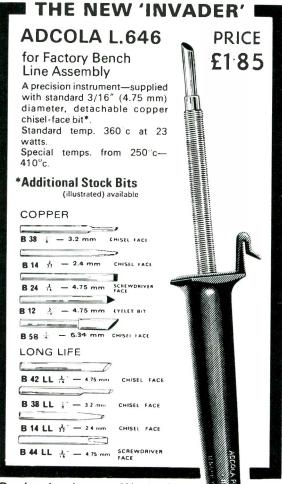
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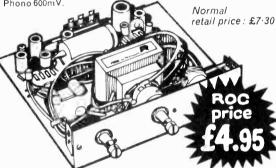
response:70-20,000 Hz 3dB.Output: 4 watts

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Normal retail price: £42:00 ROC price: £29.95

# World wide reception

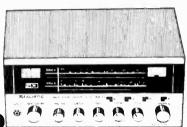
# Professional Solid-state, Four-band Communications Receiver R.135

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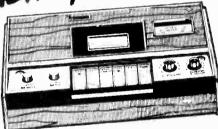
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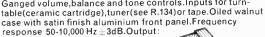
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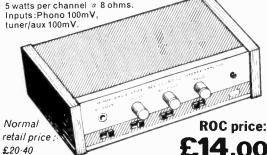
Normal retail price: £9-40





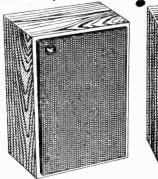
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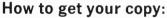
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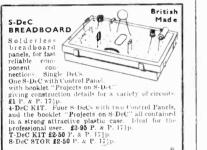


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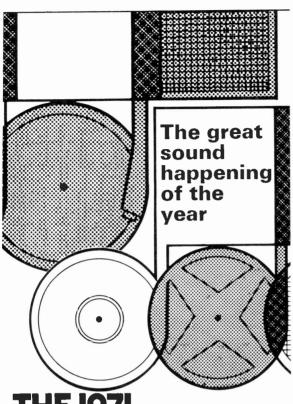
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28.846 479 28.826 179 A1161 359 B1012 850 16278 850 16278 359 100 PIV 2A 60 100 PIV 6A 750 100 PIX 6A 850 28.7712 250 28.826 179 A1161 250 B1012 150 MATIOL 300 OCCOT 755 100 PIV 2A 60 100 PIV 6A 51-10 100 PIX 6A 51-10 PIX 6A 51-10 100 PIX 6A 51-10 100 PIX 6A 51-10 100 PIX 6A 51-10 PIX 6A 51-10 100 PIX 6A 51-10 100 PIX 6A 51-10 100 PIX 6A 51-10 PIX 6A 51-10 100 PIX 6A 51-10 PIX 6A 51-	2N2613 27p 2N4255 42p AD149	47p   BD124 75p   GET896 22p   OC203 40p	ENCAPSULATED 400 PIV 4A 80p	■ 10C2 50p EF39 40p UBF89 35p
28.711 259   28.4286   179   ADID   259   MATIO   259   CC206   909   28.713   270   28.714   259   EVAPOR   179   ADID   259   EVAPOR   259	2N2646 47p 2N4285 17p AD161	35p BD132 85p GET898 22p OC205 75p	50 PIV 2A 55p 100 PIV 6A 75p	
2N2713 279   N24288 15p   AF114   25p   BDY61   125p   MAT120 25p   OCP   2N2714 30p   N24280 15p   AF116   25p   BDY61   125p   MJ400 107p   ORF60 40p   2N2904 20p   N24290 15p   AF116   25p   BDY61   25p   MJ400 107p   ORF60 40p   2N2905 25p   N24290 15p   AF118   44p   BF162   25p   MJ400 112p   P346A   2N2905 25p   N24290 15p   AF118   44p   BF162   25p   MJ400 107p   ORF60 40p   2N2906 20p   N24303 47p   AF124   22p   BF168   25p   MJ400 107p   N1480   2N2906 20p   N24303 47p   AF124   22p   BF168   25p   MJ400 107p   N1480   2N2907 23p   N2466   15p   AF126   10p   BF169   57p   MJ480   97p   T1843   2N2907 23p   N2466   15p   AF126   15p   BF169   57p   MJ480   07p   T1843   2N2907 23p   N2466   15p   AF126   15p   BF169   35p   MJ481   15p   2N2924 15p   N36028   57p   AF130   25p   MJ400   10p   12p   25p   2N2924 15p   N36028   57p   AF130   25p   MJ400   10p   12p   25p   2N2926 12p   N36028   57p   AF130   25p   MJ400   10p   12p   25p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   87p   T1845   12p   2N2926 12p   N36028   47p   AF170   45p   BF167   30p   MJ420   47p   2N2926 12p   N36028   47p   AF170   47p   MJ420   2N2926 12p   N36028   47p   AF170   47	2N2711 25p 2N4286 17p AD152 2N2712 25p 2N4287 17p AF109	35p BDY10 125p MAT100 25p OC206 90p 45p BDY20 105p MAT101 30p OC207 75p	200 PIV 2A 67p 400 PIV 6A £1:10	10P14 21·10 EF42 70p UCF80 55p
2N3904 20p   2N4290 15p   AP118   25p   BF157   25p   MJ400 17p   ORP60   40p   2N2905   25p   2N4292   15p   AP118   44p   BF152   25p   MJ430   12p   PJ46A   22p   2N303   2N394   17p   AP121   30p   BF154   35p   MJ430   12p   PJ46A   22p   2N303   2N394   15p   AP124   12p   AP130   12p   PJ46A   22p   AP130	2N2713 27p 2N4288 15p AF114 2N2714 30p 2N4289 15p AF115	25p BDY61 125p MAT120 25p OCP71 42p 25p BDY62 100p MAT121 30p ORP12 50p		12AT7 30p EF85 35p UCH42 70p 12AU7 30p EF86 30p UCH81 35p
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2Ny 2007 23p   2Ny 905   38p   AF126   18p   BF163   38p   M1481   12p   T1844   42p   2Ny 2015   52p   AF137   52p   AF138   52p   BF177   38p   M1481   137p   T1845   12p   4004 400P1V   10p   12p   25p   4004   400P1V   10p   12p   25p   4004   400P1V   10p   12p   25p   4004   400P1V   10p   12p   25p   4004   400P1V   10p   12p   25p   4004   400P1V   40p   4	2N2906 20m 2N4303 47m AF124	22p BF158 28p MJ440 95p ST141 20p	4001 50PIV 08p 10p 19p	12BH7 40m EF184 35m UF85 40m
28	2N2907 23p 2N4965 18p AF126	16p BF163 35p MJ481 125p T1843 40p	4003 200PIV 10p 12p 22p	20D1 45p EL34 50p UL41 65p
2N92966   2p   2N0303   42p   AP179   45p   BP177   30p   MLE371   87p   T1848   12p   20p   20p	2N2924 15p 2N5028 57p AF139	28p BF170 33p MJ491 137p T1845 12p	4005 600PIV 12p 15p 26p	20L1 \$1:10 EL41 55p UY41 45p
2N3929G 12p   2N31r2   12p   AF180   30p   BF178   30p   BF178   30p   BF178   30p   BF178   30p   BF180   30p   BF178   30p   BF180   30p   B	2N2926G 19h 2N5030 42h AF179	45p BF177 30p MJE370 95p T1847 12p	4006 800 PIV 15p 17p 27p 4007 1000 PIV 20p 20p 30p	20P3 60p EL81 55p VR 105/30 38p
283011   249   280175   529   AF186   459   AF186   359   BF180   359   BF180   359   BF180   359   AF186   459   AF186   359   AF186   459   AF186   359   AF186   459   AF186   359   AF186   359   AF186   459   AF186   359   AF186   AF18	2N2926Y 12p 2N5174 52p AF181	40p BF179 30p MJE520 87p T1849 12p	50+less 15% 100+ less 20%	
28303 249 2802328 369 A F273 97 B F182 309 MF103 359 T1852 129 100PIV 28 359 509 58 22 122 1834 309 AF71 871 871 871 871 871 871 871 871 871 8	2N3011 24p 2N5175 52p AF186 2N3014 25p 2N5176 45p AF239	39p BF180 35p MJE521 87p T1850 17p 30p BF181 35p MPF102 42p T1851 12p	STUD MOUNTING	25L6 45p EL91 32p for postage
283133 25p 28324 67p 88426 25p BF198 15p 88368 38p 28313 25p 28324 67p 88426 25p BF198 15p 88426 27p 88426 25p 88426 25p 88426 25p 88426 27p 88426 25p 88426	2N3053 24p 2N5232A 30p AF279 2N3054 49p 2N5245 45p AF280	47p BF182 30p MPF103 35p T1852 12p	100PIV — 45p 50p #1·22	
283134 305   28305   2	2N3055 72p 2N5246 42p AFZ11	32p BF185 20p MPF105 37p XB112 11p	200PIV 25p 50p 55p 21 42 400PIV 30p 55p 62p 21 77	1N194 7p BAX13 12p OA5 17p
28136 25p 28366 40p 18720 27p 8F197 15p NRT128 27p ZTX100 17p 283891 25p 28360 37p A8750 25p BF198 42p NRT128 27p ZTX300 17p 283891 20p 283891	2N3134 20n 2N5265 225n A8V27	31p BF195 15p NKT124 42p ZTX107 14p	600PIV 32p 60p 72p 42·12	AA119 7p BAY31 7p OA10 22p
283391 205 283396 379 A8V51 328 BP200 355 NRT135 275 ZTX301 179 ZN3301 309 ZN3309 899 A8V54 255 BP224 290 NRT135 329 ZTX302 189 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 289 A8V54 250 BP225 200 NRT210 309 ZTX303 189 ZN3309 189 ZN3309 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 189 ZN3309 ZTX300 189 ZN3309	2N3136 200 2N3306 400 ASY29	27p BF197 15p NKT126 27p ZTX109 17p	1000PIV 40p 85p £1.05 £2.77	AAZ13 10p BY100 15p OA47 7p
2N3391 A 30p   2N3309	2N3391 20p 2N5308 37p ASY51	32p   BF200 35p   NKT135 27p   ZTX301 17p	ZENER DIODES	BA100 15p BY122 87p OA73 10p
2N3393   15p   2N3354   27p   A8Y86   32p   BF237   22p   NKT211   30p   ZTX304   25p   25	2N3392 17p 2N5310 42p A8Y67	45p BF225 20p NKT210 30p ZTX303 18p	400MW   1.5 WATT   10 WATT	BA102 22p BY124 15p OA79 9p BA110 32p BY126 15p OA81 7p
283   285   287	2N3393 15p 2N5354 27p A8Y86 2N3394 15p 2N5355 27p A8Z21	32p BF237 22p NKT211 30p ZTX304 25p 37p BF238 22p NKT212 30p ZTX500 16p	15p each 20p each 25p each	BA111 27p BY127 17p OA85 7p BA112 70p BY164 57p OA90 7p
283404 28p   2N3366 38p   BC108 10p   BFW87 25p   NKT215 22p   ZTX503 17p   25 + 15%; 100+20% any one type   Post-BA142 38p   BYZ12 30p   OA200 7p   2N3414 22p   2N3463   32p   BC113   15p   BFW89 20p   NKT215 47p   ZTX504 40p   age on all Semi-Conductors 7p extra.   BA142 12p   BYZ13 25p   BYZ13 25p   A202 10p   BYZ16 20p   BYZ	2N3402 22p 2N5356 32p AUY10 2N3403 22p 2N5365 47p BC107	150p BF244	TRANSISTOR DISCOUNTS: 12 + 10%;	BA115 7p BY210 35p OA91 7p BA141 32p BYZ11 32p OA95 7p
2N3414 22p: 2N5457 34p   BC113 15p   BFW89 20p   NKT217 40p   ZTX331 28p 8.A.E. FOR FULL LISTS. BA145 20p   BYZ16 40p   OA210 17p	2N3404 32p 2N5366 32p BC108	10p BFW87 25p NKT215 22p ZTX503 17p 10p BFW88 23p NKT216 37p ZTX504 40p	25 + 15%; 100+20% any one type Post-	BA142 32p   BYZ12 30p   OA200 7p
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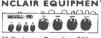
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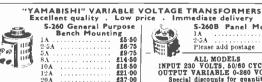
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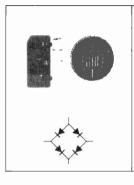
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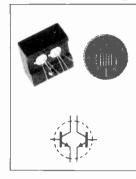
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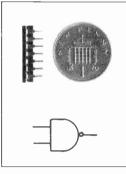
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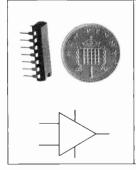
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# FET's

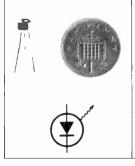
NKT markets a range of N-channel, junction-gate f.e.t.s. (field effect transistors) covering dc, a.f., r.f. and switching applications. The NKT 80420 series are in four-lead T072 metal cans and the PN 3819 in plastic T018 style. Special selections of  $V_{\rm P}$  and  $I_{\rm DSS}$  can be provided.

Send for Information Bulletin VF



# LINEAR IC'S

NKT has an expanding range of industrial linear I.C.'s, such as the LIC 709C (=uA709C), LIC 723C (=uA723C), and LIC 741C (-uA741C). Packages are normally 14-lead dual-in-line (indicated by "/14") after type number, but T05 ("/5") and 8-lead dual-in-line ("/8") are available. Send for Information Bulletin VA

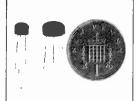


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# non-transistors from Newmarket Transistors





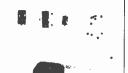
# **PLASTIC TRANSISTORS**

A wide range of plastic transistors with code numbers identifiable with the related metal-can industrial types e.g. PN70/71/72 (=BCY 70/71/72) PN 107/8/9 (=BC 107/8/9), PN 918 (=2N 918), PN 1613/1711 (=2N 1613/1711), PN 2904-7 (= 2N 2904-7), PN 3054 (3A NPN "tab" power). Send for Information Bulletin VP



# RECTIFIERS

Small flying lead rectifiers with ½ and 1A current ratings at voltages from 100 to 1000V in industry standard package. Apart from such standards as the 1N4001-4007 series, NKT provides special selections on characteristics such as leakage or forward voltage drop. Send for Information Bulletin VR





# MICRO DEVICES

As manufacturers of thick film hybrid circuits, NKT specialises in the supply of microminiature semi-conductor active devices for attachment to film circuits—the range includes unencapsulated chips, leadless inverted devices (LID's), microtab and flexible lead types. Send for Information Bulletin VS



# **THYRISTORS**

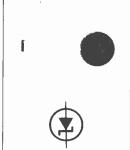
NKT specialises in the area of low current (up to 1A) thyristors in industrial metal can and economical plastic packages. The range stretches from the plastic NTS 311 (30V, 0.6A) to the T05 metal can NTS 1500 (500V, 1A) via the T018 NTS 0660 (60V, 0.6A). Send for Information Bulletin VT



# UNIJUNCTIONS

In unijunctions, NKT has available the well tried industry-standard metal-can 2N 2646/7 and 2N 1671B, as well as economical plastic devices for less onerous applications where cost is the overriding factor.

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# ZENER DIODES

Completing the array of standard non-transistor devices, NKT provides a useful range of zener diodes. As well as the industry standard 400mW "work horse" (BZY 88/3.3-30V), the range features an economical 1W zener range, the NKT 10C-V-(11-30V). Send for Information Bulletin VZ

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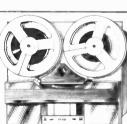
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BP93 = 7493	4-bit binary counters	0.67	0.64	0.58
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BP193 = 74193	Sync. binary up-down counter (tow	2.10	1.90	1.70
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$UIC20 = 12 \times 7420N$	$50p UIC74 = 8 \times 7474N$	50p UIC94 = 5 x 7494N 50p
$UIC40 = 12 \times 7440N$	$50p$ UIC75 = $8 \times 7475$ N	$50p \text{ UIC95} = 5 \times 7495 \text{N } 50p$
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BP935	Expandable Hex Inverter		13p	12p	11p
BP936	Hex Inverter		13p	12p	11p
BP944	Dual 4-input NAND expandable buffer				
	pull-up		13p	12p	11p
BP945	Master-slave JK or RS		25p	24p	220
BP946	Quad, 2-input NAND		12p	11p	10p
BP948	Master-slave JK or R8		25p	24p	22p
BP951	Monostable		65p	60p	55p
BP962	Triple 3-input NAND.		12p	11p	10p
BP9093	Dual Master-slave JK with separate clo		40p	38p	35p
BP9094	Dual Master-slave JK with separate clo		40p	38p	35p
BP9097	Dual Master-slave JK with Common Cl		40p	38p	35p
BP9099	Dual Master-slave JK Common Clock	IOCK	40p	38p	35p
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BP 701C-SL70IC	TO-5	8	OP Amp	63p	50p	45p
BP 702C-8L702C	TO-5	8	OP Amp Direct OP	63p	50p	45p
BP 702-72702	D.I.L.	14	G.P. OP Amp (Wide			
			Band)	53p	45p	40p
BP 709 -72709	D.I.L.	14	High OP Amp	53p	45p	40p
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BP 711-4A711	TO-5	10	Dual comparator	58p	50p	45p
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VOL. 7 No. 10 October 1971

# ELECTRONICS

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# **NON-PERMISSIVE**

Even in this permissive age editors have certain censorial duties to perform in the interests of their readers. One of these is to apply the blue pencil and expunge from the printed page any words having dubious meanings or likely to encourage the adoption of undesirable practices.

In respect of the latter hazard, this magazine has a particularly onerous responsibility; in matters appertaining to circuit design and construction, we mean. It follows that we should have our little list of disfavoured words and expressions; although some of them may be frequently used in the vernacular without so

much as an eyebrow being raised.

Yet, as we have implied, there are lines to be drawn, and altogether in our readers' own interest. Not to keep anyone in suspense any longer, let us reveal one of these disfavoured terms. It is "junk box". As alert readers will have already surmised, it is our normal policy to remove any reference to this peculiar, though fascinating, source of supply from contributors' manuscripts before they are presented to the public eye.

We recognise the partiality of many amateur

We recognise the partiality of many amateur designers for a dip into this traditional repository for temporarily abandoned components. But the advantages the junk box offers are strictly personal and local. The contents of some boxes would defy identification, let alone duplication, anywhere. That's for sure.

Obviously we cannot allow component oddities procured in this way to remain in the specification of any project offered to constructors at large. A suitable substitute, currently available, has to be found, and the design modified where necessary. (All would-be

contributors kindly note.)

Checking with our little list again, there is the somewhat allied expression "cannibalisation". This goes hand in glove with those deliberate wrecking operations know variously as "breaking up" (or "down") and "stripping down". The fruits of these labours often go to swell the contents of the junk box and to make the collection even more varied and mysterious.

Not that we are opposed to the junk box as such. Every constructor will accumulate one in the fullness of time. Actually there's nothing you can do about it; it just grows, and grows. And what strange practices are perpetrated in private workshops is not our business. But the supply of designs for other constructors to execute is.

So have no fear about our "censorship". We wield our blue pencil solely in the cause of good, sound design, and this is in the best interests of all who construct. THIS MONTH

# CONSTRUCTIONAL PROJECTS

ENGINE TEMPERATURE	
CONTROLLER	798
WAR GAMES COMPUTER	810
RAIN AND WATER LEVEL	
ALARM	820
SERVO CHART RECORDER	822

# SPECIAL SERIES

RADIO ASTRONOMY
TECHNIQUES—5 830

# GENERAL FEATURES

ELECTRONIC MUSIC	
SYNTHESIS	802
INGENUITY UNLIMITED	843

# **NEWS AND COMMENT**

EDITORIAL	797
SPACEWATCH	819
MARKET PLACE	840
READOUT	847

Our November issue will be published on Friday, October 15

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# Thermostatically controlled fan for your car

Most internal combustion engines in cars are overcooled, the manufacturers having to take into account all types of driving conditions that might be encountered. For the majority of the time, engines tend to run on the cool side, and the belt-driven fan on the water pump boss can be removed but, of course, it is inconvenient to do so en route.

With the mechanical fan removed permanently some auxiliary form of controlled cooling is necessary for those occasions when the forward motion of the vehicle does not force enough air through the radiator, for example, in traffic jams or when climbing a steep hill.

There are on the market various devices to increase the air flow; some fans "feather" according to temperature and/or engine speed. The one disadvantage these have is that they tend to be somewhat on the expensive side and are still wasteful of engine power. The controlled electric fan to be described, on the other hand, is inexpensive, only operates according to engine temperature, and takes no power from the engine.

# **AUXILIARY FANS**

The two fans in use on the author's vehicle were mounted on a metal plate in front of the radiator and behind the radiator grill, so that they draw air through the grill and push it through the radiator. Initially, they were wired up to a pair of relay contacts controlled by a switch on the dashboard—in the final version this became the manual override to an electronic switch. See Fig. 1. The fans must obviously be mounted the right way round to force air through the radiator, or to suck it out through the radiator in the case of transverse engine cars.

The circuit is basically very similar in either polarity version. Fig. 2 shows the negative earth version. For positive earth operation, all that is needed is to change the transistors from *pnp* types to equivalent *npn* and reverse C2.

# LONG-TAILED PAIR

The control circuit is a "long-tailed pair", the base of TR3 being fixed while the emitter determines how the temperature sensor (thermistor TH1) is

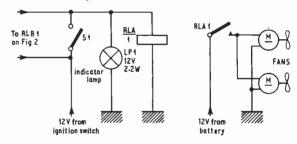


Fig. 1. The two auxiliary fans controlled by a 12V relay (RLA), switched on by RLB or S1. LPI provides visual indication of motor operation and should be fitted to the dash panel

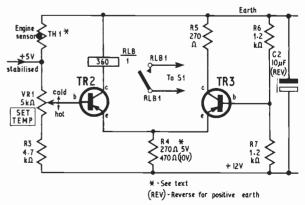
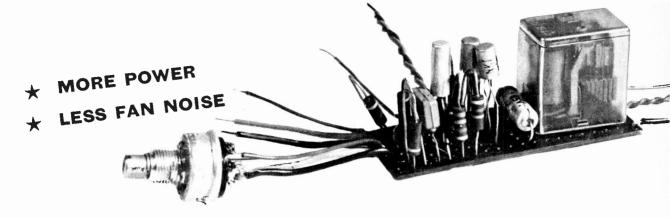


Fig. 2. Negative earth version of the electronic control circuit. For positive earth cars, change the transistors and reverse the connections of C2



# ★ BETTER HEATER EFFICIENCY ★ QUICKER WARM UP

# **COMPONENTS...**

# Resistors

RI Ik $\Omega$  (560 $\Omega$  for IOV system) R5 270 $\Omega$  R2 220 $\Omega$  R6 1-2k $\Omega$ 

R3  $4.7k\Omega$  R7  $1.2k\Omega$ 

R4  $270\Omega$  (470 $\Omega$  for 10V system) All  $\frac{1}{4}$ W  $\pm$  10% carbon

# **Potentiometer**

VRI 5kΩ carbon linear

# Capacitors

CI 0·IμF 600V C2 10μF elect. 25V

# **Transistors**

POSITIVE NEGATIVE EARTH
TRI OC35 or OC22 2N3055 or BD124
TR2 AC127 or NKT713 AC128 or OC81
TR3 AC127 or NKT713 AC128 or OC81

# Zener Diode

DI Approximately 6.3V 250mW selected from tests (see text)

# Relays

RLA 12V with single pole normally open heavy duty contacts (see text)

RLB 6V approximately 350 ohms with single pole normally open contacts (see text)

# Miscellaneous

LPI 12V 2·2W indicator lamp and holder SI Single pole on/off toggle switch Veroboard 0·15 inch matrix  $3in \times l\frac{1}{8}in$  Fan (see text) Diecast box  $4\frac{1}{4}in \times 2\frac{1}{2}in \times lin$  Sheet steel for fan mounting  $\frac{1}{16}in$  painted or p.v.c. coated

Metal brackets (see text) Clips to hold fan motors Grommets, wire and bolts

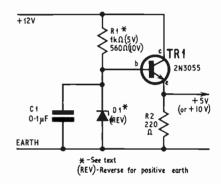


Fig. 3. Circuit of the stabilised 5V supply for cars with 12V negative earth. For positive earth, change TRI and reverse DI

going to operate relay RLB via TR2. The thermistor is the variable element, whose resistance changes inversely with temperature. It is usually fitted into the engine block and wired up to the temperature gauge on the dashboard.

The relay RLB in the collector circuit is a small one, capable of switching a heavy duty relay to turn on the cooling fans. The relay contacts RLB1 are wired across the manual override switch S1 in Fig. 1.

