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RAPID

EVERYTHING BRAND NEW AND TO EXACT SPECIFICATION • NO SURPLUS GOODS

AMPLIFIER KITS

PEAK SOUND P.W. DOUBLE 12

Complete stereo kit including cabinet, but less panel and other metalwork. £23 net. Available in separate packages as follows: Main amplifier kit £3.19.6 per channel, net. Accessories 19/mono. 36/- stereo

Pre-amplifier kit £1.7.0 per channel, net. Accessories 13/6 mono, 27/3 stereo.

Tone control kit 19/- per channel, net. Accessories 8/9 mono, 22/6 stereo.

Power supply kit £4.10.0 mono or stereo, net.

Cabinet kit £2.12.6 net. Metalwork available separately from other sources, details on request.

30 WATT (designed by Dr. A. R. Bailey). Published May 1968 W.W., modified November 1968 W.W.

Full kit for main amplifier £9.9.6 (less power supply). Transistors only for main amplifier £7.9.6. PC board supplied free with above kit. Heat sinks for output transistors 8/6 extra.

Power supply kit, unregulated, November 1969 circuit £4.14.0. Regulated version, 60V 1 6A or 0 8A, current limiting, re-entrant characteristic: does not need re-set button £8.10.0. Transformer only: 0-25-45-50V 2A 58/-.

8 x 8 watt Stereo only. Peak Sound SA 8 x 8 kit. Sensitivity 50mV into 1 M Ω , output into 5 Ω . Complete with cabinet and power supply. Kit complete £16.10.0 net. Built and tested £21 net.

BARGAINS IN BRAND NEW FIFCTRONIC COMPONENTS

Ultra low-noise resistors (under $0.1 \mu V/V$) Electrosil TR5: Metal oxide, 2% tolerance, range 10Ω to $1M\Omega$. All values in E24 series available. $\frac{1}{2}W$ rating, 1–24 10d, each; 25–99 9d, each; 100 up 8d. each. (Ohmic values may be mixed to obtain quantity price.) Potentiometers, carbon track, long plastic spindles: Single gang linear 220 Ω to 2-2M Ω 2/6 each; log 4-7K Ω to 2-2M Ω 2/6 each. Dual gang stereo-matched lin or log 10K to 1M Ω 8/6 each. Stereo balance log/anti-log 10K, 47K, 1M Ω only, 8/6 each. All types available with ½ A D.P. switch 2/3 extra.

TRANSISTORS, etc.

2N696	5/6	2N3704	3/9	BC107	3/6	BFY51	4/3
2N697	6/-	2N3705	3/5	BC108	3/-	MC140	6/3
2N706	3/5	2N3707	4/-	BC109	3/6	MJ480	21/-
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2N1303	4/-	2N4286	2/11	BC126	12/-	MJ491	31/-
2N1304	4/-	2N4289	2/11	BC148	3/3	MPF103	11/6
2N1305	4/	2N4291	2/11	BC149	4/3	MPF105	7/6
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2N3055	16/6						5/9
2N3702	3/6	AD161 \	14/-	BFX88	7/9	TPMD	
2N3703	3/3	AD162 S	pr.	BFY50	4/9	(= ORP12)	6/-

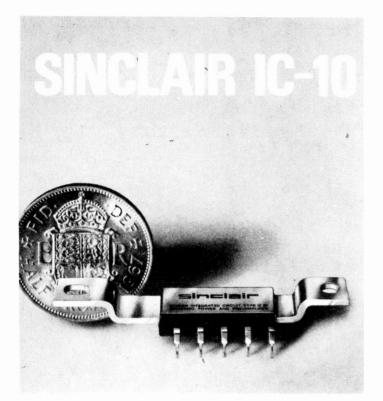
Large capacitors, high ripple current types. $2000\mu F$ 25V 7/-; $2000\mu F$ 50V 9/3; $5000\mu F$ 25V 10/3; $5000\mu F$ 50V 17/6. S-DeC 30/6; 2-DeC DeCstore 69/6; 4-DeC 119/6.

- DISCOUNTS (on all but net items): 10% for total order value of £3 or over. 15% for total order value of £10 or over.
- POSTAGE and packing: on orders up to £1 add 1/-. Over £1 post free in U.K. Overseas orders welcomed: carriage charged at cost.
- CATALOGUE gives further details of above products and much information on semiconductor characteristics etc. 1/6 post free.

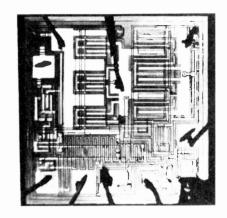
ELECTROVALUE

(Dept. P.E.11)

ST. JUDES ROAD, ENGLEFIELD GREEN, EGHAM, SURREY Tel: Egham 5533



10 WATT MONOLITHIC INTEGRATED CIRCUIT AMPLIFIER AND PRE-AMP



theworld's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output power of 10 watts. It contains 13 transistors (including two power types), 2 diodes, 1 zenor diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.

The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of the usual tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required for producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. It also enables us to give a 5 year guarantee on each IC-10 knowing that every unit will work as perfectly as the original and do so for a lifetime.

■ SPECIFICATIONS

10 Watts peak, 5 Watts R.M.S. continuous. Output 5 Hz to 100 KHz±1dB. Frequency response Total harmonic distortion Less than 1% at full output. 3 to 15 ohms. Load impedance 110dB (100,000,000,000 times) total. Power gain Supply voltage 8 to 18 volts. $1 \times 0.4 \times 0.2$ inches. Size Sensitivity 5mV Adjustable externally up to Input impedance 2.5 M ohms.

CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

■ APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

IC.10

with IC.10 manual and 5 year guar**59**/₆

POST FREE



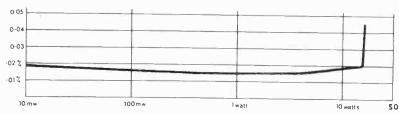
SINCLAIR RADIONICS LIMITED 22 NEWMARKET ROAD CAMBRIDGE Tel. 0233-52731



Z.30

THE WORLD'S LOWEST DISTORTION HIGH FIDELITY AMPLIFIER.

For four years, the Sinclair Z.12 dominated the constructor world, being the best selling unit of its kind this side of the Atlantic. Excellent as it was, the new Sinclair Z.30 is still better. Half the size of the Z.12, it has more than twice the power, very much greater gain and a level of distortion 50 times lower. This incredible figure results from using over 60dB of negative feed back with a constant current load to the driver stage obtained by incorporating a two transistor circuit in place of the more usual bootstrapping. 9 silicon epitaxial planar transistors are used to provide enormous power; up to 25 watts RMS sine wave (50 watts peak). The circuitry of this marvellous amplifier allows it to be operated from any voltage from 8 to 35 to perfection. At all output levels, distortion is only 0.02%. This puts true laboratory standards into the hands of every user of a Z.30. Two Z.30s and a new Stereo Sixty will make a stereo assembly of such perfection that it could not be bettered in its class no matter how much you spent. But the Z.30 has an enormous variety of applications, particularly where quality, precision and reliability are essential. It can also be used entirely on its own as an amplifier for an efficient economy record player.



Ready built and tested, with Z.30 Manual, postfree (except air mail) 89/6

sinclair

SPECIFICATIONS

Power output—15 watts R.M.S. sine wave (30w peak) into 8 ohms using 35 volts supply; 25 watts R.M.S. sine wave (50w. peak) into 3 ohms using 30 volts supply.

Frequency Response—30 to 300,000 Hz \pm 1dB.

Input sensitivity-250mV into 100K ohms.

Distortion—0.02% total harmonic distortion at full output into 8 ohms and at all lower output levels.

Signal-to-noise ratio-better than 70dB unweighted.

Power requirements—from 8 to 35 V.d.c.

Output stage—Class AB.

Size-3½ x 2¼ x ½ ins.

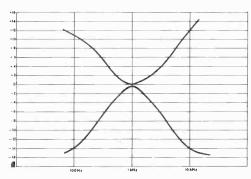
Damping factor—better than 500.

APPLICATIONS—Hi-fi amplifier; car radio amplifier; record player amplifier fed directly from pick-up; intercom; electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the Z.30.

Loudspeaker Impedances—3 to 15 ohms.

SINCLAIR RADIONICS LIMITED 22 NEWMARKET RD., CAMBRIDGE Tel: 0223 52731





Ready built and tested, with instructions, post free

£9.19.6





This attractive and completely new unit is intended for use with two new Z.30 amplifiers to provide the finest possible standards of stereo reproduction. Four press buttons and four rotary controls are used to provide on-off, three input selectors and Volume, Bass cut/boost, Treble cut/boost and Stereo balance. The on-off button also switches the power amplifiers. The front panel in brushed aluminium is flush mounted to the cabinet front, it being necessary only to drill holes to accommodate the controls. Rear adjustable brackets hold the chassis tight to the cabinet. The very latest ganged rotary controls are used to afford compactness and extra long working life free from noise.

The Stereo-60 may also be used with 2 IC-10's or any other high performance amplifiers.

Frequency range : Radio & Aux. 20-25,000 Hz \pm 1dB Pick-up corrected to within \pm 1dB for R.I.A.A. equalisation.

Inputs: Radio, pick-up (magnetic, ceramic or crystal), Auxiliary.

Overload factor: >20dB per channel on all inputs

Distortion: 0.03%

Signal to noise ratio: Better than 70dB unweighted Controls: press buttons for on-off, P.U.

press buttons for on-off, P.U. radio and aux. Treble +15dB to —15dB at 10kHz. Bass +15dB to —15dB at 100Hz. Volume.

Stereo Balance.

Size: $8\frac{1}{4}$ " x $1\frac{1}{2}$ " x 4" from front to back, plus knobs.

Finish: Brushed aluminium with black titling, knobs and press buttons.

PZ.5 POWER SUPPLY UNIT

A new heavy duty mains power supply unit designed specially to drive two Z.30s and a Stereo Sixty. New compact design. For AC Mains, 200-240V/50Hz. £4.19.6.

USE THIS COUPON FOR 2.30.STEREO 60 AND P.2.5

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SINCLAIR MICROMATIC the world's most successful miniature radio

Considerably smaller than an ordinary box of matches, this is a multi-stage A.M. receiver meticulously designed to provide remarkable standards of selectivity, power and quality. Powerful A.G.C. is incorporated to counteract fading from distant stations; bandspread at higher frequencies makes reception of Radio 1 easy at all times. Vernier type tuning plus the directional properties of the self-contained special ferrite rod aerial makes station separation much easier than with many larger sets. The plug-in magnetic earpiece which matches exactly with the output provides wonderful standards of reproduction.

Everything including the batteries is contained within the attractively designed case. Whether you build your Micromatic or buy it ready built and tested, you will find it as easy to take with you as your wristwatch, and dependable under the severest listening conditions.

Specifications

Size: $1\frac{13}{16}$ " $\times 1\frac{7}{16}$ " $\times \frac{1}{2}$ " (46 \times 33 \times 13mm).

1 oz. (28·35gm) approx.

Tuning:

Medium wave band with bandspread at higher frequency

Earpiece.

Magnetic type.

Black plastic with anodized aluminium front panel, spun

Complete kit incl. earpiece, case, solder and instructions in fitted pack.

Ready built, tested and guaranteed, with earpiece.

Plus 1/1d, P.T. surcharge Mallory Mercury Cell RM675 (2 required) each 2/9d.

USE THIS COUPON FOR MICROMATIC AND Q.16 ORDERS

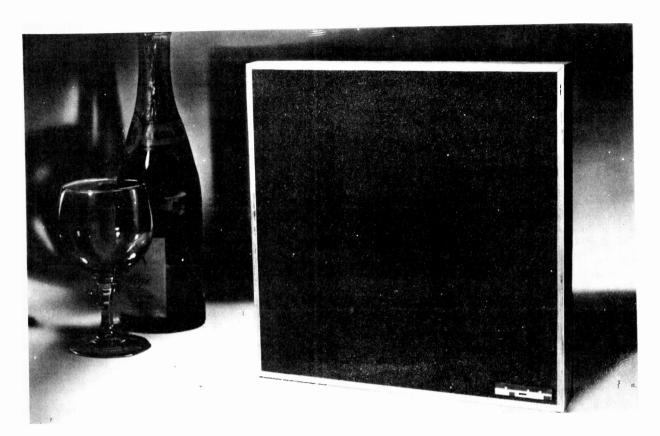
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SINCLAIR RADIONICS LTD. 22 NEWMARKET ROAD

CAMBRIDGE

Tel: 0223 52731



new elegance in a loudspeaker of outstandingly fine performance

All the superb features which went to make the Sinclair Q.14 have been incorporated in the new Q.16 which gives an exciting new opportunity for you to match your Sinclair equipment with modern decor. Employing the same well proven acoustic system in which materials, processing and styling are used in such a radical and successful departure from conventional design, the new Q.16 presents an entirely new appearance with its attractive teak surround and all-over special cellular foam front chosen as much for its appearance as for its ability to pass all audio frequencies without loss. The Q.16 is compact and slim. Its new styling makes it eminently suitable for shelf mounting, but it is no less versatile than its famous predecessor. Listen to a pair of Q.16s in stereo and marvel at the standards of quality and clarity they give.

The Q.16 will handle loading up to 14 watts R.M.S. and presents an 8 ohm impedance to the amplifier output. Frequency response extends from 60 to 16,000 Hz. with exceptional smoothness. A specially designed driver system is used in a sealed and contoured pressure chamber to ensure good transient response at all frequencies. Size: 9¾" square × 4¾" deep from front to back

£8.19.6

SINCLAIR GENERAL GUARANTEE

Should you not be completely satisfied with your purchase when you receive it from us, return the goods without delay and your money will be refunded in full, including cost of return postage, at once and without question. Full service facilities are available to all Sinclair customers.

SINCLAIR RADIONICS LIMITED

22 NEWMARKET RD., CAMBRIDGE Tel: 0223 52731



TMK METER KITS ANOTHER LASKY'S EXCLUSIVE

These two meter kits by TMK offer the unique opportunity of building a really first-class precision multimeter at a worthwhile saving in cost. The cabinets are supplied with the meter scale and movement mounted in position; the Model 200 also has the range selector in position. The highest quality in components and 1% tolerance resistors are used throughout. Both offer professional standards of accuracy. Supplied complete with full constructional, circuit and operating instructions.

20,000 O.P.V. Multimeter.

Large 3 < 2in meter. Full scale acuracy: DCV and current: ±2%, ACV: ±3%, resistance ±3%. Special 0-6V DC range SPECIFICATION

SPECIFICATION

■ DCV: 0-0-6-30-120-600-1,200V at 20K/OPV. ■ ACV: 0-6-30-120-600-1,200V at 20K/OPV. ■ DC Current: 0-0-6-8-01-20-600-1,200V at 10K/OPV. ■ DC Current: 0-0-6-8-60-600mA. ■ Resistance: 0-10K-100K-1M-10M/ohms (88-580-58K-58K at mid-scale). ● Capacitance: 0-002-0-20V (AC 6V range). ■ Decibels - 20 to +634B. ● Output: 0-05uf blocking capacitor. Uses two 1-5V (U.7 type) batterles. Black bakelite cabinet—Size 5½ 3½ 1 1¼in. Complete with test leads.



LASKY'S PRICE 85/-

Post 3/6

50,000 O.P.V. FEATURING 57 MEASUREMENT RANGES **MODEL** 5025

Uses an entirely new range selection mechanism which permits the use of a really large meter in a more compact cabinet. The range selected is clearly indicated on the actual meter face. High speed rotary range selection knob; also features polarity reversal switch, shielded meter movement with overload protection circuit; Special uA and mA measurement ranges.

measurement ranges.

SPECIFICATION DCV: 0-0-25-2:5-10-50-250-1.000V at 25K/OPV. 0-0-125-1-25-5-0-250-125-500V at 50K/OPV. ACV: 0-3-10-50-250-1200V at 50K/OPV. 0-1:5-0-25-125-500V at 50K/OPV. 0-1:5-0-25-125-500V at 250mA. DCMA: 0-2-5-25-250mA at 250mV. DCMA: 0-2-5-25-250mA at 250mV. DC Amps: 0-5-0-50-500MA at 250mV. DC Amps: 0-5-0-500MA at 250mV. DC Amps: 0-5-0-500MA at 250mV. Cesistance: 0-10M/ohms. Output: Capacitor (0-1uF, 400Vw) in series with ACV ranges. Decibels: -20 to +81-5db. Operates on two 15V batts. Black bakelite cabinet, size 5i < 6i 2 2in. Complete with test leads.



ALSO AVAILABLE READY BUILT AND TESTED £13.10.0. Post 5/-

LASKY'S PRICE £10.10.0 Post 5/-

Jarrard SP.25 Mk II

4-speed single player—less cartridge



LASKY'S PRICE £11.19.6 Post 5/-

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1025 less cartridge	£6	9	6	
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	£35	0	0	
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SINGLE PLAYERS AP75 with AD76K magnetic cartridge £21 AP75 less cartridge . £18 10 0 SRP22 Mains model less cartridge £6 12 10 TRANSCRIPTION DECKS 401 £28 10 0 GARRARD BASES: WB1 \$3, 6, 11; WB4 Mk, II \$5, 8, 11; WB5 \$5, 8, 11, CLEARVIEW PERSPEX COVERS: SPC1 23, 5, 0 SPC4 Mk. II 24, 6, 6.

NEW EXPERIMENTAL AND EDUCATIONAL CIRCUIT

SYSTEM

The **DENSHI BOARD** system enables the young experimenter and electronics hobbyist to produce a wide range of transistor circuits a wide range of transistor circuits of increasing sophistication—without soldering or the use of any tools at all I Basically the system comprises a slotted circuit board into which plug-in components and bridge pieces are set to produce up to 30 different circuits. The components are encapsulated in transparent plastic blocks bearing the appropriate circuit symbol and value thus enabling even the complete novice to visually grasp the fundamentals of circuitry after only a few moments study. In only a few moments study. In addition each DENSHI BOARD KIT comes complete with an 80 page manual of circuits and data.



THESE ARE JUST A FEW OF THE CIRCUITS YOU CAN BUILD IN MINUTES; VARIOUS RADIO RECEIVERS, AMPLIFIERS, MORSE CODE PRACTICE DEVICE, CONTINUITY TESTER, SIGNAL INJECTOR, SIGNAL TRACER, WIRELESS MICROPHONE, ETC., ETC.

DENSHI BOARD KIT SR-IA comprises:

Base board; tuner block; 4 resistors; choke coll; transformer; 28A transistor for RF;
2 diodes; 3 capacitors; battery block; morse key; antenna lead; crystal earphone; various bridge and connecting pieces and 80 page manual. This kit permits the building of 16 basic circuits.

LASKY'S PRICE £4.19.6

DENSHI KIT SR-2A as SR-1A with these additional parts: 28B transistor for AF; 2 resistors; 1 capacitor; crystal microphone; test probes; electrode; additional connecting pieces; 9V battery. This kit permits the building of 30 circuits

LASKY'S PRICE £7.2.6 Post 3/6

 $oldsymbol{EXCLUSIVE}$ FIRST THE IC-403 INTEGRATED CIRCUIT AMPLIFIER

MODULE AVAILABLE NOW!

These tiny modules—size only 25 × 10 × 5 millimetres

represent the most amazing breakthrough in circuit
design since the introduction of the transistor. The actual circuit—no bigger than a pinhead—is encapsulated in solid plastic fused with the heatsink and connecting pins to make
an almost indestructible unit. The IC-403 is an integrated power and pre-amplifier requiring
only the addition of tone and volume controls, power source and speaker to form a complete audio amplifier of 3W output. Originally developed for computer and space projects—
there are many applications for these unique devices, wherever high efficiency and utilar
compact size is required, i.e. miniature P.A. and audio amplifiers, intercoms, electronic
organs, tape recorders, etc., etc.

SPECIFICATION (ratings at 20°C): Output power typically 3W from 250mN/ imput
Prequency response 20 Hz to 80KH±±3dB. Power amp. distortion 0.3% (at IW, 400Hz).

Pre-amp. gain 24dB. Power amp. gain 26dB. Max operating voltage 21V. Min. operating
load 7-5. Noise level—75dB. Pre-amp, input imp. 2m/ohms. Pre-amp and power amp.
D.C. Input current 50N.A.

THE IC-403 IS AVAILABLE FROM STOCK EXCLUSIVELY FROM LASKY'S -COMP. WITH INS. DATA AND SUGGESTED CIRCUIT APPLICATIONS

LASKY'S PRICE 4:9/6 Post 1/6. 2 for 95/- Post free Also available SINCLAIR IC10 59/6 Post free.

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SCOOPS

THE WORLD'S SMALLEST 6 TRANSISTOR TWO WAVE-RAND RADIO RECEIVER FROM RUSSIA

THE **ASTRAD** ORION



The Orion is supplied fully built and tested complete with battery, left and right fitting earphone supports and attractive black and ivory plastic presentation/earrying case (matching the Orion). Never miss your favourite music, sport, news—the Orion is an ideal gift for all, providing a constant source of enjoyment without disturbing is an ideal gift for all,

LASKY'S SCOOP PRICE

39/6

Post 2/6 Extra rechargeable

*NOTE: The battery we supply with the Orion is a rechargeable type. Charger units are available enabling you to recharge the battery from AC Mains 220/240V supply. Frice 19/5—post free with radio—otherwise 2/-.

FOSTER "Criterion" Mk II

2 SPEAKER TWO WAY BOOKSHELF SPEAKER SYSTEM

Another high quality sub-miniature bookshelf system from Foster. The "Criterion" Mk II is a sealed infinite baffle type enclosure using 5½in bass/mid-range woofer with rolled cloth edge and a 2½in HF cone type tweeter. The compact cabinet is constructed of in laminate with handsome oiled walnut veneer finish and black woven acoustic gauze front panel with satin chrome edge insert. SPEC: Frequency range 90-20,000Hz. Power handling 10 watts. Impedance 8 ohms. HF rossover. Screw tag connections at rear, Size 12½ × 7½ × 6½ in. The performance of the "Criterion" is superior to many larger and more expensive units and at Lasky's exclusive price offers absolutely unbeatable value



Lasky's Price £9-10 or 2 for £17-10 Post: 1 7/6, 2 10/-

TTC MODEL C-1000

A really tiny 1,000 O.P.V. pocket multi-tester with "big" meter performance. Precision 2 jewel meter movement. Hand calibrated to ±3% accuracy on full scale of DC ranges, 4% on AC ranges. 2½in square meter. SPECI-FICATIONS AC/V ranges: 0-10, 50, 250, 100V at IK/O.P.V. DC currents: 0-1-100mA. Resistance: 0-150K/ohms (3,000 ohms centre resistance: 0-130x/somm (3,000 somms centre scale). Decibels: -10 to +22dB. Operated on one penlight cell. Two colour buffgreen case—size only $3\frac{1}{2} \times 2\frac{1}{2} \times 1$ in. Click stop range selection switch. Ohms zero adjust-Complete with test leads, battery and instructions with circuit data.



LASKY'S PRICE 39/6 Post 2/6

KCELITI

Precision made hand tools for the professional



PLIERS



69CG Radio - TV Pliers 70CG Flat Nose Pliers 71CG Round Nose Pliers

72CG Chain Nose Pliers 73CG Tip Cutting Pliers 74CG Diagonal Close Cutting Pliers

A complete range of miniature lightweight pliers especially designed for holding, bending, shaping and cutting of fine wires in electronic, Radio/TV, electrical and jewellery work.



