GIB LENKURT DEMODULATOR MARCH/APRIL 1979

Path Profiling with a Programmable Calculator



The time consuming effort of hand calculations and the inherent inaccuracies involved in using slide rules have been virtually eliminated by electronic calculators. The inclusion of a programmable memory increases the usefulness of a calculator for engineering applications. This issue of the Demodulator describes one of these applications.

The terrain and physical objects separating two antennas affects the transmission of microwave energy between them. When a microwave path is to be established between two points, maps are used to make a preliminary selection of a suitable path. Then, a profile of this path is plotted to determine what antenna heights are required to overcome the effects of terrain and physical objects. If the area is particularly rugged, partial profiling as well as map inspection may be needed for preliminary path selection.

A programmable calculator is a useful tool for reducing the time and effort required to prepare a path profile. Two programs for path profiling are presented at the end of this article. The programs are for the Hewlett Packard type 97 calculator but they can be easily adapted to other types of programmable calculators.

Microwave Transmission Characteristics

The curvature of the earth and the slight bending of the microwave beam as it is refracted downward by the earth's atmosphere are two factors that must be considered when constructing microwave path profiles. The earth's curvature and microwave beam refraction are commonly combined to form an equivalent earth radius factor, "K". This factor "K", multiplied by the true earth radius, is the radius of a fictitions earth curve for a microwave beam traveling in a straight line. As different atmospheric conditions change the amount of beam refraction, the value for "K" also changes.

Values for "K" during standard atmospheric conditions range from 1.2 in dry elevated areas to 2 or 3 in humid coastal areas, with 4/3 being typical of inland areas. Unusual propagation conditions, encountered a small percentage of time, can produce values of "K" ranging from 1/2 during substandard propagation to negative values during superstandard propagation. Figure 1 shows graphically how the refraction and earth's radius can be shown for a profile over flat terrain. It is convenient to plot the profile on rectangular graph paper to show both the refraction of the microwave beam and the earth curvature as a bending of

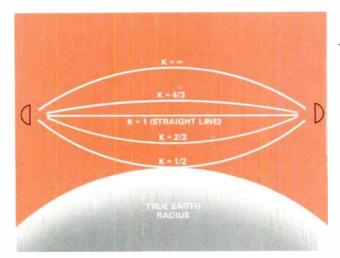


Figure 1. Beam refraction for true earth radius.

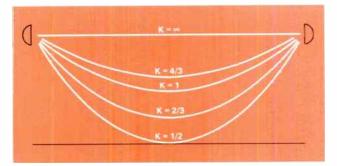


Figure 2. Relative beam curvatures for a flat earth.

the microwave beam, as depicted in Figure 2.

Another factor that must be considered in the construction of microwave path profiles is the influence of terrain and physical objects on the microwave beam. As a microwave beam passes close to an object some energy is redirected by the object, causing a variation in the receive signal level on the microwave path, as shown in Figure 3. The microwave frequency, the distance from the center of the microwave beam and the distance to the ends of the path determine where nulls and peaks in the signal will occur. The type of object and its physical shape determine the magnitude of the variations.

The distance from the microwave beam's center is commonly measured in units of Fresnel zones, to take into account both frequency and distance. The first Fresnel zone $(1.0 F_1)$ is the surface of points along which the total distance to the ends of the path is exactly one-half a wavelength longer than the direct end-to-end microwave path.

Any object within the first Fresnel zone will diffract the microwave beam. In this diffraction zone, distances from the center of the microwave beam are measured in fractions of the first Fresnel zone.

It is important to note that a clearance of at least six tenths (0.6) of the first Fresnel zone is required to

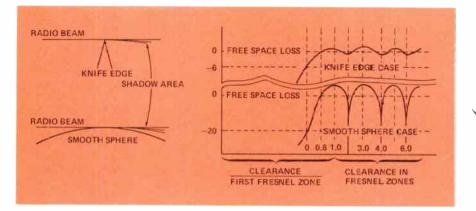


Figure 3. Diffractions caused by objects of different shapes.

maintain free space loss from end-toend on a microwave path. When less than six tenths clearance is present, the microwave beam is considered to be obstructed.

If an object is at or outside the first Fresnel zone, the distance from the object to the center of the microwave beam is measured in actual Fresnel zones. Figure 4 presents the formulas used to calculate various Fresnel zones.

