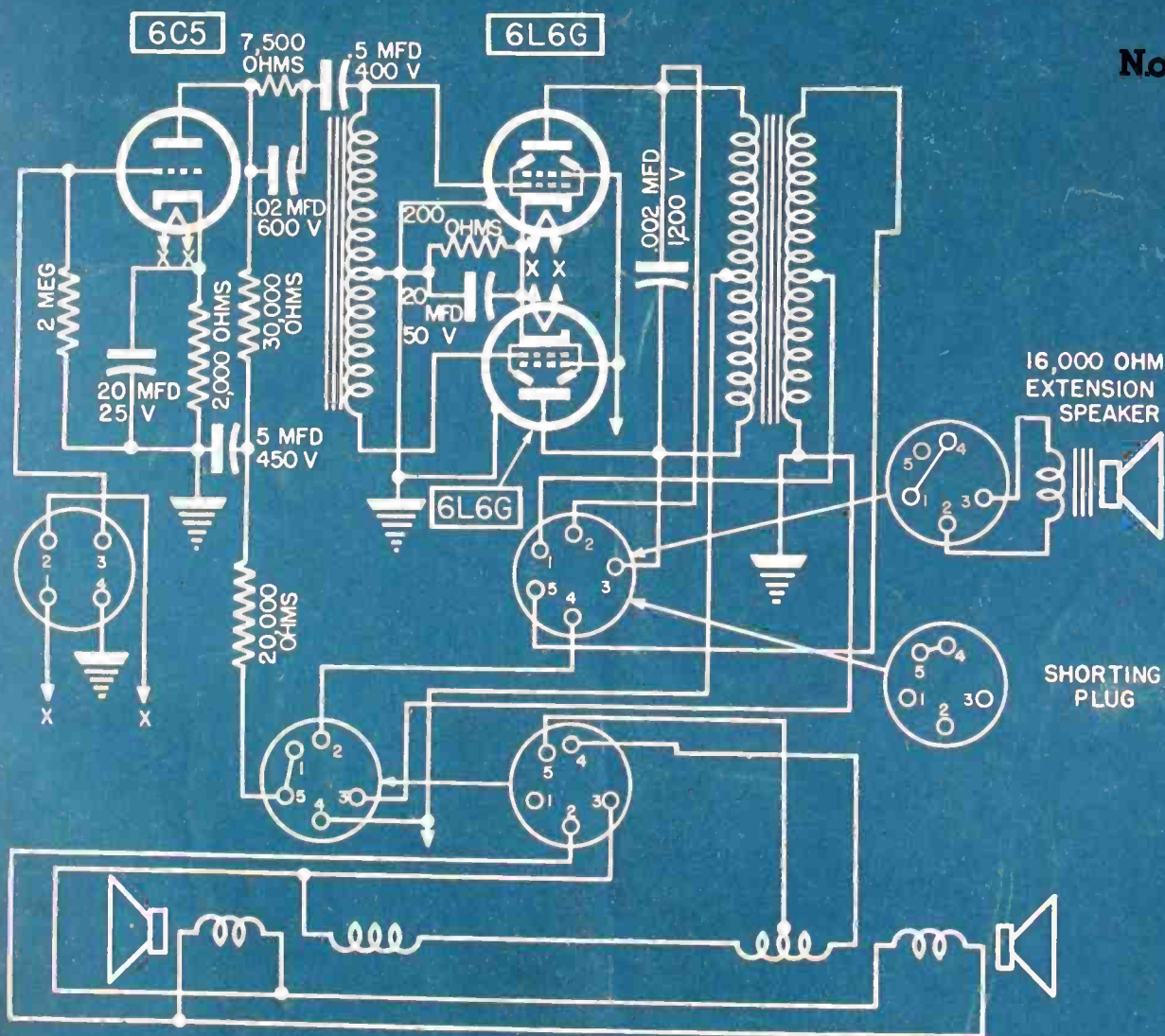


# SERVICE

November  
1945



High-fidelity 25-watt amplifier featuring bass-reducing control and provision for dual speaker operation. (See pages 46 and 47.)

# He reads the "C-D Capacitor" and gets a chance to look around



He's not a stunt man. Just a regular radio guy like you and all the others. The reason he rides so easy is that he gets a good head start . . . keeps his nose to the ground, but has his eyes wide open. Every month he pinches a couple of minutes off his working time to read the C-D Capacitor and get the tip-off on short cuts in servicing.

Imagine! A whole month's worth of service helps that you can swallow at one sitting! Nothing for you to do . . . not a penny to send; just write us and "The Capacitor" will come to you by mail regularly. Twelve times a year we'll send you this helpful, pocket-sized magazine. Write to: "The Capacitor", Cornell-Dubilier Electric Corporation, South Plainfield, N.J.



## A TIMELY POSTER FOR YOU!



An attractive blue and yellow display card for your window or wall that reads "we use no war-weary surplus". It conveys to your customers that you use only genuine and original C-D Capacitors in all service jobs. Ask your local jobber for this poster today!

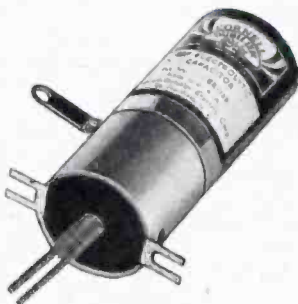
## HAVE YOU SEEN THIS CATALOG?



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## PRACTICAL E Z's!



Here's one of several types of capacitors that wins the serviceman's award for "all-around replacement." Adaptable for upright or under-chassis mounting, E Z's incorporate C-D's famous etched foil features in design and construction.

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the greatest name in  
**CAPACITORS**



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the most complete digest of  
tube information available.

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# KEN-RAD

DIVISION OF GENERAL ELECTRIC COMPANY

OWENBORO, KENTUCKY

**T**HE intensive postwar expansion plans of the aircraft industry, indicating a production of around 50,000 planes for civilian travel, projects many unusual opportunities for the Service Man. For this large program will require wide-scale installation, servicing, and maintenance facilities for the planes' receivers and transmitters . . . a program that will tax the present facilities.

Servicing of this equipment will, of course, demand not only a specialized knowledge of aircraft units, but the acquiring of either of two licenses; a first-class commercial license for transmitter tests and a CAA license to permit testing of equipment, as well as installation, or any necessary plane alteration to accommodate equipment changes. While these license examinations will require schooling and hours of study, the results should prove quite profitable.

The hundreds of airports scheduled for construction will demand one or more shops on the field for radio equipment servicing. Such servicing will call for quite a profitable rate structure, commensurate with the specialized training needed for the aircraft activities. In most instances, it will be possible to arrange for a weekly maintenance and service fee, since some equipment will require checkups quite often.

Components, accessories and battery sales will also be a profitable feature of aircraft service shops. Battery sales alone will be substantial, since all planes will use battery-operated units, dry and wet. The wet-cell batteries will require charging, another medium of income.

The CAA has published a list of current airports and will soon publish a list of those airports to be constructed. You can secure such listings from the CAA department of information.

Aircraft radio servicing offers many advantages. Study its possibilities in your community now.

**T**HE postwar f-m receivers covering the new bands are scheduled to feature an unusual tuning-dial numbering system. The first frequency (88.1 mc) will be designated as 201. The second assignment (88.3 mc) will be known as 202. This will continue up to 300. It had been planned to begin with 1 for the first channel, but the FCC said that the bands may be extended up or below the new assignments and thus provision should be made for such extensions.

This is a standard that will undoubtedly be adopted by all manufacturers to simplify f-m tuning. A wise move!

## LEWIS WINNER

Editor

**ALFRED A. GHIRARDI**

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**Paul S. Weil, Vice Pres.-Gen. Mgr.**



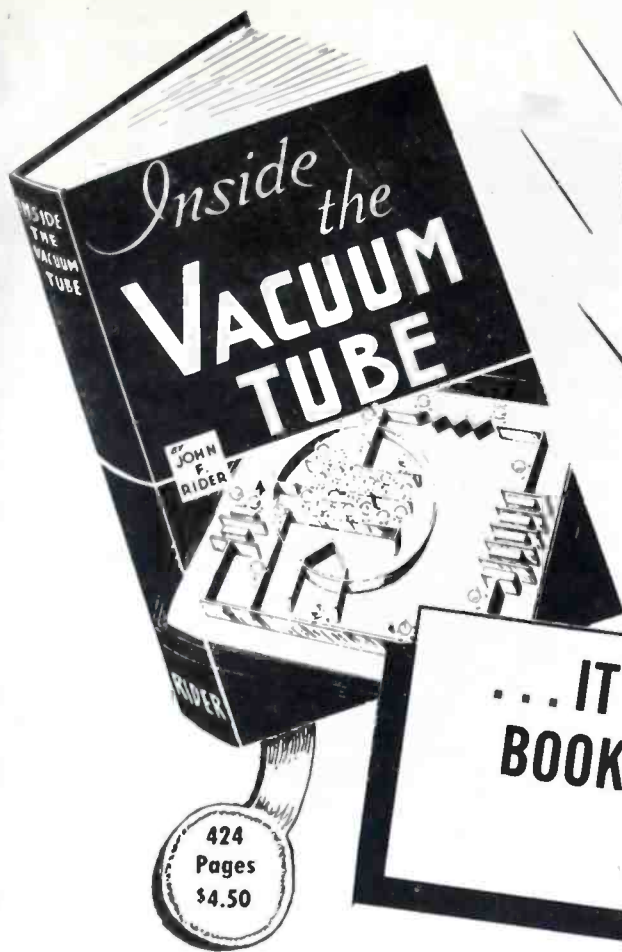
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**T**his is not just another book on the vacuum tube, but a typical Rider Book, offering a new approach to the subject—presented with a technique that makes its message clear and easy to understand. Here is a solid, elementary concept of the theory and operation of the basic types of vacuum tubes upon which can be built more advanced knowledge.

After explaining the electron theory, the text presents a discussion on electrostatic fields, on the theory that the reader's understanding of the distribution and behavior of the fields within a tube will give him a better picture of why amplification is accomplished within a tube and how the grids and plates are interrelated.

To give a clear physical picture of its subject, the book

employs novel physical devices. For example, certain diagrams and graphs are repeated, to reduce to a minimum the bother of turning pages back and forth to read text and drawings. Another innovation is the use of anaglyphs, "three-dimensional" pictures of phenomena heretofore seen only in two dimensions. Viewed through glasses supplied with the book, they are invaluable aids toward the rapid understanding of the text.

Although this is an elementary book on a fundamental subject, therefore a goldmine for the student; developments in radio and the new fields of television and microwaves make it a must for the libraries of servicemen, amateurs and engineers. Place your order today.

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Forget

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They Provide Schematics and Essential Servicing Data on American Made Radio Receivers.







# With this instrument a new era in tube testing begins

... Remember ...

As you read below the many other features of this pioneering instrument, remember this: It is a Simpson instrument, with all that implies in creative engineering research, in controlled testing and manufacture. Simpson products are not "assembled", they are engineered and built in the Simpson plant. Practically every component part, from the dial and movement to the beautifully designed panels and the bakelite cases and panels, is made by Simpson. It is this that makes Simpson's the "instruments that stay accurate" with ideas that stay ahead.

## SIMPSON MODEL 330 MUTUAL CONDUCTANCE TUBE TESTER

1. Size—15½" x 9½" x 6½"
2. Case—Sturdy plywood construction, with heavy fabricoid covering, corners trimmed in leather, rustproof hardware—removable cover with slip type hinges.
3. Panel—Heavy molded bakelite, beautiful satin grained finish. All characters, numerals, and dial divisions are engraved and filled in white, insuring long wearing qualities.
4. Meter—4½" rectangular of modern design with artistic four-colored dial indicating good, fair, doubtful, and bad—also "Percentage of Mutual Conductance" scale.
5. Sockets provided for all types of tubes with two spare socket positions.
6. Neon glow tube incorporated to indicate shorted tubes.
7. New simplified revolutionary switching arrangement (see description above).
8. The tube chart provided is arranged for quickly identifying the tube and setting the controls.
9. Tests tubes with voltage applied automatically over the entire operating range and under conditions approximating actual operation in a radio set.

Ask Your Jobber

## The New Simpson Mutual Conductance Tube Tester Brings To Radio Servicemen and Dealers An Entirely New Method of Testing Tubes And A Revolutionary New Switching Arrangement!

Tube manufacturers consider that a radio tube has reached the end of its usable life when it falls to 70% of its rated value. Until now there has never been an instrument to test tubes in percentage terms.

But now here is such an instrument. The new Simpson Model 330 tests tubes in terms of percentage of rated dynamic mutual conductance—a comparison of the tube under test against the standard rated micromho value of that tube. The colored zones on the dial coincide with the micromho rating or the percent of mutual conductance, indicating that the tube is good, fair, doubtful or definitely bad. Thus, at a glance, you can check the tube against manufacturers' ratings. If, for any reason, it becomes desirable to know the actual value in micromhos, the percentage reading may be easily converted.

This is the way tubes should be tested—the way testers always should have worked—but Simpson is first again in bringing this needed development. It tests tubes with voltage applied automatically over the entire operating range, reproducing more completely than ever before the actual conditions under which a tube functions in a radio set. No instrument, not even delicately adjusted laboratory devices, can do this 100%. But this new Simpson Mutual Conductance Tester approaches perfection as never before.

Besides this revolutionary new method, Simpson offers you an equally revolutionary switching arrangement. The circuit is so arranged that, even though there are numerous combinations possible, very few switches require moving to test any one tube. Many of the popular tubes are tested in the "normal" position without moving any of the nine tube circuit switches.

Ten push button switches and nine rotating switches of six positions each provide infinite combinations in tube element and circuit selection. Only a few settings are necessary for the most complicated tube. The tube chart provided is arranged for quickly identifying the tube and setting the controls.

When you have finished a tube test, the Automatic Reset takes over to speed and simplify the next test. Just press the reset button and instantly all switches, both push button and rotary, return to normal automatically!

Here is the test instrument you have had a right to expect from Simpson. With greater flexibility in its circuit and switching arrangement than any other tester can provide, it gives maximum provision against obsolescence. It's the tester of a new era.

SIMPSON ELECTRIC COMPANY  
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INSTRUMENTS THAT STAY ACCURATE



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**WANTED**—Complete recording set. M. Taonouchi, 6713 A. Siskya Ave., Newell, Calif.

**SELL OR TRADE**—Hammarlund variable condensers and several sets of plug-in coils for Comet Pro. What have you? D. Pommiss, 401 Schenectady Ave., Brooklyn, N. Y.

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**FOR SALE**—Four 4' morning glory horns; 4' flat horn for car; 4 Fox driver units with 1000 ohm fields; 1 Fox driver unit with 6 volt field; 4 Rola G-12 6 volt heavy duty field speakers; \$150 for lot. Also 6 volt 20-watt amplifier and 30-watt electric, \$50 ea.; G:E portable recorder and record player; Federal symphonic 16 complete and large supply recording disc. Loren Beatty, 2408 Queen Ave., Middletown, Ohio.

**WILL TRADE**—Triplet portable lab model 1181; multimeter and signal generator. Want 12" P.M. speakers or a condenser analyzer. A. T. Zintner, 3153 Agate St., Phila., 34, Pa.

**SELL OR TRADE**—SW-3 with coils and power pack. Want camera or record player. Walt Westman, 2310 Midlothian Drive, Altadena, Calif.

**WANTED**—RCA #816K chassis, less tubes and speaker. State condition and price. Kuehne Radio, Bryan, Ohio.

**WILL TRADE**—Ihagee revolving back camera with Carl Zeiss Tessar f4.5 lens focal plane shutter 1/15 to 1/1000 sec. filters and accessories. Want medium power transmitter or good communications receiver. John T. Craig, 611 S. Silver, Deming, New Mex.

**WILL TRADE**—Wells-Gardner Model 6F, 16 tube. Want ultra stratosphere "10" or other long-wave radio. H. F. Teisinger, 1256 Walker St., Waterloo, Iowa.

**FOR SALE**—Tubes and parts at bargain prices. Send for list. Want to rent code tape machine and tapes. Fred Humphrey, 117 N. 20th St., Philadelphia 3, Pa.

**WANTED**—Riders #6, 7, 8 and 10. Elliott Reames, 1149 Washington Ave., Muskegon, Mich.

**FOR SALE**—Triplet #1212 tube tester, complete with instructions and wiring diagram; A-1 condition \$18 postpaid. F. S. Tourillatte, 11 Lauren Park, Norwich, Conn.

**SELL OR TRADE**—Dumot 5" scope model #148. Want communications receiver, test equipment or camera. Ben L. Sandberg, 36 Washington Village, Asbury Park, N. J.

**WANTED**—Echophone model EC-1 or Hallcrafters model S-36. Joseph C. Baker, Weedsport, New York, R.F.D. #2.

**FOR SALE**—New tubes at list; Meissner ac-dc kits, 2-tube, \$7; 3-tube, \$8 plus 20c. postage per kit. Need test instruments. Edward Howell, Route 2, Dillon, S. Carolina.

**WANTED**—Multitester, signal generator, tube tester and set tester in good condition. Write, stating full description and price. Wm. H. Womack, Box 589, Mayfield, Ky.

**FOR SALE**—Teco tube tester T-10, almost new; Philco auto radio and one home radio; also meters, parts, etc. Write for list. Harold Mueller, Box 323, Rugby, N. Dak.

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**WANTED**—Rider's Manuals, late model tube checker, signal tracer or vacuum tube voltmeter. Bill's Radio Service, 11 Halsey St., Providence 6, R. I.

**FOR SALE**—Green Flyer dual speed phono motor, type 3DG4, complete with turntable and speed dials, \$12. A. P. Bondgill, 509 Hancock St., Wollaston 70, Mass.

**WANTED**—Majestic model 60 or 160 tuning motor; Majestic 60 chassis and speaker G5. Reasonable. Will sell 4 years back Radio World Weekly. C. E. Peters, 2925 Apple St., Lincoln, Neb.

**FOR SALE**—Over 2,000 tubes at O.P.A. list prices or less, many pre-war. M. E. Dominick, Chicago, Ill.

**WANTED**—National SW58 or Sargeant regenerative radio. Must be in good condition. J. W. King, 525 Meridian, Anderson, Ind.

**FOR SALE**—Two used Philco auto radios and used Arvin 8-tube radio, \$25 ea.; also two ¼ h.p. motors, \$14 ea., and one 25 Cabbes automatic, \$15. Paul Capito, 637 W. 21st St., Erie, Pa.

**SELL OR TRADE**—Martin handcraft cornet and case, cost \$150. Want signal generator, multimeter and Rider's Manuals. Francis E. Manigold, Box 3003 Sta. A, El Paso, Texas.

**FOR SALE**—Crosley car radio, single unit, with lead-in, \$12; other radios; small assortment volume controls, resistors, P.M. and dynamic speakers; earphones; condensers; coils; power and audio transformers, and some tubes. Also 28 back issues Radio Craft; 20 of Radio News, and 13 of Radio. Hal Bundy, 119 Chlp-deva Ave., Manistique, Mich.

**FOR SALE**—Sensitive d-c relays, coil resistance, 8,000 ohms, contacts; single pole, double throw, rated 2 amps, at 115v a-c, \$1 ea. Mack, P. O. Box 123, New Hyde Park, N. Y.

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**SELL OR TRADE**—Pilot Super Wasp, also SW5, both with coils, tubes and speakers; also two short-wave radios, 3 and 4 tubes; plug-in coils in panel, built-in power supply. G. H. Gerhold, 9307 114th St., Richmond Hill, Long Island, N. Y.

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**WILL TRADE**—Hockey type shoe skates, size 8, almost new. Want Ghirardi Radio Physics course. George E. Aldrich, 150 W. 98th St., Apt. 31-W, New York 25, N. Y.

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Isolanlite 1½" x ¼" diameter forms, threaded 2½ meter work, 5c. ea., and point stand off insulators, 2½ meter, ea. H. Arras, 277 E. 1st St., Mansfield, Ohio.

**SELL OR TRADE**—Radio Physics Course Radio Troubleshooters Handbook 3rd revised 1943, by A. A. Ghirardi, C. Mathematics for Electrician and Radiomen, by Cooke. Want 8" rim-drive tube table top, 1-11726, 1-3523, 1-2525, 2 tubes. William C. Stadler, 49 Mt. Ave., Brooklyn 7, N. Y.

**FOR SALE**—New R.C.P. #804 tube set tester, \$87. Triplet new #1213 0 tester, \$30. J. J. Lubin, 2049 McGee Ave., New York 62, N. Y.

**WANTED**—Transmitter plate transformer (1500, 1750 or 2000 volt); also, 200 300 m.a. swinging and smoothing chokes. Louis C. Selez, 357 S. 1st St., Ishpeming, Mich.

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**FOR SALE**—Weston tube, condenser and resistance checker. Tests all tubes & Acorn. Price \$45. John H. Oxley, 1905 - 17th Ave., Vero Beach, Fla.

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Dept. S-115, SPRAGUE PRODUCTS CO., North Adams, Mass.



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A background of *Performance*—over 50 years—is the *inside story* of the popularity that has brought leadership to *Thordarson* transformers. *Performance* over the years, after all, is the only true test of product quality.

Consumer acceptance will continue because *Thordarson* research and design engineers are never satisfied just keeping abreast of the times. These men are continually developing many transformer components which are instrumental in the production of new and better performing devices and equipment for the electronics industry.

This same pioneering spirit has been responsible for many new *Thordarson* transformer applications and developments during the war . . . all of which will be available shortly for civilian requirements.

*Thordarson's* well-tested methods of sales promotion and distribution will continue their joint task of making *Thordarson* Transformers, together with complete information on their applications and use, available to everyone in the field.

Always think of *Thordarson* for top-notch transformers!

500 WEST HURON ST., CHICAGO, ILL.



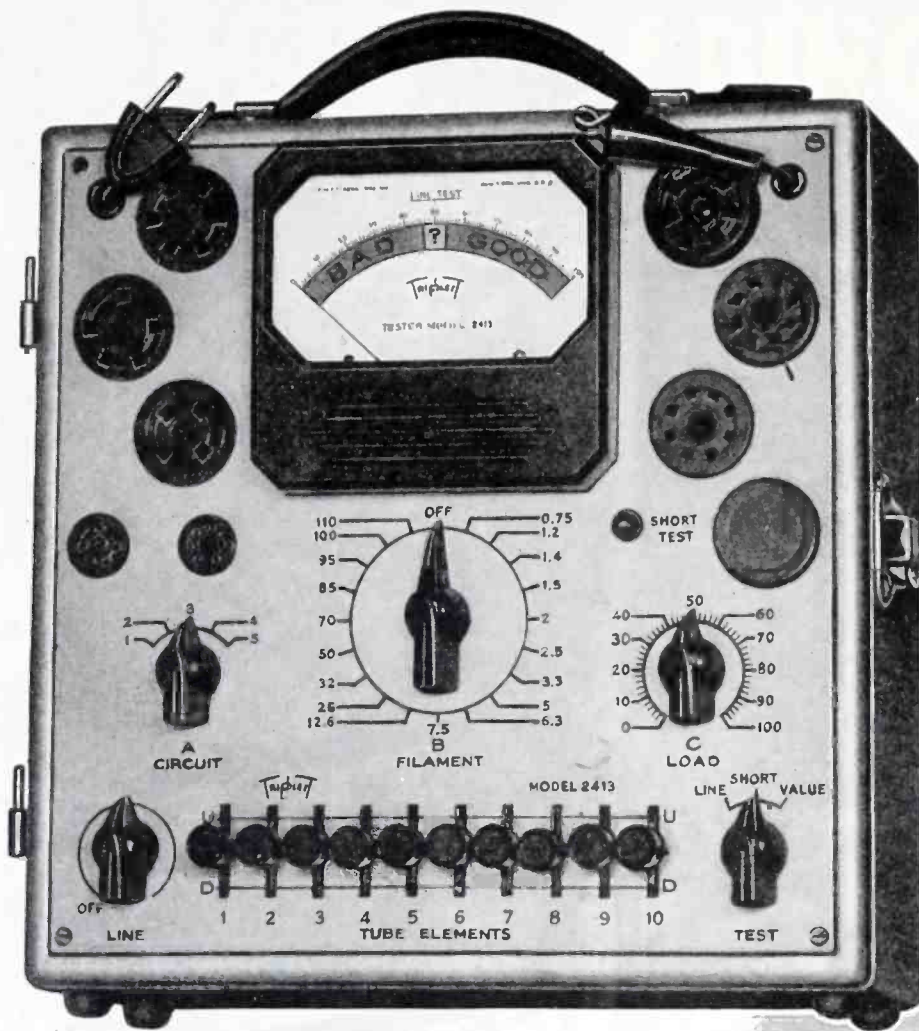
ORIGINATORS OF TRU-FIDELITY AMPLIFIERS

# THORDARSON

*ELECTRIC MANUFACTURING DIVISION*

**MAGUIRE INDUSTRIES, INCORPORATED**





**MODEL  
2413**



is another  
member of the  
**NEW TRIPLETT**  
Square Line



# The New Speed-Chek Tube Tester

**MORE FLEXIBLE • FAR FASTER • MORE ACCURATE**

Three-position lever switching makes this sensational new model one of the most flexible and speediest of all tube testers. Its multi-purpose test circuit provides for standardized VALUE test; SHORT AND OPEN element test and TRANSCONDUCTANCE comparison test. Large 4" square RED • DOT life-time guaranteed meter.

Simplicity of operation provides for the fastest settings ever developed for practical tube testing. Gives individual control of each tube element.

New SQUARE LINE series metal case 10" x 10" x 5 1/2", striking two-tone hammered baked-on enamel finish. Detachable cover. Tube chart 8" x 9" with the simple settings marked in large easy to read type. Attractively priced. Write for details.

## Additional Features

- Authoritative tests for tube value; shorts, open elements, and transconductance (mutual conductance) comparison for matching tubes.
- Flexible lever-switching gives individual control for each tube element; provides for roaming elements, dual cathode structures, multi-purpose tubes, etc.
- Line voltage adjustment control.
- Filament Voltages, 0.75 to 110 volts, through 19 steps.
- Sockets: One only each kind required socket plus one spare.
- Distinctive appearance with 4" meter makes impressive counter tester—also suitable for portable use.



# Triplet



**ELECTRICAL INSTRUMENT CO. BLUFFTON, OHIO**





designs of  
**DISTINCTION**

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For hundreds of years these proud guildsmen stamped their guild marks or signatures on their creations.

A few firms today still preserve that spirit of craftsmanship. You find it in the plants of Detrola Radio. That is why the "guild mark" of Detrola Radio on a radio receiver, record changer or other electronic instrument is a guarantee of production quality. The world's finest merchants, and their customers recognize the value of this mark.

DIVISION OF INTERNATIONAL DETROLA CORPORATION  DETROIT 9, MICHIGAN





# PRECISION MACHINERY plus PRECISION-EL means QUALITY in Mt. Carmel, Ill.

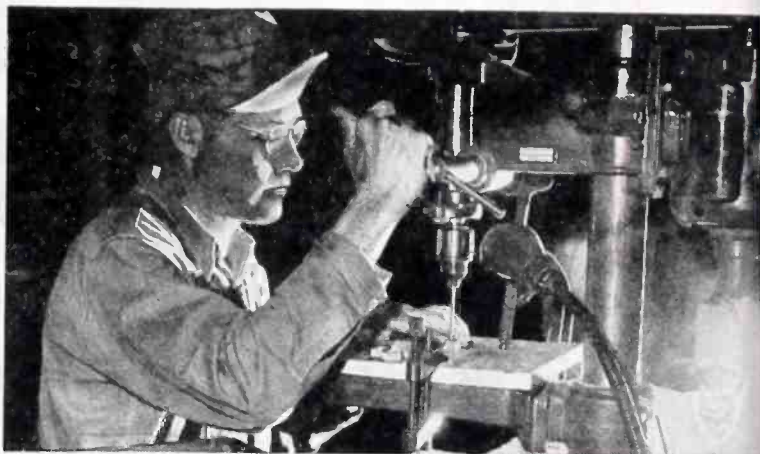
Precision machinery is part of Meissner's famed "precision-el" corps, too, and the men and women who build Meissner quality electronic equipment are the first to share the credit with their bench and tool-room friends. The photographs on this page show typical precision-el "teams" at work.



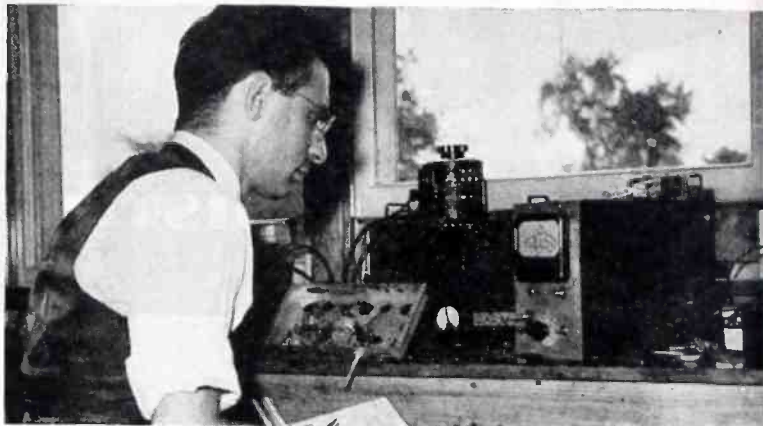
Here's a man who smiles proudly as his "helper"—a precision lathe—does a good job of holding extremely close tolerances.