SEIZERS

32H 5" Straight Nose Junior 5" Seizer 35H 5" Curved Nose Junior 5" Seizer

42H 6" Straight Nose Seizer 43H 6" Curved Nose Seizer

Box joint construction, two position snap on lock. Precision machined from perfectly tempered steel. Holds like surgical clamp and acts as heat sink. Straight or curved nose, in 5" and 6" sizes.

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for fast, easy, reliable soldering

Contains 5 cores of non-corrosive flux, instantly cleaning heavily oxidised surfaces. No extra flux required.

SAVBIT ALLOY ALSO REDUCES COPPER BIT WEAR.

Ecomically packed for



general electrical and electronic soldering, 90 ft. 18 gauge on plastic reel. Recommended retail price 15/-

THIN GAUGE SOLDER. **ESSENTIAL FOR**

soldering small components and thin wires. High tin



content, low melting point, 60/40 alloy, 202 ft. 22 gauge on plastic reel. Recommended retail price 15/-

A RANGE OF SOLDERS IN HANDY DISPENSERS.

REF. ALLOY SWG

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15 60/40 22 3/-4 *Recommended Price

INVALUABLE FOR STRIPPING FLEX, THE NEW AUTOMATIC **OPENING BIB WIRE STRIPPER** AND CUTTER, easily

adjustable for all standard diameters. Plastic covered handles can also be used as wire cutter. Recommended retail price 8/6



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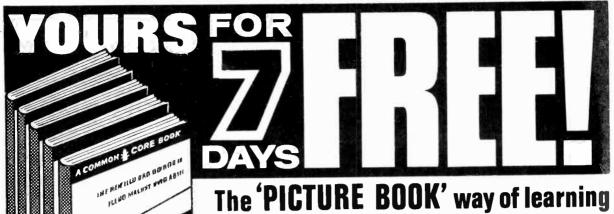
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input is correct to within + 2dB (R.I.A.A.) from 20Hz to 20KH·
Tone Control Ronge: Boss: 13dB at 60Hz. Treble: ±14dB at 15KHz. Total Distortion: (for 10 watt output) <1-5%. Signal Noise: <-60dB. A.C. Mains
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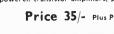


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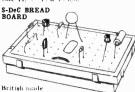


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100-500 1000 volta (10,000 ohns per volt). DC Current: 0-50µA, 0-250µA, 0-250µA, 0-250µA, 0-250µA, 0-250µA, 0-250µA, 0-260µA, 8-esistance: 0-68K, 0-5Mg (300 ohns and 30K at centre scale). Capacitance: 10µL to -001 µdA, -001µf to -1µF. Decibels: -20 to +22dB, 81ze 4j 34 lin. Complete with case 77/-, P. & P. 3/6.



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MT64	75W	21 : 21 × 21 in	11b 14oz	21/9 (P. & P. 4/6)
MT4	150W	31 21 3in	31b	33/- (P. & P. 6/-)
MT65	200W	31 ~ 41 × 4in	4lb	39/6 (P. & P. 6/-)
MT66	300W	4 4 37in	6lb 7oz	59/4 (P. & P. 9/-)
MT110	400W	41 - 41 - 4in	1.11b	85/- (P. & P. 10/-)
MT67	500W	51 4 41in	121b 8oz	89/- (P. & P. 10/6)
MT83	750W	41 51 5tin	131b 4oz	95/7 (P. & P. 10/6)
MT84	1000W	41 - 51 - 51 in	161h	142/2 (Carr. extra)
MT93	1500W	5 } - 5 } - 6∤in	281b 9oz	170'8 (Carr. extra)
MT94	1750W	5 4 - 61 - 61 in	311b	195 - (Carr. extra)
MT95	2000W	7 64 84in	4016	211/2 (Carr. extra)
MT73	3000W	61 - 74 - 81in	451b 8nz	300/- (Carr. extra)
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LOW VOLTAGE 12V RANGE

rrunary	200-200 V .	accommany 124		
MT111	0.5A	3 21 - 11in	12oz	15/3 (P. & P. 2/6)
MT71	2 A	21 21 2110	11b	19/~ (P. & P. 3/9)
MT69	4 A	31 21 × 21 In	215 4oz	28/- (P. & P. 6/-)
MT70	6A	4 3 × 31 in	31b 12oz	39/- (P. & P. 6/-)
MT72	10A	31 - 41 - 4in	6lb 3oz	51/- (P. & P. 9/-)
MT115	20A	41 41 4in	111b 13oz	95/- (P. & P. 9/-)
MT187	30A	ā≟×4₹ <4₹in	16lb 12oz	180/- (P. & P. 13/6)

LOW VOLTAGE 24V RANGE

Primary	200/250V;	secondary 24V				
MT58	1A	$21 \times 21 \times 21$	11b 702	23/9 (P. &		
MT114	3.A	$24 \times 3 \times 3$ in	31b Soz	38/- (P. &		
MT72	5.4	4 < 37 × 31 in	51b 12oz	53/10(P. &	₹°.	fi/-)
MT17	8.4	41 × 31 × 4in	71b 8oz	72/7 (P. &		
MT115	10A	$4\frac{3}{4} \times 4\frac{1}{4} \times 4$ in	111b 13oz	95/- (P. &	P.	l 1/-)

LOW VOLTAGE 30V RANGE

Primary	200/250V:	secondary tapped 12-					
MT112	0.5A	$3\frac{1}{4} \times 2\frac{7}{16} \times 1\frac{1}{16}$ in	11b 4oz		(P. &		
MT79	1.4		21b		(P. &		
MT20	3A	4 31 31 in	41b foz	46/2	(P. &	P. 6	(-)
MT51	5.1	47 × 31 × 4in	61b 8oz	60/9	(P. &	P. 9	(-)
MT88	8A	51 / 31 × 44 in	91b 6oz	92/4	(P. &	P. 11	/-)
MT89	10A	51 < 4 × 41in	121b 2oz	103/6	(P. &	P. 11	/-)

LOW VOLTAGE 50V RANGE

Primary	200-250V;	secondary tapped	19-25-33-40-50V				
MT102	0.5.A	21 21 21 in	11b 11oz	21/3	(P. &	Ρ.	6/-)
MT104	2 A	4 = 31 × 38in	51b	45/8	(P. &	P.	6/-)
MT 106	4.4	41 > 41 > 4			(P. &		
MT118	8.A	51 < 51 < 41in			(P. &		
MT119	10A	61 ~ 41 × 61 in	191b 12oz	165/-	(P. &	Р.	15/6)

		GE 60V RAN					
Primary	200/250V:	secondary tapped	24-30-40	-48 - 60 V			
MT124	0.5A	$31 \times 21 \times 21$ in	21b	4oz	24/- (P. A		
MT127	2.4	4 - 31 / 33in	51b	Boz	52/10(P. &		
MT123	4.4	41 31 41in	101b		99/- (P. &		
MT199	10.4	61 × 5 × 61 in	931b	207	152/- (Carr	. ext	ra)

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				Size	rricer	or t.
MTIAT	250-0-250V	80M A	6-3V 3-5A 5/6-3V 1A 31	- 3 × 3in	33/-	6/-
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MT110	250-0-250V	120MA	6-3V 3-5A 5/6-3V 1A 4	4 3 in	44/9	6/~
MTIIAT	300-0-300V	100MA	6-3V 3-5A 5/6-3V 1A 4	31 - 31in	37/9	6/-
MT12AT	300-0-300V	120MA	6-3V 4A 5/6-3V 1A 4	31 - 31 in	46/2	9/-
MT33AT	300-0-300 V	150	6-3V 4A 5/6-3V 1A 4	4 - 31 in	59/4	9/-
MT2AT	350-0-350V	80	6-3V 3-5A 5/6V IA 4 -	31 - 31in	38/6	6/-
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Primary vo	tage 200-2	250V; secondary 6	-12V	
MT77	1.4	21 <21 · 21 in	Hb foz	15/~ (P. & P. 4.6)
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MT146	8A	$3\frac{1}{4} \times 4 \times 4$ in	61b 4oz	75/~ (P. & P. 9/~)
MT49	9.A	41 < 31 × 4in	71b 8oz	99/- (P. & P. 9/-)
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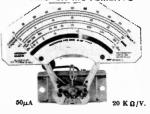
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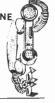
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No. 11 VOL. 5 November

PRACTICAL ELECTRONICS

A SUBSTITUTE FOR STEREO?

STEREOPHONIC reproduction from records is well established, and home performance of orchestral works can attain a state of near-perfection, assuming the various pieces of equipment that make up the complete audio system are selected with care and installed properly.

This much is known, and generally appreciated. However, despite these merits, it is open to question whether stereo in its present form is the definitive method for high quality reproduction in domestic settings. The realism of instrument placing is of limited significance in the absence of actual concert going experience. As the home audience continues to grow, so it must include an ever increasing proportion of listeners whose musical experience is confined to broadcast and recorded works. And, in any case, why assume that the concert hall style of presentation is the most appropriate for the intimate character of a domestic room?

At present electronics is being used to help synthesise a traditional style of performance originated under totally different circumstances to those under which it is later reproduced. True, there are certain exceptions, and experimental works have been performed and recorded, but mainly in the field of popular music.

If all this sounds like heresy to the classical music devotee, let him be assured that this is not some whimsy conjured up by electronics-obsessed eccentrics. Such progressive thoughts have already occurred to some members of the musical world. And the subject was given fresh airing a few weeks ago by Leopold Stokowski. During an interview on BBC Television, this eminent conductor and authority on recorded music re-stated his opinion that stereo is not the ultimate solution.

As one possible advance, Stokowski envisages the home audience seated in the centre of the room with music emanating from loudspeakers situated in the four corners. The intention is to place the audience, in effect, right among the performers. It is a fascinating concept for home listening in the electronic age.

How such an idea could be achieved artistically and technically is not clear at this stage. Certainly difficult problems would have to be solved to make this a practical proposition. The mind boggles at the complexity of a four-channel system. At anyrate, it is worthwhile remembering that such a futuristic idea based upon an awareness of electronic processes and potentialities should have come from a musician. Also, it is encouraging to learn there need be no ideological conflict between art and science where music is concerned.

F. E. Bennett—Editor

THIS MONTH

CONSTRUCTIONAL PROJECTS 810 I.C. BASIC AMPLIFIER 812 I.C. STEREO AMPLIFIER 830 P.E. ORGAN—7 P.E. COMMUNICATIONS 838 RECEIVER—2 844 TIME LAPSE CINE SPECIAL SERIES MODEL RAILWAY LOGIC SYSTEMS—3 818 COLD CATHODE TUBES—6 858 GENERAL FEATURES CONDUCTIVE GLASS 853 **NEWS AND COMMENT EDITORIAL** 809 MARKET PLACE 817 REPORT FROM AUSTRALIA 829 **SPACEWATCH** 837 **ELECTRONORAMA** 842 BRITISH MUSICAL INSTRUMENT TRADE FAIR 865

SPECIAL SUPPLEMENT

AT HOME WITH AUDIO

Our December issue will be published on Friday, November 14

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By M. J. Gay Chief Circuit Engineer (Linear), Plessey Microelectronics

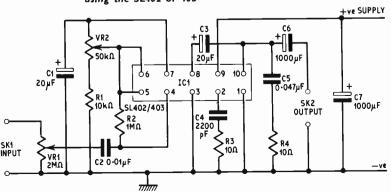
Basic operation theory was given last month for the SL402 and SL403 integrated circuit audio amplifiers. However it is not essential to have read the previous article before constructing the amplifier described here. This article will describe a complete amplifier using the Plessey SL402 or SL403 integrated circuit audio amplifiers. This is a simple arrangement providing a straightforward amplifier without tone controls.

SIMPLE AMPLIFIER

The simplest circuit using the SL402 or 403 is shown in Fig. 1. Here the pre-amplifier section is used solely to provide the bias voltage for the main amplifier. The bias voltage is generated by connecting together the pre-amplifier input and output (pins 6 and 5 respectively), and it is applied to the main amplifier input (pin 4) via the volume control. The use of the pre-amplifier to generate the bias voltage eliminates temperature effects (as explained last month).

The output is taken from pin 10 via the $1,000\mu$ F coupling capacitor C5 and the output voltage is fed back to the "bootstrap" connection (pin 8) via C3

Fig. 1. The simplest amplifier possible using the SL402 or 403



 $(20\mu F)$. C2 is a supply decoupling capacitor and C4 is the compensation capacitor necessary to ensure stability of the negative feedback loop.

While the circuit of Fig. 1 will work satisfactorily with the great majority of SL402 and SL403 amplifiers, some modifications are necessary to ensure optimum performance with all devices. The recommended circuit is given in Fig. 2.

RECOMMENDED CIRCUIT

The major modification from Fig. 1 is the addition of a bias trimming potentiometer enabling the output quiescent voltage to be precisely centred on all units, thus assuring maximum possible output before overload occurs. Bias trimming is obtained in effect by varying the pre-amplifier section current by means of VR2. The 10 kilohm series resistor R1 prevents the bias point being moved excessively negative, which can in some cases cause damage to the integrated circuit.

The bias voltage is applied to the circuit via a fixed resistor R2 (I megohm) rather than via the volume control, so that any bias errors due to the main amplifier input current flowing through this impedance will be fixed, and can be trimmed out by means of VR2.

Additional stabilising components R4 and C5 have been added; this is simply a precaution to reduce the risk of oscillation due to h.f. feedback via stray capacitances, etc. when unscreened speaker leads are used. One must always bear in mind that the SL402 and SL403 are capable of operating (and hence of oscillating) at several megahertz. The single compensation capacitor in Fig. 1 has been replaced in Fig. 2 by a resistor-capacitor combination R3 C4. This

alternative compensation system preserves the loop gain to higher frequencies and thus gives lower distortion towards the top of the audio band.

The supply decoupling capacitor C7 can be the reservoir capacitor for the power supply unit. It is placed on the board close to the integrated circuit so that it provides effective decoupling of the supply line at high frequencies. For this reason it must be used even if a battery or stabilised power supply provides power to the circuit.

Fig. 2. Recommended simple mono amplifier

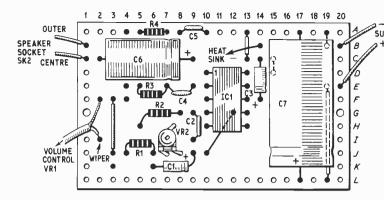


Fig. 3. Layout and wiring of the components for the simple amplifier (Fig. 2)

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1 2	3 4	4 5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	-

Fig. 4. Underside of Veroboard for the amplifier, showing breaks in copper strip and link wires

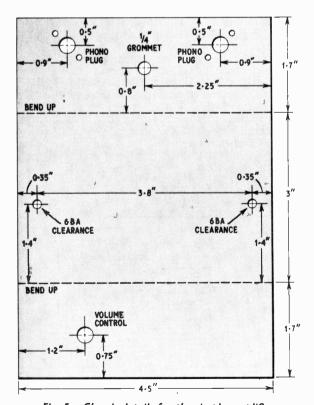


Fig. 5. Chassis details for the simple amplifier

COMPONENTS . . .

SIMPLE AMPLIFIER

Resistors

RI $10k\Omega$ **R3 10**Ω All &W, 10% carbon R2 $IM\Omega$ 10Ω R4

Potentiometers

VRI $2M\Omega \log$ carbon

VR2 50kΩ linear skeleton preset

Capacitors

20μF elect. 16V C5

 $0.047 \mu F$ polyester 0.01μF polyester C6 C2 1,000µF elect. 16V

20μF elect. 16V C7 1,000µF elect. 25V

C4 2,200pF ceramic

Integrated Circuit ICI SL402 or SL403

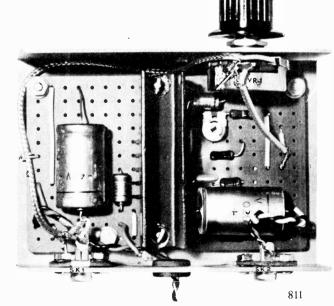
Miscel laneous

SKI, 2 phono sockets (2 off), control knob 18 s.w.g. aluminium $6\frac{1}{2}$ in \times $4\frac{1}{2}$ in and $2\frac{1}{2}$ in \times 2in Screened lead, 6B.A. fixings, grommet

CONSTRUCTIONAL DETAILS

Figs. 3, 4, and 5 show constructional details of the amplifier which was built up on a 2.6in × 4.2in Veroboard mounted in a simple chassis. Note that, as the i.c. has 0.2in pin spacing, 0.2in matrix Veroboard was used. Obviously 0.1in spaced board may be used as an alternative but care must be taken with this size to avoid excess solder shorting adjacent conductors together. If the common 0.15in matrix board is used, then insert pins into the board and solder the i.c. to these. Do not attempt to bend the leads sideways to force them into 0.15in spaced holes.

This unit may be operated from a battery, stabilised power supply, or from a mains power supply consisting simply of a transformer and bridge rectifier as detailed for the stereo amplifier in the following article. The integrated circuit is provided with a heat radiator, see Fig. 9 in the following article. Note that the metal bar of the package, to which the radiator is attached, must be earthed to the negative side of the supply. The completed amplifier measures 4.5in \times 3in \times 1.7in.



PERFORMANCE OF SIMPLE AMPLIFIER

All the characteristics given were measured with an SL403 in the circuit operating on an 18 volt supply line and a 7.5 ohm load. The performance with an SL402 and a 14V supply will be similar except, of course, that the maximum power will be 2 watts instead of 3 watts. The main characteristics for the simple amplifier are given in Table 1.

Table 1: SPECIFICATION OF SIMPLE AMPLIFIER

Sensitivity (for 3W output)	270mV r.m.s.
Input impedance: Volume control at max.	700k Ω
Volume control at min.	2MΩ
Frequency response (see Fig. 6) Distortion (see Fig. 7)	30Hz-90kHz 0·5 per cent
Noise level (referred to 3W output) Hum level (see text)	— 84dB — 63dB
Quiescent current Current consumption at 3W output	60mA 350mA

The noise level quoted is the worst case, measured with the volume contol at maximum and the input open circuit. It is furthermore the absolute level, not weighted for the ear's frequency response. This weighting would yield an even better figure (which is why weighted figures are often quoted).

For hum measurements the circuit was fed directly from a transformer and bridge rectifier. This gave a supply line ripple of 550mV peak-to-peak, which produced the quoted hum level of 63dB below full output. This can be improved proportionately if desired by increasing the value of the reservoir capacitor (C7 in Fig. 2); raising this to 5,000µF will give a hum level of 77dB below full output.

Fig. 7 shows total harmonic distortion against output level. In fact the distortion is predominantly second harmonic.

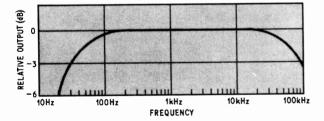


Fig. 6. Frequency response at 0.5 watt output—simple amplifier

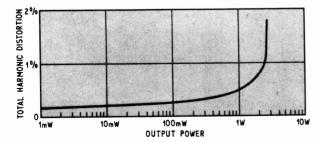


Fig. 7. Distortion curve at 400Hz—simple amplifier



The amplifier to be described uses two SL403 integrated circuits in a stereo system which can be driven by a radio tuner, or crystal or ceramic pick-ups. The design includes comprehensive tone controls and a balance control, and also incorporates the mains power supply.

TONE CONTROL CIRCUITS

There are various methods of adding tone control circuits to the SL403, for example, placing them in a feedback loop around the pre-amplifier. The method adopted here however is simply to connect a conventional tone control network between the pre-amplifier and main amplifier. This has the advantages of using normal logarithmic potentiometers and of leaving the amplifier's input impedance unaffected by tone control settings. The basic system is shown in Fig. 1

The input signal is applied to the pre-amplifier which provides the gain necessary to offset the tone control network attenuation (six times with controls set level). The tone control output is then fed directly to the main amplifier section of the SL403 which, having a very high input impedance, presents no significant loading to the network.

It will be remembered that the pre-amplifier serves not only as an amplifier but also as the generator of the temperature compensated bias voltage for the main amplifier. These functions are combined by connecting it as in Fig. 2.

Shunt feedback via R1 R2 and R3 establishes the collector potential of TR3 at approximately 6.5 volts; this allows the pre-amplifier sufficient swing to drive the tone control network. The feedback is decoupled at audio frequencies by C7, across which is established a d.c. potential sensibly equal to that at the base of TR1. This potential is the necessary bias voltage for the main amplifier, to which it is applied via the tone control network. Bias adjustment is essential in this circuit since, by raising the collector potential of TR3 we have reduced its quiescent current; it is accomplished by the pre-set potentiometer VR3 connected across the pre-

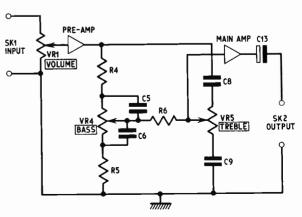


Fig. 1. Basic tone control arrangement





By M. J. Gay Chief Circuit Engineer (Linear), Plessey Microelectronics

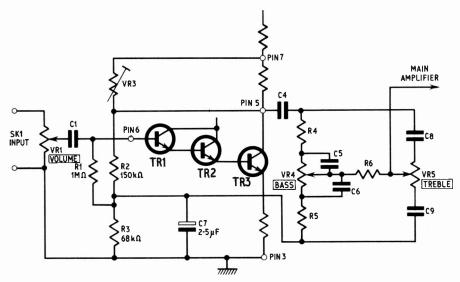
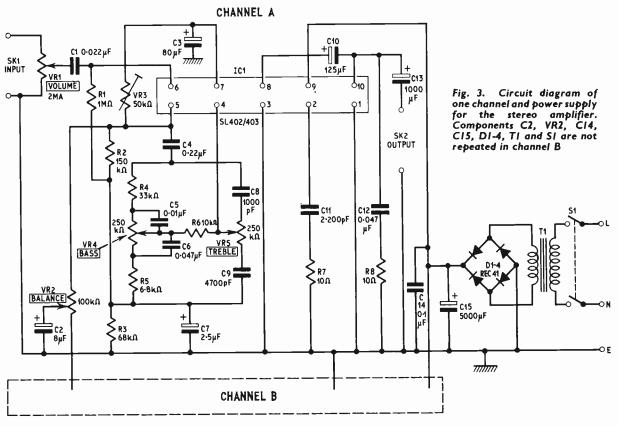
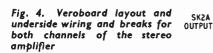


Fig. 2. Bias arrangements for the SL402 and SL403





C15 CENTRE 3 4 5 15 16 17 18 19 20 21 22 23 24 25 CENTRE o limminimi ing 0 C13 С 0 OUTER D E THE G н N 0 _ 0 R4/C8 R4/C8

CHANNEL B

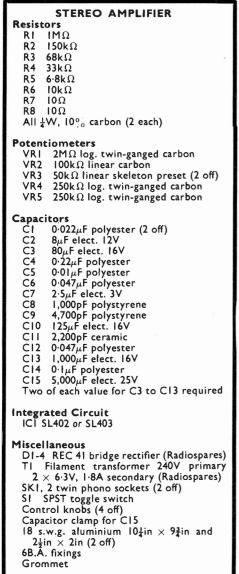
R5/C9

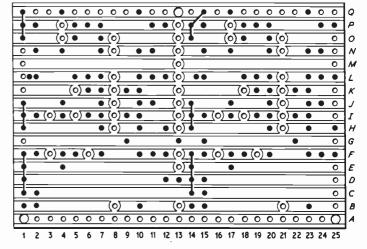
SK2B OUTPUT

R5/C9

CHANNEL A

COMPONENTS...





