PRACTICAL ELECTRONCS MARCH 1971 171/2 p (3/6)

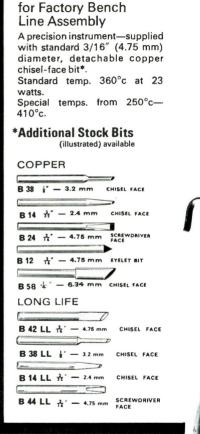
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ADCOLA 64

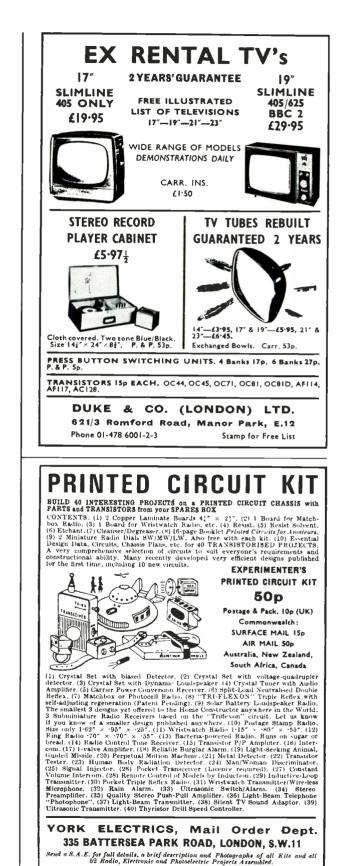


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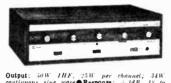


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All Silicon Transistors for Stability Cleaner Sound Extremely Wide Power Bandwidth and Frequency Response 50W IHF Power Outnut Specially Selected Low-Noise Preamp Transistors Two Printed Circuit Boards for Fast Easy Assembly Convenient Front-Panel Stereo Headphone Jack Teakfinished Extruded Aluminium Front Panel Two a.c. Convenience Outlets



Output: 50W IHF, 25W per channel; 34W continuous sine rearce Response: ±1dB, 18 to 30,00012-00 tuput Impedances: 4 transph 16 ohme, plus stereo leedophonee IM Distortion: under 1% of 60Hz and 7,000Hz mixed 4:1 at rated power ● Input Sensitivity: Magnetic Phono. 5mV; Tuner and Auxiliary, 500mV Power Require-ment: 230-250V; 500Hza.c. Rec. List Price 234 572 Assembled £30.45 £29-30 Teak Case #5 Extra

KG-625 Deluxe 6in Vacuum Tube Voltmeter Kit

Huge 6in Meter Scale \otimes Ranges: $d.e. \theta - \theta$. $1^{-5}-5-5-50-150-500-15,5001$ full scale. \oplus Accuracy: $\pm 3^{-6}$. \oplus full scale reading \oplus Input Resistance: 11M Ω to 1,500 Ψ . Ranges: a.e. 0.-15-5-5-5-5-10-500-1,50-500-1,500 full scale. a-i2-140-120-140-120-1,40400-4,200 V Juit sense Accuracy, 5% Frequency Response: $\pm 1dB$, 30Hz 3 MHz; $\pm 3dB$, 30Hz to 5MH2 Ohm-eter Ranges: 0-1,000-10,000 ohms; to $3MHz_1 = 3dB, 30Hz_10, 5MH$ meter Ranges: $\theta = 1,000-10,000$ $\theta = 1-10-100-1,000 AL\Omega$ Battery: Recommended List Price £24.97 $\frac{1}{2}$ £12.60



KG-375A Deluxe Solid-State Auto Analyzer Kit

Tune-up and trouble-shoot any car, perform actual road tests

It's several testers in one ... do all this

Set Engine Idle and Automatic Trans-mission Shift Points Detect Condition of Point Surfaces Detect Condition of Check Repersators for both Current and Voltage Output Find Poor or Open Earth Circuits Detect Variation in Dwell Angle. Recommended List Price £23:87.5: £16-80

- WHY NOT BUY THE PAIR?

KG-371 Deluxe Solid-State Timing Light

Performance surpasses assembled units costing much more

Helps Set Ignition Timing Checks Synchronisation of Double Breaker Arms Checks for Sticking Automatic Spark-Advance Mechanism Oblecks Distributor Cam Wear Bulli-in d.c. Power Supply Reliable Solid-State Circuit Your car gives More miles per gallon; Improved performance: Greater reliability. per gallon; Improved perto Recommended List Price : Available Assembled Only rice £12.50 £9.95





KG-620 41 VTVM KIT ★ NEW! SPECIFICATIONS

Ranges: 0-1:5-5-15-50-150-500-1,500 V full scale; with optional High-Voltage Probe, to 25,000 V. Accuracy: $\pm 3\%$ Of full scale reading. Input Resistance: 11 megohms (1 meg in probe) up to 1,500 V. 0 .

Ranges (Tmu); 0-1:5-5-15-50-150-500-1,500 V full scale (p-p); 0-4:2-14-42-140-420-1,400-4,200 V full scale. **Decibels**: -1θ to +65 in 7

megohms. Battery 11 V size U2.

Response: $\pm 1dB$, 30Hz to 3MHz; $\pm 3dB$, 30Hz to 5MHz; with optional H.F. Probe, to 250MHz.

Accuracy: 1.5% of full scale reading.

Ranges: 0-1,000-10,000-100,000 ohms; 0-1-10-100-1,000 meg-ohms.

Centre Scales: 10, 100. 1,000, 10,000, 100,000 ohms; 1 and 10

Recommended List Price £18-271: £9.95 Assembled Price £14 (RR Price £30)



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Introducing The New "Delta" 10 watt Enclosure

Incorporating the famous EMI 150 set consisting of a 13×8in. bass unit with a high flux ceramic magnet and a concentric tweeter impedance 8 0 20 watt peak handling power (10 watts RMS) or 20 watts peak.

Heavy duty 16mm infinite baffle case in superb quality genuine golden teak veneers with solid mahogany contrasting leading edges. High quality foam loaded cloth fret. Acoustically loaded "Jason" rotating badge in genuine gold leaf for horizontal or vertical operation. Size 19in. × 10in. × 10 in. Weight 16lbs. A price break through at only Carriage etc. 50p singly. £12.50

Carriage free in pairs.

Jason Senior 20W Enclosure. As above but with super heavy duty bass unit with 3-61b magnet in Magnadure II maderial with 1-51n speech coil and super tweeter giving frequency range of 20-20,000Hz. Blandard 80 for linepdance in beautifully linihed heavy teak veneers. Size 121x 12 x 23in. 20 Watts RMS, 40 watts peak. At a super keen price $\pm10+50$ or ±30 and ±10 m arriage and ±0.52 b for 1 or 2.

PLINTHS & COVERS for Garrard (all take current models except heavy transcription types). Beautifully heavy solid perspex top with "stereo" badge high quality base with solid wood sides machined ready for R/P deck to drop in without any further work. Terrific value at only £3.45 complete. Carr. & Insurance 37 p.





above.



Double tuned dis

USED

50µ.A

100µA

100.00

50μΑ 50-0-50μΑ 190μΑ 100-0-100μΑ

500-0-500µA

200µA

500µA

1mA

10mA

50m A

100mA 500mA

1.4

10V d.e.

50μΛ ... 50-0-50μΑ

200µA .

ImA

5m 4

100μA 100-0-100μA

500µA 500-0-500µA

1-0-1mA

5mA ... 10mA ...

 50μA
 22-80

 50-50μA
 £2-80

 100μA
 £2-80

 100-0-100μA
 £2-87

 500μA
 £2-25

 500μA
 £2-80

 42-90
 £2-90

50-0-50uA

100-0-100µA

mA

28.60

23.60 23.10 23.10 23.10 23.10 22.87 22.75

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Type MR.65P. 38in

£8·371 £2·75 £2·75 £2·60

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Type MR.52P. 21in square fronts.

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CLEAR PLASTIC METERS

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"SEW" CLEAR PLASTIC METERS

"SEW"

TYPE SW. 100

100 x 80 mm

500μA 1mA 20V d.c. ...

20V d.c. 50V d.c. 300V d.c. 1A d.c. 5A d.c.

300V a.c

50mA

100mA

500mA

30A ... 20V d.e.

50V d.e

150V d.c

300V d.c.

300V d.c. 300V a.c. 300V a.c. 8 Meter

ImA VU Meter

1A a.c.* JA a.c.*

5A a.c.* 10A a.c.* 20A a.c.*

30A a.c.*

20V d.e. 50V d.e.

300V d.c

300V d.c. 15V a.c. 300V a.c. 8 Meter

- 1mA VII Meter

1.4 a.c.* 5.4 a.c.*

10A a.c.*

-0.4 a.c.*

30.A a.c.*

20V d.c. 50V d.e.

50V d.e. 150V d.e. 300V d.e. 15V a.e. 50V a.e. 150V a.e. 300V a.e. 500V a.e. 500V a.e.

8 Meter

Shin fronts.

1A. 5A. 15A

VU Meter

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INDUSTRY.

TYPE S-80

BO mm square fronts

50μA **£3·12** 50•0-50μA **£2·97**

mannation

50μA 50-0-50μA 100μA 100-0-100μA

200µA .

1mA . 1-0-1mA

140-16 2mA 5mA 10mA 20mA

50mA 100mA

50μA ... 50-0-50μA

10mA

50mA

100mA

500mA

1A.... 5A....

50-0-50μα 100μΑ ... £2:10 100-0-100μΑ £1:87; 200μΑ ... £1:87; 500μΑ ... £1:80 500-0-500μΑ £1:50 100Λ ... £1:50 500Λ ... £1:50

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500μA £1.50 500-0-500μA £1.87

29.97

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£1-50

£1.50 £1.50 £1.50

¢1-50 £1-50

"SEW" BAKELITE

PANEL METERS

Type MR.65 31in square fronts

Type MR.45P. 2in square fronts

.. £1-371

\$1 37

100

100μΑ 100-0-100μΑ

100-0-10 500μA 1mA 20V d.c. 50V d.c.

- 300V d.c

eriminator. Ample output to feed most amplifers. Operates built ready for use. Fantastic value for money. **26 27**], P. & P. 12[P. Stereo multiplex staptors **24**.007]

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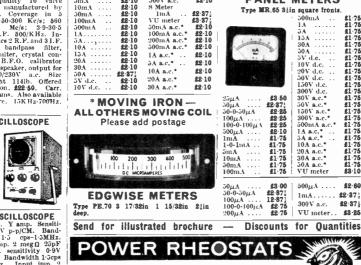
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MULTIMETERS High quality 97 range instrument which measures a.c. and d.c. Voltage. Current, Resistance and Power Output Ranges d.c. volts 250mV-10.000V (10 meg Ω -110 meg Ω iuput). D.c. current 10(A-25Å, Ohms. 0-1,000 meg Ω a.c. volt 100mV-250V (with R.F. measuring head up to 250MHz) n.c. current 10(A-25Å, Power output 55 micro-watts-5 watts. Operation 0/110/200/250V a.c. Sumplied in perfect condition compute with Supplied in perfect condition complete with circuit lead and R.F. probe. **£25**. Carr. 75p.



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High quality ceramic construction. Windings embedded in vitreous Fight quarky extrainer construction. Windings endoeders in virtuous enamel. Heavy duty brank wiper. Continuous rating. Wile range ex-stock Single hole fixing, jim. dia.shafts. Bulk quantities available. 25 WATT. 10/25/50/100/250/500/1.000/2.5000 or 5.000 ohms, 17.21. F. & P. 74 50 WATT. 10/25/50/100/250/500/1.000/2.5000 of 5.000 ohms, 17.21. F. & P. 74 100 WATT. 10/21/50/100/250/500/1.000/2.5000 ohms, 11.271. F. & P. 74 100 WATT. 10/21/50/100/250/500/1.000/2.5000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 of 5.000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 of 5.000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 ohms, 12.721. F. & P. 74 100 WATT. 10/50/100/250/500/1.000/2.5000 ohms, 12.500 oh P. 71p. MARCONI TF142E DISTORTION FACTOR METERS, Excellent condition. Fully tested. Carr. 75p. 120

TRANSISTORISED L.C.R. A.C. MEASURING BRIDGE



5

DESIGNS!

BAKELITE PANEL METERS

GOVERNMENT

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1A d.c. 5A d.c.

Type MR.38P. 1 21/32in square fronts

300V a.c

VU Meter

150mA

200m A

300m A

500mA 500mA 750mA 1A

2A . . .

3V d.c

3V d.c. 10V d.c. 15V d.c. 20V d.c. 100V d.c. 150V d.c. 300V d.c.

300 V d.e. 500 V d.e. 750 V d.e. 15 V a.e. 50 V a.e. 300 V a.e. 500 V a.e. 8 Meter 10 A

IniA . VU meter

10V d.e. 20V d.e.

50V d.c.

300V d.c. 15V a.c. 300V a.c. 8 Meter

lmA VU Meter

IA a.c.*

5A a.c.*

10A a.c.*

20A a.c.*

30A a.e.*

600mA

1.A

15A

30A

50A . 5V d.c.

5V d.c. 10V d.c. 20V d.c. 50V d.c. 150V d.c. 300V d.c. 300V a.c.* 150V a.c.* 300V a.c.*

300 V a.e.* 500mA a.e.* 1A a.e.* 5A a.e.* 10A a.e.* 20A a.e.* 30A a.e.* 50A a.e.* VU meter

500µA

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VU meter. . 48-25

5A

10A

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A new portable bridge offering ex-cellent range and accuracy at low cost. Ranges: R. $1, 0, -11 \cdot 1$ means cost. fanges: R. 1Ω-11·1 megΩ 6 Ranges ±1%. L.1 μH - 1 1 HENRYS 6 Ranges -2%. C. 10pF ±1110 m Fd. 6 . TURNS RATIO 1:1/1000-110°, Pitcher yolloga of

Ranges $\pm 2\%$. TURNS RATIO 11/1000 1:11100. 6 Ranges $\pm 1\%$, Bridge voltage at 1,000 cps. Operated from 9 volts. 10 μ A. Meter indication. Attractive 2 tone metal case. Size 7: $\times 3 \times 2$ in. **\$20**. P. & P. 25p.

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\$125. TT15. TRANSISTOR TESTER. Full range of facilities for testing PNP or NPN transistors in or out of circuit. \$37.50. Carriage 50p per item.

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1N4004	10p AC188	80p BSY95A	15p	IR5 185	85p 30C17 25p 30C18	801		56p 56p
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IN4007 IN4148	20p ACY19 71p ACY20	25p BY126 221p BY127	15p 20p	IU4 IU5	80p 30FL1 471p 30FL12	77) 924)	EY87 4	40p 21 p
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2G371	80p AD161 22 p AD162	871p MPF102 871p MPF103 991 MPF104	86p	5Y3 5Z4G	80p 30PL14 871p 35L6	851 471	KT88 #1	67 <u>}</u>
2G374 2G381	2710 AF114 259 AF115	821p MPF104	871p 40p	6/30L2	769 35W4	2.51	m U 14 4	40p 40p
2N696 2N697	17 p AF116	8910 NKT213	25p 15p	6AC7 6AG7	20p 35Z4 871p 35Z5	26) 35)	PC86 5	71p
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2N1304 2N1305		42 t DINT YZ TD 1 O 44	26p	6BR7 6BR8	85p DK91 65p DK92	35 45	PCF805 '	50p 75p
2N1306 2N1307	25p AUY10	971p	871p	6BW6 6BW7	80p DK96 67 p DL92	40	PCF806 (65p
2N1308 2N1309	80p 85p 85p	71P OA5 121p OA10	15p 25p	6BZ6	82 p DL94	401	PCL82 7	71p 39p
2N1613	224p BC108	121p OA47 121p OA70	10p 10p	6C4 6CD6	80p DL96 £1-15 DM70	8711 3211	PCL83 PCL84	65p 44p
2N1711 2N1889	82 p BC113	25p OA79 40p OA81	10n	6CL6 6CW4	50p DY86 621p DY87	8241 851	PCL85 4 PCL86 4	71p 71p
2N 1893 2N 2147	50p BC125	66miO 4 85	10p 12ip 10p	6F1 6F6G	62 p E88CC 25p E180F	6211 751	PFL200	55p 55p
2N2160	6210 00120	55p OA90 171p OA91 121p OA95	10p 7ip	6F13	85p EABC80	8211 501	PL81 4	71p 46p
2N2193 2N2217	2710 BC148	12 p OA95 20p OA200	7 <u>∔</u> ₽	6F14 6F15	60p EAF42 55p EB91	161	PL83 4	40p
2N2218 2N2219	BC167	15p OA202	7ip 10p	6F18 6F23	40p EBC41 771p EBC81	5211 8211	PL500 '	85p 75p
2N2368 2N2369	17 p BC177	171p OA210 871p OC19	17#p 87#p	6H6 6J4	771p EBC81 15p EBF80 471p EBF83	401 4211	PY32	80p 55p
2N2369A	20p BC1801	871p OC20 20p OC22	971p 471p	6J5	20p EBF89	2912	PV22 8	21p 21p
2N2484 2N2613	359 BC184L	20p 0.023	50p	6J5GT 6J6	30p EBL21 17ip EC86	60.		avn
2N2646 2N2904	SOD BCY30	221p OC24 25p OC25	50p 87ip	6J7 6K8G	4219 EC88 80p ECC40	551	PY83 3	80p 71p
2N2923 2N2924	1710 BCY32	80p OC26 50p OC28	25p 62ip	6L6GT 6LD20	45p ECC84	- 201	PY88	40p 50p
2N2925	17 p BCV34	20p OC29 25p OC35	621p 50p	6Q7	371p ECC88	40	PY801 1	50p
2N2926G 2N2926Y	121P BCY38	80p OC36	62 i p	68A7 68G7	35p ECF80 30p ECF82	351 851	U26	75p 75p
2N2926O 2N3053	1219 BCY43	200 0.042	25p 80p	68J7 68K7	85p ECF86 80p ECH21	6211 5711	U50 U52	80p 30p
2N3054	50p BCY72	80p OC44 171p OC45	17jp 15p	68L7 68N7	80p ECH35 274p ECH42	60j 65j	U191 '	70p 40p
2N3055 2N3391A	759 BCZ11 809 BD121	871p OC46 65p OC70	271p 121p	6SQ7 6U4	40p ECH81	2711	U282 4	40p
2N3416 2N3570	8719 BD123	821p OC71	15p 25p	6V6G	25p ECL80	451	U801	71p £1
2N 3702 2N 3703	871 1910 BF115	96n OC73	800	6V6GT 6X4	821p ECL82 25p ECL83	62 1	UABC80 UAF42 5	84p 21p
2N3704	1719 BF117 159 BF167	471p 0C74 96n 0C75	80p 25p	6X5G 6X5GT	271p ECL86 271p EF37A	4211	UBC41 4 UBC81	21p 71p 40p
2N3705 2N3706	2210 BF173 150 BF180	80p 0070	25p 40p	10C2 10F1	50p EF39 90p EF40	401	TIBERO 1	36p 85p
2N3707 2N3708	171p BF181	871p OC78 371p OC78 991 OC81	20p 25p	10P13	55p EF41	6211	100084 4	anb
2N3709 2N3710	191n DF182	260 OC81D	20p	10P14 12AT6	25p EF80	251	UCF80 5	40p 21p 55p
2N3711 2N3819	181p BF184 181p BF185 36p BF194 86p BF194	25p OC84	25p 25p	12AT7 12AU7	20p EF85 25p EF86	851 3211	UCH49 1	85 m -
2N3903	850 01100	15p OC139 871p OC140	25p 871p 20p	12AX7 12AV6	80p EF89 80p EF91	2711	UCH81 2	21p 35p
2N3904 2N3905	871p BF224	80p 00170	20p 25p	12BA6 12BE6	321p EF92	3711 3211	UCL83 (60p
2N 3906 2N 4058	871p BF225 171p BF244 171p BFY19	30p OC170 471p OC171 221p OC200	80p 871p	12BH7	32 p EF184	351	UF80 3'	50p 71p
2N4059 2N4061	250 21.41.4	22 p OC201	471p.	19AQ5 20D1	321p EH90 45p EL34	5241	UF89 1	40p 85p
2N4062	221p BFX29	22 p OC201 22 p OC202 30p OC202 32 p OC203 32 p OC204 32 p OC204	621p 871p	20F2 20L1	75p EL33 £1 EL41	551	UL84 8	60p 21p
2N4286 2N4287	15p BFX44 171p BFX85 15p BFX85	8710 OC204 400 OC205 8810 OC207 8810 OC207 8810 OC271	40p 621p	20P1 20P3	50p EL42	5711	UV41 4	40p 80p
2N4288 2N4289	171p Dr A00	88 p OC207	621p 75p 971p	20P4	60p EL81 £1 EL84	251	VR105/30	
2N4290 2N4291	100 DEVOC	25p ORP12	50p	20P5 25L6	21 EL85 871 p EL91	41 g 26 g	VR150/30	71p 25p
2N4292	15p BFY18 15p BFY20	821p OCP71 25p ORP12 25p ORP60 621p P346A	40p 25p	7EN	ER DIODES		COND	
2N 5354 2N 5355	271p BFY50 271p BFY51	22 p PL4001	14p	400W (3	3 to 33V)	15p	SEND SAE	
28102	259 BFY52	20p PL4002 22 p PL4003	15p 16p	1.5W (2- 10W (3.9	4 to 200V) 1 9 to 100V) 1	20p 25p	FOR	
28103 28104	871p BFY90 871p BSX19	671p PL4004 171p PL4005	171p 19p		TEGRATED	_	LISTS !	
40250 40361	569 B8X20	171p PL4006 871p PL4007	20p 24p	· · · ·			DISCOUN' 10% on	
40362	60p B8X76	150 T1843	40p	L900 4	9n: L914 4	p;	12 + any	7
AC107 AC126	871p BSY26 85p BSY27	171p T1844 20p T1843 171p T1846	121p	SL403	21p; IC-10 22- 22-121; MC1	303	one type. 15% on	
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100A —		- 22.50	971 p 12-75	871p; FJY101			7‡p; Valves lõp	ρ. Ι
Q.	ee nrev	inue na	~		C W S	B A B	THE	C



TELETON SPECIAL OFFER! 0 6

CR10T AM/FM STEREO TUNER AMPLIFIER WITH MATCHING PAIR SA1003 SPEAKER

Also available with Garrard 2025T/C Record Changer, Plinth, cover and stereo cartridge. Ready wired. **\$45**, Carr. **\$1**.



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HOSIDEN DHO4S 2-WAY STEREO HEADSETS

$28102 \\ 28103$	25p BF 87ip BF	Y90	22 p	PL4003 PL4004	16p	10W (3	3-9 to 1	.00V)			FULL LISTS !		A	MER	CAN	TAP	E
$28104 \\ 40250$	871p BS 50p BS	X19	17 ¹ n	PL4005 PL4006	190	11	NTEG	RAT	ED				'irst grade ew Disc				28.
40361 40362	569 BS 60p BS	X21	87 p	PL4007	24p		CIRC				DISCOUNT 10% on	3 3	in. 225ft.	L.P. acei	ate		
AC107	871p BS	Y26	17 p	T1843 T1844	40p 121p	L923	49p; 621p;	IC-10	22 50;		12 + any one type.	5	lin. 600ft. in. 600ft.	std. plast	ie		
AC126 AC127	25p BS 25p BS			T1845 T1846	174p 174p	£2.62}	; MC	1304	MC1303 £2.75;	1 :	15% on 25+ any	Ű.	in. 900ft. in. 1,200ft	. D.P. m	ylar .		
	ти	YRIS	TAR			PA246	; ČĂ	3011	CA3005 824p; FCH131	1	one type. Large mantity	5	in. 1,2001	t. L.P 1	uylar .		
PIV	9011 50-100	200	300	350	400	50p; F	CH161	50p;	FJH141		liscounts o	ก อี	in. 1,800	t. L.P. 1	nylar .		
1A	25p 271p	871p	40p	_	471 p	50p; F	JH221	50p;	FJH181 FJH231		pplication Postage	7	in. 1,200ft in. 1,800ft	. L.P. ac	etate .		
5A	80p 37jp — 55p	65p	45p		50p 75p	50p; F	JJ121	874p;	FJH251 FJJ131		Semi Conductors	7	in. 1,800ft in. 2,400ft	. D.P. m	ylar .		
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+ 8	}ee p	rev	iou	s pa	age		G.	W	. SN	IIT	H & I	со	. (RA	DIO) Ľ	TD.	,



Garrard 8P25/111 fitted Goldring G800 cartridge and wooden plinth and plastic cover. Ready wired. Total list price 836. OUR PRICE 432:60. Carr. 509. GOLDRING G169/3 fitted Goldring G800 cartridge complete with de luxe base and cover. Total list price 350-80. OUR PRICE 439. Carr. 509.

