# Directional Antenna Patterns

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SYSTEMATIZATION OF TWO TOWER PATTERNS



SYSTEMATIZATION OF THREE TOWER PATTERNS

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#### PREFACE TO FIRST EDITION

Directional antenna design is a specialized field of communication engineering requiring considerable mathematics and experience or education to become proficient. Furthermore, the computations in many instances become very involved and lengthy. Therefore, much time may be saved in making a design if suitable formulas and a good collection of patterns are available. The purpose of this book is to aid the design engineer by furnishing a number of useful formulas and a lengthy collection of systematized directional antenna patterns. The design formulas are supported by suitable developments since most of us do not desire to accept an unknown formula.

There is quite a wide variety of nomenclature used in directional antenna designs. Reviewing designs on file with the Federal Communications Commission reveals that practically every consultant has his own pet way of presenting the information and almost invariably uses his own variety of symbols. Recently, incollecting parameters for directional antennas from the FCC files, it was revealing to observe how difficult it was to determine some of the pertinent factors. In this book considerable thought has been given to nomenclature and in most cases the selection has been made to fit in with FCC practice, in so far as possible, and still maintain simplicity and clarity. It is hoped that some standardizations can eventually be made so everyone can speak the same language with similar symbols. The author would welcome any constructive criticisms to the nomenclature presented in this book, as well as pointing out errors which are bound to occur in a book of this nature. The book has been made loose-leafed for ease in making additions and changes.

Due to the lack of systematized directional antenna patterns an electro-mechanical calculator was constructed prior to World War II. In the fall of 1941, the machine was completed and the work was started to systematize two and three tower directional antenna patterns. The work was faithfully carried on during the war years by the operators at the WHK transmitter in Cleveland, Ohio, with the result that we now have all of the patterns that were contemplated when the systematization was started.

The electro-mechanical calculator used to systematize the patterns has proven to be a very useful instrument and with the scientific advances during the war it is hoped that a more precise machine can be constructed at an early date. In any event, it is believed, that if the patterns in this book are used merely as a guide to show trends, and not necessarily to show precise patterns, that the systematization will have served its purpose.

In the preparation of a book of this nature it is not possible to give credit to everyone involved, however, the author would like to mention some of the highlights. Mr. William G. Hutton worked with the author from the beginning of this project, In fact, at one time, the systematization project was started on his mechanical calculator and after drawing a couple of patterns it was decided that it would be quicker and easier to design a special machine to do the job.

The author wishes to give particular credit to the United Braodcasting Company and Radio Station WHK for being sympathetic to the project and furnishing the spare time help of their technicians to operate and maintain the electromechanical calculator. It is indeed a pleasure to mention the following men who did the bulk of the systematization work: James Sturdevant, over 7,000 patterns. Charles Carment, over 800 patterns. P. C. Tuttle, over 800 patterns.

In preparing the text material the author wishes to give credit to the following: Edgar F. Vandivere, Engineering Department of FCC who furnished some of the basic notes for the mutual resistance method of determining pattern size; J. F. Morrison, Bell Telephone Laboratories, for the mutual impedance data plotted in Figs. 30 and 31; William G. Hutton, for the mutual impedance data plotted in Fig. 32; Dr. Edward C. Jordan, University of Illinois, for the mutual impedance data plotted in Figs. 33 to 37; Calvin S. Warner, United Broadcasting Company, for his excellent drafting of the figures; and Mr. James Harvey, Cleveland Institute of Radio Electronics, for his patience in composing Part I.

Carl E. Smith

Cleveland, Ohio June, 1946

#### PREFACE TO SECOND EDITION

The second edition title has been changed from "Directional Antennas" to "Directional Antenna Patterns" since all of the directional antenna patterns have been retained and most of the "Theory and Design of Directional Antenna Systems" has been published in a companion book that is more complete and up to date than the original edition.

The first part on theory and application has been thoroughly revised to cover information not contained in the companion book, "Theory and Design of Directional Antenna Systems." The primary purpose of this section is to give the information necessary to make the patterns more useful. The second and third parts containing the systematization of two and three tower patterns has not been altered.

Since Parts II and III represent over four man years of work, it was not practical to rerun the patterns to improve the accuracy. As stated in the first edition preface, these patterns are to be "used merely as a guide to show trends, and not necessarily to show precise patterns." The word field intensity should read field strength to conform with the IRE definition.

Carl E, Smith

Cleveland, Ohio January, 1958

## THEORY AND APPLICATION



#### 1. FUNDAMENTAL PROPERTIES

a. Introduction. - The purpose of a radio broadcasting station is to transform sound waves into radio waves that can be picked up by radio receiving sets. The utility of this service to the public depends upon: (1) Signal Strength, (2) Program Content, and (3) System Distortion. Of these factors, the radio broadcasting station engineer is concerned with producing an intense signal that will override noise and undesired signals in the receiving sets being served and with minimizing distortion in the audio and radio facilities of the station.

The antenna is the last point in the system under the control of the radio broadcasting station. Radio waves radiated from the transmitting antenna are propagated through space to the receiving antenna. The only control over these propagated waves is the selection of the antenna site, the polarization, and the intensity of the signals leaving the transmitting antennas. The selection of the antenna site is determined by many considerations, such as; ground constants, terrain, distance and direction to the populated areas to be served, distance and direction to the areas to be protected, and last but not least is the availability of a suitable land area to install the necessary towers and ground system.

For standard broadcast stations, vertical polarization is used because of its superior ground wave propagation characteristics and the simplicity of antenna design. The intensity of the signal from the transmitting antenna, in any given direction, depends upon the output power of the transmitter and the antenna design. Since the output power is regulated by the Federal Communications Commission for the class of station involved, the only factors remaining under the engineer's control are the antenna siting and design. These factors go hand in hand when designing directional antennas for broadcasting purposes.

b. <u>Purpose</u>. – Directional broadcasting antennas are required for one or more of the following reasons:

(1) Protect the service area of other broadcasting stations by causing the waves to cancel in these directions.

(2) Increase the service area of a broadcasting station, particularly in the direction of densely populated areas, by causing the waves to be reinforced in these directions.

(3) Eliminate multiple ownership problems by controlling one or more of the directional antenna patterns of radio stations owned by the same company.

(4) Control service area to minimize population lost due to interference within the normally protected contour.

c. Control of Pattern Shape. - The usual problem in broadcast practice is to mould the radiation pattern into the desired shape to cover the service areas and give the required protection to other radio stations. As a matter of economics, it is desirable to do the job with the minimum number of antennas. With severe requirements, the number of antennas must be increased until the radiation pattern can be made to conform to the required shape. As a general rule, two stations can be given the required protection with two towers; three stations can be completely protected with three towers in line or if the protection is not severe, it is possible many times to do the job with two towers. With four towers it is always possible to completely control the nulls toward four stations; however, if the job can be done

with three towers there is a saving of the cost of one tower.

In controlling the pattern shape, consideration has to first be given to fulfilling the conditions of the required protection to other radio stations in accordance with the Rules and Regulations of the Federal Communications Commission. The FCC Rules are an excellent practical guide for allocation work. The Standards of Good Engineering Practice incorporated in the Rules and Regulations was compiled by FCC from extensive data collected by its Engineering Department over a long period of time. This material is under almost constant revision as the art progresses.

The next consideration is to locate the directional antenna system so that the horizontal lobes will be directed toward the population areas to be served without having too many people within the blanket area, that is, the area near the transmitter where the signal is so strong that other radio stations cannot be received without objectionable interference and still be able to serve the business district with at least 25 millivolts per meter field strength.

d. Determination of Pattern Size. - Pattern size is determined by the class of station and efficiency of the antenna system. The power for the class of station is regulated by the Federal Communications Commission as outlined in Part 3 of the Rules and Regulations. In general, the power ranges from 50 kilowatts for clear channel stations to 5 kilowatts for regionals down to 250 watts for local stations. The predominance of directional antenna designs are for regional stations which have to protect radio stations in other regions of the country. A few are used on clear, but none on local channels.

The efficiency of the antenna system depends upon the antenna design. It is always desirable to maintain a high efficiency in order that a high percentage of the output power of the transmitter may be radiated. To do this it is sometimes necessary to use a more complicated directional antenna system to give the required degree of protection to other radio stations. In other words, a low efficiency simple antenna system might give the required protection, but would not meet the FCC minimum requirement of 175 millivolts per meter root-mean-square unattenuated field strength for one kilowatt at one mile in the horizontal plane.

#### 2. GENERAL TREATMENT

#### a. Standard Reference Antennas. -

(1) Uniform Spherical Radiator... The Uniform, Omnidirectional, or Isotropic radiator, in free space, is taken as THE Standard Reference Antenna because it has no directivity. Such an antenna is illustrated in Fig. 1. It is defined as a theoretical antenna which radiates waves having the same field strength in all directions. Actually such a radiator of radio waves cannot be realized, because all radio antennas have directional properties. In the case of the acoustic waves, this standard is represented by a sphere pulsating radially.



