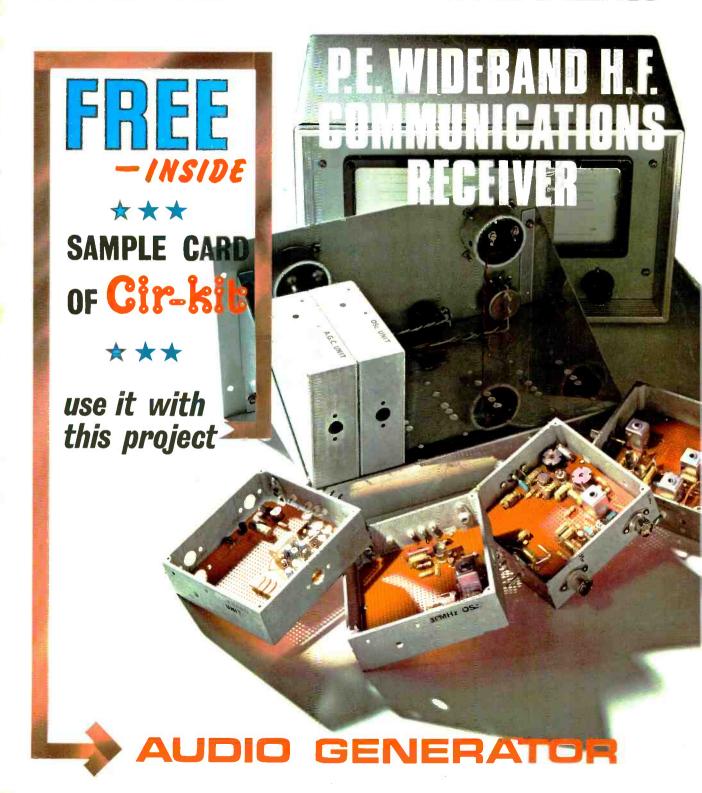
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MT122	10A	61 75 - 61 in	23lb 2c	oz 152/- (Carr.	extra)
MAINS	HT DA	NCE			

				Size Pricel'&	ı I
	MTIAT	250-0-250 V	80MA	6-3V 3-5A 5/6-3V 1A 31 3 3in 33/- 6	ij.
	MT6AT.	250-0-250V	100MA	6-3V 3-5A 5/6-3V 1A 4 - 31 - 31 in 38/3 6	ij.
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ı	MT12AT	300 -0-300V	120MA	6-3V 4A 5/6-3V 1A 4 - 37 < 31in 46/2 9	1.
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MT45	1.5A	21 ~ 21 × 21 in	11b 9oz	21/9 (P. & I	P. 4/6)
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MT86	6.A.	4 3 4 3 i in	51b 12oz	48/- (P. & 1	P, 6/-)
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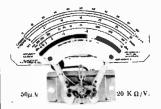
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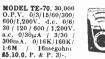


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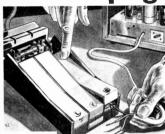
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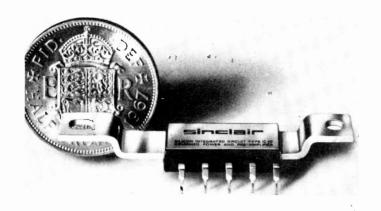
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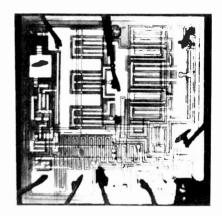
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SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. 5 Hz to 100 KHz±1dB. Frequency response Total harmonic distortion Less than 1% at full output. 3 to 15 ohms. Load impedance 110dB (100,000,000,000 times) total. Power gain 8 to 18 volts. Supply voltage $1 \times 0.4 \times 0.2$ inches. Size Sensitivity Adjustable externally up to Input impedance 2.5 M ohms.

■ CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

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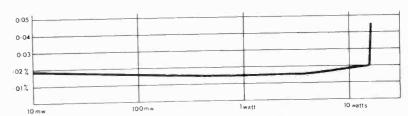
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- Class AB output
- Power requirements 8-35 volts from batteries or PZ.5

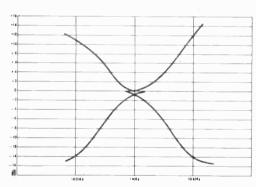


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This attractive and completely new unit is intended for use with two new Z.30 amplifiers to provide the finest possible standards of stereo reproduction. Four press buttons and four rotary controls are used to provide on-off, three input selectors and Volume, Bass cut/boost, Treble cut/boost and Stereo balance. The on-off button also switches the power amplifiers. The front panel in brushed aluminium is flush mounted to the cabinet front, it being necessary only to drill holes to accommodate the controls. Rear adjustable brackets hold the chassis tight to the cabinet. The very latest ganged rotary controls are used to afford compactness and extra long working life free from noise.

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Inputs: Radio, pick-up (magnetic, ceramic or crystal), Auxiliary Overload factor:

> 20dB per channel on all inputs 0.03%

Distortion :

Signal to noise ratio: Better than 70dB unweighted

Controls: press buttons for on-off, P.U., radió and aux. Treble +15dB to

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Size:

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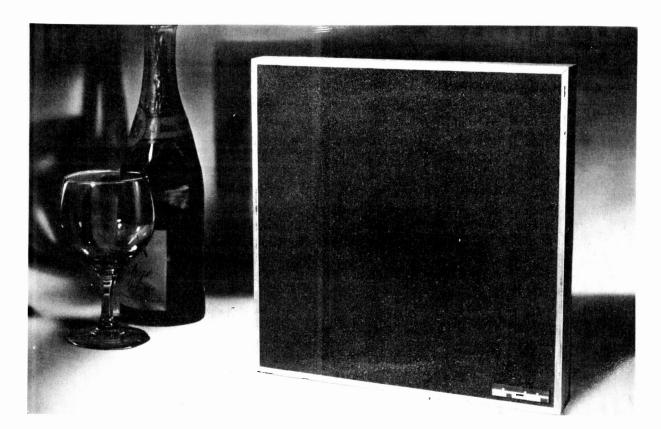
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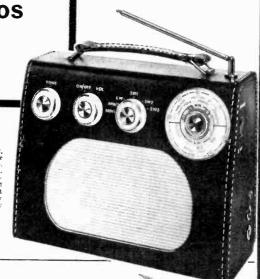
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PRACTICAL **ECTRONICS**

AUTUMNAL AWAKENING

AKE a peep into a typical amateur constructor's den or workshop, around mid-summer, and what will you discover as likely or not?

On a workbench, now collecting a film of dust, a halffinished circuit board or two, or some other partially built equipment bearing a sad air of neglect.

Clear evidence of a sudden departure some months ago. Yet the explanation is all too obvious and innocent.

The summer always makes special demands upon the active handyman. His spare time and energies are then directed outdoors. Nature in her most bounteous and prolific mood insists upon regular attention to the garden, and other outdoor maintenance jobs have to be fitted in while the weather is clement. And, of course, the annual holiday provides its welcome and long awaited, if disruptive, interlude in the year's pattern of events in most homes.

Now autumn is upon us. Both the autumn and winter seasons bring their own compensations. Soon a host of constructors will be ensconced once more in their respective dens or workshops, each one (no matter how humble or how frugally equipped) a refuge and solace from the many irritations of the outside world. If only for a few hours in the evening or at the weekend.

In his private retreat, the electronics enthusiast can read and think about circuit ideas—and their possible application to his own or the family's needs. And he can usefully employ himself and practise various skills in building and testing chosen projects.

This kind of recreational activity is, we reckon, as beneficial as a winter's cruise (!) No excuse now for further absenteeism from one's favourite hobby, or for any more accumulation of dust during the next six months or

The time has come to return to those half-built projects, also to consider making a start on other designs read about during the close season and mentally recorded as likely subjects for attention when time permitted. And there will be additional new ideas coming along regularly each month. A sample of stick-on-wiring is included in this month's issue. This should arouse the interest of novices and old hands alike and provide added incentive to start or resume building activities straightaway.

So make it a productive and rewarding season.

F. E. Bennett-Editor

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Our November issue will be published on Thursday, October 16

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IN THE light of controversy over specifications for audio amplifying equipment, it is becoming increasingly important to be sure that what is labelled "hi fi" really does live up to the conventionally accepted standards of true high fidelity reproduction.

This article is a useful practical prelude to getting started in hi fi. It shows how simple it is to construct an audio oscillator which can be used to carry out performance tests on a wide range of audio amplifiers. It is suitably styled to blend in with the domestic scene without being an eye-sore, as so often test equipment is designed for workshop decoration.

The circuit is based on the well-known Wien bridge configuration with extended ranges to provide high frequency response tests with a square wave output (Fig. 1). The unit can be arranged to provide sine or square waves, whilst a calibrated attenuator facilitates accurate signal levels. Of course, it is necessary to have an a.c. millivoltmeter with very high input impedance for measuring the resulting output from the equipment under test. Although not essential, a wide band oscilloscope also adds to the interpretation of resulting measurements by giving a direct visual image of the test waveform.

WIEN BRIDGE OSCILLATOR

Three transistors are used to provide the sine wave, TR1 and TR2 being a compounded Darlington pair to give high gain, TR3 acting as the phase inversion stage to provide regenerative positive feedback.

Because of the necessity in this circuit for additive reactionary build-up of oscillations, the feedback path must provide in-phase currents from output to input. The frequency of oscillation is determined by the feedback components and, in order to provide a wide frequency range, it is essential to employ transistors of high cut-off frequency, with switched selection of capacitance values.

Any change or mismatch in component values in the series or parallel circuits of the bridge will cause the feedback signal to TR1 base to become out of phase with the bridge input, preventing oscillation.

To achieve perfect oscillation the total phase shift through the amplifier and back through the bridge must be zero or an integral multiple of 2π radians.

FREQUENCY SELECTION

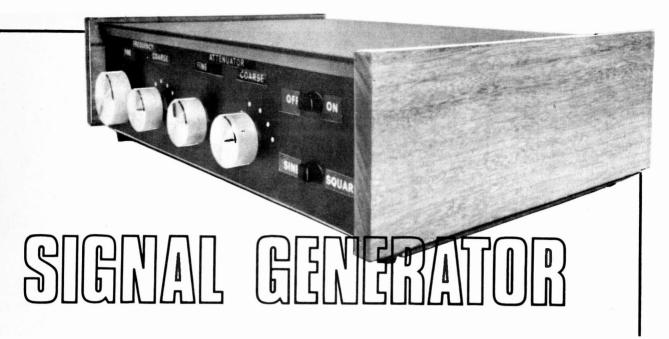
Frequency selection is by means of S1a and S1b (coarse) and the twin-ganged potentiometers VR1 and VR1 and S1a determine the series feedback characteristic and VR2 with S1b selects the parallel feedback. So to ensure correct match, VR1 and VR2 must be ganged (a "stereo" type of control is ideal) and the capacitors selected by Sla must be the same values as those selected by S1b. It is worthwhile, if at all possible, to measure the capacitance of selected samples to achieve a good match; these should be ideally within one per cent of each other for each nominal value quoted.

The resistance-capacitance network must not load the amplifier output too much, so it should be made a high impedance network compared with the output impedance of TR3. Similarly, the input impedance of the amplifier must be high so that it does not load the bridge feedback path.

The input impedance of the first stage TR1 is approximately equal to R_5 times the current gain squared. Hence, the ideal application of a Darlington pair at the front end to provide a high input impedance to the first stage.

The thermistor RT is used to provide d.c. stabilisation of the transistors because of the direct coupling configuration, necessary to avoid minor phase shift. Consequently, amplitude control is achieved and stabilised to a better degree than if a fixed resistor was used.

For most purposes a sine wave oscillator is adequate to test an audio amplifier for frequency response, power output (undistorted), and amplifier sensitivity, when used in conjunction with an oscilloscope. Tape head alignment can also be made. Bias and erase frequencies are usually greater than about 50kHz and may be as high as 120kHz; this is the reason why the range of this instrument is high to cover these applications.



SQUARE WAVE CONVERTER

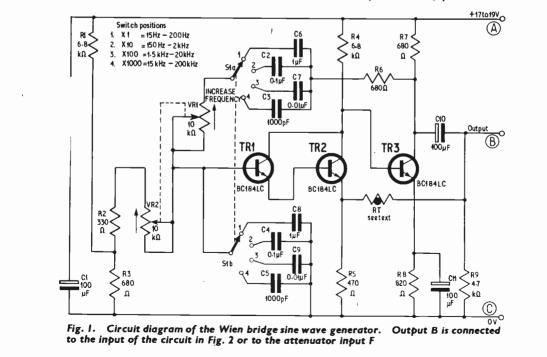
Many people prefer to use a square wave for quick frequency response checks. In this case a wide frequency range oscilloscope, extending to about 50kHz or or more with level response, is a must. With experience and practice it is a simple matter to determine the limitations of frequency response by studying the resulting wave shape at the amplifier output.

One other great advantage of this method is that high frequency oscillation (ringing) inherent in the amplifier will show up. Although this "ringing" is seldom audible on its own, it can have a serious effect on the coloration of complex waveforms, such as from violins or reed instruments. This is often the cause of disturbing "edginess" in music reproduction.

The sine to square wave converter is shown in Fig. 2 and is basically a modified form of Schmitt trigger with very rapid switching.

It is not expected that square waves above about 50kHz will be needed for audio equipment, so any deterioration of wave shape at higher frequencies is no serious handicap.

For frequencies above approximately 20kHz, C14 was added to assist TR5 during its switch-on period, and also keeps the mark/space ratio constant at these



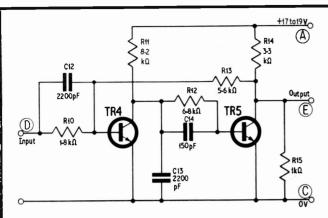


Fig. 2. Circuit diagram of the sine to square wave converter. Output E is connected to the attenuator input F; D to Wien bridge output B

Fig. 3. Stepped and continuously variable attenuator. Input F is connected to Wien bridge output B or converter output E. The output from \$3\$ wiper is fed to the apparatus under test

Note: C2 and C4 to be matched

C3 and C5 to be matched C6 and C8 to be matched

C7 and C9 to be matched

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R2	330Ω 5%	RI2	6·8kΩ 5%
R3	680Ω 5%	R13	5·6kΩ 10%
R4	6·8kΩ 5%	RI4	3·3kΩ 10%
R5	470Ω 5%	RI5	IkΩ 10%
R6	680Ω 5%	R16	680Ω 10%
R7	680Ω 5%	RI7	10kΩ 5%
R8	820Ω 5%	RI8	IkΩ 5%
R9	4·7kΩ 10%	RI9	100Ω 5%
RIO	I·8kΩ 10%	R20	12Ω 5%
	esistors ±W carbon		,,0

Potentiometers

 $\begin{array}{ll} \text{VRI} & \text{I0k}\,\Omega\\ \text{VR2} & \text{I0k}\,\Omega \end{array} \} \\ \text{twin ganged anti-log carbon miniature}$

VR3 5kΩ linear carbon

Transistors

TRI, 2, 3, 4, 5 BCI84LC or BCI07 or BCI08 (5 off)

Thermistor

RT $5k\Omega$ at 20°C, 100Ω at 5.5mA. Type R53

Switches

- SI 2-pole 6-way (only 4 ways used) rotary wafer
- \$2 2-pole changeover slide switch
- S3 2-pole 6-way (only I pole 4 ways used) rotary wafer
- S4 2-pole changeover slide switch

Capacitors

CI 100µF elect. 25V *C2 0·1µF 10% *C3 1,000pF 5% *C4 0·1µF 10%

*C5 1,000pF 5% *C6 1μF 10% *C7 0·01μF 10%

*C8 ΙμΕ΄10% *C9 0.01μΕ 10% C10 100μΕ elect. 25V

CII 100μ F elect. 25V *CI2 2,200pF silver mica 5%

*C+3 2,200pF silver mica 5% *C14 150pF silver mica 5%

* These capacitors can also be 1% polystyrene (Wima), 1% silver mica, or 2½% polystyrene according to availability (see text)

Miscellaneous

Perforated s.r.b.p. 0-lin matrix 3\frac{3}{2}\in \times 2\frac{3}{2}\in (2 off) Sample of "Cir-Kit" and extra wiring (see text) Batteries 9V type PP9 (4 off) or see text Coaxial output cable, knobs, battery connectors Aluminium sub-chassis

Metal case to choice (prototype uses Peak Sound case, $12 \text{in} \times 9 \text{in} \times 3 \text{in}$, type SA8-8 with wood ends)

high frequencies. For frequencies below about 100Hz the converter output is directly coupled to the attenuator (Fig. 3). This overcomes the charging and discharging problems of an output coupling capacitor which would otherwise prevent rapid switching at these low frequencies.

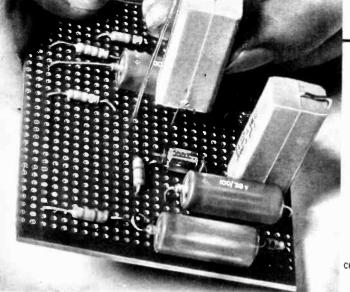
ATTENUATOR

The output attenuator is a simple potential divider arrangement with fine control at VR3 and coarse control by switched resistors (Fig. 3). All values of resistors should have five per cent tolerance, but it is well worth calibrating the output on each switch range,

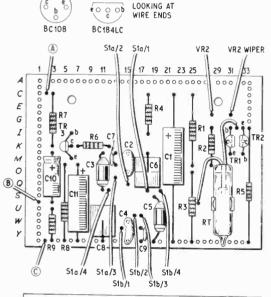
with VR3 wiper set at the R16 end of the track, against a known standard a.c. voltage source.

STICK-ON WIRING

The form of construction suggested for this project uses plain perforated s.r.b.p. board (0·1 in matrix) with "Cir-Kit" adhesive copper strip (see accompanying article on how to use this form of "stick-on" wiring). The free sample, given with this issue of PRACTICAL ELECTRONICS, is sufficient to wire up the Wien bridge oscillator only, but there is no reason why the constructor should not combine this with the sine to square wave converter on one board; additional wiring material will, of course, be needed to do this.



The capacitors are positioned. Note the lead-out wire from the centre of the lower end of the large "stand-up" capacitor



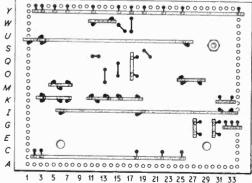
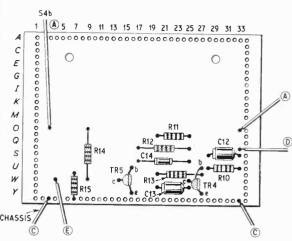


Fig. 4. Component positions and wiring layout of the Wien bridge oscillator board. To aid clarity only the relevant holes are shown for reference of positions



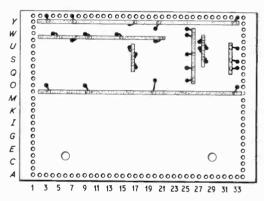
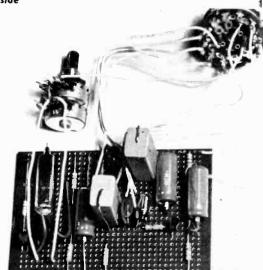


Fig. 5. Component positions and wiring layout of the sine to square wave converter. Only the outermost holes and wire fed holes are shown for reference. These drawings are shown half scale; the instructions on the free sample card apply only to full size drawings

The finished sine wave generator board with switch SI and ganged potentiometers VRI and VR2. Resistor R8 is hidden from view by CII on the right-hand side



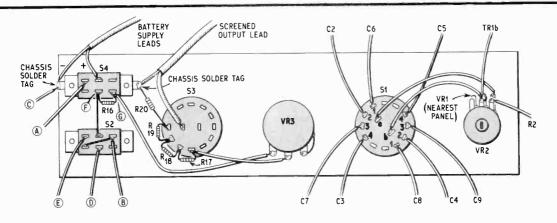


Fig. 6. Rear view of the front panel with inter-board wiring connections and attenuator (on S3). Ringed letters indicate connections shown in all previous diagrams and in Fig. 7 below

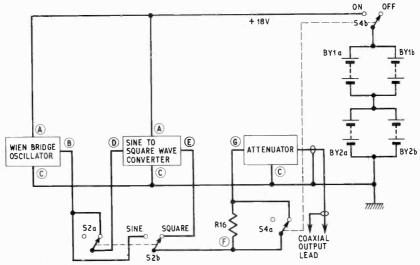
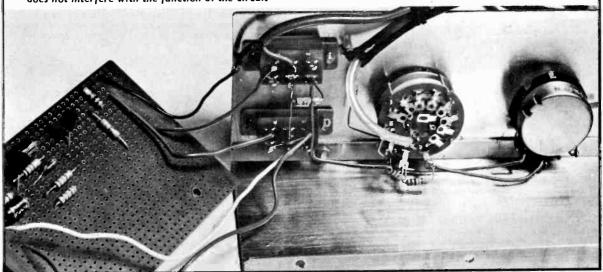


Fig. 7. Block diagram showing how the boards and attenuator are inter-connected and wired to the d.c. supply

The sine to square wave converter (below left) and the wiring of the attenuator switch S3 with control VR3. The two slide switches are S4 (upper) and S2 (lower). Resistor R16 is mounted on S4a for convenience and does not interfere with the function of the circuit



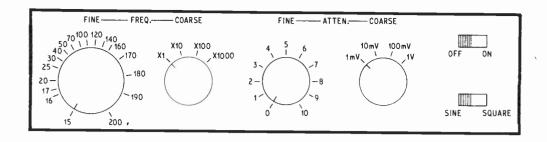


Fig. 8. Approximate positions of frequency and attenuator scale markings. The two slide switches are shown on the right

Wiring instructions are given in the drawings and photographs. The circled letters on the circuit diagrams correspond to those on the wiring diagrams.

