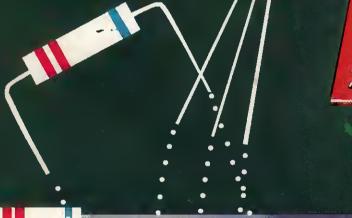
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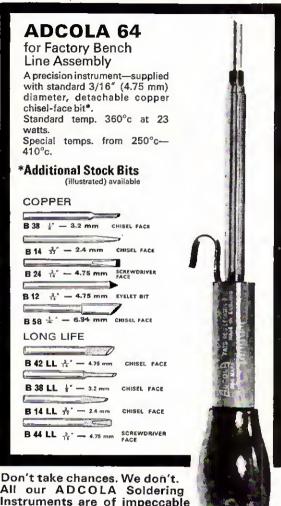


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The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output 5 watts R.M.S. (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 Zener diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.

The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required as part of the process of producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. This enables us to cover every IC-10 with the Sinclair guarantee of reliability.

SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. 5 Hz to 100 KHz±1dB. Frequency response Less than 1% at full output. Total harmonic distortion 3 to 15 ohms. Load impedance 110dB (100,000,000,000 times) total. Power gain 8 to 18 volts. Supply voltage $1 \times 0.4 \times 0.2$ inches. Size Sensitivity Adjustable externally up to Input impedance 2.5 M ohms.

■ CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, meking battery operation eminently satisfactory.

■ APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large-number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pte-amp section can be used as an R.F. or l.F. amplifier without any additional transistors.

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IC.10 With 1C-10 manual 59/6

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Project 60

laboratory standard modular high fidelity

Sinclair Project 60 comprises a range of modules which connect together simply to form a complete stereo amplifier with really excellent performance. So good, in fact, that only 2 or 3 amplifiers in the world can compare in overall performance. Now with the addition of three new modules to the range, the constructor has choice of assemblies with either 20 or 40 watts output per channel, with or without filter facilities.

The modules are: 1. The Z.30 and Z.50 high gain power amplifiers, each of which is an immensely flexible unit in its own right. 2. The Stereo 60 preamplifier and control unit. 3. The Active Filter Unit with both high and low audio frequency cut — offs. 4. The PZ.5 and PZ.6 power supplies. A complete system could comprise, for example, two Z.30's one Stereo-60, and a PZ.5. The PZ.6 is stabilised and should be used where the highest possible continuous sine wave rating is required. An A.F.U. may be added as required. In a normal domestic application, there will be no significant difference between PZ.5 or PZ.6 unless loudspeakers of very low efficiency are being used, in which case the PZ.6 will be required. For assemblies using two

Z.50's there is the new PZ.8 supply unit to ensure maximum performance from these amplifiers.

All you need to assemble your Project 60 system is a screwdriver and soldering iron. No technical skill or knowledge whatsoever is required and, in the unlikely event of you hitting a problem, our customer service and advice department will put the matter right promptly and willingly. Project 60 modules have been carefully designed to fit into virtually all modern plinth or cabinets and only holes need be drilled in the wood of the plinths to mount the control unit and A.F.U. Any slight slip here will be covered by the aluminium front panels of the Stereo 60. The Project 60 manual gives all the buildings and operating instructions you can possibly want, clearly and concisely. Perhaps the greatest beauty of the system is that it is not only flexible now but will remain so in the future as the latest additions to the range show. A stereo F.M. tuner is next to come. These and all other modules we introduce will be compatible with those already available and may be added to your system at any time. And because Sinclair are the largest producers of constructor modules in Europe. Project 60 prices are remarkably low.

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Z.30 20 WATT R.M.S. POWER AMPLIFIER (40 WATT PEAK) Z.50 40 WATT R.M.S. POWER AMPLIFIER (80 WATT PEAK)

The Z.30 together with the higher powered Z.50 are both of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use the Z.30 or Z.50 power amplifiers in your Project 60 system will depend on personal preference, but they are both the same physical size and may be used with other units in the Project 60 range equally well. The Z.30 is unique in that it may be used with any power source between 8 and 35 volts without need for adjustment and may thus be driven from a car battery for example. For operating from mains, for the Z.30 use PZ.5 power supply unit for most domestic requirements, or PZ.6 if you have very low efficiency loudspeakers. For Z.50, use the PZ.5, PZ.6 or the PZ.8 described below.

Z.30 15 watts R.M.S. into 8 ohms, using 35V/20 watts R.M.S. continuous into 3 ohms using 30 volts.

Z.59 40 watts R.M.S. Into 3 ohms: 30 watts R.M.S. into 8 ohms, continuous, using 50V.

Frequency response 30 to 300,000Hz ± 1dB

Distortion 0-02% into 8 ohms

Signal to noise ratio better than 70dB unweighted

Input sensitivity 250mV into 100 Kohms

For speakers from 3 to 15 ohms impedance Size 31" × 21" × 1"

STEREO 60 Preamp/Control unit

The Stereo 60 is a stereo preamplifier and control unit designed for the Project 60 range but suitable for use with any high quality power amplifier. 'Again silicon epitaxial planar transistors are used throughout and great attention has been paid to achieving a really high signal-to-noise ratio and excellent tracking between the two channels, input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs. The tone controls are also very carefully designed and tested.

High Pass and ACTIVE FILTER UNIT High Pass

For use between Stereo 60 unit and two Z.30s or Z.50s, the Active Filter Unit matches the Stereo 60 in styling and is as easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible by reason of the careful design and generous negative feedback employed.

Two stages of filtering are incorporated-rumble (high pass) and scratch (low pass).
Supply voltage—15 to 35V. Current—3mA H.F cut-off (-3dB) variable from 28kHz to 5kHz L.F cut-off (-3dB) variable from 25Hz to 100Hz Filterslope, both sections 12dB per octave
Distortion at 1kHz (35V supply) 0.02% at rate

Built, tested and guaranteed £5.19.6



SINCLAIR POWER UNITS

PZ-5 30 volts unstabilised

PZ-6 35 volts stabilised £7.19.6

£4.19.6

PZ-8 45 volts stabilised (less mains transformer) for use with Z.50 £5.19.6

If at any sime within 3 months of purchasing Project 60 modules from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of purchase date. There will be a small charge for service thereafter. No charge for postage by surface mail. Air-mail charge ac cost.



APPLICATIONS

Hi-fi amplifier; car radio amplifier; record player amplifier fed directly from pick-up; intercom; electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the Z.30.

The Z.50 is completely interchangeable with the Z.30 and can be used in all Z.30 applications.



Z.30

Built, tested and guaranteed with circuits and instructions manual

Built, tested and

109/6

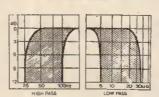
STEREO 60 SPECIFICATIONS

- Input sensitivities—Radio—up to 3mV Mag. p.u—3mV: correct to R.I.A.A. curve ±1d8: 20 to 25,000Hz. Ceramic p.u.—up to 3mV: Aux.—up to 3mV: Aux.—up to 3mV: Deput 10 3mV: Aux.—up to 3mV: Aux.
- Channel matching-within IdB.
- Tone controls—TREBLE +15 to —15dB at 10KHz: BASS +15 to —15dB at 100Hz.
- Power consumption 5mA,
- Front panel—brushed aluminium with black knobs and controls.
- Size 8½ × 1½ × 4in.



STEREO 60 Built, tested

£9.19.6





July B. A. B. M.

BUILDING A PROJECT 60 ASSEMBLY

illustration shows quite clearly how easily Project 60 can be contained in one of today's slim, modern plinths. Very little space is required to house these Sinclair units, and within the space of the motor plinth, you can install a stereo amplifier of the very highest quality. If, for example you have already put together an assembly as illustrated here, adding the Active Filter Unit would be very easy.

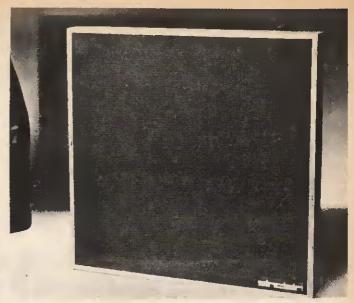
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The Q.16 will handle loading up to 14 watts R.M.S. and presents an 8 ohm impedance to the amplifier output. Frequency response extends from 60 to 16,000 Hz. with exceptional smoothness. A specially designed driver system is used in a sealed and contoured pressure chamber to ensure good transient £8.19.6 response at all frequencies. Size: 93" square \times 43" deep from front to back.

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Specifications Size: 1," x + " (46 x 33 x 13mm).

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Medium wave band with bandspread at higher frequency end. Ragnetic type.
Case: Black Plansite with anodized aluminium front
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Complete kit incl. eorpiece, case, solder and instructions in fitted back.

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Tape pre-amp E1312, as above.
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2 amp 27/6 10V. D.C. 27/6 500V. A.C. 27/1
2 amp 27/6 20V. D.C. 27/6 500V. A.C. 27/1
2 amp 27/6 20V. D.C. 27/6 500V. A.C. 27/1
2 amp 27/6 20V. D.C. 27/6 500V. A.C. 27/1
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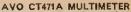
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The Classic Teak finished case

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SPECIFICATION:

Sensitivities for 10 watt output

i.p.s.) Mag. P.U.: 2 mV. Cer.P.U.: 86mV. Tuner: 100mV.

Aux. 100mV. Tape/Rec. Output. Equalisation for each

input is correct to within + 26B (R.I.A.A.) from: 20Hz to 20KHz.

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200-250V. Size 12½in long, 4½in deep, 2½in high. Built and tested.

THE RELIANT Mk. II SOLID STATE GENERAL PURPOSE AMPLIFIER

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In teak finished case

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watts into a 3 ohms speaker.

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SPECIFICATION

Output per channel—10W rms.
Prequency bandwidth 20Hz to 20kHz
±1dB @ IW.
Total distortion @ IkHz @ 9W 0.5%.
Input sensitivities—CER. P.U. 100mV
into 3 MQ: Tuner 100mV into
100kQ: Tape 100mV into 100kQ.
Overload Factor—Better than 26dB.
Signal to noise ratio—70dB on all
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Tape recording output sockets on each channel.

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An extremely reliable general purpose valve amplifier. Its rugged construction valve amplifier. Its rugged construction

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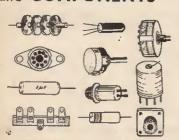
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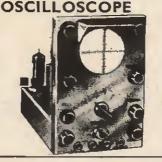
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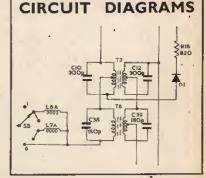


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VOL. 6 No. August 19

ELECTRONICS

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FINE ART .

NDUSTRIAL Art has become a recognised subject for comment and serious study. But surprisingly, electronic engineering is not given the amount of attention it would seem to deserve. At first, it may seem a trifle absurd to consider electronic hardware in terms of art. Yet there is a beauty of form and colour in many a humble mass produced component, and intricate patterns pleasing and attractive to the eye are composed by electronic assemblages making up severely functional equipment. No matter how practical and down-to-earth we may be, there is no reason why we should be blind to this aesthetical quality.

But this incidental, or accidental, art of the component manufacturer and the wireman is concealed from lay eyes by sombre metallic shrouds or wooden caskets which have for long been deemed the right and proper housing for much electronic equipment. For the general user, the outward sign of electronics is limited to the appendages mounted on a control panel. Notwithstanding the good styling of these adjuncts, and the obvious thought which is bestowed upon their arrangement, such items are not representative of the true "electronic art" which exists

within.

Look again at those delicate nerve-like systems traced by multi-coloured leads of a cableform; at the variety of maze patterns provided by printed circuit boards; and at the mosaics built up from resistors and capacitors variegated not only in hue and shape but in their disposition, and those tiny semiconductor devices whose jewel-like resemblance is often most striking.

Here one would have thought is wealth indeed for artist and sculptor alike to contemplate and adopt for their particular purposes—with tremendous effect. In contrast, how pitiful are certain works of art that some of our artistic contemporaries have presented to the public gaze as representative of, or inspired by, electronic tech-

nology!

The moral would seem to be this. If electronics is to have an influence in the world of art commensurate with its great impact in strictly practical matters, it must reveal more to the public eye. Maybe some drastic rethinking by industrial designers and engineers is overdue. Why not make certain domestic equipments living works of art by using transparent cases; or even encapsulating complete assemblies in blocks of transparent resin. And why not think in terms of less conventional shapes for the complete equipment. Flexible printed circuits and wiring boards could free designers from the limitations of the commonplace rectangular box; would not spherical forms be more appropriate for the space age?

F.E.B.

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Our September issue will be published on Friday, August 14

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or anyone interested in meteorology, sailing, or just wind speed, the cost of an anemometer is rather high. When the author's son became interested in meteorology, an anemometer was required, so one was constructed using readily available components.

Many commercial remote anemometers work on the a.c. generator principle, that is the faster the generator armature is rotated by the wind force on the anemometer cups, the greater the voltage produced. This has the disadvantage of not giving a linear output, with the consequent difficulty of meter scale production. It also requires about a 5 m.p.h, wind to overcome the resistance of the magnetic poles of the generator before the cups will start to rotate.

With the anemometer described, wind speeds of less than 5 m.p.h. can also be measured, and the scale is linear. The design is suitable for use on sailing yachts, and details are given on how to run the unit from the

boat's power supply.

If three anemometer cups are arranged to rotate freely in the wind, and a disc with a number of holes around the periphery is fixed to a shaft being driven by the cups, the holes can be counted as they revolve with the aid of a light source and a phototransistor. This count can then be made to register on a meter.

CIRCUIT DESCRIPTION

When the holes in the rotating disc pass over the phototransistor, light is allowed to fall on the phototransistor (TR1) from the light source, producing a pulse at the collector of TR1 as indicated in Fig. 1, the circuit diagram of the anemometer. The pulse is

squared off by transistors TR2 and TR3 which form a Schmitt trigger. The pulse is then differentiated by C2 and R8 to trigger transistors TR4 and TR5 which constitute a monostable. It is arranged by the selection of C2, that the monostable is in its unstable state for 3 milliseconds. This timing is such that at a wind speed of 100 m.p.h. (higher than one hopes to experience) the monostable has time to return to its stable state before the next pulse.

By J.S.HAGGIS

The time of 3 milliseconds is selected to correspond to the disc and hole size described in this article, and any increase or decrease in disc or hole size will have to be compensated for. Meter M1 integrates the 3 millisecond pulses which vary in frequency, but are all of the

same duration.

At wind speeds of less than 5 m.p.h. the pulses are detectable on the meter as fluctuation of the needle. The fluctuation can be reduced by fitting a 100µF capacitor (C3) across meter M1; this does not completely eliminate the pulsing, so at very low speeds one can check that the system is not missing pulses by observing a regular flick on the meter.

CIRCUIT POWER SUPPLY

It is essential for consistent reliability to have a good stabilised power supply. The mains power supply in Fig. 2, is stabilised with the aid of the Zener diode D7. It incorporates a series resistor which provides overload protection. When the anemometer is to be used from a 12 volt or 24 volt battery the supply for lamp and circuitry can be as shown in Figs. 3 and 4; all resistors used in these two circuits are wirewound types.

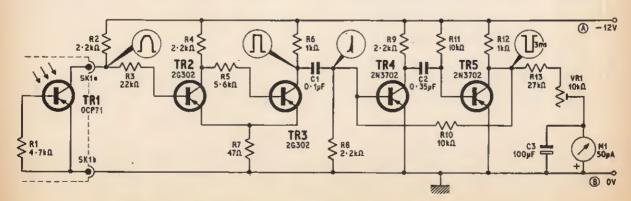


Fig. 1. Circuit diagram of the basic anemometer



As can be seen from Fig. 3 the supply circuit for a 12 volt battery only provides 10 volts d.c. to the anemometer circuit. This is so that stabilisation of the 12 volt input can be effected by R2 and D1, the lower voltage will not affect circuit operation providing that the instrument is calibrated at the lower voltage, and not used at a higher voltage afterwards.

LAMP POWER SUPPLY

A 6.5 volt 0.3 amp bulb is used to illuminate TR1; the voltage on the bulb should be kept as low as possible to increase bulb life. A mains operated circuit for the bulb supply is given in Fig. 5. A good d.c. supply must be used or the anemometer will be unreliable in operation.

The value of R1 Fig. 3, or R1 and R2 Fig. 4, or R14 Fig. 5, depends on the length of wire used to carry the supply to the anemometer; in most cases this will be many yards, therefore an appreciable volt drop can be expected. Bearing in mind the need to keep the bulb voltage as low as possible, the appropriate resistor may have to be slightly adjusted in value, as explained later.

CIRCUIT CONSTRUCTION

The circuit is assembled on a printed circuit board, details of which are given in Fig. 6. Layout is not critical, but that detailed has proved successful. If the

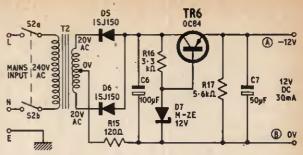


Fig. 2. Mains power supply circuit for the anemometer circuit

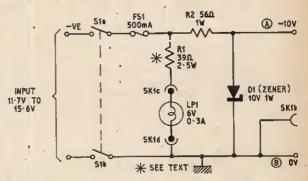


Fig. 3. Power supply to operate the anemometer circuit and lamp from a 12V battery

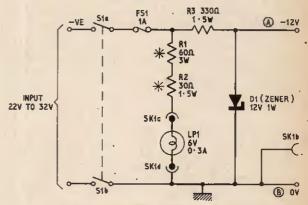


Fig. 4. Power supply to operate the anemometer circuit and lamp from a 24Y battery

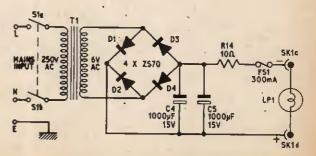
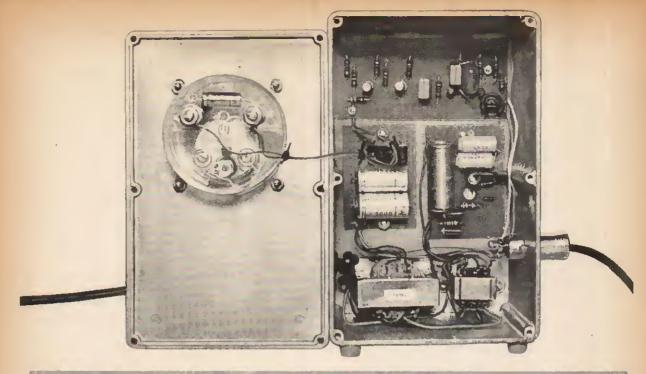
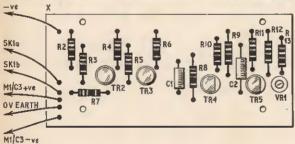


Fig. 5. Mains power supply circuit for the lamp



ANEMOMETER CIRCUIT WIRING





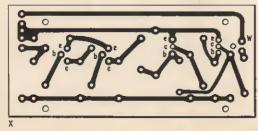


Fig. 6. Layout of the anemometer circuit on a printed circuit board

COMPONENTS . . .

Resistors

 $4.7k\Omega$

 $2.2k\Omega$ R2 $22k\Omega$

 $2 \cdot 2k\Omega$

R5 5-6kΩ

 $lk\Omega$ R6

R7 47Ω

R8 2.2kΩ

R9 $2-2k\Omega$ RIO $l0k\Omega$

RH $10k\Omega$

RI2 $lk\Omega$

R13 $27k\Omega$ All 4W, 10% carbon

Capacitors

C1 $0.1\mu F$ polyester C2 $0.35\mu F$ polyester $(0.1\mu F$ and $0.25\mu F$ in parallel) C3 $100\mu F$ elect. 12V

Transistors

OCP71 (phototransistor) TRI

TR2 2G302 TR3 2G302

TR4 2N3702

TR5 2N3702

Miscellaneous

VRI $-10 \mathrm{k}\Omega$ skeleton preset potentiometer MI $-50 \mu\mathrm{A}$ moving coil meter SKI Miniature sealed four pin plug and socket Copper clad s.r.b.p. board $-4 \mathrm{km} \times 2 \mathrm{in}$

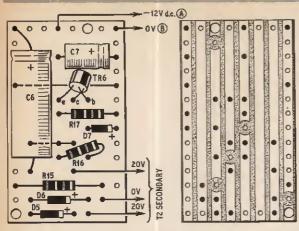


Fig. 7. Layout of the mains power supply for the anemometer circuit using Veroboard

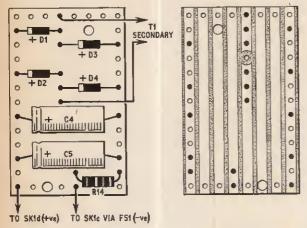


Fig. 8. Layout of the mains power supply for the lamp using Veroboard

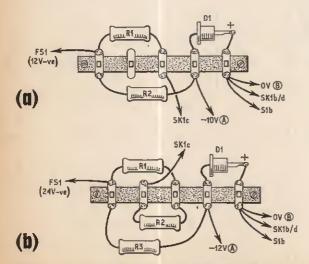


Fig. 9. Layout of the battery supplies using a five-way tagstrip (a) for a 12V battery, (b) for a 24V battery

COMPONENTS . . .

MAINS CIRCUIT SUPPLY

Resistors

RI5 120Ω R16 3.3kΩ R17 5.6kΩ

All 4W, 10° carbon

Capacitors

C6 100μF elect. 50V C7 50μF elect. 25V

Semiconductors

TR6 OC84

D5, 6 ZS70 or SX641 or DD003 or ISJ150 (2 off)

12V 250mW 5% Zener type M-ZEI2 (Radiospares) or ZI2

Miscellaneous

T2 Miniature mains transformer 220/240V primary 20V-0V-20V secondary (Radiospares)

S2 D.P.S.T. toggle switch Veroboard 2in × 1½in, 0·15in matrix

COMPONENTS . . .

