PRACTICAL NOVEMBER 19

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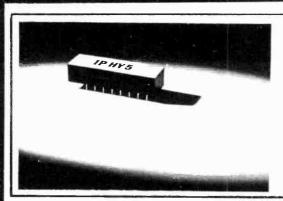
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LOAD IMPEDANCE 4-16 ohms INPUT IMPEDANCE 22Kohms at 1Khz.

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VOLTAGE GAIN 30db at 1KHz. FREQUENCY RESPONSE 5Hz-60KHz + 1db.

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Ceramic Pick-up (equalized and compensatable) 20 – 2000mV

variable. Tuner (flat) 250mV. Auxiliary 1 250mV.

Auxiliary 2 2-20mV.

OUTPUTS

Main Pre-amp output 500mV.

Direct tape output 120mV.

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Treble +12db.

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200	0-05	0.09	0.06	0.14	0.20	0.24	1.00
400	0.06	0.13	0.07	0.20	0.27	0.37	1.2
600	0.07	0.16	0.10	0.23	0.84	0.45	1.8
800	0-10	0.17	0.13	0.25	0.37	0.55	2.0
1000	0.11	0-25	0.15	0.30	0.46	0.68	2.5
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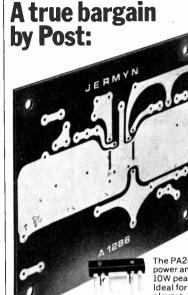
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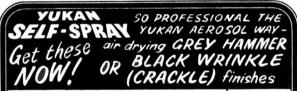
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BLACK ANODISED 16g. ALUMINIUM HEAT SINES. For TO3, complete with mica's and bushes. Size 2\frac{1}{8} \times 3" approx. 25p pair. P. & P. 5p.

# HARVERSONIC SUPER SOUND 10 + 10 STEREO AMPLIFIER KIT



REW IMPROVED MODEL WITH HIGHER OUTPUT AND INCORPORATING HIGH QUALITY READY DRILLED PRINTED CIRCUIT BOARD FOR EASY CON-STRUCTION

A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integrated pre-amp with Bass, Treble and two Volume Controls, Suitable for use with Ceramic or Crystal cartridges. Output stage for any speakers from 5 to 15 ohms. Compact design, all parts supplied including drilled metal work, high quality ready drilled printed circuit board, attractive front panel, knobs, wire, solder, nuts, bolts—no extras to buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification: Power output 14W t.ns., per channel into 5 ohms. Frequency response ± 33lB 12-30,000Hz. Sensifivity better than 80mV into 140, Full power bandwidth ± 3dB 12-15,000Hz. Bass boost approx. to ± 12dB. Treble cut approx. to - 16dB. Negative feedback 18dB over main amp. Power requirements 36V at 1-0 amp. Overall size-12° wide . 6° deep '2' high. Fully detailed 7-page construction manual and parts list free with kit or send 18p plus large 8.A.E.

PRICES AMPLIFIER KIT. \$10.50 P. & P. Lop. CABINET, \$2 P. & P. 30p. CABINET, \$2 P. & P. 30p. (Post Free if all units purchased at same time). Full after sales service. Also available ready built and tested, \$220.50. Post Free.

service. Also available ready built and tested, 0. Post Free.

Note: The above amplifier is suitable for feeding two mono sources into inputs (e.g. mike, radio, twin record decks, etc.) and will then provide mixing and fading facilities for medium powered Hi-Fi Discotheque use, etc.



PECIAL PURCHASE OF MANUFACTURER'S SURPLUS! All Transistor F. M. tuner head with twin A. M. Gang incorporated. Beautifully engineered with precision geared reduction drive. F. M. R.F. Transistor, oscillator/Mixer and first I.F. stage (10.7 Mc/s output) with optional AFC connection. Bull to a printed circuit panel and fully screened. Extremely stable over range 88-108 Mc/s. Brand new and pre-aligned. Size 24in H. ×. 1jin W. ×. 24in D. For 64 D. C. @ 2.8m.A. A.M. Gang fitted with trimmers which can be connected to standard A.M. aerial and oscillator circuits if required. LIMITED NUMBER. Only 22-25 post free. Connection details supplied.

HIGH GRADE COPPER LAMINATE BOARDS 8×6× Å in. FIVE for 50p. P. & P. 13p.

TELESCOPIC AERIALS WITH SWIVEL JOINT, Can be angled and rotated in any direction. 6 section L Brass. Extends from 6in. to approx. 221in. M diameter lin. 25p each. P. & P. 5p.

BRAND NEW MULTI-RATIO MAINS TRANSFORMERS. Glving 13 alternatives. Primary: 0-210-240V. Secondary combinations: 0-5-10-15-20-25-30-35-40-60V had wave at 1 amp or 10-0-10, 20-0-20, 30-0-30V, at 2 amps full wave.

Size 3inL 3inW × 3inD. Price £1.75.
P. & P. 30p.

MAINS TRANSFORMER. For transistor power supplies. Pri. 200/240V. Sec. 9-0-9 at 500mA. 70p. P. & P. 13p. Pri. 200/240V. Sec. 12-0-12 at 1 ann. 88p. P. & P. 13p. Pri. 200/240V. Sec. 10-0-10 at 2 amp. 21-38. P. & P. 30p. Tapped Primary 200-220-240V. Sec. 21-3V at 500mA. 63p. P. & P. 13p.

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Beautifully made teak finish enclosure with most attractive Tygan-Vynair front. Size 164in high ×104in wide ×5½ deep. Fitted with E.M.I. Ceramic Magnet 13in ×8in bass unit, two H.F. tweeter units and crossover. Power handling 10W. Available 3, 8 or 15 ohm impedance.

Our Price £8.40 Carr. 65p.

CABINET AVAILABLE SEPARATELY 44-50. Carr. 60p.
Also available in 8 ohm with EMI 13in ×8in. bass speaker with parasitic tweeter. 26-50. Carr. 60p.

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3in 4 ohm 50p, P. & P. 13p. 5in 3 ohm 80p, P. & P. 15p. 7 × 4in 3 ohm \$105, P. & P. 12p. 15in 3 ohm \$10 ohm \$1.05, P. & P. 12p. 10 × 6in 3 or 15 ohm \$1.90, P. & P. 30p. E.M.I. 8 × 5in 3 ohm with high flux magnet \$1.62, P. & P. 20p. E.M.I. 131 × 8in 3 ohm with high flux ceramic magnet \$2.10 (15 ohm \$2.25). P. & P. 30p. E.M.I. 13x 8in, 3 or 8 or 15 ohm with two inbult weeters and crossover network \$4.20, P. & P. 30p. E.M.I. 13x 8ir, 3 or 8 or 15 ohm with two inbult weeters and crossover network \$4.20, P. & P. 30p. E.M.I. 13x 8ir twin cone (parastatic tweeter) 8 ohm \$2.25, P. & P. 30p. 13"×8" twi P. & P. 30p.

RRAND NEW 12in 15w H/D Speakers 3 or 15 ohm Current production by well-known British maker. Now with Hiflux ceramic ferrobar magnet assembly \$5.50. Guitar models: 25w \$6.50. 35w \$8.50. P. & P. 38p each.

E.M.I. 34in HEAVY DUTY TWEETERS. Powerful ceramic magnet. Available in 3, 8 or 15 ohm 98p each. P. & P. 13p.

P. & F. 13p.

12in "RA" TWIN CONE LOUDSPEAKER
10 watts peak handling. 3 or 15 ohm, \$2.20, P. & P. 30p.
35 ohm \$F24KER\$ 3". ONLY 68p. P. & P. 13p.
VYMAIR & REXIME SPEAKER\$ & CABINET FABRICS
app. 64 in. wide. Usually £1.75 yd., our price 75p yd.
length. P. & P. 15p (min. 1 yd.). R.A.E. for samples.

# HI-FI STEREO HEADPHONES

Adjustable headband with comfortable flexifoam earmuffs. Wired and fitted with standard stereo in jack plug. Frequency response 39-15,000Hz. Matching impedance 8-16 ohms. PRICE 22-95, P. & P. 15p.

SINGLE HEADPHONE. With aluminium headband. Approx. 200 ohm. 25p. P. & P. 8p. CRYSTAL MIKES. High imp. for desk or hand use. High senaltivity, 93p. P. & P. 8p. HIGH IMPEDANCE CRYSTAL STICK MIKES. OUR PRICE 21.06. P. & P. & p.

GENERAL FURPOSE HIGH STABILITY TRANSISTOR PRE-AMPLIFIER, For P.U. Tape, Mike, Guitar, etc., and suitable for use with valve or transistor equipment. 9-18V. Battery or from H.T. line 200/300V. Frequency response 15Hz-25KHz. Gain 26dB. Solid encapsulation size  $1\frac{1}{4} \times 1\frac{1}{2} \times 1^{1}$ . Brand new — complete with instructions. Price 88p. P. & P. 13p.

BRAND NEW E.M.I. LIGHTWEIGHT PICK-UP ARM WITH ARM REST. Fitted mono t/o stylus and cartridge for LP/78, ONLY \$1. P. & P. 8p.

QUALITY RECORD PLAYER AMPLIFIER MK II QUALITY RECORD PLAYER AMPLIFIER MK II A top-quality record player amplifier employing heavy duty double wound mains transformer, ECC83, ELS4 and rectifier. Separate Bass, Treble and Volume controls. Complete with output transformer matched for 3 ohm speaker, Size 7in. w. - 3 d. < 6 h, Ready built and tested. PRICE \$3.75. P. & P. 40p. ALSO AVAILABLE mounted on board with output transformer and speaker ready to fit cabinet below. PRICE \$4.85. P. & P. 50p.

DE LUXE QUALITY PORTABLE R/P CABINET MK II Uncut motor board size 14½ × 12in., clearance 2 in. below, 5 in. above. Will take above amplifier and any B.S.R. or GARRARD changer or Single Player (except A760 and 8P25). Size 18×15×8in. PRICE \$2.98. P. & P. 50p.

# 10/14 WATT HI-FI AMPLIFIER KIT

A stylishly finished monaural amplifier with an output of with an output of 14 watts from 2 ELS4s in push-pull. Super reproduction of both music and speech, with negli-gible hum. Separate inputs for mike and gram allow records and announcements to follow each other



to follow each other.

Pully shrouded section wound output transformer to match 3-15Ω speaker and 2 independent volume controls, and separate bass and trobe controls are provided giving good lift and cut. Valve line-up 2 ELE4s, ECC83, EFR6 and EZ80 rectifier. Simple instruction booklet 13g (Free with parts). All parts sold separately, ONLY \$7.97, P. & P. 55p. Also available ready built and tested complete with std. input sockets, \$9.97, P. & P. 55p.

BRAND NEW TRANSISTOR BARGAINS. GET 15 (Matched pair) 75p; V15/10p, 50p; OC71 25p; OC76 30p; AF117 18p; 20339 (NPN) 15p. Set of Mullard 6 transistors OC44, 2—OC45, AC128D, matched pair AC128 21-25; ORP12 Cadmium Sulphide Cell 53p. All post free.

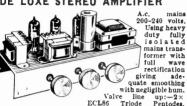
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SPEAKER CABINET FROM FAMOUS MAKER!

Beautifully made all-wooden construction cabinet with medium walnut finish front, gold anodised expanded aluminium grille and dark sides. Approx. size overall 11; high × 5' deep × 13; wide at base, Easily removable baffe cut out for 8' speaker. Fibre board back. Could accommodate amplifer or radio together with speaker. An expensively made cabinet at a give-way price. at a give-away price.

LIMITED NUMBER ONLY \$1.28 Post From

# DE LUXE STEREO AMPLIFIER



valve line up: 2-2 × 1×EZ80 as rectifier. Two dual potentiometers are provided for bass and treble control, giving bass and treble boost and cut. A dual volume control is used. Balance of the left and right hand channels can be adjusted by means of a separate "balance" control fitted at the rear of the chassis. Input sensitivity is approximately 300m/v for full peak output of 4 watts per channel (8 watts mono), into 3 ohm speakers. Full negative feedback in a carefully calculated circuit, allows high volume levels to be used with negligible distortion. Supplied complete with knobs, chassis size Ilin. w. x4in. x. Overall height including valves 5in. Ready built and Overall height including valves 5in. Ready built and tested to a high standard. Price \$8.92. P. & P. 45p.

4-SPEED RECORD PLAYER BARGAINS
Mains models, All brand new in maker's packing,
LATEST B.S.R. (109/A21 4-SPEED AUTOCHANGER.
With latest mono compatible cartridge 26-97, Carr. 50p.
With sterce cartridge 27-97, Carr. 50p.

With stereo cartridge \$7-97. Carr. 50p.
SUITABLE PLINTH UNIT FOR ABOVE with rigid plastic cover. \$25-75 complete, P. & P. 50p.
LATEST GARRAED MODELS. All types available 1025, 2025, SP25, 3000, A780, etc. S.A.E. for Latest Prices!
PLINTH UNITS cut out for Garrard Models 1025, 2025, 2000, 3000, 3500, etc. With rigid transparent plastic cover. Special design cnables above models to be used with cover in position. Also suitable for housing AT60 and SP25. OUR PRICE \$25-75 complete, P. & P. 50p.

LATEST ACOS GP91/18C Mono Compatible Cartridge with t/o atylus for LP/EP/78. Universal mounting bracket. £1.50, P. & P. 8b.

SONOTONE STANC COMPATIBLE STEREO CAPTRIDGE SONOTONE 97AHC COMPATIBLE STEREO CARTRIDGE
T/O stylus. Diamond Stereo LP and Sapphice 78, ONLY
25-50. P. & P. 10p. Also available fitted with twin
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LATEST ROMETTE T/O Stereo Compatible Cartridge for
EP/LP/Stereo/78. 21.83. P. & P. 10p.
LATEST ROMETTE T/O Mono Compatible Cartridge for
EP/LP/Stereo/78. 21.83. P. & P. 10p.

or stereo records on mono equipment. EP/LP/78 mono or 21.50, P. & P. 10p.



3-VALVE AUDIO
AMPLIFIER HA34 MK II
Designed for Hi-Fi reproduction of records. A.C. Mains operation. Ready built on plated heavy gauge metal chassis, size 7 jin w. 4 jin. d. 4 jin. h. Incorporates ECC83, EL84, EZ80 valves. Heavy duty, double wound mains transformer and output transformer and output transformer and output transformer matched for 3 ohm

speaker. Separate volume control and now with improved wide range tone controls giving bass and treble lift and cut. Negative feedback line. Output 4; watts. Front panel can be detached and leads extended for remote mounting of controls. Complete with knobs, valves, etc., wired and tested for only \$4.75. P. & P. 35p.

HSL "FOUR" AMPLIFIER RIT. Similar in appearance to HA34 above but employs entirely different and advanced circuitry. Complete set of parts, etc. 23-98. P. & P. 40p.

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A super quality gram amplifer using a double wound fully isolated mains transformer, rectifier and ECL82 triode pentode valve as audio amplifer and power output stage. Impedance 3 ohms. Output approx. 3-5 watts. Volume and tone controls. Chassis size only 71n. wide / 3in. deep × 6in. high overall. AC mains 200/240V. Supplied absolutely Brand New, completely wired and tested with good quality output transformer. FEW ONLY.

OUR ROCK BOTTOM BARGAIN PRICE

£2.75 P. & P.

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# FIRST STEP TO STEREO!

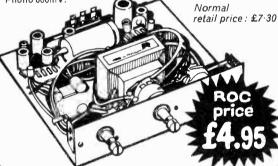
brushed aluminium front.Frequency

tuner/aux 80mV.

response:70-20,000 Hz ±3dB.Output: 4 watts per channel @ 8 ohms.Inputs:Phono 80mV;

5-Watt Transistor Stereo Amplifier Chassis R.123 Completely self-contained, fully transistorised, mains-powered

(240vAC) amplifier, needing only cabinet and knobs. Ideal for adapting mono players to stereo. Frequency response: 40-17,000 Hz ±3dB. Output: 2-5 watts per channel @ 8 ohms. Input: Phono 600mV.



# SOUNDS SENSATIONAL

AM/FM/MPX Stereo Tuner Amplifier R.124

A top quality amplifier with facility for re-

ceiving stereo broadcasts.
Separate bass and treble controls, automatic frequency re-

sponse, stereo headphone socket, output power: 8 watts. FM frequency range 88-108 M Hz; AM frequency range 535-1605 K Hz. Inputs for turntable (ceramic cartridge) and tape. Frequency response: 50-10,000 Hz ±3dB. Output: 4 watts per channel @ 8 ohms. Inputs: Phono 200mV, tape 100mV. FM: Sensitivity 20uV, stereo separation 26dB, image rejection 55dB. AM: Sensitivity 300uV

Normal retail price: £42:00

ROC price: £29.95

# World wide reception

Professional Solid-state, Four-band Communications Receiver R.135

Fully transistorised with continuous coverage from 555K Hz to 30 M Hz in four bands (with illuminated bandspread for 160-10 metres). Incorporates internal speaker, automatic noise limiter, SSB/AM/CW switch, AVC switch, S Meter, Receive and Standby switch, external socket for headphone or speaker, bandspread control, BFO control, on/off/AF gain, band selector, antenna trimmer and RF gain. Runs off 240 v AC, batteries or any 12 v DC negative ground source. Frequency ranges (in mHz): Band A, 535-1-6; B,1-55-4-5; C,4-5-13; D,13-30. Sensitivity: 0.5 μV @ 30 mHz. Bandspread: 10-160 metres.

Normal retail price: £65.00

ROC price:

Normal retail

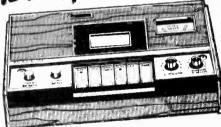
price: £14.70

£45.00



AMAZING OFFEK!

Stereo Cassette Tape Unit R.142



Complete stereo record and playback unit with line and microphone inputs. Fitted with tape counter, separate pause control, recording level metres for each channel, pop-up cassette ejection. Supplied complete with two pencil microphones. Wow & flutter better than 0-3%, frequency response 100-10,000 Hz. Tape speed: 1¼ IPS,4-75 CMS. Rewind time: Better than 60 sec (C.60 cassette). Normal retail price: £65-00

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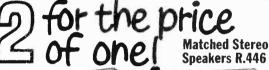


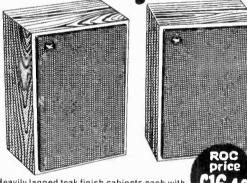
# Headphone Radio R.143

For completely private listening without the distortion of the ordinary earphone adaptor. Battery operated; PP3. Fully transistorised. Frequency range: 535-1600 K Hz, Medium Wave Band. Maximum output: 300mW.



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Heavily lagged teak finish cabinets each with large dual cone base unit and separate tweeter. Power handling:10 watts peak; frequency range:40-18,000 Hz,impedance: 8 ohms. Size:14 x 8 ł x 6 ł.

Normal retail price: £19.60

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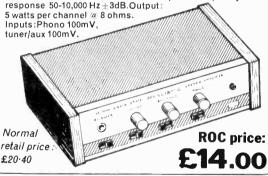
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10-watt Transistor Stereo Amplifier R.136

Ganged volume,balance and tone controls.Inputs for turn-table(ceramic cartridge),tuner(see R.134)or tape.Oiled walnut case with satin finish aluminium front panel.Frequency





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RECORD PLAYER CARTRIDGES. Well below normal prices!
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MULLARD POLYESTER CONDENSERS 1,000pF, 1,200pF, 1,500pF, 1,800pF, 2,200pF, 15p per dozen (all 400V working). 0.15µF, 0.22µF, 0.27µF, 30p per dozen (all 160V working). 25% discount for lots of 100 of any one type.

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RESISIONS 4 and 4 watt. Most values in stock. 50p per 100. 10p per dozen of any one value. WIRE WOUND MAINS DROPPERS. Hundreds of values from 0.7 ohm upwards. I watt to 50 watts. A large percentage of these are multi-tapped droppers for radio[television. Owing to the huge variety these can only be offered "assorted" at 50p per dozen.

SILVER MICA/CERAMIC/POLYSTYRENE CONDENSERS
Large range in stock, 75p per 100 of any one value. 15p per dozen.
RECORDING TAPE BARGAIN! The very best British Made lownoise high-quality Tape! 5in Standard 36p. Long-play 45p. 5½in Standard
45p. Long-play 60p. 7in Standard 60p. Long-play 82p. We are getting a
fantastic number of repeat orders for this tape. Might we suggest that you
order now whilst we still have a good stock at these low prices?

STOCKTAKING CLEARANCE! IMPOSSIBLE TO REPEAT! STOCKTAKING CLEARANCE! IMPOSSIBLE TO REPEAT!
We have huge numbers of components in quantities too small to advertise
individually. In order to "clear the decks" we have made up parcels containing
a mixture of carbon and wire-wound resistors, electrolytic and paper condensers, controls, transistors, diodes etc., for a tiny fraction of normal price.
It is emphasised that these are mixed parcels only—contents cannot be
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Gross weight 2 lb. .. .. .. £1 (postage 20p) .. £2 (postage 30p) Gross weight 5 lb. ..

Unrepeatable Offer!!!! Surplus VEROBOARDS, 3\frac{3}{4}" \times 2\frac{1}{2}" \times 15" Only 10p each or £1 00 per dozen

# TANTALUM CAPACITORS, COMPARE THE PRICE-ONLY 10p EACH !!!!

Sub-miniatur	e typ	es	Miniat	ure ty	pes		5.6	μF	35	volts	
0.047µF	50	volts	0.02	2uF	20	volts	8.2	μF	10	volts	
0 056µF	50	volts	0.03	3µF	20	volts	8.2	μF	35	volts	
0.07 µF	20	volts	0.04	7µF	20	volts	15	μF	35	volts	
0 I μF	20	volts	0.06	BuF	35	volts	18	μF	35	volts	
0 l µF	50	volts	0.12	μF	35	volts	22	μF	15	volts	
0·18 µF	20	volts	0.15	иF	35	volts	27	μF	120	volts	
0·33 μF	35	volts	0.22	μF	50	volts	56	μF.	15	volts	
0.47 µF	35	volts	0.47	цF	50	volts	56	μF	20	volts	
0.68 µF	20	volts	0.68	μF	35	volts	150	μF	6	volts	
1.0 μF	15	volts	0.68	μF	50	volts					
2.2 µF	3	volts	1.0	μF	35	volts	Standa				
2·7 µF	15	volts	1-0	μF	75	volts	6.8	μF	50	volts	
2·7 μF	35	volts	1.8	μF	20	volts	7.5	μF	20	volts	
30 μF	12	volts	2.2	μF	20	volts	8.2	μF	150	volts	
100 µF	13	5 volts	2.7	μF	50	volts	12	μF	35	volts	
			3	μF	12	volts.	12	μF	50 20	volts	
			3.3	μF	15	volts	39	μF	20	volts	
			4 4·7 5·6	μF	20	volts	82	μF	20	Volts	
			4.7	μF	35	volts	150	μF	15	volts	
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An aerosol spray providing a convenient means of producing any number of copies of a printed circuit both simply and auickly.

Spray copper laminate board with light-sensitive Method: spray. Cover with transparent film upon which circuit has Spray with developer, rinse and etch in normal manner.

Light sensitive aerosol spray Developer spray

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18 gauge on plastic reel. Recommended retail price 75p Size 12

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# SK1 SOLDERING

In rigid plastic "tool box" containing Model CN - 15 watts - 240 volts miniature iron fitted  $\frac{3}{16}$ " bit. Spare bits  $\frac{5}{2}$ " and  $\frac{3}{3}$ ". Reel of resin-cored solder, heat sink, cleaning pad, stand and booklet "How to Solder".



# SK2 SOLDERING KIT

In polystyrene pack, containing 15 watt miniature soldering iron, 240 volts fitted with  $\frac{3}{16}$ " bit, 2 spare bits  $\frac{5}{32}$ " and  $\frac{32}{32}$ ". Coil of resin-cored solder, heat sink, 1A fuse and booklet "How to Solder"

£2·40

£275



- 15 watts

- 240 volts

£1.70

Fitted with nickel plated  $\frac{3}{32}$ " bit and packed in handy transparent box.



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In transparent display pack, fitted with long life iron-coated bit  $\frac{1}{8}$ " diam. Interchangeable spare bits  $\frac{3}{32}$ ",  $\frac{1}{16}$ ",  $\frac{1}{4}$ " (extra) available. Improved design to ensure strong and reliable high speed iron. Heats up in 2 minutes.



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Available complete for only £52+£3-50

# SYSTEM 2

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# Available complete for £69+£4 P.&P.

# SYSTEM 3

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Total £52

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# SPEAKERS Duo Type II

Size approx. 17in  $\times$   $10\frac{3}{4}$ in  $\times$   $6\frac{3}{4}$ in. Drive unit 13in  $\times$  8in with parasitic tweeter. Max. power 10W, 3 ohms. Simulated Teak cabinet. £14 pair + £2 P. & P. Duo Type III Size approx.  $23\frac{1}{2}$ in  $\times$   $11\frac{1}{2}$ in  $\times$   $9\frac{1}{2}$ in. Drive unit  $13\frac{1}{2}$ in  $\times$   $8\frac{1}{4}$ in with H.F. speaker. Max. power 20W at 3 ohms. Frequency range 20Hz to 20kHz. Teak veneer cabinet. £32 pair + £3 P. & P.

# SPECIFICATION R100/101

14 watts per channel into 3 to 4 ohms. Total distortion @ 10W @ 1kHz 0-1%. P.U.1 (for ceramic cartridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K equalised within ±1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power.) Tape out facilities; headphone socket, power out 250mW per channel. Tone controls and filter characteristics. Bass: +12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble controls treble +12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. Signal to noise ratio: (all controls at max.) R101-P.U.1. and radio-65dB. P.U.2-58dB. R100 same as R101 but P.U.2 (for crystal cartridges) 450mV into 3 Meg. Cross lalk better than -35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx. 13½ × 9in × 3½in.



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185	.22	30C15	-58	DY802	.35	EM80	-41	PCL83	-58	UAF42	-51
1T4	-16	30C17	-79	EABC80	-32	EM81	-41	PCL84	-34	UBC41	-52
384	-26	30C18	-61	EAF42	-50	EM84	-32	PCL85	-40		-34
3V4	-37	30F5	.70	EB41	-40	EM87				UBF80	
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5Z4G	-35	30FL14	-29	EBC90	-22	EZ40	-43	PENA4		UCF80	-33
6/30L2	-56	30L15		EBF80	-32	EZ41	-43	PEN36		UCH42	-62
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	·13	30P4 30P12	·65		.20	GZ30	-35	PL81	-45	UCL83	-55
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25U4GT	-57	DY86	•25	EL95	-33	PCF808	-68	U801	-98	OC170	-22

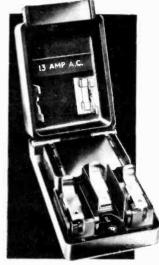
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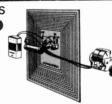
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All these and many other things you can do if you invest in an Electrical Programmer. Made by the famous Smiths Instrument Company. do if you invest in an Electrical Programmer. Made by the famous Smiths Instrument Company. This is essentially a 230/240V mains operated Clock and a 20A Switch, the switch-off time of which can be delayed up to 12 hours (continuously variable not stepped). Similarly the switch-on time can be delayed. This is a beautiful unit, size  $5\frac{1}{3}\ln \times 3\frac{3}{4}\ln \times 2\frac{1}{3}$  in deep. Metal encased, glass fronted with chrome surround. Offered at 42.40 plus 23p postage and insurance.

