches.

Morale is determined by dice throw for each ship at the commencement of the game and goes up or down according to the fortunes of war. If damage is inflicted on the enemy, morale goes up one point; if damage is sustained it goes down one point.

Shell type is a conscious choice of HE or AP, while calibre is obtained from the score card.

The whole operation takes less time to do than to read about and when all controls have been quickly set, the number of guns is dialled. This is where the indication of sweep of turrets comes in, for not all turrets will be able to bear upon the target and if in doubt the score card is laid over the token and a straight-edge laid along the extremes of the arc.

Check that both cancel switches are off and dial the number of guns firing and able to bear. The result (if any) is immediately indicated in one or more lamps lighting up.

\section*{EFFECT OF DAMAGE}

If the score card has been covered with clear plastics sheet, Chinagraph pencil may be used on it and wiped off after each game. The effect of damage is as follows:

Conning Tower. Cease firing all main armament for the number of turns determined by a throw of a dice.
Hull. Reduce speed by one-quarter.
Engine Room. Halt for the number of turns determined by a throw of dice.

Rudder. Proceed only in a circle for the number of turns determined by the throw of dice.
Aircraft or Torpedo tube. Opponent decides which he wants knocked out; you choose a particular one.
Sub-Armament. One-quarter of all sub-armament is knocked out.
Forward Turret. One forward turret of main armament is knocked out.
Rear Turret. One rear turret is knocked out.
When the appropriate notes and action are taken the cancel others switch is thrown, extinguishing the lamp. If preferred, double-pole push-buttons might be used instead of switches, thereby ensuring that they cannot accidentally be left in the cancel position.

If a fire is indicated, no action can be taken, but it will always be indicated in association with one of the above.

\section*{VARIATIONS}

Some variations to the game have already been indicated and further variations are limited only by the imagination of the users. Players may have any number of ships under their command and if imagination lags there is always history to turn to. Try running a convoy through a pack of submarines to a particular port, or fight the battles of Jutland, Midway, Otranto, Coromandel or Falkland Islands over again.

\section*{MINES AND TORPEDOES}

From the moment of firing a torpedo has a life of its own. A token with arrow showing direction is placed on the board and it must always follow a straight line course. In the first move it travels 6 in, in its second move 5in, then 4 in and then is assumed to be lost.

If it strikes a target, the computer is set for best conditions and a ten is dialled. The result is almost certainly indicated damage, but only damage below the water-line is accepted, i.e. engine room, hull, rudder, or magazine. All other damage is ignored; likewise with mines. If a ship enters a square in which is supposed to be a mine, the opponent produces his previously prepared note of mine positions. Damage is found by dialling under the same conditions and with the same provisos.

\section*{SUBMARINES}

One side of the playing token could be painted black. If this is placed uppermost the submarine is deemed to be submerged. One move is required to submerge or to surface. While submergd she is considered undetectable although she may fire torpedoes. As for striking back at submarines, readers might like to devise their own rules.

\section*{FIGHTING OTHER BATTLES}

As mentioned at the outset, the computer may be used for other wars and other periods, land as well as sea. Adaptation is simply accomplished by the use of card overlays that alter the readings of some controls and readout lamps.

The cards simply fit over the faces of the computer with the lamps shining through holes. In the case of the card altering the controls it will be necessary to remove the appropriate knob first.

\section*{NEW PCB SERVICE}

All eyes will be on the Inter/ Nepcon exhibition at Brighton this month (October 19-21). It certainly is the most successful specialised exhibition of recent years and attracts production engineers not only from British companies but also in substantial numbers from the Continent.

One of the regular exhibitors is Exacta Circuits Ltd. who, since starting up in 1962 with two men, has climbed up to be in the top three independent printed circuit board manufacturers in the country, specialising in high-quality plated-through-hole and multilayer boards. Having outgrown their old factory (a converted textile mill) in Galashiels, the company moved most of the production staff and equipment to a brand new pur-pose-built factory at Selkirk in August, leaving the Galashiels premises as a bulk store and small-run production unit.

Inter/Nepcon is the occasion chosen to launch Exactaplan, a new service to cut costs and speed delivery to the small man who wants quality boards by the hundred rather than the thousands. Alan Bruce, Exacta's technical director, told me during a sneak preview that Exactaplan, though appearing almost ridiculously simple and obvious, was quite a tough nut to crack. The, idea is to mass produce a range of standard PCBs with a grid pattern already printed on them. From the range, the circuit designer need only select that nearest his needs and indicate which interconnections he desires.

In small batch production, the precision art work is quite a high proportion of the total cost. Exactaplan cuts artwork costs and saves time too.

Exactaplan is being launched with 12 different board sizes, two packaging densities (i.e. standard and fine line) and three types of connectors which logether give a choice of 72 boards.

\section*{WHO WAS FIRST?}

The great excitement generated a few weeks ago by the almost simultaneous announcements from a number of power supply mañufacturers of a breakthrough in "transformerless" solid-state power units brought a wry smile to the lips of Dennis Hendry, managing director of Weir Electronics. Weir had, in fact, been in production with similar units for many months but as they were part of a contract order for a special customer, the company was precluded from giving them any publicity.

Weir Electronics is one of the few companies that has thrived throughout the general recession in the capital goods electronics

\(\mathrm{O}^{\prime}\)UR new feature INDUSTRY NOTEBOOK appears this month for the first time. Many P.E. readers work in the electronics industry and, Indeed, are professional electronic engineers and technicians. Others, though perhaps professionally occupied in other ways will, we believe, also welcome news and views on the electronics industry.
Our regular contributor, Nexus, is close to the industry, both in its technical and commercial aspects. Month by month he will report and comment on significant events, on current trends, on how he sees the future and, where appropriate, how new developments may inspire the electronic hobbyist.

industry. Hendry told me Weir is making a profit of over \(£ 60,000\) p.a. on capital employed of only £130,000. Some fat export contracts are helping enormously and negotiations are in hand for purchasing a production unit in Holland, which will become Weir's forward base for a drive into Europe.

The smaller companies like Weir, with their greater flexibility and faster response time in meetind changing markets are at least spared the present miseries of the giants.

\section*{WHIZZ-KID OF THE EAST}

One of the most remarkable men in the industry has his base over a row of shops in Ealing Broadway, West London. When you enter his office you can't help seeing the magnificent wild boar's head on the wall, the many other souvenirs including a photo of your host shaking hands with Harold Wilson, a smoker's compendium in the form of a wooden model train from the Soviet Union, a fine leather case containing his shot-guns.

His name is Eddie Baizert and he is owner and managing director of a group of companies operating under the generic name Uni-Export. Baizert is now a British subject but was born in Norway and reached these shores via the Middle East. He is a linguist with fluent Russian and Czech and spends most of his time getting orders for British electronic equipment from the Eastern Bloc.

His favourite souvenir, framed and hanging by his desk, is the cheque for \(£ 500\) with which he started in 1961. There was only himself and a secretary. Now he has a staff of 14 at Ealing and three people in .his office in Prague. His first sale was a telephone answering unit worth £25. Today Uni-Export turns over £1 million a year.

He handles all the best names in British equipment, bears all the cost of advertising, exhibition stands and all the other incidentals involved in selling and if he doesn't sell he doesn't charge a bean. You can't be fairer than that-but, as he smilingly points out, Baizert always sells and gets his 15 percent commission.

To keep his eye on the international scene he likes to travel round the world twice a year and normally clocks up 100 k miles in his E-Type Jaguar in Europe for good measure.

\section*{NC STILL STRUGGLING}

The much-publicised Pre-production Scheme devised by the old Mintech to put numericallycontrolled machine tools on the map in Britain cost the tax-payer £2 million and went off like a damp squib. The IRC had a qo at rationalising the industry with a splendid investment of your money and mine. And yet with all the effort and all the cash that has gone in, the numerical control business is still as flat as a pancake.

My sympathy goes to Plessey Numerical Controls which now incorporates all the business and types of equipment (most of it non-compatible) handled by Ferranti and Airmec-AEI as well as the original Plessey product lines. The general recession in the engineering industry is the culprit and, as it turned out, PNC could not have been formed at a worse time.

Nevertheless, morale remains high at PNC headquarters at Poole, even though it is rockbottom at what was to be the main production unit in Scotland, now threatened with closure. Sales mav be slack but it has been a good opportunity to start rationalising the product line, identifying new marketing slots, and preparing for the expected up-turn next year.


Do you remember the VCS3? It was the portable synthesizer from Electronic Music Studios that brought you the whole spectrum of electronic music effects.

Now the VCS3 has become even more portable in the briefcase guise of the Synthi A, but it still contains the same array of elestronic devices and yet only costs \(£ 250\).

With Synthi A the synthesizer becomes available to anyone and everyone with an interest in the excitement of electronic music.

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\section*{PLANTS AREN'T DEAF?}

Since, to the delight of farmers, the effects of playing dance records while lightening milk-laden cows has improved both quality and yield, the scene seems to have switched from the, now tianquil. ruminant to attempts at inducing a similar effect in flora.

It was in India, in fact, that some years ago changes for the better were reported in rice plant yield following about an hour per day musical treatment of the cereal. Since then most experiments have been performed at ultrasonic frequencies with fair success. The reason for the effect is not fully understood, but in part appears due to an increase in the activity of various enzymes associated with the plants growth.

Since the original tests, experiments at audio frequencies have been resumed by two Canadian workers in Ottawa. They have employed at least four different frequencies for continuously irradiating wheatseeds during a period of time (termed vernalisation) when dampened seeds are deliberately reduced to a low temperature to cause early flowering.

Following several weeks of this treatment the seeds are allowed to germinate and the resulting seedlings permitted a period of eight weeks growth. Subsequent measurement of such things as height, weight, number and size of leaves, has revealed a dramatic improvement over normally treated varieties. It is reported that the most effective stimulation frequency is around 5 kHz . This has produced in excess of 200 per cent yield over the plants used as controls.

Believe me, I've tried directing the output of my old record player at the wallflower patch, but alas, other than some raised eyebrows from already curious neighbours, no go. "Raindrops keep falling on my head" and the "Ooh ah" of the bicycling tune had a remarkable effect on the groundsel though!Perhaps the term 'ear' of the wheat is meaningful after all!

\section*{TIME FOR A CHANGE}

There can be but few professions that share the degree to which electronics serves industry; not only industry, but the professions too. Think for example, just how much electronics is now at the " beck and call" of the biological professions. Sure the biologies have given of themselves many times to mankind, however, what of their help to other sciences?
As a change wouldn't it be great if instead, say, of relying on electric motors and hydraulics for prime-movers we employed lumps of cultured muscle tissue! It is not difficult to see what an asset such a material would be, particularly if it could be electrically triggered into contraction or extension.
Apart from the very obvious advantages for the physically handicapped, who would naturally be given priority to use the special muscle, imagine how quiet an automobile would be with this kind of propulsion.

\section*{MUSCLE POWER}

Perhaps thankfully, no one has yet been able to grow muscle tissue on the scale suggested by my reverie, although I recall hearing of someone who went part-way to achieving something rather similar. He found that if a thin strip of collagen (obtained from animal connective tissue and cartilage) is placed in a strong solution of lithium bromide it will slowly contract with a force greater than 1,000 times its own weight. If it is then washed in clean water it will regain, once more, its original form. This process can be repeated, as far as I can remember, ad infinitum.

Actual motors have been built which employ the principle, and generally comprise an endless collagen tape loop running around six pulleys, or so. The tape is first arranged to enter a small tank of lithium bromide solution and, by virtue of a ratchet mechanism. the subsequent contraction pulls more (un-treated) tape into the tank. Simultaneously, since the whole tape will be on-the-move, treated tape can be drawn through yet another tank containing clean water and so complete the cycle.

Output drive is via one of the pulleys.

Just in case you reckon we might have got a perpetual motion device on our hands, and appear scheduled to make some vast fortune, let me dispel the euphoria straight away! The machine will run for several hours, I gather, but ultimately comes to a halt when the tanks become contaminated with one anothers contents.

One day, who knows, someone might invent a mechano-chemical motor which is as successful as its neuro-muscular counterpart. Picture, if you will, the economics of a motor running almost indefinitely on packets of glucose tablets and the occasional mug of beef tea!


\section*{KEEPING A "BEAD" ON THE ADS}

I thought it would only be a matter of time before TV advertisers (in the States, at least) dispensed with their " little old ladies" who diligently keep a daily check on the number of times an advert has been on the screen. A much more reliable, electronic, method of monitoring advertising has now come into being.

The ads are now tagged by a system which makes use of coded data. concealed from the public, and can be either added to an "off the picture" area of the raster, or inserted in the sound channel.
As an aid to advertisers, this holds little interest for me. However, it does of course imply that, because the code will accompany all advertising (eventually, no doubt, in this country as well) one only needs a "code present/absent detector" to automatically turn off vision and sound until programme material returns. The detector would, however, require a delayed "on period" because the code, unfortunately, only appears for a short time at the beginning and end of an ad. l just can't wait for this great new boon to reach the advertising industry!



\author{
By D. S. GIBBS and I. M. SHAW (Ferranti Ltd)
}

|N the past 40 years the performance of car engines has been improved enormously, but the ignition system has hardly changed at all and is becoming inadequate to supply the demands of today's high performance engines. The system described here overcomes the limitations of the conventional (Kettering) system and it is suitable for all types of car, although the improvement will be greatest on high performance models.

\section*{THE CONVENTIONAL SYSTEM}

Fig. 1a shows the conventional system. When the contact breaker closes current flows in the primary of the coil, and rises exponentially at a rate determined by the inductance and resistance of the transformer primary. Typical values are 11 mH and 3.5 ohms giving a time constant ( \(L / R\) ) of about 3 ms (Fig. 1b). After 3 ms the current would rise to about 63 per cent of its maximum value; after 6 ms it would be 87 per cent; and after 9 ms it would have risen to 95 per cent of its final value of 3.4 amps .

