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AMPLIFIER KITS

P.W. DOUBLE 12

Complete stereo kit including cabinet, but less panel and other metalwork. £23 net. Available in separate packages as follows: Main amplifier kit £3.19.6 per channel, net. Accessories 19/mono, 36/- stereo.

Pre-amplifier kit £1.7.0 per channel, net. Accessories 13/6 mono, 27/3 stereo.

Tone control kit 19/- per channel, net. Accessories 8/9 mono, 22/6 stereo.

Power supply kit £4.10.0 mono or stereo, net.

Cabinet kit £2.12.6 net. Metalwork available separately from other sources, details on request

30 WATT (designed by Dr. A. R. Bailey). Published May 1968 W.W., modified November 1968 W.W.

Full kit for main amplifier £9.9.6 (less power supply). Transistors only for main amplifier £7.9.6. PC board supplied free with above kit. Heat sinks for output transistors 8/6 extra.

Power supply kit, unregulated, November 1969 circuit £4.14.0. Regulated version, 60V 1-6A or 0-8A, current limiting, re-entrant characteristic: does not need re-set button £8.10.0. Transformer only: 0-25-45-50V 2A 58/-

8 x 8 watt Stereo only. Peak Sound SA 8 x 8 kit. Sensitivity 50mV into 1M Ω , output into 5 Ω . Complete with cabinet and power supply. Kit complete £16.10.0 net. Built and tested £21 net.

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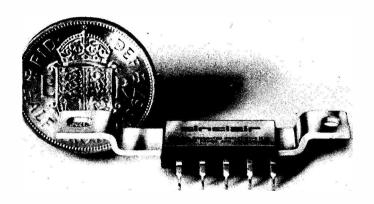
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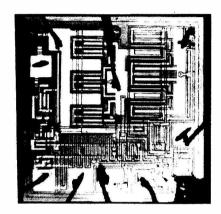
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10 WATT MONOLITHIC INTEGRATED CIRCUIT AMPLIFIER AND PRE-AMP





theworld's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output 5 watts R.M.S. (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 zenor diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.

The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of the usual tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required for producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. It also enables us to give a 5 year guarantee on each IC-10 knowing that every unit will work as perfectly as the original and do so for a lifetime.

■ SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. Frequency response 5 Hz to 100 KHz±1dB. Total harmonic distortion Less than 1% at full output. 3 to 15 ohms. Load impedance 110dB (100,000,000,000 times) total. Power gain Supply voltage 8 to 18 volts. 1 imes 0.4 imes 0.2 inches. Sensitivity 5mV. Adjustable externally up to Input impedance 2.5 M ohms.

■ CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

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C10 with IC.10 manual and 5 year guarantee

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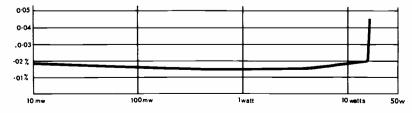
Z.30

THE WORLD'S LOWEST DISTORTION HIGH FIDELITY AMPLIFIER.

For four years, the Sinclair Z.12 dominated the constructor world, being the best selling unit of its kind this side of the Atlantic. Excellent as it was, the new Sinclair Z.30 is still better. Half the size of the Z.12, it has more than twice the power, very much greater gain and a level of distortion 50 times lower. This incredible figure results from using over 60dB of negative feed back with a constant current load to the driver stage obtained by incorporating a two transistor circuit in place of the more usual bootstrapping. 9 silicon epitaxial planar transistors are used to provide enormous power; up to 20 watts RMS sine wave (40 watts peak). The circuitry of this marvellous amplifier allows it to be operated from any voltage from 8 to 35 to perfection. At all output levels, distortion is only 0.02%. This puts true laboratory standards into the hands of every user of a Z.30. Two Z.30s and a new Stereo Sixty will make a stereo assembly of such perfection that it could not be bettered in its class no matter how much you spent. But the Z.30 has an enormous variety of applications, particularly where quality, precision and reliability are essential. It can also be used entirely on its own as an amplifier for an efficient economy record player.

APPLICATIONS

Hi-fi amplifier; car radio amplifier; record player amplifier fed directly from pick-up; intercom; electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the Z.30.



SPECIFICATIONS

Power output—15 watts R.M.S. into 8 ohms using a 35V supply: 20 watts R.M.S. into 3 ohms using a 30V supply.

Output-Class AB.

Frequency response—30 to 300,000 Hz \pm 1dB.

Distortion—0.02% total harmonic distortion at full output into 8 ohms and at all lower output levels.

Signal-to-noise ratio—better than 70dB unweighted.

Input sensitivity—250mV into $100k\Omega$.

Damping factor->500.

Loudspeaker impedances—3 to 15 ohms.

Power requirements—From 8 to 35V d.c. (The Z.30 will operate ideally from batteries if required.)

Size— $3\frac{1}{2} \times 2\frac{1}{4} \times \frac{1}{2}$ inches.

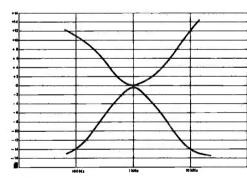
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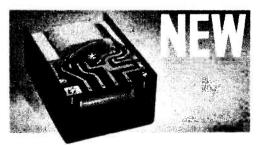




Curves to show bass and treble cut and boost

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This attractive and completely new unit is intended for use with two new Z.30 amplifiers to provide the finest possible standards of stereo reproduction. Four press buttons and four rotary controls are used to provide on-off, three input selectors and Volume, Bass cut/boost, Treble cut/boost and Stereo balance. The on-off button also switches the power amplifiers. The front panel in brushed aluminium is flush mounted to the cabinet front, it being necessary only to drill holes to accommodate the controls, Rear adjustable brackets hold the chassis tight to the cabinet. The very latest ganged rotary controls are used to afford compactness and extra long working life free from noise.

The Stereo-60 may also be used with 2 IC-10's or any other high performance amplifiers.

SPECIFICATIONS

- ●Input sensitivities—Radio—up to 3mV Magnetic Pickup-3mV: correct to R.I.A.A. curve ± 1dB; 20 to 25,000 Hz. Ceramic Pickup-up to 3mV: Auxiliary—up to 3mV.
 Output—1 volt.
- Signal-to-noise ratio—better than 70dB.
- ●Channel matching—within 1dB. ●Tone Controls—TREBLE +15 to —15dB at 10 KHz: BASS +15 to -15dB at 100 Hz.
- ●Power consumption 5mA.
- Front panel-brushed aluminium with black knobs and controls.
- ●Size 8±×1±×4 inches.

PZ.5 POWER SUPPLY UNIT

A new heavy duty mains power supply unit designed specially to drive two Z.30s and a Stereo Sixty. New compact design. For AC Mains, 200-240V/50Hz. £4.19.6

USE THIS COUPON FOR Z.30, STEREO 60 AND P.Z.5.

Q.16 LOUDSPEAKER AND MICROMATIC ON NEXT PAGE

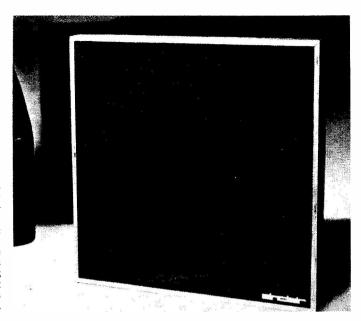
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Q.16

new elegance in an outstanding loudspeaker

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The Q.16 will handle loading up to 14 watts R.M.S. and presents an 8 ohm impedance to the amplifier output. Frequency response extends from 60 to 16,000 Hz, with exceptional smoothness. A specially designed driver pressure chamber to ensure good transient response at all frequencies. Size: $9\frac{3}{4}$ square \times $4\frac{3}{4}$ deep from front to back

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Specifications Black plastic with anodized aluminium front panel, spun aluminium dial.

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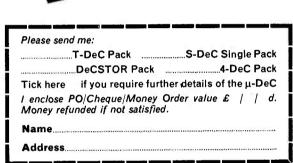


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MODEL 200

Large 3 < 2in meter. Full scale accuracy: DOY and current: £2%, ACV: ±3%, resistance ±3%. Special 0-6V DC range for transfer circuit measurements.

SPECIFICATION

■ DCV: 0-0-6-30-120-600-1,200V at 20K/OPV. ■ ACV: 0-6-30-120-600-1,200V at 10K/OPV. ■ DC Current: 0-0-6-6-00-16-00-1,200V at 10K/OPV. ■ DC Current: 0-0-6-6-00-6-00n-A. ■ Resistance: 0-10K-100K-1M-10M/ohms (68-590-58K-58K-58K at mid-scale). © Capacitance: 0-002-0-2uf (AC 6V range). ■ Decibels - 20 to +634B. ■ Output: 0-05uf (AC 6V range). ■ Decibels - 20 to +634B. ■ Output: 0-05uf (Cf. 7 type) batteries. Black bakelite cabinet- Size 5; 3; 13in. Complete with test leads.



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measurement ranges.

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DENSHI KIT SR-2A as SR-1A with these additional parts: SB transistor for AF; 2 resistors; 1 capacitor; crystal microphone; test probes; lectrode; additional connecting pieces; 9V battery. This kit permits the building of 30 circuits

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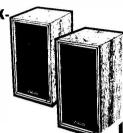
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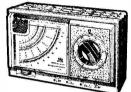


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20,000 O.P.V. pocket multimeter with mirror scate and built in thermal protection circuit. Exceptionally large easy to read meter with D/arsonval movement. Colour coded scales. Single positive click-in, recessed selection switch for all ranges. Ohns zero adjustment. Range spec. A.C. volts: 0-5-30-300-1200 v at 10/K/ohns/V. Resistance: 0-69K-6megs. D.C. curtent: 0-69/L-300nA. Decibels: -20dB to +17dB. Hand calibration gives extremely high standard of accuracy on all ranges. Uses one 12N penlight battery. Strong impact resistant plastic cabinet—size only 4\times 3; \times 1 \frac{1}{2} \times \text{Time.} Two colour buff/green finish. Complete with test leads and battery. Original list price 5gns.



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Post 2/6

TMK PL-436

20,000 O.P.V. Multitester for the amateur or professional. Features mitror scale and wood grain finish front panel. Spec.: D.C./V ranges: 9-6, 3, 12, 30, 120, 500V at 20K/O.P.V. A.C./V ranges: 3, 30, 120, 600V at 20K/O.P.V. A.C./V ranges: 3, 30, 120, 600V at RK/O.P.V. D.C. current: 50 μ A, 0-6, 60, 609mA. Resistance: 10K, 100K, 1M and 10M ohnus end scale (55, 509, 6-5K and 65K ohnus centre scale). Decibels: -20 to +57dB in four ranges. Operates on $2\times15V$ Cr type batteries. Size: $54\times4V$ 2jin. Complete with test leads, batteries and instructions.



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TRANSISTOR TWO WAVEBAND RADIO RECEIVER FROM RUSSIA

THE **Astrad** ORION



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The Orion is supplied fully built and tested complete with battery, left and right fitting earphone supports and attractive black and ivory plastic presentation/carrying case (matchin) the Orion). Never miss your favourite music sport, news—the Orion is an ideal gift for all, probabling a constant source of enjoyment without disturbing others.

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PRICE 19/6 extra. Post free with radio-otherwise 2/-

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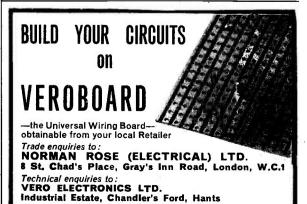
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Quette Integrated Transistor Stereo Amplifier

9GNS.

The Duetto is a good quality amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.
SPECIFICATION:

R M S, power output: 3 watts per channel into 10 ohms speakers INPUT_SENSITIVITY. Suitable for medium or high output crystal cartridges and tuners. Cross-talk better than 30dR at 1Ke 's

CONTROLS: 4-position selector switch (2 pos mono and 2 pos stereo) dual ganged volume control.

TONE CONTROL. Treble lift and cut. Separate on off switch. A preset





The Clare

81 GNS.

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SPECIFICATION:
Sensitivities for 10 watt output
at 1KHz into 3 ohms. Tape Head: 3mV (at 3)
i.p.s.) Mag. P.U.: 2mV. Cer.P.U.: 80mV. Tuner: 100mV.
Aux. 100mV. Tape/Rec. Output. Equalisation for each
input is correct to within +240 (R.I.A.A.) from 2014 to 20KHz.
Tone Control Range: Boss: 13dB at 60Hz. Treble: ± 14dB at 15KHz. Total Distortion: (for 10 watt output) < 1-5%. Signal Noise: < -60dB. A.C. Mains
200-250V. Size 12jin long, 4jin deep, 2jin high. Built and tested.

THE RELIANT Mk. II SOLID STATE GENERAL PURPOSE AMPLIFIER

61 GNS. Plus P. & F. 7/6 In teak finished case

In teak finished case

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Transistors: 4 silicon and three germanium.

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8 × 5in speaker 14/6 plus 3/- P. & P. Mk. 15 jg ms. plus 7/6 P. & P. Less teak

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Plus P. & P. 7/6

4 ohms speakers (20 watts monoral). Input: 6-position rotary selector switch (3 pos. mono and 3 pos. stereo). P.U., Tuner, Tape and Tape Rec. out. Sensitivities: All inputs 100mV into 1-8M ohm. Frequency Response: 40Hz-20KHz ±2dB. Tone Controls: Separate bass and treble controls. Treble 13dB lift and cut [at 15KHz]. Boss: 15dB lift and 25dB cut [at 60Hz]. Volume Controls: Separate for each channel. A.C. Moins Input: 200-240V, 50-60Hz. Size: 12½ × 6in × 2½in teak-finished case. Built and tested. P. & P. 7/6.

Viscount Mark II for use with magnetic pick ups specification as above. Fully equalised for magnetic pick ups. Suitable for cartridges with minimum outputs of 4mV/cm/sec. at Ikc. Input Impedance 47k. 15 gns. plus 7/6 P. & P.

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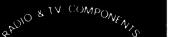
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Input 250V OUTPUT (All RMS values) 4 windings of 11-5V connected in series total 46V at 4-5 amps (conservatively rated). The following combinations may be used. 1.23—0—23V; 2. 46V. Both of these above voltages are commonly used in medium to high powered transistor amplifiers, power supplies, etc.

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Also see opposite page



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AC mains 230/250V, complete with pull switch. Size

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10W SOLID-STATE HI-FI AMP WITH INTEGRAL PRE-AMP

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Control assembly: including resistors and capacitors.

1. Volume: PRICE 5/-.

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3. Comprehensive bass and treble: PRICE 10/-.

The above 3 items can be purchased for use with the X101.

POWER Supplies for the X101: P101 M (for mono) 35/- plus 4/6 P. & P.

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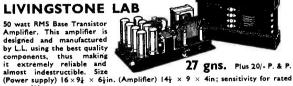
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Inputs—6 position rotary switch (3 position mono, 3 position stereo). Tuner 150 mV into 680k. Magnetic pick-up fully equalised and suitable for magnetic cartridges with minimising output of 4mV/cm/sec. Load 47k. Ceramic pick-up 150 mV into 680k. Sensitivities taken for 200mV output. Control—separate volume controls for each channel. Twin ganged bass, 12dB lift and 15dB cut at 60c/s. Twin ganged treble, 10dB lift and 15dB cut at 10kc/s. Voltage required 23-30v D.C. at 5mA. Size 12½ $^{\circ}\times 23^{\circ}\sim 10^{\circ}$. In teak finished case, complete with front panel and knobs. Built and tested.

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This PRESTOLOCK 5 station Push-Button Tuner Heart with Manual Over-ride is an ideal basis for a quality AM car radio. Size 6½ × 4 × 2in. 25/- Plus 3/- P. & P.





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Size $3\frac{7}{4}\times2\frac{1}{4}\times1\frac{3}{4}$ in. Meter size $2\frac{1}{4}\times1\frac{3}{4}$ in. Sensitivity 1000 O.P.V. on both A.C. and D.C. volts. 0–15, 0–150, 0–1000 D.C. current 0–150mA. Resistance 0–100k Ω . Complete with test prods. battery and full instructions.

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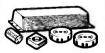


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Similar to above: 80W. Fluorescent Light Kit incorporating GEC choke size 11½ × 1½ × 1½in. 2 bi-pin holders, start and starter holder. P. & P. 6/6.

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Dart Electronics has been appointed by General Avionics Limited as their U.K. distributor for their FM Tuner kit, the first to use integrated circuits with pulse counting techniques developed by Marconi-Elliott Microelectronics.

The circuit has built-in automatic frequency control, and with the inherent stability of the integrated circuits, a reliable and easily set up circuit is offered to the home constructor in kit form. A resistively tuned version is in widespread use as an industrial radio system and is noted for its extreme reliability under continuous, unattended operation. The circuit employed effectively contains 44 transistors and, although the quantity of discrete components is fairly high, the entire unit is built on a double-sided board measuring 133 imes 98.5mm (3.875 imes 5.25in). The Tuner can be run off a 12V d.c. power supply or a combination of 6 and 12V batteries.

All components are available BY POST ONLY from Dart Electronics at a special kit price of £9 19s 6d plus 5/- post and packaging (U.K. & N. Ireland) which includes selector switch and double-sided p.c. board ready drilled and tinned. The kit is complete with all necessary circuits and instructions.

Full assembly details, circuit diagram and parts list are also available separately from Dart Electronics at 2/6 per copy and an article appeared in the June issue of the WIRELESS WORLD magazine.

DART ELECTRONICS P.O. BOX No. 47, WITHAM, ESSEX

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5 SHAW LANE HALIFAX YORKS.

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REVREBERATION AMPLIPIER. Self-contained transistorised battery operated. An entirely different approach to sound reproduction. Normally sound reproduction. Normally sound reproduction from a single source has a flat, one-dimensional effect. With this unit proper sound delay through reverberation, tones are created with a truly thrid dimension for concert hail originality. Two controls adjust volume and reverberation. Simply plug microphone, guitar, etc. in and the output into your amplifier. Supplied in a beautiful walnut cabinet. 7½ × 3× 4½in. \$10.4.0. P.P. & Ins. 6/-



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Adjustable tone. Just statach your key. Drives
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JUST ARRIVED IN STOCK. Texas transistors.
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DIMMASWITCH





This is an attractive dimmer unit which fits in place of the normal wall light switch. The mounting plate is ivory to match modern fittings and the control knob is in bright chrome. An ON/OFF switch is incorporated to control up to 500 watts at mains voltages from 200-250 volts, 50 Hz.

These are normally sold at £4 19s. 6d.— our price is £3 5s. We also offer at £2 15s. a complete kit of parts with simple instructions enabling you to build this dimmer yourself.

The circuit uses the latest miniature RCA triac and new diac triggering device to give complete reliability. Radio interference suppression included.

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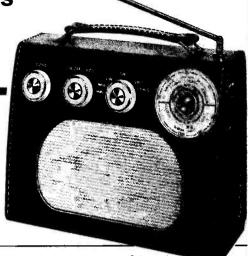
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NEW! roamer eight mk 1 WITH VARIABLE TONE CONTROL

7 Tunable Wavebands: Medium Wave 1, Medium Wave 2, Long Wave, S.W.1, S.W.2, S.W.3, and Trawler Band. Built in ferrite rod aerial for Medium and Long Waves. 5 section 22in chrome plated telescopic aerial for Short Waves can be angled and rotated for maximum performance. Push-pull output using 600Mw type transistors. Socket for car aerial. Tape record socket. Selectivity switch. Swritched earpiece socket complete with earpiece for private listening. 8 transistors plus 3 diodes. Pamous make 7 \times 4in speaker. Air spaced ganged tuning condenser. On/off switch volume control. Wave change switch and tuning control. Attractive case in rich chestnut shade with gold blocking. Size 9 \times 7 \times 4in approx. First grade components. Easy to follow instructions and diagrams make the Roamer Eight a pleasure to build. Parts price list and easy build plans 5/- (FREE with parts).

Total building costs £6.19.6



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7 FULLY TUNABLE WAVE
BANDS—M.W.1, M.W.2, L.W.,
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Band. Extra Medium waveband
provides easier tuning of Radio
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SIX WAVEBAND PORTABLE WITH 3in. SPEAKER

Attractive case in black with

Attractive case in black with red grille and cream knobs and dial with polished brass inserts. Size 9 × 5½ × 2½ in. approx. Tunable on Medium and Long Waves, 3 Short Waves and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 8 improved type transistors plus 3 diodes. All top grade components. Push-pull output. Ample power to drive a larger speaker. Parts price list and easy build plans 5/- (FREE with parts).

Total building costs

P. & P.

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Total building costs

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Attractive case with red speaker grille. Size 6½ × 4½in × 1½in. 7 stages—5 transistors and 2 diodes, ferrite rod aerial, tuning condenser, volume control, fine tone moving coil speaker also Personal Earplee with awitched socket for private listening. All first grade components. Easy build plans and parts price list 1/6 (FREE with parts).



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Attractive case with gilt fittings. Size 71 × 5; 1\frac{1}{2}\text{in.} Tunable on Medium and Long Waves, two Short Waves, Travier Band plus an extra M.W. band for easier tuning of Luxembourg, etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. All top grade components. 8 stages—6 transistors and 2 diodes including Micro-Alloy R.F. Transistors, etc. (Carrying strap 1/6 extra). Easy build plans and parts price list 2/- (FREE with parts).



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CAR LIGHT FLASHERS



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An excellent general purpose D/B oscilloscope.
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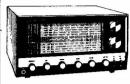
cost. Ranges: R. 10-11: meg 0 6 Ranges ±1%. L1 µH - 1 1 1 HENRYS 6 Ranges ±2%. TURNS RATIO 1:1/1000-1:11100. 6 Ranges ±1%. Bridge voltage at 1/000 cps. Operated from 9 volts. 100µA. Reler indication. Attractive 2 tone metace. Size 71 v 5 2 lin. \$20, T. & P. 5/-.

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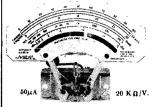


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Variable range
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If you want high fidelity in the highest class don't buy the 127 Tuner-Amplifier; it isn't meant for you. But if you want a good quality system that is a great deal better than the average radiogram, and your power requirements, as well as your budget, are of modest proportions, then this is meant for you.

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There are of course the usual facilities; pickup and tape inputs, tape recording outputs, bass and treble tone controls.

As we said at the outset, if you are after top-class hi-fi you don't want the 127, what you want is the Armstrong series 500 models.

For details and technical specifications of all models, plus list of stockists, post coupon or write, mentioning 12 PE69.