In the prototype there were two changeover contacts, and two make contacts. To reduce the mechanical load of all these contacts on the relay armature, the two changeover contacts were removed. This way the relay would operate at around 4V.

## STABILISED LINE

It was originally intended that the stabilised 5V line was derived from the car's instrument circuit. But on investigation the stabilised 5V was found to be a pulsed 12V, the average value of which was 5V. Hence a stabiliser (Fig. 3) was constructed to replace the original unit. For positive earth the stabiliser transistor is changed and the polarity of D1 reversed.

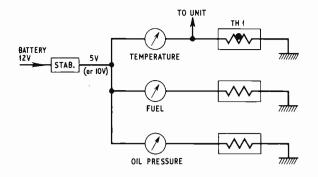


Fig. 4. Connection of the electronic stabiliser (Fig. 3) into the car instrument system (5V or 10V positive or negative earth). Also shown is the connection for the controller unit.

This system can be used for 5V (Ford) or 10V (BLMC and others) instrument systems, by alteration of R4 (Fig. 2) and R1 (Fig. 3). The power transistor TR1 has been chosen to be able to supply the current for up to three gauges as shown in Fig. 4.

If an electric temperature gauge is not fitted, or the instruments are not stabilised but fed directly from the 12V line then it is possible to construct the unit using a temperature gauge thermistor screwed into the block or a VA 1026 thermistor mounted, by epoxy resin, to the outside of the radiator just above the core and near the top hose. This thermistor then becomes THI in the circuit and the stabiliser output is connected directly to the junction of THI and VRI. The VA 1026 thermistor must not be placed in water for calibration purposes unless it has been covered in epoxy resin.

it has been covered in epoxy resin.

The power transistor (TR1 in Fig. 3) is required, in the worst case of full fuel tank, boiling engine, and high oil pressure, to carry approximately 0.75 A. So the maximum dissipation could be 0.75(14-5) watts, which is approximately 7 watts.

# SUPPRESSION

Due to the tasks expected of a car electrical system, the occurrence of high voltage "spikes" from the ignition and charging circuit are bound to effect the supply to the controller and the Zener diode and transistors must be protected from such "spikes". The  $10\mu F$  capacitor C2 across the supply line suppresses voltage spikes so preventing damage to the semiconductors. Which way round it is connected depends on the earth polarity as mentioned earlier. A  $0.1\mu F$  capacitor C1 is likewise connected across the Zener diode.

# **THERMISTOR**

If the resistance of the thermistor is not known at extreme temperatures it can be found by adopting the following course. Release the pressure of the coolant by slowly unscrewing the radiator cap and then replace the cap. Remove the sensor unit from the engine block, and plug the hole with a cork, or rag. Place the sensor in a pan of warm water and heat it up gently to boiling point. Leave the water boiling for a few minutes to allow the sensor to reach the same temperature.

Now measure the resistance of the sensor (in the prototype this was 22 ohms) and the temperature of

the water, which will be around 212 degrees F (or 100 degrees C). The sensor is now replaced in the block and allowed to cool. It is quite a good idea to leave it out until the following day. The reasoning behind this is that when cold, the sensor has a resistance of approximately 450 ohms, and to give the temperature gauge the impression of a hot engine, all that is needed is to bridge the sensor with a 22 ohm resistor.

If this is done, and the temperature gauge observed, the Zener diode voltage can be chosen to give the required voltage from the stabiliser and the appropriate water temperature reference on the meter scale. In the prototype, a 6.3V Zener was used, but different cars may require different types. Some experimentation might be necessary.

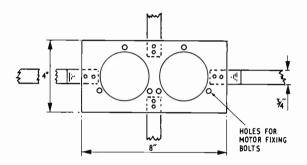


Fig. 5. The fans are mounted on a protected steel plate

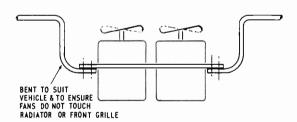


Fig. 6. Side view of the fan plate showing brackets

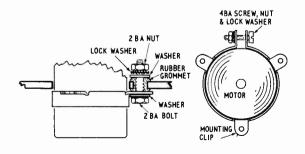


Fig. 7. Detail of mounting the motor with vibration absorbers

# **RELAYS**

For TR1, any appropriate polarity transistor would do, provided that (a) it can carry at least 600mA collector current (that is for cars with two gauges). For vehicles with an electric oil pressure gauge as well as fuel and temperature gauges, 1A collector current should be allowed. (b) it can dissipate 10 watts or more (assuming the worst case).

The main relay RLA that switches the fans on is driven from the 12V supply. It can be a common car 12 V relay as used elsewhere in car wiring, or any other 12V relay provided that the contacts are heavy duty types and are rated at 5A continuous at 12V. Do not wire this relay directly into the transistor circuit in place of RLB or transistor damage may result.

# **FANS**

The fans suitable for this particular application can be obtained from surplus equipment suppliers. They would be 12V 1.5A motors with 3inch or 5inch radius fan blades to fit on the shaft. Alternatively, an old car heater motor can be obtained from a breaker's yard. The centrifugal type is the most powerful.

A 5inch blade was tried on one fan, but it did not give as much air flow as the 3inch due to the motor running a lot slower, trying to push a greater volume of air. Also, the current rose to something in the order of 2.5A. Consequently, two 3inch fans were used in order to get a reasonable airflow through the radiator. These motors were circular with multibladed fans, the motor body diameter was 2½inches and the overall depth was 3inches excluding the fan blades.

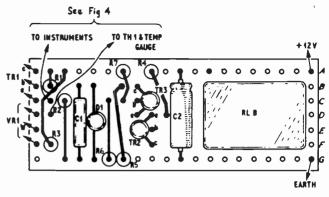
They were mounted on a piece of reinch steel sheet approximately 8 inches by 4 inches (Fig. 5). Two holes were cut to take the motors and the sheet painted and attached to the car with brackets. (Sheet steel already coated with p.v.c. is excellent for this job and does not need painting.) These brackets will differ in length, and how they are bent, depending on the vehicle to which they are fitted (Fig. 6).

The fans were attached to the plate with circular metal straps or clips fitted to the steel sheet. Rubber mountings are recommended to absorb vibrations. See Fig. 7 for details. It will be noted that the fans can slide in their mounting. This helps a great deal in positioning them clear of the radiator. Further details on fitting electric fans can be found in the July and August 1971 issues of *Practical Motorist*.

# **COMPONENT BOX**

The electronic circuit is built into a diecast box of approximate dimensions  $4\frac{1}{4}$  in  $\times$   $2\frac{1}{4}$  in  $\times$  1 in. This box can be bolted to the underside of the dashboard housing or in a glove compartment.

Although the box is robust it is not a good idea to mount it where damp and heat can get at it (such as under the bonnet) unless suitable protection is given to it. In these circumstances the box should be well painted and the joint of the lid waterproofed. A matt black finish is ideal, since this will aid any heat dissipation from TR1. Silicon grease smeared on both sides of the mica washer of TR1 will also protect from damp as well as assisting with insulation and heat transference. Similar treatment can be given to the cable entry hole when finished.



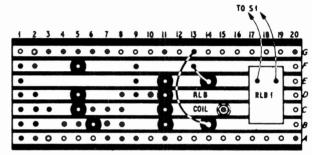


Fig. 8a. Layout of components on Veroboard

Fig. 8b. Underside view of board showing the cut out for the relay and cuts in the copper strips

The circuit board is shown in Fig. 8. Most of the components are mounted on this board, the exceptions being the thermistor TH1, transistor TR1, VR1 and RLA. The copper strips on the underside need to be cut as shown in Fig. 8b.

The components board was mounted on spacers and fitted to the box with screws, leaving sufficient space to mount the power transistor TR1 on the lid beside the potentiometer VR1. A mica washer must be fitted between the lid and TR1 to ensure insulation, as the case of TR1 will be connected to the collector. A smear of silicon grease is recommended on both sides of the washer. Nylon fixing screws or insulation bushes must also be used. A soldering tag should be fitted under the head of one of these screws to facilitate connection to the collector.

# WIRING AND SETTING UP

When finished, the board, potentiometer and transistor TR1 are all mounted in the box and connected up. The wiring to RLA, the manual override switch S1 and indicator lamp LP1 is carried out as in Fig. 1. The feed labelled on the diagram as "12V from battery" can conveniently be taken from the starter solenoid, one ammeter terminal, or the fusebox, whichever seems to be the most convenient point.

Potentiometer VR1 can now be adjusted so that the fans just come on and finally, the resistor across TH1 removed and the thermistor replaced in the engine. A few trial runs in the car will soon show any alterations necessary in the setting of VR1. Keep a watchful eye on the temperature gauge and indicator lamp during these trial runs and try leaving the car ticking over for 10 minutes when it is hot.



# A survey of the development of electronic synthesisers which provide new dimensions in tonal colouration

MUSIC is basically dependent on three factors only; pitch or frequency; loudness or intensity; and duration or time. However, other attributes are required to complete a satisfying musical sound. Firstly we must distinguish between music and noise.

Noise is a transient system having a high degree of randomness and usually consists of groups of frequencies unrelated as to pitch and power. As these transients increase in periodicity and become more symmetrical, the elements of a tone are formed. If the shape of the waveform assumes a regular character and lies within prescribed loudness and frequency limits, we have a sound which we call musical.

# THE TONE DEFINED

But to establish pitch alone creates no interest; the sound must have character. It obtains this from two important attributes, the harmonic content and the shape of the wave envelope. Other desirable components appear in complex sounds, so to form a complete musical tone we require:

- I. A pitch or frequency,
- 2. A rate at which the sound starts,
- 3. A length of time for which it persists,
- 4. A rate at which it decays,
- 5. A loudness level, not necessarily fixed,
- 6. Harmonics or partials,
- 7. Probably noise due to the mechanics of producing the sound,
- 8. Possibly vibrato or other modulation.

If any of these components is removed, the sound will be unreal, although it may be agreeable. For example, a flute or diapason-like sound on an electronic organ will probably have no "wind" noise but it can be very pleasant. However, take the corresponding organ pipe and blow it, and the synthesis is at once apparent. All of these things we, as listeners, take for granted, because we have always been brought up with them. But consider the composer for a moment.

He is in a unique position, for he requires the mental ability to create melody, harmony and rhythm (to somewhat simplify matters); yet he must thoroughly understand the capabilities of the instruments on which this music will be performed. So the music is in the end dependent on two factors; the composition, and the means to interpret that composition.

# INSTRUMENT LIMITATIONS

Now instruments of the orchestra have not changed for many years. If we look at these, two things are at once apparent; some have fixed wind valves, like the oboe, clarinet, saxophone, etc; some have fixed keys, like the organ, piano, celeste, etc. But some have infinite gradations of frequency, like the string family (violin, viola, 'cello, base viol) and the slide trombone. These differences in construction mean that the composer of Western music is tied to the semitone scale, because this is the smallest frequency interval between successive notes which is possible with keyed instruments.

Further, consider the pitch and power range. Few orchestral instruments cover more than three octaves. Extensions up or down require additional instruments, for instance, the bassoon has to be extended downwards by the contra bassoon; the flute upwards by the piccolo. The whole range of notes required cannot be incorporated in one instrument. It is just the same with the violin, viola, etc.

As to power, well this is extremely limited for all instruments; even the trombone will only deliver just over half a watt of acoustic power. So, for more power we need more instruments. All these foregoing factors are limitations on the composer.

It is true that we have rubbed along for several hundred years with the existing conditions, but this is not to say that composers were satisfied. Far from it, nearly 70 years ago Busoni attempted to introduce another musical form, followed by Webern and others.

In those days when communications were limited and there was no general dissemination of concerts,

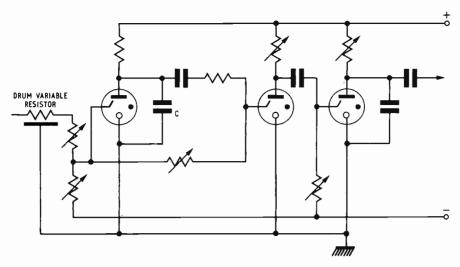


Fig. I(a). Circuit of Trautonium with frequency divider; (b) the manual drum resistor is in a flexible form, so proportioned that the frequency of oscillation is proportional to the strip in use. Playing the "keyboard" consists of pressing the tubular cover enclosing the resistance contact strip at the point required to produce the correct pitch note

convention outlawed such revolutionary ideas. And of course at that time, all sound patterns had to be produced acoustically, there being no transducers, amplifiers or loudspeakers. Such limitations defeat the boldest spirits,

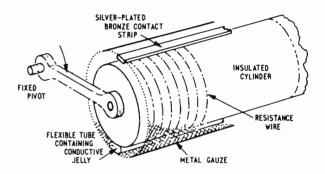
# CHANGES AND THE FIRST SYNTHESISER

Most musical performances in those days were sponsored by a patron, who usually financed the composer. As times changed, especially with the introduction of gramophone records and broadcasting, the role of the patron diminished and the financial arrangements altered. Clearly this produced an atmosphere which discouraged serious composition, for the decline in status of the composer increased as the public tastes changed owing to the ease of communication. But, as always, there comes a time when old threads are picked up again in a new guise, this time by organisations instead of individuals.

The use of the valve had become commonplace after the 1914 war, but stability was unheard of and it was not until gas tubes became highly developed in Germany that successful synthetic musical instruments were produced; for it became clear that electrical methods would have to be used to overcome the limitations of all existing physical instruments.

# THE TRAUTONIUM

Professor Friederich Trautwein designed the first, and still one of the most useful, synthesising devices, the Trautonium, in 1928. With this two keyboard instrument, instead of the conventional 12 notes to the octave, it is possible to obtain 1,200! Strangely enough, the Trautonium was for some years regarded as a device for examining the tonal spectrum of existing instruments, and for use as a solo instrument with orchestra—as Oskar Sala uses it. Its powers as a composing device were not really recognised until the North West German broadcasting authority set up a school of electronic music research into musical tone, form and composition.



By this time, tape recorders were readily available, as were good quality microphones and reverberation systems. It was the tape recorder which set the seal on the ability to construct music from the basic parameters mentioned, and without which electronic music is not possible, unless it be very elementary in form.

The circuit of the Trautonium is shown in Fig. 1a as an early example of voltage control, so often hailed as a new development. But in fact, voltage to frequency converters, variable gain circuits, vibrato and envelope shaping circuits all depending on voltage control are very old. Note the ingenious way of getting small increments of grid bias control by means of a variable resistance drum, Fig. 1b.

Dummy rubber keys were in fact mounted over the top "keyboard" to give an approximate indication of note positions.

This important instrument was extensively used all over Germany until the coming of the semiconductor. Of course, Helmholtz, Hermann Smith, Dayton Miller and especially Maurice Martenot had devised synthesisers, some purely mechanical, before this.

# MACHINE COMPOSITION ADVANTAGES

But now we must revert to more recent problems, and there are several; but most have the composer,

rather than the performer, in mind, although all composing machines can play back the composition.

In the past, a composer could put pen to paper and draft a piece of music for, say, ten players. But how could he make sure he was getting the best intended effect without employing ten musicians to play his score? This is both costly and inconvenient, and calls for a suitable acoustic environment. How much better if he could convey the musical information to a device which could play it for him. He could then listen to it in private and make any corrections thought desirable.

This was the idea behind the RCA and Oramic sound systems. Both of these enable a musician to prepare the "score" with his own hands and play it at once—no matter how long it is. The information imparted to the system can be called back and replayed again and again, and alterations made. This can only be done for very short periods of time with synthesisers of the Moog or EMS types unless they incorporate a computer and even then, the playing time per realisation is quite short—perhaps 30seconds.

## THE RCA SYNTHESISER

Let us then have a quick look at the RCA machine. This is a complete studio, and not intended to be portable, a typical installation being in a college of music or a university. No matter what the system, it must be capable of providing the eight basic parameters mentioned earlier, as a minimum. Of course, there may be extensions and there is great flexibility for each of these.

The apparatus is contained in ten standard racks, each 6ft high, see Fig. 2. It comprises a range of tuning fork oscillators, frequency multipliers and dividers, means for producing any overtone or harmonic structure, duration or decay characteristic, vibrato and "glide" circuits, loudness or level controls, relay trees for operating the foregoing from the information source, and other devices to produce deviations from the above for special effects.

All the above circuitry is duplicated so that two simultaneous channels are available. The whole of this is controlled from the keyboard perforator.

# PERFORATED ROLLS

Most readers remember the perforated paper roll used in player pianos. The information required to operate the correct notes took the form of perforations in the paper. As this was unwound from its reel by a motor, the roll passed over a perforated metal bar—there being as many apertures as there were notes on the piano.

A vacuum was created in a bellows system, and when a perforation in the roll coincided with an aperture in the tracker bar, as the perforated rod was called, air would be sucked in to the appropriate hole and this energised a small pneumatic device which actuated the correct hammer.

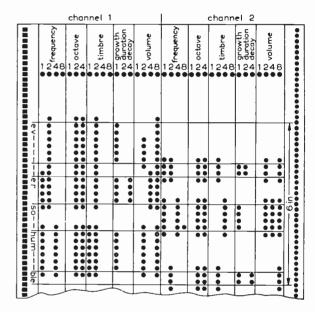


Fig. 3. Part of RCA punched roll

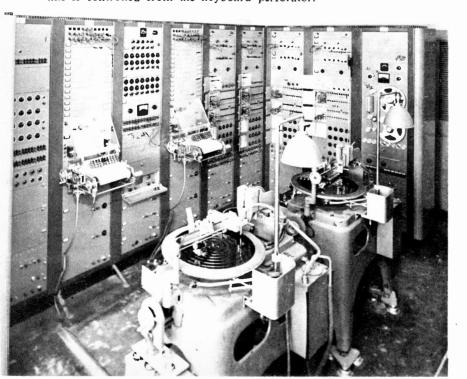


Fig. 2. RCA Synthesiser at Columbia University

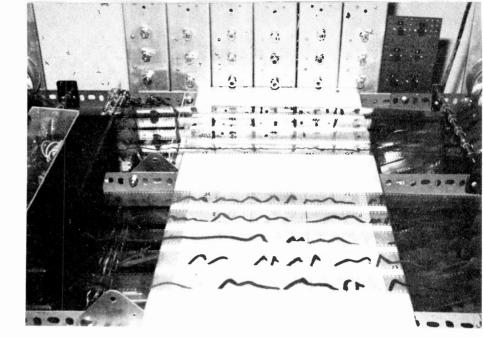


Fig. 4. Digital and analogue information on film for the Oramic Sound System

To produce a sustained note, a slot was cut in the roll, thus the hammer did not return until the end of the slot arrived, and the damper was so kept off the strings.

The same idea is used by RCA to convey the information, but as the paper roll is wider, slots make it liable to stretch and therefore a series of closely spaced holes is used for a sustained note. The little microswitches which "feel" a hole are so arranged that they will not close again if two holes immediately follow one another; in this way, sustained notes are possible.

An alternative method is to paint dots or bars for the duration of the required parameter, and then scan them photoelectrically. By this means excessive perforations in the paper are avoided. An example of the prepared roll is given in Fig. 3.

# **DISC AND TAPE LINKS**

The two perforators are mechanically linked to either disc or tape recorders, so that after the completion of a composition, the substance can be recorded and either played back or stored.

Although only two channels are provided, rerecording is resorted to, and with modern materials quite elaborate compositions can be realised and performed. But one of the prime objects is to help the composer; he can come along with a theme, punch out the parts with quite arbitrary tone colours, listen to his harmonies at once, and correct anything which he does not like. Armed with the final information, he can write out the score in completed form—and all without employing a single live musician!

It is often thought that gliding tones, percussion sounds, "wah-wah", etc. are recent ideas. This is not at all true; all of these effects have been known and used for over 40 years; it is just that until the coming of the semiconductor, the apparatus to produce the effects was too bulky to be convenient.

Today, it is hard to realise that the free cone moving coil loudspeaker is nearly 50 years old and the rigid diaphragm moving coil speaker is nearly 80 years old.

Now it is clear that the RCA system closely approaches a stepless method, for by having many perforations and restricting the frequency or other coverage per paper section, one can produce intervals smaller than a semitone and these can be bridged by the portamento (or gliding) system. Nevertheless, the fact that the holes are discrete and represent time intervals does limit the synthesiser in some ways. When all the parameters are on the one roll, it is not possible to separate them or, for example, to change their relative positions or phase relationships.

# THE ORAMIC SOUND SYSTEM

To have complete control over all the factors involved, a system such as the Oramics graphic device offers unlimited flexibility. The essential part, which provides the information, is shown in Fig. 4.

Basically, the idea of drawing a waveshape or control element is far from new; it has been extensively tried in Canada, Germany, France and this country for electronic organ generators, for example, as well as for motion picture film. But all these investigators tried to produce the fully-finished and complete complex waveform at one time, just as if it were a photographic sound film track. For composing or musical synthesis, this would be useless; no variation is possible once the track is drawn.

The Oramic system builds up a sound picture from its basic elements, related to each other only in time. Observe that there are a number of independent tracks, each consisting of a length of transparent 35mm motion picture film. These are contained on spools and are drawn up by sprockets keyed to a common shaft. Thus, however many sprockets there are, all must rotate in synchronism. Now the film passes over a large metal plate, which is the writing table and is again picked up by similar sprockets on another shaft; this is coupled by a chain to the first shaft, so they must turn together and cannot slip.

# **INFORMATION TRACKS**

Information is imparted to the film tracks in the manner shown in Fig. 5. For example, the top four



Fig. 5. Printing information on film tracks

tracks could be frequency tracks, the fifth could be noise; then the sixth could be a gating track, to initiate the signal, the seventh could be envelope control (rise time, duration, decay) and the eighth track could be vibrato. Of course, there is no limit to the number of tracks possible.

The information is painted or drawn in opaque ink, or it could be strips of adhesive tape cut to shape and stuck on (easier to alter). When the shafts are rotated, the films pass from right to left over photoscanners with suitable exciter lamps. These scanners control the different sections of the synthesiser, in much the same way as do the microswitches of RCA, but of course in a smoother and much more way. Additional harmonic control is imparted by drawn masks scanned by a cathode ray tube, and these are instantly changeable. Much more complex harmonic patterns can thus be produced than by any switching system.

The tracks are ferried back and forth until the composer is satisfied that he has the effect he wants. Then the next "bars" can be worked on and so on, because in this system there is virtually no limit to the length of the composition.

An electric motor drives the sprocket assemblies at a constant speed when the hand control is not being used, and of course the composition is recorded on tape. Even so, this need not be the end of the process; if each signal track is recorded separately on a multi-track machine, further after-treatment is possible before combining the tracks in final form.

This machine, by the way, is an excellent teaching device, since the effect of altering each parameter can not only be seen, but heard. The real meaning of a musical waveform is thus clearly brought home to the student.

# SOLID STATE VERSATILITY

We might again stress that however simple or however complex the apparatus, it must have the basic facilities mentioned at the outset and it need have no more; but it can have elaboration of each channel and more channels. Today then we find that because of the compactness and light weight of solid state circuits, there are portable or semi-portable synthesisers of formidable capabilities. The purpose of all

these devices is the same, but some have facilities for taking in existing sounds (e.g. a microphone) and processing this in some special way.

The versatility of the transistor synthesiser is largely due to the use of voltage control. As already pointed out, this is far from new, but it is more readily applicable to semiconductors. Broadly it confers the advantage of noiseless gain control, the ability to use very long signal leads, and abolition of difficulties associated with impedance matching.

R. A. Moog appears to have been the first to apply these techniques commercially and in order to draw attention to the method, he made the wellknown "Switched on Bach" record. This is indeed a combination of the old and the new, and one feels that Dr Moog was very wise not to rely on any modern composition for processing. Systems like this have no storage time, therefore only a small amount of synthesis is possible without resetting. Consequently such recordings take a long time to complete —it may run into months.

# THE SYNTHI-100

These devices contain the facilities required to form any kind of musical or non-musical sound. Later developments have abolished the cumbersome patch cord, which gets in the way and is easily broken, so we show in Fig. 6 an example of the most up-to-date studio in existence, that of the Synthi-100 made by Electronic Music Studios of London.

Readers will of course have seen the advertisements for the VCS-3 in this journal, and the author has one of these, with keyboard. But the Synthi-100 is something far in advance of anything else, not only because of its facilities and long-term stability (which has always been poor with solid state synthesisers) but because for the first time it includes a small special purpose digital computer, complete with converters from analogue to digital and vice versa.