PATTERN OF A UNIFORM RADIATOR WHICH IS THE THEORETICAL STANDARD REFERENCE ANTENNA

#### Fig. 1

For a 1 kw power source, a uniform radiator will produce a field strength of -

$$E_{S} = 107.6$$
 (l)

where  $E_s = millivolts$  per meter unattenuated field strength at one mile for one kilowatt. This standard has come into rather common use. With this information, the figure of merit of other antennas can be compared with this basic standard. Other secondary standards for free space may be selected and used as convenience demands.

(2) Uniform Hemispherical Radiator... If a uniform radiator is placed at the surface of a perfectly conducting earth, all of the power must be radiated in the hemisphere above the surface of the earth as shown in Fig. 2. For a given power source, the power flow will have twice the intensity of a uniform radiator in free space; hence, the power gain is said to be 2. For this case, the field strength gain is  $\sqrt{2}$ , therefore, the field strength is  $107.6\sqrt{2}$ or,

$$E_{S} = 152.1$$
 (2)

where  $E_s$  = millivolts per meter unattenuated field strength at one mile for one kilowatt.



PATTERN OF A UNIFORM RADIATOR AT THE SURFACE OF A PERFECT REFLECTING EARTH

#### Fig. 2

At the present state of the art this antenna has only academic interest; however, it is a standard for antennas at the surface of the earth, such as radio broadcasting antennas. It is particularly useful in the computation of antenna gains. This type of antenna can be considered as a standard for determining the directivity of antennas located on the surface of the earth.

(3) Current Element Antenna in Free Space...An electric current element in free space, sometimes referred to as an elementary doublet or dipole, consists of a very short conductor (mathematically of infinitesimal length) having a uniform current distribution. This infinitesimal antenna is universally used in developing the radiation property of an antenna of any configuration. This current element antenna is a mathematical convenience only, because such an antenna in practice for a specified field strength would require excessive transmitter power because of the high losses due to the radiation resistance being low in comparison to the loss resistance encountered in practice. The field strength at any distant point in space as shown in Fig. 3(a) is given by:

$$E = \frac{60\pi}{d\lambda} I (\delta G) \cos \Theta$$
 (3)

or

$$=\frac{60\pi f}{dc} I (\delta G) \cos \Theta$$

where E = field strength in volts per meter at point P

- $\pi = 3.1416$
- d = distance in meters from current element to the point P
- $\lambda$  = wave length of radiated wave in meters
- f = frequency of current in cycles per
   second
- $c = 3 \times 10^8$  meters per second, the velocity of light
- L = effective current in amperes flowing in the conductor
- $\delta G$  = elementary length (or height) of conductor measured in meters
  - $\Theta$  = elevation angle of point P measured from a plane perpendicular to the conductor.

When this elementary antenna radiates one kilowatt of power the field strength at one mile is -

 $E = E_0 \cos \Theta$ 

= 131.8 cos  $\Theta$ 

(4) where E = millivolts per meter unattenuated field strength at one mile for one kilowatt











c) HORIZONTAL CROSS-SECTION VIEW OF TOROIDAL RADIATION PATTERN SHOWING ZERO HORIZONTAL DIRECTIVITY



(d) SURFACE PATTERN SHOWING TOROIDAL OR DOUGHNUT SHAPE

## THE RADIATION PATTERN OF A VERTICAL ELECTRIC CURRENT ELEMENT

#### IN FREE SPACE

#### Fig. 3

- $E_0$  = millivolts per meter field strength measured on a plane perpendicular to the conductor and in this case at the distance of one mile for one kilowatt of radiated power
- $\Theta$  = elevation angle as shown in Fig. 3(a).

The value of 131.8 is the maximum field strength and is a constant in the horizontal plane. See Fig. 3(c). This current element antenna is sometimes used as a secondary standard reference antenna.

(4) Vertical Current Element Antenna Over a Perfectly Conducting Earth...If a



(.) VERTICAL RADIATION PATTERN

q = 3

TOP OF VERTICAL

CURRENT ELEMENT

SE0= 186.3 MV/M AT I MILE FOR I KW

F



(b) SIDE CROSS-SECTION VIEW OF THE TOROIDAL HEMISPHERICAL PATTERN SHOWING THE VERTICAL DIRECTIVITY.



(c) HORIZONTAL CROSS-SECTION VIEW OF TOROIDAL HEMISPHERICAL RADIATION PATTERN SHOWING ZERO HORIZONTAL DIRECTIVITY

Ś

(d) SURFACE PATTERN SHOWING TOROIDAL HEMISPHERICAL SHAPE

THE RADIATION PATTERN OF A VERTICAL ELECTRIC CURRENT ELEMENT OVER A PERFECTLY CONDUCTING EARTH vertical current element antenna is located at the surface of a perfect earth, the radiation will be hemispherical as shown in Fig. 4. When this vertical current element radiates 1 kw of power the field strength at one mile is

$$\mathbf{E} = 186.3 \cos \Theta \tag{5}$$



(a) VERTICAL RADIATION PATTERN



(b) SIDE CROSS-SECTION VIEW OF THE RADIATION PATTERN SHOWING THE VERTICAL DIRECTIVITY





(c) HORIZONTAL CROSS-SECTION VIEW OF RADIATION PATTERN SHOWING ZERO HORIZONTAL DIRECTIVITY

(d) SURFACE PATTERN SHOWING DOUGHNUT SHAPE

## THE RADIATION PATTERN OF A VERTICAL HALF WAVE RADIATOR

## where E and $\Theta$ are defined in Eq. (4) and Fig. 4(a).

This vertical current element antenna is sometimes used as a secondary reference antenna. It gives the vertical pattern of a zero height antenna. See Eq. (10). While one of these infinitesimal antenna itself is of no practical value it is useful in summing up the radiation effects of antennas having practical dimensions.

(5) Half Wave Antenna in Free Space ... A half wave antenna in free space will have essentially a sinusoidal current distribution as shown in Fig. 5(a). If the radiation



effects of the current elements as given in Eq. (3) are summed up for the whole antenna the field strength pattern is given by

$$\mathbf{E} = \frac{137.6 \cos (90 \sin \Theta)}{\cos \Theta} \tag{6}$$

where E and  $\Theta$  are defined in Eq. (3) and Fig. 5(a).

This type of antenna is often used as a secondary standard reference antenna because it is a practical type of antenna that is easy to setup experimentally. For example, the Federal Communications Commission uses this standard for FM and TV Broadcast Stations.

(6) Quarter-Wave Vertical Antenna Over a Perfectly Conducting Earth... This type of antenna is very common and is often used as a secondary standard reference antenna. With a sinusoidal current distribution as shown in Fig. 6(a) the radiation pattern is given by

$$E = \frac{194.9 \cos (90 \sin \Theta)}{\cos \Theta}$$
(7)

where E and  $\Theta$  are defined in Eq. (3) and Fig. 6(a).

Many directional antenna arrays are designed with quarter-wave elements because of the ease of making computations in design and adjustments during the proof of performance.

(7)  $0.311\lambda$  Vertical Antenna Over a Perfectly Conducting Earth...The Federal Communications Commission at the present time uses this height antenna G = 111.96°) as their standard reference antenna. It at one time represented the average height of broadcast antennas in the United States. With sinusoidal current distribution the radiation pattern is given by

$$E = 200 \frac{\cos (G \sin \theta) - \cos G}{(1 - \cos G) \cos \theta}$$
(8)

= 319.5 
$$\frac{\cos(111.96\sin\Theta) + 0.3740}{\cos\Theta}$$

- where E and  $\Theta$  are defined in Eq. (3) and G = 111.96° the height of the antenna in electrical degrees.
  - (8) Half-Wave Vertical Antenna Over

a Perfectly Conducting Earth... For comparison purposes it is of interest to present the radiation pattern of a half-wave antenna. With sinusoidal current distribution the radiation pattern is given by

$$E = 236.5 \frac{\cos (G \sin \theta) - \cos G}{(1 - \cos G) \cos \theta}$$
(9)  
= 118.25 
$$\frac{\cos (180 \sin \theta) + 1}{\cos \theta}$$

where E and  $\Theta$  are defined in Eq. (3) and G = 180° the height of the antenna in electrical degrees.

(9) Comparison of the Vertical Radiation Patterns of Primary and Secondary Standard Reference Antennas... Figure 7 gives a comparison of the radiation patterns of primary and secondary standard reference antennas. The vertical patterns are expressed in millivolts per meter at one mile for one kilowatt of input power. The field strength in millivolts per meter at one mile as a function of antenna height is given in Fig. 8.

b. Vertical Radiation Characteristics. – Already we have considered a number of vertical radiation patterns in Fig. 7. If these patterns are made equal to unity in the horizontal plane they are then known as vertical radiation characteristics. If this is done the curves of Fig, 9 result.

For a vertical antenna having a sinusoidal current distribution with a current node at the top, the vertical radiation characteristic takes on the form

$$f(\Theta) = \frac{\cos (G \sin \Theta) - \cos G}{(1 - \cos G) \cos \Theta}$$
(10)

where  $f(\Theta) = vertical radiation characteristic$ 

- G = electrical height of the antenna in electrical degrees
- elevation angle of the observa- tion point measured up from the horizon in degrees.

