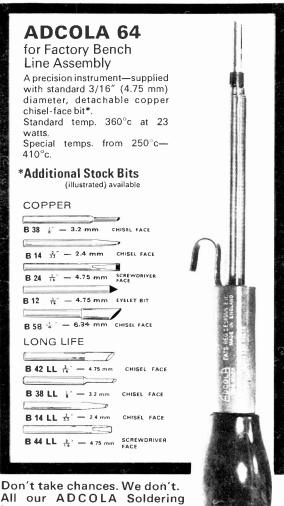
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Decibels: -- 10 to +65 in 7

Response: $\pm 1dB$, 30Hz to 3MHz; $\pm 3dE$, 30Hz to 5MHz; with optional H.F. Probe, to $250\,MHz$.

Accuracy: ±5% of full scale reading.

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 Aerial: unbalanced 300-ohm i-sput

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 Range: 8·*3 to 10N·5MHz

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 IF Bandwidth: 300kHz

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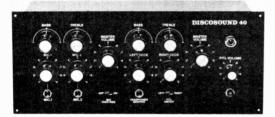
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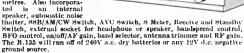
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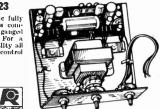
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Mounted on a heavy gauge chassis the fully transistorised R.123 stereo amplifier is completely self-contained even down to ganged volume and separate tone controls. For a simple stereo amplifier of excellent quality all you have to provide is the cabinet and control knobs.

knobs.

SPECIFICATION:
Output: 5W total. 2-5W per channel.
Input sensitivity: 600mV at 2-2Mohnis.
AC 240V operation.

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5 WATT 8 TRACK CARTRIDGE STEREO AMPLIFIER

Model R.133

Just slot in one of the many 8 track cartridge tapea available for a continuous programme of your favourite music. A manual programme override switch enables you to switch from one track to the next at the push of a button at the same time a numbered indicator lights up to show which track is playing. Beautifully finished in an oiled wainut cabinet the R.133 is mechanically engineered to provide long and reliable service. SPECIFICATION—Tape speed: 9-5 cm/sec (3½ 1.p.s.). Wow & flutter: better than 0-3%. Frequency range: 40-12,000Hz. Cross talk: better than 4bdB at 1,000Hz. Output: 5W total. 2-5W per channel. Annulfifer outputs: 290my.

channel. Amplifier outputs: 200mV



Model R.133



£36.0.0 PRICE

40 WATT STEREO AMPLIFIER





Looking as good as it sounds the R.131 stereo amplifier offers excellent quality and value for money. Housed in a handsome wooden cabinet this new Roc Amplifier uses the latest solid state circuit techniques to give a specification second to none at the

specification second to none at the price.

SPECIFICATION—Output: 40W total 20W per channel. Frequency Range: 20-35000 Hz. Inputs: Phone: Mag, 3.6nV R.I.A.A.: Xtal, 100mV; tape, 200mV; tuner, 200mV: control: Bass, treble, volume left, volume right, selector main/remote speakers, power on/off, loudness and stereo/mone.



AM/FM/MPX STEREO TUNER Model R.132

Matching the R.131 amplifier in both styling and performance the R.132 tamer covers. AM and FM including stereo multiplex channels. A separate meter indicates signal strength and tuning on both AM and FM Bands. A usable FM sensitivity of 3µV means that the R.132 can be used anywhere, even in different stereo reception areas.

SPECIFICATION: FM: frequency range: 87-108MHz. Usable sensitivity: 34µV for 204B quieting. Stereo separation: 304B at 1KHz. Image rejection: 604B. AM: frequency range: 525-1005Hz. Useable sensitivity: 250µV.

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10 WATT TRANSISTOR STEREO **AMPLIFIER** Model R.137 With severate tone and volume controls



on each channel and inputs for both phono and tuner, this 10 transistor amplifier is the ideal start to an excellent budget system. Frequency response 70-20 KHz. Output impedance 8-16 ohm.

Attractively styled with brushed aluminium front panel.



10 WATT BUDGET STEREO ALL TRANSISTOR **AMPLIFIER Model R.136**



Amplifier Model R. 130
Ideal as a second stereo system or for
the newconier to Hi-Fi who wishes to
upgrade existing equipment the R. 136
sounds every bit as good as it looks. As
well as inputs for crystal or ceramic
cartridge the R. 136 has a Stereo Tuner
input which accepts the nutching R. 134
Stereo AM/FM Tuner.

The satin Fishs front panel carries a stereo headphone socket as well as volume, balance, tone (all ganged) spenker, mode and selector controls. Supplied complete with older walnut

SPECIFICATION: Output: 10 watts total. 5 watts per channel. Frequency Range: 35-18,000 Hz. Inputs: Phono and Tuncr.

Frequency Range: 35-18, PRICE £13.0.0

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to none.

Housed in a handsome wainut
cabinet the classical low line styling of the R.124 will grace any home.

SPECIFICATION: FM: Frequency Range: 88-108MHz. Usable
sensitivity: 20µV. Stereo Separation: 25dB at 1kHz, 20dB minimum.
Inage Rejection: 55dB. AM: Frequency Range: 535-109MHz. Usable
Sensitivity: 30µV. Audio Section: Total Output Power: 4W. Phono
Input: 200mV at 1M Q. Tape Input: 100mV at 100K Q. ne. ed in

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Peatures 24 measurement ranges with mirror scale. Large 3 x 2 in with mirror scale. Large 3 x 2 in more resistors are strongly constructions. SPECIFICATION

OCV: 0-0-6-6-30-120-600-1.200V at 20K/OPV

SPECIFICATION

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5≩in.	Double play, 1800ft.		7in.	Double play, 2400ft.	
	Mylar	113p		Mylar	125p
5}in.	Long play 1200ft. Ace-		7in.	Long play 1800ft.	
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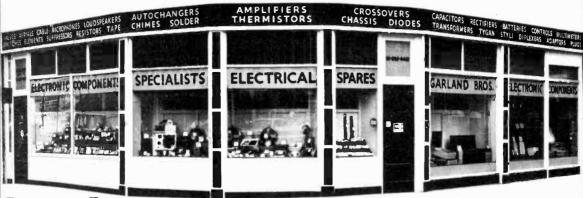
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Size

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NEW TUBULAR ELECTROLYTICS NEW TUBULAR ELECTROLYTICS | CAN TYPES | 2/350V | 2/9 | 100/25V | 2/- | 16 + 18/500V | 1, - 4/350V | 2.9 | 250/25V | 2/- | 16 + 18/500V | 1, - 4/350V | 2.9 | 500/25V | 2/- | 60 + 100/350V | 1/- | 16/450V | 2.9 | 500/25V | 4/- | 60 + 100/350V | 1/- | 16/450V | 3.7 | 32 + 32/250V | 3/7 | 32/450V | 4/- | 8 + 16/450V | 3/- | 32 + 32/450V | 6/7 | 50/50V | 2/- | 32 + 32/350V | 5/- | 100 + 50 + 50/350V, 9/7 | 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/2 + 3/

25/25V 2 - 18+19/450V 5: | 32:-32/350V 8.7
50/50V 2: | 32+32/350V 5: | 100+50+50/350v, 9.7
SUB-MIN. ELECTROLYTICS 1. 2. 4. 5. 8. 18. 25. 30. 50. 100,
200 mP 15V 2: | 500. 1000 mF 19V 3:7; 2000 mP 25V 7:CERAMIC. 1pF 10 0 01mF 94. Silver Mica 2 to 500 pF, 94.
APPER 350V-0-194. 0 5 2'6; 1mF 3/-; 2mF 150V-6
1,000V-0 001. 0 00 22, 0 0047, 0 01. 0 02, 1/6; 0 047 5/1,000V-0 001. 0 00 22, 0 0047, 0 01. 0 02, 1/6; 0 047 5/1,000V-0 001. 0 00 22, 0 0047, 0 01. 0 02, 1/6; 0 047 5/1,000V-0 001. 0 00 22, 0 0047, 0 01. 0 02, 1/6; 0 047 5/1,000V-0 001. 0 00 22, 0 0047, 0 01. 0 02, 1/6; 0 047 5/1,000V-0 001. 0 00 22, 0 0047, 0 01. 0 02, 1/6; 0 047 5/1,000F 2/-; 2,700-5,800pF 4/-5,800pF 2/-; 2-500pF 1/-; 500pF 1/-; 500pF

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Complete: a die, a punch, an Allen screw and key in. 16/7 in. 17/7 1in. 19/7 1in. 24/2 2 in. 16/3 in. 16/1 1in. 19/7 1in. 29/2 1in. 29/2 2 in. 5/3 in. 16/9 1 is. 19/7 12in. 21/7 2in. 39/9 1in. sq. 36.7

AM — FM/VHF TUNING GANG



Super quality small size 11x11x14in. plus spindle $1! \times lin$. 365 + 365 pFwith 25+25 pF. British made, Geared slow motion drive 6:1. Plastic dust cover. 6BA tapped front flxing.

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E.M.I. $13\frac{1}{2} \times 8$ in. LOUDSPEAKERS

With flared tweeter cone and ceramic magnet, 10 watts, Bass res. 45-60 cps. Flux 10,000 ganss. 45/-45/-State 3 or 8 or 15 ohm. Post 3/- each Also with twin tweeters. With crossover, 10 watt. State 3 or 8 or 15 ohm. Post 3/- each

Recommended Teak Cabinet Size 16 × 10 × 9in, Post 5

MINI-MODULE LOUDSPEAKER KIT

10 WATT 65/- CARRIAGES-

Triple speaker system combining on ready cut baffle. in chipboard 15 in. / 81 in. Separate Bass, Middle and Treble loudspeakers and crossover condenser. The heavy duty 5 in. Bass Wooler unit has a low resonance cone. The Mid-Range unit is specially designed to add drive to the middle register and the tweeter recreates the top end of the musical spectrum. Total response 20-15,000 cps. Full instructions for 3 or 8 ohm.

TEAK VENEREED BOOKSHELF ENCLOSURE. 18: 10.4 9 in Modern Scandinavia. 16:: 10 × 9 in. Modern Scandinavian fluted front design for Mini-Module. £5 Post 5/-

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BAKER 12in MAJOR £9



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30-14,500 c.p.s., 12in double cone, woofer and tweeter cone together with a BAKER ceramic magnet assembly having a flux density of 14,000 gauss and a total flux of 145,000 Maxwells. Bass resonance 40 c.p.s. Rated 20 watts. State 3 or 8 or tweeter 20 watts. State 3 or 15 ohm. Post Free.

Module kit, 30-17,000 c.p.s. with baffle tweeter, and £11.10.0 instructions.

BAKER "GROUP SOUND" SPEAKERS 8 or 15 ohm. Group 50 Group 25 Group 35 12 inch £7 12 inch £9 15 inch £19

LOUDSPEAKER CABINET WADDING 18in wide, 3'- it

TWO-WAY CROSSOVER NETWORK 3,000 c/s With variable tweeter attenuator giving accurate high, low frequency balance. Mounted on panel 5 in. 4in. with control knob, tweeter and woofer leads and input 38/-terminals. Suitable for 3 to 8 ohm impedance. Post 2...

Horn Tweeters 2-18kc.s. 10W 8 ohm or 15 ohm 30,De Luxe Horn Tweeters 2-18 Kc.s. 15W, 8 ohm 60:ELAC Moving Coil De Luxe Cone Tweeters 3 or 15 ohm 35;TWO-WAY 3000 c.p.s. CROSSOVERS 3 or 8 or 15 ohm 35;SPECIAL OFFER! 80 ohm. 21in. 21in. dia.; 35 ohm. 3 in.
25 ohm. 3in. dia.; 6 din; 8 5in.

18 - EACH
15 ohm, 3jin. dia.; 7 din; 8 5in.
18 - EXCH
15 ohm, 3jin. dia.; 7 din; 8 5in.
18 - EXCH
15 ohm, 3jin. dia.; 7 din; 8 5in.
18 - EXCH
15 ohm, 3jin. dia.; 7 din; 8 5in.
2 cin. 3 ohm. 3 ohm.
15 ohm. 3 ohm.
15 ohm. 3 ohm.
16 ohm.
17 din.
18 cin. 3 ohm.
18 cin. 25 cin.
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Portable minip As, system, Many uses — ideal for Parties, or as a Baby Alarm, Intercom, Telephone or Record Player Amplifer, etc. Attractive rexine covered cabinet, size 12 9 4 in., with powerful 7 4 in. speaker and four transistor one watt power amplifer. Uses PP9 battery, Brand new with famous makers' guarantee. 75/-Post 5;— Ö ď

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BARGAIN AM TUNER. Medium Wave. Transistor Superhet. Ferrite aerial. 9 volt.

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Printed Circuit. Calibrated slide dial tuning. £10
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FM STEREO MULTIPLEX ADAPTOR for above or general use. Ready made with 4 transistors, 6 diodes £10

BARGAIN 3 WATT AMPLIFIER. 4 Transistor £3.10
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COAXIAL PLUG 1.3, PANEL SOCKETS 1.3. LINE 3 7
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Chrome Lead Socket 7.7, Phono Plurs 1.—Phono Socket 1,7
JACK PLUGS Std. Chrome 3.—; 35 mm Chrome 2,9. DIN
SOCKETS Chassis 3-pin 1.7; 5-pin 2.— DIN SOCKETS
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VALVE HOLDERS, 1.—; CERAMIC 1/7; CANS 1/-.



E.M.I. TAPE MOTORS. 120v. or 240v. AC. 1,200 r.p.m. 4 pole 135mA. Spindle 0.187 v 0.75in. Size 31 × 25/-21 × 21in. (illustrated). Post 3/-. BALFOUR GRAM. MOTORS. 120v. or 240v. AC. 1,200 r.p.m. 4 pole 50mA. Spindle 1 × 3/20. Size 17/-21×24×11in. Post 3/-.

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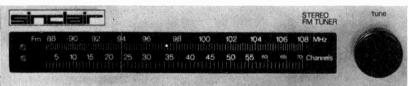
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Project 60







the world's most advanced high fidelity modules,

With the introduction of an entirely new and original high fidelity stereo F.M. tuner, the Project 60 range can be said at this stage to be complete. It offers the constructor a most attractive choice of modular arrangements whereby a high fidelity system can be selected to suit the user's personal requirements. Equally, it is possible to use any Project 60 modules separately or partially grouped and so benefit greatly from the flexibility in use these modules afford. The chart below shows some of the most popular applications for constructors to assemble. The Project 60 manual (free with the modules) suggests others as well and its 48 pages are packed with valuable information. The new tuner, for example can be used with any good high fidelity system as well as Project 60.

Project 60 now falls into four interdependent groups: – 1. The Z.30 and Z.50 amplifiers which have only 0.02% distortion at all output levels and are useful in a wide variety of other applications. 2. The control units comprising the Stereo 60 preamp and control unit and the Active Filter Unit (A.F.U.) with which both high pass and low pass filtering can be introduced between control unit and power amplifiers. 3. The Stereo F.M. tuner as described opposite; and 4. The power supply units PZ.5.

PZ.6 and PZ.8. For most requirements when using Z.30 power amplifiers, the PZ.5 will be perfectly adequate; if low efficiency (high quality) loud speakers are used, the PZ.6 stabilised power supply unit will be used. The PZ.8 will be needed with Z.50s which can be used for any Project 60 system.

Project 60 modules incorporate some of the most advanced circuitry in the world to achieve unsurpassed standards of high fidelity and modern manufacturing techniques enable these modules to be sold at exceptionally attractive prices. Assembling the modules requires no skill or previous experience since the manual supplied with the modules explains clearly how everything can be done with nothing more than the simplest of domestic tools.

Project 60 manuals

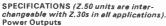
How to assemble and use Project 60 modules to best advantage in the above and other applications will be found in the fully descriptive Project 60 manual included with Project 60 systems. This 48 page manual is available separately, price 2/6d including postage.

	System	The Units to use	In conjunction with	Cost of Units	+ Project 60 tuner
А	Car Radio	Z.30	Existing carradio, Sinclair Micromatic	89/6	
В	Simple battery powered record player	Z.30	Crystal pick-up, 12V or more battery supply and volume control	89/6	
С	Mains powered record player	Z.30 and PZ.5	Crystal or ceramic P.U. Volume control etc.	£9.9.0	£34.9.0
D	20+20 watts R.M.S. stereo amplifier for most needs	Two Z.30s, Stereo 60 and PZ.5	Crystal, ceramic or magnetic P.U., most dynamic speakers, F.M. tuner etc.	£23.18.0	£48.18.0
E	20+20 watts R.M.S. stereo amplifier for use with low efficiency (high performance) speakers	Two Z.30s, Stereo 60 and PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc All dynamic speakers	£26.18.0	£51.18.9
F	40+40 watts R.M.S. de-luxe stereo amplifier	Two Z.50s, Stereo 60 PZ.8 and mains transformer	As for E	£32.17.6	£57.17.6
G	Outdoor public address system	Z.50	Microphone, up to 4 P.A. speakers, 12V car battery with converter, or 45V d.c., controls	£5.9.6	
Н	Indoor P.A.	One Z.50, PZ.8 and mains transformer	Microphone, guitar, heavy duty speakers etc., controls	£17.8.6.	
J	High pass and low pass filters	A.F.U.	D, E or F as above	£5.19.6	



Sinclair Radionics Limited, London Road, St. Ives, Huntingdonshire Telephone: St. Ives (04806) 4311 Z.30 & Z.50 power amplifiers

The Z.30 together with the Z.50 are both of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use the Z.30 or Z.50 power amplifiers in your Project 60 system will depend on personal preference, but they are the same physical size and may be used with other units in the Project 60 range equally well. For operating from mains, for the Z.30 use PZ.5 for most domestic requirements, or PZ.6 if you have very low efficiency lcudspeakers. For Z.50, use the PZ.8 described below.



Z.30 15 watts R.M.S. into 8 ohms, using 35V: 20 watts R.M.S. into 3 ohms using 30 volts.
Z.50 40 watts R.M.S. into 3 ohms from 40 volts: 30 watts R.M.S. into 8 ohms, using 50 volts. Frequency response 30 to 300,000 Hz± 1 dB

Distortion 0.02% into 8 ohms Signal to noise ratio better than 70 dB unweighted Input sensitivity 250mV into 100 Kohms For speakers from 3 to 15 ohms impedance Size 31 x 21 x 1 ins.



Z.30 Built. tested and guaranteed with circuits and instructions manual 89/6

Built, tested and guaranteed with circuits and instructions manual 109/6

Stereo 60 pre amp/control unit

Designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout. achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS

- Input sensitivities Radio up to 3mV, Mag. p.u. –
 3mV: correct to R.I.A.A. curve ± 1dB: 20 to 25,000 Hz. Ceramic p.u. – up to 3mV : Aux. – up to 3mV.

 Output – 250mV.
- Signal-to-noise ratio better than 70dB.
- Channel matching within 1dB.
 Tone controls TREBLE +15 to —15dB at 10kHz: BASS +15 to —15dB at 100Hz.

- Front panel brushed aluminium with black knobs
- a Size 81 x 11 x 4 ins

Built, tested and guaranteed

£9.19.6



variable from 28kHz to 5kHz, L.F cut-off (-3dB) variable from 25Hz to 100Hz. Filter slope, both sections 12dB per octave. Distortion at 1kHz (35V supply) 0.02% at rated output

Built, tested and guaranteed

£5.19.6

Active Filter Unit

For use between Stereo 60 unit and two Z.30s or Z.50s, the Active Filter Unit matches the Stereo 60 in styling and is as easily mounted. It is unique in that styling and is as easily mounted, it is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The Sinclair A.F.U. is suitable also for use with any other amplifier system.

Two stages of filtering are incorporated rumble (high pass) and scratch (low pass). Supply voltage – 15 to 35V. Current – 3mA. H.F. cut-off (–3dB)

Power Supply Units

The units below are designed specially for use with the Project 60 system of your choice.

Illustration shows PZ.5 power supply unit to left and PZ.8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stabilised supply is essential.

PZ-530 volts unstabilised £4.19.6 PZ-635 volts stabilised £7.19.6 PZ-8 45 volts stabilised (less mains transformers) £5.19.6 PZ-8 mains transformer £5.19.6



GUARANTEE If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail, Air-mail charged at cost.



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Stereo FM tuner



first in the world to use the phase lock loop principle

Before production of this tuner, the phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio over other systems. Now, for the first time the principle has been applied to an FM tuner with fantastically good results. By the inclusion of other original features such as varicap diode tuning, printed circuit coils and an I.C. in the specially designed stereo decoder, the tuner has an unsurpassed specification, which also incorporates a squelch circuit for silent tuning between stations, A.F.C. and A.G.C. Sensitivity is such that good reception becomes possible in difficult areas, foreign stations can be tuned in suitable conditions and often a few inches of wire are enough for an aerial. In terms of high fidelity, this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. Although the tuner is intended primarily for use with a Project 60 system, it can be used to advantage with any other high fidelity system. It is easily mounted into any cabinet as shown in the manual supplied with it.

Specifications

Number of transistors 16 plus 20 in I.C. Tuning range 87.5 to 108 MHz Capture ratio 1.5dB Sensitivity 2µV for 30dB quieting 7µV for full limiting Squelch level 20µV A.F.C. range ± 200 KHz Signal to noise ratio > 65dB Audio frequency response 10Hz-15kHz(±1dB)

Total harmonic distortion 0.15% for 30% modulation Stereo decoder operating level 2µV Pilot tone suppression 30dB Cross talk 40dB

I.F. frequency 10,7 MHz Output voltage 2 x 150mV R.M.S. Aerial Impedance 75 Ohms

Indicators Mains on; Stereo on; tuning indicator Operating voltage 25-30 VDC



Price: £25 built and tested. Post free.

Sinclair IC10/Q16/Micromatic

IC₁₀



The world's most advanced high fidelity amplifier

This is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself is a chip of silicon only a twentieth of an inch square by one hundredth of an inch thick, having 5 watts RMS output (10 watts peak). It contains 13 transistors (including two power types), 2 diodes. 1 zener diode and 18 resistors, and is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is more rugged and has considerable performance advantages, including complete freedom from thermal runaway and very low level of distortion. The IC10 is primarily intended as a full performance high fidelity power and preamplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. It may also be used in other applications including car radios, electronic organs, servo amplifiers (it is dc coupled throughout),

Circuit Description

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of tempera-Generous negative feedback round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

Each IC10 is sold with a comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include oscillators, etc. The pre-amp section can be used as an RF or IF, additional without any amplifier transistors.

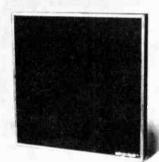
Specifications
Output: 10 watts peak, 5 watts RMS continuous.
Frequency response: 5Hz to 100kHz 1dB.
Total harmonic distortion: Less than 1% at

full output.
Load impedance: 3 to 15 ohms.
Power gain: 1104B (100,000,000,000 times) total.
Supply voltage: 8 to 18 volts.
Size: 1 0.4 0.2 in plus heat sink and tags.

Sensitivity: 5mV

impedance: Adjustable externally up to 2.5 Mohms. Price (with manual) 59/6.

