

JUNE 1960

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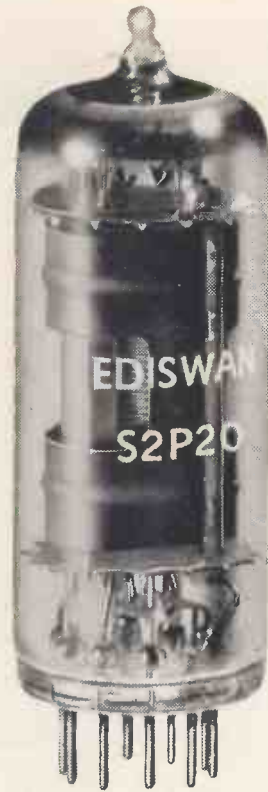
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Wireless World

ELECTRONICS, RADIO, TELEVISION

JUNE 1960

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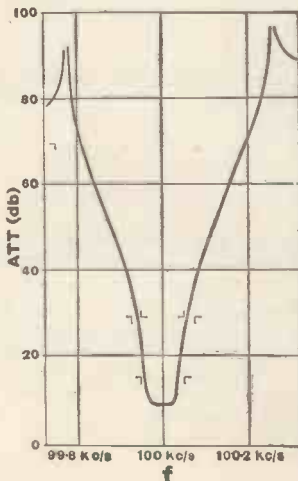
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The Universal Language

IF circuit diagrams are the universal language of electronics it is only right and proper that they should have a standardized grammar. Without this, communication becomes difficult. On the other hand, it is unreasonable to expect all who use the same grammar to speak with the same accent.

We are delighted with the lively discussion in our correspondence columns resulting from L. H. Bedford's letter on circuit conventions in the April issue. It is a subject on which everyone feels justifiably entitled to express an opinion, and on which the views of the young technician can be as sensible and worth-while as those of the experienced and highly qualified engineer. But in all these letters there does not seem to be any serious disagreement on the basic grammar of circuit drawing—only on such things as wiring cross-overs and junctions, valve envelopes and resistor "squiggles". Whether one would describe these as matters of grammar or of accent is open to question. They are certainly important to the easy reading of circuit diagrams, but not so important, we feel, as the general layout, the spacing and grouping of component symbols, the use of easily recognized configurations—and even the relative thicknesses of lines.

Several correspondents have reminded us that there is a British Standard on circuit conventions. We agree that these recommendations are an excellent guide to the draughtsman. But it is unreasonable to expect that everyone should follow B.S.530 slavishly and make all circuit diagrams look alike—just as it is unreasonable to expect a Mancunian to sound like a Londoner. The point is, surely, that circuit diagrams are drawn for very different purposes and on very different media—technical reports in laboratories, servicing manuals for technicians, wiring diagrams for the work bench, technical journals for general publication—and each of these has its own particular requirements and limitations. For practical reasons, then, the actual techniques of presentation must differ also.

In our own case (and we are often under fire on this subject), besides the general requirement of clarity and easy reading we have problems of sizing, space limitation, balance of diagrams to text and making our diagrams acceptable to people who

cannot be expected to know anything about B.S.530—Continental readers, for example. To cover new developments without delay it is often necessary to design new symbols: we cannot wait for the standardizing committees. In this way, in fact, *Wireless World* played a considerable part in developing the actual grammar of modern circuit symbolism from the old pictorial diagrams used in the early days of radio. We say this, not to pose as grey-beards, but to show that we have had a good deal of experience in evolving a system to suit the purposes of technical publication. We do not wish to impose this system on anybody else and we may well change it to keep in step with changes in electronics or technical journalism. A case in point is the transistor symbol (e.g., March, 1960, issue, p.110) on which one correspondent accuses us of being "the odd-man out". Even if we are the odd-man out, we feel quite justified in departing from the present convention (junction transistors looking like the now-obsolete point transistors) if it helps our readers and possibly has other advantages (e.g., May, 1960, issue, p.228).

Our critic on transistor symbols has a very good point, however, about the usefulness of redundancy in communicating information. This fact, if not already understood, has certainly been brought to attention by modern Communication Theory. We in the radio and electronics field therefore ought to take note of it, not only when providing the means of communication for other people, but when communicating amongst ourselves.

Third-party Messages

HAS the time come for a change in the regulations which the P.M.G. is empowered to make to protect the telecommunications monopoly which prohibits a listener, radio amateur or radio operator from passing on a message for a third party?

Legally, Bill Hayes, of the B.B.C.'s Aerial Radio Club, was breaking the law when he passed on to the police an appeal from a Moroccan amateur for drugs for the Agadir earthquake victims. So was the driver of a radio-equipped taxi who, seeing some act of violence, called his control room to notify Scotland Yard. Such acts should be not, even technically, against the law.

hi-fi

By P. P. ECKERSLEY, M.I.E.E., F.I.R.E.

*He knows what's what, he knows hi-fi;
Is not a true Fidelity.*

(Adapted)

WHAT a term! How can fidelity be high? Lack of it can stink to high heaven but that hardly justifies an opposite. Perhaps it is something raised up, usually in volume! But let that pass, "we know what we mean". In my young day we used to speak of quality, good and bad, or, if faithful is the code word, of faithful reproduction.

But do we know what we mean? I know that perfect reproduction would be that which caused a loudspeaker to create a field of sound around a listener's ear identical to that existing around the ears of an individual situated in the auditorium, studio, or whatever, where the reproduced sound originated.

The diagram of Fig. 1 helps the understanding of the definition and is an aid to an explanation why truly faithful reproduction, according to any means known to me, cannot be achieved.

For the sake of example we postulate an orchestra spread around one end of the auditorium and a microphone (M) facing it. This microphone is connected by a single channel to a loudspeaker (L) placed opposite to the listener, in the room where he listens.

Apart from any distortion that may be created by the transducers and in the channel connecting them the principle inherent artificialities, which militate against perfect reproduction (hi-fi to you) are:

1. The acoustics of the room in which the loudspeaker is situated are superimposed on those of the auditorium.

2. The source of the sounds impinging on the listener's ears is a point source, the sources of sound in the auditorium are spread over a relatively wide area.

3. A minor cause of distortion is produced because the microphone, not being the shape of a human head (and not having two ears) must in some degree alter the composition of the sound field from its form as it would be created around the ears of one listening in the auditorium.

Neglecting for a while the problem of superimposed acoustics (paragraph 1 foregoing) the artificialities of a point source of reproduction and a single microphone (as distinct from two ears) it has been suggested (and the suggestion taken up in modern equipment) that more faithful reproduction would arise by the use of so-called stereophony, consummated by the use of, typically, two microphones, two channels and two loudspeakers. Dr. Leakey has more than adequately discussed the possibilities in a recent article (April and May issues).

While it may be, and often is, claimed that two-channel reproduction is an improvement we must

nevertheless appreciate that it cannot achieve the ideal of true fidelity.

I recollect, and this, though it is related to "binaural" rather than "stereophonic" listening, may be of some academic interest, that in the very early days of broadcasting, when we transmitted opera from Covent Garden, H. J. Round set up two microphones spaced feet apart, among the footlights, and connected each one to each earpiece of a two-earpiece headphone. It was remarked that as a singer moved across the stage parallel or at some angle to the line joining the microphone he (or she) appeared to us wearing the headphone to move not from side to side but in an arc above our heads. Thus if one kept one's eyes shut one looked upwards!

One of the more dramatic effects of stereophony is the verisimilitude of movement of a sound source. Properly located in relation to the loudspeakers the listener hears an aeroplane flying over his room diagonally or a speaker appears to move from side to side. Orchestra players, however, sit still, but it is claimed that two-channel broadcasting adds realism in the sense that, for instance, the fiddlers do appear to play to one side, the wood wind to another; is there a claim for depth?

Stereo Assortments

An American friend of mine, writes to me and starts a paragraph with the words "Why Stereo?" and goes on "Dr. Harry Olson wrote an interesting paper . . ." on "the psychological response to monaural" (sic Mr. Editor) "low-fi" (sic), "monaural hi-fi" (he is unrepentant) "with several spaced speakers . . . playing the same record; binaural fringe-channel two-speaker reproduction and "filled-in" binaural hi-fi, three channel, with speakers respectively playing the left-ear channel, the right-ear channel, and (at intermediate position for the speaker) the mixed left and right-ear channels.

"The results indicate successive improvements between each of these and the preceding but very unequal steps. The big jumps were to hi-fi and spaced speakers whether two . . . or single channel."

I envy Dr. Harry Olson, he must have had a lot of fun; I would join in it more thoroughly, however, were I better acquainted than I can be, without a sight of his paper, with the meaning of some of the terms he uses.

It is time for a confession—quite simply I do not find any real improvement between any single- and any multi-channel reproduction I have heard demonstrated and I hasten to say that many, whose powers of observation and whose integrity in expressing their opinions I respect, hold different views;

I must add that some equally competent people agree with me. There is, without doubt, a difference between the two systems but to me it is no more than a difference; it is not an improvement.

I would characterize this difference as giving one a feeling that the sound from two-channel reproduction is more diffused, it is fuller than when the single channel system is compared. But, with a limited number of observations, I have remarked this same improvement when two or more loudspeakers are energized from a single-channel source. Moreover I would say that those loudspeakers which are designed to be facing the corner of a room and are responsive to single channel energization give much the same effect. It is, I repeat, a difference that I observe, and a pleasing one in some instances, but it is still artificial, reminding one of reality rather than copying it.

No! What I believe is that the primary need in improving reproduction is not so much a perfect copy of the original but rather a result, limited in certain respects as it may be, which pleases because it is free from the intrusions of the several types of non-linearities, and is unaccompanied by extraneous noise.

Art and Artificiality

This is where I mount my hobby horse and discuss art and artificiality. There is some rather involved phrase implying that the object of the artist is to conceal art. It is doubtful if artists are objective, but if the sense of the statement is that art produces emotion in those who appreciate it without the means to this end being obvious (and certainly being artificial and distinct from realism) then one can agree with a supposed meaning.

When it is seen how a two-dimensional picture can represent a three-dimensional subject, or how in statuary without loss of the value as art, dimensions are shrunk or expanded below or above those of reality then the artificiality of these forms of art are its obvious characteristics. The artist paints not what he sees but from a sub-conscious which tells his hand to register the emotion a scene conjures in it. This is not realism but it can be good art. I must say, in passing, that it would help if some painters would issue a guide to the operation of their sub-conscious; it is not always easy to join in as it were. Is it, as a final example, necessary to call attention to the artificiality of the theatre and to its impact as an art?

This may seem to have wandered a long way from hi-fi, but surely not. Surely in broadcasting there is on the one hand an artist creating a programme and upon the other the person upon whom an effect is produced and between the two a medium, a means, indeed, an artificiality, namely the technique of "reproduction." In television, as in the film, it is again the two-dimensional image that creates a three dimensional impression; in sound it is more usually the point not the diffused source which stimulates the listener's sensibilities. And provided always that these artificialities are such as to convey reality without precisely reproducing it, and provided in so doing at least some of those who look or listen are moved, and provided, in other words, their sensibilities are awakened, what more is required?

But if the artificiality of reproduction has added to it the distractions of dissonances and the peevish

introduction of irrelevant noise then its value as an art is at least reduced, in some cases destroyed. So in discussing hi-fi, I would count it of greater importance to consider chiefly the effect of the generation of harmonics, and combination tones and the presence of noise than what, in a cynical mood, I describe as the sales gimmick of stereophony.

In discussing the kind of distortion I have in mind it helps to consider the graphs of Fig. 2*. In this figure the ordinate represents pressure (a scale of decibels is also shown) and the abscissæ frequency on a log. scale. The upper full-line graph shows sound intensities at which the ear experiences pain, or "which stimulate the sensation of feeling"; the threshold of feeling is therefore the intensity at which the listener starts to experience painful sensations.

The lower graph delineates the threshold of audi-

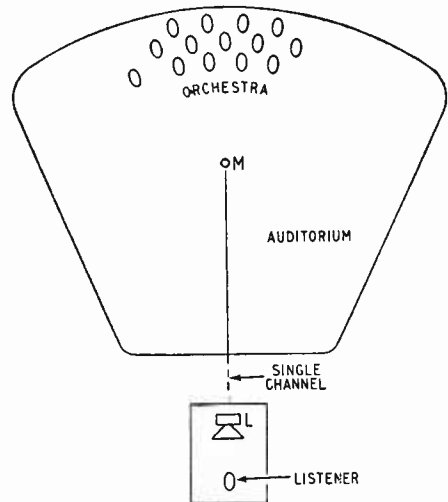


Fig. 1. Illustrating the obstacles to fidelity of reproduction.

bility, intensities less than those shown by the graph are inaudible. It is remarkable that the maximum pressure at the threshold of feeling is some 130dB greater than the minimum of audibility. The ratio of fortissimo to pianissimo of a symphony orchestra is of the order of 80dB. The contrast ratio of hi-fi reproduction is of the order of 40dB at maximum; if it were more faithful to the original with respect to contrast ratio pianissimo passages would be masked or spoiled by noise. Fi cannot be so hi as some would believe.

The upper broken-line graph in Fig. 2 is drawn to illustrate the performance of a poor quality receiver; typically one designed for medium wave reception or perhaps one of those little snarlers that use transistors and pick up anything anywhere without visible means of aerial.

In drawing the graphs of Fig. 2 we have assumed "attenuation distortion," i.e. "distortion due to variation of loss or gain with frequency"; in jargon terms the frequency characteristic is not "flat." Another assumption, alas by no means unjustified, is that there is considerable mains hum (frequency 100c/s).

The lower dotted graph illustrates a contrast ratio

* Based on Fig. 70, p. 141 of "Speech and Hearing"—Harry Fletcher, (Macmillan and Co., 1929).

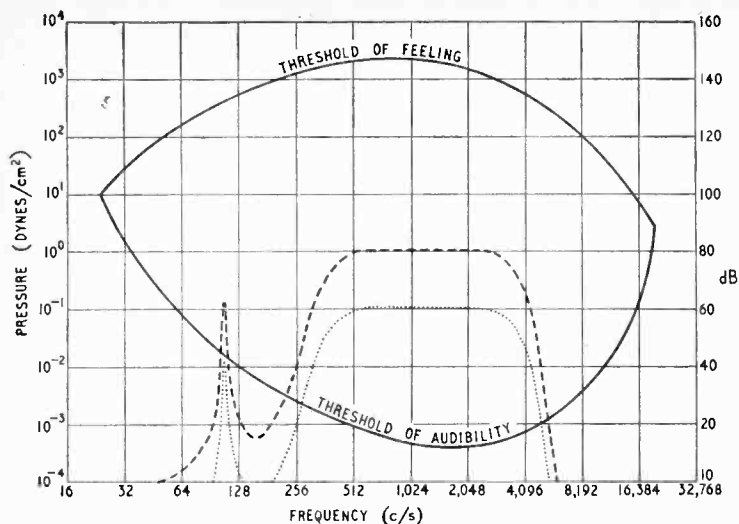


Fig. 2. Fletcher-Munson curves of the upper and lower limits of hearing, with superimposed (dotted) response curves of a poor-quality receiver at two different volume levels.

of 20dB, may be a pessimistic value, but not greatly so for medium-wave broadcasting.

We notice that the reproduction of the upper and lower frequencies varies with the volume knobs and this may explain, if it does not excuse, why the user of an inferior type of set turns up his volume. It is seen from Fig. 2 that as volume is increased so the frequency gamut is increased but now the middle frequencies must approach nearer to sensation level. The result may well be to overload the audio amplifiers with a consequent introduction of amplitude distortion "the lack of constancy of the r.m.s. value of the output of the system to that of the input at different amplitudes of the input," also of harmonic distortion "the production of harmonic frequencies at the output by the non-linearity of a network when a sinusoidal voltage . . . is applied at the input." In other words turning up the volume produces a harsh and unpleasing result marred by the introduction of spurious frequencies not existing in the original.

Noise and Bandwidth

It is also remarkable that as the volume is increased the bandwidth of reception is also increased and so any noise picked up is also increased—"the wider you open a window the more dirt that comes in." Maybe this noise is masked by the greater intensities of speech or music, while this is transmitted, but during quiet passages or during pauses noise is annoyingly audible.

Perfect quality would be represented by points lying within the lozenge-shaped area, indicated by the full lines of Fig. 2; it would demand a frequency characteristic, including the loudspeaker, which was flat between, say, 30 to 16,000c/s, freedom (to, say, 80dB) from harmonic or amplitude distortion and a contrast ratio without the introduction of noise of, say, 80dB.

There is another form of distortion which may or may not be audible, namely, phase distortion "distortion due to variation of the group velocity of the system with frequency" and, as explained later on,

a distortion associated with a Doppler effect in the loudspeaker. There is also the effects due to hangover of oscillation of the loudspeaker diaphragm. We know that if the frequency characteristics of a system is flat then the group velocity of waves transmitted through it is constant; phase change is then proportional to frequency. If, however, the effects of reactance are present, causing a variation of the ratio of the output to the input of the system with frequency, then inevitably phase distortion appears. This is why some argue that the frequency characteristic of the amplifiers in a receiver should extend to, say, 100,000c/s and then fall off gradually. In common practice cut-off is allowed just above the highest frequency it is desired to reproduce. Whether this effect, other distortions being eliminated, is audible, I do not know.

The Doppler principle is that which makes the frequency of waves

appear to change when there is a relative velocity between the wave source and the observer. Thus if a loudspeaker diaphragm is moving as a piston at a low frequency, and if it is simultaneously reproducing a higher frequency than there is, so far as the higher frequency is concerned, relative velocity between observer and source; the higher frequency is thus frequency-modulated by the lower. The degree to which the effect is audible is not known to me; it may well be negligible.

But there are more things in transducers and amplifiers than are dreamed of in some philosophies; flattening the frequency characteristic, as judged by audio oscillator and output volt-meter (electrical or acoustical) is a step on the way, but there are other side effects which this simple test cannot remark. For example, there is the hang-over of the diaphragm of a loudspeaker which, given a steep wave front, continues to oscillate long after the impulse which sets it in motion has died away. By the same token it will not immediately and therefore properly respond to a steep wave-front. These are effects which subtract from good quality by robbing music of its attack, its crispness, which when present is an engaging characteristic of good reproduction.

Obscure Distortions

There are other distortions which defy analysis; recounting an experience may illuminate my meaning.

A friend, whose judgment of quality is of a very high order, installed an allegedly hi-fi single channel radio-gramophone which, at first hearing, pleased him. The same impressive housing beautiful wood, discreet lid cushioning into place, contained tuner and turntable while a set of loudspeakers, contained in what might be described as a cupboard, radiated their output through an elegant grill.

As time passed my friend's satisfactions diminished until, thoroughly disillusioned, he decided to install a separate loudspeaker in substitution for those boxed in what I have described as a cupboard.

A change-over switch allowed a comparison. It only needed to be operated once to demonstrate excellent as compared with indifferently good quality. Incidentally, the single loudspeaker which gave the improved quality was one which faced into the corner of the room.

What can one conclude and what more when it is recounted that the substitution of the tuner and the gramophone pickup by others of different design made a further improvement? Perhaps all is not fi which is described as hi; except the latter abbreviation did truly qualify the cost of my friend's set.

I can hear my critics saying, "What after all have you said, that the elimination of harmonic, amplitude and phase distortion is essential? We hi-fi experts are quite aware of that."

I reply "Yes! But if you are why can someone buy an expensive hi-fi equipment and find it lamentably wanting and why do I and others feel that stereophony is no more than a gimmick, not a fundamental improvement?"

Another critic might exclaim, "Are you so simple as to neglect the cost factor? It's all very well to ask for a wide frequency gamut, amplifiers free from distortion, elimination of mains hum, but have you considered the cost?"

"I am," I reply, "quite aware of the cost factor and that is one reason why I have continuously and persistently (without making much impression) argued the merit of wire-broadcasting." Let me once more, in the light of the foregoing, point out its advantages with respect of reproduction.

Essentially, given a conductor, joining programme source and loudspeaker, the receiver can be simpler than when radio is used. In audio frequency technique the receiver is no more than a loudspeaker; if a carrier frequency method is essential, then the received level is not a few, but hundreds of millivolts and the receiver is consequently cheaper and gives better reproduction in spite of its decreased cost.

In sum, while I respect those who believe that

stereophony represents a major advance in the art of reproduction, my own ears fail to notice more than a difference, not an improvement. I am not alone in this belief.

The greatest step towards hi-fi would be that which concentrated on removing distortions due to non-linearities and the effects of noise from the average receiver.

A wider application of wire broadcasting would be a major advance towards hi-fi. It would also perhaps be easier, because of its facility to provide more channels, to introduce stereophony with wire rather than radio broadcasting.

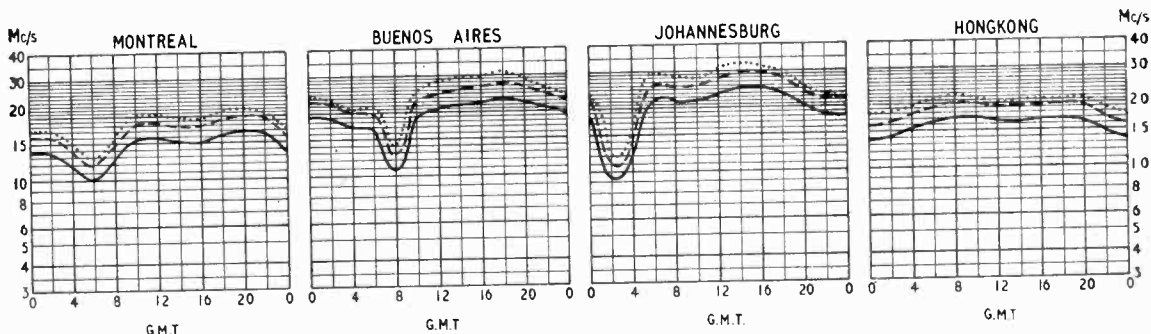
Excessive Volume

As a final and possibly "tantrumistic" contribution to the subject I must air a grievance. What is it that turns ordinary decent folk, once they get their hands on the steering wheel of a motor car or the volume knob of a loudspeaker into sadists demonstrably hating their fellow men? As one who suffers from my neighbour's ever-louder speaker, I pray that the designers of reproduction equipment should limit volume output and should not give the user the excuse to increase it by the limitation of the frequency characteristic. If I were in charge of a wire broadcasting system I would deserve the thanks of many, because I would make it impossible for the reproduced sounds to exceed a certain level. I am aware that a reduced level may subtract from realism, but then I deny the need for realism. I would and do accept limitations both of contrast level, frequency characteristic, and volume, but I cannot abide the invasion of spurious tones; I want clean reception and the crisp reproduction of transients.

Good quality, as I define it, at a lower volume than may be theoretically desirable is, as I prove whenever I listen, satisfactory, but the quality must be good quality, and the operator of the set, like me, a good neighbour.

SHORT-WAVE CONDITIONS

Prediction for June



THE full-line curves indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during June.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.

- FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE FOR 25% OF THE TOTAL TIME
- PREDICTED MEDIAN STANDARD MAXIMUM USABLE FREQUENCY
- FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE ON ALL UNDISTURBED DAYS

Noise Level Measurement in Television

Method for Use When the Video Signal is Present

By L. E. WEAVER,* B.Sc., A.M.I.E.E.

THE following method of measuring the level of random fluctuation noise in a television signal was originally developed in response to a request within the BBC for an accurate and completely objective procedure for use with camera tubes, and in particular image orthicons. It has proved to give very consistent and accurate results, and for this reason it has for some time past been adopted as the standard method of test for the acceptance and maintenance checking of these tubes.¹

Although such a measurement may seem to concern only a comparatively few specialists, in fact the manner in which the method operates, by taking advantage of certain characteristics of a television signal, is of much wider interest. It can also be applied to other random noise measurements in the television field.

Difficulty of Measurement

For the present purpose it is only necessary to explain that the principal difficulty in measuring this random noise level arises because these camera tubes can only operate while being scanned, so that their output signal always contains both scanning and random noise components. Even in the extreme case where the lens is capped and the synchronizing pulses are removed, the output signal still contains enough energy from the line and field components to frustrate any attempt to estimate the random noise by a direct measurement of the output level of the tube.

Evidently what is needed is some means for distinguishing clearly between the random noise and the signal components. The standard method hitherto achieves this by making use of the storage property of the eye and its ability to interpret

* British Broadcasting Corporation.

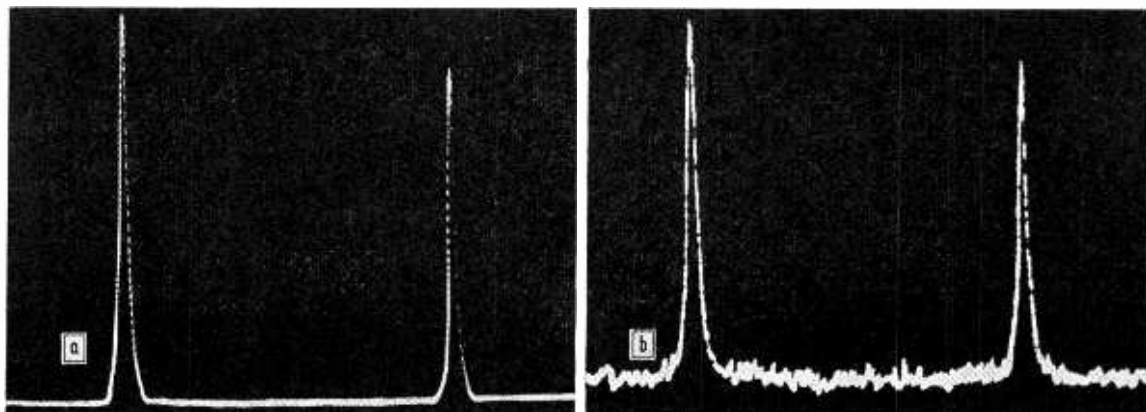
patterns. The signal is displayed on a waveform monitor and the apparent or quasi peak-to-peak noise voltage is measured separately from the signal voltage by recognizing the difference in waveform. Unfortunately there is a degree of uncertainty inherent in this method which makes it inadvisable for the present purpose. For example, the conversion factor from quasi peak-to-peak to r.m.s. noise voltage, which is the quantity required for the signal-to-noise ratio, is given values ranging from 14 to 18 dB by various authorities.

Nature of the Video Spectrum

The preferred method takes advantage of the difference in spectrum between the signal and the random noise components. It was shown by Mertz and Gray² more than a quarter of a century ago that the spectrum of a television signal is basically discontinuous, that is, in general the energy is almost entirely concentrated in the area immediately surrounding each line-frequency harmonic in the form of a rapidly decreasing series of sidebands, which originate from both the synchronizing information and the picture content. On the other hand, the spectrum of random fluctuation noise is inherently continuous, with the energy, on an average, distributed evenly over the spectrum.

This is well illustrated by Fig. 1, which shows two photographs of the same portion of the spectrum of a television signal comprising two adjacent line-frequency harmonics in the neighbourhood of 600 kc/s. Fig. 1 (a) corresponds to the original, almost noise-free, signal and (b) to the same signal but with added white noise. The resolving power of the apparatus was not sufficient to show the sidebands in detail, but their presence is indicated. The apparent erratic nature of the noise spectrum

Fig. 1. Portion of the spectrum of a television signal comprising two adjacent line-frequency harmonics: (a) original noise-free signal, (b) the same signal with added white noise.



between the harmonics is due to the fact that the sweep shows the conditions existing at a series of successive instants, and not the average condition over the area concerned.

This leads one to suppose that if it is possible to measure the energy in a narrow frequency band situated midway between two such line-frequency harmonics, the reading will be independent of the signal content and will, in fact, represent the noise power distribution with frequency in that region of the spectrum.

The simplest satisfactory way of making use of this principle in practice is shown in Fig. 2. A more refined version has already been described elsewhere³ and an improved form of this is at present under investigation.

In the "measure" position of the switch the incoming video signal is connected through a fixed attenuator pad to the input of a communications receiver, which covers the video band down to 60 kc/s and is provided with a choice of bandwidths between 6 kc/s and 100 c/s. The input circuit has been modified to provide a good 75-ohm impedance, and the pad serves to prevent overloading the receiver. The audio output terminals are connected

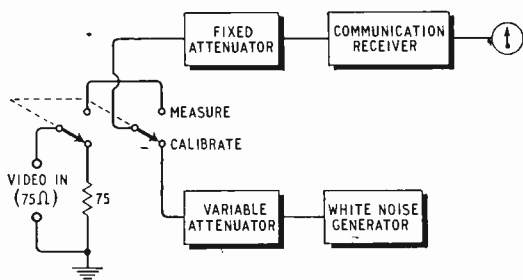


Fig. 2. Simplest technique for measurement of random noise level.

to a meter which reads a close approximation to r.m.s. values.

In the "calibrate" position of the switch the incoming signal is terminated and at the same time the receiver with its input pad is connected through a variable attenuator to a standard white-noise generator. This generator furnishes an accurately known and constant random noise power per unit of bandwidth.

Use of the Apparatus

With the switch in the "measure" position, the receiver is set to a convenient bandwidth, say 600 c/s. When it is tuned slowly through the region where a reading is required a series of sharp maxima corresponding to the line-frequency harmonics are shown on the output meter. The receiver is then tuned accurately to the exact minimum point midway between two such maxima, and the gain is adjusted until a convenient output reading is obtained.

The switch is next placed in the "calibrate" position and the setting of the fixed attenuator is varied until precisely the same reading is given by the output as in the previous instance.

When this has been achieved, the noise power per unit of bandwidth from the generator has been made the same as that existing at the point in the

video spectrum where the measurement was made. If the random noise has a flat spectrum, then a knowledge of the generator constant and the attenuator setting are sufficient to enable one to calculate the total noise power in a 3-Mc/s band, and hence the r.m.s. noise voltage. If the noise spectrum is not constant a few more readings must be taken, in most instances three or four are sufficient, and the calculation is just a little more complicated but nevertheless still very simple.

The great advantage in calibrating the receiver with the standard white-noise generator lies in the removal of two important sources of error, the variations in the pass-band of the receiver and the behaviour to noise voltages of its diode detector. The adjustment to equality of output meter reading means that the noise powers per unit bandwidth are the same in the two instances, and the shape of the receiver pass-band is therefore quite immaterial. At the same time the detector is operating at the same level with applied voltages of the same nature, and consequently no correction is needed for this effect.

A Practical Example

Suppose that when noise with a flat spectrum is measured, the attenuator reading for equality of output level is found to be 20 dB. The reference generator furnishes a noise power of $20 \mu\text{W}$ per Mc/s. Now for a picture signal amplitude of 0.7 volt peak-to-peak in a 75 ohm circuit and 3 Mc/s bandwidth the random noise power distribution corresponding to a signal-to-noise ratio of 0 dB is easily found to be $220 \mu\text{W}$ per Mc/s. The actual ratio is therefore $20 + 10 \log_{10} 220/20$ dB = 30 dB to the nearest 1 dB. In practice the added 10 dB constant would be known in advance, so that the answer would be obtained without the necessity of calculation.

When the measured spectrum is not flat a small number of readings is taken. The fact that these are expressed in power per unit bandwidth makes it possible to use immediately one of the rules for approximate integration such as the trapezoidal rule, and the calculation then reduces to a quick and simple arithmetical operation. The details, if required, are given in reference³.

This series of readings at different frequencies also gives the shape of the noise spectrum, which is a further useful piece of information. For example, when testing image orthicon tubes it is usual to present the camera with a standard test scene and to adjust the overall resolution of the camera with its control unit in a standardized manner. Since the noise spectrum of an image orthicon should itself be flat, the measured deviation from flatness is an accurate measure of the resolution of the tube itself under working conditions¹.

A small correction to the overall signal-to-noise ratio has to be made when the signal is blanked, since this process reduces the total random noise power without changing the noise voltages which are superimposed upon the unblanked portions of the waveform. With 405-line signals, 1 dB must be subtracted from the measured value.

There is a limit to the lowest signal-to-noise ratio which can be measured, which arises from the fact that the energy from the signal components in the region of measurement, although normally extremely small, is not in fact absolutely zero. The exact

amount is a function of the subject matter of the picture signal, the frequency of measurement, and the time stability of the waveforms composing the synchronizing signal, so that it is impossible to give a single figure for the limiting signal-to-noise ratio measurable to a certain degree of accuracy. Further information and a curve are given in reference³. Very broadly, however, it can be stated that this limitation has not been found at all restrictive for the type of measurement for which the method is intended.

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2. "A Theory of Scanning and its Relation to the Characteristics of the Transmitted Signal in Telephotography and Television." P. Mertz and F. Gray, *Bell System Technical Journal*, Vol. 13, p. 464, July 1934.
3. "The Measurement of Random Noise in the Presence of a Television Signal." L. E. Weaver, BBC Engineering Division Monograph No. 24, March 1959.

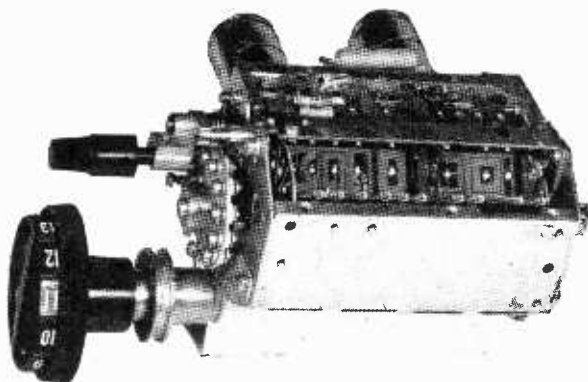


HANOVER FAIR

If the radio and television sections seem to occupy an insignificant part of the 7 million square feet of this vast exhibition, they are nevertheless comparable in size with our annual and the German biennial special radio shows. Indeed, Hanover is regarded by many of the German radio manufacturers and their customers as the most important event of the year, and this applies particularly to those interested in portable and car radio receivers, for the Fair is invariably held at the beginning of the summer season.

The valve has virtually disappeared from portable

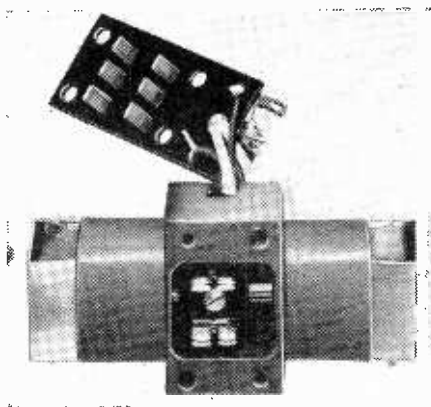
Deutsche Philips "Memomatic" tuner with printed inductances and independently adjustable trimmer stops on each channel.



receivers and most of the new all-transistor models have provision for v.h.f. as well as medium and long waves. The introduction of a v.h.f. band has spread even to some personal portables, e.g., the Telefunken "Partner" (v.h.f. and medium waves) and Siemens RT10 (the latter with three wavebands). Although operating on medium waves only, the new Grundig "Mini-Boy" is the smallest transistor pocket receiver at present on the German market; it weighs 250gm (10oz) and measures 104 × 65 × 27mm.

The vogue of the dual-purpose car-radio/independent

Band switching in some Nordmende sets is effected remotely by a miniature switch operated by an electromagnet, shown open to reveal sliding contacts.



battery portable first noted last autumn in London and Frankfurt is well established and has been strengthened by the introduction of the "Westerland" combination by Blaupunkt. In this an independent transistor portable with self-contained batteries is designed, as usual, to fit neatly into a recess in the car dashboard. When the set is pushed home an additional 4-watt output stage, feeding a larger loudspeaker also permanently installed in the car, is brought into operation. This auxiliary reproducer has its own separate bass and treble tone controls.

Although the promised second television programme in Germany is still delayed by organizational questions, for which satisfactory answers have not yet been found, it is confidently expected at the turn of the year (1960/61). One consequence of the delay is that set manufacturers have had to produce sets with provision for Band IV tuners which can be bought and fitted later on by customers who are reluctant to spend money so far in advance of fulfilment. To ensure that realignment will be unnecessary when the u.h.f. units are added, Blaupunkt are using a non-reactive bridge filter in the output from the mixer. This causes some loss of gain, so all new Blaupunkt models have 4-stage i.f. amplifiers.

"Fully automatic" operation is still obligatory in television sets which hope to sell in Germany, and contrast control by ambient light, as well as "automatic fine tuning" on both v.h.f. and u.h.f., are now common. The method adopted by Deutsche Philips in their "Memomatic" tuner for Channels 2-11 is to pay particular attention to oscillator stability and then to provide independently adjustable trimmer stops for each channel on the selector switch mechanism. These determine the setting of the trimmer through a rocker arm.

A neat method of band switching is used by Nordmende in some of their television sets, which not only cases design problems in the layout of the tuner unit but also provides for simple remote control. The switch slider is actuated by the armature of a solenoid in which there are two windings connected in series in the valve heater circuit. One or other of these coils is short-circuited by push buttons on the front panel or by



The inexpensive Grundig television camera, mentioned last autumn in our report of the Frankfurt radio show, can now be obtained with a portable battery-operated radio link, working on 440-460 Mc/s. The range is stated to be 2km average.

switches in a cable-connected remote control unit.

Considerable prominence is being given in Germany at the present time to *störstrahlung*—radiated interference from TV tuner units, timebases, etc. With the coming of the second programme on Band IV the problem is appreciated as a serious one and is being so treated by the manufacturers, who are giving particular attention to the design of screening in tuning units and to the establishment of radiation measuring laboratories in order to be able to meet the requirements laid down by the German Post Office.

Television sets capable of receiving the four standards at present in use in Europe are now offered by Blaupunkt, Graetz and Telefunken.

Although the Hanover Fair is predominantly the shop window of German industry it is open to all and is gaining in international significance. It is gratifying to record that many British radio and component manufacturers were represented, either as individual exhibitors or as participants in the British Electronics Centre.



Nordwest Deutsche Rundfunk television studio and O.B. equipment installed adjacent to Hall 9 for the broadcast of special programmes relating to the Fair. These and other programmes were distributed by cable to exhibitors' stands.



Using the Simple Analogue Computer

SETTING UP THE INSTRUMENT TO REPRESENT A MECHANICAL SYSTEM

By G. B. CLAYTON*, B.Sc.

LAST month the author described the design and construction of a simple analogue computer that could be used for demonstration purposes in educational and other training establishments. As a suitable exercise in connecting up the computer to represent a physical system, consider the mechanical arrangement in Fig. 1. This consists of a mass M suspended in a viscous liquid by a light spiral spring.

It is required to determine the subsequent motion of the mass if it is displaced from its equilibrium position and then released. Let S represent the force required to produce unit extension of the spring (S being a measure of the "stiffness" of the spring) and let D be the viscous force per unit velocity acting on the mass. Let y measure the displacement of the mass from its equilibrium position.

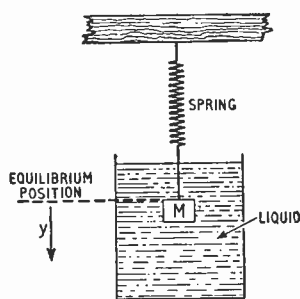


Fig. 1. Mechanical system to be represented on the analogue computer.

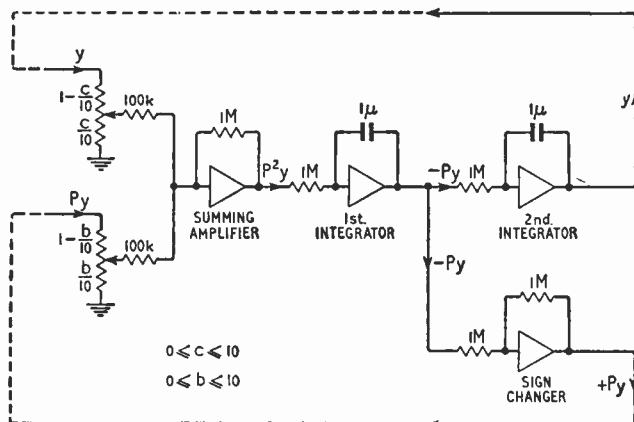


Fig. 4. Combination of Fig. 2 and Fig. 3 to form the complete computer set-up for solving the equation for Fig. 1.

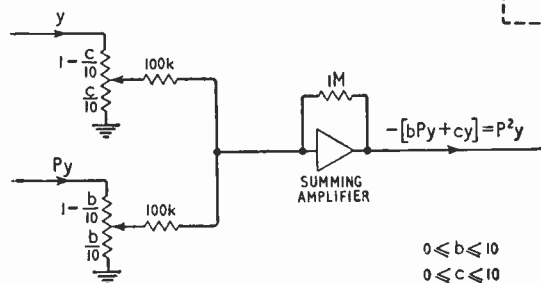


Fig. 2. The summing operation necessary in solving the equation for Fig. 1.

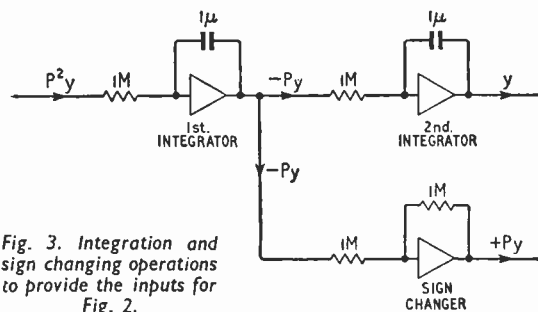


Fig. 3. Integration and sign changing operations to provide the inputs for Fig. 2.

The force acting on the mass will be

$$F = -Sy - D \frac{dy}{dt}$$

and the equation of motion of the mass will thus be

$$M \frac{d^2y}{dt^2} = -Sy - D \frac{dy}{dt}$$

Rearranging this gives

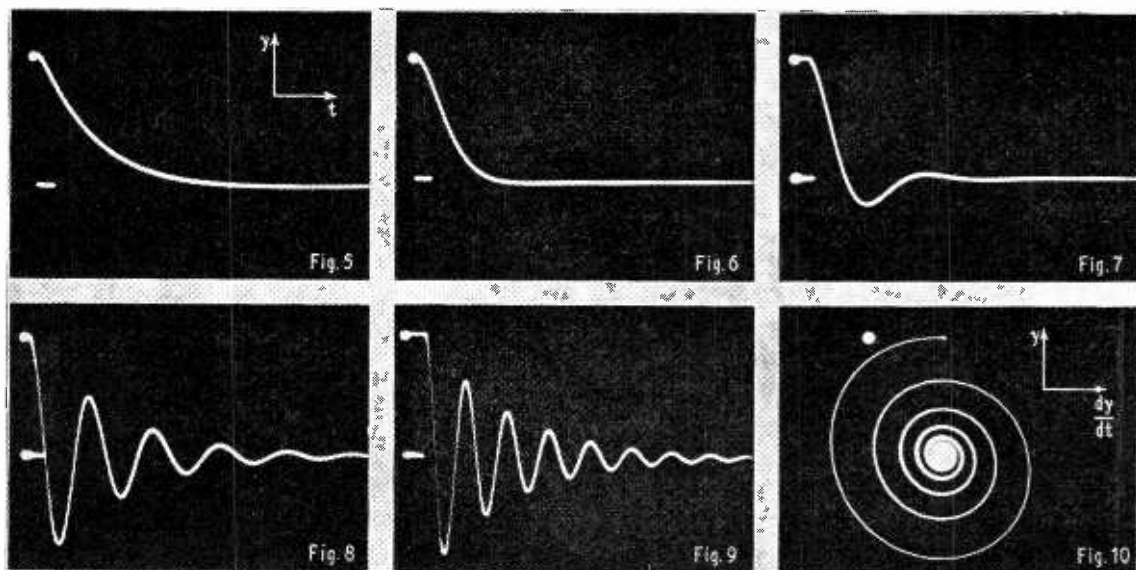
$$\frac{d^2y}{dt^2} + \frac{D}{M} \frac{dy}{dt} + \frac{S}{M} y = 0 \text{ or } P^2y + bPy + cy = 0$$

where $P = \frac{d}{dt}$, $b = \frac{D}{M}$, and $c = \frac{S}{M}$. Many physical

systems may, in fact, be represented by a second order differential equation of this type, e.g. a damped galvanometer movement, or an LCR electrical circuit.

In order to solve the above equation it is first rearranged: $-(bPy + cy) = P^2y$. Terms bPy and cy are represented by voltages which are applied to the input terminals of a summing amplifier. This performs the operation of addition and multiplication by -1 , and its output must therefore represent

* Liverpool College of Technology.



Figs. 5—10. Oscillograms of solutions of equations obtained using the analogue computer arrangement in Fig. 4.

P^2y (Fig. 2). The voltages representing Py and y are dependent on the value of P^2y and are obtained from P^2y by successive integrations.

P^2y is assumed to be known and is applied to the input of an integrator. The action of an integrator being essentially that of multiplication by $-1/P$, the output of this integrator gives $-Py$. A second integrator changes $-Py$ to $+y$ and a sign changing amplifier changes $-Py$ to $+Py$ (Fig. 3). The voltages representing Py and y are now available for application to the summing amplifier of Fig. 2, and the complete computer set up for the solution of the equation is shown in Fig. 4.

This circuit causes the variable voltages to change in exactly the same way as the physical variables that they represent. At the start of a computer run the integrator control switch is put in the "reset" position and a voltage representing the initial value of the displacement y is put across the capacitor of the second integrator. On switching to the "compute" position the integrators are placed in circuit and the computer run commences.

The oscillograms above are a record of some solutions obtained using the circuit of Fig. 4. Figs. 5 to 8 show the displacement y as a function of time for a constant value of the coefficient c but successively smaller values of the coefficient b . The coefficient b , which depends on the viscosity of the liquid, controls the damping of the motion; Fig. 6 corresponds to critical damping. Figs. 8 and 9 are solutions for the same value of b , but in 9 the coefficient c has been increased. This corresponds to an increased spring "stiffness" with a consequent increase in the frequency of oscillations, the damping remaining the same. Fig. 10 shows the displacement

y as a function of the velocity $\frac{dy}{dt}$ for a damped

oscillation. The recordings were made using an oscilloscope with d.c. coupled amplifiers, slow sweep facilities and a long-persistence screen.

Thanks are due to D. L. McCluskey who did most of the constructional work on the apparatus described last month.

B.B.C. HANDBOOK

WITH the object of giving "a comprehensive and up-to-date picture of what the B.B.C. is and what it does," the Corporation publishes each year a handbook. The 1960 edition, like its predecessors, does just that. Although a considerable part of its 270-odd pages is devoted to programme matters, there is much of technical and general interest in the Handbook. Here are some points of interest culled from the section devoted to engineering activities.

"Approximately 50% of the programme output is recorded in advance. . . . During the year recordings were made on 108,000 disks and 24,000 miles of magnetic tape. . . . B.B.C. tape recording facilities include 241 static, 88 mobile and over 225 midget machines. There are also 68 static and 29 transportable disk-recording machines."

"While it may well be possible to build at great cost a loudspeaker or combination of loudspeakers, which in

a specially arranged setting will be the ultimate in performance in the light of present knowledge, this is of little use to a broadcasting authority [for monitoring]. Here the need is for some hundreds of high-quality loudspeakers, all of which must have an identical performance within normal manufacturing limits. Since nothing meeting these requirements is available commercially, the B.B.C. has designed and produced its own loudspeaker system, including the design of a suitable cabinet."

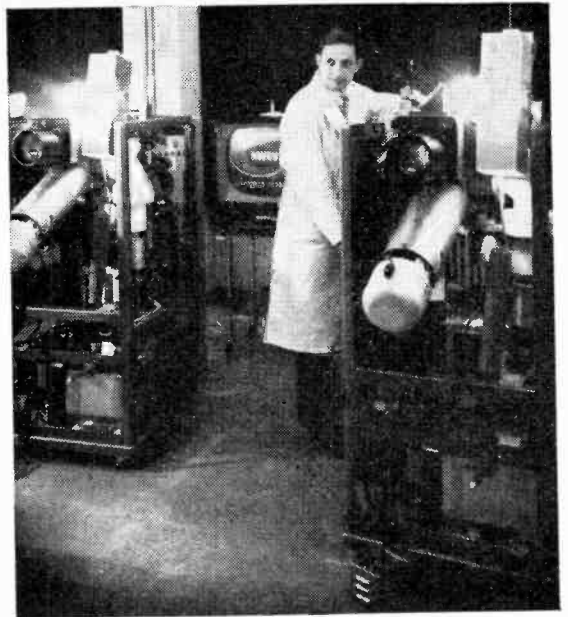
It is interesting to see that the cost of running the television service in 1958/59 was £14M as against £11.1M for the domestic sound service and £5.9M for the external services. The percentage of each of these figures attributed to "engineering" is 33, 23 and 25, respectively. Of the total of £4.6M for television engineering, £775,086 was for the rental of Post Office lines.

LARGE SCREEN COLOUR TV

THE Eidophor system for projecting television pictures on large screens has now been adapted for colour television, and recently we saw a demonstration of its capabilities for closed-circuit work at Belle Vue, Manchester, given by CIBA Clayton Ltd., the dye manufacturers. In the Eidophor projector (made in Switzerland by Gretag A.G., with the backing of CIBA, the Swiss chemical combine) light from a powerful xenon arc lamp is modulated by means of an oil film which is electrostatically deformed in the pattern of the television picture by a scanning electron beam. The deformations in the film actually modulate the light by refraction—by altering the angle at which the light is reflected from a concave mirror behind the oil film. An optical interception system (Schlieren system) in the path of the reflected light then causes the beam-angle variations to produce corresponding beam-intensity variations in the light emerging from the projector.

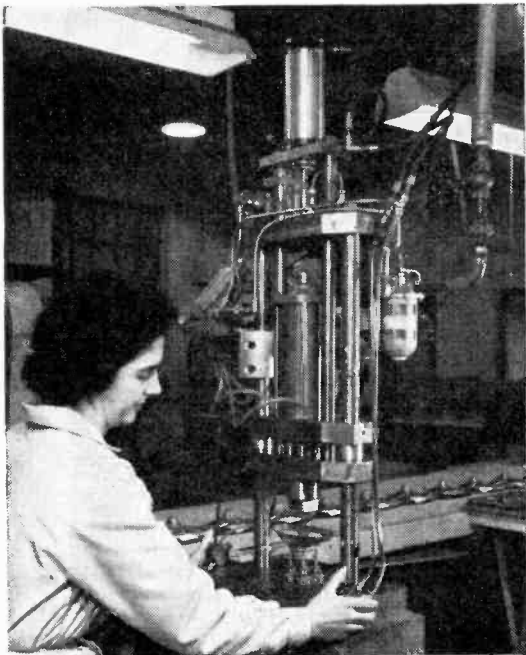
Adaptation to colour television has been achieved by using the frame-sequential system with synchronized rotating colour filters in front of the camera and projector. For the demonstration three image orthicon cameras were set up at CIBA Clayton's Technical Service Laboratories in Manchester and the signals were transmitted 1½ miles by microwave link to Belle Vue for projection on a screen measuring 10ft x 7ft. The cameras were American types and the 525-line standard was used.

The advantage of the Eidophor system over c.r. tube projection systems is, of course, the greater



Eidophor projectors in process of manufacture.

brightness obtained by modulating a normal light source. This was very evident at the demonstration, although the pictures suffered a certain amount of spasmodic flicker. Definition was excellent for a large screen (there are no image registration problems with the frame sequential system) and the colour rendering was as good as the quality of the rotating colour filters.



Multi-Riveting Machine

A DOUBLE-ACTING air-operated press tool especially suitable for radio assembly work involving riveting of any kind has been introduced by Rhoden Partners Ltd., design and development engineers of 19, Fitzroy Square, London, W.1. It is shown in the illustration in use in the production of loudspeakers.

A feature of this machine is that it automatically feeds and punches a whole pattern of rivets in one operation and it is claimed that the squeezing action of the air-operated punches is less violent than mechanical impact operation as it produces little or no distortion in the immediate vicinity of the riveted parts.

The working cycle is as follows: the operator loads the parts to be riveted together on to the spring-tensioned location pins in the bottom bolster, then releases compressed air to the upper ram punch holder. For this latter operation two press buttons have to be operated simultaneously, one by each hand. This is a safety precaution. After the riveting operation is completed the rams rise automatically to the "ready" position. This sequence of operations takes about three seconds.

Power for the press is a single-phase (230-250V) a.c. supply for the rivet vibratory-bowl feeder, and an air supply of preferably 80lb sq in.

Rhoden multi-riveting machine.

WORLD OF WIRELESS

Trade and Production

FIGURES contained in the twenty-seventh annual report of the Radio and Electronic Component Manufacturers' Federation show that production of components during 1959 increased by over 20% compared with 1958. Total production for 1959 was about 2,400M components, worth £120M. On average this represents an output of one million components for each working hour.

Domestic equipment manufacture absorbed 43% of the total, an increase of 1.4% over 1958, professional equipment took 30.4% and 14.6% (- 0.9%) was exported. The remainder comprised a.f. equipment and military use, retail sales, etc. Exports of components returned £21.5M, compared with £20M in 1958.

The total value of parts and assembled equipment exported was £53.4M (+17.5%), the most significant increase being in professional equipment, which rose by 35% to £21M. The largest individual markets (up to November) for components continued to be Australia (£1.34M) and India (£0.96M) and for a.f. equipment the U.S.A. (£5.03M); but the largest increase, 50%, in sales over £0.5M was in Italy. Total exports to America top the list at £5.6M, a rise of 28.2% over 1958. Total audio exports, however, fell.

Imports to the U.K. rose to £20.3M from £13.5M in 1958. Biggest increase here was £2M, to £5.7M, for valves, tubes and parts; but imports of domestic receivers nearly trebled to £0.61M. Tape recorder imports were three times our exports and Great Britain now has an adverse balance of £3.8M with the Netherlands and W. Germany. The total deficit with the Common-Market countries was £2.7M and the credit with Outer Seven £1.2M.

New Post Office Director General

On June 1st Sir Gordon Radley, K.C.B., first engineer to be director general of the Post Office, retires after five years in office. He joined the Post Office in 1920 and was controller of research before being appointed engineer-in-chief in 1951. Sir Gordon, who was knighted in 1954 and was for some time chairman of the technical sub-committee set up by the Television Advisory Committee, was awarded the I.E.E. Faraday Medal in 1957 for his "outstanding contributions in the field of international communications and particularly in the development of long-distance, deep-sea telephone cables and their repeaters."

The new director general is Sir Ronald German, C.M.G., who entered the Post Office in 1925 and left in 1950 to become Postmaster General in East Africa, where he did much to develop the telephone service in that area. He returned to the British Post Office in 1959 as a deputy director general. Sir Ronald is succeeded as deputy director general by W. A. Wolverson, C.B., who entered the Post Office in 1928. In 1951 he was appointed commandant of the Post Office Residential Management Train-

ing Centre. He was more recently in charge of the Radio Services Department and since 1955 has represented the Post Office on the Council of the International Telecommunication Union.

Data Processing Expansion

THE Electronic Engineering Association, which represents the capital goods side of the industry and is now separated from the Radio Industry Council, is setting up more groups to deal with electronic data processing matters. The 1959 Annual Report of the E.E.A. reveals that in addition to the data processing executive committee formed in 1956 there are now two technical committees, on digital and analogue data processing respectively, with working parties on coding of punched paper tape, storage systems, input and output equipment, international data transmission, core stores, magnetic tape, single-purpose computers and on transistors and semiconductor devices for computers. In 1959 exports of electronic computers amounted to £1.75M, the total exports in the field of the E.E.A. being £28M. Recent achievements of the capital goods section of the industry are described in an illustrated annual review obtainable from the E.E.A.

Servicing Examination Problems.—The practical tests for entrance for the sound radio servicing certificate examination of the Radio Trades Examination Board on May 21st had to be postponed. This was because of "the difficulty of concluding a satisfactory arrangement with the patent holders" of the trainer-tester system introduced last year. This test has been deferred until the autumn when actual receivers will be used. Because of the problem of securing the necessary number of receivers, which are lent by manufacturers, it has been decided to restrict the practical course to candidates who succeed in the written papers.

The Paul Instrument Fund Committee have awarded a grant of £2,500, with the probability of further grants totalling up to £3,000, to Dr. J. H. Sanders, university lecturer and demonstrator in physics, Clarendon Laboratory, Oxford, for the construction of an optical maser; and another of £3,000 to H. W. Gosling, lecturer in the department of engineering, University College of Swansea, for the construction of an instrument for checking the stability of the standard ampere.

Institution of Electronics 15th annual electronics and instruments exhibition and convention is to be held at the Manchester College of Science and Technology from July 7th to 13th. It is again being organized by the northern division of the Institution and will include a manufacturers' section and a section devoted to scientific and industrial research. Complimentary tickets of admission to the exhibition and also details of the convention are obtainable from W. Birtwistle, 78 Shaw Road, Rochdale, Lancs.

Electronic Organs.—The first general meeting of the recently formed Electronic Organ Constructors' Society, of which Alan Douglas is president, will be held on May 28th at 2.30 in Room 45, Northern Polytechnic, Holloway Road, London, N.7. The secretary of the society, which has a membership of nearly 80, is A. Le Boutillier, 26 St. Catherines Road, London, E.4.

R.E.C.M.F.—At the annual general meeting of the Radio and Electronic Component Manufacturers' Federation on April 22nd, the following member firms (whose representatives' names are in parentheses) were elected to the council: Belling & Lee (N. Dundas Bryce), Garrard (H. V. Slade), A. H. Hunt (S. H. Brewell), Multicore Solders (R. Arbib), Painton & Co. (C. M. Benham), Plessey (P. D. Canning), S.T.C. (L. T. Hinton), Telcon Metals (G. A. V. Sowter) and Bakelite (G. J. Taylor). In addition Texas Instruments (D. Saward), Reliance Cords & Cables (C. H. Davis), and Morganite Resistors (J. Thomson) were subsequently co-opted to the council. Hector V. Slade and Dr. G. A. V. Sowter were re-elected chairman and vice-chairman, respectively, of the Federation.

B.R.E.M.A.—The new council of the British Radio Equipment Manufacturers' Association elected at the annual general meeting on April 29th consists of the following member firms whose representatives' names are in parentheses: A. J. Balcome (E. K. Balcombe), British Radio Corp. (F. W. Perks), Bush Radio (G. Darnley-Smith), E. K. Cole (W. M. York), Ferguson Radio Corp. (S. T. Holmes), G.E.C. (M. M. Macqueen), Kolster-Brandes (L. R. Tyne), Philips (A. L. Sutherland), Radio & Allied Industries (R. H. W. Pengelly), Rediffusion Vision Service (M. Exwood), Roberts Radio Co. (H. Roberts), and Ultra Radio & Television (E. E. Rosen). The new chairman of the association is A. L. Sutherland with W. M. York as vice-chairman.

Channel Islands TV.—The Television Act, which governs the I.T.A.'s operations, does not at present apply to the Channel Islands, but provision is made in the Act for its operation to be extended by Order in Council. If this is done, the I.T.A. plans to build a station, probably in Jersey, which will receive some of its programmes *via* the Authority's Devonshire station, due to be opened early next year. It is announced by the I.T.A. that if the Act is extended to the Channel Islands, they will offer the programme contract to Channel Islands Communications (Television) Ltd., which has recently been formed in Jersey.

"**Designers Guide**" is the title of an information sheet introduced by Mullard's Semiconductor Division to assist industrial designers to plan equipment in the knowledge that the semiconductors they specify will continue to be available when the equipment comes into production. It gives essential data on every Mullard transistor, rectifier and diode available. Readers wishing to receive "Designers' Guide", which will be issued three times a year, should write on their organizations' letter heading to: Semiconductor Division, Mullard Ltd., Mullard House, Torrington Place, London, W.C.1.

A **radar training school** is being established by Decca at the recently acquired site at Cowes Airport, Isle of Wight. Technical training courses of eight or ten months will be provided for the staffs of overseas Governments and authorities installing Decca civil or military radar systems. There will also be shorter courses of about six weeks for service engineers. The company already operates a technical training scheme at its service headquarters in London and a marine operational school at Blackfriars Pier, London.

"**Engineers in Communications**" is the title of a half-hour film surveying the research and development in telecommunications undertaken by Post Office engineers, which is now available for hire from the C.O.I. Central Film Library, Government Building, Bromyard Avenue, London, W.3. It costs 15s to hire and is considered particularly suitable for students.

Apprenticeship schemes offered by E.M.I. are outlined in a well-illustrated 32-page book "A Career in E.M.I. Electronics," which also deals with the group's various products. Career masters and others concerned with young people leaving schools and colleges may obtain copies of the book from the Group Personnel Department, E.M.I. Ltd., Hayes, Middx.

The **Orkneys** v.h.f. sound broadcasting station at Netherbutton, near Kirkwall, was brought into full-power service on May 2nd. Its directional aerial, giving a maximum e.r.p. of 25kW, radiates the B.B.C.'s three sound services on 89.3, 91.5 and 93.7Mc/s. A single-programme low-power transmitter has been in service on the site since December, 1958. Netherbutton picks up its programmes direct from the v.h.f. station near Wick, which in turn receives the programmes from the v.h.f. station at Meldrum, Aberdeen.

15,000,000 broadcast receiving licences were in force in the U.K. at the end of March. During the month the number of combined television/sound licences increased by 101,430 to 10,469,753. Sound only licences totalled 4,535,258, including 427,491 for sets fitted in cars. During the same period television licences in Holland rose to 640,000 and sound licences to 2,621,000.

H.P. and Hiring Restrictions.—Under new restrictions imposed by the Board of Trade on April 29th on the initial deposit and repayment period for hire-purchase and credit sales agreements (S.I. 1960, No. 762) a deposit of 20% of the cash price is now required on sound radio and television sets and gramophones. The period for repayment is limited to two years. Another Order (S.I. 1960, No. 763) stipulates that the initial payment on hiring agreements for these equipments is a quarter's hire charge.

Norway.—The official opening of the Norwegian television service has now been fixed for August 20th. At present experimental transmissions are radiated by a transmitter in the Oslo area, where some 14,000 licences have been issued. A second station, in Bergen is being introduced.

Armour Research Foundation of the Illinois Institute of Technology is acting as host for the fourth annual Joint Military-Industrial Electronic Test Equipment Symposium which will be held in Chicago on September 14th and 15th.

Two-year sandwich course in telecommunications, providing alternate 6-monthly periods in college and industry, commences at the South East London Technical College, Lewisham Way, London, S.E.4, on October 3rd. The London fee is £17 per year. C. W. Robson, head of the electrical engineering department, has also sent us details of a four- or five-year engineering sandwich course in which provision is made for specialization in communication engineering.

Technical books to the value of £200 are to be provided during each of the next seven years to the Holborn (London) Central Library under a deed of covenant presented by Philips Electrical Ltd.

Valve Dimensions.—Two new sections of BS448, specifying the base and bulb dimensions of the B5G/F and B7E/F sub-miniature valves with flexible connecting leads, have been issued by the British Standards Institution. They cost 2s each.

"**Hardwood Instrument Cases.**"—Because of the misspelling of the name of a resin glue in the footnote on p. 178 of our April issue some confusion might arise with Casein type glues which are not so suitable for hardwood gluing. The correct name is Cascamite.

"**Dynamic Side Thrust in Pickups.**"—Owing to a typographical error in this article in our May issue, the steady stylus displacement was given on p. 215, column 2, line 30, as 25×10^{-3} cm; it should, of course, be 2.5×10^{-3} cm. On page 216, column 2, at the end of line 39, "other" should read "outer."

Advance Components Ltd. have asked us to point out that the price of their TC1 transistorized counter, which was quoted on page 254 of our May issue as £425, is now £335.

Heathkit Ham Transmitter Kit.—We regret that the price of the Model DX-40U on page 24 of the advertisements in our May issue, was given in error as £12 10s. The correct figure is £29 10s.

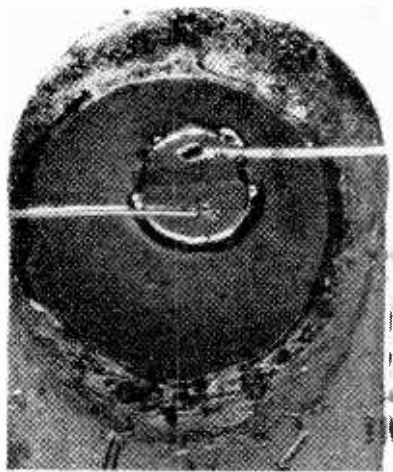
Personalities

Royal Signals Institution.—Membership of the Royal Signals Institution, which has in the past been restricted to Officers of the Royal Corps of Signals, is now open to all ranks of the Corps, both past and present. Its object is to foster the professional and technical interests of the Corps by publishing a journal (at present bi-annually), arranging lectures, maintaining the Royal Signals museum and conducting an annual essay competition. Details of membership, for which the fee is 15s a year, are obtainable from Brigadier W. T. Howe, Royal Signals Institution, 88 Eccleston Square, London, S.W.1.

Twelve Scholarships to men wishing to study for the Radio Amateurs' Examination are being offered by 404 Signal Squadron (Press Communications), Army Emergency Reserve. The scheme is open to fit men between the ages of 18 and 40 who are prepared to enlist in the Squadron for three years. When they attend the annual 15-day camp (the only peace-time training) they will be given intensive courses in basic theory and Morse. At home they will continue their theory studies by means of a free correspondence course in preparation for the 1961 radio amateur examination. Details are obtainable from Major J. A. Bladon (G3FDU), 28 Jack Lane, Davenham, Northwich, Cheshire.

I.E.E. On The Pipe.—The Institution of Electrical Engineers building is now permanently connected by a 5-Mc/s wide-band coaxial cable to the Post Office distribution network for television or other wide-band signals. The cable, which goes to the Gerrard exchange, was actually put in for the colour television relay from Paris reported on p. 287.

Stereophonic broadcasting using a time-multiplex pulse-amplitude modulation system for the transmission of two channels from one transmitter has been developed by Siemens & Halske AG., of West Germany. The system, which is compatible, is one of several being tested in Germany.



Portrait of a Mesa.—The central section, to which the two wires are attached, is the raised plateau of semiconductor material which is characteristic of a mesa transistor. This specimen, magnified 53 times, is the Ferranti double-diffused silicon transistor ZT20, which has a cut-off frequency of 80 Mc/s. Its construction was described and illustrated in the March issue, p. 127. The two gold wires, one mil in diameter, are pressure-bonded to the base and emitter, while the metal tab supporting the main body of the semiconductor forms the collector connection. By mid-1960 production of these transistors is expected to be 25,000 per year.

J. A. Saxton, D.Sc., Ph.D., A.R.C.S., M.I.E.E., head of a division of the D.S.I.R. Radio Research Station at Slough for the past five years, has been appointed deputy director of the station. Dr. Saxton has been in the scientific civil service since 1938, when he joined the staff of the N.P.L. Radio Division. As already announced, the present director, **Dr. R. L. Smith Rose**, retires on September 30th, and is succeeded by **J. A. Ratcliffe**. Dr. Saxton has been responsible for carrying out a considerable programme on research in the propagation of microwaves over the ground and through the troposphere. He has twice served in the U.K. scientific mission in Washington and has been a U.K. delegate at many international scientific meetings. He is chairman of the U.K. national study group of the C.C.I.R. covering groundwave and tropospheric propagation.



Dr. J. A. Saxton



Prof. C. W. Oatley

C. W. Oatley, O.B.E., M.A., M.Sc., M.I.E.E., who since 1945 has been a Fellow of Trinity College, Cambridge, and University lecturer in electrical engineering, has been elected Professor of Electrical Engineering by the University. He will succeed **Professor E. B. Moullin**, who, as announced in our January issue, is retiring in October after occupying the chair since it was established in 1945. For twelve years prior to the war Professor Oatley was a member of the staff of the physics department of King's College, London, and for some time during the war was in charge of basic work on radar transmitters and receivers at the Radar Research and Development Establishment of the Ministry of Supply. He was chairman of the Radio Section of the I.E.E. in 1954/55 and is a member of the measurements and standardization committee of the International Scientific Radio Union.

J. Bell, B.Sc., F.Inst.P., deputy director of the G.E.C.'s Research Laboratories at Wembley, Middx., which he joined in 1929, has been appointed a director of the M.O. Valve Co., a subsidiary of the G.E.C. Mr. Bell, whose scientific work has been largely in the field of radio and radar transmitting valves, has been manager of telecommunications division of the laboratories since 1953.

P. J. Walker, president of the British Sound Recording Association for 1960/61, is managing director of Acoustical Manufacturing Co., of Huntingdon, which he formed in 1936. Mr. Walker, who has been responsible for most of the design and development of audio equipment made by his company, is also very well known as a lecturer on loudspeakers and high-quality reproduction. Readers will recall his articles in *Wireless World* on the electrostatic loudspeaker.

A. L. Sutherland, director of Philips Electrical, which he joined in 1933, and of Cossor Radio and Television since its acquisition by Philips, is the new chairman of the British Radio Equipment Manufacturers' Association. After war service in the Royal Artillery, in which he rose to the rank of major, and the Air Branch of the General Staff, Mr. Sutherland rejoined Philips in 1946 and managed the tungsten lamp department until being appointed commercial manager of the television and radio division in 1950. Six years later he was appointed to the board. Mr. Sutherland has represented Philips in B.R.E.M.A. for some years and has been vice-chairman of the council since 1957.



A. L. Sutherland.



J. F. Winterbottom.

J. F. Winterbottom, M.Sc., A.M.I.E.E., A.M.Brit.I.R.E., has been appointed chief engineer of Data Recording Instrument Co., of Ashford, Middx., which is associated with International Computers and Tabulators Ltd. Mr. Winterbottom was previously with the Motor Industry Research Association.

P. A. Charman, who joined Semiconductors Ltd. on its formation in 1957, has been appointed sales development manager and will be concerned with the company's technical information service. After ten years in the Electrical Branch of the Royal Navy and of the Royal Canadian Navy he was for two years with Philco (Great Britain), Ltd., where he set up a training equipment division.

Joseph Samuels, purchasing director of Winston Electronics, Ltd., Shepperton, Middx, for several years, has been appointed works director in charge of production. Before joining Winston Electronics in 1954, Mr. Samuels, who is 49, was for several years with Standard Telephones & Cables and later Sunvic Controls of A.E.I., Ltd.

V. P. Cole, who joined Grundig (Great Britain) Ltd. as sales manager in 1955, has been appointed sales director to the board. He started his career in 1917 as a wireless operator with Marconi's and during the last war he was with the Radio Production Executive of the Ministry of Aircraft Production.

James C. Pledger has been appointed technical director and chief engineer at the Coventry factory of Lexor Electronics Ltd. He succeeds **R. Grey**, who has taken an overseas appointment.

E. G. Wakeling, who joined Advance Components, Ltd., as general manager in February last year, has been appointed a director. He was formerly manager of the servo division of Elliott Brothers, Lewisham.

A. B. Clarke has joined Cossor Instruments Ltd. as sales manager. He was previously instrumentation sales manager of J. Langham Thompson Ltd., which he joined from the G.E.C. Applied Electronics Laboratories.

Cecil Dannatt, O.B.E., M.C., D.Sc., M.I.E.E., has been appointed vice-chairman of Associated Electrical Industries Ltd., with the special responsibility of co-ordinating both commercial and technical policy. Dr. Dannatt, formerly group managing director of Metropolitan-Vickers, has been group managing director of Associated Electrical Industries (Manchester) since it was formed earlier this year. He joined the board of Metro-Vick in 1947 as director and chief electrical engineer. Four years later he became assistant managing director and director of research and education. Dr. Dannatt, who is 63, and a director of a number of companies in the A.E.I. Group, was professor of electrical engineering at Birmingham University from 1940 to 1944.

H. West, M.Sc., M.I.Mech.E., M.I.E.E., assistant managing director of A.E.I. (Manchester) since last January, succeeds Dr. Dannatt as managing director. He joined Metropolitan-Vickers as an apprentice in 1918. In 1946 he was appointed assistant to the chief electrical engineer of the company; three years later he became chief electrical engineer, and was appointed to the board in 1951.

Peter Axon, O.B.E., Ph.D., M.Sc., A.M.I.E.E., managing director of Ampex Electronics Ltd., is now also managing director of Redwood City Engineering Ltd., the U.K. marketing subsidiary of Ampex International, S.A., of Fribourg, Switzerland. Dr. Axon joined Ampex Electronics Ltd., the organization's U.K. manufacturing subsidiary, last year from the Research Department of the B.B.C. where he had been engaged mainly in magnetic recording research and development since joining the Corporation in 1947.

D. H. Follet, M.A., Ph.D., F.Inst.P., keeper of the Department of Electrical Engineering and Communications in the Science Museum, London, since 1957, has been appointed director of the Museum. He succeeds Dr. T. C. S. Morrison-Scott, who has become director of the British Museum (Natural History). Dr. Follet joined the museum in 1937 as an assistant keeper in the department of physics. He was previously an industrial physicist.

OUR AUTHORS

D. Saull, who on page 306 discusses mains transformer design, is on the development engineering staff of a firm of instrument manufacturers, where he is mainly concerned with the design of a wide variety of transformers. Following war-time military service in radar, he served for eight years in the Police Force and then entered the Diplomatic Wireless Service in which he was engaged on technical security work. For several years immediately prior to joining his present company he was in the Plessey applications laboratory at Towcester.

L. E. Weaver, B.Sc., A.M.I.E.E., author of the article on the measurement of random noise in television receivers, is head of the measurements group of the B.B.C.'s Designs Department which he joined in 1955. Prior to joining the B.B.C. he was with Standard Telephones and Cables where in the transmission laboratory he was engaged on the design of multi-channel telephone systems and networks and was for some time leader of a group specializing in the design of terminal equipment.

John E. Robson, B.Sc., A.M.I.E.E., senior development engineer of Redifon's Communications Laboratory, Crawley, Sussex, contributes an article on the calculation of standing-wave ratio to this issue. After serving in Royal Signals from 1940 to 1946 he studied at King's College, Newcastle, where he graduated in electrical engineering in 1948 and then went into industry. For seven years prior to joining Redifon in 1959 he was with Weymouth Gauges, Ltd. He is 39.

V.H.F./F.M. Car Radio

By R. V. TAYLOR,
Assoc. Brit.I.R.E.

USE OF F.M. TUNER, A.F. AMPLIFIER AND POWER
SUPPLY UNIT FOR MOBILE BROADCAST RECEPTION

THE B.B.C.'s v.h.f./f.m. services now cover all the major populated areas, and the greater part of the country is served by the 20 transmitting stations. In many areas medium and long-wave reception is not as satisfactory as v.h.f. and, of course, the relatively short car-radio aerial is very inefficient at low broadcast frequencies. Many listeners now use v.h.f.-only receivers in their homes and would, no doubt, be satisfied with restriction to B.B.C. only on their car radios; especially in view of the freedom from interference given by f.m. Thus it seems only logical to use a v.h.f./f.m. car-radio receiver.

Two difficulties arise when considering such an installation. The first, common to most car radios, is the provision of power supplies. Many modern cars use 12-volt positive-earthed batteries; thus valves must either have 12-volt heaters or be connected in series pairs. Also the positive earth may limit the choice of vibrator units.

The second apparent difficulty concerns the aerial. Only a vertical aerial could be kept reasonably clear of the car body and one would expect reception of horizontally-polarized transmissions on a vertical aerial to be unsatisfactory. Fortunately this is not so; a vertical quarter-wavelength rod fitted to the car roof (which will serve as a ground plane) has been found to provide a good signal in the service area of a v.h.f. station. Such an aerial is usually omni-directional and is also suitable for direct connection by coaxial cable to the receiver input.

The principal requirements for a mobile v.h.f./f.m. receiver are met by most good f.m. tuners at present available, so the simplest method of obtaining v.h.f. car radio is to use a "standard" tuner and add a.f. stages and a power unit.

Tuner Requirements

The principal requirements of the tuner are:—

Sensitivity.—A figure of the order of $10\mu\text{V}$ input for effective limiting has been found to be adequate in most areas. Greater sensitivity is not an advantage, as in places where it would be warranted for domestic use a moving vehicle would pass through rapid variations of signal strength, the minimum values of which might be too low for satisfactory use. A tuner of $10\mu\text{V}$ sensitivity normally gives good reception or no reception at all, an ideal state of affairs where borderline operation may distract a driver.

Frequency Stability.—Naturally, retuning during the warm-up period is undesirable and automatic frequency control is a useful "extra." However, despite the variations of temperature and supply voltage which arise in a car, many tuners seem to be stable enough to operate satisfactorily.

Good a.m. rejection.—It is vital where signal levels are low and ignition interference, vibrator hash, and generator "whine" abound, that a good a.m. rejection factor should be achieved. Tuners having a

limiter stage preceding a ratio detector, or two limiters and a Foster-Seeley discriminator, should be suitable.*

Automatic Gain Control.—Good a.m. rejection can be achieved by "dynamic" limiting, but a limiter of this type is not able to compensate for variations in signal strength. Thus a.g.c. is necessary and this may also help to hold constant the a.f. level when using a static type of limiter.

Free Tuning.—Switched tuning is unsuitable unless the receiver is to be used in the service area of only one station. A large-reduction tuning drive is, naturally, an aid to tuning.

A.F. Gain Control and Switch.—Some v.h.f. tuners incorporate an a.f. gain control and a power switch. This is desirable as then only the tuner need be accessible from the driving position and the power supply and amplifier can be mounted elsewhere.

Many of the kits and ready-assembled tuners on the market satisfy these requirements with little modification, so the choice of "front end" for the receiver is largely a matter of size (both in regard to the pocket and the tuner).

Preparing the Tuner

For a 12-volt supply the valve-heater circuit will have to be re-arranged unless 12-volt valve equivalents are available. The simplest method is to connect the valves in series pairs, remembering that a shunt resistor will be necessary across the lower-current heater if valves of different heater-current rating are connected in series.

The heaters of the local oscillator and discriminator valves (if germanium diodes are not used for the latter) should be at the "earthy" side of their pairs. The extra wiring involved may cause instability. New leads should be run close to the chassis and kept away from signal wiring: extra decoupling may be necessary. Microphony, too, can be a problem, so this should be eliminated from the tuner before installation. Any leads or components likely to move under vibration should be secured. To ease servicing problems plug-and-socket connections for aerial, power supply, switch and a.f. output are desirable.

A.F. Stages

Most tuners provide an a.f. output of at least 0.3 volts at high impedance and the author finds that a power output of one to two watts is ample for use in a car—in most modern cars no more than 0.5W will be required. Thus a single-ended two-stage amplifier is adequate. Where space is limited a single triode-pentode valve (an ECL80 or ECL82, for example) could be used.

* *Editorial note.*—Readers are reminded of the excellent and simple limiter/discriminator described by J. G. Spencer on p. 492 of our November 1959 issue.

TABLE: SUITABLE OUTPUT VALVES

Valve	Bias Resistor (ohms)	Output Transformer Ratio for 3-Ω Load	Heater Rating		H.T. Current (mA)
			V	A	
6BW6	270	40 : 1	6.3	0.45	50
6V6					
6J5	470	50 : 1	6.3	0.3	15
6C4					
EL91	680	75 : 1	6.3	0.2	19
EL32	470	50 : 1	6.3	0.2	37
12A6	330	50 : 1	12.6	0.15	33

Transistors could be used with advantage in both the a.f. amplifier and power supply units. However, the intention was to keep down costs by using components available either from the "junk" box or the surplus market. Kits for both transistor amplifiers and power units are available, though, and the saving in battery drain through the use of transistors may be thought worthwhile. Also data sheets giving details of suitable 12-volt power units and a.f. amplifiers are obtainable from some transistor manufacturers.

Fig. 1 shows a circuit in which various combinations of valves may be used—a 6BR7 voltage amplifier and 6BW6 output stage are indicated. The a.f. input, from the tuner gain control (a screened lead is necessary), has connected across it a 1MΩ resistor to prevent the grid circuit becoming "open"

Other Possibilities.—If battery drain is the only consideration, a 6J5 or 6C4 may be used as an output valve. No heater shunt resistor is required with a 6SJ7/6J5, or 6BR7/6C4 combination.

Other pairs not requiring a shunt resistor for 12-V operation are EF86/EL32 and EF86/EL91. No change in component values, except heater shunt, need be made for any of the voltage-amplifier valves mentioned. Of course, a 12A6 and 12SJ7 or 12AT6 could be used with parallel-connected heaters on a 12-V supply. The Table gives further details of the valves suggested.

Layout of the a.f. stages is not critical; normal precautions should be taken to keep input leads away from the output and heater wiring.

Interconnections

The connection between tuner and a.f. unit will carry a.f., h.t., l.t. and leads to the switch thus, for convenience, plug and socket connections are a good idea, although it would be unwise to add a bulky socket to a compact tuner. Multiple earthing should be avoided and the outer braid of the screened a.f. lead must be connected to earth only at one point. It will thus require a separate pin on the plug. L.T., earth and, possibly, the switch leads carry high currents, and need conductors thick enough to keep the total potential drop within bounds—say a maximum of half a volt with a six-volt supply, and double that on 12V.

Connections from the a.f. unit to the power supply

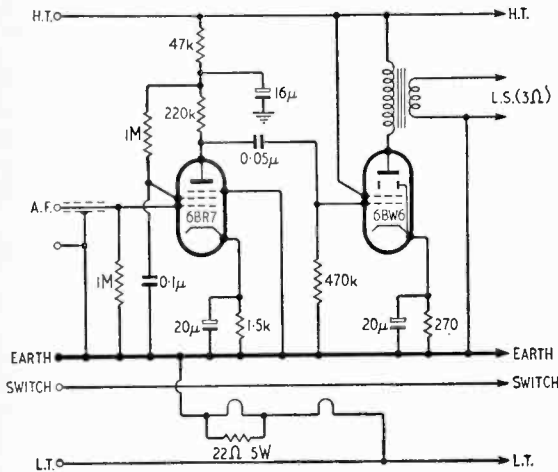
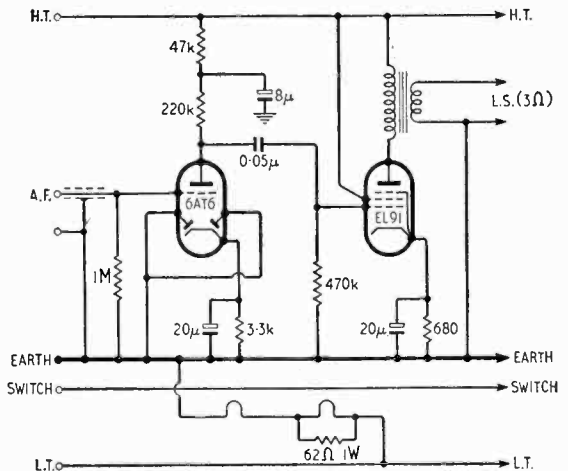


Fig. 1. Audio amplifier showing heaters connected for operation from 12-V battery. On 6V, heaters should be connected in parallel and 22-Ω shunt resistor omitted.

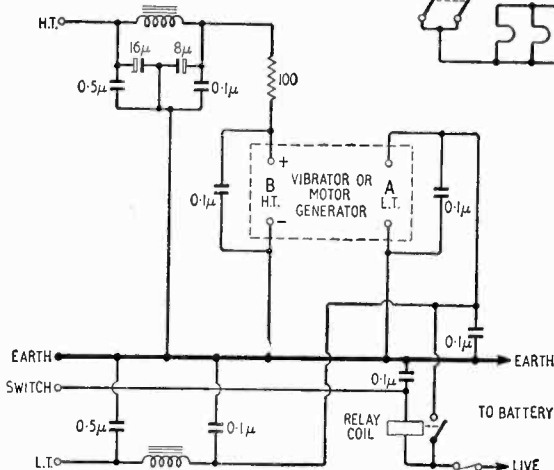
Fig. 2. "Economy" a.f. amplifier requiring only 19mA at 220V h.t. Heaters shown wired for 12-V operation.



if the lead is disconnected. This first stage provides a voltage gain of about 140; it is thus capable of driving fully the least-sensitive output valve listed in the Table from a tuner output of as little as 0.15V. Octal-based near equivalents of the valves shown are 6SJ7 (V1) and 6V6 (V2) but a 43-Ω 2-W heater shunt will be required for the 6SJ7 instead of 22Ω.

An "economy" version of the a.f. unit, given in Fig. 2, is intended for use where space is limited and battery drain must be kept at a minimum. An output of over one watt is available, but distortion is higher than in the first circuit.

Fig. 3. (Below) Filter and switch circuits added to vibrator or motor-generator h.t. supply. If the h.t. unit has only three terminals its input polarity should match that of the car supply. Switch on volume control switch lead to earth in the "on" position.



should be made in the same way and a screened lead should also be used for the loudspeaker. The loudspeaker should be earthed only at the amplifier chassis (the earthy connection of the cathode-bypass capacitor for V2 seems to be the best place). All these measures are taken to avoid noise pick-up from the electrical-system currents flowing in the body of the vehicle; these may reach the loudspeaker, even when the receiver is switched off, if earth connections are made at several points on the car body.

Power Supplies

A variety of vibrator and motor-generator units are available on the surplus market. A vibrator is more efficient than a motor generator and is therefore kinder to the battery. Care must be taken to check that the polarity of the supply acceptable by the vibrator unit is the same as that used on the car, although some units are designed to be compatible, usually by a simple modification, with either polarity of supply. The h.t. current of both the tuner and the a.f. unit (see Table for values at 220V) must be added to give the total power required from the h.t. supply.

Fig. 3 shows the connections for a typical vibrator or motor-generator unit. The filters shown in the h.t. and l.t. leads should not be necessary where the unit has its own filters, but the additional capacitors will generally be required to reduce radiation or pick-up of noise by the leads. The l.t. choke may be made by winding about three yards of 14-s.w.g. enamelled-copper wire on to a 1-in long by ½-in diameter former. An ordinary smoothing choke rated at the full h.t. current is suitable for the h.t. filter.

The contacts of the switching relay must be capable of carrying in the region of 12A for 6-V operation or 5A on a 12-V supply. If a suitable

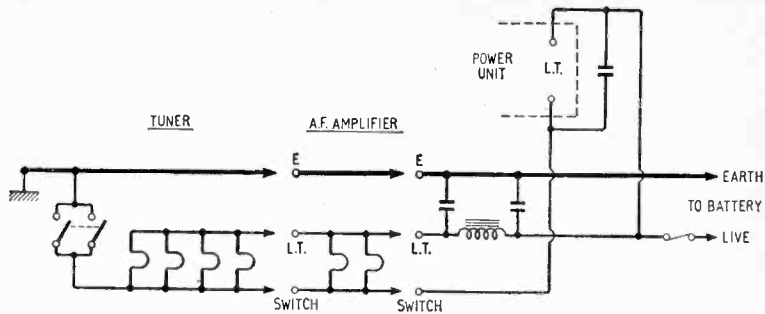


Fig. 4. Power switching without relay. The h.t. unit must be isolated from earth: i.e. there must be no d.c. earth connection in the unit. Switch lead may require filtering similar to l.t. lead.

type cannot be found on the "surplus" market a horn relay from a motor-accessory dealer would be suitable.

If the space available allows a compact layout, and leads between battery and power unit (via the tuner power-on/off switch) can be kept short (less than about six feet total) the relay can be dispensed with and the alternative circuit of Fig. 4 may be used. If the switch is incorporated in the tuner volume control it is advisable to connect in parallel the two halves of a double-pole type.

The lead from the power-supply unit to the car battery should follow the most direct route possible, passing through grommets where necessary to avoid chafing. Remember that the movement of the car may damage a heavy cable that is not securely fixed. The fused lead may be connected directly to the battery terminals; but if an "auxiliary" connection is provided (usually on the cut-out panel) this should be used in preference to the direct connection.

The author used a 7×4-in elliptical loudspeaker as space was available. Generally, the largest-possible loudspeaker with the highest-flux magnet will give the best results; but avoid damp or hot places or its life may be shortened. A large baffle area also helps.

Aerials

At v.h.f. a resonant aerial can easily be used. A quarter-wavelength vertical whip mounted at the centre of a sheet of metal is a simple and effective aerial. As long as the metal sheet extends for more than a quarter wavelength in all directions from the base of the aerial it will behave as a ground plane and the aerial will have an impedance of about 50Ω at its base (but 75-Ω coaxial cable is suitable). For Band II the sheet of metal must be at least five feet across its smallest dimension; a car roof is obviously ideal.

A 2-ft 6-in whip in the centre of a car roof thus makes a simple and effective aerial. Despite the apparently incorrect plane in which it is mounted, it will operate because the signal at or near ground level will have a considerable vertically-polarized component.

Details of easily constructed or adapted aerials are given in Fig. 5. Where a quarter-wave whip and ground plane cannot be used (for example, on a sports car) a coaxial dipole (each element 2ft 6in long) may be suitable. In most cases the lower ele-

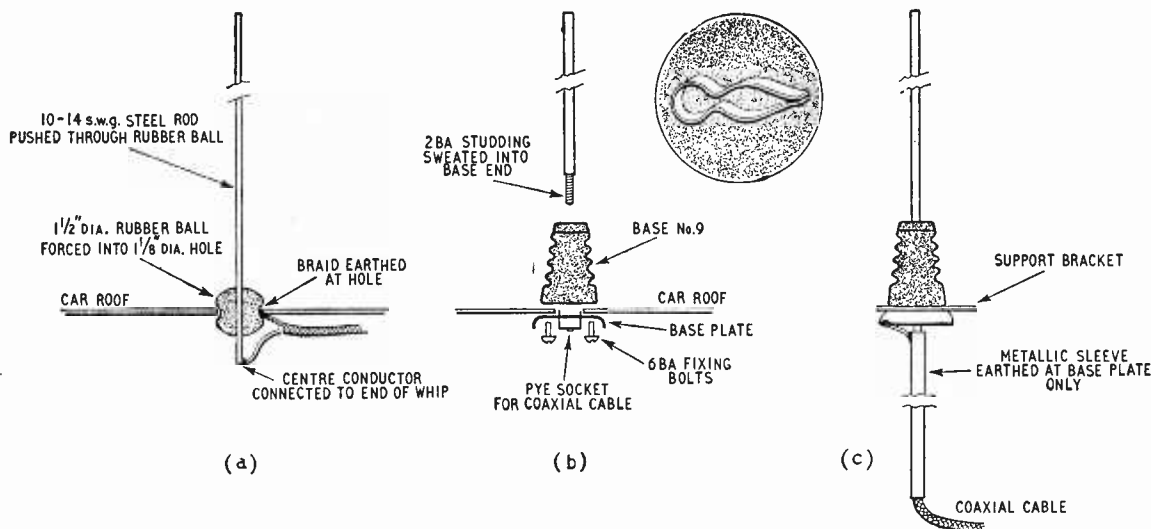


Fig. 5. Some methods of mounting the aerial: (a) uses rubber ball as insulator and (b) employs ex-Govt. aerial base. For cars with non-metallic bodies (c) shows a coaxial dipole. Sleeve can be formed from outer covering and braid from large-diameter coaxial cable. Aerial elements are about 2ft 6in long. (Inset). Cable clip to secure aerial feeder. Springy clip material enables "legs" to enter slot in bodywork, then open out to hold cable firmly.

ment will be close to the bodywork, reducing the efficiency of the aerial, but a good signal should still be obtained.