The storage capacity of this device is 10,240 bits, and the start of each event can be controlled to an accuracy of 1 part in 1,024; thus, if the clock is set to a rate of, say, 100 pulses per second, each event



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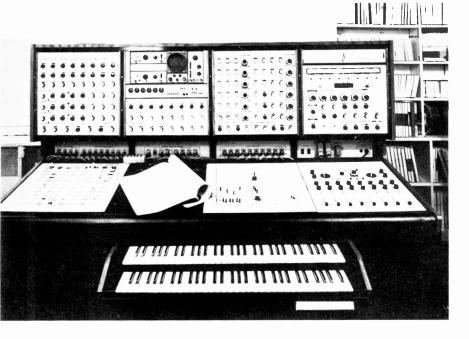


Fig. 6. EMS Synthi-100 studio

may be adjusted backwards or forwards in increments of one hundredth of a second. The total sequence length would be 10 seconds.

The many signal and processing circuits can be controlled from two 5 octave dynamically proportional keyboards. These operate the studio in real time, on six tracks, with the sequencer (the computer) remembering what is played.

This performance can be played backwards or forwards, at any speed, and edited to any degree of precision, prior to recording on magnetic tape. It is as if an infinite number of pianola rolls could be made instantly, but for any parameter.

# SIGNAL AND PROCESS CIRCUITS

Briefly, this ingenious device contains voltage controlled slew limiters, a frequency to voltage converter and a two-output random staircase generator with controllable time and amplitude variations. Twelve drift-free oscillators, from 20kHz to 40 seconds per cycle; eight dynamic filters and three transformerless ring modulators, which in fact can be cascaded to give double or even triple modulation—a fearsome thought!

Also there are eight voltage controlled output channels, eight input amplifiers, two joystick controllers, three envelope shapers and followers, a noise generator and reverberation units. All of these, and many other functions, are controlled by two cordless 60 by 60 way patchboards, a total of 7,200 pin locations.

It is not surprising that the BBC bought this unit in preference to all others, although it has VCS-3's as well.

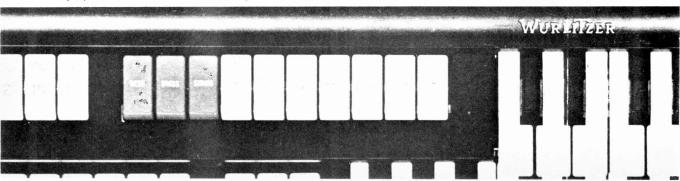
We cannot, of course, give any examples of sounds created by such systems, because a sound cannot be written down and even if this were possible, it would mean different things to different people. But we can say that it can produce musical effects of surpassing beauty, and at the other extreme, noises of an alarming nature. One could never exhaust the versatility of the Synthi-100.

And so to computers. Of course, any system feeding in digital information—like the RCA roll—is a kind of computer. But the description implies a logic device. It further suggests ownership of a computer, and this limits the field to those so equipped and with the time to spare. Consequently it is not surprising that most of the work along these lines has been carried out by the Bell Telephone Laboratories. Nevertheless, one of the most modern computer studios in the world is in London.

# SYNTHESIS BY COMPUTER

Frequency and any function which can be specified numerically requires digital treatment; duration, envelope control and other factors involving time need analogue circuitry; but various compromises are necessary because of the enormous amount of detail required.

Fig. 7. Showing the short manual of the new Wurlitzer 4037 organ. This controls the Orbit III Synthesiser which adds a new realism to conventional stops. The controls to the right provide a whole new repertoire of totally new sounds for the performer. This means that the scope of the total instrument is almost limitless



Numbers stored in a computer represent the desired sound waves to be generated. These numbers are converted to pulses of constant width but of amplitudes corresponding to numbers; for example, twelve is twice as "loud" as six. These pulses are then smoothed to produce a sound. Frequencies from 0Hz to nHz can be generated by 2n pulses per second, so we require 10,000 per second to obtain 5kHz at the loudspeaker.

But this is far too tedious a process for any length of time, so simplifications have been made by grouping frequency bands and other parameters into blocks or "instruments" as they are called, so that the number of operations to release or call up a complex event is reduced. Modifying parameters are introduced by the composer, and the computer reads a line from the instrument signals and inserts the chosen modifiers at the correct time, thus activating the instrument with generated numbers equivalent to the duration of the note.

This process can also be made self-repetitive in a random manner, so that the same effect is never repeated twice; it is then rather like throwing a number of dice into a bowl and then shaking them out, in the hope that a certain total number will appear!

# THE HUMAN ELEMENT

All in all, and from such recorded computer music as is available, it is irrefutable that if one wants music agreeable to our ears at this time, it is impossible to dispense with the human composer, although it is true that some sort of form can emerge from a process based on an order of probability.

Work has been done on the songs of Stephen Foster, so well known to all. All Foster's works have some resemblance to each other, so that it is possible to analyse them and establish an order of recurrence for all the notes used. If suitable deductions are made from these figures, and the result fed into a computer, sounds will emerge which, in their fundamental structure, bear a resemblance to Foster's compositions but do not sound like any of them. However, here we have a simple case, involving not more than 12 notes in all, because these are folk tunes.

# PERFORMANCE DEFICIENCIES

A disadvantage of the conventional computer is that the composer is unlikely to be able to re-cast his thinking into suitable "language" acceptable to the computer; hence he may have to work through a programmer, and this may very well upset his musical judgement and certainly any spontaneity.

There are some simplifications of the computer system, notably the serial structure method, but there is no doubt that when the machine takes charge, the warmth of character and the nuances of expression disappear completely, however "clever" the result may appear to be.

Therefore we can assume that no machine is likely to supplant the human brain, any more than an electronic synthesiser is likely to take the place of a member of the orchestra. But certainly it can augment and extend his facilities and of course, can produce special effects as we all know. This would seem to be a likely exploitation of musical electronics in the future.

# LINKING ORGAN AND SYNTHESISER

Readers have no doubt grasped that time is required to set up effects on any synthesiser, but if this range is limited, or complex mixing is not required, some of the facilities can be made available very quickly. We therefore see, in the new Wurlitzer 4037 organ, a simple Orbit III synthesiser built into the console and playable from a short compass third manual.

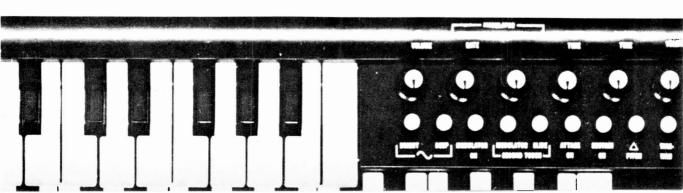
A vast number of extra effects came from this circuit, which has double touch keys so that yet further circuits can be brought into action. Because of the variable pitch characteristics of the Orbit III section, it must be on a keyboard separate from the main organ. Fig. 7 shows the lay-out.

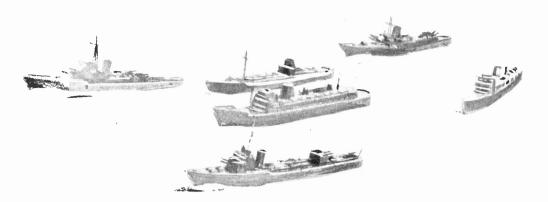
# TRENDS FOR THE FUTURE

Finally, one must appreciate that the performeraudience relationship might change so far as the concert hall is concerned. Since the advent of multitrack recording for cinema films, loudspeakers have been used above and behind an audience as well as behind the screen. The listener can be immersed in the sound field, and this produces strong psychological reactions in many people and is a powerful factor in estimating the effect of sound.

Because of the increasing use of magnetic tapes and the excellence of reproduction now obtainable, recorded sound can be as realistic as the original except for the dynamic or loudness range. It is therefore altogether possible that some synthetic music, alone or combined with recorded conventional music, may be played before audiences in halls designed acoustically so as to favour the loudspeaker and no other kind of sound source.

This could already be so in the cinema, were it not required to be so heavily damped because of the speaking voice. We await the developments of the next few years with great interest.





# COMPUTER WAR GAMES

# PART THREE By D. R. Daines

HE basic concept of the War Games Computer has been described together with the constructional information required to build up to the Third Stage (Fig. 3). The remaining stages convert the computer for fair assessment of any "damage" sustained during battle. Additionally this next stage will provide various types of target.

# STAGE FOUR -- PANEL 'B'

Panel B (Figs. 12 and 13) and switch S11 begin to open up the real potential of the computer, for this panel adds up the energy of the incoming pulses and gives us an indication when a preset amount has been received, or when a ship is sunk (Fig. 12).

Incoming pulses of various amplitudes are amplified by TR10. This is not to say that the previous stage has been a wasted effort, for all pulses are amplified- the strong and the weak. Capacitor C2 blocks d.c. and leaves only pulses swinging about zero volts, which any high impedance voltmeter or oscilloscope will show. In order to charge the storage capacitor C12, however, only negative-going pulses are required and this is achieved by the diode clamp D9 and R77. The exact value of R77 will depend on the characteristics of the particular diode used. Adjust this until the positive swing of the pulses is exactly zero volts.

# SCHMITT TRIGGER

The Schmitt trigger formed by TR11 and TR12 will fire briefly when the voltage at the base of TR11 reaches 2 volts, which it does when C12 is charged through R78. Switch 59a is a cancel switch to discharge C12 completely; C13 is an anti-surge capacitor to prevent the Schmitt from firing when the switch is snapped open.

The brief outgoing pulse passes through diode D10 and a flying lead (k) to (i) on D11 routes it to switch S11. Resistor R85 provides a convenient method of adjusting the energy available to the much larger storage capacitors C14 to C23, while diodes D10 and D11 prevent leakage of charge already on the selected capacitor. If constructors have no intention of going beyond this stage of construction, one of the Schmitt triggers (Trigger 1) can be omitted, the output from R78 going direct to D11 via points (h) and (i) on Fig. 12.

The storage capacitors C14 to C23 can be of any desired capacitance; those shown in the components list are for guidance only.

No accurate work has been done on the exponential curve comparing with size of ship, but the above component values have worked very well in dozens of games. (N.C. is no connection.)

# **EXTERNAL STORAGE CAPACITORS**

Switch S11 is a single-pole twelve-way wafer switch fitted with a skirted knob, which has the figures 0-10 on the skirt plus a blank space. In the 0 position no capacitor (n.c.) at all is fixed, which is a useful facility when checking the correct functioning of the circuit, while in the blank position a single wire leads to a socket which also has a chassis contact. In this way external storage capacitors C14a to C23a may be switched in. Such external additions might be temporary, or favourite values permanently soldered to the tags of a switch and housed in a little box. Notice that the positive side of all capacitors must be returned to computer chassis.

From point (I) two wires are taken off—one to \$10a and one back to panel B at TR13 base. (Fire bistable line is mentioned later). When the charge across the capacitor selected by S11 reaches two volts, Schmitt trigger 2 fires. The resulting brief pulse passes through C25 to Bistable 2 which switches to its second stable condition with TR15 hard on and TR16 fully off. The voltage TR16 collector rises, switching on TR17 and TR18, which are arranged

in a super-alpha pair.

Since R100 carries considerable current it generates some heat. For this reason it is better to keep it away from where the increase in temperature may affect the working characteristics of transistors or even destroy them. It is used for final adjustment of lamp voltage for LP2, after some 20 V has been dropped across R16 in the power supply.

The lamp itself is mounted behind a plastic lens and marked "Magazine", the return wire being

connected to chassis (Fig. 10b).

Switch S10 is a double pole on/off which discharges the capacitors on switch S11 (S10a) and also earths the base of TR15, thereby switching it off (S10b) and extinguishing the lamp. Resistor R101 is a low value discharge load for the capacitors on

S11; the value should be found to be sufficiently low not to interfere with the circuit operation (about 22 ohms). Although not shown in the wiring diagram (Fig. 10b) R101 can be inserted between S10a and Trigger 2 input (1).

#### USE OF STAGE FOUR

The knob-skirt numbers correspond to numbers assigned to ships and as long as players remember to turn to the correct target number each time, they may happily bang away at each other confident in the knowledge that the lamp will glow when any ship has been at the receiving end of sufficient computed damage. Fuller details will be given later.

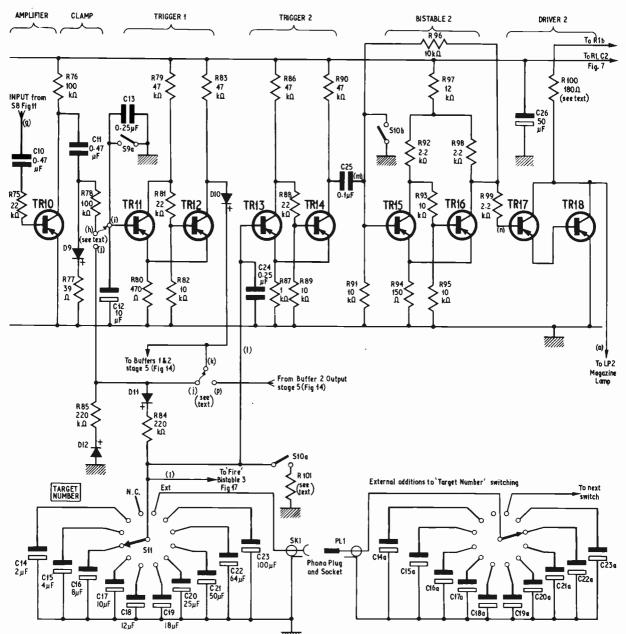
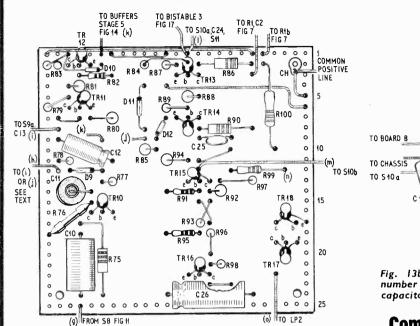


Fig. 12. Circuit diagram of Panel B (stage four). Incoming pulses are passed to the selected storage capacitor (C14-C23); trigger 2 fires when this capacitor is fully charged, bistable 2 operates, and driver 2 switches on LP2



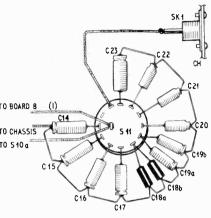


Fig. 13b. Wiring details for target number switch SII and the storage capacitors

## Components . . .

#### STAGE FOUR (Panel B Figs. 12 and 13)

Resista	ors				
R75	22k $\Omega$	R84	220k $\Omega$	R93	l0kΩ
R76	100k $\Omega$	R85	220k $\Omega$	R94	150 Ω
R77	39 Ω	R86	47k Ω	R95	10k Ω
R78	100k $\Omega$	R87	Ik $\Omega$	R96	l0k Ω
R79	47k Ω	R88	22k Ω	R97	l2k Ω
R80	470 Ω	R89	10k $\Omega$	R98	2·2k Ω
R81	22k $\Omega$	R90	47k $\Omega$	R99	2·2k Ω
R82	10k Ω	R91	l0k $\Omega$	R100	180 Ω TW
R83	47k Ω	R92	2·2k Ω	RIOI	22 Ω IW
					(see text)

All ±10% 4W carbon except where shown

#### Capacitors

- $0.47\mu\text{F}$  polyester 125V (or  $0.5\mu\text{F}$ ) 0.47 $\mu\text{F}$  polyester 125V (or  $0.5\mu\text{F}$ ) CI0
- CII
- CI2 10μF elect. 50V
- $0.22\mu\text{F}$  polyester I25V (or  $0.25\mu\text{F}$ ) C13
- CI4 2uF elect. 15V
- 4μF elect. 15V C15 C16 8μF elect. 15V
- CI7 IOμF elect. I5V
- ${8\mu F \atop 4\mu F}$  12 $\mu$ F elect. 15V C18a
- C18b
- C19a 8μF elect. I5V
- C19b  $10\mu F$  elect. 15V25μF elect. 15V
- C20  $50\mu$ F elect. 15V
- C2I C22 64μF elect. 10V
- C23  $100\mu$ F elect. 15V
- C24  $0.22\mu$ F polyester 125V (or  $0.25\mu$ F)
- $0.1\mu\text{F}$  polyester 125V  $50\mu\text{F}$  elect. 50VC25
- C26

#### Transistors and Diodes

TR10 to TR18 OC71 or similar pnp germanium type D9 to D12 OA91 or similar germanium type

#### Switches

- **S9** Double-pole, on/off or changeover toggle
- STO Double-pole, on off or changeover toggle
- SII Single-bank, single-pole, 12-way wafer

#### Miscellaneous

LP2 6V 0.06A m.e.s. lamp and holder SKI, PLI Phono or coaxial socket and plug Veroboard 0.15 in in matrix  $3\frac{3}{4}$  in  $\times$   $3\frac{7}{8}$  in with copper strips.

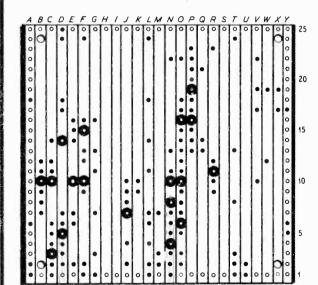


Fig. 13a. Layout of components on Panel B with underside view showing the breaks in the copper strip

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3∄ × 5	27p	27p
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17 ×32 €	100p	75p
17 × 5 (plain)	_	75p
17 ×3∄ (plain)	_	52 jp
17 × 2⅓ (plain)	_	37 ip
2+ × 5 (plain)	_	17 p
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#### STAGE FIVE-PANEL 'C'

One criticism of the computer to date is that ships blaze away at each other unabated until the sudden moment of oblivion. This is hardly realistic. A much more interesting and exciting game results when damage occurs bit by bit, affecting the fighting qualities in various ways. Panel C does that.

First, the lead (k) is disconnected from point (j) (Figures 12 and 13) and instead the damage pulses are passed equally from (k) to two buffers TR19 and TR20 (Fig. 14). These are arranged in emitter follower mode, and are designed so that the two halves of the readout section do not interfere with each other. From TR19 the output is taken through C27 and then reconnected to point (j) via (p) as in Fig. 12. The output from TR20 is taken through

R108 and C30 to switch over the bistable formed by TR21 and TR22 and so drive lamp LP3 in the now familiar way through TR5 and TR6 and point (s).

#### **TESTING AND USING**

Lamp LP3 will now glow every time there is a pulse from Trigger 1 and may be extinguished by the use of S9. The number of times that this may be done before lamp LP2 glows depends entirely upon the size of storage capacitor selected by S11.

In use a dice may be rolled each time a unit of damage occurs, in order to see where it is. A six for instance might indicate the captain killed and the conning tower in flames; a one might indicate an aircraft catapult destroyed. Further examples will be given later.

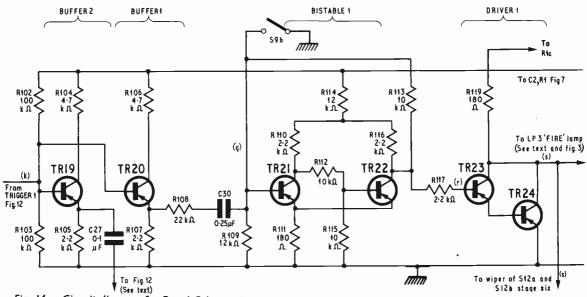


Fig. 14a. Circuit diagram for Panel C (stage five). This adds a further hazard in the form of "fire" (lamp LP3)

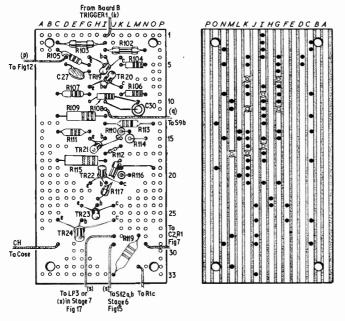


Fig. 14b. Layout of components on Panel C with underside view showing the breaks in the copper strips

## Components . . .

#### STAGE FIVE (Panel C Fig. 14) Resistors R102 100k $\Omega$ RIII $180 \Omega$ R103 100k Ω **R112** I0k Ω 10k $\Omega$ R104 4·7k Ω R113 2.2k Ω R105 **R114** 12k $\Omega$ $4.7k\Omega$ 10k Ω R 106 R115 R107 2-2k Ω **R116** 2.2k Ω R108 22k Ω **R117** 2-2k Ω R119 180 Ω1W R109 12k $\Omega$ 2.2k Ω R110 All $\pm$ 10% $\frac{1}{4}$ W carbon except where shown Č27 0 IμF polyester I25V C30 0.25μF polyester 125V Transistors TRI9 to TR24 OC71 or similar germanium pnp type Miscellaneous LP3 6V 0.06A m.e.s. lamp and lampholder Veroboard 0·15in matrix 5in × 2½in with copper strips

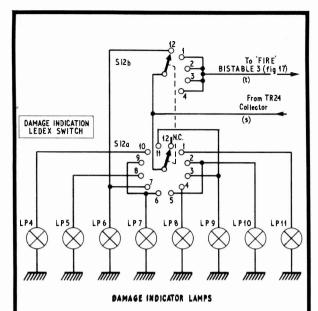


Fig. 15. "Random damage" selection circuit (stage six) using a Ledex switch

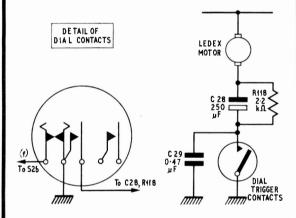


Fig. 16. Circuit details of the Ledex motor

## Components . . .

STAGE SIX (Ledex switching Figs. 15 and 16)

Resistor

R118 2.2k  $\Omega = 10\% \frac{1}{2}W$  carbon

Capacitors

C28 250μF elect. 64V C29 0·47μF polyester 125V

Switch and motor

S12a Single-pole, 12-way wafer S12b Single-pole, 5-way wafer

Both wafers assembled on a miniature Ledex rotor and ratchet mechanism available from suppliers of surplus Post Office equipment and components. (Manufacturer is N.S.F.) Alternative suggestions see text.

Lamps

LP4 to LPII 6V 0.06A m.e.s. lamps and lampholders

#### STAGE SIX—AUTOMATIC INDICATION

Actually attempting to compute just where damage should occur would be impossible and quite beyond the needs of a game. What is required is a random selection, with some types of damage occurring more often than others. One method of doing this would be by a twisted-ring counter in conjunction with gates -a method rather lavish in its use of semiconductors. Another more simple method would be to spin a twelve-way switch with the click-stop mechanism removed. No doubt other methods will occur to readers. The system used in the prototype was to move a Ledex motor-driven rotary switch of the double-pole twelve-way type or a uniselector switch one space each time the dial was operated. The wiring of the wafers will be seen in Fig. 15. The output of the driver is thus routed to any one of eight lamps, with four having twice the chances of the other four created by S12b. It should be noticed that one of the second wafer tags covers the n.c. condition of the first wafer.) The lamps are labelled as follows:

Single chance

Lamp 4 Conning tower

Lamp 5 Hull

Lamp 6 Aircraft or torpedo tubes

Lamp 7 ½ sub. armament

Double chance

Lamp 8 Engine room

Lamp 9 Rear turret

Lamp 10 Forward turret

Lamp II Rudder

The lamps may be arranged in any order for viewing, but it is difficult in the excitement of a game to keep track of what the next indication will be, particularly as threequarters of diallings will produce no visible effect. Moreover, no player could do anything to affect the outcome, even if he did remember the sequence.

#### DRIVING THE LEDEX

The Ledex coil requires 48 volts (24 volt versions are available) and draws a heavy current. It was required to keep everything as automatic as possible and so the telephone dial was used again. There is a pair of contacts that makes when the dial is drawn back, and remain closed until the dial is again at rest. Fig. 16 shows how this contact is used.

Resistor R118 passes insufficient current to pull the armature when the dial contacts are closed. However, C28 is very large and the surge of current charging it plus the small amount going through R118 is enough to activate the coil. It is only momentary; C28 is soon charged and the current passing through R118 is insufficient to hold the coil. The armature drops back and now the current used by the circuit is limited to the tiny amount through R118. Capacitor C29 is a surge suppressor to prevent supply line variations triggering Schmitts.

When dialling is completed, the dial trigger contact opens and C28 slowly discharges through R118. This takes about three seconds and if dialling is attempted before C28 completely discharges, the Ledex coil may not operate satisfactorily. In game conditions this is of no moment.

Next Month: Stage seven "fire" switching from Ledex. Further notes regarding how to get the best out of the computer.