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# ANKET SWITCH

Double pole with neon let into side so luminous in dark. ideal for dark room light or use with waterproof element, new plastic case 30p each. 3 heat model 40p.



# 24kW FAN HEATER

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#### SPARTAN Portable RADIO

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sinks can easily see heatsinks can easily see the protected. Slimple
make the contact thermostat part of the heat sink.

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# please state whether for positive or

# RADIO STETHOSCOPE

RADIO STEPHOSCOPE

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to speaker—when signal stops you've found the
fault. Use it on Radio, TV,
amplifier, anything — complete kit comprises two special
translators and all parts including probe tube and crystal
earpiece. 42—twin stethoset instead of earpiece 75p
extra—post and inc. 20p.



#### P.E. GEMINI

Dual purpose twin 30W stereo amplifier for exceptional per-formance. Complete kit of parts less case \$45 or reprint of data and parts list 55p.

0

No. of Poles 1 pole 2 poles

3 poles 4 poles 4 poles 5 poles 6 poles 7 poles 8 poles 9 poles

10 poles 11 poles 12 poles



# STANDARD WAFER SWITCHES

Standard size  $1\frac{1}{4}$  wafer—silver-plated 5-amp contact-standard  $\frac{1}{4}$ " spindle 2" long—with locking washer and nut-6 8 9
way way way
40p 40p 40p
40p 40p 40p
70p 70p 70p 70p
95p 95p 95p
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#### THIS MONTH'S SNIP

15 WATT 12in HI-FI SPEAKER. Is undoubtedly one of the finest loudspeakers that we have ever offered, produced by one of the country's most famous makers. It has a die-cast metal frame and is strongly recommended for thi-Fi and public address. Handling 15W R.M.S.—Cone moulded fibre—Freq. response 30-10,000 c.p.s. specify 3 or 15 ohms. Chassis diam. 12 in—12½ in over mounting lugs. Overall height 5½ in. A £10 speaker offered this month for £3.75 plus 30p post and ins.



## TANGENTIAL HEATER UNIT



This heater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoover and blower heaters coeting 215 and more. We have a few only. Comprises motor, impeller, 2kW element and 1kW element allowing switching 1, 2 and 3kW and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only need control switch. 25.50. 2kW Model as above except 2 kilowatts 25.50. Don't miss this. Control 8witch 256. P. & P. 400. except 2 kilowatts \$2.50. Do Control Switch 35p. P. & P. 40p.

## HONEYWELL PROGRAMMER

HONEYWELL PROGRAMMER

This is a drum type timing device, the drum being calibrated in equal divisions for switch setting purposes with trips which are infinitely adjustable for position. They are also arranged to allow 2 operations per switch per rotation. There are 15 changeover micro switches each of 10 amp type operated by the trips thus 15 circuits may be changed per revolution. Drive motor is mains operated 5 revs per min. Some of the many uses of this timer are Machinery control, Boller firing. Dispensing and Vending machines, Display lighting animated and signs, Signalling, etc. Price from makers probably over £10 each. Special snip price £5.76 plus 25p post and insurance. Don't miss this terrific bargain.

# INTEGRATED CIRCUIT BARGAIN

INTEGRATED CIRCUIT BARGAIN

A parcel of integrated circuits made by the famous Plessey Company. A once-in-a-lifetime offer of Micro-electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect. first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP amplifiers. The 5th is a monolithic NPN matched pair. Regular price of parcel well over \$5. Full circuit details of the ICs are included and in addition you will receive a list of many different ICs available at bargain prices 5f- upwards with circuits and technical data of each. Complete parcel only \$1 post paid. DON'T MISS THIS TERRIFIC BARGAIN.



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# Where postage is not stated then orders over £5 are post free. Below £5 add 20p. Semiconductors add 5p post. Over £1 post free. S.A.E. with enquiries please.



# DRILL CONTROLLER NEW IKW MODEL



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#### HIGH ACCURACY THERMOSTAT

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# P.E. CONSTRUCTIONAL **PROJECTS**

We can probably supply the com-ponents to build projects described in this issue and companion magazines. Send S.A.E. for list naming the project.

#### **AUTO-ELECTRIC** CAR AERIAL



with dashboard control switch—fully extendable to 40 in or fully retractable. Suitable for 12V positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. \$6 plus 250 post and insurance.

#### **TOGGLE SWITCH**

3 amp 250V, with fixing ring 7 p each, 75p doz.

# CAR ELECTRIC PLUG



Fits in place of cigarette lighter. Useful method for making a quick connection into the car electrical system. 389 each or 10 for 23-42.

# **ROCKER SWITCH**

13A self-fixing into an oblong hole, size approximately lin x in sp each, 10 for 54p.



# MAINS RELAY BARGAIN

natruction

Special this month are some single, double and treble pole changeover relays. Contacts rated at 15A. Operating coil wound for 240V a.c. Good British make Unused. Size approx. 1inxlin. Open

# **BALANCED ARMATURE UNIT**

500 ohm, operates speaker or microphone, so useful in intercom or similar circuits. 6/6 each, \$3.50 doz.



# **THERMOSTAT**

Continuously variable 30°-90°C. Has sensor bulb connected by 33 in of flexible tubing. On operation a 15 amp 250V switch is opened and in addition a plunger moves through approx. i in. This could be used to open valve on ventilator etc. \$1.50 plus 23p p. and ins.

# 5A 3-PIN SWITCHED SOCKETS

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# MAINS MOTOR



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# J. BULL (ELECTRICAL) LTD.

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It's ALMOST UNBELIEVABLE! Just think of the year 1984 and the "perfect radio" that might be produced then, with all the advanced qualities it could possibly have—now place the fantastic ASTRAD (VEF) 17 in front of you and switch on, and you'll see for yourself that the incredible Russians have done it all HERE AND NOW! It's the radio perfectionist's dream come true! THIS ONE SUPERSEDES ALL EARLIER MODELS! It will probably make your present radio seem like a "crystal set"! Complete with optional battery eliminator for both battery and mains use! We're almost giving them away at only £19.75—a mere fraction of even today's Russian miracle price! In fact we challenge you to compare the performance and value with that of £75 radios! "You just can't lose, we'll refund your money instantly if you are not ascounded! Purer and sweeter tone than ever! Much wider band spread than hitherto, for absolute "pin-point" station selection! Plus "MAGIC EYE" tuning level indicator for ultra perfect tuning sensitivity! Yes, the Russians have really surpassed themselves this time, proving once again their fantastic ability in the field of electronics and brilliantly reflecting their advanced micro-circuity techniques in the field of spaceship and satellite communications. YOU GET THIS AMAZING SET FROM U.S. AT A PRICE THAT BEARS NO RELATION TO ITS TRUE VALUE! Yes, EVERY WAVEBAND instantly at your fingertips including Standard Long, Medium, Short and Ultra Short Waves to cover the four corners of the earth 24 hours a day, including all normal transmissions VHF, AM, FM, W, LW, U.S.W, plus local and new stations not yet operational, Ships at Sea, etc., short mobile transmissions and messages from all over the world—truly nothing is secreet! (Even getting "private transmissions" is a piece of calle. Unique side control waveband selection unit gives incredible ease of station tuning! Superb sweet tone—controlled from a whisper to a roar that will fill a hall! Genuine push-pull output! ON/OFF volume and separate Treble and Bass tone contro

CONTROL TO AIRCRAFT, SHIPS, POP PIRATES, TAXIS, AMBULLANCES, LOCAL AND CONTINENTAL STATIONS, ALL B.B.C. VHF AND MANY MORE, including public service transmissions we are not allowed to mention! Far more than an ordinary radio! Bring a new dimension to your world of sound! Range: MW 540-1600 KHz, FM 88-108 MHz Air 108-145 MHz, Intermediate Frequency: AM 455 KHz, FM 10.7 MHz. Air 10.7 MHz. 18 SEMI-CONDUCTORS: Transistors II, Diodes 6 + Thermistor! Automatic frequency control "locks-in": eliminating drift. Pinpoint selection! Built-in 8-section aerial extending to over 30in approx. Strong leather grained finish case with handle, 10/in × 6/in × 4in overall approx. Written gitee, Only 19.99 post 38p. Runs off mains—a.c. 230/250V, or off standard batteries. That's not all! It's got a built-in Battery Booster too! Just plug in to mains whenever you wish! "Compare it with sets costing 640 or more. Refund if not delighted. BONUS: Shoulder Strap, earphone for personal listening and dry batteries, all for 31p extra. Refund Guaranteed.

Make no mistake — this is the expensive model with "piano keyboard" control panel and "Magic Eye" automatic recording SAVE £13-98! Due to price Make

SAVELIS-98 NOVIL fabulous and

Due to price
we cannot
mention
famous
maker's
name — but

In the put have but have been accounted microelone. In the put have but have but have but have been as some put have been as a consette and you're getting one of the BEST! 1971 cassette model—no fiddling with awkward tape and reels, just "slap in" a cassette and off you go! (takes 30, 60, or 90-minute standard Philips cassette tapes obtainable everywhere). Amazing performance ensures perfect tapings and superb reproduction! Remote control microphone. Separatee voluments and superb reproduction! Remote control microphone, etc. Size 9in × 4½ × 2½ in overall approx. Case design can vary slightly. With carry handle or strap. WRITTEN G'TEE and instructions. Only £12-99 post 30p. Refund g'tee. BONUS one per customer: Cassette tape, set of standard batteries AND microphone stand all for 51p extra if required. A visit to Shopertunities will save you £6's!



Never before Nationally advertised to the general public in this country. These amazing Brand New Russian multi-wave portable radios designed for inter-continental reception are truly Fantastic—and brilliantly reflect advanced Russian micro-circuitry developments in space communications. We we advanced one space communications, see we advanced one space communications with the space communications are truly Fantastic—and brilliantly reflect advanced Russian micro-circuitry developments in space communications, see we advanced one space of the sp

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**VOL. 7 No.** 11 **November** 1971

# PRACTICAL ELECTRONICS

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# RETROSPECT AND PROSPECT

SEVEN years is a long time in electronics . . . PRACTICAL ELECTRONICS first appeared on the scene in mid October 1964. The very next day (!) Sir Alec Douglas-Home conceded victory to Mr. Harold Wilson. Shortly afterwards the Ministry of Technology was set up, intended by the incoming administration to be the symbol of a new technological era, and the British electronics industry received assurances of determined government backing in their battle with foreign competitors. At this time, valve manufacturers continued to face the future stoically despite the formidable progress of the transistor, but P.E. put its money on solid state from the word go.

Seven years on . . . the thermionic valve has all but conceded victory to the semi-conductor, and prepares to make its final stand in the high power region. On the other hand the transistor, after enjoying a few delightfully expansive years of near total sovereignity, is itself alerted to a serious threat from nearer home as that more recent offspring of solid state technology, the IC, makes its bid to take over the strategic small signal areas from its discrete brethen.

In the meanwhile . . . the government has changed once again and MinTech, child of that now demised white-hot technological revolution, is demolished and replaced by the no-nonsense, businesslike—if prosaic sounding—Department of Trade and Industry. Our semiconductor manufacturers, now "freed" after several years of cossetting at the taxpayers expense, bravely face the cold, hard outside world—as true exponents of private enterprise should—without a murmur (save perhaps, just a little one).

On the home constructor front developments proceed apace. It's an ill wind . . . IC manufacturers pour many thousands of their excess production onto the amateur market. Private designers and constructors get bigger ideas as the devices get smaller. Miniaturisation and yet expansion seems the order of the day.

Today . . . the outlook is, indeed, promising. Yet how does one magazine such as ours cope with the inordinate demands arising from the increasing popularity of amateur electronics as a hobby? For, considering the various types of individuals already involved, or likely to become so any moment now, it is obvious that technical knowledge, practical skills, and areas of special interest and involvement range enormously.

continued on page 938

# THIS MONTH

# CONSTRUCTIONAL PROJECTS

RHYTHMETRON 890
WAR GAMES COMPUTER 902
P.E. SCORPIO 910
PROIECTOR LAMP PROTECTOR 924

# SPECIAL SERIES

RADIO ASTRONOMY TECHNIQUES—6

# **GENERAL FEATURES**

INTRODUCTION TO
LOUDSPEAKERS 895
INGENUITY UNLIMITED 926
SUBSTITUTES FOR ZENERS 918

# **NEWS AND COMMENT**

EDITORIAL	889
INDUSTRY NOTEBOOK	906
ON THE FRINGE	909
ELECTRONORAMA	916
PATENTS REVIEW	922
NEWS BRIEFS	925
SPACEWATCH	928
BOOK REVIEWS	929
READOUT	941

Our December issue will be published on Saturday, November 13.

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930



MANY circuits for simple electronic metronomes have been published but almost all of these have employed a multivibrator with one output coupled directly to a small high resistance loud-speaker. The resultant sound is a click, usually not very loud and bearing little resemblance to the more resonant beat produced by a mechanical metronome.

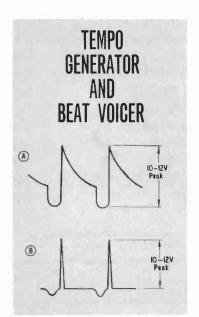
Unless an amplifier is included the loudness from a multivibrator and loudspeaker is not normally sufficient to make itself clearly audible above modern amplified musical instruments like the electronic organ or indeed above the sound produced by a small orchestra or choir.

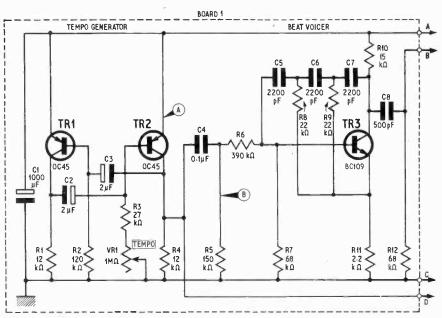
The signal output from the generator described in this article is more than sufficient to drive almost any amplifier but as the sound it produces has no bass content quite a loud sound will be obtained even with a 3W amplifier and relatively small speaker, certainly sufficient for practice with a domestic electronic organ or piano and probably enough for school music classes.

# DRUM BRUSH RHYTHM

In addition to beat notes the generator will produce a steady drum brush effect with variable attack and decay so it also becomes a very simple rhythm unit. The tempo is continuously variable over the usual music range of about 40 to 250 beats per minute and to assist constructors a cut-out calibration scale is included with beats per minute marks and approximate settings for tempo variations between largo (very slow) and presto (very fast).

The generator does not produce accented beats as this requires complex counting circuitry but as the beats are steady it is quite easy to play against them in three-four, two-four or four-four time, or multiples, depending on the setting of the tempo control. As the drum brush attack and decay can be controlled, the "voicing" can be set to produce a fast attack and short decay for fast tempi and soft attack and slow decay for slow tempi such as the slow waltz.





# THE CIRCUIT

The generator can be operated from batteries or a small mains power supply. It consumes only 2mA so it would run economically from two 9V batteries in series. The circuit given in Fig. 1 shows the complete generator with a battery supply. An alternative mains operated power unit is given in Fig. 2.

The first stage consists of a multivibrator. TR1 and TR2 are pnp transistors with emitters connected to the +18V rail. The tempo is controlled by VR1.

The output from TR2 collector provides a positive going pulse which is coupled via C4 to the "beat" voicer TR3. This transistor is an npn type and is connected as a phase shift oscillator biased to cut-off. The positive pulse from C4 instantly drives TR3 on but the short time constant provided by C4/R5 allows the pulse voltage to decay quickly. The output from TR3 is, therefore, a short but gradually decaying burst of oscillation of about 1,500Hz. The sound is a resonant tapping not unlike that of a clave and closely resembling the sound of a mechanical metronome.

# THE DRUM BRUSH VOICER

The output from TR2 is also fed to R15 and the diode D2 which together with the attack/decay network VR2, R16, C11, C12 and VR3 provides a positive pulse with variable rise and decay time. This pulse, from C11, drives the drum brush amplifier TR4.

The white noise for the drum brush voicing is obtained from the special Zener diode D1. It must be emphasised that any "noisy" Zener may fail to produce the required amount of white noise which must be at least 50 to 100mV r.m.s. in level. The Z1J Zener diode specified will produce in excess of 100mV of noise and can be obtained from Semitron Limited, Cricklade, Wiltshire, price 40p including packing and postage.

The outputs from the beat voicer (TR3) and the drum brush voicer (TR4) are taken to S1 which enables selection of either voice. The "mute" switch

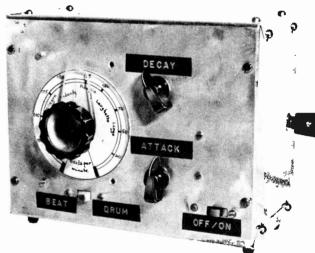
S3 is optional but it is a worthwhile addition as it will enable the user to leave the generator running but stop and start the signals as required.

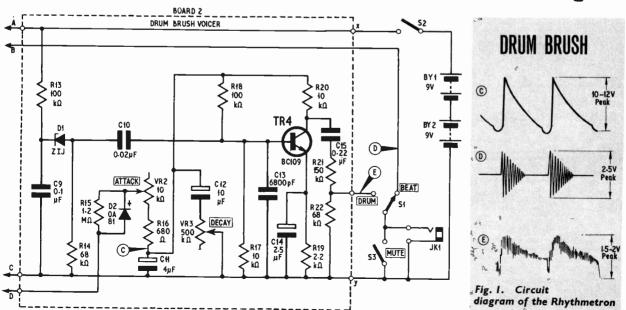
# THE POWER SUPPLY

The alternative mains power supply of Fig. 2 requires a transformer with a secondary delivering between 12 and 18V. The current consumption required by the generator is small but the line voltage must be adjusted on load to 18V, hence the resistor R23 in the power supply may need to be larger depending on the transformer secondary voltage. If the transformer specified is used it can be mounted on a piece of Veroboard together with the rectifier and the reservoir capacitor C16 and R23 omitted as shown in Fig. 3. If two 9V batteries are used they can be retained within the generator case by suitable clips.

# CONSTRUCTION

In the prototype the generator was constructed on two boards as shown in Figs. 4 and 5. Board 1





# COMPONENTS . . .

			WEST OF	
Resist	tors			
RI	12kΩ R9 22k	$\bar{\Omega}$ R17	l0k $\Omega$	
R2	120kΩ R10 15k		100k Ω	
R3				Transistors
R4	12kΩ R12 68k		10k Ω	TR1, TR2 NKT214 or OC45 (2 off)
R5	150k Ω R13 100		150k Ω	TR3, TR4 BC109 (2 off)
R6	390k Ω R14 68k		68k Ω	11(3, 11(1 BC10) (2 011)
R7	68kΩ RI5 I-2N		470 Ω (see text)	
R8	22kΩ R16 680	$\Omega$		Diodes
All	10% ½ watt carbon			DI ZIJ Zener (see text)
1				D2 OA8I ´
Poter	ntiometers			D3-D6 Bridge rectifier LTI19
VR	I IM $\Omega$ log. carbon	VR3 5	00k Ω linear carbon	
VR2	$\Omega$ = 10k $\Omega$ linear carbor	า		
1				Switches
Capa	citors			SI S.P.D.T. slide switch
Ċı	$1,000\mu F$ elect. 25V	C9 (	$0.1 \mu$ F polyester	S2 Single pole on/off switch
C2	$2\mu$ F elect. 15V		0·02μF polyester	S3 Single pole on/off (see text)
C3	2μF elect. 15V		μF elect. 15V	
C4	0·IμF polyester		0μF elect. 15V	Miscellaneous
C4 C5 C6	2,200pF polystyrene		,800pF polystyrene	TI-I2-0-I2V 50mA Eagle transformer type MRI2
C6	2,200pF polystyrene		1.5μF elect, 15V	Universal chassis 8 in $\times$ 6 in $\times$ 4 in.
C7	2,200pF polystyrene		0.22µF polyester	BYI-BY2 9V batteries (2 off). JKI Standard jack
C8			,000μF elect. 25V	socket.
C0	500pF polystyrene	CIO	,000µ1 e1ect. 23 V	CONTRACTOR OF THE PROPERTY OF

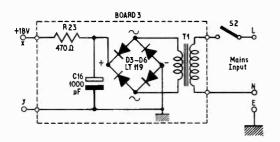
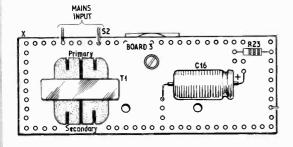


Fig. 2. Circuit diagram of the mains power supply unit



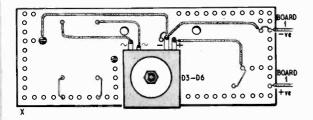
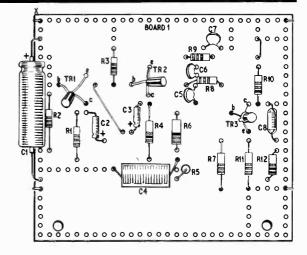
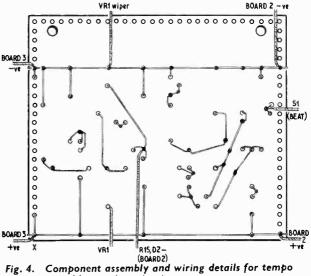
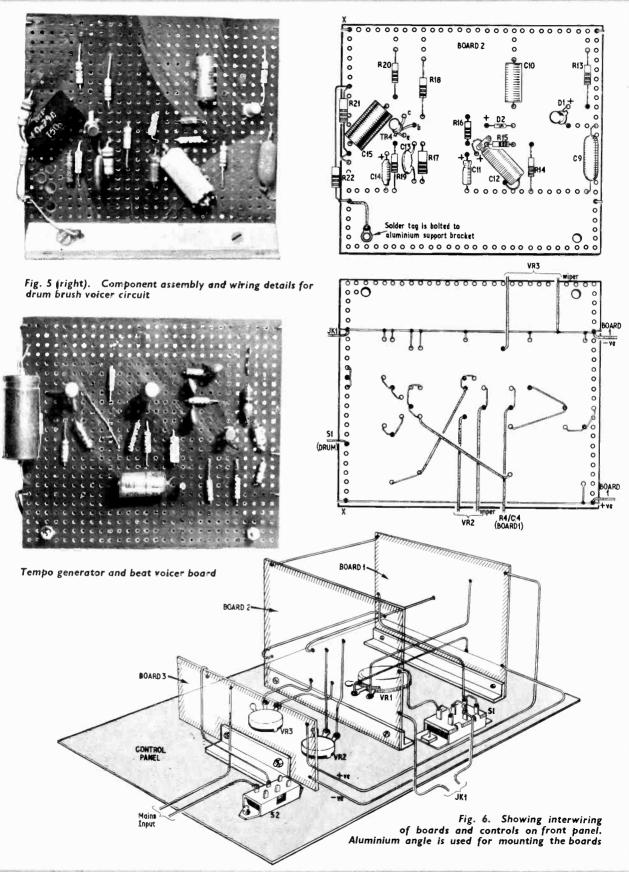


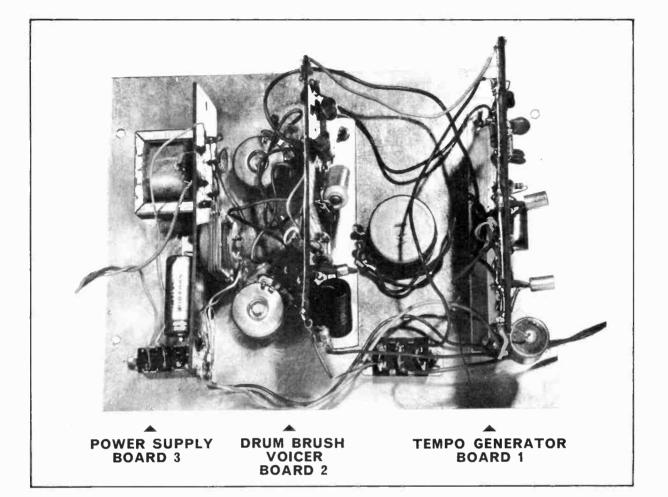
Fig. 3. Component assembly and wiring details for power supply board





generator and beat voicer circuits





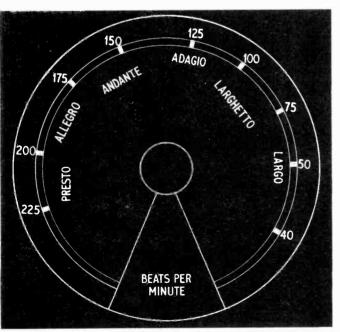


Fig. 7. Tempo calibration scale which can be cut out and pasted on the front panel

carries the multivibrator and beat voicer (TR3) and Board 2 contains the white noise generator and drum brush voicer (TR4).

The prototype was built into a case approximately  $8 \text{ in } \times 6 \text{ in } \times 4 \text{ in.}$  Board interwiring and the layout of the front panel components is given in Fig. 6.

Note that VRI, which is a log potentiometer, is wired so that tempo increases with anti-clockwise rotation. This arrangement was found to provide a more linear calibration for the beats per minute scale. The scale is reproduced in Fig. 7 and can be cut out and used with the specified tempo potentiometer VRI.

# OSCILLOGRAMS AND VOICE VARIATIONS

To check the correct circuit functioning the oscillograms in Fig. 1 should be found by monitoring at the letter reference points. Of course, depending on the time base speed of the oscilloscope used, there may be some departure from these shapes.

Some adjustment can be made to the voicing. For example, the pitch of the metronome beat can be raised or lowered slightly by slightly changing the value of R8.

The drum brush voicing can be made sharper by omitting C13 and connecting a 200pF mica capacitor between the collector and base of TR4. The variable controls VR2 and VR3 will provide a more than sufficient range of attack and decay requirements.

It is nearly 100 years since Bell demonstrated the first working telephone at Philadelphia. It was the culmination of many experiments with sound waves in search of a method by which deaf children might be taught to speak, and was the practical application of an idea by Charles G. Page in 1837 that electric current might carry sound.

The receiver used was a simple device enabling variations in electric current to produce magnetic attractions of related strength and frequency to a metal disc. The resulting piston-like vibrations of the disc modulated the air pressure between the disc and the ear of the person listening and produced intelligible sound, but it was necessary to place the earphone against the ear to hear the sounds clearly.

Further sound amplification was obtained by adding a megaphone-shaped horn to an appropriately modified earphone so that several people could hear the sound at the same time, and thus the earphone was turned into a loudspeaker. Alas, the sound it produced was far from a faithful reproduction of the original, and engineers were challenged with the task of improving the sound reproduced in order to satisfy the needs of the rapidly developing electric gramophone, talking pictures and wireless receiver.

# MOVING COIL SPEAKERS

The horn speaker was gradually replaced by a reed-driven cone speaker which could be mounted inside the same cabinet that would contain the radio receiver or gramophone. Still the quality left much to be desired and the moving iron type of drive unit was eventually superseded by the moving coil system very similar to that being used today.

In its early stages the magnetism of the moving coil speaker was provided by a large coil energised by the h.t. current of the receiver amplifier. This was necessary because at that time permanent magnet material was not very efficient and proved too expensive for the popular speakers.

Advances in both magnet steel and later the development of ferrite ceramics has resulted in the replacement of the energised magnet by the now total use of permanent magnets. These are applied in two basic ways, the screened magnet system Fig. 1 and the unscreened magnet system Fig. 2.