Feeder losses are negligible on the short run required in a car and the unbalanced aerial is better suited to connection to a coaxial cable than a balanced dipole. The normal telescopic car-roof aerial may be used as long as the outer braid of the coaxial cable is earthed effectively to the car roof at the aerial base.

The inset in Fig. 5 shows a cable clip for use in a slot in the bodywork. To avoid a loop in the receiver earthing it may be necessary to isolate the aerial-feeder "outer" at the tuner-input socket. This can be done by using a coaxial socket of the type employed on live-chassis television receivers. The sleeve (outer braid connection) of this socket is connected to the chassis through a 1,000-pF capacitor shunted by a 1-MΩ resistor. The resistor provides a leakage path for any "static" charges picked up by the aerial.

Mounting the Units

Of course, the tuner chassis must be insulated from the car body—if the tuner has rubber feet it may be stood on the parcel shelf. Strips of plastic-foam draught excluder stuck to the bottom of the tuner make a good substitute for rubber feet. Some form of insulated resilient retaining clips are also advisable. For the a.f. unit the same considerations apply as far as vibration and earthing is concerned—the units should be placed rather than mounted, but must be restrained from "wandering" due to the movement of the car.

The power-supply unit, as it is much heavier than the other units, must be firmly anchored. The vibrator or generator is likely to be noisy acoustically so it is best placed outside the passenger compartment, either in the boot or in the engine space. To prevent the transmission of noise by the bulkhead or body work, the unit should be fixed by bolts, pass-

ing through rubber grommets in its chassis and in the mounting holes in the car.

Conclusion

A receiver made up on the lines suggested should give good results in almost any part of the country. However, many apparently small points may have a noticeable effect on performance and a certain amount of trial and error is inevitable if the best results are to be obtained. A last word—don't forget that a separate licence is required for a car radio!



Foreign Body Locator, developed by the University of Birmingham Department of Physics, will detect an object of about 1 cu. mm size at a distance of 1cm with an accuracy of better than 1mm. It uses a search coil in one arm of an R-L bridge, and the presence of a magnetic or metallic object causes an impedance change which unbalances the bridge (indicated by a meter reading and a variation in pitch of an audible note). A phase-sensitive detector indicates whether the object is magnetic or not.

LONDON AUDIO FAIR

SELECTED EXHIBITS OF INTEREST

"THE mixture as before," only more so, might be said to describe the recent Audio Fair, since most of the changes from last year were continuations of trends which were already noticeable then.

One trend which had perhaps hardly begun last year but which was very noticeable this year was an increase in the number of imported foreign (and in foreign we hope we are allowed to include U.S.A.) exhibits.

As before, while the main emphasis was on stereo, the main developments were in tape recording. This year, however, stereo has well and truly invaded the tape recording field, with stereo recording as well as replay facilities being offered in many of the new models and with the introduction of several new stereo microphones. Stereo microphones and tape recorders which can both record and replay stereo are thus now no longer the rarities they once were.

Four-track tape recorders are also now no longer a rarity, many of the new models coming into this category. As many as three such models were introduced by T.S.L.—the Harting HM8, the Korting and the Electron 9S/4K. All of these can also record stereo (as well as mono). Both the Korting and Harting HM8 use a transistor in the pre-amplifier to reduce hum and noise. In the Harting HM8 this transistor is not in its usual position before the first valve, but rather after it, this latter arrangement being claimed to allow better matching to the tape head.

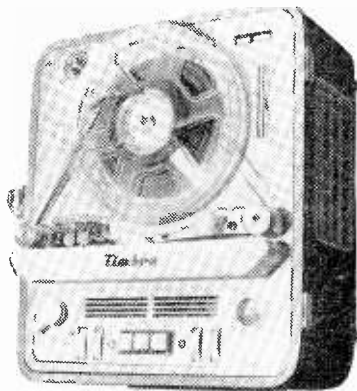
Four- and two-track recorders, both of which used the same deck,

were introduced by Multimusic (Reflectograph). One unusual feature of this deck is that variable-speed fast forward and fast rewind are provided by a single control. This control consists of a potentiometer. The ends of the element are connected to the fast forward and rewind motors while the slider is connected to one side of the mains supply: the other side of the mains supply is connected to the other inputs to the motors. In this deck no idler wheels are used to drive the tape, the capstan being directly attached to the spindle of a synchronous "inside-out" motor. The rotor of this motor then acts as a flywheel to reduce fluctuations in the tape speed. Speed change is effected electrically. No pressure pads are used, the required close contact between the head and tape being produced by means of fingers bearing on the tape at each side of the head: a method being increasingly used nowadays. The signal-to-noise ratio is quoted as 50dB for the two-track model A; for the four-track model B this ratio is reduced to 45dB because of the narrower track width.

A stereo recorder shown by Ampex—the 970—has several unusual features. One of these is that the numbers of tracks used on record and replay can be different, since two-track heads are used to record and four-track heads to replay. Thus, while only two-track tapes can be recorded, both four- and two-track tapes can be replayed. Since the tape track positions are different for two- and four-track stereo tapes, and since the replay head gaps should lie centrally across each track for

minimum crosstalk, the optimum head positions for minimum crosstalk are also different for replaying two- and four-track stereo tapes. This factor is allowed for in the Ampex 970 by making the position of the four-track replay head adjustable relative to the tape width—another unusual feature.

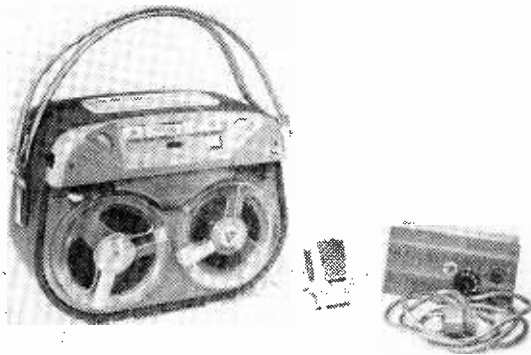
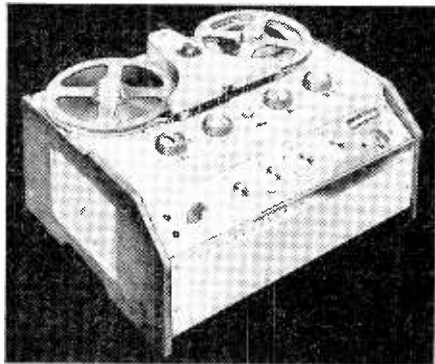
A very unusual feature of the two-track Timbra recorder shown by T.S.L. is that the two tape reels are



Timbra recorder showing reels in playing position one on top of the other.

placed one on top of the other. To raise the tape from one reel to the other it is first twisted through a right angle until it lies horizontally, then raised, and finally twisted back through a right angle. Impressive performance figures are quoted for this recorder: at the two provided

Multimusic Reflectograph 4-track recorder



Butoba battery/mains transistor recorder showing mains converter on right.

tape speeds of $3\frac{1}{2}$ and $1\frac{1}{2}$ in/sec the frequency responses are stated to be within ± 2 dB from 30 to 18,000 c/s and 30 to 12,500 c/s respectively, and the total wow and flutter less than 0.05% and 0.1% respectively.

An unusual facility of the Vollmer 120 tape deck shown by Chitnis is that the tape speed can be continuously varied from $1\frac{1}{2}$ to $7\frac{1}{2}$ in/sec. This variable speed is obtained simply by driving the capstan flywheel by means of a rubber wheel which can be shifted along a shaft perpendicular to the flywheel axis. Even at the slowest tape speed of $1\frac{1}{2}$ in/sec, the wow and flutter is quoted as less than 0.1%. Space for up to six miniature Bogen heads is available on this deck.

Two new two-track transistorized battery tape recorders were shown—the German Butoba MT4 (distributed in England by Denham and Morley) and the Challen Minivox. In the latter recorder, although the high-frequency recording bias is provided by the transistors, permanent magnets are used for erasing the tape. Two magnets are used in an arrangement which is claimed to result in much less tape noise than is produced by a single magnet. The fast forward and rewind motors are designed so that the battery current does not increase when the tape is fast wound (at about 40 in/sec). The tape is capstan driven in the usual way in both this and the Butoba MT4 recorder. In this latter recorder the tape drive motor speed is kept constant as the battery voltage falls by means of a transistor switched by a centrifugal governor. The wow and flutter is quoted as 0.3% at a tape speed of $3\frac{1}{2}$ in/sec. Both high-frequency bias and erase are provided by two OC74 transistors in push-pull. A converter for operating this recorder from the mains is available.

TAPE

American Irish (Orr) tape was shown by Wilmex. The recording surface of this tape is polished so as to produce closer contact between the head and tape and thus improve the high-frequency response.

Pre-recorded four-track $7\frac{1}{2}$ in/sec stereo tapes produced by the United Stereo Tape group of American manufacturers were demonstrated by Ampex.

MICROPHONES

Stereo twin moving-coil cardioid microphones were shown by the Austrian firm A.K.G. (distributed in England by Politechna (London)), Chitnis, T.S.L. and Telefunken. In the Telefunken model the two moving-coil units can be rotated relative to one another or even separated altogether: in the other models the units are fixed at right angles to each other.

A close-talking high-quality ribbon microphone—the 4104—was

shown by S.T.C. A ribbon microphone normally responds to the sound pressure gradient or sound velocity and the low-frequency response rises for close sound sources. In the S.T.C. 4104, however, for a person speaking from a controlled standard distance from the microphone set by a mouth guard, this rise in the low-frequency response has been eliminated to give an output which is flat within ± 3 dB from 60 c/s to 10 kc/s. Distant sound sources will then appear to have their lower frequencies attenuated by amounts which range from about 5 dB at 1000 c/s to 25 dB at 60 c/s. Since these lower frequencies form an important part of most background noises, the response to such noises is considerably reduced. Another feature of this microphone is that the responses to sounds from the mouth and nose have been carefully equalized.

A number of useful facilities are offered with Austrian A.K.G. moving-coil and condenser microphones (distributed in England by Politechna (London)). For example, in several of the moving-coil units the bass response can be usefully reduced to eliminate the normal rise when close talking. This reduction in the low-frequency response is usually produced simply by connecting a choke across the microphone. A variable polar response is offered for both the D30 and D36 moving-coil and C12 condenser microphones. Essentially this variable polar response is obtained by mounting two cardioid units back to back and combining a varying proportion of their outputs in or out of phase—in the case of the condenser unit by altering the relative magnitudes and polarities of the two polarizing voltages. Omni-directional and figure-of-eight responses, for example, are then obtained by combining the two

cardioid responses in or out of phase respectively.

Many of the moving-coil units in the A.K.G. range have been given a cardioid response. This is done by combining the omni-directional sound pressure response of a diaphragm exposed on only one side to sounds with the figure-of-eight pressure-gradient response of a diaphragm exposed on both sides to sounds. Basically these microphones are thus constructed with the diaphragm enclosed on one side except for a release tube.

LOUDSPEAKERS

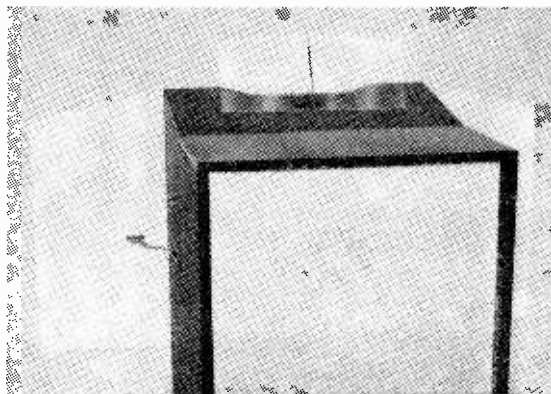
An interesting single-cabinet stereo loudspeaker system—the Acousta-Twin—was demonstrated by Lowther. In this system frequencies below 200 c/s—which convey only a small part of the directional information—are combined together by loading the rear of each of the two loudspeakers via a cavity (to cut off frequencies above 200 c/s) with two folded horns having a common mouth. Frequencies above 200 c/s which are radiated from the front of the speakers are reflected both sideways and upwards by wedges at the top of the cabinet. Further reflections at the room walls and ceiling then produce apparent sound sources much further apart than the speakers themselves. The separation and height of the sound sources produced by the upward-directed portion of the sound can be modified if desired by tilting a Perspex reflector on top of the cabinet. When the speaker system is used for reproducing mono sound this reflector is turned round through 180° and can then be raised or lowered to reflect a variable proportion of the upward-directed sound forwards. A variable proportion of the sideways-directed sound can also be reflected forwards by rotating two hinged Perspex panels at the side of the cabinet. For reproducing stereo, these hinged panels should be flat against the wall.

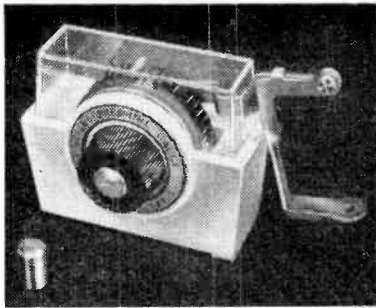
A number of unusual loudspeakers and loudspeaker mounting arrangements were shown by the French



Above: A.K.G. stereo moving-coil cardioid microphone.

Below: Lowther Acousta-Twin stereo loudspeaker system.





Garrard stylus pressure gauge showing check weight at front left.

firm Teppaz whose equipment is distributed in England by Selecta Gramophones. For example, in their portable record players high-impedance crystal loudspeakers are used to reproduce frequencies above 3000c/s, and, in order to save space, the lower frequencies are reproduced by inside-out loudspeakers—i.e., loudspeakers in which the magnet is inside rather than outside the cone angle. These inside-out loudspeakers are mounted on flat lid baffles with the mounting deliberately made non-rigid. Moreover, both the front and back of these speakers are covered by grilles which are deliberately designed to impede the free flow of sound. The Teppaz Duo Dynamic enclosure has a long slit opening at its rear which leads to two expanding chambers terminated by hinged doors. By adjusting these doors the bass response of the system can be varied.

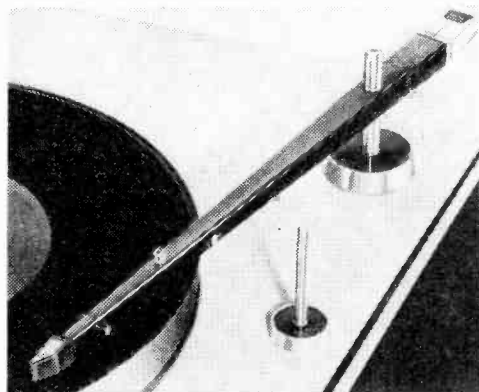
A recent modification to the Stantel column loudspeakers made by S.T.C. for sound reinforcement purposes is that they have been given a slight curvature in the vertical plane. This widens the high-frequency vertical polar response to the same width as the low-frequency vertical polar response.

A 10-in version of their well-known Dual Concentric loudspeakers—the IILZ—was shown by Tannoy. In this new unit the high-frequency response can be altered by using a capacitor to shunt a variable fraction of a resistor in series with the horn-loaded high-frequency unit. Alternative speaker impedances of 4, 8 or 15Ω can be selected by means of an auto-transformer.

High-quality moving coil headphones with quoted responses from 30c/s to above 15kc/s were shown by A.K.G. (distributed by Politechna (London)) and Chitnis (the Beyer DT48). The low-frequency response of course depends on how airtight the earpiece to head joins can be made.

PICKUPS

A rather unusual arm is used in the American Shure Studio Dynetic



Above: H.M.V. pickup arm and stereo cartridge.

Left: Shure pickup arm and stereo cartridge.

pickup (distributed in England by Maunder). In this arm the vertical- and lateral-motion pivots are well separated rather than close together. The two vertical motion point pivots, being only about an inch from the head, carry little more than the head and head counterweight. The arm is balanced about the point and sleeve pivots for lateral motion so as to reduce interference by external vibrations and to avoid the need for levelling. The main arm counterweight is attached by means of a vertical strip embedded in a special damping material to reduce the effects of the low-frequency arm resonance. A magnet in the arm attaches it to its rest. This arm is straight, the offset angle necessary to reduce tracking error being provided in the head itself. This head uses a moving-magnet system, both mono and stereo versions being available. For the stereo or mono cartridge respectively the effective mass at the stylus tip is quoted as 1.3 or 1.25mgm and the compliance as 9×10^{-6} or 7×10^{-6} cm/dyne.

A high-quality stereo pickup and arm were shown by H.M.V. The pickup uses a variable-reluctance vertical-lateral motion system, the correct outputs for the standard 45/45 recording system being obtained by the usual method of summing (adding) and differencing (subtracting) the vertical and lateral outputs. The effective mass at the stylus tip is quoted as about 1mgm vertically or laterally, and the vertical and lateral compliances as 3.5×10^{-6} and 7×10^{-6} cm/dyne respectively. The arm is suspended on a single pivot, movement being damped by a viscous fluid. The counterweight is mounted asymmetrically to provide the sideways balance necessitated by the head offset. The head offset angle is adjusted to minimize the distortion

produced by the angular tracking error rather than to minimize the tracking error itself. Minimizing the tracking error will not necessarily minimize the distortion since this is not only proportional to the tracking error but also inversely proportional to the distance from the record centre. A raising and lowering mechanism is also incorporated in this arm.

In the Mark II version of the Tannoy Vari-Twin stereo cartridge an extra pair of pole pieces has been added. These are cross-connected to the bottom two pole pieces so that any hum picked up by either of the bottom two pole pieces and induced in the coil wound on it is cancelled by the hum induced via one of the extra pole pieces. A hum reduction of the order of 20dB has been obtained in this way.

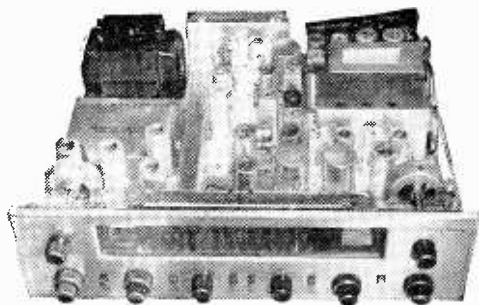
A new stylus force gauge—the SPG3—was shown by Garrard. This is graduated in $\frac{1}{2}$ gm intervals from 0 to 12gm. A 5gm check weight is provided. The stylus force is balanced via a lever against that of a spiral spring.

RECEIVERS

Two American models consisting of independent a.m. and f.m. tuners mounted on the same chassis for receiving suitable stereo transmissions were shown by Ampex and Wilmex. The Wilmex unit—the Fisher 202-T—is claimed to effectively limit f.m. inputs below 1μV, four i.f. and limiter stages being used. A stereo pre-amplifier and tone control unit is incorporated on the same chassis.

A new Chapman tuner—their S6BS/FM—is a combination of their older FM91 f.m. and S6BS a.m. tuners. Nine a.m. bands are provided, six being bandspread.

The range of Goldhorn transistor sets shown by Denham and Morley



includes the TK110 which can receive short waves down to 16 metres.

S.T.C. were showing a relatively inexpensive triple-crystal unit for use in f.m. receivers.

AMPLIFIERS & PRE-AMPLIFIERS

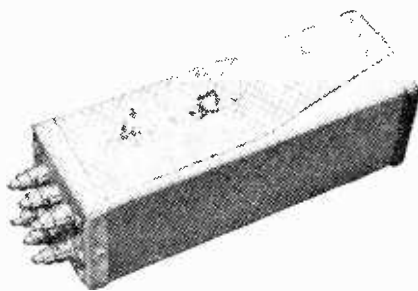
Transistorized units seemed to be more common this year. Pre-amplifiers were shown by Cintel, Wellington Acoustic Laboratories, and Reslosound. The Reslo Transistor Coupler is designed for microphones with impedances from 30 to 1,000 Ω and uses a common-base transistor circuit. Wellington Acoustic Laboratories showed two units for use with both high and low impedance pickups—one unit for mono and the other for stereo. The crosstalk on the latter—the Stereo Wal Gain—is claimed to be as low as -60dB at 1,000c/s and better than -50dB at 10kc/s. (Any capacitive coupling would tend to make crosstalk increase with increasing frequency.) Special features of the Cintel prototype unit are high- and low-pass filters cutting off at 18dB/octave from 30c/s and 7kc/s respectively.

A transistorized combined pre-amplifier and 15W (5% distortion) power amplifier on the same chassis—the BCS2429—was shown by G.E.C. In the pre-amplifier mixing of the signals from two 15 to 30 Ω microphones and a high-impedance crystal pickup is possible. In the power amplifier the base bias of the driver and two output transistors can be adjusted to obtain the optimum

Above: Fisher a.m./f.m. stereo tuner and tone control unit.

Rogers stereo tone control unit.

Right: Wellington Acoustic Laboratories transistor stereo pickup pre-amplifier.



performance. A prototype power amplifier shown by Cintel gave an output of 10W at less than 0.5% distortion.

Turning now to valve amplifiers, for reducing stereo "hole in the middle" a variable output proportional to the sum of the two stereo signals and designed for feeding a central third speaker (third channel) is provided in the American Fisher X202 combined stereo pre-amplifier, tone control unit and 2x25W power amplifier shown by Wilmax. Variable crosstalk between the two channels can be artificially introduced in this unit so as to reduce the width of the overall sound field. Other unusual facilities in the Fisher X202 are controls for adjusting the bias and d.c. balance to optimum.

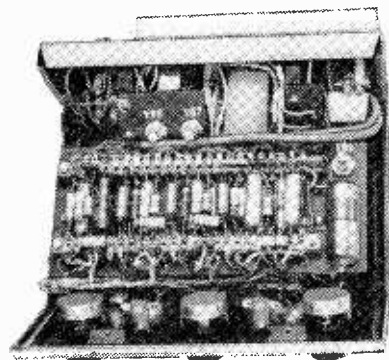
An unusual feature of a range of 30W (1.5% distortion) and 60W (3% distortion) portable combined pre-amplifiers and amplifiers designed by S.T.C. for use in public address systems is the provision of cathode-ray output level indicators. The out-

put impedance is 333 Ω for the AP30/2IP and AP30/3IP 30-W amplifiers and 166 Ω for the AP60/3IP 60-W amplifiers. The signal-to-noise ratio for these amplifiers is as high as 54dB even at the maximum input sensitivity of 0.5mV (at 600 Ω).

Special features of a very comprehensive stereo pre-amplifier and tone control unit shown by Rogers are a maximum sensitivity of 2mV, provision of as many as 18 inputs, 10 of which can have their sensitivities varied, a low-pass filter with variable slope and choice of three alternative cut-off points, a high-pass filter with two alternative cut-off points, and coarse and fine balance controls.

An American stereo amplifier balance indicator using a meter—the Kinematix SB-1—was shown by Wilmax. If an acoustic balance different from the amplifier balance is required and obtained, the indicator can be adjusted to re-indicate balance, and the same acoustic conditions for balance can then be readily reproduced.

A 25-W guitar amplifier combined with a 12-in loudspeaker—the Vibromajor—was shown by Grampian. A special feature of this is an amplitude modulation vibrato variable both in frequency and depth. The very high peak to mean ratio of the input signal necessitates an amplifier specification somewhat different from that for normal high fidelity. For example, the power requirements are somewhat higher, although a higher distortion—up to about 2%—is quite acceptable. The amplifier should have a smooth overload characteristic (i.e. less feedback than is usual can be employed) and not block or oscillate when overloaded.



Left: Underneath view of G.E.C. transistor combined pre-amplifier and power amplifier.



Right: S.T.C. triple-crystal unit for use in f.m. receivers.

Self-Balancing Push-Pull Circuits

2.—Practical Design Considerations

By D. R. BIRT*

(Concluded from page 221 of the May, 1960 issue)

FROM the discussion of general principles in last month's article, the requirements for the first stage of a practical amplifier are now fairly clear. We have seen that for good balance and low push-push gain, V_1 and V_2 should have a high g_m and large anode impedance. This suggests the use of pentode valves. However, there is an attendant disadvantage associated with the screen grid supply in this type of circuit, which may be of importance in the most critical applications. As may be seen from Fig. 8, the screen grids of V_1 and V_2 must be held at cathode potential as far as a.c. signals are concerned, and not at earth, to avoid application of one half of the input signal to the common screen junction. This may be accomplished by decoupling the screen grids to cathode. However, when this is done, the screen dropping resistor appears effectively in shunt with the cathode impedance. A better plan is to substitute cascode stages for V_1 and V_2 .¹² It is generally possible to achieve a higher gain in this way, and a screen grid supply is not required.

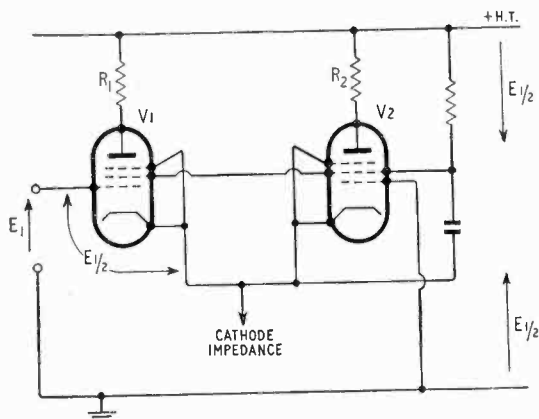


Fig. 8 Long-tailed pair using pentodes.

The grids of the upper triodes of the cascode pair require ideally to be at a constant potential relative to cathode. This is not a difficult problem, as we may decouple the grids to cathode, and make the grid feed resistor large.

Alternatively, a cross coupling arrangement can be used as shown in Fig. 9. The operation of this circuit is rather interesting. When a push-pull signal is applied, it can be seen that the drive to the upper triodes of the cascode pair is applied to both the grid and cathode, in antiphase. As far as the cathode circuit is concerned, this turns out to be equivalent to doubling the g_m of the upper valve, and therefore the cathode impedance is halved and the voltage

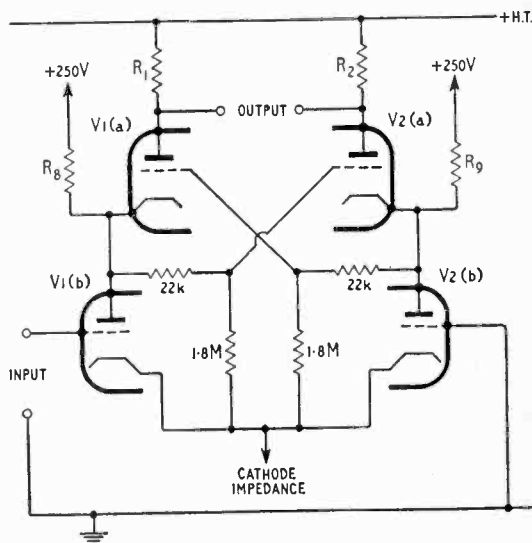


Fig. 9 Long-tailed pair using cascode stages with cross coupling.

gain to this point is halved. However, the grid-to-cathode voltage of each upper triode is the same as it would be in a conventional cascode amplifier, and the overall gain is similar.

If we now consider a push-pull signal, we find that the signal voltages at the grid and cathode of the upper triodes are in phase, and of almost equal amplitude, so that the amplifier has less gain in this case.

The basic cascode amplifier may be improved by the addition of two resistors, R_8 and R_9 , in Fig. 9.¹³ This modification promotes a higher g_m in the lower triodes by reason of the additional anode current bled through R_8 , R_9 . The gain of each cascode stage is the product of the g_m of its lower valve and the anode load resistor of its upper valve. It would appear advantageous to operate the lower triode over the region of its characteristics where the g_m is highest. This implies working at a high anode current. In a conventional cascode amplifier, an increase in lower triode anode current increases the voltage dropped across the upper triode anode load resistor. In a driver stage, where we want a large output, we cannot tolerate this reduction of anode voltage as it reduces the available output voltage. Therefore we have to reduce the anode load resistance, and we find that what we gained on the "swings" of higher g_m we have substantially lost on the "roundabouts" by reducing the load resistance. In the modified circuit, however, current fed to the anode-cathode junction allows the anode current (and hence the g_m) of the lower triode to be greater

* Mullard Research Laboratories.

than that of the upper triode. The effective g_m is increased by this means without affecting the current in the load resistor, and it follows that there is an increase in gain over the conventional form of circuit.

Having considered the general requirements of the circuit, it is now appropriate to consider particular requirements with respect to valve operating conditions. The first step is to plot the cascode characteristics of the double triode to be used. Fig. 10 shows the characteristics of an ECC83 plotted for an upper valve grid voltage of 170 volts. The characteristics are similar in form to those of a pentode, and it is a useful rule of thumb to take the knee voltage at a practical working current as being approximately equal to 120% of the potential of the upper triode grid. It is emphasized that, although these characteristics represent a fair average in respect of valves measured by the author, they are not necessarily those of a nominal valve.

The value of the anode load resistor may now be chosen. A high value will give a large gain, and the first limit is often set by the bandwidth requirements of the amplifier. It is necessary to ensure that the load is such that the operating point does not move into the knee region or beyond cut-off, under normal operating conditions.

In determining the operating conditions, one must bear in mind the fact that grid current may begin to flow at about -1.3 volts V_{g1} , and one must therefore ensure that the grid voltage does not normally approach this value. If supply voltages are subject to variation, allowance should be made to prevent an increase in distortion with a low h.t. voltage.

As an example, suppose the bandwidth required is 20 kc/s, and that the load presented by the following stage is 10 pF in parallel with $2M\Omega$. A load resistor of $470k\Omega$ is suitable, and a loadline of the appropriate slope is drawn in Fig. 10. Fig. 11 shows

Fig. 10 Cascode characteristics of the ECC83 double triode.

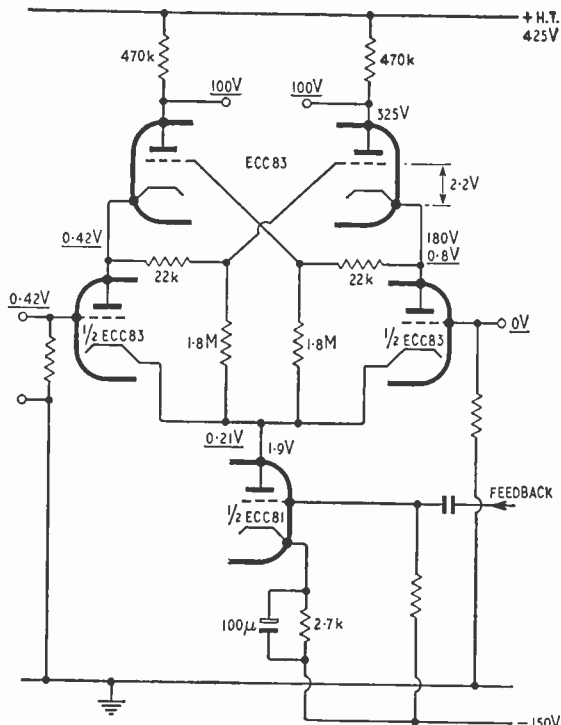
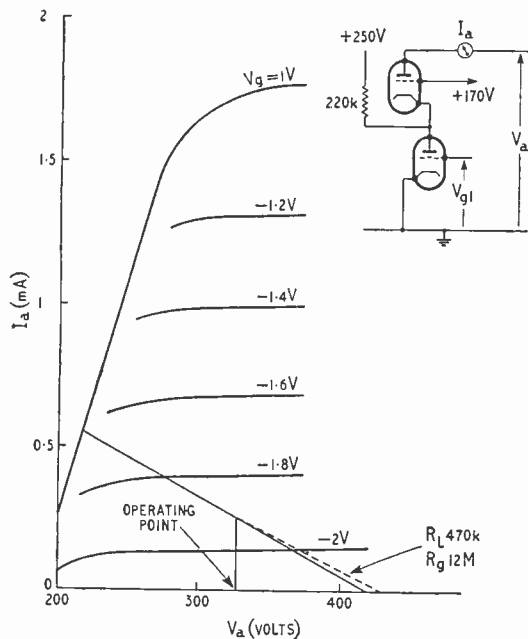


Fig. 11 Operating potentials of the cascode pair.

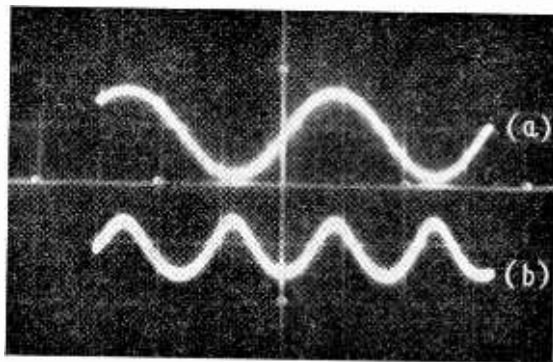


Fig. 12 Degree of balance in an experimental audio amplifier is shown by these oscillograms: (a) amplifier output voltage, (b) output stage cathode current.

the operating voltages. Figures underlined are peak-to-peak a.c. voltages relative to earth for a push-pull output of 200V peak-to-peak. The measured push-pull gain is some 500 times, and with feedback taken from a resistive divider connected between the output terminals, the push-push gain is -88 dB relative to the push-pull gain. Although a pentode is the ideal cathode impedance, the above figures demonstrate that it is frequently possible to obtain the required characteristics with a triode.

Experimental Audio Amplifier

An experimental 10-watt audio amplifier which utilizes overall push-push feedback has been built (and it is hoped to describe a development of this amplifier in a future article). The amplifier embodies

a modified cascode phase splitter of the type described above. The phase splitter precedes a Class A pentode output stage, and the push-push feedback loop is taken from the common cathode bias resistor of the output stage to the grid of a pentode forming the cathode impedance of the cascode pair. The degree of balance obtained with components of 20% nominal tolerance may be seen from Fig. 12. The upper trace displays the output waveform at an output of 11 watts. The lower trace shows the residual voltage across the output stage cathode resistor. This represents an alternating h.t. current which is predominantly second harmonic and which has an r.m.s. value of 500 μ A. This compares favourably with the peak anode current per valve, which is 120mA. Practical advantage of this

feature is reflected in an extremely simple RC power supply, which may be used to feed a high-gain pre-amplifier simultaneously, without risk of instability; and a signal/hum ratio in excess of 60 dBm.

Finally, the author would like to thank many of his colleagues, and in particular K. W. Moulding and P. L. Mothersole, for encouragement and help in the preparation of this article.

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Causes of Low Outputs*

WHY AUDIO OUTPUT STAGES OFTEN DO NOT ACHIEVE THE EXPECTED PERFORMANCE

IN some valve manuals the data for most types of output pentode include a figure for the output power available at 10% total harmonic distortion. It is not always realized that this figure represents the power available at the valve with the values of voltages, current and external anode resistance quoted. Consequently, the values of output power actually obtained in practical equipment are often lower than those which seem, from the data, to be available.

The values of output power quoted in the manuals are usually given for fixed bias and screen-grid voltages because these closely represent the values actually available for speech or music reproduction. Where a cathode-bias resistor and/or a series screen-grid resistor are used, measurements with a continuous sine wave will show lower output powers than those obtained with fixed voltages. At full drive, the screen-grid current will be appreciably higher than without the signal. Therefore, if the signal is a sustained sine wave, the valve operating conditions will readjust themselves to an increased bias voltage and/or a reduced screen-grid voltage. During the reproduction of speech or music, the waveforms are complex and the sine waves are never sustained at full-drive amplitudes for a long enough time to affect the valve operating conditions.

If it is desired to know how much power is available at a certain level of distortion under speech or music conditions, the direct voltages between the various electrodes and the cathode can be measured and can then be maintained at these values by auxiliary supplies. As a rough guide, the output power measured with a sustained sine wave under cathode-bias conditions is approximately 10% less than that measured with a fixed bias voltage. A simple correction allowing for the effect of a screen-grid resistor cannot be given—it depends both on the value of the resistor and on the ratio of screen-grid current at zero signal to that at full drive.

The voltages quoted in the valve manuals are usually given with respect to the cathode, and should not be confused with the voltage between the h.t.

line and the chassis. Usually, the actual anode voltage will be the h.t. line voltage less the voltages dropped across the primary winding of the output transformer and the cathode resistor.

Valve manuals usually give an optimum value of effective external anode load resistance, and the output power quoted is for this optimum value. At all other values of resistance, the output power will be lower. For single-valve operation, if the effective anode load resistance R_a is greater than the optimum value $R_{a(opt)}$, the anode voltage swing at a given distortion is almost independent of the value of R_a .

For a resistance less than the optimum, the anode current swing is roughly independent of R_a .

Therefore, for $R_a > R_{a(opt)}$:

$$P_{out} \approx \frac{R_{a(opt)}}{R_a} \times P_{out(opt)}$$

and for $R_a < R_{a(opt)}$:

$$P_{out} \approx \frac{R_a}{R_{a(opt)}} \times P_{out(opt)}$$

where P_{out} and $P_{out(opt)}$ are the values of output power corresponding to R_a and $R_{a(opt)}$ respectively.

One of the most common causes of mismatching is that the resistances of the primary and secondary windings of the output transformer and of the leads to the loudspeaker have been neglected. The effect of the resistance of the secondary winding and the speaker leads is to increase the secondary load resistance. The effect of the primary resistance R_p is twofold: it increases the external anode load resistance, and it influences the valve operating conditions in that it lowers the anode voltage and, hence, the optimum anode load resistance. The effective external anode load resistance R_a is given by:

$$R_a = R_p + n^2 (R_s + R_L)$$

where n is the transformer turns ratio, R_s is the

*This article is based on a report in *Mullard Technical Communications*, Vol. 4, No. 40 (August 1959).

resistance of the secondary winding and R_L is the secondary load resistance (including the resistance of the leads). Corrections to the optimum value of anode resistance can be made if it is assumed that the optimum value is roughly proportional to the anode voltage and the reciprocal of the anode current.

Practical Example.—Some time ago it was found that, in an amplifier which incorporated a single-ended EL84 audio output stage, the anode current was low with many samples of the valve and the output power delivered to a 7.5Ω secondary load was only $2W$ instead of the $4.2W$ indicated in the valve manual. The h.t. line voltage in the amplifier was $250V$, and the current in the output stage was $36mA$. The relevant data, abstracted from the valve manual, are given below:—

V_a	=	$250V$
V_{g2}	=	$250V$
R_a	=	$7k\Omega$
R_k	=	210Ω
V_{g1}	=	$-8.4V$
I_a	=	$36mA$
P_{out} ($D_{tot} = 10\%$)	=	$4.2W$

It was found that a cathode resistance of 210Ω was used in the output stage of the amplifier. The actual screen-grid voltage (with reference to the cathode) was therefore only about $242V$, which explained why the anode current was often low.

However, the loss in power resulted mainly from mismatching and the resistance of the windings of the output transformer. Measurements showed that the turns ratio of the transformer was $30.5 : 1$,

which transforms 7.5Ω connected to the secondary winding into $7k\Omega$ across the primary. However, the primary resistance was 700Ω and the resistance of the secondary winding was 0.9Ω .

The current of $36mA$ through the primary winding caused a voltage drop of $25V$, so that the actual anode-to-cathode voltage was only $217V$. At this voltage, the optimum anode resistance for an EL84 is approximately $(217/250) \times 7$, or $6.1k\Omega$, and at this optimum value the output power would be $(217/250) \times 4.2$, or $3.65W$. However, the transformer, with its winding resistances and a secondary load of 7.5Ω , presented to the valve an effective anode resistance given by:

$$R_a = 700 + (30.5)^2 (7.5 + 0.9)\Omega.$$

That is, the effective anode resistance in the amplifier was $8.5k\Omega$. The output power available from the valve at this optimum value is approximately $(6.1/8.5) \times 3.65$, or $2.63W$. There is, however, a loss of power of $0.47W$ in the resistances of the primary and secondary windings, so that the useful power delivered to the load is about $2.2W$ instead of the expected $4.2W$.

Because the calculation of output power at an anode resistance different from the optimum is only approximate, and also because the transformer resistances were measured on a cold transformer, this value of $2.2W$ is in reasonable agreement with the output of $2W$ obtained with the amplifier. A small reduction in the cathode resistance, and the use of a different, though somewhat larger, output transformer ($R_p = 305\Omega$, $R_s = 0.2\Omega$, $n = 28.3$) resulted in an increase in output power to $3.5W$ delivered to a secondary load of 7.5Ω .

Phonetic Alphabet

IT is understood that many hours were spent during the Geneva Conference discussing the merits and demerits of the various phonetic alphabets now in use, before adopting the one which has been used by N.A.T.O. forces and civil airlines since March 1st, 1956. It is a great improvement on the alphabet incorporated

in the Atlantic City Regulations (1947), and will be used in international radiotelephony from May 1st next year when the Geneva Regulations come into force. However, even after that date stations of the same country may continue to use when communicating between themselves any other phonetic alphabet recognized by their own administration.

We give in the table first the N.A.T.O./I.C.A.O. phonetics adopted at Geneva (with the syllables to be emphasized in heavy type), then the well-known Able-Baker-Charlie list, which is still used for working between British ships and British coast stations, and finally the cumbersome words approved at Atlantic City which will continue to be used for international working until the Geneva Regulations are introduced.

The first ten words of the new alphabet are also to be used for verifying the numerals 1 to 0 respectively, and the following four words for a comma, fraction bar, break sign and full-stop. When transmitting figures or marks they must be preceded and followed by the words "as a number" or "as a mark" spoken twice, e.g., the number 1960 will read: "as a number, as a number, Alpha, India Foxtrot Juliet, as a number, as a number."

This method of verifying numerals is not used by operators in British ships and coast stations. The G.P.O. "Handbook for Wireless Operators" gives the following rules for the pronunciation of numerals: 0, zero; 1, wun; 2, too; 3, thuh-ree; 4, fo-wer; 5, fi-yiv; 6, six; 7, seven; 8, ate; 9, niner. Each transmission of figures is preceded and followed by the words "as a number" spoken twice.

A	Alfa	Able	Amsterdam
B	Bravo	Baker	Baltimore
C	Charlie	Charlie	Casablanca
D	Delta	Dog	Danemark
E	Echo	Easy	Edison
F	Foxtrot	Fox	Florida
G	Golf	George	Gallipoli
H	Hotel	How	Havana
I	India	Item	Italia
J	Juliet	Jig	Jerusalem
K	Kilo	King	Kilogramme
L	Lima	Love	Liverpool
M	Mike	Mike	Madagascar
N	November	Nan	New York
O	Oscar	Oboe	Oslo
P	Papa	Peter	Paris
Q	Quebec	Queen	Quebec
R	Romeo	Roger	Roma
S	Sierra	Sugar	Santiago
T	Tango	Tare	Tripoli
U	Uniform	Uncle	Upsala
V	Victor	Victor	Valencia
W	Whisky	William	Washington
X	X-ray	X-ray	Xantippe
Y	Yankee	Yoke	Yokohama
Z	Zulu	Zebra	Zurich

COLOUR TELEVISION FROM PARIS

DEMONSTRATION OF FRENCH SYSTEM AT THE I.E.E.

TECHNICAL history was made in a small way on the evening of 27th April, when colour television pictures were relayed for the first time from Paris to London. The occasion was a lecture at the I.E.E. on the Henri de France system of colour television, by R. Chaste and P. Cassagne of, respectively, the Compagnie Générale de Télégraphie Sans Fil and the Compagnie Française de Télévision, in which organizations the system has been under development. (C.F.T. is a subsidiary of C.S.F.) After the formal paper a demonstration was given, on colour and black-and-white receivers, of compatible colour pictures transmitted on the Henri de France system over a special relay network from the C.F.T. laboratories in Paris. The 625-line television standard was used and the programme material consisted of colour slides and colour films.

A 500-km television relay system was specially arranged for this occasion as a joint effort by the French P.T.T., British Post Office and B.B.C., and was described by W. J. Bray of the Post Office. It used a number of existing installations and some temporary stations. A temporary microwave link connected the C.F.T. laboratories to the P.T.T. establishment at the Tour de Meudon in Paris, from which the signals passed to Loos (near the town of Lille) on the permanent P.T.T. microwave relay system. From Loos they were transmitted to the Post Office radio station at Tolsford Hill, near Folkestone, by the permanent G.P.O./P.T.T. microwave link which normally serves for Eurovision and multi-channel telephony circuits.

The connection from Tolsford Hill to London was not made by the existing cables because these can only handle a bandwidth of 3Mc/s, whereas the 625-line colour signals require their normal 5Mc/s. Two temporary microwave links, connected in tandem, were therefore set up by the B.B.C., terminating at the Crystal Palace television station. From Crystal Palace the rest of the link-up to the I.E.E. was made by coaxial cable via Broadcasting House, the Post Office switching centre at the Museum telephone exchange and the Gerrard telephone exchange.

Characteristics of the System

Some readers may recall that the Henri de France system of colour television* has certain features in common with the American N.T.S.C. system, now operating in the U.S.A., but is distinguished by the sequential method of transmitting the chrominance (colour without brightness) information. It is a compatible system which transmits the brightness information in a wide band on the main carrier, so that it can be picked up by existing monochrome receivers as a black-and-white picture, and the chrominance information on a narrow-band sub-carrier. As in the N.T.S.C. system, the colour sub-carrier conveys two sets of chrominance information (called colour difference signals), but sequentially, on alternate lines, rather than simultaneously by an amplitude- and phase-modulation multiplexing process.

At the colour receiver the sequential colour informa-

tion is turned into simultaneous form for display by a storage system based on a delay line. Thus the complexity of the synchronous detectors and associated circuits of the N.T.S.C. receiver is avoided, but a somewhat expensive delay line is required. The whole transmission system, unlike the N.T.S.C. one, is insensitive to spurious phase delays (as was demonstrated at the I.E.E. by the deliberate introduction of 40° of phase change in the incoming cable) and the receivers are inherently stable. On the other hand there is a loss of vertical colour definition, due to the line sequential method of transmitting the colour information, and a slight misregistration of displayed colour information, due to the fact that the storage causes colour information belonging to one line to be presented also on the next line of the frame (next-but-one of the picture).

Colour Receiver Design

Such points were brought out at the discussion following the lecture by various speakers, the majority of whom were critical of the Henri de France system but at the same time expressed their appreciation of the excellent demonstration and their admiration for the French authors' presenting a paper in a foreign country and in a foreign language. Regarding the receiver problem—which is certainly the main stumbling-block in the adoption of any system of colour television—it was generally felt that although the Henri de France receiver had the advantage over the N.T.S.C. receiver in fewer valves and less complexity, this was partly offset by the price of the delay line (about £6). In any case the price of receivers was largely controlled, not by these factors, but by the price of the colour c.r. tube.

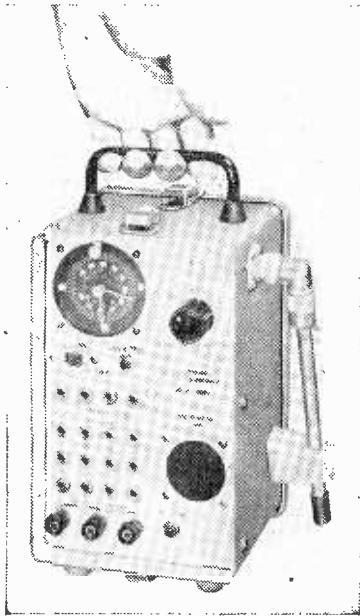
Recent work at C.F.T. has been aimed at reducing the cost and bulk of the delay line. Whereas it was originally a length of special coaxial cable, the present receiver uses a compact acoustical system based on multiple reflections inside a block of quartz to get the required path length. Other developments mentioned by the authors have been concerned with the reduction of noise visibility on the colour picture by the use of frequency modulation of the colour sub-carrier instead of amplitude modulation. With a.m. the system is somewhat worse than the N.T.S.C. system in this respect, having a threshold of noise visibility of about 7-8dB lower (both systems being worse than monochrome television). Demonstrations of pictures using the f.m. sub-carrier were in fact given at the I.E.E. Unfortunately the visibility of the f.m. sub-carrier on the picture is greater than that of the a.m. sub-carrier, but experiments are in progress to reduce this by trying sub-carrier frequencies specially related to the line scan frequency.

On the question of standards, one speaker reminded any members of the Television Advisory Committee present (in fact there were several) that the French had shown us colour television on 625 lines. Representatives of the B.B.C. and the French Centre National d'Etudes des Télécommunications put in heartfelt pleas for common international standards for colour television, saying that they had suffered enough already from different standards in monochrome!

* As described in our September 1957 issue, under the title "Sequential Colour Again."

Technical Notebook

Portable Time Standard, controlled by standard time transmissions, has been developed by Zenith in the U.S.A. It is a transistorized, battery-powered instrument, and is accurate to approximately ± 16 seconds per year. A possible



application is for precise time switching of recording instruments, telemetering transmitters, etc., in isolated areas. The instrument uses a transistor receiver—a crystal-controlled a.m. circuit—and is designed to receive the National Bureau of Standards station WWV, and other accurate sources of “seconds tick,” at any of three frequencies, 2, 5 and 10Mc/s. The receiver output is fed to a circuit which filters out all information except the one-second “tick.” This “tick” is applied to a pulse generator which gives a pulse of the required amplitude and duration to synchronize the electric clock (a type in which the balance wheel operates contacts for pulsing the mechanism). A “programme matrix,” comprising a set of contacts utilizing the clock hands, is capable of providing a variety of switching time intervals for controlling external

apparatus. An aural check of WWV signals is also incorporated.

Polymerization of Propylene (formula C_3H_6 —the “next one up the chain” from ethylene, C_2H_4) by methods similar to those used to produce polyethylene, or polythene, result in a substance of very variable and not very useful properties. This variability is caused by the random placing of the “extra” CH_3 groups along the polymer molecule. However, research undertaken in Italy has resulted in the discovery of a new catalyst for the polymerizing process, a catalyst which enables the CH_3 groups to be aligned in a regular fashion. The result is a polymer of propylene with consistent and useful properties; in fact, it seems to possess most of the advantages of polythene and few of its disadvantages. Most valuable features of polypropylene for electronic purposes are its high melting point ($170^\circ C$ approx. compared with $108^\circ C$ approx. for polythene), its hardness (Rockwell 90 to 95), small linear coefficient of expansion ($11 \times 10^{-6} cm/cm/^\circ C$) and high tensile strength ($4,000 lb/in^2$). In other respects it is broadly similar to polythene. Polypropylene is made in this country by the Telegraph Construction and Maintenance Company in the basic form of sheets from 0.020in to 0.375in thick, and it may be processed by all methods at present used with polythene (higher processing temperatures must, of course, be used).

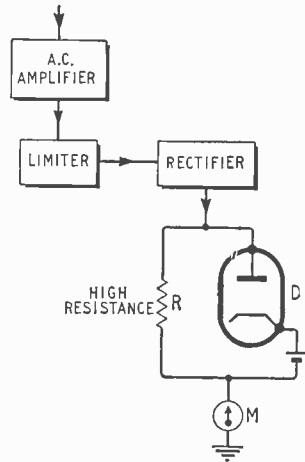
Minute Sealed Switch, only 0.32in diameter by 0.44in long, has a breaking capacity of 3A at 28 volts (resistive load). Of welded stainless-steel



construction, the switch has a snap-action W-shaped blade operated by a push button, and the casing, before

being hermetically sealed, is filled with an inert gas. The photograph shows the switch (made by Spencer Products Group, Texas Instruments, U.S.A.) against a background of aspirin tablets.

Balance Indicating non-linear amplifier forms part of audio-frequency current and voltage standardizing equipment developed by the Electrical Inspection Directorate. The standardization is carried out by means of thermo-junctions working at a fixed input current level. To avoid damaging or altering the characteristics of these thermo-junctions, the level must be set close to the fixed value before they are connected. This initial level setting is achieved to within 0.2% by means of a non-linear amplifier whose output is arranged to vary rapidly with the input when this input is near the required fixed value, but only slowly with the input otherwise. The output of the non-linear amplifier thus



provides a sensitive indication of when the input is near the required fixed value. The non-linear amplifier consists basically of an ordinary a.c. amplifier followed by a limiter and rectifier; across the rectifier output is connected a biased diode (D) in parallel with a high-value resistor (R) and in series with the output meter (M). At low input levels to the non-linear amplifier the biased diode does not conduct so that the output meter is fed from the high resistance. Thus the output meter reading increases only slowly with the input level at low input levels. Just below the fixed input level the biased diode suddenly starts to conduct and short circuits the high resistance feeding the output meter. Thus the output meter reading increases rapidly with the input near the fixed input level. At still higher input levels the limiter ensures that the meter reading again increases only slowly with the input level.

Elements of Electronic Circuits

14.—THE MILLER TIMEBASE

By J. M. PETERS, B.Sc. (Eng.), A.M.I.E.E., A.M.Brit.I.R.E.

ONE of the most widely used linear timebase generators depends for its action on the Miller integrator circuit, in which negative feedback is introduced by an externally coupled capacitor between anode and grid. A single valve is used to control the charging and discharging of the time-base capacitor, which is initiated by switching pulses applied to the suppressor grid. It may be noted here that variations of this circuit (such as the "phantastron") differ in respect of the method of switching and the complexity of the associated amplifier circuit.

Before attempting to describe the operation of the circuit shown in Fig. 1 it will be necessary to

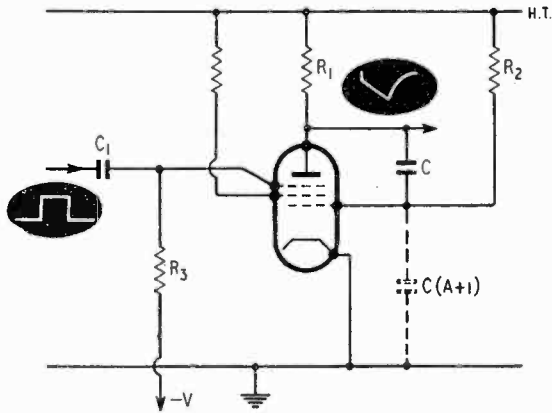


Fig. 1

understand what is meant by the Miller effect. First, let us consider a triode amplifier with gain $=A$, the valve developing its output voltage across a resistive load. As the anode voltage is 180° out of phase with the input voltage it can be shown that feedback to the grid is introduced by the inter-electrode capacitance C_{ga} . This has the effect of modifying the input capacitance of the valve, which can be written $C_{input} = C_{gk} + C_{ga}(1+A)$, the suffixes representing the respective inter-electrode capacitances. This increase in input capacitance, i.e., $A.C_{ga}$, is due to the Miller effect (named after its discoverer, J. R. Miller, in 1919).

A capacitor connected externally between the anode and control grid of a pentode amplifier will modify the input capacitance in a similar fashion, and this is the basis upon which the circuit shown in Fig. 1 operates. In this circuit the control grid is connected to a positive voltage source through a high-value resistor, R_3 , and it is also connected to the anode via a capacitor, C . The grid circuit can therefore be regarded as consisting of a resistor R_3 in series with a capacitor $C(A+1)$.

Referring to the waveform diagram in Fig. 2, the action of the circuit is as follows:—

Stage (a)

The suppressor is biased to a negative voltage via R_3 sufficient to prevent the flow of anode current, so that initially the valve is cut off as far as the anode is concerned, and V_a is at h.t. voltage. Grid current flows since g_1 is just above cathode potential (a few volts positive). C is charged practically to h.t. voltage.

Stage (b)

The action starts with the application of a positive-going square pulse to g_3 . This is sufficient to cause anode current to flow. V_a falls and this drop in voltage is applied via C to g_1 . As g_1 goes negative, less anode current flows; therefore V_a tends to rise. A state of equilibrium is eventually reached when

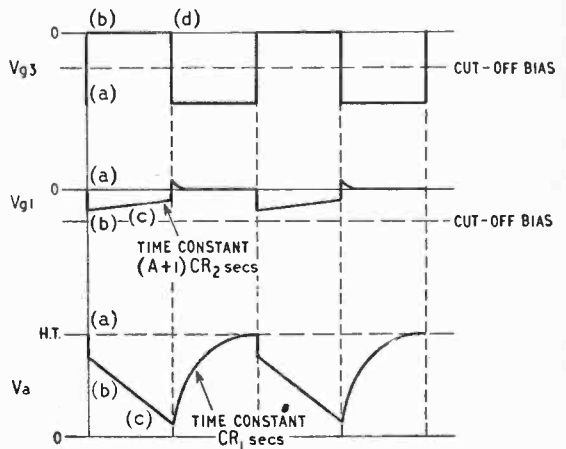


Fig. 2

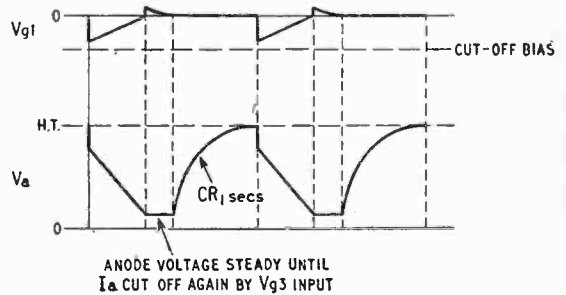


Fig. 3

the anode current is only just sufficient to cause a voltage drop in R_1 equal to the amount V_{g1} has gone negative from its original potential. V_{g1} is now negative and I_{g1} ceases.

Stage (c)

The side of C connected to g_1 is negative and as it is tied to h.t. via R_2 the h.t. voltage tries to charge it in the opposite direction through R_2 . The voltage across C gradually falls. V_{g1} gradually rises and V_a consequently falls. The rate at which V_{g1} rises (V/CR volts/second in a CR circuit) is

$$\frac{V}{C(A+1)R_2} \text{ volts/second, where } V \text{ is the h.t.}$$

voltage. The time constant is $(A+1)CR_2$ seconds. Note that C becomes $(A+1)C$ due to the Miller effect described above. V_a changes at A times the rate of change of grid voltage; therefore V_a falls at

$$\frac{V}{C(A+1)R_2} \times A \text{ volts/sec}$$

This can be written

$$\frac{V}{CR_2} \times \frac{A}{A+1} \text{ volts/sec}$$

Now if A is large (pentode amplifier) $A/(A+1) \approx 1$. Therefore the rate of fall becomes V/CR_2 volts/sec,

which is independent of the valve characteristics—an important attribute of this circuit. This is therefore the timebase sweep voltage.

Stage (d)

When the input square pulse ends, the suppressor voltage again cuts off the anode current and V_a rises, carrying V_{g1} with it until I_{g1} flows. C charges exponentially in the opposite direction through R_1 with time constant CR_1 (not $C(A+1)R_1$ as the Miller effect is now absent since the valve is not amplifying during this period). V_a finally reaches h.t. and the cycle of operation ceases.

If we make R_2 a smaller value, or if the square pulse which starts the action lasts long enough, the grid current region will be reached before the end of the period. This is illustrated in Fig. 3. V_a remains steady until the pulse on the suppressor ends and the recovery phase begins. Thus the slope of the timebase waveform can be altered by varying R_2 .

Provided that A is large, the slope has been shown to be independent of the valve characteristics and also of the anode load R_1 . The output impedance of the circuit is therefore low (approximately $1/g_m$). This means that the Miller timebase can develop its waveform with negligible distortion across quite low impedances.

Calculation of Standing Wave Ratio

Effects of the Terminating Load on Line of Known Characteristic Impedance

By JOHN E. ROBSON*, B.Sc., A.M.I.E.E.

IT was the author's original intention to sub-title this article, "or how to do without a Smith Chart," but this would have seemed ungracious in view of R. A. Hickson's excellent series of articles on the subject.¹ However, the problem does arise in practice, and the main result obtained here is the outcome of a frequently recurring situation.

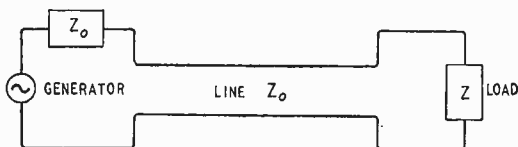
The essence of the problem is shown in Fig. 1. A transmission line of given characteristic impedance Z_0 is being driven by a generator, whose output impedance is taken as Z_0 also for the sake of simplicity, and is terminated in an impedance of value Z. What effect will this have on the performance of the system?

In an actual case, which does occur in practice, the generator of Fig. 1 is a source of signals in the frequency range 3 to 10Mc/s, the line is a coaxial cable for which Z_0 is 75 ohms resistive, and the terminating impedance Z is the input impedance of a level indicator or a receiver. The expression "the effect on the system" comes down to mean "the standing wave ratio," or "the return loss" caused by the impedance.

The Importance of Standing Wave Ratio.—In some previous treatments of the problem, the existence of standing waves was taken merely as an

indication that all was not well at the far end of the line. Most probably, there was an amount of mismatch between the line and the load: in other words, the load was not exactly a pure resistance in value equal to that of the characteristic of the line. In fact, Hickson showed how a measurement of the magnitude and spatial distribution of the standing wave could be manipulated to provide a value for the terminating impedance. It is the purpose of this article to look at the problem from the other side; that is, to take a given impedance, and determine the standing wave ratio caused by it on a line of given characteristic impedance. This is the viewpoint of the transmission line engineer, who regards a standing wave as a bad thing in itself, being caused as it is by reflected power. The line has to be made "flat," and there are in general, many more than one

Fig. 1. Transmission line of characteristic impedance Z_0 driven by a generator and terminated in a load of value Z



*Redifon Ltd., Crawley.

junction at which reflection can take place. It is for this reason that the transmission line engineer works in terms of return loss, and here the author can do no better than refer to an earlier series of articles.² Another situation in which a high standing wave ratio is an inherently bad thing is that of a transmitter feeding an aerial via a transmission line. If the transmitted power is large, then dangerously high voltages can be developed across the line conductors, or even within the transmitter. Again, long before the danger point has been reached, the attenuation, or power loss in the line, has begun to rise quite steeply. In brief, the extra power losses at the high-voltage points on the standing wave pattern are not made good by the reduced losses at the low-voltage points.

Determination of Standing Wave Ratio.—

Several measurement techniques have been evolved to determine the standing wave ratio, either by direct measurement or by calculation from a measurement of a related quantity. Thus, by means of a slotted line and probe, the electric field distribution along a line under given conditions of termination may be explored, and this will give the required quantity directly. Unfortunately, the line needs to be at least one half-wavelength long at the frequency of interest, and at 10Mc/s that would mean a line of some 47ft long.

Then the power flow in each direction along the line can be sampled, and two readings obtained which are proportional to the forward and to the reverse power flow. This technique is that of the Reflectometer, and "Cathode Ray" has recently illuminated it for us⁴.

Finally, a kind of radar method can be used, in which signal pulses are sent off up the line, and the returns are displayed on a cathode-ray oscilloscope. This method is of wide application, though obviously the technique is fairly sophisticated.

A method will now be described in which a single impedance measurement is sufficient to allow of calculation of standing wave ratio.

Calculation from Impedance Measurement.—

If the terminating impedance is purely resistive, and equal in value to the characteristic impedance of the line, then it is well known that no reflection of power will take place at the load. Everywhere along the line, the relationship $V = Z_0 I$ will hold, including at the load itself. Now if the load is not equal to Z_0 , then that relationship cannot hold, and so some power is sent back. It is easy to see that if the load is purely resistive and of a different value from that of Z_0 , then there will be no phase change in voltages or currents, and the standing wave ratio will be given by $S = Z_0/R$ or R/Z_0 . That fraction is chosen which makes S greater than unity, as the use of this convention appears to be increasing.

The next step is to consider the effect of a loading impedance which includes some reactance. For even if the resistive part of the load is equal to the Z_0 of the line, the relationship $V = Z_0 I$, which holds good for either wave on the line, cannot hold equally for a load in which $Z = R_0 + jX$.

Consider now the situation as shown in Fig. 2. This illustrates part of the complex plane of impedance: in other words, two axes are drawn at right angles, the real, or resistive, and the imaginary, or reactive. With reference to these axes, points may be plotted which represent impedances. The two impedances actually shown are the terminating

impedance $Z_1 = R_1 + jX_1$ and the characteristic impedance of the line Z_0 . This is purely resistive, and so is represented by a point on the real axis.

Now the value of standing wave ratio at the load, due to the particular value of Z , can be denoted by S_1 , and the question arises, do any other values of terminating impedance give rise to this same value, S_1 ? This question can be put another way; given any value of standing wave ratio, what shape will the curve be which passes through all the points on the plane with that value? The answer is, interestingly enough, a circle, and a quick derivation of this result is now given.

By definition, the standing wave ratio is:—

$$S = \left| \frac{1 + K}{1 - K} \right|$$

where K is the ratio of reflected voltage to forward voltage. Recalling that a phase change occurs for a

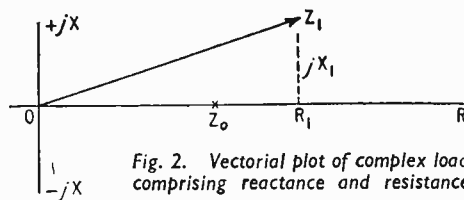


Fig. 2. Vectorial plot of complex load comprising reactance and resistance

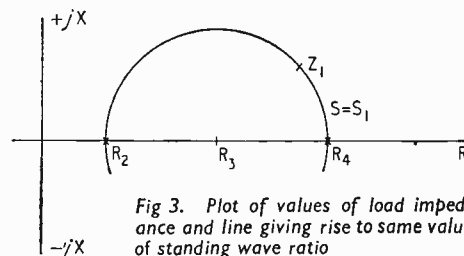


Fig. 3. Plot of values of load impedance and line giving rise to same value of standing wave ratio

reactive load, it can be seen that K in general will be complex, that is, of the form $x + jy$.

This leads to:—
$$S = \left| \frac{1 + x + jy}{1 - x - jy} \right|$$

and so:—

$$S^2 = \frac{(1 + x)^2 + y^2}{(1 - x)^2 + y^2}$$

After a little algebra this comes out to be:—

$$y^2 + x^2 - 2x \frac{S^2 + 1}{S^2 - 1} - \frac{1}{S^2 - 1} = 0$$

which is the equation of a circle.

Fig. 3 shows part of one such circle passing through the point representing the particular impedance $Z_1 = R_1 + jX_1$. In order to be able to describe this circle we need to know its centre and its radius, that is, to be able to determine the points R_2 , R_3 and R_4 along the real axis. The points R_2 and R_4 are given by terminating loads of those values, and, it is to be noted, purely resistive in nature. Thus an earlier result can be used, and the value of standing wave ratio written at once as:—

$$S = \frac{R_4}{Z_0} \text{ and } S = \frac{Z_0}{R_2}$$

The reason for the inversion of one fraction is that

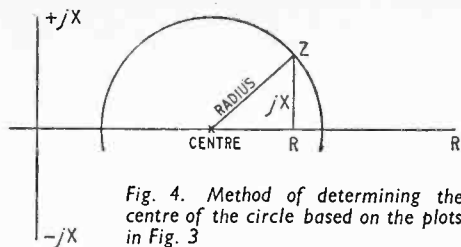


Fig. 4. Method of determining the centre of the circle based on the plots in Fig. 3

one value of resistance is greater than Z_o , and one smaller. Thus:—

$$R_1 = SZ_o \text{ and } R_2 = Z_o/S$$

The centre of the circle is R_3 , and this is given by:—

$$R_3 = \frac{R_1 + R_2}{2}$$

which means that the circle has its centre at the point:—

$$\frac{SZ_o + Z_o/S}{2}$$

Again, the radius of the circle is given by:—

$$\frac{R_1 - R_2}{2} = \frac{SZ_o - Z_o/S}{2}$$

Finally, the line is terminated in any impedance $Z = R + jX$, and so the circle of constant standing wave ratio must pass through this point. This means that the distance from the centre to the point Z is equal to the radius of the circle. Thus there is a right-angled triangle shown in Fig. 4 whose sides are:—

$$X, R - \frac{SZ_o + Z_o/S}{2} \text{ and } \frac{SZ_o - Z_o/S}{2}$$

Applying Pythagoras gives:—

$$X^2 + \left[R - \frac{SZ_o + Z_o/S}{2} \right]^2 = \left[\frac{SZ_o - Z_o/S}{2} \right]^2$$

or

$$4X^2 + 4R^2 + S^2Z_o^2 + \frac{Z_o^2}{S^2} + 2Z_o^2 - 4RZ_o \left(S + \frac{1}{S} \right) = S^2Z_o^2 + \frac{Z_o^2}{S^2} - 2Z_o^2$$

and, on solving for S , we have:—

$$S^2 - S \left[\frac{R}{Z_o} + \frac{Z_o}{R} + \frac{X^2}{RZ_o} \right] + 1 = 0$$

Applications of the Result.—The equation just arrived at is of great interest, and the author believes it to be original, never having seen that result stated in the literature. Its interpretation is straightforward: given a line of characteristic impedance Z_o , and a terminating load Z , whose components as measured on an impedance bridge are R and jX , then a value of standing wave ratio at the load will be observed, as given by the expression for S .

It would appear that, as the equation is quadratic in S , the two roots will give two differing values of S . That this is not so can be seen by noting that the equation is of reciprocal type, which means that if $S = \alpha$, say, is one root, then $S = 1/\alpha$ is the other. This follows from the well-known point in the theory of equations that the constant term is the product of all the roots taken singly, and the fact that the constant term in the equation for S is unity.

This result can perhaps be expressed more fanci-

fully by saying that one root of the equation gives S in its British form, and the other root in American.

As an interesting check on the correctness of the approach, set the reactance term equal to zero; in other words, consider a purely resistive load of value R . Then the equation reduces to:—

$$S^2 - \left[\frac{R}{Z_o} + \frac{Z_o}{R} \right] S + 1 = 0$$

Here again the theory of equations helps, for the sum of the roots is the negative of the coefficient of S , and so the roots are obviously R/Z_o and Z_o/R . Which is the correct value for the standing wave ratio under that circumstance.

Reverting to the general equation, it may well be that the measurement of the termination is in the form of parallel admittance components, and over the radio frequency range under consideration this is the more likely case. Then the unknown will be stated as $Y = G + jB$, and the line will have a characteristic admittance of Y_o . The equation then becomes:—

$$S^2 - \left[\frac{G}{Y_o} + \frac{Y_o}{G} + \frac{B^2}{Y_o G} \right] S + 1 = 0$$

and the conclusions are unchanged.

There is one particularly useful feature of the equation whenever normalized impedances, or admittances, are employed. The termination will then be written as:—

$$\frac{Z}{Z_o} = \frac{R}{Z_o} + j \frac{X}{Z_o}$$

or

$$Z' = R' + jX'$$

the primes denoting normalized values. With this in mind, the basic equation may be written at once as:—

$$S^2 - \left[R' + \frac{1}{R'} + X' \left(\frac{X'}{R'} \right) \right] S + 1 = 0$$

owing to the fact that the various ratios within the bracket are already normalized.

One final point concerns the actual solution of the equation. No explicit solution for S has been exhibited, as the author feels nothing is gained thereby. It is best to substitute actual measured values, and solve the resulting simple quadratic equation.

As an example; the normalized form of an impedance is:—

$Z' = 0.6 + j0.4$. Thus we have $R' = 0.6$; $X' = 0.4$ and $X'/R' = 2/3$. Substituting in the basic equation gives:—

$$S^2 - \left[0.6 + \frac{1}{0.6} + 0.4 \times \frac{2}{3} \right] S + 1 = 0$$

$$S^2 - 2.53S + 1 = 0$$

and

$$S = 2.04 \text{ or } 0.49$$

and it can be checked that these are reciprocal values.

REFERENCES

- 1 R. A. Hickson: "The Smith Chart," *Wireless World*, Jan., Feb. and March, 1960.
- 2 Thomas Roddam: "Return Loss": *Wireless World*, Nov. and Dec., 1957.
- 3 "Cathode Ray"; "The Reflectometer": *Wireless World*, March, 1960, p. 137.

LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

Negative Impedance

IN your May issue Mr. D. L. Clay has responded to my request to explain what he means by negative impedance, but he has still not convinced me that anything but confusion is to be gained by the concept. In an attempt to avoid the confusion invited by using "negative" in two different senses with reference to the same thing, he rules out the combination of a positive resistance and the reactance of a negative component, because it is unstable. On the same ground he must rule out the combination of a negative resistance and the reactance of a positive component. Since the latter is a commonly occurring one, its exclusion to suit Mr. Clay would be inconvenient.

He also appears to confuse dissipative losses due to the resistance of a reactor with the energy taken in by its reactance and returned in full during the same cycle.

Again, his use of the word "complex" in connection with impedance leaves one in doubt whether it is to be interpreted in its usual mathematical sense in that context or just as meaning "not simple."

I hope I am correct in interpreting his further remarks on phase difference as illustrating the worthlessness of any attempt to apply this concept to dissimilar wave-forms.

Regarding Ohm's law and negative resistance: Mr. Clay said in his first letter "further explanation is wanted here." His second letter has convinced me that it is. But if I tried to compress it into a letter the confusion I appear to have created already might be worse confounded.

"CATHODE RAY"

Circuit Conventions

THE letter from Mr. Bedford (April issue) and your own comments on circuit conventions were interesting. The function of a circuit drawing is to convey information to the reader "unambiguously and without interference to thought sequences" of that reader. Is not the draughtsman's liability to error—on which the Editor appears to base his opinion—of very secondary importance?

On the other hand Mr. Bedford's mixing of X junctions (with a dot) and cross-overs (without) is indefensible. A dot omitted, or a slight merging of two ink lines and the whole meaning is changed.

In the diagrams in his letter in the April issue the loops may be acceptable to some, but more complex circuits may involve dozens—even hundreds—of "little bridges." They then become tedious to read and equally tedious and expensive to draw.

What is wrong with the recommendations of B.S.530? No X junctions, use only T junctions, and no looped cross-overs. If these sound conventions are followed the correctness of the drawing does not depend upon the presence or absence of dots and semicircles; it is more quickly drawn and traced and—most important—more easily read.

East Barnet, Herts.

V. L. BUTCHER

WHILST congratulating Mr. L. H. Bedford on his prodigious achievements between the ages of four and five (April issue), may I, as a struggling technical author, advise him not to attempt any questions on circuit drawing which may crop up in his eleven-plus examination.

The recommendations of B.S.530 are not the perfect guide by any means but, if intelligently applied, they

could make a very noticeable improvement to Mr. Bedford's Fig. 3.

However, I must side with Mr. B. (and with the B.S.I.) in deprecating the looped crossing, partly because of the time involved in drawing the wretched things.

To return to B.S.530, the requirements concerning T-junctions and crossovers are so sensible (even to a child of five), that it seems pointless to deviate from them. You see, Mr. Bedford, most diagrams have to be reduced photographically, and printed—often on inferior-quality paper—with ink which tends to spread. (Look what happened to your capacitors, Mr. B.!) It is thus quite possible to produce an accidental blob at an X junction.

I think most users of circuit diagrams would support my next point, namely that the inclusion of valve envelopes is of considerable value in identifying the separate stages in a complex circuit diagram. (How would you draw a gas-filled valve, Mr. B.?)

The following points come under the heading of "delicate points of style."

(1) If the Ω symbol is redundant in resistor values, the letter "F" is equally redundant in capacitor values (see B.S.530).

(2) The comma, such as appears in "5,000 pF" should never be used in circuit diagrams.*

(3) Those diodes are not "D," but "MR."

(4) Potentiometers are not "R," but "RV."

(5) If C26 is an electrolytic capacitor (as seems likely since the polarity is shown) it should be drawn as an electrolytic capacitor.

It would be interesting to submit Mr. Bedford's diagram to the Admiralty department which recently told me that resistors have four wiggles on one side and three on the other, and that anything else is not a resistor. (Probably Nelson drew his resistors that way.)

In conclusion, it may be relevant to point out that the majority of people concerned with the presentation of electronics diagrams blunder on, using B.S.530 as a guide, and (you may not believe this, Mr. Bedford), our readers understand us!

Belfast, 5.

L. DENNIS

* We accept responsibility for this "error"—Ed.

YOUR correspondent, Mr. Bedford, seems to have forgotten that some degree of redundancy is essential to good communications. Looped connections, giving an absence of information, prevent the mind from wandering. In his diagram, Fig. 3 (April issue), is the cross at R23, R24, R26, C23, D2 really a junction, or did the ink flow? I stop to find out and communications are interrupted.

Similarly with the valve "bottle." The valve is the centre of a stage of the circuit; the circle is a spot-light and helps in rapid assimilation.

Adding pin numbers to valves has been tried and discarded: they clutter the diagram. If numbers for valves, why not for transformers and other sub-assemblies which cannot be found in a book?

The circuit is only of interest to the man who has never seen the junk before and has to find trouble quickly and to the engineer who has to make time to read the article. Anything to help and not hinder their efforts is worth while.

While I am writing, may I ask the W.W. not to be the odd-man out when drawing transistors (as, for example, in the March, 1960, issue, p. 110). Also, though a circuit

with a negative supply at the top makes the transistor easier to us poor valve technicians, ought we not to start right with the positive at the top? Just one argument: with the negative supply at top, is a positive going pulse drawn downwards?

Bracknell, Berks.

WALTER DALTON

“Ring Angels”

I SHOULD like to comment on “Diallist’s” note on “Ring Angels” in the April, 1960, issue of *Wireless World*.

Expanding ring echoes of this kind were recorded as early as 1956 on radar equipment operated by the Meteorological Office at East Hill in Bedfordshire. They were recognized as being caused by birds. At various times since then seven different centres of ring echoes were recorded within a radius of 15 miles of the radar installation, and each one was found to be the site of a starling roost.

It is not difficult to see why these movements are seen as expanding rings. Starlings leave their roosts at around dawn in a series of “explosions,” and the echoes appear as rings because their flight paths to their feeding grounds radiate outward in almost every direction from the roost with a surprisingly uniform flight speed. Sometimes the directions of flight are more limited, and then the echoes expand as arcs rather than as rings. A description and explanation of ring echoes were given by me in *Ibis*, the journal of the British Ornithologists’ Union (Vol. 101, 1959, p. 201).

I think that few meteorologists will find support for the view that ring echoes are caused by “rapidly expanding thermal fronts in the upper atmosphere.”

Meteorological Research Unit, W. G. HARPER
Great Malvern, Worcs.

[Since receiving the above letter from Mr. Harper, an article by E. Eastwood, G. A. Isted and G. C. Rider, of the Marconi Research Laboratories, Great Baddow, has been published in *Nature* (April 9th) describing further work to establish the correlation between “ring angels” and starling flights.—ED.]

Increasing Video Gain

FOR some time past I have felt dissatisfied with the performance of the single v.f. stage fitted to television receivers. In a fringe area, the low gain obtained is a serious disadvantage.

In my efforts to obtain an image free from “ringing” and “smearing” I have evolved the accompanying circuit for a high-gain v.f. amplifier.

The exact gain *in situ* proved unexpectedly difficult to measure, but appears to be of the order of volts \times 120, and peak-to-peak output is 150 volts max. The cathode

follower is connected in a manner calculated to give maximum d.c. protection to the c.r.t. in event of valve failure. The noise suppressor is highly efficient and does not affect the d.c. restorer.

The picture obtained is really beautiful, showing the 3 Mc/s (Test Card “C”) lines with a minimum of ringing. (The exact amount of ringing is determined by the 500pF cathode bypass capacitor in the first stage.)

Peacehaven, Sussex.

R. G. YOUNG.

Deeper Amplitude Modulation?

SOME time ago, when listening on my car radio in the London area, I noticed that the French 164-kc/s transmission appeared to be louder than the B.B.C. on 200 kc/s, but a check on the receiver a.g.c. showed that the B.B.C. had the stronger carrier. I assumed that the French were using more modulation than the B.B.C., and this was confirmed recently when I had a look at both carriers on a “panadaptor,” which showed quite clearly that the French modulation, besides being considerably deeper than the B.B.C.’s, was also slightly clipped. The difference in quality was not immediately noticeable on a car radio, although it could be heard on hi-fi equipment, but this very slight loss of quality was easily offset by the great gain in intelligibility, and it occurred to me that now that the v.h.f./f.m. broadcasts are available to anyone expecting high-quality reception, the B.B.C. should adopt a higher percentage of modulation in its medium and long-wave transmissions and make them a little easier to listen to under marginal conditions, in a car or otherwise. From the amount of sideband splatter to be heard on the medium waves at night, most of the Continentals are already doing this without troubling unduly about their filtering! Another possibility is the adoption of single-sideband with carrier transmission, as used by the Voice of America on 173 kc/s.

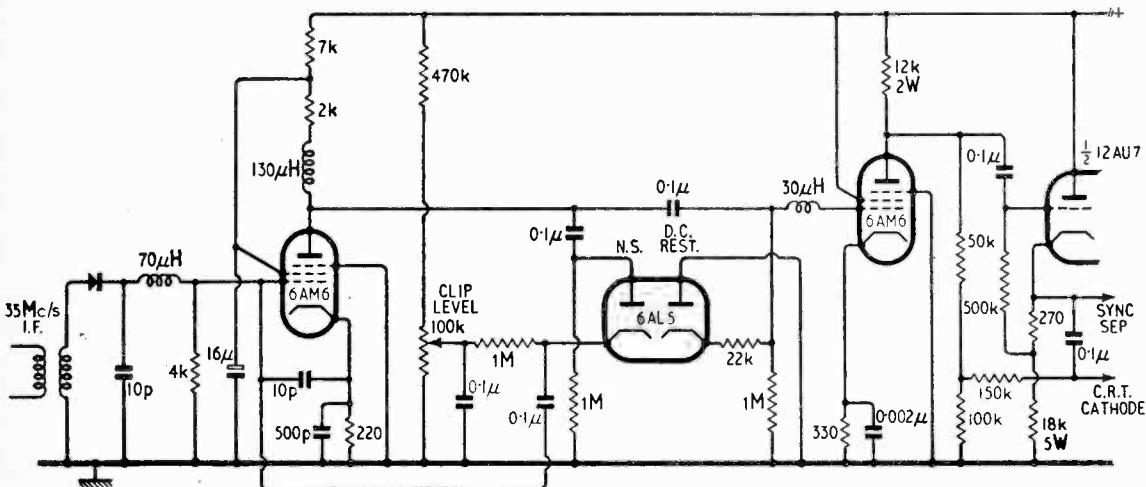
I feel that the B.B.C. should make some sort of effort in this direction, since I find that more and more of my acquaintances, having good v.h.f. installations at their homes, listen on the medium- and long-wavebands only while in their cars.

Chichester.

W. BLANCHARD

Economical High-gain A.F. Amplification

IN reply to Mr. Short’s letter in the May issue, I would first like to apologise to him for quoting a gain of less than 200 for a “straight” pentode 6BW7 amplifier. The error arose due to having just written a reply to another correspondent who was contemplating using an EF86.



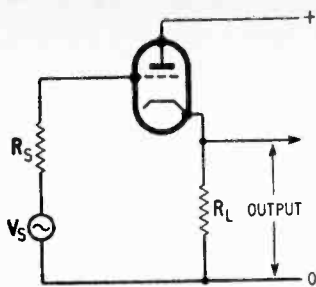


Fig. 1

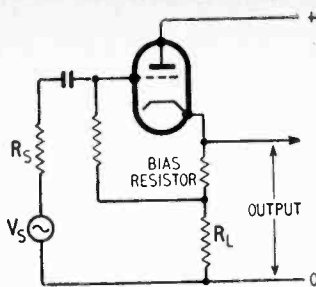


Fig. 2

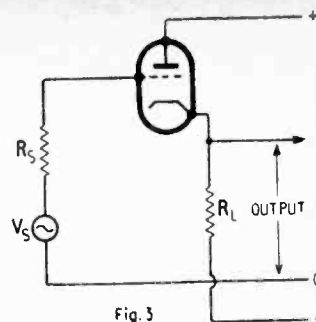


Fig. 3

I still feel, however, that 6dB loss in gain is a small price to pay in return for a stable high-gain amplifier which is not fussy about circuit layout.

With regard to Mr. Short's second point, I agree that the circuit that he shows (Fig. 1) has an output impedance that is independent of the input impedance for most practical purposes. It should be noted, however, that the output voltage is limited to a small amount due to the voltage drop across R_L providing the valve bias. For a 12AT7 valve operating with 250 volts on the anode at an anode current of 10 milliamperes, the correct operating bias is about 2.5 volts. This makes R_L equal to 250Ω . The peak output voltage will be in the region of 2.5 volts also and the output impedance will be less than $1/g_m$ ohms (180Ω) as R_L is in parallel with

the output impedance of the valve itself. To give increased output voltage the circuit shown in Fig. 2 is normally used, this providing bias by feeding back only a small amount of the d.c. voltage across the cathode load. This, however, makes the output impedance of the cathode follower vary with the input impedance.

To overcome both difficulties, the circuit shown in Fig. 3 can be used if a negative supply is also available. This has the same advantage as Mr. Short's circuit in being d.c. coupled but can give a much greater output as the valve bias is developed automatically and is much less than the voltage drop in the load resistor R_L .

ARTHUR R. BAILEY,
Bradford, 7. Bradford Institute of Technology.

News from the Industry

A.E.I.—The consolidated profit and loss account of Associated Electrical Industries and its subsidiaries for 1959 shows an excess of income over expenditure of £16,972,609; just over £1M more than the previous year. After setting against this figure various charges, including nearly £5M taxation, the profit was £6,489,807 compared with £5.1M in 1958.

T.C.C. announce a group trading profit for 1959 of £769,980 which is a 45% increase on the preceding year. At the board meeting which followed the annual general meeting D. W. Aldridge resigned from the chairmanship and his place has been taken by W. C. Handley. The vacancy on the board has been filled by Dr. L. G. Brazier who is also director of research and education of B. I. Callender's Cables the parent company of T.C.C.

Ekco airborne weather radar is being fitted in the fifteen Boeing 707 airliners on order for British Overseas Airways Corporation. All B.O.A.C. Britannia and Comet 4 airliners are already equipped with Ekco radar.

Ampex.—According to figures issued by Ampex International, of Switzerland, there are now 65 of the corporation's Videotape recorders in use in Europe. Of this total 42 are in the U.K.

Fraser Electronics and Communications Ltd. has been set up by J. Fraser (until recently with Land, Speight and Company), and W. O. Buchanan, to act as Scottish agents for electrical and electronic manufacturers. They have premises at 1103 Argyle Street, Glasgow C.3 (Tel.: Central 9301).

Reynolds (Packaging) Ltd., of Alfred's Way, Barking, Essex, have constructed a dust-free air-conditioned room for the cleaning and packing of specialized equipment including electronic gear for guided weapons.

Mills & Rockleys (Production) Ltd. have announced three appointments in their printed circuits division. J. R. Atkinson has taken over production from A. K. Bullock who will concentrate on planning. T. L. Harcombe has joined the company from the G.E.C. and will be responsible for development and application engineering.

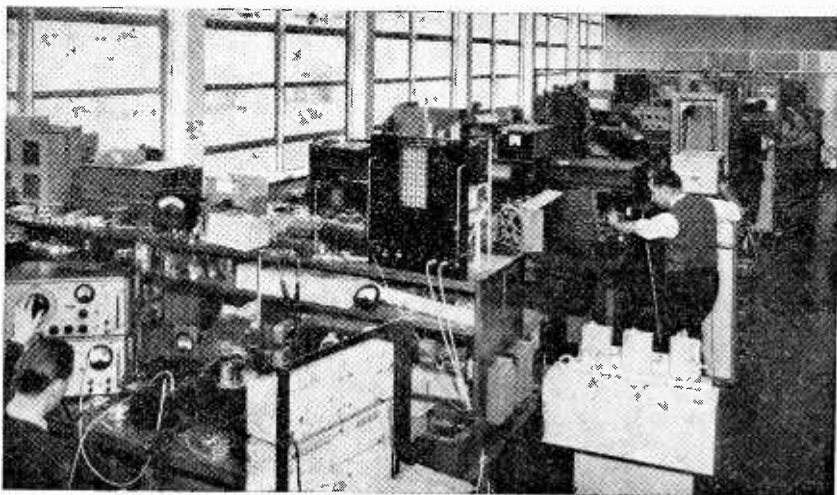
Transitron Electronic Corp., of Wakefield, Mass., have set up a European sales subsidiary, Transitron Electronic S.A., with its headquarters in Zug, Switzerland, and Offices in London, Paris and Munich. The London offices will be run by a new company, Transitron Electronic Ltd., of which D. P. O'Connell, formerly with British Electric Resistance Co., is manager.

Ferranti Ltd. have signed an agreement with Bendix Aviation Corporation for them to sell in the U.S.A. Ferranti machine tool control systems. Bendix, who made the initial move in the negotiations, will set up a computer centre in Detroit to supply magnetic tapes for the equipment.

Amplivox Ltd., of Wembley, Middx., has been awarded contracts by the General Post Office for the supply of miniature magnetic microphones and earphones for the new transistorized hearing-aid issued under the National Health Scheme.

Swiss made apparatus for the speedy insertion of soldering tags into printed circuit boards is being handled in this country by R. H. Cole (Overseas) Ltd., of 2 Caxton Street, London, S.W.1, who are agents for Kumag, of Zürich.

Grundig (Great Britain) Ltd. have extended the guarantee period for their tape recorders from six months to one year. This will apply to all guarantees registered on or after January 1st this year.



Communication systems laboratory at the new establishment of Standard Telecommunication Laboratories, at Harlow, Essex. This particular laboratory is used for investigations into television transmission by pulse code modulation. S.T.L., a wholly owned subsidiary of Standard Telephones & Cables, was formed in 1945 with laboratories at Enfield, to take over the advanced research and development work of S.T.C.

Direct TV Replacements, of 138 Lewisham Way, London, S.E.14 (Tel.: Tideway 6666) are now manufacturing their own replacement transformers for Ferguson television models 306T and 308T. This component is also used in H.M.V. models 1865 and 1869 and Marconiphone model VT153.

Miniature Electronic Components, Ltd., of St. Johns, Woking, Surrey, are producing under licence from Con-Elco, of California, a range of miniature trimmer potentiometers specially designed and developed for the guided weapon and aircraft industries. The range extends from 10 ohms to 50k Ω .

Precision Components (Barnet) Ltd. have moved from Barnet to Kabi Works, Cranborne Road, Potters Bar, Middx. (Tel.: Potters Bar 3444).

Precision Jigs Company Ltd., of 79 Caterham Avenue, Barkingside, Essex, has acquired a factory on the new industrial estate, Thetford, Norfolk.

Hagan Controls, Ltd., a member of the Plessey group, has moved to 14, Grosvenor Place, London, S.W.1 (Tel.: Belgravia 6382).

EXPORT NEWS

Tropospheric scatter link equipment is being supplied by Marconi's to Cable & Wireless (W.I.) Ltd. to establish a quadruple diversity u.h.f. link between the West Indies islands of Barbados and Trinidad. The system will carry six telephone speech channels and will be capable of enlargement to twelve channels.