127 STEREO TUNER-AMPLIFIER £43.13.9 OPTIONAL CASE. As illustrated £3.17.0

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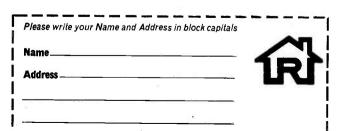
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VOL. 5 No. 12 December 1969

PRACTICAL LECTRONICS

THE NON-REGISTERED ENGINEER

HE news that a national register of qualified engineers and technicians is planned will certainly provoke argument amongst the professional engineering community. The idea will no doubt appeal to those eligible for inclusion in the register, that is those who have attained membership of one of the engineering institutions. On the other hand, practising engineers and technicians who do not possess the appropriate qualifications may fear their professional prospects could be harmed by the existence of such a register. Indeed, they may suspect this to be the first step towards the total exclusion of nonregistered persons from the more rewarding and responsible posts in industry, government departments, and other establishments.

It is understandable that members of the engineering institutions should endeavour to enhance their status and terms of employment, just as members of other professional bodies do. But concern must be expressed about the possible harm this could also cause. With regard to electronics specifically, if this scheme is carried out to the detriment of non-member engineers and technicians, the loss will not be the latter's alone, but the electronic industry as a whole would suffer.

Much normal commercial development and application work does not necessarily demand the higher academic qualifications. Given a sound basic knowledge of electronic principles and circuit practice, the most important and desirable asset, in many instances, would seem to be an imaginative mind. Some engineers and technicians have an innate ability to invent and develop ways and means for exploiting electronic devices and circuits. Surely these are the kind of people industry should be looking for, without too much concern about qualification

The expansion of electronics is not entirely a selfgenerating process, as may be innocently believed by some. New ideas must, constantly, be found to widen further the infiltration of this branch of technology into everyday activities. Microcircuits provide a topical illustration. These devices are a key factor in future expansion of the industry; however, their economic viability depends upon large scale production and this can only be maintained if a large user demand exists.

The national register sounds fine in its way, but it is impossible to detect a potential inventor or innovator by examination alone. Somehow we must guard against any academic barrier denying us the fruits of ingenious minds. just because they have not been formally examined and attested.

F. E. Bennett-Editor

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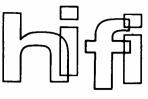
Our January issue will be published on Monday, December 15

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By M. J. Gay Chief Circuit Engineer (Linear), Plessey Microelectronics

HIS, the last article in the series describing the use of the Plessey SL402 and SL403 integrated circuit audio amplifiers, will describe a high fidelity stereo system using SL403's and a pre-amplifier suitable for feeding the system from magnetic, crystal, tape or radio inputs.

BASIC SYSTEM

The essential feature of the system is that a three speaker set-up (bass, middle, treble) with one SL403 feeding each speaker is used (Fig. 1). The part of the frequency spectrum fed to each speaker is selected by an active filter formed around the pre-amplifier section of the corresponding SL403. Potentiometers between the pre-amplifiers and main amplifiers allow differences in the sensitivities of the speakers to be corrected for.

This system has a number of advantages over the conventional arrangement in which the speakers are fed from a single amplifier via passive cross-over filters and attenuators. These are:

- (a) All speakers are always voltage fed.
- (b) The frequency spectrum is split before passing through the power amplifiers, so intermodulation distortion is reduced.

- (c) The cross-over frequencies and filter characteristics may be freely and independently chosen; the system is free from spurious electrical resonances.
- (d) No inductors are required.

ACTIVE FILTER DESIGN

The part of the frequency spectrum to be handled by each amplifier is selected by its pre-amplifier section connected as an active filter. Thus we have one pre-amplifier acting as a low-pass filter for the bass range amplifier, one acting as a band-pass filter for the midrange amplifier and one acting as a high-pass filter for the treble range amplifier. The active filter design is of the basic two integrator type, the particular arrangement being commonly attributed to Rauch. It generates a second order filter characteristic giving a cut-off rate of 12dB per octave.

The low-pass design is shown in Fig. 2a and Fig. 2b shows the high-pass design. The responses are characterised by the equations given. By suitable choice of the passive components we may produce responses corresponding to any of the standard forms, e.g. Butterworth, Bessel, Chebyshev, Gaussian. Of these Cheby-

SPECIFICATION ...

Output power: 3 watts r.m.s. per channel into 15 ohm loads.

Frequency response: 13Hz to 100kHz ± 3dB.

Total harmonic distortion—at full output: 0.3% at lkHz.

Integrated noise level: 90dB below full output.

Tone control characteristics Treble: ± 15dB at 15kHz.

Bass: ± 18dB at 20Hz.

Sensitivity

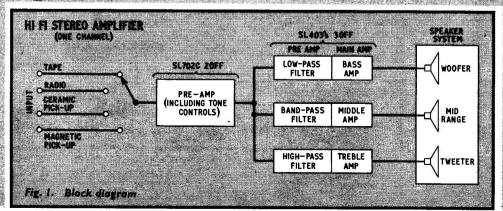
Radio: 35mV r.m.s.

Ceramic p.u.: 400mV r.m.s.

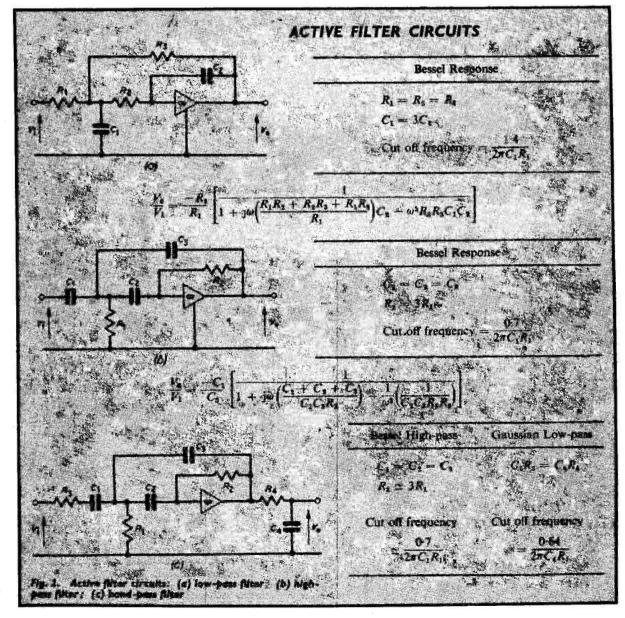
Magnetic p.u. and tape: 2.5mV r.m.s, at 1kHz.

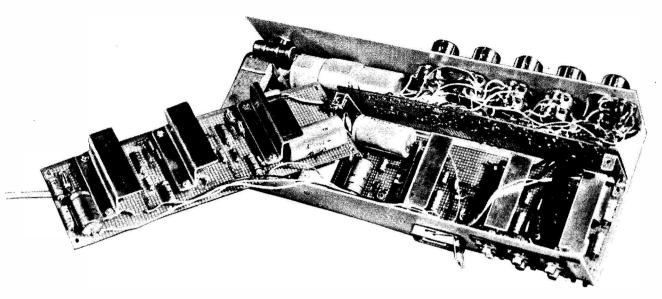
Crosstalk: -40dB at 1kHz

Speaker system: two three-channel speakers having individual 15 ohm impedance low, middle and high frequency units.



amplifer





General view of the hi fi stereo amplifier with one board removed to show layout and construction

shev gives the sharpest cut-off but will ring badly on transients; Gaussian will not ring or overshoot on transients but gives a rather slow initial roll-off; Butterworth and Bessel are in between.

Bessel response was in fact selected as about the best compromise giving reasonably sharp cut-off with negligible overshoot on transients. The second order Bessel polynomials are of the form

$$1/(1 + \sqrt{3j\omega t} - \omega t^2)$$
, low pass with cut-off at $\omega t = 0.8$

$$\omega t = 0.8$$

$$1/(1 + \frac{\sqrt{3}}{j\omega t} - \frac{1}{\omega^2 t^2}), \text{ high pass with cut-off at}$$

$$\omega t = 1.25$$

and these forms are produced with the component ratios tabulated in Fig. 2. The component values are not too critical; it suffices to use low tolerance resistors (preferably \pm 2 per cent, but \pm 5 per cent will suffice) and \pm 10 per cent capacitors.

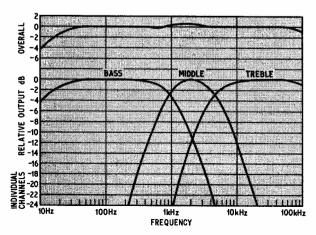


Fig. 3. Frequency responses of the hi fi stereo amplifier—individual and overall

The mid-range filter being band-pass has a rather more difficult task to perform. It is shown in Fig. 2c and consists of a second order Bessel high-pass section as in Fig. 2b, followed by a simple RC low-pass section giving 6dB per octave roll-off at the top end of the pass band and preceded by a series resistor R3, which generates a further 6dB per octave roll-off at the top end by virtue of the input impedance of the basic high-pass section being reduced to C1 at high frequencies. The addition of R3 necessitates slight modifications to the other resistor values to maintain the desired high-pass characteristic.

A set of response curves of the three filter sections and the resultant overall response are shown in Fig. 3. It will be seen that the high frequency cut-off rate of the mid-range filter is initially less sharp than the other cut-off rates. This is because it is generated differently as outlined above; in fact this particular characteristic is second order Gaussian. The slower cut-off rate is acceptable here as it is not too important to remove the treble from the mid-range speaker.

Table I. ACTIVE FILTER COMPONENT VALUES FOR VARIOUS CROSS-OVER FREQUENCIES

Lower cros	s-over	Bass c	hannel	Middle	channel
		RI	СІ	RI	CI
250Hz 400Hz 600Hz 950Hz		56kΩ 33kΩ	IOnF IOnF IOnF IOnF	I8kΩ	10nF 10nF * 10nF * 10nF
Upper cross-over		Midd			eble eble
	R3	R4	C4	RI	CI
3kHz 5kHz	3·3kΩ -2·2kΩ				l ·5nF l ·5nF

NOTE: where resistor and capacitor ratios of 3: I are required take nearest standard values.

* Reduced to correct for presence of R3.

CROSS-OVER FREQUENCIES

The cross-over frequencies shown in Fig. 3, 950Hz and 5kHz, are those recommended for a Goodman's three speaker system consisting of Audiom 61, Midax and Trebax. The frequencies can readily be set virtually anywhere in the audio range by scaling the resistor and/or capacitor values in the filters. The cut-off frequencies (-3dB) are given in Fig. 2 and Table 1 gives a list of component values for some typical choices. Note that for smooth cross-over the cut-off frequency of the bass filter must coincide with the lower cut-off frequency of the mid-range filter and the upper cut-off frequency of the mid-range filter must coincide with the cut-off frequency of the treble filter.

COMPLETE DESIGN—POWER AMPLIFIER

The complete circuit for the three amplifiers of a single channel is shown in Fig. 4; this has the cross-over characteristics shown in Fig. 3. As always the pre-

amplifier must provide the main amplifier bias. The filter arrangement provides 100 per cent d.c. shunt feedback around the pre-amplifier in all cases, so that its output and input quiescent voltages are equal and provide the correct temperature compensated bias voltage as detailed in the first article (October issue).

The bias voltage is applied to the main amplifier via the pre-set potentiometers VR6, VR8 and VR10 (Fig. 4) which allow the gain of each amplifier to be adjusted to balance out differences in the sensitivities of the loudspeakers. Bias adjustment is by means of pre-set potentiometers VR5, VR7 and VR9 which are set so that the quiescent output voltages of the main amplifier are at half supply potential.

The main amplifier sections are connected in the usual manner except that the values of speaker coupling capacitors, bootstrap capacitors and compensation components have been altered where appropriate, in accordance with the frequency range to be handled

POWER AMPLIFIER (one channel only)

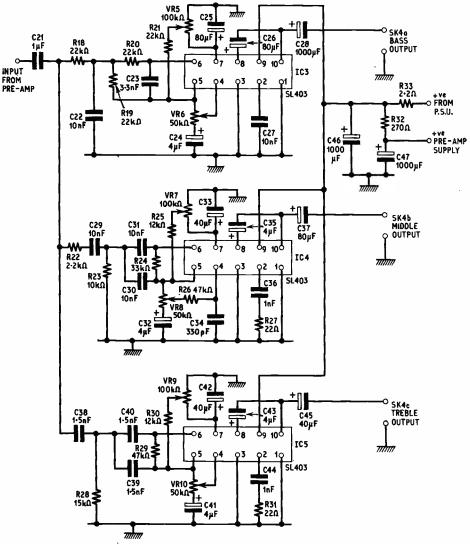


Fig. 4. Circuit diagram of one channel of the hi fi stereo power amplifier; not including the pre-amplifier

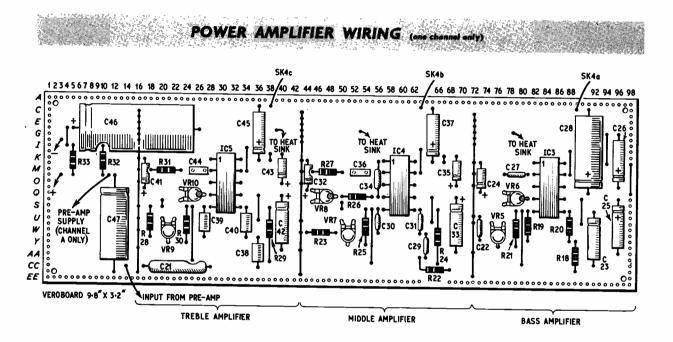
(one should not use a 1,000µF coupling capacitor to the treble speaker for example).

Note that although all amplifiers have been provided with level and bias adjustment potentiometers, some of these are not really necessary in practice. Commonly, middle and treble speakers are more efficient than bass units so that the bass amplifier level adjustment potentiometer VR6 and the blocking capacitor C24 could be dispensed with. The treble range output is much smaller than the bass and middle range outputs, so the treble range amplifier need not be provided with bias adjustment to obtain maximum possible output. Thus VR9 and R30 could be dispensed with.

CONSTRUCTION OF POWER AMPLIFIER

A Veroboard layout for a single channel power amplifier is shown in Fig. 5. In this design 0-1in matrix Veroboard was used to allow a more compact layout. A number of copper strips were tinned and connected in parallel to provide a low impedance earth line.

When using 0·lin matrix Veroboard, great care must be taken to avoid short circuiting adjacent conductors. Finished boards should be very carefully inspected; it is a good idea to run a small screwdriver blade along the spaces between conductors to ensure that no bridges are present.



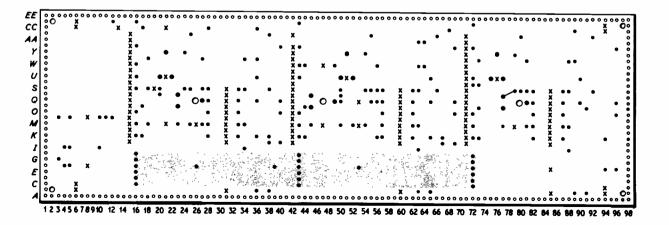
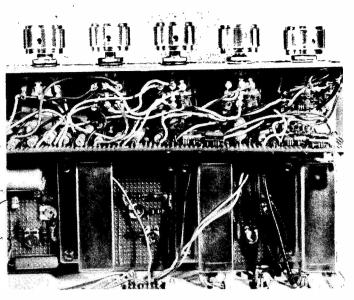


Fig. 5. Component layout and wiring diagram of one channel of the power amplifier. Conductors within the tinted area to be tinned for earth line



Part of one complete main amplifier board, with heat sinks attached, mounted in the chassis

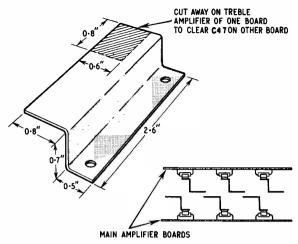


Fig. 6. Showing constructional details of the heat sinks for the six SL403's used in the main amplifiers and the arrangement of the amplifier boards

POWER AMPLIFIER PERFORMANCE

Because most multiple speaker systems are based on 15 ohm units, the amplifier performance is specified into that impedance. The amplifier can of course be operated quite satisfactorily into 7.5 ohm speakers (though the speaker coupling and bootstrap capacitors on the bass channel should be doubled to maintain the same 1.f. response). The only performance difference with 7.5 ohm speakers will be a rise in maximum output power to 3 watts maximum into each speaker and a

COMPONENTS...

			MAII	1 AMF	PLIFIER		
	All	components	except R32 an	d C47	must be	e duplicated for channel B	
Resistors					C34	330pF polystyrene	
RI8	22k Ω	± 5%h.s.			C35	4μF elect. I6V	
	22kΩ	± 5%h.s.			C36	InF ceramic	
	22kΩ	± 5%h.s.			C37	80μF_elect. 16V	
	22kΩ	±10%			C38	I-5nF polystyrene	
	2·2kΩ	± 5% h s			C39	1-5nF polystyrene	
	10kΩ	± 5% h s			C40	I-5nF polystyrene	
	33kΩ	± 5%h.s. ± 5%h.s. ± 5%h.s.			C41	4μ F elect. 16V	
	12kΩ	±10%			C42	40μF elect. 16V	
	47kΩ	$\pm 5\%$ h.s.			C43	4μF elect. I6V	
	22Ω	±10%			C44	InF ceramic	
R28	I5kΩ	\pm 5%h.s.			C45	40μF elect. 16V	
	47kΩ	± 5%h.s.			C46	$1,000 \mu F$ elect. 25V	
R30	12kΩ	±10%			C47	1,000μF elect. 16V	
R3I	22Ω	±10%					
R32	270Ω	±10%			Potenti	ometers	
R33	2.2Ω	±10%			VR5	$100k\Omega$ skeleton preset	
1133		⊥ • ✓ /0			VR6		
Capacitor	re				VR7		
-					VR8		
C2I	IμF polye				VR9		
	10nF poly				VR10	50k Ω skeleton preset	
C23	3·3nF pol		*			•	
C24	4μF elect				Integrat	ted circuits	
	80μF elec				_	and 5 SL403 Plessey (3 off)	
	80μF elec			· ·	100, .	and 9 02.02	
C27	IOnF poly				Miscella	aneous	
		elect. I6V					
C29	10nF pol			SK4 12 pole sub miniature plug and socket (Radio-			
C30	IOnF pol				spares	oard 0·lin matrix 9·8in×3·2in	
C31	10nF pol				verou	e.g. aluminium 2.6in×2in (3 off for heat sinks)	
C32	4μF elect	:. 16V :t. 16V			10 S.W	fixings	

slight rise in distortion (to around 0.5 per cent).

The frequency response of the three amplifiers and the overall frequency response is shown in Fig. 3, while Fig. 7 shows distortion at the onset of clipping over the audio frequency range. The rise at l.f. is due to thermal feedback in the integrated circuit. Distortion is once again predominantly second harmonic and falls as power is reduced in a similar manner to the curves given in previous articles; since the amplifier is biased in class AB, cross-over distortion does not occur. Fig. 8 shows the output noise voltage $(\mu V/\sqrt{Hz})$ as a function of frequency over the audio band. This is measured

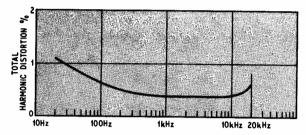


Fig. 7. Distortion curve for the stereo amplifier at full output

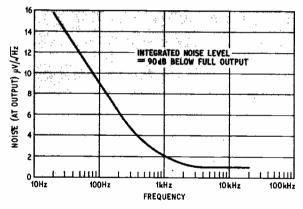
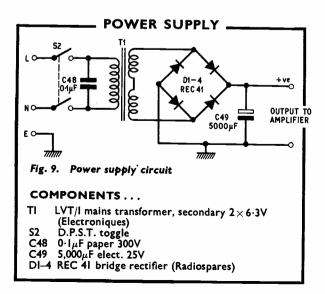


Fig. 8. Noise output curve for the stereo amplifler



with short circuit input and at the output of the appropriate amplifier for each frequency. The integrated noise level over the band is 90dB below full output; the perceived noise level will be about 5dB lower since the l.f. components which are significant in the integrated figure are much less audible.

OUTPUT POWER

The output power available is 2 watts r.m.s. (continuous sine wave) from each amplifier into a 15 ohm load on an 18 volt supply or 3W into a 7.5 ohm load. The effective r.m.s. output power on music depends on how the music frequency spectrum, during fortissimo passages, splits between the ranges covered by each amplifier. Some simple tests indicate that with the cross-over frequencies at 950Hz and 5kHz the effective power rating for music is around 1.5 times the individual amplifier rating. Thus the effective music power rating is 3W r.m.s. into 15 ohm speakers and 4.5W r.m.s. into 7.5 ohm speakers. With a 400Hz cross-over frequency the effective power rating would be about twice the individual amplifier rating.

These powers may seem rather low by the standards of hi fi amplifiers but it must be remembered that 30W sounds only twice as loud as 3W. Using the types of speakers envisaged for this system, 3W r.m.s. music power per (frequency) channel is more than adequate.

POWER SUPPLY ARRANGEMENTS

The main amplifiers are fed from a transformer and bridge rectifier with a 5,000µF reservoir capacitor, see Fig. 9. This produces a hum level of -70dB which is normally considered adequate. With a simple power supply such as this, however, the supply ripple is a sawtooth wave-form containing significant components at 300Hz, 500Hz, etc. which are much more audible than the fundamental 100Hz ripple. For this reason additional smoothing is incorporated by including the 1,000µF capacitors and 2·2 ohm supply line resistors on each power amplifier. This gives 12dB attenuation of the 300Hz component, 17dB attenuation of 500Hz, etc.

PRE-AMPLIFIER SUPPLY

The pre-amplifier supply is taken via an additional decoupling network (R32 and C47 in Fig. 4) from one of the power amplifiers. If power supply for external equipment is required, it can be taken from the other power amplifier via a similar decoupling network.

The amplifier described offers a novel approach to high fidelity reproduction. The emphasis of the design is on establishing ideal feed conditions for all speakers and on ensuring that they are fed with a properly selected section of the frequency spectrum. Incidental advantages of the system are reduction in intermodulation distortion and improved transient performance, due to the fact that low and high frequency components are not handled by the same power amplifier. Particular attention has been paid to obtaining low hum and noise levels.

Next month: Pre-amplifier and final construction details

Note. In Fig. 3 page 813 (last month) VR1 should have been $2M\Omega$ and C11, 2,200pF. The distortion curves on pages 812 and 816 must be transposed.





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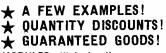
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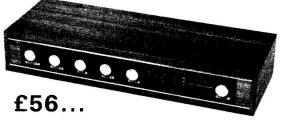
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MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

EQUIPMENT CASE

Finding a means of obtaining an attractively finished case for a piece of equipment can become a problem to the amateur constructor, since there are several proprietary cases now on the market.

The Contil Mod-2 case from West Hyde Developments is available in varying sizes each with a p.v.c. coating. It comes in kit form and is easily assembled with a special crosshead screwdriver, included with each case kit.