MAINS LAMP SUPPLY

Resistor

RI4 10Ω (see text)

Capacitors

1,000μF elect. 15V

1,000 uF elect. 15V

DI-4 ZS70 or DD003 (4 off)

Transformer

TI Miniature mains transformer 220/240V primary 6V, 300mA secondary

Miscellaneous

FSI 300mA fuse and holder

SI D.P.S.T. toggle switch

LPI 6.3V, 0.3A m.e.s. bulb

Clip on m.e.s. bulb holder (Radiospares)

Veroboard 2in × 14in, 0-15in matrix

constructor is not able to etch the component board, then Cir-kit copper strip can easily be made to follow the layout given.

Layout and wiring diagrams for the circuit and bulb supplies are given in Figs. 7, 8 and 9. The two layouts shown in Fig. 9 use tag strips because some of the components may warm up when the unit is in use. It is not normally necessary to provide a heat sink for the Zener diode as this diode will only pass current near to its maximum capability when no current is taken by the anemometer circuitry, and when battery voltage is at its highest.

The circuit boards, MI, and SI can be mounted in a die cast box, the size of which will depend on the type of power supply used. If the unit is for use on a sailing boat, or will be out in the elements, both the inside and outside of the case should be painted; the lid, supply lead and SK1 should be sealed.

Meter M1 can be any 50μ A type available with as large a scale as possible and is best mounted on a rubber



HEAD DETAILS

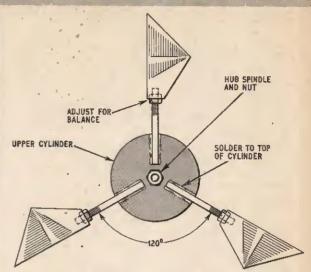


Fig. 12. Arrangement of the cups and arms on the rotating cylinder

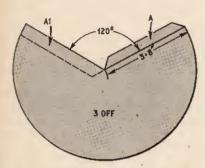


Fig. 10. Development of one cup

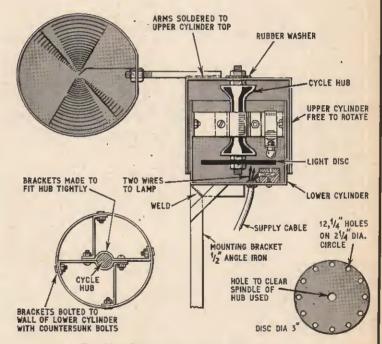


Fig. 11. Construction of the anemometer head, a four core lead out wire is needed

MATERIALS . . .

Brass plate $3\frac{1}{2}$ in \times $3\frac{1}{2}$ in \times $\frac{1}{16}$ in (disc) Copper sheet 20in \times 20in, 20 s.w.g. (cups, cylinders and hub brackets) Round brass rod 12in $\times \frac{1}{4}$ in diameter (cup arms) Whitworth nuts $\frac{1}{4}$ in 6 off (cup fixings)

Bicycle front wheel hub complete with nuts (see text) Nylon or rubber washer to fit hub

Countersunk bolts 4B.A., Jin, 4 off (hub bracket fixings) .

Round head bolts 4B.A., 1in, 3 off (hub bracket and TRI block fixings)

Nuts 4B.A., 6 off Angle iron $12in \times \frac{1}{2}in \times \frac{1}{2}in$ (mounting bracket if required) Tuffnol I $\frac{1}{2}$ in $\times \frac{3}{2}$ in $\times \frac{3}{2}$ in (TRI and RI mounting)

Diecast case (see text)
Veropins 3 off (TRI and RI mounting)

washer. The circuit boards can be mounted on foam rubber to provide shock protection where necessary.

MECHANICAL CONSIDERATIONS

With reference to the Handbook of Meterological Instruments, it was found that the best arrangement is an anemometer using 3 cups of 5 inches diameter, the centre of the cups rotating 6½ inches from the axis. As will be appreciated, the aerodynamics of the cups bear some relation to the efficiency of the rotation. The cups described here are not the ultimate in design, but they can easily be constructed and are quite adequate for the job, giving reasonable accuracy to the anemometer.

Ideally, all metal work is best made from copper or brass, as there is then no trouble from corrosion, bearing in mind that the instrument will suffer the worst of the elements.

CUP CONSTRUCTION

A development of one cup is shown in Fig. 10; three of these are required to make the three cups. The copper is bent smoothly round so that tab "A" lies on

"Al" where it is soldered in position.

On the edge of each cup, by the joint of tabs "A" and "Al", the shape is slightly flattened to take the arms, as shown in Fig. 11. The arms are made from \(\frac{1}{4}\) inch brass rod 4 inches long, threaded at one end. The threaded end passes through a hole in the side of the cup wall near the periphery. One nut either side of the cup wall is used so that the position of the cups on the arms can be adjusted in order that the three can be balanced. It is best not to bolt the cups to the arms at this stage, but to wait until the arms have been soldered to the top of the anemometer body.

BODY CONSTRUCTION

As can be seen in Fig. 11 the body of the instrument consists of two copper cylinders, one fitting over the other. The lower cylinder is fixed, while the upper cylinder is free to be rotated by the pressure of the wind on the cups. The upper cylinder has a diameter of 4.4 inches and is 4 inches deep, while the lower cylinder has a diameter of 4 inches and is 3.6 inches deep. The construction of these two open ended cylinders is quite simple therefore no further details will be given here.

Some form of bearing is required to support the upper cylinder; the prototype unit used the hub from a bicycle front wheel. It is quite important that this hub be in good condition, for if low and reliable wind speeds are to be recorded, there must be very little mechanical

friction.

The hub must be secured to the walls of the lower cylinder; this is achieved by making 4 brackets from 20 s.w.g. copper strip as illustrated in Fig. 11. The brackets must be made to fit tightly around the hub—the diameter of the clip will depend on the make of hub used. The brackets should be about I inch deep.

The four brackets are bolted around the centre of the hub and placed inside the lower cylinder to ensure that

the hub fits precisely in the centre.

The light disc is constructed from $\frac{1}{16}$ inch brass plate as shown in Fig. 11, and is 3 inches in diameter. A hole is drilled in the centre to take the spindle of the hub. Twelve $\frac{1}{2}$ inch diameter holes are drilled around the disc, the centre of the holes being $\frac{3}{6}$ of an inch from the periphery; the holes are set 30 degrees apart. It is advisable to paint the disc with matt black paint when complete, this will stop any chance of light reflections affecting the phototransistor. The inside of both cylinders should also be painted matt black.

ASSEMBLY

The disc is bolted to one end of the hub spindle and the whole assembly, that is the hub complete with brackets and disc, is placed in the lower cylinder leaving a clearance of 0.8 inch between the disc and the bottom of the cylinder. The Tuffnol phototransistor mounting block is situated beneath the disc. No precise measurements are given for the fitting of the hub, because it depends a great deal on the type of hub used. With the hub held in the centre, and with 0-8 inch clearance between the disc and cylinder base, the 4 holes that secure the brackets to the cylinder walls can be drilled through the wall and bracket at the same time. It is necessary to countersink the cylinder holes as much as possible, this being done the brackets can be bolted to the cylinder. The heads of the countersunk bolts are then filed down to conform to the radius of the cylinder wall, to prevent them touching the inner wall of the upper cylinder. The spindle and disc should now spin freely in the lower cylinder.

The upper cylinder is completed by drilling a hole in the centre of the top to take the hub spindle. The arms are soldered in place on the top of the cylinder, they are placed at an angle of 120 degrees to each other, as shown in Fig. 12. The arms are not taken to the centre of the top, as a space is left in the centre to take the nut

of the spindle.

When this has been done the cups can be fitted onto the threaded ends of the arms as shown in Figs. 11 and 12. The assembly can now be tried out in position over the lower cylinder by placing the top end of the hub spindle through the hole in the top of the upper cylinder. A nylon or rubber washer is placed over the spindle and the nut is screwed on and tightened; the nylon or rubber washer scals the spindle hole.

The upper cylinder, complete with cups, should be free to rotate over the lower cylinder without touching. Check that there is good clearance between the two all

the way round and correct if necessary.

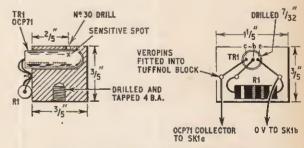


Fig. 13. Mounting block for TRI and RI

PHOTOTRANSISTOR MOUNTING

Phototransistor TR1 is mounted on a block of Tuffnol as shown in Fig. 13. A $\frac{1}{32}$ inch hole is drilled into the side of the block, as close to the top as possible, this hole is to hold the phototransistor. A second hole is drilled at right angles to the first hole with a No. 30 drill. The two holes connect with each other as shown in Fig. 13. The second hole is to allow light from LP1 to reach the sensitive spot of phototransistor TR1.

In the block, at the rear of TR1, three small holes are drilled to take three Veropins. These pins act as connecting points for TR1 and R1. Resistor R1 is mounted close to TR1 to reduce the number of wires from the anemometer head to the remote circuitry.

A 4B.A. hole is drilled and tapped in the base of the block to secure it to the base of the lower cylinder.

Inspection of the internals of the OCP71'will reveal two junctions, one either side of a flat plate, it is the smaller of these junctions that is sensitive to light, and it is this junction that must be positioned under the small hole in the mounting block. Once TR1 is in position with the sensitive spot placed correctly, a dab of adhesive is applied to prevent the phototransistor from moving.

The bulb to supply the light is mounted in a clip on bulb holder. The clip is pushed over one of the hub brackets, as shown in Fig. 11. It should be positioned

close to the disc and directly over the holes.

SETTING-UP

Before any setting up can be completed, the phototransistor block must be secured in position. To do this remove the upper cylinder from the spindle, and remove the hub and bracket from the lower cylinder. Remove the disc from the spindle, and replace the hub, less the disc, and secure. Now position the phototransistor block with its light hole immediately under the bulb and mark its position on the base of the cylinder. Remove the hub and secure the phototransistor block, complete with the phototransistor and R1, to the marked position.

The hole that secures the block to the base of the cylinder can be slightly larger than the 4B.A. bolt as this will allow the block to be finally adjusted. Now

re-assemble the lower cylinder.

With the anemometer on the bench, rotate the disc until a hole is directly under the bulb so that light can fall on TR1. Connect the power supply to the anemometer circuit, ensuring the correct polarity, and connect up the bulb supply, using the same length of cable as will be required when the anemometer is installed.

Aim to apply the minimum voltage to the bulb to reliably operate the circuit. In the prototype, the component values shown in Fig. 5 were used. The circuit arrangements shown in Figs. 3, 4 and 5 apply approximately 4 volts to the bulb at the end of 40 yards of 14/0-0076 cable. The d.c. voltage supplied by the circuit of Fig. 5 has a ripple of 270 millivolts.

COLLECTOR VOLTAGE

With light falling on TR1, collector voltage must be less than minus 0.5 volts. If the collector voltage is above 0.5 volts when measured with a d.c. meter, adjust the bulb position, or the position of TR1, until the voltage is correct. In some cases it may be necessary to reposition TR1 in the mounting block. If this fails, then the bulb voltage should be increased by changing the value of R1 in Figs. 3 and 4 or R14 in Fig. 5. Once the voltage has been set rotate the disc to cut off the light, and check that the collector voltage of TR1 has increased to almost the supply voltage. When a battery supply is to be used the above procedure should be carried out at the lowest normal battery voltage.

The upper cylinder complete with cups can now be fitted and revolved. If an oscilloscope is available observe the output from TR1 collector to ensure that the circuit is not missing any pulses. If no oscilloscope is available, connect meter M1 into the circuit with C3 disconnected. Revolve the cups slowly and check that the meter registers regular pulses.

CALIBRATION

At a height of 33 feet above ground level, wind speeds will seldom exceed 70 m.p.h. in this country,

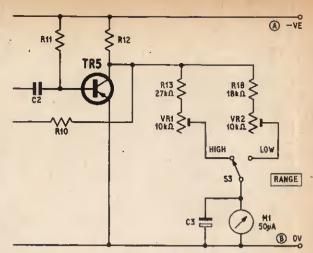


Fig. 14. Diagram of the additional range circultry

therefore it is suggested that the maximum reading of the meter be 70 m.p.h. If it is required to operate in very exposed areas it may be necessary to have a full scale reading of 100 m.p.h., but the lower the maximum can be kept the better it will be for reading low wind speeds, unless a very large meter is used.

It is possible to add a lower scale to the anemometer by including a range switch and additional resistor and trimmer as shown in Fig. 14. If this is done both ranges will have to be calibrated as described below.

Having decided what maximum scale is required it is necessary to draw the scale on a plain meter backing card, numbering every 10 m.p.h. and marking every

single m.p.h. The scale is linear,

The best way to calibrate the instrument is against the reading of an existing anemometer, but an alternative is to calibrate against a car speedometer. To do this a calm day is needed so that the only airflow is that of the cups through still air, and not against a wind adding to the required speed. Hold the anemometer as far away from the car body as possible to get away from any slipstream. With the car travelling at a steady 10 m.p.h. adjust VR! until the meter of the anemometer reads 10 m.p.h. Then travel at greater speeds to check through the range.

POSITION OF ANEMOMETER

The wind speed near the surface of the Earth varies rapidly with height and is also greatly affected by the presence of obstacles such as trees or houses. The Handbook of Meteorological Instruments defines the conditions under which measurements should be made for climatological records, as over open level terrain at a height of 33 feet above ground level. "Open level terrain" is defined as an area where the distance between the anemometer and any obstruction is at least 10 times the height of the obstruction above ground level at the anemometer.

It is unlikely that all constructors will be able to fulfill these requirements, but the position should be chosen with these requirements in mind and a suitable com-

promise can usually be reached.

The constructor may wish to build the mechanical parts of the instrument in a different manner than that described, or with slightly different dimensions. A pair of small roller bearings can be utilised if this is found to be more convenient than the "hub" system described.



AM constantly being re-assured of the advantages of this table-top hobby. One's husband can be at home, in fact in the very same room as his wife and still pursue his hobby—no gallivanting, leaving a distraught and worried wife at home wondering where on earth he is. True—and this as far as I can see is the only advantage of this hobby, though there are others, I am told.

Think of all the marvellous "mod-ns" one can have! The Jones' will really have their work cut out keeping up with us. Automatic garage doors and gates which save us the tedium of getting out of the car to open them; a lawn mower which goes scampering off round the lawn on its own, while my husband sits in a deck chair occasionally glancing up from his paper to see that it is not making a bee-line for him; the automatic camera which clicks each time a little bird sits on the bird table; the automatic chicken feeder which sprays food out to the freerange chickens at regular intervals; and the washing machine which miraculously switches itself on at four in the morning, and by the time we get up, all the weekly wash is done! So what am I complaining about? You may well ask.



As yet, these and many other ideas are only on the drawing board, so to speak, and some, not even as far advanced as that, but are only ideas lurking darkly in my husband's imagination. To begin with, we have not even our own house, let alone garage, gates and lawn and certainly no chickens! However, the projects go ahead as if we had all these things and each time we move, we leave behind a landlady bewildered by what she saw of those embryonic inventions!



By JUDITH TERRY

Consider the words "table-top hobby". Indeed this is no misnomer! Oh no! There are always little "bits" (and some not so little!) on our dining room table and were it not for the fact that my husband likes food even more than electronics, we should never clear even the smallest space for our meals.

As it is, we sit amidst a jumble of soldering irons smoking ominously, circuit diagrams and hundreds of little striped things, with fine wirylegs which I am told are very expensive. Not that that makes them any the more acceptable!

I noted with a sigh this morning, that when we leave a bewildered landlady behind this time—we will leave an irate one because there are now a dozen little drill holes in that polished table.

When we move, and it seems we are destined to be an itinerant family, all the "bits" go with us. They are carefully and lovingly packed in tin boxes and huge wooden crates.

Amongst the things we carry round with us are several old washing machine motors, which "may come in handy" (I ask you!) and a pair of the most incongruous binoculars I

have ever seen! These latter are almost 2ft long and weigh about 9lb and have to be strapped onto one's head. If you have ever tried strapping a 2ft long, 9lb weight onto your head (as if you would!) you will know that it results in your having to gaze permanently at your feet!

The strange thing with these binoculars is that one cannot actually see one's feet—or anything else for that matter. I am told the reason for this is that they have infra-red lenses. My husband hopes now to use them for his "anti-crash-on-motorways-in-fog" device but initially they were bought for seeing reindeer in the dark in Lapland! Curiouser and curiouser!

When we were in Germany, my husband discovered a "wonderful" electronics shop in Dusseldorf where one could buy all manner of switches, knobs, resistors, capacitors and the like. He and some other enthusiasts all left for Dusseldorf one Saturday morning at 7 a.m.—to be there when the shop opened.

My biggest agony is to be dragged round the electronics shops up and down the Tottenham Court Road (apologies to any advertisers!) Oh I know I could go shopping on my own in Oxford Street, but I know too that my husband would never meet me at the given time or place later. In fact, I very much doubt whether I would ever see him again.





EMMA

ANALYTICAL ELECTRON MICROSCOPE

A GREAT deal that has been written and said about electron microscopes may tend to be glamourised by their ability to show clear pictures of minute particles beyond the scope of conventional optical instruments.

Although the same can be said about the latest instrument, developed jointly by scientists from A.E.I. and Tube Investments Research Laboratories near Cambridge, it is now possible for the operator to correlate the results precisely with information on elemental composition. This information can be obtained from a much smaller area than has been achieved before, even with separate instruments.

In the new instrument, called "EMMA-4", thin film samples can be electron-optically magnified up to 160,000 times, with a resolution of about 10Å. For the first time, they can be simultaneously probed with an electron beam focused down to about 1,000Å in diameter (about four millionths of an inch) which is over ten times smaller than is possible in the normal electron microscope.

This permits both x-ray spectrometric analysis to identify the elements present, and the production of an electron diffraction pattern characteristics of the crystal structure and orientation, from the same very small selected area.

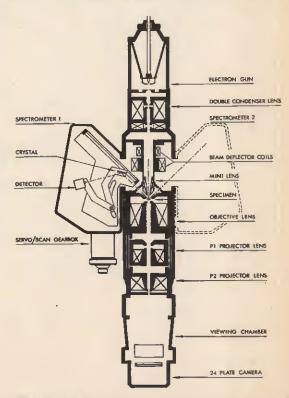
An important characteristic of any instrument designed to perform these functions is ease of operation; the operator must be able to select the facility he requires in a matter of seconds. Only then can the operation of the machine be truly problem-oriented.

It frequently arises, for example, that the classification of a field of particles into several different types requires repeated correlation between position and chemical analysis, with occasional checks on the type of crystal structure. Or again, in a tissue section, details of cell structure may be recognised only by their thin-section morphology, and the chemical analysis of any one feature must be correlated with its position within the cell.

For this reason, particular attention has been paid to the control layout; all controls are grouped on one console and the instrument can be switched very quickly from one mode of operation to another, and all necessary adjustments made from the operating position.

HISTORY AND DEVELOPMENT

The ideas which have culminated in the production of EMMA-4 arose out of earlier work, whereby the first scanning microanalyser was produced. In this instrument, a finely focused electron beam was scanned over a



Simplified section of EMMA-4. The transmission electron image is viewed on a screen at the bottom of the column. X-rays from the specimen are analysed by the crystal spectrometers. Note how the small size of the mini-lens leaves a clear exit path for X-rays from the specimen





F40 watts, Fitted 5/16" bit, Interchangeable bits 1/4", 3/16" 1/8", 3/32" available. Very high temperature iron. For 240, 220, 110, 24 or 20 volts, From 42/6 Spare bits and elements for all models and voltages immediately available from stock.





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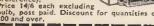
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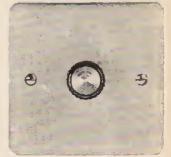
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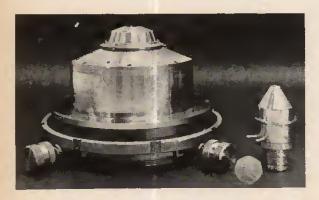
solid specimen; the x-ray emission characteristic of one element present was used to produce an enlarged cathode ray tube image representing the distribution of the selected element over a chosen area. At the same time, the electrons back-scattered from the specimen could be used to present a picture comparable to that produced by an optical microscope.

This instrument proved extremely useful in the identification of local concentrations of residual elements in steel, and of non-metallic inclusions of great significance in the seamless tubemaking process.

A limitation of all instruments dealing with solid specimens is that, due to scattering of electrons within the specimen, the smallest area which can be probed at any instant is about 1µm across. At the same time, neither the electron image, nor the optical microscope with which such instruments are fitted, enables a very high magnification to be used.

EMMA-I

These limitations were overcome by the development of a new instrument in which a thin sample could be used; for example, a metal film, a carbon film carrying particles extracted from a bulk sample, or a thin section of biological tissue. The electrons could then be



A conventional magnetic lens compared with the mini-lens. Elimination of the bulky and heavy Iron core leads to a dramatic reduction in size and a great improvement in performance

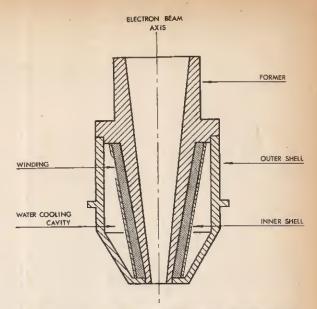
focused into a probe only 1,000Å in diameter, which passes straight through the specimen without appreciable sideways scattering, exciting x-rays from a region an order of magnitude smaller in diameter than is possible with a solid specimen.

Alternatively, the defocused beam could be used to illuminate a wider area of specimen. The transmitted electrons are then used to produce a magnified image on a fluorescent screen, as in a straightforward electron

This was found to be the first practical combination of electron microscope and microanalyser, and was called "EMMA-1", but was built for development of the technique itself without particular regard for convenience in use. The maximum beam energy was limited to 50keV for ease of construction.

SECOND SPECTROMETER

One early improvement was the addition of a second spectrometer, which permitted the simultaneous analysis of two elements. This was more than a time-saving addition; the ratio of the amounts present could be



Simplified section of liquid-cooled mini-lens developed for EMMA-4. The precision winding is supported on a copper former, and there is no magnetic core of any kind. This design not only improves focusing performance but gives better access to the specimen

measured independently of any slight instability of the specimen, since small drifts affect equally the x-ray intensity from each element.