Although the prototype version used "Cir-kit", there is no reason why the instructions given in the diagrams should not be applied to plain tinned copper wire. This can be anchored by threading into vacant holes and securing by the soldered joints. These must be sound in any case to avoid faults.

Rearrangement of the wiring layout can be done for other proprietary wiring boards without adversely affecting the circuit operation

affecting the circuit operation.

Because the circuit wiring is so simple the component boards can be easily mounted vertically on an aluminium sub-chassis, which would also take the front panel controls (see photographs).

ASSEMBLY

The diagrams in Figs. 4 and 5 show the inter-board connections and cross-reference is given in the schematic diagram in Fig. 6, to show more clearly the switching arrangement. It will be noted that S4a is used only as an anchor point for R16. The battery connections are also shown.

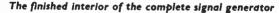
The front panel will need to be labelled as shown in Fig. 7, but the exact positions of fine frequency values will probably vary slightly between one potentiometer and another. It is desirable if at all possible to calibrate this scale using a reliable frequency source for comparison on an oscilloscope display. This would be more important for work with tuned filters than with a straightforward amplifier.

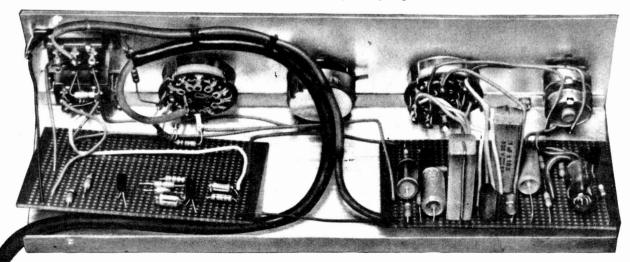
The attenuator scale should also be compared with an accurate known a.c. voltage source using a calibrated high impedance meter.

POWER SUPPLIES

It is recommended that the whole circuit is driven by four PP9 (or equivalent) batteries; two parallel pairs are wired in series to give a high capacity 18 volt supply. If the supply voltage is allowed to drop below about 17V the oscillator will cease to operate. In this respect, some constructors may prefer to incorporate a stabilised low voltage (18V) supply, details of which can often be found in text books and magazines.

One other advantage of a constant voltage source is that it overcomes problems of frequency variation and distortion which could otherwise result from too low a supply voltage.





CIR-KIT STICK-ON WIRING

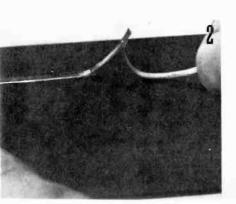
GIVEN FREE with this issue is a sample card of "Cir-kit", a versatile form of circuit wiring using self-adhesive copper strip (1). The strip has a protective paper backing which is peeled off when the copper strip is required to be stuck down on a plastics sheet (such as s.r.b.p.), cardboard, or wood.

T is a simple matter to arrange a circuit wiring lay-out with this strip cut to the required lengths and positioned anywhere on the board. It is also possible to arrange crossed over-lapping strips without short circuit risks, not easily achieved with conventional printed circuit board without using connecting link wires.

One example of a circuit that can be made up using this technique is shown in the previous article— Audio Signal Generator. There is

sufficient "Cir-kit" on the card to build *one* of the modules for this project; further supplies are only obtainable through the normal retail channels, many of which advertise in this magazine. It





should be noted that further supplies cannot be obtained direct from the magazine publishers.

CIRCUIT BUILDING

The series of photographs shown on this page illustrate how to use "Cir-kit" with s.r.b.p. sheet. The technique can be applied to almost any circuit construction using transistors and a typical stage by stage procedure is shown.

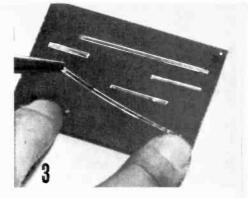
Cut the strip to the required length for the first piece and stick down before going on to the next (2). Do not remove the paper backing until after cutting. Maximum protection should be given to the adhesive until ready for sticking down. Do not allow the fingers to touch the adhesive unnecessarily or the sticking power will be impaired. Do not moisten the adhesive.

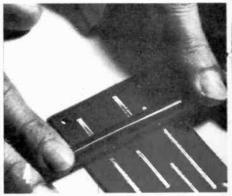
If a mistake is made the strip can be lifted and repositioned as required (3). When satisfied that each piece is correctly laid, smooth down all the strips firmly (4), then mark the positions of the holes on the s.r.b.p. with a scriber (5).

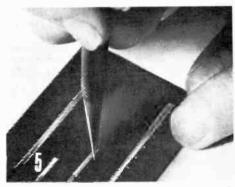
It is not necessary to drill through the copper (which might produce rough burrs); if holes are drilled beside the strips the component wires can be passed through the board, bent over on to the copper and then soldered (6). Use a small drill just big enough to accept the wires through the holes.

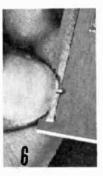
If the adhesive becomes softened by the heat from the soldering iron the copper may lift slightly; wait for it to cool and press down again firmly into position.

Crossovers can be made by building up the circuit on both sides of the board, or by placing one strip over another with thick paper insulation between them (7).

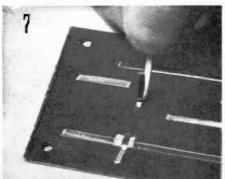














THE RADIO ASTRONOMY SATELLITE

Explorer 38, now in orbit, has confirmed that the earth radiates in the decametre band. In the part of the spectrum below 10MHz the radiation shows similar characteristics to that of the radiation from Jupiter. The sharp bursts narrowly beamed indicates a similar mechanism operating in the magnetosphere.

There is still much to be investigated in the decametre band, for some radiation is affected by the satellites of Jupiter particularly 10, Amalthea and the newly discovered

satellite.

The fact that the earth's magnetic field is very considerably less than that of Jupiter will almost certainly show a diminishing level of intensity from the lower frequency end of the decametre band to the higher frequency end. The effects of the solar wind are thought to be greater at the earth, and no doubt this will have to be taken into account.

There is evidence to suggest that there is a continuous background of radiation from Jupiter, its detection dependent upon the size of the aerial arrays used. There are also indications of pulses of radiation of a very rapid nature. The manner in which rapid changes in level, up to more than 100 times that of the normal background, arise has not been satis-

factorily explained so far.

The fact that the solar radiation, as indicated by Explorer 38, is very much higher than was previously thought at these low frequencies, may have a considerable bearing on future observations. From the point of view of earth based observatories, the ionosphere has a significant effect below 10MHz, though in some places like Tasmania satisfactory observations down to 2MHz have been made. The purpose of the large aerials (four of them each 230 metres long) was to monitor the region of the spectrum below 10MHz from its orbit well above the ionosphere.

RADIO SOURCES STUDIED BY BRITAIN AND USSR

Two major surveys have been completed by Jodrell Bank and the Ukranian Academy of Science at Grakovo. The Jodrell Bank survey is a very complete one covering 387

sources at frequencies of 2.695 and 4.996GHz. The Russian survey covered 80 sources at 12.6, 14.7, 16.7, 20.0 and 25.0MHz. This low frequency survey is an important one and may help to answer some of the questions relating to the grouping of the sources.

Some spectra show a characteristic shape particularly at low frequencies. Many of the sources have a relatively flat spectra at high frequencies and then show a wide change below about 50MHz. Making due allowance for the various effects of the ionosphere, some sources such as 3C48, a quasar, has a spectra which bends down sharply. On the other hand 3C295 shows a turn down for a few megahertz and then a rise. Others yet again show a sudden steep rise at low frequencies.

The value of the work done by Jodrell Bank and Ukranian Academy of Science lies in the wide range of frequencies covered. It is now possible with these two surveys added to the Cambridge surveys to plot the spectra of a significant number of known sources.

Three of the sources examined in the Russian survey had a variation pattern of emmission over a period of several months. In particular 3C461, which is a supernova remnant, and 3C48, a quasar, have doubled their intensity in the low frequency part of the spectrum. This fact had not previously been noted in the literature.

As it is not related to the season of the year, it is not an ionospheric effect and must be a characteristic of the source. Some of the variations in the shape of the spectra must be due to differences in emmission mechanism.

In the synchrotron process, radiations are developed in a weak magnetic field by fast electrons. The bending downwards of the spectra (lower intensity) could be due to the absence of slow moving electrons or to the absorption of the radiation by the source.

A sudden increase in intensity is more difficult to account for and there may be a more complicated method of production of low frequencies. One possible way this could take place is the acceleration of electrons by a shock wave condition operating in the source itself or between it and the earth.

It is clear that further work in this frequency range may add a great deal to our understanding of the physics of cosmic sources.

CANADA SHAPES HER SATELLITE BEAM

Canada has departed from normal in the coverage of territory by the aerial pattern of her satellite for synchronous orbit. If the normal type of aerial were used it would be necessary to provide ground stations with much larger aerials at the edge of the beam.

The new aerial that has been developed will have a basically parabolic beam but so shaped that a kidney pattern will result. The difference in level overall is reduced to less than 1.0dB and all the ground stations can therefore be of one standard type. The aerial measures 1.3 metres by 1.5 metres and there is an offset horn-fed driver to a nominally parabolic reflector.

Allowances have been made in the design for satellite positioning and altitude variations and for the northern latitude path length which adds attenuation losses. The aerial will be arranged on the satellite so that its beam points always to the

earth.

COLOUR TELEVISION FROM SPACE

The normal colour television equipment is physically too large to have aboard a spacecraft and a last minute decision to transmit live colour from *Apollo 10* was the result of a successful demonstration of a new system small enough to be accommodated in the module. The *Apollo 11* spacecraft also carried the same system.

In essence the system is little more than a black and white camera with a three colour disc spinning between the lens and the tube. A series of pictures are taken through the red, green and blue filters on the disc, which spins at 60 revolutions per second, and amplified and recorded on a six track disc recorder. After a series of each colour has been received, the three colours are read out simultaneously.

INTERNAL REFLECTION

The camera shots from the fixed camera on Eagle showed many internal surface reflections within the lens system and on several of the shots, where Aldrin walked diagonally away from the camera, the reflection revealed a figure moving divergently; when the astronauts stepped into shadow they disappeared from sight. These are some of the facts known and spoken of by many people before the moon landing, often they were at best half believed. Once more the proof appeared.

It is worthwhile contemplating on the amount of right thinking that has gone to make space a success.

ROYAL RADAR ESTABLISHMENT

A BRIEF LOOK AT BRITAIN'S LARGEST ELECTRONICS RESEARCH CENTRE

In an idyllic setting in peaceful Worcestershire countryside with the Malvern Hills rising steeply just a mile away in the west, is the Royal Radar Establishment, Britain's largest centre for electronics research. (The Ministry of Technology suggest it may well be the largest in Europe.) The Royal Radar Establishment evolved from two famous war-time establishments, T.R.E. and R.R.D.E. which were concerned with methods of locating aircraft by radar reflections. R.R.E. is still responsible for the development of radar systems for all three Services, but its activities are now much wider and cover an extensive range from basic physics research to advanced equipment development.

There are apparently no recruitment problems at R.R.E. Despite attractive offers from certain overseas countries, the brain drain has little effect at Malvern; quite the reverse in fact, since many British engineers and scientists earlier wooed away to North America have eagerly seized opportunities to return to the United Kingdom and to

work at the R.R.E.

It is not the wonderful pastoral location which provides the magnet—although this must surely add to the attraction of working at Malvern. The incentive to join the Establishment is the nature and scope of the research and development being undertaken there. Some idea of the extent and importance of this work was revealed during the Open Days in June last.

There are two major departments in R.R.E. The Physics and Electronics Department specialising in the development of new electronic materials and devices, and the Military and Civil Systems Department which is concerned with electronic systems for particular applica-

tions.

SOLID STATE MICROWAVE DEVICES

It is difficult for an outsider to attempt to evaluate, and place in any order of importance, the great variety of activities the Establishment is currently engaged upon.

This battery-operated radar transmitter and receiver uses a pin-head size crystal of gallium arsenide as the generating source of microwaves. It can be used for detecting moving objects and indicating their speeds on the meter shown. The equipment is potentially suitable for use in



In terms of emerging technology, however, the value and future significance of the present work in the field of semiconductor microwave oscillators is clear to see.

The first gallium arsenide X band oscillators were made at the R.R.E. in 1965. Since then, they have been manufactured commercially, and have found application in hand-held radar speed-meters, train approach warning systems, burglar alarms, signal generators, microwave communication links, and as local oscillators in radar equipments.

Particularly interesting as an example of recent work is the portable c.w. radar, with solid state generator, which can measure the velocity at which a ship is approaching its berth. This system was designed by R.R.E. in conjunction with Esso Petroleum Co. Ltd., specially to facilitate the

docking of super tankers.

INFRA-RED DETECTORS

One of the activities of the Physics Group is the development of infra-red detectors and the study of the fundamental properties of the semi-conductor and other materials from which detectors are made.

materials from which detectors are made.

There are two main types of infra-red detectors. Thermal detectors such as the thermopile, bolometer and the Golay cell. A newer one, which R.R.E. is working on at present is the pyroelectric detector. This makes use of the temperature coefficient of the internal electrical polarization of materials such as triglycine sulphate or lithium niobate.

Then there are photoconductive detectors, now becoming commercially available, due to a mixed compound material discovered at R.R.E.

MATERIALS DIVISION

The reference to new electronic materials brings into the picture a very important part of the Physics Group.

The Materials Division has grown up over the past decade to meet the need for new materials among teams working within the Establishment on new solid state devices. As the number and variety of such devices has increased so the Division has grown until it is now one of the largest teams in Europe dedicated solely to the preparation of single crystals.

The successful development of the many solid state devices on which scientists have been and are still working depends on the constant availability of well-characterised high-quality single crystals of the essential materials. The newest materials are not usually available from commercial sources and of necessity must be specially developed.

In its early days the Division was concerned with growing the elements silicon and germanium for use in semiconductor devices. After this came an interest in compound semiconductors beginning with the pioneer work on indium antimonide for use in far infra-red detectors. Another very important semiconducting compound is gallium arsenide, which has come into prominence for the fabrication of Gunn effect oscillators. Recently the work has been extended to include a number of ternary semiconducting materials with device potential.

LASER AND ELECTRO-OPTIC MATERIALS

With the invention of the laser the research broadened to include work on the production of suitable host-lattice materials such as ruby, calcium fluoride, calcium tungstate and yttrium aluminium garnet. Electro-optic devices have necessitated the growth and investigation of a variety of materials including lithium niobate, thio-acid salts such as proustite (silver ortho-thioarsenite) and pyrargyrite (silver thioantimonite) and various water-soluble com-

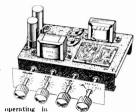




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recongry constructed on right steel chassis bronze hammer enamel finish, size 91 5 4 jin. high.

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PU2—110m/v, 1 meg input impedance.
Tape—110m/v, 1 meg input impedance.
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Circuit diagram, construction details and parts list (free with kit) 1/6, (S.A.E.).

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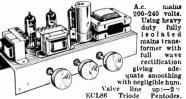
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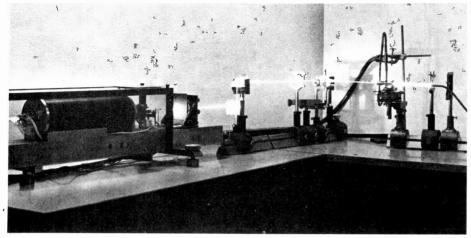
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Turbulence studies by laser doppler spectroscopy. This technique, developed at R.R.E., in collaboration with A.E.R.E. and University of Kent, offers several advantages over previous methods, e.g. high spatial resolution, absolute velocity measurement, and no disturbance of the flow. The argon-ion laser in the foreground was developed by the British Admiralty and is the most powerful sealed-off laser of its type in the world

pounds such as potassium dihydrogen phosphate. Among the most recent developments are pyroelectric and electroacoustic materials, for example, triglycine sulphate and zinc oxide.

A new class of materials is that of the semiconductor eutectics consisting of two sets of single crystals grown simultaneously from the melt. An interesting example is the cadmium arsenide/nickel arsenide eutectic whose rod morphology affords useful magnetoresistive properties.

Examples of non-crystalline materials also developed in the Division are a series of chalcogenide glasses transmitting in the infra-red.

NEW GROWING TECHNIQUES

Concurrently with growing crystals there has been much work on the development of techniques and equipment for the growth of crystals together with research on a variety of related topics. The technique most frequently employed in the Division for the production of crystals has been growth from the melt by vertical pulling (usually referred to as the Czochralski process). Other meltgrowth techniques such as zone-melting and the Stockbarger, Bridgeman and Kyropoulos processes have also been used.

The simple puller originally designed by the Division to produce its first germanium crystals has been developed over the years into a refined and highly versatile apparatus which can produce a whole range of single crystals of refractory materials with melting points up to that of spinel (2,135°C). Spinel crystals with masses up to 150gm and sapphires up to 250gm have been grown. To extend the range of temperatures still further, a new crystal growth technique has been developed using gas laser power as the source of heat. By this means oxide crystals have been grown with melting points up to 2,500°C; for example, yttrium oxide.

The applications of vertical pulling have been further extended by the development of the liquid encapsulation technique to prevent the loss of volatile constituents from the melt. Gallium arsenide and indium arsenide have been produced using this technique. The latest addition to the R.R.E. puller is a work-chamber capable of withstanding a pressure of 200 atmospheres. This is used, in conjunction with liquid encapsulation to pull crystals of substances that have a high vapour pressure at the melting point, for example gallium phosphide and indium phosphide

MILITARY AND CIVIL SYSTEMS

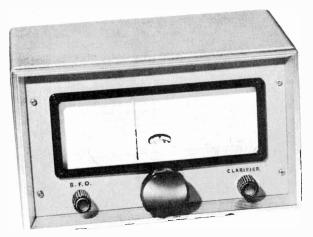
Advanced electronic equipment for particular applications is the concern of the Military and Civil Systems Department. Research is now being carried out in respect of the combined use of radars and computers to assist Air Traffic Controllers to handle air traffic. The computer assisted approach sequencing system (C.A.A.S.) aims to increase the landing capacity of a busy airport by assisting controllers to attain consistent intervals between landing aircraft.

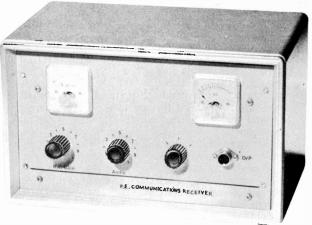
The Touch-Display is a novel input/output device for computers which has been developed at R.R.E. to provide an efficient method of communication between man and machine. The device has a number of wires placed on the face of the ray tube. These wires are made, by electronic means, sensitive to the touch of a finger and information is written by the computer as characters, words or even complete sentences against them. The "controller" indicates his reaction to the information shown by touching the appropriate wire. The Touch-Display is thus an integration of the electronic data display and a keyboard whose engravings can be varied to suit the needs of the moment. Its possible commercial application include air traffic control, car ferry bookings, etc.

Much of the Establishment's work in the field of military radar is necessarily of a restricted nature, and details are not generally revealed. But one example on display was The Rapier guided weapon system. This permits a supersonic direct-hitting missile to be automatically commanded to follow an optically established sightline to the target. A surveillance radar is used for target detection and provides information from which the optical sight can be laid on the target. Flares are mounted in the tail of the missile to provide a light source for detection by a television camera in the tracking head of the control unit.

The R.R.E. Small Portable Radar Torch (SPRAT) is an experimental hand-held radar which weighs less than 5½ pounds. It is completely self contained and will operate for several hours from a rechargeable battery housed in the handle. It is intended for use at night or when visual observation is impossible and under such conditions a trained operator can detect, locate and classify moving







P.E. WIDEBAND H.F. GOMMUNIGATIONS RECEIVER

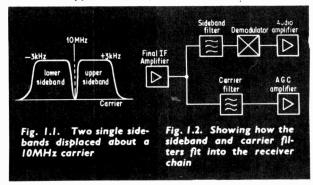
By R. HIRST S.T.C. LTD.