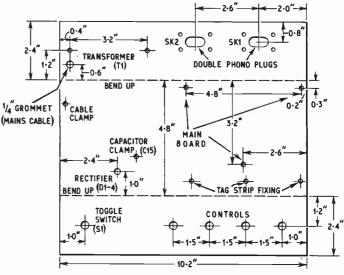
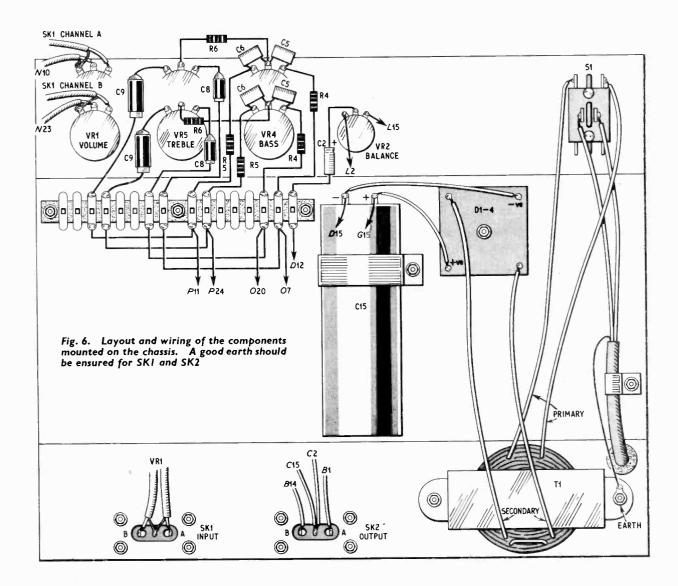


Fig. 5. Chassis details for the stereo amplifier



amplifier load. This potentiometer is adjusted as before to set the quiescent output voltage to half the supply voltage.

Balance adjustment is obtained by connecting a 100 kilohm potentiometer between the pre-amplifier outputs of the two channels with the wiper earthed via a capacitor. By adjusting this control the gain of either channel may be reduced to achieve balance.

The complete circuit of the stereo amplifier is shown in Fig. 3. It will be seen that the main amplifier section is connected essentially as in the simple amplifier described earlier.

CONSTRUCTIONAL DETAILS

Figs. 4, 5 and 6 show the constructional details of the unit. The power supply components are mounted directly on the chassis, as are the controls, while the main circuitry of the amplifiers is mounted on the 3.6in \times 5.2in piece of 0.2in matrix Veroboard. The tone control network components are wired directly to the potentiometers or between the potentiometers and a tagstrip fixed to the chassis beneath them (see Fig. 6). Screened leads are used for the input connections. The arrangement gives a very compact design without

needing a shoehorn to fit the components in. Complete unit measures $10\cdot 2$ in $\times 4\cdot 9$ in $\times 2\cdot 4$ in. The recommended construction order is as follows.

- 1. Build up tone control networks on chassis.
- 2. Build main board with flying leads attached for connection to tone, volume and balance controls, speaker sockets and power supply. Do not forget to earth the heat sinks.
- Affix main board to chassis after thorough checking (it is very trying taking it out again) and wire up to controls.
- 4. Attach and connect up power supply components.

Because, in this layout, the supply reservoir capacitor is connected via leads of about six inches in length, it is necessary to provide supply decoupling directly on the main board; hence the additional $0.1\mu F$ capacitor (C14 in Fig. 3) across the supply.

PERFORMANCE OF STEREO AMPLIFIER

The characteristics were measured with a 7-5 ohm load on the output of each channel. The power supply generated a quiescent supply line voltage of 17-4V. With one amplifier driven to full output this dropped to

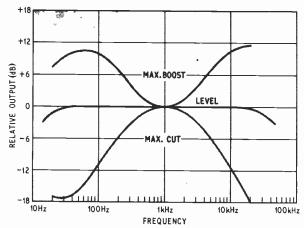


Fig. 7. Frequency response and tone control characteristics—stereo amplifier

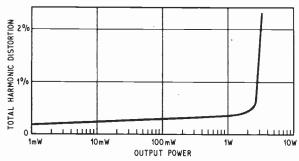


Fig. 8. Distortion curve at 400Hz-stereo amplifier

16.5V, while with both driven to full output it dropped to 15.8V. There are thus three maximum output power figures that can be quoted:

- 1. Music power, which assumes that full power is demanded for only very short periods so that the supply remains at 17.4V.
- Continuous sine wave output power with one channel driven only.
- Continuous sine wave output power with both channels driven.

In this case measurements were made with one channel driven, giving 2.7 watts r.m.s. continuous sine wave output at the onset of clipping. The music rating corresponding to this will be 3W r.m.s. per channel, while the maximum continuous sine wave

output per channel with both channels driven is 2.5W r.m.s. per channel. The remaining major characteristics are listed in Table 1.

Table I: SPECIFICATION FOR STEREO AMPLIFIER

Sensitivity (for 2.7W r.m.s. output)	160mV r.m.s.
Input impedance: Volume control	
at max. Volume control	700 kΩ
at min.	2M Ω
Frequency response (see Fig. 7) Tone control range: Bass (40Hz) (see Fig. 7) Treble (15kHz)	-17dB, +10dB
Distortion (see Fig. 8)	less than I per
Noise level (ref. 2.7W output, controls level)	
Hum level (ref. 2.7W output, controls level)	—72dB
Crosstalk level	— 40dB

As for the simple amplifier the noise level quoted is worst case and is unweighted. The distortion curve Fig. 8 shows higher distortion than for the simple amplifier due to the additional contribution from the pre-amplifier. Again the distortion is predominantly second harmonic. Crosstalk was measured with one channel driven to 2W r.m.s. output.

SUPERIOR PERFORMANCE

This and the previous article have shown how the SL402 and 403 can be used in amplifier systems. These i.c. devices enable the home constructor to produce complete amplifiers of high reliability in a very small size without recourse to elaborate constructional techniques.

The performance of the designs given will be adequate for many applications (being superior to that of many programme sources and loudspeakers), but it is not claimed however that it reaches real high fidelity standards, although many so-called hi fi amplifiers fall sadly short of a -84dB noise level.

Next month's article will show how advantage may be taken of the low cost and simplicity of use of these units to produce an unconventional stereo system which really does merit the title high fidelity.

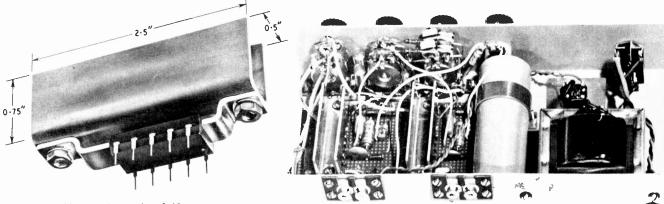


Fig. 9. Heat sink, made of 18 s.w.g. aluminium, attached to the i.c. package

MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

F.M. TUNER KIT

A new f.m. tuner kit from General Avionic Associates Ltd., 9 Wimpole Street, London, W.I., is believed to be the first kit to be made available using integrated circuits in a pulse-counting design.

The tuner is capacitively tuned and incorporates automatic frequency control. A voltage tuned version is

available as an alternative.

The use of integrated circuits in the tuner is claimed to be equivalent to 44 transistors and also eliminates the need for discriminator and i.f. transformers. The use of i.c.'s also makes alignment much simpler.

The kit price is £9 19s 6d plus 5s postage and packing. No technical specification was given but an illustrated instruction booklet is

included with the kit.

WORK BENCH AID

When working on the test bench, the wish for a third hand before becoming entangled in wire, fumbling with components and the work piece, and trying to juggle with a hot soldering iron at the same time, is quite a common scene.

The vice is a useful "third hand" for holding items but is limited in the number of angles that the work can be held. The Pana Vise system from Special Products Distributors is a base and vice head arrangement that allows the work piece to be pivoted

360 degrees in any tangent to a half sphere to achieve any compound angle, i.e. tilted 180 degrees and rotated 360 degrees.

There are four types of bases and seven work holder attachments available. The holders are easily locked into position by a single patented lock screw.

Further details and price list is obtainable from Special Products Distributors Ltd., 81 Piccadilly, London, W.1.

SOLDER PINS

Solder pins that can be soldered onto component leads so that they can be readily plugged into printed circuit and 0.050in matrix perforated boards are the latest product from Oxley Development Co. Ltd.

These tapered, splined and barbed pins are particularly useful for enabling components to be removed and replaced without damage to the board, mounting transistor and integrated circuits, and for connecting wires between boards.

Further information is available from Oxley Developments Co. Ltd., Priory Park, Ulverston, North Lancashire.

LITERATURE

A designer's guide to mercury and alkaline primary cell power systems has been published by Mallory Batteries Ltd.

The guide, in addition to describing the two primary cell systems, explains their advantage under widely differing conditions.

One of the guide's objectives is to assist design engineers of battery powered equipment to make the best possible choice when specifying a particular battery. The technical specifications of 126 different mercury and alkaline manganese cells and batteries are included in the guide.

Further information and copies of the guide can be obtained from Mallory Batteries Ltd., Gatwick Road, Crawley, Sussex. Another guide of particular interes to electronics firms is the new edition of the Guide to Northern Engineering, price 5s, now available from the North East Engineering Bureau, 15, Walker Terrace, Prince Consort Road, Gateshead-on-Tyne, 8.

The guide contains the names and addresses, with a description of capacity and products of most engineering and allied trades in the Northern Region. There is also a classified index to all products.

Featured in this issue are articles from most of the development organisations in the region, giving valuable information and contacts for expansion in the North.

COMPONENT ORDERING SCHEME

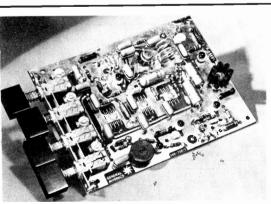
It is always frustrating that just as a project is nearing completion, components are urgently required, and being a spare time hobby or private enterprise it invariably occurs in the evenings or weekends when components shops are closed.

To eliminate the unnecessary delays involved when posting orders to dealers and the time taken for dealers to dispatch orders, Home Radio (Components) are running a special deposit credit account scheme to individuals. They have installed a special telephone answering machine for customers wishing to place orders outside normal business hours and the scheme is claimed to cover over 8,000 components.

The Credit Deposit Account is similar to a scheme that has been available for several years to industry, government departments and education authorities. Complete details can be obtained from Home Radio (Components) Ltd., 234–240 London Road, Mitcham, Surrey.

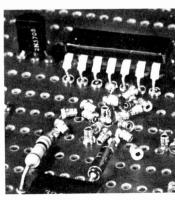
NOTICE

It should be noted that the Peak Sound advertisement on page 740 of the October issue should read "Cir-Kit" is supplied in spools, \(\frac{1}{16} \) in wide \(\times \) 5ft long" (not 50ft).

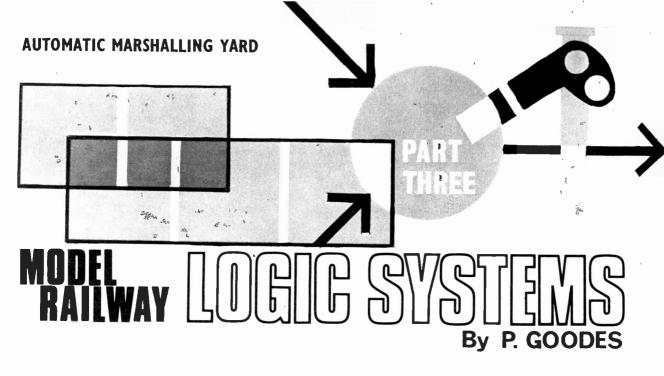


Completed tuner kit from General Avionic Associates





Solder pins manufactured by Oxley Development Co.



HIS is a fairly complex circuit for an automatic marshalling yard and should not be attempted by anyone who has not some knowledge of electronics. No printed circuit layouts are given since it is assumed that those building this circuit are capable of laying out the components for themselves. The object of this circuit is as follows (refer to the block diagram Fig. 3.1 and track layout Fig. 3.2).

SHUNTING

Suppose a train of five trucks and an engine enters the initial section of the yard. The engine is uncoupled conventionally and is removed.

When the circuit supply is switched on and the start button pressed, the control unit operates points P5 to its b position and allows the shunting engine to come out of the siding (Fig. 3.2). This engine pushes the five trucks up the slope where each is uncoupled in turn and allowed to roll down the other side under gravity.

As the first truck runs down it passes over switch block \$1 and trips one or a combination of the switches in this block. The resulting pulse is fed into a switch decoder and operates a particular combination of points; the truck is routed into the associated siding.

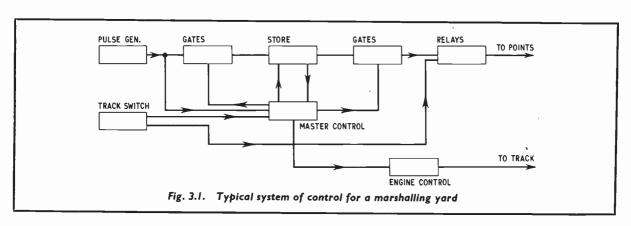
The rest of the trucks are still being pushed slowly up the ramp and each is in turn uncoupled and routed into its respective siding.

At any point during this sequence, the number store may be programmed. This is achieved by dialling pulses from an ordinary telephone dial into the store, whose input is fed by gates biased from master control.

When the shunting engine reaches switch \$2 (which it cannot do until all the trucks have been dispersed), a pulse is fed to master control which primes the gates on the number store read out, and also a pulse to the engine control amplifier.

The first output from the store represents the first digit dialled during programming, and this output is fed to the relay which operates the points combination required to reach this truck.

Suppose that truck number 4 was required as the first truck (i.e. 4 was the first digit dialled). During the uncoupling sequence, truck 4 was directed into a particular siding. Then the first read-out operates the points giving access to this siding and the engine proceeds to collect this truck.





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The engine, meantime, has been slowing down (due to the pulse from S2 to the engine control amplifier). The engine couples with the truck and continues to slow down, stop and reverse out of the siding with the truck. As it reverses out and once more trips S2 switch, it starts slowing down again and starts going forward again. As it trips S2, a pulse is fed to master control to read out the second digit in the store. The engine then proceeds to collect this truck also.

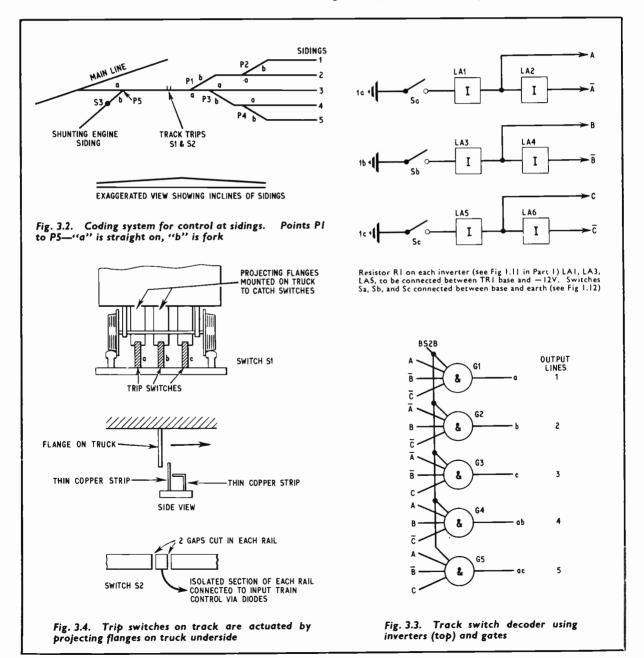
When all trucks have been collected in this manner, master control operates uncoupler number 2 and the trucks are left where they were initially. The shunting engine returns to its siding, trips switch S3, and resets the circuit. The main engine may now return and collect the newly formed train.

TRACK SWITCH DECODER

The main requirement for this section was simplicity and reliability. The object of the decoder is to be able to distinguish any one truck from any other truck (Fig. 3.3). The idea of reflecting light from coloured patches on the trucks was unnecessarily complex and would require some very careful setting up.

Consequently trip switches were used. These were made from off-cuts of old relay contacts and mounted in a bank of three (Fig. 3.4) which for the purpose of the circuit description will be called \$1a, \$1b, and \$1c.

In the quiescent state of all three switches being open, inverters 11, 13, 15, are giving a 0 output and hence 12, 14, 16 are giving a 1 output. When S1a operates, 11 gives a 1, 12 a 0 and similarly for S1b and S1c.



Combinations of the six inverter outputs are fed to AND gates controlled by master control. Thus for any one switch or combination of switches operating, one gate will give an output.

Considering a few codes:

Sla operates alone

The only gate with this input combination is G1, therefore G1 gives a 1 output (assuming that master control gives the O.K.).

Considering S1a and S1b operating together:

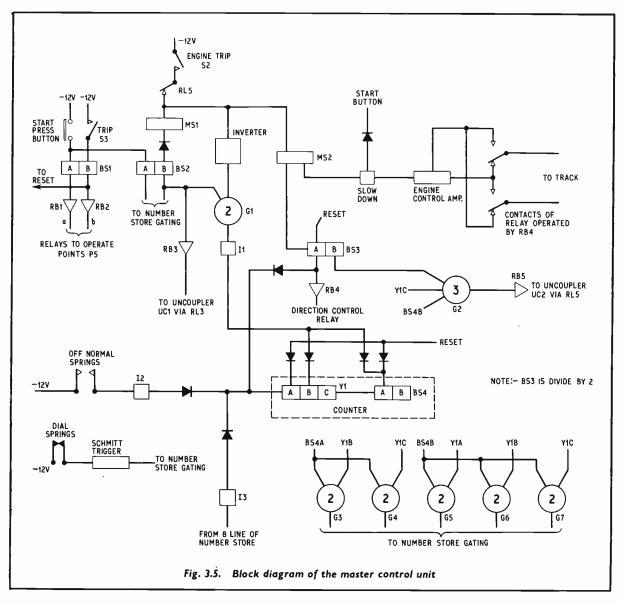
Gate G4 will then give an output.

Thus each truck may be coded by fitting small projections to the underside to trip combinations of these switches (Fig. 3.4).

MASTER CONTROL UNIT

This section, as the name implies, controls all the switching sequences required to build up the train. When the start button is depressed, BSI is triggered. This means that BSIb gives a 1 output which operates points P5 to allow the shunting engine to leave its siding. Fig. 3.5 shows the master control system.

The depression of this switch also gives BS2b a 1 output which primes the store input gates and also the decoder gates. The pulse feeding the slow down amplifier causes the engine to speed up, and it proceeds to disperse the trucks as they pass over uncoupler number 1 operated via relay RLA (see Fig. 3.6 points actuators).



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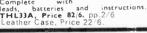
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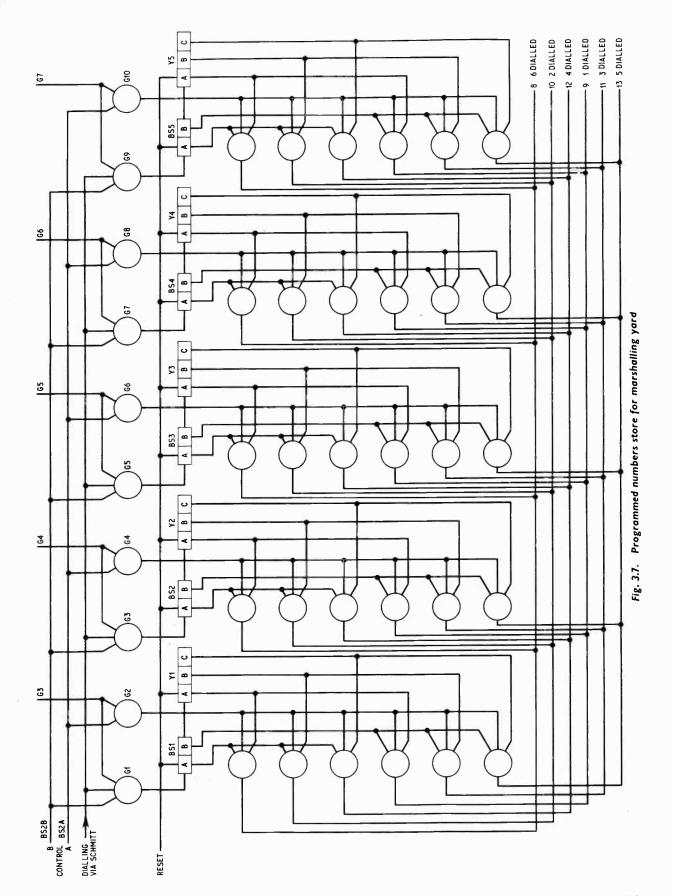


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During programming, the normally off springs of the dial are used to shift the ring counter Y1 which primes the associated store input gates. Thus every time a digit is commenced, the 1 in the counter moves along one section and opens gates to another part of the store.

REQUIRED ORDER MOVEMENT

Assuming now that the required order of the train has been dialled into the store (which is dealt with later), and that the engine has routed all the trucks into the required sidings, switch S2 is now tripped by the engine. This sends a 1 pulse into MS2 (which controls the slowing down of the engine) and a 1 pulse into gate G1 which, being already primed by BS2b, gives in turn a 1 output. This is fed via 11 to set ring counter Y1 to its "1" position.

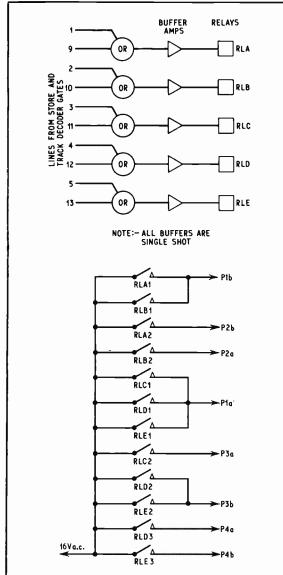


Fig. 3.6. Siding selector relays. Points "a" to straight on, "b" to fork. Other side of 16V a.c. wired to common coil tags of points motors

Monostable MS1 was also triggered by S2 and after about four milliseconds, triggers bistable BS2 so that BS2a gives an output. This primes the store read-out gates and the points corresponding to the first required truck operation.

The engine proceeds to this siding, still slowing down, and couples with the truck there. When MS2 reverts to its quiescent state, it feeds a pulse to BS3 which is a divide-by-two circuit. This operates a relay via buffer RB4, which reverses the polarity of the supply to the track. Thus, the engine reverses out of the siding with the truck, gradually building up speed.

As it passes over switch S2 again, it starts slowing, reverses, and speeds up again. A pulse is also fed to BS3 which in turn shifts the ring counter to its C position. This reads out the second digit dialled and operates the associated points; the engine continues on its way to collect this truck. On the way it trips S2 again, starts slowing down and removes the truck from the siding.

This procedure continues until all trucks are collected by which time Y1 has reached the end position. This means that gate G2 is primed.

As the engine reverses out for the last time with a 1 on BS3B, RB5 operates relay RLE which disconnects switch S2 and operates uncoupler number 2. The train thus leaves the trucks as it passes over the uncoupler and the engine proceeds back to its siding where it trips S3, changing points P5 back to "straight on" and resetting the ring counter, the memory, and the bistable BS3 with a 0 pulse.

POINTS ACTUATORS

A line from the track switch decoder and corresponding line from the store are fed via an OR gate to a relay buffer. The associated relay then operates the required points. The system is shown in Fig. 3.6.