The curves in Fig. 10 represent the solution of this equation over the most useful range of antenna heights. The vertical radiation characteristic is plotted as a function of



REFERENCE ANTENNAS WITH A RADIATED POWER OF I KILOWATT

#### Fig. 7

elevation angle for various values of tower height. A representative set of tower heights have been selected for Fig. 10. Figure 11 represents this same information in a different form; that is, the vertical radiation characteristic is plotted as a function of electrical tower height for various values of elevation angle. In order to prevent reversals of the lines as plotted in Fig. 11, the curves are extended to negative values in Fig. 10. This merely means that the high angle lobe is of opposite phase to the low angle radiation.

The vertical radiation characteristic will be used in the generalized equation for determining the shape of the directional antenna pattern. See Eq. (15). In the horizontal plane this function reduces to unity and simplifies the design equation.

#### TABLE I

TYPE OF ANTENNA	VERTICAL PATTERN SHAPE	MV/M FOR I WATT AT I MILE E <sub>0</sub>	NV/N Forikw Atimile E <sub>o</sub>	POWER GAIN G	d b GAIN G	TYPE OF ANTENNA	VERTICAL PATTERN SHAPE	MV/M Foriwatt Atimile E <sub>o</sub>	MV/M FORIKW Atinile E <sub>o</sub>	POWER GAIN Q	dh Gain G
UNIFORM SPHERICAL Radiator	$\odot$	3.402	107.6	-	0	UNIFORM Hemispherical Radiator	funtant	4.811	(52.)	2	3,010
CURRENT Element	$\bigcirc$	4.167	1-31.8	1,5	1.761	VERTICAL CURRENT ELEMENT		5,893	86,3	3	4.771
HALF WAVE Antenna	$\mathcal{O}\mathcal{O}$	4,358	3 7.8	1.641	2,151	OUARTER WAVE Vertical Antenna		6.163	194.9	3,282	5,161
0.622 X Antenna	$\bigcirc$	4.472	141.4	1.728	2,375	0.311 X VERTICAL ANTENNA		6.324	200	3.456	5.386
TWO END ON HALF WAVE IN PHASE ANTENNA	$\phi$	5.283	167.1	2.411	3,822	HALF WAVE Vertical Antenna	finition	7.471	236.2	4.822	6,832

SUMMARY OF STANDARD REFERENCE ANTENNAS

#### c. Directivity Definitions. -

(1) On the Basis of Equal Powers... Directivity or directive gain of a given antenna can be defined as the ratio of the maximum power flow intensity to the power flow intensity of a uniform radiator when the total power output of both sources are equal. In Equation form,  $P_m$ 

$$g = \frac{P_m}{P_s}$$
 (equal powers) (11)

where g = directivity or power gain

- P<sub>m</sub> = maximum power flow intensity from the directional antenna radiating 1 kw of power
- $P_{s}$  = uniform power flow intensity from the standard reference antenna radiating 1 kw of power.

1.10







COMPARISON OF THE VERTICAL RADIATION CHARACTERISTICS FOR SEVERAL STANDARD REFERENCE ANTENNAS

Fig. 9

Or, in terms of field strengths, power gain can be determined by the following equation,

$$g = \left[\frac{E_m}{E_s}\right]^2 (equal powers)$$
(12)

where

g = directivity or power gain

- $E_m = maximum$  field strength in mv/m from the directional antenna at 1 mile for 1 kw of radiated power
- $E_s = field strength (107.6 mv/m)$ from a uniform spherical antenna at 1 mile for 1 kw of radiated power.

(2) On Basis of Equal Field Strengths .... The directivity can also be defined by taking the ratios of the power radiated when the maximum field intensity of the directional antenna is made equal to the field strength from a uniform spherical antenna.



Fig. 10



In equation form,

$$g = \frac{P_s}{P_r}$$
 (equal field strengths) (13)

g = directivity or power gain

 $P_{S}$  = power radiated (1 kw) from a uni-

form spherical antenna to produce a given field strength of  $E_s$  (107.6 mv/m) at 1 mile

 $P_r$  = power radiated from the directional antenna to produce the same given maximum field strength  $E_m$ .

#### (107.6 mv/m) at 1 mile.

To illustrate, let the field strength of a uniform hemispherical antenna be adjusted to produce 107.6 mv/m unattenuated field strength at 1 mile. The power radiated will be 500 watts; hence,

$$g = \frac{P_S}{P_r} = \frac{1.0 \text{ kw}}{0.5 \text{ kw}} = 2$$

the power gain of a uniform hemispherical antenna. In other words, twice the amount of power has to be supplied to the uniform spherical radiator to produce the same maximum field strength at one mile. In the uniform spherical radiator, the additional 500 watts is used in the other hemisphere to make the radiation pattern spherical.

(3) On Basis of Decibels... The directivity can also be computed in terms of decibels by the equation,

$$G = 10 \log g \tag{14}$$

where G = decibels directive gain

g = directivity or power gain.

d. Generalized Equation to Determine Pattern Shape. – The generalized equation for a directional antenna array as given here is based upon the following assumptions:

- (1) That the antennas are over a perfectly conducting plane earth surface
- (2) That the distance from the space reference point to the observation point is great in comparison to the physical dimensions of the directional antenna array.

The generalized equation for n antennas in the directional antenna array is -

$$E = E_{1}f_{1}(\Theta) / \beta_{1} + E_{2}f_{2}(\Theta) / \beta_{2} + E_{k}f_{k}(\Theta) / \beta_{k} + \dots + E_{n}f_{n}(\Theta) / \beta_{n}$$
(15a)

By using the summation sign this equation can be written

$$E = \sum_{k=1}^{k=n} E_k f_k(\Theta) / \beta_k$$
(15b)

where E = the total effective field strength

vector at unit distance for the antenna array with respect to the voltage reference axis

- $k = the k^{th}$  antenna in the system
- n = the total number of antennas in the directional-antenna array
- $E_k$  = the horizontal magnitude of the field strength at unit distance produced by the k<sup>th</sup> antenna
- $f_k(\Theta) =$  vertical radiation characteristic of the k<sup>th</sup> antenna-see Eq. (10) for a vertical thin conductor
  - $\Theta$  = elevation angle of the observation point measured up from the horizon
  - $\beta_{k} = S_{k} \cos (\phi_{k} \phi) \cos \Theta + \Psi_{k}$  (16)
    - = phase relation of the voltage (or current) in the k<sup>th</sup> antenna with respect to the voltage reference axis
  - $S_k \cos (\phi_k \phi) \cos \theta$  = space phasing portion of the  $\beta_k$  due to location of the k<sup>th</sup> antenna
  - $S_k$  = electrical length of spacing of the  $k^{th}$  antenna from the space reference point
  - $\phi_k$  = true horizontal azimuth, orientation of the k<sup>th</sup> antenna, with respect to the space reference axis
  - $\phi$  = true horizontal azimuth angle of the direction to the observation point P (measured clockwise from true north)
  - $\Psi_k = \text{time phasing portion of } \beta_k \text{ due to} \\ \text{electrical phase angle of the volt-} \\ \text{age (or current) in the } k^{\text{th}} \text{ anten-} \\ \text{na with respect to the voltage ref-} \\ \text{erence axis.}$

The generalized equation for n antennas as given in Eqs. (15a) and (15b) treats only the  $k^{\text{th}}$  antenna. All of the antennas in the directional antenna array can be handled in a sim-

ilar fashion and the vectors finally added together as indicated by the summation sign. It will be noted in this equation that the field strength vector for the k<sup>th</sup> antenna has a magnitude of  $E_k$  in all directions in the horizontal plane. This magnitude is modified by the vertical radiation characteristic  $f_k(\Theta)$  which corrects the magnitude of the field strength vector  $E_k$  to give the correct value of the elevation angle being considered. For simple vertical antennas Eq. (10), Figs. 10 and 11 can be used to determine the value of  $f_k(\Theta)$ .

The vector field strength from the k<sup>th</sup> antenna in any direction is illustrated in Fig. 12.



SUMMATION OF FIELD INTENSITY VECTORS FOR A ANTENNAS

#### Fig. 13

In the space phasing portion of Eq. (16), the term  $\cos \Theta$  reduces to unity in the horizontal plane. In this plane the space phasing is simply the difference in distance from the observation point to the k<sup>th</sup> antenna and the space reference point as shown in Fig. 15.

Since the observation point is assumed to be at a great distance, a perpendicular dropped from the k<sup>th</sup> antenna to the straight line connecting the observation and reference points creates a right triangle, the side of



#### Fig. 14



VECTOR REPRESENTATION OF THE MAGNITUDE  $E_k f_k(\Theta)$ AND PHASE ANGLE  $\beta_k$ OF THE FIELD INTENSITY FROM THE  $k^{th}$  ANTENNA

#### Fig. 12

It has a magnitude of  $E_k f_k(\Theta)$  and makes an angle of  $\beta_k$  with respect to the voltage reference axis. The summation of these vectors for the n antennas in the directional antenna array, as indicated in Eq. (15), is illustrated in Fig. 13. The vector angles, as will be noted in the figure, are all measured from the voltage reference axis.

The angle  $\beta_k$ , of the field strength vector, as defined in Eq. (16), is a function of space phasing and time phasing. The space phasing parameters for the k<sup>th</sup> antenna are illustrated in Fig. 14.