This series of articles describe a modern high frequency receiver working on the principle of single sideband (s.s.b.) transmission and reception. The main features of the design lie in the introduction of a wideband front end r.f. amplifier and a simple modular constructional approach. This does not mean to imply that the receiver is necessarily a simple unit to construct or to electrically "set up" but indicates that the mechanical design is broken down into a number of easily recognisable sub-units.

Before the specific design is described in detail it is desirable, for the sake of newcomers to this field, that some of the more fundamental aspects of single sideband transmission, and the resultant reception, are presented in a simple form.

PRINCIPLES OF S.S.B.

Fig. 1.1 shows two single sidebands displaced about a 10MHz carrier, one above the carrier frequency, this is called the upper sideband, and one below the carrier,



this being the lower sideband. For normal speech transmission and reception a 3kHz bandwidth is quite adequate, therefore the upper sideband will be between 10MHz and 10·003MHz and the lower sideband between 9·007MHz and 10MHz. A receiver is called a single sideband receiver when it is capable of receiving information in one sideband or the other and an independent sideband receiver when it is capable of receiving and presenting information in both sidebands simultaneously.

The receiver described in this series is a single sideband receiver but it is relatively simple to convert it to an independent sideband receiver, that is, from s.s.b. to i.s.b.

In single sideband operation two distinct pieces of information are transmitted; these are, the carrier—to operate automatic gain control and automatic frequency control—and the sideband information—to convey the required information to the receiver. Usually only a small portion of the transmitted power is used to provide the carrier and the much larger proportion contains the intelligence. It is common to find that the carrier level is 16dB or 26dB below the sideband information and for the sake of simplicity during this initial examination it is proposed to consider that the carrier is 26dB below the sideband.

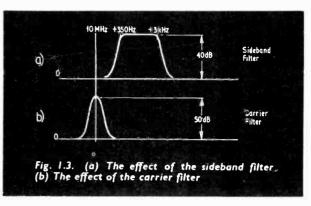
After the last i.f. amplifier the received signals are split into two paths, the carrier path and the signal path. The carrier path is used to provide automatic gain and frequency control, the latter for more complex receivers, and the signal path converts the sideband information into audio. It is therefore necessary to adequately filter out the frequencies required for both paths and the diagram of Fig. 1.2 indicates how these two filters fit into the back end of a receiver chain.

NOISE EXCLUSION

Due to the fact that the carrier signal is so much lower than the sideband signal, it is essential to reduce the bandwidth of the carrier acceptance filter to exclude noise from the circuit. 'If a sideband signal of approximately 1 microvolt is considered with a signal to noise ratio of 12dB in a 3kHz bandwidth, then the carrier signal in the same bandwidth would have a noise to signal ratio of 14dB if this signal was 26dB below the sideband signal. Under these circumstances the noise would operate the a.g.c. and the sensitivity of the receiver would be considerably reduced.

In order to have a workable signal in the carrier path it is desirable that the signal to noise ratio is better than 10dB, therefore the signal to noise ratio in the carrier path has to be improved by 14 + 10dB, i.e. 24dB or eight times. The method of working out the bandwidth of the carrier filter is very simple once the relative levels have been determined and from the formula in expression 1:

Carrier filter bandwidth =
$$\frac{\text{sideband width (Hz)}}{X}$$
 (1) = $\frac{3,000}{8} = 375 \text{Hz}$



AUTOMATIC GAIN CONTROL

The information derived from the carrier path is converted into a d.c. voltage and fed back to the preceding amplifiers to promote automatic gain control holding the gain of the receiver relatively constant over a considerable range of input signals. The a.g.c. is fast in its attack but when the carrier signal is removed, some considerable time may elapse before the receiver is returned to its fully sensitive state. This is to stop the receiver gain moving up and down by large amounts when the carrier signal is affected by a

SPECIFICATION

Sensitivity Signal to Noise ratio Audio bandwidth	2 microvolts in the sideband for S.S.B. operation to produce full output. Better than I0dB at 2 microvolts sensitivity. 750Hz to I-75kHz or 350Hz to 3kHz.	Intermodulation products	With the r.f. gain control set for maximum sensitivity, two unwanted signals, with an amplitude of 100 millivolts will not produce in band interference of more than an equivalent aerial signal of	
Frequency range Stability	2MHz to 30MHz. With crystal operation better than four parts in ten to the sixth.	Emissions (Receptive modes) Power supply	8 microvolts. A3h (compatible d.s.b.), A3a (s.s.b.), A1 with suitable attachment (see text). 0-220-240 volts 50Hz.	
A.G.C.	For a change in level from 2 microvolts to 65dB above 2 microvolts, the audio output will not vary by more than 4dB.	Controls Metering	I. R.F. gain. 2. Audio gain. 3. Function switch. 4. Tuning control (optional). I. Signal strength. 2. Audio level.	

(Where X has been computed as described in the preceding paragraph.) The carrier filter is equally displaced about the fundamental signal of 10MHz, accepting signals 187.5Hz either side of 10MHz. In order to avoid accepting sideband information in the carrier filter, it is usual to make the carrier filter between 40Hz and 100Hz wide. Fig. 1.3 shows (a) the effect of the sideband filter and (b) the effect of the carrier filter.

fast fade. The a.g.c. has not been fed back to the r.f. amplifier in the following receiver as this level may be stabilised by the introduction of an aerial attenuator when the aerial signal reaches large proportions.

DOUBLE SIDEBAND OPERATION

For double sideband operation (d.s.b.), the transmission is treated as a single sideband piece of informa-

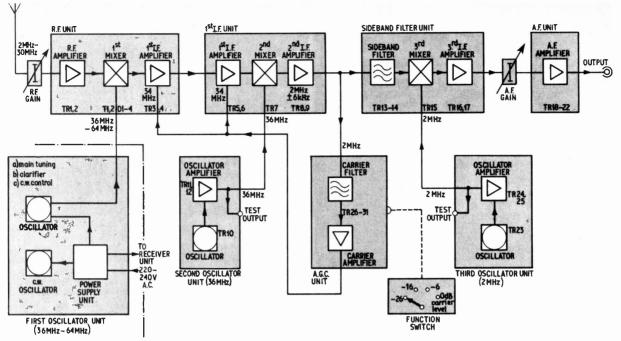


Fig. 1.4. The block schematic diagram of the complete P.E. wideband h.f. communications receiver

tion but the carrier amplifier has its gain adjusted by the function switch to take into account the increased level of the carrier. This type of d.s.b. operation is classed as "A3h" where the signal to noise ratio will be somewhat reduced upon the standard form of transmission due to the acceptance of only one of the sidebands.

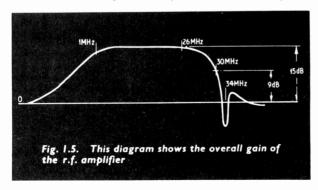
While the introductory paragraphs have only skirted the workings of a modern sideband receiver, it is hoped that some of the elementary points have been made in such a manner as to clear certain relevant principles.

RECEIVER CIRCUIT

Moving into the receiver proper it is intended to present the equipment as a series of modules for ease in construction. This part describes the basic operation of the receiver and gives a block diagram showing the functions of its various parts. Following articles will detail the circuitry and give full constructional details of the modules and the final assembly.

As indicated earlier, this is not a project to be lightly undertaken as it does require some reasonable knowledge of soldering and previous experience of laying out circuits dealing with relatively high frequencies.

The majority of the filters have been designed around coils even though high frequency crystal filters have been available for quite a few years. This is mainly to



keep the cost of the overall receiver within a reasonable budget. For the more affluent, crystal filters may be used and full directions will be given to incorporate a number of alternatives. A circuit of a b.f.o. is included to enable the operator to deal with the more simple "on/off" keyed transmissions (c.w.).

R.F. UNIT

This module is described fully here and constructional details and a circuit diagram will be published next month. In the block schematic shown in Fig. 1.4 the aerial signal is fed into an attenuator which may be manually operated by the user. The r.f. amplifier contains a wideband two stage amplifier which is not affected by a.g.c., and amplifies aerial signals in the range 2 to 30MHz. The gain of this amplifier is shown in Fig. 1.5 over the frequency range and the fall off at the upper end is due to the introduction of the 34MHz i.f. rejection filters. However there is sufficient gain in the range 26MHz to 30MHz to make the receiver perfectly usable in the top 4MHz.

The first two stages comprising the r.f. amplifier have an overall gain in the order of 5 times and the output of this amplifier is fed into the first mixer. The amplifier has a considerable dynamic range and is quite capable of handling signals from 1 microvolt to half a volt without the introduction of detrimental intermodulation and crossmodulation. This is a dynamic range of 54dB and accounts for the use of a high supply voltage and power devices in the front end stages.

The 2N3866 transistors used in this r.f. amplifier can in fact handle up to 5 watts of power over the complete frequency range. It is in this area that the whole performance of a receiver can be determined, therefore the introduction of relatively expensive components in the early stages may be excused. Due to the considerable amount of current passed through the first two devices, the signal to noise ratio of the receiver is not necessarily as good as professional receivers covering the same range but it must be appreciated that the very high grade communication receiver complexes may cost anything up to five or six thousand pounds.

UP-CONVERSION TECHNIQUE

Coils L1 and L2 are rejection filters set accurately at 34MHz to ensure that the i.f. amplifier is not loaded by a direct aerial signal of 34MHz. T1, T2, and D1 to D4 form the first mixer in the well-known "ring modulator" configuration where the aerial frequency is subtracted from the first oscillator frequency giving an output at 34MHz. This "up-conversion technique" is well proven and ensures that the image response, that is to say, the aerial signal plus the oscillator frequency, is well above the response of the following amplifier. It is this up-conversion that enables the normal front end coil system to be dispensed with.

It is often mistakenly assumed that the introduction of a number of selective tuned circuits prior to the first mixer removes intermodulation and cross-modulation distortion. However, while it may be that some hundreds of kilohertz away from the fundamental frequency, assistance is given by the inclusion of such circuits, they have virtually no effect when the receiver is measured in accordance with C.C.I.R. as these measurements are made only 10kHz removed from the

required frequency.

The first i.f. of 34MHz has now been established and it would be desirable to pass these signals through a narrow band crystal filter, however, this type of filter is expensive and could cost in the order of £30, therefore a three stage coil filter has been introduced, two of which appear in the r.f. unit. The first filter has been introduced before the first stage of the i.f. amplifier to get some discrimination as soon as possible, this is immediately followed, after some amplification, by another tuned circuit which is in the collector of the first stage of the i.f. amplifier. This is also the first amplifier to be controlled by the a.g.c. system and due to the forward a.g.c. action the i.f. discrimination improves as the aerial signal increases due to the lowering of the input impedance of TR3, therefore effectively increasing the Q of the first tuned circuit in series with TR3 base.

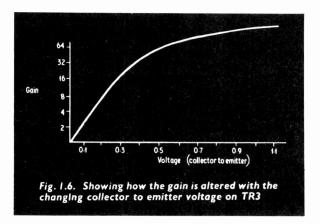
A.G.C. OPERATION

The a.g.c. works on the forward characteristic where a reduction in the collector to emitter voltage, due to an increase in base and collector current, reduces the gain of the stage by as much as 35dB. Part of this reduction in gain is due to the reducing input impedance of TR3, this acting as an attenuator in conjunction with the series element L3 and C.

This curve is shown in Fig. 1.6 and is more commonly referred to as the V_{CEsat} condition. This is one of the many forms of applying automatic gain control to a transistor and where signals of a relatively small amplitude are being dealt with, little or no distortion is introduced. The gain of these latter two stages are in the order of six times giving an overall gain in the r.f. unit of approximately thirty times. Some loss occurs in the mixer, therefore the full overall gain available is reduced by the amount of this loss. The two inputs and the one output of the r.f. unit are terminated in 50 ohm coaxial sockets which are readily available.

FIRST I.F. UNIT

Transistor TR5 is the last stage of the first i.f. filter, tuned to 34MHz. The stage gain is variable due to the a.g.c. voltage applied to the base of the transistor and the stage gain is reduced in an identical manner to that indicated in Fig. 1.6. The overall change in gain of TR5 is approximately 30dB, giving a total of 65dB for the whole of the first i.f. amplifier. TR6 presents a high



impedance to the tuned circuit in the collector of TR5 thus avoiding undesirable damping with a consequent reduction in selectivity. TR6 converts an approximate input impedance of 5 kilohms into an output impedance of 200 ohms which feeds the following mixer.

The second frequency changer TR7 is a combined converter and amplifier where the signal is fed into the base at 34MHz and the oscillator frequency of 36MHz is applied to the emitter of TR7 at sufficient level to promote good switching. The collector circuit is tuned to 2MHz thus accepting the wanted frequency of 2MHz and rejecting to some degree the 34MHz input signal and the switching frequency of 36MHz. This time, to avoid damping the tuned circuit, the impedance change to the following circuit is effected by a capacitor divider where the impedance change is a function of the square of the capacitor ratio.

Transistors TR8 and TR9 form the second i.f. amplifier at 2MHz and considerable voltage gain is effected by the common base stage, TR8. The voltage gain of this stage is approximately equal to collector load divided by the source resistance. In order to take advantage of the voltage gain available, TR9 has been introduced as an emitter follower with an input impedance in the order of 30 kilohms, the output of which feeds into the next module, the sideband filter and third converter.

It is possible to directly couple this particular amplifier as a.g.c. has not been applied, therefore the d.c. conditions remain the same irrespective of signal input level at the aerial. For an aerial input of 5 microvolts in the sideband the output at 2MHz is approximately 500 microvolts. Therefore the nine stages employed up to this point have an overall gain of 100 times, i.e. 40d B.

This amount of gain may appear to be paltry for such a considerable amount of circuitry but each of the mixers have a loss in terms of efficiency of about 6dB therefore the overall gain of the amplifying stages is something in the order of 52dB.

SIDEBAND FILTER UNIT

This module commences with a five stage crystal filter which separates the upper sideband of the transmission from the carrier and the lower sideband. This filter has a relatively flat passband from 2 000750MHz to 2 001750MHz which determines the final audio bandwidth of 750Hz to 1 75kHz. An eight stage crystal filter is described later for the constructor who requires a passband in the order of 3kHz.

The five stage filter however is relatively economical and just about suffices the requirements of speech trans-

mission and reception. Having separated the required upper sideband, the resultant signal is fed into the demodulator where it is converted to audio and the high unwanted frequencies are filtered out by a simple *LC* filter. The level is now amplified sufficiently to drive the audio amplifier.

A.F. UNIT

As there is considerable work involved in constructing this receiver, there seemed little point in building an audio output amplifier when a pre-built unit is available which adequately meets the required specification at a reasonable cost. This is the Newmarket packaged circuit module Type PC2 which may be purchased from Newmarket Transistors Ltd., or their accredited agents. It uses five transistors, TR18-22.

This unit can deliver 100 milliwatts into a speaker or up to 5 milliwatts into headphones and the level of the output may be controlled from the front panel of the

receiver.

SECOND OSCILLATOR UNIT (36MHz)

This is a crystal high stability oscillator of the emitter coupled variety where the high impedance in the collector circuit is transferred into the required low impedance drive for the emitter, by a capacitive divider network. The crystal used is of the overtone variety and it is therefore necessary to tune the collector of the transistor circuit to obtain the required frequency.

The single stage oscillator TR10 is followed by a d.c. coupled pair TR11 and TR12 which provides up to a volt of output at low impedance to act as the switching voltage in the second mixer thus converting the intermediate frequency of 34MHz into the required 2MHz.

A.G.C. UNIT

In this unit the 2MHz carrier signal is sampled and selected from the upper and lower sideband by a narrow band crystal filter. As previously explained in the introduction, this filter is necessarily narrow in order to improve the signal to noise ratio of the carrier signal. The carrier signal is now amplified and converted into d.c. by the voltage doubler circuit D5 and D6.

Even though the following capacitor is very large the attack time of the system is less than 50 milliseconds due to the low impedance of the source. Once the a.c. signal is removed the capacitor cannot discharge through the source as the diodes are now almost open circuit, therefore the following series resistor acts as the discharge path taking approximately 20 seconds to discharge fully when an aerial signal in the order of 10 millivolts is removed. This avoids the gain of the receiver changing rapidly as a result of rapid carrier fading.

Having converted the carrier signal to d.c. by D5 and D6, the d.c. voltage is amplified and fed to the bases of TR3 and TR5 in the r.f. unit and the i.f. amplifier. With a signal in the order of 5 microvolts in the sideband at the aerial, with the carrier 26dB below this level the d.c. voltage is approximately 2.5 volts. However, when the aerial signal has increased to about 5 millivolts with the r.f. gain set for maximum sensitivity, the d.c. output of the a.g.c. unit is 11 to 12 volts thus promoting full a.g.c. over the receiver chain. Once the aerial input has exceeded 5 millivolts it is necessary to reduce the sensitivity of the receiver with the r.f. gain control which is mounted on the front panel.

The level of the a.g.c. voltage is monitored on the front panel by amoving coil meter and when this indicates that the full a.g.c. condition has been reached the

r.f. gain control should be used to introduce some attenuation so that there is always some a.g.c. in hand. For different carrier levels of the transmitted information, a calibrated potentiometer is located on the front panel so that the carrier level may be adjusted to give zeroreading on the v.u. meter.

THIRD OSCILLATOR UNIT (2MHz)

This unit is almost identical to the 36MHz oscillator but the frequency of operation is 2MHz to provide the switching voltage for the final converter. The crystal used is of the fundamental type, therefore it would not normally be necessary to include a tuned circuit in the collector of the oscillator. However, to reduce the effects of the second harmonic that may be generated in the oscillator stage, a simple tuned circuit has been included. The output from the single stage oscillator is fed into a d.c. coupled pair which gives up to one volt of signal at low impedance. The frequency may be adjusted to within 1Hz and once set there should be no need to make any further adjustment for some months.

MAIN CHASSIS ASSEMBLY

The main chassis contains all the inter-module wiring and the external controls which would be used during normal day to day operating. The r.f. gain control may be adjusted to reduce the input level received by the first amplifying stage in the r.f. unit. This control would only be brought into operation when the aerial signal has reached something between 1 and 5 millivolts. However, if considerable interference is present on the frequency required the r.f. gain control can be used to see whether the level of the interfering signal is sufficiently high to generate intermodulation products within the receiver itself.

The audio gain control is to enable the operator to adjust the output level at the speaker or the headphones and does not have any affect upon the working characteristics of the receiver. The function switch adjusts the level at which the automatic gain control comes in and can cater for carrier levels of -26dB, -16dB, -6dB and 0dB. If the constructor so desires this switch may be replaced by a potentiometer that will give a constantly variable adjustment of carrier level but it will be necessary to calibrate the control so that the required condition may be located to suit the service being received.

FIRST OSCILLATOR UNIT

This unit has been presented in a separate container of similar dimensions to that of the receiver cabinet. This has been arranged so that the constructor may choose one of a few different methods of obtaining the tuning mechanism for the receiver. In one instance the unit comprises an LC oscillator and a mixer system so that fully variable coverage over the range 2MHz to 30MHz may be obtained. Another unit is a simple crystal oscillator with a high degree of stability for spot frequency working.

Included in this cabinet is a b.f.o. for c.w. reception. The first oscillator unit also contains the power supply for the entire system and is connected to the receiver unit by a multicore cable. The whole of this cabinet will be described in more detail in later articles when the constructional and operational details are

presented.

Next month: circuit diagram, components list, and constructional details for the r.f. unit module.



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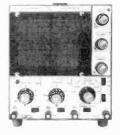
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control networks to be driven.

This article will cover the design and basic performance of the amplifier, the essential features of its use and the design of a suitable power supply. The subsequent constructional articles will cover its use in different amplifier designs.

for use in mains operated record players, etc. They deliver up to 3 watts r.m.s. continuous sine wave output and can operate directly from crystal or ceramic pickups. They also contain an integral preamplifier providing sufficient gain to allow tone

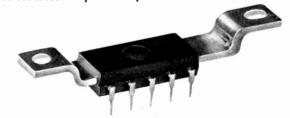
A PHOTOGRAPH of the amplifier, which is fabricated on a silicon chip measuring 0.05 in $\times 0.05$ in (by 0.008 in thick), is shown on this page. To allow removal of the heat dissipated, the chip is mounted on a steel bar in a special package to which a heat sink can be attached (see photograph). The circuit is available for operation at 2 watts output on a 14 volt nominal supply (SL402) or for operation at 3 watts output on an 18 volt nominal supply (SL403). The specifications allow adequate margin for normal supply voltage variations.

