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| B 24 ブ |  |
|  |  |
| $\square$ |  |
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| － |  |
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| －$\square^{\square}$ |  |
| B 42 LL $\frac{1}{6}$－ 4.75 mm | chiset face |
| $\bigcirc 0$ |  |
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d.c. $02 \mathrm{~K} / 200 \mathrm{~K} / 20 \mathrm{meg} . \quad \mathrm{ohm}$. f.c. P. 25 p .


RODEL 5025. 57 ranges, glant blin
ineter, polarity polarity
reverse swltch. Sen-
altivity altivity: $50 \mathrm{~K} /$ Volt
 $125,260,50,1,000$. A.c. , $1050,500,1000 \mathrm{~V}, 3,5$.
 current: $20,50 \mu \mathrm{~A}, 2 \mathrm{~s}, 5,5,25,50,150$,
500 mA,
$5,10 \mathrm{~A}$. Hesistance: $2 \mathrm{~K}, 10 \mathrm{~K}$, $100 \mathrm{~K}, \mathrm{i}$ meg, 10 meg. Decibels: $-\because 0$ to +85 dB . 818 -60. P. E P. 171 p .


MODEL TE12. 20,000 O.P.', $\quad 0 / 0 \cdot 6,30 / 120 / 600$ 1/6/30/100/600/1,200V



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MODEL TE-200. 20,000 O.P.V. Mirror scale, over-:
load protectlon. $0 / 5 / 25$; $125 / 1,000 \mathrm{~V}$ d.c. $0 / 10 / 50 /$ $250 / 1,000 \mathrm{~V}$ a.c. $0 / 50 \mu \mathrm{~A} /$
250 MA.
$0 / 80 \mathrm{~K} / 6^{0} \mathrm{meg}$ $\begin{array}{ccc}\text { MODEL } & 500 & 30,000\end{array}$ OP.V. with overload $0 / .5 / 2-5 / 10 / 25 / 100 /$ $250 / 500 / 1,000 \mathrm{~V}$ d.c. $0 / 2 \cdot 5 /$
$10 / 25 / 100 / 250 / 500 /$ $10 / 25 / 100 / 250 / 500 /$
$1,000 \mathrm{~V} . \mathrm{a.c.0/50} \mathrm{\mu A/5/50/}$ 1,000 V. a.c. $0 / 50 \mu \mathrm{~A} / 5 / 50 /$
500 ma .12 amp. d.c. $0 / 60 \mathrm{~K} / 6$ Meg./60 Mego 080K/ Poserid Meg

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O.P.V. Míror load protectlon $0 / 0 \cdot 6 / 1 / 15 /$
$60 / 300 / 1,200 \mathrm{~V}$ d.c. $0 / 6 / 30 /$ $120 / 600 / 1,200 \mathrm{v}$ a.c. $0 /$ $30 \mu \mathrm{~A} / 6 \mathrm{~mA} / 60 \mathrm{~mA}$ $300 \mathrm{~mA} / 600 \mathrm{~mA} . \quad 0 / 8 \mathrm{~K} / 80 \mathrm{~K} / 800 \mathrm{~K} / 8 \mathrm{meg}$ -20 to +63 dB . ES.972. P.\& P. 15 p . TODEL TE 80. 80,000 $0 . P . V$
$1,000 \mathrm{~V}$. $50 / 100 / 500$ $250 / 500$ a.c. $0 / 5 / 25 / 50 /$ $0 \cdot 5 \mu \mathrm{~A}$. $1,000 \mathrm{~V}$ d.c $0 / 6 \mathrm{~K} / 60 / \mathrm{K} / 600 \mathrm{~K} / 6 \mathrm{Meg}$ 14.871. P. \& P. 15p.


MODEL TE-90. 50,000 O.P. Mirror scale, over*
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currents: $0-0.05,0.5,5,50,500 \mathrm{c}$ $\begin{array}{lllll}\text { currents: } 0-0-0 \delta_{y} & 0.5, & 5, & 50, & 500 \mathrm{mAA} \\ \text { Realetance: } 0-5 K & 50 \mathrm{~K}, & 0-500 \mathrm{~K}, 5 \mathrm{meg}\end{array}$ Decibels: - 20 to +52 dB . 111.50 . P. \& P. 17 1 p .

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| ${ }_{2} \mathrm{~N}_{1} 1303$ | 17 | ${ }_{2} \mathrm{~N}$ | ${ }_{3}$ |  |  |  |  |  |  |  | 148 |  | ${ }^{4821}$ | ${ }_{\text {cke }}^{\text {B8X } 28}$ |  | ${ }_{\text {MJ M }}^{\text {M }}$ | 97．98 | NK |  |  | ${ }^{5}$ |
| $2^{2} \mathbf{N} 13$ | 22 |  | 324 |  |  |  |  | AF117 | ${ }_{25 p} 2$ | вс170 | 17 id | 8F9\％ | ${ }_{878}$ | ${ }_{\text {H8X }}^{61}$ | ${ }_{82}^{82 p}$ | M 1490 | ${ }_{11}$ | NKT6 |  | （c811） | ${ }_{\text {cop }}$ |
| ${ }^{-1306}$ | ${ }_{285}$ | ${ }^{2} \mathrm{~N} 30{ }^{\text {a }}$ | 2 | 2 N | ${ }_{3}$ |  |  |  | ${ }^{800}$ | ${ }^{13 C 171}$ | 17 | ${ }^{18}$ |  |  |  |  |  | Nкт677\％ |  |  | ${ }^{\text {sp }}$ |
| $2{ }^{2} 13$ | 25 p | 2 N 3 | ${ }^{75}$ | 2－ 3904 | 35. |  |  | A12 | 22；p | 1 C |  | ${ }_{\text {BFIP8 }}$ | 412p | 78 |  |  |  | NKT713 | 2sp |  | sp |
| 2N |  |  |  |  | ${ }^{3711}$ |  |  |  | 20 p |  |  |  |  |  |  |  |  | NKT734 |  |  | p |
| ${ }^{2} \mathbf{N 1 : 3 0 7}$ | 27 |  | 25 | 2N3946 | ${ }^{377 \mathrm{p}}$ | 40030 |  | ${ }^{2}$ | 20， | ${ }^{1 \mathrm{BC}}$ | ${ }^{22}$ | ${ }^{\text {BF }}$ |  |  | 27 p |  | 87t | $\times \mathrm{x} 7738$ |  |  |  |
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| 2－16311 | $42 \pm$ | －2N3349 | ${ }_{\substack{\text { 973 } \\ \text { ¢1．30 }}}$ |  | 2210 |  | 97 fP |  | ${ }^{45}$ |  | 17 p | ${ }^{\text {RF }}$ |  | B8y | 17 p |  |  | NKT1033 |  | OCO |  |
| $\stackrel{\mathrm{N}}{\mathrm{N}}$ | ${ }_{42}$ | ${ }_{2 \times 3394}$ |  |  |  | 40310 |  |  |  |  |  | ${ }^{\text {BFP257 }}$ |  |  | 7 |  |  |  |  |  | ${ }^{\text {p }}$ |
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| ${ }^{\text {N }}$ | 3781 | 2N | ${ }^{301}$ |  | ${ }_{4}^{42 p}$ | 031 |  |  | A | ${ }^{\text {BCPL }} 13 \mathrm{LL}$ | ${ }^{267}$ | BFX |  | B83 3： | ${ }^{25 p}$ | NKTI | ${ }^{42} \mathrm{P}$ P |  |  | Oc 204 |  |
|  |  | 2 N | 20 p |  | ${ }_{42}$ | 4 |  |  | 47 | ${ }_{\mathrm{BCY}}$ | ${ }^{277 p}$ | ${ }_{8}^{\text {BFX }}$ |  | ${ }_{\text {B8837 }}^{1883}$ | ${ }_{25 \mathrm{p}}^{28 \mathrm{p}}$ | NK | ${ }^{277 p}$ |  |  | Oc |  |
| $\stackrel{2 N}{2 \times 1899}$ | ${ }_{42}$ | －${ }^{2 \times 394} 3$ | 22¢p |  | ${ }_{17}^{17 \%}$ |  | ${ }_{472} 82$ |  |  |  | 咗1 | ${ }_{\text {Br }}^{\text {Br }}$ |  | ${ }_{\text {B8 }}^{188}$ |  |  | 27.1 | NKTO |  |  | 42t |
| ${ }^{2}{ }^{2} 21$ | 72 |  | ${ }_{22}$ |  | 17p | 403 | 67 | A8 | 325p |  | 887 | ${ }_{\text {ifx }}{ }_{\text {ifx }}$ |  | ${ }_{\text {B8Y }}^{\text {B8Y }}$ |  |  |  | NKT801 |  |  |  |
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| － | ${ }_{47} 5$ | －2N34 | ${ }^{\text {4，5p }}$ |  | 17 | 4 | 48. | ARY28 | ${ }^{27} 7$ | ${ }^{\mathrm{BCY}}$ | 29 | ${ }^{\text {BFP8 }} 8$ |  |  |  | NK | ${ }^{80 \mathrm{~B}}$ | NKт80 |  |  | p |
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| ${ }^{2} 2228$ | ${ }_{32}$ | 2N3 | ${ }_{\text {che }}^{\substack{31 \\ 4180}}$ | － | ${ }_{62}$ |  | －${ }_{48, p}$ |  | ${ }_{\text {28p }}$ | ${ }_{\text {BC }}$ |  | ${ }_{\text {Br }}^{\text {Br }}$ |  |  | ${ }^{475 p}$ |  |  | NKT80 |  | T1849 | 硣 |
| 19 | 32tp | －${ }^{\text {N }}$ |  | 2 N | ${ }^{57}$ | 403 | 68 P |  | ${ }^{258}$ | ${ }^{\text {HCY }}$ |  |  |  |  | ${ }^{52+1}$ |  | \％ | nkT802 |  | T1850 | 27 |
| － | 250 |  | ${ }_{87}^{87}$ |  | 42 | 403 | ${ }_{689} 6$ | －${ }^{\text {AYY63 }}$ |  |  | ${ }_{22}$ |  |  |  |  |  |  | Nкт802 |  | ${ }_{T 18}$ | p |
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The first of Lasky's new-look top value meters, the TM-I is a really tiny pocket multimeter providing"'big" meter accuracy and performance. scale. Clisk stop range selection switch Beautifully designed and made impact resistant black case-with whie and metallic red/green ige case-with whice and merallic redgreen - DC/V: 0-10-50-250-1,000 at IK/OPV AC/V: $0-10-50-250-1,000$ at IK/OPV DC CURRENT: $0-1 \mathrm{~mA}, 100 \mathrm{~mA}$ - Resistance: $0-150 k \Omega$. Decibels: -10 dB to +22 dB

## Complete with test leads, battery and

LASKY'S PRICE $\{1.95$ POST 13p
MODEL TM-5 EX OHMS/V POCKET MULTIMETER
Another new look pocket multimeter from "asky's providing top quality and value. The in $\times 1$ in, fitted with extra large 2fin square meter. Readability is superior on all low ranges; making this an excellent instrument for servicing transistorised equipment. Re. cessed click stop selection switch. Ohms zero adjustment. Buff finish with crystal clear merer cover.

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- DC Current: $0-3301 \mathrm{~A}$, $0-300 \mathrm{~mA}$
- Resistance : $0-10 \mathrm{k} \Omega, 0-1 \mathrm{Ma}$
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High-precision low mass fully counter balanced pick-uparm, heavy balanced turntable, simply operaced controls operated controls, viscous cueing device, slide in cartridge carrier, four POST pole motor.

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Same specifications as the MP. 60 but with synchronous four pole motor and full automatic change facilities.
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BSR McDONALD 3104 Speed Autochanger
AD76K Magnetic Cartridge.
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$20,000 \mathrm{~Hz}$. Input imp.: 8 ohms. Size: It $20,000 \mathrm{~Hz}$. Input imp.: 8 ohms. Size: Iltin 14 thin Only LASKY'S PRICE $\mathbf{6 5} 75$ each fll for two.
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sound damping with chrome trim，strong carrying handle．
sound damping with chrome trim，strong carrying handle．
$\begin{aligned} & \text { The SONY TFM 8030L will enliven your leisure hours anywhere，anytime with exciting sound，} \\ & \text { sport music，etc．Technical specification：Freq．range．FM } 87-108 \mathrm{MHz}, \mathrm{LW} 150-\mathrm{Z85} \mathrm{kHz} \text { ，MW530－1，605 }\end{aligned}$
$\mathbf{k H z}$ ．Circuit：II transistors， 7 diodes and 2 thermistors．Aerial System：Directional telescopic for
FM，internal ferrite bar for LW／MW Power Output： 1.85 W max．Speaker PM Dynamic－4Simp
Power Source： 9 V power pack battery（Ever Ready PP9 or equiv．），AC mains with adaptor，Car battery
with adaptor．Size： $9 \mathbf{1}(\mathrm{~W}) \times 8$ 有 $(\mathrm{H}) \times 3$（D）．Complete with earphone and battery．


MANUFACTURER＇S LIST PRICE $£ 29.75$
Optional Exeras．SONY AC－90e AC
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This unique DIGITAL CLOCK is now available EXCLUSIVELY FROM LASKY＇$\$$ in chassis form for you to mount in any housing that you choose． All settingsareachieved by rwodual－concentric controls at the front including ＂click＂set alarm（up to 12 －hour delay），time adjustment．Ultra simple mechanism and high quality manufacture guarantee reliable operation and long life．
The sleep switch will automatically turn off any appliance－radio，TV，light， etc．，at any pre－set time up to 60 min ．and in conjunction with the AUTO The clock measures $44 \mathrm{~W} \times 1+\mathrm{H} \times 3 \mathrm{BD}$（overall from fron The clock measures plete with instructions．HUNDREDS OF APPLICATIONS．
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Project 60 is a range or modules which connect togeiher to form a complete stereo amplifier．The modules are： $1, Z-30$ high gain power ampi 2 power supplies．A complete system comprizes two Z－30＇s，one Stereo－60 and a PZ－5 or PZ－6
STEREO 60 SPECIFICATION
Input sensitivities：Radio up to 3 mV ，Magnetic Pick－up 3 mV ：correct to R．I．A．A curve $\pm \mathrm{IdB}: 20$ to $25,000 \mathrm{~Hz}$ ．Ceramic Pickup up to 3 mV ：Auxiliary up to 3 mV Output Signal to noise better than 70dB e Front panel：brushed aluminium with black knobs and Post $17 \frac{1}{2} p$
controls Size： $5 \frac{1}{4} \times 1 \frac{1}{2} \times 4 i n$ ．

## Z－30 SPECIFICATION

Power output： 15 W R．M．S．into Sohms using a 35 V supply Frequency better than 70 dB Input sensitivion $0.02 \%$ Signal to noise speaker imp： 3 to 15 ohms Power require ments：from 8 to $35 V$ DC（The $\mathrm{Z}-30$ will operate
from batteries if required）Size： $3 \frac{1}{2} \times 2 \frac{1}{4} \times \frac{1}{2}$ in $: 4047 \frac{1}{2}$ Post $17 \frac{1}{3} p$ P75 $\quad \begin{aligned} & \text { two Z－} 30 \text {＇s and a Stereo } 60 \text { for } \\ & \text { domestic applications．}\end{aligned}$ PT66 $\begin{aligned} & \text { 25Vstabilised－ideal for driving two } \\ & \text { Z－30＇s and a Stereo } 60 \text { for low } \\ & \text { efficiency speakers．}\end{aligned}$


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Portage on Kits A and B 23p for one or two Pootage on Kits A and B 23 p for one or two kits then 23p for each two kits ordered．Kits
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Double pole with neon let
Into side so luminous in dark，
Ideal for dark room light or for
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Whifature．lin long $x$ approximately tin dia－ meter．Wrill make and break up to $I A$ up to 300
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Brand new，not cx－equipment．

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8 ANP 12V BATTERY CHARGER KIT－con．－ prislog $230 / 40$ mains transiormer with 3 anf necondary and 3 amp rectifer $21.16+33$ p post． SONOTONE STEREO CARTRIDGE．Turnover type，ref．No． 19 T1．This fts most British pick－ upe，and in a really execlent reproducer．Línited
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2 AMP ${ }^{2}$ PIN BWITCEEED SOCKARTS for surfice mounting，brown bakelite．Made by famous maker， 18 p each or 1.20 dozen，
100 AssontrD SILICON RECTIFIERS G．P． AMD swirching diodzs．Small and very smial gizes．A real smip ior experinenters， 65 per 100.
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Laarn in your aloep：Have Radio playing and kettle boiling as you awake－switch－on lights to Ward of intruderi－have warm house to come do if you invest in an Electrical Programmer． Made by the fantous Smithe Instrument Company．


This is essentially a $230 / 240$ volt mains operated Clock and a 20 amp Switch． the switch－off time of which can be delayed up to 12 hours（continuously variable not stepped）．Simitarly the switch－on time can be delayed．This is a beautiful unit，size $5!\times 3 z \times 2 \nmid \mathrm{in}$ ，deep．Metal encaaed，glass fronted
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Is undoubtedly one of the finest loudspeakers that we have ever offered，produced by one of the country＇s most famous makers．It has a die－cant metal frame and is strongly recommended for Hi－Fi and public address．Handling
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$30-10,000$ c．p．s．－specify 3 or 15 ohme．Chassis diam． 30－10，000 c．p．s．－ppecify 3 or 15 ohme．Chassis diam． A \＆10 apeaker offered thla month for 87 plus 38 p port and ins．

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A parcel of integrated circuits made by the famous Plessey Company，A
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definitely not sub－standard or seconds． 4 of the ICs are single silicon chip
GP anpllfers．The 5th is a monolithic NPN matched pair．Regular prlce
of parcel well over $\& 5$ ．Full circuit detaila of the $I C B$ are included and in
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prices $85 p$ upwarda with circuith and technical data of each．Completc parcel
$\begin{aligned} & \text { prices } 20 \mathrm{p} \text { upwards＂ith circuith and technica data of each．Comple } \\ & \text { only } 81 \text { post paid．DON＇T MISS THIS TERRIFIC BARGAIN．}\end{aligned}$

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Made by Smlths these are AC mains operated， NOT CLOCK WORK．Ideal for mounting on rack or shelf or can be built into box with 13A per 24 hours， 5 anp changeover contacts will per＂4 hours，
switch a circuit on or off tluring these perlods． e28．50，post and ins．$\because 3 p$ ．Additional time contacta 00 p pair．

DISTRIBUTION PANELS Just what you need for work bench or lab． standard 13 amp fused pluge and on／off switch with neon warninglight，supplied complete with 7 feet of heary cable．Wired up ready to work， 42 lesa plug：
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This is a drum type tining device，the drum bein or 貯位ch setting purposes with trips which are
infinitely adjustable for position．They are also arranged to allow 2 operations per switch peer rotation．There are $1 \bar{v}$ changeover micro $s w i t c h e s$ each of 10 andp type operated by the trips thus $1 \bar{u}$ circuits may be changed per revolution． Drive motor is mains operated $\overline{3}$ revs per niln．
Some of the many uses of this timer are Machinery control，Boiler firing，Dispensing and Vuding machines，Display
Machinery control，Boiler firing，Dispensing and Vonding machinea，Display \＆10 each．Special snip price $\mathbf{5} 5-75$ plus $2 J \mathrm{p}$ post and insurance．Don＇t miss this terriffe bargain．

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These units made by the Mullard Group are for operating and con rolling d．c．Motors and equipment rom A．C，mains．
Thyristors are used and these supply a variable d．c．resulting in motiler spey far superior to most other methode．
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Model 2411 for up to 10 amps
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A quick way to connect equipment to the mains connection．by plugg preventa accidental swltching on；has sockets which allow insertion of meter without diseonnec－ ion；cable inlets firmly one tair wire on up top each．


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PROTECT VALUABLE
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ROI THRRMAL EUN－ AWAT OR OVERHEAT－ fiers，transistors，etc． which use heat－ oinks can easily be
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THERMOSTAT WITH This bas an This has a sentor attached to a 16 A switch by a
14 in length of fin length
tubing－control rauge is $20^{\circ} \mathrm{F}$ to $150^{\circ} \mathrm{F}$ so it if sultable to control soil heating and liquid heating sullable to contro solly heat or portable veasels an the gensor can be raised out and lowered into the ressel．This thermostat could also be used to sound a bell or other alarm when critical temp．is reached in stack or heap subject to spontaneous combustion or if liquid is being heated by igas or other means not controllable by the swiech． these at 60 each．Postage and inaurance 14 p ．


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2 pole， 2 way－4 pole， 2 way－ pole， 4 way－ 3 pole， 4 way ${ }^{2}$ pole 6 way－ $\mathbf{1}$ pole， 12 way．All at 18

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26 yards length 70W．Self－regulating
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BPOO 7400N BP01 7401N BP04 7404N BP04 7404 N
BP10
7410 N BP10 7410N BP30 7430N BP40 7440N BP41 7441 N

BP42 7442N BP50 7450N
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| Trpe 10. | Case | Lesds | Description | 1－24 | 25－99 | 100 up |
| BP 201C－SL20IC | TO－5 | 8 | G．P．Amp | 68p | 88. | 480 |
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| BP 702 －72702 | D．I．L． | 14 | G．P．OP Amp（Wide Band） | 83p | 450 | 407 |
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| BP $741-72741$ | D．I．L． | 14 | High Gain OP Amp （Protected） | 75p | 609 | 507 |
| $\mu \mathrm{A} 703 \mathrm{C}-\mu .4703 \mathrm{C}$ | T0．J | 0 | R．F．－I．F．Amp | 48p | 80\％ | 875 |
| TAA 263 － | T0．72 | 4 | A．F．Amp | 700 | 600 | 55 p |
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| PAE \％o． |  |  | $e_{p}$ | PAE To． |  |  |  | ${ }_{60}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| U1000 | J | 7400 N | 0.50 | UIC73 | \％ | 7473N | $\cdots$ | 0.50 |
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| UIClo | 5 | 7410 N | $0 \cdot 50$ | UIC83 | j | 7483N | ． | 0.50 |
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| U1C42 | J | 7442 N | 0.50 | UIC92 | 5 | 7492 N |  | 0.50 |
| Uicso | 5 | 7450 N | 0.50 | UIC98 | 5 | 7493 N |  | 0.80 |
| UIC31 | 5 | 7401 N | 0.50 | UIC94 | 5 | 7494 N |  | 0.50 |
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| U1C70 | 0 | 7470 N | 0.50 | UIC96 | 5 | 7496 N |  | 0.80 |
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14 and 16 lead sockets for use with dual－in－line Integrated Circuits． Order No．
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ETL Mierologic Circath Cty．pricat each
Epoxy case To－u temp．range $1 \bar{v}^{\circ} \mathrm{C}$ to $\overline{\mathrm{a}} \bar{v}^{\circ} \mathrm{C}$
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Postage and packing adk 7p．Overseas audd extrs for Alrinail．Minimun order 50 p ．Cash with order pleasc．Giro No． 388 －7006．