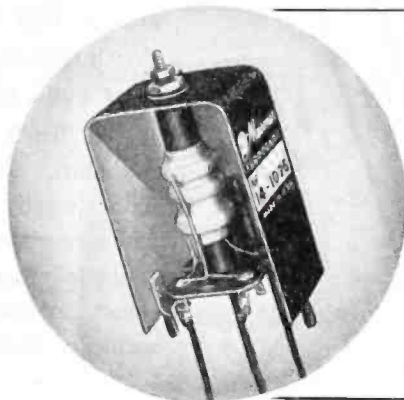
His "partner" receives a delicate adjustment with all the skill he can command. This care of equipment by Meissner *precision-el* has meant higher quality and fewer shut-downs for repairs on a big war job.



Here's another winning combination. Even the smallest parts warrant careful machining at Meissner. It's another reason for precision performance by Meissner products.



This is the proof of the pudding. "Rejects" are surprisingly few, even under the sharp eye of the sensitive testing instruments used by this member of Meissner's *precision-el*.



#### Replace Broadcast Band Coils Easily

These Adjustable-Inductance Ferrocart (iron core) coils will replace Antenna, RF or Oscillator coils without the trouble of locating "exact duplicates" because they are continuously variable in inductance over a wide range. The inductance of the old coil is easily matched by simple screwdriver adjustment. Ferrocart iron cores add gain and selectivity to the receiver. Available shielded or unshielded, shipped with complete instructions. Order by number. 14-1026 Univ. Ant. Coil; 14-1027 Univ. R.F. Coil; 14-1028 Univ. Osc. Coil. Price \$1.50 each.



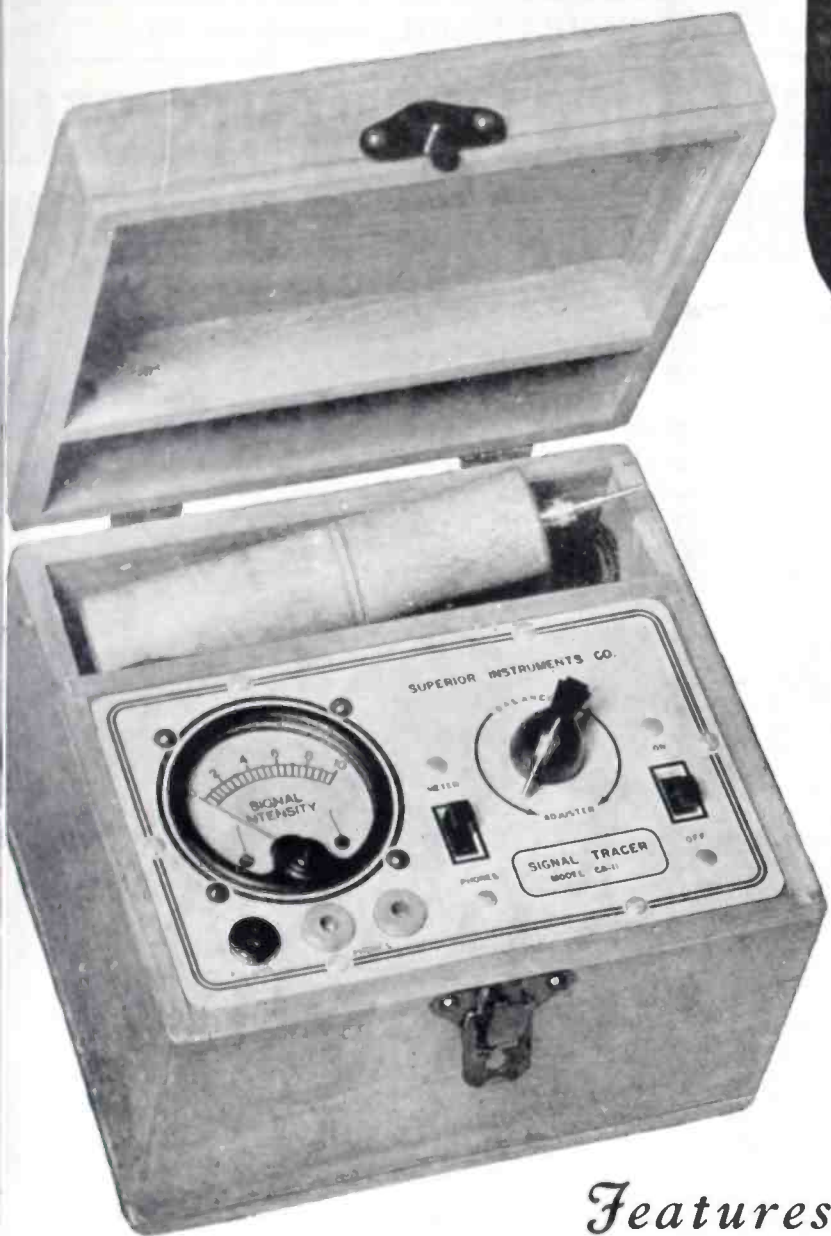
# MEISSNER

MANUFACTURING COMPANY • MT. CARMEL, ILL.

**ADVANCED ELECTRONIC RESEARCH AND MANUFACTURE**  
Export Division: 25 Warren St., New York; Cable: Simontrico

The New Model CA-11

# SIGNAL TRACER



*Simple to operate*  
*... because it has only*  
**ONE** connecting cable—  
**NO** tuning controls!

**I**NTRODUCED in 1939-1940 Signal Tracing, the "short-cut" method of Radio Servicing quickly became established as the accepted method of localizing the cause of trouble in defective radio receivers. Most of the pre-war testers (including ours) were bulky requiring a number of connections before the unit was "set for operation" and included a tuned amplifier which had to be "retuned" to compensate for signal shift.

The new model CA-11 affords all the advantages offered by the pre-war models and only weighs 5 lbs. and measures 5"x6"x7".

Always ready for immediate use without the necessity of connecting cables, this amazingly versatile unit has **NO TUNING CONTROLS**.

Essentially "Signal Tracing" means following the signal in a radio receiver and using the signal itself as a basis of measurement and as a means of locating the cause of trouble. In the CA-11 the Detector Probe is used to follow the signal from the antenna to the speaker—with relative signal intensity readings available on the scale of the meter which is calibrated to permit constant comparison of signal intensity as the probe is moved to follow the signal through the various stages.

## Features

- ★ **SIMPLE TO OPERATE**—only 1 connecting cable—  
**NO TUNING CONTROLS.**
- ★ **HIGHLY SENSITIVE**—uses an improved Vacuum Tube Voltmeter circuit. Tube and resistor-capacity network are built into the Detector Probe.

- ★ **COMPLETELY PORTABLE**—weighs 5 lbs. and measures 5"x6"x7".
- ★ **Comparative Signal Intensity** readings are indicated directly on the meter as the Detector Probe is moved to follow the Signal from Antenna to Speaker.
- ★ Provision is made for insertion of phones.

Please place your order with your regular radio parts jobber. If your local jobber cannot supply you kindly write for a list of jobbers in your state who do distribute our instruments or send your order directly to us.

The Model CA-11 comes housed in a beautiful hand-rubbed wooden cabinet. Complete with Probe, test leads and instructions.

**\$18.75**  
NET PRICE



**SUPERIOR INSTRUMENTS CO.**  
DEPT. B-227 FULTON STREET  
NEW YORK 7, N. Y.



# SYLVANIA NEWS

## RADIO SERVICE EDITION

NOV. Published by SYLVANIA ELECTRIC PRODUCTS INC., Emporium, Pa. 194

# SYLVANIA "LOCK-IN" ADVERTISEMENTS SEL THIS SUPERIOR TUBE TO NATION'S MILLIONS

**SYLVANIA  
SERVICEMAN  
SERVICE**

by  
**FRANK FAX**



A large, attractive, three-color display banner featuring the phrase "Complete Radio Service" is now ready for distribution to servicemen by Sylvania.

The banner measures 46 by 28 inches, is printed in black, green and white on special weather-proofed "duckine" material, making it suitable for use either inside or outside of the store. It has six metal grommets to provide extra reinforcement.

This useful, durable and attractive display banner may be obtained for only \$.40—or three for a dollar—from your local Sylvania distributor, or by writing to me at Sylvania Electric Products Inc., Emporium, Pa.

This banner is only one of the items on an extensive list of Sylvania promotional material designed to help servicemen merchandise both their own service and Sylvania radio tubes.

**YOUR NEXT RADIO NEEDS "LOCK-IN!"**

"PROVED IN RADAR!  
BEST FOR YOUR SET!"

LOOK FOR LOCK-IN TUBES BEFORE YOU BUY A RADIO!  
Why? Because more than any other tubes, Lock-Ins are in step with the trend in modern radio—a trend toward higher and higher frequencies.  
Proved in Radar and secret radio equipment—Lock-Ins are perfect for FM and Television.  
Be sure your next radio is truly up-to-date! Look for Lock-Ins!

"PERFECT FOR EVERY TYPE OF RADIO!"

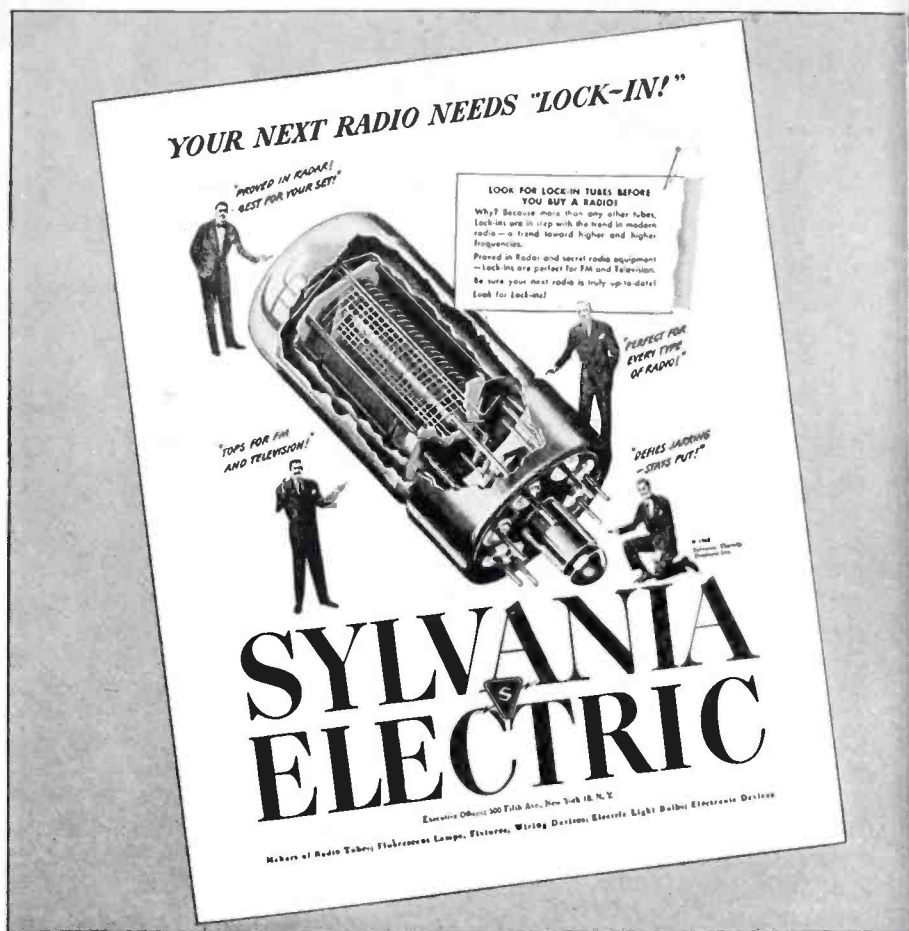
"TOPS FOR FM AND TELEVISION!"

"DEFIES JARRING—STAYS PUT!"

**SYLVANIA ELECTRIC**

Executive Office: 300 Fifth Ave., New York 10, N.Y.

Makers of Radio Tubes, Fluorescent Lamps, Fixtures, Wiring Devices, Electric Light Bulbs, Electronic Devices



Servicemen will find even more people asking about the war-famed Sylvania Lock-In Tube—because of big, full-page Lock-In advertisements appearing in eight national magazines. These ads are telling over ten million people that Lock-Ins have advantages possessed by no other radio tube.

Lock-Ins are noted for their electrical efficiency and rugged durability. Element leads are brought directly through a low-loss glass header to become sturdy

socket pins—effecting a much desired reduction in lead inductance and interelement capacitance. Support rods are stronger and thicker. There are few welded joints and no soldered joints.

These remarkable tubes are designed and built to handle the high and ultrahigh frequencies of FM and Television—as well as the lower frequencies. Today, set-manufacturers are looking for the Lock-In Tube as the perfect electronic unit for all new radios.

# SYLVANIA ELECTRIC

Emporium, Pa.

MAKERS OF RADIO TUBES; CATHODE RAY TUBES; ELECTRONIC DEVICES; FLUORESCENT LAMPS, FIXTURES, WIRING DEVICES; ELECTRIC LIGHT BULBS

Fig. 1 (right) A crystal unit in its holder, with the cover removed. The two springs serve to hold the electrodes against the crystal surface. (Courtesy Crystal Research Laboratories)

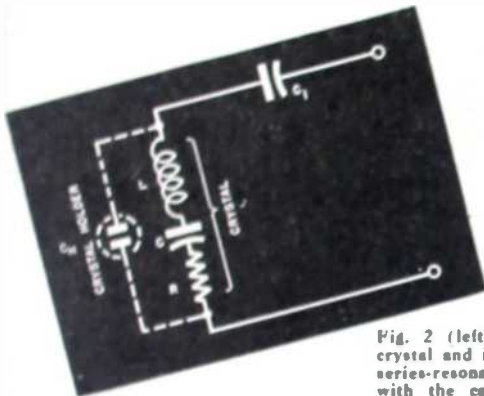


Fig. 2 (left). The electrical equivalent of the crystal and its holder. In effect, the crystal is a series-resonant circuit, consisting of  $L$ ,  $C$ , and  $R$ , with the capacitance of the holder across the entire system.  $C_1$  represents the series capacitance between the crystal proper, and the electrodes.

## CRYSTAL-CONTROLLED OSCILLATORS

by J. GEORGE STEWART

series capacitance between the crystal proper, and the electrodes.

IN many types of postwar receivers crystal-controlled oscillators will be quite an important feature. The extensive use of these oscillators in Army-Navy equipment has developed crystal manufacture to the point where they are economically feasible for mass production. At the winter IRE meeting last January, we were shown a receiver which tuned the entire b-c band through the use of push-button crystal oscillators.

Most of the new f-m receivers will use crystal-controlled oscillators. Stability requirements in the newly assigned v-h-f band will create a need for double superheterodyning, in which one of the fixed oscillators will probably be crystal controlled.

In the past most Service Men have had little opportunity to work with crystal controlled oscillators, since their use has been restricted to transmitters and fixed frequency receivers.

### Physical Properties of Crystals

Physically, the quartz crystal is less than an inch square and only several thousandths of an inch thick. This crystal is sandwiched between two small, flat squares of metal, called electrodes, which serve as surface con-

tacts. Spring pressure is usually applied to these metal squares to hold them firmly in place, and leads are brought out from these electrodes to external pins or contacts. The entire assembly is housed in a unit called the crystal holder. This has been the practice in the past. However, cost economy factors in receiver design may change the form of crystal holder, so that a simpler device embodying the same principles may be used.

### Electrical Crystal Properties

The crystal may be likened to a two-plate condenser, with the crystal acting as the dielectric, Fig. 1.

Electrically, the crystal is equivalent to a high  $Q$ , parallel resonant-tuned circuit, whose frequency is largely determined by the physical dimensions of the quartz crystal. Its electrical equivalent is shown in Fig. 2, where  $L$ ,  $C$  and  $R$  are the series electrical constants of the crystal unit, and  $C_H$  represents the capacitance between the metal electrodes, with the crystal acting as the dielectric.  $C_1$  represents the

### Crystal Operation

When an electrical current of approximately resonant frequency is applied across the crystal, sympathetic vibrations are set up in the crystal structure. This vibration, in turn, causes large voltages to appear between the electrodes. For this reason, the crystal may be used in place of an  $LC$  element in the grid circuit of an oscillator to supply the necessary grid driving voltage. Since the physical dimensions of the crystal are constant, and do not expand appreciably with heat, and since these same dimensions determine the frequency of operation, in the same way that the dimensions of a tuning fork determine its audible frequency, it can be seen that a high degree of frequency stability is thus obtained.

### Grid Circuit Activity

When installed in the grid circuit of an oscillator, the value of  $C_H$  is further increased by the input capacitance of the tube, and the capacitance of the associated wiring. The result-



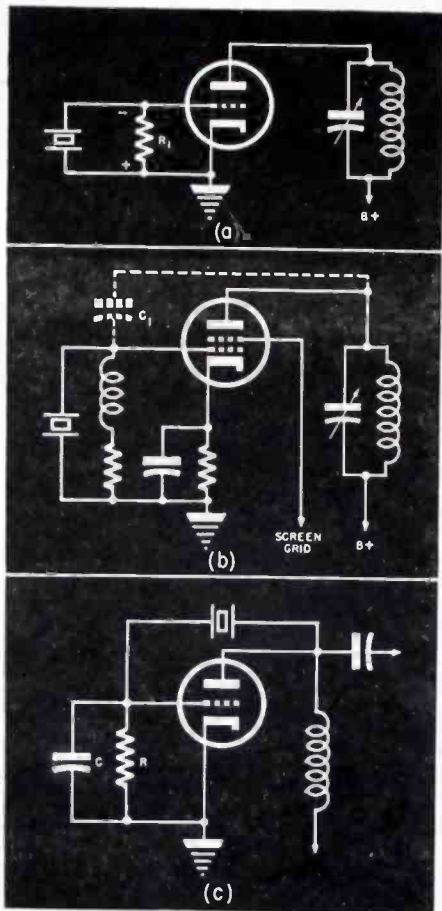


Fig. 3. Three circuits employing crystals for frequency control. In *a*, a triode circuit in its simplest form is shown. In *b*, we have a pentode circuit, while *c* shows the Pierce oscillator, which does not require a resonant circuit in the plate.

ages used, and they must be watched carefully to make sure that they are not excessive. Since power is not important in a receiver, high value grid resistors, and low grid and plate voltages may be used.

#### Pierce Oscillators

Fig. 3c shows a third method of crystal control for frequency stability the Pierce oscillator circuit. A triode is used, although a pentode may be used too. Here, the crystal is used as the coupling element between the plate and grid circuits. Note that the plate circuit is untuned. Its use in a crystal filter, in which only resonant voltages are passed by the crystal, the crystal performing as a series resonant circuit. For all other frequencies, the crystal acts as a pure capacitor.  $C_1$  and the crystal may be considered as a load across the output of the tube. Therefore increasing the value of  $C_1$  increases the load across the output circuit and the resultant grid current. Because of its position in the circuit the crystal is subject to high voltage strains. Therefore the plate voltage of Pierce oscillators is usually lower than for other crystal circuits.

must be kept below the crystal rating, else the crystal may be punctured and rendered inoperative. Expressed another way, the activity of the crystal is a function of the r-f voltage across it. If this voltage exceeds the limits of the crystal, the overactivity will shatter the crystal. Therefore, decreasing the value of the grid resistor reduces the current through the crystal. In Fig. 3a the cathode has been returned to ground, so that the grid bias is a function of the grid current which creates the bias across the grid resistor.

#### Pentode Circuit

In Fig. 3b a pentode has been substituted for the triode. Since the gain of a pentode is higher than that of a triode, less grid excitation is needed. The feedback from the plate to the grid has been reduced by the lower g-p capacitance inherent in the pentode structure. If this capacitance is too low, an external coupling capacitor represented by  $C_1$  is added, so that sufficient feedback is available. The size of the grid resistor for pentode crystal oscillators is usually 20,000 ohms or less. Since the lower value of resistor may shunt the crystal too effectively, and prevent oscillation, a r-f choke is usually added in series with the resistor. The choke supplies the necessary a-c impedance to reduce the shunting effect of the resistor, at the same time introducing a negligible amount of d-c resistance. Where cathode bias is used, the size of the grid resistor is reduced.

#### Harmonic Oscillators

Fundamental frequency operation of crystal oscillators is limited by crystal size to about 15 mc. Crystals for frequencies above 6 or 7 mc are very expensive. To overcome this condition, the crystal may be cut to operate on a mechanical harmonic of its fundamental frequency, or may be employed in a circuit where some harmonic of the fundamental frequency of the crystal is amplified. When the crystal is operated on a mechanical harmonic of its fundamental frequency, the resonant circuit in the plate of the oscillator is tuned to the desired harmonic. The crystal then behaves as though it were oscillating fundamentally at the harmonic frequency. When the crystal is used to drive the frequency multiplier,

tant influence on the crystal frequency is quite small, and insofar as related to receivers, may be considered negligible.

#### Crystal Outputs

Crystal units are capable of delivering large values of r-f voltage, depending on the tube used, and the circuit voltages. However, in receiver applications, the amount of power required is small, and the circuit components reflect this in their size.

Any of several standard circuits may be employed using a crystal as the frequency-controlling element. Three typical circuits are shown in Fig. 3a, b, and c.

#### Triode-Crystal Oscillators

In Fig. 3a is shown a triode-crystal oscillator in its simplest form. This circuit is essentially a tuned-plate tuned-grid oscillator, with the feedback supplied by the grid-plate capacitance of the tube. Since the crystal itself is a discontinuous d-c circuit, the grid of the tube is returned to ground through the resistor  $R_1$ . This resistor serves a second purpose, since it also limits the r-f current in the grid circuit. This grid current limitation is important, since the permissible current through the crystal

#### Crystal Excitation

The crystal excitation is a direct function of the plate and screen volt-

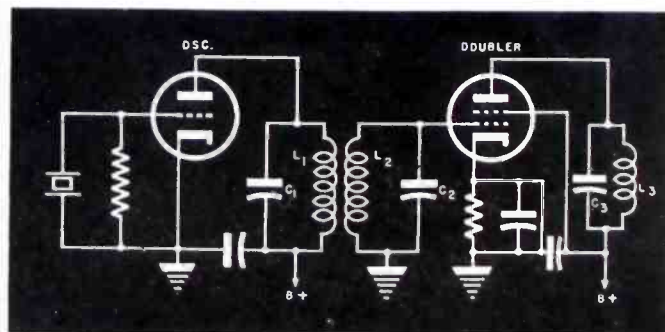


Fig. 4. A method for doubling the frequency of the crystal circuit. The first r-f transformer is tuned to the crystal frequency, while  $L_3C_3$  is tuned to twice the crystal frequency.

he crystal first oscillates at its fundamental frequency. This fundamental frequency is then used to drive the multiplier stage. Sometimes, where the desired frequency is quite high, both methods are used concurrently.

### Frequency Multiplier

Fig. 4 shows a typical crystal oscillator and frequency multiplier. In this circuit,  $L_1C_1$  and  $L_2C_2$  are tuned to the crystal frequency.  $L_2C_2$  is tuned to twice the crystal frequency. Thus, the output of the doubler stage is twice the fundamental or crystal frequency.

### Tri-tet Circuits

This same principle may be so used that only one tube is necessary for both operations. For example, the crystal oscillator may be one-half of a twin triode, and the doubler may be the other half. Or, a pentode may be used, as shown in Fig. 5. This circuit is known as the *tri-tet*. Here, the control grid, cathode, and screen grid perform as a triode-crystal oscillator. The screen grid serves as the plate of the triode. The plate of the tube is then used as the multiplier, with  $L_2C_2$  tuned to the desired harmonic. This circuit is usually used where even multiples of the fundamental frequency are desired. The circuit of Fig. 6 is used where odd multiples of the fundamental frequency are desired. This circuit is known as the *grid-plate oscillator*. The essential difference between the two circuits is that in Fig. 5 the crystal is returned to ground through the resonant circuit  $L_1C_1$ , whereas in Fig. 6 the crystal is returned to ground directly.

### Resonant Circuit and Cathode Return

Actually, the circuit of Fig. 6 is a Pierce oscillator, since the screen grid, which is being used as the plate of a triode oscillator, and the crystal return, are connected together through their common ground terminals. Since the cathode of a tube may be considered as a continuation of the plate circuit, the placing of the resonant circuit in the cathode return does not change the relationship, other than placing the actual plate of the tube at -f ground.

### Oscillator Tuning

All crystal oscillators are tuned in essentially the same way. Fig. 7 shows a typical plate-current characteristic

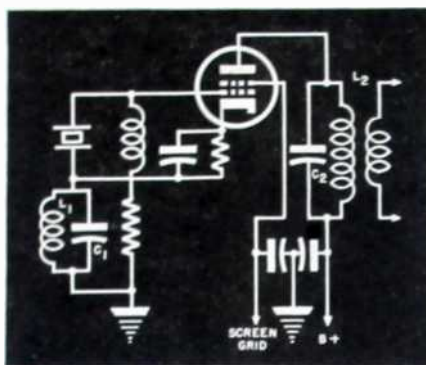


Fig. 5. A crystal frequency multiplier using one tube.  $L_1C_1$  is tuned to the crystal frequency, while  $L_2C_2$  is tuned to a multiple of this frequency. This circuit is used where even multiples of the crystal frequency are desired.

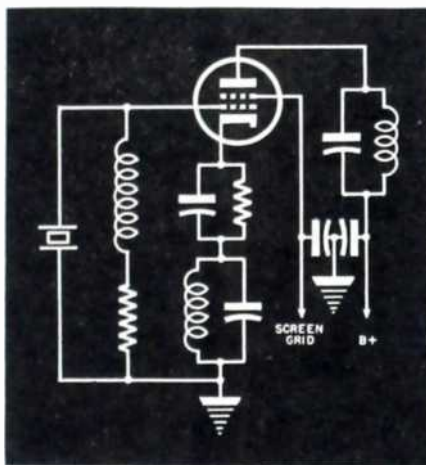


Fig. 6. This multiplier circuit is used where odd multiples of the crystal frequency are desired. The crystal portion of the circuit is essentially a Pierce oscillator, with the screen grid acting as the plate of a triode oscillator.

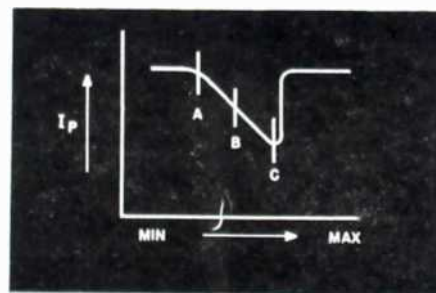


Fig. 7. Plate current characteristic of a crystal oscillator. For stability requirements, the circuit is tuned so that the current is in the vicinity of point B. This also prolongs the life of the crystal.

for a crystal oscillator. When the oscillator is in the non-oscillating stage, the plate current will be found to be at some high level. As the plate-tank tuning capacitor is tuned from minimum capacitance, the plate current will dip as shown in Fig. 7; the

current decreases slowly until it reaches some minimum value, and then rises sharply. The maximum oscillation will take place at the point of minimum plate current. However, for stability purposes, it is best to operate the crystal oscillator at some point about halfway between maximum and minimum plate current. This point of operation also limits the amount of r-f current in the crystal, and will help prolong its useful life.

### Causes of Non-Oscillation

If the crystal oscillator stops oscillating, the cause may be traced to physical and electrical problems.

For instance, dirt on the crystal faces will interfere with oscillation. To clean crystals, carbon tetrachloride should be used. The faces of the crystal should be immersed in the liquid and then carefully dried on some lint-free cloth. The faces of the crystal should never be touched with the fingers, since a light film of grease is thus deposited on the crystal impairing its performance. The crystal should always be picked up by its edges, and care should be exercised not to chip the edges. The electrodes should receive similar care, since dirt or grease on their faces will produce the same effects as they would on the crystal.

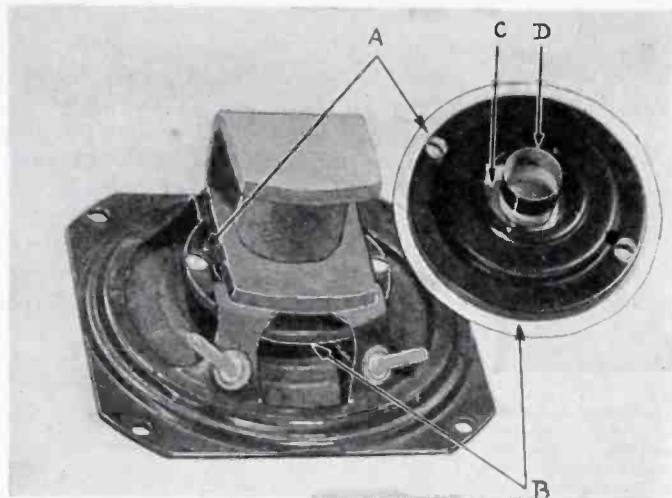
### Tight Coupling

If the crystal oscillator is coupled too tightly to the load, oscillations will cease. This condition will be rare in receivers, but is mentioned here in case some variable coupling method is used.