CIRCUIT DESIGN

The complete circuit is shown in Fig. 1. The ensuing description is included so that those interested in the circuit's operation may be satisfied. It is not necessary that the reader should be able to follow the detailed points of design in order to use the devices satisfactorily and indeed, since the description has been kept fairly brief, only those with appreciable experience of transistor circuit design could expect to understand the operation at first reading.

The circuit (Fig. 1) will be seen to consist of a simple preamplifier (TR1 to TR3) followed by the main amplifier (TR4 to TR13). The basis of the design is of course the output stage whose operation we will now consider. An all *npn* design is used since the integrated circuit process is not suited to the manufacture of high current *pnp* transistors.

The integrated circuit package used to house the SL402 and 403 silicon chip—shown full size



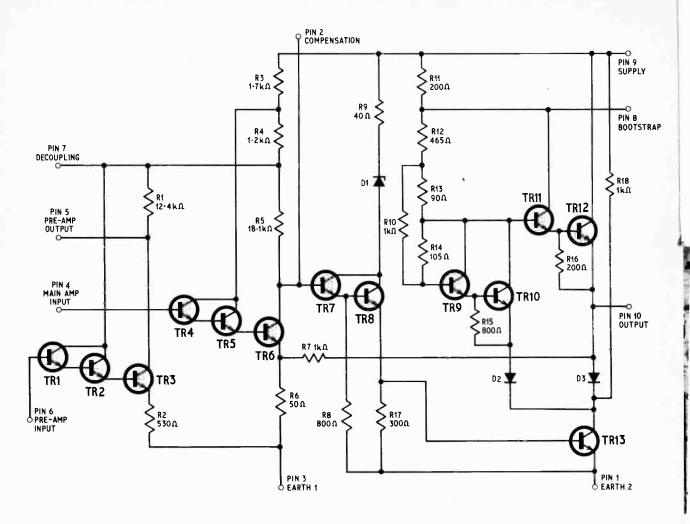


Fig. 1. Complete circuit diagram of the SL402 and SL403 integrated circuit audio amplifier

OUTPUT STAGE

The basic output stage is shown in Fig. 2. The three diodes serve to define the quiescent current and to steer the dynamic output current through one or other output transistor. It can readily be shown, from exponential characteristics of the transistors and diodes, that

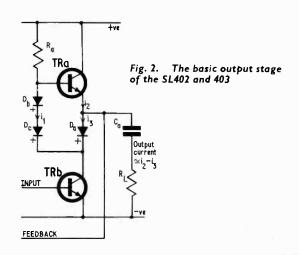
$$i_2.i_3 = Constant \times i_1^2 \tag{1}$$

Under quiescent conditions, neglecting any d.c. flowing in the feedback network, i_2 and i_3 are equal and thus controlled by i_1 , which is in turn controlled by R_a .

When signals are present the overall feedback assures the correct voltage and the biasing arrangements ensure that the output current is steered via one or other output transistor, since from equation (1) i_2 and i_3 cannot be simultaneously large. Thus during positive half cycles when i_2 is large, i_3 must be small, i.e. D_a is virtually out of conduction, R_a acts as the load of TR_b and TR_a acts as an emitter follower. During negative half cycles when i_3 is large, i_2 must be small, i.e. TR_a is virtually out of conduction and TR_b feeds directly into the load resistor R_{L^*}

Naturally the open loop gain is very different between positive and negative half cycles, and considerable negative feedback is required to linearise the operation.

Fortunately the integrated circuit process automatically gives us transistors with very high cut-off frequencies (approximately 1GHz) which, by keeping spurious phase shifts low, allow this feedback to be applied.



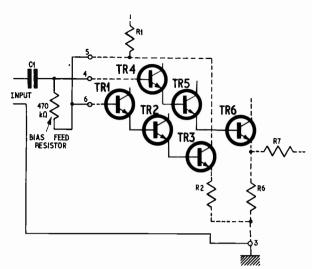


Fig. 3. Connections for using the preamplifier to bias the main amplifier

In the complete circuit, Fig. 1, it will be seen that TRa of Fig. 2 has been replaced by a Darlington pair (TR11 and 12) and D_b by another Darlington pair (TR9 and 10); the bias resistor has been provided with a bootstrap connection and an offset voltage has been generated in series with the bias "diodes" by means of R10, R13 and R14 (this voltage could be generated by a single low value resistor but the three resistor arrangement takes up less area on the integrated circuit). This offset voltage adjusts the constant in equation (1) and thus allows us to control the relationship between bias current through R12 and quiescent current in the output stage.

An external bootstrap capacitor (50µF is normally used) is connected between the output and bootstrap connections. This causes the voltage at pin 8 (bootstrap) to follow that at the output, so that the bias current through R12 is maintained at a constant level during positive half cycles; this is essential to guarantee sufficient base current for the Darlington output pair TR11 and TR12.

Incidentally D2 and D3 will not be readily seen in the chip photograph; they have combined with TR13 to form the lower of the two power transistors on the right hand side.

AMPLIFIER SECTION

The remainder of the main amplifier section is essentially straightforward. TR13 is fed via two emitter followers TR7 and TR8 from an input stage TR4, TR5 and TR6. This cascade provides very high input impedance and very low input current. Overall series voltage feedback is used and the collector of TR6 is brought out so that an external compensation capacitor can be connected to ensure stability of the negative feedback loop (the required capacitor— $0.01\mu\text{F}$ —is too large to be integrated economically).

Various precautions are taken to protect the amplifier against excess supply voltage: these include bypassing the emitter-base junctions with resistors, the inclusion of D1 and most important, the tapping of the collectors of TR4 and TR5 into the input stage load resistor. This is designed to achieve a situation in which, if the supply rises too high, TR5 protected by R3 breaks down before any other device in the circuit and in so

doing switches the rest of the circuit into a nonoperating state in which it can sustain much higher voltages than when operating normally. Thus the circuit is protected against overvoltages well in excess of the nominal operating value.

PREAMPLIFIER SECTION

The preamplifier (TR1, TR2 and TR3) serves also to provide a temperature compensated bias voltage for the main amplifier. It will be seen from Fig. 1 that the input bias required consists of the voltage across the feedback resistor R6 plus the base-emitter voltages of TR4, TR5 and TR6. Now base-emitter voltage varies with temperature at a rate of -2mV per degree C and it is therefore essential that the bias voltage be derived from a source with corresponding temperature variation. The preamplifier provides this source. Fig. 3 shows how it may be connected simply as a biasing network for the main amplifier.

Due to the very small input current of the amplifier the voltage drop along the external bias feed resistor will be small and can be neglected. The sum of the base-emitter voltages of TR4, TR5 and TR6 are matched by those of TR1, TR2 and TR3, so that the resultant voltage which must be developed across R6 is equal to that derived from the supply line across R2. Later we will see how the preamplifier may be used as such

whilst still providing the bias required.

To allow the use of a simple power supply with high ripple content, the supply to the pre-amplifier and main amplifier input stage is provided with a decoupling point (pin 7) to which an external capacitor (25µF suffices) is to be connected.

AMPLIFIER CHARACTERISTICS

The amplifier is available in two versions, distinguished by different operating supply voltage ranges. The ratings of the two versions are as follows:

Operating Range	SL402	SL403
Nominal operating supply voltage	14	18 volts
Maximum operating supply		
voltage Absolute maximum supply	16	21 volts
voltage Maximum output current	20	24 volts
(peak)	ı	l amp
Minimum load impedence	5.5	7.5 ohms

The "absolute maximum supply voltage" is the maximum transient voltage the amplifier will withstand without damage; it may, however, switch into a non-operating state as detailed earlier while the transient is present. The amplifier is guaranteed to operate at up to the rated "maximum operating supply voltage" which is 15 per cent above the "nominal operating supply voltage". This 15 per cent is intended to cover mains voltage variations. The power supply should be designed to give 14V nominal for the SL402 or 18V nominal for the SL403.

The amplifiers are rated to handle 1A peak (sine wave or square wave). The minimum load impedances specified ensure that this level is not exceeded at the nominal operating supply voltage. The small increase in current which may occur when the supply voltage is high, but within the limits specified, is allowable. If the load impedance used is significantly reduced however, the peak current rating will be

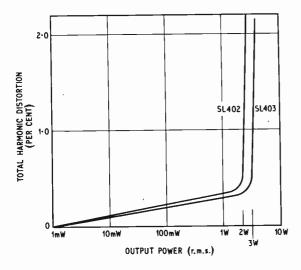


Fig. 4. Graphs showing total harmonic distortion of the two main amplifiers

considerably exceeded at full output, and prolonged operation under these conditions may cause failure of the circuit.

The amplifier characteristics are listed below for the two versions:

Test Conditions: SL402: 14V supply, 7.5 ohm load SL403: 18V supply, 7.5 ohm load

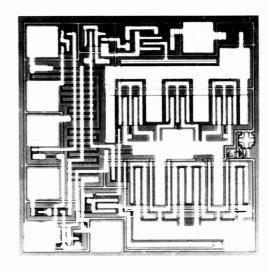
Characteristic	SL402	SL403
Maximum output power		
typical	2 watts	3 watts
Maximum output power		
minimum	1.5 watts	2.5 watts
Distortion: main amplifier	See	Fig. 4
pre-amplifier		er cent
F		n.s. output
Voltage gain: main amplifier	20	20 '
pre-amplifier	20	20
Input impedance: main		
amplifier	$>$ 10M Ω	$>$ 10M Ω
pre-amplifier	$> 10 \text{M} \Omega$	
Maximum input current:		
main amplifier	0·25µA	0.25 / A
pre-amplifier	0·25µA	0·25μA 0·25μA

Hum, noise and frequency response have not been listed here; they depend on how the device is used and will be covered in the later articles.

HEAT SINK REQUIREMENTS

The amplifiers dissipate up to 3W at full output and must be provided with a heat sink, or more accurately a heat radiator, to keep their temperature within reasonable limits. A total radiating surface of 10 square inches is required. This can be conveniently obtained from a channel section radiator, bolted to the package as shown in Fig. 5. The material may be aluminium, copper, brass or steel and should be 18 s.w.g. or thicker. The fixing bolts should be firmly tightened and fitted with plain washers both sides, but it is not necessary to use silicon grease between the surfaces, though it will do no harm.

As an alternative to using a separate radiator the amplifier may be bolted to the chassis of a complete



Photograph of the silicon chip as used in the SL402 and SL403

equipment. It must be remembered, however, that the metal bar through the package will be connected to the negative side of the supply, via the chip. It cannot therefore be directly affixed to the chassis if this is connected to the positive side of the supply (as in car radios if the vehicle has a positive earth for example).

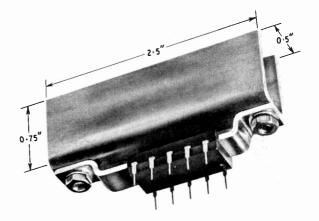


Fig. 5. Heat sink attached to the amplifier package

ESSENTIAL PRECAUTIONS

The following precautions should be observed when building and commissioning equipment using the SL402 and 403:

- (a) Do not short circuit the output; this is not invariably fatal but can be, and certainly will be, if the short circuit is maintained for more than a few seconds.
- (b) Never use the device without the prescribed heat radiator attached.
- (c) Do not short pin 4 (the main amplifier input) directly to ground; this upsets the output stage biasing and can cause failure.
- (d) Ensure that the supply potential is correct before switching on for the first time.
 - (e) Do not exceed the rated voltage and currents.

POWER SUPPLY

The SL402 and 403 are specifically designed to run on the simplest of power supplies. They may be operated from an unregulated car supply for instance or from a basic mains power supply consisting simply of transformer, bridge rectifier and reservoir capacitor, Fig. 6. The SL402 operating on a nominal 14V supply is particularly suited to operation from a car battery, in a radio or tape player for instance. The higher power, higher voltage, SL403 is more suited to operation on mains supplies.

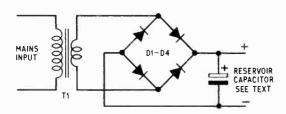


Fig. 6. Basic power supply circuit

The mains transformer for an SL403 power supply should give, ideally, 14V r.m.s. output and should be rated at 0.5A or higher per amplifier to be supplied. The voltage specified is the unloaded value and can be obtained from heater transformers. The following types are suitable and readily available:

- (a) Radiospares hygrade filament transformer Rated output: 2 × 6.3V at 1.8A (connect secondaries in series).
- (b) Radiospares standard filament transformer 13V Rated output: 13V at 0.5A Suitable for supplying a single amplifier only.

A mains power supply for the SL402 would require a transformer giving 11V r.m.s. unloaded output and rated at 0.5A per amplifier to be supplied.

The bridge rectifier again should be rated at 0.5A per amplifier to be supplied. It should also have a p.i.v. (peak inverse voltage rating) of 50V minimum. The following types are suitable and readily available:

- (a) Radiospares REC 41 Rated output: 1.5A
- (b) STC selenium rectifier bridge type P66E/1B Rated output: 1A Supplier: Electroniques.
- (c) Slater Electric potted rectifier bridge type SLA—50—LCD

Rated output: 2A Supplier: Electroniques.

The reservoir capacitor value required depends on the application. A value of $5{,}000\mu F$ will be sufficient for almost all requirements and in many cases $2{,}000\mu F$ or even $1{,}000\mu F$ will be found satisfactory. The voltage rating should be 25V.

The transformers listed are not fully enclosed types; it is worthwhile enclosing the whole power supply in a separate metal box to ease problems of hum pick-up.

The Plessey integrated circuits SL402 and SL403 are available from various retail suppliers.

Following articles will describe a simple mono record player amplifier without tone controls, a more elaborate stereo record player amplifier with full tone controls, and a stereo hi fi system. Full constructional information will be provided for all three systems.

NEWS BRIEFS

Equipment Confiscated

A RADIO communications expedition to North, East and South Africa, led by 25-year-old Mr David Dunn, of Cardiff, has run into difficulty with the Moroccan police.

The main objective of the four-man expedition is to study the reliability of low power short wave radio communications. Mr Dunn—a senior draughtsman with the Powell Duffryn Group company Hydraulic Machinery (Great Britain) Limited, did not have a transmitting licence for Morocco and, in accordance with Moroccan law, the radio equipment was confiscated.

Mr F. J. Seller, secretary of the Amateur Radio Society at the University College, Cardiff, said the party were told the equipment would be returned when the expedition left the country, but this promise was not fulfilled.

Mr Seller said in a recent letter from Addis Ababa, Mr Dunn told him that he was beginning to despair of ever seeing the equipment again.

"If this is so it will, of course, mean the end of any short wave communication aspect of the expedition," said Mr Seller. "This is most unfortunate since I understand Mr Dunn has transmitting licences for almost all the countries he has yet to visit."

New TV Equipment

A COMPLETELY new range of rugged, reliable and extremely compact television equipment, tested to stringent international military specifications, has been introduced by the Electro-Optical Systems Division of The Marconi Company. The new range, comprising a number of units which can be built up as required, caters for a wide variety of military applications, and sensor tubes are available to cover light levels from the brightest sunlight to the darkest night. A working demonstration of the new equipment was recently given in London before representatives of the governments, armed forces and industrial concerns from more than 25 countries.

MP's to Get New Telephones

A MASSIVE reorganisation of Whitehall's telephone network to meet the greatly increased demands of the next 20 years is being launched by the GPO and the first orders have now been placed with Plessey Telecommunications Group.

The project will be split into two stages. The first, covering about 30,000 telephone extensions, will modernise and extend existing facilities to bring them into line with the forecast requirements of the 1970's. The second, covering a further 30,000 extensions, will concentrate on the advanced facilities envisaged for the 1980's—including push-button access by phone to a central computer for all MP's.

The first stage, costing over £2 millions for telecommunications equipment alone, is due for completion in 1972/3. This will replace a large number of manually operated switchboards at present in use.

Export Success

A TARGET export growth of 70 per cent for the current year is already virtually assured by orders now in hand, report Electrosil Ltd. Electrosil confidently expect this success to continue and to cope with the demand on their export department, an assistant export manager has been appointed. The bulk of the exports are of resistors.

EORGAN

By Alan Douglas, Sen. Mem. I.E.E.E.

Last month we looked at the more theoretical aspects of the various kinds of basic subtractive filter used for tone forming. In essence, these consisted of the low pass filter which attenuated high notes, the inversion of this circuit, the high pass filter which removes the low notes, and the resonant band pass or band stop filter which accentuates some frequencies at the expense of others.

All of these filters can be extended or combined as will be seen in the practical voicing circuits presented in

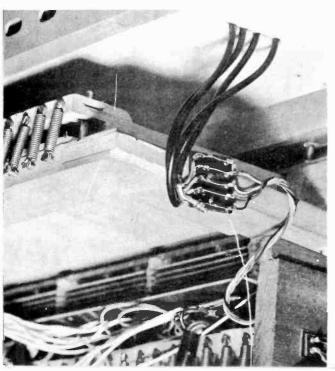
this article.

VOICE GROUPING

An organ is a blend of voices and this means that there must be no gaps in the sound spectrum when stops are combined and that the recognised groupings of such stops will produce a melodious effect.

In Fig. 6.1 is given a detailed block diagram of the voice groupings of our organ in relation to both manuals and pedalboard. When we key these we route a signal very rich in overtones from the pitch busbars, shown marked in Fig. 6.1, to the stop selecting voice networks. The tonal quality of this waveform is subsequently modified by partial removal of harmonics by the subtractive filters to produce the distinctive sound of the organ voices.

Solo tagstrip attached to edge of Goddard keyframe. Here five busbar wires connect to four screened inputs to emitter followers



EMITTER FOLLOWERS AND PRE-AMPLIFIERS

In producing a note at either of the two keyboards, the square wave output from the dividers must pass via the 100 kilohm anti-robbing resistors which are integral

to the manual contact assembly.

In combining several notes in a chord the net value might be 25 kilohms when lumping these resistors in parallel. To offset this and keep the loading substantially constant, each busbar feeds directly into an emitter follower and pre-amplifier as shown in Fig. 6.2.

The output level from TR1 can be conveniently adjusted by the slider of VR1, this being a.c. coupled to

the pre-amplifier via C2.

The frequency pass band is to some extent controlled by this capacitor and the input capacitor C1, so it is necessary to alter these capacity values with different pitch inputs. A table showing these changes is given under the circuit of Fig. 6.2.

From Fig. 6.1 it can be seen that each pitch busbar on each keyboard has its own emitter follower and preamplifier. The pedal busbars have only pre-amplifiers

to feed its filters.

The supply for these amplification units is derived from P.S.U. 1, the power supply unit which feeds the generator and divider units.

SOLO PRE-AMPLIFIER CONSTRUCTION

The four emitter followers and pre-amplifiers, fed from the solo 2ft, 4ft, 8ft and 16ft busbars, are constructed on a single piece of Veroboard as shown in Fig. 6.3.

Since the component complement is almost identical for each pitch assembly, a balanced layout is possible, and each assembly is easily identifiable in the figure, it being contained by dotted lines.

The wiring and cutouts for the Veroboard underside

are given in Fig. 6.4.

After soldering wires or cutting the copper, make sure that no solder or swarf is bridging adjacent copper strips or there may be trouble with inter-modulation faults.

BUSBAR TAGSTRIPS

In Fig. 6.3 the inputs to the emitter followers are given colour identification. These colours refer to the wires from the solo manual busbar outlets which are yellow for 4ft, red for 2ft, grey for 8ft, and blue for 16ft. There is also a black earth wire.

This bunch of five wires is shown coiled on the left hand side of Fig. 2.1. First, uncoil these, bringing them out parallel to the edge of the upper keyframe. To fix their position a five way miniature tag strip should be screwed to the rear edge of the keyframe as shown in the photograph. The busbar wires can now be bared, connected and soldered.

TONE CIRCUITS

This organ will be demonstrated at The International Audio Festival and Fair, Olympia, London, October 16 to 22

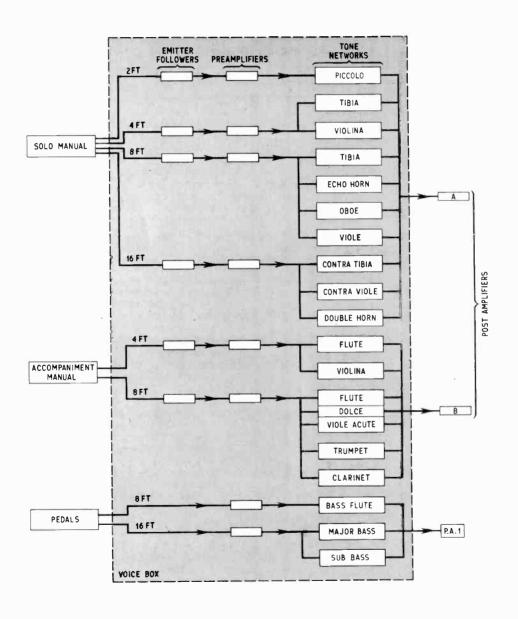


Fig. 6.1. Block diagram of the organ's manual and pedal voicing circuits. Note the inclusion of the Dolce stop which is additional to the specification given in Part One. This voice derives from the flute family but has a quieter sound achieved by additional low pass filtering

At this stage the wires from the lower manual busbars can be similarly connected. Here, of course, only three wires are involved coloured yellow, grey and black, so a three way tag strip is required.