Reflections

For very shallow angles of reflections, a 180° ($\lambda/2$) phase delay occurs at the reflection. The phase delay of the reflected signal, plus the $\lambda/2$ difference in the path length of the first Fresnel zone, will produce an in-phase addition of the direct and reflected beams at the receive antennas. This addition can give up to 6 dB increase in received signal level, depending on how well the signal is reflected. If the reflection point falls on an even Fresnel zone, a null in the receive signal can occur due to an out of phase addition of the direct and reflected signals.

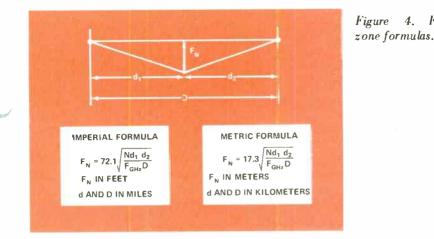
Microwave paths with strong reflections are usually designed to take advantage of odd Fresnel zone reflections. When even order reflections cannot be avoided, space diversity systems are normally used. These systems are designed so that only one of the space diversity antennas encounters an even Fresnel zone reflection at any single value of K.

Path Clearance Criteria

Earth curvature, microwave beam refraction and Fresnel zone clearance are combined into clearance criteria for a microwave path. Two basic sets of criteria, heavy route and light route, are in common use for microwave communication systems. Each set of criteria should be maintained along the entire microwave path. Earth bulge and Fresnel zone radii vary in a different way along the path and often one criterion is controlling near the center of the path and the other is controlling near the path ends.

• Heavy Route Clearance:

At least $0.3F_1$ at K=2/3 and $1.0F_1$ at K=4/3, whichever is greater. In cases of very difficult propagation, grazing at K=1/2 may be added to this criteria to assure adequate



clearance. (For 2 GHz paths longer than 36 miles substitute 0.6F at K=1.0).

• Light Route:

At least $0.6F_1$ at K=1.0 plus 10 feet.

At points quite near the ends of the paths, the Fresnel zones and earth bulge become vanishingly small. However, it is still necessary to maintain a minimum of 15 to 20 feet clearance from all obstacles.

Sources of Terrain Information

Maps that accurately show physical objects and terrain contours are required for the path profile. In the United States 7-1/2 or 15 minute maps are used for the detailed information required in path profiling. Indexes and maps are available from the United States Geological Survey, Branch of Distribution. For areas east of the Mississippi River, the address is 1200 South Ends Street, Arlington, Virginia 22202. For areas west of the Mississippi River including Louisiana, the address is Box 25286 Federal Center, Denver, Colorado 80225. The indexes list state, government and private locations where maps are for sale. After maps are obtained, preliminary path selection can be started.

4. Fresnel

Preliminary Path Selection

It is sometimes difficult to determine a useful microwave path over rugged terrain by inspection only. In these cases, at least part of the path is usually profiled. Programmable printing calculators can greatly speed up the process of selecting paths, in rugged terrain, by eliminating the necessity for plotting partial path profiles. To maintain proper clearance, the calculator program produces a profile of clevation points which the actual terrain, including obstructions, should not exceed. To use the "Profile Program" for path selection:

- Establish possible antenna centerline elevation by adding reasonable tower heights to the ground elevations of the selected end-points.
- 2) Run the "Clearance Elevation at Incremental Distances" part of the "Profile" program, for the desired Fresnel zone clearance and carth curvature criteria, incrementing the program at even distance incre-

ments approximately 1/20 of the end-to-end path distance (for example 0.5. mi, 1.0 mi. or 2 mi.).

3) Check map elevations for the required path clearance, as shown in Figure 5. Trees and buildings located along the path will increase the map elevations of the path profile and must be taken into account. Any time the elevation exceeds the elevation given by the calculator output, additional tower height will be required at one or both ends of the microwave path. Terrain high-points that occur between calculator increments can be checked by interpolating between successive increments.

If the comparison of the calculator output and the map elevation look reasonable, a detailed path profile can be made of the microwave path.

Detailed Path Profile

In profiling a microwave path, the terrain contour heights found on the maps are entered on the profile graph paper. Enough points should be plotted so that high, low and relatively flat areas of contour are shown. Regular

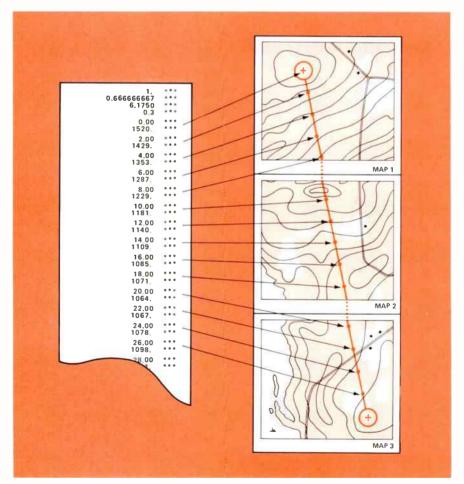


Figure 5. Checking map terrain against calculator generated output.

rectangular graph paper is used for this profile so that several values of K can be more easily shown on the final product.