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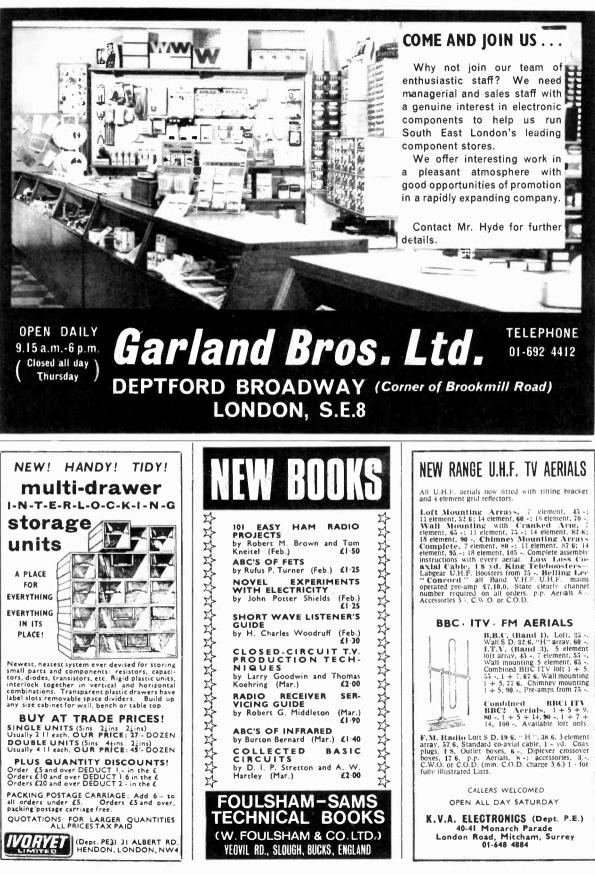
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6 STEREO Wonderfully com-fortable. Light. List 261:80 pr. OUR PRICE 5496 pr. Carr. £1. Mambo teak. List 260:20 pr. OUR PRICE 559:60 pr. Carr. £1. Mambo teak. List 244:65 pr. OUR PRICE 525:66 pr. Carr. 50. Marimba teak. List 244:65 pr. OUR PRICE 525:67 pr. Carr. 50. Marimba teak. List 248:01 pr. OUR PRICE 559:76 carr. 51. Magister teak. List 257 each. OUR stereo jack plug. 25-17.000 cps. 8 Magister stand 22:97 extra. P. & P. 12;p.



Practical Electronics March 1971





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MOTORS

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Incorporating two colls. Each coil when energised will produce opposite rotation of output shaft. 120V 60Hz 1/10 r.p.m. When run on 50Hz it will give a speed of 1/12 r.p.m. Price \$1.25. P. & P. free.

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Extremely quiet running motor with high starting torque. Has many uses such as

Has many uses such as chart drives, disco-theque colour wheels, etc. 1/20 r.p.m., 1/12 r.p.m., 1² r.p.m. 120V 50Hz, 1/12, 4, 1/18, 1/24, 1/240 r.p.m. 1/20, 1/60, 4, 1/16, 1/15, 1 r.p.m., 20 r.p.m. **g1-50** post free.

HYSTERESIS CLUTCH MOTOR



 Hysteresis clutch motor

 With integral clutch allowing the motor to drop out of engagement with the gear train, thereby facilitating easy resetting when used in timers or in conjunction with a light spring. 6 oz torque at 240V 50Hz, 1/12 c.p.m., 4 c.p.m., 15 c.p.m., 12 c.

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Similar to above type MD 83, 28V 1/20 r.p.m., 1/60 r.p.m., 1 r.p.m. 12V 1/20 r.p.m. 24V 1/15 r.p.m. 30V 1/12 r.p.m. **£1:50**. P. & P. 25p.

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200/230V 30Hz. New condition, ex-equip-ment. 8.7 1 r.p.h. and 1 r.p.m. Self starting, complete with gearing shaft in dia., in long. £1-50.

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NEW 200-250V, 50Hz, 2W. Synchronous induction motor. 2 revs. per hour. 0/P shaft, Jin dia. Jin long. Clockwise rota-tion. Three-holed mounting at 120° on 2in PCD. Price £1 post free.

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in tape, takes 7in spools, 1 in per sec. 3 motors, facility for remote control operation. Record/replay heads with separate crase head plus fast crase facility. Ex-equipment. Less spools. Price **25-98**. P. & P. 75p.

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PORTABLE WHEATSTONE BRIDGE Specification. Typ:: Moving Coll Galvano-meter. Ranges: 1. 0.05 to 5 ohms. 2. 0.5 to 50 ohms. 3. 5 to 500 ohms. 4.50 to 5.000 ohms. 5.500 to 50.000 ohms. Scales: Switched. Bildewire: 0.5 to 50. Galvanometer Scale: 10-0-10. Case: Moulded plastic. Internal Source: 4V Dry battery. Dimensions: 200 x 110 x 65mm. Weight: 0.9kg. List price \$25. Our neice \$9.990. 65mm. Weight: Our price \$9-99p.

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These well-known portable test instru-ments have been overhauled and are offered complete with leads, crocodile clins and prode clips and prods.

	Model D			. 114
	Model 40,	47A, 48A		
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Mailal IQL	an and a suit	th voltage		sulfi.

Model 48A complete with voltage multi-piler for 480V and 3600V. Current shunts for 120A and 480A. A.C. Current trans-former for 20A and 60A. In special wooden box. 47A and 48A are Admiralty patterns of the model 40. \pounds 16-75. P.4.P.750 the patterns o P. & P. 75p

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HIGH SPEED IMPULSE COUNTERS

HIGH SPEED IMPULSE COUNTERS by Davis, Wynn & Andrews. Ain dial and pointer registers up to 100 and 4-digit counter is by air inverse escape-ment so that there is no loading of the pointer mechanism when digits are clanged and adjustable pawls are unnecessary. Coll resistance 100 ohms are unnecessary. Coll resistance 100 ohms for mominal voit operation, but the device works reliably from 20V at rates up to 100 impulses/sec. In circuit with a thyratron, or neostron, counting rates up to 100 impulses/sec are possible provided pulse width is restricted to keep mean current to 100mA. New, \$6:38.





Gear boxes give a drive ratio of $2\cdot5:1$ at right angles to the input. Driveable through the 1/p shaft only. Dimensions 4in wide $\lesssim 3\frac{1}{2}$ in dep $\ll 4\frac{1}{2}$ in high. Robust construction in cast iron. Price £3.20

With pulley and ball race shaft mountings. Price **\$4.97**. Carriage 75p.



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AVO TRANSISTOR ANALYSER CT 446 A portable direct-reading instrument capable of giving accurate transistor measurements in the grounded emitter configuration. Battery power unit 1.3W to 10.6V in 5 steps. Base current 0-1mA, 1-40 mA. Collector current 250 mA. Nice: 164 \times 94 \times 5 ms. Weight with batters: 151b. Price **\$42**-50. Carriage extra.

6 DIGIT ELECTRICAL IMPULSE COUNTER

COUNTER New Type EM 101 24V Resettable £5 New P.O. Type 5 digit 330 Ohms ... £3-50 114V D.C. 4400 Ohms coil Ex-equip. £2-98 Packing and postage free.

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Suitable for counting all kinds of pro-duction runs, business machine operation. Mechanically driven. Reset type KA 1337, manual knob. Ex-equip. but new con-dition. Special price **£1-25** plus 25p, P. & P.

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Totalising 48V d.c. at 48mA: 10 impulses sec. Length 4in × fin × 1in. Price sec. Leng £4 post free.

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Totalising 240V 50Hz. Viewing window 2in x in. Ex-equipment. Price **12-75**. P. & P. 25p.

BERKELEY DECIMAL COUNTING **UNIT 0-9**

Direct reading octal base plug in unit elec-tronic counter. The number counts received reading number counts received is indicated by one of ten neon lamps behind acetate panel. The unit counts from 0-9 the tenth pulse resetting to zero and simultaneously recerting an ele signal

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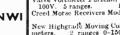
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EAC DIGIVISOR Mk. II DIGITAL READ-OUT DISPLAY

Uses a sensitive moving coil movement to project digits 0-9 on to a viewing screen via an optical lens system. Image height lin. Lamp 6-37. Sensi-tivity 2:50 micro-amp. Dimensions L. 4, in. W. 23in. H. 1 jin. Price \$3-50. P. & P. 25p. a sensitive







with electrical reset



RELAY STIS By Sangamo Weston, suitable for D.C. circuit. A high sensitivity relay more sensitive than the electromagnetic type. Single Coil Resistance 310 micro amps. 315 Ω. Our price £1.15.

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LIGHT DIMMER—BRAND NEW High grade full wave bridge circuit gives bridge circuit gives linear control of light brightness. Ideal



light brightness. Judeal for controlling room lighting and a.c./d.c. commutator motors fitted to portable electric hand dirlls. Fits standard 2in conduit box. 240V, 30Hz, 400W. Price 2290. P. & P. 13p.

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HAYDON Synchronous motor driven timer providing manual adjusted delay. Delay time is set on graduated dial. Press button closes contact and drives motor which drives an arm until it actuates the load switch. The cam then returns to initial position for repeat action. Various ranges available. 230V 50Hz Load contacts 15A 230V. **25**.

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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	DC400 8/8 DC4008C 8/8 105 D/8	70p	GP96 HGP37	.33p 47p 13p 37p 33p 47p	81-2-3 33p TS1 33p TS2 33p	47p 47p 47p
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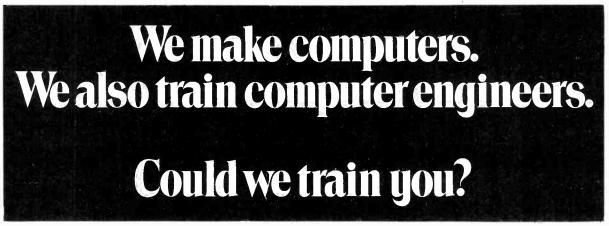
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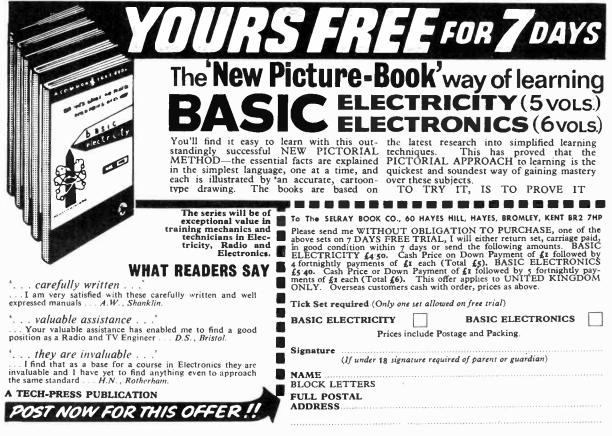
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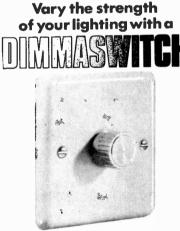


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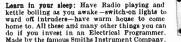
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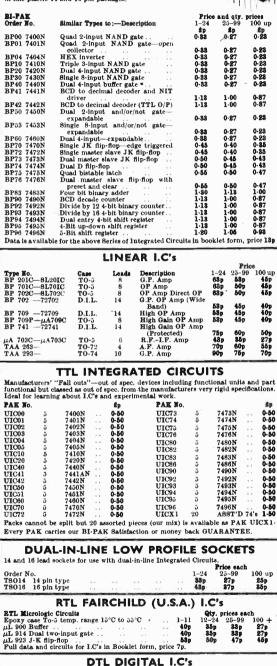
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PRACTICAL No. 3 **VOL. 7** CTRONIC 1971 March

Editor F. E. BENNETT Assistant Editor M. A. COLWELL Editorial Assistants D. BARRINGTON G. GODBOLD M. KENWARD Art Editor J. D. POUNTNEY Technical Illustrators J. A. HADLEY P. A. LOATES Advertisement Manager D. W. B. TILLEARD

BUT, SERIOUSLY

Do some of us on occasion take this business a trifle too seriously? We feel this could be true, for now and again someone is heard to imply that so and so design is a flippant use of electronics.

Getting straight down to grass roots, let us consider any classic circuit arrangement; in fact suppose we take a well known building block such as the multivibrator, as a general illustration. This circuit has a habit of cropping up in the most unlikely guises, as we all know. It may appear in an item of test gear such as a c.r.o. trace doubler or a voltage to frequency converter, in a car lamp flasher, in the tone generator section of an organ, in a digital calculator, or in a "toss the coin" game, to name but a few. This ubiquity helps to demonstrate the point that an electronic circuit as such has no innate purpose apart from the purely electronic function it has been expressly designed to perform; and this alone is not enough. Outside purely academic circles, the circuit requires some gainful employment to justify its existence. Providing it is within the circuit's capabilities, the precise nature of the task it may be given is, in an electronic sense, irrelevant. It may be useful or it may be frivolous. There is no list of prescribed duties that circuits must restrict themselves to! They work for us as we decree.

Electronics is a very "human" technology, simply because it is easily adaptable to most of our whims and needs. And it plays, quite rightly, a major part in our amusement and entertainment, no less that in the "serious" activities of life.

To be fair we must not forget that to some individuals the study of electronic circuitry can be an end in itself. Academic minds so inclined can derive plenty of intellectual pleasure from the analysis of circuit behaviour without too much worrying about specific applications. But to most of us electronics surely means more than conducting a minute anatomical examination of a pretty trace on the c.r.t., or indulging in a prolonged immersion in mathematics, however good all this may be for the mind. When it comes to the crunch, electronics is a tool and the most proper and sensible thing is to apply it however and wherever we can, to serve us at both work and play.

If there are theoreticians who still shudder at some frivolous application of the technology, there is a homely example for them to ponder. Let them consider the television receiver-that embodiment of many elegant electronic techniques, a mass produced complex of circuitry that has been designed principally for our entertainment. Just dare suggest that this cathode ray companion and comforter for millions be redesignated something like a "communications monitor" and provide nothing but news and elevating cultural programmes, and the whole nation would go on strike! F.E.B.

this month

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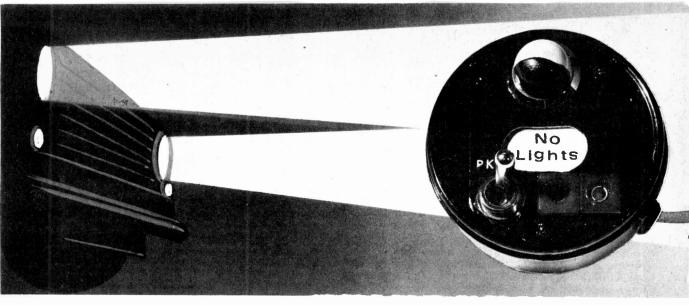
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Our April issue will be published on Friday, March 19

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MANY drivers are not regular users of parking lamps and tend to use side lights when parking in a strange situation. Because they would not use an automatic parking light very often, they do not consider it a worthwhile investment. The added facility of a lighting up reminder that this circuit offers will thus make the parking lamp worthwhile. The circuit is very simple and provides the following facilities:

(a) An automatic parking lamp that turns itself on and off at dusk and dawn.

(b) A warning system when the car is used with no lights in poor light or after lighting up time.

(c) A warning indication, while driving, as lighting up time approaches.

(d) Automatic cancellation of either system when the sidelights are switched on.

(e) No additional control switching when on route.

The complete unit can be attached to the car dash panel or to the windscreen where it is in view of the driver. Only three wires need to be connected to the car wiring which is not altered in any way. Both positive and negative earth 12 volt circuits are given, and for cars already fitted with an automatic parking light, only part of the circuit need be built. The unit utilises a standard parking lamp so if such a lamp is already used it can now be automated.

CIRCUIT

The fundamental circuit adapted for both positive and negative earth systems is shown in Figs. Ia and 1b; this illustrates the operation of the system using normal ignition and side light switching. With switch SI in the "normal" position the circuit is operative when the ignition is on and the sidelights off. The circuit is then in the lighting up reminder state and LP2 will signal the approach of lighting up time when *en route*, or when about to move off without lights when they are required.

With S1 in the "park" position, the sidelights switched off and a parking lamp (LP1) plugged into SK1 and SK2, the circuit will function as an automatic parking light, the ignition switch and LP2 being out of circuit.

LIGHT DEPENDENT RESISTOR

As daylight decreases, the l.d.r. (light dependent resistor—XI) resistance increases and since this forms a potential divider with R1 at the base of TR1, when

the determined light level is reached, a switching function is triggered between transistors TR1 and TR2 so that TR2 conducts and consequently illuminates LP2 to show up the expression "no lights". The switching function is preferred to an emitter follower because there is no heat build-up across transistor TR2 while the input signal is developing. The life of the transistor is therefore prolonged. Resistor R3 is made up of two 22 ohm resistors in parallel.

The same circuit operation is carried out for both the parking lamp and internal warning system and the ignition/battery supplies are selected in conjunction with the appropriate lamp by the operation of the double pole changeover switch S1.

SYSTEM CANCELLATION

Both systems are cancelled when the normal sidelight switching operation is carried out following the internal warning, or where sidelights are required when parked. The circuit is completed via the filaments of the sidelights, rear light and number plate light; with the sidelight switch off, the small current required for the system flows through the paralleled filaments of the sidelights and associated lamps. When, however, these lamps are switched on, the circuit is shorted out and the no lights warning or the parking lamp, cease to operate.

If the car is garaged or parked within the law, the switch remains in the normal position and both systems are isolated. A check is readily available for both systems when light is shielded from X1. It is to be noted that LP2 will hunt if the l.d.r. picks up reflected light from the hand or any other adjacent surface capable of reflecting light on to the sensor.

OPERATIONAL LIGHT RANGE

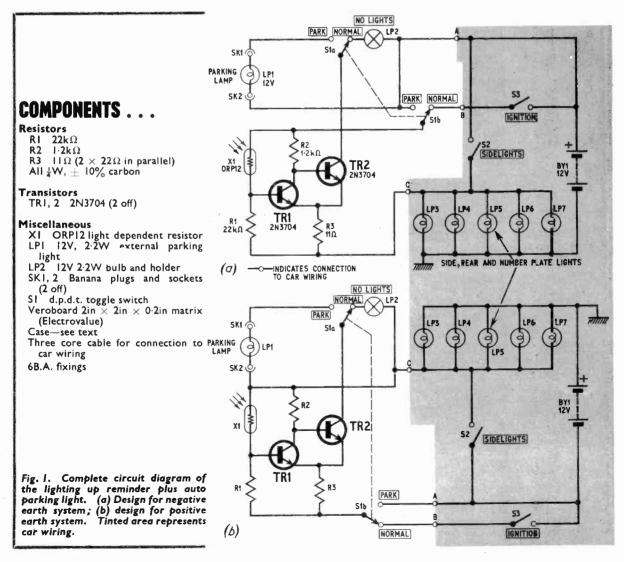
The operational range of the system is good and operational levels of light may be selected by the insertion of light filters under the cover of the l.d.r. These may be in the form of ordinary thin paper and are far more economical than the inclusion of a variable resistance in the circuit.

With the engine running when *en route*, the internal lamp may flicker as the critical light period approaches. This is due to voltage variation of the car's supply (the charging system) but since the flicker is an added attraction factor, the necessity for voltage stabilisation is considered unnecessary and not in the interests of economy.

AUTOGREGKLIGHT

A LIGHTING-UP REMINDER AND AUTOMATIC PARKING LIGHT . . . BY G. W. JONES

3-14



CONSTRUCTION

The prototype unit was housed in a small tobacco tin, the lid of which was reinforced with aluminium. Holes can be cut in the lid and aluminium plate for X1 mounting, SK1 and SK2, S1 and the "no lights" indication. The legend "no lights" may be printed on tracing paper and inserted, between two protective celluloid layers, under the aluminium panel which is attached to the lid by three 6B.A. screws.

The mounting for X1 and LP2 holder were obtained from a single indication lamp dismantled for the purpose. SK1 and SK2 can be banana sockets or any

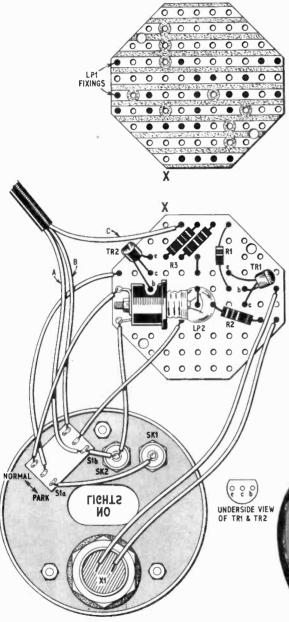


Fig. 2. Layout and wiring diagram of the prototype unit housed in a tobacco tin case. This is the negative earth system; for positive earth version the wire connected to SIb wiper is removed and reconnected to SK2, link between SK2 and SIb is removed. Wire "C" is taken to SIb wiper and a new wire—which now becomes "C"—is connected to SK2

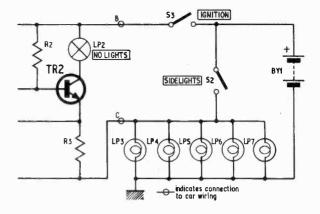


Fig. 3. Circuit diagram of the negative earth system for lighting up reminder only. Connections "B" and "C" are reversed for a positive earth system

special socket to suit the parking light. The three core lead that connects the circuit to the car wiring can be taken out through a grommet hole in the side of the case.

Components in the prototype were mounted on a piece of 0.2 inch matrix Veroboard, fixed inside the tin by two 6B.A. screws and spacers (see Fig. 2). The inside of the tin should be protected by insulation tape so that no connection is made between the circuit and earth on the car. It is, of course, possible to use any form of construction, since the layout of components is not critical—the unit could be built into the dashboard of many cars and LP2 could be housed in a warning light mounting chosen to correspond with the other panel warning lamps.

REMINDER ONLY

If it is required to provide a lighting up reminder only—without the facility of an automatic parking light—then S1, SK1 and SK2, and the connection to S2 (sidelights switch) on the car battery side may be omitted (see Fig. 3).

When the complete system is operated in the lighting up reminder mode, LP1 can be unplugged from SK1 and SK2 and hence the no lights warning may be cancelled by operation of S1 (change to "park" position) as well as by switching on the sidelights.





SOVIET ACHIEVEMENTS IN SPACE

After a period of apparent inactivity, the Soviet Union has in the past two years or so made some significant advances that have been spread over the whole area of space activities. The Russians have for a long time favoured the use of space platforms and automatic probes. They have covered the human element involved by longer periods under space conditions, and experimented with the transfer of astronauts from one vehicle to another.

The local earth-moon activities have formed a part of their programme but they have paid a good deal of attention to the special techniques required to explore the other planets. Already they have had two attempts to land robot craft on Venus and now a third attempt has been made.

The unfortunate loss of *Lunik 15* at the time of the *Apollo 11* mission was a particular disappointment, but served to indicate the difficulties that attend attempts to maintain communication, with vehicles that are at a low level in areas where there are mountains involved.

COLLECTING MOON SAMPLES

However the loss of control of *Lunik 15* was more than compensated by the successful mission of *Lunik 16*. This vehicle departed from the earth for the moon with the main task of collecting, automatically, samples of lunar soil, putting them into containers, and returning them to earth. The vehicle consisted of a descent platform carrying the return vehicle, which carried the drilling mechanism and control. Altogether something in excess of 100 grammes of lunar material was recovered.

The point of operation was in the Sea of Fertility, 56° 18' W and 0° 41' S, which is some 900km from the site of the *Apollo 11* landing. The material was friable surface substance of fine grain, for the first 15cm of the sample. The next section from 15cm to 33cm was of variable granular material with some larger inclusions of the order of 3mm in diameter. The last section from 33cm to 35cm was of large grain with some fragments of bedrock.

In appearance the material is a very dark grey almost black powdery substance. The mean specific gravity of the material was of the order of 1.2 and the variation in particle size ranged from 70μ m at the surface to 120μ m at the lowest depth. The composition appears to be basaltic with some feldspar and some metallic iron and vitreous particles. Some isotopes of short life were found and altogether about 70 chemical elements were present.

A comparison with the specimens brought back by *Apollo 12* shows very close agreement in the percentage of the various elements.

SOYUS 9

Andrian Nikolayev, who captained Soyus 9, has made some interesting comments on the 18-day flight. Month long flights are feasible but anything longer would require different techniques. There would be need for more efficient and extensive conditioning and also new medical procedures.

The post flight effects of this mission were very much more marked than those encountered with the shorter flights. Walking was found to be difficult over a period of days and there was frequent stumbling. They found it difficult to climb stairs, sometimes hard to stand upright.

A notable feature was the wasting of the lower limbs by as much as 4cm round the hips and 2cm round the shins. This appears to result from the loss of muscle tissue in the legs which are normally used to support the body at 1g. There was a loss of body weight of 5kg for the new astronaut Sevastianov and a little less for Nikolayev. However, they both recovered their normal weight in three weeks.