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## RESISTORS

$\frac{1}{2}$ W iskra high stability carbon film－very low noise－capless con struction．tW Mullard CR25 carbon film－very small body size $7.5 \times 2.5 \mathrm{~mm}$ ．4W Erie wire wound
Power

| Tolerance | Range |
| :---: | :---: |
| $5 \%$ | $4 \cdot 7 \Omega-2 \cdot 2 \mathrm{M} \Omega$ |
| $10 \%$ | $3 \cdot 3 \mathrm{M} \Omega-10 \mathrm{M} \Omega$ |
| $10 \%$ | $1 \Omega-3 \cdot 9 \Omega$ |
| $5 \%$ | $4 \cdot 7 \Omega-1 M \Omega$ |
| $10 \%$ | $1 \Omega-10 \Omega$ |

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available
E24
E12
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E12
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DEYELOPMENT PACK
0.5 watt $5 \%$ iskra resistors 5 off each value $4.7 \Omega$ to $1 \mathrm{M} \Omega$

E12 pack 325 resistors $\mathbf{E 2} \mathbf{2 0}$ ．
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MULLARD POLYESTER CAPACITORS C296 SERIES
$400 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F}, 0.0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 2 \frac{1}{2} \mathrm{p} .0 .0068 \mu \mathrm{~F}$ $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 3 \mathrm{p} . \quad 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 4 \mathrm{p}$ ． $0.15 \mu \mathrm{~F}, 6 \mathrm{p} . \quad 0.22 \mu \mathrm{~F}, 7 \pm \mathrm{p}: \quad 0.33 \mu \mathrm{~F}, 11 \mathrm{p} . \quad 0.47 \mu \mathrm{~F}, 13 \mathrm{p}$ ．
$160 \mathrm{~V}:{ }^{\circ} 0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 3 \mathrm{p}, 0.1 \mu \mathrm{~F}$, $0.15 \mu \mathrm{~F}, 0.22 \mu \mathrm{~F}, 4 \mathrm{p}, \quad 0.33 \mu \mathrm{~F}, 6 \mathrm{p}, \quad 0.47 \mu \mathrm{~F}, 7 \frac{1}{2} \mathrm{p}, \quad 0.68 \mu \mathrm{~F}, \quad \mid \mathrm{P}, \quad 1.0 \mu \mathrm{~F}$ $12 \frac{1}{2} \mathrm{p}$ ．
MULLARD POLYESTER CAPACITORS C280 SERIES
250 V P．C．mounting： $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 3 \mathrm{p} .0 .033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}$ ， $0.068 \mu \mathrm{~F}, 3 \frac{1}{2} \mathrm{p}, \quad 0.1 \mu \mathrm{~F}, 4 \mathrm{p}, \quad 0.15 \mu \mathrm{~F}, 0.22 \mu \mathrm{~F}, 5 \mathrm{p}, \quad 0.33 \mu \mathrm{~F}, 6 \frac{1}{2} \mathrm{p}, ~ 0.47 \mu \mathrm{~F}$ ， $8 \ddagger \mathrm{p} . \quad 0.68 \mu \mathrm{~F}, \mathrm{IIp} .1 .0 \mu \mathrm{~F}, 13 \mathrm{p}$ ．
MYLAR FILM CAPACITORS
$100 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.02 \mu \mathrm{~F}, 2 \frac{1}{2} \mathrm{p}, 0.04 \mu \mathrm{~F}, 0.05 \mu \mathrm{~F}$, $0.068{ }_{\mu} \mathrm{FF}, 0.1 / 4 \mathrm{~F}, 3 \frac{1}{3} \mathrm{P}$ ．
CERAMIC DISC CAPACITORS
100 pF to $10,000 \mathrm{pF}, \mathbf{2 p}$ each．
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Selection of 100 ceramic and polyester capacitors， 100 pF to $1.0 \mu \mathrm{FF}, \mathbf{6 2} .90$ ．
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Mullard C426 series（ $\mu$ F $/ V$ ）：25／6．4． $50 / 6 \cdot 4,100 / 6 \cdot 4,200 / 6 \cdot 4,320 / 6 \cdot 4$ ， $16 / 10,32 / 10,64 / 10,125 / 10,200 / 10,10 / 16,20 / 16,40 / 16,80 / 16,125 / 16$ ， $6 \cdot 4 / 25,12.5 / 25,25 / 25,50 / 25,80 / 25,4 / 40,8 / 40,16 / 40,32 / 40,50 / 40$ ， 2．5／64，5／64，10／64，32／64．
Miniarure P．C．mounting（ $\mu \mathrm{F} / \mathrm{V}$ ）： $10 / 12,50 / 12,100 / 12,200 / 12,5 / 25$ ， $10 / 25,25 / 25,100 / 25$.

## POTENTIOMETERS

Carbon track $5 k \Omega$ to $1 M \Omega$ ，log or linear $(\log t W$, lin $t W)$
Single， $12 \frac{1}{2}$ p．Dual gang（stereo），40p．
SKELETON PRESET POTENTIOMETERS
Linear： $100,250,500 \Omega$ and decades to $5 \mathrm{M} \Omega$ ．Horizontal or vertical P．C mounting（ 0.1 matrix）．
Sub－miniature 0.1 watt，4p each．Miniature 0.25 watt， 5 p each SEMICONDUCTORS

| 6 | 15p | BFY |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | 15p | BFY52 | 22 $\frac{1}{2} \mathrm{P}$ | OC81 | 15p | 2N3055 | p |
| ACl27 | $15 p$ | BSY56 | 30p | OC82 | $15 p$ | 2N3702 | 15p |
| $\mathrm{ACl}^{28}$ | 15p | BSX21 | 25p | ORP12 | 471 P | 2N3703 | 14p |
| ADI40 | 40p | BY124 | $71 p$ | IN4001 | $7 \frac{1}{2} p$ | 2N3704 | 171 1 p |
| AFI 15 | 171p | BYZ10 | 30p | IN4002 | 10p | 2N3705 | 15p |
| AFII7 | 171p | BYZI3 | 20p | IN4003 | $11 p$ | 2N3706 | $12 p$ |
| BC107 | 14 P | OA85 | $7 \frac{1}{2} p$ | IN4004 | 12 ${ }^{1} \mathrm{p}$ | 2N3707 | 181p |
| BCl08 | 10p | OA91 | $7 \frac{1}{2}$ | IN4005 | 14p | 2N3708 | 10p |
| BC109 | 14p | OA202 | 71P | IN4006 | 15p | 2N3709 | $11 p$ |
| BFY50 | 22p | OC71 | 15p | IN4007 | 16p | 2N3710 | 12p |
| BFY51 | 19p | OC72 | $15 p$ | 2N2926 | IIp | 2N3711 | 14p |

## ZENER DIODES

$400 \mathrm{~mW} 5 \%$ 3．3V to $30 \mathrm{~V}, 17 \frac{1}{2} \mathrm{p}$ ．
VEROBOARD

|  | 0.1 | 0.15 |  |  | 0.15 | 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2 \frac{1}{2} \times 3 \frac{3}{4}$ | 22p | 16 p |  | $\times 3 \frac{2}{4}$（plain） | 521p | － |
| 21 $\times 5$ | 24p | 24p |  | $\times 2 \frac{1}{2}$（plain） | 371 P | － |
| $37 \times 37$ | 24p | 24p |  | $\times 5$（plain） | 17⿺辶 ${ }^{\text {P }}$ | － |
| 3亲×5 | 27p | 27p |  | $\times 3 \frac{3}{4}$（plain） | 15 P |  |
| － $17 \times 2 \frac{1}{1}$ | 75p | 571 P | Pin | sertion tool | 471p | 471p |
| $17 \times 3 \frac{5}{4}$ | 100p | 75p | Spot | face cutter | $37 \frac{1}{2} p$ | 371p |
| $17 \times 5$（plain） | － | 75p | Pkt． | 36 pins | 15p | 15p |

ROTARY SWITCHES
2P2W，IP12W，2P6W，3P4W，4P3W，22 $\frac{1}{2} p$ ．
PLUGS AND SOCKETS

| Standard $\frac{1}{\text { in }}$ screened | $17 \frac{1}{1}$ | 2.5 mm insulated | 71p |
| :---: | :---: | :---: | :---: |
| Standard tin insulated | 14p | 3.5 mm insulated | $7 \frac{1}{2} p$ |
| Stereo tin screened | 35p | 3.5 mm screened | 12，${ }^{\text {P }}$ P |
| Standard tin socket | 15p | 2.5 mm socket | $7 \frac{1}{2}$ |
| Stereo tin socket | $17 \frac{1}{2} p$ | 3.5 mm socket | $7 \frac{1}{2} P$ |

BRUSHED ALUMINIUM PANELS
$12^{\prime \prime} \times 6^{\prime \prime}-25 p ; 12^{\prime \prime} \times 2 \frac{1}{2}^{\prime \prime}-15 p ; 6^{\prime \prime} \times 1 \frac{1^{\prime \prime}}{2}-10 p$ ．
C．W．O．please．Post and packing，please add $7 \frac{1}{2} p$ to orders under $\mathbb{L 2}$ ． Data sheets are available for most of the components listed，and will be sent free on request．
$8 E 39$ ELSTOW STORAGE DEPOT，KEMPSTON HARDWICK，BEDFORD

##  roo oulv $£ 40 \cdot 95$ <br> 

PREMIER STEREO SYSTEM "ONE" Consists of all all transistor stereo ampliner. Garrard $2025 \mathrm{~T} / \mathrm{C}$ auto/manual record player unit fitted stereo/mono cartridge and mounted in teak finish plinth with perspex cover and two matching teak finish loudspeaker systems. Absolutely complete and supplied ready to plug in and play. The io transistor amplifier has an output of 5 watts per channel with inputs for pick-up, tape and tuner also tape output socket. Controls Bass, Treble, Volume, Balance, Selector. Power on/off, stereo/mono switch. Brushed aluminium front panel. Black metal case with teakwood ends: Size $12 \times 5 \frac{1}{2} \times 3 \frac{1}{2} \mathrm{in}$. high (Amplifier available separately if required $£ 14.95$. Carr. 40 p). Now Available MATCHING F.M. TUNER £22.05.

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As mstem "ONE" above but with Garrard SP25.
$\underset{\text { PREMCER }}{ } \quad £ 47 \quad$ Cart.

## 

MODEL 19—520


MODEL 19—542


FI SPEAKERS Fitted two ${ }^{2}$ Hind treetera
 ohnt impedance. Hand. ling capazity low. Brand £3.47 1. \& P. 40


HI-FI STEREO HEADPHONE Designed to the higheat possible standard. Fitted 2 in. speaker units with soft padied ear muins. 8 ohm impedance. Contplete with 6ft. leat and stereo jack plug. £2.47 $\underset{25 \mathrm{p}}{\mathrm{P}, ~ \&}$

HTEREO STETHOSCOHF SET LOW imp. 21.25. P. \& P. 10p

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Imputs

\section*{| 20 |
| :--- |
| Specihtations |
| semi $\begin{array}{l}\text { conductors } \\ \text { Tuning } \\ \text { range } \\ \text { Aerial } \\ \text { Frequency } \\ \text { Responge } \\ \text { Power } \\ \text { Output }\end{array}$ |}

## impedance

impedance
Controls

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POCKET SIZE MOLTL-TESTER With wide angle, jewelled meter movement, ceramic long-life, low-lons switching, tough impact resisting case
Sensitivity
20.000
ohms/volt D.C $0,000 \mathrm{ohmas} /$ Yolt A.
18 Renges: 0-5-25-50-350-500-2500 volta D.C. $0-10-50-100-500-1000$ voltt 1.C. $0-50 \mu \mathrm{~A}-2.5 \mathrm{~mA}-250 \mathrm{~mA}$ D.C. $0-$ 6000 ohms-6 megohme, $10 \mu \mu t-0.001$ mid- 1 mid. -20 to +22 dB . Complete
battery, teat lead and inst ruct ions. £4.90
tone, balance, tuning, AFC. Stereo indicator Ah, FM, FM Stereo, Phollo (stereo $\underset{10^{7}}{\text { entor light) }} 8$
ize $15^{\prime \prime}=8$ it $3_{2}^{1 \times 1}$
$330 \cdot 45$
Model 19-542 9 trimaistorg, ${ }^{\text {br }}$ diode 2 varistors
FM $88-108 \mathrm{MHz}$ rM 8tereo Multiplex AM $535-1635 \mathrm{kHz}$ finternal AM ant ternal FM
$50-17,000 \mathrm{H}$ $2!$ watts tma fer chan. Ceramic pheno 4-8 ohm
Power on/off, Volume 8 and
On/off, Volume, bass, treble, balance, tuning AFC. FM, FM Stereo Ceramic, Magnetic. Aux
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184 Carr. \& Inh. DOp

"VERITONE" RECORDING TAPE SPECLALLY GAMUFACTUEED IN U.S.A. FROM EXTRA STRONG PRE-GTEETCHED MATERIAL THE QUALITY IS UREQUALLED. TENSILISED to ensure the most permanent base. Highly resistant to breakage, molature, heat, cold or humidity. High poliahed splice free finish. Smooth
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 DT5 5. 1200 POLIEBTER 75p DT7 7" $2400^{\circ}$ POLIESTER 21.25
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top quality amplifer giving 50 watts rms power output (80W peak). Incorporates 8 transistors and 4 silicon diodes (silicon output transistors). Inputs for 2 microphones each with ind widual volume controls, plus phono aux lnput. Master volume control and Bass and Treble Controls. Well premented front panel for ease of operaion, on/ofl power fick switch and pilot light. Output imperlance $4 / 8 / 16$ oams Mike 1 and 2 senaitivlty 2 mV ( $50 \mathrm{k} \Omega$ ) Phono/Aux 300mV (100k $\Omega$ ). Frequency response $50-20,000 H z$. Fused output and thermal verloal protection A. Mains into $950 \mathrm{~V}-\mathrm{Jo/60Hz}$ size $13 \frac{1}{\operatorname{in}} \times 9 \mathrm{in} \times$ in.

## PREMIER $£ 39$

P. \& P. 50p

## SPECIAL OFFER!



Garrard ates Mk. II ingle Record Player. Fitted Goldiring G850 Magnetic tereo Cartridge. Complete n Teak Plinth with Rigid Peraper Oover.
Total list Price over $8 \% 4$ prgmier $\& 18.90$ PRICE
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TAPE CASSETTES
$060\binom{60}{\min } 37 p_{81.05}^{2}$
$090\binom{90}{\min } .62 p_{81-80}^{8102}$
$\mathrm{C} \left\lvert\, 20\binom{120}{$ min } $87 \boldsymbol{p}_{22.55}^{8 \mathrm{ior}}\right.$
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20 PROJECT SOLAR ELECTRONIC KIT Mod. R. 128
This mira modern Project Kit is shaped for the space age. Carried inside a transparent tomed 4 in capsule the R. 128 comes complete with a sclf-eontained solar cell to power any one of 20 projects ranging from a one transistor radio to a morse set complete with key and morse training code. supplied complete with easy to follow mique electronic space capsule uniquue electronic space capsule.

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Using a robust Bolid State Integratel circuit the R. 127 kits will build any one of these projects: (1) Gicrmanium Radio. (2) Test Oscillator. (3) Morse Telegraph Training Player Amp. (7) Continuity Te日ter. (8) AF Sirnal I'racer. (9) Radio Transmitter (10) Water Purity Tester

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Like all Roc Eleetronic Kite the R. 126 uses reliable no-solder connections
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This eagy to milld Radlo is bascd on the aame circuit developed by
Marconi for the very first radio transmiseion but uses a nodern ferrite Marconi for the very first radio transnigsion but uses a modern ferrite

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16 WATT STEREO AMPLIFIER
Model R. 138
As well as separate bass and treble controls the R. 138 features asitchel main and remote speaker outputs can be used to drive independent stereo apeaker systems.
Fitted in ia well finiahed waluut cablnet the brushed aluminiunt front panel and semsible control knobs set this amplifier in the protessional class.
SPECIFICATION: Output: 16 Watta Total. 8 Watts per Cbannel. Frequency range: $30-$ $20,000 \mathrm{~Hz}$. Inputs: Phono \& Tuner. Outpute: Speakers Main, speakers Remote, Tape Out, and Headphones. Controls: Bass, Treble, Volume, Baiance (all ganged) Mode, speakers Stereol
PRICE Mono and Power on/off.

5 WATT 8 TRACK CARTRIDGE STEREO AMPLIFIER

## Model R. 133

Just slot in one of the many 8 track cartridge tapes available for a con tinuous programme of your favourite music. A manual programme override switch enables you to switich from one track to the next at the puoh of a button at the sane tine a numberen is playing Beautifully tinished in an is playiag. Beautifully the walnut cabinet the in in


PRICE $£ 36.00$
reliable service. SPECJFICATION-Trpe speed; $9.5 \mathrm{~cm} / \mathrm{sec}$ ( 3 i.p.s.). Wow \& flutter: better than $0.3 \%$. Frequency range: $40-12,000 \mathrm{~Hz}$ Cross talk: beiter than 45 dB at 1,000


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This is the communica
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10 WATT TRANSISTOR STEREO AMPLIFIER
Model R. 137



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Stcreo AM/FM Tuner.
The Satin Finish front pan The san socket as well as valume caries a stere (all ganged) speaker, mode and selector controls. Supplied complete with oiled wainut SPECIFICATION: Output: 10 watts total. Fivatts per channel. requency Range: $30-18,000 \mathrm{~Hz}$. mputs: Phom and Tuner.
PRICE $£ 13.00$
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Model R. 134


Perfect Matching Amplifier. The R. 134 Stereo Tuner designed to give yearn of reliable performance. The Tuning Band covers AM \& FM with a geparate atereo beacon to indicate when eceived.
SPECIFICATION
FM: frequency range: $88-108 \mathrm{mHz}$.
eparation 26 dib at 1 kHz . Image rejection 55ilB. AM: frequency range: 535 separation: 26 dB at 1 kHz . Image PRICE $£ 21.00$

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With separate tone and rolunue control on each channel and inputs for both phono and tuner, this 10 transistor amplifer is he ideal start to an excellent budget gatem. Frequency response $70-20 \mathrm{KHz}$ Output impedance 8-16 ohm. Attractively styled with rushed alumiaium front rushed alumialum front
 to none
Housed in a handsome walnut
cabinet the classical low line efyling of the R. 124 will grace any home. ensiticit: : $20 \mu$ V). Fidere Frequency Jange: $88-108 \mathrm{MHz}$. Usable Image Rejection: 551 B . AN: Frequency Range: $535-1605 \mathrm{kHz}$. Usable sensitivily: $300 \mu \mathrm{H}$. Audio Section: Total Output Power: 4W. Phono uput: 200 mV at $1 M \Omega$. Tape Jnput; 100 mV at $100 \mathrm{k} \Omega$
PRICE £29.95


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## BUT, SERIOUSLY

Do some of us on occasion take this business a trifle too seriously? We feel this could be true, for now and again someone is heard to imply that so and so design is a flippant use of electronics.
Getting straight down to grass roots, let us consider any classic circuit arrangement; in fact suppose we take a well known building block such as the multivibrator, as a general illustration. This circuit has a habit of cropping up in the most unlikely guises, as we all know. It may appear in an item of test gear such as a c.r.o. trace doubler or a voltage to frequency converter, in a car lamp flasher, in the tone generator section of an organ, in a digital calculator, or in a "toss the coin" game, to name but a few. This ubiquity helps to demonstrate the point that an electronic circuit as such has no innate purpose apart from the purely electronic function it has been expressly designed to perform; and this alone is not enough. Outside purely academic circles, the circuit requires some gainful employment to justify its existence. Providing it is within the circuit's capabilities, the precise nature of the task it may be given is, in an electronic sense, irrelevant. It may be useful or it may be frivolous. There is no list of prescribed duties that circuits must restrict themselves to! They work for us as we decree.

Electronics is a very "human" technology, simply because it is easily adaptable to most of our whims and needs. And it plays, quite rightly, a major part in our a musement and entertainment, no less that in the "serious" activities of life.
To be fair we must not forget that to some individuals the study of electronic circuitry can be an end in itself. Academic minds so inclined can derive plenty of intellectual pleasure from the analysis of circuit behaviour without too much worrying about specific applications. But to most of us electronics surely means more than conducting a minute anatomical examination of a pretty trace on the c.r.t., or indulging in a prolonged immersion in mathematics, however good all this may be for the mind. When it comes to the crunch, electronics is a tool and the most proper and sensible thing is to apply it however and wherever we can, to serve us at both work and play.
If there are theoreticians who still shudder at some frivolous application of the technology, there is a homely example for them to ponder. Let them consider the television receiver-that embodiment of many elegant electronic techniques, a mass produced complex of circuitry that has been designed principally for our entertainment. Just dare suggest that this cathode ray companion and comforter for millions be redesignated something like a "communications monitor" and provide nothing but news and elevating cultural programmes, and the whole nation would go on strike!

## CONSTRUCTIONAL PROJECIS

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Friday, March 19


MANY drivers are not regular users of parking lamps and tend to use side lights when parking in a strange situation. Because they would not use an automatic parking light very often, they do not consider it a worthwhile investment. The added facility of a lighting up reminder that this circuit offers will thus make the parking lamp worthwhile. The circuit is very simple and provides the following facilities:
(a) An automatic parking lamp that turns itself on and off at dusk and dawn.
(b) A warning system when the car is used with no lights in poor light or after lighting up time.
(c) A warning indication, while driving, as lighting up time approaches.
(d) Automatic cancellation of either system when the sidelights are switched on.
(e) No additional control switching when on route.

The complete unit can be attached to the car dash panel or to the windscreen where it is in view of the driver. Only three wires need to be connected to the car wiring which is not altered in any way. Both positive and negative earth 12 volt circuits are given, and for cars already fitted with an automatic parking light, only part of the circuit need be built. The unit utilises a standard parking lamp so if such a lamp is already used it can now be automated.