Q16



High fidelity loudspeaker

The Q16 employs the well proven acoustic principles specially developed by Sinclair in which a special driver assembly is meticulously matched to the characteristics of the uniquely designed cabinet. In reviewing this exclusive Sinclair design, technical journals have justly compared the Q16 with much more expensive loudspeakers. Its shape enables the Q16 to be positioned and matched to its environment to much better effect than is the case with conventionally styled enclosures. A solid teak surround with a special all-over cellular foam front is used as much for appearance as its ability to pass all audio frequencies.

This shelf-mounted speaker brings genuine high fidelity within reach of every music lover.

Specifications

Construction: Special sealed seamless sound or pressure chamber with internal baffle. Loading: up to 14 watts RMS.

Input impedance: 8 ohms.

Frequency response: From 60 to 16,000Hz, confirmed by independently plotted B and K curve.

Driver unit: Special high compliance unit having massive ceramic magnet of 11,000 gauss, aluminium speech coil and special cone suspension.

Size and styling: 97 in square on 41 in deep with neat pedestal face 4% in deep with neat pedestal base. Black all-over cellular foam front with natural solid teak surround.

Price: £8 19 6.

Micromatic



Britain's smallest radio

Considerably smaller than an ordinary box of matches, this is a multi-stage AM receiver meticulously designed to provide selectivity, power and quality. Powerful AGC counteracts fading from distant stations; bandspread at higher fre-quencies makes reception of Radio 1 easy. The plug-in magnetic earpiece provided matches the Micromatic's output to give wonderful standards of reproduction. Everything including the special ferrite rod aerial and batteries is contained within the minute and attractively designed case. Whether you build a Micromatic kit or buy this amazing receiver ready built and tested, you will find it as easy to take with you as your wrist-watch, and dependable under the severest listening conditions.

Specifications

Size: $46 \times 33 \times 13$ mm, $(15 \times 1\frac{3}{10} \times \frac{1}{2}$ in). Weight: including batteries, 28.4 gm (one ounce).

Case: black plastic with anodised aluminium front panel and spun aluminium dial.

Tuning: medium wave band with bandspread at higher frequencies, (550 to 1,600kHz).

Earpiece: magnetic type.

On/off switching: by inserting and withdrawing earpiece plug.

Kit in pack with earpiece, case, instructions and solder 49/6.

Ready built, tested and guaranteed, with earpiece 59/6.

Two Mallory Mercury batteries type RM675 required. From radio shops, chemists, etc.



Sinclair Radionics Ltd., London Road, St. Ives, Huntingdonshire. Tel.: St. Ives (048 06) 4311

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2N919	4 -	AF118	12/6	OA10 OA47	5/- 2/-	100 + 3/6	I amn Plastic
2N920 2N922	5/- 8/6		6/- 5 -	OA70 OA71	2/- 2/-		100 + 2/3
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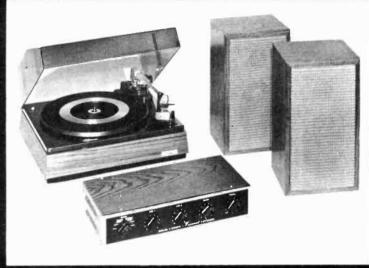
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SOUND 50

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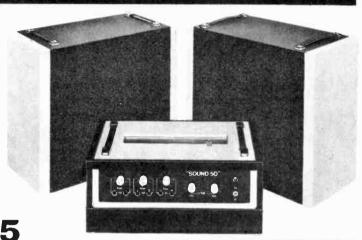
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inputs at 200 my into 470 K.

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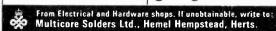
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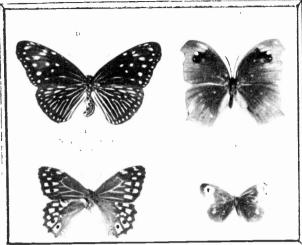


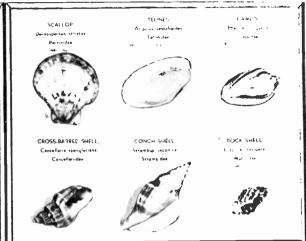
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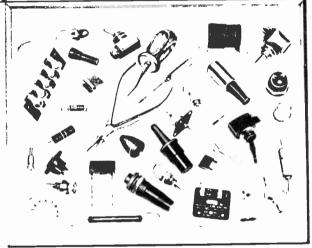
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ASTRONAUTS OR AUTOMATONS?

The landing of the unmanned vehicle *Lunokhod-1* on the moon's surface and its subsequent control from earth some 239,000 miles away was a unique and outstanding technical achievement: model control *par excellence!* This Soviet exploit has demonstrated quite clearly that man can devise and build automated equipment that will extend his influence over vast distances in space without incurring hazard to himself.

In everyday earthbound affairs, automation—which generally relies upon electronics for its brain power—has already made its indelible mark. Introduced primarily for sound economic reasons to overcome manpower shortage and to provide improved all-round efficiency, it brings about undoubted social improvements by removing many unattractive and irksome tasks from human hands. While automation can already supplant man to a lesser or greater degree in many activities, the ultimate extent of this takeover by machines is hard to predict. But the indications are that it will be determined by man's wishes, rather than by any technological limitations.

Clearly there are particular areas where man will not willingly abdicate his personal involvement in favour of a robot. The challenge of the unknown has impelled men to embark upon heroic adventures from the beginning of time. The mere invention of more speedy and comfortable means of conveyance has not extinguished the pioneer spirit that feels the urge to circumnavigate the globe alone, or to climb some colossal mountain peak. When all the formidable tasks of exploration presented by this earth have been successfully undertaken, man must needs look elsewhere for fresh fields to conquer. He is already looking impatiently out into space.

In this connection the achievement of the Russian lunar vehicle is especially interesting. It adds further fuel to the argument concerning whether it is wise or not to send men to the moon when the same kind of information they bring back can be gathered by an unmanned vehicle equipped with measuring and sensing devices and telemetry apparatus for transmitting data back to earth; and when rock specimens can be cored from the moon's surface and then be brought back to earth entirely by automatic means.

On a purely rational basis it would seem more sensible and logical to opt for the automated approach. Human lives would not be put in jeopardy and the cost would be a fraction of that for a comparable manned mission. But technical competence and cost efficiency will never dampen the human instinct to go and see for oneself; nor will risk to the person. The American astronaut Aldrin, the second man on the moon, afterwards remarked of "... the human need to do these things ..." This is certain, man will not be satisfied with exploring by remote control alone.

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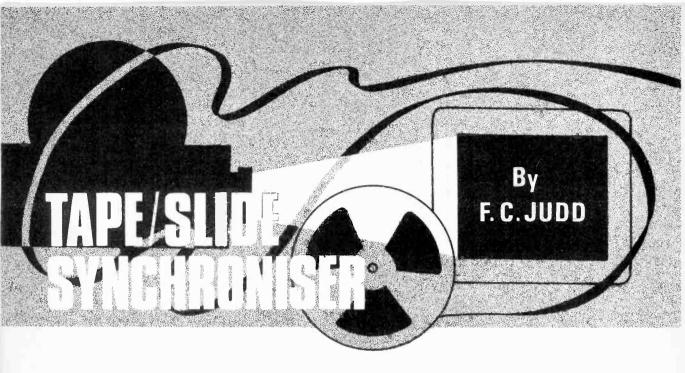
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Our March issue will be published on Friday, February 19

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A COLOUR slide show can be enhanced with a well spoken commentary, background music and even sound effects which, if recorded on magnetic tape, leaves the projector operator free to concentrate on changing the slides in time with the recording.

If the slide projector is an automatic one, normally operated from a remote control box, then it can be directly controlled from the tape on which the commentary has been recorded, which means that the slides can be changed automatically in accordance with the sound track.

CONTROL SYSTEMS

The operator's slide change button on the projector remote control box simply actuates a make and break contact which, in turn, applies current to the mechanism for changing the slides. This contact needs only to be replaced by a relay contact which can be operated electronically by impulses recorded on the magnetic tape containing the sound track.

One way of doing this is to record sub-audio impulses on the same track as the commentary and music but this necessitates filter circuits in the sound replay amplifier chain. One could, of course, fit an extra record/replay head on the tape deck so that impulses could be recorded on an unused track. This is fine providing there is space for the head and that it could be fitted without spoiling the tape deck.

The ideal system is one which can be used with any conventional tape recorder, stereo or mono, half-track or quarter-track, at any of the standard tape speeds and without any modification whatsoever to the tape recorder or of tape cutting and splicing.

The impulse control system to be described can be used with any automatic slide projector that requires only a single make and break contact to change the slides.

AUTOMATIC PROJECTORS

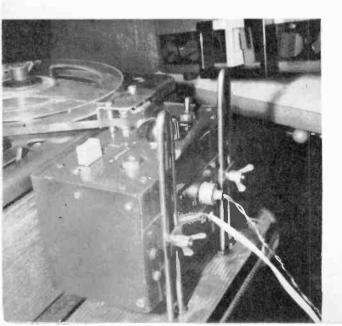
Automatic slide projectors are normally controlled from a push button on a small remote control box attached to the projector by a long cable. When the button is pressed the slide is changed and the slide carrier moves up ready for the next slide.

The remote control box has additional buttons for remote focusing and for reversing the slide change. These functions are not affected in any way by the use of an impulse controller and all that is required for impulse control is a pair of leads connecting the impulse control unit to the two contacts of the slide change button in the manual control box.

Most automatic slide projectors do in fact have a socket on the projector for connection to an impulse controller.

CIRCUIT DESCRIPTION

The circuit diagram shown in Fig. 1 is designed to record 100Hz pulses on to the lower half or quarter-track of standard ‡in wide tape. The pulses can be recorded whilst listening to the pre-recorded sound track.



When the tape is running through the controller the pulse track is being constantly erased by a direct voltage applied to the head X1, via R10 and S2a. With the controller switched to "Record" the record indicator

lamp will also be switched on.

When the pulse record button is depressed the direct erase voltage is disconnected and a 100Hz pulse, derived from the rectified supply input, is connected to the record/replay head. This pulse will be recorded on the tape. About one second is quite sufficient for the pulse time.

As the pulse button is depressed the 100Hz signal is also applied to the D1, C7, R12 network and consequently to the base of TR3 which will now conduct and

close the relay. This means that whilst the pulses are being recorded the slides will automatically change.

When the pulses have been recorded the controller is switched to "Playback", the tape rewound and the projector re-loaded. The whole programme can now be run entirely from the tape recorder as the projector will change slides automatically and in synchronism with the sound track.

During playback the pulses from the tape are picked up by the record/replay head on the controller, amplified by TR1 and TR2 and applied to the network C7, D1 and R12. On each pulse TR3 will conduct, the relay will operate and a slide will be changed.

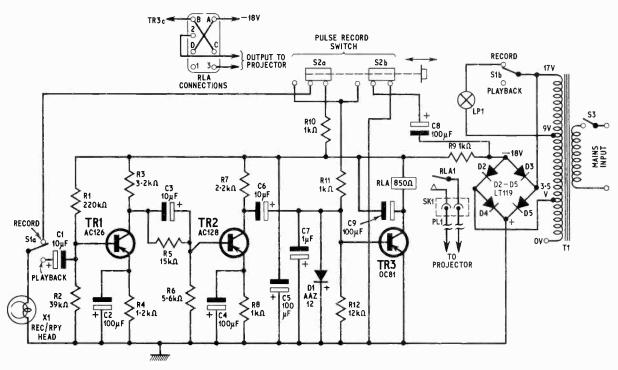


Fig. 1. Circuit diagram of tape/slide synchroniser

COMPONENTS

Resistors RI 220kΩ R4 I·2kΩ R7 2·2kΩ R10 IkΩ R2 39kΩ R5 I5kΩ R8 IkΩ R11 IkΩ R3 3·2kΩ R6 5·6kΩ R9 IkΩ R12 J2kΩ	S3 Single pole, on-off toggle switch Transformer T1 Mains transformer Type CTI/I (Henry's Radio)
All 4 watt, 10% carbon Capacitors	Record/Replay Head XI Marriott R/RPI half track
C1 10µF elect. 12V C6 10µF elect. 25V C2 100µF elect. 12V C7 1µF elect. 12V C3 10µF elect. 12V C8 100µF elect. 25V C4 100µF elect. 12V C9 100µF elect. 25V C5 100µF elect. 25V	Relay RLA $1,700\Omega + 1,700\Omega$ single pole changeover (Henry's Radio)
Transistors TRI ACI26 TR2 ACI28 TR3 OC81	LPÍ 12 V 0·1A MES Pilot lamp Miscellaneous
Diodes DI AAZ 12 (Mullard) D2-D5 Bridge rectifier Type LT119 (Henry's Radio)	Universal Chassis 6in \times 4in \times 3in and 6in \times 4in bottom plate (Home Radio) 18 s.w.g. aluminium base plate $7\frac{1}{4}$ in \times $3\frac{1}{2}$ in Mild steel rod 14in \times $\frac{3}{4}$ in (2 off)
Switches S1 2-pole, 2-way wafer switch S2 6-pole, 2-way; push on, release off (Henry's Radio)	Brass rod or sleeves for guides \$\frac{1}{4}\text{in dia (2 off)}\$ 4B.A. wing nuts (2 off), s.r.b.p. board and pins SKI, PLI Two pin plug and socket

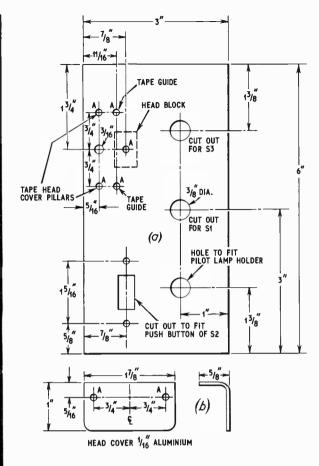


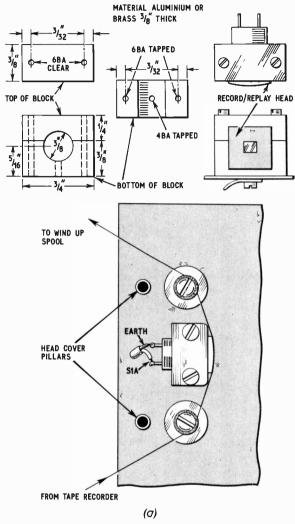
Fig. 2 (above). (a) Cutting and drilling details of top panel; (b) drilling and bending details of head cover

Fig. 3 (top right). Head mounting clock assembly details

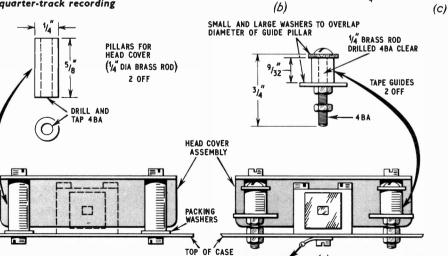
Fig. 4 (below). (a) Construction and mounting details of the head cover pillars; (b) tape guide assembly and mounting details

Fig. 5 (right) (a) Showing the mounting of the pillars and guides on the control panel. The spooling direction at the head is made clear by reference to the photograph on page 000; (b) alignment of tape for half-track pulse recording; (c) alignment for quarter-track recording

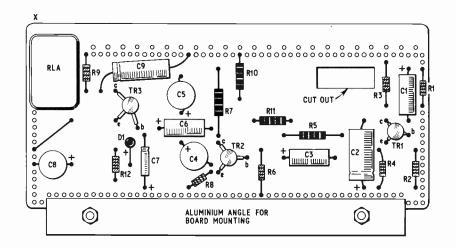
(0)



STANDARD 1/4 TAPE



EARTH



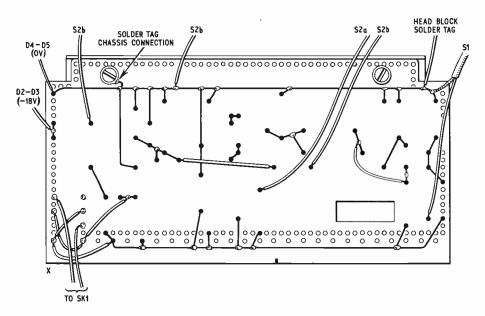


Fig. 6. Top and underside details of component mounting and wiring on plain Veroboard. Details of the relay wiring is given in Fig. I

CONSTRUCTION

The prototype unit was made up of 20 s.w.g. aluminium, but 18 s.w.g. is to be preferred for the extra rigidity afforded. A Universal chassis, 6in by 4in by 3in with a bottom plate, is suitable for housing and mounting the various parts.

Drilling and cutting details for the top panel are given in Fig. 2 (a). Fig. 2 (b) shows the tape head cover which is made from aluminium.

The tape head specified is a Marriott R/RPI high impedance type, and is supplied without a mounting. Details of the mounting block are given in Fig. 3.

This forms a clamp for the cylindrical body of the head and can be made from brass or aluminium to the dimensions given. The centre hole, tapped 4B.A. at the base of the block, is for the bolt which secures it to the top of the controller box.

Next for construction are the tape guides as shown in Figs. 4 (a) and (b). These can be adjusted for height so aligning the tape with the head gap as seen in Fig. 5.

BOARD ASSEMBLY

The transistors and small components are mounted and wired on a piece of plain Veroboard, 3in by 5\frac{1}{2}in as in Fig. 6. The cut-out at the end allows for the projection of the S2 switch assembly inside the case.

The relay has a double winding which, in this particular application, is connected in parallel to give a total resistance of 850 ohms. On the prototype no screws were needed to fix the relay to the board as the solder connections at the pins were sufficient to retain it in position.

CHASSIS ASSEMBLY

The tape head assembly and pillars should first be mounted on the drilled top panel followed by the various controls as shown in Fig. 7. The chassis base plate bears the mains transformer T1, the bridge rectifier and the two-pin socket which carries the twin lead to the projector automatic control socket or remote control, whichever is applicable.

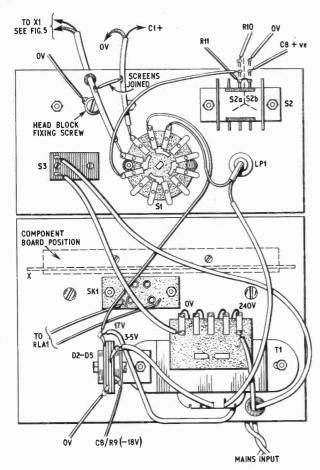
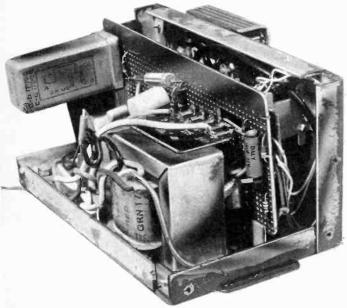
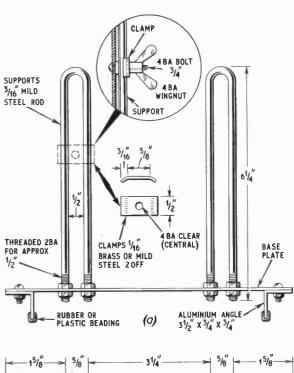


Fig. 7. Interwiring between control panel and base plate components. For Verboard connections Fig. 6 should be consulted



Interior view of the tape; slide synchroniser



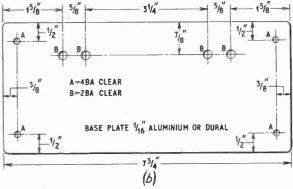
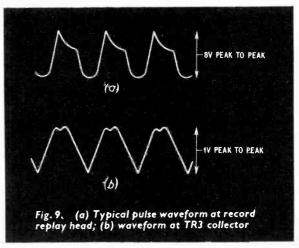


Fig. 8. (a) Supports and fixing clamps which allow the synchroniser to be positioned relative to the tape recorder deck; (b) base plate for support mounting



Mount the assembled board on a piece of aluminium angle, $\frac{3}{4}$ in by $\frac{3}{4}$ in by $\frac{5}{2}$ in, then fix this to the chassis, where indicated, using kalons.

Interwiring should now be completed using Figs. 6 and 7. Note that screened leads must be used for the head connections with the screening braid earthed at the solder tag under the head block fixing screw.

CONTROLLER STAND

The stand for the controller unit allows the height of the tape head to be varied from about $4\frac{1}{2}$ to over 8 inches above table top level so that it can be used with almost any domestic tape recorder.

Details for the base of the stand and the two main supports and the remainder of the assembly are given in Fig. 8. Note that the $\frac{3}{4}$ in, 4B.A. bolts on which the wing nuts are used, go through from the inside of the box and are then secured with 4B.A. nuts. The clamps and wing nuts will firmly hold the box at any height on the supports.

CHECKING OPERATION

The measured supply should be approximately 18V at the junction of R9 and C8 with the unit switched to "Playback". The total current measured at this point should be approximately 8mA.

When the unit is switched to "Record" and S2 button depressed the line voltage should fall to about 14V and the current will increase to around 18mA.

With the unit still switched to "Record" but with the impulse button off, the voltage across the record/playback head should be approximately IV.

With the controller switched to "Playback" the voltage at the junction of R7 and R9 should be about 14V

If an oscilloscope is available, the waveforms and their respective peak to peak amplitudes at the record/replay head and at TR3 collector can be checked as shown in Fig. 9.

TRACK ALIGNMENT

The tape head and guides can be aligned for either the lower half or quarter-track width as shown in Figs. 5 (b) and (c). With half-track recorders the upper half-track is used for sound. With quarter-track recorders the two inner tracks could be used for sound and the two outer tracks for pulses, which means that

two different programmes could be accommodated on one length of tape.

Accurate azimuth alignment of the head is not necessary and so long as the gap is vertical, it will operate efficiently. It is more important to get the track width aligned so that the pulse track does not overlap the sound track. If this should occur the pulses would be audible whilst playing the sound track.

USING THE CONTROLLER

First the sound track should be completed in its entirety, then the projector set up and the slide carrier loaded with all the slides in the correct order. Set the tape recorder for replay so that the sound track is audible and set the controller to "Record". The tape is taken off the tape recorder, around the controller head and back onto the wind up spool.

Set the tape recorder running and then simply press the pulse record button for about half to one second each time a slide is to be changed. When the pulses have been recorded, switch the controller to replay, disengage the tape from the controller head and rewind it.

If the tape is rewound whilst still in contact with the controller head and with the controller switched to record, all the pulses will be erased. If rewound with the controller set to replay then the slide projector mechanism will be rapidly operated.

For entirely automatic projection of the slides in synchronism with the sound track, it is only necessary to load the slides, connect up the controller and play the tape.

CONNECTING TO A PROJECTOR

For connections to a projector, twin leads should be suitably terminated with a two-pin plug for connection to the controller output socket SK1.

If the projector has a socket for connection to a controller, and most of them do, simply connect the free lead ends to this as instructed in the manufacturer's booklet.

Both the manual button on the projector control box and the pulse button on the controller can be used to override the recorded pulses during replay, but this will, of course, throw the slide sequence out of synchronism with the sound track.