When this is completed a link wire is made to join the

busbar black, or earth, wires at their tags.

For connection from the upper tagstrip to the emitter follower input, four, one yard lengths of single miniature microphone cable are needed. This cable is screened and to prevent hum and crosstalk arising it is necessary to connect the screens with the busbar black wires at their common tag.

The cable inners are now connected at the tags at one end and the Veroboard at the other as shown in Fig. 6.3.

SUPPLY CONNECTIONS

Since we need to tap a 15V supply to test the preamplifier board, the wiring from P.S.U.1 to the oscillator and dividers can now be completed. This is a simple task since the oscillators are in position as are the divider boards.

To mount the power unit, a wooden shelf $6\frac{1}{2}$ in \times 8 in should be made up and fixed to the console side using angle brackets. To establish the positioning of this, refer to the rear view photograph given in Part Two.

If wood quadrant is added to the edge of the shelf, this

will prevent any movement of this unit.

A $2\frac{1}{2}$ ft length of twin cable will suffice to connect from the power supply output terminal block to the oscillator shelf.

SOLO PRE-AMPLIFIERS

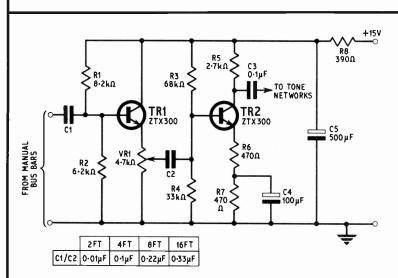


Fig. 6.2. Circuit diagram of the solo emitter followers and preamplifiers which are fed from the solo manual busbars. Changes in capacitance of CI and C2 necessary to accommodate pitch variation are shown in the table

COMPONENTS

SOLO EMITTER FOLLOWERS AND PRE-AMPLIFIERS

Resistors RΙ

R2 **6.2**kΩ 4 off R3 $68k\Omega$ 4 off $33k\Omega$ 4 off R4 $2.7k\Omega$ 4 off R6 470Ω 4 off **R7** 470Ω 4 off R8 **390**Ω 4 off All 10% ½ watt carbon

4 off

 $8.2k\Omega$

Capacitors

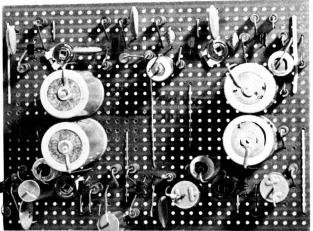
> Values according to pitch. See Fig. 6

0-1 µF disc ceramic 4 off 100μF elect 6V 4 off

500µF elect 25V 4 off

Transistors

TRI ZTX300 (Ferranti) 4 off TR2 ZTX300 (Ferranti) 4 off



Topside view of solo emitter follower and pre-amplifier board

Potentiometers

VRI $4.7k\Omega$ miniature horizontal presets 4 off

Miscellaneous

Veroboard 33in × 5in

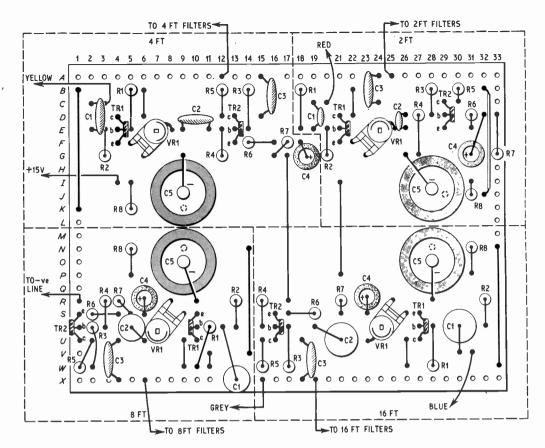


Fig. 6.3. Component layout of the four solo emitter followers and pre-amplifier circuits

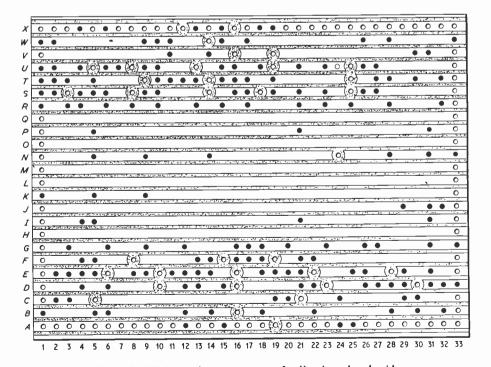
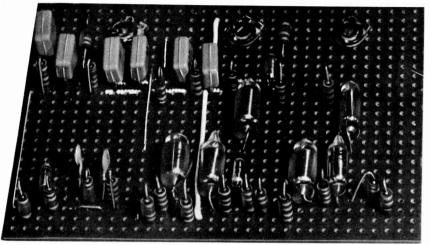


Fig. 6.4. Wiring and copper cut out for Veroboard underside



Topside view of solo filter networks mounted on board. The inductors are not shown as these are mounted in the screening box

Since all the oscillators and dividers require 15 volts they are all wired in parallel across this supply which is a simple operation provided the diagrams given in Parts Two and Three are referred to.

When this wiring is completed a 1,000µF 25V electrolytic capacitor should be connected across the supply line as an additional aid to smoothing.

TESTING THE VEROBOARD ASSEMBLY

We can now take supply leads from any one of the oscillators to the pre-amplifier board, these connections being given in Fig. 6.3.

To generate a test signal a 30,000pF capacitor should be connected across one of the oscillator coils, at the same time taking particular notice of the note sign of the divider which it feeds as a busbar signal will only be apparent when the corresponding key on the solo manual is depressed.

To complete the test circuit, join the black leads at the busbar tagstrip to the negative side of the 15V supply.

First switch on the supply, then with a pair of high impedance headphones connected between the negative supply line and the 4ft pitch output capacitor C3, depress the appropriate manual key and a clear note should be heard. If the note is fuzzed or not apparent then the cause is almost certainly a faulty transistor.

Variations in amplitude can be made by adjusting VR1.

To check the other pitch pre-amplifiers, the headphones should be connected to the other output capacitors in turn, these all being annotated C3 in Fig. 6.3.

If the same key is depressed and four sections are functioning correctly, you will immediately be aware of octave changes upwards when moving from the 4ft output to the 2ft, and downwards when moving from the 4ft to the 8ft then to the 16ft.

This board should now be disconnected and put to one side.

SOLO FILTERS

The filters for the solo or upper keyboard are given in Fig. 6.5. As can be seen, the tone nets are fed from the four pitch pre-amplifiers.

In the solo keyboard four pitches are required as more kinds of sounds are needed for melodic effects. In these circuits we have all three types of filter discussed in Part Five.

The three tibia are low pass circuits with somewhat differing characteristics, dependent on the pitch and degree of filtering.

The string stops, violes and violina, are high pass circuits and again the component values are chosen to produce a difference in character.

The oboe is a parallel tuned circuit using a Mullard Ferroxcube coil type LA2 which has no external fields.

STOP SWITCHES

The considerable resistance that precedes any one of the stop switches S1 to S10 means that there is little, if any, change in volume when adding stops and one network does not influence another so that the character of the tones is unimpaired and we get the effect of adding quite distinct sounds instead of one compound sound.

Although the inputs come from separate preamplifiers, the outputs are combined and fed into a common post amplifier. It will be noted that there is an adjustment for volume on some of the voices, this being provided by small preset potentiometers.

SOLO VOICE DETAILS

Three stops follow the 16ft pre-amplifier, these being the contra tibia, contra viole, and double horn.

One must be very careful with this pitch, because the lower notes run down to 32Hz and chords formed in the bottom octave are unusable. Even on the best pipe organ there would be very few 16ft stops per manual, often none at all. We use such stops because solo voices are excellent down to tenor C and the bottom octave is useful for special effects—one can form a good bass here.

The 16ft tibia is an essential part of the theatre chorus, therefore we keep it round in character with virtually no harmonics. It is a strict foundation tone derived from a low pass filter.

The contra viole is a string voice devoid of fundamentals which is kept low in amplitude so that it can be used in chords down to tenor C.

The double horn is a series resonant circuit, designed to give useful results over the whole keyboard. It is really a solo voice and if made too loud, would overload the post amplifier when played in chords.

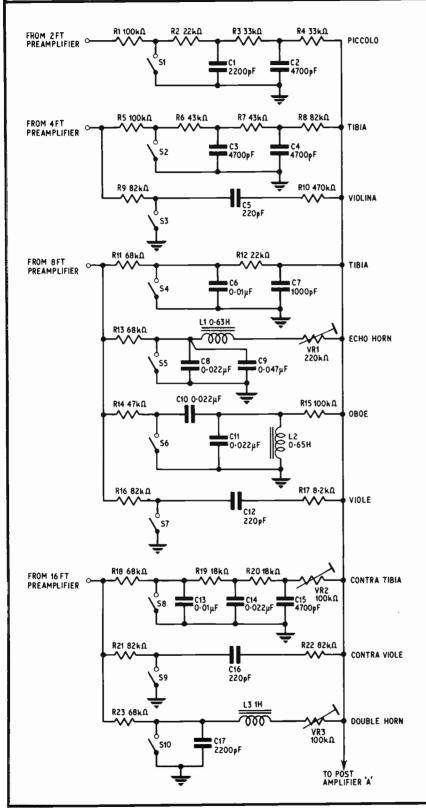
8ft STOPS

The 8ft pre-amplifier supplies a tibia tone, a string tone and two 8ft reeds.

The tibia is similar to the 16ft one, voiced to give more harmonics than a flute. Then we have the echo horn, a smooth sound of value for quiet work.

The oboe, which is quite characteristic of the pipe organ stop, is not nearly so plaintive as the orchestral

SOLO TONE NETWORKS



COMPONENTS.

SOLO TONE NETWORKS

Resistors RI $100k\Omega$ RI3 $68k\Omega$ R2 $22k\Omega$ RI4 $47k\Omega$ 100kΩ R3 $33k\Omega$ RI5 82kΩ R4 $33k\Omega$ R16 I00kΩ RI7 8-2kΩ RI8 68kΩ R6 $43k\Omega$ R7 82k Ω RI9 I8kΩ R8 82kΩ R20 I8kΩ 82kΩ R2I R9 82 $k\Omega$ RIO 470k Ω R22 82kΩ RII $68k\Omega$ R23 68kΩ RI2 $22k\Omega$

All 10% 1 watt carbon

Capa	citors		
Ċι	2,200pF	CI0	0.022µF
C2	4,700pF	CII	0-022µF
C3	4,700pF	C12	220pF
C4	4,700pF	C13	0.01µF
C5	220pF	C14	0-022μF
C6	0.0ĺµF	C15	4,700pF
C7	1,000pF	C16	220pF
C8	0.022µF	CI7	2,200pF
C9	0-047µF		-

Potentiometers $\begin{array}{ccc} \text{VR1} & 220 k \Omega \\ \text{VR2} & 100 k \Omega \\ \text{VR3} & 100 k \Omega \\ \end{array} \begin{array}{c} \text{miniature} \\ \text{horizontal} \\ \text{VR3} & 100 k \Omega \\ \end{array}$

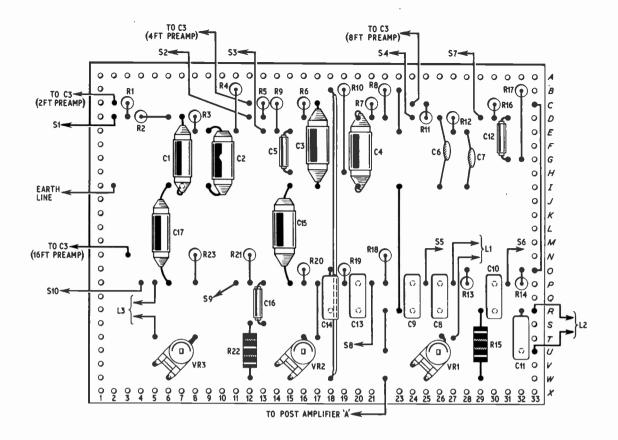
Inductors

LI 0-63H All Mullard ferrite pot cores type LA2. For winding details see text.

Miscellaneous Veroboard 3¾in × 5in

Fig. 6.5. Circuit diagram of the solo tone networks with the piccolo and tibias made up from low pass RC filters and the strings—violes and violina—made up from high pass filters. Resonant circuits are used for the other wind family members.

Note the inclusion of a preset potentiometer in series with the outputs of the more strident voices. This permits volume adjustment



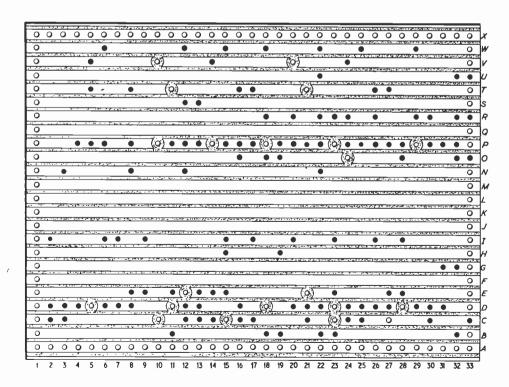


Fig. 6.6. Component layout and underside wiring of solo filter board

oboe, as a square wave will not produce a perfect oboe sound.

Finally, the viole, which is not quite so strong as its counterpart in the lower keyboard because it is meant to mix with the 16ft and 4ft strings.

4ft AND 2ft STOPS

The two voices feeding from the 4ft pre-amplifier are the tibia, an important register only slightly louder than the 8ft, but sounding very similar, and the violina which may be regarded as an extension of the 8ft viole.

We are left with the 2ft piccolo, a most useful sound for brightening everything else, and a vital component

of the tibia chorus.

There is no adjustment for this low pass filter which covers the keyboard range right up to B, 7902Hz. This is at least an octave higher than one would find in any but the largest electronic organs.

As many high harmonics are retained, an unusual brilliance is imparted to the sound and lets us dispense with the twelfth, 23ft, which is very difficult to regulate with a square wave generator, and is only of real value with sine wave systems.

The 2ft stop can be used as a solo voice on its own.

SOLO FILTER CONSTRUCTION

All of the solo filter components, with the exception of the coils, are mounted on a single Veroboard as shown in the component layout and wiring of Fig. 6.6.

Eventually, all of the voicing sub-assemblies will be contained in a metal screening box, so no inter-board wiring will be done at this stage, only board assemblies.

Since these circuits are passive, testing is not really necessary so this board can be laid aside after component mounting, first making sure that the wipers of the preset potentiometers are set at mid travel.

COIL WINDING

To calculate the number of turns to be wound on the LA2 coil former we use the formula:

$$n = 65\sqrt{L} \times 10^3$$

where n is the number of terms to produce L the coil inductance. The factor 65 is the number of turns required for 1 millihenry with this particular coil.

Using 44 s.w.g. enamelled copper wire, the approximate number of turns required for each coil are:

> L1-1,600 turns L2-1,650 turns L3-2.000 turns

When these are wound and the Ferroxcubes reassembled, these should be placed to one side as they will eventually be mounted in the voice screening box.

KIMBER-ALLEN KEYBOARDS

Upon investigation it has been discovered that the Kimber-Allen keyboard and the Harmonics contact assembly are dimensionally incompatible. The author apologises for any inconvenience to readers, but the original recommendation was based on his own personal measurement of a sample Kimber-Allen keyboard. Constructors intending to purchase keyboards and contact assemblies are now advised to purchase Goddard keyboards and Harmonics contact assemblies.

Readers who have already purchased the Kimber-Allen keyboards may be able to negotiate their return for credit. In this connection it should be noted that the Kimber-Allen stop switches (specially engraved) and pedalboard will be specified as standard items for the P.E. Organ in

forthcoming articles.

To be continued

NEWS BRIEFS

Ultrasonics Conference and Exhibition

MPORTANT advances in ultrasonics techniques for industry and medicine will be discussed in sixteen 30-minute lectures at the Sixth Ultrasonics for Industry Conference, to be held at St. Ermin's Hotel, London, on October 7 and 8.

An exhibition, run in conjunction with the conference, will display a range of ultrasonic equipment for cleaning. degreasing, flaw detection, thickness measurement, level sensing and control, medical diagnosis, welding, drilling and cutting, homogenising and depth sounding. Senior engineers will attend the stands to provide information and discuss application possibilities.

The conference is divided into four half-day sessions: Materials Evaluation; Medical and Biophysical; Electronics Applications; Non-destructive Testing.

Registration fee for the conference is £8 for the whole conference or £6 for a single day. Admission to the exhibition is free. Full details and registration forms can be obtained from the Organiser, Ultrasonics Conference and Exhibition, Dorset House, Stamford Street, London,

Miniature Battery in Moon Experiment

MINIATURE mercury battery, smaller than a thimble, is A serving as the power source for the seismic experiment package that Apollo 11 astronauts "planted" on the moon.

Designed to last two years or more, the battery controls the timing mechanism of instrumentation that gathers and

transmits scientific data from the lunar surface.

The tiny Mallory battery is similar to those used to power a heart pacemaker. It is encapsulated in a special casing as protection against severe environmental strains.

Radio Buses

WITHIN the next few months, 37 Corporation buses in Coventry will be fitted with GEC mobile radio communications systems which will provide crews with a permanent and instant radio contact with their new traffic control centre in the centre of Coventry.

This system is designed to provide the crews with a measure of protection against hooliganism and vandalism, and is particularly important on the newer types of "pay-as-you-enter" bus, where the driver is completely on

his own.

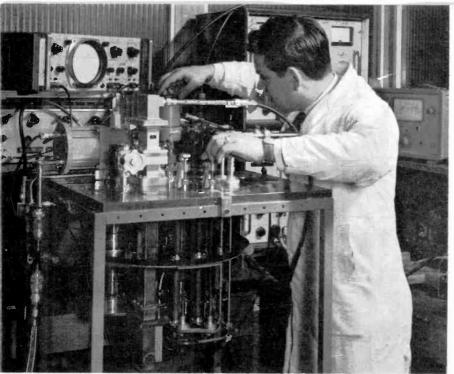
Two of these units have been in trial operation for some six months, and their success has decided the Transportation and Highways Committee to order an additional 35 systems, in addition to the 11 GEC Courier v.h.f. pocket transceivers which are already being used by inspectors patrolling the routes, and also by the management. Two of the mobile systems are now installed in vehicles used by traffic inspectors.

New Structure for GEC-Marconi Electronics

A NEW management structure was announced recently for the GEC-Marconi Electronics group, with the formamation of the following four new management companies responsible to Mr R. Telford, Managing Director of The Marconi Company Ltd.

Marconi Communication Systems Ltd. Marconi Radar Systems Ltd.

Marconi-Elliott Avionic Systems Ltd. GEC-Elliott Space and Weapons Systems Ltd.



Goonhilly 1. Refurbished

THE Goonhilly 1 installation recently reopened, after being re-equipped, receives and transmits signals via satellite to the Americas. One of the main improvements resulting from this updating is the conversion from narrow band to wide band operation, thus making possible the simultaneous reception and transmission of television programmes and hundreds of telephone channels. Goonhilly 1 was used to receive Apollo 11 television pictures bounced off satellites above the Indian and Pacific oceans.

Parametric amplifiers, supplied by Mullard Ltd., boost the very weak television and telephone signals received via satellite from Japan and Australia at Goonhilly Down.

Two Mullard parametric amplifiers have been installed at Goonhilly: one for operational use; the other on standby. Designed and built by scientists at the Mullard Research Laboratories and the Mullard Mitcham plant, they operate over a bandwidth of 3·7-4·2GHz. One of the amplifiers is shown (left) being checked before installation.

ELECTRONORAMA

Optical Mark Reading System

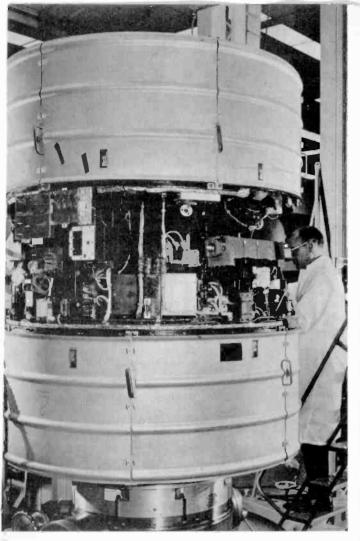
In many modern organisations there is a need to collate and analyse a large amount of statistical data. Prior to the introduction of the computer, however, such data was prepared in a conventional words and-figures form, which cannot be "read" by computers. It has therefore now become necessary to convert the conventional data into a coded form which is acceptable as a direct input to an automatic data-processing system.