The screened magnet type of loudspeaker is particularly useful in transistor portables and similar equipment, where the loudspeaker is in close

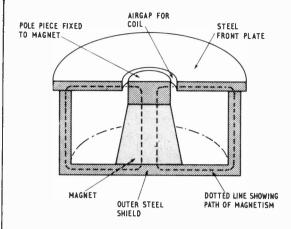


Fig. 1. Cutaway view of shielded magnet

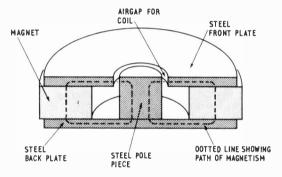


Fig. 2. Cutaway view of unshielded ceramic magnet

proximity to components such as coils and aerials with ferrite cores, which would be affected in performance by stray magnetism. Fortunately, this problem does not exist with speakers housed in separate enclosures, so unscreened ceramic magnet systems are commonly used in these types with a saving in cost over equivalent steel magnet types.

Advances in knowledge of electronic sound reproduction and manufacturing techniques, and a steady improvement in the characteristics of materials used

# LOUDSPEAKERS

By H. E. BARNES

(E.M.I. Sound Products Ltd.)

has resulted in the modern speaker having improved frequency response, efficiency and power output. The most popular loudspeaker unit uses the moving coil system of drive and the explanations which follow apply to this particular type.

Before dealing with the technical details of units and completed loudspeaker systems in enclosures, a general appreciation might prove useful, particularly

to newcomers to hi fi.

# **OPERATING PRINCIPLES**

The diagram Fig. 3 shows the important details of a moving coil speaker unit. It consists of a rigid frame or chassis, the front edge of which has a flange for fixing the chassis to the baffle board of an enclosure. At the rear of the chassis is the magnet system, which generates magnetic field in a circular gap formed between the centre pole and the front plate of the system, this plate being firmly attached to the chassis.

The diaphragm used to generate the sound waves is usually cone shaped, although it may be dome shaped in some high frequency speaker units. It is fixed at its outer edge to a flexible section of material which in turn is fixed to the flange of the chassis.

The inner portion of the cone or diaphragm is attached to a lightweight tube upon which a coil of copper or aluminium wire is wound. A circular flexible suspension diaphragm keeps the coil clear of the magnet system parts by centring the coil around the pole. The combination of the front and rear suspensions enables the cone and coil to move backwards and forwards under control.

The ends of the coil are attached to flexible connecting leads to which the amplifier is ultimately connected. The output signal from the audio amplifier comprises a complex series of alternating currents which pass through the speaker coil (or speech coil

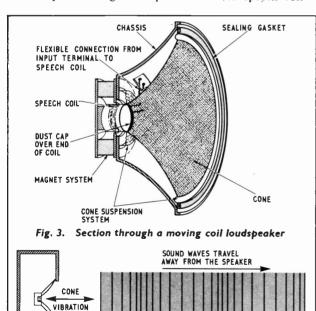
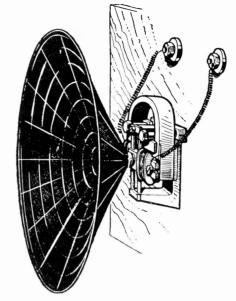


Fig. 4. How piston action of the cone creates sound pressure waves

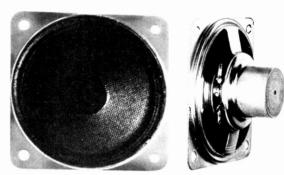
LOW

AIR PRESSURE WAVES

LOW



An early direct radiator loudspeaker by Celestion



Popular small Plessey 3in loudspeaker frequently used as inexpensive tweeters or as pocket radio speakers

as it is also called), driving it and the cone to and fro in a similar complex series of vibrations.

Since the cone is in contact with air, its vibrations are transmitted in the form of pressure waves to the listeners' ears, Fig. 4. The type of sound one hears depends upon the nature of the pressure waves. The purpose of the whole audio reproducing system is ultimately to regenerate sounds of a loudness and quality as closely resembling the original as possible.

In the case of bass frequencies, the air is displaced at comparatively low speeds. To obtain the required loudness, a much greater amount of air has to be moved per cone movement than at higher frequencies. Without a baffle board around the speaker orifice, air movement at the front of the cone would interfere with that at the back. The neatest form of baffle is usually that shaped into a box and is most effective when it is a sealed box, so that no air movement from the front of the cone can interfere with that at the back of the cone.

# FREQUENCY RESPONSE

Sounds audible to a good human ear range from approximately 30Hz to 20kHz and loudspeaker units can vary considerably in the way they produce this sound spectrum, mainly due to the characteristics of the materials used in speaker manufacture. Some units are designed primarily to reproduce their best at the bass end of the audible range, say, up to 500Hz. There are mid-range units designed to cover

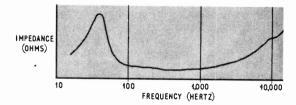


Fig. 5a. Impedance characteristic of a typical single speaker of wide range compared on the same scale with Fig. 5b below

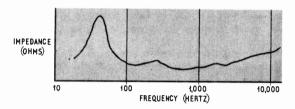


Fig. 5b. Impedance characteristic of a typical complete three-speaker system. Crossover frequencies are shown by the slight humps at approximately 250Hz and 2kHz

500Hz to 5kHz for example, and high frequency units complete the audio range from 5kHz to 20kHz. There are also units which cover wider frequency ranges in each classification. It is possible to have a loudspeaker with one unit which has a limited range from, say, 100Hz to 10kHz or two complementary types of unit, with a crossover frequency network, covering from, say, 50Hz to 15kHz. Three types of units, with two crossover frequency networks, could cover a wide range from, say, 40Hz to 20kHz.

The crossover frequency networks are usually specified by the manufacturer to suit the frequency responses of the individual speaker units. The frequency of crossover is chosen so that the response of one unit is cut as the next one is introduced to give a smooth overall response.

# **IMPEDANCE**

The electrical resistance provided by the speech coil to the applied alternating drive current is the impedance, which is measured in ohms. Because it is the result of coil resistance and the effect of induced voltage in the coil when it vibrates, it is not constant in value over the frequency range of the speaker.

At the lower end of the frequency range of any particular unit, the moving system reaches a point of resonance where the amplitude of vibration is easily maintained for comparatively little input energy. This can produce a point of higher impedance than normal. Similarly, towards the upper end of the frequency range of the unit, the impedance can tend to rise (Fig. 5). The manufacturer generally quotes a nominal value which is usually 400Hz for a bass unit. This is not necessarily the lowest value but normally the difference is small enough to be ignored.

# **MAGNET STRENGTH**

The performance of a speaker for sensitivity and overall frequency response depends a lot upon the power of the magnet system, because the current in the coil reacts with the magnetic field to produce the mechanical vibrations of the cone.

Speakers have various sizes of coil from about in up to 3in diameter depending upon their function in the system and the amount of acoustic power they have to produce. In general the larger the total lines of force (larger magnet), the more likely the speaker is to have a superior performance.

# **FUNDAMENTAL RESONANCE**

All speaker units have a fundamental resonance. This is of particular importance in the case of the bass speakers because it has a direct bearing upon the bass response of the loudspeaker in an enclosure.

One should select a speaker unit whose bass resonance is as low as possible so that the final resonance in the enclosure is also kept low, otherwise the sound will lack bass quality.

The aim should be to produce a completed speaker with a bass resonance below 100Hz, and this can normally be achieved in infinite baffle enclosures with units which have a fundamental free air resonance of 35Hz or less.



EMI 215 system incorporating a  $14in \times 9in$  elliptical bass unit, two 5in mid-range units, a moulded chassis high frequency unit, and crossover network

# **EFFICIENCY**

Efficiency is the relationship between electrical power input to the loudspeaker and its sound power output in equivalent units. For example, a 10 watt power input into a speaker having 10 per cent efficiency will result in one tenth of the input power leaving the speaker as acoustic power—in this case, 1 watt.

Loudspeaker manufacturers rarely quote efficiency figures but as a general rule a unit with a large magnet can have an efficiency of 5 per cent for an 8-inch round unit and about 10 per cent for a 12-inch round unit. Bear in mind, however, that this figure is for total radiated sound power from the unit. When it is fitted into an enclosure only about a half of this power is radiated; the other half is absorbed in the enclosure. The efficiency, therefore, of the complete speaker is half that of the unit in free air.

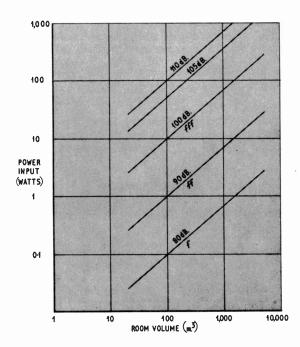


Fig. 6. Electrical input required for a speaker of 5 per cent efficiency related to room volume and sound intensity within

# **POWER RATING**

The loudspeaker is usually rated in terms of the amplifier which can be used to drive it. If the amplifier is rated at 15 watts r.m.s. maximum at, say, 0.1 per cent total harmonic distortion at 4 ohms impedance, then the loudspeaker will need to have a nominal impedance of 4 ohms and a rating of 15 watts r.m.s. at least. It is not wise to use a loudspeaker with a lower watts rating than the amplifier (each channel in the case of stereo) otherwise the life of the speaker may be reduced.

Many studies have been made by acoustic engineers which have resulted in a relationship being established between power input to a speaker and the loudness of the sound it produces in an average furnished room of known dimensions. This is called acoustic intensity, which is the effect of air pressure waves at the point it is measured. Units are measured in decibels (dB) where 0dB represents the reference intensity level equivalent to  $10^{-16}$  watts per square centimetre.

It has been established that an intensity level of 100dB is extremely loud fff in musical terms. 90dB is very loud, ff in musical terms. 80dB is loud, f in musical terms.

# POWER DRIVE REQUIREMENT

The results of the studies have concluded with a mathematical relationship between room volume and acoustic intensity, so that if we know the efficiency of a loudspeaker we can obtain a close approximation to the input power required. For the data (Fig. 6), an efficiency of 5 per cent for the loudspeaker unit in free air is assumed. The reader can make proportional adjustment to suit. If he has a speaker with 10 per cent efficiency, the input power for a given loudness will be halved.

Remember that the data give the power requirements for one loudspeaker. When stereo is used, theoretically the total power required will be shared equally between the two speakers and amplifier channels. In practice a degree of uneven sound absorption occurs, and it is recommended that each channel is rated at 50 per cent more than the theoretical amount to avoid overload on either channel when the loudness of the channels is corrected by the balance control.

Taking an example, a room with a volume of 100 cubic metres will require a total input power of 10 watts to give a level of 100dB intensity. If you have a stereo system, each channel will then be rated at 7½ watts r.m.s. If you double the power available you will raise the maximum level to 103dB which does not look much on this scale, and the increase in loudness is just noticeable. Having attained this level of loudness it would cost more money to obtain any marked increase than would be worthwhile.

# LOUDSPEAKER ENCLOSURES

If you intend to construct a loudspeaker enclosure with speaker units of your own choice it would be wisest to build an infinite baffle type, which is free from tuning problems. Vented cabinets can give low bass frequency response but unless one is prepared to experiment it is easy to spoil the quality of the bass response.

The principle of the infinite baffle enclosure is to seal the speaker units in a rigid walled box so



Cutaway view of a Tannoy folded horn enclosure used with a 15in dual concentric unit

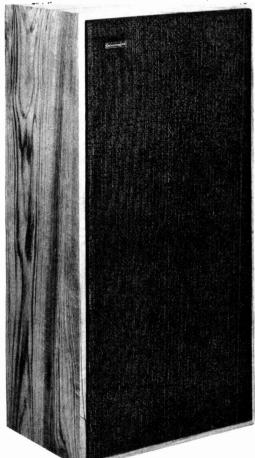
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44 Watts (D45.500)

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Crossover:

4 to 6 011111S

Treble:

500 & 5,000 Hz HF2,000 (pressure)

Mid:

MF Super 5"

Bass:

.... Oupoi o

Finish:

LF Long drive 12"

\_ \_ \_

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Left to Right: Ditton 10 Mark II, Ditton 120, Ditton 15, Ditton 44, Ditton 25.



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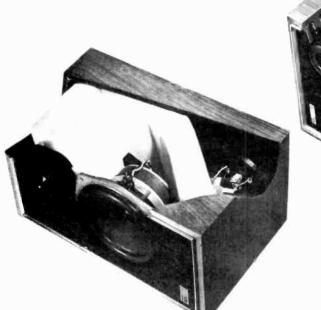
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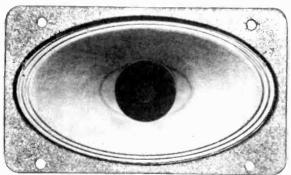


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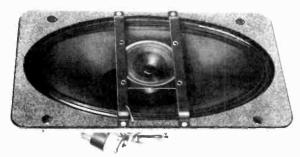
A fairly recent innovation in extending bass response down to 30Hz is achieved by using an auxiliary bass radiator (right) of similar dimensions to the mid range unit. In this Celestion system (Ditton 15) the ABR is a rigid diaphragm with a linear air suspension capable of large excursions. It is pressure driven by the rear radiation from the adjacent 8 in bass unit



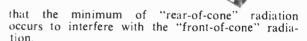
Very good results are obtained by padding a small enclosure with plastics foam as shown in this photograph of the Ditton 10. Notice the rolled neoprene suspension on the cone of the larger unit to give optimum excursion capability



Elliptical speaker ( $13\frac{1}{2} \times 8\frac{1}{4}$ in) with parasitic concentric tweeter — E.M.I. type I 50



Elliptical speaker with coaxially mounted  $3\frac{1}{4}$  in h.f. unit and crossover unit — E.M.I. type 350



Loudspeaker manufacturers give guidance on enclosure volumes suitable for their units which will give the best results and they often quote examples of enclosure construction. As a general rule, the enclosure walls should be as rigid as possible, and internally lined with absorbent material such as glass wool or acoustic wadding, to prevent reflections of sound back through the speaker cone. All joints of the enclosure and points of entry should be sealed and care should be taken to make sure the speaker units are also sealed to the baffle board.

#### **MULTI UNITS**

Should your loudspeaker contain a combination of units, place the mid-frequency and high-frequency units off centre in unequal amounts to reduce effects of reflection from the enclosure edges. The mounting of the high frequency unit is usually quite critical and unless you have special equipment for response testing, it is difficult to obtain an optimum result. However, if you mount the unit on the front surface of the baffle board this will be better usually than if it is sunk in a tunnel of baffle board thickness (i.e. on the rear surface of the baffle board).

Make sure all leads are correctly connected and internal components are unable to produce buzzing sounds by vibrating. Keep them completely clear of the speaker units and clamp them firmly to adjacent surfaces, preferably with felt or foam rubber mounting cushions.

There is no mystery around the efficiency of loudspeaker systems; having understood basic principles and peculiarities in certain operating conditions, a great deal of common sense and help from published books will help the reader devise a system to suit his needs. This last part shows how a "fire" is indicated and offers some ideas on how added "realism" can be effected by producing suitable battle sounds. Operational tactics are also given.

#### STAGE SEVEN—FIRE

One third of the positions of the Ledex switch will pass current to Panel D (Fig. 17). The leading edge of this current is shaped by the differentiator circuit C30, R120 and passed to a ten second timing circuit. One has already been given (Fig. 10) and here is another. The shaped pulse switches a bistable formed by TR25 and TR26. The result is a slow charge of C31. The trigger formed by TR27 and TR28 finally fires, switching the bistable off again. While the bistable was on it primed the lamp driver TR29 and TR30 and also delivered a charge to the magazine storage capacitors through D13 and R129.

In play, some of the damage indications will be accompanied by a fire indication. The player can do nothing about the fire but watch and wait. If he is lucky, the lamp will go out in ten seconds with nothing untoward happening. If he is unlucky, the charge on his magazine storage capacitor will reach the critical value and the magazine lamp will glow, putting him out of the game.

#### SOUND EFFECTS

Because of the belief that many constructors will want to add sound effects, the writer has spent some time experimenting with circuitry to do this. Various conclusions emerge. First, it would be annoying for sound to be emitted all the time. An on-off switch might serve, but the easiest method would be for sound to be emitted only during dialling. Secondly, hum and noise, oscillation and warble are not unacceptable in the war situation, if suitably filtered or chopped, so nothing elaborate is called for.

Taking off through a  $0.1\mu F$  capacitor at the point (f) indicated in Fig. 3 is satisfactory only at heavier calibre settings, when the sound is like a heavy machine gun. At lighter calibres a buzz is emitted, as would be expected from the higher frequency. Such noises are of course intermittent as the pulse contacts on the dial open and close and do give some indication of hits scored. Figure 18 is given for those who might like to experiment further.

Taking off from point (k) (Fig. 12) gives an indication of damage pulses. As such it is useful, but

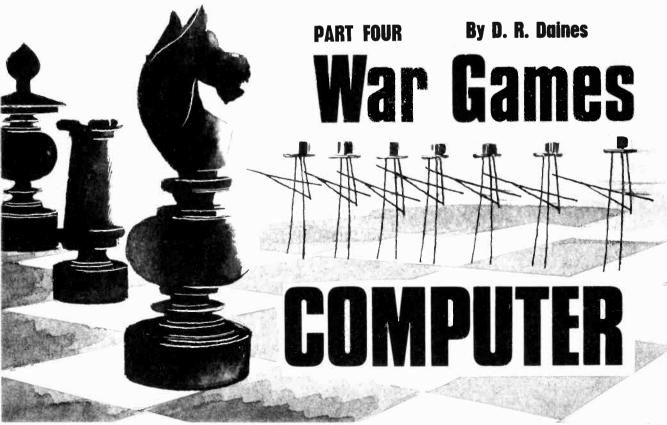
again, not very realistic.

Examining the back of a telephone dial reveals a third pair of contacts that, like the ones that motivate the Ledex, close when dialling commences. If sound effects are desired the best method is a simple multivibrator giving good voltage swing and of appropriate frequency feeding directly into a permanent magnet loudspeaker and keyed from the dial (Fig. 19).

#### PLAYING TABLE

For a full treatment of the subject the reader is referred to any of the books on war games, particularly "Naval War Games" by Featherstone (Stanley Paul, London, 1969). Here we can give only a sufficient outline. The first requirement is a playing board as large as possible and preferably marked in inch squares. Several sheets of card would do, or even a roll of ceiling paper.

If desired, shallows, rocks, islands and coastlines are marked in. Minefields might also be "laid" by each side and their position not divulged to the opponent. A token for each ship is required, clearly numbered. Simple card shapes will suffice, although for many it could be the beginning of a collection of any of the excellent little models available.



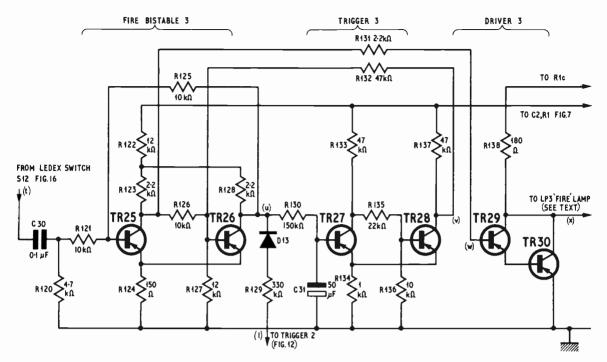


Fig. 17a. Fire indicating circuit on Panel "D"

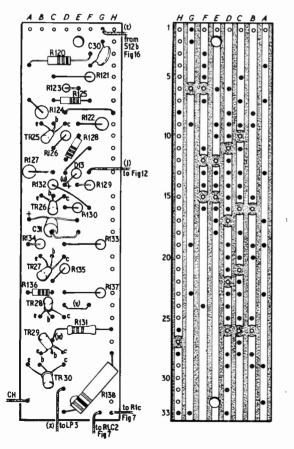
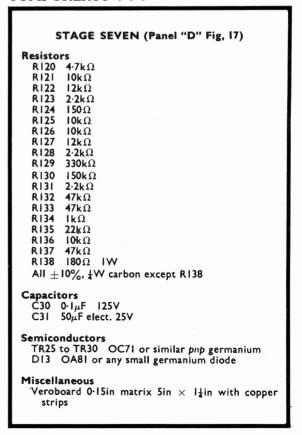


Fig. 17b. Layout of Panel D and cuts in the copper strips

#### COMPONENTS . . .



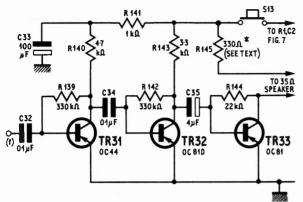


Fig. 18a. Experimental sound effects amplifier

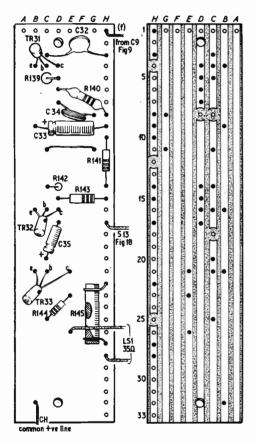


Fig. 18b. Layout of experimental amplifier boards and cuts in the copper strips

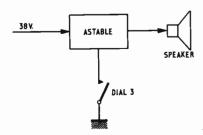


Fig. 19. Using an astable multivibrator switched into use by dial contact in the common chassis line

#### COMPONENTS . . .

STAGE EIGHT (Experimental sound effects amplifier)					
Resistors					
R139 330kΩ					
R140 4·7Ω					
RI4I IkΩ					
R142 330kΩ					
R143 3·3kΩ					
R144 22kΩ					
R145 330Ω (for 35 ohm LS)					
Capacitors C32 0·1μF 125V C33 100μF elect. 25V C34 0·1μF 125V C35 4μF elect. 25V					
Semiconductors					
TR31 OC44					
TR32 OC81D					
TR33 OC81					
Miscellaneous  LSI Small 35-40 ohm loudspeaker  Veroboard 0·15in matrix 5in × 1½in with copper strips					

Note: The lamps 6 and 7 should be "Double chance" and lamps 8 and 11 should be "Single chance", and not as indicated on page 816, October issue.

not as indicated on page 816, October issue.
On page 810, half way through "STAGE FOUR—PANEL B", should read "Capacitor C11 blocks d.c. and leaves only pulses swinging about zero volts . . ."

#### **SCORE CARDS**

Finally a score card for each ship is needed upon which is marked full details of armament, torpedo tubes, aircraft carried and thickness of belt armour. Speed is also marked, scaled down to inches per move at full speed, and turning circle, expressed as a 45 degree turn every so many squares. Examples are given in Table 1.

On the reverse side of the card a sketch plan of the ship is made, clearly showing the position and sweep of all turrets and torpedo tubes. When the card is complete it may be covered with clear adhesive tape or sheet and used over and over for many years. Details as required may be obtained from any public library.

Size	Name	Speed (in/move)	Turning distance (for 45°)
Battleship	Vanguard	3in	4in
Carrier	Eagle	4in	3in
Cruiser	Essex	5in	3in
Destroyer	Ajax	7in	2in
Submarine	Neptune	surface 4in submerged	2in
		2in	2in
M.T.B.	T107	8in	lin

When all is ready, tokens are placed on the board and play begins. Dice are rolled to determine the state of the sea and the visibility. The dice reading is transferred directly to the computer, and agreement reached as to how often this shall be done. Usually they are rolled for every ten moves. Both CANCEL switches are put in the cancel position and S11 (target number) slowly rotated all the way round, ensuring that all storage capacitors are completely discharged. A coin is tossed, the winner deciding whether to go first or last. Player A moves; player B moves; player A fires; player B fires. Damage is recorded and the coin tossed again. Play continues until one ship or the other is sunk.

#### USING THE COMPUTER

When either player fires, the computer is set up as follows:

Target number corresponds to the number of the token and so must be carefully chosen at the outset.

Target speed is a direct reading in inches and is the speed the vessel is actually supposed to be going (which might be less than its possible maximum).

Armour thickness is taken from the score card and is a direct transfer in inches, as indicated by the knob.

Target size: twelve types of ship are given and

the nearest in size to the target is registered.

The angle subtended is the angle the target ship makes to the line of fire; 90 degrees is broadside on, while 180 degrees is bow or stern on; 45 degrees is provided as a halfway condition. There is no need to get a protractor out; simply set the control to the nearest position. Range is directly read in inches and is quickly counted along the inch squares.

Firing ship's speed is also the actual speed

indicated by movement in inches.

Morale is determined by dice throw for each ship at the commencement of the game and goes up or down according to the fortunes of war. If damage is inflicted on the enemy, morale goes up one point; if damage is sustained it goes down one point.

Shell type is a conscious choice of HE or AP,

while calibre is obtained from the score card.

The whole operation takes less time to do than to read about and when all controls have been quickly set, the number of guns is dialled. This is where the indication of sweep of turrets comes in, for not all turrets will be able to bear upon the target and if in doubt the score card is laid over the token and a straight-edge laid along the extremes of the arc.

Check that both CANCEL switches are off and dial the number of guns firing and able to bear. The result (if any) is immediately indicated in one or more lamps lighting up.

#### **EFFECT OF DAMAGE**

If the score card has been covered with clear plastics sheet, Chinagraph pencil may be used on it and wiped off after each game. The effect of damage is as follows:

Conning Tower. Cease firing all main armament for the number of turns determined by a throw of a dice.

Hull. Reduce speed by one-quarter.

Engine Room. Halt for the number of turns determined by a throw of dice.

**Rudder.** Proceed only in a circle for the number of turns determined by the throw of dice.

Aircraft or Torpedo tube. Opponent decides which he wants knocked out; you choose a particular one.

Sub-Armament. One-quarter of all sub-armament is knocked out.

Forward Turret. One forward turret of main armament is knocked out.

**Rear Turret.** One rear turret is knocked out.

When the appropriate notes and action are taken the CANCEL OTHERS switch is thrown, extinguishing the lamp. If preferred, double-pole push-buttons might be used instead of switches, thereby ensuring that they cannot accidentally be left in the cancel position.

If a fire is indicated, no action can be taken, but it will always be indicated in association with one of the above.

#### **VARIATIONS**

Some variations to the game have already been indicated and further variations are limited only by the imagination of the users. Players may have any number of ships under their command and if imagination lags there is always history to turn to. Try running a convoy through a pack of submarines to a particular port, or fight the battles of Jutland, Midway, Otranto, Coromandel or Falkland Islands over again.

#### MINES AND TORPEDOES

From the moment of firing a torpedo has a life of its own. A token with arrow showing direction is placed on the board and it must always follow a straight line course. In the first move it travels 6in, in its second move 5in, then 4in and then is assumed to be lost.

If it strikes a target, the computer is set for best conditions and a ten is dialled. The result is almost certainly indicated damage, but only damage below the water-line is accepted, i.e. engine room, hull, rudder, or magazine. All other damage is ignored; likewise with mines. If a ship enters a square in which is supposed to be a mine, the opponent produces his previously prepared note of mine positions. Damage is found by dialling under the same conditions and with the same provisos.

#### SUBMARINES

One side of the playing token could be painted black. If this is placed uppermost the submarine is deemed to be submerged. One move is required to submerge or to surface. While submergd she is considered undetectable although she may fire torpedoes. As for striking back at submarines, readers might like to devise their own rules.

#### FIGHTING OTHER BATTLES

As mentioned at the outset, the computer may be used for other wars and other periods, land as well as sea. Adaptation is simply accomplished by the use of card overlays that alter the readings of some controls and readout lamps.

The cards simply fit over the faces of the computer with the lamps shining through holes. In the case of the card altering the controls it will be necessary to remove the appropriate knob first.

#### **NEW PCB SERVICE**

All eyes will be on the Inter/ Nepcon exhibition at Brighton this month (October 19-21). It certainly is the most successful specialised exhibition of recent years and attracts production engineers not only from British companies but also in substantial numbers from the Continent.