LUNOKHOD

The mobile moon vehicle Lunokhod was an exciting event and represented a new era in space technology. Although an instrument unit, previously landed by the United States, had been made to hop, Lunokhod 1 is the first vehicle to be landed on the moon and become mobile under guidance from the earth direct. When the difficulties are properly realised, a task of this kind becomes a major point in history.

Because it is the first time that such a successful operation has been mounted, a whole new vista in the exploration of the moon becomes available. Provided that communications between the base station and the unit can be maintained, many new areas of the moon can be explored in detail.

At the moment this is feasible only in open areas because in hilly or mountainous regions loss of communication could be disastrous. This points to the likelihood that control from a space platform would be the ultimate aim. A very great advantage is that a mobile system remotely controlled would enable special regions to be explored which might be impossible for manned units.

MANNED FLIGHTS

It is significant that the Soviet space scientists do not regard the robot as the principal method. This is borne out by the fact that the internal environment of *Lunokhod 1* is similar to a life support system having a temperature between 16 and 18 degrees centigrade and a pressure of between 730 and 780mm Hg.

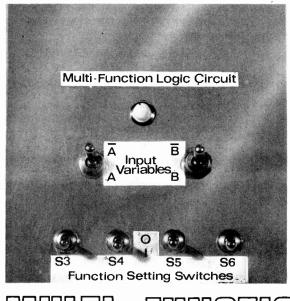
The present instrumentation could be built into a manned cabin without modification. From this it could well be surmised that a manned landing is still part of Soviet plans. Also there is a distinct suggestion that the Russians are looking further afield to Mars for automated surface units.

LUNAR EXPERIMENTS

Although not much appeared in the initial stages about the type of experiments being undertaken, the following were included in the mission.

- (a) Determination of the composition of the surface of the moon using x-ray photometry.
- (b) Measurement of extra-galactic x-radiation using an x-ray telescope to make long exposure studies of weak sources. These cannot be done effectively (where distant sources are concerned) with rockets and satellites.
- (c) Assessing the mechanical properties of the lunar soil by impressing a special stamp.
- (d) The study of cosmic radiation from the sun.
- (e) Experiments which involve the radiation from the moon itself.
- (f) The very important cooperative effort of France and the Soviet Union in a laser experiment to determine accurately the earth-moon distance.

A special system of telemetric sensors is in use to measure the stresses acting on the chassis of the vehicle and a great deal of television recording is being made of the tracks that are made on the lunar surface.



For demonstration purposes, it is convenient to be able to produce any of these 16 functions without having to construct separate gates. The multifunction logic circuit makes it possible to establish any required function simply by selecting the appropriate combination with four switches.

FUNCTIONS OF BINARY VARIABLES

In the logic diagram of Fig. 1, each of the four switches S3, S4, S5, and S6 puts a 0 or 1 condition on its respective gate input, according to Table 1. This lists the function logic output corresponding to each of the 16 functions.

The switch settings are, in fact, those that would appear in a truth table of the desired function.

The A,B inputs are connected to decode each of the four possible input conditions and so select the appropriate gate as follows:

		-		
Input state	A.B	A.B	A.B	A.B
Gate selected	Gl	G2	G3	G4

The G5 gate output will therefore assume a 0 or 1 condition depending both on the position of the



A LOGIC function expresses the relationship between the input and output logic states of a circuit. The basic logic functions AND, OR and NOT are part of a series of functions.

With two input variables, A and B, four different input conditions can occur:

Ā.B A.B Ā.B A.B

These four conditions could produce a 0 or 1 at the output, depending on the circuit logic, hence a total of 2^4 or 16 functions are possible.

function setting switches and on the particular combination of the A, B inputs. A 1 condition will light the lamp via the lamp driver

By P. A. Davis, A.M.Inst.E.

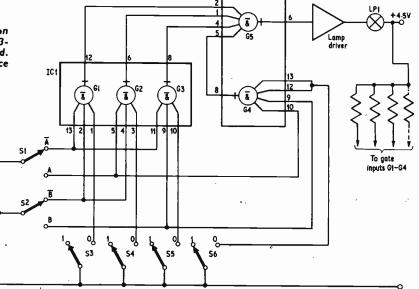
but a 0 condition will not.

CIRCUIT

The multi-function logic circuit makes use of two integrated circuits. These i.c.s are three and four input NAND gates; the SN7410N and SN7420N respectively.

IC2

Fig. 1. Logic diagram of multi-function unit. Here two i.c.s incorporating 3and 4-input NAND gates are used. Gate input numbers refer to the device pin connections as seen in Fig. 2



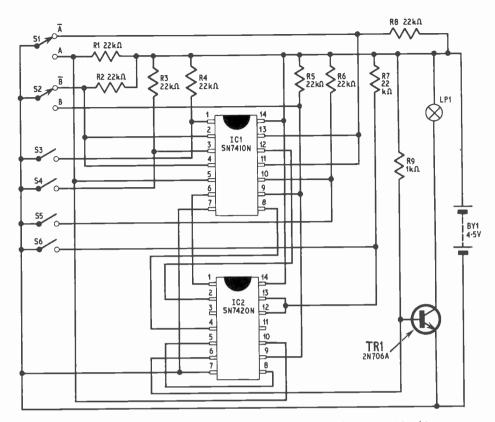


Fig. 2. Circuit diagram of unit. Note that all gate inputs have a positive bias

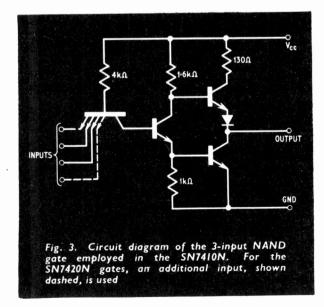
In the circuit diagram (Fig. 2), all the switched gate inputs are taken to the positive rail by way of resistors. This ensures that each input is held at logic 1 when its switch is opened.

The unused input at gate G4 is connected to a used input rather than left floating.

Fig. 3 shows the i.c. gate configuration used.

١

3



	20.04X	VARIAB				
Table I		FUNCTIONS	OF	TWO	BINARY	

Function number	5	sett	tio ting che S5	s	Logic function produced	Function name
1	0	0	0	1	A.B Ā.B B A.Ē	AND
2 3 4 5 6 7 8 9	000000-	00	!	0	A.B	В
3	0	i	0	ò	AB	
5	õ	i	õ	ĭ	A	A
6	õ	i	ī	Ó	$\mathbf{\hat{\bar{A}}}_{\mathbf{\bar{A}},\mathbf{B}}+\mathbf{A},\mathbf{\bar{B}}$	Exclusive OF
7	0	1	1	1	A ± B	OR
8		00	0	0	$ \begin{array}{c} \mathbf{A} + \mathbf{B} \\ \overline{\mathbf{A}} \cdot \mathbf{B} = \overline{\mathbf{A} + \mathbf{B}} \\ \mathbf{A} \cdot \mathbf{B} + \overline{\mathbf{A}} \cdot \overline{\mathbf{B}} \end{array} $	NOR
9	1	0	0	1	A.B + A.B	Logical
10		•		•	x /	Equivalence NOT A
10	1	00	1	0	+ B	NOTA
12	1	i	ò	ò	B	NOT B
13	i	i	õ	ĭ	$\vec{A} + \vec{B} = \vec{A} \cdot \vec{B}$	
14	i	1	1	0	$\overline{A} + \overline{B} = \overline{A.B}$	NAND
15	1	1	1	1	1	
16	0	0	0	0	0	0

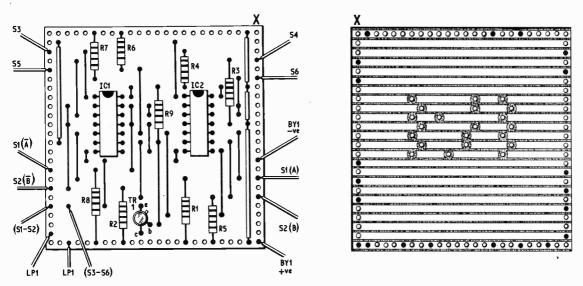


Fig. 4. Component layout and wiring for topside and underside of Veroboard

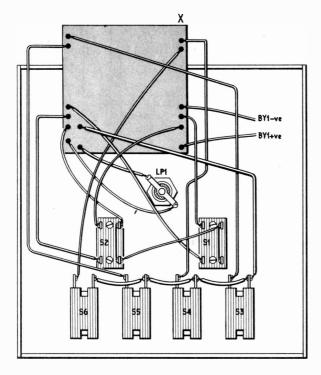


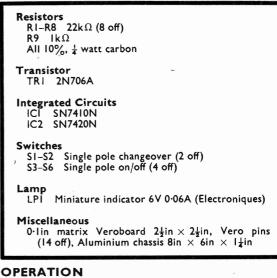
Fig. 5. Veroboard and control panel interwiring on an aluminium chassis plate

CONSTRUCTION

Apart from the chassis mounted switches and lamp, all of the components are mounted on a single piece of Veroboard as given in Fig. 4. To accommodate the dual-in-line i.c. packages, Veroboard of 0-1in matrix is used.

Wiring of the switches to the board is shown in Fig. 5. Positioning of these will depend very much on the preference of the user; whether a large or small display is required.

COMPONENTS . . .



To operate the completed unit, first select the required function from Table 1. This function is then set using the switches S3, S4, S5, and S6.

Each input combination of A,B is then operated on by this function, and the result, a 1 or 0, will appear at the output of gate G5. If the output is 1 the lamp will light.

Say, for example, the or function is required. Table 1 gives the function switch setting as 0111 (Function 7).

With these switches set accordingly, the switches S1 and S2 are set to A,B. It will be found that the lamp lights, hence, we can conclude that provided that A or B (or both) is present at the input, the lamp lights.

Apart from the convenience of the unit for demonstrating logic functions, it can be useful as part of a training programme — particularly if the function governing the input-output relationship has to be deduced from the unit's behaviour.

MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

WIPER DELAY

There are many windscreen wiper control units on the market and, as our readers will have noted, the problem with many circuits is that they are unable to accommodate the various wiring configurations and wiper motor types in use on all modern cars.

Wiperdwell, a unit manufactured by Automents Ltd., is one unit that can be used with all types of selfparking wiper motors and can easily be fitted by the average motorist in a very short time. The unit allows the selection, by a single control, of the most suitable wiping frequency for slight rain, fog and snow—a principle that works extremely well.

The unit can be fitted using a drill and screwdriver, comprehensive connection instructions are supplied and physical connection is made by way of "piggy back" connectors thus avoiding altering existing wiring and obviating soldering.

obviating soldering. The Wiperdwell unit will not affect the normal operation of the wipers, can give up to 20 seconds between sweep delay, costs $\pounds 4.75$ and is supplied with a six month guarantee.

MINIATURE SWITCHES

Sub-miniature toggle-switches with a rating of 6A at 125V or 3A at 250V a.c. suitable for most of our constructional projects are now being marketed by WEL Components Ltd.

The switches have a breakdown voltage of 1,000V a.c. with insulation resistance of more than 100 megohms at 500V d.c. The switch contact resistance is typically less than 5 milli-ohms at 1A 2.4V d.c.

The switches are moulded in phenolic melamine with solder tag connections and are available in two types—Type TS106D is a single-pole double throw and costs approximately $37\frac{1}{2}p$ (7s 6d) each. Type TS206N is a double-pole double throw and costs approximately $47\frac{1}{2}p$ (9s 6d).

Addresses of nearest stockists can be obtained from WEL Components Ltd., 5 Loverock Road, Reading, Berkshire. Another range of sub-miniature toggle and pushbutton switches suitable for many P.E. projects are those manufactured by **Birch Stolec Ltd.**

The switches include toggle, lever lock, rocker and momentary pushbutton types with one, two, three or four poles.

Contact ratings are: coin silver contacts, 5A resistive load at 115V a.c., or 2A at 250V a.c.; brass contacts with gold over nickel plate, 0.4V/A maximum at 20V maximum (a c. or d.c.); coin silver contacts with gold over nickel plate, 5A resistive load at 115V a.c. or 28V d.c., or 2A at 250V a.c., and 0.4V/A maximum (a.c. or d.c.).

Available with short or long toggles with nine different colour caps, the switches can also be supplied for printed circuit board or angled mounting.

Full details of these switches and addresses of nearest stockists can be obtained from Birch-Stolec Ltd., Ponswood Industrial Estate, Windmill Road, Hastings, Sussex.

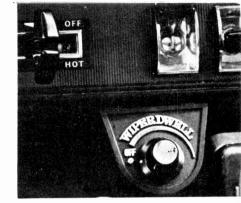
Also, we have been informed that Gothic Electronic Components, Beacon House, Hampton Street, Birmingham 19, have been appointed stockists and distributors of the complete range of standard and miniature thumbwheel switches from Birch-Stolec.

REED RELAY

Two new miniature encapsulated reed relays supplied with either one normally open reed switch or one changeover contact are the most recent products from Osmor Ltd.

Ideal for printed circuit board mounting, the type ERA has maximum d.c. contact ratings of 10W 200V 0.5 d.c. and type ERC is rated at 4W 28V 0.1A d.c.

The relays are available for 6V, 12V and 24V operation, and are colour coded for easy identification. The



Wiperdwell windscreen wiper control from Automents

coil is wound on a glass-filled nylon bobbin, and a magnetic screen is fitted as standard.

The complete relay is encapsulated in glass-filled nylon and measures only 22mm ($\frac{2}{8}$ in) × 10.5mm ($\frac{1}{2}$ in) diameter.

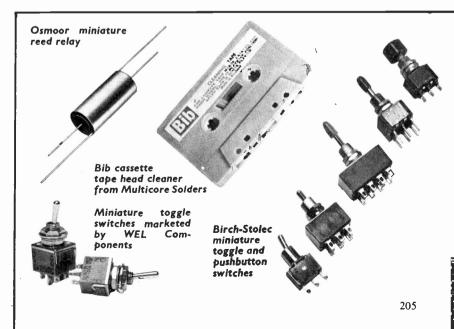
Price of the relays vary according to type and quantity; full details can be obtained from Osmor Ltd., 540 Purley Way, Croydon, Surrey, CR9 4DY, or at 53 London Road, Leicester, LE2 0PD.

TAPE HEAD CLEANING

Suitable for all compact casette type tape recorders and car player units, Multicore Solders have recently introduced a new tape head cleaning cassette tape.

It comprises a cassette tape container in which high quality cleaning tape is incorporated to clean tape heads, capstan and pinch wheel. Used in the same manner as a tape cassette by placing in the machine and operating in the play-back position, the whole operation takes approximately one minute.

Supplied in a plastics container the Bib Size 31 cassette tape head cleaner retails at 53p (10s. 7d.) and is available from most hi fi shops.



GEMIN DUAL PURPOSE FAR STERED AMPLOFIER By D. S. GIBBS and I. M. SHAW (FERANTI LTD)

GEMIN

N this, the final part of the P.E. Gemini dual purpose stereo amplifier, we give final construction details of the pre-amplifier, a fault finding chart and hints on using the completed amplifier.

SELECTOR

FILTER

VOLUM

DRILLING

The pre-amplifier is housed in a Contil Mod-2 case size G and the dummy front panel (aluminium $12\frac{3}{4}$ in \times $2\frac{3}{4}$ in \times 18 s.w.g.) was actually cut from the unused main amplifier chassis. Full drilling dimensions for the box and panels are given in Figs. 36, 37, and 38.

Miniature toggle switches were used in the prototype for S1, S2, and S5 and the holes for these and the pilot light LP1 must be drilled to suit whatever components the constructor has available. The best arrangement is to drill the front panel and the dummy front panel whilst they are clamped together to ensure that any slight errors do not prevent the components from fitting through the holes. All the holes must be de-burred with a file or a large drill.

FRONT PANEL

To obtain a presentable finished article the dummy front panel can be rubbed with wire wool, using household soap and water, in one direction along the length of the panel. This process should be continued until all the scratches have been removed. A very good "brushed aluminium" finish can be obtained in this way; a satin finish can be obtained if the panel is coarse sand blasted by some local workshop or garage. Care must be taken not to introduce any fingerprints or grease before the panel is sprayed with Letracote gloss.

LABELLING

OFF ON

The front and rear panels can now be labelled using the same method as for the main amplifier cabinet, i.e. one light coat of Letracote gloss, apply the letters and then a further two coats of Letracote. As can be seen in the photographs, the prototype controls have numbers of relative magnitude arranged around them. The indication dots for these numbers can be marked first lightly in pencil with the help of the template. Fig. 39. The template is transferred to a thin piece of celluloid by drilling small holes in the required places. The celluloid template can then be placed over the dummy front panel and the dots marked in lightly in This method ensures that the dots exactly line pencil. up with the 30 degree switch positions and that the dots round the other controls are all at the same angles and radii.

ASSEMBLY

The front panel components are now mounted, not forgetting the dummy front panel which is held on by the control spindle nuts. Care must be taken not to mark the dummy front panel whilst tightening the various nuts and screws. The rear panel components, C52 (using a suitable capacitor clamp) and the assembled printed circuit board should be mounted on the appropriate parts of the case.

WIRING

The wiring should be executed with the case dismantled, i.e. opened out like an exploded diagram, to make the connections to the front and rear panels easier. Any systematic way of wiring the interconnections can be adopted but it is recommended that many

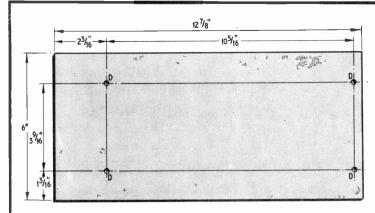


Fig. 36. Drilling details of the base of the pre-amplifier case. The small chassis supplied with the case is used to mount C52 and has one hole drilled in it $\frac{2}{3}$ inch down and $3\frac{1}{6}$ in across the panel. This hole can be seen as the earthing point in Fig. 42 top right hand diagram Fig. 39. Template for marking out indicator dots on the dummy front panel

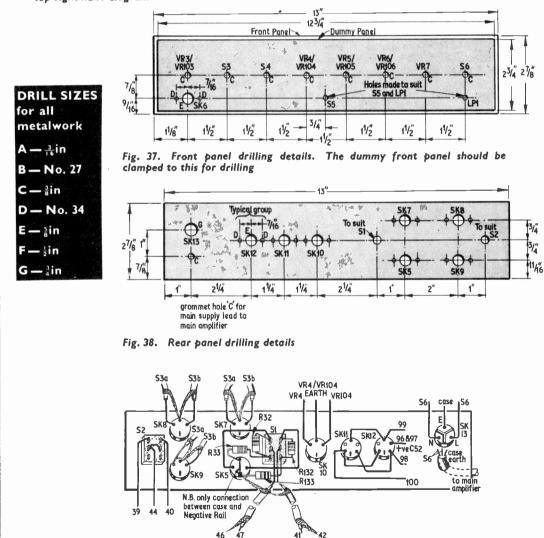
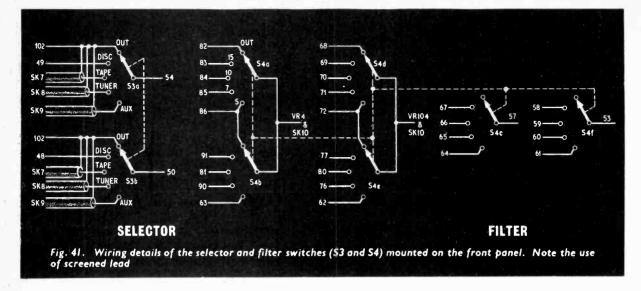
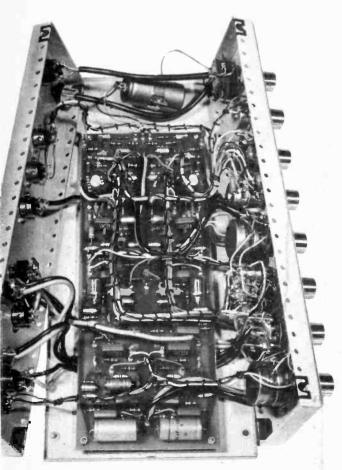


Fig. 40. Wiring of components mounted on the rear panel



different colours are used for identification purposes. The components which are wired to the tone controls, C45, C46, C47, C145, C146, C147, must have sleeved wire ends and as short leads as practicable. The same applies to the four resistors in the area around S1, and SK5. The only internal screened cables necessary are the ones from the input sockets to S3, with the actual



screens being connected to a stout tinned copper wire joining the "Out" positions of the selector switch. The sole connection between the case and the negative rail must be at SK5 as indicated, or complications may arise due to an earth loop being formed which could result in an incurable hum. The earth from the mains input cable is connected to a solder tag which is on the same bolt as C52 capacitor clip, but on the other side of the screening plate. This screen is fitted on final assembly in convenient holes between the mains switch and. balance control such that it touches neither. As with the main amplifier the paint may have to be removed from around the screw holes to ensure that all the different sections of the box make electrical connection with each other. Finally, the feet can be fitted to the base of the case. Figs. 40, 41 and 42 give the wiring up details.

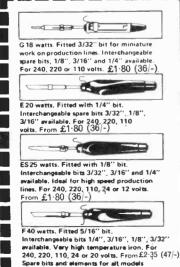
INTER UNIT CONNECTIONS

The cable which supplies power to the pre-amplifiers and audio to the main amplifor must be made a suitable length to suit the particular installation. Any multicore (at least three core) screened cable can be used since the output impedance of the pre-amplifier is quite low. We have not given any pin connection numbers for this cable because we have noticed that in some cases the numbers on plugs and sockets do not always correspond with each other. All that is required is that the channels do not inadvertently get reversed and that the earth and supply rails have a continuous path from the main amplifier. This cable must be in place before power is applied to the main amplifier or the charging current taken by C6 and C106, if this plug is inserted after the power has been applied, may damage the driver and output transistors.

FAULT FINDING

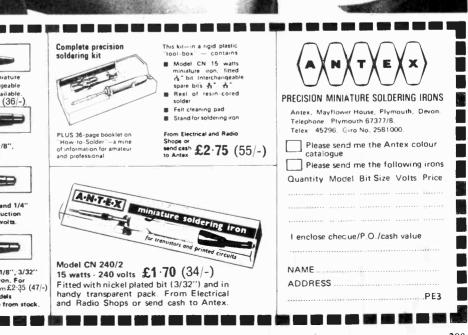
This is a complex amplifier and it is possible that the constructor will have some problems to iron out before it works perfectly. Most faults will be due to: wires left unconnected or connected to the wrong place, components inserted at the wrong place on the printed circuit board, transistors or diodes inserted the wrong way round (easily done with the Ferranti devices), or surplus solder bridging the gap between two printed circuit tracks.

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March 1971 Practical Electronics



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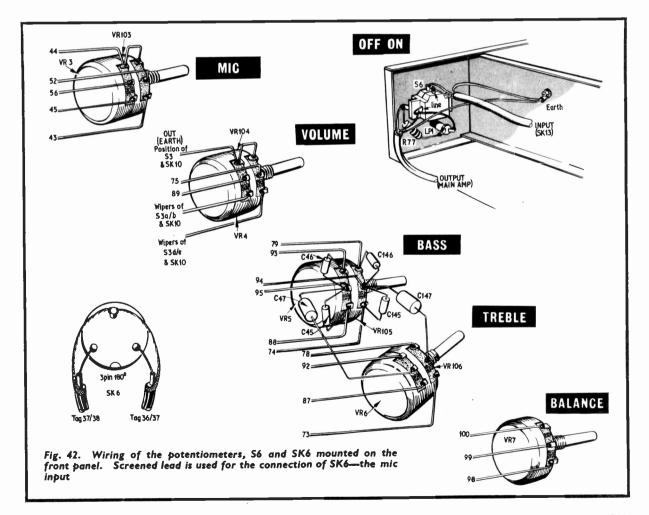


Photograph of the front panel showing control designations

Faulty components are rare, especially if one uses new components of good quality, and if it is found that one of the transistors or diodes is defective after testing the amplifier, make sure that it was not destroyed by a wiring error before replacing it. To avoid expensive accidents great care should be taken to check all the wiring thoroughly before connecting the amplifier to the mains—it will be too late afterwards.

Given time and patience, most faults can be tracked down with a multimeter. An instrument of at least 20,000 ohms per volt is recommended. An oscilloscope and an audio oscillator can save a lot of time and trouble, particularly with faults such as distortion and oscillation. And if it is required to test the amplifier through it's full specification, a wave analyser and a squarewave generator will also be required.

To assist in getting the amplifier to work correctly, a table giving the normal voltages at various points in the circuit, is given on page 212, together with a list of fault symptoms and their most likely causes. This will help to track down most faults with the minimum of trouble, but we can not claim to have thought of everything.



CONNECTING UP

The amplifier is working perfectly, a record deck or f.m. tuner is connected to it; on switching on there is a loud hum on both channels. This happens to nearly every audio enthusiast sooner or later and the usual cause is an earth loop. This arises when both the amplifier and the piece of equipment to which it is connected are earthed separately to the mains. A small a.c. voltage is induced into the earth leads of both units and when they are connected together a 50Hz current flows in the outer braid of the coax cable between them, causing an objectionable hum. The cure is simply to disconnect one of the earths, preferably not the amplifier, and so break the loop. The record player deck or f.m. tuner, etc. will then be earthed via the amplifier. Another source of hum arises if the earth connection between the amplifier and the ancillary equipment gets broken whilst still leaving the signal lead (coax inner) connected. This causes a really colossal hum, often accompanied by a chorus of radio stations.