When the contact breaker points open the current is suddenly interrupted and a high voltage (about 300 V ) is generated across the primary. This is stepped up to about \(15-20 \mathrm{kV}\) at the secondary, and an arc forms between the plug electrodes.
At low and medium engine speeds this works perfectly well but at high engine speeds the current
in the coil does not have time to reach its full value. As an example, take a four cylinder engine going at 6,000 r.p.m. The engine needs two sparks per revolution which is 12,000 sparks/minute and the time between each spark is 5 ms . Now the contact breaker points are open for 40 per cent of the time and closed for 60 per cent, so that at 6,000 r.p.m. the contact breaker points are closed for just 3 ms . In this time the current in the coil primary can only reach 63 per cent of its low speed value, and if we take into account contact bounce and wear the figure is nearer 50 per cent. Nearly all modern four cylinder engines can reach 6,000 r.p.m., some can reach 7,000 or 8,000 r.p.m., and with a six cylinder engine the situation is still worse because this needs three sparks per revolution.

\section*{TRANSISTOR ASSISTED IGNITION}

Many of the " bolt-on" electronic ignition systems consist of no more than a special high ratio coil switched by a high voltage transistor. The contact breaker is used to interrupt the base current of the transistor. These do give a higher kilovolt output at high r.p.m. and greatly reduced contact breaker wear but they require much more current, sometimes as much as \(10-12 \mathrm{~A}\). This places a severe additional load on an already overburdened electrical system.


(b)

Fig. I(a). The conventional ignition system. (b) graph of current rise with time in ignition coil primary



Fig. 2. Output voltage with engine speed for conventional and capacitor discharge systems


\section*{Fig. 3(a)}


\section*{Fig. 3(b)}


Fig. 3(a). Oscillogram of open circuit secondary voltage with electronic system. Vertical is \(10 \mathrm{kV} / \mathrm{cm}\) and horizontal \(200 \mathrm{\mu s} / \mathrm{cm}\). (b) open circuit secondary voltage with conventional system. Vertical is \(10 \mathrm{kV} / \mathrm{cm}\) and horizontal \(500 \mu \mathrm{~s} / \mathrm{cm}\)

\section*{CAPACITOR DISCHARGE IGNITION}

In the past few years another system has been gaining in popularity-the capacitor discharge system. In this system a transistor inverter is used to charge up a capacitor to about 400 V . Energy is stored in the capacitor, and when the contact breaker opens, a silicon controlled rectifier is triggered and discharges the capacitor through the coil. This system has several important advantages:
1. The kilovolt output has a very fast rise time, typically \(20-30 \mu \mathrm{~s}\) as compared with \(100 \mu \mathrm{~s}\) for the conventional systems. This enables it to fire fouled plugs more easily and gives easier starting and smoother running when cold.
2. Low current drain. At low speeds it needs only about 1 A , rising to 34 A at very high speeds.
3. It will work with the ordinary ignition coil, a high ratio coil is not required, and in the unlikely event of failure the system can be put back to normal merely by reconnecting a few leads.
The circuit described here gives virtually constant output voltage over the whole speed range,

\section*{Fig. 4(a)}


Fig. 4(a). Output voltage of electronic system loaded with \(470 \mathrm{k} \Omega\) and 40 pF . Vertical is \(10 \mathrm{kV} / \mathrm{cm}\) and horizontal \(200 \mu \mathrm{~s} / \mathrm{cm}\). (b) output voltage of conventional system loaded as before. Vertical is \(10 \mathrm{kV} / \mathrm{cm}\) and horizontal \(500 \mu \mathrm{~s} / \mathrm{cm}\)
to over 10,000 r.p.m. for a four cylinder engine and 7,000 r.p.m. for six cylinder. This gives improved combustion and more accurate timing. The greatly reduced contact breaker wear allows the engine to remain "in tune" and improves the petrol consumption and power, and the contact breaker will not need adjustment for about 20,000 miles.

\section*{PERFORMANCE}

Figs. 2 to 6 compare the performance of the capacitor discharge and the conventional system. Fig. 2 shows how the output voltage of the electronic system remains almost constant, and is still high enough to produce a good spark even when heavily loaded with a parallel combination of 470 kilohms and 50 picofarads (simulating a badly fouled plug). The prototype actually operated up to the equivalent of 15,000 r.p.m. (four cylinder) although the circuit is only designed to work up to two thirds of this speed.

In Figs. 3 and 4 are shown the actual secondary voltage waveforms obtained. Fig. 5 shows the much faster rise time of the electronic system.


\section*{Fits. 5 (b)}


Fig. 5(a). Expansion of Fig. 3(a), showing rise time of electronic system. Vertical is \(10 \mathrm{kV} / \mathrm{cm}\) and horizontal \(50 \mu s / \mathrm{cm}\). (b) expansion of Fig. 3(b) showing rise time of conventional system. Vertical is \(10 \mathrm{kV} / \mathrm{cm}\) and horizontal \(50 \mu \mathrm{~s} / \mathrm{cm}\)

The spark current traces shown in Fig. 6 are particularly interesting. In the conventional system the spark current is unidirectional. This causes erosion of the sparking plug gaps due to deposition of metal from one electrode to the other.
In the electronic system not only is the spark much shorter -0.2 ms as compared with 1 ms for the conventional system-but it also has nearly equal positive and negative half cycles. This greatly reduces plug erosion and increases spark plug life.

\section*{CIRCUIT DESCRIPTION}

The complete circuit diagram is shown in Fig. 7. Transistor TR1 is not required for positive earth use but it may be left in circuit if desired. This will enable the ignition unit to be used in cars of either polarity merely by altering a few connections. It is only suitable for 12 V systems.
Assume that the circuit is wired for negative earth with tag 9 earthed and the contact breaker connected to tag 8.

When the contact breaker closes TRI is saturated and TR2 is cut off. When the contact breaker opens TR1 turns off and C 1 is rapidly charged via R3. TR2 turns on and the positive pulse at its collector is differentiated by C2 and R11 and applied to the gate of SCR 1 as a trigger pulse.

\section*{Fig. \(6(a)\)}



Fig. \(\mathbf{G ( b )}\)

Fig. 6(a). Spark current produced by electronic system. Vertical is \(100 \mathrm{~mA} / \mathrm{cm}\) and horizontal \(50_{\mu} \mathrm{s} / \mathrm{cm}\). (b) spark current produced by the canventional system. Vertical is \(50 \mathrm{~mA} / \mathrm{cm}\) and horizontal \(20 C_{\mu \mathrm{s}} / \mathrm{cm}\)

Transistors TR4 and TR5 with the ferrite core transformer T1 form a very efficient push-pull inverter, oscillating at about 2 kHz . The 400 V alternating output from the secondary is rectified by the bridge D3-D6 and charges the energy storage capacitors C6 and C7 in about 1.5 ms (Fig. 8).

When fully charged the capacitors store 80 millijoules, which is about the same as the energy produced by the conventional system under ideal conditions.

When the thyristor is triggered C6 and C7 are switched directly across the coil so that the coil primary voltage instantanecusly rises to minus 400 V . The coil voltage then follows a cosine law whilst the coil current follows a sine law, the frequency being determined by the coil primary inductance in parallel with C6 and C7. See Figs. 9 and 10.
As the coil voltage reaches its positive peak the coil current passes through zero and the thyristor turns off. Then, as the coil voltage begins to fall, the diodes in the rectifier bridge become forward biased allowing the coil current to reverse. As the coil voltage reaches its second negative peak the current has again reached zero, but since the thyristor is now turned off the current cannot reverse again, and the remaining coil voltage is left on the storage capacitors C6 and C7. The capacitors then start to recharge for the next pulse.


\section*{\(2 T \times 500\) \\ 000
\(06:\)}


Fig. 7. Circuit diagram of the capacitor discharge system

\section*{COMPONENTS...}
\begin{tabular}{|c|c|c|c|}
\hline \multicolumn{4}{|l|}{Resistors} \\
\hline RI & 22 S & R7 & 1 k , \\
\hline R2 & \(150 \Omega 2 \mathrm{~W}\) & R8 & \(1 \cdot 2 \mathrm{k} \Omega\) \\
\hline R3 & \(150 \Omega 2 \mathrm{~W}\) & R9 & \(150 \Omega 2 \mathrm{~W}\) \\
\hline R4 & Ik \(\Omega\) & R10 & \(15 \Omega \mathrm{IW}\) \\
\hline R5 & \(470 \Omega\) & RII & \(100 \Omega\) \\
\hline R6 & IkS & RI2 & 330 S S IW \\
\hline
\end{tabular}

All \(\frac{1}{2} W 10 \%\) carbon except where otherwise stated

\section*{Capacitors}
\begin{tabular}{ll} 
C1 & \(0.22 \mu \mathrm{~F} 250 \mathrm{~V}\) Mullard C280 \\
C2 & \(0.1 \mu \mathrm{~F} 250 \mathrm{~V}\) Mulard C280 \\
C3 & \(0.47 \mu \mathrm{~F} 250 \mathrm{~V}\) Mullard C280 \\
C4 & \(250 \mu \mathrm{~F} 40 \mathrm{~V}\) Mullard C437 \\
C5 & \(0.01 \mu \mathrm{~F} 1,000 \mathrm{~V}\) \\
C6 & \(0.47 \mu \mathrm{~F} 1,000 \mathrm{~V}\) \\
C7 & \(0.47 \mu \mathrm{~F} 1,000 \mathrm{~V}\)
\end{tabular}

\section*{Transistors}

TRI-TR3 ZTX500 Ferranti (3 off)
TR4, TR5 2N3055 Ferranti (2 off)

\section*{Diodes and Thyristor}
\begin{tabular}{lll} 
D1,D2 ZS170 or ZS270 & Ferranti (2 off) \\
D3-D6 ZS178 or ZS278 & Ferranti (4 off) \\
SCR1 2N4444
\end{tabular}

SCRI 2N4444

\section*{Transformer}

TI-Two Mullard FX2243 ferrite cups with DT2206 former (see text). Ready wound transformer available from A.M.C. Electronics Ltd., 160 Drake Street, Rochdale, Lancs.

\section*{Miscellaneous}

Eddystone diecast case \(7 \frac{1}{4}\) in \(\times 4 \frac{1}{2}\) in \(\times 2\) in
6 -way 5A connector block, mica washers, screws, spacers, turret tags, 14/0076 connecting wire, TO3 transistor covers
An etched printed-circuit board is available from A.M.C. Electronics Ltd. (see above)


Fig. 8. Voltage on thyristor anode. Vertical is \(100 \mathrm{~V} / \mathrm{cm}\) and horizontal \(0.5 \mu \mathrm{~s} / \mathrm{cm}\)


Fig. 9. Voltage across coil primary. Vertical is 200V/cm and horizontal \(50 \mu \mathrm{~s} / \mathrm{cm}\)


Fig. 10. Current in coil primary. Vertical is \(5 A / \mathrm{cm}\) and horizontal \(50 \mu \mathrm{~s} / \mathrm{cm}\)


The completed electronic ignition unit in a diecast box. Note the terminal block and power transistors with plastics covers

\section*{PREVENTING LATCH ON}

When the thyristor turns on it places a short circuit across the rectifier bridge. This does not damage the inverter because the base drive to TR4 and TR5 disappears at the same time, but the inverter tends to produce a low amplitude oscillation at several hundred kilohertz. Normally the output current under these conditions will be insufficient to cause the thyristor to latch on, but to ensure reliable operation TR3 acts as a monostable which switches off the base bias to TR4 and TR5 for about 0.3 ms after the thyristor fires. This stops the inverter completely so that there is no possibility of the thyristor latching on.

It is important to prevent the thyristor from triggering on spurious pulses produced by contact bounce when the contact breaker points close. In the circuit this is prevented by diode DI and capacitor Cl

When the contact breaker closes, TR1 turns on and diode D 1 is reversed biased. Cl then discharges slowly through R4 and R5, holding TR2 on for a further 0.3 ms . Any spurious pulses arriving in this period cannot trigger the thyristor as TR2 is still saturated.

Further noise immunity is provided by C 2 which takes about 0.3 ms to discharge fully after TR2 turns off.

Next month: Complete constructional details for the ignition system will be given together with information on testing and installing the unit in the car.



\title{
ELEOTRONORAM
}

\section*{University to use OB Television Recording Van}

A
mOBILE television unit equipped and staffed to produce material required by colleges of the University of Durham's Institute of Education has just completed its initial term's work and will begin its first full year of operation this autumn. Designed and constructed by the Video Systems Division of Bell \& Howell. it is housed in a specially modified van. The unit is to be operated by Durham's recently established educational television consortium, and will spend at least four days of every term at the disposal of lecturing staff
To meet these and other production requirements, the unit is equipped with three Bell \& Howell


\section*{Laser Memory}

THE development of a crystal that stores hologram images as atomic patterns that can be read out one by one by slow rotation in a laser beam, like photographic slides in a projector, is reported by RCA.

As the laser beam traverses the crystal part of it is diffracted (bent) to fall on a round mirror where it reconstructs any stored information in the crystal (left).

This new advance in holography may lead to a revolutionary document storage system in which files of statistics, architectural drawings, computer data, photographs, maps and other graphic materials are stored permanently in crystals the size of sugar cubes.
A novel computer memory which for the first time will make it possible for a million bits of data to be written, stored, read out repeatedly, or erased by laser light will be built by RCA for NASA, the American Space agency.