Closed-circuit television equipment manufactured by E.M.I. Electronics has been installed in a Wall Street stockbrokers' office. The television system relays to large-screen monitors in seven offices a continuous picture of moving ticker-tapes giving stock market movements.

H.F. telecommunications equipment is being supplied to Turkey and Iran by Marconi's under a £225,000 order placed by H.M. Government as part of its programme of technical assistance to member countries of the Central Treaty Organization. The contract calls for the supply and installation of independent sideband telephone and multichannel telegraph circuits between Istanbul, Ankara, Teheran and London.

Telemechanics Ltd., who recently moved into new premises at Brokenford Lane, Totton, Southampton (Tel.: Totton, Southampton 3666), have appointed Conway Electronic Enterprises Reg'd., of Toronto, as their Canadian agents, and M. Rietveld, e.i., of Rotterdam, as agents in Holland.

Milan's first radio taxi service, comprising a fleet of 250 vehicles, is fitted with Pye equipment. The service was introduced at the opening of the Milan Fair at which the theme of the Board of Trade exhibit was "British electronics in the service of mankind."

Weather radar has been supplied by Decca to several U.S. television stations for their weather forecasting services. The radar pictures are transmitted to viewers while an announcer interprets the information.

Indian Agents.—Capital Industries, of 8, Kapurthala Road, Jullundur City, who have been established since 1925, want to represent a British manufacturer of radio equipment.

I.L.S. equipment is being supplied by Pye for Nairobi's new international airport.



The "Automorse" machine illustrated enables anyone without knowledge of the Morse Code to operate a telegraph communications system of either the wire or radio type. On depressing a key on the typewriter-like keyboard the machine automatically selects the correct Morse sequence of dots and dashes relevant to the figure, letter or other character marked on the key. Cams are not employed, the selection of dots and dashes being effected by an ingenious system of wiping contacts. The machine has a capacity of 180 characters per minute and it operates normally from 6V d.c. consuming 3A. It was demonstrated recently at the Norwegian Export Centre, 20 Pall Mall, London, S.W.1, and the makers are Automorse Ltd., N ktergalsgatan 6, Gothenburg, Sweden.

THE COSH AT WORK

By "CATHODE RAY"

PRACTICAL USE OF A HYPERBOLIC FUNCTION

LAST month we saw that plotting the equation $y = \sqrt{r^2 - x^2}$ gives us a circle of radius r , so long as x is confined to the range of values from $-r$ to $+r$. Certain ratios in this graph are very well known and useful; for example, x/r is called $\cos \theta$, y/r is $\sin \theta$, and y/x is $\tan \theta$, where θ is the angle of the radius from any point x, y , relative to the "3 o'clock" radius. Directly x goes beyond $\pm r$, y is the square root of a negative quantity, described by mathematicians as imaginary. An alternative form of the same equation, $y = j\sqrt{x^2 - r^2}$, is then more convenient. Just as in a.c. vectors we interpret

θ is the angle AOP_1 , η is definitely not the angle AOP_2 or any other angle visible as the inclination of one line to another. It was to emphasize this very important point that I used separate symbols, θ and η ; but both just stand for a number, and it may often happen that they are the same number.

Because both sets of ratios are derived from the same equation, requiring only j as a key for passing from one set to another, we have

$$\begin{aligned} \cos A &= \cosh jA & \cosh A &= \cos jA \\ j \sin A &= \sinh jA & j \sinh A &= \sin jA \end{aligned}$$

Consequently the trigonometrical formulae for circular angles all have their hyperbolic counterparts, differing only by the appropriate power of j (j^2 being of course -1). For example:

$$\cos A = \frac{e^{jA} + e^{-jA}}{2} \quad \cosh A = \frac{e^A + e^{-A}}{2}$$

$$\begin{aligned} e^{jA} &= \cos A + j \sin A & e^A &= \cosh A + \sinh A \\ \cos^2 A + \sin^2 A &= 1 & \cosh^2 A - \sinh^2 A &= 1 \\ \cos(A+B) &= \cos A \cos B - \sin A \sin B & \cosh(A+B) &= \cosh A \cosh B + \sinh A \sinh B \end{aligned}$$

Now circles, and angles thereof, are involved in a great variety of practical activities, so we are familiar with the circular side of the picture. The very name hyperbola suggests something much more academic, and it is certainly not familiar to the great non-technical public. So the usefulness of hyperbolic functions is much less obvious than that of circular functions. Another thing: we usually have some warning, in the shape of an angle, that circular functions may soon appear; but hyperbolic functions have a way of cropping up suddenly and apparently inconsequentially, to the dismay of the reader. Last month's effort was intended to make clear what hyperbolic functions are, and we have just recapitulated. The next thing is to show how they can be used, by taking a simple example.

It is the familiar ladder arrangement, Fig. 2, in which the impedances Z_1 and Z_2 can be of any kind, usually pure resistances and/or pure reactances (or as close approximations to them as practicable). If both Z_1 and Z_2 are resistances—or both reactances of the same kind—we have an attenuator, treating all frequencies alike; if they are a mixture, we have a filter, the purpose of which is to discriminate between frequencies. When the number of stages or sections is even as few as two, it becomes a little

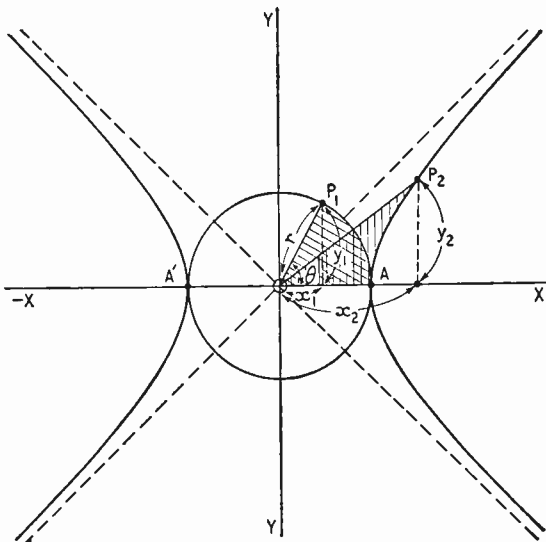


Fig. 1 Believe it or not, this graph all arises from Pythagoras— $x^2 + y^2 = r^2$. The circle part is mathematically real, and comes from values of x between $-r$ and $+r$. The hyperbolic parts can be plotted only after the factor j has been introduced, so are (by comparison) imaginary.

j as an instruction to break away at right angles into a new world that can only be imagined by single-dimensional x -axis beings, now we can interpret it as a break away from the two-dimensional plane of the paper on which our circle is drawn into a plane at right angles. Continuing to plot the equation there, we find the graph takes the form of a rectangular hyperbola. The complete graph of the equation therefore consists of the circle and two-part hyperbola, shown (without distinction between real and imaginary) in Fig. 1. P_1 is a typical point on the circle, x being less than r ; namely, x_1 . x_1/r is $\cos \theta$. To distinguish the ratios in the hyperbolic world, "h" is added to their names; so x_2/r is $\cosh \eta$. And if you ask to be shown η on the diagram, the best that can be done is to note that it is proportional to the shaded area AOP_2 , just as the angle θ is proportional to the shaded area AOP_1 . Although

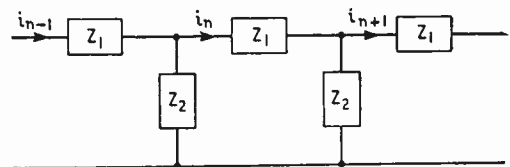


Fig. 2 General form of ladder network, made up of impedances in two sizes.

complicated to calculate it by ordinary circuit methods, and above two the paper work rapidly gets out of hand. However, if one can assume that the number of sections is unlimited—or alternatively that the chain is terminated by an impedance equivalent to an unlimited sequence—it becomes quite simple. The other necessary assumption is a signal source—a.c. or d.c.—somewhere to the left, to make current flow. The currents through the three Z_1 elements shown in Fig. 2 are named thereon. The current downwards through the left-hand Z_2 is obviously $i_{n-1} - i_n$, and that through the right-hand Z_2 is $i_n - i_{n+1}$.

The total voltage around any complete loop being necessarily zero, apply this principle to the loop formed by the two Z_2 s and the middle Z_1 . The clockwise voltage across the first Z_2 is $(i_{n-1} - i_n) Z_2$; across the Z_1 , $-i_n Z_1$; and across the second Z_2 , $-(i_n - i_{n+1}) Z_2$. So

$$(i_{n-1} - i_n) Z_2 - i_n Z_1 - (i_n - i_{n+1}) Z_2 = 0 \quad (1)$$

Since every section is exactly the same as every other, the ratio of i_{n+1} to i_n is the same as that of i_n to i_{n-1} . Call it a , so that $i_{n+1} = ai_n$ and $i_{n-1} = i_n/a$. Substituting this in (1) we get

$$(i_n/a - i_n - i_n + ai_n) Z_2 - i_n Z_1 = 0$$

which can be divided throughout by i_n and Z_2 giving

$$a + \frac{1}{a} - 2 - \frac{Z_1}{Z_2} = 0 \quad \dots \quad (2)$$

We are interested in a , because it is the input/output current (and voltage) ratio of each section; and the attenuation of any number of sections, m , is a^m . So the natural thing is to lick equation (2) into a shape giving a directly. It turns out to be a quadratic, and the answer is in the usual rather untidy form of the solution of a quadratic:

$$a = \frac{Z_1}{2Z_2} + 1 \pm \sqrt{\left(\frac{Z_1}{Z_2}\right)^2 + 1} \quad \dots \quad (3)$$

There is nothing actually wrong with that, and it can be used for computing a , given the ratio

Z_1/Z_2 and a good deal of time and patience if it varies with frequency and a is required over a wide band. The more sophisticated worker, being $e^x + e^{-x}$ conscious, notices with interest the $a + 1/a$ in (2) and wonders if there would be any advantage in putting a into the form e to the something. He, of course, is of the type who would in any case require attenuation to be specified in decibels or even nepers (which are to decibels as natural (base e) logs are to common (base 10) logs).^{*} Now the attenuation in nepers is defined as the natural log of the input/output current ratio. If this attenuation per section is denoted by α , then, $\alpha = \log_e (1/a)$, which can also be written $1/a = e^\alpha$, or $a = e^{-\alpha}$. Substituting $e^{-\alpha}$ for a and e^α for $1/a$ in (2), and dividing throughout by 2, our smart worker gets

$$\cosh \alpha = 1 + \frac{Z_1}{2Z_2} \quad \dots \quad (4)$$

a decidedly neater result than (3) and one that gives him the answer direct in nepers instead of needing a separate operation to convert into them from the plain ratio a . The coshes can simply be looked up in a table.

If you are thinking that seems too dead easy you may be partly right. Some queries can arise when the values of Z_1 and Z_2 have been filled in. So let us look into the various possibilities.

When Z_1 and Z_2 are both resistances, the procedure really is as simple as it looks. To convince the sceptics, let us work an example out both ways. Suppose Z_1 is 100Ω and Z_2 is 250Ω (or any two values in the same ratio, 0.4). Using equation (3) first, we find $a = 1.862$ or 0.538 . As we are assuming the only source is on the left, i_n must be less than i_{n-1} , so a is less than 1, and the solution 1.862 can be eliminated. As one might reasonably expect, 1.862 is the answer for signals coming from the right, so for left-coming signals it is $1/a$, which may actually be a little more convenient for calculating the decibels. Either way, the impedance of every section being the same, this current ratio is equivalent to 5.4dB; and as $8.686 \text{ dB} = 1 \text{ neper}$, that is 0.62 neper.

Now try equation (4). The right-hand side is clearly 1.2 and a table of coshes (or Fig. 3) shows that if $\cosh \alpha = 1.2$, α is 0.62. It's as easy as that.

Strictly, because of the symmetry of the cosh hanging-chain curve, α is ± 0.62 , but since we know our attenuator can't amplify the signals put into it our common sense again tells us which answer is right: -0.62 , denoting a loss.

Next, suppose Z_1 and Z_2 are reactances of the same kind—both inductors or both capacitors. The j and ω ($=2\pi f$) cancel out in Z_1/Z_2 , so we are left with the ratio of inductances or capacitances, which is a real number just like the ratio of resistances in the previous case. So it is just as easy, except that the impedance of the ladder varies with frequency, which is the reason that this kind of

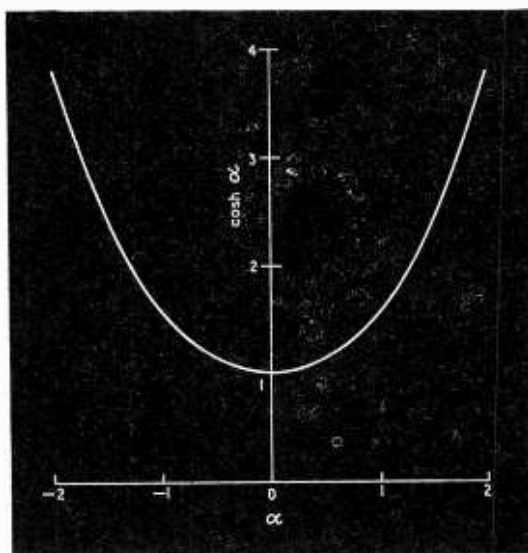


Fig. 3 Here, repeated from last month, is a cosh curve.

^{*}Whereas decibels are power ratios expressed as common logs, nepers are current ratios expressed in natural logs. Current (or voltage) ratios can only be stated in dB on the understanding that both currents (or voltages) are in (or across) the same impedances. While the number of dB is correctly $10 \log_{10} (P_2/P_1)$ where P_2 and P_1 are two powers being compared, powers in equal impedances are proportional to current (or voltage) squared, so the number of dB is then $20 \log_{10} (I_2/I_1)$. The number of nepers is defined as $\log_e (I_2/I_1)$, and as $\log_{10} e^x = \log_e x / 2.3026$, the number of dB is $20/2.3026 = 8.686$ times the number of nepers (always assuming the equal-impedance clause applies).

attenuator is seldom seen. The only example I can think of is the capacitance potential-divider sometimes used in the probe of a valve voltmeter, where a main object is to minimize the input capacitance.

We enter much the largest division of the subject when we pass on to reactances of opposite kind. Most filters use them. The vital feature is that a and α vary with frequency. So they have to be computed not once per filter but many times, and any short cut is that number of times more helpful.

Suppose Z_1 is an inductor and Z_2 a capacitor, both assumed devoid of resistance, as in Fig. 4. Then $Z_1/2Z_2$ in (4) is $j\omega L \times j\omega C/2 = -\omega^2 LC/2$. This not only varies as the square of the frequency, but is invariably negative, which will make us think a bit. For a start, it means that (except at zero frequency, when the filter does precisely nothing) according to (4) $\cosh \alpha$ is always less than 1. But if we search Fig. 3 for a typical (or any) example we might as well look for an atheistic Pope.

For a hint of an escape from this impasse we can turn back to Fig. 1, where we see that x/r is a cosh when it is 1 or more and a cos when it is 1 or less. We know that a cos is a cosh of an imaginary quantity. There is no real value of a that makes $\frac{1}{2}(a + 1/a)$ less than 1; if one of the two terms in the brackets is less than 1, the other exceeds 1 by a greater margin, so their average is more than 1. But if instead of assuming a is equal to e^α , α being a real number, we consider the possibility of the index being imaginary, we can try $e^{j\beta}$. Since $\frac{1}{2}(e^{j\beta} + e^{-j\beta}) = \cos \beta$, we have as an alternative form of (4), for use when $\cosh \alpha$ is "off the map,"

$$\cos \beta = 1 + \frac{Z_1}{2Z_2} \dots \dots \dots (4a)$$

Until we are used to switching back and forth between a real world and (relative to what we have just left) an imaginary one, the transition may make us a little dizzy and in need of recovering our sense of direction. Fortunately there is always one point common to both worlds (A in Fig. 1), so let us pause on that threshold for a moment. From the hyperbolic point of view, it means that α —the attenuation in nepers—is zero. That is what we would expect, because $\cosh \alpha$ can (from (4)) only be 1 when $Z_1/2Z_2$ is zero, which in our Fig. 4 case means zero frequency and a perfect straight-through connection. From the circular point of view, $\cos \beta = 1$ means $\beta = 0$. We could have chosen to call it $\cos \alpha$, to emphasize that it is basically the same quantity in both worlds, but it is rather more convenient to use a different symbol to indicate that in the circular world it is a circular angle. The physical interpretation of this is that instead of the attenuation, α , we are now going to have a phase shift, β . Our Fig. 4 filter at zero frequency obviously causes no attenuation and no phase shift, so is aptly represented by the common point A.

As the frequency rises, $-Z_1/2Z_2$ rises and makes $\cos \beta$ fall. That clearly indicates an increasing phase shift, which is what we get in an actual filter.

You will remember that there were two possible answers to the attenuation question, one representing movement away from the signal source and the other towards it, the first being a loss and the second an equal gain. In the same way there are two solutions to equation (4a); one a positive

angle and the other an equal negative angle. Again, these represent what we find when we move away from or towards the source. Meanwhile, there is no attenuation. Two months ago we checked that $e^{j\theta}$ and $e^{-j\theta}$ represent vectors of variable angle but constant (unit) length.

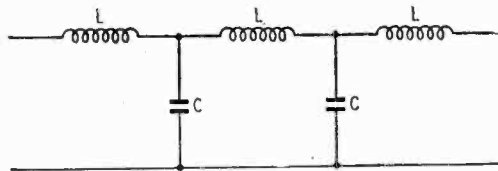


Fig. 4 A particular variety of Fig. 2—a low-pass filter.

The picture, then, is one of steadily increasing phase shift per section as the frequency of the signal entering the filter rises. Does it keep on doing this?

When the frequency is high enough to make $\omega^2 LC/2 = -1$, this cancels the 1 in (4a), so $\cos \beta = 0$ and $\beta = \pi/2$, or 90° . We are now half-way across Fig. 1, moving left. Doubling the frequency makes $\cos \beta = -1$, so $\beta = \pi$, or 180° . That brings us to A' in Fig. 1. What next? Do we keep on going round the circle, or is this another threshold to an imaginary world (for now we are in the circular world. it is the hyperbolic one that seems imaginary)? We can soon find out by increasing the frequency another step, making $\omega^2 LC/2 = 3$, for $1 - \omega^2 LC/2$, is then -2 , and this is certainly not to be found in the table of cosines. Neither is it to be found in a cosh table or in Fig. 3. So where are we now? Completely lost, it seems!

Our mistake was being in too much of a hurry to get past A'. We should have paused there for a moment's reflection like we did at A. So let us go back to it. At that point there is still no attenuation, but a 180° phase shift, which means that the signal loses no strength in its progress down the filter but does reverse its polarity at every section. So, changing over once more to the hyperbolic or attenuation viewpoint, we can say that a is -1 , which modifies (4) to

$$-\cosh \alpha = 1 + \frac{Z_1}{2Z_2} \dots \dots \dots (4b)$$

This puts us back on to Fig. 3, and we can stay there indefinitely as the frequency rises. If you object that an infinitely large piece of graph paper would be needed, and that even cosh tables don't go to infinity, I would point out that if a is very large then $1/a$ is very small and can be neglected, simplifying (4b) to

$$a \approx 2 + \frac{Z_1}{Z_2}$$

which in our example is $2 - \omega^2 LC$. The phase shift vector meanwhile sticks at 180° , represented by the minus sign in (4b).

Corresponding, then, to the abrupt mathematical change from circular to hyperbolic world as we pass through A', there is an abrupt physical change in the performance of the filter. At frequencies from zero to there, it doesn't attenuate the signal at all, but it does introduce an increasing phase delay.

Directly that delay equals 180° per section it sticks at that and attenuation begins, increasing with

frequency. The change-over point is, understandably, called the cut-off frequency, usually denoted by f_c . We can easily find it for our simple Fig. 4 low-pass filter by remembering that the transition occurred when $\omega^2 LC/2$ was equal to 2:

$$\frac{4 \pi^2 f_c^2 LC}{2} = 2$$

$$\therefore f_c = \frac{1}{\pi \sqrt{LC}}$$

Just for the fun of it let us plot the attenuation curve from (4b), choosing our frequency scale in multiples of f_c , so as to make it applicable to any Fig. 4 filter. The result is Fig. 5. To put it in the

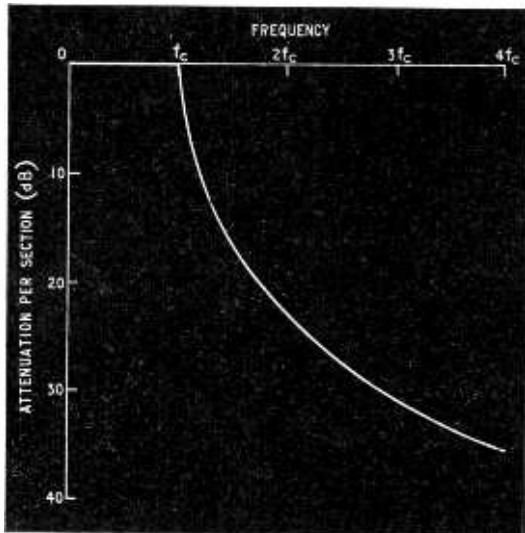


Fig. 5 Attenuation/frequency characteristic curve of Fig. 4, the frequency scale being in terms of the cut-off frequency f_c . From 0 to f_c there is a phase delay increasing from 0° to 180° ; above f_c it remains constant at 180° .

form we expect for a filter curve I have drawn it upside down, and with α in dB rather than nepers.

We could do a high-pass filter in much the same way; the difference is that zero frequency is out at minus infinity on Fig. 1, and A is only reached at infinite frequency. And band-pass filters, with both Z_1 and Z_2 comprising both kinds of reactance as tuned circuits, are the same in principle, but of course $Z_1/2Z_2$ is a more complicated expression.

Having followed us so far, the earnest but inexperienced student may be disappointed, if not actually aggrieved, on being informed that the filters we have been considering are never used, or alternatively if they are used they don't work as hereinbefore described, because the conditions cannot be fulfilled. Quite apart from the inevitability of resistance, which smooths the sharp cut-off in Fig. 5, there is the awkwardness of having to provide an infinite number of sections, or an impedance equivalent thereto. This characteristic impedance Z_0 , as it is called, has to vary in an extremely awkward manner with frequency. We went into the matter just over 10 years ago, and if you weren't with us then you can look it up somewhere, because it is outside

our scope at present. To calculate it, the filter sections must be made symmetrical by dividing them either half-way along Z_1 to form Ts or down the middle of Z_2 to form π s. The Z_0 /frequency curve for the Fig. 4 filter in T sections begins at zero frequency with a pure resistance equal to $\sqrt{L/C}$, curves downwards in a semicircle to reach zero at f_c , and after that is a pure reactance which rises indefinitely in a hyperbola. In fact, the curve is the same as P_1AP_2 in Fig. 1. The π form is even more awkward, going to plus and minus infinity at f_c . No practical load behaves like this.

If an ordinary resistance or reactance termination is used, the performance of the filter naturally departs considerably from that worked out here, and as one would expect from the general cussedness of things it is worse. So in high-class practice somewhat elaborated forms of filter are used.

The only simple basic combination of Z_1 and Z_2 we have not yet considered is resistance and reactance. There are practical examples in almost every radio receiver, Z_1 being resistance and Z_2 capacitive reactance. If we put $Z_1=R$ and $Z_2 = 1/j\omega C$, equation (4) becomes

$$\cosh \alpha = 1 + \frac{j\omega CR}{2}$$

In this, the 1 is real and the $j\omega CR$ is imaginary. In other words, the total is complex. Switching over to cos avails nothing, because making the imaginary part real makes the real part imaginary and one is no better off. Neither $\cosh \alpha$ nor $\cos \beta$ is sufficient by itself. There is both attenuation and phase shift at all frequencies, instead of these effects being segregated into their own frequency bands.

By means of a rather tricky bit of work, formulae have been found for $\cosh \alpha$ and $\cos \beta$ separately, when $Z_1/2Z_2$ is complex and therefore has the general form $a + jb$:

$$\cosh \alpha = \frac{1}{2} \sqrt{(a+2)^2 + b^2} + \sqrt{a^2 + b^2}$$

$$\cos \beta = \frac{1}{2} \sqrt{(a+2)^2 + b^2} - \sqrt{a^2 + b^2}$$

These equations can obviously be used to calculate LC filters, taking account of resistance. But in our particular example, $a = 0$ and $b = \omega CR/2$, so the equations simplify to

$$\cosh \alpha = \sqrt{p+1} + p$$

$$\cos \beta = \sqrt{p+1} - p$$

where p is short for $\omega CR/4$.

Since $1 + Z_2/2Z_1$ can't be fully expressed as either $\cosh \alpha$ or $\cos \beta$ ($= \cosh j\beta$) when it is complex, you may be wondering what it is equal to. $\cosh \alpha + \cosh j\beta$? One can soon find, from the above equations, that that doesn't work out. Actually it is $\cosh(\alpha + j\beta)$. The combination $(\alpha + j\beta)$ is known as the propagation constant, the α part being the attenuation constant and β the phase constant. Or, if you rightly object that these things are not constant at all but vary with frequency, you will call them coefficients.

When one turns to transmission lines, hyperbolic and circular functions of complex variables arrive in a big way. That subject would be rather too much to bite off at this stage, but perhaps the foregoing introduction will help to make it more digestible when it does come.

Manufacturers' Products

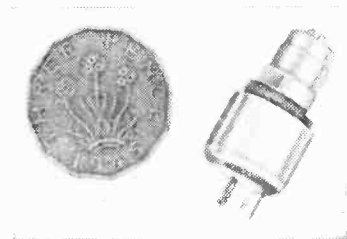
NEW ELECTRONIC EQUIPMENT AND ACCESSORIES

Very Small Potentiometer

IN response to the growing demand for miniaturized components of all types, Plessey have introduced the Type L potentiometer. Measuring only 0.5in in diameter, it is housed in an aluminium case and the construction follows the well-tried Plessey practice of using

a moulded carbon track with, in this case, a concentric metal track (silver loaded), the two being bridged by a moving contact mounted on an insulated carrier arm.

Rating of the new potentiometer is 0.25W and the current range covers resistance of from $1k\Omega$ to $2.5M\Omega$. A pre-set type only, with



Plessey miniature Type L pre-set potentiometer.

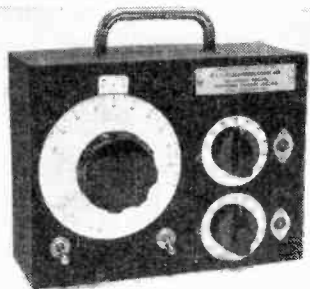
screw-driver slotted spindle, is available at present. The temperature range is -55°C to $+85^{\circ}\text{C}$ and a voltage limitation of 350 is imposed.

The makers are The Plessey Co. Ltd., Vicarage Lane, Ilford, Essex.

Transistorized V.H.F. Generators

R.E.E. TELECOMMUNICATIONS have recently introduced three new transistorized sine wave oscillators. Model A covers 40 to 70Mc/s and Model B 100 to 150Mc/s; Model C was developed for servicing v.h.f. mobile radio receivers and covers both 70 to 72Mc/s as well as 85 to 87Mc/s. In all three models the output can be amplitude modulated at 400c/s with a depth variable from 0 to 100%. Each model also contains attenuators which allow a maximum output level variation of 90dB down to approximately $1\mu\text{V}$. An internal 6-V battery supply is used.

Models A and B, which both cost £65, and Model C, which costs £70, are made by R.E.E. Telecommunications Ltd., Market Square, Crewkerne, Somerset.



R.E.E. Telecommunications single-band transistorized v.h.f. signal generator.

Potential-Indicating Lamps

THE Acru Electric Tool Manufacturing Co. Ltd. have introduced two neon lamps in which the length of the glow column depends on the current flowing through the lamp. Thus, with the normal high-value series resistors the lamps may be used to indicate applied potential. In the $\frac{1}{8}$ in diameter, $1\frac{1}{2}$ in long Type 93 (of "festoon" form) one electrode is in the form of a button

at one end of the tube and the other extends along the tube: this is available also with a moulded housing containing either resistors appropriate for potentials from 60 to 250V (Type 103L) or 100 to 600V (Type 103H) a.c. The lamp is viewed through a calibrated slot in the cover. In another lamp (Type 98) the glow starts at the centre of the tube and extends towards the ends as the current increases.

Other lamps in Acru's range include a snap-in one-hole-fitting type moulded in polystyrene and fluorescent-green types (only 7160V).

The address of the manufacturers is Acru Works, Demmings Road, Cheadle, Cheshire.



Acru potential-indicating neon lamp and housing for 100-600V.

Printed Resistors

A FURTHER development in the printed circuit technique is a new printed resistor made as a separate component on a base material of paper. The specification of the paper used is; breakdown voltage 1.5kV, tensile strength 45lb/in; thickness 0.006in and upper temperature limit 150°C .

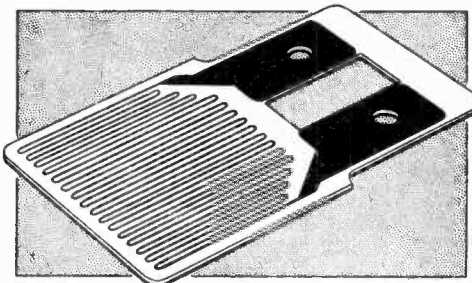
The resistance material can be either cupro-nickel, nickel-chrome or certain other alloys and the bond with the paper base is said to be so secure that it cannot be peeled off without destroying the component. Where complete insulation of the resistance is required the paper base can be bonded across the exposed face of the element.

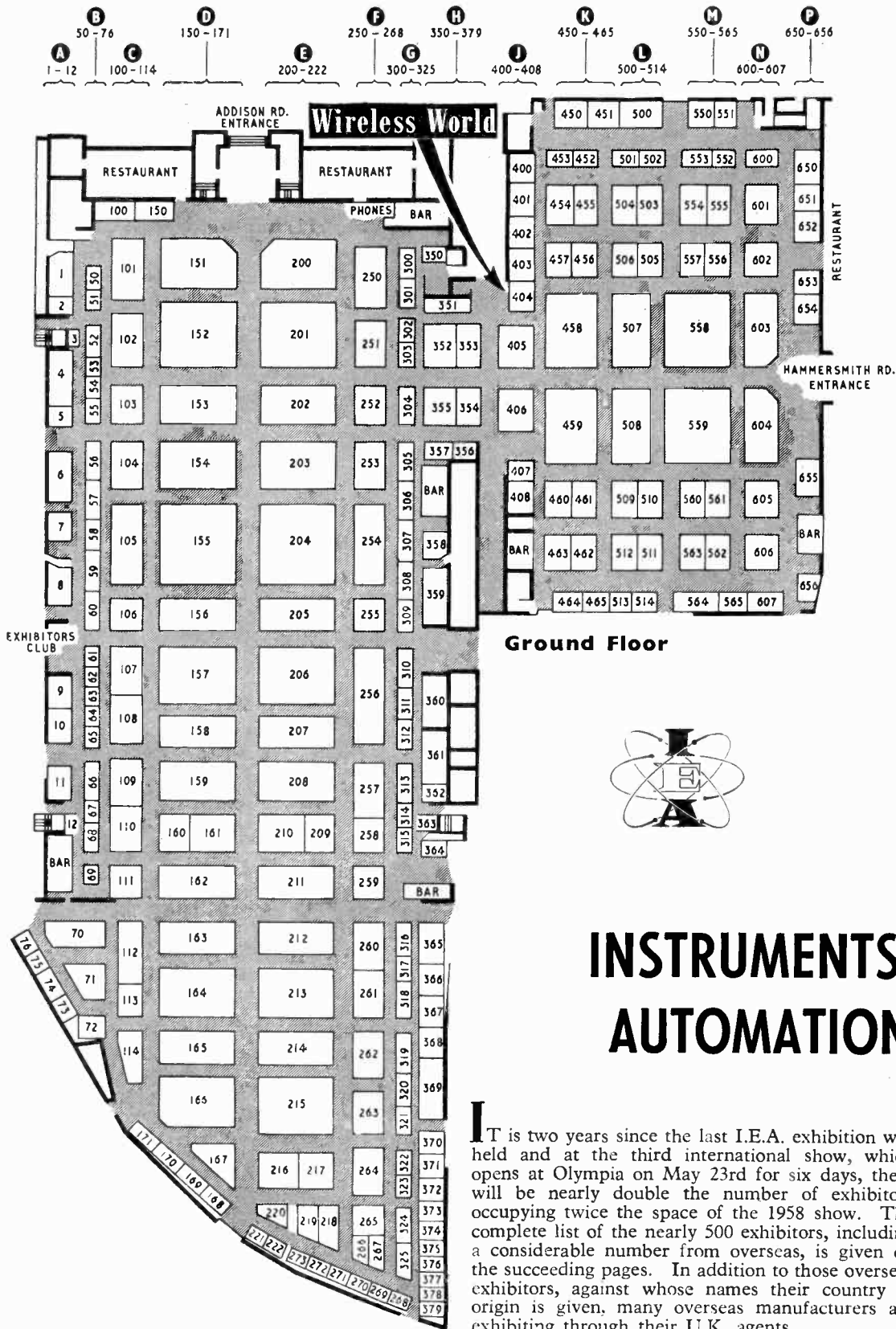
Among the applications for these resistors is where good heat dissipation is required in a restricted space, such as, for example, a contact-cooled mains dropper in radio and TV sets using the chassis as a heat sink.

These resistors are made to customers' requirements and the range of resistance can be anything up to $100\Omega/\text{sq in}$.

Further details can be obtained from Mills and Rockleys (Production) Ltd., Printed Circuit Division, Swan Lane, Coventry.

One of Mills and Rockleys' printed resistors. This resistance element measures approximately $\frac{1}{8}$ in square.

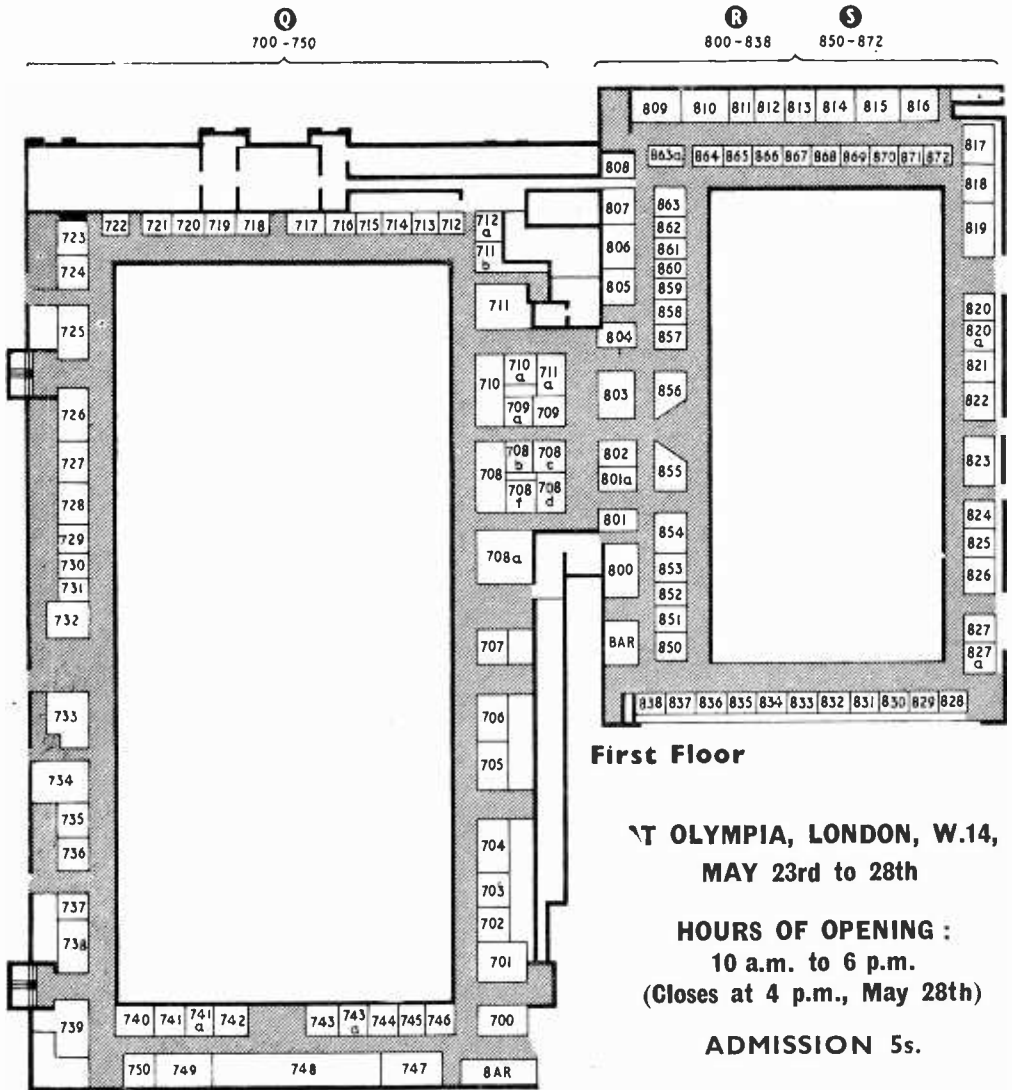




Ground Floor

INSTRUMENTS, AUTOMATION

IT is two years since the last I.E.A. exhibition was held and at the third international show, which opens at Olympia on May 23rd for six days, there will be nearly double the number of exhibitors occupying twice the space of the 1958 show. The complete list of the nearly 500 exhibitors, including a considerable number from overseas, is given on the succeeding pages. In addition to those overseas exhibitors, against whose names their country of origin is given, many overseas manufacturers are exhibiting through their U.K. agents.



First Floor

**AT OLYMPIA, LONDON, W.14,
MAY 23rd to 28th**

HOURS OF OPENING :
10 a.m. to 6 p.m.
(Closes at 4 p.m., May 28th)

ADMISSION 5s.

ELECTRONICS, AND EXHIBITION

In our next issue we hope to review some of the outstanding equipment shown at the exhibition which is promoted by the six industrial organizations listed below*.

Admission to the exhibition costs 5s. It will be opened by the Rt. Hon. Lord Mills at 11.30 on

* British Electrical and Allied Manufacturers' Association; British Industrial Measuring and Control Apparatus Manufacturers' Association; British Lampblown Scientific Glassware Manufacturers' Association; Drawing Office Material Manufacturers' and Dealers' Association; Electronic Engineering Association; and Scientific Instrument Manufacturers' Association.

May 23rd, but on succeeding days will open at 10.0. The closing time is 6.0 except on Saturday when it will close two hours earlier.

For three days during the exhibition the Electronic Forum for Industry (E.F.F.I.) is holding a conference on "User Experience of Electronics." Each of the three sessions will cover a different field of application of electronics in industry. On the 24th the theme will be electronics in data processing; on the 25th, factory applications of electronics (chairman, Lt. Col. Sir John Eldridge) and on the 26th electronics in instrumentation and control (chairman, Viscount Caldecote). Each day's programme begins at 2.30.

This is the first full-scale conference organized by E.F.F.I., which consists of nine associations of manufacturers in or pertaining to the electronics industry, and the object quoted in the prospectus of the conference is: "To project to all users and potential users of electronics equipment the wide and varied scope of the electronics industry, and

to receive from them inspiration and guidance on new uses, and the improvement or modification of established application."

A fee of £1 11s 6d is being charged for each session of the conference and this includes admission to the

exhibition and a report of the proceedings. Details are obtainable from the Honorary Secretary, E.F.F.I., c/o The Electronic Engineering Association, 11 Green Street, London, W.1. (Tel.: Mayfair 7874).

LIST OF EXHIBITORS

STAND NO.		STAND NO.		STAND NO.	
AAP-Allgemeiner Apparatebau GmbH, W. Germany	M565	Communication Systems	F261	Firth Cleveland Instruments	H353
A.B. Metal Products	F267	Compagnie Francaise Thomson-Houston, France	Q708c	Fischer & Porter	A10
A.D.S. Relays	Q728	Connollys (Blackley)	R834	Fisher Governor Co.	D155
A.F.S. Developments	S861	Constructors John Brown Control	H361	Fleming Radio (Developments)	P652
A.K. Fans	S872	Correx Communications Equipment	A8	Flexonics	M563
A.O.I.P. Mesures, France	R831	Cossor	R817	Floform Paris	F264
A.P.T. Electronic Industries	P650	Coulter Electronics	E212	Formica	J403
A.T.E. (Bridgnorth)	F261	Counting Instruments	Q743a	Fortiphone	Q711a
Advance Components	C107	Coventry Controls	Q717	Foster Instrument Co.	C111
Aircraft-Marine Products (G.B.)	N602	Crompton Parkinson	E222	Fox, P.X.	L514
Airflow Developments	B66	Crosby Valve & Engineering Co.	C104	Foxboro-Yoxall	E202
Airmec	D162	Crouzet & Company, France	F253	Furzehill Laboratories	Q721
Alexander Controls	G318	Croydon Precision Instruments Co.	Q716	General Controls	H375
Allspeeds	R810	Cu-Ni-Craft	L500	General Electric Co.	E211
Alma Components	F268	Cuthberts, Ralph	G320	General Post Office	R823
Alto Instruments (G.B.)	R816	Data Recording Instrument Co.	G325	General Precision Systems	M560
Ampex International S.A., Switzerland	S863a	Dawe Instruments	Q727	General Radio Co., U.S.A.	Q733
Amphenol	K453	Day, J., & Co.	B53	General Radiological	E209
Analytical Measurements	G303	Daystrom	G302	Geyer, Christian, W. Germany	Q746
Anderton Springs	S850	DEAC (Great Britain)	R816	Gilbarco	G301
Antiference	G321	Decker's, R., Verlag, G. Schenk, W. Germany	F269	Glass Developments & Ultrasonoscope Co.	A3
Ardente Acoustic Laboratories	S865	Degussa Hanau, W. Germany	M561	Gloster Aircraft Co.	L508
Arrow Electric Switches	Q738	De Havilland Propellers	R730	Goodman, George	F264
Associated Automation	D155	Department of Scientific and Industrial Research	E214	Goodmans Industries	K462
Associated Electrical Industries	D152 & E213	Deutscher Innen-und Aussenhandel	Q748	Gordon, James & Co.	D155
Astralux	Q711b	Elektrotechnik, E. Germany	M554	Goring Kerr	Q736
Audley Engineering Co.	K454	Dewrance & Co.	B64	Graticules	B62
Aumann, Willy K. G., W. Germany	B73	Diamond H. Switches	S852	Graviner Manufacturing Co.	R827
Automation Progress	G314	Direct TV Replacements	K452	Griffin & George	R803
Autronic Developments	Q715	Dobbie McInnes (Electronics)	S858	Grubb, Sir Howard, Parsons & Co.	P651
Aviation, Ministry of Avo	J406	Doran Instrument Co.	K455	Grundy & Partners	S868
	D156	Drayton Regulator & Instrument Co.	K461	Guest Keen & Nettlefolds	F264
B & K Laboratories	E203	Dubilier Condenser Co.	E208	Guyson Industrial Equipment	Q742
B & R Relays	R824	Dynatron Radio		Haddon, Thomas & Stokes	F264
B.O.B. (Arundel)	R817	E.M.I. Electronics	D166	Haddon Transformers	D170
Bailey Meters & Controls	L507	E.M.O. Instrumentation	F251	Halden, J., & Co.	Q701
Baird & Tatlock (London)	N603	Ekco Electronics	E208	Hallam, Sleigh & Cheston	J408
Baldwin Industrial Controls	K463	Electran Coil Co.	Q711a	Hall Harding	F256 & L505
Baldwin Instruments	R805	Electrical Development Association	F250	Harper & Tunstall	M551
Belling & Lee	D165	Electrical Remote Control Co.	F266	Harris Plating Works	H379
Bellingham & Stanley	G315	Electro Automat	S851	Harwin Engineers	L513
Beulah Electronics	S852	Electrofflo Meters Co.	D155	Hassett & Harper	R832
Black Automatic Controls	H359	Electrolube	S871	Hatfield Instruments and Balun	G305
Blackburn Electronics	Q710	Electro-Mechanical Systems	D167	Hawker Siddley Group	L508
Blakeborough, J. & Sons	F265	Electro Mechanisms	M563	Headland Engineering Developments	Q745
Boulton Paul (Aircraft)	B72	Electronic Associates	R825	Heathway Machinery Co.	H367
Bradley, G. & E.	Q743	Electronic Components	Q714	Heidenhain, Dr. Johannes, W. Germany	E218
Brannan, S. & Sons	B52	Electronic Engineering	L502	Hendrey Relays	C113
Braun, G., Publishers, W. Germany	F269	Electronic Instruments	Q711	Henry & Thomas	S869
Bray, Geo. & Co.	Q731	Electronic Machine Co.	R818	Herbert Publishing Co.	D150
Bribond	H368	Electronic Technology and Data Processing	J404	Heywood & Co.	N600
Bristol Aircraft	B58	Electronic Tubes	H373	Hivac	F261
Bristol's Instrument Co.	D155	Electronics & Automation (London)	R816	Holmes Bros. (London)	R806
British Area Regulators	R807	Electrothermal Engineering	G319	Honeywell Controls	E200
British Electric Resistance Co.	R801	Elga Products	G304	Hughes International	G310
B. I. Callender's Cables	R813	Ellenberger & Poensgen, GmbH, W. Germany	Q746	Hunt, A. H. (Capacitors)	M562
British Physical Laboratories	H351	Elliott-Automation	D155	Hunt & Mitton	H357
British Power Transformer Co.	R801	Emeco Electronics Co.	R816	Hunting Engineering	R830
British Rototherm Co.	Q729	Enalon Plastics	H372	Ide, T. & W.	H350
British Sarozal	Q712a	Endocotts (Filters)	B69	Ilford	B70
British Scientific Instrument Research Assoc.	Q744	Engelhard Industries	N606	Imhof, Alfred	H360
Brookhirst Igranic	D156	Engis	R819	Industrial Pyrometer Co.	L509
Brown, Neville, and Co.	H377	English Electric Co.	E215	Inertia Switch	Q722
Brown, S. G.	H366	English Electric Valve Co.	E215	Infra Red Development Co.	P654
Bruce, Peebles & Co.	R802	English Numbering Machines	H370	Institution of Electrical Engineers	R824a
Brush Crystal Co.	Q704	Epsylon Industries	D167	Instron Engineering Corp., U.S.A.	Q705
Bryans Aeroequipment	J400	Equipment & Services	F266	Integra, Leeds & Northrup	D163
Budenberg Gauge Co.	A4	Ericsson Telephones	D153	International Electronics	R811
Bulmers Business Machines	S864	Erie Resistor	D169	International Rectifier Co. (G.B.)	Q739
Burndopt	B68	Ether & Electro Methods	E205	Ionic Plating Co.	F264
Bush Beach & Segner Bayley	M561	Evans Electro Selenium	A11	Jobling, James A., & Co.	C112
Cambridge Instrument Co.	F259	Everett, Edgcombe & Co.	Q747	K.D.G. Instruments	K457
Camlab (Glass)	G322	Ever Ready Co.	K465	K.L.G. Sparking Plugs	Q735
Carlo, Erba S.p.A., Italy	Q709	Evershed & Vignoles	K450	Kelvin & Hughes	F257
Carr Fastener Co.	R814	Fairey Aviation	L503	Kent, George	D159
Casella, C. F., & Co.	K460	Faraday Electronic Instruments	D154	Kovo-Foreign Trade Corp., Czechoslovakia	G306
Cathodeon Crystals	G311	Farris Engineering	D155	Krizik n.p., Czechoslovakia	G306
Cementation (Muffelite)	R838	Ferranti	N604	Kumag A.G., Switzerland	B73
Chapman & Hall	S862	Fielden Electronics	C110	Kynmore Engineering Co.	R801a
Chemical Cutting Co.	R817	Filhol, J. P.	R829	Labgear	D154
Clarke, H., & Co. (Manchester)	Q732	Fireye Controls Co.	Q726	Laboratory Equipment	G313
Cole, R. H. (Overseas)	B73				
Coley Thermometers	Q708f				
Colvern	Q723				
Colyer & Southey	B75				

	STAND NO.		STAND NO.		STAND NO.
Lancashire Dynamo Electronic Products	E205	Radiometer, Denmark	J402	Technicon Instruments Co.	P653
Langham Thompson Group, J	H364	Rank Cintel	N605	Technograph Electronic Products	K451
Langley London	N601	Recorder Charts	A5	Telcon Metals	B59
Laurence, Scott & Electromotors	L510	Reliance Cords & Cables	Q724	Teledictor	C114
Leach Corp., U.S.A.	D167	Reliance Manufacturing Co. (Southwark)	H376	Telegraph Condenser Co.	L511
Leeds Meter Co.	J401	Research & Control Instruments	D164	Telephone Manufacturing Co.	H352
Leavers-Rich Equipment	R837	Richard Allan Radio	H371	Tequipment	S853
Levell Electronics	H363	Rivlin Instruments	R815	Tesla n.p., Czechoslovakia	G306
Lewis Spring Co.	S867	Roband Electronics	R808	Texas Instruments	E216
Lintronic	B55	Robinson D., & Co.	B76	Thermal Syndicate	C106
Lion Electronic Developments	L500	Robinson, F. C., & Partners	B51	Thorn Electrical Industries	H369
Livingston Laboratories	F254	Rola Celestion	F271	Tinsley, H., & Co.	N607
Lloyds Bank	A9	Rotameter Manufacturing Co.	E210	Tintometer	A12
Lodge Plugs	M553	Royal Worcester Industrial Ceramics	B54	Torsion Balance Co., U.S.A.	Q719
London Electric Wire Co. and Smiths	B71	Royston Instruments	R821	Trist, Ronald & Co.	F262
Loughborough Glass Co.	M556	Rumburske Kovozaovody, Czechoslovakia	G306	Trumeter Co.	R836
Lucas, Joseph (Electrical)	Q743			Turner, Ernest, Electrical Instruments	C100
Lyons, Claude	Q733			Turton Bros. & Matthews	Q720
		S.E. Laboratories	D167	20th Century Electronics	Q713
M.B.C. (Office Systems)	R822	S.FIM (Great Britain)	E211	Tylers of London	A1
M.C.P. Electronics	Q708c	Salford Electrical Instruments	E220		
M-O Valve Co.	E211	Samson Controls (London)	E220	Ultra Electronics	H364 & R820
MSS Recording Co.	Q712	Sanders, W. H. (Electronics)	L506	Unicam Instruments	D154
Magnetic Devices	J407	Sangamo Weston	R826	United Trade Press	G300
Mallory Batteries	P656	Saunders-Roe	R828		
Marconi Instruments	D157	Saunders Valve Co.	R828		
Markem (U.K.)	R835	Savage, W. Bryan	D154	Vactric (Control Equipment)	M555
Marrison & Catherall	R812	Sciaky Electric Welding Machines	R833	Veb Elektro-Apparate-Werke, E. Germany	Q748
Marshall of Cambridge Electronics	B63	Scott, James & Co.	Q703	Veeder-Root	S857
Mason, E. N., & Sons	E201	Servomex Controls	F255	Venner Electronics	Q737
McMurdo Instrument Co.	D168	Shaw Moisture Meters	S856	Vieweg, Friedr. & Sohn, W. Germany	F269
Measurement	E221	Short Brothers & Harland	M557		
Mec-Test	Q740	Short & Mason	G301	Walker, Crossweller & Co.	Q700
Metaducts	R820a	Siemens & Halske AG., W. Germany	B73	Waveforms	M550
Metal Detection	G233	Sierex	G324	Wayne Kerr Laboratories	E217
Meterflow	D167	Sifam Electrical Instrument Co.	S855	Webb, William A.	B50
Metrix Instruments	E219	Smith & Nephew	L501	Welwyn Electrical	S863
Micanite & Insulators Co.	L512	Smiths Aircraft Instruments	F257	West, A., and Partners	F252
Microcell Electronics	C108	Société D'Applications des Machines Motrices, France	B72	West Instrument	H354
Midland Bank	Q734	Solartron Electronic Group	E206	Westinghouse Brake and Signal Co.	Q707
Mine Safety Appliances Co.	Q718	Southern Instruments	D158	Westminster Bank	Q708
Minerva Detector Co.	G309	South London Electrical Equipment Co.	B56	Westool	Q725
Ministry of Electric Components	S854	Sovirel, France	Q710a	Whiteley Electrical Radio Co.	R800
Moncrieff, John	H356	Spear Engineering Co.	D171	Willy, Aumann K.G., W. Germany	B73
Morbark	S860	Sperry Gyroscope Co.	C101	Williams & James (Engineers)	D160
Morgan Crucible Co.	K456	Standard Telephones and Cables	K459	Wilmot Breeden	Q708d
Muirhead & Co.	E207	Stanley, W. F., & Co.	Q706	Winston Electronics	M564
Mullard	C102 & M559	Stanton Instruments	G316	Wire Products & Machine Design	B65
Murphy Radio	E209	Stevens Manufacturing, Co., U.S.A.	Q746	Wireless World	J404
		Stonebridge Electrical Co.	S859	Woden Transformer Co.	A7
		Stratton & Co.	K450	Wolsey Electronics	S863a
NSF	B57	Submarine Signal Co. (London)	H366	Worcester Royal Porcelain Co.	H356
Nagard	G312	Swartwout Co.	D155		
Nalzer Bros. & Thompson	C109	Swift Levick & Sons	F273	X-Lon Products	B67
Nash & Thompson	F258	Taylor Electrical Instruments	P655	Zeal, G. H.	L504
Negretti & Zambra	C105	Taylor Controls	D161	Zenith Electric Co.	F272
Neoflex	F270	Techna (Sales)	Q746		
New Western (Eng.)	A6				
Newmark, Louis	B74				
Newmarket Transistors	G307				
Newport Instruments	Q715				
Nicolson, W. B. (Scientific Instruments)	N603				
Norgren, C. A.	B61				
Normalair	R826				
Nottingham Thermometer Co.	L509				
O.M.I. Instruments (G.B.)	R816				
Oldenbourg, R., Verlag, W. Germany	F269				
Oliver Pell Control	R809				
Opancol	Q708b				
Optical Works	H362				
Otter Controls	Q741				
Ozalid Co.	D151				
P. & H. Engineering Co.	S866				
Packaging Centre	Q749				
Painter & Co.	B60				
Palmer, G. A. Stanley	R816				
Panax Equipment	S870				
Panellit	D155				
Parmeko	R804				
Payne & Griffiths	H358				
Peel, H. W., & Co.	H374				
Pergamon Press	H378				
Perkin-Elmer	1405				
Permalit	Q702				
Phoenix Telephone & Electric Works	R817				
Photoelectronics (M.O.M.)	A2				
Planche, M., France	S861				
Plannair	K464				
Platon, G. A.	G317				
Plessey Group	M558				
Polypenco	Q709a				
Precision Tool & Instruments Co.	M552				
Process Control and Automation	G308				
Pullin, R. B., & Co.	C103				
Pye	D154				
Pye, W. G., & Co.	D154				
Quickfit & Quartz	C112				
RCA Great Britain	Q708a				
Racal	F260				
Radiochemical Centre U.K.A.E.A.	H355				

BOOKS RECEIVED

Basic Electronics, by Bernard Grob. Vol. 1 follows the order of topics presented in the first term's work of the technicians' training course at RCA Institutes, starting with elementary electricity and magnetism and ending with a brief insight into valves, transistors and radio frequency losses. It is to be followed by a second volume on Applied Electronics. Pp. 524; Figs. 383. Price 50s 6d. McGraw-Hill Publishing Co., Ltd., 95, Farringdon Street, London, E.C.4.

Proceedings of the National Electronics Conference, 1958 (Vol. 14). Illustrated record (99 papers) of the annual conference held at Hotel Sherman, Chicago, Illinois, covering all aspects of radio and electronics from antennas to automatic navigation and from audio to computers. Pp. 1074, profusely illustrated. Price \$7.50. National Electronics Conference, Inc. 228, N. La Salle Street, Chicago 1, Illinois, U.S.A.

A Quality-Checking Receiver for V.H.F./F.M. Sound Broadcasting, by C. G. Mayo, M.A., B.Sc., M.I.E.E., B.B.C. Engineering Division Monograph

No. 25, gives circuit diagrams and performance details of two alternative prototype receivers, designed, without compromise to give a high standard of performance. Pp. 15; Figs. 13. Price 5s. B.B.C. Publications, 35, Marylebone High Street, London, W.1.

Testing of Screened Enclosures, by J. Miedzinski, B.Sc., A.M.I.E.E. Methods of measuring insertion loss and its dependence on the details of experimental arrangements as well as on frequency and the construction of the enclosure. Pp. 27; Figs. 19. Price 24s. The British Electrical and Allied Industries Research Association, Thorncroft Manor, Dorking Road, Leatherhead, Surrey.

Insulation for Small Transformers, by J. H. Mason and C. G. Garton. Handbook for designers reviewing the factors influencing electric strength and life of insulation, methods of non-destructive testing and data on new materials. Pp. 93; Figs. 33. Price 37s 6d. The British Electrical and Allied Industries Research Association, Thorncroft Manor, Dorking Road, Leatherhead, Surrey.

Power Transformer Design

With Special Reference to Paper Interleaved Windings

By D. SAULL

THE development engineer in the electronic industry requires, from time to time, to design a power transformer for the equipment he is developing. The number of transformers he designs in the course of a year is usually relatively few; consequently it is necessary for him to become familiar with the "know how" of space factor, compensation, winding resistances, etc., each time.

In various technical journals are published graphs and charts for establishing space factor and gauges of wire, etc., but to date the writer has not come across any data which does not require some preliminary digesting before a start can be made.

The most common need in this industry is for relatively low-power mains transformers usually not in excess of 150VA. The writer's aim is to present a really easy, straight-forward method of design to cover six VA ratings, the first four applicable to equipment requiring valve heater supplies, and the remaining two for transistor power units of smaller physical size. The factors presented in the design data contained in this article are based upon practical results obtained from more than a hundred experimental transformers wound with terminal voltages to

M.O.S. specification ($\pm 2\frac{1}{2}\%$ below 100V and $\pm 5\%$ above 100V).

The VA ratings referred to are 150VA, 100VA, 60VA, 35VA in the first group, and 20VA and 10VA in the second group.

The development engineer in the first instance requires to produce a transformer that will function in the equipment he is designing. His second need is to produce this transformer as a practical production winding which may be passed on to the drawing office without further modification. It must, therefore, be electrically and constructionally sound. It must not be a tight wind but must possess sufficient space tolerance to allow for variation in wire sizes ($\pm 10\%$ diameter = 20% cross-sectional area—wire manufacturers' tolerance).

Transformer windings may be layer wound on formers with end cheeks, or paper interleaved and wound on cheekless formers. This article is based upon the latter method. Cheekless-former windings lend themselves to better inspection during the winding process, it being very easy to detect a dropped down turn, which in the end cheek variety could not be detected and might result in a shorted

TABLE I—PRIMARY RATINGS

	100-150VA	60-100VA	35-60VA	25-35VA	10-25VA	8-10VA
Laminations (M.E.A.: Silcor 25) ..	60A	75A	75A	24A	101A	68
Stack size	1½ in	1½ in	1 in	1½ in	1½ in	¾ in
Window area	2.75 sq. in	2.375 sq. in	2.375 sq. in	1.42 sq. in	0.84 sq. in	0.644 sq. in
Primary turns per volt	3.56	4.42	6.68	7.83	7.4	10.5
Secondary turns per volt ..	3.81	4.76	7.15	8.4	7.9	11.2
Overall space factor	44%	46%	46%	48%	50%	50%
Area occupied by 250V primary winding	0.585 sq. in	0.624 sq. in	0.65 sq. in	0.363 sq. in	0.267 sq. in	0.194 sq. in
250V primary (Turns and wire gauge)	890t: No. 23 s.w.g.	1104t: No. 24 s.w.g.	1670t: No. 26 s.w.g.	1960t: No. 30 s.w.g.	1850t: No. 32 s.w.g.	2620t: No. 36 s.w.g.
Remaining area for h.t. and l.t. windings	0.955 sq. in	0.656 sq. in	0.63 sq. in	0.365 sq. in	0.153 sq. in	0.128 sq. in
6.3-V winding to fill layer ..	3.6A—7.2A 24t. 2 × 18 s.w.g.	4A—8A 30t. 15 s.w.g.	1.8A—3.6A 45t. 18 s.w.g.	0.5A—1.2A 51t. 22 s.w.g.	1A—2A 50t. 20 s.w.g.	—
5-V winding to fill layer	19t. 2 × 16 s.w.g.	24t. 2 × 19 s.w.g.	36t. 17 s.w.g.	42t. 21 s.w.g.	—	—
Former length	2¾ in	2¾ in	2¾ in	1¾ in	1¾ in	1¾ in

turn, or worse, a failure occurring early in the life of the transformer.

L.T. windings should be wound on first for two reasons:—

- (1) They are wound with the thickest wire, and therefore form a good base on which to wind the thinner wire of the remaining windings.
- (2) The l.t. windings carry the heaviest current, thus putting these windings on first results in a shorter mean-turn length. They consequently have a lower d.c. resistance and a better regulation percentage figure.

The l.t. winding should completely fill the available width, a bifilar wind can be used if a single winding at the required current capacity does not fill the layer. Current densities of these windings may be 1,500A or 2,000A per square inch.

A transformer design may call for four or more separate l.t. windings, perhaps two at 4A and two at 2A with a primary rating of the order of 150VA. In this case the 4-A winding should be wound on first, and the two 2-A windings wound side by side as a single layer with $\frac{1}{2}$ in spacing at the centre between them. This saves valuable space which might well be required to allow a more generous wire gauge on the h.t. winding.

Where the occasion arises calling for a l.t. winding of low-current capacity (e.g. order of $\frac{1}{2}$ A) difficulty might be experienced in choosing a wire gauge to fill the layer. In this case, this winding may be wound on last, and placed centrally on the windings. Due to the low current value the voltage regulation would not be effected by the increased length of wire, and it would be convenient to operate the winding with a current density not greater than 1,000A per square inch.

The primary winding is wound on next with voltage taps as required, followed by the h.t. windings.

The choice of wire gauge for the h.t. winding should be as generous as possible to keep its d.c. resistance as low as possible. With full-wave rectification a good practical rule is to assume that each half winding will carry not less than an average of 0.7 of the d.c. output current, at a current density of 1,000A per square inch (this is not strictly true because a.c. current surges are in excess of the d.c. current and dependent on the rectifier used and the value of the reservoir capacitor—the 0.7 factor is a practical compromise).

Windings throughout the transformer should be in order of wire gauges, that is, the heaviest wire nearest the core, the lightest wire on the outside winding.

Table I sets out for easy reference the information required when designing a transformer. The space factor given is an overall figure and takes into account the former, insulation and wire tolerances. The space factor for a given lamination will remain reasonably constant for any gauges likely to be used at the respective VA rating.

Insulation throughout the transformer is as follows:—

- (1) Three layers of Britain's (0.002in) tissue on the former.
- (2) 2 layers of Symax (0.005in) between windings.
- (3) One layer of Britain's tissue (0.002in) interleaving between layers throughout primary and h.t. windings.
- (4) Two layers of Symax (0.005in) between layers of l.t. windings occupying more than one layer.

TABLE II

Dia.	T/in	T/in ²	Current at 1,000A/in ²	S.W.G.
0.131	7.6	57.8	12.9	10
0.119	8.4	70.6	10.6	11
0.107	9.3	86.5	8.5	12
0.095	10.5	110	6.65	13
0.083	12.0	144	5.03	14
0.0745	13.4	180	4.07	15
0.0665	15.0	225	3.22	16
0.0586	17.0	289	2.46	17
0.0505	19.8	392	1.81	18
0.0422	23.6	557	1.26	19
0.0382	26.1	681	1.02	20
0.0340	29.4	864	0.804	21
0.0300	33.3	1,110	0.616	22
0.0257	38.9	1,520	0.452	23
0.0237	42.1	1,770	0.380	24
0.0217	46.0	2,120	0.314	25
0.0197	50.7	2,570	0.255	26
0.0179	55.9	3,120	0.211	27
0.0163	61.3	3,760	0.172	28
0.0151	66.2	4,380	0.145	29
0.0136	73.5	5,400	0.121	30
0.0128	78.1	6,100	0.106	31
0.0120	83.3	6,940	0.0916	32
0.0112	89.2	7,960	0.0785	33
0.0102	98.0	9,600	0.0665	34
0.0094	106	11,200	0.0554	35
0.0086	116	13,500	0.0454	36
0.0078	128	16,400	0.0363	37
0.0070	143	20,400	0.0283	38
0.0059	169	28,600	0.0212	39
0.0055	182	33,100	0.0181	40
0.0051	196	38,400	0.0152	41
0.0047	212	44,900	0.0126	42
0.0043	233	53,300	0.0102	43
0.0039	256	65,500	0.0080	44

Table II sets out details of characteristics of enamelled copper wire for use with the design data given here.

Example of Practical Design—

- (a) Tabulate the secondary VA ratings required:—

LT1. 5.0V at 2.5A = 12.5VA
 LT2. 6.3V at 3A = 18.9VA
 HT. 250-0-250V at 60MA = 15.0VA

Total = 46.4VA

Primary VA at 86% efficiency = $46.5/0.86 = 54VA$.

- (b) From Table I No. 75A laminations and a 1in stack is required.

- (c) Windings (from Table I)

LT1. 36 turns of 17 s.w.g. En Cu wire.
 LT2. 45 turns of 18 s.w.g. En Cu wire.
 Space remaining for l.t. and h.t. = 0.63 sq in.
 LT1. = $36/216 = 0.167$ sq in.
 LT2. = $45/392 = 0.115$ sq in.

Total = 0.282 sq in.

Space remaining for h.t. winding = 0.348 sq in.

- (d) Turns required for h.t. winding at 7.15 turns per volt = $7.15 \times 500V = 3,576$ turns.

- (e) Choice of wire gauge = $\frac{\text{Number of turns}}{\text{Space available}} =$
 T/in^2 (turns per square in) = $3576/0.348 = 10,800 T/\text{in}^2$
- (f) From Table II nearest gauge = 35 s.w.g. (55.4mA)
 or even gauge No. 36 s.w.g. (45mA).
- (g) Winding details would then be:—
 LT1. 36 turns No. 17 s.w.g. En Cu wire.
 LT2. 45 turns No. 18 s.w.g. En Cu wire.

Primary 230V, 1,533 turns } No. 26 s.w.g.
 240V, 1,602 turns } En Cu wire.
 250V, 1,671 turns }
 H.T. 3,576 turns No. 36 s.w.g. (or 35 s.w.g.)
 En Cu wire tapped at 1,788 turns.

It will be seen that the time required to design a transformer from the given data should not be more than half an hour.

After the prototype has been tested in circuit, and any necessary modifications due to circuitry changes have been made the transformer is ready to be placed in production.

Nuclear Explosions and Radio Noise

EFFECT OF HIGH ALTITUDE BURSTS ON RADIO PROPAGATION

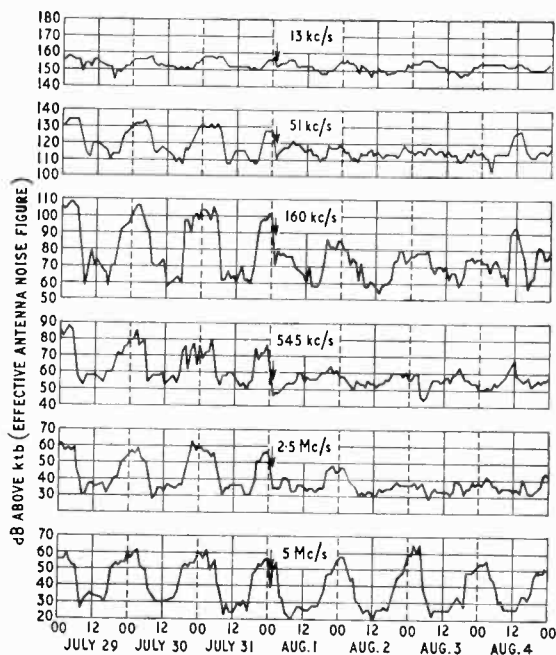
By MICHAEL LORANT

THE U.S. National Bureau of Standards recorded the changes in radio noise power that occurred when two high-altitude atomic explosions were set off over Johnston Island in the Pacific Ocean in August, 1958. The explosions appear to have had a pronounced effect on the radio noise as recorded at Kekaha, Hawaii. This recording station, located on the south-west coast of the island of Kauai, about 700 miles north-east of Johnston Island, is part of a world-wide chain of noise-recording stations supervised by the Bureau's Boulder (Colorado) laboratories.

Two bomb bursts occurred shortly after midnight on August 1 and August 12 at elevations estimated to be from 25 to 100 miles. Recordings were made of the received atmospheric radio noise power for a period before and after the first explosion. The usual diurnal pattern is evident on the graphs* during the three days prior to the blast, with the highest noise levels recorded at night and a rapid decrease in level between 0400 and 0800 local time. In the hour following the blast, however, the noise decreased by as much as 32dB (at some frequencies) at a time of day when it would normally be rising or holding steady. Recovery apparently occurred in a matter of hours at 13kc/s and 5Mc/s, but from 51kc/s through 2.5Mc/s a changed pattern is evident for several days, and records for August 5-11 indicate that a disturbed condition persisted until the second test on August 12. The after-blast effects on this date were similar to those on August 1, with abnormal noise conditions continuing on some frequencies until about September 1.

Because of the very low incidence of thunderstorms in Hawaii, most of the received radio noise is believed to be propagated from storms at a considerable distance. Thus, changes in propagation conditions are reflected more on the Kekaha noise records than at stations situated on large masses,

* The "effective antenna noise figure" is the mean noise power averaged over several minutes and is defined as the noise power available from an equivalent lossless antenna in decibels above the thermal-noise power available from a passive resistance. See "N.B.S., Radio and Ionospheric Observations During the I.G.Y.," David M. Gates, *J. Res. N.B.S.* 63D, July-August, 1959, p. 11.—Ed.



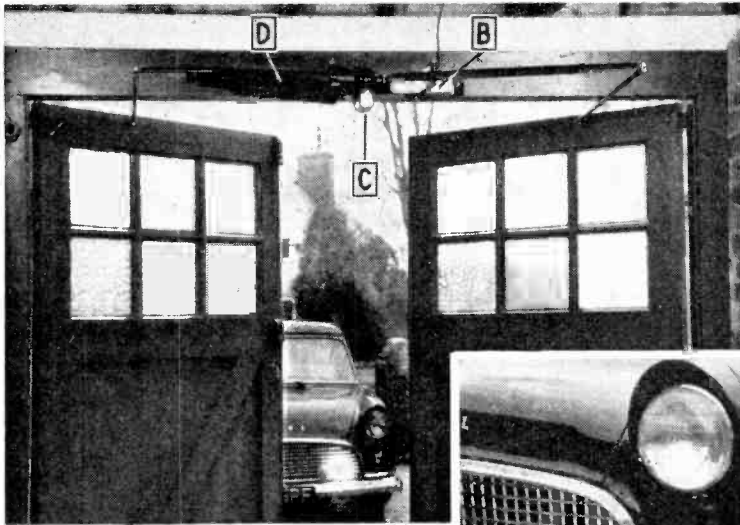
Graphs of radio noise power recorded at Kekaha, Hawaii, July, 29 to August 4, 1958. Time of nuclear explosion on August 1 indicated by arrows.

where local and short-distance storm effects tend to mask changes in propagation.

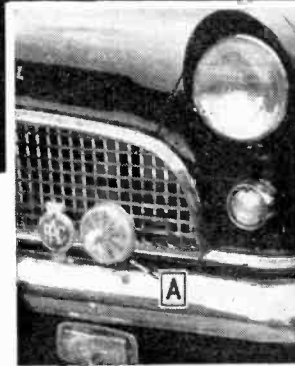
It would appear likely that a highly ionized region was formed by the bomb explosions over Johnston Island and that this ionized region persisted for a period of at least several days after each test, causing greatly increased ionospheric absorption.

REFERENCE

"Effects of High-Altitude Nuclear Explosions on Radio Noise," by C. A. Samson, *J. Res. N.B.S.* 64D, p. 37 (Jan.-Feb. 1960).



Kinetrol "Magi-Dor" mechanism for opening garage doors. A, "chopped" light source; B, transistor amplifier and relay; C, latch solenoid; D, control spring and damper.



TRANSISTORIZED DOOR CONTROL

IN a light-controlled garage door opening mechanism developed by Kinetrol Ltd., Trading Estate, Farnham, Surrey, the use of a photo-transistor followed by a transistor a.c. amplifier ensures that the device operates only with light interrupted within a specified range of frequency; it cannot be triggered by steady light or even by headlamps switched on and off by hand. The high-speed chopped light source necessary to actuate the mechanism is provided by a rotating shutter driven by a small d.c. motor incorporated in the transparent plastic lens of a small spot light mounted on the front of the car and controlled from the dashboard.

The photo-transistor is housed in a black moulding about 1 inch in diameter, screwed to the garage door frame. Saturation by ambient light is avoided by restricting the aperture of exposure. The alternating component resulting from illumination by the car's special lamp is amplified, rectified and applied to a P.O.-type relay with mains contacts which energizes a solenoid and releases the bolt latch. The doors, which are spring loaded, then open at constant speed under the control of a linear damping device.

We have had an opportunity of examining one of these installations, which operated reliably under daylight conditions at a distance of 20ft

or less and seemed to us to be soundly designed and made.

The complete installation costs £39 10s.

CLUB NEWS

Birmingham.—John Savage, director of engineering of Collins Radio Company of England, is to give a lecture-demonstration on the new Collins series of s.s.b. equipment at the meeting of the Slade Radio Society on June 17th at 7.45 at The Church House, High Street, Erdington. Admission is by ticket only obtainable from the secretary, C. N. Smart, 110, Woolmore Road, Erdington. The subject to be discussed at the June 3rd meeting is entitled "Technical problems in sound and vision."

Bristol.—The third mobile rally to be organized by the Bristol Group of the Radio Society of Great Britain will be held on June 26th at Longleat House, near Warminster, Wilts. Details of the day's programme are obtainable from the secretary, D. F. Davies (G3RQ), 51, Theresa Avenue, Bishopston, Bristol, 7.

Mitcham & District Radio Society, which meets every Friday at 8.0 at The Canons, Madeira Road, now has four slow-morse tapes available for loan to members.

Prestatyn.—At the June 6th meeting of the Flintshire Radio Society, J. Thornton Lawrence (GW3JGA), secretary of the society, will give a talk on audio amplifiers. The meeting will be held at 7.30 at the Railway Hotel.

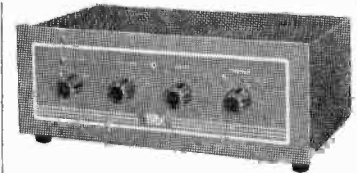
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RANDOM RADIATIONS

By "DIALLIST"

"Things Great and Small"

THE National Bureau of Standards and the International Committee on Weights and Measures of the U.S.A., have, I see, approved for general use four numerical prefixes which have been used for some time in Europe. They are tera (symbol T) = 10^{12} , giga (G) = 10^9 , nano (n) = 10^{-9} , and pico (p) = 10^{-12} . Their adoption is most welcome, for it should help to clear up the confusion which terms such as billion (10^{12} with us, 10^9 with the Americans) and trillion (10^{18} and 10^{12} respectively) have long been causing. I do think, however, that the names might have been more happily chosen. In the metric system the terms are based on Greek and Latin numerals; Greek as you go up from unity (deca-, hecto-, kilo-, etc.) and Latin as you go down (deci-, centi-, milli-, etc.) though there's a slip-up over micro-. The system worked splendidly until

vey in fact vague suggestions of the enormous, gigantic, the dwarfish and the tiny. I can't see why terms such as hectomega (10^8), kilomega (10^9) and megomega (10^{12}) shouldn't have been chosen, with symbols hM, kM and MM, for the big numbers. As micro and micromicro have already made their Greek appearances among the tinies why not millimicro ($m\mu$) for 10^{-9} ? These prefixes would anyhow show definitely what they mean without any sort of vagueness.

819-line DX

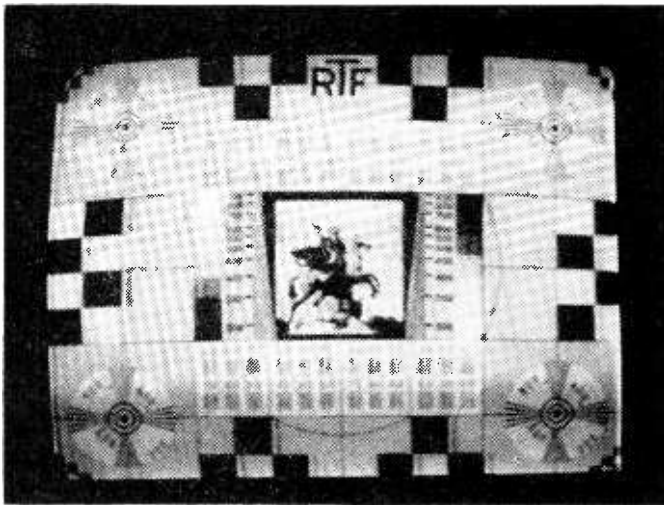
FROM a Harrow, Middlesex, reader comes a most interesting account of a deliberate attempt made to receive French television programmes here. That it was a success you'll gather from the accompanying photograph of the R.T.F. test card on his screen. His firm, he writes, when faced with some knotty problems brought about by their expanding export market,

Medium Waves Too

MY recent note on long-distance v.h.f. reception has also brought forth a letter from an enthusiastic night-owl reminding me that there are still those who are interested in long-distance medium-wave reception. Time was when there was no more enthusiastic night prowler on this band than myself and this sort of reception as a hobby is most rewarding in the way of thrills. I recall, for example, hearing a mysterious heterodyne on a German station at about 9.30 p.m. one winter's night. I left the tuning as it was and switched off, for I'd an idea about that heterodyne. At 2 a.m. or thereabouts, I switched on again and there almost on the same frequency was an American station. There can't be much doubt that its carrier had caused the heterodyne on Hamburg. If any readers who haven't gone in for this kind of exploration care to try it out on a good night, I'm sure they'll be rewarded. There is, of course, the Medium-Wave Circle, which publishes its own duplicated monthly newsletter "Medium Wave News." The January issue had a 6-page supplement of western hemisphere m.w. stations logged in the U.K. since 1951.

Entertainment by Line

THOUGH, as stated in the May *Wireless World*, the relaying of broadcast programmes by wire is nearly as old as broadcasting itself (relaying started in 1927 and broadcasting in 1922) there was in London and possibly in some other cities a wired entertainment service long before that. It was run by a company called, I think, Electrophone, Ltd. and I first came across it when shortly after the end of the first war (possibly in 1919) I was invited as a youngster to stay with some friends of my father's in London. To make use of the service you had to be on the G.P.O. telephone and to subscribe to Electrophone, or whatever its name was. This company paid half a dozen theatres and other places of entertainment, fees for the right to relay their entire programmes for a week or more. The subscriber's home was provided with a small square-topped table, at each side of which hung a set of ear-



words for very large numbers had to be found.

Could be Better

The trouble is that neither the Greeks nor the Romans had any definite single words for quantities above 1,000 or for very small quantities. Hence names for the enormous and extremely minute numbers in use today had to be invented. The four prefixes in question aren't very good inventions because they don't suggest anything definite; they con-

decided to try to obtain direct reception from Lille. A modified British television receiver was used, with an 11-element Yagi mounted on the factory roof some 260-feet above sea level. I congratulate my correspondent most heartily and I hope that his success will induce others to try their hands at long-distance TV reception. In the U.S.A. and Canada it's quite a popular hobby—but the would-be DX-er is more luckily placed as all north American stations use the same standards.

phones. You consulted the list for the current week supplied by the company, then called exchange and asked to be connected to the theatre of your choice. That done you turned a switch which connected the telephone wires to a small distributor box on the table. Four people could then listen to their hearts' content. There was, I recall, an arrangement, whereby, should a call come through for you, the operator at the exchange could break in and inform you. You then switched back to the telephone and took the call, returning when it was finished to the theatre.

V.H.F./F.M. Goes Ahead

WITH the opening of the Orkney v.h.f. sound transmitter on May 2nd, the B.B.C. completed one of the last stages necessary for full country-wide coverage by its three-programme network. Just how wise the B.B.C. was after the war in deciding to plump for v.h.f. for sound broadcasting is very clear to those who live near the south and east coasts and in other places where heterodyning, sideband splutter, and even virtual jamming too often occur on the medium and long waves. One's experience in East Anglia, for instance, is that with a moderately good receiver no station is of much use on the long waves except at odd times. On the medium waves the only B.B.C. programme fairly well received is the Home. Turning to v.h.f. is like going into another world—no interference, no fading, and always clear steady Home, Light or Network Three signals.

Electron Welding and Cutting

THE electron has long proved itself a useful ally when harnessed by the ingenuity of man to perform tasks for him. We're all familiar with its work in the valve and the c.r. tube. But recently new applications have been found for sharply focused, high-velocity electron beams. Two firms, in W. Germany and Switzerland, have, it is reported, developed methods of electron-beam welding for use on metals ordinarily very difficult to join satisfactorily. A similar beam is being used successfully for drilling tiny holes in metals and for cutting slots in steel plates up to one fiftieth of an inch in thickness. The metal pieces that can be welded, drilled or cut must, one imagines, be very small, for an electron-beam can't be sharply focused except in a vacuum chamber.

THE BULGIN BULLETIN

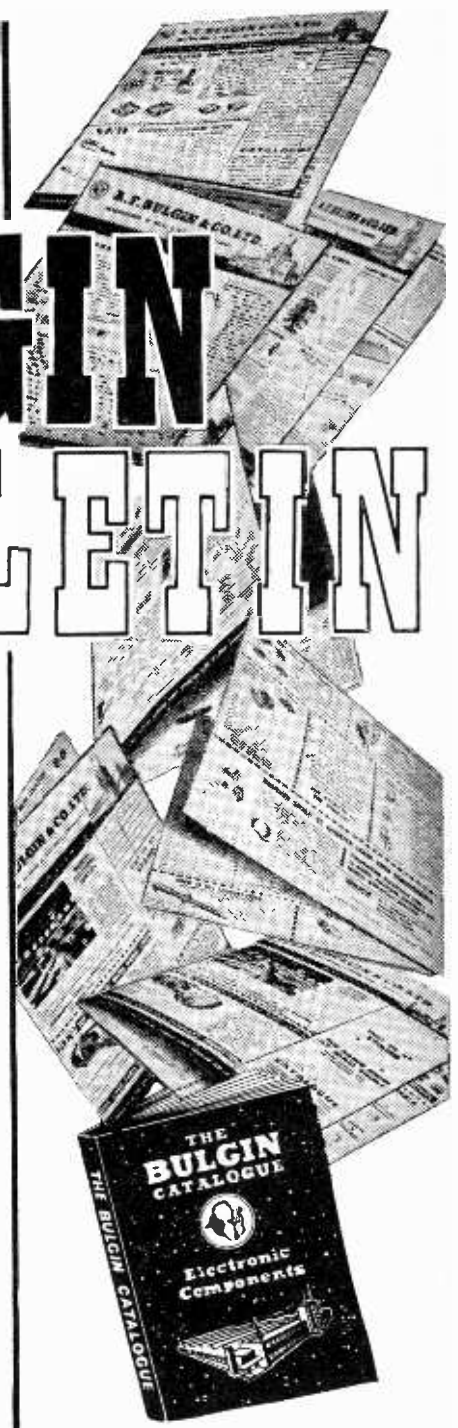
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Audio Fair

THE most obvious new thing at this year's Audio Fair was the presence of stereo tape recorders whereby you could make your own stereo recordings as well as play commercial tapes. Last year there was one such instrument shown but it was a prototype and not actually on sale.

Stereo tape recorders have, of course, been with us for some years but only very expensive super ones not normally intended for home recording.

There is one thing about these new instruments which was not stressed and which I think ought to have been, as several non-technical people to whom I spoke were under quite a false impression about the instruments. They imagined that by using one of them they would be able to "bottle" their favourite broadcast programmes *stereophonically*.

I had quite an argument with some people about it who imagined that it was only necessary to stand the two mikes in suitable positions in front of their sets or to take two feeds from the set to the "radio" input of the recorder. I explained that this would be quite impossible until the B.B.C. starts regular stereo broadcasting.

All this made me rather wonder if the new machines will be used as *recorders* for few people nowadays make their own music at home, although those that do will, of course, be able to record it stereophonically. Also, it will be possible for them to record the amateur theatrical performances in the village hall.

There was also one complete stereo machine which operated at the two speeds of $3\frac{3}{4}$ and $1\frac{7}{8}$ i.p.s. I know that there are some commercial tapes recorded at $3\frac{3}{4}$ i.p.s., but most of them are $7\frac{1}{2}$ i.p.s. I think that if I were paying 89 guineas—the price of this recorder—I should expect to have the $7\frac{1}{2}$ i.p.s. speed. It would, in fact, seem to me to be rather a waste of money to buy a stereo machine at all if I could not have this "hi-fi" speed.

The Fair seemed as crowded as ever on the day I visited it. I understand the total attendance was approximately 32,000.

All the demonstrations at the Fair were as good, or bad, as might be expected when a couple of dozen perspiring people are packed in an hotel bedroom. But quite frankly I don't see what the industry can do about it short of building an exhibition centre incorporating demonstration halls.

The stereo demonstrations did, however, make me realize that listen-

ing conditions in the average home leave much to be desired. My suggestion is that the garages in new houses should be built primarily as listening rooms with soundproof walls and built-in loudspeakers. Then, when it is desired to do some serious listening, the family limousine could be backed out and some chairs taken in.

My suggestion is primarily made because of the terrific volume which, judging by the demonstrations, it is necessary to have nowadays. The neighbours simply would not stand for it. The size and shape of the garage would also enable domestic listeners to sit far enough back from the loudspeaker to get a proper perspective of sound if that is the correct expression to use; more especially for stereo listening.

Fiat Lux

IN the May issue, "Cathode Ray" tells us that he has forgotten the reason why a complete turning of an angle—or in other words a circle—is divided into 360 degrees. So have I, but I believe I am right in saying that the 60-cycle a.c. frequency in the U.S.A. is based on it. If so, maybe some American reader can lighten our darkness.

Bridal Larinometry

WE have all heard that "gentlemen prefer blondes" but this obviously cannot refer to Africa where blondes are conspicuous by their absence; at any rate among the native population. But even there men have their preferences, and it is a matter of common knowledge that among

certain tribes "gentlemen prefer fat girls," in fact for a really outstanding specimen a father can command a price of many head of cattle from his would-be son-in-law.

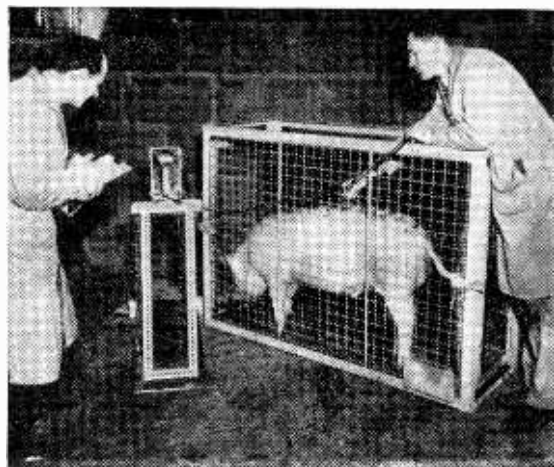
Hitherto a prospective African bridegroom has had to use the necessarily rather crude method of visual inspection when deciding whether one girl was fatter than another. But science has changed all that, as I have been reading in *Pulse*, the bulletin of technical development published by Kelvin & Hughes. An ultrasonic flaw detector is now being used to measure with great accuracy the thickness of body fat. It is true that the technique has not been developed specifically for the African marriage market, but for measuring the thickness of fat on a pig's back, such thickness being, strangely enough, important also in the porcine marriage market.

For this purpose, ultrasonic waves at a predetermined frequency of between 0.5 and 5 Mc/s are transmitted through the fat, and are reflected back at the boundary between the backfat and the lean muscular tissue. The time taken depends on various factors including the thickness of the fat. The measurement is read directly on the graduated scale of a cathode-ray tube.

This technique has, so it is said, already been used to obtain a "photograph" of a man's back muscles and vertebrae, and it is obviously but a step to apply it to performing a similar service in the fatty areas of a female African matrimonial candidate. One can visualize the live-wire salesmen of the firm hastily packing their bags and their portable larinometers.

It won't be long before a prospective African bridegroom will be able to demand the production of an ultrasonic chart by any girl offered to him; and double-crossing fathers-in-law will no longer be able to practise any Laban-like tricks in getting rid of their less attractive daughters.

It is obvious that there are many other uses for this fat-measuring set-up, not the least being to let the surgeon know exactly the amount of fat he has got to cut through before he reaches the seat of the trouble.



An unusual use for a Kelvin Hughes flaw detector.

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* Display storage tubes

Advanced development is now in progress on both bi-stable and half-tone storage tubes. The bi-stable tubes are electrostatically deflected and are intended for use in infinite persistence oscillograph applications. The half-tone tubes are magnetically deflected and provide a bright flicker-free display with controllable persistence characteristics. Uses for these half-tone tubes include radar displays where ambient light levels are high and equipment for the display of information received on slow-scan narrow bandwidth systems.

* Information storage tubes

Tubes are being developed which provide electronic writing and reading facilities for use in information processing systems. Of particular interest is a single-gun tube capable of storing a high resolution television picture for purposes of standards conversion, or processing for band-width compression. In the radar field it has applications in systems employing true-motion display or moving target indication.

* Solid State display devices

Among the solid state devices under active investigation is a light amplifier which utilises a combination of electroluminescent and photoconductive principles. Other devices in this sphere of activity include solid state image converters and multi-element devices.

* Transparent Phosphors

In applications where the ambient light is extremely strong it is possible, in some instances, to maintain contrast by using display tubes with transparent phosphors. Experimental tubes show that although the brilliance of the trace is naturally less than that of a normal tube, only negligible ambient light is reflected from the transparent tube screen, and an effective display is obtained.

* Scan Magnification

Deflection sensitivities of both magnetic and electrostatic industrial and radar tubes of conventional design can, under certain conditions, be increased by factors of 10 times by the use of magnetic and electrostatic lens systems of scan magnification. Substantial progress is being made at the Mullard Research Laboratories in the complex problems which must be resolved before this attractive system becomes a practical proposition.