One of the regular exhibitors is Exacta Circuits Ltd. who, since starting up in 1962 with two men, has climbed up to be in the top three independent printed circuit board manufacturers in the country, specialising in high-quality plated-through-hole and multilayer boards. Having outgrown their old factory (a converted textile mill) in Galashiels, the company moved most of the production staff and equipment to a brand new purpose-built factory at Selkirk in August, leaving the Galashiels premises as a bulk store and small-run production unit.

Inter/Nepcon is the occasion chosen to launch Exactaplan, a new service to cut costs and speed delivery to the small man who wants quality boards by the hundred rather than the thousands. Alan Bruce, Exacta's technical director, told me during a sneak preview that Exactaplan, though appearing almost ridiculously simple and obvious, was quite a tough nut to crack. The idea is to mass produce a range of standard PCBs with a grid pattern already printed on them. From the range. the circuit designer need only select that nearest his needs and indicate which interconnections he desires.

In small batch production, the precision art work is quite a high proportion of the total cost. Exactaplan cuts artwork costs and saves time too.

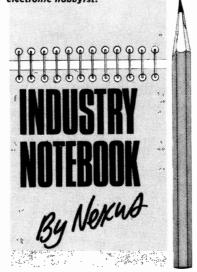
Exactaplan is being launched with 12 different board sizes, two packaging densities (i.e. standard and fine line) and three types of connectors which together give a choice of 72 boards.

#### WHO WAS FIRST?

The great excitement generated a few weeks ago by the almost simultaneous announcements from a number of power supply manufacturers of a breakthrough in "transformerless" solid-state power units brought a wry smile to the lips of Dennis Hendry, managing director of Weir Electronics. Weir had, in fact, been in production with similar units for many months but as they were part of a contract order for a special customer, the company was precluded from giving them any publicity.

Weir Electronics is one of the few companies that has thrived throughout the general recession in the capital goods electronics OUR new feature INDUSTRY NOTEBOOK appears this month for the first time. May P.E. readers work in the electronics industry and, indeed, are professional electronic engineers and technicians. Others, though perhaps professionally occupied in other ways will, we believe, also welcome news and views on the electronics industry.

Our regular contributor, Nexus, is close to the industry, both in its technical and commercial aspects. Month by month he will report and comment on significant events, on current trends, on how he sees the future and, where appropriate, how new developments may inspire the electronic hobbyist.



industry. Hendry told me Weir is making a profit of over £60,000 p.a. on capital employed of only £130,000. Some fat export contracts are helping enormously and negotiations are in hand for purchasing a production unit in Holland, which will become Weir's forward base for a drive into Europe.

The smaller companies like Weir, with their greater flexibility and faster response time in meeting changing markets are at least spared the present miseries of the giants.

#### WHIZZ-KID OF THE EAST

One of the most remarkable men in the industry has his base over a row of shops in Ealing Broadway, West London. When you enter his office you can't help seeing the magnificent wild boar's head on the wall, the many other souvenirs including a photo of your host shaking hands with Harold Wilson, a smoker's compendium in the form of a wooden model train from the Soviet Union, a fine leather case containing his shot-guns.

His name is Eddie Baizert and he is owner and managing director of a group of companies operating under the generic name Uni-Export. Baizert is now a British subject but was born in Norway and reached these shores via the Middle East. He is a linguist with fluent Russian and Czech and spends most of his time getting orders for British electronic equipment from the Eastern Bloc.

His favourite souvenir, framed and hanging by his desk, is the cheque for £500 with which he started in 1961. There was only himself and a secretary. Now he has a staff of 14 at Ealing and three people in his office in Prague. His first sale was a telephone answering unit worth £25. Today Uni-Export turns over £1 million a year.

He handles all the best names in British equipment, bears all the cost of advertising, exhibition stands and all the other incidentals involved in selling and if he doesn't sell he doesn't charge a bean. You can't be fairer than that—but, as he smilingly points out, Baizert always sells and gets his 15 percent commission.

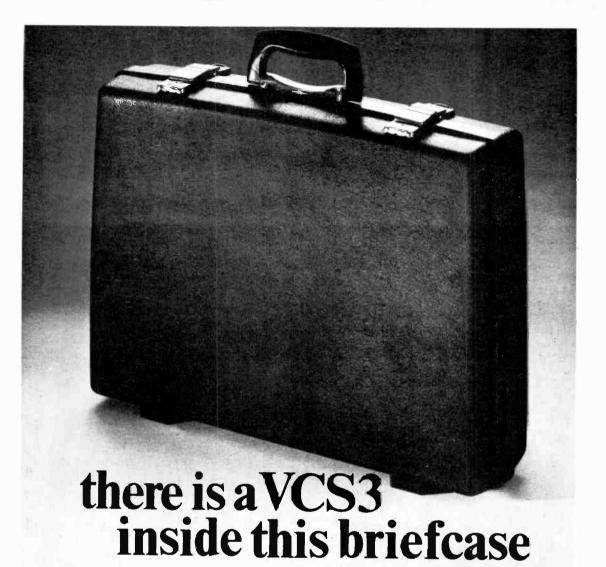
To keep his eye on the international scene he likes to travel round the world twice a year and normally clocks up 100k miles in his E-Type Jaguar in Europe for good measure.

#### NC STILL STRUGGLING

The much-publicised Pre-production Scheme devised by the old Mintech to put numerically-controlled machine tools on the map in Britain cost the tax-payer £2 million and went off like a damp squib. The IRC had a qo at rationalising the industry with a splendid investment of your money and mine. And yet with all the effort and all the cash that has gone in, the numerical control business is still as flat as a pancake.

My sympathy goes to Plessey Numerical Controls which now incorporates all the business and types of equipment (most of it non-compatible) handled by Ferranti and Airmec-AEI as well as the original Plessey product lines. The general recession in the engineering industry is the culprit and, as it turned out, PNC could not have been formed at a worse time.

Nevertheless, morale remains high at PNC headquarters at Poole, even though it is rock-bottom at what was to be the main production unit in Scotland, now threatened with closure. Sales may be slack but it has been a good opportunity to start rationalising the product line, identifying new marketing slots, and preparing for the expected up-turn next year.





Do you remember the VCS3? It was the portable synthesizer from Electronic Music Studios that brought you the whole spectrum of electronic music effects.

Now the VCS3 has become even more portable in the briefcase guise of the Synthi A, but it still contains the same array of electronic devices and yet only costs £250.

With Synthi A the synthesizer becomes available to anyone and everyone with an interest in the excitement of electronic music.

For information contact Electronic Music Studios (London) Limited, 49 Deodar Road, London, SW15. Telephone 01-874 2363

The Synthi Range by

**EMS** 

# MAIL ORDER DIVISION

28 BURNT MILL HARLOW ESSEX **HARLOW 32947** 

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15p

10p

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7p

40p

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£1.50

20p

£1.25

#### OUR ORDERS wait weeks? - ALL OF POST! DISPATCHED BY RETURN Why

Transistors, Diodes and Integrated Circuits

Transist	Ors, Diods	IIP BFX86	30p	2N3055	Amp
. 51971	Matched BC	20p BFX87	30P	115 Watt 15	22p
A) DIODERE ACISS	NJ PILES BC114	20p BFX00 25p BFY34	30p	2N3053 I Amp TO-5	
INIA001 7P AC192	15p BC115	30p			
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BDI	2/ DE BC14	2	50 <b>22p</b>	1 (2) DI	NP Matched
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our prices AFIG	06 350 BC14	300 REY	752 20p 0404-1 12p	10 Watts.	AUDIO OUTPUT
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2N2369 20P	NAME OF TAXABLE PARTY.		ME8003	OP	LA
2N2407 45p	Component E	Discoulits	ME3001	5p   30 Am	p, 150 Volts
2N2904	10% on order	s over £3	MELII	40p	
2N2707A 46p		A STATE OF THE PARTY OF THE PAR	MEL12	40p I Ami	, 100 Volts
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2N3055 70p	AU106 70p	BCY71 26p BCY72 25p	OC25		
2N3442	AU108 93P	20157	C) INTEGRAT	ED BFY5	
2N3638 £1.50	AU110 70p	BF153	CIRCUITS	2N38	366 att output at 400
2N4347 £1750	AUYZIA BOP	BF158 BF159 35p	709C (TO-9'	950	
2N4356 40411 £2:50	AUY22A 45p AUY35 40p	BF160 250		9) Hig	h gain: 200 at ImA
AC138 13P	AUY37	BF178 35p	- 11 C (DIP)	(1.25	
AC141 250	BC 107	DE179C			or TO-99 h gain operational
AC141H 25p AC142 15p	BC108	. C. ADD 100 T	O YOUR OF	RDER   HIE	proof
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Watt output at 400MHz

High gain operational amp. S/C proof





#### PLANTS AREN'T DEAF?

Since, to the delight of farmers, the effects of playing dance records while lightening milk-laden cows has improved both quality and yield, the scene seems to have switched from the, now tranquil, ruminant to attempts at inducing a similar effect in flora.

It was in India, in fact, that some years ago changes for the better were reported in rice plant yield following about an hour per day musical treatment of the cereal. Since then most experiments have been performed at ultrasonic frequencies with fair success. The reason for the effect is not fully understood, but in part appears due to an increase in the activity of various enzymes associated with the plants growth.

Since the original tests, experiments at audio frequencies have been resumed by two Canadian workers in Ottawa. They have employed at least four different frequencies for continuously irradiating wheatseeds during a period of time (termed vernalisation) when dampened seeds are deliberately reduced to a low temperature to cause early flowering.

Following several weeks of this treatment the seeds are allowed to germinate and the resulting seedlings permitted a period of eight weeks growth. Subsequent measurement of such things as height, weight, number and size of leaves, has revealed a dramatic improvement over normally treated varieties. It is reported that the most effective stimulation frequency is around 5kHz. This has produced in excess of 200 per cent yield over the plants used as controls.

Believe me, I've tried directing the output of my old record player at the wallflower patch, but alas, other than some raised eyebrows from already curious neighbours, no go. "Raindrops keep falling on my head" and the "Ooh ah" of the bicycling tune had a remarkable effect on the groundsel though!—Perhaps the term 'ear' of the wheat is meaningful after all!

#### TIME FOR A CHANGE

There can be but few professions that share the degree to which electronics serves industry; not only industry, but the professions too. Think for example, just how much electronics is now at the "beck and call" of the biological professions. Sure the biologies have given of themselves many times to mankind, however, what of their help to other sciences?

As a change wouldn't it be great if instead, say, of relying on electric motors and hydraulics for prime-movers we employed lumps of cultured muscle tissue! It is not difficult to see what an asset such a material would be, particularly if it could be electrically triggered into contraction or extension.

Apart from the very obvious advantages for the physically handicapped, who would naturally be given priority to use the special muscle, imagine how quiet an automobile would be with this kind of propulsion.

#### MUSCLE POWER

Perhaps thankfully, no one has yet been able to grow muscle tissue on the scale suggested by my reverie, although I recall hearing of someone who went part-way to achieving something rather similar. He found that if a thin strip of collagen (obtained from animal connective tissue and cartilage) is placed in a strong solution of lithium bromide it will slowly contract with a force greater than 1,000 times its own weight. If it is then washed in clean water it will regain, once more, its original form. This process can be repeated, as far as I can remember, ad infinitum.

Actual motors have been built which employ the principle, and generally comprise an endless collagen tape loop running around six pulleys, or so. The tape is first arranged to enter a small tank of lithium bromide solution and, by virtue of a ratchet mechanism, the subsequent contraction pulls more (un-treated) tape into the tank. Simultaneously, since the whole tape will be on-the-move, treated tape can be drawn through yet another tank containing clean water and so complete the cycle.

Output drive is via one of the pulleys.

Just in case you reckon we might have got a perpetual motion device on our hands, and appear scheduled to make some vast fortune, let me dispel the euphoria straight away! The machine will run for several hours, I gather, but ultimately comes to a halt when the tanks become contaminated with one anothers contents.

One day, who knows, someone might invent a mechano-chemical motor which is as successful as its neuro-muscular counterpart. Picture, if you will, the economics of a motor running almost indefinitely on packets of glucose tablets and the occasional mug of beef tea!



#### KEEPING A "BEAD" ON THE ADS

I thought it would only be a matter of time before TV advertisers (in the States, at least) dispensed with their "little old ladies" who diligently keep a daily check on the number of times an advert has been on the screen. A much more reliable, electronic, method of monitoring advertising has now come into being.

The ads are now tagged by a system which makes use of coded data, concealed from the public, and can be either added to an "off the picture" area of the raster, or inserted in the sound channel.

As an aid to advertisers, this holds little interest for me. However, it does of course imply that, because the code will accompany all advertising (eventually, no doubt, in this country as well) one only needs a "code present/absent detector" to automatically turn off vision and sound until programme material returns. The detector would, however, require a delayed "on period" because the code, unfortunately, only appears for a short time at the beginning and end of an ad. I just can't wait for this great new boon to reach the advertising industry!





By D. S. GIBBS and I. M. SHAW (Ferranti Ltd)

In the past 40 years the performance of car engines has been improved enormously, but the ignition system has hardly changed at all and is becoming inadequate to supply the demands of today's high performance engines. The system described here overcomes the limitations of the conventional (Kettering) system and it is suitable for all types of car, although the improvement will be greatest on high performance models.

#### THE CONVENTIONAL SYSTEM

Fig. 1a shows the conventional system. When the contact breaker closes current flows in the primary of the coil, and rises exponentially at a rate determined by the inductance and resistance of the transformer primary. Typical values are 1 ImH and 3.5 ohms giving a time constant (L/R) of about 3ms (Fig. 1b). After 3ms the current would rise to about 63 per cent of its maximum value; after 6ms it would be 87 per cent; and after 9ms it would have risen to 95 per cent of its final value of 3.4 amps.

When the contact breaker points open the current is suddenly interrupted and a high voltage (about 300V) is generated across the primary. This is stepped up to about 15-20kV at the secondary, and an arc forms between the plug electrodes.

At low and medium engine speeds this works perfectly well but at high engine speeds the current

in the coil does not have time to reach its full value. As an example, take a four cylinder engine going at 6,000 r.p.m. The engine needs two sparks per revolution which is 12,000 sparks/minute and the time between each spark is 5ms. Now the contact breaker points are open for 40 per cent of the time and closed for 60 per cent, so that at 6,000 r.p.m. the contact breaker points are closed for just 3ms. In this time the current in the coil primary can only reach 63 per cent of its low speed value, and if we take into account contact bounce and wear the figure is nearer 50 per cent. Nearly all modern four cylinder engines can reach 6,000 r.p.m., some can reach 7,000 or 8,000 r.p.m., and with a six cylinder engine the situation is still worse because this needs three sparks per revolution.

#### TRANSISTOR ASSISTED IGNITION

Many of the "bolt-on" electronic ignition systems consist of no more than a special high ratio coil switched by a high voltage transistor. The contact breaker is used to interrupt the base current of the transistor. These do give a higher kilovolt output at high r.p.m. and greatly reduced contact breaker wear but they require much more current, sometimes as much as 10-12A. This places a severe additional load on an already overburdened electrical system.

5 per cent more BHP

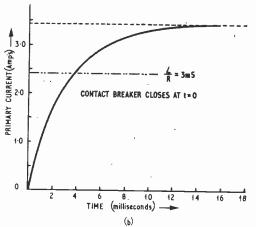


Fig. 1(a). The conventional ignition system. (b) graph of current rise with time in ignition coil primary

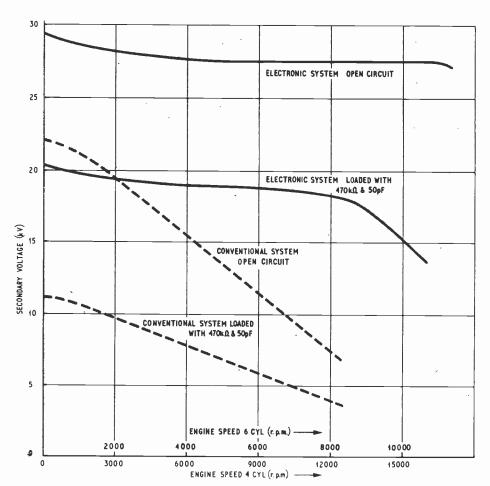
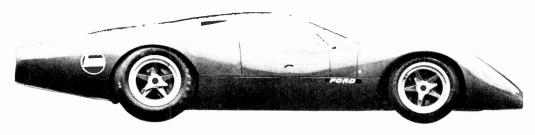
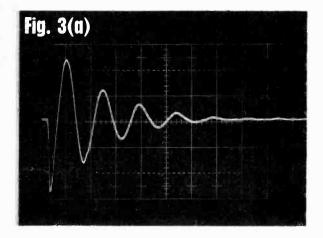


Fig. 2. Output voltage with engine speed for conventional and capacitor discharge systems





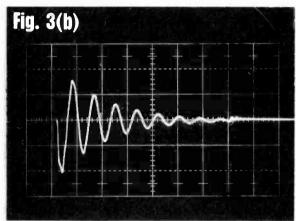


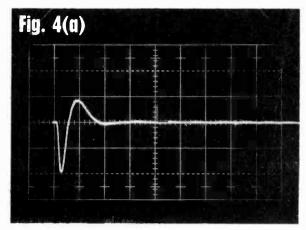
Fig. 3(a). Oscillogram of open circuit secondary voltage with electronic system. Vertical is 10kV/cm and horizontal  $200\mu s/cm$ . (b) open circuit secondary voltage with conventional system. Vertical is 10kV/cm and horizontal  $500\mu s/cm$ 

#### CAPACITOR DISCHARGE IGNITION

In the past few years another system has been gaining in popularity—the capacitor discharge system. In this system a transistor inverter is used to charge up a capacitor to about 400V. Energy is stored in the capacitor, and when the contact breaker opens, a silicon controlled rectifier is triggered and discharges the capacitor through the coil. This system has several important advantages:

- 1. The kilovolt output has a very fast rise time, typically 20-30 ns as compared with 100 ns for the conventional systems. This enables it to fire fouled plugs more easily and gives easier starting and smoother running when cold.
- 2. Low current drain. At low speeds it needs only about 1A, rising to 3-4A at very high speeds.
- 3. It will work with the ordinary ignition coil, a high ratio coil is not required, and in the unlikely event of failure the system can be put back to normal merely by reconnecting a few leads.

The circuit described here gives virtually constant output voltage over the whole speed range,



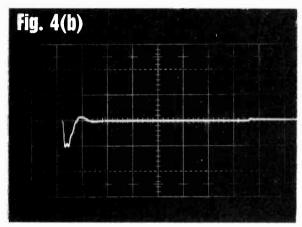


Fig. 4(a). Output voltage of electronic system loaded with 470k $\Omega$  and 40pF. Vertical is 10kV/cm and horizontal  $200\mu s/cm$ . (b) output voltage of conventional system loaded as before. Vertical is 10kV/cm and horizontal  $500\mu s/cm$ 

to over 10,000 r.p.m. for a four cylinder engine and 7,000 r.p.m. for six cylinder. This gives improved combustion and more accurate timing. The greatly reduced contact breaker wear allows the engine to remain "in tune" and improves the petrol consumption and power, and the contact breaker will not need adjustment for about 20,000 miles.

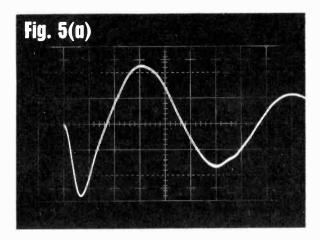
#### **PERFORMANCE**

Figs. 2 to 6 compare the performance of the capacitor discharge and the conventional system. Fig. 2 shows how the output voltage of the electronic system remains almost constant, and is still high enough to produce a good spark even when heavily loaded with a parallel combination of 470 kilohms and 50 picofarads (simulating a badly fouled plug). The prototype actually operated up to the equivalent of 15,000 r.p.m. (four cylinder) although the circuit is only designed to work up to two thirds of this speed.

In Figs. 3 and 4 are shown the actual secondary voltage waveforms obtained. Fig. 5 shows the much faster rise time of the electronic system.







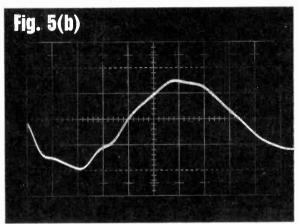


Fig. 5(a). Expansion of Fig. 3(a), showing rise time of electromic system. Vertical is 10kV/cm and horizontal  $50\mu s/cm$ . (b) expansion of Fig. 3(b) showing rise time of conventional system. Vertical is 10kV/cm and horizontal  $50\mu s/cm$ 

The spark current traces shown in Fig. 6 are particularly interesting. In the conventional system the spark current is unidirectional. This causes erosion of the sparking plug gaps due to deposition of metal from one electrode to the other.

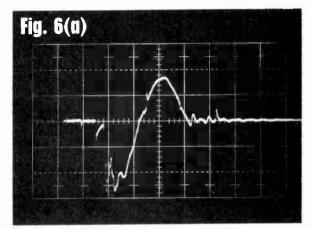
In the electronic system not only is the spark much shorter—0.2ms as compared with 1ms for the conventional system—but it also has nearly equal positive and negative half cycles. This greatly reduces plug erosion and increases spark plug life.

#### CIRCUIT DESCRIPTION

The complete circuit diagram is shown in Fig. 7. Transistor TR1 is not required for positive earth use but it may be left in circuit if desired. This will enable the ignition unit to be used in cars of either polarity merely by altering a few connections. It is only suitable for 12V systems.

Assume that the circuit is wired for negative earth with tag 9 earthed and the contact breaker connected to tag 8.

When the contact breaker closes TR1 is saturated and TR2 is cut off. When the contact breaker opens TR1 turns off and C1 is rapidly charged via R3. TR2 turns on and the positive pulse at its collector is differentiated by C2 and R11 and applied to the gate of SCR1 as a trigger pulse.



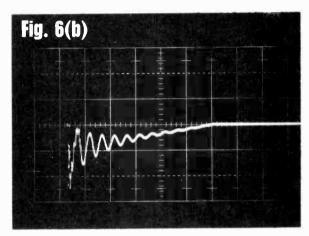


Fig. 6(a). Spark current produced by electronic system. Vertical is 100mA/cm and horizontal 50µs/cm. (b) spark current produced by the canventional system. Vertical is 50mA/cm and horizontal 20Cµs/cm

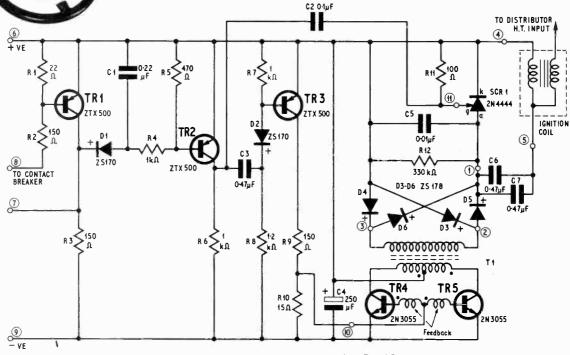
Transistors TR4 and TR5 with the ferrite core transformer T1 form a very efficient push-pull inverter, oscillating at about 2kHz. The 400V alternating output from the secondary is rectified by the bridge D3-D6 and charges the energy storage capacitors C6 and C7 in about 1.5ms (Fig. 8).

When fully charged the capacitors store 80 millijoules, which is about the same as the energy produced by the conventional system under ideal conditions.

When the thyristor is triggered C6 and C7 are switched directly across the coil so that the coil primary voltage instantaneously rises to minus 400V. The coil voltage then follows a cosine law whilst the coil current follows a sine law, the frequency being determined by the coil primary inductance in parallel with C6 and C7. See Figs. 9 and 10.

As the coil voltage reaches its positive peak the coil current passes through zero and the thyristor turns off. Then, as the coil voltage begins to fall, the diodes in the rectifier bridge become forward biased allowing the coil current to reverse. As the coil voltage reaches its second negative peak the current has again reached zero, but since the thyristor is now turned off the current cannot reverse again, and the remaining coil voltage is left on the storage capacitors C6 and C7. The capacitors then start to recharge for the next pulse.





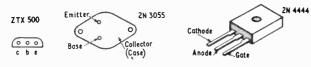


Fig. 7. Circuit diagram of the capacitor discharge system



#### **COMPONENTS...**

Resis	tors		
RI	22 $\Omega$	R7	lk Ω
R2	150 Ω 2W	R8	l·2k Ω
R3	150 Ω 2W	R9	150 Ω 2W
R4	Ik $\Omega$	RIO	15 Ω IW
R5	470 Ω	RII	100 Ω
R6	lk Ω	RI2	330k Ω 1W
Ali	½₩ 10% carbo	on excep	t where otherwise stated
Capa	citors		
ĊI	0·22µF 250∨	Mullard	C280
C2	0.1./F 250V I	Mulland	~290

C3 0.47 µF 250V Mullard C280 C4 250 µF 40V Mullard C437 C5 0.01 µF 1,000V C6 0.47 F 1,000V

C6 0.47μF 1,000V

0.47µF 1,000∨

TR1-TR3 ZTX500 Ferranti (3 off) TR4, TR5 2N3055 Ferranti (2 off)

Diodes and Thyristor

D1, D2 ZS170 or ZS270 Ferranti (2 off) D3-D6 ZS178 or ZS278 Ferranti (4 off) SCRI 2N4444

Transformer

TI-Two Mullard FX2243 ferrite cups with DT2206 former (see text). Ready wound transformer available from A.M.C. Electronics Ltd., 160 Drake Street, Rochdale, Lancs.

Miscellaneous

Eddystone diecast case  $7\frac{1}{4}$ in  $\times$   $4\frac{1}{2}$ in  $\times$  2in 6-way 5A connector block, mica washers, screws, spacers, turret tags, 14/0076 connecting wire, TO3 transistor covers

An etched printed-circuit board is available from A.M.C. Electronics Ltd. (see above)

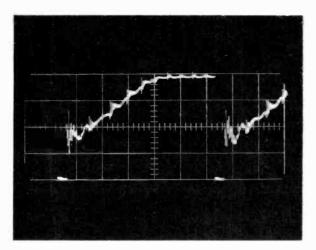


Fig. 8. Voltage on thyristor anode. Vertical is 100V/cm and horizontal  $0.5\mu s/cm$ 

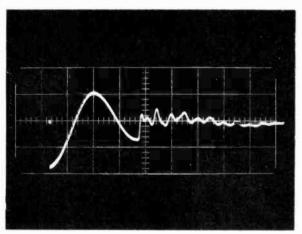


Fig. 9. Voltage across coil primary. Vertical is 200V/cm and horizontal  $50\mu s/cm$ 

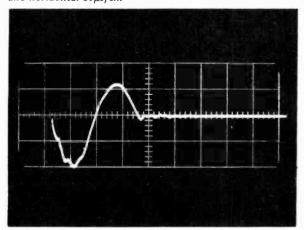


Fig. 10. Current in coil primary. Vertical is 5A/cm and horizontal  $50\mu s/cm$ 



The completed electronic ignition unit in a diecast box. Note the terminal block and power transistors with plastics covers

#### PREVENTING LATCH ON

When the thyristor turns on it places a short circuit across the rectifier bridge. This does not damage the inverter because the base drive to TR4 and TR5 disappears at the same time, but the inverter tends to produce a low amplitude oscillation at several hundred kilohertz. Normally the output current under these conditions will be insufficient to cause the thyristor to latch on, but to ensure reliable operation TR3 acts as a monostable which switches off the base bias to TR4 and TR5 for about 0.3ms after the thyristor fires. This stops the inverter completely so that there is no possibility of the thyristor latching on.