### Other Sources of Trouble

Detuning of the plate tank circuit is another source of trouble. The cure is obvious. All bypasses and coupling capacitors should be checked if some unusual condition appears. For example, an open g-p coupling capacitor, or if a variable coupling capacitor is used, a low value of coupling capacitance will prevent oscillations from starting. An open screen-grid bypass, or a reduction in its value, may cause excessive excitation of the crystal. Another cause of excessive excitation is high bias. This should be checked with a v-t voltmeter in the grid circuit. For other troubles, the crystal-controlled oscillator may be treated in the same manner as any oscillator.





Construction of the Adjust-A-Cone assembly; the spider is kept in position with a pressure or clamping ring, which in turn is held down by two machine screws. In insert view, we have a closeup of pressure ring, which is underneath at B. At C is the spider; D shows the voice coil.

# SERVICING HELPS

## RECENTERING LOUDSPEAKER CONES WITH QUAM-NICHOLS ADJUST-A-CONE

**T**HE loudspeaker is a device for the conversion of electrical energy into sound. It is composed of electrical and mechanical parts which acting in conjunction with each other make the conversion possible. Thus the electrical components control the mechanical ones, and the electrical impulses to which the loudspeaker is subjected are converted into mechanical action which creates the sound waves.

### Analysis of Two Types

In this discussion we will consider only two types of loudspeakers (though there are at least three others). The most commonly used, namely, the electrodynamic and the permanent magnet type will be discussed. Both of these function exactly alike, the sole difference lying in the method employed to obtain the magnetic flux in the field in which the voice coil moves. In the former, it is created by an electromagnet and in the latter by a permanent magnet.

The electrical parts of the loudspeaker are the magnet, pot assembly, and the voice coil; while the mechanical parts are the housing and the cone or diaphragm. The voice coil assembly, known as the driver mechanism, is rigidly attached to the cone so that whatever movement is electrically caused in the driver is transmitted directly to the cone. The movement of the cone against the air in contact with it causes the radiation of air waves, or sound.<sup>1</sup>

In order for the voice coil to func-

### by FRANK C. KEENE

tion, it must be concentrically located around the end of the magnetic pole-piece of the loudspeaker with a clearance between it and the pole-piece. The clearance between the pole-piece and the pot is very close so that the air gap energy is held at a maximum. It is the action of the audio currents through the voice coil while it is in the direct-current magnetic field that causes the voice coil to move in and out.<sup>2</sup> This movement, when transmitted to the cone to which the voice coil has been rigidly attached, causes the propagation of sound waves and hence sound.<sup>3</sup>

### Clearances

Clearances must be close for optimum results, but it is imperative that the voice coil ride free within the space between the pole-piece and the pot which is termed the gap. If, for instance, grit or dust gets into the gap, the efficiency and work of the voice coil is thereby impeded. Similarly, the voice coil cannot rub either against the pole-piece or against the pot and give good reproduction.

To center the voice coil within the gap, a membrane, called a spider is built

<sup>1</sup>Terman, *Radio Engineering*, page 767.

<sup>2</sup>Terman, *Radio Engineering*, page 765.

<sup>3</sup>Olson-Massa, *Allied Acoustics*; Massa, *Electronics*, Feb. 1936; Seabert, *Electrodynamic Speaker Design Considerations*, Proc. IRE, June 1934.

into the loudspeaker assembly. This supports the voice coil at the pole-piece, while the housing (or basket, as it is termed) supports the outer edge of the cone. The spider normally permits movement of the voice coil parallel with the side of the pole-piece, but restricts all side-way movements. If the spider itself gets off center, then the voice coil is no longer concentrically located over the end of the pole-piece and a rubbing voice coil results. The same would occur if the voice coil itself were bent at its junction with the spider.

### Rubbing Voice Coils

A rubbing voice coil not only causes losses in power because of the friction developed between the voice coil and the pole-piece or the pot, as the case may be, but it also introduces distortion.<sup>4</sup> Such off-center operation is apparent in the reproduction in the sound by rasps and rattles and by highly distorted frequency responses. This widely divergent output response from that of a normal speaker cannot be reconciled by the human ear which, while not intolerant of small aberrations and distortions,<sup>5</sup> does and can register those of this magnitude.

The result is that the user of a loudspeaker with an off-center or rubbing voice coil usually calls in the Service-Man to restore the quality which has

(Continued on page 51)

<sup>4</sup>Knowles, *Electronics*, Sept. 1933; Terman, *Radio Engineering*, page 774.

<sup>5</sup>Terman, *Radio Engineering*, page 763.

Many headlines like this  
have raised the question

RADIO RACKETEERS  
ASSAILED BY COURT

Declaring that radio repairmen were fleecing customers by charging all the traffic

Should Radio Service Dealers be Licensed?

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RADIO RECEIVING TUBE DIVISION

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# RAYTHEON

*Radio Tubes*

DEVOTED TO RESEARCH AND THE MANUFACTURE OF TUBES FOR THE NEW ERA OF ELECTRONICS



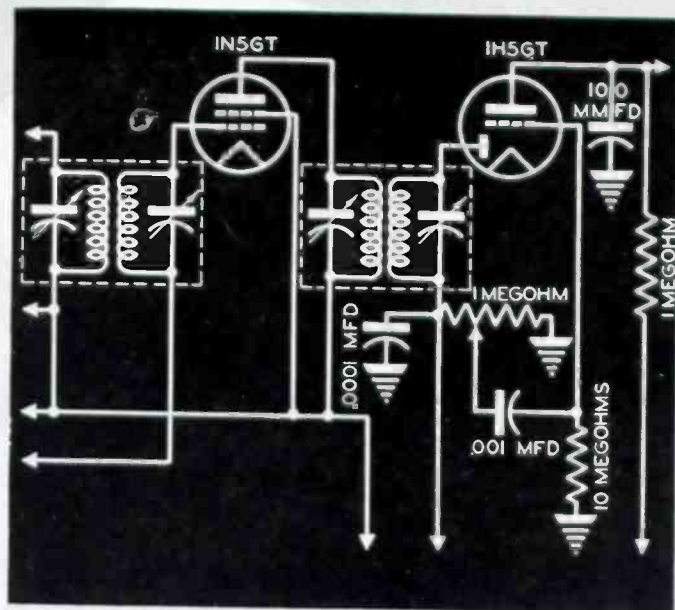


Fig. 1. The i-f system of the Westinghouse WR-678. The sensitivity of portable-receivers is about 30  $\mu$ P for an output of 50 mw. Most of this gain is supplied by the high gain i-f stage.

by L. E. EDWARDS

# I - F A M P L I F I E R S

**D**URING the past few months we have been discussing some of the important circuit systems that constitute the modern receiver. Thus far we have covered inputs. (Martin W. Elliott's analysis of mixers appeared last month and continues in this issue on page 32.) In the i-f amplifier we have another vital element of receivers. For this section provides both sensitivity and selectivity.

High-gain remote cut-off pentodes are the most suitable amplifier tubes, allowing a wide range of avc control without detuning, and have thus been used in most i-f amplifiers.

## I-F Transformers

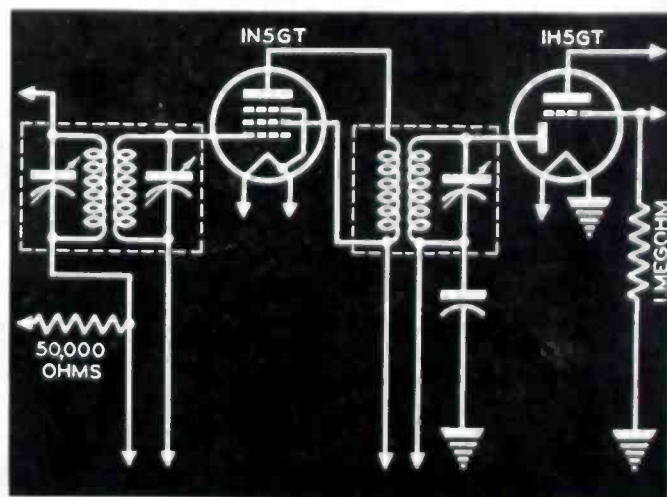
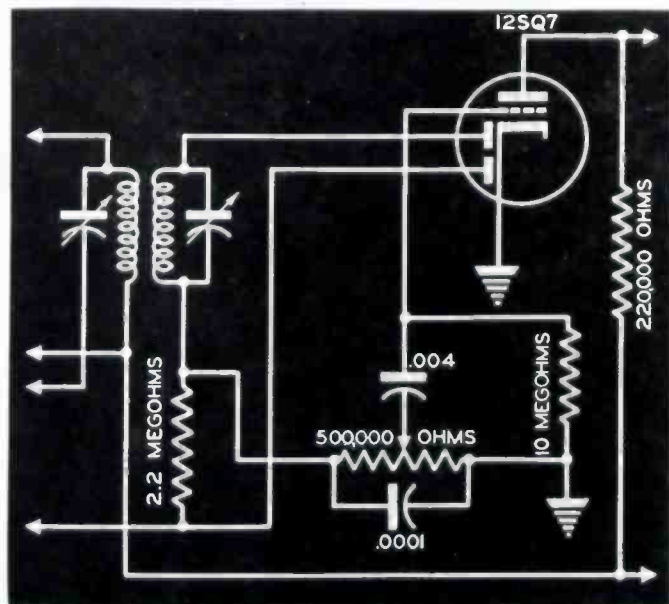
I-f transformers may be divided into

two classes based upon their inductance; high-inductance coils of 2.0 to 2.5 mh and low-inductance coils of 1.0 mh or less. The former are tuned to 455 kc by low-capacity trimmers of 50 to 100 mmfd, giving a high  $L/C$  ratio and a high anti-resonant impedance which presents a good match to the pentode plate resistance. However, this arrangement is extremely critical to adjust to resonance and still harder to keep there because the trimmer is subject to change with temperature and age. Mechanical fatigue and warping are also annoying. Therefore, the attainable gain is not usually obtained for very long. On the other hand, low  $L$  transformers can use larger tuning capacitors, 150 mmfd and up, which are less subject to mistuning or detun-

ing because they are not so critical. Small changes in capacity cause less change in resonant frequency.

Personal receivers using only 45 or 67 volts  $B$  must use very high quality, high  $Q$  transformers of the order of 80 to 100, to obtain sufficient overall gain. Some of these types are potted, forming a closed magnetic circuit like two  $E$  laminations, or shell type which greatly reduces absorption in the shield, or even eliminates the shield in some instances.

I-f coils of the low-priced a-c/d-c receivers are wound with No. 37 or 38 solid copper, while the higher-priced receiver i-f's use 3 to 5 strand Litz for the input and either solid or Litz for the output, or second detector transformer. The i-f's of the very high



Figs. 2 (left) and 3 (above). Fig. 2 shows the i-f section of the Spiegel 1-40. No i-f tube is used, the gain of the single i-f transformer being enhanced by a small amount of regeneration. Fig. 3. I-f section of the Allied D-366. Primary of the second i-f transformer is untuned. The elimination of this tuned stage reduces both the gain and the selectivity of the receiver.

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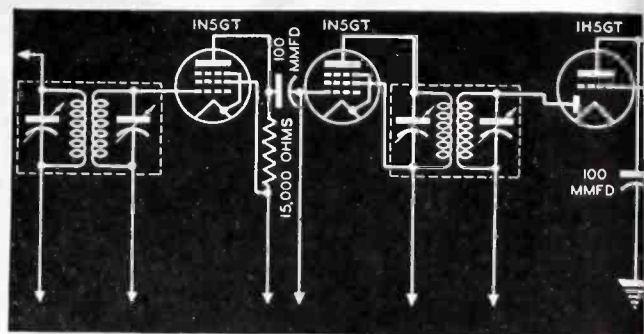
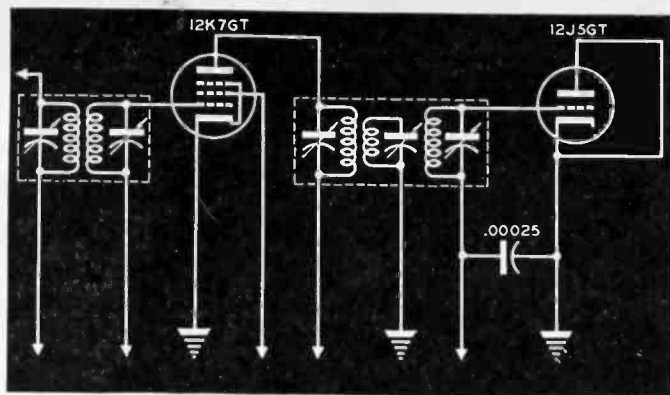
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quality receivers have been wound with 7 to 10 strand Litz on larger coils, and often are triple-tuned or iron-cored, and encased in cans. For improved stability, the tuning capacity is often divided between a fixed silver mica capacitor and a small trimmer, any variation in the latter representing only a small part of the total.

#### Westinghouse WR-679

In Fig. 1 we have a conventional i-f amplifier of a portable, Westinghouse WR-679, using a 1N5GT with standard dual air-core transformers. Portables of this type have a sensitivity of about 30 microvolts from converter grid to speaker for an output of 50 milliwatts, the principal part of the gain coming from the i-f. For comparison, a typical a-c/d-c job has a sensitivity of about 180 microvolts.

The detector transformer is loaded by a 1H5 diode and its load resistance, a 1-megohm volume control. It is important that the second detector be well grounded to the chassis to prevent coupling to the loop antenna. Sometimes eddy currents are formed in the chassis which act as coupling loops. This condition is worse where the loops are poorly designed, since this prompts broad tuning because the i-f frequency

Figs. 4, (above left) and 5 (above right). In Fig. 4 appears the i-f system of the Air-King 4034. Triple tuning in the second i-f transformer provides good gain. At the same time the band-pass characteristic is improved, resulting in high fidelity reception. Fig. 5. Resistance coupling in an i-f stage in the Ward O4WG-2672. This is an inexpensive way of increasing the gain of a receiver with very few parts. The increase in gain is of the order of 12-20.

of 455 kc is quite close to the 540-kc setting at the low end of the band.

#### Spiegel 1-40

The i-f section of a midget 3-tube and rectifier superhet without an i-f amplifier tube is shown in Fig. 2. In this receiver, Spiegel 1-40, a 12SA7 modulator feeds a 12SQ7 second detector through the single i-f transformer. Sensitivity and selectivity are both enhanced by regeneration by returning the primary tuning capacitor to an RC-feedback element in the cathode circuit. One diode is used as detector, the other as a gate on the avc system.

#### Allied D-367

In Fig. 3, we have another portable receiver, Allied D-367, which contains a conventional i-f input transformer but uses a single-tuned detector transformer. This transformer is a cartwheel type, wound on a single ceramic

base, with the windings very closely coupled. This type of unit hasn't much selectivity.

#### Air-King 4034

In Fig. 4 appears the i-f system of the Air-King model 4034. In this system we have a triple-tuned second detector transformer which provides good gain and, at the same time, band-pass characteristics for passing a wide band for high fidelity. This may be accomplished by staggering the tuning of the three circuits so they resonate at three equally separated frequencies. The added tank circuit is grounded to prevent electrostatic coupling. The detector is a 12J5 used as a diode with 1/2-megohm load resistance. The input i-f transformer is standard.

#### Ward O4WG-2672

A Ward portable, model O4WG-2672, with a resistance-coupled second i-f stage, is shown in Fig. 5. This method is ideal for portables, since it provides an additional gain of 12-20 with but one extra tube, two resistors and a coupling capacitor. Its use is generally limited to applications in which selectivity is not a problem. There is a further disadvantage in the reduction of the signal/noise ratio. With the additional i-f gain in this type of receiver, the circuits are pretty hot compared to the standard single i-f circuits; hence, such items of stability as bypass capacitors must be watched carefully. Replacement units must be of good quality and adequate capacity.

The first i-f plate load consists of 15,000 ohms. Some designers have used up to 75,000 ohms. The coupling capacitor is 100 mmfd.

#### G. E. L-643, 653, 663, 673

In Fig. 6 (G. E. L-643, 653, 663, 673), we have an iron-core i-f input system, with a large air-core unit for the second detector, the pair providing exceptionally good i-f gain without the use of high-inductance coils. In some receivers the cores are sometimes made

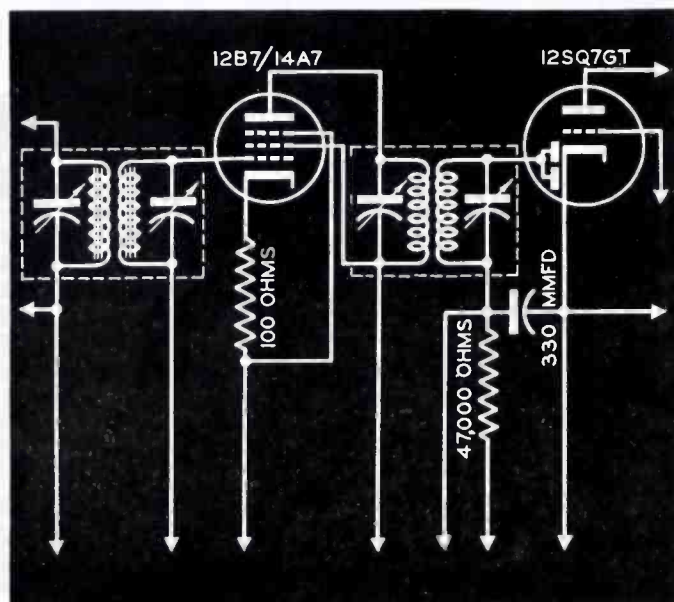
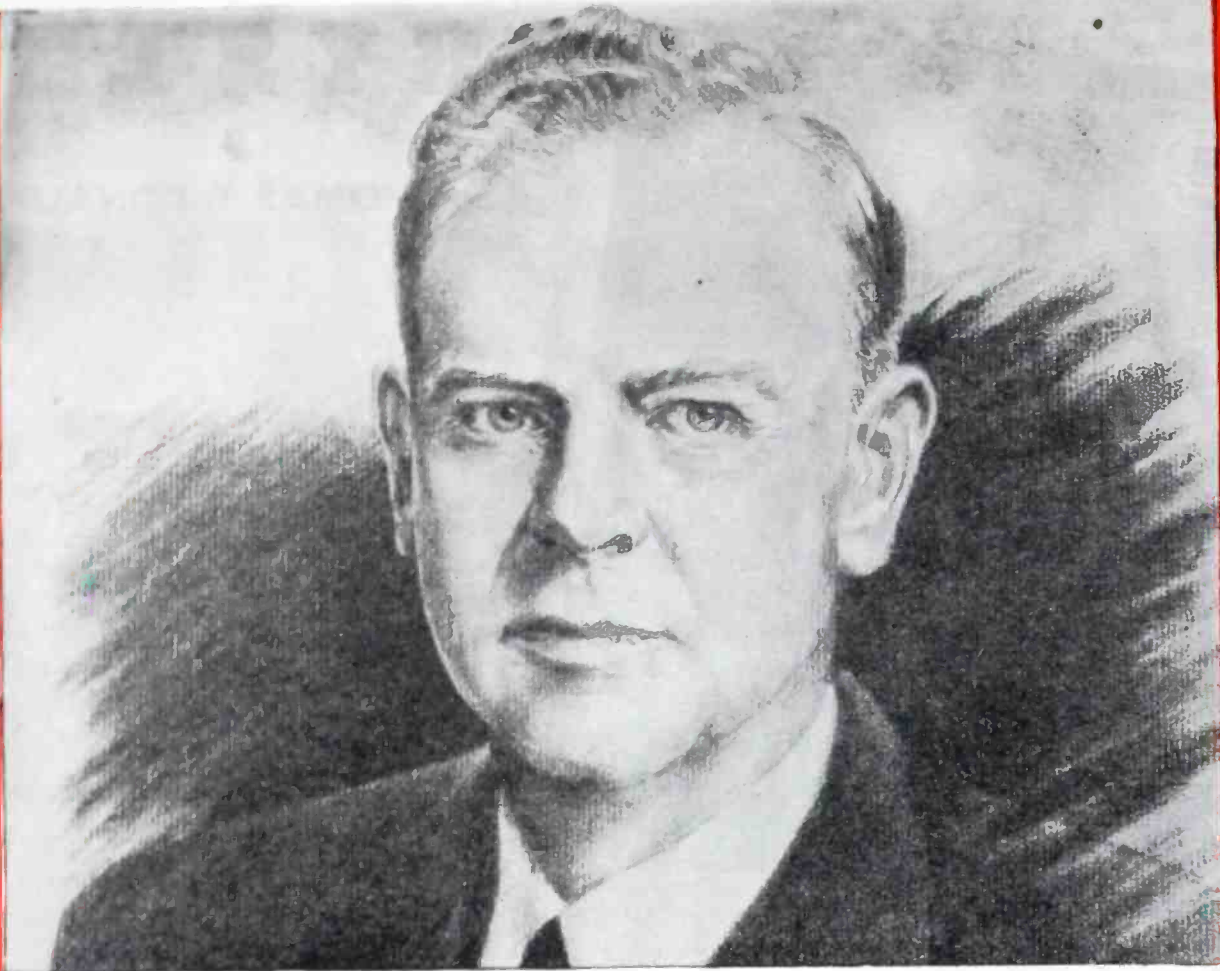


Fig. 6. The G.E. L-243 i-f system. Iron core coils are used to improve the Q of the i-f system. In some receivers, the cores are made adjustable, permitting the use of stable, fixed capacitors.



Portrait of Randolph C. Walker by John Carlton

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# CRYSTAL

by THOMAS T. DONALD

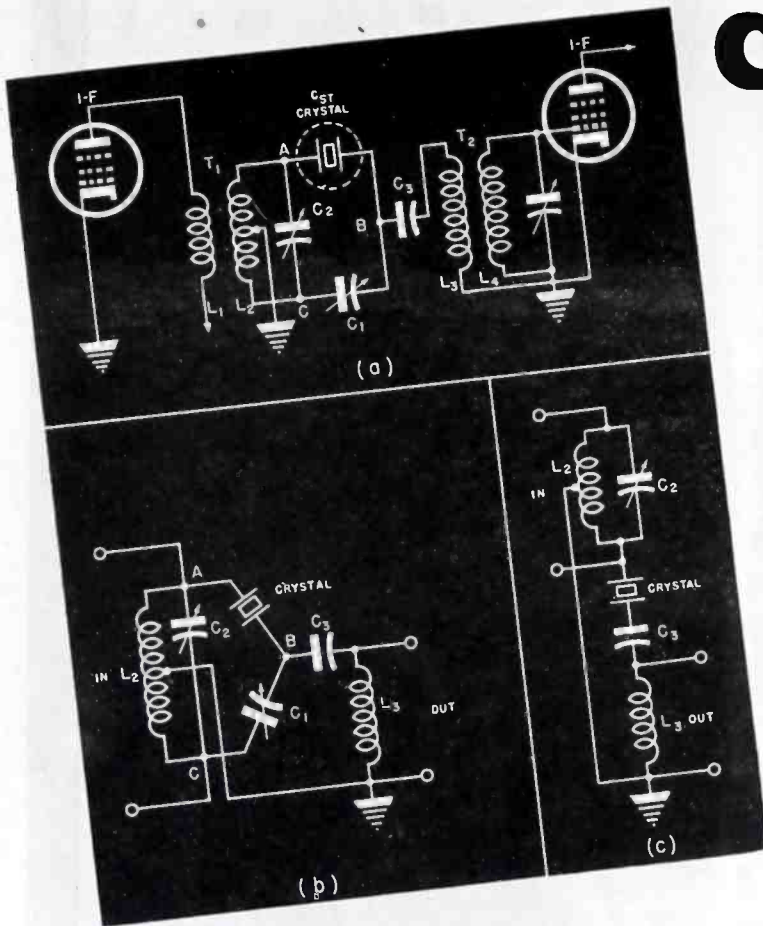


Fig. 1. A typical crystal filter i-f network. In *a*, the crystal filter circuit is shown; *b* shows its close relationship to a balanced-bridge type network; *c* shows how the series resonant characteristic of the crystal is used to provide extreme selectivity.

**M**ANY types of communications receivers feature single-signal circuit design for c-w or code reception.

In c-w (continuous waves) we have the transmission of an r-f carrier only, with no audio modulation. The carrier is then broken up into short and long dashes, or coded. Since there is no audio modulation, the only means of detecting the signal, is through the use of a beat-frequency oscillator or b-f-o which was analyzed in last month's article. However, in the bands used for this type of communication, two adjacent signals may be no more than a few cycles apart, since the volume of air traffic is quite heavy. Therefore, the selectivity of a broadcast type receiver, and its band acceptance of ten kc required to accommodate the side band transmissions necessary for true fidelity of music and voice, would be unaccept-

able for c-w work. It therefore becomes necessary to improve the selectivity of the receiver to a point where the band acceptance is 100 cycles or less. The best method for accomplishing this is through the use of a crystal filter. In addition, a narrow band acceptance helps to reduce static as well as other types of interference. Many Service Men may have noted that when European pickups are retransmitted in this country c-w signals are heard in the background. With a sharp crystal filter, it is possible to receive the code signal, and almost completely obliterate the broadcast signal.

### Crystal Filter Positions

Crystal filters are usually installed between the first detector of a superheterodyne receiver, and the following i-f stage, or between i-f stages. A typical crystal filter i-f network is shown in Fig. 1a. It is redrawn in

Fig. 1b to show its close relationship to a bridge type, or balanced network. In this figure  $C_1$  is the phasing control. If the crystal could be installed in the circuit without the accompanying capacitance introduced by the crystal holder and associated wiring,  $C_1$  as well as the balanced type circuit, would be unnecessary. However, due to the introduction of this stray capacitance, represented by  $C_{ST}$  in Fig. 1a, it is necessary to balance out its effect. This is accomplished with  $C_1$ , the phasing control. If this were not done, the circuit enclosed by the dotted line in Fig. 1a, would act as a coupling capacitor, with the crystal assuming the role of a dielectric, serving to link  $T_1$  and  $T_2$ , and permitting the passage of all r-f signals present in  $T_1$ . However, when  $C_1$  is adjusted so that it is equal in value to  $C_{ST}$ , any non-crystal-resonant voltage developed between points *A* and *B*, is cancelled out by a like voltage between points *C* and *B*. A study of Fig. 2b shows how the balanced-type circuit accomplishes this. For crystal resonant voltages, the crystal acts as a series resonant circuit, thereby providing a coupling path between  $T_1$  and  $T_2$ .

### Phasing Controls

The phasing control,  $C_1$ , also performs another function. Since it is a

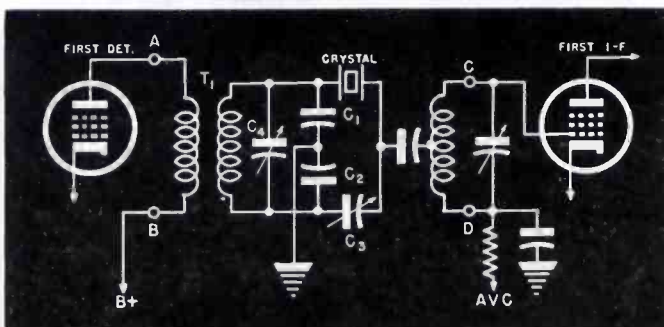


Fig. 2. The crystal filter network of the National NC 100 XAB.  $C_1$  and  $C_2$  split the secondary of the first i-f transformer capacitively.  $C_3$  is the phasing control. This is a plug-in type stage, *A*, *B*, *C*, and *D* representing the four prongs of the plug.

# FILTERS USED IN COMMUNICATIONS RECEIVERS

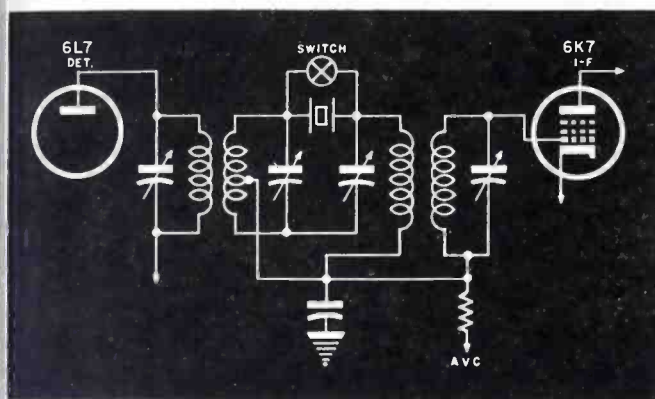


Fig. 3 (above). Crystal filter of the Hallicrafters SX 18. Here, the transformer is split inductively. A panel switch is provided to cut out the crystal for voice reception.