When completed next spring, the experimental, six-foot-long, telescope-shaped device will be the first fullcycle, all-optical memory ever built.

The experimental system is being built under a \(\$ 193,000\) NASA contract, with the Marshall Space Flight Center having overall technical direction. The system is expected to validate the optical memory concept and to establish a base for the possible development of units that could be installed in space stations. earth resources satellites and similar spacecraft that need to store and process extremely large volumes of data at high speed. The laboratory model is shown below.

The optical memory appears suited for such applications because of its freedom from dependence on any sort of mechanical motion and its reliability. Such a memory, because it combines extremely large data storage with electronic access, could sometime in the 1980s replace the entire hierarchy of magnetic tapes. discs. drums and cores now used in modern computers.


\section*{Monochrome Telecine for Education Studios}

ANEW monochrome telecine unit specially designed for professional closed-circuit television work has been introduced by EMI Electronics Ltd. Designated the type " 416 " the new EMI equipment enables material on 16 mm film and 35 mm slides to be used in the production of educational television programmes, and also provides captioning facilities.

SINCE the behaviour of silicon semiconductor devices follows a common pattern, it will be found that the base emitter junction can be used as a conventional diode. Similarly, the base-emitter junction of a silicon planar \(n p n\) transistor can be used as a low power Zener diode under certain operating conditions.

The reverse breakdown voltage of almost all silicon planar transistors usually lies somewhere between 7 and 10 volts. This is why the maximum reverse rating of such base-emitter junctions is quoted at 5 to 6 volts, since Zener breakdown is not normally required in the application to which it is subjected.

However, provided steps are taken to limit the power dissipated to around 100 mW or so in the case of low power transistors, it will be found that the Zener voltage of any particular specimen remains remarkably constant.

\section*{ZENER VOLTAGES}

The graph in Fig. la shows, by means of a histogram, the range of base-emitter Zener voltages measured on a batch of 30 unmarked npn silicon transistors at 5 mA Zener current.

Although these transistors were unmarked, they were quoted as all being of a similar type.

It is reasonable to suppose that a batch of 30 guaranteed manufacturer's transistors would show a much closer spread-although it might be considered an advantage to have a range of Zener diodes so readily available in this way.

In point of fact, a measurement of a few new transistors, type BSY95a, did show a much tighter spread of base-emitter Zener breakdown voltage.

The graph A in Fig. 1b shows the voltage-current curve for one of the batch of 30 mentioned above.

The circuit configuration when using a transistor in this way is given in Fig. 2. Note that the emitter is made positive with respect to the base.

The value of R 1 is chosen, after \(V_{0}\) and \(I_{\mathrm{L}}\) are known, by Ohms law, that is:
\[
R_{1}=\frac{V_{\mathrm{R}}}{I_{\mathrm{R}}}=\frac{V_{\mathrm{i}(\min )}-V_{Z}}{I_{\mathrm{L}}+I_{\mathrm{Z}}}
\]

Iz should be about 3 mA for a small transistor used as a Zener.

Note that if the load current falls to zero by, for example, the load going open circuit, all the former load current will flow in the Zener and due allowance must be made for this.


Fig. Ia. Range of base-emitter Zener voltages of a number of sample silicon transistors


Fig. Ib. Voltage/current characteristic of one sample


Fig. 2. Circuit used to measure the graph in Fig. Ib

The maximum dissipation in the Zener substitute should be restricted to about 100 mW in the case of small 300 mW transistors such as BC108; more powerful transistors, such as BCY51, can handle 300 mW in this mode.

Details of how to regulate greater power levels follow later.

If, as in Fig. 3, the base-emitter junction is biased forward (as it would be in normal transistor use), then once again a closely controlled voltage is obtained, this time of around \(600-700 \mathrm{mV}\).

Fig. 4 shows on a histogram the range of such voltages measured on the same batch of 30 transistors mentioned earlier, again at a current of 5 mA . Graph B in Fig. 1b gives the performance of one of these transistors used in this way at various base-emitter currents.


Fig. 5. Series transistors as Zener diodes

\section*{SERIES DIODES}

It is possible, of course, to use Zener diodes in series, and the same applies to transistor substitutes. For example, Fig. 5 gives the set-up to provide 9 volts \((8.4+0.6)\) from an unregulated supply.

Since the temperature coefficients of a base-emitter junction are of opposite sigh, according to which polarity is connected, some measure of temperature compensation is obtained in this last circuit. This is useful in, say, motor car applications, where the voltage supply to instrumentation circuitry can thus be stabilised against battery fluctuations over a wide temperature range.

In view of the availability from a number of advertisers of npn silicon planar transistors at prices around 20 to 30 for 50 p , it is well worthwhile to consider these devices for use as Zeners in regulated power supplies.

Even if more than one device is required for a single application, there could still be cost savings; this will allow the constructor to make use of some of the more sophisticated circuits which follow, at no greater expense. Thus, greater flexibility and improved performance are obtained.

Substitute Zeners can be employed in a variety of regulated supplies, and those given here are intended to be typical. Any component values quoted are not necessarily optimum, but do show the principles involved, while the simple design formulae given should allow experimenters to adapt circuits to their own requirements.

There is (naturally!) a disadvantage in the use of a transistor as a Zener diode, and that is the limited range of voltages available.

\section*{HIGHER OUTPUT}

It is, however, easy to arrange for a higher output voltage, and the method used is shown in Fig. 6. (Although a transistor used as a Zener is shown, a conventional Zener diode can be used.)

The output voltage is
\[
V_{\mathrm{o}}=\frac{R_{\mathrm{3}}+R_{2}}{R_{3}}\left(V_{\mathrm{z}}+V_{\mathrm{BE}}\right)
\]

Fig. 4. Range of baseemitter forward voltages from the sample batch
for 9 V supply


Fig. 6. Arranging higher output voltage by using a transistor
where \(V_{\mathrm{BE}}\) is the base-emitter voltage of the transistor TR1. This voltage is effectively in series with the Zener voltage and must be included. With a silicon transistor used for TR1, \(V_{\text {BE }}\) will be about 0.6 V ; a germanium transistor will have a \(V_{\mathrm{BE}}\) of about half this.

The maximum dissipation of the "amplified Zener", as this arrangement has been called, is that of the Zener plus the transistor TR1.

Typical values of R2 and R3 are \(15 \mathrm{k} \Omega\) and \(3 \cdot 3 \mathrm{k} \Omega\) respectively; such values give a \(V_{0}\) of 9 V with a Zener of \(6 \cdot 8 \mathrm{~V}\).

Calculation of the value of R1 in Fig. 6 follows the procedure given for the simple Zener circuit.

It is not as straightforward to arrive at an output voltage lower than the Zener voltage, and although it can be done, it would be better to leave consideration of this point until somewhat later, when we come to consider series regulators.

\section*{MEASURING ZENER VOLTAGE}

Before any transistor is used as a Zener it would be desirable to measure its Zener voltage, bearing in mind the likely variation in that voltage from sample to sample.


Fig. 7. Simple means of measuring Zener voltage


Fig. 8. F.E.T. Zener voltmeter for use with constant current tester. Values for \(R_{M}\) are as follows: \(5.6 \mathrm{k} \Omega\) fixed and \(5 \mathrm{k} \Omega\) preset for 1 mA meter \(10 \mathrm{k} \Omega\) fixed and \(10 \mathrm{k} \Omega\) preset for \(500 \mu \mathrm{~A}\) meter \(56 \mathrm{k} \Omega\) fixed and \(50 \mathrm{k} \Omega\) preset for \(100 \mu \mathrm{~A}\) meter

A suitable arrangement for this measurement is given in Fig. 7. The voltage at the base is fixed by the two bias resistors and thus the emitter voltage is fixed too. Hence with a fixed value of emitter resistor a constant current will flow through the transistor when the collector circuit is completed.

If the substitute Zener is connected as shown, the constant current mentioned will flow through it and so a useful measurement can be made of its Zener voltage. This will be the more useful since various samples of Zeners will all automatically be tested at the same current.

The above reasoning naturally assumes that the supply voltage is high enough to develop the required voltage across the Zener and in addition provide voltage for the constant current transistor to function. A supply of about \(30 \%\) greater than the highest Zener voltage likely to be measured should suffice.

In Fig. 7 the test current will be 5 mA for the value of R1 shown. Lower values of R1 will give larger currents and vice versa, so permitting testing at other currents if desired.

In practical use, any low or medium power \(p n p\) transistor, such as ACY17, can be used. Remember that maximum dissipation will take place in the transistor with the lower values of Zener voltage, for it is then that most voltage appears across the transistor. Thus when measurements of the forward voltage drop of base-emitter junctions (about 600 mV ) are being made, almost all the supply voltage will appear across the transistor, so dissipating 75 mW at a test current of 5 mA . At higher test currents, some form of heat sink may be needed.

\section*{F.E.T. ZENER VOLTMETER}

Measurement of the Zener voltage itself can be carried out with a high resistance testmeter on the appropriate voltage range. However, if testing of Zener diodes is to be done at low currents or if only a low resistance testmeter is available, then a simple f.e.t. voltmeter has several advantages, and a suitable circuit is shown in Fig. 8.

A popular type of f.e.t. is used. The set zero control is used to show zero volts on the meter with the switch in the "zero" position. The Zener under test is connected and the switch put to "read"; after the reading is taken, the switch should be returned to "zero" to prevent the meter reading the 15 V supply voltage when the Zener is removed.

Values of external series resistance \(\mathrm{R}_{\mathrm{M}}\) are given in Fig 8 caption for some popular meter sensitivities. It is required to be adjustable to allow for various f.e.t. characteristics and meter resistances, and is quite easily set up.
First, switch to "zero" and adjust the set zero control for zero on the meter. With the "zero/read" switch still at "zero", connect the positive terminal of, say, a 6 volt battery to the point marked " \(X\) " in Fig. 8, with the battery negative to the tester negative rail. Monitor this battery voltage with a suitable test-meter (this can be of a low resistance type). Adjust \(R_{M}\) to give a suitable reading on the meter used; for example, with a 1 mA meter aim for an indication of 0.6 mA with 6 volts applied.
The advantages of this circuit are that a basic meter of low sensitivity can be utilised, and that Zener voltages can be measured at low currents. If a simple voltmeter circuit were used, it would have to be ensured that the current taken by the voltmeter was small compared with the test current, for otherwise the level of test current would vary as the current into the voltmeter varied. The f.e.t. voltmeter shown does not have this disadvantage even at test currents as low as \(100 \mu \mathrm{~A}\).

\section*{ZENER REGULATORS}

As mentioned earlier, the upper limit of power handling for a substitute Zener is reached at a few hundred milliwatts or so.

However, it is easy to arrange for greater levels to be regulated, and there are basically two ways of achieving this, using additional power handling transistors: as will be shown next month.

Get the facts you need to identify and use the mass of linear and digital integrated circuits now available. Classified tables of data and applications information are given in the supplement in our December issue.

\section*{Integrated Circuit Survey}

\section*{Logical Radio Control}

Integrated circuits are used to great advantage in coding and decoding proportional radio control functions for models. Wiring is simplified with printed circuit cards making control systems small enough for a wide range of models.

\section*{Digital Dice}

This small battery operated dice has a neat array of spots in conventional dice configuration, and is illuminated by pressing a button. The actual value shown is determined by random switching of a counter and gating circuit.

\section*{An Added Attraction EIECTROLVMHFSCEMEE AND MAIIERALICS}

This
article
principles of light explains the conductor materialting semition with moderials in conneccommunication.


\section*{DECEMBER ISSUE}

\section*{"IOEAS" LIBRARY}

For the electronics enthusiast there is a wealth of interesting ideas buried in the millions of patents kept in the library attached to the British Patent Office in Southampton Buildings, Chancery Lane. And the numbers are added to every week. It costs nothing to refer to anything kept there and it only costs 25p to buy a copy of any British patent specification. The only trouble is finding interesting needles in the haystack.

The idea behind this column is
that circuit by the dozen and advertising them for sale.

So if anyone has ideas from this or any subsequent article, please use some common sense and if in doubt take professional advice from a chartered patent agent. Bear in mind that agents' time is not cheap to buy and so professional advice should only be sought where really necessary. The Editor cannot enter into any correspondence on the legal aspects of patent applications, inventions, or specifications.

One final point. A reasonable estimate would be that 90 per
synchronisers have been marketed although for one reason or another their presence have tended to complicate the overall system in a manner which Elektroakusztikai Gyar maintain is unnecessary.

The Hungarians suggest solving the problem by using a separate synchroniser, but one which records the control signals on the tape from an amplifier with switchable positive feedback. By means of a capacitor this positive feedback converts the circuits used into an approximately assymetrical multivibrator so that the amplifier can handle the function of a code
to pick out a few of those "needles" and in view of the massive numbers of specifications involved it seems sensible to concentrate only on those that are being newly published. So a few of those most likely to interest Practical Electronics readers will be mentioned in this series.

\section*{LEGAL ASPECT}

On the legal side of things, remember that a patent serves two purposes. Firstly, it discloses to the public the details of what the patentees have been doing, and secondly-for a period of up to sixteen years while the patent is in force-it gives the patentee a monopoly on whatever is really new in his activities.

The scope of this monopoly is defined by the claims which are found at the end of the specification and so-in theory at leastyou are liable to be sued if you do what the patentee is claiming. But in practice, of course, the average reader of Practical Electronics is likely to be far less bothered by the legal side of things than he might at first fear.

Quite apart from the question of whether what he is doing actually meets 'the requirements of the patent claims, and quite apart from the question of whether those claims are really valid (these are questions that only a chartered patent agent can advise you on) it is common sense that a reader playing about in his garden shed with a bit of one-off circuitry is unlikely to find himself sued by a multi-million pound electronics firm on the grounds that he has made up a version of a patented device or circuit.