When the profile contour has been completed, the desired Fresnel zone clearance is calculated for the profile high points, utilizing the "Calculate Fresnel zone Radius" portion of the "Profile" calculator program. The values of Fresnel zone clearances are then entered on the profile as shown in Figure 6.

Profiles drawn on rectangular graph paper use $K=\infty$ as a reference. Because of this reference, the difference between $K=\infty$ and the desired earth clearance K is next calculated for the high points utilizing the "Elevation at a Specific Distance" portion of the calculator program. Zero should be entered for the Π_X and Π_Y end-point clevations. The program will then give a negative value for the desired clearance. This value should be added to the desired Fresnel zone clearance on the profile. Figure 7 shows the placement of these points.

The antenna center-line heights can now be established by drawing a straight line (K= ∞) through or above the K clearance dots between the ends of the path. Once the antenna mounting heights are established, the antenna center-line elevation above mean sea level (AMSL) can be entered into the program for H_x and H_y. Then the "Path Profile Elevation at Incremental Distances" section of the program can be run for the locus of point elevations describing several K lines, as shown in Figure 8.

Reflection Point Analysis

If areas of water, swamps of flat ground exist along the microwave

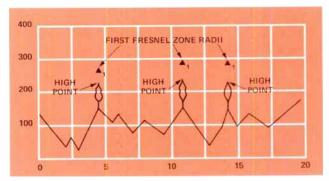
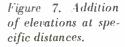
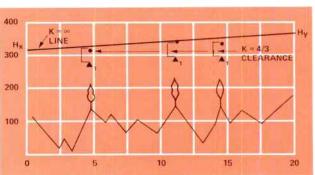


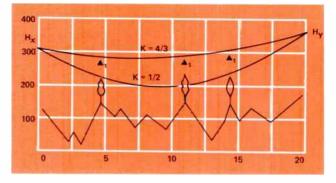
Figure 6. Fresnel zone clearance points.





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Figure 8. Profile elevations for different K values.



path, reflections can occur and affect the receive signal level. The Reflection Program can be used to calculate reflection points when the reflection point is level. Reflection points caused by sloping or rolling terrain can be adequately defined only by path tests.

The reflection point program calculates the distance at which reflections will be encountered for a given reflection point elevation. Figure 9 shows a set of reflection point calculations and the profile of a typical path. In this example, the mounting height of the antenna at point B was specifically chosen to create a reflection path that is obstructed by land at point C. The use of a calculator allows an engineer to try mounting heights antil the proper one to produce the desired obstruction is found.

After the profile is completed, it is field checked to accurately establish any map elevations that may be questionable. Tree and structure heights along the path are measured and enter-

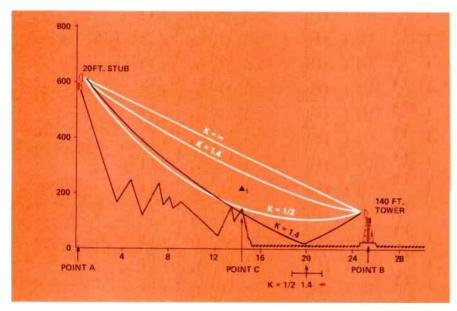


Figure 9. Obstructed reflection path.

ed on the profile. Potential reflection points along the path are visited to see if these points are adequately blocked by local obstructions.

The foregoing discussion briefly describes path profiling to provide a background for using the calculator programs presented below. The references listed in the bibliography describe path profiling in more detail and should be reviewed before preparing an actual path profile.

Calculator Programs

Two application programs are presented in the following pages. The first is called "Profile" and the second is called "Reflection". Each program is divided into three parts.

The first part, "Program Description" describes the programs purpose, lists the formulas on which it is based and states the program's operating limits. Warnings about common mistakes are also included in the Program Description.

The second part, "User Instructions" provides step by step instructions for using the calculator to perform the calculations specified in the instructions column of the User Instructions form.

The calculator must have the program listing stored in memory to perform the calculations.

The third part of each program is the "Program Listing". The Program Listing may be considered as a set of instructions to the calculator. It is keyed into the calculator memory before the calculations in the User Instructions are performed.