## CIRCUIT

The fundamental circuit adapted for both positive and negative earth systems is shown in Figs. 1a and 1 b ; this illustrates the operation of the system using normal ignition and side light switching. With switch $\mathbf{S} 1$ in the "normal", position the circuit is operative when the ignition is on and the sidelights off. The circuit is then in the lighting up reminder state and LP2 will signal the approach of lighting up time when en route, or when about to move off without lights when they are required.

With Sl in the "park" position, the sidelights switched off and a parking lamp (LPI) plugged into SK1 and SK2, the circuit will function as an automatic parking light, the ignition switch and LP2 being out of circuit.

## LIGHT DEPENDENT RESISTOR

As daylight decreases, the l.d.r. (light dependent resistor-XI) resistance increases and since this forms a potential divider with R1 at the base of TRI, when
the determined light level is reached, a switching function is triggered between transistors TR1 and TR2 so that TR2 conducts and consequently illuminates LP2 to show up the expression "no lights". The switching function is preferred to an emitter follower because there is no heat build-up across transistor TR2 while the input signal is developing. The life of the transistor is therefore prolonged. Resistor R3 is made up of two 22 ohm resistors in parallel.

The same circuit operation is carried out for both the parking lamp and internal warning system and the ignition/battery supplies are selected in conjunction with the appropriate lamp by the operation of the double pole changeover switch SI.

## SYSTEM CANCELLATION

Both systems are cancelled when the normal sidelight switching operation is carried out following the internal warning, or where sidelights are required when parked. The circuit is completed via the filaments of the sidelights, rear light- and number plate light; with the sidelight switch off, the small current required for the system flows through the paralleled filaments of the sidelights and associated lamps. When, however, these lamps are switched on, the circuit is shorted out and the no lights warning or the parking lamp, cease to operate.

If the car is garaged or parked within the law, the switch remains in the normal position and both systems are isolated. A check is readily available for both systems when light is shielded from XI. It is to be noted that LP2 will hunt if the I.d.r. picks up reflected light from the hand or any other adjacent surface capable of reflecting light on to the sensor.

## OPERATIONAL LIGHT RANGE

The operational range of the system is good and operational levels of light may be selected by the insertion of light filters under the cover of the l.d.r. These may be in the form of ordinary thin paper and are far more economical than the inclusion of a variable resistance in the circuit.

With the engine running when en route, the internal lamp may flicker as the critical light period approaches. This is due to voltage variation of the car's supply (the charging system) but since the flicker is an added attraction factor, the necessity for voltage stabilisation is considered unnecessary and not in the interests of economy.

## AU T0 HEE 3 , DE did

# A LIGHTING-UP REMINDER AND aUtomatic parking light . . . bY G. W. JONES 



## CONSTRUCTION

The prototype unit was housed in a small tobacco tin, the lid of which was reinforced with aluminium. Holes can be cut in the lid and aluminium plate for X 1 mounting, SK1 and SK2, S1 and the "no lights" indication. The legend "no lights" may be printed on tracing paper and inserted, between two protective celluloid layers, under the aluminium panel which is attached to the lid by three 6B.A. screws.

The mounting for X1 and LP2 holder were obtained from a single indication lamp dismantled for the purpose. SK1 and SK2 can be banana sockets or any


Fig. 2. Layout and wiring diagram of the prototype unit housed in a tobacco tin case. This is the negative earth system; for positive earth version the wire connected to SIb wiper is removed and reconnected to SK2, link between SK2 and SIb is removed. Wire " $C$ " is taken to SIb wiper and a new wire-which now becomes " $C$ "-is connected to SK2


Fig. 3. Circuit diagram of the negative earth system for lighting up reminder only. Connections " $B$ " and " $C$ " are reversed for a positive earth system
special socket to suit the parking light. The three core lead that connects the circuit to the car wiring can be taken out through a grommet hole in the side of the case.

Components in the prototype were mounted on a piece of 0.2 inch matrix Veroboard, fixed inside the tin by two 6B.A. screws and spacers (see Fig. 2). The inside of the tin should be protected by insulation tape so that no connection is made between the circuit and earth on the car. It is, of course, possible to use any form of construction, since the layout of components is not critical-the unit could be built into the dashboard of many cars and LP2 could be housed in a warning light mounting chosen to correspond with the other panel warning lamps.

## REMINDER ONLY

If it is required to provide a lighting up reminder only-without the facility of an automatic parking light-then S1, SK1 and SK2, and the connection to S2 (sidelights switch) on the car battery side may be omitted (see Fig. 3).

When the complete system is operated in the lighting up reminder mode, LP1 can be unplugged from SK1 and SK2 and hence the no lights warning may be cancelled by operation of S1 (change to "park" position) as well as by switching on the sidelights.



## SOVIET ACHIEVEMENTS IN SPACE

After a period of apparent inactivity, the Soviet Union has in the past two years or so made some significant advances that have been spread over the whole area of space activities. The Russians have for a long time favoured the use of space platforms and automatic probes. They have covered the human element involved by longer periods under space conditions, and experimented with the transfer of astronauts from one vehicle to another.

The local earth-moon activities have formed a part of their programme but they have paid a good deal of attention to the special techniques required to explore the other planets. Already they have had two attempts to land robot craft on Venus and now a third attempt has been made.

The unfortunate loss of Lunik 15 at the time of the Apollo 11 mission was a particular disappointment, but served to indicate the difficulties that attend attempts to maintain communication, with vehicles that are at a low level in areas where there are mountains involved.

## COLLECTING MOON SAMPLES

However the loss of control of Lunik 15 was more than compensated by the successful mission of Lunik 16. This vehicle departed from the earth for the moon with the main task of collecting, automatically, samples of lunar soil, putting them into containers, and returning them to earth. The vehicle consisted of a descent platform carrying the return vehicle, which carried the drilling mechanism and control. Altogether something in excess of 100 grammes of lunar material was recovered.

The point of operation was in the Sea of Fertility, $56^{\circ} 18^{\prime} \mathrm{W}$ and $0^{\circ} 41^{\prime} \mathrm{S}$, which is some 900 km from the site of the Apollo 11 landing. The material was friable surface substance of fine grain, for the first 15 cm of the sample. The next section from 15 cm to 33 cm was of variable granular material with some larger inclusions of the order of 3 mm in diameter. The last section from 33 cm to 35 cm was of large grain with some fragments of bedrock.

In appearance the material is a very dark grey almost black powdery
substance. The mean specific gravity of the material was of the order of $1 \cdot 2$ and the variation in particle size ranged from $70 \mu \mathrm{~m}$ at the surface to $120 \mu \mathrm{~m}$ at the lowest depth. The composition appears to be basaltic with some feldspar and some metallic iron and vitreous particles. Some isotopes of short life were found and altogether about 70 chemical elements were present.

A comparison with the specimens brought back by Apollo 12 shows very close agreement in the percentage of the various elements.

## SOYUS 9

Andrian Nikolayev, who captained Soyus 9, has made some interesting comments on the 18 -day flight. Month long flights are feasible but anything longer would require different techniques. There would be need for more efficient and extensive conditioning and also new medical procedures.

The post flight effects of this mission were very much more marked than those encountered with the shorter flights. Walking was found to be difficult over a period of days and there was frequent stumbling. They found it difficult to climb stairs, sometimes hard to stand upright.

A notable feature was the wasting of the lower limbs by as much as 4 cm round the hips and 2 cm round the shins. This appears to result from the loss of muscle tissue in the legs which are normally used to support the body at ig. There was a loss of body weight of 5 kg for the new astronaut Sevastianov and a little less for Nikolayev. However, they both recovered their normal weight in three weeks.

## LUNOKHOD

The mobile moon vehicle Lunokhod was an exciting event and represented a new era in space technology. Although an instrument unit, previously landed by the United States, had been made to hop, Lunokhod I is the first vehicle to be landed on the moon and become mobile under guidance from the earth direct. When the difficulties are properly realised, a task of this kind becomes a major point in history.

Because it is the first time that such a successful operation has been
mounted, a whole new vista in the exploration of the moon becomes available. Provided that communications between the base station and the unit can be maintained, many new areas of the moon can be explored in detail.

At the moment this is feasible only in open areas because in hilly or mountainous regions loss of communication could be disastrous. This points to the likelihood that control from a space platform would be the ultimate aim. A very great advantage is that a mobile system remotely controlled would enable special regions to be explored which might be impossible for manned units.

## MANNED FLIGHTS

It is significant that the Soviet space scientists do not regard the robot as the principal method. This is borne out by the fact that the internal environment of Lunokhod I is similar to a life support system having a temperature between 16 and 18 degrees centigrade and a pressure of between 730 and 780 mm Hg .

The present instrumentation could be built into a manned cabin without modification. From this it could well be surmised that a manned landing is still part of Soviet plans. Also there is a distinct suggestion that the Russians are looking further afield to Mars for automated surface units.

## LUNAR EXPERIMENTS

Although not much appeared in the initial stages about the type of experiments being undertaken, the following were included in the mission.
(a) Determination of the composition of the surface of the moon using x-ray photometry.
(b) Measurement of extra-galactic $x$-radiation using an $x$-ray telescope to make long exposure studies of weak sources. These cannot be done effectively (where distant sources are concerned) with rockets and satellites.
(c) Assessing the mechanical properties of the lunar soil by impressing a special stamp.
(d) The study of cosmic radiation from the sun.
(e) Experiments which involve the radiation from the moon itself.
(f) The very important cooperative effort of France and the Soviet Union in a laser experiment to determine accurately the earth-moon distance.
A special system of telemetric sensors is in use to measure the stresses acting on the chassis of the vehicle and a great deal of television recording is being made of the tracks that are made on the lunar surface.


For demonstration purposes, it is convenient to be able to produce any of these 16 functions without having to construct separate gates. The multifunction logic circuit makes it possible to establish any required function simply by selecting the appropriate combination with four switches.

## FUNCTIONS OF BINARY VARIABLES

In the logic diagram of Fig. 1, each of the four switches S3, S4, S5, and S6 puts a 0 or 1 condition on its respective gate input, according to Table 1. This lists the function logic output corresponding to each of the 16 functions.
The switch settings are, in fact, those that would appear in a truth table of the desired function.

The A,B inputs are connected to decode each of the four possible input conditions and so select the appropriate gate as follows:
Input state
$\overline{\mathrm{A}} . \overline{\mathrm{B}}$
A. $\bar{B}$
$\overline{\mathrm{A}} . \mathrm{B}$
A.B
Gate selected G1 G2 G3 G4

The G5 gate output will therefore assume a 0 or 1 condition depending both on the position of the


By P. A, Davis, A.M.Inst.E.

ALogic function expresses the relationship between the input and output logic states of a circuit. The basic logic functions AND, OR and NOT are part of a series of functions.

With two input variables, $A$ and $B$, four different input conditions can occur:

$$
\overline{\mathrm{A}} \cdot \overline{\mathrm{~B}} \quad \mathrm{~A} \cdot \overline{\mathrm{~B}} \quad \overline{\mathrm{~A}} \cdot \mathrm{~B} \quad \mathrm{~A} \cdot \mathrm{~B}
$$

These four conditions could produce a 0 or 1 at the output, depending on the circuit logic, hence a total of $2^{4}$ or 16 functions are possible.
function setting switches and on the particular combination of the $\mathrm{A}, \mathrm{B}$ inputs.
A 1 condition will light the lamp via the lamp driver but a 0 condition will not.

## CIRCUIT

The multi-function logic circuit makes use of two integrated circuits. These i.c.s are three and four input NAND gates; the SN7410N and SN7420N respectively.

Fig. I. Logic diagram of multi-function unit. Here two i.c.s incorporoting 3and 4 -input NAND gates are used. Gate input numbers refer to the device pin connections as seen in Fig. 2



Fig. 2. Circuit diagram of unit. Note that all gate inputs have a positive bias

In the circuit diagram (Fig. 2), all the switched gate inputs are taken to the positive rail by way of resistors. This ensures that each input is held at logic 1 when its switch is opened.

The unused input at gate G4 is connected to a used input rather than left floating.

Fig. 3 shows the i.c. gate configuration used.


Table 1. FUNCTIONS OF TWO BINARY VARIABLES

| Function number | Function setting switches S3 S4 S5 S6 |  |  |  | Logic function produced | Function name |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | 0 | 0 | 1 | A. B | AND |
| 2 | 0 | 0 | 1 | 0 | A. B |  |
| 3 | 0 | 0 | 1 | 1 | ${ }^{\text {B }}$ | B |
| 4 | 0 | 1 | 0 | 0 | A. $\bar{B}$ |  |
| 5 | 0 | 1 | 0 | 1 |  | A |
| 6 | 0 | 1 | 1 | 0 | $\bar{A} \cdot B+A \cdot \bar{B}$ | Exclusive OR |
| 7 | 0 | 1 | 1 | 1 | $A \pm B$ | OR |
| 8 |  | 0 | 0 | 0 | $\bar{A} \cdot \bar{B}=\bar{A} \square^{B}$ | NOR |
| 9 |  | 0 | 0 | 1 | $\mathrm{A} \cdot \mathrm{B}+\overline{\mathrm{A}} \cdot \overline{\mathrm{B}}$ | Logical Equivalence |
| 10 | 1 | 0 | 1 | 0 |  | NOT A |
| 11 | 1 | 0 | 1 |  | $\bar{A}+B$ |  |
| 12 | 1 | 1 | 0 | 0 |  | NOT B |
| 13 | 1 | 1 | 0 | 1 | $\bar{A}+\bar{B}$ |  |
| 14 |  | 1 | 1 | 0 | $\bar{A}+\bar{B}=\bar{A} \cdot \bar{B}$ | NAND |
| 15 | 1 | 1 | 1 | 1 | 1 |  |
| 16 | 0 | 0 | 0 |  | 0 | 0 |



Fig. 4. Component layout and wiring for topside and underside of Veroboard


Fig. 5. Veroboard and control panel interwiring on an aluminium chassis plate

## CONSTRUCTION

Apart from the chassis mounted switches and lamp, all of the components are mounted on a single piece of Veroboard as given in Fig. 4. To accommodate the dual-in-line i.c. packages, Veroboard of 0.1 in matrix is used.

Wiring of the switches to the board is shown in Fig. 5. Positioning of these will depend very much on the preference of the user; whether a large or small display is required.

## COMPONENTS . . .

```
Resistors
RI-R8 \(22 k \Omega\) (8 off)
R9 \(1 \mathrm{k} \Omega\)
All \(10 \%, \frac{1}{4}\) watt carbon
Transistor
TRI 2N706A
Integrated Circuits
ICl SN74ION
IC2 SN7420N
```


## Switches

SI-S2 Single pole changeover (2 off)
S3-S6 Single pole on/off (4 off)

## Lamp

LPI Miniature indicator 6 V 0.06 A (Electroniques)

## Miscellaneous

$0 \cdot 1$ in matrix Veroboard $2 \frac{1}{2}$ in $\times 2 \frac{1}{2}$ in, Vero pins ( 14 off), Aluminium chassis 8 in $\times 6$ in $\times 1$ itin

## OPERATION

To operate the completed unit, first select the required function from Table 1. This function is then set using the swifches S3, S4, S5, and S6.

Each input combination of $\mathrm{A}, \mathrm{B}$ is then. operated on by this function, and the result, a 1 or 0 , will appear at the output of gate G5. If the output is 1 the lamp will light.

Say, for example, the OR function is required. Table 1 gives the function switch setting as 0111 (Function 7).
,With these switches set accordingly, the switches SI and S2 are set to A,B. It will be found that the lamp lights, hence, we can conclude that provided that $A$ or $B$ (or both) is present at the input, the lamp lights.
Apart from the convenience of the unit for demonstrating logic functions, it can be useful as part of a training programme - particularly if the function governing the input-output relationship has to be deduced from the unit's behaviour.

# marhet PLate 

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

## WIPER DELAY

There are many windscreen wiper control units on the market and, as our readers will have noted, the problem with many circuits is that they are unable to accommodate the various wiring configurations and wiper motor types in use on all modern cars.

Wiperdwell, a unit manufactured by Automents Ltd., is one unit that can be used with all types of selfparking wiper motors and can easily be fitted by the average motorist in a very short time. The unit allows the selection, by a single control, of the most suitable wiping frequency for slight rain, fog and snow-a principle that works extremely well.

The unit can be fitted using a drill and screwdriver, comprehensive connection instructions are supplied and physical connection is made by way of "piggy back" connectors thus avoiding altering existing wiring and obviating soldering.

The Wiperdwell unit will not affect the normal operation of the wipers, can give up to 20 seconds between sweep delay, costs $£ 4.75$ and is supplied with a six month guarantee.

Another range of sub-miniature toggle and pushbutton switches suitable for many P.E. projects are those manufactured by Birch Stolec Ltd.

The switches include toggle, lever lock, rocker and momentary pushbutton types with one, two, three or four poles.

Contact ratings are: coin silver contacts, 5 A resistive load at 115 V a.c., or 2 A at 250 V a.c.; brass contacts with gold over nickel plate, $0.4 \mathrm{~V} / \mathrm{A}$ maximum at 20 V maximum (a c. or d.c.); coin silver contacts with gold over nickel plate, 5A resistive load at 115 V a.c. or 28 V d.c., or 2 A at 250 V a.c., and $0.4 \mathrm{~V} / \mathrm{A}$ maximum (a.c. or d.c.).

Available with short or long toggles with nine different colour caps, the switches can also be supplied for printed circuit board or angled mounting.

Full details of these switches and addresses of nearest stockists can be obtained from Birch-Stolec Ltd., Ponswood Industrial Estate, Windmill Road, Hastings, Sussex.

Also, we have been informed that Gothic Electronic Components, Beacon House, Hampton Street, Birmingham 19, have been appointed stockists and distributors of the complete range of standard and miniature thumbwheel switches from Birch-Stolec.

## REED RELAY

Two new miniature encapsulated reed relays supplied with either one normally open reed switch or one changeover contact are the most recent products from Osmor Ltd.

Ideal for printed circuit board mounting, the type ERA has maximum d.c. contact ratings of 10 W 200 V 0.5 d.c. and type ERC is rated at $4 \mathrm{~W} 28 \mathrm{~V} 0 \cdot 1 \mathrm{~A}$ d.c.

The relays are available for $6 \mathrm{~V}, 12 \mathrm{~V}$ and 24 V operation, and are colour coded for easy identification. The


## Wiperdwell windscreen wiper control from Automents

coil is wound on a glass-filled nylon bobbin, and a magnetic screen is fitted as standard.

The complete relay is encapsulated in glass-filled nylon and measures only 22 mm ( $\frac{7}{8} \mathrm{in}$ ) $\times 10.5 \mathrm{~mm}$ ( $\frac{1}{2} \mathrm{in}$ ) diameter.

Price of the relays vary according to type and quantity; full details can be obtained from Osmor Ltd., 540 Purley Way, Croydon, Surrey, CR9 4DY, or at 53 London Road, Leicester, LE2 OPD.

## TAPE HEAD CLEANING

Suitable for all compact casette type tape recorders and car player units, Multicore Solders have recently introduced a new tape head cleaning cassette tape.

It comprises a cassette tape container in which high quality cleaning tape is incorporated to clean tape heads, capstan and pinch wheel. Used in the same manner as a tape cassette by placing in the machine and operating in the play-back position, the whole operation takes approximately one minute.

Supplied in a plastics container the Bib Size 31 cassette tape head cleaner retails at 53 p ( 10 s .7 d .) and is available from most hi fi shops.

## MINIATURE SWITCHES

Sub-miniature toggle-switches with a rating of 6 A at 125 V or 3 A at 250 V a.c. suitable for most of our constructional projects are now being marketed by WEL Components Ltd.

The switches have a breakdown voltage of $1,000 \mathrm{~V}$ a.c. with insulation resistance of more than 100 megohms at 500 V d.c. The switch contact resistance is typically less than 5 milli-ohms at 1 A 2.4 V d.c.

The switches are moulded in phenolic melamine with solder tag connections and are available in two types-Type TS106D is a single-pole double throw and costs approximately $37 \frac{1}{2} p$ ( 7 s 6 d ) each. Type TS206N is a double-pole double throw and costs approximately $47 \frac{1}{2} \mathrm{p}$ (9s 6d).

Addresses of nearest stockists can be obtained from WEL Components Ltd., 5 Loverock Road, Reading, Berkshire.



By D. S. GIBBS and I. M. SHAW (ferranti lto)

|
N this, the final part of the P.E. Gemini dual purpose stereo amplifier, we give final construction details of the pre-amplifier, a fault finding chart and hints on using the completed amplifier.

## DRILLING

The pre-amplifier is housed in a Contil Mod-2 case size $G$ and the dummy front panel (aluminium $12 \frac{3}{4}$ in $\times$ $2 \frac{3}{4} \mathrm{in} \times 18 \mathrm{~s} . \mathrm{w} . \mathrm{g}$.) was actually cut from the unused main amplifier chassis. Full drilling dimensions for the box and panels are given in Figs. 36, 37, and 38.
Miniature toggle switches were used in the prototype for S1, S2, and S5 and the holes for these and the pilot light LPI must be drilled to suit whatever components the constructor has available. The best arrangement is to drill the front panel and the dummy front panel whilst they are clamped together to ensure that any slight errors do not prevent the components from fitting through the holes. All the holes must be de-burred with a file or a large drill.

## FRONT PANEL

To obtain a presentable finished article the dummy front panel can be rubbed with wire wool, using household soap and water, in one direction along the length of the panel. This process should be continued until all the scratches have been removed. A very good "brushed aluminium" finish can be obtained in this way; a satin finish can be obtained if the panel is coarse sand blasted by some local workshop or garage. Care must be taken not to introduce any fingerprints or grease before the panel is sprayed with Letracote gloss.

## LABELLING

The front and rear panels can now be labelled using the same method as for the main amplifier cabinet, i.e. one light coat of Letracote gloss, apply the letters and then a further two coats of Letracote. As can be seen in the photographs, the prototype controls have numbers of relative magnitude arranged around them. The indication dots for these numbers can be marked first lightly in pencil with the help of the template, Fig. 39. The template is transferred to a thin piece of celluloid by drilling small holes in the required places. The celluloid template can then be placed over the dummy front panel and the dots marked in lightly in pencil. This method ensures that the dots exactly line up with the 30 degree switch positions and that the dots round the other controls are all at the same angles and radii.

## ASSEMBLY

The front panel components are now mounted, not forgetting the dummy front panel which is held on by the control spindle nuts. Care must be taken not to mark the dummy front panel whilst tightening the various nuts and screws. The rear panel components, C52 (using a suitable capacitor clamp) and the assembled printed circuit board should be mounted on the appropriate parts of the case.