But it could be very different if the same reader starts making up
cent of everything disclosed in any patent specification is established knowledge anyway. Most patents need pages of background information to highlight the novel and inventive step-and of course those pages of background information are often of the most interest to the amateur constructor. If something described is old and known, it is assumed free for anyone to use.

\section*{SIMPLE SLIDE SYMC}

THE Hungarian firm Elektroakusztikai Gyar have a new British Patent 1230040 which concerns a synchroniser for automatically operating a multitrack tape recorder and an electronically remote-controlled slide projector. To date a wide variety of control systems have been devised for ganging tape recorders and slide projectors so that a recorded commentary automatically controls slide change.

Recently some fairly sophisticated set-ups have emerged. For instance where a built-in synchroniser is used, the synchronising signal has been recorded and reproduced by means of an erase head. 50 Hz signals are taken off the mains and fed to the erase head for recording onto a second track. On playback these signals are detected by the same erase head and used with amplification to operate the projector control relay. (Tape erasure may also be handled by erase head when fed by a d.c. voltage.) This all works well but problems arise when the tape recorder does not have a built-in synchroniser. So separate
oscillator as well as its other routine functions (see Fig. 1).

The patent specification describes some convenient transistorised circuitry for positive

BP 1230040


Fig. 1


Fig. 2
feedback production-and most important of all-the circuitry looks fairly simple and thus should provide an equally fairly cheap system for "add-on" synchronisation. The feedback switch of course also provides for easy manual control of the projector. The detailed circuit without component values is in Fig. 2.

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\(\qquad\)I

A\(S\) an enthusiastic user of a 35 mm still projector, the author has found that the cost of replacing blown bulbs can be rather high. It is common knowledge that a lamp's filament is more likely to fuse at the instant of switch-on than at any other time. The reason for this can be seen best by taking an example.

A 500 watt, 250 volt lamp in normal use carries a current of 2 amp. However, if the cold lamp's resistance is measured by an ohmmeter, it is found to be \(4-5\) ohms. By Ohm"s Law this indicates that, it switch-on, the current carried will be 50 amps .


Fig. I. Switch protection for the Projector lamp thermistor


Fig. 2. Circuit diagram of the Automatic Projector Lamp Protector

It is, therefore, not very surprising that lamps will tend to fuse at switch-on.

\section*{SURGE LIMITING}

In order to reduct this initial surge, thermistors are made which have cold resistance of about 120 chms and hot resistances of approximately one ohm. If this 120 ohms and the lamp's \(4-5\) ohms are connected in series across the mains, the current at switch-on will be 2 amps.

As this current heats up the thermistor its initial resistance value will begin to fall and hence the current through it will rise. The temperature of the lamp's filament will also rise, and so will its resistance.

These two changes occurring at the same time tend to balance one another out and the current through the lamp and the thermistor remains at about 2 amps, or a little lower since the lamp heats up more rapidly than the thermistor.

\section*{THERMISTOR PROTECTION}

If the thermistor is left in circuit, its effect on the lamp's brilliance will be negligible. However, the temperature of the thermistor may reach \(200-250^{\circ} \mathrm{C}\) in free air and higher if enclosed.

At these temperatures the thermistor is rather fragile, and unless it is shorted out soon after switchon, may, easily break as a result of vibration. In addition any subsequent switch-on must be delayed by \(10-15\) minutes as it requires this period to cool down.

A manually operated switch, SI, connected in parallel with the thermistor as in Fig. I, is apt to be overlooked and in consequence the life of the CZ12 is reduced.

\section*{RELAY SWITCHING}

To overcome this problem, automatic switching using a relay was devised as in Fig. 2. Since initially most of the voltage appears across the thermistor
there will be a delay period before the relay operates as R1 and R2 form a divider to provide a suitable voltage for the relay. As the line volts are alternating a rectifier DI and smoothing capacitor are required.

The relay used in the prototype had a coil resistance of 700 ohms. With an operating voltage from 12-24 volts, a 2 kilohm resistor for \(\mathbf{R 2}\) is suitable.

If other relays of similar operating requirements are available the value of this resistor should be tailored to provide contact pull-in after about six seconds.

\section*{COMPONENTS . . .}
\[
\begin{array}{lll}
\mathrm{R1} & 12 \mathrm{k} \Omega 5 \mathrm{~W} \\
\mathrm{R} 2 & 2 \mathrm{k} \Omega \mathrm{IW}
\end{array}
\]
Capacitor
\(\mathrm{Cl} 25 \mu \mathrm{~F}\) elect. 50 V
Thermistor
XI CZI2 (Henry's Radio) (See text for type variants)
Diode
DI BYIOO
Relay
RLA 2 pole, 2 way, 12-24V 700 ohm type 4189GD contact rating 2A (Henry's Radio)
Miscellaneous
Standard tag board, wire


Fig. 3. Tag board assembly and wiring details for the Lamp Protector

\section*{CONSTRUCTION}

The relay and associated components shown contained in the dashed box can be assembled on a piece of standard tag board as shown in Fig. 3. As wiring is not at all critical other layouts may be employed.

If lower voltage lamps are used, the thermistor type should be changed as follows. For lamps up to 150 W -CZ9A. And for lamps up to 300 W CZ11. With these alternatives there is no need to change any of the relay circuit components values.

If the projector has a fan, it should be left connected to the mains and not included in the lamp control circuit. The tag board assembly should be clear of this if mounting in the projector is intended.

\section*{NEWS BRIEFS}

\section*{Patents and The Patent Office}

AmOST useful and informative booklet has just been A published by The Patent Office, London. It describes the information retrieval services provided by the Patent Office ("the largest technical publisher in the country") and how to make use of them
The booklet also deals briefly with applying for a patent, and the exploitation of a patent. And contains a list of publications available concerned with invention and patent literature.

The booklet is available free of charge from Sale Branch, The Patent Office, Orpington, Kent BR5 3RD.

\section*{Worldwide Communication}

The North Staffordshire Polytechnic has recently improved its amateur radio station equipment and now has a rotating complex of beam aerials on top of a 60 ft tower mounted on the roof at the polytechnic.

The new aerial system. the wide range communications equipment and the facilities at the adjacent electronics laboratory have made this station the most advanced installation of its type in the country. Signals from the station can be received, the Polytechnic say, anywhere in the world.
The equipment which includes three transmitters has been acquired over the past four years and some of it has been built or modified by students. Officially G3VZI -the station's call sign-is operated by North Staffordshire Polytechnic's Amateur Radio and Electronic Society.

\section*{Dimmer Switches}

The Accessories Section of the Initallation Equipment
Division of BEAMA has recently extended its scope to cover dimmer switches for domestic and similar lighting circuits.
A technical panel has been set up in collaboration with the Appliance Control Section of BEAMA and other interested bodies, to produce a draft British Standard Specification covering dimmer switches.

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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thoushe.
This is YOUR page and any idea published will be awarded payment according to its merit.

\section*{IC TEST JIG}

BEING faced with the need to test and experiment with a variety of dual-in-line type i.c.s, and not wishing to part with the cost of an expensive commercial type "breadboard", I evolved the following extremely handy inexpensive test jig.
The complete unit can be built in under 30 minutes, costs less than 50 pence and consists of one 16-pin DIL i.c. socket, one small piece of 0.1 matrix Veroboard size \(17 \times 24\) holes, and 16 Veropins.
The jig is constructed as shown in the photographs. The distance between the Veropins is great enough to allow connection of crocodile clips with minimum risk of short circuits.

It should be noted that the \(+V_{C C}\) and earth connections for 14-pin DIL's are different and the necessary modification will have to be made to the board.
This system could be enlarged using a larger board and it could also be adapted for TO5 type i.c.s using the sockets and pin spreaders available from advertisers.

\author{
Jnr. Tech. Nekrews, Royal Air Force, BFPO 45.
}

\section*{LIFT-NOTE GENERATOR}

THE circuit in Fig. 1 will produce tones in increasing frequencies until the highest one is reached. Then the cycle repeats again from the lowest frequency. The circuit consists of an astable multivibrator, a pump counter, and a tone generator.

The switching frequency of the astable is varied by the potentiometers VR1, VR2, and this frequency decides the speed at which the tone changes from one frequency to a higher one.

The voltage across transistor TR3 is used to control the pump counter. When this is conducting, only a low voltage is obtained across it. But when TR3 is cut off, this voltage increases considerably. A negative signal is then introduced to the base of TR4 and this turns TR4 on.

When TR4 is cut off a high resistance appears between its emitter and collector. C5 then charges through R6, C4 and D2. Depending on the value of C4, a fixed fraction of the supply voltage appears across C5.

When TR4 turns on, resulting in a low resistance between collector and emitter, C4 discharges through TR4 and D1. Notice that capacitor C5 is prevented from discharging quickly via D2.

Next time TR4 is cut off C5 charges a little more, and so on. In this way the emitter voltage of the unijunction transistor TR5, after some pulses, gets high enough to fire TR5. Capacitor C2 then discharges, and the process starts all over again.

This staircase voltage is further fed to the tone generator unit. This is simply a direct coupled amplifier stage with a regenerative feedback causing oscillation. The oscillation frequency depends on the base bias of TR6 taken from TR5 emitter via VR3. The base bias must not be too high and is adjusted by VR3, beginning with its maximum value and slowly reducing it until the tones are heard.

The circuit has many application possibilities, one being doorbell alarm. It is wise to mount the three units on separate boards, because all the units can be used separately.

\section*{Renny Skagestad, \\ Norway.}




\section*{CONVERSION TO 24 HOUR CLOCK SYSTEM}

WITH regard to your Digital Clock, here are one or two modifications that your readers may be interested in.

The first enables the Clock to be converted to read a 12 or 24 hours cycle when the alarm system is not being incorporated. As shown in Fig. 1, the counter for HOURS \(\times 10\) is made on SN7490, and the mode of the clock is changed by switching the inputs to RESET ZERO gates of the hours \(\times 1\) and HOURS \(\times 10\) counters.

Because the clock is to read both 12 and 24 hours, the hours \(\times 10\) Nixie is connected to the hours \(\times\) 10 decoder. The clock, therefore, reads at the recycle times 11.58-11.59-00.00-00.01 and so on, in the 12 hour mode and 23.58-23.59-00.00-00.01 in the 24 hour mode which means in the 12 hour mode the clock never reads 12.00 hours.

The second modification concerns the RESET facilities. The circuit shown in Fig. 2 enables the clock to be reset in faster time; also the clock can be held at a particular time in order that it can be
accurately set up. As can be seen, the circuit makes IC6 and SI redundant, but introduces more discrete components at four switches. The second half of ICl (IClb) is used as a three-frequency multivibrator, the individual frequences being switched by SI, S2 and S3 in Fig. 1. With all three in the closed position, the circuit does not oscillate, and therefore, when S 4 is in the RESET position, the clock receives no input pulses. With S 4 in this position, and S1 open the multivibrator oscillates at a frequency that charges the HoURS counter approximately once per second. With S2 open and S1 and S3 closed, the minutes \(\times 10\) counter changes approximately once per second. S3 performs the same function for the minUtes \(\times 1\) counter. This results in the clock being completely recycled in 55 seconds in the hour mode and 25 seconds in the 12 hour mode.
K. D. Brown,

Southend-on-Sea.



\section*{GLOBAL WEATHER STUDY}

With the launching of the French satellite EOLE a new step forward has been made in the expansion of meteorological studies. Satellites in the service of man are beginning to reap the harvest of space technology spin-off. It is interesting that the French have chosen a name which means "God of the Winds."
The satellite will gather data from as many as 500 free ranging meteorological balloons. The existing systems which have been so outstandingly successful in the case of the Nimbus satellites, gather mainly data from the higher levels, though some balloon interrogation is carried out.

Both Nimbus 3 and 4 which carried the interrogation, recording and location system was able to show its efficiency in tracking balloons, aircraft and other types of instrumental platforms.

The Omega position location equipment which was installed in the geostationary satellites ATS / and ATS 3 tracked balloons and buoys successfully.

The doppler system installed in EOLE is superior to the others in that they cannot cope with the same number of balloons. This satellite will take over in an area where expensive rocket methods have been used, namely the 30 to 60 km levels in the atmosphere.

The EOLE satellite weighs about 160 lbs and was designed, under the direction of Professor P. More] from the University of Paris, at the Centre Nationale D'Etudes Spaciales. It will occupy a 560 mile orbit with a 50 degree inclination to the equator. The orbital period is 103 minutes and the satellite will have a pattern of interrogation which will continue day and night.

The data will be stored until the satellite passes over a tracking station which will command the
telemetry at 136 MHz to release its store. The experiment is expected to last some 6 months.

The lifetime of the balloons used will vary from one to 5 months. These will be released by researches in the southern hemisphere at the rate of three a day from each of the stations at Mendoza, Neuquen and Lago Fagano.

The balloons, which are twelve feet in diameter, will drift at an altitude of 12,000 metres. Each balloon will carry a payload of instruments in a 32 ft long string which will consist of temperature and pressure sensors, together with batteries and solar cells. These will serve the receiver operating at \(464 \cdot 4864 \mathrm{MHz}\) and the 4 watt transmitter which will radiate on \(401 \cdot 71796 \mathrm{MHz}\).
It is expected that the satellite system will be able to locate a balloon to within 3 km .

\section*{ATLANTIC AIRLANE CONTROL}

In August an agreement was made between the United States government and ESRO (European Space Research Organisation). Ten countries are represented in ESRO and the agreement arranged through the FAA (Federal Aviation Administration) of America may well end the hazards that exist in the aircraft lanes.