The IIP 97 uses a magnetic card for permanent storage. The Program Listing may be stored on a magnetic card for future use. Instructions for using magnetic cards are contained in the HP 97 Instruction Manual.

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Program Description

ity San	E Lenkurt 1105 County R Carlos	oad State	CA	Zip Code 94070
		Jiaie	<u>ол</u>	20000 04070
	tion, Equations, Variables, etc. am is designed to assist in preparir		At the option o	f the user, the program can
	ulations in imperial units (feet and			
The progra	m contains two subroutines; Fres	nel zone radius calculation:	s and beam center	line elevation calculations.
The subroutines	may be used separately or togethe	er as desired by the user. P	rint subroutines a	re also included at appropriate
oints to provid	e hard copy records of the calcula	tions.		
Any of the	following calculations may be pe	erformed:		
1.	Calculate and print the Freshel a	zone radius at a specific dist	tance.	
2.	Calculate and display the beam of	center-line elevation at a sp	ecific distance.	
3.	Calculate and print the beam cer			
4.	Calculate and print the clearance			
	Clearance elevation is the beam	center-line elevation minus	the desired Fresh	el zone radius.
This progr	am is referenced to the GTE Lenk	urt publication, "Engineeri	ing Consideration	s for Microwave Communi-
cations Systems.	" The following formulas appear	in that reference: Fresnel	Zone Radius; Imp	erial page 38; Metric page 82;
Earth Curvature	; Imperial page 12; Metric page B1			
Path Slope				
He =	$H_{X} - \left(\frac{H_{X} - H_{Y}}{D} * d\right)$ where: $H_{X} =$	= elevation of point x. Hy =	elevation of poi	nt v. D = total path distance.
d = distan	te to desired slope location.	y		
	·			
nerating Limits	and Warnings There is much	confusion regarding Fresh	el Zone radius les	s than 1. This program uses
· •	ing convention:			
For Fresh	el Zone radius less than 1 the prog	ram is always the value tim	es the first Fresh	el Zone radius (i.e., 0.6F1).
For Fresh	el Zone radius greater than or equi	al to 1, the program always	uses the square r	oot of the value times the
	el Zone (i.e., ÄF1).			

		PROFILE	6/29/78 Issue 3	
1 FreqGHz	∆d		d∔K>Hd I⊘M	2
H _X + H _y	D	d>Fz	z + K>H _{Ad} K>H _{Ad}	_

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(meters & kilometers) are required or a change back to Imperial ut is required, the following is performed: (units designation 1 = Imperial, 2 = metric) Operating frequency Total Path Distance Distance from one end of the path to the location at which the Fresnel Zone is to be calculated	hits None Freq/GHz D/Miles(Km)		designatio
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(units designation 1 = Imperial, 2 = metric) Operating frequency Total Path Distance Distance from one end of the path to the location at which the Fresnel Zone is to be calculated	Freq/GHz D/Miles(Km)		units designatio
Operating frequency Total Path Distance Distance from one end of the path to the location at which the Fresnel Zone is to be calculated	D/Miles(Km)		
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Distance from one end of the path to the location at which the Fresnel Zone is to be calculated			
Distance from one end of the path to the location at which the Fresnel Zone is to be calculated		B	
Fresnel Zone is to be calculated	d/Miles(Km)		
Fresnel Zone is to be calculated	d/Miles(Km)		
Fresnel Zone is to be calculated	d/Miles(Km)		
		c	See Below
Francel Zoco			
Units Designation			
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	Meters)	15	
	Meters)		
1st Fresnel Zone Radius Feet (Meters)		
1st Fresnel Zone Radius Feet (*NOTE: If these entries remain unchanged from previous	Meters)		
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STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEY\$	OUTPUT DATA/UNITS
	PATH PROFILE ELEVATION			
1*	The program is set for Imperial units (feet & miles). If metric units			
	(meters & kilometers) are required or a change back to Imperial			
	units is required, the following is performed:			
	(units designation 1 = Imperial, 2 = metric)	None	f_le	units designation
2°	Total Path Length	D/miles(Km)	B	
3°	Antenna center-line elevation AMSL at site X	H _X /feet (m)	4	
	Antenna center-line elevation AMSL at site Y	Hy/feet (m)	A	H _X
	AT A SPECIFIC DISTANCE			
4	Distance to point of calculation	d/miles (Km)	(4)	displayed output
5	Value of earth curvature	К	f_Ld	d/miles(Km)
	AT INCREMENTAL DISTANCES			
6*	Distance increment	∆d/miles(Km)	[f] [b	
7	Value of earth curvature	к	E	See Below
H _X ↓	$H_{d} H_{2d} ETC H_{y}$ $- \Delta d - \Delta d - ETC $			
	Units Designation		+ 1.333333333	
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	Distance to 2nd Point Miles (Km) ———— K Elevation at 2nd Point feet (m) ————— Other Points ————————————————————————————————————			•••
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	reet (m)		1 200.	