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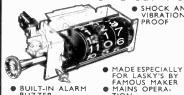
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ACI07	15p   AFI15	17p BC140	35p BCY31	22p BF272	80p EC403	15p ORP60	40n 2N930	25p 2N2904A	30p 2N3706	6 12p
ACII3 ACII5	20p AFII6 23p AFII7	17p BC141 17p BC142	35p BCY32 45p BCY33	25p BF273	30p GET880	27p ORP61	40p 2N1131 12p 2N1132	20p 2N2905 22p 2N2905A	25p 2N3707	
AC12S	17p AFIIB	30p BC   43	40p BCY34	17p BF274 20p BF308	30p MAT100 35p MAT101	15p ST140 17p ST141	17p 2N1302	17p 2N2906	30p   20:3708 25p   20:3709	
ACI26	17p AF124	21p BC145	45p BCY70	17p BF309	37p MAT/20	ISp TIS43	40p 2NI303	17p 2N2906A	27p 2N3710	
ACI27	17p AF125	20p BC   47	17p BCY71	30p BF316	75p MAT121	17p UT46	27p 2N1304	20p 2N2907	25p 2N371	
ACI28 ACI41K	17p AFI26 17p AFI27	20p BC   48 20p BC   49	12p BCY72 17p BCZ11	15p BFW10 20p BFX29	55p MPF102 27p MPF105	43p V405A 43p V410A	25p 2N1305 45p 2N1306	20p 2N2907A 22p 2N2923	30p 2N3819 13p 2N3820	
ACI42K	17p. AF139	33p BC150	17p 8D121	85p BFX84	20p OC19	30p 2G301	19p 2N1307	22p 2N2924	13p 2N390	
ACI51	15p AF178	50p BC151	20p BD123	85p BFX85	27p OC20	50p 2G302	19p 2N1308	27p 2N2925	13p 2N3904	4 27p
ACI54 ACI55	15p AF179 17p AF180	50p BC152 50p BC153	17p BD124	75p BFX86	22p OC22	30p 2G303	19p 2N1309 20p 2N1613	27p 2N2926 17p (G)	2N3905	
ACI56	17p AF191	50p BC   54	27p BD131 30p BD132	80p BFX87 80p BFX88	25p OC23 22p OC24	33p 2G304 45p 2G306	20p 2N1613 35p 2N1711	20p 2N2926(Y	12p 2N3906 1 1 p 2N4058	
ACI57	17p AF186	45p BC157	20p BDY20	€I BFY50	20p OC25	25p 2G308	35p 2N 1889	35p 2N2926	2N4059	
AC165	17p AF239	37p BC158	17p BF115	22p 8FY51	20p OC26	25p 2G309	35p 2N1890	45p (O)	10p 2N4060	
AC166 AC167	17p AFZ11 20p AFZ12	37p BC159 45p BC167	20p BF117 13p BF118	45p BFY52 60p BFY53	20p OC28 17p OC29	40p 2G339 40p 2G339A	17p 2N1893 15p 2N2160	37p 2N3010 60p 2N3011	80p 2N406 20p 2N406	
AC168	20p AL102	85p BC168	13p BF119	70p BSX19	15p OC35	33p 2G344	15p 2N2147	75p 2N3053	20p 2N517	
AC169	142 AL103	85p BC169	13p BF152	35p BSX20	15p OC36	40p 2G345	15p 2N2148	60p 2N3054	50p 2N5459	
AC176 AC177	23p ASY26	25p BC170	12p 8F153	35p BSY25	15p OC41	20p 2G371	13p 2N2192	30p 2N3055	63p 2S034	75p
A 2 187	20p A5Y27 30p A5Y28	30p BC171 25p BC172	13p BF154 13p BF157	35p BSY26 45p BSY27	15p OC42 15p OC44	22p 2G3718 15p 2G374	10p 2N2193 17p 2N2194	30p 2N3391 27p 2N3391A	17p 25301 20p 25302A	50p \ 45p
AC188	30p ASY29	25p BC173	13p BF158	25p BSY28	15p OC45	12p 2G377	27p 2N2217	20p 2N3392	17p 25302	45p
ACY 17	25p ASY50	25p BC174	13p BF159	30p B\$Y29	15p OC70	15p 2G378	15p 2N2218	25p 2N3393	15p 2\$303	60p
ACY18 ACY19	20p ASY51 22p ASY52	25p BC175	22p BF160	30p BSY38	15p OC71	9p 2G382	15p 2N2219	27p 2N3394	15p 2\$304	£1-10
ACY20	20p ASY54	25p BC177 25p BC178	17p 8F162 17p 8F163	30p BSY39 35p BSY40	15p OC72 30p OC74	12p 2G401 12p 2G414	30p 2N2220 30p 2N2221	22p 2N3395 22p 2N3402	20p 25305 22p 25306	£1 £1-10
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A CY22	19p ASY56	25p BC180	20p BF165	35p BSY95	12p OC76	15p 2N388	30p 2N2368	17p 2N3404	32p 25321	60p
ACY27 ACY28	18p ASY57 19p ASY58	25p BC181 25p BC182	22p BF167 10p BF173	22p BSY95A 22p BU105	12p OC77 £3:90 OC81	25p 2N388A 15p 2N404	50p 2N2369 22p 2N2369A	15p 2N3405 15p 2N3414	45p 2\$322 20p 2\$322A	50p 45p
ACY29	30p ASY58	25p BC182L	10p BF176	35p CILLE	60p OCBID	15p 2N404A	30p 2N2411	50p 2N3415	20p 25322	60p
ACY30	25p ASZ21	40p BC183	10p BF177	35p C400	30p OC82	15p 2N524	55p 2N2412	50p 2N3417	37p 25324	£1-20
ACY31 ACY34	25p BC107 18p BC108	10p BC183L 10p BC184	10p BF178	45p C407	25p OC82D	15p 2N527	60p 2N2646	55p 2N3525	74p 25325	£1 20
ACY35	18p BC109	IID BCI84L	13p BF179 13p BF180	50p C424 30p C425	17p OC83 40p OC84	20p 2N696 20p 2N697	12p 2N2711 15p 2N2712	22p 2N3702 22p 2N3703	12p 2\$326 12p 2\$327	£1:20 £1:20
ACY36	30p BC113	25p BC186	27p BF181	30p C426	30p OC139	15p 2N698	24n			
ACY40 ACY41	5p BC114	30p BC187	27p BF182	30p C428	20p OC140	17p 2N699	55p DI(	DDES & R	ECTIFIER	S
ACY44	18p BC115 35p BC116	30p BC207 35p BC209		30p C441 25p C442	27p OC170 35p OC171	15p 2N706 15p 2N706A	7p 8p.AAII9	8p BYZII	32p OA81	7p
AD140	40p BC117	35p BC209	IIp BFI85	30p C444	37p OC200	25p 2N708	12p AA 120	8p BYZIZ	30p OA85	7p
AD142	40p BC118	25p BC212L	11p BF188	30p C450	17p OC201	27p IN709	45p BA116	22p BYZ13	25p OA90	6р
AD149 AD161	43p BC119 35p BC125	45p BC213L 35p BC213L	IIp BF194	23p C720 24p C722	12p OC202 25p OC203	27p 2N711	40p BA126 42p BY100	22p BYZ16 15p BYZ17	35p OA91 35p OA95	7p
AD162	35p BC126	35p BC214L	12p BF196	30p C740	25p OC204	25p 2N717 25p 2N718	24p BY101	12p BYZ18	35p OA95 30p OA200	7p
AD161/	BC132	25p BC225	25p BF197	35p   C742	17p OC205	35p 2N718A	50p BY105	15p BYZ19	25p OA202	
162(MP) ADT140	63p BC134 50p BC135	30p BC226 30p BC317	35p BF200	45p C744	17p OC309	35p 2N726	27p BY114	12p OA5	17p 5010	4p
ADZII	£2 8C 36	30p BC317	12p BF222 12p BF257	80p C760 35p C762	17p P346A 17p P397	17p 2N727 45p 2N743	27p BY126 17p BY127	15p OA10 17p OA47	22p SO19 7p IN914	4p 6p
ADZ12	62:10 BC137	35p BC319	12p BF270	25p C764	60p OCP71	43p 2N744	17p BY130	15p OA70	7p IN916	6p
AFI14	17p BC139	45p BCY30	20p BF271	17p EC401	ISp ORP12	43p 2N914	17p BYZ10	35p OA79	8p IN4148	

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#### RADIATION FROM JUPITER

New light on the variations of the radiation from Jupiter has been offered by a team from Meudon Observatory. Recent observations carried out by Messrs. L. Consiel, Y. Leblanc, G. Antonini and D. Quemada has led them to the conclusion that Jupiter has a plasmasphere similar to that of the earth. It must also be concluded that this plasmasphere is very strongly affected by the solar wind, even though Jupiter is some five times as far away from the sun as the earth.

The difference between the earth's plasmasphere and Jupiter's plasmasphere is the size. The magnetosphere (the boundary across which the solar wind cannot go) is determined by the magnetic field. It is not regular in shape and in fact can be and is very much distorted by the pressure of the solar wind and its interaction at the boundary. In the case of the earth it is pushed back on the sunward side and causes the whole boundary to swell up in size as it were on the lee side, see Fig. 1.

The normal radius of the magnetosphere of Jupiter is some 50 times that of the planet. This boundary is determined by the electrical effects in the plasma around Jupiter. The co-rotating plasma has an upper limit which depends on the interaction between the rotating electric field and the solar wind. This limit in the case of Jupiter is only about eight times the radius of Jupiter.

#### **EFFECTS OF SATELLITE 10**

This fact has led the Meudon observers to suggest that the effects known to be made on the Jupiter radiations by this planet's No. 1

satellite named IO, is the direct result of changes of level in the plasmasphere.

The effects of IO, first suggested by Bigg in 1964 were observed before this by the writer and the team led by C. H. Barrow under a NASA contract with Florida State University.

There are other considerations to be taken into account, for example, the effect of the next two satellites. Although the effect of these was slight it was detectable. As the writer predicted in 1966, Amalthea the innermost satellite was also a factor in modifying radiations as was confirmed a few years later. Still another effect has to be remembered, and that is that not all the radiation that has been observed in the decametre region is effected by IO. Some remains continuous whatever the position of IO.

#### THE PLASMAPAUSE

Basically the theory put forward by the French observers does add an important viewpoint. The mechanism they are suggesting works as follows. The solar wind velocity was compared with the radiation activity time and the position of IO. The results were then correlated. It seems clear that the radiation received did occur when IO crossed the upper boundary of the plasmasphere. This boundary is called the plasmapause.

During the quiet sun it would appear that the plasmasphere is able to extend outwards from its normal position, but when the sun is active it is forced downwards to a much lower level. This places the boundary within the orbit of IO, and the bursts of radiation appear when the satellite crosses the boundary.

This is of course valuable additional data but there are still a number of anomalies. Moreover in the first study undertaken by the writer in co-operation with the team previously mentioned a direct correlation between solar activity and Jupiter activity could not be found, as was reported in "Nature". However, it was always considered that the sun was a cause as the writer has always held. This new work confirms the validity of the supposition and it is now only necessary to pursue the French work further to find a satisfactory answer.

There are two prime questions which are not satisfied as yet.\* The first is, why is there so much difference in the level of the radiation in the northern and southern hemispheres and why is the radiation frequency selective at different stations?

This last question is a very important one since it is quite often the case that two or three stations working on the same frequency do not simultaneously receive the radiations and where the stations are

working on say three frequencies, station 'A' may receive radiation at say 18MHz, station 'B' at 20MHz, and station 'C' at 22MHz at a particular time, but in each case the other operating frequencies show no results.

#### JUPITER'S ATMOSPHERE

Attempts to measure the depths or even the existence of atmosphere on planets and satellites use observation in the visual spectrum. The usual visual method is the observation of an occultation. In the case of Jupiter which is one of the brightest objects in the sky it eclipsed the bright star Beta Scorpii. This is the first time this century that this has happened.

Naturally full advantage was taken of this by astronomers. A team from the University of Texas led by Prof. David Evans and Dr. William Hubbard observed the occultation from observatories in India, Australia, South Africa and the Virgin Islands. Specially designed scanning photometers were used since it was necessary to make very quick determinations of the star's light curves.

New information as to the temperature of the planets reveals that instead of the previous figure of 100 degrees K for the outer atmosphere the observers all agree on a figure between 150 degrees and 200 degrees K. The atmospheric gradient also turned out to be less steep than had been thought.

A bonus on this observation was the fortuitous occultation of the star by IO, which proved that the satellite was larger than the earth's moon with a negligible atmosphere. The observations have enabled a more precise position for Jupiter's orbit to be determined and new information on the weight of the gases in its atmosphere.

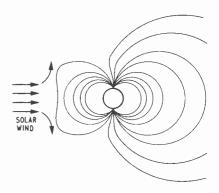


Fig. 1. A section through the magnetosphere at noon. The solar wind has pushed the sunward side of the magnetic field away to form a tail which at times is so long that a tadpole shape appears



"HE unit to be described will act as a tireless sentry, sounding off as soon as water level rises or, perhaps more practically for most of us, will give you early warning of rain or snow so that washing left in the garden can be quickly brought

The unit can be left switched on for months on end as the quiescent current is in the order of nanoamps. Assuming that the alarm is not left on for hours on end, the battery will decay of old age rather than run down and for the specified type the life is at least a year.

#### **CIRCUIT ACTION**

To understand the circuit consider the block diagram in Fig. 1. The unijunction relaxation oscillator TR2 has a highly sensitive electronic switch, triggered by water or damp, in its positive supply—TRI acts as the switch.

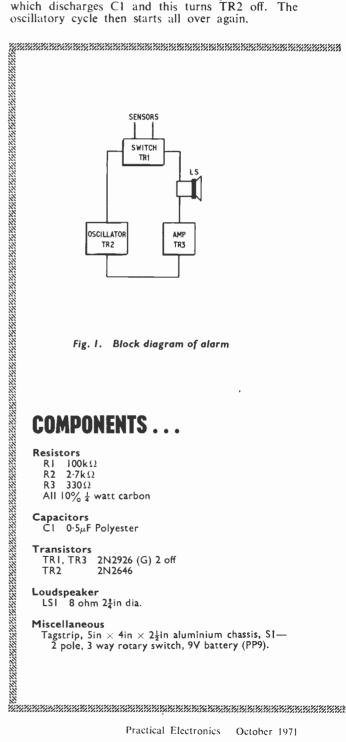
The output of the oscillator is insufficient for a practical alarm system so it is coupled to TR3 which switches on and off in sympathy with TR2 and passes the alarm signal to the loudspeaker.

Referring to the actual circuit in Fig. 2 it will be seen that in the "on" state (assuming the sensors are inoperative) the only current drawn will be the leakage of TR1 and TR3 since the base of TR1 is

floating and the base of TR3 is held at negative potential.

When the sensors are shorted out, R1 applies bias to TRI turning it on and although there is a volts drop across it, this is small and not enough to affect the operation of TR2.

The resistor R2 charges up C1 when TR1 allows current to pass; this raises the potential at the emitter of TR2 and because of the mode of operation of the unijunction transistor, when a certain level has been reached the device passes current which discharges C1 and this turns TR2 off. The oscillatory cycle then starts all over again.

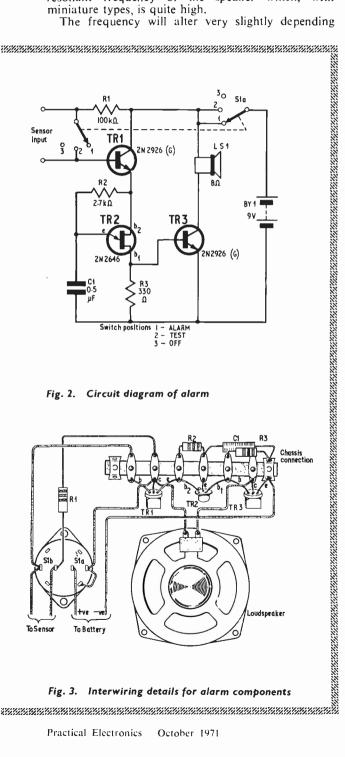


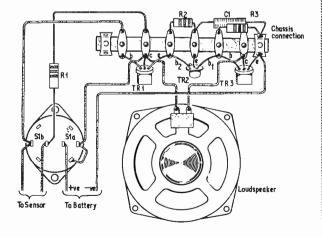
#### LOUDSPEAKER DRIVER

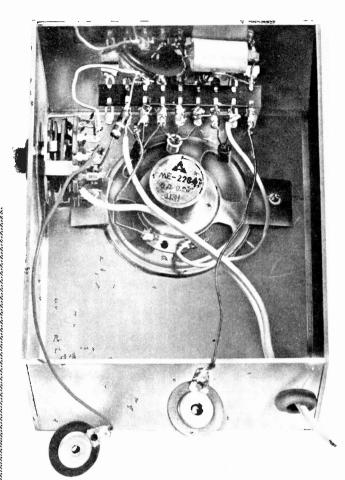
When TR2 is on, a potential is developed across R3 and this switches on TR3. What we get in effect is most of the battery potential being applied across the loudspeaker in a series of rapid pulses which together form a note.

The pitch of the alarm note is controlled by the ratio of R2/C1 and it can be changed by altering either. Greater effective output can be achieved by selecting the note so that it corresponds to the resonant frequency of the speaker which, with miniature types, is quite high.

The frequency will alter very slightly depending







on the resistance between the sensors. In operation the alarm will sound if any resistance between zero and five megohms is connected between the sensors.

#### SWITCH POSITIONS

Three positions can be selected by the switch. In position "1" the unit is on standby. In position "2" the sensors are shorted out setting the alarm in operation for testing. This is necessary because after about a year the battery will eventually run down and if it has not been operated, some check is needed

on the battery condition.

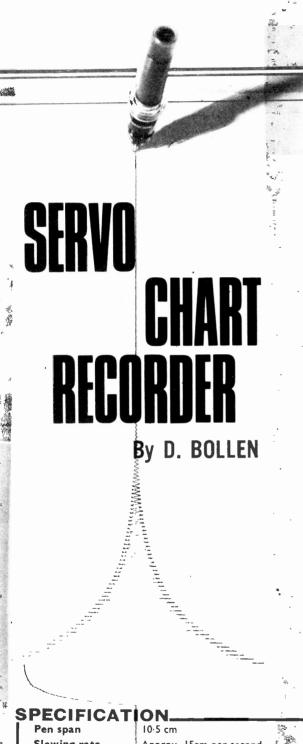
Position "3" is used once the alarm has been noted and is no longer required. If a mains power supply is used instead of batteries this could be wired to a bulb whose other connection runs to chassis giving a visual indication that the alarm is not set. A warning bulb can of course be used with battery operation but battery life will be greatly reduced.

#### CONSTRUCTION

All components, except of course the sensors are mounted into an aluminium chassis 5 in × 4 in ×  $2\frac{1}{2}$  in; this makes for a neat wall mounted unit.

A series of holes should be drilled for the loudspeaker vents and others for the switch spindle, the sensor wires and the tag-strip mounting screws.

The three transistors are fixed to an 8-way tagstrip, the two extreme tags being chassis connections, Both this, the loudspeaker and the switch are wired up as shown in Fig. 3. continued on page 829



Slewing rate Input resistance Dead zone Accuracy Set zero Inputs (1)

Approx. 15cm per second  $20k\Omega$  per full span volt  $+ 6k\Omega$ Less than 0.5mm (0.5%) Typically  $\pm$  2% Anywhere on paper Eleven attenuator settings covering 5mV/cm-10V/cm

SIV/cm for timing pulses Frequency response D.C.-IHz at 5cm peak to peak

HE rate of change of some electrical signals is too slow for convenient measurement with ordinary test instruments. Examples of such signals are; the charge-discharge characteristics of large batteries and capacitors, long-term drift voltages in electronic circuits, outputs from light, pressure and temperature sensors, biological impulses and waveforms, long period earthquake waves, and radio astronomy

Recorders for handling very slow electrical events are expensive to buy, and some will consume hundreds of feet of specially sensitised film or paper each week when running continuously. The recorder design offered here can be built for as little as £15-£20 and draws a linear ink trace on cheap rolls of adding and accounting machine paper. Rolls cut from decorator's lining paper can also be used.

It is a simple matter to take measurements from unruled paper with the aid of a transparent graticule, similar to that employed with oscilloscope screens, and the instrument is conveniently calibrated in terms of volts per centimetre of pen deflection.

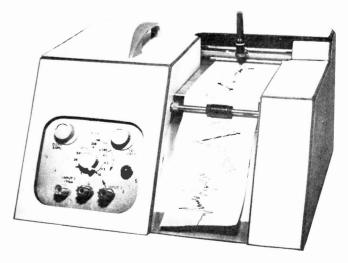
Although no attempt was made to exploit the high accuracy possible with a servo recorder, the accuracy achieved with standard components is equal to, or better than, that offered by most quality testmeters. The recorder pen mechanism is made up from radio dial cord drive parts, and a model boat motor supplies the necessary motivating force.

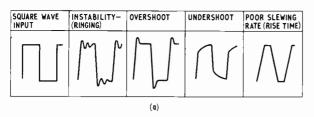
#### **DESIGN CONSIDERATIONS**

A simple, uncorrected servo system would drive the recorder pen in a most erratic manner. The pen could oscillate, overshoot the mark, undershoot, or take a long time to traverse the paper. As with audio amplifier testing, servo faults really come to light when the system is subjected to a step or square wave input, see Fig. 1a.

Of course, we are concerned here with a very low frequency square wave test signal, say 0.01Hz, as there is a limit to how fast a heavy pen can be made to respond. Most servo recorders have a frequency response extending to not more than a few Hertz at most.

Yet another fault, as shown in Fig. 1b, is where the pen moves in a series of jerks or steps when the input signal varies very slowly.





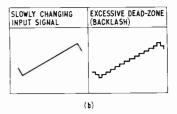


Fig. 1 (a) Oscillograms indicating various faulty recorder responses for a test square wave input. (b) ramp distortion oscillogram, the result of a jerky pen action.

#### **BASIC CIRCUIT**

The basic circuit of the chart recorder is given in Fig. 2. A high gain operational amplifier, ICI is arranged to compare two voltages at its inverting input, one via RI from the slider of VRI, and the other an output voltage via R2. VRI is mechanically linked to the pen drive, and has a reference voltage  $V_{\rm B}$  across its track.

Because of its very high gain, ICl can be thought of as a switch which is off when both inputs are equal and of opposite polarity. If one input is slightly different to the other, the output will switch hard on in a positive or negative direction, depending on the relative polarities of the inputs.

With the servo motor at rest, there is zero volts relative to earth at the operational amplifier output, and the voltage from VRI exactly cancels the input voltage, assuming that RI equals R2.

Suppose now that the input increases by positive 30 millivolts; this small change of input is amplified and causes the output to switch hard on and place something like negative 6 volts across the motor brushes. The motor now rotates in a direction dictated by output polarity and moves VR1 slider to a new position where the slider output has increased by a negative 30 millivolts, thus cancelling the change of input voltage, and reducing the voltage across the motor to zero again.

The distance travelled by VRI slider during the above operation is equivalent to the positive 30 millivolt input change.

When R1 equals R2, the full pen deflection, or span, will represent an input voltage equal to  $V_{\rm B}$ , and if R2 is halved in value the span will be equivalent to half  $V_{\rm B}$ . All that is necessary, therefore, to provide a choice of calibrated inputs, is single switched values of R2.

#### **OVERCOMING INSTABILITY**

The servo system shown in Fig. 2 would be unstable if the dotted components C1 and  $R_r$  were omitted. There are two forms of instability at work here, the first caused by too much amplifier gain, and the second by the delaying action of the servo motor, or electro-mechanical integrator effect. The inclusion of a feedback resistor  $R_r$  serves to reduce amplifier gain to a manageable level, but if it is made too small in value there will be a large unwanted dead zone, giving a result similar to Fig. 1b.

The function of C1 is to supply a differentiating action which almost exactly cancels servo motor integration. Without it there would be instability and overshoot resulting from a sudden change of input voltage.

If, however, C1 is too large in value, over correction leading to undershoot will be the result. It

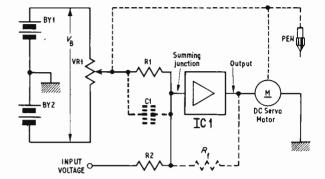


Fig. 2. Basic chart recorder circuit

follows that C1 and  $R_f$  should be made adjustable to cater for individual variations of motor speed and amplifier gain.

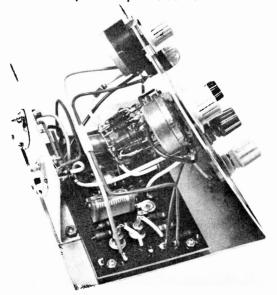
The remaining factor of a poor slewing rate is largely determined by the power of the motor and gear reduction used.