At the present time the minimum separation limits are \(2,000 \mathrm{ft}\) vertical, 120 nautical miles horizontal and 15 minutes in longitude. At any one moment the accuracy of the known position is not better than ten miles. Using satellite methods the position could be known to half a mile.

In view of the amount of interference that can occur in the normal aircraft communication bands it is expected that the aircraft communication will be shifted to the L band ( 390 to 1550 MHz ). It has been tentatively suggested that the specification might follow this form: world wide coverage; accuracy 0.5 Nautical miles deviation to allow separation to be reduced to 30 nautical miles horizontal; \(1,000 \mathrm{ft}\) vertical; and 5 minutes longitudinal.

\section*{VIKING MISSION}

Some rather disturbing conditions are forecast as a possibility in the Martian atmosphere when the Viking spacecraft attempts the landing on Mars in five years time.

Cornell University has been making a study of the possibilities of high winds over the surface. It is difficult to forecast exactly what will happen for the meteorology can only be known from indirect methods.

The terrestrial experience does not help very much for the atmosphere on Mars is tenuous and a key factor is the height of the
atmosphere and mountain range height. On Mars the scale height is comparable with height of the mountain ranges over a distance of perhaps a hundred miles. The scale height (the point at which the pressure of the atmosphere falls by half) may have the changes of as much as ten miles in height and therefore be very much dependent on the topography.

Carl Sagan and Peter Gierasch have derived solutions to the problems of thermal winds and predict speeds of up to 250 mile per hour in some regions. This will dictate to a great extent where the spacecraft could safely land.

For certain technical reasons the landings have to be made within a limited equatorial belt and there are forbidden areas within these limits where the winds will be too high. Thus it means that regions of great scientific interest will not be suitable for a landing. One of these is the Hellas region.

The lowland flats will be the best choice for landings, but it would appear that the value of the scientific work will be reduced.

Last year there were a number of yellow clouds detected and these may well be dust swept up by very large gale force winds. Some of these lasted for several weeks.

It seems that there are new techniques to be perfected for the later manned landing and that the astronauts who visit will have new techniques to learn.

\section*{ASTEROIDS MAY HAVE MAGNETOSPHERES}

During the grand tour of the planets which is to be made in the late 70's the spacecraft used will traverse the asteroid belt. This lies between the orbits of Mars and Jupiter.

There are many hundreds of these minor planets and it may well be that the probes will pass in the vicinity of one of the larger ones. If this should be so then there may be effects on the instruments carried, particularly the magnetometers.

It is known that none of the asteroids have an atmosphere but it is possible that they have a magnetosphere. The magnetosphere is the zone of magnetic influence round a body which acts as a barrier to penetration by the fast charged particles in the solar wind.

It appears that the solar system has a small residual magnetic field and therefore an asteroid could have a low surface magnetism. If this magnetism were as low as one thousandth of that of the earth then a magnetosphere could exist.

The magnetosphere extends a considerable distance from the body it encloses (the tail of the Earth's magnetosphere extends as far as the Moon) so that a wide pass could yield some data.

\section*{CHARACTER RECOGNITION 1971}

\section*{Published by the British Computer Society 212 pages, \(8 \frac{1}{4}\) in \(\times 5 \frac{3}{4} \mathrm{in}\). Price \(\mathbf{E 2}\)}

THIS is an up-dated version of the handbook originally published in 1967. It is intended to assist the layman in his comprehension of character recognition; particularly those who may wish to discuss the techniques and possibilities with manufacturers of reading machines.

Physical and optical properties of paper, printing methods, the design of alphabetic and numeric characters and symbols that are suitable for automatic reading by machines are described. Optical mark reading (OMR); magnetic ink character recognition (MICR); and optical character recognition (OCR) techniques are all explained and the text is well illustrated with excellent diagrams. The variety of electronic systems employed in OCR is impressive: after the mechanical scanner (Nipkow disc), come laser-beam, flying-spot, Vidicon, and photocell matrix scanners. This portion of the book offers a good, concise technical introduction to the subject for the general reader.

Proprietary equipment and services are reviewed in the final chapter. This will be most valuable to potential buyers or users of such commercial equipment.
F.E.B.

\section*{MICROWAVE SEMICONDUCTOR DEVICES}

\section*{By H. V. Shurmer, PhD, CEng, FIEE. \\ Published by Pitman Publishing.}

\section*{223 pages, \(8 \frac{1}{4}\) in \(\times 6\) in. Price \(\mathbf{E 2} 25\)}

THIS is one of an Electronic Engineering Series of monographs written at a level ranging from undergraduate to postgraduate and professional standard. It is therefore, a specialist's book. It deals with certain types of semiconductor devices which are employed in the rather rarified regions of the frequency spectrum remote and foreign to most laymen, but where much professional activity is taking place involving radar, telemetry, and instrumentation applications, for industrial and defence requirements.

A brief outline of the history of origin, or development of the particular device is given at the commencement of each chapter. The theory of operation is treated concisely, but in some depth with extensive recourse to mathematical proof, the level (as stated by the author) being suitable for students on an engineering degree course. It goes without saying that the usefulness of this authoritative work will extend even further, to others with serious interest in this rather specialised area of electronics.
The scope of the book is best indicated by listing the devices described (each having one chapter): Point-contact, varactor, Schottky-barrier, tunnel, backward, pin, Gunn effect, and avalanche diodes, transistors, and finally, integrated circuits, an area still in its infancy--in microwave terms-but holding out interesting possibilities for the future.

\section*{TRANSISTOR CIRCUIT DESIGN TABLES}

By David S. Taylor, M.A. (Oxon), Ph.D. Published by The Butterworth Group \(\mathbf{I} 20\) pages, 9 in \(\times 6\) in. Price \(\mathbf{6 2 . 8 0}\)

WHEN first seeing the title of this book, then reading the publisher's blurb on the jacket, one would naturally expect to find a great deal of information on the various basic transistor building block circuits. The Preface goes on to tell us how the material is a direct reprint from data derived from computer calculations. Discrepancies, we are told, may be as high as +20 to -30 per cent of the indicated values due to variations in transistor characteristics.

I used these tables in a test case, in which only one line of figures was required. It can be concluded that the value of the book as a whole is minimal since a great deal of the data given is seldom likely to be used. It is like choosing one or two ties from a shop full of ties of different kinds. The designer is rarely likely to require more than basic information on circuit values for only a couple of supply parameters.

One must credit the author with the effort involved in collecting all this data, but for the price of the book I personally do not consider this a "value-formoney" buy. If, however, the designer requires to use this information, a quick peep at the book in a library will be a great help to him.

Probably the most useful chapter is that on Schmitt trigger circuits, but capacitor and inductor reactances are more easily assimilated from nomograms or abacs. Parallel and serjes resistor and capacitor calculations involve basic arithmetic and excellent approximations can be achieved by mental calculattion.

The other three chapters on common emitter amplifier stages (restricted to somewhat outdated RC coupling) and multivibrators are useful and relevant to the title.

\section*{M.A.C.}

\section*{COLOUR TELEVISION THEORY}

By G. Hutson

\section*{Published by McGraw-Hill Ltd}

326 pages, IOin \(\times 7 \frac{1}{2}\) in. Price \(\mathbf{6 3 . 8 5}\)

THIS is a very well prepared textbook on colour television engineering embracing both the PAL and NTSC systems, but with the emphasis on PAL. As is the wont of most textbooks, this is particularly aimed at those students who are preparing for examinations which include colour television principles, particularly those offered by the City and Guilds of London Institute and the Radio Trades Examinat tion Board.

The fact that the use of mathematics is small will no doubt induce lay readers with a working knowledge of monochrome television principles, to invest in this, for not only is it an excellent tutor but a valuable reference.

Commencing with chapters on the physics of light and colour television signals, the book goes on to analyse the various receiver sections that makes reception possible.

The book is very well illustrated with a 14 -page index that makes reference a very easy business.
F.E.B.


Our nearest neighbour the Andomeda Nebula. It resembles our own galaxy and has enabled astronomers to make a more accurate model of our galaxy. It is about 200,000 light years in diameter and is about \(2,200,000\) light years distant from our golaxy. Its number is M3I and is one of the nebule that is visible to the naked eye on a clear night and easily seen through modest binoculars.

\section*{TECHNIQUES}

|N this part the various pieces of equipment from the aerial system to the recorder will be brought together to form the radio telescope. The setting up of the receiving system will be covered in some detail. much of which may be familiar to some readers. However, this is a very necessary step for the newcomer and those more experienced can go straight to the setting up in their own way.

In order to check each stage certain test equipment is desirable. One test unit which would be of great help is a signal generator of good standard. If this is not available then the next best thing is to make up a noise generator and use this to provide a setting-up signal. This presupposes that some means will be available to set the correct frequencies which are to be used. The nominal operating frequency of this telescope has been set at 137 MHz . It is essential therefore that both the pre-amplifier and the converter are centred on this frequency.

\section*{NOISE GENERATOR}

A suitable noise generator may be made up quite simply and a diagram of a suggested circuit is shown in Fig. 6.1. It is possible to purchase noise generators on the surplus market at reasonable prices and they have the advantage of being calibrated. However, the simple one that is described will serve the purpose very well.

For the sake of making an alternative available that is within the ability of the constructor, a valve diode circuit is shown in Fig. 6.2. It must be pointed out that in the case of the valve diode its life is
limited and that if this unit is made up, the time in use at maximum noise should be kept to a minimum.

Either of these noise generators can be used to measure the noise factor of a receiver or amplifier, although this is not the purpose in this case. It will be used in order to ensure that each unit in the chain of apparatus is operating under optimum conditions.

\section*{LOW RESISTANCE RECORDER}

Certain alternative methods of recording have been given, so the order of setting up will vary slightly accordingly.

Taking the simplest of the arrangements, that of connecting a low resistance recorder directly to the cutput transformer of the receiver final stage, the procedure will be as follows.

Switch on the converter and the communications receiver and let them warm up for about 20 min . Connect the recorder in parallel with the loudspeaker. Disconnect the output from the converter to the receiver.

Set all gain controls at maximum while watching the pen on the recorder. If this goes to full scale before the controls are at maximum, reduce the a.f. gain control progressively while increasing the r.f. control. If the a.f. control is at a point less than 50 per cent of its travel then reduce the r.f. control till the a.f. gain can be set at the halfway point.

The loudspeaker may now be disconnected after reducing the pen position to half scale by the con-

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trols on the receiver. If the sensitivity available is such that the loudspeaker needs to be in parallel all the time, then to avoid causing disturbance by the continual hiss of the speaker, a simple muting arrangement of switching in a dummy load resistor in place of the loudspeaker can be used.

The case of high receiver noise level has been covered so far. The other case, that of the quiet receiver, which incidentally is the more desirable, a different technique is required. If the recorder does not respond to full scale with the a.f. control at the halfway mark and the r.f. gain at maximum, then a short piece of wire connected to the aerial input socket of the receiver should give sufficient noise to enable the sequence to be followed.

\section*{OTHER TYPES OF RECORDER}

Having dealt with the simplest form of recorder connection, the alternative arrangements discussed in the previous article for connection to the receiver cutput stage will now be covered. In the case of the special winding on the output transformer, this will accommodate a high resistance order. The sequence of the setting up procedure will be identical with that for the low resistance recorder.

Where the potentiometer system in the output stage is used there will be the additional control which sets the recorder level, whether this be high or low resistance coil. The same conditions apply,


Fig. 6.I. A simple noise generator using a solid state diode. In raising the noise level by increasing the voltage it will be noticed that the noise increases and then passes through a decreased level finally rising again. As this generator is being used for testing only, any convenient noise point may be used


Fig. 6.2. An alternative noise generator circuit, using a valve diode. Care should be exercised when using this type of circuit because the life of the diode is not much in excess of 500 hours. For that reason it should be used at the lowest level consistent with the test being made


Fig. 6.3. A receiver tuning test recorded on the chart for reference purposes
that is to say the r.f. and a.f. controls are set as previously described, with the additional advantage of varying the sensitivity of the recorder.

In both these cases the muting of the loudspeaker using the switching network will apply.

\section*{USING D.C. AMPLIFIERS}

When d.c. amplifiers are employed, a similar procedure so far as the setting up of the receiver is concerned will be followed, but before connecting the recorder in the circuit the d.c. amplifier will need to be balanced as follows.

In place of the recorder insert a milliammeter. Set this at the 10 mA range to begin with. The pointer should be set at midscale by adjusting the controls and the meter brought to the lower current settings until the halfscale reading is the same as that for the recorder. In general this will be 0.5 mA since most recorders will be of the \(0-1.0 \mathrm{~mA}\) fullscale type.

Having set up the d.c. amplifier, it may be connected into the receiver and checked before replacing the meter with the pen recorder. Again the same sort of procedure will be followed. In the case of the rather more complicated amplifier a greater sensitivity will be available, so this needs to be taken into account.

\section*{ADDING IN THE CONVERTER}

The next step is to connect the converter to the receiver and to reduce the r.f. gain until the recorder is at the same level as in the first setting-up using the receiver alone. A check can be made at this point to see if the receiver has been set to the correct i.f. frequency. It is assumed that the converter has been checked for its mid-point frequency of 137 MHz .

With no aerial connection to the converter, the tuning of the receiver can be adjusted slightly to each side of the i.f. frequency to see if the noise level falls equally. If the wideband system of the receiver's own i.f. transformers shows two humps a visual and audio adjustment will perhaps be necessary. The correct tuning will be for the receiver tuning to be set midway between humps. This will show'a slight rise of the pen level on each side of the datum. Let this fact be borne in mind for all subsequent checks. A note made on the test chart showing all three points would be useful. See Fig. 6.3.