View of the control panel. Here the head cover is removed



DUAL PURPOSE PAGE STEREO AMPLIFIER

By D. S. GIBBS and I. M. SHAW (FERRANTI LTD)

AVING introduced the pre-amplifier circuit briefly last month and given some of the individual circuit descriptions, we now go on to describe the rest of the circuit parts in detail, give the components list and start construction details of the pre-amplifier. Now that we are able to specify all the components, it is possible to say that the approximate cost of the complete amplifier and pre-amplifier will be £45. This cost is made up of £28 for the main amplifier and £17 for the pre-amplifier; prices of components vary by large amounts for some items and this price is only to give readers an approximate estimate of overall cost.

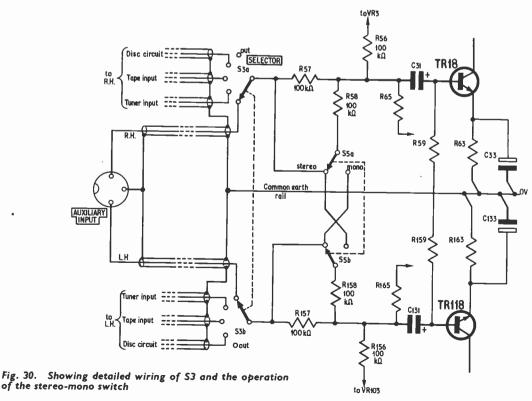
STEREO-MONO SWITCHING

Stereo-mono switching (Fig. 30) is performed by switch S5 which cross-connects the inputs so that

equal amounts of left and right are fed into each of the input mixers. This facility is useful when playing mono records with a stereo pick-up as it cancels out certain distortion products present in the output of the pick-up. It also enables a stereo recording to be converted to mono so that it may be recorded on a mono tape recorder.

TREBLE FILTER

The treble filter has two sections. The first section comprises capacitors C40 to C43 which appear in parallel with the amplifier feed-back resistor R60. These capacitors cause the gain of the amplifier to fall at 6dB per octave above the cut-off frequency. The second section is provided by inductor L2 and capacitors C36 to C39 which give a further 12dB per





octave to give a total slope of 18dB per octave. The LC section has been designed to give a peak of about 3dB before its cut-off to compensate for the initial slowly falling frequency response of the amplifier section.

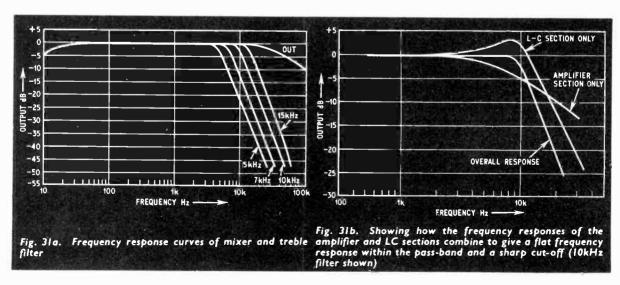
The overall frequency response is quite flat up to the cut-off point and has a sharp knee as shown in Fig. 31. Four cut-off frequencies have been provided. The 5, 7 and 10kHz positions can be used to remove spurious noise or harsh treble from poor recordings, whilst the 15kHz filter makes very little difference to the reproduced sound but gives a worthwhile reduction in the 19kHz and 38kHz components present in the output of a stereo v.h.f. tuner. In the out position the frequency response is -3dB at 40kHz.

The transient response of the treble filter is illustrated by Figs. 32a to 32e which show that the ringing produced is very well damped and inoffensive. Generally speaking the sharper the cut-off in the frequency response the worse the transient response becomes so that one has to strike a compromise which gives both a well damped transient response and a satisfying clean frequency response. The popular "parallel T" type of treble filter is particularly difficult in this respect.

TONE CONTROL

The tone control circuit comprising TR20, TR21, TR120 and TR121, uses the popular Baxendall configuration. In this design the tone control circuit is after the volume control so that it does not impose any limitation on the dynamic range of the preamplifier. When the tone control is placed before the volume control the dynamic range is reduced by the amount of boost employed, i.e., assuming such a pre-amplifier with a dynamic range of 20dB, turning up the bass control to give 15dB of bass boost will cause the dynamic range at low frequencies to be reduced to 5dB.

However when the tone control is placed after the volume control one has to take particular care to achieve a low noise level, since the noise output remains constant instead of being proportional to the setting of the volume control. The noise level generated by this design is 90dB below maximum output (-100dB weighted) and with loudspeakers of average efficiency this is inaudible at more than about three feet away from the loudspeakers. With loudspeakers of very high efficiency the noise level may be just perceptible under normal listening conditions. If this is found to



PRE-AMPLIFIER

(both channels-components for L.H. channel are R.H. numbers plus 100)

	to	

R32 R132	47kΩ	R57 R157	10 0 kΩ
R33 R133	2·7kΩ	R58 R158	100kΩ
R34 R134	$IM\Omega$	R59 R159	100kΩ
R35 R135	$IM\Omega$	R60 R160	220kΩ
R36 R136	100kΩ	R61 R161	$27k\Omega$
R37 R137	56 kΩ	R62 R162	27kΩ
R38 R138		R63 R163	22 kΩ
R39 R139	180kΩ	R64 R164	$3.3 k\Omega$
R40 R140	l0kΩ	R65 R165	4·7kΩ
R41 R141	10kΩ 10kΩ 4·7kΩ	R66 R166	47kΩ
R42 R142	4·7kΩ	R67 R167	3·3kΩ
R43 R143	$IM\Omega\pmIO\%$	R68 R168	3·3kΩ
R44 R144	$470\Omega \pm 10\%$	R69 R169	47 Ω
R45 R145	$10M\Omega \pm 10\%$	R70 R170	100kΩ
R46 R146	470kΩ 470kΩ 470kΩ 100kΩ	R71 R171	330k Ω
R47 R147	470k Ω	R72 R172	100kΩ
R48 R148	470kΩ	R73 R173	220k Ω
R49 R149	100kΩ	R74 R174	2·2kΩ
			I0kΩ
R51 R151	I0kΩ	R76 R176	IkΩ
R52 R152	470Ω	R77 I	00 k $\Omega \pm 10\%$
R53 R153	56Ω	R77 is not	required if
R54 R154	10kΩ 470Ω 56Ω 4·7kΩ 10kΩ	the neon la	amp has a
R55 R155	I 0 kΩ	built in res	sistor.
R56 R156	100kΩ		

Unless otherwise stated all resistors are $\frac{1}{2}$ watt carbon film or metal oxide of 5% tolerance or better. 2 off each except R77.

Potentiometers

VR3 VR103	100kΩ log twin-gang (single gang
***************************************	for mono microphone—see text)
VD 4 VD 104	
VR4 VR104	10kΩ log twin gang
VR5 VR105	470k Ω linear twin gang
VR6 VRI06	100kΩ linear twin gang
VR7	10kΩ linear single gang wirewound
	(see text)

Capacitors		
C16 C116	250μF elect. 40V	Mullard
C17 C117	IμF plastic film 63V	WIMA MKS
C18 C118	50μF elect. 40V	Mullard
C19 C119	0·022μF polyester 160V	Mullard
C20 C120	1500pF polystyrene 125V	Radiospares
C21 C121	8200pF polystyrene 125V	Radiospares
C22 C122	47pF polystyrene 125V	Radiospares
C23 C123	20μF elect. 16V	-Mullard
C24 C124*	lμF plastic film 63V	WIMA MKS
C25 C125	IμF plastic film 63V	WIMA MKS
C26 C126	lμF plastic film 63V	WIMA MKS
C27 C127	50μF elect. 40V	Mullard
C28 C128	47pF polystyrene 125V	Radiospares
C29 C129	20μF elect. 16V	Mullard
C30 C130*	lμF plastic film 63V	WIMA MKS
C31 C131*	lμF plastic film 63V	WIMA MKS
C32 C132	10pF polystyrene 125V	Radiospares
C33 C133	20μF elect. 16V	Muliard
C34 C134	5μF elect. 64V	Mullard
C35 C135*	lμF plastic film 63V	WIMA MKS
C36 C136	1500pF polystyrene 125V	Radiospares
C37 C137	2200pF polystyrene 125V	Radiospares
C38 C138	3300pF polystyrene 125V	Radiospares
C39 C139	4700pF polystyrene 125V	Radiospares
C40 C140	220pF polystyrene 125V	Radiospares
C41 C141	150pF polystyrene 125V	Radiospares
C42 C142	100pF polystyrene 125V	Radiospares
C43 C143	47pF polystyrene 125V	Radiospares
C44 C144	2·5μF elect. 64V	Mullard

C45 C145	6800pF polyster 400V	Mullard
C46 C146	6800pF polyester 400V	Mullard
C47 C147	1500pF polystyrene 125V	Radiospares
C48 C148	2·5μF elect. 64V	Mullard
C49 C149	10pF polystyrene 125V	Radiospares
C50 C150	20μF elect. 16V	Mullard
C51 C151	8μF elect. 40V	Mullard
C52	500μF elect. 64V	Mullard

* plastic film IµF capacitors are recommended for these positions but as these are rather expensive IµF 40V electrolytic capacitors may be used instead if desired. The correct polarity is shown on the circuit diagram. 2 off each except C52.

Semiconductors

T14 T114 T15 T115 T16 T116 T17 T117 T18 T118 T19 T119 T20 T120 T21 T121	ZTX 107 Ferranti ZTX 531 Ferranti ZTX 107 Ferranti ZTX 503 Ferranti ZTX 107 Ferranti ZTX 107 Ferranti ZTX 107 Ferranti ZTX 107 Ferranti ZTX 107 Ferranti
721 1121 2 off each	ZIX 10/ Ferranti

Switches

- DPDT toggle or slide switch
- **S2** DPDT ditto
- S2 2 pole 5 way rotary Maka switch
- 6 pole 5 way rotary Maka switch
- DPDT rotary mains switch

Inductors

L2 L102 FX2239 pot core assembly with DT2204 coil former wound with 228 turns of 34 s.w.g. enamelled wire tapped as follows (2 off):

> 5kHz full winding tapped at 196 turns 7kHz 10kHz tapped at 162 turns 15kHz tapped at 134 turns

Note that two FX2239 Ferrite cups are required for each complete pot core.

Miscellaneous

01–232	DIN 180° 3 pin or 5 pin socket (6 off)
SKII SKI2	DIN 300° 5 pin socket (2 off)
SK13	3 pin mains plug & socket (Bulgin P429
	and P430)
LPI	neon panel lamp
	Control knobs: Eagle type k30/3 used

on the prototype (8 off)
Case Contil MOD-2 size G obtainable from West

Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middlesex.

Printed circuit board Capacitor clamp in spacers 6B.A. 4 off 6B.A. fixings

Aluminium panel $12\frac{3}{4} \times 2\frac{3}{4} \times 18$ s.w.g. for dummy front panel (cut from unused main amplifier chassis)
C3-2800 µF 100V Mullard is obtainable from Home Radio Ltd.

Electroniques address is Edinburgh Way, Harlow, Essex.

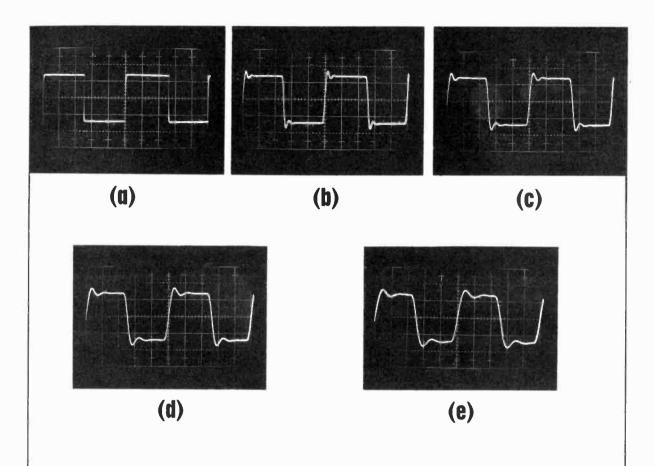
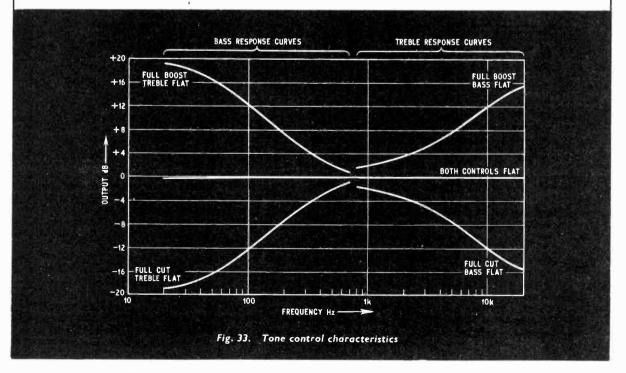
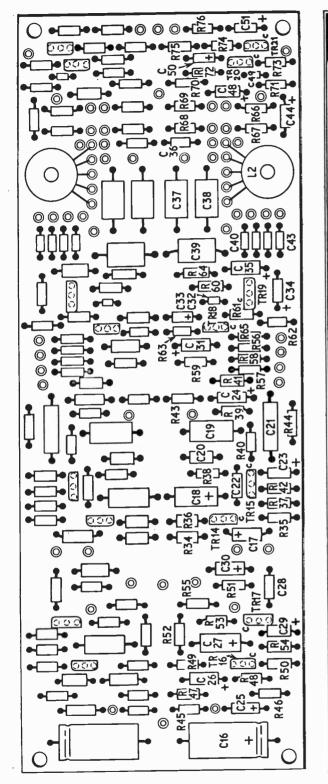


Fig. 32. Treble filter transient response (a) filter out—IkHz signal, (b) I5kHz position—IkHz signal, (c) I0kHz position—IkHz signal, (d) 7kHz position—IkHz signal, (e) 5kHz position—IkHz signal





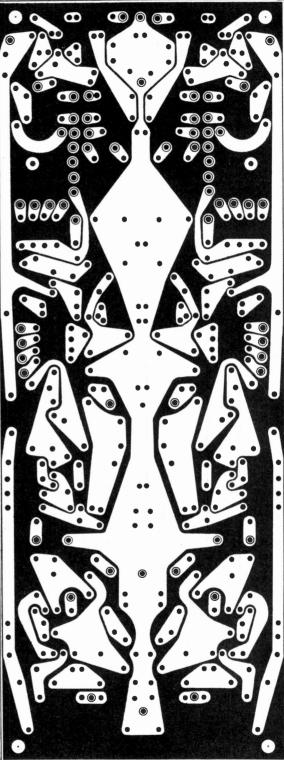
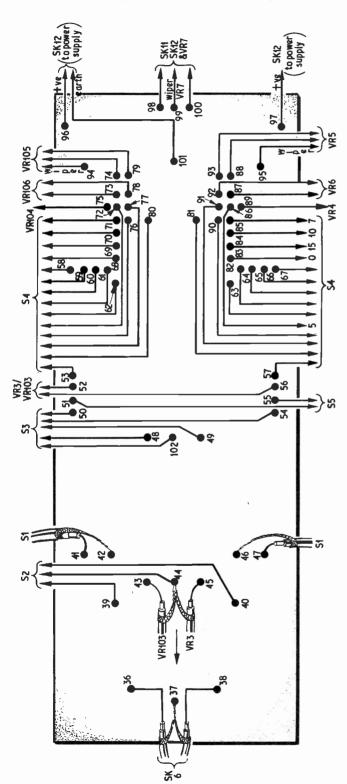


Fig. 34. Layout diagram of both channels of the pre-amplifier printed circuit board. Components for the left-hand channel have not been designated as this section is a mirror image of the right-hand channel—designations are right-hand channel numbers plus 100. The finished size of this board is $10\frac{3}{4}$ in by $4\frac{1}{8}$ in

Fig. 35 (right). Tag numbering and wiring details of the printed circuit board. Care must be taken when wiring up that left and right channel leads are identified and wired to the correct switch, potentiometer or socket positions

be the case the situation can be improved by increasing R76 and R176 to 4.7 kilohms or 10 kilohms, giving a 6 or 10dB reduction.

The tone control circuit uses two transistors instead of the usual single transistor to enable a very low noise



level to be obtained and to minimise distortion. The distortion generated is below 0.01 per cent at maximum output between 100Hz and 10kHz. The balance control is connected to the output of the tone control and works by progressively shorting out one channel or the other so that either channel can be completely cut off. To minimise cross-talk a wire wound potentiometer is preferred for VR7 but excellent results can be obtained with the ordinary carbon type.

Full rotation of the bass control gives a cut or boost of $\pm 12 dB$ at 100Hz and $\pm 18 dB$ at 30Hz. The treble control gives $\pm 12 dB$ at 10kHz and $\pm 15 dB$ at 20kHz. The frequency response curves of the tone

control are shown in Fig. 33.

POWER SUPPLY

The complete stereo pre-amp requires approximately 35mA at 40 volts. A 470 ohm dropping resistor (R7) is included on the power supply board previously described and the h.t. line is decoupled in the preamp by C52 (500µF 64V).

The mains supply lead is connected to the preamplifier where the earth is connected, the live and neutral leads being switched by S6 and fed out to the main amplifier together with the earth. This part of the circuit must be carefully screened from the rest of the pre-amplifier, the small chassis supplied with the case specified being ideal for this.

CIRCUIT BOARD CONSTRUCTION

The pre-amplifier components are mounted on one large fibreglass printed circuit board, Fig. 34. Sixty-seven turret tags are used, numbered 36 to 102 as indicated in Fig. 35. The high frequency filter coils L2 and L102 should be wound as indicated in the pre-amplifier components list, with the wires colour coded with sleeves for identification. The coils are fastened to the printed circuit board with either nylon or brass 4B.A. bolts and connected as follows:—

L2 Start-82, 15kHz-83, 10kHz-84, 7kHz-85, 5kHz-86. L102 Start-68, 15kHz-69, 10kHz-70, 7kHz-71, 5kHz-72.

The component values should be thoroughly checked at this stage since it will be difficult to rectify mistakes after the 67 tags have been wired up.

Note: In Fig. 23 (December 1970 issue) the lead from the neutral connection on SK4 should go to the OV tag on TI and not to the screen as indicated.

Next month: final construction details.

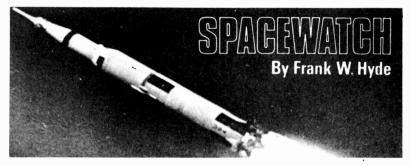
-P.E. PROJECTS ON VIEW-

The P.E. Gemini aroused much interest when it was demonstrated, together with the P.E. Aurora Lighting Display, last Autumn at the London Audio Fair.

It is hoped to provide a further opportunity for readers to hear this amplifier during the Public Address Engineers' Exhibition "Sound 71" to be held at Camden Town Hall, London, from March 16-19.

The P.E. Aurora Lighting Display, due to commence publication in a few months' time, will also be on show at "Sound 71," and additionally, at the "Electric Theatre" Exhibition organised by the Institute of Contemporary Arts, and to be held in London, mid-March to mid-April.

Further details will appear next month.



THE MAN WHO CAME BACK

The United States' first man in space, Alan B. Shepard, watched with satisfaction the slow movement of the Saturn-Apollo rocket moonship to become Apollo 14 as it moved toward the launching pad on November 9, 1970.

He first made history in the space age when he made a 15 minute suborbital flight almost ten years ago on May 5, 1961. From then, he became almost forgotten for he was grounded by a condition of the inner ear.

During the remainder of the 60's he remained on the sidelines, although still in the "astronaut corps", where he helped to train young and new astronauts, some of whom became heroes of space. Now he comes back as mission commander for the

Apollo 14 flight.

Captain Shepard undertook, on his own decision, to have an operation for the minor problem of his inner ear. Although he was perfectly fit on the ground, space doctors were afraid that his balance might be affected under space conditions. This has now been cured and the first astronaut becomes the leader of the Apollo 14 mission to the Fra Maro region.

SPIN-OF FROM SPACE RESEARCH

When space research comes up in conversation, there are still many who do not appear to be aware of the advantages that have affected the daily life of the community. Indeed, many would be surprised at the number of new techniques that are in common use, which were the direct result of some specialised facet of a space requirement.

A few of these are given here and will help perhaps to act as a reminder of the number of things that are taken for granted with no thought

given to their origin.

The latest example is an automated technique for the detection of urinary tract infections. The device uses a very sensitive photo-electronic recorder to detect a flash of light when certain chemicals (luciferin and luciferase) contact bacteria in the urine sample.

A single specimen can be tested in 15 minutes and the instrument can accept a further sample in one minute after completion of the previous one. This compares with the normal 24-48 hour period required with the bacteria culture methods.

This new technique opens up many possibilities. With such rapid testing there is no need to treat patients with anti-biotics while waiting for results. The new device also paves the way for inexpensive mass testing of people for suspected infections like diabetes, kidney and bladder diseases. Experienced microbiology staff would be freed for more advanced work.

The testing of urine is a common diagnostic tool in many hospitals no matter what the suspected ailment may be. The origin of this particular device came from the design of an instrument to detect life on other

planets.

The chemicals responsible for the "cold light" emitted by fireflies, spark when coming into contact with a high energy biochemical called adenosine triphosphate. This compound is found universally in living organisms so that the activation of the chemicals would indicate that a form of life was present.

OTHER EXAMPLES

A few more examples of spin-off are listed below with their origins.

(a) A special computer technique developed to enhance the television pictures sent back fron Venus and Mars is now in use to clarify X-ray photographs in medical centres.

(b) A minute instrument developed to measure air pressures on small flight models used in wind tunnels has been applied to medicine. The instrument is so small that it can be introduced into an artery through a hypodermic needle, then manœuvred through the artery to the heart, where it measures the blood pressure.

(c) In order to prevent the icing of spacecraft a special canopy was developed. This has been adapted as a cradle type of cover for the precise temperature control of a unit for housing premature babies. It has also been adapted for adults and a number of severely burned patients have been successfully treated.

(d) A sensor developed for astronauts sounds an alarm within ten seconds when a patient is threatened with the clogging of the trachea and there is danger of strangulation. Immediate efforts to restore the breathing can be made.

(e) A new switch which is controlled by small movement of the head alone was developed for astronauts. This is now being used for handicapped patients who, with what is virtually another "arm", can operate a call board or even manipulate an electric wheel chair.

(f) Spray-on electrodes are now available so that a patient's electrocardiogram, taken while he is being rushed to hospital, can be radioed ahead to the waiting doctor, who can take immediate action on the patient's

arrival

(g) New alloys, that have been developed for space use, can be adapted for use in artificial limbs and joints. The alloys are the result of a discovery by NASA metallurgists that hexagonal crystals make better bearings than the normal cubic crystal structure.

(h) A lunar walker with eight legs has been applied to the relief of handicapped people. It allows a considerable freedom of movement and can be controlled from a chin cup by those who are not able to use

arms or hands.