The finish makes the case look equally attractive in the living room or laboratory. It is quite easy to add your own lettering to the front panel. The cases would seem to be suitable

The cases would seem to be suitable for housing any of the P.E. i.c. amplifiers described last month and in this issue.

The prices of the Contil Mod-2 cases vary from 29s 6d to 129s 6d, postage extra.

Sizes and prices of the cases are contained in a short form catalogue available from West Hyde Developments Ltd., 30 High Street, Northwood, Middlesex.

TEST EQUIPMENT

A regulated d.c. power supply, designed for operating or testing transistor receivers, amplifiers and other low voltage equipment is the latest product from Nombrex (1969) Ltd., Exmouth, Devon.

Known as the Model-22 Mk11 it provides a variable voltage from zero to 15V at currents of up to 500mA. Any short circuit or overload condition (approximately >600mA) is indicated instantly by a red warning light on the front panel.

The required output voltage is selected by a control on the front panel and both voltage and current can be monitored on separate scales of the output meter. The maximum loading for the power supply unit is 12 watts. Regulation accuracy from zero to full load is claimed at better than 2 per cent, and ripple is less than 5 mV at maximum current.

The Model-22 d.c. power supply is mains operated and is priced at £14 18s 6d.

Another item of importance for the test bench is the oscilloscope and although this is a rather expensive item it should be considered a must for any amateur experimenter.

A fairly inexpensive oscilloscope is the EA 0699-1 from Mitre Electronic Products, 22 Powis Terrace, London, W.11. Intended for use in schools, as a monitor, or for use in the service repair laboratory, it costs £24 10s.

It features a 2½ in diameter tube and has a Y bandwidth from d.c. to 100kHz. The Y sensitivity at maximum gain with full Y shift is claimed to be less than 100mV/cm. The timebase covers a range of approximately 10µs/cm to 100ms/cm.

SOLDERING IRON

A new miniature 12V 12W soldering iron, type L20, has just been

L20
Miniature 12V
12 watt soldering
iron from Adcola Products
introduced by Adcola Products Ltd

introduced by Adcola Products Ltd., price 28s 6d. The iron is ideal for printed circuit work and being 12V operated is a useful addition to the car tool box for carrying out small or temporary electrical repairs on printed circuits.

The iron can also be powered from the mains using a transformer which will become available as an extra.

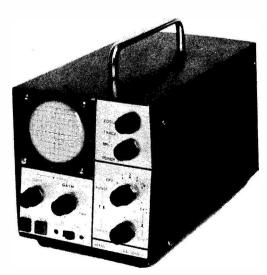
SMALLEST RADIO

The introduction of the world's smallest radio in production is now claimed by Lasky's Radio Ltd. Called the Astrad Orion it is made in Russia and is a six transistor two-waveband receiver measuring only $1\frac{1}{16}$ in \times $\frac{1}{16}$ in.

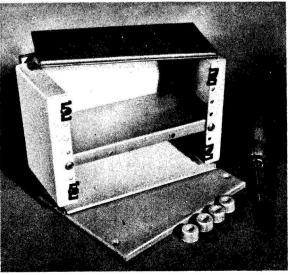
waveband received measuring only $1\frac{11}{18}$ in $\times 1\frac{1}{18}$ in $\times \frac{1}{18}$ in.

The set has a built-in ferrite rod aerial and is fully tunable over the medium and long waves. The signal output is heard through a miniature earphone and the set is powered by either a rechargeable nickel cadmium cell or a hearing aid mercury cell.

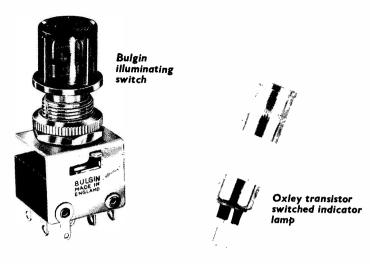
Complete with earpiece and battery the Astrad Orion costs 39s 6d.



EA 0699-I Oscilloscope manufactured by Mitre Electronic Products



West Hyde Developments Contil Mod-2 case kit



SWITCHES AND LAMPS

The practice of illuminating controls seems to be on the increase each month, whether this is due to an increase in general short-sightedness, or the ever increasing sophistication and greater demand expected of the electronics industry, is a matter of conjecture.

But following this trend is the latest range of illuminated switches from A. F. Bulgin & Co. Ltd., Bye-Pass Road, Barking, Essex. The switch unit has a normally biased push action which can be locked in the depressed position by twisting the lens cap.

Two versions are available with either single-pole changeover or twin single-pole changeover switches. The maximum switch contact ratings are 8A 250V a.c.

The lampholder accepts l.e.s. lamps up to 28V and the lens caps are available in five different colours. The lamp contacts are isolated from the switch.

A new product from Oxley is a range of transistor switched indicator lamps. The lamp contains its own driver stage enabling the bulb to be controlled from a low-current signal and is available in two versions, normally on and normally off.

The lamp holders have been specifically designed to indicate the state of logic or counting circuitry, but no doubt many ingenious readers will find other applications when they finally appear on the retail market.

CINE/TAPE SYNC

Many of our photographically minded readers may be interested in the new Carol Model CS/2 pulse system of tape/film synchronisation. This new version is very similar to the original one and incorporates all of the more proven facilities of the previous model, as well as some new features.

The tape/film synchroniser is housed in a two-tone metal case with controls and a frames per second meter all mounted on the front panel.

The recommended selling price, including tax, is £46 13s 6d and is designed so that most projectors can stand on top of the case, making a neat compact set-up.

The main feature of the CS/2 model is the inclusion of a motor speed control circuit, which eliminates the need for heavy ballast resistors and gives more precise sync control.

The Carol Cinesound Model CS/2 is obtainable at most photographic shops or direct from Contronics Ltd., Deepcut, Camberley, Surrey.

LITERATURE

Some 5,800 semiconductor devices, including integrated circuits, f.e.t.'s and thyristors are given in the new semiconductor price list now being issued by W.E.L. Components Ltd., 5 Loverock Road, Reading, Berks.

Items listed cover devices manu-

factured by Texas, A.E.I. Semiconductors, Ferranti and Sprague; a large number of CV types are also listed. The semiconductor price list is available free of charge, but all applications for copies must be made on company letterhead paper.

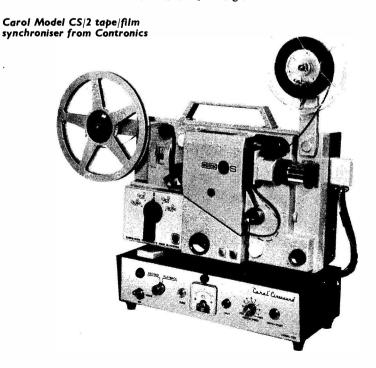
Also recommended is the added service of Mainline Electronics who now provide a catalogue of semiconductor devices which they can supply from S.G.S., R.C.A., International Rectifier, Emihus, Semitron, and Plessey. Additions to their components of all kinds are the i.c. amplifiers 12A, 25A, and 70A at £7, £8 5s, and £10 10s respectively. These are R.C.A. designs that are available in kit form. Details are given in 4s catalogue by post from Mainline Electronics Ltd., Thames Avenue, Windsor, Berkshire.

Two new editions of component catalogues are now available from LST Electronic Components Ltd., 7 Coptfold Road, Brentwood, Essex, and Adcola Products Ltd., Adcola House, Garden Road, London, S.W.4.

The LST catalogue lists many new semiconductor devices, including a special pnpn unijunction, type D13T, which is claimed to be programmable. Also listed in the catalogue are complete power supply and audio amplifier kits.

The Adcola catalogue contains details of their complete range of soldering instruments from replacement bits to de-soldering irons. The new de-soldering instrument styled on the lines of their soldering irons is also shown.

Both of the above mentioned catalogues are available free of charge.



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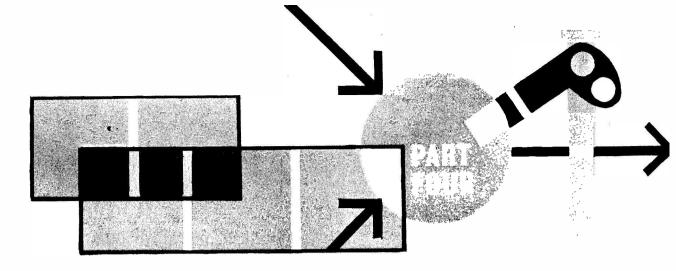
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MODEL RAILWAY LOGIG SYSTEMS By P. GOODES

AUTOMATIC MARSHALLING YARD AND TURNTABLE

Last month's article gave some suggestions, based on the author's layout, for automatic control of a marshalling yard. The gates used on the master control panel (G3, G4, G5, G6, G7) and those on the store (G2, G4, G6, G8, G10) require buffer amplifiers on the output. The gate and buffer are shown in Fig. 4.1.

For added security, gates G1 to G5 on the track switch decoder should each have an input from bistable

BS2B on the master control.

A greater degree of flexibility can be provided if a loco unit can be made to turn round or change track. This is where an automatic turntable can come in useful. The remainder of this last part of the series will describe the author's home-made unit.

TURNTABLE

The turntable to be described was built entirely from scratch, since those obtainable commercially were unable to give the required facilities. The requirements were as follows:

To allow a train on to the turntable at any one outlet and to enable it to be removed either forwards or backwards from any preselected one of five outlets.

BISTABLE CONTROL

Obviously a bistable is required to do this, giving a sharp control so that it is either stationary or rotating. Rotation is started by a push button on the control panel. This sets the bistable BS1 in Fig. 4.2 with a 1 at its B output and a 0 at its A output. Since the control amplifier is an inverting device, the A output 0 is fed to it, starting the turntable rotating.

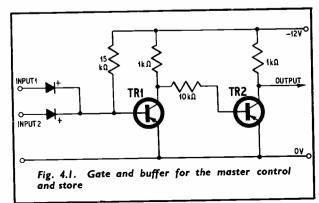
To stop the turntable at the required outlet, a negative voltage "1" is taken from the output of monostable MS1 and is applied to a control wiping contact mounted on the underside of the turntable. On the fixed base, five contacts are mounted and as the turn-

table rotates a 1 pulse is fed through each of these five contacts in turn. A rotary switch S3, mounted on the control panel, is used to select the particular outlet and when the 1 pulse reaches the corresponding fixed contact, it is fed through to switch off the bistable.

Monostable MS1 is used to overcome such conditions as follows: if, for example, the turntable starts at position 2, it is impossible to bring the engine out in reverse at, say, outlet 5 without the turntable stopping at outlet 5 and then needing to be restarted to take it through another 180 degrees.

When switch S1 is closed the 1 pulse from BS1B output triggers the monostable which has a time constant of approximately the time taken for the turntable to complete a quarter of a revolution. Thus the output becomes 0 for this period of time and the bistable cannot be triggered off until the monostable reverts to its quiescent state.

The speed of the turntable was made adjustable, but optimum speed was found to be about 1½ rev/minute.



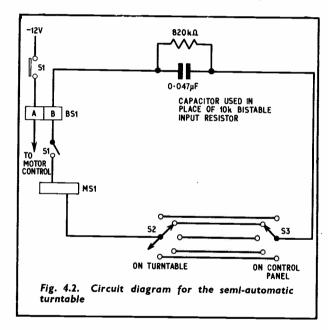
TRIP SWITCH

As an alternative to the start button a trip switch may be mounted on the turntable so that the engine starts the turntable rotating. In this case a relay buffer and relay should be used instead of the control amplifier and should be operated from the B output of BS1. One pair of contacts is used to switch the turntable motor on and another two pairs to cut off the supply to the engine.

The circuitry is mounted on a printed circuit board, the layout for which is shown in Fig. 4.3. The board shown caters only for the bistable and monostable and it is left to the reader to build up a relay buffer or control amplifier according to which ever he requires.

WIPER SWITCH MECHANISM

The moving part of the turntable consists of a circle of hardboard 12in in diameter. On to the underside of this is fixed a circle of ordinary railway track (Fig. 4.3). The central wiping contacts are also fitted to the underside of this piece of hardboard and may be made

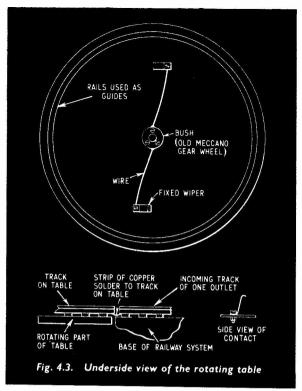


from old relay contacts or similar springy material and bent to shape. This contact is connected electrically to a Meccano wheel which is screwed on to the board and acts as a bush.

The base carries four cradles set at 90 degree intervals. Slots are cut in the tops of these cradles to carry truck axles and wheels and the whole so set that the rails of the rotating part run on these wheels. At the centre of the base another Meccano wheel is fitted and a short piece of rod is secured through this wheel. Using this as the axis of rotation, the rotating table should now run smoothly on the base. At this stage the piece of straight railway track, which carried the engine to be turned, may be fitted and this should be a little over 12in in length.

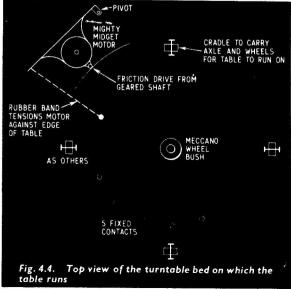
The five fixed contacts should now be fitted to the base so that contact is made between the wiper and each fixed contact as the track on the table is opposite the associated incoming track.

The motor may be fitted now (Fig. 4.4). The motor used was a "Mighty Midget" motor with gears.



This is screwed to an aluminium base which in turn is hinged to the base. A rubber band connected between the motor and the base ensures that the drive shaft is tensioned against the edge of the rotating table. The electronics may now be incorporated and a dummy run attempted. When the turntable stops at each point the incoming tracks should be aligned to the track on the rotating table and secured.

Finally, a piece of spring strip should be soldered to each rail of the turntable track so that connection is made to the track at the outlets selected, thereby ensuring that the train supply gets through to the turntable track.



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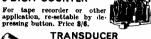
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a stack or heap subject to spontaneous com
bustion or if liquid is being heated by gas or

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In long : approximately lin dismeter. Will make and break up to ; amp up to 300 volts. Price \$\frac{1}{2}\text{ e} = \text{ dozen.}\$

Standard; 2m long × ; in diameter. This will break currents of up to 1 amp, voltages up to 250 volts. Price \$\frac{1}{2}\text{ e} = \text{ dozen.}\$

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FLUORESCENT CONTROL KITS

FLUORESCENT CONTROL KITS
Each kit comprises seven items—Choke, 2 tube
ends, starter, starter holder and 2 tube clips,
with wiring instructions. Suitable for normal
fluorescent tubes or the new Crolux' tubes for
flab tanks and indoor news. Chokes are supersilent mostly resin flind.
196. Kit 8—30-40 v. 19/8. Kit 1—60 flips.
Kit 8—35 w. 19/8. Kit MF1 for 61 m.
196. Kit 8—36 w. 19/8. Kit MF1 for 62 m.
A and 12 in miniature tubes, 19/8. Poor 63 m.
A kit 8—46 v. 19/8. Kit MF1 kit hen 4/8 on 8 m.
A and 8 4/8 for one or two kits then 4/8 on 8 m.
Kit ben 3/6 for each kit ordered. Kit MF1 3/6
on first kit then 3/6 for each kit ordered. Kit MF1 3/6
on first kit then 3/6 on each two kits ordered. first kit then 3/6 on each two kits or

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JUPITER PROBE

The fly-by probes scheduled for launching to study the Jupiter environment in 1973 and 1974, are making demands on the time of astronomers for planning the trajectories. Accurate observations are required of the positions of the Galilian satellites Io, Europa, Ganymede and Callisto.

There are a number of difficulties here, the principal one being the uncertainty of predicting the orbits of these bodies. The errors at present are high and amount to some thousands of kilometres. Amateur observers have been able to establish this with their much less sophisticated

apparatus than that of the professional observatories.

The general studies to be made of the Jovian environment includes the study of particles, magnetic and electric fields, gravitational fields, effect of the solar wind and the atmospheric constituents of the planet!

One of the instruments used will be an imaging photo-electric polarimeter which will observe the Galilean satellites and Jupiter itself. Unfortunately, the error noted above is certainly larger than the field of view

of the imaging instrument.

Locking on to the satellites could be impossible unless the astrometric data is improved and NASA is therefore urgently seeking positional data of the four Galilean satellites, and if possible also the position of Amalthea (satellite V).

If the position is not improved, particularly for the next two apparitions, NASA made be forced to set up conventional observatories to deal with this problem.

HONEYSUCKLE DISH

The rapid growth of Australia's contribution to the U.S.A. space programmes may have a spectacular reward. As a result of the successful Apollo 11 mission NASA have indicated that Honeysuckle Creek tracking centre near Canberra will be up-graded by the addition of a 200ft dish aerial.

The existing 85ft aerial was able to receive the telemetry quite satisfactorily but its ability to deal with the television signals was marginal. It was as a result of this situation that the Commonwealth Scientific and Industrial Research Organisation made the Parkes 210ft dish available during the critical moon transmissions.

The geographical position of Australia in relation to Cape Kennedy has been the reason for the close co-operation between the personnel and their contact with advanced space techniques. These facilities in the southern hemisphere are essential to the future projects of space exploration and the moon based stations of the future.

WATCHING THE BIRTH OF **STARS**

The dark clouds in the Orion Nebula look like "protostars" con-densing and the Green Bank radio astronomers have found some very compact clouds in regions of star formation.

These clouds of ionised hydrogen emit radio waves at 2cm. The emission at 18cm of the hydroxyl radical (OH) is believed to come from protostars and there is also the possibility that the OH radical also emits at 2cm. Some nebulae also show that they contain concentrations of

ionised hydrogen.

In 1947 Bok, working with the Mount Palomar telescope, noticed the dark patches against bright emission nebulae and suggested that they were clouds of matter. Since then Dr M. Penston has studied several of the Bok globules which are seen against the bright Orion nebula, three of these are like spheres of gas, and they appear to have cooled down well below the usual temperature in interstellar space. Their mass is of the order of one solar mass and this supports the idea that they are stars in formation.

SATELLITE AERIAL WITHOUT A DOME

On October 1 this year Raistang 2, a new large radio aerial for satellite communications, went into opera-tion. Raistang 1 went into service in 1964 and was 25 metres in diameter, housed in a radome of plastic kept inflated by internal excess pressure.

The theory was that by housing it in a protective cover the construction could be both lighter to erect and easier to maintain. Also working conditions for staff would be more amiable.

In practice however, a number of grave disadvantages appeared. When wet the radome causes a higher level in the noise component of the system and this leads to considerable damping of the signal in passing through the wet shell. Also the wet shell reflects earth radiation back to the aerial. With a rainfall of 1mm/h there is a rise of noise temperature of 3.5db and when the rainfall rises to 10mm/h the increase is as much as 7 Bels.

The second aerial, which was built without the radome, has a far more robust structure and provision is also made for differing weather conditions

according to location.

Some five thousand 150 watt radiators (infra red) are arranged in groups behind the reflector to take care of snow and ice. The rear of the dish aerial is totally enclosed so that the supporting struts of the aerial are shaded from the heat of the sun in order to reduce distortion.

An axially mounted horn feed enables both transmitter and receiver electronics to remain in position wherever the aerial is moved. diameter of this dish is 28 metres.

There are plans for two more aerials in this complex which is the measure of what is expected from the increase in communications traffic when Intelstat III programme gets under way.

The next major event to be handled by the present aerials will be the 1972

Munich Olympics.

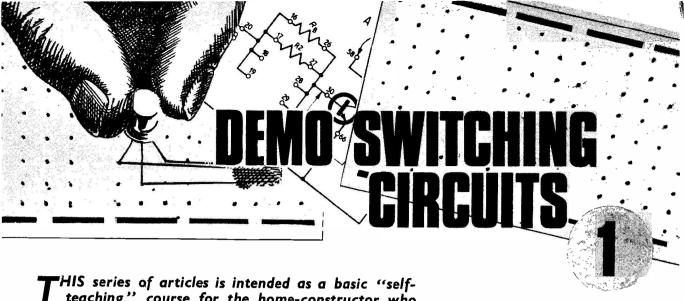
METEORS ON TAPE

A machine which will increase man's knowledge of the origin of meteors has been developed by Sheffield University and the Projects Division of Dunford Hadfields. The University team under Prof. Kaiser have installed an automatic digital recording system to process and analyse meteor echoes at the radio astronomy observatory at High Brad-

For some 12 years meteors have been observed at Bradfield using the technique of reflected pulses from ionised meteor trails. The new technique being developed by Prof. Kaiser's team will help to remove the laborious analysis work involved in the old method.

THE MOON AIDS THE **MOTORIST**

A new synthetic rubber which man used to make his first footprints on the moon may help the motorist. The material, a fluoro-elastomer can be used for seals, disc brake systems and other places where very high temperatures occur. Full return after deformation is possible up to 200 degrees centigrade.



THIS series of articles is intended as a basic "self-teaching" course for the home-constructor who wishes to design his own transistor switching circuits. Component values may be calculated from the simple theory given and it will be shown how the circuits may be assembled and tested.

Expensive test gear will not be required; neither will elaborate power supplies. Battery operation will be utilised throughout so that circuits may be tested without the need for setting up elaborate equipment.

By B. Pounder

A NYONE with a knowledge of little more than Ohm's law can easily acquire the facility of arriving at first-approximation circuit designs from which improvements can be made as experience develops. The designs given start with basic transistor operation and lead on to practical circuits.

BREADBOARD ASSEMBLY

One of the easiest methods of construction is the "breadboard" assembly technique based upon the use of component push-in boards such as S-Dec, μ -Dec and T-Dec. These are available from component suppliers and from M.L.I. for members of the teaching profession.

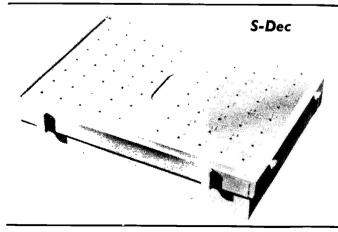
The use of these Decs enables a limited kit of components to be used many times over, and makes the task of changing components in an already assembled circuit simplicity itself. Because of this easy form of component assembly, a number of circuits can be built and tested very quickly. If a mistake is made in the connections, correction is straightforward without using a soldering iron.

There are three basic types of "Dec", S, μ , and T. Each contains rows of phosphor bronze contact strips mounted in a small box beneath a plastics panel. The panel contains rows of numbered holes above the contact strips through which component leads may be inserted into the contact strips. Contacts are electrically and mechanically sound. Once a lead has been set in a particular position and attitude, so it will remain unless pushed or bent into another.

The arrangement of sockets on the three types of Dec is shown in the photographs. Circuit layouts are similar to those used with Veroboard, except that no solder is required.