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STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNITS
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	(meters & kilometers) are required or a change back to Imperial			
	units is required, the following is performed:			units
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2*	Total Path Distance	D/miles (Km)	в	
3*	Antenna center-line elevation AMSL at site X	H _x /feet (m)	[`+] {]	
	Antenna center-line elevation AMSL at site Y	Hy/feet (m)	[A] []	Hx
4*	Distance increment	∆d/miles(Km)	fb	
5*	Operating Frequency	Freq/GHz	_f a]	
6	Portion of first Fresnel Zone required**	Fz		
	Value of earth curvature	к	D	See 8 elow
1	Fresnel Zone Radius Hat K Hat K Earth curvature Hy Hat H2c Hy Ad ETC D			1
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Other Points		
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snel Zone is required (i.e., $\sqrt{N} \cdot F_1$).		
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Program Listing

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	RTN	24		_	RCL5	36 05	
	*LBLb	21 16 12	Store Incremental		DSP4	-63 04	
10	STO3	35 03	Distance		PRTX	-14	1
	RTN	24	∆d		RCL7	36 07	
	*LBLa	21 16 11	Store Frequency		DSP1	-63 01	
	STO5	35 05	FGHz		PRTX	14	
	RTN	24	0.12	070	SPC	16-11	
	*LBLe	21 16 15	Set or Reset Metric		0	00	
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	GTOD	22 00	And Output		RCLO	36 00	
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	CFI	16 22 01			STO6	35 06	Preset Distance
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	*LBL1	21 01	1		-	-45]
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	RCL6	36 06			*LBLC	21 13	Run Fresnel Zone
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	RCL3	-55	1		GSB9	23 09	Units Subroutine
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	SPC	16-11					÷		-24	$H_s = H_x - \left(\frac{H_x}{I}\right)$	-Hy _]]
	RCLB	36 08			1	70	RCL6		36 06	$H_{s} = H_{x} - ($	5 ° //
		62			Ļ		X	_	-35		
	6	06			- F				_45	0 In 1995 Earth	Currentered
	DSP1	-63 01			Ļ		RCL1		36 01	Calculate Earth	Curvature
	PRTX	-14			L		RCL6		36 06		
	X	-35					-		-45	Imperial	
120	DSP0	63 00			L		RCL6		36 06		.
	PRTX	-14	= 0,6 F	1	-		X		-35	$H_{k} = \frac{(D \cdot d)}{k} \cdot \frac{d}{1.5}$	-
	SPC	16-11			- I		F1?	16	23 01	K K 10	
	1	01			-		GTOO		22 00		
	DSP1	-63 01			_	180	1		01	Metric	.
	PRTX	_14			1				62	$H_{k} = \frac{(D-d)}{k + 12.7}$	d
	RCLB	36 OB					5		05	^H k k • 12.7	75
	DSPO	-63 00	_		- I		*LBL5	_	21 05		
	PRTX	-14	= F 1		[RCL4		36_04		
	SPC	16-11	-1 ·				X		-35		
130	SPC	16-11	_				÷		-24		
	SPC	16-11			1		-		-45		
	SPC	16-11					RTN		24	$H_d = H_s - H_k$	
	DSP2	-63 02	-				*LBL0		21 00		
	CLX	-51			1	190	1		01	Metric Constan	t for
	RTN	24					2		02	Earth Curvatur	е
<u> </u>	*LBL6	21.06	Fresne	I Subroutine					62		
	RCL1	36 01					7		07		
	RCL6	36 06	-				5		05		
	RULO	45		Lat	1		GT05		22 05	[
140	-	36 06			-		*LBLB		21 08	Print Subrouti	ne
140	RCL6			2.1 $\sqrt{\frac{(D-d)d}{f_{GHz}D}}$	_		DSP2		63 02	[
	X	-35	—- F1= /	2.1 V fGHz D			RCL6		36 06		
L	RCL5	-		. 0.112			PRTX	\vdash	-14	Print Output	
<u> </u>	RCL1	36 01	_			200	Rŧ		-31	Subroutine	
	×	-35		-			DSPO	-	-63 00	1	
·	÷	-24		-			PRTX	+	-14	1	
	X	54	_	[10] IN 1	-		SPC	+	16-11	1	
L	F1?	16 23 01		7.3 $\sqrt{\frac{(D-d)d}{f_{GHz} D}}$	-		RTN	-	24		
	GTO0	22 00		7.5 V TGHz D			*LBL9	+	21 09	Print Units De	cignator
	7	07				<u> </u>		+	16-11		signator
150	2	02					SPC	+	01	1	
	·	-62				———	DSP0	+	-63 00	1 = Imperial	
	1	01						+ ;	6 23 01	2 = Metric	
	*LBL4	21 04				210	F1?	+-'	023 01	-	
[X	_35	5			210		+	14	-	
	STOB	35 08					PRTX	+-		4	
	RTN	24			_		RTN	+	24		
	*LBLO	21 00) Metri	c Constant		L	*LBLd	12	1 16 14	Run Specific I	Earth
	1	01		resnel Subroutin	е		STO4	+-	35 04	Curvature	
	7	07				L	Rt	+-	_31	4	
160		-62	2			L	STO6	+	35 06	4	
	3	03	3				GSB7	+-	23 07	4	
	GTO4	22 04	+				RCL6	-	36 06	4	
	*LBL7	21 07	7 Earth	Curvature			DSP2	+-	-63 02	4	
	RCLO	36 00) Subr	outine		220	PSE	+	16 51	4	
	RCL0	36 00	2			<u> </u>	R†	+-	-63 00	-	
	RCL2	36 02					DSPO	+	-03 00	-	
	-	4!		e Elevation			RTN	+	51	-	
	RCL1				_		R/S FLAGS	4	- 51	SET STATUS	
				BELS	E		10				0100
A 00		006 ^C	093	096		025	1 Imperial ((FLAGS ON OFF	TRIG	DISP
a 01	12 ^b	015 ^C		^d 213	e		1 Imperial (C Metric (C	Σ'n)	0 🗆 🛛	DEG 🖾 GRAD 🗆	FIX 🛛
0 21,1	157,1B9 ¹	035 ²	046	³ 074	4	154		-	1 2 8	RAD	ENG C
-1 ⁵ 18	B3 6	136 7	163	⁸ 196	9	205	3	-	3 🗆 🛛		n_2
					-			_			