MAKING WATER ON THE MOON

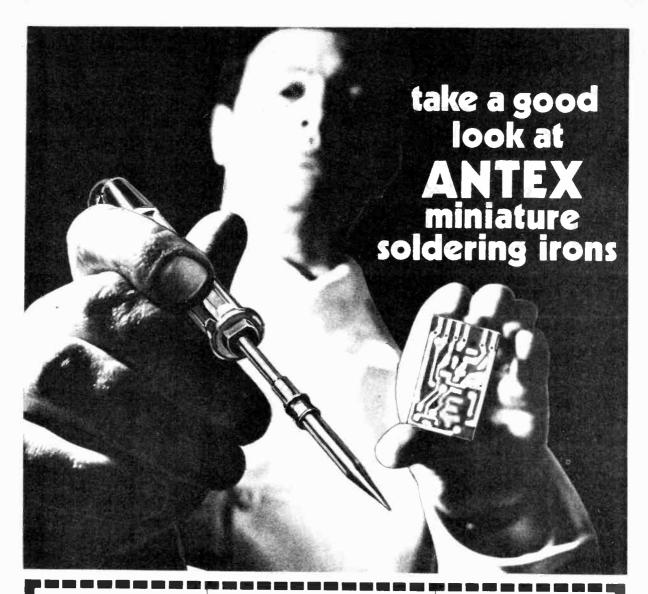
A new and important step toward the sustaining of life on the moon has been made at the Manned Spacecraft Centre of the U.S. Space Agency. The first experiments provided a pound of water from 100 pounds of soil. This could be increased to 14 pounds per 100 pounds of soil, if it were concentrated magnetically.

The process is a simple one and ideally suited to the moon (though it can be used on earth). A mirror is used to concentrate the sun's rays on a container of soil and raise its temperature to between 600 and 1,300 degrees centrigrade. Hydrogen is then introduced into the container. It reduces the oxygen atoms in the soil to form steam. When this is cooled it condenses to water.

To obtain oxygen, steam is passed through an electrolysis cell where the steam separates into oxygen and hydrogen. The oxygen can come from an iron-titanium oxide called ilmenite. This is abundant in the lunar soil as revealed by the samples brought back by the Apollo 11 and Apollo 12 astronauts.

The hydrogen would have to be taken to the moon but it could be recirculated and used many times over to produce more oxygen.

None of the lunar specimens have been used for the purpose of this experiment. The soil was made from the proper proportions of ground basalt from Hawaii and ilmenite from Canada. However, the scientists responsible have sufficient faith in the process to have taken out a patent for the process.





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PART EIGHT—By R. W. COLES

TTL SYSTEMS

AVING discussed TTL gates and flip-flops in previous articles, let us now see how these circuits can be put together to perform specific tasks.

SYNCHRONOUS COUNTER

These counters can become quite complex when counts which are not binary multiples are required, and it is beyond the scope of this article to delve into the

design procedure necessary.

Straight binary counts are, however, quite simple in design. As an example, have a go at a divide-by-sixteen counter of this type. Remember that a JK flip-flop will change state when both its J and its K input, or inputs, are at 1. If they are anything other than this, the information presented will merely be stored in the flip-flop. The truth table of a binary counter shows that any given flip-flop in the chain is required to change state only when all the flip-flops preceding it are in the 1 state.

If all the stages are clocked simultaneously, but only the J and K inputs of any stage are at 1 when the preceding flip-flop outputs are also 1, the flip-flop acts as a synchronous counter. By feeding the Q outputs of the earlier stages into an AND gate, and feeding its output into the J input (the K input may be left as a permanent one), the required JK inputs are satisfied.

Fortunately, flip-flops are available with this AND gate built in. The 7472 will be ideal as a synchronous counter and is shown in Fig. 8.1. Note that with this type of counter the number of AND gate inputs increases linearly with the number of stages in the counter.

If a five stage version is required, external gates would be needed because there are only three inputs to the internal J gates on the 7472.

SHIFT REGISTERS

Shift registers are used in logic circuitry as a form of temporary storage, or memory, and may contain either a number or some form of instruction which is represented by a number. The basic shift register would consist of a string of flip-flops with the outputs of the first connected to the inputs of the second and so on. A common clock line initiates the propagation of information down the register when required.

If JK flip-flops are employed in such a register, the Q outputs are connected to the J inputs of the following flip-flop, and the \overline{Q} outputs are connected to the K inputs. If, on the other hand, a type D flip-flop is employed, only one interconnection is needed, i.e. Q output to D input. For this reason, it is easier to deal with the type D for such use, and the diagrams will

be simpler as a result.

SERIAL INPUTS

A basic shift register is shown in Fig. 8.2a. If the register is in the all 0 state, and the data input is connected to the output of a similar register which contains a binary word, say 10101, then on the first clock pulse (both registers clocked), a 1 will be entered into the first flip-flop.

On the second clock pulse a 0 will be shifted into the first flip-flop, and the one which it contained previously

will be shifted into the second flip-flop.

On the third clock pulse another 1 will be entered into the first stage, a 0 will be entered into the second

stage and a 1 into the third stage.

This process continues until after five clock pulses; the word which was in the first register has been transferred completely into the second. If the input of the first register had been connected to a permanent 0 during this period, it would now contain all 0.

This type of shift register operation is termed serial-in/serial-out, and although it is the primary way in which registers are employed, it is by no means the only way. Consider Fig. 8.2b; the register shown here is identical to the first except that all the Q outputs are taken out at once, enabling us to extract the stored word in parallel form, perhaps to drive indicator lamps, or even another register.

This kind of register is operating in the serial-in/parallel-out mode, and its operation is obvious.

PARALLEL INPUTS

Its complement, the parallel-in/serial-out register, shown in Fig. 8.2c, takes advantage of the type D flip-flop asynchronous inputs to enter data into the register.

This input data could come from the type of register described previously or from a bank of switches or relays. The only thing to bear in mind in this case is that a "low" voltage on the preset input sets the Q output to 1 (high voltage level) and a low voltage on the clear input sets the \overline{Q} output to a 1.

To start the sequence the register must be cleared by applying a low input to the common clear line, so that all the stages contain zeros. Next the input data to be stored is connected in parallel to the preset inputs; this must be inverted data, because a low input sets up a

high output.

When the data is required to be shifted out, five clock pulses are applied to the clock line, and the output data is taken from the final stage of the register in serial form

As an alternative, the circuit in Fig. 8.2d could be employed to achieve the same result if both the "true" and the "not" version of the input data is available. In

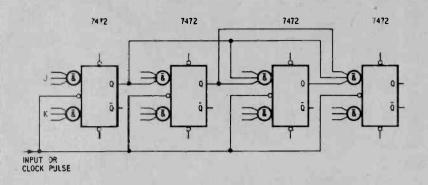


Fig. 8.1. Synchronous counter to divide by sexteen

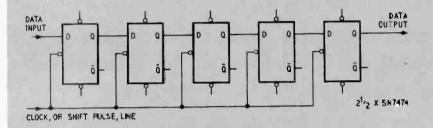


Fig. B.2a. Serial In, serial out register

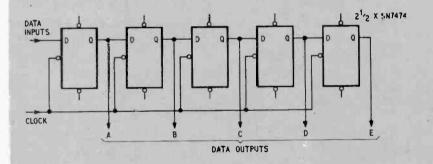


Fig. 8.2b. Serial in, parallel out register

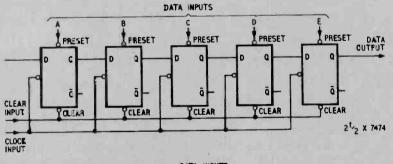


Fig. 8.2c. Farallel in, serial out register

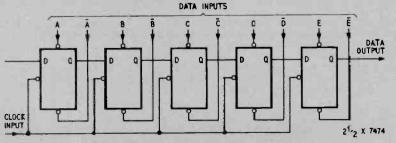
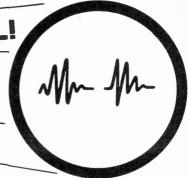


Fig. 8.2d. Alternative version of Fig. 8.2c

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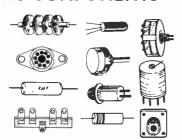


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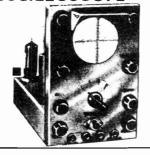
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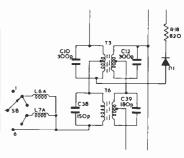


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3 in. 1/6 4 in. 1/10			in Plastic Librar 260 10/6	y Packs	(DN2) Dual CDS/320	6/6	9/6
5 in. 2/3 5% in. 2/6		(290 12/6 2120 17/6		(DN3) ELAC KST9	6/6	9/6
7 in. 2/7			on all orders.		(PE10)	6/6	9/6

		STY	/LII		
	Sapphire	Diamond	ELAC KST9		Diamond
GP59	,2/6	7/6	(PE1B)		9/6
GP65	2/6	7/6	ER5MB	6/6	9/6
GP67	2/8	7/6	ER5MX	2/6	7/6
GP73-1	6/6	9/6	ER5 SB	6/6	9/6
GP73-2	6/6	9/6	ER60 Stereo	6/6	9/6
GP79	2/6	7/6	DECCA		
GP81-1	2/6	7/6	Deram., diame	and only	27/9
GP91-1	6/6	9/6	GARRARD		
GP91-2	6/6	9/8	EV26 Stereo	2/6	7/6
GP91-3	6/6	9/6		2/6	7/6
GP91-18c	6/6	9/6			7/6
GP91-38c	6/6	9/6			
GP93-1	6/6	9/6	GCE12		7/6
GP94-1	6/6	9/6	GCS10/1		7/6
GP95-1	6/6	9/6	GCS10/2		7/8
GP96	6/6	9/6	8 1-2-3		9/6
HGP37	2/6	7/6	TS1		9/6
104	6/6	9/6	TS2	6/6	9/6
104	0/0	8/0	TS3	6/6	9/6
B.S.R.			GOLDRING		
BSR C1 (8T3)	6/6	9/6	CM50	2/6	7/6
BSR TCSH	2/6	7/6	CM60	2/6	7/6
BSR TC8M	2/8	7/6	MX1	2/6	7/6
BSR ST8	8/6	9/6	MX2	2/6	7/6
BSR ST9	6/6	9/6	Stereo CS80	2/6	7/8
BSR ST10	-,-	9/-	PERPETUUM ER		.,.
BSR X1M	6/6	9/6	PE188	6/6	9/6
BSR X1H	6/6	9/6	PHILIPS	0,0	-,-
BSR X3M	6/6	9/8		0.10	710
BSR X3H	6/6	9/6			7/6
BSR X5H	6/6	9/6	AG3063	2/6	7/6
BSR X4H	6/6	9/6	AG3306	6/6	9/6
	0,0	0,0	AG3310/3306	6/6	9/6
COLLARO			AG3400	2/6	7/6
Collaro Studio			RONETTE BINOI		
"O"	2/6	7 6	BF40	2/6	7/6
Collaro-Rouett			DC284	2/6	7/6
TX88	2/6	7.6	SONOTONE		
Collel SK 1	2/6	7/6	2T	6/6	9/6
Dual CD82/CD8			3 T	6/6	9/6
(DN2)	6/6	9 6	8T4A	6/6	9/6
Dual CDS/320	-, •	-, -	9TA	6/6	9/6
(DN3)	6/6	9/6	9TA/HC		9/6
ELAC KST9	0,0	0,0	19T	2/6	7/6
(PE10)	6/6	9/6	20T	2/6	7/6

SEMI	CONDUC	TORS	BRAND	NEW - M	ANUFAC	TURERS'	MARKINGS	· NO	REMARKED D	EVICES
2N388A	12/6 2N2613	7/- 2N3708	3/8 2N5267		4/- BC115	6/6 BD132		D16P4		C22 10/-
2N404 2N696	4/6 2N2614 4/- 2N2646	6/- 2N3709 11/6 2N3710	3/6 2N 5305 4/- 2N 5306		4/6 BC116 5/- BC116A	12/6 BDY10 7/6 BDY11	27/6 BFY41 10/- 37/6 BFY43 12 6	GET113		OC23 10/- OC24 11/6
2N697	4/- 2N2696	6/6 2N3711	4/- 2N5307		12/6 BC117	7/9 BDY17		GET114		C25 10/-
2N698	5/- 2N2711	6/- 2N3713	30 - 2N5308	7/8 AC188	7/6 BC118	6/6 BDY18	49/6 BFY51 4/6	GET118	4/- NKT243 12/6 C	OC26 6/6
2N699 2N706	12/6 2N2712 2/6 2N2713	6/- 2N3714 5/6 2N3819			5/6 BC121 5/- BC122	4/- BDY19 4/- BDY20		GET119 GET120		OC28 12/8 OC29 15/-
2N706A	2/6 2N2713 2/6 2N2714	5/8 2N3819 6/- 2N3823			5/- BC122 5/- BC125	11/- BDY38		GET120		0C35 8/-
2N708	3/- 2N2865	12/6 2N3826	6/- 2N 5355	5/6 ACY20	5/- BC126	11/- BDY60	36/- BFY75 6/-	GET880	6/- NKT264 8/- C	C36 12/6
2N709	12/6 2N2904	7/- 2N3854	5/6 2N5350		5/- BC134	11/6 BDY61		GET887		341 4/6
2N718 2N718A	5/- 2N2904A 6/- 2N2905	8/- 2N384A 8/- 2N3855			4/- BC140 4/- BC147	7 6 BDY62 3/6 BF115		GET890		OC42 5/= OC44 4/=
2N726	6/- 2N2905A	9/- 2N3855			4/- BC148	3/- BF117		GET896		C45 2/6
2N727	8/- 2N2906	6/- 2N3856		7/6 ACY41	5/- BC149	3/6 BF163	7/- BFW59 5/-	GET897		C46 3/-
2N914 2N916	3/6 2N2906A 3/6 2N2907	6/8 2N3856		15/- ACY 44 37/6 AD140	8/- BC152	3/6/BF167 4/- BF173	5/- BFW60 5/- 6/6 BPX25 37/-	GET898 MAT100		C70 3/-
2N918	6/- 2N29023	8/- 2N3858 3/6 2N3858		37/8 AD140 8/8 AD149	8/- BC157 11/6 BC158	4/- BF173 3/6 BF177	6/6 BPX 29 36/-	MAT101		0C71 2/6 0C72 2/6
2N929	4/8 2N2924	3/6 2N3859		6/6 AD150	12/6 BC159	4/- BF178	7/- BPY10 29/-	MAT 120		C74 6/8
2N930	5/6 2N2925	3/6 2N3859		6/6 AD161	7/8 BC160	12/6 BF 179	14/6 BSX 19 3/6		6/- NKT405 15/- O	C75 4/6
2N987 2N1131	10/6 2N2926 5/6 Green	2/9 2N3866		5/8 AD162 5/8 AF106	7/6 BC167 8/6 BC168B	3/- BF180 2/9 BF181	7/- BSX20 3 6 6/6 BSX21 7/6	MJ400 MJ420		C76 4/8
2N1132	6/6 Yellow	2/6 2N3877		5/8 AF114	5/- BC168C	3/- BF 184	5/- BSX26 9/-	MJ421		0C77 5/6 0C78 5/-
2N 1302	3/6 Orange	2/6 2N3877		37/6 AF115	8/- BC169B	2/9 BF 185	8/6 BSX 27 9/6	MJ 430	20/6 NKT453 9/6 O	C81 4/-
2N1303 2N1304	3/6 2N3011 4/6 2N3014	6/- 2N3900 6/6 2N3900		18/6 AF116	5/- BC169C	3/- BF194 3/6 BF195	4/6 BSX28 6/6 5/6 BSX60 16/6			C81D 4/-
2N 1304	4/8 2N2053	6/6 2N3900 5/6 2N3901	A 8/- 3N140 19/6 3N141	19/8 AF117 19/6 AF118	5/- BC170 12/- BC171	3/6 BF195 3/6 BF196	8/6 BSX61 12/6	MJ481	0.5	C83 5/
2N1306	5/- 2N3054	11/- 2N3903	7/- 3N142	19/8 AF119	4/- BC172	3/6 BF197	6/4 BSX76 4 6	MJ490	20 - NKT6771 6/- 0	C84 5/- C139 6/6
2N1307	5/- 2N 30 55	15/- 2N3904			4/6 BC175	5/6 BF198	8/6 BSX77 5/6	MJ491	27 6 NKT713 5/- O	C140 6/6
2N1308 2N1309	6/- 2N3133 6/- 2N3134	6/- 2N3905 6/- 2N3906		22/6 AF125 AF126	4/- BC182 4/- BC183	4/6 BF200 4/6 BF224	7/4 BSX78 5,6 6/- BSY10 5,6	MJ1800 MJE340		C169 4/8
2N1507	5/8 2N3135	5/- 2N4058		13/6 AF127	3/8 BC184	4/8 BF225	6/- BSY11 56	MJE520	17 4 Marian man 19	C170 6/- C171 6/-
2N1613	5/- 2N3136	5/- 2N4059		10/- AF139	7/6 BC182L	4/- BF237	6/6 BSY24 3/-	MJE521	17 6 NKT773 5/- 0	C200 6/8
2N1631 2N1632	8/6 2N3349 8/6 2N3349	19/6 2N4060 26/- 2N4061		19/8 AF178 8/- AF179	9/- BC183L 9/- BC184L	3/6 BF238 4/- BF257	6/6 BSY25 3/- 9/6 BSY26 3 6	MPF102 MPF103	8 6 NKT781 6/- 0	C201 9/6
2N1637	8/6 2N3390	7/8 2N4062		11/6 AF180	10/8 BC187	5/8 BF22A	9/6 BSY27 3/6	MPF104	78 311110000 0/0	C202 9/6
2N1638	7/8 2N3391	4/- 2N4244	9/6 40311	9/6 AF181	8/6 BC212L	4/8 BFX12	4.6 BSY28 3.6	MPF105	4/0 NTV: MT0400 # 0 0	C203 6/6 C204 8/6
2N1639	7/6 2N3391A	6/- 2N4245		12/6 AF186	13/4 BC2131.	5 4 BFX 13	4/6 BSY29 3/6 7/- BSY32 5/-	MPS3638 NKT001:	0/0	C205 8/6
2N1701 2N1711	32/6 2N3392 5/- 2N3393	4/- 2N4254 4/- 2N4255	8/6 40314 8/6 40315	9/6 AF239 9/6 AF279	9/6 BCY10	5 6 BFX29 5 6 BFX43	7/- BSY32 5/- 7/8 BSY36 5/-	NKT124	8 6 NK TO0300 0 8 0	C207 12/6
2N1889	8/6 2N3394	4/- 2N4284		12/6 AF280	12/8 BCY30	5 6 BFX44	7/8 BSY37 5/-	NKT125	5/8 NKT80111	CP71 8/6
2N1893	8/6 2N3402	4/8 2N4285		9/8 AFZ11	6/8 BCY31	5 6 BFX 68	13/6 BSY38 4/6		0,0	346A 4/6 1834 12/6
2N2147 2N2148	14/6 2N3403 12/6 2N3404	4/6 2N 4286 7/6 2N 4287	3/6 40319 3/6 40320	13/6 ASY26 9/6 ASY27	5/- BCY32 7/6 BCY33	7 6 BFX84 4/- BFX85	6/- BSY39 4/6 7/- BSY40 6/6	NKT128 NKT135		1843 8/-
2N2160	11/6 2N3405	9/- 2N4288		8/6 ASY28	5/8 BCY34	4 8 BFX 86	6/- BSY51 6/6	NKT137	6/6 NKT80113 T	1844 2/6
2N2193	9/6 2N3414	5/8 2N4289	3/6 40324	11/6 ASY29	5 6 BCY38	4/6 BFX87	6/- BSY52 6/6			1845 3/6
2N2193A 2N2194A	10/- 2N3415 4/6 2N3416	5/6 2N4290 7/6 2N4291	3/6 40326 3/6 40329	19/6 ASY36 7/- ASY50	5/ BCY39	8/6 BFX88	5/- BSY53 7/8 12/6 BSY54 8/-	NKT211 NKT212		1846 3/6 1847 3/6
2N2194A 2N2217	5/6 2N3417	7/8 2N4291		7/- ASY50 7/- ASY51	5/ BCY40 6/6 BCY42	7/6 BFX 89 3/- BFY 10	6/6 BSY56 18/-			1848 8/6
2N2218	6/8 2N3439	26/- 2N5027	10/6 40347	8/6 ASY53	5/- BCY 43	3/- BFY11	8/6 BSY78 9/6	NKT214	4/6 18/6 <u>T</u>	1849 3/6
2N2219	6/6 2N3440	19/6 2N5028		12/6 ASY54	5/- BCY54	8/6 BFY17	4/6 BSY79 9/- 6/6 BSY82 10/6	NKT215	210 12.11	1850 4/6 1851 3/6
2N2220 2N2221	5/- 2N3570 5/- 2N3572	17/6 2N5029 17/6 2N5030	9/6 40360 8/6 40361	11/- A8Y62 12/6 A8Y63	5/- BCY58 3/6 BCY59	4/8 BFY18 4/8 BFY19		NKT216 NKT217		1862 3/6
2N2222	6/- 2N3605	5/6 2N5172		13/6 ASY72	5/- BCY60	19/8 BFY20	12/6 BSY95A 2/6	NKT219	6/- 18/6 <u>T</u>	1853 6/
2N2287	21/6 2N3606	5/8 2N5174		7/6 ASY83	5/- BCY70	4/_ BFY21		NKT223		1860 6/ 1861 6/-
2N2297 2N2368	6/- 2N3607 3/6 2N3662	4/6 2N5175 7/6 2N5176		14/6 ASY86 12/6 ASZ20	6/8 BCY71 7/6 BCY72	8/6 BFY24 3/6 BFY25	9/- BSW70 5/6 5/- D16P1 7/8			1861 6/- 1P29A 13/6
2N2369	3/6 2N3663	7/6 2N5176		16/6 ASZ21	8/6 BYZ10	5/8 BF Y26	4/- D16P2 8/-			IP30A 15/-
2N2369A	4/- 2N 3702	3/6 2N5245	12/6 40467.A	14/6 AUY10	30/- BCZ11	7/6 BFY29		NKT237	7/- OC20 15/- T	
2N2410 2N2483	8/6 2N3703	4/8 2N5246		14/6 BC107	3/- BD116	22/6				
2N2484	5/6 2N3704 6/6 2N3705	4/6 2N5249 4/- 2N5249	13/6 AC107 A 13/6 AC117	6/- BC108 12/- BC109	3/- BD121 3/- BD123	13/- 16/6 TERM	S, CASH WITH C	RDER	DNLY. POST AND	PACKING
2N2539	4/8 2N3706	4/6 2N5265	65/- AC126	4/~ BC113	5/6 BD124	12/-	PAYABLE ON O	RDERS	UP TO £6. AFTER T	HATFREE
2N2540	4/6 2N3707	4/- 2N5266	55/- AC127	5/- BC114	7/6 BD131	19/6	EXCE	P C.R.T	'.'s. ADD 6d, PER IT	EM P. & P.

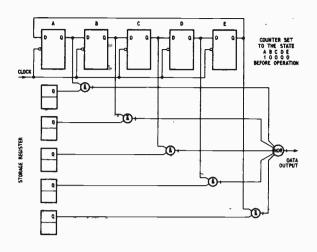


Fig. 8.3. Unitary or ring counter

this case there is no need for a common clear input, as any residual data in the register is "overwritten" by the input data.

Perhaps it would be as well to mention here that it is also possible to perform the parallel-in/serial-out function using the synchronous flip-flop inputs, but this does require extra gating to allow the D input to be connected either to the input data, or the preceding stage. A control line to order the register to "enter data" or "shift data" would also be necessary.