PROGRAMMED NUMBER STORE

This is a straightforward circuit using 3-ring counters and bistables. Pulses are dialled in from the telephone dial via a Schmitt trigger circuit.

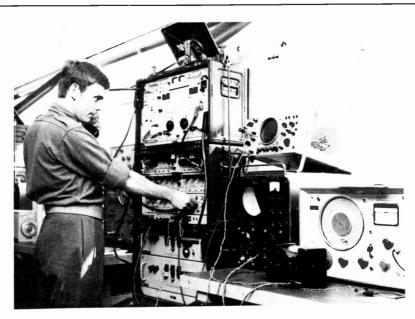
Consider the first digit to be dialled. During dispersal of the trucks BS2b is at 1 and before dialling Y1 is at position 1. When this train of pulses starts, the normally off springs of the dial close, allowing a pulse into the ring counter Y1 shifting the 1 to position Y1b. This then primes gate G1 and pulses may be fed into section 1 of the store and so on until all required digits have been dialled.

When BS2 changes state, BS2a gives a 1 output thus priming gates G2, G4, G6, G8, G10; Y1 again selects the required section of the store. An output is obtained on the appropriate line and this feeds the required combination of points. The action of the engine shifts Y1 along and the second section may then be read.

The gates associated with line 8 of the store are included to allow for the fact that fewer than five trucks may be required. Then with no digit in that section of the store the 8 line will have a 1 pulse on it. This is fed to the input of Y1 so that it scans on until a section is found with a digit in it.

Section 5 of the store must always have a digit in it, and earlier positions filled up by blanks if necessary. Thus if only three trucks are required in the order, say, 3, 5, 2, the dialled code should be 6, 6, 3, 5, 2,

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INTEGRATED CIRCUIT F.M. TUNER

Dart Electronics has been appointed by General Avionics Limited as their U.K. distributor for their FM Tuner kit, the first to use integrated circuits with pulse counting techniques developed by Marconi-Elliott Microelectronics.

The circuit has built-in automatic frequency control, and with the inherent stability of the integrated circuits, a reliable and easily set up circuit is offered to the home constructor in kit form. A resistively tuned version is in widespread use as an industrial radio system and is noted for its extreme reliability under continuous, unattended operation. The circuit employed effectively contains 44 transistors and, although the quantity of discrete components is fairly high, the entire unit is built on a double-sided board measuring 133 imes 98.5mm (3.875 imes 5.25in). The Tuner can be run off a 12V d.c. power supply or a combination of 6 and 12V batteries.

All components are available BY POST ONLY from Dart Electronics at a special kit price of £9 19s 6d plus 5/- post and packaging (U.K. & N. Ireland) which includes selector switch and double-sided p.c. board ready drilled and tinned. The kit is complete with all necessary circuits and instructions.

Full assembly details, circuit diagram and parts list are also available separately from Dart Electronics at 2/6 per copy and an article appeared in the June issue of the WIRELESS WORLD magazine.

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A 4 Germ. R.F. PNP T0-1 = OC44-45, NKT72/125, ASY54	£1.10	£4.10	£7.10	€60
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A 7 Assorted Germ. A.FR.F. PNP mixed cans, general purpose	15s.	€2.10	€4	£32
A 8 Germ. A.F. S0-2 PNP = 2G371-89, ACY27-31, OC71-75	£2	67.10	£12.10	£100
A 9 Sil. Alloy PNP T0-5 =25301-5, BCY17-29, BCY30-34	£2	£7.10	£12.10	£100
A10 Sil. Alloy PNP S0-2 = 25321-325, OC200-205	£2	£7.10	£12.10	£100
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Report from AUSTRALIA

BY D. F. MOODY



THERE is an old Chinese proverb—"he who works with a machine must think like a machine". This saying pre-dates, probably by a few thousand years, much of the so-called modern science fiction which uses this concept as the basis for so many stories, and it causes one to wonder whether to pay any heed or not to the warnings so common these days of the impending computer-run society of tomorrow.

However, it is interesting to observe the ways in which we are being led, slowly and subtly, to accept and depend upon modern automation and give up our freedom in little bits and pieces.

SPEEDING THE POST

The distribution of mail in the huge outback areas of Australia has always held a fascination whether by the one-man and pack horse, or by the 2,000 miles round trip "milk runs" carried out by the Royal Mail aircraft today.

There is one thing that the postman on these rounds can be sure of, and that is to receive a hearty and friendly welcome from the bush-folk who are so very glad to get their mail when they do, and not just to accept the daily postal delivery as we do in the city (and grumble when the daily deliveries were cut from two to one).

However, although personalised service for the mail is desirable, due to the explosion in the quantity of mail handled (the Australian Post Office handled over 2½ billion articles of mail last year), it would be impossible to cope with this without mechanical and electronic help. This is not only an Australian problem, and the Universal Postal Union has been active for some time in trying to achieve a higher standard of service in those areas where the mail situation is rapidly reaching a state of chaos.

In Sydney we have one of the most modern electronic mail sorting machines in the world, with a capability of handling a quarter of a million letters an hour. In order to achieve high sorting rates the public have to co-operate by using a four figure post-code which was introduced in 1967 and covers all areas in Australia.

LUMINESCENT CODING

At the moment in the Redfern mail exchange, the destination information is stamped on the reverse side of the envelope in the form of a set of luminescent spots. This is done by a trained operator who sits in front of a display screen, and according to the marked destination or post code and a pre-fixed code the appropriate dots are punched onto the back of the envelope. These dots are practically invisible under normal lighting conditions, but when exposed to ultra-violet light, they glow with sufficient intensity to be detected by photoelectric devices. Hence in this way, the "brain" in the exchange can be told the address on the letter, and automatically arrange for the correct chutes to open up at the right time so that the mail is selectively filtered in a manageable fashion.

Further research is aimed at attempting to handle all stages of the actual transmission using electronic techniques, and may well affect the whole concept of mail as we know it today. It has been said that the mail of the future will be of a similar form to Telex—Heaven forbid!

Surely this step would be even too cold hearted for the most ardent "systems" man to contemplate. However, for business correspondence, I will be most surprised if such a system is not eventually employed with a Big Brother computer keeping its steely eyes on "who from", "to whom" and "how much".

UFO's OVER ALICE SPRINGS

With so much interest and activity in the American Apollo project, the continuing work at Woomera tends to get more or less forgotten, at least on the international scene. Although the recent failure in attempting to hurl a test satellite load into orbit from the Europa I rocket did manage to get a mention in the papers, it appears that this news is not considered so glamorous as that emanating from Cape Kennedy—at least to terrestrial eyes.

It is rewarding however to note that sightings of mysterious flying objects in Central Australian skies have followed the recent setting up of space research facilities at Pine Gap near Alice Springs. This at least seems to indicate that "someone" is interested in what goes on in Australia. After all, Woomera is one of the oldest rocket sites in the world.

COPPER PROSPECTING

When you are hard at work soldering COPPER wire to your COPPER deposited printed wiring board and probably using a COPPER soldering iron bit, perhaps you may care to think of the romance behind a recent copper strike in Papua, New Guinea, particularly when you also bear in mind that the known world land supplies of copper are doomed to be worked out within the next sixty years.

About a year ago an Australian Company sent an American Explorer into the jungle in the far north-western corner of Papua. He found villages and people who had never before seen a white man, unknown streams, and more significantly, he found copper. Now there is a base camp there (known as Oregalore), with a team of 25 men from Canada, USA, Australia, New Zealand, South Africa and Northern Ireland.

The team exist under extreme conditions and the work is very tough, and their sole contact with the outside world is vested in a helicopter.

The next question to be answered is whether or not there is sufficient copper there to warrant the immense cost of extraction and transport.

I wonder what the electronics industry would do without copper?

AUDIO SUPPLEMENT

To coincide with the International Audio Festival and Fair at Olympia, this issue contains an extra 16-page Supplement (bound in the centre) aimed to help readers sort out the jungle of specifications and terms found in audio equipment brochures, and to guide the potential buyer on how to buy wisely.

PART 7

EORGAN

By Alan Douglas, Sen. Mem. I.E.E.E.

In this article we will complete the remaining accompaniment tone forming elements and also the post amplifiers which are fed from the passive voicing networks.

ACCOMPANIMENT PRE-AMPLIFIERS

As there are only two pitch busbars used for the accompaniment voicing, two pre-amplifiers are required. These, of course, are identical to the solo pre-amplifiers, a circuit diagram of which is given in Fig. 6.2. As before the function of these pre-amplifiers is to provide both a high impedance to the busbar input and an increase in signal level prior to feeding the voicing filters.

ACCOMPANIMENT FILTERS

The circuit diagram of the accompaniment tone filters following the 8ft and 4ft pre-amplifiers is given in Fig. 7.1. Here, as in the solo filters, low pass, high pass, and resonant types are in evidence. The two flutes are low pass circuits, with somewhat differing characteristics, because we do not want the 4ft to sound just like the octave of the 8ft.

The string stops—Viole Acute and Violina—are high pass circuits and again the values are chosen to

produce a difference in character.

The clarinet is a parallel tuned circuit with the filter coil wound on a ferrite core. The potentiometer VR3 combines in varying the response and broadening the resonance peak necessary to accommodate the formant band.

In practice the correct adjustment of this potentiometer encompasses a band of two octaves which correspond fairly well with the actual instrument.

The Trumpet stop is another parallel resonant circuit with different characteristic which is very useful as a solo voice.

The addition of the Dolce stop provides a reduced flute tone by shunting the 8ft flute capacitor C2 when the stop key is depressed.

Inclusion of preset potentiometers in some of the filter outputs enable volume adjustment.

PRE-AMPLIFIERS AND FILTER BOARD

Since only two pitches are used in the accompaniment manual, both the pre-amplifiers and tone networks can easily be assembled on one $3\frac{1}{2}$ in \times 5 in Veroboard as given in Fig. 7.2. The wiring and cutouts for the underside are given in Fig. 7.3.

cutouts for the underside are given in Fig. 7.3. In Fig. 7.2 the 4ft and 8ft pre-amplifiers are shown contained within a dashed box. For the components of this section refer to the components list for the solo pre-amplifiers given last month as the annotation is identical.

FUNCTIONAL CHECK

The checking of this board follows the same lines as that carried out in the solo pre-amplifiers detailed last month.

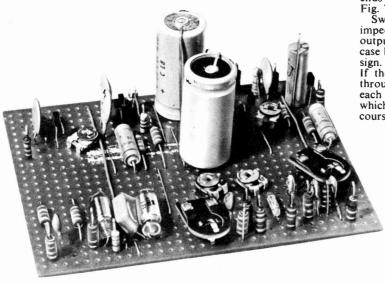
First we take off a +15V tap and earth return from the oscillator shelf, making the connections as shown. A 30,000pF capacitor connected across one of the oscillators will generate the test signal with subsequent division through its related divider. The note sign of the divider will indicate, of course, the key to be depressed when testing.

Since we need to pick up square waves from the 8ft and 4ft lower manual busbar, we must connect two 1yd lengths of single miniature microphone cable to the lower tagstrip which is attached to the lower keyframe. The busbar wires to this are coloured yellow for 4ft and grey for 8ft.

The coaxial screens are earthed at the tagstrip in common with the solo manual cables and their free ends connected to the Veroboard as indicated in

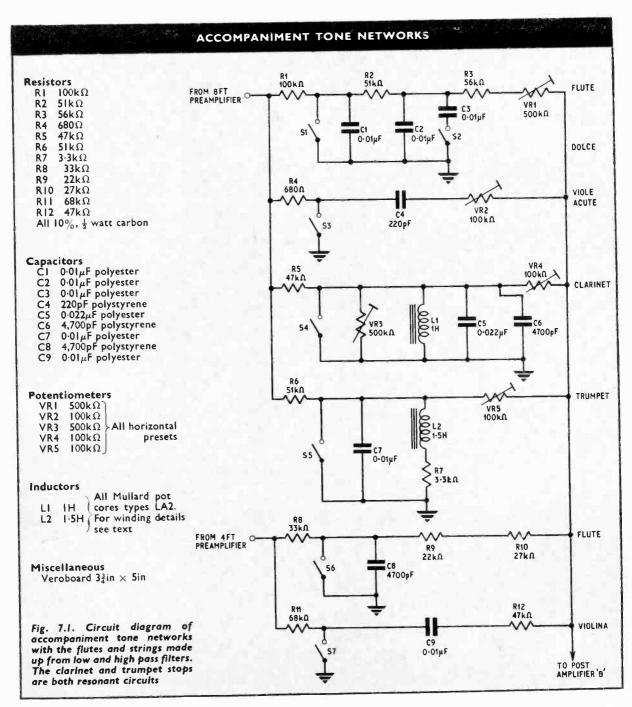
Fig. 7.3 by the identifying colours.

Switch on the supply, then connect a pair of high impedance headphones at each of the pre-amplifier output capacitors C3 in turn; the return line in each case being earth. Depress a key of the divider note sign. This should produce a clear, unsullied tone. If there is nothing or a distorted product, check through from the input and then at the collectors of each stage to pinpoint the offending component which will probably be a transistor. Here, of course, replacement will be necessary.



TONE CIRCUITS

This organ will be demonstrated at The International Audio Festival and Fair, Olympia, London, October 16 to 22



ACCOMPANIMENT PRE-AMPLIFIER AND FILTER BOARD

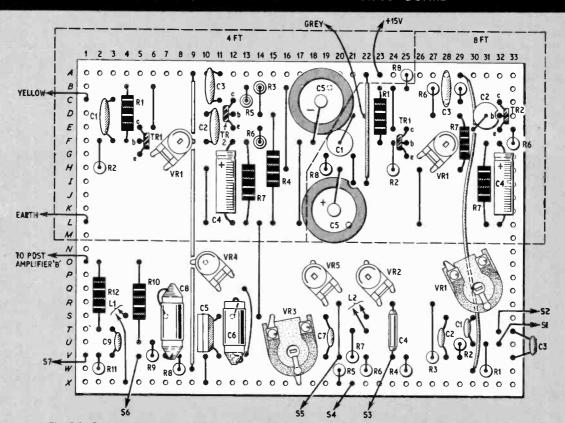


Fig. 7.2. Component layout of the accompaniment pre-amplifiers and associated tone networks

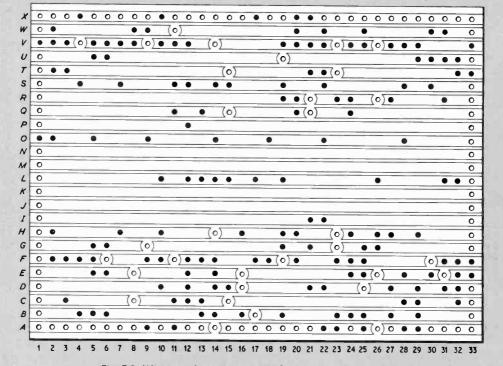


Fig. 7.3. Wiring and copper cutouts for Veroboard underside

PEDAL PRE-AMPLIFIERS +150 16 FT 8 FT Resistors RI 68kQ R7 $33k\Omega$ 3900 R6 R2 $33k\Omega$ **R8** 2.7kΩ >2.7ka 68kA >2.7kn 68k0 R3 $2.7k\Omega$ R9 470Ω R4 470Ω R10 470Ω TO TONE NETWORKS TO TONE 0-1 µF R5 470Ω RII 390Ω 0-1 uf **R6** 68kΩ (R1) (RS) All 10%, ½ watt carbon C4 0-33μF C1 0-22µF TX300 7TX300 500 µF Capacitors CI 0.22μF C5 100µF elect. 12V **₹**33kΩ R4 470Ω 100µF elect. 12V 33kΩ 470Ω C6 0.1μF C7 500μF elect. 25V **C3** 0·1μF 0-33μF All polyester except where marked R10 470.0 R5 470Ω CS 10 O µ F 100 µl **Transistors** TRI, TR2 ZTX300 FROM 16FT (Ferranti) 2 off FROM 8FT PEDAL BUSBAR PEOAL BUSBAR Fig. 7.4. Circuit diagram of pedal pre-amplifiers for 8ft and 16ft pitches

ACCOMPANIMENT FILTER ASSEMBLY

The accompaniment filter networks, with the exception of the coils, occupy the lower half of the board shown in Fig. 7.3. The winding data for the two coils L1 and L2—both LA2 Ferroxcubes—follows from the formula given last month. Using 44s.w.g. enamelled copper wire the approximate number of turns required for each coil are:

L1-2,000 turns L2-2,500 turns

With these coils wound they should be placed to one side prior to mounting in the voice screening box.

PEDAL PRE-AMPLIFIERS

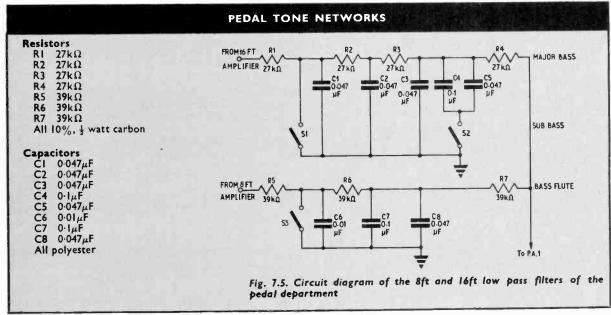
Since only one note is played at a time on the pedals, we can dispense with the emitter followers as used in the manuals and employ only the pre-

amplifiers as shown in Fig. 7.4. Here capacitors Cl and C4 are fed directly from the 8ft and 16ft pedal busbars.

PEDAL FILTERS

The outputs from the pre-amplifier feed two low pass filters, a 16ft Major Bass and an 8ft Bass Flute as shown in Fig. 7.5.

S2 provides a Sub Bass stop as the depression of this key removes the additional filtering of the capacitors C4 and C5. The filter outputs are not routed to post amplifiers as in the manuals, but go directly to the pedal power amplifier P.A.1. Not only does this allow the setting of a volume level independent of the manuals, but it reduces the risk of intermodulation and prevents the tremulant getting onto the pedal tones. Of course, it is more expensive, but once again if the pedal section is altered or enlarged in the future, the advantages of an independent channel will be considerable.



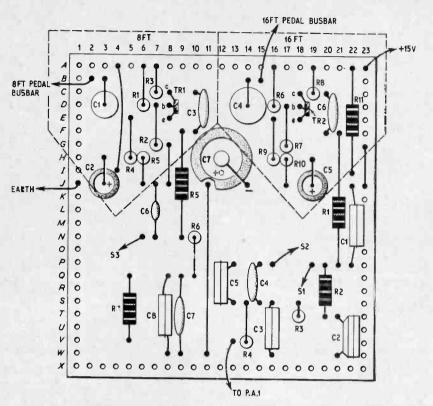


Fig. 7.6. Component layout of the pedal pre-amplifiers and tone networks

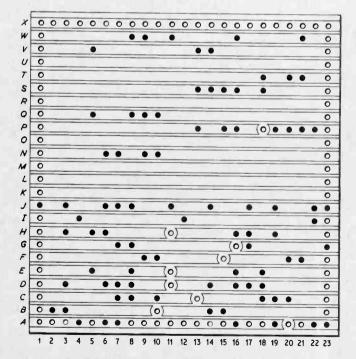
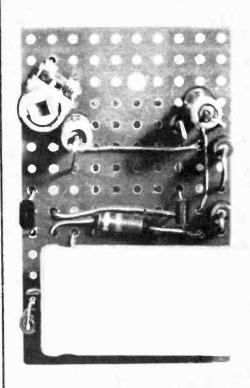


Fig. 7.7. Underboard wiring of pedal circuitry

POST AMPLIFIERS "A" AND "B"

0 +15V Resistors R5 100Ω $68k\Omega$ RI R2 330kΩ R3 C3 500µF 8-2kA R3 8·2kΩ R1 530kΩ R4 47Ω R5 100Ω All 1000, 1 watt carbon TR2 ZTX300 C1 4µF Capacitors TR1 ZTX300 CI 4μ F elect. 15V C2 0.1μ F polyester C3 500μ F elect. 25V C2 0.1 µF FROM SOLO TONE NETWORKS TO P.A.2 VR1 4 INPUT **≤** R4 47Ω 68kD **Potentiometers** VRI 4-7kΩ VR2 47kΩ 4.7k A **Transistors** TRI, TR2 ZTX300 (Ferranti) 2 off

Fig. 7.8. Circuit diagram of a post amplifier. Two of these ere required



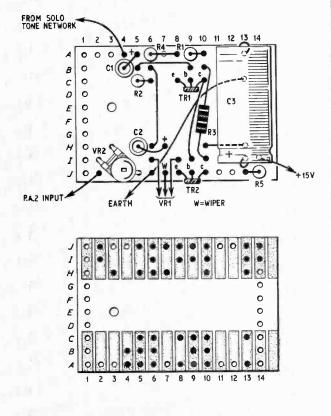
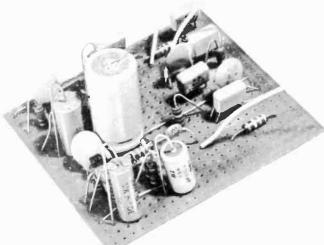


Fig. 7.10. Component layout and underside connections of post amplifier assembly



PEDAL CIRCUIT ASSEMBLY

The components making up the pedal preamplifiers and tone nets are mounted on Veroboard as shown in Fig. 7.6. Underboard wiring and copper strip cutouts required can be seen in Fig. 7.7.

TESTING

The testing of the pre-amplifiers follows that given for the manual pre-amplifiers. However, since we have no pedals as yet, we can use the 8ft and 16ft coaxial cables from the solo manual busbars for test purposes. These should be connected as shown in Fig. 7.6. With the supply lines connected, headphone checks can now be carried out.

POST AMPLIFIER

With the exception of the pedal department, the filter outputs, both solo and accompaniment, are routed via intermediary post amplifiers. These recover any signal losses due to the voice nets.

The manual amplifier P.A.2 requires only 20 millivolts for full power output and this is easily provided by a d.c. coupled pair, the circuit of which is given in Fig. 7.8.

Two post amplifiers are required for the two manuals; these have been designated "A" for solo and "B" for accompaniment in the filter circuit diagrams. Before the signals from the post amplifiers are applied to P.A.2, they are mixed after going through the output potentiometers VR2.

These allow relative manual balance to be achieved both in loudness and total input setting to the main amplifier. As with the pre-amplifiers the +15V supply for the post amplifiers derives from P.S.U.1. Decoupling from the line is the simple CR filter seen in Fig. 7.8.

POST AMPLIFIER CONSTRUCTIONS

The post amplifiers are assembled individually on Veroboard strips as shown in Fig. 7.9. Underside connections are given in Fig. 7.10.

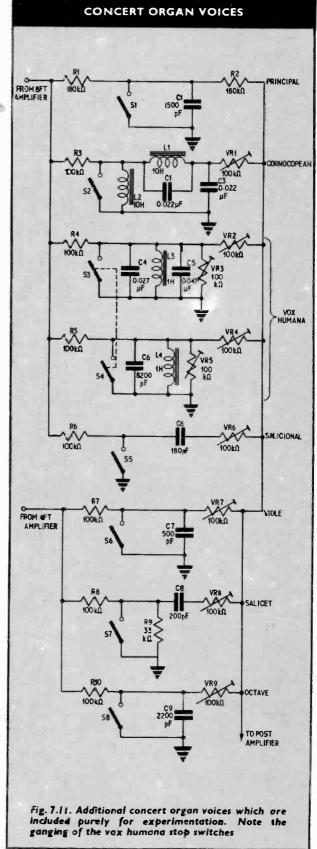
In common with the guidelines provided previously in checking the pre-amplifiers, the post amplifier can be functionally vetted. As before, the test requirements are a signal source and a headset.