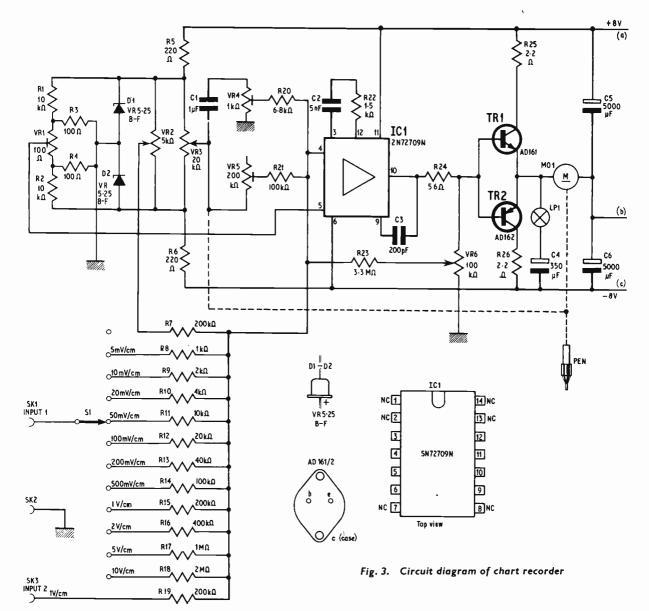
#### PAPER FEED PROBLEMS

A few problems can occur with the chart paper feed. Usual faults are short-term speed discrepancies, and lateral shifting, or wobble of the paper.

The former is quite difficult to cure, even when the paper has sprocket holes, and is due to paper imperfections, etc. A timing pulse fed to the pen at regular intervals will, however, serve to calibrate paper speed. Lateral shift can be prevented by correct design of the paper feed mechanism.

Controls are mounted on a single piece of aluminium which also forms a chassis for the amplifier panel. Note the heat sink for the output transistors





#### CHART RECORDER CIRCUIT

The complete circuit of the chart recorder is given in Fig. 3. A brief comparison with the circuit of Fig. 2 will help to identify the main component functions.

VR3 in Fig. 3 is the mechanically driven potentiometer equivalent to VR1 in Fig. 2. VR5 and R21 are equivalent to R1, pin 4 of the i.e. package is the inverting input, inputs R8 to R18 are switched values for R2, diodes D1 and D2 provide the reference voltage VRB, VR4 gives a variable output from differentiating capacitor C1, and VR6 acts as an adjustable dead zone or  $R_f$  value.

Now looking at Fig. 3 in more detail, VR1 ensures that the chart recorder will maintain its zero setting with the input terminal open or short circuited, by supplying a small offset compensating voltage to the amplifier non-inverting input, pin 5. VR2 allows the pen to be set anywhere on the chart paper (centre zero, or zero either side) by injecting a large offset voltage to the summing junction via R7.

VR5 is for initial calibration of the instrument.

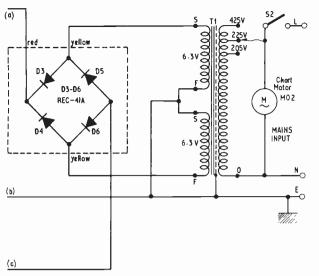
Attenuator steps (resistors R8 to R18) are in a 1, 2, 5 sequence, from 5mV/cm up to 10V/cm, plus an additional input for timing pulse calibration of chart speed.

The motor specified for use with the recorder has a stall current of 500mA at 6V d.c., far in excess of the output capability of an i.c. operational amplifier.

Complementary emitter followers TR1 and TR2 serve to boost the amplifier output current to a maximum of 1A, thus allowing other motors of heavier consumption to be substituted.

#### **HUM INDICATOR**

If mains hum or other higher frequencies are present at the recorder input they could be amplified and fed to the motor as a.c. power, thus causing it to overheat. There is no visible response from the servo to input frequencies above about 15Hz, so some method of indicating these unwanted inputs must be devised.



## **COMPONENTS...**

Resist	ors				
RI	$IOk\Omega$	RIO	4kΩ 1%	R19	200kΩ 2%
R2	$10k\Omega$	RII	10kΩ 1%	R20	6·8kΩ
R3	$\Omega$ 001	R12	20kΩ 1%	R21	100kΩ
R4	$\Omega$ 001	RI3	40kΩ 1%	R22	$1.5 k\Omega$
R5	$220\Omega$	R14	100kΩ ĺ%	R23	$3.3M\Omega$
R6	220 $\Omega$	R15	200kΩ I%	R24	<b>56</b> Ω
R7	200k $\Omega$	R16	400kΩ 1%	R25	2·2Ω IW
R8	lkΩ 1%	RI7	$1M\Omega 1\%$	R26	2·2Ω IW
R9	2kΩ 1%	R18	2MΩ 1%		
All 🚊	10%, ½ w	att ca	rbon except	whe	re stated.

#### **Potentiometers**

VRI 100 $\Omega$  miniature horizontal mounting pre-set

VR2 5kΩ linear carbon

VR3 20kΩ wirewound or linear carbon (see text)

VR4 | IkΩ miniature horizontal pre-set

VR5 200kΩ miniature horizontal pre-set

VR6 100kΩ linear carbon potentiometer

#### Capacitors

C1  $I\mu F$  polyester C4  $350\mu F$  elect. ISV C2 5nF polystyrene C5  $5,000\mu F$  elect. I2V

C3 200pF polystyrene C6 5,000µF elect. 12V

#### **Integrated Circuit**

ICI SN 72709N, BP 709 or 709 OPA

#### **Transistors**

TRI ADI61 TR2 ADI62

#### Diodes

DI, D2 VR5·25B-F 5·25V 2W Zener (2 off)

#### Rectifier

D3-D6 Rec-41A

#### **Transformer**

T1 Filament transformer, secondaries 6.3V 1.8A; 6.3V 1.8A (Radiospares "Hygrade")

#### Switches

SI Single pole 12 way wafer

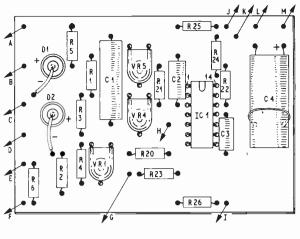
S2 Single pole mains on/off

#### Lamp

LPI 6V 0-36W

#### Miscellaneous

 $4\frac{1}{4}$ in  $\times$   $2\frac{1}{2}$ in 0-lin matrix s.r.b.p. or copper laminate board, 16 s.w.g. sheet aluminium, knobs, terminals, lampholder, TO-66 mica washers with insulating bushes. For mechanical components see text. SK1-SK3 Miniature sockets with plugs. M01, M02 (see text).



TERMINAL PINS- ● CONNECTIONS TO UNDERSIDE - ●

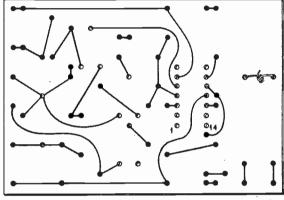


Fig. 4. Component assembly and wiring details of amplifier panel

It might be thought a simple matter to just filter out all frequencies above 15Hz, but this could upset the servo compensation and cause undershoot and instability. Instead, a lamp LPI and capacitor C4 are included to give a visual warning of hum.

Recorder accuracy is mainly determined by the track linearity of VR3 and the tolerance of input resistors R8-R18.

#### GENERAL CONSTRUCTION

The layout of individual chart recorders may differ from the prototype, to suit individual preferences and mechanical components to hand. Some readers may wish, for example, to increase the pen span and paper width to, say, 10 inches, or merely tailor the instrument to fit an existing box.

To facilitate custom building, the recorder is broken down into the following sub-units: amplifier panel, power pack, TR1 and TR2 heat sink, control panel, pen drive, and chart drive. The chassis frame to which the pen drive and chart drive are mounted can be fashioned from brass or alloy angle, sheet aluminium, or Meccano parts.

#### AMPLIFIER PANEL CONSTRUCTION

Fig. 4 shows the amplifier panel layout. As there are no wiring crossovers, components can either be assembled on a 0·1 inch matrix, punched s.r.b.p. board or a printed circuit. In the latter case it is

advisable to use a 14 way dual-in-line socket for the i.c. package owing to the difficulty of desoldering in the event of a failure.

Panel leads are labelled A to M for quick identification during final wiring of the chart recorder.

#### **POWER PACK CONSTRUCTION**

With only four components, the power pack can be quickly assembled on a suitable piece of aluminium sheet, with clips for the capacitors. The sheet acts as a heat sink for the rectifier bridge assembly.

Yellow rectifier pins are wired to the transformer output, and the connection to C5 is the red pin. Finally, ensure that the finish of one transformer 6.3V winding is connected to the start of the other winding when forming the centre tap. See Fig. 5.

#### HEAT SINK AND CONTROL PANEL CON-STRUCTION

TR1 and TR2 should be provided with a heat sink equivalent to at least 16 square inches of 16 s.w.g. aluminium sheet. If the control panel is bent to form a chassis for the amplifier panel, this will act as an auxiliary heat sink. The power transistors must be mounted with insulating washers, and it is advisable to check this insulation with a testmeter during construction.

#### PEN DRIVE UNIT

Details of the pen drive are given in Fig. 6. The pen boom can be made of a section of chromed tubing taken from an old portable radio or television telescopic aerial, or just plain brass tubing.

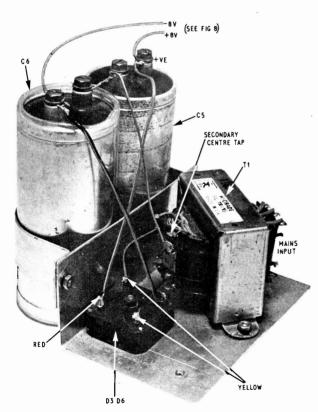


Fig. 5. Modular assembly of power pack on aluminium sheet

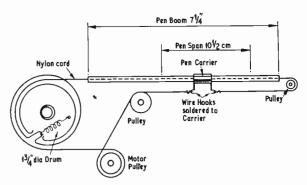


Fig. 6. Details of the pen drive assembly

The short piece of brass tubing which acts as a pen carrier should be a snug sliding fit on the boom. A compass attachment is securely glued to the carrier with epoxy resin to accept a range of tubular nib drawing pens of the Varient type.

VR3 is an ordinary wirewound or linear carbon one to three watt potentiometer, which is easy to obtain and cheap to replace when worn out. If the user wishes to extract the best possible slewing rate from his recorder, it should be specially selected or treated for minimum spindle torque.

It is possible to lighten the action of many wirewound pots by taking the back off and removing any thick protective grease with switch cleaner.

If the component used for VR3 is later found to have a linearity error of more than 1 per cent, this can often be improved by wiring a 1 Megohm preset resistor between the slider and one end of the track. The linearity error of general purpose potentiometers is seldom quoted by manufacturers, but those with values above 10 kilohms can be surprisingly good. If in any doubt, a precision potentiometer with low torque and a linearity error of less than 0.5 per cent can be purchased.

#### D.C. MOTOR

The d.c. motor (M01) employed for the recorder must have carbon brushes, a stall current of less than 1A, and be fitted with a gear reduction in the region of 16: 1.

A motor with a multi-speed gearbox is preferable as it allows the reduction ratio to be adjusted to suit the frictional loading of the cord drive for optimum slewing rate.

The motor pulley is a brass or plastics bush mounted on the gearbox spindle with a tight fit p.v.c. grommet. Rubber grommets are useless in this application and will wear out quickly. Conventional brass or plastics pulleys, on the other hand, are prone to slipping. It is advisable to support the free end of the gearbox spindle with some form of bush bearing.

After assembly, check the pen drive for smooth action by connecting a  $1\frac{1}{2}$ -3V battery to the motor. It may be necessary to alter the tension of the drum spring and remove high spots from the boom tube with glasspaper.

If a longer pen span is required, this can be achieved by fitting an extended boom tube and a larger diameter drum. The diameter of drum needed for a given span is equal to the span in centimetres divided by 5.97, assuming that VR3 has a 270 degree effective rotation.

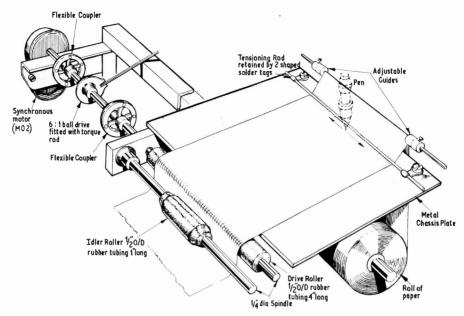


Fig. 7. Details of the chart drive unit

#### **CHART DRIVE UNIT**

The drive mechanism shown in Fig. 7 accepts any width of paper, up to the full pen span, without lateral shifting. The paper moves from the roll, through adjustable guides, and under a tensioning rod; this rod, in conjunction with the short idler roller, maintains a stable feed. Smooth, seam free rubber tubing is glued to the drive spindles to form the rollers.

Ball reduction drives are used to give a selection of speeds from one chart motor. For example, a one r.p.m. motor with three cascaded 6:1 ball drives gives the following speeds with a  $\frac{1}{2}$  inch diameter drive roller: 4cm/min, 40cm/hr,  $6\cdot6\text{cm/hr}$ , and  $1\cdot1\text{cm/hr}$ .

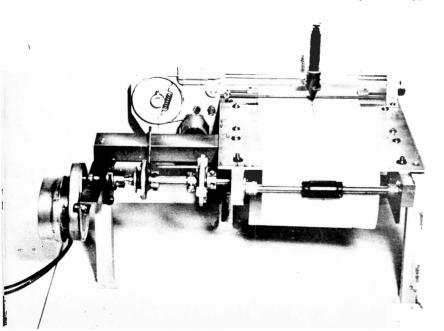
When a reduction drive is not needed it can be replaced by a flexible coupler or short length of 4 inch spindle.

The prototype chart drive employed roller spindles mounted in thick brass bearers, but this was later found to be too robust and difficult to adjust. A much simpler form of construction would be with spindles revolving in bearings made from old potentiometer bushes, which are bolted to angle or sheet aluminium.

#### **MECHANICAL COMPONENTS**

A Mini-Richard motor with six speed gearbox can be ordered from most model shops and is imported by Ripmax, 80 Highgate Road, London, N.W.5. A Variant pen with 0.2mm nib, and a compass attachment is available from large stationers. Electronic Brokers Ltd., of 49-53 Pancras Road, London, N.W.1. can supply MA23 chart motors with fixed speeds ranging from 20 r.p.m. to 1/240th r.p.m.

Silver steel \(\frac{1}{4}\) inch diameter spindles are stocked by ironmongers, and the dial drum, flexible couplers, and reduction drives by the usual electronic component suppliers.



Chassis frame with pen and chart drive unit

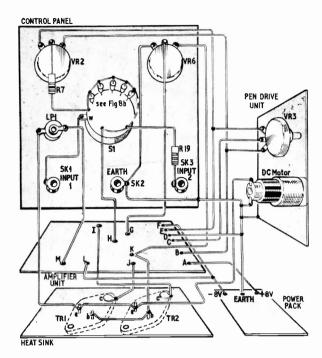
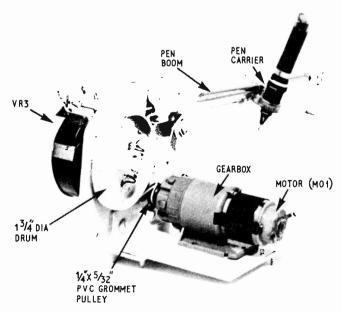


Fig. 8a. Interwiring diagram of chart recorder subassemblies

#### FINAL ASSEMBLY AND SETTING UP

Chart recorder sub-units are wired together as shown in Figs. 8a, b. The following points should be borne in mind before testing the recorder, and during final assembly.

Connections to the track of VR3 may need to be reversed to give the desired direction of pen travel for a positive input voltage. If the leads to the d.c. motor are out of "sense" with VR3 rotation the pen will move hard over to one side of the paper



Pen drive unit

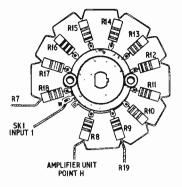


Fig. 8b. Wiring of switch SI

and will not respond to an input signal. A peculiarity of the Mini-Richard gearbox is that it changes its direction of rotation for each step change of gear ratio, thus necessitating reversal of motor leads when changing gear.

To set up and calibrate the recorder, all pre-sets and VR2 and VR6 should first be placed in the mid-track position. Stick a 0-10cm scale (cut from an exercise book or a thin plastics ruler) under the pen and switch the recorder on. The pen should move to somewhere near the 5cm mark and stop. If the pen oscillates, increase the VR6 dead zone setting. Position the pen at exactly 5cm with VR2.

If the input attenuator is set to 5mV/cm, and input 1 is shorted to earth, the pen will be seen to shift to a new position. Bring the pen back to the 5cm mark with VRI while the input is still shorted. There should be no movement of the pen when the input is open or short circuited. Now set the attenuator to IV/cm and inject a known d.c. voltage into input I. Calibrate the pen deflection by adjustment of VR5.

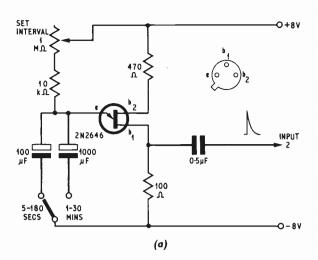
To check for over or undershoot, have the chart paper moving at maximum speed and switch a fixed input voltage on and off, this should trace a rough square wave. Adjust VR4 and VR6 for best square wave response, with reference to Fig. 1a.

As a final test for smooth pen travel in response to a slowly changing signal (Fig. 1b), charge a 1,000 pF capacitor to about 10V and connect it across input I and earth with the attenuator set to 2V/cm. The pen will trace the discharge curve of the capacitor and if it moves in a series of jerks or steps, try increasing the gearbox reduction ratio or use a smaller dead zone. The recorder should now be ready for use.

#### **USING THE RECORDER**

Normal precautions should be taken to avoid input hum when connecting the recorder to other equipment, in some cases it will be necessary to increase the dead zone setting to extinguish LP1. If desired, limit switches can be fitted, to open circuit trace, try another brand of ink, or water down the ink.

Ensure that the servo motor does not remain stalled for long periods with the pen at span limits. If desired, limit switches can be fitted, to open circuit the collector of TR1 or TR2. Alternatively, the pen drive cord tension can be carefully adjusted so that the motor pulley slips when the pen reaches the end of its travel.



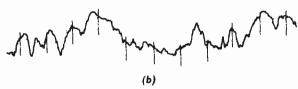


Fig. 9(a). Simple u.j.t. oscillator circuit that can be built for calibrating chart speeds. (b) Showing timing pulses superimposed on trace

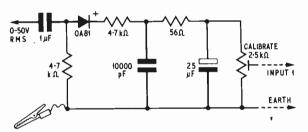


Fig. 10. Circuit diagram for a divide by ten probe. This extends the measurement capability of the recorder to higher frequencies

The circuit of Fig. 9 shows a simple pulse generator for calibrating chart speeds. A pulse output is obtained at intervals ranging from 5 seconds to 30 minutes by switch selection of two capacitors and adjustment of a 1 megohm potentiometer. An example of timing pulses superimposed on a trace is given in Fig. 9b.

As it stands, the recorder will display an undistorted sine wave of 1Hz at more than 5 cm peak to peak, and 5Hz at 1cm peak to peak. It is possible to measure and record the average level of higher frequencies by using a radio frequency probe, such as that shown in Fig. 10.

The probe has a frequency response extending from 100Hz to tens of megahertz, and with its division ratio of ten will offer 0-10V r.m.s. when the recorder attenuator is set to 100mV/cm, 0-20V r.m.s. at 200mV/cm, and 0-50V r.m.s. at 500mV/cm. If the probe is used with attenuator settings below 100mV/cm it will need to be recalibrated because of resistive loading, and linearity will be poor.

The servo chart recorder is well suited for use with the Seismograph described last month, and with Radio Astronomy receivers.

### RAIN & WATER LEVEL ALARM

continued from page 821

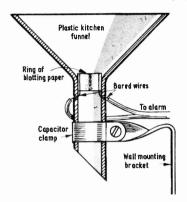


Fig. 4. Funnel arranged as a sensor for rain or snow

#### **SENSORS**

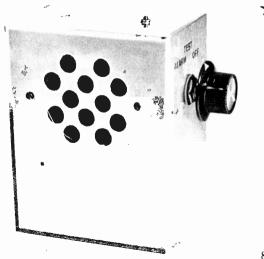
The sensors can take two forms. For water level warning two brass rods should be spaced about an inch apart and positioned above the water surface at the required level.

For rain or snow a plastic kitchen funnel can be used as seen in Fig. 4. Here two copper wires are fitted through small drilled holes at the top of the neck and a circle of blotting paper is slipped in so that it touches both. By using this arrangement snow, which may not soak into the blotting paper, will also build up until it bridges the sensors. Very light rain will tend to stick to the sides of the funnel and run down, soaking into the paper. A simple bracket should grasp the neck of the funnel for mounting to an outside wall or post.

Very long lengths of wire can be run between the sensors and the alarm because of the sensitivity of the unit.

#### LDR CUT-OUT

A simple refinement to the circuit can make sure that you are not disturbed by the alarm at night—after all if used as a rain alarm you usually couldn't care less if it pours after dark. Simply insert a light dependent resistor such as the ORP 12, in the collector supply to TR1. The resistance will stop operation of the whole unit except during daylight. Obviously this l.d.r. will have to be mounted outside.





The North American Nebula (N.G.C. 7,000). The shape of this nebula shows how it became so named. It is about 3 degrees east of  $\alpha$  Cygni.

BY F.W.HYDE Part 5

The previous article dealt with the setting up of the aerial system and the construction of a suitable corner reflector. This article deals with the pre-amplifier, the converter, the receiver, and the recording system.

#### PRE-AMPLIFIER

Although a general specification has been laid down for the pre-amplifier, some latitude is permissible provided that certain of the important parameters are kept in mind. For example, the desired gain has been stated as not less than 16dB. There is no reason why this should not be greater, provided that the unit is stable and the noise level at a reasonable figure.

More than one unit could be used up to a maximum overall gain of 100dB. Again, it is the stability and noise factor which will be important. If the noise level is too high the latter stages of the amplifiers may be overloaded, not forgetting the receiver. The result in such a case would be useless. The pre-amplifier gain must be consistent with low noise and real amplification of signal.

It is preferable to have a pre-amplifier at the aerial itself, and if two units or more are available then the first can be mounted on the aerial and the others located nearer the receiver. It will be clear that the screening and earthing of high gain units will need care. The interconnecting coaxial leads will have to be routed and be cut so that nodes do not appear on the screening. This is best accomplished by avoiding multiples of one -half wavelength when cutting to size.

#### POWER SUPPLY ARRANGEMENTS

The pre-amplifier can be a standard commercial type, built round either valves or transistors. Where the aerial is at the observation position the power supply offers no problem whether valve units or transistor units are employed. However where the aerial is some distance away there can be problems.

If valve units are decided upon, and provided the distance is not excessive, mains leads may be run. If this is the case it is recommended that they are laid in the ground, since this will generally avoid any local interference being picked up and conveyed to the amplifier.

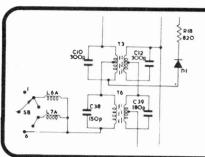
An alternative arrangement is to use low voltage transmission by means of a step-down, step-up system at the ends. Since this will require rather larger cable it could be more costly than the simple system.

If the units are transistorised then the power can be taken via the aerial lead with suitable filter networks at each end. Alternatively the power pack may be an integral part of the unit, and normal mains leads taken to the point of use.

It is not recommended that dry batteries be used. Wet (secondary) batteries are a possibility if they happen to be available. On the whole it is perhaps best to use the mains feed for this will provide a point for appliances that may be used when working on or modifying the aerial or ancillary systems.

A watertight case or box should be provided to house the unit since exposure to the weather will cause serious problems. It is also a wise precaution to tape up the coaxial connection points.

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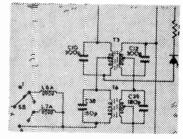
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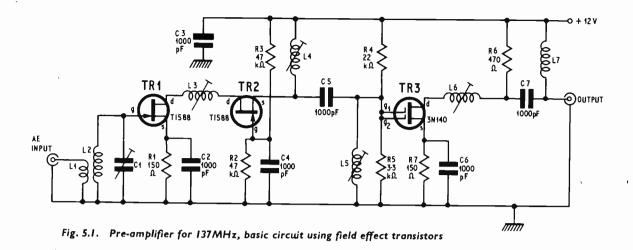


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#### PRE-AMPLIFIER CIRCUITS

The choice of pre-amplifier circuitry is a wide one, and some examples for the home constructor are given in Figs. 5.1 and 5.2.