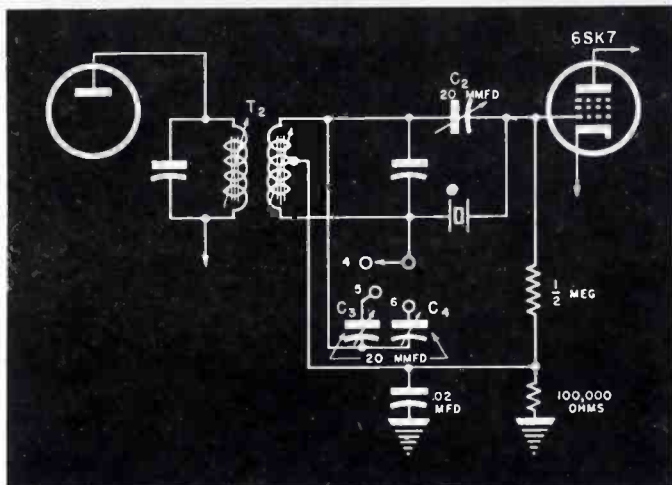


Fig. 4. The variable-selectivity system used in the Hallicrafters SX 28. Capacitors  $C_3$  and  $C_4$  detune the secondary of  $T_2$ , thereby increasing the effectiveness of the crystal and improving the selectivity of the system.

ancelling agent, any partial cancellation of the distributed capacity in the crystal circuit would tend to decrease its selectivity. Therefore, the phasing control may also be used to control the selectivity of the crystal filter.

### Selectivity Control

The adjustment of  $C_2$ , which tunes  $T_2$ , may also be used as a selectivity control. When  $C_2L_2$  is tuned to the resonant frequency of the crystal, it places a high resistance in series with the crystal, since, at resonance, a parallel tuned circuit offers the greatest impedance, or resistance. (The circuit is shown in Fig. 1c.) Therefore the effectiveness of the crystal  $Q$  is reduced, since it only represents a small portion of the entire resistive network represented by  $L_2C_2$ , the crystal,  $C_3$ , and  $L_3$ . However, if  $L_2C_2$  is detuned, the resistance of this portion of the network is reduced to the reactance of either  $L_2$  or  $C_2$ , whichever is smaller, and the effectiveness of the crystal is increased. Thus, the selectivity of the circuit is increased.

### Basic Designs

The three points previously discussed are important since they are not only the basis of most of the crystal-filter network communications

receiver designs, but a major factor in servicing and alignment.

### National NC 100 XAB

Figs. 2 to 6 show the crystal-filter networks used in typical communications receivers.

Fig. 2 is the crystal-filter circuit of the National NC 100 XAB.  $C_1$  and  $C_2$  are used to split the secondary of  $T_1$  to obtain a balanced circuit.  $C_3$  and  $C_4$  are the phasing and selectivity controls, respectively. This particular model is so arranged that a standard i-f transformer of the plug-in type may be used instead of the crystal-filter unit, which is also a plug-in type. The plug-in points are represented by  $A$ ,  $B$ ,  $C$ , and  $D$ . The selectivity of the crystal unit is preset, before insertion.

### Hallicrafters SX 18

Fig. 3 shows the crystal system used in the Hallicrafters SX 18. Here, the primary of the first i-f transformer is tuned, and its secondary split inductively. A panel switch is provided to cut out the crystal when the set is used for b-c reception. Note the similarity of this circuit to Fig. 1a.

### Variable Selectivity Filters

The circuits shown previously have been simple versions of crystal filters. More expensive types of communications receivers feature a variable selec-

tivity i-f system, with and without crystal filters.

All variable selectivity crystal-filter systems revolve around some method of decreasing the  $Q$ , or band acceptance, of the crystal. This is necessary, since it permits easier tuning of c-w signals when noise conditions are not restrictive. It can be appreciated that when dialing for a signal with an i-f channel that is only 100-cycles wide, the slightest movement of the dial would pass over the signal. Figures 4 to 6 show three such systems.

### Hallicrafters SX 28

Fig. 4 shows the variable selectivity system used in the Hallicrafters SX 28. Three positions, 4, 5 and 6, are provided for crystal *broad*, *medium*, and *sharp*. In position 4,  $T_2$  is tuned accurately to the crystal frequency. This causes broad-band acceptance, as explained in Figure 1c. Position 5 adds trimmer  $C_3$ , which detunes  $T_2$  slightly, thereby increasing the effectiveness of the crystal filter. Position 6 further

(Continued on page 50)



# ELECTRONIC ALARM SYSTEMS

## SYSTEMS

by WILLARD MOODY

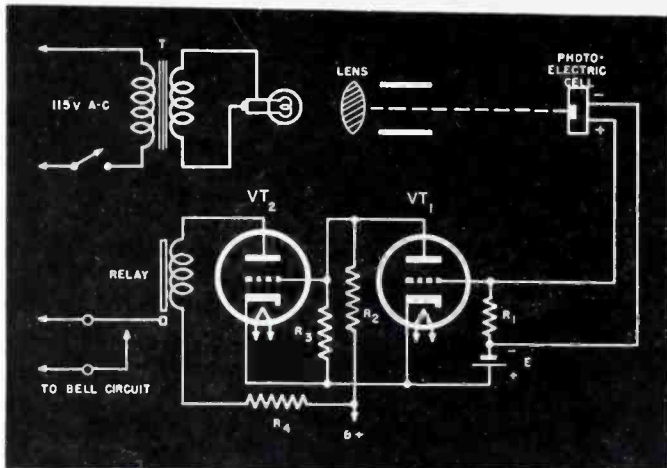


Fig. 1. An elementary photoelectric alarm system. Interruption of the light source reduces the voltage across  $R_1$ , which is bucking the bias voltage. This reduces the plate current, and thereby actuates the bell system.

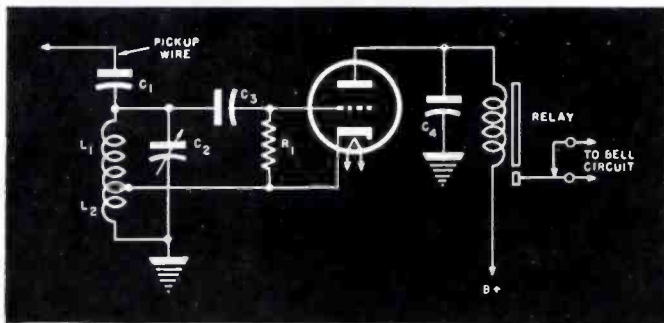


Fig. 2. A circuit typical of r-f types of alarm systems. Variation in the capacity across the grid circuit of the oscillator causes a decrease in plate current, which in turn closes or opens a relay.

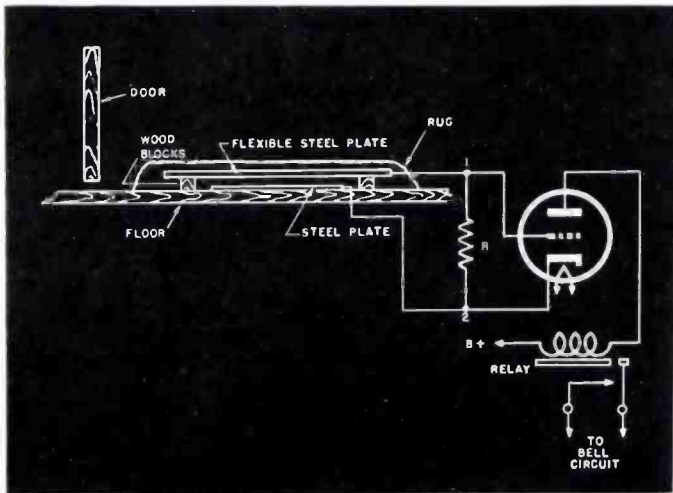


Fig. 3. A step-operated type of alarm system. Resistor  $R$  is usually of the order of 10 to 15 megohms. Shorting of the flexible steel plates by stepping on them shorts out the grid resistor, causes the plate current to rise, and actuates the relay.

**E**LECTRONIC circuit developments have introduced many unusual tube applications, such as the electronic alarm. During the war electronic alarms were used in a variety of installations. The postwar era will see an extensive use of these alarms in industry and the home.

### Types of Alarm Systems

There are several types of electronic alarm systems. In Fig. 1 we have one where light from an auto type bulb is directed through a lens and barrel-like tube to a photoelectric cell which may be four or five feet away. In some cases a filter is used in front of the barrel for passing invisible infrared rays only. In other cases, ordinary white light is used. In operation, the light strikes the photocell which develops a potential across the cell terminals. This voltage is applied to the grid of the first tube and is bucked out by a bias voltage. When light no longer strikes the cell, the voltage is zero and the grid bias potential causes a decrease in the plate current, since the bias is more negative.

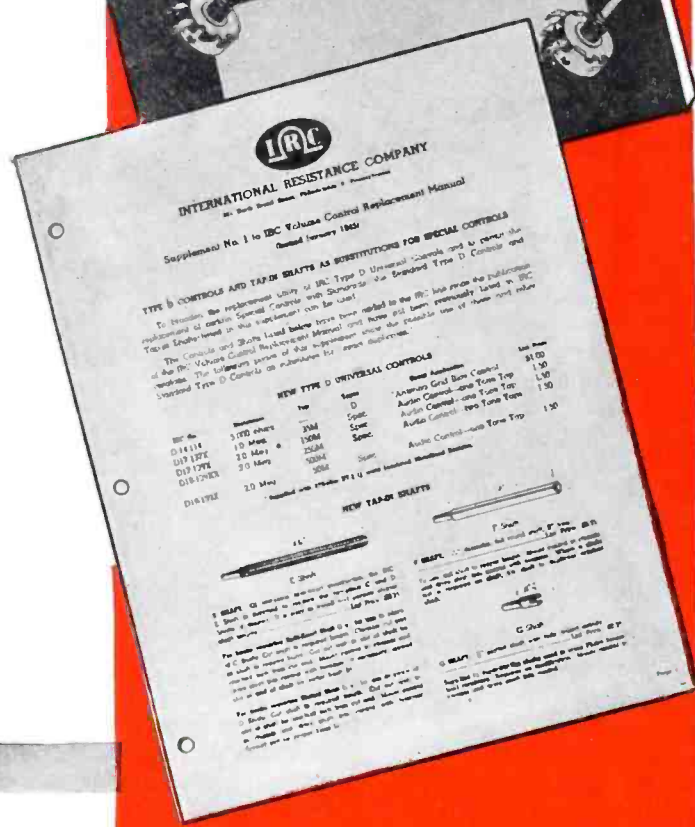
### Relay Activity

The interruption of the light beam thus actuates the alarm system. That is, the drop in plate current, with an increased negative grid potential, causes less current flow in  $R_2$  and a decreased voltage drop across  $R_2$ . Then, the increased positive potential on the grid of the second tube causes a rise in plate current and the relay closes. A latching or lock-in arrangement may be used on the relay, so that

(Continued on page 38)

# IT'S A HUNDRED TO ONE YOU'LL FIND THE RIGHT CONTROL

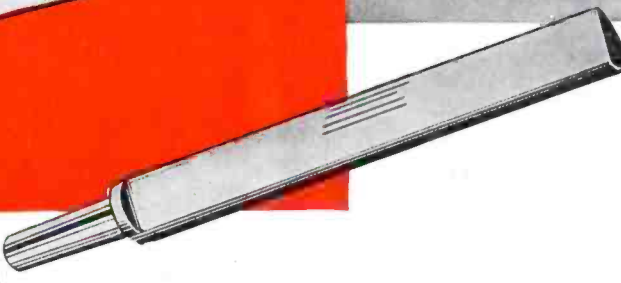
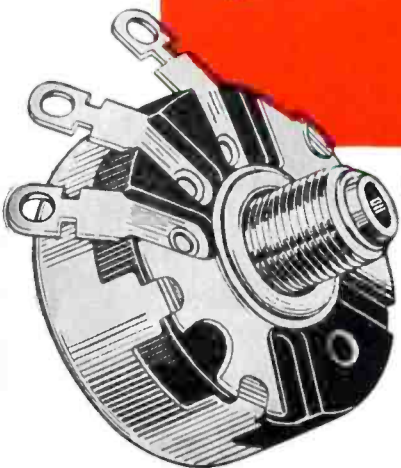
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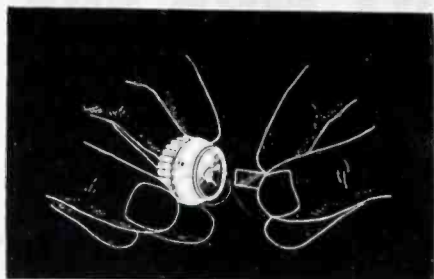
If you do not have an IRC Volume Control Replacement Manual or a copy of Supplement No. 1 you can readily obtain one from your IRC Distributor—or by writing direct to Dept.



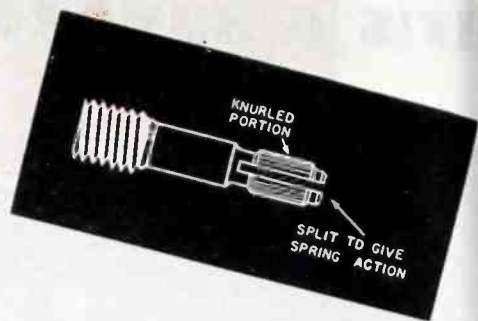
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Figs. 1 (left) and 2 (right). Fig. 1. How the metal spacer is inserted in the knob against the flat spring in push-on type knobs requiring only a 1/32" flat. (Courtesy P. R. Mallory & Co., Inc.) Fig. 2. Split-knurled type shaft that makes a set screw or spring in the control knob unnecessary.



# VOLUME AND TONE CONTROL RESISTORS

VOLUME and tone controls have, in part, reached standardization of certain mechanical dimensions. In general, the tendency has been toward a reduction in overall size, particularly for automobile and midget receiver applications. Perhaps the greatest variance in the controls used as original equipment concerns the length of shaft and the method of fastening the control knob to the shaft.

## Control Shafts and Knobs

The knobs used on most of the home and portable receivers have been of two general designs, the *set-screw* type and the *push-on* type knob. The shaft diameter has (practically from the start) been 1/4" in diameter and the bushing 3/8" in diameter, so from the replacement-control angle, the main problem involves the providing of a universal means which will allow the use of either the screw type or the push-on type of knob.

Provision of a *flat* on the shaft accommodates the screw type; it provides a secure mounting. The *push-on* type also utilizes a flat on the shaft, but in the design of such knobs two sizes have been developed, one which uses a shaft milled down 3/32" and one which uses a 1/32" milling. The former was extensively used in earlier receivers. The problem of making a universal line of home receiver controls has been met by one manufacturer by milling all shafts to 3/32". This covers the majority of *push-on* type knobs and also accommodates the *screw* type. Then, for those cases which require a 1/32" milling, a small 1/16" metal insert or spacer is used on the deeper milling to bring it up to 1/32". This spacer is inserted in the

## Part Nine of a Series on Receiver Components

by ALFRED A. GHIRARDI

Advisory Editor

knob, resting it on the flat spring member (as illustrated in Fig. 1) before assembling the knob to the shaft. When this assembly is pushed on the shaft, it provides a secure and simple method of application. The milled side of the shaft is turned to the downward position allowing the insert to remain in the proper location in the knob during assembly.

Split-knurled shafts and correspondingly knurled knobs also have become popular, especially in auto-radio receivers, because the split gives a spring action and no additional set-screw or spring insert is needed in the knob. Furthermore, the knob can be pushed on the shaft in any relation to the sliding contact arm of the control. A split-knurled shaft is illustrated in Fig. 2. The knobs for split-knurled shafts will not fit the conventional flattened shaft.

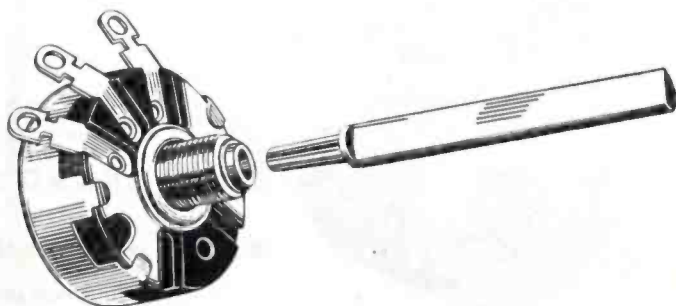
## Plug-in Shafts

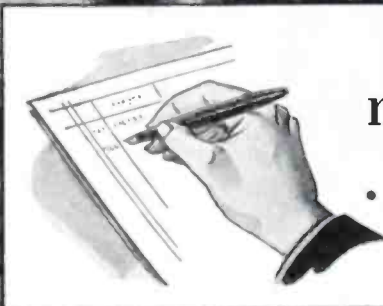
The *plug-in* type shaft is a recent

innovation in universal shaft design. Such shafts are made in plug-in form to fit a special line of controls made by the particular manufacturer. The shaft is easily attached or detached to a special fitting in the bushing, and is held rigid. A recent shaft design employing a tapered plug-in portion is illustrated in Fig. 3; a complete line of plug-in shafts is illustrated in Fig. 4. With this entire set, the Service Man is sure of always having the right replacement control shaft at hand for nearly every job. For household receivers a kit comprising eight shafts (SS1, 2, 5, 16, 18, 22, 25 and 26) answers most needs. For automobile radios, a kit comprising twenty-two shafts (SS1, 2, 3, 4, 6, 10, 11, 12, 14, 15, 17, 19, 20, 21, 23, 24, 27, 28, 29, 30, 31 and 32) will meet all requirements.

Plug-in type shafts are becoming increasingly popular for the following reasons: (1)—They result in a tremendous increase in the flexibility of control applications, for only a few types of controls are required to service the large majority of receivers. Hence they reduce the stocking and inventory problem. (2)—They either replace the original shaft exactly, or they can be made into exact replicas by simply cutting to the required length.

Fig. 3. A recent design of tap-in (plug-in) shaft. (Courtesy IRC)





more efficient  
... in miniature

The old quill was picturesque but it lacked the compactness, convenience and dependability of our modern fountain pen. Its development was the usual evolution. Changes and reduction in size made for greater efficiency. The same took place in the development of the modern miniature electronic tube.

While the reduced size of TUNG-SOL Miniatures alone warrants a preference for them, their greater efficiency has resulted in their general adoption, especially for high frequency circuits. Smaller elements make them more rigid. Shorter leads result in lower lead inductance. TUNG-SOL Miniatures have low ca-

capacity and high mutual conductance.

The many advantages of TUNG-SOL Miniatures will cause them to be used in much of the new equipment. It is important that TUNG-SOL Jobbers and Dealers are in position to supply miniatures as well as G-G's-metal and large glass tubes.



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SERVICE, NOVEMBER, 1945 • 27



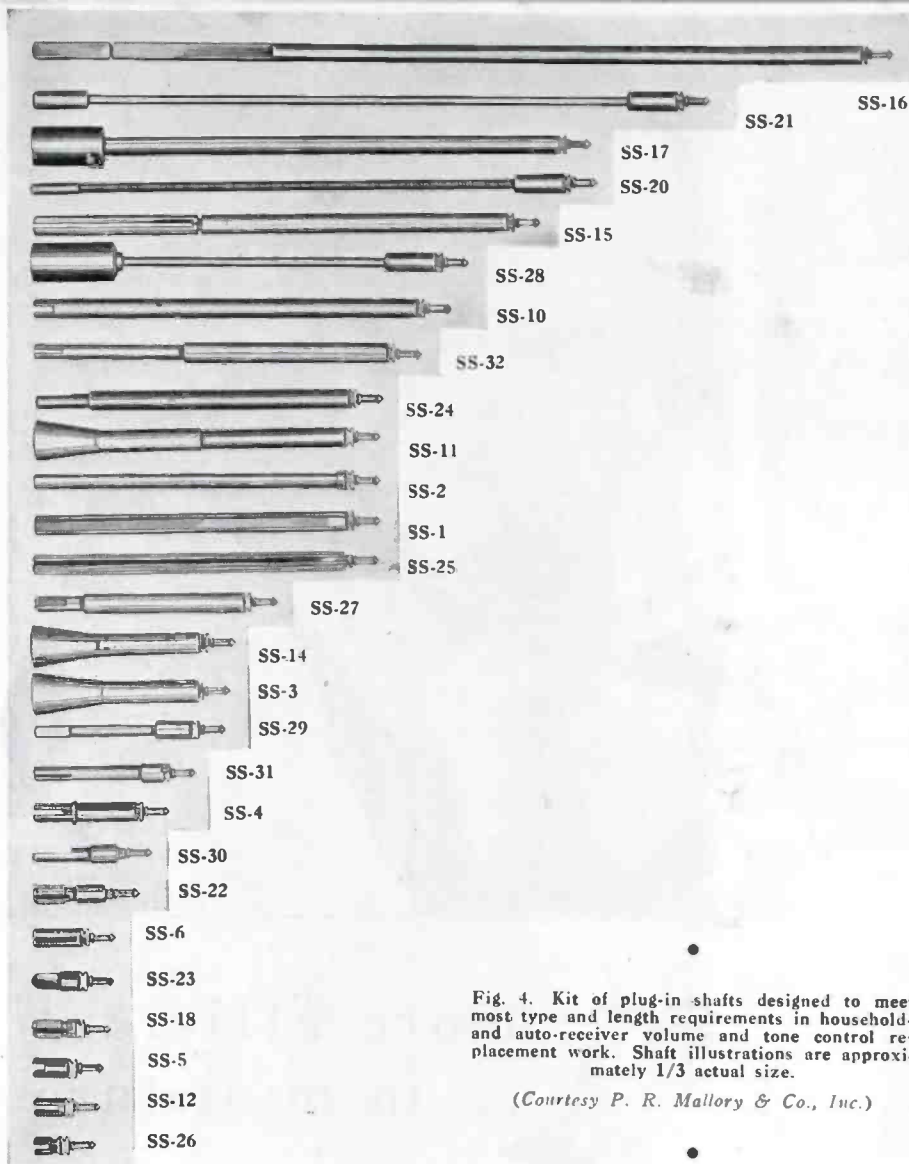


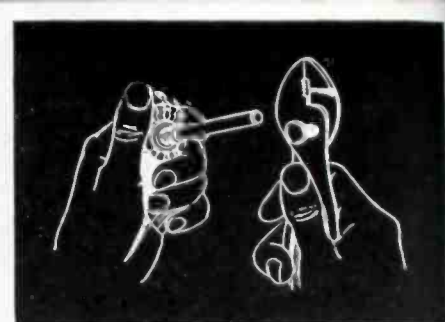
Fig. 4. Kit of plug-in shafts designed to meet most type and length requirements in household and auto-receiver volume and tone control replacement work. Shaft illustrations are approximately 1/3 actual size.

(Courtesy P. R. Mallory & Co., Inc.)

(3)—They speed up volume and tone control replacement in the many receivers in which other components are crowded against the back of the control. In such cases, the replacement control may be inserted in place *before* attaching the shaft, thus eliminating the necessity of first having to disconnect and remove nearby components from behind the control to

provide sufficient space in which to work. (In such cases, if the defective control that is to be replaced is constructed so its shaft is not removable, it may be slipped out from a crowded place by first cutting off its shaft as close to the panel as possible by means of a hacksaw.)

The length of shaft used on controls in receivers is a variable. It de-



A sharp tap is all that is necessary to drive the shaft into the control.

pends on the chassis mounting, thickness of the receiver panel, etc. This dimension varies from 1/2" to 6" or more, with the majority of controls having shaft lengths of 1" to 1 1/2". To adapt a line of fixed-shaft replacement controls to all receivers, the shaft usually is made 3" or 4" in length. For the few receivers having longer shaft controls, extension shafts are obtainable. For shorter shaft controls the ordinary shaft (which usually is made from a special grade of aluminum or other fairly soft alloy) can be notched at the required length by means of a file or knife, as shown in Fig. 5, after which it can be easily broken, as shown.

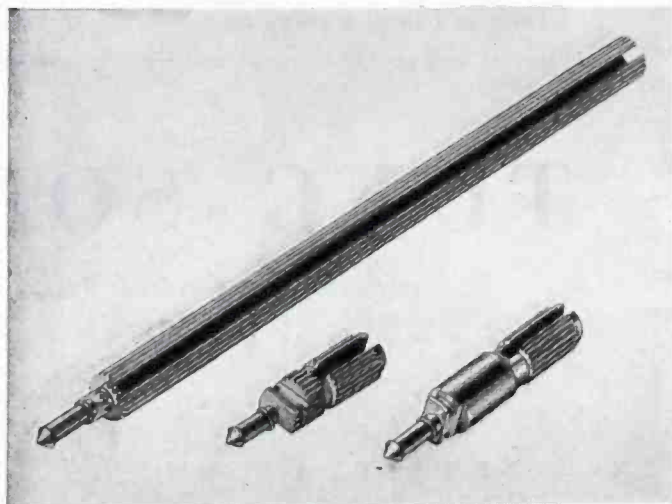
A set of knurled, plug-in shafts of three different lengths up to 4", illustrated in Fig. 6, provide a flexible kit for plug-in shaft type replacement controls where a simple type of shaft is required. These may be cut to the required dimensions to make plug-in shafts of any desired shorter lengths.

#### Clutch Type Controls

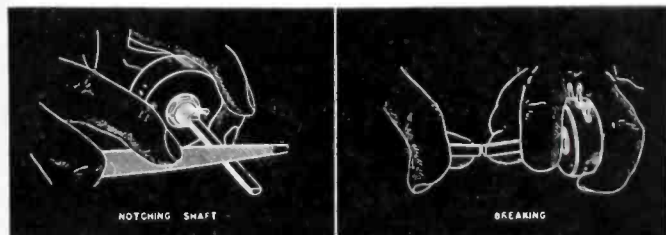
A large number of auto-radio receivers have been constructed with the *on-off* switch that is in or upon the control head located on the car instrument panel, instead of being attached to the volume control in the receiver, Fig. 7.

This arrangement requires a special type of control known as the friction *clutch type* because it contains a friction clutch which permits the shaft to

(Continued on page 30)



Figs. 5 (below) and 6 (left). Fig. 5 Shortening a long shaft to the correct length. Fig. 6. Knurled plug-in shafts in three sizes up to 4". (Courtesy P. R. Mallory & Co., Inc.)





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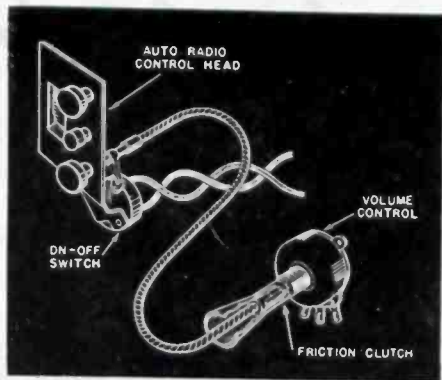


## RADIO CORPORATION OF AMERICA

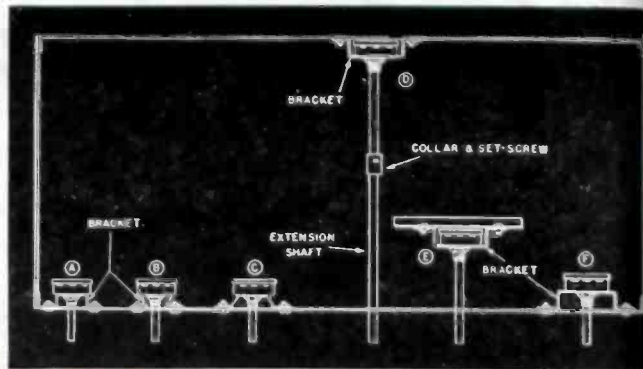
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Phonographs . . . Records . . . Electronics





Figs. 7 (left) and 8 (right).  
 Fig. 7. Application of special type controls having a friction clutch-drive arm which permits the shaft to slip. Used in auto sets. Fig. 8 illustrates the use of brackets for mounting volume and tone controls to front panel and sub panels; also the use of an extension shaft where an extra long shaft is required.  
 (P. R. Mallory & Co., Inc.)



slip in order to allow alignment of the contact arm of the control with the knob indicator on the tuning head so that the on-off switch operates at the correct position. When installing a repaired or replacement control of this type, we must first install the control and insert the driving shaft; then the control knob is turned through its full rotation in both directions. The result is the proper alignment of the contact arm of the control with the driving knob so that the switch operates at the correct position.

Controls having this clutch feature are usually provided with a plain cover, but with a proper portion of the resistance shorted out, so the volume control does not begin to function until the switch has been operated.

Several clutch-type control shaft assemblies of the plug-in type and in different lengths for various models of auto-radio receivers are illustrated at SS-3, SS-14 and SS-11 in Fig. 4.

#### Mounting Brackets, Extension Shafts and Bushings

Metal mounting brackets with slotted mounting holes are available to enable the Service Man to accommodate available replacement controls to most of the special methods of control mounting which are found in some radio chassis, or for attaching the controls to special mounting brackets provided on the receiver chassis. Fig. 8 illustrates several ways of using such brackets.

A narrow bracket may be used, as

shown at *A*, *B*, and *C*, where the control is to be fastened to the panel by means of two screws instead of by its bushing. In arrangements *B* and *C* the bracket is simply bent so that the spacing between the centers of its mounting-screw holes will be the same as that of the holes already in the receiver panel.