## WIRING

The wiring should be executed with the case dismantled, i.e. opened out like an exploded diagram, to make the connections to the front and rear panels easier. Any systematic way of wiring the interconnections can be adopted but it is recommended that many


Fig. 36. Drilling details of the base of the pre-amplifier case. The small chassis supplied with the case is used to mount C52 and has one hole drilled in it $\frac{3}{4}$ inch down and $3 \frac{1}{3}$ in acrass the panel. This hole can be seen as the earthing point in Fig. 42top right hand diagram

Fig. 39. Template for marking out indicator dots on the dummy front panel
DRILL SIZES
for all
metalwork
A - $\frac{3}{16}$ in
B-No. 27
C $-\frac{3}{8}$ in
D - No. 34
E $-\frac{\sin }{8}$
F $-\frac{1}{2}$ in
G $-\frac{3}{4}$ in


Fig. 37. Front panel drilling details. The dummy front panel should be clamped to this for drilling


Fig. 38. Rear panel drilling details


Fig. 40. Wiring of components mounted on the rear panel


Fig. 41. Wiring details of the selector and fiker switches (\$3 and S4) mounted on the front panel. Note the use of screened lead
different colours are used for identification purposes. The components which áre wired to the tone controls, C45, C46, C47, C145, C146, C147, must have sleeved wire ends and as short leads as practicable. The same applies to the four resistors in the area around S1, and SK5. The only internal screened cables necessary are the ones from the input sockets to S 3 , with the actual

screens being connected to a stout tinned copper wire joining the "Out" positions of the selector switch. The sole connection between the case and the negative rail must be at SK 5 as indicated, or complications may arise due to an earth loop being formed which could result in an incurable hum. The earth from the mains input cable is connected to a solder tag which is on the same bolt as C52 capacitor clip, but on the other side of the screening plate. This screen is fitted on final assembly in convenient holes between the mains switch and balance control such that it touches neither. As with the main amplifier the paint may have to be removed from around the screw holes to ensure that all the different sections of the box make electrical connection with each other. Finally, the feet can be fitted to the base of the case. Figs. 40,41 and 42 give the wiring up details.

## INTER UNIT CONNECTIONS

The cable which supplies power to the pre-amplifiers and audio to the main amplif $\neg r$ must be made a suitable length to suit the particular installation. Any multicore (at least three core) screened cable can be used since the output impedance of the pre-amplifier is quite low. We have not given any pin connection numbers for this cable because we have noticed that in some cases the numbers on plugs and sockets do not always correspond with each other. All that is required is that the channels do not inadvertently get reversed and that the earth and supply rails have a continuous path from the main amplifier. This cable must be in place before power is applied to the main amplifier or the charging current taken by C6 and C106, if this plug is inserted after the power has been applied, may damage the driver and output transistors.

## FAULT FINDING

This is a complex amplifier and it is possible that the constructor will have some problems to iron out before it works perfectly. Most faults will be due to: wires left unconnected or connected to the wrong place, components inserted at the wrong place on the printed circuit board, transistors or diodes inserted the wrong way round (easily done with the Ferranti devices), or surplus solder bridging the gap between two printed circuit tracks.



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$100 \mathrm{ohm}, 3 \mathrm{~A} ; 25 \mathrm{ohm}, 2 \mathrm{~A}: 50 \mathrm{ohm}, 1 \cdot 4 \mathrm{~A}$;
$100 \mathrm{ohm}, 1 \mathrm{~A}: 250 \mathrm{ohm}, 0.7 \mathrm{~A}: 500$ ohmm
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| 230 | $6-12$ | $2 \mathrm{c} / \mathrm{o}$ | 62p* | 1250 | 36-45 | 6M | 62p* |
| 280 | 6-12 | $2 \mathrm{c} / \mathrm{o}$ | 73p* | 2500 | 36-45 | 6M | 62p* |
| 700 | 16-25 | 4M 28 | 62p* | 5800 | 80-85 | $4 \mathrm{c} / \mathrm{O}$ | 62p* |
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Photograph of the front panel showing control designations

Faulty components are rare, especially if one uses new components of good quality, and if it is found that one of the transistors or diodes is defective after testing the amplifier, make sure that it was not destroyed by a wiring error before replacing it. To avoid expensive accidents great care should be taken to check all the wiring thoroughly before connecting the amplifier to the mains-it will be too late afterwards.

Given time and patience, most faults can be tracked down with a multimeter. An instrument of at least 20,000 ohms per volt is recommended. An oscilloscope
and an audio oscillator can save a lot of time and trouble, particularly with faults such as distortion and oscillation. And if it is required to test the amplifier through it's full specification, a wave analyser and a squarewave generator will also be required.

To assist in getting the amplifier to work correctly, a table giving the normal voltages at various points in the circuit, is given on page 212 , together with a list of fault symptoms and their most likely causes. This will help to track down most faults with the minimum of trouble, but we can not claim to have thought of everything.


## CONNECTING UP

The amplifier is working perfectly, a record deck or f. m . tuner is connected to it; on switching on there is a loud hum on both channels. This happens to nearly every audio enthusiast sooner or later and the usual cause is an earth loop. This arises when both the amplifier and the piece of equipment to which it is connected are earthed separately to the mains. A small a.c. voltage is induced into the earth leads of both units and when they are connected together a 50 Hz current flows in the outer braid of the coax cable between them, causing an objectionable hum. The cure is simply to disconnect one of the earths, preferably not the amplifier, and so break the loop. The record player deck or f.m. tuner, etc. will then be earthed via the amplifier. Another source of hum arises if the earth connection between the amplifier and the ancillary equipment gets broken whilst still leaving the signal lead (coax inner) connected. This causes a really colossal hum, often accompanied by a chorus of radio stations.

The prototype amplifier did not show any sign of radio breakthrough but if it is to be operated near a
transmitter and breakthrough is experienced, connect a capacitor of 100 to $1,000 \mathrm{pF}$ directly between each input and earth, alternatively a ferrite bead may be placed on each of the input leads (directly at the input sockets in both cases). Radio breakthrough can also be a symptom of h.f. oscillation in the circuit.

Supposing the amplifier is working perfectly, but there is only an output from one channel. The first thing to do is to check the wiring of the input plug, especially if using a ready made lead. The P.E. Gemini is wired as Fig. 43a which is the DIN standard for amplifiers but many of the ready made leads, intended for tape recorders, etc. are wired as Fig. 43b.

Low impedance signal sources, such as a tape recorder, f.m. tuner or low impedance dynamic microphone, can be connected up with ordinary twin screened (stereo) cable, but low capacitance screened cable should be used for high impedance sources, particularly magnetic pickups. The popular stereo cable has a capacitance of 100 pF or more per foot, and only 4 to 5 feet is required to produce a resonance at 10 kHz with a normal 500 mH magnetic pickup. Twin lighting flex is quite suitable for connecting up the loudspeakers.

## PE GENINI OHEGK GHART

| POWER SUPPLY <br> Nermal Voltages (no load) |  |
| :---: | :---: |
| Across secondary . | $\begin{gathered} 45-55 \mathrm{~V} \\ (50 \mathrm{~Hz}) \end{gathered}$ |
| Across C3 | 65-75V |
| Across output terminals. | 55 V |
| Across DI and C2 | 10 V |
| Between OV rail and TRI base | 9.3 V |
| Across R4 | 0.7 V |
| Across R5 | 1.4V |

Fault symptoms and possible causes
Output voltage zero
(I) Fuse blown. Check for cause before replacing.
(2) Bad contact in mains plug and socket.
(3) CI short circuit, or short circuit present across output.
(4) R6 omitted or open circuit.
(5) D2, D3, D4, or D5 open circuit.

Output voltage low
(1) DI or C2 wrong way round.
(2) TRI, TR2 or TR3 open circuit or wrongly connected.
(3) RI or R2 wrong value.
(4) Wrong transformer taps connected.

Output voltage high
(1) DI omitted or open circuit.
(2) TRI, TR2 or TR3 short circuit or wrongly connected.
(3) RI, R2, or R6 wrong value.

IMPORTANT: The power supply should be tested and adjusted to the correct voltage before the ht + leads to the amplifier are connected.

| MAIN AMPLIFIER <br> Normal Voltages |  |
| :---: | :---: |
|  |  |
| (Referred to common rail unless otherwise specified.) |  |
| H.T. rail | 55V d.c. |
| Output terminal | 27.5 |
| Emitter of TR4 | 26.7 V |
| Junction of R | 26.2 V |
| Base of TR5 | 0.7 V |
| Collector of TR5 | .5V |
| Base of TR6. | 1.3 V |
| Collector of TR6 | 27 V |
| ross TR7 coll/em | 1-1.5V |
| Junction of R15 and R16 | 47V |
| Across R25 and R |  |

## Fault symptoms and possible causes

Voltage at output terminal high
(1) TRIO or TRI2 short circuit or wrongly connected.
(2) TR4, TR5, TR6, TRII or TR13o/c.
(3) R9, R10 wrong value or R10 o/c.
(4) $\mathrm{C} 8 \mathrm{~s} / \mathrm{c}$ or leaky.

Voltage at output terminal low
(1) TR4, TR5, TR6, TRII or TR13 s/c or wrongly connected.
(2) TRIO or TRI2 open circuit.
(3) R9, R10 wrong value or R9 open circuit.
(4) C6, C7 leaky or short circuit.

Bias current too low
(1) TR7 short circuit.
(2) R18 or R19 wrong value.

Bias current too high
(1) TR7 o/c or wrongly connected.
(2) R18 or R19 wrong value.

## PREAMPLIFIER Normal Voltages

(Referred to common rail unless otherwise specified) H.T. rail ...................... 40 V Across CI6.................. 37.5 V TR14 and TR16 emitters .... I8V TRIS and TRI7 collectors... 18V TRIS and TRI7 emitters .... 28.5V TRI8 emitter ................. 6.8 V TRI9 emitter ................ 24 V TR20 emitter ................ 9 V
TR21 emitter ................. 20 V

## Fault symptoms and possible causes

No output for all inputs
(1) No h.t., check wiring and C52.
(2) TRI8, 19, 20, or $21 \mathrm{~s} / \mathrm{c}$ or $\mathrm{o} / \mathrm{c}$.
(3) Wiring error after 53.

Weak distorted output for all inputs
(I) H.T. voltage excessively low.
(2) TRI8, TR19, TR20, or TR2I inserted wrong way round.
(3) C33, C48, or C50 leaky or s/c.
(4) Incorrect resistor value.

No output or weak distorted output on dise
(1) TR14, TR15 o/c, s/c, or connected wrong way round.
(2) $\mathrm{Cl} 7, \mathrm{Cl}$, or C 23 leaky.
(3) Incorrect resistor value.

No output or weak distorted output on Mic
(I) TR16, TRI7 o/c, s/c, or connected wrong way round.
(2) C25, C27, or C29 leaky.
(3) Incorrect resistor value.

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88p；R．P．D．T．centre of 25p．

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| $\begin{gathered} 12+12 \\ \text { watia } 11{ }^{18} \\ \text { per channel } \end{gathered}$ |  |
| :---: | :---: |
| Sterco amplitier in mondalar kit form 12wath per chaniel E88－45．Cabinet prices nett． | including cabinet） it only 26．The日e |
| BAXANDALL SPEAKER SYSTEM |  |
| Designed by Peter Baxandall．8 reproduction for its aize．Handles 10 with ease．Uses ELAC $105 \Omega 591$ geaker unth．Kit $\mathbf{1 3}-90$ nett； 218．40 nett． | jerb ratta M109 huilt |
| MAINLINE AMPLIFIER KITS |  |
| RCA／BGA designed main amplifler kits．Input sensitivity $500-700 \mathrm{mV}$ for full output into $8 \Omega$ ． <br> EIt price <br> Suitable unreg． |  |
| Power inclading components | power supply kit e4．60 |
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| 70w 12．60 nett | E6．04 |

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Dual gang linear
$4.7 \mathrm{~K} \Omega$ to $9-2 \mathrm{Mn}$ 日 Dual gang linear
4.7 MO to $2 \cdot 2 \mathrm{Mn}$ Log／antilog
$10 \mathrm{~K}, 47 \mathrm{~K}, 1 \mathrm{Mn}$ only Dual antilog

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#### Abstract

A new conception in modular assembly which makes construction even easier then ever and results even better. Two pre-amp and two power amp modules, factory buift, tested and guaranteed by a world famous maker come to you ready mounted with mains power unit on chassis forming part of the attractive TRS cabinet and simply need wiring for immediate use. A generous 8 watt RMS output per channel into $\mathbf{3 - 5}$ ohms is assured. Cabinet with aluminium front, charcoal grey top and wood sides measures $12 \mathrm{in} \times 8 \frac{1}{2} \mathrm{in} \times 27 \mathrm{in}$


- Frequency resp.: $\quad 50 \mathrm{~Hz}$ -
- Input: 110 mV per P.U., Input: 110 m
radio 240 mV .
- Output. 8W

Output: 8W per channel. RMS into $3-5 \Omega$. Slightly less
per $8-150$ speakers.

- Recordand playback

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(via external tape pre=amp).
Bass/Treble/Volume/Balance
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Fig. 43. (a) Input wiring of the P.E. Gemini; (b) wiring of some ready-made leads


## TAPE INPUT

The tape input of the P.E. Gemini preamplifier has a flat frequency response and a sensitivity of 100 mV at 50 kilohms, suitable for connection to the equalised output of a tape recorder or tape unit. The input is like this to accommodate the wide choice of speeds and equalisation standards (DIN; CCIR, and NAB at 15 , $7 \frac{1}{2}, 3 \frac{3}{4}, 1 \frac{7}{8}$ i.p.s.) many extra components and some complicated wiring and switching would be needed. If the low level output of your tape recorder is not equalised you will have to construct an "add on" equalisation stage to give an output of 100 mV .


Fig. 45. Method of mounting the pre-amplifier in a console

## HEADPHONE OUTPUT

The headphone output from the main amplifier is connected directly to the loudspeaker outputs and in most cases it will be necessary for the constructor to add an attenuator to reduce the volume to a comfortable level. Because of the wide variation in heatiphone impedances ( 4 to 600 ohms ) and sensitivity between different types, the constructor will have to determine the correct values experimentally; Fig. 44 shows the circuit used, the values given being suitable for AKG K50 headphones of 400 ohms impedance. Resistor R1 should not be greater than the impedance of the earpiece and $(R 1+R 2)$ should not be less than 15 ohms, and preferably greater than 100 ohms if the attenuator is permanently wired to the amplifier. Some headphones have a built in attenuator and these can be connected directly to the headphone output socket.

## CASES

The Contil Mod 2 cases, used for both units, were chosen because they are relatively cheap, easily obtainable, and have an attractive if somewhat functional appearance. There is no reason why the constructor should not design his own case to match other equipment, provided that the case is well screened and the layout given is closely adhered to.

The preamplifier may be mounted in a console by increasing the size of the front panel so that it covers the hole required, as shown in Fig. 45. The front panel can be secured by screws from the front or clamps behind the panel.

ACKNOWLEDGEMENTS
The authors wish to thank Ferranti Ltd. for permission to publish this article and also L. Morral, R. J. Grundy and M. A. Rambaut for help given at various stages of the construction of the P.E. Gemini Amplifier.


# OITM GLOER By R.W. Coles 

$\mathrm{A}^{s}$S MENTIONED in the first part of this article, "Contil" Mod-2 case type " $C$ " " is used to house the DigiClock, and this makes construction much simpler than if a "one-off" case design were to be employed.

The front and back panels of these cases are formed from p.v.c. covered aluminium, which makes the necessary hole cutting quite easy. The only tools absolutely necessary are a hand drill and a good file, but a clean and neat finish can be more easily achieved with a nibbling tool such as the "Monodex" sheet metal cutter.

## CONSTRUCTION ON CHASSIS

The chassis supplied with the case is also made of aluminium and is used as a base-plate for all the mairı components, including the three circuit boards which are spaced from it only by three 6BA nuts. The chassis is earthed and acts as a low impedance "ground plane". for the logic circuitry, thus increasing the noise immunity of the system.

The series pass transistor TR2 employed by the 5 V regulator uses the chassis as a heat sink; it is vital that this transistor is isolated from the aluminium by an insulating mica washer of the type normally supplied with this type of device.

Drilling dimensions for the chassis and front and back panels are given in the diagrams, and it is important to remember that some of the chassis holes are required to match other holes drilled by the constructor in the circuit boards and the display panel bracket. It is preferable to match these chassis holes to the latter, rather than drill all the holes straight from the diagrams.

The mounting bracket for the "Nixie"' tubes is made from $\frac{1}{8}$ in s.r.b.p. sheet, and as can be seen from the diagram, the tubes are inserted directly into holes drilled in this bracket, no bases being employed.

With the dimensions given, the tubes are a tight fit in their mountings, and no extra fixative was used in the prototype. A dab of contact adhesive could be used if necessary, and still allow the tubes to be removed should this ever be desirable. Valve bases type B12A are available for the GN5A although the numeral spacing would have to be altered if these are used, since the tubes would not be so close together.

The decimal point indicator is mounted in a $\frac{3}{8}$ in coil former or some other suitable tube, cut to the dimensions shown, and fastened to the display panel with contact adhesive. When being installed, the neon is simply pushed through from the rear of the bracket, its insulated leads providing all the tension necessary to retain it in the tube.



Fig. 17. Chassis drilling details assuming components used are as specified in the components list. Modifications may be necessary for variations of component type. Clearance above chassis $2 \frac{3}{4}$ in


Fig. 18. Display panel drilling for "Nixie" tubes


Fig. 19. Back panel drilling details for components specified


Fig. 20. Front panel drilling details for components specified

Table I: CONNECTIONS TO MAIN CLOCK BOARD "A"
(a) Plain side terminations

| IC Number | Hole Number | Board " ${ }^{\prime}$ " Outlet | Wire Colour | Destination |
| :---: | :---: | :---: | :---: | :---: |
| -Resistor | for RI- | I | green | T2, 6.3V |
| 1 | 6E | 2 | black | Sla wiper |
| 6 | 2E | 3 | red | Sle wiper |
| 6 | 6A | 4 | orange | Sib wiper |
| 13 | 4F | 5 | red | Board B5 |
| 13 | 3 C | 6 | orange | Board 84 |
| 13 | 3 B | 7 | pink | Board B3 |
| 9 | 2 H | 8 | violet | Board BI |
| 12 | 3 E | 9 | green | Board B9 |
| 9 | 2 F | 10 | blue | Board B13 |
| ALL | Ground Rail | 11 | black | chassis |
| ALL | $+V_{\text {ce }}$ rail | 12 | red | Board B12 |
| 12 | 3B | 13 | brown | Board BIO |
| 9 | 3 G | 14 | yellow | Board B2 |
| 11 | 7H | 15 | (optional zero lin | hours $\times 10$ <br> e to VI pin 10) |
| 11 | 7G | 16 | yellow | VI pin! |
| 13 | 6 H | 17 | grey | V3 pin 10 |
| 13 | 6G | 18 | pink | V3 pin 1 |
| 13 | 3 A | 19 | white | V3 pin 2 |
| 13 | 6A | 20 | violet | V3 pin 3 |
| 13 | 7 E | 21 | yellow | V3 pin 4 |
| 13 | 6 F | 22 | green | V3 pin 5 |

(b) Copper side terminations

| IC Number | Hole <br> Number | $\begin{aligned} & \text { Board } \\ & \text { "A" } A \text { " } \\ & \text { Outlet } \end{aligned}$ | Wire Colour | Destination |
| :---: | :---: | :---: | :---: | :---: |
| - | - | 23 | - | - |
| - |  | 24 | - |  |
| 14 | 6 H | 25 | pink | V4 pin 10 |
| 14 | 6G | 26 | green | $\checkmark 4$ pin 1 |
| 14 | 2A | 27 | red | $\checkmark 4$ pin 2 |
| 14 | 6A | 28 | brown | $V_{4}$ pin 3 |
| 14 | 6E | 29 | black | $V_{4}$ pin 4 |
| 14 | 6 F | 30 | white | $V_{4}$ pin 5 |
| 14 | 6 C | 31 | yellow | $\checkmark 4$ pin 6 |
| 14 | 6 B | 32 | orange | $V 4$ pin 7 |
| 14 | 2 H | 33 | grey | $\checkmark 4$ pin 8 |
| 14 | 2G | 34 | violet | $V_{4}$ ping |
| 12 | 6 H | 34 | orange | V2 pin 1 |
| 12 | 7 G | 36 | green | $\mathrm{V}_{2} \mathrm{pin} 2$ |
| 12 | 2A | 37 | grey | $V_{2} \mathrm{pin} 3$ |
| 12 | 7 A | 38 | brown | V2 pin 4 |
| 12 | 7E | 39 | pink | $\checkmark 2$ pin 5 |
| 12 | 7 F | 40 | yellow | $V_{2}$ pin 6 |
| 12 | 7 C | 41 | red | $V_{2}$ pin 7 |
| 12 | 78 | 42 | black | $\checkmark 2$ pin 8 |
| 12 | 2 H | 43 | white | V2 2 in 9 |
| 12 | 2G | 44 | violet | $\checkmark 2$ pin 10 |



Table 2: CONNECTIONS TO ALARM BOARD "B" Copper side terminations only

| IC Hole <br> Number <br> Number | Board "B" Outle | Wire Colour | Destination |
| :---: | :---: | :---: | :---: |
| 19 7D | 1 | violet | LSI |
| 15 3H | 2 | yellow | Board A14 |
| 15 3F | 3 | pink | Board A7 |
| 15 3A | 4 | orange | Board A6 |
| 15 7B | 5 | red | Board A5 |
| 15 3E | 6 | black | S2a/4 |
| 15 3B | 7 | violet | S2a/2 |
| 15 6C | 8 | brown | S2all |
| $16 \quad 2 \mathrm{H}$ | 9 | green | Board A9 |
| 16 3F | 10 | brown | Board Al? |
| ALL Ground | 11 | black | chassis |
| $A L L \quad+V_{\text {ce rail }}$ | 12 | red | Board A12 (5V) |
| 16 2A | 13 | blue | Board A10 |
| 16 6B | 14 | violet | Board A8 |
| 16 6H | 15 | orange | S2b/8 |
| 16 3E | 16 | grey | S2b/4 |
| 16 3B | 17 | red | S2b/2 |
| 16 -6C | 18 | blue | S2b/1 |
| 18 6D | 19 | orange | S3 (OFF) |
| (collector of TRI) | 20 | red 1 | (TR2 collector, (10V). |
| Resistor R21, 2248 | 21 | yel | TR2 emitter |
| (TRi ${ }^{22}$ | 21 |  |  |
| emitter) 3F | 22 | green | TR2 base |

## PRINTED BOARDS "A" AND "B"

The circuit boards carrying the i.c.s are mounted on the chassis by means of 6BA bolts passing through each corner. Remember that the printed sides of these boards are adjacent to the chassis in the final assembly, and it will be necessary to make breaks in some cases in the printed tracks near the corner holes to prevent shorts to the chassis via the spacer nuts. Any breaks made for this purpose must be reconnected with wire links on the wiring side of the board.