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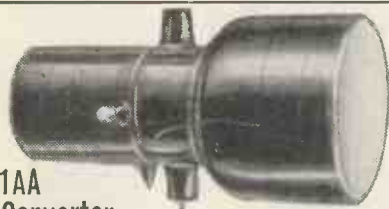
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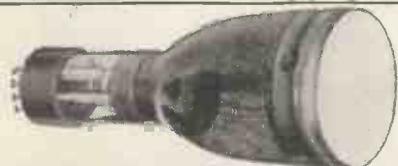
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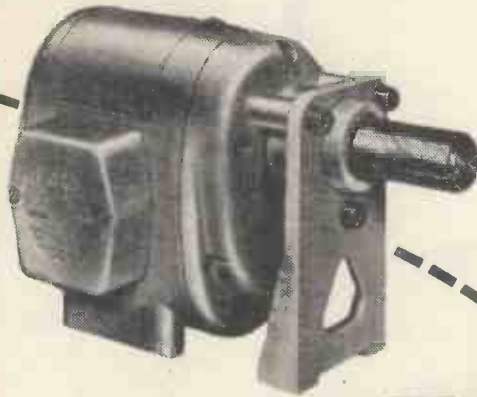
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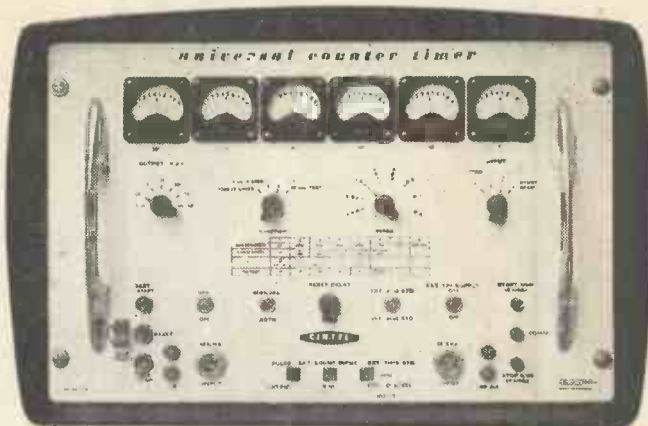
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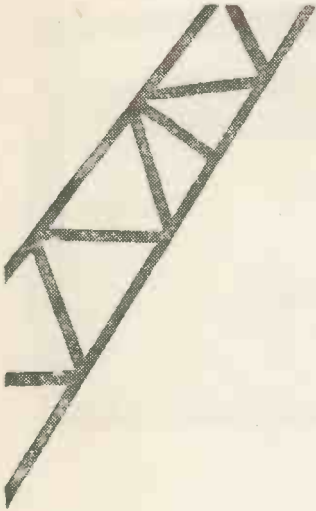
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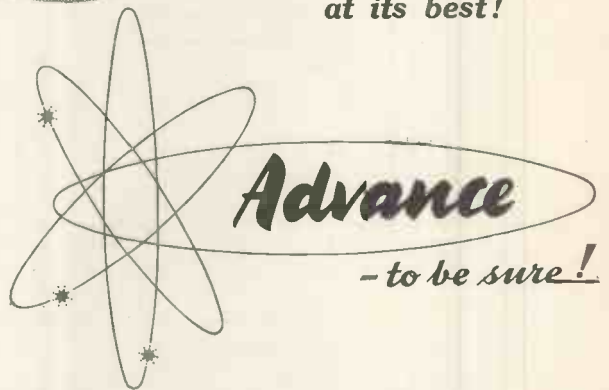
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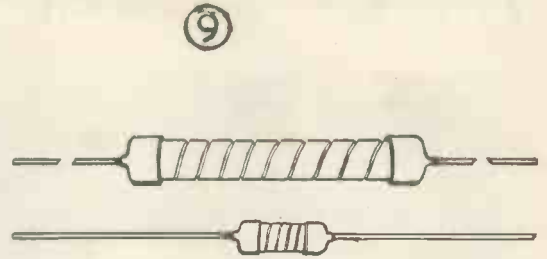
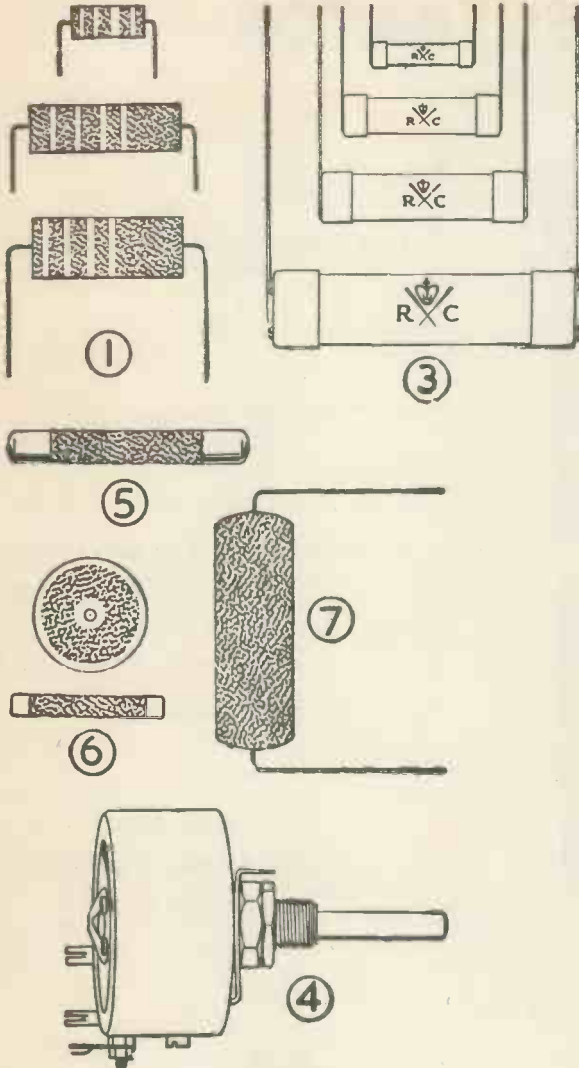
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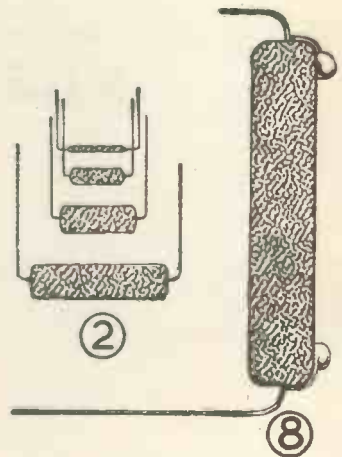
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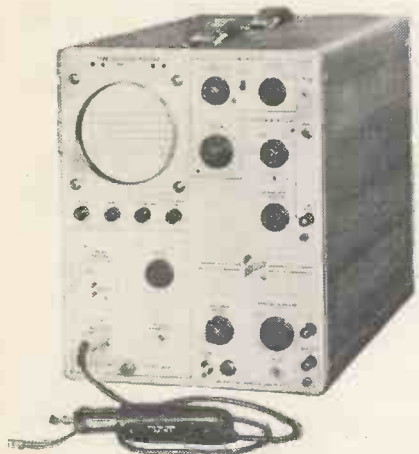
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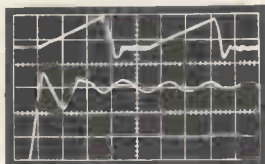
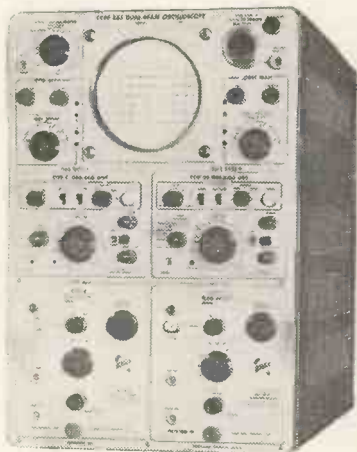
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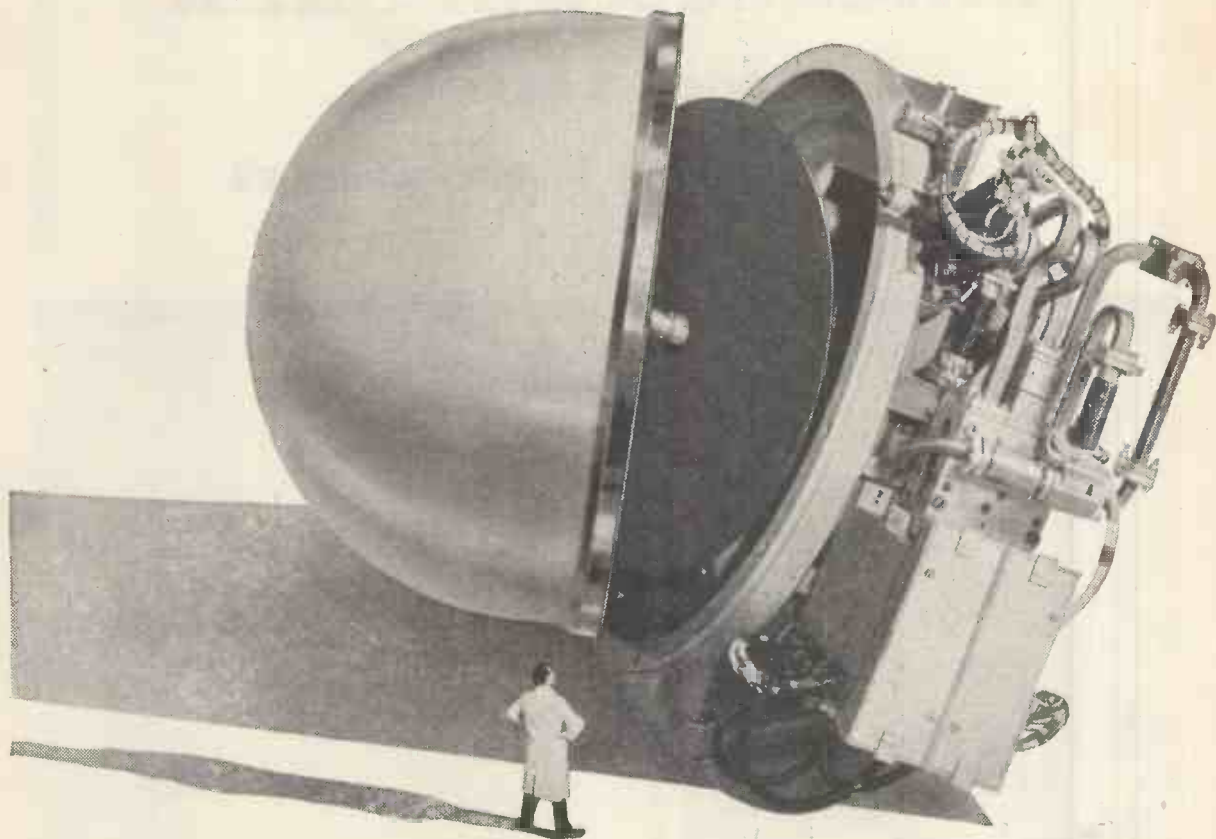
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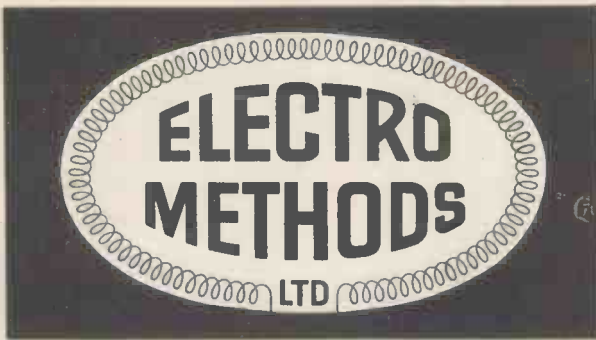
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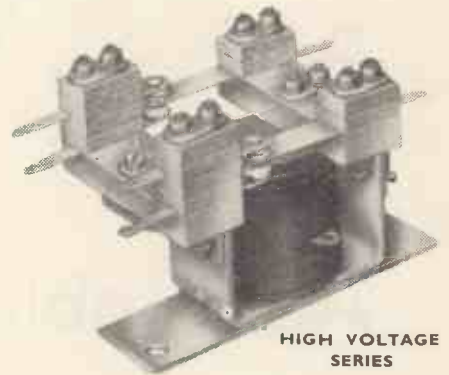
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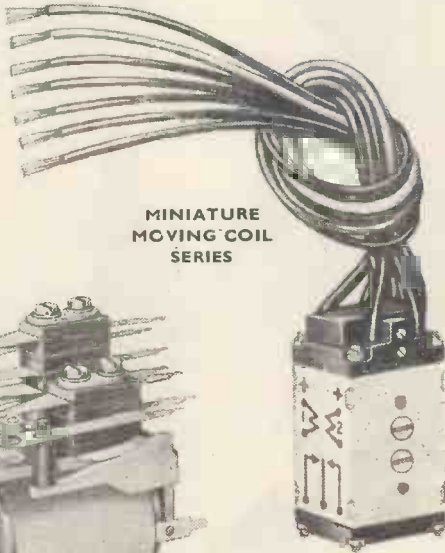
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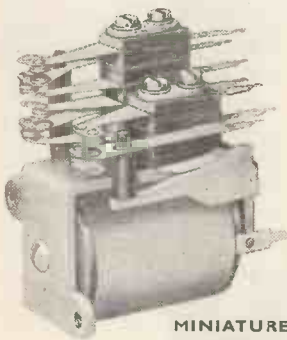
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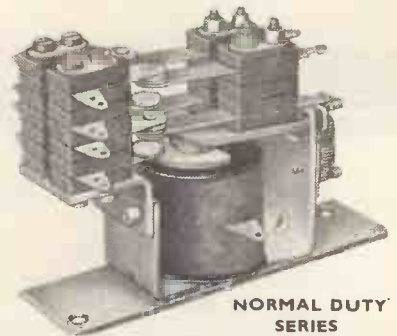
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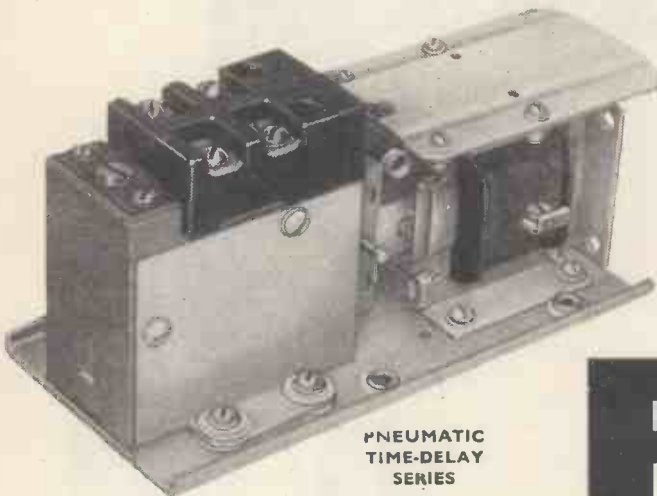
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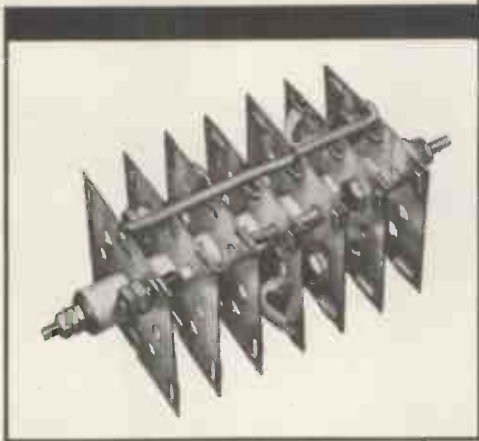
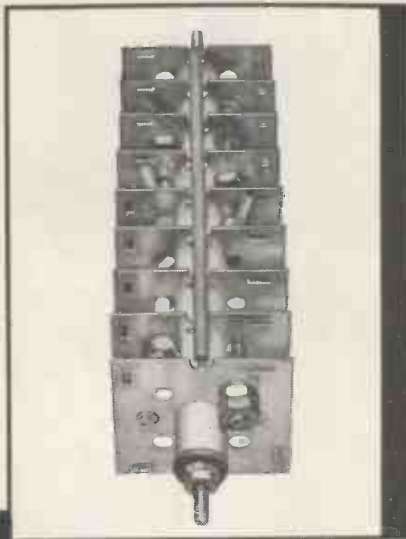
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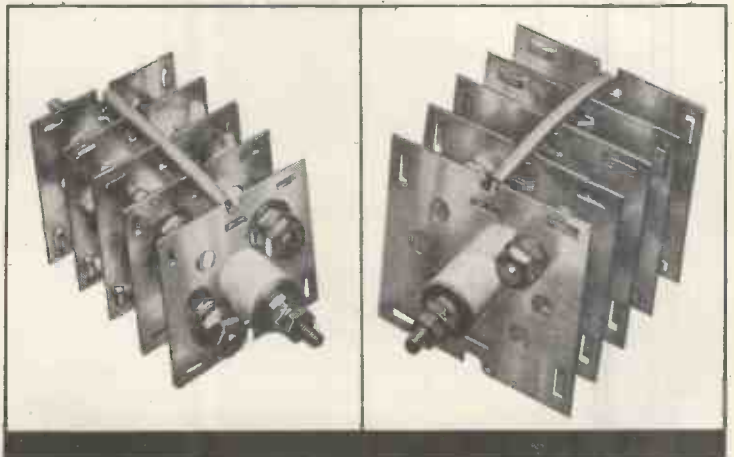
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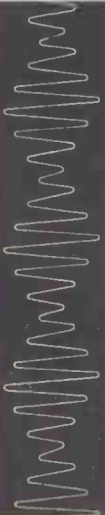
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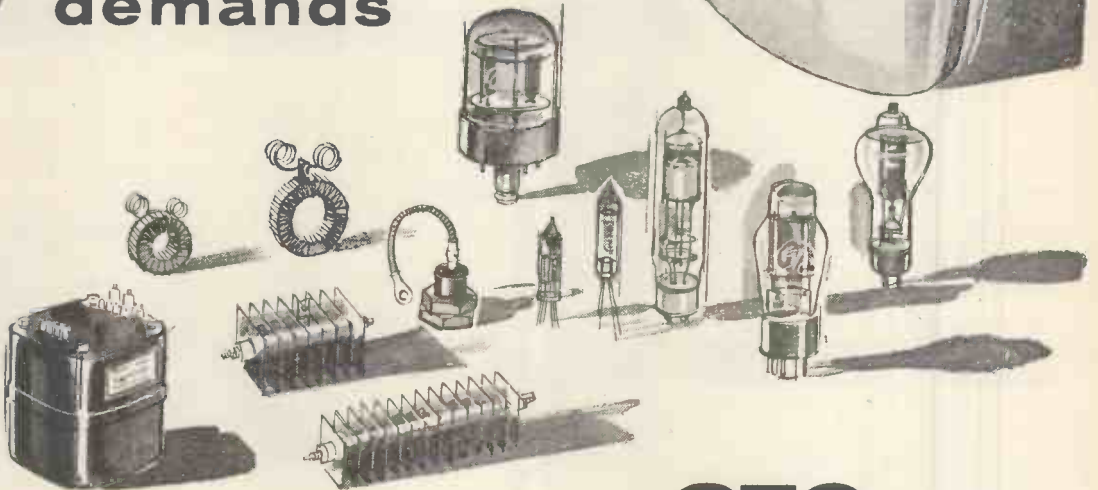
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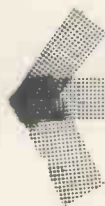
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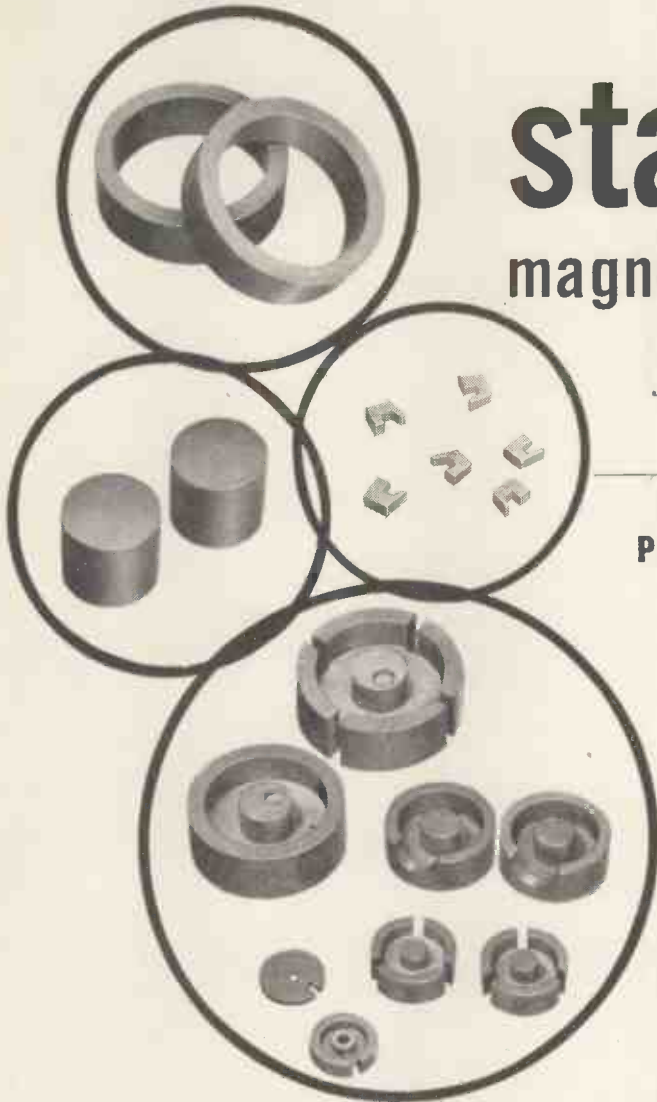


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Material	Initial Permeability	Frequency range of application	Typical applications	Typical Core Shapes
S.F.1 S.F.15	2 000 to 3 000 1 100 to 1 900	Up to 1 Mc/s Up to 1 Mc/s	(Manganese Zinc Ferrites) — both of which have high permeability and low-loss at frequencies up to 1 Mc/s. Wide band and Miscellaneous Types of Transformers High quality Inductors, Communication Transformers, Delay Lines and Recording Heads.	"U" Pot
S.F.3 S.F.11 S.F.14	100	Pulse " "	(Mixed Ferrites)—having substantially rectangular hysteresis loops and therefore eminently suitable for data-processing applications. Memory Arrays and Switching for Data Processing.	Small Toroid and Magnetic Cell
S.F.4 S.F.5 S.F.6 S.F.7 S.F.8	650 250 100 30 15	50 kc/s to 2 Mc/s 200 kc/s to 5 Mc/s 500 kc/s to 15 Mc/s 1 Mc/s to 50 Mc/s 10 Mc/s to 150 Mc/s	(Nickel Zinc Ferrites) — having extremely low eddy-current and dielectric losses rendering them useful over a very wide frequency range up to 150 Mc/s. H.F. Transformers and Inductors, Tuning Coils, Saturable Reactors.	Toroid, "U" Pot and Cylinder

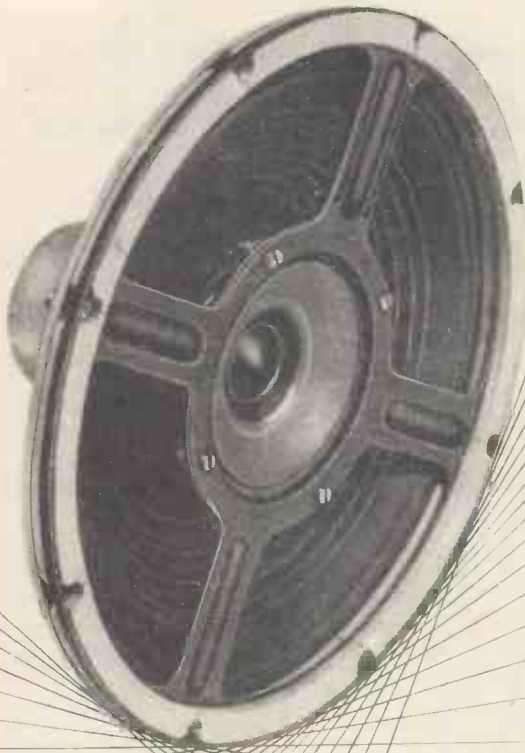
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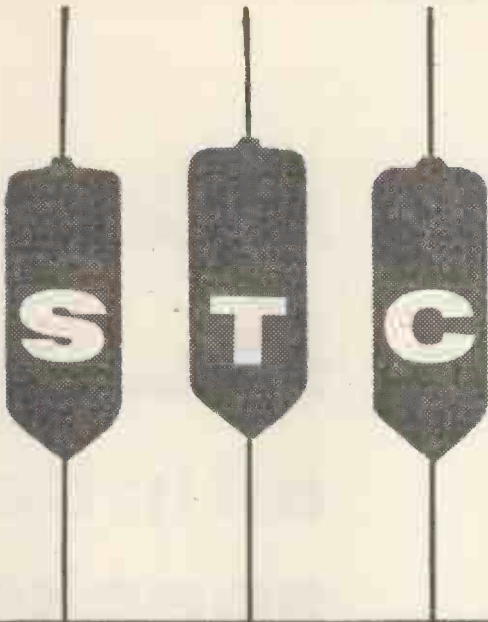




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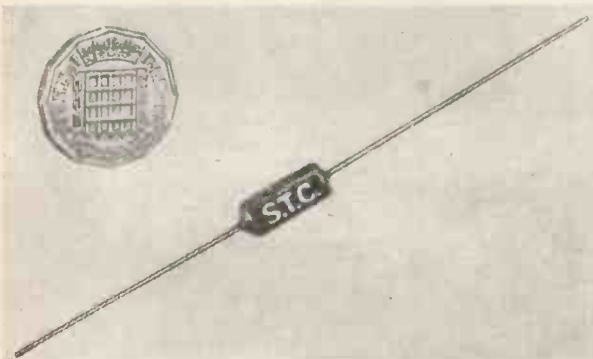
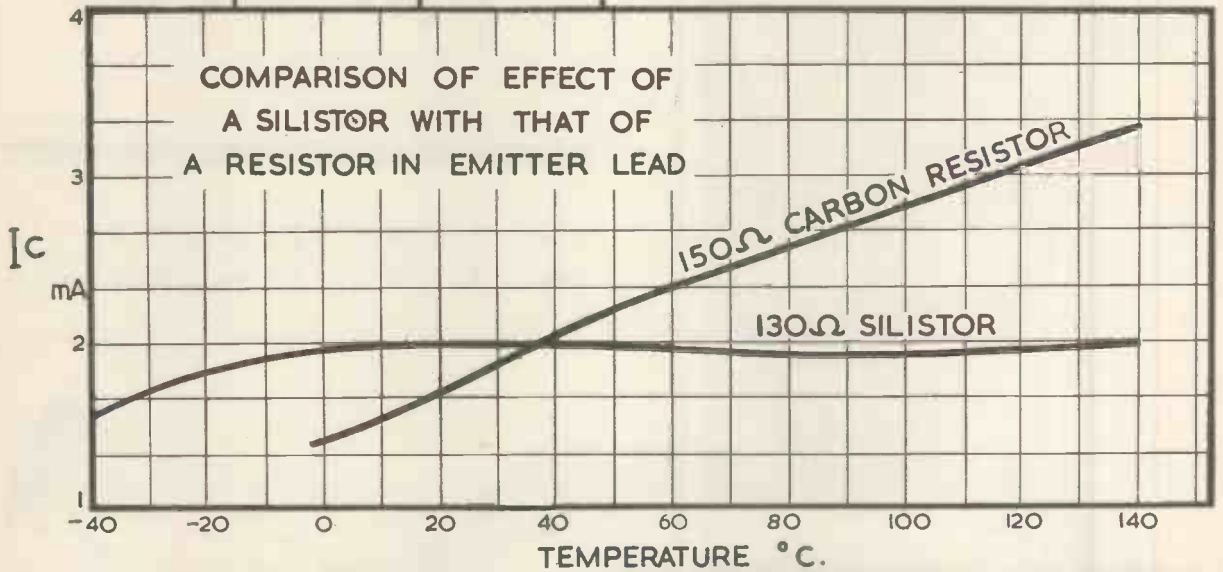
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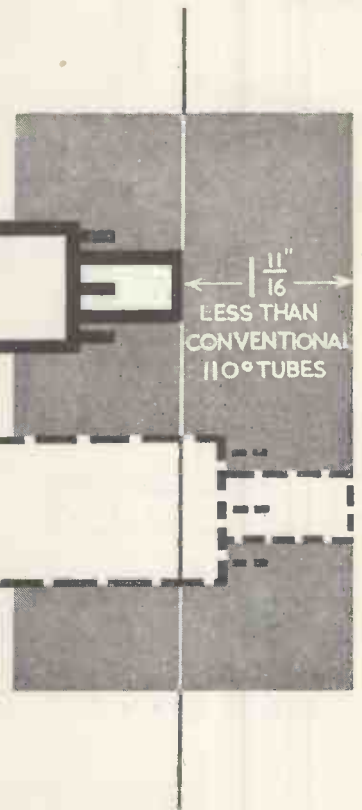
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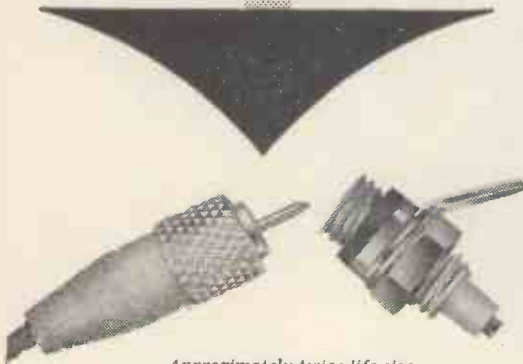
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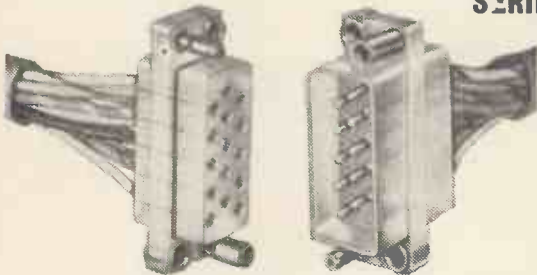
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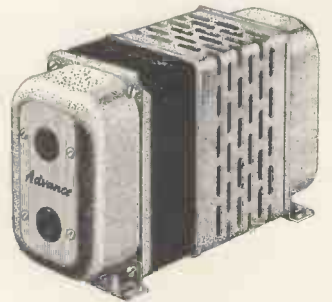
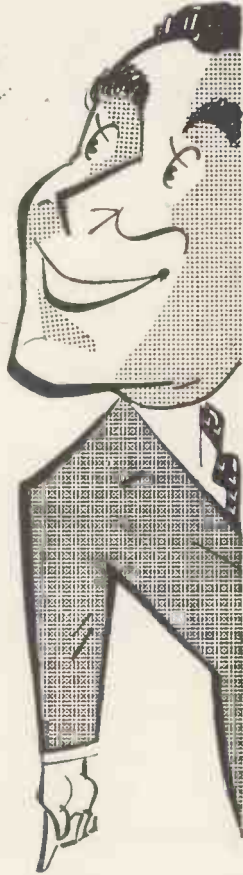
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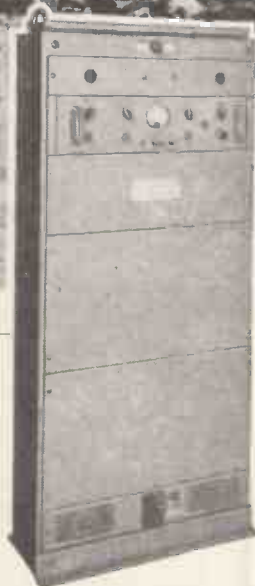


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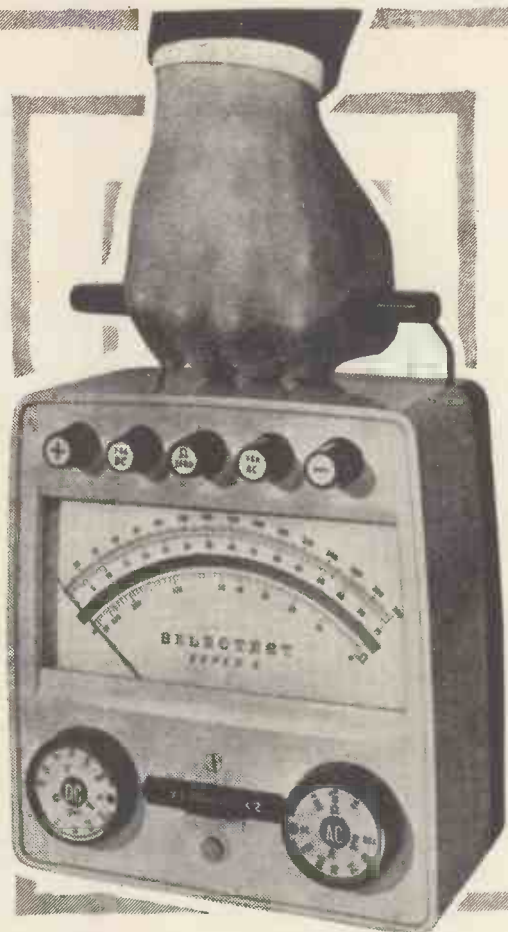
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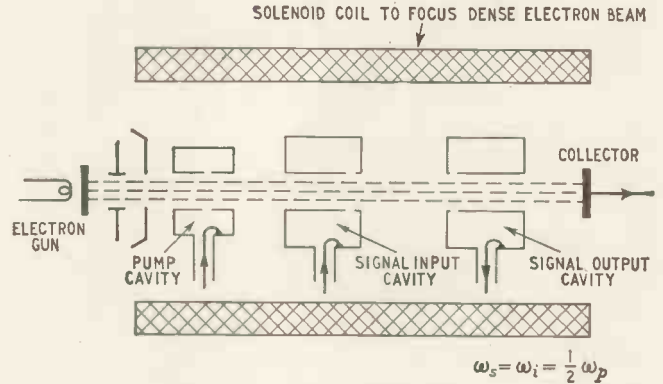
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Masers or Parametric Amplifiers?

Included in the May issue of **ELECTRONIC TECHNOLOGY** is an article which surveys two important recent developments in low-noise microwave amplification—the maser and the parametric amplifier. A discussion of the principles of operation is followed by a brief outline of the various types of amplifier in each of these two groups. The noise arising in these devices is contrasted with that originating outside the amplifier itself, such as may be found in a practical receiver system. In addition, the choice of a low-noise amplifier for a specific application is discussed on the basis of practical considerations as well as the important electrical ones.

ARTICLES IN THE JUNE ISSUE INCLUDE:

TUNNEL DIODES

One of the most promising solid-state devices that has emerged since the advent of transistors in 1948 is the tunnel diode. The author gives in this article details of their principles of operation, characteristics and applications. Also, a number of practical circuits using the tunnel diode are given and they are discussed in detail.

MODERN TRENDS IN MAGNETRON DESIGN

In this article, the author discusses the developments in magnetrons that have taken place since the end of the war. He outlines the reasons for certain designs, gives details of those magnetrons that are currently being used, and considers the future of magnetrons and competitive devices such as the klystron.

ELECTRONIC TECHNOLOGY covers all technical interests in electronics, using this word in its widest possible sense. All the familiar features of ELECTRONIC & RADIO ENGINEER are retained, including, of course, the well-known Abstracts and References section. Regular readership will keep you in constant touch with progress in the entire field.



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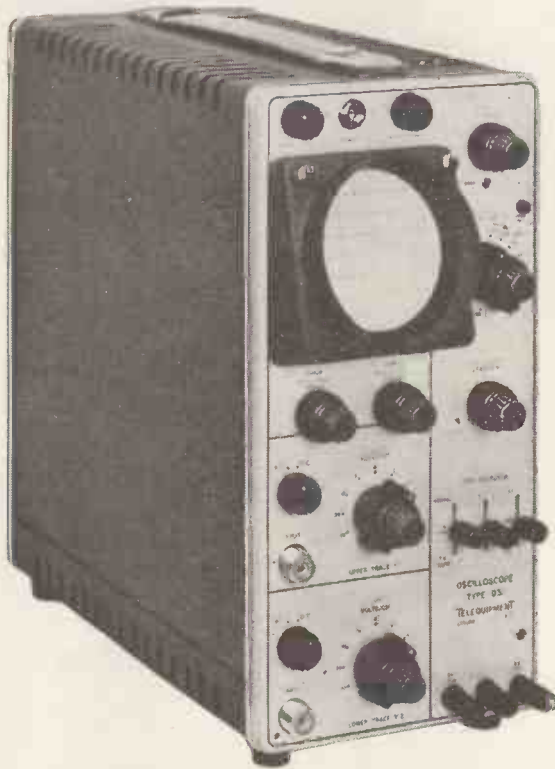
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D 3 1 double beam Serviscope . . . a logical development of the original, highly successful S.31 single beam Serviscope. Though weighing only 26 lbs. in its rugged steel case, the D.31 has capabilities greater than many more elaborate instruments, plus many improved features which make for wider application, more accurate measurements and simpler operation.



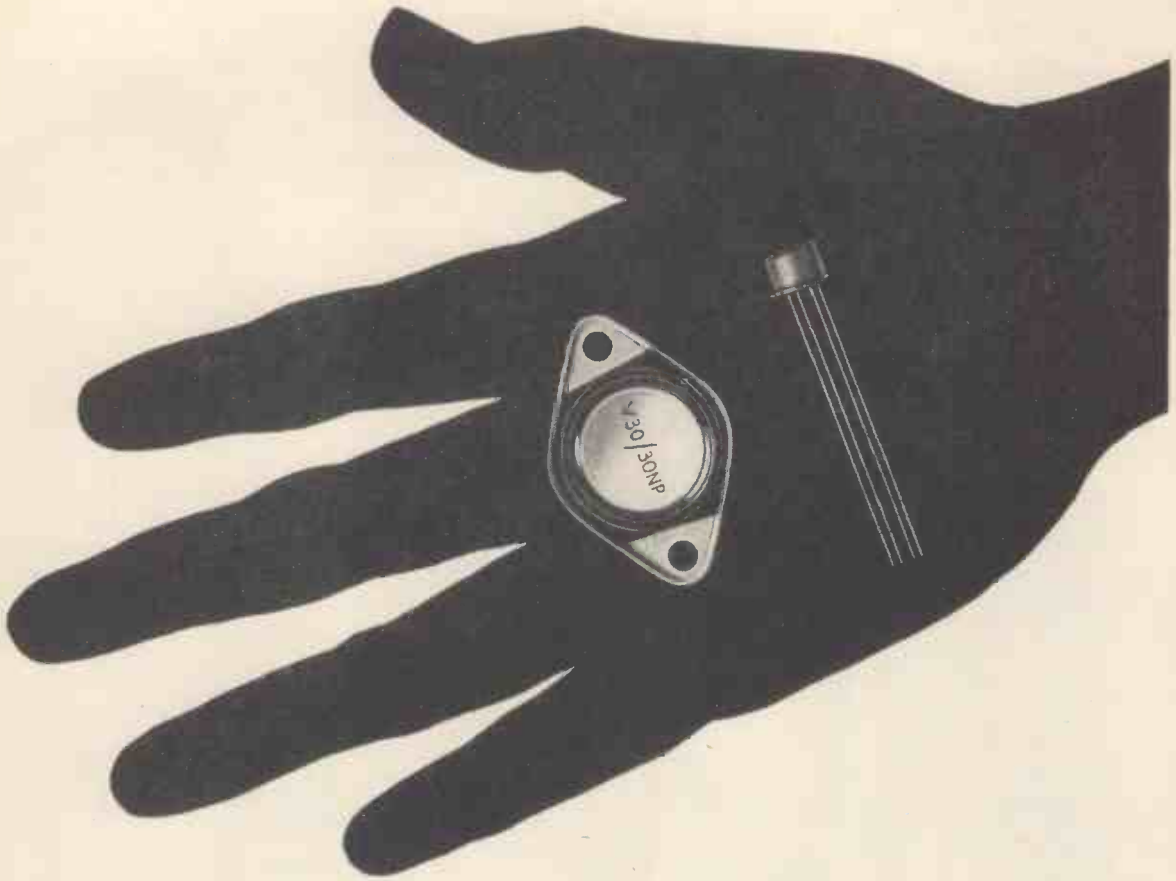
D.C. amplifiers and slow speed time base (down to 5 sec/cm if necessary) are eminently suitable for servo work and similar applications. Fast rise time ($.06 \mu\text{sec}$) and high writing speed (10 cm/ μsec at maximum expansion) are essential for any work dealing with fast pulses or TV waveforms. The unique triggering arrangements enable complex waveforms to be examined in detail with complete accuracy of synchronisation. At this moment D.31 is in use in the diverse fields of computer development and servicing, radar equipment, telemetering applications, closed circuit and broadcast TV, automatic telephone equipment—in fact in any field where a double beam oscilloscope is essential.

The D.31 costs £95

See the D.31 double beam 'Serviscope' on stand 5853 at the IEA Exhibition.

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It is important for stereo microphones that the individual microphones are matched in regard to frequency and direction, and this has been achieved with the MDS 1 with a very wide frequency range (up to 15,000 c.p.s.) so as to satisfy any application. This achievement is particularly remarkable as it has only been possible up to now with very expensive condenser microphones.



Hand Microphone MD 42

For applications as the MD 4 but for frontal speech input. Range 200 to 10,000 c/s; impedance 200 ohms. Normal voice output 2.5 mV. size 1.85in. dia. x 4.72in. Approx. weight 4.75 oz. Press-to-talk-switch optional.



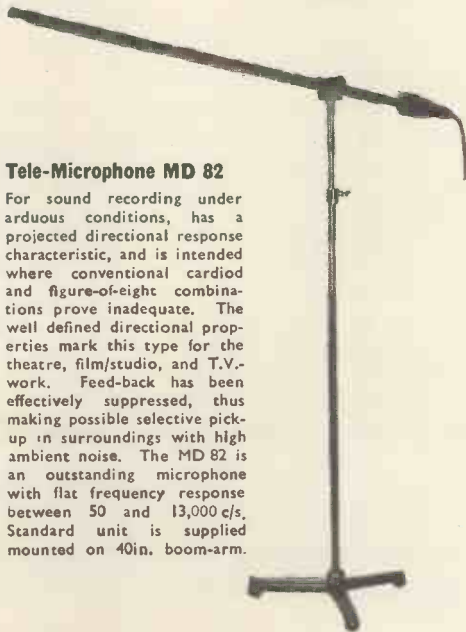
Hand Microphone MD 4

For voice transmissions in environments liable to feedback, the MD4 is invaluable. High effective compensation results in strong attenuation of distant, stray, or reflected sound. Thus MD 4 is equally useful for high ambient noise conditions. Range 50-10,000 c/s. Impedance 200 ohms. Normal voice output 4 mV. The case is 2.36in. dia. x 7.1in. Weight 13.4 oz. MD 4 is also available as high impedance model and with press-to-talk switch.



Tele-Microphone MD 82

For sound recording under arduous conditions, has a projected directional response characteristic, and is intended where conventional cardioid and figure-of-eight combinations prove inadequate. The well defined directional properties mark this type for the theatre, film/studio, and T.V.-work. Feed-back has been effectively suppressed, thus making possible selective pick-up in surroundings with high ambient noise. The MD 82 is an outstanding microphone with flat frequency response between 50 and 13,000 c/s. Standard unit is supplied mounted on 40in. boom-arm.



Floor Stand Microphone MD 31

Extremely slim, has hardly noticeable speech head, and is useful for stage work. This microphone is a new version of the well proven inconspicuously sized MD3-series. Flat response 50 to 10,000 c/s. Delivers approx. 0.1 mV/μbar. Omnidirectional. The plexi-glass sound-disc fits on the speech head; when in position raises treble and slightly modifies directional performance.



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Treble lift imparts extra intelligibility, ideal for paging and dictation. Soft rubber case resists wear and rough treatment. High or low impedance types supplied. Size: 3in. x 2in. x 2in.

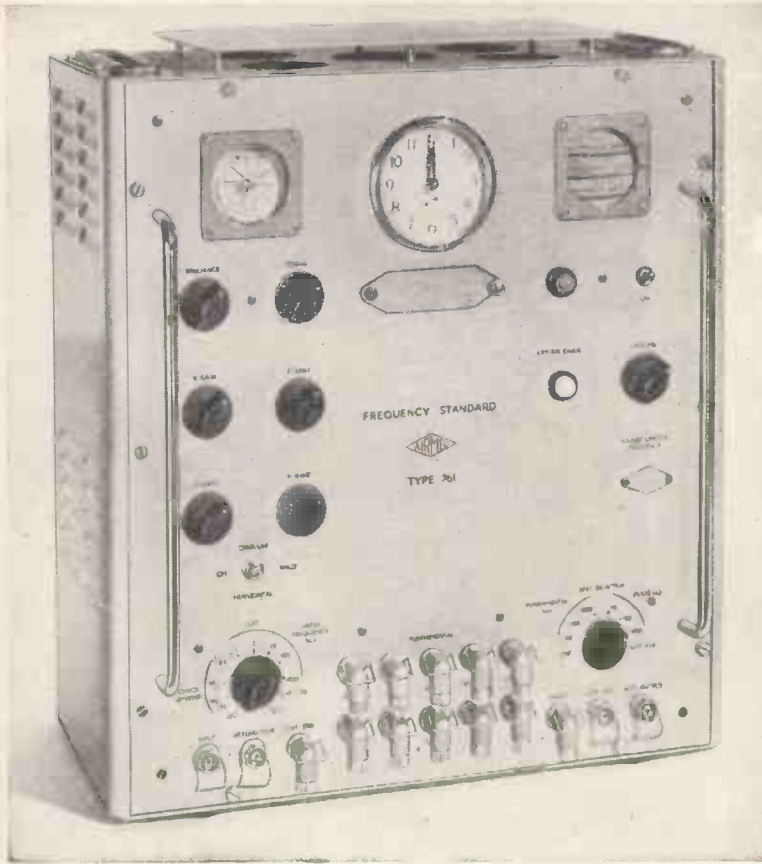


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makes most things . . .
better

AIRMEC LIMITED
HIGH WYCOMBE · BUCKS
Telephone: High Wycombe 2501/7

FUNCTION

Provides an excellent crystal controlled frequency and time standard of small size and moderate cost. The short term frequency stability of better than 1 part in 10^6 obtainable upon installation improves with time and correct treatment up to a working stability approaching 1 part in 10^7 .

OPERATION

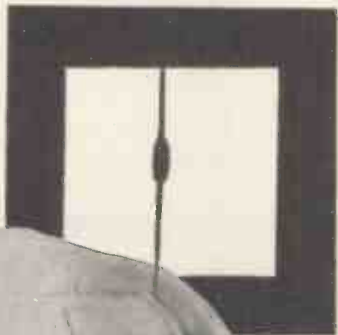
Sinusoidal and pulse signals are produced at five standard frequencies, the pulse waveform being rich in harmonics. The instrument includes both an Oscilloscope and Heterodyning Circuit as independent facilities and is therefore extremely flexible in operation.

FEATURES

- 100 kc/s crystal housed in an oven controlled at 70°C.
- Standard signals provided at 100 c/s, 1 kc/s, 10 kc/s, 100 kc/s, and 1 Mc/s.
- Identification of an unknown signal by Lissajous figure or beam modulated circular trace.
- Beat output available from a plug on the front panel.
- Suitable for rack mounting.

IMMEDIATE DELIVERY

one of the world's smallest



Actual Size

SILICON
DIODES
MULLARD
OA202

Generously rated
Wide temperature range
High back resistance
Ideal for automatic wiring
Rugged construction
ECONOMICALLY PRICED

Despite its extremely small size, the Mullard Silicon Junction Diode OA202 will handle peak currents of up to 250 mA at 25°C. Apart from other favourable electrical and mechanical characteristics, the OA202 is distinguished by its cost which is kept at the lowest possible level by very large scale production. This all-glass diode is hermetically sealed and really is a rugged device. It is made in exactly the same way as the Government Type Approved CV7040, whose rigorous specification includes temperature cycling, climatic cycling, fatigue and shock tests, 1000 hour life tests and high temperature storage.

Brief electrical data is given below. For further information please contact Mullard House.

ABRIDGED DATA (AT 25°C UNLESS OTHERWISE STATED)

Max. peak inverse voltage.....	150 V
Max. peak forward current.....	250 mA
Max. d.c. forward current.....	160 mA
*Average forward current (sinusoidal input with resistive load).....	80 mA
Typical forward voltage drop at 30 mA.....	0.9 V
Inverse current at -150 volts:	
Maximum at 25°C.....	0.1 μA
Maximum at 125°C.....	10 μA
Ambient temperature range.....	-55 to +125°C

*Max. averaging time 50 milliseconds.

(An alternative type, OA200, is available for lower voltage applications.)

See Mullard Semiconductor Devices
on Stand M559 at the
**INSTRUMENTS, ELECTRONICS
AND AUTOMATION EXHIBITION**

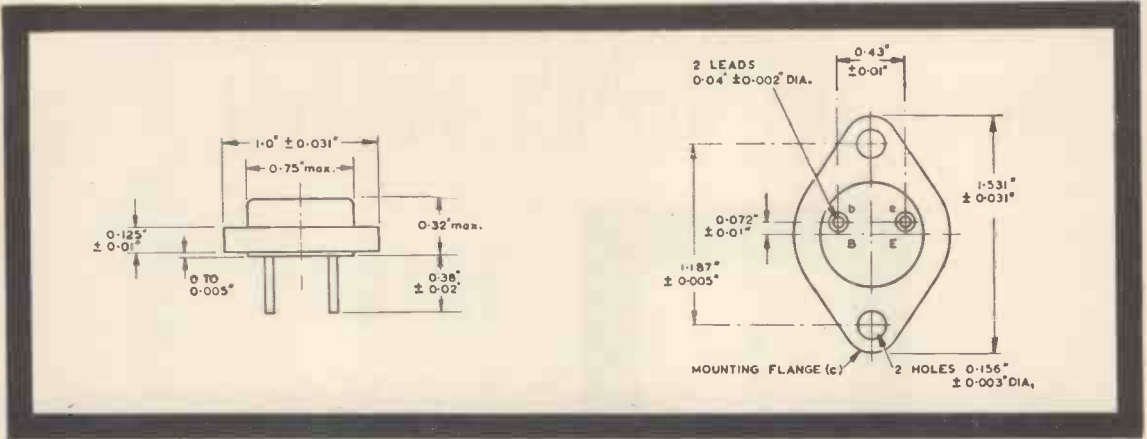


MULLARD LIMITED · SEMICONDUCTOR DIVISION
MULLARD HOUSE · TORRINGTON PLACE · LONDON · WC1
TELEPHONE : LANGHAM 6633

Mullard

industrial
semiconductors





POWER TRANSISTORS TYPES XC155 and XC156

These germanium p-n-p alloy transistors are intended for power switching, voltage regulator, convertor and other heavy duty industrial applications. Full particulars of these and other Ediswan Mazda semiconductor devices will be sent gladly on request. If you wish to keep up to date with the latest developments in this field, please ask us to add your name to our semiconductor mailing list.

Maximum Ratings (Absolute Values)	XC155	XC156	
Peak collector to base voltage (volts).....	-80	-100	
Peak collector to emitter voltage, base open circuit (volts).....	-50	-65	
Peak collector to emitter voltage, base and emitter joined or with an external base/emitter circuit resistance less than 40 ohms (volts)	-65	-80	
Peak emitter to base voltage (volts).....	-60	-60	
Peak collector current (amps).....	-10	-10	
D.C. Collector current (amps).....	-5	-5	
Collector dissipation (mounting flange temperature 85°C) (watts)....	10	10	
Switching Characteristics (Common Emitter) (Typical production spreads)			
D.C. Current gain ($V_{ce} = -1.5V, I_c = -4A$).....	minimum	20	20
	average	26	26
	maximum	50	50
D.C. Collector to emitter saturation voltage ($I_c = -4A, d.c. I_b = -400\text{ mA}$) (volts).....	average	-0.4	-0.4
	maximum	-0.8	-0.8

EDISWAN SEMICONDUCTORS
MAZDA

Associated Electrical Industries Ltd

Radio and Electronic Components Division

PD 15, 155 Charing Cross Road, London, W.C.2

Tel: GERrard 8660 Telegrams: Sieswan Westcent London

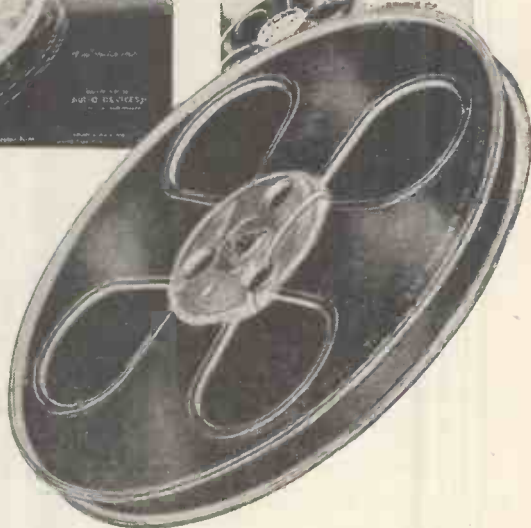
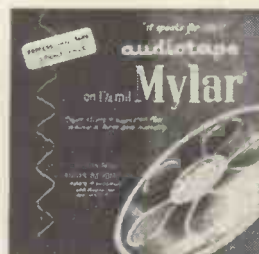
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Sensational Success of **audiotape**

TRADE MARK

Tape Recording experts and enthusiasts all over the country are changing to AUDIO-TAPE for its flawless perfection of sound reproduction over the entire audio range and its **consistent, uniform quality** from reel to reel

Available on all standard reel sizes, there are eight different types to meet every recording requirement . . . **AUDIOTAPE**, manufactured in the U.S.A. by Audio Devices Inc., gives you the truest sound your recording equipment can produce—try **AUDIO-TAPE** . . . it speaks for itself.



sensational C-SLOT REEL!

All 5in. and 7in. reels of **AUDIOTAPE** are supplied on the exclusive C-slot Reel—the fastest-threading tape reel ever developed. The tape end, dropped into a slot in the hub anchors itself automatically at the first turn of the reel.

ELPICO A NAME FOR BETTER PERFORMANCE

Concessionaires to the United Kingdom.

LEE PRODUCTS (G.B.) LIMITED, "Elpico House," Longford Street, London, N.W.1

Telephone: EUSton 5754 (all lines). Telegrams: Leprod, London.



- ONE DOWNLEAD.
- ROTATABLE 360 deg.
- TILTABLE 300 deg.
- HORIZONTAL OR VERTICAL AT WILL.
- FULLY ASSEMBLED COMPLETE WITH MAST.
- ELEMENTS "CLICK" INTO POSITION
- NO "COMBINER" REQUIRED.
- RESONATES ON BOTH BANDS.
- OVERALL HEIGHT LESS THAN 5FT.

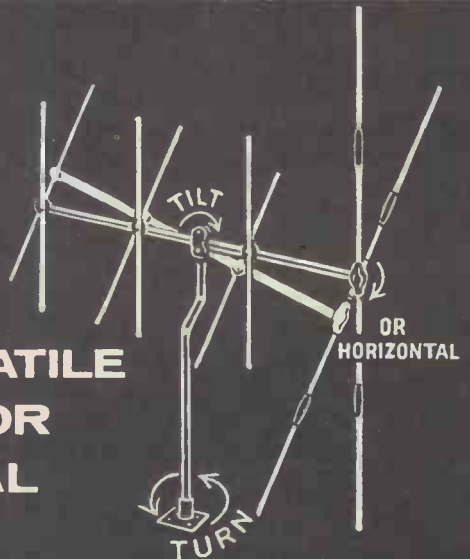
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TRADE MARK



**THE
MOST
VERSATILE
INDOOR
AERIAL
YET
PRODUCED**



- THE CONSTRUCTION ALLOWS THE ARRAY TO BE ACCURATELY POSITIONED FOR MAXIMUM RECEPTION.
- OFTEN WORTH 2 or MORE EXTRA PARASITIC ELEMENTS.
- HIGH GAIN ON BAND III.
- BAND I EQUAL TO ORDINARY LOFT.

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Quadrant Works, Wortley Road, Croydon, Surrey
Telephone: Thornton Heath 1191/2/3

Depots at : Newcastle-on-Tyne · Doncaster · Sheffield
Birmingham · Southampton

2-3 kW channelised transmitter

The versatility and reliability of this new, tropicalised Mullard transmitter make it eminently suitable for h.f. en-route, ground-to-air services and point-to-point communication networks.

The GFT.560/2 is of unit construction and consists of three basic cabinets — r.f. unit, modulator unit and power supply units — which can be used in combination for multi-frequency working and a number of types of emission.

There are ancillary units available that permit remote control of the transmitter over telephone circuits.

Frequency Range 1.5 to 30 Mc/s.
Frequency Stability to Atlantic City 1947 standards.

Power Output 3kW. c.w., 2kW m.c.w. or r/t.

Types of Emission c.w., m.c.w., telephony, frequency shift (with external keying unit), A1, A2, A3, F1.

Output Impedance 600 ohms balanced.

Power Supply 400V, 50-60c/s 3-phase.



A PRODUCT OF
MULLARD EQUIPMENT LIMITED
A COMPANY OF THE MULLARD GROUP

MULLARD LIMITED
Mullard House, Torrington Place,
London · W.C.1



from AIRPORTS

to ZYMURGISTS

Multitone leads in pocket staff location



By far the largest number of hospital and industrial installations of the pocket receiver type in this country, and overseas, are Multitone. Our selective induction system "Personal Call" is saving time, money and worry in well over 100 different types of industrial concerns from airports to zymurgists. (We are looking for a Quill Manufacturer to complete the alphabet.)

The New MULTI-CHANNEL equipment provides over 400 individual channels using the new flat receiver (as illustrated)

THE MULTITONE

personal call

system of staff location

Additional Facilities

ELECTRONIC TRUNCHEON

The Electronic Truncheon is no bigger than standard equipment carried by guards and serves the same purpose, but inside there is a transmitter which, when the button is pressed, sends out a signal. This is picked up by the loop of wire around the area to be protected. The pulse is used to operate a small receiver, which automatically switches on any form of electrical alarm. It can be operated from any point in the area.

INTERNAL TRANSPORT COMMUNICATION

The Multitone "Personal Call" loudspeaker-receiver has been designed to solve the problem of conveying verbal instructions to transport vehicles used for handling loads inside a given area. Messages can be conveyed to all or selected vehicles from the central transmitter.

MULTITONE INDUCTION SYSTEMS CAN SOLVE YOUR STAFF LOCATION PROBLEMS:

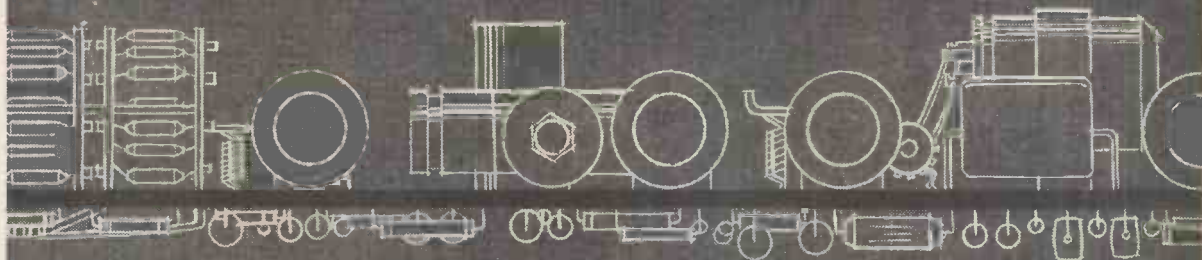
- ★ Equally suitable for large and small areas or concerns
- ★ Low rental terms
- ★ Virtually no internal wiring

(the 'peep-peep' in the pocket), the only staff location system worth installing

Write or 'phone for further particulars. We can be found in 10 seconds.

MULTITONE ELECTRIC COMPANY LTD., 12/20 Underwood St., LONDON, N.1. (CLERkenwell 8022)

Speed is the need in Printed Circuits



BRIBOND *print circuits faster*



The Printed Circuit is rapidly becoming established assembly practice in every field of electro-mechanics. Meeting this increasing demand takes specialist production such as only Bribond offers. Bribond manufacture circuits complete from design to finished board, and every stage is organised on modern line production methods providing outputs of any quantity. And each individual circuit is subjected to three critical inspections. This is increased when the copper is plated with either rhodium, silver, or gold.

BRIBOND *make prototypes quicker*



The prototype department is at the service of all Bribond customers. It can produce within 48 hours or less, the initial circuit from which future production can be planned. All that is needed is a clean circuit image from which reproduction can be made. Where desired, and time permits, the whole of this work can be carried out in our drawing office. Bribond recognise that quick prototypes—whether for complete units or small sub-assemblies—are essential in these highly competitive days when anything that shortens the time-lag between drawing board and production can mean a big reduction in marketing costs.

BRIBOND *maintain prompt deliveries*

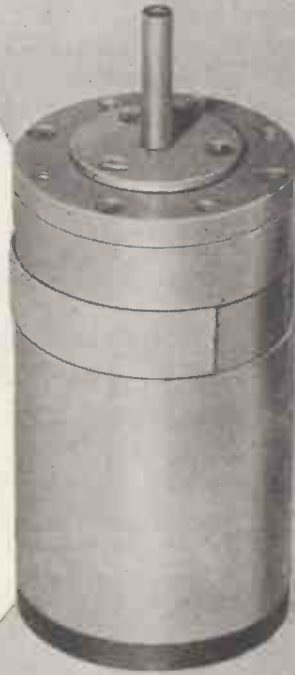
Bribond have organised production to guarantee prompt delivery of customer's requirements. Consultation and planning of any form of printed circuit—double sided, component notated, flexible, flush surfaced, plated, etc.—is freely offered and your enquiry is invited.



Write for full details
and samples to

BRIBOND LIMITED
Burgess Hill, Sussex
Telephone: Burgess Hill 85611

A NEW EMI HIGH TORQUE BATTERY MOTOR



*Illustration
actual size*

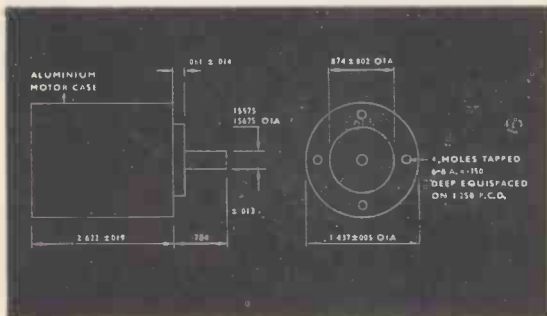
Provisional Technical Specification

Voltage Range: 8v to 12v D.C.
Current: No load 120mA max. 8-12v
 At 45 gcms 310mA max. 8-12v
Rotation: Anticlockwise viewed from spindle end.
Speed and Output: Max. continuous rating,
 2440-2500 r.p.m. at 45 gm. cms. torque at 12v DC +0v
 2390 r.p.m. minimum at 45 gm. cms. torque at 8v DC -0v
 Speed regulation over governed range at constant voltage 0.75 r.p.m. per gm. cm. torque.
 Speed regulation over governed range at constant torque 12.5 r.p.m. per volt D.C. Max.
 No load ungoverned 12v
 No load governed 8v
 Minimum torque at governed speed 15 gm. cm. at 12 v DC.

For Professional and Scientific Applications

Designed primarily for Professional Tape Recorders this new EMI Battery Motor (part no. 98170D) is also suitable for Television camera remote control, and for medical and other scientific uses. A high-grade precision-built Motor for long life and exceptional speed regulation over a wide range of load and voltage. A Multi-pole Armature gives low electrical interference, long brush life and high efficiency and a Ball Race bearing is incorporated for handling heavy duty side loads.

EMI also manufacture a wide range of inexpensive battery motors suitable for Domestic Tape Recorders, Gramophones, Fans and a host of other applications where a governed torque of up to 10 gm. cm. at 1600 r.p.m. or 2600 r.p.m. is required.



THE GRAMOPHONE COMPANY LIMITED
 (Components Division)

Hayes · Middlesex · England
SOUTHALL 2468 · EXT. 635

6cld1 (One of the EMI Group of Companies)

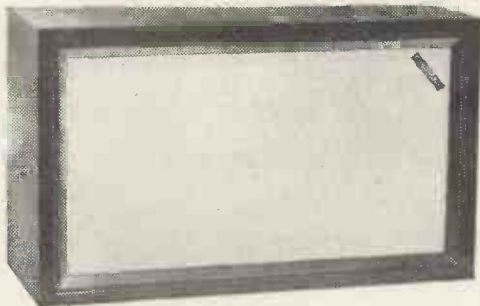
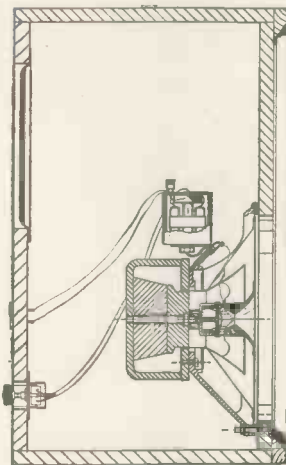
GOODMANS

**PIONEERS OF
COMPACT
LOUDSPEAKER
SYSTEMS**

There was once a time when Full Range High Fidelity reproduction from a Loudspeaker housed in a *small* enclosure was considered impracticable—the text books said so and this appeared to be confirmed by experimental work.

The first real break-through came before the war—from GOODMANS—with the introduction of a high compliance twin-cone unit mounted in a totally enclosed 18" cube. After the war, development was taken up again and complete Loudspeaker Systems were developed for use specifically in very small enclosure volumes. Again GOODMANS led the market. Then the research and development effort was directed to overcome the remaining disadvantages; complexity, low efficiency, high cost. The result was Model A.L/120—incorporating all the valuable experience gained over many years as well as the latest developments in enclosure loading, diaphragm design, high frequency radiation, magnet design, to say nothing of advanced methods of precision manufacture.

This achievement is best judged and appreciated by ear; the actual description of the A.L/120 is as follows:—
Frequency range 35 c/s to 20,000 c/s with a maximum power handling capacity of 15 Watts. Overall enclosure size—24" x 11½" x 14¼". Enclosure loading—Acoustical Resistance. (GOODMANS Patent No. 790997 [British]). Drive unit: 12" Triaxial unit comprising *three concentrically mounted radiating elements*, each designed to specialise in low distortion reproduction of one part of the overall scale; bass, middle, treble; and integrated on to a common axis to approach the ideal of the "point source" radiator with its freedom from phase interference between the separate units. Bass radiation is from a large diaphragm with plastic treated high compliance suspension, with mechanical crossover to a moulded high stability mid-range radiator; and finally electrical crossover (twin ½-section L.C. network 12 db/octave) to a high precision horn loaded high frequency pressure unit, with separate L-pad balance control.



Model A.L/100 also follows these lines in most respects, except that it employs a two element drive unit and provides smooth coverage from 35 c/s to 15,000 c/s., with a power handling capacity of 12 Watts.

THESE LOUDSPEAKER SYSTEMS ARE DESIGNED AND BUILT WITH GREAT CARE TO BRING TRUE HIGH FIDELITY INTO YOUR HOME—COMPACTLY, ELEGANTLY, EXCITINGLY. WRITE NOW FOR ILLUSTRATED BROCHURE.

A.L/120... Price £29. 10. 0

as illustrated

A.L/100... Price £23. 10. 0

Both models available in walnut or mahogany finish.

GOODMANS INDUSTRIES LIMITED, Axiom Works Wembley, Middx.

Tel. : WEMbley 1200 (8 lines) Grams : Goodaxiom, Wembley, England.

In every sense the greatest range—in every country the greatest name.

Hermetic Sealing

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NICKEL METALLISING**

Quality Approved (Joint Service R.C.S.C.)

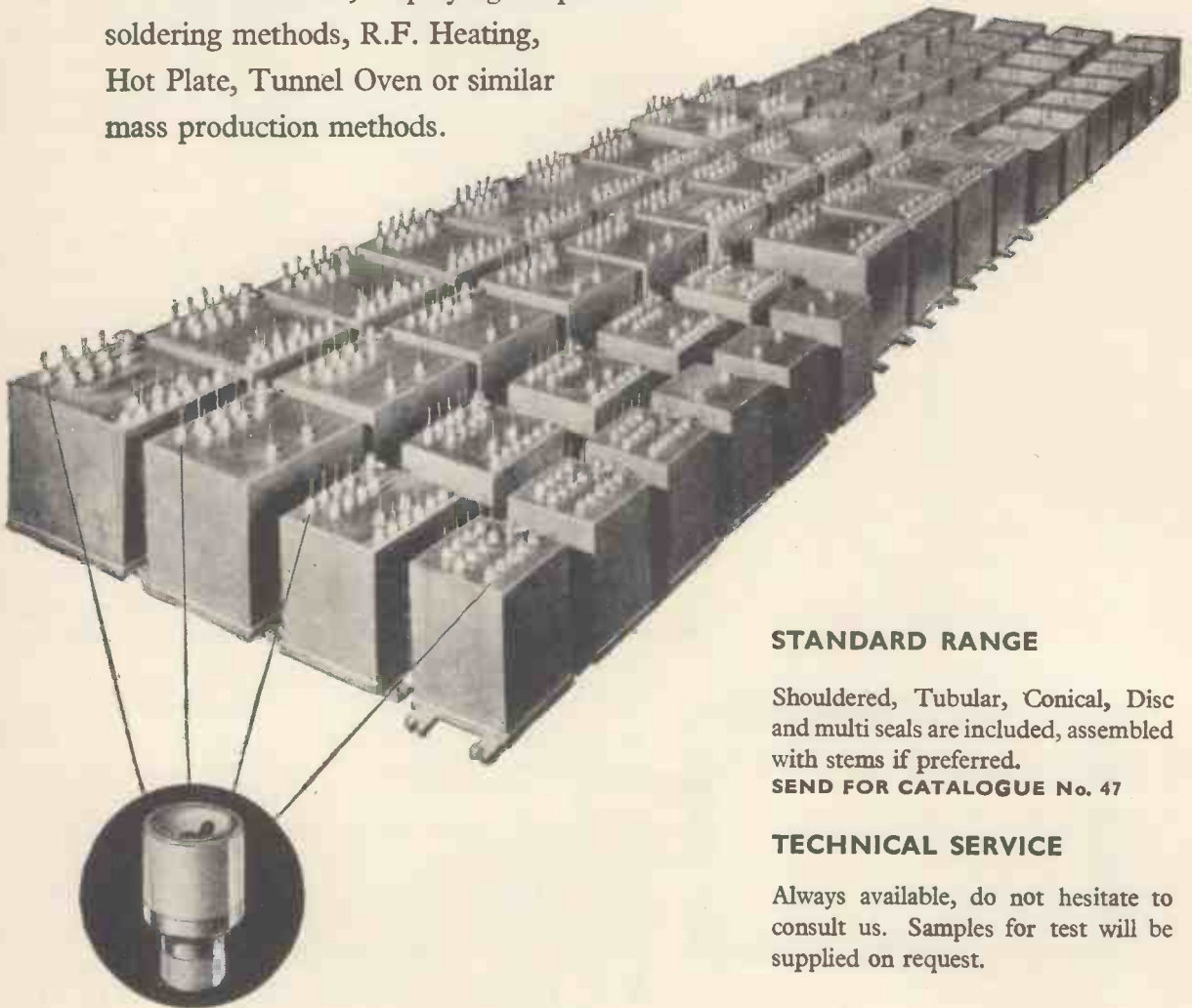
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**METALLISED
BUSHES**

Perfect Terminations

—made readily without special precautions by semi-skilled labour, employing simple hand soldering methods, R.F. Heating, Hot Plate, Tunnel Oven or similar mass production methods.



STANDARD RANGE

Shouldered, Tubular, Conical, Disc and multi seals are included, assembled with stems if preferred.

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TECHNICAL SERVICE

Always available, do not hesitate to consult us. Samples for test will be supplied on request.

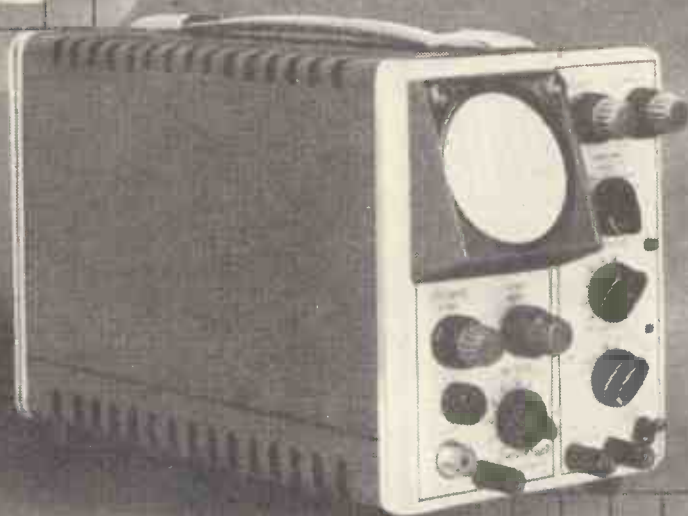
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Telephone: Stourport 2271

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FOR MEASUREMENT OF TIME AND VOLTAGE



THE S31

The type S31 Oscilloscope is an improved version of the now famous Serviscope.

It is extremely compact (8½ in. x 6½ in. x 13 in.) and has a performance and specification unequalled by many much larger instruments.

The D.C. coupled amplifier (-3db at 6 Mc/s), voltage calibration, wide-range calibrated time base (5 sec. to 1µ sec. per cm.) and a precision flat-faced C.R. Tube are only a few of the features that put the S31 far ahead of any other portable scope.

TELEQUIPMENT LTD

313 Chisle Road · Brompton · London N.14 Tel: Fox Lane 1165

VISIT US ON STAND S853 AT THE I.E.A. EXHIBITION.

THE PRICE OF THE S31 IS £75.



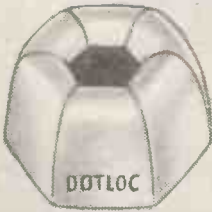
**regular
type**

Used alone as a load-carrying nut on light duty assemblies, or used on top of ordinary nuts on high stress assemblies



**acorn
type**

Smooth dome shape covers up unsightly rough bolt ends for attractiveness and protection against scratching



**adjusting
type**

Used as a lock nut when seated, or as an adjusting nut or stop nut anywhere on threads



**wing
type**

Combines locking principle of Dotlocs with ease of finger tightening and removal



**tension
nuts**

Holds adjusting screws to desired setting. For ease of assembly and simple adjustments



**washer
type**

Incorporates grounding base and seal against water and dust

Improve production with **DOTLOC** **REDUCE** parts operations and **COSTS!**

DOTLOCS are single-thread precision-made locking nuts made of spring-tempered steel. A single DOTLOC replaces two, three or even four fastening parts.

The economy of handling one DOTLOC instead of many fasteners, simplifies not only assembly, but the whole ordering, stocking and accounting procedure.

DESIGN & LOCKING PRINCIPLE

The thread engaging portion is formed in true relation to the pitch of the screw thread. The inner contour is designed to provide maximum strength from a single-thread nut.

Perfect hexagon shape, straight sides, ample height for easy, speedy handling and wrenching.

Save weight. DOTLOCS save more than 65% of the weight of plain nuts, 80% of nut and lockwasher, 85% of nut, lockwasher and plain washer.

Save space. DOTLOCS require less space than many other fastenings. This is especially true where lockwashers and flat washers are eliminated.

Interchangeable. DOTLOCS are interchangeable with other commonly used locking devices and generally require no change in design.

Withstand high temperatures. Spring steel DOTLOCS are not affected by temperatures up to 400°F.

Quick assembly. Either the DOTLOC or the screw can be driven in the assembly procedure, whichever is more convenient.

Locking action. Safer for assembling fragile or brittle parts and materials. Resilient DOTLOC thread form permits firm but spring-cushioned pressure on assembled parts.

CARR FASTENER COMPANY LIMITED
Stapleford, Nottingham. Phone: Sandiacre 3085

LONDON:
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quick secure fastening at LOW COST with

DOTLOC

A new Grommet development

THE DOUBLE SEALING EMPIRE RUBBER GROMMET

infinitely accommodating in use:
considerably reduces range of sizes
because the same grommet can be used with
several plate thicknesses or cable sizes



PAT. APP. No. 5255/59

This newly developed self-conforming grommet, because it is immediately self-locking against the elements, is the solution to many of an engineer's sealing problems.

Any one size will not only accommodate itself to a variety of mounting plate thicknesses, but (designed for cable or control rod) will take these in a variety

of sizes and be weather-, water- and dust-proof at a variety of angles to the cable or rod.

Because of its capacity to conform to many varying requirements, it enables a workshop stock range of grommets to be reduced to perhaps one tenth of that at present maintained.

THE NEW BLIND GROMMET



FREE

Note how when sprung into position the grommet provides a perfect double seal by its own permanent pressures. The angled groove also creates a tight pressure hold on the metal plate.

THE NEW DESIGNED GROMMET



FREE



FITTED

In the cable grommet variety the same double pressure seal is created, allied to tight seal on various diameters of cable. This new grommet gives sound sealing at all vital points.



A useful feature of this cable grommet is that by reason of the designed taper of the cable entry and the flexibility of the web, a considerable angle of cable entry and a variety of cable size are possible. This avoids necessity for special grommets with angled bores.



In the conventional grommet, only one thickness of plate and only one size of cable can be accommodated. No effective seal is afforded by the parallel groove.

Now being produced in a range of sizes
THESE GROMMETS WILL SOLVE
YOUR SEALING PROBLEMS



ENQUIRE
for catalogue section
and detailed particulars.

INTERCHANGEABILITY

of the 5 different sized bits with the 1 Precision iron, creates the most versatile soldering tool yet produced. Bit sizes of .040in., 3/32in., 5/32in., 3/16in. and 3/16in. heavy duty complete the range.

FINGERTIP CONTROL, sharp, regulated heat, ensures a quicker better job. Model C.240 (230/240 volts) illustrated, is available from the usual wholesalers or direct from the manufacturers at 29/6 (complete with one bit). Other models for voltages ranging from 6 to 230 volts also available.

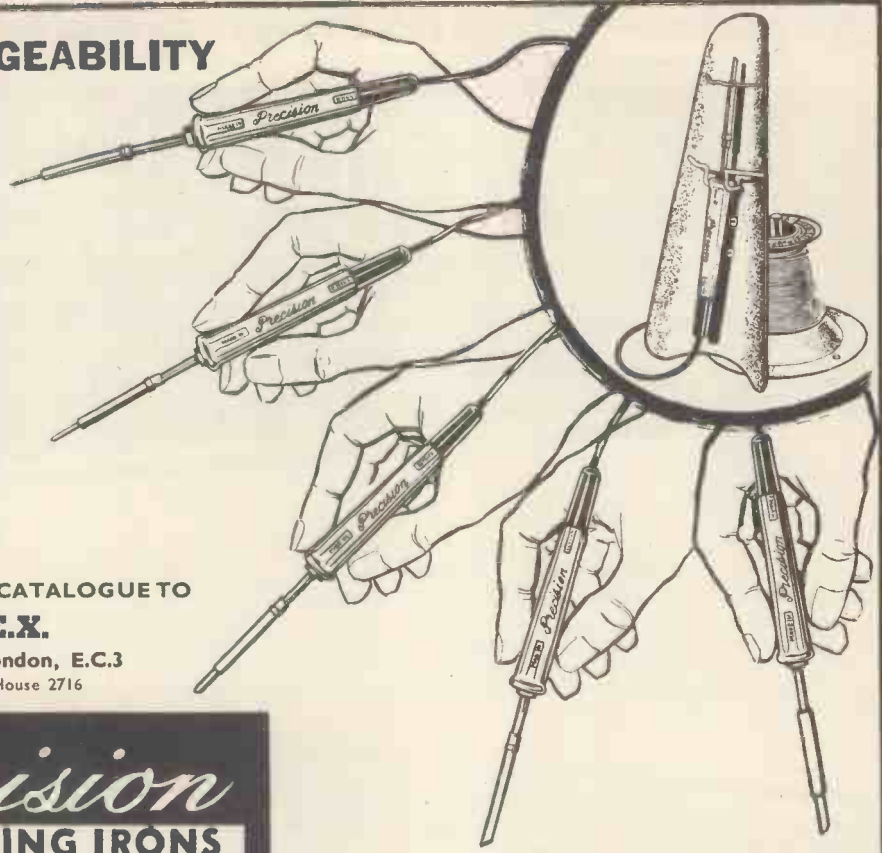
Stands as illustrated at 12/6.
(ALL PRICES SUBJECT)

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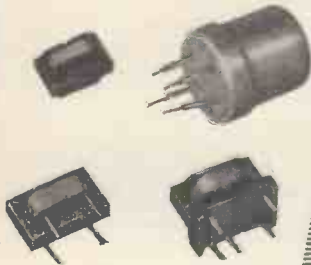
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Phone: Mansion House 2716



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SOLDERING IRONS

TRANSFORMERS



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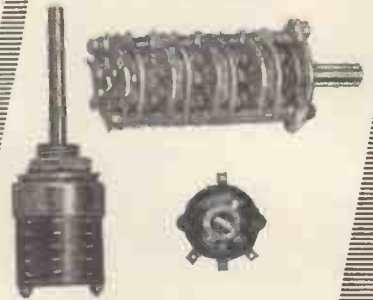
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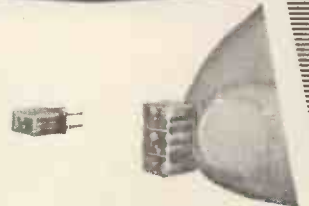
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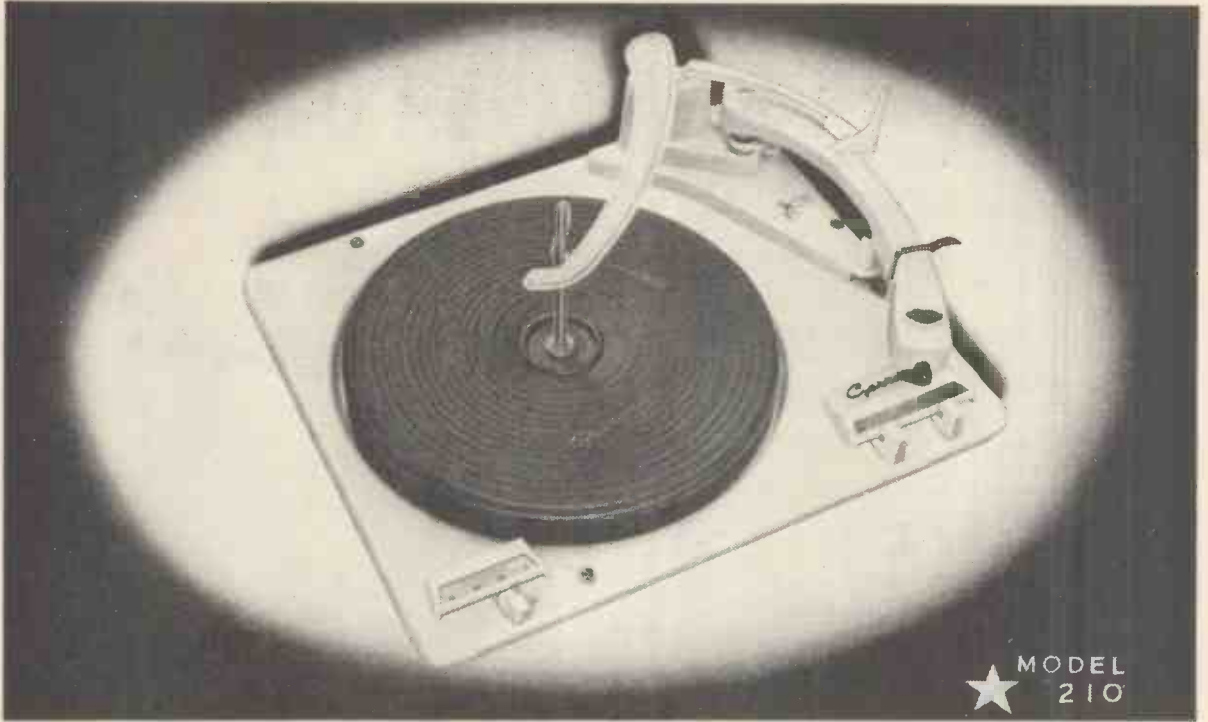
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ARDENTE ACOUSTIC LABORATORIES LTD

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Phone: ELGAR 3923 (6 lines) Telegrams: HAILER LONDON



fit **Garrard** for Good....



MODEL 4 HF

A high quality single Record Player elegantly styled and carefully designed to provide maximum reliability with fidelity of reproduction. Fitted with TPA 12 Pick-Up Arm which allows records up to 16in. to be played.

And now the latest unit to bear the Garrard name—**Model 210 Record Player and Automatic Record Changer.** Elegantly styled to match in with modern equipment design. Produced with the same engineering skill that characterises everything in the Garrard range.



MODEL 210

Plays any number of records up to eight, either 7in., 10in. or 12in. at 16 2/3, 33 1/3, 45 and 78 r.p.m. 10in. and 12in. of the same speed can be mixed in any order. May also be played manually.



MODEL TA Mk. II

A single Record Player particularly suitable for the home constructor. It is mounted on a rectangular unit plate. Voltage range 100/130 and 200/250 A.C. only. A model for battery operation is also available.



MODEL TPA 12

Transcription Pick-Up Arm designed for monaural and stereophonic record reproduction. It is an instrument of the highest quality with its modern styling finished in Ivory, Chrome and Red. Fitted with M.P.M.4 Plug-in moulding which accepts most cartridges, it is the companion to the Model 301 Transcription Motor.



.... and always



GARRARD ENGINEERING & MANUFACTURING CO. LTD.

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Telephone: SWINDON 5381 (5 lines)

TELEX 44-271



*Reduce
with the*

your press tool costs

HUNTON

UNIVERSAL BOLSTER OUTFIT

In addition to the range of Punches and Dies $\frac{1}{8}$ in. to $3\frac{1}{2}$ in. dia. available from stock, some of the tools usually required in the Radio and Electronic Industries have been standardised for use with the Hunton Universal Bolster Outfit. Illustrated here are a few which can be supplied quickly or from stock.

In London and Home Counties, ask for a practical demonstration in your own works.

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Telegrams:
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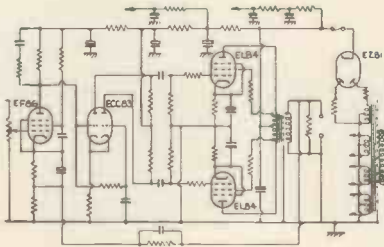
Catalogue giving full technical details, response curves and oscillograms of the above models, available on request.

Telephone: Idle 1235/6

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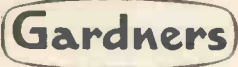
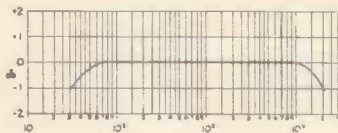


designed for



The Solent Series Audio Output transformer (type AS 7012 illustrated above — price 49/3) has been designed by Gardners specially for the Mullard 5-valve, 10-watt High Quality Amplifier. It has a grain-oriented laminated core, a primary inductance of 120H with a leakage reactance of 14mH, and is one of 22 Audio Output transformers detailed in the new catalogue of the Solent series.