It is important to prevent the thyristor from triggering on spurious pulses produced by contact bounce when the contact breaker points close. In the circuit this is prevented by diode D1 and

capacitor C1.

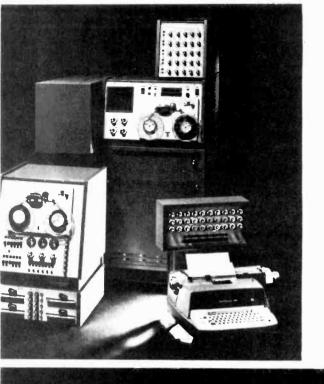
When the contact breaker closes, TR1 turns on and diode D1 is reversed biased. C1 then discharges slowly through R4 and R5, holding TR2 on for a further 0.3ms. Any spurious pulses arriving in this period cannot trigger the thyristor as TR2 is still saturated.

Further noise immunity is provided by C2 which takes about 0.3ms to discharge fully after TR2 turns off.

Next month: Complete constructional details for the ignition system will be given together with information on testing and installing the unit in the car.



all-weather starting and increased engine performance



#### Electronic Photo-typesetting using Magnetic Tape

THE photograph (left) shows an example of modern electronic phototypesetting equipment. The Alphatype is an American system allowing one operator to perform all the operations that standard metal casting machines perform, plus all of the hand make-up operations.

The heart of the Alphatype system is the "Multimix" recorder enabling any operator, after a minimum of training, to begin setting phototype. With the aid of sophisticated solid state electronics, type instructions fed in at the keyboard are relayed via magnetic tape to the "Multimix" print-out.

To set type in any of 10 alphabets the operator loads the recorder with magnetic tape and sets the dial to the proper unit measure for the desired pica width. Finally, he inserts the proper style cards for the 10 desired alphabets (5 type founts) in the recorder.

When a change of measure is required, he simply types the new information and the "Multimix" recorder holds it in memory until otherwise instructed. When keyboarding is complete, the operator removes the magnet tape with "hard copy" instructions and takes it to the print-out unit.

The magnetic tape is loaded into the Multimix printout with the proper founts. At the push of a switch the print-out automatically begins to compose the job, changing founts as it reads the recorded instructions.

## ELECTRONORAM

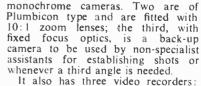
#### University to use OB Television Recording Van

A MOBILE television unit equipped and staffed to produce material required by colleges of the University of Durham's Institute of Education has just completed its initial term's work and will begin its first full year of operation this autumn. Designed and constructed by the Video Systems Division of Bell & Howell, it is housed in a specially modified van.

The unit is to be operated by Durham's recently established educational television consortium, and will spend at least four days of every term at the disposal of lecturing staff.

To meet these and other production requirements, the unit is equipped with three Bell & Howell





a lin recorder with editing facilities; a lin non-editing recorder; and a ½in machine, mainly to record material for colleges whose own VTR equipment is of the ½in type. In addition the van is fitted with effects and mixing equipment and a sync-pulse generator.









THE development of a crystal that stores hologram images as atomic patterns that can be read out one by one by slow rotation in a laser beam, like photographic slides in a projector, is reported by RCA.

As the laser beam traverses the crystal part of it is diffracted (bent) to fall on a round mirror where it reconstructs any stored information in the crystal (left).

This new advance in holography may lead to a revolutionary document storage system in which files of statistics, architectural drawings, computer data, photographs, maps and other graphic materials are stored permanently in crystals the size of sugar cubes.

A novel computer memory which for the first time will make it possible for a million bits of data to be written, stored, read out repeatedly, or erased by laser light will be built by RCA for NASA, the American Space agency.

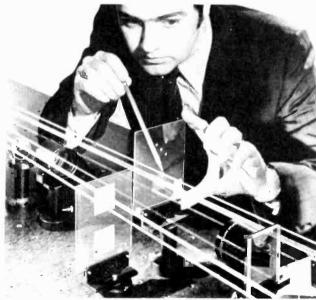
When completed next spring, the experimental, sixfoot-long, telescope-shaped device will be the first full-

cycle, all-optical memory ever built.

The experimental system is being built under a \$193,000 NASA contract, with the Marshall Space Flight Center having overall technical direction. The system is expected to validate the optical memory concept and to establish a base for the possible development of units that could be installed in space stations, earth resources satellites and similar spacecraft that need to store and process extremely large volumes of data at high speed. The laboratory model is shown below.

The optical memory appears suited for such applications because of its freedom from dependence on any sort of mechanical motion and its reliability. Such a memory, because it combines extremely large data storage with electronic access, could sometime in the 1980s replace the entire hierarchy of magnetic tapes, discs. drums and cores now used in modern computers.





#### Monochrome Telecine for Education Studios

A NEW monochrome telecine unit specially designed for professional closed-circuit television work has been introduced by EMI Electronics Ltd. Designated the type "416" the new EMI equipment enables material on 16mm film and 35mm slides to be used in the production of educational television programmes, and also provides captioning facilities.



By J. N. WATT

Since the behaviour of silicon semiconductor devices follows a common pattern, it will be found that the base emitter junction can be used as a conventional diode. Similarly, the base-emitter junction of a silicon planar *npn* transistor can be used as a low power Zener diode under certain operating conditions.

The reverse breakdown voltage of almost all silicon planar transistors usually lies somewhere between 7 and 10 volts. This is why the maximum reverse rating of such base-emitter junctions is quoted at 5 to 6 volts, since Zener breakdown is not normally required in the application to which it is subjected.

However, provided steps are taken to limit the power dissipated to around 100mW or so in the case of low power transistors, it will be found that the Zener voltage of any particular specimen remains remarkably constant.

#### **ZENER VOLTAGES**

The graph in Fig. 1a shows, by means of a histogram, the range of base-emitter Zener voltages measured on a batch of 30 unmarked *npn* silicon transistors at 5mA Zener current.

Although these transistors were unmarked, they were quoted as all being of a similar type.

It is reasonable to suppose that a batch of 30 guaranteed manufacturer's transistors would show a much closer spread—although it might be considered an advantage to have a range of Zener diodes so readily available in this way.

In point of fact, a measurement of a few new transistors, type BSY95a, did show a much tighter spread of base-emitter Zener breakdown voltage.

The graph A in Fig. 1b shows the voltage-current curve for one of the batch of 30 mentioned above.

The circuit configuration when using a transistor in this way is given in Fig. 2. Note that the emitter is made positive with respect to the base.

The value of R1 is chosen, after  $V_0$  and  $I_L$  are known, by Ohms law, that is:

$$R_1 = \frac{V_{\rm R}}{I_{\rm R}} = \frac{V_{\rm i(min)} - V_{\rm Z}}{I_{\rm L} + I_{\rm Z}}$$

 $I_{\rm Z}$  should be about 3mA for a small transistor used as a Zener.

Note that if the load current falls to zero by, for example, the load going open circuit, all the former load current will flow in the Zener and due allowance must be made for this.

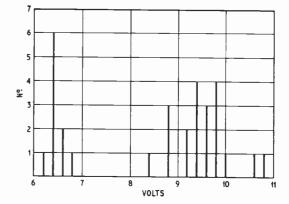


Fig. 1a. Range of base-emitter Zener voltages of a number of sample silicon transistors

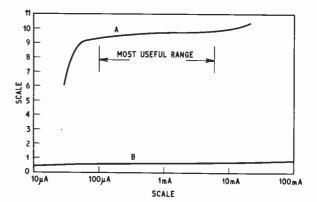


Fig. 1b. Voltage/current characteristic of one sample

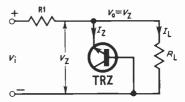


Fig. 2. Circuit used to measure the graph in Fig. 1b

The maximum dissipation in the Zener substitute should be restricted to about 100mW in the case of small 300mW transistors such as BC108; more powerful transistors, such as BCY51, can handle 300mW in this mode

Details of how to regulate greater power levels follow later.

If, as in Fig. 3, the base-emitter junction is biased forward (as it would be in normal transistor use), then once again a closely controlled voltage is obtained, this time of around 600-700mV.

Fig. 4 shows on a histogram the range of such voltages measured on the same batch of 30 transistors mentioned earlier, again at a current of 5mA. Graph B in Fig. 1b gives the performance of one of these transistors used in this way at various base-emitter currents.

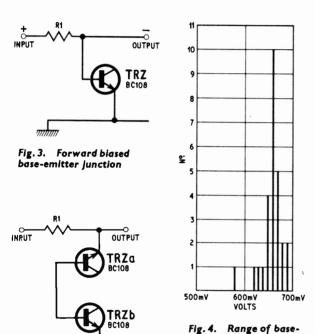


Fig. 5. Series transistors as Zener diodes

for 9V supply

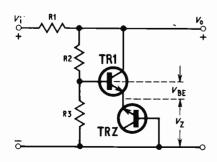


Fig. 6. Arranging higher output voltage by using a transistor

#### **SERIES DIODES**

It is possible, of course, to use Zener diodes in series, and the same applies to transistor substitutes. For example, Fig. 5 gives the set-up to provide 9 volts (8.4 + 0.6) from an unregulated supply.

Since the temperature coefficients of a base-emitter junction are of opposite sigh, according to which polarity is connected, some measure of temperature compensation is obtained in this last circuit. This is useful in, say, motor car applications, where the voltage supply to instrumentation circuitry can thus be stabilised against battery fluctuations over a wide temperature range.

In view of the availability from a number of advertisers of *npn* silicon planar transistors at prices around 20 to 30 for 50p, it is well worthwhile to consider these devices for use as Zeners in regulated power supplies.

Even if more than one device is required for a single application, there could still be cost savings; this will allow the constructor to make use of some of the more sophisticated circuits which follow, at no greater expense. Thus, greater flexibility and improved performance are obtained.

Substitute Zeners can be employed in a variety of regulated supplies, and those given here are intended to be typical. Any component values quoted are not necessarily optimum, but do show the principles involved, while the simple design formulae given should allow experimenters to adapt circuits to their own requirements.

There is (naturally!) a disadvantage in the use of a transistor as a Zener diode, and that is the limited range of voltages available.

#### HIGHER OUTPUT

It is, however, easy to arrange for a higher output voltage, and the method used is shown in Fig. 6. (Although a transistor used as a Zener is shown, a conventional Zener diode can be used.)

The output voltage is

$$V_0 = \frac{R_3 + R_2}{R_3} (V_Z + V_{BE})$$

where  $V_{\rm BE}$  is the base-emitter voltage of the transistor TR1. This voltage is effectively in series with the Zener voltage and must be included. With a silicon transistor used for TR1,  $V_{\rm BE}$  will be about 0.6V; a germanium transistor will have a  $V_{\rm BE}$  of about half this.

The maximum dissipation of the "amplified Zener", as this arrangement has been called, is that of the Zener plus the transistor TR1.

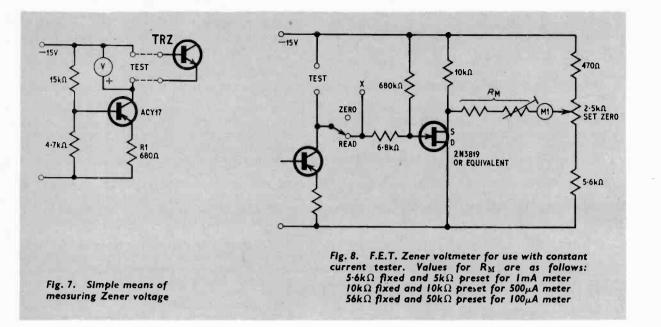
Typical values of R2 and R3 are  $15k\Omega$  and  $3.3k\Omega$  respectively; such values give a  $V_0$  of 9V with a Zener of 6.8V.

Calculation of the value of R1 in Fig. 6 follows the procedure given for the simple Zener circuit.

It is not as straightforward to arrive at an output voltage lower than the Zener voltage, and although it can be done, it would be better to leave consideration of this point until somewhat later, when we come to consider series regulators.

#### **MEASURING ZENER VOLTAGE**

Before any transistor is used as a Zener it would be desirable to measure its Zener voltage, bearing in mind the likely variation in that voltage from sample to sample.



A suitable arrangement for this measurement is given in Fig. 7. The voltage at the base is fixed by the two bias resistors and thus the emitter voltage is fixed too. Hence with a fixed value of emitter resistor a constant current will flow through the transistor when the collector circuit is completed.

If the substitute Zener is connected as shown, the constant current mentioned will flow through it and so a useful measurement can be made of its Zener voltage. This will be the more useful since various samples of Zeners will all automatically be tested at the same current.

The above reasoning naturally assumes that the supply voltage is high enough to develop the required voltage across the Zener and in addition provide voltage for the constant current transistor to function. A supply of about 30% greater than the highest Zener voltage likely to be measured should suffice.

In Fig. 7 the test current will be 5mA for the value of R1 shown. Lower values of R1 will give larger currents and vice versa, so permitting testing at other currents if desired.

In practical use, any low or medium power pnp transistor, such as ACY17, can be used. Remember that maximum dissipation will take place in the transistor with the lower values of Zener voltage, for it is then that most voltage appears across the transistor. Thus when measurements of the forward voltage drop of base-emitter junctions (about 600mV) are being made, almost all the supply voltage will appear across the transistor, so dissipating 75mW at a test current of 5mA. At higher test currents, some form of heat sink may be needed.

#### F.E.T. ZENER VOLTMETER

Measurement of the Zener voltage itself can be carried out with a high resistance testmeter on the appropriate voltage range. However, if testing of Zener diodes is to be done at low currents or if only a low resistance testmeter is available, then a simple f.e.t. voltmeter has several advantages, and a suitable circuit is shown in Fig. 8.

A popular type of f.e.t. is used. The set zero control is used to show zero volts on the meter with the switch in the "zero" position. The Zener under test is connected and the switch put to "read"; after the reading is taken, the switch should be returned to "zero" to prevent the meter reading the 15V supply voltage when the Zener is removed.

Values of external series resistance  $R_{\rm M}$  are given in Fig 8 caption for some popular meter sensitivities. It is required to be adjustable to allow for various f.e.t. characteristics and meter resistances, and is quite easily set up.

First, switch to "zero" and adjust the set zero control for zero on the meter. With the "zero/read" switch still at "zero", connect the positive terminal of, say, a 6 volt battery to the point marked "X" in Fig. 8, with the battery negative to the tester negative rail. Monitor this battery voltage with a suitable test-meter (this can be of a low resistance type). Adjust R<sub>M</sub> to give a suitable reading on the meter used; for example, with a 1mA meter aim for an indication of 0.6mA with 6 volts applied.

The advantages of this circuit are that a basic meter of low sensitivity can be utilised, and that Zener voltages can be measured at low currents. If a simple voltmeter circuit were used, it would have to be ensured that the current taken by the voltmeter was small compared with the test current, for otherwise the level of test current would vary as the current into the voltmeter varied. The f.e.t. voltmeter shown does not have this disadvantage even at test currents as low as  $100\mu$ A.

#### ZENER REGULATORS

As mentioned earlier, the upper limit of power handling for a substitute Zener is reached at a few hundred milliwatts or so.

However, it is easy to arrange for greater levels to be regulated, and there are basically two ways of achieving this, using additional power handling transistors: as will be shown next month.

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Get the facts you need to identify and use the mass of linear and digital integrated circuits now available. Classified tables of data and applications information are given in the supplement in our December issue.

#### Integrated Circuit Survey



. . . follow up by trying out the constructional features:

#### **Logical Radio Control**

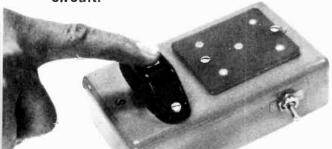
Integrated circuits are used to great advantage in coding and decoding proportional radio control functions for models. Wiring is simplified with printed circuit cards making control systems small enough for a wide range of models.

#### **Digital Dice**

This small battery operated dice has a neat array of spots in conventional dice configuration, and is illuminated by pressing a button. The actual value shown is determined by random switching of a counter and gating circuit.

## An Added Attraction ELECTROLUMINESCENCE AND MATERIALS

This article explains the principles of light emitting semiconductor materials in connection with modern means of communication.



DECEMBER ISSUE ON SALE -- NOVEMBER 13

#### "IDEAS" LIBRARY

For the electronics enthusiast there is a wealth of interesting ideas buried in the millions of patents kept in the library attached to the British Patent Office in Southampton Buildings, Chancery Lane. And the numbers are added to every week. It costs nothing to refer to anything kept there and it only costs 25p to buy a copy of any British patent specification. The only trouble is finding interesting needles in the haystack.

The idea behind this column is

that circuit by the dozen and advertising them for sale.

So if anyone has ideas from this or any subsequent article, please use some common sense and if in doubt take professional advice from a chartered patent agent. Bear in mind that agents' time is not cheap to buy and so professional advice should only be sought where really necessary. The Editor cannot enter into any correspondence on the legal aspects of patent applications, inventions, or specifications.

One final point. A reasonable estimate would be that 90 per

synchronisers have been marketed although for one reason or another their presence have tended to complicate the overall system in a manner which Elektroakusztikai Gyar maintain is unnecessary.

The Hungarians suggest solving the problem by using a separate synchroniser, but one which records the control signals on the tape from an amplifier with switchable positive feedback. By means of a capacitor this positive feedback converts the circuits used into an approximately assymetrical multivibrator so that the amplifier can handle the function of a code

## PATENTS BEVIEW...

to pick out a few of those "needles" and in view of the massive numbers of specifications involved it seems sensible to concentrate only on those that are being newly published. So a few of those most likely to interest Practical Electronics readers will be mentioned in this series.

#### LEGAL ASPECT

On the legal side of things, remember that a patent serves two purposes. Firstly, it discloses to the public the details of what the patentees have been doing, and secondly—for a period of up to sixteen years while the patent is in force—it gives the patentee a monopoly on whatever is really new in his activities.

The scope of this monopoly is defined by the claims which are found at the end of the specification and so—in theory at least—you are liable to be sued if you do what the patentee is claiming. But in practice, of course, the average reader of Practical Electronics is likely to be far less bothered by the legal side of things than he might at first fear.

Quite apart from the question of whether what he is doing actually meets the requirements of the patent claims, and quite apart from the question of whether those claims are really valid (these are questions that only a chartered patent agent can advise you on) it is common sense that a reader playing about in his garden shed with a bit of one-off circuitry is unlikely to find himself sued by a multi-million pound electronics firm on the grounds that he has made up a version of a patented device or circuit.

But it could be very different if the same reader starts making up

cent of everything disclosed in any patent specification is established knowledge anyway. Most patents need pages of background information to highlight the novel and inventive step—and of course those pages of background information are often of the most interest to the amateur constructor. If something described is old and known, it is assumed free for anyone to use.

#### SIMPLE SLIDE SYNC

THE Hungarian firm Elektro-akusztikai Gyar have a new British Patent 1 230 040 which concerns a synchroniser for automatically operating a multitrack tape recorder and an electronically remote-controlled slide projector. To date a wide variety of control systems have been devised for ganging tape recorders and slide projectors so that a recorded commentary automatically controls slide change.

Recently some fairly sophisticated set-ups have emerged. For instance where a built-in synchro-niser is used, the synchronising signal has been recorded and reproduced by means of an erase head. 50Hz signals are taken off the mains and fed to the erase head for recording onto a second track. On playback these signals are detected by the same erase head and used with amplification to operate the projector control relay. (Tape erasure may also be handled by erase head when fed by a d.c. voltage.) This all works well but problems arise when the tape recorder does not have a built-in synchroniser. So separate

oscillator as well as its other routine functions (see Fig. 1).

The patent specification describes some convenient transistorised circuitry for positive

#### BP 1 230 040

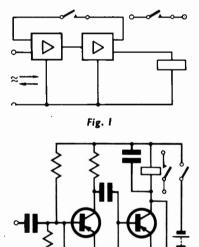
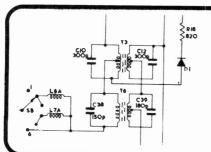


Fig. 2

feedback production—and most important of all—the circuitry looks fairly simple and thus should provide an equally fairly cheap system for "add-on" synchronisation. The feedback switch of course also provides for easy manual control of the projector. The detailed circuit without component values is in Fig. 2.

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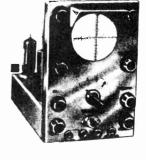


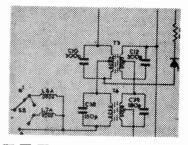
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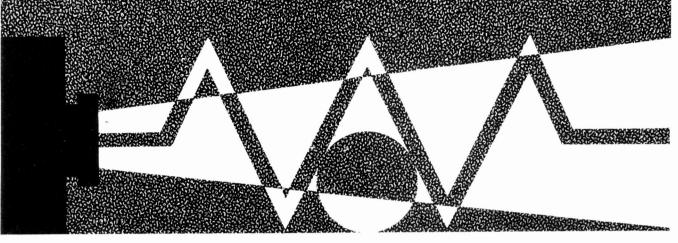
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P.E.10



## PROJECTOR LAMP PROTECTOR

By J. KAY

As an enthusiastic user of a 35mm still projector, the author has found that the cost of replacing blown bulbs can be rather high. It is common knowledge that a lamp's filament is more likely to fuse at the instant of switch-on than at any other time. The reason for this can be seen best by taking an example.

A 500 watt, 250 volt lamp in normal use carries a current of 2 amp. However, if the cold lamp's resistance is measured by an ohmmeter, it is found to be 4-5 ohms. By Ohm's Law this indicates that, at switch-on, the current carried will be 50 amps.

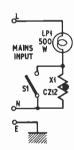


Fig. 1. Switch protection for the Projector lamp thermistor

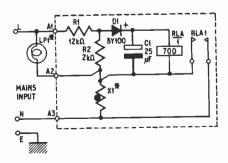


Fig. 2. Circuit diagram of the Automatic Projector Lamp Protector

It is, therefore, not very surprising that lamps will tend to fuse at switch-on.

#### SURGE LIMITING

In order to reduce this initial surge, thermistors are made which have cold resistance of about 120 chms and hot resistances of approximately one ohm. If this 120 ohms and the lamp's 4-5 ohms are connected in series across the mains, the current at switch-on will be 2 amps.

As this current heats up the thermistor its initial resistance value will begin to fall and hence the current through it will rise. The temperature of the lamp's filament will also rise, and so will its resistance.

These two changes occurring at the same time tend to balance one another out and the current through the lamp and the thermistor remains at about 2 amps, or a little lower since the lamp heats up more rapidly than the thermistor.

#### THERMISTOR PROTECTION

If the thermistor is left in circuit, its effect on the lamp's brilliance will be negligible. However, the temperature of the thermistor may reach 200-250°C in free air and higher if enclosed.

At these temperatures the thermistor is rather fragile, and unless it is shorted out soon after switch-on, may easily break as a result of vibration. In addition any subsequent switch-on must be delayed by 10-15 minutes as it requires this period to cool down.

A manually operated switch, S1, connected in parallel with the thermistor as in Fig. 1, is apt to be overlooked and in consequence the life of the CZ12 is reduced.

#### **RELAY SWITCHING**

To overcome this problem, automatic switching using a relay was devised as in Fig. 2. Since initially most of the voltage appears across the thermistor

there will be a delay period before the relay operates as R1 and R2 form a divider to provide a suitable voltage for the relay. As the line volts are alternating a rectifier D1 and smoothing capacitor are required.

The relay used in the prototype had a coil resistance of 700 ohms. With an operating voltage from 12-24 volts, a 2 kilohm resistor for R2 is suitable.

If other relays of similar operating requirements are available the value of this resistor should be tailored to provide contact pull-in after about six seconds.

#### COMPONENTS . . .

Resistors

R1 12kΩ 5W R2 2kΩ IW

Capacitor

CI  $25\mu$ F elect. 50V

Thermistor

XI CZI2 (Henry's Radio) (See text for type variants)

Diode

DI BY100

Relay

RLA 2 pole, 2 way, 12-24V 700 ohm type 4189GD contact rating 2A (Henry's Radio)

Miscellaneous

Standard tag board, wire

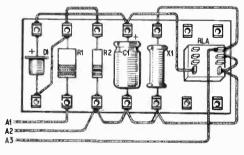


Fig. 3. Tag board assembly and wiring details for the Lamp Protector

#### CONSTRUCTION

The relay and associated components shown contained in the dashed box can be assembled on a piece of standard tag board as shown in Fig. 3. As wiring is not at all critical other layouts may be employed.

If lower voltage lamps are used, the thermistor type should be changed as follows. For lamps up to 150 W—CZ9A. And for lamps up to 300 W—CZ11. With these alternatives there is no need to change any of the relay circuit components values.

If the projector has a fan, it should be left connected to the mains and not included in the lamp control circuit. The tag board assembly should be clear of this if mounting in the projector is intended.

### NEWS BRIEFS

#### Patents and the Patent Office

A most useful and informative booklet has just been published by The Patent Office, London. It describes the information retrieval services provided by the Patent Office ("the largest technical publisher in the country") and how to make use of them.

The booklet also deals briefly with applying for a patent, and the exploitation of a patent. And contains a list of publications available concerned with invention

and patent literature.

The booklet is available free of charge from Sale Branch, The Patent Office, Orpington, Kent BR5 3RD.

#### Worldwide Communication

THE North Staffordshire Polytechnic has recently improved its amateur radio station equipment and now has a rotating complex of beam aerials on top of a 60ft tower mounted on the roof at the polytechnic.

The new aerial system, the wide range communications equipment and the facilities at the adjacent electronics laboratory have made this station the most advanced installation of its type in the country. Signals from the station can be received, the Polytechnic say, any-

where in the world.

The equipment which includes three transmitters has been acquired over the past four years and some of it has been built or modified by students. Officially G3VZI—the station's call sign—is operated by North Staffordshire Polytechnic's Amateur Radio and Electronic Society.

#### Dimmer Switches

THE Accessories Section of the Installation Equipment Division of BEAMA has recently extended its scope to cover dimmer switches for domestic and similar lighting circuits.

A technical panel has been set up in collaboration with the Appliance Control Section of BEAMA and other interested bodies, to produce a draft British Standard

Specification covering dimmer switches.

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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

This is YOUR page and any idea published will be awarded payment accord-

ing to its merit.

#### IC TEST JIG

Being faced with the need to test and experiment with a variety of dual-in-line type i.c.s, and not wishing to part with the cost of an expensive commercial type "breadboard", I evolved the following extremely handy inexpensive test jig.

The complete unit can be built in under 30 minutes, costs less than 50 pence and consists of one 16-pin DIL i.c. socket, one small piece of 0·1 matrix Veroboard size 17 × 24 holes, and 16 Veropins.

The jig is constructed as shown in the photographs. The distance between the Veropins is great enough to allow connection of crocodile clips with minimum risk of short circuits.

It should be noted that the  $+V_{CC}$  and earth connections for 14-pin DIL's are different and the necessary modification will have to be made to the board.

This system could be enlarged using a larger board and it could also be adapted for TO5 type i.c.s using the sockets and pin spreaders available from advertisers.

> Jnr. Tech. Nekrews, Royal Air Force, BFPO 45.



HE circuit in Fig. 1 will produce tones in increasing frequencies until the highest one is reached. Then the cycle repeats again from the lowest frequency. The circuit consists of an astable multivibrator, a pump counter, and a tone generator.

The switching frequency of the astable is varied by the potentiometers VR1, VR2, and this frequency decides the speed at which the tone changes from

one frequency to a higher one.

The voltage across transistor TR3 is used to control the pump counter. When this is conducting, only a low voltage is obtained across it. But when TR3 is cut off, this voltage increases considerably. A negative signal is then introduced to the base of TR4 and this turns TR4 on.