Note that in Fig. 13 last month C8 should be comected to the link wire to C7 and pin 4 of IC19.

Using lin long bolts at the board corners allows their' use as "legs" to support the chassis during wiring up, damage to the delicate boards being avoided. The transformers perform a similar task on the other side of the chassis.

## WIRING UP

Once all the major components have been mounted on the chassis and the circuit boards have been tested for accuracy of fit, wiring up of the power supplies can be carried out. There is no need to attach the back panel wiring permanently at this stage, although it should be hooked in temporarily while the power supplies are tested, before proceeding further.
When the power supplies are operating satisfactorily, the interboard wiring can be started, remembering that the 5 V regulator board has two wires leaving it which do not pass through the edge connector. All connections are given in Tables 1 and 2 for the boards

carrying the i.c.s. It is most important that only very fine p.v.c. covered flexible wire be used for this stage of the wiring, no other type of wire is suitable, as will become obvious as you proceed to wire up the Main Clock Board " $A$ " edge connector with its 42 connections.

On completion of the interboard wiring the front and rear panels and their associated components can be attached to the chassis and the wiring finished off. The alarm speaker should be glued carefully to the rear panel with contact adhesive, making sure that it does not foul the smoothing capacitor or bridge rectifier wiring. The orange tinted Perspex filter is also fixed to the outside of the "Nixie" window front-panel cut-out with contact adhesive, and of course it is important that this operation be carried out with care to ensure a neat appearance.

The front and rear panels are finished off with "Letraset'" dry print transfer lettering. The lettering should be sprayed with clear lacquer fixative to avoid damage during handling.

## TESTING

There are no controls on the Digi-Clock which have to be set-up before operation, except the voltage control on the 5 V regulator which should be set-up when the regulator wiring is completed, before its connection to the $V_{\text {ec }}$ lines to the i.c. boards. This control setting should be rechecked with the clock operating normally, to ensure that the 5 V line is as accurate as possible.

If on switching on for the first time, all appears healthy, the set-time switch may be used to set the display to the correct time.

With the switch set to the "fast" position, the minutes counter will be counting 600 times faster than normal, making it a simple job to set the display to within about 15 minutes of the correct time. The slow position is then used to facilitate the final setting, a minute being clocked up every second. As soon as the display is correct the switch is returned to the "normal" position, and the clock continues normally.

If all is still well, the alarm circuit can now be checked. With the alarm "reset" switch in the "off" position, any valid time may be entered on the thumbwheel switches, after which the "alarm reset" switch is returned to the "set" state. When the "hours" and "tens of minutes" display counts to the same time as the alarm setting, the alarm should sound, and may be silenced by returning the "reset" switch to the "off" position. This check can be carried out with the clock running at a fast speed, making it a quick job to test all the alarm settings.

## FAULT LOCATION

If problems are encountered during any of these tests, a constructor who has become familiar with the logic of the Digi-Clock should find it a fairly simple matter to trouble-shoot with the aid of a logic probe such as that shown in Fig. 22 or even a multimeter set to the low voltage range.


Fig. 22. Simple test circuit or logic probe

The important thing to remember if a fault is present in the logic circuitry, is that ten minutes working out what could be the problem with a pencil and paper, is worth hours of aimless probing and measuring. Logic faults, providing they have symptoms observable through the display, are not hard to find because they always follow some form of sequence, which, when analysed, usually yields the answer, without any testing in the usual sense.

One of the easiest faults to occur is the incorrect sequence of time indication, possibly with more than one digit showing on one tube. In this case, check that there are no short circuits or solder runs between adjacent outlets on the Main Clock Board "A". If erroneous alarm triggering should occur, check for a similar fault on the Alarm Board "B". Also make sure that the copper strips are cut correctly as shown at " $X$ " in the first photograph (last month).

Check for solder runs between adjacent strips of copper; where these should not occur remove the solder. The wiring diagrams in Figs. 5 and 13 show the only places where these may occur intentionally.
The wiring tables and diagrams give colours to the wires as they were in the prototype. There is no reason why these should not be changed, but they are given to help the constructor to follow the wiring through if a fault is apparent.

## TENS OF HOURS DISPLAY

Readers may have noticed that in the block diagram given in part one of this project, the tens of hours "Nixie" has two connections to its cathodes, one being a dotted line to the " 0 " numeral. This connection was shown in this way because it is a matter of personal taste whether the " 0 ", needs to be used at all, a more conventional readout being given by allowing this tube to be completely blank during the hours of one to nine o'clock.
The decoder is, of course, able to accommodate either method, and the wiring diagram given in part one includes an edge connector contact for the " 0 " at outlet 15 of Board "A" so that it can be wired up if desired. This would be connected to pin 10 of V1.

## MODIFICATIONS

Apart from the alarm expansion scheme discussed in Part 2, many other improvements can be incorporated in the Digi-Clock if required. The operation of the clock counters could be altered to conform to the 24 hour system, counting could be extended to include an a.m./p.m. flip-flop, or even a calendar, provided the extra components required could be accommodated.

A slave display, or even several slave displays, could be driven by the basic circuit. In this case the outputs of the clock counters should be buffered by TTL gates or inverters and fed to lines which terminate in further buffers at the slave end.

Fairly long lines could be driven by this method because of the slow speed operation and the relative unimportance of noise at this end of the system. The slave units would consist of a few buffer gates as mentioned and four SN7441AN decoders to drive the "Nixies". A simple power supply would also be needed.

Finally, for anyone who finds the fairly high outlay on the Digi-Clock components unjustifiable, the masterslaves system might tip the balance, because this type of system would become more economic as more slaves were added.


Following its recent success at the Audio \& Music Fair, Practical Electronics now presents the full do-it-yourselfdetails of this fascinating addition to the sound scene. Part one of thisseries appears in the April issue.
P.E. Aurora is a controlled colour light display system which can be fed from any audio amplifier to provide the appropriate mood setting in the home or discotheque. It will respond to serious music or pop and can be arranged to give random displays from a digital sequencer.

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# SIMPLE REFLEX <br>  <br> > A SPECIAL PROJECT FOR BEGINNERS <br> <br> A SPECIAL <br> <br> A SPECIAL PROJECT FOR 

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THE crystal receiver has for a long time been for many their first introduction to table top electronics. It isn't difficult to seek out the reason for its appeal, for this first-time project can be an unending source of entertainment pleasure for a modest outlay.

For the T-Dec form of plug-in construction that has been maintained throughout this series, the choice of receiver circuit was based on the requirements of good stability, that is no "howls" or unwelcome oscillations, and excellent volume with little aerial and no earth in areas of good signal strength.

## REFLEX ACTION

Radio signals are characteristically of high frequency. For the medium wave-band which this receiver will tune to, this covers the range from 500 to $1,500 \mathrm{k} \mathrm{Hz}$ ( 200 to 600 metres).

Since many transmitters are sending out signals in this band, the receiver must be able to select the one required. In the block diagram of the receiver Fig. 1, the tuned circuit enables such selection to be made.
Since the currents generated in the aerial system are extremely weak, it is necessary to amplify them before they reach the diode detector.

The detector has the job of removing the desired audio signal from the high frequency signal which has, in effect, carried it pick-a-back from the transmitter.

The title of the circuit, "reflex", derives from what now follows. Audio output from the detector is reflected back through the r.f. amplifier so that this stage plays a dual role in boosting first the r.f. and then the extracted a.f. signals.

The output is taken through a further amplifying stage and then to the headphones.


## RECEIVER CIRCUIT

The complete receiver circuit diagram is given in Fig. 2. Here the tuned circuit consists of Tl primary and TC1. An aerial coupling capacitor Cl is included to improve selectivity; however, it must be borne in mind that with this simple type of single tuned circuit receiver, station separation is not ideal since it follows that the more tuned circuits used, the sharper is the tuning of that receiver.

The coils of the aerial transformer are wound on a ferrite slab which has the capacity to concentrate r.f. energy in its length and so improve signal strength. In areas where signals are very strong, it may be possible to dispense with a wire aerial and earth provided the slab aerial is orientated for maximum signal.

## CHOKES

The selected r.f. signal voltage is passed to the base of TR I by transformer action. Biasing of this amplifier is achieved by R1, R2 and R4.

The low level signal appears amplified at the collector but at this juncture it is faced with two routes to follow. The choke LI offers a high impedance path to radio frequency signal current whilst C3 does not. Signal voltages developed across L2 are applied to the detector D1, the desired audio programme material is then "unloaded" from the r.f. carrier and passed back to the input of TR1, via C6.

The audio signal is amplified and passed directly to the load resistor R3 since at low frequencies the resistance of the choke LI is small. The capacitor C5 passes this a.f. signal to a second amplifier stage, TR2, which provides the power for the headset.

## SETTING UP

Providing the component layout of Fig. 3 is adhered to, no reception problems should be encountered.

Whilst this receiver will give a good account of itself even with a short length of wire connected to CI , a good aerial will increase the sensitivity enormously in areas of difficult reception.

To demonstrate the effectiveness of a fair sized aerial, try connecting the co-axial outer of the television aerial to Cl , after first removing it from the set. Crocodile clips can be used for this. Bedtime listeners will find the bedsprings a convenient aerial, here once again, a crocodile clip will prove a suitable connector.

In general, at medium wavelengths, the receiving aerial takes the form of a vertical wire length, a common variant includes a horizontal top section of a few metres, but this sort of receptor would only be justified with the most elementary of crystal receivers.

## SPANNING THE BAND

To cover the medium waveband, it may be necessary to adjust the aerial coils on the ferrite slab. This merely involves moving the coil former until, say, Radios 1 to 4 can be tuned using TCI.

| Resistors |  |
| :--- | :--- |
| R1 | $20 \mathrm{k} \Omega$ |
| R2 | $3.9 \mathrm{k} \Omega$ |
| R3 | $6.8 \mathrm{k} \Omega$ |
| R4 | $4.7 \mathrm{k} \Omega$ |
| R5 | $27 \mathrm{k} \Omega$ |
| R6 | $10 \mathrm{k} \Omega$ |
| R7 | $3.3 \mathrm{k} \Omega$ |
| All | $\pm 10 \%$, $\frac{1}{4}$ watt ca |
| Capacitors |  |
| CI | 100 pF |
| C 2 | $0.01 \mu \mathrm{~F}$ |
| C 3 | $0.001 \mu \mathrm{~F}$ |
| C 4 | $25 \mu \mathrm{~F}$ elect. 6 V |
| C 5 | $10 \mu \mathrm{~F}$ elect. 15 V |
| C 6 | $8 \mu \mathrm{~F}$ elect. 15 V |
| C 7 | $0.01 \mu \mathrm{~F}$ |
| C 8 | $25 \mu \mathrm{~F}$ elect. 6 V |

Transistors
TRI OC44
TR2 AC126
Diodes
DI IGPIO
or OA81 (germanium)
Aerial Transformer
TI FS3 Ferrite slab aerial
(G. W. Smith \& Co. (Radio) Ltd)

Inductors
L1, L2 $\quad 1.5 \mathrm{mH}$ r.f. chokes (2 off)

Tuning Capacitor
TCl 208pF variable
Miscellaneous
XI High impedance
headphones or earpiece,
BYI 9 volt battery
T-Dec, wire links

Fig. 3. Component layout on TDec. Small Terry clips connected back-to-back are used for aerial retention


Fig. 2. Circuit diagram showing T-Dec connections. Thick lines indicate wire links



Above: A transmitter being fitted to a racing car Below: One of the 60 foot display pylons

## Racing Car Data Display

$M^{\prime}$iniature, battery powered transmitters, fitted to the sides of racing cars, are being used for the first time in America, to increase spectator interest. They give instant, continued information on the position of every car on the track.

Underground sensors at the track-Ontario Motor Speedway, California-enable the transmitters accurately to "fix" the car's position at all stages of a race. The transmitters feed this information direct to a computer which evaluates it, prints out the race order, and relays the race data direct to visual displays on three 60 foot pylons.

The radio transmitters used in this revolutionary scoring system rely upon the power provided by four 1.5 V Mallory alkaline batteries (left).

The innovation has proved so popular with spectators that the track organisers now plan to install an additional and even more sophisticated display-a mammoth animated sign which gives times, laps, car numbers and other digital information.

Unfortunately electronics does not always keep everybody happy. Used on the race track it has information and entertainment value and probably upsets or inconveniences nobody, however a slightly different application-still relating to cars-and many motorists get hot under the collar and start writing letters to magazines and the police about unfair and unashamed trickery. The application is of course the radar speed meter and no doubt many readers will be interested to know that an improved version has recently been announced by Shorrock Developments Ltd, part of the Hawker Siddeley Group Ltd. (see
below).



## Quietened noise on Musicassettes

DECCA 8-track stereo Musicassettes are now in full production at the Company's own factory at Bridgnorth and made exclusively from master tapes utilising the Dolby " $A$ " noise reduction system which produces a significantly improved signal to noise ratio. It is claimed that these Musicassettes offer the best quality of sound now available on this format and that this single factor will be one of the most significant selling points.

The tape duplicating equipment consists of two mother reproducers (also known as "master machines"), two loop bins and 13 slave recorders. One mother reproducer and loop bin is seen in the foreground of the photograph.


## Computerised Telephone Trouble Shooter

A N aptly-named Argus computer system to watch over the reliability of the telephone service has been ordered by the Post Office from Ferranti Ltd. The Argus 500 configuration is to be installed in Leicester about the end of 1971 for trials that could lead country-wide to the faster detection of faults, further improvements of service for customers, and cost sảvings.

Acting as a round-the-clock trouble shooter, the $£ 180,000$ on-line computer system will monitor performance, draw instant attention to faults and impending breakdowns and alert maintenance engineers, enabling them to start repair work much sooner. Repairs will often be completed without the customers being aware that a fault has ever developed.

The computer will help network development staff to provide additional plant where it is needed by tracing the pattern of calls and identifying the most commonly used routes, and by keeping a constant check on the volume of calls being made. It will also analyse signals from the equipment-testing devices already used to provide engineers with information on fault-prone equipment. The computer's analysis of these tests of individual pieces of exchange will show where overhaul is needed and provide an additional safeguard against breakdown.

Right-a typical Argus 500 configuration, this is a similar system to that to be installed at West Wigston Exchange, Leicester.


## Infra-red Thermometer Finds Faults in Wiring

ANEW infra-red thermometer-the $\mathbb{L} R 120$ Raynger-has recently been announced by A. Levermore and Co. Ltd. The LR120, shown above, has many industrial uses but the prime applications are in the electricity generating and distribution industry for locating faults in overhead cable connectors, transformers, splices, etc. which show themselves by small temperature rises.

To cope with these difficult operating conditions, the Raynger, which is battery operated and completely poriable, has been designed to measure temperatures between 0 and 100 degrees Centigrade above ambient, giving a resolution of better than 2 degrees. The ratio of distance to object size is $120: 1$, e.g. a 2 inch diameter area can be accurately measured at 20 feet distant.



A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.
This is YOUR page and any idea published will be awarded payment according to its merit.

## FUSE FAILURE INDICATOR

ASIMPLE way of giving an indication of when a mains fuse has blown is to connect a neon and its series resistance in parallel with the fuse as in Fig. 1. When the fuse is intact the resistor and neon are shorted, but when the fuse has blown they are effectively connected across the mains via the load resistance and the neon will strike.
A neat way of using a neon to indicate in a positive manner if the fuse is intact or not, is to have the neon lit steadily under normal conditions and for it to flash at a desired rate, should the fuse blow. The circuit evolved is a simple modification to an RC relaxationoscillator in which a capacitor is charged via a resistor (see Fig. 2a) until it reaches the striking voltage of the neon. At this point the neon strikes, discharging the capacitor to a level at which the neon extinguishes. The capacitor then commences to recharge and the cycle repeats, Fig. 2 b .

Referring to Fig. 3, with the fuse intact, on positive half cycles current is fed to the neon and capacitor via D1, D2, R1, and R2, whose resultant resistance is such that good, even illumination of the neon takes place. Should the fuse blow, however, diode D2 is connected via the load to the neutral side of the supply and is therefore reverse biased. Current is then linited by the larger resistance RI to give a long time constant. The capacitor takes longer to reach the striking voltage of the neon with the result that the neon flashes repeatedly drawing the attention of the operator to it. One advantage of this circuit is that the neon will flash irrespective of the load resistance, whether it is open or short circuit.

The flash rate can be adjusted by altering the value of either C1 or R1, but if R1 is altered then corresponding alterations will have to be made to R2.

One point to notice is that as Cl is charged to the striking voltage of the neon, the diodes should have a peak inverse voltage rating greater than peak mains plus this striking voltage.

## S. J. Forrest <br> Witney, Oxford.



Fig. I. Simple fuse failure circuit diagram

(a)

Fig. 2a. Circuit diagram for a flashing neon indicator


Fig. 2b. Groph showing the effect of the capacitor on the voltage across the neon


Fig. 3. Final circuit diagram for the flashing neon version of the fuse failure indicator
enclose a circuit for a linear scale ohmmeter which may be of interest to your readers.
The circuit diagram Fig. la consists of a constant current generator TRI and TR2, and a high input impedance meter driver TR4. A constant current is sent through the unknown resistor $R_{\mathrm{x}}$ and the voltage across it measured. Transistor TR3 compensates for the $V_{b c}$ drop across TR4. The current is set by varying

(a)

Fig. Ia. Circuit diagram of the linear scale ohmmeter


Fig. Ib. Adding a switched range
potentiometer VR1, which can be replaced by several resistors to give switched ranges, Fig. Ib.
On setting up, a one per cent resistor of value equal to the desired f.s.d. is used as $R_{\mathrm{x}}$ and VR1 is adjusted to give full scale deflection. The meter will then read any value resistor in that range as a linear proportion of full-scale.

For very high range;, the single emitter follower should be replaced by a two-stage circuit as shown in Fig. 2. In theory there is no limit to the range, but in practice, components limit the maximum range.

The advantages of this circuit over conventional linear ohmmeters is that a cheap meter can be used, and the unit is accurate over a wide range of temperatures.
lan R. Hornby,
Timperley,
Cheshire.


Fig. 2. Two-stage version for very high ranges

The "P.E. Aurora Lighting Display" will be included among the exhibits making up the Electric Theatre. This is an exhibition of artistic works which make specific use of electrics, electronics and mechanics to create effects with light and sound.
The Electric Theatre will be held at the Institute of Contemporary Arts, Nash House, The Mall, London, S.W.1., from March 18 to April 18 inclusive, 11 a.m. to 10.30 p.m. daily. Admission (at the door) 25p, students and members ICA 15 p .


## PART NINE-By R. W. COLES

MEDIUM SCALE INTEGRATION

ALL monolithic i.c.s start off as discs of silicon, an inch or so in diameter, on which may be built several thousand simple gates. We have already seen that by connecting together gates only, it is possible to build many different types of flip-flop, and by connecting together flip-flops it is possible to build counters and shift registers.

It is only a short step from this line of reasoning, that counters and shift registers could be built at the i.c. processing stage, by joining together a large number of gates to produce the logic required. This is, in fact, how MSI devices are built.

## BASIC MSI CONCEPT

A chip of silicon cut from the disc and containing around 30 gates, has a layer of metal deposited as an interconnection pattern, perhaps to form a four stage binary counter. The finished chip is mounted on a lead frame and packaged in the usual way as there are no space problems to worry about.

A dual-in-line pack is vast compared with the silicon chip it contains, whether it forms a flip-flop or a counter. The limitation to this process comes only with the restricted number of lead-outs the standard package can accommodate, not the size of the chip it can contain.

Fortunately the lead-out problem is not as severe as one might imagine, because most of the interconnections required to produce a complex function device are performed internally. Only the essential inputs and outputs are required to see the light of day.

What does this process do to help the designer or experimenter? The most obvious effect is the reduction in cost, a decade counter built using separate gate and flip-flop packages could cost in the region of $£ 310$ s ( $£ 3 \cdot 5$ ), whereas the same function can be obtained from the MSI range for about $£ 2$. The number of packages in this example is reduced by a factor of three, another very important saving.

Using MSI, it is possible to think in terms of counters
as building blocks instead of just flip-flops. The design of this larger block has already been carried out by the manufacturer, so a system is much easier to design, or it may be more complex for the same design effort.

All these things add up to an impressive list of advantages, which can be put to good use by the amateur constructor.

## BUILDING BLOCKS

TTL complex functions are contained in the usual 14and 16 -pin dual-in-line packages, and their equivalent in the flat-pack range; there is no external difference apart from the way the pins protrude. The inputs and outputs are completely compatible with the rest of the family, and usually employ the same type of circuitry.

However, the gates used inside the package are sometimes different in construction, because internal gates may not need the fan-out capability of others which have to drive external circuits. It is not intended here to go too deeply into the internal workings of MSI devices; earlier articles have already described the individual circuits in the TTL range.

We need only treat them as the useful building blocks that they are.

## MSI COUNTERS

Several different counters are available in the 74 series, each of which may be used for many different jobs and connected in several different configurations. Let us have a look at a typical example, the 7490 decade counter, which is shown in Fig. 9.1.

This counter, like the others in the series, is a ripple type, made up of four master/slave flip-flops; three of them are JK types and one a set/reset. It consists of two separate sections, a divide-by-five stage and a divide-by-two stage, which may be externally interconnected to give two different count modes, depending on the application.

The asynchronous flip-flop inputs are connected to two internal NAND gates which, when enabled, allow the counter to be reset either to zero ( 0000 ) or nine (1001).

If the count input is connected to the divide-by-two input, and the output of flip-flop A is connected to the divide-by-five input, the counter will count in the binary coded decimal code, as shown in the truth table in Fig. 9.la. In this mode the counter behaves as a normal four-stage binary counter until it reaches the count of nine; the next clock pulse sets the counter to the all zeros state.