\section*{ADDING THE PRE-AMPLIFIER}

The pre-amplifier (without the aerial connected) is now linked with the converter. There will be a rise in the noise level and the first adjustment will be made to the receiver r.f. gain control so that once again the recorder pen is at its datum.

If there is so much gain in noise that additional reduction is required at the a.f. gain control, it may well be that the inherent noise of the amplifier is too high. In order to check this connect the aerial to the pre-amplifier. If there is a rise in noise then all is well. If there is no detectable difference then the internal noise of the system is too high.

Before opening up the pre-amplifier make the following recheck. Set the controls so that the pen recorder has a tracing which is clearly one of varying noise. Feed in the noise generator at the aerial input of the pre-amplifier-which should be brought into the vicinity of the other apparatus. Set an optimum noise level with the noise generator "on". Note the reading and then disconnect the generator. Note the fall in noise level and if this is substantial it will establish that the system is all right but that somewhere there is an overload condition arising. This may be because the a.g.c. circuit is over sensitive.

It is better that there should be no a.g.c. applied when the system is used as a telescope. It may be necessary to interpose between the amplifier and the converter some form of attenuator, or it may be that this is needed between the converter and the receiver. This will have to be a matter of empirical investigation.

In the other case, where no change of level is noted when the noise generator is used, then the units must each be checked for noise level. For this purpose, of course, the noise generator can be used. No doubt some form of audio amplifier with a diode detector will be available and this can be used to check the noise level of the pre-amplifier.

\section*{INTO PRACTICE}

Having set up the system and checked its operation, a note should be made of the positions of all controls. As the time constants at the recorder sections are long it might appear that the whole system is not working. To check this (in the case of recorders being connected directly to the output stages) a pair of phones or the loudspeaker kept in operation for final setting up will indicate the sensitivity of the system.

The reason for using the long time constants is to remove the high level random noise peaks of short duration and also the modulated transmissions which might appear from time to time. To appreciate this perhaps a few words of explanation are required.

The noise that is received by the aerial is randomly distributed but contains in its spectrum some coherent noise from extra terrestrial sources. Over a period of time the random noise will tend to cancel itself out but the coherent noise will over the period of time show a level which is higher than the purely random noise. To this is added the random noise of the aerial itself and that of the system to which it is connected.

Using a long time constant, the coherent noise tends to assume a noticeable level because the purely random noise cancels itself over the period of integration. In the case of this telescope, 4 seconds and 8 seconds approximately have been chosen as
integration times. This will be satisfactory for most purposes and for the early stages of this project.

\section*{MONITORING ARTIFICIAL SATELLITES}

When using the telescope for the monitoring of artificial satellites, there will be no need to change the time constant on the recorder unless the details of the telemetry are required. The automatic picture satellites (APT) used for meteorology will register a signal on the chart, but if actual picture reception is contemplated then the receiver will be quite different. A picture receiver needs to be a frequency modulated unit and a crystal controlled oscillator is essential.

Everything is now ready for the first observations. Each of the three positions of the telescope will require a change of altitude. To ensure that the same position is located each time, it is a good idea to make or buy a protractor. This can be fitted to the end of the reflector and with a suitable plumb bob the exact position repeated at each change.

If the telescope is to be used for satellite tracking then it is best to turn the aerial upwards so that the aperture points to the zenith. Most satellite passes will then be recorded, though any that are low, near the horizon, and cross on short arcs may not be detected.

\section*{TYPES OF SOLAR BURSTS}

In the previous article some elementary information regarding the sun was given so that some elements of the observations would become clearer. A brief description will now be given of the types of solar bursts that may be recorded during the observations. The types of burst are classified by numbers, each group having some special characteristic. The centres of activity are the disturbed regions and to give a basis of understanding the schematic diagram in Fig. 6.4 should be borne in mind.


Fig. 6.4. Solar bursts. Diagram of a centre of radio activity on the sun

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Fig. 6.5. Active ("radio") sun, showing concentration of high level activity

A centre of activity is visually observed as a sunspot. However the activity begins before the appearance of the actual spot and also continues atter. During this time many changes of radio activity are observed. A magnetic field develops and it is as though a giant magnet lies beneath the surface of the photosphere. Where the field pro-
trudes through the chromosphere, the gas is made to glow and the hydrodynamic waves travel up the magnetic lines and produce bright streaks known as facula. The corona is also heated. It is after this phase that the actual sunspots appear.

The sunspots appear dark against the surface because they are at a slightly lower temperature. They are an indication of where the greatest magnetic concentration crosses the photosphere. Above the spots there is great activity. A great intensity of gas clouds occur high up in the corona: these are the prominences and are supported in their positions by the magnetic field.

During the time of the spot the major activity eften results in flares. Although the flare is only an increase of intensity of line emission, the results are extensive. A terrific explosion may result with far reaching effects. A vast cloud of gas is ejected and drags the magnetic field with it. The gas and the magnetic field reach the earth about a day or so after, causing magnetic storms and aurora. A picture diagram of the radio sun is shown in Fig. 6.5.

Type I bursts do not follow closely after at flare but are nevertheless very important because the effect of such a burst lasts for a whole day. They are only found in the metre wave part of the spectrum, mostly between 100 and 150 MHz . During such a storm there appear short bursts of great intensity that last only a few seconds. The trace that appears on the long time constant will not normally register these. They need a much higher recorder speed.

Type II bursts usually appear with very intense outbursts and are often associated with and follow Type 111 bursts. These are both the result of special


Fig. 6.6a, b. Recordings of the sun. Two examples of noise storms with random bursts and showing varying amplitude due to Faraday rotation


Fig. 6.7a Pen recording of a satellite and Cassiopeia. b Recording of two satellite passes
and fast moving disturbances in the corona resulting in the bunching of electrons.
Type IV bursts have a broad spectrum and show a high temperature. They follow after Type II bursts and seem to be a continuum.

Not so much is known about Type \(V\) bursts, but they may be similar in nature. Usually this activity is more noticeable at much higher frequencies and much remains to be done before the phenomena is fully understood.

\section*{OBSERVATIONS}

It is now time to make the observations, and to
help in recognising the results, the pen recordings in Figs. 6.6 and 6.7 are given as a guide.

It would be a good plan to do a three- or fourdays run in the noon period so that the observer becomes familiar with the appearance of the charts. Having found that the results are satisfactory, the full observations may then be undertaken.

The next article will deal with the extension of the simple telescope to form an interferometer. Details of the additional equipment that is required will be given so that the benefits of greatly increased sensitivity and resolving power can be obtained.

\section*{RETROSPECT AND PROSPECT} continued from page 889
After careful thought we have decided upon a solution. We are convinced there are many people who would like just to dabble without becoming too deeply involved in the subject. At the same time, there are endless possibilties using only simple and modest circuits for creating gadgets and items of real practical worth in all manner of everyday affairs. Designs for such gadgets ought to be even more widely disseminated than they are at present; and of course presented in a form to suit the person with limited experience. Also, the novice needs particular consideration and help.

We feel that such needs warrant the creation of an additional magazine-independent, yet having a certain association with Practical electronics. So a new popular magazine, entitled Everyday Electronics, is due to make its bow next week. Our new companion will augment the service that Practical

Electronics' already provides, and will, we trust, encourage many more people to make their very first entry into this exciting branch of technology. And in a practical purposive manner, of course.

When our readers have examined a copy of this new magazine, we are sure they will wish to recommend it to many of their friends and acquaintances, as well as to their sons and other younger relatives.
Truly it can be said that electronics is a subject with many facets, and each facet seems to be taking on a different or certainly a broader countenance as the years go by. It is a challenging task, but Practical Electronics will continue to cover this expansive subject in the best manner to suit those tens of thousands of keen and serious devotees electronics has attracted. We like to feel that many of these followers were first introduced to electronics through this magazine, sometime during the last seven years.
The prospect looks good-and exciting.
F.E.B.


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All items advertised in September issue of Practical Electronics still available. Special Prices for quantity.

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}

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\title{
Ridadart A SELECTION FROM OUR POSTBAG
}

Correspondents wishing to have a reply must enclose a stamped addressed envelope. We regret we are unable to guarantee a reply on matters not relating to articles published in the magazine. Technical queries cannot be dealt with on the telephone.

\section*{Trial by Fury}

Sir-For unmentionable years I being of almost sound mind have read \(P\).E., in fact I have that many that my wife gave me an ultimatum, either my P.E.'s go or she does. I might add that I miss her.

Now the thing that's worrying me is "why"?

Why is it that no matter how you plan a circuit, the transistors almost inevitably end up with the tails all but tied in a granny knot.

Why when one buys a packet of assorted resistors or capacitors after ten years you still have them around. Why is it that your transistor collection, considered by friends to be so, well planned an assortment, never contains the ones you want for a new circuit you fancy.
Why is it that, no matter where you put the soldering iron, the smell of burning sleeve or flesh is ever present. Why is it that the wife never appreciates the new gadget you've built even though you have offered to pay for a new tablecloth (it's only a small hole).

Why is it that even if you've successfully built a multi-frequency astable-bistable double switched stereophonic thingumy with a.g.c. at all levels, the main topic of conversation with visiting friends is the Browns' new baby.

Why is it that friends consider your life should be spent repairing Japanese transistor radios, you spend three hours taking it out of the case, two hours finding a substitute transistor, another four hours putting back the guts and the run is usually ten fags and the remark that he thought it was only the battery.

Is it worth it, or should I give it all up? By the way, do you publish a book on Practical Knitting?
R. G. Taylor,
Birmingham.

\section*{Any offers!}

Sir-I wonder if any reader or designer can help with the following project.

I am chairman of the Grimsby Group Hospitals Sports and Social Club, and since music and electronics are my hobbies, I am usually responsible for playing, organising
music and purchasing or making amplifiers.
The sports club was founded just after the N.H.S. was formed and is run on a subscription basis; assets are obviously very limited.

During the past twenty years, rooms that used to be available for activities, in the local hospitals, have been swallowed up for other essential purposes. However, some twelve months ago we were given a disused old ward block. With our capital and voluntary labour from members, we have altered this building to our requirements, having used almost all our money.

Certain members have donated different items (e.g. piano, psychedelic lighting, etc). I have supplied a tape recorder, built a sound system and even installed my electronic organ.
We are, however, very much in need of an auto-rhythm unit, but find these far too expensive for us to purchase. I have constructed drum units for contact (pedal) sounding for the organ-these work well. However, although I know that autorhythm units must be driven by pulses from a binary ring counter logic I cannot devise one myself.

I wonder if any of your readers can help with this project. Other items of less importance, e.g. echo, would be useful.
E. C. Darnell,

Waltham, Grimsby.

\section*{How about it!}

Sir-I would like to say a few words, through your magazine, aimed at manufacturers and suppliers.

Now that D.I.N. connectors are becoming more popular and standard on most equipment nowadays, how about making 5 -core cable readily available, and 4 -core individually screened cable at least a vailable, if not readily available.
A few words also, to other users.

How about creating a demand for these cables by using them whenever you make up D.I.N. leads. It's cheaper in the long run, instead of making up dozens of different. single twin-core leads.

> R. Williams,

\section*{Sparking power unit!}

Sir-Your Editorial on electronics in motor cars was timely and "enthusiastic, without being at all "Beyond the Fringe"-no disrespect to Gerry Brown!
But the most telling point was "even the magic of electronics cannot save the internal combustion engine from ultimate extinction." I have for many years championed the cause of electric cars, and have urged the British car companies to do something. Only amateurs (as in radio's early days) appear to be doing anything.

Ten years ago, we were well ahead, and I made a forecast then that the first commercial electric car would be Japanese or European or American. How can we expect an electric car from this country when the designers haven't yet heard of electronics?

Readers of P.E. must surely wince at a power unit which needs oil, petrol, sparks, air, water and grease pumped to it in sequence, all to drive four captive cannonballs, which drive a bent piece of metal, which turns a cog, which . .

Over the years I have written to practically every newspaper and magazine trying to promote an Electric Car Rally, but with no takers.
E. A. Wadsworth,

Scarborough.

\section*{BACK NUMBERS}

We regret that back numbers of Practical Electronics can no longer be supplied. We are conscious that many readers frequently require reference to past projects and in order to go some way toward helping them we are prepared to devote a limited amount of editorial space to announcements of readers' requirements. We will try to publish these (without a guaranteed date) free of charge on the following conditions:
I. The announcement must be restricted to issues of Practical Electronics only that are required.
2. Any communication regarding any announcement should be addressed to the advertiser and not to this office.
3. The Editor cannot enter into correspondence on matters relating to back numbers, nor can he accept any money, postal orders, cheques or postal reply coupons in connection with any sale of back numbers of Practical Electronics.
4. Advertisers should send full name, permanent address and dates of issues required to the Editor, Practical Electronics, Fleetway House, Farringdon Street, London EC4A 4AD.
Finally, it is worth remembering that several public libraries hold copies of Practical Electronics and indexes for reference. Better still, make sure of getting a copy in future by placing a regular order with your newsagent now.


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Approximately 300 micro Tape Recorders, ete sto type dual coloured dial. 50 p


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tumes. Price \(\& \mathbf{j}\). P. \& . 22p.

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ins easy to build Projects. No solder ns, no special tools required. The Transformer Speaker, Meter, Relay components and a 56 -page inst other leafler. Some examples of the 50 possible Projects are: Sound Level Merer, 2 Transistor Radio. Amplifier etc. Price \(\mathbf{4 7} 7 \mathbf{7 5}\). P, \& P, 30p.