Of the three types of Dec, the S-Dec is the least expensive and the easiest to get components into and out of on account of the relatively wide pitch between socket rows. It is designed for long-lead transistors in TO1 or TO5 encapsulations and will only accept shortlead TO18 or plastics devices if these are used in conjunction with transistor sockets to which leads about 1.5in long have been pre-soldered.

The other two types are more expensive but much more versatile. They will accept both long- and short-lead transistors directly as well as the standard integrated circuit packages provided that they are purchased with the appropriate i.c. carriers. The small socket spacings on the μ - and T-Decs enables circuits of considerable complexity to be assembled as will be shown as this series develops.



If required, two or more of these "breadboards" can be fitted together by their dovetail slots and panel mounted components can be fitted to the associated metal brackets.

COMPONENTS

Before getting down to the actual circuits, a word or two about the components to be used is appropriate here.

Apart from the breadboard and some single stranded connecting wire, a stock of transistors, resistors and capacitors will be required for all the circuits to be discussed. In addition, one or two extras will be required for some circuits, for example, diodes, bulbs, a relay, and so on. Some of these may need wires attached to facilitate insertion in the breadboard holes.

The transistor stock need only consist of a few general purpose types, *npn* or *pnp*, silicon or germanium; few circuits will require both *npn* and *pnp* devices. If the transistors will stand currents of up to one ampere, they will be capable of working in all the circuits, but smaller types can be substituted in low current applications up to about 100mA.

The circuit layouts to be given will be based on the assumption that the transistors used have an e-b-c lead sequence. It should be noted that some readily available plastics devices have an e-c-b sequence. It will be a simple matter to modify the suggested layouts to accommodate devices of this type. Some specimen lead arrangements are shown in Fig. 1.1.

For resistors, it is advisable to have a few of all the 10 per cent values. This may not be as expensive as it seems and has the advantage that a component of approximately the same value as that calculated will always be available for use in a circuit.

Capacitor requirements will be modest. If a few components of about 100pF, $0\cdot1\mu F$, $10\mu F$ are available, most needs should be met.

TRANSISTOR CHARACTERISTICS

Fig. 1.2 shows the basic diagram of a one transistor operational test circuit with S-Dec hole numbers given at the appropriate junctions. This is converted to a practical layout in Fig. 1.3. This circuit is used to illustrate the function of a transistor under linear d.c. conditions.

Before using transistors as switches, it will be useful to have a look at those characteristics which illustrate the behaviour of a typical device under d.c. conditions and see how a set of these characteristics may be plotted

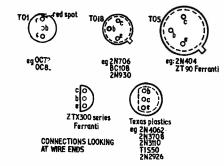


Fig. I.I. Lead arrangements for some commonly used types of transistors

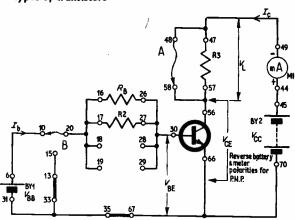


Fig. 1.2. A test circuit used to demonstrate the function of a transistor. S-Dec hole numbers are given at the component junctions

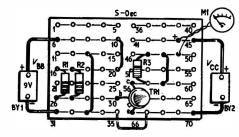
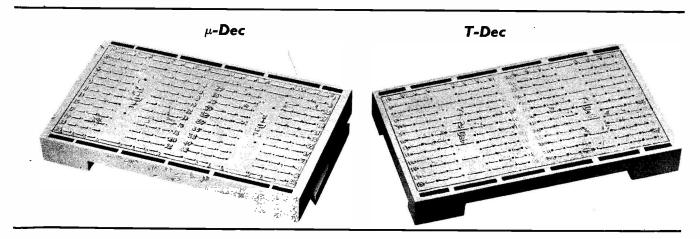


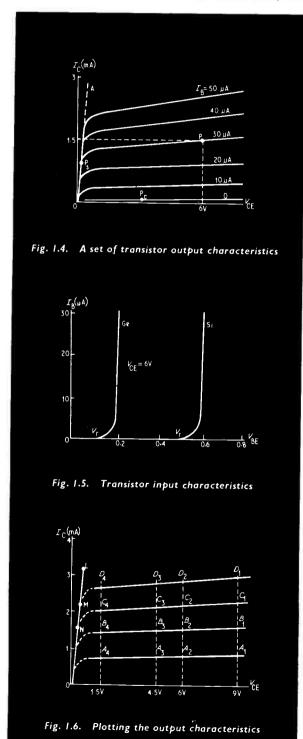
Fig. i.3. Practical arrangement of circuit given in Fig. 1.2



quickly to a degree of accuracy sufficient for many practical purposes.

Fig. 1.4 shows a set of output characteristics, that is, curves of collector current I_C against collector-emitter voltage V_{CE} , each plotted for a constant base current I_B .

A point P is shown on one of the curves, and for the particular transistor to which these curves refer, the



collector current and collector-emitter voltage are $1.5 \, \text{mA}$ and 6V respectively. Also, the base current is $30 \, \mu \text{A}$. The ratio of the collector current to the base current at this point is the d.c. current gain for a grounded emitter configuration, usually given one of the symbols β or h_{FE} .

Thus
$$\beta = h_{\rm FE} = \frac{I_{\rm C}}{I_{\rm B}} = \frac{1,500}{30} = 50$$

Roughly the same value would be obtained at other points on the other curves, except at values of $I_{\rm C}$ very much greater or very much less than that chosen.

Note that all the curves merge into a line OA. If the transistor is operated at a point such as P_S on this line, the transistor is said to be saturated; I_C and V_{CE} for this point could correspond to any one of the base current values of all the curves which pass through this point, i.e. to all base currents greater than $30\mu A$ in the example shown. Conversely, if the transistor is operated at a point such as P_C on the zero base current curve. it is said to be cut-off.

Two input characteristics are shown in Fig. 1.5. These are curves of base current $I_{\rm B}$ against forward bias base-emitter voltage $V_{\rm BE}$, drawn for a particular value of $V_{\rm CE}$. Curves drawn for other values of $V_{\rm CE}$ differ only slightly from one another.

The curves shown are typical for germanium and silicon transistors, and show an important difference between the two types, namely that the base current is approximately zero for forward bias voltages of less than about 0.1V for germanium and 0.4V for silicon. Further, the curves rise rapidly with increase in $V_{\rm BE}$ beyond about 0.2V for germanium and 0.6V for silicon.

When saturated, $V_{\rm BE}$ values are approximately 0.3V and 0.8V for germanium and silicon transistors respectively. These figures are worth remembering.

PLOTTING THE CHARACTERISTICS

A quick method of plotting a set of output characteristics is as follows.

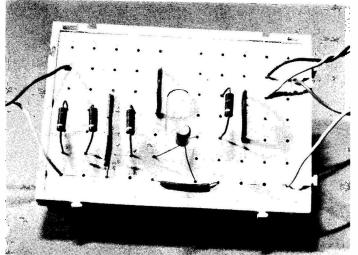
Connect up the circuit shown in Fig. 1.2 with R3 shorted by means of the link A. Use a 9V battery for $V_{\rm CC}$. Insert a 2 megohm resistor for $R_{\rm B}$ and connect the link B to contact 15. The collector current should be small, much less than 0·1mA for a germanium transistor and negligibly small for a silicon device.

Now connect link B to contact 10 and note I_C . This will probably be less than 1mA. Whatever the value of I_C , replace R_B by a resistor of value such that $I_C = 1$ mA (as near as possible). The base current corresponding to this collector current is calculated as follows.

From Fig. 1.2, it can be seen that the battery voltage $V_{\rm BB}$ is divided by the potential difference across $R_{\rm B}$ and that between the base and emitter terminals of the transistor. Thus the potential difference across $R_{\rm B} = V_{\rm BB} - V_{\rm BE}$. But since $V_{\rm BE}$ is much less than $V_{\rm BB}$, even if a silicon transistor is used, it can be neglected by comparison; the whole of the base circuit supply voltage $V_{\rm BB}$ can be considered to exist across $R_{\rm B}$.

Ohm's Law now tells us that the base current $I_{\rm B} \simeq V_{\rm BB}/R_{\rm B}$. Having calculated this current, and knowing $I_{\rm C}$ and $V_{\rm CE}$, mark in a point such as A_1 shown in Fig. 1.6.

Next shunt R_B with a resistor of the same value in order to double I_B . Read the new value of I_C and mark in point B_1 on Fig. 1.6: Next shunt R_B with two further resistors of the same value so that I_B is three times and then four times its initial value. Note the corresponding values of I_C and mark in points C_1 and D_1 .



Photograph of the arrangement shown in Fig. 1.3

The whole procedure is then repeated using batteries, for $V_{\rm CC}$ of 6V, 4.5V and 1.5V, and points A_2 , B_2 , C_2 , D_2 etc. marked in on Fig. 1.6. The small-slope sections of the characteristics can be drawn in as shown. The saturation part of the characteristic can now be found.

Replace the supply battery V_{CC} by one of 9V and remove the link A in order to place the collector load resistance R3 in circuit. A suitable value is 3.3 kilohms. Insert resistance $R_{\rm B}$ of gradually decreasing value until the collector current no longer rises. This occurs when the transistor saturates.

Calculate the voltage dropped along $R_{\rm C}$ at saturation using Ohm's Law, i.e. $V_L = I_C R_3$, where I_C is the saturation collector current $I_{C(sat)}$. The collectoremitter voltage at saturation is therefore $V_{CE(sat)} =$ $V_{\rm CC} - V_{\rm L}$. Mark in the point L corresponding to these values of $I_{C(sat)}$ and $V_{CE(sat)}$ on Fig. 1.6.

Repeat the whole procedure with $R_3 = 4.7$ and 5.6 kilohms, and obtain points such as M and N. Join points L, M and N by a smooth curve to complete the characteristics.

The whole procedure described above need take no longer than it does to read the instructions, once a little practice is obtained.

For the home experimenter who is interested in a quick check of a particular transistor, rather than a more complete knowledge of the characteristics as a set, all that is usually required is to check that I_C is approximately zero at $I_B = 0$, and then find a value of R_B for which I_C is about 1mA. The current gain is then obtained by dividing the indicated I_C by the calculated value of $I_{\rm B}$.

TRANSISTOR OPERATED AS A SWITCH

The circuit shown in Fig. 1.7 depicts a transistor amplifier with collector load resistance R_L. Part of the supply voltage V_{CC} is dropped across R_{L} , the remainder between the collector and emitter terminals Thus

$$V_{\rm CC} = V_{\rm L} + V_{\rm CE}$$
 But $V_{\rm L} = I_{\rm C}R_{\rm 2}$ so $V_{\rm CC} = I_{\rm C}R_{\rm L} + V_{\rm CE}$ or $V_{\rm CE} = V_{\rm CC} - I_{\rm C}R_{\rm L}$.

This last equation is the load-line equation for the load $R_{\rm L}$. It shows that

(a) if
$$I_{\rm C}=0$$
, $V_{\rm CE}=V_{\rm CC}-0=V_{\rm CC}$, (b) if $V_{\rm CE}=0$, $I_{\rm C}R_{\rm L}=V_{\rm CC}$, so $I_{\rm C}=V_{\rm CC}/R_{\rm L}$, (c) if $V_{\rm CE}=V_{\rm CC}/2$, $I_{\rm C}=V_{\rm CC}/2R_{\rm L}$.

These points are plotted at the extremities and centre of a load line in Fig. 1.8 (p, q, r).

A transistor can be used to switch the current through $R_{\rm L}$ on and off if it is operated between cut-off (i.e. point Pc almost at the lower end of the load line) and a point higher up the load line corresponding to the required current. The higher point is frequently the saturation point Ps for the following reason. At Ps, $V_{\rm CE} = V_{\rm CE(sat)}$ and is very small, so although $I_{\rm C}$ may be large, the power dissipated in the transistor, $V_{CE}I_{C}$, is small. The power is also small at cut-off, since I_C is very small even though V_{CE} may be large.

At a point about half way up the load line however, the power dissipated in the transistor is a maximum, and equal to $(V_{\rm CC}/2) \times (I_{\rm C(sat)}/2)$. For example, suppose we have the following numerical values,

$$I_{\rm C} \simeq 0.1 \, {\rm mA}$$
, $V_{\rm CE} = 6 \, {\rm V}$ at cut-off, $I_{\rm C} \simeq 100 \, {\rm mA}$, $V_{\rm CE} = 0.1 \, {\rm V}$ at saturation,

then $I_{\rm C}=50{\rm mA},\ V_{\rm CE}=3{\rm V}$ at the mid-point of the load line. The power dissipations are therefore:

At cut-off, $0 \cdot 1 \text{mA} \times 6 \text{V} = 0 \cdot 6 \text{mW}$, At saturation, $100\text{mA} \times 0.1\text{V} = 10\text{mW}$, At mid-point, $50mA \times 3V = 150mW$.

It can be seen from these results that a transistor with a maximum rated dissipation of only 100mW could be used for switching between saturation and cut-off,

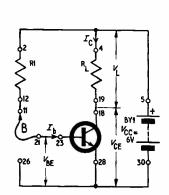


Fig. 1.7. A transistor amplifier circuit

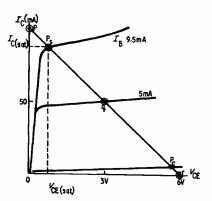


Fig. 1.8. Plotting the load line for the circuit given in Fig. 1.7

provided first that it can carry a steady current of 100mA, and second that it is made to spend most of its time at cut-off or in saturation. The transitions between cut-off and saturation would have to be fast.

It is for this reason that in first-approximation designs using small low power transistors as switches, it is important to be certain that sufficient base current can be supplied in order to ensure saturation.

LAMP DRIVER

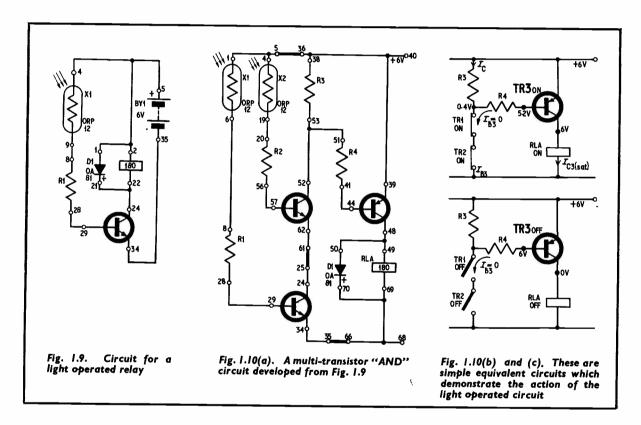
When TR1 in Fig. 1.7 is cut-off, $I_{\rm C}=0$ so $V_{\rm L}=0$. When it is saturated, $V_{\text{CE}} = V_{\text{CE(sat)}} \simeq 0$, so $V_{\text{L}} = 6V$. Also, if $R_{\text{L}} = 60$ ohms, $I_{\text{C(sat)}}$ will be 6/60 = 100 mA. Hence if R_L is a 6V, 100mA lamp, it will be off when the transistor is cut-off, and on when the transistor is saturated.

Connect up the circuit and check that the bulb is switched on and off when the link B is changed from socket 11 to socket 26. If the transistor used happens to have an h_{FE} value greater than 20, the base current being supplied will be more than sufficient to ensure saturation. Check this by changing R_B in small steps, keeping a careful watch on the bulb.

As soon as the bulb glows with less than its maximum brightness, the transistor is not being operated under saturation conditions. The power which is not now being dissipated by the bulb is being dissipated as heat

from the transistor.

Some high-gain TO18 or plastics transistors may be harmed in this circuit, e.g. 2N930 or BC108. TO5 size devices, or TO1 metal-canned devices such as the OC72 will operate satisfactorily.



In order to avoid excess power dissipation in the transistor, the base current supply must be sufficient to ensure saturation. At 100mA collector current, the average general purpose or switching transistor might have a d.c. current gain of only 20. Thus the base current must be 100/20 = 5 mA to meet this "worst case" possibility.

If a surplus transistor is used, it might be desirable to double this current to allow for a minimum possible $h_{\rm FE}$ of 10. The base current flows through $R_{\rm B}$ which drops a voltage $V_{\rm CC}-V_{\rm BE(sat)}$ under saturation conditions. Hence using the value of 20 for the minimum

 $R_{\rm B} = (6 - 0.8)V/5 \simeq 1,000$ ohms for a silicon device. or $R_B = (6-0.3)V/5 \simeq 1,200$ ohms for a germanium device.

LIGHT OPERATED RELAY

The ORP12 photo-conductive cell shown in Fig. 1.9 has a low resistance when brightly illuminated and a high resistance when in darkness (megohms). The cell is used to pass base current under conditions of bright illumination and in sufficient quantity to saturate the transistor. When the transistor saturates, the collector current, which also flows through the relay coil, actuates the relay. The relay used is a 6V, 180 ohm type. Calculation of component values is as follows.

$$I_{C(sat)} = 6/1 \dot{80} = 30 \text{mA}$$

If $h_{FE(min)} = 20$
 $I_{B(sat)} = 30/20 = 1.5 \text{mA}$.

Let the combined resistance of the ORP12 and R1 be equal to $R_{\rm B}$

Then $R_{\rm B}=(6-0.8)/1.5$ kilohms for silicon, or $R_{\rm B}=(6-0.3)/1.5$ kilohms for germanium. Thus try $R_{\rm B}=3.3$ k Ω (Si) or 3.9k Ω (Ge)

The extra base resistor R1 is included to protect the transistor from too high a base current under conditions of extremely bright illumination when the resistance of the ORP12 may be very small. Any transistor should be able to withstand a base current of 5mA without harm.

Thus we arrange for R1 to limit the base current to this value even under the lower possible resistance of the ORP12, namely zero. Hence $R_1 = 6V/5 = 1,200$ ohms (we have ignored $V_{\rm BE}$ here).

The diode shown shunting the relay coil can be almost any type to absorb the stored energy (back e.m.f.) from the relay coil when the magnetic field collapses during the switch-off period. If the diode is not included, the back e.m.f. set up by the relay coil might be sufficiently large to exceed the collector-emitter breakdown voltage and possibly damage the transistor. Such diodes are always included across inductive loads in switching circuits.

LIGHT OPERATED AND CIRCUIT

The circuit shown in Fig. 1.10 is included to show how to calculate the component values in a multi-transistor circuit. TR1 and TR2 are npn transistors while TR3 is pnp. There is no reason why TR1 and TR2 should not be pnp and TR3 npn, provided that the battery and diode polarities in the current are reversed.

Collector current cannot flow through TR1 if TR2 is cut off and vice-versa, because the two transistors are connected in series. Therefore, these transistors can only saturate when both photo-conductive cells are illuminated simultaneously.

If both TR1 and TR2 are cut off, the base current flow path for TR3 is blocked as shown, so TR3 is also cut off. If both TR1 and TR2 are saturated, they act as low resistances and allow a path along which current can flow from the base of TR3. TR3 can therefore saturate if R_4 has a low enough value.

Typical voltage values are shown in Fig. 10 for a circuit employing silicon transistors. Component values are calculated starting from the output end of the circuit as follows.

If the relay is a 6V, 180Ω type,

$$I_{C_3(sat)} = 6/180 = 33 \text{mA}$$

Assuming $h_{\text{FE3(min)}} = 20$, $I_{\text{B3(sat)}} = 33/20 = 1.6\text{mA}$. Hence $R_{4(\text{min)}} = (5\cdot2 - 0\cdot4)/1\cdot6 \simeq 3,300 \text{ ohms}$. Let $I_{\text{C1(sat)}} = I_{\text{C2(sat)}} = 5\text{mA}$ (a current at which the

Let $I_{C_1(\text{sat})} = I_{C_2(\text{sat})} = 5\text{mA}$ (a current at which the average small switching transistor will have plenty of current gain) and assume a minimum current gain of 20. Then $R_C = (6 - 0.4)/5 = 1,100 \text{ ohms}$. and $I_{B_1} = I_{B_2} = 5/20 = 0.25\text{mA}$.

The resistance in each base lead of the series transistors must therefore be $(6-0.9)/0.25 \approx 2,200$ ohms. (The 0.9V is the average base voltage on TR1 and TR2). The limiting resistors R1 and R2 can be about 4.7 kilohms each in order to limit the base currents to about 1mA.

If these calculations are repeated with base-emitter voltages assumed to be zero, it will be seen that few errors of importance will be made. If germanium transistors are to be used, the above component values will therefore suffice. If need be, the values can easily be recalculated using the base-emitter voltage of 0.3V under saturation conditions, instead of the 0.6V used above.

To be continued



EXHIBITION

"CRITICS of annual exhibitions are often heard to complain that they become in time the mixture as before. To some extent this is true of our International Radio Engineering and Communications Exhibition, but I venture to suggest that this sameness is one of its salient features... Yet from another point of view we must try never to be accused of sameness." Thus wrote, Mr John Swinnerton, President of the R.S.G.B., in his "Foreword" for the show catalogue.

As one of the participants of this exhibition, held at the New Horticultural Hall, London, from October 1 to 4, *Practical Electronics* is well aware of this "sameness."

If ever an exhibition, albeit for amateur interests, needs progressive thought in its design, this one does to update the image of modern communications to its rightful position in modern society.

HOME CONSTRUCTION

Practical Electronics had a communication receiver on show of revolutionary design (now being published). Practical Wireless exhibited a panoramic receiver of simple construction and suitable for visual display of signals on the 80 and 160 metre bands.

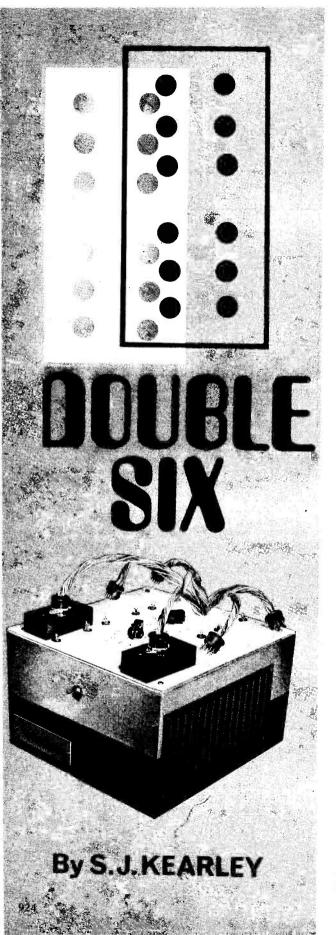
Although not strictly communications, P.E. were fully justified in showing advanced techniques in the "50 plus 50" fully stabilised power transistor amplifier, which can deliver up to 120 watts r.m.s. power from each channel of a stereo outfit. This design will no doubt find many homes in ham shacks for transmitter modulation when published in the near future.