This winds up the subject of shift register construction and operation, but before leaving them, have a look at

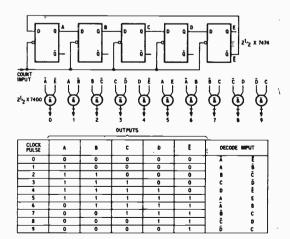


Fig. 8.4. Johnson decade counter with decoding

some uses of these registers, apart from simple data storage.

RING COUNTER

Several types of counter can be built using a shift register, the simplest being the "unitary counter" or commutator. In this application the register is set, by means of the asynchronous inputs to the state $100000\ldots$; that is, a 1 in the first stage and zeros in all the others. The output is connected back to the input. On receipt of clock pulses, the 1 in the first stage is propagated down the register, round the end and back into the first stage again.

This process gives rise to another name for it, the "ring-counter", as all the stages of the register form a complete loop. These counters need a separate stage for each of the required counter states, but they have the advantage that no gates are necessary to decode a particular state.

A typical application of this kind of counter is shown in Fig. 8.3. Here the 1 travelling round the counter is used to enable each of the five NAND gates in turn, the other inputs of which are connected to a storage register. The outputs of the NAND gates are fed to a NOR gate, to convert the parallel data stored in the parallel register into serial form; the output is taken from the output of the NOR gate. If a binary counter is used in this position, decoding gates would be necessary.

TWISTED RING COUNTER

A similar sort of arrangement is used to construct a "Johnson", or "twisted ring" counter, only in this case the \overline{Q} output of the final stage is fed back to the input, not the Q output as before. These counters require only half as many stages as the unitary counters of the same cycle length, and do not normally need to be set to any special starting state, although this depends on the cycle length employed.

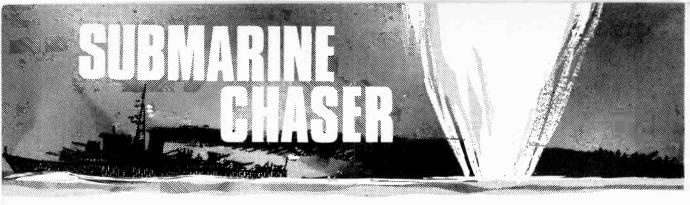
Their main advantages over binary counters are that they are synchronous and also any state, no matter how long the cycle length, can be decoded with only a 2-input gate. A typical application is shown in Fig. 8.4, a decade (divide by ten) counter, with decoding to decimal so that it could be used in frequency counters or similar equipment, where the outputs are used to drive "Nixie" indicator tubes.

TTL MEDIUM SCALE INTEGRATION

When the manufacturers of logic integrated circuits were in full volume production of gate and flip-flop families, and the "bugs" were ironed out of the manufacturing process, so that a high yield was being obtained from each slice of silicon, it was a relatively straightforward process to increase the amount of logic contained in each package. The results of this second generation of i.c. manufacture are now readily available, under the name "medium scale integration" (MSI) or "complex function devices".

The logic family which has by far the greatest range of these is TTL.

Next month's article will consider the advantages of medium scale integration (MS1), in which several logic circuits are contained in one package, such as is used in the "Digi-Clock".



Another war game by D. R. DAINES.

This can be added to Operation Seasearch, published in December 1970, or built on its own

Submarine Chaser is very different from Operation Seasearch (December 1970 issue), but because both games utilise co-ordinate switching the opportunity has been taken to enclose both in the same unit, the game to be played being selected by a two-way four-pole rotary switch. As before we have North/South and East/West co-ordinates but with the added dimension of depth. To the submarine player, the depth represents the actual depth he is supposed to be; to the destroyer player the depth represents that at which his depth charges are set to explode.

By far the greater difference between this and last month's game, however, is in the method of search. Hunting the raider in Operation Seasearch was very largely blind; Submarine Chaser uses a pseudo Asdic.

ASDIC

It is fair to say that the invention of asdic revolutionised anti-submarine warfare in World War 2, and the present game arose out of a desire to simulate as closely as possible the conditions arising out of the use of it, in game form. In real life, a searching vessel emits a high-frequency sound at regular intervals. The sound wave travels underwater at a regular speed dependent upon the temperature and salinity of the water. If the sound wave strikes a solid object it is reflected back and detected by listening gear. Obviously,

the time taken for the sound wave to travel the double journey is a fair indication of distance. If the reflecting body is a submarine, a series of readings taken over a period will enable course and speed to be determined.

The asdic used in this game works on a completely different principle, but is utilised in the same way and gives a convincing impression of genuine asdic. The difference of position between the submarine and the destroyer is represented by electrical resistance which affects the rate of a slow-running multivibrator. The multivibrator gates a high frequency audio tone which is monitored by both players through earpieces. The closer together the two vessels are supposed to be, the faster is the repetition rate. Means are provided whereby each player may obtain a "fix" on the position of the other.

ASDIC PRINTED CIRCUIT BOARD

The asdic circuit is mounted on Veroboard, and comprises nine transistors (Fig. 1). Transistors TR1 and TR2 together comprise a fast-running multivibrator giving a high frequency square wave output taken off through D31. The variable clock circuit is formed by TR3 and TR4. The base voltage of TR4 is varied through a series of resistors shown in Fig. 2 (R18 to R27). The output is taken through D30, which, together with D31 and R7 comprises the gate.

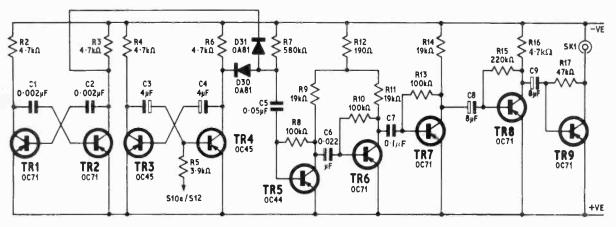


Fig. 1. Circuit diagram of the asdic board used in the Submarine Chaser game

The signal from TR2 will not pass forward unless a pulse is also present from TR4. Capacitor C5 is a d.c. de-coupler feeding the simple amplifier formed by TR5 to TR9. Final output from TR9 is fed to a miniature jack socket (SK1) into which a crystal earpiece may be plugged. This is situated at the side of the unit, between the two players.

DIRECTION FINDING

Referring briefly to Operation Seasearch, switches S5 and S6 controlled the horizontal co-ordinates of the destroyer. Here they do so again, but whereas switches S7 and S8 controlled the cruiser, S7 must now control the depth of depthcharges and S8 becomes redundant. Therefore the connecting link between S7 and S8 must be disconnected at "X".

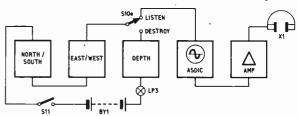
In a similar way, switches S3 and S4 originally controlled the position of the supply ship. Switch S3 must now control the submarine depth and S4 becomes redundant. The two depth control switches S3 and S7 therefore work together and since this is a third dimension, extra wiring is called for here as well as an extra wafer on each; Fig. 2 will establish the idea.

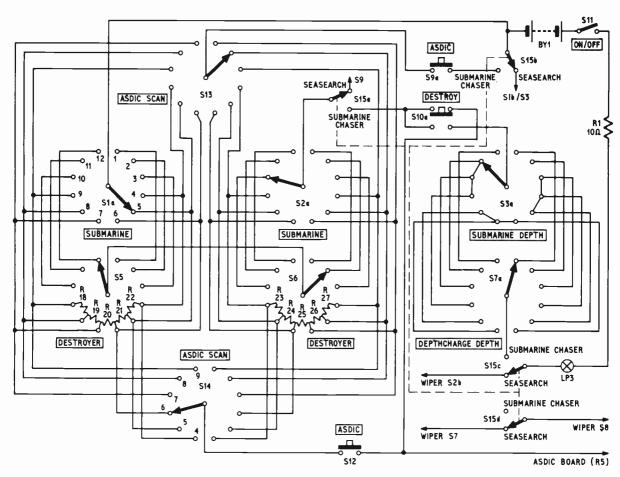
Fig. 2a. Block diagram of Submarine Chaser

Fig. 2b. Wiring diagram of the switching arrangements for Submarine Chaser. If only this game is to be built, switch S15 can be omitted and this diagram and Fig. I then give the complete circuit

It will be realised that what is required for accurate direction finding of the opponent is a method of sampling the various co-ordinate lines. If this could be done, the one that gives the fastest repetition rate on the asdic will be the one which by-passes all the resistors and hence the one which corresponds with the position of the opponent's switch. If this is done with the North/South lines and the East/West lines, a very accurate "fix" can be achieved; Fig. 2 illustrates the method—the sampling switch is \$14. As this switch passes through the left half of its sweep, it progressively by-passes resistors R18 to R22. When it coincides with the position of switch Sla (shown as position 5) the voltage applied to the asdic board will be at maximum, giving the fastest repetition rate. The player will therefore have detected the position of switch Sla.

In the right half of the sweep, the sampling switch will detect the position of switch S6, which is the player's own. This half of the sweep is therefore used by the





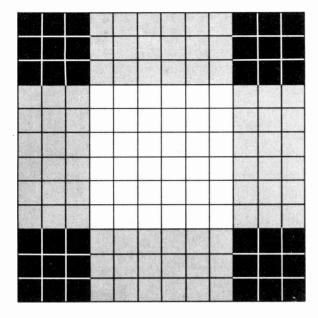


Fig. 3. Asdic detection pattern; white area—total detection; shaded area—partial detection; black area—no detection

opponent. It will be seen that two sampling switches are needed, the second is \$13, which will detect switches \$2a and \$5. In use, the players in turn will use both switches but at opposite parts of the sweep. For convenience, the two halves of each sweep are given a dab of colour; red and blue corresponding to the Redland or Blueland player.

The sampling switches do not give a total fix, but only sample the centre six lines in each direction. This gives a detection pattern as in Fig. 3, where the white areas denote total detection, the shaded areas partial detection, and the black areas no detection at all. The game was designed in this way partly on the grounds of economy and partly because it was felt that total detection overall would not lead to such an interesting game. Readers who would prefer total detection will be able to adapt the circuit, but of course four sampling switches would be required instead of two.

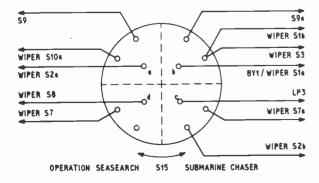


Fig. 4. Wiring of the game change switch \$15

CONSTRUCTION

Readers who built Operation Seasearch will have no difficulty if they installed the recommended switches. All wires are severed at the points marked "X" in the Seasearch diagram and taken to the game-change switch, which is a four pole changeover switch—not three pole. Then the wiring to switches S13 and S14 (Fig. 2) is added, as well as the wiring to the second wafers of S3 and S7. Constructors interested in this game only will find a complete parts list in this article; Fig. I and Fig. 2 form the complete circuit, game change switch S15 may be omitted if one game only is built.

COMPONENTS . . .

Resistors

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	easearch has been built) 10 100k Ω 11 19k Ω 12 190 Ω 13 100k Ω 14 19k Ω 15 220k Ω 16 4-7k Ω 17 47k Ω 18 to R27 2·2k Ω (10 off)				
Capacitors CI 0·002μF	.6 0·022μF				
C2 0.002µF	.7 0·1μF				
C3 4µF elect, I2V C	8 8μF elect. 12V 9 8μF elect. 12V				
C5 0.05μ F	.7 ομε elect. 12 v				
Switches					
For Submarine	Additional to				
Chaser only SI Ip 12w	Operation Seasearch				
S2 Ip I2w					
S3					
S6 Ip I2w					
S7 Ip 12w S9 Ip make push button					
S10 2p 2w push button	Ip 2w				
SII S.P.S.T. toggle SI2 Ip make push button	lp make				
S13 Ip 12w	Ip I2w				
S14 Ip I2w S15	lp 12w 4p 2w				
(S15 is a four pole two-way s	witch, not three pole as				
stated in Seasearch article) All rotary wafer switches exc	cept where stated				
	•				
Semiconductors TR1, 2 OC71 (2 off) TR3, 4 OC45 (2 off) TR5 OC44 TR6-9 OC71 (4 off) D30, 31 OA81 (2 off)					
,					
Miscellaneous SKI Miniature jack socket LP3 6·3V 0·06A (MES bulb, clip-on holder—not required if Seasearch has been built) BYI 9V battery type PP6 (not required if Seasearch has been built) Case components (see list in Dec. 70 issue) Three knobs with pointers Crystal earpiece lead and jack plug Veroboard 6B.A. fixings and spacers					

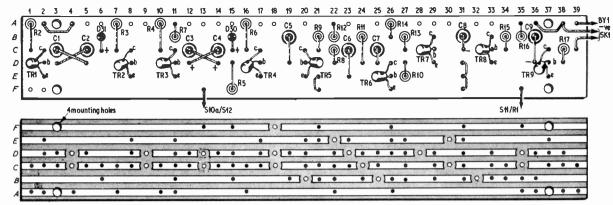
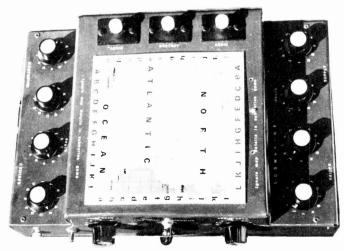


Fig. 5. Component layout and wiring of the asdic board

S10 is a two-pole change-over type, a d.p.d.t. switch may be used, but when playing, care must be taken to leave it in the off position; one pole is of course used for Operation Seasearch, and the other pole for this game. Switches S9 and S12 are labelled "Asdic" and S10 labelled "Destroy". In the off position S10 shunts the output from S2a to the asdic board. When depressed, the output goes to the depth wafers, switches S3a and S7a. If these are set at the correct depth lamp LP3 is lit and a hit registered. The asdic board is constructed as shown in Fig. 5 and fitted under the chassis near the lamps.

Switches S13, S14 and S15 are inserted through the three holes made in the side of the case described in the previous article. Push-button S12 is inserted in the spare hole on the top panel and SK1 can be sited in any position convenient to both players and the asdic board. The switches can be labelled as shown in Fig. 2.

Submarine Chaser is designed to be built in conjunction with Operation Seasearch but where the reader wishes to build Submarine Chaser alone it can be constructed in a case similar to that shown in the photographs. No map details are required for this game, the map—which is 7 inches square—is simply lettered to designate the co-ordinates. The case is constructed of aluminium and when bent to shape is pop rivited; the case shown measures $15 \times 9\frac{1}{2} \times 3\frac{1}{2}$ inches.



Lamps LP1, LP2 and LP3 are arranged under the map to illuminate corresponding numbers.

DEPTH

It will be seen that no Asdic detection is used for the destroyer player to determine depth. This is partly off-set by grouping the depth lines in the following way. The first position of the submarine switch (S3a) denotes that the sub is on the surface—this line is left on its own. The second line denotes periscope depth; the last denotes that the sub is sitting on the bottom; these two are also solo lines. The other nine positions are grouped in threes by shorting links on S3a (Fig. 2), which are optional and left to the constructor's discretion. It is felt that if the destroyer player has to guess the submarine depth it is asking too much for him to choose from 12 positions.

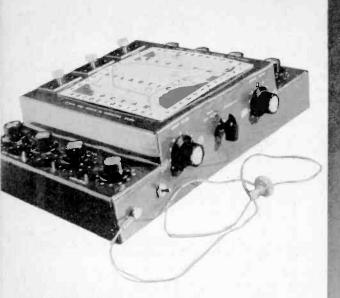
METHOD OF PLAY

The co-ordinates of the destroyer are adjusted so that he is at any peripheral square. Since the action is assumed to take place in a section of open sea, map details are totally ignored. A token is placed on the map to correspond with the destroyer's position. The submarine's position is adjusted to any one of the four central squares and at any depth he chooses. Only if he chooses to be on the surface must a token be placed because of course each ship can see the other. If he chooses depth two (periscope depth) the destroyer token remains but the submarine token is removed, whereas if he is any deeper both tokens are removed as neither can see the other. This simple rule of course applies throughout the game.

The destroyer moves first—or a coin is tossed. The destroyer moves a knight's move of two forward and one to the side, or one forward and two to the side. He may "drop" depth charges on each square through which he passes, he does this by pressing the "destroy" button. The depth charges may be adjusted for depth once each move.

The submarine moves minimum while submerged. That is, one square in any direction and one square up or down. Only while on the surface may he move two squares.

For the destroyer the game is thus quite simple—the destruction of the submarine, signalled as soon as the lamp is lit. For the submarine, life is a little more complicated. He can win the game either by escape or by sinking the destroyer. He escapes when he manages to reach the edge of the playing area, but with this one proviso—if the opponent can correctly guess the very first time to which edge he has gone, the game must continue for at least another ten moves.



TORPEDOES

The submarine can sink the destroyer by means of torpedoes. Only one is required. He may fire torpedoes only whilst on the surface or at periscope depth, but may not rise and fire in the same turn. A torpedo is fired when he is in line with the destroyer—a queen's move of any number of squares up, down, across, or diagonally. Here he simply claims the hit and reveals the positions of his controls.

VARIATIONS

For a really exciting game, try using a stopwatch or kitchen timer, allowing each player 30 seconds to listen and move. Better still, allow the first player one minute, but each succeeding move must be made in less time than the one preceding. Another variation would render it impossible for vessels to reverse direction in succeeding moves. The destroyer would then move in a series of loops, and the submarine would turn a maximum of 45 degrees on each move. The submarine might be allowed to sit on the bottom with engines off. Disconnect the Asdic and allow the destroyer three or four runs before giving up.

USING BOTH GAMES TOGETHER

The two games can be used together in a variety of ways. For example, the "Blue" player might run a convoy from Halifax to Britain, trying to avoid the submarine wolf-pack lying in wait. If contact is made the Red player scores one ship sunk before the destroyer escort is alerted. Play then transfers to the second game. If the sub escapes, play goes back to the first, and so on, until either the remnants of the convoy reaches Britain, or (say) five submarines are sunk. It might also be pointed out that the third dimension need not necessarily be depth. It might just as well be height. For submarines, read "bombers" and for asdic read radar. The two games together really have very wide scope, but perhaps enough has been said to get readers thinking for themselves.

Some readers might want to have their submarines rising to the surface in order to use deck guns as well as torpedoes, but here we are entering the very complicated world of naval gunnery. For this we really need the subject of a future article—a naval gunnery computer.

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ELECTRONICS

MARCH ISSUE
ON SALE FEBRUARY 18

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MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

I.C. POWER AMPLIFIER

We have recently received a comprehensive pamphlet describing four types of hybrid audio power amplifiers. These integrated circuit amplifiers require only the addition of a power supply, coupling capacitor and loudspeaker to form a high quality audio amplifier capable of giving 10, 20, 25 or 50 watts continuous output power, depending on the type.

Manufactured by Sanken Electric Co. Ltd. (Japan) and available through Photain Controls Ltd., Randalls Road, Leatherhead, Surrey, the amplifiers have the following brief specification:

Harmonic Distortion at Full Power Level 0.8 per cent maximum.

for S1-1010A (10W) and SH020B (20W), 0.5 per cent maximum

for \$1-1020A (25W) and \$1-1050A

Frequency range at 1W output 20Hz to 100kHz for all types. Price S1-1010A—£5, S1-1020B—£7, S1-1020A—£8, S1-1050A—£11.

The amplifiers must be driven from a preamplifier or other source giving approximately 1V audio output to the amplifier. A feedback resistor is incorporated to give a voltage gain of about 30dB and the circuits will withstand an output short circuit for more than 5 seconds.

The modules are intended for use in hi-fi, public address and musical instrument applications, and should prove excellent due to their small size and high output power.

COMPONENT SPARES

Many readers like to carry out their own repairs to their television receivers but often find great difficulty in replacing components.

We have been informed that the firm of Claygate Electronics specialise in radio and television replacement components and as a result of recent expansion plans are now able to supply readers with any of their large range of components in small quantities.

As a result of the expansion they are now approved stockists for: Plessey, Hunts, ITT, Lemco, Egen Electric, Erie, Morganite, Newmarket, Multicore and Solderstat components. For small items like resistors and capacitors they can only supply a minimum number of five components. But for larger items they are prepared to supply "one off's".

At the time of going to press they were preparing to publish a catalogue and details and further information can be obtained from Claygate Electronics Ltd., 2, Stoke Newington High Street, London, N.18.

IRON ACCESSORIES

New from Solderstat (manufacturers of the Elremco-Wolf range of soldering tools) are a snap on iron transit cover and a universal iron stand. The transit cover is for use with the firm's MS and HMS series of miniature and heavy duty miniature soldering irons. This inexpensive accessory is particularly useful where soldering irons are used for servicing and maintenance work, since it allows the user to pack away the iron without waiting for it to cool down;



Group of television components available from Claygate Electronics

for this reason the transit cover has been included in the new Solderstat 12 volt motorist pack.

Suitable for the same range of irons as the transit cover, the universal stand is a die cast aluminium alloy stand that can either be fixed to a vertical or horizontal surface. The stand contains a bit cleaning pad, is finished in stove enamel and retails at around 27s (£1·35).

MULTI-PURPOSE PLIER

A useful tool for the workshop is the Hunter 55 multi-purpose plier that can cut, strip and crimp wires, now being marketed by Henri Picard and Frere Ltd.

A serrated edge between the handles and the plier joint has six notches in graduated standard sizes to strip wires. Just between the serrated edge and the pivot joint the handles are sharpened to form a cutting edge for wire trimming.

The standard corrugated plier snout is extra long and has, close to the joint, a pair of specially designed shapes for crimping wires together.

The price of the Hunter 55 is 21s (£1.05) and details of local stockists can be obtained from Henri Picard & Frere Ltd., 34 Furnival Street, London, E.C.4.



Meet the ladies...

Why are there not *more* women in the electronics industry? It is undoubtedly one of the most popular branches of engineering for women, partly because it is a profession which can be applied in many widely differing fields; partly because it is a relatively new science with little tradition attached; and partly because the Second World War introduced many women into the vagaries of electronics. Yet only one engineer in the U.K. out of every 500 is a woman.

Perhaps some may think that girls don't have the capability, but this is far from the truth. Girls in other countries take up engineering as a career in far greater numbers, so why not British girls. It can't be lack of opportunity. There is a strong need for good engineers today, and Universities and Colleges up and down the country, offer places to suitably qualified girl students.

It seems that, in too many cases, girls, parents and teachers don't even consider electronics as a possible career for a girl. How many girls are brought up in such a way that, any innate interest in what is considered as boys' games and hobbies, is discouraged from a very early age. At school, girls are encouraged to take domestic science and biology rather than maths or physics. But in spite of all this, women have shown that they can be just as good as the men in electronics, if given the training and the opportunity.

There are organisations that do try to further the aims and interests of women in engineering, and especially in the electronics field. More about this later, but first let us look quickly at some typical examples.

ELSIE: INDUSTRIAL AUTOMATION

Elsie's favourite subjects at school were maths and physics. After passing her G.C.E. "O" levels she took a post as Laboratory Assistant at a large local electronics factory, and studied electrical engineering on a part-time day release basis at the local technical college.

She worked first in the Test Department where she learned to use a wide variety of measuring and test instruments, and went on to designing and building special test equipment, under supervision of course.

Later she worked as one of a team of engineers on the digital control system for a satellite communications station, and as her interest in digital work increased she started to specialise in digital data transmission systems. Later she became a Contracts Engineer, responsible for more than one project, and discussing customers' problems, finding the solutions, and evolving detailed system specifications.