UF.

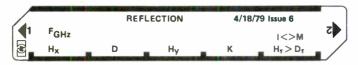
Program Description

Program Title	REFLECTION			
lame	John E. Hendricks, Jr., Staff Engineer			Date 2/6/79
Address	GTE Lenkurt, 1105 County Road			
City	San Carlos	State (CA	Zip Code 94070
This prog	ption, Equations, Variables, etc. ram calculates the parameters normally used in de e option of performing the calculations in imperia			
	be program uses a solution to the cubic equation d			
program listing		D		
The follo	wing formulas appear in that publication:			
	snel Zone radius – Imperial, page 38; metric, page	B2.		
	th Curvature – Imperial, page 12; metric, page B1			
	ence for the reflection point angle is: Appendix A			ting for Controlled

For Fresnel Zone radius greater than or equal to 1, the program always uses the square root of the value times the first Fresnel Zone (i.e., $\sqrt{N}F_1$).

This program will not work for negative values of K or when the reflection point elevation exceeds either end point elevations. For K = ∞ , use K = 9 X 1010, Larger values than 9 X 1010 may give erroneous answers. Program is accurate to 0.01 miles (0.016 Km) and reflection point clearance of 0.1 ft (.003 meters) for total path distances to 100 miles (160 Km).

16



TEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNIT
1	The program is pre-set for Imperial units (feet & miles).			
	If metric units (meters & kilometers) are required or if a change			
	back to Imperial units from metric units is required the following			
	step is performed:			
	(units designation 1 = Imperial, 2 = Metric)	None	f	units designatio
2*	Antenna center-line elevation AMSL at site X	H _x /Feet (m)	A	H _X
3*	Total path length	D/miles(Km)	8	D
4*	Antenna center-line elevation AMSL at site Y	Hy/Feet (m)		HV
5*	Value of earth curvature	K		к
6°	Operating frequency	Freg/GHz	fla	Freq
	Operating nequency	rieg/driz		Freq
7	Enter the elevation AMSL at the suspected reflection point	H _r /Feet (m)	E	See Below
°No	te: If these entries remain unchanged from previous calculations they	do not need to be re	e-entered.	
-	+ +			
	Units Drsignation		2095.00000 2015.00000 226.600000 240.00000 1.3333333 6.15 92.97 6.1750 2.20 0.11	