Probably the most interesting feature of an otherwise clerical R.S.G.B. stand is the section devoted to the display of home constructed equipment, including transmitters, receivers and even a discotheque control panel. The standard achieved by the worthy award winners is often on a par with professional work, and one tends to think that many of these undertake similar work as a full time occupation.

WORKING DEMONSTRATIONS

It was apparent that working demonstrations attracted some of the best crowds. These included those put on by the British Amateur Television Club, Cable and Wireless with their teleprinters and facsimile transmitters and receivers, British Amateur Teleprinter Group, and the Royal Navy Amateur Radio Society who conducted morse code proficiency tests. The Post Office celebrated their change to the Ministry of Posts and Telecommunications by demonstrating their latest type of television detector vehicle for the u.h.f. as well as v.h.f. bands.

Several visitors come to the exhibition every year, and it was obvious that this is a good way of meeting those faceless radio contacts over a sandwich downstairs. But behind the very conspicuous R.A.F. Skynet satellite world communications demonstration, there was an equally large and conspicuous empty space. If only some seats could have filled this space many a QSO could have taken place face to face in comfort.



OUBLE SIX is a machine which plays dominoes. In operation Double Six is given six dominoes, face down, and plugged into them. When it is Double Six's turn to play, the machine causes a light to appear opposite the most favourable domino, at the same time emitting a "cackling" noise. If unable to play, Double Six makes a dismal moaning noise. Full playing instructions and the rules by which Double Six plays will be given later in this article.

STRATEGY

Double Six's strategy has been kept fairly simple so as to keep down the complexity and price of the machine. If allowed to play first against good opposition, Double Six should win just over half the time.

The strategy is as follows:

- 1. To play a domino matching one of those on the end of the chain.
- 2. When there is a choice between two dominoes, to play the domino with the most spots on. This gives the machine a useful chance of winning if nobody is able to play, and the total number of spots are counted. This rule is broken for "doubles" which are played in preference to any other dominoes—even those with more spots on. This is for three reasons:
 - (a) One has two chances of disposing of most dominoes, as they have two different numbers on. However, "doubles" have the same number on both ends, and so there is a correspondingly smaller chance of disposing of them, especially towards the end of the game. So it is advisable to play "doubles" while one has the chance.
 - (b) If the opponent plays onto the opposite end from the "double", Double Six will certainly be able to play on its next turn.
 - (c) If the opponent cannot play and the machine plays a "double", the opponent will still be unable to play, and so he will miss yet another turn.
- 3. When unable to play, the machine must acknow-ledge this fact. In the prototype this was achieved by making the machine "moan", and this has proved one of Double Six's most popular features. The machine may easily be modified to make a "knocking" sound if a more conventional response is desired.

DOUBLE SIX CIRCUIT

The main circuit diagram is shown in Fig. 1. TR1 and TR2 form a multivibrator, the output of which is fed to TR6 via the emitter follower TR3. The emitter follower prevents TR6 from loading the multivibrator and so stopping it oscillating. When TR6 is being driven the primary of T1—the winding that was originally the 6·3 volt secondary—has an a.c. voltage of approximately 9V across it and an output of approximately 350V is obtained at D2 causing a high voltage to build up across C3.

If any indicating neons (V2 to V13) strike current flows through R6 and R7 making the base of TR5 negative and hence turning on TR4 and TR5. This virtually shorts the base of TR6 to the positive line and prevents it being driven by TR3; it also turns off TR10, reverse biasing D4. Transistor TR9 will now oscillate in bursts, unaffected by TR8 which is turned off via D3. The bursts of oscillation form the "cackle".

heard when Double Six can play, and this can be adjusted by VR2; the pitch can also be varied by altering C5.

Once the oscillation at TR6 collector has stopped, the voltage across C3 will fall until the neon which has fired extinguishes, returning the circuit to its original condition. The voltage across C3 then begins to build up again. This process causes the neon to flash and prevents the voltage across C3 from rising above the striking voltage of the neon in the lowest resistance path.

If the machine cannot play a domino, V1 eventually strikes, this turns on TR7, reverse biasing D3 and allowing TR8 to oscillate, producing the "moan". By increasing R12 in value the oscillator can be made to block and so produce a "knocking" sound.

While Double Six is on, a rising voltage is applied to the pins of plugs PL1 to PL6 (Fig. 3), for this reason a biased off switch has been used for S1.

CONSTRUCTIONAL DETAILS

Most of the circuitry was constructed on a piece of plain Veroboard using pins for transistor and fly lead connection and the component wires for wiring up where possible, see Fig. 2. The transistors should be added when the rest of the circuit has been completed and the whole unit can then be housed in a suitable wooden case similar to that shown in the photographs. The case must be large enough to house the circuit board, batteries, transformer and loudspeaker, and there should be plenty of room under the top panel to allow for wiring to switches S2 and S3; the suggested case size is $10 \text{in} \times 9 \text{in} \times 6 \text{in}$ deep.

FRONT PANEL CONSTRUCTION

The front panel is made of paxolin, ‡in diameter holes are drilled for the neons (see Fig. 6), rubber grommets are inserted, and the neons pushed into the grommets. (If the glass envelopes of the neons are moistened slightly, this job is made much easier.) Switches S2 and S3 are single pole, 10- or 12-way wafer switches; only seven positions are used.

Wiring to the switches and neons on the top panel is shown in Fig. 5. Two small tag strips were used for the wires from pins 1 and 9 on the B9A plugs but these are not essential if longer wires are fitted. The wiring connections to the B9A plugs are shown in Figs. 3 and 4; each wire is thin p.v.c. covered, preferably colour coded to make wiring easier. The wires to each plug are twisted together. As seven wires are to be connected to each tag of S2, each individual wire should be carefully inserted into its tag, and bent over to keep it in place. Solder is not applied until all the wires are in place.

It is wise to check the wiring to each plug with a continuity tester or an ohmmeter before soldering, in case wiring errors have been made. Such errors would be extremely difficult to track down at a later stage. The length of the wires to each B9A plug should be adjusted so that each plug matches its own position on the top panel.

DOMINO DETAILS

The dominoes are made from solid blocks of wood, a 3-in diameter hole being drilled in each to accept a B9A valveholder, see Fig. 7. It is advisable to obtain the valveholders either off old TV chassis, or from a "surplus" supplier, as otherwise the cost of these components may be rather high. The inside of each hole should be varnished to prevent leakage through the wood. The dominoes are painted matt black, and

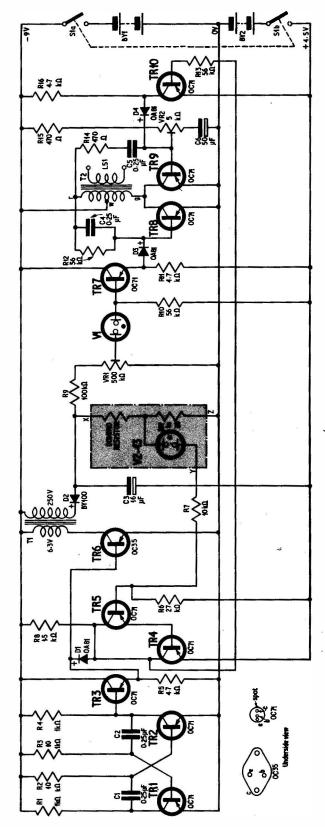
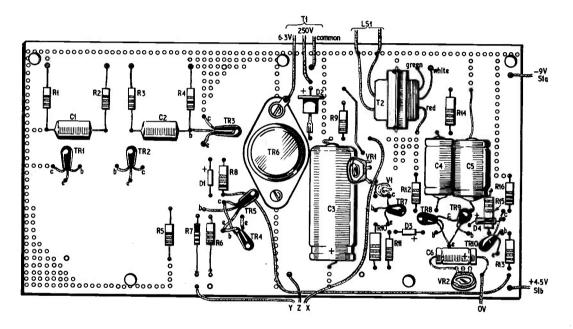


Fig. 1. The main circuit diagram of Double Six

Table I. DOMINO WIRING DATA

Domino	Resistor	Pins	Resistor	Pins	Dominio	Resistor	Pins	Resistor	Pins
6–6	0	1-8	0	9-8	4-3	150kΩ	1-6	100kΩ	0.5
6–5	56k Ω	1-8	$22k\Omega$	9_7	4-2	220kΩ	I-6	100kΩ	9-5
6-4	100kΩ	1-8	$22k\Omega$	9-6	4-1	330kΩ	1-6	100kΩ	9-4
6–3	150kΩ	1-8	22kΩ	9_5	4-0	470kΩ	1-6	100kΩ	9–3
6-2	$220k\Omega$	1-8	22kΩ	9-4	3-3	0	1-6 1-5	100K12	9–2
6-1	$330k\Omega$	1-8	22kΩ	9-3	3–3	220kΩ	1-5 1-5	150kΩ	9–5
6-0	$470k\Omega$	1-8	22kΩ	9–2	3-1	330kΩ	i-5	150kΩ	9_4
5-5	0	1-7	0	9 <u>-</u> 7	3-0	470kΩ	1-5		9–3
5-4	$100k\Omega$	1-7	56kΩ	9-6	2-2	0 .	1-4	150kΩ	9–2
5-3	150kΩ	1-7	56kΩ	9-5	2-1	330kΩ	1-4	2201-0	9-4
5-2	220kΩ	1-7	56kΩ	9_4	2-0	470kΩ	1-4	220kΩ	9-3
5-1	330kΩ	1-7	56kΩ	9 <u>~3</u>	1-1	0	1-3	220kΩ	9-2
5-0	$470k\Omega$	1-7	56kΩ	9-2	1-0	470kΩ	1-3	0	9-3
4_4	0	1–6	0	9-6	0-0	0	1-3 1-2	330kΩ 0	9-2 9-2

Note: Resistors shown as 0 must be wire links between the pins indicated



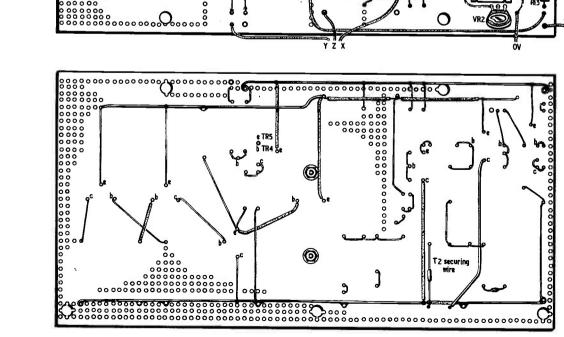


Fig. 2. Component layout and wiring of the circuit board

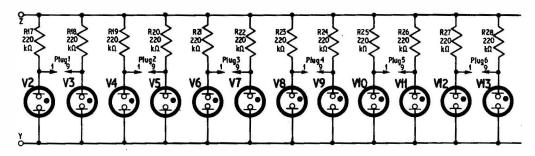


Fig. 3. Circuit diagram of the components mounted on the front panel

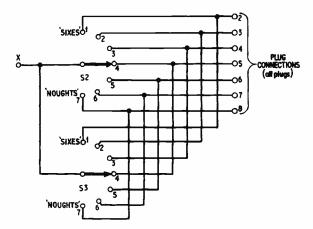


Fig. 4. Circuit details of the selector switches

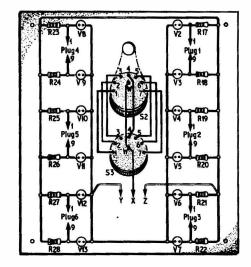


Fig. 5. Top panel wiring details

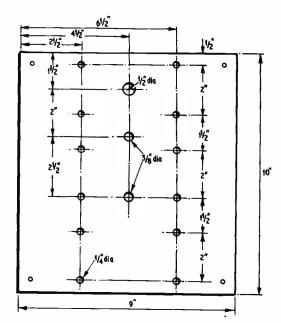


Fig. 6. Top panel drilling measurements

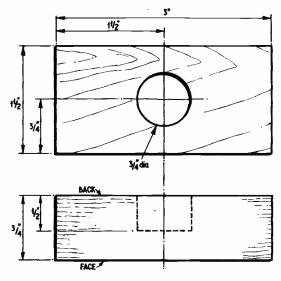


Fig. 7. Details of a domino. The 28 dominoes can be made from one 7ft 6in length of $l\frac{1}{2}$ in \times $\frac{1}{4}$ in wood

COMPONENTS . . . Resistors RI $lk\Omega$ $10k\Omega$ R3 l0kΩ R4 $\mathsf{Ik}\Omega$ $4.7k\Omega$ $27k\Omega$ R6 R7 $10k\Omega$ **R8** $1.5k\Omega$ 100k O R9 RIO $56k\Omega$ RH 4.7kΩ RI2 $56k\Omega$ RI3 56k Ω 470 Ω R14 RIS 56k Ω RI6 $4.7k\Omega$ R17-R28 220k $\Omega \pm 5\%$ All $\pm 10\%$, $\frac{1}{4}$ watt carbon except where stated Resistors for dominoes (6 of each) $\begin{array}{ccc} \textbf{22k}\Omega & \pm \textbf{10}\% \\ \textbf{56k}\Omega & \pm \textbf{10}\% \end{array}$ 100kΩ $\pm 10\%$ $150k\Omega \pm 5\%$ 220k Ω $\pm 5\%$ \pm 5% 330k Ω ±5% 470kΩ All & watt carbon Capacitors 0.25µF C2 0.25μF 16μF elect. 450V C30-25µF 0.25 uF 50μF elect. 12V **Potentiometers** VRI 500k Ω skeleton preset VR2 $5k\Omega$ skeleton preset **Semiconductors** TRI-TR5 OC71 (5 off) TR6 OC35 TR7-TR10 OC71 (4 off) DI OASI BY100 D2 D3 OA81 D4 OA81 **Switches** SI D.P.D.T. biased off S2 Single pole 10- or 12-way wafer (only 7 ways Single pole 10- or 12-way wafer (only 7 ways used) Miscellaneous VI-VI3 miniature (wire ended) neons TI Mains transformer. Secondary 0-6-3V (used in oscillator) LT700 transistor push/pull output type, 19-4:1 Small 3\O loudspeaker BYI 3V type 800 (3 off) BY2 4.5V type 1289 PLI-PL6 B9A plugs (6 off) B9A valveholders (28 off)

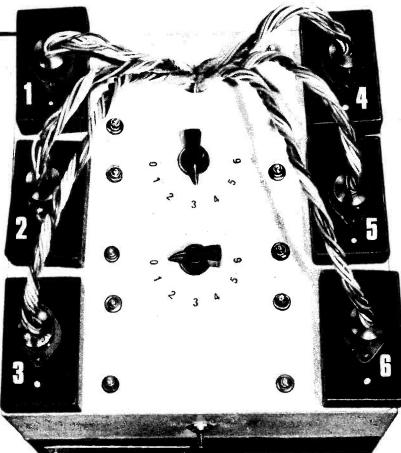


Fig. 8. View of the top panel of Double Six showing the dominoes in their positions and the indicating marks on the dominoes

drawing pins with white plastic covered heads inserted as the spots on the dominoes.

It is necessary to place a small dab of glue under the head of each drawing pin, or the plastic covering the heads may fall off. The connections of the resistors inside each domino are given in Table 1.

BASIS OF OPERATION

The pins of the socket in the dominoes to which resistors are connected define the number of spots on either face of the domino; the value of the resistor defines how many spots are on the other face. To give an example of Double Six in action, let us assume that the 6-0 domino is in position 1 (Fig. 8) and that the 6-4 is in position 2.

When S2 or S3 is switched to "sixes", a steadily rising voltage is applied to pin 2 on each B9A plug. So the neon indicating position 1 is connected to h.t. via a 470 kilohm resistor, whilst the neon indicating position 2 is connected via a 100 kilohm resistor. Therefore there is a greater fraction of the h.t. voltage across the neon indicating position 2 than across the neon indicating position 1, therefore it will strike first. This is arranged to cause the h.t. voltage to fall and therefore the neon will switch off allowing the voltage to rise again.

Grommets small (12 off)

Wood for case and dominoes (see text)

This results in the neon indicating position 2 to flash and the "cackling" to be heard, while the neon indicating position 1 will not attain its striking voltage. The machine thus indicates that the 6-4 domino is to be played, in accordance with its strategy.

DOMINO MARKING

It is desirable to make the machine light the neon opposite the end of the domino which matches, e.g. when set to play "sixes" (tag 1 on S2 and S3 connected) and playing a 6-4 domino, to light the neon opposite the "six" end rather than the "four" end.

For this reason the dominoes are marked with a locating spot as in Fig. 8. This is done by the following method:

- (a) Fit the valveholder such that pins 1 and 9 are on the same side as the locating mark.
- (b) For each domino, ensure that the higher number of spots is on the same side as the locating mark.
- (c) When plugging dominoes onto the machine, orient them so that the locating mark always faces the front, i.e., S1 end of Double Six.

SETTING UP

When the wiring has been completed, the following setting up operations are required. Disconnect the wire from h.t. to S2, and turn VR1 clockwise (no voltage across V1). Check that the voltage across C3 exceeds 310 volts. It will possibly be well in excess of this and if it is over 350V a resistor should be placed in series

Fig. 9. Prototype wiring; the main circuitry has now been included on a single board. This shows the positioning of the major components in the case

with TR6 collector and T1. The value of this resistor can be determined by trial and error to obtain an output of around 350 volts.

The current drawn by TR6 when oscillating is approximately 350mA, so large capacity batteries must be used. Turn VR1 anticlockwise until V1 strikes; this should be accompanied by the "moan" from the speaker. If all is well, connect point X to S1 wiper, and plug in a domino, setting up its value on S2 and S3. Soon after switching on S1 the "cackling" sound should be heard and a neon should flash alongside the domino. If not, check the connections to first the domino, then the plug. If the neon comes on but does not flash, check the circuitry around TR4 and TR5.

When Double Six is functioning satisfactorily, it is ready for its "test" game. Put six dominoes face down in positions I to 6, with the locating marks facing the front of the machine and plug them in. Choose six dominoes for yourself, and play one of them. Set S2 and S3 to inform the machine as to what you have played and switch on S1. A cackle will probably be heard, accompanied by a neon flashing alongside a domino. Switch off S1, remove the domino, and play it next to your own. The correct end to play is that alongside which the neon was flashing (for this reason it is necessary to put the dominoes in the right way round). Continue in this way until the game is finished.

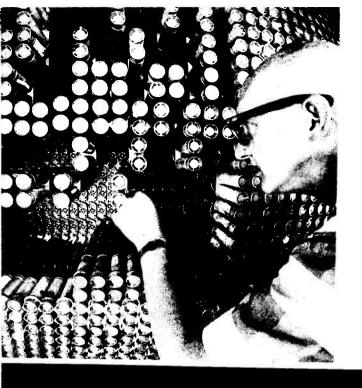
This design has no provision for starting the game—the procedure adopted is to set S2 and S3 to "sixes or fives" and if Double Six has none of these (very un-

likely) to try fours. If preferred, a seven pole two-way switch could be wired between h.t. and S2, in order to connect tags 1 to 7 to h.t. when S1 is in the "on" position. The machine would then play a "double" or a six or five if it had no "double".

RULES OF THE GAME

Since there are many variations of the game of dominoes, it would be as well to state the rules of the game which Double Six plays. (By modifying the circuit slightly, it should be possible to programme the machine to play other variations.) Each player is given six dominoes face-down, which he does not show to his opponents. The first player may put down any domino he chooses to start with. If a player has no domino matching the ones on the table, he admits this, usually by knocking on the table, and misses his turn.

The first player to dispose of all his dominoes is the winner. If no player has a domino which matches, the player with the lowest total number of spots on his remaining dominoes is the winner. It should be noted that, as no player knows which dominoes his opponents have, and the selection of dominoes which each player gets depends on chance alone, the outcome of the game is not strictly determined, and no strategy can guarantee a win. This is in contrast to games like Noughts and Crosses, or Nim, where correct play always arrives at a predetermined result. \star



Advanced Radar System

SYSTEM tests on a new advanced radar prototype—forerunner of what could be the world's most powerful radar for defence against missile attack in the 1970's and beyond—have begun at Hughes Aircraft Company in California.

The tests include radar range exercises and actual detection and tracking of air traffic. The prototype, a scale version of a proposed long-range system called ADAR (Advanced Design Array Radar), will be the most powerful radar yet built by Hughes.

An engineer is shown making adjustments to energy feeds on a scale prototype of the new phased-array radar. The energy feeds are devices that channel radio-frequency energy between points in the system.

ELECTRONORAMA

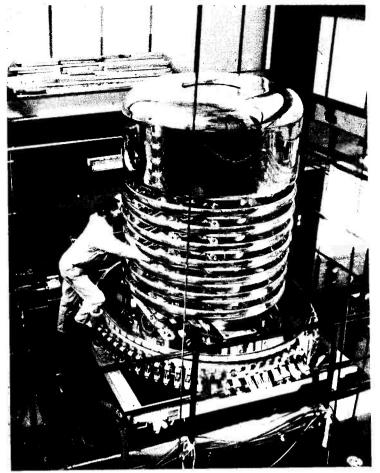


Laser Television Tape Player

A LABORATORY model of a revolutionary, low-cost colour television tape player built around lasers and holography and destined for home use in the early 1970's was unveiled recently by RCA. In commercial form the tape player, named "Selectavision", is expected to be the first consumer product to employ lasers, and will be designed to attach to any standard colour or black and white television set. It will play full-colour programmes recorded on tapes made of the same clear, inexpensive plastic material used in supermarkets to wrap and display meats. The material for the tapes will cost only about one-tenth as much as conventional type films.

The clear plastic Selectavision programme tapes will be scratch-proof, dust-proof, and virtually indestructible under conditions of normal use. They will have countless replay capabilities, be able to run in slow motion, or be able to be stopped and started at will so that a single frame can be studied at length, if desired. The player itself will be compact, and as easy to operate as a modern cartridge player.

The television tape player is shown in use on the left—tape cartridges can be changed easily as can be seen from the photograph



Giant Microscope

The first of five giant electron microscopes is nearing completion at the AEI Scientific Apparatus Limited; it has already been operating successfully at one million volts during tests.

In November the UKAEA, Harwell, will take

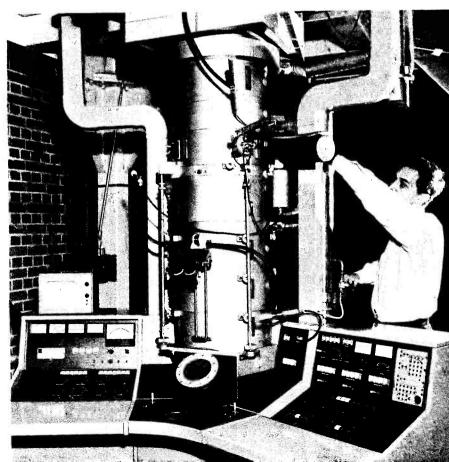
In November the UKAEA, Harwell, will take delivery of this advanced instrument, the first commercial million-volt electron microscope to be built in Europe. It will be used to investigate thicker sections of metals and materials than hitherto possible using an electron beam accelerated by ten times the voltage used in a conventional high resolution electron microscope. The beam will probe the samples in an effort to discover new information about the structure and behaviour of metals both in common use and those with special properties needed for new technological developments.