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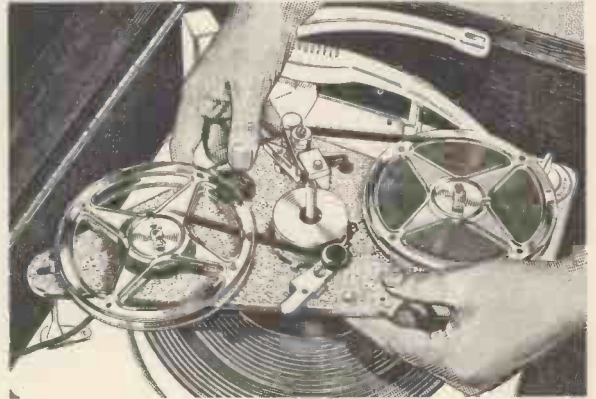


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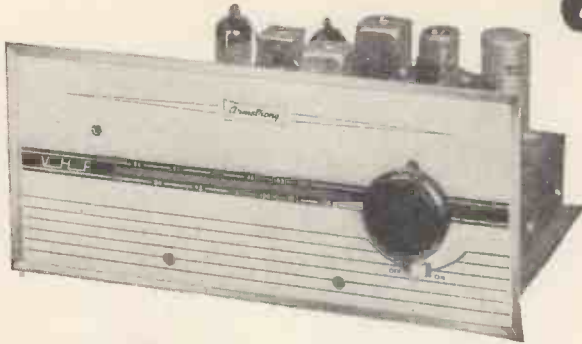
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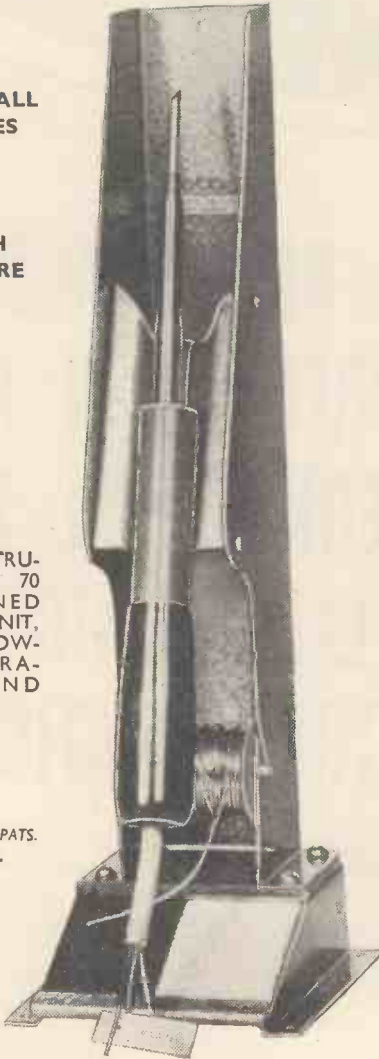
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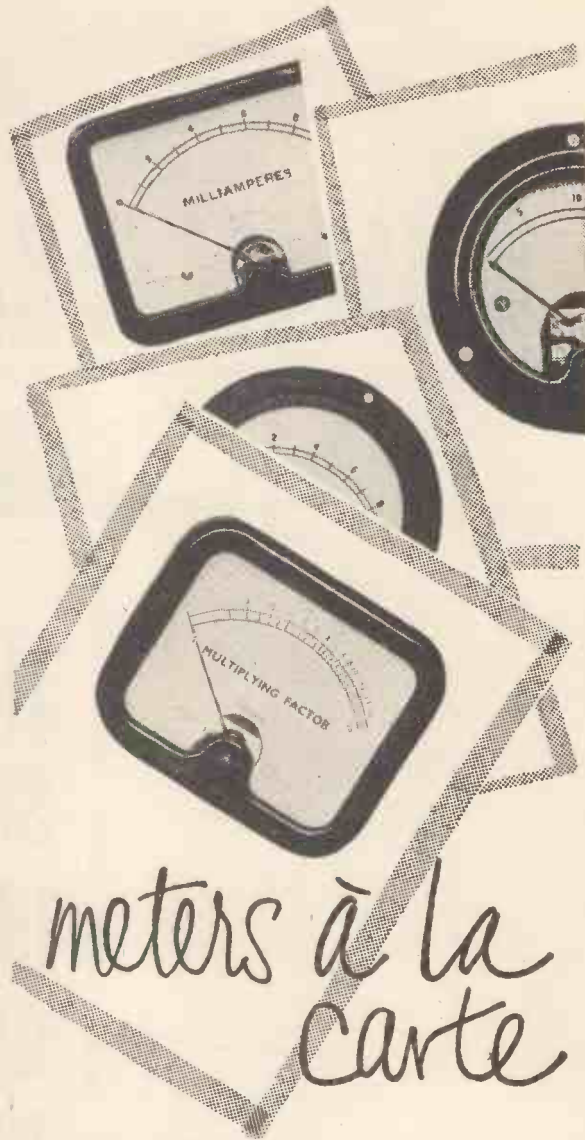


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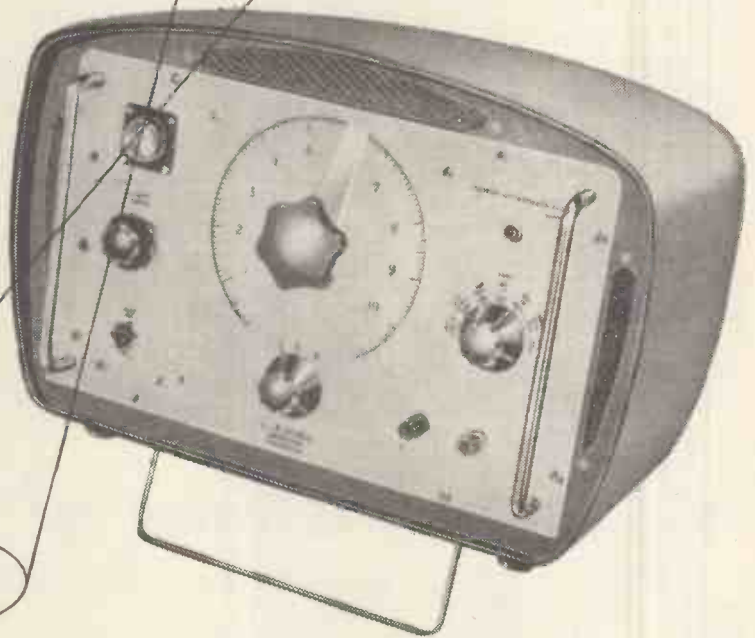
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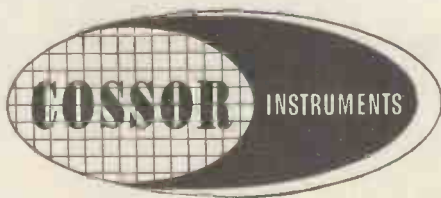
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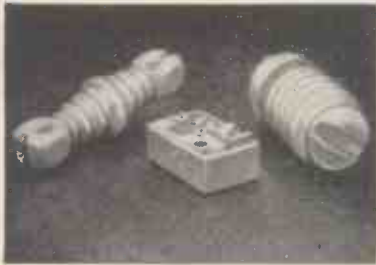
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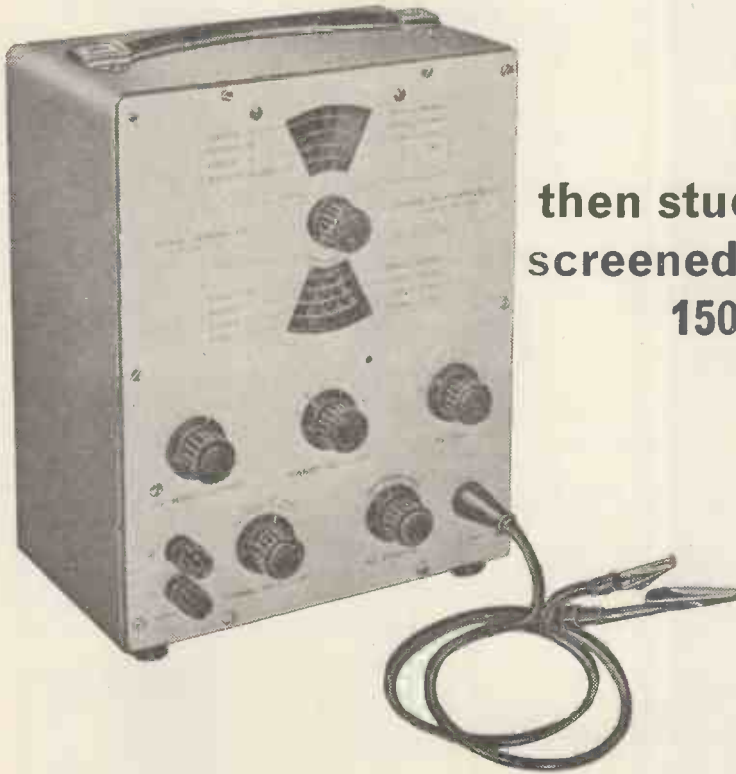
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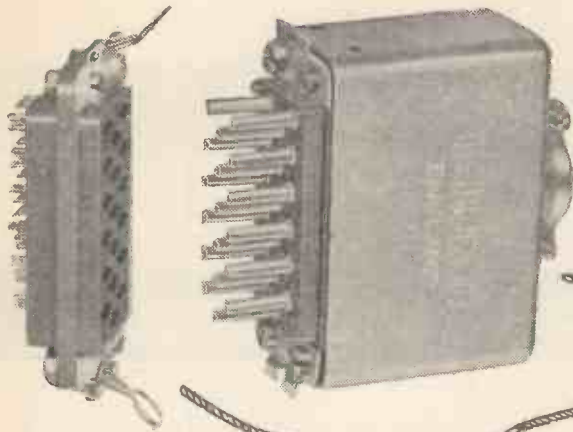
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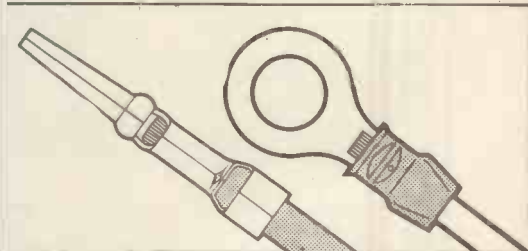
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Published on the 15th December, 1959, 7,000 copies had been sold and dispatched by the end of February, 1960.

Here are a few reactions

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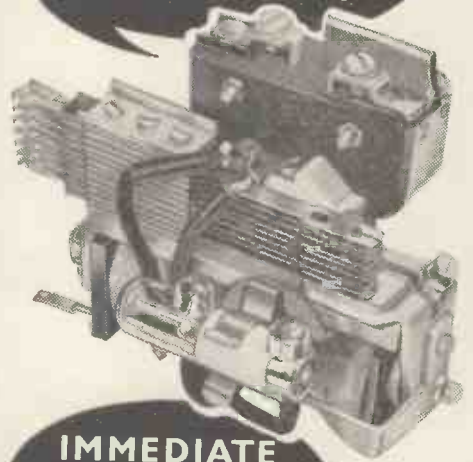
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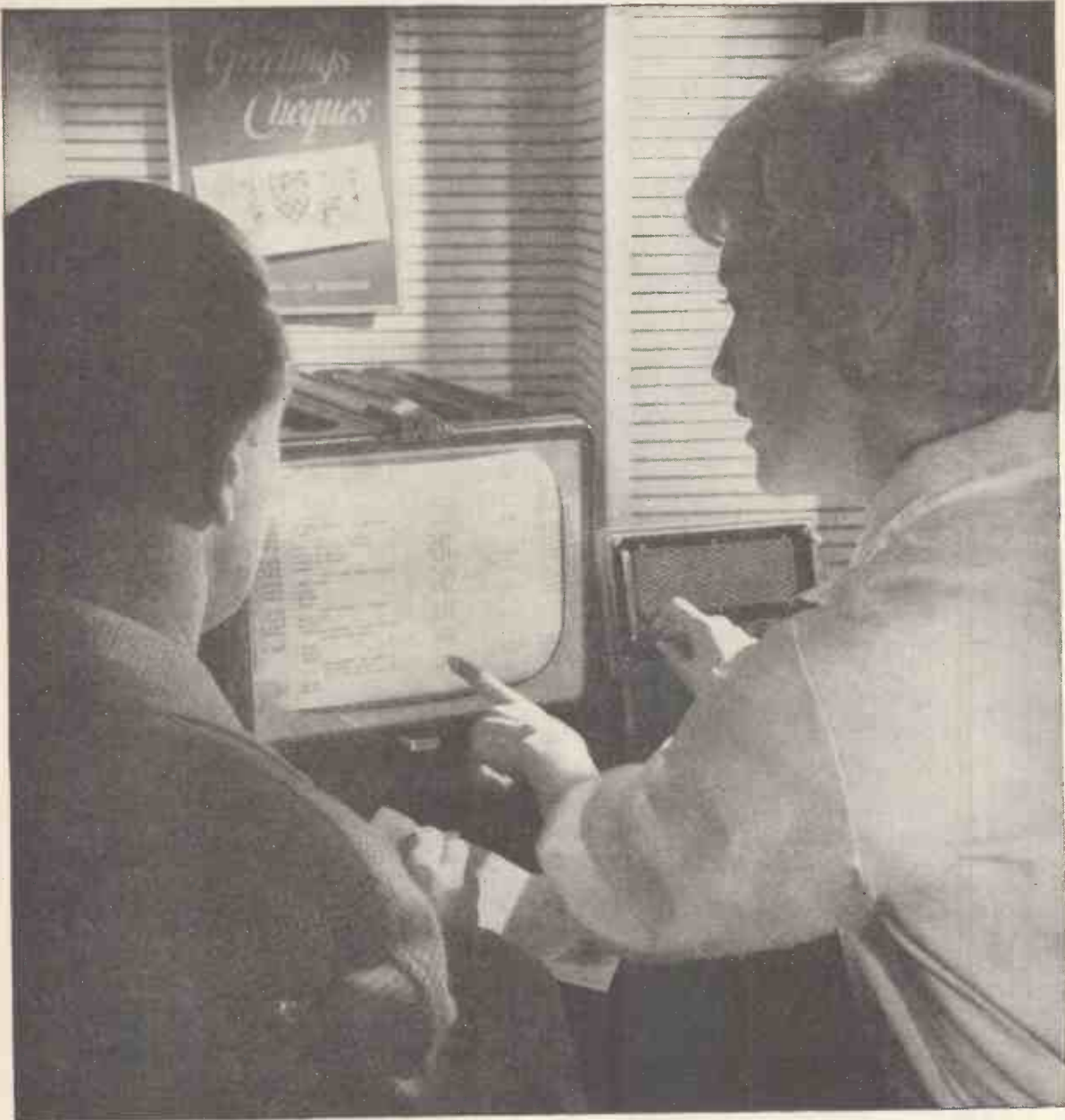
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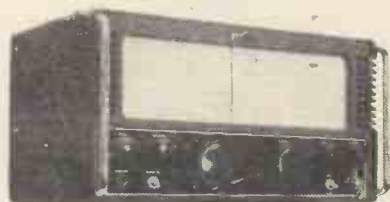
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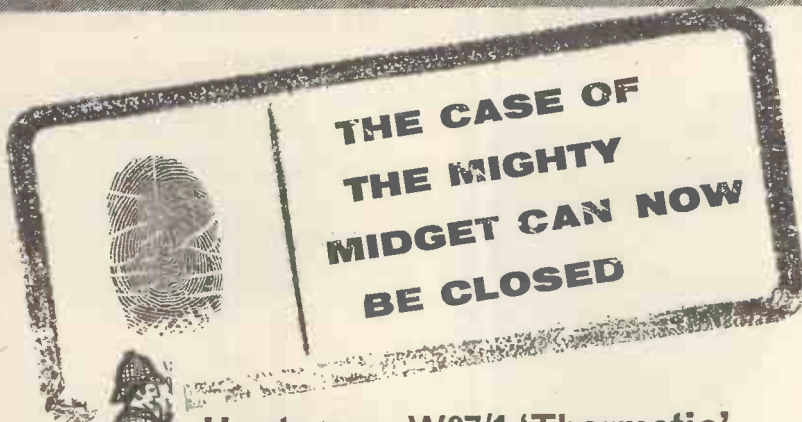
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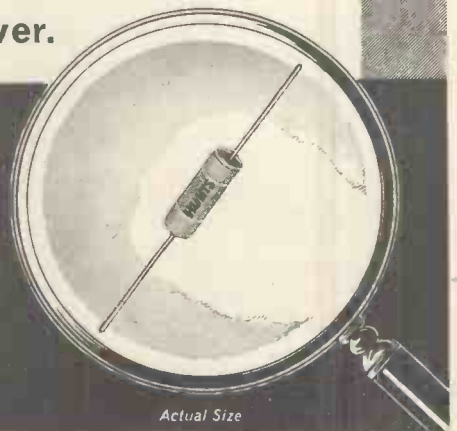
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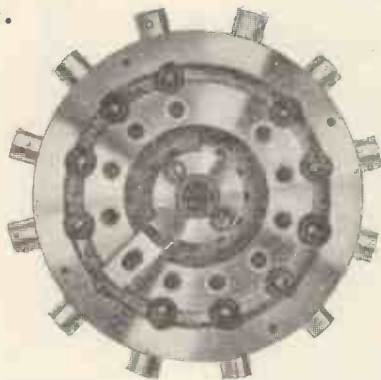
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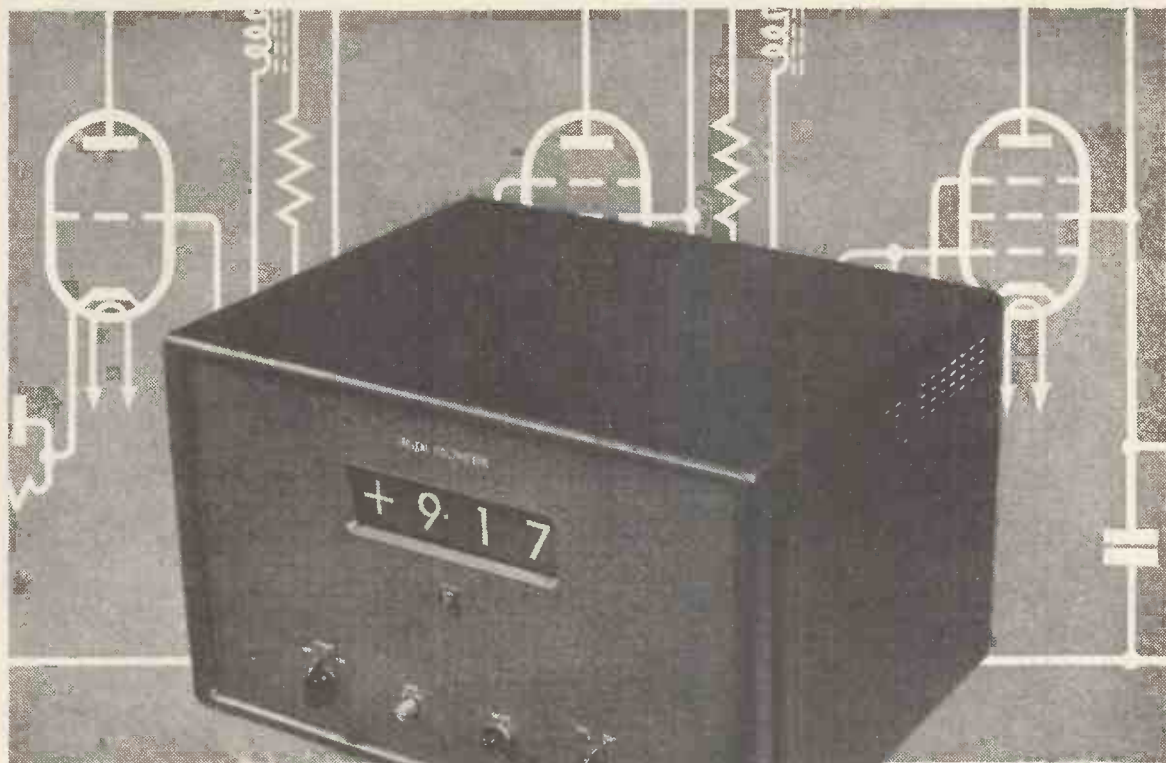
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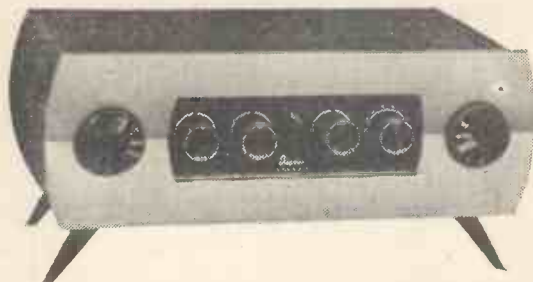
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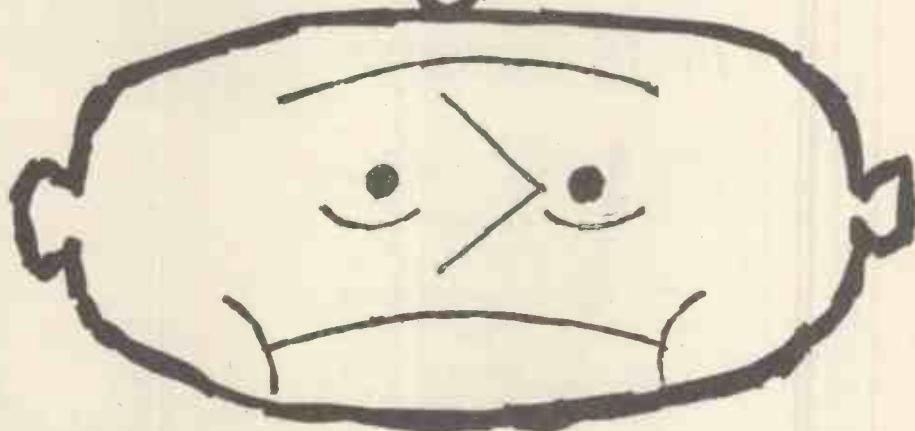


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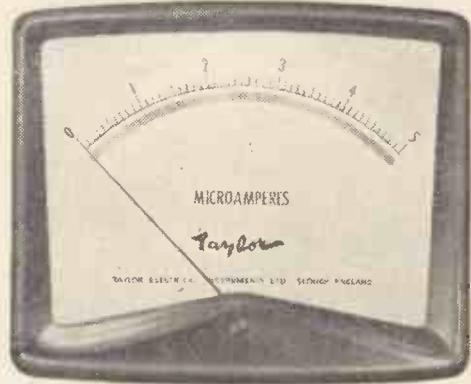
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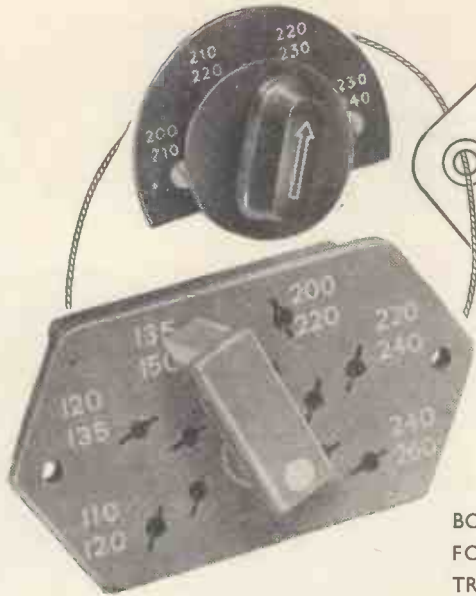
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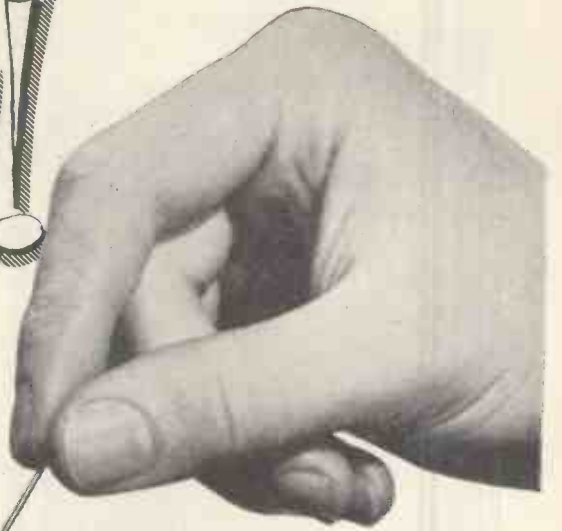
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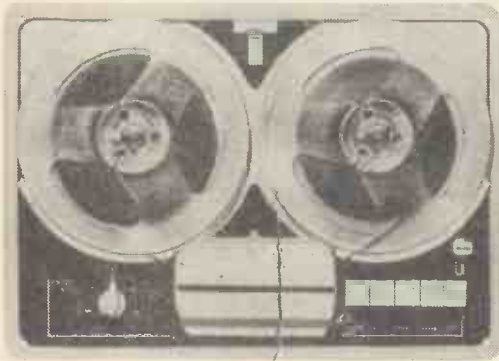
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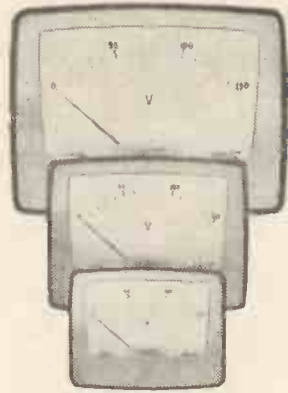
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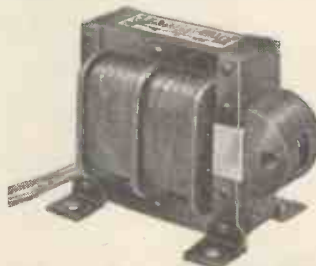
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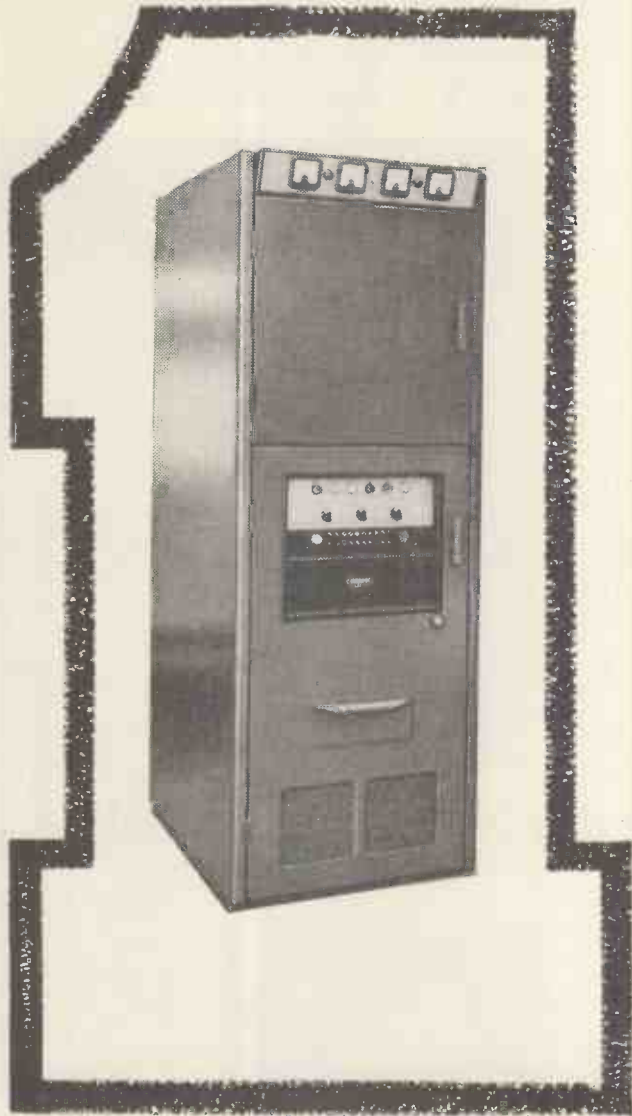
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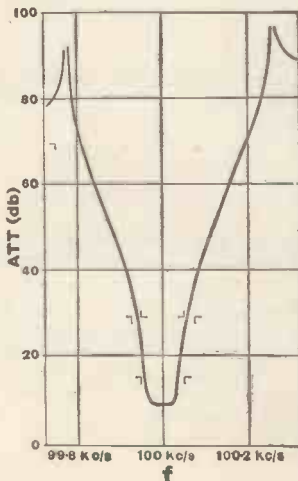
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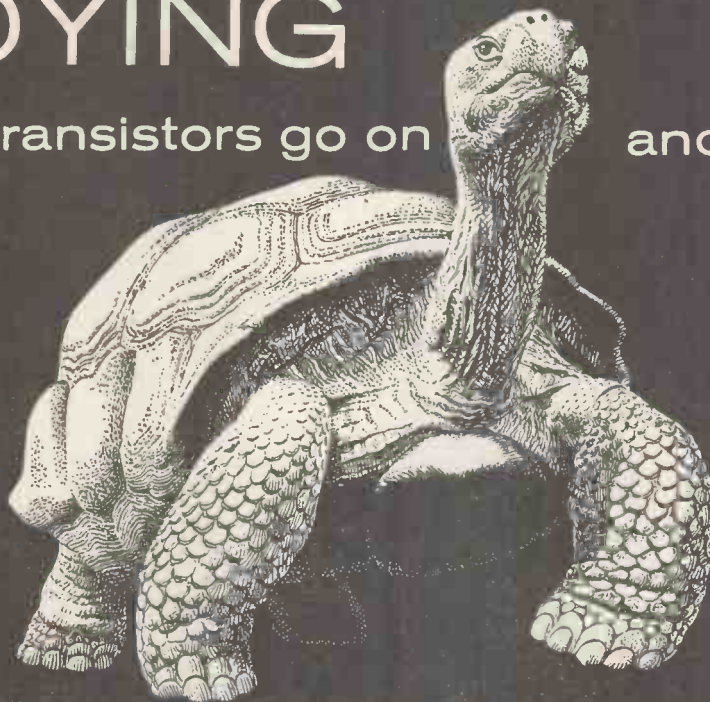
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Thank goodness the days of re-wiring domestic fuses with odd scraps of wire, or hairpins, have almost gone. The advent of the ring main system, with its convenient enclosed cartridges, has had something to do with this. Yet the principle of the hairpin still persists, due to lack of knowledge of the requisites of safety and the dangers involved in ignoring them. There must be many thousands of circuits with 13 amp. fuselinks installed, where 2 amp. should be fitted.

What does it matter? Consider that old flex under the carpet—quite half its conductors have been broken due to continual trampling, and its maximum load capacity is now a mere 10 amp. If the appliance at the end "shorts," the flex will blow for the fuse will never have a chance to do its job. The result may be a hole in the carpet, or perhaps much worse. But suppose the appliance becomes faulty, so that the current increases, say, to 10 amp. This will not blow the fuse, but will certainly result in overheating of the lead, and probably the appliance. Or an additional load may be connected by means of an adaptor, which may also overheat the lead. Remember that the heat developed at 10 amp. is 100 times greater than at 1 amp.—obviously there is grave risk of fire.

Do not imagine, however, that all will be made well simply by changing to a 2 amp. fuselink. There is more to the science of fusing than a piece of wire; we shall discuss some of the factors involved, also different types and their main characteristics, another time. Reliability, too, is a most important factor. A fuse is a protective device—it may never have to operate but, if it does, it must be fully functional in order to do its job. Even if accurately made, will it retain its characteristics throughout its working life? We are thinking of such things as embrittlement of the element. Designs, too, can be frustrated by the processes of manufacture, and a cheap, unbranded fuselink may prove more costly in the end than a slightly dearer one from a maker of established reliability. There is no way of testing a fuse to ensure it will perform correctly, except by blowing it. Be wise and fit the best—you can't afford to economize on safety measures.

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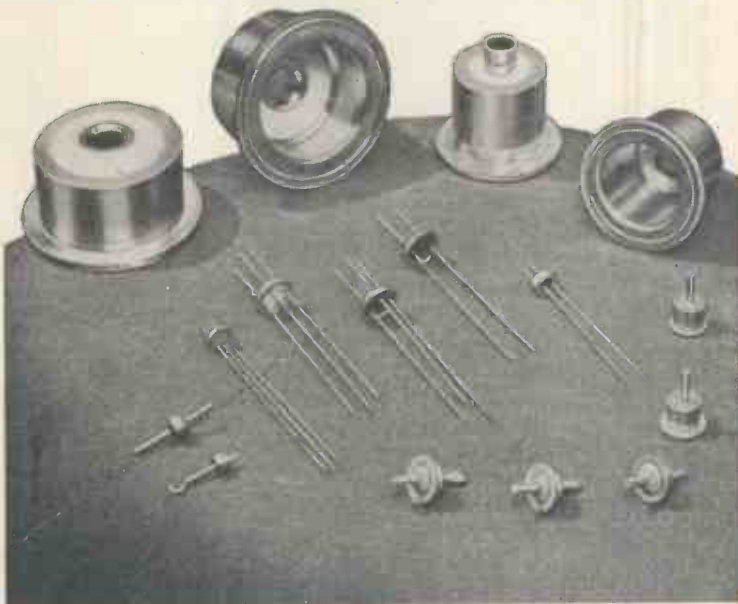
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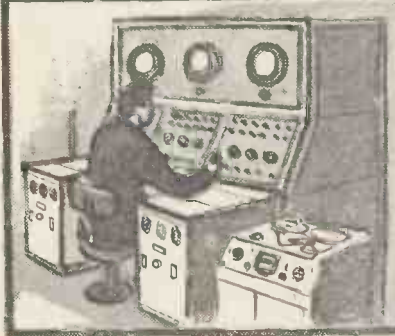
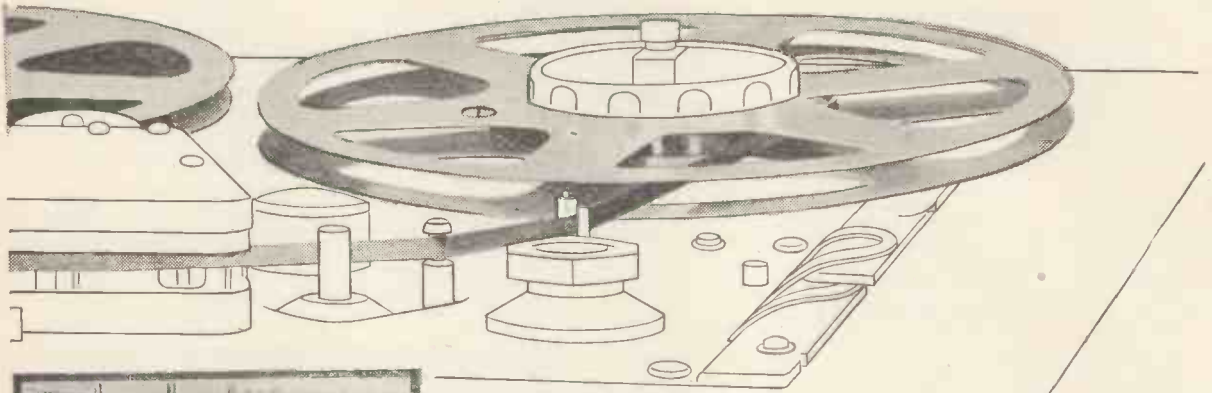


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Aspects of design

This is the twenty third of a series of special features dealing with advanced problems in television and radio circuit design to be published by The Ediswan Mazda Applications Laboratory. We will be pleased to deal with any questions arising from this or other articles, the twenty fourth of which will appear in the July 1960 issue.

Last month the conditions for the Class B stage under quiescent conditions only were considered, but it is also necessary to ensure that the maximum collector dissipation is not exceeded under drive conditions, and that thermal runaway does not occur when the drive is removed.

The maximum collector dissipation per transistor in a matched Class B stage is given very closely by

$$P_c = \frac{E^2}{\pi^2(R_L + R_e)} + I_q^2(R_L + R_e)$$

where R_L and R_e are the lower tolerance limit of the speaker load and emitter resistor, and I_q is the quiescent current corresponding to the peak junction temperature.

A value is assumed for I_q , and ΔT_j calculated from $\Delta T_j = P_c \theta + \Delta T_{amb}$ where θ is the thermal resistance of the transistor, putting this value for ΔT_j in the expression -

$$\left(2\Delta T_j + \frac{R_b + R_e + r_{bb}}{\beta} I_{ceo} + 20 \right) \text{ mV,}$$

and reducing the value of V_{be} in the $V_{be} I_c$ curve at 20°C by this amount, the V, I_c characteristic at the working junction temperature (ΔT_j above standard) is obtained. If the initial estimate for I_q is right, this curve will intersect the load line $V = V_{bb} - \frac{R_b + (\beta + 1)R_e}{\beta} I_c$ at $I_c = I_q$. If the curve intersects the load at a lower point, then the value of I_q has been over-estimated, and similarly if the curve intersects the load line at a higher point the value of I_q has been underestimated. A few successive approximations will give the correct value of I_q and the corresponding peak junction temperature. It is unnecessary to draw the whole curve, for (see Fig. 4) if the estimated value of I_q is high, the point (V, I_q) will lie to the right of the load line and similarly if it is low the point (V, I_q) will be to the left of the load line.

The requirements to be met are that (a) at the highest ambient temperature, the junction temperature does not exceed the rating for the transistor given in the data sheets, and, (b), I_q is less than the value of I_c given by the second intersection of the load line and the V, I_c characteristic (point B in Fig. 4).

If condition (a) is not met, then the value of R_L should be increased to a value at which it is satisfied. If (a) is met, but not (b), then R_L can be increased, which will decrease the peak dissipation, and/or R_e can be increased, which will principally affect the slope of the load line and the point of intersection B. In general, it will be found that the greater audio output will be obtained when R_e is made as small as possible, and R_L is increased to a safe value. This also has the advantage of giving a better power gain.

The maximum available power output (collector voltage swinging to zero volts) is given by $\frac{E \cdot R_L}{2(R_L + R_e)}$

EXAMPLE : A class B output stage using an XC131 unit.

The average value of V_{be} for $I_c = 2 \text{ mA}$ at 20°C ambient is 170 mV, and the average direct current β at 2 mA is 64. The value of R_b is made 100 Ω , and R_e is estimated to be 4.7 Ω . Then

$$V_{be} \text{ (at 2 mA)} + \frac{2}{\beta} \{ R_b + (\beta + 1) R_e \} = 170 + 12.5 = 182.5 \text{ mV.}$$

With 6 volts across the base potentiometer and $R_2 = 51 \Omega$, a value of 1600 Ω for R_1 makes the average value of $V_{bb} = 185 \text{ mV}$. Using 5% resistors the maximum value for V_{bb} is

$$204 \text{ mV. The value for } \frac{R_b + R_e + r_{bb}}{\beta} \text{ in deriving the expression}$$

$$\text{for } V \text{ versus } I_c \text{ is taken as } \frac{100 + 4 + 50}{70} = 2.2 \Omega, \text{ and the}$$

limit value of I_{ceo} is 10 mA at a junction temperature of 65°C (doubling in value for every 7°C increase in temperature). The average (V, I_c) curve at a junction temperature of 20°C, and the limit curve at 55°C ambient are shown in Fig. 5.

23

CLASS B TRANSISTOR OUTPUT STAGES (Part 2)

If it is considered that the maximum permissible quiescent current at 55°C, ambient should not exceed 18 mA, the load line is drawn through the 18 mA point on the V versus I_c curve and the point $V = 204 \text{ mV}$ on the axis. This line has a slope of 5.6 Ω .

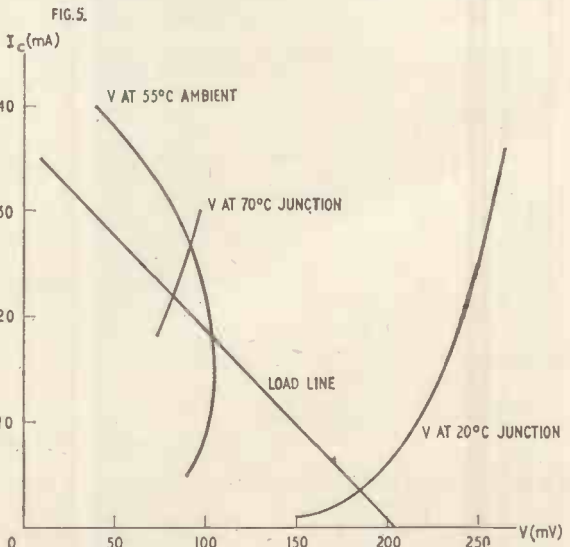
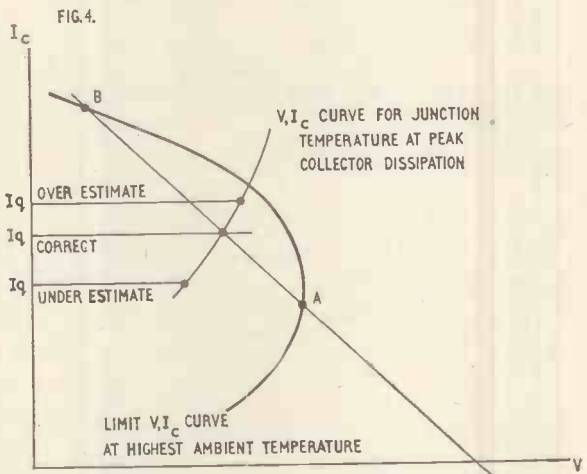
Putting $R_b = 100 \Omega$, the minimum value of R_e is $5.6 - \frac{100}{70} = 4.2 \Omega$,

and if the tolerance for R_e is $\pm 0.5 \Omega$, the nominal value becomes 4.7 Ω . Using a nominal speaker impedance of 25 Ω with a low limit of 22 Ω , the low limit for R_e of 4.2 Ω , and estimating the quiescent current at the working junction temperature under drive as 22 mA, the peak collector dissipation is

$$\frac{6^2}{\pi^2} \times 26.2 + (.022)^2 \times 26.2 = 0.152 \text{ watts.}$$

With a thermal resistance of 0.1°C/mW, the temperature rise is 15.2°C. This corresponds to a maximum junction temperature of 70.2°C. The V, I_c curve for this junction temperature intersects the load line well below the second intersection point, and so the circuit is thermally stable, and the quiescent current is 22 mA (which is the estimated value). The maximum nominal

$$\text{power output is } \frac{6^2 \times 25}{2(25 + 4.7)^2} = 0.51 \text{ watts.}$$



EDISWAN MAZDA XC131 OUTPUT TRANSISTOR

The XC131 unit consists of a matched pair of germanium pnp junction transistors, supplied in a special holder designed to give a low thermal resistance when mounted on a heat sink. These transistors are intended for use in a Class B Push Pull Output stage.

TENTATIVE RATINGS AND DATA

Maximum Temperature Ratings (Absolute Values)	
Junction Temperature (°C)	75
Storage Temperature (°C)	75
Maximum Ratings (Absolute Values for T_{amb} = 45°C)	
Peak or Mean Collector to Base Voltage (Common Base Circuit) (Volts)	-35
Peak or Mean Collector to Emitter Voltage (Common Emitter Circuit) (Volts)	-16
Peak Collector to Emitter Voltage with Base driven to cut-off (Common Emitter Circuit) or with R _{be} < 500 Ω (Volts)	-35
Peak or Mean Emitter to Base Voltage (Volts)	-12
Collector Dissipation (mW) (Per Transistor)	300

Note: The user must also ensure that operating conditions and circuit stability are such that thermal runaway cannot occur under the most adverse conditions likely to be encountered.

General Characteristics (T_{amb} = 25°C)

Thermal Resistance per Transistor with Heat Sink (for unit clamped to a 20 S.W.G. aluminium plate of 12 sq. ins. minimum area) (°C/mW)

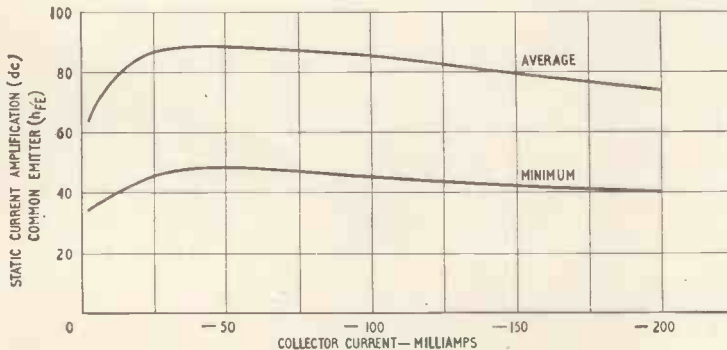
	Min.	Av.	Max.
Collector to Base Leakage Current (V _{cb} = -15 V, Emitter Open Circuit) (μA)	-	-	-10
Collector to Emitter Leakage Current (V _{ce} = -12 V, Base Open Circuit) (μA)	-	-	-250
Static Current Amplification (d.c.) (V _{ce} = -1 V, I _c = -200 mA)	40	74	-
Base to Emitter Forward Voltage (V _{ce} = -6 V, I _e = -2 mA) (mV)	-138	-158	-178

TYPICAL OPERATION

Class B Single Ended Push Pull—Common Emitter	†	††
Battery Supply Voltage (Centre Tapped), Total (Volts)	-12	-12
Speaker Load Resistance (ohms)	25	15
Emitter Stabilising Resistance, per Transistor (ohms)	4.7	3.9
Equivalent d.c. Resistance of Base Circuit, per Transistor i.e. Transformer and Bias Potentiometer (ohms)	100	100
No Signal Collector Current per Transistor, Average Transistors (mA)	2.8	2.9
Open Circuit Bias Voltage Required Across Lower Limb of each Potentiometer (mV)	184	184
Maximum Power Output for Less than 10% Total Harmonic Distortion, Average Transistors (mW)	500	750
Peak Collector Current at Maximum Power Output (mA)	200	317
Peak Base Current at Maximum Power Output, Average Transistors (mA)	2.7	5.0
Peak Base Current at Maximum Power Output, Low Limit Transistors (mA)	5	9.3

†Data given for 25°C ambient, but the circuit conditions will give satisfactory operation up to an ambient temperature of 55°C.

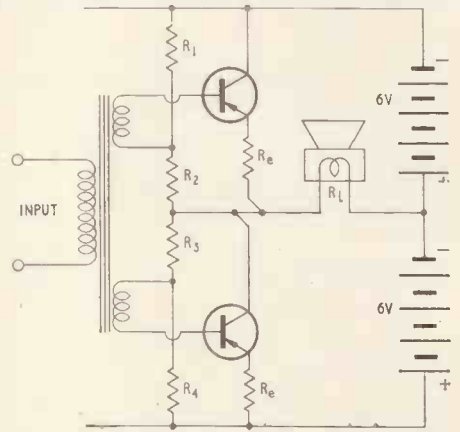
††Data given for 25°C ambient, but the circuit conditions will give satisfactory operation up to an ambient temperature of 45°C.



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TYPICAL CIRCUIT

Class B Single-ended Push Pull—Common Emitter

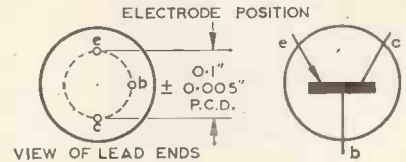
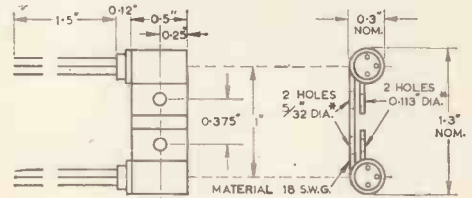


R _L (speaker) (ohms)	25	15
R ₁ , R ₃ (ohms)	1600	1600
R ₂ , R ₄ (ohms)	51	51
R _e (ohms)	4.7 ± 0.5	3.9 ± 0.5

Resistor tolerances ±5% except where stated otherwise.

Notes:
 † This circuit will give satisfactory operation up to an ambient temperature of 55°C.
 †† This circuit will give satisfactory operation up to an ambient temperature of 45°C.

DIMENSIONS AND BASING



Note:
 The lead wires should not be bent close to the glass seal. Solder should not be applied closer to the seal than 0.375 in. and during the soldering operation a heat sink (e.g. pliers) should be applied between seal and joint.

Recommended screw sizes, Barber-Coleman Type 1. 6BA for screwing to chassis or 4BA for screwing to clip.

Tentative characteristic curves of Ediswan Mazda Transistor Type XC131.

Variation of static current amplification (dc) with collector current. (Common Emitter Configuration.)

Curves taken with short duration pulse (collector dissipation less than 3mW). Collector Voltage -1V. Ambient Temperature 25°C.

Note: The minimum curve is typical of production spread.

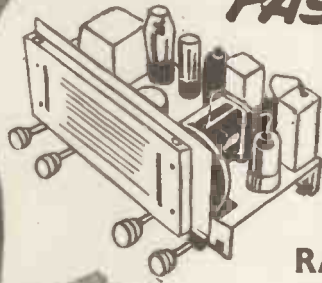
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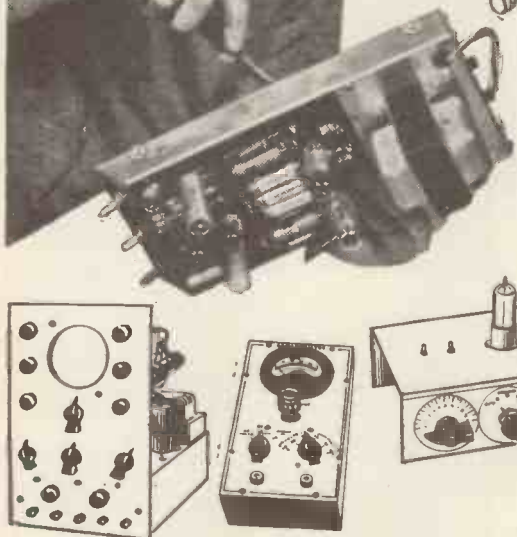
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Equivalent internal resistance	less than 0.05 ohm.	Efficiency at full load	57%
Output impedance	less than 0.15 ohm up to 50 kc/s.	Overall dimensions	length 17½", depth 17½", height 13" (44.5 × 45.1 × 33 cms)
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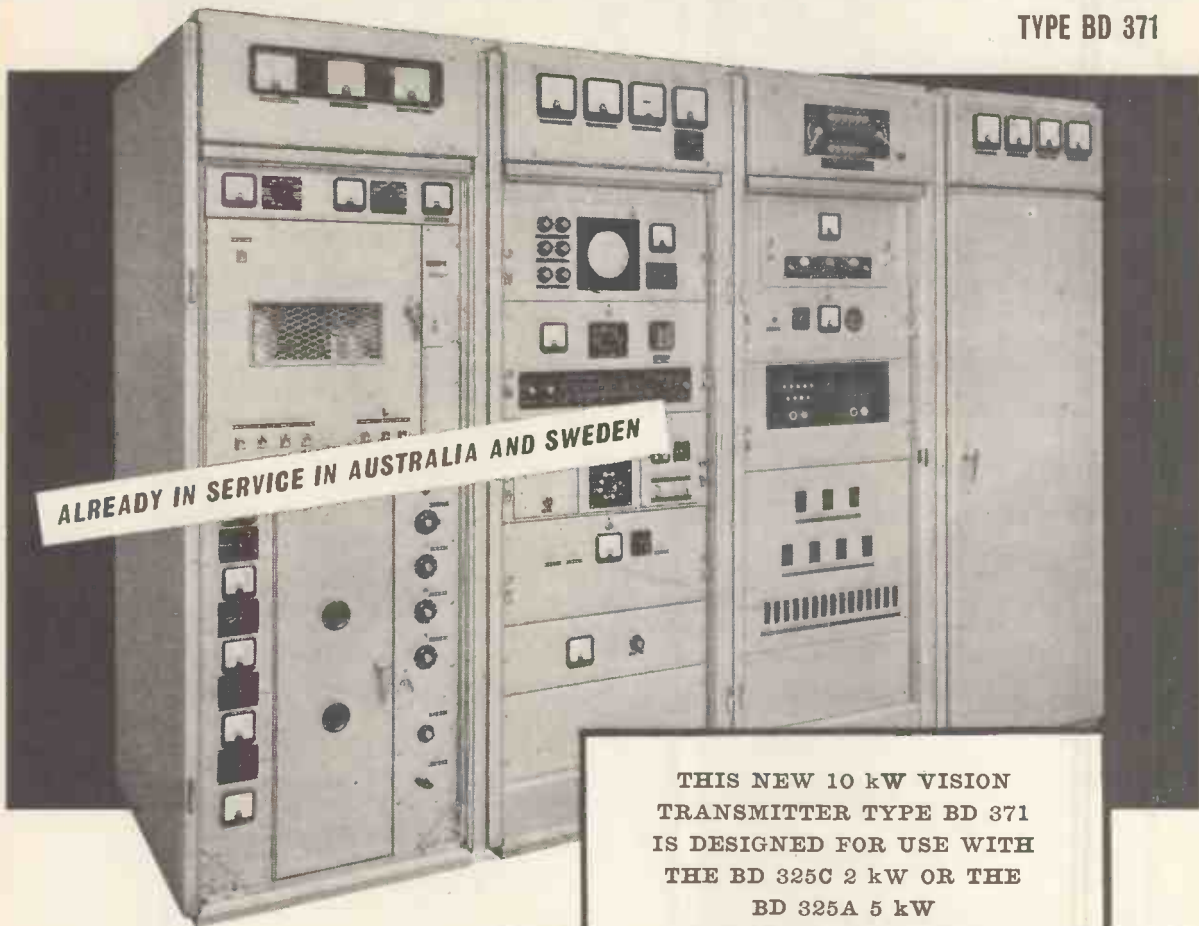
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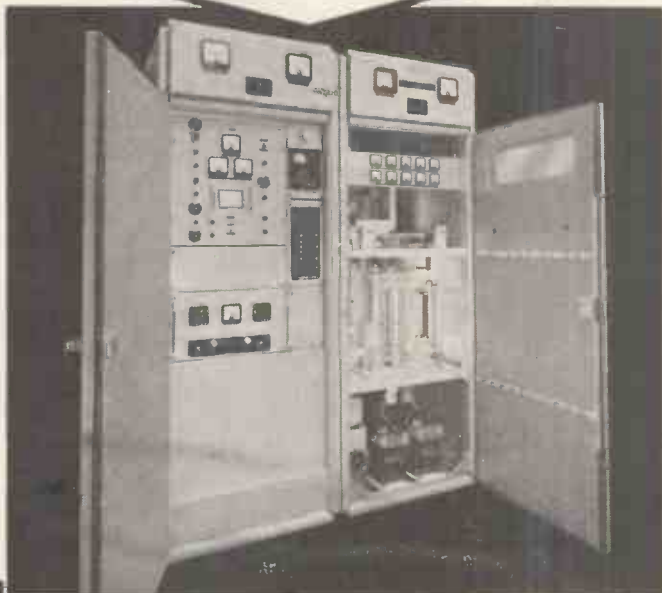
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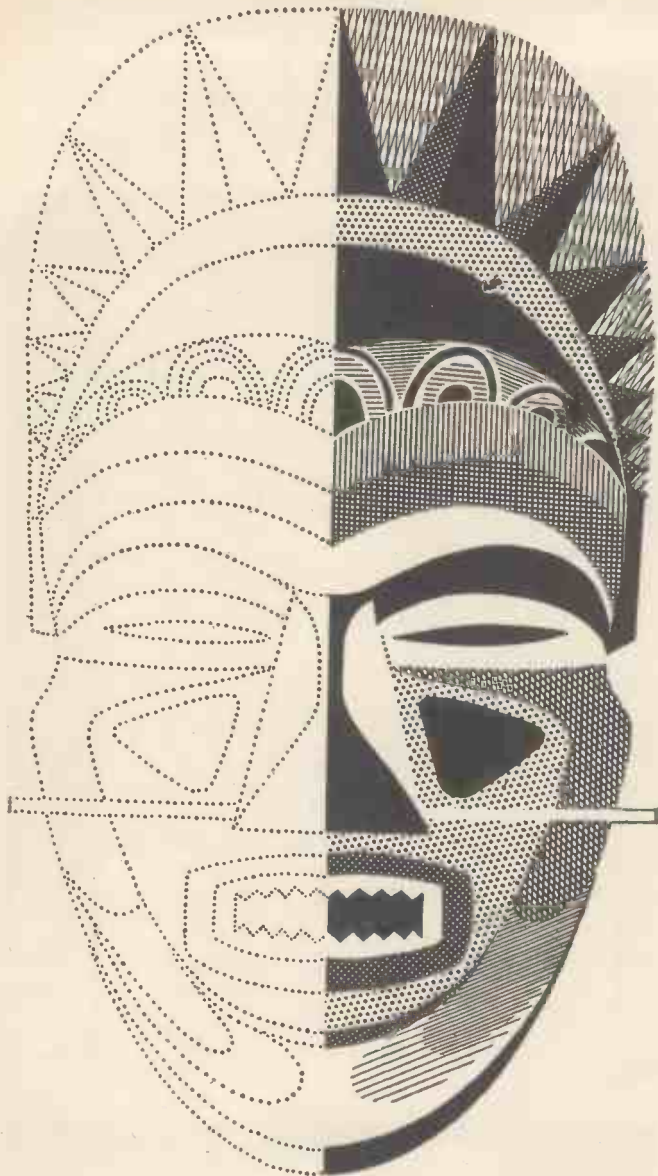
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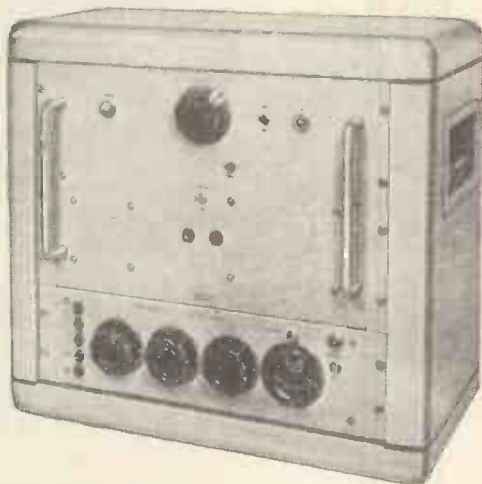
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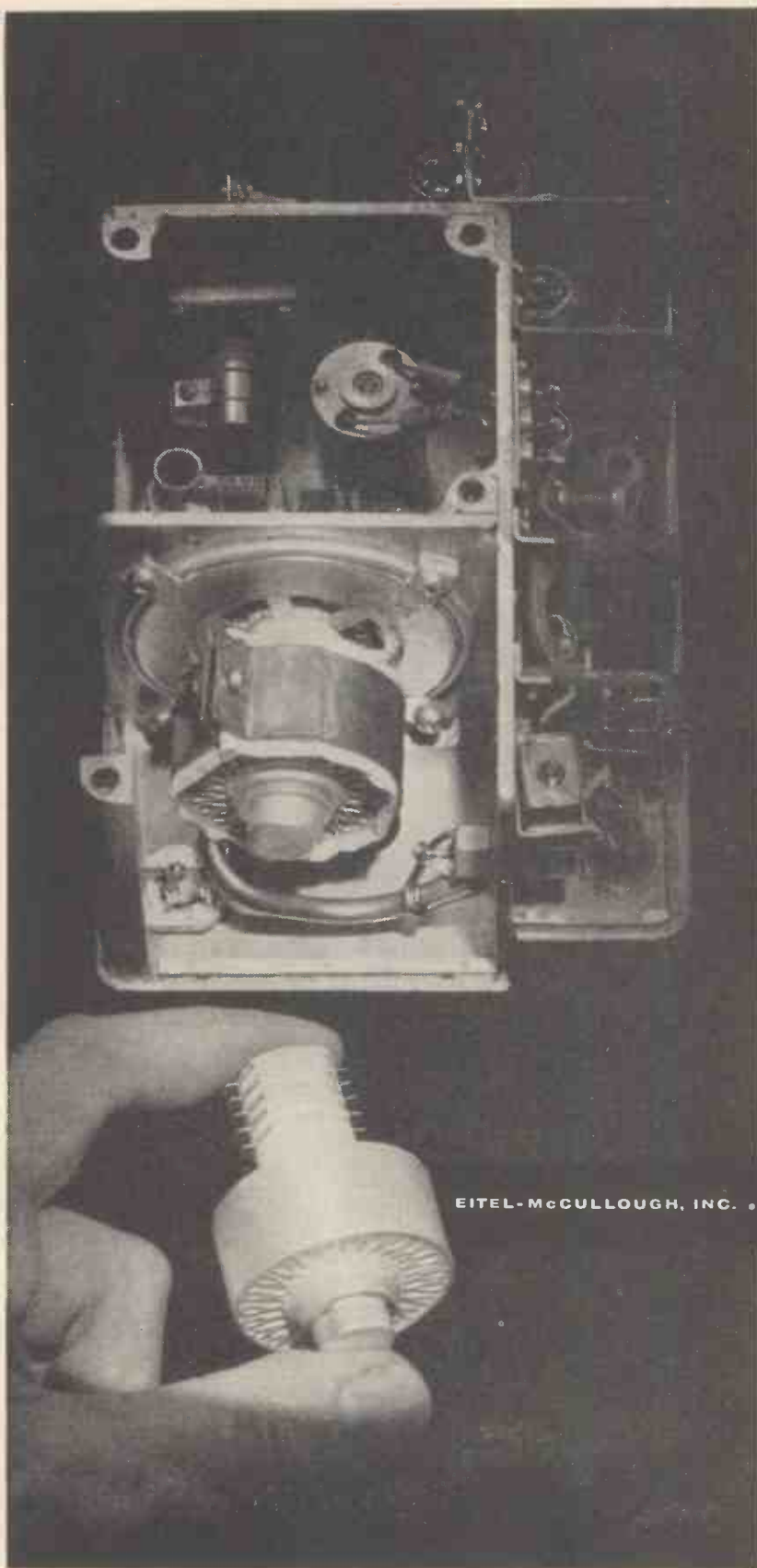
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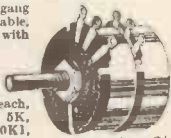
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Heater Current (amps)	I_h	0.1
Heater Voltage (volts)	V_h	19

MAXIMUM DESIGN CENTRE RATINGS

Anode Dissipation (watts)	$P_a(max)$	2.25
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Anode Voltage (volts)	$V_a(max)$	250
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Screen Voltage (Anode Current > 8mA) (volts)	$V_{g2(max)}(I_a > 8mA)$	125
Diode Peak Inverse Voltage (Each Section) (volts)	PIV _{max}	200
Peak Diode Anode Current (Each Section) (mA)	$i_{ad(pk)max}$	5
Mean Diode Anode Current (Each Section) (mA)	$I_{ad(max)}$	0.8
Cathode Current (mA)	$I_k(max)$	16.5
Resistance Control Grid to Cathode ($M\Omega$)	$R_{g1-k(max)}$	3
Resistance Control Grid to Cathode (Grid Current Biasing) ($M\Omega$)		22
Heater to Cathode Voltage (volts)	$V_{h-k(max)}$	100*

*From cathode to higher potential heater pin.

INTER-ELECTRODE CAPACITANCES (pF)†

PENTODE		
Input Capacitance	C_{in}	5.0
Output Capacitance	C_{out}	5.2
Anode to Grid 1	C_{a-g1}	< 0.0025
DIODES		
Anode Diode 1 to Cathode	$C_{a'd-k}$	2.5
Anode Diode 2 to Cathode	$C_{a''d-k}$	2.5
Anode Diode 1 to Anode Diode 2	$C_{a'd-a''d}$	< 0.25

CROSS CAPACITANCES

Anode Diode 1 to Grid 1	$C_{a'd-g1}$	< 0.001
Anode Diode 2 to Grid 1	$C_{a''d-g1}$	< 0.0008
Anode Diode 1 to Pentode Anode	$C_{a'd-ap}$	< 0.025
Anode Diode 2 to Pentode Anode	$C_{a''d-ap}$	< 0.15

†Inter-electrode capacitances in fully shielded socket, without can.

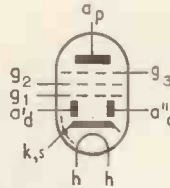
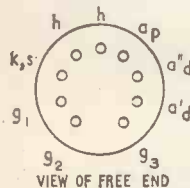
TYPICAL OPERATION

Supply Voltage (volts)	V_b	170	170	200	200
Anode Voltage (volts)	V_a	170	170	200	200
Suppressor Voltage (volts)	V_{g3}	0	0	0	0
Grid No. 1 Voltage (volts)	V_{g1}	-0.5‡	-1.5	-0.5‡	-1.5
Screen Resistor ($k\Omega$)	R_{g2}	27	21	47	30
Cathode Resistor (Ω)	R_k	—	105	—	105
Anode Current (mA)	I_a	11	11	9.5	11
Screen Current (mA)	I_{g2}	3.4	3.4	2.8	3.3
Mutual Conductance (mA/V)	g_m	5	4.5	5	4.5
Mutual Conductance for $V_{g1} = -20V$ ($\mu A/V$)		65	65	115	120
Valve Anode Resistance ($\partial v_a / \partial i_a$) ($M\Omega$)	r_a	0.45	0.45	0.6	0.6
Equivalent Grid Noise Resistance ($k\Omega$)	R_{eq}	2.5	3.5	2.5	3.5

‡This voltage is produced by the grid current flowing through the grid resistor and the steady current of the diode. If this condition is not acceptable the negative grid bias should be increased to -1.5V.

MOUNTING POSITION: Unrestricted.

BASE B9A (Noval)



MAXIMUM DIMENSIONS (mm)

Overall Length	67.5
Seated Height	60.5
Diameter	22.2

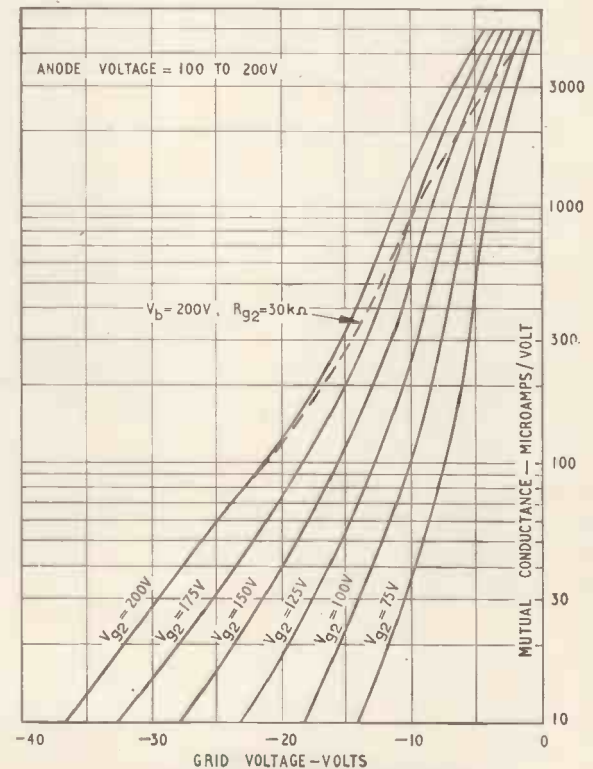
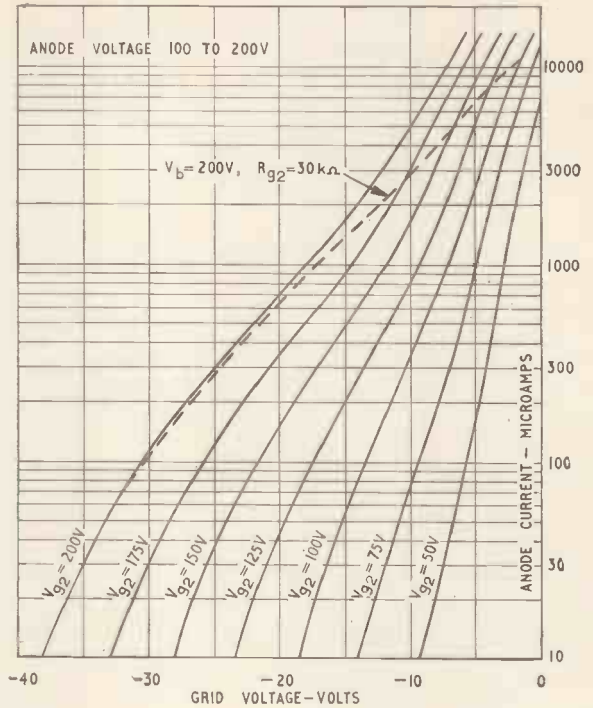
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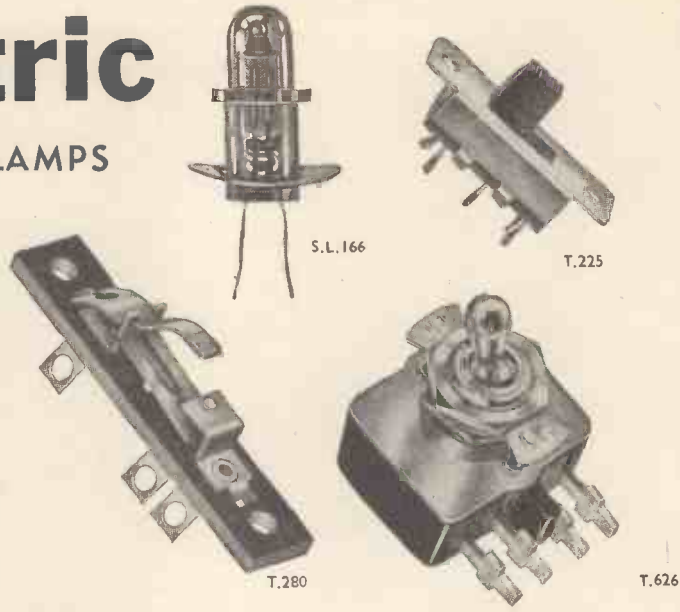
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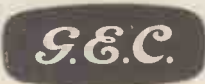
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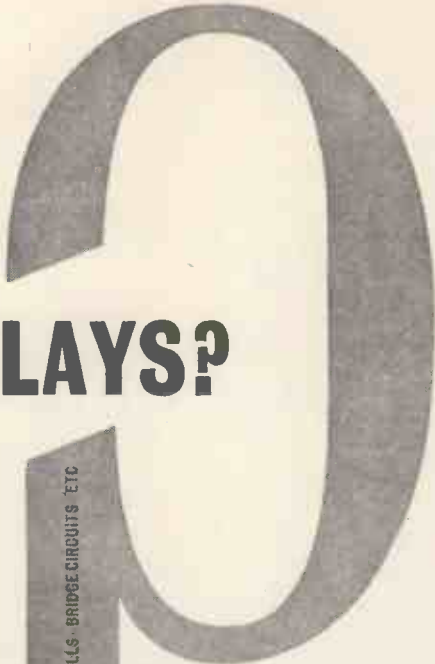
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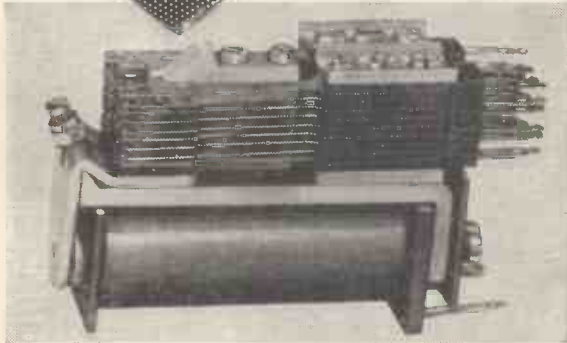


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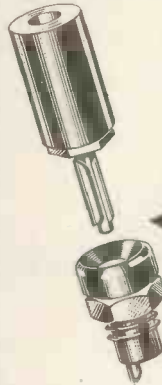


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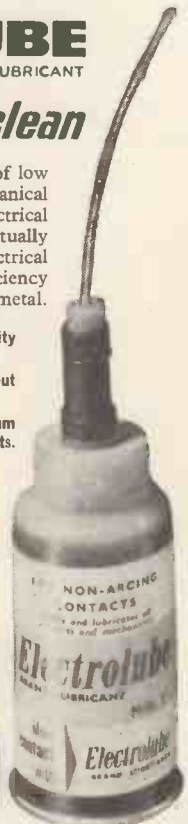
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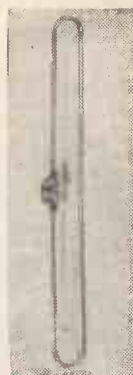
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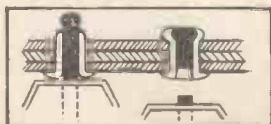
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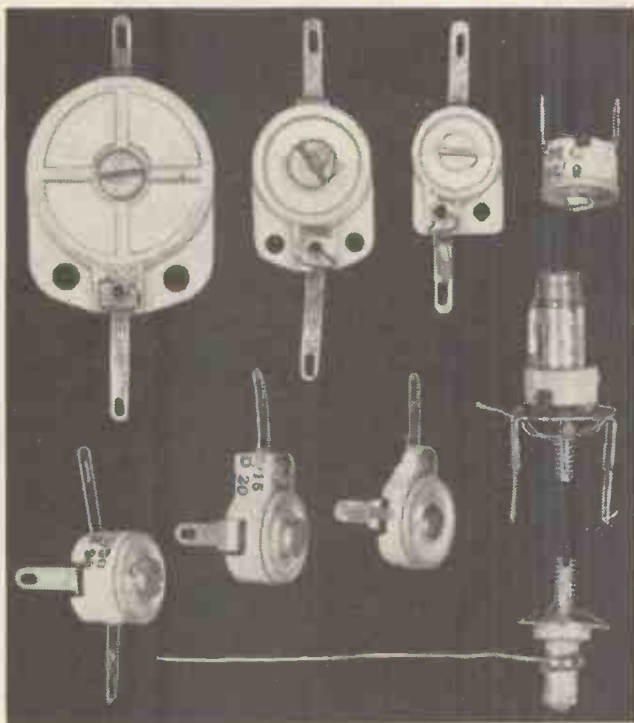
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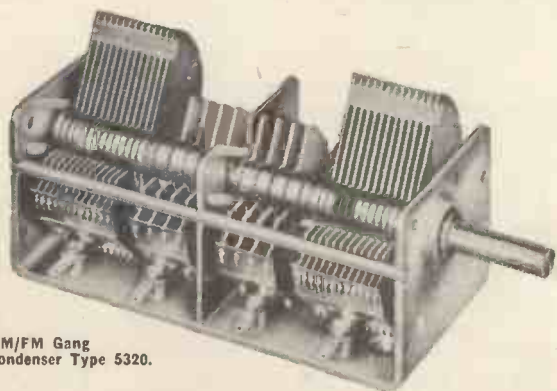
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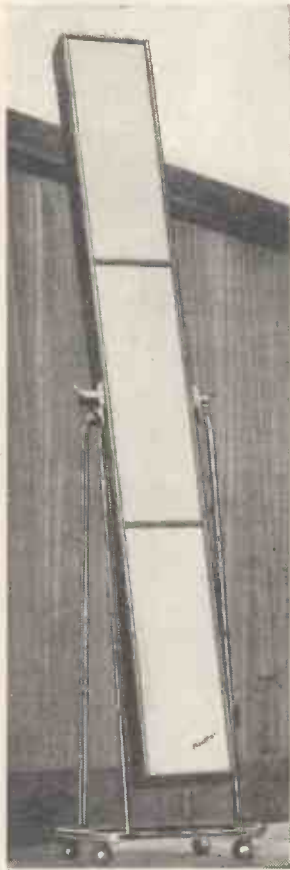
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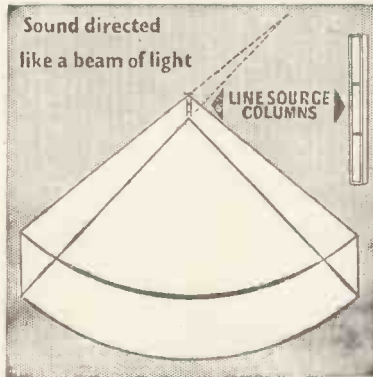
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Any stabilized output voltage in the range 200-250 v. can be selected by plug-board tappings. The selected output voltage is automatically maintained constant within $\pm\frac{1}{2}\%$, at all loads 0 to 30/37½ amps., when the supply voltage is varying over the range +8% to -12%.

- Frequency compensated 45-55 and 54-66 c/s.
- Excellent output wave-form.
- Can also be used as a variable transformer.
- **Unused.** Complete with spares and instruction book.

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TRANSISTORISED POWER AMPLIFIERS

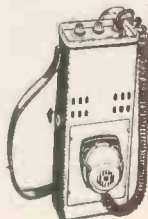
PORTABLE, MOBILE, MAINS

FOR ALL RADIO, AMPLIFIER & SOUND INSTALLATIONS

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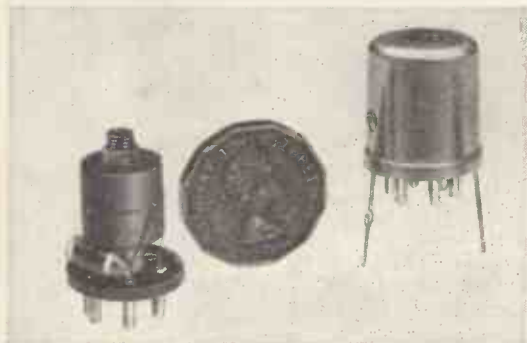
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STANSTED 3132

WEYRAD P.50 TRANSISTOR COILS AND I.F. TRANSFORMERS

FOR 2-WAVE PORTABLE WITH PRINTED CIRCUIT AND ROD AERIAL



P50/1AC M.W. OSCILLATOR COILS. For 176pF TUNING CONDENSER PRICE **5'4d.**

P50/2CC 1st and 2nd I.F. TRANSFORMER. 470 Kc/s. OPERATION. "Q" = 150..... PRICE **5'7d.**

P50/3CC 3rd I.F. TRANSFORMER. 470 Kc/s OPERATION. "Q" = 170 PRICE **6'0d.**

RA2W L.W. and M.W. ROD AERIAL 6in. long, flying-lead connections. For 280pF TUNING CONDENSER PRICE **12'6d.**

LFTD2 DRIVER TRANSFORMER. Split Secondary Type, semi-shrouded. With 6 connecting tags PRICE **9'6d.**

PCAI PRINTED CIRCUIT PANEL, 2½ x 8½in. ready drilled with component positions and references printed on rear PRICE **9'6d.**

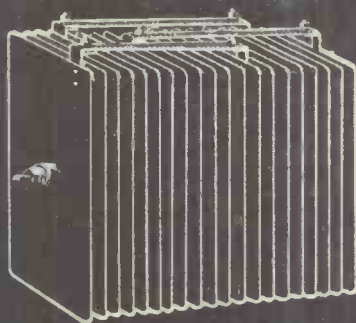
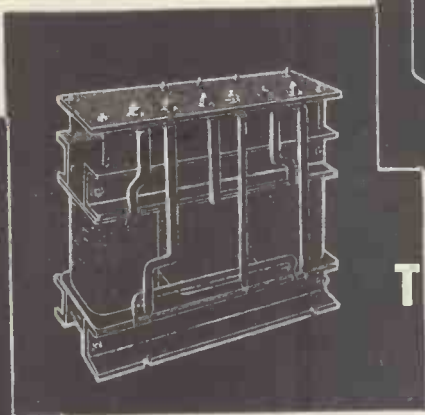
BOOKLET OF DETAILED ASSEMBLY INSTRUCTIONS AND CIRCUIT DIAGRAMS FOR 6-TRANSISTOR LONG AND MEDIUM WAVE SUPERHET PRICE **2'0d.**

ALL IN BULK PRODUCTION—TRADE ENQUIRIES INVITED

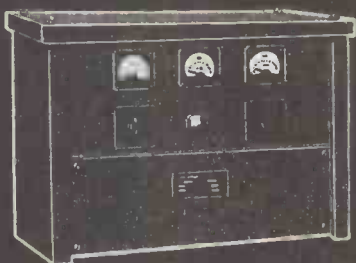
WEYMOUTH RADIO MFG. CO. LTD., CRESCENT STREET WEYMOUTH, DORSET

AUTOMAT.

RECTIFIERS



TRANSFORMERS



D C EQUIPMENT

AUTOMAT Moorside Swinton Manchester Tel: Swinton 4242-3-4

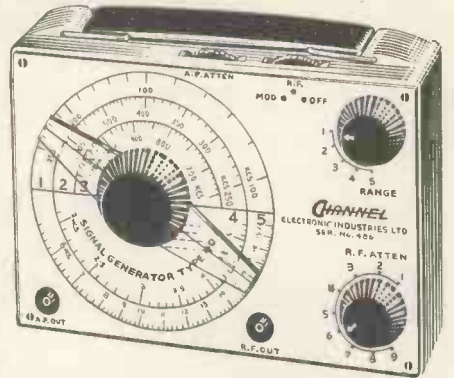
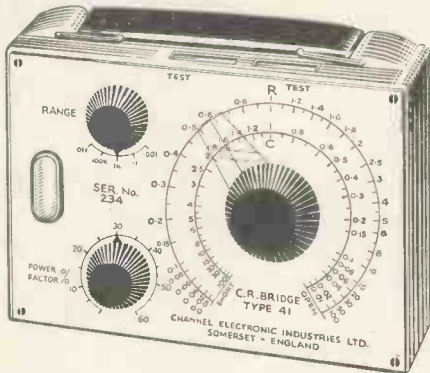
GOOD COMPANIONS!

MINIATURE TRANSISTORIZED SIGNAL GENERATOR TYPE 40

- ★ Up to 20 Mc/s on fundamentals.
- ★ R.F. and Audio Output, Attenuated.
- ★ Accuracy better than 2%.
- ★ Miniature size only 4½ in. x 3½ in.

PRICE NET **£5.15.0.**
Post (C.O.D. or C.W.O.), 2/6.

Battery
2/6 extra



MINIATURE TRANSISTORIZED R.C. BRIDGE TYPE 41

- ★ Capacitance 5 μμF to 20 μF.
- ★ Resistance 5 Ω to 20 M/Ω.
- ★ Magic Eye Balance Indicator.
- ★ Calibrated Power Factor Check.
- ★ Miniature Size—Light Weight.

PRICE NET **£5.10.0.**
Post (C.O.D. or C.W.O.), 2/6.

Battery
3/3 extra.

EXPORT ENQUIRIES INVITED.

SEND S.A.E. FOR LEAFLETS, OR ORDER TODAY, FROM

CHANNEL ELECTRONIC INDUSTRIES LTD.

DEPT. P., DUNSTAN RD.
BURNHAM-ON-SEA, SOM.

MARCUS FISHER

9 BRONDESBURY RD., LONDON, N.W.6

ESTABLISHED 1918

Phone: MAldA Yale 7554

BRAND NEW PRODUCTS OF LEADING MANUFACTURERS ONLY, AT STUPENDOUS PRICES.

PORTABLE RADIO CABINETS. Beautifully finished in grey lizard washable rexine, 10in. x 8½in. x 4in. closed. Med. & L. aerial assembly under lid, detachable. All fittings. Ideal for many purposes. Unrepeatable at 12/6. P. & P. 2/-.

TURRET TUNERS. As incorporated in well known television receivers, and in original packing. I.F. 34/65 Mc/s.-38/15 Mc/s. complete with Mullard PCC84 and PCF80 Valves. Channels fitted, 1, 2, 3, 4, 5, 8, 9. Limited Quantity at 35/6 Post Free.

VALVES: Comprehensive range of Radio and Television Valves, fully guaranteed, at prices incomparable. Special quotations to wholesalers, etc.

JACK PLUGS: Standard type, fit all equipment. Black bakelite cover, 2 contact. 2/6 each, 24/- dozen.

FERRODYNAMICS RECORDING TAPE. UNSURPASSED IN QUALITY AND REPRODUCTION OF SPEECH AND ORCHESTRATION ON ALL FREQUENCIES, AND WELL PRESENTED. TRY IT ONCE, YOU'LL USE NONE OTHER. PRICE: 1,200ft. STANDARD, 25/-; 1,800ft. L.P., 35/-, POST FREE.

Cash with order. If under £2 add postage. Overseas Postage at cost.

Also numerous items not listed, in great variety, at special prices for quantities, Resistors including transistor types, tubular and can condensers and clips, single and stranded equipment P.V.C., coils, vol. controls, gangs, etc. Also extensive range of new back-draught Mullard and similar makes of valves and American types in great demand.

WE SPECIALISE IN MANUFACTURERS' & WHOLESALE'S REQUIREMENTS.

Open from 9 till 6, Monday till Friday.

VITREOUS ENAMELLED RESISTORS

R.C.S.C. Style RWV4-L

FULLY R.C.S.C. TYPE APPROVED, 10Ω to 22KΩ, our RWV4-L style resistors conform to Inter-Services Spec. RCS III.

Other styles available. R.C.S.C. type approval applied for.

RCSC Style	CGS Style	Rating in watts		
		Service	Commercial	Range
RWV4-J	VPF4	3	4	5Ω to 8KΩ
RWV4-K	VPF10	4.5	10	5Ω to 68KΩ
RWV4-L	VPF14	6	14	10Ω to 100KΩ

THE C.G.S. RESISTANCE CO.

EVERTON, LYMINGTON, HANTS. Tel. Milford-on-Sea 269

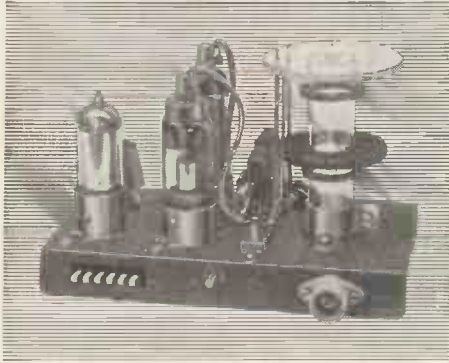
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SOUTHERN TECHNICAL SUPPLIES

TRANSFORMERS FOR ALL MULLARD AMPLIFIERS

OUTPUT TRANSFORMER (Secondaries for 3.75 and 15 ohms)
 T.44. 5-10 amp. ultra linear, 5,000 ohm. 43% tapplings 30/- P/P 2/-
 T.182. 5-10 amp. and output 915, 6,800 ohm. 20% tapplings 30/- P/P 2/-
 T.100. 5-10 amp. LOW loading, 6,040 ohm. 28/- P/P 2/-
 T.142. 7 watt stereo amp., 9,000 ohm. 20% tapplings, 26/- P/P 2/-
 T.140. 3 watt amp., type A tape amp., 3 watt stereo, 3,000 ohm. 12/- P/P 1/6
 MAINS TRANSFORMERS (Primaries 240-220-260; 0-10 v. 50 c/s.)
 T.55. 5-10 amp. and tuner, 300-0-300 v., 120 mA., 6.3 v. 2.5 a., 6T., 6.3 v. 2 j a., 6.3 v. 1 a., 32/- P/P 2/6
 T.58. 5-10 amp. 300-0-300 v., 100 mA., 6.3 v. 2.5 a., cT. 6.3 v. 1 a., 27/- P/P 2/6
 T.101. Two 5-10 amp. Low loading, 300-0-300 v., 150 mA., 6.3 v. 4 a., cT. 6.3 v. 1 a., 34/- P/P 2/9
 T.143. 7 watt stereo 250-0-250 v., 150 mA., 6.3 v. 4 a. cT., 6.3 v. 1 a., 33/- P/P 2/9
 T.141. 3 watt, 300-0-300 v., 60 mA., 6.3 v. 1 a., cT., 6.3 v. 1 a., 22/- P/P 2/-
 T.183. 2 watt stereo 250-0-250 v., 80 mA., 6.3 v. 2 a. cT., 6.3 v. 1 a., 25/- P/P 2/6
 T.A. Trans. and Rectifier. 270 v. D.C. 100 mA., 6.3 v. cT., 3 a., 32/- P/P 2/-
 T.B. Trans. and Rectifier. 270 v. D.C. 60 mA., 6.3 v. cT., 2 a., 25/- P/P 2/-
 All transformers fully guaranteed, all shrouded fully except T140 and TB. Write for our fully illustrated catalogue, with all data.
 SPECIAL OFFERS T44 and T55, 59/-; T143 and two T142's, 82/- P/P 3/6 on both. Mullard's latest Publication detailing the complete range, "CIRCUITS FOR AUDIO AMPLIFIERS," 8/6 P/P 1/-
SOUTHERN TECHNICAL SUPPLIES, 83 Station Road, Portslade, Sussex

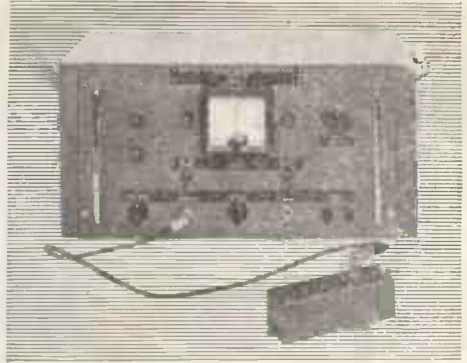
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and you want it
Designed and Developed or produced*
to your specification



Compact Stabilised High Voltage Supply. Safe and reliable supply for photo-multiplier cells and cathode ray tubes. Variable output between 0-1250V D.C. at 250 micro amps. Size 6" x 4" x 3".

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TYER

(formerly P.A.M. Ltd.)



This instrument has been specially designed for the routine production testing of Commutators; its function is to indicate surface roughness and eccentricity to within very close limits.

Tyer & Co. Ltd. Electronics division combines the technique of several companies, long-established in the Electronic field, with the extensive modern production resources of Tyer & Co. Ltd. Examples of recent work are illustrated.

** Whichever stage of the struggle you've reached, we can save you time and trouble—maybe money too—write or 'phone without delay.*



TYER & COMPANY LTD

PERRAM WORKS, MERROW SIDING, GUILDFORD, SURREY Telephone Guildford 2211

A member of the Southern Areas Electric Corporation Group



HETERODYNE FREQUENCY METERS

BRITISH MANUFACTURED

Designed and built to rigid services specifications.

TYPE T75.

Frequency Range: 85 to 1,000 megacycles.

TYPE T74.

Frequency Range: 20 to 250 megacycles.

Frequency calibration accuracy: .002% at 25° C. (or .01% between -20° C. to +70° C.).

Crystal-controlled, portable heterodyne-type Frequency Meters used for Field testing and measurement of pulsed, modulated, or C.W.R.F. transmitters, receivers and signal-generators.

Mains Operated Power Unit available as optional extra and designed to fit into the battery compartment.

Reconditioned and calibration-checked B.C.221 Frequency Meters, range 125 Kc/s to 20 Mc/s, still available.

Provisional specifications on a new wide-range, very high accuracy Frequency Meter and also an instrument covering the range 100 Kc/s to 1,000 Mc/s (higher under favourable conditions) available on request.



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Complete Specifications on application to:—

Sole Manufacturers **TELEMECHANICS LTD**

(Instrument Division Dept. W.W.8)
 BROKENFORD LANE, TOTTON, HANTS, ENGLAND.

Telephone: Totton, Southampton 3666 Cables: "Teleset," Totton, Southampton

Agents: Some overseas territories still available.

Makers of High Voltage Test Sets and other Electronic Equipment for H.M. Government.

WE SEND THE BEST OF BRITAIN'S HI-FI EVERYWHERE

EVERYTHING FOR RADIO, RECORD & TAPE

- PROMPT DESPATCH SERVICE
- HOME AND EXPORT ENQUIRIES WELCOMED AT ALL TIMES
- 110 VOLT ITEMS AVAILABLE

★ RECORDERS

Vortexion W.V.A.	£93 13 0	\$267
Vortexion W.V.B.	£110 3 0	\$315
Brenell Mk. V	64 gns.	\$192
Brenell 3 Star Stereo	89 gns.	\$267
Cossor 4 Track Stereo P3 ...	37 gns.	\$111
Cossor 4 Track Stereo P3 ...	53 gns.	\$127
Simon SP4	95 gns.	\$285
Simon Minstrelle	39 gns.	\$117
Ferrograph 4AN	81 gns.	\$243
Ferrograph 4AH	86 gns.	\$258
Ferrograph 8B8	105 gns.	\$315
Grundig TK60 Stereo	128 gns.	\$384
Grundig TK55 Stereo	92 gns.	\$276
Grundig TK20 with Mic.	52 gns.	\$156
Grundig TK30	72 gns.	\$216
Philips 4 Track Stereo PB ..	59 gns.	\$117
Philips 4 Track Stereo	92 gns.	\$276
Philips 4 Track Stereo PB ..	37 gns.	\$111
Stuzzi Transistor 2 Speed ...	69 gns.	\$207
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Steel nax Battery 2 Speed ...	55 gns.	\$165

★ DECKS

Waarite 4A	£35 16 0	\$105
Waarite 4B	£41 10 0	\$119
Brenell	28 gns.	\$84
Brenell Pre-Amp. and Amp. ...	24 gns.	\$72

Above in Stereo at extra cost.
 Microphones by Lustraphone, Reslo, Acos, Simon Sound, Geloso, etc.
 ★ TAPES BY ALL LEADING MAKERS

★ SPEAKER SYSTEMS

Quad electrostatic	£52 0 0	\$149
Wharfedale SFB/3	£39 10 0	\$113
Wharfedale Coaxial 12	£25 0 0	\$156
Wharfedale Golden 10	£8 14 11	\$18
Tannoy 12in. Monitor	£30 15 0	
Tannoy 15in. Monitor	£37 10 0	
WB. 1016	£7 12 3	\$22
Goodmans Triaxiom	£25 0 0	\$71
Goodmans 300	£11 5 9	\$32
Goodmans 400	£16 10 0	\$46
Kelly Ribbon Mk. II	£10 1 0	\$30
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Decca Stereo PU	£20 19 5	\$45
Lenco GL60 Trans. Unit	£27 12 6	\$60
Lenco GL58/R	£27 16 6	\$60
Garrard 301	£22 7 3	\$48
Garrard 4HF/Stereo P.U.	£19 4 8	\$40
Garrard TA/Mk. II	£8 10 0	\$19
Connoisseur motor	£27 16 1	\$59
Golding 700	£9 14 9	\$21
Rone to DC284	£3 19 6	\$9
FME P.U. 12in. arm	£17 10 0	\$60

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Quad 22-Control Unit	£25 0 0	\$72
Quad 11 Amplifier	£22 10 0	\$64
Leak Stereo 20 Amp.	£30 9 0	\$87
Leak Point One Pre-Amp.	£21 0 0	\$60
Jason J.2-10/Mk. III	£37 10 0	\$107
Quad FM Tuner	29 gns.	\$60
Chapman AM/FM	£29 8 0	\$60
Jason JTV/2 Tuner	£25 7 3	\$41

Enquiries for new items by firms mentioned in this advertisement invited.