CONCERT ORGAN VOICES

For the benefit of the experimenter a number of conventional church or concert organ voices are given in Fig. 7.11.

ADDENDUM

The output from the 8ft tibia, shown in Fig. 6.5 of last month, should be attenuated by a 100 kilohm preset potentiometer. This is connected between C7 and the common post amplifier line.







N about ten years from now we shall be able to celebrate the centenary of sound recording for it will then be 100 years since Edison produced the first talking machine, the "Phonograph". Since that time engineers have constantly strived for perfection in sound recording and reproduction, working always to maintain a standard which even as early as the 1930's became known as "high fidelity".

Today "high fidelity" means more than just good quality gramophone records and equipment for playing them. It sets a standard for the whole field of sound recording, broadcasting and

the reproduction of sound from these sources.

NFORTUNATELY the specifications for the electrical and mechanical performance of domestic high fidelity sound reproducing equipment are somewhat elastic and lacking in specific terms of reference.

Some manufacturers have taken unfair advantage of this and exploit the public at large who may have little or no idea as to what "hi fi" really means.

OBJECTIVE REQUIREMENTS

Although the object of hi fi is to reproduce as closely as possible that which might have been heard in the concert hall or the broadcasting or recording studio, there are certain limitations. For example, it is not normally practicable or even desirable to reproduce the sound of a symphony orchestra life size in the living room since this would require peak power approaching 70 to 80 watts (Fig. 1).

The "dynamic range" or degree of relative loudness must therefore be compressed somewhat for technical as well as aesthetic reasons. Much the same applies to the spatial effect obtainable with stereo, for one cannot normally hope to produce the original sound width of a large orchestra within the confined space of a living room.

On the other hand a wide frequency response, low distortion, and an absolute minimum of unwanted noise is essential. Frequency variation, caused by the

mechanical parts of recording or replay systems, must also be so low as to be virtually undetectable by ear.

SPECIFICATIONS FOR HI FI

The Consise Oxford Dictionary defines "fidelity" as "an exact correspondence of the original". When applied to sound recording, broadcasting and especially to sound reproduction in the home, the term "high fidelity" infers a faithful re-creation of the original sound. To achieve this the whole chain of equipment, from microphone to loudspeaker must perform to a very high standard, which involves laying down separate electrical and mechanical performance specifications for each piece of equipment in the chain.

Many of the terms quoted in the specification for any one piece of equipment are directly related to each other. For example, the frequency response of an amplifier is, or should be, relative to a given power output with negligible distortion. Equally, the power rating of an amplifier is, or should be, relative to a given amount of

distortion as well as to frequency response.

The signal level from any hi fi signal source (for example, a tape recorder or radio tuner) is relative not only to frequency response but also to the noise level produced within the equipment. Such information is not always given and without it a specification can be almost meaningless or even give a false impression.

PRACTICAL ELECTRONICS AUDIO SUPPLEMENT - PAGE 2

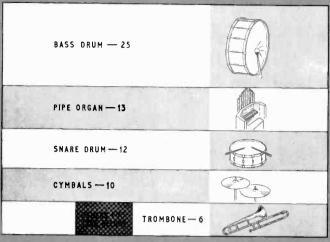


Fig. 1a. Approximate peak power of musical instruments (fortissimo playing) in watts based on measurements of sound pressure. The large outer rectangle represents 70 watts for a large orchestra

Other Instruments shown as 1.75 watts total are divided into groups of related peak power in the panel on the right

FRENCH HORN 0-05 CLARINET 0-05 FLUTE 0-06 PICCOLO 0-08 BASS VIOL 0-16 BASS TUBA 0-2 BASS SAXOPHONE 0-3	
FLUTE 0-06 PICCOLO 0-08 BASS VIOL 0-16 BASS TUBA 0-2	
BASS VIOL 0-16 BASS TUBA 0-2	
BASS TUBA 0-2	(Fig)
//	10)
BASS SAXOPHONE 0-3	Carlle Carl
TRUMPET 0:3	
PIANO 0-5	

Power output (co tinuous sine wa rating)	
Power bandwidth	20-25,000Hz (ref. 1,000Hz)
Frequency response	20-20,000±1dB (ref. 1,000Hz)
Harmonic distortion	Less than 0.5% at 1,000Hz at rated power output
Loudspeaker impedan	ce 4 to 16 ohms
Crosstalk	Better than -40dB
Channel matching	+ IdB
Bass control	± I0dB at 70Hz
Treble control	± 10dB at 10,000Hz
*Loudness Control	70Hz + I0dB, I0,000Hz +
_	5dB (ref.1,000Hz - 20dB)
Tape recording outpu	t 400mV (low impedance)
Inputs	Sensitivity Hum and Noise
	(reference 25W
	output)
Tape	400mV — 70dB
Radio	100mV 60dB
Pick-up I (ceramic)	60mV — 55dB
Pick-up 2 (magnetic)	3·5mV — 55dB
, , ,	
* Loudness controls	are not always found in British

Fig. 2. Typical example of a well presented specification for a hi fl amplifier showing acceptable terms and definitions

equipment.

A specified noise level given without reference to an output signal or power level is just as meaningless as a frequency response given without a reference frequency, or a distortion level without reference to a specified output power.

Specifications for hi fi equipment should be read very carefully. The sample specification shown in Fig. 2 is of a well known maker's amplifier and is a good example of how the technical performance should be stated. Note, for example, that hum and noise is quoted with reference to the rated r.m.s. power output. The

distortion factor is given with reference to a signal of 1kHz at the rated output power. The specification is typical of a good hi fi amplifier.

TECHNICAL REQUIREMENTS

Let us deal now with the general technical requirements for domestic hi fi and some of the facts and figures concerned with performance.

POWER OUTPUT

Here we are concerned only with hi fi amplifiers and some confusion can arise because of the different ways in which output power is quoted, one being the r.m.s. (root mean square) rating the other being so-called "music power" rating. Provided they are relative to themselves and to other performance factors, both may well amount to the same thing in the end although apparent differences may occur.

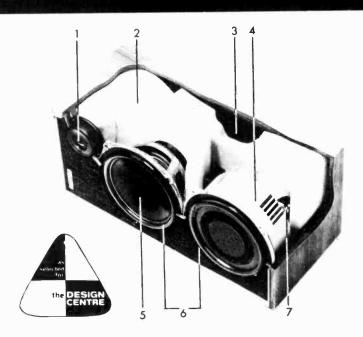
However, the r.m.s. power rating does not take into account the very short power peaks from music and is the average power developed by a continuous sine wave signal. Music power rating does take into account the peaks of power required for music which may be as much as twice the r.m.s. power. Many manufacturers have adopted the music power rating in their specifications simply because it looks more impressive. (Needless to say it originates from the U.S.A.)

Unfortunately music power ratings can be quoted in such a way as to give an unrealistic impression. For example, let's take a stereo amplifier for which the specification simply reads "50 watts output". Now the manufacturer may have deliberately failed to mention that this 50 watts is a music power rating and is also the combined output of both channels. This could therefore be 25 watts music power per channel, and may well turn out to be only 8 to 10 watts r.m.s. per channel (a more familiar rating).

With modern transistor amplifiers the so-called music power output depends very much on the d.c. power supply regulation and the efficiency of the heatsinks of the output transistors. The power supply should provide the required voltage for instantaneous large current demands, and the heatsinks should be large

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A new loudspeaker has been added to the Heathkit range. The 'Ambassador' is a first-class hi-fi loudspeaker. The cabinet comes ready assembled and finished in teak or walnut to match other current Heathkit equipment. It uses three loudspeaker unitsa 12" bass unit, a 5" mid range and a small tweeter.

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enough to prevent the start of thermal runaway in the output transistors during prolonged peaks.

With a well regulated power supply and large heatsinks, the available r.m.s. power might well be equal to the music power. A poorly regulated power supply and small heatsinks may well allow short peaks of power just long enough for the music rating to be adequate, but severely limit the available r.m.s. or continuous power.

It is always best to think in terms of r.m.s. power and unless one has an exceptionally large living room and very tolerant neighbours, 8 to 10 watts r.m.s. (per channel for stereo) is ample for a domestic hi fi system, and should be capable of handling transient peaks.

FREQUENCY RESPONSE

To say that an amplifier (or any other piece of hi fi equipment for that matter) has a wide frequency response does not mean very much. A reference frequency, usually 1,000Hz, should be given together with a reference power output or signal output at that frequency. The output level at all other frequencies can now be compared with the reference.

It is not unusual for a manufacturer to quote the overall frequency response of a hi fi amplifier relative to about half the rated r.m.s. power, although some do give a "power response", i.e. the frequency response at the full rated r.m.s. power. It would be as well to look for this in the specification because transistorised amplifiers especially will not always maintain the rated power output at the extreme upper and lower frequencies

Some manufacturers deliberately quote a "frequency range" which can make the performance look very



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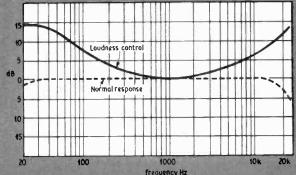


Fig. 3. Loudness control modifies the overall frequency response to match natural average hearing losses at low volume level

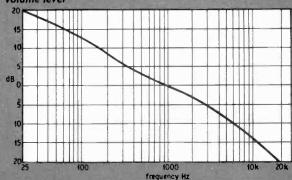


Fig. 4. Typical R.I.A.A./B.S. frequency response characteristic for the replay of fine groove discs

impressive. However, the "frequency range" is merely an extension of the uniform frequency response to the lower and higher frequencies, where the equipment may develop far too little power or signal output to be of any value. This applies equally to tape recorders, pick-up cartridges and even microphones and loudspeakers.

With hi fi amplifiers we are also concerned with the frequency responses provided by the tone controls, the loudness control (if this is incorporated) and also the special responses for signal sources such as direct replay from a tape head and pick-up. The tone controls should provide approximately 10 to 12 dB lift or cut for both the bass and treble at around 100 and 10,000Hz respectively, and with reference to 1,000Hz.

The "loudness" control, which is sometimes incorporated in some of the more expensive amplifiers from the U.S.A. and elsewhere, is designed to compensate for certain natural hearing losses when the amplifier is operating at low volume. The control automatically provides a predetermined degree of lift to the bass and treble resulting in an overall response like that shown in Fig. 3. However, some British pundits believe that this creates an unnatural phenomenon to hearing.

For reasons too complex to go into here, disc records have a special frequency characteristic. To ensure replay with a linear frequency response, it becomes necessary to emphasise the lower frequencies and deemphasise the higher frequencies and to do this the amplifier must have a special frequency response like that shown in Fig. 4. This frequency response correction (or equalisation) is normally carried out in the pre-amplifier stages and, to comply with the requirements for hi fi, must not introduce unnecessary distortion or excessive hum and noise.

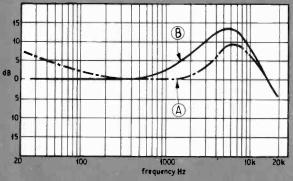


Fig. 5. Curve B Is the C.C.I.R. frequency response characteristic for a magnetic tape recording at $7\frac{1}{2}$ inches per second. In practice, and for improved signal to noise ratio, a response like that shown by curve A would be acceptable for modern tape recorders

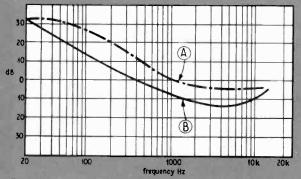


Fig. 6. Frequency response required for direct replay from a tape head. Curve B is the C.C.I.R. response for a tape speed of $7\frac{1}{4}$ inches per second. Curve A is more likely practical characteristic, particularly with modern fine gap tape heads

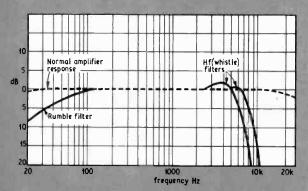


Fig. 7. Typical responses for a rumble filter and whistle filter

Much the same applies to magnetic tape replay directly from a replay tape head which also requires a special frequency response. Tape is recorded with a frequency response characteristic like that shown in Fig. 5 which necessitates bass emphasis during replay as in Fig. 6. Tape replay from a tape recorder or record/replay unit, where the signals are taken from the head pre-amplifier, does not require special frequency response correction.

Some of the more expensive hi hamplifiers have built-in filters for reducing rumble (low frequency noise) from record turntables and for reducing heterodyne whistles from a.m. radio. Such filters simply alter the frequency response of the amplifier by providing sharp cut off at the appropriate frequencies. Typical responses for rumble and whistle filters are shown in Fig. 7.

SIGNAL LEVEL AND NOISE

In this day and age of transistors, the hum and noise level in hi fi amplifiers has been very considerably reduced and performance in this respect is now generally better than that hitherto obtainable with valves.

It is not unusual to find hum and noise levels (for radio and tape recorder inputs) of 60 to 70dB below the rated output, or a ratio of -60 to -70dB, and for pick-up of -50 to -55dB. Again figures can be made to look impressive so a reference, such as the rated r.m.s. output power, should be looked for in the specification.

Much the same applies to harmonic distortion which is usually quoted as a percentage with reference to one or more fixed frequencies and the full rated output. Harmonic distortion should be less than one per cent at full rated output and preferably less than 0.5 per cent in the more expensive amplifiers.

Specifications for hi fi equipment and especially amplifiers, can be difficult to interpret and unless one is in a position to carry out a full set of performance tests there is no way of proving, other than by objective listening, whether or not the equipment really does perform as the manufacturer claims. Test reports published in the technical press can be relied upon to give a pretty clear indication as to performance for the price of the equipment, otherwise one must rely entirely upon the integrity of the manufacturer and dealer.

THE HI FI SYSTEM

So far this supplement has dealt mainly with the general technical requirements for hi fi and especially those concerned with the amplifier. Although the amplifier is the nucleus of a hi fi system, and all other units depend on its performance, even the very best of amplifiers cannot improve the performance of poor quality auxiliary equipment.

This is well worth remembering because one of the advantages of the hi fi system is, that it can be built up gradually and one need not be faced with a large initial outlay in order to get the best equipment. You can still buy the best as and when you can afford it, which immediately raises the question of what to start with and what will ultimately be worth adding.

For those who can afford the outlay for a complete ready to use system, many manufacturers are now marketing hi fi systems in matching style and performance, although even these can often be purchased piece by piece. Prices for complete outfits vary from around £80 to well over £300 with performance accordingly.

A popular system is the integrated stereo amplifier/f.m. tuner plus a disc transcription unit complete with pick-up arm and cartridge and two loudspeakers. It should be mentioned here that very few manufacturers are now making hi fi mono amplifiers except for special requirements; almost all domestic hi fi amplifiers, tuners and tape recorders are transistorised. Nearly all tape recorders in the hi fi category now being sold are also for stereo record and replay.

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Extract of letter from Mr. Wendell G. Ward, of Texas, U.S.A., Sept. 1968.

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Extract of letter from Mr. R. G. Bernaldez, of Madrid, Spain.

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The first part of this supplement dealt mainly with the objective requirements of hi fi and some of the facts and figures associated with the specification for hi fi amplifiers and ancillary equipment. One of the major problems is the choice and price bracket of the various items of equipment that constitute a hi fi system, i.e. amplifiers, tuners, turntables, pick-up arms and cartridges, tape recorders and loudspeakers.

A hi fi system can of course be made up from separate items of equipment by different manufacturers, or of units matched in design and finish made by one manufacturer. Most of the units that go to make a hi fi system, with the exception of the loudspeakers, can be installed in one large cabinet or neatly arranged on bookshelves; in fact bookshelf sized loudspeakers and amplifiers are becoming popular and greatly favoured by those who have little room space to spare.

LOUDSPEAKERS

Whilst compact amplifiers, tuners, and even tape recorders intended for bookshelf mounting, are quite efficient, the same cannot always be said of miniature loudspeakers, often with enclosures no more than 12 inches or so high. These are usually single speaker systems that often require a fairly large driving power, and lack the extended and smooth low frequency response of larger multiple speaker systems.

A good loudspeaker, capable of handling 10 to 15 watts r.m.s. power and which has a uniform and wide frequency response will invariably have two, if not three, internal speaker units plus an appropriate fre-

quency dividing network.

The frequency range covered by the speaker system as a whole is divided between the individual speaker units, i.e. bass and treble, or bass mid-range and treble as the case may be. For such systems either corner reflex or completely closed cabinets are popular although there is frequent argument among hi fi enthusiasts as to which type of enclosure offers the best performance. Listen to any of the different makes and designs and they will probably all sound slightly different anyway, but only by listening to loudspeakers in the same room setting can the hi fi enthusiast make his choice.

Generally speaking, the greater the cost the better the performance and really good speaker systems are not cheap, especially when two are required for stereo. The prices of speaker systems that could be labelled "hi fi" range from about £10 upwards per channel. The average price for a good 15 to 20 watt loudspeaker with three units, crossover network and a well designed

enclosure is around £30 to £40.

Of course, loudspeaker systems are not difficult to construct and some of the large manufacturers of speaker units may supply working plans for building enclosures to suit their particular units. Complete kits for building speaker units are also available. The saving can be quite considerable.

LOUDSPEAKER IMPEDANCE

One final point which concerns the loudspeaker impedance, and this is a very important one, has arisen with the popularity of transistor amplifiers. The common impedance of hi fi speakers has hitherto been 15 ohms to match the common output impedance of valve amplifiers, also 15 ohms.

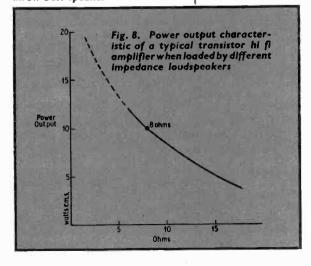
Nearly all present day transistor amplifiers will only develop full rated power at an impedance of 8 ohms. The power output decreases as the impedance of the output load (the speaker) increases. Some transistor amplifiers will develop a little more power as the load impedance is reduced but are then inclined to go unstable, or at worst the output transistors can become overheated and may even destroy themselves.

The graph (Fig. 8) shows the power output against load impedance of a typical transistor amplifier.



Ditton 25 speaker unit by Rola Celestion Ltd. Power rating is 25 watts r.m.s. using a 12in auxiliary bass radiator, 12in long throw bass speaker

WHAT
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WHEN
BUYING



AMPLIFIERS

Part 1 of this supplement dealt fairly extensively with the technical requirements and specifications for hi fi amplifiers. The earlier arrangement of a separate pre-amplifier and power amplifier that was popular for valve amplifiers is gradually disappearing, and almost all transistorised amplifiers are integrated, i.e. the pre-amplifier and power amplifier is made in one complete unit.

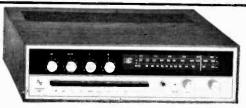
There is now a trend toward integrated tuner/amplifiers, i.e. an a.m. and f.m. tuner with a built-in amplifier having the necessary inputs for disc and tape reproduction. Some tape recorder manufacturers are also including hi fi power amplifiers within the tape recorder so that one can buy what is literally an integrated tape recorder/amplifier having inputs for disc and radio reproduction.

So the choice in this respect is quite wide and useful. For instance, for those who are inclined toward tape recording, especially for its creative aspects, may find it cheaper to buy a tape recorder with built-in power amplifiers. Those whose chief interest is radio programmes at high quality, may of course find the integrated tuner/amplifier a better proposition.

The prices of these combination systems vary very little as far as different makes of repute are concerned and the outlay would be in the region of £80 to £120 for a top performance tuner/amplifier and certainly over £100 for a hi fi stereo tape recorder with built-in power amplifiers.

The now more conventional integrated hi fi preamplifier/power amplifier systems range in price from about £40 (budget class and limited flexibility and performance) to over £100 for top performance and fairly large power rating.

One in this latter category, oringinating from Japan, is rated at 60 watts music power per channel. Its r.m.s. power performance is also very good as is the general overall performance. This retails at £90 and caters for mono or stereo, tape, disc, radio and microphone and includes such refinements as overload meters, loudness control, filters for treble and bass, separate tone controls for each channel, and so on.

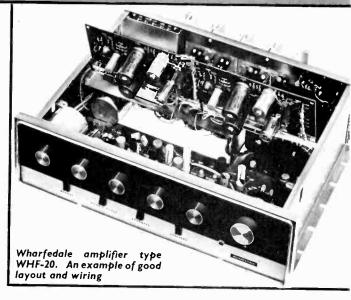


Armstrong 526 f.m./a.m. mono/stereo tuner

TUNERS

The radio side of hi fi is, of course, mainly concerned with v.h.f./f.m. mono and stereo broadcasting, which should but does not always reach the strictly hi fi level. However, the tuner and/or tuner/amplifier, employ much about the same kind of circuitry, so there is little choice from this point of view, and most available now are transistorised. A good signal to noise performance is important especially for the reception of stereo broadcasts.

Tuners are available for mono reception only, in which case they will not include a stereo decoder unit,



AMPLIFIER PERFORMANCE

Unfortunately the buyer of hi fi equipment often has no way of assessing the quality and performance of items like an amplifier or tuner except by listening, and even this will convey very little unless a direct comparison can be made with other equipment of known performance.

The ears can become quite satisfied with the reproduction from a radio set or record player of moderate performance; even a very cheap so-called hi fi system (and there are plenty on the market) can sound quite pleasing to those who have heard nothing better.

When buying any hi fi equipment it's not a bad idea to have one or two of the most expensive items demonstrated first and then hear how cheaper versions compare with them. The dealer might be offended but it's your money that's being spent. It is also worthwhile studying the reviews and test reports that appear in the "hi fi" technical magazines.

but since stereo/mono transmissions are compatible, a mono tuner will receive stereo transmissions and provide the audio signal output in mono. Tuners are available for f.m. reception only and, unless one really wants medium and long-wave reception, there is little point in spending the extra money for it.

There are few if any technical problems with tuners except perhaps with reception in fringe areas, i.e. on the edge of the expected good reception zone, or in low lying pockets with intervening hills. An a.f.c. control is valuable if frequency drift is likely to occur.

A good aerial is essential for proper reception of f.m. stereo broadcasts in which the noise level is around 3dB greater than that of mono transmissions. A poor aerial will increase the noise level even more. You should consult your local dealer to find out if a specially large array is needed.

Most manufacturers can supply stereo decoders that can be fitted later to mono only tuners, but be sure to verify that the mono tuner can be adapted for stereo, and allow for the possibility of having to increase the number of elements on the aerial for stereo if perhaps only one or two elements were adequate for mono.

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As we said at the outset, if you are after top-class hi-fi you don't want the 127, what you want is the Armstrong series 400 or series 500 models.

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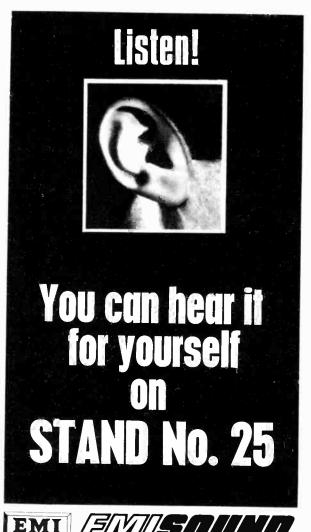
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RECORD TRANSCRIPTION UNITS

The hi fi enthusiast recognises that the turntable unit must be of a high quality, especially if he respects his records and cares for them. He does not like the "record player" which often denotes an automatic record changer that are often more clumsy than the human hand.