This figure illustrates that any antenna in the directional antenna array can be located with respect to the space reference axis by the true orientation angle  $\phi_k$ , and with respect to the space reference point by the distance  $S_k$ .



PLAN VIEW OF K<sup>th</sup> ANTENNA SHOWING SPACE PHASING IN THE HORIZONTAL PLANE

#### Fig. 15

which is  $S_k \cos (\phi_k - \phi)$ . This space phasing quantity is the required difference distance for any direction in the horizontal plane.

When the observation point is at some elevation angle  $\Theta$  the k<sup>th</sup> antenna will appear to be closer to the space reference point by the multiplying factor cos  $\Theta$ . Referring to Eq. (16) and Fig. 16, a right triangle can be formed by dropping a perpendicular to the line connecting the space reference point and the observation point.



ELEVATION ANGLE  $\theta$  SHORTENS THE SPACING  $S_k$  TO THE VALUE  $S_k$  COS  $\theta$ 

Fig. 16

The k<sup>th</sup> antenna then appears to have a space phasing of  $S_k \cos (\phi_k - \phi) \cos \theta$  from the space reference point. This is the complete expression for the space phasing of any antenna in the system and for any observation point in the hemisphere.

The direction of the observation point P in terms of the true orientation  $\phi$  and elevation angle  $\Theta$  is illustrated in Fig. 17. The magnitude of the total effective field strength E, as given in Eq. (15), is represented along the direction of the line from the space reference point toward the observation point P. This is for convenience in drawing polar charts.



VECTOR REPRESENTATION OF THE TOTAL FIELD INTENSITY IN SPACE

#### Fig. 17

Referring again to Eq. (16), it is seen that the phase angle of the voltage vector is a function of space phasing and time phasing. The space phasing, as discussed above, varies with the position of the observer, while the time phasing is a constant that is set by the phase angle of the voltage (or current) in the  $k^{th}$  antenna.

It is of interest to note that a pattern can be calculated for a given elevation angle which is equivalent to a horizontal pattern that has field strength vector magnitudes of the respective antennas equal to  $E_k f_k(\Theta)$  and spacings reduced to  $S_k \cos \Theta$ . This scheme of drawing patterns at the various elevation angles is a useful method for determining the

#### TABLE 2

Antenna No.	True Orientation Ø•	Spacing S <sup>•</sup>	Phasing <b>V</b> •	Horizontal Field Strength <sup>E</sup> mv/m	Vertical Radiation Characteristic f(Θ)
1					
2					
•					
•					
k					
•					
•					
n					

#### DIRECTIONAL ANTENNA PARAMETERS

vertical pattern of an equivalent non-directional antenna. All that is required to make this computation is to determine the rootmean-square value of the pattern for each elevation angle.

e. Directional Antenna Parameters. - In general this system specifies all of the parameters required to determine the shape and size of the directional antenna pattern. To be specific the system specifies:

- (1) The number of antennas in the directional antenna array,
- (2) The true orientation of each antenna from the space reference axis,
- (3) The spacing of each antenna from the space reference point,
- (4) The time phasing of the voltage (or current) in each antenna with respect to the voltage reference axis,
- (5) The horizontal field strength of each antenna,
- (6) The electrical height of each antenna, if a uniform cross-section tower, or the vertical radiation characteristic if it cannot be determined from Eq. (10).

\*-

The general scheme for specifying the parameters of a directional antenna system can be tabulated as shown in Table 2. where  $\mathbf{k} = \mathbf{k}^{\mathbf{th}}$  antenna in the array

- n = total number of antennas in the array
- $\phi^{\bullet}$  = true orientation in degrees
- $S^{\bullet} =$ spacing in degrees
- $\Psi^{\bullet}$  = phasing in degrees
- $E_{mv/n}$  = horizontal field strength in millivolts per meter
  - $f(\Theta)$  = vertical radiation characteristic
- f. Systematization of Directional Antenna.

(1) General...A pattern numbering system has been devised which furnishes the antenna parameters in an orderly fashion. The first digit specifies the number of antennas in the directional antenna array. Succeeding sequences of three digits specify the orientation, spacing and phase of each antenna in the array. To simplify this numbering system, the orientation, spacing, and phase of each antenna is shifted in steps of 45 degrees. Rather than specify these steps directly in degrees, the number of degrees is divided by 45 to produce small whole numbers that can be used more conveniently in the pattern numbering system. The orientation, spacing, and phasing sequences are followed by two digit figures to specify, in percent, of the maximum lobe field strength,

the horizontal field strength from each antenna and finally the last two digits specify in percent the r-m-s field strength in the horizontal plane for the directional antenna array.

The basic idea of the pattern numbering system is illustrated in Fig. 18. Referring to this figure the first digit specifies the number of antennas and will require only 1 digit for 9 or less antennas. Each antenna in



PATTERN NUMBERING SYSTEM

#### Fig. 18

the array will require 3 digits to specify its orientation, spacing and phase plus 2 digits to specify its field strength in percent. Finally, the r-m-s field strength will require 2 digits.

On this basis the pattern number will require,

Total number of

digits in the pattern number = 1 + 3n + 2n + 2 = 5n + 3

where n = number of antennas in the array. However, if No. 1 antenna is placed at the space reference point and the phase is held at zero, the first set of three digits will always be zero. Therefore, the pattern number can be reduced by three digits if No. 1 antenna is used as the reference antenna. The first set of 3 digits will then specify the orientation, spacing and phase of No. 2 antenna with respect to No. 1 antenna. Using this modification the number of digits required will be,

Total number of digits in modified pattern number = 1 + 3(n - 1) + 2n+ 2 = 5n (18)

where n is defined in Eq. (17). On this basis a two tower systematization will require 10 digits, a three tower systematization will require 15 digits and a four tower systematization will require 20 digits. Figure 19 illustrates respectively a two, three and four tower directional antenna array using this pattern numbering system.

(2) Systematization of Two Tower Patterns...For two towers the pattern numbering system consists of a 10 digit number as shown in Fig. 19(a) and Fig. 20.

Number 1 antenna is placed at the space reference point so its orientation, spacing and phase are zero. The orientation of No. 2 antenna is made zero or true north of No. 1 antenna for all patterns. However, its spacing is varied from 45 degrees to 1,440 degrees (from 1 to 32 in the pattern numbering system) and for each placement of No. 2 tower its phase is varied from 0 degrees to 315 degrees (from 0 to 7 in the pattern numbering system). Since the orientation of No. 2 antenna is always zero the second digit of the pattern number, which is ordinarily used to specify the orientation of No. 2 antenna, is used in this particular systematization to specify the spacings which require two digits for spacings greater than 405 degrees (9  $\times$  45 = 405).

For the purpose of systematization, the magnitude of the field strength are each made equal to 50 percent of the maximum value. This results in complete nulls whenever the voltage vectors swing exactly out of phase.

(17)

The maximum field strength is 100 percent when the vectors are in phase and is represented by the outer circle of the simple polar chart. The field strength is a maximum when the two field strength vectors are exactly in phase.

In some cases, especially for very close spacings, the field strength vectors are never exactly in phase; hence, the percent field strength from each antenna must be increased above 50 percent to secure the desired 100 percent maximum value. This is illustrated by the pattern No. 2 014 129 129 69, where the percent field strength from each antenna must be 129 percent to produce a maximum field strength of 100 percent. The theoretical r-m-s value is only 69 percent.

In other cases the field strength vectors are never exactly out of phase with the result that the pattern will not have a complete null. Pattern No. 2 010 50 50 85 is an example where the minimums are very shallow.

For the two tower systematization with spacings out to four wavelengths (1440°) the number of settings of each parameter is given in Table 3.



Fig. 20



USING THE PATTERN NUMBERING SYSTEM

#### Fig. 19

#### TABLE 3

#### TWO TOWER SYSTEMATIZATION PARAMETER SETTINGS

Parameters	Ø1	S <sub>1</sub>	$\Psi_1$	Ø2	S <sub>2</sub>	$\Psi_2$	
No. Settings	1	1	1	1	32	8	

The product of the number of settings results in

> Number of two tower patterns =  $1 \times 1 \times 1 \times 1 \times 32 \times 8 = 256$  (19)

which is the number of patterns in the two tower systematization. This systematization is presented in PART II.

Since two tower patterns are so important in directional antenna work, particularly in multiplying patterns, a more detailed systematization has also been prepared and presented in PART II. In this more detailed systematization the spacing and phasing have been shifted in steps of only 15 degrees, thus making 13 patterns for each spacing. The numbering system has been altered to present the spacing and phasing in degrees instead of numbers which have to be multiplied by 45.

(3) Systematization of Three Tower Patterns... For three tower patterns the numbering system consists of a 15 digit number; however, for convenience this number is divided into two parts as shown in Fig. 19(b). The first part as shown in Fig. 21 gives the number of antennas in the system, followed by the orientation, spacing, and phase of the second and third antennas with respect to the first or reference antenna. This part of the number is located in the lower left hand corner of the pattern sheet.