Biologists will also use these electron microscopes to study the structure of cells. There is also the exciting possibility that the great penetrating power of these new instruments may permit observation of living material in special protective surroundings

in the microscope.

The accelerator and voltage generator (above) of the AEI million-volt electron microscope during manufacture. Five of these instruments are on order from AEI

The massive microscope column (right), over 8ft high and 18in diameter, and the control desks



ECHONES PARTS

By Alan Douglas, Sen. Mem. I.E.E.E.

N the last two parts we have presented all of the tone forming circuitry as Veroboard modules.

Since the solo accompaniment and pedal subassemblies are contained in a metal box, details of the shelf needed for mounting this are presented first. In addition to the screening box this shelf also serves as a platform for the 23 stop tab units used variously for voice selection.

VOICE BOX SHELF

The shelf supporting the voice box and stop tab assemblies measures 4ft 3½in by 8in by ½in and is of plywood. Reference to the console rear view given in Part Two shows that the shelf just clears the upper manual assembly.

To fix this position, measure off 6in from the lower keyframe and make pencil marks on the console sides "A" shown in Fig. 1.4. Angle brackets or lengths of lin batten can be affixed at these marks and the shelf attached.

STOP PANEL ASSEMBLY

In Fig. 8.1 is given details of the stop panel (A) and keyboard flanking panels (B).

Whilst the latter need not be made up at this stage, it is rather important that the stop panel is, as the four rectangular apertures will fix the final placement of the stop tab units. With the panel completed this can be temporarily screwed to the top panel B of Fig. 1.4. If the keyboard flanking panels have been made up it should be possible to press fit this without a screw.

STOP TAB UNITS

The stop tab units used are made by Kimber-Allen Ltd. These are manually operated switches which are used to activate or de-activate the individual voice nets of the tone forming circuitry.

Each switch has a smooth positive toggle action and there is screw adjustment with felt stops for correct positioning of the tab.

In the tone networks of Fig. 6.5 the stop switches, S1-S10, are shown open; here the voices are active as square waves from the pre-amplifier are not short circuited to ground.

For this condition to prevail, the switch tabs would normally be depressed hence the stop tab unit required is of the depress-to-break variety.

However, for the 8ft Dolce in the accompaniment and the 16ft Sub-Bass of the pedals a depress-to-make type of switch is required as additional filtration is being included to soften the voice it complements.

Of the 23 stop units called for, two are spares—for additional functions as required—and one used for switching the tremulant motor.

Details of a stop unit is given in Fig. 8.2. The accompanying photograph shows the order of the stop voices as viewed at the stop panel.

TAB ENGRAVING

The tabs used are standard K-A types, again available from Kimber-Allen Ltd. These are tapered and radiused at the nose. Made from cellulose sheet, they can be obtained in a choice of three colours: grained ivorine, red, and black. On the prototype organ the choice was ivorine for the solo tabs, red for the accompaniment, and black for the pedals.

When ordering the stop units and tabs, engraving details should be included as follows:

"我们们的我们的我们		
化二氯甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基	Table &I.	
为是 AS 体系 为非 特别的特别	THE SECTION OF	
725 No Solo 15 19 19	Accommonlment	Table 1
Contra Viole 16	Dolce &	
Contra Tibia 16	Flute 1	Major Bass 16
Viole E	Viole Acute 8	Sub Best 16 Base Plate 1
Tible	Flute 4	
This is	Violina 4	Trembut
Violina a	Clarinet 8	Leslie Trem
Piccolo 2.	Trumpet 8	
Double Horn 16		
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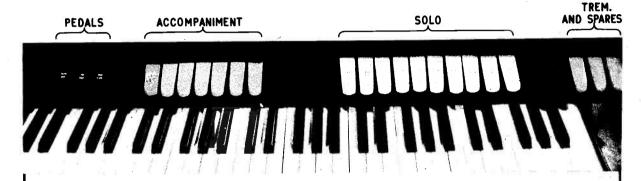
SCREENING BOX ASSEMBLIES

When the stop tab units have been shelf mounted, we can proceed with the mounting of the voicing sub-assemblies in a metal screening box.

The screening box, which measures 24in by 5½in by 2in is shown in the photograph with the sub-assemblies mounted inside. The chokes, boards and relevant cables are shown annotated. The box drilling requirements are for busbar, filter and stop unit leads; the placement of these is not critical. This 16 s.w.g. aluminium box must have a lid to be effective. It can be obtained undrilled from H. L. Smith and Co., Ltd., 287/289 Edgware Road, London, W.2.

To insulate the Veroboard modules, two lengths of 5in by 8in s.r.b.p. board are used, one for each pair of sub-assemblies. Reference to the photograph shows the coils centrally placed between these assemblies. These coils are in fact the first items to be mounted, this being achieved by Aralditing.

With this completed, the two tag strips can be mounted. These serve merely as junctions between the fragile choke wires and Veroboard assemblies.



Stop units in position with tabs shown projecting at stop panel aperatures. Table 8.1. gives the order of the stop engravings reading from left to right

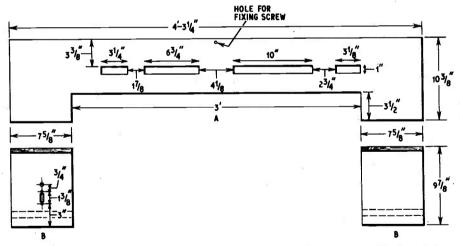


Fig. 8.1. Details of stop panel (A) and keyboard side panels. With the stop aperatures cut these should be lined with green felt

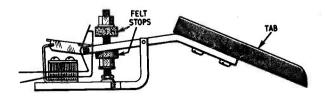


Fig. 8.2. Details of a stop tab unit

The wires should be carefully cleaned with a fine gauge sandpaper before soldering. The first unit to be wired up and mounted is the solo pre-amplifier board. Details of this are given in Fig. 6.3 where it can be seen that there are four busbar connections and two positive and negative supply connections.

We have previously connected coaxial cables at the busbars so it only means routing these as shown in the photograph and connecting at the points shown in Fig. 6.3.

As these cables travel the length of the box, cable clip fixing is necessary. Small polythene press-fixing straps were used here.

The supply lines can be conveniently picked off from the oscillators and taken through a hole drilled in the shelf. This supply, of course, will feed all of the preamplifiers in the box, it only being necessary to parallel the connections.

WIRING THE SOLO FILTERS

The next board to wire is that of the solo filters. Wiring between this and the adjacent pre-amplifier board is fully detailed in Fig. 6.6 so this can be undertaken.

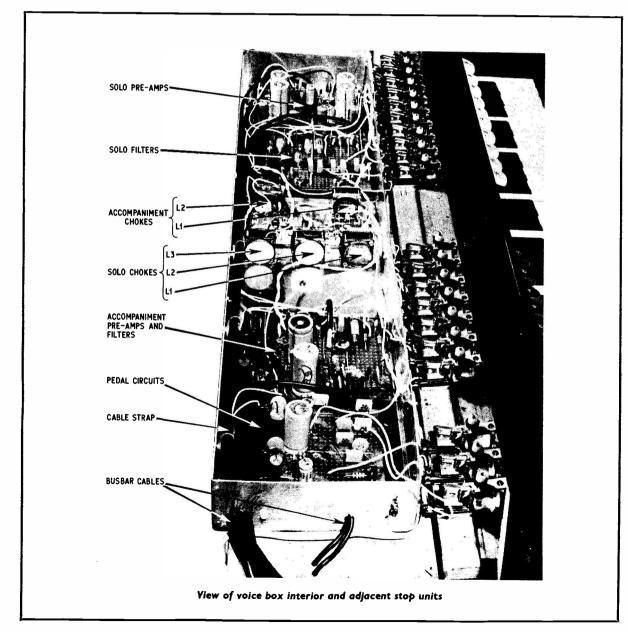
Lengths of sleeved wires are connected at the stop units shown as S1-S10 in Fig. 6.5 and then run through the holes drilled as shown in Fig. 8.3.

Connections to the chokes at the tag strips are by twisted wire pairs.

ACCOMPANIMENT AND PEDAL BOARDS

The wiring of the accompaniment and pedal boards follow the same general procedure as has gone before.

The 8ft and 4ft pitch coaxial cables are routed from the accompaniment busbars through the box and connected as in Fig. 7.2; then the stop switches are con-



nected. At this stage connection from the solo and accompaniment filter outputs can be made with 2ft lengths of miniature coaxial cable.

As was described in Part Four, the pedal inputs are taken from pins 31 and 32 of one of the pedal sockets, so lengths of coaxial cable can be taken from the pedal socket chosen. The accompanying photograph to Fig. 4.1 shows these cables clearly.

With these terminated at the pedal pre-amplifiers it remains to earth their screens. This is done at the pedal sockets by baring the coaxial braid and soldering a common wire connection to a simple aluminium surround seen in the photograph of the pedal resistor boards in Part Four. This screens the pedal plugs and resistor boards from extraneous field influences.

With the stop switches wired, it only remains to loop in the supply lines from the pre-amplifier board. Now, since the negative supply line is finally grounded, this should be connected to the aluminium of the voice box; suitable connection will be found at the screwed terminals of the choke tag strips.

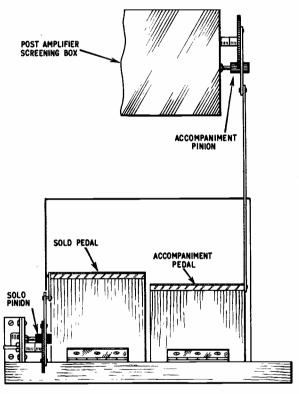
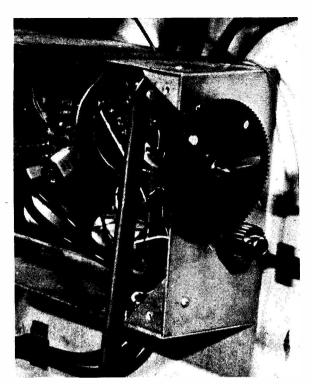


Fig. 8.3. Solo and accompaniment swell pedals shown hinge mounted

To complete the earth line of the voicing circuits, a length of 22 s.w.g. tinned copper wire is strung along the unattached connectors of the stop tab units and soldered. The free wire end is soldered to a tag at the screening box.

POST AMPLIFIER SCREENING

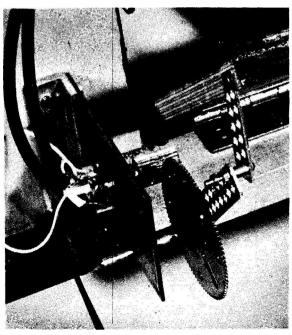
The outputs from the manual filters terminate at the post amplifiers "A" and "B" as described in Part Seven. The two cables used are again miniature coaxial. Before any flying connections are made to these Veroboard assemblies a 7in by 5in by 2½in screening box should be fixed to the kneeboard with two binder screws, positioning being indicated in the



Details of accompaniment swell linkage at post amplifier screening box

rear console view given in Part Two. This box is lidded an can also be obtained from H. L. Smith Ltd. In this is mounted the post amplifiers "A" and "B" using s.r.b.p. insulating boards. Sufficient space should be left for mounting the swell potentiometer and gear wheel as seen in Fig. 8.3 and the photograph.

Details of solo swell linkage. The bush for mounting the large wheel spindle is soldered to the brass plate



Now we can go on to wiring these amplifiers. First, 15V supply leads are taken again from the oscillator shelf and connected as shown in Fig. 7.10. Then the filter coaxial cables are connected, making sure that the copper braid is grounded at the box.

EXPRESSION PEDALS

The next thing to tackle is the expression pedals. Two have to be made from $9\frac{1}{2}$ in by 5 in by $\frac{3}{4}$ in plywood and faced one side with ribbed rubber or linoleum. In the usual type of construction, these pedals are carried on substantial metal rods and pivots, but we are not making them do much work so plain 3 in steel hinges will suffice as shown in Fig. 8.3 and Fig. 8.4.

First of all a piece of 2in by 1in hardwood is screwed across the swell aperture of the kneeboard at the bottom. This is reinforced at the end with metal strips which are screwed to the lower frame member. This can be seen in the photograph.

Two lengths of pierced s.r.b.p. or metal strip are used to transmit the pedal movement. To fix the strip at the pedal end a 1in round head wood screw with washer is used. The shorter strip is bolted to the large gearwheel to give about 25 degrees of movement to the pedal for a full rotation of the potentiometer.

The small pinions will need to be drilled out slightly to fit the ‡in spindle of the potentiometer. Standard Meccano spindles support the 60 tooth wheels.

The potentiometer for the accompaniment swell is situated near to the bottom of the post amplifier screening box as seen in the photograph. The fitting of this component is not critical, the main object being to ensure a straight pull being exerted on the connecting strip by the pedal. Full details of the gear assembly are given in Fig. 8.3.

If 4B.A. screws with nylon locknuts are used to assemble the moving parts, a good degree of stiffness can be imparted to the movement.

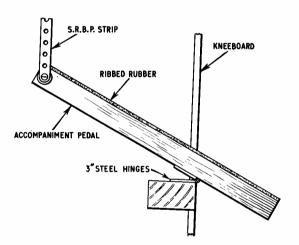


Fig. 8.4. Side view of accompaniment pedal

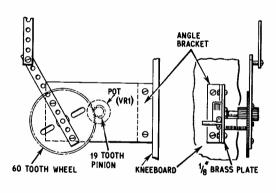


Fig. 8.5. Detail of solo swell linkage which is identical to the accompaniment assembly on the post amplifier screening box. To stiffen the pedal action nylon, lock nuts should be used at the junction of the s.r.b.p. strips

The hinges are then attached to the wood block and pedals; plain wood side of course.

SWELL MECHANICS

We could control the volume by several means, including photocells, but to keep the circuits as simple as possible we use logarithmic 4.7 kilohm potentiometers as the emitter resistors of the post amplifier emitter follower outputs as shown in Fig. 7.8.

The potentiometer for the solo post amplifier "A" is mounted below the divider boards. The potentiometer for the accompaniment post amplifier "B" is on the post amplifier screening box. For the gear assembly we need two No. 26A 19 tooth pinions and two No. 27D 60 tooth gear wheels. These items should be obtainable from any Meccano parts stockist.

Fig. 8.5 gives details of the solo swell linkage. Here the potentiometer and gear train are mounted on $\frac{1}{8}$ in brass plate which is fixed to the kneeboard by way of an angle bracket.

With the potentiometers connected, these can be wired to the post amplifier outlets, making sure that all earth return lines terminate at the post amplifier screening box.

MAINS WIRING

The mains wiring layout is given in Fig. 8.6. A three-pin 5A socket is fitted to a wooden bracket as shown in the photograph of the console rear given in Part Two. Two terminal strips serve to route the supply to the master switch S1 and neon indicator to the left keyboard flanking panel shown in Fig. 8.1.

The switch is an on/off rocker switch type RS200 available from Henry's Radio Ltd. S2 is the tremulant stop unit, the capacitor across it being used for spark suppression as without it unpleasant thumps feed through to the speakers when the tremulant motor is switched in.

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A CONTRACT worth £73,000 to supply the European Space Technology Centre with airborne telemetry equipment has been awarded to Dynatel Ltd. This is the first time a contract of this kind has been awarded to a British company.

The telemetry equipment will be installed in sounding rockets and used in a number of research projects to transmit data picked up by the sensors in the vehicle to a

receiving station.

Memory Drum

SPERRY HAVE introduced a new magnetic storage drum (the J101) which has been designed as an economical memory storage unit for a wide range of digital data applications, including use as a back-up store for computers and invoicing machines.

Read/write heads which float on a minute air cushion, are used to record the information as binary digits (bits) on the ferric oxide covered drum surface. The average access time to retrieve stored information is 10 milliseconds.

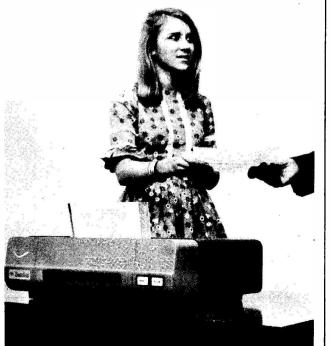
Telephone Messenger

PUBLICLY demonstrated for the first time at the Business Efficiency Exhibition at Olympia was a new business communication machine (shown below) that can send and receive documents and drawings over any distance by telephone.

Sendox, as the new system is named, will provide the much-needed breakthrough in inter-office and inter-city document communication by overcoming current problems of availability of messengers, transport and skilled

operators.

Sendox has been developed by Muirhead Ltd. of Beckenham—suppliers of facsimile systems to newspaper publishers, police forces and meteorological services. It can operate over private or public telephone lines or radio circuits, to an office in the same building or a customer or supplier miles away.



FUNCTIONAL CHECKS

With the mains wiring completed we can start making functional checks on the manuals.

First switch off P.S.U.2, the pedal power unit.

Now adjust all of the potentiometer wipers in the voice box to mid-travel.

With a WB HF.1214 loudspeaker connected at the terminal block of P.A.2 the mains supply can be switched on.

Checking the solo and accompaniment stops merely means depressing each tab individually, noting the voice and balancing the output level with the filter attenuators.

As we have not, as yet, tuned the oscillators it is necessary for these checks to add capacitors to one oscillator, at least.

Roughly tune one oscillator to B flat by adding one 500pF and one 10pF capacitor connected in parallel

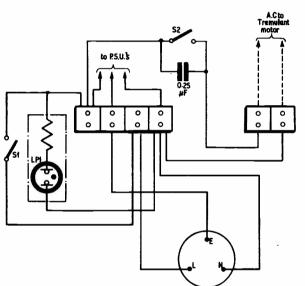


Fig. 8.6. Mains wiring layout for organ console. For plug mounting details refer to rear view photograph of organ given in Part Two

across the coil. These components should be close tolerance silver mica types.

The related divider will be indicated as shown in Fig. 3.5 if the method of annotating the retaining bars has been followed.

If the supply is now switched on and the middle keyboard B flat depressed and held, it should be possible to check the stops and output levels. This method should be followed for both keyboards and at the same time the action of the swell pedals can be examined.

If all is well, the solo and accompaniment tone box assemblies can be fixed with binder screws. It is important that no screw should come in contact with active circuitry and in this connection reference should be made to the relative underboard wiring diagram given in Parts Six and Seven.

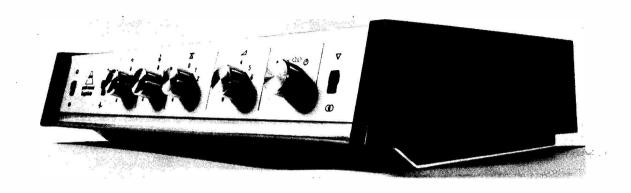
Next month we will start on the pedalboard assembly.

To be continued

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All tested	perfect function	nal devices
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		ND NPN			
AC125	ACY22	ACY36	NKT677	OC81	2G381
ACI26	ACY27	NKTI4I	NKT713	OC82	2G382
ACI27	ACY28	NKTI42	NKT773	2G301	2G399A
ACI28	ACY29	NKT212	OC44	2G302	
AC!30	ACY30	NKT213	OC45	2G303	
ACY19	ACY31	NKT214	OC71	2G308	1/6
ACY20	ACY34	NKT215	OC72	2G371	
ACY21	ACY35	NKT271	OC75	2G374	each

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Further improvements incorporated in this circuit are an internal warning of flasher lamp failure, without affecting the operation of the remaining lamps, and the inclusion of an audio bleeper as an alternative, or additional warning system if preferred. The design is illustrated for positive 12V car battery systems, but can be modified for negative earth systems (see later).

TRANSISTOR TIME SWITCH

A simple two wire flasher circuit for flashing any low power indicator lamp from 6 to 24V is shown in Fig. 1.

When the circuit is switched on, practically the full battery voltage appears across TR1 bias chain but the transistor is held off until the capacitor C1 charges up through R4 and the lamp causing TR1 to conduct. The resulting collector current of TR1 is then amplified by complementary transistor TR2, increasing the lamp voltage and decreasing the control circuit voltage.

As the emitter voltage of TR1 is held by the voltage across C1, the bias of TR1 is increased causing a further increase of collector current. This action is cumulative, producing a rapid switching action which saturates TR1 and TR2, holding the lamp on until C1 discharges through TR1, R3, and the base emitter junction of TR2. When the capacitor discharge current drops below the saturation current of TR1 and TR2, the switching action is reversed and the cycle is repeated.

The "off" time of the lamp depends on the charging time constant C_1R_4 ; the "on" time depends on the discharging time constant C_1R_3 . Hence the p.r.f. is

proportional to $1/(C_1R_3 + C_1R_4)$. Resistor R4 limits TR2 overload current by prewarming the lamp; switching on from cold can produce a peak of about five times the normal lamp current. A 10 ohm resistance in series with LP1 is preferable for switched lamp circuits as this extends the life of the

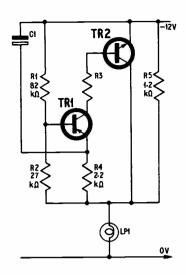


Fig. 1. Circuit diagram of a simple lamp flasher

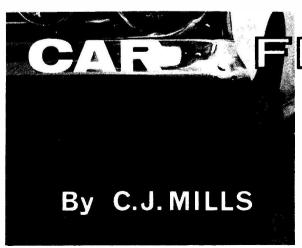
lamp as well as the transistor but it requires a supply voltage higher than the normal lamp voltage.

COMPLETE BLEEPING FLASHER

The final circuit (Fig. 2) is developed from the above by adding a power transistor TR3 and an indicator switching transistor TR4. The 0.25W resistor in series with TR3 provides enough bias to switch the indicator lamp on via TR4 when two 20 watt flasher lamps are used. If only one or both flasher lamps fail, the indicator lamp will not light.

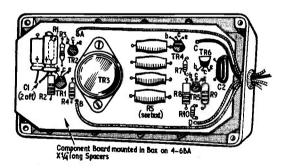
For the motorist who prefers an audio indicator, the circuit in Fig. 1 can be used as a "bleeper" by changing the value of C1 to 0.25μ F (selected to suit preferred tone). This is an aid for forgetful drivers and produces some interesting comments from passengers who hear it for the first time. A limiting resistor R10 to control the amplitude from the loudspeaker completes the circuit.

The final circuit (Fig. 2) includes the bleeper and its components are re-numbered around TR5 and TR6.