The transcription unit, however, does imply a heavy turntable, precision pick-up arm and cartridge and all three items can be purchased as completely separate items from two or more manufacturers or as one complete unit by one manufacturer, ready to install and use. The choice is wide and prices range from around £15 for a complete but modest form of unit to over £40 for a top quality turntable alone.

Pick-up arms and cartridges also have a very wide price range, making choice somewhat difficult; they can cost as little as £8 or up to over £30. The variations in design are so complex and so varied that a whole article could be devoted to any one type and its technical performance.

Pick-up cartridges that can be classified as hi fi also vary in price from around £4 to £5 to nearly £50! Again the variations in design and performance are too numerous to deal with here.

The average ear, especially one unaccustomed to hi fi reproduction, would find it difficult to detect audibly any great difference in performance between all but the very cheapest and most expensive of the pick-up



cartridges. Price is the best guide and the average price for a good cartridge is around £12 to £15.

Beware of very cheap or even so-called "budget priced" equipment. A complete transcription unit comprising turntable, pick-up arm and cartridge that would stand up to exacting tests for hi fi performance would cost in the region of £30 to £40 minimum.

TURNTABLE

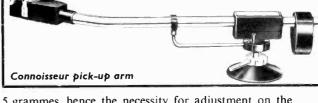
What should one look for technically? Well as far as turntables are concerned the platter itself should be heavy and turn with a speed accuracy of less than ± 1 per cent. Wow and flutter (or variations of nominal running speed) should be less than 0.1 per cent, and few except very cheap turntables are any worse than this.

PICK-UPS

The best pick-up arms often incorporate a number of devices to ensure correct tracking, balance and stylus pressure. They are usually fairly expensive but one is at least assured of a really high performance with minimum disc wear. Such pick-up arms do, of course, warrant the use of an equally expensive cartridge and there would be little point in doing otherwise.

Whatever the other performance factors may be and whether they are adjustable or not, a good hi fi pick-up arm must have provision for setting the tracking pressure to between a \(\frac{1}{4} \) and 5 grammes. The exact pressure depends on the pick-up, so the manufacturer's recommendation should be followed.

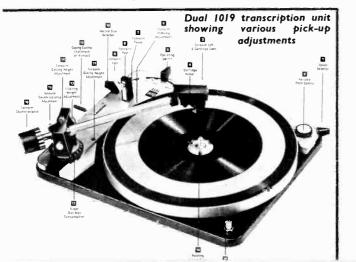
The performance of a pick-up cartridge is almost impossible to estimate just by listening and the technical specification will convey little to the layman. However, a low tracking force (sideways movement restriction) is essential, although this may be anything between $\frac{1}{4}$ and



5 grammes, hence the necessity for adjustment on the pick-up arm.

The frequency response of a good cartridge should be in the region of 20-20,000Hz \pm 2dB and for stereo cartridges the channel separation should be better than 25dB. Deviation in the output signal from each channel should be not more than \pm 1dB over its working frequency range.

Most modern magnetic cartridges have an output of around 5mV at 50 kilohms or so impedance, so remember that the amplifier must have appropriate input facilities if a magnetic cartridge is to be used. Average price for a good cartridge is about £15, but one at £20 to £25 will sound just that bit better.



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TAPE RECORDERS

The tape recorder is now very much considered as part of a hi fi system and for this reason many hi fi tape units have made their appearance recently. The tape unit has full provision for recording, with inputs for radio and microphone, sometimes with provision for mixing, and suitable recording level meters.

They also have playback pre-amplifiers that provide a linear output signal suitable for direct connection to a hi fi amplifier system. For this reason they seldom have built-in power amplifiers and loudspeakers.

A more recent arrangement is to incorporate hi fi power amplifiers but not loudspeakers. This enables one to use the recorder with appropriate hi fi speakers as a hi fi system.

The majority of tape recorders rated as hi fi are also stereo machines; in fact few mono only recorders are now being made. Aside from such functions as stereo or mono recording, or replay, many of the higher priced recorders include the track-to-track or multi-play facility, dual channel mixing, provision for introducing echo, and so on.

The choice of a tape recorder as a hi fi signal source warrants a little thought since tape recording itself can be quite creative as one may soon discover when using a tape recorder. The machine should not be too limited for really creative purposes.

If the recording activity is to be strictly for hi fi listening, then a good quality stereo tape replay unit (or



Trio TT-10 4-track stereo tape deck

one with output stages) may suffice. However, tape recorders that could be classified as having a hi fi performance do not come cheaply.

Tape units range from about £50 to £60 upwards; it is very unlikely that lower priced machines will have provision for mixing and track-to-track recording. Tape recorders with power output stages and with extra facilities like track-to-track dubbing will be over £150 for something strictly hi fi and can cost as much as £300.

TAPE PERFORMANCE

The technical performance of tape recorders that come within the hi fi category is fairly standard and has improved quite considerably with the introduction of extra low noise transistors. Few, if any, tape recorders of good quality now employ valves.

One can expect a good frequency response from 30 to 18,000Hz even for a tape speed of 3\(^4\) inches per second with modern tapes and ferrite heads. Signal to noise ratio of better than 50dB is possible on quarter-track recording. As far as quarter-track or half-track is concerned, there is little difference these days in actual performance and if one requires to make long recordings with a minimum amount of tape then quarter-track is recommended.

The mechanical performance of modern tape recorders of good quality can also be relied upon. Wow and flutter and nominal speed variation is usually so low as to be undetectable by ear even at the lower popular tape speeds of $1\frac{7}{8}$ and $3\frac{3}{4}$ inches per second. As with most transistor audio equipment made now, printed circuit assembly is employed and some manufacturers even fit exchangeable circuit boards, thus simplifying service and repair.

CONCLUSION

Readers who have read this supplement through from Part I will realise that the technical performance, specifications and choice of hi fi equipment could not possibly be covered to its fullest extent nor in any great detail here. The choice of equipment is enormous and the variations may at first cause confusion.

The first step to making a choice is best taken by collecting as many leaflets and brochures as possible on different makes and types of equipment and by these compare specifications and prices. Make a short list and then try to find a dealer willing to demonstrate various combinations of the different items you have chosen. Try not to be put off by sales talk that may confuse you even more. The price tag can give a pretty good idea as to quality and performance but is not in itself conclusive evidence of true hi fi standards throughout.

Hi fi is a very broad term, so far without laid down minimum performance figures. It has developed over several years from the experience and desire of enthusiasts, who wish to reproduce in their own homes as near a faithful acoustic quality as was heard at the performance. The two parts of this supplement has attempted to illustrate how one can achieve this measure of fidelity within the limitations of currently available equipment.

A later article will be published describing installation and maintenance of hi fi equipment.

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RECORD PLAYING UNITS

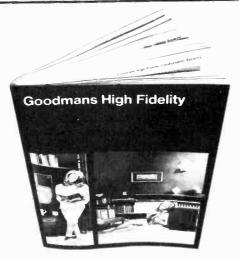
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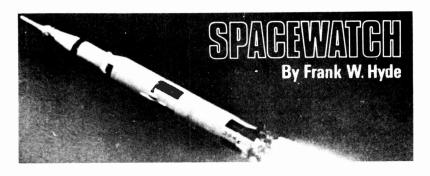
The Wharfedale Unit 3 kit includes an 8" speaker unit, an acoustiprene tweeter, a cross-over unit, and acoustic wadding with all the necessary bolts and wiring. The detailed instructions are easy to follow and include full assembly diagrams and plans for two different styles of speaker cabinets.

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MOON ROCK RESULTS

In the first reports of the biological examination of the lunar rock samples collected by Armstrong and Aldrin, Dr W. Schopf of the University of California finds no evidence of lunar organisms "living, dead, or fossilised". It seems that earlier reports are now discounted and the apparent organisms the result of earth contamination. The carbon content so far established is less than ten parts per million. This can be the level that could result from the handling of the materials using rubber gloves and tools.

Mice injected with lunar material have not exhibited any unusual behaviour. Six cell culture samples have been examined and some of the cultures of human embryo lungs and kidneys have shown no signs of the growth of bacteria. The experiments in this field will go on with special observation of the effects on reproduction of animal and plant

species.

Radiation checks on lunar rocks have shown the presence of thorium, potassium, sodium-22, strontium-46 and manuranium. cobalt-56, strontium-46 and man-ganese-54. The level of the thorium content of both the rocks and the dust is higher than that found in meteorites but lower than that found in terrestrial basalt.

This part of the work carried out by Dr D. O'Kelly of the Oak Ridge National Laboratory has also disclosed that the moon rocks contain less uranium and potassium than earth rocks. He states that the sodium-22 is formed by cosmic ray

bombardment.

SOLAR-WIND GASES

At New York State University, Dr O. Schaeffer has detected a large amount of solar-wind gases, more than anyone has suspected. The gases are mainly hydrogen and helium but he has also detected argon, neon, krypton and xenon. The blackish colour of the surface dust is thought to be the result of bombardment by the solar gas. It is claimed that some 20 to 30 per cent of the moon dust comes from molten particles.

In the second box of rocks which was opened on August 4 there were 30 rocks of various sizes. Some of these are quite different from anything on earth and may offer some interesting minerological facts. There were about 40lb weight of rocks of a medium grey colour and more angular and fractured than those in the first box opened. In these latest rocks to be examined there are signs of crystalline and opaque metallic clusters.

MARINERS 6 and 7

The results that are now being released from the two Mars probes, which were so successful in the Mars flypast in July and August, are causing a considerable amount of speculation and quite a number of new questions are posed when the data is examined. The Mariners have shown that Mars is anything but a hospitable planet by earth standards, it would seem that it is more like the moon than the earth. thing is certain and that is that there are many questions to be answered and that we know somewhat less than was thought as far as this red planet is concerned.

Photographs taken with filters attached to the cameras show no signs of the blue haze consistently reported by earth based astronomers. Again the close-up shots with provision for seeing in ultra-violet and blue light, do not confirm the haze at the poles which appears on the distant

SPECTROSCOPIC STUDIES

Dr G. C. Pimentel of Berkley, California, who is concerned with the spectroscopic studies, asks why is it that the absorption lines which indicate the presence of methane and ammonia appear just above the dark rim which surrounds the receding polar cap. Why is it that these gases appear there and only there. Could it be that life of a sort could exist in this marginal area where there is possibly melting hoar-frost.

The spectrometer experiment set up by Dr C. A. Barth of the University Colorado has revealed that of although there are features on the surface of Mars which suggest volcanic conditions, there is no sign of molecular or atomic nitrogen in the upper atmosphere of the planet. These findings differ from those that occur on earth.

One explanation from Dr D. N. Horowitz of California Institute of that suggests Technology, Martian nitrogen may have been oxidised by carbon dioxide in the atmosphere and is now in the soil as nitrate. Some experiments carried out at Caltech support this view.

POLAR CAPS

Meanwhile a controversy arises from the differing views of Dr R. R. Leighton of Caltech and Dr C. Hord of the University of Colorado regarding the nature of the polar caps. Dr Leighton, basing his statements on radiometer and ultra-violet spectrometry, argues that the polar caps are solid carbon dioxide some three or four feet thick and deposited by conditions of the Martian winter as snow. He maintains that water vapour is only present in very small amounts in the atmosphere and could not be transported to the poles with enough speed to form more than a very thin layer of hoar-frost.

As further support for Leighton's view is the presence of what appear to be configurations of the caps resembling snow drifts. As against this the infra-red spectrometer gives a temperature which is too high for the presence of solid carbon

dioxide.

While Dr Hord is prepared to accept thin water ice with carbon dioxide superimposed, his ultra-violet spectrometer measurements do not support the presence of carbon dioxide clouds, because the atmosphere above the polar caps is highly transparent.

PLAIN OF HELLAS

Another puzzling observation by the Mariners shows the plain of Hellas, which is about one million square miles in extent, to be quite different from all other areas on Mars in that there are no craters within the

boundary escarpments.

Interest has also been aroused by the observations from the spacecraft of bright streaks curling across the high plateau known as Tharsis, and earth based observers have reported similar recurring features, thought to be cloud formation. At Goldstone, Dr R. Goldstein has used the large space tracking telescope in the radar mode and finds that this area is very high above the surrounding terrain.

Photographs from Mariners 6 and 7 spaced several revolutions of Mars apart, do not confirm the recurrence of markings which change in character. It is suggested by this that rather than cloud formations these are variations which appear on the surface due to the changing of the incident light in the Martian after-

noon.

P.E. WIDEBAND H.F. GOMMUNIGATIONS RECEIVER

By R. HIRST S.T.C. LTD.

PART TWO R.F. MODULE

Last month an overall description of the complete receiver was given. Now each module has to be considered in detail. This present article deals with, firstly, the construction of a standard housing for the modules; and secondly, the assembly and testing of the first module—the R.F. Unit.

MECHANICAL CONSTRUCTION OF MODULE CONTAINERS

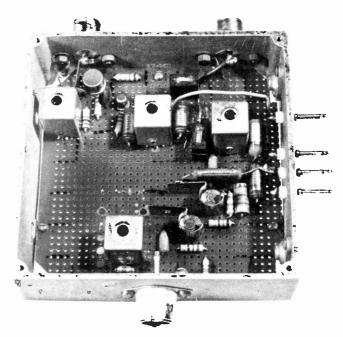
As it is difficult to locate suitable boxes for this type of construction it was decided to manufacture a set of identical containers from sheet aluminium. These boxes have to be reasonably accurate if the final mechanical assembly is to go together with ease.

The first step is to accurately cut a piece of wood, preferably a very hard wood, into the shape indicated in Fig. 2.1. This is now the master template for all the boxes (seven will be needed). The 16 s.w.g. aluminium should be cut into strips 14½ inches long and 1½ inches wide and two holes should be drilled in one end as shown in Fig. 2.1. This end of the strip should be fixed to the wooden template, exactly on the marker, with two screws. Now proceeding to the first corner, bend the aluminium strip firmly at this point and after bending tap both sides of the corner with a hide or wooden mallet. Having ensured that the corner is a good fit proceed to the next corner and so on until all the corners have been made.

If the job has been carried out correctly there should be a 4in overlap. Temporarily easing the strip to one side, remove the two pilot screws and trim the last quarter of an inch at each end. The assembly should now be squared up and two further holes drilled in the other end of the strip to line up with the joining strip. When the container is bolted up, the box should be rigid.

The round rod should be cut into the required length and drilled and tapped accordingly. These rods are Araldited into the corners of the container as shown in Fig. 2.1. The corner blocks should be allowed to set for 24 hours in a reasonably warm room. Two 6B.A. hank bushes should be fitted into the base of the box and the lead through connectors can also be fitted in this final stage. Fig. 2.1. also shows an alternative method of making the corner fixings.

It is wise to take considerable care in the manufacture of the boxes as it will save endless filing and cutting at some later stage, possibly with detriment to the circuitry. For the constructor who does not wish to go to the bother of making the mechanical assemblies it is possible to use the diecast box type 46RCS00043A00, stock number 268X0075F supplied by Electroniques at 6s 11d each. It will mean that a slightly larger cabinet will have to be purchased to house the receiver.



R.F. UNIT CONSTRUCTION

The complete circuit of the r.f. unit (module 1) appears in Fig. 2.2. This should be studied in conjunction with the description given in Part 1 last month. Reference should also be made to the block diagram of the complete receiver. Fig. 1.4.

of the complete receiver, Fig. 1.4.

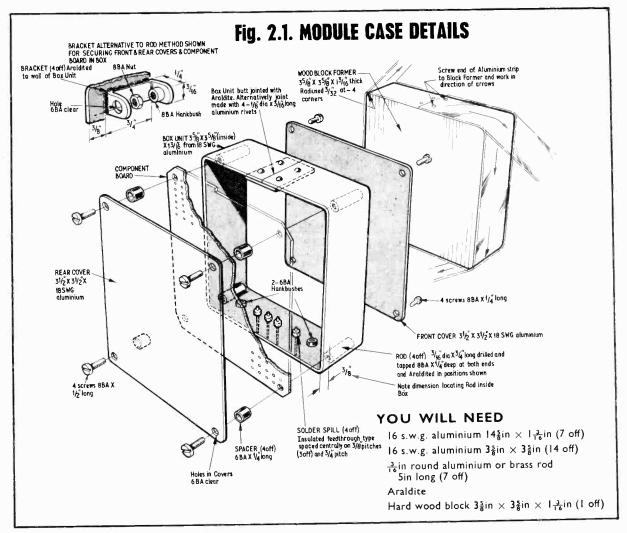
The inductors L1, L3, L4, L5, and the transformers T1, T2 have to be constructed according to information given in Fig. 2.5. All winding details, as well as the various purchased items needed, are included in this drawing.

When these components are completed, work can commence on the circuit board assembly. A piece of s.r.b.p. board 3½in by 3½in with perforations on a 0.1in grid (plain Veroboard) is required. Components are mounted as shown in Fig. 2.3 and the wiring completed on the underside as in Fig. 2.4. Note that four capacitors are also mounted on the underside.

The completed circuit board is screwed into the module container and the three coaxial sockets SK1, 2, 3, and the four pins of PL4 wired up as shown in the diagrams.

SETTING UP INSTRUCTIONS

The following instructions are for the constructor who has sufficient resources at his command to enable the setting up of the units to be carried out individually.



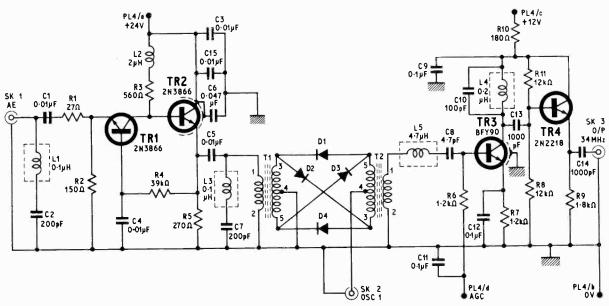
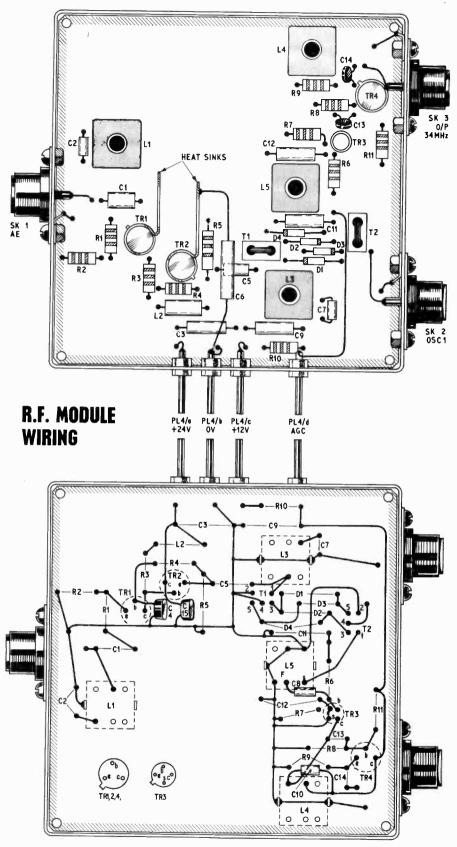


Fig. 2.2 The complete circuit diagram of the r.f. module



COMPONENTS ...

JUMI	YUNI	EN IS	.
Resis	tore	_,,,,	•••
R I R2 R3 R4 R5	27 Ω 150 Ω 560 Ω 39k Ω 270 Ω	R7 R8 R9 R10 R11	
carbo			stability
Capa	citors 0·01μF	paper	foil
C2	200 _P F	lunts Me polysty	etalmite) yrene, 5%
C3 C4 C5 C6 C7	0·IμF 0·0IμF 0·0IμF 0·047μF 200pF	polyes cerami paper polyes polysty	ter ic foil ter yrene.
C8	4·7pF	polyst	5% yrene, 5%
C9 C10	0·1μF 100pF	polyes polysty	ter
C11 C12 C13 C14 C15	0 lμF	polyest polyest cerami cerami	ter ter c c
Trans TRI	istors 2N386	6 R.C.	A . or
TR2	2N386	6 R.C.	lotorola A. or
TR3 TR4	BFY90 2N2218 Texas	Mulla	ard,
Induct L1 L2 L3 L4 L5	0·IμΗ 2μΗ (Paintoi 0·IμΗ 0·2μΗ 4·7μΗ	}	ambion) ig. 2.5
Diode: DI D2	OA47 OA47	_	DA47 DA47
TI T2	ormers Widebar Widebar see Fig.	nd Trans	former former
Socket SKI-	coax	miniatu ial chass	sis
PLI-3 PL4	(3 of Plug (3 of Four insul lead- conn	s for abo f) Helleri	ove man
Plain	l aneous Veroboa o.), 0·lin	rd (perf grid, 3	orated ½in ×

Fig. 2.3 and 2.4 Component layout and wiring of the complete r.f. module

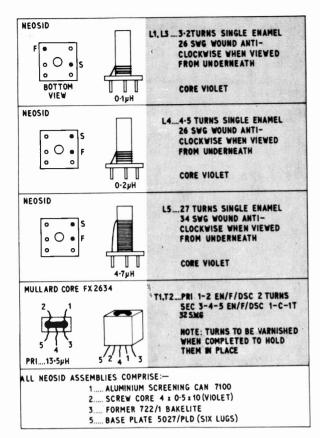


Fig. 2.5 Coil winding details

(Similar instructions will be given for all seven modules, as they are dealt with in turn.)

Equipment required

(a) Power supplies, 24V 100mA, 12V 20mA and 2.5V 5mA.

(b) High frequency generator. Capable of delivering 100 millivolts into 50 ohms at 2MHz to 34MHz.

(c) High frequency generator. Capable of delivering 500 millivolts into 50 ohms at 32MHz to 64MHz.

(d) Valve voltmeter. Capable of measuring 2MHz to 34MHz from 100 microvolts to 1 volt.

PROCEDURE

Apply the two h.t. potentials and set the incoming a.g.c. voltage at the terminal to read 2.5 volts. Check all the d.c. potentials at the base collector and emitter of each of the transistors to ensure that they coincide with the levels indicated in the D.C. Voltage Chart (Table 2.1). If the potential at the emitter of TR2 is not within 2 volts of the specified value R4 may be increased or decreased until the voltage level at the point in question is approximately 17.3 volts. Once this level has been achieved check the other d.c. levels again.

Having ensured that the circuit is working from a d.c. point of view apply a 100 microvolt signal to the input Socket SK1 and measure with a low capacity, high impedance, high frequency valve voltmeter across pins 1 and 2 of T1. The frequency of the input signal should be 2MHz. Approximately 500 microvolts of signal should be measured upon the valve voltmeter.

Change the frequency at the input Socket SK1 to 34MHz and increase the level of the input signal to

Table 2.1. R.F. UNIT D.C. VOLTAGES

	age	Voltage
TRI	Vc	187
	Ve	1·25V
TR2	Vc	24V
	Ve	17·3V
TR3	Vc	IIV
	Ve	1·75V
	Vb	2·4V
TR4	Vc	11.17
	Ve	4.57
	VЬ	5V
-at for 2.5	V at a.g.c. terminal	All above reading

100 millivolts. Tune L1 and L3 for minimum output on the meter. (Core sealer should have been applied to the cores of both these coils before this adjustment is made).