			Prograi	n Li	sung		
STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11			\sqrt{X}	54	
	STOD	35 00	Store H _x		STO8	35 08	
	RTN	24		060	3	03	
	*LBLE	21 12		060	Υ×	31	
	ST01	35 01	Store D TOTAL		RCLO	36_00	
	RTN	24			RCL2	36 02	
	*LBLC	21 13			PRTX	-14	Print Hy
	STO2	35 02	Store H _V		-	-45	
	RTN	24			STO6	35 06	
010	LBLD	21 14			ROL1	36 01	
	ST03	35 03	Store K		X	-35	
	RTN	24			ABS	16 31	
	*LBLa	21 16 11			RCL3	36 03	
	STO5	35 05	Store Frequency	070	PRTX	-14	Print K
	RTN	24			SPC	16-11	1
	*LBLe	21 16 15	Set Units		×	_35	
	F07	16 23 00	Designation		3	03	1
	GTOe	22 16 15	Ĵ,		X	-35	1
	SFO	16 21 00	Set Metric		1	01	
020	2	02			6	06	_
	RTN	24			÷	-24	1 🗐
	*LBLe	21 16 15			F07	16 23 00	1 <u>±</u> 1
	CFO	16 22 00	Set Imperial		GSB4	23 04	Store 8 = q * 2 COS $(240 + \frac{1}{3} COS^{-1} \frac{3 H_{x} - H_{y} + D + K}{16 q^{-3}})$
	1	01	out imperial	080	XZY	-41	
	RTN	24	ł			-24	1 1 명
		21 15	Run Program	+	COS-1	16 42	19 H
	*LBLE STO4	35 04	in on thogram		3	03	<u>m</u>
	DSPO	-63 00			÷	-24	5.
<u> </u>					2	02	ğ
030	F07	01			4	02	- 10
	2				0	00	+
		02	Print Units Designation		+	-55	40
	PRTX	-14	Print Units Designation		COS	42	
	DSP9	-63 09		090		02	l S
	RCLO	36 00	Beima ki	030	2 X	-35	8
	PRTX	-14	Print H _x				
	RCL4	36 04	a		ST•B	35-35 OB	σ
L	PRTX	-14	Print H _r		RCL1	36 01	
	-	-45			2	02	e e
	STOA	35 11			÷	-24	. ĝ
040	RCL2	36 02			ST+B	35-65 08	Ś
	RCL4	36 04			RCL6	36 06	
	-	-45			X<0?	16-45	
	STOB	35 12			GTO0	22 00	IF H _x ≥H _y
	+	-55		100	RCL1	36 01	D
	RCL3	36 03			RCLB	36 08	$O_{xr} = \frac{D}{2} - \text{Store B}$
	L X	-35				-45	Else
	F0?	16 23 00			STOB	35 OB	
	GSB4	23 04			*LBL0	21 00	$D_{xr} = \frac{D}{2} + \text{Store B}$
	RCL1	36 01			RCLB	36 08	
050	PRTX	-14	Print Total Distance		DSP2	-63 02]
	X ²	53	<u> </u>		PRTX	14	Print D _{xr}
	3	03	$q = \sqrt{(H_A + H_B) * K + \frac{D^2}{3}}$		RCL1	36 01	
	÷	-24	q = (I –	_45]
	+	-55	γ 4	110	STO9	35 09	
	4	04			PRTX	14	Print Dyr
	÷	24	Metric K = K + 8.5		SPC	16-11	
				STERS			
0 н _х	¹ D	2 H _V	³ K ⁴ H _R	⁵ FRE		7 <u>F</u> resnel	⁸ D _{xr} ⁹ D _{yr}
	DTOTA	L ^H Y				Zone	
S0	S1	S2	S3 S4	S5	S6	S7	S8 S9
<u> </u>	L,			-	,		
A ⊢	H _x – H _r	^Β H _γ – H _r	C D _{xr} * (D _{yr})	D		E	I
L .	<u> </u>	. ¥ ∵.(1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				