CAR FLASHER -.12V TR₂ TR4 56<u>0</u> 2N3702 INDICATOR SWITCH FRONT AND REAR EXTERNAL FLASHER LAMPS LEFT

Fig. 2. Complete circuit diagram of car flasher unit. The circuit includes the audio bleeper section and is wired for positive earth systems. See Fig. 4 for negative earth circuit



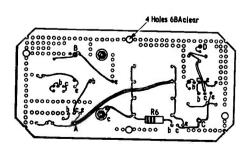


Fig. 3. Component layout and wiring of the flasher unit for positive earth systems

COMPONENTS

₹esis'	tors.				
RI	82k Ω	R6	56Ω		
R2	27kΩ	R7	82kΩ		
R3	470Ω	R8	$27k\Omega$		
R4	2·2kΩ	R9	$2 \cdot 2k\Omega$		
R5	0.25Ω (see text)	RIO	150Ω		
$11 \pm 10\%$, $\frac{1}{4}$ watt carbon except R5.					

Capacitors

C1 175 μ F elect. 16V (120 μ F + 50 μ F in parallel) C2 0.25 μ F polyester

Transistors

2N3702 or OC202 TRI TR2 2N3704 or BFY50 TR3 OC28, OC29, or OC35 2N3704 or BFY50 for positive earth TR4 OC205 for negative earth systems 2N3702 or OC202

TR5 TR6 2N3704 or BFY50

Miscellaneous

Die cast box $4\frac{2}{8}$ in \times $2\frac{2}{8}$ in \times $1\frac{1}{4}$ in Perforated s.r.b.p. 4 in \times 2 in Wire, car connectors

INSTALLATION

The following plan indicates connections to the car for both positive and negative earth systems.

Circuit Pin

A Ignition switch В Indicator switch wiper C Dashboard flasher lamp D Loudspeaker Ē Loudspeaker to chassis

Details are not given for 6V systems since this would need a complete redesign of the whole circuit.

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A.W. 534 20 planes 64×64		
cores/per plane	489.	10.0
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per plane	255.	8.0
Single plane $40 \times 25 \times 4$	\$8.	10.0

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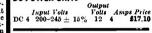
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703, as new	£45. 0.0
V.H.F. "Q" Meter-Marconi	
TF886B	£45, 0.0
Wide Band Millivoltmeter-	
Marconi TR1371	£85,10,0

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Precision—Tinsley 5205C	£55.	0.
Precision Vernier Pot.—Cam-		_
bridge	£65.	
Wheatstone Bridge—Tinsley	£35.	0.

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Cossor 1035	£25. 0.0
Cossor 1035 Mk. III	£35. 0.0
Cossor 1049 Mk. III	£40. 0.0
Solartron CD513.2, CD5238.2—	
LF and Servos, Long Persistent	
tube	\$49,10.
Solartron AD557—Pulse and	
Radar Field	£55. 0,0
Solartron CD711S.2-Double	
Beam DC.7 Meg	£65, 0.0
Mullard L101/3 Double Beam	£99.10,
Furzehill 0-100	£25. 0.
Airmec 723	£19.10.
Airmec 249	£25. 0.

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Portable Single Pen—Record
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Suitable for sleeping, learning, teaching pro-

grammes. Programming machine tools, telephone answering, etc. Complete with replay/record head and separate erase head, iln. tape, twin track tape. Price 23.9.6. P. & P. 7/6.

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SINGLE SPEEU IAFE DELK Driven by 240 50 Hz power supply. Speed 3‡in. per sec. Remote control operation, 3 motors, record/replay heads with separate erase head. Fast erase facilities and ounter. Price \$2.19.6. P. & P. 10/-.

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42 × 52 2K bit ferrite core store complete with 84 OA 10 load diodes. Ideal for building computer store or holding information in binary form. Price \$4,10.0. P. & P. 6/-.

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by Veeder Root. Rotary ratchet type, adds 1 count for each 36° movement of shaft 9/6 + 2/6 P. & P.

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SHUBE
List 28.10.6. Premier Price 26.19.6
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AT78 Stereo List £22.0.0 Our Price £15.0.0
AT7X Elliptical List £25.0.0 Our Price £18.0.0

"NOVA" TRANSISTOR STEREO AMPLIFIER

A superb stereo amplifer offering every facility for the hi-fie enthusiast. Output 10 watts per channel. Frequency response 40-20,000 Hz ± 3dB. Inputs for Radio, P.U. Ceramic, P.U. Magnetic Tape. Separate bases and treble controls, Volume and Balance Controls. Mono/Stereo switch. Also features headphone socket and tape output. Teak case with attractive illuminated front panel. Size 14; 9; 33im., a.c. 200/250V.

WONDERFUL VALUE AT 25 gns. Carr.

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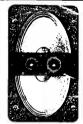
GOLDRING G800 (Stereo)	28.19.6
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RONETTE 106 (Stereo)	£1.15.0
All complete with mounting brack	ets and
instructions. Post and Packing 1/6	each.



the Premier Stereo System consists of an all transistor stereo amplifier, Garrard Model 2025 auto/manual record player unit fitted stereo/mono cartridge and mounted in teak finish plinth with perspex cover and two matching teak finish loudspeaker systems. Absolutely complete and supplied ready to plug in and play. The 10 transistor Amplifier has an output of 5 watts per channel with inputs for pick-up, tape and tuner also tape output socket. Controls:Bass, Treble, Volume, Balance, Selector. Power on/off, stereo/mono switch. Brushed aluminium front panel. Black metal case with teakwood ends: Size 12" × 5½" × 3½" high (Amplifier available separately if required £14.19.6. Carr. 7/6).

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Designed to the highest possible standard. Fitted 21 in speaker units with soft padded ear nuffs, Adjustable headband. 8 ohm impedance. Complete with 6ft lead and stereo jack plug.

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Battery operated - channel audio mixer providing four separate inputs. Size 6 × 3 × 2in. suitable for crystal nicrophone, low impedance microphone with tractice addictage, etc. Max. mput. 15V, max. etc. Max. ping socket inputs, phonoplug socket inputs, phonoplug soutput. Attractive teak wood grain finish case.

grain finish case Mono 59/6

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A must for all tape users! Tape heads become per-manently magnetized with constant use; this leads to background noise that

ound noise that prevents perfect ngs. Simply applied to recording he V313 leaves head free of magieaves head free of ma any tape head in second head the mag-conds. P. & P. 1/6

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pause lever, bias compensator, stylus pressure adjuster, etc. Complete with Sterco/Mono Cartridge. Original Price £25.18.8 OUR PRICE

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Complete with battery and 50ft connecting wire. Compact size, two way call system. Ideal for home, office, factory, etc.

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FOUR STATION INTERCOM. Master unit and 3 slaves. Ideal for office and home. Complete with battery and connecting wire \$7.19.6. P. & P. 5/6.

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C60 (60 min.) 7/6 3 for 21/-C90 (90 min.) 12/6 3 for 36/-C120 (120 min.) 17/6 3 for 51/-

"WELLER EXPERT"
SOLDER GUN.
Saves time and simplifies
soldering in the home and
service dept. Two position
trigger gives instant dual heat.
100/140 watt. 240 volt A.C.

100/140 watt. 240 volt A.C. 67/6 P. & P. 2/-.

POCKET SIZE MULTI TESTER With wide-

SIZE MULTI TESTER With wide-angle, iewelled meter movement, ceramic long-life, low-loss switching, tough impact resisting case. Sensitivity 20,000 ohms/volt d.c. 10,000 ohms/volt d.c. 0,000 ohms/volt a.c. 0-10-50-100-500-1,000 volts a.c. 0-50/A-2-50nA-250mA d.c. 0-5,000 ohms-6 megohms, 10 μ μ F-0-001 mF-1 mF-20 to +22dB. Complete battery, test lead and instructions. **24.19.6** 9, & P. & P.

P. & P. 1/-. CASSETTE HEAD CLEANER

Removes unwanted deposits from delicate tape heads. Fits all cassette recorders.

11/6 P. & P.
1/-.

"VERITONE" RECORDING TAPE SPECIALLY MANUFACTURED IN U.S.A. FROM EXTRA STRONG FRE-STRETCHED MATERIAL. THE QUALITY IS UNEQUALLED.

TENSILISED to ensure the most permanent base. Highly resistant to break-age, moisture, heat, cold or humidity. High polished spike free finish. Smooth output throughout the entire audio range. Double wrapped—attractively boxed.

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TAPE SPOOLS 3" 1/-, 5", 52", 7" 1/9. TAPE CASES 5", 7" 2/6. Post and Packing 3" 1/-, 5", 52" 1/6, 7" 2/-. (3 reels and over Post Free.)



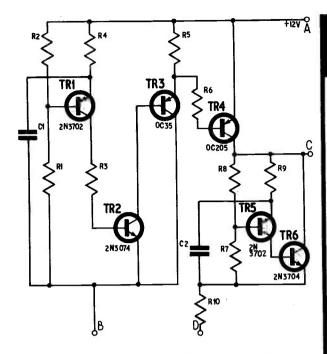


Fig. 4. Alternative arrangement for negative earth systems. Connections from A, B, C, and D to car components are the same as for the positive earth system. TR4 here is an OC205; all other components are as given in the components list

CONSTRUCTIONAL DETAILS

A piece of perforated s.r.b.p. board is trimmed to fit inside a 4in × 2in (internal size) diecast box and is drilled for mounting on four 6B.A. screws. The components are then mounted on the board and connected up as shown in Fig. 3 for positive earth systems, using the termination wires whenever possible. If the circuit in Fig. 4 is used this layout must be modified to suit it.

The 0.25 ohm resistor consists of four 1 ohm wirewound resistors connected in parallel or alternatively a 9in length of 22 s.w.g. eureka wire can be used. It should be insulated with heat resistant sleeving and wound on a small bobbin or former.

Due to the on/off time ratio of about 1:3, the mean current through R5 and the power transistor is less than 1 amp and the power dissipated is less than ¼W and 1W respectively. Hence the heat generated is comparatively low and a heat sink should not be required.

The bleeper circuit is mounted at the opposite end of the board to the main flasher components and miniature components may be required to fit it into the space available. Three leads from pins A, B and C are brought out through grommeted holes to flat male "car connectors". A mounting bracket is screwed to the case to complete the unit—a direct replacement for an electro-mechanical flasher. When the bleeper circuit is used in positive earth systems, the third lead should be connected from pin D to the loudspeaker as shown in Fig. 2; another lead connects the loudspeaker to the positive earth terminal of the car battery.

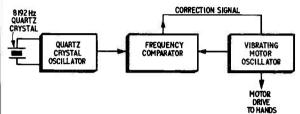
An alternative method of construction with the bleeper circuit is to use a slightly larger case with a small speaker mounted inside it. The unit is then completely self-contained.

NEWS BRIEFS

Ouartz Oscillator Wristwatch

N SPITE of improved timekeeping in modern wrist watches. the Longines company of Switzerland have developed an electronic watch, called the "Ultra Quartz", which is claimed to maintain an accuracy of one tenth of a second per day or less than one minute per year.

It uses a quartz crystal oscillator to control the speed of a vibrating motor by comparison with actual motor speed. The quartz resonator operates at a frequency of 8,192Hz while the vibrant motor oscillator runs at a much lower frequency, 170Hz. The difference signal detected by the comparator is used to stabilise the motor speed.



The electronics comprises 14 transistors, 19 resistors and 7 capacitors which, with the motor drive and 1.35V screw-in battery, is built into a case. Battery life is in excess of 18 months. The watch is not expected to become generally available until late 1970, when it will retail for about £150.

A Register of Engineers

THE organisation of a composite register covering the principal sections of the engineering community is proposed by The Council of Engineering Institutions. Those to be eligible for inclusion in this register are Chartered Engineers, Technician Engineers, and Engineering Technicians.

A Working Party has been set up to implement the intention and its first duty will be to prepare a submission to the Privy Council to get agreement to such modifications to the CEI Charter and By-laws as may be necessary, and then to determine which other interested parties should be invited to collaborate.

The Council of Engineering Institutions embraces all branches of engineering. Its constituent members include the I.E.E. and the I.E.R.E.

Instant Banking

NINE BANKS have commissioned NDPS (GPO National Data Processing Service) to set up and operate a computing system for handling nearly 20 million transactions a year.

Customers' records will be maintained on a large magnetic disc file and will be amended in real time by transactions received from bank branches. The terminals will automatically align the passbook and will print transaction details and new balances in the book while the customer waits, the entire process taking a claimed maximum of five

The system will cover other aspects of TSB work, including the automatic processing of standing orders and savings scheme transactions and the maintenance of customer records.

ELECTRONICS AT THE DUTCH

INTERNATIONAL EXHIBITION

HE 16th biennial Firato International Electronics Exhibition held at the R.A.I. Gebouw in Amsterdam attracts a very large audience. This year colour television was competing heavily with hi fi, electronic musical instruments and home video recording.

One of the highlights of the exhibition was a display of "50 years in sound recording and broadcasting" in which the original transmitter of the first Dutch broadcasting station PCGG was featured.

The Dutch Amateur Radio organisation V.E.R.O.N. were operational with s.s.b. transmitters on 80, 40, and 20 metres and the N.V.G. tape recording and colour slide society were showing the new Philips domestic

video tape recorder in action.

An organisation called "Elektron", which is an information centre for students and others interested in electronics, were also displaying a vast range of equipment, books and literature. Elektron is sponsored by the joint efforts of various Government departments, professional institutions, major electronics companies and industrial and scientific organisations.

SMALLEST TELEVISION

The Firato is a very large exhibition covering even domestic electrical products and although most of the hi fi equipment, electronic musical instruments and other equipment on show were of either British, Dutch, German or Japanese manufacture, there were items being shown for the first time that have not yet appeared in the U.K.

Some of these may have arrived here by the time this report appears in print. For example, what is claimed to be the world's smallest complete television receiver was being shown by the National Company of Japan. This tiny receiver, called the National Panasonic, is operated entirely from an internal battery and has a screen only 25mm $\times 25$ mm.

VIDEO AND TAPE

The Japanese Akai company were showing for the first time a domestic video tape recorder that uses

standard 4in wide tape and converts to a conventional quarter-track stereo recorder. This can be supplied complete with a standard television receiver and video camera and it employs twin rotating heads for video recording and playback.

No details were available regarding video frequency response but recordings from the tape taken off camera were producing pictures as well defined as those from

average television broadcast reception.

Philips also introduced their new domestic video tape. recorder which employs ½in wide tape and a scanning head record/replay system. This too is available complete with camera and a standard television receiver on which video recordings can be reproduced.

Another unusual tape recorder was the Japanese made "Dokorder" which makes copies, hence the four spools as can be seen in the photograph. It has separate tape head sets for recording, replay and copying but employs a common tape drive for both normal recording and the copying facility. The tape drive is a centre capstan system and will run the tape in either direction.

Most of the hi fi equipment on show was the same as that available in the U.K., in fact quite a number of British manufacturers were exhibiting. One novel item however, was a stero headphone set with a built-in f.m. receiver and aerials. This was produced by the Japanese National Company and the receiver covers the normal 87 to 108MHz band. The outfit is battery operated, has a stereo balance control and can also be connected to a hi fi amplifier system.

ELECTRONIC ORGANS

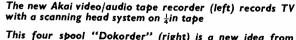
Electronic organs were also attracting a good deal of attention. The Hammond Netherlands NV were demonstrating a completely new series of transistorised Hammond organs with the "tone wheel" sound, but which despite the vast range of voices and facilities, sells in Holland at only £500.

Another novel feature now being incorporated in electronic organs is a tape cassette recorder, which records directly from the organ pre-amplifier or replays via the main amplifier. The new Gawina organ (Dutch made) has this facility and they also supply prerecorded cassette tapes for instructional and practice purposes.

A large annual exhibition on the lines of the Firato might be a worthwhile proposition in this country instead of the many small and separate "trade only" and/or "open to the public" exhibitions now being run

at odd intervals during the year.

F.C.J.



This four spool "Dokorder" (right) is a new idea from Japan, that makes copies of tapes but employs a single tape drive system

The latest from Philips in Holland. A domestic video tape recorder (below) which uses $\frac{1}{2}$ in wide tape and a scanning head system for video recording and playback







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Incaluable to handymen. servicemen, demonstrators, etc.

39/6 P. & P.

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VHF AIRCRAFT BAND CONVERTOR. When placed within 1in. of a MW band radio full coverage of VHF Air-craft Band 108-135Mc/s. can be obtained. All transistor, 9V battery operation. Fully tunable 18jin. × 7 *section tele-scopic aerial. Size 4 × 22 1 jin. 79/6, P. & P. 3/6,



MODEL MAKER'S MOTOR
No. 15EN. Voltage 11-5V.
Current 400mA. Torque
12g.cm. Boly size
11f. long ½ dia.
Shaft ½ long ½ dia.
Shaft ½ long ½ dia.
toys. 5/6 each.
P. & P. 1/3. 3 for 15/-. P. & P. 2/6.



NEW STEREO/MONO HEADPHONES. SDH-7. Soft rubber

SDH-7. Soft rubber earpieces with slide switch for mono/ stereo listening and ind. vol. controls. Impedance 8-16 ohn Freq. response 25-15,000cps. With lead and stereo place and stereo plug. \$6.6.0. P. & P. 3/6.



SINCLAIR IC-10 INTEGRATED CIRCUIT



10 watt Amplifier. Size only 1 \times 0.4 \times 0.2in. A true hl-fi amplifier complete with manual giving details of a wide range of applications and instructions. Guaranteed 5 years. ONLY 59/6. P. \times P. 1/6.

SPECIAL TRANSFORMER FOR OPERATING SINCLAIR IC-10 from A.C. mains 230/250V. Output 13V. at 0.5 amps. 12/6. P. & P. 2/6.

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39 gns.

Carr. & Ins. 25/-.

NEVER BEFORE SUCH VALUE!

Big sound at low cost! 6 watt r.m.s. per channel. Controls: Bass, Treble, Volume, Balance, Function selector. MonofStereo switch. Tape record outlet. Inputs for Tape replay/Tuner. Headphone facility. Beautiful teak case with matched loudspeakers. Garrard Autochanger unit fitted Stereo Cartridge.

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		BRITISH MADE TO	POUALI
J 100 I	3"	Long Play PVC	225ft
J 1002	3*	Triple Play Poly	600ft
J1003	5*	Long Play PVC	900ft
J1004	5"	Double Play Poly	1200ft
J1005	51"	Long Play PVC	1200ft
J1006	51"	Double Play Poly	1800ft
J1007	7.7	Standard Play PVC	1200ft
J1008	7"	Long Play PVC	1800ft
J1009	7-	Double Play Poly	2400ft
J1010	7"	Triple Play Poly	3600ft



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TRANSISTOR STEREO

AMPLIFIER

Microscopes, Binoculars, Telescopes and Watches at 18/19 Tottenham Court Road TTC. C1001 MULTITESTER in leather case.

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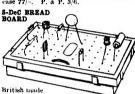
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Overload protection.
20,000 opv. AC volts
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Megohm. Decibels Megohm. Decibels -20 to + 22 dB. Size of meter $4\frac{1}{2} \times 3\frac{3}{4} \times 1$ in. 85/-. P. & P. 3/6.

SHIRA 62D MULTI-

SHIRA 62D MULTI-TESTER 90.000 o.p.v. DC voltage: 5-25-50-250-500-2-2-8K (20,000 ohms per volt). AC Voltage: 10-50-100-500 1000 volts (10,000 ohms per volt). DC Cur-rent: 0-50µA, 0-2-5mA, 0-250mA. Resistance: 6-6K 6-6Mg (300 ohm and 30K at centre scale). Capacitance: 10pf. to -001 mfd, -001µf to -1µF. Decibels: -20 to +22dB. Size 4j 3j -1m. Complete with case 77/-. P. & P. 3/6.



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Panels, Jigs and Accessories and, the book-let "Projects on S-DeC" all contained in a strong attractive plastic case. Ideal for the professional user. 25,17.6. P. & P. 3/6.

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One of the most popular models from the fabulous Teleton range. Incorporates 16 transistors and diodes producing superb quality hls. 10 watts per channel music power. Inputs for Gram (Magnetic and Crystal), Tuner and Auxiliary. Tape Record output. Controls: Volume, Balance, Bass, Treble. Stereo/Mono slides witch. Stereo happhone socket. Attractive offed walnut cabinet with brushed aluminium front panel. List Price 223.7.0

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MT4	150W	31 × 21 × 3in	31b	33/- (P. & P. 6/-)
MT65	200W	$3\frac{1}{4} \times 4\frac{1}{4} \times 4$ in	41b	39/6 (P. & P. 6/-)
MT66	300W	4 < 4 < 33in	6lb Toz	59/4 (P. & P. 9/-)
MT110	400W	42 × 41 < 4in	111b	85/- (P. & P. 10/-)
MT67	500W	51 < 4 41 in	121b 8oz	89/- (P. & P. 10/6)
MT83	750W	41 51 :51in	13lb 4oz	95/7 (P. & P. 10/6)
MT84	1000W	41 < 51 × 51 in	16lb	142/2 (Carr. extra)
MT93	1500W	5 1 5 / 6 in	281b 9oz	170/6 (Carr. extra)
MT94	1750W	5 % × 6 1 × 6 1 in	311b	195/- (Carr. extra)
MT95	2000W	7×61×81in	40lb	211/2 (Carr. extra)
MT73	3000W	67×74×83in	451b 80z	300/- (Carr. extra)
LOW V	/OLTAGI	E 12V RANG	E	
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MT111	0.5A	$3 \times 2\frac{1}{4} \times 1\frac{3}{4}$ in	120z	15/3 (P. & P. 2/6)
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MT115	20A	41×41×4in	111b 13oz	95/- (P. & P. 9/-)
MT187	30A	$51\times41\times41$ in	16lb 12oz	180/- (P. & P. 13/6)

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SP25 less	cart., with base	\$13,10,0
P. & P. D	ecks 12/6, Cover 4/6	. Base 4/6.
P. & P. De	eck/Cover/Base 17/-	

MINIATURE SOLDERING IRON British made and designed for use with transistor circuitry but ideal for many other uses. A.C. 240V, 18W. Length 7& in, 4 in slide on bit. Price 32/6. P. & P. 2/-.



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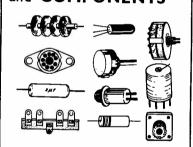
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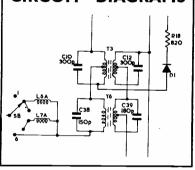


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PART THREE FIRST I.F. MODULE

The circuit diagram of the first i.f. is given in Fig. 3.1. This unit was described in reasonable functional detail in the first article of this series. The following paragraphs should be studied in conjunction with the previously presented material and with the block diagram Fig. 1.4.