The prototype amplifier did not show any sign of radio breakthrough but if it is to be operated near a

transmitter and breakthrough is experienced, connect a capacitor of 100 to 1,000pF directly between each input and earth, alternatively a ferrite bead may be placed on each of the input leads (directly at the input sockets in both cases). Radio breakthrough can also be a symptom of h.f. oscillation in the circuit.

Supposing the amplifier is working perfectly, but there is only an output from one channel. The first thing to do is to check the wiring of the input plug, especially if using a ready made lead. The P.E. Gemini is wired as Fig. 43a which is the DIN standard for amplifiers but many of the ready made leads, intended for tape recorders, etc. are wired as Fig. 43b.

Low impedance signal sources, such as a tape recorder, f.m. tuner or low impedance dynamic microphone, can be connected up with ordinary twin screened (stereo) cable, but low capacitance screened cable should be used for high impedance sources, particularly magnetic pickups. The popular stereo cable has a capacitance of 100pF or more per foot, and only 4 to 5 feet is required to produce a resonance at 10kHz with a normal 500mH magnetic pickup. Twin lighting flex is quite suitable for connecting up the loudspeakers.

PE GEMINI CHECK CHART

POWER SUPPLY

FOWER SUFFLY	
Normal Voltages (no load))
Across secondary	45 –55∨
	(50Hz)
Across C3	65–75V
Across output terminals	55V
Across DI and C2	107
Between 0V rail and TR1 base	9.3∨
Across R4	0·7V
Across R5	I∙4V

Fault symptoms and possible causes

Output voltage zero

- (1) Fuse blown. Check for cause before replacing.
- (2) Bad contact in mains plug and socket.
- (3) CI short circuit, or short circuit present across output.
- (4) R6 omitted or open circuit.
- (5) D2, D3, D4, or D5 open circuit.

Output voltage low

- (1) DI or C2 wrong way round.
- (2) TRI, TR2 or TR3 open circuit or wrongly connected.
- (3) RI or R2 wrong value.
- (4) Wrong transformer taps connected.

Output voltage high

- (1) DI omitted or open circuit.
- (2) TRI, TR2 or TR3 short circuit or wrongly connected.

(3) R1, R2, or R6 wrong value. IMPORTANT: The power supply should be tested and adjusted to the correct voltage before the ht+ leads to the amplifier are connected.

MAIN AMPLIFIER

Normal Voltages

(Referred to common rail unless otherwise specified.)

H.T. rail	55V d.c.
Output terminal	27∙5V
Emitter of TR4	26·7V
Junction of R9 and R10	26·2V
Base of TR5	0·7V
Collector of TR5	0·5V
Base of TR6	1·3V
Collector of TR6	27V
Across TR7 coll/emitter	I-1-5V
Junction of RI5 and RI6	47 V
Across R25 and R26	0·7V

Fault symptoms and possible causes

- Voltage at output terminal high
 - (1) TRIO or TRI2 short circuit or wrongly connected.
 - (2) TR4, TR5, TR6, TR11 or TR13 o/c.
 - (3) R9, R10 wrong value or R10 o/c.
 - (4) C8 s/c or leaky.

Voltage at output terminal low

- (1) TR4, TR5, TR6, TR11 or TR13 s/c or wrongly connected.
- (2) TRIO or TRI2 open circuit.
- (3) R9, R10 wrong value or R9 open circuit.
- (4) C6, C7 leaky or short circuit.

Bias current too low

- (1) TR7 short circuit.
- (2) R18 or R19 wrong value.

Bias current too high

- (1) TR7 o/c or wrongly connected.
- (2) R18 or R19 wrong value.

PREAMPLIFIER . . I. V. . I. . . .

Normal Voltages	
(Referred to common rail	unless
otherwise specified)	
H.T. rail	40V
Across C16	37·5V
TRI4 and TRI6 emitters	18V
TRI5 and TRI7 collectors	18V
TRIS and TRI7 emitters	28·5V
TRI8 emitter	6.8V
TRI9 emitter	24V
TR20 emitter	9∨
TR21 emitter	20V

Fault symptoms and possible causes

No output for all inputs

- (1) No h.t., check wiring and C52.
- (2) TR18, 19, 20, or 21 s/c or o/c.
- (3) Wiring error after S3.

Weak distorted output for all inputs

- (1) H.T. voltage excessively low.
- (2) TR18, TR19, TR20, or TR21 inserted wrong way round.
- (3) C33, C48, or C50 leaky or s/c.
- (4) Incorrect resistor value.

No output or weak distorted output on disc

- (1) TR14, TR15 o/c, s/c, or connected wrong way round.
- (2) CI7, CI8, or C23 leaky.
- (3) Incorrect resistor value.

No output or weak distorted output on Mic

- (1) TR16, TR17 o/c, s/c, or connected wrong way round.
- (2) C25, C27, or C29 leaky.
- (3) Incorrect resistor value.

Add 100 for right-hand channel component numbers o/c = open circuits/c = short circuit

EVER					PEC.		RGES	TOCKS NO SURPLUS
BAR	GAI	NS IN	NEW	SEMIC	OND	UCT		PEAK SOUND PRODUCTS ENGLEFIELD AMPLIFIER
2N606 2N607 2N706 2N706 2N1131 2N1132 2N1130 2N1303 2N1303 2N1305 2N1306 2N1306 2N1306 2N1306 2N1306 2N1307 2N1307 2N1307 2N1307 2N1307 2N1307 2N1307 2N1307 2N1307 2N2147 2N2219 2N2219 2N2219 2N2219 2N2219 2N2219	20p 22p 12p 29p 36p	tems at new reduc 2N2924 2N2925 2N2925 2N2925 2N3925 2N3925 2N3925 2N395 2N3702 2N3705 2N3705 2N3705 2N3705 2N3705 2N3707 2N3704 2N3704 2N3704 2N3711 2N3704 2N3711 2N3704 2N3711 2N3704 2N3704 2N3704 2N3704 2N3906 2N4058 2N40	20p 40361 22p 40382 40382 40382 40382 40382 13p AC127 13p AC128 13p AC127 13p AC128 13p AC127 13p AC128 13p AC129 13p AC129 13p AC129 13p AC129 13p AD140 13p AD140 14	wer types supplied wit	14p 14p 35p 35p 11p 11p 11p 11p 11p 11p 12p 25p 25p 25p 12p 33p 35p 34p 34p 35p 55p	BFX87 BFY50 BFY50 BFY51 BFY51 BFY52 BKX20 C307 MC140 MF86334 MF86334 MF86334 NKT212 NKT212 NKT214 NKT214 NKT214 NKT214 NKT214 NKT214 ZTX301 ZTX301 ZTX303 ZTX303	29r 28p 28p 20p 23p 18p 18p 23p 23p 23p 23p 23p 23p 23p 23p 23p 23	12 + 12 watis BLBS Stereo amplifier in modular kit form (including cabinel) 12 watis per channel Stereo amplifier in modular kit form (including cabinel) 12 watis per channel Stereo amplifier in modular kit form (including cabinel) 12 watis per channel BAXANDALL BAXANDALL Stereo amplifier in modular kit form (including cabinel) reproduction for its size. Handles 10 wath with ease. Uses ELAC 15D 3HRM199 speaker unit. Kt 213-90 mett; mult E19-40 nett; MAINLINE AMPLIFIER KITS RCA/80:8 designed main amplifier kits. ROA/80:8 designed main amplifier kits. Stable ansar
2N2484 2N2904 2N2904A 2N2905 2N2905A	42p 38p 42p 44p 47p	2N4284 2N4286 2N4289 2N4291 2N4292	15p BC108 15p BC109 15p BC125 15p BC126 15p BC126 15p BC147	12p BF194 14p BF195 55p BFX29 55p BFX84 15p BFX85	17p 18p 31p 25p 34p	ZTX 500 ZTX 501 ZTX 502 ZTX 503	25p 25p 30p 25p 60p	Kit price Suitable unreg. 10000 including components power supply kit 12W £2640 nett \$4.60 25W £9.50 nett N/A 40W £10.50 nett \$5.75 70W £12.60 nett £6.94
Code C 1, C	Power /20W #W #W	Tolerance 5% 5% 10%	Range 82 Ω - 220 4-7 Ω - 330 4-7 Ω - 101	kΩ E24	1 to 9 (see 7p 1p 1p	10 to 99 note below 6p 0.8p 0.8p	6p 0·7p 0·7p	30 WATT BAILEY AMPLIFIER KIT Sensitivity 1-2V for full output into 8Ω. Transistors and PCB for one channel \$7-30. Transistors and PCBs for two channels \$14-60. Capacitors and resistors (metal oxide) \$2p er channel. Complete unregulated power supply kit \$4-76.
C C MO WW WW	1W 1W 1W 1W 3W 7W	5% 10% 2% 10% ± 1/20 ດ 5% 5%	$\begin{array}{c} 4.7 \ \Omega - 100 \\ 4.7 \ \Omega - 100 \\ 10 \ \Omega - 100 \\ 0.22 \ \Omega - 3.9 \\ 12 \ \Omega - 100 \\ 12 \ \Omega - 100 \\ 12 \ \Omega - 100 \end{array}$	4 Ω E12 Ω E24 Ω E12 α E12 α E12	1-2p 2-5p 4p 7p 7p 9p	1p 2-5p 3-5p 7p 7p 9p	0.9p 1.9p 3p 6p 6p 8p	ZENER DIODES 5% full range E24 values: 400mW: 2-7V to 30V 19p ea. 1W: 6.8V to 82V 33p ca. 1-3W: 4-7V to 75V 60p ca. Clip to increase 1-3W rating to 3 watts (type 206P) 4p.
CODES: C wound Pless VALUES: H plus 11, 13, Pricet are in NOT mized order.)	e carbon fi sey. S12 denotes 16, 20, 24, 3 pence each j values. (I)	Im high stability series: 10, 12, 15, 30, 36, 43, 51, 62, 7 for same ohmic value grove fractions of 1	low noise. MO = 18, 22, 27, 33, 39, 4 15, 91 and their dec e and power raling, p on total resistor LIFJERS	metal oxide Electrosi 47, 56, 68, 82 and their ades. MULLARD PO 250V 20%: 0.01, 0 0-15, 4p e: 1.022, 5 1µF, 13p: 1.5µF, 21	il TR5 ultra decades. E LYESTER 022, 0033, (p. 10%: 033 p; 2.2µF, 24	low noise. 24 denotes s C280 se -047, 3p ea , 7p: 0.47, 4 p.	eries: as E12 ries .; 0.068, 0.1, 8 p; 0.68, 11p;	CARBON TRACK POTENTIOMETERS, long spindles. Double wiper ensures minimum noise level. Bingle gang linear 2200 to 2-2M0 129 Bingle gang log 47K0 to 2-2M0 229 Dual gang linear 47K0 to 2-2M0 429 Dual gang log 47K0 to 2-2M0 429 Dual gang log 47M0 to 2-2M0 429 Dual gang log 10K,47K,1M0 only 429 Dual to 2-2M0 429 429 Dual gang log 10K only 429 Please note: only decades of 10, 22 and 47 are available within ranges quoted. 47
SINCLAIR amplifier cir Componenta etc., 54-75 r PLESSEY SI	IC.10 comp cuit details s pack for st- nett. L463A. Onl	slete with instruct and range of applic ereo inc. mains tran y £2-75 each nett, on data 10 p: free	tion book giving ations, £2-95 nett. asformer, controls, 3W into 7-50 for	$\begin{array}{c} \mbox{\bf MULLARD SU} \\ C426 \ range axial leav \\ Values (\mu F V): \ 0.64 \\ 4/40, \ 5/64, \ 6.4/64, \ 6 \\ 12.5/25, \ 16/40, \ 20 \\ 32/10, \ 32/40, \ 32/64, \ 4 \\ 64/10, \ 80/2\cdot5, \ 80/16, \ 160/2\cdot5, \ 200/6\cdot4, \ 20 \\ 100/2\cdot5, \ 200/6\cdot4, \ 200/2\cdot5, \ 200/6\cdot4, \ 200/2\cdot5, \ 200/2\cdot$	1 6p each. 1/64, 1/40, 1 5-4/25, 8/4, 8 0/16, 20/64, 10/16, 40/2-5, 80/25, 100/6	6/25, 2·5/16 /40, 10/2·5, 25/6·4, 50/6·4, 50/2 ·4, 125/4, 1	2.5/64. 4/10, 10/16, 10/64,, 25/25, 32/4, 5, 50/40, 64/4, 25/10, 125/16,	CARBON SKELETON PRE-SETS Small high quality, type PR, linear only 100Ω, 220Ω, 470Ω, 1K, 2K2, 4K7, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M2, 5M, 10MΩ. Vertical or horizontal mounting 5p each.
1P 12W: 2	P6W; 3P	CHES LONG SPI 4W; 4P 3W .P.D.T.	NDLES 24p each	500/2-3. LARGE CAPAC High ripple current 1000/100 82p; 2000 2500/70 97p; 5000/2 10000/15 85p; 10000	types: 100			TYGON SPEAKER MATERIAL Seven designs, 36in × 27in sheets, 21-67 . Pattern books, send S.A.E. plus 3p in stamps.
Square beze Round chro Toggle swi chrome nill 28p; S.P.D .S-DeC's pu plug in S.	el, red only me bezel re itches, 250 led nut S.F. .T. centre o t an end t	d, amber, clear V a.c. 1.5A. Cl 28.T. 19p; S.P.D. ff 25p. o "birdsnesting". le time. Use com	19p 23p each rrone dolly and T. 22p; D.P.D.T. Components just ponents again and	MEDIUM RAN Axial leads: 30/30 9 330/25 129; 250/30 209; 100/350 309; 2 SMALL ELECT Axial leads: 4-7/10, 4 33/10, 50/10, 5p ea. 6p ea.	IGE ELEC p; 100/25 9p 19p; 500/25 ; 2000/25 80p. ROLYTIC 4:7/25, 5/50, 5 25/25, 25/4 COPPER	TROLY 100/50 12p 19p: 500/50 CS p es. 10/10 50, 47/25, 1 WIRE ex	FICS 5: 250/25 12p; 22p; 1000/25 0: 10/25, 10/50, 00/10, 220/10, en No. SWG.	 10% on orders for components for £3 or more. 15% on orders for components for £15 or more (No discount on nett items). POSTAGE AND PACKING Free on orders over £2. Please add 10p if under. Overseas orders welcome: carriage charged at cost.
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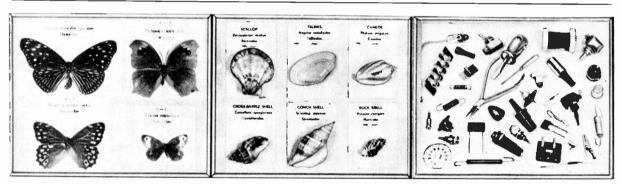
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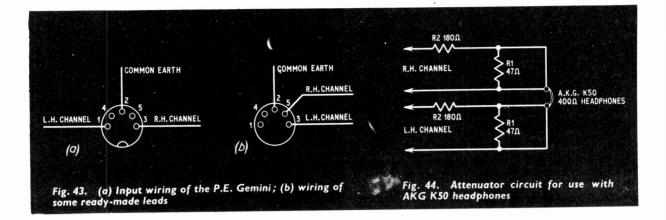
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TAPE INPUT

The tape input of the P.E. Gemini preamplifier has a flat frequency response and a sensitivity of 100mV at 50 kilohms, suitable for connection to the equalised output of a tape recorder or tape unit. The input is like this to accommodate the wide choice of speeds and equalisation standards (DIN, CCIR, and NAB at 15, $7\frac{1}{2}$, $3\frac{3}{4}$, $1\frac{7}{8}$ i.p.s.) many extra components and some complicated wiring and switching would be needed. If the low level output of your tape recorder is not equalised you will have to construct an "add on" equalisation stage to give an output of 100mV.

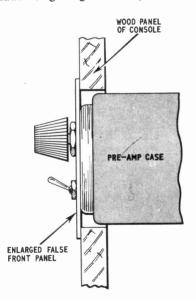


Fig. 45. Method of mounting the pre-amplifier in a console

HEADPHONE OUTPUT

The headphone output from the main amplifier is connected directly to the loudspeaker outputs and in most cases it will be necessary for the constructor to add an attenuator to reduce the volume to a comfortable level. Because of the wide variation in headphone impedances (4 to 600 ohms) and sensitivity between different types, the constructor will have to determine the correct values experimentally; Fig. 44 shows the circuit used, the values given being suitable for AKG K50 headphones of 400 ohms impedance. Resistor R1 should not be greater than the impedance of the earpiece and (R1 + R2) should not be less than 15 ohms, and preferably greater than 100 ohms if the attenuator is permanently wired to the amplifier. Some headphones have a built in attenuator and these can be connected directly to the headphone output socket.

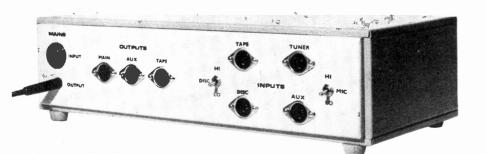
CASES

The Contil Mod 2 cases, used for both units, were chosen because they are relatively cheap, easily obtainable, and have an attractive if somewhat functional appearance. There is no reason why the constructor should not design his own case to match other equipment, provided that the case is well screened and the layout given is closely adhered to.

The preamplifier may be mounted in a console by increasing the size of the front panel so that it covers the hole required, as shown in Fig. 45. The front panel can be secured by screws from the front or clamps behind the panel.

ACKNOWLEDGEMENTS

The authors wish to thank Ferranti Ltd. for permission to publish this article and also L. Morral, R. J. Grundy and M. A. Rambaut for help given at various stages of the construction of the P.E. Gemini Amplifier.



Note: In Fig. 14 the arrow from tag 24 should go to FS2 not FS1. Main amplifier components list— R12 and R112 should be $1.2k\Omega$ not $1k\Omega$.



A^s MENTIONED in the first part of this article, "Contil" Mod-2 case type "C" is used to house the Digi-Clock, and this makes construction much simpler than if a "one-off" case design were to be employed.

The front and back panels of these cases are formed from p.v.c. covered aluminium, which makes the necessary hole cutting quite easy. The only tools absolutely necessary are a hand drill and a good file, but a clean and neat finish can be more easily achieved with a nibbling tool such as the "Monodex" sheet metal cutter.

CONSTRUCTION ON CHASSIS

The chassis supplied with the case is also made of aluminium and is used as a base-plate for all the main components, including the three circuit boards which are spaced from it only by three 6BA nuts. The chassis is earthed and acts as a low impedance "ground plane" for the logic circuitry, thus increasing the noise immunity of the system.

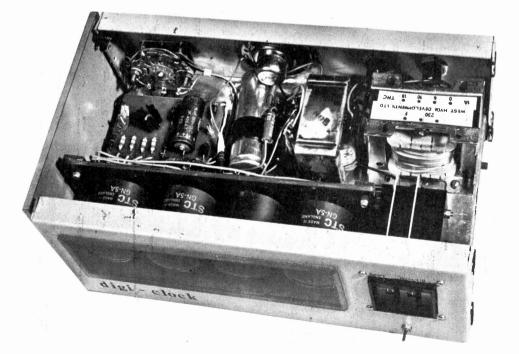
The series pass transistor TR2 employed by the 5V regulator uses the chassis as a heat sink; it is vital that this transistor is isolated from the aluminium by an insulating mica washer of the type normally supplied with this type of device.

Drilling dimensions for the chassis and front and back panels are given in the diagrams, and it is important to remember that some of the chassis holes are required to match other holes drilled by the constructor in the circuit boards and the display panel bracket. It is preferable to match these chassis holes to the latter, rather than drill all the holes straight from the diagrams.

The mounting bracket for the "Nixie" tubes is made from $\frac{1}{2}$ in s.r.b.p. sheet, and as can be seen from the diagram, the tubes are inserted directly into holes drilled in this bracket, no bases being employed.

With the dimensions given, the tubes are a tight fit in their mountings, and no extra fixative was used in the prototype. A dab of contact adhesive could be used if necessary, and still allow the tubes to be removed should this ever be desirable. Valve bases type B12A are available for the GN5A although the numeral spacing would have to be altered if these are used, since the tubes would not be so close together.

The decimal point indicator is mounted in a sin coil former or some other suitable tube, cut to the dimensions shown, and fastened to the display panel with contact adhesive. When being installed, the neon is simply pushed through from the rear of the bracket, its insulated leads providing all the tension necessary to retain it in the tube.



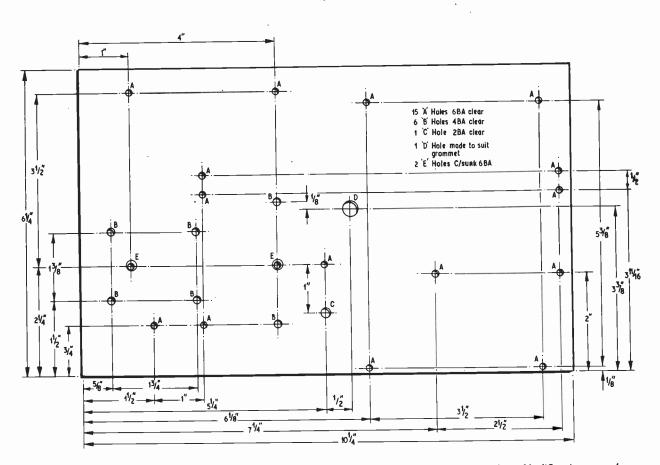


Fig. 17. Chassis drilling details assuming components used are as specified in the components list. Modifications may be necessary for variations of component type. Clearance above chassis $2\frac{1}{4}$ in

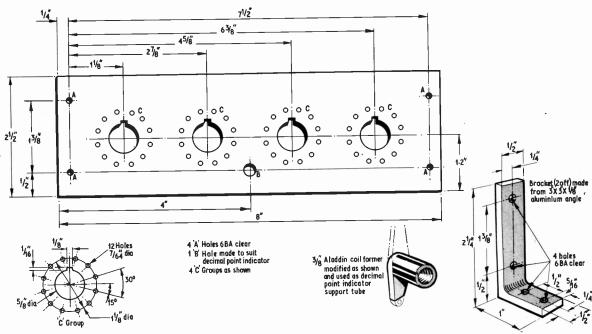


Fig. 18. Display panel drilling for "Nixie" tubes

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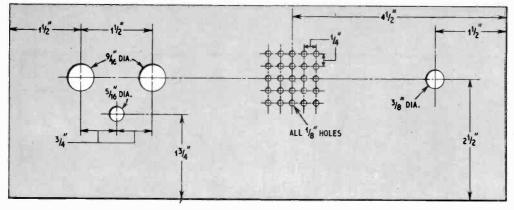


Fig. 19. Back panel drilling details for components specified

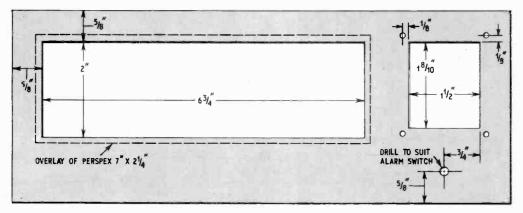


Fig. 20. Front panel drilling details for components specified

Table I: CONNECTIONS TO MAIN CLOCK BOARD "A"

(b) Copper side terminations

IC Numb	Hole er Number	Board ''A'' Outlet	Wire Colour	Destination \	IC Number	Hole Number	Board ''A'' Outlet	Wire Colour	Destination
-Resi	stor RI-	1	green	T2, 6·3∨				1000	
L .	6E	2	black	Sla wiper	1. I		23		
6	2E	3	red	Sic wiper			24		-
6	6A	4	orange	SIb wiper	14	6H	25	pink	V4 pin 10
13	4F	5	red	Board B5	14	6G	26	green	V4 pin L
13	3C	6	orange	Board B4	14	2A	27	red	V4 pin 2
13	3B	7	pink	Board B3	14	6A	28	brown	V4 pin 3
9	2H	8	violet	Board BI	14	6E	29	black	V4 pin 4
12	3E	9	green	Board B9	14	6F	30	white	V4 pin 5
9	2F	10	blue	Board BI3	14	6C	31	yellow	V4 pin 6
ALL	Ground	11	black	chassis	14	6B	32	orange	V4 pin 7
	Rail				14	2H	33	grey	V4 pin 8
ALL	+Vce rail	12	red	Board B12	14	2G	34	violet	V4 pin 9
12	3B	13	brown	Board BIO	12	6H	34	orange	V2 pin I
9	3G	14	yellow	Board B2	12	7G	36	green	V2 pin 2
11	7H	15	(optional	hours × 10	12	2A	37	grey	V2 pin 3
			zero li	ne to VI pin 10)	12	7A	38	brown	V2 pin 4
11	7G	16	yellow	VI pin 1	12	7E	39	pink	V2 pin 5
13	6H	17	grey	V3 pin 10	12	7F	40	yellow	V2 pin 6
13	6G	18	pink	V3 pin l	12	7C	41	red	V2 pin 7
3	3A	19	white	V3 pin 2	12	7B	42	black	V2 pin 8
13	6A	20	violet	V3 pin 3	12	2H	43	white	V2 pin 9
13	7E	21	yellow	V3 pin 4	12	2G	44	violet	V2 pin 10
13	6F	22	green	V3 pin 5					

⁽a) Plain side terminations

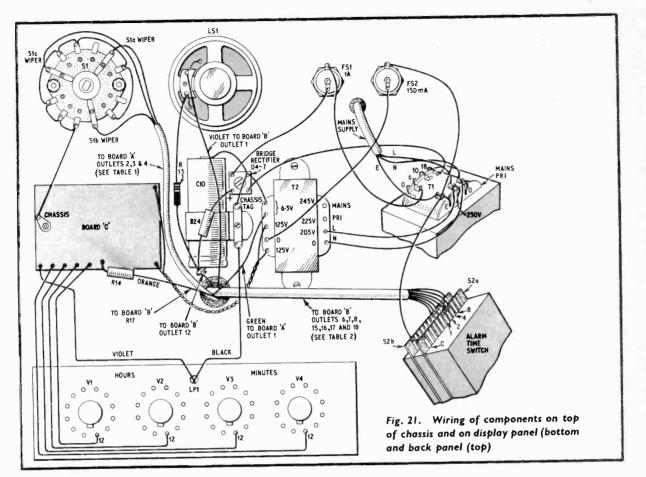


Table 2: CONNECTIONS TO ALARM BOARD "B" Copper side terminations only

IC Number	Hole Number	Board "B" Outlet	Wire .Colour	Destination
19	7D	1	violet	LSI
15	3H	2	yellow	Board AI4
15	3F	3	pink	Board A7
15	3A	4	orange	Board A6
15	7B	5	red	Board A5
15	3E	6	black	S2a/4
15	3B	7	violet	S2a/2
15	6C	8	brown	S2a/I
16	2H	9	green	Board A9
16	3F	10	brown	Board A13
ALL	Ground Rail	11	black	chassis
ALL	+Vce rail	12	red	Board A12 (5V)
16	2A	13	blue	Board A10
16	6B	14	violet	Board A8
16	6H	15	orange	S2b/8
16	3E	16	grey	S2b/4
16	3B	17	red	S2b/2
16	6C	18	blue	S2b/1
18	6D	19	orange	S3 (OFF)
(collecto Resisto	or of TRI)	20	red 1	TR2 collector, (IOV)
R21, 22		21	yellow	TR2 emitter
(TRI				
emitter) 3F	22	green	TR2 base

PRINTED BOARDS "A" AND "B"

The circuit boards carrying the i.c.'s are mounted on the chassis by means of 6BA bolts passing through each corner. Remember that the printed sides of these boards are adjacent to the chassis in the final assembly, and it will be necessary to make breaks in some cases in the printed tracks near the corner holes to prevent shorts to the chassis via the spacer nuts. Any breaks made for this purpose must be reconnected with wire links on the wiring side of the board.