Adds a New Dimension to Sound

THE BINSON "ECHOREC," distributed by us (see W.W. Feb. page 92), is a device for superimposing controlled echo on to any audio signal. It achieves within the size of a compact, fully portable instrument, effects normally requiring large echo chambers and associated equipment. Three working channels are provided, the echo interval is variable, and swell and other effects are obtainable.

ABRIDGED DESCRIPTION

- Three inputs and outputs.
- Push-button channel selection for 1, 2 or 3 channels.
- ★ Controls for echo intervals, volume of echo, swell effect, volume level on input channels, etc.
- Complete with fitted carrying case leads, plugs.
- A.C. mains operated.

Professional Discounts

140 gns. \$420 Leaflet on request. Trade enquiries invited.

We carry extensive and up-to-date stocks of equipment, components and accessories by Britain's leading makers. Enquiries dealt with by return.

164 CHARING CROSS ROAD, LONDON, W.C.2

(3 shops from Tottenham Court Road Station Underground)

Tel: TEM 7587 & COV 1703

Cables: MODSHAREX, LONDON

MODERN ELECTRICS (RETAIL) LTD.

STEREO £7.7.0

Independent twin channel amplifier with excess of 3 watts per channel.
 Concentric volume control (optimum balance arranged immediately without additional knobs).
 Stoved grey or blue hammer chassis 9 1/2 in. x 5 1/2 in. x 6 in.
 Input suiting most modern crystals; output matching 3 ohm speaker each channel.
 For operation on AC mains 200/250 v. Post & pkg. 4/-



E.K.E.

BROTHERTON, KNOTTINGLEY, YORKS.

If your local dealer has not one in stock we will gladly loan him one for you to hear. Another Model, £3/12/- carriage paid

LARGE STOCK ALWAYS AVAILABLE OF

BELLING-LEE
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WELWYN, etc. etc.

SOLE LONDON DISTRIBUTORS OF
ELCOM
 MINIATURE MULTI-WAY PLUGS & SOCKETS

HAVE YOU HAD OUR NEW FULLY ILLUSTRATED CATALOGUE OF HI-FI AND ELECTRONIC EQUIPMENT

6d. Post Free.

BERRY'S RADIO

25, HIGH HOLBORN, LONDON, W.C.1.

Telephone: HOLborn 6231/2.

C.R.T. ISOLATION TRANSFORMERS

For Cathode Ray Tubes having Heater/Cathode short circuit and for C.R. Tubes with falling emission. Full instructions supplied.

Type A. Low Leakage windings. Optional Boost 25% and 50%. Tapped mains primaries.

2 volt 12/6 each
 4 volt 12/6 each
 6.3 volt 12/6 each
 10 volt 12/6 each
 13.3 volt 12/6 each

OUR LATEST SUPERIOR PRODUCT. Type A2.
 High Quality. Low capacity. 10/15pf. **16/6** each
 Optional boost 25%, 50%, 75%.
 Type B. Mains input. Low capacity. Multi Output 2, 4, 6.3, 7.3, 10 and 13 volts. Optional boost 25% and 50%. Suitable for all Cathode Ray Tubes 21"-.

RESISTORS. All preferred values. 20%, 10 ohms to 10 meg. 1 w., 4d.; 1 w., 4d.; 1 w., 6d.; 1 1/2 w., 8d.; 2 w., 1/1-
HIGH STABILITY. 1/2 w., 1%; 2/-. Preferred values 100 to 10 meg. Ditto 5% 9d., 100 to 5 mcg.

5 watt } **WIRE-WOUND RESISTORS** { 1/3
 10 watt } 25 ohms-10,000 ohms. { 1/6
 15 watt } 25 ohms-10,000 ohms. { 2/3
 15,000 ohms-50,000 ohms, 5 w., 1/9; 10 w., 2/3
WIRE-WOUND POTS, 3 w. **WIRE-WOUND POTS, 4 w.**
 Pre-set Min. T.V. type Standard size Pots, long
 Knurled Slotted knob Spindle High Grade. All
 All values 25 ohms to 25K. All values 100 ohms to 50 K.
 3/- ea., 30 K., 50 K., 4/- 6/6; 100 K. 7/6.
 Ditto, 1/2 w. Carbon Track **W/W EXT. SPEAKER**
 10 to 2 Meg., 3/-. **CONTROL 100, 3/-**
OP TRANSFORMERS Heavy duty 50 mA., 400 Multi-
 ratio push-pull, 7/6. Miniature 3V4, etc., 4/6. Hygrade
 Push-pull 10 watts, 15/6. **MULLARD "610" 6k or 8k 30/-**
L.F. CHOKES 15/10H 60/65 mA., 5/-. 10H 85 mA., 10/6.
 10H 150 mA., 14/-.

MAINS TRANSFORMERS 200/250 v. A.C.
STANDARD 250-0-250, 80 mA., 6.3 v. 3.5 a.
 tapped 4 v. 4. Rectifier 6.3 v. 1 a., tapped 5 v.
 or 4 v. 2 a. Ditto 350-0-350 22/6
MINIATURE 220 v. 20 mA., 6.3 v. 1 a. 10/6
MIDGET, 220 v. 45 mA., 6.3 v. 2 a. 15/6
SMALL, 220-0-220 50 mA., 6.3 v. 2A. 17/6
STANDARD, 250-0-250, 65 mA., 6.3 v. 3.5 a. 17/6
HEATER TRANS., 6.3 v. 1 a., 7/6; 3 amp., 10/6
GENERAL PURPOSE LOW VOLTAGE. Outputs 3, 4, 5, 6, 8, 9, 10, 12, 15, 18, 24 and 30 v. at 2 A. 22/6

ALADDIN FORMERS and cores, 1/4in., 3/4in., 1in., 10d.
 0.3in. **FORMERS 5937 or 8** and Cans TV1 or 2. 1in. sq. x 2in. or 3in. sq. x 1 1/2in., 2/- with cores.
SLOW MOTION DRIVES. Epicyclic ratio 6:1, 2/3.
SOLEN. Midget Soldering Iron, 230 v., 25 w., 24/-.
REMPLOY INSTRUMENT IRON. 230 v., 25 w., 17/6.
MAINS DROPPERS. 3 x 1/4in. Adj. Sliders, 3 amp., 1,000 ohms 4/3. 2 amp. 4/3. 1 amp. 2,000 ohms, 5/-
L.I.N.E. CORD. 3 amp., 60 ohms per foot, 2 amp., 100 ohms per foot, 2 way, 6d. per foot, 3 way, 7d. per foot.

CRYSTAL MIKE INSERT by Acos 6/6
 Precision engineered. Size only 1/4 x 1/4 in.
ACOS CRYSTAL STICK MIKE 39-1. Bargain 37/6.

MIKE TRANS. 50:1, 3/9 ea.; 100:1 Potted 10/6.
LOUDSPEAKERS P.M. 3 OHM. 5in. Rola, 17/6.
 6in. x 4in. Rola, 18/- 7in. x 4in. Rola, 21/-
 10in. x 6in. Rola, 27/6 8in. Plessey, 19/6
 6in. Rola, 18/6 8in. Rola, 21/- 10in. Rola, 30/-
HI-FI TWEETERS, 4in. 25/- 12in. Plessey, 30/-
 12in. Baker 15 wt. 3 ohm and 15 ohm models, 105/-
 12in. Baker foam suspension 15 v. 15 ohm. 28/-
 12in. 15 ohm Plessey 10 wt., 45/-.

I.F. TRANSFORMERS 7/6 pair
 465 kc/s. slug tuning miniature can 2 1/2 x 1 1/2 in. High Q and good bandwidth. By Pye Radio. Data sheet supplied.
 Wearite M800 I.F. Miniature 465 kc/s., 12/6 pair.
 Weymouth I.F. Standard size 465 kc/s., 12/6 pair.

CRYSTAL DIODE G.E.C., 2/-. GEX34, 4/- 40 Circuits, 3/-
H.R. HEADPHONES. 4,000 ohms, brand new, 15/- pair.
SWITCH CLEANER Fluid, squirt sprout, 4/3 tin.
TWIN GANG CONDENSERS. 365 pf. Miniature, 1 1/2in. x 1 1/2in. x 1 1/2in., 10/- 0005 standard with trimmers, 9/-; less trimmers, 8/- Midget 7/6; Single 50 pf., 2/6; 100 pf., 150 pf., 7/- Solid dielectric 100, 300, 500 pf., 3/6
VALVE HOLDERS. Pax. int. Oct., 4d. EP50, EA50 6d.
B12A, CRT, 1/3. Eng. and Amer. 4, 5, 6, 7 pin 1/-
**MOLDED Mazda or Int. Oct. 6A, 6Y6, 6BA, 6BC6, 6BA, 6A, 6Y6 with can, 1/6; B12A, 1/3. B9A with can, 1/9. CERAMIC EP50, 6Y6, B9A, Oct. 1/-; B7G, B9A Cans, 1/-
SPEAKER PAPER. Gold Cloth 17in. x 25in., 5/- 25in. x 35in., 10/- Tygan 5 1/2in. wide, 10/- ft. 27in. wide, 5/- ft. Samples, S.A.A.**

WAVELENGTH SWITCHES
 2 p. 2-way, 3 p. 2-way; short spindle 2/6
 2 p. 4-way, 2 water, long spindle 6/6
 2 p. 6-way, 4 p. 2-way, 4 p. 3-way, long spindle 3/6
 3 p. 4-way, 1 p. 12-way, long spindle 3/6
 Wave change "MARKIS" 1 water, 6/6; 2 water, 12/6; 3 water 18/-; 4 water 19/6; 5 water 23/-; 6 water 26/6.
TOGGLE SWITCHES. S.F., 2/-; D.P., 3/6; D.P.D.T., 4/-
MORSE KEYS, good quality, 2/6.
SUB-MINIATURE ELECTROLYTICS (15 v.), 1, 2, 4, 5, 8, 25, 50 mid., 100 mid., 3/- each.

EDISWAN TRANSISTORS JUNCTION TYPE P.N.P.
AUDIO XB102, for amplifiers. B.F. XA104 frequency changer up to 4 Mc/s., 18/- to 250 milliwatts in push-pull.
PRICE 10/- XA103 IF amp. etc. up to 2 Mc/s. **15/-**
 Mullard OC44, 26/-, OC45 23/-, Power V15/10p 20/-.

RCS "REGENT" 4 VALVE

"96" RANGE VALVES

KIT PRICE **£6. 6. 0.**

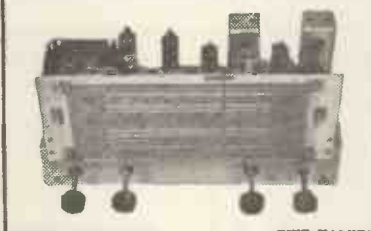
Carr. 4/-.



PRINTED CIRCUIT BATTERY PORTABLE KIT

Medium and long wave. Powerful output from 6in. high Flux Speaker. T.C.C. Printed circuit and condensers. All components of finest quality clearly identified for assembly with full instructions. Osmor Ferrite Aerial and Coils, Rexine covered attache case type cabinet. Size 12in. x 8in. x 4in. Batteries used B126 (L5512 and AD35 (L5040), 10/- extra. Details and instructions 1/9 (free with kit). Mains Unit ready made for above 39/6. Same size as batteries, sold separately.

1960 RADIOGRAM CHASSIS



THREE WAVEBANDS S.W. 18 m.—60 m. **LATEST MULLARD** ECH81, EF89, EBC81, L.W. 800 m.—2,000 m. EL84, EZ83, 12-month Guarantee. A.C. 200/250 v., 4-way switch. Short-Medium-Long-Gram. A.V.C. and Negative Feedback. 4.2 watts. Chassis 13 1/2in. x 5 1/2in. x 2 1/2in. Glass Dial Size 10 x 4 1/2in. horizontal or vertical. Two Pilot Lamps. Four Knobs. Walnut or Ivory. Aligned and calibrated. Chassis isolated from mains.

BRAND NEW £9. 10. 0. Carr. 4/6.

TERMS: Deposit £5/5- and 3 monthly payments of £1. MATCHED SPEAKERS 8in. 17/6; 10in. 25/-; 12in. 30/-.

RECORD PLAYER BARGAINS

4 Speed Autochangers, B.S.R., U.A.8 **£6 19 6**
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 Garrard RC121 Mk. II **£9 19 6**
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THE HI-GAIN BAND 3 PRE-AMP

Cascade circuit using Valve ECC84. 17db gain. Kit 29/6 less power; or 49/6 with power pack. Plans only 6d. Also Band 1 version same prices. (PCC84 Valve if preferred)

TELETRON POCKET RADIO KIT
 Transidyne Superhet Six 6" x 4" x 1 1/2"
 T.C.C. Printed Circuit, internal Ferrite aerial, Rola loudspeaker push-pull output. All parts, cabinet, 6 Ediswan transistors, GEX34 diode. Details 9d. **£9. 9. 0.**

VOLUME CONTROLS 80 ohm Coaxial Semi-air spaced. 1/4in. dia Ideal Band III **6d.** 1 year. All values. Losses cut 50% Post lid. per yard extra. **FRINGE QUALITY AIRSPACED 1/- yd.**

COAXIAL PLUGS 1/- LEAD SOCKETS 2/6
PANEL SOCKETS 1/- **OUTLET SOCKETS 4/6**
BALANCED TWIN FEEDER per yd. 8d., 80 Ω or 300 Ω **TWIN SCREENED BALANCED FEEDER** 1/6 yd., 80 ohm.

ALUMINIUM CHASSIS. 18 s.w.g. Flat, undrilled with 24in. sides, riveted corners and lattice fixing holes, with 24in. sides, 7 x 4in., 4/8; 9 x 7in., 5/9; 11 x 7in., 6/9; 13 x 9in., 8/6; 14 x 11in., 10/6; 15 x 14in., 12/6 and 18 x 16 x 3in., 16/6.

BLACK CRACKLE PAINT. Air drying, 3/1 tin. **CONN. WIRE,** coloured, single or stranded, 2d. yd. **NEON MAINS TESTER SCREWDRIVERS,** 5/- **CORED SOLDER RADIOGRADE,** 4d. yd., 1lb., 2/6. **PAXOLIN 1/15in.** 8in. x 10in., 1/6. **ION TRAPS** 5/-.

PLASTIC RECORDING TAPE

Long Play 7in. reel, 1,700ft. 39/6
 5 1/2in. reel, 1,200ft. 29/6
 5in. reel, 850ft. 19/6
 3in. reel, 225ft. 7/6
 Standard 7in. Reel, 1,200ft. 21/-
 5in. reel, 300ft. 15/6
 "Instant" Bulk Tape Eraser and Head DeFuzzer, 200/250 v. A.C. 27/6. Leaflet, S.A.E.

RECTIFIERS, RMI, 5/-; RM2, 6/-; RM3, 8/-; RM4, 16/-; RM5, 20/-; RM6, 27/6; RM7, 30/-; RM8, 45/-; RM9, 25/-
MINIATURE CONTACT COOLED RECTIFIERS, 250 v. 50 mA., 7/6; 60 mA., 8/6; 85 mA., 9/6; 200 mA., 21/-; 300 mA., 27/6; Full Wave 250 v. 120 mA., 15/-
COILS. Wearite "P" type, 3/- each. Osmor Midget "Q" type add dust core 4/- each. All ranges.
L. and M. T.R.F. with reaction, 3/6.
FERRITE ROD AERIALS. M.W., 9/8; M. & L., 12/6. **T.R.F. COILS.** A/HF, 7/- pair. H.F. **CHOKES,** 2/6.

JASON F.M. TUNER COIL SET, 26/-. H.F. coil aerial coil, Oscillator coil, two I.F. transformers 10.7 Mc/s., Detector transformer and heater chokes. Circuit and component book using four 6AM6, 2/6. Complete kit FM71 with Jason Calibrated dial and 4 valves, 26/5-.
 With new Jason Cabinet, FM72, 30/- extra.

CONDENSERS. New Stock. .001 mid. 7V. T.C.C., 5/8. 20 kV., 9/6. 1 mid. 7kV., 9/6. 100pf to 500pf. Mica, 8d. Tubular 500 v., 0.001 to 0.05 mid. 9d.; 0.1, 1/-; 0.25, 1/6; 0.5, 1/9; 0.1/350 v., 9d.; 0.1/1,000 v., 1/9; 0.1 mid., 2,000 v., 3/6; 0.01 mid., 2,000 v., 1/9.
CERAMIC CONDS. 500 v. 0.3 pf. to 0.01 mid., 9d. **SEVEN MICA CONDENSERS.** 10% 5% to 300 pf., 1/-; 800 pf. to 3,000 pf., 1/3.
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TRIMMERS. Ceramic, 30, 50, 70 pf., 9d., 100 pf., 150 pf., 1/3. 250 pf., 1/6. 600 pf., 750 pf., 1/9. Phillips, 1/- ea.

NEW ELECTROLYTICS. FAMOUS MAKES

TUBULAR	TUBULAR	CAN TYPES
1/350 v. 2/-	50/350 v. 5/6	8/500 v. 3/-
2/450 v. 2/3	100/25 v. 3/6	16/500 v. 4/-
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8/450 v. 2/3	500/12 v. 4/6	100/270 v. 5/6
8/500 v. 2/9	8+8/450 v. 4/6	2,000/3 v. 4/-
16/450 v. 3/6	8+8/500 v. 5/-	5,000/6 v. 5/-
16/500 v. 4/6	8+16/450 v. 5/-	8+16/500 v. 7/-
32/450 v. 5/6	8+16/500 v. 5/6	8+16/2,450 v. 6/6
25/25 v. 1/9	16+16/450 v. 6/6	50/30/350 v. 9/-
50/25 v. 2/-	16+16/500 v. 6/-	64+120/350 v. 11/6
50/50 v. 2/-	32+32/350 v. 4/6	100+200/275/12/6

FULL WAVE BRIDGE/SELENIUM RECTIFIERS. 2.5 or 12 v. 11 amp., 8/9; 2 a., 11/3; 4 a., 17/6; 6 a., 22/6.
CHOKER TRANSFORMERS. Tapped input 200/250 v. for charging at 2, 6 or 12 v., 1 1/2 a., 15/6; 2 a., 17/6; 6 a., 22/6. Charger circuit free. **AMPMETERS,** 4 a., and 5 a., 13/6.

NEW and boxed VALVES 80-day guarantee

1R5	7/6	6L6G	10/6	EA50	1/6	EY51	9/6
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6AM6	5/-	12A6	7/6	ECL50	10/6	PCNR25	8/6
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6BH6	9/6	12AU7	8/-	EF39	5/6	PY80	7/6
6BW6	9/6	12AX7	8/-	EF41	9/6	PY81	9/6
6D6	6/-	12BA6	8/6	EF50	5/6	PY82	7/6
6F06	7/6	12BE6	8/6	EF80	8/-	SP1	3/6
6K6GT	3/6	12K7	6/6	EF86	14/6	UCB41	9/6
6J6	5/6	12Q7	6/6	EF92	5/6	UCB42	9/6
6J7G	6/6	15L6	9/6	EL32	5/-	UF41	9/6
6J7G	6/6	35Z4	7/6	EL41	9/6	UL41	9/6
6K6GT	6/6	80	9/6	EL42	8/6	UY41	8/-
6K7G	5/-	807	5/6	EZ40	7/6	U22	8/-
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"PLUG-IN" 3,000 Type Relay

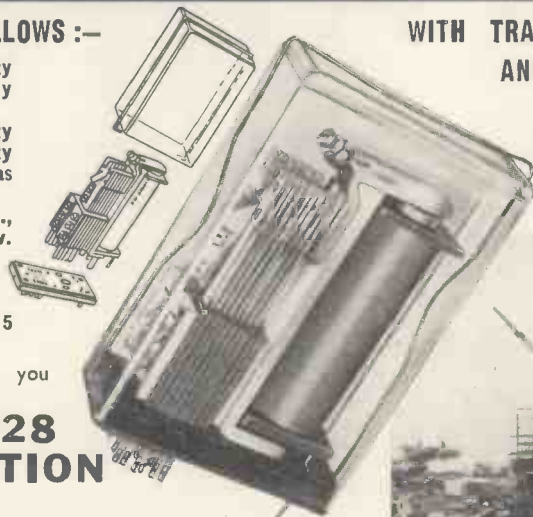
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- 6 Change-overs Light Duty
- 6 Makes or 6 Breaks Heavy Duty
- 2 Change-overs Heavy Duty and 2 Change-overs Light Duty
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- A.C. operation for: 6 v., 12 v., 24 v., 50 v., 110 v. and 250 v. A.C.
- Double Wound Coils
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WITH TRANSPARENT DUST COVER AND PLUG-IN BASE

As supplied exclusively for

BERKELEY POWER STATION



We shall be pleased to see you on our

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I.E.A. EXHIBITION

May 23-38

A.I.D. A.R.B.
ADMIRALTY APPROVED
3000 & 600 TYPE RELAYS

SIZE OF BASE

2 3/4" x 1 1/8" x 1/4"

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89-97, ST. JOHN STREET, CLERKENWELL, E.C.1.
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MORE BARGAINS FROM OUR EXTENSIVE STOCK

POTENTIOMETERS

	Each
6 ohm, small Colvern w/w	1/6
60 ohm, Plessey carbon, linear	1/3
100 ohm, Burco w/w	3/6
270 ohm, Colvern w/w	2/6
400 ohm, 4 watt w/w	1/6
400 ohm, small Colvern w/w	1/6
2K w/w for CR.100	2/6
2.5K Colvern large precision w/w	4/6
3K American w/w, with switch	2/6
3K Burco w/w, instrument	1/6
3K + 50 ohm Colvern tandem	3/-
5K Transistor preset	6d.
10K Colvern w/w	1/3
10K + 10K American ganged type J	2/6
10K + 10K Morganite, ganged carbon	2/-
20K Colvern w/w	1/6
50K Colvern w/w	1/9
50K + 50K Colvern ganged w/w	3/-
75K Colvern precision, new and boxed	4/6
200K Instrument, new and boxed	6/6
500K Carbon	1/6
2M Miniature Slides	6d.
2M Miniature Deaf Aid	1/3

SWITCHES

	Each
(Yaxley)	
2p. 2w. Type A	2/6
2p. 2w. Type B	1/6
2p. 4w.	2/9
3p. 4w.	1/6
3p. 3w., with on/off switch	1/9
4p. 3w.	1/9
2 bank 2p. 2w.	1/6
(Ceramic)	
2 bank 2p. 3w.	2/6
2 bank 2p. 2w.	2/6
(Key)	
Ex. equipment	9d.
2 way, new	1/9
(Micro)	
Press to make or press to break	2/6
Sensitive press to make	2/6
Press to make with reset	2/6
Press to make, roller type	2/6
B. & L. Miniature protective: 0.2A and 0.4A, with cut-out on overload	1/6

	Each
Battery Charger Croc. Clips	1/-
Clarostat Mains Droppers, 250-110V.	2/6
Small Inspection Lamps with on/off switch, lead and plug for dashboard	2/6
Junction Box, GPO 4 way, brand new	1/-
Meters 0-1mA. 2in., square, new	18/6
GPO Jack Plugs	1/9
Bulgin Jack Plugs	1/6

	Each
Meters, 500 microamp., 2in. round	12/6
I.F. Transformers, 100 Mc/s, new	6d.
Hand Mic., Canadian No. 3	3/6
Morse Keys, Canadian	1/-
Ringin Generators	3/6
Mic. Transformers	1/-
American Jack Sockets	1/-
5A. Mains Plugs and Sockets	1/-

VALVES

954 1/3 ea.	9001 1/3 ea.	EF50 (red) 1/3 ea.	KTW61 4/6 ea.
	6H6 1/- ea.	EF50 (silver) 1/- ea.	KTW62 4/6 ea.

POSTAGE & PACKING on all the above, 6d. each.

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Wilkinsons

EST. 1921

METERS GUARANTEED

F.S.D.	Size	Type	Price
50 Microamps	2½in.	MC/FR	70/-
100 Microamps	2½in.	MC/FR	60/-
100 Microamps	3½in.	MC/FR	70/-
500 Microamps	2in.	MC/FR	22/6
500 Microamps	2½in.	MC/FR	37/6
1 Milliamp	2in.	MC/FS	27/6
1 Milliamp	2½in.	MC/FR	35/-
30 Milliamps	2½in.	MC/FR	12/6
100 Milliamps	2in.	MC/FR	12/6
200 Milliamps	2½in.	MC/FR	12/6
500 Milliamps	3½in.	MI/FR	30/-
5 Amperes	2in.	MC/FS	27/6
15 Amperes	2in.	MC/FR	10/6
25 Amperes D.C.	2½in.	MI/FR	7/6
50 Amperes	4in.	MI/FR	65/-
30-0-30 Amp.	2in.	MC/FR	15/6
50-0-50 Amp.	2in.	MC/FS	12/6
10 Volts	2in.	MCR/FS	25/-
50 Volts	3½in.	MC/FS	45/-
300 Volts	2½in.	MI/FR	25/-



Postage on meters 1/6



Complete list available

METER RECTIFIERS. 250µA 1 M.A., 5 M.A., F.W. bridge, 8/6, post 6d.
CROSS POINTER METERS. 2 separate 100 microamp movements, 22/6.
MICROAMMETER. 250 F.S.D. 3½in. F.R. Sangamo Mod. S37. Scaled for valve voltmeter. Circuit available free. 55/-, post 1/6.
UNI-PIVOT GALVANOMETER by Cambridge Instruments, 50-0-50 microamps, dia. 4in. Knife pointer, mirror scale, Complete with leather carrying case. Ideal for laboratory use, £10, carriage 3/-.
PORTABLE VOLTMETER. 0-180 volts A.C./D.C., accuracy within 2%, 8in. mirror scale, knife pointer, in polished case. A precision moving iron instrument at a very low price, £4/19/6, post 3/6.
RADIOACTIVITY MEASURING INSTRUMENTS. Philips Type 1092B. A portable self-contained unit in haversack. Scaled 0 to 10 millirontgens per hour, using Mullard Geiger Counter MX115, £16/10/-, cge. 15/-.
WHEATSTONE RESISTANCE BRIDGE 1 to 10,000 ohms, plug type, £5, carriage 7/6.
OSCILLOSCOPE No. 11 with high-class amplifier. All normal controls 230 volts. £12/10/-, carriage 15/-.
AVO TEST BRIDGES. 220/240 volt A.C. Measure capacities from 5 pf. to 50 mfd. and resistances from 5 ohms to 50 megohms. Valve voltmeter range 0.1 to 15 volts and condenser leakage test. Full working instructions supplied with instrument. £9/19/6, post 3/-.
WAVE CHANGE INDICATOR UNIT. Admiralty patt. 2415, £7/10/-.
OSCILLOSCOPE. Type 43. With 3½in. C.R.T. 138A, 4-617, 3-VR54, 524, VU120. Brand new with usual controls, power pack and leads. Suitable for 230 volts, £10/10/-, carriage 12/6.
FREQUENCY METERS. 45-55 Cycles per second 230 volts, 6in. dia. Flush Round. Brand new in maker's box, £10/10/-, post 3/6.

RELAYS P.O. TYPE 3000



Built to your own specification
Keen Prices
Quick Delivery
Contacts up to 8-Changeover

MINIATURE RELAYS:

Siemens High Speed Sealed.	H96A	15/6	2Ω	2 C.O.	4184GA	18/6
2.2Ω + 2.2Ω	H96A	15/6	2Ω	2 C.O.	4184GA	18/6
145Ω + 145Ω	H96C	19/6	700Ω	2 C.O.	4184GD	19/6
500Ω + 500Ω	H96D	22/6	2500Ω	1 make	HD4186EE	22/6
1700Ω + 1700Ω	H96E	25/-	2700Ω	2 C.O.	4184GE	21/6
Siemens High Speed Open			180Ω	2 m 2 b	M1087	19/6
100Ω + 100Ω	H85N	15/-	670Ω	4 C.O.	M1092	21/6
850Ω + 850Ω	H85V	15/-	2500Ω	1 C.O.	M1022	22/6
1000Ω + 1000Ω	H95A	17/6	5000Ω	2 C.O.	M1052	25/-

ERICSSON SEALED. Highly sensitive. 7000Ω 1 C O 24 v. 25/-.
 Comprehensive range available from stock.

SWITCHES. 1 hole fixing, 3 amp. 250 volt. 1/6 each, 12/- doz.

RACKS—POST OFFICE STANDARD. 6ft. high with U-channel sides drilled for 19in. panels, heavy angle base, 4ft. 10in. in stock.

LOUDSPEAKERS. AXIOM 150 DUAL CONE 12in. 15 WATTS 15 OHMS, FULLY DUSTPROOF, £7/19/6, POST 7/6. PYE 10in. PORTABLE 3 OHMS 50/-, CARR. 7/6. 3in. ROUND PLESSEY SPEAKER, SEALED TYPE WITH PROTECTIVE GRILLE 19/6, POST 1/6. P.M. ELAC 5in. ROUND, 15/6, POST 1/6.

JACK PLUGS. Cylindrical bakelite screw-on cover, 2 contact 2/6, post 6d.

SOCKETS. One hole fixing for above, 3/6, post 6d.

TERMINAL BLOCKS. 2-way 4/- doz., or box of 50 for 15/-, 3-way 6/- doz., 50 for 22/6, post 1/6.

VARIAC. Type 200 CUH. Infinitely variable 0-270 volts, 2.5 amps. In case with 0-250 voltmeter and 0-1 ammeter with own input and output leads, £12/10/0, carriage 7/6.

VARIAC. Input 230 volts. Output infinitely variable 0-230 volts and 0-270 volts. 9 amps., bench or panel mounting, £15, carriage 12/6.



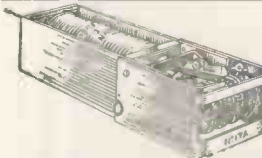
Your Own Telephone

75/-



Telephone Set Type "A." Ringing and Speaking both ways on a four-core cable. Carries the voice loudly and clearly over any distance. Two handsets are supplied as illustrated and the set is complete with Pushes, Buzzers, Battery, Plugs and Sockets. We can supply 4-core PVC cable at 8d. per yard or 2-core at 3d. per yard extra. Price 75/- set, post 3/6.
TELEPHONE SET "TELE-F" This is the best known portable telephone ever made, it has a built-in generator for ringing the other instrument and requires only twin wire between the sets. The set of two instruments and batteries in carrying case, £7/10/0, post 7/6. Twin flat P.V.C. wire 3d. yard.
ROTARY CONVERTERS. Input 12 D.C. Output 230 A.C. 50 cy. 135 watts. In fitted case with variable resistance, 0/300 voltmeter. The ideal job for T.V. and tape recorders where A.C. mains are not available. £10, carr. 15/-. Special connectors, one fitted with 6ft. heavy duty flex and clips for D.C. side. 10/- set, post 1/-. **ROTARY CONVERTER,** input 12 v. or 24 v. D.C., output 230 v. A.C., 135 watts, £8/10/-, carriage 7/6.
BATTERIES. Portable Lead Acid type, 6 volts 125 ampere hours. In metal case 16in. x 18in. x 11in. (Two will make an ideal power supply for our 12 volt Rotary Converters.) Uncharged, £6/10/- each, carriage 15/-. 24 volts 85 ampere, £14 each, carriage 15/-.
GEARED CAPACITOR MOTORS. 220-240 v. 50 cy. 30watts, 300 r.p.m., also spindle for 1425 r.p.m. A very powerful and useful motor for only 75/-, post 3/6.
BARTLETT DRYING OVEN. Interior dimensions 18in. x 15in. x 15in. Automatic temperature control. 230/250 volts A.C. 1500 watts.
BAIRD & TATLOCK HOT AIR OVEN. Interior dimensions 14½in. x 12in. x 12in. Copper framed. Double Jacketed "Stabilec." 110/115 volts 14.8 amps., with adjustable temperature control.
KEY SWITCH LOW CAPACITANCE. 2 C.O. locking, 7/6 each. 4 C.O. Non-locking, 10/6 each. 6 C.O. locking/2 C.O. locking, 17/6 each.
T.C.C. CONDENSERS. 0.1 Mfd., 31 kv. 75/- each, 1 Mfd. 10 kv. 45/- each. **SOLENOIDS** suitable for remote control, mechanical indicators, etc. 12 v. D.C., 400 M.A., 30Ω, 3½in. arm, ½in. movement, 5/- each, post 1/6.

RESISTORS EX STOCK IN QUANTITY WIRE WOUND, HIGH STABILITY CARBON ETC., BEST MAKES AT LOWEST PRICE.



MAGNETIC COUNTERS

Counting to 9999.
 2.6 v. D.C., 15/- each, post 1/6.
 75-230 v. D.C. 15/- each, post 1/6.
HIGH SPEED TYPE No. 100c. 35/-, post 1/6.
HIGH SPEED COUNTER with zero reset, 45/-, post 1/6.

VEEDER-ROOT MAGNETIC COUNTER. General purpose type with zero reset. 800 counts per minute up to 999,999. 48 volt D.C. 55/-, post 2/6.
THERMOSTAT SATCHWELL, 12in. stem 0/250 volt A.C./D.C. 15 amps. A.C. 10 to 90 degrees cent. 25/-, post 2/6.
ROOM THERMOSTAT. Adjustable between 45 and 75 deg. Fahr., 250 v. 10 amp. A.C. Ideal for greenhouses, etc., 35/-, post 2/-.

THIS MONTH'S SPECIAL OFFER.

TRUVOC LOUD HAILERS in slope wood front case with 180 line transformer and condenser. Impedance 7.5Ω capacity 8 watts. Complete with hand power microphone with built-in switch 27/-, post 5/6.

MULTI RANGE TESTMETER

20,000 ohms per VOLT
TAYLOR MODEL 127A
HIGH SENSITIVITY
POCKET SIZE!
 Performance equal to a high priced instrument.

20 Ranges
 D.C. Current 50µA, 1 mA. 10 mA, 100 mA, 1 Amp.
 Volts D.C. 0.3, 2.5, 10, 25, 100, 250, 1,000.
 Volts A.C. 10, 25, 200, 250, 1,000.
 3 Resistance Ranges from 0-20 meg-ohms.
 40µA Meter 3½ in. arc. Accuracy D.C. 3% A.C. 4%, Ohms 5%.
 Dimensions 5½ x 3½ x 1½ in.
 Weight 14 oz.

Price: £10.0.0 Post 2/6.



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3-34 LISLE STREET, LONDON, W.C.2

UNIVERSAL AVOMETER MODEL "D"

D.C. VOLTS	A.C. VOLTS	D.C. Current	A.C. Current
150 mv.	7.5 v.	15 ma.	75 ma.
300 mv.	15 v.	30 ma.	150 ma.
1.5 v.	75 v.	150 ma.	750 ma.
3 v.	150 v.	300 ma.	1.5 amp.
15 v.	300 v.	1.5 amp.	7.5 amp.
30 v.	600 v.	3 amp.	15 amp.
150 v.	750 v.	15 amp.	Resistance
300 v.	1,500 v.	30 amp.	1,000Ω
750 v.			10,000Ω
1,500 v.			

Supplied reconditioned as new, with internal battery, instructions and leads £8/19/6 each. P/P. 3/6.



WESTON MODEL 772 TESTMETER

A.C. VOLTS	D.C. CURRENT	A.C. CURRENT
2.5 v.	100 micro/a.	500 ma.
10 v.	1 ma.	1 amp.
50 v.	10 ma.	5 amp.
250 v.	50 ma.	RESISTANCE
1,000 v.	100 ma.	100 ohms
D.C. VOLTS	500 ma.	1,000 ohms
2.5 v.	OUTPUT METER	100k. ohms
10 v.		10 megohms
50 v.		
250 v.		
1,000 v.		

Supplied In perfect working order complete with internal batteries. £7/10/- P/P. 4/-.



BRAND NEW RCA EXTENSION LOUDSPEAKERS



Bin., 3 ohm Quality Speaker mounted in attractive black crackle case to match AR88 Receivers, etc.
45/- each. P/P 3/6.

8-RANGE SUB-STANDARD D.C. AMMETERS



Ranges 1.5, 3, 7, 15, 30, 60, 300 and 450 amps. 8in. mirror scale. Meter housed in polished teak case. Supplied complete with all shunts and leather carrying case. £15 each. P/P. 7/6.

FIELD TELEPHONES TYPE F. Generator

bell ringing. Supplied complete with batteries fully tested and complete with wooden carrying case 59/6 each. P/P. 3/6. 5/- pr.



PORTABLE PRECISION VOLTMETERS

Brand new instruments by famous manufacturer. In polished teak case. Moving iron instrument reading A.C. or D.C. volts on 2 ranges 0-160 v. or 0-320 v., 8in. mirror scale. Accuracy within 2%. £5/19/6 ea. P.P. 3/6.



METER BARGAINS

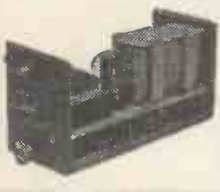
25 microamp D.C. M/C flush rd. 2 1/2in.	69/6
25 microamp D.C. M/C. proj. rd. 2 1/2in.	59/6
50 microamp D.C. M/C. proj. rd. 2 1/2in.	49/6
100 microamp D.C. M/C. flush rd. 3 1/2in.	62/6
500/0/500 microamp. D.C. M/C. proj. rd. 2 1/2in.	19/6
1 milliamp D.C. M/C. flush sq. 2in.	22/6
1 milliamp D.C. M/C. flush rd. 2 1/2in.	25/-
1 milliamp D.C. M/C. flush rd. 3 1/2in.	50/-
1 milliamp D.C. M/C. flush sq. 4in.	69/6
200 milliamp. D.C. M/C. flush rd. 2 1/2in.	9/6
15 amp. D.C. M/C. Proj. rd. 2"	8/6
30 amp. D.C. M/C. flush rd. 2 1/2in.	9/6
15 volt D.C. M/C. flush rd. 1 1/2in.	10/6
120 volt D.C. M/C. flush rd. 3 1/2in.	32/6
300 volt A.C. M/L. flush rd. 2 1/2in.	25/-
300 volt A.C. M/C. rect. flush rd. 2 1/2in.	25/-
500 volt A.C. M/L. flush rd. 2 1/2in.	25/-

DON Mk. 5 FIELD TELEPHONES

Ideal for all inter-communication. Buzzer calling. Supplied fully tested, complete with batteries and instructions. 39/6 each, P/P. 3/6 ea., 5/- pr.



EDDYSTONE MAINS POWER PACKS



200/250 volts input. Output 175 volts 60 mA. and 12 volts 2.5 amps. Double choke and condenser smoothed. 5Z4 rectifier. Supplied as new and unused. 22/6 each. P/P. 3/6.

RCA PLATE TRANSFORMERS

Input 200/250 volts. Output 2,000/0/2,000 volts 500 mA. tapped 1,500/0/1,500 volts. Supplied brand new boxed, £6/10/- each, carriage 10/-.



BRAND NEW MEDRESCO HEARING AIDS



Fully tested, complete with earpiece, all necessary leads and battery pouch. Incorporates three sub-miniature valves and sensitive crystal microphone. Price only 32/6 each, plus 1/- P. & P. Batteries 5/- extra.

MARCONI TYPE TF340 OUTPUT POWER METERS



Meter calibration 50 MW/17DB F.S.D. Meter multipliers, 0.1-1-10-100. Impedance values, 25-30-40-50-60-80-100-125-150-200 ohms. Impedance multipliers, 0.1-1-10-100. Perfect condition. £9/19/6 each, 7/6 carriage.

FIELD TELEPHONES TYPE L. Generator



bell ringing. Light and very portable. Ideal for all installations. Supplied complete with batteries, fully tested. As new, 59/6 each. P/P. 3/-, 5/- pr.

PARMEKO TABLE TOP TRANSFORMERS



Input 230 v. 50 c/s. Output 620/550/375/0/375/550/620 volts 250 mA. Also 2.5 v. 3 amp. windings Size 6 1/2 x 6 1/2 x 5 1/2 in. Brand new only, 45/- each. P/P. 5/-.




COSSOR 339
DOUBLE BEAM
OSCILLOSCOPES

Operation 110/200/250 volts A.C.
 Ten position time base, 6 cps. to 250,000 cps. Amplifier 10 cps. to 2,000,000 cps. Perfect working order.

ONLY £15 EACH
 Carriage 10/-.

G.E.C. SELECTEST MULTI-RANGE TESTMETERS



D.C.	A.C.	D.C.	A.C.
Volts	Volts	Current	Current
150 mv.	7.5 v.	15 ma.	75 ma.
300 mv.	15 v.	30 ma.	150 ma.
1.5 v.	75 v.	150 ma.	750 ma.
3 v.	150 v.	300 ma.	1.5 amp.
15 v.	300 v.	1.5 amp.	7.5 amp.
30 v.	600 v.	3 amp.	15 amp.
150 v.	750 v.	15 amp.	Resistance
300 v.	1,500 v.	30 amp.	1 K. ohm
750 v.			10 K. ohm

Incorporated overload trip and special safety interlocking switches. Supplied in perfect condition with leads and battery at £7/10/- each. P/P. 3/6.

MARCONI TF410C VIDEO OSCILLATORS. Ranges 20 cps. to 30,000 cps. and 30 kc/s. to 5 Mc/s. Variable attenuator. 200/250 v. A.C. Reconditioned, perfect order. £35 each.

MARCONI TF-373 UNIVERSAL IMPEDANCE BRIDGE. Reconditioned to makers' spec. 1,000 c/s. Ranges: 100H. 100 mhd. 1 MEG. 100 Q. 200/250 v. A.C. operation. £35 each.

MARCONI STANDARD SIGNAL GENERATOR TF-144G. 85 kc/s. to 25 Mc/s. Output 1 microvolt to 1 volt. 200/250 volts A.C. operation. Reconditioned to maker's spec. £55 each.

PHOTO VOLTAGE AMPLIFIERS. These special units contain a 1 microamp. Tinsley mirror galvo and a double selenium photo cell. Brand new, £9/19/6 each. P/P. 7/6.

MARCONI TF-329 "Q" METERS. Range 0 to 500 Q. Frequency 50 kc/s. to 50 Mc/s. 200/250 volts A.C. operation. Reconditioned to maker's spec. £65 each.

MARCONI TF-428 B/I. VALVE VOLT-METERS. 5 ranges A.C. and D.C. 1.5, 5, 15, 50 and 150 volts. Complete with internal H.F. probe. Operation 200/250 volts A.C. Brand new, £17/10/- each. P/P. 10/-.

AMERICAN SUPER LIGHTWEIGHT HEADSETS. Res. 50 ohms. Brand new, 15/- P/P. 1/6.

SOUND-POWERED TELEPHONE HANDSETS. No batteries required. 15/- each. P/P. 1/6.

LEACH 12 VOLT AERIAL C/OVER RELAYS. Double pole, 7/6 each. P/P. 9d.

MUIRHEAD PRECISION STUD SWITCHES. 4 bank, 4 pole, 24 positions. New, boxed, 17/6 each. P/P. 1/3.

CR.100 SPARES KITS. Contains 15 valves, resistors, pots, condensers, output trans., etc All brand new, 59/6 set. P/P. 3/6.

24 AMP. VARIAC TRANSFORMERS. 230 v. input. Variable output 185 to 250 volts. Can be used reversely giving 230 volts out with variable input. £12/10/- P/P. 10/-.

1,000 WATT MAINS ISOLATION TRANSFORMERS. 230 to 230 volts. Heavy duty, ex-Admiralty. New, boxed, £5 each. P/P. 10/-.

750 WATT AUTO TRANSFORMERS. Tapped from 110 to 230 volts. Fine heavy duty type, 69/6 each. P/P. 5/-.

AR.88 WAVECHANGE SWITCH ASSEMBLY. Brand new with screens, 17/6 each. P/P. 2/6.

MARCONI TF-517 SIGNAL GENERATORS. 10-18 Mc/s; 33-58 Mc/s; 150-300 Mc/s. 200/250 v. A.C. operation. 65/- each. FOR CALLERS ONLY.

24 VOLT ROTARY CONVERTERS

Input 24 volts D.C.
 Output 230 volts A.C. 50 cycles, 100 watts. Housed in metal carrying case with inlet/outlet plugs.
 Brand new, 92/6 each. P/P. 7/6.



R.1155 RECEIVERS

Standard Model B with improved geared drive, perfect order, £8/19/6 each, 7/6 P/P. Trawler Band Model L or N, £12/19/6 each. P/P. 7/6. Combined Power Pack and Audio Output Stage suit either model, 85/- extra.

ROTARY CONVERTERS

12 v. D.C. input 230 volt A.C. 150 watts 50 cycles output. Housed in wooden case and fitted with voltage control slider resistance switch, plugs and A.C. mains voltage output check meter. Supplied in perfect condition, individually tested £9/19/6 each. P/P. 10/-.



MINE DETECTORS No. 4a

Complete equipment comprises Search Head, Amplifier Headset, Control Box, Telescopic Rods for Search Head, Search Head Test Unit and Test Depth Measure and Haversack. Operation is from a standard 60 v./1.5 v. combined dry battery. The unit will detect ferrous or non-ferrous metals to a depth of 24in. giving maximum signal but can be used at greater depths giving lower output. Ideal for tracing underground pipes or cables and any hidden metallic objects. Complete equipment supplied brand new in original transit cases complete with circuit and operating instructions.




PRICE
99/6 EACH
 Carriage 10/6.

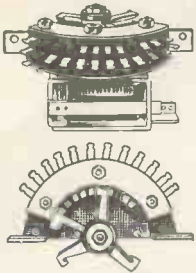
BC 221 HETERODYNE FREQUENCY METERS

125 kc/s to 20 mc/s

Complete with all valves, crystal, headset and instruction book, but less calibration charts. 100% condition.

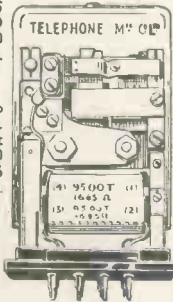
SPECIAL PRICE **£14-10-0**
 each
 Carriage 7/6 extra.



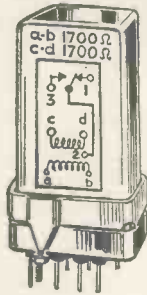


MINIATURE UNISELECTOR SWITCH. Two banks of ten plus home contacts one bank continuous of normal. 30 ohm coil for 24 volt operation. Brand new, manufacturer's packing. Price 22/6 each. P. & P. 2/6. As illustrated.

NEW CARPENTER'S TYPE POLARISED RELAYS. 2 x 9,500 turns at 1,685 ohms. Price 22/6 each. P. & P. 1/-. Carpenter's, similar to above, but type 5A48. Coils 1 x 3200 turns at 100 ohms and 1 x 2000 turns at 145 ohms, 22/6 each. P. & P. 1/-. Bases for same 2/6.



SIEMENS H.S. RELAY. Very latest type, sealed. H9E. 1,700 ohms. plus 1,700 ohms, single C.O. contacts. Brand new with fixing clip. In maker's cartons. Price 16/6 each, plus 1/- P. & P. Siemens sealed similar relay to above, but 2.2 ohms plus 2.2 ohms. Minus clips, 12/6 each. Plus 1/- P. & P.



MINIATURE MOVING COIL DIFFERENTIAL RELAY. Two coils 350 ohms each. Operating current minimum 140 microamp., nominal 400 microamp, maximum 8 milliamp. One pole two way, or centre stable. Two way contact current 100 mA. at 50 V. A.C. or D.C. Size 1 1/2 x 3/8 x 3/16 in. Price 22/6 each.



A VERY SUPERIOR BRAND NEW RELAY IDEAL FOR MODEL WORK. 7,000 ohms coil. Will pull in at 750 microamp and out at 450 microamp. Change-over. platinum contacts. Vacuum sealed, will therefore not be affected by oil, moisture or water and never needs adjusting. Weight 2 1/2 oz. Price 18/6. P. & P. 1/-.

U.S.A. 27-volt 4-pole CHANGE-OVER RELAYS. Brand new and boxed, 5/6 each. P. & P. 6d.

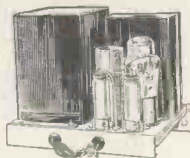
ROTARY RELAY. 12 volt. Heavy duty change-over contacts and one low current for external circuit, plus one break set. Price 7/6. P. & P. 1/6.

NEW WIRE WOUND RHEOSTAT ON CERAMIC. 58 ohm. 50 watt, complete with instrument knob. Price 8/6. P. & P. 1/6.

W. W. RHEOSTAT. New. 3.5K or 5K 25 watts. Price 7/6. P. & P. 1/6.

EX P.O. MAGNETIC COUNTER. 3 ohms type for 4 1/2 volt D.C. operation. Price 6/6 each. P. & P. 1/-.

AS ABOVE 500 ohm for 24/36 volt D.C. operation. Price 6/6 each. P. & P. 1/-.



MAINS POWER SUPPLY UNITS Potted and sealed transformer and choke by famous maker. Mounted on metal chassis 6 1/2 x 7 1/2 in., complete with 5Z4 rectifier valve and full smoothing.

Input tapped 220-230-240 volts. Output: 300 V. D.C. at 100 mA. 6.3 V. A.C. at 4.5 amp. 6.3 V. A.C. at 2 amp. Rectifier supply 5 V. A.C. at 3 amp. Very conservatively rated. Price 42/6 plus P. & P. 6/6.

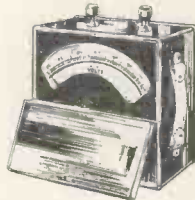
DESK TELEPHONE HANDSETS

Brand new (perfect) complete with two-way calling system (buzzer), internal battery. All ready for simple two-wire connection. Price £3/5/- each, or £6/5/- the pair. P. & P. 3/6 each unit.



BRAND NEW FREQUENCY METERS manufactured by Crompton Parkinson. Calibrated 45 cycles to 55 cycles per second. 6" dial. Panel mounting type. In original manufacturers' boxes. PRICE £10.15.0 each. Postage 3/6.

AUTO TRANSFORMERS. Step up, step down, 110-200-220-240 v. Fully shrouded. New. 300 watt type £2/2/- each. P. & P. 2/6. 500 watt type £3/3/- each. P. & P. 3/9. 1,000 watt type £4/4/- each. P. & P. 6/6.



LABORATORY PRECISION VOLTMETER. Brand new in polished teak case. Moving iron instrument reading D.C. or A.C. 0-160 volt on 8 in. mirror scale. Accuracy 2% £4/19/6 each. P. & P. 3/6.

BRAND NEW SOUND POWER OPERATED EX ADMIRALTY HEAD AND BREAST SETS.

Two such sets connected up will provide perfect intercomm., no batteries required. Will operate up to 1/2 mile. Original manufacturer's boxes. Price 17/6 each, plus P. & P. 2/-; or 32/6 per pair. P. & P. 3/-.

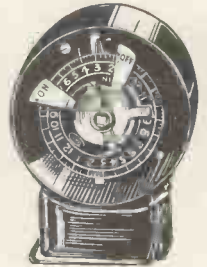


MUIRHEAD PRECISION, 4 bank, 1 pole 24 position Stud Switch. Heavy duty contacts. Brand new, Original boxes. Price 17/6 each. P. & P. 1/-.

CERAMIC PRECISION SWITCH. 2 pole, 6 way, 4 banks. New in manufacturer's boxes. Price 10/6 each. P. & P. 1/6.

MINIATURE INSTRUMENT RECTIFIERS, Bridge Type 1 milliamp. Guaranteed perfect. 7/6 each.

8-day clockwork Time Switch. Contacts 2 1/2 amp., 230 volt, 24 hour phase, 1/4 hour divisions, allow setting for one make and one break to be made every 24 hours. complete with key. Used but guaranteed perfect. Price 27/6 each. P. & P. 1/6.



METERS GUARANTEED PERFECT Charging Types

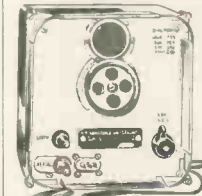
2 1/2 amp. D.C. M.I. 2 1/2 in. fl. rnd.	7/6
5 amp. D.C. M.I. 2 1/2 in. fl. sq.	11/6
7 1/2 amp. D.C. M.I. 3 1/2 in. proj. rnd.	12/6
9 amp. D.C. Hot Wire W.R. 2 1/2 in. fl. rnd	6/6
Voltmeters	
12 v. D.C. M.C. 2 1/2 in. proj. rnd.	8/6
20 v. D.C. M.C. 2 in. fl. sq.	9/6
25 v. D.C. M.C. 2 in. fl. rnd.	7/6
30 v. M.I. 3 in. proj. rnd.	10/6
40 v. M.C. 2 in. fl. sq.	9/6
300 v. A.C. M.I. 2 1/2 in. fl. rnd.	22/-
400 v. A.C. M.I. 4 1/2 in. fl. rnd.	35/-
Milliammeters	
1 mA. M.C. 2 1/2 in. fl. rnd.	25/-
2 mA. M.C. 2 1/2 in. fl. rnd.	14/6
500 mA. M.C. 2 1/2 in. fl. rnd.	9/6
Microamp.	
50 microamp., scaled 0-100, M.C. 2 1/2 in. fl. rnd.	42/6
200 microamp., M.C. 2 1/2 in. fl. rnd. (calibrated 0-50).	29/6
50 microamp. 2 1/2 in. squares, idefitting 3 scales	35/-
500 microamp. M.C. 2 in. rnd.	16/6

Postage on all meters 1/- each.

Miniature latest type moving coil 0-5 milliamp meter, 1 1/2 in. diameter, flush fitting complete with fixing clip. Price 17/6. P. & P. 1/-.



CRYSTAL CALIBRATOR No. 10.



A crystal controlled 4-valve high-grade instrument in the same category as the famous B.C.221. Directly calibrated, does not require cross reference or charts - functions as follows: (1) A crystal controlled oscillator which provides fixed frequency signals of 500 KC and all harmonics of 500 KC to beyond 10 Meg. and up to 30 Meg. (2) A variable oscillator from 250 KC to 5 KC, this enables all intermediate frequencies between 250 Kc/s. and 30 Meg. to be produced and modulated. Supplied complete with 3 spare valves, all leads and maker's instruction book in carrying haversack. The complete outfit is brand new - repeat NEW. Price: £4/19/6. Carr. 3/-.

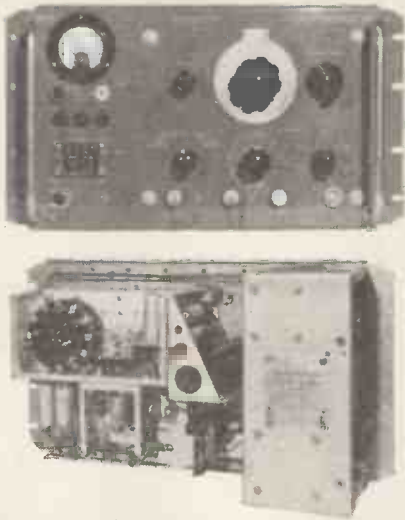
TWELVE PLATE F.W. BRIDGE CONNECTED RECTIFIER mounted on 200/250 volt A.C. input transformer. Output 36/40 volt D.C. at 1.2 amps. New, perfect. Price 16/6. P. & P. 3/6.



SOLENOID OPERATED MAGNETIC RELAY. Type 5CW/3945, 4 pole changeover, 10A contacts 24v. operation. Brand new 13/6 P. & P. 1/6.

WE ARE EXPERTS AT OVERSEAS PACKING & SHIPPING! PERSONAL CALLERS ONLY: 8 Little Newport Street, London, W.C.2. Tel: GER 0576
SERVICE TRADING Co. ALL MAIL ORDERS: (Early Closing Thursday.)
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A few with superficial damage offered unguaranteed and less cables, etc. for £12.10. plus 15/- carriage.

Another striking Proops buy gives anyone a chance to use professional gear and do some serious alignment work with stable frequencies and accurate signal levels right up through FM and all the TV channels to the beginning of UHF.

PRECISION SIGNAL GENERATOR CT53

A modern laboratory standard instrument by Wayne Kerr, British Communications Corporation, H. C. Atkins Laboratories, etc., made as common radio test equipment for the Navy and R.A.F. (Still in current use and undoubtedly in the £150 class).

FEATURES

- Vernier tuned, Triple screened, 6-band coil turret covering 8.9 to 300 Mc/s with 72 ohm output from 100 mV to 1μV.
- Precision decade ladder and silver slide wire attenuator calibrated in voltage and 0-90 db.
- Variable carrier level monitored by cathode follower and VTVM.
- CW or modulated 30% by 1000 c/s sine or square wave (variable mark/space ratio.)
- External mod by sine wave from 50 c/s to 10 kc/s or pulses down to ½ μ Sec.
- Seven B7G valves, Potted 'C' core transformers, Paper capacitors, Stabilised HT.
- Selected spare oscillator, pre-aged spare monitor, 100 μA meter.
- Mains, HT, Bias and Filament supplies fully RF filtered.
- Combined cabinet/rack mounting case, Pressure sealed, Desiccator, Panel mains voltage adjustment, Triple fused, in fact, "the lot"!

Offered straight from Service use, complete with calibration book, cables, circuit diagram and principal technical information, checked serviceable and fully guaranteed.

£17.10.0 plus 15/- for careful packing and carriage.

PROOPS

BROTHERS LTD. 52 Tottenham Court Rd., London, W.1
 Head Office and Mail order enquiries. LAngham 0141
 Shop hours 9 a.m. to 6 p.m. Thurs. 9 a.m. to 1 p.m. OPEN ALL DAY SATURDAY.

DEAF AID VEST POCKET RADIO 55/-

Three modern low-consumption miniature valves in a very sensitive hi-fidelity circuit that only requires the addition of a simple tuned input circuit and a crystal diode to bring your favourite programme in loud and clear. Pre-wound aerial coil on hi-Q ferrite rod. Conversion takes less than an hour without previous experience and using only ordinary tools. Brand new in original pack with latest type crystal earpiece and detachable plastic ear mould plus all conversion parts. Sensitive crystal microphone suitable for immediate use with tape recorder becomes spare on conversion to radio. Kit of parts sold separately—Deaf Aid 40/-, Conversion parts 15/-, batteries 5/- post free.

ETCH YOUR OWN PRINTED CIRCUIT KITS 21/- post free

Each contains over 60 sq. in. of laminated board and sufficient chemicals to make dozens of printed circuits, plus comprehensive instruction book giving advice and examples on translating theoretical circuits into layouts ready for etching. High-quality materials—completely safe to handle—carefully prepared to ensure fine definition and uniform results without laboratory control.

£10 GEIGER COUNTER

Circuit embodies U.K.A.E.A. patent. Specially moulded case. Currently being supplied throughout the world. Three ranges—highly sensitive—light—portable—visual and audible response—plus output socket. Ideal for introduction to radiation measurement and nucleonic circuitry. Specially written 40-page instruction manual supplied. Batteries £2/15/3 extra.

KIT OF PARTS £4/17/6

Identical parts. Guaranteed performance. Manual and printed circuit plates for battery pack supplied (assembled pack £2/15/3 extra). Fully illustrated assembly instructions. Spares and service permanently available.

3A-ARR-2X MIDGET 12v RECEIVERS

Beautifully made, compact, double-conversion, aircraft set. Dynamotor powered, 10 B7G valves, seven 9001, three 6AK5, and 12A6 output into 300 or 4,000 ohms. Three RF stages tuned over 234-258 Mc/s from panel knob by lockable calibrated dial which operates ganged inductors. Two IF stages, oscillator, modulator, 1st and 2nd detectors and beat frequency control stages. Six switched channels are provided between the 1st detector and oscillator stages (each with externally accessible tuning) all switched from front panel or by flexible cable from neat remote control box which also provides volume control, OFF-NAV-VOICE switch and BFO pitch control. By feeding aerial to alternative panel socket provided (instead of input) coil inductors can be set to a different MEDIUM WAVE station for each channel. Potential car radio, consumption only 2½ amps. BRAND NEW complete with valves, control box, three adaptors, and circuit diagram . . . 55/- plus 7/6 carriage.

VARIABLE SPEED HYDRAULIC GEARBOX

This specially made oil-filled casing houses a hydraulic torque conversion unit originally precision made by Westinghouse from high quality materials for the U.S. Government at an acquisition cost exceeding £150 each. Highly suitable for lathe head drive, workshop variable speed power take-off, etc.

Basically the unit is a back-to-back mounted, oil submerged, variable displacement hydraulic pump (input shaft) feeding a reversible hydraulic motor (output shaft) so that variation of the pump displacement by manual control gives very fine selection of output speed from zero up to 6% below input speed while a changeover valve in the supply lines to the motor provides instantaneous reverse at any speed. Recommended input speed 500-1,000 r.p.m., maximum power 1½ h.p. Both shafts ½ in. dia. with Woodruff key.

Tested and fully guaranteed, supplied complete with technical data and performance curves for the remarkable price of £16 only, carriage paid. Size 8 x 10 x 12in.

LOW-VOLTAGE, HALOGEN-QUENCHED, GEIGER-MUELLER TUBES 25/- post free

Working voltage 400-450. Highly sensitive. Effective length 11.8 cm. Background count 90/minute. Response 30,000 counts/minute. 80-volt plateau. Standard British 4-pin base, stainless iron electrode. Ideal for basic experimentation and instructional demonstration. Circuits of simple all-transistor and conventional valve counter circuits supplied on request with each tube. Brand new, individually tested, fully guaranteed.

DESK MICROPHONES

High-grade crystal desk microphone in contemporary styled diecast case, originally designed for use with world renowned recording equipment. Incorporates sliding note tray in base and rubber mounting feet; attractive green crackle finish. Fitted with two heavily chromed flap type switches for Record/Playback operation, and complete with multi-cored cable and plug. Brand new, boxed.



PROOPS THE WALK-AROUND STORE

R.S.C. HI-FI TAPE RECORDER KIT

OR DEPOSIT 3 GNS. and 18 monthly payments of 45/9. Cash price if settled in 3 months.

Build a high quality recorder in the £70 class for only

25½ GNS. Carr. 17/6.

Can be assembled in ½ to 1 hour.

INCORPORATING THE LATEST COLLARO STUDIO TAPE TRANSCRIPTION, THE LINEAR LT45K HIGH QUALITY TAPE AMPLIFIER. A HIGH FLUX 7 x 4in. LOUDSPEAKER, Reel of Best Quality TAPE. Spare Tape Spool, a Portable Cabinet, size approx. 18 x 13 x 9in., finished in two-tone rexine, and connection diagram for wiring amplifier to transcription.

FEATURES INCLUDE

- ★ 3 SPEEDS. ★ FREQUENCY RESPONSE 50-11,000 c.p.s. ★ SWITCHED NEGATIVE FEEDBACK EQUALIZATION FOR EACH SPEED. ★ OUTPUT 4 WATTS. ★ MAGIC EYE RECORDING LEVEL INDICATOR. ★ 3 MOTORS. Fast rewind. ★ TAPE MEASURING AND CALIBRATING DEVICE. ★ TAKES FULL 7in. DIAMETER REELS OF TAPE. ★ NEGLIGIBLE HUM. ★ ENTIRELY EFFECTIVE AUTOMATIC ERASURE.

Full descriptive leaflet supplied on receipt of S.A.E.



HI-FI 10 WATT AMPLIFIERS

BRAND NEW BUT IN SLIGHTLY SOILED CONDITION

£5-19-9 Carr. 7/6

A REMARKABLE OPPORTUNITY
Push-pull output. Latest high efficiency Mullard valves. Dual separately controlled inputs, for mike and gram. Separate bass and treble controls. High sensitivity. Output for 15 ohm loudspeaker. Guaranteed, tested, and in perfect working order.

VALVES! Full range at really competitive prices! All guaranteed!

SUPERHET RADIO FEEDER UNIT

Design of a high quality Radio Tuner Unit (specially suitable for use with any of our Amplifiers). A Triode Heptode P/charger is used. Pentode I.F. and double Diode 8-cond Detector, delayed A.V.C. is arranged so that A.V.C. distortion is avoided. The W. Ch. Sw. incorporates Gram-position. Controls are Tuning, W. Ch. and Vol. Output will load most Amplifiers requiring 500 mV. input depending on A.C. location. Only 250 v. 15 mA. H.T. and L.T. of 6.3 v. 1 amp. required from amplifier. Size of unit approx. 9-6 7/8in. high. Send S.A.E. for illustrated leaflet. Total building cost is £4/15/-. Point-to-Point wiring diagrams and instructions 2/6.

WAYNE KERR SIGNAL GENERATORS Type CT58. 3.9 to 300 megacycles. Suitable for aligning V.H.F. Radio or TV. receivers. Output 1 microvolt to 10 millivolts. Worth approx. £100. Few only at 19 Gns. with charts.

METERS

0-50 micro-amperes, 2 1/2in. scale, scaled 0-100. 39/6.

0-500 micro-amp., 3 1/2in. scale, scaled in decibels. 59/6.

Ferranti Multimeters, D.C. and A.C., complete in carrying case, 59/6.

ACOS HI-FI CRYSTAL 'MIKES'

Mic 40 hand or Desk type

27/9 (Listed) 45/- 39-1 Stick type

39/6 (Listed) 5 Gns. Limited number.

R.S.C. BATTERY TO MAINS CONVERSION UNITS

Type BM1. An all-dry battery eliminator. Size 5 1/2 x 4 1/2 x 2in. approx. Completely replaces batteries supply 1.4 v. and 90 v. where A.C. mains 200-250 v. 50 c/s. is available. Suitable for all battery portable receivers requiring 1.4 v. and 90 v. This includes latest low consumption types. Complete kit with diagram 39/9 or ready for use 46/8.

Type BM2. Size 8 x 5 1/2 x 2 1/2in. Supplies 120 v. 90 v. and 50 v., 40 mA. and 2 v. 0.4 a. to 1 amp., fully smoothed. THEREBY COMPLETELY REPLACING BOTH H.T. BATTERIES AND H.T. 2 v. ACCUMULATORS when connected to A.C. mains supply 200-250 v. 50 c/s. SUITABLE FOR ALL BATTERY RECEIVERS normally using 3 v. accumulator.

Complete kit with diagrams and instructions. 49/9 or ready for use 59/6.



BUILD A PORTABLE BATTERY OPERATED RECORD PLAYER FOR ONLY £6/19/6. Portable Cabinet, Garrard 45 r.p.m. motor and pick-up unit, all parts for transistor amplifier, and circuit diagrams. Parts sold separately.

THE SKY FOUR T.R.F. RECEIVER



A design of a 3 valve 200-250 v. A.C. mains L. and M. wave T.R.F. receiver with selenium diode rectifier. For inclusion in cabinet illustrated or walnut veneered type. It employs valves 6K7, 6F6, 6BE and is specially designed for simplicity in wiring. Sensitivity and quality are well up to standard. Point-to-Point wiring diagram. Instructions and parts list 1/9. This receiver can be built for a maximum of £4/19/6 including cabinet. Available in brown or cream bakelite or veneered walnut.

EXTENSION SPEAKERS. Handsome walnut veneered cabinets. All standard 2-3 ohms. 6 1/2in. 29/9; 8in. 35/9.

PARMEKO RE-ENTRANT LOUDSPEAKERS. Horn type for factory or outdoor use. Highly efficient, will handle up to 10 watts. Matching 15 ohms or 200 ohms. Brand New. Boxed. 59/6. Carr. 5/6.

R.S.C. A12 STEREO AMPLIFIER KIT

4 GNS.

A complete kit of parts to construct a good quality 3 + 3 watt (total 6 watt) stereo amplifier providing really life-like reproduction. Suitable for use with all stereo pick-up heads at present available. Ganged volume and tone controls. Preset balance control. Outputs for matched 2-3 ohm speakers. For 200-250 v. A.C. mains Astonishing value.

W.B. "STENTORIAN" HIGH FIDELITY P.M. SPEAKERS

HF1012, 10 watts, 15 ohms (or 3 ohm) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this unit with an amazing performance. £4/10/9. Please state whether 3 ohm or 15 ohm required.

SELENIUM RECTIFIERS

We can quote special prices for quantities of 12 to 10,000 of most types. Special types made to order.

L.T. Types	H.T. Types H.W.
2/6 v. 8 a. h.w. ... 1/9	120 v. 40 mA. 3/9
6/12 v. 1 a. h.w. ... 2/9	250 v. 50 mA. 3/11
Following F.W. (Bridge)	250 v. 60 mA. 4/11
6/12 v. 1 a. 3/11	250 v. 80 mA. 6/11
6/12 v. 2 a. 6/11	250 v. 250 mA. 12/9
6/12 v. 3 a. 9/9	Contact Cooled
6/12 v. 4 a. 12/3	250 v. 80 mA. 6/11
6/12 v. 5 a. 14/6	250 v. 75 mA. 8/11
6/12 v. 6 a. 15/6	F.W. (Bridge)
6/12 v. 10 a. 25/9	
6/12 v. 15 a. 35/9	

JACK PLUGS. Standard type complete with 4ft. screened lead. 1/11 each.

JUNCTION TRANSISTORS. R.F. Type 11/6, Audio type 5/9. Power type Goltop V15102 2 watts. 17/9. OC71, 10C4, OC72 17/-. XB102 10/-. XB104 10/-. XA101, OC44, XA102 17/6, and many other types.

RECORDING HEADS. Baird Record Playback and Erase. (Housed in one container.) 9/6 pr.

All Battery Chargers and Kits for 200-230-250 v. 50 c/s. A.C. Mains

HEAVY DUTY CHARGER KIT

6/12 v. variable charge rate up to 6 amps. Consisting of Mains Trans., F.W. (Bridge) Selenium Rectifier, 0.7 amp. meter, multi-position switch with knob, fuses, fuse-holders, panels, plugs, and circuit. Only 59/6 Post 4/6.

TANNAY RE-ENTRANT LOUDSPEAKERS. 8 watt. 7.5 ohms 19/6 Or a pair for only 35/-

ASSEMBLED CHARGERS

6 v. 1 a. 19/9
6 v. 2 a. 29/9
6/12 v. 1 a. 29/9
6/12 v. 2 a. 38/9
6/12 v. 4 a. 56/9
Above ready for use with mains and output leads. Cases well ventilated and finished in stoved blue hammer. Carr. & pkg 3/6.

CHARGER TRANSFORMERS

200-230-250 v. 50 c/s.
0-9-15 v. 1 a. 12/9
0-9-15 v. 2 1/2 a. 15/9
0-9-15 v. 3 a. 16/9
0-9-15 v. 5 a. 19/9
0-9-15 v. 8 a. 23/9

BATTERY CHARGER KITS

Consisting of Mains Transformer F.W. Bridge, Metal Rectifier well ventilated steel case. Fuses, fuse-holders, grommets, panels and circuit. Carr. 2/9. extra.
6 v. or 12 v. 1 amp. 24/9
As above, with ammeter 32/9
6 v. 2 amps. 25/9
6 v. or 12 v. 2 amps. 31/6
6 v. or 12 v. 2 amps. 42/9 (inclusive of ammeter)
6 v. or 12 v. 4 amps. 53/9
6 v. or 12 v. 4 amps. with variable charge rate selector and ammeter 59/9

CHARGER AMMETERS

0-1.5 amp., 0-3 amp., 0-4 amp., 0-7 amp., 0-25 amp., 0-60 amp. 8/9

ASSEMBLED CHARGER

6 v. or 12 v. 2 amps. Fitted Ammeter and selector plug for 6 v. or 12 v. Louvred metal case, finished attractive hammer blue. Ready for use with mains and output leads. Double Fused. Carr. 3/9. **49/9** As above, but for 3 amp. charging. Only 59/6. Carr. 3/9

ASSEMBLED 6 v. or 12 v. 4 amps.



Fitted Ammeter and variable charge selector. Also selector plug for 6 v. or 12 v. charging. Double fused. Well ventilated steel case with blue hammer finish. Ready for use with mains and output leads. Carr. 5/- Or Deposit 13/3 and 5 monthly payments of 13/3.

As above, but for 6 amp. charging 4 GNS. Carr. 5/-. Or Deposit 16/- and 5 monthly payments of 16/-. The 6 amp. model only is slightly store soiled and is being offered at well below usual price.

VISITORS. Oak and Wearite, synchronous 7-pin, 2 v. 7/9, 6 v. 8/3, 12 v. 4-pin non-synchronous 7/9.

2 v. 16 A.H. EX. GOVT. ACCUMULATORS. New Boxed. Only 5/6 each, 3 for 15/-, plus 3/6 carr.

EX. GOVT. MAINS TRANSFORMERS

All 200-250 v. 50 c/s. input.
Pr. 0-110-200-230-250 v., 275-0-275 v. 100 mA., 6.3 v. 7 a., 5 v. 3 a. 22/9
250 v. 60 mA., 6.3 v. 2 a. 10/11
300-0-300 v. 60 mA. 6.3 v. 2 a. 11/9
265-0-265 v. 150 mA., 6.3 v. 1 1/2 a., 9 v. 3 a., 5 v. 3 a. 29/11
350-0-350 v. 100 mA., 6.3 v. 2 a., 5 v. 2 a. 18/9
0-24-26-28 v. 15 amps. A.C. conservative Govt. rating (marked with D.O. rating after rectification) 69/9. Carr. 15/-
0-10-20-25 v. 24 a. (Govt. rating) 79/6. Carr. 15/-
AUTO 500 watts 0-215-220-225-230-235-240 v. 29/9 Carr. 7/6. 50 watts, 0-110-120-230/250 v. 8/11

D.C. SUPPLY KITS. Suitable for electric trains. Consists of mains trans. 200-250 v. 50 c.p.s.; 12 v. 1 amp. selenium rect. (F.W. Bridge); 3 fuseholders, 2 fuses, change direction switch, variable speed regulator, partially drilled steel case and circuit. Very limited number, 33/9.

EX. GOVT. SMOOTHING CHOKES
200 mA., 3-5 H., 50 ohms. Parmeko 6/9; 100 mA., 5 H., 100 ohms 3/11; 150 mA., 10 H., 50 ohms 9/9; 90 mA., 20 H., 900 ohms 5/9; 120 mA., 12 H., 100 ohms 8/9; 50 mA., 50 H., 1,000 ohms 6/9; 100 mA., 10 H., 100 ohms 6/9; 60 mA., 5-10 H., 250 ohms. 2/11.

EX. GOVT. CASES. Well ventilated, black crackle finished, undrilled cover. Size 14 x 10 x 8 1/2in. high. IDEAL FOR BATTERY CHARGERS OR INSTRUMENT CASE. COVER COULD BE USED FOR AMPLIFIER. Only 9/9, plus 2/9 post.

POWER PACK KITS. Only 18/11. Fully smoothed H.T. output of 250 v. 60 m.a., and L.T. supply of 8.3 v. 1.5 amp. Consisting of Double Wound Mains Transformer 230/250 v. 50 c.p.a. A.C. primary. Selenium Rectifier, Smoothing Choke, Double Electrolytic Condenser, Aluminium Chassis and Circuit.

P.M. SPEAKERS. 2-3 ohm 2 1/2in. Perdio 21/9. 5in. Goodmans 17/9. 7 x 4in. R.A. Elliptical 19/9. 6 1/2in. Rola 19/9. 8in. Rola 19/9. 8in. Goodmans 25 9. 8 x 6in. Elac with high flux magnet 25/9. 10in. R.A. 28/9. 10 x 10in. Elliptical Goodmans 29/9. 12in. R.A. 39/11. 12in. R.A. 9 or 15 ohms. 10 watts, 12,000 lines, 59/6.

TWEETERS, 4in. Plessey, 3 ohms, 18/9. R.A. 15 ohm 25/9.

R.S.C. A10 ULTRA LINEAR 30 WATT AMPLIFIER

HIGH FIDELITY PUSH-PULL UNIT EMPLOYING SIX VALVES. E786, E788, E803, 807, 807, 8Z34. Tone Control. Free Amp. stages are incorporated. Sensitivity is extremely high. Only 12 millivolt minimum input is required for full output. **THIS ENSURES THE SUITABILITY OF ANY TYPE OR MAKE OF MICROPHONE OR PICK-UP.** Separate Bass and Treble controls give both "lift" and "cut" with ample tone correction for long playing records. An extra input with associated vol. control is provided so that two separate inputs such as "mike" and gram, etc., can be simultaneously applied for mixing purposes. **AN OUTPUT SOCKET WITH PLUG IS INCLUDED FOR SUPPLY OF 300 v. 20 mA. and 6.3 v. 1.5 A. FOR A RADIO FEEDER UNIT.** Price in kit form with easy-to-follow wiring diagrams.

ONLY 11 Gns. Or factory built with 12 months guarantee £13/10/6. TERMS ON ASSEMBLED UNITS. DEPOSIT 24/8 and 12 monthly payments of 24/8.

Carr. 10/- Cover as illustrated. Type 807 output valves are used with High Quality Sectionally wound output transformer specially designed for Ultra Linear operation. Negative feedback of 20 D.B. in main loop. **CERTIFIED PERFORMANCE FIGURES ARE EQUAL TO MOST EXPENSIVE TYPES AVAILABLE.** Frequency response ± 3 D.B. 30-20,000 c/s. Tone Controls ± 12 D.B. at 90 c/s. ± 12 D.B. to -5 D.B. at 12,000 c/s., hum and noise 70 D.B. down. Good quality reliable components used. Chassis finish blue hammer. Overall size 12 x 9 x 9 in. approx. Power consumption 150 watts. For A.C. mains 200-250 v. 50 c/s. Outputs for 3 and 15 ohm speakers. **EQUALLY SUITABLE FOR THE CONNOISSEUR OR FOR LARGE HALLS, CLUBS OR OUTSIDE FUNCTIONS, IDEAL FOR USE WITH MUSICAL INSTRUMENTS SUCH AS STRING BASS, ELECTRIC ORGAN, GUITARS, etc. FOR DANCE BANDS, GARRISON THEATRES, etc. etc.** We can supply Microphones, Speakers, etc., at keen cash prices or on terms with amplifiers. **EXPORT ENQUIRIES INVITED.**

FULL RANGE OF LINEAR HIGH FIDELITY AMPLIFIERS ALWAYS IN STOCK.
LINEAR L45 MINIATURE 4/5 W. QUALITY AMPLIFIER. Suitable for use with any record playing unit and most microphones. Negative feedback 12 D.B. Bass and Treble controls. For A.C. mains input of 200-250 v. 50 c.p.s. Output for 2-3 ohm speaker. Three miniature Mullard valves. Size only 6 x 5 1/4 in. high. Chassis fully isolated from mains. Guaranteed 12 months. Only **£5/19/6** Or Deposit 22/- and 6 monthly payments. of 22/- . Send S.A.E. for leaflet.

GL3A MINIATURE 3 WATT GRAM AMPLIFIER
 For 200-250 v. 50 c.p.s. A.C. mains. Overall size only 11 1/2 x 2 1/2 in. Fitted Vol. and Tone Control with mains switch. Designed for use with any kind of single player or record changing unit. Output for 2-3 ohm speaker. Guaranteed 12 months. Only 59/6.

R.S.C. A7 3-4 WATT QUALITY AMPLIFIER. Spec. exactly as A5 below with exception of output valves. Complete kit of valves, dividers and instructions £3/15/-, carr. 3/6.

R.S.C. A5 4-5 WATT ALUM GAIN AMPLIFIER
 A highly sensitive 4-valve quality amplifier for the home, small club, etc. Only 50 millivolts input is required for full output so that it is suitable for use with the latest high fidelity pick-up heads in addition to all other types of pick-up and practically all mikes. Separate Bass and Treble controls are provided. These give full long playing record equalisation. Hum-level is negligible being 71 D.B. down. 15 D.B. of negative feedback is used. H.T. of 300 v. 26 mA. and L.T. of 6.3 v. 1.5 a. is available for the supply of a Radio Feeder Unit or Type Deck amplifier. For A.C. mains input of 200-250 v. 50 c/s. Output for 2-3 ohm speaker. Chassis is not alive. Kit is complete in every detail and includes fully punched chassis (with baseplate) with the blue hammer finish, and point-to-point wiring diagrams and instructions. Exceptional value at only £4/15/- or assembled ready for use 25/- extra, plus 3/6 carriage. Or Deposit 22/- and five monthly payments of 22/- for assembled unit.

R.S.C. TRANSFORMERS. Fully Guaranteed. Interleaved and Impregnated.	
MAIN TRANSFORMER. Primaries 200-250-250 v. 50 c/s. FULLY SHROUDED UPRIGHT MOUNTING	
250-0-250 v. 60 mA., 6.3 v. 2 a., 5 v. 2 a.	17/6
250-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	25/8
300-0-300 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	25/8
350-0-350 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	25/9
350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.	33/9
425-0-425 v. 200 mA., 6.3 v. 4 a., c.t. 5 v. 3 a.	49/9
TOP SHROUDED DROP-THROUGH TYPE	
250-0-250 v. 70 mA., 6.3 v. 2 a., 5 v. 2 a.	16/9
350-0-350 v. 80 mA., 6.3 v. 2 a., 5 v. 2 a.	18/9
200-0-250 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	23/9
300-0-300 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	23/9
300-0-300 v. 130 mA., 6.3 v. 4 a., c.t. 6.3 v. 1 a., suitable for Mullard 610 Amplifier	29/9
350-0-350 v. 100 mA., 6.3 v. 4 a., 5 v. 3 a.	23/9
350-0-350 v. 150 mA., 6.3 v. 4 a., 5 v. 3 a.	29/9
ELIMINATOR TRANSFORMERS. Primaries 200-250 v. 50 c/s.	
120 v. 40 mA., 5-0-5 v. 1 a.	14/9
90 v. 15 mA., 6-0-6 v. 2 a.	8/11
FLAMENT TRANSFORMERS. Primaries 200-250 v. 50 c/s.	
6.3 v. 1.5 a.	5/9
6.3 v. 1.5 a.	7/6
6.3 v. 2 a.	7/9
6.3 v. 3 a.	8/11
6.3 v. 6 a.	17/9

STOP PRESS: All deposits must now be 20% of the cash price.

R.S.C. MANCHESTER, LEEDS & BRADFORD

(LEEDS) LTD.

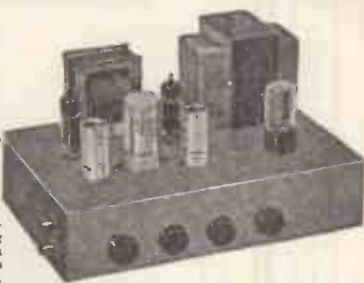
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- 5-7 County (Mecca) Arcade, Leeds, 1.
- 54-56 Morley Street (above Alhambra), Bradford.
- 8-10 Brown Street (Market St.), Manchester, 2.

TERMS: C.W.O. or C.O.D. No C.O.D. under £1. Postage 1/9 extra on all orders under £2, 2/9 extra under £5 unless carriage stated. Trade supplied. Post orders to Mail Order Dept. 29-31 Moorfield Road, Leeds, 12.

HIGH FIDELITY 12-14 WATT AMPLIFIER TYPE A11

PUSH-PULL ULTRA LINEAR OUTPUT "BUILT-IN" TONE CONTROL PRE-AMP STAGES



Two input sockets with associated controls allow mixing of "mike" and gram, as in A10. High sensitivity. Includes 5 valves: EOC83, EOC83, EL84, EL84, 5Y3. High quality sectionally wound output transformer specially designed for Ultra Linear operation and reliable small condensers of current manufacture. **INDIVIDUAL CONTROLS FOR BASS AND TREBLE "LIFT" and "CUT."** Frequency response ± 3 D.B. 30-30,000 c/s. Six negative feedback loops. Hum level 60 D.B. down. **ONLY 23 millivolt INPUT required for FULL OUTPUT.** Suitable for use with all makes and types of pick-ups and microphones. Comparable with the very best designs. **FOR STANDARD or LONG PLAYING RECORDS. FOR MUSICAL INSTRUMENTS** such as STRIDING BASS, GUITARS, etc. **OUTPUT SOCKET with plug provides 300 v. 30 mA. and 6.3 v. 1.5 a.** For supply of a RADIO FEEDER UNIT. Size approx. 12.9-7in. For A.C. mains 200-250 v. 60 c/s. Output for 3 and 15 ohm speakers. Kit is complete to last. Chassis fully punched. Full instructions and point-to-point wiring 8 Gns. 10/- diagrams supplied. (Or factory built 45/- extra). **ONLY 8 Gns. 10/-** If required louvred metal cover with 2 carrying handles can be supplied for 18/9. **TERMS ON ASSEMBLED UNITS. DEPOSIT 18/9, and 12 monthly payments of 18/9.** Send S.A.E. for illustrated leaflet detailing Ready-to-assemble Cabinets, Speakers, Microphones, etc., with cash and credit terms.

R.S.C. PORTABLE GUITAR AMPLIFIERS



JUNIOR 5 WATT. High Quality Output. Separate Bass and Treble "cut" and "boost" controls. Sensitivity 15 mv. High Flux 8in. 1/speaker. Input sockets for Radio/Tape or Gram Pick-up and Mike /Instrument Pick-up. Handsome strongly made cabinet (size approx. 14 x 14 x 7in.). Finished in satin walnut and fitted carrying handle. **£8/19/6** Carr. 7/6. Or Deposit £1 and nine monthly payments of £1. Send S.A.E. for leaflet.

Size approx. 18 x 18 x 8in. 15 u.a. Plus 10/- carr. E.P. TERMS. DEPOSIT. 22/8 and 12 monthly payments 22/8. Both models for 200-250 v. A.C. mains.

STAR GALAXY 4-SPEED MIXER AUTO-CHANGERS. Brand New, cartoned. Turnover sapphire stylus. Many exclusive features. Unique design motor virtually free from rumble. For 200/250 v. A.C. mains. Limited number tested and guaranteed, £5/19/6. Carr. 4/6.

COLLARO CONQUEST 4-SPEED AUTO-CHANGERS. With studio pick-up with turnover head. BRAND NEW. Cartoned. Latest model. For 200-250 v. A.C. mains. £7/19/6. Carr. 4/6. **B.S.R. MONARCH AUTO-CHANGER.** Type UA8, 4 speed T/O Pick-up with sapphire stylus £7/19/6. Carr. 4/6.

COLLARO JUNIOR. 4-speed Single Players with Hi-Fi T/O crystal pick-up head. £3/19/6.

LOUDSPEAKER IN POLISHED WALNUT FINISHED CABINET. Basses 12 ohms, 15 ohms. Speed coil 3 ohms or 15 ohms. Only £2/19/6. Carr. 5/-. TERMS: DEPOSIT 11/- and 9 monthly payments of 11/-.

12in. 20 WATT 15,000 line /speakers 15 ohms, in Cabinet finished as above. Size 18 x 18 x 8in £7/19/6 or Deposit 13/10 and 12 monthly payments 13/10.

ACOS HGP59 HI-FI Crystal Cartridges. (Turnover type with sapphire stylus.) Standard replacement for Garrard and Collaro. Only 19/9. B.S.R. Full-Fi 19/9. Garrard GC2 19/9.

ACOS HIGH FIDELITY PICKUPS. GP54 with HGP59/52 cartridge. Turnover sapphire stylus, cream finish. Limited number at approx. half price. Only 29/11.

PLESSEY DUAL CONCENTRIC 12in. P.M. SPEAKERS



(15 ohms), consisting of a high quality 12in. speaker of orthodox design supporting a small elliptical speaker ready wired with choke and condensers to act as tweeter. This high fidelity unit is highly recommended for use with our A11 or any similar amplifier. Rating is 10 watts. Gauss 12,000 lines. Price only £5/17/6 Or Deposit 10/6 and 12 monthly payments of 10/6

HARVERSON SURPLUS CO LTD

Phone : CHerrywood 3985|6|7

83, HIGH STREET, MERTON, S.W.19.

Phone : CHerrywood 3985|6|7

The world famous E.M.I. Angel Transcription P.U.

SPECIFICATION

Physical
 Length 15½ inches (40.32 cms.).
 Height 2½ inches (6.41 cms.).
 Width 2½ inches (6.03 cms.).
 Centre of base to stylus tip 12 inches (30.72 cms.). Approx. overall.
Stylus
 A diamond stylus is fitted to the 33½/45 r.p.m. head supplied.
Head Impedance
 1 ohm. (measured at 1,000 c.p.s.).
Frequency Response
 For a constant recorded velocity the frequency response is sensibly level within the following limits: with micro-groove stylus 20—16,500 c.p.s. With standard stylus 20—20,000 c.p.s.
Distortion
 Measured at 400 c.p.s., the total harmonic distortion is less than 5% for a recording level of +20 db referred to 1 cm./sec. r.m.s. transverse velocity.
Sensitivity
 50 mV at secondary of transformer provided from a recording level of +10 db referred to 1 cm./sec. r.m.s. velocity.
Weight at Stylus Point
 Variable from 3—10 grammes as required.



★ (MODEL 17A)

A PICKUP FOR THE CONNOISSEUR ORIGINALLY PRICED AT £17/10/-. WE CAN OFFER THE LAST REMAINING FEW AT

£5.10.0

PLUS P. & P. 5/-

★ WITH DIAMOND STYLUS

SPECIAL OFFER FOR 1 MONTH ONLY

8 WATT Push Pull MONAURAL AMPLIFIER

By well-known manufacturer—employing four Mullard valves: ECC.83, 2 EL.84 and EZ.80. Bass, treble and volume on remote panel. Elegant knobs.

OUR PRICE—Plus P. & P. 4/6.

£5.18.6

Also a few Stereo left.



PLESSEY TWEETER

This well-known Plessey 3 ohm Tweeter at our amazing price of . . .

12'6 TAX PAID
 Plus P. & P. 1/6.



SPECIAL OFFER FOR 1 MONTH ONLY

Ex. Speaker, 5" Goodman unit. Cabinet 8" x 6" x 2". Complete, including lead. P. & P. 2/-.

18/6



AMAZING SCOOP

Coscor 10in. Tubes 108K. Brand New, boxed and guaranteed. Manufacturer's Surplus. Equiv. HMV3/16
15/- each
 Plus P. & P. 12/6.

DIAMOND STYLUS

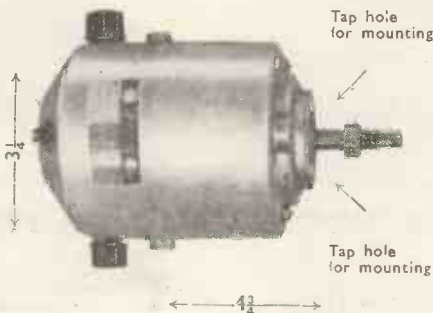
Cost £8/15/-. Brand new. **78 AT £2.0.0**

33½-45 AT £4.0.0
 P. & P. 1/6.