The second part of the number as shown in Fig. 19(b) and Fig. 22 gives the magnitude of the various horizontal field intensities in percent of the maximum lobe field strength. For a three tower pattern each antenna will require two digits and finally two digits will be required for the r-m-s horizontal field intensity for the antenna array. This number is placed at the lower right hand corner of the pattern sheet.

NNAS	DEGREES 45	DEGREES	DEGREES	DEGREES	DEGREES	DEGREES
NUMBER OF ANTE	ORIENTATION OF	SPACING OF	PHASING OF	ORIENTATION OF	SPACING OF	PHASING OF
	NO.2 ANTENNA =	NO. 2 ANTENNA =	NO. 2 ANTENNA =	NO.3 ANTENNA =	NO. 3 ANTENNA =	NO. 3 ANTENNA =
<i>No.</i>	Ø2	5g	¥2	Ø3	53	¥3
3	0	6	7	1	6	7

LEFT HAND THREE TOWER PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA



NO. 3 ANTENNA ANTENNA SYSTEM RADIATED IN HORIZONTAL % FIELD STRENGTH RADIATED IN HORIZONTAL PLANE FROM NO.I ANTENNA PLANE FROM NO. 2 ANTENNA % FIELD STRENGTH RADIATED IN HORIZONTAL FIELD STRENGTH HORIZONTAL FIELD STRENGTH STRENGTH STRENGTH PLANE FROM FROM z RADIATED % FIELD % RMS PLANE E3 E Ee Eo 48 35 30 49

RIGHT HAND THREE TOWER PATTERN NUMBER GIVES ANTENNA FIELD INTENSITY DATA IN PERCENT

#### Fig. 22

For the purpose of systematization of three tower patterns, No. 1 tower is located at the space reference point, then its orientation, spacing and phase can be considered zero and thus be deleted from the pattern numbering system. Number 2 tower, for convenience, can be located due north of No. 1 tower; hence, its orientation  $\phi_2$ , will always be zero. The spacing, S<sub>2</sub>, can be varied from 45 degrees to 360 degrees (from 1 to 8 in the pattern numbering system) and the phasing  $\Psi_2$ , for each placement of the towers can be varied from 0 degrees to 315 degrees (from 0 to 7 in the pattern numbering system).

Number 3 tower orientation,  $\phi_3$ , will vary from 0 degrees to 315 degrees (0 to 7 in the pattern numbering system). The spacing,  $S_3$ , will vary from 45 degrees to 360 degrees (from 1 to 8 in the pattern numbering system). The phasing,  $\Psi_3$ , for each placement of the towers will vary from 0 degrees to 315 degrees (from 0 to 7 in the pattern numbering system).

The restrictions placed on the field strength from the respective antennas is in general that they add up to produce a maximum of 100 percent in at least one direction and that they completely cancel in at least one other direction. The suggested procedure for accomplishing this is to at first make the field strength from all three antennas equal, then inspect the pattern for minimums. With the orientation that gives the lowest minimum the magnitude of the respective field strength can be adjusted for a null if possible. This is usually accomplished by increasing a field strength that produces a lower minimum. Usually a little manipulation of the field strength magnitudes and perhaps a slight change in orientation will result in the required null.

This procedure eliminates the field strength as parameters in the systematization. If this was not done the number of patterns required would soon become prohibitive. It is believed that this procedure is a good compromise because it gives complete nulls in most cases. Of course when there are several possible nulls it would be desirable to present patterns for each of them.

For the three tower systematization with spacings out to one wavelength (360°) the total number of settings is given in Table 4.

The product of the number of settings results in, Number of three tower settings =  $1 \times 1 \times 1 \times 1 \times 8 \times 8 \times 8 \times 8 \times 8 = 32,768.$  (20)

#### **TABLE 4**

#### THREE TOWER SYSTEMATIZATION PARAMETER SETTINGS

Parameter	Ø1	S <sub>1</sub>	$\Psi_1$	Ø2	S <sub>2</sub>	$\Psi_2$	Ø3	S <sub>3</sub>	$\Psi_3$
No. Settings	1	1	1	1	8	8	8	8	8

The systematization placement chart is illustrated in Fig. 23. A study of this chart and the systematization problem reveals that several things can be done to decrease the number of patterns, and thus eliminate duplications.



THREE TOWER SYSTEMATIZATION PLACEMENT CHART

#### Fig. 23

The number of patterns in the three tower systematization is decreased by

(a) Eliminating the cases where No. 3 tower falls on No. 2 tower. These cases actually result in two tower directional antenna patterns as given in Part II.

The number of patterns eliminated from the three tower systematization by using the two tower patterns is given in Table 5.

#### TABLE 5

### NUMBER OF TWO TOWER SETTINGS ELIMINATED FROM THE THREE TOWER SYSTEMATIZATION

Parameters	Ø1	S <sub>1</sub>	$\Psi_1$	Ø2	S <sub>2</sub>	$\Psi_2$	Ø3	S3	$\Psi_3$
No. Settings	1	1	1	1	1	8	1	8	8

Performing the multiplication indicated in Table 5 gives,

Number of two tower patterns eliminated =  $1 \times 1 \times 1 \times 1 \times 1 \times 8 \times 1 \times 8 \times 8 = 512$  (21)

In Table 5,  $S_2$  and  $S_3$  step along together making a total of 8 settings when  $\phi_3 = 0$ .

(b) Eliminating all three tower patterns in line which are the duplicate of another placement of the towers even though the pattern is turned around 180°.

Number of three tower patterns eliminated =  $84 \times 8 \times 8 = 5,376$  (22)

(c) Eliminating the cases where No. 2 and No. 3 towers have the same spacing and orientation. For this case the orientation of No. 3 tower for 225, 270 and 315 degrees which corresponds to  $\phi_3 = 5$ , 6 and 7 in the pattern numbering system can be omitted from the systematization. These placements can be exactly duplicated when the orientation of No. 3 tower is 135, 90 or 45 degrees, respectively. The only difference is that the whole pattern will be rotated. This sort of restriction has been placed upon both the two and three tower systematizations when No. 2 tower was arbitrarily placed due north of No. 1 tower. It would be foolish, for example, to present all of the same two tower patterns eight times, the only difference being that the patterns would be rotated in steps of 45 degrees as the orientation of No. 2 tower is varied from 0 to 315 degrees.

Performing the indicated multiplications,

Number of three tower patterns eliminated (by not using  $\phi_3 = 5$ , 6 or 7 when  $S_2 = S_3$ ) =  $1 \times 1 \times 1 \times 1 \times 1 \times 8 \times 3 \times 8 \times 8 = 1,536$  (23) NUMBER OF THREE TOWER SETTINGS ELIMINATED FROM THE SYSTEMATIZA-TION BY NOT USING  $\phi_3 = 5$ , 6 OR 7 WHEN S<sub>2</sub> = S<sub>3</sub>

TABLE 6

Parameters	Ø1	S1	$ \Psi_1 $	Ø2	S <sub>2</sub>	$ \Psi_2 $	Ø3	S <sub>3</sub>	Ψ3
No. Settings	1	1	1	1	1	8	3	8	8

(d) Another reduction in the total number of patterns could be achieved by eliminating all image patterns. For example, when  $S_2$ = 90° and  $S_3 = 180°$  the patterns produced when  $\phi_3 = 315^{\circ}$  is the image of the patterns produced when  $\phi_3 = 45^{\circ}$ . This was not done in the systematization because of the difficulty of visualizing the shape of the image patterns, or actually having to supply a mirror with the pattern book and having to explain how to write the pattern number. The production of the image patterns was accomplished by printing image patterns and deleting the numbers. The image patterns are then presented on the left hand side of the page opposite the original set of patterns from which the images were made. The pattern number of the respective image pattern is the same as the original with the exception of the orientation. The orientation of the image pattern is such that if the systematization placement chart is folded along the north-south line through No. 1 and No. 2 towers the location of No. 3 tower for the image pattern will coincide with the location of No. 3 tower of the original pattern.

(e) The elimination of three tower patterns which are duplicates of original or image patterns but shifted in orientation amounts to 10,752 patterns. For example when  $\phi_3 = 1$ the patterns produced when  $S_2 = 1$  and  $S_3 = 2$ is the same as for the case when  $\phi_3 = 7$  with  $S_3 = 1$  and  $S_2 = 2$  with the exception that the patterns are rotated 45 degrees counterclockwise. For each value of the orientation,  $\phi =$ 1, 2, 3, 5, 6 and 7, there are 28 placements that are duplications of this nature. The number of patterns eliminated are then Number of three tower patterns eliminated by not duplicating patterns shifted in orientation =  $6 \times 28 \times 8 \times 8 = 10,752$  (24)

After eliminating these various types of duplications as given in Eqs. (21), (22), (23) and (24), the resulting number of patterns is,

Substituting values,

$$32,768 - 18,176 = 14,592$$
 (25)

Dividing this number by 64 gives 228 pages of patterns as furnished in Part III of this book.

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ELECTRO-MECHANICAL DIRECTIONAL ANTENNA PATTERN CALCULATOR FIG. A



(q) MAGNITUDE CONTROL AND TURNTABLE PANELS



(b) TURNTABLE AND COSINE GENERATOR PANELS CLOSE-UP VIEWS OF CALCULATOR

FIG. B



SYSTEMATIZATION OF

TWO TOWER PATTERNS

This section furnishes 568 patterns as described on page 1.19 of Part 1, "Theory and Application."