It soon became evident, however, that the beam energy should be increased to a level similar to that of conventional electron microscopes—say 100keV, to give adequate penetration of a wide range of sample types. The main difficulty here was that this would require heavier lenses. In particular, the probeforming lens would be a heavy and bulky item, tending to obscure the x-ray path into the spectrometer.

MINI-LENS

It was at about this time that the Technical University of Delft showed that, if the lens windings could be formed accurately enough, no iron shield or pole-piece would be necessary. Elimination of these heavy and bulky components itself made even smaller windings possible, the result being a spectacular reduction in overall size of the lens—the now well-known "mini-lens", in fact.

It then became apparent that the new A.E.I. EM802 microscope would provide an ideal instrument in which to mount such a lens, having adequate space in the region above the specimen for this purpose, and room on the column to attach two spectrometers.

The joint development work was started, the prime aim being to add the microanalysis system to this microscope with a minimum of modification.

A special design of mini-lens was evolved by T.I. together with a new form of high-sensitivity spectrometer, while A.E.I. concentrated on the specimen stage and other aspects of the microscope. The work was completed in under two years with the emergence of the prototype "EMMA-3".

The production version, "EMMA-4", differs from EMMA-3 only in having the instrument and control equipment fully integrated into a single operating console.



Controls are conveniently grouped on the operating console in the production EMMA-4



Transmission Electron Micrograph

10 microns

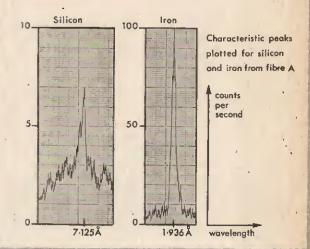


Fig. 1. Electron micrographs diffraction pattern and spectrometer plots identifying fine particles of aluminium nitride in a tube steel

EMMA-4

The microscope column of "EMMA-4" is mounted in the centre of the console, the spectrometers attached on either side. Control of the spectrometers is simplified in that each one carries a tuning scale, which is set out something like that on a radio receiver. Four wavebands are selected by different crystals and each is calibrated directly in x-ray wavelength with each station marked by element name. Tuning may be carried out either by a fine manual control for accurate wavelength determinations or by a servo system, enabling any one of six preset elements to be selected by push-button. A complete spectrum may also be plotted on a chart recorder with the aid of a slow-scan motor. The instrument can analyse for all elements from atomic number 11 (sodium) to atomic number 92 (uranium).

Six specimens up to 3mm in diameter, some of which can be calibration standards for microanalysis, may be accommodated on the specimen stage. These are directly interchangeable without breaking the vacuum but when reloading is necessary, the stage may be withdrawn from the column through an airlock.

APPLICATIONS

EMMA-4 offers unique facilities for the intensive and correlated examination of the morphology, chemical composition and crystallographic structure of extremely small specimen areas. It is expected to be useful in many fields of research where thin film examination is feasible and relevant. Obvious areas are metallurgy, where the prototype instruments have already provided valuable new information on the composition of

precipitates and inclusions in steels; biology, in which it has great potential in the examination of bone and tissue sections; and generally for the analysis of particles deposited on thin substrates.

DETECTING SURFACE CRACKS ON STEEL TUBING

During the final stages in the manufacture of steel tubing, the base material is subjected to very severe mechanical working at elevated temperatures. This can result in the surface of the tubes breaking up and the incidence of such defects can be related to the aluminium content of the material.

It is, therefore, important to find where the aluminium is located and since the distribution turns out to be on a very fine scale, the electron microscope is one of the few research tools which can be usefully employed. With the facilities afforded by EMMA-4 it is possible to identify one site for aluminium as a precipitate of aluminium nitride. The aluminium content of the particles is demonstrated by x-ray microanalysis and the specific compound confirmed by electron diffraction.

Fig. 1 illustrates the results of a study of an extraction made from a tube showing surface defects. The precipitates are supported on a carbon film in the conventional manner for electron microscopy. Particle A is identified as aluminium nitride and particle B, and its surrounding neighbours, as pearlite (Fe₃C)—a normal precipitate in the material. The smaller of these particles (A) measures only 1,500Å across and is therefore well below the detection limit of the normal electron probe microanalyser (about 1 micron).

Transmission Electron Micrographs





5 Microns



Electron diffraction pattern from particle A

Characteristic x-ray peaks from particles

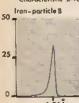






Fig. 2. Electron Micrographs and spectrometer plots showing presence of AMOSITE asbestos fibres in human lung tissue

ASBESTOSIS IN HUMAN LUNG

An example of the application of the EMMA-4 technique in medical research concerns the study of asbestos fibres extracted from human lungs.

Recent work in several laboratories has demonstrated the danger of inhaling such fibres, and has shown that the ill-effects may not manifest themselves until many years after the inhalation. The problem therefore arises of establishing to which group of the asbestos materials particular extracted fibres belong, in order to be able to relate this to the lung damage and also to trace the source.

Fig. 2 illustrates the type of results obtained with the new instrument. The transmission image shows the fibres on this sample, a lung tissue section, to be as thin as about 1,000Å, often with "trains" of growth along them (top centre of the image). Surface and internal detail are also made visible.

The direct spectrometer output in the form of peaks plotted for silicon and iron (K) radiations from the fibre A is also shown in this illustration. Simply by measuring fibre composition in the form of element ratios from such peaks it is possible to identify these particular fibres as AMOSITE asbestos. Further confirmation can be obtained by electron diffraction, if required.

The essence of the problem posed by this particular specimen, i.e. the 'correlation of chemical, morphological and crystallographical information on a submicron scale is, of course, very general and it is for this reason that the scope for application of the new instrument is likely to be very widespread.

SEPTEMBER

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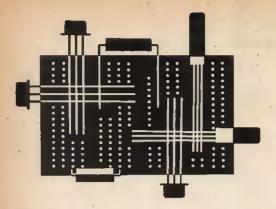


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ELECTRONICS



THE new series of practical subjects for beginners to build commences in this issue. Subsequent articles in the series will be easily identified under the "Beginners" heading in the Contents and by the symbol which will appear at the beginning of each article.

THE projects are shown built up on a "breadboard" system for four main reasons.

- Whilst the initial cost of the systems may be high, this could be more than offset by the fact that components can be easily removed, re-positioned or used again in a more permanent construction.
- 2. The circuit can be assembled very quickly or expanded by adding extra functions later.
- 3. The actual layout of the components can follow a similar layout to that in the circuit diagram,
- Soldering is only needed for connecting wires to large components, such as switches and potentiometers; inter-component wiring is already provided.

USING T-DEC

The "breadboard" system used is called T-Dec. It is a manufactured plastics base plate with a matrix of numbered holes. Certain combinations of interconnection are provided by spring strips underneath the holes. These are snown in Fig. 1a corresponding to the raised lines moulded on to the surface of the board itself.

T-Dec is divided into two sections which are electrically isolated, enabling two or more separate circuits to be built on to the same board. If required any part of one circuit can be connected to any part of the other circuit by using single strand copper link wires.

Some components have very thin connecting wires; these should be helped into the holes by holding the wire with a pair of long-nose pliers.

Transistor and diode wires can be inserted directly into the holes if spacing permits. It may be necessary to open up the spacing of these wires; in which case, careful bending with pliers at least \(\frac{1}{2}\) in from the encapsulation can do this without damaging the transistor or diode seal. Alternatively, special adaptor plugs supplied by the T-Dec manufacturers can be used to mount these components.

PROJECT

The component wires should be at least 3 in and preferably 5 in long to ensure satisfactory connection. Longer wires will of course, make the components more versatile in their use. It is never good practice to trim these wires short if they are to be used again.

Whole systems of breadboarding can be built by fitting two or more boards together by the dovetail tongues and grooves around the sides. Small panels for switches, potentiometers, lamps and so on are provided and are easily fitted into the slots on the edge of the boards.

HOLE IDENTIFICATION

Coming now to the numbering of holes for identification you will notice that the T-Dec has two blocks side by side with letter references A to H on both.



Fig. 1a. The T-Dec breadboard. Notice the connections between holes are shown as raised lines

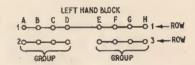


Fig. 1b. How the T-Dec holes are identified. Only the first two rows are shown here

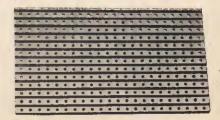


Fig. 2a. Underside view of Veroboard showing the copper strips

BUILDING -

for BEGINNERS

The numbers run in sequence for each row or group of holes in a row (see Fig. 1b). It is important not to be confused with these since, in each alternate row per block, there are two groups of four holes which are numbered separately.

In the other rows connection is already indicated between the two groups; these cannot be separated. If insufficient holes are available for a particular junction of components, a link wire can be carried to another vacant group elsewhere on the board.

ALTERNATIVE CONSTRUCTION

Some readers may prefer to use alternative construction systems, perhaps in a more permanent form. These will probably require the use of a soldering iron and, although component recovery is possible, it is not as easy as with T-Dec.

Suggestions for some construction systems are given here, using mainly some form of s.r.b.p. sheet machined or treated by proprietary manufacturers.

In order to simplify translation from T-Dec to these other forms, the same basic layout is assumed and connection code numbers correspond. If the board is too large, it can be trimmed before commencement to the size required, but the basic layout remains the same.

COPPER STRIP WIRING BOARD

Veroboard is the first of the alternative examples here because translation is very straightforward. Fig. 2a shows this board with the copper strips on the underside. To keep the same layout appearance the holes are numbered in sequence so that the top surface is that without the copper.

If the copper strips are cut to conform with the T-Dec



Fig. 2b. Veroboard with the strips cut to show the T-Dec wiring pattern

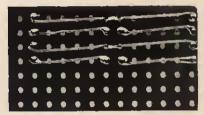


Fig. 4a. Plain perforated s.r.b.p. sheet with copper wire connections and soldering pins



Fig. 3a. Veroboard strips prepared for the first project

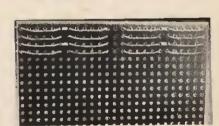


Fig. 4b. Plain s.r.b.p. with the connecting wire hooked through the end holes in the rows

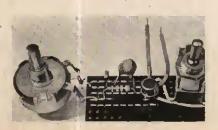


Fig. 3b. The finished metronome project



Fig. 5. Cir-kit adhesive copper strips fixed between rows of holes on plain perforated board

layout the appearance would be as shown in Fig. 2b.

The strips can be cut with a special spot-face cutter,

a kin drill, or a sharp knife.

Before cutting any strips, study the project circuit layout in the practical article to see how many breaks are really necessary. If only one half of the T-Dec is used none of the centre breaks will be necessary. However, if at a later stage you decide to assemble another circuit on the same board, the copper around the centre columns of holes, between column H on the left and A on the right, will need to be cut. Before doing so, check to see if any links are needed between left and right, in which case leave the appropriate strips uncut.

Next look at the project layout to see if any connections are needed between column D and column E. Having established those required cut all the other copper strips between D and E to form the groups of

four holes (Fig. 3a).

Now the columns and rows of holes can be numbered exactly as for T-Dec. You can do this by laying the board on a sheet of paper and marking through each required hole in the board with a pencil. Remember that the T-Dec numbering follows that for Veroboard that has the copper side face down.

Carry out the assembly and soldering making sure that no solder bridges two or more adjacent strips. Good clean soldering is the keynote to success; dry joints will not do. Fig. 3b shows the finished project.

PERFORATED S.R.B.P. AND WIRE

The next system is simple and follows the same lines as with Veroboard, except that plain perforated board has no copper face. All connections are carried out using soldering pins and tinned copper wire; see Fig. 4a. However, do not fit wires that are unlikely to be used; this is a waste of materials and effort.

The pins can be dispensed with if the copper wire is hooked through the end holes of each row and secured with solder. An example of a typical layout is shown

in Fig. 4b.

STICK ON WIRING

The third system is a development of the previous one except that the wires are replaced by self-adhesive copper strips called "Cir-kit". The method is otherwise exactly the same (Fig. 5). The narrow strip will just fit between adjacent rows of holes on plain perforated board.

PRINTED CIRCUIT

There is no reason why printed circuit board should not be used. This will require more patience by following the instructions given with the printed circuit kit. Not all kits carry instructions, so if you are unfamiliar with printed circuit techniques try and obtain a kit that has.

It will probably be necessary to sketch out a layout of the copper pattern corresponding to the project actually being built. It is recommended that an experienced friend helps you with this as mistakes can be expensive.

This short introductory article is not intended to provide comprehensive details of using these alternative methods. Full details and instructions can be obtained from manufacturers of these and other proprietary items which are advertised in this magazine.

The project which follows can be built very easily using one of the methods described here. Future projects in the same series are to be dealt with in a

similar manner.



To study a musical instrument, one of the most important requirements is strict attention to playing speed. To assist in the correct interpretation of the music's tempo the composer conveniently heads his composition with a rough guide to the rate at which it should be played like Andante or Allegro, this usually being followed by the number of crotchets, quavers, etc. that should be played per minute.

Whilst the accomplished musician has little difficulty in interpreting these tempo marks, the beginner does need some sort of aid to assist in establishing a sense of

time.

More than a hundred years ago Maelzel provided such an aid in his invention of the mechanical metronome which produced loud ticks with the movement of a weighted pendulum. With the simple electronic metronome to be described, we can reproduce these ticks just as effectively without the labour of winding up springs.

RELAXATION OSCILLATOR

To simulate the sound of its mechanical counterpart the circuit of Fig. 1 was designed to produce asymmetric pulses of short width and rapid rise and fall times. The pulse generated across the loudspeaker LS1 is shown in this diagram, and it ensures a very rapid cone movement.

The frequency range extends from 40 to 220 beats per

minute, which is adequate.

As this little device is very precise in its counting, it can also be used as an audible "darkroom" timer when

set to 60 beats/minute.

The circuit itself is a simple relaxation oscillator where two complementary *npn* and *pnp* transistors are made to switch on and off at a rate determined by the resistance chain VR1, R1 and capacitor C1. With S1 closed, C1 charges until it reaches about 650mV when TR1 is switched on and immediately discharges the capacitor.

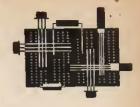
The current pulse produced by TR1 in turn switches on TR2 with the result that almost the whole of the supply voltage is made to appear across the loudspeaker.

The actual discharge time of the capacitor depends on the base-emitter impedance of TR1, the loudspeaker impedance and the output impedance of TR2 which collectively account for the exponential hump on the output pulse waveform.

With the completion of the pulse the capacitor again charges to the conduction potential of TR1, when the

pulse cycle starts again.

METRONOME



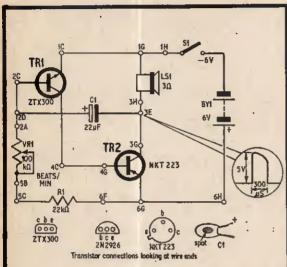


Fig. 1. Circuit diagram of the metronome showing the T-Dec hole connections, transistor wire identification and output waveform

COMPONENTS.

RI 22kΩ 10% + watt carbon

Potentiometers

VRI 100kΩ linear carbon

Capacitor

CI 22µF tantalum elect. 16V

Transistors

TRI ZTX300 (Ferranti) or 2N2926 orange spot

KT223 (Newmarket) GET102 (Mullard) TR2 NKT223

Switch

SI on/off toggle switch

Loudspeaker

LSI 3Ω 5in permanent magnet moving coif unit

Battery BYI 6V type 996

Miscellaneous

T-Dec. .

Single strand connecting wire Battery connectors or clips

LOW LEAKAGE

In the application of this unit timing precision is important. The simple factor most likely to give trouble in this aspect is leakage current. The choice of a silicon transistor for TRI and a tantalum electrolytic capacitor for C1 virtually eliminates the problem.

In the choice of speaker it will be found that sound output is a function of cone diameter. In practice, a

5in speaker proved very satisfactory.

CONSTRUCTION

Construction of the unit merely involves plugging the components into the T-Dec as shown in the photograph: For the holes employed refer to Fig. 1, which shows the hole numbers for each junction.

If it is intended to make a permanent unit of this, the wiring configuration will readily translate to any of the board constructional methods outlined in the intro-

ductory article.

If such construction is undertaken the potentiometer setting must be calibrated in terms of the number of beats produced per minute. Using a wrist watch with seconds sweep or preferably, a stop watch, the potentiometer should be advanced at 20 beat intervals. These positions can be recorded on a piece of white card. A pointer knob attached to the potentiometer shaft will simplify this operation.

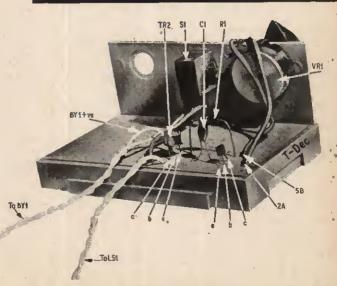


Fig. 2. The layout of components on T-Dec. Make sure the battery is correctly connected



APOLLO 13 RESULTS

The results of the special investigation into the results of the Apollo 13 troubles have been released by the chairman of the committee, Edgar M. Cortright. The explosion was caused by the failure of two thermal switches in the system which controlled the heater inside the oxygen tank. The failure allowed the wires inside the tank to heat up to a high temperature, the insulations burned off and the spark resulting from the short circuit caused the explosion.

The cause of the failure of the switches is thought to be the detanking sequence which is part of the countdown procedure. This procedure does in fact place a much more severe strain on the system than the actual spaceflight. The reason for this is that during the checking sequence the heaters are on for a much longer period and at a higher current level than when in flight.

The necessary modifications are being carried out and at the time of writing the next launch is not likely to take place before December 3 this year.

MARINER 7 PHOTOGRAPHS PHOBOS

Mars has two satellites, Phobos and Diemos, and one of these satellites has been successfully photographed by *Mariner 7*. Both are very small and near to the planet surface, Phobos being some 3,700 miles from the surface and Diemos about 12,500 miles.

The Mariner spacecraft was about 82,000 miles from Phobos when the picture was taken. The satellite was near one of the dark areas on Mars known as Syrtis Major, and appeared as a dark spot on the lighter background of the Aeria region.

Analysis of the photograph was carried out by Dr Bradford A. Smith of New Mexico State University, and he deduced that the satellite was oval shaped with a diameter of 13.75 miles in the plane of its orbit and 11.25 miles diameter across its poles. A significant result of the analysis is that the "albedo" (the ability to reflect light) has proved to be very low, the lowest in fact of any satellite or asteroid in the solar system.

The darkness of the satellite appears to be due to its small size

and dust from the surface could easily escape due to the low gravity. In fact it is so low, that should one of the suggestions that it could be used as a space station be implemented, the personnel would have to be careful not to jump with too much enthusiasm or they might go into orbit. The escape velocity is 12 metres a second.

Since the satellite is elongated it is unlikely that it came into being by accretion and it is possible that it is a captured asteroid.

GERMAN SATELLITE

The contract for the construction and systems management of Aeros, the second German satellite, has been awarded to the Dornier-System GmbH. Aeros is the successor to the recently launched Azur and is devoted to the study of the physical processes in the upper layers of the atmosphere. There will be five experiments, four German and one American and it is expected that it will be put into orbit in the summer of 1972, from the Vandenberg test range in California using an American Scout rocket.

The instruments to be carried for the German experiments are a mass spectrometer for the study of the atmosphere's chemical composition. This is done by measuring the number density of ions and neutral particles. An impedance probe will determine electron density in the ionosphere. A retarding potential analyser will measure the energy distribution of electrons and ions. An ultraviolet spectrometer will measure the flux and spectral distribution of the far ultraviolet radiation of the Sun.

The American experiment will measure the nitrogen present in the various layers of the upper atmosphere and the overall density of the neutral particles.

As the results of the last experi-

An engineer uses a microscope to examine and find the cause of discolouration to the Surveyor 3 television camera landed on the moon in April 1967, and returned to Earth by the Apollo 12 astronauts last November.

The scientists expect the study to provide a guide in selecting materials and components for future space exploration.

ment are required for a NASA satellite due to be launched in 1973, it will be essential that the construction programme and launch date be on time. The planned orbit is a specially selected one and the satellite will be placed in a polar orbit with a perigee of 235km and an initial apogee of 1,000km. The friction of the atmosphere at these altitudes will cause the satellite to fall towards the Earth.

After 105 days the apogee will have been reduced to 580km; at this point it will be raised again by 200km using a hydrazine chemical rocket. The reason for doing this is to collect data from comparable altitudes at different times of the year.

different times of the year.

After a period of six months at this new altitude the satellite will then enter the denser parts of the atmosphere and finally burn up.

Measurements during the final phase of its life are expected to be of considerable interest.

After each measuring orbit there will be one or two idle orbits to allow the batteries time to be recharged and the stored data transmitted back to Earth. The satellite is an airtight cylinder with one flat and one conical end.

NIMBUS D SATELLITE

Nimbus D was launched from the Western test range in California by a Thorad Agena D. The butterfly shaped satellite weighs 620kg, and is in a circular near polar orbit 1,110km above the Earth and orbits in 107.3 minutes.

The British experiment was developed by GEC-Elliot for Oxford and Reading Universities and uses a very sensitive selective chopper radiometer which can detect radiation at low levels over six discrete bands. The measurements will give the first complete continuous picture of the 15 micron radiation. The temperature field in the region 25-50km above the surface and the conditions below 25km will be of considerable importance to forecasting in the future.

GEC-Elliot are now working on Nimbus E due to be launched in late 1972. In this satellite the number of channels will be increased to 16. The Meterological Office will check the data against Radio Sonde measurements and provide daily charts for the Northern Hemisphere with information relating to several levels.