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Extremely powerful with approx. 141b. pull, I" travel. Fitted with mounting feet
Sire: 4" long 2年" wide,
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All Types (and Spares)
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100 WATT. \(10 h m, 10 \mathrm{~A} ; 5 \mathrm{ohm}, 4.7 \mathrm{~A}\). \(10 \mathrm{ohm}, 3 \mathrm{~A}_{i} 25 \mathrm{ohm}, 2 \mathrm{~A}: 50 \mathrm{ohm}, 1-4 \mathrm{~A}\); 100 ohm, \(1 \mathrm{~A}: 250\) ohm; \(0.7 \mathrm{~A} ; 500\) ohm;,\(~\)
\(0.45 \mathrm{~A} ; 1 \mathrm{k} \Omega, 280 \mathrm{~mA} ; 1.5 \mathrm{k} \Omega, 230 \mathrm{~mA} ; 2.5 \mathrm{k} \Omega, 2 \mathrm{~A}: 5 \mathrm{k} \Omega, 140\)
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Build a Strobe Unit, using the latest type Xenon white light flash tube. Solid state timing and triggering EXPERIMENTERS' ECONOMY KIT
Speed adjustable 1 to 36 Flash per sec. All electronic components including Veroboard S.C.R. Unijunction NEW INDUSTRIAL KIT
Ideally suitable for schools, laboratories, etc. Roller tin printed circuit. New trigger coil, plastic thyristor HY-LYGHT STROBE MK III
This strobe has been designed and produced for use in large rooms, halts and the photographic field, and printed circuit for easy assembly, also a special trigger coil and ousput capacitor. Speed adjustable \(0-30\) f.p.s. Light output approx. 4 joules. \(\& 12 \cdot 00\) P. \& \(P\). 50p. METAL CASE. Including reflector. \&4.00 P. \& P. 45p.
AND NOW!

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- Heavy duty power supply.
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gives fabulous effects with colour filters.
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\hline 600 & 18-32 & \(4 \mathrm{c} / \mathrm{O}\) & \(78{ }^{\prime \prime}\) & 2,400 & 30-48 & \(4 \mathrm{c} / \mathrm{O}\) & 50p \\
\hline 700 & 16-24 & 4M2B & 63p* & 5,800 & 40-70 & \(4 \mathrm{c} / \mathrm{o}\) & 63 p * \\
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\hline \multicolumn{8}{|l|}{(1) Coil ohms: (2) Working d.c. voles; (3) Contacts; (4) Price (HD) Heavy Duty. All Post Paid.} \\
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230 V a.c. coil \(3 \mathrm{c} / \mathrm{o}\). 10 amp a.c. contacts, 50 p plus 8 p P. \& P .
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The MPR 3065 is a communications receiver and entertainment source in one neat, transistorised, portable package. Features a colour coded illuminated tuning dial and band selector, AFC, squelch, BFO (optional extra), large speaker, Ext. Aerial Socker. Works off mains or batteries. Size: 10tin
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\section*{new}

\section*{Super IC-12}


\section*{HighfidelityMonolithic Integrated Circuit Amplifier}

Two years ago Sinclar Radionics announced the World's first monolithic integrated circuit \(\mathrm{Hi}-\mathrm{Fi}\) amplifier. the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12.
This 22 trarsistor unit has all the virtues of the original \(I C .10\) plus the following advantages:
1. Higher power.
2. Fewer e>ternal components
3. Lower quiescent consumption.
4. Compatible with Project 60 modules.
5. Specially designed bult-in heat sink. No other heat sink needed.
6. Full output into 3.4 .5 or 8 ohms
7. Works on any voltage from 6 to 28 volts without adjustment.
8. NEW 22 transistor circuit.

Output power 6 watts RMS continuous (12 watts peak).
Frequency Response 5 Hz to \(100 \mathrm{KHz} \pm\) 1 dB .
Total Harmonic Distortion Less than \(1 \%\) (Typical 0.1\%) at all output powers and all frequencies in the audio band.

Load Impedance 3 to 15 ohms.
Power Gain 90dB (1.000,000.000 times) atter feedback.

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Size \(22 \times 45 \times 28 \mathrm{~mm}\) includıng pins and heat sink.
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With the addition of only a very few externa resistors and capacitors the Super IC. 12 makes a complete high fidelity audio amplifier suitable for use with pick-up. F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radıos, oscillators etc. The very low quiescent consumption makes the Super IC. 12 ideal for battery operation.


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The easy way
to buy and
build
Project 60


Project 605 is one pack containing: one PZ5, two Z30's. one Stereo 60 and one Masterlink This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with nea: little clips to plug straight on to the modules Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become avallable adapted to the Project 605 method of connecting.
Complete Project 605 pack with \(£ 29.95\)
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Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.
Performance characteristics are so good they hold their own with any other available system irrespective of price or size.
Project 60 modules are more versatile - using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages. there remains the most attractive of all - price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

Typical Project 60 applications
\begin{tabular}{|c|c|c|c|}
\hline System & The Units to use & together with & Cost of Units \\
\hline Simple battery record player & 2.30 & Crystal P.U.. 12 V battery volume control & ¢4.48 \\
\hline Mains powered record player & 2.30, PZ.5 & Crystal or ceramic P U. volume control etc. & ¢9.45 \\
\hline \(20+20 \mathrm{~W}\). stereo amplifier for most needs & \[
\begin{aligned}
& 2 \times 2.30 \text { s, Stereo } 60, \\
& \text { PZ. } 5
\end{aligned}
\] & Crystal, ceramic or mag. P.U., F.M. Tuner, etc. & £23.90 \\
\hline \(20+20 \mathrm{~W}\). stereo amplifier with high performance spkrs. & \[
\begin{aligned}
& 2 \times \mathrm{Z.30s}, \text { Stereo 60, } \\
& \text { PZ.6 }
\end{aligned}
\] & High quality ceramic or magnetic P.U., F.M. Tuner. Tape Deck, etc. & £26.90 \\
\hline \begin{tabular}{l}
\(40+40\) W. R.M.S. \\
de-luxe stereo amplifier
\end{tabular} & \(2 \times Z .50\) s, Stereo 60 PZ.8, mains trsfrmr & As above & £34.88 \\
\hline Indoor P.A. & \begin{tabular}{l}
2.50, PZ.8, mains \\
transformer
\end{tabular} & Mic., gultar, speakers, etc., controls & £19.43 \\
\hline
\end{tabular}

\footnotetext{
F.M. Stereo Tuner ( \(\mathbf{( 2 5 )}\) \& A.F.U. Filter Unit ( \(\mathbf{( 5 . 9 8 )}\) ) may be added as required.
}

\title{
from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules
}

\section*{Z. 30 \& Z. 50 power amplifiers}


The \(Z .30\) and \(Z .50\) are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Totai harmonic distortion is an incredibly low \(0.02 \%\) at full output and all lower outputs. Whether you use \(Z .30\) or \(Z .50\) amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well. SPECIFICATIONS ( 2.50 units are inter-
changeable with 2.30 s in all applications). Power Outputs
2.3015 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. Into 3 ohms using 30 volts. 2.5040 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts. Frequency response: 30 to \(300.000 \mathrm{~Hz} \pm 1 \mathrm{~dB}\). Distortion: \(0.02 \%\) into 80 hms .
Signal to noise ratio: better than 70 dB unweighted. Input sensitivity: 250 mV into 100 Kohms . For speakers from 3 to 15 ohms impedance.
Size: \(14 \times 80 \times 57 \mathrm{~mm}\).
2.30

Built, tested and guaranteed with circults and instrucuons manual.
£4.48
2.50
with circuits and instruc.
Built, rested and guaranteed with circu
tions manual.
\(\mathbf{~} 5.48\)

\section*{Project 60 Stereo F.M. Tuner}


First in the world to use the phase lock loop principle

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils. an I.C. in the specially designed stereo decoder and squelch circuit for stlent tuning between stations Good reception is possible in difficult areas, and often a few inches of wire are enough for an aertal. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.
SPECIFICATIONS-Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz . Capture ratio: 1.5 dB . Sensitivity: \(2 \mu \mathrm{~V}\) for 30 dB auieting: \(7 \mu \mathrm{~V}\) for lock-in over full deviation. Squelch level: \(20 \mu \mathrm{~V}\). A.F.C. range; \(\pm 200 \mathrm{KHz}\). Signal to noise ratio: \(>65 \mathrm{~dB}\). Audio frequency response: \(10 \mathrm{~Hz}-15 \mathrm{KHz}\) ( \(\pm 1 \mathrm{~dB}\) ). Total harmonic distortion: \(0.15 \%\) for \(30 \%\) modulation. Sterso decoder operating level: \(2 \mu \mathrm{~V}\). Cross talk: 40 dB . Output voltage: \(2 \times 150 \mathrm{mV}\) R.M.S. Operating voltage: 25-30 vDC. Indicators: Power on/tuning/stereo. Size: \(93 \times 40 \times 207 \mathrm{~mm}\).
£25

\section*{Stereo 60 Pre-amp/control unit}


Designed for Project 60 range but suttable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-nose ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.
SPECIFICATIONS—Input sensitivities: Radio -up to 3 mV . Mag. p.U. 3 mV : correct to R.IA.A curve \(\pm 1 \mathrm{~dB}: 20\) to 25.000 Hz . Ceramic p.u. - up to 3 mV : Aux -up to 3 mV . Output: 250 mV . Signal to noise ratio: better than 70 dB . Channel matching: within 1 dB . Tone controls: TREBLE +15 to -15 dB at 10 KHz : BASS +15 to -15 dB at BOOHz . Front panel: brushed aluminium with black knobs and controls. Size: \(66 \times 40 \times 207 \mathrm{~mm}\).
Built tested and guaranteed.

\section*{A.F.U. High \& Low Pass Filter Unit}


For use between Stereo 60 unit and two 2.30 s or 2.50 s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid ( 12 dB /octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages - rumble (high pass) and scratch (low passi. Supply voltage -15 to 35 V . Curfent - 3 mA . H.F. cut-off ( -3 dB ) varable from 28 KHz to 5 KHz . L.F. cut-off ( -3 dB ) varrable from 25 Hz to 100 Hz . Distortion at 1 KHz ( 35 V . supply ( \(0.02 \%\) at rated output. Size: \(66 \times 40 \times 90 \mathrm{~mm}\).

Built tesfed and guaranteed.
£5.98


\section*{Sinclair Q16/Micromatic}

\section*{Q16 High fidelity loudspeaker}

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design. technical journals have justly compared the 016 with much more expensive loudspeakers. Its shape enables the 016 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies without loss

This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

\section*{Specifications:}

Construction: Special sealed seamless sound or pressure chamber with internal baffie.
Loading : up to 14 watts RMS.
Input Impedance: 8 ohms.
Frequency response: From 60 to 16,000
Hz . confirmed by independently plotted B and K curve.
Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special cone suspension for excellent transient response.
Size and styling: 9录 in. square on face \(x\) \(4 \frac{3}{4} \mathrm{in}\). deep with neat pedestal base. Black all over cellular foam front with natural solid teak surround.
Price f8.98.

\section*{Britain's smallest radio}

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver brilliantly designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading from distant stations: bandspread at higher, frequencies makes reception of Radio 1 easy. The plug-in magnetic earpiece provided, matches the Micromatic's output to give wonderful standards of reproduction. Everything including the special ferrite rod aerial and batteries is contained within the minute attractively designed case. Whether you build a Micromatic kit or buy this amazing recerver ready built and tested, you will find it as easy to take with you as your wrist watch, and dependable under the severest listening conditions.

\section*{Specifications:}

Size: \(36 \times 33 \times 13 \mathrm{~mm}(1.8 \times 1.3 \times 0.5 \mathrm{in}\).) Weight: including batteries, 28.4 gm (1 oz.)
Case: Black plastic with anodised aluminium front panel and spun aluminium dial.
Tuning: medium wave band with bandspread at higher frequencies \(\langle 550\) to \(1,600 \mathrm{KHz}\) ).
Earpiece: Magnetic type.
On/off switching: By inserting and withdrawing earpiece plug.
Kit in pack with earpiece, case, instructions and solder \(£ 2.48\).