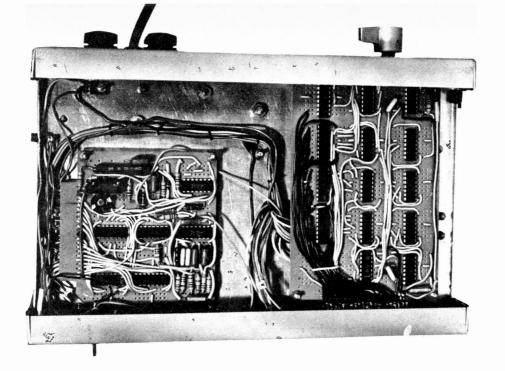
Note that in Fig. 13 last month C8 should be connected to the link wire to C7 and pin 4 of IC19.

Using 1in long bolts at the board corners allows their use as "legs" to support the chassis during wiring up, damage to the delicate boards being avoided. The transformers perform a similar task on the other side of the chassis.

WIRING UP

Once all the major components have been mounted on the chassis and the circuit boards have been tested for accuracy of fit, wiring up of the power supplies can be carried out. There is no need to attach the back panel wiring permanently at this stage, although it should be hooked in temporarily while the power supplies are tested, before proceeding further.

When the power supplies are operating satisfactorily, the interboard wiring can be started, remembering that the 5V regulator board has two wires leaving it which do not pass through the edge connector. All connections are given in Tables I and 2 for the boards



carrying the i.c.s. It is most important that only very fine p.v.c. covered flexible wire be used for this stage of the wiring, no other type of wire is suitable, as will become obvious as you proceed to wire up the Main Clock Board "A" edge connector with its 42 connections.

On completion of the interboard wiring the front and rear panels and their associated components can be attached to the chassis and the wiring finished off. The alarm speaker should be glued carefully to the rear panel with contact adhesive, making sure that it does not foul the smoothing capacitor or bridge rectifier wiring. The orange tinted Perspex filter is also fixed to the outside of the "Nixie" window front-panel cut-out with contact adhesive, and of course it is important that this operation be carried out with care to ensure a neat appearance.

The front and rear panels are finished off with "Letraset" dry print transfer lettering. The lettering should be sprayed with clear lacquer fixative to avoid damage during handling.

TESTING

There are no controls on the Digi-Clock which have to be set-up before operation, except the voltage control on the 5V regulator which should be set-up when the regulator wiring is completed, before its connection to the V_{ee} lines to the i.c. boards. This control setting should be rechecked with the clock operating normally, to ensure that the 5V line is as accurate as possible.

If on switching on for the first time, all appears healthy, the set-time switch may be used to set the display to the correct time.

With the switch set to the "fast" position, the minutes counter will be counting 600 times faster than normal, making it a simple job to set the display to within about 15 minutes of the correct time. The slow position is then used to facilitate the final setting, a minute being clocked up every second. As soon as the display is correct the switch is returned to the "normal" position, and the clock continues normally. If all is still well, the alarm circuit can now be checked. With the alarm "reset" switch in the "off" position, any valid time may be entered on the thumbwheel switches, after which the "alarm reset" switch is returned to the "set" state. When the "hours" and "tens of minutes" display counts to the same time as the alarm setting, the alarm should sound, and may be silenced by returning the "reset" switch to the "off" position. This check can be carried out with the clock running at a fast speed, making it a quick job to test all the alarm settings.

FAULT LOCATION

If problems are encountered during any of these tests, a constructor who has become familiar with the logic of the Digi-Clock should find it a fairly simple matter to trouble-shoot with the aid of a logic probe such as that shown in Fig. 22 or even a multimeter set to the low voltage range.

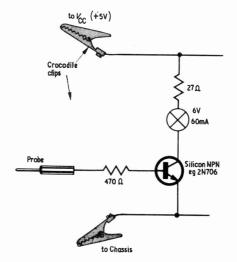


Fig. 22. Simple test circuit or logic probe

The important thing to remember if a fault is present in the logic circuitry, is that ten minutes working out what could be the problem with a pencil and paper, is worth hours of aimless probing and measuring. Logic faults, providing they have symptoms observable through the display, are not hard to find because they always follow some form of sequence, which, when analysed, usually yields the answer, without any testing in the usual sense.

One of the easiest faults to occur is the incorrect sequence of time indication, possibly with more than one digit showing on one tube. In this case, check that there are no short circuits or solder runs between adjacent outlets on the Main Clock Board "A". If erroneous alarm triggering should occur, check for a similar fault on the Alarm Board "B". Also make sure that the copper strips are cut correctly as shown at "X" in the first photograph (last month).

Check for solder runs between adjacent strips of copper; where these should not occur remove the solder. The wiring diagrams in Figs. 5 and 13 show the only places where these may occur intentionally.

The wiring tables and diagrams give colours to the wires as they were in the prototype. There is no reason why these should not be changed, but they are given to help the constructor to follow the wiring through if a fault is apparent.

TENS OF HOURS DISPLAY

Readers may have noticed that in the block diagram given in part one of this project, the tens of hours "Nixie" has two connections to its cathodes, one being a dotted line to the "0" numeral. This connection was shown in this way because it is a matter of personal taste whether the "0" needs to be used at all, a more conventional readout being given by allowing this tube to be completely blank during the hours of one to nine o'clock.

The decoder is, of course, able to accommodate either method, and the wiring diagram given in part one includes an edge connector contact for the "0" at outlet 15 of Board "A" so that it can be wired up if desired. This would be connected to pin 10 of V1.

MODIFICATIONS

Apart from the alarm expansion scheme discussed in Part 2, many other improvements can be incorporated in the Digi-Clock if required. The operation of the clock counters could be altered to conform to the 24 hour system, counting could be extended to include an a.m./p.m. flip-flop, or even a calendar, provided the extra components required could be accommodated.

A slave display, or even several slave displays, could be driven by the basic circuit. In this case the outputs of the clock counters should be buffered by TTL gates or inverters and fed to lines which terminate in further buffers at the slave end.

Fairly long lines could be driven by this method because of the slow speed operation and the relative unimportance of noise at this end of the system. The slave units would consist of a few buffer gates as mentioned and four SN7441AN decoders to drive the "Nixies". A simple power supply would also be needed.

Finally, for anyone who finds the fairly high outlay on the Digi-Clock components unjustifiable, the masterslaves system might tip the balance, because this type of system would become more economic as more slaves were added.



SOUND CONTROLLED LIGHT DISPLAY

Following its recent success at the Audio & Music Fair, Practical Electronics now presents the full do-it-yourself details of this fascinating addition to the sound scene. Part one of thisseries appears in the April issue.

P.E. Aurora is a controlled colour light display system which can be fed from any audio amplifier to provide the appropriate mood setting in the home or discotheque. It will respond to serious music or pop and can be arranged to give random displays from a digital sequencer.

Also:

* BOAT SPEED INDICATOR * DOOR YODELLER



APRIL ISSUE ON SALE MARCH 19

SIMPLE REFLEX A SPECIAL RECEIVER



A SPECIAL PROJECT FOR BEGINNERS

THE crystal receiver has for a long time been for many their first introduction to table top electronics. It isn't difficult to seek out the reason for its appeal, for this first-time project can be an unending source of entertainment pleasure for a modest outlay.

For the T-Dec form of plug-in construction that has been maintained throughout this series, the choice of receiver circuit was based on the requirements of good stability, that is no "howls" or unwelcome oscillations, and excellent volume with little aerial and no earth in areas of good signal strength.

REFLEX ACTION

Radio signals are characteristically of high frequency. For the medium wave-band which this receiver will tune to, this covers the range from 500 to 1,500kHz (200 to 600 metres).

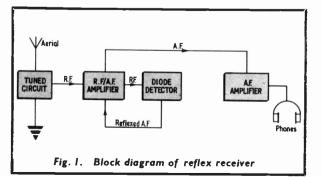
Since many transmitters are sending out signals in this band, the receiver must be able to select the one required. In the block diagram of the receiver Fig. 1, the tuned circuit enables such selection to be made.

Since the currents generated in the aerial system are extremely weak, it is necessary to amplify them before they reach the diode detector.

The detector has the job of removing the desired audio signal from the high frequency signal which has, in effect, carried it pick-a-back from the transmitter.

The title of the circuit, "reflex", derives from what now follows. Audio output from the detector is reflected back through the r.f. amplifier so that this stage plays a dual role in boosting first the r.f. and then the extracted a.f. signals.

The output is taken through a further amplifying stage and then to the headphones.



RECEIVER CIRCUIT

The complete receiver circuit diagram is given in Fig. 2. Here the tuned circuit consists of T1 primary and TC1. An aerial coupling capacitor C1 is included to improve selectivity; however, it must be borne in mind that with this simple type of single tuned circuit receiver, station separation is not ideal since it follows that the more tuned circuits used, the sharper is the tuning of that receiver.

The coils of the aerial transformer are wound on a ferrite slab which has the capacity to concentrate r.f. energy in its length and so improve signal strength. In areas where signals are very strong, it may be possible to dispense with a wire aerial and earth provided the slab aerial is orientated for maximum signal.

CHOKES

The selected r.f. signal voltage is passed to the base of TRI by transformer action. Biasing of this amplifier is achieved by R1, R2 and R4.

The low level signal appears amplified at the collector but at this juncture it is faced with two routes to follow. The choke L1 offers a high impedance path to radio frequency signal current whilst C3 does not. Signal voltages developed across L2 are applied to the detector D1, the desired audio programme material is then "unloaded" from the r.f. carrier and passed back to the input of TR1, via C6.

The audio signal is amplified and passed directly to the load resistor R3 since at low frequencies the resistance of the choke L1 is small. The capacitor C5 passes this a.f. signal to a second amplifier stage, TR2, which provides the power for the headset.

SETTING UP

Providing the component layout of Fig. 3 is adhered to, no reception problems should be encountered.

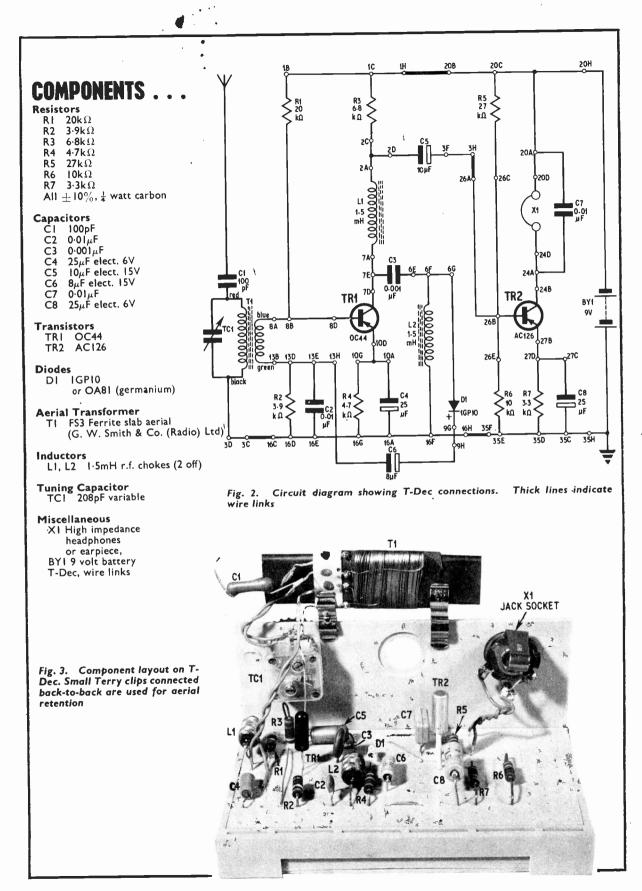
Whilst this receiver will give a good account of itself even with a short length of wire connected to C1, a good aerial will increase the sensitivity enormously in areas of difficult reception.

To demonstrate the effectiveness of a fair sized aerial, try connecting the co-axial outer of the television aerial to Cl, after first removing it from the set. Crocodile clips can be used for this. Bedtime listeners will find the bedsprings a convenient aerial, here once again, a crocodile clip will prove a suitable connector.

In general, at medium wavelengths, the receiving aerial takes the form of a vertical wire length, a common variant includes a horizontal top section of a few metres, but this sort of receptor would only be justified with the most elementary of crystal receivers.

SPANNING THE BAND

To cover the medium waveband, it may be necessary to adjust the aerial coils on the ferrite slab. This merely involves moving the coil former until, say, Radios I to 4 can be tuned using TC1.





Above: A transmitter being fitted to a racing car Below: One of the 60 foot display pylons

Racing Car Data Display

M^{INIATURE}, battery powered transmitters, fitted to the sides of racing cars, are being used for the first time in America, to increase spectator interest. They give instant, continued information on the position of every car on the track.

Underground sensors at the track—Ontario Motor Speedway, California—enable the transmitters accurately to "fix" the car's position at all stages of a race. The transmitters feed this information direct to a computer which evaluates it, prints out the race order, and relays the race data direct to visual displays on three 60 foot pylons.

The radio transmitters used in this revolutionary scoring system rely upon the power provided by four 1.5V Mallory alkaline batteries (left).

The innovation has proved so popular with spectators that the track organisers now plan to install an additional and even more sophisticated display—a mammoth animated sign which gives times, laps, car numbers and other digital information.

Unfortunately electronics does not always keep everybody happy. Used on the race track it has information and entertainment value and probably upsets or inconveniences nobody, however a slightly different application—still relating to cars—and many motorists get hot under the collar and start writing letters to magazines and the police about unfair and unashamed trickery. The application is of course the radar speed meter and no doubt many readers will be interested to know that an improved version has recently been announced by Shorrock Developments Ltd., part of the Hawker Siddeley Group Ltd. (see below).

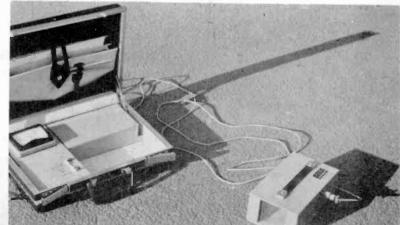


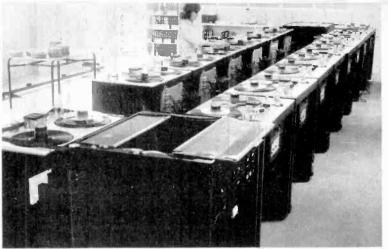
New Sh(orr)ock for Fast Drivers

The Shorrock microwave radar meter has two advantages over equipment at present used by the police: firstly, it is about two-thirds cheaper; and, secondly, it is much less obtrusive.

The Shorrock equipment is contained in a standard document case, weighing 20lb (9kg) complete. For use, the radar head is left at the roadside and a cable is run to the document case which can be used from a car parked in a side turning or other *comfortable* site. Power is provided by two 9V dry batteries and calibration can be carried out using the tuning fork provided.

More than 40 county authorities are using Shorrock speed indication equipment and police forces are showing interest in it.





Oujetened noise on Musicassettes

DECCA 8-track stereo Musicassettes are now in full production at the Company's own factory at Bridgnorth and made exclusively from master tapes utilising the Dolby "A" noise reduction system which produces a significantly improved signal to noise ratio. It is claimed that these Musicassettes offer the best quality of sound now available on this format and that this single factor will be one of the most significant selling points.

The tape duplicating equipment consists of two mother reproducers (also known as "master machines"), two loop bins and 13 slave recorders. One mother reproducer and loop bin is seen in the foreground of the photograph.



Computerised Telephone Trouble Shooter

A N aptly-named Argus computer system to watch over the reliability of the telephone service has been ordered by the Post Office from Ferranti Ltd. The Argus 500 configuration is to be installed in Leicester about the end of 1971 for trials that could lead country-wide to the faster detection of faults, further improvements of service for customers, and cost savings.

Acting as a round-the-clock trouble shooter, the £180,000 on-line computer system will monitor performance, draw instant attention to faults and impending breakdowns and alert maintenance engineers, enabling them to start repair work much sooner. Repairs will often be completed without the customers being aware that a fault has ever developed.

The computer will help network development staff to provide additional plant where it is needed by tracing the pattern of calls and identifying the most commonly used routes, and by keeping a constant check on the volume of calls being made. It will also analyse signals from the equipment-testing devices already used to provide engineers with information on fault-prone equipment. The computer's analysis of these tests of individual pieces of exchange will show where overhaul is needed and provide an additional safeguard against breakdown.

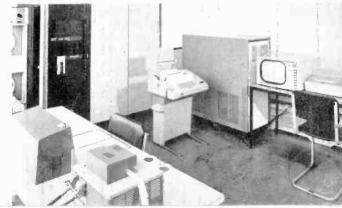
Right—a typical Argus 500 configuration, this is a similar system to that to be installed at West Wigston Exchange, Leicester.



Infra-red Thermometer Finds Faults in Wiring

A New infra-red thermometer—the LR120 Raynger—has recently been announced by A. Levermore and Co. Ltd. The LR120, shown above, has many industrial uses but the prime applications are in the electricity generating and distribution industry for locating faults in overhead cable connectors, transformers, splices, etc. which show themselves by small temperature rises.

To cope with these difficult operating conditions, the Raynger, which is battery operated and completely portable, has been designed to measure temperatures between 0 and 100 degrees Centigrade above ambient, giving a resolution of better than 2 degrees. The ratio of distance to object size is 120:1, e.g. a 2 inch diameter area can be accurately measured at 20 feet distant.



Practical Electronics March 1971



A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded payment according to its merit.

FUSE FAILURE INDICATOR

A SIMPLE way of giving an indication of when a mains fuse has blown is to connect a neon and its series resistance in parallel with the fuse as in Fig. 1. When the fuse is intact the resistor and neon are shorted, but when the fuse has blown they are effectively connected across the mains via the load resistance and the neon will strike.

A neat way of using a neon to indicate in a positive manner if the fuse is intact or not, is to have the neon lit steadily under normal conditions and for it to flash at a desired rate, should the fuse blow. The circuit evolved is a simple modification to an RC relaxationoscillator in which a capacitor is charged via a resistor (see Fig. 2a) until it reaches the striking voltage of the neon. At this point the neon strikes, discharging the capacitor to a level at which the neon extinguishes. The capacitor then commences to recharge and the cycle repeats, Fig. 2b.

Referring to Fig. 3, with the fuse intact, on positive half cycles current is fed to the neon and capacitor via D1, D2, R1, and R2, whose resultant resistance is such that good, even illumination of the neon takes place. Should the fuse blow, however, diode D2 is connected via the load to the neutral side of the supply and is therefore reverse biased. Current is then limited by the larger resistance R1 to give a long time constant. The capacitor takes longer to reach the striking voltage of the neon with the result that the neon flashes repeatedly drawing the attention of the operator to it. One advantage of this circuit is that the neon will flash irrespective of the load resistance, whether it is open or short circuit.

The flash rate can be adjusted by altering the value of either C1 or R1, but if R1 is altered then corresponding alterations will have to be made to R2.

One point to notice is that as C1 is charged to the striking voltage of the neon, the diodes should have a peak inverse voltage rating greater than peak mains plus this striking voltage.

S. J. Forrest, Witney, Oxford.

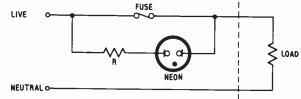


Fig. 1. Simple fuse failure circuit diagram

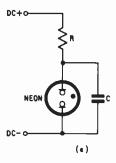


Fig. 2a. Circuit diagram for a flashing neon indicator

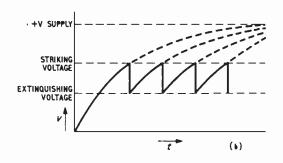
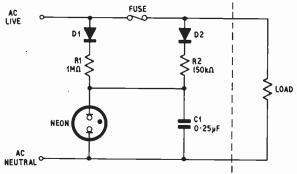


Fig. 2b. Graph showing the effect of the capacitor on the voltage across the neon



FLASH RATE FOR VALUES GIVEN = APPROX 2 PER SEC

Fig. 3. Final circuit diagram for the flashing neon version of the fuse failure indicator

LINEAR SCALE OHMMETER

ENCLOSE a circuit for a linear scale ohmmeter which may be of interest to your readers.

The circuit diagram Fig. 1a consists of a constant current generator TR1 and TR2, and a high input impedance meter driver TR4. A constant current is sent through the unknown resistor R_x and the voltage across it measured. Transistor TR3 compensates for the V_{be} drop across TR4. The current is set by varying

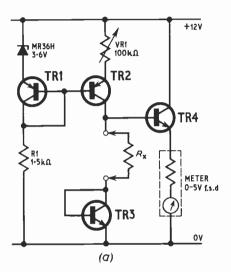


Fig. Ia. Circuit diagram of the linear scale ohmmeter

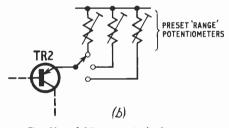


Fig. 1b. Adding a switched range

potentiometer VR1, which can be replaced by several resistors to give switched ranges, Fig. 1b.

On setting up, a one per cent resistor of value equal to the desired f.s.d. is used as R_x and VR1 is adjusted to give full scale deflection. The meter will then read any value resistor in that range as a linear proportion of full-scale.

For very high ranges, the single emitter follower should be replaced by a two-stage circuit as shown in Fig. 2. In theory there is no limit to the range, but in practice, components limit the maximum range.

The advantages of this circuit over conventional linear ohmmeters is that a cheap meter can be used, and the unit is accurate over a wide range of temperatures.

lan R. Hornby, Timperley, Cheshire.