NOTICE

WHY NOT VISIT OUR NEW SHOW-ROOM. LARGEST WALK AROUND IN LONDON. 1 min. South Wimbledon Tube.

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 83 HIGH ST., MERTON, SURREY.
COME AND SEE US.



NOT GOVT. SURPLUS

½ H.P. 220-250 A.C. motor, ideal for lathe, coil winder, drill, saw motor, etc. Don't miss it. Dimensions: 6½ x 3½

45/- P. & P. 2/3.

Just right for a day's outing ★

"CONTINENTAL-6" Combined Portable/Car Radio

MEDIUM AND LONG WAVE FULL TUNING

- ★ Plessey Printed Circuit
- ★ 6 Top Grade Ediswan Transistors
- ★ 5" High Fidelity Speaker
- ★ 400mW Push-Pull Output
- ★ Internal Ferrite Aerial
- ★ Slow Motion Tuning
- ★ Full instructions
- ★ Printed Circuit marked with Component Numbers
- ★ Double Tuned I.F.s
- ★ All Components Guaranteed
- ★ Size 9½ x 7 x 3½
- ★ Weight 4 lbs.

Total Cost of all Components

£11.10.0 p.p. 3/6

including Cabinet, Battery, Transistors, Car Radio, AVC and all necessary items.

A highly sensitive and selective portable fully tunable on medium and long waves. Performs equally well as a car radio. Low running costs, good looks and ease of construction combine to produce a radio equal to commercial receivers in the 20 gns. class.

NEW FREE ILLUSTRATED LEAFLET

★ FOR STYLE, QUALITY, PERFORMANCE AND VALUE FOR MONEY ★

All components available separately.
CALL FOR DEMONSTRATION

Our Customers say:—

"More than full value for money."

"Pleased with performance—cheque enclosed for another one."

"Best I've seen in 14 years of radio work."

"Excellent design and performance."

"Appearance and quality really outstanding."



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6-Ranges: 0-3-10-30-100-300 and 1,000 volts. Input res.: 11-meg. constant on all ranges. Sensitivity: 3,666,666 ohms per volt on 3 v. scale.

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Input 110-250 volts A.C.

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(3-Transistor Pocket Radio)



All parts sold separately.

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- ★ 5-stage Reflex Circuit.
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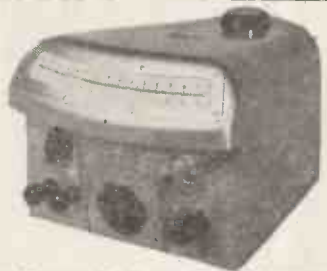
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FROM 5/- EACH

From 6 Kc/s-47 Mc/s. FT243, FT241, 10XJ and B7G.

All types for all purposes. Send for free list.



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- ★ 2 watts per channel
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and Head Demagnetiser. Erases a complete reel of magnetic Tape in few seconds. 27/6. Post free.

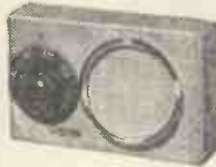
"KLENZATAPE" KIT 12/6



FOR YOUR HOLIDAYS! BUILD THE COSSOR "TRAVELLER'S FRIEND"

4-Transistor
POCKET SUPERHET

Uses 9 v. PP4 battery.
Covers 190-550 metres.
Power output 30MW.



LASKY'S PRICE £7.19.6

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Originally nearly £20.

All components available separately.

All components including 4 transistors. OC44, OC45, OC45, OC72, two OA70 diodes, two AGC systems, 2 1/2in. M.C. speaker, Ferrite slab aerial, etc., with leatherette case, size 6 x 3 1/2 x 1 1/2in. Complete with Printed Circuit and easy-to-follow instructions.

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FOR A.C. MAINS 200/250 V.

A neat, compact and highly transportable Tape Recorder, size only 10 1/2 x 9 x 6in. Fitted fully self-contained Amplifier and 7 x 4in. Speaker. Clock type face indicator. Monitoring and L.S. sockets. Two speeds, 3 1/2 and 1 1/2 i.p.s. Fast forward and fast rewind. Record level indicator. Facilities for recording from two inputs. Plays for one hour one reel of tape. Carrying Case with attractive rexine finish and detachable hinged lid.

LISTED AT 29 GNS.

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Nothing like this has ever been offered before. Note the large size page, 11 1/4 x 8 1/2in., approx 100 pages in photogravure. This is a COMPARATOR CATALOGUE to enable you to choose from all the latest and most advanced equipment. Every hi-fi enthusiast will want it. Send for your copy today.

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Famous make. For 200-250 v. A.C. Output 4 watts matched to 3 ohms speaker. 7 valves: ECC85, ECH81, EF88, EABC80, EL84, EZ80, EM81, magic eye tuning indicator. Covers medium, long and FM bands. Length 12in., height 7 1/2in., front to back 8 1/2in.

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"ALFA" MULTI-RANGE RADIO TEST METER. A.C. and D.C. 3,333 ohms per volt. Ohms ranges to 2 megs. Volts A.C. and D.C. up to 1,200. 300 microamps—300 mA. Decibels, 2 ranges -20 to +23 db; +20 to +37 db. Accuracy ±3%. Large full vision dial. Overall size: 5 1/2 x 3 1/2 x 1 1/2in.

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Wide choice including W/B PRELUDE, G-PLAN, NORDYK and CAPRIOL.



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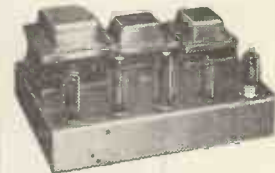
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TAPE RECORDER AMPLIFIER for use with Collaro Studio Transcriptor. Size 11 1/4 x 5 x 3in. Uses 3 valves, magic eye, contact cooled metal rectifier. Incorporates mike/gram/radio inputs, ext. l.s. jack, superimposing switch. Complete with matching knobs. Post (Gold/Black) 12 gns. 3/6.

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"LIGHT" TAPE RECORDER (foreign) 2 spd., 3 1/2 and 7 1/2, with inputs for mike and tuner. In blue/grey carrying case. For 200/250 v. A.C. LASKY'S PRICE 21 gns. Including Tape, Crystal Hand Mike and Radio Jack. Carr free.

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MAESTROVOX 10-12 watt High Fidelity AMPLIFIER AND PRE-AMPLIFIER

Built to latest Mullard circuit and complete with Mullard valves: two EL84 pp., two EF86, one ECC83 and E281 rectifier. Mains Amplifier chassis size 7 1/2in. x 10in., maximum height 5in., gold hammer finish. Separate Pre-Amplifier in polished wood case, walnut veneered, with smart maple and gold escutcheon size 10 1/2in. x 3 1/2in. x 4in.

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**RECORD PLAYER
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Balance at 3/11 a week for 19 weeks. This contemporary cabinet in two-tone grey rexine is ideal for the modern home. Added attraction is the cream plastic speaker fret. Press button lid; lock. Fittings for screw-in legs. Internal measurements 14½ × 18 × 8½ in. deep. Takes a Garrard 121 Mk. 2 or B.S.R.

U.A.12; 9½ × 4½ in. elliptical speaker; our Mk. 2 control portable amplifier. Carr. & ins. 5/6.

LEADS YOU TO

**STEREO RECORD
PLAYER CABINET**

With Extension Speaker Cabinet

Portable 1960 Show Model in two-tone colours. Extension speaker cabinet secured in lid. Size 18 × 14 × 8½ in. high. This stereophonic player complete, retails at 35 gns. in the shops today. Ins. & carr. (with order) 5/6, or initial payment plus ins. & carr. of 6/1 and 19 weekly payments of 4/11.



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**WE HAVE A LARGE SELECTION OF
ASSORTED TYPES AND SIZES RECORD
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All rexine covered in modern two-tone colours. Your enquiries invited. Please let us have your requirements.

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TAPE
RECORDER
CABINET**



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29/9

Beautifully made Tape Recording Cabinet. Size: 13 × 10½ × 7 in. Covered in two-tone coloured rexine cloth. Stylish design. Carrying handle with detachable lid with lock and key. Easily adapted to Record Player Cabinet.

Exceptional value at this very low price. P. & P. 4/6.

**B.S.R. MONARCH U.A.8
4-SPEED AUTOCHANGER
£6.19.6 or Terms**

4-speed Autochanger. Incorporating auto and manual control complete with turnover crystal P.U. and Sapphire stylus, A.C. P. & Ins. 5/6 or initial payment 8/11, plus P. & Ins. and 19 weekly payments of 6/11. T.U.9 B.S.R. 4-speed single player 24/9.6. Collaro Conquest 4-speed single player 26/19.6. Collaro Conquest Stereo autochanger 9 gns. P. & P. on each above 5/6.



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**MODERN
17" T.V.
CHASSIS
COMPLETE
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19 gns**

A chassis including 17in. tube, permanent magnet speaker, 13-channel Turret Tuner (any two selected channels fitted). Other channels supplied on request at 7/6 each. 13 valves. Chassis and valves guaranteed for three months. Tube 12 full months guarantee. A.C. only. Ready and working to fit into your own cabinet. Carr. & ins. 25/-.

As above with 14in. tube, complete and working 12 gns.

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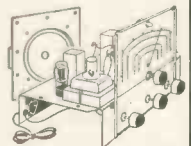
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110 v., 6 v. or 12 v. (special adaptor for 200/250 v. 10/- extra). Automatic solder feed including a 20ft. reel of Ersin 60/40 solder and spare parts. It is a tool for electronic soldering or car wiring. Revolutionary in design. Instantly ready for use and cannot burn. In light metal case with full instructions for use. Post 3/6.

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**EXTENSION
SPEAKERS
19/9**



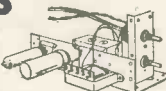
This superbly finished, polished oak cabinet fitted with 8in. P.M. speaker W.B. or Goodmans of the highest quality, will sound and look ideal in any part of your home. Standard matching to any receiver (2.5 ohms). Switch and flex included. Ins. & carr. 3/9. Elliptical Speakers, 9½ × 4½ in. and 7 × 4 in. 19/6. Post 2/11.

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MK. D.I. 59/6

Brand new. Latest design with printed circuit. Dimensions 7 × 2½ × 6 in. A.C. only. Mains isolated 3 watts output. Incorporating EL84 as high gain output valve. Volume and tone controls. Knobs 2/6 extra. P. & P. 3/6.



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Printed circuit. Latest design. Dimensions 7 × 2½ × 6 in. A.C. only. Mains isolated. 4 watt output. Incorporating the latest ECL82 triode pentode output valve, giving high undistorted output. Volume and tone controls. Knobs 2/6 extra. P. & P. 3/6.

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As above but with 3 controls, incorporating a special tone connector circuit for extra base and top boost, giving a tone of reproduction seldom heard on a very expensive amplifier. Must be heard to be appreciated. Knobs 3/6 extra. P. & P. 3/6.

**T.V. CHASSIS IS FOR SPARES 9/6
ALL THIS FOR ONLY**

56 resistances including 7 variable controls. 54 condensers including electrolytics. Coils 7 I.F. and R.F. transformers. 13 valve holders (8-B8A, 2-B7G and 3-octal), 4 transformers—Mains-Output-Line-Frame. Chokes 250 m/a. Metal rectifiers, 300 volts at 250 m/a. Fuse panel, scanning coils, focus magnets. Plugs, sockets, switch, chassis screws, tag strips, etc. I.F. strip can be separated. Power pack can be used without dismantling. These chassis have been used, but were working when stored. 6 page circuit and instruction, showing position of each component. Carr. 7/6.

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79/6



A.C. or Universal Mains. Five valve octal superhet. 3 waveband receiver can be adapted to g. am. P.U. In attractive wooden cabinet. 9½ × 18½ × 11½ in. Ins. and carr. 4/6.

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Mains Auto 0-205-225-245 Volts @ 300 m.a. Isolated windings of 6.3v @ 2.6 amp. 6.3v. @ 3-6 amp. 2v. @ 1-4 amp. Post 3/9.

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Wide angle 90 deg. 38 mm. Low imp. P. & P. 1/3.

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Designed by MULLARD—presented by STERNS strictly to specification

MULLARD "5-10" MAIN AMPLIFIER

For use with the MULLARD 2-stage pre-amplifier with which an undistorted power output of up to 10 watts is obtained. We supply SPECIFIED COMPONENTS AND NEW MULLARD VALVES including PARMEKO MAINS TRANSFORMER and choice of the latest Ultra-Linear PARMEKO or PARTRIDGE Output Transformer

Price: COMPLETE KIT (Parmeko Output Trans.) **£10.00**

Alternatively we supply ASSEMBLED AND TESTED **£11.00**

ABOVE INCORPORATING PARTRIDGE OUTPUT TRANSFORMER £1/4/- extra.

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PRE-AMPLIFIER TONE CONTROL UNIT

Employing two 6F96 valves and designed to operate with the Mullard MAIN AMPLIFIER, but also perfectly suitable for other makes.

Supplied strictly to MULLARD SPECIFICATION and incorporating:

- Equalisation for the latest R.I.A.A. characteristics.
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- Input (a) Direct from High Imp. Tape Head. (b) From a Tape Amplifier or Pre-Amplifier.
- Sensitive Microphone Channel

Alternatively we supply ASSEMBLED AND TESTED **£8.00**

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COMPLETE MULLARD 5-10 AMPLIFIER

The popular and very successful complete "5-10" incorporating Control Unit providing up to 10 watts high quality reproduction.

Specified components and new MULLARD VALVES are supplied including PARMEKO MAINS TRANSFORMERS and choice of the latest PARMEKO or PARTRIDGE ULTRA Linear Output Transformers.

Price: COMPLETE KIT, Parmeko Transformer..... **£11.00**

Alternatively we supply ASSEMBLED AND TESTED **£13.00**

Alternatively we supply ASSEMBLED AND TESTED. Hire Purchase (Assembled Amp. only). Deposit £2/14/-, 12 months at 19/10.

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COMPLETE MULLARD 3-3

A VERY HIGH QUALITY AMPLIFIER DEVELOPED FROM THE VERY POPULAR 3-VALVE 3-WATT AMPLIFIER DESIGNED IN THE MULLARD LABORATORIES.

Price for COMPLETE KIT OF PARTS **£7.10**

(Plus 6/6 carriage and insurance).

Alternatively supplied ASSEMBLED AND FULLY TESTED (Plus 6/6 carriage and insurance).... **£8.19.6**

H.P. TERMS: Deposit £2 and 8 monthly payments of £1.

Our kit is complete to the MULLARD specification including supply of specified components, valves and PARMEKO OUTPUT TRANSFORMER. We also include switched inputs for 78 and L.P. records plus a Radio position. Extra power to drive a Radio Tuning Unit is also available.

COMPLETE STEREO AMPLIFIER

A thoroughly recommended design that very effectively meets the many requests for a low priced but good quality DUAL CHANNEL STEREO PHONIC AMPLIFIER.

Price: COMPLETE KIT OF PARTS **£8.10.0**

Alternatively ASSEMBLED AND TESTED **£10.10.0**

Two Mullard ECL82 Triode Pentode Valves are incorporated in the design, they form a "CLASS A" single ended output stage in each channel. The input sensitivity is 300 mv/olts, therefore when used with most STEREO Crystal Pick-ups, or Radio Tuning Units, an output of 2 watts per channel is achieved, or similarly when switched to MONAURAL Pick-up position a combined output of 4 watts is produced.

SPECIAL CASH ONLY OFFER !!

This very attractive PORTABLE AMPLIFIER CASE together with a good quality GRAM AMPLIFIER and a matched P.M. SPEAKER. ALL FOR ONLY **£8.7.6** (plus 7/6 carr. and ins.). The Amplifier consists of a 2-stage design incorporating the 3 modern BVA valves and has separate BASS and TREBLE CONTROLS. The Portable Case will also accommodate almost any make of Autochanger and is attractively finished in Grey Colour. Recline—WE ALSO SUPPLY SEPARATELY:—

(a) The 2-stage (plus Rectifier) AMPLIFIER **£4 2 6**

(b) The PORTABLE CARRYING CASE **£3 17 6** (Carriage and Insurance 4/- extra).

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"Hi-Fi" LOUDSPEAKERS

WE HAVE IN STOCK A COMPLETE RANGE BY

GOODMANS WHARFEDALE

W.B. STENTORIAN

ILLUSTRATED AND PRICED LEAFLETS ON REQUEST

!! HOME CONSTRUCTORS !!

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Designed by the W.B. "STENTORIAN" COMPANY for "Hi-Fi" Loudspeaker systems or to accommodate high quality equipment. The acoustically designed Bass Reflex Cabinets containing the very successful "Stentorian" Speakers give really first-class reproduction and are well recommended. Models are also available to accommodate high-quality Amplifiers, Pre-amplifiers, Tuning Units, Record Players, etc. All models are very easily assembled in fact only a screwdriver is required. Fully illustrated leaflets are available including complete specifications of the various STENTORIAN LOUDSPEAKERS. Please enclose S.A.E.

Please enclose S.A.E. if ILLUSTRATED and DESCRIPTIVE LEAFLETS are required... alternatively the COMPLETE ASSEMBLY MANUALS containing component Price List and practical Drawings, etc., are available at 1/6 each.

SPECIAL PRICE REDUCTIONS

(e) The COMPLETE KIT OF PARTS to build both the "5-10" Main Amplifier and the 2-Stage Pre-Amplifier Control Unit..... **£15.15.0**

(d) The "5-10" and the 2-Stage Pre-Amplifier both Assembled and Tested..... **£18.18.0**
H.P. TERMS: Deposit £3/16/- and 12 months of £1/7/8.

(c) The COMPLETE KIT OF PARTS to build the Dual Channel "3-3" Amplifier and the Dual Channel Pre-Amplifier Control Unit..... **£21.10.0**

(f) The Dual Channel "3-3" Amplifier and the Dual Channel Pre-Amplifier Control Unit both Assembled and Tested..... **£25.0.0**
H.P. TERMS: Deposit £5 and 12 months of £1/16/8.

(g) The COMPLETE KIT OF PARTS to build one "5-10" Main Amplifier (Parmeko Transformer) and the Dual Channel Pre-Amplifier Control Unit..... **£21.10.0**

(h) One "5-10" Amplifier (Parmeko Transformer) and the Dual Channel Pre-Amplifier both Assembled and Tested..... **£25.0.0**
H.P. TERMS: Deposit £5 and 12 months of £1/18/8.

(i) COMPLETE KIT OF PARTS to build Two "5-10" Main Amplifiers (incorporating Parmeko Output Transformers) and the Dual Channel Pre-Amplifier Control Unit..... **£31.0.0**

(j) Two "5-10" Amplifiers (Parmeko Output Transformers) and the Dual Channel Pre-Amplifier Control Unit both Assembled and Tested..... **£36.0.0**
H.P. TERMS: Deposit £7/4/- and 12 months of £2/12/-.

Carriage and insurance 7/6 extra.

Prices quoted are subject to £1/6/- extra for Partridge Trans.

STEREO

3-3 MAIN AMPLIFIER

Comprises two "3-3" MAIN AMPLIFIERS on one chassis and is designed to operate with our DUAL CHANNEL PRE-AMPLIFIER for both STEREO PHONIC or MONAURAL operation.

Price: COMPLETE KIT OF PARTS **£10.0.0**

Alternatively ASSEMBLED AND TESTED **£11.15.0**

H.P. Terms: Deposit £2/7/-, 12 months at 17/4.

Its output power is 6 watts (3 watts per channel) and together with our PRE-AMPLIFIER provides a first-class STEREO installation.

STEREO DUAL CHANNEL PRE-AMPLIFIER

This model incorporates two 2-valve Pre-Amplifiers (described above) combined into a Single Unit enabling it to be used for both STEREO PHONIC or MONAURAL operation. It is designed primarily to operate with our range of MULLARD MAIN AMPLIFIERS but will also operate equally well with any make of Amplifiers requiring an input of 250 mv.

Price: COMPLETE KIT OF PARTS **£12.10.0**

Alternatively ASSEMBLED AND TESTED **£15.0.0**

H.P. Terms: £3 Deposit and 12 months of £1/2/-.

Perfectly suitable for MONAURAL only operation, with any "3-3" or any "5-10" MAIN Amplifier to which the second Main Amplifier can at one time be added thus very easily providing for both STEREO or MONAURAL reproduction.

Recommended combination for STEREO operation.

(a) The DUAL CHANNEL PRE-AMPLIFIER together with the Dual "3-3" MAIN AMPLIFIER.

(b) The DUAL CHANNEL PRE-AMPLIFIER together with two "5-10" MAIN AMPLIFIERS. Assembly Manual is available for 3/- or send S.A.E. for Descriptive Leaflet. When ordering please advise MAKE and MODEL OF AMPLIFIER in use.

!! RECORD PLAYERS !!

The LATEST MODELS are in Stock. Many at REDUCED PRICES!!!

Send S.A.E. for ILLUSTRATED LEAFLET

B.S.R. MONARCH UA8 4-spd. Mixer Autochanger with Crystal Pick-up. **£6.19.6**

The COLLARO "CONQUEST" 4-spd. Autochanger, Studio "O" Pick-up. **£7.10.0**

The latest COLLARO "CONTINENTAL" 4-spd. MIXER Autochanger, Studio "O" Pick-up. **£8.10.0**

The NEW COLLARO model RP594, 4-speed Single Record Player, Studio Cartridge **£9.18.9**

The COLLARO 4-speed Single Record Player, incorporating the Studio "O" Pick-up **£6. 9.6**

The NEW B.S.R. model UA12 is in stock. A 4-"SPEED" MIXER AUTOCHANGER **£8. 7.6**

UA12 is also available incorporating the B.S.R. STEREO Pick-up, plays L.P. and 78 records **£10.10.0**

GARRARD RC210 4-speed Autochanger fitted with latest Crystal Pick-up **£10.10.0**

The latest GARRARD TRANSCRIPTION MOTOR "301" with Stroboscopically marked turntable **£23.18.4**

The new GARRARD Model 4HP High Quality Single Record Player fitted with the latest T.F.A. 12 Pick-up arm and G.C.S. Crystal Cartridge **£18. 7.6**

GARRARD Model TA/Mk. II Single Record Player fitted with high output Crystal Pick-up, detachable head **£8.10.0**

HIRE PURCHASE TERMS available on all units £2/19/6 and over Carriage and Insurance on each above 5/- extra.

STERN RADIO LTD.

DEPT. W 109 FLEET ST.,

LONDON, E.C.4

Telephone: FLEET STREET 5812/3/4

Each Model incorporates the highly successful HF/TR3 Amplifier (described opposite), thus ensuring truly "Hi-Fi" record and playback facilities.

All prices quoted provide for the COMPLETE RECORDER including CRYSTAL MICROPHONE and 1-200ft. Spool of Tape.

There are no "better value for money" Tape Recorders on the market—if you can't call and hear them—send S.A.E. for fully descriptive leaflets.



Stern's "fidelity" TAPE RECORDERS

BEFORE YOU BUY—YOU SHOULD HEAR THESE RECORDERS—THEY ARE COMPARABLE TO THE MUCH HIGHER PRICED MODELS

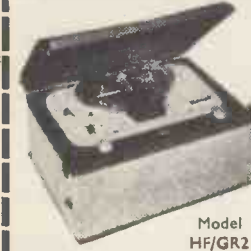
- MODEL GR3/3, Incorporates the New COLLARO "STUDIO" TWIN TRACK 3-speed Deck **£41.0.0**
H.P. Terms: Deposit £3/4/- and 12 months of £3/0/2.
- MODEL GR3/T, Incorporates the very popular 3-speed COLLARO Mk. IV "TRANSCRIBTOR" Deck, which has both upper and lower tape tracks **£49.10.**
H.P. Terms: Deposit £9/18/- and 12 months of £3/12/7.
- MODEL TR3 Mk. VI, Incorporates the New TRUVOX Mk. VI TWIN TRACK 2-speed Tape Deck **£49.10.0**
H.P. Terms: Deposit £3/18/- and 12 months of £3/12/7.

and NOW — WE INTRODUCE

- THE MODEL HF/G2P TAPE PREAMPLIFIER
- THE MODEL HF/G2A TAPE AMPLIFIER

Designed to our usual High Technical Standard, being based on the very successful Mullard Tape Designs. They incorporate MULLARD VALVES and only HIGH-GRADE COMPONENTS... AS A RESULT WE PRESENT TWO UNITS METICULOUSLY MATCHED TO CORRECTLY OPERATE

THE NEW GARRARD "MAGAZINE" TAPE DECK



Model HF/GR2



Model HF/G2A-D

Both Units form an entirely new "Easy to handle" presentation, each is completely self contained with power supply, Loudspeaker (Amplifier HF/G2A only), and all INPUT and OUTPUT sockets being incorporated on the chassis, which itself is constructed to allow for direct attachment to the tape deck (as shown in illustration). Thus the tape deck with the Amplifier (or Preamplifier) fixed to it form ONE COMPLETELY SELF-CONTAINED WORKING UNIT which requires only screwing into a Cabinet and Connecting to the Mains supply.

Model HF/G2A Amplifier

- A Complete Tape Amplifier—Incorporating...
 - Magic Eye Level Indicator
 - Volume Control.
 - Superimpose Switch.
 - Effective Tone Control.
 - Monitoring Facilities.
 - Extension Loudspeaker Socket.
 - Inputs for recording from Mike, Gram, and Radio Tuner.
 - Incorporates Loudspeaker and Power Supply on Chassis.

Model HF/G2P Preamplifier

- Forms the Ideal "Link" to add High Quality Tape Recording facilities to existing Audio Installations, such as our MULLARD RANGE of Amplifiers and also admirably suitable to operate through the Pick-up sockets of most Radio Receivers.
- It incorporates:
 - Magic Eye Level Indicator and Control.
 - Superimpose Switch.
 - Inputs for recording from Mike, Gram, and Radio

BOTH UNITS CARRY MESSRS. GARRARD'S FULL RECOMMENDATION

As is usual with GARRARD products this Tape Deck is a Precision Engineered Unit of Excellent quality operating two tracks at 3 1/2 in./sec. speed. It is the "Easiest to Handle" Tape Deck, having only two controls and incorporates the new instantaneous Tape Loading Magazine which makes tape loading as simple as putting on a Record.

WE OFFER AS FOLLOWS:

- (a) MODEL HF/G2R PORTABLE TAPE RECORDER. Includes spool of L.P. tape and crystal microphone. H.P. TERMS: Deposit £8/12/-, 12 monthly payments £2/8/5. **£33.0.0**
- (b) MODEL HF/G2A/D, comprising AMPLIFIER and TAPE DECK. Includes spool of L.P. tape and loudspeaker. H.P. TERMS: Deposit £5/10/-, 12 monthly payments £2/0/4. **£27.10.0**
- (c) ASSEMBLED and TESTED AMPLIFIER MODEL HF/G2A H.P. TERMS: Deposit £3, 12 monthly payments £1/2/-. **£15.0.0**
- (d) MODEL HF/G2PP PORTABLE PREAMPLIFIER. Complete in portable case (like HF/G2R). H.P. TERMS: Deposit £6, 12 monthly payments £2/4/-. **£30.0.0**
- (e) MODEL HF/G2P-D comprising PREAMPLIFIER and TAPE DECK. Includes spool of L.P. tape. H.P. TERMS: Deposit £5/4/-, 12 monthly payments £1/18/2. **£26.0.0**
- (f) ASSEMBLED & TESTED PREAMPLIFIER MODEL HF/G2P H.P. TERMS: Deposit £2/18/-, 12 monthly payments £1/0/6. **£14.0.0**

!! RADIOGRAM CHASSIS !!

- ARMSTRONG MODEL A F 208 Complete AM/FM chassis. Separate Bass and Treble controls. **£23.2.0**
- ARMSTRONG "STEREO TWELVE" The most complete A.M./F.M. stereo chassis yet produced. **£37.16.0**
- ARMSTRONG "JUBILEE" An AM/FM chassis with nine valves and with push-pull output stage providing 8 watts. **£29.8.0**
- ARMSTRONG AM/FM "STEREO 44" Provision is made for Stereo and Monaural playback (from pick-up or **£28.7.0**

RADIO TUNING UNITS

- The JASON "MERCURY" Switched F. M. TUNER. PRICE ASSEMBLED AND TESTED **£13.10.0**
 - DULCI Model FMT/2 A complete self-powered FM Tuner incorporating automatic frequency control. **£24.13.4**
 - ARMSTRONG "S.T.3" AM/FM Tuning Units A self-powered tuner covering VHF, medium and long wavebands with automatic frequency control on VHF. **£27.6.0**
 - DULCI "H4/T" AM/FM Tuning Units A 4-waveband self-powered tuner covering the FM transmission plus the long, medium and short wavebands. **£25.15.2**
- NEW HIRE PURCHASE TERMS are available on all above. Illustrated leaflets available—send S.A.E. (Carr. and Ins. 5/- extra.)

STERN'S MK. II "fidelity" F.M. TUNING UNIT

(Plus 5/- carr. and ins.)
HIRE PURCHASE: Deposit PRICE **£14.5.0**
£2/17/- and 12 months at £1/0/11. Incorporates the latest MULLARD PERMEABILITY TUNING HEART and the corresponding MULLARD VALVE LINE UP comprising 6OC85, 2 type EF85s (or EF86s), EM84, Tuning Indicator, plus 2 type O.A. 79s Germanium Diodes. A really first-class Tuner very attractively presented and comparable to many offered at much higher prices. Power consumption is only 1.5 amps at 6.3 volts and 25 m.a. at 250 volts.



! HOME CONSTRUCTORS
YOU CAN BUILD YOUR TUNING UNIT **£10.10.0**
FOR ONLY
Send S.A.E. for descriptive leaflet, or (Plus 5/- carr. and ins.)
Assembly Manual for 1/6.

THE "ADD-A-DECK"

incorporating the **NEW B.S.R. "MONARDECK"** and MATCHED PREAMPLIFIER

£17.17.0 Deposit £3/12/-, 12 months £1/6/2 (Plus 7/6 carr. and Ins.)

Designed to operate through the Pick-up Sockets of the standard RADIO RECEIVER through which first-class results are obtained. It consists of a single speed Twin Track Tape Deck, incorporating matched Preamplifier, and operates at 3 1/2 in./sec. speed. It uses 5in. Tape Spools, thus providing up to 1 1/2 hours' playing time on L.P. Tapes or 1 hour on the standard 6in. Tape Spools.

The equipment is supplied fully tested and completely assembled on an attractive wood plinth. It can therefore be "dropped" directly into an existing cabinet and only requires connections to the mains supply and the Pick-up Sockets, for which purposes "floating" leads are incorporated on the Preamplifier.



STERN'S 12 VOLT CAR

RADIO incorporating PRINTED CIRCUIT and POWER TRANSISTOR



A versatile design covering both LONG and MEDIUM WAVEBANDS, incorporating Transistor Output thus having very low battery consumption. Is operated direct off 12 volt car battery. We offer it on the UNIT ASSEMBLY BASIS... consisting of THREE SEPARATE, FULLY WIRED, ALIGNED AND TESTED UNITS ALL FOR Only 12 solder joints are required to finish the complete receiver. **£15.0.0**
Send 1/6 for manual containing complete data.

Stern's "fidelity" TAPE EQUIPMENT

THE FINEST RANGE OF TAPE EQUIPMENT FOR THE HOME CONSTRUCTOR

A SELECTION OF HIGH FIDELITY PORTABLE TAPE PRE-AMPLIFIERS

Adds "Hi-Fi" Tape Recording to your existing Audio Installation.

IN ALL MODELS WE INCORPORATE THE

TYPE "C" PRE-AMPLIFIER

and offer it complete in portable case with . . .

- (a) The new "COLLARO" STUDIO 3 speed Deck. Deposit: £7/6/-. 12 months £2/13/6. **£36.10.0**
- (b) The COLLARO Mk. IV "Transcriptor" 3 Speed Deck. Deposit: £8/6/-. 12 months £3/0/11. **£41.10.0**
- (c) The new TRUVOX Mk. VI Tape Deck. Deposit: £8/14/-. 12 months £3/3/10. **£43.10.0**
- (d) The BRENNEL Mk. V 3 Speed Deck. Deposit: £10/6/-. 12 months £3/15/7. **£51.10.0**
- (e) The WEARITE MODEL 4A Tape Deck. Deposit: £12/4/-. 12 months £4/9/5. **£61.0.0**



STERN'S MULLARD TYPE "C" TAPE PRE-AMPLIFIER—ERASE UNIT

INCORPORATING THE NEW FERROXCUBE POT CORE PUSH-PULL OSCILLATOR and 3 SPEED TREBLE EQUALISATION by means of the latest FERROXCUBE POT CORE INDUCTOR.



PRICES . . . INCLUDING SEPARATE SMALL POWER SUPPLY UNIT COMPLETE KIT **£14.0.0** ASSEMBLED AND TESTED **£17.0.0**

Deposit £3/8/- and 12 months of £1/4/11. Assembled unit only. ALSO AVAILABLE EXCLUDING POWER SUPPLY UNIT FOR **£11.15.0** and **£14.10.0** respectively. (Carr. and Ins. 5/- extra)

Send S.A.E. for leaflet or 2/6 for Complete Assembly Manual. WHEN ORDERING PLEASE STATE MAKE OF TAPE DECK TO BE USED We present this "Hi-Fi" Pre-amplifier strictly to Mullard's specification etc., incorporating ONLY NEW HIGH GRADE COMPONENTS and the SPECIFIED NEW MULLARD VALVES. It comprises a COMPLETELY SELF-CONTAINED UNIT, all components and valves being contained in a well ventilated Box—Chassis neatly finished in Hammered gold with a very attractively engraved PERSEPEX FRONT PANEL.

FOR PERMANENT HIGH FIDELITY INSTALLATIONS

WE ALSO OFFER (excluding Case) the following

- (a) The COLLARO "STUDIO" TAPE DECK and our Mullard Type "C" PRE-AMPLIFIER and Power Unit Assembled and Tested. **£32.10.0**
H.P. Terms: Deposit £6/10/- and 12 months at £2/7/8
- (b) As above but TYPE "C" PRE-AMPLIFIER supplied as complete Kit of Parts. **£29.0.0**
- (c) The COLLARO Mk. IV TAPE DECK and the MULLARD Type "C" Pre-amplifier and Power Unit assembled, tested. **£35.0.0**
H.P. Deposit £7 and 12 months £2/11/4
- (d) As in (a) above but the Type "C" supplied as COMPLETE KIT OF PARTS. **£32.0.0**
- (e) The TRUVOX Mk. VI TAPE DECK and the assembled Type "C" Pre-amplifier and Power Unit. **£40.0.0**
H.P. Deposit £8 and 12 months £2/18/8
- (f) As above but the Type "C" supplied as complete KIT OF PARTS. **£36.10.0**
- (g) The BRENNEL Mk. V Deck and the assembled Type "C" PRE-AMPLIFIER and POWER UNIT. **£46.0.0**
- (h) As above, but the Type "C" supplied as complete KIT OF PARTS. **£43.0.0**
- (i) The WEARITE 4A DECK with Type "C" assembled and tested. **£56.0.0**
H.P. Deposit £11/4/- and 12 months £4/2/1.
(Carriage and Insurance on above quotes 10/- extra)



YOU CAN BUILD A COMPLETE HIGH QUALITY TAPE RECORDER for **£36.0.0**

H.P. TERMS . . . Deposit £7/4/-, 12 months £2/12/10

FOR THIS WE SUPPLY:—

COMPLETE KIT OF PARTS TO BUILD THE HF/TR3 TAPE AMPLIFIER.

THE NEW COLLARO "STUDIO" TAPE DECK. PORTABLE CARRYING CASE (as illustrated). ROLA/CELESTION 10in. x 6in. P.M. LOUDSPEAKER. ACOS CRYSTAL MICROPHONE 1,200ft. SPOOL E.M.I. TAPE.

Alternatively for those who prefer another type of TAPE DECK we will supply precisely as above—but IN PLACE OF THE COLLARO "STUDIO" DECK—WE INCLUDE:—

- (a) The Mk. IV COLLARO "TRANSCRIPTOR" DECK . . . H.P. TERMS . . . Deposit £8, 12 monthly payments of £2/18/2 (£1 extra if we are required to wire up the Transcriptor Switch Banks). **£39.15.0**
- (b) The new TRUVOX Mk. VI DECK. **£45.0.0**
H.P. TERMS: Deposit £9, 12 months of £3/6/- (Carr. and Ins. on all above is 12/6 extra).

For constructors with their own Cabinet—WE OFFER:—

- (a) COMPLETE KIT to build the HF/TR3 Amplifier, together with the COLLARO "STUDIO" DECK. **£28.0.0**
- (b) As above but HF/TR3 ASSEMBLED and TESTED. **£31.10.0**
H.P. TERMS: Deposit £6/6/-, 12 months of £2/6/2.
- (c) COMPLETE KIT to build the HF/TR3 together with the Mk. IV COLLARO "TRANSCRIPTOR" DECK (£1 extra if we are required to wire up Deck Banks) **£30.15.0**
- (d) As above but HF/TR3 ASSEMBLED and TESTED. **£34.10.0**
H.P. Terms: Deposit £7, 12 months at £2/10/5. (£1 extra if we are to wire up Deck Switch Banks)
- (e) COMPLETE KIT to build the HF/TR3 together with the NEW TRUVOX Mk. VI TAPE DECK. **£36.0.0**
- (f) As above but HF/TR3 ASSEMBLED and TESTED. **£39.10.0**
H.P. Terms: Deposit £7/18/-, 12 months of £2/17/11.
- (g) COMPLETE KIT to build the HF/TR3 AMPLIFIER with the BRENNEL Mk. V TAPE DECK. **£41.10.0**
- (h) As above but HF/TR3 ASSEMBLED and TESTED. **£45.0.0**
H.P. Terms: Deposit £9, 12 months of £3/6/-.
- (i) THE ASSEMBLED and TESTED HF/TR3 AMPLIFIER with the WEARITE MODEL 4I DECK, incorporates Wearite Head Lift Transformer, etc. **£55.0.0**
H.P. TERMS: Deposit £11, 12 months of £4/0/8. (Carriage and Insurance on each above is 10/- extra.)

Attractive PORTABLE CASE is available to accommodate the TRUVOX or COLLARO TAPE DECKS and we offer it together with ROLA/CELESTION 10/ 6in. LOUDSPEAKER—ACOS CRYSTAL MICROPHONE —and 1,200ft. SPOOL E.M.I. TAPE—ALL FOR. **£9.0.0**
(Carriage and Insurance 5/- extra.)

WE HAVE THE NEW 2-SPEED TWIN TRACK

TRUVOX Mk. VI Tape Deck in stock **£26.5.0** Deposit 25/5/-, 12 months £1/18/6
It incorporates PRECISION REV. COUNTER and PAUSE CONTROL and fully maintains the general high standard of all Truvox equipment. The very popular COLLARO Tape Decks and the BRENNEL Mk. V Decks are also available.

THE MODEL HF/TR3 TAPE AMPLIFIER

Incorporating 3-SPEED TREBLE EQUALISATION by means of the latest FERROXCUBE POT CORE INDUCTOR
PRICES for COMPLETE KIT OF PARTS FULLY ASSEMBLED AND TESTED
HIRE PURCHASE: Deposit £3/6/6 and 12 months at £1/4/2. A very high quality amplifier based on the very successful Type "A" design completed in the MULLARD LABORATORIES. ONLY NEW HIGH-GRADE COMPONENTS are incorporated including MULLARD VALVES and a GILSON OUTPUT TRANSFORMER . . . other features are: Magic Eye Recording Head Indicator—Effective Tone Control—Monitoring and Extension Speaker Sockets—has own Power Supply and can be used as independent Amplifier for direct reproduction of Gram. Records or from Radio Tuner. Overall size 11 x 6 x 6in.—Truvox—Collaro—or Brenell—please specify which. Send S.A.E. for leaflet or 2/6 for Assembly Manual.



PLEASE ENCLOSE S.A.E. WITH ALL CORRESPONDENCE

STERN RADIO LTD.

109 FLEET ST., LONDON, E.C.4

Telephone: FLEET STREET 5812/3/4

FOR VALVES, TUBES AND COMPONENTS: BY RETURN POST SERVICE



ACHLDD	10/-	EL36	19/11
AC/P	7/6	EL38	26/6
ACSPEND	26/6	EL41	10/6
AC6PEN	6/6	EL42	10/6
ATP4	10/-	EL81	16/7
AZ1	10/-	EL83	19/11
AZ31	10/-	EL84	9/-
AZ41	13/11	EL91	5/6
B36	10/-	EL821	26/6
CBLL1	26/6	EM34	9/6
CBLL3	23/3	EM80	10/-
CCH35	23/3	EM81	10/6
CL4	12/6	EY51	10/-
CL33	19/3	EY81	13/3
CY31	16/7	EY86	10/-
CY1	18/7	EZ35	16/7
CV73	4/-	EZ40	7/6
C36A	6/6	EZ41	7/6
DAF96	8/9	EZ80	7/-
DF96	8/9	EZ81	7/-
DH63	7/6	EZ90	7/6
DK56	8/9	E1148	2/-
DL96	8/9	FC4	26/6
DM70	7/6	FC13	6/6
DN41	12/6	FW4/500	10/-
EA50	1/6	GTIC	27/6
EAFBC80	9/6	GZ32	12/-
EAB42	10/6	H30	5/-
EB34	2/-	H63	10/6
EB41	8/6	HL23DD	8/-
EB91	6/6	HL22	6/6
EB33	6/9	HN309	24/7
EB41	9/6	K40N	9/-
EB81	11/4	KF35	8/6
EB89	12/7	KK32	21/11
EB91	12/7	KLL32	24/7
EBF80	9/9	KT2	5/-
EBF89	9/6	KT24	5/-
EBL21	23/3	KT32	14/-
EBL31	23/3	KT33C	8/6
ECC40	23/3	KT36	29/10
ECC81	8/-	KT61	13/6
ECC82	7/6	KT63	7/6
ECC83	9/-	KT66	17/6
ECC84	10/-	KT88	22/6
ECC85	9/6	KTW61	6/6
ECC86	12/-	KTW63	7/6
ECC87	13/-	KTZ41	3/6
ECH3	26/6	MH41	7/9
ECH21	23/3	ML4	8/6
ECH35	23/3	MSP4/5	7/6
ECH42	9/6	MS40	12/6
ECH81	9/-	N147	14/6
ECH83	13/11	N37	19/11
ECL80	10/-	N78	19/11
ECL82	12/6	N339	17/6
ECL83	19/3	OZ4	5/6
EF9	23/3	P61	3/6
EF22	8/6	PAB80	13/11
EF36	5/-	PCC84	9/-
EF37A	15/-	PCC85	14/7
EF40	14/6	PCC88	23/11
EF41	9/9	PCC89	19/11
EF42	11/-	PCF80	9/6
EF50	4/-	PCF82	12/6
EF50SYL	7/6	PCF84	16/7
EF54	6/-	PCL82	12/-
EF55	10/-	PCL83	14/6
EF80	8/-	PCL84	16/7
EF85	7/6	PL36	17/6
EF86	13/-	PL81	12/6
EF89	8/9	PL82	8/6
EF91	5/9	PL83	11/6
EF91 (BVA)	9/-	PL84	12/7
EF97	13/3	PL820	18/7
EF98	13/3	PX25	12/6
EL32	4/6	PY31	16/7
EL33	14/-	PY32	17/11
EL34	19/11	PY80	7/6
		PY81	8/6
		PY82	7/-

PY83	8/6	IA3	3/6
PZ30	19/11	IA7GT	12/6
PEN4DD	26/6	IC2	11/6
PEN4VA	10/-	IC5GT	12/6
PEN25	6/-	ID5	12/6
PEN46	7/-	ID6	12/6
PEN383	23/3	IHSGT	8/6
PEN220A	4/-	IL4	4/6
PEN45DD		ILD5	3/6
		IN5	10/6
PENA4	12/6	IR5	7/6
PM12M	8/-	IS4	10/6
QP21	5/-	IS5	6/6
R16	26/6	IT4	6/-
SP41	3/-	2C26	1/6
SP61	3/-	2P	26/6
SP45	10/6	3A5	12/6
SP47	10/6	3A8GT	6/-
T41	23/3	3D6	5/-
TP25	10/-	3Q4	8/-
U10	10/6	3Q5GT	9/6
U14	8/6	354	7/6
U16	12/6	3V4	8/6
U22	8/-	4D1	3/-
U25	14/-	5R4GY	9/6
U26	12/6	5U4G	6/6
U37	26/6	5V4	11/6
U45	15/-	5Y3G	8/-
U50	8/-	5Y3GT	8/-
U76	8/-	5Z4G	9/-
U339	12/-	5Z4M	10/-
U403	16/7	6A7	10/6
U404	11/4	6A8G	9/-
U801	29/10	6AC7	4/-
UABC80	10/-	6AG5	5/6
UAF42	9/6	6AK5	5/-
UB41	9/-	6AL5	4/6
UBC41	9/-	6AM5	7/6
UBC81	11/4	6AM6	4/6
UBF80	9/6	6AQ5	7/6
UBF89	13/11	6AT6	8/6
UBL21	23/3	6AU6	10/6
UC92	13/3	6B8G	4/-
UCC84	10/11	6BA6	7/6
UCC85	10/6	6BE6	8/-
UCF80	16/7	6BG6G	23/3
UCH21	23/3	6BH6	9/-
UCH42	10/6	6B16	9/-
UCH81	10/6	6BR7	12/6
UCL82	16/7	6BV6	9/-
UCL83	13/6	6BW7	8/6
UF41	9/-	6C4	4/6
UF42	17/3	6C5GT	6/6
UF80	13/11	6C6	5/-
UF85	9/-	6C9	17/3
UF86	17/11	6C31	7/6
UF89	9/-	6CD6G	29/10
UL41	10/-	6D6	5/-
UL44	26/6	6CH6	10/6
UL46	26/6	6F6G	7/6
UL84	9/-	6F6M	7/6
U06	19/11	6F1	14/-
U08	26/6	6F13	14/-
UYIN	12/6	6F14	26/6
UY41	7/6	6F15	14/-
UY85	7/-	6F18	15/3
VP13C	3/6	6F23	18/7
VP23	6/6	6F33	7/6
VP41	8/6	6H6	2/6
VR22 (PM2A)	3/-	6H6GT	2/6
VR105/30	8/-	6I5G	3/6
VR116	4/-	6I5GT	5/-
VR150/30	7/6	6I5M	6/6
VI120A	3/6	6I6	6/6
VU39 (MU12)	14/-	6I7G	6/6
VU11	2/6	6K7G	4/-
W101	8/-	6K7M	6/9
W61M	8/-	6K8G	7/6
W76	7/6	6K6GT	7/-
W77	8/6	6K7GT	5/9
W729	10/6	6K8GT	10/-
Y63	7/6	6K25	19/11
Z21 (4 pin)	8/6	6L6G	8/-
Z309	7/6	6L6M	9/6
Z359	7/6	6L7G	7/6
		6L1	23/3
		6L18	11/6
		6L19	23/3
		6LD20	15/11
		6M1	17/3

6N7GT	7/6	30FL1	10/6
6P1	19/3	30L1	19/11
6P26	19/11	30L15	23/3
6P28	26/6	30P4	15/-
6Q7G	7/6	30P12	12/6
6Q7GT	9/6	30P16	9/6
6SA7GT	8/-	30P11	12/6
6SG7	7/6	30PL13	21/11
6SH7	4/6	35L6GT	10/-
6SHT	8/6	25Y5	9/9
6SK7	6/-	35W4	7/6
6SL7GT	8/-	35Z4GT	8/-
6SN7GT	7/6	42	8/-
6SQT	9/3	35Z3	16/7
6U4GT	12/-	35Z5GT	9/-
6U5G	8/6	50C5	11/6
6U7G	8/6	50CD6G	29/10
6V6G	6/-	50L6GT	8/6
6V6GT	7/9	75	11/6
6X4	7/6	77	7/6
6X5G	7/-	80	8/6
6X5GT	7/-	142BT	3/6
6/30L2	12/6	185BT	33/2
7B6	10/6	210DDT	4/6
7B7	8/6	210VPT	3/6
7B8	6/6	83	10/-
7C5	8/-	301	10/6
7C6	8/-		
7D6	13/6		
7H7	9/-		
7Q7	9/-		
7S7	9/6		
7Y4	8/6		
8D2	2/9		
9D2	3/6		
10C1	17/3		
10C2	17/6		
10D2	12/-		
10F1	12/6		
10F3	23/3		
10F9	15/3		
10F18	15/3		
10L1	15/11		
10LD11	12/-		
10M2	23/3		
10P13	15/-		
10P14	19/3		
12A6	6/6		
12A8H	12/-		
12AT6	10/6		
12AT7	7/6		
12AU6	8/-		
12AU7	8/-		
12AX7	8/-		
12BA6	9/-		
12BE6	9/-		
12C8	9/-		
12H6	3/6		
12J5GT	3/6		
12J6T	10/6		
12K6T	13/6		
12K8M	13/-		
12Q7GT	7/6		
12S6T	7/6		
12SH7	6/-		
12S17	6/-		
12SK7	6/-		
12SL7	8/-		
12SN7GT	10/-		
12SQ7	8/6		
14S7	17/-		
15D2	7/9		
19AQ5	9/9		
19B6G	23/3		
20D1	15/3		
20F2	26/6		
20L1	26/6		
20P1	26/6		
20P3	23/3		
20P4	26/6		
20P5	23/3		
25A6G	10/6		
25L6GT	10/6		
25Z4	9/6		
25Z5	8/-		
25Z6	10/-		
27SU	19/11		
30C1	10/6		
30F5	10/6		

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Monarch UA8, 4-speed automatic record changers with Full-Fi turnover crystal cartridge, £6/19/6. Carriage 3/6. Colloredo Conquest, 4-speed fully mixing changer complete with Studio "O" crystal cartridge, £7/19/6. Carriage 3/6. Garrard RC120/D, Mk. II, 4-speed unit manual control to enable records to be played singly, £8/19/6. Carriage 3/6.

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Best Quality Recording Tape 1,200ft. on 7in. spool 21/- 850ft. on 5 1/2in. spool 18/6 600ft. on 5in. spool 13/9 200ft. on 3 1/2in. spool 5/3

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12 v. 25 A.H. (as on left) 45/- Carr. 7/6.



2 v. 100 A.H. 75 actual ex Govt., with carrying handle. Size 6½ x 6½ x 1½in. 15/- each. Carr. 3/6.

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6 for 24/- P. & P. 10/-.

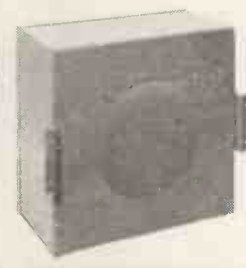
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VITAVOX PRESSURE UNITS TYPE N Heavy Duty. Special quality. 20 watts P.M. Brand new 80/- Ditto but in good order, 40/- Carr. 5/- on each.



NEW P.M. HEAVY DUTY SPEAKERS

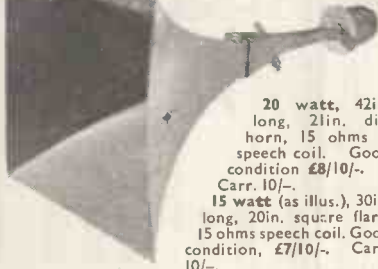
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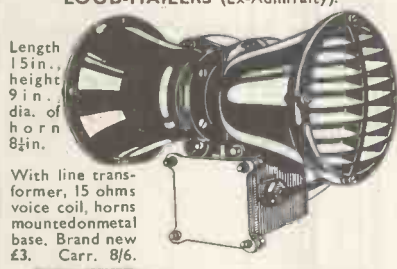
EXPONENTIAL HORNS by famous manufacturer of P.A. systems.



20 watt, 42in. long, 21in. dia. horn, 15 ohms speech coil. Good condition £8/10/- Carr. 10/-.

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PARMEKO TWIN BAKELITE LOUD-HAILERS (Ex-Admiralty).

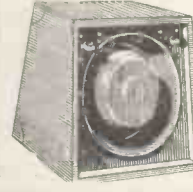


Length 15in., height 9in., dia. of horn 8½in.

With line transformer, 15 ohms voice coil, horns mounted on metal base. Brand new £3. Carr. 8/6.

TRUVOX/TANNOY LOUD-HAILERS

With 180 ohm line transformer and condenser. Impedance 7½ ohms, handling capacity 8 watts. Complete in slope-front wooden case. Brand new 25/- Carr. 4/6.



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6ft. channel uprights (as illustrated) £5. Carr. 15/-.

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19in. x 14in. PANEL SHELF in 14 s.w.g. steel. Suitable for above racks. 15/- P. & P. 5/-.



TELEPHONE SETS (TELE "F") Housed in Bakelite cases, complete with built-in ringing generators and batteries. Ideal between two or more positions up to practically any distance. Tested before despatched. ONLY 70/- P. & P. 3/6. 2 sent for £6/10/- Carr. paid.

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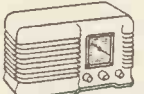
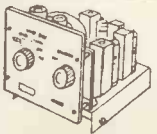
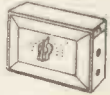
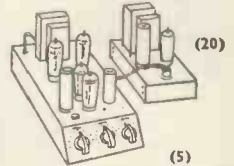
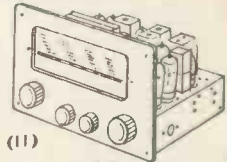
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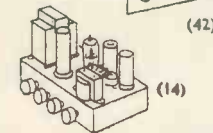
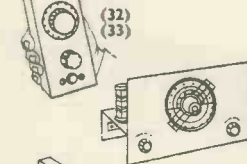
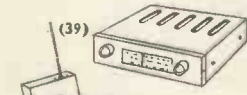
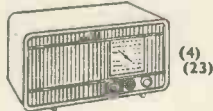
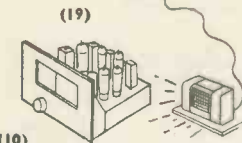
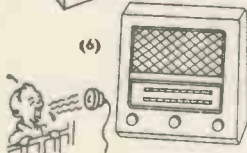
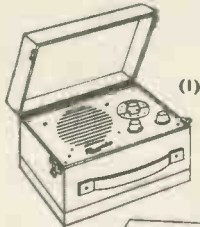
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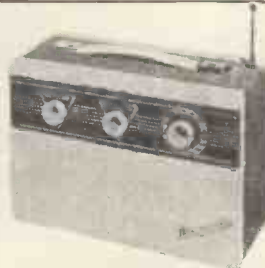


(22)



NEW! NEW! THE "WAVEMASTER" 7-TRANSISTOR LUXURY PORTABLE 400 MILLIWATTS OUTPUT

To build yourself! Medium and Long Waves—Push-Pull Superhet A.V.C. Perfect Car Radio reception. Size 10in. x 8in. x 4 1/2in. at base tapering to 4in. at top. Very attractive two-tone Vynide covered cabinet with cream and gold printed etoucheon plate, cream and gold knobs, handle and cabinet fittings. Weight complete with long-life 7 1/2 volt battery—4 1/2 lb. Mazda High-grade transistors throughout. High-Flux 7in. x 4in. Elliptical Speaker, slow motion tuning, coaxial socket at rear for direct connection to Car Radio Aerial. Improved reception by use of seven-section plated telescopic aerial disappearing into Cabinet when closed, 34in. above Cabinet when fully extended. Construction simplified by Bakelite chassis board with the following components already mounted—T.F. Transformers (2), Oscillator Coil, Trimmer Bank, Output Transformer, Intermediate Transformer, Aerial Brackets and Earth Bar. SPECIAL INCLUSIVE PRICE for all required components, full assembly instructions—nothing more to buy—is £10/19/6 plus 8/6 P. & P. Alignment service available. Full assembly instructions and individually priced parts list, all of which are available separately 2/6 post free.



NEW! THE R.C. TRANSISTOR SIX!

Now ready. Six Transistor Portable—Long and Medium Waves. Attractive blue/grey or red/grey portabel cabinet. Printed Circuit. Six New first-grade Ediswan Transistors. High Flux 7in. x 4in. Speaker, A.V.C., Ferrite Rod Aerial, Car Radio Aerial Socket. Size 12 x 8 x 4in. weight 4lb. including long life battery. Full assembly instructions and individual parts list 2/6 post free, and all required Components at special inclusive price £9/19/6, plus 3/6 P. & P.

VISIT OUR FULLY EQUIPPED
HI-FI SHOWROOM
AT TOTTENHAM COURT ROAD FOR
DEMONSTRATIONS OF THE LATEST
HI-FIDELITY EQUIPMENT
BY ALL LEADING MANUFACTURERS

We stock equipment of Quality by all leading makers: i.e., Leak, Quad, Armstrong, Dulci, Ferragraph, Reflectograph, Vortexion, Linear, Wharfedale, Grundig, Goodmans, W.B., Rogers, Garrard, Lenco, B.T.H., Pamphonic, Simon, Brenell, Collaro, Telefunken, Fi-Cord, etc., etc. A full range of high quality cabinets to suit all purposes is on show, i.e., "RECORD HOUSING," "W.B.," "A.D.," etc. Enquire about our interesting part-exchange scheme for personal callers.

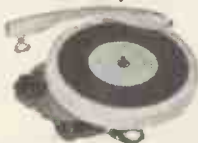


**ALLAN DOUGLAS
ELECTRONIC
ORGAN**

Readers will no doubt be pleased to know that our working model of this amazing organ for home construction, may now be heard and seen, at our Hi-Fi Showroom in Tottenham Court Road, W.1. For the benefit of constructors all components, keyboards, chokes, etc., are available ready made. Full constructional details are available in book form at 15/- plus 1/6 p. and p. We shall be happy to forward a complete price list on receipt of a stamp. Please address all organ enquiries for the attention of Mr. L. Roche.

RECORD PLAYERS
Full range at usual competitive prices. Interesting H.P. facilities.

COLLARO JUNIOR



4-speed turntable and pick-up complete with crystal cartridge and sapphire styli.
SPECIAL OFFER at only 75/- plus 2/6 P. & P. Or **TURN-TABLE** and **MOTOR** only at 52/6 plus 2/6 P. & P. **PICK-UP** only at 27/6 plus 1/6 P. & P.

B.S.R. TU9. 4-speed single-record unit with separate lightweight pick-up fitted with T.C.8H. crystal insert and sapphire styli. An ideal unit for a small portable gramophone. Brand new and fully guaranteed. **SPECIAL PRICE:** 75/- plus 2/6 P. & P. or motor and turntable only at 52/6 plus 2/6 P. & P. or Pick-up only at 27/6 plus 1/6 P. & P.

E.M.I. 4-SPEED STEREO SINGLE RECORD UNIT. Complete with Stereo Head and Sapphire Styli Brand New and Fully Guaranteed. **ONLY 66/19/6 plus 3/6 P. & P.**

GARRARD RC120/4H. 4-speed autochanger with GC2 insert. Brand new, fully guaranteed. 88/19/6. P. & P. 3/6.

GARRARD RC.121D MK. II STEREO/MONAUROAL 4-SPEED AUTOCHANGER. Complete with latest G73/1 plug in crystal head for Stereo or Monoaural recordings. Fully guaranteed. Few only. 111/0/6 plus 5/- P. & P.

B.S.R. U48 MONARCH. 4-speed Mixer Autochanger complete with turnover crystal insert and Sapphire Styli. Few only, now at 66/19/6 plus 3/6 P. & P. Brand new and fully guaranteed.

THE LATEST COLLARO "CONQUEST." 4-speed autochanger in cream with Studio "O" insert. Brand new, fully guaranteed. 67/19/6 plus P. & P. 3/6.

COLLARO "CONQUEST" STEREO/MONAUROAL. Latest type—full guarantee. Brand new. 68/19/6 plus 3/6 P. & P.

No. 38 AFV WALKIE-TALKIE. A wonderful offer. This famous trans-receiver unit, with relay operated SEND/RECEIVE switch, covering 7.4-9 Mc/s band, range approx. 5 miles. Good condition. **ONLY 22/6 plus 2/6 P. & P.** per unit (less accessories). Quantity export inquiries welcomed.

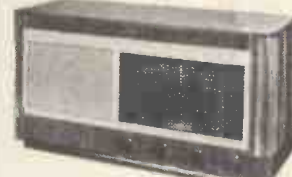
PNEUMATIC LID STAY with pressure-adjuster. Heavy duty 10/- complete. P. & P. 1/6.

TRANSISTORS I I I I
SURPLUS-P.N.P.

RED SPOT (Audio/Experimental Application) 5/- ea.
WHITE SPOT, R.F. up to 2.5 Mc/s 5/- ea.
Attractive discounts for bulk purchases. The above is a selection only. Full range in stock by all leading manufacturers. Let us have your enquiries.

(ALL POST FREE)

FRUSTRATED EXPORT—Not repeatable! L. M. and S.W. SUPER-HEATER RECEIVER. Manufactured by McCarthy for export. At present for operation on 6 volts, but conversion details supplied free.



Valve line-up: 6K8G, 6K7G, 6Q7G, 6FG6, 6X5G and 6 volt 4-pin non-synchronous vibrator. 8in. P.M. Speaker, 4 watts output, P.U. socket. Ext. L.S. socket, etc. Tone control. Fitted in polished wood cabinet, size 21 1/2in. x 10 1/2in. x 10 1/2in. These cabinets are slightly soiled owing to storage, but each is guaranteed unused, in serviceable condition, tested prior to despatch. Price 15/19/6 only plus P. & P. 7/6, plus 27/6 for A.C. Mains Conversion Components if required. **OUTSTANDING BUY!**
★ BARGAIN CORNER ★

SPEAKER BARGAINS
Goodmans 8in. x 2 1/2in., 3 ohms, 24/- plus 1/6 P. & P. 10in. Elac High Flux 3 ohm, 39/6 plus 2/6 P. & P. 8in. Celestion High Flux 3 ohm, 32/6 plus 2/- P. & P. 4in. Plessey Tweeter, 15/- plus 1/6 P. & P. R. & A. Type 9120, Mk. II, 12in., 10-12 watts, 3 ohm, 12,000 gauss, 55/- plus 3/6 P. & P. R. & A. Type 8120, Mk. II, 12in., 10-12 watts, 3 ohm, 10,000 gauss, 39/6 plus 3/6 P. & P. 12in. Bakers Selhurst, 15 ohms, 15 watts, 30-14,000 c.p.s., 14/10/- plus 3/6 P. & P. All the above brand new and fully guaranteed. Special! Latest E.M.I. full frequency speaker. Size 1 1/2in. x 8 1/2in., 3 ohm speech coil. Double cone. Unrepeatable at 39/6 Plus 3/6 P. & P.

12 CHANNEL TV TURRET TUNER (By famous manufacturer.)

Brand new, NOT surplus or ex-equipment, 35 Mc/s. I.F. PCC 84



and PCF 80 valves. Complete with coils: Band I Channels 1 to 5. Band III Channels 8 to 11. In manufacturers original carton. Fully guaranteed at only 39/6 plus 2/6 P. & P.

SUPER MAGNETIC RECORDING TAPE SPECIAL!!!

Trade enquiries invited!

First delivery Famous American Ferrodynamics Acetate Base High Quality Recording Tape. An enthusiast's "must." Brand new (NOT SUB-STANDARD), 5in. 600ft. 16/-, 5in. 900ft. 18/6, 5 1/2in. 1,200ft. 23/6, 7in. 1,200ft. 25/-, 7in. 1,800ft. 35/-. Professional quality "MYLAR" Du Pont 5in. 1,200ft. 37/6. 7in. 1,800ft. 44/-, 7in. 2,400ft. 60/-, each on plastic spool. P. free.



DECCA PORTABLE AMPLIFIER. As supplied in famous DECCA-MATIC III. Complete with small cream knobs. Full range tone and volume controls. Employs ECL82 valve. Size 3 x 3 1/4 x 8 1/2in. Only 59/6 plus 2/6 P. & P. **SPECIAL CELESTION** 8 x 6in. elliptical high flux loudspeaker 30/- plus 1/- P. & P. to fit.

VERY ATTRACTIVE PORTABLE CABINET in two-tone rexine covering for accommodating the above items and ancillary equipment. 75/- plus 5/- P. & P.

Note. If the above three items are purchased together they will be supplied at the special inclusive price of 172/6 plus 6/6 P. & P.

EXTRA SPECIAL OFFER!!

A small three-valve **PORTABLE RECORD-PLAYER AMPLIFIER** mounted on baffler 12 x 7in., with High Flux 6 1/2in. Loudspeaker. Valve line-up ECC83, EL84, EZ80. Incorporates separate bass and treble controls. Max. output 3 watts. Will match all types of high impedance pick-up. Ready to use, 15/12/6. P. & P. 3/6. **NEW STYLE CABINET** finished in two-tone Leatherette. Will accommodate above Amplifier and Baffle without modification. Also most types of Ancillary Equipment. Overall size 18 x 13 1/2 x 8 1/2in. Fitted with carrying handle, 13/9/6 plus 5/- P. & P.

NOTE. If both items purchased together they will be supplied at a special inclusive price 18/7/6 plus 6/6 P. & P.



LATEST COLLARO STUDIO TAPE TRANSCRIBER. 3 motors, 3 speeds: 1 1/2, 3 1/2, 7 1/2 i.p.s., takes 7in. spools. Push-button controls, 15/15/- plus 5/- P. & P. Usual H.P. facilities.

TAPE RECORDER AMPLIFIER for use with Collaro Studio Transcriber. Size 1 1/2 x 5 x 3in. Uses 3 valves, magic eye, contact cooled metal rectifier. Incorporates mike/gram/radio inputs, ext. i.s. jack, superimposing switch. 12/12/-. Complete with matching knobs (Gold/Black). Circuit, etc. Post 3/6.

LATEST B.S.R. "MONARDECK." Single speed Tape Deck. Takes 5 1/2in. spools—3 1/2 i.p.s. At 49/19/6 only plus 5/- P. & P.

**NEW COMPETITIVELY PRICED
TAPE RECORDER KIT
NOW READY!!**

3 watts output, printed circuit construction, valve line-up EF86, EL84, ECC83, EZ80 and EM84 recording indicator. Latest 9in. x 4in. High Flux Speaker. Complete with Tape and empty Spool, and Acos 39-1 stick mike with stand. Attractive two-tone Cabinet. Supplied with latest COLLARO Studio 3-speed deck. Total price 25 guineas. N.B. The amplifier kit is supplied with basic components already mounted on the printed circuit board. Full assembly instructions are included. Please add 7/6 for packing and carriage. All parts available separately. Full details on application.

**New City Branch now open at
99 CHEAPSIDE EC2**

Midway between Bank, Mansion House and St. Paul's station, and no more than one min. from each. Mon. to Fri., 9 a.m.-6 p.m. Sat. 1 p.m.

GLYNE RADIO LTD.



162 Holloway Road, London, N.7.
99 Cheapside, London, E.C.2.
18 Tottenham Court Road, London, W.1.

THE
COMPONENT
SPECIALISTS

VALVES

Brand new, individually checked and guaranteed

AC/DD	2/6	EA50	1/6	FW4/500	6/6	PM4DX	3/-	1A5GT	5/-	6F8G	6/6	12AH7	7/-	813	67/6
AC/P	4/6	EAC91	4/6	H30	5/-	PT25H	7/6	1C5GT	7/6	6F12	4/6	12AT7	6/6	815	80/-
AC/P1	2/6	EB34	1/6	H63	3/6	PY82	8/-	1D8GT	6/6	6G6G	3/-	12AU7	7/6	816	30/-
AC/SPENDD	4/-	EB91	4/3	KBC32	5/-	QP21	6/-	1E7GT	7/6	6H6M	2/-	12AX7	7/-	829A	30/-
AC6/PEN	5/-	EB91	3/7	KF35	5/-	QV25	5/3	1L4	3/9	6H6GT	1/9	12C8	7/6	843	7/6
AC/SP3	4/6	E1524	6/6	KT2	4/-	QV50 6-40	45/-	1LDS	3/6	6J5	3/6	12E1	22/6	861	15/-
AL60	6/-	EBC33	6/-	KT31	8/-	QV75/20	6/9	1R5	6/9	6J7	7/6	12H6	2/-	866A	10/-
AR8	5/-	EC52	3/-	KT33	4/-	QS95/10	6/9	1S5	6/-	6J5G	3/3	12ISGT	3/6	872A	35/-
ARDD5	2/-	ECC32	4/-	KT44	7/-	QS108/45	6/9	1T4	4/-	6L6	4/3	12SC7	4/6	930	8/-
ARP3	3/-	ECC81	6/6	KT63	6/-	SI150/15	6/9	2A3	8/-	6K6GT	6/6	12SG7	6/6	954	2/-
ARP2	2/9	ECC82	6/9	KT241	9/-	R10	12/6	2A6	7/6	6K7G	2/3	12SH7	4/9	956	2/-
ARP21	5/6	ECC84	7/9	KTW62	7/6	REL21	25/-	2C34	2/6	6K7GT	5/3	12S17	6/-	1619	5/-
ARP24	3/6	ECC91	4/-	KTW63	6/6	RK34	2/6	2D4A	4/-	6K8G	6/6	12SK7	5/-	1625	6/-
ARP34	4/6	ECL80	9/6	L30	4/6	SP2	4/-	2X2	4/-	6L5G	6/-	12SL7	7/-	1626	4/6
ATP4	2/9	EF22	7/3	MH4	3/6	SP14C	7/6	3A4	6/-	6L6	9/-	12SR7	6/-	1629	4/6
ATP7	5/6	EF32	5/-	ML4	4/-	SP13C	4/6	3B24	3/-	6L6G	6/6	15D2	6/-	7193	1/9
AU1	5/-	EF36	3/6	MPT42	5/3	SP41	2/6	3E29	3/-	6L34	4/6	15R	7/6	7475	5/-
AU4	5/-	EF39	4/6	MR15A	3/-	SP61	2/-	(829B)	60/-	6N7G	5/6	30	5/-	8010AR	22/6
AW3	4/-	EF50	2/6	N34	8/-	SP210	4/-	3Q5GT	9/-	6N7GT	7/-	35T	30/-	8013A	10/-
BL63	6/-	EF52	5/-	NR15A	3/-	STV280/40	12/-	3V4	7/3	6Q7G	6/3	35Z4	5/-	8020	6/-
BT45	40/-	EF54	3/6	NT37	10/-	SU2150A	4/9	4A1	2/6	6R7G	7/6	35Z4GT	7/-	9001	5/-
BT9B	40/-	EF55	6/-	OD3	5/-	T41	3/6	4D1	4/6	6R7GT	8/-	39/44	6/-	9003	5/6
D41	3/3	EF70	4/-	OZ24	5/-	TP25	15/-	5U4G	5/-	6SA7	6/-	53A	3/-	9004	4/-
D42	4/3	EF80	6/9	OZ4A	5/-	TT11	3/-	5V4	7/-	6SC7G	5/6	58	6/-	9006	4/-
D77	4/3	EF85	6/10	P61	2/6	U17	5/-	5Y3GT	6/9	6SC7GT	6/-	59	6/-	Cathode Ray Tubes:	
DA30	12/6	EF86	9/-	PCC84	8/-	U18	5/-	5Z3	8/6	6S7G	5/-	71A	4/6	3BP1	25/-
DAF86	8/-	EF89	8/9	PCC85	8/-	U27	8/-	5Z4G	8/-	6SH7	5/-	77	6/-	5BP1	35/-
DETS	15/-	EF91	4/10	PCF80	8/-	UL2	5/-	5A6	5/-	6S17	6/9	78	7/-	5CP1	42/6
DET19	2/6	EF92	5/-	PEN25	4/6	UL84	8/6	6AB7	5/-	6SF5	8/-	80	6/3	5FP7	45/-
DET20	2/6	EL32	3/9	PEN45	5/6	UL85	7/6	6AC7	4/3	6S17G	6/6	82	8/-	VCRX258 (with scanning coil)	45/-
DF70	9/-	EL35	9/-	PEN46	5/6	V238B	8/-	6AG5	4/6	6SK7	5/6	83V	12/-	Photo Tubes:	
DF72	7/6	EL84	8/3	PEN220A	3/-	V248A	4/-	6AG7	8/-	6SL7GT	6/9	84	12/6	GS16	12/6
DF96	8/-	EL91	7/6	PENDD1	3/-	VP23	3/6	6AJ7	4/3	6SN7GT	4/6	85A1	12/-	Special Valves:	
HD76	4/9	EM4	4/-	1360	9/6	VR78	4/-	6AK5	6/9	6SQ7	6/6	89	6/-	231	45/-
DK96	8/-	ESU208	8/-	PL81	11/-	VR99	8/-	6AK7	8/-	6SR7	6/6	210F	3/-	3J1481	45/-
DL72	7/6	EY51	7/6	LP82	8/-	VR105/30	7/6	6AM5	5/-	6SS7	5/-	210VPT 7 pin	2/6	3J170E	635
DL71	8/-	EY91	3/6	PL83	9/-	VR150/30	7/3	6AM6	6/3	6V6GT	5/6	217C	17/6	3J192/E	£37/10
DL96	8/-	EZ40	7/-	W31	7/-	VS110	4/6	6B4G	4/6	6V6GT	6/-	446A	14/-	723AB	52/6
E1323	25/-	EZ80	7/6	Y63	5/-	VT25	3/6	6BB	5/6	6X4	5/6	705A	17/6	726A	27/6
				Y11	11/-	VU111	3/3	6BBG	2/6	6X5GT	6/6	715B	97/6	ACT25	40/-
				Y66	8/-	VU120	3/-	6C4	4/-	723A/B	45/-	717A	8/6	CV691	60/-
				Y66	8/-	VU133A	3/-	6C5	6/-	7Q7	7/-	801	6/-	KR3	45/-
				Y66	8/-	W31	7/-	6C6G	4/6	810	8/3	803	22/6	WX7110	15/-
				Y66	8/-	Y63	5/-	6C8G	5/-	8D2	6/6	805	30/-	WL417A	15/-
				Y66	8/-	Y66	8/-	6E5	5/-	9D2	3/-	807 AMER	5/3		
				Y66	8/-	Z31	6/-	6F5G	5/6	10Y	8/6	807BR	3/9		
				Y66	8/-	IA3	3/6	6F6	7/-	12A6	5/-	808	8/-		

AND MANY OTHERS IN STOCK including Cathode Ray Tubes and Special Valves.

All U.K. orders below 10/- P. & P. 1/-; over 10/- 1/6: orders over £3 P. & P. free. C.O.D. 2/- extra. Overseas postage extra at cost.

BRAND NEW ORIGINAL SPARE PARTS FOR AR88 RECEIVERS.

Please write your requirements.

MOVING COIL ROUND HAND MICROPHONE No. 13. 2 1/2 in. diam. with press switch. 12/6. P. & P. 1/-.

PLATE TRANSFORMER. Input 190-210-230-250 v. Output 2,250-02,250 C.T. 400 mA, 13 x 9 x 6 1/2 in. Weight 75lb. £6/10/- Carr. 10/-.

I.F. TRANSFORMERS. 4-5 Mc/s. American made in black crackle finish housing. 6/- P. & P. 1/-.

HRO MAINS power pack, input 115/250 v. A.C. Output 250 v. 75 mA. and 6.3 v. 3.5 amps. £3, inc. carr.

VARIOMETERS for WJS No. 19. Fully tested and working 12/6. P. & P. 2/6.

COMPLETE V.F.O. UNIT from TX53. Frequency in 4 switched bands from 1.2-17.5 mc/s. Two V.T. 501s. as oscillator and buffer, 807 as driver, two 5130s as voltage stabilizers. Output sufficient to drive two 813s in parallel. Slow motion drive directly calibrated in mc/s. Provision for crystal control, metering of buffer and driver stage. Power requirements 400 v. and 6.3 v. D.C. Can also be used as low power transmitter. In excellent condition with valves and circuit diagram. £5. P. & P. 15/-.

FILAMENT TRANSFORMERS. Primary 0-190-210-230-250 v., 50 c/s. Sec. 1. 2.5 v. CT at 10 amps. 2. 2.5 v. CT at 10 amps. 3. 10.5 v. CT at 11 amps., 4,000 v. insulation. Price £2/19/- P. & P. 5/-.

LOW RESISTANCE HEADPHONES. Brand new, type CLR 5/-; Balanced Armature, 7/6. P. & P. 1/-.

TELEPHONE HANDSET. Standard G.P.O. type, new, 12/- P. & P. 1/6.

AVOMINORS in leather case with leads. Fully tested and guaranteed, with batteries. 2,000 v. D.C., £2/19/6. P. & P. 2/6.

NEW PRODUCT OF TAYLOR

Model 127A Pocket size meter. Sensitivity 20,000 o.p.v. D.C. 1,000 o.p.v. A.C.

20 ranges. D.C. current 50µA to 1 amp. D.C. volts 0.3 v. 1,000 v. (25 kV. by probe). A.C. volts 10 v. 1,000 v.

3 resistance ranges from 0-20 meg-ohms (self contained). Metre 40µA 3 1/2 in. arc. Accuracy D.C. 3% A.C. 4% ohms 5%.

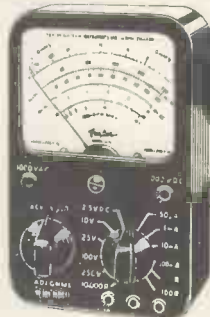
Dimensions 5 1/2 x 3 1/2 x 1 1/2 in. Weight 14 oz. Price £10 complete with instruction manual, test prods and clips. Leather case £1/12/- extra.

OUTPUT TRANSFORMER, in screening can giving 9 different ratios 10:1 up to 120:1 for battery receivers or any high resistance pentodes used as output valves, 6/6. P. & P. 1/6.

DRIVER TRANSFORMERS. Primary 500 ohms imp. Sec. to match two 805 in push-pull £1/7/6. P. & P. 5/-.

TRANSFORMERS. Relay supply. Primary 230 v. Sec. 0-27/29/31 v. at 0.5 amps., 15/- P. & P. 5/-.

ROTARY TRANSFORMERS. 171 watt, 12 v. input. 1,600 v. 110 mA. output, 30/- P. & P. 7/6.



COMPLETE SET OF STRONG AERIAL RODS (American). Screw-in type MP49, 50, 51, 52, 53, total length 15ft. 10in., top diameter 0.615in., bottom diameter 0.185in., together with matched aerial base. MP37 with ceramic insulator. Ideal for car or roof insulation. £2/10/-, post free.

AR88D and L.F. Receivers, completely overhauled and tuned, £60 and £57/10/- respectively. Completely rebuilt with P.V.C. wiring £85.

MODULATION TRANSFORMERS (U.S.A., Collins), primary imp. 6,000 ohms. C.T., secondary 6,000 ohms, 20 W., 9/6 each, post free.

R109 RECEIVER. Covering 2-8 Mc/s. 6 v. D.C. New and tested, £4/5/- Carriage paid.

VIBRATOR UNIT. 12 v./160 v. 35 mAmps. Exceedingly well filtered and smoothed, excellent for car radios. New. Including one 6X5G valve and vibrator. 17/6. P. & P. 5/-.

CARBON INSET MICROPHONE. G.P.O. type 2/6. P. & P. 1/-.

INSULATION TEST METER. Testing voltage adjustable up to 6,000 v. D.C. Mains supply 180/250 v. In wooden case £25. Carr. 10/-.

COSSOR DOUBLE BEAM OSCILLOSCOPES. 339A. Fully tested and working, £15. Carr. 10/-.

NO. 62 TRANSMITTER-RECEIVER. 1.6 12 mc/s in two ranges. Ideal for mobile use. Total 11 valves. Rx—A super with separate mixer and local oscillator. Tx uses QVO4-7 as power amplifier VFO or switched selected crystals. C.W., phone (grid modulation) metered for operation and valve testing, Pi output to match rod aerials or long wire "Press to send" operation from mike. Size 8 1/2 in. x 17 1/2 in. x 13 1/2 in. weighs only 29lb. Completely self contained with internal power unit for 12 v. operation. Power consumption 4.4 amps. on send, 3.4 amps. on receive. As new condition, tested, complete with operation instructions. Price £27/10/- Delivery included.

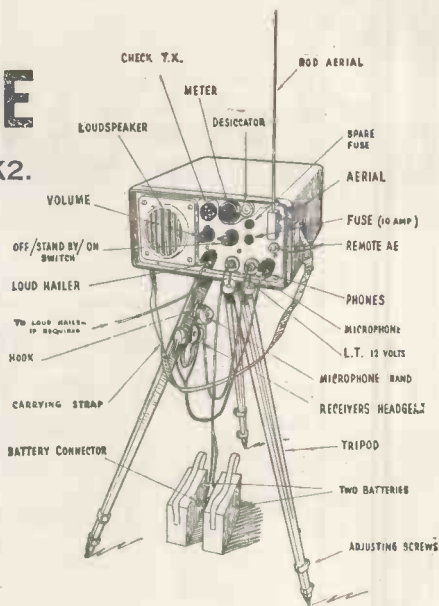
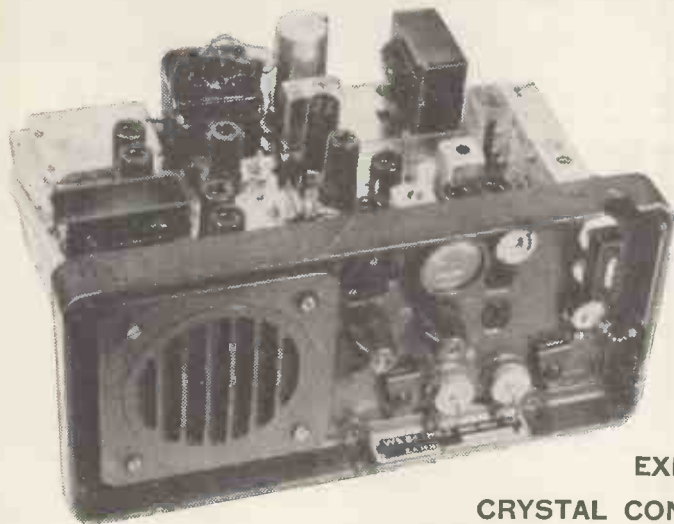
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V.H.F RADIO TELEPHONE

TYPE W.S B44 MK2.



EXPORT ONLY

CRYSTAL CONTROLLED 60-95mc/s.

A modern double superhet receiver and AM transmitter using the current series of B7g valves. Robust cast aluminium case includes loudspeaker. Operates from 12-volt accumulators or vehicle power supply, in fixed or mobile use. Each unit is fully tested and in good order. Available less crystals and accessories ex stock. Accessories can be supplied to meet most requirements together with crystals for specified frequencies. PRICE (FOB LONDON) £20 each. Special quotation for quantities up to 500 sets.

50 MICRO AMP MOVING COIL METERS

(Brand New & Boxed)

Made on Government Contract by Famous British Maker

3 1/8" Square—800 ohms resistance. 4 Scales operated by lever "Set-zero"—"0-3"—"0-30"—"0-300". Easily coupled to rotary range switch by cord or lever. Ideally suitable for transistor tester, output meter, volt-milliammeter.

A RANGE OF METER BOXES

Completely finished and enamelled, with all screws, sockets, etc., designed to take one or two meters and with provision for controls, caters for all kinds of applications of this meter.

One Meter, small 5/6, medium 7/6, large 10/6.

Two Meters, small 9/6, large 15/6.

Circuits for many applications—free.



Complete with data and circuits

one for **19/6** (plus post 6d in U.K.)

two for **35/-** (plus post 1/- in U.K.)

TEST GEAR COMPONENTS (LONDON) LTD

15 ARCANY ROAD, SOUTH OCKENDON, ESSEX TEL: SOUTH OCKENDON 2610

Premier RADIO

(Dept. W.W.) 23 TOTTENHAM COURT RD., LONDON, W.1. Tel.: MUSeum 3451/2

★ VISIT OUR NEW BRANCH AT 309 EDGWARE RD., W.2. TEL.: PADdington 6963

The Truchord 'MINUETTE' HIGH FIDELITY RECORD AMPLIFIER with 3D Sound System 14 Gns P. & P. 10/-



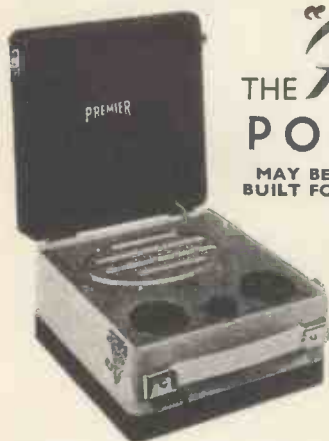
This Unit consists of a high quality 4-watt amplifier with separate bass, treble and volume controls, and also switching for L.P. standard records and radio, with separate inputs for pickup and radio. Valve line-up: EF86, EL84, EZ80. Specially wound Parmeko output and mains transformers are used. Two High-flux 8½ x 5½in. elliptical speakers are used, the units are mounted in an attractive good quality walnut cabinet, the top board of which is detachable and can be replaced by a further board which is cut out ready to accept a Garrard 4SP 4-speed single player. This board is included in the price, together with a matching lid. Cabinet size 17 x 16 x 9½in. The Amplifier as used in the above unit can be supplied separately complete with escutcheon at £6/19/6. P. & P. 3/6. Garrard 4SP 4-speed single player £6/19/6.

NO ELECTRICITY? Here's your answer

THE BERIC BATTERY RECEIVER

For 99/6 plus 5/- pkg. & post

This receiver is ideally suitable for use in the home or where normal electricity supply is not available, remarkable reception on both medium and short wavebands, incorporating latest-type miniature Battery Valves: DK92, DF96, DAF96, DL96 and operates on an external B.103 Battery or equivalent. The receiver is housed in an attractive two-tone metal case. Size 11½ x 7½ x 5½in. This receiver can also be supplied with 2 short wavebands instead of medium and short, covering 2.5-7 Mc/s. and 6.5-17 Mc/s. Price 79/6.



"Petite" THE PORTABLE MAY BE BUILT FOR £7-7-0

- plus 3/- Post & Pkg. Batteries extra.
- H.T. 10/- (Type B126) or equivalent.
- LT 1/6 (Type AD. 35) or equivalent.
- ★ High Q frame aerials.
- ★ High sensitivity on both wavebands.
- ★ Medium and long wave superhet circuit.
- ★ Instruction book 1/6.
- ★ Size only 8 x 8 x 4½in.
- ★ 4 valves of the economy type.

★ Weight including batteries 5½lb. ★ 4 valves of the economy type.

PREMIER BATTERY ELIMINATOR Housed in two containers which are to replace AD 35 and B126 batteries. KIT 37/6 plus 2/- post and packing. Only suitable for use with DK96 Series valves.



DRAMATIC PRICE REDUCTIONS

SUPERHET may be built for **£7.7.0** plus 3/- p.p.
T.R.F. may be built for **£5.10.0** plus 3/- p.p.

These two receivers [use the latest type circuitry and are fitted into attractive cabinets 12 x 6½ x 5½in., in either walnut or ivory Bakelite or wood 1/- extra. Individual instruction books 1/- each, post free.

RECORD CHANGERS

- BSR UAB 4-speed£6/19/6
 - Collaro Conquest 4-speed£7/19/6
 - Garrard RC120, Mark 2 4-speed£9/19/6
- Please 5/- each for packing and postage.



THE COSSOR TRANSISTOR POCKET RECEIVER

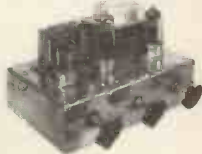
MAY BE BUILT FOR **£7-19-6**
 Plus 2/- P. & P.

This receiver uses the most up-to-date printed circuit method and with the aid of the easy to follow point-to-point instructions assembly is simplicity itself. Four first-grade Edison Swan transistors are used, one XA102, two XA101, one XC101 and two diodes. The receiver covers 190/550 metres on medium wave operating on a P.P.4 9-volt battery. When constructed it is housed in an attractive maroon leather case. Size 5½ x 3½ x 1½in., weight 17 oz. Ins. books available 2/6. Battery 2/-.

THE "MID-FI"

A NEW DESIGN 4½-WATT AMPLIFIER KIT MAY BE BUILT FOR 95/- Plus 3/- P. & P.

A new circuit for the home constructor requiring a good-quality medium-powered amplifier for reproduction of records or F.M. broadcasts. Technical specifications: separate bass and treble controls. Valve line-up: EF86, EL84, EZ80. Voltage adjustment for A.C. mains from 200/250 volt, 3 or 15 ohms impedance. Negative feedback. Size 7 x 5 x 2in., overall height 5in. Silver-hammered finished chassis.



TAPE DECKS

- Latest BSR Monardeck. Single speed 3½ i.p.s. Will take 5½in. spools £9/19/6, 5/- P. & P.
 - Collaro Studio Tape Transcriber. 3 speeds 1½, 3½, 7½ i.p.s. 3 motors. Push button controls. Will take 7in. spools. 15 gns., 7/6 P. & P.
 - Collaro Mk. 4 Tape Transcriber. Twin track operation. 3 speeds, 3½, 7½, 15 i.p.s. Will take 7in. spools. £17/19/6, 7/6 P. & P.
 - Tape Recorder Amplifier, specially designed to match the Collaro Studio Tape Deck. £12/17/6. P. & P. 4/-.
- Size 11½ x 5 x 3in., uses 3 valves, magic eye, contact cooled metal rectifier. Incorporates mike/gram/radio inputs, ext. l.s. jack, superimposing switch, with matching knobs.

RECORDING TAPE

- By well-known manufacturers, brand new, boxed and fully guaranteed.
- 1,800ft. on 7in. spool 32/6
 - 1,200ft. on 5½in. spool 22/6
- Postage and packing 1/- per spool.
- AMERICAN RECORDING TAPE**
 Manufactured by Ferrodynamics, brand new and fully guaranteed.
- 1,200ft. on 7in. spool 25/-
 - 1,800ft. on 7in. spool 35/-
 - 600ft. on 5in. spool 14/6
- Postage and packing 1/- per spool.

Get Finest Value from IRONGATE—England's Leading Equipment Wholesalers
Bulk Buying means LOWEST PRICES. All Equipment is in TIP-TOP condition

WORLD FAMOUS TELEPHONES



"F" TYPE
 IN ATTRACTIVE CASE
 The best portable telephone ever made. With a range of up to 5 miles is ideal for
FACTORIES, BUILDING SITES, FARMS, CIVIL ENGINEERING PROJECTS, OUTSIDE BROADCAST UNITS AND OFFICES.
 2 perfect sets (**SUPERIOR QUALITY**) in individual carrying cases, complete with long life batteries, bells, magneto and 100ft. telephone cable.

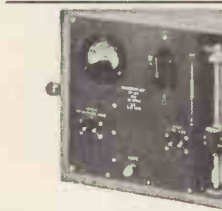
£7.10.0 per pair. Carr. 7/-.