256 of these patterns are general patterns with spacings out to four wavelengths, while 312 are detailed patterns for spacings out to one wavelength. The general patterns are for spacings in steps of 45 degrees and phasings in steps of 45 degrees. The detailed patterns are for spacings in steps of 15 degrees and phasings in steps of 15 degrees. The phasings are only presented from 0 to 180 degrees since the same patterns, oriented 180 degrees, result for phasings from 180 degrees to 360 degrees. This is readily observed by inspecting the general patterns which present the phasings.

Directional

Antenna

Patterns



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THREE TOWER PATTERNS

SYSTEMATIZATION OF

This section furnishes 14,592 patterns, as described on page 1.20 of Part 1, "Theory and Application."

There are 228 placements (pages) of the three towers to cover spacings out to one wavelength. For each placement of the towers there are 64 different phasings presented. The field strengths were eliminated as parameters by making magnitude adjustments to give at least one maximum of 100 percent and where possible, at least one null.

Directional

Antenna

Patterns



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PLACEMENT AND PHASING DATA.

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LEFT HAND PATTERN NUMBER GIVES ANTENNA

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PATTERN NOMENCLATURE

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 $\psi_3$ 

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RIGHT HAND PATTERN NUMBER

GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

Eo

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↓3 = PHASING OF ANTENNA No. 3 IN DEGREES 3.5 °, 45° 90° 135° 225° 180 270° 315° 0°-0 45° 1  $\psi_{Z}$  = PHASING OF ANTENNA No. 2 IN DEGREES 214151 501105 DEGREES 4 90° 2  $\psi_{2}$  = PHASE PATTERN NUMBER = 10130 135° 7 180º 225° 5 2343740 270° 6 1144574 4164172 2154272 1016155 b18:262 17415 315 - 7 H1705 914475 16516 101705 165175 10170 174778 30170 3134474 5+17056 351 54465 3615455 301705 2 3 4 5 0 6 DEGREES 45  $\psi_3$  = PHASE PATTERN NUMBER = 0 % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 1 ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 45 42 4 5 45 NUMBER OF ANTENNAS SPACING OF NO. 3 ANTENNA = NO.2 ANTENNA = . á ORIENTATION OF NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA . IN THE SYSTEM PHASING OF NO. 3 ANTENNA SPACING OF NO. 2 ANTENNA PHASING OF 5 NO. Ø2 Se E2 E3 Ø3 53 42 EI EO 43 3 65 0 1 0 0 5 0 23 24 47 4 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER PLACEMENT AND PHASING DATA. GIVES ANTENNA FIELD INTEN-SPOTS LOCATE THE ANTENNAS FOR SITY DATA IN PERCENT.

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 $\psi_3$  = PHASING OF ANTENNA No. 3 IN DEGREES

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LEFT HAND PATTERN NUMBER GIVES ANTENNA

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SITY DATA IN PERCENT.

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3,61  $\psi_3$  = PHASING OF ANTENNA No. 3 IN DEGREES 225 o° 315 270° 90° 135° 180 45° 0°--0 1620135 1020132 1111103 3020133 12128 102013 A12128 45°  $\psi_{\mathcal{E}}$  = PHASING OF ANTENNA No. 2 IN DEGREES ALLALD -02113 2191289 .02113 2141280 12113 121087 .02113 : 180 102113 3121182 3021132 1218 ₩2 = PHASE PATTERN NUMBER = DEGREES 2 90<sup>2</sup> ...... 135 111291 102513 1421112 103818 3623134 121081 180° 5 225° 013187 13117 1025138 2191271 .02518 151.207 141180 6 270° 1111 151088 302613 12108 51(1180 .7 315° 313 13120 512128 7 6 4 5 0 2 3  $\psi_{3}$  = PHASE PATTERN NUMBER =  $\frac{\text{Degrees}}{45}$ % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. 0 % FIELD INTENSITY RADIATED IN MORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES 45 DEGREES PHASING OF DEGREES DEGREES DEGREES DEGREES 45 42 40 45 45 NUMBER OF ANTENNAS NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA = = NO. 2 ANTENNA = ORIENTATION OF NO. 3. ANTENNA = IN THE SYSTEM SPACING OF NO. 2 ANTENNA PHASING OF SPACING OF E2 Ø3 53 EI E3 Eo NO 43 \$2 S2 ¥2 5 77 12 90 2 3 0 12 3 0 0 ï 80 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA SITY DATA IN PERCENT. SPOTS LOCATE THE ANTENNAS FOR THIS PAGE OF PATTERNS IN THE NOMENCLATURE PATTERN SYSTEMATIZATION PLACEMENT CHART,

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*ψ*<sub>3</sub> = PHASING OF ANTENNA No. 3 IN DEGREES 3.75 0° 270° 315° 180° 90° 135° 225° 45° 0 o-03015 1 45°  $\psi_2$  = PHASING OF ANTENNA No. 2 IN DEGREES 203135 21 3260  $\psi_2$  = PHASE PATTERN NUMBER = DEGREES 2 90°-135-3 13115 180° 5 225° 311305 2175260 303:15 6 270 91933 7 315 52202655 41144354 3037150 3637151 3037152 3037153 42173172 3037154 3037156 5425254 40143963 47163274 3037155 51272474 58282676 3037157 6 7 3 4 5 0 2 DEGREES W3 = PHASE PATTERN NUMBER = 45 % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. 0 % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO, 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 43 45 4 42 45 NUMBER OF ANTENNAS IN THE SYSTEM NO. 3 ANTENNA = -ORIENTATION OF NO.2 ANTENNA = SPACING OF NO.2 ANTENNA = NO. 2 ANTENNA = NO.3 ANTENNA = ORIENTATION OF SPACING OF NO. 3 ANTENNA PHASING OF PHASING OF E2 E3 Eo Ø2 Se Ø3 53 43 EI NO. 42 42 60 3 5 0 51 25 3 0 0 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA. SITY DATA IN PERCENT. SPOTS LOCATE THE ANTENNAS FOR NOMENCLATURE

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PATTERN NOMENCLATURE





 $7_{0}^{8}$   $6_{0}^{6}$   $8_{0}^{6}$  $8_{$ 

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45°

90°

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 $\psi_3$  = PHASING OF ANTENNA No. 3 IN DEGREES

180

225°

135°

3.85

DEGREES

 $\psi_2$  = PHASE PATTERN NUMBER =

315°

270°





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SYSTEMATIZATION PLACEMENT CHART,





 $\psi_3$  = PHASING OF ANTENNA No. 3 IN DEGREES

3.89

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NO.

3

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SYSTEMATIZATION PLACEMENT CHART,

3.91



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PATTERN NOMENCLATURE 3.97



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 $\psi_3$  = PHASING OF ANTENNA No. 3 IN DEGREES 3.101 135° 225° o° 45° 90° 180 270° 315° 0°-0 45°  $\psi_{\mathcal{L}}$  = PHASING OF ANTENNA No. 2 IN DEGREES DEGREES 4.5 90° 2  $\psi_{\mathcal{L}}$  = PHASE PATTERN NUMBER = 135° 3 180° 225° 5 270°-6 .7 315° 46341364 3077187 ATT185 1121265 837176 341857 9341755 34372055 -07718 .42210 47718 7 0 2 3 4 5 6  $\psi_{3}$  = PHASE PATTERN NUMBER = DEGREES % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL, PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA, % FIELD INTENSITY RADIATED IN HORIZONTAL PLÂNE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 45 4 5 45 0 45 NUMBER OF ANTENNAS -NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA = SPACING OF NO. 2 ANTENNA = PHASING OF NO. 2 ANTENNA = NO.3 ANTENNA = ORIENTATION OF IN THE SYSTEM NO. 3 ANTENNA SPACING OF PHASING OF E3 NO Øz Se Ø3 53 43 EI E2 Eo 42 61 7 0 8 0 21 31 45 3 0 1 4 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA. SPOTS LOCATE THE ANTENNAS FOR SITY DATA IN PERCENT. THIS PAGE OF PATTERNS IN THE

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3.103



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NOMENCLATURE

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SITY DATA IN PERCENT.

PATTERN



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3.107



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43 = PHASING OF ANTENNA No. 3 IN DEGREES 3.109 45° 225° o° 90° 135° 180° 270° 315° 0°-0 45° 1 ₩2 = PHASING OF ANTENNA NO. 2 IN DEGREES DEGREES 45 90°-2  $\psi_{\mathcal{E}}$  = PHASE PATTERN NUMBER = 135-3 180º 225° 5 270°-.6 .7 315 33134269 37144370 4124671 31144760 0134560 1154565 3467.08 108728 308728 3087283 16 7 0 2 3 4 5 DEGREES 45 ₩3 = PHASE PATTERN NUMBER = % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO.3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. SPACING OF NO. 2 ANTENNA = DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 45 45 45 45 NUMBER OF ANTENNAS 11 NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA . NO. 2 ANTENNA = NO. 3. ANTENNA = ORIENTATION OF IN THE SYSTEM NO. 3 ANTENNA 6 PHASING OF SPACING OF PHASING OF 53 W3 Eo NO. Ø2 Se Ø3 E, E2 E3 5 42 16 69 0 28 45 3 0 8 0 2 8 80 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA. SPOTS LOCATE THE ANTENNAS FOR SITY DATA IN PERCENT.