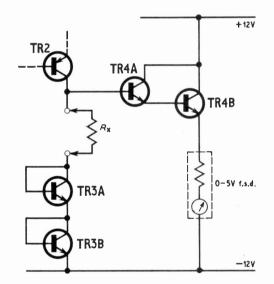
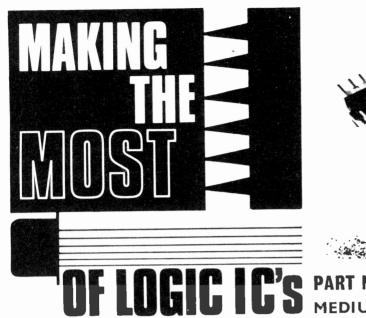


Fig. 2. Two-stage version for very high ranges

The "P.E. Aurora Lighting Display" will be included among the exhibits making up the *Electric Theatre*. This is an exhibition of artistic works which make specific use of electrics, electronics and mechanics to create effects with light and sound.

The *Electric Theatre* will be held at the Institute of Contemporary Arts, Nash House, The Mall, London, S.W.1., from March 18 to April 18 inclusive, 11 a.m. to 10.30 p.m. daily. Admission (at the door) 25p, students and members ICA 15p.

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GIC IC'S PART NINE-By R. W. COLES MEDIUM SCALE INTEGRATION

ALL monolithic i.c.s start off as discs of silicon, an inch or so in diameter, on which may be built several thousand simple gates. We have already seen that by connecting together gates only, it is possible to build many different types of flip-flop, and by connecting together flip-flops it is possible to build counters and shift registers.

It is only a short step from this line of reasoning, that counters and shift registers could be built at the i.c. processing stage, by joining together a large number of gates to produce the logic required. This is, in fact, how MSI devices are built.

BASIC MSI CONCEPT

A chip of silicon cut from the disc and containing around 30 gates, has a layer of metal deposited as an interconnection pattern, perhaps to form a four stage binary counter. The finished chip is mounted on a lead frame and packaged in the usual way as there are no space problems to worry about.

A dual-in-line pack is vast compared with the silicon chip it contains, whether it forms a flip-flop or a counter. The limitation to this process comes only with the restricted number of lead-outs the standard package can accommodate, not the size of the chip it can contain.

Fortunately the lead-out problem is not as severe as one might imagine, because most of the interconnections required to produce a complex function device are performed internally. Only the essential inputs and outputs are required to see the light of day.

What does this process do to help the designer or experimenter? The most obvious effect is the reduction in cost, a decade counter built using separate gate and flip-flop packages could cost in the region of £3 10s (£3.5), whereas the same function can be obtained from the MSI range for about £2. The number of packages in this example is reduced by a factor of three, another very important saving.

Using MSI, it is possible to think in terms of counters

as building blocks instead of just flip-flops. The design of this larger block has already been carried out by the manufacturer, so a system is much easier to design, or it may be more complex for the same design effort.

All these things add up to an impressive list of advantages, which can be put to good use by the amateur constructor.

BUILDING BLOCKS

TTL complex functions are contained in the usual 14and 16-pin dual-in-line packages, and their equivalent in the flat-pack range; there is no external difference apart from the way the pins protrude. The inputs and outputs are completely compatible with the rest of the family, and usually employ the same type of circuitry.

However, the gates used inside the package are sometimes different in construction, because internal gates may not need the fan-out capability of others which have to drive external circuits. It is not intended here to go too deeply into the internal workings of MSI devices; earlier articles have already described the individual circuits in the TTL range.

We need only treat them as the useful building blocks that they are.

MSI COUNTERS

Several different counters are available in the 74 series, each of which may be used for many different jobs and connected in several different configurations. Let us have a look at a typical example, the 7490 decade counter, which is shown in Fig. 9.1.

This counter, like the others in the series, is a ripple type, made up of four master/slave flip-flops; three of them are JK types and one a set/reset. It consists of two separate sections, a divide-by-five stage and a divide-by-two stage, which may be externally interconnected to give two different count modes, depending on the application.

The asynchronous flip-flop inputs are connected to two internal NAND gates which, when enabled, allow the counter to be reset either to zero (0000) or nine (1001).

If the count input is connected to the divide-by-two input, and the output of flip-flop A is connected to the divide-by-five input, the counter will count in the binary coded decimal code, as shown in the truth table in Fig. 9.1a. In this mode the counter behaves as a normal four-stage binary counter until it reaches the count of nine; the next clock pulse sets the counter to the all zeros state.

This type of counter is employed when the outputs have to be decoded to drive indicator tubes, for instance in a frequency counter, or integrating digital voltmeter.

The secondary count mode is obtained by connecting the count input to the divide-by-five input, and the output of flip-flop D to the divide-by-two input, in effect causing the output of the divide-by-five counter to be divided by two, the opposite of the first count mode.

The truth table for this type of count is also shown in Fig. 9.1b, and it can be seen that the divide-by-ten output is taken from flip-flop A as a symmetrical waveform, up for five counts and down for five counts. This kind of count code is generally called the 1245 code, and is useful where these counters are used just as frequency dividers, for instance in frequency synthesisers.

These counters may be used to divide by numbers less than ten by using the reset gates to detect the desired final count plus one, and reset the counter to 0000, or even nine, at this time. Any division by less than ten is possible, and an application is shown in Fig. 9.2, where a 7490 is used as a divide-by-six counter.

The other two counters in the series are similar to the 7490, but have a divide-by-six and divide-by-eight section respectively, instead of the divide-by-five of the 7490. They also do not have the facility of nine reset, only the zero reset is included.

MSI DECIMAL DECODERS

Very often, the output of a decade counter is required to be decoded to the "one-of-ten" decimal equivalent of the binary count, in order that it may be displayed on some form of indicator. It is not surprising then, to find that the 74 MSI range contains several circuits which are capable of achieving this.

As an example let us look at the 7441 decoder/driver package. The 7441 takes a four-line binary coded decimal input word, and by means of gates and inverters, decodes this information into its decimal form, giving ten separate outputs. The outputs in this case are not designed to drive other logic gates, but to drive neon number indicating tubes such as "Nixies".

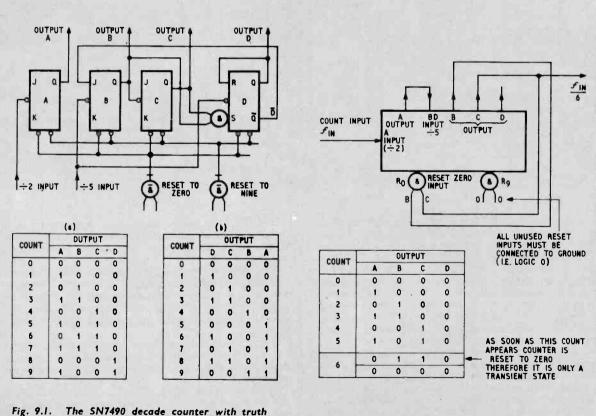


Fig. 9.1. The SN1490 decade counter with truth tables for (a) binary coded decimal (b.c.d.) count mode and (b) symmetrical÷10 mode

Fig. 9.2. The SN7490 used as a $\div 6$ counter with truth table

This type of indicating tube uses ten separate cathodes, each in the shape of a decimal character, and a common anode. The anode is connected, through a limiting resistor, to an h.t. supply of the order of 200 volts. When a particular cathode is grounded the number it represents is illuminated by the ionisation of the neon gas surrounding it.

Fortunately, it is not necessary to use transistors 'which will stand 200 volts on their collectors to drive these tubes, because reducing the voltage across them by only (say) 50 volts is sufficient to extinguish them, as this reduces the total voltage to below the "striking" potential.

In fact, the output transistors of the 7441 will withstand at least 55 volts, and to ensure that this rating

Many other types of decoding may be performed with the large range of circuits available in the 74 series. Some have the standard TTL output stage, others will drive incandescent lamps. Some will even drive seven segment display systems, and in these, more than 35 separate gates are employed.

MSI ADDERS

Adder circuitry, as we have already seen, is fairly complex, and now that computers are growing faster and faster, the use of parallel arithmetic is increasing, bringing with it a demand for large numbers of separate "full-adder" blocks.

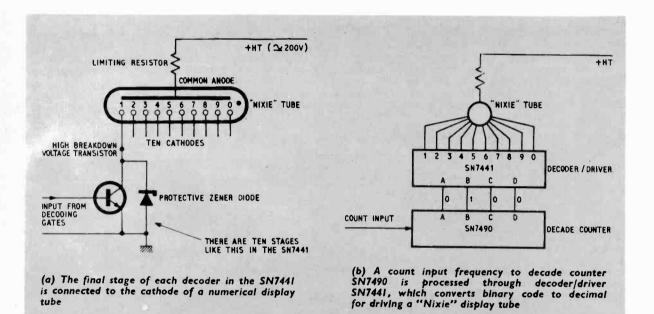


Fig. 9.3. MSI used to drive a cold cathode display

is not exceeded a Zener diode is connected from collector to ground. The basic idea of the output circuits used with these i.c.s is shown in Fig. 9.3.

To drive the ten output stages the four line binary word at the input to the 7441 has to be decoded by appropriate gating, and to carry out this decoding correctly, complementary information is necessary, i.e. A and NOT A, B and NOT B, etc. The generation of the inverted form of the input word is carried out internally, which makes things much easier, as only the true information needs to be supplied.

There is no doubt that this i.c. represents excellent value for money when compared with any of the possible discrete approaches. Even if i.c.s were employed to perform the gating, the price of ten high breakdown transistors would be more than a single 7441, which is a fraction of the size.

Fig. 9.3b shows the 7441 being used to decode the output of a 7490 decade counter, which has reached a count of two. This could represent one stage of a frequency counter.

The 74 MSl range offers three separate types of full-adder. The one which is, perhaps, most interesting is the 7483, so let us have a closer look at this one as an example.

The 7483 has four complete full-adders crammed into one 16-pin dual-in-line package. Because it is intended for use in parallel addition computers, the carry line is internally connected between the four adders, making it possible to add two four-bit numbers together in less than 50ns.

There are A and B inputs to each adder, with a single carry input to the first stage, and a single carry out from the fourth stage; four separate sum outputs are provided.

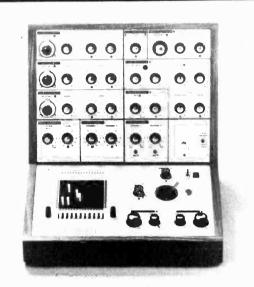
The logic of the 7483 is shown in Fig. 9.4; it is left to the interested reader to work out the truth table of the entire system, which will be in line with that given with the discrete-gate version in the section on gates.

Readers may think that it is unlikely they will be building a parallel arithmetic computer in the near future, and so this particular i.e. is of little interest, but a

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$1N85 \\ 1N253$	0-88 0-50	AC187 AC188	0·30 0·30	BF184 BF185	0-25 0-25	GJ7M HG1005	0-38 0-50	0C45	0·18 0·15
$1N256 \\ 1N645$	0.50 0.25	ACY17 ACY18	0·30 0·25	BF194 BF195	0-18 0-15	HS100A MAT100	0·20 0·25	OC45M OC46	0·18 0·28
1N725A	0.20	ACY19	0.25	BF196	0.28	MAT101	0.30	OC57 OC58	0.60
1N914 1N4007	0.23	ACY20 ACY21	$0.23 \\ 0.23$	BF197 BF861	0-28 0-28	MAT120 MAT121	0.30	OC59	0.65
18021 18113	0.20 0.15	ACV99	0·18 0·25	BF898 BFX12	0.28	MJE520 MJE2955	0-88 1-75	OC66 OC70	0-50 0-13
18130 18131	0·13 0·13	ACY27 ACY28 ACY39	0-18	BFX13 BFX29	0-23	MJ E3055 NKT128	0-93	OC71 OC72	0.15
18202	0.23	ACY40	0.55 0.15	875 30	0.33	NKT129 NKT211	0.30	0C73 0C74	0.80
2G240 2G301	1.98 0.18	ACY41 ACY44	0-25 0-38	BFX35 BFX63	0.98	NKT213	0-25 0-25	0C75	0-30 0-25
2G302 2G306	0.23	AD140 AD149	0-50	BFX84 BFX85	0-30 0-40	NKT214 NKT216	0.15	OC76 OC77	0.25
2G371	0.23	AD161	0.38	BFX86	0.33	NKT217	0.40	OC78	0.20
2G381 2G414	0-25 0-30	AD162 AF106	0-38 0-30	BFX87 BFX88	0-88 0-25	NKT218 NKT219 NKT222	1.13 0.33	OC78D OC79	0·13 0·23
2G417 2N214	0·23 0·43	AF114 AF115	0.33 0.30	BFY10 BFY11	1.00 1.25	NKT222 NKT224	0-20	0C81 0C81D	0-25 0-20
2N247 2N250	0.25	AF116	0.33	BFY17 BYF18	0.25	NKT224 NKT251 NKT271	0.24	OC81M OC81DM	0-20 0-18
2N404	0.23	AF117 AF118	0-25 0-63	BFV19	0.25	NKT979	0.25	OC81Z	0-55
2N697 2N698	0.18 0.43	AF119 AF124	0·20 0·25	BFY24 BFY44	0-45 1-00	NKT273 NKT274	0.20	OC82 OC82D	0-25 0-15
2N706 2N706A	0.10	AF125 AF126	0.20	BEV50	0.23	NKT275	0.25	OC83 OC84	0-25
2N708	0.15	AF127	0-18 0-18	BFY51 BFY52	0.23	NKT277 NKT278	0.25	OC114	0-38
2N709 2N711	0-63 0-38	AF139 AF178	0-30 0-48	BFY53 BFY64	0-18 0-43	NKT301 NKT304	0·30 0·35	OC122. OC123	0-50 0-50
2N987 2N1090	0.53 0.30	AF179 AF180	0-48 0-53	BFY90 BSX27	0-68 0-50	NKT403 NKT404	0.75	OC139 OC140	0-25 0-38
2N1091 2N1131	0.33	AF181	0.43	B8X60	0.93	NKT678	0.80	OC141 OC169	0.63
2N1132	0·30 0·30	AF186 AFY19	0·40 1·13	BSX76 BSY26	0-15 0-18	NKT713 NKT773	0-25	OC170	0.25
2N1302 2N1303	0·20 0·23	AFZ11 AFZ12	0.63	BSY27 BSY51	0-20	NKT777 078B	0-38 0-38	OC171 OC200	0.30
2N1304 2N1305	0.25	ASY26 ASY27	0.25	BSY95A BSY95	0-15	0A5 0A6	0.15 0.13	OC201 OC202	0-48
2N1306	0.25	ASY28 ASY29	0·33 0·25	BT102/50	0 R	OA47	0.10	OC203	0.38
2N1307 2N1308	0·25 0·30	ASY29 ASY36	0-30 0-25	BTY42	0-75 0-93	0A70 0A71	0-10 0-10	OC204 OC205	0-40 0-68
2N1309 2N1420	0-25 0-93	ASY50 ASY51	0.18	BTY79/10		0A73 0A74	0.10 0.10	OC206 OC207	0-75 0-75
2N1507	0.28	ASY53	0-20	BTY79/40	10 R	0.479	0.10	OC460	0-20
2N1526 2N1909	0-38 2-25	ASY55 ASY62	0-20 0-25	BY100	1.75	0A81 0A85	0·10 0·13	OC470 OCP71	0-80 0-98
2N2147 2N2148	0-75 0-60	ASY86 ASZ21	0-33 0-43	B¥126	0.15	0A86 0A90	0·15 0·10	ORP12 ORP60	0-50 0-40
2N2160 2N2218	0.63	ASZ23	0.75	BY127 BY182	0-20 0-75	OA91	0.08	ORP61 S19T	0-43
2N2219	0-30 0-33	AUY10 AU101	0.98	BY213	0.25	0A95 0A200	0-08 0-08	SAC40	0-25
2N2287 2N2297	1.03 0.30	BC107 BC108	0-25	BYZ10 BYZ11	0-40 0-35	0A202 0A210	0·10 0·25	SFT308 ST722	0-38 0-38
2N2369A 2N2613	0-20 0-28	BC109 BC113	0.25	BYZ12	0.80	0A211 0AZ200	0-38 0-55	ST7231 SX68	0-63 0-20
2N2646	0.53	BC115	0.33	BYZ13 BYZ15	0-25 1-00	OAZ201	0.50	SX631	0.20
2N2712 2N2784	0-25 0-50	BC116 BC116A	0-40 0-45	5YZ16	0-63	OAZ202 OAZ203	0-43 0-43	SX635 SX640	0.25
2N2846 2N2848	2·25 0·43	BC118 BC121	0.38	BYZ88C3	V3 0-18	OAZ204 OAZ205	0.43	SX641 SX642	0-25 0-38
2N2904 2N2904A	0-30 0-33	BC122 BC125	0-20	C111 CR81/05	0.65	OAZ206 OAZ207	0-43 0-48	8X644 8X645	0-48 0-75
2N2906	0.30	BC126	0.65	CR81/40	0-48	0 AZ208	0.33	V15/30P	0-50
2N2907 2N2924	0-38 0-23	BC140 BC147	0-55 0-18	CS4B CS10B	2·50 3·13	OAZ209 OAZ210	0-83 0-33	V30/201P V60/201	0-38 0-38
2N2925 2N2926	0-18 0-13	BC148	0.13	DD000 DD003	0-15 0-15	0AZ211 0AZ222	0-33	V60/201P XA101	0-38 0-10
2N3054 2N3055	0.50	BC149 BC157	0-20	DD006 DD007	0.18	OAZ223 OAZ224	0-40	XA102 XA151	0-18 0-18
2N3702	0.13	BC158	0-20	DD008	0.38	OAZ241	0.23	XA152	0-15
2N3705 2N3706	0-15 0-23	BC160 BC169	0-63 0-13	GD3 GD4	0.33 0.05	OAZ242 OAZ244	0-23 0-23	XA161 XA162	0-25 0-25
2N3707 2N3709	0-15 0-13	BCY31	0.30	GD5 GD8	0-33 0-25	OAZ246 OAZ290	0-23	X B101 X B102	0-43
2N3710 2N3711	0·13 0·13	BCY32 BCY33	0.50 0.20	GD12 GET102	0.05	OC16 OC16T	0.43	XB103	0.25
2N3819	0.35	BCY34	0.25	GET103	0.23	OC19	0-88	X B113 X B121	0·10 0·43
2N3820 2N3823	0-88 0-75	BCY38 BCY39	0-30 0-48	GET113 GET114	0-20 0-15	OC20 OC22	0-98 0-48	ZR 24	0.63
2N5027 2N5088	0-53 0-33	BCY40 BCY42	0-43 0-15	GET115 GET116	0-45 0-50	OC23 OC24	0-50 0-50	Z8170 Z8271	0·10 0·18
28005	0-75	BCY70 BCY71	0.20	GET120	0.25	0C25	0.38	Z5211 ZT21	0.25
28301 28304	0-43 0-63	BCZ10	0-30 0-30	GET872 GET875	0-30 0-25	OC26	0.25	ZT43	0.25
28501 28703	0+38 0+63	BCZ11 BD121	0-38 0-65	GET880 GET881	0-38 0-25	OC28 OC29	0·63 0·63	ZTX107 ZTX108 *	0-15 0-15
AA129	0-20	BD123 BD124	0-83	GET882 GET885	0-25 0-20	OC30	0-40	ZTX 300	0-13
AAZ12 AAZ13	0-30 0-13	BDYII	1.63	GEX44	0.08	OC35 OC36	0-50 0-68	ZTX 304 ZTX 500	0-28 0-15
AC107	0.13	BF115 BF117	0-25 0-50	GEX 45/1 GEX 941	0-08 0-15	0C41	0.25	ZTX503	0.20
AC126	0-25	BF167	0.25	GJ3M	0-25	OC42	0.80	ZTX 531	0-80
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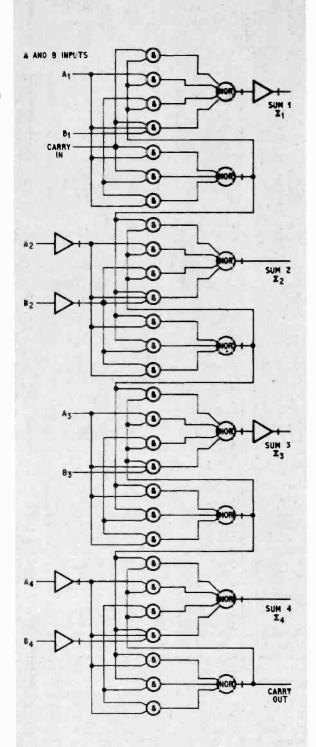


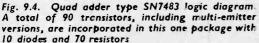
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package such as this could come in handy for all sorts of uses, apart from computer arithmetic.

Counters of a most useful type can be built using this package in conjunction with a shift register. Counting is, after all, just the repeated addition of one to the contents of a store. Counting down requires the subtraction of one; both operations are made simple with these adders.

If the carry input is grounded, and two changing words applied to the A and B inputs, the four sum outputs will only go to a 1 when the two input words are exactly opposite, or complementary. By feeding the sum outputs to a 4-input NAND gate, a four bit nonequivalence gate emerges using only one and a half

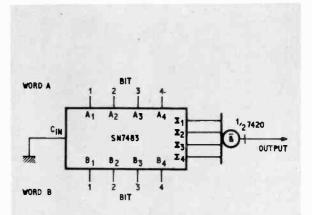


Fig. 9.5. Using the SN7483 as a non-equivalence array. By using inverted data for one of the words, this array will detect equivalence instead. The output goes low only when the two input words are exactly complementary

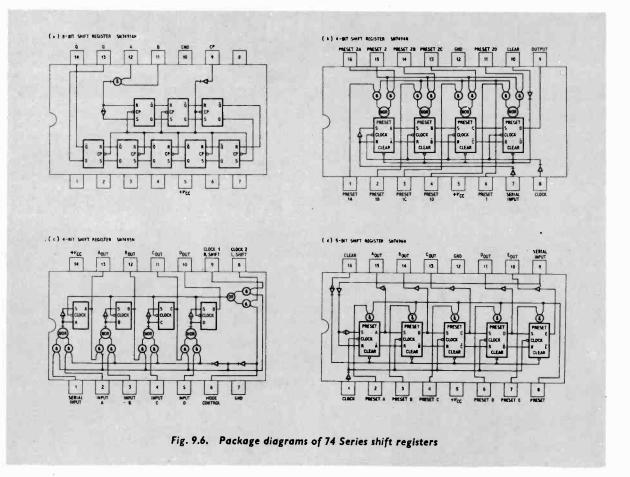
packages, a useful device indeed which can be better appreciated by looking at Fig. 9.5.

The other adders in the series are the 7480 single-bit and the 7482 double-bit devices, both of which have greater versatility than the 7483 due to the extra pins available on the package.

MSI SHIFT REGISTERS

Several types of shift register are available in this series, and between them they cover almost all the likely applications. All the shift registers use RS master/ slave flip-flops, but because the clock input to these devices is buffered, and therefore inverted, they shift data on the positive edge of the input clock. As all these registers have different applications

As all these registers have different applications and we have already gone over basic principles in the TTL flip-flop section last month. It is only necessary here to have a brief look at them all. The block diagrams and package layouts are shown in Fig. 9.6.



7491 Eight-bit Register

The 7491 is an eight-bit serial register, and information must be both inserted and withdrawn serially, as no individual inputs or outputs are available from the separate flip-flops. As with the other registers the clock input is buffered and therefore represents only one load. Data input gating is provided allowing "input enable" logic to be performed.

7494 Four-bit Register

This register is organised as a dual source parallel to serial converter, data being entered by means of the asynchronous inputs. Two preset enable inputs allow the data to be entered from either of the two sources, through four AND-OR-INVERT gates. The common clock and clear lines are buffered, and a serial input is provided.

7495 Four-bit Register

The 7495 is a versatile register which has both parallel inputs and outputs provided. Parallel entry is synchronous, and is entered through AND-OR-INVERT gates which are controlled by the mode control input. When the mode control input is low, the register will shift data serially, from left to right.

Separate clock inputs are available for the two operational modes, and these are again controlled by the mode control input. By using external gates it is possible to make this register shift in both directions, i.e. right to left or left to right.

7496 Five-bit Register

The 7496 is similar to the 7494 except that asynchronous data can be entered from only one source, but parallel outputs from each flip-flop are available. A preset enable input is provided. As all inputs and outputs are available from each stage parallel/serial, parallel/parallel, serial/parallel and serial/serial operation may be employed.

VERSATILITY

As can be seen, these shift registers leave little to be desired in the way of versatility, and of course by cascading several of them it is possible to build a register of any length which may be required. Apart from their use as storage devices it is also possible to build counters of various kinds, including the Unitary and Johnson types.

We have, in this brief introduction, only scratched the surface of the series 74 MSI, but the examples examined should set many an inventive mind buzzing, and there is really no reason why simple computers should not be designed by amateur constructors, using these devices, almost all of which are now available from advertisers in this magazine.

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TRIAC is the name used to identify the triode a.c. semiconductor bidirectional switch. It is basically two reverse blocking triode thyristors or silicon controlled rectifiers connected in inverse parallel, but with a common control electrode (gate). As the triac is a development of the thyristor, it is logical to describe this first and then compare with the triac to show the advantages and disadvantages of both devices.