One technique, which has been applied manually for many years, is to use a "grid" system. In this, a grid of columns and lines is printed on a document, and the location of each box in the grid thus formed is assigned a particular value or represents a unique item of information. It is then a simple matter to make a mark in the predetermined positions on the grid.

Data Recognition have now automated this principle and have produced a versatile reading machine. This has been designed to read marks entered on documents, and provide a punched paper tape version of the document.

The DR 500 will read a wide range of sizes and thicknesses of documents.





ATS-E shown during final tests (left and below) at Hughes Aircraft Company, El Segundo, California, where the spacecraft were built for MASA. The rectangle with a dozen small circles at upper right section of the spacecraft (below) is the antenna portion of an L-Band communications system.

Another Satellite

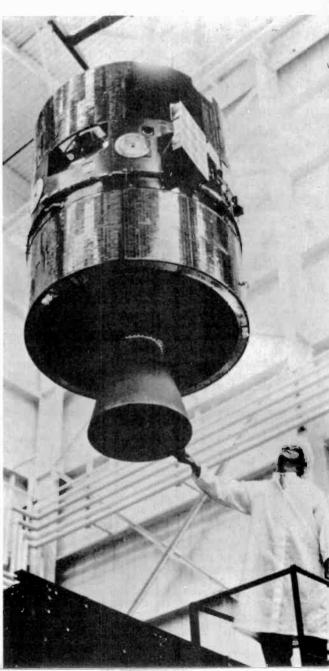
THE fifth Applications Technology Satellite built for NASA by Hughes Aircraft Company of California which was launched from Cape Kennedy on August 12, carried 13 experiments into space—more than any of its predecessors.

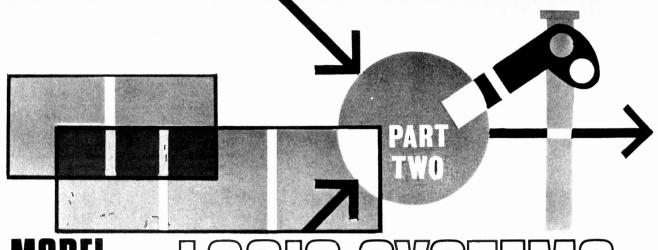
The ATS-E, renamed ATS-5 after launch, joins ATS-1 and ATS-3 in synchronous orbit 22,300 miles above the earth. It is 5ft in diameter, 11ft from the bottom of the apogee motor to the tip of the omni-directional antenna and weighs 1,901lb at separation from the booster.

The satellite extends arm-like booms into a giant X nearly the length of a football field, in a "gravity gradient" experiment designed to use the earth's gravity to stabilise the spacecraft in orbit.

The satellite carries an L-band repeater, recently developed by Hughes, that may pave the way for development of an improved system of using satellites for aircraft communications and navigation

The objectives of the experiment are: to determine the reliability of an L-band system for aircraft-toground voice communications; to study its use in voice communications between aircraft, and to study its accuracy in locating the positions of many aircraft and tracking their progress.





MODEL LOGIG SYSTEMS By P. GOODES

N this second article of the present series, logic circuits are employed to make up interlocking signalling systems.

SIGNALLING SYSTEMS

The purpose of an interlocking signalling system on a model railway is to enable two or more trains to be run on the same track without the possibility of an accident.

Three circuits have been designed and constructed by the author, the first being very basic and the other two somewhat more complex. Although it is quite possible to have the whole of the layout on an interlock system, this type of signalling was used in one main line with suburban line loop only.

SIMPLE TRACK SIGNALS

Referring to Fig. 2.1 it will be seen that the track is split up into isolated sections. The longer sections are all joined electrically to the controller of the train and the smaller sections are connected via relay contacts to the controller.

Consider now the mode of operation. A train may not enter a section unless that section is clear of all other trains. When a train enters a section it must inform the previous section that it has done so. At no time must there be two trains in one section.

Two-coloured light signals are used and these are controlled as shown in Fig. 2.2 by bistables feeding relay buffers. (These circuits were described in Part 1.)

Assume a train is going past signal X2 which is at green. It then trips switch S2, which feeds a 1 pulse into bistables BS2A and BS3B. BS2B now has a 1 output which operates relay RLB, changing X2 signal to red and cutting off the supply to the short section immediately before signal X2. The operation of bistable BS3 causes RLC to drop out, changing X3 to green and applying engine power to the short section in front of X3. Thus another train may progress beyond X3 and will stop at X2, until X2 is cleared from red to green by the previous train tripping switch S1.

This process is repeated at each signal giving a complete loop, which may be quite simply expanded according to size of railway layout, the number of trains to be run on the one track, and introduction of points hazards.

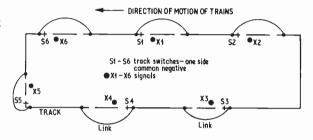


Fig. 2.1. Track layout for simple signalling

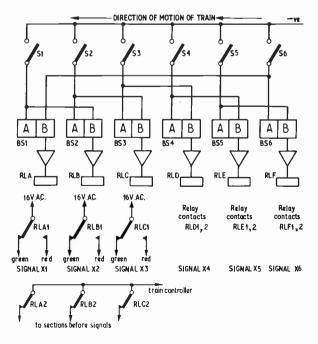
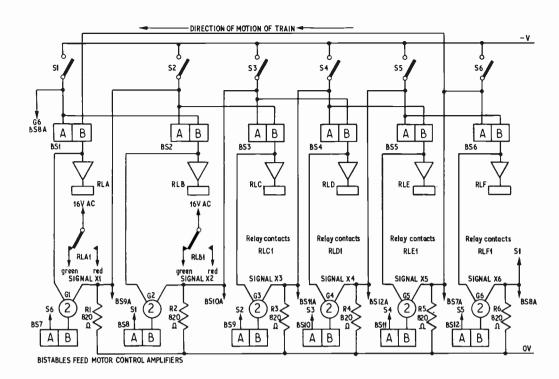


Fig. 2.2. Block diagram of the signalling logic system



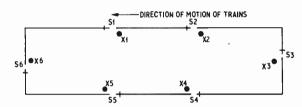
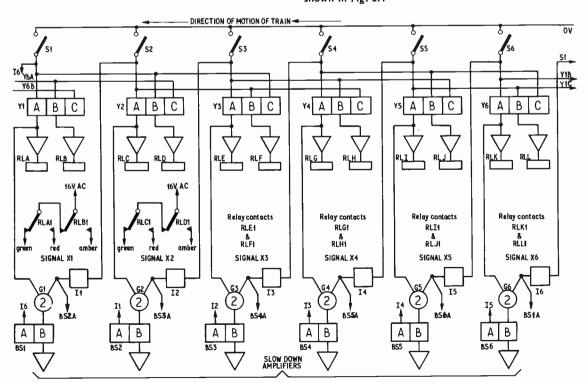


Fig. 2.3 (above). Stop and start control is achieved by using AND gates. When feeding a bistable from an AND gate, replace the bistable input resistor by a diode, input to cathode

Fig. 2.4 (left). Track layout for circuit shown in Fig. 2.3. Signals are indicated by X numbers

Fig. 2.5 (below). Logic diagram for home and distant signals with slow down amplifiers using the track layout shown in Fig. 2.4



STOP AND START CONTROL

Another more superior system is shown in Fig. 2.3. The splitting up of the track loop into sections is slightly different as will be seen in Fig. 2.4. All the short isolated sections have been disposed of and each long one now has its own engine control amplifier.

It is possible to have one control amplifier per train, but a very complicated switching network would result. To ensure individual control, a control amplifier was required for each section. This would enable the system to be expanded quite simply for use with three or four trains.

The operation of the signal bistables is as explained in the previous section but, using an engine control amplifier, a more realistic stopping and starting of the train with gradual acceleration and deceleration is effected.

Assume signal X1 is at red and a train is approaching passing signal X2. As S2 switch is tripped, signal X2 changes to red. Gate G1 is primed by the condition that signal X1 is red, i.e. a 1 on BS1B output. Thus as S2 is tripped, this gate gives a 1 pulse output which triggers bistable BS7 and causes the control amplifier for that section to slow the train down and bring it to a halt.

This train will then remain stationary until signal XI changes to green. This occurs when the previous

going train passes signal X6 and trips S6.

The pulse from switch S6 also resets the bistable BS7 and allows the train to start off. As it strips S1 switch, it sets X1 signal to red and, if X6 signal is at red also, it starts slowing the train down again via BS12 bistable. If however gate G6 is unprimed (i.e. signal X6 is green) no output pulse occurs and the train continues without slowing.

All bistables on signalling should have their input resistors replaced by diodes—input to cathode, anode to base of transistor. Although the circuit does work using the input resistor, analysis shows that under adverse conditions, misfiring may occur.

HOME AND DISTANT SIGNALS

The most realistic signalling system is the home and distant where three-colour lights are used. These

signals are obtainable commercially although an avid modeller will have no difficulty in constructing his own. Again the loop or track length is divided up into sections (Fig. 2.4) and, considering any one signal, the following colour codes are used.

RED: The section immediately after the signal is occupied by a train. Any further train coming will

stop at the signal.

AMBER: The section immediately after the signal is unoccupied but the next section along is occupied by a train. Trains may pass an amber signal.

GREEN: There are two or more clear sections after the signal and a train is allowed through.

Thus the signal colour sequence is red-amber-green, when considering a single train going round the track. In Fig. 2.5 on the shift register, A represents red,

B represents amber, C represents green.

Suppose a train has just passed X2 signal. When S2 switch is tripped, Y2A gives a 1 output operating relay RLC through its buffer, applying red to X2. S2 also sets Y3B which changes X3 to amber, and also Y4C which sets signal SX4 to green. If signal X1 is red when S2 is tripped, then gate G1 gives a 1 output into BS1 bistable. This bistable feeds its control amplifier and causes the train to slow down before the signal X1. When this signal has been cleared by a previous going train the engine speeds up and on tripping, switch S1 changes X1 to red, X2 to amber and X3 to green.

Once again this is a loop system and may be extended quite easily to cater for more signals. The engine control section is exactly the same as that used in the previous system, but in this case the common side of the trip switches S1 to S6 is connected to 0V. Thus, when a switch operates it cuts off the associated

transistor in the shift register.

Next month: An automatic marshalling yard

APOLOGY

We regret that the title of the first part of this article last month was omitted due to a printing error.

DOUBLE DATE

PRACTICAL ELECTRONICS will participate in two London exhibitions during October

R.S.G.B. STAND 14

AUDIO FAIR STAND 73

INTERNATIONAL ENGINEERING AND RADIO COMMUNICATIONS EXHIBITION Royal Horticultural Hall, London, S.W.1., Wednesday, October 1 to Saturday, October 4.

The Wideband Communications Receiver, and a 100W Public Address Amplifier can be seen on Stand 14

INTERNATIONAL AUDIO FESTIVAL AND FAIR National Hall, Olympia, London, S.W.5., Thursday, October 16 to Wednesday, October 22.

The P.E. Organ and a novel integrated circuit hi fi system will be demonstrated on our Stand 73

We hope many of our readers will be able to visit us on one (or both!) occasions Our exhibits will represent examples of modern techniques applied in two different fields



ECTRONIC BROKERS

TEST EQUIPMENT



HIGH VALUE RESISTANCE **BOX TYPE R.7003**

Specification. Range: 0-01-111 Megohm in 0-01 Megohm divisions. Accuracy: 0-05%. Maximum power rating: 0-1W yer step. Case: Hammer finished stove 0.01-111

List price £60. Our price £22,10, P. & P. £1

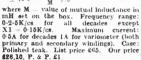
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MUTUAL INDUCTANCE BOX TYPE R.7005

Specification. Range: 0-11-110mH in 0-002mH Accuracy: 0.012





PORTABLE WHEATSTONE

Specification. Type: Moving Coil Gal-vanometer. Ranges: 1, 0-05 to 5 ohms. 2, 0-5 to 50 ohms. 3, 5 to 500 ohms. 4, 50 to 5,000 ohms. 5, 500 to 50,000 ohms. Scales: Mwitched: Slidewire: 0 ohms. Scales: Mwitched: Slidewire: 0 Case: Moulied plastic. Internal Source: 6.9 to 90.

Case: Mouliled plastic. Internal Source: 4V. Dry battery. Operating Temperature: +10 to +55 deg. C. Operating Humidity: up to 80% R.H. Dimensions: 200 × 110 × 65mm. Weight: 0-948g.

List price £25. Our price £9,19.6. P. 10/-

MUTUAL INDUCTANCE COLL

TYPE R.7006

Greeification. Value: 0-001H. Accuracy: 5Kc/8. Operating Frequency: 5Kc/s
Maximum current: 1A, 3A
of coils 4 ohin, 1 ohin Resistance of coils 4 ohin, 1 ohi Case: Moulded plastic. List price 8 gns. Our price 50/-. P. 7/6



PORTABLE MULTIRANGE

METER

Specification. Ranges: 0-60 and 0-300uA.

D.C. 0-3, 0-30 and 0-12mA, D.C. 1-2 and

12 amps D.C. 0-8-3 and 6-30mA, A.C.

24-120mA, A.C. 0-24-12A, A.C. 3-12-30
300-600-1,200 and 6,000V, D.C. 0-6-3,

24-12. 6-30, 60-300, 120-600, 240-1,200

and 1,200-6,000V A.C. 3-333 ohms,

03-30 Kohms, 0-03-3 megohms D.C.

Resistance —12 to + 78 Decibels. Frequency: 50eps. Input Resistance D.C.:

20,000 ohms/voit. Input Resistance D.C.:

20,000 ohms/voit. Input Resistance A.C.:

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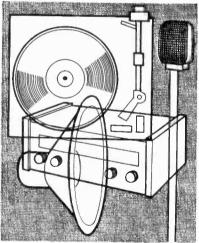
Stereo amplifier with tone controls.

High Fidelity Stereo amplifier for twin three channel speaker systems.

The first designs will appear next month. All three projects have been specially designed for Practical Electronics readers, and are based on the Plessey SL402 and SL403 integrated circuits described in this current issue.

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PRACTICAL SELECTRONICS

NOVEMBER ISSUE ON SALE THURSDAY OCTOBER 16

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MOTORISTS often have to leave their cars in daylight and return to them after dark. If they park in an area where lights are required they must switch on a parking light when leaving the car. The light then stays on right through the hours of daylight, resulting in battery drain; especially undesirable in wintry conditions. The remedy is a parking light that will remain off in daylight and switch itself on automatically at dusk.

CIRCUIT DESCRIPTION

Light falling on the light dependent resistor (X1) reduces its resistance and switches on TR1 (Fig. 1). Practically all the voltage drop is then across the 680 ohm resistor (R2). The base of TR2 is thus well positive and TR2 is cut off. In very bright sunlight the resistance of the l.d.r. (X1) may fall to a very low value, thus R1 is inserted in series with the cell to limit the current.

When darkness falls the resistance of the cell increases and TR1 switches off, most of the voltage drop is then across TR1 and TR2 base becomes negative causing TR2 and LP1 to switch on.

The diode protects the circuit against damage from accidental reversal of supply polarity. This circuit can be used with positive or negative earth cars.

CONSTRUCTIONAL DETAILS

Drill a lin hole in the underside of the parking light and attach the photo cell using epoxy resin (see photograph). Leave the leads to the cell about lin long. The rest of the circuit is assembled as a five terminal encapsulated module on the back of a power transistor (TR2). The power transistor has two holes in its case (collector), drill a third hole in the case large enough for two leads to pass through (see Fig. 2).

Start the assembly by soldering R2 and the collector terminal of TR1 (the terminal with the spot) to the base pin of TR2. To the other end of R2 solder the negative end of D1 and a short lead and pass this lead through the new hole in TR2. The positive lead



The completed photo electric parking light; position of XI can be clearly seen

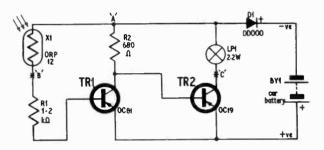
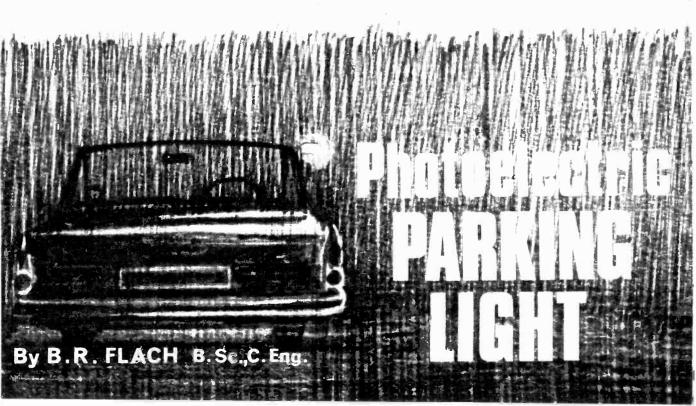


Fig. I. The complete circuit diagram of the photo electric parking light



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COMPONENTS . . .

Resistors

RI $1.2k\Omega$ R2 680 Ω $\pm 10\%$, $\frac{1}{4}W$ carbon

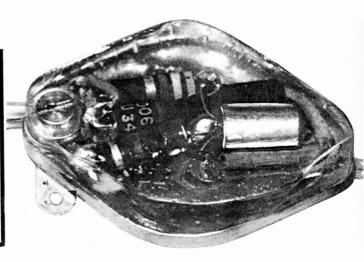
Semiconductors

TRI OC81 TR2 OC19

D1 DD000 silicon rectifier

Miscellaneous

XI ORP12 light dependent resistor Parking light (large enough to hold unit) 4B.A. screw and solder tag Insulated wire Epoxy resin (Araldite, Bondaglass or Cataloy)



Photograph of the completed electronic assembly encapsulated in epoxy resin

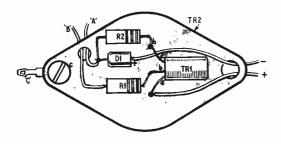


Fig. 2. Layout and wiring of all components except LPI and $\boldsymbol{X}\boldsymbol{I}$



from D1 is sleeved, soldered to the negative battery supply and passed through the original hole in the power transistor. The positive supply lead is passed through the same hole and soldered to the emitter terminal of TR2 together with the emitter of TR1. Next connect R1 to the base of TR1 and the other end of R1 to a thin lead (connection "B") and pass it out through the new hole. Bolt a tag (connection "C") to the collector of TR2 by means of a 4B.A. screw.

With this assembly all the circuit components are on one side of TR2 and the five connections are on the other side; the rim of TR2 is free from any obstructions. Test the circuit at this stage and see that there are no shorts.

Stop up the holes in TR2 case with plasticine or candle wax, and put insulating tape all around the rim of TR2 forming a vessel containing the components. Place the assembly on a level surface, mix some epoxy resin with its hardener and pour it into the vessel to cover the components. On the following day remove the tape and finish the module by painting the other side of the transistor with epoxy resin to provide complete insulation.

The module can then be carefully inserted into the parking light and attached with epoxy resin. There is no need to modify the wiring of the light as only the two supply leads leave it, the other three leads are connected to the cell and lamp—connection "A" to the cell and lamp—connection "B" to the cell only—connection "C" to the lamp only.

OPERATION

The switching of this unit is entirely electronic and, with the components chosen, quite fast. The author has made several units and all switch on at the correct ambient light. However, the light may be made to switch on earlier by partially obstructing the photo cell.

The current drawn by the unit is about 10mA in its quiescent state and 200mA when the light is on. The circuit is suitable for 12V or 6V operation although with a 6V supply R2 could be reduced to 470 ohm.

The external appearance of the light does not betray its electronic contents and it is therefore no more liable to pilfering than an ordinary parking light.

COLD CATHODE **TUBES**

By J.B.Dance M.Sc.



DECADE COUNTING TUBES

OLD cathode decade counting tubes (also known as "stepping tubes") were first produced about 1950 mainly for counting the electrical pulses from nucleonic detecting devices. They have since been used for many other medium speed counting applications and have also been used for other purposes not directly involving counting.

Most decade tubes can count up to a few kilohertz, some up to approximately 20kHz, whilst two highspeed tubes have been developed for counting up to 1MHz. The first important tube of this type was developed by Ericsson Telephones and was marketed under their trade name "Dekatron"

A cold cathode decade counting tube usually consists of a ring of electrodes (normally cathodes) surrounding a single electrode (usually the common anode). These electrodes are all situated in the domed end of the tube so that they can easily be seen.

VISIBLE GLOW INDICATION

When a suitable h.t. potential is applied to the tube via a current limiting resistor, a visible glow will be formed in the gas between one cathode and the nearest point on the anode to that particular cathode. If appropriately shaped pulses (which are the units to be

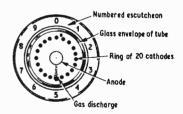


Fig. 5.1. End view of an asymmetrical tube indicating digit 5. A ring of 20 cathodes is used

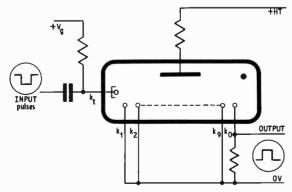


Fig. 5.2. Typical circuitry used to operate an asymmetrical tube

counted) are applied to the tube in a suitable way, the glow can be made to rotate around the ring of cathodes in the dome of the tube in a series of ten steps per revolution. Each step represents a single count.