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E2

22

E3

48

Eo

58

Se NO. Ø3 Ø2 53 43 EI 42 0 6 3 0 4 0 25 1 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA. GIVES ANTENNA FIELD INTEN-SITY DATA IN PERCENT.

> PATTERN NOMENCLATURE

SPOTS LOCATE THE ANTENNAS FOR THIS PAGE OF PATTERNS IN THE SYSTEMATIZATION PLACEMENT CHART,

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303



RIGHT HAND PATTERN NUMBER GIVES ANTENNA FIELD INTEN-SITY DATA IN PERCENT.

PATTERN NOMENCLATURE

LEFT HAND PATTERN NUMBER GIVES ANTENNA

PLACEMENT AND PHASING DATA.

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PATTERN NOMENCLATURE

3.119



3.121 ₩3 = PHASING OF ANTENNA No. 3 IN DEGREES 225° o° 90° 135 180 270° 315° 45° 0°-0 45° ₩2 = PHASING OF ANTENNA No. 2 IN DEGREES DEGREES 45 2 90  $\psi_2$  = PHASE PATTERN NUMBER = 135-3 4 180 5 225° 472 55 1 270°-6 .7 315 01727 264067 501727 161727 301727 19314167 3017277 1930406 498859 30:22 17 3 6 0 2 4 5  $\psi_3$  = PHASE PATTERN NUMBER =  $\frac{\text{Degrees}}{45}$ % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO.3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DECREES 4.0 40 40 45 42 40 NUMBER OF ANTENNAS . = = NO.2 ANTENNA = ORIENTATION OF ORIENTATION OF NO. 3 ANTENNA = IN THE SYSTEM PHASING OF NO. 2 ANTENNA NO. 3 ANTENNA NO. 3 ANTENNA NO. 2 ANTENNA 6 PHASING OF SPACING OF SPACING OF Eo Ø2 Se 53 E2 E3 NO Ø3 EI 3 43 5 42 80 47 72 7 31 0 0 2 0 16 3 1 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA. SPOTS LOCATE THE ANTENNAS FOR SITY DATA IN PERCENT.

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SYSTEMATIZATION PLACEMENT CHART,

PATTERN NOMENCLATURE 3.123



SITY DATA IN PERCENT.

PATTERN NOMENCLATURE

₩3 = PHASING OF ANTENNA No. 3 IN DEGREES 3.125 90° 225° 315 o° 135 180° 270° 45° o-0 75376 45° = PHASING OF ANTENNA No. 2 IN DEGREES 12 8 26.1 1111262 DEGREES 45 2 90°-PHASE PATTERN NUMBER = 123.26 135-3 1:232 4 180º 424262 . 42 5 225° 42 302523 33333358 343-344 w25232 30333663 M2425 6 31 36.50 13455 allars. - 6 270° 313160 32326 1.156.1 313155 1313152 131315 פתונונ .7 315°-\$2723 131316 14313063 11313162 312723 -7 5 6 0 3 4 ź  $\psi_{3}$  = PHASE PATTERN NUMBER =  $\frac{\text{Degrees}}{45}$ % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. 0 % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 40 45 45 45 45 NUMBER OF ANTENNAS FIELD INTENSITY si 11 ORIENTATION OF NO.2 ANTENNA = PHASING OF NO. 2 ANTENNA = ORIENTATION OF NO. 3 ANTENNA = -IN THE SYSTEM PHASING OF NO. 3 ANTENNA NO. 3 ANTENNA SPACING OF NO. 2 ANTENNA SPACING OF Eo E3 EI E2 NO. Ø2 Se Ø3 53 43 42 80 39 78 40 2 0 2 3 0 39 3 0 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA SITY DATA IN PERCENT.

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3.127



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W3 = PHASING OF ANTENNA No. 3 IN DEGREES 3.131 o° 45 90° 135 225° 315° 180 270° 0°-0 45° 1 ₩2 = PHASING OF ANTENNA No. 2 IN DEGREES DEGREES 2  $\psi_2$  = PHASE PATTERN NUMBER = 3 5 453153 270° 6 315 7 3427266 2027485 102726 2721-859 7204573 0 3 2 7 4 5 6  $\psi_{3}$  = PHASE PATTERN NUMBER =  $\frac{\text{Degrees}}{45}$ 0 % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 4 5 45 45 42 NUMBER OF ANTENNAS 11 NO. 3. ANTENNA = .. NO. 2 ANTENNA = ORIENTATION OF NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA = IN THE SYSTEM PHASING OF NO. 3 ANTENNA SPACING OF NO.2 ANTENNA PHASING OF SPACING OF 53 Eo NO. Ø2 Se Ø3 43 ¥2 EI E2 E3 3 0 2 0 2 6 36 25 51 67 0 4 RIGHT HAND PATTERN NUMBER

LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA

SITY DATA IN PERCENT. PATTERN NOMENCLATURE

GIVES ANTENNA FIELD INTEN-

45

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LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA.

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315° o° 45° 90° 225° 135° 180° 270 0°-0 45  $\psi_{Z}$  = PHASING OF ANTENNA No. 2 IN DEGREES 2 90°-135 3 180º 5 225° 7145 32116 6 270°-162155 13:2 -7 315° 52262363 224365 48232166 343725 3037:52 0322765 303725 9242168 232970 M 1725 \$222072 M3725 28251.5 10 17252 303725 M3725 +7 6 0 2 3 4 5 DEGREES W3 = PHASE PATTERN NUMBER = 45 % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. 0 % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HQRIZONTAL PLANE FROM NO.3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 4 45 45 40 45 NUMBER OF ANTENNAS SPACING OF NO. 2 ANTENNA = = PHASING OF NO. 3 ANTENNA = PHASING OF NO. 2 ANTENNA = NO. 3. ANTENNA = NO.2 ANTENNA . ORIENTATION OF ORIENTATION OF IN THE SYSTEM NO. 3 ANTENNA 6 SPACING OF E, E2 E3 Eo NO. Se Ø3 53 43 Ø2 42 5 80 5 45 24 63 62 0 2 3 0 3 0 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA 4 PLACEMENT AND PHASING DATA. GIVES ANTENNA FIELD INTEN-

 $\psi_{3}$  = PHASING OF ANTENNA No. 3 IN DEGREES

3.139

DEGREES 45

₩2 = PHASE "PATTERN NUMBER =

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PATTERN NOMENCLATURE

W3 = PHASING OF ANTENNA No. 3 IN DEGREES 3.145 225° 315° o° 90° 135° 180° 270° 45 0°-0 45°  $\psi_{\mathcal{L}}$  = PHASING OF ANTENNA No. 2 IN DEGREES  $\psi_{2}$  = PHASE PATTERN NUMBER = DEGREES 90°-2 \$2453 135-3 35335 42216 4 180° 5 225° - 6 270°--7 315°-1038 101.26 3 7 0 2 6 4 5 DEGREES  $\psi_3$  = PHASE PATTERN NUMBER = 45 % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. 0 % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 45 4 5 45 40 NUMBER OF ANTENNAS SPACING OF NO. 3 ANTENNA = NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA = -NO. 3. ANTENNA = PHASING OF NO. 2 ANTENNA = ORIENTATION OF IN THE SYSTEM SPACING OF NO. 2 ANTENNA PHASING OF E, E2 E3 Eo S2 Ø3 53 NO. Ø2 42 43 27 64 2 8 21 40 3 0 3 0 0 80 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA. SPOTS LOCATE THE ANTENNAS FOR SITY DATA IN PERCENT.

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PATTERN

NOMENCLATURE

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36

RIGHT HAND PATTERN NUMBER

GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

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36

59

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PATTERN NOMENCLATURE

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LEFT HAND PATTERN NUMBER GIVES ANTENNA

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PLACEMENT AND PHASING DATA.



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₩3 = PHASING OF ANTENNA No. 3 IN DEGREES 3.153 225° 45° 90<sup>°</sup> 135° 270° 315 o° 180 o-0 45° · 1 # PHASING OF ANTENNA No. 2 IN DEGREES DEGREES 2 90°  $\psi_{2}$  = PHASE PATTERN NUMBER = 135°-3 4 (80° 5 the second 225° 270°-6 7 315° 3313558 304728 362451 423845 304728 30472 551346 3141304 +7 6 3 5 0 2 4  $\psi_3 = \text{PHASE PATTERN NUMBER} = \frac{\text{DEGREES}}{45}$ % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO.3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 40 45 54 40 40 42 NUMBER OF ANTENNAS NO. 3 ANTENNA = = IÍ ORIENTATION OF NO.2 ANTENNA = đ PHASING OF NO. 2 ANTENNA = ORIENTATION OF IN THE SYSTEM NO. 3 ANTENNA NO. 3 ANTENNA SPACING OF NO. 2 ANTENNA PHASING OF SPACING OF E3 Eo 53 EI E2 Ø2 Ø3 NO Se 42 43 39 30 61 2 8 0 30 3 0 4 0 вÒ 4 LEFT HAND PATTERN NUMBER GIVES ANTENNA RIGHT HAND PATTERN NUMBER GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA

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PATTERN NOMENCLATURE

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PATTERN NOMENCLATURE

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E2

33

SITY DATA IN PERCENT.