This type of counter is employed when the outputs have to be decoded to drive indicator tubes, for instance in a frequency counter, or integrating digital voltmeter.

The secondary count mode is obtained by connecting the count input to the divide-by-five input, and the output of flip-flop D to the divide-by-two input, in effect causing the output of the divide-by-five counter to be divided by two, the opposite of the first count mode.

The truth table for this type of count is also shown in Fig. 9.1b, and it can be seen that the divide-by-ten output is taken from flip-flop A as a symmetrical waveform, up for five counts and down for five counts. This kind of count code is generally called the 1245 code, and is useful where these counters are used just as frequency dividers, for instance in frequency synthesisers.

These counters may be used to divide by numbers less than ten by using the reset gates to detect the desired final count plus one, and reset the counter to 0000 , or even nine, at this time. Any division by less than ten is possible, and an application is shown in Fig. 9.2, where a 7490 is used as a divide-by-six counter.

The other two counters in the series are similar to the 7490, but have a divide-by-six and divide-by-eight section respectively, instead of the divide-by-five of the 7490. They also do not have the facility of nine reset, only the zero reset is included.

## MSI DECIMAL DECODERS

Very often, the output of a decade counter is required to be decoded to the "one-of-ten" decimal equivalent of the binary count, in order that it may be displayed on some form of indicator. It is not surprising then, to find that the 74 MSI range contains several circuits which are capable of achieving this.

As an example let us look at the 7441 decoder/driver package. The 7441 takes a four-line binary coded decimal input word, and by means of gates and inverters, decodes this information into its decimal form, giving ten separate outputs. The outputs in this case are not designed to drive other logic gates, but to drive neon number indicating tubes such as "Nixies".

( 1 )

| COUNT | DUTPUT |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | A | 8 | $C$ | 0 |
| 0 | 0 | 0 | 0 | 0 |
| 1 | 1 | 0 | 0 | 0 |
| 2 | 0 | 1 | 0 | 0 |
| 3 | 1 | 1 | 0 | 0 |
| 4 | 0 | 0 | 1 | 0 |
| 5 | 1 | 0 | 1 | 0 |
| 6 | 0 | 1 | 1 | 0 |
| 7 | 1 | 1 | 1 | 0 |
| 8 | 0 | 0 | 0 | 1 |
| 0 | 1 | 0 | 0 | 1 |

(b)

| (b) |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  | OUTPUT |  |  |  |
| 0 | 0 | $C$ | 0 | 1 |
| 1 | 1 | 0 | 0 | 0 |
| 2 | 0 | 1 | 0 | 0 |
| 3 | 1 | 1 | 0 | 0 |
| 1 | 0 | 0 | 1 | 0 |
| 5 | 0 | 0 | 0 | 1 |
| 6 | 1 | 0 | 0 | 1 |
| 7 | 0 | 1 | 0 | 1 |
| 0 | 1 | 1 | 0 | 1 |
| 9 | 0 | 0 | 1 | 1 |



Fig. 9.2. The SN7490 used as $a \div 6$ counter with
Fig. 9.1. The SN1490 decade counter with truth tables for (a) binary coded decimal (b.c.d.) count mode and (b) symmetrical $\div 10$ mode
trugh table

This type of indicating tube uses ten separate cathodes, each in the shape of a decimal character, and a common anode. The anode is connected, through a limiting resistor, to an h.t. supply of the order of 200 volts. When a particular cathode is grounded the number it represents is illuminated by the ionisation of the neon gas surrounding it.

Fortunately, it is not necessary to use transistors "which will stand 200 volts on their collectors to drive these tubes, because reducing the voltage across them by only (say) 50 volts is sufficient to extinguish them, as this reduces the total voltage to below the "striking" potential.
In fact, the output transistors of the 7441 will withstand at least 55 volts, and to ensure that this rating

Many other types of decoding may be performed with the large range of circuits available in the 74 scries. Some have the standard TTL output stage, others will drive incandescent lamps. Some will even drive seven segment display systems, and in these, more than 35 separate gates are employed.

## MSI ADDERS

Adder circuitry, as we have already seen, is fairly complex, and now that computers are growing faster and faster, the use of parallel arithmetic is increasing, "ringing with it a demand for large numbers of separate "full-adder" blocks.


Fig. 9.3. MSI used to drive a cold cathode display
is not exceeded a Zener diode is connected from collector to ground. The basic idea of the output circuits used with these i.c.s is shown in Fig. 9.3.

To drive the ten output stages the four line binary word at the input to the 7441 has to be decoded by appropriate gating, and to carry out this decoding correctly, complementary information is necessary, i.e. A and not A, B and not B, etc. The generation of the inverted form of the input word is carried out internally, which makes things much easier, as only the true information needs to be supplied.

There is no doubt that this i.c. represents excellent value for money when compared with any of the possible discrete approaches. Even if i.c.s were employed to perform the gating, the price of ten high breakdown transistors would be more than a single 7441, which is a fraction of the size.

Fig. 9.3b shows the 7441 being used to decode the output of a 7490 decade counter, which has reached a count of two. This could represent one stage of a frequency counter.

The 74 MSI range offers three separate types of full-adder. The one which is, perhaps, most interesting is the 7483, so let us have a closer look at this one as an example.

The 7483 has four complete fuli-adders crammed into one 16 -pin dual-in-line package. Because it is intended for use in parallel addition computers, the carry line is internally connected between the four adders, making it possible to add two four-bit numbers together in less than 50 ns.

There are A and B inputs to each adder, with a single carry input to the first stage, and a single carry out from the fourth stage; four separate sum outputs are provided.

The logic of the 7483 is shown in Fig. 9.4; it is left to the interested reader to work out the truth table of the entire system, which will be in line with that given with the discrete-gate version in the section on gates.

Readers may think that it is unlikely they will be building a parallel arithmetic computer in the near future, and so this particular i.c. is of little interest, but a

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| $1 \mathbf{N} \boldsymbol{3} 1$ | $\begin{aligned} & 2 p \\ & 0.18 \end{aligned}$ | ACLEV | $\begin{aligned} & \operatorname{sp}_{0} \\ & 0.25 \end{aligned}$ | $\begin{array}{cc} \\ \\ \text { BFJ\％3 } & \\ \text { £p } \\ 0.30\end{array}$ | （1．34 | ${ }_{0.28}^{6 . p}$ | Oca 3 | $\operatorname{ing}_{0.40}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 N 23 | 0.20 | ACl 28 | 0.25 | BF181 0.38 | GJom | 0.25 | 0 CH 4 | 0.18 |
| $1 \times 85$ | 0.88 | $\mathrm{ACl}^{-}$ | 0.30 | 13 F 18400.28 | C．37M | 0.38 | $0 \mathrm{CL4M}$ | $0 \cdot 18$ |
| 120．853 | 0.50 | AC18\％ | 0.30 | BF185 0.25 | 1 $1: 1000$ | 0.50 | OC4 | 0.15 |
| 1 N 2－t | 0.50 | ACY17 | 0.30 | BF194 0.18 | HS100A | 0.20 | OC4，m | $0 \cdot 18$ |
| 1 N 640 | 0.25 | ACY18 | 0.25 | BF190 0.15 | Mat 100 | 0.25 | OCif | 0.88 |
| 1NT20． | 0.20 | ACY19 | 0.25 | BF196 0.28 | Matiol | 0.30 | OC5 | 0.60 |
| 1N914 | 0.08 | ACY：0 | 0.23 | BFI9s 0.88 | MAT 120 | 0.25 | OC， 8 | $0 \cdot 60$ |
| 1N4007 | 0.23 | ACY ${ }^{\text {d }}$ | 0.23 | $\begin{array}{ll}\text { BFS61 } & 0.28\end{array}$ | MAT121 | $0 \cdot 30$ | Ocs9 | 0.65 |
| 180：1 | 0.20 | ACY2－3 | 0.18 | BF＇g98 0.28 | MJEJ20 | 0.88 | OC66 | 0.50 |
| 18113 | 0.15 | 10ッ27 | 0.25 | BFXI： 0.28 | MJE29J． | 1.75 | Oc70 | 0.13 |
| 18130 | 0－13 | AC＇res | 0.18 | BFX13 0．23 | MJE309． | 0.83 | $06 \square$ | 0.15 |
| 18131 | 0.13 | ACY39 | 0.55 | Brx29 0.80 | NKT128 | 0.30 | OC7\％ | 0.95 |
| 18902 | 0.23 | ACY40 | 0.15 | BFX $30 \quad 0.33$ | NKT109 | 0.30 | OCJ3 | 0.80 |
| $2 \mathrm{G} \cdot 40$ | 1.88 | ACY＋1 | 0.25 |  | NKT： 11 | 0.25 | 0 Ca 4 | 0.30 |
| －G301 | 0.18 | ACY44 | 0.38 | $1 \mathrm{FFX63} \quad 0.50$ | NKT2l3 | 0.25 | Oça | 0.25 |
| $\bigcirc \mathrm{Ca302}$ | 0.23 | A5140 | 0.50 | $\begin{array}{ll}\mathrm{BFX} 84 & 0.30\end{array}$ | NKT214 | 0.15 | OC＇s | 0.25 |
| 2 G 306 | 0.30 | ADl4 | 0.50 | BFX85 0.40 | NKT216 | 0.38 | 0 O 78 | $0 \cdot 40$ |
| 2（1371 | 0.23 | AD1til | 0.38 | BFX8\％ 0.33 | NKT＊17 | 0.40 | OC78 | 0.20 |
| 2（9381 | 0.25 | ADIBE | 0.38 | $\begin{array}{ll}\text { HFX87 } & 0.83\end{array}$ | NKT：14 | 1.13 | OC78 | 0.13 |
| 2 CH 14 | 0.30 | AF106 | 0.30 | BF＇X88 0.25 | NKT219 | 0.33 | Ocas | 0.23 |
|  | 0.23 | AF114 | 0.33 | BFY10 1.00 | NKT202\％ | －0．20 | OC81 | 0.25 |
| 2N214 | 0.43 | AF15 | 0.30 | BFY11 1.25 | NK T204 | 0.23 | OC81D | 0.20 |
| 2N247 | 0.25 | AF16 | 0.33 | BFY17 0.25 | NKT201 | 0.24 | OC81M | 0.20 |
| 2 N 2 JO | 0.50 | AF117 | 0.25 | HYF18 0.25 | NK＇T271 | 0.25 | OC81DM | 0.18 |
| 2N404 | 0.23 | AFII | 0.63 | $\begin{array}{ll}\text { BFY19 } & 0.25\end{array}$ | NKT27？ | 0.25 | 0¢817， | 0.55 |
| －N69 | 0.18 | AFlly | 0.20 | BFY24 0.45 | NKT2\％3 | 0.20 | OC\＆2 | 0.85 |
| 2N698 | 0.43 | AF124 | 0.25 | BFY44 1.00 | NKT274 | 0.20 | O（8：2） | 0.15 |
| 2N706 | $0-10$ | AF1世5 | 0.20 | BFYう0 0．23 | NKT2\％o | 0.25 | OC83 | 0.25 |
| 2N：Oina | 0.13 | AF126 | 0.18 | BFYJ1 0.20 | NKT：\％7 | 0.20 | OC＇8 4 | 0.25 |
| ${ }^{2} \mathrm{~N} / 0 \mathrm{OH}$ | 0.15 | AF127 | 0.18 | ВFY近 0．23 | NKT2\％ | 0.25 | （6C114 | 0.38 |
| －N709 | 0.63 | AFI3： | $0-30$ | ВFYう3 0．18 | NKT301 | 0.30 | OC12\％ | 0.50 |
| －N711 | 0.38 | AF178 | 0.48 | BFY64 0.43 | NKT304 | 0.35 | $0 \mathrm{CL123}$ | 0.50 |
| －N987 | 0.53 | AF179 | $0-48$ | 13FY90 0．68 | NKT403 | 0.75 | OC139 | 0.25 |
| －N1040 | $0-30$ | AFiso | 0.53 | $38 \times 270$ | NKT404 | 0.83 | OCd 40 | 0.38 |
| 2N1091 | 0.33 | AF181 | 0.43 | $138 \times 60 \quad 0.93$ | NKT678 | 0.30 | OC141 | 0.63 |
| 2N1131 | $0-30$ | AFi86 | 0.40 | BSX ${ }^{\text {B6 }} 0.15$ | NKT713 | 0.25 | OC169 | 0.20 |
| 2N113： | 0.30 | AFY゙19 | 1.13 | 3SY26 0.18 | NKT－73 | 0.25 | OC170 | 0.25 |
| － N 1302 | 0.20 | AFZ1I | $0 \cdot 63$ | BSYer 0－20 |  | 0.38 | OC17 | 0－30 |
| 2N1303 | 0.23 | AF＇Z12 | ． 0.75 | BSY  <br> 150  | 078 B | 0.38 | OC200 | 0.38 |
| 2N1304 | 0.25 | A89 ${ }^{\text {¢ }}$ | 0.25 | BSY95A 0.15 | 0.9 | 0.15 | OC 201 | 0.48 |
| 2N1305 | 0.25 | ASY2\％ | 0.33 | 18Y05 0.15 | OAf | 0.13 | OC：20 | 0.63 |
| 2N1304 | 0.85 | A6Y28 | 0.25 | BT 102／500 | OA4： | 0.10 | OC－03 | 0.38 |
| 2N1307 | 0.25 |  | 0.30 | 0.75 | 0.70 | 0.10 | $\mathrm{OC}^{2} \mathbf{2} 4$ | 0.40 |
| －2N1308 | 0.30 | ASY 36 | 0.25 | 13TY4゙ 0.93 | 0.81 | 0.10 | $00^{2} 20$ | 0.68 |
| 2 N 1309 | 0.25 | AsYu0 | 0.18 | 13TY\％9／100R | 0.173 | 0.10 | OC206 | 0.75 |
| 2 N 1420 | 0.93 | －\＄9\％1 | 0.40 | 0.75 | 0.74 | 0－10 | OC207 | 0.75 |
| －N1J07 | 0.28 | ASY ${ }^{\text {S }}$ | 0.20 | ВTY79／400R | 0.179 | 0.10 | OC460 | 0.20 |
| －N1包 | 0.38 | ASY 0.0 | 0.20 | 1.75 | OA81 | 0－10 | 0 C 470 | 0.30 |
| 2N 1909 | 2.25 | －sy ${ }^{\text {¢ }}$ | 0.25 | $\begin{array}{ll}13 \mathrm{Y} 100 & 0.18\end{array}$ | 0.08. | 0.13 | OCPr 1 | 0.88 |
| 2N2147 | 0.75 | ABY89 | 0.33 | HY126 0.16 | 0.886 | 0.15 | ORP12 | 0．50 |
| － 22148 | 0.60 | ASZ：l | 0.43 | BY197 0－20 | 0.490 | 0.10 | ORP60 | 0.40 |
| －N2160 | 0.83 | 18823 | 0.75 | BY18． 0 | OA91 | 0.08 | ORP61 | 0.48 |
| 2N2018 | 0.30 | AUY10 | 0.98 | BY180 0.75 | OA90 | 0.08 | S19T | 0.30 |
| 2N2219 | 0.38 | 4U101 | 1.50 | BY213 0．25 | O．t200 | 0－06 | GAC40 | 0.25 |
| 2 N 2287 | 1.03 | $\mathrm{BCl}^{-7}$ | 0.25 | BYZ10 0.40 | OA： $0 \because$ | 0.10 | SFT308 | 0.38 |
| 2 N 2297 | 0.30 | BC108 | 0.25 | HYZ11 0.35 | OA210 | 0.25 | 8T722 | 0.38 |
| －N23tita | 0.20 | 13C109 | 0.25 | $\begin{array}{ll}13 \mathrm{YZ} & 0.8 \\ 0.80\end{array}$ | OA？11 | 0.38 | 8Tie31 | 0.68 |
| 2N2h13 | 0.28 | PC11：3 | $0 \cdot 30$ | BYZ12 0－80 | OAZ：00 | 0.55 | $4 \times 68$ | 0.20 |
| － $2 \times 645$ | 0.58 | 18Clls | 0.33 | $\begin{array}{ll}\text { HYZ13 } & 0.25\end{array}$ | OAZ201 | 0.50 | 9X631 | 0.20 |
| 2N2712 | 0.25 | ICP116 | 0.40 | $13 Y Z 15$ <br> 100 | 0．AZ202 | 0.43 | $8 \times 635$ | 0.30 |
| －N2784 | 0.50 | Br｀llis | 0.45 | －YZ16 0－63 | OAZ203 | 0.48 | SX640 | 0.25 |
| 2N2846 | 2.25 | BC118 | 0.38 | BYZ88C3V3 | OAZ204 | 0.48 | －X 641 | 0.25 |
| 2 N 2848 | 0.43 | BCl2 | 0.20 | 0.18 | oazeoj | 0－43 | 8X642 | 0.38 |
| $\because \mathrm{N} 2904$ | 0.30 | 13C12： | 0.20 | Cl11 0．65 | OAZ206 | 0.43 | 8 C 644 | 0.48 |
| －N2904A | 0.33 | B6120 | $0 \cdot 68$ | CH81／0u 0.20 | OAZ 207 | 0.48 | $8 \times 64$ | 0.76 |
| － $\mathbf{N} 2906$ | 0.30 | 13C126 | 0.65 | $\begin{array}{lll}\text { CRS1／40 } & 0.48\end{array}$ | OAZ 208 | $0-38$ | V10／301＇ | 0.50 |
| 2 N 2907 | 0.38 | BC140 | 0.65 | CS5B 2.50 | OAZ209 | 0.83 | V301201P | 0.38 |
| － 2924 | 0.23 | 12C14 | 0.18 | C810］ 3.13 | OAZ210 | 0－33 | V60／201 | 0－38 |
| 2N2g2， | 0.18 | BCl4＊ | 0.13 | L1 100000.16 | OAZ：11 | 0.33 | V601201P | 0.38 |
| ON292t | 0.18 0.50 | BC149 | 0.20 | DD003 0.16 | OAZ229 | 0.40 0.40 | XA101 | 0.10 |
| －N 30.54 | 0.50 0.75 | BC15 | 0.20 0.20 | $\begin{array}{ll}\text { DDO0 } & 0.18 \\ \text { DD00 } & 0.40\end{array}$ | OAZ223 | 0.40 0.38 | XA10： | 0.18 |
| 2N305． | 0.75 0.18 | BCiJ\％ BCy 88 | 0.20 0.20 | $\begin{array}{ll}\text { DD00 } & 0.40 \\ \text { D10008 } & 0.28\end{array}$ |  | 0.38 0.23 |  | 0.15 0.16 |
| －N3702 | 0.18 0.15 | 13C158 13 C 160 | 0.20 0.63 | $\begin{array}{ll}\text { D1P008 } & 0.38 \\ \text { GD3 } & 0.33\end{array}$ | $0.2 Z 241$ $0 A Z 24 \leq$ | 0.23 0.23 |  | 0.15 0.28 |
| － N 3706 | 0.23 | BC169 | 0.13 | $9 \mathrm{O} 4 \quad 0.05$ | 0AZP44 | 0.23 | XA162 | 0.25 |
| 2 N 3707 | 0.15 | BCY31 | 0.30 | GDJ 0－83 | 0.18246 | 0.23 | X 13101 | 0.48 |
| －N3703 | 0.13 | BCy31 | 0 | （11） 0.25 | OAZ290 | 0．38 | X H 102 | 0.10 |
| －N 3710 | 0.13 | HCY3\％ | 0.50 | GD13 0.05 | 0 Cl 16 | 0.43 | X Bl 103 | 0.25 |
| － N 3711 | 0.13 | BCY 33 | 0.20 | GET10：－0．30 | $0 \mathrm{OC15T}$ | 0.38 | X $B 113$ | 0.10 |
| 2N3819 | 0.35 | R1＇Y34 | 0.25 | GET103 0－28 | OC19 | 0.88 |  |  |
| －N3820 | 0.88 | НСУ 3 K | 0.30 | GETH13 0 | Oいこ | 0.98 | 人 3121 | 0.43 |
| 2 N 38.3 | 0.75 | BCV 39 | 0.48 | GETlli 0.15 | OC2\％ | 0.48 | ZR24 | 0.68 |
| $2 \mathrm{~N} \mathbf{2} 027$ | 0.53 | 13CY40 | 0.43 | GET115 0－45 | 0 C 23 | 0－50 | Z8170 | 0－10 |
| 2 N 5088 | 0.33 | 13CY42 | $0 \cdot 15$ | GET16 0.50 | OC：4 | 0－50 | 28251 | 0.18 |
| $\because 8005$ | 0.75 | $\mathrm{BCY}^{-10}$ | 0.20 | GET120 0．25 | OC53 | 0.38 | ZT 21 | 0.25 |
| 28301 | 0.43 0.63 | $\underset{\text { BCZ }}{ } \mathrm{BCY} 10$ | 0.30 0.30 | $\begin{array}{ll}\text { GET87\％} & 0.30 \\ \text { GET87 } & 0.25\end{array}$ | OC26 | 0.25 | ZT43 | 0.25 |
| 28304 | 0.68 0.38 | BCZ10 | 0.30 0.38 | $\begin{array}{ll}\text { GET87J } & 0.26 \\ \text {（iFT880 } & 0.38\end{array}$ | OC\％ | 0.26 0.63 | ZTX10\％ | 0．25 |
| 28701 | 0.38 0.63 | BCZ11 | 0.38 0.65 | $\begin{array}{ll}\text {（EET880 } & 0.38 \\ \text {（1ET881 }\end{array}$ | OC：9 | 0.63 | ZTX108． | 0．15 |
| AA129 | 0.80 | BDI？3 | 0－83 | GET88？ 0.25 | OC30 | 0.40 | ZTX300 | 0.18 |
| AAZI？ | 0.30 | BD124 | $0.63$ | GET885 000 | OC35 | 0.50 | 2TX304 | 0.28 |
| AAZ13 | 0.13 | $\mathrm{BF}^{\text {B11\％}}$ | 0．25 | GEX4v／1 ${ }^{0.08}$ | OC36 | 0.68 | ZTX 000 | 0.15 |
| $\mathrm{ACl}^{\text {c }}$ | 0.38 | BF117 | 0.50 | GEX941 0.15 | 0 C 41 | 0．26 | 2TXi03 | 0.20 |
| AC1－6 | 0.25 | BF167 | 0.85 | GJ3M 0．25 | OC42 | 0．30 | ZTXJ31 | 0.80 |

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bargain price. Silver and Dargain price. Siver and
groy deck enamelied
 45 and 78 r.p.m. Play ${ }^{\prime}, 10$, 12 in. disen which can be mised. Eitted renowned Philips plog-in Xtal AG3308 with Trequency response for LP/EP/ $16 \mathrm{Kc} / \mathrm{F}$. Sensitivity 100 mV . presaure 3-6 grammes. Board apace required 14 121in, Above tin. Below 2 !in. 12 monthe guarantee. (Also available with GP910 dismond stylus LP Stereo'EP and 8apphife 78. 21 exira)
MATCEED TEAK PLINTH with PLASTIC COVER. Only 26 extra of Cnt-out plywood bate bosid 10 /- extr
BSR 4-SPEED SUPERSLIM AUTO RECORD CHANGER Playil $12^{\prime \prime}, 10^{\prime \prime}$ or " ${ }^{\prime \prime}$ records. Arto or Menuel. A hith
eality unit becked by rolleblity with 12 montha' grarantee, size 13 t motor bosrd 8 Bolow 2tin. AC $200 ; 250 \mathrm{v}$ with STEREO/MONOXTAL $\leq 7$ POR 28R Minichanger DA50 8tereo/ Mono. lica 12 : 8in AC 800 is 5
. Post 5
GARRARD PLAYERS with sonotone 9TA Cartridgen. Sterso Diamond/Mono Sapphire. SP25 Mk II 215 , Model 3000 Stereo/Mono Autochanger 213. Pont 5 , hecord player portable cablict $\quad 75$ byece lor
RCA DE-LUXE 3 WATT AMPLEFIER. Ready made teated. 2-atage with triode pentode Falve, \& watti output. Tone and
volume controlt. Isolated mining tranalormer. Knobs londipeaker, valven ECL82, EZ80. Responge $50-12,000 \mathrm{cps}$. gengitivity 200 mV . Post 5 ' RCS \& WATT AMPLIFIER with loudapeaker and valves UCL82 and UY85. Font 5!-
R.C.S. TEAKWOOD BASE Resdy cut out tor $65 /=$ R.C.g. PLAgTIC COVERS FOR ABOVE BAEE. 65/
Durabia tinted platic, attractive appearance.