With a.g.c. voltage set at 2.5 volts the input signal should be removed from Socket SK1 and transferred to Pins 1 and 2 of T2, the level being set at 10 millivolts at 34MHz. The valve voltmeter should be placed across Socket SK3 and L4 and L5 should be tuned to give maximum reading on the valve voltmeter.

Now remove the input signal from T2 and apply it once again to Socket SK1 with the frequency set at 2MHz at a level of 10 millivolts. Leave the valve-voltmeter connected across Socket SK3 and then apply a 500 millivolt signal at 36MHz to Socket SK2 (this level measured after connection). Retune L4 and L5 for maximum output. (Core sealer should have been applied to these cores prior to adjustment.)

The r.f. unit can now be considered to be set up. *Note*: it was incorrectly stated last month that the dynamic range of the r.f. amplifier was 54db, it is in fact 114db.

Next month: constructional details of the i.f. unit

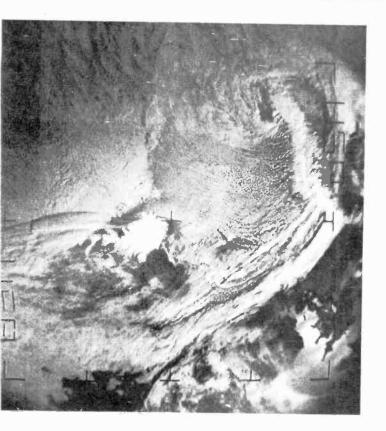
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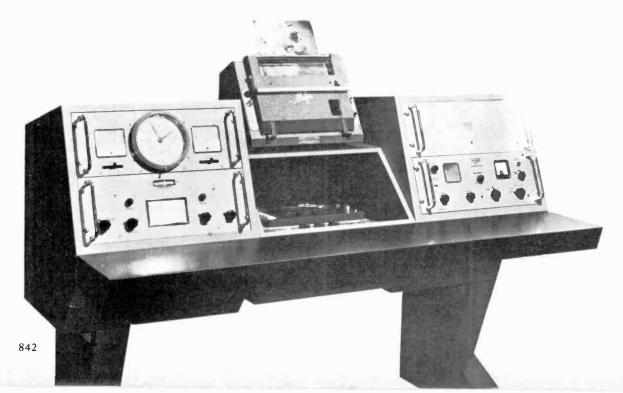


Five New Picture Receiving Stations

THE British Meteorological Office has ordered five automatic picture transmission receiving stations to improve short and long term weather forecasts. The receiving stations will be installed overseas in Europe, Africa and the Middle East by Meteorological Office engineers. Each receiving station consists of four principle units; an antenna assembly, a receiver, a facsimile recorder and a tape recorder. With the exception of the antenna, all units are situated on the control console shown below. Pictures, such as that on the left, covering an area of about 2.5 million square miles and showing cloud cover over the earth, can be received direct from weather satellites while they are above the stations' horizon.

The picture transmitted from an ESSA 8 satellite (left) shows cloud cover over Iceland, Greenland, Norway and Sweden. A ridge of high pressure over the United Kingdom (bottom right) is forcing the weather front to the north-east, giving fine weather

The basic console of the receiving station (below) manufactured by Hawker Siddeley and incorporating a Muirhead picture recorder. The picture can be seen at the top centre of the console





X-ray Equipment Helps Search for Life's Secrets

SPECIAL x-ray defraction equipment that allows scientists to examine protein molecules, which are a central component of living matter, has been developed by Elliott-Automation in collaboration with the Medical Research Council's Molecular Biology Laboratory at Cambridge.

The device, called a fine focus, rotating-anode x-ray diffraction equipment, is to be used to help determine the three-dimensional chemical architecture of protein molecules, an essential step in understanding the basic processes of life and therefore of abnormalities such as cancer.

The x-ray equipment has become an important export; sales have already reached £250,000. The equipment, shown in use on the left, is the only system with this capability available anywhere in the

world.

Fuel-cell Battery for Undersea House

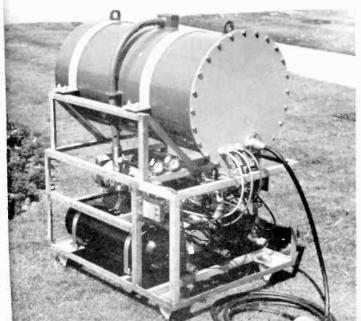
A TEAM of British scientists and engineers from Imperial College and Enfield College has recently successfully completed a series of experiments with a new "undersea house" submerged off the Maltese Coast. Relays of divers used the house and lived in it continuously for up to six days, during which time the structure and systems needed to operate the house above and beneath the water were sested.

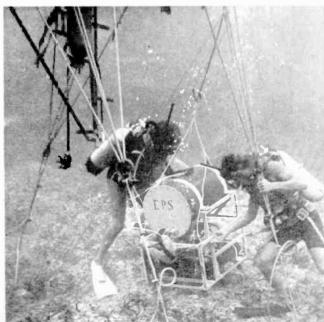
The new type of house needs no "umbilical cord" to the surface as food, air and water are provided by a life-support module powered by a fuel-cell battery designed and manu-

The complete fuel cell pictured before its installation. Supply cylinders can be clearly seen under the drum which houses the cell factured by Electric Power Storage Ltd. This is the first time that such a cell has been operated at the surrounding pressures involved; the metal drum which houses the cell is filled with nitrogen to balance the pressure inside the drum to that of the sea water.

The battery produces 12 volts from 16 hydrogen-oxygen cells and the supply cylinders contain enough gas to produce 50 watts of power for seven days' continuous operation. The battery can operate continuously for one month and, apart from replenishing the supply cylinders, needs no attention for this period; the design on which the cell is based has been in operation for up to three years under laboratory conditions.

Two divers working on the fuel cell during its installation. The entrance to the house can be seen in the background





TIME

LAPSE CINE

By
D. Burn Ph.D.
and
E. W. Summers B.Sc.

A NYONE who has seen films which apparently speed up movement, like the miraculous unfolding of a flower in a matter of seconds, will no doubt have been intrigued at the results of time-lapse cinephotography. Although widely used as a scientific tool, this branch of the camera-man's art can also provide interest and some amusement by enabling one to compress into half a minute a continuous event which may have taken hours or even days to complete.

A simple and inexpensive device is described which will allow cine-camera owners to photograph their own time-lapse sequences. In essence, a relay is energised at pre-determined intervals, actuating the camera shutter and exposing a single frame of film at a time.

As the normal running speed of a cine camera is 16 or 18 frames per second, this means that for a "shooting" interval of one second, the action is speeded up nearly twenty times; the result is that pedestrians appear to rush about at 40 m.p.h. to dodge cars hurtling along at 600 m.p.h.

It is essential that the cine camera should have provision for single frame operation. Less essential, but none the less desirable features include electric drive, for extended runs, and automatic exposure control to compensate for varying light conditions.

TIMED PULSE GENERATOR

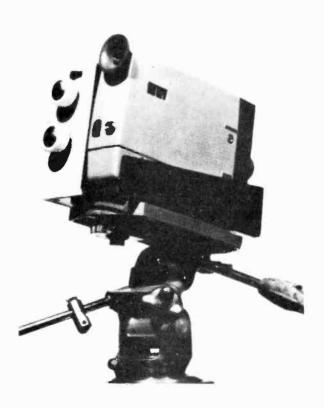
The circuit was designed around a P.O.3000 type relay. Preliminary tests had shown that this relay, in a suitably modified form, had sufficient power to operate the shutter. Timing pulses are produced by the relaxation oscillator TR1 (Fig. 1).

Three ranges are provided, selected by switch SI, continuous control within each range being provided by the variable resistance VR1. The frame rates with the capacitors shown are roughly 1-10 seconds (C1), 6-70 seconds (C2), and 35 seconds to 7 minutes (C3).

The pulses obtained at base-2 of the unijunction transistor are much too short to operate the relay and are therefore "stretched" to about 0.5 second, determined by R7 and C5, by the monostable formed by TR2 and TR3. The fastest practical pulse rate is therefore about 1 frame per second, and is set by the smallest timing capacitor C1 and resistor R1, with VR1 at minimum value.

The negative-going 0.5 second pulses at TR3 collector are passed via R9 and R10 to the output stage consisting of TR4 and TR5 arranged as a Darlington pair.

Although the power requirements of the relay are quite modest, a power transistor has been selected for TR5 to ensure that no overheating occurs, particularly during long runs at high pulse rates. R11 is included to keep down the leakage current of TR5, whilst D2 protects it from transient back e.m.f. when the relay turns off.



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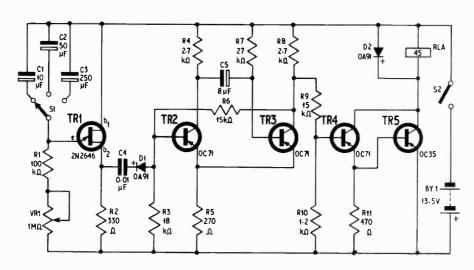


Fig. 1. Complete circuit of the camera triggering unit

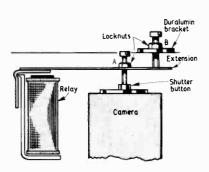


Fig. 2. An extension bar is fixed to the relay armature (Araldite can be used), but at a slight angle to suit the position of the camera button (see photograph). Relay movement is adjusted by set screws A and B

glued or bolted to the armature) should be positioned so that the extension comes just in front of the shutter button. It can then be firmly bolted to the base.

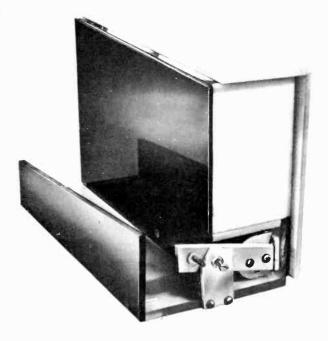
Adjustment of the relay is quite critical and is accomplished by means of two set-screws, A and B (Fig. 2). Screw A is fitted to the relay extension and is adjusted so that the shutter is just operated when the relay is fully closed. Screw B is fitted to a bracket mounted on the base and is set so that the extension arm moves back just sufficiently to allow the shutter to reset.

PHYSICAL LAYOUT

Since a compact and rigid unit is desirable, it was decided to build the device to fit the camera. For this reason, no detailed drawings are given of the case. The photographs and drawings illustrate the essential features and it should not be difficult to design a unit suitable for the type of cine camera used. The case is made from sheet Perspex since it is easily worked and results in a pleasing appearance.

The author's camera (an Ilford "Elmo") was very easy to use since the shutter button is situated at the bottom edge of the front panel, and both the camera and the relay could be mounted on a common baseboard. Along one side of the base is a side wall which serves to locate the camera, which in turn is held firmly in place by a \$\frac{1}{2}\$ in Whitworth bolt into the tripod bush. The other side of the base is occupied by a box housing the relay and, over it, the batteries and electronics.

Once the camera has been fixed, the relay (minus its contacts and with a lin duralumin extension arm



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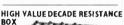
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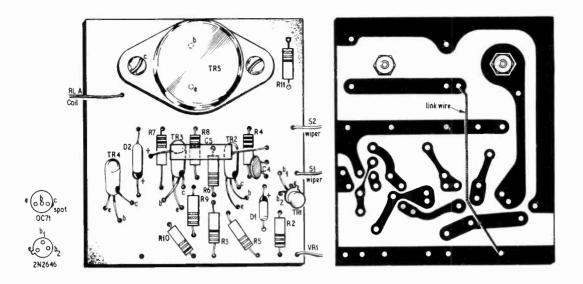


Fig. 3. Full size layout of components on the printed circuit board

COMPONENTS ...

Resistors $100k\Omega$ RI R2 330Ω I8kΩ R3 R4 $2.7k\Omega$ R5 270Ω $15k\Omega$ R6 R7 $\textbf{27} \textbf{k} \Omega$ R8 $2.7k\Omega$ R9 $15k\Omega$ RIO $1.2k\Omega$ RII 470Ω All 10% &W carbon

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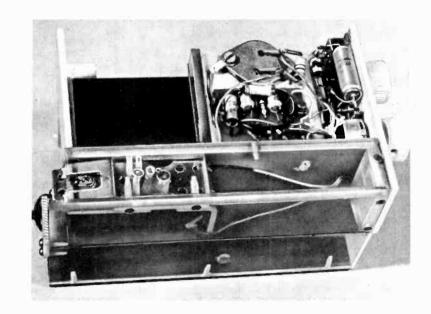
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Batteries

BY1 13.5V (made up from three 4.5V flatpack batteries No. 1289)



Switches

- S1 Single-pole, 3-way wafer switch or 4-pole 3-way wafer using only I pole
- S2 Single-pole on-off slide switch or 2-pole 2-way slide using only I pole I way

Miscellaneous

Printed circuit board $2\frac{1}{2}$ in \times $2\frac{1}{4}$ in Perspex sheet \$\frac{1}{4}\in, \frac{1}{6}\in, \text{thick} Sponge plastics padding Knobs, nuts and bolts

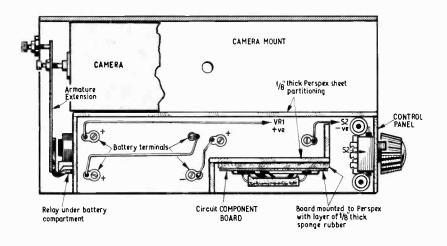


Fig. 4. Layout of the triggering unit showing the battery positions and component board

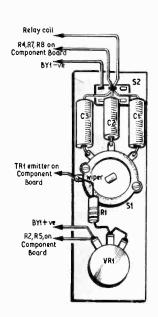


Fig. 5. Wiring of the control panel components

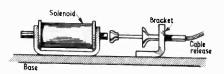


Fig. 6. Solenoid operated cable release as an alternative shutter control

ELECTRONICS BOARD

The circuit requires a 13.5 volt d.c. supply which is obtained from three 4.5V flatpack batteries. They are mounted in the box with their contacts folded over to press on suitably placed 4B.A. bolts (with solder tags) set in the base. To allow easy changing of the batteries, the side and top of the box can be removed together. A block of sponge plastics is glued to the top to ensure that good contact is maintained between the batteries and the terminals.

The space corresponding to what would be the fourth battery, is in fact occupied by the electronics, mounted on a printed circuit board. This board (Fig. 3) holds all the components except switches S1 and S2, capacitors C1, C2, and C3 and VR1 together with R1. The power transistor TR5 operates well within its ratings and does not require a heat sink; it may therefore be mounted on the circuit board.

A compartment, constructed of h in Perspex, is fixed into the box to keep the batteries in place, and the circuit board is fitted with sponge plastics glued to the Perspex. The complete wiring diagram is given in Fig. 4, with front panel wiring in Fig. 5.

OPERATION

A standard 50ft run of film, having 72 frames per foot, has about 3,500 frames available for a run, allowing some 100 frames for a safety margin. Knowing how long is required for a run, it is easy to calculate the required frame rate, and the controls on the unit can then be set to give this rate.

The camera should be mounted on the base plate of the control unit, and the set screws A and B checked to ensure that the shutter is operating correctly. Where the camera cannot be adapted, an alternative solution would be to use a cable release and actuate it by means of a small solenoid. Fig. 6 illustrates one way this might be achieved.

Before starting a run, care should be taken to fix the unit very firmly so that no movement can occur. Now all that is needed is patience!

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KING OF THE PAKS BI-PAK GUARANTEE SATISFACTION OR MONEY BACK By F. J. Stone

CONDUCTIVE GLASS

CONDUCTIVE glass to many people will trigger off inventive thoughts connected with photo-electric devices. Anyone who wishes to obtain some of this material to experiment with will find out that it is not so easy as it might seem. But if they are determined enough they can make their own. This article describes the method developed by the author for making transparent conductive glass, by plating glass with a thin film of tin oxide. It also describes some unusual properties and possible applications of conductive glass.

The processes detailed below are safe and harmless if all normal precautions are taken. This implies that some experience in chemical laboratory practice is required.

MATERIALS REQUIRED

The materials required are glass, stannous oxide (SnO); hydrochloric acid (HCI); and an electric hot plate. Glass is easy to obtain (a local glazier will only be too pleased to sell some odd cuts). Stannous oxide generally needs to be ordered through a local chemist (100g are about 25 shillings). But most chemists can supply hydrochloric acid (about 5 shillings a bottle). Both the stannous oxide and the hydrochloric acid must be as pure as can be obtained. The electric hot plate must be of the square type.

PREPARATION OF STANNOUS CHLORIDE

Mix a small amount of stannous oxide with some hydrochloric acid in a test tube. Warm this over a candle or a gas burner, adding more hydrochloric acid until all the stannous oxide has dissolved. Place a small amount of this liquid (stannous chloride solution SnCl₂:2H₂O), on to a piece of glass 2 to 4 inches square on top of an electric hot plate that is just warm (30 deg. C to 40 deg. C), making sure none of the liquid runs off the glass on to the hot plate. Add more of the liquid every time it evaporates to a solid, until it is all converted. Note there is no reason why any other method of obtaining stannous chloride should not be used. The method detailed above was used by the writer as stannous oxide was already at hand.

PREPARING THE GLASS

Cut two pieces of glass 2 to 4 inches square. Cut eight small pieces of glass $\frac{3}{8}$ of an inch square. Clean the two large pieces of glass with, if possible, ammonium carbonate, then wash them well under cold running water. This is necessary because any minute speck of dirt will break up the film.

Remove the stannous chloride (SnCl₂) from the first piece of glass and make a pile on the edge of one of the cleaned glass plates, see Fig. 1. Put this glass plate on top of the electric hot plate. Place two of the 3 of an inch square pieces of glass one on top of another, in each corner of the glass. Place the other cleaned glass plate on top of this. Bring the electric hot plate up to full heat slowly.

BLOWING THE VAPOUR

When the pile of stannous chloride begins to smoke heavily, very very gently blow this vapour through between the two glass plates. A battery operated fan positioned about 2 to 3 feet away is normally sufficient. The slower the vapour passes through between the glass plates the more the glass is plated. Continue

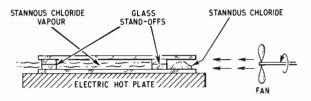
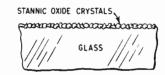


Fig. 1. The two glass plates in position for the tinning process

Fig. 2. Greatly magnified cross-section of the coated glass



blowing until it has stopped smoking, then turn off the hot plate, letting the glass cool down with the hot plate (about 40 minutes).

When the glass has cooled down remove it from the hot plate. Cut \(\frac{3}{8}\) of an inch from each side of the lower glass plate where the glass stand-offs and stannous chloride were, leaving a transparent conductive glass, a glass just as transparent as a thick polythene sheet.

If insufficient stannous chloride is used the glass will have a rainbow effect across it. This is still conductive but of very high resistance; it is also more transparent.

The amount of stannous chloride used will depend on the resistance and transparency required and also the area to be plated. This must be worked out by trial and error to suit different types of hot plates and fans etc.

IMPORTANT WARNING

Most people have heard of tin poisoning, and all should know that hydrochloric acid is poisonous and can burn the skin and eyes. The stannous chloride vapour will not burn the skin, but it should not be inhaled or swallowed as it can be very dangerous. Therefore the vapour should have a free path to the open air and of course food and any cooking utensils should be well away and covered up. It should also be realised that if the windows are wide open a slight draft could blow the vapour into one's face.

All the rules of chemistry must be followed regarding the use of test tubes and acids. However, with a sensible attitude one can proceed without any danger.

HEATING THE GLASS

Anyone who has had to repair a pane of glass knows that cutting glass is more of an art than a science. This is also true when heating plate glass. For any kind of success two rules must be followed. Never heat or cool glass too quickly, and keep the whole piece of glass at an even temperature. It is no good trying a square piece of glass on a round type of hot plate as the heat is not distributed evenly. Nor a square piece of glass the same size as a square hot plate since the heat is not evenly distributed at the edges of the hot plate. The glass should be in even contact with the hot plate.

CHEMICAL THEORY

The stannous chloride changes to vapour at about 400 deg. C, and is mixed with the air. When this vapour comes into contact with the hot glass some of the molecules dis-associate into tin and chlorine. One tin atom combines with two atoms of oxygen from the air and this molecule combines with others and crystallises on to the semi-molten glass, where the crystals grow in all directions until each crystal is in contact with its neighbours forming a continuous thin film of stannic oxide on the glass, see Fig. 2.

PROPERTIES OF GLASS AND FILM

The glass, after plating with stannic oxide, retains the same physical properties as ordinary glass except that it is slightly harder and, of course, not so transparent. Stannic oxide films are used in the automatic bottle manufacturing process as a lubricant to stop the breakages due to the cold metal jaws coming in contact with the hot glass bottles.

The film itself is very hard and very firmly adhered to the glass. It is like a very fine transparent sand paper. If one tries to remove it with a razor blade or a knife all one can see is a thin film of steel left on the stannic oxide.

There is one way of removing the stannic oxide film. This is by making the stannic oxide the negative electrode in a bath of hydrochloric acid and have a positive electrode of zinc and connect it up to a battery charger.

MASKING

If it is desired to leave portions of the glass free of the film, these areas should first be covered with small strips of glass or painted with a paste made of powdered glass.

Although the glass is conductive it is not of zero resistance. A resistance of less than 1 kilohm has been achieved, measured between two strips of copper both one inch long and one inch apart. The linearity of the resistance across the glass plate depends on the even flow of the stannous chloride vapour. This can be improved upon by using glass strips in place of square glass stand-offs.

The thickness of the stannic oxide film cannot be determined as the glass in the first place is not even within a few thousandths of an inch.

INCREASING THE RESISTANCE

The resistance of the film is greatly increased if a very small amount (1 part in 10³) of impurities is added to the stannous chloride solution, like copper, zinc, or even silver salts. No impurities have been found that decreased the resistance. If the stannic oxide film is rubbed with copper the over-all resistance is decreased.

ELECTROPLATING

The conductive glass can be electroplated with copper from the cupric sulphate solution. Make sure that the stannic oxide film is very clean first by dipping it in a bath of hydrochloric acid, then under cold running water, then in a bath of sulphuric acid, then again under cold running water.

Make a connection at one end and dip the opposite end in the solution up to \(\frac{1}{2}\) of an inch away from the connection. At first, use a low plating current. Only the top \(\frac{1}{2}\) of an inch or so that is in the solution will become plated with copper, because of the resistance of the stannic oxide film.

When the top $\frac{1}{4}$ of an inch is plated with a thin film of copper withdraw it and when the next $\frac{1}{4}$ of an inch is plated withdraw that and so on. In this way an even film can be plated across the stannic oxide film. The plating current can then be increased and a thicker plate of copper laid.

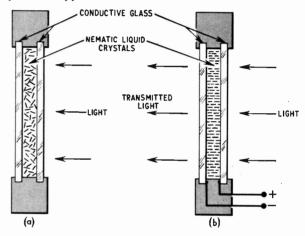


Fig. 3. The variable transparent window. (a) not energised, not transparent; (b) energised, transparent

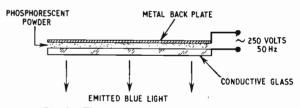


Fig. 4. The electroluminescence panel lamp

The copper can be etched off using a solution of ferric chloride, provided nail varnish is painted on those areas where the copper is to remain.

TIN OXIDE RESISTORS

Using the above techniques it is possible to make many tin oxide resistors, even variable resistors, on one piece of glass with copper circuitry and soldered-on capacitors and transistors. Fine adjustment of the resistors can be achieved by rubbing the stannic oxide film with copper, then painting with varnish or epoxy resin. Commercially made tin oxide resistors are well known for their good temperature stability, but this cannot be claimed for these "home made" varieties.