Practical Electronics August 1970 625

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EF94	15/6	PD500	30/6	Z759			
			30/0	2/37	24/6	30PL13	18/6
EF95	12/6	PFL200	14/9		8/6		18/6
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	CME1703	6.12.0	4.12.6
	CME1706 CI7AA	6,12.0	4.12.6
	CITAR	6.12.0 6.12.0	4.12.6
AW43-88	CME1705	6.12.0	4.12.6 4.12.6
AW47-90	CITETIOS	4.12.0	7.12.0
AW47-91	A47-14W	7.13.4	5, 7.6
A47-14W	CMEI90I	7.13.4	5, 7.6
	CME1902	7.13.4	5. 7.6
	CME1903	7.13.4	5. 7.6
	CI9AH	7.13.4	5. 7.6
A47-13W	CME1906	10. 5.6	8.10.0
A47-11W	CME1905	8,17,3	7. 0.0
A47~26W A47~26W/R	CME1905	8.17.3	7.15.0
A50-120W/R	CME1913R CME2013	7. 6.8	
AW53-80	CPIEZUI3	8.81.8	/ = 4
AW53-88	CME2101	8.18.8	6. 5.0 6. 5.0
AW59-90	CITEZIOI	0.10.0	0. 5.0
AW59-91	CME2303	9.11.8	7. 4.0
A59-15W	CME2301	,,,,,,	11 410
	CME2302	*	
	CME2303	9.11.8	7. 4.0
A59-11W	CME2305		
A59-13W	CME2306	13.13.0	10.19.6
A59-16W A59-23W	CME2306	13.13.0	10.19.6
A59-23W/R	CME2305	12.12.0	10.10.0
PORTABLE SET	Tripec	12.12.0	10.10.0
TSD217	I O D E 3		6.15.0
TSD282	•		6.15.0
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TERMS, CASH WITH ORDER ONLY. POST AND PACKING PAYABLE ON ORDERS UP TO £3, AFTER THAT, FREE EXCEPT C.R.T.'s.



A square wave generator for calibrating oscilloscope Y amplifiers, and the frequency compensation of probes and attenuators.

Is also useful as a general purpose unit for checking audio amplifiers, tone control circuits, Schmitt triggers, monostables, etc.

SPECIFICATION -

OUTPUT

Square wave, 10V peak-to-peak max.

OUTPUT LEVEL 0.1V, 0.2V 0.5V, 1V, 2V, 5V, 10V

FREQUENCIES 1kHz, 10kHz, and 25kHz CALIBRATION With ordinary d.c. voltmeter

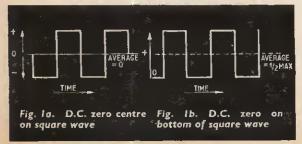
RISE TIME Better than 1µs

NE problem often associated with home constructed projects is that of calibration. This article describes a small unit for calibrating the "Y" amplifier of an oscilloscope.

The best calibration waveform for this purpose is the square wave, its flat top and bottom make it easy to see and align with graticule markings. It can also be used for adjusting the frequency compensating capacitance of an attenuator or probe. Having decided on the waveform, we need a method of calibrating the calibrator.

USING A VOLTMETER

A conventional multimeter could be used on the a.c. voltage ranges (but see end of article). Rather old a.c. meters are not recommended because their meter rec-



tifiers tend to change their characteristics with age. In any case, multimeters are usually considered to be more accurate and are more easily checked on the d.c. ranges. It would, therefore, be more convenient to use the d.c. ranges because the meter is an average reading instrument.

If we try to measure a square wave voltage on a d.c. meter, the reading will be zero (Fig. 1a) because the positive parts of the waveform cancel the negative sections. If we offset the d.c. level to the bottom of the square wave, the meter will read half the maximum (Fig. 1b).

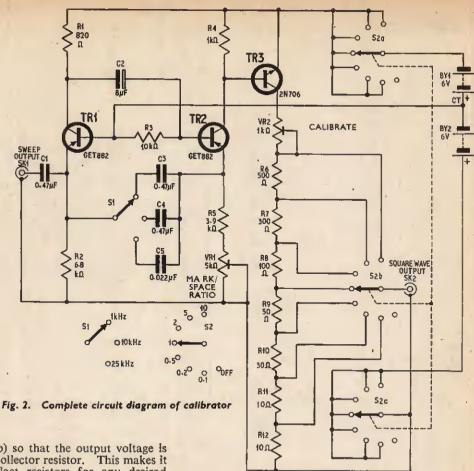
EMITTER TIMING CIRCUIT

The circuit (Fig. 2) is quite straightforward, consisting of a multivibrator followed by an output stage. The multivibrator, TR1 and TR2, has the timing components in the emitters and uses only one capacitor. This is an advantage if different frequencies are required since only one capacitor is required for each frequency.

It is also possible to adjust the frequency by varying the value of the collector resistor of TR1. This makes it possible to set the multivibrator to an exact frequency if required.

The basic frequency of the instrument is lkHz; this is a "standard" frequency for voltage calibration and is used on commercial oscilloscopes.

The output transistor TR3 has its current set to 10mA



by VR2 (see setting up) so that the output voltage is directly related to the collector resistor. This makes it a simple matter to select resistors for any desired sequence of output voltages.

The output is taken from this resistor, the earth being the positive side of the supply. This method of connection gives the d.c. level to the signal. This resistor is divided into sections which subdivide the output voltage in a 1, 2, 5 sequence from 100mV to 10 volts peak-to-peak.

Only the 10 volts position of output voltage selector needs to be adjusted; all other positions depend on the accuracy of the resistors used.

CONSTRUCTION

Layout is not critical, except that the voltage selector switch and VR2 should be close to TR3. See Fig. 3. The resistors used in the voltage selector switch should be selected to 2 per cent or better from 5 per cent stock; all other resistors can be 5 per cent.

Any transistors having similar specifications to those quoted should work satisfactorily. Take care to connect them correctly; the first two are pnp and the output transistor is an npn type.

SETTING UP

After checking the wiring for errors, switch on and view the output on the oscilloscope. Set the mark space ratio to exactly 1:1 by adjusting VR1. Then, set the output switch to the 10 volts position, connect a d.c. voltmeter to the output socket and adjust the set output control until the reading is 5 volts. The unit is now ready for use. Connect it to the "Y" amplifier input on the oscilloscope.



COMPONENTS.

Resistors

RI 820Ω 59 6.8kΩ 5%

10kΩ 5% R3

R5

 $1k\Omega$ 5% $3.9k\Omega$ 5% 500Ω ($1k\Omega + 1k\Omega$ in parallel) 300Ω ($150\Omega + 150\Omega$ in series) R7

R8 100Ω

R9 50Ω ($100\Omega+100\Omega$ in parallel) R10 30Ω ($15\Omega+15\Omega$ in series) R11 10Ω

All & watt, 5% carbon except R6 to R11 at 2%

Potentiometers

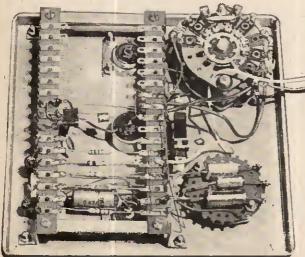
VRI $5k\Omega$ skeleton preset or slider preset VR2 $-1k\Omega$ linear preset control

Capacitors
C1 0.47 μ F polyester 5%
C2 8 μ F elect. 15V
C3 0.47 μ F polyester 5%
C4 0.047 μ F polyester 5%
C5 0.02 μ F polyester 5%
(See Table !)

Transistors TRI, TR2 GET882 or 2N1305 (2 off) TR3 2N706

Switches

 Single pole, 3-way rotary switch
 3-pole, 7-way (8 positions minimum) can be made up from wafer switch parts, two or three wafers, up to 12-way, 8 used



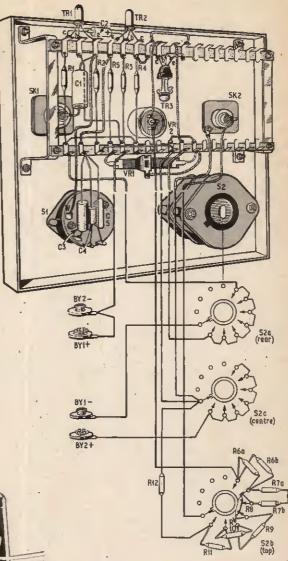


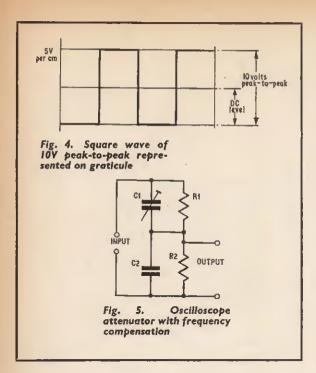
Fig. 3. Wiring and component layout

Sockets (with plugs)
SKI, SK2 Coaxial panel mounted sockets and plugs or "u.h.f." style p.t.f.e. connectors as on model

Miscellaneous

Aluminium case to hold components and batteries approx. $6in \times 5in \times 5in$

Miniature tag strips, knobs and wire



USING THE CALIBRATOR

To calibrate an oscilloscope, set the calibrator output voltage switch to the 10 volts position, set the "Y" input switch on the 'scope to 10 volts per centimetre and adjust the preset "Y" gain control until the top and bottom of the square wave are in line with graticule lines 1 centimetre apart (Fig. 4).

Repeat this for the other ranges, checking that the square wave is not distorted on any of them. If it is, adjustment of the attenuator trimmer should correct this to a good waveform with a square corner and flat top. Incorrect compensation will show up as overshoot of the leading edge (over compensated) or as a rounded corner (under compensated).

It does not matter if the 'scope is a.c. or d.c. coupled. If the 'scope is a.c. coupled it will be immune to the d.c. level in the signal. If the 'scope is d.c. coupled a slight readjustment of the "Y" shift control is all that is required.

The signal has a d.c. level so that the unit can be calibrated using an ordinary d.c. voltmeter (preferably an Avo "8"). Once the mark space ratio is set to 1:1 the d.c. level is always half the peak to peak value. This feature makes it unnecessary to use Zener diodes to stabilise the supplies, since it only takes a moment to check the calibration.

FREQUENCY COMPENSATION

As well as voltage calibration the unit is also useful for frequency compensation of attenuators and probes.

The risetime is better than 1μ s and the top is flat so that observation of the unit's waveform on the 'scope under test will show if adjustment of the 'scope is required.

The circuit of a typical 'scope attenuator section is shown in Fig. 5. When in correct adjustment the time constant of C1, R1 will be equal to that of C2, R2.

Because a square wave contains high frequency components in the verticals and low frequency com-

ponents in the flat sections, a square wave at the input will be undistorted at the output only if C_1 R_1 equals C_2 R_3

In practice the unit is connected to the 'scope input, the waveform is observed and any departure from the correct waveform is compensated for by adjustment of the trimmer C1 in Fig. 5.

OTHER USES

Apart from these two jobs the unit is useful as a square wave generator for general purposes. Checking audio amplifiers, tone controls, Schmitt triggers, monostables and other switching or CR circuits.

The ramp output SK1 is for checking trigger circuits. If the oscilloscope is fitted with a "Trigger Level" control it should be possible to select any point on the

ramp and trigger at that point.

To make the unit more useful as a general purpose square wave generator, two other frequencies are available. These are (on the author's unit) 10kHz and 25kHz. When the original was built, these two frequencies were chosen, together with a slightly different output stage which gave a much faster rise time, for work on oscilloscope delay lines.

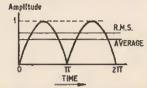
They are rather high for audio work though, and some constructors may prefer lower frequencies such as 500Hz and 5kHz for this work. All that needs to be done is to change the timing capacitor, C2, as indicated in Table 1.

Table I. EMITTER COUPLING CAPACITANCE Frequency Capacitance 500Hz 1.0 µF IkHz 0.5 uF 0-1µF 5kHz 10kHz 0.05µF 0.025uF 20kHz 0.02 uF 25VHz

METER MEASUREMENTS

There is sometimes confusion about measurements with moving coil meters and especially about the terms "average" and "r.m.s." when applied to readings taken with such meters. The output waveform from the meter rectifier on sine waves is shown in Fig. 6. If the

continued on page 654



To find the average value of the sine between zero and π , find the area and divide by the base.

Area =
$$\int_{0}^{\pi} \sin x \, dx = \left[-\cos x\right]_{0}^{\pi} = [1] - [-1] = 2 \text{ sq. units.}$$

Average $=\frac{2}{\pi}=0.637$

Form factor = $\frac{0.707}{0.637}$ = 1.11

Fig. 6. Meter rectifier output wave form for sine wave input. To find the average value of the sine between zero and π find the area and divide by the base



PHOTOELECTRONIC DEVICES

By J. B. Dance, M.Sc., B.Sc. Published by Hiffe Books Ltd. 172 pages, 8½in × 5½in. Price 42s.

to the exploitation of the photoelectronic effect. It follows that full appreciation of electronic circuits is not possible without a good knowledge of photoelectronic devices. This book is timely and offers a sound introduction to the subject to readers who have a previous knowledge of basic physics to about G.C.E.

"advanced" level.

After an introduction to the basic physics of infrared, visible light and ultra-violet radiation, there follow chapters on semiconductor fundamentals, with emphasis on electron energy levels, and photoemissive materials. The remainder of the book deals with a variety of different devices: evacuated tubes, such as photoemissive diodes, photomultiplier tubes, and image intensifiers and converters; semiconductor photodevices, including junctionless photoconductive cells such as the familiar cadmium sulphide and cadmium selenide devices; junction photodevices such as phototransistors, and more sophisticated integrated circuit light detectors, based on new principles.

The final chapter is devoted to electroluminescent devices and provides a valuable curtain raiser to what is undoubtedly going to be a most exciting develop-

ment area in the future.

To the student and amateur enthusiast alike, the value of this book is enhanced by the inclusion of practical circuits illustrating some everyday applications for the devices described. Component values are included, and device types are specified.

F.E.B.

M.A.C.

110 SEMICONDUCTOR PROJECTS FOR THE HOME CONSTRUCTOR

By R. M. Marston Published by Iliffe Books Ltd. 125 pages, $8\frac{1}{2}$ in \times $5\frac{1}{2}$ in. Price 18s (soft back).

Basic differences between silicon and germanium transistors and their circuit configurations provide an essential introduction to the common usage of silicon devices. From here on this book describes many well established circuits or "building bricks"

which can be found elsewhere.

With a title such as this book carries, one would expect to find more practical details in addition to theory, such as is found in the book "Using Semiconductors" (reviewed in our May issue). This book has no practical guidance at all, and it is left to the "home constructor" to sort out the information himself. He can do much the same by obtaining technical application reports.

The circuits dealt with include one- and two-stage linear amplifiers (small signal only), switching circuits, regulators, f.e.t. amplifiers, unijunction oscillators, s.c.r. switching at low voltages, and a variety of circuits using the simple "dual gate" integrated circuit.

CIRCUIT CONSULTANT'S CASEBOOK

By T. K. Hemingway Published by Business Books Ltd. 210 pages, 9in × 5\(\frac{3}{2}\)in. Price 75s.

For circuit designers and trouble shooters alike, this excellent volume goes a long way towards attacking design defects that are all too often overlooked.

Although a circuit can be designed to function fairly easily by using reference works, there are factors which can make the reliability of long term safe operation an unknown quantity. The principle concern of the author here is to safeguard transistors in spurious, irregular, or transient overload conditions.

As Head of Electronic Technology at the Guided Weapons Division of B.A.C., it is easy to understand that diagnosis and cure are by-products of a reliability conscious designer. Yet he has attempted here to help other designers to adopt such an approach to first principles design philosophy.

The text is written in an absorbing manner and should be of value to designers with a fairly broad

background in circuit design.

While openly admitting that the examples given are not intended to be the last word in all applications, the author does set the designer on his toes for some of

the more common pitfalls.

This book is divided into two parts: Part I discusses basic design problems, common errors and their correction; Part 2 deals with the ways of meeting specification requirements not readily achieved by standard textbook circuits. The maths is kept to a minimum and only involves the simple algebra normally expected in basic principles.

It is a curious thing that some of the best books on electronics tend to be pricy, but 75 shillings spent on this could save several pounds on damaged components.

M.A.C.

LUMINESCENT SCREENS, PHOTOMETRY AND COLORIMETRY

By J. Kalmer M.Sc. Published by Iliffe Books Ltd. 200 pages, 8½in×6½in. Price 60s

As the title of this book suggests, colorimetry and photometry form the subject matter, it is not concerned with luminescence generally, and anyone expecting an explanation of the luminescence mechanism will be disappointed.

The author is concerned only with cathodoluminescence (this is the principle used in cathode ray tubes where phosphors are excited by an electron beam) and then only with the testing of emitted light rather than production of the radiation. Other forms of luminescence, photoluminescence, electroluminescence, etc. are defined on page 1 and then disregarded.

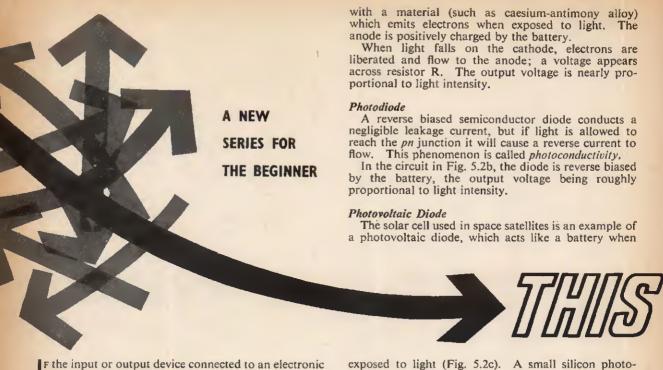
As a book on television screen testing, however, it is difficult to rival. The author, a Czechoslovakian, has had many years experience in objective methods for assessing TV picture quality in both monochrome and colour and practically all aspects are covered. Chapter four, "Colour Measurements" is particularly good.

This book is likely to be of interest to the television enthusiast, particularly with regard to colour, but it is not for casual, general interest reading. The testing methods described are not for the amateur, they are rigorous and require a well equipped laboratory. Mathematical treatment is used throughout.

In all, a very specialised book, but certainly an

authoritative work in its field.

K.J.M.



F the input or output device connected to an electronic circuit converts one form of energy into another it is called a "transducer".

The block diagram in Fig. 5.1 shows a typical transducer application, the Geiger counter. A Geiger Müller tube converts energy resulting from radioactive decay processes into pulses of electrical energy, which are then amplified for conversion into "clicks" of sound energy by a loudspeaker.

In the following descriptions transducers are grouped under six main headings; light, heat, sound, magnetism, motion, and atomic radiation, denoting the type of

energy conversion involved.

LIGHT SENSORS

Photoemissive Cell

The photoemissive cell in Fig. 5.2a consists of two electrodes in a vacuum or gas. The cathode is coated

ATOMIC RADIATION

GEIGER TUBE
INPUT TRANSDUCER

Fig. 5.1. Block diagram of a simple Geiger counter with the circuit symbol for a Geiger-Müller tube

exposed to light (Fig. 5.2c). A small silicon photovoltaic diode will generate a current of several milliamps at a potential of about 0.5V in direct sunlight,

Photovoltaic cells used in photographic light meters employ selenium as the photosensitive material.

Light Dependent Resistor

A photoresistor or light dependent resistor (Fig. 5.2d) has a resistive element, usually made of cadmium sulphide, contained in a transparent case. When light shines on the element its resistance decreases. In the circuit in Fig. 5.2d, the output voltage increases with illumination.

The photoresistor is not polarised like a diode, and behaves like an ordinary resistor under conditions of constant illumination, so can be fed from an a.c. as well as d.c. source.

Phototransistor

The phototransistor has a built-in amplification characteristic. Light on the base-emitter junction causes an internal base current to flow, even when the base lead is left disconnected, and this gives rise to a much larger collector current. In the circuit in Fig. 5.2e, the output varies inversely with light intensity.

Response

There is a limit to the speed with which a photosensor will respond to rapid changes of light intensity. For example, the output signal from cadmium sulphide photoresistors and selenium cells tends to fall off if the light input is made to pulsate rapidly at frequencies in excess of a few hundred hertz.

Ordinary silicon phototransistors and photodiodes can respond quite well to light pulsating at 20kHz, while special photoconductive diodes will reach 300MHz. The upper frequency limit of photoemissive cells is theoretically high, but is usually limited in practice, by the high impedance of the device, to around 25kHz.

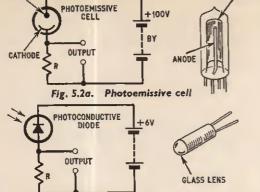


Fig. 5.2b. A semiconductor diode used as a lightsensor

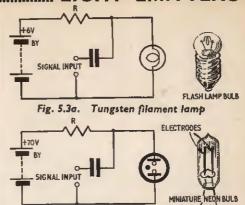


Fig. 5.3b. Gas discharge lamp

WAY TO ELECTRONICS

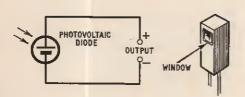


Fig. 5.2c. Photovoltaic diode or solar cell

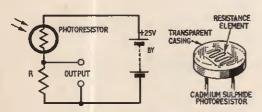


Fig. 5.2d. Light dependent resistor

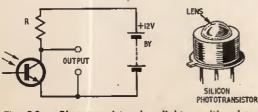


Fig. 5.2e. Phototransistor has light sensitive base emitter junction

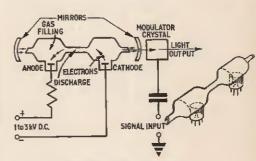


Fig. 5.3c. Laser tube

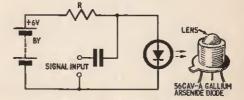


Fig. 5.3d. Gallium arsenide diode

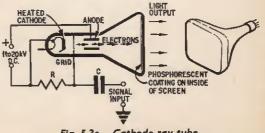


Fig. 5.3e. Cathode ray tube

LIGHT EMITTERS

Filament Lamn

Tungsten filament lamps can be used as output transducers to convert an electrical signal into a modulated light signal, (Fig. 5.3a) examples being colour organs, psychedelic displays, and systems for transmitting information by modulating light instead of radio waves to one of the photosensors mentioned above.

Unfortunately, the tungsten filament transducer is hampered by thermal inertia and cannot respond efficiently to a.c. input signals of more than a few hundred herry.

Gas Discharge Tuhe

Gas discharge tubes (Fig. 5.3b) can give pulsating light outputs up to several kilohertz when fed from a high voltage input signal. Applications are similar to those of the tungsten lamp, but also include the stroboscope and photographer's electronic flash gun,

The light amplifier or laser shown in Fig. 5.3c is basically a gas discharge tube, arranged so that most of its light output is reflected back into the tube by mirrors, thus causing a build-up of energy. The output taken from a small orifice in one of the mirrors can be a narrow, high intensity parallel beam of coherent light or infra-red.