The dome of each tube is mounted in an escutcheon which is numbered as in Fig. 5.1. The number of counts is indicated by the figure on the escutcheon which is nearest the glow in the gas.

A single decade tube can indicate any number of counts up to nine. However, at the tenth count (when the glow returns to the zero position), an output pulse can be obtained from the zero cathode and, after amplification, this pulse can be used to feed another decade tube which indicates the number of tens counted. Output pulses from the zero cathode of this latter tube may be fed to a third tube which indicates the number of hundreds and so on.

ASYMMETRICAL TUBES

One type of tube (shown in Fig. 5.1) employs 20 cathodes surrounding a common anode. Ten of these cathodes are placed opposite numbers on the escutcheon and are known as main cathodes.

The other ten cathodes are placed in between the main cathodes and are known as auxiliary, guide or transfer cathodes. These transfer cathodes receive a positive bias; the glow does not therefore remain at a transfer cathode for more than a very short time, since the anode to main cathode potential is greater than the anode to transfer cathode potential.

In tubes which employ 20 cathodes in the ring, all of the transfer cathodes are connected together. The basic circuit in which they would be used is shown in Fig. 5.2; the circular structure of the tube is usually represented as shown for convenience.

A suitable bias potential V_g is applied to the common connection for all of the transfer cathodes kt by the method shown. The square bracket on kt indicates that there is more than one transfer cathode in each tube, although only one is shown for simplicity. The main cathodes are numbered k_0 to k_0 .

OPERATION

When h.t. is first applied, the anode voltage will rise until it reaches the striking voltage of the anode to main cathode gap. A discharge will then be initiated to one of the main cathodes and the anode potential will fall to the maintaining voltage of the tube, the remainder of the applied potential appearing across the anode resistor.

The anode voltage is now inadequate to cause any other gap to strike. Once conduction has been initiated in any gap, no other main gap will strike.

If a suitable negative going input pulse is now applied to all of the transfer cathodes via the capacitor shown in Fig. 5.2, their potential can be made to fall below that of the main cathodes for a short time.

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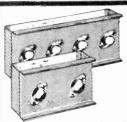
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At the end of the input pulse, the transfer cathodes return to their quiescent bias potential (positive) and the glow now tends to move to a main cathode, since the main cathode to anode potential is now greater than

the transfer cathode to anode potential.

The only main cathode which is sufficiently primed by the ions is the one following the glowing transfer cathode and the discharge accordingly moves to this main cathode. A single count is thus registered.

Tubes which employ this principle are known as asymmetrical tubes, since they are not symmetrical in the two possible directions of rotation. The direction of rotation of the glow is determined by the shape of the cathodes used.

DEKATRONS

The Ericsson "Dekatrons" and similar double pulse tubes are symmetrical tubes, the direction of rotation of the glow being determined by the order in which two successive pulses are applied to groups of transfer cathodes. Tubes of this type have a structure rather similar to that of the tube illustrated in Fig. 5.1, but there are two transfer cathodes in between each main cathode. Thus there are 30 cathodes in the ring surrounding the anode.

In this type of tube all of the transfer cathodes on the clockwise side of the adjacent main cathode are connected together and are known as the first guides. Similarly all of the transfer cathodes on the counterclockwise side of the adjacent main cathode are joined together and are known as the second guides. A positive bias is applied to both sets of guides, the basic

circuit being shown in Fig. 5.3.

When the discharge is resting at a main cathode and a negative going pulse of a suitable amplitude is applied to all of the first guides, the glow will move to the first guide which is one place in a clockwise direction from

guide which is one place in a clockwise direction from the previously glowing main cathode. There is no tendency for the glow to move to any other transfer cathode, since only the transfer cathode adjacent to the previously glowing main cathode has been appreciably

primed by the ions from the discharge.

The glow remains at the first guide during the time this guide is receiving a negative going pulse but, before this pulse terminates, a second similar negative pulse is applied to the second guides. At the end of the first guide pulse, the discharge therefore moves to the second guide succeeding the previously glowing first guide. No other second guide is sufficiently primed for the discharge to move to it.

At the end of the second guide pulse, the discharge moves to the succeeding main cathode. Thus each time a count is registered, the glow moves in three successive steps. As in the case of asymmetrical tubes, an output pulse can be obtained from the zero cathode for the operation of a succeeding tube if a resistor of a suitable value is included in the cathode circuit as shown in Fig. 5.3.

In actual practice only a single input pulse is available for the operation of a double pulse tube. This input pulse is normally applied directly to the first guides, the pulse for the second guides being obtained by means of

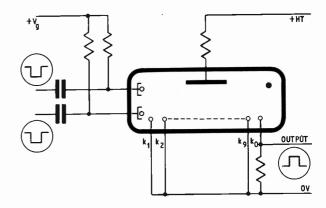


Fig. 5.3. Double pulse tube with two sets of guide cathodes

a resistor capacitor integrating circuit which effectively delays the pulse. Although the integrating circuit also alters the shape of the pulse, this is not usually too important unless it is vital to obtain the maximum possible operating speed. Practical circuits employing the integration method will be discussed later in this article.

PRACTICAL CIRCUITS

A simple circuit for the S.T.C. G10/241E "Nomotron" asymmetrical tube is shown in Fig. 5.4. This tube contains a shield electrode to promote rapid deionisation; this electrode is shown on the right-hand side of the circuit symbol. The circuit is suitable for use up to 5kHz, but another circuit has been recommended for use at counting speeds up to 20kHz.

The input pulses required are negative going pulses of about 120 volts in amplitude, rectangular in shape, and of about 16 microseconds in duration. (Suitable circuits for the generation of these input pulses have been published by the manufacturers of the counting tube.) For simplicity, only two of the cathode circuits are shown in Fig. 5.4, but the other cathodes are connected in the same way as those shown.

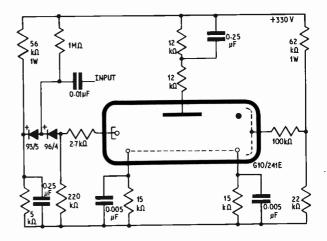
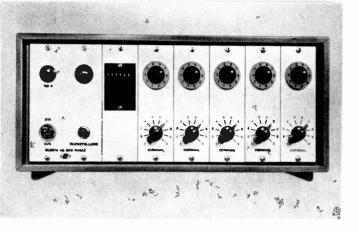


Fig. 5.4. Low speed counting circuit for the S.T.C. "Nomotron" tube



Elesta EZIOB with electromagnetic counter in this scaler

FAST COUNTING

A circuit published by the Elesta Company of Switzerland for their high speed EZ10B tube is shown in Fig. 5.5. This tube can count at speeds up to at least 1MHz, but the circuit shown is designed for frequencies of up to 100kHz. The tube is an asymmetrical type, the indication being given as a blue glow instead of the red glow emitted by most decade tubes. The gas filling controls the colour of the glow; in the case of the EZ10B it is hydrogen.

The input circuit consists of a transistor blocking oscillator, all of the coils L1, L2 and L3 being wound on a common Philips pot core type S14/8. The coil L1 consists of 400 turns of 46 s.w.g. enamelled copper wire, L2 of 60 turns of 42 s.w.g. enamelled wire, and L3 of 15

turns of 42 s.w.g. enamelled wire.

The input pulses used to trigger this blocking oscillator circuit should have an amplitude of about 10 volts and a duration of at least 3μ s; they should be fairly rectangular, the rise time being less than 1μ s. The blocking oscillator converts the input pulses into pulses of an amplitude great enough to operate the EZ10B tube. Diodes are used to protect the transistor against transient peak voltages and to prevent excessive free oscillations at the end of each input pulse.

DOUBLE PULSE TUBE CIRCUITS

A circuit designed by Ericsson Telephones for the operation of their 4kHz double pulse tubes is shown in Fig. 5.6a. The output pulses from this circuit may be fed into the circuit shown in Fig. 5.6b, which contains another decade tube for counting the number of tens. Any number of circuits of the type shown in Fig. 5.6b may be cascaded so that the whole circuit will count up to any desired number.

The circuit of Fig. 5.6a requires a positive pulse of not less than 20V in amplitude to drive it. This pulse causes the monostable circuit of V1a and b to switch, V1a conducting instead of V1b. A negative pulse is taken from the anode of V1a. The duration of this pulse is determined by the component values used and is independent of the input pulse duration. It is passed through the cathode follower stage V2a, from which it emerges as a negative going pulse suitable for driving the decade counting tube V3.

The pulse from V2a cathode is passed through a coupling capacitor C3 to the first guides in V3. It is also passed through R16 to the second guides; R16 and C4 serve as an integrating circuit to delay the pulse at the second guides. Diode D3 in the guide circuit prevents the guide potential from becoming too positive when the current passed by the tube flows to the guides.

The reset line is connected to earth through a resistor which is normally shorted by a switch. When the switch is opened the potential of the reset line should increase by about 100 volts so that the discharge in all tubes connected in the circuit jumps to the zero cathode.

The grid of V2b in Fig. 5.6b is normally biased to cut off because the output cathode k_0 of V3 in Fig. 5.6a is returned to the -20V line. When the discharge rests at this cathode, V2b conducts and the negative pulse thus produced at its anode is used to drive the second decade tube V4. A valve or transistor is required in each coupling circuit to amplify the output pulse from the previous tube and to invert its phase.

REVERSIBILITY

Circuits have been designed for double pulse tubes which can count in either direction. In order to make a symmetrical tube count in reverse, it is only necessary to apply the second guide pulse slightly before the first

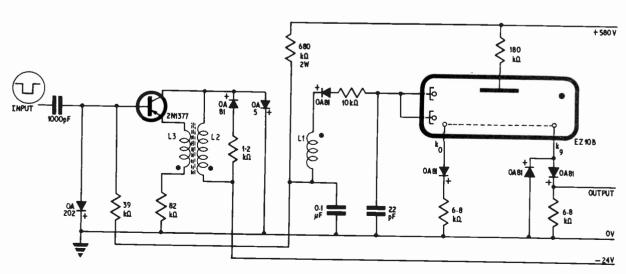


Fig. 5.5. High speed counting circuit for the Elesta EZIOB

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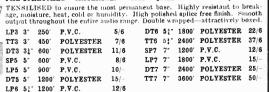
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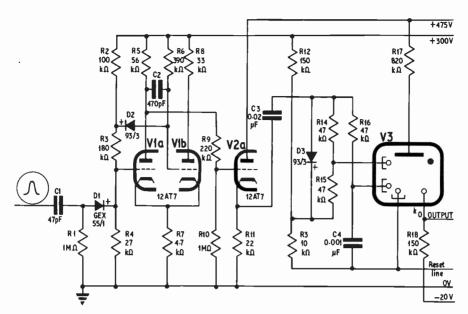
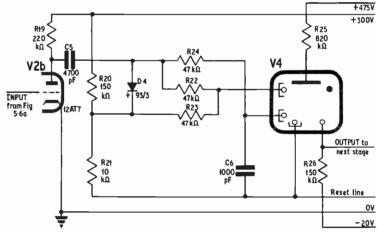


Fig. 5.6a. Input circuit for a double pulse tube



Elesta EZIOB fast asymmetrical tube

Fig. 5.6b. Double pulse tube coupling circuit for (a) above

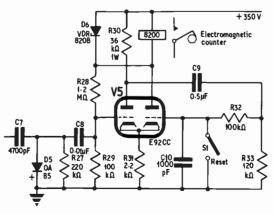


Fig. 5.6c. Coupling a decade tube to an electromagnetic counter



Cerberus GZII double pulse tube

guide pulse. A consideration of the principles of operation of these tubes should enable one to understand why they can count in reverse.

The Elesta Company manufacture a 1MHz reversible counting tube operating on somewhat different principles to the other tubes so far described.

FAST DOUBLE PULSE TUBES

Many common double pulse tubes can count at frequencies of up to about 4kHz. Some tubes (such as the Ericsson GS10D) can operate at frequencies up to 10kHz, whilst the Mullard Z505S can operate up to 50kHz. Such tubes operate at a rather greater anode current than the 4kHz tubes and require pulses of smaller duration.

The type of circuit shown in Fig. 5.6 will usually be able to drive such tubes, but the pulse length should be shortened by reducing the value of C2 in Fig. 5.6a to about 82pF. In addition the values of R17 with R12 and R13 will probably need alteration.

The Sylvania and Raytheon Companies of the U.S.A. manufacture tubes which can count at frequencies up to about 100kHz; these tubes employ the double pulse principle, but the conditions of operation are rather critical at such high pulse frequencies.

DRIVING AN ELECTRO-MAGNETIC COUNTER

A decade tube can operate at a much greater speed than an electromagnetic counter, but can indicate only one digit whereas electromagnetic counters can each indicate four to eight digits, depending on the type.

In economical equipment, it is common practice to employ one or more decade tubes to reduce the counting rate by a large factor and then to use the resulting output pulses to operate an electromagnetic counter. This enables a simple circuit to be made which will register many digits.

The output of the circuit in Fig. 5.6b may be fed directly into the electromagnetic register circuit shown in Fig. 5.6c, provided the output cathode of V4 is returned to earth instead of to the -20V supply. Each time the glow reaches the output cathode of V4, the monostable circuit (Fig. 5.6c) is switched, and the counter in the anode circuit of the one section of the double triode registers a count.

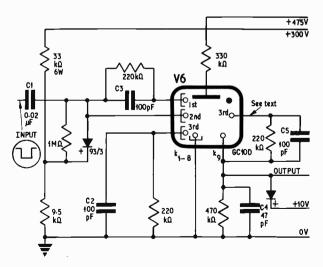


Fig. 5.7. Typical circuit employing a high frequency double pulse tube GCI0D

This circuit has been designed by the Sodeco Company of Switzerland for their magnetic counters. The counter employed should have a coil resistance of about 8.2 kilohms. The reset switch should be closed when the decade tubes are reset or the magnetic counter will probably record a spurious pulse when the glow returns to the zero cathode of the final decade tube.

SINGLE PULSE DEKATRON

The Ericsson single pulse "Dekatron" is a unique decade tube which contains 40 cathodes in a ring around the central anode. The basic circuit in which this tube is used is shown in Fig. 5.7. The three groups of electrodes shown on the left-hand side of the tube symbol are the first, second and third sets of guide electrodes. The third guide immediately preceding the output cathode k_0 is brought out to a separate base connection and is shown on the right-hand side of the circuit symbol.

The single pulse "Dekatron", as its name implies, requires only a single pulse to cause it to count. It also has the advantage that it is a fairly fast tube, its upper frequency limit being quoted as 20kHz. It contains hydrogen and emits a blue glow in operation.

When a negative going pulse is applied to the first guide (uppermost in the symbol in Fig. 5.7) and also to the second guide, the glow will initially move to the first guide, since this is strongly primed with ions from the previously conducting main cathode. However, as the current flows to this guide, C3 charges and a potential is built up across it. This results in the discharge being transferred to the second guide.

At the end of the pulse both the first and second guides return to their quiescent bias potential and therefore the discharge moves to the third guide; this is the only guide which is at earth potential and which is strongly primed. However, C2 in the third guide circuit becomes quickly charged to such a potential that the discharge moves one further step to the succeeding main cathode.

The single pulse "Dekatron" requires four separate steps to take place before a count can be registered. However, as these steps take place automatically without an additional pulse being necessary, the single pulse tube can count more quickly than some of the double pulse decade tubes.

ANODE CIRCUIT CAPACITANCE

It is very important to minimise anode circuit capacitance in all types of decade tube circuit, but it is absolutely vital when high speed tubes are being used. Excessive stray anode capacitance will reduce the rate of rise of the tube anode potential at the end of the input pulse and may result in the glow being extinguished. In this case the discharge may be reformed at any point in the tube.

It is a wise precaution, especially when high speed tubes are being employed, to solder the anode resistor directly to the anode tag of the tube base.

APPLICATIONS

Typical examples of the use of decade tubes are in digital voltmeters, synchronous timers for resistance welding, time markers, batching counters, displaying transitor characteristic curves on a cathode ray tube, routing telephone calls, in pulse generators at fairly low frequencies, and so on.

Next month: The concluding article looks at cold cathode indicator and display tubes



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The new Duo general-purpose 2-way speaker system is beautifully finished in polished teak veneer, with matching vynair grille. It is ideal for wall or shelf mounting either upright or

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Type 1 SPECIFICATION:-

Impedance 10 ohms. It incorporates Goodmans high flux 6" ×4" speaker and 2½" tweeter. Teak linish 12" -6½" ×52", 4 guineas each. 7/6d, p. & p. Type 2 as type 1. Size 17½" ×102"×6½". Incorporating Elac 10½"×6½" 10.000 lines and 2½ tweeter. 3 ohms impedance 5½ guineas plus

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Duello Integrated Transistor Stereo Amplifier

9GNS. plus 7/6d. p. & p

The Duetto is a good quality amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

SPECIFICATION

R.M.S. power output: 3 watts per channel into 10 ohms speakers. INPUT SENSITIVITY: Suitable for medium or high output crystal cartridges and tuners. Cross-talk better than 30dB at 1Kc/s.

CONTROLS: 4- position selector switch (2 pos. mono and 2 pos. stereo)

dual ganged volume control.

TONE CONTROL: Treble lift and cut. Separate on off switch. A preset balance control





The Classic

Teak finished case

81 GNS.

Plus P. & P. 7/6

SPECIFICATION:

Sensitivities for 10 watt output

at 1KHz into 3 ohms. Tape Head: 3mV (at 3\frac{3}{4}\text{ (i.j.s.) Mag. P.U.: 2mV. Cer. P.U.: 80mV. Tuner: 100mV.

Aux. 100mV. Tape/Rec. Output: Tuner. Equalisation for each input is correct to within +2d8 (R.I.A.A.) from 20Hz to 20KHz.

Tone Control Range: Boss: 13dB at 60Hz. Treble: = 14dB at 15kHz. Total Distortion: (for 10 watt output) < 15\%. Signal Noise: < -60dB. A.C. Mains 200-250V. Size 12\frac{1}{2}\text{ in long. 4\frac{1}{2}\text{ in long. 4\frac{1}{2}\text{ in high. Built and tested.}



The Viscount INTEGRATED HIGH FIDELITY TRANSISTOR STEREO AMPLIFIER

> 131 GNS. Plus P. & P. 716

SPECIFICATION: Output: 10 wates per channel into 3 to 4 ohms speakers (20 wates monoral). Input: 6-position rotary selector switch (3 pos. mono and 3 pos. stereo). P.U., Tuner, Tape and Tape Rec. out. Sensitivities: All inputs 100mV into 18M ohm. Frequency Response: 40Hz-20KHz ±2dB. Tone Controls: Separate bass and treble controls. Treble 13dB lift and cut [at 15KHz]. Boss: 15dB lift and 25dB cut [at 80Hz]. Volume Controls: Separate for each channel. A.C. Mains Input: 200-240V, 50-60Hz. Size: 12½in x 6in x 2½in teak-finished case. Built and tested. P. & P. 7/6. Viscount Mark II for use with magnetic pick ups specification as above. Fully equalised for magnetic pick ups. Suitable for cartridges with minimum output of 4mV/cm/sec. at 1kc. Input Impedance 47k. 15 gns. plus 7/6 P. & P.



THE RELIANT Mk. II SOLID STATE GENERAL PURPOSE AMPLIFIER

61 GNS. Plus P. & P. 7/6 In teak-finished case

SPECIFICATION: Output: 10 watts into a 3 ohms speaker.

Inputs: (1) for mike (10mV). Input (2) for gram, radio (250mV) individual bass and treble control.

Transistors: 4 silicone and three germanium. Mains input: 220/250 volts. Size: 10½ × 4½ × 2½in. Mike to suit (crystol): 12/6 plus 1/6 P. & P. 8 × 5in speaker 14/6 plus 3/- P. & P. Mk. I 5½ gns. plus 7/6 P. & P. Less teak



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KIT: 9/6 extra.

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A complete Loud Speaker system on one
frame combining three matched ceramic
magnet speakers with a low loss cross-over
network. Peak handling power 10W.
gauss. Resonance 40-60c/s. Size 13‡ y
8½ × 4½ in. By famous mandacturer.
List price 47. Our price 74/6 plus 5/P. & P. Similar speaker to the above
minus tweeters in 3 and 15 ohms 44/6 plus
5/- P. & P. THREE-IN-ONE HI-FI 10 WATT SPEAKER !