REVERSE BLOCKING THYRISTOR

The thyristor is a four-layer semiconductor device which has two stable states, one being the conducting state and the other the non-conducting state. The characteristics are shown in Fig. 1.

In the forward blocking region, i.e. when the anode is positive with respect to the cathode, an increase in the voltage across the device has little or no effect on the leakage current until the forward breakover voltage is reached. Increasing the voltage past this point causes the current through the device to increase rapidly, and the voltage across it to fall to about a volt.

The device is now in the conducting state and will remain in this state providing the anode current is above a certain minimum value known as the holding current. If the current through the device falls below the holding current, the device again reverts to the nonconducting state.

If the voltage across the thyristor is increased in the reverse direction, only a small current flows until the voltage reaches the reverse avalanche region where the anode current increases very rapidly and may destroy the device.

Looking again at Fig. 1, we can see that as the gate current I_g is increased, the breakover voltage is reduced. If the gate current is high enough, the device will act like a rectifier.

Normally the thyristor is used in applications where the voltage across the device is well below the forward breakover voltage and is triggered into the conducting region by increasing the gate current. This method requires only small gate currents to switch large anode currents and is therefore the most useful method of turning the device on.

Once the thyristor goes into the conducting state, the gate has no control, and the device continues to conduct, therefore the gate current may be removed as soon as the device is turned on. This typically takes 20μ s, and so a fast pulse can be used for triggering.

TRIAC

The characteristics of the triac are shown in Fig. 2. From the characteristics it can be seen that the triac

operates like the thyristor, but can breakover into the conducting state for either polarity of applied voltage. The triac, like the thyristor, can be triggered into the conducting state by a gate signal, but unlike the thyristor it can be triggered by a positive or negative gate signal. Thus the triac has four possible modes of operation within first and third quadrants of current/ voltage characteristic:

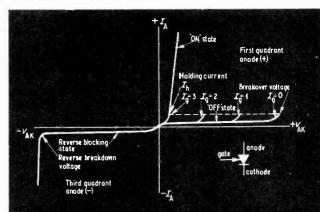


Fig. 1. Voltage current characteristic of a reverse blocking triode thyristor and circuit symbol

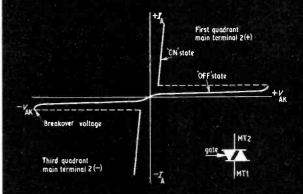


Fig. 2. Voltage current characteristic of a bidirectional triode thyristor or triac and circuit symbol

- I(-) MT2 positive and gate signal negative with respect to MT1
- I(+) MT2 positive and gate signal positive with respect to MT1
- III(-) MT2 negative and gate signal negative with respect to MT1
- III(+) MT2 negative and gate signal positive with respect to MT1

MT1 and MT2 are "main terminals 1 and 2" and used in place of cathode and anode, because the device conducts in either direction.

With no gate signal, the triac blocks in both directions so long as the voltage across it remains below the breakover voltage. If the voltage does exceed the breakover voltage, the triac turns on, and providing the current through it is limited to a safe value, then the device is unharmed, unlike the thyristor which may be damaged by an excessive reverse voltage.

Once in the conducting state, the triac will remain so until the current through the device is reduced to less than the holding current, and only then will the device turn off.

If the voltage applied to a triac is reversed in a very short time, then the triac, instead of turning off as the thyristor would do, merely turns on in the opposite direction. In order to ensure that the triac turns off reliably, it is necessary to reduce the current through it to below the holding current for a period of time before reapplying a voltage. This limits the frequency of operation of the triac to somewhere over the 60Hz mark, but as the main use for the triac is in 50Hz and 60Hz control circuits, this is not a serious limitation.

TRIGGERING

The triac may be triggered into conduction by either d.c., a.c. or pulsed signals applied to the gate. If d.c. is used, the voltage must exceed about 3V, but the power in the gate circuit must be limited.

An example of d.c. triggering is shown in Fig. 3. This type of circuit is useful for switching large currents using a low current switch.

A.C. triggering is perhaps the most useful method to use for a.c. mains power control, because the gate signal is synchronised from the controlled supply. An example of a.c. triggering is shown in Fig. 4.

TRIGGER DIODE

A.C. triggering may also be achieved by using a bidirectional trigger diode (diac), the characteristics of which are shown in Fig. 5.

From these characteristics it can be seen that the device has similar properties to that of the triac, but because the negative resistance portion of the characteristic extends over the whole operating range the device does not latch into the conducting state. A typical breakover voltage for the trigger diode is $\pm 30V$.

An example of a circuit using a trigger diode and triac is given in Fig. 6. More will be said about this type of circuit later.

with a u.j.t. for triggering a

thyristor or triac

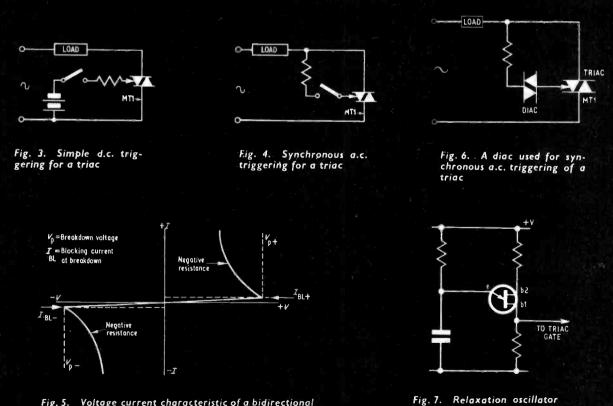


Fig. 5. Voltage current characteristic of a bidirectional trigger diode or diac

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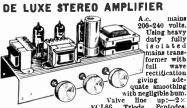
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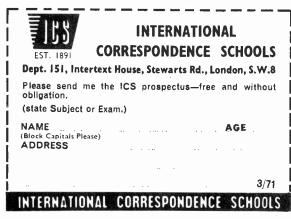
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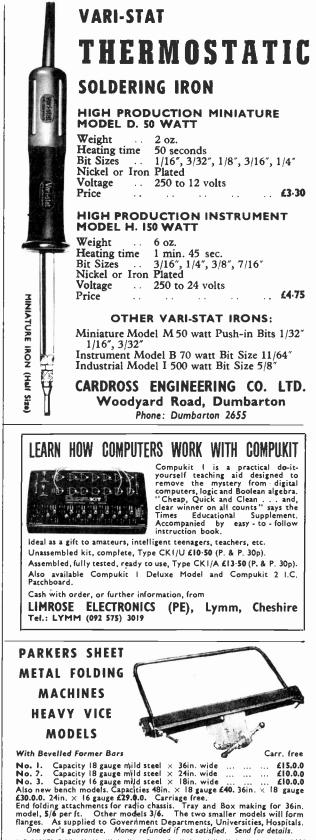
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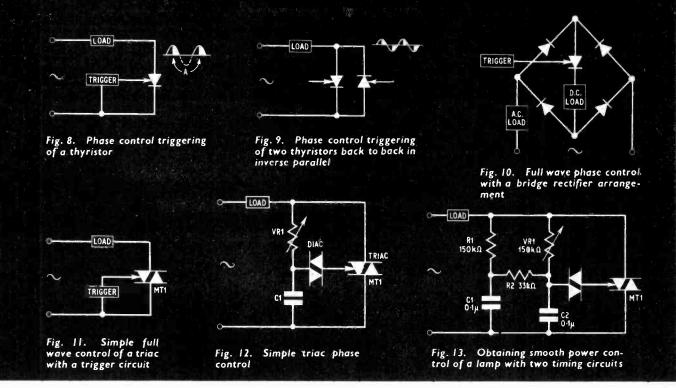
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UNIJUNCTION TRANSISTOR TRIGGERING

The third type of triggering mentioned is pulse triggering and this is sometimes achieved by using a unijunction transistor. The basic u.j.t. relaxation oscillator used for triggering purposes is shown in Fig. 7.

There are many other methods of triggering thyristors and triacs such as pulse transformers and neon lamps, but the last few examples illustrate the main methods of triggering.

The most common applications for the triac is in motor speed control, heater control, or light dimming. By using the triac instead of the thyristor, a consider-

able saving in components may be made.

This coupled with the fact that the triac is less expensive than using two thyristors makes the triac very attractive indeed.

PHASE CONTROL

In the majority of domestic controllers, such as lamp dimmers, phase control is used to vary the brightness. In phase control, current from an a.c. supply is connected to the load for part of each cycle. The length of time during each cycle for which the current is connected to the load, determines the amount of power dissipated in the load. Therefore if the load is a lamp, then the brightness of the lamp may be varied.

Using a thyristor for phase control, as in Fig. 8, we can achieve half-wave control, i.e. only positive halfcycles are controlled, negative ones being blocked by the thyristor. If the thyristor is triggered at point A in Fig. 8, then the white portion of the waveform represents the power supplied to the load. Thus if the triggering point is moved to a point earlier in each half-cycle, then more power will be dissipated in the load, and vice versa.

FULL WAVE CONTROL

If we use two thyristors, as in Fig. 9, then we can achieve full-wave control, one switching the positive half-cycles and the other switching the negative halfcycles. Unfortunately this method requires insulated gate signals for the two thyristors, which is commonly achieved by using pulse transformers in the gate circuits.

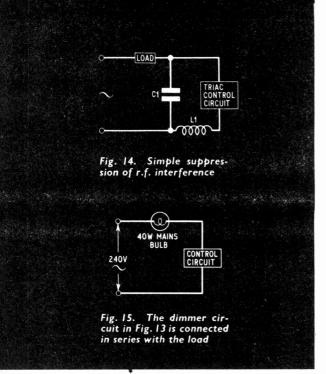
Yet another way of achieving full-wave phase control using a thyristor is illustrated in Fig. 10. This circuit has the great advantage that it may be used for controlling a.c. or d.c. loads, but for purely a.c. control it is an expensive method as it requires four diodes with a high p.i.v., and a current rating equal to that of the load.

By far the most simple and reliable method of fullwave a.c. control is the circuit shown in Fig. 11. This circuit uses a triac as the controlling element and requires only a simple trigger circuit to make it function.

The simplest practical triac phase control circuit is shown in Fig. 12. This circuit is extremely economical as it uses only four components, the function of which are as follows. VR1 and C1 form a phase shift network, the amount of phase shift varying with the setting of VR1.

When the voltage on Cl exceeds the breakover voltage of the diac, it conducts and Cl is partially discharged into the triac gate. The triac is triggered into conduction for the remainder of the half-cycle.

Unfortunately this simple circuit has a limited range of control the load current jumping from zero to some intermediate value as the control is advanced and only then may be controlled smoothly up to full power. This effect may be reduced by using a circuit with a double time constant as shown in Fig. 13, giving very smooth power control.



INTERFERENCE SUPPRESSION

In thyristor and triac control circuits, the load current rises from zero to maximum in a few microseconds. This sharply rising current causes radio frequency interference to be generated, which can cause great annoyance on the a.m. bands. Fig. 14 shows a very simple method of interference suppression.

A small inductor of a few microhenries is used to slow the rate of rise of current, but if used on its own, the interference can still be sufficient to be annoying. The addition of the shunt capacitor C1 further reduces the interference to negligible proportions for domestic applications.

TRIAC LAMP DIMMER

The circuit given in Fig. 13 can form the basis of a triac lamp dimmer which can be fitted behind a wall It is advisable to incorporate the suppression shown in Fig. 14 to reduce interference, starting with component values of 0.1μ F for C1, and adjusting for the best results, with an r.f. choke rated at a minimum of 2A. This choke could be made by winding about 40 turns of thin single core p.v.c. connecting wire on a ferrite ring core or rod.

The triac should be rated at a minimum of 400V p.i.v. 3A for domestic lamp dimming. There are several available that would suit the purpose; the author used a General Electric type SC35D in conjunction with diac type ST2. Some readers may prefer to try a quadrac which incorporates a triac and diac in one encapsulation.

The triac is mounted on a small "L" shaped bracket which is mounted on to a small component board. No difficulty should be experienced in constructing the unit and providing care is taken, the unit is perfectly safe.

The potentiometer may be wired to give full brightness immediately the switch on the potentiometer goes on, and then dim the light as the control is advanced, or to give minimum brightness rising to maximum as the control is advanced. The triac should be rated to withstand initial surge of current which occurs due to the cold filament, when the lamp is first switched on.

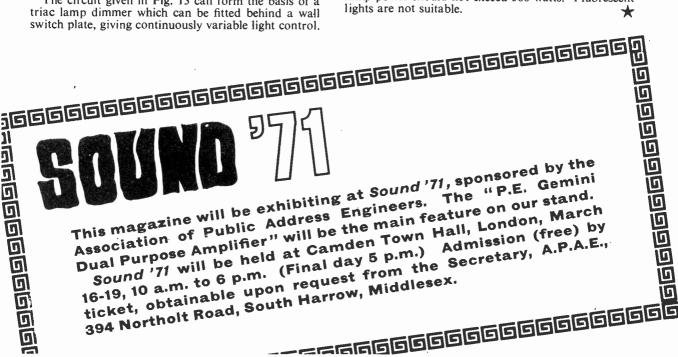
CHECKING AND FITTING

When the circuit has been wired up, the circuit may be tested by wiring it in series with a mains bulb and connecting these across the mains as in Fig. 15. The control should give smooth flicker-free control of the lamp up to full brightness, and the lamp should be extinguished by the switch.

Before fitting the dimmer, it is wise to wrap a piece of heavy polythene around the circuit to ensure that nothing shorts to the metal switch box. It may be found that the switch box is too shallow for the body of the potentiometer. If this is the case then it will be necessary to obtain a deeper box from an electrical shop.

After fitting the unit, the mains should be reconnected and the unit tried out. If everything has been carefully insulated, then no trouble should be encountered.

This dimmer should only be used with incandescent filament lamps rated at 230-250 volts a.c. 50Hz. The lamp power should not exceed 500 watts. Fluorescent lights are not suitable. \star



B -P		PAK
FULLY TESTED AND MARKED 4C107 613 0C170 623 AC126 0.13 0C171 0233 AC127 0.17 0C200 033 AC128 0.13 0C201 0.13 AC176 0.23 2G301 0.13 AC176 0.32 2G301 0.13 AC176 0.32 2N1102.3 0.30 AF186 0.50 2N1302.5 0.30 BC174 BC107 013 2N1306.9 0.33 BC172 BC108 0.13 2N1306.9 0.33 BC174 0.15 Dewer Transistors 50 BSY25 0.57 OC26 0.23 0.23 0.23 BSY26 0.13 OC26 0.23 0.23	CLEARAANCE LINES DON'T MISS THIS LAST CHANCE ONLY A FEW LEFT UHF/VHF T.Y. TUNER UNITS TU.2 CONTAINING 2 AFIBO'S & 2 AFIBO'S PARICE 50p. All the units have many other components. e.g. Capacitors. Resistors, Coils and tuning con- densers, etc. Although these are manufacturers' rejects they are not beyond repair as has been proven by many of our customers. AlL TUNER UNITS ARE SUPPLIED WITH CONNECTION DATA COLOUR T.Y. LINE OUTPUT TRANSFORMERS Designed to give 25kV when used with PL509 and PY500 valves. As removed from colour receivers at the factory. ONLY £I each Dob of PLY.=23p. 400 PLY.=33p. 800 PLY=40p. PAK F.3. Complementary Set. NPN/PNP Germ. Trans.	NEW TESTED AND GUARANTEED PAKS B2 4 Photo Cells, Sun Batteries. 50p B7 2 ADI61-ADI62 NPN/PNP 50p B77 2 ADI61-ADI62 NPN/PNP 50p B77 2 ADI61-ADI62 NPN/PNP 50p B81 10 Reed Switches, mixed types 50p B89 2 SSP5 Light Sensitive Cells, Sop 50p B91 8 NKT163/164 PNP Germ, TO-5 50p B92 4 NPN. Sil. Trans, AC6 ≅ 50p B93 5 GET113 Trans, equiv, to 50p B93 5 GET113 Trans, equiv, to 50p B99 200 Mixed Capacitors. Postage 13p. 50p B99 200 Mixed Capacitors. Postage 13p. 50p B99 10 XEI12 and XB102 equiv, to AC126, AC156, OC81/2, 50p H4 250 Mixed Resistors. Mixed Sop 50p H7 40 Wirewound Resistors. Mixed Sop 50p H7 40 Wirewound Resistors. Mixed
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Exsanguinated

There I lay, exchanging platitudes with this bright young nurse, as 450 odd milligrams of my life-blood trickled into some remote bottle. Would it, I wondered, be converted direct to plasma, or perhaps help to save some drunken driver's neck the following week-end. As I, somewhat mechanically, continued with the conversation my mind entered a reverie of ideas about this rather wonderful stuff that we would all find it so hard to do without.

Blood is supposed to contain a fair quantity of iron, I mused. Could it be magnetic? It is difficult to remember ever having sufficient amounts of it to experiment with and, in any case, not being charged with the motive to become a second "Dracula", had never really given such matters another thought!

Nevertheless, it now occurred to me that if, indeed, blood was magnetic (or perhaps, more likely, magnetically susceptible), the possibilities could be quite awe-inspiring. For example, the earth's magnetic field might have some influence on the flow of blood around our systems, and what about the effect of stray fields from transformers and the like? The effect on the capillary action of the smaller blood vessels could be quite dramatic could'nt it? Surely, I told myself, things were getting out of all proportion.

Not to be deterred, I changed tack slightly away from the gory path, and began entertaining thoughts about the chances of inducing currents in the nervous system through similar agencies. "Do you think", I butted into the, now one-sided, conversation, "that it would be a possibility to influence the brain with magnetic fields?". As you may imagine, the nurse knew little more about what I was talking about than I did, and she replied in a hushed whisper, as though to one demented, "You've nearly given your pint, I 'spect you'll feel better after your tea 'n biscuits".

Putting an optimistic face on the situation and dropping back onto my pillow, I lapsed into day dreaming again. Electric currents can be induced in copper wires, so why shouldn't the same apply to the effects of magnetism on liquids. Subtle influence

If such really is the case this could mean that, quite unbeknown to us, magnetic fields might have some kind of modulating influence upon certain parts of the body and, who knows, perhaps even modify our very thoughts in certain subtle ways!

No, this was too much to accept in one go; the loss of blood must obviously be having its effect I considered, so decided to re-examine the idea later and in the meantime put up with the good-natured ministrations of my N.B.T.S. attendant.

Two months later I was chatting with an old friend of mine, a librarian, about this rather crazy idea of mine and, would you believe..., he referred me to a paper written only a couple of years or so ago about the effect on reaction-time performance by magnetic fields! The paper concerned was pretty lengthy, so only the main import of its discussion will be given here.

Apparently, three individuals of the medical profession, and all from the Syracuse area of New York, have discovered quite a profound relationship between the difference in the time taken to react to the appearance of a light source with and without the influence of a fairly weak (5 to 11 gauss) magnetic field. Initially, the field, which was generated by a couple of 14.5in diameter Helmholtz coils placed near the head, was nonoscillatory and showed no effect.

Later, instead of a d.c. current being used to drive the coils, a low frequency a.c. signal was employed. Immediately, there appeared to be a perceptible change in the rate of response and, indeed, this was confirmed over some four groups of 50 subsequent trials. Every time the field was present a distinct increase in the reaction time occurred.

It is extremely difficult to know just what to make of their findings. One thing though is sure, never will I go out again in a magnetic storm without first donning my lead-lined crash hat!

By any other name

Only a matter of months ago I was nattering about tomatoes showing electrical reactions to the application of heat to their skins! Well it seems they are not the only ones among the vegetable kingdom to "blow their cool" in this way! The latest addition to the "psychosensitive" list is the "veg" which one would have thought held first place; it's the rose,

This time it is the Russians who have un-earthed the effect. It seems that hundreds of experiments have recently been performed at the Moscow Agricultural Academy which reveal that in addition to the rose reacting to tactile (touch) stimuli, it also displays a form of crude memory. According to *Pravda*, the Communist newspaper, the researches show that rose bushes exhibit electrical activity similar to nerve discharges observed in man!

All this has yet to be demonstrated to me; perhaps we shall be hearing a lot more of these findings in the not too distant future though.



So long

Wouldn't it be nice if we could gain access to the methods (whatever they may be) employed in man and other animals for generating huge time-constants? I mean if someone says "See you in an hour and a half", the chances are that, provided they said where, you will see them.

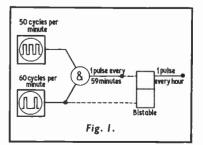
Yes, I agree, we would probably be using our watch, or maybe available clocks; who knows, we may even be relying upon the position of the sun in the sky. Assuming though that none of these methods were available, we would still feel fairly confident that the time period could be judged with a reasonable degree of accuracy. How?

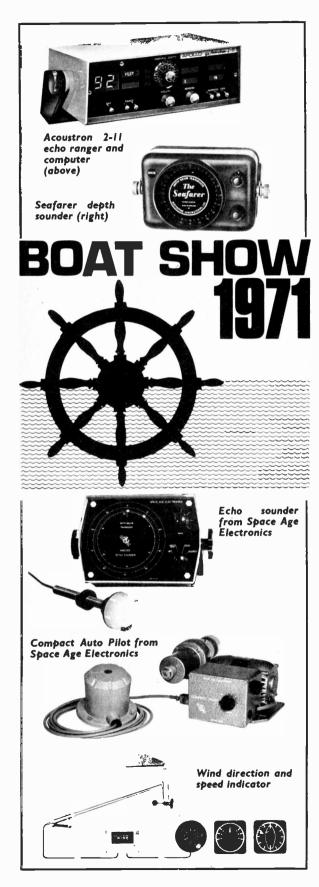
Well, "hunger-pains" aside, no one is by any means certain. It could have an oscillatory principle I am told, and someone has even suggested a pulse coincidence basis.

Actually, in electronic practice, this latter idea works well for generating long time-constants; perhaps you would like to try it. Fig. 1 shows the general arrangement. An AND gate receives the outputs from two astable pulse generators, the frequencies of which are both very low and slightly different; the gate thus only returns an output when the input pulses are coincident.

With the frequencies given, only one pulse should appear at the output of the gate approximately every hour! This can be used to set a bistable or whatever application one may have in mind.

Only one problem exists with this kind of timer... one has to wait such a long time during the setting-up periods to establish that the correct frequencies exist!





T is always interesting to note the developments in marine electronics during the past year at the London International Boat Show. Last year in our Boat Show report we noted that there were more firms displaying electronic gear and a greater range of instruments available; the same trend is repeated this year.

The advantages of solid state electronics in marine equipment were particularly evident from two new equipments, these are: the Acoustron 2-11, forward looking echo ranger and computer by Apollo Electronics Ltd., and a digital readout echo sounder by Marine Electronics Ltd. These instruments use integrated circuits to provide, compact design with clear, unmistakable readout, low power consumption and greater reliability than more conventional designs.

Acoustron 2-11 will no doubt interest almost every owner of power craft of a reasonable size. This computerised sonar uses two narrow transducer beams to probe under and ahead of the boat. The resultant echoes are used by computer circuitry to predict the possibility of grounding and to give visual and audible warning of impending danger. Warning time and depth warning can be selected as can the memory time to suit various coastlines and conditions.

LOW COST RADAR AND SONAR

Low cost is always an attraction when buying equipment, particularly if it is well constructed and has a good specification. This year has seen the first under £500 radar for small boats from Electronic Laboratories (Marine) Ltd.; the radar, called Seascan, is completely housed in two units—the scanner transceiver and the display unit. It has a working range from 25 yards to 16 nautical miles, which is covered in six switched ranges. If this radar is as popular as the Seafarer depth sounder from the same firm, and we think at the price (£450) it will be, both yachtsmen and Electronic Laboratories should be very pleased.

Space Age Electronics Ltd. are marketing what is claimed to be the world's most powerful small boat echo sounder for £35, using neon readout, and an auto pilot costing £99 that is claimed to be the world's cheapest pilot for small yachts and motor cruisers. This company is one to watch for future developments and they have said that they should be showing some interesting new instruments next year. Marine Electronics are marketing a neon echo sounder for £39 with built-in depth warning; they also sell a meter type sounder and the digital readout unit mentioned earlier.

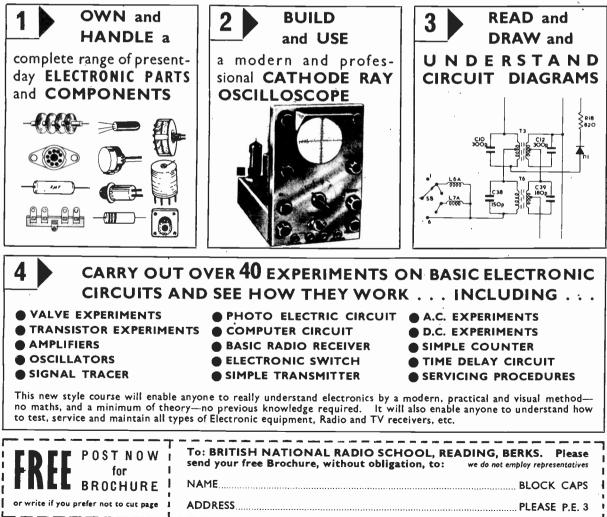
WIND SPEED INDICATOR

New developments in equipment from Brookes and Gatehouse consist of a simplified, lightweight wind direction and speed indicator—Hengist and Horsa model C—although primarily intended for the cruising yachtsman, these models will no doubt appeal to the racing man since they are lighter in weight, more simple to use and the masthead unit will give slightly less windage.