Illustration *D* shows the use of a longer mounting bracket, and an extension shaft with its collar and set-screw, when the control is to be mounted to a panel behind the front panel of the receiver. Notice the inverted position of this longer bracket.

In *E* we see the same type of mounting where however the shaft of the control is long enough to make the use of an extension shaft unnecessary. The mounting bracket can be used in the same way as in illustration *F*, if more convenient.

In some types of receivers, particularly auto-radio and communications-type receivers, many parts are mounted by means of such brackets, so some should be included in the Service Man's kit as a matter of convenience and to promote rapid replacement work.

Most controls employed as original equipment on receivers use a standard bushing  $\frac{3}{8}$ " long. This has been adopted as standard by the RMA standards committee. Accordingly, a standard  $\frac{3}{8}$ -32 bushing,  $\frac{3}{8}$ " long is supplied on most commercial replacement controls.

In a few cases it is necessary to

mount replacement controls on extra thick panels. To accomplish this at minimum cost, hex-type shoulder nuts are available as accessories to the control and are sold separately. In using these hex-type shoulder nuts, it is necessary to enlarge the hole in the panel slightly by reaming it. These nuts are screwed on over the standard bushing; the regular flat nut supplied with all controls is not used.

#### Wire-Wound/Composition-Element Control Applications

Two broad types of volume controls are in general use . . . the composition-element or so-called carbon type and the wire-wound type<sup>1</sup>. The former is popular applications of volume controls in cathode and voltage-supply circuits required controls having fair low resistance but a definite current-carrying capacity. Thus wire-wound controls were mostly employed in such circuits. However, the increasing popular practice of using a volume control that controls the audio circuit in AVC receivers, calls for a high-resistance type control which is not required to dissipate much power.

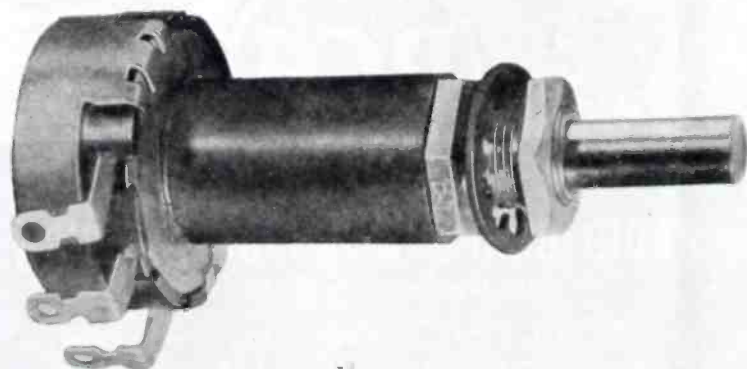
Because it is possible to manufacture the carbon-type control in a greater resistance range and flexibility in the matter of resistance taper<sup>2</sup>, it is the type most used for such control circuits today, especially when intricate resistance tapers are required.

It is obvious that both types have a definite receiver application. It cannot be said that either one type or another is best for all purposes, for each has distinct advantages and disadvantages. Consequently, each type of control is limited in its application to the circuits or conditions requiring the particular advantages of its type.

#### Substituting Controls

Although volume- and tone-control manufacturers offer both types of controls

(Continued on page 61)



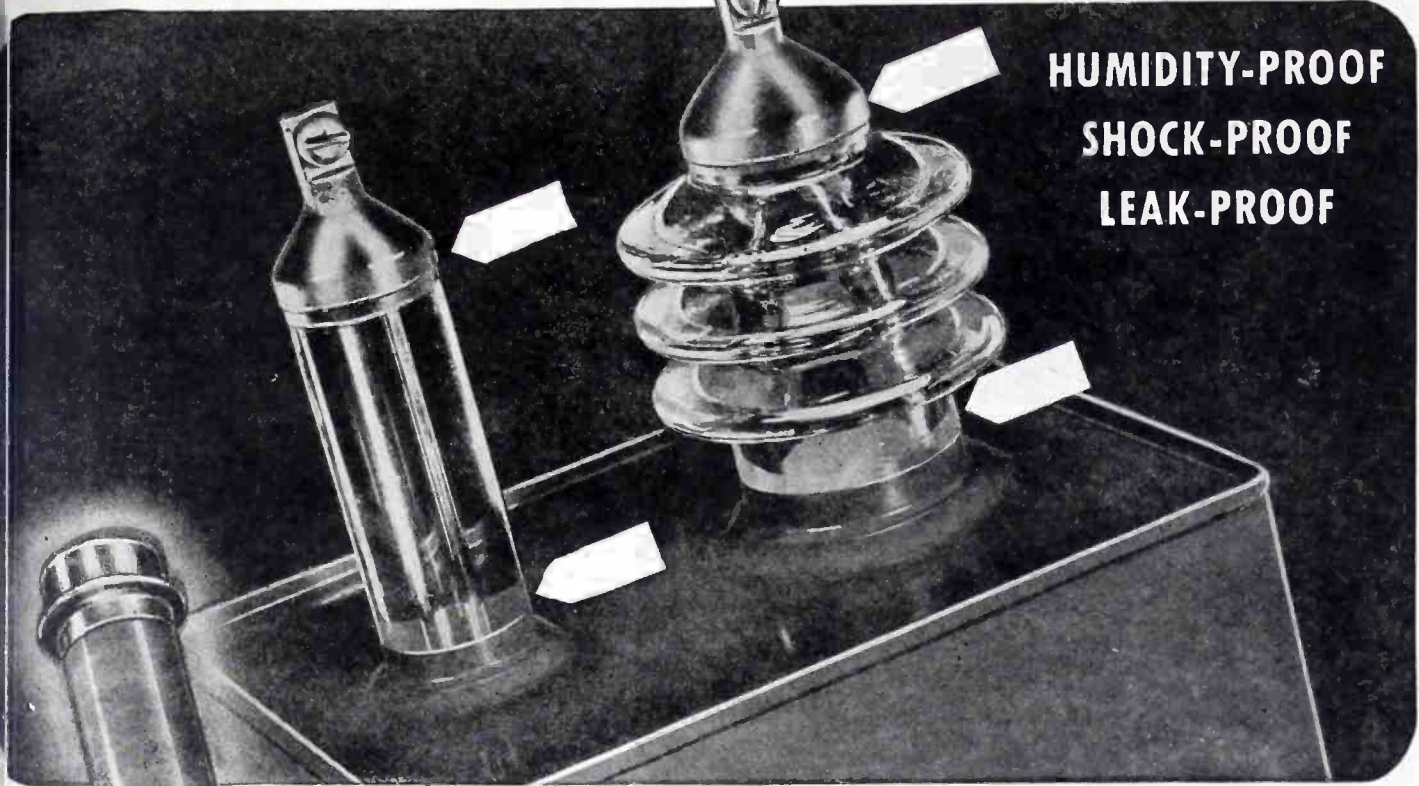
High-voltage insulating coupler applied to control that must be used in high-voltage circuits such as in television, c-r oscillographs, etc.

(Courtesy Clorostat Mfg. Co., Inc.) [Additional data on these couplers will appear in next month's installment.]

<sup>1</sup>See Part 6 of this series, August 1944 SERVICE.

<sup>2</sup>See Part 7 of this series, September 1944 SERVICE.

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# SUPERHETERODYNE MIXERS

by MARTIN W. ELLIOTT

[Part Two]

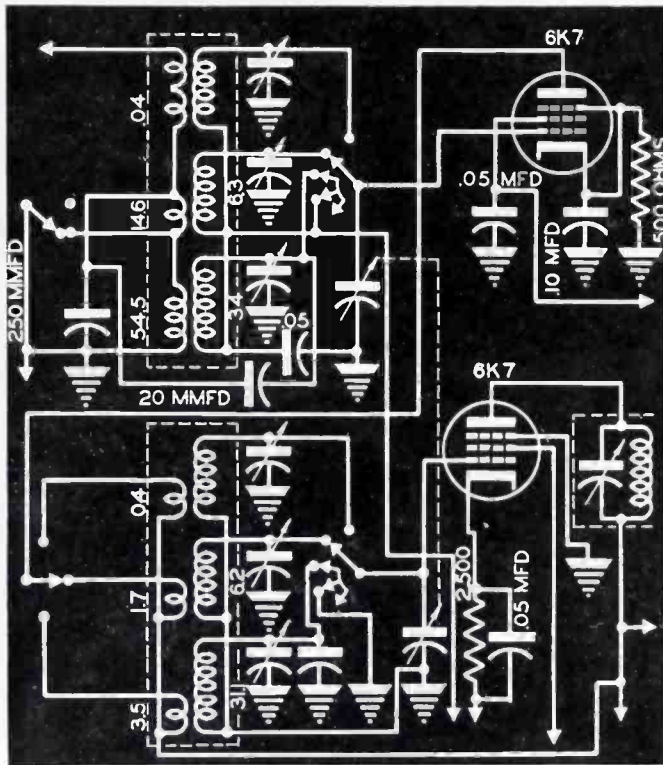
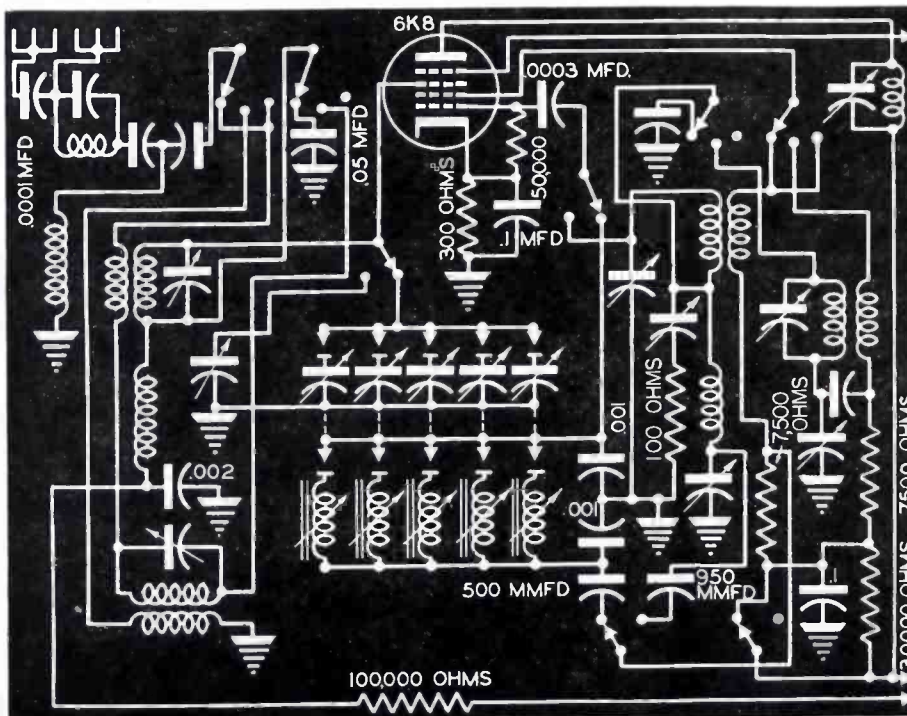


Fig. 11. Mixer circuit of the Ward 62-262. Here, a separate oscillator, not shown, is used. Coupling to the mixer tube is accomplished by tying the oscillator plate to the mixer screen grid.

Fig. 10 (below). Mixer circuit of the Lafayette C-37. A Colpitts-type oscillator is used to simplify the wiring, since only two terminals are required. Note the d-p-d-t switch used to change from manual to automatic tuning.



THE mixer of a 3-band receive Lafayette C-37, using a 6K8, shown in Fig. 10. Provision made for long and short antennas, 456-kc i-f wavetrap, a shunt r-f choke isolated by two capacitors and push button automatic tuning with capacitor tuning for the signal frequency, a permeability tuning for the oscillator frequency. A 300-ohm cathode resistor and 50,000-ohm grid leak provide tube biasing. A Colpitts oscillator circuit with the grid at one end of the coil and the plate at the other end, and the cathode at the potential of the center of the coil by virtue of two .001-mfd capacitors affords a convenient tuning circuit because only two coil terminals are required. The grid is connected through a large .0003-mfd grid capacitor, while the plate is connected through a .0005-mfd capacitor. This is called a shunt-feed system. A 50,000-ohm leak is connected between the grid and cathode. Manual to automatic tuning is controlled by a d-p-d-t switch.

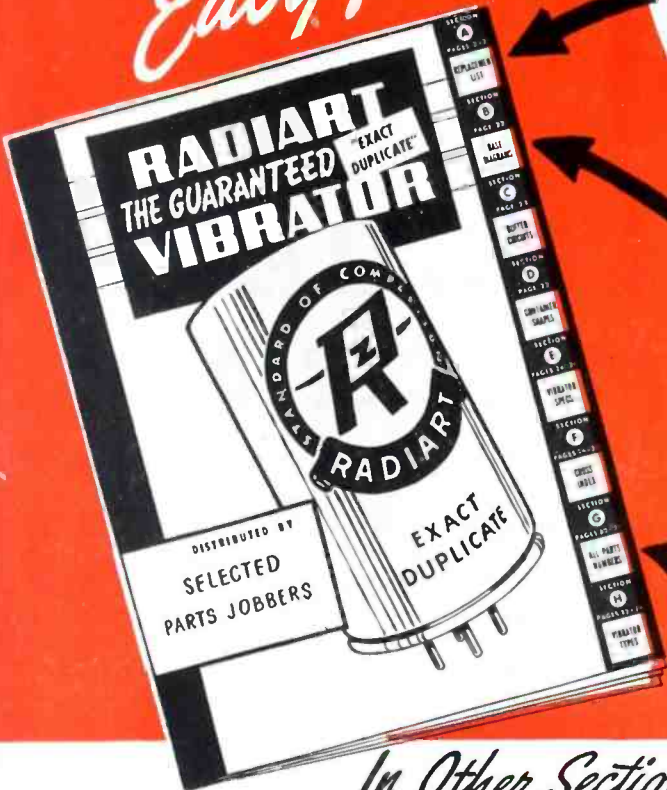
### Capacitor-Tuned Oscillator Control

The capacitor-tuned oscillator used in the manual position is also unconventional. On the s-w position shown the grid is connected to the top of the oscillator-tuned circuit. The plate is connected through a tickler coil and .00075-mfd capacitor to the opposite end of the tuned circuit. The junction of the two coils in the tuned circuit is connected to ground through a trimmer and 100 ohms, also through a switch to ground through a .0065-mfd capacitor, virtually shorting the low coil. On the police band the low coil is shunted by a grid coil of second-oscillation transformer. The

(Continued on page 39)

# RADIART VIBRATOR GUIDE (Most Complete Published)

Makes  
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**Section A...Vibrator**

MFRS. PART NO.      RADIART NO.      BASE DIA.  
SERIES NO. SET MFR. YEAR MADE      LIST PRICE      BUFFER COND.

CAR MAKER

Name, Model No.	Mfrs. Part Number	Radiart Number	List Price	Base Dia.	Buffer Condenser
<b>CHRYSLER</b>					
C1808 (Elec. P. B.) (Philco—1941)...	83-0027	5326P	3.00	A	.005
25C6 (Wells-Gardner—1938)...	19A32	5437	5.95	AB	.018
600 (Mech. P. B.) (Colonial—1941)...	43697	5301	3.55	A	.004
601 (Colonial—1942)...	911545	5301	3.55	A	.004
800 (Philco—1941)...	83-0027	5326P	3.00	A	.005

Every model listed includes all available data. The correct Radiart Replacement number and other essential information is determined instantly.

**SECTION "B"—Cross**

Diagram Number	Shape	Voltage	Diam.	Ht.	Freq.	Identifying Characteristics	Max. Load Amps
B 3417	2	6	1 1/4	4 1/2	105	.....	6
3815	9	6	1 1/8	4 1/2	105 Spec. Cup	.....	6
C 5309	1	6	1 1/2	2 3/4	105	.....	6
5331	1	6	1 1/2	3 1/4	105	.....	6
D 4256	1	6	1 1/2	3 3/4	105	.....	10
4256-12	1	12	1 1/2	3 3/4	105	.....	6

In addition to conventional base diagram drawings this section is unique in that it groups all similar base types together indicating readily the differences between vibrators with the same base wiring. All characteristics are shown, including frequency and maximum load limit of each type.

## In Other Sections..

- Section "C"—Buffer Condenser Values and Circuits.
- Section "D"—Container Shapes permitting an easy method of "visual" identification.
- Section "E"—Complete Vibrator Specifications arranged numerically by number. Contains necessary data not published in any other replacement guide.
- Section "F"—Long a favorite with users of this guide. The only cross-index of all other manufacturers or merchandisers of vibrators, converting their type numbers to the Correct Radiart Replacement.
- Section "H"—Numerical Listing of Radiart Vibrators. Furnishes complete information as to all models serviced by each unit. Also advises year each type was originated.

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**SECTION "G"—Radiart and Original Equipment**

Original Equipment Part No.	Radiart Part No.	Original Equipment Part No.	Radiart Part No.	Original Equipment Part No.
75	3283	1974	5301	8539
80-161	5421	2080	3417	8540
82B	5341M	2110	3417	8541
83-0017	5326P	2269	5413	8542
83-0025	5326P	2404	5340M	8601
83-0026	5326P	2501	5411	8602

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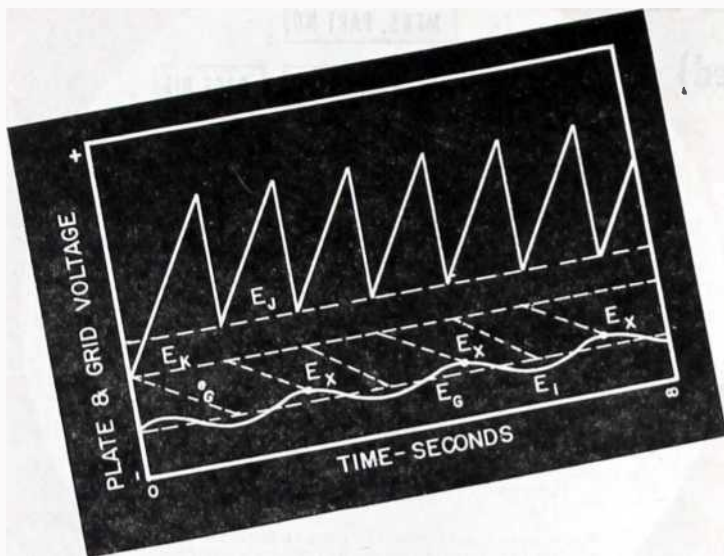


Fig. 1. Graphical synchronization of the linear time-base oscillator system. The critical grid voltage  $E_g$ , at which the thyatron conducts, is proportional to the plate-to-cathode voltage  $E_p$ . Thus when the timing capacitor voltage, which is the thyatron plate voltage, is near a maximum value, the signal voltage component  $E_i$  exceeds the critical grid-to-cathode voltage level. This condition occurs at the critical grid voltage level  $E_x$ , and the thyatron relaxes the capacitor charge synchronously with the arrival of the maximum positive potential level of the signal voltage.

# C-R OSCILLOGRAPHS SERVICING... APPLICATIONS...

WHERE the oscillograph is utilized to provide a visual analysis of voltage variations, under the condition that the linear time-base oscillation system is not synchronized to oscillate in phase with the frequency of the variation under observation, the image appearing on the screen appears to be in continuous motion. This condition results from the existence of the heterodyne or beat frequency which is developed between the frequency of the voltage under analysis and that of the linear time-base system output.

In order that the waveform appearing on the screen be stationary, it is imperative that the frequencies of the incoming signal voltage and of the linear time-base oscillator synchronize perfectly. Thus, if the image or waveform which is written on the screen varies in exactly the same pattern with each positive motion or sweep of the electron beam, the image of the waveform is written on the screen in exactly the same manner with each succeeding sweep. If, however, the subject waveform occurs earlier in each of the succeeding sweeps of the electron beam, the waveform written on the screen is altered in position with each sweep. Moreover, since the waveform is recurrent earlier in each charging of the linear time-base timing capacitor, the resulting image of the waveform on the electron screen appears to *move to the left*. Again, if the waveform should occur later in each positive motion of the electron beam, a similar alteration of the wave

[Part Five of a Series]

by S. J. MURCEK

image position obtains, and the image appears to move to the *right*.

As a direct consequence of the definite motion which is imparted to the wave image written on the screen by the beat which is present between the two frequencies, it becomes possible to determine accurately the frequency of the voltage variation which is under visual analysis. This, if the motion of the written image is in a left hand direction, the frequency of the signal voltage is greater than that of the linear time-base oscillator. Conversely, if the image motion is in a right hand direction the signal voltage frequency is less than that of the linear time-base oscillator. Zero beat, or synchronization of the two frequencies, occurs when the image is stationary.

For wave- or voltage-variation analysis, it is essential that the image remain stationary. This, in turn, requires that the oscillation of the linear time-base oscillator occur in exact synchronism with the voltage variation which is under analysis. Commercial oscillographs are, therefore, provided with suitable means for the necessary synchronization of the linear time-base system and the signal voltage frequencies. In all of these oscillographs, the

synchronization is usually effected through the modulation of the linear time-base relaxation tube grid bias potential by a portion of the voltage variation.

The synchronizing system utilized in the du Mont 164E oscillograph is shown in the circuit diagram, Fig. 2. Here, the voltage which is under observation is impressed across the synchronization system input terminals *H* and *G*. Since the capacitance of the dynamic coupling capacitor  $C_{12}$  is large, and the resistance of the synchronization potentiometer  $R_s$  is high, the voltage variation impressed across the input terminals *EXT* and *G* appears, in the greatest part, across the resistance element of the synchronization control potentiometer. Further, since a portion of this potential appears between the slider arm and the grounded terminal of the synchronization control potentiometer, and is thus directly in series with the control grid of the 2B4 thyatron, together with the grid current limiting resistor  $R_{g1}$ , a part of the signal voltage variation is effectively in series with the thyatron control grid-to-cathode bias potential, the latter maintaining the thyatron control-grid negative. Hence, each positive alternation of the signal voltage effects a reduction of the negative grid-bias voltage present between these electrodes.

The effects of the signal-voltage modulation of the 2B4 grid-to-cathode potential are evident from the graphical illustration of Fig. 1. Here the

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# GENERAL ELECTRIC

176-05-8880



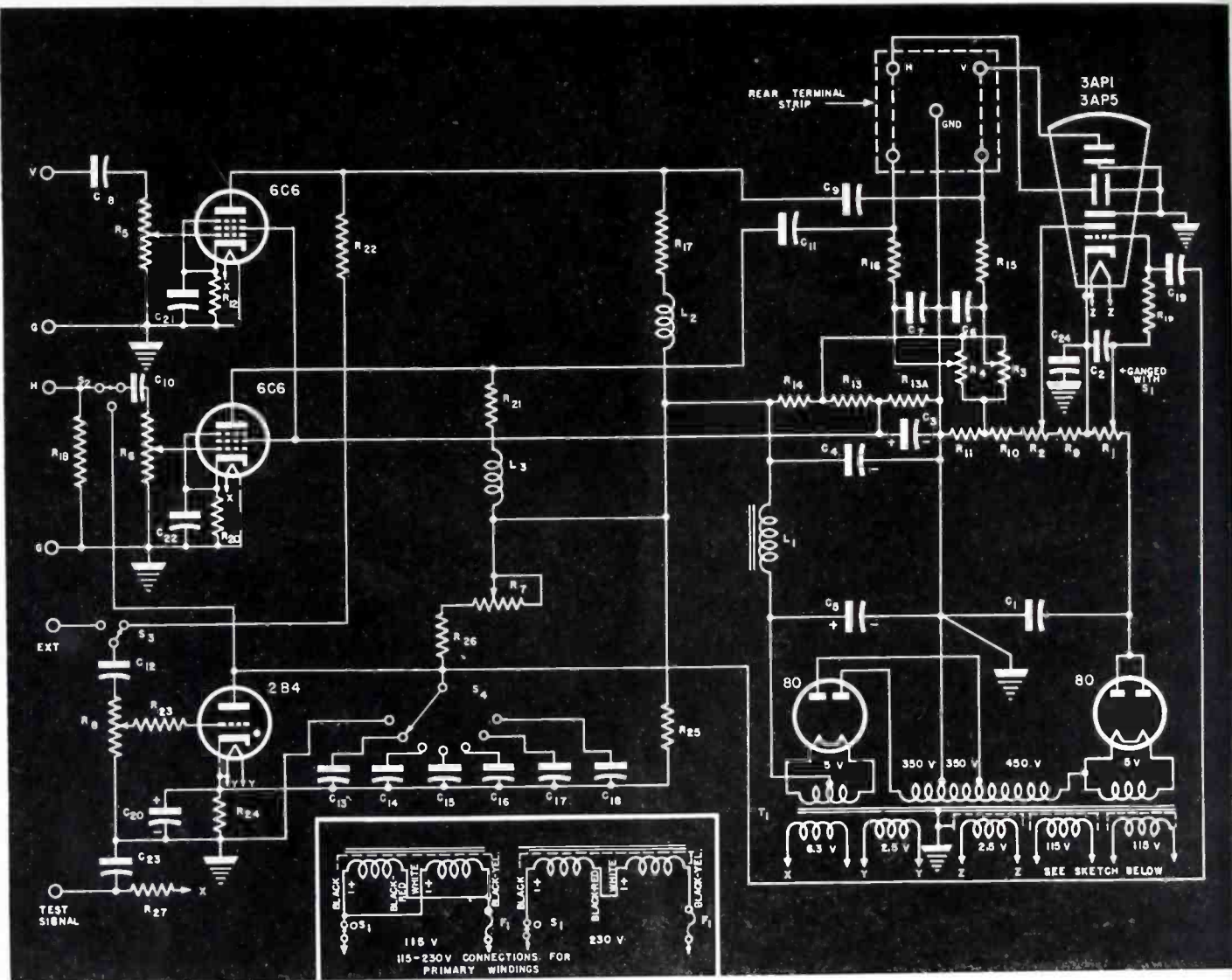


Fig. 2. Circuit of Du Mont 164 E oscillograph.

relations of the various voltage variations occurring in the synchronized linear time-base oscillator operation are plotted with respect to the 2B4 cathode potential level  $E_k$ . The d-c component of  $E_c$ , which is negative, is shown to be modulated by a portion of the signal voltage variation  $E_s$ . Since the critical grid potential  $E_r$  is increasingly negative with each increase of the plate-to-cathode potential,  $E_p$ , and the latter increases directly in proportion with the charge on the timing capacitor, the positive variations of the grid-to-cathode control voltage eventually exceed the critical voltage  $E_r$ . Thus the control grid of the thyratron is effectively positive and becomes conductive, at which instant the tube relaxes the charge on the timing capacitor. Therefore, when the linear time-base oscillation circuit is so adjusted that the frequency of the relaxations is near that of the signal voltage, as we see in Fig. 1, each relaxation must occur in synchronism with each positive alternation or peak of the signal voltage.

Further study of Fig. 1 indicates that thyratron breakdown and the relaxation of the charge on the timing

capacitor occur when the signal voltage attains its maximum positive crest, under the condition that the signal voltage wave is of sine wave form. Since the maximum positive voltage level in any sine wave alternation occurs  $90^\circ$  after the inception of the cycle, the relaxations of the linear time-base capacitor charge occur  $90^\circ$  out of phase with the signal voltage variation. The wave image written on the screen is consequently initiated at the maximum positive potential level in its pattern.

Studying the circuit of Fig. 2, we note that the signal voltage variation required for the synchronization of the linear time-base oscillations is obtained either from the plate circuit of the vertical amplifier, or from the external signal synchronizing voltage source, available through the input terminals *EXT* and *G*. A convenient switch,  $S_3$ , is provided to connect the ungrounded terminal of the synchronization control potentiometer,  $R_8$ , to either voltage source. The series resistor,  $R_{22}$ , connected between the *INT* contact of the

switch  $S_3$  and the plate of the vertical amplifier pentode prevents excessive loading of the vertical amplifier plate circuit by the linear time-base synchronizing input circuit. Only a very small portion of the vertical amplifier output voltage is necessary to effect satisfactory synchronization of the two frequencies.

In general, modern electronic apparatus is designed for synchronous operation from low-frequency commercial power sources. Hence, synchronization of the horizontal sweep frequency in the oscillograph with that of the voltage variations usually encountered in industrial electronic apparatus, is most effectively accomplished through a linear time-base synchronization circuit connected directly to a voltage source of the same frequency. This type of operation is especially important where the phase relation of the voltage variation under observation to that of the source voltage wave must be ascertained, inasmuch as such phase relationships are not evident when the synchronizing system is activated by the plate circuit of the vertical amplifier.

Where the synchronization of the

linear time-base frequency to that of the voltage under study is accomplished by exciting the plate circuit of the vertical-amplifier pentode, relaxation of the timing capacitor charge must always occur at the maximum positive voltage level attained by the amplified signal voltage.

Thus, if the maximum positive voltage crest occurs when the vertical-amplifier output voltage is completely out of phase with that of the voltage source wave, the linear time-base capacitor relaxations occur at the maximum positive peak of the amplifier output voltage and are, therefore, completely out of phase with relation to the source voltage wave. Further, if the phase position of the amplifier positive peak voltage swing varies with relation to its initial position, the linear-time base capacitor relaxations must also vary in phase position, and the wave image written on the screen shows no resultant motion. This factor is of great importance where the signal voltage is, for example, the a-c component of a phase-controlled rectifier grid-to-cathode control potential, where the phase position of the a-c component must be shown to vary directly with the operation of the phase-control potentiometer.