When TR4 is cut off a high resistance appears between its emitter and collector. C5 then charges through R6, C4 and D2. Depending on the value of C4, a fixed fraction of the supply voltage appears

across C5.

When TR4 turns on, resulting in a low resistance between collector and emitter, C4 discharges through TR4 and D1. Notice that capacitor C5 is prevented from discharging quickly via D2.

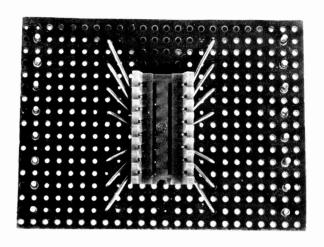
Next time TR4 is cut off C5 charges a little more, and so on. In this way the emitter voltage of the unijunction transistor TR5, after some pulses, gets high enough to fire TR5. Capacitor C2 then discharges, and the process starts all over again.

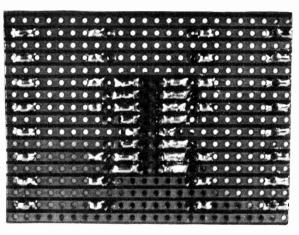
This staircase voltage is further fed to the tone generator unit. This is simply a direct coupled amplifier stage with a regenerative feedback causing oscillation. The oscillation frequency depends on the base bias of TR6 taken from TR5 emitter via VR3. The base bias must not be too high and is adjusted by VR3, beginning with its maximum value and slowly reducing it until the tones are heard.

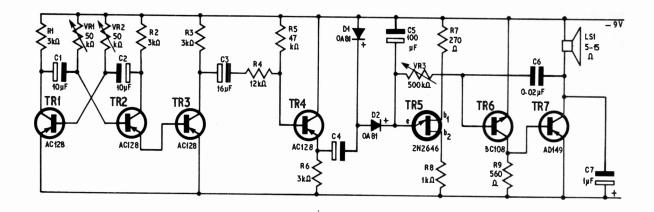
The circuit has many application possibilities, one being doorbell alarm. It is wise to mount the three units on separate boards, because all the units can

be used separately.

Renny Skagestad, Norway.







#### **CONVERSION TO 24 HOUR CLOCK SYSTEM**

WITH regard to your Digital Clock, here are one or two modifications that your readers may be interested in.

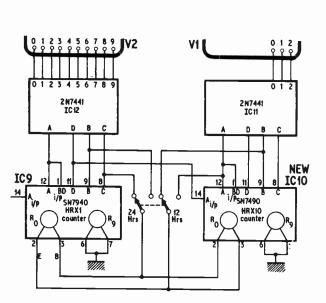
The first enables the Clock to be converted to read a 12 or 24 hours cycle when the alarm system is not being incorporated. As shown in Fig. 1, the counter for HOURS × 10 is made on SN7490, and the mode of the clock is changed by switching the inputs to RESET ZERO gates of the HOURS × 1 and HOURS × 10 counters.

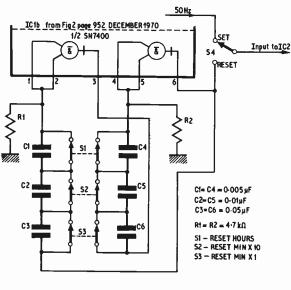
Because the clock is to read both 12 and 24 hours, the HOURS  $\times$  10 Nixie is connected to the HOURS  $\times$  10 decoder. The clock, therefore, reads at the recycle times 11.58-11.59-00.00-00.01 and so on, in the 12 hour mode and 23.58-23.59-00.00-00.01 in the 24 hour mode which means in the 12 hour mode the clock never reads 12.00 hours.

The second modification concerns the RESET facilities. The circuit shown in Fig. 2 enables the clock to be reset in faster time; also the clock can be held at a particular time in order that it can be

accurately set up. As can be seen, the circuit makes IC6 and S1 redundant, but introduces more discrete components at four switches. The second half of IC1 (IC1b) is used as a three-frequency multivibrator, the individual frequences being switched by S1, S2 and S3 in Fig. 1. With all three in the closed position, the circuit does not oscillate, and therefore, when S4 is in the RESET position, the clock receives no input pulses. With S4 in this position, and S1 open the multivibrator oscillates at a frequency that charges the HOURS counter approximately once per second. With S2 open and S1 and S3 closed, the MINUTES × 10 counter changes approximately once per second. S3 performs the same function for the MINUTES X 1 counter. This results in the clock being completely recycled in 55 seconds in the hour mode and 25 seconds in the 12 hour mode.

K. D. Brown, Southend-on-Sea.







BY FRANK W. HYDE

#### **GLOBAL WEATHER STUDY**

With the launching of the French satellite EOLE a new step forward has been made in the expansion of meteorological studies. Satellites in the service of man are beginning to reap the harvest of space technology spin-off. It is interesting that the French have chosen a name which means "God of the Winds."

The satellite will gather data from as many as 500 free ranging meteorological balloons. The existing systems which have been so outstandingly successful in the case of the Nimbus satellites, gather mainly data from the higher levels, though some balloon interrogation is carried

Both Nimbus 3 and 4 which carried the interrogation, recording and location system was able to show its efficiency in tracking balloons, aircraft and other types of instrumental platforms.

The Omega position location equipment which was installed in the geostationary satellites ATS 1 and ATS 3 tracked balloons and buoys successfully.

The doppler system installed in *EOLE* is superior to the others in that they cannot cope with the same number of balloons. This satellite will take over in an area where expensive rocket methods have been used, namely the 30 to 60km levels in the atmosphere.

The EOLE satellite weighs about 160lbs and was designed, under the direction of Professor P. Morel from the University of Paris, at the Centre Nationale D'Etudes Spaciales. It will occupy a 560 mile orbit with a 50 degree inclination to the equator. The orbital period is 103 minutes and the satellite will have a pattern of interrogation which will continue day and night.

The data will be stored until the satellite passes over a tracking station which will command the

telemetry at 136MHz to release its store. The experiment is expected to last some 6 months.

The lifetime of the balloons used will vary from one to 5 months. These will be released by researches in the southern hemisphere at the rate of three a day from each of the stations at Mendoza, Neuquen and Lago Fagano.

The balloons, which are twelve feet in diameter, will drift at an altitude of 12,000 metres. Each balloon will carry a payload of instruments in a 32ft long string which will consist of temperature and pressure sensors, together with batteries and solar cells. These will serve the receiver operating at 464-4864MHz and the 4 watt transmitter which will radiate on 401.71796MHz.

It is expected that the satellite system will be able to locate a balloon to within 3km.

#### ATLANTIC AIRLANE CONTROL

In August an agreement was made between the United States government and ESRO (European Space Research Organisation). Ten countries are represented in ESRO and the agreement arranged through the FAA (Federal Aviation Administration) of America may well end the hazards that exist in the aircraft lanes.

At the present time the minimum separation limits are 2,000ft vertical, 120 nautical miles horizontal and 15 minutes in longitude. At any one moment the accuracy of the known position is not better than ten miles. Using satellite methods the position could be known to half a mile.

In view of the amount of interference that can occur in the normal aircraft communication bands it is expected that the aircraft communication will be shifted to the L band (390 to 1550MHz). It has been tentatively suggested that the specification might follow this form: world wide coverage; accuracy 0.5 Nautical miles deviation to allow separation to be reduced to 30 nautical miles horizontal; 1.000ft vertical; and 5 minutes longitudinal.

#### VIKING MISSION

Some rather disturbing conditions are forecast as a possibility in the Martian atmosphere when the Viking spacecraft attempts the landing on Mars in five years time.

Cornell University has been making a study of the possibilities of high winds over the surface. It is difficult to forecast exactly what will happen for the meteorology can only be known from indirect methods.

The terrestrial experience does not help very much for the atmosphere on Mars is tenuous and a key factor is the height of the atmosphere and mountain range height. On Mars the scale height is comparable with height of the mountain ranges over a distance of perhaps a hundred miles. The scale height (the point at which the pressure of the atmosphere falls by half) may have the changes of as much as ten miles in height and therefore be very much dependent on the topography.

Carl Sagan and Peter Gierasch have derived solutions to the problems of thermal winds and predict speeds of up to 250 mile per hour in some regions. This will dictate to a great extent where the space-

craft could safely land.

For certain technical reasons the landings have to be made within a limited equatorial belt and there are forbidden areas within these limits where the winds will be too high. Thus it means that regions of great scientific interest will not be suitable for a landing. One of these is the Hellas region.

The lowland flats will be the best choice for landings, but it would appear that the value of the scientific work will be reduced.

Last year there were a number of yellow clouds detected and these may well be dust swept up by very large gale force winds. Some of these lasted for several weeks.

It seems that there are new techniques to be perfected for the later manned landing and that the astronauts who visit will have new techniques to learn.

#### ASTEROIDS MAY HAVE MAGNETOSPHERES

During the grand tour of the planets which is to be made in the late 70's the spacecraft used will traverse the asteroid belt. This lies between the orbits of Mars and Jupiter.

There are many hundreds of these minor planets and it may well be that the probes will pass in the vicinity of one of the larger ones. If this should be so then there may be effects on the instruments carried, particularly the magnetometers.

It is known that none of the asteroids have an atmosphere but it is possible that they have a magnetosphere. The magnetosphere is the zone of magnetic influence round a body which acts as a barrier to penetration by the fast charged particles in the solar wind.

It appears that the solar system has a small residual magnetic field and therefore an asteroid could have a low surface magnetism. If this magnetism were as low as one thousandth of that of the earth then a magnetosphere could exist.

The magnetosphere extends a considerable distance from the body it encloses (the tail of the Earth's magnetosphere extends as far as the Moon) so that a wide pass could yield some data.



#### **CHARACTER RECOGNITION 1971**

Published by the British Computer Society 212 pages,  $8\frac{1}{4}$  in  $\times$   $5\frac{3}{4}$  in. Price £2

This is an up-dated version of the handbook originally published in 1967. It is intended to assist the layman in his comprehension of character recognition; particularly those who may wish to discuss the techniques and possibilities with manufac-

turers of reading machines.

Physical and optical properties of paper, printing methods, the design of alphabetic and numeric characters and symbols that are suitable for automatic reading by machines are described. Optical mark reading (OMR); magnetic ink character recognition (MICR); and optical character recognition (OCR) techniques are all explained and the text is well illustrated with excellent diagrams. The variety of electronic systems employed in OCR is impressive: after the mechanical scanner (Nipkow disc), come laser-beam, flying-spot, Vidicon, and photocell matrix scanners. This portion of the book offers a good, concise technical introduction to the subject for the general reader.

Proprietary equipment and services are reviewed in the final chapter. This will be most valuable to potential buyers or users of such commercial equip-

ment.

F.E.B.

#### MICROWAVE SEMICONDUCTOR DEVICES

By H. V. Shurmer, PhD, CEng, FIEE. Published by Pitman Publishing. 223 pages, 8½ in × 6in. Price £2.25

This is one of an Electronic Engineering Series of monographs written at a level ranging from undergraduate to postgraduate and professional standard. It is therefore, a specialist's book. It deals with certain types of semiconductor devices which are employed in the rather rarified regions of the frequency spectrum remote and foreign to most laymen, but where much professional activity is taking place involving radar, telemetry, and instrumentation applications, for industrial and defence requirements.

A brief outline of the history of origin, or development of the particular device is given at the commencement of each chapter. The theory of operation is treated concisely, but in some depth with extensive recourse to mathematical proof, the level (as stated by the author) being suitable for students on an engineering degree course. It goes without saying that the usefulness of this authoritative work will extend even further, to others with serious interest in this rather specialised area of electronics.

The scope of the book is best indicated by listing the devices described (each having one chapter): Point-contact, varactor, Schottky-barrier, tunnel, backward, pin, Gunn effect, and avalanche diodes, transistors, and finally, integrated circuits, an area still in its infancy—in microwave terms—but hold-

ing out interesting possibilities for the future.

TRANSISTOR CIRCUIT DESIGN TABLES

By David S. Taylor, M.A. (Oxon), Ph.D. Published by The Butterworth Group 120 pages, 9in × 6in. Price £2.80

HEN first seeing the title of this book, then reading the publisher's blurb on the jacket, one would naturally expect to find a great deal of information on the various basic transistor building block circuits. The Preface goes on to tell us how the material is a direct reprint from data derived from computer calculations. Discrepancies, we are told, may be as high as +20 to -30 per cent of the indicated values due to variations in transistor characteristics.

I used these tables in a test case, in which only one line of figures was required. It can be concluded that the value of the book as a whole is minimal since a great deal of the data given is seldom likely to be used. It is like choosing one or two ties from a shop full of ties of different kinds. The designer is rarely likely to require more than basic information on circuit values for only a couple of supply parameters.

One must credit the author with the effort involved in collecting all this data, but for the price of the book I personally do not consider this a "value-formoney" buy. If, however, the designer requires to use this information, a quick peep at the book in

a library will be a great help to him.

Probably the most useful chapter is that on Schmitt trigger circuits, but capacitor and inductor reactances are more easily assimilated from nomograms or abacs. Parallel and series resistor and capacitor calculations involve basic arithmetic and excellent approximations can be achieved by mental calculation.

The other three chapters on common emitter amplifier stages (restricted to somewhat outdated RC coupling) and multivibrators are useful and relevant to the title.

M.A.C.

#### **COLOUR TELEVISION THEORY**

By G. Hutson Published by McGraw-Hill Ltd 326 pages, I0in × 7½in. Price £3.85

This is a very well prepared textbook on colour television engineering embracing both the PAL and NTSC systems, but with the emphasis on PAL. As is the wont of most textbooks, this is particularly aimed at those students who are preparing for examinations which include colour television principles, particularly those offered by the City and Guilds of London Institute and the Radio Trades Examination Board.

The fact that the use of mathematics is small will no doubt induce lay readers with a working knowledge of monochrome television principles, to invest in this, for not only is it an excellent tutor but a valuable reference.

Commencing with chapters on the physics of light and colour television signals, the book goes on to analyse the various receiver sections that makes reception possible.

The book is very well illustrated with a 14-page index that makes reference a very easy business.

G.G.



Our nearest neighbour the Andomeda Nebula. it resembles our own galaxy and has enabled astronomers to make a more accurate model of our galaxy. It is about 200,000 light years in diameter and is about 2,200,000 light years distant from our galaxy. Its number is M31 and is one of the nebulæ that is visible to the naked eye on a clear night and easily seen through modest binoculars.

## **TECHNIQUES**

BY F.W.HYDE · PART 6

In this part the various pieces of equipment from the aerial system to the recorder will be brought together to form the radio telescope. The setting up of the receiving system will be covered in some detail, much of which may be familiar to some readers. However, this is a very necessary step for the newcomer and those more experienced can go straight to the setting up in their own way.

In order to check each stage certain test equipment is desirable. One test unit which would be of great help is a signal generator of good standard. If this is not available then the next best thing is to make up a noise generator and use this to provide a setting-up signal. This presupposes that some means will be available to set the correct frequencies which are to be used. The nominal operating frequency of this telescope has been set at 137MHz. It is essential therefore that both the pre-amplifier and the converter are centred on this frequency.

#### **NOISE GENERATOR**

A suitable noise generator may be made up quite simply and a diagram of a suggested circuit is shown in Fig. 6.1. It is possible to purchase noise generators on the surplus market at reasonable prices and they have the advantage of being calibrated. However, the simple one that is described will serve the purpose very well.

For the sake of making an alternative available that is within the ability of the constructor, a valve diode circuit is shown in Fig. 6.2. It must be pointed out that in the case of the valve diode its life is

limited and that if this unit is made up, the time in use at maximum noise should be kept to a minimum.

Either of these noise generators can be used to measure the noise factor of a receiver or amplifier, although this is not the purpose in this case. It will be used in order to ensure that each unit in the chain of apparatus is operating under optimum conditions.

#### LOW RESISTANCE RECORDER

Certain alternative methods of recording have been given, so the order of setting up will vary slightly accordingly.

Taking the simplest of the arrangements, that of connecting a low resistance recorder directly to the cutput transformer of the receiver final stage, the procedure will be as follows.

Switch on the converter and the communications receiver and let them warm up for about 20min. Connect the recorder in parallel with the loud-speaker. Disconnect the output from the converter to the receiver.

Set all gain controls at maximum while watching the pen on the recorder. If this goes to full scale before the controls are at maximum, reduce the a.f. gain control progressively while increasing the r.f. control. If the a.f. control is at a point less than 50 per cent of its travel then reduce the r.f. control till the a.f. gain can be set at the halfway point.

The loudspeaker may now be disconnected after reducing the pen position to half scale by the con-

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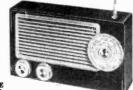
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trols on the receiver. If the sensitivity available is such that the loudspeaker needs to be in parallel all the time, then to avoid causing disturbance by the continual hiss of the speaker, a simple muting arrangement of switching in a dummy load resistor

in place of the loudspeaker can be used.

The case of high receiver noise level has been covered so far. The other case, that of the quiet receiver, which incidentally is the more desirable, a different technique is required. If the recorder does not respond to full scale with the a.f. control at the halfway mark and the r.f. gain at maximum, then a short piece of wire connected to the aerial input socket of the receiver should give sufficient noise to enable the sequence to be followed.

#### OTHER TYPES OF RECORDER

Having dealt with the simplest form of recorder connection, the alternative arrangements discussed in the previous article for connection to the receiver cutput stage will now be covered. In the case of the special winding on the output transformer, this will accommodate a high resistance order. The sequence of the setting up procedure will be identical with that for the low resistance recorder.

Where the potentiometer system in the output stage is used there will be the additional control which sets the recorder level, whether this be high or low resistance coil. The same conditions apply,

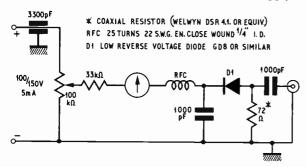


Fig. 6.1. A simple noise generator using a solid state diode. In raising the noise level by increasing the voltage it will be noticed that the noise increases and then passes through a decreased level finally rising again. As this generator is being used for testing only, any convenient noise point may be used

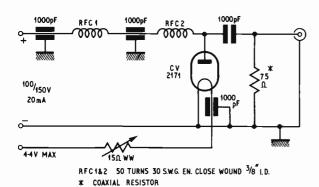


Fig. 6.2. An alternative noise generator circuit, using a valve diode. Care should be exercised when using this type of circuit because the life of the diode is not much in excess of 500 hours. For that reason it should be used at the lowest level consistent with the test being made



Fig. 6.3. A receiver tuning test recorded on the chart for reference purposes

that is to say the r.f. and a.f. controls are set as previously described, with the additional advantage of varying the sensitivity of the recorder.

In both these cases the muting of the loudspeaker

using the switching network will apply.

#### USING D.C. AMPLIFIERS

When d.c. amplifiers are employed, a similar procedure so far as the setting up of the receiver is concerned will be followed, but before connecting the recorder in the circuit the d.c. amplifier will need to be balanced as follows.

In place of the recorder insert a milliammeter. Set this at the 10mA range to begin with. The pointer should be set at midscale by adjusting the controls and the meter brought to the lower current settings until the halfscale reading is the same as that for the recorder. In general this will be 0.5mA since most recorders will be of the 0-1.0mA full-scale type.

Having set up the d.c. amplifier, it may be connected into the receiver and checked before replacing the meter with the pen recorder. Again the same sort of procedure will be followed. In the case of the rather more complicated amplifier a greater sensitivity will be available, so this needs to be taken into account.

#### ADDING IN THE CONVERTER

The next step is to connect the converter to the receiver and to reduce the r.f. gain until the recorder is at the same level as in the first setting-up using the receiver alone. A check can be made at this point to see if the receiver has been set to the correct i.f. frequency. It is assumed that the converter has been checked for its mid-point frequency of 137MHz.

With no aerial connection to the converter, the tuning of the receiver can be adjusted slightly to each side of the i.f. frequency to see if the noise level falls equally. If the wideband system of the receiver's own i.f. transformers shows two humps a visual and audio adjustment will perhaps be necessary. The correct tuning will be for the receiver tuning to be set midway between humps. This will show a slight rise of the pen level on each side of the datum. Let this fact be borne in mind for all subsequent checks. A note made on the test chart showing all three points would be useful. See Fig. 6.3.

#### ADDING THE PRE-AMPLIFIER

The pre-amplifier (without the aerial connected) is now linked with the converter. There will be a rise in the noise level and the first adjustment will be made to the receiver r.f. gain control so that once again the recorder pen is at its datum.

If there is so much gain in noise that additional reduction is required at the a.f. gain control, it may well be that the inherent noise of the amplifier is too high. In order to check this connect the aerial to the pre-amplifier. If there is a rise in noise then all is well. If there is no detectable difference then the internal noise of the system is too high.

Before opening up the pre-amplifier make the following recheck. Set the controls so that the pen recorder has a tracing which is clearly one of varying noise. Feed in the noise generator at the aerial input of the pre-amplifier—which should be brought into the vicinity of the other apparatus. Set an optimum noise level with the noise generator "on". Note the reading and then disconnect the generator. Note the fall in noise level and if this is substantial it will establish that the system is all right but that somewhere there is an overload condition arising. This may be because the a.g.c. circuit is over sensitive.

It is better that there should be no a.g.c. applied when the system is used as a telescope. It may be necessary to interpose between the amplifier and the converter some form of attenuator, or it may be that this is needed between the converter and the receiver. This will have to be a matter of empirical

investigation.

In the other case, where no change of level is noted when the noise generator is used, then the units must each be checked for noise level. For this purpose, of course, the noise generator can be used. No doubt some form of audio amplifier with a diode detector will be available and this can be used to check the noise level of the pre-amplifier.

#### INTO PRACTICE

Having set up the system and checked its operation, a note should be made of the positions of all controls. As the time constants at the recorder sections are long it might appear that the whole system is not working. To check this (in the case of recorders being connected directly to the output stages) a pair of phones or the loudspeaker kept in operation for final setting up will indicate the sensitivity of the system.

The reason for using the long time constants is to remove the high level random noise peaks of short duration and also the modulated transmissions which might appear from time to time. To appreciate this perhaps a few words of explanation are required.

The noise that is received by the aerial is randomly distributed but contains in its spectrum some coherent noise from extra terrestrial sources. Over a period of time the random noise will tend to cancel itself out but the coherent noise will over the period of time show a level which is higher than the purely random noise. To this is added the random noise of the aerial itself and that of the system to which it is connected.

Using a long time constant, the coherent noise tends to assume a noticeable level because the purely random noise cancels itself over the period of integration. In the case of this telescope, 4 seconds and 8 seconds approximately have been chosen as integration times. This will be satisfactory for most purposes and for the early stages of this project.

#### MONITORING ARTIFICIAL SATELLITES

When using the telescope for the monitoring of artificial satellites, there will be no need to change the time constant on the recorder unless the details of the telemetry are required. The automatic picture satellites (APT) used for meteorology will register a signal on the chart, but if actual picture reception is contemplated then the receiver will be quite different. A picture receiver needs to be a frequency modulated unit and a crystal controlled oscillator is essential.

Everything is now ready for the first observations. Each of the three positions of the telescope will require a change of altitude. To ensure that the same position is located each time, it is a good idea to make or buy a protractor. This can be fitted to the end of the reflector and with a suitable plumb bob the exact position repeated at each change.

If the telescope is to be used for satellite tracking then it is best to turn the aerial upwards so that the aperture points to the zenith. Most satellite passes will then be recorded, though any that are low, near the horizon, and cross on short arcs may not be detected.

#### TYPES OF SOLAR BURSTS

In the previous article some elementary information regarding the sun was given so that some elements of the observations would become clearer. A brief description will now be given of the types of solar bursts that may be recorded during the observations. The types of burst are classified by numbers, each group having some special characteristic. The centres of activity are the disturbed regions and to give a basis of understanding the schematic diagram in Fig. 6.4 should be borne in mind.

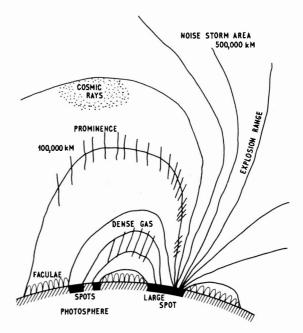


Fig. 6.4. Solar bursts. Diagram of a centre of radio activity on the sun

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2N697	18p	2N2925	22p	ACI26	20p	BC154	20p	BFY51	
2N706	12p	2N2926	Hp	ACI27	20p	BC157	12p	BFY52	20p
2N930	29p	2N3053	27p	AC128	20p	BC158	lip	BSX20	23p
2N1131	29p	2N3055	60p	ACI53K	22p	BC159	12p	C407	16p
2N1132	29 <sub>D</sub>	2N3702	13 <sub>p</sub>	ACI76	16p	BC167	ΙÍΡ	MC140	17p
2N1302	19p	2N3703	13p	ACY20	20p	BC168			25p
2N1303	19p	2N3704	13p	ACY22	16p	BC169	10p	MPS6531 MPS6534	35p
2N1304	26p	2N3705	i3p	ADI40	63p	BC177	14p	NKT211	30p
2N1305	26p	2N3706	13p	AD142	50p	BC178	13p	NKT212	25p
2N1306	33p	2N3707	13p	ADI49	58p	BC179	14p	NKT214	25p
2N1307	33p	2N3708	10p	ADI61	33 p	BC182L	iip	NKT274	23p
2N1308	36p	2N3709	Πp	AD162	36p	BC183L	100	NKT403	18p
2N1309	36p	2N3710	13p	AFI14	24p	BC184L	Пр	NKT405	65p
2N1613	23p	2N3711	13p	AFI15	24p	BC212L	16p	OC71	79p
2N1711	26p	2N3819	230	AFI17	22p	BC213L	16p	OC81	38p
2N1893	54p	2N3904	35p	AFI24	24p	BC214L	l6p	OCSID	25p
2N2147	95p	2N3906	35p	AF127	22p	BCY70	18p	ZTX300	25p 14p
2N2218	34p	2N4058	13p	AFI39	33 p	BCY71	33p	ZTX301	
2N2218A	44p	2N4059	10p	AF239	36p	BCY72	15p	ŽTX302	16p
2N2219	38p	2N4060	Hp	ASY26	27 p	BFI15	23p	ZTX303	22p
2N2219A	53p	2N4061	Πp	ASY28	27p	BF167	18p	ZTX304	27p
2N2270	62p	2N 4062	12p	BC107	ĪŽp	BF173	19p		
2 N2369A	I9p	2N4124	18p	BC 108	Hp	BF194	14p	ZTX500	18p
2N2483	35p	2N4126	27p	BC109	12p	BF195	15p	ZTX501	2lp
2N2484	42p	2N4284	15p	BC125	15p	BFX29	31p	ZTX502	25p
2N2646	47p	2N4286	15p	BC126	22p	BFX84	25p	ZTX503	22p
2N2904A	42p	2N4289	15p	BC147	10p	BFX85	52p	ZTX504	52p
							and here		

#### RESISTORS

Code	Power	Tolerance	Range	Values available	l to 9 (see no	10 to 99 te below)	100 up
0 0 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	1/20W 1/8W 1/4W 1/2W 1W 1/2W 1W 3W 7W	5% 55% 10% 55% 10% 20% ±1/20Ω 55%	82Ω-220ΚΩ 4-7Ω-470ΚΩ 4-7Ω-10ΜΩ 4-7Ω-10ΜΩ 4-7Ω-10ΜΩ 10Ω-1ΜΩ 0-22Ω-3-9Ω 12Ω-10ΚΩ 12Ω-10ΚΩ	E12 E24 E12 E24 E12 E24 E12 E12	9   	8 0-8 0-8 1 2 3-5 7	7 0·7 0·7 0·9 1·9 3 6

Codes: C=carbon film, high stability, low noise.
MO=metal oxide, Electrosil TR5, ultra low noise.
WW =wire wound, Plessey.