Now she has moved into industrial automation where she is Head of the Data Transmission Group, responsible for the profitability of all contracts within her Group and for the day-to-day supervision of 17 design and commissioning engineers.

ANNE: MICROWAVE ENGINEERING

Anne graduated in physics but now works as a microwave engineer in an industrial research laboratory. Although her physics course covered the fundamentals, Anne was very unfamiliar with the practical aspects of microwave engineering.

However, she soon gained experience of using microwave instruments and applying microwave measuring techniques, and after a year or so was given a small project of her own, to develop a microwave Colometer for measuring microwave power. She has been given increasing responsibility involving the direction of junior engineers, the planning and costing of her work and liaison with the customer.

WOMEN IN
ELECTRONICS

By Dr. Elizabeth Laverick

PhD., F.I.E.E., F.Inst.P., S.M.I.E.E.E.





Looking at the spectrum of a microwave solid state oscillator (Elliott Bros. (London) Ltd)



Another application of electronics very much to the fore nowadays is associated with computers, the design of computers and the use of computers in the business world, i.e. the scientific world, solving problems and in automation.

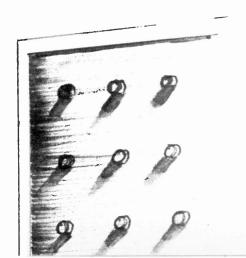
Pat joined an electronics firm at the age of 18 when they offered to sponsor her for a four year sandwich course in Applied Physics at City University. She worked for one year before her course started, and then spent alternate six month periods at College and at the firm, gaining practical experience in laboratory applications.

On graduating she decided to go in for programming, and she joined a project team in the Computing Research Laboratory, investigating the feasibility of computer aided design, in particular, the automatic production of a printed circuit master from a logic diagram.

SUSAN: COMPUTER AIDED DESIGN

Susan, too, works in computing. Unlike Pat she went for a full-time degree at Cambridge where she qualified as a physicist. Equipped with a degree, she moved into the computing industry. She became a project leader on computer aided design.

Women can also be found in production and in sales associated with electronics, the latter area involving much travel and liaison with customers.





Setting up a problem on an analogue computer

THE WOMEN'S ENGINEERING SOCIETY

In the light of the success which these women have made as electronic engineers, what can be done to encourage more girls to take this up as a career?

The Women's Engineering Society (which celebrated its fiftieth anniversary last year) does a considerable amount of voluntary work in this direction. The Society is a group of women with a common interest in a profession which is still generally considered to be a male preserve, and with a desire to help other girls and women who would like to be engaged in engineering, including electronics.

The coverage of the membership of the Society is large including every branch of professional engineering and the allied fields of metallurgy, physics, chemistry, mathematics and even personnel work. It covers also the fields of technical and scientific teaching, of technical writing and information services, and of engineering factory inspection.

The two most important aims of the Society are

(i) To promote the study and practice of engineering among women, and

(ii) To enable technical women to meet and correspond and to facilitate the exchange of ideas respecting the interests, training and employment of technical women and the publication and communication of information on such subjects.

It has been responsible for launching in 1923 the Women's Electrical Association to "interest the non-technical woman in electrical development". The name was soon changed to the "Electrical Association for Women", and as the E.A.W. it has grown exceedingly, now having several thousands of members throughout the country.

UNIVERSITY SCHOLARSHIPS

This Society, the Caroline Haslett Memorial Trust, is a charitable body whose aims are to provide scholarships, travelling exhibitions and other educational opportunities for women who are seeking or already pursuing careers in the electrical industry or in other related fields requiring qualifications in science, engineering or domestic science. Among other things the trust awards university scholarships to girls in science, engineering and mathematics.

The Society maintains a list of engineering companies willing to train and employ women. A booklet on the

training of women for engineering under the title "Training and Opportunities for Women in Engineering", is available from the Society's offices.

CAREERS ADVISORY COMMITTEE

The Society is actively engaged in careers work, taking part in conferences and exhibitions, contributing to careers conventions, giving talks at schools, answering careers enquiries, and giving advice and information on request to parents, careers teachers, Youth Employment Officers, and anyone who requires some guidance.

As a result of increasing government and public interest in women engineers, the Society has set up a Careers Advisory Committee as a Working Party to co-ordinate the Society's interests and activities in the fields of education, training and careers advice.

CAREER AND MARRIAGE

Why, you may ask, should girls train for a career when they will almost certainly marry, and have a family? Well, there are several reasons. Quite apart from the fact that all young people, irrespective of sex, should be encouraged to develop their capabilities to the full, it is worth knowing that already more than one third of the jobs in this country are held by women. Statistics show that the average young lady of the 1970's will have finished having her family by the time she is thirty, leaving another thirty years in which to fulfil herself in other directions. It is also worth remembering that many semi-skilled jobs are being taken over slowly but surely by automation.

All of the four girls described in this article married early in their careers, and have managed to find time for hobbies, home and husband (not necessarily in

that order!) as well as their careers.

It is quite surprising how many women have entered electronic engineering through a maths or physics degree, or have graduated or otherwise qualified

through alternative training schemes.

Electronics as a career can be hard work but the rewards are good in all senses. There are equal opportunities in the majority of firms today—and equal pay—so if you have a daughter who wants to help you when you're building that latest circuit, don't discourage her—you may have a budding electronics engineer in the family after all.

The following organisations may be approached for further information appropriate to this article:

The Women's Engineering Society, and The Electrical Association for Women, 25 Foubert's Place, London, W.I.

Central Office of Information, Hercules Road, London, S.E.I.

Council of Engineering Institutions, 2 Little Smith Street, London, S.W.I.

The Careers Centre, 42 Conduit Street, London, W I

Women's Employment Federation, 251 Brompton Road, London, S.W.3.

Student Advisory Centre, 44 Albion Street, London, W.2.

NEWS BRIEFS

Radio Controlled Lunar Vehicle

THE Luna-17 automatic station soft landed on the moon in the area of the Sea of Rains on November 17. Installed on board was a self-propelled moon vehicle Lunokhod-1. This vehicle has made short excursions over the moon's surface under direct radio control from the Russian earth station, where a crew of six technicians "drive" the vehicle and monitor the data transmitted from the many scientific devices carried aboard.

A programme of scientific studies and tests is being carried out by this automatic station, including investigation of cosmic rays, panoramic survey of the terrain, analysis of the chemical and physical properties of the lunar surface soil and rock, and the measurement of

different parameters inside the vehicle.

In December, following a 2-week hibernation during the lunar night, *Lunokhod-1* resumed exploration activities upon command from earth control.

100 Years of Telecommunications in the City

SIR Peter Studd, in entering his year as Lord Mayor of the City of London, has chosen Communications as a theme for his year of office. This is an appropriate choice, since 1970 marked the centenary of the Post Office responsibility for telecommunications. In 1870, the Post Office took over the inland telegraph system. Nine years later the first telephone exchange in Britain was opened in the City of London. There were 13 names in the first telephone directory.

Video Recording

VIDEO recording is a fast moving business at the present time and we are constantly receiving news of new products, processes and business agreements. In our December issue we published an *Electronorama* feature on this subject and since then we have received news of a portable recorder from Akai—the VT100—and two new licence agreements made by the E.V.R. Partnership.

The V100 recorder is said to be the first fully portable record/playback video recorder and it uses \$\frac{1}{4}\$ inch tape. The Rank Organisation are marketing the complete Akai system consisting of the VT100 recorder, a camera with 4:1 zoom lens, clip on 3 inch monitor and batteries. The complete system costs £568 and a \$\frac{1}{4}\$ inch tape giving 20 minutes recording time costs £4. The VT100 is intended for non-domestic use and is shown below.

The E.V.R. Partnership have recently announced two licence agreements, one with Mitsubishi Electric of Japan for the manufacture and distribution of EVR teleplayers internationally (with the present exception of the USA and Canada), and a similar agreement with Hitachi Ltd. of Tokyo. The agreement with Hitachi was concluded first and preceded the Mitsubishi agreement by less than one week.

These new agreements with giants in the powerful Japanese electronics industry add immensely to the international strength of the EVR organisation. In Great Britain, Rank Bush Murphy has announced that it will bring its new colour teleplayer into full production early in 1971.





THE MUSIC LOVER'S ALL-IN-ONE GRAMOPHONE BOOK

By Vivian Capel
Published by Focal Press Ltd.
196 pages, 7in × 43in. Price 15s (75p)

WITH a title brief like this the author has had to bend over backwards to compound an embracing 'all' in one slim volume. Whether he succeeds depends on the degree of technical sophistication of the music lover; certainly for the man who is a prospective equipment purchaser and who wishes to be led painlessly through the edge of the hi-fi jungle, this is a good buy.

From an opening chapter on the price versus quality aspect of reproducing equipment, the author goes on to examine sound and what constitutes music.

The translation of sound to disc, or the recording process is dealt with briefly with a succeeding chapter on simple stereo technicalities.

A comprehensive chapter on pickups and gramophone mechanics is simple and instructive, as is the chapter on amplifiers which also clarifies the bogey of specifications.

Loudspeakers and enclosures have a chapter to themselves and the advantages of earphones are discussed.

The remaining half of the book covers choice of equipment, improvements to existing equipment, practical hints on wiring, record selection and equipment maintenance.

Apart from a chapter describing the instrument members of the orchestra, which seemed rather misplaced in the context, I found this book both interesting and instructive.

G.G.

RADIO AND AUDIO SERVICING HANDBOOK

By Gordon J. King Published by Newnes-Butterworths 283 pages 10 in \times 6 $\frac{1}{2}$ in. Price 60s (£3.00)

The second edition of this established work contains most of the original material published in the 1965 and 1967 editions, but includes up-dated information relevant to recent design techniques. These include field effect transistors, integrated circuits, stereo broadcasting and reception, stereo amplifiers, tuner amplifiers, compact music systems, cassette recorders.

A great deal of general information and advice is given in a straightforward manner. Some sections on valve equipment have been retained because of the large quantity still in everyday domestic use.

Although transistor equipment is usually very reliable, there are occasions when an understanding of principles goes a long way to avoid accidental damage during servicing, the most likely cases being during the insertion of semiconductors and testing. Several examples of different types of circuit are given to explain these principles and assist with fault location.

۸.A.C.

TUNERS AND AMPLIFIERS

By John Earl Published by Fountain Press Ltd. 184 pages 8½in × 5½in. Price 42s (£2.10)

This is the first of a new series in the Fountain "How to Choose and Use" range of books. The author of this one uses his extensive background in the testing and description of commercial hi fi equipment to bring home to the hi fi enthusiast recent trends in equipment design in a very, readable manner.

Technical descriptions are given in very plain language, so that the reader can attempt to unravel the many

expressions appropriate to the subject.

Circuit design has progressed quite considerably during the past five years or so. In fact, much of the criticism levelled at transistor tuners and amplifiers in the past can be answered in the newest designs to be made available. Examples are the improved performance and reliability from the use of integrated circuits, varicap diodes for tuning, field effect transistors for front end amplification, inter-station muting, ceramic "crystal" i.f. resonators, overload protection circuits.

The merits of these and alternative designs are described in some detail. For those readers who have some background in audio and radio techniques, this book will help to up-date the image of quality sound reproduction, where it may have previously become prejudiced by old well-established valve equipment.

M.A.C.

DICTIONARY OF TELECOMMUNICATIONS

By R. A. Bones Published by Newnes-Butterworths 200 pages. 7½in × 5in. Price 45s (£2.25)

As stated in the title, this dictionary is concerned basically with telecommunications and only relates to associated electronic fields such as radio broadcasting and television where these fields overlap. However, taking into account the specified field of the book, one gets the impression that there can be very few terms not listed or adequately described by Mr Bones. In his preface he states that he gives the most recent terminology and that at the time of going to press the dictionary was as up to date as possible, and this is evident from the text.

Terms consisting of two or more words are adequately cross referenced and the descriptions given are concise if a little basic in some cases. No lengthy descriptions on operation of components or instruments are given, simply a description of the item and its function. A comprehensive and useful book for students and engineers alike.

M.K.

RADIO AND TELEVISION YEAR BOOK 1970/71

Edited by Eric Ickinger
Published by IPC Electrical-Electronic Year
Books Ltd.
226 pages 83 in × 51 in Price 20s (41.00)

226 pages $8\frac{3}{4}$ in \times $5\frac{1}{2}$ in. Price 20s (£1.00)

TELEVISION has been included in the title of this, the third edition, colour and monochrome receivers being listed. Special attention is given to the "unit audio" type of system up to about £150. An introductory article on this subject is given at the beginning of the book. These and other equipments are listed with specifications and prices on the same lines as in the Hi Fi Year Book, and include radio and television receivers, tape recorders and record players.

Registration of the control of the c

N this, the second and final article, the construction of the various sub-assemblies, setting up and final calibration of the locator will be dealt with.

TRANSMITTER CIRCUIT PANEL

The layout and underside connections of the transmitter panel is shown in Fig. 9. Here a 4·1in by 1·7in Veroboard is bolted to a 3in by 1·8in sheet of 16 s.w.g. aluminium, which acts as a heat sink for TR7, and a mount for the transformer T1.

The complete transmitter panel assembly is bolted to the baseplate of the aluminium box by means of screws and stand-off spacers; this method of mounting also applies to the receiver circuit panels.

Drill holes to accept mounting screws for T1, and TR7. The two holes, where the circuit board bolts to the heat sink, should be reinforced with a solder tag soldered to the copper strip.

TRANSFORMER ASSEMBLY

To prepare transformer T1, first remove the bobbin from inside the pot core by undoing the four clamp screws, taking care not to drop or otherwise damage the ferrite pot. Wind on by hand two layers (15 turns) of 20 s.w.g. enamelled copper wire for L2, and secure with a layer of plastics insulating tape. Slip red and blue sleeving onto the L2 leads, as shown in Fig. 10a.

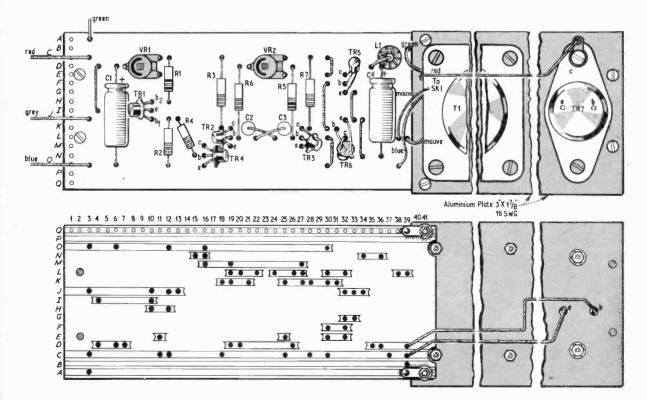
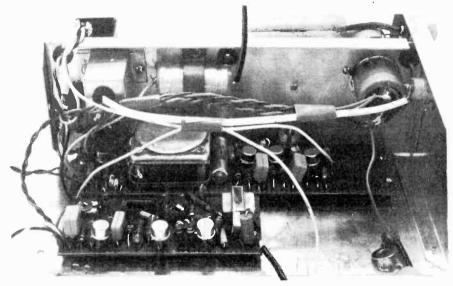


Fig. 9. Component layout and underside connections for transmitter panel

LOCATOR By D. Bollen



View of the sonic locator interior showing the tuned amplifier panel and the decoder, the latter in the foreground. The transmitter panel is screened by the metal partition and so prevents circuit interaction. This can be seen more clearly in Fig. 13

L3 consists of four layers of the same wire (30 turns) similarly secured with tape, and with mauve and green sleeving on the leads.

Bolt the assembled transformer to the heat sink, and mount TR7 complete with mica insulating washer, spacers, and collector solder tag.

When components have been assembled on the Veroboard, scrape the enamel off the ends of T1 leads, tin them, and insert in appropriate holes in the circuit board, then bolt the board to the heat sink and complete all wiring.

PRELIMINARY TRANSMITTER TESTS

Connect a small 3 ohm loudspeaker to the green wire from the transmitter circuit panel and the mauve wire from T1. Place a non-polarised capacitor of about 4μ F in parallel with the loudspeaker.

Rotate VR1 and VR2 to the mid-track position, then join red and blue wires to a 12V battery. If the transmitter is working correctly, regular, loud clicks should come from the loudspeaker.

To check transmitter output, measure the peak to peak amplitude of the output at the loudspeaker with an oscilloscope, and convert the result to r.m.s.

If an oscilloscope is not available, temporarily short the collector and emitter of TR4. Connect an a.c. voltmeter across the speaker, and re-connect the battery leads briefly. If all is well, an output in the region of 10-15V r.m.s. will be obtained.

Bearing in mind that the circuit is intended for pulsed operation, do not leave the battery connected for more than a few seconds while TR4 is shorted, otherwise the loudspeaker and output transistor could overheat.

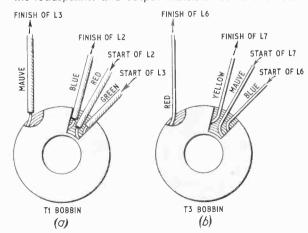


Fig. 10. (a) Coloured sleeves applied to T1 leads for identification; (b) sleeves applied to T3

TUNED AMPLIFIER CIRCUIT PANEL

Drill mounting holes in the 6.9in by 1.6in amplifier Veroboard panel, according to Fig. 11.

An easy method of winding transformer T3 bobbin is as follows. A mandrel to take the bobbin is made by cutting a short length of dowel and inserting a twist drill tightly in its centre. If the dowel is a sloppy fit in the bobbin hole, it can be built up with Selotape.

With the mandrel twist drill gripped in the chuck of a hand-drill, which is mounted horizontally in a vice, L6 and L7 turns can be wound on quickly.

The fine 40 s.w.g. enamelled wire used for the T3 windings needs to be terminated by soldering on leads

VR5 and C11, and orange and blue wires to the screened cable of a 50 kilohm output impedance moving coil microphone. Note that the cable outer screen should connect to the blue wire.

Modifications to the microphone will be described later in the article.

Green and grey wires are left disconnected during the following tests. First, place a milliammeter in series with the red wire and the positive terminal of a 12V battery, then touch the remaining blue wire to the negative battery terminal. When assured that the amplifier current consumption is around 4mA, the milliammeter can be removed.

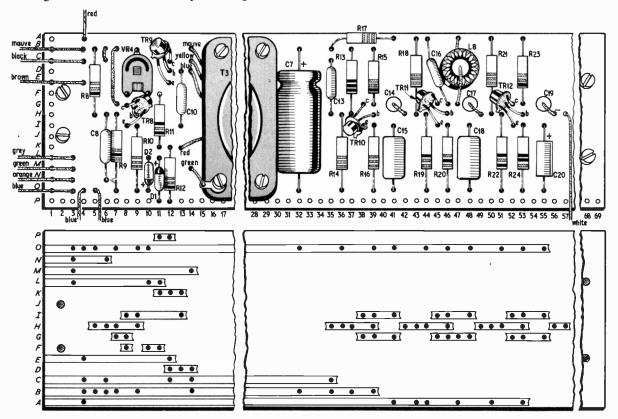


Fig. 11. Component layout and underside connections for tuned amplifier panel

of thin, multi-stranded (7/40) plastics covered wire; the joints thus made should be insulated with small pieces of plastics tape.

Starting with a mauve lead, wind on as evenly as possible 500 turns of 40 s.w.g. wire for L7. Finish off with a yellow lead, and secure the winding with tape.

L6 starts with a blue lead and consists of 100 turns of 40 s.w.g. wire wound in the same direction as L7, and is then terminated with a red lead. Bobbin details for T3 are given in Fig. 10b.

After gluing the completed transformer to the Veroboard, proceed with the assembly of the other components.

PRELIMINARY TUNED AMPLIFIER TESTS

For the purposes of the following tests, the tuned amplifier circuit panel can be laid on a table top with the associated controls grouped around it.

Referring to Fig. 13, solder black and mauve circuit panel wires to TC1 and C12; blue and brown wires to

USING THE TELEVISION SET

Position the microphone close to a 405 line television set, first making sure that the amplifier panel is some distance away to prevent stray inductive pick up from the TV line transformer.

Clip an a.c. voltmeter onto the white amplifier output lead and to battery negative, and re-couple the red lead to battery positive. With VR5 at half-track the a.c. voltmeter should read zero.

If there is a steady meter reading this will be caused by tuned amplifier instability. To minimise unwanted stray feedback, rearrange the meter leads and microphone cable, and slightly reduce the VR5 setting.

Now switch on the TV set and, with the volume control at minimum, obtain a steady picture. A 10·125kHz sound signal, picked up from the line transformer by the microphone, should now cause the a.c. voltmeter to read somewhere in the region of 1-4V. Tune the amplifier by adjustment of TC1 for a peak in output voltage.

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noise levels are low. High starting torque enables relative high inertia loads to be driven up to 60z/in. Available in the following speeds and ranges: 240 ° 50Hz, 1½ r.p.m., ½ r.p.m., ½ r.p.m., 1/10 r.p.m., 1/12 r.p.m., 1/20 r.p.m., 1/46 r.p.m., 1/360 r.p.m., 25/- each. P. & P. 5/-



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4-16

3-15 V

26-37 V

Adjustable 12V

. 900 V

153

12V

20V

6V }

94V

481

48\

350V or 250V

190-350

6-3V-0-6-3V

6V

at 30 V

150mA

300mA

20A 12A

8A 16A

20A

AC 5A

· > A

 4Λ

60

500mA

250mA

940

240

240

110

110

240

240

240 Stabilised Adjustable

240 Stabilised

210 Stabilised

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Similar to above type MD 83, 28V 1/20 r.p.m., 1/60 r.p.m., 1 r.p.m., 12V 1/20 r.p.m., 24V 1/10 r.p.m., 30V 1/12 r.p.m., 30/-, P. & P. 5/-.

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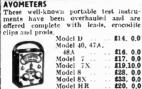
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to follow each other.

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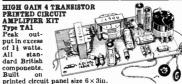
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As a double check, to make sure that there is no spurious oscillation from the unscreened tuned amplifier, and that the amplifier is really responding to the signal, alter the timebase frequency by adjustment of the TV line hold control, whereupon the whistle note will change and the amplifier output voltage should drop.

The tuned amplifier is now ready for final assembly and the flexible, coloured leads can be unsoldered from the potentiometers and trimmer capacitor. Avoid altering the TCl setting.

Make up the chassis and mark all panels for later identification, not forgetting the screen partition, then dismantle it completely.

Take the box baseplate and mark and drill mounting holes for the three circuit panels. Ensure that there will be sufficient clearance between the decoder panel and the crystal insert X2.

Fix the tuned amplifier and decoder circuit panels to the baseplate, with lockwashers under the mounting nuts, but leave the transmitter panel unmounted for the time being.