When it is necessary to synchronize the oscillograph horizontal sweep voltage with that of the line frequency, or that of the source, it is only necessary to connect the terminal, *test signal*, to that marked *EXT*, and to operate the switch,  $S_8$ , to the *EXT* position. Then the horizontal sweep voltage will be synchronized with the a-c or source voltage frequency, at a  $90^\circ$  phase lead angle. When the oscillograph is operated with this form of horizontal frequency synchronization, application of the input voltage results in the development of a wave image which is initiated at the *positive* zero voltage inflection of the sine voltage wave. The maximum positive crest of the signal potential is shown clearly as a positive peak or cusp in the screen image. Moreover, if the phase position of the signal voltage wave with relation to that of the source voltage wave is varied, the extent of the variation is clearly visible in the motion of the screen image.

Where the oscillograph is operated from a stable voltage source, the voltage present across the phase-shifting capacitor,  $C_{20}$ , may be readily utilized to calibrate the vertical deflection system. The calibration is accomplished through connection of the capacitor terminal, *test signal*, to the vertical amplifier input terminal,  $V$ , and the subsequent adjustment of the vertical gain control to such a position that the height of the vertical motion of

the luminous spot on screen is twice the division number.

The horizontal voltage sweep-frequency range is arranged for operation over a frequency range extending from a low frequency limit of approximately 12 cps to a high-frequency limit approaching 50 kc. Since this extended range cannot be practicably arranged in a circuit comprising a single capacitor and a single variable resistor or potentiometer, a multiplicity of capacitors,  $C_{13-14-15-16-17-18}$ , of various capacities are used, together with a *vernier frequency* control potentiometer,  $R_{20}$ , and range selector switch,  $S_4$ . Each of these capacitors is so selected that the frequency ranges covered appreciably overlaps the ranges covered by the capacitors adjacent to the former. It should be observed here that the shield terminal of each capacitor is common with the cathode of the relaxation thyatron, and that the maximum potential which is developed across these capacitors is relatively low in level. Further, because of the low-capacitor operational potential, the charge stored is correspondingly low, necessitating the application of high capacitances in the lower-frequency ranges.

It is the horizontal deflection system, together with the linear time-base oscillator, which must be generally depended upon to effect the writing of recognizable waveforms on the screen. Where the signal input or dynamic voltage variation applied to the input terminals of the vertical deflection amplifier is subject to sporadic disturbances or interruptions, the continuous horizontal motion of the beam, effected by the linear time-base oscillator and the horizontal deflection amplifier, prevents accidental damage to the screen which would result with a stationary luminous spot. Hence, before any cathode-ray oscillograph is placed into actual operation, it is prudent to be sure that the beam will be in motion when the cathode of the tube reaches operating temperature.

In the du Mont unit of Fig. 2 the *intensity* or beam control is ganged with the primary or power input control switch,  $S_1$ . Thus, when the unit is placed into operation, it is only necessary to partially turn the intensity control to the a-c line control switch,  $S_1$  to the *on* position. The slider arm is then placed so that the grid is maintained quite negative. This prevents further development of an electron beam during the period in which the tube heaters rise to operating temperature. Then, it is necessary to see that the horizontal amplifier input control switch,  $S_2$ , which is usually ganged with the linear time-base *coarse-frequency* control switch,  $S_4$ , is in the

linear sweep position, if no other form of horizontal deflection potential input is to be used. In this way we can be sure that the beam will be in motion when the beam is permitted to strike the screen.

Since the first plate, or accelerating electrode, is effective in the development of the beam, it is necessary to turn the *focus* control potentiometer knob a complete half-turn in a clockwise direction. The *vertical* and *horizontal* positioning controls determine the normal or *idle* position of the electron screen pattern.

The length of the horizontal sweep pattern is governed by the amplification level at which the horizontal amplifier operates. Inasmuch as no actual deflection of the electron beam occurs if this control is left in the minimum or zero position, it is advisable to advance the horizontal or  $X$  axis amplifier gain control, in a clockwise direction, at least to the 50% dial position. At this time, the intensity control may be advanced in a clockwise direction until a visible green trace is written on the screen. The intensity of the luminous trace is then carefully adjusted to the desired level or brightness, and focussed to the desired clarity, by manipulation of both the intensity and the focus control potentiometers. Here, it may be found that the horizontal sweep voltage causes the written trace to extend beyond the edges of the electron screen area, causing a visible parasitic glow at either of its extremities. This condition is corrected by appropriate reduction of the horizontal amplifier gain. The final position of the trace may be brought to the geometric center of the screen by the proper manipulation of the vertical and horizontal positioning controls. In the instance of the vertical control, the screen pattern moves *upward* when the vertical control is turned in a clockwise direction, and, in the instance of the horizontal control potentiometer, the pattern moves to the *right* when the control is turned in a clockwise direction.

Under the condition that the controls are in the position just described, the pattern written on the screen will be a short, straight line. If, at this time, an a-c potential is applied to the input terminals  $V$  and  $G$  of the vertical amplifier, and the vertical gain control is advanced slightly, the beam will be subjected to deflection voltages which operate at a right angle with respect to each other. Briefly, the vertical deflection is perpendicular to the horizontal deflection. The pattern written on the screen is reformed into rectangular coordinates, the actual

(Continued on page 52)



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127 West 26th Street



New York 1, N. Y.

# ELECTRONIC ALARMS

(Continued from page 24)

once it is tripped it remains closed until opened manually.  $R_1$  limits the plate voltage on tube 2, so that the plate current will not be too high for the positive grid condition of operation.

Although circuits of this kind can be developed experimentally, it usually is better to purchase commercially manufactured products which have had the kinks removed.

Another type of alarm control is

shown in Fig. 2.\* The operation is very simple. The oscillator may be tuned to a fairly high frequency, perhaps 7000 kc. If a small change in capacity occurs in the grid circuit, the oscillator plate current will change. Adding capacity to the grid circuit causes a decrease in the operating frequency, which, in turn, causes the oscillator plate current to rise. This increase in current may be sufficient to

cause the closing of a sensitive relay in the plate circuit of the oscillator tube. When the relay contacts close, an external bell system circuit is set in operation, giving the alarm.

In this circuit,  $C_1$  is a small capacitance to limit the detuning effect.  $L_1$  and  $L_2$  represent the oscillator coil, the lower section  $L_2$  serving to provide inductive coupling between grid and plate circuits and develop oscillations.  $C_2$  the tuning capacitor to set the frequency of operation.  $C_3$  and  $R_1$  are the usual gridleak and capacitor, and  $C_4$  is a plate circuit r-f bypass capacitor which keeps the plate-circuit impedance low in value, and aids oscillation.

In a typical installation the pickup wire would be connected to the object to be protected. If the object were a safe, it would be insulated from the ground by rubber pads and serve as the pickup wire. Anyone coming near the safe would upset the capacity of the circuit and detune the oscillator, setting off the alarm. Anyone approaching a door or window where the pickup would be located would also cause the alarm to be set off.

Another type of alarm is shown in Fig. 3. Two metal plate electrodes are used. Normally, they are separated, but when anyone exerts pressure on them the plates touch and the alarm is set off. Once the alarm is set, the relay stays closed, due to a locking arrangement, until turned off manually. Normally, with the plates not touching, the grid circuit of the tube is open, since  $R$  may have a value of 10 or 15 megohms. Closing the grid circuit causes the plate current of the tube to rise and the relay swings into operation, causing the alarm to go off.

Thin steel plates are probably the best to use, for they are quite tough and flexible.

Electrically, the steel is not very conductive, but since the resistance can be fairly high and still permit efficient operation of the tube this is no particular disadvantage.

Alarm circuits may also be devised to actuate cameras. The cameras may be concealed in the walls. The relay contacts are simply connected in series with a flashbulb circuit using a couple of dry cells to set off the bulb. The shutter on the camera can be left open. The speed of the flash explosion is sufficient to catch the action without using intricate timing arrangements.

\*Some of these circuits are covered by patents and cannot be duplicated for sale to others.

## MIXERS

(Continued from page 32)

plate is switched to the tickler of the second transformer. On b-c both the coils of the first transformer are used in series. The plate voltage is increased for automatic tuning by shorting a 30,000-ohm series resistor in the B supply.

### Ward 62-262

A complex mixer system with a tuned r-f stage, 3-gang capacitor and a separate 6C5 triode oscillator, Ward 62-262, is shown in Fig. 11. This model uses 6K7s for both r-f amplifier and mixer. Three bands are covered; 148 to 380 kc, b-c and s-w. The antenna transformer has three primary coils in series with a shorting switch for the l-f and b-c primaries, as well as a .00025-mfd capacitor across them. A 20-mmfd coupling capacitor links the b-c primary and the l-f secondary for additional l-f coupling. A separate secondary is used for each band with a combination selector and shorting switch for wavechanging. The interstage transformer is similar except that the r-f amplifier plate is switched to individual primaries.

The oscillator transformer uses separate cathode ticklers for l-f and b-c and a combination of cathode-tapped Hartley and plate tickler for s-w. The mixer tube is excited by cathode-to-cathode coupling through a bias resistor of 2500 ohms and its .05-mfd bypass. The oscillator plate is also directly connected to the mixer screen. The plate is at ground potential at l-f and b-c but is hot on the short-wave band because of the plate tickler. Therefore, this tie to the screen constitutes an additional source of excitation. In some receivers with a separate oscillator, supplementary short-wave coupling is supplied to the signal grid. Still other sets use magnetic coupling between oscillator and converter by winding the coils on the same coil form.

### VIDEO WINDOW DISPLAY



One of a series of five window displays used by Gimbel's-Philadelphia to promote the RCA in-store television demonstration being staged by Gimbel's.

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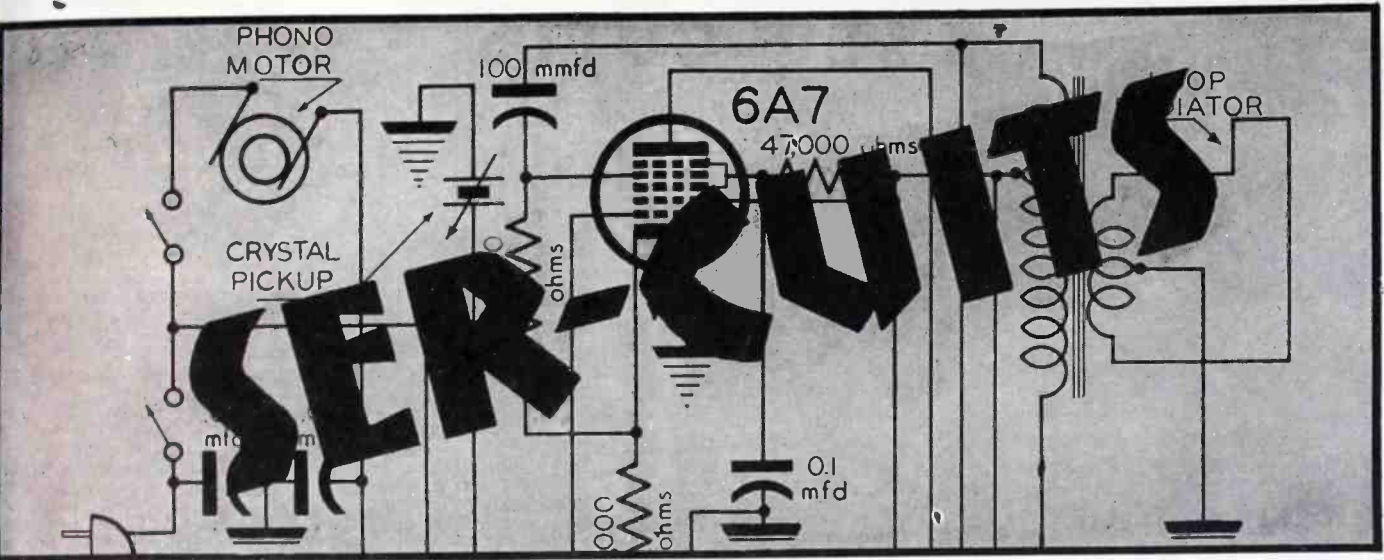
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THE postwar receivers, long anticipated, have now begun to come off the production line. From the circuits of several of the models, just received, we find that quite a few interesting features have been included.

### by HENRY HOWARD

a-c/d-c 4-tube and rectifier unit, model 571. One of the features of this model is a fixed bias for the avc bus. This may be considered delayed avc and is ob-

tained from the rectified grid voltage developed by a 12SA7 oscillator across a 22,000-ohm grid leak. Since this voltage is usually of the order of 5 volts, it is necessary to reduce it considerably. This is done by a 15-meg-ohm resistor. This resistor also serves as a filter in cooperation with a .05-mfd bypass capacitor. The filter is required to keep oscillator r-f out of the avc system.

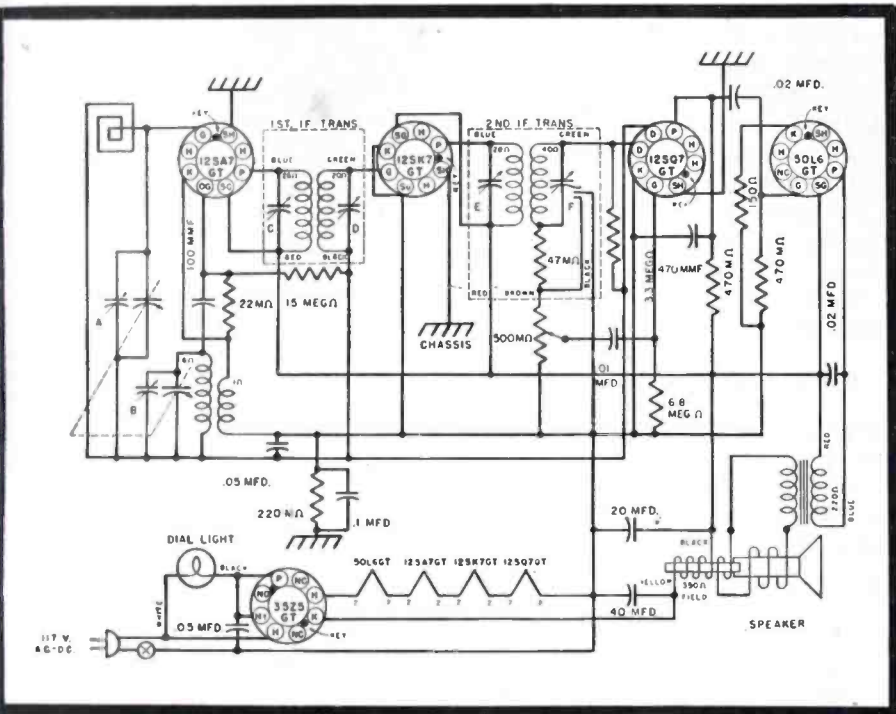
The oscillator uses a cathode-type tickler circuit. Chassis is connected to the B-supply through a 0.1-mfd capacitor and 0.22-megohm resistor in parallel. A 350-ohm series field speaker supplies the only series filter element; no resistors are used in the power supply.

#### Meck RC-5C5

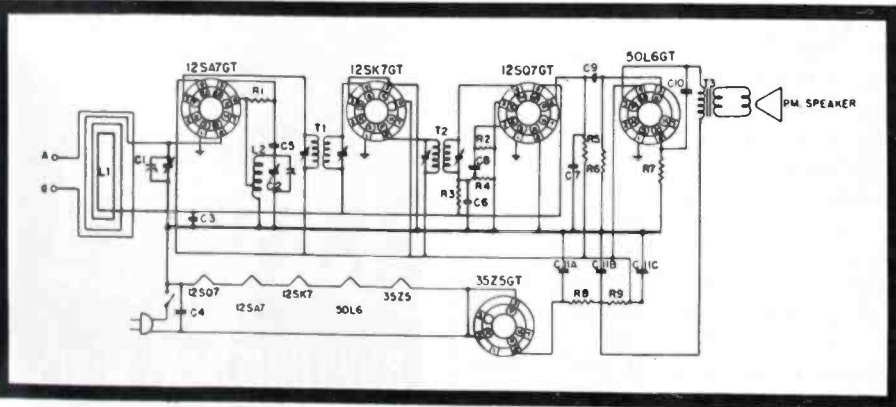
In Fig. 2 appears a Meck Industries postwar loop receiver, model RC-5C5. Provision for an external antenna is also provided in this model. The oscillator is a grounded-plate hot-cathode type Hartley. To afford a negative bias one of the 12SQ7 diodes is directly connected to the avc bus. The 150-ohm bias resistor of the 50L6 power tube is not bypassed.

A p-m speaker is used, necessitating a two-section resistance filter consisting of 200 ohms and 1,000 ohms, the

(Continued on page 42)



Figs. 1 (above) and 2 (below). Fig. 1. Detrola 571. Fig. 2. Meck Industries RC-5C5. List of parts at right.



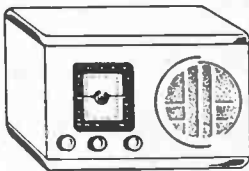
Circuit Symbol	Description	Model
C1, C2	Condenser-Variable, with pulley	RC-5C5
C1, C2	Condenser-Variable, with pulley	RC-5C5-A
C1, C2	Condenser-Variable, with pulley	RC-5C5-B
C1, C2	Condenser-Variable, with pulley	RC-5C5-C
C3, C4, C10	Condenser-Paper, 0.05mfd, 400V	All
C5	Condenser-Mica, 0.0005mfd.	All
C6, C7	Condenser-Mica, 0.00025mfd.	All
C8, C9	Condenser-Paper, 0.01mfd, 400V	All
C11A, C11B, C11C	Condenser-Electrolytic 20/20/20 mfd 150V	All
R1	Resistor-Carbon, 20,000 ohms	All
R2	Resistor-Carbon, 10 megohms	All
R3	Resistor-Carbon, 2 megohms	All
R4	Control-Voltage, with switch, 1 megohm	All
R5	Resistor-Carbon, 250,000 ohms	All
R6	Resistor-Carbon, 500,000 ohms	All
R7	Resistor-Carbon, 150 ohms	All
R8	Resistor-Carbon, 200 ohms	All
R9	Resistor-Carbon, 1000 ohms	All
L1	Antenna-Loop	RC-5C5, A, B, C
L2	Antenna-Loop	RC-5C5-C
L3	Coil-Oscillator	RC-5C5, A, B, C
T1	Transformer-1st I.F.	RC-5C5-C
T2	Transformer-2nd I.F.	All
T3	Transformer-Output	All
SPKR	Speaker-P.M. 4" round, less T3	All
SPKR	Speaker-P.M. 4" round, with T3	All



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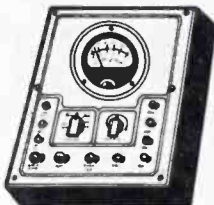
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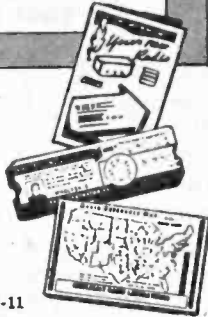
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# SER-CUITS

(Continued from page 41)

electrolytic being a triple 20-mfd capacitor.

## Detrola 568

A postwar a-c/dc 2-band receiver, Detrola, model 568, is shown in Fig. 3 (page 44). This model has an unusual bandswitch system. The signal grid of a 12SA7 is switched to either the short-wave or broadcast transformer. A supplementary 2.2-mmfd capacitor acts as a capacity coupling from antenna to grid, boosting the high-frequency end. In the circuit diagram the switch is shown in short-wave position. Here the antenna is connected to the short-wave primary through a .002-mfd capacitor, the primary circuit being completed through the bandswitch to B-. The same switch member also shorts the unused broadcast oscillator coil, completing the short-wave oscillator circuit to B-. A third section of the switch connects the 12SA7 cathode to a tap on the short-wave oscillator coil, or to the cathode tickler of the broadcast coil.

A 150-ohm resistor is connected in series with a 100-mmfd grid capacitor. A 5100-mmfd padder is in series with the oscillator coils. Bias for the 50L6 is supplied by an unbypassed 150-ohm resistor. The chassis is connected to B- through a 0.1-mfd capacitor and 220,000 ohms, in parallel.

## Garod High-Fidelity Receiver

A prewar high-fidelity a-m receiver with several interesting design features is shown in Fig. 4 (page 44). This model has a variable bandwidth and separate low and high-frequency p-m speakers. The tuner and power amplifier are built on separate chassis, each with its own power supply. A 2-section 10-kc low-pass filter has been included. This may be switched into the audio amplifier between the tuner and power amplifier to minimize interference in the high-frequency audio range, including the 10-kc beat between adjacent channel carriers.

In the input is an iron-core antenna transformer, designed for a short antenna or a long antenna, in series with a .0001-mfd capacitor. A .006-mfd blocking capacitor prevents grounding the antenna. In the tuned secondary circuit is a 150-ohm series resistor. There is a similar 50-ohm unit in the tuned first detector circuit to broaden the response of these circuits for acceptance of an extended treble range.

A 6SA7 converter employs a 300-



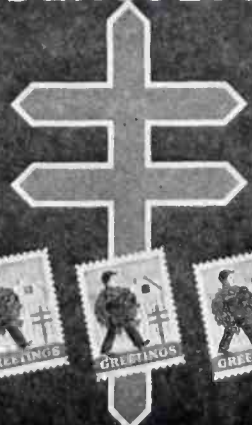
STATEMENT OF THE OWNERSHIP, MANAGEMENT, CIRCULATION, ETC., REQUIRED BY THE ACTS OF CONGRESS OF AUGUST 24, 1912, AND MARCH 3, 1933

OF SERVICE, published monthly at New York, N. Y., for October 1, 1945.  
State of New York } ss.:  
County of New York }

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The r-f, converter and two i-f screens are tied to a common supply. The first three stages are supplied with avc bias. The r-f detection components are filtered out by a low-pass filter consisting of 50 mmfd, 100,000 ohms and another 50 mmfd. A ¼-megohm resistor is connected in series with the volume control to prevent overloading of the detector with the consequent distortion. The treble tone control is connected in parallel with the volume control. When the grounded arm is at the lower end of the control, a .001-mfd capacitor is connected in shunt with the volume control, cutting the highs. When the arm is at the top, the .001-mfd unit is in series with a ½-megohm resistor making the shunting ineffective. However a .05-mfd capacitor is connected across a 2,000-ohm cathode bias resistor which causes an increase in highs. This action may be called selective degeneration because the bypassing action of the .05-mfd unit is confined to the treble only, increasing the gain in proportion to the frequency. Low frequencies are not bypassed, so the full amount of degeneration is present.

The 6J5 first audio has a grid leak of only 150,000 ohms. A 6C8G is used for the second and third a-f stages, the gain being limited by interposed feedback from the second audio plate to the first audio cathode and by a 1,000-ohm second a-f bias resistor without bypass. There is also some attenuation in the bass tone control and the associated 15,000-ohm grid leak in the third a-f stage. This control consists of a 2-megohm potentiometer which acts as a variable shunt to a .001-mfd audio-coupling capacitor. The capacitor is so small

(Continued on page 44)



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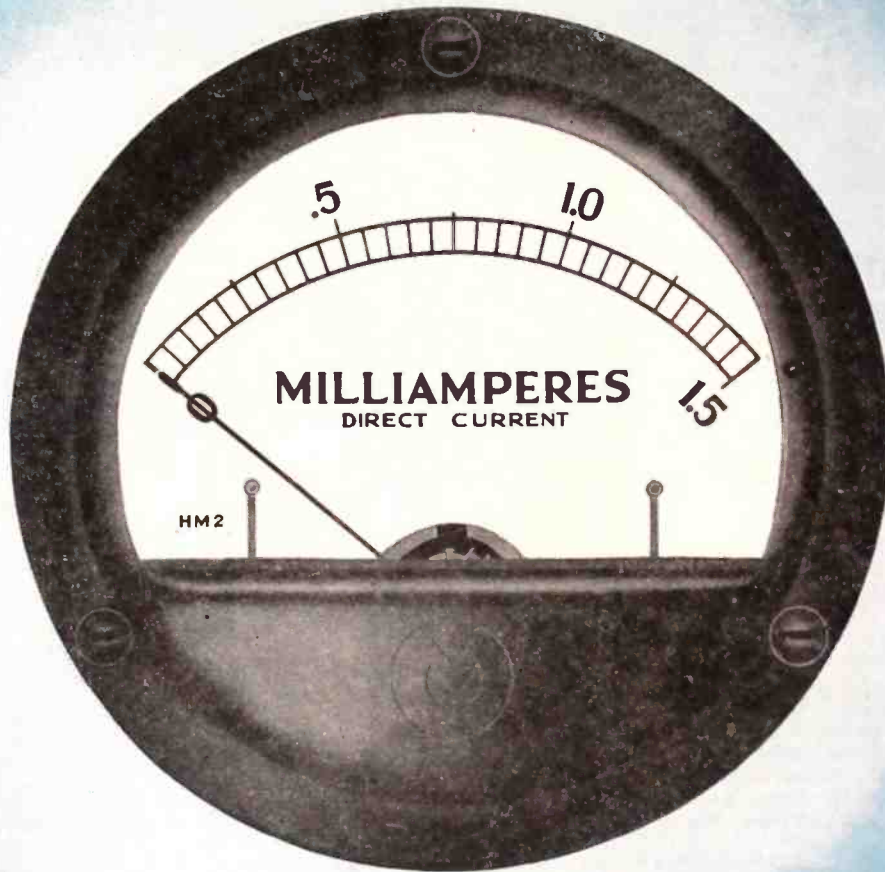
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cles which is around the highest  
 te normally reproduced, a difference  
 40 to 1. The 1-megohm shunt helps  
 e bass along but it has little effect on  
 e treble. As the resistance is de-  
 ceased, we note that the bass is in-  
 creased considerably while the treble  
 increased only slightly.

### Treble Booster

A treble-boosting tone control is  
 so included. More correctly, per-  
 aps, this control should be termed a  
 ss-reducing control as it shunts a  
 oke coil across the line which by-  
 sses the low frequencies but allows  
 ost of the highs to go by unmolested.  
 .002-mfd capacitor in series with  
 e choke makes the control non-  
 ear, particularly near the resonant  
 equency of the choke and capacitor.

### Hum and Decoupling Filter

A 2-megohm grid leak establishes  
 e input impedance of the amplifier  
 2 megohms for bass frequencies and  
 bit less than 2 megohms for the  
 reble. The 6C5 first audio is biased by  
 000 ohms and a 20-mfd capacitor.  
 ere we also have a separate R-C  
 um and decoupling filter. Coupling  
 p the power stage is completed by a  
 0,000-ohm plate resistor and a center-  
 apped grid choke. An equalizer, .02-  
 pfd and 7,500 ohms, is in series with  
 he blocking capacitor.

### External Speakers

Two output impedance taps, 1.12  
 nd 2.25 ohms, and an extra plug is  
 rovided for an external speaker. The  
 oice coils are arranged in parallel  
 with the fields in series, excitation be-  
 ng provided by the current in the  
 5L6 screens and 6C5 plate. A .002-  
 nfd 1,200-volt bypass capacitor is  
 onnected from plate to plate in the  
 output stage. The entire record player  
 draws an average of 134 watts from  
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 tation was made by Dr. W. R. G. Baker (left),  
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# I-F AMPLIFIERS

(Continued from page 20)

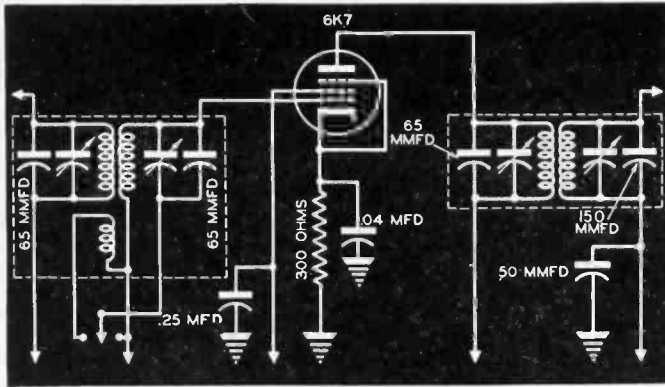


Fig. 7. The Wells-Gardner A-7 variable-width i-f transformer system. The tertiary winding provides tight coupling between primary and secondary, broadening the i-f response. The tertiary winding is shorted out for greater selectivity.