One method of modulating the light output is to pass the beam through a crystal which exhibits variable light transmission with applied voltage. Lasers also make effective heat emitters due to the high energy content of the beam

Semiconductor Diode

Semiconductor diodes made of gallium arsenide will emit infra-red energy (just beyond the red end of the visible spectrum) when forward biased (see electroluminescent diode Fig. 5,3d). Light output is proportional to forward current and can be modulated up to 100MHz

Cathode Ray Tube

In a television cathode ray tube, a narrow, controlled beam of electrons bombards a phosphorus coating and

causes it to emit visible light, Fig. 5.3e.

Although the cathode ray tube is electrically capable of responding to high frequency signals, and can give a fine definition picture of slow moving images, the rate at which the phosphorescent output can change state from white to black is restricted by the afterglow properties of the coating.

Special phosphors used with film scanners can have an afterglow persistence of less than 0.2 us, equivalent to a modulated light output of 5MHz, but ordinary television tubes are much slower than this, say 50 us or more.

HEAT SENSORS

A heat sensor can either work by conduction, in direct physical contact with a heat emitting substance or device, or by radiation when infra-red energy is absorbed. The energy and wavelength of infra-red radiation is dependent on temperature. Several types of light sensor will also respond to infra-red emissions from substances which are not quite red hot, say at 300 degrees C, but are unsuitable for lower temperatures.

There are certain semiconductor devices—mainly confined to the laboratory-that will detect the heat of

HEAT SENSORS INSULATING CONNECTING THERMOCOUPLE OUTPUT TYPICAL THERMOCOUPLE Fig. 5.4a. Thermocouple THERMISTOR OUTPLE READ THE PHISTOR Fig. 5.4b. Thermistor MALL SILICON OUTPUT FORWARD BIASED Fig. 5.4c. Heat sensitive diode

the human body, but they usually have to be refrigerated in a cryostat at near absolute zero temperature. For temperatures below 300°C there remain the devices which operate by conduction.

Thermocouple

The first example of a heat sensor is the thermocouple in Fig. 5.4a. Two wires of dissimilar metals, say copper and constantan, are joined together to form a bimetal junction. A voltage will be produced across this junction when it is heated or cooled relative to the connecting wires. Output is zero at ambient temperature and of opposite polarities for hot and cold.

Thermistor

A thermistor (Fig. 5.4b) has an exaggerated negative temperature coefficient, that is to say its resistance

HEAT EMITTERS REVOLVING METAL DRUM PAPER SPARK GAP SCANNING SCREW ELECTRONIC STENCIL

Fig. 5.5a. Electronic stencil cutter

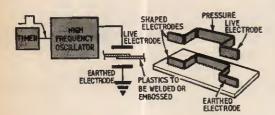


Fig. 5.5b. Dielectric heater

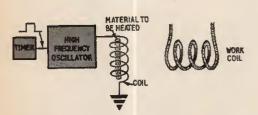


Fig. 5.5c. Inductive heater

decreases markedly with a rise in temperature. In the circuit in Fig. 5.4b, a thermistor is arranged in series with a resistor, so that output voltage will increase with temperature.

The response of a thermistor to temperature is not linear, but varies exponentially with inverse absolute temperature (°K). Positive temperature coefficient thermistors are shown in circuit diagrams with a small circle in place of the black dot.

Heat Sensitive Diode

An ordinary silicon signal diode of the type commonly encountered in electronic circuits will act as a heat sensor when forward biased. The output voltage taken from across the diode in the circuit of Fig. 5.4c is inversely proportional to temperature.

HEAT EMITTERS

Heat emission occurs in electronic circuits as a byproduct when resistive components are conducting a current, but this is not the deliberate use of heat as output energy from a transducer.

Spark Maker

The humble electric spark is a heat emitter which is often taken for granted. For instance, the output from an electronic car ignition system is applied at precise intervals by means of a spark.

Then there is the electronic stencil cutter which employs a spark to burn holes of variable diameter in ink duplicator stencils, see Fig. 5.5a. A similar idea is sometimes used to reproduce weather maps from satellite transmissions, on heat sensitive paper.

Dielectric Heater

A dielectric heater—resembling a capacitor—can weld or emboss sheets of thermoplastic material, in the manufacture of motor car seats, purses, wallets, and so on (see Fig. 5.5b).

The plastics to be heated are inserted between two cold electrodes of almost any desired shape and surface finish, which are then pressed together by a spring. One electrode is earthed and the other is fed from the output of a powerful high frequency oscillator (30–50MHz at 1–10kW).

Molecular disturbance within the plastics generates internal heat without appreciable heating of the electrodes, thus softening the plastics. A microwave household oven works on a very similar principle to cook food right through in a short time.

Inductive Heater

Inductive heaters (Fig. 5.5c) are suitable for heat treatment of conductive materials, or materials enclosed in a conductive container. Processes such as melting, hardening, tempering, annealing, soldering, brazing, and sintering can be performed with great precision in this manner.

In Fig. 5.5c an oscillator supplies a.c. to a coil of copper tubing, into which the work to be heated is placed. At low frequencies the work will be heated uniformly, but if the oscillator is tuned to several megahertz, heating will take place only at the surface of the workpiece.

Gas Discharge

Lasers have been successfully employed as heat emitters for micro-spot welding of metals and for fixing detached retinas in eye operations, refer back to Fig. 5.3c.

Part six next month will continue the section on transducers and the series will be concluded with descriptions of miscellaneous electronic devices.

POINTS ARISING

MUSICAL STAVE (May 1970)

In the paragraph relating to power output the r.m.s. output voltage should have been given as

 $\frac{9}{2\sqrt{2}}$ since a sinusoidal swing would be between \pm

41 volts. As the actual output from the circuit is rectangular, the power available will vary with the signal mark-space ratio reaching a peak of 580 milliwatts when the ratio is unity.



ELECTRONORAMA

B.B.C. Automatic Data Exchange

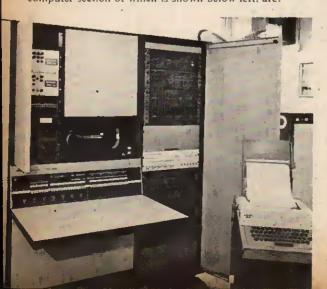
On April 6 the B.B.C. brought into service a new automatic message switching system using an

STC 6350 automatic data exchange (ADX).

The B.B.C.'s Teleprinter network for the transmission of news and other messages serves 60 outstations in London and the Regions. It handles more than 700,000 messages each year and has had an annual growth rate of some 3 per cent. The hub of the system is at the London Communications Centre in Broadcasting House.

Before the introduction of the new system a point had been reached where further expansion was not possible and the congestion that inevitably occurred at peak periods, due to manual connection to addressee outstations, could not be relieved. This congestion created delays in message transmission. Moreover, a substantial amount of urgent news traffic for non-metropolitan stations had to be diverted to the public telephone service to ensure immediate delivery.

In addition to routing and retransmitting messages automatically through the communications centre with a transit time of only milliseconds, some of the major facilities provided by the new 6350 ADX system, the computer section of which is shown below left, are:





On-line message preparation for messages telephoned into the centre or delivered by messenger, there are six 8-unit code 100 word per minute teleprinters, shown above; which feed the messages to the ADX system that immediately puts the messages into the standard format and transmits them to various outstations according to the addressing information given.

Connection to the automatic Telex network; under licence from the Post Office connections to the network have been included to cater for both incoming and out-

going messages.

System reporting and control facilities that report abnormal conditions for supervisory action. These facilities include a visual display unit, shown in operation above, for the inspection and correction of messages rejected by the ADX because of incorrect or incomplete routing information.



Climatological Station

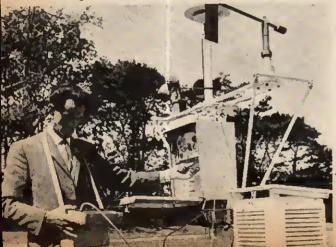
THE photograph below shows a "Hy-Met" recorder test set being used to check the functioning of a Climatological Recording Station. Both the equipments in the photograph are manufactured by the Environmental Sensors Division of Plessey.

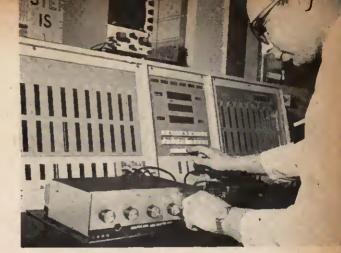
The Climatological Station makes and records over 55,000 measurements. It is self-contained and can monitor such parameters as rainfall; humidity; wind speed and direction; air, soil and water temperatures; barometric pressure; solar radiation; water level, flow and pH.

The equipment can be installed on land, drilling rigs, or on board ships and the information is recorded on standard 1 inch magnetic tape. This tape is translated using standard Plessey equipment to provide computer compatible paper tape.

Designed for use with Plessey hydrological and meteorological monitoring and recording systems, the "Hy-Met" recorder test-set provides facilities for readily

checking the function of the station.





Electronic Test Equipment

Two recently announced electronic circuit test equipments are shown above and left, they are: the Fixit (left), an inspection test system for checking mass-produced electronic circuit board assemblies, and the test console (above) used by H. J. Leak for checking tuners and amplifiers.

Fixit, a plugboard or tape programmed test system, has been introduced by Systomation, Inc., New York. The system has the ability to check the exact values of electronic components, such as resistors, diodes, transistors, etc., even though they are wired together in complex parallel electronic circuits. The system is already in use

in the United States.

The comprehensive final testing of high fidelity tuners and amplifiers takes up to forty-five minutes by hand. Now H. J. Leak, part of The Rank Organisation, are using a £10,000 Ethermatic test console that carries out an exhaustive test procedure on each unit in about one-tenth of that time. A print-out of all readings made on a tuner or amplifier is available at the end of each test-cycle. The unit is shown in use testing a stereo hi-fi amplifier.

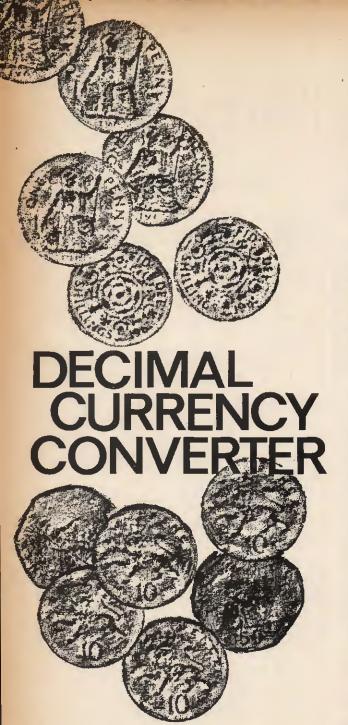
Mini-Computer

The latest commercial mini-computer from Raytheon Computers is only 16 inches high and weighs 75 pounds, yet has a memory expansion of up to 32,000. The computer is particularly suitable for applications relating to instrument and process control, data communications and data acquisition as well as basic scientific research.

A small Raytheon digital computer that was produced specifically for space flight is shown being programmed via a display keyboard, during testing, below. The "brain" of the Apollo flights, these computers are only

approximately one cubic foot in volume.





By G. A. Cozens

THE change to decimal currency in the U.K. on February 15, 1971 draws nearer as the series of new coins is introduced. But the fact remains that we have undertaken a very difficult operation by maintaining the pound as the major unit of currency, and created the task of relating 24 old pennies to 10 new pence.

Electronic methods of conversion to cope with all the 199 values under £1 fall into two categories: analogue

or digital computer techniques.

The analogue method using a simple Wheatstone bridge type of balance was tried, but it was difficult to obtain a sufficient degree of accuracy, it being necessary to be within 0.5 per cent. It is difficult to achieve this, even with quite sophisticated circuits and impossible with simple electronics using dials or meters, so this method was abandoned.

DIGITAL CONVERSION

When one tries the digital method it is then that the problems which our planners have imposed become apparent. The instrument finally devised uses switches to select the shilling and pence values, while lamps show the new pence equivalents. Some way of combining the switches and reducing the number of lamps had to be found to reduce the cost of the instrument. It is emphasised at this stage that this instrument carries out conversion only and is not suitable for use as an adding machine. The circuit diagram of the Decimal Currency Converter is shown in Fig. 1.

DIODE LOGIC

This conversion unit uses diode logic. Following the front panel layout in Fig. 2, the selector switches are divided into three rows, one for the even values of shillings (two to eighteen), one row for the odd values of shillings (one to nineteen) and one row for the old pence values—1d, 2d and 3d, 4d, 5d, 6d, 7d, 8d, 9d and 10d, and 11d, thus giving a total of 28 switches. Notice that 2d and 3d are combined on one switch, so are 9d and 10d.

The lamps are arranged in two vertical columns, the left-hand column of nine lamps representing 10p at the bottom of the column, 20p, 30p and so on up to 90p at the top. There is a single lamp to the right of these columns which correspond to $\frac{1}{2}$ p.

In this way any of the 199 values of shillings and old pence can be selected using two switches. The equivalent value in new pence will appear in the columns of lamps, one lamp in each column lighting up.

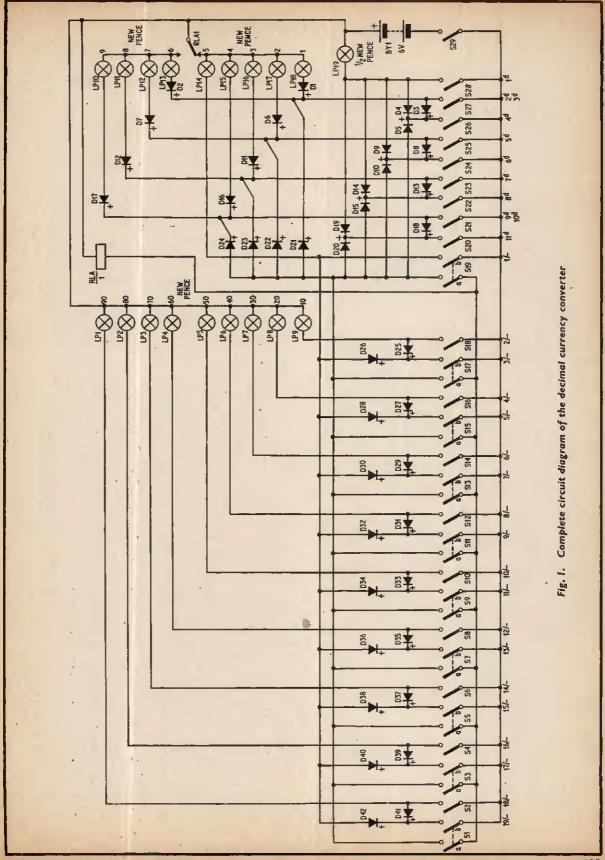
The lamps can be 6 volt 0.1A m.e.s. bulbs or 6V 0.75W l.e.s. bulbs. The relay coil must also be rated for 6 volts operation. Of course, other lamp and relay voltages can be used, but care must be taken not to use current ratings which are too heavy for the diodes to handle.

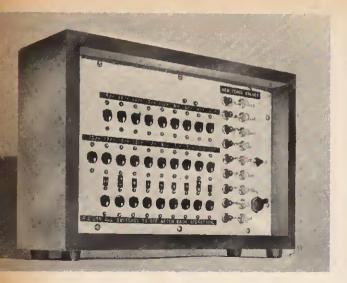
These diodes are small silicon types such as OA200 or OA202. Some suitable types of diodes are available at very low cost and it may be possible to economise considerably by selecting from these. They are germanium types and are obtainable for as little as 2.5p (6d) each when purchased in bulk quantities.

SWITCH WIRING

Starting with the 1d value, this switch S28 is wired directly in series with the ½p lamp LP19, and S29. See Fig. 3. The 2d and 3d values are combined in the next switch, which is in series with the 1p lamp.

The 4d switch is also in series with this lamp, but there is a diode D1 between the switches and the lamp, which will conduct when either switch is closed.





Front view of the converter giving layout positioning of components. All switches must be returned to the off position after each calculation

COMPONENTS ...

Diodes DI-D42 Any type that will carry 100mA or more (42 off) Lamps LPI-LPI9 6 volt 0-1A or less: with panel lampholders (19 off) Relay RLA Any 6V type with at least one set of changeover contacts **Switches** SI to S28 Double-pole changeover slide or toggle switches (28 off)
Single-pole, on/off, toggle switch (S2, S4, S6, S8, S10, S12, S14, S16, S18, S20 to \$28 can be single pole) Battery BYI 6V type 996 or 2 imes 3V type 800 Miscellaneous Single row tag strips, ‡in pitch, 7in long (2 off) Wood for case, p.v.c. covered wire, lettering

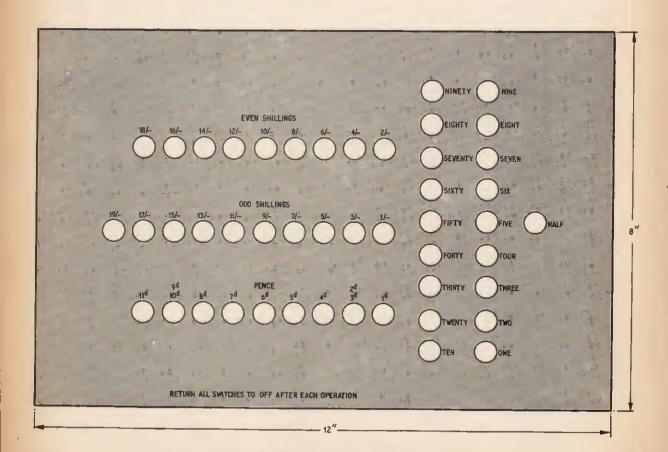
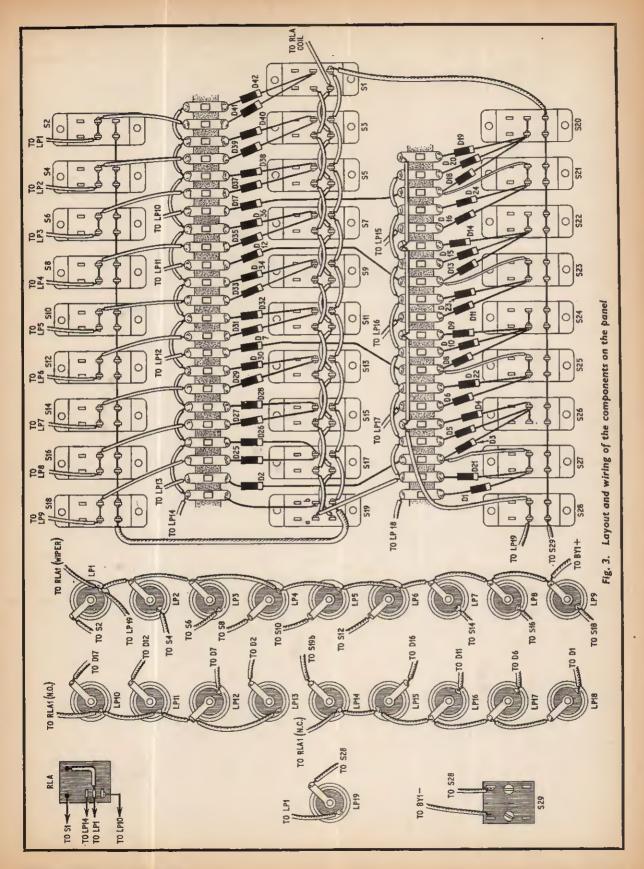
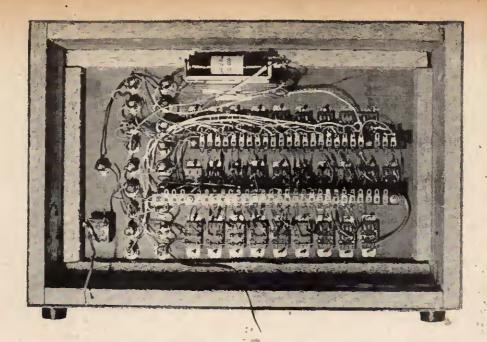


Fig. 2. Front panel layout of lamps and switches





Rear view of the converter showing components and wiring. The relay can be mounted in any convenient position on an aluminium bracket screwed to the case

Diode D3 separates the 4d switch from the 2d/3d switch and D4 connects the 4d switch to the ½p lamp.

This pattern is repeated for all the values up to 1s, so that the 5d switch turns on the 2p lamp, and the 6d switch the 2½p lamp, the 7d switch the 3p lamp, and the 8d switch the 3½p lamp. 'The values 9d and 10d and combined in one switch which operates the 4p lamp and the 11d switch operates the 4½p lamp. The 1s switch operates the 5p lamp.

The 2s switch at the start of the row of even shillings switches is in series with the 10p lamp at the bottom of the left hand column of lamps. The even shillings switches are each in series with a corresponding lamp up to the 18s switch, which operates the 90p lamp at the

top of the column.

The line of switches corresponding to the odd numbers of shillings calls for comment since these switches are double-pole, single-throw types. One side is in series with the coil of a relay and a diode. When any one of the odd value paths is completed through another diode, and the "pence" switch and back to the battery, the relay operates.

RELAY CONTACTS

The relay contacts are single-pole changeover, changing the battery return lead for the 1p, 2p, 3p, 4p and 5p lamps, so that the 6p, 7p, 8p, and 9p lamps are operated. In this way 5p are added to the value each time an odd number of shillings is selected.

For example, suppose we select the value 2s 11d. The 2s switch operates the 10p lamp, and the 11d switch operates the 4p lamp via diodes D18 and D16,

and the 1p lamp via diode D19.

Now try the value 15s 6d. The 15s switch operates the 70p lamp via D37. When the 6d switch is made the circuit through the relay coil is completed via the second contact on the 15s switch and diode D10. The relay contacts change over and the 7p lamp is lit by the circuit through D8 and D7. The ½p lamp is lit through D9.

Thus the 70p lamp, and 7p lamp and the 1p lamp give a complete reading of 77½p.

The fact that the 15s switch and the 6d switch must both operate to bring on the 7p lamp make this an example of the classic AND gate.

COMPONENTS

The bulb holders used in this model are instrument panel indicators. If a protruding lamp is used, it is sometimes difficult to see when the lamp is on in conditions of bright sunlight; the front panel can be set back so that the sides of the case shield the lamps.