Fig. denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24 denotes series: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

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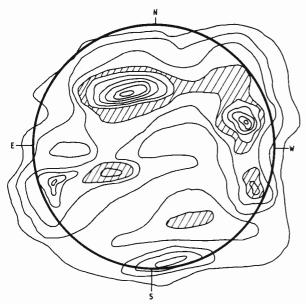


Fig. 6.5. Active ("radio") sun, showing concentration of high level activity

A centre of activity is visually observed as a sunspot. However the activity begins before the appearance of the actual spot and also continues after. During this time many changes of radio activity are observed. A magnetic field develops and it is as though a giant magnet lies beneath the surface of the photosphere. Where the field pro-

trudes through the chromosphere, the gas is made to glow and the hydrodynamic waves travel up the magnetic lines and produce bright streaks known as faculæ. The corona is also heated. It is after this phase that the actual sunspots appear.

The sunspots appear dark against the surface because they are at a slightly lower temperature. They are an indication of where the greatest magnetic concentration crosses the photosphere. Above the spots there is great activity. A great intensity of gas clouds occur high up in the corona: these are the prominences and are supported in their positions by the magnetic field.

During the time of the spot the major activity often results in flares. Although the flare is only an increase of intensity of line emission, the results are extensive. A terrific explosion may result with far reaching effects. A vast cloud of gas is ejected and drags the magnetic field with it. The gas and the magnetic field reach the earth about a day or so after, causing magnetic storms and aurora. A picture diagram of the radio sun is shown in Fig. 6.5.

Type I bursts do not follow closely after a flare but are nevertheless very important because the effect of such a burst lasts for a whole day. They are only found in the metre wave part of the spectrum, mostly between 100 and 150MHz. During such a storm there appear short bursts of great intensity that last only a few seconds. The trace that appears on the long time constant will not normally register these. They need a much higher recorder speed.

Type II bursts usually appear with very intense outbursts and are often associated with and follow Type III bursts. These are both the result of special

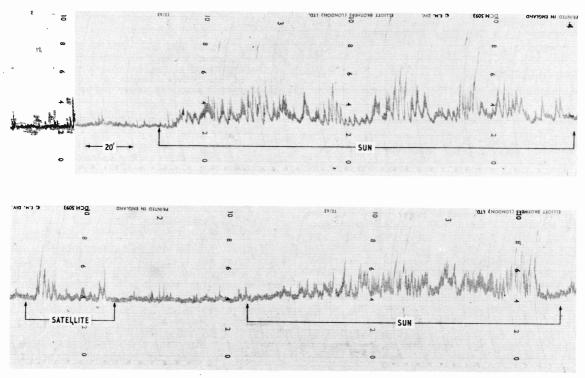
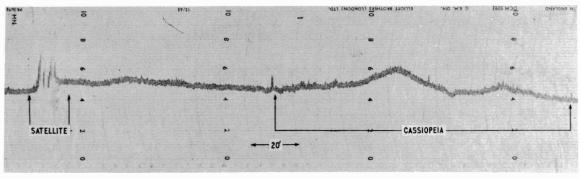


Fig. 6.6a, b. Recordings of the sun. Two examples of noise storms with random bursts and showing varying amplitude due to Faraday rotation



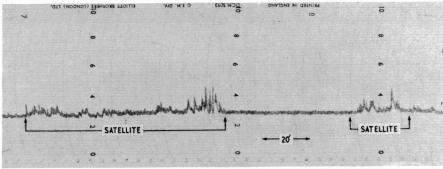


Fig. 6.7a Pen recording of a satellite and Cassiopeia. b Recording of two satellite passes

and fast moving disturbances in the corona resulting in the bunching of electrons.

Type IV bursts have a broad spectrum and show a high temperature. They follow after Type II bursts and seem to be a continuum.

Not so much is known about **Type V** bursts, but they may be similar in nature. Usually this activity is more noticeable at much higher frequencies and much remains to be done before the phenomena is fully understood.

#### **OBSERVATIONS**

It is now time to make the observations, and to

help in recognising the results, the pen recordings in Figs. 6.6 and 6.7 are given as a guide.

It would be a good plan to do a three- or four-days run in the noon period so that the observer becomes familiar with the appearance of the charts. Having found that the results are satisfactory, the full observations may then be undertaken.

The next article will deal with the extension of the simple telescope to form an interferometer. Details of the additional equipment that is required will be given so that the benefits of greatly increased sensitivity and resolving power can be obtained.

#### RETROSPECT AND PROSPECT

continued from page 889

After careful thought we have decided upon a solution. We are convinced there are many people who would like just to dabble without becoming too deeply involved in the subject. At the same time, there are endless possibilties using only simple and modest circuits for creating gadgets and items of real practical worth in all manner of everyday affairs. Designs for such gadgets ought to be even more widely disseminated than they are at present; and of course presented in a form to suit the person with limited experience. Also, the novice needs particular consideration and help.

We feel that such needs warrant the creation of an additional magazine—independent, yet having a certain association with PRACTICAL ELECTRONICS. So a new popular magazine, entitled *Everyday Electronics*, is due to make its bow next week. Our new companion will augment the service that PRACTICAL

ELECTRONICS' already provides, and will, we trust, encourage many more people to make their very first entry into this exciting branch of technology. And in a practical purposive manner, of course.

When our readers have examined a copy of this new magazine, we are sure they will wish to recommend it to many of their friends and acquaintances, as well as to their sons and other younger relatives.

Truly it can be said that electronics is a subject with many facets, and each facet seems to be taking on a different or certainly a broader countenance as the years go by. It is a challenging task, but PRACTICAL ELECTRONICS will continue to cover this expansive subject in the best manner to suit those tens of thousands of keen and serious devotees electronics has attracted. We like to feel that many of these followers were first introduced to electronics through this magazine, sometime during the last seven years.

The prospect looks good—and exciting.

F.E.B.



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## **Trial by Fury**

Sir-For unmentionable years I being of almost sound mind have read P.E., in fact I have that many that my wife gave me an ultimatum, either my P.E.'s go or she does. I might add that I miss her.

Now the thing that's worrying me is "why"?

Why is it that no matter how you plan a circuit, the transistors almost inevitably end up with the tails all

but tied in a granny knot.

Why when one buys a packet of assorted resistors or capacitors after ten years you still have them around. Why is it that your transistor collection, considered by friends to be so well planned an assortment, never contains the ones you want for a new circuit you fancy.

Why is it that, no matter where you put the soldering iron, the smell of burning sleeve or flesh is ever present. Why is it that the wife never appreciates the new gadget you've built even though you have offered to pay for a new tablecloth (it's only a small hole).

Why is it that even if you've successfully built a multi-frequency astable-bistable double switched stereophonic thingumy with a.g.c. at all levels, the main topic of conversation with visiting friends is the

Browns' new baby.
Why is it that friends consider your life should be spent repairing Japanese transistor radios, you spend three hours taking it out of the case, two hours finding a substitute transistor, another four hours putting back the guts and the run is usually ten fags and the remark that he thought it was only the battery.

Is it worth it, or should I give it all up? By the way, do you publish a book on Practical Knitting?

R. G. Taylor, Birmingham.

## Any offers!

Sir-I wonder if any reader or designer can help with the following project.

I am chairman of the Grimsby Group Hospitals Sports and Social Club, and since music and electronics are my hobbies, I am usually responsible for playing, organising music and purchasing or making amplifiers.

The sports club was founded just after the N.H.S. was formed and is run on a subscription basis; assets are obviously very limited.

During the past twenty rooms that used to be available for activities, in the local hospitals, have been swallowed up for other essential purposes. However, some twelve months ago we were given a disused old ward block. With our capital and voluntary labour from members, we have altered this building to our requirements, having used almost all our money.

Certain members have donated different items (e.g. piano, psychedelic lighting, etc). I have supplied tape recorder, built a sound system and even installed my elec-

tronic organ.

We are, however, very much in need of an auto-rhythm unit, but find these far too expensive for us to purchase. I have constructed drum units for contact (pedal) sounding for the organ—these work well. However, although I know that autorhythm units must be driven by pulses from a binary ring counter logic I cannot devise one myself.

I wonder if any of your readers can help with this project. Other items of less importance, e.g. echo, would be useful.

> E. C. Darnell. Waltham, Grimsby.

#### How about it!

Sir-I would like to say a few words, through your magazine, aimed at manufacturers and suppliers.

Now that D.I.N. connectors are becoming more popular and standard on most equipment nowadays. how about making 5-core cable readily available, and 4-core individually screened cable at least available, if not readily available.

A few words also, to other users.

How about creating a demand for these cables by using them when-ever you make up D.l.N. leads. It's cheaper in the long run, instead of making up dozens of different, single twin-core leads.

R. Williams, St. Albans,

## Sparking power unit!

Sir-Your Editorial on electronics in motor cars was timely and enthusiastic, without being at all "Beyond the Fringe"—no disrespect to Gerry Brown!

But the most telling point was "even the magic of electronics cannot save the internal combustion engine from ultimate extinction." I have for many years championed the cause of electric cars, and have urged the British car companies to do something. Only amateurs (as in radio's early days) appear to be doing anything.

Ten years ago, we were well ahead, and I made a forecast then that the first commercial electric car would be Japanese or European or American. How can we expect an electric car from this country when the designers haven't yet

heard of electronics?

Readers of P.E. must surely wince at a power unit which needs oil, petrol, sparks, air, water and grease pumped to it in sequence, all to drive four captive cannonballs, which drive a bent piece of metal, which turns a cog, which . . .

Over the years I have written to practically every newspaper and magazine trying to promote an Electric Car Rally, but with no takers.

E. A. Wadsworth, Scarborough.

#### **BACK NUMBERS**

We regret that back numbers of Practical Electronics can no longer be supplied. We are conscious that many readers frequently require reference to past projects and in order to go some way toward helping them we are prepared to devote a limited amount of editorial space to announcements of readers' requirements. We will try to publish these (without a guaranteed date) free of charge on the following conditions:

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40486						£1.20
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40432	6 Amp (RMS at 75° Amb.) 400 PIV* TO-	5 Mc	d.			£1-50
40512	2-2 Amp (RMS at 25° Amb.) 400 PIV*					£1-45
	*These types have integral triggering					
40576	15A (RMS) 400 PIV TO-66					£1.70
	BARGAIN TRIAC OF	FER				

40533 RCA 400V 2.5 AMP 60p

THYRIST	ORS				-	
	I Amp 50 PIV TO-5					40
CR1/401C	I Amp 400 PIV TO-5		 			50
2N3525	5 Amp 400 PIV TO-66		 	 		£1.0
40739	10 Amp 400 PIV Stud t	1tg.		 		£1.6

#### **ULTRASONIC TRANSDUCERS**



Operate at 40 kc/s. Can be used for remote control systems without cables or electronic links. Type 1404 transducers can transmit and receive. FREE: With each pair our complete transmitter and receiver circuit. PRICE (Sold only 10 casts) 15-90

(Sold only in pairs)

#### **ELECTRONIC** COMPONENTS

Mail Order Dept.: (PE) 7 Coptfold Road, Brentwood, Essex Industrial Sales Dept.: Tel.: Brentwood 226470/I Telex 99443

#### BODINE TYPE N.C.I. GEARED MOTOR



Torque 10b. inch. Reversible. 1/70th h.p., 50 cycle, 0.38 amp. (Type 2) 28 r.p.m. Torque 20lb. inch. Reversible. 1/80th h.p., 50 cycle, 0.28 amp. 50 cycle, 0.28 amp. 50 cycle, 0.28 amp. 15V a.c. Supplied complete with transformer for 230/240V a.c. input. Price, either type £3-15 plus 35 p P. & P. or less transformer £2-13 plus 27p P. & P. or less transformer £2-13 plus 27p P. & P. or less transformer £2-10 carr, where not specified.

#### 12 VOLT DC MOTOR

Powerful I amp. RE-VERSIBLE motor. motor. Speed 3,750 RPM complete with external gear train (removable) giving final speed of 125 RPM. Size: 4½" × 2½" dia. Price 95p inc. post.

#### 230Y/240Y COMPACT SYNCHRONOUS GEARED MOTORS



Manufactured by either Sangamo, Haydon or 5mith. Built-in gearbox. I rev. per hour. Clockwise rotation. I rev. per hour. Anti-clockwise rotation. 2 revs. per hour. Anti-clockwise rotation. 3 revs. per hour. Anti-clockwise rotation. 60 revs. per hour. I, r., m. Clockwise. Fraction of makers' price. All at 75p incl. P.&P

#### MICRO SWITCH

5 amp. c/o contacts. Fitted with removable push button assembly. Ex. P.O. 20 for £1 inc. post. (Min. order 20)

MINIATURE LEVEL METER

Approximately 300 micro amp basic, as fitted to Tape Recorders, etc. Strip type dual coloured dial. 50p + 8p P. & P.

A - NEW STREET



ELECTRONIC ORGAN KIT

Easy to build, Solid State. Two full octave (less sharps and flats). Fitted hardwood case. Powered by two penlite 1½V batteries. Complete set of parts including speaker, etc., together with full instructions and 10 tunes. Price £3-00. P. & P. 22p.

#### 50 in I ELECTRONIC PROJECT

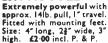
50 in I ELECT REJECT.

KIT

50 easy to build Projects. No soldering, no special tools required. The kit includes Speaker, Meter, Relay, Transformer, plus a host of other components and a 56-page instruction leafler. Some examples of the 50 leaflet. Some examples of the 50 possible Projects are: Sound Level Meter, 2 Transistor Radio, Amplifier, etc. Price £7-75. P, & P, 30p.

CRYSTAL RADIO KIT
Complete set of parts, including:
Crystal Diode, Ferrite Aerial, Drilled
Chassis, and Personal Ear Piece. No soldering, easy to build, full step by step instructions. £1.75 inc. post.

#### 230v AC SOLENOID





Mfg. by Westool, approx. I b pull (similar in appearance to above illustration). Size of feet 1 × 1 ¾ °. Price 85p incl. Post.

**VENNER Electric Time Switch** VENNER EIECCITIC IIME DWITCH 200/250V Ex. GPO. Tested. Manually ast 2 on, 2 off every 24h. Overrides switch: 10A (22.75, 15A 62.25, 20A 63.75, P. & P. 20p. Also off dawn. Price as above.

#### VARIABLE VOLTAGE TRANSFORMERS

All plus £1:00 carr, where not specified.

OPEN TYPE (Panel Mounting) ½ amp, £3.93.

1 amp, £5.50. 2½ amp, £6.63. Carr. 40p on open types.

2.5 AMP

## Superior Quality Precision Made

100 WATT. 1 ohm, 10A; 5 ohm, 4-7A; 10 ohm, 3A; 25 ohm, 2A; 50 ohm, 1-4A; 100 ohm, 1A; 250 ohm, 0-7A; 500 ohm, 1-4A; 100 ohm, 1A; 250 ohm, 0-7A; 500 ohm, 0-7A; 51 kΩ, 280 mA; 1-5 kΩ, 230 mA; 2-5 kΩ, 2A; 5kΩ, 140 mA. Diameter 3fin Shaft length fin, dia. fin, All at £1-50 each, P, & P, 5p, 50 WATT. 1/5/10/25/50/100/250/500/1/1-5/2-5/5kΩ. All at £1-10/25/50/100/250/500/1/1-5/2-5/3-5/5kΩ. All at 78p each, P, & P, 15p.

#### STROBE! STROBE! STROBE!

Build a Strobe Unit, using the latest type Xenon white light flash tube. Solid state timing and triggering circuit, 230/250V a.c. operation.

EXPERIMENTERS' ECONOMY KIT

Speed adjustable 1 to 36 Flash per sec. All electronic components including Veroboard S.C.R. Unijunction Xenon Tube and instructions £6:30 plus 25p P. & P. NEW INDUSTRIAL KIT

Ideally suitable for schools, laboratories, etc. Roller tin printed circuit. New trigger coil, plastic thyristor. Speed adjustable I-80 fp.s. Price £10:50. P. & P. 50p.

HY-LYGHT STROBE MK III

This strobe has been designed and produced for use in large rooms, halls and the photographic field, and utilizes a silica plugi-in tube for longer life expectancy, printed circuit for easy assembly, also a special trigger coil and output capacitor. Speed adjustable 0-30 fp.s. Light output approx. 4 joules. £12:00. P. & P. 50p.

SPECIALLY DESIGNED, FULLY VENTILATED

METAL CASE. Including reflector. £4:00 P. & P. 45p. Post paid with kit.

AND NOW!

#### AND NOW! THE 'SUPER' HY-LYGHT KIT

Approx. four times the light output of our well proven Hy-Lygh strobe. Incorporating:

Heavy duty power supply.

Variable speed from 1-23 flash per sec.

Fantastic Octal based tube with massive electrodes.

Fantastic Octal based rube with fantastic Hy-LyGHT gives fabulous effects with colour filters.

Never before a Strobe Kit with so HIGH an output at so LOW a price. ONLY £20 plus 75p P. & P.

ATTRACTIVE. ROBUST, FULLY VENTILATED METAL CASE specially designed for the Super Hy-Lyght Kit Including reflector, 67:00 P. & P. 45p.

7-inch POLISHED REFLECTOR

Ideally suited for above Strobe kits. Price 31p. P. & P.

Ideally suited for above Strobe kits. Price 53p. P. & P. 13p or post paid with kits.

#### RELAYS SIEMENS, PLESSEY, Etc. MINIATURE RELAYS . COMPETITIVE PRICES

1	2	3	4		_ 2	3.	4
45	6-9	2 HD M	50p	700	15-35	2 c/o HD	73p*
185	6-12	4 c/o	73p*	700	16-24	6M	63p*
230	9-12	4 c/o	78p*	1,250	24-36	4 c/o	63p*
280	9-12	2 c/o	73p*	2,500	36-45	6M	63p*
600	18-32	4 c/o	78p*	2,400	30-48	4 c/o	50p
700	16-24	4M 2B	63p*	5,800	40-70	4 c/o	63p*
700	16-24	4 c/o	78p*	9,000	40-70	2 c/o	50p*
700	12-24	2 c/o	63p*	15k	85-110	6M	50p*
(1) Coil ohms; (2) Working d.c. volts; (3) Contacts; (4) Price							

(HD) Heavy Duty. All Post Paid. \*Including Base

MAINS RELAY
230V a.c. coil 3 c/o. 10 amp a.c. contacts, 50p plus 8p P. & P.

#### ALARM BELL

Manufactured by GENTS. 6 inch bell 3/6 volt D.C. operation. As NEW. ONLY £1-50 P. & P 45p.



## D)

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Personal callers only. Open Sat. 9 LITTLE NEWPORT ST. LONDON WC2H 7JJ 01-437 0576 Professional receivers. supplied to Govt. Depts., Laboratories, Industry, Radio and TV Authorities. etc.

**BUY DIRECT AT PRICES 15% BELOW RETAIL VALUES** 

#### THE MENULLET TE 3065

is a high quality COMMUNICATIONS **RECEIVER** 

(replaces NA 5018A) Recommended Price

£37.80 @



(Cash only) plus 62p P. & P. Complete y standard batteries and earpiece. BFO (optional extra) add £1-75.

(optional extra) add £1/75.

IT NOT ONLY RECEIVES Aircraft, Shipping (VHF and SW), Taxis, Ambulances, Fire Service, TV Sound, Hams, Gas and Electric Boards, Public Services and many other radio telephone mobiles—BUT ALSO Classical Music, Pop and all that Jazz.

The MPR 3065 is a communications receiver The MPR 3065 is a communications receiver and entertainment source in one neat, transistorised, portable package. Features a colour coded illuminated tuning dial and band selector, AFC, squelch, BFO (optional extra), large speaker, Ext. Aerial Socket. Works off mains or batteries. Size: 10½in × 7½in × 4in. 22 Transistors/Diodes. FREQUENCIES: Medium Wave, 540-1,600Kcs.; Marine, 1-6-4-6Mcs.; FM/VHF, 88-108Mcs.; Aircraft, 108-136Mcs. (Military, Civil and Ground control); High VHF/PB, 146-176Mcs. (Commercial and Industrial RT mobiles). Industrial RT mobiles).

#### **MODEL MPR 3016 6 BAND**



SAME BANDS AND FREQUENCIES AS MODEL MPR 3065 PLUS ADDED FEATURE OF SW 50–12-0Mes. (with Fine Tuner). Batts, and Earpiece incl. Plus 62‡p P. & P. Styled in elegant black case with luxury Chrome trim, soft padded speaker grille, die-cast sides and walnut insert. Size 83in × I lin × 3∄in. Wt. 5lb approx. Enclose 5d stamp for-reply. Trade supplied

#### NEW! FROM "LAFAYETTE"

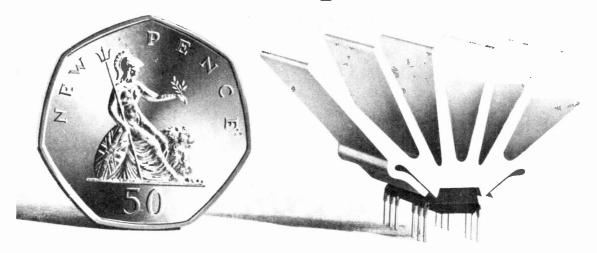
4 Band TV Sound Battery Portable with PB Mobile Band (146-176MHz).

TV sound channels 2-13, VHF/FM local and national radios, PSB RT mobiles. Our Price £27-95 Plus 50p P. & P. complete with batteries, earpiece, circ. diagram, AC adaptor socket; external aerial socket.

STOCKTON PARTNERS (Dept. "PE") Importers and Distributors Brighowgate, Grimsby, Lincs. Tel. 0472 64196/58815



# Super IC-12



## High fidelity Monolithic Integrated Circuit Amplifier

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

- 1. Higher power.
- 2. Fewer external components.
- 3. Lower quiescent consumption
- 4. Compatible with Project 60 modules.
- Compatible with Project 60 modules
   Specially designed built-in heat sink.
- No other heat sink needed.

  6. Full output into 3, 4, 5 or 8 ohms
- 7. Works on any voltage from 6 to 28 volts without adjustment.
- 8. NEW 22 transistor circuit

#### SINCLAIR GENERAL GUARANTEE

Should you not be completely satisfield with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are available to all Sinclair customers.

Output power 6 watts RMS continuous (12 watts peak).

Frequency Response 5 Hz to 100KHz  $\pm$  1 dB.

Total Harmonic Distortion Less than 1%. (Typical 0.1%) at all output powers and all frequencies in the audio band.

Load Impedance 3 to 15 ohms.

Power Gain 90dB (1,000,000,000 times) after feedback.

**Supply Voltage** 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).

Size  $22 \times 45 \times 28$  mm including pins and

Input Impedance 250 Kohms nominal.

Quiescent current 8mA at 28 volts.

With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Price, inc. **FREE** printed circuit board for mounting.

£2.98 Post free

Sinclair Radionics Ltd, London Rd, St. Ives Huntingdonshire PE17 4HJ Telephone St Ives (048 06) 4311



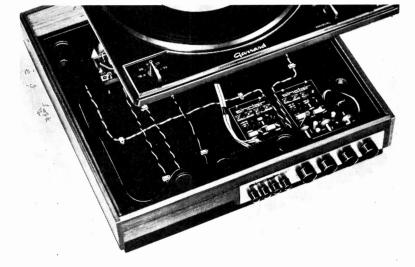
Practical Electronics November 1971 945

## Sinclair Project 60

## The World's leading range of high fidelity modules







## New! Project 605

The easy way to buy and build **Project 60** 



Project 605 is one pack containing: one P25, two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free £29.95

All you need for a superb 30 watt high fidelity stereo amplifier.

Sinclair Radionics Limited, London Road, St. Ives, Huntingdonshire PE17 4HJ. Tel: St. Ives (048 06) 4311



Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

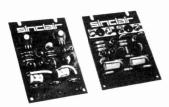
Project 60 modules are more versatile — using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all — price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

#### Typical Project 60 applications

System	The Units to use	together with	Cost of Units			
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control	£4.48			
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P U. volume control etc.	£9.45			
20 + 20 W. stereo amplifier for most needs	2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90			
20 + 20 W. stereo amplifier with high performance spkrs.	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90			
40 + 40 W. R.M.S. de-luxe stereo amplifier	2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As above	£34.88			
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43			
F.M. Stereo Tuner (£25) 8	F.M. Stereo Tuner (£25) & A.F.U. Filter Unit (£5.98) may be added as required.					

## from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules

#### Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications). **Power Outputs** 

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts.

Frequency response: 30 to 300,000Hz±1dB Distortion: 0.02% into 8 ohms

Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms For speakers from 3 to 15 ohms impedance.

Size: 14 x 80 x 57 mm

Built, tested and guaranteed with circuits and instructions manual. £4.48

Built, tested and guaranteed with circuits and instructions manual. £5.48

#### Power Supply Units

Designed special for use with the Project 60 system of your choice. Use PZ 5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

PZ.530 volts unstabilised £4.98 PZ.635 volts stabilised £7.98 PZ.8 45 volts stabilised less mains transformer) £7.98 PZ.8 mains transformer £5.98



#### The Sinclair Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charged at cost

#### Project 60 Stereo F.M. Tuner



First in the world to use the phase lock loop principle

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz. Capture ratio: 1.5d8. Sensitivity: 2µV for 30d8 quieting: 7µV for lock-in over full deviation. Squelch level: 20µV. A.F.C. range: ±200 KHz. Signal to noise ratio: > 65d8. Audio frequency response: 10 Hz - 15 KHz (±1d8). Total harmonic distortion: 0.15% for 30% modulary. tion. Stereo decoder operating level: 2µV. Cross talk: 40dB, Output voltage: 2 x 150mV R.M.S. Operating voltage: 25-30 VDC, Indicators: Power on/tuning/stereo, Size: 93 x 40 x 207 mm. £25

Built and tested. Post free.

#### Stereo 60 Pre-amp/control unit



Designed for Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS—Input sensitivities: Radio - up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A curve ±1dB:20 to 25,000 Hz. Ceramic p.u. - up to 3mV: Aux - up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE + 15 to -15dB at 10 KHz: BASS + 15 to -15dB at 100Hz. Front panel: brushed aluminium with black knobs and controls, Size: 66 x 40 x 207mm. £9.98 Built tested and guaranteed.

#### A.F.U. High & Low Pass Filter Unit



For use between Stereo 60 unit and two 7 30s or 7 50s and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less

loss of the wanted signal than has previously been possible. Amplitude and phase disloss of the wanted signal than has previously open possible. Ampirical and priese distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. Two filter stages – rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V, supply (0.02% at rated output. Size: 66 x 40 x 90 mm. Built tested and guaranteed.

To: SINCLAIR RADIONICS LTD LONDON ROA	D ST. IVES HUNTINGDONSHIRE PE17 4HJ
Please send .	Name
	Address
l enclose cash/cheque/money order.	P.E. 1171

## Sinclair Q16/Micromatic

#### Q16 High fidelity loudspeaker

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies without loss.

This elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

#### Specifications:

**Construction:** Special sealed seamless sound or pressure chamber with internal haffle.

Loading: up to 14 watts RMS.

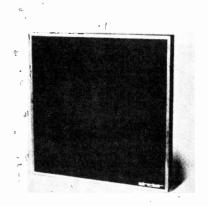
Input Impedance: 8 ohms.