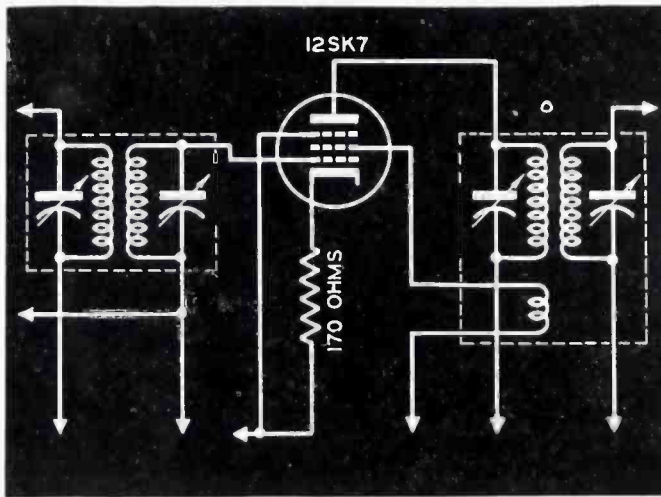


Fig. 8. I-f system of the Westinghouse M-104. The gain of this i-f system is increased by feedback, introduced into the circuit by coupling the screen grid of the i-f tube back into the detector transformer.

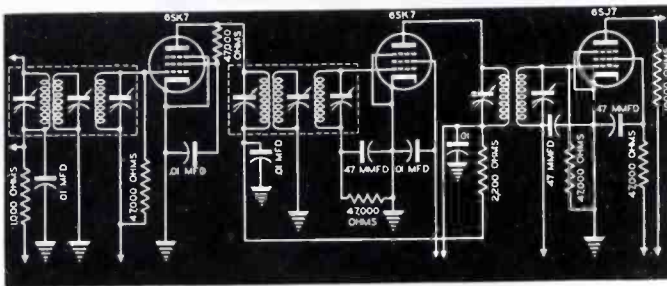


Fig. 9. The f-m i-f of the G.E. 60. Because of the high i-f frequency, and the broadband response, the gain of the i-f stage is reduced considerably. For this reason two i-f stages are usually necessary.

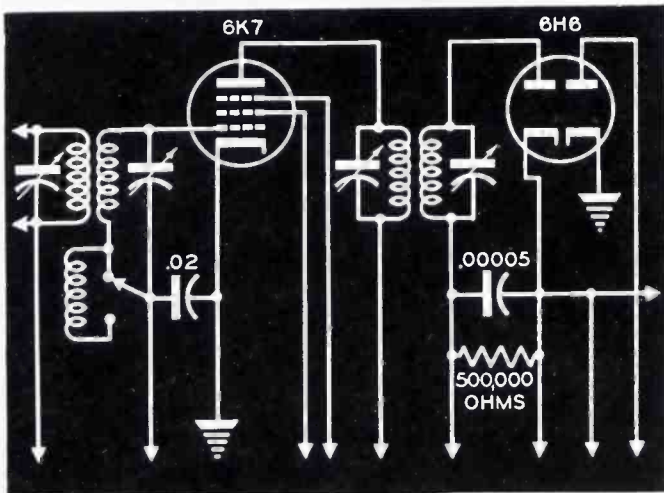


Fig. 10. The sharp-broad i-f system of the Ward 62-319. This circuit is similar to that shown in Fig. 7. A switch across a tertiary winding broadens or increases the frequency admittance of the i-f system.

adjustable, eliminating the need for trimmers. Silver mica fixed capacitors are used instead.

## Wells-Gardner A-7

Fig. 7, from a Wells-Gardner model A7, introduces another type of i-f with variable selectivity transformers. The input transformer from a 6J7 first detector has a tertiary winding which is connected in series with the secondary for wide-band reception. It is cut out of the circuit for sharp tuning, the trimmers being adjusted for the sharp position. The band is widened by virtue of the tight coupling provided by the tertiary.

Other methods of selectivity control in i-f amplifiers have included the insertion of resistance in the tank circuit, shunting of the primary or secondary with resistance, moving the coils mechanically and coupling variation by means of a variometer. Combinations of these systems have also been used.

In this model fixed silver-mica tuning capacitors are used in both primary and secondary circuits of both i-f transformers, the first three having a value of 65 mmfd, the detector capacitor, 50 mmfd.

## Westinghouse M-104, 204

It is often desirable to introduce regeneration into the i-f amplifier to increase gain or selectivity, or both. Westinghouse uses a method of screen-grid feedback in the detector transformer in models M-104 and 204, shown in Fig. 8. Improved performance is obtained without expensive transformers, but at the expense of critical tuning.

Other means of adding regeneration include removing the bypass from the screen grid and placing a small r-f choke in series with the screen. A 2 to 1 improvement in gain is often possible by such devices, enabling the Service Man to pep up a deficient receiver. If the amplifier tends to oscillate with the series choke, wire should be removed until stability returns.

## G. E. 60, 80

The broad band i-f channels of f-m sets preclude the possibility of obtaining high gain per stage, hence at least two stages are required. Also, the gain is not as high at 4.3 mc as at 455 kc, all other factors being equal. The high i-f is necessary, of course, to obtain a wide band simply. In Fig. 9 we have an f-m model of G. E., type 60/80, with a dual 6SK7 amplifier, the first two transformers being triple-tuned. The

(Continued on page 52)

# New!

## Series 200

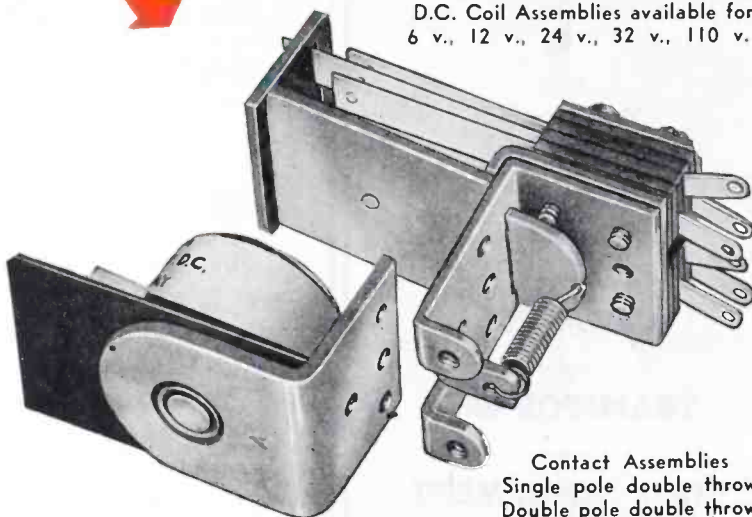
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# CRYSTAL FILTERS

(Continued from page 23)

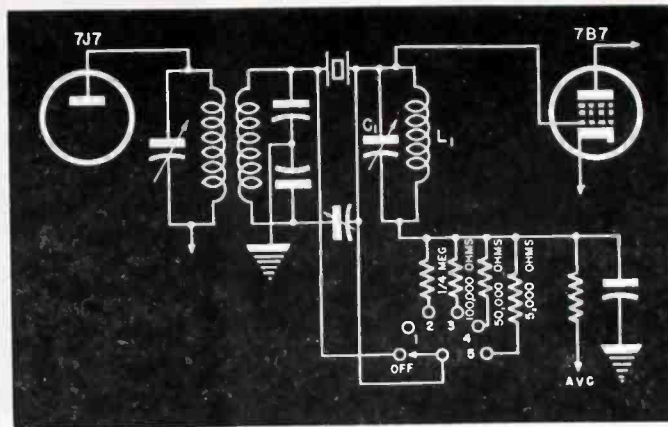
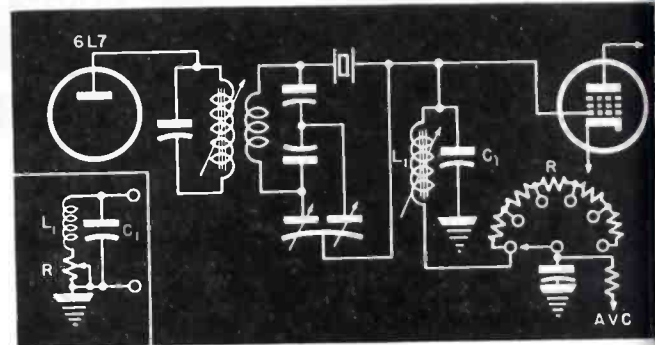


Fig. 5. The variable selectivity system of the RME 41-43. Variable selectivity is accomplished by varying the size of the resistor across  $L_1C_1$ , the larger the value of resistor the greater the selectivity.

Fig. 6. Hammarlund Super-Pro variable selectivity system. Here, the selectivity is varied by inserting resistance in series with  $L_1C_1$ . Increasing the value of resistance improves the selectivity by increasing the effectiveness of the crystal.



detunes the circuit, and permits the crystal to exert its greatest influence on circuit  $Q$ , or sharpness of resonance.

**RME 41-43**

Fig. 5 shows the variable-selective circuit used in the RME model 41-43. The tuned circuit here is on the crystal output side instead of the input. The effective resistance of the tuned circuit represented by  $C_1$  and  $L_1$  in series with the crystal is varied by shunting it with various size resistors, in very much the same manner as is used to broaden the response of i-f transformers used in f-m receivers. The lower the value of the shunting resistor, the greater will be the effectiveness of the

crystal and the resultant selectivity.

**Hammarlund Super-Pro**

In Fig. 6 we have the method applied in the Hammarlund Super-Pro. Here again, resistance is used to increase the effectiveness of a tuned circuit in series with a crystal filter. However, the resistance is used differently than for the circuit shown in Fig. 5. The  $Q$  of a coil is a function of its reactance over its resistance,  $Q = X/R$ . Since the resistance is introduced into the tuned circuit so that it is in series with  $L_1$ , and  $C_1$  is across both the resistance and the inductor, the effective resistance of the circuit as represented by  $L_1C_1R$  is reduced and  $C_1$  then acts as a bypass capacitor. Thus the effectiveness of the crystal is increased.

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# CENTERING CONES

(Continued from page 16)

lost. Every effort is made by the manufacturer to build his loudspeaker so it will stand up not only for normal operation, but that it has a safety factor which will permit some limited amount of abuse or abnormal operation without affecting the performance.

When confronted with a rubbing voice, the Service-Man can do one of two things.

First, he can replace the whole speaker with a new one and second, he can try to repair the one that is damaged.

In these days when production is so high and the demand so much, there is little chance in trying to replace the unit when the chances of getting a new speaker are slim indeed. Therefore, the Service-Man usually tries to repair it.

A new development, the *Adjust-A-Voice* unit, developed by Quam-Nichols, is an effective solution to the rubbing-voice-coil problem. In this unit, the voice coil, instead of being permanently attached or fastened to the housing, is kept in position with a pressure or clamping ring which is in turn held down by two clamping screws. This construction is illustrated at A in Figure 1, the inset showing a closeup of the pressure ring, which is underneath, at B, and the spider which is in turn held down by two clamping screws.

Loosening the screws holding the pressure ring (A in the illustration) will permit a small amount of movement of the spider in a lateral manner which will allow the voice-coil to be centered around the pole-piece and within the gap.

It is to be noted that the screws holding the clamping ring are so positioned that it will be often unnecessary for the Service-Man to remove the loudspeaker cabinet to re-center the voice coil.

In conditions of severe rubbing voice coils, a better job can be done by moving the speaker from the cabinet; when in either instance, no audio signal generator is necessary, and only the radio (or public address system) or voice signals are required for testing and maintenance.

The repair of a speaker with this new unit is quite simple. Before attempting to re-center the voice coil, one first determines on which side the voice coil is rubbing by pushing it up and down in the gap. Then it is necessary to loosen the clamping ring screw nearest the point of the rubbing is found. Using the screwdriver, the voice coil is gently pulled toward the loosened clamping screw. The screw is then tightened and a check made to see if the voice coil now rides freely.

Caution should be used at this time not to be too violent with the screwdriver because of the possibility of breaking the juncture of the voice coil and the cone neck.

If this operation does not correct the rubbing voice coil, another method will have to be employed. One must first remove the felt dust cap over the voice coil by saturating it with lacquer or thinner, allowing it to soak a few minutes before picking it off. Then strips of ordinary wrapping paper approximately 5/16" wide by 1 1/2" long should be cut.

The clamping ring screws should be loosened until the clamping ring is free, then the wrapping paper shims are inserted.

(Continued on page 52)



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.00001 to .001 mfd. 50 to 1000 mfd.

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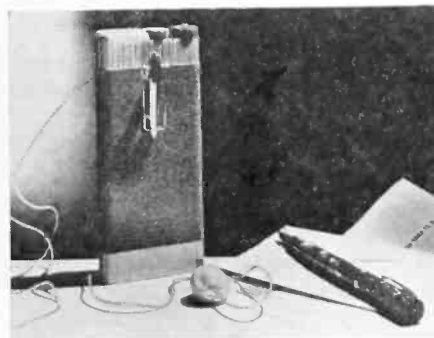
## C-R OSCILLOGRAPHS

(Continued from page 37)

form depending on the settings of the linear time-base oscillator controls. In any event, the characteristic sine wave form of the a-c supply frequency waveform is evident in the pattern.

Manipulation of the linear time base coarse and vernier sweep frequency controls permits the reduction of the pattern written on the screen to either a single a-c wave pattern, or to a pattern containing a number of similar a-c cycle forms, whichever may be desired. In either case, the pattern will appear to be in motion, and complete synchronization of the sweep frequency with that of the a-c supply source will be found difficult. If, however, the test signal terminal is connected to the linear time-base synchronizing voltage input terminal *EXT*, synchronization control selector switch, *S<sub>3</sub>*, turned to the *EXT* position, and the synchronization control potentiometer advanced slightly, the written wave pattern will stabilize completely. The wave pattern being written from the positive zero voltage inflection due to the phase-shift will be effected by the positioning capacitor *C<sub>23</sub>*.

## MINIATURE POCKET SETS



Five-tube pocket receivers produced by Belmont, using Raytheon sub-miniature tubes. Case is 3" wide, 1/4" thick and 6 1/4" high. Weighs 10 ounces, including batteries. Circuit is super-heterodyne. Cases will be supplied in solid gold, sterling silver, morocco, suede, etc.



## RECENTERING CONES

(Continued from page 51)

serted between the voice coil and pole-piece (the inside of the voice coil). The three strips are not used one on top of the other, but merely to assure that at least one thickness of the strip circumscribes the pole-piece entirely. The final step the clamping ring screw should be tightened a little at a time, tightening first one, then the other, gradually and alternately so as to bring clamping action to bear on the ring evenly all around.

This should result in a perfectly centered voice coil. The wrapping papers can then be removed, and the dust cap glued back on with lacquer cement.

## I-F AMPLIFIERS

(Continued from page 48)

third transformer which feeds the limiter stage is a conventional detuned job.

Ward 62-319, 329, 409, 419

Another receiver using sharp-tuning (i-f of 465 kc) is shown in Fig. 10, Ward 62-319, 329, 409, 419. The input transformer has a switchable tertiary winding similar to that shown in Fig. 7. The output transformer feeding the 6H6 detector is standard.

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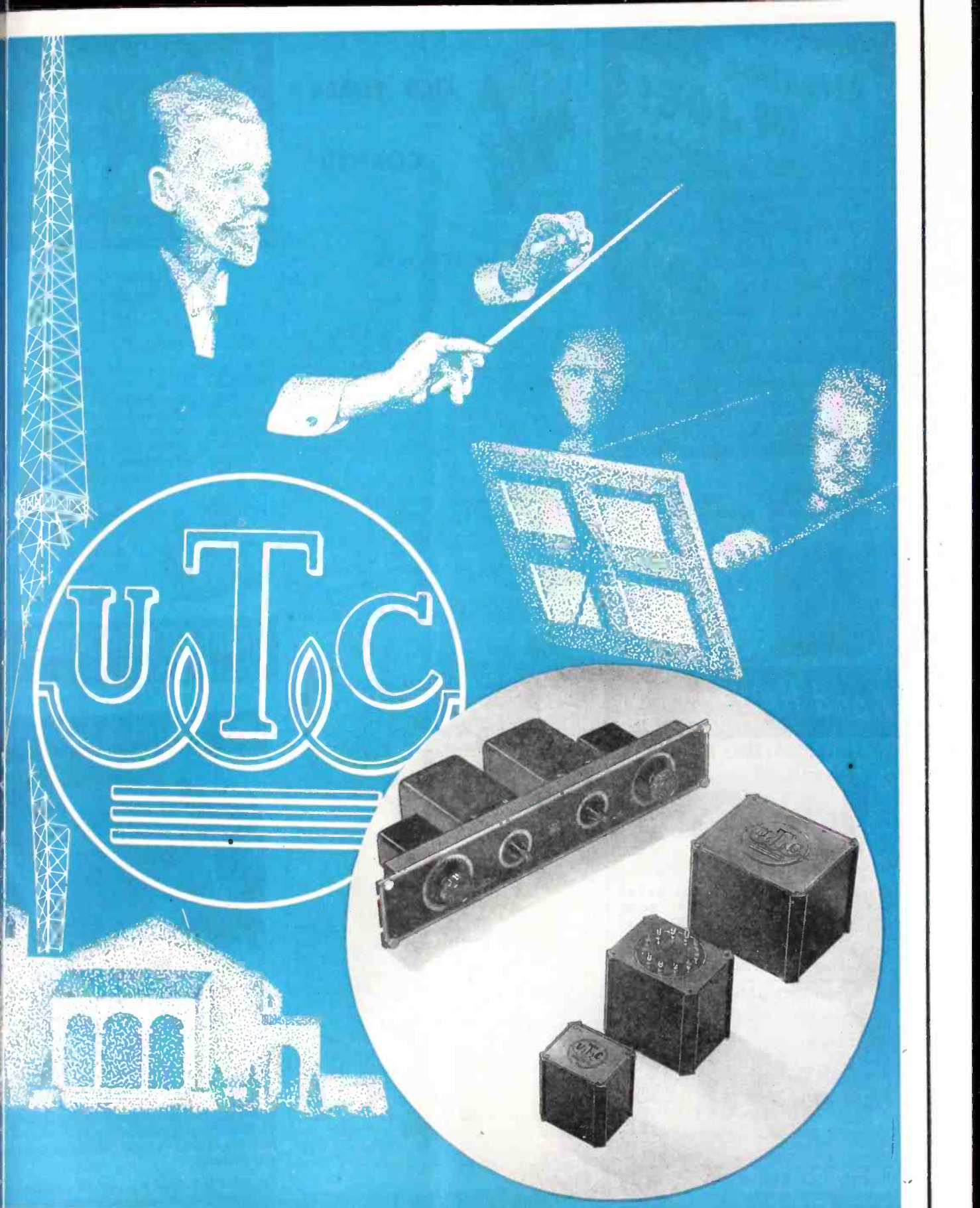
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## OLD TIMER'S CORNER

by **SERVICER**

WE had quite an unusual session at an end-of-the-day get-together some weeks ago, a session that provided many unusually interesting and useful facts.

It all began when Roy walked in quite pleased with himself.

"What's with you, Roy?" I asked. "You sure look spirited."

"Well, fellows," said Roy with a grin, "I have just made a swell contact."

"What kind?" we asked.

"With a manufacturer of capacitors," answered Roy. "With my plans I will be able to cut out everybody except the manufacturer. No more distributor, and no more company representative for me. I'll deal right with the capacitor maker, direct."

"What will that mean in dollars and cents?" we asked him.

"Well, I should be able to buy at better prices. Then deliveries will be faster, and also I'll have a wider choice than any of you have been able to get from John's Radio Company, the distributor up here. That in itself is worth the deal to me. But best of all I will be buying at rock-bottom, manufacturer's prices!"

"I think you're dead wrong, Roy," said Bill.

### Bill's Opinion

We picked up our ears. Bill was one of the older crowd who usually did not have anything much to say. He and his type just went ahead year in and year out, not making a very big splash in the waters of radio servicing business, but at the same time syphoning off a fair share of profits and keeping themselves high in the opinions of the community. Bill was not only conservative, but he was also highly respected for his ethics, business acumen and community pride. He was no world-winner, but his hard-headedness and carefully thought out plans often wrung a lot of silent (and sometimes not so silent) acclaim from our gang.

So when Bill fired his opinion at Roy, we were quite surprised.

"You see, boys, Roy thinks that he has made a world-winning deal by cutting out the distributor! Well, instead he has just done himself a great disservice! Sure, this particular manufacturer probably now has almost everything in stock that Roy could want. And he's anxious to get it out. So he'll do almost anything to see that Roy gets what he wants. But wait until this man-

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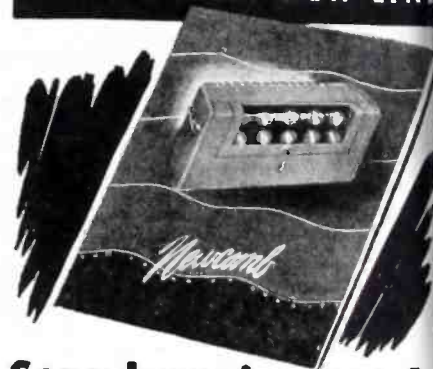
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Our newest amplifiers offer greater excellence in sound reproduction than ever before available to the public address field. Designed by an organization devoted exclusively for seven years to the perfection of sound equipment, they embody all the benefits of today's most advanced electronic achievements.

Send for the catalog . . . you'll find no other amplifier has so many advantages.

THE SOUND OF QUALITY

Newcomb

AUDIO PRODUCTS CO.  
MANUFACTURERS

DEPT. E. 2815 S. HILL STREET  
LOS ANGELES 7, CALIFORNIA



er—and I'm sure that he is not the old line men—gets going. He gave a big business some day. And he will recognize that it doesn't have Roy's orders lying for, say, ten 25-mfd 25-volt electro's, and two dozen .05 mfd's and a couple ten half mikes at 450 volts. He is to tell his production men to set aside until he gets into those runs for a set manufacturer. Thus of the capacitors Roy wants, will be only run through with the manufacturer. Now the .05 mfd's that are made for the set manufacturer are very different in size than the type ordered before, and so Roy gets the size which may or may not fit. Also price may be different each time, due to change in specifications.

#### Replacement Problems

and that isn't all. Suppose that Roy ordered some faulty capacitors. Can he get immediate replacements? No, not, for at that very time the type he ordered is out of stock, and another size is being run through, a size of no use to him.

So poor Roy will have to wait until the manufacturer runs through the kind Roy wants before he can get his replacements. Now since Roy has been dealing with the manufacturer directly, he not only has lost contact with the local distributor, but he has also encouraged that worthy to discontinue him. As a result, Roy can't get his capacitors from the distributor.

So he must go out and buy them himself, or hope that one of you—or me—will help him out for the time being. Normally, we would be more than willing to help out a fellow Service Man—especially Roy, because we all like to help. But business is business, and we don't like to have the returned capacitors be similar to those we gave Roy. We are not interested in the few cents that the capacitors cost. What we are interested in is some of Roy's units when his next shipment gets in. But Roy isn't going to receive the same standard parts we have been using, even when his shipment arrives. And we are not sure of exactly he is going to get. So we won't let him have any of ours, and he will find himself in quite a spot!

#### Virtues of Distributors

Now, if Roy trades with the local distributor he'll get what he needs right from the distributor's stock. The distributor pools all of his orders and sends them in to his standard manufacturers as they make, taking in all the Service Men accounts of the distributor, and order and quite a run. If something goes bad with the units, the manufacturer cannot afford to ignore the distributor, and so he makes it good. The distributor knows that and will replace defective units for Roy on sight. Then, the distributor is a local man. Every time Roy buys from him and pays his bill promptly, he establishes a better relationship. That may come in handy when time rolls around and Roy needs a reference. Some of the boys just think much of references from an out-of-the-state place where people don't know each other except via the postage stamp route.

# 33 well overlapped ranges . . . .

## plus long-life dependability!



## WESTON

(Model 665 Type 1)

### VOLT-OHM-MILLIAMMETER

Its compactness, versatility and rugged dependability make Model 665 the ideal instrument for use in the field, or in the shop . . . whether servicing communications equipment, testing electrical components in production, or research or maintenance work. Provides 33 AC and DC voltage, DC current, and resistance ranges . . . with simplified switching arrangement for rapid operation. Built to WESTON standards to assure dependable measurement accuracy throughout the years. Full details on request. Weston Electrical Instrument Corporation, 605 Frelinghuysen Avenue, Newark 5, N. J.

## WESTON Instruments

"So if you want some sound advice, play ball with your local distributor. The prices may seem a bit higher than those a manufacturer selling direct may offer. But when the smoke clears away, you are getting so very much more for your dollar in the form of reputation, good will and fine service, that in reality the costs are cheaper."

#### No Sale

"I think you have something there, Bill," said Roy. And from the way he spoke, I guess that a certain manufacturer, who sells capacitors directly to the radio Service Man, had just lost a fairly nice account.

#### POSTWAR RECEIVER



Receiver of the future shown at a recent postwar display by the Hallicrafters, Chicago.





## Plug in METAL TUBE RESISTORS

★ To facilitate the servicing of AC-DC sets equipped with plug-in metal-tube resistors, Clarostat offers 10 Universal Types which replace 90% or better of the original numbers.

The Clarostat Universal Type operates within voltage ranges specified on tube, regardless of what pilot current is drawn or of any pilot light combination. Operates regardless of burnt-out pilot lights, and well within the .3 ampere range required for tube filaments. Operates efficiently regardless of line-voltage variation.

### ★ Ask Your Jobber . . .

Ask for these Clarostat plug-in metal tube resistors. Type MT. Ask for other servicing aids—controls, resistors, attenuators, etc. Ask for latest catalog—or write us direct.



CLAROSTAT MFG. CO., Inc. • 285-7 N. 6th St., Brooklyn, N. Y.



### RAYTHEON BONDED SERVICE MAN PROGRAM

A Bonded Electronic Technician Program to improve standards of practice among Service Men and provide work guarantees, has been announced by the Raytheon Manufacturing Company. The program provides for the bonding of Service Men through the facilities of Raytheon distributors, Raytheon and a bonding group.

According to Arthur E. Akeroyd, distributor sales manager, the program will assist the Service Man in building a solid foundation for postwar activities.

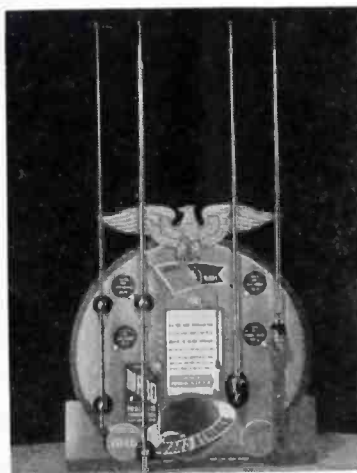
It will offer deserving newcomers such as returning veterans, the opportunity to establish themselves in business, without being handicapped by the questionable practices of some widely publicized repairmen.

Mr. Akeroyd said that it was felt that the plan should be based on guarantees to the much maligned Service Man as well as the customer. Every radio shop is entitled to a legitimate profit, he said. Thus with widely divergent costs under different conditions and in different locations, any bonding program must not interfere with the established business policies of the ethical shop. By the same token, the program must also recognize the fact that the majority of Service Men are honest. The bond provided by this program will assure the public of the Service Man's honesty and integrity, said Mr. Akeroyd.

To qualify as a Raytheon Bonded Electronic Technician, a Service Man will have to meet certain qualifications of experience, reputation and ability, and also state that he has and will use adequate equipment to do skilled service work efficiently.

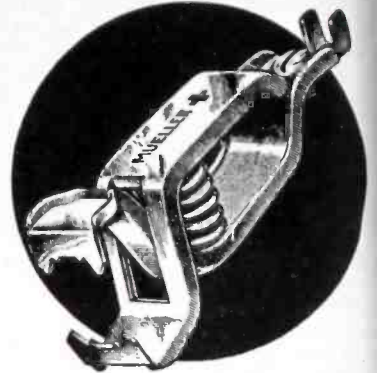
The Service Man's application will have to be approved by his Raytheon distributor, Raytheon and the bonding company. When accepted by all parties, he will become bonded for the period of one year by the Western National Indemnity Company of the Firemen's Fund Group. The bond states that the Service Man agrees to guarantee complete satisfaction

### POSTWAR ANTENNAS



Ward store display featuring four postwar antennas. Highlights of the antennas are said to be H-Q low-loss detachable polyethylene lead with silver-to-silver contact; one man installation and fluid type anti-rattle construction.

## MUELLER



## CLIPS

For Quick Temporary Connections

- Made in 10 sizes—from the tiny wee-pee-wee to the 300 ampere Big Brute.
- Offered in both steel and solid copper.
- Red and black rubber insulators to fit each size.
- A complete line with

A CLIP FOR EVERY PURPOSE

Send for free samples and catalog 810

*Mueller Electric Co.*

1565 E. 31st St. - Cleveland, Ohio

## MONEY-SAVING SPECIALS

Immediate Delivery. Orders filled same day received.



AIRPLANE  
CODE KEY  
\$2.25

Knee type. Strong spring holds securely. Black enamel and brass finish. Complete with plug and cord. Limited supply. Order now. Only—\$2.25

DESK TYPE KEY—\$1.69

Cadmium plated. A good practice key for amateurs.



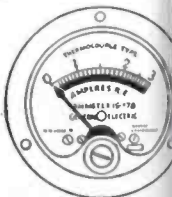
PL-55 PLUG—34¢

A high grade, dependable plug.

### G. E. AMMETER

General Electric Thermocouple R.F. type—only \$4.95.

NEW ITEMS DAILY  
Tubes . . . test equipment  
. . . meters . . . cords and  
cables . . . condensers . . .  
resistors . . . switches . . .  
speakers.