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WEYRAD P50 - TRANSISTOR COILS AEW Ferrite Aerial .. Oic. PSO/1AC 3rd I.F. P50/3CC Rd 1.F. P50/3C PS0/8V.
Mulisrd Forrite Rod 8 in. $4 /-8$ in. 5
VOLUMECONTROLS 800mm Coax 9 d. yd. ong spindies. Midget size BRITISH AERIALITE E. ohms to 2 Meg . LOG or AERAEIAL-AIR SPACED LIM, L/8 $3 /-\quad$ D.P. $5 /-40$ Yd. $28 /-: \quad 80 \mathrm{yd} 40 /$.

FIRE-WOUND 3-WATT POT8. WIRE-WOUND 3-WATT mall type with gmell knob. STANDARD SIZE POTS. $\left.\begin{aligned} & \text { Valuen } 10 \mathrm{n} \text { to } 30 \mathrm{~K} ., \\ & \text { Carbon } 80 \mathrm{~K} \text { to } 2 \mathrm{meg} .\end{aligned} \quad \right\rvert\, \begin{aligned} & \text { LoNG PPIMDLE } \\ & 100 \mathrm{OHM} \text { to } 100 \mathrm{~K} .8\end{aligned}$ 2t - 5in. 3/9, $25 \times 3!\mathrm{in}, 3 / 2,3!\cdot 31 \mathrm{in} .3 / 9$. EDGE CONYECTOR 18 way $\$ /-; 24$ way $7 / 7$.
FIN 36 per packet $3 / 5$. FACE CDTTERS 7/7. E.E.E.P. Board 0.15 MATRIT 2 tin. wide 7 d , per lin.



 lifoch DIAMETER WAVE-CHANGE SWITCHES. 2 p. $2-$ way, or 2 p. 8-way, or 3 p. 4-way 5/-each, 1 p. 12 -way, or 4p, 2-way, or ${ }^{4} \mathrm{p} .3$ 3-way 5 , each. 1 inch DIANETER


TOGGLE 8WITCHES, sp. 2/9; ap, dt. 3/7; dp. $3 / 7$; dp. dt. 4/7
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 PRE AMPLIFIER BRITISH MADEior Mike, Tape, R.D., Guitar.
Battery 9-127. or H.T. line 200-800\%. D.C. operation. Sise For use with valve of trancisior equipment. Full ingtractions supplied. Brand new. Guarantractions supplied.

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$4 / 350$ $4 / 350 \mathrm{~V}$ $8 / 450 \mathrm{~V}$ $8 / 450 \mathrm{~V}$
$16 / 450 \mathrm{~V}$ $16 / 450 \mathrm{~V}$
$32 / 450 \mathrm{~V}$ $25 / 25 \mathrm{~V}$

$50 / 50 \mathrm{~V}$ | $25 / 25 \mathrm{~V}$ | $\cdots$ | $2 /-$ | $16+18 / 450 \mathrm{~V}$ | $4 /-$ | $32+32 / 450 \mathrm{~V}$ | $8 / 450 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $5 /-$ | $32+32+32 / 350 \mathrm{v}$ | $8 / 7$ |  |  |  |  |
| $50 / 50 \mathrm{~V}$ | $\therefore$ | $2 /-$ | $32+32 / 350 \mathrm{~V}$ | $5 /-$ | $100+50+50 / 850$ | $8 / 7$ | SOB-MIN, ELECTROLYTICS. 1, 2, 4, 3, 8, 16, 25,30 50,100 $200 \mathrm{mF} 15 \mathrm{~V} 2 /-; 500,1000 \mathrm{mF} 12 \mathrm{~V} 3 / 7 ; 2000 \mathrm{mF} 25 \mathrm{~V}$ 7/ CERAMIC. 1 pF to $0.01 \mathrm{mF}, 9 \mathrm{~d}$. Silver Mica 2 to $5000 \mathrm{pF}, 9 \mathrm{~d}$ PAPER 350V-0.19d, $0.5 \mathrm{R} / 6 ; 1 \mathrm{mF} 3 /-2 \mathrm{gmF} 150 \mathrm{~V} 3:-$ $500 \mathrm{~V}-0.001$ to $0.059 \mathrm{~d} ; 0.11 /-0.251 / 6 ; 0.475 / 0$ | $1,000 V=0.001,0.0022,0.0047,0.01,0.02,1 / 6 ; 0.047,0.1,2 / 9$ |
| :--- |
| IILVER MICA. Close tolerance $10.2 .2-500 \mathrm{~F}$ | $2,200 \mathrm{pF} 2 / \cdot ; 2,700-5,600 \mathrm{pF} 4 /-6,800 \mathrm{pF}-0.01$, mfd $8 /-$; each.

 dpive $365 \mathrm{pF}+365 \mathrm{pF}$ with $25 \mathrm{pF}+25 \mathrm{pF}, 11 / \circ ; 500 \mathrm{pF}$ slow

SHORT WAVE SIIGLE. 25pF, $50 \mathrm{pF}, 11$
CEROME TELESCOPIC AERIALS 23 in, Swivel base $4^{\prime}-$ TUNIMG. Solid dielectric, $100 \mathrm{pF}, 500 \mathrm{pF}, 7 /-$ each.
TRIMMERS. Compresion $30,50,70 \mathrm{pF}$, I
$100 \mathrm{pF}, 150 \mathrm{pF}, 1 / 7 ; 250 \mathrm{pF}, 1 / 7 ; 800 \mathrm{pF}, 750 \mathrm{pF}, 2 /-1000 \mathrm{pF}, 2 /$ RECTIFIERS CONTACT COOLED half wave $80 \mathrm{~mA} 7 / 7$; $85 \mathrm{~mA} 9 / 7$. SILICON BYZI3 $6 /-$; BY100 $10 /-$
Full wave Bridge Rectiters $75 \mathrm{~mA} 10 /-150 \mathrm{~mA} 10: \%$ MEOP PANEL INDICATORO 2505 ACDC
NEON PANEL INDICATORS 2507. AC/DC Red or Amber 4! Resistors. Preierred palues, 10 ohms to 10 mer.
 Ditto 5:'. Preferred valuez 10 ohmz to 10 meg., 9 d .
WIRE-W0UND RESISTORS 5 watt, 10 watt, 15 watt
10 ohms to 100K, 2/-each; $2!$ watt. 1 ohm to 8.2 ohms. $2 j-$ Q MAX CHASSIS CUTTER

Complete: a die, a punch, an Allen screw and key

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|  |
| :---: | Super quality mall size 1 ! 1 lin. plus spindle 1 ! din. $365+385 \mathrm{pF}$ with $25+25 \mathrm{pF}$. British made. Geared slow motiou drive $6: 1$. Platic duat over. 8BA tapped front fixing.

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 MIDGET 280 下. 45 m HEATER TRARS, B.3 $\nabla, 1 \frac{1}{2}$.
 GEMERAL PORPOSE LOW VOLTAGE. Tapped outputa $8,4,5,6,8,9,10,12,15,18,94$ and 30 v. at $2 \mathrm{~s}, \ldots 3 / 4$
$1 \mathrm{smp}, 6,8,10,12,16,18,20,24,30,38,40,48,60.38 /-$ ADTO TRANBFORMERS $0-115$-230 vinput/Output CHARGER TRANSFORMERS. Input 200/2007

FULL WAVE BRIDGE CHARGER RECTIFIERS: 6 or 12r. outpute. $11 \mathrm{amp} .8 /-; 2 \mathrm{amp} .11 /-; 4 \mathrm{amp} .17 /-$.

E.M.I. $13 \frac{1}{2} \times 8 \mathrm{in}$. LOUDSPEAKERS
With fiared tweeter cone and ceramic magnet. 10 ซratta.
Bass ref, $45-60 \mathrm{cps}$.
Fiux 10,000 gans. State 3 or 8 or 15 ohm. Post 3 ;- each Alfo with twin tweeters., $\quad \mathbf{S 4}$ State 3 or 8 or 15 ohm, Post 3/- each Recommended Tenk Cabinet $\quad \mathbf{5 5}$

## IOW MINI-MODULE 65 / LOUDSPEAKER KIT Pont 5-

Triple speaker ayatem combining on ready cut batie 1 in. chipboard 15 in .81 in . Separste Bass, Middle and Treble loucapearers and crossover condenser. The heavy duty 5 in , Bass Woofer unit has a low resonance cone. The Mid-Range unit is specially designed to add drive to the middle register and the tweeter recreates the top end of the masical spectrum. Total resp TEAK VENEERED BOOKSHELF EMCLOSURE. $16: 10: 9$ in, Modern Scandinavian $\quad$ fated front design for Mini-Module.
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t RADIO BOOKS - LISTS S.A.E.

ALL HODELS "EAETR SPEAKERB" IM HTOCE BAKER 12in MAJOR £9

$30-14,500$ c.p.B., $18 i n$ tweter cone together with a BKKER ceramic maznet asombly having a fux density of 14,000 gaus a ad a toial fux ol
145,000 Maxwell reponance 40 c.p.s. Rated enonatice 40 c.p.s. Rated 15 ohm . Poit Free.

Module kit, 30-17,000 c.p.s. with ITeter, cromovar bame and
instructions. \&|l|0.0

BAKER "GRODP SOUND" SPEAKERS
 3 or 8 or 15 ohm 3 or 8 or $15 \mathrm{ohm} \quad 8$ or 15 ohm TEAK HI-FI SPEAKER CABINETS. FInted wood front, For 10 or 12 in round Loudaperiker 5 Pont $5 /=$ For $13: 8$ in or 8 in round Loudspeaker 5 Poat 5/ FOUDSPEAKER CABINET WADDING ${ }_{24}$ Pont 5/0

## THIS ELACCONETWEETERISOFTHEVERY

 ATEST DESIGN AND GIVES A HIGHER STANDARD OF PERFORMANCE THAN MORE EXPENSIVE UNITS The moving coil diaphragm gives a good radiation pattern to the higher trequencies and a amooth ertenaion of total response from $1,000 \mathrm{cps}$ to $18,000 \mathrm{cps}$. Size 3 ! $31 \times$ Rin. deep. Reting 10 watts. 3 ohm or 15 ohm models. $38 /$ - Post $2 /-$TWO-WAY CROSSOYER NETWORK $3,000 \mathrm{c} / \mathrm{s}$ With variable tweeter attenuator giving accurste high/low Irequency balance. Mounted on panel 5 !in. 4in, with control knob, tweeter and woofer leads and input $38 /=$

Horn Tweeters 2-18kc/a, 10 W 8 ohm or 15 ohm $30 /-$ De Laye Horn Tweeters 2-18 Kc/s, 15W, 8 ohm $60 /=$ TPECHAL OFFER ; 80 ohm 8 in 27 or 8 or 16 ohm 19/$5 \mathrm{ohm}, 3 \mathrm{in} . \mathrm{dia} . ; 64 \mathrm{in} ; 8$. $8 \mathrm{in} . \quad 2 \mathrm{in}$ dit, $35 \mathrm{ohm}, 3 \mathrm{in}$,

 LOUDSPEAKERS P.M. 3 OHISS, 61 in $3<21$ in $18 /-: 8$ in $35 /-; 10 \times 6 \ln 38 /--$
in. WOOFER. 8 watto mar. $20-10,000 \mathrm{cps}, 8$ or $15 \mathrm{ohm}, 38 j-$ ELAC 8 in. De Luxe Ceramic 3 ohm or 15 ohm $50 /$ in 4 watt or 10 in 5 watt or 12 in 6 watt, 3 or 8 or 15 ohm $\left.\begin{array}{l}30 /- \text { each. } \\ 0 U T P U T R A N S, ~ E L 84 ~ e t c . ~ \\ 5\end{array}\right)$ MIKE TRANS. $50: 1 \mathrm{~s}$ PEAKER COVERING MATERIALS. Samples Large 8.A.I. HOODIIAN8 OUTPUT TRANSFORDER 4 watt pugh pull for 100 WATT HIGH POWER P.A. AMPLIFIER
100 WATT HIGH POWER P.A. AMPLIFIER Matches all loudapeakers (4 ohm for full
power 100 watts British rating) Details S.A, $\mathbf{E}$. $\mathbf{S 6}$ Preet
ALL EAGLE PRODUCTS SUPPLIED AT LOWEST PRICES
ILLUSTRATED EAGLE CATALOGDE $5 /-$.

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Transistor Superhet. Ferrite aerial. $\underset{\text { wolt. }}{\text { E4 }}$ Transistor Superhet. Ferrite aerial. 9 volt.
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Add musical highlights and sound effects to recordinga. Will mix Microphone, records, tape and tuner
with separate controls into single output. 9 volt. BARGAN FM TDNER 88-108 Mc/a Six Transistor, 9 volk. Printed Circuit. Calibrated slide dial tuning. $\leq 10$ Walnut Cabinet. Size 7 4in
67.10

Chasuis only, less cabinet.
FM STEREO MOLTIPLEX ADAPTOR for above or $\quad$ SS
EARGAIN 3 WATT AMPLIFIER. 4 Tranistor
Push-Pull Ready built, with volume control. 8 y .10 Push-Pull Ready built, with volume control.
COAZIAL PLUG 1/3, PANEL SOCKETS 1/3. LIHE 3:7 OUTLET BOXES, SURFACE OR FLOSH $5 /-$
BALAKCEDTWIN EEEDERS $1 /$ yd, 80 ohme or 300 ohme Chrome Lead Socket 7/7. Phono Plugs $1 /-$, Phono Socket $1 / \%$, JACK PLUGS Std. Chrome $3 /-: 3.5 \mathrm{~mm}$ Chrome $2 / 9$, DIN SOCKETS Chassis 3-pin 1,7; 5-pin 2!-, DIN SOCXETS Lead 3-pin 3/7; $5-$ pin $5 /-$ DIN PLUGS $3-$ pin $3 / 7 ; 5-p i n ~ 5$
VALVE HOLDERS, $1 ;$; CERAMIC $1 / 7 ;$ CANS $1!-$.
E.M.I. TAPE MOTORS. 1207. or $\begin{array}{ll}240 \% \text {. AC. } 1,200 \text { r.p.m. pole } & 135 \mathrm{~m} A \\ \text { Spindle } 0.187 \% 0.75 i 0 . ~ S i z e ~ & 21 \\ 25 /=\end{array}$ 2! 2lin. (illustrated). Pont $3 /-$.
BALFOUR GRAM. MOTORS. 120 v . or 240 v . AC. 1,200 r.p.m. \& pole



Fig. 9.4. Quad adder type SN7483 logic diagram A total of 90 trensistors, including multi-emitter versions, are incorporated in this one package with 10 diodes and 70 resistors
package such as this could come in handy for all sorts of uses, apart from computer arithmetic.

Counters of a most useful type can be built using this package in conjunction with a shift register. Counting is, after all, just the repeated addition of one to the contents of a store. Counting down requires the subtraction of one; both operations are made simple with these adders.

If the carry input is grounded, and two changing words applied to the A and B inputs, the four sum outputs will only go to a 1 when the two input words are exactly opposite, or complementary. By feeding the sum outputs to a 4 -input NAND gate, a four bit noncquivalence gate emerges using only one and a half


Fig. 9.5. Using the SN7483 as a non-equivalence array. By using inverted data for one of the words, this array will detect equivalence instead. The outpuit goes low only when the two input words are exactly complementary
packages, a useful device indeed which can be better appreciated by looking at Fig. 9.5
The other adders in the series are the 7480 single-bit and the 7482 double-bit devices, both of which have greater versatility than the 7483 due to the extra pins available on the package.

## MSI SHIFT REGISTERS

Several types of shift register are available in this series, and between them they cover almost all the likely applications. All the shift registers use RS master/ slave flip-flops, but because the clock input to these devices is buffered, and therefore inverted, they shift data on the positive edge of the input clock.

As all these registers have different applications and we have already gone over basic principles in the TTL flip-flop section last month. It is only necessary here to have a brief look at them all. The block diagrams and package layouts are shown in Fig. 9.6.


Fig. 9.6. Package diagrams of $\mathbf{7 4}$ Series shift registers

## 7491 Eight-bit Register

The 7491 is an eight-bit serial register, and information must be both inserted and withdrawn serially, as no individual inputs or outputs are available from the separate flip-flops. As with the other registers the clock input is buffered and therefore represents only one load. Data input gating is provided allowing "input enable" logic to be performed.

## 7494 Four-bit Register

This register is organised as a dual source parallel to serial converter, data being entered by means of the asynchronous inputs. Two preset enable inputs allow the data to be entered from either of the two sources, through four AND-OR-INVERT gates. The common clock and clear lines are buffered, and a serial input is provided.

## 7495 Four-bit Register

The 7495 is a versatile register which has both parallel inputs and outputs provided. Parallel entry is synchronous, and is entered through AND-OR-INVERT gates which are controlled by the mode control input. When the mode control input is low, the register will shift data serially, from left to right.

Separate clock inputs are available for the two operational modes, and these are again controlled by the mode control input. By using external gates it is possible to make this register shift in both directions, i.e. right to left or left to right.

## 7496 Five-bit Register

The 7496 is similar to the 7494 except that asynchronous data can be entered from only one source, but parallel outputs from each flip-flop are available. A preset enable input is provided. As all inputs and outputs are available from each stage parallel/serial, parallel/parallel, serial/parallel and serial/serial operation may be employed.

## VERSATILITY

As can be seen, these shift registers leave little to be desired in the way of versatility, and of course by cascading several of them it is possible to build a register of any length which may be required. Apart from their use as storage devices it is also possible to build counters of various kinds, including the Unitary and Johnson types.

We have, in this brief introduction, only scratched the surface of the series 74 MSI , but the examples examined should set many an inventive mind buzzing, and there is really no reason why simple computers should not be designed by amateur constructors, using these devices, almost all of which are now available from advertisers in this magazine.

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TRIAC is the name used to identify the triode a.c. semiconductor bidirectional switch. It is basically two reverse blocking triode thyristors or silicon controlled rectifiers connected in inverse parallel, but with a common control electrode (gate). As the triac is a development of the thyristor, it is logical to describe this first and then compare with the triac to show the advantages and disadvantages of both devices.

## REVERSE BLOCKING THYRISTOR

The thyristor is a four-layer semiconductor device which has two stable states, one being the conducting state and the other the non-conducting state. The characteristics are shown in Fig. 1.

In the forward blocking region, i.e. when the anode is positive with respect to the cathode, an increase in the voltage across the device has little or no effect on the leakage current until the forward breakover voltage is reached. Increasing the voltage past this point causes the current through the device to increase rapidly, and the voltage across it to fall to about a volt.

The device is now in the conducting state and will remain in this state providing the anode current is above a certain minimum value known as the holding current. If the current through the device falls below the holding current, the device again reverts to the nonconducting state.

If the voltage across the thyristor is increased in the reverse direction, only a small current flows until the voltage reaches the reverse avalanche region where the anode current increases very rapidly and may destroy the device.

Looking again at Fig. 1, we can see that as the gate current $I_{g}$ is increased, the breakover voltage is reduced. If the gate current is high enough, the device will act like a rectifier.

Normally the thyristor is used in applications where the voltage across the device is well below the forward breakover voltage and is triggered into the conducting region by increasing the gate current. This method requires only small gate currents to switch large anode currents and is therefore the most useful method of turning the device on.

Once the thyristor goes into the conducting state, the gate has no control, and the device continues to conduct, therefore the gate current may be removed as soon as the device is turned on. This typically takes $20 \mu \mathrm{~s}$, and so a fast pulse can be used for triggering.

## TRIAC

The characteristics of the triac are shown in Fig. 2.
From the characteristics it can be seen that the triac operates like the thyristor, but can breakover into the conducting state for either polarity of applied voltage. The triac, like the thyristor, can be triggered into the conducting state by a gate signal, but unlike the thyristor it can be triggered by a positive or negative gate signal. Thus the triac has four possible modes of operation within first and third quadrants of current/ voltage characteristic:


Fig.2. Voltage current characteristic of a bidirectional triode thyristor or triac and circuit symbol

I(-) MT2 positive and gate signal negative with respect to MT1
I( + ) MT2 positive and gate signal positive with respect to MTI
III(-) MT2 negative and gate signal negative with respect to MTI
III(+) MT2 negative and gate signal positive with respect to MTI
MT1 and MT2 are "main terminals I and 2" and used in place of cathode and anode, because the device conducts in either direction.