Frequency response: From 60 to 16,000 Hz. confirmed by independently plotted B and K curve.

**Driver unit:** Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special cone suspension for excellent transient response.

**Size and styling:**  $9\frac{1}{4}$  in. square on face x  $4\frac{3}{4}$  in. deep with neat pedestal base. Black all over cellular foam front with natural solid teak surround.

Price £8.98.



#### Britain's smallest radio

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver brilliantly designed to provide remarkable standards of selectivity, power and quality for its size. Powerful AGC counteracts fading from distant stations: bandspread at higher frequencies makes reception of Radio 1 easy. The plug-in magnetic earpiece provided, matches the Micromatic's output to give wonderful standards of reproduction. Everything including the special ferrite rod aerial and batteries is contained within the minute attractively designed case. Whether you build a Micromatic kit or buy this amazing receiver ready built and tested, you will find it as easy to take with you as your wrist watch, and dependable under the severest listening conditions.

#### Specifications:

Size:  $36 \times 33 \times 13$  mm (1.8 x 1.3 x 0.5 in.) Weight: including batteries, 28.4 gm (1.0z.)

Case: Black plastic with anodised aluminium front panel and spun aluminium dial

**Tuning:** medium wave band with bandspread at higher frequencies (550 to 1,600 KHz).

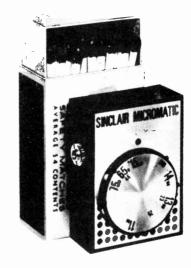
Earpiece: Magnetic type.

**On/off switching:** By inserting and withdrawing earpiece plug.

Kit in pack with earpiece, case, instructions and solder £2.48.

Ready built, tested and guaranteed, with earpiece £2.98.

Two Mallory Mercury batteries type RM675 required from radio shops, chemists, etc.



Sinclair Radionics Ltd., London Rd, St. Ives
Huntingdonshire PE17 4HJ.
Telephone St. Ives (048-06) 4311

To: SINCLAIR RADIONICS LTD LONDON	ROAD ST. IVES HUNTINGDDNSHIRE PE17 4HJ
Please send	Name
	Address
for which I enclose cash/cheque/money order	P.E. 31 71



## YATES ELECTRONICS

(FLITWICK) LTD

#### RESISTORS

W Iskra high stability carbon film—very low noise—capless construction. W Mullard CR25 carbon film—very small body size 7.5 × 2.5mm. 4W

Power			Valves	Price	
watts	Tolerance	Range	available	1-99	100+
1	5% 10%	4-7Ω=2-2MΩ 3-3MΩ=10MΩ	E24 E12	1 Op	0.8p
1	io%	$1\Omega = 3.9\Omega$	E12	I-0p I-0p	0.8p
	5%	4·7Ω-IMΩ	E12	I-Op	0.8p
. 4.	10%	$1\Omega = 10\Omega$	E12	6p	5-5p

Quantity price applies for any selection. Ignore fractions on total order

#### DEVELOPMENT PACK

0.5 watt 5% Iskra resistors 5 off each value  $4.7\Omega$  to IM $\Omega$ . E12 pack 325 resistors £2.40, E24 pack 650 resistors £4.70.

#### POTENTIOMETERS

Carbon track  $5k\Omega$  to  $2M\Omega$ , log or linear (log  $\frac{1}{2}W$ , lin  $\frac{1}{2}W$ ). Single, 12p. Dual gang (stereo), 40p. Single D.P. switch 24p.

#### SKELETON PRESET POTENTIOMETERS

Elinear: 100, 250, 500 \( \Omega\$ and decades to 5M\( \Omega\$. Horizontal or vertical P.C. mounting (0-1 matrix). Sub-miniature 0-1W, 5p each. Miniature 0-25W, 6p each.

SEMICO	NDUC	TORS
AC126	12p	BFY52

AC126 AC127 AC128 AD140 AF115 AF117 BC107 BC108 BC109 BFY50 BFY51	12p 12p 12p 40p 20p 10p 10p 10p 22p 22p	BFY52 B5Y56 B5X21 BY124 BYZ10 BYZ13 OA85 OA91 OA202 OC71 OC72	22p 30p 25p 74p 20p 20p 7p 5p 7p 12p	OC81 OC82 ORP12 IN4001 IN4002 IN4003 IN4004 1 N4005 IN4006 IN4007 2N2926	12p 12p 48p 71p 10p 11p 12p 13p 13p 13p	2N3055 2N3702 2N3703 2N3704 2N3705 2N3706 2N3707 2N3708 2N3709 2N3710 2N3711	72p 15p 14p 17:p 12p 18:p 10p 11p 12p
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ZENER DIODES 400mW 5% 3 3V to 30V, 15p.

ROTARY SWITCHES 2P2W, IP12W, 2P6W, 3P4W, 2P2W, IP 4P3W, 23p.

BRUSHED ALUMINIUM PANELS

 $12in \times 6in = 25p$ ;  $12in \times 24in = 10p$ ;  $9in \times 2in = 7p$ .

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5p stamp appreciated.

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0.015μF, 0.022μF, 0.033μF, 13p. 0.047μF, 0.068μF, 0.1μF, 4p. 0.15μF, 6p. 0.22μF, 71p.
160V: 0.01μF, 0.015μF, 0.022μF, 0.033μF, 10-068μF, 3p. 0.1μF 31p. 0.15μF 41p.
0.22μF, 5p. 0.33μF, 4p. 0.47μF, 71p. 0.68μF, 11p. 1.0μF, 13p.

MULLARD POLYESTER CAPACITORS C283 SERIES
250V P.C. mounting: 0.01μF, 0.015μF, 0.022μF, 3p. 0.033μF, 0.047μF, 0.068μF,
31p. 0.1μF, 4p. 0.15μF, 0.22μF, 5p. 0.33μF, 61p. 0.47μF, 81p. 0.68μF, 11p. 1.0μF, 13p.

MYLAR FILM CAPACITORS 100V 0·001μF, 0·002μF, 0·005μF, 0·01μF, 0·02μF, 2½p. 0·04μF, 0·05μF, 0·068μF, 0·1μF, 3½p.

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	0.1	0.15
21 × 31	22p	16p
2½×5	24p	24p
3½ × 3½	24p	24p
3∄ × 5 ¯	27p	27p
17 × 2+	75p	57 i p
	100p	75p
17 × 5 (plain)		75p
17 ×3∄ (plain)		52 ip
17 ×2+ (plain)		3212
$2\frac{1}{2} \times 5$ (plain)	_	37 ip
21 0 3 (Plain)		17 1p
$2\frac{1}{2} \times 3\frac{1}{4}$ (plain)	<del></del>	15p
Pin insertion tool		47 p
Spot face cutter	37 fp	37 p
Pkt. 50 pins	20p	20p

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Standard screened trandard insulated Stereo screened Standard socket Stereo socket	12p 35p 15p	2:5mm insulated 3:5mm insulated 3:5mm screened 2:5mm socket 3:5mm socket	8p 8p 13p 8p 8p
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2N1309 2N1613 2N1711	22p 25p	BC147 BC148 BC149	12p 20p	MPF104 87p MPF105 40p	١
2N2147	75p	BC154 BC157	87p	NKT21740p	۱
2N2160 2N2218	60p 20p	DOTES	20p 17p	NKT27720p NKT40375p NKT40482p	ı
2N2219 2N2222	20p 20p	BC159 BC169C BC177	20n	NKT40462p OA5 20p	١
2N2222	425p	BC177	15p 25p	OA9 10p	١
2N2369 2N2484	20p 35p		25p 27p	OA10 25p OA47 10p	ı
2N2484 2N2646 2N2904	50p 20p	BC179 BC182L BC183L	12p 12p	OA70 10p	
2N2904	4.25p	BC184L	15p	OA79 10p	1
2N2905 2N2906	25p 20p	BC212	12p 25p	OA81 10p OA85 12p	1
2N2906	425 b	DOVES	30p	OA90 10p	1
2N2907 2N2926	23p 10p	BCY32 BCY33	50p 25p	OA95 7n	1
2N3011 2N3053 2N3054	25p 20p	BCY32 BCY33 BCY34 BCY38 BCY39	30p 40p	OA200 7p	
2N3054	50p	BCY39	8 <b>5</b> p	LOC16 50n	ı
2N3055 2N3525	75p	BCY40 BCY58	50p 25p	OC20 97p OC22 50p OC23 60p	
2N3709	1·10 10p	BCY59 BCY70	25p 15p	LOC24 60n	ı
2N3703 2N3704	100	BCY71 BCY72	20p	LOC'05 97n	1
1 2 N 3705	15p 15p	BCY78	15p 80p	OC28 60p	ı
2N3707 2N3709	15p 10p	BCY79 BCZ10	30p 35p	OC29 60p OC35 50p	
2N3710	10n	BCZ11	45p	OC36 60p	١
2N3819 2N3820	35p 60p	BD112 BD121	50p 65p	OC41 25p OC42 30p	-
2N4058 2N4061	15p 15p	BD123	80p 75p	OC43 40p	
2N5457	25n	BD124 BD125	50p	OC45 15p	ı
2N5458 2N5459	37p 50p	BD131 BD132	75p 85p	OC70 12p OC71 15p	-
28301 28302	50p	BD132 BD153 BD156	62p 57p	OC72 25p	
28302 28303 28304	60p	BDY10#	1.25	LOC74 20b	
40250	75p 50p	BDV17	1.50	OC75 25p OC76 25p	
40361	50p	BDY182	1.75	OC77 40p OC81 25p	
AAY30	10p	BDV61#	1 - 2.5	OC82 25p	
AAY30 AAY42 AAZ13 AAZ17	15p 12p	BDY62£ BF115	1.00 25p	OC84 25p	
AAZ17	10p	BF152 BF154	30n	IOC139 25 p	ı
AC126 AC127	37p 25p 25p	BF154 BF158 BF159	40p 30p	OC141 82p	J
AC127 AC128	9.5 n	BF167	60p 25p		ı
AC127 AC128 AC176 AC187 AC188	25p	BF170	35p	OC170 25p OC171 30p OC200 40p OC201 70p OC202 80p OC203 40p OC204 40p OC205 75p	ı
AC188	30p 30p	BF170 BF173 BF177	30p 40p	OC201 70p	ı
ACY17 ACY18 ACY19	80p	BF178 BF179	25p 40p	OC203 40p OC204 40p	ı
ACT19	25n	BF180	35p	OC205 75p OC206 90p	ı
ACY20 ACY21	20p 20p	BF181 BF182	35p 30p	OC207 90p	ı
LACY22	10p 50p	BF184 BF185	20p 20p	OCP71 97p ORP12 50p	ı
ACY39 ACY40	15n	BF194 BF195	17p 15p	ORP60 40p	ı
AD140 AD149	50p 50p	BF195 BF196	15p 15p	ORP61 42p TIP29A 50p TIP30A 60p	ı
AD161 AD162		BF197 BF200	15p	TIP31A 62n	ı
AF114	37p 37p 25p	BF274	37p 37p	TIP32A 75p TIP33A	۱
AF115 AF116	25p	BFX13 BFX29 BPX30	25p 25p	£1 00	ı
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AF118 AF124	25 <sub>0</sub>	BFX37 BFX84 BFX85	25 n I	TIS43 40p	ı
AF125 AF126 AF127	20p 17p 17p	BFX86	25p	TIS60 22p TIS61 25p	ı
AF139	3lln I	BFX86 BFX87 BFX88	25p 20p	T1862 27p	۱
AF178 AF179	47p 65p	BFY18 BFY50	30p I	ZTX 108 15p	۱
AF180	52n	BFY51	22p 20p	ZTX300 12p ZTX301 15p	į
AF181 AF186	42p 40p	BFY52 BFY53	22p 17p	ZTX302 20p ZTX303 20p	١
AF239	40p	BFY90	65 p l	ZTX504 25p	ı
ASY26 ASY27 ASY28	25p 32p	BSX20 BSX21 BSX76	17p 20p		ı
A8Y28	25p	BSX76 BSY95	15p	ZTX502 25p ZTX503 20p ZTX504 40p	١
A8Y29 A8Y67	47p 42p	BSY95A	15p 15p	ZTX504 40p ZTX531 30p	ı
ASZ21 BA115	7D I	BY100 BY126	15p 15p		ı
RA164	10p 6p	8Y127 BY182	20p 85p	DISCOUNTS 10% 12+	ı
BAX16	7 P I	BYZ10	40p	15% 25+	ı
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## HENRY'S LOW INTEGRATED CIRCUITS

WE OFFER FROM STOCK AN EXCLUSIVE RANGE OF BRAND NEW CERAMIC FULL SPECIFICATION LOW COST TTL 7400 RANGE BY I.T.T., TEXAS, FAIRCHILD

	_			_						
Part					rice					
No.	Ceramic Description		1-2				100		50 +	
7400	Quadruple 2-input NAND Gate		20	p	18p		15p		13p	
7401	Quadruple 2-input Positive NAND Gate									
=+00	(with open collector output)		20		18p		15p		13p	
7402	Quadruple 2-input Positive NOR Gates		20	p	18;	)	15p		13p	
7403	Quadruple 2-input Positive NAND Gates									
	(with open collector output)		20		18;		15p		13p	
7404	Hex Inverters		20		18p		15p		13p	
7405	Hex Inverter with open collector		20		18;		15p		13p	
7410	Triple 3-input Positive NAND Gates		20		18p		15p		13p	
7413	Dual 4-input Schmitt Trigger		35 <sub>1</sub>		32p		29p		25 p	
7420	Dual 4-input Positive NAND Gates		26		18p		15p		13p	
7430	8-input Positive NAND Gates		20		18p		15p		13p	
7440	Dual 4-input Positive NAND Buffers		20		18p		15p		13p	
7441	BCD to decimal nixie driver		871		77p	11	ввр		60p	
7442	BCO to decimal decoder (4-10 lines, 1 of 10)		871	)	77p		67p		60p	
7447	BCD-Seven Segment Decoder/Drivers									
	(15-V Outputs)	£1	40	£1	30	£1	20	£1	05	
<b>74</b> 50	Expandable dual 2-input AND-OR-INVERT		20		18p		15p		13p	
<b>745</b> 1	Dual 2-wide 2-input AND-OR-INVERT GATES		20	p	18p		15p		13p	
7453	Quad 2-input Expandable AND-OR-INVERT		20	p	18p		15p		18p	
7454	4-wide 2-input AND-OR-INVERT Gates		20	P	181	•	15p		12p	
7460	Dual 4-input Expander		20	p	18p		15p		13p	
7470	Single-phase J-K Flip-Flop		351	,	32p		29p		25p	
7472	Master-slave J-K Flip-Flop		351	,	32p		29p		25p	
7478	Dual Master slave J-K Flip-Plop		431	,	40p		37p		33p	
7474	Dual O type Flip-Flop		43		40p		37p		33p	
7475	Quad latch		471		45p		43p		40p	
7476	Dual J-K with pre-set and clear		471		45p		43p		40p	
7480	Gated Full Adders		871	,	77p		67p		60p	
7481	16-bit read/write memory	£1.			25				00	
7482	2-bit Binary Full Adders	£1	.30	£1	20	£1	-00		85p	
7488	Quad Full Adder		871		77p		67p		60p	
7496	Quad 2 input Exclusive OR Gates		801	,	70p		60p		50p	
7490	BCD decade counter		871		77p		67p		60p	
7491	8-bit Shift Registers	£1	21	£1	.00		87p		75p	
7492	Divide-by-Twelve Counters		871	)	77p		67p		60p	
7493	4-bit Binary Counters		871	,	77p		67p		60p	
7494	Dual entry 4-bit shift register		871	,	77p		67p		60p	
7495			871	)	77 p		67p		60p	
7496	5-bit Parallel in parallel out Shift Register		871		77p		67p		60p	
74100	8-bit Bistable Latches	£1	75	±1	65	21	65	£1-	85	
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74121	Monostable Multivibrators		871	)	77p		67p		60p	
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44101	o-bit Data Selectors (With Strobe)	£1	40	£1	80	£1	20	£1.	05	
	Dual 4-Line-to-1-Line Data Selectors/Multiplexer	я 🛃	l 40	£1	30	£1	20	£1.	05	
		£2	-50	£2	•25	£2	00	£1	50	
Device	es may be mixed to qualify for quantity price.									
Data e	wailable for above series in booklet form, price 10p.									
Large	quantity prices Extn. 4. Dual Inline 14 Pin Socke	et :	30p	eac	h 16	Pi	n 3	óρ (	ach.	

SI	LI	CO	N	RE	C.	TI	FI	E	R	S

1 AMP	MINIA		WIR		ED PL	ASTIC
		K EU	LILIE	RS		
Type	P.I.V.	1-49	50 +	100 +	500 + 1	+000
IN4001	50	8p	7p	6р	5p	4 p
IN4002	100	9p	8p	7p	5 ∤ p	4 t p
IN4003	200	10p	9p	710	6р	5 p
IN4004	400	10p	9p	8p	7p	Ğр
IN4005	600	12p	10p	9 p	7p	7 p
IN4006	800	15p	14p	12p	11p	9p
IN4007	1000	20p	16p	13p	12p	10p
1.5 AM	MINIA	ATURE	wir	EEND	ED PL	ASTIC

1.5 AM	MINI		E WIR		ED PLA	ST
Туре	P.I.V.	1-49	50 +	100 +	500 + 10	000
PL4001	50	10p	9p	8p	7p	
PL4002	100	11p	10p	9p	8p	7

PL4003	200	12p	11 p	10p	9p	8p
PL4004	400	12p	11p	10p	8p	8p
PL4005	600	15p	13p	11p	10p	91
PL4006	800	17p	15p	13p	12p	10
PL4007	1000	20p	17p	15p	13p	11p
3 AMP P	LASTI	C WI	RE EN	DED I	RECTIF	TERS
Type I	P.I.V.	1-49	50+	100+	$500 \pm 1$	000+
PL7001	50	20p	18p	17p	16p	14p
PL7002	100	20p	19p	18p	17p	15p
PL7003	200	22p	20n	19n	18n	160

## POTTED BRIDGE RECTIFIERS (SILICON) SIZE 1 x 1 x 1ins.

1		Cur-				
Type	P.I.V	. rent	1-49	50 +	100 +	500 +
1002	100	2 amps	60p	55p	50p	45p
2002	200	2 amps	70p	65p	60p	55p
4002	400	2 amps	80p	75p	70p	65p
1004	100	4 amps	70p	60p	55p	50p
2004	200	4 amps	75p	70p	65p	60p
4004	400	4 amps	80p	75p	70p	65p
6002	600	2 amps	90p	80p	75p	70p
6004	600	4 amps	90p	8 <b>0</b> p	75p	70p
1006	100	6 amps	75p	70p	65p	60p
2006	200	6 amps	80p	75p	70p	65p
4006	400	6 amps	£1·10	£1.00	90p	80p
6006	600	6 amps	#1-25	£1-10	£1 00	90 n

## INTEGRATED CIRCUITS

THOT CAU	/UF	עטט טאוען ווע
	£1·12	MC1304 £2.75
I.C. 12	£2.75	MC724P 60p
PA246	£2·45	741c (T05) 85p
TAA263	75p	741c (DIL) 85p
TAD100	£1-97	709c (T05) 65p
TAD110	£1.97	709c (DIL) 65p
MC1303	£2-60	Toshiba 20 watt
UL900	40p	Amp 24.47
UL914	40p	Toshiba
UL923	40p	PreAmp 21:50
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Volt. 15p each.
25+ 12p; 100+ 10p; 500+ 8p;
1000 + 6p. Any one type.
11 Watt 5% Metal case. Wire Ends.
6.8V. all voltages to 100V. 25p each.
25+ 22p; 100+ 19p; 500+ 17p;
1000+ 15p. Any one type.
3 Watt Plastic Wire Ends 5%
All voltages 6-8-100V. 30p each.
95 ± 97n · 100 ± 95n · 500 ± 99n ·

25+ 27p; 100+ 25p; 500+ 23p; 1000+ 21p. Any one type. 10 Watt Stud Mounting 5% All voltages 5:1-100V. 40p each. 25+37p; 100+35p. Any one type.

#### TRIACS

	P.I.	Cur-	(All stu	id moi	inting)
Type	Volts	rent	1-49	50 +	100+
8C35A		3 amps	90p	75p	65p
8C35B		3 amps	95p	80p	70p
8C35D		3 amps	£1.00	85p	75p
SC40A		6 amps	£1.00	85p	75p
SC40B		6 amps	£1-20	£1 00	
8C40D		6 amps	£1.25	£1·10	£1.00
		0 amps	£1.25	£1·10	£1.00
		0 amps	£1.35	£1 20	£1-10
8C45 D	400 3	0 amps	±1.50	£1:35	£1-20
		5 amps	£1.65	£1 50	£1.35
		5 amps	£1.75	£1.60	£1-45
SC50D	4001	5 amps	£2.00	£1.75	£1.60
		6 amps	£1.50	£1.25	£1-10
8C45 E	500 ]	0 amps	£1.75	£1-50	£1 35
SC50E	500 1	5 amps	£2.25	£2-00	£1.75
DIAC					
Larger	quant	ity price	s Extn.	4	

#### **SEMI-CONDUCTORS**

LOOK AT THESE PRICES FOR QUANTITIES FROM STOCK

25 + 20p	25 + 20p
100 + 17p	100 + 17p
500 + 15p	500 + 15p
AFII6 Mullard 25p	AFII7 Mullard 25p
25 + 20p	25 + 20p
100 + 17p	100 + 17p
500 + 15p	500 + 15p
2N3055 75p	2N3819 Texas 35p
Mullard 115watt	25 + 30p
Silicon Power	100 + 25p
25 + 65p	500 + 20p
100 + 50p	1000 + 18p

Name and Address of the Owner, where the Owner, where	A DESTRUCTION OF THE PARTY OF T
BFY90 65p	2N2646 40p
1000 MC/5	Motorola
25 + 60p	Unijunction
100 + 55p	25 + 35p
500 + 50p	100 + 30p

300 + 30p	500 + 25p
AF139 30p Siemens V.H.F. 25 + 25p 100 + 22p 500 + 19p	AF186 40p Mullard V.H.F. 25 + 35p 100 + 30p 500 + 25p
OC170 Mullard 25p	

C170 Mullard 25p 25 + 21p 100 + 17p 500 + 15p	BYZI3 25p Mullard 6a 200v 25 + 20p 100 + 17p
CI71 Mullard 30p	
25 + 27p	BCIOT BCIOS

100 + 22p	BC107, BC108,
DVIOTAL II 120	BCI09 I2p each
BY127 Mullard 20p 1000v I amp Plastic	
25 + 17p	100 + 10p
100 + 15p	500 + 8p

300 + 13p	OCP71 97p
BCII3 SGS I5p	Muliard Photo
25 + 13p 100 + 11p	25 + 85p 100 + 80p
500 + 9n	500 + 75p

OA202	I0p	OC28 62
SILICON D	iodes	Mullard Power
25 + 8		25 + 55p
100 + 6	P	100 + 50p
500 + 5	р	500 + 42p
1000 + 4	P	Company of the second second

	OC71 Mullard 15p
0C42 Mullard 30p 25 + 25p	25 + 12p 100 + 10p
100 + 23p	500 + 8p
500 + 21p 1000 + 18p	OPPL2 Mulland FOR

	OKP12 Mullard 50
0C45 Mullard 15p 25 + 13p 100 + 12p	25 + 45p 100 + 42p 500 + 40p
500 + 10p 1000 + 8p	2N930 25p
OC75 Mullard 25p	100 + 20p

25 + 21p 100 + 17p	100 + 20p 500 + 17p 1000 + 15p
500 + 15p 1000 + 13p	0C72 Mullard 25p 25 + 20p
C20 97p	100 + 17p 500 + 15p 1000 + 13p

OC20 97p Mullard 100v 25 + 85p	500 + 15p 1000 + 13p
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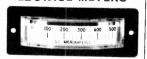
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2N1305 22p 2N3715 222p 40348	52p BC182 12p BSX28 32p OC19 37p		6BR8 65p DK92 50p PCF806 70p
2N1306 24p 2N3716 290p 40360	42p         BC182L         10p         B8X60         82p         OC20         75p           47p         BC183         10p         B8X61         62p         OC22         50p           55p         BC183L         10p         B8X76         15p         OC23         60p	CA3049 160p MC1305P 225p	6BW6 85p DK96 42p PCF808 75p
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2N1308 25p 2N3791 275p 40362		CA3051 184p MC838P 225p	6BZ6 35p DL94 45p PCL83 65p
2N1309 24p 2N3819 34p 40370	32p         BC184         15p         BSX77         20p         OC24         60p           57p         BC184L         12p         BSX78         25p         OC25         37p           40p         BC186         25p         BSY24         15p         OC26         25p	CA3052 165p 549p 8N74193	6C4 33p DL96 42p PCL84 45p
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2N2193 40p 2N3866 150p AC127 2N2193A 42p 2N3877 40p AC128 2N2194 27p 2N3877A 40p AC151	24p BCY39 60p BSY51 32p OC72 12p 20p BCY40 50p BSY52 32p OC73 30p 18p BCY41 15p BSY53 37p OC74 30p	FCH181 105p   PA424   285p   TAA521 132p   FCH191 105p   PA264   447p   TAA522 360p   FCH201 180p   PA265   487p   TAA530 495p	6J6 20 EC86 60 PY82 30 F 6J7 45 EC88 60 PY83 38 F
2N2194A 30p 2N3900 37p AC152 2N2217 27p 2N3900A 40p AC154 2N2218 20p 2N3901 97p AC176	22p BCY42 15p BSY54 40p OC75 22p 22p BCY43 15p BSY56 90p OC76 22p 22p BCY54 32p BSY79 45p OC77 30p	FCH211 180p   SL403A 187p   TAA811 445p   FCH221 180p   SL702C 147p   TAB101 97p   FCH231 150p   SN7400 23p   TAD100 150p	6K8G 35p ECC40 60p PY88 40p 6L6GT 45p ECC84 30p PY800 50p 6LD20 40p ECC85 60p PY801 50p
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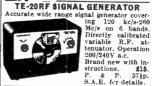
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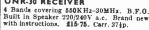
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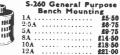
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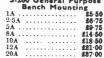
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ACI27	17p AF125	20p BC147	17p BCY71	30p BF316	75p MAT121	17p UT46	27p 2N1304	20p 2N2907 20p 2N2907A	25p 2N3711 30p 2N3819	
ACI28 ACI41K	17p AF126 17p AF127	20p BC148 20p BC149	12p BCY72 17p BCZ11	15p BFW10 20p BFX29	55p MPF102 27p MPF105	43p V405A 43p V410A	450 2NI306	22p 2N2923	13p 2N3820	21
AC142K	17p AF139	33p BC150	17p BD   21	85p BFX84	20p OC19	30p 2G301	19p 2N1307 19p 2N1308	22p 2N2924 27p 2N2925	13p 2N3903	
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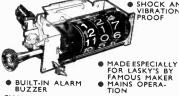
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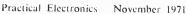
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2N2848	0.42 0.20	BC121	0.20 0.20	C111	0·15 0·65	0AZ203	0.42	SX 645	0.75 0.75
2N2904 2N2904		BC122 BC125	0.68	/YD 611/05	0.05	OAZ207	0.47	V15/30P	0.50
2N2906	0.20	BC126 BC140	0-65 0-55	CRS1/40	0.17	OAZ208 OAZ209 OAZ210 OAZ211	0.32	V15/30P V30/201F V60/201	0.75
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