Write for bulletin listing hundreds of items

## Lifetime

SOUND EQUIP. CO., Dept. 65

911-913 JEFFERSON AVE., TOLEDO 2, OHIO



every radio repair job for 90 days, outlines a code of ethics that he expects to observe in the conduct of his business.

Mr. Akeroyd said that the requirements for certification have been drawn up so that they parallel the now generally accepted practices and standards of the competent qualified Service Man. The requirements do not represent the ideas of any single group, but rather the suggestions and opinions of hundreds of Service Men. Adequate provision is said to be provided to prevent the exclusion of any Service Men from this program, without prejudice, in the event that they feel rejection is not justified.



A. E. Akeroyd

**GRENBY BUYS CARDWELL**

Grenby Mfg. Co., Plainville, Conn., has acquired full control of The Allen Cardwell Mfg. Corp., Brooklyn, N. Y.

W. L. Gray, president of Grenby, has become chairman of the Cardwell board. He will handle the sales and development engineering departments of Cardwell while the manufacturing departments of Cardwell will continue to operate from their present location at 81 Prospect St. The manufacturing division has been moved to Plainville, Conn.

John H. Soby, vice president and director of Grenby, has been elected president of Cardwell, following the retirement of Mr. Cardwell. Joseph K. Fabel will continue to serve as vice president and sales manager of the Cardwell development and engineering division. Ray Brehouse will also continue as Cardwell sales manager.



C. A. Gray

**CAPACITOR COLOR CODE CARDS**

Color code charts and cards for small capacitors with RMA six-dot color code and three-dot color code as well as Army-Navy standards, have been prepared. (Continued on page 58)

**N. U. DISTRIBUTOR ON RANCH**



Olsen, National Union distributor in Antonio, with Jack Clune, N.U. sales manager, on the Olsen ranch.

# Wait for these new

# HICKOK

## Radio Service Instruments



Model 532  
Tube Tester

*If It Isn't A Hickok Indicating  
Micromhos It's Not  
Dynamic Mutual Conductance*

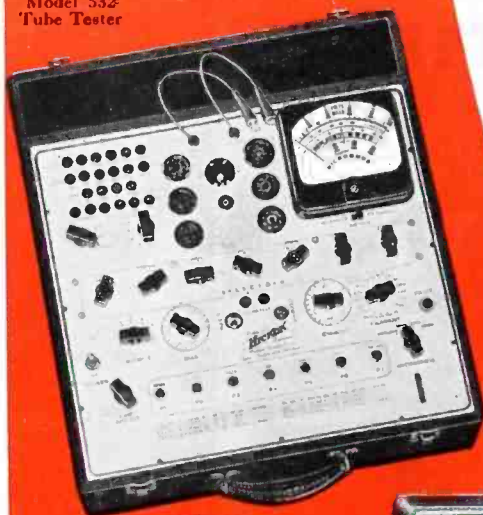
Your patience in waiting for these new 1916 HICKOK models will be richly rewarded for these new HICKOK tube and set testers make still closer tests, with finer accuracy, rejecting tubes that might get by with an ordinary tester.

Now you have 7 selector switches instead of 2. That aims to prevent obsolescence. Isn't that worth waiting for?

What's more, Dynamic Mutual Conductance, indicated in Micromhos, is a duplicate of the manufacturer's method of checking when he makes the tubes. Remember, if it isn't a HICKOK Indicating Micromhos, it isn't Dynamic Mutual Conductance.

The new Electronic Volt-Ohm-Capacity Milliammeter Model 203 reads as low as 1.0 mmf and up. It will measure at frequencies to over 10 mc with no frequency error and the ohm meter will measure up to 10,000 megohms.

Keep patiently in touch with your jobber and you will soon get the instruments that are held in highest esteem.



Model 534  
All Purpose Tube and Set Tester

**THE HICKOK  
ELECTRICAL  
INSTRUMENT CO.**

10521 Dupont Avenue  
Cleveland 8, Ohio



Model 203  
Electronic Volt-Ohm-Capacity Milliammeter



# NEW SOLDERING GUN

THE SPEED IRON\*



## Soldering Heat in 5 Seconds

Wherever you have a soldered joint in radio, electrical or electronic repair and service work, the Speed Iron will do the job faster and better.

The transformer principle gives high heat—in 5 seconds—after you press the trigger switch. Convenient to hold with a pistol grip handle, the compact dimensions of this new soldering tool permit you to get close to the

\*T.M. Reg. U. S. Pat. Off.

joint. The copper loop soldering tip permits working in tight spots. The heat is produced by the high current flowing through the soldering tip—permitting direct and fast transfer to the soldered connection.

If you want to save time on soldering jobs with a tool that is ready to use in 5 seconds, get a Speed Iron today. See your radio parts distributor or write direct.

**WELLER MFG. CO.**  
DEPT. S-1 • EASTON, PA.



## UNIMETER

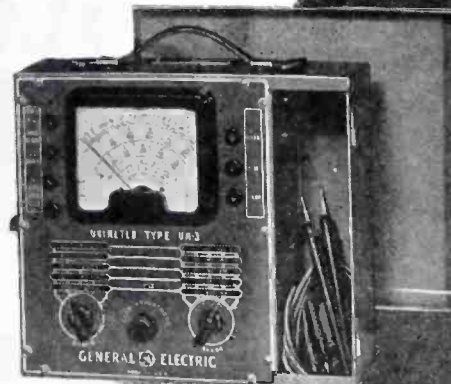
This unit fulfills an extremely important need for general utility portable service equipment. It has wide range coverage for both a-c and d-c measurements of voltage, current measurements on d-c and the popular ranges on resistance.

The UM-3 is designed to clearly indicate all the functions which aid in the prevention of application of high voltages when preparing for current or resistance measurements.

Other G-E units for better servicing include: Tube Checker TC-3, Unimeter UM-4, and Oscilloscope CRO-3A.

For details write: *Electronics Department, Specialty Division, General Electric, Syracuse, New York.*

*Electronic Measuring Instruments*



**GENERAL ELECTRIC** **UM-3**

## NEWS

(Continued from page 57)

pared by Cornell-Dubilier Electric Corporation, New Bedford, Mass.

The basis of the code is the use of distinct color for every number from zero to nine inclusive.

### TECHNICAL APPLIANCE CONSOLIDATED PLANTS

Technical Appliance Corporation consolidated its wartime New York City and Flushing plants and will hereafter be located at 41-06 DeLong Street, Flushing, N. Y.

The postwar Taco line will include antenna systems and kits for broadcast reception and also for f-m and television purposes.

### RADIONIC EQUIPMENT CATALOG

A 32-page catalog listing components, test instruments, sound equipment and accessories, and technical books, has been released by the Radionic Equipment Company, 170 Nassau Street, New York, N. Y.

### NEWS OF THE REPRESENTATIVE

John B. Tubergen, 1406 S. Grand Ave., Los Angeles 15, and Joe W. Marsh, 1100 West Pica Blvd., Los Angeles 15, have become members of the Los Angeles chapter. Jerry W. Miller, 5917 S. Normandie St., Los Angeles 3, Cal., has become an associate member of the Los Angeles chapter.

T. M. Graner, 600 Camelia St., Berkeley, is now a California chapter member.

O. N. Jones, 1085 The Arcade, Cleveland 14, O., is now a member of the Buckeye chapter.

At a recent meeting of the Wolverine chapter, H. E. Walton was elected president; J. C. P. Davenport, vice president; and Robert Milsk, secretary-treasurer.

The Hoosier chapter elected Leslie DeVoe president; Chuck Southern, president; Bruce McPherson, treasurer; and Bud M. W. Fisch, secretary.

Martin Friedman, a member of the Mid-Lantic chapter has moved to the Real Estate Trust Bldg., Philadelphia, Pa.

### H. E. HARRIS PROMOTED BY BELL SOUND

Harry E. Harris, formerly sales engineer of the Bell Sound Systems, Columbus, Ohio, has been appointed general sales manager of the manufacturing and jobbers sales division.

### CANNON CONNECTOR BULLETIN

A revised 64-page edition of the Cannon Electric K bulletin on electric connectors has been released by Cannon.

### AT EASTERN AMPLIFIER "E" CEREMONIES



Left to right, Lt. Col. Harold L. Lister, Comdr. William J. Warburton, Harry Friedman and Leonard Meyerson of Eastern Amp Corp., and Major Meredith J. Roberts



Development Company, 3209  
 1st St., Los Angeles 31, California.  
 This publication contains data on receptacles,  
 taps, junction shells, stowage re-  
 ceptacles for instruments, radio, motors,  
 and general electrical applications.

**TRANSFORMER BROCHURE**

A 18-page brochure, *Engineering a Transformer*, covering lamination size, degage and magnetic performance; size, type and gage; winding details; transformer-reactor physical and electrical aspects; electrical-mechanical considerations of core laminations; im-  
 position, assembling and casing; and  
 and sealing, has been released by  
 Transformer Corporation, Chi-  
 cago, Ill.



**LABORATORY REPLACEMENT VIBRATOR GUIDE**

A 16-page replacement vibrator guide  
 replacement listings for auto radio  
 battery-operated household receiv-  
 er circuit diagrams, installation  
 cross references of vibrators and  
 connections, buffer capacitor reference  
 list, and notes on an assortment of

**FREE TO YOU**

**COLOR CODE  
 OHMS LAW CALCULATOR**

**Great Time Saver**  
 Burstein-Applebee of Kansas  
 City offers you this great con-  
 venience FREE. Easy to work.  
 Solves many problems in a jiffy.  
 FREE to Radio men, electronic  
 engineers and others in the  
 business. Attach coupon to  
 your letterhead.

**MAIL COUPON NOW**

**BURSTEIN-APPLEBEE CO.**  
 22 MCGEE ST.  
 KANSAS CITY 6, MO.

Send me FREE Color Code and Ohms Law Cal-  
 culator along with latest catalog.

NAME \_\_\_\_\_  
 ADDRESS \_\_\_\_\_  
 CITY \_\_\_\_\_ STATE \_\_\_\_\_

vibrators, has been published by P. R.  
 Mallory & Co., Inc., Indianapolis 6, Indi-  
 ana.

**CAMBURN TO PRODUCE AUTO/FM/  
 TELEVISION ANTENNAS**

A variety of antennas for auto sets,  
 and f-m, television and marine receivers  
 will be included in the postwar line of  
 the Camburn Products Company, 490  
 Broome Street, New York 13, N. Y.

A new plant will be built on Long  
 Island to produce the new postwar items.  
 M. B. Bernstein is president of Camburn  
 Products Co.

**BROWNING JOINS NORMAN B. NEELY**

Robert Browning has been appointed  
 special field engineer for Norman B.  
 Neely Enterprises, Hollywood, California.  
 Mr. Browning was formerly with  
 Western Electric as a radar field engi-  
 neer.

**PLYTUBE F-M MAST KIT**

A plytube antenna kit for f-m and  
 television has been announced by the  
 Plymold Corporation, Lawrence, Massa-  
 chusetts.

The mast is supplied with fittings for  
 attachment atop a roof or side of a build-  
 ing. Mast, antenna system, and all fit-  
 tings are offered as a unit.

**JACK BEEBE JOINS SWAIN NELSON**

Jack Beebe has joined the transformer  
 division of the Swain Nelson Company,  
 Glenview, Illinois, and will be in charge  
 of manufacturing and distributing of  
 S-N-C transformers. Mr. Beebe was  
 formerly general sales manager of the  
 Thordarson Electric Manufacturing Com-  
 pany.



**MUELLER INCREASES PLANT  
 FACILITIES**

A postwar plant expansion program  
 has been announced by the Mueller Elec-  
 tric Co., Cleveland.

The first step in this program pro-  
 vides for the installation of new plating  
 and finishing facilities.

**BURGESS BATTERY REPLACEMENT  
 GUIDE**

A guide listing replacement batteries  
 for approximately 1,000 models of port-  
 ables and farm type receivers has been  
 prepared by the Burgess Battery Com-  
 pany, Freeport, Ill. Included also are  
 a list of private brand portables. Also

(Continued on page 60)

**HEAVY-DUTY  
 Electrolytics**

• Now that V-J Day has come and  
 gone, those heavy-duty metal-can  
 electrolytics are once again be-  
 coming available for civilian use.  
 Once again the Aerovox electro-  
 lytic line is providing that outstand-  
 ing choice of types for the better  
 jobs you are out to do, in this post-  
 war radio and electronic world.

For your very best maintenance  
 work where equipment must be  
 kept going day in and day out;  
 for those power packs that have  
 to keep delivering properly filtered  
 voltages hour after hour; for those  
 radio sets that "must stay put" —  
 you can depend on these Aerovox  
 metal-can heavy-duty electrolytics.

**• Ask Our Jobber...**

Ask him about the Aerovox heavy-duty elec-  
 trolytics that are now starting to come through  
 for civilian use. Ask about the other types in  
 the outstanding choice of Aerovox capacitors.  
 Ask for a catalog—or write us direct.

**AEROVOX  
 Capacitors**

INDIVIDUALLY TESTED

AEROVOX CORP., NEW BEDFORD, MASS., U. S. A.  
 In Canada: AEROVOX CANADA LTD., HAMILTON, ONT.  
 Export: 13 E, 40 St., New York 16, N. Y. Cable: 'ARLAB'





# PHONO - RADIO MATCHING UNIT

**BOON FOR SERVICERS!** A time-saver and moneymaker that just had to come . . . fruit of ADAPTOL initiative and research, supported by technical help from your own profession.

**HOW SIMPLE!** Without removing anything from either housing . . . without even breaking a circuit . . . you can install this long-wanted convenience wherever there is a radio to be utilized for reproducing record entertainment!

**THINK OF THE** technical data you DO NOT have to wade through! And the time you can save! And the satisfaction for your customers, while you are making a nice profit and adding to your professional prestige!

ANY  
RECORD  
PLAYER

ADAPTOL  
supplies the  
MISSING LINK

write  
QUICK  
for the  
WHOLE STORY

ANY  
RADIO

**ADAPTOL COMPANY**  
260 Utica Avenue, Brooklyn 13, New York



## Antennas

**FIRST CHOICE . . .  
OF AMERICA'S RADIO DEALERS**

Radio dealers, too, recognize the factors that long ago made Ward Antennas most popular with auto manufacturers and dealers. They see the top quality, precision workmanship, and now the new war-created designs that make Ward better than ever! The world's finest antennas for car and home were made, are made, and will continue to be made by Ward. Place your order for Ward Antennas now!



BUY VICTORY BONDS  
**THE WARD PRODUCTS CORPORATION**  
1523 EAST 45th STREET - CLEVELAND 3, OHIO

## NEWS

(Continued from page 59)

presented is a numerical and alphabetic listing of all Burgess Battery products. Free copies of the guide are available from department RG.

\* \* \*

### JENKINS JOINS FORSHAY

Victor E. Jenkins, formerly test equipment sales manager for the Weston Electrical Instrument Corp., has joined Joe M. Forshay, 27 Park Place, N. Y., N. Y., factory representative in New York City and New Jersey for Simple Electric Company and Industrial Condenser Corporation.

\* \* \*

### COLEMAN NOW ASST. DIRECTOR RCA VICTOR ENGINEERING DIV.

J. B. Coleman has been named assistant director of engineering for the RCA Victor division. M. C. Batsel has been chief engineer of engineering products. Mr. Coleman will make his headquarters at the company's home office Camden, N. J.

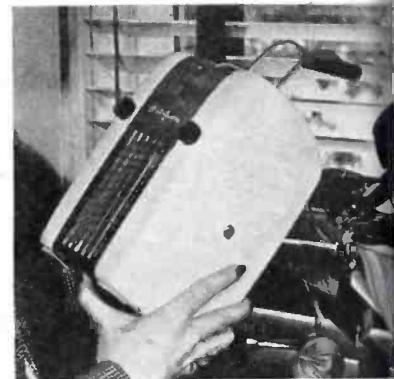
Previous to his new assignment, Batsel was chief engineer at the RCA Victor plant in Indianapolis, Ind.

\* \* \*

### COMMUNICATIONS PARTS MOVES NEW PLANT

Communication Parts has moved to 1101 North Paulina Street, Chicago.

## POSTWAR RECEIVERS



Portable and phono-table postwar models Westinghouse. Unit, above, can be mounted wall or set up on flat surface. Combination, below, can be operated as a phono-receiver or with separate units, it being possible to remove receiver and using as a straight table model.



## VOLUME AND TONE CONTROLS

(Continued from page 30)

in practically all the necessary resistance values and tapers in the wide range of resistance wherein the type may be used, the Service Man should make it a policy, when confronted with the replacing of controls of either type, to replace an original wire-wound control with a similar wire-wound control, and an original carbon type control with a similar carbon type control whenever possible to do so. By adhering to this policy, customer dissatisfaction will be avoided in most cases.

The circuit design of many receivers recently includes special considerations which make it necessary for proper operation to replace the volume control with one of the same type. There are many receivers (especially older models) in which the use of a wire-wound control is definitely indicated, and where the carbon type will not give satisfactory service. Wire-wound units are frequently used in control circuits which require a comparatively high circuit-carrying capacity. Compact, low-resistance controls of this type can be made to handle greater currents than a carbon control. They are also used in critical circuits where it is necessary to have a higher degree of resistance permanence, or much closer resistance tolerance, than is possible with the carbon type.

There are certain conditions where

it might be desirable or even necessary to change the type of control; i. e., use a carbon control having the proper resistance value, taper and wattage rating to replace an original wire-wound control or vice versa. This is a matter of discretion for the Service Man. Unless it cannot be avoided, the exchange should not be made unless the advantages to be gained are not offset by the disadvantages of the particular type control. Quite often this can be correctly ascertained only by trial and error.

### Midget Versus Large Size Controls

In some receivers, particularly in off brand or a few trade name receivers in which small midget-type volume controls are used in current-carrying circuits of the antenna-bias type, repeated volume-control trouble due to the overheating may be experienced. If the original midget control is damaged or burned out and a check reveals that the failure is due to excessive current in the control, the defective unit should be replaced with one of the larger type controls if there is space available.

On the other hand, a midget type may be used to replace a large type control in an audio type of control circuit whenever this procedure tends to simplify a crowded installation.

(To Be Continued)

## NEW PRODUCTS

### NE-O-LITE TESTER

Best unit, Ne-O-Lite Test-Lite, for testing a-c lines, checking polarity of a-c or d-c, and tracing ground lines, has been announced by the Ne-O-Lite Mfg. Co., Rockford, Illinois. Tests voltage from 60 volts a-c to 550 volts a-c or d-c by variable light intensity. Has a neon lamp. Has a clear plastic shell and insulated test points.

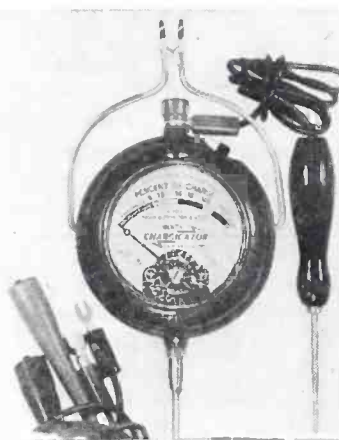


### HICKOK CHARGICATOR

Chargicator to indicate electrically equivalent gravity of any lead-acid battery, regardless of size or voltage has been developed by the Hickok Electrical Instrument Company, 10521 East Avenue, Cleveland 8, Ohio.

Probe type, illustrated, gives instantaneous measurement of battery condition. It shows what charging rate to use, either for trickle charging or for an efficient, safe, high-rate charge. It indicates the percentage of charge and charging danger and warns of destructive overcharging.

Has a four-color scale dial. All models are sealed in molded acid-proof bakelite cases.



### RADIART MIDGET VIBRATORS

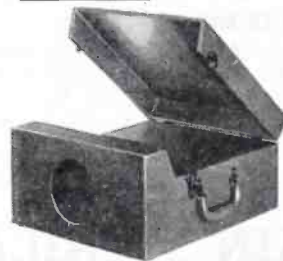
Midget vibrators, type VR-2, 2 1/8" high x 1 1/8" in diameter, have been announced (Continued on page 62)

# LAKE

has a better selection of  
**RADIO**  
Parts, Cabinets  
and Equipment!



Portable Phonograph Case of sturdy durable plywood, in handsome brown leatherette finish. Inside dimensions 16 1/2" long, 14" wide, 9 1/2" high. Has blank motor board. As illustrated above, specially priced at **\$6.95**



Portable Phonograph Case in brown leatherette covering. Inside dimensions 17 1/2" long, 13" wide, 7 1/2" high. Has blank motor board and opening for speaker. As illustrated at left, specially priced at

**\$7.95**

### SOUND EQUIPMENT

Complete line of amplifiers, microphones, speakers and sound accessories. WRITE TODAY!

Also blank table cabinets of walnut veneer in the following sizes, with speaker opening on left front side:

(Note: \*7 has center speaker grill.)

#1	8 1/4"	L x	5 1/2"	H x	4"	D	\$1.95
#2	10 1/4"	L x	6 3/8"	H x	5"	D	\$2.75
#3	13 1/2"	L x	7 7/8"	H x	6 1/4"	D	\$3.25
#7*	10 3/4"	L x	7"	H x	5 1/2"	D	\$2.50
#8	17 1/4"	L x	9"	H x	9 1/2"	D	\$4.50
#9	21"	L x	9 1/4"	H x	10 1/2"	D	\$5.50

\*Speaker Opening in center of front side. Cabinets available in ivory color and Swedish Modern. Write for prices.

### POWER TRANSFORMERS

4, 5, or 6 Tube—6.3 V at 2 amp	\$1.49
50 Mill Power Transformer.....	
7, 8 or 9 Tube—6.3 V at 3 an	\$1.89
70 Mill Power Transformer.....	



All types of radio cabinets, equipment and parts are available at Lake's lower prices. A large stock is listed in our catalog.

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Vibrator frequency, 185 cps  $\pm 10\%$ ; input voltage (nominal), 6.0; input voltage range, 4.5 to 7.5; input current, 1.5 amperes maximum at 6.0 v; output voltage, 200 d-c maximum; and potential difference between primary reed and secondary reed, 25 v maximum.



**INSULINE MIDGET JACKS**

A series of midget-sized jacks has been developed by the Insuline Corporation of America, Long Island City, N. Y. Models include single closed-circuit,

**NEW PRODUCTS**

(Continued from page 61)

single open-circuit, and three-way microphone types. Jacks have a tooled-brass body with phosphor-bronze spring members, nickel plated.

**SHALLCROSS AXIAL LEAD RESISTORS**

Fixed wirewound axial lead 1-megohm, 1-watt resistors have been announced by the Shallcross Manufacturing Co., Jackson & Pusey Avenues, Collingdale, Pa. Known as Akra-Ohm type 188, the resistors are 1 3/16" long x 3/8" diameter. Axial leads, 3" long, of No. 20 tinned copper wire. Standard tolerance is said to be  $\pm 1\%$ .



**WESTON DIRECT-READING INSULATION TESTER**

A direct-reading insulation measuring device, model 799, providing a single range for .1 to 10,000 megohms with the 10,000 mark at 8% of the scale length, has been announced by Weston Electrical Instrument Corporation, 617 Frelinghuysen

sen Avenue, Newark 5, New Jersey.

The circuit is said to have a test potential of less than 50 volts d-c. Its use includes checking leakage between windings in transformers, leakage of low-voltage paper and mica condensers, etc. Size 5 3/8" x 3 1/4" x 4 7/8".



**REINER VACUUM-TUBE VOLTMETER**

A vacuum-tube voltmeter, 451, amplifier, 101, featuring 25 millivolts on the lowest range, 1,000 volts on the highest range, 10 cps to 700 mc frequency range, and 7 mmfd input capacity has been announced by Reiner Electronic Co., Inc., 152 West 25th Street, New York 1, N. Y.

Model 451 ranges are: a-c volts, 0-.02-.1-25. (with amplifier)-2.5-10-25-100-250-1,000; d-c volts, 0-2.5-10-25-100-250-1,000; d-c current, 0-2.5-10-25-100-250-1,000; ohms; 1 ohm to 1,000 megohms.

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frequency range, 10 to 5,000 cps, amplifier) 50 cps to 700 mc. D-c ohm and current accuracy is said to be 2% on full scale. A-c volt accuracy to be 2%, 50 cps to 50 mc; entire frequency range 5% accuracy. Weight, 20 lbs. Size, 10 3/4" x 9" x 8".



**OHMITE PIE-WOUND RESISTORS**

A series of pie-wound resistors, Rite-types 844A/844B/842A, that can be mounted by means of a through-bolt, has been announced by the Ohmite Manufacturing Company, 4835 Flournoy St., Chicago 44, Ill. Available in 3 sizes: 9/16" diameter x 1/2" long, 9/16" diameter by 7/8" long,

and 3/4" diameter x 1 3/16" long. The smallest is a 2 pie while the other two are 4-pie units. The minimum resistance is 1 ohm for the 2-pie unit and small 4-pie unit, and .10 ohm for the large 4-pie unit. The maximum resistance is 200,000 ohms for the 2-pie, 400,000 ohms for the small 4-pie, and 1.5 megohms for the large 4-pie unit.

Uses enameled alloy resistance wire non-inductively pie-wound on a non-hydroscopic ceramic bobbin.



**CARTER MOTOR FREQUENCY-CONTROLLED D-C TO A-C CONVERTER**

A frequency-controlled d-c to a-c rotary converter has been announced by Carter Motor Company, 1608 Milwaukee Avenue, Chicago, Illinois.

Designed with the frequency control in the base, including a vibration reed-type meter to visually indicate the frequency of the output.

In the 110-120 volt d-c to 117-volt a-c models, the output control is said to be within ± 10 volts at 60 cycles, over a ± 10-volt d-c fluctuation.

Models can be supplied with input voltages ranging from 6 through 64 volts for battery conversion and also 110-120 volts d-c for line conversion. Wattage ranges are from 40 through 250, continuous duty.



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**JOYS AND FLASHES**

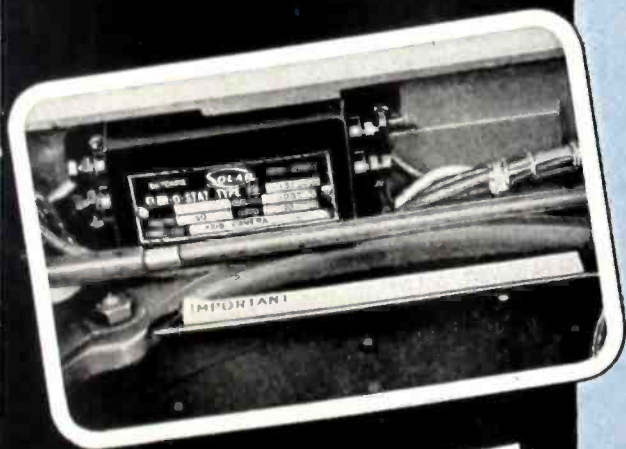
OVER 10,000,000 f-m sets will be sold during the next two or three years, according to Frank Mansfield, director of sales research of Sylvania, who based his data on a survey recently completed. . . . Irving P. Wolfe has become a distributor and opened a store at 224 Main Street, Poughkeepsie, New York. His company will be known as Chief Electronics. . . . Olson Radio Warehouse, 73 E. Mill Street, Akron, Ohio, have been appointed distributors for Philco. . . . John Meck Industries now have a Cessna T 50 plane for transportation of company personnel and special equipment. . . . Jack Kaufman, former president of Heintz and Kaufman, Ltd., has been named vice president of Aireon Manufacturing Corporation and manager of the San Francisco office of Aireon. . . . A one-story plant on a 7½-acre tract on Skokie Highway near Waukegan, Illinois, has been purchased by Belmont Radio. This will supplement the Belmont plant on Dickens Avenue, Chicago for receiver production. . . . Ray T. Schottenberg, jobber sales manager of Astatic Corporation, visited jobbers in the New England states recently. H. A. Chamberlin, Astatic New England rep., accompanied Mr. Schottenberg. . . . George Balsam has been named ad manager and director of sales promotion of Aerovox Corporation, New Bedford, Mass. . . . Westchester Electronic Supply Company, 333 Mamaroneck Avenue, White Plains, N. Y., was recently appointed distributor for RCA, IRC and Cornell-Dubilier. . . . T. R. McElroy, president of the McElroy Manufacturing Corporation, 62 Brookline Avenue, Boston, Mass., has rejoined the Merchant Marine as a radio operator, Lt. Senior Grade, and is now making the regular run between Europe and U. S. . . . Amphinol Phenolic Corporation, 1830 South 54th Avenue, Chicago, Ill., are expanding their plastics manufacturing facilities and building a three-story building next to their present plant. . . . V. Hutto has been named Georgia factory representative for Universal Microphone Company, Inglewood, Calif. . . . Radiart Industries, Cleveland, Ohio, has been bought by Maguire Industries, Inc., Leslie K. Wildberg and William H. Lamar of Radiart have sold all their common and preferred stock to Maguire. . . . James H. Hickey has been appointed general manager of the Zenith Radio Distributing Corporation.

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Filament Current.....	300 ma.

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