With no gate signal, the triac blocks in both directions so long as the voltage across it remains below the breakover voltage. If the voltage does exceed the breakover voltage, the triac turns on, and providing the current through it is limited to a safe value, then the device is unharmed, unlike the thyristor which may be damaged by an excessive reverse voltage.

Once in the conducting state, the triac will remain so until the current through the device is reduced to less than the holding current, and only then will the device turn off.

If the voltage applied to a triac is reversed in a very short time, then the triac, instead of turning off as the thyristor would do, merely turns on in the opposite direction. In order to ensure that the triac turns off reliably, it is necessary to reduce the current through it to below the holding current for a period of time before reapplying a voltage. This limits the frequency of operation of the triac to somewhere over the 60 Hz
mark, but as the main use for the triac is in 50 Hz and 60 Hz control circuits, this is not a serious limitation.

## TRIGGERING

The triac may be triggered into conduction by either d.c., a.c. or pulsed signals applied to the gate. If d.c. is used, the voltage must exceed about 3 V , but the power in the gate circuit must be limited.

An example of d.c. triggering is shown in Fig. 3. This type of circuit is useful for switching large currents using a low current switch.
A.C. triggering is perhaps the most useful method to use for a.c. mains power control, because the gate signal is synchronised from the controlled supply. An example of a.c. triggering is shown in Fig. 4.

## TRIGGER DIODE

A.C. triggering may also be achieved by using a bidirectional trigger diode (diac), the characteristics of which are shown in Fig. 5.

From these characteristics it can be seen that the device has similar properties to that of the triac, but because the negative resistance portion of the characteristic extends over the whole operating range the device does not latch into the conducting state. A typical breakover voltage for the trigger diode is $\pm 30 \mathrm{~V}$.

An example of a circuit using a trigger diode and triac is given in Fig. 6. More will be said about this type of circuit later.


Fig. 3. Simple d.c. triggering for a triac


Fig. 4. Synchronous a.c. triggering for a triac


Fig. 5. Voltage current characteristic of a bidirectional trigger diode or diac


Fig. 6. . A diac used for synchronous a.c. triggering of a triac


Fig. 7. Relaxation oscillator with a u.j.t. for triggering a thyristor or triac

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Fig. 8. Phase control triggering of a thyristor


Fig. 9. Phase control triggering of two thyristors back to back in inverse parallel


Fig. 10. Full wave phase controk with a bridge rectifier arrangement


Fig. 13. Obtaining smooth power control of a lamp with two timing circuits

## UNIJUNCTION TRANSISTOR TRIGGERING

The third type of triggering mentioned is pulse triggering and this is sometimes achieved by using a unijunction transistor. The basic u.j.t. relaxation oscillator used for triggering purposes is shown in Fig. 7.

There are many other methods of triggering thyristors and triacs such as pulse transformers and neon lamps, but the last few examples illustrate the main methods of triggering.

The most common applications for the triac is in motor speed control, heater control, or light dimming.

By using the triac instead of the thyristor, a considerable saving in components may be made.

This coupled with the fact that the triac is less expensive than using two thyristors makes the triac very attractive indeed.

## PHASE CONTROL

In the majority of domestic controllers, such as lamp dimmers, phase control is used to vary the brightness. In phase control, current from an a.c. supply is connected to the load for part of each cycle. The length of time during each cycle for which the current is connected to the load, determines the amount of power dissipated in the load. Therefore if the load is a lamp, then the brightness of the lamp may be varied.

Using a thyristor for phase control, as in Fig. 8, we can achieve half-wave control, i.e. only positive halfcycles are controlled, negative ones being blocked by the thyristor. If the thyristor is triggered at point $\mathbf{A}$ in Fig 8, then the white portion of the waveform represents the power supplied to the load. Thus if the triggering point is moved to a point earlier in each half-cycle, then more power will be dissipated in the load, and vice versa.

## FULL WAVE CONTROL

If we use two thyristors, as in Fig. 9, then we can achieve full-wave control, one switching the positive half-cycles and the other switching the negative halfcycles. Unfortunately this method requires insulated gate signals for the two thyristors, which is commonly achieved by using pulse transformers in the gate circuits.

Yet another way of achieving full-wave phase control using a thyristor is illustrated in Fig. 10. This circuit has the great advantage that it may be used for controlling a.c. or d.c. loads, but for purely a.c. control it is an expensive method as it requires four diodes with a high p.i.v., and a current rating equal to that of the load.

By far the most simple and reliable method of fullwave a.c. control is the circuit shown in Fig. 11. This circuit uses a triac as the controlling element and requires only a simple trigger circuit to make it function.

The simplest practical triac phase control circuit is shown in Fig. 12. This circuit is extremely economical as it uses only four components, the function of which are as follows. VR1 and C1 form a phase shift network, the amount of phase shift varying with the setting of VR1.

When the voltage on Cl exceeds the breakover voltage of the diac, it conducts and Cl is partially discharged into the triac gate. The triac is triggered into conduction for the remainder of the half-cycle.

Unfortunately this simple circuit has a limited range of control the load current jumping from zero to some intermediate value as the control is advanced and only. then may be controlled smoothly up to full power. This effect may be reduced by using a circuit with a double time constant as shown in Fig. 13, giving very smooth power control.


Fig．14．Simple suppres－ sion of r．f．interference


Fig．15．The dimmer cir－ cuit in Fig． 13 is connected in series with the load

## INTERFERENCE SUPPRESSION

In thyristor and triac control circuits，the load current rises from zero to maximum in a few micro－ seconds．This sharply rising current causes radio frequency interference to be generated，which can cause great annoyance on the a．m．bands．Fig． 14 shows a very simple method of interference suppression．

A small inductor of a few microhenries is used to slow the rate of rise of current，but if used on its own， the interference can still be sufficient to be annoying． The addition of the shunt capacitor Cl further reduces the interference to negligible proportions for domestic applications．

## TRIAC LAMP DIMMER

The circuit given in Fig． 13 can form the basis of a triac lamp dimmer which can be fitted behind a wall switch plate，giving continuously variable light control．

It is advisable to incorporate the suppression shown in Fig． 14 to reduce interference，starting with component values of $0.1 \mu \mathrm{~F}$ for Cl ，and adjusting for the best results，with an r．f．choke rated at a minimum of 2 A ． This choke could be made by winding about 40 turns of thin single core p．v．c．connecting wire on a ferrite ring core or rod．

The triac should be rated at a minimum of 400 V p．i．v． 3A for domestic lamp dimming．There are several available that would suit the purpose；the author used a General Electric type SC35D in conjunction with diac type ST2．Some readers may prefer to try a quadrac which incorporates a triac and diac in one encapsulation．

The triac is mounted on a small＂L＂shaped bracket which is mounted on to a small component board．No difficulty should be experienced in constructing the unit and providing care is taken，the unit is perfectly safe．

The potentiometer may be wired to give full bright－ ness immediately the switch on the potentiometer goes on，and then dim the light as the control is advanced，or to give minimum brightness rising to maximum as the control is advanced．The triac should be rated to withstand initial surge of current which occurs due to the cold filament，when the lamp is first switched on．

## CHECKING AND FITTING

When the circuit has been wired up，the circuit may be tested by wiring it in series with a mains bulb and connecting these across the mains as in Fig． 15 ．The control should give smooth flicker－free control of the lamp up to full brightness，and the lamp should be extinguished by the switch．

Before fitting the dimmer，it is wise to wrap a piece of heavy polythene around the circuit to ensure that nothing shorts to the metal switch box．It may be found that the switch box is too shallow for the body of the potentiometer．If this is the case then it will be necessary to obtain a deeper box from an electrical shop．

After fitting the unit，the mains should be reconnected and the unit tried out．If everything has been carefully insulated，then no trouble should be encountered．

This dimmer should only be used with incandescent filament lamps rated at $230-250$ volts a．c． 50 Hz ．The lamp power should not exceed 500 watts．Fluorescent lights are not suitable． Association Amplifier＂will Camden Town Hall，Lission（free）by Sound＇ 71 will be held at（Final day 5 p．m．）secretary，A．P．A．E．，

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Blood is supposed to contain a fair quantity of iron, 1 mused. Could it be magnetic? It is difficult to remember ever having sufficient amounts of it to experiment with and, in any case, not being charged with the motive to become a second "Dracula", had never really given such matters another thought!

Nevertheless;" it now occurred to me that if, indeed, blood was magnetic (or perhaps, more likely, magnetically susceptible), the possibilities could be quite awe-inspiring. For example, the earth's magnetic field might have some influence on the flow of blood around our systems, and what about the effect of stray fields from transformers and the like? The effect on the capillary action of the smaller blood vessels could be quite dramatic could'nt it? Surely, I told myself, things were getting out of all proportion.
Not to be deterred, I changed tack slightly a way from the gory path, and began entertaining thoughts about the chances of inducing currents in the nervous system through similar agencies. "Do you think", I butted into the, now one-sided, conversation, "that it would be a possibility to influence the brain with magnetic fields?". As you may imagine, the nurse knew little more about what I was talking about than I did, and she replied in a hushed whisper, as though to one demented, "You've nearly given your pint, I 'spect you'il feel better after your tea ' $n$ biscuits".

Putting an optimistic face on the situation and dropping back onto my pillow, I lapsed into day dreaming again. Electric currents can be induced in copper wires, so why shouldn't the same apply to the effects of magnetism on liquids.

## Subtle influence

If such really is the case this could mean that, quite unbeknown to us, magnetic fields might have some kind of modulating influence upon certain parts of the body and, who knows, perhaps even modify our very thoughts in certain subtle ways!

No, this was too much to accept in one go; the loss of blood must obviously be having its effect 1 considered, so decided to re-examine the idea later and in the meantime put up with the good-natured ministrations of my N.B.T.S. attendant.

Two months later I was chatting with an old friend of mine, a librarian, about this rather crazy idea of mine and, would you believe . . ., he referred me to a paper written only a couple of years or so ago about the effect on reaction-time performance by magnetic fields! The paper concerned was pretty lengthy, so only the main import of its discussion will be given here.
Apparently, three individuals of the medical profession, and all from the Syracuse area of New York, have discovered quite a profound relationship between the difference in the time taken to react to the appearance of a light source with and without the influence of a fairly weak ( 5 to 11 gauss) magnetic field. Initially, the field, which was generated by a couple of 14.5 in diameter Helmholtz coils placed near the head, was nonoscillatory and showed no effect.

Later, instead of a d.c. current being used to drive the coils, a low frequency a.c. signal was employed. Immediately, there appeared to be a perceptible change in the rate of response and, indeed, this was confirmed over some four groups of 50 subsequent trials. Every time the field was present a distinct increase in the reaction time occurred.
It is extremely difficult to know just what to make of their findings. One thing though is sure, never will I go out again in a magnetic storm without first donning my lead-lined crash hat!

## By any other name

Only a matter of months ago I was nattering about tomatoes showing electrical reactions to the application of heat to their skins! Well it seems they are not the only ones among the vegetable kingdom to "blow their cool" in this way! The latest addition to the "psychosensitive" list is the "veg" which one would have thought held first place; it's the rose.

This time it is the Russians who have un-earthed the effect. It seems that hundreds of experiments have recently been performed at the Moscow Agricultural Academy which reveal that in addition to the rose reacting to tactile (touch) stimuli, it also displays a form of crude memory. According to Pravda, the Communist newspaper, the researches show that
rose bushes exhibit electrical activity similar to nerve discharges observed in man!

All this has yet to be demonstrated to me; perhaps we shall be hearing a lot more of these findings in the not too distant future though.


## So long

Wouldn't it be nice if we could gain access to the methods (whatever they may be) employed in man and other animals for generating huge time-constants? I mean if someone says "See you in an hour and a hall", the chances are that, provided they said where, you will see them.

Yes, I agree, we would probably be using our watch, or maybe available clocks; who knows, we may even be relying upon the position of the sun in the sky. Assuming though that none of these methods were available, we would still feel fairly confident that the time period could be judged with a reasonable degree of accuracy. How?

Well, "hunger-pains" aside, no one is by any means certain. It could have an oscillatory principle I am told, and someone has even suggested a pulse coincidence basis.
Actually, in electronic practice, this latter idea works well for generating long time-constants; perhaps you would like to try it. Fig. 1 shows the general arrangement. An AND gate receives the outputs from two astable pulse generators, the frequencies of which are both very low and slightly different; the gate thus only returns an output when the input pulses are coincident.
With the frequencies given, only one pulse should appear at the output of the ga:e approximately every hour! This can be used to set a bistable or whatever application one may have in mind.
Only one problem exists with this kind of timer ... one has to wait such a long time during the setting-up periods to establish that the correct frequencies exist!


Fig. 1.


T is always interesting to note the developments in marine electronics during the past year at the London International Boat Show. Last year in our Boat Show report we noted that there were more firms displaying electronic gear and a greater range of instruments available; the same trend is repeated this year.

The advantages of solid state electronics in marine equipment were particularly evident from two new equipments, these are: the Acoustron 2-11, forward looking echo ranger and computer by Apollo Electronics Ltd., and a digital readout echo sounder by Marine Electronics Ltd. These instruments use integrated circuits to provide, compact design with clear, unmistakable readout, low power consumption and greater reliability than more conventional designs.

Acoustron 2-11 will no doubt interest almost every owner of power craft of a reasonable size. This computerised sonar uses two narrow transducer beams to probe under and ahead of the boat. The resultant echoes are used by computer circuitry to predict the possibility of grounding and to give visual and audible warning of impending danger. Warning time and depth warning can be selected as can the memory time to suit various coastlines and conditions.

## LOW COST RADAR AND SONAR

Low cost is always an attraction when buying equipment, particularly if it is well constructed and has a good specification. This year has seen the first under $£ 500$ radar for small boats from Electronic Laboratories (Marine) Ltd.; the radar, called Seascan, is completely housed in two units-the scanner transceiver and the display unit. It has a working range from 25 yards to 16 nautical miles, which is covered in six switched ranges. If this radar is as popular as the Seafarer depth sounder from the same firm, and we think at the price ( $£ 450$ ) it will be, both yachtsmen and Electronic Laboratories should be very pleased.

Space Agc Electronics Ltd. are marketing what is claimed to be the world's most powerful small boat echo sounder for $£ 35$, using neon readout, and an auto pilot costing $£ 99$ that is claimed to be the world's cheapest pilot for small yachts and motor cruisers. This company is one to watch for future developments and they have said that they should be showing some interesting new instruments next year. Marine Electronics are marketing a neon echo sounder for $£ 39$ with built-in depth warning; they also sell a meter type sounder and the digital readout unit mentioned earlier.

## WIND SPEED INDICATOR

New developments in equipment from Brookes and Gatehouse consist of a simplified, lightweight wind direction and speed indicator-Hengist and Horsa model C -although primarily intended for the cruising yachtsman, these models will no doubt appeal to the racing man since they are lighter in weight, more simple to use and the masthead unit will give slightly less windage.

From chatting to various stand holders, it is apparent that most of the firms are engaged in development of various new equipments and some, such as Baron Instruments and Space Age Electronics, are hinting strongly of exciting new projects next year. The added competition from new firms that have launched marine electronic equipment within the last few years, has brought about a fast moving industry that is quality and price conscious and that will have to be up to date to survive.

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## Shipwreck

Sir-I recently finished making your game "Operation Seasearch" and I am writing to point out a defect in the circuit given for this game in your December 1970 edition. I feel that this should be pointed out to other readers who may be considering building the game. This defect will not usually cause difficulty but it may in certain circumstances as explained below.

This difficulty is as follows. With reference to the enclosed diagram, Fig. 1, it can be seen that if the "Raider" is at say, $A a$, and the "Supply Ship" at Ba, current can pass to $S 5$ when it is in position " $A$ " or " $B$ ". If S 6 is in position " $a$ ", current will be passed to $S 2$ a and thus to LP1 when S9 is depressed. Thus $\mathbf{S 5}$ can be in position " $B$ " and on depressing S9 LP1 will glow showing that the raider has been detected, when in fact it hasn't. This situation can occur in a number of positions.
D. W. Guest, St. Helens, Lancs.


Fig. 1

Mr. Guest is quite right; this is a point that was omitted in the original article. The condition occurs when either searching ship is in line with the "Raider" along one axis and also in line with the "Supply Ship" along the other axis. Overcoming the condition can be done quite simply by inserting a second pole of each push button where indicated. This was not done in the prototype on the grounds of economy. as a second pole was needed in the later "Submarine Game", and three pole push buttons come a bit expensive!
Actually, in the game situation the phenomenon is not so drastic as it might appear. Firstly, the chances of the right conditions arising in any one game move are approximately 70 to 1 against. (Suffice to say that in innumerable games, it has occurred only two or three times.) Secondly, since both players take turns to control the "Raider", the chances against each player are exactly equal.

On the few occasions that the situation has arisen, we have attributed the discovery of the "Raider's" position to an accidental sighting by long-range aircraft, which satisfied our sense of the proprietry of things-it, gave the searcher another "fix" on the "Raider's" position just as he has in variations 3 and 6, page 989.-D.R.D.

## Economic damper

Sir-May I congratulate you on the series of articles currently running on using logic i.c's; they are very useful to me. Also, the "Digital Clock" is a very useful design but, as is very often the case, the difficulty in obtaining parts (Nixie tubes in this case) at the right price, tends to put a damper on one's enthusiasm.

After several enquiries and visits to shops I may be able to satisfy my requirements, given several more weeks. Of course, I know it is possible to get anything if your are prepared to pay top prices, but I begrudge doing this when I know that someone must be selling the equivalent article much cheaper.

Referring to Gerry Brown's brake fluid level detector (On The Fringe, November 1970 issue), I had the same idea myself a few months ago but on trying it out I found that as soon as the fluid was shaken up a thin film of fluid adhered to the insulated cap,
thus permanently shorting the probe, see Fig. 1 (below).

Did Mr. Brown have this trouble or was it just a theoretical circuit?

John Westmoreland, Bispham,


Fig. 1

## Full thump

Sir-Reference to the "Fuzz Circuit" included in Ingenuity Unlimited, December 1970 issue. Having constructed this circuit, I found as have probably many of your readers, that it needs quite a considerable clout, on even the lowest guitar string (open $E$ ) to set off the trigger circuit, once it is stable, and it has zero response to the top $E$ and $B$ strings at standard tuning.

Modifying the circuit by wiring resistor R1 ( $1 \mathrm{M} \Omega$ ) directly between the base and collector of TR1 and changing the value of C 5 to $10 \mu \mathrm{~F} 10 \mathrm{~V}$ working should cure the above problems.
B. K. Cox,

Wellingborough,
Northants.

## DECIMAL CURRENCY AND P.E.

Readers throughout the world are probably aware that British currency is being decimalised with effect from February 15, 1971. The following notes are issued for their guidance when writing to Practical Electronics.

1. Cheques and postal orders should show amounts payable in decimal currency. Leaflets are available at all branches of British Banks.
2. Readers' cheques and postal orders written in $E s d$ will not be accepted by the publishers of Practical Electronics after February 15, 1971.
3. Handwritten cheques of more than $\& 1$ which include new pence, should use a hyphen in piace of the decimal point (e.g. 67-80, £30-06).
4. Postage rates in the U.K. on and after February 15 will be $2 \frac{1}{2} p$ second class and 3 p first class for up to 4 ounces. Old $\mathcal{E}$ sd stamps used on and after this date must be at the new rate of $6 d$ second class, 7d first class for up to 4 ounces. Readers requiring a reply to correspondence are asked to use the correct postage rate on s.a.e.

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SPECIFICATIONS（Z．50 units are inter－ changeable with $Z .30$ s in all applications） Power Outputs
2.3015 watts R．M S into 8 ohms using 35 volts： 20 watts RM S，into 3 ohms using 30 volts．
Z．50 40 watts R．M S．into 3 ohms using 40 volts
30 watts R M．S．into 8 ohms，using 50 volts
Frequency response： 30 to $300,000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$
Distortion： $002 \%$ into 8 ohms
Signal to noise ratio：better than 70 dB un－ weighted．
Input sensitivity： 250 mV into 100 Kohms
For speakers from 3 to 15 ohms impedance
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Designed specially for use with the Project 60 system of your choice．
Illustfation shows PZ 5 to left and PZ． 8 （for use with Z．50s）to the right．Use PZ． 5 for normal 2.30 assemblies and PZ．6 where a stablised supply is essential．
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## SPECIFICATIONS

Input sensitivities：Radio－up to 3 mV ．Mag．p．u 3 mV ：correct to R．I．A．A．curve $\pm 1 \mathrm{~dB}: 20$ to $25,000 \mathrm{~Hz}$ Ceramic p．u．－up to 3 mV ：Aux－up to 3 mV ．
Output： 250 mV ．
Signal－to－noise ratio：better than 70 dB
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Front panel：brushed aluminium with black knobs． and controls．
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## SPECIFICATIONS：

Number of transistors： 16 plus 20 in I．C．
Tuning range ： 87.5 to 108 MHz
Captureratio： 1.5 dB
Sensitivity： $2 \mu \mathrm{~V}$ for 30 dB quieting： $7 \mu \mathrm{~V}$ for full limiting．
Squelch level： $20_{\mu} \mathrm{V}$
A．F．C．range：$\pm 200 \mathrm{KHz}$
Signal to noise ratio：$>65 \mathrm{~dB}$
Audio frequency response： $10 \mathrm{~Hz}-15 \mathrm{KHz}$ （ $\pm 1 \mathrm{~dB}$ ）
Total harmonic distortion： $0.15 \%$ for $30 \%$ modulation
Stereo decoder operating level： $2 \mu \mathrm{~V}$
Pilot tone suppression： 30 dB
Crosstalk： 40 dB
I．F．frequency： 10.7 MHz
Out put voltage： $2 \times 150 \mathrm{mV}$ R．M．S
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# Sinclair IC10 O16 Micromatic 

## IC10



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Circuit Description
The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class $A B$ output is used with closely controlled quiescent current which is independent of temperature. There is generous negative feedback round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory. Each IC10 is sold with a comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include oscillators, etc. The pre-amp section can be used as an RF or IF. amplifier without any additional transistors.

## Specifications:

Output: 10 watts peak, 5 watts RMS contunuous. Frequency response: 5 Hz to $100 \mathrm{kHz} 1 \pm \mathrm{dB}$. Total harmonic distortion: Less than $1 \%$ at full Total ha
output.
Loutput
Load impedance : 3 to 15 ohms.
Power gain: 110 dB ( $100,000,000.000$ tımes) total.
Supply voltage: 8 to 18 volts. (A Sinclar power unit, PZ.7 is available for mains operation).
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