From chatting to various stand holders, it is apparent that most of the firms are engaged in development of various new equipments and some, such as Baron Instruments and Space Age Electronics, are hinting strongly of exciting new projects next year. The added competition from new firms that have launched marine electronic equipment within the last few years, has brought about a fast moving industry that is quality and price conscious and that will have to be up to date to survive.



a new 4-way method of mastering **ELECTRONICS** by doing — and — seeing . . .



G. F. MILWARD

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	le/Retail: 369 Alur	n Rock Road,	Birmingham E	38 3DR. Tel. 02	1-327 2339
WIRE-ENDED TYPES REF. No. G1/11 20/450V G1/13 40/50V G2/5 G2/6 B/12V G3/7 100/15V G3/14 100/180V G5/9 B/8/450V G6/13A H1/1 H/4 H1/4 4/6V H1/4 4/6V	NOTE: IT IS ESSENTI, REF. No. 10p H1/11 8/6V 5p H2/1 32/150V 4p H2/2 64/275V 4p H2/6 42/275V 10p H2/8 32/150V 10p H2/8 32/150V 10p H2/9 A 1/150V 10p H2/9 A 1/150V 10p H2/10 A 16/32/350V 10p H2/10 A 16/32/350V 10p H3/10 A 500/12V 3p H3/0 750/12V 3p H3/10 A 300/0V) 3p H3/12 16/50 REV)	AL THAT REFERENC REF: No. 3p H4/I 20/4/27 5p H4/I3 400/50' 4p H4/I3 400/50' 5p H5/7 30/64' 5p H5/11 400/6-4 5p H5/12 320/10' 8p H6/12 320/10' 8p H6/7 200/14' 8p H6/7	REF. No. No. 5V 8p H7/3 v 10p H7/3 4p H7/4 3p 3p H7/4 10p V 3p H7/4 V 3p H7/5 y 3p H7/6 3p H7/7 4p V 8p H7/7 y 8p H7/7 4p H7/8	20/6 4V 4p H7 25/12V 4p H7 25/12V 8p H7 25/25V 8p H7 25/25V 8p H7 25/25V 8p H7 25/25V 8p H8 50/3V 3p H8 50/12V 8p H8 50/12V 8p H8 50/12V 8p H8	(11 64/25 V 8p (13 75/15 V 8p (14 100/4 V 5p (13 75/15 V 5p (13 3/50 V 5p (13 3/50 V 5p (16 8/50 V 5p (17) 15/15 V 8p (10 2/75 V 5p (11) 250/12 V 8p
CAN TYPES REF. No. G2/1 6,000/30V G2/5 125/200V (REV) G3/4 650/300V G3/4 650/300V G3/10 40/20/10/350V G3/13 2,000/30V G3/14 650/300V G3/15 0,00/200V G3/16 40/20/10/350V G4/16 50/350V G4/6 60/320V/275V	REF. No. 38p G4/7 40/40/275V 25p G4/7A 40/40/450V 3bg G4/11 2.000/25V 38p G4/12 150/30V 30p G4/13 100/200/16/275' 15p G5/1 8.000/70V 10p G5/3 35,000/15V 38p G5/4 39,000/15V 3p G5/4A 500/10V	Bp G 5/7 100/400 13p G 5/7A 45,000 13p G 5/1 12,000/ 13p G 6/1 12,000/ 13p G 6/3A 2,000/1 130p G 6/5A 1,000/1 130p G 6/6 1,000/2 130p G 6/6A 2,001/2	(12V 75p G6/12A) (15V 75p H5/4 (50V 38p G6/14 15V 15p H1/5 (500/25V 38p H1/6 30V 38p H1/12 30V 30p H2/6	60/200/300V 25n H2	/4 1,000/50V 30p /6 2,500/9V 13p /9 100/275V 10p /13 16/16/375V 10p /3 500/12V 8p /9 500/6V 5p /11 78/400/16/275V 38p
TAG ENDS REF. No. G1/4 4/150V G1/5 8/275V G1/5 8/275V G1/7 16/16/275V	REF. No. 2p G1/12 40/450V 5p G2/4 40/300V 8p G2/13 100/50V 10p G4/3A 200/25V	REF, No. 10p G4/5 16/300 8p G4/9 8/8/350 5p G4/10 350/25 8p G6/1A 3,000/1	V 10p G6/7 V 10p G6/12	1,000/50V 30p H 100/275V 10p H 1,000/12V 10p H 4	V/2 250/25V 8p
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RESISTORS, 4/4 watt assorted Wire-wound I to 3 watt 5 to 7 watt 10 watts Multi-tapped PAPER CONDENSERS TV types Miniature ELECTROLYTIC CONDEJ Suitable for Mains Radio/TV Transistor types Mixed (both types) POLYSTYRENE CONDENSERS MULLARD POLYESTER CONDC SILVER.MICA WIRE.WOUND 3-Watt SLIDERS VOLUME CONTROLS. Assorted NUTS AND BOLTS. Mixel length/type 8 B.A. 6 B.A. 6 B.A. 7 J.A. 8 B.A. 7 J.A. 8 B.A. 8 B.A. 7 J.A. 8 B.A. 8 B.A. 8 B.A. 9 B.A. 8 B.A. 9 J.A. METAL SPEAKER GRILLE 7 T/AL * 3 J;in. EARPIECES, Magnetic No Plug 3.5mm	t 15 50p N.P.N. Untestee 0 50p O.C. 12 50p O.C.71 equivale Light-sensitive E 50 50p (These produce u) 100 50p O.C.44 Mullard 1 0.50p ASY 22. Miseked 100 50p KI 22 Rectifier 100 50p KI 22 Rectifier 100 50p CO-AXIAL CAR 100 50p CRYSTAL TAPP 115 S0P TRANSISTORIS 5 50p TRANSIST	S but mainly but mainly so to Ima from light) st grade 4 500 marked 4 500 marked 4 500 marked 4 500 marked 4 500 marked 4 500 s 4 500 s 4 500 s 4 500 s 4 500 s 4 500 s 5 4 500 s 5 4 500 s 5 500 s 500 s 500 s 500 m 2 500 s 500 m 2 500 s 500	All at 10% discount VEROBOARD 24in × 1in × 0-15in 3in × 24in × 0-15in 3in × 24in × 0-15in 5in × 24in × 0-15in 5in × 24in × 0-15in 5in × 52in × 0-15in For the second second second Cutter-30p. RECORD PLAYER G90 Magnetic Stereo GP 67/2 (Mono. Cry ACOS GP 93/1 (Stere Crystal, Diamond) £1- ACOS GP 93/1 (Stere Crystal, Diamond) £1- ACOS GP 94/1D (Stere Crystal with two L.P./ TRANSISTORISED reverse polarity pro- ctc., £1. Postage/Packing 25p. Postage/Packing 25p.	on list. 6p 5in × 3‡in × 0-15in 16p 17in × 2‡in × 0-15in 20p 17in × 2‡in × 0-15in 20p 17in × 2‡in × 0-15in 20p 3‡in × 2‡in × 0-15in Pin Insert Tool 48p. Ter ack consisting of 5 2‡in × CARTRIDGES. Well be Cartridges. Diamond Nee stal) 75p. ACOS GP 91 io, Crystal, Sapphire) £1.2 63. ACOS GP 94/1 (Ster- reo, Caramic, Diamond) £1 Stereo needles) £1-25. FLUORESCENT LIG stereion. 8 watt type with 13 watt type, batten with THESE CAN BE SENT ON ESTER CONDENSERS 10, 1,800pf, 2,200pf, 15p re 30p per dozen (all 160V wo b.	minal Pins (0 or 0:15) 36 for I in boards and a Spot Face How normal prices! die, 6mV output, £4. ACOS (3 (Compatible, Crystal) £1. 5. ACOS GP 93/1D (Stereo, 88. ACOS GP 95/1 (Stereo, HTS, 12 volt. All with h reflector, suitable for tents patten fitting for caravas £4. Switch. 22in × 2in × 1in £5. I APPROVAL AGAINST FULL ber dozen (all 400V working). rkking). 25% discount for lots 0. 10p per dozen of any one indreds of values from 0.7 ohm age of these are multi-tapped ige variety these can only be
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Correspondents wishing to have a reply must enclose a stamped addressed envelope. We regret we are unable to guarantee a reply on matters not relating to articles published in the magazine. Technical queries cannot be dealt with on the telephone.

Shipwreck

Sir—I recently finished making your game "Operation Seasearch" and 1 am writing to point out a defect in the circuit given for this game in your December 1970 edition. I feel that this should be pointed out to other readers who may be considering building the game. This defect will not usually cause difficulty but it may in certain circumstances as explained below.

This difficulty is as follows. With reference to the enclosed diagram, Fig. 1, it can be seen that if the "Raider" is at say, Aa, and the "Supply Ship" at Ba, current can pass to S5 when it is in position "A" or "B". If S6 is in position "a", current will be passed to S2a and thus to LP1 when S9 is depressed. Thus S5 can be in position "B" and on depressing S9 LP1 will glow showing that the raider has been detected, when in fact it hasn't. This situation can occur in a number of positions.

D. W. Guest, St. Helens, Lancs.

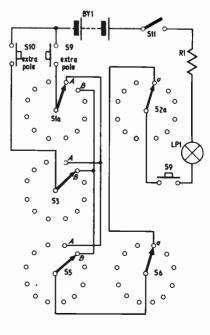


Fig. 1

Mr. Guest is quite right; this is a point that was omitted in the original article. The condition occurs when either searching ship is in line with the "Raider" along one axis and also in line with the "Supply Ship" along the other axis. Overcoming the condition can be done quite simply by inserting a second pole of each push button where indicated. This was not done in the prototype on the grounds of economy, as a second pole was needed in the later "Submarine Game", and three pole push buttons come a bit expensive!

Actually, in the game situation the phenomenon is not so drastic as it might appear. Firstly, the chances of the right conditions arising in any one game move are approximately 70 to 1 against. (Suffice to say that in innumerable games, it has occurred only two or three times.) Secondly, since both players take turns to control the "Raider", the chances against each player are exactly equal.

On the few occasions that the situation has arisen, we have attributed the discovery of the "Raider's" position to an accidental sighting by long-range aircraft, which satisfied our sense of the proprietry of things—it gave the searcher another "fix" on the "Raider's" position just as he has in variations 3 and 6, page 989.—D.R.D.

Economic damper

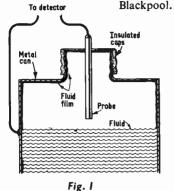
Sir—May I congratulate you on the series of articles currently running on using logic i.c's; they are very useful to me. Also, the "Digital Clock" is a very useful design but, as is very often the case, the difficulty in obtaining parts (Nixie tubes in this case) at the right price, tends to put a damper on one's enthusiasm.

After several enquiries and visits to shops I may be able to satisfy my requirements, given several more weeks. Of course, I know it is possible to get anything if your are prepared to pay top prices, but I begrudge doing this when I know that someone must be selling the equivalent article much cheaper.

Referring to Gerry Brown's brake fluid level detector (On The Fringe, November 1970 issue), I had the same idea myself a few months ago but on trying it out I found that as soon as the fluid was shaken up a thin film of fluid adhered to the insulated cap, thus permanently shorting the probe, see Fig. 1 (below).

Did Mr. Brown have this trouble or was it just a theoretical circuit? John Westmoreland,

Bispham,



Fuzz thump

Sir—Reference to the "Fuzz Circuit" included in *Ingenuity Unlimited*, December 1970 issue. Having constructed this circuit, I found as have probably many of your readers, that it needs quite a considerable clout, on even the lowest guitar string (open E) to set off the trigger circuit, once it is stable, and it has zero response to the top E and B strings at standard tuning.

Modifying the circuit by wiring resistor R1 (1M Ω) directly between the base and collector of TR1 and changing the value of C5 to 10 μ F 10V working should cure the above problems.

> B. K. Cox, Wellingborough, Northants.

- DECIMAL CURRENCY -AND P.E.

Readers throughout the world are probably aware that British currency is being decimalised with effect from February 15, 1971. The following notes are issued for their guidance when writing to Practical Electronics. I. Cheques and postal orders should

I. Cheques and postal orders should show amounts payable in decimal currency. Leaflets are available at all branches of British Banks.

2. Readers' cheques and postal orders written in £s d will not be accepted by the publishers of *Practical Electronics* after February 15, 1971.

3. Handwritten cheques of more than £1 which include new pence, should use a hyphen in place of the decimal point (e.g. £7-80, £30-06).

4. Postage rates in the U.K. on and after February 15 will be $2\frac{1}{2}p$ second class and 3p first class for up to 4 ounces. Old \pounds s d stamps used on and after this date must be at the new rate of 6d second class, 7d first class for up to 4 ounces. Readers requiring a reply to correspondence are asked to use the correct postage rate on s.a.e.

Sinclair Project 60



the world's most advanced high fidelity modules

Sinclair Project 60 presents high fidelity in such a way that it meets every requirement of performance, design, quality and value and now that the remarkable phase lock loop stereo FM tuner is available, it becomes the most versatile of high fidelity systems. With Project 60, it is possible to start with a modest mono record reproducer and expand it to a sophisticated stereophonic radio and, record reproducing system of fantastically good quality to hold its own with any other equipment, no matter how expensive. Project 60 is a unique high fidelity module system where compactness and ease of assembly are combined with

_	System	The Units to use	together with	Cost of Units
Ą	Simple battery record player	Z.30	Crystal P.U., 12V battery volume control	89/6 (£4.47 ¹ / ₂)
В	Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control etc.	£9.9.0 (£9.45)
С	20+20W. R.M.S. stereo amplifier for most needs	2 x Z.30s, Stereo 60, PZ.5	Crystal, ceramic or mag. P.U., most dynamic speakers, F.M. tuner etc.	£23.18.0 (£23.90)
D	20+20 W. R.M.S. stereo amplifier with high performance spkrs.	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.18.0 (£26.90)
E	40+40 W. R.M.S. de- luxe stereo amplifier	2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As for D	£32.17.6 (£32.87 ¹ / ₂)
F	Outdoor P.A. system	Z.50	Mic., up to 4 P.A. speakers controls, etc.	£5.9.6 (£5.47½)
G	Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£17.8.6 (£17.42 ¹ / ₂)
Н	High pass and low pass filters	A.F.U.	C, D or E	£5.19.6 (£5.973)
J	Radio	Stereo F.M. Tuner	C, D or E	£25.0.0

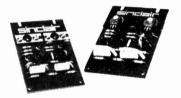
circuitry that is far in advance of any other manufacturer in the world. Thus it is extraordinarily easy to assemble any combination of modules using nothing more complicated than the simplest of tools, and you certainly do not have to be experienced to build with complete confidence. The 48 page manual free with Project 60 equipment makes everything easy and you can house your assembly in an existing cabinet, motor plinth, free standing cabinet or virtually any arrangement you wish. Once you have completed your assembly you will have superlatively good equipment to give you years of service and enjoyment. You will have obtained superb value for money because Project 60 is the best selling modular system in Europe and can therefore be produced at extremely competitive prices and with excellent quality control.

Sinclair Radionics Ltd., London Road, St. Ives, Huntingdonshire PE17 4HJ. Tel. St. Ives (048.06) 4311



Sinclair Project 60

Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 rance equally welt

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications). Power Outputs

Power Outputs 2.30 15 watts R.M.S into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts. 2.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 6 ohms, using 50 volts Frequency response: 30 to 300,000 Hz±1dB Signal to noise ratio: better than 70dB uneighted. Input sensitivity: 250mV into 100 Kohms. For speakers from 3 to 15 ohms impedance. Size 3½ x 2¼ x ½ in. Z.30 Built, tested and guaranteed with circuits and instructions manual **89/6** ($f \Delta \Delta 7 \pm$) 89/6 (£4.47¹/₂) Z 50

Built, tested and guaranteed with circuits and instructions manual **109/6** (f5 471) 109/6 (£5.47¹/₂)

Power Supply Units



Designed specially for use with the Project 60 system of your choice.

Illustration shows PZ 5 to left and PZ.8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stablised supply is essential.

PZ-5 30 volts unstabilised £4.19.6 (£4.97¹/₂) PZ-6 35 volts stabilised £7.19.6 (£7.97¹/₂) PZ-8 45 volts stabilised (less mains transformer) £5.19.6 (£5.973) PZ-8 mains transformer £5.19.6 (£5.971)

Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever Unce and without any cost to you whatsbeer provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail, Air-mailcharged at cost

Stereo 60 pre-amp/control unit



Designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS

Input sensitivities: Radio-up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A. curve ± 1dB:20 to 25,000 Hz. Ceramic p.u.-up to 3mV: Aux-up to 3mV. Output: 250mV Signal-to-noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE + 15 to -15dB at 10KHz. BASS + 15 to-15dB at 100Hz. Front panel: brushed aluminum with black knobs. and controls. Size: 81 x 13 x 4 ins. Built, tested **£9.19.6** (£9.97¹/₂) and guaranteed **Active Filter Unit** . + e Surcion In For use between Stereo 60 unit and two Z.30s

or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U, is suitable for use with any other amplifier system. Two stages of filtering are incorporated rumble (high pass) and scratch (low pass). Supply voltage - 15 to 35V. Current - 3mA. H.F. cut-off (-3dB) variable from 28k Hz to 5kHz. L.F cut-off (-3dB) variable from 25Hz to 100Hz, Distortion at 1kHz (35V, supply) 0.02% at rated output. Built, tested

£5.19.6 (£5.973) and guaranteed

Stereo FM Tuner



first in the world to use the phase lock loop principle

Before production of this tuner, the phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio over other systems. Now, for the first time, the principle has been applied to an FM tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Sensitivity is such that good reception becomes possible in difficult areas. Foreign stations can be tuned in suitable conditions and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

SPECIFICATIONS:

Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz. Capture ratio: 1.5dB Sensitivity: 2µV for 30dB quieting: 7µV for full limiting. Squelch level: 20µV. A.F.C. range: ±200 KHz Signal to noise ratio: >65dB Audio frequency response: 10Hz-15KHz (±1dB) Total harmonic distortion: 0.15% for 30% modulation Stereo decoder operating level: 2µV Pilot tone suppression : 30dB Crosstalk: 40dB I.F. frequency: 10.7 MHz Output voltage: 2 x 150mV R.M.S Aerial Impedance: 75 Ohms Indicators : Mains on: Stereo on; tuning indicator Operating voltage: 25-30 VDC Size: 3.6 x 1.6 x 8.15 inches: 91.5 x 40 x 207 mm Squerch and and deserved Phase Desector LF Ame Stereo T A G C Amptehar detector Vortage controlled Price: £25 built and tested. Post free

To: SINCLAIR RADIONICS LTD LONDON	ROAD ST. IVES HUNTINGDONSHIRE PE17 4HJ
Please send	Name
	Address
for which I enclose cash/cheque/money order	. PE371

Sinclair IC10/Q16/Micromatic 016



The world's most advanced high fidelity amplifier

This is the world's first monolithic integrated circuit high fidelity power amplifier and preamplifier. The circuit itself is a chip of silicon only a twentieth of an inch square by one hundredth of an inch thick, having 5 watts RMS output (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 zener diode and 18 resistors, and is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is more rugged and has considerable performance advantages, including complete freedom from thermal runaway and a very low level of distortion. The IC10 is primarily intended as a full performance high fidelity power and preamplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. It may also be used in other applications including car radios, electronic organs, servo amplifiers (it is dc coupled throughout) etc.

Circuit Description

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. There is generous negative feedback round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

Each IC10 is sold with a comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include oscillators, etc. The pre-amp section can be used as an RF or IF, amplifier without any additional transistors.

Specifications:

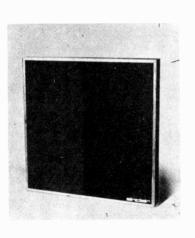
Output: 10 watts peak, 5 watts RMS continuous. Frequency response : 5Hz to 100kHz 1 ± dB. Total harmonic distortion : Less than 1% at full output Load impedance: 3 to 15 ohms

Power gain: 110 dB (100,000,000,000 times) total

Supply voltage: 8 to 18 volts. (A Sinclair power unit, PZ.7 is available for mains operation). Size : 1 x 0.4 x 0.2 in. plus heat sink and tags.

Sensitivity 5 mV. input impedance: Adjustable externally up to

5 Mohms Price (with manual): 59/6 (£2 971) post free.



High fidelity loudspeaker

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies.

elegantly designed shelf mounting speaker brings genuine high fidelity within reach of every music lover.

Specifications:

Construction: Special sealed seamless sound or pressure chamber with internal baffle. Loading : up to 14 watts TMS. Input impedance: 8 ohms. Frequency response: From 60 to 16,000 Hz. confirmed by independently plotted B and K curve. Driver unit: Special high compliance unit having massive teramic magnet of 11,000 gauss, aluminium speech coil and a special cone suspension for excellent transient response. Size and styling: 9# in square on face x 4# in. deep with neat pedestal base. Black all-over cellular foam front with natural solid teak surround. Price £8.19.6. (£8.971).





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Specifications: Size: 36 x 33 x 13 mm (14/5 x 13/10 x 1/2 in.) Weight: including batteries, 28.4 gm (1 oz.).

Case: Black plastic with anodised aluminium front panel and spun aluminium dial.

Tuning: medium wave band with bandspread at higher frequencies, (550 to 1,600 Hz).

Earpiece: Magnetic type. On/off switching: By inserting and withdrawing

Rit in pack with earpiece, case, instructions and solder 49/6 (£2.471).

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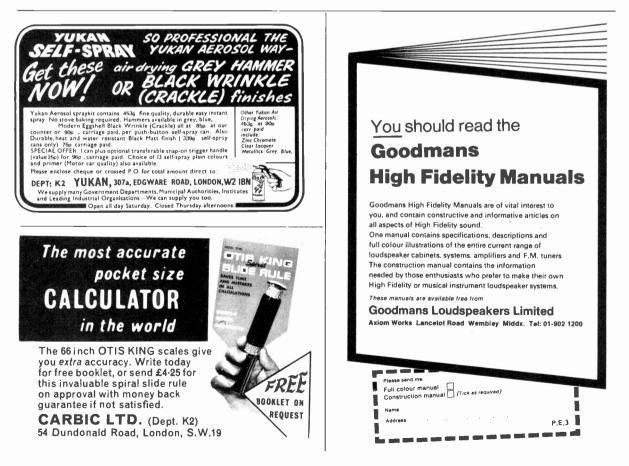


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21310 32p BDT12 50p CA395 7 SC45A 100 10A 2135 2110 2100 90p CA301 115 CA3045 21.25 2N3803 60p BD121 65p OA200 7p SC45B 200 10A £135 £110 £100 90p CA3021 £1.35 CA3045 £1.25 2N4805 17p BD123 80p OA202 10p SC45D 400 10A £135 £1.10 £1.00 CA3023 £1.25 CA3046 £3.25 2N4605 15p BD124 63.2p OC16 30p SC508 200 15A £1.35 £1.30 £1.30 £1.30 CA3028 £1.20 CA3028 £1.35 £1.30 £1.35 £1.30 CA3028 £1.35 £1.45 £1.35 £1.30 £1.35 £1.30 CA3028 £1.35 £1.30 CA3028 £1.30 CA3028A £1.30 CA3028A £1.30 CA3028A £	1 amp Plastic 500 + 8p 25 + 17p 1000 + 6p BCI13 25p OCP71 97p
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N 1131 N 1132 N 1302	25p 2N3855 25p 2N3855A 171p 2N3856	80p AC127	25p BD123 20p BD124	821p BSY51 60p BSY52 971p BSY53	32]p NKT6771 32]p NKT713 37]p NKT781	201	AA119 10p BAX16 12;p	BYZ13 25p 0A202 10
N 1303 N 1304	171p 2N3856A 221p 2N3858	850 AC134 250 AC176	25p BD132 891n BDY10	971p B8Y54 £1-371 B8Y56	40p NKT1041 90p NKT1043	19 301 39 3711	AAZI3 10p BAY31 7p AAZI5 12p BAY38 12p	F8T3/4 22.p OA5 17.p OA9 10p
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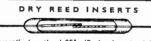
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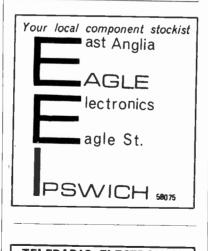
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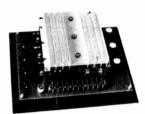


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