Elegant Seven Mk. III (350mW Output)



The ASSUM W Output)
T-transistor fully tunable M.W.-L.W. Superhet portable. Set of parts. Complete with all components, including ready etched and drilled printed circuit board—back printed for foolproof construction MAINS POWER PACK KIT: 9/6 extra.

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Size $3\frac{3}{4}\times2\frac{1}{4}\times1\frac{1}{2}$ in. Meter size $2\frac{1}{4}\times1\frac{1}{4}$ in. Sensitivity 1,000 O.P.V. on both a.c. and d.c. volts. 0–15, 0–150, 0–1,000 d.c. current 0–150mA. Resistance 0-100kohms. Complete with test prods, battery and full instructions, 42/6. P. & P. 3/6. FREE GIFT for limited period only, 30W Electric Soldering Iron Value 15/- to every purchaser of the Pocket Multi-Meter.

This tape deck takes 5\(\frac{1}{2}\)in spools complete with two-track heads. Size 13\(\frac{1}{2}\)in long by 8\(\frac{1}{2}\)in wide.

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Build a Strobe Unit, using the latest type Xenon white light flash tube. Solid state timing and triggering circuit. 230/250v. A.C. operation.

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I to 36 Flash per sec. All electronic components includ-ing Veroboard S.C.R. Unijunction Xenon Tube and in-structions 45.5.0 plus 5/- P. & P.

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Ideally suitable for schools, laboratories, etc. Roller tin printed circuit. New trigger coil, plastic thyristor I-80 f.p.s. Price 9 gns. 7/6 P. & P.

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This strobe has been designed and produced in response to wide public demand, for use in large rooms, halls and the photographic field. It has four times the light output at 30 f.p.s. and utilizes a silica plug-in tube for longer life expectancy, printed circuit for easy assembly, also a special trigger coil and output capacitor. Light output approx. 4 foules. Price 410.17.6. P. & P. 7/6.

Trinch POLISHED REFLECTOR

Ideally suited for above Strobe kits. Price 10/6. P. & P. 2/6 or Post Paid with kits.

100 WATT POWER RHEOSTATS (NEW)

AVAILABLE IN THE FOLLOWING VALUES: Tohm, 10 a.; 5 ohm, 4.7 a.; 10 ohm, 3 a.; 25 ohm, 2 a.; 50 ohm, 1.4 a.; 100 ohm, 1 a.; 250 ohm, .7 a.; 500 ohm, .45 a.; 1,000 ohm, 280 mA; 1,500 ohm, 230 mA; 2,500 ohm, .2 a. Diameter 3½in. Shaft length ¼in., dia. ½in. All at 27/6 each. P. & P. 1/6.

1/5/10/25/50/100/250/500/1,000/1,500/2,500 50 WATT.

All at 21/- each. P. & P. 1/6. /ATT. 10/25/50/100/250/500/1,000/1,500/2,500 WATT. ohm. All at 14/6 each. P. & P. 1/6.

VEEDER ROOT, 230V a.c. 50 cycle, 5-figure counter 18/6, P. & P. 1/6. (non-resettable).



Large Digit 12V d.c. MAGNETIC COUNTER. 4in drum calibrated 1-9. Figures 1 in high, 3in wide. Set of 1m, 1b; Ic/o contacts operated by drum cam. The units can be used in pairs and are ideally suited for batch or lap recording or for the many purposes where large easily read numerals are required. Price 18/6, P. & P. 2/6.

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The above two precision made U.S.A. motors
are offered in 'as new 'condition. Input voltage
of motor 115v. A.C. Supplied complete with transformer for
230/240v. A.C. input. Price, either type £2. 17. 6 plus 6/6
P. & P. or less transformer £2. 2. 6 plus 4/6 P. & P.

NICKEL CADMIUM BATTERY. 1.2 volt 35 AH.

Size 8½ in. high ~ 3 ~ 1½ in. 30/- each plus 4/- P. & P.

Sintered Cadmium Type 1-2 v. 7AH. Size: height 3½ in., width 2½ × 1¾ in. Weight: approx. 13 oz. Ex-R.A.F.

Terred 1.2 & 8.8 % 2.4 & 8.8 width 28 × 13 in. W Tested. 12/6. P. & P. 2/6.

DRY REED SWITCHES

2... I amp Dry Reeds (makes contacts). Mounted in 870 ohm 9-18 v. coil. Size 3" > \frac{1}{2}" > \frac{1}{2}". New. Price 8/6 of the above mentioned units [1] pull. 10/6, P. & P. 1/6. SOLENOID. Approx. Ilb per pair. Post Paid. Six of the above mentioned units [1] pull. 10/6, P. & P. 1/6. OLC. SOLENOID. Approx. 21b Mfg. by Elliott Bros. New. 45/- each. Post Paid. pull. 12/6, P. & P. 1/6. pull. 12/6, P. & P. 1/6.

Kit of parts, including ORPI2 Cadmium Sulphide Photocell, Relay, Transistor and Circuit, etc., 6-12 volt D.C. op., price 25j- plus 2/6 P. & P. ORP 12 including circuit, 10/6 each, plus 1/- P. & P. A.C. MAINS MODEL. Incorporates Mains Transformer, Rectifier and special relay with 2 5 amp mains c/o contacts. Price inc. circuit 47/6 plus 2/6 P. & P.

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light source with focusible lens assembly and ventilated lamp housing, to take MBC bulb. Separate photo cell mounting assembly for ORP. 12 or similar cell. Both units are single hole fixing. Price per pair £2.15.0. P. & P. 3/6.
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Adjustable tone control. Fitted with moving coil speaker, also earpiece for personal monitoring. Complete with morse key. 45/- plus 3/6 P. & P.

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respectively. respectively. A com-posite apparatus designed for

class demonstration. Electro magnetic induction, jumping ring, induction lamp, relationship between field intensity and ampere turns, induction melting, are just a few of the possible experiments. Ne modified model. £14.10.0, P. & P. 10/-.

RELAYS New SIEMENS, PLESSEY, etc. mini-ature plug in relays complete with base, athighly COMPETITIVE PRICES

Coil Ω	Working Voltage	Contacts	Price
280	6-12	2 c/o	14/6
700	12 - 24	2c/o	12/6
700	16-24	4 c/o	15/6
700	16-24	4M 2B	12/6
1250	20 - 40	2 c/o H.0	
2500	30 - 50	2 c/o H.E	0. 12/6
9000	40 - 70	2 c/o	10/-
M n	Manus Dua	POST	ALD.

230 volt AC Coil. Three c/o 5 amp. contacts. 17/6 post paid. LONDEX 4 c/o 3 amp contacts. 18/6 inc. base acad paid.

MINIATURE RELAYS
30-36 D.C. operation. 2 c/o. 500 M.A. contacts. 3,200 ohm coil. Size only 1 4 4 11.

8/6 post paid SANWA MULTI RANGE METERS

New Model U50D Multi tester, 20,000 OPV, mirror scaled with overload voluv Orv, mirror scaled with overload protection. Ranges d.c. volts: 100mV. 0:5V, 5V, 250V, 1,000V; a.c. volts: 2:5V, 10V, 50V, 250V, 1,000V; d.c. current: 5/rA, 0-5MA, 5MA, 50MA, 250MA Complete with battery and test probe. £7.5.0 post paid.

230V A.C. SOLENOID Heavy duty type. Approx. 21b pull. 17/6, P. & P. 2/6. 12V D.C. SOLENOID.





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Constructional projects in microelectronics for the amateur experimenter

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AMATEUR SSB RADIO GUIDE, by Harry D. Hooton. 30/-. Postage 1/-. THE RADIO AMATEUR'S HAND-

BOOK, by A.R.R.L. 45/-. Postage 4/6.

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REVERBERATION AMPLIFIER. Self contained transistorised battery operated. An entirely different approach to sound reproduction. Normally sound reproduction from a single course has a flat one dimensional effect. With this, proper sound delay through reverberation, tones are created with a truly third dimension for concert hall originality. Two controls adjust volume and reverberation. Simply plug microphone, guitar, etc., in and the output into your amplifier. Supplied in a beautiful walnut cabinet 7½ × 3 × 4½ in. £10.4.0, P. & P. & Ins. 6/-.

P. & P. & Ins. 6/-.

POWER CONTROLLER. Power at your finger tips. Not just half wave control but full wave. One variable control gives zero to full power. Uses latest 15 amp 3 kw triac and special triggering device. Complete with box, power socket, etc. Ideal for flood lights, fires motors, etc. In kit form 65.9.6., ready built £9.4.6. + 3/6 P. & P.

VOX SWITCH KIT. This sound operated switch is ideal for mobile T.X. work tape recorder switching, etc., etc., you speak it switches. High & med. imp. inputs. A.F. take off point. Drives your 12 volt relay. 42/6, off point. P. & P. 2/6.

METRONOME KIT. Variable beat, lister whilst you play and keep in the groove. Easy to build, pocket size with personal mini earphone 25/- P. & P. 2/6.

43/- F. & F. 2/6.

MORSE OSCILLATOR KIT. P.C. board, transistors, high stab. components battery carrier, ear piece. Adj. tone. Just attach your key. Drives phones or speaker. 15/6. P. & P. 2/-.

Free lists with every order. For lists only send 1/- P.O. (deductable from first order).

AUDIO EFFECTS 5 SHAW LANE, HALIFAX

MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

CIRCUIT MONITOR

Any indication of what's happening in any experimental or prototype circuit is always invaluable to designers and experimenters, and the new surge indicating meter from John Howard Industrial Electronics Ltd., should be most useful in this respect.

Believed to be the first of its kind, the meter is simply clipped across the supply to be monitored and any surges which occur on the line of microsecond duration or longer are instantly displayed on a large mirror scale meter. The reading is automatically held for approximately 30 seconds and is reset by a push button control mounted on the front panel.

The stand may be mounted either horizontally or vertically and there is no danger of grasping the iron at the wrong end. The interior of the stand is fully ventilated and is fitted with a black-anodised heat shield. These features ensure that the soldering iron is maintained at its normal operating temperature and that the external parts of the stand remain cool.

There is an easily replaceable bit cleaning pad and the complete stand costs 25s from any good components shop or direct from Light Soldering Developments Ltd., 28, Sydenham Road, Croydon.

MAINS WIRING SYSTEM

Have you ever wished you could plug your equipment into a socket anywhere around the room, or reduce the liability of accidents caused by trailing mains cables?

The "Extenda-Plug" is a new method of running mains wiring so that the sockets can be clipped onto

the wiring track at any convenient position (see photograph). The space between each socket is fitted with safe plastics covering to hide the earthing conductors.

The system is completely safe from young fingers and the sockets do not make contact with the conductors

way only, making this system ideal for d.c. supplies as well as a.c.

Typical applications are where several appliances are to be plugged into a common supply source; the total consumption must not exceed the main socket rating, e.g. 13A. The system can be equally well used in re-wiring or where trunking systems are required.

The complete basic kit comprising 3 metres of wiring track, three snapon socket outlets, three fused plugs, plastics cover strip, junction box and blind end caps, cost £5 9s 6d direct from Extenda-Plug, Amhurst Park Works, Tottenham, London, N.15.

Extra parts can be obtained also, and the system can be extended for as long and as complex as required.

LITERATURE

As a preview to the introduction of colour television by the Independent Television Authority, a series of brochures has just been released to help explain their future developments.

Leaflets of particular interest to readers include ITA Colour, What The Viewer Needs To Know, and Good Viewing of Independent Televi-

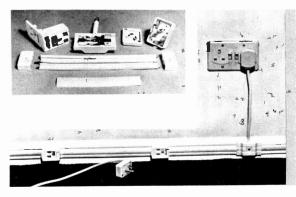
The leaflet ITA Colour explains the first phase of the colour/u.h.f. network and includes a list of the first 60 u.h.f. stations. In simple question



Surge meter from John Howard Industrial Electronics



Litegard bench stand manufactured by Light Soldering Developments



Extenda-Plug mains wiring system marketed by Extenda-Plug

Two stock models are available with ranges of 0 to 200 volts and 0 to 2 kilovolts f.s.d., price £20. Other ranges can be supplied to order and further details can be obtained from John Howard Industrial Electronics Ltd., 32, Oaks Road, Great Glen, Leicester.

IRON STAND

The new Litegard bench stand has been specially designed to completely cover the soldering iron bit and hot element for complete protection against accidental burns.

until the hinged top is pressed down into place. To remove the socket this top must be lifted; on doing so the claw contacts are released from the conductors before the socket comes right away. The action of the socket top is deliberately stiff to prevent children pulling the socket off.

Although a non-standard three-pin plug is used, this disadvantage is easily offset by the versatility and safety of the system. Each plug is fused and the pins are different sizes, so it is impossible to plug in the wrong way. The sockets can be fitted one

and answer form the basic facts about three-channel colour, u.h.f., 625 lines and "duplication" is described in What The Viewer Needs To Know.

Advice on questions of u.h.f. and v.h.f. reception, stressing the importance of good aerials and low-loss feeders for u.h.f. and v.h.f. reception, choice of station, reception of colour, and problems arising from supply voltage variations are given in Good Viewing of Independent Television.

Further details of the leaflets can be obtained from ITA, 70 Brompton Road, London, S.W.3.

SELECTION FROM OUR POSTBAG

correspondents wishing a reply must enclose a stamped addressed envelope

E-waves

Sir-The letter "Strobe Effect" from C. J. Manwell in your August 1969 issue mentions the book Living Brain by Dr Grey Walter. This was first published as long ago as 1953, and your readers may be interested to hear of more recent developments in

electroencephalography.

The most interesting of these is the discovery of E-Waves (Expectancy, Decision and Intention which are electrical oscillations in brain-cells arising when acts of will or decisions are made. These impulses can be fitered and passed through suitable electronic circuits and relays. to operate mechanisms which carry out the wishes of the operator without any muscular movement being necessary. For example, the operator could select a particular television channel by merely desiring or willing to do so, without pressing any buttons or carrying out any movements at all.

Further details for those interested can be found in our publication "E-Waves", price 6s, obtainable from our address below.

B. Herbert, M.Sc., B.A.(Oxon.), Paraphysical Laboratory, Downton, Wilts

Film Trailer

Sir-A Television Servicing and Installation film is being produced by this Company and will be available later this year for rental or purchase by responsible organisations. Perhaps your readers may care to know of the production of this film as there are some rather unique features. We have carefully searched for a film which deals exhaustively with Colour Television and Installation which would clearly and comprehensively give the average service engineer all the information he requires.

The film will be of use to Colleges of Further Education, Technical Schools and Companies who have many service engineers on their payroll, such as Television Rental

Companies.

Manufacturers of test equipment. of television receivers, of components and other Companies who have an interest in colour television are being invited to supply their latest products for inclusion in the film, this will allow the audiences to become acquainted and familiar with the latest techniques and equipment for speedy and efficient repair, maintenance and installation of colour television receivers.

A precis of this film is available and any of your readers, either manufacturers, students or responsible organisations generally may receive a copy of this if they care to write to us.

Donald Blakey, Donald Blakey Ltd., 339 Clifton Drive South. St. Annes-on-Sea, Lancs.

Electronics clubs?

Sir-With reference to the letters relating to Electronics Clubs. would like to be able to ascertain from your readers living in East Sussex as to the demand for such clubs in our county.

May I suggest that interested readers write to this address giving the following information:

(a) Area in which club is required.

(b) A brief outline of their interests in Electronics.

(c) Type of club they envisage. social, workshop e.g. facilities, educational, etc.

Trusting that I may be able to help your readers.

> J. A. Dixey, 62 St. Leonards Gardens, Hove.

Sir-Would anyone who is interested in re-establishing the Wanstead and Woodford Radio Society to be active again in forwarding the hobby of radio and electronics in the London E.11/E.18 area, please contact me at either 82, Granville Road, Walthamstow, E.17., or at The Electronics Laboratory, The University, Canterbury, Kent.

Ken Smith, G3JIX, Canterbury, Kent.

Amplify please

Sir-As an amateur constructor of projects in your magazine, I am constantly asked to build guitar and public address amplifiers, rated at. anything from 50 to 100 watts, for pop groups. The look on their faces is both surprising and increasingly frustrating when I shake my head and say that I have no circuit to meet their requirements.

Whilst I agree that various different accessories in use by these "pop" musicians have been previously described in Practical Electronics, it would seem that a feature on a 50 to 100 watt amplifier is not to be forthcoming. It has been suggested to me, that you (P.E.) would rather not 'step on manufacturers' toes", which

I disbelieve.

In view of these circumstances, I would ask if readers might help, as I surely cannot be the first in this predicament and I would be grateful if you will publish this letter with a view to me getting help and thus relieving my frustration.

J. T. Jones, Liverpool.

We have just completed the preparation of a 100 watt amplifier, and it is hoped to commence publication in the near future.

Courses . . .

BRENTFORD

September 22, Radio Amateurs' Course, at Brentford Centre for Education, Brentford Secondary Girls' School, Clifden Road, Brentford.

September 24, High Fidelity and Tape Recording, at Brentford Centre for Adult Education, Brentford Secondary Girls' School, Clifden Road, Brentford.

Enrolments: September 11, 12, 15 and 16; 6.30-8.30 p.m. Fees: £2 10s for one subject; £1 for each additional subject.

GLASGOW

September 9, 7 p.m. Radio Amateurs' Course, at Glasgow College of Nautical Studies, 21 Thistle Street, Glasgow, C.5.

Enrolments: September 9. Fees: £1.

LONDON

September 23, 7.30 p.m. Radio Amateurs Course, at Gascoigne Recreation Centre, Gascoigne School, Marley Road, Barking.

Applications should be addressed to the Warden.

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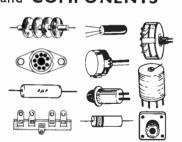
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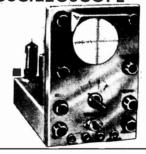
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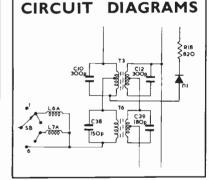
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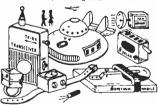
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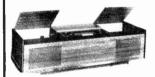
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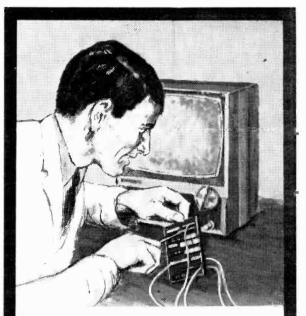
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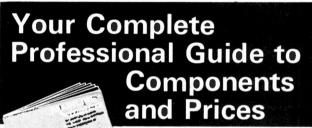
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1,000, 1,200, 1,500, 2,200, 2,7 3,300, 3,900, 4,700, 5,600	1/9 1/9 2/– 2/3 2/6 2/9 3/–	13/10 27/11 14/1 31/- 15/2 32/10 15/11 34/9 17/3 37/10 20/1 43/6 22/1 47/10 24/9 53/8 26/1 56/6	96/- 101/- 107/4 115/- 133/9 147/4 165/4 173/9	Price POLYESTER Tubular, 10% 0·1μF, 9d. 0· 2/3. 1μF, 2/8. 400V: 1,000, 1	, 160V: 0.01, 15/4F, 11d. 0 .500, 2,200, 3,	1/6 RS (Mulia 0·015, 0·02 22μF, 1/	2/- ard) (2μF, 7d. (0·33μF, F, 6d. 6,	1/3. 0·4 800 _p F, 0·	2/6 047μF, 8α 7μF, 1/6. 01, 0·015,	3/- 1. 0.068, 0.68μF,
82,000 0-1µF 0-12µF 0-15µF 0-18µF 0-22µF	3/6 3/9 4/3 5/- 6/-	27/5 59/4 30/3 65/10 34/2 73/7 37/10 81/11 47/- 101/10	182/8 202/- 228/- 252/3 313/4	7d. 0.033μF, 2 I/6. 0.33μF, 2 Modular, mer 0.033, 0.047μF 0.47μF, I/8. 0	2/3. 0-47/4F, 2 tallised. P.C. n , 8d. 0-068, 0-	/8. nounting, 2 1	20%, 250\	/: 0·01, 0	0.015, 0.0	22μF, 7d.
0·27μF	6/9 7/3 7/9 9/9	53/9 16/8 58/10 126/11 65/- 140/10 75/2 137/7	358/4 390/- 433/4 500/	SEMICOND OC81D, OC82 2/6. AF115, 5/ OC139,	:D, 2 /~. OC7 AFII6, AFII7,	0, OC72, 2 . ACY19, A	/3. ACII CY21, 3/3	07, OC7! I. OCI	5, OC170 140, 4/3.	, OC171,
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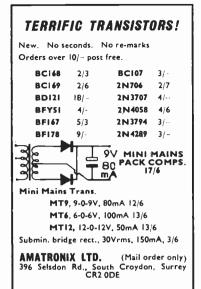
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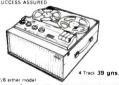
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