The whole instrument can incorporate a small power pack for mains operation; a 6 volt mains transformer and rectifier only is necessary. These should be capable of handling the total current consumption from the relay and the maximum number of lamps in operation at any time. The model shown here used two 3 volt batteries in series; a high capacity 6 volt battery would be equally suitable, for example type 996.

The relay can be almost any type that will operate at 6 volts and has a set of changeover contacts. Examples are Post Office type 600 or Omron type MH2. It is recommended that the coil resistance is as high as is

practical to conserve battery power.

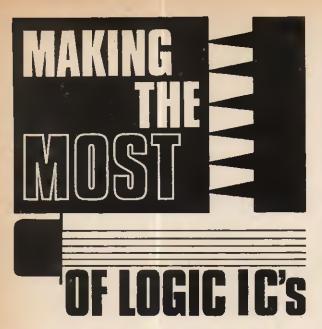
TAG STRIPS

This instrument does not lend itself to any of the modern wiring methods; that shown in the diagram uses long tag strips between the switches.

It is important to make sure that the diodes are connected correctly. The end with the coloured spot or band corresponds to the cathode and is shown on the circuit diagram with a + sign. Relay contacts RLAl

are shown in the non-operative position.

The layout of the instrument with component positions is shown in Fig. 3. It is not essential to follow this rigidly. The drilling details of the front panel will depend on the sizes of the lamps and switches; it should not be beyond the ingenuity of the constructor to arrange these as he chooses.



PART TWO-By R. W. COLES

PRACTICAL RTL DICE

ARMED with the basic facts of RTL from Part I, we can now consider a simple "novelty" application, an electronic dice unit, which will take the place of the usual cube of dots used in so many games of chance.

Anyone interested in RTL will find plenty to get his teeth into, as the design employs the main elements of this family as well as interface circuits and a multivibrator.

This article will describe the design of a small electronic unit which will replace the conventional playing dice.

It must be appreciated that this is intended purely as an exercise in the use of RTL; it is possible to design a

more simply way of simulating dice.

The system is designed around RTL logic integrated circuits, and serves as a useful introduction to the use of

these versatile devices, which are now available quite cheaply from several different advertisers in this magazine.

OPERATION OF THE SYSTEM

The operation of the system is quite simple: a free running astable multivibrator is used as the input to a binary counter, which is programmed to divide by six. The six separate states of the counter are decoded by a system of gates, and are used to illuminate six miniature lamps, only one of which will be on at a given time.

Each of the bulbs is assigned a decimal value between one and six, and the bulb which is illuminated at the end of the count represents the "up" side of the dice.

of the count represents the "up" side of the dice.

The element of chance is introduced by allowing the "thrower" to control the input to the counter by means of a push button. The multivibrator, or "clock", speed is arranged to be fast enough to prevent the eye from following the count, which will be "frozen" when the button is released.

The unit employs a total of five integrated circuits: two ML914 dual two-input negative logic NAND gates and three ML923 JK bistable flip-flops. These i.c.s are also shown as μ L914 and μ L923 in suppliers' lists. In addition, eight npn silicon bulb-driver stages, ten resistors, and two capacitors are employed.

The "clock" is made by a.c. coupling a dual gate to form a multivibrator which oscillates at approximately IkHz, and gives a square-wave output to drive the counter. The circuit of the ML914, with the two resistors and two capacitors which set the frequency and pulse width of the output, is shown in Fig. 2.1. To enable the clock to be switched on and off, a push button switch is connected in its positive supply line.

BINARY COUNTER

The divide by six counter is formed from three JK bistables, with feedback to prevent it cycling in unwanted states (because a three-stage counter would normally have eight separate states), each stage dividing by two. The 'text-book' way to make a divide by six counter is to force a divide by eight counter to reset to zero when a count of seven is decoded by an AND gate. However, by using JK flip-flops, the same result can be achieved in a simpler way, with the added advantage that bulb decoding gating can also be made simpler than would be the case with a conventional binary divider.

The simplest way to set about designing a counter which is not required to divide to a binary multiple (two, four, eight, 16, etc.), is to divide the required divisor by two until the lowest odd integer is obtained. A counter, with feedback, is then designed to divide by this number, followed by (or preceded by) a number of divide by two stages, to make the final divisor up to the

required number.

Our divide by six counter can be constructed by using a divide by three counter followed by one divide by two stage. A further divide by two stage would turn it into a divide by 12 counter, and so on. The advantage of using this method is that it is much simpler to arrange the feedback for resetting a divide by three counter than for a complete divide by six counter.

There is a disadvantage which could be important in some other applications, the counter outputs are not in the natural binary code, as can be seen from the truth tables of the two types of counter discussed (see Fig. 2.2).

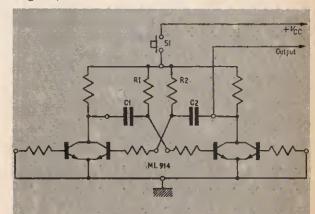


Fig. 2.1. Clock pulse generator made up from two 2-input NAND gates with C1, C2, R1 and R2 added to make up an astable multivibrator. R1=R2=1k Ω . C1=C2=0.68 μ F

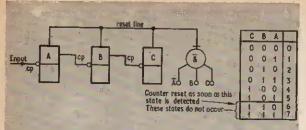


Fig. 2.2a. Conventional +6 counter

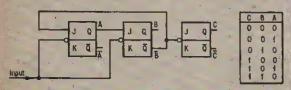


Fig. 2.2b. This 46 counter is used in the dice system

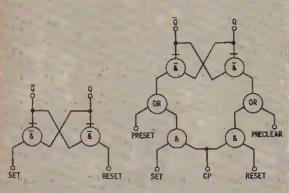


Fig. 2.3a. Simple Fig. 2.3b. Shift register bistable latch bistable

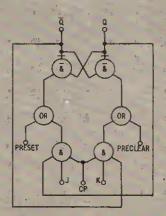


Fig. 2.3c. Simplified logic diagram of a JK bistable

VERSATILE JK

Perhaps it might be as well to consider the way in which the JK has developed to become the "do-anything" device, suitable for use in memory circuits, shift registers, and various forms of counters, used in logic circuitry today.

The simplest form of bistable is the set/reset or latch, which is formed simply from two NAND or NOR gates, as in Fig. 2.3a. The inputs to this circuit must be complementary, and there is no provision for a clock input, so its use is limited and confined to simple memory applications.

The first step in improving the set/reset type is to add AND gates to the inputs, enabling information to be gated in synchronism with a clock pulse, which is common to both gates. The asynchronous inputs of the simple latch can be retained if required by adding an OR gate between the bistable and the AND gates. A circuit of this type is shown in Fig. 2.3b.

This is a useful circuit which may be used in shift registers, but the inputs must still be complementary to ensure proper operation. To enable the circuit to be self-complementing, feedback can be provided from the collector outputs of the bistable to the inputs of the AND gates, ensuring that if two "ones" are present at the inputs of the AND gates, the bistable will change state. This circuit is the basis of the JK flip-flop, and is shown in Fig. 2.3c.

It must be appreciated that this is a simplified representation, and there are some problems which have not been considered in this treatment.

DICE COUNTER

The complete logic system of the electronic dice is shown in Fig. 2.4. A divide by three synchronous counter is made up from the JK flip-flops A and B. The third JK flip-flop C is a divide by two stage. The complete counter conforms to the truth table given in Fig. 2.2.

The decoding of the six separate states of the counter is likely to appear very complicated to those unfamiliar with the "dodges" which are often used in this type of circuitry. A knowledge of Boolean algebra is necessary to design such circuits, but a simple explanation will be given here. By using this in conjunction with the truth table a constructor should be able to sort out exactly what is going on.

The transistors used to drive the bulbs are also used as a form of AND gate. This is possible as a transistor requires both that its base be taken positive, and that its emitter be grounded, before it will turn on, assuming npn transistors are used.

Therefore, if we let bistable C control the grounding of the emitters of the bulb drivers, we can see from the truth table that output C is down for three counts. Output \bar{C} is down for the other three counts, enabling the emitters of bulb drivers 1, 2 and 3 to be connected together and ground them through another transistor, whose base is controlled by the \bar{C} output. Drivers 4, 5, and 6 can be similarly controlled by the C output.

Having dealt with the C bistable, A and B can be decoded having gone through two complete counts of three in any count of six. The bases of drivers 1 and 4, 2 and 5, 3 and 6 can be connected together in pairs and driven from the decoded states, which represent the three separate states of bistables A and B.

The decision as to whether 1 or 4, 2 or 5, 3 or 6 is illuminated is carried out by bistable C, switching on only one emitter of each pair.

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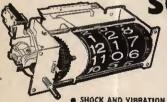
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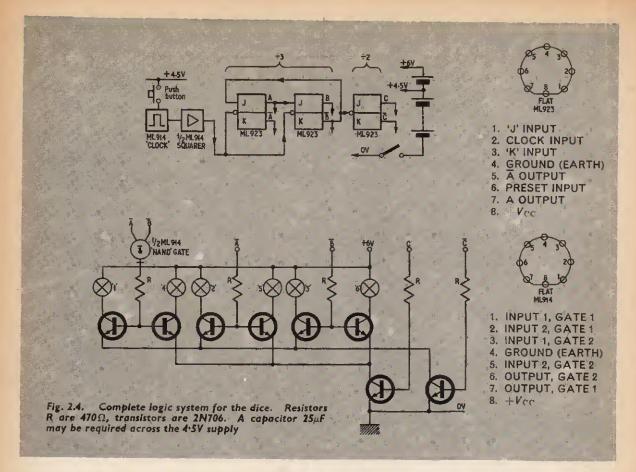
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The decoding of each of the three states of A and B is rendered simple by the type of counter employed. The first state has to be described in terms of A and B, but states 2 and 3 are described merely by deciding whether the A output or the B output is "up". A gate is only necessary to decode counts 1 and 4; counts 2 or 5 can be driven by the Not output of bistable A, as this is positive only during these two states. Similarly, counts 3 and 6 can be driven by the B output.

The gate used to decode the first stage of the counter uses half of an ML914, used as a 2-input negative logic NAND gate, its inputs being A and B, which are both

negative at a count of one only.

As a bit of light relief, let us see what has happened to the spare half of the ML914, left over from the decoding circuit. It is in fact being used as an amplifier, with both its inputs connected together, to square up the edges of the clock waveform.

This is necessary, as the JK flip-flop needs a very fast negative edge on the clock input, for it to operate correctly; our clock multivibrator cannot be relied

upon to produce such edges.

PRACTICAL DETAILS

This completes the circuit description, except for a few practical details. The supply voltage used poses a bit of a problem, the RTL i.c.s. specified are designed for a supply voltage of 3.6 volts. Since this is not easily obtained from dry batteries, a compromise is used of 4.5 volts, and an extra cell is used to boost this to 6 volts for the bulb circuitry.

The bulbs used must be low consumption types, requiring in the region of 50mA at 6V. Although they will be slightly under-run, due to the saturation voltages of the two driver transistors appearing in series with each of them, this is not a bad thing from the point of view of reliable readout.

The actual layout of the circuit can be safely left to the constructor, as there are no special problems involved, but perhaps a few hints would be useful. There are several kinds of perforated baseboard suitable for the support of this kind of circuit on the market. Veroboard is one which can be used for this particular application.

Using this type of board in the 0-lin matrix size the integrated circuits can be directly inserted, but due to the component density, a good deal of the connections will have to be made using "jumper" wires to realise a

compact unit.

The i.c. leads can be left at least ½ in long, if desired, but to be sure of re-use of the i.c.s, Lektrokit board can be used. In this case a ring of terminal pins can be used for the i.c.s, which can be mounted upside down on the board, wiring being carried out underneath.

A miniature soldering iron is a virtual necessity when working on this sort of layout, unless the constructor

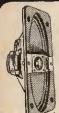
possesses a very steady pair of hands.

The completed unit can be accommodated in a small plastics box, the only controls being the on/off switch, the push button, and a row of six miniature lamp holders.

Next month's article in this series will look into Diode Transistor Logic or DTL.



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TRANSISTOR BY W. CLELAND

N this, the final part of the "Transistor D.C. Multi-meter", we give mounting details of the components and boards inside the diecast case, final wiring details and setting up instructions.

CASE DETAILS

The multimeter is housed in a diecast case of outside dimensions $8\frac{3}{4}$ in \times $5\frac{3}{4}$ in \times $2\frac{5}{32}$ in. The box is used upside down, since the screws of the lid prevent the lid from being used as the top panel. The lid, therefore, becomes the underside of the instrument, to which four rubber feet are screwed, and the bottom of the box makes a satisfactory top panel. Top panel dimensions are hin less than the overall dimensions, because, with a diecast box, the sides taper slightly inwards. When drilled, as in Fig. 9, the case is painted to protect it; paint has to be removed from openings and from the edges and interior of the case when dry.

The neon signal lamp is mounted just under the edge of M1 and is raised lin, by fitting a piece of black

Bakelite under it as shown in Fig. 10. This is positioned on the top panel between the milliammeter and the Perspex switch escutcheon. On final assembly, the signal lamp is fastened from the inside, by pushing on a spire nut, over the plastic lampholder.

SWITCH ESCUTCHEON

The Perspex switch escutcheon is shaped to fit between the signal lamp and terminals, and is dimensioned as shown in Fig. 11. Two 3 in diameter holes enable it to fit around the nuts securing the range switches, and it is held in place by two 8B.A. countersunk screws. These are situated under the knobs of the range switches.

To set the switch knobs accurately, a small depression has to be drilled in the shaft for the grub screw. The smooth end of the grub screw can be scored with a file, so that the grub screw will leave a mark on the shaft at the required position. An indentation is made on this spot with a small drill.

NOTE: It is recommended that a suitable meter be obtained before drilling the box. Modifications to layout and drilling may be necessary to accommodate other meters such as the MR-65P

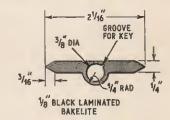


Fig. 10. Signal lamb surround

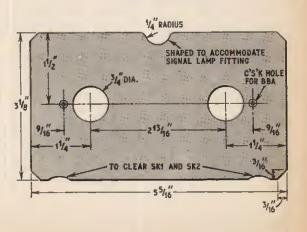
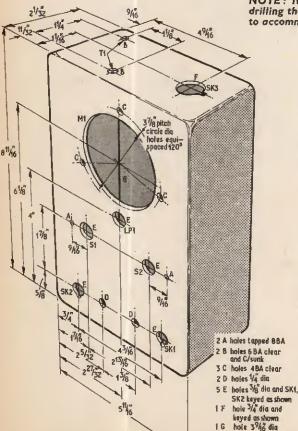
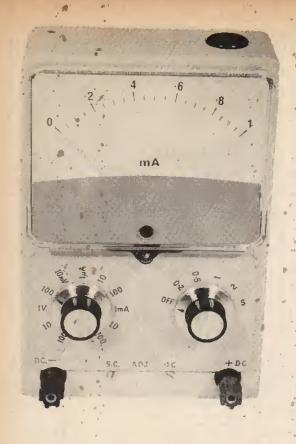


Fig. 11. Perspex switch escutcheon





Adequate clearance has to be ensured between the knobs and the Perspex escutcheon. The escutcheon can be marked, as shown in the photograph, to give switch positions and potentiometer designations.

MAINS WIRING

The metal case of the testmeter has to be earthed to the mains earth via SK3. The circuit of the testmeter is in no way connected to the metal case or to mains earth.

The insulated mounting for the miniature mains transformer T1 (Fig. 12) insulates it from the metal case, and provides a junction box for the transformer connections. The p.v.c. insulation of the connecting leads is carried into the insulated mounting, which consists of three rectangular pieces of insulating material sandwiched together. Parts B and C are of in laminated Bakelite, and can be bonded with adhesive. These are bolted at two corners to part A, which is of in material. A pair of 6 B.A. countersunk bolts at the other corners, secure the mounting to the inside of the case.

The insulated leads from the signal lamp are hardly long enough to reach the mains switch S26, and to avoid running these wires very close to the range resistors, it is necessary to increase the length of the existing leads.

Details are given in Fig. 13 of a special insulated cover for the mains switch, which ensures safety if tests have to be made on the low voltage wiring with the unit turned on. All the mains wiring is double insulated, by wrapping each pair of p.v.c. covered wires with cloth insulation tape, avoiding an excessive thickness.

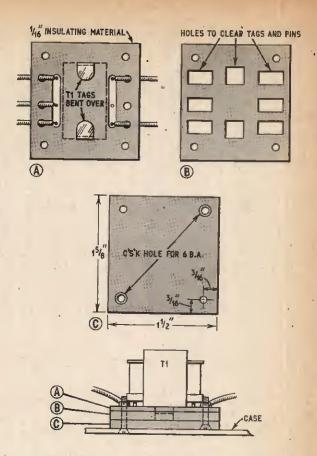


Fig. 12. Insulated mounting for TI, holes are arranged to clear transformer tags. Sections B and C are in thickness Bakelite

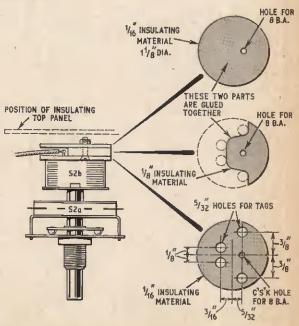


Fig. 13. Insulated cover for S2b. The lower section with the screw in position should be fitted before the wiring is connected to the switch

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ACY34	8/5 BC182L	2/8 B8X19		6/- NKT143	9/6 NKT275	8/4 OC22	8/- BT141	5/- 20371	3/- 2N3235	28/6 BYX36/	
ACY35			3/8 GET890	8/8 NKT144	8/- NKT276	8/8 OC23	8/- BT2	9/9 2G371R	8/- 2N3234	27/8	2/10
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YCA38	12/- BC2121.	8/4 BSX60	12/7 GET898	6/- NKT154	6/- NKT301	18/- OC26	6/6 TIS44	1/9 2N174	16/- 2N 3392	5/- BYZ10	9/9
ACY40	3/- BCY30	5/- B8X61	7/1 GEX 45/1		6/- NKT302	12/5 OC28	12/- TIS45	8/8 2N385A		5/- BYZ12	6/-
AD140	11/- BCY31	5/8 BSX76	4/- 0J6M	4/- NKT162	6/- NKT303	17/6 OC29	15/- TIS46	8/8 2N388A	15/- 2N3394	4/8 BYZ13	5/-
AD149	11/6 BCY32	10/- BSX77	6/- GP297/1	B/- NKT163	6/- NKT304	9/10 OC35	9/- TIS47	3/8 2N404			
AD161	6/- BCY33	4/- B8X78	6/8 GP826	20/- NKT164	6/- NKT351	10/- OC36	12/6 TIS48	3/8 2N696	4/6 2N3402	5/6 EA403	3/6
AD162	8/- BCY34	5/- BSY27	4/- KBS2	5/- NKT166	6/- NKT352				8/7 2N3403	5/8 EC401	5/-
ADT140	12/6 BCY38	6/- B8Y29	5/- MAT100			17/6 OC41	4/6 TIS49	3/6 2N697	8/10 2N3404	7/8 OA5	8/8
ADZII	32/- BCY40	10/- BSY32		5/- NKT201	6/- NKT361	20/- OC42	4/8 TIS50	5/8 2N699	6/- 2N3414	5/8 OA10	8/-
AF102	12/6 BCY42		5/~ MAT101	5/6 NKT202	6/- NKT362	20/- OC43	4/8 T1851	4/- 2N706	2/4 2N3415	6/- OA47	1/8
		4/- BSY36	5/- MAT120	5/- NKT204	6/- NKT401	14/8 OC44	3/- TI852	4/- 2N706A	2/6 2N3416	7/8 OA70	1/8
AP106	7/6 BCY48	4/- BSY37	5/- MAT121	5/6 NKT205	6/- NKT402	15/- OC45	3/- TIS58	8/6 2N708	3/8 2N3436	15/- OA73	1/8
AF114	5/- BCY70	8/10 BSY38	4/- ME1100	6/- NKT200	6/ NKT403	14/9 OC70	2/6 T1860	6/6 2N709	B/8 2N3525	21/9 OA79	1/8
AF115	5/- BCU71	7/8 BSY95	3/2 MJ400	21/6 NKT208	8/- NKT404	11/- OC71	3/- TIS61	7/- 2N711	7/8 2N3528	19/- OA81	1/8
AF116	5/- BCY72	8/2 B8 Y95A	2/11 MJ420	22/6 NKT210	4/2 NKT405	11/- OC72	4/6 TIP31A		7/8 2N3702	2/6 OA85	1/8
AF117	5/- BCY87	86/9 BYZ14	38/8 MJ421	22/6 NKT211	8/9 NKT406	9/11 OC74		14/10 2N749			
AF118	8/10 BD119	15/- BYZ15	38/8 MJ480	20/6 NKT212	8/8 NKT420	8/11 OC75	4/6 U23AA		4/6 2N3703		1/8
AF124	4/2 BD121	18/- C106P	9:- MJ481	27/- NKT213					6/- 2N3704	3/2 OA91	1/8
AF128	4/8 BD423	21/6 C111	18/- MJ490	ONIO NIUMOLA	4/7 NKT461	9/11 0076	2/6 V205	20/- 2N929	5/8 2N8705	2/8 OA95	1/8
AF126	3/6 BD124	12/- C111E		22/6 NKT214	3/5 NKT452	9/8 OC77	5/6 V495A	9/3 2N930	6/- 2N3706	2/8 OA200	2/-
			12/- MJ49I	29/6 NKT215	8/7 NKT453	6/6 OC81	4/8 XB113	6/- 2N 1090	6/8 2N3707	2/10 OA202	2/-
AF127	3/6 BDY20	20/8 C400	9/- MPF102	B/6 NKT216	7/0 NKT603F	4/8 OCSID	3/- XK508	20/- 2N1131	6/11 2N3708	1/10 SD19	74
AF178	9/6 BF115	5/- C426	8/3 MPF103	7/8 NKT217	9/- NKT613F		5/- 40250	10/9 2N1132	7:8 2N3709	2/- TD716	12/-
AF179	11/6 BF152	18/6 C444	9/8 MPF104	7/6 NKT218	0/- NKT854F	4/2 OC82D	3/- 40309	6/6 2N1302	8/7 2N3710	2/8 1N34A	41-
AF180	12/6 BF154	9/- CG50	2/8 MPF105	8/- NKT219	4/7 NKT675	6/8 OC82	4/6 40310	9/- 2N1303	8/7 2N3711	2/6 1N82A	9/6
AF181	8/8 BF159	15/- CG61	2/6 NKT11	7/6 NKT221	7/- NKT676	5/- OC84	6/- 40311	6/9 2N1304		7/- 1N914	1/9
AP186W	9/- BF163	9/- CG62	2/6 NKT12	5/5 NKT222	6/- NKT677F		7/- 40311		4/11 2N3819	77- ALVOLA	
AF186G	9/- BF167	5/- CG62H	2/6 NKT32	6/2 NKT223	5/- NKT703	8/- OC139		9/6 2N1305	4/11 2N3920	18/0 IN4148	1/9
AF239	7/6 BF172	6/- CG63					5/- 40314	7/8 2N1306	6/- 2N3826	6/- 1844	1/9
AFY19	22/6 BF178		2/6 NKT42	6/- NKT224	8/7 NKT713	3/10 OC140	7/- 40815	7/8 2N1307	6/- 2N3866	25/- 18113	4/6
		10/8 CG64	2/6 NKT43	8/- NKT225	8/6 NKT717	5/10 OC170	5/- 40316	9/8 2N1308	6/8 2N3903	7/- 18130	2/-
AFZ11	8/- BF179	12/8 CR6E	2/8 NKT72	8/9 NKT226	11/- NKT734	4/11 OC171	8/~ 40317	7/8 2NIS09	6/8 2N3904	71-	
ASY26	4/5 BP180	6/- CG83	2/6 NKT73	8/7 NKT227	9/8 NKT736	6/2 OC200	6/8 40319	10/9 2N1496	24/- 2N3905	7/6	
ASY27	6/- BP181	8/8 CG84	2/8 NKT101	6/- NKT228	6/6 NKT773	8/7 OC201	9/6 40320	7/8 2N1618	4/5 2N3906	7/6	
A9Y28	4/5 BF184	7/- CG85	2/6 NKT102	8/- NKT229	3/11 NKT774	6/- OC202	18/- 40323		29/6 2N4037	15/-	
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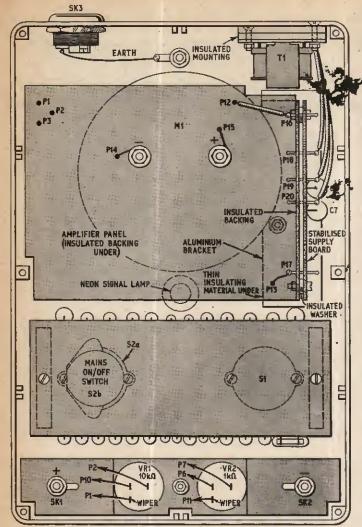


Fig. 14. Interior of the multimeter showing component positioning and potentiometer wiring

COMPONENTS . . .