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Sinclair Radionics Ltd., London Rd, St. Ives Huntingdonshire PE17 4HJ.
Telephone St. Ives (048 06) 4311

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\(100 \mu \mathrm{~A}\)


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\(\Omega .-20\) to +48 dB. R. -20 to +46 dB .
88.87. P. P .121 p .
 MODEL 500 r 20,000
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\(250 / 500 / 1.000 \mathrm{Vd.c} .0 / 2 \cdot 5 /\)
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58.87 f - Post pald.
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OPV d.c. S/Volta, OPV d.c. 5/Volt a.c.
D.c. volts: \(0.5,2.5\). A.c. Volts: \(3,10,60,250,500,1,000 \mathrm{~V}\) D.c. current: \(10,100 \mu \mathrm{~A}, 10,100,500 \mathrm{~mA}\) \(2.5,10 \mathrm{~A}\). Resistance: \(1 \mathrm{~K}, 10 \mathrm{~K}, 100 \mathrm{~K}\) \(10 \mathrm{meg}, 100\) meg. Decibels: -10 to
+49 dB . Platic case with carrying handle. +49dB. Platic case with carrying handle,
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\(270^{\circ}\) WIDE ANGLE


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\(1,000 \mathrm{~V}\) a.c. \(0 / 50 \mu \mathrm{~A} / 2 \cdot 5 \mathrm{~mA}\)} \begin{tabular}{l}
\(1,00 \mathrm{~mA}\) a.c. \\
\(\mathbf{~ d . c . ~}\) \\
\(0 / 50 / 6 \mathrm{~K} / 6 \mathrm{meg}\) \\
\hline 0
\end{tabular} \begin{tabular}{lll}
250 mA \\
ohnı. & d.e. & \(0 / 6 \mathrm{~K} / 6 \mathrm{meg}\) \\
to \\
\hline 202 dB
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\(A C 115\) \\ \(A C 154\)
\(A C 155\) \(A C 155\)
\(A C 156\)
\(A C 157\) \\ AC167
AC168 \\ ACl 68
ACl 69
\(4 C 176\) \\ AC176
AC177
AC187 \\ AC187
AC188 \\ \(A C 188\)
\(A C Y 17\) \\ \(\begin{array}{ll}\text { ACY19 } & 20 \\ \text { ACY20 } & 20 \\ A C Y 21 & 20 p\end{array}\) \\ \(A\)} \begin{tabular}{l|l|l} 
5p & AF 115 \\
\(\mathbf{2 0 p}\) & AF 116
\end{tabular} \(\begin{array}{ll}\text { AC125 } & \text { 23p AF117 } \\ \text { AF } & \text { AF } 118\end{array}\) \(\begin{array}{ll}\text { AC126 } & 17 p \\ \text { AF AF } 124 \\ \text { AC127 } & 17 p \\ \text { AF } & \end{array}\) \(\begin{array}{ll}\text { AC127 } & 17 p \text { AF124 } \\ \text { AC128 } & 17 p \text { AFI2 }\end{array}\) \(\begin{array}{lll}\text { ACl28 } & \text { 17p } & \text { AFl2 } \\ \text { ACl4 } \\ \text { AC } & 17 p & \text { AFl } 27\end{array}\) \(\begin{array}{ll}\text { AClitK } & \text { 17p AFI } 27 \\ \text { ACl } & 12 \mathrm{~K} \\ \text { 17p AFI39 }\end{array}\) \(\begin{array}{lll}\text { ACIS1 } & 17 p & \text { AF139 } \\ \text { ACISI } & 15 p & \text { AFi78 } \\ \text { ACIS } & 15 p & A F I 79\end{array}\) \(\begin{array}{ll}\text { AC156 } & 17 p \\ \text { AF } & \text { AF181 } \\ \text { AC157 } & 17 p \\ \text { AF186 }\end{array}\) \(\begin{array}{ll}\text { AC165 } & \text { 17p } \\ \text { AF186 } \\ \text { AC166 } & \text { 17p } \\ \text { AF } & \text { AF } \\ \text { C1 }\end{array}\) \(\begin{array}{ll}\text { AC166 } & \text { 17p AFZII } \\ \text { AC167 } & \text { 20p } \\ \text { AFZI2 }\end{array}\)

\(A\)

\(\begin{array}{ll}A C Y & 18 p \\ A C Y 35 & 18 p \\ \text { BC108 } \\ A C Y 36 & 30 p \\ B C 113 \\ A C Y 40 & 15 p \\ \text { BC114 } \\ \text { ACY41 } & 18 p \\ \text { ACY } & \end{array}\)
\(\begin{array}{ll}A C Y 4 & 18 p \\ A C 114 \\ A C Y 41 & 18 p \\ \text { BC115 } \\ \text { ADI40 } & \mathbf{4 0 p} \text { BC116 } \\ \text { AD }\end{array}\)



\begin{tabular}{lr|l} 
ADZ12 & 62.10 & \(8 C 136\) \\
AF1 \\
\hline
\end{tabular}
AFII4 17p/BCI39

BRAND NEW FULLY GUARANTEED DEVICES
\(\begin{array}{ll}17 p B C 140 & 35 p B C Y 31 \\ 17 p & B C 141 \\ 17 p & 35 p \\ \text { BCY }\end{array}\)


 \(\begin{array}{ll}\text { 17p } & \text { BF274 } \\ \text { 20p } & \text { BF308 } \\ \text { 17p } & \text { BF309 }\end{array}\) \begin{tabular}{l|l|l} 
20p & BF308 \\
17p & BF309 \\
30p & BF316
\end{tabular} 30p BF316 15 BFW10 \begin{tabular}{l|l} 
15p & BFW 10 \\
20p & BF 29
\end{tabular} \begin{tabular}{l|l}
\(10 p\) & BF \(\times 29\) \\
\(85 p\) & BF \(\times 84\) \\
\(\mathbf{8 5 p}\) & BF \(\times 85\)
\end{tabular} \begin{tabular}{l|l|} 
65p & BFX85 \\
75p & BFX86 \\
\(80 p\) & BFX87
\end{tabular} \(35 p\)
37 37p MATI20
75p
55p
 15 p ST141
15 S \begin{tabular}{lll|l}
\(75 p\) & MATI21 & \(17 p\) & UT46 \\
\(55 p\) & MPFIO2 & \(43 p\) & U
\end{tabular}
 \begin{tabular}{lll|l}
\(\mathbf{2 0 p}\) & MPF195 & 43p & \(V 410 A\) \\
27p & OC 20 & 30p & 2301
\end{tabular} \begin{tabular}{l|l|} 
33p & BC 150 \\
\(50 p\) & BC 151 \\
\(50 p\) & BC 152
\end{tabular} \begin{tabular}{l|l|l}
50 p & BC152 \\
50 p & BC153
\end{tabular} 50 p BC154
45 BCl \begin{tabular}{l|l|l|}
\(\mathbf{4 5 p}\) & BC157 \\
\(\mathbf{3 7 p}\) & BC15B
\end{tabular} \begin{tabular}{l}
\(37 p\) \\
37 \\
\(\mathbf{3 7 p}\) \\
\hline
\end{tabular} \begin{tabular}{l}
\(37 p\) \\
45 P \\
\(\mathbf{4 5}\) BC159 \\
\hline 8
\end{tabular} \begin{tabular}{l} 
45p \\
85 \\
8 BC 168 \\
\hline
\end{tabular} \begin{tabular}{l|l|l|}
\(\mathbf{8 5 p}\) & BC168 \\
\(\mathbf{8 5 p}\) & BC 169 \\
\(\mathbf{2 5 p}\) & BC170
\end{tabular} \begin{tabular}{l|l}
\(\mathbf{2 5 p}\) & BC 170 \\
\(\mathbf{3 0 p}\) & BC171
\end{tabular} \begin{tabular}{l|l|}
\(\mathbf{3 0 p}\) & BC 171 \\
\(\mathbf{2 5 p}\) & BC 172
\end{tabular} \begin{tabular}{l|l|}
\(\mathbf{2 5 p}\) & BC \\
\(\mathbf{2 5}\) & BC 173 \\
\(\mathbf{2 5 p}\) & BC 174
\end{tabular} \begin{tabular}{l|l|l|}
\(\mathbf{2 5 p}\) & BC 174 \\
\(\mathbf{2 5 p}\) & BC 177
\end{tabular} \begin{tabular}{l|l|}
\(\mathbf{2 5 p}\) & BC 177 \\
\(\mathbf{2 5 p}\) & BC 178
\end{tabular} \begin{tabular}{l|l}
\(\mathbf{2 5 p}\) & BC179 \\
\(\mathbf{2 5 p}\) & BCIB0
\end{tabular} \begin{tabular}{l|l}
\(\mathbf{2 5 p}\) & BCl 180 \\
\(\mathbf{2 5 p}\) & \(8 \subset 181\) \\
\(\mathbf{2 5 p}\) & BC182
\end{tabular} \(\begin{array}{ll}25 p & B C 182 \\ 25 p & B C 182 L\end{array}\) 40p BC183 \(10 p\) BC183L \(10 p\) BC184
\(11 p\) BC184L 25 p BC186 30p BC187 3p BC207 \(\begin{array}{ll}35 p & \text { BC209 } \\ 35 & 8 C 209\end{array}\) 25p \(B C 212 L\)
\(45 p\) BC213L \begin{tabular}{l}
\(35 p\) \\
35 \\
35 \\
\hline 15 \\
BC214L
\end{tabular}
\(25 p\) BC225 \begin{tabular}{l|l|}
30 PC & BC 26 \\
30 p & BC 317
\end{tabular} \begin{tabular}{l|l}
\(30 \%\) \\
30 & BC318
\end{tabular}
\begin{tabular}{l|l|}
30 p & BC 318 \\
35 BC 319 \\
45 BCY
\end{tabular}
45p BCY30
12p BCY72
\(17 p\) BCZ11
\(17 p\) BDI21
\(20 p\) BD 2123
 \begin{tabular}{l|l} 
27p & BD 131 \\
30p & BD132 \\
20p & BD
\end{tabular} 20p BD
17p
BF 20
20p \begin{tabular}{l|l|} 
17p & BF115 \\
20p & BF1 17 \\
\(13 p\) & BFIIB
\end{tabular} \begin{tabular}{l|l}
\(80 p\) & BFX87 \\
\(80 p\) & BF \(X 88\) \\
EI & BFY 50
\end{tabular} 22p BFYSI
45 BFY52 \begin{tabular}{l|l|}
\hline \(\mathbf{6 0 p}\) & BFY52 \\
70p & BSX19 \\
35 & BSX
\end{tabular}



 \begin{tabular}{l|ll} 
13p & BF159 & 30p \\
22p & BSY29 \\
27p & BF160 & 30p \\
BSY & \\
17p & BF162 & 30p \\
BSY & B9 \\
17p & BF163 & 35p \\
BSY40
\end{tabular}
 \begin{tabular}{lll} 
20p & BF165 & 35p \\
22SYY5 \\
22p & BF167 & 22p \\
10p & BFI73 & 22p \\
BU & \\
\hline
\end{tabular} \(\begin{array}{rrrr}10 p & \text { BFI73 } & \text { 22p } & \text { BUIO5 } \\ \text { 10p } & \text { 12 } \\ \text { 10p } \\ \text { BFI76 } & 35 p & \text { CIIIE } & 60 p\end{array}\) 10p BF177
10p BF178
13p BF179 \(13 p\)
BF179
13p
27p
BF180
BFI
 \begin{tabular}{lll|ll|l} 
50p & C424 & 25p & OCB2D & 15p & \(2 N 527\) \\
30p & C425 & 40p & OC84 & 20p & \(2 N 696\) \\
\hline
\end{tabular} \begin{tabular}{lll|l|l|}
\(30 p\) & \(C 425\) & 40p & OC84 & 20p \\
30p & 2N697 \\
3026 & \(30 p\) & OC 139 & \(15 p\) & \(2 N 698\) \\
\hline
\end{tabular} 27p BFIB1
27 P BFI82
11 p
11 BF 183 11 P
IPFIB3
IIp BFIB5
IIP BFIB8 \(11 p\)
IPF188
IP
BFI94
\(11 p\)
\(B F 195\) \(12 p\) BF/94
25 BF/95
\(35^{2}\) BF/97
\(\qquad\)
30 p C428
 \begin{tabular}{l|ll|l}
\(\mathbf{2 0 p}\) & OC140 & \(17 p\) & \(2 N 699\) \\
\(\mathbf{2 7 p}\) & OC170 & \(15 p\) & \(2 N 706\) \\
\(\mathbf{3 5 p}\) & 2C & 171 & \(15 p\) \\
\(\mathbf{3}\) & \(2 N 706 A\)
\end{tabular}
 \(\begin{array}{llllll}\text { 23p } & C 720 & \text { 17p } & \text { OC201 } & \text { 27p } & \text { 1N709 } \\ \text { 24p } & \text { OC202 } & \text { 27p } & \text { 2N711 } \\ \text { 24p } & C 722 & \text { 25p } & O C 203 & \mathbf{2 5 p} & 2 N 717\end{array}\)

40
 \(2 N 918\)
\(2 N 929\)
\(2 N 930\)
\begin{tabular}{l|ll|l}
\(\mathbf{3 0 p}\) & \(\mathbf{2 N} 2714\) & \(\mathbf{2 5 p}\) & \(2 N 3704\) \\
\(\mathbf{2 2 p}\) & \(2 N 2904\) & \(\mathbf{2 5 p}\) & \(2 N 3705\)
\end{tabular} \begin{tabular}{l|ll|l}
\(\mathbf{2 2 p}\) & 2N2904 & \(\mathbf{2 5 p}\) & 2N3705 \\
25p & 2N2904A & \(\mathbf{3 0 p}\) & 2N3706
\end{tabular} \begin{tabular}{l|ll|l}
\(\mathbf{2 5 p}\) & \(\mathbf{2 N 2 9 0 4 A}\) & \(\mathbf{3 0 p}\) & \(\mathbf{2 N} 3706\) \\
\(\mathbf{2 0 p}\) & \(\mathbf{2 N 2 9 0 5}\) & \(\mathbf{2 5 p}\) & \(\mathbf{2 N} 3707\)
\end{tabular} \begin{tabular}{ll|l|l|} 
20p & \(2 N 2905\) & 25p & \(2 N 3707\) \\
\hline \(12 p\) & \(2 N 2905 A\) & \(30 p\) & \(2 N\)
\end{tabular}
 \(15 p\)
\(12 p\)
\(12 p\) \(2 p\)
\(2 p\) \(13 p\)
\(8 p\)
\(8 p\) \(8 p\)
8 p
10 p \begin{tabular}{l|ll|l}
\(17 p\) & \(2 N 2906\) & 25p & \(2 N 3709\) \\
17p & 2N2906A & 27p & 2N3710 \\
20p & \(2 N 2907\) & \(25 p\) & \(2 N 3711\)
\end{tabular}
 22 p
27 p
27 p
17 p \begin{tabular}{l|l} 
27p & \(2 N 2925\) \\
17p & \((G)\)
\end{tabular} 20p \(2 N 2926(Y)\)
\(35 p\) (Y) 12 p 12p 2NII32 40 p 2 N 1303 25p
45p
\(19 p\)
\(19 p\)


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