CONSTRUCTION

The complete circuit of the i.f. unit (Module 2) is shown in Fig. 3.1. As before the inductors L6, L7 and L8 should be wound first, to the information given in Fig. 3.2. The winding of L7 and L8 is carried out in the following manner: a 12in length of 20 strand 50 s.w.g. wire is doubled and wound onto the bobbin as if it were a single wire. The 11 turns of wire should make up slightly more than one complete layer. Once the wire is in place the bobbin is covered with varnish and allowed to set. The cores are then glued around the bobbin and fixed to the circuit board.

Once the inductors have been completed the circuit board should be constructed in a manner similar to that indicated last month for the r.f. unit. Layout and wiring details for the i.f. module are shown in Fig. 3.3. The construction of the module case was detailed last month.

SETTING UP INSTRUCTIONS

This particular section applies to the constructor who has sufficient equipment to make the necessary measurements listed below. The instruments required are as follows:

- (a) Power supply: 12 volts, 50mA and 2.5V, 5mA.
- (b) 34MHz signal generator capable of delivering ImV into 50 ohms.
- (c) 36MHz signal generator capable of delivering 1V into 50 ohms.
- (d) Valve voltmeter capable of measuring 100μV to 1V at 2MHz to 36MHz.

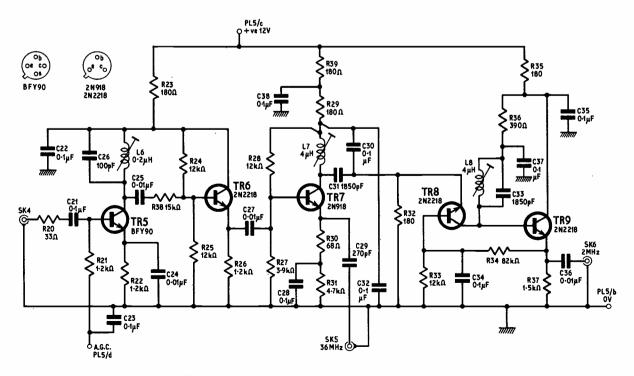
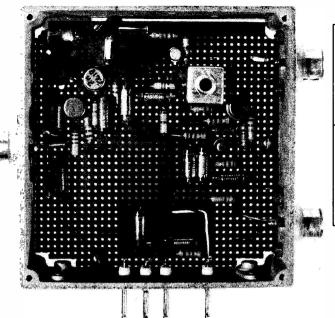


Fig. 3.1. The complete circuit diagram of the i.f. unit



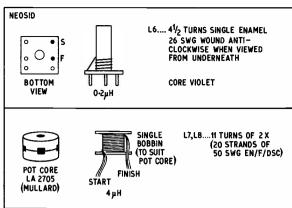
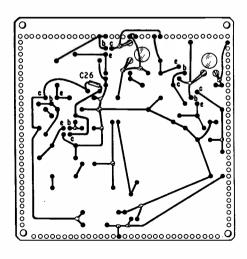


Fig. 3.2. Coil winding details for the i.f. unit

PROCEDURE

Apply the required h.t. potential, ensuring correct polarity, and set the a.g.c. voltage at the incoming terminal (PL5/d) to 2.5 volts. Check all potentials at the base, collector and emitter of each stage to ensure that they correspond with the levels indicated in Table 3.1. Resistor R34 may be adjusted in value if the voltage at the emitter of TR9 is less than eight volts or more than ten volts. Once R34 has been adjusted recheck all the potentials. If the circuit appears to be functioning correctly from a d.c. point of view the a.c. testing can be undertaken as follows.

Apply a 34MHz signal to SK4 and set the level of this signal to 1 millivolt. Connect the valve voltmeter across R27 and adjust L6 for maximum signal. Now apply a 36MHz signal at a level of 400 millivolts to SK5 (this level to be measured when connected to SK5) and transfer the millivoltmeter to SK6. Inductors L7 and L8 should now be adjusted so that a maximum reading is obtained on the meter. Having adjusted the two coils in this latter measurement it is advisable to reduce the input signal of 34MHz by 10dB and readjust coils L6, L7 and L8 for maximum output. If the 34MHz input signal is set so that the output at SK6 is 500 microvolts and the a.g.c. voltage adjusted for maximum output at SK6 by measuring the input signal



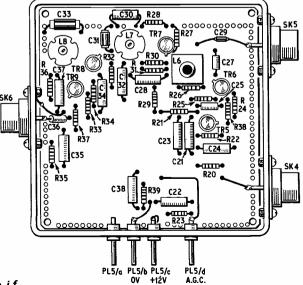


Fig. 3.3. Veroboard layout and wiring details of the i.f. module

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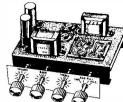
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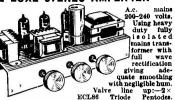
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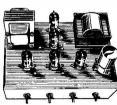
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	R22	I·2kΩ	R29	180Ω	R36	390Ω
	R23	80 Ω	R30	68Ω	R37	1·5kΩ
	R24	12kΩ	R31	4·7kΩ	R38	15kΩ
	R25	12kΩ	R32	180Ω	R39	180Ω
	R26	1.2ks2	R33	12kΩ	1/32	10012
				gh stability	carban	6lm
	Capacit	5 %, 4 VV L	3 44 111	gii stability	Carbon	101111
L	Capacit C21		Dal.		.:1	
		0·1μF		ester or fo		
-	C22	0·1μF	POI	ester or fo) 	
	C23	0·1μF	POI	ester or fo	110	
	C24	0.01μF		amic		
	C25	0.01μ F		amic		
	C26*	100pF	Poly	styrene		
	C27	0·01μF		amic		
ł	C28	$0.1 \mu F$		ester or fo	oil	
1	C29	270pF	Poly	styrene		
	C30	0·1μF	Poly	ester or fo	oi ł	
	C31*	1,850pF	Poly	styrene		
ı	C32	0·1μF	Poly	ester or fo	il	
ı	C33*	1,850pF	Poly	styrene		
1	C34	0·1μF	Poly	ester or fo	il	
ı	C35	0·IμF	Poly	ester or fo	il	
1	C36	0.01µF	Cer	amic		
ı	C37	0·1μF	Poly	ester or fo	il	
ı	C38	0.1 µF	Poly	ester or fo	il	
ı	* The ex	act value	of these	e capacitor	s will d	lepend on
ı	the coi	ls: it may	be nec	essary to a	diust th	e capacity
ł	to suit				•	
ı	Transis	tors				
ı	TR5	BFY90	TR7	2N918	TR9	2N2218
1	TR6	2N2218	TR8	2N2218		
1	Inducto					
ı	L6	0·2μH				
ı	L7	4μH Se	e Fig. 3	.2		
ı	L8	4μΗ		-		
1	Miscella					
1		oard $3\frac{1}{2}\times 3$	14in 0-1	in grid		
1	PL5/a,	b, c, d in	sulated	lead throu	gh con	nectors (4
1	off)					•
		, 6 coaxial	chassis	mounted so	ockets (3 off)

of 34MHz, the overall gain of the unit may be determined. This input level should be in the order of 25 microvolts. The i.f. unit is now complete.

Table 3.1. I.F. UNIT D.C. VOLTAGES

Stage		Voltage	
TR5 V _e		HV	,
V _b	=	2·3V	
V_{e}	==	1⋅8∨	
TR6 V _c	=	HV	
V _b	` =	5·6V	
${\sf V}_{\sf b}^{\sf v}$	` = = =	5V	
TR7 V _c	=	IIV	
V _b	=	2·8V	
V _e		2·1V	
TR8 V _c		9·6V	
V _b		IV	
V _e	=	0·4V	
TR9 V _c		10·5V	
· V _b		9·6V	
Ve	=	9V	

The measurements for TR5 were taken with the incoming a.g.c. voltage set for 2.5 volts at the input terminal. A 20 kilohm per volt voltmeter was used in all the measurements.

Next month: details of further modules

HIGHLIGHTS

OF THE JANUARY ISSUE

THYRISTORS

and the experimenter . . .

Featuring one of the most versatile and important solid state devices now available. The thyristor, or silicon controlled rectifier (s.c.r.), extends the functions of electronic circuits into the field of power control and switching. This article explains the properties of the thyristor and its circuit operation and gives design information and suggested applications.

EMMA HAS GROWN!

During the months following her birth in our March issue, EMMA (Electronic Mime Mobile Animal) has developed a self-preservation awareness—she has learnt to "work" for her keep. EMMA's circuitry has also improved in various other details recently and her new powers will be described in this supplementary article.

TREASURE HUNT?

You can locate hidden metal objects under floors or behind walls with this sensitive inductive detector, or trace the route of buried cables and pipes. As for treasure—well, coins can be found up to six inches away, while larger objects of about half a square foot in size can be detected at distances of up to 18 inches.

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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought.

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LOGICAL STATE INDICATOR

THE circuit diagram in Fig. 1 was designed to enable the logical state of i.c. flip-flops, such as the Motorola MC790P or the Fairchild μ L923 to be determined.

The high input impedance avoids any possibility of the flip-flop outputs being loaded down, which would inhibit their operation.

When the input is at 0V (logical 0 in positive logic system) the lamp is off. When the input is at 3V or so (logical 1) the lamp is on.

L. F. Heller, London, W.4.

ţ.

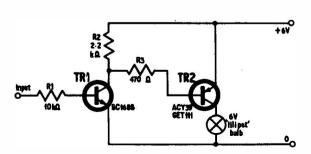


Fig. 1. Logical state indicator circuit diagram

TAPE STOP-FOIL DEVICE

Some years ago, I decided to build a stop-foil device for my tape recorder, and not wanting the machine to draw any current, even the small amount needed to hold the relay down, I devised a latching relay using a small permanent magnet. The applied voltage is derived from the tape recorder 6.3V heater supply, and is rectified and smoothed by D1 and C1 before it is connected to the relay, Fig. 1.

The relay used is a Keyswitch subminiature, type 1051, having a 6V 120 ohm coil, and single-pole changeover contacts rated at 250V 5A continuous load. The diagram in Fig. 2 shows the positioning of the permanent magnet glued to the top of the armature. The foil contacts are arranged as shown in Fig. 3, and only about an inch of foil is actually required.

The permanent magnet has to be mounted so that the polarity of the electromagnet on the relay is opposite to the bottom end of the magnet glued to the armature. Once the relay has been triggered the relay is then held on by the attraction of the permanent magnet, even though the supply voltage has been removed.

Any small type of magnet will suffice, and the beauty of the device is that it effectively turns the whole machine off. The relay is reset manually by pushing a lever connected to the armature as shown in Fig. 2, although an electrical reset is also possible.

T. Price, Pencoed.

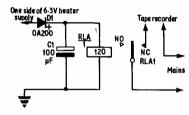


Fig. 1. Tape stop-foil circuit

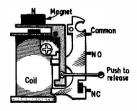


Fig. 2. Positioning of permanent magnet on relay

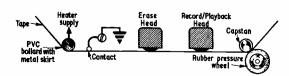


Fig. 3. Contact arrangement of tape stop-foil device

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3 5 7 2 3 2 3 1 2 3 3 2 1	OC81 Type Trans. OC171 Trans. 2N2926 Sil. Epoxy Trans. OC71 Type Trans. 28701 Sil. Trans. Texas 12 Volt Zener 400mW	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 2 1	OC81 Type Trans. OC171 Trans. 2N2926 Sil. Epoxy Trans. OC71 Type Trans. 28701 Sil. Trans. Texas 12 Volt Zener 400mW	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 3 2 1 3 4	OC81 Type Trans. OC171 Trans. 2N2926 Sil. Epoxy Trans. OC71 Type Trans. 28701 Sil. Trans. Texas 28701 Sil. Trans. Texas 12 Volt Zener 400mW 10 A 600 PIV Sil. Rects. 1845R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 1-5 A R63310 AF R8Y95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 PNP High Freq. Trans. NPN 17ans. 1 87141 & 287140 Madt's 2 MAT100 & ZMAT120	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 3 2 1 3 4 3	OCSI Type Trans. 0CSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 FIV Sil. Rects. 1846 R E108 Sil. NPN High Gain Trans. 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. NPN 200Mc/s CSTS80 LOW Noise Ceron. Trans. 4F139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Pred. Trans. AF130 PNP Trans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1 MAT121	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 3 2 1 3 4 3	OCSI Type Trans. 0CSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 FIV Sil. Rects. 1846 R E108 Sil. NPN High Gain Trans. 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. NPN 200Mc/s CSTS80 LOW Noise Ceron. Trans. 4F139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Pred. Trans. AF130 PNP Trans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1 MAT121	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 2 1 3 4 3 4 3 4	OCSI Type Trans. 0CSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 FIV Sil. Rects. 1846 R E108 Sil. NPN High Gain Trans. 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. VCB 100 2NS10 NPN Sil. Trans. NPN 200Mc/s CSTS80 LOW Noise Ceron. Trans. 4F139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Pred. Trans. AF130 PNP Trans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1 MAT121	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 3 2 1 3 4 3 4 3	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 FIV Sil. Rects. 1846 R E108 Sil. NPN High Gain Trans. 2NS10 NPN Sil. Trans. VCB 100 1000 FIV Sil. Rect. 1-6 A R63310 AF BC 200 Sil. Trans. NPN 200Mc/s GCTS80 Low Voice GCrom. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Freq. Trans. AF139 PNP High Fred. Trans. AF139 PNP High Fred. Trans. AF139 MAT101 & 1 MAT121 OC44 Germ. Trans. AF AC127 NPN Germ. Traps.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 3 2 1 3 4 3 4 3	OC81 Type Trans. OC171 Trans. 2N2926 Sil. Epoxy Trans. OC71 Type Trans. 28701 Sil. Trans. Texas 28701 Sil. Trans. Texas 12 Volt Zener 400mW 10 A 600 PIV Sil. Rects. 1845 R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 1-5 A R83310 AF R8Y95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 PNP High Freq. Trans. NPN 17ans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1MAT121 OC44 Germ. Trans. AF AC127 NPN Germ. Trans. MOC44 Germ. Trans. AF AC127 NPN Germ. Trans.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 2 1 3 4 3 4 3 1 1	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 PIV Sil. Rects. 1846R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 1-0 A R53310 AF RSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 FNF High Freq. Trans. NFN Trans. 187141 & 287140 Madt s 2 MAT100 & 2MAT120 Madt s 2 MAT101 & 1 MAT121 Od44 Germ Trans. AF1 AC44 Germ Trans. AF1 AC47 NFN Germ. Trans. 2N18966 Sil. PNP Trans. Motorola	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 2 1 3 4 3 4 3 1 2	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 PIV Sil. Rects. 1846R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 1-0 A R53310 AF RSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 FNF High Freq. Trans. NFN Trans. 187141 & 287140 Madt s 2 MAT100 & 2MAT120 Madt s 2 MAT101 & 1 MAT121 Od44 Germ Trans. AF1 AC44 Germ Trans. AF1 AC47 NFN Germ. Trans. 2N18966 Sil. PNP Trans. Motorola	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 2 1 3 4 3 4 3 1 1	OC81 Type Trans. OC171 Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Volt Zener 400mW 10 A 600 PIV Sil. Rects. 1845 R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 1-5 A R83310 AF R8Y95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 PNP High Freq. Trans. NPN 17ans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1MAT121 OC44 Germ. Trans. CA4 Germ. Trans. AF AC127 NPN Germ. Trans. Sil. Power Rects. BYZ13 Sil. Power Trans. Motorola Sil. Power Trans. MNPN 100Mc/s.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 2 3 1 2 3 3 2 1 3 4 3 4 3 1 2	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 PIV Sil. Rects. 1846R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 15 A R53310 AF RSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. A139 PIN 1814 Feq. Trans. 511 POWN GERM. Trans. AF AC127 NPN GERM. Trans. AF AC127 NPN GERM. Trans. 2N3906 Sil. PNP Trans. Motorola Sil. Power Rects. BYZ13 Sil. Power Rects. BYZ13 Sil. Power Trans. NPN 100Mc/s.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
3 5 7 2 3 3 2 2 3 3 4 3 4 3 4 3 1 2 1	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 PIV Sil. Rects. 1846R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 15 A R53310 AF RSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. A139 PIN 1814 Feq. Trans. 511 POWN GERM. Trans. AF AC127 NPN GERM. Trans. AF AC127 NPN GERM. Trans. 2N3906 Sil. PNP Trans. Motorola Sil. Power Rects. BYZ13 Sil. Power Rects. BYZ13 Sil. Power Trans. NPN 100Mc/s.	10/-10/-10/-10/-10/-10/-10/-10/-10/-10/-
3 5 7 2 3 2 3 1 2 3 3 2 1 3 4 3 4 3 1 2 1 6	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 PIV Sil. Rects. 1846R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 15 A R53310 AF RSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. A139 PIN 1814 Feq. Trans. 511 POWN GERM. Trans. AF AC127 NPN GERM. Trans. AF AC127 NPN GERM. Trans. 2N3906 Sil. PNP Trans. Motorola Sil. Power Rects. BYZ13 Sil. Power Rects. BYZ13 Sil. Power Trans. NPN 100Mc/s.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
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357232312332134343121 62341212	OC81 Type Trans. OC81 Type Trans. 2N2926 Sil. Epoxy Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 P1V Sil. Rects. 1845R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 P1V Sil. Rect. 10 A R63310 AF BSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 PNP High Freq. Trans. NPN 1rans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1MAT121 OC44 Germ. Trans. AF AC127 NPN Germ. Trans. AF AC127 NPN Germ. Trans. Sil. Power Rects. BYZ13 Sil. Power Trans. MPN 100Mc/s. TK201A. Zener Diodes 3-15V Sub-min. 2N1132 PNP Epitaxial Planar Sil. 2N897 Epitaxial Planar Sil. 2N897 Epitaxial Planar Sil.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
357232312332134343121 623412128	OC81 Type Trans. OC81 Type Trans. 2N2926 Sil. Epoxy Trans. 2N2926 Sil. Epoxy Trans. 2S701 Sil. Trans. Texas 2S701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 P1V Sil. Rects. 1845R BC108 Sil. NPN High Gain Trans. 2N910 NPN Sil. Trans. VCB 100 1000 P1V Sil. Rect. 10 A R63310 AF BSY95A Sil. Trans. NPN 200Mc/s OC200 Sil. Trans. GET880 Low Noise Germ. Trans. AF139 PNP High Freq. Trans. NPN 1rans. 1 ST141 & 2ST140 Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 1MAT121 OC44 Germ. Trans. AF AC127 NPN Germ. Trans. AF AC127 NPN Germ. Trans. Sil. Power Rects. BYZ13 Sil. Power Trans. MPN 100Mc/s. TK201A. Zener Diodes 3-15V Sub-min. 2N1132 PNP Epitaxial Planar Sil. 2N897 Epitaxial Planar Sil. 2N897 Epitaxial Planar Sil.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
357232312332134343121 62341212	OC81 Type Trans. OC81 Type Trans. 2N2926 Sil. Epoxy Trans. 28701 Sil. Trans. Texas 28701 Sil. Trans. Texas 28701 Sil. Trans. Texas 12 Voit Zener 400mW 10 A 600 PIV Sil. Rects. 1846 R BC108 Sil. NPN High Gain Trans. NS10 NPN Sil. Trans. VCB 100 1000 PIV Sil. Rect. 16 A R53310 AF R8 Y95A Sil. Trans. VRN 200Mc/s OC200 Sil. Trans. GF 189 NP High Gern. Trans. GF 189 NP High Gern. Trans. GF 180 PNP High Gern. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 PNP High GF 200 Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Trans. GF 200 Sil. Sil. Trans. GF 200 Sil. Sil. Trans. GF 200 Sil. Sil. Trans. Sil. Power Trans. AF AC127 NPN Germ. Trans. Zener Diodes 3-15V Sub-min. Zener Sub-min. Zener Bert Sub-min. Zener Sub-min. Zener Bert Sub-min. Zener Sub-min. Zener Bert Sub-min. Zener Sub-min. Zener Bert Sub-min. Zener Sub-min. Zener Bert Sub-min. Zener Sub-min. Zener Bert Sub-min. Zener Bert Sub-min. Zener Bert Sub-min. Zener Bert Sub-min. Zener Bert Sub-min. Zener Bert Sub-min. Zener Be	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-
357232312332134343121 623412128	OCSI Type Trans. OCSI Type Trans. 2N2926 Sil. Epoxy Trans. 2N2926 Sil. Epoxy Trans. 28701 Sil. Trans. Texas 28701 Sil. Trans. Texas 10 A 600 FIV Sil. Rects. 1846 R EC108 Sil. Trans. VCB 100. 1000 FIV Sil. Rects. 16 A R63310 AF BC108 Sil. Trans. VCB 100. ECT880 Low Trans. NPN 200Mc/s CET880 Low Trans. NPN 200Mc/s Madt's 2 MAT100 & 2MAT120 Madt's 2 MAT100 & 2MAT121 CC44 Germ. Trans. AF AC127 NPN Germ. Trans. 2N3906 Sil. PNP Trans. Motorola Sil. Power Trans. MPN 100Mc/s TK201A. Zener Diodes 3-15V Sub-min. ZN1132 FNP Epitaxial Planar Sil.	10/- 10/- 10/- 10/- 10/- 10/- 10/- 10/-

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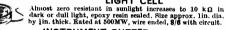
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10 6·4 20 12·5	4 2·5 8 5	1/2 10/6 2	16/6 89/6 13/- 80/3 12/6 77/9		lW;	10 4.3			
125 100 64 250 200 125	40 25 80 50	16 10 32 20	1/ 8/9 1 1/1 9/6 2	.8/9 63/6 10/9 70/9	10% ranges; 10 5% ranges; 4	Ohms to 10 Meg 7 Ohms to 1 Meg	gohnis (E12 Rena gohnis (E24 Rena	ard Series). ard Series).		
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3,200 2,500 1,600	1,000 640 800	400 250 500 320	5/8 46/6 10	1/- 343/9	iw iw	10% 5%	2 d 3 d	1/9 2/-	3/8 4/-	11/7 12/1
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0.068 0.1	8d 9d	5/8 6/6 6/8	11/10 18/6 14/8	37/6 43/9 47/7	AF116 AF117	2/6 2/6	18/9 18/9		15/ 15/	166/3 166/8
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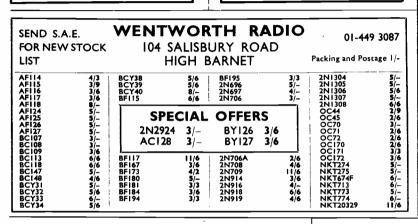
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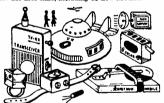
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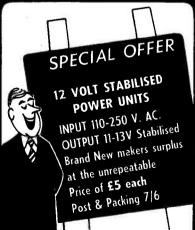
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