Potentiometers 10kΩ miniature carbon IkΩ miniature carbon VR2 Sockets SKI Red insulated screw terminal Black insulated screw terminal SK2 Miniature three pin SK3 mains connector Transformer TI Miniature mains, primary 0-220/240V, secondary 12-0-12V, 40mA, type P9005 (Electroniques) Meter M1 Moving coil milliammeter, B.P.L. type S40-VI (ImA f.s.d.) or SEW type MR-65P Miscellaneous LPI Neon signal lamp type SGF9/A (Electroniques) Knobs pointer (2 off) Diecast case $8\frac{3}{4}$ in \times $5\frac{3}{4}$ in \times $2\frac{5}{34}$ in Bakelite; $\frac{1}{4}$ in thickness, $5\frac{7}{16}$ in \times $3\frac{1}{8}$ in, $\frac{1}{4}$ in thickness 4 in \times $1\frac{1}{2}$ in,

in thickness black 216in × in

Perspex $3\sin \times 5\sin \times \sin$ thickness

CONNECTING UP

6B.A. and 8B.A. fixings

The Veropins on the amplifier board are connected up with reference to the pin numbers on the circuit diagram (Fig. 2), the switch connection diagram (Fig. 8), and Fig. 14, the plan of the interior of the multimeter. The two Veropins adjacent to the meter terminals are connected to the terminals by short leads, and the Veropins nearest to the stabilised voltage supply, are connected to the two on the vertical panel as shown in Fig. 14. The row of Veropins on the left of the amplifier board are connected by flexible p.v.c. covered wires to the range switching assembly, and to the two potentiometers that are mounted as shown in Fig. 15 by means of strips of \(\frac{1}{2} \) in insulating material.

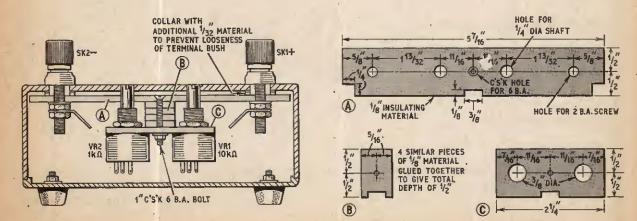


Fig. 15. Potentiometer mounting details, the ends of the spindles should be flush with the top of the case when fitted

The three secondary connections from the mains transformer are joined to the terminal pins on the

voltage stabiliser panel,

Positioning of all components is shown in Fig. 14 and once the various sections have been mounted and wired up as described previously the meter can be connected to the mains supply ready for setting up and testing.

OFFSET ADJUSTMENT

A high gain differential d.c. amplifier needs pre-set adjustments to take up the mismatch in transistors and other components; adjustment is at the input stage where the sensitivity is greatest.

In the absence of an applied input, the terminals of the testmeter should be at the same potential. A small difference of potential at the input is called offset voltage, and arises from mismatch in the base-emitter potentials of the two input transistors. It can be balanced out by adjusting VR2, thus bringing the two input terminals to the same potential.

There is also an offset in the bias current of the two input transistors. The bias currents-less than a microampere-flow through the two 1MΩ feedback resistors and produce a small potential drop between output and input. The bias current adjustment is carried out indirectly by VR1 in the collector circuit of the input stage. When both offsets have been balanced out, there will be no potential difference, either at the input or at the output.

METER ZEROING

The two adjustments are not independent of each other. Each potentiometer has to be adjusted in turn to bring the pointer of the meter exactly to zero. A short insulated wire is connected between the input terminals each time that VR2 is adjusted, and temporarily disconnected when adjusting VR1. The potentiometer VR1 is thus the open circuit adjustment. and VR2 the short circuit adjustment, and the two are marked "O.C." and "S.C." respectively on the Perspex escutcheon.

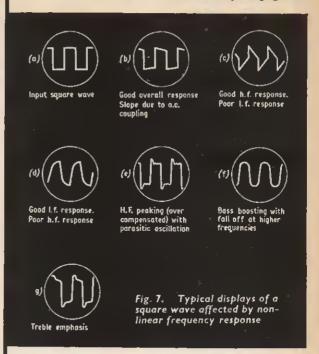
Successive adjustments become smaller and should be continued on the most sensitive 2mV range until the pointer is at zero under both input conditions. The short circuit adjustment (VR2) is rather critical on the 2mV range, and it is probably advisable to solder a 470 ohm carbon film resistor permanently across it to make adjustment easier, providing that the narrower range of adjustment contains the required setting.

Once the above adjustments have been made and the meter has been tested on all ranges it is ready for use.



OSCILLOSCOPE CALIBRATOR

continued from page 630



maximum amplitude is 1 unit the average is 0.637 and this is what the meter will read.

However, we are usually more interested in the r.m.s. value which is, for sine waves, 0.707. If we divide the r.m.s. value by the average, we find the form factor, in this case 1.11. This is the amount by which the meter is scaled or calibrated. So the meter is known as average reading, r.m.s. calibrated. The form factor is obviously different for other waveforms, this calibration is therefore true only for sine waves.

AMPLIFIER TESTING

Square wave testing of amplifiers has the advantage of time saving. Plotting a frequency response curve is a tedious business. It involves changing the frequency of the signal generator point by point along the frequency base, and noting the amplifier's output reading. From this the output voltage versus frequency graph is drawn.

It is obvious that examining the effects of tone controls of an audio amplifier can be a long and dreary process. But, by applying a square wave to the amplifier input, and monitoring the output on an oscilloscope, the effects of tone controls and filters can be seen by the alteration to the wave shape. See Fig. 7.

Treble boost will show up as overshoot of the leading edge and treble cut as a rounding off. Bass boost will tilt the flat top left to right and bass cut right to left.

Checking a pre-amplifier with a square wave for the first time you may be dismayed to find that the output appears to be distorted. Even at the mid-point of the controls, the leading edge will probably display a slight kink and the top a slight curve. This is due to the type of tone control circuit which is common to many pre-amplifiers. However, the basic square shape, and the variation as the tone controls are adjusted is quite



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Totalising 48 ° d.c. at 48mA; 10 impulses/ sec. Length 4in × 1ln × 1in, Price 43.15.6, P. & P. 5/-.

4 DIGIT NON-RESETTABLE COUNTER

Totalising 16 impulses per second. Length 3½in × 1½in × 1½in. 24V d.c., 300 ohm. Price 6/6. P. & P. 5/~. **6 DIGIT RESETTABLE COUNTER**

Totalising 240V 50Hz. Vlewing window 2in × fin. Ex-equipment. Price 55/-, P. & P. 5/-.

6 DIGIT TOTALISING NON-RESETTABLE COUNTER

Mechanical operation. Chromium finish. Length 14in × 1in × 1in with viewing window 1in × 1in. Ex-equipment, Price 9/8, P. & P. 2/6.

BERKELEY DECIMAL COUNTING UNIT 0-9

ONI 0-9

4 valves double triode type 5965 special quality Unit plugs into standard octal base. Modular construction with -10 ministure neon lamps on display pacel, Power supplies 6-3V, a.c., 150V d.c. Cutton or Cut-off-15V. Size 5jin × 5jin × 10 ministure con Cut-off-15V. Size 5jin × 5jin × 10 ministure processing the control of the cut-off-15V.

MINIATURE DIGITAL DISPLAY



Operates on a rear projection 6-3 pilot lamp. The lamp projects the corres-ponding digit on the condensing lens through a projector

the condensing lens through a projector tens, on to the viewing screen at lin width. 3½ in deep. 1½ in high. 0-9 with 8 right hand decimal point and degree. List price 6 gns. Our price 49/6, P. & P. 5/-.

EAC DIGIVISOR Mk. II DIGITAL READ-OUT DISPLAY

READ-OUT DISPLAY
Ideally suitable for use
in conjunction with transistorised decade counting devices. The DIGIVISOR incorporates an
moving coil movement
which moves a translucent scale through an
optical system and the resultant single
plane image is projected on a screen.
The translucent scale is made to represent digits 0-9. Specifications: 6-3V 250
microamp. Image height in. Size 4
9/16 × 2 39/64 × 1 lin. Our price 3; gns.
List price 8; gns. P. & P. 5/-.

LAMPS 250V, 18W, MBC. Panel lamps. Ideal making up displays, etc. Length 2½m × 1½m dia. Special offer, 10 for \$1. P. & P.

Assorted ministure types. Special offer, 15 for £1. P. & P. 5/-.

MINIATURE MOVING COIL RELAY SIIS



By Sangamo Weston, suitable for D.C. circuit. antiable for D.C. circular, A high sensitivity relay more sensitive than the electromagnetic type. Single Coil Resistance 310 micro amps. 315 \(\text{\Omega} \). List price £4.10. Our price 20/-. P. & P. 3/-.

NUMICATORS



S
Fig. size 13mm.
Cold cathode gas filled in
line 0-0 digital display
tubes. Long life expectancy. Minimum artifact
Type XN 13 and XN 3,
amber. Frice 18/6 ench.
P. & P. 2/6.
Fig. size 20 mmr.
Type XN 11. End reading.
Frice 21 each. P. & P. 2/6.

DOUBLE AUDIO FADERS



These hard to get, professional recording studio units are ideal for audio signal mixing, fading programmes in and out, etc. Two bank 1,000 + 1,000 ohm wice-wound parallel connection to give 500 ohm live-wound parallel makings, with red and blue control knobs. Panel mounting. Ex-equipment. Price 23,19.6, P. & P. 7/6,

LINEAR THYRISTOR CONTROLLED LIGHT DIMMER-BRAND NEW

High grade full wave high grade init wave bridge circuit gives linear control of light brightness, Ideal for controlling room lighting and a.c./d.c.



figuring and h.c.(d.c. commutator motors fitted to portable electric hand drills. Fits standard 2in conduit box. 240V, 50Hz, 600W. Price 59/6. P. & F. 2/6.

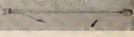
POCKET CALCULATOR

POCKET CALCULATOR
Save time and solve all
your multiplication, division, percentage, cube
and squareroof problems.
Easy to use pocket calculator with no errors. Inreal calculation with no errors. Insultable daily aid,
should last a lifetime,
offered complete in black
wallet with full instructions, 33 in diam. 12:6
each, P. & P. 1/6.



New complete telephone dial assemblies Clear perspex dial - no markings 20/-each, P. & P. 5/-.

RAPID HEAT SOURCE . . .



from brand new Inira Red Tubular Quartz Lamps, Ideally suited as heat source for Drying Overa, Egg Hatching, Incubators, etc. 240V, 1,440V, 20,000 Angstroms. Length 12in x jin dia. Price 15i-., P. & P. 6i-.

SOLENOIDS

High quality solidly constructed solenoids. Actuated by 48V 300 Ω coil. Overall length 3"×1" square with a ½" travel of the ½" dia, shaft. 3|0, P. & P. 3|-.

INDICATOR LAMPS

Panel-mounting. Various colours and types. Press to test facility, Prices from 5/- each. P. & F. 1/6.

ELECTRONIC BROKERS LTD., 49-53 PANCRAS RD., LONDON, N.W.I Tel. 01-837 7781/2 Cables: SELELECTRO

TRANSISTOR RADIOS TO BUILD YOURSELF

Backed by after sales service

NEW! roamer eight mk 1 WITH VARIABLE TONE CONTROL

7 Tunable Wavehands: Medium Wave 3, Medium Wave 2, Long Wave, S.W.1, S.W.2, S.W.3, and Trawler Band. Built in ferrite rod aerial for Medium and Long Waves. 5 section 22in chrome plated telescopic aerial for Short Waves can be angled and rotated for maximum performance. Fund-puil output using 600Mw type transistors. Socket for car serial. Tape record socket. Selectivity switch. Switched expiece socket complete with earpices for private listening. 8 transistors plus 3 diodes. Famous make 7 × 4 in speaker. Air spaced ganged tuning condense. On/off switch volume control. Wave change switch and tuning control. Attractive case in rich chestnut chade with gold blocking. Size 9 × 7 × 4 in approx. Easy to follow instructions and diagrams make the Roamer Eight a pleasure to build. Parts price list and easy build plans 5/- (FREE with parts).

Total building costs **£6.19.6** P. & P. & P. 7/6



roamer seven mk IV

7 FULLY TUNABLE WAVE
BANDS—M.W.1, M.W.2, L.W.,
8.W.1, S.W.2, S.W.3 and Trawler
Band. Extra Medium waveband
proyldes easier tuning of Radio
Luxembourg, etc. Bullt in ferrite
rod serial for Medium and Long
Wayes. S Section 22in chrome plated
telescopic aerial for Short Waves—
can be angled and rotated for peak
8.W. listening. Socket for Car Aerial.
Powerful push-pull output. 7 transistors and two diodes
including Micro-Alloy R.F. Transistors Famous make
lackeding Micro-Alloy R.F. Transistors. Famous make
lackeding Micro-Alloy R.F. Transistors and two diodes
including Micro-Alloy R.F.

Total building costs

P. & P. Personal Earplece with switched sucket for private listening, 5/- extra.

NEW!

transeight

SIX WAVEBAND PORTABLE WITH 3in. SPEAKER

Attractive case in black with red grille and cream knobe and dial with pollohed brass inserts. Size 9 x 5½ x 2 im.

approx. Tunable on Medium and Long
Waves, 3 Short Waves and Trawler Band.

Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves.

8 improved type translators plus 3 diodes. Push-pull output. Ample power to drive a larger speaker. Parts price list and easy build plans 5/- (FREE with parts).

Total building costs

5/6

P. & P. Earpiece with switched socket for private listening 5/- extra.

pocket five

MEDIUM WAVE, LONG WAVE AND TRAWLER BAND PORTABLE WITH SPEAKER AND EARPIECE

Attractive black and gold case. Size 51 × 11 54m. Trasble over both Medium and Long Waves with extended M.W. band for easier tuning to Luxembourg, etc. 7 stages—5 transistors and 2 dlodes, supersensitive ferrite rod actial, fine tone moving coil speaker, also Personal Earpiece with eviltched socket for private listening. Easy build plans and parts price list 1/6 (FREE with parts).



Total building costs P. & P. 3/6

transona five

MEDIUM WAVE, LONG WAVE AND TRAWLER BAND **PORTABLE** WITH SPEAKER

Attractive case with red speaker grille. Size 63 × 41in x 13in. 7 stages—6 transistors and 2 diodes, territe rod aerial, tuning condenser, volume control, tine tone moving coll speaker. Easy build plans and parks price list 1/6 (FRE with parks).



roamer six

SIX WAVEBAND PORTABLE WITH 3in. SPEAKER

Attractive case with gilt fittings. Size 7½ × 5½ × 1½in. Tunable on Medium and Long Waves, two Bhort Waves, Trawier Band plus an extra M. W. band for easier tuning of Luxembourg, etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. S stages—6 transistors and 2 diodes including Micro-Alboy R.F. Transistors, etc. (Carrying strap 1/6 extra). Easy build plans and parts price list 2/- (FREE with parts).



Total building costs

- * Callers side entrance Stylo Shoe Shop
- * Open 10-1, 2.30-4.30 Mon.-Fri. 9-12 Sat.

RADIO EXCHANGE

61a, HIGH STREET,	BEDF	ORD.	Tel. 0234	52367
I enclose £	please	send iten	ns marked	
ROAMER EIGHT		ROAME	R SEVEN	
TRANSEIGHT		POCKE	T FIVE	

MOAINER EIGHT	L.J	ROAMER SEVEN	17
TRANSEIGHT		POCKET FIVE	П
TRANSONA FIVE		ROAMER SIX	
Parts price list and pla	ns for	*************************	

TRANSONA FIVE ROAMER SIX	
Parts price list and plans for	*********
Name	
Address	

... PE 20

MURK

items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

RHYTHM UNIT

To interest our musically minded readers this month is a versatile automatic rhythm unit to add complete accompaniment to an organ or other solo instruments.

Known as the Rhythm Ace it gives a choice of 10 different percussion tones: bass drum; small drum; conga (high and low); brush; claves;



Rhythm Ace from Severn Musical Industries

cow bell; cymbal, maraccas, and bongo. There are 16 different rhythm patterns ranging from waltzes to samba and cha-cha.

The required performance is selected by push-buttons and there are four separate cancel buttons for cutting out the cymbal, cow bell, bass drum and claves. The unit is operated by manual start or footswitch operation and a tempo or speed control, mounted on the front panel, is also incorporated.

The rythm unit is designed to play through any high impedance amplifier, retails at £147 and is available from any branch of Selmer Musical Instruments Ltd., or for nearest stockist write to Severn Musical Instruments Ltd., Woodchester, Stroud, Gloucester.

Another sound effect in vogue at the present time is that of reverberation. Readers who are experimenting in this field may be interested in the range of Gibbs Spring Line units from Hammond Organ (U.K.) Ltd. These units range from a delay time of 0.027sec large spring, 0.022sec small spring to 0.038sec large spring, 0.025sec small spring. The times vary from 2sec to 1.5sec The delay

Prices and further particulars can be obtained from Hammond Organ (U.K.) Ltd., Deansbrook Road,

Edgware, Middlesex.

SPEED SENTRY

The fear of prosecution for speeding and the inevitable licence endorsement which accompanies this offence is always a threat to the person who is dependent on his licence for his livelihood. The Speedset Audible Speed Indicator from Automents Ltd. is a worthwhile fitment for the car as it removes the necessity for constantly looking down at the speedometer to check the speed, and enables the driver to give full attention to the road.

The Speedset gives an audible alarm instantly a preselected road speed is exceeded. The selection of the required road speed is accomplished by depressing push buttons, the range available is 30, 40, 50, 60 and 70 m.p.h. or for continental use 50, 65, 80, 100 and 120 k.p.h.

The speed alarm consists of two main units, the control unit which is fitted beneath the dashboard, and a self-adhesive transducer which fixes to the back of the vehicle's speedo-meter and plugs into the control unit. The transducer detects the rotor speed within the speedometer and transmits this to the control unit where the actual road speed is computed and triggers the alarm if the selected speed is exceeded.

An adjustable volume control is fitted and preset potentiometers are accessible from the front panel of the control unit enabling a certain amount of speed setting variations, i.e. 30 m.p.h. can be set between 28 and 38 m.p.h.

Designed to fit any 12V positive or negative earth vehicle the current consumption is claimed to be less than a car parking light. The prize of the Speedset is £19 15s and further particulars can be obtained from Automents l.td., New Street, Oadby, Leicester.

STROBOSCOPE

The latest version of the Dawe transistor stroboflash, type 1209C, is ideal for educational and industrial laboratories (not psychedelic).

The new model has internal modifications and additional facilities and is intended for the measurement of the repetition rate of cyclical events, or for observing such events in slow motion.

The instrument has a basic operating range from 300 to 18,000 flashes per minute in three switchable ranges. Speeds up to 180,000 rev/min can be measured by using harmonics by virtue of the very short flash duration of 5-10 microseconds. depending on flash rate. The Xenon tube used gives high-intensity white light and provides a mean illumination at 1 metre distance which increases from 50 lux on the 18,000 flashes/min range to 100 lux on the 1,800 flashes/min range. Mean flash tube power is 6W maximum. The flash rate is controlled by a

variable transistorised oscillator, which also drives the anologue frequency meter calibrated directly in flashes/min. Alternatively, external mechanical contactor or photoelectric pick-up can be used; in both cases the flash rate is indicated on the meter.