Commercial units can be purchased from a number of suppliers. Among these commercial units will be found some specially designed for the 144MHz amateur band. It should be a simple matter to modify these for the chosen frequency of 137MHz. This can be done in such a way that the pre-amplifier may be used for both purposes.

#### THE CONVERTER

Considering the converter, it is better in some ways to use a commercial product since all the "bugs" will have been dealt with in the course of development. However, if the urge to start from scratch is strong, then there are commercial units that can be modified or entirely new units may be designed and made up.

To cover this aspect two circuits have been drawn as a guide and are shown in Figs. 5.3 and 5.4. Commercial television converters can be modified for the purpose and both valve and transistor types are available. Alternatively, local radio service dealers may have suitable turrets available from obsolete television sets.

One particular example which the writer used was a turret from a Murphy Television receiver which was manufactured as a unit by Sidney Bird Ltd. Some of these are likely to be still around. The coils on these units were easily accessible and gave no difficulty when it came to modification.

As in the case of the pre-amplifier, there are some commercial converter units built for the exact frequency band required and others that are available for the amateur band of 144MHz. Generally, these latter are easily modified, but if crystal controlled the latitude on such units as regards tuning coverage would be too narrow. In such cases, the crystal will need to be deleted and the necessary circuit modifications made.

Another point to bear in mind is that some of the converters that may be available on the surplus market have an intermediate frequency which is above 30MHz. Here, unless the communication receiver to be used has a range above 30MHz, additional modification would be required.

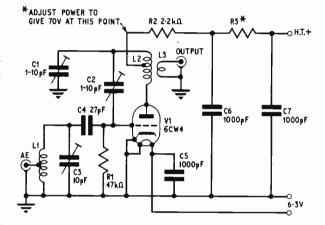


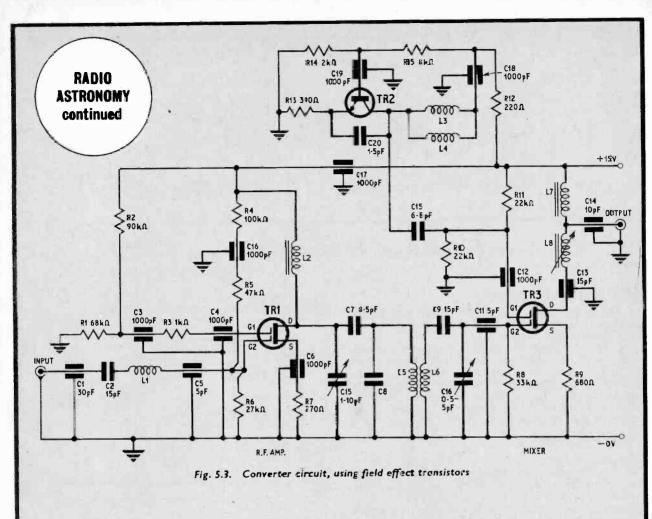
Fig. 5.2. Pre-amplifier for 137MHz, basic circuit using triode valve

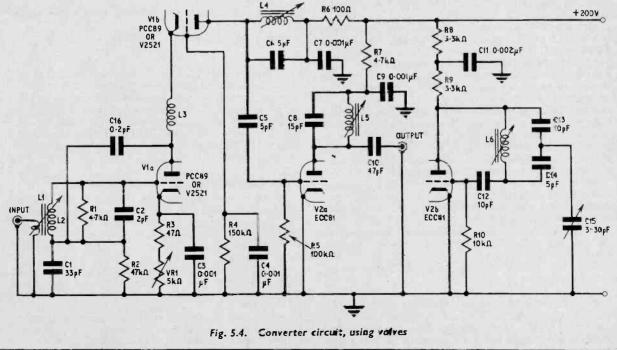
A final point that must be emphasised is that the converter must be adequately bonded to the receiver. The i.f. output of the converter will come to the aerial terminal of the receiver, but it will not be sufficient to rely on the earthing provided by the coaxial lead. The chassis of the converter and the chassis of the receiver must be properly electrically bonded together.

#### THE COMMUNICATIONS RECEIVER

In the case of the receiver, if there is the need to acquire one, there are two groups to choose from: the current range of commercial receivers, and those which appear on the surplus market.

There are many well known brand names that come to mind, and some of these receivers may already be in the possession of readers who propose to attempt this radio astronomy project. Some of the "surplus" types have increased in price over the last year or so. This usually means that they are almost in mint condition. The most important point to be made in regard to the older types of communications receivers is the availability of spare valves.





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Code	Power	Tolerance	Ronge	Values available	l to 9 (see no	10 to 99 te below)	100 up
000000	1/20W 1/8W 1/4W 1/2W 1W 1/2W	5% 10% 5%. 10%. 2%	82Ω –220K Ω 4·7Ω –470K Ω 4·7Ω –10MΩ 4·7Ω –10MΩ 4·7Ω –10MΩ 10Ω –1MΩ	E12 E24 E12 E24 E12 E24	9 1 1 1-2 2-5	8 0 8 0 8 1 2	7 0.7 0.7 0.9 1.9
***	3W 7W	10% ± 1/20Ω 5% 5%	0·22Ω+3·9Ω 12Ω-10ΚΩ 12Ω-10ΚΩ	E12 E12 E12	7 7 9	7 7 9	6 6 8

Codes: C=carbon film, high stability, low noise.
MO=metal oxide, Electrosil TR5, ultra low noise.
WW = wire wound, Plessey.

Values: E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24 denotes series: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and their decades.

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30p; 6V 0·04A clear type LSSC/C-6V, 30p; 6V
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**82 BATH STREET** WALSALL WSI 3DF Of the many newer types of communications receivers available there are reconditioned models and some commercial firms specialise in such equipment.

#### **ESSENTIAL FEATURES**

There are one or two points that need emphasising in regard to the receiver specification. An r.f. gain control is desirable. It would be an advantage if the a.g.c. can be switched. It would be useful if a noise limiter is fitted. Last but not least is the importance of stability of the power supply; on cheaper types of receiver this is unlikely to be good enough, so to the price of the receiver must be added something for the provision of stabilisation.

In spite of what has been said above, it need not prevent any one "having a go". Even if the results are not all that is to be desired the thrill of getting some results will be the greatest urge to improve the

equipment.

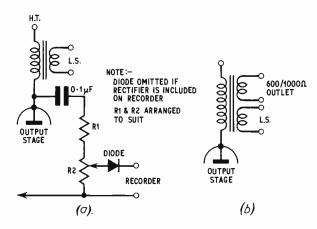


Fig. 5.5 a, b. Alternative arrangements for connecting recorder to receiver output stage

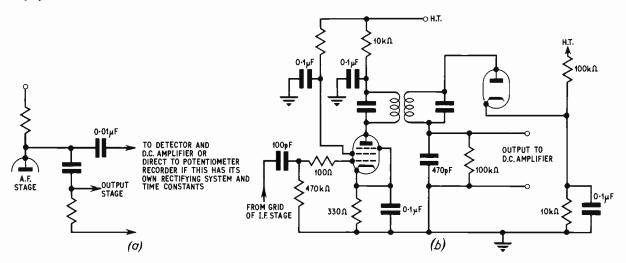


Fig. 5.6 a, b. Arrangements for connecting recorder to receiver via d.c. amplifier

#### **RECORDING UNITS**

The most basic recording system will be the pen recorder connected to the output of the receiver. If the recorder is of the low resistance coil type it can be connected directly to the output transformer at the speaker terminals via a diode or metal rectifier. Some recorders are fitted with the alternative terminal board arrangements for a.c. or d.c. operation. Where the coil is of high resistance then the output can be taken off the anode of the output section via a suitable network. Alternative systems are shown in the diagrams in Fig. 5.5 a, b.

There are other alternatives for the connection of the recorder when the coil resistance is high or the recorder is of the potentiometer type. A modification has to be made to the receiver circuitry in this case. The actual modification detail will naturally depend on the type of receiver in use, however the basic requirements for this modification are indicated in the examples of circuitry given in Fig. 5.6 a, b.

#### TYPES OF RECORDER

At this point it will be useful to describe the various types of recorder and the principles of operation. The simplest form is the moving coil system

which is a "giant" version of the ordinary moving coil meter as used for measuring current and voltage. It consists of a magnet within which a coil is suspended between bearings. There is an arm attached to the coil which is a capillary tube type of pen, one end submerged in an ink reservoir and the other in the form of tube resting on the paper. The pen moves across the paper leaving an ink trace. The paper itself is driven by a clock of high precision or a synchronous motor. Provision is made for the speed to be changed by the use of gears.

Another type of recorder is generally known as the "potentiometer" form. This consists basically of an amplifier into which the signal is fed and the output drives a motor system which carries the pen across the paper. There are a number of forms of this but the basic principle is the same. The main difference between this type and the pen motor type is that the potentiometer version has a system of mechanical or electrical means of "chopping" the input signal so that it can be amplified sufficiently to drive the motor to which the pen is attached.

There are also a number of variations in the way the paper is marked. The ink method has been mentioned so far, but there are other ways such as hot stylus on a waxed paper, a current conveyed through

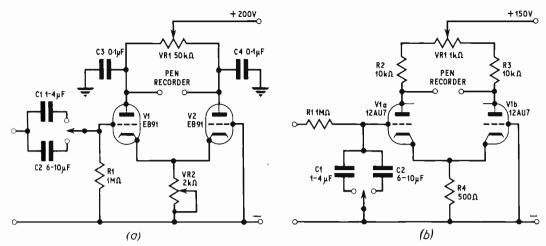


Fig. 5.7 a, b. D.C. amplifier circuits

a sensitive paper which in effect colours the paper, or maybe a system where the pen is pulled down on to the paper and the result is a series of dots. Whatever the system used the end result is a visible trace on some form of paper.

(A potentiometer recorder which will be ideal for this project appears in this month's issue.)

#### D.C. AMPLIFIERS

Two examples of d.c. amplifiers for recorders are shown in Fig. 5.7 a, b. Each has time constant circuits incorporated, these are necessary to record a clearer trace. If the normal time constant in the receiver were used then all the random noise received will obscure the solar noise proper. The length of the time constant is made variable so that there is a choice when looking for special effects.

For example, certain solar bursts are short in duration and therefore the best results will be obtained with a short time constant. Other phenomena is slow acting and this is better detected when using a longer time constant.

#### TAPE RECORDING

It is very useful to keep a tape recording of all observations since this provides an additional catalogue of events even when a pen recorder is used. For those who are unable to use a pen recorder at the beginning it may be possible for them to arrange for the tape recording to be transferred to paper at a later date.

When using the tape recorder for the observations the time of the observation must be recorded accurately, preferably on the tape as well as in the log. It would be an advantage to have a timing device that could superimpose a "time tick" on the track, but for this particular project it is not essential.

#### **SOLAR PHENOMENA**

The project being described is directed primarily to the study of certain solar phenomena. A brief survey of this phenomena will now be made so that when all the equipment is ready for operation, some idea of what the recordings will mean is understood by the observer.

The sun is one of a hundred million similar stars in the Galaxy. It is a yellow star classified as a

"G" type. Though it is quite insignificant as a star in the Galaxy, it is nevertheless the most important unit in the solar system since the earth and its people could not exist without it. It is the source of energy necessary to life.

The sun has a peculiarity so far as astronomers are concerned, and that is that it is a variable star. Because this is so a great deal can be learned about processes which cannot be reproduced on earth but which enable important deductions to be made about some of the fundamental principles of the universe.

The sun is a vast sphere of highly compressed gas some 864,000 miles in diameter. It is visible as a bright disc which is called the photosphere. It has a well defined edge because there is a sharp boundary where the temperature of the main body and the chromosphere and corona suddenly changes.

The actual temperature of the photosphere is of the order of 6,000 degrees K (degrees Kelvin = degrees Centigrade + 273 degrees). Temperature measured in degrees Kelvin is known as the Absolute Temperature. From the size and the mass of the sun it can be deduced that the temperature at the centre must be of the order of 15 million to 20 million degrees. About half the mass of the sun is hydrogen and a large part of the remainder helium.

This mass of gas can be likened to a vast reactor where the energy is radiated from the centre outwards from the central core to the surface of the photosphere. From the surface it then escapes in various forms over the whole of the electromagnetic spectrum. The sun consumes some 4,000 tons of its own mass each second.

#### THE CHROMOSPHERE

The chromosphere, or coloursphere, is so named because of its pinkish appearance. The chromosphere is about 12,000 miles thick. It has certain special characteristics one of which is the "reversing layer" which exists at the lower levels and is about 600 miles deep. This area contains many ionised atoms, that is atoms which have lost one electron.

Under such conditions visible light can be absorbed by these atoms. Such is the activity in this area that electrons are continually jumping from one level to another. In the process intense ultraviolet radiation is produced. This extends toward the earth and causes the ionosphere layer round the earth.

TABLE 5.1
TYPES OF SOLAR EMISSION

TYPE	DURATION	POLARISATION	MECHANISM	TEMP K°	
Quiet Sun	Constant	Random	Thermal		
Slowly varying component	Days or months	Generally random but circular at cm wavelength	Thermal	<2 × 10 <sup>6</sup>	
Rapidly varying components					
(after flare)					
Initial phase					
Type III	Seconds	Random	Płasma	>1011	
Type V	Minutes	Usually random	Synchrotron	1011	
Second phase		,	-	10	
Type II	Minutes	Random	Plasma	< 1011	
Type IV	Hours	Varies random to circular	Synchrotron	1011	
Type I	Hours	Random to circular	7	10*	

#### THE CORONA

The corona is an extension of a more tenuous part of the sun and is normally seen only at the time of an eclipse. It extends out in an irregular manner dependent upon the magnetic field of the sun.

Over a period of about 11.2 years there is a variation of the coronal activity which depends upon the number of sun spots that occur during this period. This cycle, which is regular in its rhythm but varies in maximum intensity, has many effects on the solar system.

#### **OTHER SOLAR ACTIVITIES**

In addition to the sunspots themselves there is considerable other activity. When the photosphere is examined closely it is found to be granular in appearance. These granules are of various sizes varying between 150 and 800 miles in length. There is a slightly different temperature between the darker granules and photosphere proper. This difference is something of the order of 200 degrees.

The surface is however constantly changing and great spouts of gas are thrown off to enormous

heights, areas flare up and there is a constant stream of plasma which is radiated into space and known as the solar wind. Each of these activities have certain effects and these will be dealt with in more detail when the work on the project begins. In the meanwhile a list is given in Table 5.1 which summarises the various types of activity and their effects on the earth's environment.

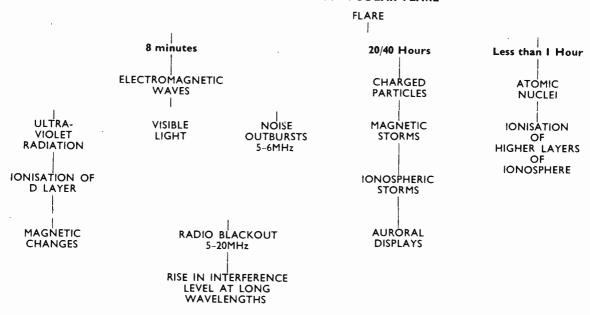
#### THE RADIO SUN

The radio sun is very much greater in extent than the visible corona would suggest. The radio sun is invisible and extends to something like an ellipse which is 80 solar radii in one direction and 110 solar radii in the other. This was established during the period of activity that existed in 1960 by O. B. Slee in Sydney. Australia, More will be said about this again in another project using the interferometer.

The effects of a flare are shown in Table 5.2.

The next article will describe the setting up and testing of the telescope units and the commencement of the first observations.

TABLE 5.2
THE RESULTING EFFECTS OF A SOLAR FLARE



# 

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

#### **AUDIOPHILE**

It is not often that Ferrograph find it desirable to make technical changes to their professional quality tape recorders, but when they do it is usually carefully noted by other manufacturers.

The latest modification to their eries 7 range of recorders is Series claimed to make them the only hi fi. domestic use, tape recorders incorporating the Dolby "B" noise reduction system on the market at

the moment.

The type "B" system for use in the home recorder is based upon, and works on the same principles as, the Dolby "A" type professional noise reduction system. The "B' system eliminates the background noise once considered inevitable when recording wide-frequency-range sounds at the low speeds generally associated with domestic tape recorders. At low speeds tape hiss is usually the primary barrier to satisfactory quality, and this system was designed to reduce such hiss.

The high quality of the Ferro-graph tape transport, heads, and electronics are such that when any inherant noise resulting from low recording speeds is reduced (a claimed 10dB) through use of the Dolby system; the overall quality of recordings made at  $1\frac{7}{8}$  in/sec is claimed to be comparable to that produced at 7½ in/sec without this

system.

Available direct from Ferrograph Co. Ltd. at The Hyde, Edgware Road, London, N.W.9, or through selected dealers, the Ferrograph recorders with the Dolby system start at £187 for a monaural recorder, and go to £263 for a high speed, high performance stereo recorder. Purchase tax is not included.

#### COMPACT STEREO

Since manufacturers realised that people wanted a good performance amplifier incorporated in the compact type record player/amplifier units, they are now generally accepted and gaining increasing

Now most manufacturers produce excellent amplifiers for these units and the **Permic** 6-6 stereo amplifier/player is one such unit.

The amplifier has a claimed output of 6 watts r.m.s. per channel, measured at 1kHz continuous sine wave into 8 ohm loads. Distortion is in the order of 0.3 per cent. The frequency response at 1 watt r.m.s. with tone circuits flat is 20Hz to  $20kHz \pm 2dB$ .

Inputs are provided for record, tape and radio and the input sensitivity is claimed to be better than 100mV into 3 megohm for a rated output at 1kHz.

An output socket on the front panel is provided for low impedance stereo headphone listening.

The price of the Permic 6-6 is £39. which does not include the price of speakers. All models are fitted with a Garrard turntable, and a Sonotone 9. TAHC or KS41C cartridge with a diamond stylus.

Full details of the Permic 6-6 stereo amplifier and other models can be obtained from Permic Ltd. 17 Upland Road, Bexleyheath, Kent.

Permic also run a special customer service for those who wish to have the amplifiers installed in their own favourite piece of furniture.

#### HEADPHONE LISTENING

For those who prefer to listen to their favourite programme or piece of music without any outside distractions, then the new Ravensbrook senior professional stereo headphones from Rogers Developments Ltd., 4-14 Barmeston Road, London, SE6 3BN, should be most popular.

The headphones, although intended primarily for their own

amplifiers, are compatible with other high quality amplifiers. Particular features include a twin moving coil system, individual volume controls integral with each earpiece and excellent bass response, claimed to be above average.

The recommended U.K. retail price for the Ravensbrook Stereo

Headphones is £18.50.

#### BENCH LIGHT

Designed primarily to aid operators and inspectors engaged on assembly or inspection work of an intricate nature, the Allen A90 4 and 6 tube bench floodlights would be a handy luxury to have in the workshop.

Costing from £24 to £55 there are two models available with either four or six 8 watt 12 inch (300mm) fluorescent tubes providing illumination levels of 11,000 and 16,000 Lux respectively 4 inches (100mm) distant from the lamps. Precise positioning is provided by a spring-balanced support arm and ball-joint mechanism.

It is claimed that the large area light source obviates distracting shadows from tools or hands, even when located very close to the work area. The maximum reach of the arm is 26 inches (640mm).

In addition to the screwdown base for bench mounting, two other alternative mountings are available; a bench clamp and a wall bracket.

Applications advice, and an illustrated leaflet is available from the manufacturers, P. W. Allen & Co., 253 Liverpool Road, London, N1 INA.



Allen A90 benchlight



Ferrograph Dolby "B" Recorder



Rogers Ravensbrook stereo headphones

Permic stereo 6-6 amplifier/player



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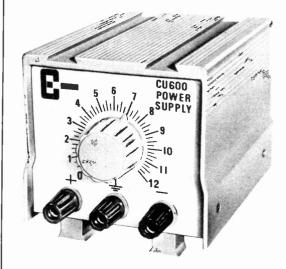
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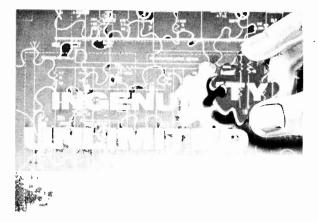
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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

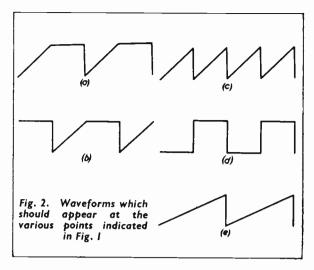
This is YOUR page and any idea published will be awarded payment according to its merit.

ORGAN DIVIDER CIRCUIT

Tone generators of frequency divider type electronic organs are usually either driven by bistable multivibrators or synchronised blocking oscillators.

Substantial cost saving can be accomplished by using a multivibrator chain with each multivibrator cycling at one-quarter (normally half) of the frequency of the previous, and each multivibrator providing two outputs, one being twice the frequency of the other. The blocking oscillator transformers are dispensed with and only half the number of multivibrators are required.

The circuit diagram in Fig. 1 shows a circuit that has been tested and works well. Fig. 2a and 2b show the waveforms on the bases of TR1 and TR2. By combining the two, the waveform in Fig. 2c results. This is one of the outputs and has a frequency twice that of the multivibrator.



The waveform in Fig. 2d is taken from the collector of TR1. When combined with the waveform of 2c and reduced to half the magnitude the resultant effect is shown in Fig. 2e. This has the same frequency as the multivibrator and is the second output.

The values of the capacitors have, of course, to be scaled proportionately to the frequency of each multivibrator.

The synchronising output to the next multivibrator contains some of the input sychronising pulse. If desired, to make the synchronising easier an r.c. filter may be introduced between each stage to reduce this unwanted signal.

Each output is connected to the switching resistors for the various footages.

The amplifier following the keyboard switching should be biased so that the d.c. potential of the input is the same as the d.c. potential of the earth side of the keyboard switches.

J. H. Asbery, Wembley.

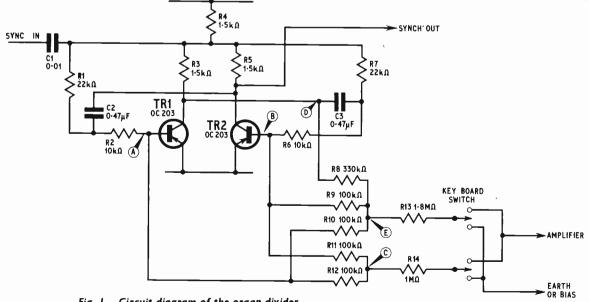


Fig. 1. Circuit diagram of the organ divider

#### TIME SWITCH

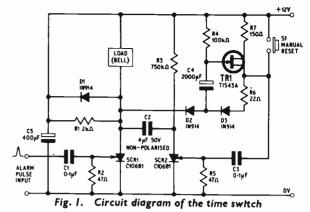
SOME of your readers might be interested in the circuit shown in Fig. 1 that I have designed. Basically it is a monostable with a high power output and a very long time delay, approximately 10 minutes.

I am using the circuit to ring a bell for 10 minutes after a light beam is broken, but there are obviously many other ingenious applications that readers could experiment with.

An input pulse turns the thyristor SCR1 "on" and rings the bell. The resistor R1 passes more than the required holding current, while diode D1 kills any back e.m.f. The capacitor C2 charges via R3 and capacitor C4 charges via R4, D2 and SCR1. After 10 minutes TR1 fires and capacitor C4 discharges via R6 and D3. A pulse across R6 fires SCR2 via capacitor C3 and capacitor C2 switches SCR1 "off", stopping the bell ringing.

Capacitor C4 and resistor R4 determine the delay time and may be altered over a wide range, remembering that R4 should be greater than 3 kilohms. If C4 is larger than specified the value of R6 should be increased. Capacitor C5 smooths out any spikes on the supply rail, which could upset the operation of the thyristors. Resistors R2 and R5 stop any

misfiring.



Thyristor SCR1 can handle 1A easily (12 watts load); for larger loads the thyristor must be uprated and C2 and R3 changed to ensure reliable turn-off of the SCR.

This circuit has been built and works perfectly. However, would-be constructors should note that if different thyristors are used then resistor R3 should be chosen to pass less holding current, but be low enough to charge C2 in approximately five minutes.