VARIABLE TRANSPARENCY

Another application of conductive glass is the variable transparent window, see Fig. 3. This device depends on the action of the so-called nematic liquid

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crystals. This type of liquid appears as if it had millions of very small elongated needlelike crystals immersed in it. The crystals are normally quite haphazardly arranged and the liquid is not transparent. But when the liquid is subject to an electric field the crystals align themselves parallel to the electric field and the liquid becomes transparent.

In the variable transparent window the liquid is placed between two plates of conductive glass anything up to a \(\frac{1}{4}\) of an inch apart. A direct voltage is applied between the two conductive glass plates and therefore the crystals align and the window becomes transparent. By varying the applied voltage the transparency can be varied.

COLOUR CONTROL

It has been recently discovered in America that by mixing a small amount of dye in a solution of one of the nematic liquid crystals it is possible to vary the colour of the transmitted light by varying the applied voltage, although only from a reddish-orange to a yellow. In this type of device the resistance of the stannic oxide film is of no consequence as it is purely electrostatic and no current flows.

It has been known for a long time that not only does an electrostatic field align molecules and crystals, but it can also modify the electronic valency of atoms in a crystal thus altering the properties of the material.

It has been recently discovered in Russia that when a photographic film of a special type is placed between a metal back plate and a piece of conductive glass at the front, the speed of the film can be varied by varying the applied voltage. Thus it is possible to vary the speed of the shutter as well as the speed of the film without changing the roll of film that is in the camera.

ELECTROLUMINESCENCE PANEL

The electroluminescence panel lamp is another example of the use of conductive glass. This devise consists of a phosphorescent powder (ZnS) sandwiched between a piece of conductive glass and a metal back plate, see Fig. 4. When it is supplied with an alternating voltage the phosphor emits light. This type of lamp is the most efficient known with an efficiency of 95 per cent to 99 per cent, although the light is very dull. It is, after all, only a parallel-plate capacitor. Furthermore it is only possible to obtain two colours, blue and green.

One interesting fact about this type of lamp is that there is a colour shift of the blue type to green with an increase in the applied frequency up to 400Hz, above which the efficiency falls off. This type of lamp is a solid state device and never burns out.

There are many devices built around this effect, including a picture intensifier, which has a layer of photoconductive material (CdS) laid on top of the phosphor, then another piece of conductive glass on top of that.

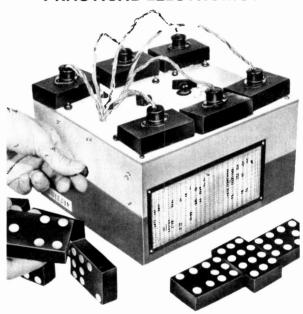
FURTHER IDEAS?

Conductive glass is used in many types of T.V. camera tubes and photoelectric devices. But it can also be used in applications that are not so sophisticated, like heating the back window of a car, for instance.

It would seem there are many uses that conductive glass could be put to by electronics enthusiasts. How about, for example, a pair of variable sun glasses electronically controlled by a photoconductive cell?

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COLD CATHODE TUBES By J. B. Dance M.Sc.



INDICATOR TUBES

Cold cathode gas filled tubes have been widely used for providing a visual display of information stored in a circuit, for example, for displaying the state of the count in a counting circuit or the switching state of a logic circuit.

Miniature neon diodes are often used as a simple and economical device for providing a display of information, but they can act only as on-off indicators, the indication being provided as a glow or the absence of a glow.

Other types of cold cathode tube are available, however, which indicate the state of the count as a glow in the gas, the glow being in the actual shape of the digit to be indicated. A row of such tubes can be used to display any number of digits in the same way that the number would be written down on paper.

READOUT

Any system used to provide information from an electronic circuit is known as a readout system, since the information is read out of the circuit concerned. Cold cathode tubes and other devices which provide a display of information for an observer to see are said to provide visual readout, but circuits can also provide electrical readout in the form of electrical pulses to an output socket or in the form of a changing voltage or current.

Electrical readout signals can be used to operate other electronic equipment or to operate an electronic typewriter which will print out the information onto paper, thus avoiding the possibility of human error in copying the information.

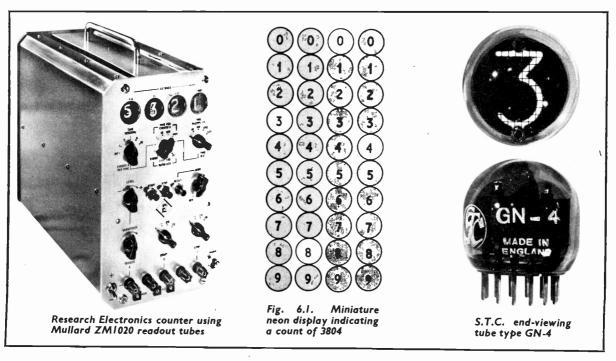
Both visual and electrical readout can be in either digital or analogue form. A digital readout system provides a display in numerical form, whilst an analogue system provides a display as a variable quantity such as the movement of a meter needle, or the movement of a spot of light on a cathode ray tube.

Various pseudo-digital readout systems are also available, such as that provided by decade stepping tubes. Although such a display is not in actual numerical form, each stepping tube nevertheless displays a single digit.

IN-LINE DIGITAL SYSTEM

Ideally a readout system should be of an "in-line" digital type in which the information is displayed as numbers in a horizontal line, just as the number would be written down.

Miniature neon diodes may be used to display the number of counts recorded in a circuit if they are arranged in rows, each vertical row containing ten diodes (Fig. 6.1). Only one of the diodes in any



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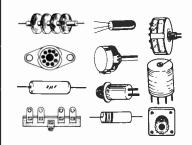
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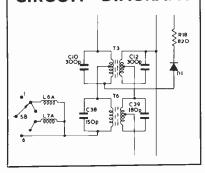
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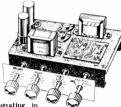
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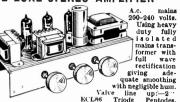
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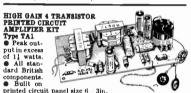
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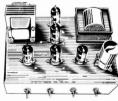
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vertical row glows at any one time, the number being painted on a transparent mask through which the light from the glowing tube passes.

Neon tube readout from valve circuits is easy to arrange, since it is only necessary to connect a neon diode across the valve anode resistor or from the valve anode to chassis (with a suitable current limiting resistor in series with the diode).

However, most transistor circuits operate at voltages which are less than the striking voltage of any available neon tubes. Special tubes and circuits have been developed to overcome this difficulty and some of these are described as follows.

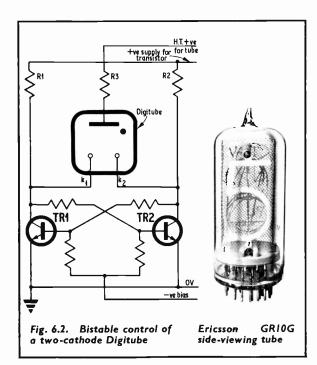
THE "DIGITUBE"

The "Digitube" (a product of the Fujitsu Company of Japan) can be used to provide visual readout from a transistor binary stage. This type of tube contains two cathodes and a single anode; it may be used in the type of circuit shown in Fig. 6.2.

The transistors TRI and TR2 are connected as a bistable circuit. When TR1 is conducting, TR2 will be non-conducting. In this case the potential drop across the collector load resistor R1 will ensure that the cathode k_1 of the Digitube is kept at a lower potential than cathode k_2 , since there is no appreciable voltage drop across R2 when TR2 is cut off.

The potential between the tube anode and k_1 is thus greater than that between the anode and k_2 ; all of the current passing through the tube tends to pass to k_1 which is surrounded by a glow. The current flowing through the Digitube anode resistor R3 to the cathode k_1 is sufficient to keep the potential between the anode and k_2 below the maintaining voltage for this gap.

When the bistable circuit is switched and TR2 conducts, the cathode k_2 of the Digitube will glow, but the glow at k_1 will be extinguished. An observer can see a glow only when one of the two cathodes is glowing, since the other cathode is screened from view.



"DIGITUBE" BINARY STAGE

The simple circuit of Fig. 6.2 is used as a binary stage and can in this case only indicate a count of zero or unity. In most transistor counting circuits a number of these binary stages can be cascaded so that a larger number can be indicated. Four cascaded binary stages can indicate a count of up to fifteen (i.e. they will count on a scale of sixteen), but a feedback system is usually employed so that the four cascaded binaries are reset at the tenth pulse. Thus four Digitubes are required in each decade of the transistor counting circuit.

lons are always present in the Digitube when the circuit is in use, thus enabling the glow to be transfered easily from one cathode to the other when the binary circuit changes its state. The anode to cathode striking voltage of the non-conducting section of the tube is lowered almost to the maintaining voltage by the presence of the ions from the discharge in the other section of the tube. Thus a change of a few volts is sufficient to change the position of the glow in the tube.

TRANSISTOR CONTROLLED NEON DIODE

The Hivac Company have devised a rather different type of circuit for the control of a miniature neon diode by a low voltage transistor circuit. Although their miniature indicator diodes have only two electrodes, steady ionisation is maintained by a very small current which passes through the tube at all times when it is operational.

This current is not great enough to produce a glow in the gas which is visible in daylight, but a larger current passes when the binary to which the tube is connected is in one of its two states; the indicator tube then emits a glow.

NUMERICAL INDICATOR TUBES

Tubes which indicate actual digits are known as numerical indicator tubes or digital indicator tubes. Various trade names are also applied to them: for example, the Ericsson digital indicator tubes are known as "Digitrons"; the Hivac tubes as "Numicators"; the S.T.C. tubes as "Nodistrons"; the Burroughs (U.S.A.) tubes as "Nixie" tubes.

Similar tubes can be used to indicate letters of the alphabet, mathematical signs, or any one of several other symbols. Some are made to indicate a combination of two symbols, such as mA or μ s.

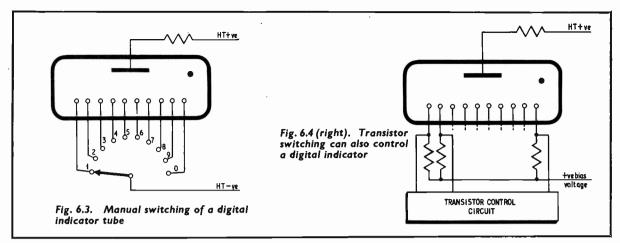
Numerical and symbol indicating tubes have a number of cathodes stacked closely behind one another, each cathode being in the shape of one of the digits or symbols to be displayed. The stack of cathodes is surrounded by a common anode in the form of a wire mesh.

At any one time when one of the cathodes is conducting this is surrounded by a red glow. The presence of any other cathodes in between the observer and the glow does not greatly impair visibility of the glow, since the glow is several times wider than the cathode material itself.

SWITCHING CONTROL

One type of circuit in which a numerical indicator tube may be used is shown in Fig. 6.3. The potential is applied between the anode and the particular cathode which is selected by means of a switch. Only this cathode can pass a current and therefore it is only this selected cathode which glows.

In most practical applications it is often necessary to control the display by means of a transistor switching



circuit. The type of basic circuit shown in Fig. 6.4 may be suitable. A positive bias voltage is applied to all of the tube cathodes via resistors, as shown. The transistor control circuit effectively earths only one of the cathodes at any time. This cathode is therefore at a lower potential than the other cathodes and will pass a current.

If the positive bias voltage is adequate, no other cathode will pass enough current to cause it to emit an appreciable glow.

The bias voltage applied to the non-glowing cathodes is known as the pre-bias voltage. If this voltage is too low, all of the cathodes will be surrounded with some glow and a rather indistinct or even unreadable display will result.

If it is required to use digital indicator tubes to provide an in-line display from a transistor cascaded binary counting circuit, some means must be employed to convert the binary electrical readout from the counting circuit into decimal readout. A matrix of diodes is often used for this purpose.

If, however, the transistor counting circuit consists of a "ring of ten" circuit, the readout is of a more suitable type for the operation of a numerical indicator tube.

CURRENT LIMITATIONS

The manufacturers of numerical and symbol indicator tubes recommend maximum and minimum values of the current which should be passed through the tube. If the maximum current is exceeded, excessive sputtering will probably result in a very much reduced tube life, whereas if the current passing is below the minimum recommended value, some of the larger cathodes may not be completely covered by the glow and a defective display will result.

In some tubes a resistor should be employed in series with one or more of the cathodes of small area so that the current passing to these cathodes when they are glowing is less than that which passes to the other cathodes.

LIFE AND RELIABILITY

Numerical indicator tubes employ metal cathodes and have an extremely long life when used in correctly designed circuits. Some cathode material is gradually sputtered away, but the wire mesh anode prevents an excessive amount of this material from being deposited on the glass envelope of the tube where it would cause unwanted reflections and may even obscure the display.

Some long life numerical indicator tubes contain mercury vapour which emits a blue glow when the tube

is operating. A red filter is often employed on the front of the envelope of such tubes so that the blue glow is not visible. Some of these tubes have a life of about 150,000 hours or even more and will therefore normally outlast the equipment in which they are being used.

TWO VIEWING TYPES

Small numerical indicator tubes are useful for miniature equipment, but larger types are available which can provide a display which is readable from a considerable distance. Tubes which display large digits require more current, but the operating potentials are very similar to that of the smaller tubes.

Some tubes are side viewing types, but others are viewed through the domed end of the tube. It is usually easier to fit large cathodes in the side viewing tubes and such tubes have the advantage that they occupy less depth behind the instrument panel than the end viewing types. However, the latter have the advantage that they occupy less front panel space and are more easily arranged in rows or columns close together.

POINT INDICATOR TUBES

Another type of indicator tube displays a single digit by means of the position of a point of light in the tube. Such tubes are of a similar construction to a decade stepping tube, but have only ten wire cathodes surrounding a common anode. The domed end of such a tube is placed in a numbered escutcheon, as in the case of the decade stepping tube.

The glow in a point indicator tube steps around the tube as the circuit counts. The current passed by this type of tube is much smaller than that passed by numerical indicator tubes due to the smaller cathode area.

Point indicator tubes are especially useful when a decade stepping tube circuit is preceded by a fast valve or transistor scaling circuit, so that the overall counting speed is much greater than that of the decade stepping tube circuit.

Such tubes can be used to display the state of the count in the fast valve or transistor counting circuits and have the advantage that the type of display is then the same in all decades of the instrument. This arrangement is usually more economical than if transistor or valve circuits were used throughout for the counting.

CLOCK FACE TUBES

Clock face tubes are useful for displaying the count in transistor counting circuits. In such a tube the

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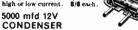
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digits are displayed in a circle like the figures on a clock face. The Z550M tube has been developed by Mullard especially for this purpose. A basic circuit for the use of this tube is shown in Fig. 6.5.

The tube consists of an upper common anode ring, a cathode ring (k) and a lower anode ring. Parts of the cathode ring are covered with material of high work function so that the discharge can take place only at ten points in the tube. The control voltage from the switching circuit is applied to ten trigger electrodes (T) (only two of which can be seen in the cross sectional diagram in Fig. 6.5).

When one of the triggers is at least 5V positive with respect to the other trigger electrodes, that trigger will cause striking at the cathode ring in its immediate neighbourhood. No striking will occur at other points on the cathode ring, since the current taken by the conducting cathode passes through the cathode resistor and produces a potential drop across this resistor.

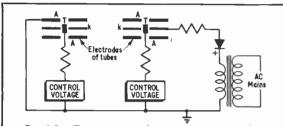


Fig. 6.5. Two sections of a ten-trigger clock face tube with a controlled wave supply

At the end of one half cycle of the sine wave supply, the glow in the tube is extinguished. If the trigger voltages change before the diode in the cathode circuit conducts again, another part of the cathode ring will conduct and another digit will then be indicated.

The light from the gas discharge passes through the holes marked A in Fig. 6.5 to provide the visual display. These holes are in the shape of the digits to be indicated.

Circuits have been developed for the Z550M tube which enable it to count at speeds up to 1kHz. Thus the tube can be used as an indicator for high speed transistor scalers, but in the slower decades the tube can carry out the actual counting operation itself. A uniform type of display is thus presented by all of the decades, but such a scaler is more economical than if transistor counting circuits were used throughout.

ALPHA-NUMERIC DISPLAYS

The alpha-numeric type of tube employs a number of straight line cathodes (usually 13 or 15) in each tube, which are positioned in the shape of a combination of letters or numbers. When certain selected combinations of these cathodes glow, any number or letter can be indicated.

Alpha-numeric tubes tend to require more complicated circuits for their operation than the normal numerical indicator tubes, and the form of the display is not normally as good as that of the tubes which employ separate shaped cathodes for each symbol or digit to be indicated.

In conclusion it should be mentioned that, although cold cathode tubes offer one of the simplest and best methods of displaying information which is stored in electronic circuits, there are a number of other techniques employed, many of which are based on some form of projection device. Electroluminescent digital indicators are also available.

BRITISH MUSICAL INSTRUMENT TRADE FAIR

AUGUST 69

By F. C. Judd

So impressive has been the growth of the British musical instrument trade that its fair this year occupied two large adjacent London hotels. Electrical and electronic musical instruments, their amplifiers and accessories formed the greater part of the show with electronic organs creating by far the largest interest although not quite the biggest noise.

SOUNDS CURIOUS

It is these instruments of course that have done much to expand the trade as a whole resulting in keen competition for sales both at home and abroad, although without "electronics" the story might be different.

Even the musical instrument trade jargon has become a curious mixture of musical and electronics terms, but no more curious perhaps than some of the musical instruments whoses sounds are generated electronically and reproduced by amplifiers and loudspeakers.

For instance there were the new Jennings electronic tympani units and their equally new device called the "Bushwhacker" which electronically produces the rhythmic sound favoured by TV entertainer Rolf Harris. This device also creates many "space" noises that will undoubtedly prove attractive to pop groups looking for new sounds.

FOR AMPLIFIED GUITARS

For guitarists there were many new accessories like the Jennings "Scrambler" which is a combination wah-wah, fuzz and volume control unit with rotating foot controls and foot operated switches.

Add-on units for producing teverberation and various percussive and tremulant effects suitable for amplified guitars, as well as electronic organs, were yet another attempt to satisfy the demand for new sounds, although many guitar amplifiers, like those by Dallas Arbiter and Selmer, were being offered with such facilities built in.

ROTATING LOUDSPEAKERS

Rotating loudspeaker tremulant systems are much in demand now and there were many of these on show under such names as pulsation units, rotary loudspeakers, Leslie units etc., by makers such as Jennings, Dallas Arbiter and others.

To cope with these, as well as the more standard form of P.A. type loudspeaker, solid state amplifiers capable of 100 and 200 watts (r.m.s.) appeared to be outmoding the more conventional 50 to 60 watt models.

One demonstrator guitarist mentioned that the constant use of fuzz, plus 200 watts (r.m.s.) power was affecting his hearing! One manufacturer claimed that a group using



his equipment generated a combined power of over 1,500 watts whilst playing! Electronics have indeed contributed much to music.

ELECTRONIC ORGANS

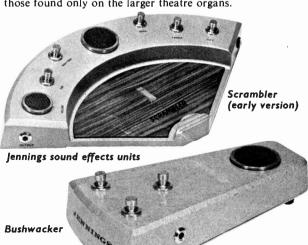
The range of electronic organs now available is comprehensive to say the least, and everything from miniature chord organs at around £15 to full scale electronic church and theatre organs at £5,000 or more could not only be seen but very much heard. The popular "domestic" range by Hammond, Thomas, Lowry, Wurlitzer, to mention only a few, offer a pretty wide choice not only of different models but of effects, voicings and facilities.

The miniature table top chord organs (with loudspeakers) such as those by Rose Morris Limited, start at around £15 and end at around £200 with the smaller transistor chord/keyboard instruments like the Philips Philicord.

The "pop" portables which require external amplifiers range from below £100 to over £500. Among these were the more pretentious models like the PT75 by Harmonics (Bromley) Limited which they claim plays everything from groovy to soft piano and features wah-wah, chimes and a steam organ sound as well as a vast range of percussive and other effects all for £325.

The popular "domestic" range of two manual organs with half or full pedal boards also offers a pretty wide choice. It is quite evident from the great variety of styles, facilities, effects and gadgetry available that the various manufacturers compete pretty fiercely to capture and retain their share of the domestic electronic organ market.

The new Hammond T200, for instance, classified as being "suitable for the entire family", not only features their tone wheel generator system and drawbar harmonic selectors, but also a range of voices and effects approaching those found only on the larger theatre organs.



866



Dallas Arbiter Sound City 200 p.a. amplifier

MUSIC TUTORS

It is one thing to design and sell an electronic organ for family entertainment, but quite another getting them to play it with some satisfaction. To this end the Thomas domestic range on show this year featured two unique teaching techniques. One, which has been derived from the Thomas "Colorglow" keyboard system, is called "Chordglow" and helps the player to master chord combinations quickly on the (left hand) lower manual. The required notes for any given chord all light up at the touch of a button. They have also devised recorded tape cassettes which enable the beginner to play with recorded exercises.

Last but not least it should be mentioned that coloured light and stroboscopic light systems electronically controlled from music or direct from musical instruments now seems to be part and parcel of pop music.

Many of these systems were also on show by Rotasound, Jennings, Dallas and others. Several thousand watts of intense flickering light accompanied by around 2,000 watts of highly distorted music power seems to be the ultimate in electronics and pop music at the moment, but—according to the trade experts and many of the musicians (?)—there is now a trend toward quieter and much more pure sound!

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15 amp 3 Core Non-Kink Flex. 70/0076 insulated coloured cores, protected by tough rubber sheath, then black cotton braided with white tracer. A normal domestic flex as fitted to 3kW fires. Regular price 3/6 per yd. 50yd coil, \$4,10 or cut to your length 2/6 per yd.

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Made by Smiths, these are A.C. mains operated, NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be bull into box with 13A, socket. 2 completely adjustable time periods per 24 hours, 5 amp changeover contacts will switch circuit on or off during these periods. 59/8, post and ins. 4/6. Additional time contacts 10/- pair.

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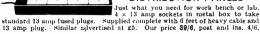
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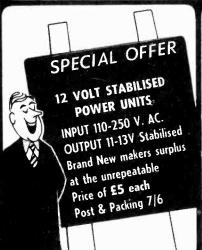
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0·0068, 0·01 0·015 0·022	7d 7d 7d	5/1 5/2 5/3	10/11 11/10 12/-	36/5 37/6 37/9	OA5 2/- OA81 2/-	15/- 15/-	36/- 36/-	133/4 133/4 133/4
0.033 0.047	8d 9d	5/8 6/7	12/7 14/5	42/7 49/-	OA202 2/- OC23 7/4	58/8	36/- 132/- 108/-	497/8 399/
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0·15 0·22 0·33	1/2 1/6 2/3	10/8 14/3 19/7	22/- 28/5 42/3	74/- 95/10 140/7	OC44 3/- OC45 2/6	22/6 18/9	54/- 45/	199/6 166/3 133/4
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0·01, 0·015 0·022 0·033, 0·047	7d 7d 8d	5/2 5/4 5/11	11/9 12/10	38/7 41/8 43/9	OC82D 2/4 OC139 3/4	17/6 25/-	42/- 60/- 45/-	155/4 221/8 166/3
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