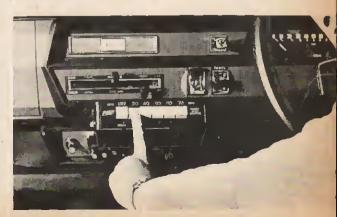


Dawe Stroboflash type 1209C

An extension lamp can be plugged in and there is now a selector switch which enables the output to be switched between the built-in and extension lamps.

Further specifications and application details can be obtained from Dawe Instruments Ltd., Concord Road, Western Avenue, London, W.3.

Speedset audible speed indicator marketed by Automents Ltd.



LOGIC TESTER

A new logic tester, designed to ease the problem of checking a digital system is being manufactured by Southern Techniques (Electronics) Ltd., Waideck House, Waldeck Road, Maidenhead, Berks.

The tester emits an audible tone, the pitch of which is high when its probes are connected to a logical "1" level, and low when its probes are connected to a logical "0" level. An open circuit condition between the probes is indicated by the absence of tones. An earphone jack is provided which disconnects the internal loudspeaker when the earphone plug is inserted.

A particularly useful feature is a built-in transient detector. With the tester switched to transient detection and the probes connected to a circuit under test, then the arrival of a logical "1" pulse causes the tester to emit a continuous tone until reset.

JA.

JA.

STEL SARKE

Logic Tester from Southern Techniques (Electronics) Ltd.

Models of this tester are available for operation from internal batteries or mains supply, and suitable for high or low voltage logic systems, prices range from £15 to £20.

DIGITAL CLOCK

Readers experimenting with their own designs for constructing digital clocks may be interested in the recent product introduced to the U.K. market by ITT Component Group Europe. It is a synchronous motor-driven digital time indicator incorporating an alarm setting mechanism. The alarm operates a changeover microswitch which permits any desired warning device to be triggered at the selected time.

The standard model operates from 240V a.c. 50Hz. Time indication is for a 12-hour clock, divided into minute intervals and the alarm graduation is for 24 hours at 10 minute intervals. The indicating numerals are white on black.

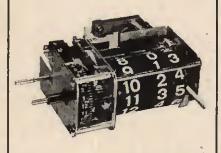
Full particulars are available from ITT Components Group Europe, Trading Services, Edinburgh Way, Harlow, Essex.

INTEGRATED CIRCUITS

A 250mW low power audio i.c. amplifier, type MFC 4000, is the first of a new range of low cost integrated circuits designed specifically for the consumer market by Motorola Semiconductors.

The special feature of this i.c. is that the pin spacing is wider, uses smaller chips, fewer circuit elements and is designed so that it will easily mount on the standard perforated boards. Built in a four-lead package, it is the equivalent to six transistors, three diodes and five resistors.

The transformerless output is suitable for loads up to 16 ohms and a typical harmonic distortion figure at 50mW is 0.7 per cent. The input sensitivity is 15mV r.m.s. for 50mW



ITT Synchronous motordriven digital time indicator

output. Powered by a 9V d.c. supply the quiescent current is 3.5mA.

The type MFC 4000 is designed mainly for small radios but can be used for any low power amplifier output stages.

Also in the same range is the type MFC 4010 which is a high gain wide-band amplifier that could be used either as a general purpose a.f. amplifier or as an i.f. amplifier at 465kHz.

This i.c. contains three transistors and five resistors. Typical output noise is ImV r.m.s. and with a 18V supply the current drain is 3mA.

Another integrated circuit for use either as a television intercarrier sound limiter-amplifier, detector and a.f. pre-amplifier, or for a similar function in high quality f.m. stereo radio receivers and tuner units is the TAA661 from SGS (United Kingdom) Ltd.

At an input level of 1mV the a.m. rejection is better than 40dB. It is claimed to give good performance from a supply voltage ranging from

4.5 to 15V, with a typical quiescent current of 15mA at 12V. The limiting threshold voltage is about $100\mu V$ and remains independent of the supply voltage.

Designed to replace the conventional complementary-symmetry audio output stage, driver and preamplifier stages in 9V or 12V battery-operated radio receivers, record players and tape recorders, the TAA661 is capable of delivering IW r.m.s. from a 9V supply without a heat sink.

The integrated amplifier can be directly driven from a diode detector circuit or crystal pick-up with negligible distortion. Few external components are required and bias conditions are stabilised; no pre-set resistor or setting-up procedure is necessary. Feedback is available if required by the use of one external resistor.

A 3 watt 24V version is available and is designated TAA621,



Integrated circuits from Motorola Semiconductors

LITERATURE

The new edition of the excellent Henry's Radio components catalogue has a new companion in the form of a special audio catalogue. Like their other catalogue the same high standard is maintained throughout and separate sections deal with amplifiers, tuners, tape recorders, record decks and accessories.

The catalogues are to be revised every three months in future.

Henry's are now expanding their business to further premises and the electronic components and equipment section is moving to 354 Edgware Road, London, W.2. The high fidelity section, with four demonstration rooms, to 356 Edgware Road, and the store at 309 Edgware Road is to become the electronic organ department coupled with public address and discotheque equipment.

The existing premises at 303 Edgware Road will handle all mail order and identical sales for the time being.

MICRO SWITCH

5 amp. changeover contacts, 1/9 each, 18/- doz. 15 amp. model 2/- each or 21/- doz.



TOGGLE SWITCH 3 amp. 250V with fixing ring. 1/6 each, 15/- doz.

CONSTRUCTORS' PARCEL

CONSTRUCTORS' PARCEL

1. Pleasey miniature 2 gang tuning condenser
with built-in trimmers and wave gang switch.

2. Perrite slab aerial with coils to suit the above
tuning condenser. 3. Circuit diagram giving all
component values for 6 transistor circuit covering
full medium wave and the long wave band around
radio 2. The three items for only 7,6 which is
half of the price of the tuning condenser alone.

10 AMP 24Y BATTERY CHARGER Ideal unit for garage, boat station, etc., \$22,18.0 each plus carriage and cost.

BEHIND THE EAR DEAF-AID

Made by a very famous maker. Thoroughly overhauled, cleaned and reconditioned. Quaranteed 6 months. Regular price around £50. Our price £10,

ISOLATION TRANSFORMERS

200-250 MAINS
A must if you work on mains equipment. Prevents accidents and shocks even in danip conditions. Input and output separately screened by connection block. 100 watt £3.10.0, 250 watt £5.

SLOW MOTION DRIVES

For coupling to tuning condensers, etc. One end tin shaft, the other end fits to a lin shaft with grub screws. Price 4/8 each, 48/- dozen.

LARGE PANEL MOUNTING MOVING COIL METERS

Size 5ia × 4ia Centre zero 200-0-200 micro amp, made by Sangamo Weston. Regular price probably £8. Our price 59.8. Ditto but 100-0-100 79/6.

A.C. AMMETER

0-5 amps. flush mounting—moving iron. Ex equipment but guaranteed perfect 29'6.

CIRCUIT BOARDS

Heavy copper on 3/32 paxolin sheet ideal for making power packs, etc., as sheet is very strong and thick enough to allow copper to be cut away with hacksaw blade. 5in × 5in 1/6 each.

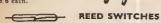
4kVA AUTO-TRANSFORMER

in ventilated sheet steel case—tapped 110V-140V-170V-200V-230V. Ex equipment but guaranteed perfect \$19.10.0, carriage at cost.

PP3 BATTERY ELIMINATOR

Run your small transistor radio from the mains—full wave chreuit. Made up ready to wire into your set and adjustable high or low current.





tilass encased, switches operated by external magnet—gold welded contacts. We can now offer

magnet—gold welded contacts. We can now offer 3 types:

Ministure. Im long × approximately im diameter. Will make and break up to 1A up to 300 volts. Price 2/6 such, 24/- dozen.

Standard. 2in long × 3/in diameter. This will break currents of up to 1A, voltages up to 250 volts. Price 2/- ench, 14/- per dozen.

Flat. Flat type, 2in long, just over , in thick, flattened out, so that t can be fitted into a smaller space or a larger quantity may be packed into a square solenoid. Rating 1 amp 200 volts. Price 6/- each. 23 per dozen.

Small ceramic magnets to operate these reed switches 1/8 each. 18/- dozen.

0-005mFd TUNING CONDENSER Proved design, ideal for straight or reflex circuits 3/8 each, 24/- dozen.

SUB-MINIATURE MOVING COIL

as used in behind the ear deaf-aids Acts also us earphone size only \$\frac{1}{2}\ln \times \frac{1}{2}\ln, \times \frac{1}{2}\ln, \times \frac{1}{2}\ln, \times \frac{1}{2}\ln, \times \frac{1}{2}\ln \times \frac{1

CHART RECORDER MOTOR

Small (2in diameter approx.) instrument motor with fixing flange and apintile (3in long, 3in diameter) integral gear box gives 1 rev. per 24 hours. 298.

IGNITION (E.H.T.)TRANSFORMER Made by Parmeko Ltd., Primary 240V 50Hz. Secondary 6kV at 23mA. Size approx. 4iin · 3iin × 2iin thick. 29:6 plus 4;6 P. & P.



12 VOLT EXTRACTOR FAN BY DELCO

Ideal for ventilation in Caravan, Car of Boat, 6 Bladed 5in diameter fan inside heavy duty cylinder with 3 point Rxing flange. 5jin diameter fixing hole. Length approx. Sjin. Exceptional bargain 27/6 plus 5/6 post and insurance.

INTEGRATED CIRCUIT BARGAIN

INTEGRATED CIRCUIT BARGAIN

A parcel of integrated circuits made by the fannous Pleasey Company. A
once-in-a-lifetime offer of Micro-electronic devi-es well below cost of manufacture. The parcel contains 5 ICs all new and parfect, first-grade device,
definitely not sub-standard or seconds. The ICs are all single silicon chip
General Purpose Amplifiers. Regular price of which is well over \$\pm\$ can be considered and in addition you will receive a list
of 50 different ICs available at bargain prices \$\pm\$/- upwards with circuits and
technical data of each. Complete parcel only \$\pm\$ 1 post past; or Itsh and all
data 10/- post free. Credited when you order ICs value 30/- and upwards.

24-HOUR TIME SWITCH

24-HOUR TIME SWITCH
Mains operated. Adjustable Contacts give 2 on/offs
per 24 hours. Contracts rated 15 amps. repeating
nechanism so ideal for shop window control, or to
switch ball lights (anti-burglar precaution) while you
are on holiday. Made by the famous Smiths Company.
This month only 80/6 with Perspex cover, plus 3/6
postage and insurance, a real snip which should not be
missed.

DISTRIBUTION PANELS

DISTRIBUTION PANELS
Just what you need for work bench or lab.
4 × 13 amp sockets and on/off switch with
neon warning light in metal box. Takes standard 13 mnp
complete with 7 feet of heavy cable.
89/8 wired up, ready to work plus 4/6 post and insurance.
5 amp 3 pin model 35/-.

BARGAIN OF THE YEAR Takes standard 13 amp fused plugs. Supplied

MICROSONIC RADIOS

Transistor Key chain Radio in very pretty case, alze 2\frac{1}{2} \times 2\frac{1}{2}

Sensitivity: 5 int/m. Intermediate frequency: 468kc/s, or 465kc/s. Power output: 40ntw. Antenna: ferrite red. Loudspeaker: Fernment magnet type. In transit from the East these sets suffered slight corrosion as the batteries were left in them but when this corrosion is cleared away they should work perfectly—offered without guarantee except that they are new Price only 24/8 plus 2/8 post and insurance, less batteries. 6 for \$7, post free.

THE 5-5 WATT STEREO AMPLIFIER

Made by one of our most famous makers for a de-luxe player. This amplifier has a quality of reproduction much better than average. Using a total 16 transistors and a generously sized mains power pack. Controls include bass, treble, balance and volume. Suitable for 8-16 others impedance speakers with eroseovers for tweeter mid-range and bass thus giving option of 1, 2 or 3 speakers per channel. Offered at about one third of its original price only \$9.10.6 plus 6/6 post and insurance.

OUT OF SEASON BARGAIN 3 KW TANGENTIAL HEATER UNIT



HEATER UNIT
This heater unit is the very latest type, most efficient and quiet running. Is as fitted in Hoover and blower heaters costing £16 and nore. We have a few only. Comprises motor, impeller, 2kW element and 1kW element and lowing switching 1, 2 and 3kW and with thermal safety cut-out. Can be fitted into any nutell line case or cabinet. Only need control switch. 59/6. 2kW Model as above except 2 kilowatte 39/6. Postage and insurance 6/6. Don't mise this.

THIS MONTH'S SNIP AUTO ELECTRIC CAR AERIAL

With dash board control switch—fully extendable to 40" or fully retracted. Suitable for 12V positive or Neg. earth—supplied complete with fitting instructions and ready wired dash board switch \$5.18.8 plus 5/-.



" RECORD CHANGER BARGAIN

The "Princess" 4-speed automatic record changer and player for beauty, long-life. Will take up to ten records which may be mixed, stylus brush cleans stylus after each playing—other features include pick-up height adjustment and stylus pressure adjustment. This truly is a fine instrument which is a cancelled export order. Therefore they have travelled back and forth and may need mechanical re-adjustment. We offer these at less than the price of a single player— The "Princess" these at less than the price of a single player only 49/6 plus 9/6 p. 4 p. 200-240V.



STANDARD WAFER SWITCHES



Standard size 11 wafer—silver-plated 5-amp contact, standard in spindle 2in long—with locking washer and nut.

No. of Poles 2 way 3 way 4 way 5 way 6 way 8 way 9 way 10 way 12 way

	1 pole	8/6	8/6	6/6	6/6	8/6	6/6	6/6	6/6	5/6
	2 poles	8/6	6:6	6/6	6/6	6/6	6:6	6/6	10/6	10/6
	\$ poles	6/6	6/6	8/6	6/5	10/0	10/6	10/6	14/6	14/6
	4 poles	6/6	6:6	6/6	10/8	10/6	10/8	10/6	18/6	18/6
	5 poles	0/6	6/6	10/6	10/6	14/0	14/6	14/6	22/6	22:6
	ti poles	6/6	10/6	10/6	10/6	14/6	14/6	14/8	26/6	28/6
ľ	7 poles	10/8	10/6	10/6	14/6	18/6	18/8	18/6	80/6	80/6
	8 poles	10/6	10/6	10/6	14/6	18/6	18/0	18/6	84/6	34/6
	9 polea	10/6	10/6	14/6	14/6	22/6	22/6	22/6	38/6	88/6
	10 poles	10/6	10/6	14/6	18/6	22/6	22/6	22/6	42/6	42/6
	Il poles	10/6	14/6	14/6	18/6	26/6	28/8	26/6	46/6	46/6
	12 poles	10/6	14/6	14/6	18/6	26/6	26/6	26/6	50/6	50/6

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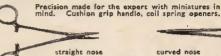
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						(886	note below)
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•0	1 W	5%		4·7 Ω -330k Ω	E24	'2-5d	2d	1.75d
C	1W	5% 5% 10%		4-7Ω~10MΩ	E12	2-5d	24	1.75d
C)W	10%		4·7 Ω -10M Ω	E24	34	2.54	2 25d
C	iw	10%		4·7Ω-10MΩ	E12	6d	5d	4-5d
MO	1W	2%		10Ω~1MΩ	E24	94	84	7à
WW	1W	10% ± 1/200	3	0.22 Ω - 3.9 Ω	E12	15d all qu	unntities	
WW	8W	5%	-	12Ω-10kΩ	E12	15d all qu	rantities	
WW	7W	ō%		12Ω-10kΩ	E12	18d all or	uantities	
CODES	C = earbon	film high stability	low	noise, MO - metal	oxide Electrosi	TRo nitra	low noise.	WW - wire

60DES: C = carbon film high stability low noise. And method in the processor.

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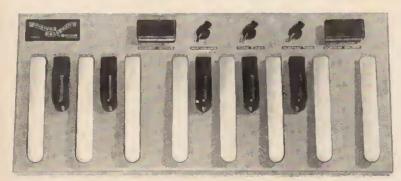
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A really high fidelity mon-aural amplifier with performance charac-teristics to suit the most dis-criminating listener. 6 tran cicemit mith integrated preamplifler assembled on special printed AD161-AD162 operating



ADISIA-D162 operating in aymmetrical complementary pair. Output transformer complete to 3 ohm and 15 ohm speaker sockets. Standard phono input sockets. Pull wave bridge rectifier power supply for s.c. mains 200–240v. Controls: bass, treble, volume/on/off. Function selector for PUI, PUZ, tape, radio. The HSL.700 is strongly constructed on rigid steel chassis bronze hammer enamel finish, size 91.25 ×41 in. high. Sensitivity—PUI—50m/v, 1 meg input impedance. PUZ—110m/v, 1 meg input impedance. Tape—110m/v, 1 meg input impedance. Tape—110m/v, 1 meg input impedance. Tape—140m/v, 1 meg input impedance. Tape—150m/v, 56k input impedance. Tape—150m/v, 56k input impedance. Tape—160m/v, 1 meg input impedance. Tape—160m/v, 1 meg input impedance. Tape—160m/v, 1 meg input impedance. Tape—170m/v, 1 meg input impedance. Tape—17

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chassis, size 71 in w. X sin. d. x 4 in. h. neorporates ECC39, 4 in. h. neorporates ECC39, EL84, EZ80 valves. Heavy duty, double wound mains transformer and output transformer matched for 3 chm speaker. Separate volume control and now with improved wide range tone controls giving base and treble lift and cut. Negative feedback line. Output 4 whats. Front panel can be detached and leads extended for remote mounting of controls. Complete with knobs, valves, etc., wired and tested for only \$4.15.9, P. & P. 5/-.

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A super quality gran amplifier using a double wound mains transformer, EZ80 rectifier and ECL82 triode pentode valve as audio amplifier and power output stage. Impedance 3 ohms. Output approx. 3-5 watts. Volume and tone controls. Chassis size only 71n, widex 31n, deep x 6in, high overall, AC mains 260/240V. Supplied absolutely Brand New completely wired and tested with valves and good quality output transformer. FEW ONLY.

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2N916 4/6 AF110 6/6 OAT 3/2 2N918 7/6 AF117 5/- OAB 3/4 2N919 4/- AF117 5/- OAB 3/4 2N919 4/- AF118 18 6/- OA70 2N920 5/- AF181 8/6 OA70 2N920 8/6 AF132 8/6 -OA70 2N920 8/6 AF132 8/6 -OA70 2N920 8/6 AF132 8/6 -OA70 2N11922 8/- AF127 4/- OA71 2N11929 8/- AF127 4/- OA71 2N11929 8/- AF127 4/- OA73 2N11930 4/- AF128 8/- OA74 2N1304 5/- AF181 8/6 OA80 2N1304 5/- AF181 8/6 OA80 2N1305 6/- AF181 8/6 OA80 2N1305 6/- AF181 8/6 OA80 2N1305 6/- AF181 8/6 OA80 2N1306 6/- AF181 8/6 OA80 2N1307 6/- AF181 8/6 OA80 2N1307 6/- AF181 8/6 OA80 2N1308 6/- AF181 8/6 OA80 2N1309 6/- AF181 8/6 OA80 2N1613	2N914	4/8	AF114	6/6	MPF105	8/-	1 1/2 100 t 1/0	300 T A/-
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2N1306 5/ AF238 8/- OASS 4/- 2N1308 6/ AFX19 28/8 0A90 4/- 2N1308 6/ AFX19 28/8 0A90 1/6 2N1308 6/ AFX12 10/- OASS 1/6 2N1318 8/- OASS 1/6 2N1318	2N1132	B/-		8/-	OA74	2/-		
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28832		8/6	BC109	8/	OC22	9/8	, -/- 100 , 1/-	
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2N3710 2N3619 2N3820 2N3823 2N3900 2N3900 2N5027 2N5027 2N5028 2N5307	8/ 20/ 17/ 10/6 11/ 10/6 11/6 7/6	BC145 BC147 BC148 BC149 BC157 BC160	4/9 4/6 5/- 4/-	D246 DD006 DD007 DD008	7/6	OAZ207 OAZ208 OAZ210 OAZ222 OAZ224	6/6 6/8 9/6	XA162 XA162 XB101	6/- 6/- 8/6 8/6
2N3710 2N3619 2N3820 2N3823 2N3900 2N3900 2N5027 2N5027 2N5028 2N5307	8/ 20/ 17/ 10/6 11/ 10/6 11/6 7/6	BC145 BC147 BC148 BC149 BC157 BC160 BCY31	4/9 4/6 5/- 4/-	D246 DD006 DD007 DD008 GD3	7/6 6/6 8/- 7/6 6/6	OAZ207 OAZ208 OAZ210 OAZ222 OAZ224	6/6 6/8 9/6	XA162 XA162 XB101	6/- 6/- 8/6 8/6
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2N3710 2N3819 2N3820 2N3823 2N3900 2N3900A 2N5027 2N6028 2N5307 2N5309 2N0309 2S005 28013	8/ 20/ 17/ 10/6 11/ 10/6 7/6 7/6 7/6 11/ 14/ 15/ 16/6	BC145 BC147 BC148 BC149 BC157 BC160 BCY31 BCY32 BCY32 BCY34 BCY38	4/9 4/6 5/- 4/- 12/6 6/- 7/6 5/- 5/6- 7/-	D246 DD006 DD007 DD008 GD3 GD4 GD5 GD6 GD6 GD8 GET102	7/6 6/6 8/- 7/6 6/6 7/- 6/6 5/- 5/-	OAZ207 OAZ208 OAZ210 OAZ222 OAZ224	10/- 6/6 6/8 9/6 9/6 7/6 4/6 9/- 15/-	XA162 XA162 XB101 XB121 XK505 XK518 Z2A82CR ZR24	5/- 5/- 8/6 8/6 5/- 6/- 5/-

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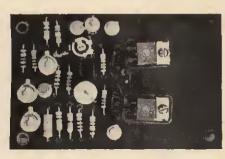
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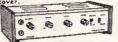
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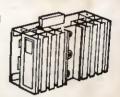
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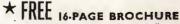
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