L. Cook, Prescot, Lancashire.

#### CRYSTAL OSCILLATOR FOR CLOCK

The "Digi-Clock" published in the December 1970 to March 1971 issues of P.E. relies for its accuracy on the stability of the mains voltage frequency used to power the clock. This may be accurate enough for most people but for high accuracy, a crystal oscillator unit is the answer.

The frequency of the mains supply varies slightly during the day, and it can cause a clock to be 8 seconds slow in any one day. It is true that at sometime after midnight this error is eliminated by increasing the frequency of the mains supply to cancel any error. Also, at times during the winter months, just prior to voltage reductions, the frequency is reduced by a few per cent.

For readers who require an accurate clock, instead of one with an alarm, the enclosed circuit could be included in the original design using approximately the same number of components and occupy the same amount of area as the alarm.

The circuit of the crystal oscillator is shown in Fig. 1. The 100kHz crystal operates in the parallel mode and the 60pF trimming capacitor in series with the crystal is adjusted to give exactly 100kHz. A convenient frequency standard for this adjustment is the B.B.C. Radio 2 carrier frequency of 200kHz.

An oscilloscope is triggered from the 100kHz crystal oscillator and the 200kHz waveform is displayed on the screen. The 60pF trimmer is then adjusted for minimum horizontal shift of the waveform.

The oscillator is followed by seven divider stages where the frequency of pulses is reduced to one every minute, see Fig. 2. The first six of these dividers are decade counters in the form of integrated circuits and the seventh stage is a divide by 6 integrated circuit.

For setting the clock to exactly the correct time,

the Greenwich time signal can be used. On the last of the six "pips" the clock can be switched on and adjusted to read the correct time. If a clock with seconds indication has been constructed, then the output from IC5, which has a frequency of IHz, can be fed to the input neglecting IC6 and 7.

The actual accuracy obtained with the prototype was the loss of only I second per week. After running for a month in a room in which the ambient temperature varied by about 10°C, the clock was found to be only 4 seconds fast.

J. A. Wise,

Watford.

+5-0V

R2
0-60pF

C2
0-60pF

TR1
0C44

C4
4700pF

OV

Fig. 1. Circuit diagram of the crystal oscillator

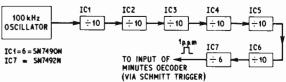


Fig. 2. Block diagram showing arrangement of oscillator and divider stages

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B60	10	7 Watt Zen Mixed Volta		50p
H6	40	250mW. Ze DO-7 Min. 0		50p
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B99	200				stage 13p ounted by	
H4	250	Mixed R Approx. weight	esisto quan	ors. Po	stage 10p unted by	50p
H7	40	Wirewood types and	and P	lesistor les. Po	s. Mixed stage 8p	50p
Н8	4	BY 127 Si 1000 PIV			stic	50p
H9	2	OCP71 L Photo Tr	ight ansis	Sensitiv tor	re .	50p
HI2	20	NKT155 brand ne	259 C	Germ. o	liodes. rance	50p
нів	10	OC71/75 type PNF	unco Ger	ded bla	ck glass	50p
H19	10	OC81/81				50p
H28	20	OC200/I uncoded	/2/3 P T O-5	NP Sili	con	50p
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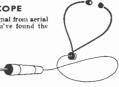
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> Practical Electronics October 1971

# SELECTION FROM OUR POSTBAG

Correspondents wishing to have a reply must enclose a stamped addressed envelope. We regret we are unable to guarantee a reply on matters not relating to articles published in the magazine. Technical queries cannot be dealt with on the telephone.

### **Build or bust!**

Sir-Of date I have read with interest letters from the readers of your esteemed magazine in the Readout section, concerning the state of "chaos" brought about by the unavailability of special com-ponents for some of the projects that are published in your magazine.

It surprises me very much that your readers "at home" (the U.K.) like the Old Mariner, keep wailing "water, water everywhere but not a drop to drink." What would some of these gentlemen do if they had to hunt for i-c's or special components in this country?

A group of us interested in such projects have evolved a way around this problem by forming a Club and when we see that we have an order to make it "well worth the while" of the various mail-order houses that advertise with your magazine. I send off an order for

the required parts.
Sometimes however, we do come across a special relay or switch that cannot be supplied or is out of stock, or by writing to the manufacturer we cannot get a "one-off" job. It is here that we cannibalise parts from old equipment which have been junked, to the extent of rebuilding some of the switches to

suit our needs.

It seems that your modern readers want things laid out on the table for them to go ahead and build some piece of equipment that takes their fancy. Why not improvise? If a particular transistor is not available or is obsolete, why not find an alternative? After all, we are in this hobby to enjoy ourselves, not to make a profit like the component dealers (who, must, if they want to keep their business from running into the red). What greater satisfaction in making a piece of quipment that requires something special through improvisation rather than frowning that "that damned thing isn't going to work without that thingamaile"? that thingamajig'

Now before some keen reader bops me for saying that, I would suggest that snould your magazine wish to co-operate, and I am sure

it has done all it can for its readers these past many years, is to have a Swap-Box column whereby readers could exchange parts with each other (without asking for monetary remunerations) and thus solve some of their problems if not all of them.

Supplying home experimenters is big business in the U.S.A. and why dealers in the U.K. do not try to capture this large source of revenue is something very surprising!! Of course, dealers that do extend certain services to experimenters beyond the call of service will note that they have a customer who chooses to deal with no one else in the long run. I hope that some enterprising mail-order house in the U.K. finds a practical solution to this tangled problem.

Keep on publishing your specialised designs. "WE SHALL BUILD THEM OR BUST".

S. M. Sharifi, Teheran, Iran.

### **American way**

Sir-The amateur is very well catered for in this country. Early this year I received the latest catalogues FREE from the mail-order component houses I buy parts from

on occasion.

Newark's catalogue for 1971 runs to 736 pages; Allied Radio Shack's to 460; Lafayettes to 467. It is impossible to detail their offerings which run the whole gamut from individual components of every conceivable kind through brand name kits to commercial equipment, hi-fi systems and so on, and on. I would almost say that there is no component available to the professional engineer which the amateur cannot purchase by mail. He must be prepared to pay for it though!

In Cincinnati there is also a branch of a local Ohio concern, Hughes Peters, and they have an across the counter service daily and Saturday mornings. Parts immediately available here are ordered from their suppliers and the

customer is advised by phone when they arrive. There is no extra charge for this service,

Mail orders from the other firms are processed in about fourteen days. A sign of the times, however, has been an increase in the minimum value of a mail order that these firms will handle.

Some of the firms also run their own hire-purchase plans, which cover components as well as kits and ready to use equipment.

Firms offer quantity discounts, these vary with quantity and the kind of item. Generally it pays to buy as large a number as possible, as for small items savings can be substantial.

There are also firms specialising in selling complete ready-to-assemble kits for the more sophisticated projects published in the popular magazines, and also special components that may be called for.

I expect that the hobbiest here has more to splurge on bits than his UK counterpart and his potential business attractive to the component suppliers. Having the cash and an American philosophy he will tend to do the job right and not save pennies adapting old junk if the correct part can be purchased.

L. Huggard, Cincinnati, U.S.A.

### **New hobby**

Sir—At the moment, (having just completed the first part of the "War Games Computer" successfully), I am rather keen on constructing similar projects, such as the "Operation Seasearch.

I am hoping you can give me the date of the magazines in which it appeared and where I might obtain them? Also any similar projects which might have been shown in your magazine?

I must confess that this month's is the first of your magazines I have bought, for although very interested in electronics, I have up until now mostly constructed radios.

Needless to say, from now on I shall place a regular order for PRACTICAL ELECTRONICS, which has given me a "start" on a wonderful new hobby.

Hope to hear from you soon.

N. Early, Langport, Somerset.

"Operation Seasearch" appeared in the December '70 issue; "Submarine Chaser" in February this year.

We regret that all back numbers of our magazine are no longer available. We can only suggest you try your local technical or reference library.

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100 μF   15 volts	27 μF 50	volts	12	μF	35	volts	
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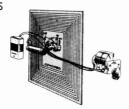
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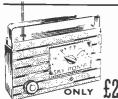
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Ernest Turner Ernest Turner	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2¾in dia. 270° Movement/Centre zero Cir	eniar enlar	4	8-25 8-00 4-25 3-00
Ernest Turner	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2¾in dia. 270° Movement/Centre zero Cir	eniar enlar	8	3-25 3-00 1-25 3-00
Ernest Turner Sangamo-Weston Illuminated Meter	50-0-50tA edgewise 2½in scale 2703 Movement/Centre zero cir 0-5-0-0-5mA 2‡in dia. 2703 Movement/Centre zero Cir 1-0-1mA 3‡in dia. 500tA F.S.D. 4‡in × 3‡in	eniar enlar	8	3-25 3-00 1-25 3-00 4-25 3-90
Ernest Turner Sangamo-Weston Illuminated Meter Sangamo Weston	50-0-50uA edgewise 21in scale 270 Movement/Centre zero cir 0-5-0-0-5mA 21in dia 270 Movement/Centre zero Cir 1-0-1mA 31in dia 500uA F.S.D. 41in × 31in	eular eular	4	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner Sangamo-Weston Illuminated Meter Sangamo Weston	50-0-50tA edgewise 2½in scale 2703 Movement/Centre zero cir 0-5-0-0-5mA 2‡in dia. 2703 Movement/Centre zero Cir 1-0-1mA 3‡in dia. 500tA F.S.D. 4‡in × 3‡in	eular eular	4	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.	50-0-50tA edgewise 2½in scale 270 'Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270 'Movement/Centre zero Cir 1-0-1mA 3½in dia 500tA F.S.D. 4½in × 3½in 50tA F.S.D. 4½in × 3½in assorted meters of different shap	eular eular es/sizes/	4 4 8 4 8	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.	50-0-50uA edgewise 21in scale 270 Movement/Centre zero cir 0-5-0-0-5mA 21in dia 270 Movement/Centre zero Cir 1-0-1mA 31in dia 500uA F.S.D. 41in × 31in	eular eular es/sizes/	moveme	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large mumber of in stock.  SOUND-TO-LIGHT MOD Single Channel 750W mod	50-0-50tA edgewise 2½in scale 270 Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270 Movement/Centre zero Cir 1-0-1mA 3½in dia. 500tA F.S.D. 4½in × 3½in 500tA F.S.D. 4¼in × 3½in f assorted meters of different shap ULES SUITABLE FOR DISCOTHE	eular eular es/sizes/	\$ 4 \$ 4 \$ 5 \$ 4 \$ 5 \$ 4 \$ 5 \$ 5 \$ 6 \$ 6 .00	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mod Three Channel Model	50-0-50tA edgewise 2½in scale 270 'Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270 'Movement/Centre zero (ir 1-0-1mA 3½in dia 500tA F.S.D. 4¼in × 3¼in 50tA F.S.D. 4¼in × 3¼in assorted meters of different shap ULES SUITABLE FOR DISCOTHE	eular eular en/sizes/	8 4 5 4 6 6 6 6 6 6 6 1 .	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mod Three Channel Model	50-0-50tA edgewise 2½in scale 270 Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270 Movement/Centre zero Cir 1-0-1mA 3½in dia. 500tA F.S.D. 4½in × 3½in 500tA F.S.D. 4¼in × 3½in f assorted meters of different shap ULES SUITABLE FOR DISCOTHE	eular eular es/sizes/	\$ 4 \$ 4 \$ 5 \$ 4 \$ 5 \$ 4 \$ 5 \$ 5 \$ 6 \$ 6 .00	3.25 3.00 1.25 3.00 4.25 3.90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number o in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P	50-0-501A edgewise 2½in scale 270 Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270 Movement/Centre zero Cir 1-0-1mA 3jin dia 500A F.S.D. 4jin × 3jin 500A F.S.D. 4jin × 3jin f assorted meters of different shap ULES SUITABLE FOR DISCOTHE let	enlar enlar en/sizes/	ETC. Each £ 6-00 35-00 35-00	3-25 3-00 1-25 3-00 4-25 3-90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number o in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P	50-0-50tA edgewise 2½in scale 270 Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270 Movement/Centre zero Cir 1-0-1mA 3½in dia 500tA F.S.D. 4¼in × 3½in f assorted meters of different shap ULES SUITABLE FOR DISCOTHE 101 COMPONENTS 2% T.R.5 Complete range	eular es/sizes/	ETC. Each £ 6-00 18-00 6-00	3-00 1-25 3-00 1-25 3-00 4-25 3-90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD!  Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270° Movement/Centre zero (ir 1-0-1mA 3½in dia. 500uA F.S.D. 4¼in × 3¼in 500uA F.S.D. 4¼in × 3¼in assorted meters of different shap ULES SUITABLE FOR DISCOTHE itel rojectors, complete with wheel COMPONENTS 2% T.R.5 Complete range 1 off 50 each, 100 off 3¼p each,	ewar es/sizes/ QUES, 1	ETC. Each £ 6-00 18-00 6-00	3-00 1-25 3-00 1-25 3-00 4-25 3-90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Mullard Electrolytic Capacitors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270° Movement/Centre zero Cir 1-0-1mA 3½in dia. 500uA F.S.D. 4¼in × 3¼in 500uA F.S.D. 4¼in × 3¼in assorted meters of different shap ULES SUITABLE FOR DISCOTHE itel rojectors, complete with wheel COMPONENTS 2% T.R.5 Complete range 1 of 59 each, 100 off 3½ each. Complete range always in stock Complete range always in stoc	emar cular  es/sizes/ QUES, 1	ETC. Each £ 6-00 18-00 6-00	3-00 1-25 3-00 1-25 3-00 4-25 3-90
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Delyester Capacitors Mullard Polyester Capacitors Mullard Polyester Capacitors Lemco Silver Mica Capacitors	50-0-50tA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270° Movement/Centre zero Cir 1-0-1mA 3½in dia. 500tA F.S.D. 4½in × 3½in 500tA F.S.D. 4½in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 161 rojectors, complete with wheel 176 COMPONENTS 2% T.R.5 Complete range 1 off 59 each, 100 off 3½9 each, 100 of	eular eular es/sizes/ es/sizes/ QUES, 1	ETC. Each 2 6-00 18-00 6-00 in sto	8-25 3-00 4-25 3-90 4-25 25 4-75 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Mullard Electrolytic Capacitors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2½in dia. 270° Movement/Centre zero Cir 1-0-1mA 3½in dia. 500uA F.S.D. 4½in × 3½in 500uA F.S.D. 4½in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 161  COMPONENTS 2% T.F.S. Complete range 1 off 5p each, 100 off 3½p each 200 off 3½p eac	eular eular es/sizes/ es/sizes/ QUES, 1	ETC. Each 2 6-00 18-00 6-00 in sto	8-25 3-00 4-25 3-90 4-25 25 4-75 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors  Mullard Electrolytic Capacitors Mullard Polyester Capacitors Lemco Silver Mica Capacitors Polystyrene Capacitors Polystyrene Capacitors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 500uA F.S.D. 4½in × 3½in 500uA F.S.D. 4½in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 101 of 1500uA F.S.D. 4½in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 102 of 1500uA F.S.D. 4½in × 3½in 1000uA F.S.D. 600uA F.S.D.	eniar	ETC. Each £ 6.00 18-00 35-00 in sto	8-25 3-00 4-25 3-00 4-25 3-90 4-25 9-7-8 9-8 9-8 9-8 9-8 9-8 9-8 9-8 9-8 9-8 9
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors  Mullard Electrolytic Capacitors Mullard Polyester Capacitors Lemco Silver Mica Capacitors Versewound Resistors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 3jin d	eniar	ETC. Each £ 6.00 18-00 35-00 in sto	8-25 3-00 4-25 3-00 4-25 3-90 4-25 9-7-8 9-8 9-8 9-8 9-8 9-8 9-8 9-8 9-8 9-8 9
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Polyester Capacitors Mullard Polyester Capacitors Folystyrene Capacitors Polystyrene Capacitors Semiconductors  Semiconductors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 500uA F.S.D. 4½in × 3½in 500uA F.S.D. 4½in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 101 of 1500uA F.S.D. 4½in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 102 of 1500uA F.S.D. 4½in × 3½in 1000uA F.S.D. 600uA F.S.D.	QUES, 1	ETC. Each	1.25 3.00 1.25 3.00 4.25 3.90 4.25 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Mullard Electrolytic Capacitors University of the Capacitors Wirewound Resistors Semiconductors  Semiconductors	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 3jin d	eniar	ETC. Each  2 6-00 13-00 6-00 in sto	1.25 3.00 1.25 3.00 4.25 3.90 4.25 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Holyatyrene Capacitors Lemco Silver Mica Capacitors Wirewound Resistors  Semiconductors  10° DISCOUNT On any cash sa	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 3jin d	eniar	ETC. Each  2 6-00 13-00 6-00 in sto	1.25 3.00 1.25 3.00 4.25 3.90 4.25 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large mumber of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Divester Capacitors Lemco Silver Mica Capacitors Lemco Silver Mica Capacitors Volvatyrene Capacitors Wirewound Resistors  Semiconductors  10° o DISCOUNT On any cash sa	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 3jin d	ewisizen/siz	ETC. Each g 6-00 in stc Thyrist Thyrist Place Thyrist Place Thyrist Thyrist Thyrist Thyrist Thyrist	1.25 3.00 1.25 3.00 4.25 3.90 4.25 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6 in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Mullard Polyester Capacitors Lemos Silver Mica Capacitors Very Mica Capacitors Very Mica Capacitors Very Mica Capacitors Very Mica Capacitors Polystyrene Capacitors Very Mica Capacitors On any cash sa  C.T  267 ACTON LA	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero Cir 1-0-1mA 3jin dia. 350uA F.S.D. 4¦in × 3½in 50uA F.S.D. 4¦in × 3½in assorted meters of different shap ULES SUITABLE FOR DISCOTHE 101 and 101 an	ewisizen/siz	ETC. Each g 6-00 in stc Thyrist Thyrist Place Thyrist Place Thyrist Thyrist Thyrist Thyrist	1.25 3.00 1.25 3.00 4.25 3.90 4.25 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Lemco Silver Mica Capacitors Wirewound Resistors  Wester Capacitors Wirewound Resistors  10°c, DISCOUNT On any cash sa C.T  267 ACTON LAM Nearest Underground—Chievic	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero cir 1-0-1mA 3jin dia. 3jin d	ewisizen/siz	ETC. Each g 6-00 in stc Thyrist Thyrist Place Thyrist Place Thyrist Thyrist Thyrist Thyrist	1.25 3.00 1.25 3.00 4.25 3.90 4.25 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Lemco Silver Mica Capacitors Wirewound Resistors  Wirewound Resistors  10°c, DISCOUNT On any cash sa C.T  267 ACTON LAM Nearest Underground—Chiewic Acton T Bus Routes E3, 88, 207, 15, 7, 18  Bus Routes E3, 88, 207, 15, 7, 18	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero cir 1-0-1mA 3jin dia. 3jin d	ques, il always control of the contr	EETC. Each \$ 6-00 18-00 in stc Thyristers, Pho	3-25 3-00 4-25 3-90 4-75 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD' Single Channel 750W mor Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Electrolytic Capacitors Lemco Silver Mica Capacitors Wirewound Resistors  Wirewound Resistors  10°c, DISCOUNT On any cash sa C.T  267 ACTON LAA Nearest Underground—Chiswic Acton T Bus Routes E3, 88, 207, 15, 7, (Please note: As yet we do not call at the above address).	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero cir 1-0-1mA 3jin dia. 3jin d	always  Com Blocks, 1  10% Ivertiser  1994 62	Each g and a stock of the stock	3-25 3-00 4-25 3-90 4-75 ents
Ernest Turner  Sangamo-Weston Illuminated Meter Sangamo Weston We also have a large number of in stock.  SOUND-TO-LIGHT MOD  Single Channel 750W mod Three Channel Model 150W Liquid Oil Wheel P Extra Wheels 6in dia.  Metal Oxide Resistors Mullard Polyester Capacitors Mullard Polyester Capacitors Lemco Silver Miclo Capacitors Polystyrene Capacitors Witewound Resistors  Semiconductors  10° DISCOUNT On any cash sa C.T  267 ACTON LA Nearest Underground—Chiswich Russel Capacitors Control Chiswich Con	50-0-50uA edgewise 2½in scale 270° Movement/Centre zero cir 0-5-0-0-5mA 2jin dia. 270° Movement/Centre zero cir 1-0-1mA 3jin dia. 3jin d	always C. Com Blocks, Zen 10% 10% 10% 10% 10% 10% 10% 10% 10% 10%	EEC.	3-25 3-00 3-00 3-00 4-25 3-90 4-75 ents