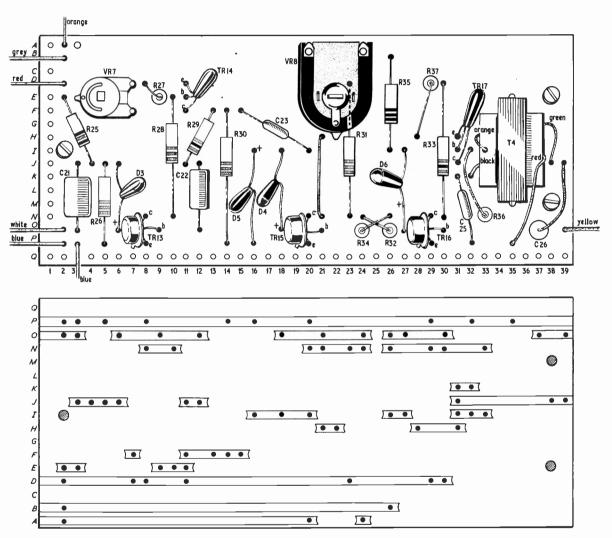


Fig. 12. Component layout and underboard wiring for decader panel

DECODER CIRCUIT PANEL

The decoder panel layout appears in Fig. 12, and construction of this unit is quite straightforward. Holes are drilled to accept mounting screws, and existing holes are enlarged to take VR8 and T4 tabs.

The finished decoder can only be tested after final assembly.

FINAL ASSEMBLY

Details of the internal arrangement of the chassis housing, the circuit panels and other components are given in Fig. 13.

Drill the front panel according to Fig. 14; if desired, an identically drilled plastics laminate faceplate can be glued to the front panel to enhance the finished appearance. Mount VR3, VR5, and VR6, also the meter, on the front panel. Glue a small square of loudspeaker grille material to the inside of the crystal insert front panel aperture, then glue X2 to the grille.

SCREEN PARTITION

Drilling details will not be given for the screen partition as the size of components used for T2, C5, C6, and C9 may vary.

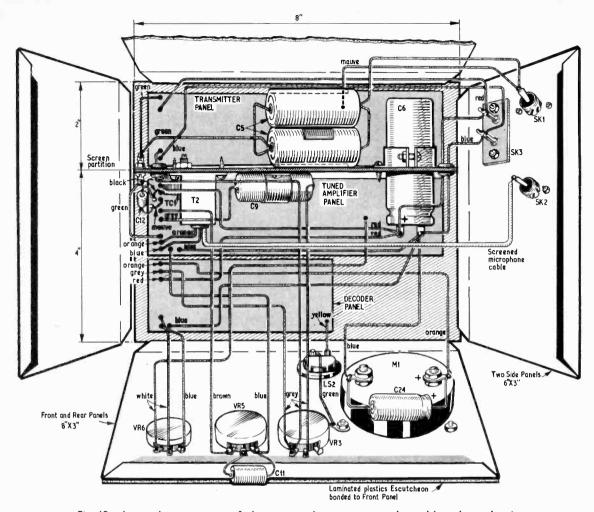


Fig. 13. Internal arrangement of plate mounted components and panel boards on chassis

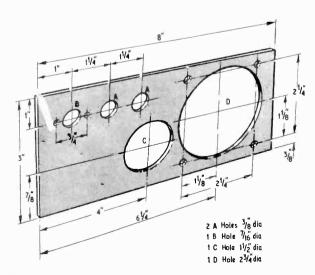


Fig. 14. Drilling details for front control panel

It is obviously a simple matter to find the best position for components on the partition when circuit panels and partition are in place on the baseplate; then the partition can be removed for drilling.

With the prototype, T2 was taken from inside a moving coil stick microphone (see Fig. 16), and was then enclosed in an old I.F. transformer can.

To obtain maximum transmitter output, C5 must be adjusted in value to suit individual loudspeaker resonances. A single $2\mu F$ capacitor can be mounted in the C5 position on the partition, and can be padded later by wiring another capacitor in parallel, as depicted in Fig. 13.

Mount the front panel, partition, transmitter circuit panel, and right-hand box side with sockets on the baseplate, then proceed with all interconnecting wiring. The remaining box side panels and top plate are left off until after the unit has been tested and calibrated.

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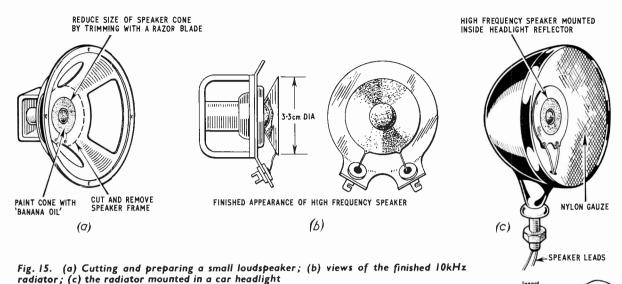
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TRANSMITTER LOUDSPEAKER

If there is a choice of small 3 ohm loudspeakers, select one that gives the loudest output when coupled to the sonic transmitter.

With a sharp razor blade or modelling knife, cut away the outer section of the loudspeaker cone (see Fig. 15a) taking care not to sever the pigtail leads leading to the voice coil. The remaining part of the cone, Fig. 15b, should be close to 3.3cm diameter—the wavelength of 10kHz sound—and is stiffened by applying two or three coats of modelmaker's banana oil.

The loudspeaker metal frame should also be cut away with tin snips or a hacksaw, but make sure that iron filings are not collected by the loudspeaker magnet.

A suitable mount for the high frequency loudspeaker is a car headlamp as shown in Fig. 15c. The headlamp reflector will not make a significant contribution to the loudspeaker directional characteristic but side and back radiation will be reduced if the headlamp interior is filled with acoustic wadding or felt.

Protection against small flying stones is afforded by nylon gauze across the front of the reflector, attached to the headlamp rim.

RECEIVER MICROPHONE

Fig. 16 shows how a conventional dynamic microphone can be converted for use with the Obstacle Locator. After completely dismantling the microphone, the rear of the "stick" is cut away. The microphone transformer is removed for use as T2.

Holes to take three screw eyes are drilled 120 degrees apart around the microphone casing, and a hole is also drilled to take the microphone cable.

Epoxy resin glue can be employed to retain the screw eyes, as well as the aluminium disc which is inserted to block off the opening in the end of the casing.

When re-assembling the microphone after soldering the screened cable to the insert terminals, fill the inside of the casing with plastic foam material.

HEADLAMP MOUNTING

The microphone is suspended at the focus of a parabolic headlamp reflector by rubber bands; facing inwards towards the back of the reflector as shown in Fig. 17. Other forms of mounting were tried, but the rubber band method gave better noise rejection.

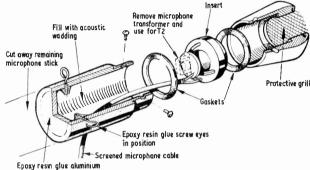
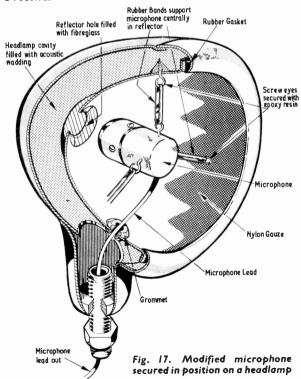


Fig. 16. Converting a dynamic stick microphone for use as a receiver

disc in end of case



Before preparing the headlamp, measure the distance from the bulb filament to the back of the reflector, to find the focal point. Fill the hole in the back of the reflector with a fibreglass compound, and sandpaper when dry to conform with the reflector contour.

Position the microphone diaphragm at the focal point of the reflector and mark the location of holes for the reflector screw eyes, opposite those on the microphone

casing, and in the same vertical plane.

Fix the screw eyes to the reflector and drill a hole to take the microphone cable, then attach the microphone

to the reflector with rubber bands.

As with the loudspeaker, nylon gauze covers the opening in the headlamp to protect the microphone. Finally, fill the inside of the headlamp with acoustic wadding.

It is difficult to fully waterproof both headlamps. without reducing efficiency, therefore, when the Obstacle Locator is not being used the headlamps should be covered with thick polythene bags.

SETTING UP

As a preliminary to setting up the Obstacle Locator, adjust VR1, VR2, and VR5 to a mid-track setting; VR3 to minimum resistance; VR4 and VR7 to maximum resistance; and rotate VR6 fully anti-clockwise.

Leaving loudspeaker and microphone plugs disconnected from SK1 and SK2, couple the power supply to SK3, making sure that the aluminium chassis is earthed either to the positive or negative supply rail, and switch on.

Set VR8 to give a full scale meter reading.

In the absence of a signal (VR6 fully anti-clockwise) full scale deflection of the meter needle indicates battery condition

With VR5 and VR6 rotated fully clockwise, an almost continuous note should be heard from the crystal insert X2 and the meter reading will drop to almost zero. Back off VR5 to just beyond the point where the note ceases and the meter again reads tull scale.

CALIBRATION

Find an open area of ground with a fairly flat surface, uncluttered by large stones and other objects. Position loudspeaker and microphone headlamps side by side, about 18in off the ground, and facing some large reflective object at exactly 20 feet distance.

Rotate VR6 fully anticlockwise, but do not alter any other settings. Connect up the loudspeaker cable to SK1, microphone cable to SK2, and power supply

to SK3, and switch on.

Advance VR6 slowly until a regular bleep note is heard from X2, and the meter reading drops to some-

Calibrate by means of VRI for an exact meter reading of 20.

No difficulty should be experienced in obtaining a response at 20 feet, even with the transmitter off tune. If an echo is not received, try connecting a pair of high impedance headphones across the track of VR6, to the tuned amplifier output. A regular click from the transmitter output will be clearly audible.

Now adjust tuning control VR2 and listen for additional echo clicks at a particular setting of VR2. If necessary, also trim TC1, VR7, and VR5 for a response.

SENSITIVITY ADJUSTMENT

The purpose of the next test is to establish optimum sensitivity. An oscilloscope can be coupled to the tuned amplifier output to display echo waveforms and

noise levels, but failing this, the following procedure should be adopted.

Set up loudspeaker and microphone 50 feet away from a large wall, in an area free from other echo

producing objects.

Switch on, then, with VR6 set fully clockwise, rotate VR7 until a response is obtained. The meter should now read 50 and the mark-space ratio of the bleep from X2 will be equal.

Back off VR6 to the point where the signal ceases. Now adjust VR2, VR7, and VR5 for maximum response at the lowest possible setting of VR6. Also try placing various capacitors in parallel with C5 to

bring up the transmitter sonic output.

It will be found that, when the loudspeaker and microphone are close to the ground, back-scatter echoes will be received, if the surface is at all rough, when VR3 is turned anti-clockwise. The range of back-scatter control presented by VR3 is fixed later by suitable adjustment of VR4.

Finally, see if a strong signal can be received from a large wall or a building at 95 feet distance; in this case the note from X2 will be of such short duration that it sounds like a click.

USING THE LOCATOR

In uncluttered conditions, where the equipment is working over a smooth area of water or tarmac, and the best possible response to small objects at near distances is desired, set VR4 to mid-track and advance VR3 until a suitable response is achieved.

Where there are numerous small objects in front of the loudspeaker transducer, VR3 should be left at

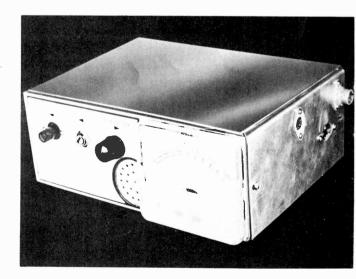
minimum resistance.

The only control likely to need adjustment under operating conditions is VR6. In difficult, built-up areas for example, VR6 will be set low, to avoid spurious echoes, but in more open situations a high setting of VR6 will give long range working.

When visibility is constantly changing, the equipment can be left ready on stand-by with VR6 rotated fully

anticlockwise.

If the Sonic Obstacle Locator is to be used at sea, adequate precautions must be taken to thoroughly moisture proof all aluminium parts against corrosion. including the interior of the microphone unit; this can be done with a varnish.



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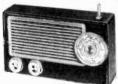


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G2/6 8/12V (REV) G3/7 100/25V	9d H2/2 64/2.SV 2/- H2/6A 24/275V	9d H5/3A 500/25V 1/- H5/6A 40/3V	2/- H7/3 25/12V 6d H7/4 25/25V	9d H7/13 75/15V 1/6 H7/14 100/4V	1/-
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H1/7 20/6V	6d]H3/10A 30/10V	6d H6/7 200/16V	1/6 H7/8 50/15V	1/6 H8/11A 2S0/12V	1/6
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52/1 6,000/30V	7/6 G4/1 300/700/320V	7/6 G5/4A 500/100V	3/- G6/9 60/200/300V	5/- H3/4 1,000/S0V	6/-
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53/2 200/200/350V	6/- G4/7A 40/40/450V	2/6 G6/1 12,000/15V	15/- G6/14 400/275V	3/- H3/9 100/275V	2/-
53/2A 200/200/100/350V	7/6 G4/11 2,000/25V	3/- G6/2 2,500/40/60V	7/6 H1/5 2,000/18V	3/- H3/13 16/16/375V	2/-
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53/13A 2,000/30V	5/- G5/2A 30,000/40V G5/3 35,000/15V	15/- G6/5A 1 600/80V	7/6 H2/9 16/16/450V	1/- H6/10 250/25V	1/6
	G5/3 35,000/15V G5/4 39,000/10V	15/- G6/6 1,000/60V 10/- G6/8 200/250V	6/- H2/10 1,000/100V 3/- H3/2 2,500/100V	7/6 H8/13 6,000/6V 7/6	4/-
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31/5 8/275V 31/5A 32/350V	1/- G2/13 100/50V 1/6 G4/3A 200/25V	1/- G4/10 350/25V 1/6 G6/1A 3,000/15V	2/- G6/12 1,000/12V 3/- H1/9A 50/150V	2/- H4/7A 32/32/275V 1/- H4/12 500/50V	2/6 2/-
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51/8A 16/350V	1/- G3/13 64/275V	2/- G6/4A 1.000/25V	2/6 H3/10 100/250V	2/- H5/3 500/25V (REV)	2/6
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33/6 100/250V 53/6A 50/50/350V	2/- G5/11 100/200/25V 2/- G5/12 100/20/10/350/20	2/- H2/5 100/100/100/27 50V 2/6 H2/6 50/275V	5V 2/6 H4/10 10/10/425V 1/6 H4/13 400/250V	1/6 H8/11 250/25V 3/- H8/12 3,000/6V	2/- 3/-
33/8A 100/25V, 100/12V	2/- G5/13 40/100/3SOV	2/6 H2/1 32/32/250V	1/6 H5/1 150/200V	2/- H8/I3A 100/25/200/25V	1/6
3/11 100/350V	1/6 G5/13A 40/40/40/40/350V	2/6 H2/1 32/32/250V 2/6 H2/12 50/50/150V	1/6	H3/11 150/200V	2/-
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42/12A 350/12V	I/- H5/I4A I,100/I0V	2/1 H6/14A 900/15V	1/- H8/I 1/350V	I/- H8/9 40/15	1/-
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By R. W. Coles Part 3

This month we give details of the alarm board construction, discuss the power supplies, and give the high voltage regulator board details.

CONSTRUCTION OF BOARD "B"

The wiring of the alarm board follows the same general principle as that employed with the clock board described last month. In this case there are a large number of discrete components and it must be admitted that wiring up is quite tricky because of this.

It is best to construct the regulator first and test its operation before attempting the alarm circuit; the connection diagram for this circuit is given in Fig. 13. Note that there are three breaks to be made in the printed copper power supply strips, so that these tracks can be used for other connections, and also that the wire to the 200V supply does not pass through the edge contacts.

In all there are two wires which leave the board in this way, due to the shortage of edge contacts on the 22-way version used in the prototype. If desired the DL109/44 type of "Dualine" card could be used to prevent this.

REGULATOR TESTS

To test the regulator it is desirable to have the power supplies already built, but any power supply providing the correct voltages can be used. It is also possible to drive the 12V bias line from a 20V supply if a 680 ohm resistor is used instead of the 15 kilohm R14 required when a 200V supply is employed.

The MJE521 power transistor is mounted on the chassis near the regulator, and is insulated with a mica washer which should be supplied with the device. A smear of silicon grease on either side of this washer helps heat transfer and should be used if available.

This transistor is much easier to mount compared with the traditional TO-3 packaged devices, only a single hole being required, facilitating its attachment to a temporary heat sink if desired for testing purposes—remember to bolt the transistor down with the brass collector tab next to the heat sink, and do not forget the washer.

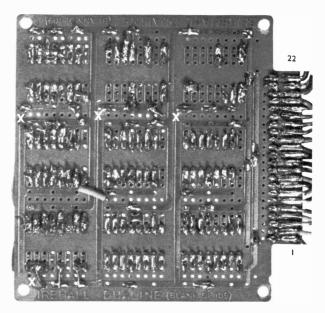
When the test arrangement is wired up, connect the power supplies and monitor the output voltage, which should be somewhere between 3 and 8V. Adjust VR1 to obtain the required 5V, preferably with a load of about 20 ohms connected.

If all is well, decrease the load to about 4 ohms; the output voltage should drop under the control of the

current limiter. As the final test, short out the output while monitoring the current. The output voltage will drop to zero, and with any luck the current will drop to about 400mA. If it does not, there is probably something wrong with the wiring, and you may need a new output transistor.

ALARM CIRCUIT WIRING

When the regulator is tested and performs satisfactorily, the wiring of the alarm circuit can be carried out, first the package interconnections, then the discrete components and finally the wiring to the edge connector. The wiring on the plain side is shown in Fig. 13 with the edge connector wiring. Testing this circuit is difficult to achieve in isolation, and in this case it is better to wait until the clock is nearing completion. There is no reason why the alarm oscillator should not be checked with an oscilloscope or even an earphone.



Underside view of the Alarm Board B showing positions of cuts in copper strips at four places marked X

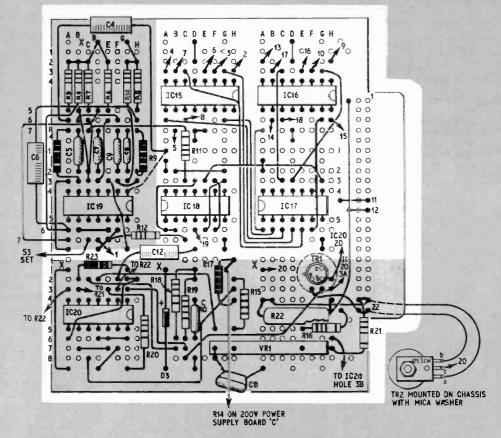


Fig. 13. Layout and wiring of the complete Board "B" incorporating the alarm sircuit and 5V regulator

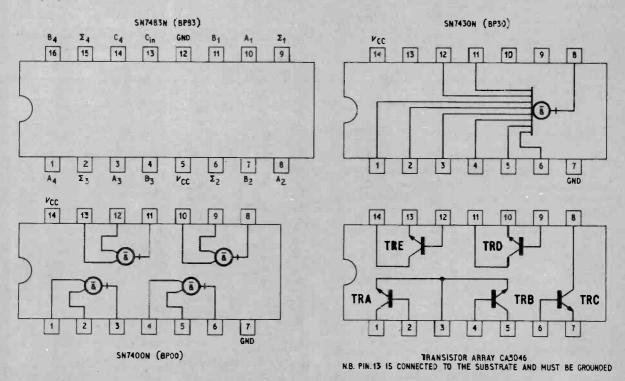


Fig. 14. Integrated circuit diagrams and pin connections for Board "B"

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kits then 4/6 for each two kits ordered. Kits
C, D and E 4/6 on first kit then 3/6 for each
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200 mfd. 25V, 1/3 each 18;- doz.
400 mfd. 20V, 3/4 each 48;- doz.
400 mfd. 12V, 2/;- each 48;- doz.
600 mfd. 25V, 3/6 each 48;1.0, doz.
600 mfd. 25V, 3/6 each 48,1.0, doz.
600 mfd. 35V, 3/6 each 48,1.0, doz.
600 mfd. 35V, 3/6 each 48,1.0, doz.
1000 mfd. 18V, 3/4 each 51,10,0 doz.
1000 mfd. 18V, 3/4 each 51,10,0 doz.
1000 mfd. 12V, 3/6 each 81,10,0 doz.
10,000 mfd. 12V, 4/9 each 82,8.0 doz.
10,000 mfd. 12V, 4/9 each 82,8.0 doz.
10,000 mfd. 10V, 3/6 each 81,00 doz.
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Č	110	5%	4·7 Ω -330k Ω	E24	2·5d	2d	1-75d
Ċ	± W	10%	4·7 Ω -10M Ω	E12	2·5d	2d	1.75d
Ċ	3w	5%	4·7 Ω-10M Ω	€24	3d	2·5d	2·25d
C	iw	10%	1-7 Ω -10M Ω	E12	6d	5d	4-5d
MO	4 W	2 %	10 Ω –1 M Ω	E24	9d	8d	7d
WW	įw.	$10\% + 1/20 \Omega$	$0.22 \Omega - 3.9 \Omega$	E12		juantities	
ww	3W	5%	12 Ω −10k Ω	E15		_l uantities	
ww	7 W	5 %	12Ω-10kΩ	E12		quant it ies	_
CODES	C = earbon	film high stability low	poise. MO metal	oxide Electrosi	l TRő ultra	i low noise.	WW = wire

BC126

wound Plessey.

WW = wire

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12-5/25, 16/40, 20/16, 20/16, 20/64, 25/6-4, 25/25, 32/4,
32/10, 32/40, 32/64, 40/16, 40/2-5, 50/6-4, 50/2-5, 50/6-0, 4/4
4/10, 80/2-5, 80/16, 80/2-5, 100/6-4, 126/4, 125/10, 125/16,
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POWER SUPPLIES AND CONSTRUCTION

The power supplies that provide the various d.c. voltages required by the Digi-Clock circuitry are quite conventional in design, as can be seen from Fig. 15. Outputs required from the supplies are:

(a) 10 volts (nominal) at 1A (max), from which the regulated 5 volt supply is derived.

(b) 180 volts at 10mA (nominal), which is used to drive the anodes of the "Nixie" tubes and decimal-point indicator.

(c) 200 volts (nominal) at 25mA (max), which is used to supply the 180 volt regulator, and to drive the 12 volt bias line of the 5 volt regulator.

In addition a 6.3V r.m.s. (50Hz) low current supply is required to provide the clock timing waveform.

No on/off switch was fitted to the prototype, as permanent use when plugged into the 230/250V a.c. mains supply makes it unnecessary. A mains switched socket with fused plug or a fused spur outlet is recommended for installation. A clock will normally be left on permanently, only being switched off at holiday times or other occasions when the house is vacated for long periods.

If the constructor's house wiring uses the non-fused type of plug then it is vital that a separate fuseholder be incorporated in the clock design to provide protection of the transformer primaries. While on the subject of fuses, remember that all fuses used in this design are necessary for safety, the clock is intended to run continuously, often unattended, and the only way safety can be assured is by proper fusing.

LOW VOLTAGE SUPPLY

Two power transformers were used in the prototype to provide the necessary a.c. supplies (Fig. 15). This proved to be necessary because of the difficulty of finding a single transformer with suitable ratings and of the correct physical size.