Program Listing

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
	RCLA	36 11			0	00	<i>w</i>
	RCL6	36 06]	170	*L8L3	21 03	radians
	RCL1	36 01			RCL3	36 03	9
	÷	-24			X	-35	0
	RCL8	36 08	1 5		ST÷6	35-24 06	1 0 2
	×	-35	0 _{xr} • (-D _{yr})		RCLO	36 00	1 1
	-	-45			RCL4	36 04	
120	RCL8	36 08	<u></u>		+	55	x - Hr • (K2a + Hr+Hr) adians
	STO6	35 06	$\frac{D_{Xf}}{D} (H_X - H_y) - \left(\frac{1}{2} + K \right)$		GSB7	23 07	
	RCL9	36 09	L	-	+	55	s 3 +
	CHS	-22	l T		RCL6	36 06	$I_X - H_r$ • (K2a
	X	-35	É É	180	R-+0	16 46	HX
	STOC	35 13			TAN	43	1 1 2
	1	01	× o v		X	-35	2 o 7
		-62	L 10		÷	-24	
	5	05	1 ÷ °		TAN"	16 43	TAN
			H _x -H _r		-		
130	F0?	16 23 00	- I I		RCL6	36 06	- 7.
130	GSB4	23 04	1 i i i i i i i i i i i i i i i i i i i		R+O	16 46	- Le
	÷	-24	h _c = H _x Metric K		-	-45	1 .
	RCL3	36 03	Path _C Met		PRTX	-14	LR = Tan'
	÷	-24	6		STO6	35 06	-
	_	-45		190	SPC	16-11	1
	PRTX	-14	Print Path Clearanc	e	RTN	24	Print Reflection Ar
	X<0?	16-45	Stop Program		*L8L4	21 04	Metric
_	RTN	24	IF Path Obstructed		8	08	K Conversion
	RCLC	36 13					
140		-				-62	<u>-</u>
	RCL5	36 05			5	05	K Metric = K + 8.5
	OSP4	-63 04			X	<u>-35</u>	
	PRTX	-14	Print Frequency		RTN	24	
	DSP2	-63 02			*L8L5	21 05	
	÷	-24			1	01	Metric
	RCL1	36 01	8	200	7	07	Fresnel Zone
	÷	-24				-62	Constant
	_√X	54	CLEARANCE D _{Xr} * (-D _{yr}) frequency • DTOTAL		3	03	-
150	F07	16 23 00			GTO1	22 01	-
							A
	GT05	22 05	PATH CLEARANCE $D_{xr} \cdot (-D_{yr})$ frequency $\cdot D$		°L8L6	21 06	Metric
	7	07			1	01	Earth
	2	02	A P	۷ L	2	02	Radius • 2
	•	-62			7	07	
	1	01	ປີ ດີ ະ "		4	04	7
	*L8L1	21 01	F		6	06	1
	X	-35	V	210	GTO3	22 03	-
	÷	-24	PATH CLEAF 72.1 Imperial) (Dxr + (frequer fe > Then F = ./F.	. –	*L8L7	21 07	-
	1	01	het 7	۷	F0?	16 23 00	
	XZY	-41			GT08	22 08	Convert
	X <y?< td=""><td>16-34</td><td></td><td></td><td>5</td><td>05</td><td>Feet To</td></y?<>	16-34			5	05	Feet To
	X ²	53	, N		2	02	Miles
60	STO7	35 07			8	08	
	PRTX	-14	Print Fresnel Zone		0	00	
	RCLA	36 11			÷	-24	1
	GSB7	23 07			RTN	24	1
	F0?	16 23 00		220	*L8L8	21 08	
	GTO6	22 06			EEX	-23	Convert
	7	07			3	03	Meters To
	9	09			 	-24	Kilometers
	2	02			RTN	24	Knometers
	4	<u> </u>	LABELS	L	FLAGS	24	SET STATUS
A 00	D1 ^B 00		007 ^D 010	E 026	⁰ On=Metric		
2		14	d 010	e U20	1.	FLAGS ON OFF	TRIG DISF
0	13				016/022		OEG 🔯 FIX
) 10	04 1 15	5 3 2	3 170	4 192	2	1 2 2	GRAD SCI RAD ENG n_2
	00 6 20		211 8 220	9			



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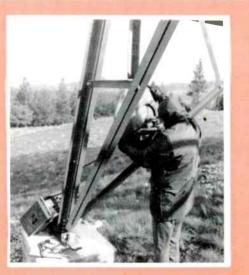
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EF&I GTE Lenkurt's Engineer Fur-

nish and Install service provides overall management of planning, engineering, construction, installation, testing and maintenance of GTE Lenkurt communications systems.

GTE Lenkurt personnel will plan a system in detail; conduct cost studies, obtain all



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necessary parts and equipment; arrange for construction of access roads; supervise installation; provide comprehensive project information and conduct on-the-job training for operating and maintenance personnel. Or, if the customer prefers, GTE Lenkurt will perform only specific portions of planning and installation.





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