LS	T	FOR S		S, NEWN TEXAS,		ET, IR, I RANTI.	RCA GE
	37 p 25 p 25 p	BY100 BYX10 BYZ10	20p 15p 40p	NKT10339 NKT10419 NKT10439	9 25p	IN4005 IN4006 IN4007	12p 15p 20p
AC107 AC126 AC127 AC128 AC151 AC176 AC187	20p 12p 25p	BYZIZ BYZIZ BZY88	30p 20p	NKT1051 NKT2032	9 22p	IN4148 2G302 2G371	7p 19p 15p
ACIB7 ACIB8 ACYI7 ACYI8	30p 30p 29p	C3V3	15p 15p 15p	NKT8011 NKT8011 NKT8011	l 67p 2 83p 3≰I-00	2G374 2N174	25p 80p
	20p 20p 19p	C3V9 C4V3 C4V7 C5V1 C5V6	15p 15p 15p	NKT8021 NKT8021 NKT8021	75p 75p 75p	2N385A/ 2N388A 2N404	75è 23p 15p
ACY20 ACY21 ACY22 ACY40 ACY41	19p 19p	C6V2	15p 15p 15p	NKT8021 NKT8021 NKT8021	4 75p 5 75p 6 75p	2N696 2N697 2N698 2N706	17p 30p 10p
ACY41 AD140 AD149	15p 55p 57p	C6V8 C7V5 C8V2 C9VI	15p 15p	OA5 OA10 OA47	20p 25p 8p	2N706A 2N708	12p 16p
AD161 AD162 AF106	37p 37p 24p	C10 C11 C12	15p 15p 15p	OA70 OA73 OA79	8p 8p 8p	2N711 2N711A 2N911	37p 37p 50p
AFII4 AFII5 AFII6	25p 25p 25p	C13 C15 C16	5p  5p  5p	OA81 OA85 OA90	8p 8p 8p	2N914 2N918 2N1090	20p 42p 30p
AF117 AF118 AF124	25p 44p 25p	C18 C20 C22	15p 15p 15p	OA91 OA95 OA200	8p 8p 10p	2N1091 2N1131 2N1132	33p 30p 30p
AF126 AF139 AF186	17p 33p 40p	C9VI C10 C11 C12 C13 C15 C16 C20 C22 C24 C27 C30	15p 15p 15p	OA202 OC19 OC20	10p 37p 97p	2N1302 2N1303 2N1304	20p 20p 25p
AF239 . A5Y26 A5Y27	37p 25p 30p	MJE520 MJ480	45p 75p 97p	OC22 OC23 OC24	47p 60p 60p	2N1305 2N1306 2N1307	25p 30p 30p
ASY28 ASY29 A5Z21 AUY10	22p 30p 37p £1.50	MJ481 MJ490 MJ491	£1-25 £1-00 £1-35	OC19 OC22 OC23 OC24 OC25 OC26 OC28 OC29 OC35	37p 33p 60p	2N1308 2N1309 2N1507 2N1613	34p 31p 23p 22p
	8p	MPF102 MPF103 MPF104	37p 37p	OC35 OC36	75p 50p 63p	2N1711 2N2147	25p 82p
BC107 BC108 BC109 BC147 BC148 BC149	12p 12p 15p	MPF105 NKT12 NKT12! NKT12	40p	OC36 OC41 OC42 OC44	25p 30p 15p 15p	2N2148 2N2160 2N2368	63p 62p 17p 17p
BC148 BC149 BC158 BC167	15p 15p 17p	NKTI2	3 25p 5 26p	OC42 OC44 OC45 OC71 OC72	15p 23p	2N2369 2N2369A 2N2646 2N2904	20p 50p 44p
BC169	p   10 p   19 p	NKT210 NKT21 NKT21	25p	OC72 OC75 OC76 OC77 OC81 OC81D OC81Z	23p 25p 40p 23p	2N2904A 2N2905 2N2905A	49p 65p 75p
BC182 BC182L	12p 10p	NKT21	3 25p 4 23p	OCBID OCBIZ	20p 55p 25p	2N2906A 2N2906A 2N2926 a	44p 54p
BC183L BC184	9p 15p 15p	NKT21	5 46p 7 50p	OC82 OC82D OC83 OC84	15p 23p	colours 2N3053	10p 25p
BC169C BC182L BC183L BC183L BC184L BC1212 BC212L BC212L BCY30 BCY33 BCY33 BCY33 BCY33	1/p 12p 25p	NKT21 NKT22 NKT22	9 25p 3 27p	OC84 OC139 OC140 OC170 OC270 OC200 OC201 OC202 OC203 OC204 OC205 OC206 OC207 OC771/M ORP12	25p 35p 25p	2N3054 2N3055 2N3702 2N3703	63p 75p 11p 10p
BCY31 BCY32 BCY33	48p 50p 20p	NKT22! NKT22! NKT23!	21p	OC171 OC200 OC201	30p 37p 47p	2N3704 2N3705 2N3706	IIp IOp 9p
BCY3B	25p 30p 19p 37p	NKT238 NKT239 NKT240	9 13p 23p	OC202 OC203 OC204	63p 37p 40p	2N3707 2N3708 2N3709	lip 7p 9p
BCY70 BCY71 BCY72 BD121	37p 16p £1·10	NKT24 NKT24: NKT24:	1 21p 2 15p 3 56p	OC205 OC206 OC207	65p 75p 75p	2N3710 2N3711 2N3819	9p 9p 35p
BD124 BDY20	£1.10 £1.03 £1.05	NKT24 NKT24! NKT26	4 17p 5 17p 1 21p	ORP60	600	2N3820 2N3826 2N4058	60p 30p 17p
BF115 BF163 BF167	25p 40p	NKT267 NKT27	2 19p 4 21p 1 18p	ORP61 P346A ST140	40p 19p	2N4060 2N4061 2N4062	20p 20p 20p
BF173 BF177 BF178	30p 25p 52p 37p	NKT27; NKT27; NKT27;	2 17p 4 18p 5 23p	STI4I TD716 TiP31A	60p	2N4284 2N4287 2N4289	15p 15p 15p
BF180 BF181 BF184	37p 25p	NKT279 NKT28 NKT301 NKT304	29p	TIP32A TIS88A V405A	74p 45p 46p	2N4871 2N5254 3N84	40p 45p £1-30
BF1B5 BF194 BF195	25p 17p 15p	NKT30 NKT35 NKT40	75p	ZTX108 ZTX300 ZTX302	11p 13p 18p	3N128 3N140 3N141	69p 76p 73p
BF200 BFX13 BFX29	35p 25p	NKT40 NKT40 NKT40 NKT40	65p 65p 60p 79p		18p 27p 11p	3N 152 40250 40309	86p 55p 33p
BFX84 BFX85	31 p 26 p 34 p 25 p	NKT406 NKT426 NKT45	62n	ZTX304 ZTX314 ZTX320 ZTX330 ZTX500 ZTX501	30p 18p 16p	40310 40312 40320	45p 48p 36p
BFX86 BFXB7 BFX88 BFY50 BFY51	30p 25p 23p	NKT45 NKT45 NKT60 NKT60	) 54n	ZTX502 ZTX503 ZTX504	16p 20p 17p 40p	40360 40361 40362	43 p 48 p 58 p
I RFY52	19p 20p	NKT67	4F 30p	IN34A IN60 IN64	20p 20p	40406 40407 40408	56p 39p 51p
BFY53 BFY90 BSX19 B5X20	67p 16p	NKT670 NKT671 NKT711 NKT711	3 29p	IN82A IN87A IN914	47p 23p 7p	40409 40468A 40600	54p 35p 58p
B5X20 B5X21 B5Y27 BSY29	37p 20p 25o	NKT734 NKT736 NKT77	4 26p 5 32p 3 25p	IN4001 IN4002 IN4003	7p 7p 10p	40601 40602 40603	55p 49p 49p
BSY95A	15p EXAM	NKT78 PLES OF	I 29p OURBU	IN4004 J <b>LK QUA</b> 1	TITY	40673 PRICES:	90p
25 + 100	07 & 9 Sie 10p; 100 00 pcs £6 per 100	mens + 8p; 20	25 + 28p; OF	Siemens 100 + <b>24</b> p 1712	25 +	161/2 Sieme PN—PNP Pa 50p; 100+ per pair	ir
25 →	108 Sieme 9p; 100 -	+ 7n:	Cadmiun	3 Valvo) n Sulphide Cell 100 + 30p	25 +	C176 Siemer 13p; 100 +	l lp
l	per 100 1055 5iem		BY 127	Mullard 100 + 15p;	25+	187/8 Sieme 32p; 100+ per pair	27p
AF 25 + 2	139 Sieme 5p; 100	ens +22p	2N3819 25+21p;	Texas Fet 100 + 18p	25 +	47 & 9 Lock 8p; 100 + 1000 + 5p	7p;
LST	FOR	QUA	LITY	AND	SER	/ICE i	

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Part	No. Description	Equal	1-24	25-99	00 up		No. Description				100 up				1-24	25-99	100 up
FLH		to				FLH		to						to			
101	Quadruple 2-input					271	Hex inverter with					FLJ					
101	NAND gate	7400	20p	14-	14-	271	open collector					141	Dual D-type edge	7.47.			
1111	Triple 3-input NAND	7400	ZUP	16p	ł4p		output	7405	25p	21p	18p	151	triggered flip-flop Quad bistable latch	7474		38p	
	gate	7410	20p	16p	140	281	BCD to decimal	7403	A-SP	Z.P	тор	161		7475	45p	40p	
121	Dual 4-input NAND	7410	AVP	тор	IPP		decoder TTL						Decade counter	7490	80p	67 p	
141	gate	7420	20p	16p	1.4-		output	7442	£1-16	94p	81p	171	Divide-by-12 counter		85p	71p	
131	8-input NAND gate	7430	20p		14p	291	Quadruple 2-input					181	4-bit binary counter	7493	80p	67p	57p
141		/430	ZUP	16p	14p		NAND gate with					191	4-bit shift register	7495	87p	72p	62p
171	Dual 4-input NAND buffer	7440	24p	20p			open collector out-					201	Synchronous up down	1			
151		/ 110	44p	20p	17p	341	Quadruple 2-input	7403	20p	16p	14p		4-bit decade				
131	Expandable dual 2-wide 2-input					341	exclusive-OR						counter with one				
	AND-OR-INVERT						element	7486	33p	27 p	23p	211	line mode control	74190	₹1.80	£1-48	£1-27
	gate	7450	20p	160	14p	351	Schmitt Trigger	7413	35p	29p		211	Synchronous up down 4-bit binary counte	1			
161	Dual 2-wide 2-input	, 150	Tob	, op	тър	361	Excess 3 to decimal			2.0	-50		with one line	r			
	AND-OR-INVERT						decoder	7443	£1-45	£1-20	£1.08			74191	£1.80	41-4R	63-27
	gate	7451	20p	16p	140	371	Excess 3 gray to					221	8-bit shift register	7491A			
171	Expandable 4-wide					381	_ decimal decoder	7444	£1.45	£1 20	80-13	231	4-bit shift register	7494	£1-13		
	2-input AND-OR-					381	Quad 2-input positive AND gate Totem					241	Synchronous up down	1		•	
	INVERT gate	7453	20p	16p	14p		pole output	7408	25p	21-	10		4-bit decade				
181	4-wide 2-input			-		391	Quad 2-input positive		Tob	21p	18p	251		74192	£1.74	£1:45	£1-25
	AND-OR-INVERT						AND gate open					231	As above—binary counter	74103		41.45	£1-25
	gate	7454	20p	16p	14p		collector	7409	25 p	210	18p	261	5-bit shift register				£1 05
191	Quadruple 2-input					FLY	_		- •			271	Dual J-K master-slave	7470	E1 40	11.77	E1.03
	NOR gate	7402	20p	16p	14p	101	Dual 4-input						flip-flop with prese				
201	Quadruple 2-input						expander	7460	20p	16p	14p		and clear	74107	52p	43 p	36p
	NAND gate					FLJ 101	J-K flip flop	7.170	4-			108	Dual quadruple				
	with open collector output	7401	20p	14-	14p	111	J-K flip flop J-K master-slave	7470	45p	37 <sub>P</sub>	32p		bistable latch	74100	£1-64	£1:37	£1:17
211	Hex inverter	7404		16p			flip-flop	7472	32 p	27 <sub>P</sub>	23 <sub>p</sub>	FLK 101	M				
221	Gated full adder		25p	2ip	18p	121	Dual J-K master-	1412	31p	∡/ p	73b	101	Monostable multi- vibrator	74124	40	40	34.
		7480	67p	56p	48p		slave flip-flop	7473	45 p	40p	35p	FLL	VIDIACOF	74121	48p	40p	34p
231		7482	87 p	73p	62p	131	Dual J-K master-					101	BCD to decimal				
241	Four-bit binary	7.00					slave flip-flop with						decoder and nixie				
	full adder	7483	£1:32	£1-16:	£1.00		preset and clear	7476	45p	40p	36p			74141	£1-22	£1:02	87p
					VDEC	MAY	DE MIVED TO O						_				

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NEW PRODUCT!!	0·1 0·15 0·22	***	4p 5p 5p
(Siemens Tantalum Bead	0.33		. 7p
Capacitors)  Mfd. Voltage Mfd. Voltage	0.47		8p
1 35 2·2 16 22 35 4·7 16	1.0		14p
47 35 10 16	2.2		24p
1 35 15 16 2-2 35 22 16			
4-7 35 33 10	Mullard	Electrolytic	C437 series
10 25 27 6.3	Mfd. 250	Volt. Wkg. 16	, 9p
15 20 47 6-3	400	16	12p
Epoxy encapsulated miniature sinter	640	6  6	15p 18p
Tantalum Electrolytics—polarized Size example : 10mfd 16v	160 250	25 25	9p
4.5 × 17.5 mm.	400	25	12p 15p
All one price: 12p each; 25 pieces 1 type 10p each.	640 100	25 40	18p 9p
	160	40	12p
BZY88 SERIES ZENERS 400mW	250 400	40 40	15p  8p
All voltages available	-		
3·3 to 33 Volt 25 + 12p 100 + 10p	Mullard :	Sub-Miniatus	e Ceramic
500 + 9p 1000 + 8p	Plate		C333 series
SPECIAL OFFER IN4000	63 volt w 220pf (usu	orking. Rang Ial pref. value	
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P.i.y. 1-49 50 + 100 + IN4001 50 070 060 050	-		
IN4002 100 070 065 060	ture Elec	TORS—Mull	ard Minia- C426 series
IN4003 200 090 085 070 IN4004 400 100 090 080	Mfd.	Volt Wkg.	
IN4005 600 120 100 090 IN4006 800 140 130 110	2·5	16 16	8p 6p
IN4007 1000 190 150 120	20 40	16	6р
p.i.v 500 + 1000 + IN4001 50 045 040	80	16	6р 6р
IN4002 100 055 045	l -6 6-4	25 25	8p 6p
IN4003 200 060 050 IN4004 400 070 060	12.5	25	6р
IN4005 600 075 070	25 50	25 25	бр бр
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voltage rated item at no extra	8 16	40 40	6p 6p
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	LINEAR	AND DI	GITAL ICS		
R.C.A.		Fairchile		12-24	25+
CA3004	£1-80	µL900	40 <sub>D</sub>		32 <sub>D</sub>
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(DIL high gain	•	PHASE	LOCKED L	OOP 45	98
op-amp)		LST break	the price b	arrier on th	is fantastic
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(equiv. \$N72741P)		stockda	ta IOp.		
			- 1971 - P. C.	-	
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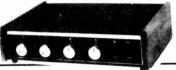
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A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors including Silicon Transistors in the first five stages on each channel resulting in even lower noise 14 transistors including Silicon Transistors in the first tree stages on each channel resulting in even lower noise level with improved sensitivity. Integrated pre-amp with Bass, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridges. Output stage for any speakers from 5 to 15 nhms. Compact design, all parts supplied including drilled metal work, high quality ready drilled printed circuit board, attractive front panel, knobs, wire, solder, nuts, botts—no extrast ob by. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification: Power output 14W r.ns., per channel into 5 ohns. Frequency response = 3dB 12-30,000Hz. Sensitivity better than 80mV into 1M Oz. Fullpower bandwidth ± 3dB 12-15,000Hz. Bass boost approx. to ±12dB. Treble cut approx. to -16dB. Negative feedback 18dB over main amp. Power requirements 35V at 1-0 aup. Overall size—12° wide 8° deep 22° high. Fully detailed 7-page construction manual and parts list free with kit or send 18p plus large A.E.

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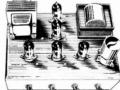
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to follow each other.

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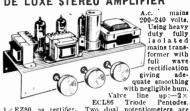
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rectification giving adequate smoothing with negligible hum.

Valve line up:—2×

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2613 35p 2N5232A 30p A8Y26 25p BFX1 2614 30p 2N5245 46p A8Y27 374p BFX2	2219 MJ 440
2646 521p 2N5246 421p A8Y28 271p BFX3 2696 321p 2N5249 671p A8Y29 271p BFX4	30p 100400 9/1p 0C84 25p 371n M1481 21.25 0C84
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2713 271p 2N5267 22-621 ASV51 281p BFX8	
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2923 15p 2N5365 47ip BC113 15p BFY1 2924 15p 2N5366 32ip BC115 15p BFY1	32ip MPF105 37ip ORP61 50p 2iin × 3iin 17ip 20p WIRE-WOUND RESISTORS
2925 15p 2N5367 574p BC116A 15p BFY2 2926 2N5457 374p BC118 10p BFY2	21.60 MP83638 32*p   P346A 22*p   24*in × 5*in 21*p 24*p   2.5 watt 5% (up to 270 ohm
Green 14p 28005 75p BC121 20p BFY2	45p NKT124 424p TIP30A 60p 32 in $\times$ 5 in 274p 274p 5 watt 5% (up to 8.2k $\Omega$ only), 10
Orange 124p 28102 50p BC125 20p BFY2	20p NKT126 27 p TIP 32A 75p Vero Pins (bag of 36), 20p. 12 p.
3011 30p 28103 25p BC126 20p BFY2 3014 32pp 28104 25p BC140 37pp BFY3	50p NKT128 27 p TIP33A 21-05 Vero cutter, 45p; Pin insertion 50p NKT135 27 p TIP34A 22-05 Tools (0-1 and 0-15 matrix) at 55p. POTENTIOMETERS
3054 46n 28502 35n RC148 10n BFY4	50p NKT137 32ip T1834 62ip Carbon:
3055 620 28503 2710 RC140 10 DFY 3	23p NKT211 30p T1843 27p TEA SINKS Log, and Lin., with switch, 25p.
3133 30p 3N128 70p BC152 17 p BF 13	23p NKT212 30p T1845 10p T0-3 Trans., 47 p. 4.8 × 2 × 1in Twin Ganged Stereo Pots. Lo
2126 0Km 2N141 701m BC158 11p BEV5	A 57 p Nr. 7015 9015 71847 11p 32 p. For 80-1, 2 p. For TO-5,
3390 25p 3N142 55p BC159 12p BFY7 3391 20p 3N143 674p BC160 624p BFY7	30p NKT216 37ip T1849 12ip bp Finned. For TO-18, 5p Finned. PRESETS (CARBON)
3391A 30p 3N152 87 p BC167 11p BFY7	57in NKT217 42in T1850 17in
3393 15p 40050 55p BC168C 11p BPX2	21.85 N. 1225 273 T1852 1231 Cashon Film
	\$1.80   NKT225 22   T1860 22   Larbon Film   22   Wat 5%   1p.   W &   W are   THERMISTORS
3403 221p 40309 321p BC170 121p BRY3 3404 321p 40310 45p BC171 15p B8W4	474p NKT229 30p T1861 20p ( water 5/6, 14p. 20 et les.   R03 (S1C) 212/1
Matching charge (audio transistors of	v. 12 p extra per pair. w M/O 2% 4p. are E12 series. VA3705 87 p
st & Packing 12½p per order. Europe 25p. Commonwealt Prices subject to alteration wit	
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A.C. volts: 12, 120, 480, 1,200.
Amps: 0.012, 0.12, 1.2, 12.
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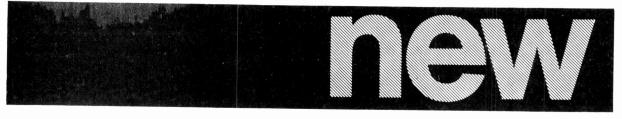


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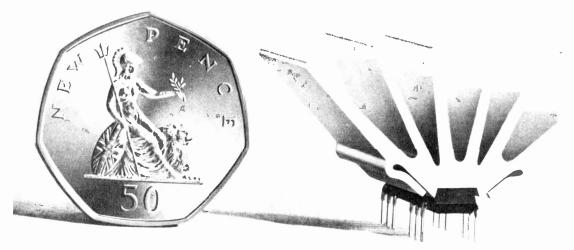
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# Super IC-12



## High fidelity Monolithic Integrated Circuit Amplifier

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor, the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

- 1. Higher power.
- 2. Fewer external components.
- 3. Lower quiescent consumption.
- 4. Compatible with Project 60 modules.
- Specially designed built-in heat sink. No other heat sink needed.
- 6. Full output into 3, 4, 5 or 8 ohms.
- 7. Works on any voltage from 6 to 28 volts without adjustment,
- 8. NEW 22 transistor circuit.

### SINCLAIR GENERAL GUARANTEE

Should you not be completely satisfield with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are available to all Sinclar customers. Output power 6 watts RMS continuous (12 watts peak)

Frequency Response 5 Hz to 100KHz  $\pm$ 

Total Harmonic Distortion Less than 1% (Typical 0.1%) at all output powers and all frequencies in the audio band.

Load Impedance 3 to 15 ohms.

Power Gain 90dB (1,000,000,000 times) after feedback.

**Supply Voltage** 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).

Size 22 x 45 x 28 mm including pins and heat sink

Input Impedance 250 Kohms nominal.

Quiescent current 8mA at 28 volts

With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F,M. tuner etc. Alternatively, for more elaborate systems, modules in the Project-60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Price, inc. FREE printed circuit board for mounting.

£2.98

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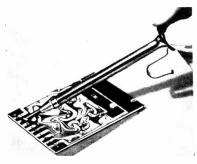


# Sinclair Project 60

### The World's leading range of high fidelity modules

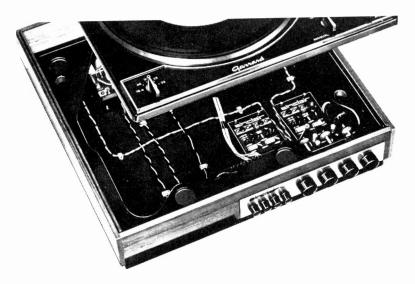






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Project 60 offers more advantage to the constructor and user of high fidelity equipment than any other system in the world.

Performance characteristics are so good they hold their own with any other available system irrespective of price or size.

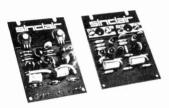
Project 60 modules are more versatile — using them you can have anything from a simple record player or car radio amplifier to a sophisticated and powerful stereo tuner-amplifier. Either power amplifier can be used in a wide variety of applications as well as high fidelity. The Stereo 60 pre-amplifier control unit may also be used with any other power amplifier system, as can the AFU filter unit. The stereo FM tuner operates on the unique phase lock loop principle to provide the best ever standards of sensitivity and audio quality. Project 60 modules are very easily connected together by following the 48 page manual supplied free with all Project 60 equipment. The modules are great space savers too and are sold individually boxed in distinctive white and black cartons. With all these wonderful advantages, there remains the most attractive of all – price. When you choose Project 60 you know you are going to get the best high fidelity in the world, yet thanks to Sinclair's vast manufacturing resources (the largest in Europe) prices are fantastically low and everything you buy is covered by the famous Sinclair guarantee of reliability and satisfaction.

Typical Project 60 applications

The Units to use	together with	Cost of Units	
Z.30	Crystal P U , 12V battery volume control	£4.48	
Z.30, PZ.5	Crystal or ceramic P U volume control etc	£9.45	
2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag P.U., F.M. Tuner, etc	£23.90	
2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P U , F M Tuner, Tape Deck, etc	£26.90	
2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As above .	£34.88	
Z.50, PZ.8, mains transformer	Mic , guitar, speakers, etc , controls	£19.43	
	Z.30, PZ.5  2 x Z.30s, Stereo 60, PZ.5  2 x Z.30s, Stereo 60, PZ.6  2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr Z.50, PZ.8, mains	Z.30 Crystal P U , 12V battery volume control  Z.30, PZ.5 Crystal or ceramic P U volume control etc  2 x Z.30s, Stereo 60, PZ.5 P.U. F M Tuner, etc  2 x Z.30s, Stereo 60, PZ.6 Mains trsfrmr  Z.50, PZ.8, mains  Crystal P U , 12V battery volume control etc  Crystal or ceramic P U volume control etc  Crystal or ceramic or mag P.U. F M Tuner, etc  High quality ceramic or magnetic P U , F M Tuner, Tape Deck, etc  As above   Mic. guitar, speakers, etc.	

### from a simple amplifier to a complete stereo tuner amplifier with Project 60 modules

### Z.30 & Z.50 power amplifiers



The Z 30 and Z 50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z 30 or Z 50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications).

Power Outputs
Z.30 15 watts R.M.S into 8 ohms using 35 volts:
20 watts R.M.S into 8 ohms using 30 volts.
Z.50 40 watts R.M.S, into 3 ohms using 40 volts 30 watts R M S. into 8 ohms using 50 volts

Frequency response: 30 to 300,000 Hz 1dB Distortion: 0.02% into 8 ohms

Signal to noise ratio: better than 70dB unweighted. Inputsensitivity: 250mV into 100 Kohms For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57 mm

7.30

Built, tested and guaranteed with circuits and instructions manual. £4.48

Z.50

Built, tested and guaranteed with circuits and instructions manual £5.48

### Power Supply Units

Designed special for use with the Project 60 system of your choice Use PZ.5 for normal Z 30 assemblies and PZ 6 where a stabilised supply is essential.

PZ.5 30 volts unstabilised £4.98 PZ.635 volts stabilised £7.98 PZ.8 45 volts stabilised (less mains transformer) £7.98

PZ.8 mains transformer £5.98



### The Sinclair Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once Each module is quaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date There will be a small charge for service thereafter. No charge for postage by surface mail Air-mail charged at cost.

### Project 60 Stereo F.M. Tuner





First in the world to use the phase lock loop principle

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Good reception is possible in difficult areas, and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz. Capture ratio: 1.5dB. Sensitivity: 2 pt/ for 30dB quetong. 7 pt/ for full limiting sange: 87.5 to 108 MHz. Capture ratio: 1.5dB. Sensitivity: 2 pt/ for 30dB quetong. 7 pt/ for full limiting. Squelch level: 20 pt/ A.F.C. range: \_200 kHz. Signal to noise ratio: > 65dB. Audio frequency response: 10 Hz \_ 15 kHz ( ± 1dB). Total harmonic distortion: 0.15% for 30 % modulation. Stereo decoder operating level: 2 pt/. Cross talk: 40dB. Output voltage: 2 x 150mV R M.S. Operating voltage: 25-30 VDC. Indicators: Mains on: Stereo on: tuning.

Size: 93 x 40 x 207 mm.

Built and tested. Post free

£25

### Stereo 60 Pre-amp/control unit



Designed for Project 60 range but suitable for use with any high quality power amplifier Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS-Input sensitivities: Radio - up to 3mV Mag p u, 3mV correct to R | A A SPECIFICATIONS—Input sensitivities: Radio – up to 3mV Mag pu, 3mV correct to NIAA curve : 1dB 20 to 25,000 Hz. Ceramic pu – up to 3mV: Aux – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE – 15 to –15dB at 10 KHz BASS + 15 to –15dB at 100Hz. Front panel: brushed aluminiumwith black knobs and controls Size: 66x40x207mm. £9.98

Built tested and guaranteed.

### A.F.U. High & Low Pass Filter Unit



For use between Stereo 60 unit and two Z 30s or Z 50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less

loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The AF U. is suitable for use with any other amplifier system. Two filter stages – rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB) variable from 28KHz to 5KHz. L.F. cut-off (–3dB) variable from 25Hz to 100Hz. Distortion at 1 KHz (35V. supply (0.02% at rated.) output Size: 66 x 40 x 90 mm Built tested and guaranteed.

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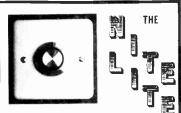
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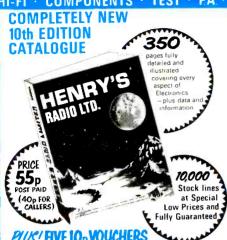
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