E3

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RIGHT HAND PATTERN NUMBER GIVES ANTENNA FIELD INTEN-

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3.157



E2

17

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46

E3

26

RIGHT HAND PATTERN NUMBER

GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

Eo

63



ORIENTATION OF NO. 2 ANTENNA = SPACING OF NO. 2 ANTENNA S2 NO. Ø2 3 0 5

LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA.

PHASING OF

42

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PATTERN NOMENCLATURE

53

8

Ø3

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PHASING OF

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02 3 80 4

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3,159



GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

SPOTS LOCATE THE ANTENNAS FOR THIS PAGE OF PATTERNS IN THE SYSTEMATIZATION PLACEMENT CHART,

PATTERN NOMENCLATURE

PLACEMENT AND PHASING DATA.



PLACEMENT AND PHASING DATA.

SPOTS LOCATE THE ANTENNAS FOR THIS PAGE OF PATTERNS IN THE SYSTEMATIZATION PLACEMENT CHART,

PATTERN NOMENCLATURE

GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

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PATTERN NOMENCLATURE

PLACEMENT AND PHASING DATA.



3 0 6 0 2 8 LEFT HAND PATTERN NUMBER GIVES ANTENNA PLAGEMENT AND PHASING DATA.

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₩3 = PHASING OF ANTENNA No. 3 IN DEGREES 3.175 0° 45° 90° 135° 180 225° 270° 315 0°-0 45°  $\psi z$  = PHASING OF ANTENNA No. 2 IN DEGREES 31313172 301 12 DEGREES 45 90°-2  $\psi_{\mathcal{E}}$  = PHASE PATTERN NUMBER = 135-10183 180 5 225 Se 163 270° 6 7 315 32323273 3017327 312:317 4543470 301732 30173 0504577 301732 31313177 301732 W 10117 301732 3017 301732 17 6 5 0 2 3 4  $\psi_3 = \text{PHASE PATTERN NUMBER} = \frac{\text{Degrees}}{45}$ % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES 45 DEGREES DEGREES 4 5 45 45 45 NUMBER OF ANTENNAS = NO. 3 ANTENNA = NO.2 ANTENNA = NO.3 ANTENNA = NO.2 ANTENNA = NO. 2 ANTENNA = OPIENTATION OF ORIENTATION OF IN THE SYSTEM NO. 3 ANTENNA PHASING OF SPACING OF PHASING OF SPACING OF E2 E3 Eo Ø2 Sz Ø3 53 E, 7 NO. 42 43 80 2 0 29 29 29 82 3 0 1 0 3 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA SITY DATA IN PERCENT. SPOTS LOCATE THE ANTENNAS FOR

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SITY DATA IN PERCENT.

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PATTERN NOMENCLATURE



E3

45

RIGHT HAND PATTERN NUMBER

GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

Eo

77

EI

22

Ee

21

PATTERN NOMENCLATURE

53

8

43

0

Ø3

5

42

0

LEFT HAND PATTERN NUMBER GIVES ANTENNA

NO.

3

Ø2

0

Se

2

PLACEMENT AND PHASING DATA.

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4

03

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62

LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA.

5

0

3

0

3

PATTERN NOMENCLATURE

5

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8¢ 4

0

22

26

52

**RIGHT HAND PATTERN NUMBER** 

GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

 $\psi_{3}$  = PHASING OF ANTENNA No. 3 IN DEGREES 315° 270° 90° 135° 225° o 45° 180° 0°-0 11.1.24 1 45°  $\psi_{\mathcal{Z}}$  = PHASING OF ANTENNA No. 2 IN DEGREES ₩2 = PHASE PATTERN NUMBER = DEGREES 2 90° 3 135-1 180° 2650 5 225 6 270°-21414 -7 315 1224 247 22264160 30373 503735 427405 12647 276155 4.17 17 4 5 -6 3 0 2 1  $\psi_{3}$  = PHASE PATTERN NUMBER =  $\frac{\text{DEGREES}}{AE}$ % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HÖRIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 42 45 40 45 40 45 NUMBER OF ANTENNAS --NO. 2 ANTENNA = ORIENTATION OF 18 ORIENTATION OF NO.2 ANTENNA = NO.3 ANTENNA = IN THE SYSTEM SPACING OF NO. 3 ANTENNA NO. 3 ANTENNA SPACING OF NO.2 ANTENNA PHASING OF PHASING OF 6 E3 Eo E, E2 Se Ø3 53 43 Ø2 42 3 NO 5 62 52 26 22 3 0 3 5 0 3 0 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA 4 GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA SITY DATA IN PERCENT.

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NOMENCLATURE PATTERN

3,203

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RIGHT HAND PATTERN NUMBER GIVES ANTENNA FIELD INTEN-

SITY DATA IN PERCENT.

LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA.

PATTERN NOMENCLATURE

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0° 45 = PHASING OF ANTENNA No. 2 IN DEGREES 90 135-54333 180° 42 225 10353 270°-315 4234562 303737 343737 28284 26 726405 3 0 2 4 5 DEGREES 45  $\psi_3$  = PHASE PATTERN NUMBER = O Qe DEGREES 45 DEGREES DEGREES DEGREES DEGREES DEGREES 42 45 45 45 NUMBER OF ANTENNAS NO. 3 ANTENNA = PHASING OF NO. 3 ANTENNA = 1 11 NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA = ORIENTATION OF IN THE SYSTEM NO. 2 ANTENNA SPACING OF NO. 2 ANTENNA PHASING OF SPACING OF Se 42 53 NO Ø3 Ø2 43

90°

3 3 0 3 7 0 LEFT HAND PATTERN NUMBER GIVES ANTENNA PLACEMENT AND PHASING DATA.

*ψ*<sub>3</sub> = PHASING OF ANTENNA No. 3 IN DEGREES

180°

225°

270°

135°

3.207

0

I.

DEGREES 45

NUMBER =

 $\psi_2 = PHASE PATTERN$ 

2

3

5

- 6

-7

% RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM.

Eo

74

1925476

23234464 5437377

% FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA.

E2

25

SITY DATA IN PERCENT.

% FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA.

E3

51

RIGHT HAND PATTERN NUMBER

GIVES ANTENNA FIELD INTEN-

6

% FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA.

EI

25

14324

16 204

-----

315°

SPOTS LOCATE THE ANTENNAS FOR THIS PAGE OF PATTERNS IN THE SYSTEMATIZATION PLACEMENT CHART.

80

4

PATTERN NOMENCLATURE

0

o°

45°

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SITY DATA IN PERCENT.

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SYSTEMATIZATION PLACEMENT CHART,

PATTERN NOMENCLATURE

3.209



 $\psi_3$  = PHASING OF ANTENNA No. 3 IN DEGREES o° 45° 90° 135 225° 315° 180° 270° 0°-0 12125 45° 1 W2 = PHASING OF ANTENNA No. 2 IN DEGREES 333255 304135 31325 42275 DEGREES 90°-2  $\psi_{\mathcal{L}}$  = PHASE PATTERN NUMBER = 135-3 402 is . 304335 180° 1 2383252 314261 224416 2.345 225° 5 04535 5124846 4264857 384535 9215871 4155079 304535 8235068 \$373058 270° 6 43235 61 225 687261 442562 9351467 1243359 1314447 \$04635 315° 7 27345 52(3755 29365 2285 3047357 45203452 -3 6 17 2 4 ò 5  $\psi_{3}$  = PHASE PATTERN NUMBER =  $\frac{\text{Degrees}}{45}$ 0 % RMS FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM ANTENNA SYSTEM. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 2 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. 3 ANTENNA. % FIELD INTENSITY RADIATED IN HORIZONTAL PLANE FROM NO. I ANTENNA. DEGREES DEGREES DEGREES DEGREES DEGREES DEGREES 45 40 45 40 45 45 NUMBER OF ANTENNAS . -. = PHASING OF NO. 2 ANTENNA = ORIENTATION OF NO. 3 ANTENNA = ORIENTATION OF NO.2 ANTENNA = IN THE SYSTEM PHASING OF NO. 3 ANTENNA NO. 3 ANTENNA SPACING OF NO. 2 ANTENNA SPACING OF 0's E3 Eo NO. Ø2 Se 53 E, E2 3 42 Ø3 43 5 3 4 0 3 5 63 31 30 59 0 0 89 4 RIGHT HAND PATTERN NUMBER LEFT HAND PATTERN NUMBER GIVES ANTENNA GIVES ANTENNA FIELD INTEN-PLACEMENT AND PHASING DATA SPOTS LOCATE THE ANTENNAS FOR SITY DATA IN PERCENT.

PATTERN NOMENCLATURE

3.211

45

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GIVES ANTENNA FIELD INTEN-SITY DATA IN PERCENT.

RIGHT HAND PATTERN NUMBER

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PLACEMENT AND PHASING DATA.



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