TELE "F" HIGH POWER as above, but complete with amplifier, **£6/10/-** each. Carr. 12/6

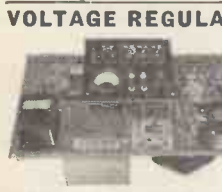
D3 STRANDED TELEPHONE CABLE.
 New Mile Drum 85/-, Carr. 17/6.
ENGLAND'S LARGEST STOCKS OF TELEPHONE EQUIPMENT



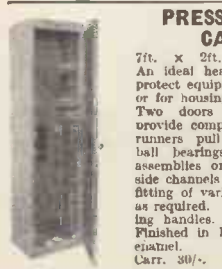
G.E.C. L.T. SUPPLY UNIT
OUTPUT: 24 volts 10 amps. D.C.
INPUT: 200/250 volts A.C.
 New and in original cases.
£13.10.0
 Carr. 9/6.



ROTARY CONVERTERS. 12 v. D.C. input. 230 volts A.C., 150 watts, 50 cycles output. Housed in wooden case and fitted with voltage control slider resistance switch, plugs and A.C. mains voltage output check meter. Supplied in perfect condition, individually tested, **£9/19/6** each. P. & P. 10/-.



VOLTAGE REGULATOR—115v.
 For relay control and motorised variac. Suitable for hand or automatic control. Mains Input Range 100/120 v. Separate meters for input and output reading. Contains complete overload cut-out (switch type) and sensitive 4in. moving coil (meter reading type). Handling capacity 8 amps. **£15.** Delivered Free.



PRESSED STEEL CABINETS
 7ft. x 2ft. wide. An ideal heavy-duty cabinet to protect equipment or instruments or for housing instrument panels. Two doors (front and back) provide complete access. Sliding runners pull out operating on ball bearings to carry chassis assemblies or shelving. Vertical side channels are pierced to allow fitting of variable height shelving as required. Positive action locking handles. Limited quantity. Finished in Dark Green sprayed enamel. Carr. 30/-.
£26.10.0

HEAVY DUTY 20 AMP. L.T. SUPPLY UNIT



Normal cost over £100 by **S.T.C.**
 Essential equipment for Electronic Engineering, research laboratories, schools. Ideal for battery charging, etc. Guaranteed for 20 amps. Output: D.C. Variable up to 20 amps, and 24 v. or trickle charge 125/350/700 ampere hours.
Input: A.C. 100/260 volts 45/65 cycles.
Size: 16 x 24 x 32in. high.
 In attractive Grey Cabinet.

ex Warehouse **£22-10-0**
 (Circ. diags and instr. loaned for 10/- deposit)

CONSTANT VOLTAGE TRANSFORMERS

FERRANTI 71-KVA MOVING COIL
 Stabilized output voltage in the range 200-250 v. Plug-board tappings. The selected output voltage is constant with $\pm 1\%$ at all loads 0 to 30/371 amps. when the supply voltage is varying over the range +8% to -12%.
 ● Frequency compensated 45-55 and 54-66 c/s.
 ● Excellent output wave-form.
 ● Can be used as a variable transformer.
 ● Unused. Complete with spares and instruction book at a fraction of the normal cost, only **£65.**
 ● A.C. MAINS STABILIZER.



AUTO TRANSFORMERS
 3 KVA Air Cooled (100% under-rated).
GUARANTEED 230/250 tapped, 12 amps.
 6 KVA 105/120 tapped, 28.5 amps.
 Made by well-known manufacturer and housed in strong metal case. Weight: 2 cwt. Brand new, in original maker's cases.
PRICE £15.0.0 Carr. 25/-.

EXPORT ONLY

Just released by the Ministry of Supply. "88" SETS. Manufactured by E. K. Cole. Walkie Talkie—3,000 available. "22" SETS ALSO—300 available only. TELEPRINTERS—120 Creed 7B for immediate disposal. Enquiries are invited for Bulk supply at reducing low prices.

MICRO SWITCHES

BURGESS BRAND NEW MINISTRY RELEASE (Mk. 4 BR. METAL BODY) UNIVERSAL CONTACT
 A.M. Ref. 50/4098
 Compare this remarkable almost half-price offer.
78/- per doz. (min. quantity) £25 per 100

1,000,000 YARDS !! SCREENED WIRE FLEX FOR ONLY 3d. per yard

For Immediate Delivery—priced far below cost. Specification: Close braided 14/10048 in. Covered .024 p.v.c. Tinned Copper. Screened. Assorted colours. Applications: Microphone leads, pick-up heads, etc.
ON MAKER'S REELS
 220 yd. REELS (min. quantity) 55/- P. & P. 5/-
TEN REELS £25. Carr. Paid.



SUPER POWER AMPLIFIER



Multiple Speaker System
 Output: 30 to 60 watts. Valves: Four 6L6, Parallel Push-Pull.
 Input: 200-250 volts.
 Leads, hand microphone, plugs and spares included. In robust wooden transistor case 17 1/2 x 15 1/2 x 2 1/2 in. Will take up to 20 Speakers.
£22/10/- Carr. 17/6.
 Speakers 18/6 each extra. 3/6 carr.

P.A. SYSTEM (EX GOVT.)

Complete with amplifier unit, 4 speakers, microphone, headphones and all spares packed in wooden cases. 6 or 12 volts D.C., handling capacity 8 watts. Ideal for cars, boats, factories, etc. **£7/10/0**, Carr. 30/-.

AERIAL MASTS

IMPROVED TYPE 50 MK.II 36 ft. HIGH

Kits comprise—six 2 1/2in. dia. Tubular Steel Sections of 6ft. length, top-section and base. Pickets, Guys and Fittings. YOU can purchase this normally expensive MAST for a fraction of its cost. Please add £1 for (returnable) wooden carrying case. The MAST is particularly suitable to take aerials for Tx., Rx. F.M. and TV. (especially COMMERCIAL) and has many other uses. Extra 6ft. sections can be supplied at 17/8 per section.
£8.10.0 only Carr. 15/8



U.S.A. Type 45ft. TELECOM. AERIAL MAST. (7 sections, 6ft. Bin. x 2 1/2in., guys, etc.). This entirely complete set in carrying case 12 1/2 Gns. Carr. 17/6. Or 2 sets for £25. Carr. extra. British Manufacture only.

ARMY TYPE 32ft. MASTS similar to above but 10 lin. screw-sections, suitable for permanent lightweight installation. Kit in canvas bag, **£3/15/-**. Carr. 7/6. Limited Quantity

36ft. TELESCOPE MASTS
 Finest quality brass. Non-rusting. Base diameter 2 1/2in. Complete with hand-winding winch for easy, rapid extension; and cable-wire bracing stays. One of the best masts ever produced. **£35** each. Carr. £1/10
 Winds down to 9ft.



AVOMETER MODEL D.

£8.19.6 (P. & P. 3/6)

D.C. Volts	A.C. Volts	D.C. Current	A.C. Current
150 mV.	7.5 V.	15 mA.	75 mA.
300 mV.	15 V.	30 mA.	150 mA.
1.5 V.	75 V.	150 mA.	750 mA.
3 V.	150 V.	300 mA.	1.5 Amps.
15 V.	300 V.	1.5 Amps.	7.5 Amps.
30 V.	600 V.	3 Amps.	15 Amps.
180 V.	750 V.	15 Amps.	
300 V.	1.5 KV.	30 Amps.	
750 V.			Resistance
1.5 KV.			0-1000 ohms.
			0-10 Kc ohms.

Thoroughly overhauled. Complete with batteries and instructions. An extremely robust meter at a very reasonable price.

CRYSTAL CALIBRATOR No. 10.

A crystal controlled heterodyne wave-meter covering 500 Kc/s. to 10 Mc/s. (Harmonics up to 30 Mc/s.) Requires 15 m/a. and 12 v. 0.3a D.C. but can be easily modified for 120 v. and 1.4 v. working. Size 7x7x4in. First class condition, complete with valves, crystal, instruction manual and circuit. ONLY 59/6. Post 3/6.

CHOKES. Parmeko 5 H, 200 m/amps., 6/6. AR-88 chokes, 15 H., 90 m/amps., 8/6. Parmeko 8 H., 100 m/amps., 7/6. Postage any type, 1/6.

SELENIUM BRIDGE RECTIFIERS. Funnel cooled. A.C. Input 45 v. RMS. D.C. output 30 v. 10 amps. BRAND NEW. Boxed. 45/-. Post 3/6.

MARCONI IMPEDANCE BRIDGE

Type TF373. Measures, L, C & R at 1,000 cycles. Accuracy 1%. 0-100H; 0-100µF; 0-1M Ω each in 5 ranges. Power Factor and "Q." First-class condition, £35, carr. paid.

6-VOLT VIBRATOR PACKS. HRO type, 180 v. D.C., 65 m/amps. BRAND NEW. 29/6, post 3/6. Type PU2, 200 v. D.C. 100 m/amps., with OZ4 rectifier. BRAND NEW, 25/- Post FREE.

ADMIRALTY HT TRANSFORMERS

Pri 230 v. 50 c/s. Secs. 620-550-375-0-375-550-620 v. (620 and 550 v. 200 m/amps., 375 v. 250 m/amps.), plus two 5 v. 3 Amp. rectifier windings. Total rating 278 VA. Upright mtg. Wt. 25 lb. Made 1953. BRAND NEW. Original boxes. 45/-. Carr. 5/-.

INSTRUMENT TRANSFORMERS.

230 v. A.C. input. Outputs 0.65-130-195 v. 85 m/amps., 6.3 v. 5 amps., 6.3 v. 0.3 amps. Shrouded. Size 3¼x3¼x3¼in. high. 15/-, post FREE.

AR88D MAINS TRANSFORMERS.

Input 110-240 v. Output 345-0-345 v. 125 m/amps., 6.4 v., 4.5 amps., 5 v. 2 amps. 4¼x4x5¼in. high. Wt. 12 lb. Ported. Tag ends. RCA BRAND NEW. Boxed. 29/6, post 3/6.

"C" CORE TRANSFORMERS.

Pri. 230 v. 50 c.p.s. 510-0-510 at 275 mA. 375-0-375 at 83 mA. 6.3 v. at 9 A. 6.3 v. at 2A (twice), 6.3 v. at 1A (twice), 6.3 v. at 1.5A. 6.3 v. at 0.5A, 5 v. at 3A. 6½ins. X 6ins. X7½ins. high. Weight 25lbs. Removed from equipment but in perfect condition, 52/6. Carr. 5/6.

MARCONI CR100

Completely overhauled. In perfect working order. LOOK LIKE NEW. £21. Later model with Noise Limiter, £25. Carr. Eng. and Wales 30/-. Send S.A.E. for full details.

RCA AR-88 SPEAKERS

A high quality 3 ohm unit fitted into heavy gauge black cracked steel cabinet, size 10½x11½x6in. Fitted with rubber feet and 6ft. lead. Ideal for extension speaker. CR100, etc. In original cartons. BRAND NEW. 45/-. Post 3/6.

MINIATURE 373 IF STRIPS.

For FM tuner described in "Practical Wireless." Complete with 3 of EF91, 2 of EF92 and 1 of EB91. A fresh release enables us to offer these once again. BRAND NEW. Complete reprint of conversion instructions and circuit supplied free. 35/- OR less valves, 12/6. Post, either, 2/6.

LOUD HAILER EQUIPMENT

IDEAL FOR CROWD CONTROL, FACTORIES, FETES, ETC. CONSISTS OF 4 SPEAKER UNITS AND CONTROL UNIT. COMPLETE WITH MICROPHONE, HEADPHONES AND SPARES. OPERATES FROM 12 VOLTS D.C. (OR 6 VOLTS D.C. WITH SLIGHTLY REDUCED OUTPUT), CONSUMING ONLY 3 AMPS. OUTPUT POWER 8 WATTS. ALL TESTED AND WORKING, BUT SLIGHTLY SOILED. A GENUINE BARGAIN. £4 19/6. CARRIAGE 25/6.

SIGNAL GENERATOR TYPE 54.

Marconi 762A. Frequency 430 to 610 Mc/s. Square or Pulse Int. Mod., provision for Ext. Mod. Attenuation range +10 to -100 dB. Directly calibrated dials. As new, £35, carr. paid.

COMMUNICATIONS RECEIVERS R-1155B.

A first class 10 valve Communication receiver, covering 75 Kc/s. to 18 Mc/s. (16.2-4,000 m.) in 5 bands. The large scale and superior dual ratio slow-motion drive make tuning easy, and the R.F. stage and 2 I.F. stages ensure world-wide reception. All the receivers we sell have been thoroughly overhauled, completely re-aligned, and are in first class working order, ONLY 59/19/6.

A.C. MAINS POWER PACK OUTPUT STAGE.

In handsome black-cracked steel cabinet to match the R-1155. Fitted with RCA 8in. speaker. JUST PLUG IN and switch on! Only the finest quality components are used, and we guarantee OUR power packs for 6 months. ONLY 56/10/- Deduct 10/- when purchasing receiver and power unit together. Send S.A.E. for further details, or 1/3 for 14 page illustrated booklet giving technical data and circuits etc. (FREE with each receiver.) Add 10/6 carriage for receiver, 5/- for power unit.

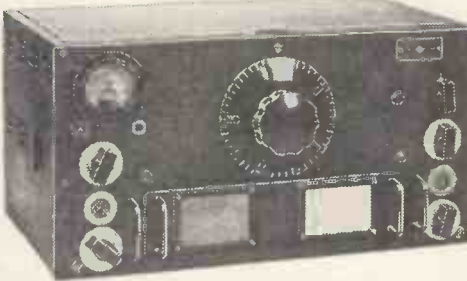
T.C.C. VISCONOL CONDENSERS.

8 mfd. 800 v. D.C. wkg. at 71 deg. C. CP152V. Size 3x1¼x5in. high. BRAND NEW. Boxed. 8/6 each, post paid.

MINIATURE RELAYS (ALL BRAND NEW and BOXED)

G.E.C. sealed, wire ends, 670 2M2B H/D M1095..... 8/6
G.E.C. sealed, wire ends, 670 Ω, 2 H/D makes, M1099... 15/-
G.E.C. sealed, wire ends, 670 Ω, 4 c/overs, platinum, M1092 19/6
G.E.C. sealed, wire ends, 5,000 Ω, 2 c/overs, platinum, M1052 17/6
Siemens High Speed, 1K+1KΩ, 1 c/over..... 10/6

HRO SENIOR RECEIVER



Complete with ALL NINE general coverage plug-in coil sets for 50 Kc/s. to 30 Mc/s. Instruction booklet, and circuit, but less external power supply unit. Table models, as new condition, 21 GNS. Rack mounting, 18 GNS. Packing and carriage 22/- extra. Send S.A.E. for further details. HRO POWER PACKS. 115/230 v. A.C. mains input. Tested, and in good condition. Table or rack, 69/6. Post 4/-.

CHARLES BRITAIN (Radio) LTD.

11 UPPER SAINT MARTIN'S LANE LONDON, W.C.2 TEMple Bar 0545

One minute from Leicester Sq. Station. (Up Cranbourne St.) Shop Hours: 9-6 p.m. (9-1 p.m. Thursday.) Open all day Saturday

TRIPLETT METER MOVEMENT



This article consists of a basic 400 microamp meter movement mounted on a bakelite panel 5¼x2½. The dial is scaled as a 15 range Testmeter. A circuit and parts list of the original instrument is supplied.

BRAND NEW. Boxed. 35/-, post paid.

ELECTROSTATIC METER. Dia. 6½in. reads 5-185 Kv. Manufactured 1953. Contained in wooden case 10x10x9in. high. £9/19/6. Post paid.

SANGAMO-WESTON ANALYSER E772.

A useful multi-range meter. Thoroughly overhauled and in perfect working order. For full details see previous adverts. £7/10/-. Carr. 4/6.

AVO LC and R BRIDGES. Capacity 5 pFd to 50 mFd. Resistance 5 ohms to 50 megohms. Inductance can be measured against external standard. Balance is indicated on a meter, which can be used as a valve voltmeter from 0.1 to 15 v. Leakage test and Power Factor scale. For use on A.C. mains. Tested and guaranteed. £8/10/-, Post 3/6.

HICKOCK I-177 VALVE TESTERS.

Checks dynamic mutual conductance, checks, emission, gas, and noise. For UX4 UX5, UX6, UX7, Octal, Local, 87G, and Acorn types. Portable, in wooden carrying case 15½x8x5¼in. Wt. 13½lb. BRAND NEW. Complete with instruction book and valve testing charts. For 117 v. A.C. 10 gns. Carr. 7/6. Matching auto. transformers for 230 v. A.C. 12/6.

MARCONI SIGNAL GENERATORS

85 Kc/s. to 25 Mc/s. A.C. mains operation. In fair condition and good working order. TFI44F. £40. TFI44G. £50.

MARCONI TF987/I NOISE GENERATORS.

Range 100 Kc/s. to 200 Mc/s. Determines noise factor of AM and FM receivers. Fully stabilised H.T. supply A.C. mains operation. Brand new and in original boxes. £15. Carr. 7/6.

MARCONI TF340 OUTPUT METERS.

Perfect working order, £9/19/6. Carr. 7/6.

SCR522 TRANSMITTER/RECEIVERS.

100-150 Mc/s. Comprises BC624A rec., and BC625 trans., with valves, and in good condition. BC624A, less relay 19/6. With relay, 25/- BC625 22/6. These two, on rack 47/6. Carr. 7/6.

MOVING COIL PHONES.

Finest quality Canadian with chamois ear-muffs and leather-covered headband. With lead and jack plug. Noise excluding and supremely comfortable. 19/6. Post 1/6.

RESISTORS

Morgan "T" (½ watt) and "R" (1 watt). Latest types, all BRAND NEW. 100 assorted, 10/- Post 1/-.

HEAVY DUTY SLIDER RESISTORS.

1.25 Ω 20 A., 12/6, post 3/6. 1 Ω 12 A., 8/6. ZENITH ADJUSTABLE 25 Ω 4 A., 8/6. Post 2/6.

PRECISION RESISTORS.

1 Megohm. 1% 1 watt wire wound, Ex-U.S.A. BRAND NEW. 10/6 per dozen.

D.C./A.C. CONVERTERS.

Input 12 v. D.C. Output 230 v. 50 c/s. A.C. at 135 watts. Fitted with 0-300 v. A.C. 2½in. meter and slider resistor for voltage adjustment. In stout wooden carrying case with lid. Perfect working order. £9/19/6. Carr. 10/6. 24 v. Input 230 v. A.C. 50 c/s. 100 watts output. In grey metal case. BRAND NEW. 92/6. Carr. 7/6.

RADIATION METERS.

Portable dose-rate meter, containing modern type rectangular 50 micro-amp. meter, CX494 electrometer valve, etc. BRAND NEW. In canvas carrying case, £3/19/6. Post 2/6. For details of other equipment, see our previous adverts.

SAMSON'S SURPLUS STORES LTD.

LONDON'S GREATEST DEALERS IN RADIO AND ELECTRONIC EQUIPMENT

HEAVY DUTY L.T. TRANSFORMERS

- All ratings tropical and in perfect condition.
- No. 1. Pri. 210-230 v. Sec. 10 v. C.T. 5 A. and 5 v. C.T. 10A. Admiralty rating, 27/6, carr. 3/6.
 - No. 2. Pri. 230 v. Sec. tapped 4, 6, 11 v. 200 amps. £8/10/-, carr. 7/6.
 - No. 3. Pri. 200-250 v. Sec. 50 v. 30 A. £6/10/-, carr. 7/6.
 - No. 4. Pri. 200-240 v. Sec. 50 v. 20 A. £4/10/-, carr. 7/6.
 - No. 5. Pri. 200-250 v. Sec. tapped 28, 29, 30, 31 v. 21 A. £4/17/6, carr. 7/6.
 - No. 6. Pri. 100-250 v. Sec. two separate windings tapped 15, 16, 17 v. 4 A. 35/-, carr. 4/-.
 - No. 7. Pri. 220-240 v. Sec. three separate windings 6.5 v. 50 A., 6 v. C.T. 15 A., 6 v. C.T. 2.5 A. £4/19/6, carr. 7/6.
 - No. 8. Pri. 220-240 v. Sec. 6.3 v. 15 A. 25/- p.p. 3/6.
 - No. 9. Pri. 220-240 v. Sec. four separate windings 3 x 5 v. C.T. 4 A., 4 v. 4 A., potted type. 32/6, p.p. 3/6.
 - No. 10. Pri. 220-240 v. Sec. three separate windings 3 x 6.3 v. C.T. 4 A., potted type. 29/6, p.p. 3/6.
 - No. 11. Pri. 200-240 v. Sec. 6.3 v. C.T. 3.25 A. 30 v. 1.2 A. 17/6. P.P. 4/-.
 - No. 12. Pri. 220-240 v. Sec. 45 v. 2 A. 17/6, carr. 3/6.
 - No. 13. Pri. 200-240 v. Sec. 12 v. 40 A. Built in strong metal case with carrying handle. 52/6, carr. 4/-.
 - No. 14. Pri. 200-240 v. Sec. tapped 9-15 v. 4 A. 22/6, p.p. 2/6.
 - No. 15. Pri. 220-240 v. Sec. tapped 10, 17, 18 v. 10 A. 52/6, carr. 4/-.

BRAND NEW AMERICAN OIL-FILLED POTTED LF CHOKES. 8 H. 800 mA. 26 ohms. 7,000 v. R.M.S. test. 45/- Carr. 7/6.
 3 H. 600 mA. 25 ohms. 18,000 v. R.M.S. test. 45/- Carr. 7/6.
 11 H. 600 mA. 65 ohms. 4,080 v. R.M.S. test 45/- Carr. 7/6.
 10 H. 200 mA. 135ohm. 2,000 v. R.M.S. test 12/6. P.P. 3/-.

S.T.C. FIELD TELEPHONES.

Type YA7783. Buzzer calling, operates from 4½ v. battery. A self contained unit which can be easily held in one hand. Ideal for Aerial Riggers. Building sites, farms, workshops, etc. Size 9½in. x 2½in. x 2½in. Supplied brand new, complete with 4½ v. battery. £5/10/- per pair P.P. 3/6.

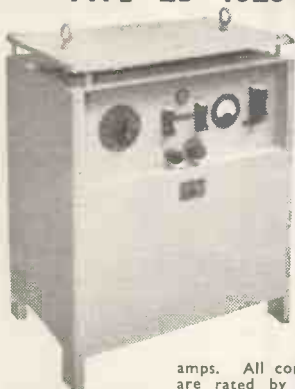
BRAND NEW TELEPHONE CABLE.

Twin D.8, one-mile drums £7/10/- Carr. 15/-.
 Twin D.3, 500-yd. drums, 35/- Carr. 7/6.
 Single D.3, one-mile drums, 85/- Carr. 7/6
 also 1/3rd-mile drums, 27/6 Carr. 5/-.
 Commando Assault Cable, P.V.C. covered, 1,000-yd., drums, 8/11 carr. 4/- Cartons of five drums, 42/6 Carr. 7/6.

VENNER 14-DAY CLOCKWORK TIME SWITCHES. One make one break every 24 hours. Complete with key and mounting bracket. 1-amp. 230 v. contacts, 27/6. 5-amp. contacts, 32/6, p.p. 2/-.

SPERRY H.T. TRANSFORMERS. Tapped Pri. 110-250 v. Sec. 450-0-450 v. 106 M.A. 6.3 v. 2 A., 6.3 v. 1.5 A., 5 v. 3 A Potted. type. Brand new. 35/- Carr 5/-

S.T.C. BATTERY CHARGER TYPE ZB 10234



A.C. input 100-260 volt 45-65c/s. D.C. output 24 volts 10amps. at max. ambient temperature of 131° F. but guaranteed max. output of 20

amps. All components are rated by manufacturers at this current. The charger is fitted with 20 amp. fuses on the D.C. output, 10 amp. fuses on the A.C. input. 2½in. 0-20 M.C. D.C. ammeter. On/off full charge/trickle charge switch. Heavy duty output terminals and mains neon indicator lamp. Behind control panel are mounted full charge ballast and trickle charge resistances. These units are designed to charge all 24 volt lead-acid battery combinations. That is two 12 volt or four 6 volt batteries in series at a 20 amp. max. rate. Can also be used for trickle charging 24 volt batteries at 125, 350 and 700 m.a.; are ideal for the electronic industry, research laboratories, schools, etc., as a general purpose L.T. supply unit. Supplied brand new at a fraction of maker's price. Size: 2ft. x 1ft. 3½in. x 2ft. 8in. Weight: 14lb.

£22-10-0 Ex warehouse.

JUST ARRIVED. PARMEKO POTTED LT TRANSFORMERS. No. 1. Pri. 230 v. Sec. 24 v. 2 A. Tropically rated. Mounted in metal case with fitted fuses and neon indicators. Size 8½ x 4 x 4in. 25/- P.P. 3/6. No. 2 Pri. 230. Sec. 10 v. C.T. 10 A. and 4 v. 7 A. Brand new 32/6. P.P. 3/6.



BRAND NEW AMERICAN AIRCRAFT LANDING LIGHTS. 250 watts. 8in. dia. Retractable reflector. Operated by fitted geared motor. 24 volt. 37/6. Carr. 5/-.

AMERICAN CAPACITORS OIL-FILLED. 4 mfd. 4,000 v. wkg. 17/6. P.P. 3/6. 5 mfd. 1,500 v. wkg. 7/6. 8 mfd. 1,000 v. wkg. 8/6. 16 mfd. 400 v. wkg. 8/6. 45 mfd. 200 v. wkg. 10/6. 2 mfd. 1,500 v. wkg. 5/6. 1 mfd. 750 v. wkg. 3/6. 0.1 mfd. 7,500 v. wkg. All capacitors tropically rated and supplied brand new and guaranteed. Please add 2/- P.P.

SPECIAL PURCHASE !!

NIFE ALKALINE BATTERIES. 6 VOLT. 75 A.H. TYPE LR7. SUITABLE FOR ENGINE STARTING. Five 1.2v. cells crated and connected to give 6 v. Brand new and fully guaranteed. Size of crate 15½ x 12 x 6¼ins. £7/10/- carr. 15/-.

HEAVY DUTY SLIDING RESISTORS

- (1) 26 ohms. 6-5 A. Double tube slider control, 45/- P.P. 3/6.
 - (2) 0.4 ohms. 25 A. Geared drive control, 17/6. P.P. 3/6.
 - (3) 1,000 ohms. 100 mA. Enclosed type slider control, 17/6. P.P. 3/6.
 - (4) 80 ohms. 0.5-5 A. Slider control. Ex. equipment, 15/- P.P. 3/6.
 - (5) 1 ohm. 12 A., 8/6. P.P. 2/6.
 - (6) 1.2 ohms. 15 A., 12/6. P.P. 3/6.
 - (7) 3 ohms. 10 A. 15/- P.P. 3/6.
- Above four types single tube slider. Fixed resistors 605 ohms. 2.8-0.4 A., 10/- 17.5 ohms. 5 A. 12/6. 1 ohm. 12 A. 5/- 496 ohms. 0.5 A. 7/6. P.P. on all above types 2/-.

S.P.E. BOOSTER FUEL PUMPS TYPE 1207 Mk. I. 112 v. D.C. 3.25 A. 1,200 G.P.H. 11 P.S.I. Submerged flange mounting. Brand new 65/- Carr. 7/6.

MASTER RADIO 12 VOLT VIBRATOR PACKS. Complete with 4 pin vibrator and OZ4 rectifier. Output 250 volts 75 mA. Size 5½ x 4 x 6¼ins. Brand new 25/- P.P. 3/6.

OIL FILLED HEAVY DUTY L.T. TRANSFORMERS. Pri. 380-400-420 v. Sec. 19 v. 150 amps., single phase. Weight 141 lb. Supplied dry. Price £10. Carr. 15/-.

ADMIRALTY THREE-PHASE TRANSFORMERS. Pri. 400-440 v. 50 cycles. Sec. 50 v. 6 amps. Completely tropicalised. Size 7½ x 14 x 5in. weight approx. 60 lb. Brand new in maker's cases. Price 85/-, Carr. 7/6.



L.T. SUPPLY UNIT No. 19 YA 8087. A.C. input 100-250 v. D.C. output tapped 12/24 volts, continuous tropical rating, 3 amps. Built in metal case 17 x 7 x 6¼in., with fuses and switch. An ideal L.T. supply unit for operating relays, contactors, battery charging etc. In perfect condition £3/17/6. Carr. 7/6.

S.T.C. F.W. RECTIFIERS. Brand new. Max. A.C. input 75 volts. Output 18 amps. £7/10/- Carr. 5/-.

L.T. CHOKES to smooth 12-24 v. 5 amps. Res. ½ ohm, 17/6. Carr. 5/-.

AMERICAN OHMITE RHEOSTATS. 15 ohms. 2.24 A., 12/6. 25 ohms 0.75 A., 15/6. 350 ohms, 25 watts, 3/6. Tubular adjustable. Length 10¼in., dia. 1½in. 2 ohms 6 amps, 7/6. 100 ohms 1 A., 5/6. P.P. on all resistors 2/-.

CENTRE ZERO M.C. METERS. 5-0.5 mA., 2½in. round, flush, 27/6. P.P. 2/-.

NUTS, BOLTS, WASHERS. Special bargain offer 5/- carton of 2, 4, 6 B.A. nuts, bolts and washers. P.P. 1/- SLEEVING, mixed bundle, 1½-4 mil., various colours. Wonderful offer. 2/6. P.P. 9d.

THERMOSTATS. A.C. 250 v. 15 AMP. 1½in. stem. Adjustable from 100-190 degrees F. Complete with sleeve, 22/6. P.P. 2/6.

HEAVY DUTY AUTO TRANSFORMERS

Tropically rated at 5 KVA. Tapped 250-240-230-220-120-115-110-105 v. Completely enclosed in metal case. Size 23 x 14 x 1½in. Weight approx. 2 cwt. Brand new. Price £15 ex-warehouse.

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AMPLIFIERS, STEREO AND MONAURAL, BY:
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DEFINITELY THE LAST FEW
 At this drastically reduced price. The famous R.C.A. orphonic amplifier. 12-20 watt output. Distortion: harmonic less than 1% at 10 watts/700 c.p.s. Noise Level: 85 D.B. below rated output. Frequency Response: within .2D.B., 20/25,000 c.p.s., within .5 D.B., 10/60,000 c.p.s. Feedback: 40 D.B. total. Output Impedance: 3.4 ohms, 7 ohms and 15 ohms. Spare Power: 395 v./45 M.A. and 6.3 v. 2.5 amps. for pre-amp, radio tuner and tape amp. A.C. Input: 100/150 v. and 200/250 v. Valve Line-up: two EF86, two KT66, one GZ32. Dimensions: 16½ x 8 x 7½ in. Weight: 32lb.
 Complete with circuit and instructions £18/19/6 plus 10/- crating and carriage.

THE JUNIOR RCA 3-8 WATT PUSH/PULL AMPLIFIER

A compact Amplifier complete with plug-in Power Pack, valve line-up HY90, 2-19AQ5 and 12AX7, separate bass and treble control, suitable for Speakers of 15 ohms impedance and two 3-ohm tapings for Tweeters. For use on A.C. mains, tapping 115-150 and 210-250 can also be supplied with Power Pack suitable for AC/DC mains. PRICE COMPLETE WITH ESCUTCHEON AND KNOBS, £6/19/6, 3/3 post and pkg.

THE VERDIK "QUALITY TEN"

10 watt push-pull ultra linear hi-fi amplifier with hi gain pre-amp. Mic., radio, gram and tape inputs, bass and treble controls. Beautifully finished. Control panel in gold lettering on grey green. Fully guaranteed. Original price 23 gns. Our price £14/19/6. P. & P. 7/6.

SPECIAL OFFER

2 valve 3 watt printed circuit amplifier made by famous manufacturer, completely assembled, needs output T x F and speaker, at the very low price of 39/6, plus 2/6 post and pkg.

BRAND NEW AND GUARANTEED

7in. reels of 1,200ft. P.V.C. base tape, 21/-, plus 1/6 post and pkg.
 5in. reels of 600ft. P.V.C. base tape, 14/6, plus 1/6 post and pkg.
 4in. reels of 300ft. P.V.C. base tape, 9/6, plus 1/- post and pkg.
 7in. reels of 1,800ft. L.P. P.V.C. base tape, 32/6, plus 1/6 post and pkg.
 5½in. reels of 1,200ft. P.V.C. base tape, 25/-, plus 1/6 post and pkg.
 Brand new E.M.I. 7in. take-up spools in polythene bag, 3/9 each post free, 6 for 20/-.
 The New American Audio Tape with plastic base. Also supplied in green or blue at no extra cost.

3in. reel 150ft. ... 6/- 4in. reel 300ft. ... 10/6
 5in. reel 600ft. ... 18/- 7in. reel 1,200ft. ... 30/-
 Post and packing 1/- per spool.

HI-FIDELITY TAPE HEADS

Made by famous manufacturer. Brand new. Upper or lower track, record/play-back, high impedance giving up to 12,000 c.p.s. at 7½ I.P.S. output 5 mvolts at 1 KC at 7½ I.P.S. Erase heads low impedance. Only 39/6 per pair. Post 1/- . State upper or lower track.

THE NEW "INSTANT" BULK TAPE ERASER
 Can erase a spool of magnetic tape in a few seconds. Demagnetises oxide deposits on tape heads. Only 27/6, post free.

THE NEW TAPE EDITING BLOCK. For standard ½ in. mag. tapes. Can be fixed to tape deck. Only 7/6, 6d. post and pkg. The new Acos telephone adaptor can be attached to any recorder. 21/- post free.

ANOTHER SNIP FOR TAPE RECORDER CONSTRUCTORS.

The new Collaro studio tape deck using 3 motors, 3 speeds at 1½, 3½ and 7½ I.P.S., will take 7in. spools, push button controls, £12/19/6, 5/- post and pkg. Well designed tape recorder amplifier (not a kit) for the studio deck, incorporating Mic/Gram/Radio inputs, ext. loudspeaker, super imposing switch, with matching knobs, separately mounted mains transformer. Frequency response 60-10KC 3DB at 7.5 I.P.S., magic eye level indicator. Using ECC 83, ECL82 and EM85 and Metal rectifier. Assembly instructions. The 2 units, £25/10/- complete. Crating and Insurance, 17/6. Suitable Acos mic. 40 for above, 25/-.

A repeat of our previous popular offer. The Collaro Mk. IV tape transcription tape deck, £17/10/-, Crating and carr. 11/6. The Collaro tape pre-amp and powerpack. The 2 items £30 complete. Crating and carriage 17/6.

THE LATEST BSR. Monardeck 3½ I.P.S., single speed. 5½ spool simple controls. Brand new, £9/19/6, Carriage free.

A FEW ONLY. The famous Cossor battery portable radiogram with Garrard motor and pick-up. Plays 45 r.p.m. records. Ideal for picnics and use in the car or garden. Brand new, £13/19/6 exclusive of batteries. P. P. 4/6

A FEW SNIPS IN SPEAKERS

Brand new Perdio 2½ in. speakers for transistor constructors.
 3 ohms, 5 ohms or 25 ohms 19/6, 1/6 P. & pkg.
 5in. Hiflux heavy magnet speaker 16/6, 1/6 P. & pkg.
 8 x 5 Hiflux heavy magnet speaker 17/6, 1/6 P. & pkg.

Ideal for stereo. 10in. Hiflux speaker's by famous manufacturer. 30/-, plus 2/- post and pkg.

SPECIAL OFFER

For the Hi-Fi enthusiast—Collaro 4-speed transcription motor and p/up using the new TX88 Studio cartridge. Brand new. List price £19/10/- . OUR PRICE £15/19/6. Crating and carr. 12/6. Easily wired for stereo to use Ronette stereo t/o cartridge.

BARGAINS IN PICK-UP CARTRIDGES

Brand new and complete with sapphire styli.
 B.S.R. T.C.8, less bracket, 15/- each.
 B.S.R. Hi-G, 37/1; with bracket, 17/6.
 Acos Hi-G 59, with bracket, 17/6.
 Acos Hi-G, with bracket, 17/6.
 Starr LP and 78 dual stylus cartridge 15/- .
 Post and packing 9d. extra.

REPEAT OFFER

A GIFT FOR THE SERVICE MAN

BRAND NEW IN WOODEN CASE
 The Weston Model 772 Type 6 super sensitive analyser. This precision designed multi-range test instrument has a large visible finely divided scale giving some of the range shown.

Range: D.C. volts 20,000 ohms per volt or 1,000 per volt. 2.5 volt range 53,000 ohms. 10 volt range 200,000 ohms. 50 volt range 1 megohm. 250 volt range 5 megohms. 1,000 volt range 20 megohms. Ohms: 0-3,000 ohms, 0-30,000 ohms, 0-3 meg, 0-30 meg. D.C. milliamps: 10, 50, 250 1mA or 50 microamps. A.C. volts: 1,000 ohms per volt. ONLY £12/10/- plus post and pkg. 7/6.

ANOTHER OF OUR AMAZING SCOOPS

A snip for the Constructor



Build this Cossor Pocket 4 Transistor Superhet Receiver.

Circuit description: 4 transistors (OC44, OC45, OC45, OC72), two OA70 diodes, two AGC systems, coverage 190-550 metres. Power output 30 m/w. Ferrite slab aerial, 2½ in. moving coil speaker, printed circuit, attractive tuning control knob, leatherette case 6 x 3½ x 1½ in. All components including theoretical and point-to-point diagram for easy construction.
 ONLY £7/19/6. Post & Pkg. 2/6. All parts available separately.
 9 v. PPA battery 2/- . Maker's original price nearly £20.

BRAND NEW T.V. TUBES, CHEAPER THAN REBUILDS

All brand new in famous maker's cartons. (1) 17in. rectangular aluminized 6.3 HRTS. .3A current; max. anode voltage 16 kV. Usual price £17/5/- . OUR PRICE £7/19/6. Crating and carr. 15/- .
 (2) 14in. rectangular Tube, 6.3 heaters; .3 amp. current; max. anode 14kV; ion trap; external conducting coating; B12A base. £7/19/6. Crating and carriage 12/6.
 (3) Ferranti T12/44 12in. magnetic white fluorescence; 4 v. heater; max. anode 10 kV. As used in many TV receivers. Original price £17/15/- . OUR PRICE £2/19/6. Crating and carr. 12/6.
 (4) Ferranti 9in. Tube, round white fluorescence, 4 v. heater, max. anode voltage 7 kV. OUR PRICE £2/5/- . Crating and carr. 11/6.

LIMITED NUMBER

F.M. Tuner by the Ferguson Company. An attractive and compact unit in gold finish hammered metal case 10in. wide, 7½ in. deep, 2½ in. high. Neat escutcheon and tuning dial. Has own power supply. Uses two EF80, one ECF80, 2 Germanium diodes and metal rectifier. Coverage 87.6 Mc/s (continuously). Will feed into any amplifier or radio.
AT THE AMAZING PRICE OF £13/19/6, 2/6 post and pkg.

BARGAINS IN MICROPHONES

Acos crystal mic. 39/1 complete with cable. Manufacturer's price 84/- . OUR PRICE 39/6, post free.
 Acos crystal mic. 40 on folding stand with cable. OUR PRICE 25/-, post 1/- .

SOMETHING NEW FOR THE CONSTRUCTOR

Etch your own printed circuits; complete kit with instructions comprising 3 laminate sheets, copper faced etching bath, 4 bottles, etchant, resist solvent and cleanser and brush. 19/6 complete. P. & Pkg. 1/6.

PORTABLE BATTERY ELIMINATOR

House in two containers which are to replace AD35 and B126 Batteries. 37/6, Plus 2/- P. & P. Only suitable for use with Dk96 Series valves.

OSCILLOSCOPE No. 11



Made by A. G. Cossor. Incorporates Hard Valve Time Base with speeds of 1.5-40 milliseconds, but simply converted to produce 3 cycles per second to 30 kc/s. Controls include Fine and Coarse Gain, Brightness, Focus, X and Y shifts. Has Power Pack for nominal 115 v. and 230 v. A.C., with adequate fuse protection. Employs 2½in. tube type 6CR10. Grey and black engraved front panel, size 19 x 17in. For standard rack use if required, depth of unit being 12in. In steel transit case as illustrated. Complete with leads and suggested modification data. **BRAND NEW. ONLY £12/10/-** (carriage 15/-).

CRYSTAL CALIBRATOR No. 10



A superb Crystal Controlled Wavemeter just released by the Ministry of Supply. Has directly calibrated dial for nominal coverage of 1.5-10.0 Mc/s. but may actually be used from 500 kc/s. up to 30 Mc/s. Complete with 500 kc/s. Crystal, 2 valves type 1E4, 1 or 1R5 and 1 of CV283 (Neon Stabiliser), and Instruction Book. Size 7in. x 7½in. x 4in., weight 5lb. Used but in first class condition. **ONLY £2/19/6.** Carr. 3/6.

POWER UNITS TYPE 234

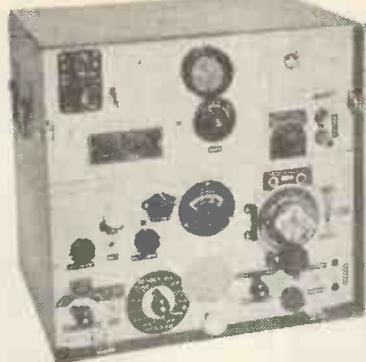


Primary 200/250 v. 50 cycles. Outputs of 250 v. 100 mA., and 6.3 v. 4 amps. Fitted double smoothing. For normal rack mounting (or bench use) having grey front panel size 19in. x 7in. **BRAND NEW. ONLY 59/6.**

ALSO POWER UNIT TYPE 3. Specification as above, but has two meters mounted on front panel to read H.T. Current, and Voltage. **BRAND NEW. ONLY 79/6** (Carriage on either unit 7/6).

12 VOLTS AMERICAN DYNAMOTOR. Delivers 220 volts at 100 milli. Size 5½ x 3½in. diameter. Ideal for running Radio and Electric Shaver, etc., from car battery. **ONLY 32/6.**

MARCONI SIGNAL GENERATOR TF 1446/7. Coverage 85 Kc/s.-2.5 Mc/s. and 8 Mc/s.-70 Mc/s. Complete, and in **AS NEW CONDITION. ONLY 285.**



CANADIAN RECEIVER No. 52

A magnificent 10 valve Receiver covering 1.75-16.0 Mc/s. (19-170 metres) in 8 switched bands. Has built in 3 valve Crystal Calibrator employing dual 100/1,000 Kc/s. Crystal to provide marker check points at 10-100-1,000 Kc/s. Other refinements include Valve-check Voltmeter, Internal 3in. Speaker, R.F. and A.F. Gain Controls, Noise Limiter, B.F.O. Switch, Heterodyne Pitch Control, choice of Wide or Narrow Bandwidth, Speaker or Headphones and Manual or Automatic Volume Control on both C.W. or R.T. There are Fast and Slow Tuning Controls, with additional Oscillator Control for Fine adjustment. In steel carrying case as illustrated, size 15in. x 12in. x 15in. First class condition, thoroughly checked and tested, and in perfect working order before despatch. Circuit supplied. Voltages required 12 volts L.T. and 160 volts H.T. **ONLY £11/19/6** (carriage etc. 15/-).

A suitable Power Pack, for use on 110-250 volts A.C. or 12 volts D.C., can be supplied (less outer case) for 60/- plus 5/- carriage.

DOUBLE BEAM OSCILLOSCOPE TUBES

Type CV 1596 equivalent to Cossor O9D as used in oscilloscopes by Cossor (339 series). Hartley and Erskine (13 series). Listed at **£12/10/-**.

Our price £2/19/6 (carriage 5/6)
Brand New in makers' crates.

R1155 RECEIVERS

The famous Bomber Command Receiver known the world over to be supreme in its class. Covers 5 wave ranges: 18.5-7.5 Mc/s., 7.5-3.0 Mc/s., 1,500-600 kc/s., 600-200 kc/s., 200-75 kc/s., and is easily and simply adapted for normal mains use, full details being supplied. All sets thoroughly tested and in perfect working order before despatch, and on demonstration to callers. Fitted with latest type Super Slow Motion tuning assembly. Have had some use, but are in excellent condition. **ONLY 29/19/6.**

A.C. MAINS POWER PACK OUTPUT STAGE in black metal case to match receiver, enabling it to be operated immediately, by just plugging in, without any modification. Fitted with 8in. P.M. Speaker 66/10/- DEDUCT 10/- IF PURCHASING RECEIVER AND POWER PACK TOGETHER.

Send S.A.E. for illustrated leaflet, or 1/3 for 14-page booklet which gives technical information, circuits, etc. and is supplied free with each receiver. Add carriage 10/6 for Receiver, 5/- for Power Unit.

RCA RECEIVERS AR88D. Thoroughly re-conditioned and in perfect working order. Cover 500 Kc/s-31 Mc/s. **ONLY £60** (carriage etc., 25/-).

RCA 8in. P.M. SPEAKER



In heavy black crackled metal case, designed for use with AR 88 Receiver, or any set with 3 ohm Output. **BRAND NEW IN MAKERS' CARTONS. ONLY 45/-** (Post 3/6).

AMPLIFIER N24



Utilises 4 valves, 1 each 6Z4G, 6V6G, 6J7G, 6J5G and high quality components such as "C" Core Transformers and Block Paper Smoothing Condensers. A.C. Mains Pack for nominal 110/230 volts. Provision for 600 ohm or High Impedance Input. Output to 600 ohm Line. For normal use only requires changing Output Transformer. Output approximately 4 watts. Designed for Standard Rack Mounting, having grey front panel size 19in. x 7in. All connections to rear panel, front having "On/Off" Switch, Gain Control, Indicator Light, Fuses and Valves Inspection Panel. **BRAND NEW IN MAKER'S PACKING. ONLY 24/9/6** (carriage 10/6).

EHT TRANSFORMERS. 5.5 kV (Rect.) with 2 v. 1 a., 79/6. 7 kV (Rect.) with 2 v. 1 a., 89/6. 2.5 kV (Rect.), with 2-0-2 v. 1.1 a., 2-0-2 v. 2 a. (for VCR 97 tube, etc.), 47/6 (postage 2/- per trans.)



SELECTEST TESTMETER DIII

Manufactured by General Electric Co., and has exactly the same ranges as the Avometer D, but with a rather larger mirror scale. Size 9in. x 7in. x 5in., with carrying strap. Thoroughly overhauled, and in perfect order, with batteries and instructions. A real "snip" while they last. **ONLY 27/10/-** (postage, etc., 3/6).

UNIVERSAL AVOMETER 34 RANGE MODEL D

Ex-Air Ministry, but thoroughly reconditioned and checked. Supplied with internal batteries and instructions. Covers ranges as follows:

D.C. VOLTS	A.C. VOLTS	D.C. Current	A.C. Current
150 mV.	7.5 v.	15 mA.	75 mA.
300 mV.	15 v.	30 mA.	150 mA.
1.5 v.	75 v.	150 mA.	750 mA.
3 v.	150 v.	300 mA.	1.5 amp.
15 v.	300 v.	1.5 amp.	7.5 amp.
30 v.	600 v.	3 amp.	15 amp.
150 v.	750 v.	15 amp.	
300 v.	1,500 v.	30 amp.	
750 v.			Resistance
1,500 v.			1,000 Ω
			10,000 Ω

ONLY 28/19/6 (Postage, etc., 3/6).



Cash with order please, and print name and address clearly.
PLEASE ADD POSTAGE OR CARRIAGE COSTS ON ALL ITEMS

HARRIS ELECTRONICS (LONDON) LTD.

Radio Corner, 138 Gray's Inn Road, London, W.C.1. Phone: TERMINUS 7937

Open until 1 p.m., Saturdays.

We are 2 mins. from High Holborn (Chancery Lane Station) and 5 mins. by bus from King's Cross.



MOVING COIL VIBRATOR

TYPE V1000C

This vibrator has been developed to fill in the need for a medium power vibrator with a table surface in place of the usual single point drive spigot. The table is cast from a high duty magnesium and is 6in. (15.2 cms) in diameter and provided with $12 \times \frac{3}{8}$ in. B.S.F. tapped holes for attachment of the test object. The moving coil is attached directly to the table casting. The weight of the moving system is 17.6 lbs. (8 Kgs.), and a bare table acceleration of 31 'G' peak can be obtained for an input current of 10 amps., which is equal to a thrust of 550 lbs. peak for an input power of 1 KW. The vibrator can also be supplied with a blower (V.1000C.B.) and will deliver a thrust of 750 lbs. peak for an input power of 2 KW.

Can be trunnion mounted if required.

W. BRYAN SAVAGE LTD.

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BLOCK PAPER TYPES. 0.002 mfd., 15,000 V.P.K., 100 amps. discharge at 500 times per second, size 10 $\frac{1}{2}$ x 9 x 3 $\frac{1}{2}$ in. ceramic insul., 25/6 each, 3/- post. 0.05 mfd., 16 kv. wkg. at 71 deg. C., ceramic insul., size 14 x 12 $\frac{1}{2}$ x 8in., 30/- each, 5/- post. 10 mfd., 1,500 v. wkg., 15/- each, 3/6 post. 8 mfd., 1,200 v. wkg., 11/6 each. 8 mfd., 500 v. wkg., 5/- each. 6 mfd., 500 v. wkg., 5/6 each. 4 mfd., 500 and 750 v. wkg., 4/6 each. 4 mfd., 1 kv., 5/6 each. 4 mfd., 2 kv. wkg., 6/8 each.

25FT. AERIALS

Super quality very heavily galvanised steel tubes, no guy ropes needed, four 5ft., 2in. dia. steel tubes fit into the ceramic insulated base, these are then pegged to the ground. Aerial mast in four sections steel tubes 2 $\frac{1}{2}$ in. dia., tapering to 1in., at top of mast. Complete aerial with all poles, base and stakes, etc. £12/10/- Weight packed 2 $\frac{1}{2}$ cwt.



POWER UNITS

100-250 volt A.C., input, 24 v. at 3 amps. or 12 v. twice at 3 amps. each winding. Continuous tropical rating, switched and fused, etc., in metal case that fits any 19in. rack, size 19 x 7 x 7in. Brand new £3/15/-, carr. 7/6 (with circuit).



SMOOTHING UNIT

for the above power supply, 2 chokes and 0.1 mA. meter (grade 1) in metal case, same as the p.u., £2, carr. 7/6.



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(part of B20 6 Rec.), 115-600 kc/s, on three bands large dial with a Multhead slow motion drive. Valves EF39, ARTE2, the set can be used with R107, R208, and many other types of receivers. 32/6 each. Carr. 7/6.



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115 volts A.C., 1/6th H.P., variable speed box 0-166. Size of unit 14 $\frac{1}{2}$ x 9 $\frac{1}{2}$ x 8in. £8/10/-, Carr. 10/- Transformers to operate this unit 35/- each.

SILICA GEL in 16 oz. bags, 5 for 5/- Post 2/-.
WIRELESS SET No. 19, Mk. 2. Two trans./Recs. in one case. "A" set 2-6 Mc/s. R/T and CW, "B" set 240 Mc/s. R/T only. 15 valves 500 microamp meter, Variometer, Control box 3B, all leads, key and plug assembly. No. 1 headset Microphone and headphones M/C, and 12-volt rotary power unit. All mounted on the rack, the complete station, £3/10/- Carr. 2/-
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RACKS. 5ft. high, takes 19in. panels at £2, 5/- carr.
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AMERICAN L.T. TRANSFORMERS. Potted type, finished in black crackle and very conservatively rated. (1) 230 v., input 2 x 6.3 volts CT., at 3 amps. and 6.3 volts at 3 amps. output, 18/6 each. (2) 230 volt input, 2 x 6.3 volts at 3 amps., and 6.3 volts CT., at 3 amps. output, 17/6 each. (3) 230 volts input, 25 volts at 2 amps. and 2 volts at 1 amp., 12/6 each. (4) 230 volts input, 3 x 6.3 volts at 3 amps. CT., 1, 6.3 volts 3 amp., 22/6 each. (All these transformers are new and boxed, please include postage 3/6 each.)
MODULATION TRANSFORMERS as used in the BO 640, 40 watts, modulate two 811's, 39/6 each, brand new, boxed, 3/- post.
AMERICAN COMPUTERS AN-170A. Single parallel. Contains 8 relays 10 k., 2 change-over plat. contacts, 8 relays 300 ohms, 2 change-over silver contacts (all relays are small type), 9 x 6V6 small GT., 3 x 6X5 GT., and 2 6SN7. Seven small D.C. motors 27 v. 6 solsyn motors, 10 small micro switches. Plus gears, condensers, ball bearings and pots., etc. This unrepeatable bargain £10 each.
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New additions to GOODMANS speaker range

Latest release of two 10" units

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The well-known 8in. Axiette (£6/12/-) and the 12in. Audiom 60 (£9/12/-) as recommended for two speaker systems, are still available, ex stock.

RECOMMENDED RECORD PLAYER BARGAIN

E.M.I.—4-speed Single Player Unit, fitted with latest stereo and monaural Xtal cartridge and dual sapphire styl. Auto stop and start. A fidelity unit and bargain buy at only £6/19/6 (carr. and insurance 3/6).

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AUTOCHANGERS: BSR (UAB), £6/19/6. BSR UAB fitted with Stereo/Monaural cartridge, £7/19/6; COLLARO Conquest £7/19/6; GARRARD (RC121 4D, Mk. II), plug-in head, stereo adapted, 10 gns. Stereo head £2 extra.

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Contemporary styled, rexine covered cabinet in two-tone fawn and brown, or mottled red with white polka dot. Size 18½ x 13½ x 11in., fitted with all accessories, including buffer board and anodised metal fret. Space available for all modern amplifiers and autochangers, etc. Uncut record player mounting board 14 x 13in. supplied.

Cabinet Price £3/3/-, Carr. and Ins. 3/6.

2-VALVE 2-WATT AMPLIFIER

Twin stage ECL82 with vol. and neg. feedback. Tone controls AC 200/250 v. with double-wound mains trans. Complete with knobs, etc., ready wired to fit above cabinet.

£2/17/6 P. & P. 1/-.

6in. Speaker and matching trans., 22/-, P. & P. 1/6.

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- OA70 3/- All branded
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NOW! The TOURIST Portable

4 valve. Med. & L.W., L'tweight battery Radio. Size only 8in. x 5½in. x 4in. Weight 3½lb. with battery— P. & P.

Complete receiver component kit 57/8 1/8 Set 4 miniature valves (9 series) 35/- 9d. 6in. Speaker & O/put Trans. 21/- 1/6 Cabinet, Dial and Knobs, etc. 22/6 2/- Latest superhet circuitry delayed AVC and A.F. Neg. feedback.

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12 v. operation Med. & Long Waves

Modern development of the famous Brimar Hybrid vibratorless car radio circuit. Five latest type Brimar low voltage valves and power transistor. R.F. stage and permeability pre-aligned Cyclon Tuner Unit provide extremely good sensitivity and signal noise ratio. Printed circuit for easy construction and 7 x 4in. elliptical speaker for fidelity output. Self-contained in neat metal cabinet 8 x 7 x 2½in., with attractive calibrated dial. Speaker and power transistor stage mounted separately approx. 8 x 5 x 3in.

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£12.19.6

P. & P. 3/6.

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Send for list of more valve bargains.

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1R5, 1T4, 1R5, or 3V4, 27/6
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COAX 80 OHM CABLE.

Stand ½in. diam. Low Loss Semi-Air Spaced Aerial. Top grade cable—not to be confused with inferior types.

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Designer-approved kits of parts for these quality and highly popular tuners available as follows.

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MULLARD "3-3" AMPLIFIER

Quality built to Mullard's specification, with special sectionalised O/P Trans. Complete kit with front panel only £6/19/6. P. & P. 3/6.

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New improved types—mains prim. 200/250 v. tapped

All Isolation Transformers now supplied with alternative no boost, plus 25% and plus 50% boost taps at no extra charge.

- 2V. 2A type.... 12/6 (P. & P. 1/6)
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Small size and lag terminated for easy fitting. Other voltages available.

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All tubes rebuilt with new heater, cathode and gun assembly—reconditioned virtually as new.

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CONDENSERS—Silver Mica. All pref. values, 2 pf. to 1,000 pf., 6d. each. Df10 ceramics 9d. each. Tubulars 450 v. T.C.O. etc., .001 mid-.01 and 1/350 v., 9d. each. .02-1/500 v., 1/- each. .25 Hunts 1/6. 5 T.C.O. 1/9. .001 8 kv. 5/6. .001 20 kv. 9/6.

RESISTORS—FULL RANGE 10 ohms—10 megohms 20%, ½ w. and ¼ w. 3d., ¼ w. 5d. (Midget type modern rating), 1 w. 6d., 2 w. 9d., 10% Hi-Stab. ½ w., 5d., ¼ w., 7d., 5% ½ w., 9d., 1% Hi-STAB, ¼ w., 1/6 (10-100 ohms 2/-).

PRE-SET W/W POTS. T/V Type, 25 ohms—50 K ohms 3/-. 50K—2 Meg. (Carbon 3/-).

SPEAKER FRET—Expanded Bronze anodised metal 8 x 8in. 2/3; 12 x 8in. 3/6; 12 x 12in. 4/6; 12 x 16in. 6/-; 24 x 12in. 9/-; 36 x 12in. 13/6, etc., etc.

TYGON FRET (Contemporary pat.), 19 x 12in. 2/-; 12 x 18in. 3/-; 12 x 24in. 4/-, etc.

Loudspeakers—P.M. 3 ohms, 2½in. Elac, 17/8. 3½in. Goodmans 18/6; 5in. Rola, 17/6. 6in. Elac, 18/6; 7 x 4in. Goodmans Elliptical, 18/6; 8in. Rola, 20/-; 10in. R. and A., 25/-; 10in. W.B. HF1012, 99/9. 12in. Plessey 15 ohms with 6/4in. Tweeter and Cross Over Filter, 97/6.

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25/25 v. 50/12 v. 1/9	8+8/450 v. 4/6
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18+18/450 v. 5/6	60+250/275 v. 12/6
32+32/450 v. 6/6	100+200/275 v. 12/6

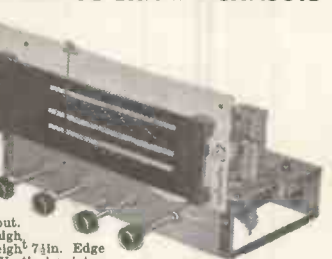
Comprehensive range in stock.

VOLUME CONTROLS—10K—2 Megohms. ALL LONG SPINDLES, MOCCANTITE MIDGET TYPE, 1½in. diam. Guar. 1 yr. LOG or LIN Ratios less Sw., 3/-. D.P. Sw., 4/6. Twin gang controls ½ Meg., ¼ Meg., 1 Meg. less Sw., each, 8/9.

7 VALVE AM/FM RADIOGRAM CHASSIS

Valve Line-up: ECC85, ECH81, EF89, EABC80, EL84, EM81, EX80.

Three Waveband and Switched Gram positions. Med. 200-500 m., Long 1,000-2,000 m., VHF/FM 88-95 Mc/s. Philip's Continental Tuning Insert with permeability tuning on FM and combined AM/FM IF transformers, 460 Kc/s and 10.7 Mc/s. Dust core tuning all coils. Latest circuitry including AVC and Neg. Feedback. Three watt output. Sensitivity and reproduction of a very high standard. Chassis size 13½ x 6½in. Height 7½in. Edge illuminated glass dial 1½ x 3½in. Vertical pointer. Horizontal station names. Gold on black background. A.C. 200/250 v. operation. Aligned and tested ready for use. £13.10.0 Carr. & Ins. 5/-



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- 8in. Goodmans special cone 21/6
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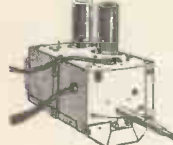
0A2 .. 17/6	6AV6 12/7	6S17GT 8/8	12K5 17/11	83... 15/-	DL96 9/-	ECL82 10/6	EZ81 7/-	FCP89 11/6	U22 .. 8/-	UL46 14/6	CG12E 7/8
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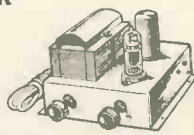


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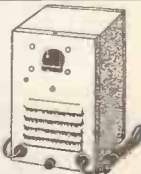
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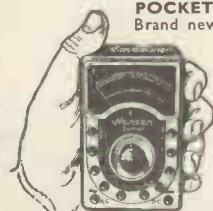


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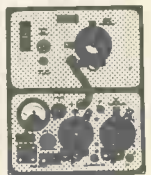
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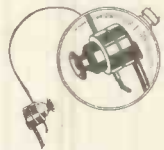


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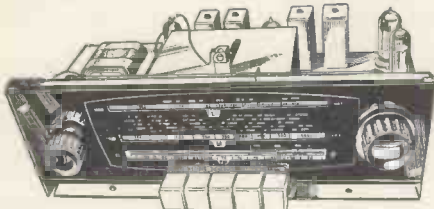


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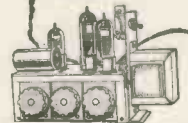
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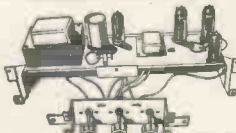
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(2) Ferranti T12/44 and T12/54G 12 in. magnetic white fluorescence; 4 v. heater; max. anode 10 kV. As used in many TV receivers. Original price £175/-. **Our price £4/19/6.** Crating and carr. 12/6.
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JONES PLUGS AND SOCKETS. 4 pin 2/6 pair; 6 pin 3/6 pair; 8 pin 4/6 per pair; 12 pin 6/6 per pair. If cover required send 1/6 extra per cover.

WANDER PLUGS. Red and black doz. 2/-
PHILIPS TRIMMER TOOLS 1/- each doz. 10/6
4-WAY PUSH-BUTTON UNITS 2/6 each. Knobs for same, 3d. each.
POINTER KNOBS. Small black with white line, 7/6 per doz. Small white with black line 8/- per doz. Both types 1/2 in. spindle. Large price reductions for 1,000 lots and over.

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We invite your enquiries for items not listed.

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Also 9 to 1 Saturday. Callers welcomed.
Large stocks of all types of resistors, condensers, valveholders always available ex stock. Manufacturers' enquiries welcome.

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A.C. MAINS 200-250 VOLTS

SIMPLIFIED SERVICING
PROBLEMS WHEN USING
THE
'TESTGEAR' SCOPE

3in. D.C. OSCILLOSCOPE



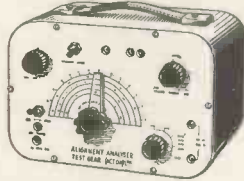
Engineered to precision standards, this high-grade instrument is made available at the lowest possible price, incorporating the essential features usually associated with luxury instruments. This "SCOPE" will appeal particularly to Service Engineers and Amateurs. A high gain, extremely stable differential Y-Amplifier (30 mV/C.M.). Provides ample sensitivity with A.C. or D.C.

inputs. Especially suitable for measurement of transistor operating conditions where maintenance of D.C. levels is of paramount importance. Push-pull X amplifier. Flyback suppression; Internal Time-base Scan Waveform available for external use; pulse/output available for checking T.V. Line O/P Transformers, etc.; Provision for external X 1/P and CRT. Brightness Modulation. Size 10in. high, 6 1/2in. wide, 9in. deep. Wgt. 11lb. £15/15/- plus P. & P. 7/6, or 30/- deposit, plus P. & P. 7/6 and 12 monthly payments of 2/6.

FULL 12 MONTHS' GUARANTEE INCLUDING VALVES AND TUBE

ALIGNMENT ANALYSER TYPE MC12

A.C. MAINS, 200/250 volts. Provides—"WOBBULATOR" (SWEEP FREQUENCY) OPERATION, for FM/TV alignment linear frequency sweep up to 12 Mc/s. From 400 Kc/s.—80 Mc/s. CAPACITANCE MEASUREMENT. Two ranges provided 0—40 pF. and 0—120 pF. SPECIAL FACILITY enables true resonant frequency of any tuned circuit I.F. transformer, etc., to be rapidly determined. Cash price £6/19/6 and 5/- P. & P. H.P. terms 25/- deposit and 5/- P. & P. and 6 monthly payments of 2/1/6.



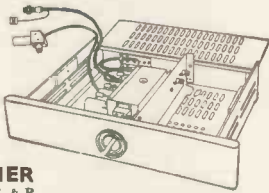
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Will tune to all Band I and Band III stations. BRAND NEW by famous manufacturer. Complete with P.C.C. 84 and P.C.F. 80 valves (in series). I.F. 16-19 or 33-38. Also can be modified as an aerial converter (instructions supplied.) Complete with knobs.

22/6 Plus 3/6 P. & P.

HEATER TRANSFORMER

To suit the above, 200-250 v., 6/- Plus 1/6 P. & P.



B.S.R. MONARCH UA8 with FUL-FI HEAD



4-speed plays 10 records 12in., 10in., or 7in. at 16, 33, 45 or 78 r.p.m. Intermixes 7in., 10in. and 12in. records of the same speed. Has manual play position; colour brown. Dimensions: 12 1/2in. x 10 1/2in. Space required above baseboard 4 1/2in., below baseboard 2 1/2in. Fitted with Ful-Fi turnover crystal head. £6/19/6, Plus 5/- P. & P.

STEREO HEAD £7/19/6 Plus 5/- P. & P.

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With built-in line and width control. 14 KV. Scan coll. 90° deflection, on ferrite yokes. Frame O.P. transformer 500 pF. 18 KV. smoothing condenser. Can be used for 14in., 17in. or 21in. tubes. Complete with circuit diagram.

29/6 Plus 4/- P. & P.

FOCUS MAGNET suitable for the above (state tube), 10/- 2/6 P. & P.

MAINS TRANSFORMERS

All with tapped primaries 200-250 volts.

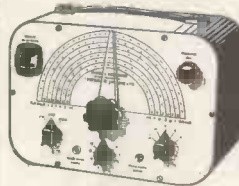
0-160, 180, 200 v., 60 ma., 6.3 v., 2 amps., 10/6 200-0-200 v., 75 ma., 6.3 v., 2.5 amp., 5 v., 2 amp., 10/6 280-0-280, 80 ma., 6.3 v., 2 amp., 6.3 v., 1 amp., 10/6 350-0-350, 70 ma., 6.3 v., 1 amp., 6.3 v., 2 amp., 10/6 250-0-250, 70 ma., 6.3 v., 2 amp., 10/6. Postage and packing on the above 3/-.

WOLSEY 3-ELEMENT FOLDED DIPOLE

I.T.V. Aerial less mounting bracket for external use, complete with 12 yds. of coaxial cable, 15/-; 4 element, 17/6; 5 element, 25/- P. & P. on above, 3/6.

INTERCOM or BABY ALARM in Wooden Cabinet with 8in. speaker and 3 valves. Transistorised input. Provision for talk-back, 49/6. Plus 5/- P. & P.

SIGNAL GENERATOR



£6/19/6

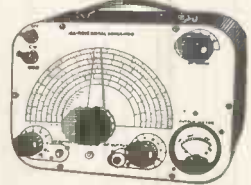
Covering 100 Kc/s.-100 Mc/s. on fundamentals and 100 Mc/s. to 200 Mc/s. on harmonics. Metal case 10in. x 6 1/2in. x 5 1/2in., grey hammer finish. Incorporating three miniature valves and Metal Rectifier. A.C. Mains 200/250 v. Internal Modulation of 400 c.p.s. to a depth of 30%. Modulated or unmodulated R.F. output continuously variable 100 millivolts C.W. and mod. switch, variable A.F. output. Incorporating magic-eye as output indicator. Accuracy plus or minus 2%.

Or 25/- deposit and 6 monthly payments of 21/6. Post & Packing 5/- extra.

SIGNAL GENERATOR

Coverage 120 Kc/s.—230 Kc/s., 300 Kc/s.—900 Kc/s., 900 Kc/s.—2.75 Mc/s., 2.75 Mc/s.—8.5 Mc/s., 8 Mc/s.—28 Mc/s., 16 Mc/s.—56 Mc/s., 24 Mc/s., 84 Mc/s. Metal case 10in. x 6 1/2in. x 4 1/2in. Size of scale 6 1/2in. x 3 1/2in. 2 valves and rectifier A.C. mains 230-250 v. Internal modulation of 400 c.p.s. to a depth of 30 per cent., modulated or unmodulated R.F. Output continuously variable, 100 millivolts C.W. and mod. switch variable A.F. output and moving coil output meter. Grey hammer finish case and white panel. Accuracy plus or minus 2%.

£4/19/6



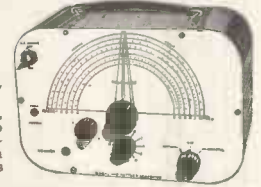
Or 25/- deposit and 4 monthly payments 21/6. P. & P. 5/- extra.

SIGNAL & PATTERN GENERATOR

£6/19/6

P. & P. 5/-

Or 25/- deposit. P. & P. 5/- and 6 monthly payments of 21/6. Coverage 7.6 Mc/s.-210 Mc/s. in five bands, all on fundamentals, slow motion tuning audio output. 8 vertical and horizontal bars, logging scale. In grey hammer finished case with carrying handle. Accuracy ±1% A.C. mains 200-250 v.



F.M. TUNER UNIT

By famous German manufacturer. Coverage 88—100 Mc/s. Complete with ECC85. Size 4in. x 2in. x 2in.

25/- Plus P. & P. 1/6.

Circuit diagram free with unit. 1/-

10.7 Mc/s. I.F. and Discriminator Coil 4/- pair

3-TRANSISTOR POCKET RADIO Plus GERMANIUM DIODE ON PRINTED CIRCUIT

Size 3 1/4" x 4" x 7/8"

Incorporating Ferrite Rod Aerial. Tuneable over medium and long waves.

Kit of parts. 39/6 Plus 1/6 P. & P.

Circuit diagram 1/6 free with kit.

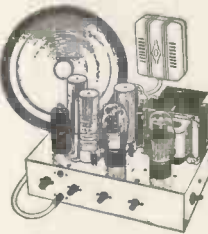
8 WATT PUSH-PULL AMPLIFIER

COMPLETE WITH CRYSTAL MIKE AND 8in. LOUDSPEAKER

A.C. mains 200/250 v. Size 10 1/2in. x 6 1/2in. x 2 1/2in. Incorporating 6 valves, H.F. pent., 2 triodes, 2 output pens., and rectifier. For use with all makes and types of pick-up and mike. Negative feed-back. Two inputs, mike and gram., and controls for same. Separate controls for Bass and Treble Hft. Response flat from 40 cycles to 15 Kc/s. ±2 db; 4 db down to 20 Kc/s. Output 8 watts at 5%, total distortion. Noise level 40 db down, all hum. Output transformer tapped for 3 and 15 ohm speech coils. For use with Std. or L.P. records, musical instruments such as Guitars, etc.

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PORTABLE AMPLIFIER on printed circuit for A.C. Mains 200/250 v. Size 4in. x 3in., with tone and volume control. Valves: ECL82 and EZ80. 39/6. P. & P. 2/6.

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1. C/O ...	1/3	4/-
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10,000	6/-	8/6
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40,000	8/-	—
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*Slugged coils extra.

SIEMENS HIGH SPEED C/O RELAYS

250+250 ohm Twin Coils	6/6	1,000+1,000ohmsTwinCoils	10/6
850+850	8/6	1,700+1,700	17/6

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Z530001	40	4 C/O	6 v.	17 6
Z530005	2	2 C/O	1.3 v.	12 6
Z530006	40	2 C/O	6 v.	15 0
Z530008	670	2 C/O	24 v.	19 6
Z530010	40	2 C/O 2K	7 v.	17 6
Z530014	2	1 C/O	1.3 v.	10 6
Z530015	40	1 C/O	6 v.	12 6
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Z530020	2	4 C/O	1.3 v.	16 6
Z530021	2	2M	1.3 v.	10 6
Z530022	2	1M 1B	1.3 v.	12 6
Z530023	2	2B 2M	1.3 v.	12 6
Z530024	40	2M	6 v.	12 6
Z530025	40	1M 1B	6 v.	12 6
Z530026	40	2B 2M	6 v.	15 0
Z530027	180	2M	12 v.	17 6
Z530028	180	1M 1B	12 v.	17 6
Z530030	670	2M	24 v.	17 6
Z530031	670	1M 1B	24 v.	17 6
Z530034	2,500	1M 1B	48 v.	£1 2 6
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4184GD	700	2C	24	19 6
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1/6 Post & Packing on all relays.



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Delivery ex stock. Quotations on application.

H.T. 31
Input 11.5 v.
Output 250 v. at 120 mA.

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Both types dual output. Made in U.S.A.



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114	3/8	6L6	9/8	25A6G	8/8	E8C41	3/8	EZ40	7/3	U34	7/6
1N5GT	9/8	6L9	7/8	25L6G	6/8	E8C81	7/8	EZ41	7/6	U55	6/6
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3A4	8/8	6P28	6/	30F4	12/8	E8C81	9/8	HLA30	9/8	U56	6/6
3Q4	7/3	6Q7G	6/8	31P12	8/	E8C32	14/-	HL14DD9	6/	U52	5/6
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6AG7	8/6	6V6GT	6/6	955	3/8	E8C81	8/3	N7	11/-	UBC41	8/3
6AK5	6/8	6X4	6/	956	2/8	E8C30	8/3	N83	15/-	UBC81	10/-
6AL5	3/8	6X6	5/6	2050	3/8	E8C82	10/8	P41	4/8	UBF80	8/8
6AM6	3/8	6X6GT	6/6	9001	4/8	E8C83	14/6	PL22	7/6	UBF89	9/6
6AQ3	7/	7B6	9/6	9003	4/	E8P22	12/-	PAC8011	1/	UB121	14/6
6AT6	7/-	7B7	7/3	ATP4	2/8	E8P36	3/3	PCC84	7/9	UCH21	14/6
6AU6	8/6	7C5	7/6	AZ31	9/	E8P39	4/8	PCC85	9/3	UCB42	8/6
6BBG	3/8	7C8	7/3	B36	8/8	E8P40	12/8	PCC89	13/8	UCH91	8/6
6BAL	6/-	7H7	7/8	B65	5/8	E8P41	8/8	PCP80	7/6	UCL82	11/3
6BE6	6/8	7H7	9/8	CB131	23/3	E8P42	7/6	PCP82	9/	UCL83	13/8
6BG6G	12/6	7Y4	7/6	CY31	9/	E8P50-BR2	6/	PCL82	9/3	UF41	8/6
6BW6	8/8	10C1	11/-	D63	1/8	E8P50-AM2/6	6/	PCL83	11/6	UF42	7/8
6BW7	7/-	10C2	13/6	DA30	2/6	E8F54	3/8	PCL84	9/8	UF80	9/-
6C4	3/8	10F1	6/8	DA32	8/8	E8P80	5/8	PEN25	4/8	UF85	9/-
6C9	4/3	10F9	10/8	E8P91	8/	E8P83	7/6	PE45	7/8	UM92	9/6
6C9	9/8	10F13	9/6	DF46	9/3	E8P86	11/-	PE48	5/3	UF89	7/3
6CD6G	18/8	10P14	9/6	DF33	8/8	E8P89	8/	PL33	9/	UL41	7/6
6CH6	9/3	12A8H	9/8	DF91	5/-	E8F91	3/8	PL36	12/-	UL44	12/6
6D6	4/8	12A7H	7/8	DF96	8/3	E8F92	4/8	PL38	14/8	UL46	9/8
6F1	6/8	12A7	7/8	DE77	7/-	E8L32	4/8	PL81	10/8	UL54	8/6
6F6G	6/8	12A7	6/8	DK32	12/6	E8L33	7/6	PL82	9/	UM90	9/6
6F13	6/8	12A7	7/8	DK91	8/8	E8L35	11/6	PL83	8/	UU6	12/6
6F14	9/8	12J5GT	3/6	DK92	8/8	E8L37	11/6	PL84	11/-	UU7	9/6
6F15	9/8	12K7GT	6/8	DK96	9/3	E8L38	12/6	PY31	8/3	UY1N	11/-
6E6	2/-	12K8GT12	8/	DL33	8/8	E8L41	9/	PY32	11/-	UY41	6/6
8J5G	2/8	12Q7GT	8/-	DL35	11/6	E8L42	9/8	PY80	7/8	UY85	7/-
8J5GT	3/8	12SK7	6/8	DL81	8/8	E8L34	8/	PY81	7/8	VB150/306H	8/6
8L6	4/-	12SN7GT	8/6	DL82	8/8	E8L91	4/8	PY82	7/8	X65	11/-
6J7G	5/3	1487	14/8	DL94	7/8	EM34	8/6	PY83	8/8	X66	11/-
6J7GT	7/8	19B6G015	8/	DL96	8/3	EM80	9/3	PZ30	12/-	X78	14/8
4K6GT	6/8	20D1	9/6	E8A50	9d.	EM81	9/3	R19	12/8	X79	16/8
6K7G	2/3	20P2	8/6	E8A80	7/6	EM84	9/8	SP41	2/8	Y63	6/3
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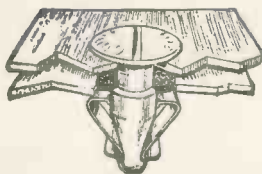
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- (2) Test specification engineers
- (3) Technical editors

Category (1) requires engineers who possess academic qualifications to O.N.C. standard or above and who have gained experience in design and/or maintenance of electronic equipment. Category (2) requires engineers with similar technical training to the above, but who have gained experience in test rooms or inspection departments associated with the manufacture of electronic equipment.

Experience in the writing of technical documents is not essential but senior posts in the above categories are available to applicants with previous experience in this profession.

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
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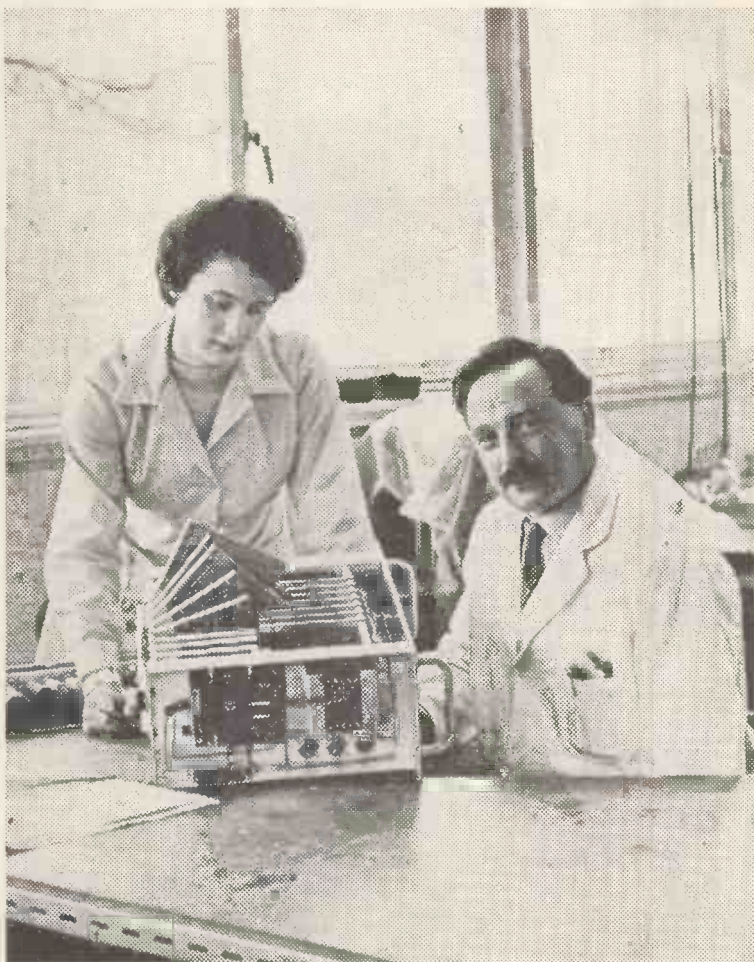
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The designer would be required to work in close liaison with Production sections with emphasis on fully practical and economic designs.

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to travel anywhere in this country in order to assist in the installation and maintenance of electronic equipment. This post will be located at the Harrow factory but will transfer to the Stevenage factory approximately October 1960. Sound knowledge of electro mechanical devices and electronic theory equivalent to at least Inter City and Guilds standard is essential. Excellent salary. The Company operates non-contributory sickness and pension plans and a part contributory life insurance scheme.

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Candidates must have had recent experience of this type of work on Civil or Military equipment. Write stating age, experience and present salary to the Personnel Manager.

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Applications should be addressed to the Professor of Astronomy, The University of Manchester, Oxford Road, Manchester 13.

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The selected applicant will be expected to handle the design or supply of test equipment over the range D.C. to 400 Mc/s. on commercial radio and TV, private venture and Ministry projects.

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- (c) Mechanical aspects of instrument design.

2. JUNIOR ENGINEERS

to assist in the above projects.

3. TECHNICIANS

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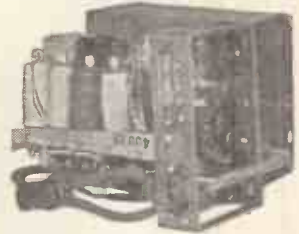
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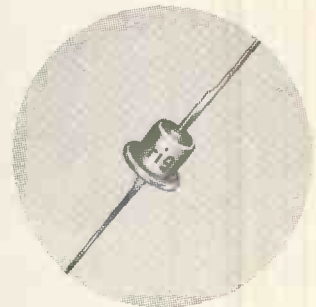
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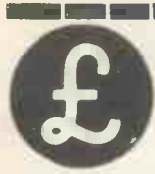
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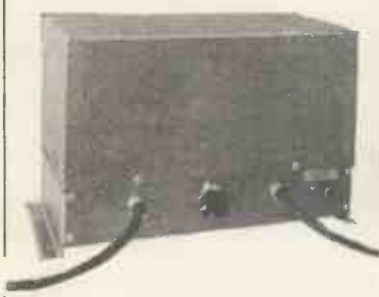
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URGENTLY wanted, manuals or instruction books, data, etc., on American or British Army, Navy or Air Force radio and electrical equipment.—Harris, 95, Wardour St., W.1. Gerrard 2504. [8880]

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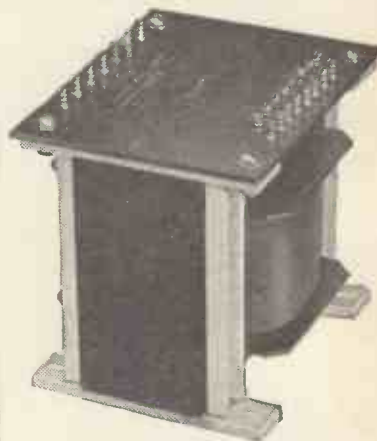
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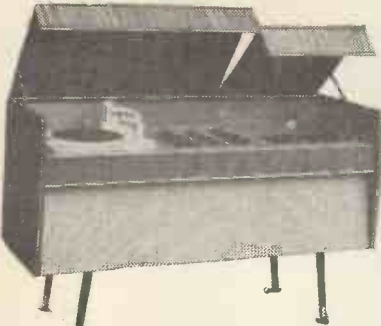


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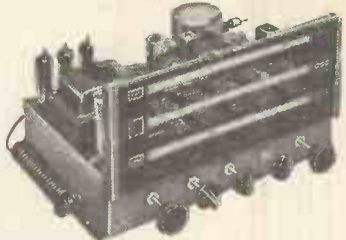
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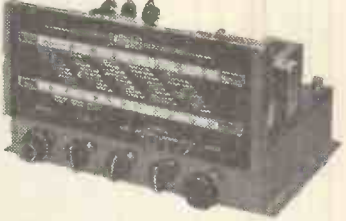


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TECHNICAL author, electronics; exceptional opportunity for fully experienced man with proved technical and writing background; minimum salary £1,250 per annum.—Applications in confidence to The Drawing Office (Baldock), Ltd., 23a, High St., Baldock, Herts. [9073]

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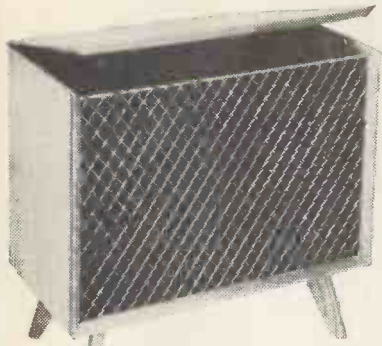
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TECHNICAL authors required for the preparation of handbooks giving full technical descriptions, setting-up procedures and servicing instructions for a wide range of equipment in the fields of radar, aids to navigation, air traffic control and industrial electronics. Applicants should have a good command of English and familiarity with the requirements of the Services ATP and with specification ATA 100 would be an advantage; pension scheme, housing assistance available in approved cases.—Write giving full details and salary required to: Personnel Officer, Cossor Radar & Electronics, Limited, The Pinnacles, Elizabeth Way, Harlow, Essex. [9071]



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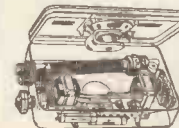
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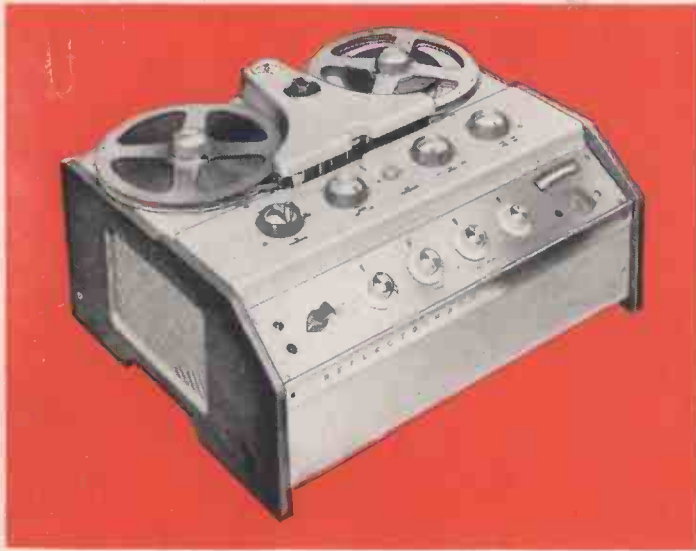
The principle employed results in an exceptionally high degree of frequency stability. Throughout the tuning range of the receiver, which is from 500 kc/s to 30.5 Mc/s, the long term drift does not exceed 50 cycles. Particular care has been taken to reduce spurious responses to an absolute minimum and the figures for such characteristics as cross-modulation, blocking, inter-modulation and image ratio are extremely good. The electrical performance is well maintained in every way and conforms to accepted professional standards.

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REFLECTOGRAPH MODEL B



New QUARTER TRACK TAPE RECORDER

This is probably the first tape recorder with a professional specification which enables you to record on 4 tracks and compare instantly the input signal with the signal recorded on the tape.

A total recording time at $7\frac{1}{2}$ i.p.s. on 3,600 feet of tape is 6 hours 24 minutes and this time is doubled for recordings made at $3\frac{3}{4}$ i.p.s.

At the slower speed an exceptionally good frequency response has been achieved and a special compensation network operates at this speed.

The quarter-track facilities provided make it possible, when connected to a suitable external amplifier, to reproduce pre-recorded $\frac{1}{4}$ track or $\frac{1}{2}$ track stereo tapes.

A PROFESSIONAL SPECIFICATION IS COMMON TO ALL REFLECTOGRAPH MODELS

DIMENSIONS: 20" long x 16" deep x 10" overall.
WEIGHT: Approx. 50 lb.
TAPE DECK: *Motors:* Direct drive synchronous capstan motor. Two Garrard side motors.
Tape-Speed: $7\frac{1}{2}$ and $3\frac{3}{4}$ i.p.s.
Tape Speed Control: Switched two speed capstan motor.
Long Term Speed Stability: Better than 0.2% for 1200 feet.
Spool Size: Up to $8\frac{1}{4}$ ".
Wow and Flutter: At $7\frac{1}{2}$ i.p.s. better than 0.2% R.M.S.
Starting & Stopping time: Less than 1 sec.
Tape Loading: Visible placing across heads.
Magnetic Heads: Reflectograph Types E.4. Erase, R.4. Record, P.4. Playback.
Tape Wind: Controlled by single knob electrical wind with mechanical 'PARK' position. Less than 45 secs. for 1200 ft. tape.
Position Indicator: Clock type.
Controls: 3 position function lever; mains OFF/ON knob; push button OFF; motors $7\frac{1}{2}$ / $3\frac{3}{4}$ /OFF knob; wind on/wind back knob.
Splicer: Provision for mounting Bib Tape Splicer.

AMPLIFIERS: Separate record and playback amplifiers providing continuous monitoring from the tape with provision for instant comparison between input signal and recorded signal.

Controls: Record/Playback, with safety button on record. Red and green warning lamps automatically illuminated.

AMPLIFIERS (cont.) Bass Cut/Boost with calibrated skirt marked for C.C.I.R. response. Treble Cut/Boost with calibrated skirt marked for C.C.I.R. response. Playback Volume with calibrated skirt. Record Volume with calibrated skirt. Tape/Input switch.

FREQUENCY RESPONSE: At $7\frac{1}{2}$ i.p.s. to C.C.I.R. specification (or to N.A.R.T.B. to special order). ± 2 dB 50 c/s-10,000 c/s (± 3 dB 30-50 c/s and 10,000-15,000 c/s). At $3\frac{3}{4}$ i.p.s. ± 2 dB 40-7,500 c/s.

SIGNAL/NOISE RATIO: Better than -43dB (unweighted including hum).

INPUT SENSITIVITIES: High Gain: not more than 6 mV for peak record level. Low Gain: not more than 0.25 V for peak record level.

OUTPUT VOLTAGES: From pre-amplifier 150 mV. R.M.S. medium impedance. From amplifier 3 watts across 15 ohms.

ERASE AND BIAS FREQUENCY: 63 Kcs.

TAPE SPEED EQUALIZING: Automatic for $7\frac{1}{2}$ and $3\frac{3}{4}$ i.p.s.

RECORD LEVEL: Meter indicator, edgewise reading with coloured and calibrated scale.

INPUT SOCKETS: High Gain and Low Gain.

OUTPUT SOCKETS: Head pre-amplifier. External speaker (15 ohms).

AMPLIFIER CONSTRUCTION: Separate record and playback amplifiers across front of instrument.

Access to valves by removing 5 screws from front panel.

VALVES: 1/EF86, 1/6BR8, 1/ECC82, 2/ECC83, 1/EL84, 1/EF91, 1/EZ80.

MONITOR LOUDSPEAKER: Special Goodmans $10" \times 7"$ high quality elliptical high flux, low field.

Reflectograph instruments are covered by Patent Application 1109/60. Registered Design 895860. World Patents pending.

The Model B will not make stereo recordings but in due course facilities will be available for conversion of a Model B for stereo recording if required.

PRICE
105 GNS.

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