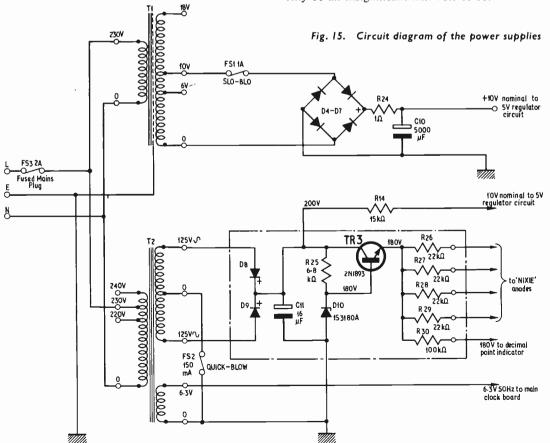
The transformer selected for the low voltage supply not only provides the required 10V at 2A, but also has the highly desirable feature of an interwinding screen, which reduces the coupling of mains-borne r.f. interference into the logic supply lines.

Constructors who may prefer to use a different case design from that used in the prototype, may like to know that West Hyde Developments make a single transformer that will supply all the voltages required by the clock. This is type TRA which is too large to

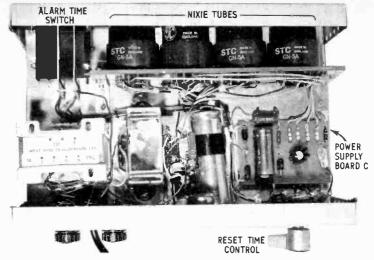
fit into the specified Case "C".

An encapsulated bridge rectifier (D4 to D7 in Fig. 15) with a current rating of 1A (continuous) is used as the low voltage full wave rectifier, and this is followed by a 5,000/F smoothing capacitor C10 in the usual way. Two "protection" components are included in this circuit.

When switching on, a very large surge current flows for a short period as the capacitor is charged. This current would be limited only by the internal impedance of the transformer, and might exceed the 8A surge rating of the bridge, were it not for the inclusion of R24 between it and C10. The resistor, of course, imposes a large voltage drop under surge conditions, and ensures that the current cannot exceed 8A, whereas during normal operation the voltage drop across it will only be an insignificant half-volt or so.



Top view of the chassis showing power supply components



The increase in the impedance of the supply caused by its inclusion does not pose a problem because the final 5V output is provided by a feedback regulator, which as we have already seen, reduces the supply impedance to a fraction of an ohm.

The use of an anti-surge fuse in this supply allows very close protection of the bridge and transformer, without having to increase the fuse rating to accommodate surge currents, as would be the case with quickblow devices. Fuse FSI ignores short duration current transients, but will blow within a few tens of milliseconds should its rating be continuously exceeded.

The smoothing capacitor C10 should be a good quality type with a high ripple-current rating. Components inadequate in this respect will have a reduced life in this type of circuit.

HIGH VOLTAGE SUPPLY

Transformer T2 is used to provide the high voltage supply for the display and 6.3V a.c. for the timing circuits. The two diodes (D8 and D9) and the smoothing capacitor C11 complete the full-wave rectification circuit as shown in Fig. 15.

The nominal 200V supply developed across C1 is fed to the 5V regulator via R14. This resistor should be mounted as close to the board as possible to reduce the risk of direct short circuits, but it cannot be mounted on the board because of the amount of heat it dissipates. Although not used in the prototype, a small tag-strip could be employed to support it, and allow air circulation.

The 180V regulator is simply an emitter follower circuit with the base voltage of transistor TR3 set by the breakdown voltage of a 180V Zener diode D10.

COMPONENTS . . .

POWER SUPPLIES

Resistors

R24 $I\Omega$ 3W wirewound

 $\begin{array}{ccccccc} \text{R2S} & 6 \cdot 8 k \Omega & \text{R28} & 22 k \Omega \\ \text{R26} & 22 k \Omega & \text{R29} & 22 k \Omega \\ \text{R27} & 22 k \Omega & \text{R30} & 100 k \Omega \\ \end{array}$

All 5%, ½W high stab. except R24

Capacitors

C10 5,000 μ F elect. 15V C11 16 μ F elect. 350V

Diodes

D4 to D7 Bridge rectifier IBI0JI0 100 p.i.v. 1A (Texas)

D8, D9 PL4004 (General Instruments) or any 400 p.i.v., >50mA

D10 IS3180A (Texas) or ZX180. Zener 180V, >2mA

Transistor

TR3 2N1893

Transformers

- TI Mains primary; 10V IA secondary with interwinding screen (e.g. Type TRC by West Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middlesex).
- T2 Mains primary; 250V c.t. 25mA and 6.3V IA secondary (e.g. "Midget Mains 250V" type by Radiospares).

Loudspeaker

LSI 80Ω 2‡in diameter

Display Tubes

VI to V4 GN-5A (S.T.C.) "Nixie" numerical indicators or similar (Electroniques (S.T.C). Ltd., Edinburgh Way, Harlow, Essex)

LPI Neon indicator lamp miniature (e.g. type IMH)

Switches

\$1 3-pole, 3-way rotary wafer switch.

- 52 Decade thumbwheel switch, 2 banks with 2 side plates. (Type SBI0N1248, Birch Stolec Ltd.). Alternatively 2 wafer thumbwheel switches, 4-pole, 10 way
- S3 Single-pole changeover miniature toggle

Fuses

FSI 1A Slo-Blo cartridge with fuseholder

FS2 150mA cartridge with fuseholder "Behind-panel" depth not more than lin

Miscellaneous

Case Contil Mod-2 Type C (West Hyde Developments)

Display panel, s.r.b.p. $8in \times 2\frac{1}{4}in \times \frac{1}{8}in$ Printed circuit Board "C" copper clad $3in \times 2in$ Aluminium brackets for display panel $2\frac{1}{4}in \times lin \times \frac{1}{2}in$ wide

Capacitor clip for C10 Perspex sheet orange translucent $7\frac{1}{6}$ in \times $2\frac{3}{6}$ in Heatsinks, clip-on for TR1 and TR3 (see photos) Thin flexible connecting wire different colours Nuts and bolts 4 B.A. and 6 B.A. \times 1 in Grommets and soldering tags. Lettering transfers

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Resistance 0-60 k Ω
0-60 R Ω; decibels

62 D. MULTI-TESTER

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0-250 M $_{\odot}$, resistance $0-66\,\Omega_{\odot}$, $0-66\,\Omega_{\odot}$, $0-60\,\Omega_{\odot}$ also ohms and $30\,\mathrm{k}\,\Omega_{\odot}$ at centre scale); capacitance 10F to $0.00\,\mathrm{lm}\,\mathrm{F}_{\odot}$, $0.00\,\mathrm{lm}\,\mathrm{F}_{\odot}$ to $0.1\,\mathrm{m}\,\mathrm{F}_{\odot}$; decibels $-20\,\mathrm{to} + 22\,\mathrm{d}\,\mathrm{B}_{\odot}$. Size 4 $\frac{1}{2}$ in $\approx 3\frac{1}{2}$ in $\approx 1\,\mathrm{in}$. 71/ $_{\odot}$, P. & P. 3/6.



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	3 poles	6/6	6/6	6/6	6/6	10/6	10/6	10/6	14/6	14/6
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	6 poles	6/6	10/6	10/6	10/6	14/6	14/6	14/6	26/6	26/6
- 1	7 poles	10/6	10/6	10/6	14/6	18/6	18/6	18/6	30/6	30/6
	8 poles	10/6	10/6	10/6	14/6	18/6	18/6	18/6	34/6	34/6
	9 poles	10/6	10/6	14/6	14/6	22/6	22/6	22/6	38/6	38/6
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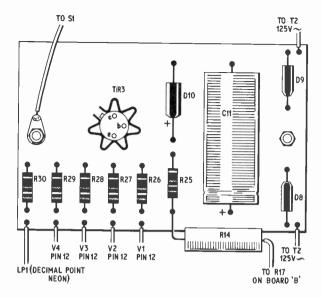
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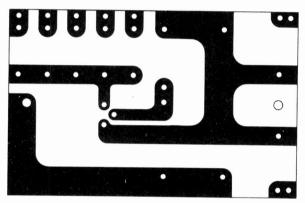


Fig. 16. Layout of components on Board "C", the high voltage regulator—shown full size

The transistor used in this position must have a high $V_{\rm cb}$ rating to allow for the difference between the unregulated input and the regulated output voltage, even under transient conditions. The regulator may be called on to provide up to 10mA at 180V.

If the nominal 200V supply rises to more than 220V, the transistor would get quite hot; hence the clip-on heat sink used in the prototype. The anode resistors R26 to R30 for the four "Nixie" tubes and the decimal-point indicator are mounted alongside the regulator on the same printed circuit board to give a neat appearance and to reduce the risk of a damaging short circuit.

Shorting the individual anode outputs to earth will not harm the regulator, because these resistors limit the current to a safe value. However, if the 180V output is shorted, the transistor will be instantly destroyed. In fact, in this design, the series pass transistor is used as a "fuse", it being impossible to use a conventional fuse link to afford any protection to a device operated under these conditions.

The 150mA fuse FS2 in the "earthy" line of the transformer will only be able to act fast enough to protect the diodes and the transformer itself, and the only way the transistor can be protected is by using a current limiter similar to that used in the 5V regulator, a course considered unnecessarily expensive in the prototype.

PRINTED CIRCUIT

The printed circuit used for the 180V regulator is of a simple design which lends itself to home production using the "paint and etch" system of printed circuit board construction which many readers will have used before.

The layout is shown in Fig. 16, which also gives component mounting details. It is recommended that the holes be drilled before the printed pattern is painted on, as this gives a good guide, and enables more accurate painting to be achieved.

If the constructor does not have facilities for producing printed circuits there is no reason why a tagboard of similar dimensions should not be used to support the regulator components, though the appearance would not be as neat in this case.

NIXIE DISPLAY

The drivers and power supplies used in the Digi-Clock are capable of handling any type, or make, of gas filled numerical indicator tubes currently available, and alternatives may be directly substituted for the STC GN5A used in the prototype, with appropriate wiring changes according to the pin connections.

Manufacturer's data on "Nixie" tubes usually states that the highest anode voltage available should be used to drive these devices, and readers may be a little puzzled by the choice of 180V for this design, as this is very close to the minimum voltage allowable.

The reason for the choice of such a low voltage is that the SN7441AN decoder driver is only guaranteed to "hold off" 55V; a Zener diode connected to each output breaks down if this voltage is exceeded. This means that the maximum voltage differential which can be achieved across the tube is 55V.

In our case, the voltage across the tube when it is supposed to be off is 180-55V which means that 125V can still be applied in these circumstances. Obviously, if the anode supply is raised too far, the 55V differential will be insufficient to ensure that the cathodes, which are supposed to be off, do not conduct.

COLOUR FILTER

If these cathodes do conduct, an unpleasant background haze is produced which impairs the readability of the display, and in extreme cases more than one numeral could become lit within the same tube. For a clear "Nixie" display with the view of the unlit numerals completely suppressed, it is important that a red or orange coloured filter be employed between the tubes and the observer.

Although tubes are available with this filter applied as a lacquered coating on the outside of the glass envelope, by far the best system is to use clear tubes with a common external filter sheet. In this design the filter is produced from a sheet of ordinary orange tinted Perspex, which performs admirably in this role, mounted on the front of the clock to form the viewing window.

The decimal point separating the two "minutes" indicators from the "hours" section has to be provided separately when using the GN5A "Nixies", as these devices do not have integral points as do some other types. In the prototype a Hivac type 1MH "Minicator", miniature neon, performed well in this role, and was driven from the 180V supply via a 100K resistor. Any small neon lamp, such as used for mains indicators, could be used with the correct value of series resistor R30.

Next month: Final wiring and testing

REGULOTIC— A SELECTION FROM OUR POSTBAG

Correspondents wishing to have a reply must enclose a stamped addressed envelope. We regret we are unable to guarantee a reply on matters not relating to articles published in the magazine. Technical queries cannot be dealt with on the telephone.

Time expense

Sir—I have been a faithful reader of PRACTICAL ELECTRONICS for a good many years now, and I have not until this month's issue (December 1970), come across a Digital Clock.

But I would like to express my disappointment when I saw the circuit, and found the cost of it was in the region of twenty-five to thirty pounds to produce. This puts the clock well beyond my, and I should imagine many other readers' grasp, and even then with a little too much heat on one of the pins the complete project could be destroyed.

I have also seen on the market a digital clock using a cold cathode display, costing under twenty pounds, so I was naturally assuming that your project would cost much less,

-but it doesn't.

I'm sure many other readers must feel the same way about the high cost, and I cannot see many readers attempting the project.

C. Honeyands, Cosford, Wolverhampton.

The estimated cost of making the complete "Digi-Clock" using the components specified is in the region of £40. No doubt many readers will be able to find ways of reducing this cost, but in order to build an all-electronic digital clock the degree of circuit complexity involved, whether using integrated circuits or discrete components, is bound to make this an expensive project. However, one must consider the accuracy and reliability together with long life in comparing the cost with any clock using electromechanical devices.—M.A.C.

Not for Fun?

Sir—Congratulations! You are now printing some really worth while designs in P.E. I am specifically thinking of the "Digital Clock" and the "P.E. Gemini Amplifier", and the forthcoming Sound/Light Controller. We want far more articles of this calibre, not designs for radios, metal detectors, electronic dice, war games,

etc. You should take a poll of readers' wants—I am sure that the majority of them, like me, want to build useful things, not toys!

M. J. Clarke, London, S.E.I.

I am pleased to learn that you have reacted favourably to some of our recent designs. On the other hand, I cannot agree with you so far as your comments relating to metal detectors, war games, etc. Electronics is a servant to all, and we must be very broadminded concerning the applications of this technology.

I certainly see no reason why amusements such as "War Games" should not be described. After all, the electronic circuitry involved can be as technically fascinating as that used for more prosaic projects, i.e. commercial com-

puters.—Ed.

Biased view

Sir—I have been a regular reader of your magazine for many years, and find it very enjoyable to read, and the circuits are really up-to-date. I also attend day-release Technical College and have an Intermediate Certificate in City and Guilds Radio and T.V. Servicing.

Nevertheless, I have come across a problem which no-one can explain, and I can find no book in the whole of Cambridgeshire which can give me an answer, so I am writing to you in the hope that you can help me before

I go mad!

In the latest circuits, for example, audio amplifiers, which are d.c. coupled, it often appears that the a.c. signal input is fed straight to the base of the first transistor, without the transistor having any d.c. base bias on it (from resistors, potential dividers, etc.). Therefore is it possible for a transistor to amplify the input a.c. signal without having any base bias?

Also, in a transistor configuration such as the "Super-Alpha pair", the first transistor usually has a base bias resistor, but the second transistor's base is connected straight to the first

transistor's emitter.

Even in PRACTICAL ELECTRONICS the text usually just states that the

emitter current of the first transistor is the base current of the second transistor; but how can that be—if there is no base bias resistor on the second transistor, there can be no voltage on the base, hence no current (Ohm's Law).

I must apologise if my query has a very simple explanation, which I should know, but technical college lecturers tend to show you a circuit of a transistor amplifier, and just say, "The signal goes in there, and comes out here," and expect you to accept it!

J. Hammond, Great Abington.

When an alternating voltage is present at the collector of a transistor, this consists of an alternating direct voltage. If this is passed to a succeeding stage by way of a capacitor, only the alternating component is passed. If this component is passed to an unbiased transistor, this signal will be rectified and amplified; an audio signal so treated would be distorted.

With d.c. coupled linear amplifier, the d.c. component from the previous stage is so arranged to correctly bias the succeeding transistor so that an exact reproduction of the a.c. com-

ponent is made.

A "Super-Alpha" pair is a compound of two transistors, d.c. coupled to form, in effect, a high gain transistor. This gain, ideally, approaches the product of the individual transistor gains, hence "Super-Alpha" as a description.

For pulse amplification, such combinations do not need a second transistor base resistor. In a.f. amplifier applications, this resistor is

required.—G.G.

- DECIMAL CURRENCY -AND P.E.

Readers in the U.K. are probably aware that British currency will be decimalised with effect from February 15, 1971. The following notes are issued for their guidance when writing to Practical Electronics.

1. Cheques and postal orders should show amounts payable in decimal

currency.

2. Readers' cheques and postal orders written in £ s d will not be accepted by the banks or Post Office after February 15, 1971.

3. Handwritten cheques of more than £1, which include new pence, should use a hyphen in place of the decimal point (e.g. £7-80, £30-06).

decimal point (e.g. £7-80, £30-06).

4. Postage rates on and after February 15 will be 2½p second class and 3p first class for up to 4 ounces. Old £s d stamps used on and after this date must be at the new rate of 6d second class, 7d first class for up to 4 ounces. Readers requiring a reply to correspondence are asked to use the correct postage rate on s.a.e.

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2N1613 2N1711	5/- BC108 4/6 BC109 5/- BC113	2/6 OA47 2/6 OA70 K/- OA79	2/- 2/-	6C4
2N1889	6/6 BC116	0A81	2/- 2/- 2/6	6CD6
2N1893 2N2147 2N2160	6/6 BC116 10/- BC125 15/- BC126	777 OA90	2/-	6CW
2N2160 2N2193	15/- BC126 12/6 BC147 9/6 BC148	0/8 OA95	2/- 1/6 1/6	6F60
2N2193 2N2217 2N2218 2N2219	5/6 BC149	4/- OA200 OA202	1/6 2/-	6F14 6F15
2N2219 2N2369	6/6 BC172	3/6 OA210 7/6 OC19	8/6 7/6	6F18 6F23
2N2369 2N2369 2N2369A	4/- BC186	8/6 OA210 7/6 OC19 7/6 OC20	19/6	ISHG
2N2484	12/6 BC147 9/6 BC147 9/6 BC149 9/6 BC149 8/7 BC149 8/7 BC149 8/7 BC182 1/7 BC182 1/7 BC182 1/7 BC184 1/7 BC184	7/6 OC20 4/- OC22 4/- OC23 4/6 OC24 4/6 OC25 6/- OC26 10/- OC28 10/- OC29 4/- OC35	9/6 10/-	6J4 6J5
2N2613 2N2646	7/- BC184L 10/6 BC212L BCY30	4/6 OC24 OC25	10/- 10/- 7/6	6J5 6J5(+ 6J6
2N2904 2N2923	6/- BCY31	6/- OC26 OC28	5/-	6J7 6K80
2N2924 2N2925	3/6 BCY33	10/- OC25 4/- OC25	12/6 12/6	6L6G
2N2926G	2/6 BCY34	a) IOC36	10/- 12/6	6LD: 6Q7
2N2926O 2N2926Y	2/6 BCY42 2/6 BCY43	8/_ UC41	5/- 6/-	168 A 7
2N3053 2N3054	10/a BCY71	4/ OC42 8/ OC44 8/8 OC45	9/6	68G7 68J7 68K7 68L7 68Q7 6U4 6V60
2N3054 2N3055 2N3391A	15/- BCZ11 6/- BD121	8/- 0C44 3/6 0C45 7/6 0C46 13/- 0C70 16/6 0C71 12/- 0C72	3/- 5/6 2/6	6SL7
2N3416 2N3570	6/- BD121 7/6 BD123 2/6 BD124	18/- 16/6 0C71 0C72	3/-	68Q7
2N3702 2N3703	17/6 BF115 2/6 BF117	5/- OC73 9/6 OC74	5/- 6/-	6V6(
2N3704		5/- OC73 9/6 OC74 5/- OC75	6/- 5/-	6V60
2N3705 2N3706	3/- BF167 4/6 BF180 3/- BF181	8/- OC76	D/-	6X4 6X50 6X50
2N3707 2N3708 2N3709	3/- BF181 3/6 BF182	5/- OC75 6/- OC76 7/6 OC77 7/6 OC78 6/6 OC81	8/- 4/- 5/-	10C2 10F1 10P1
2N3709	2/6 BF184	5/-IOC81D	4/-	10P1
2N3710 2N3711	2/6 BF185 2/6 BF194	2/a/OC84	5/- 5/-	10P1 12A7
2N3819 2N3903 2N3904	7/- BF195 7/- BF200	3/- OC139	5/- 7/6	12A7 12A7 12A7 12A7
2N3904 2N3905	7/- BF224 7/6 BF225	6/- OC169 6/- OC170 9/6 OC171	4/- 5/-	12AX
2N3906 2N4058	7/0 BF244	9/6 OC171	6/- 7/6	119B /
2N4059	5/- BFX 12	9/6 OC171 4/6 OC200 4/6 OC201 6/6 OC202 6/6 OC203	9/6	12BF
2N4061 2N4062	5/- BFX 13 8/- BFX 29 4/6 BFX 30	6/6 OC203	12/6 7/6	20D1 20F2
2N4286 2N4287	8/6 DEV 05	6/- OC203 7/6 OC204 8/- OC205 6/6 OC207 6/6 OCP71 5/- ORP12	8/- 12/6	20F2 20L1 20P1
2N4288 2N4289	8/6 BFX85 3/- BFX86 8/6 BFX87	6/6 OC207	15/- 19/6	20P3
2N4290 2N4291	3/- BFX88 3/- BFY18	5/- ORP12 5/- ORP60	10/-	20P4 20P5
2N4292 2N5354	9/* REV-90	12/6 P346A	5/- 2/9	7
2N5355	BFY50	4/- PL4002	8/-	400
28102 28103	5/- BFY52 7/6 BFY90	4/6 PL4003 18/6 PL4004 8/6 PL4005	3/3 3/6	1.5
28104 40250	7/6 BSX 19		3/9 4/-	_
40361	5/6 BFY51 5/- BFY52 7/6 BFY90 7/6 BSX19 10/- BSX20 11/- BSX21 12/- BSX76	7/6 PL4007 3/- TIS43	4/9	
40362 AC107	12/- B8X76 7/6 B8Y26 5/- B8Y27 5/- B8Y28	9/8/T1944	8/- 2/6	L900
AC126 AC127	5/- BSY27 5/- BSY28	4/- TIS45 3/6 TIS46	3/6 3/6	12/6 42/6
				55/- 25/6

THYRISTORS

PIV	50	100	200	300	350	400	
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6/- PCC88
6/- PCC88
6/- PCC189
30/- PCF80
30/- PCF80
7/- PCF82
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CIRCUITS

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26/6: CA2011 16/6: CA2002

26/6: PCH131 10/-: FH161

10/-: FJH141 10/-: FJH141

10/-: FJH211 10/-: FJH191

10/-: FJH211 10/-: FJH231

10/-: FJH211 17/6: FJH231

17/6: FJJ211 17/6: FJJ311

17/6: FJJ211 17/6: FJJ101

10/-: FJJ211 17/6: FJJ101

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Project 60. Package offers. 2. 230 amplifier, stereo 60 pre-amp. P.25 power supply, stere

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5MH: Pass Band. Separate Y1, Y2 amplifers. Calibrated triggered sweep from 0-2µsec to 100msec/cm.

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BELCO AF-5A SOLID STATE SINE SQUARE WAVE C.R. OSCILLATOR



Sine 18-200,000Hz; 18-200,000Hz; Square 18-50,000Hz. Output max +10dB (10kΩ). Operation internal batteries.

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AUTO TRANSFORMERS 0/115/230v. Step up or step down. Fully abrouded.

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VOLTAGE REGULATORS
Compact and panel mounting. Ideal for control of lappling defills, electrical solid policy of lappling defined and lappling defills of l

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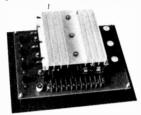
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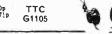
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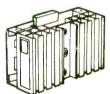


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