

SCIENCE and
MECHANICS

Complete 2-Meter Ham Station

RADIO-TV EXPERIMENTER

No. 569
75c

FALL
1960

37 Electronic
Projects



- TRANSISTOR ANALYZER
- FREQ STANDARD
- 2-TUBE LW RCVR
- TUNNEL DIODE OSC
- VAN de GRAEFF GEN
- MUSIC-ANNUNCIATOR
- WIRELESS INTERCOM
- AC POWER PANEL
- DRY BATTERY TESTER-CHARGER
- MINIATURE TAPE RECORDER
- TYPACODE

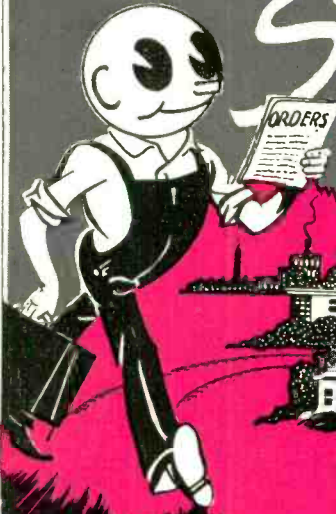
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plans for this
WAVEFORMER, p. 43

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RADIO-TV EXPERIMENTER

Fall 1960 Edition

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Chicago 11, Illinois

The Radio-TV Experimenter contains a selected few of the most popular electronics projects and radio and TV maintenance articles that have appeared in *Science and Mechanics Magazine*, plus a number of projects and helpful articles on the same subjects appearing for the first time.

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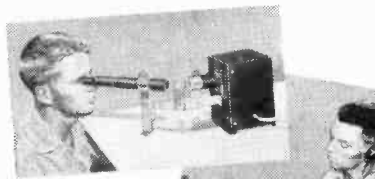


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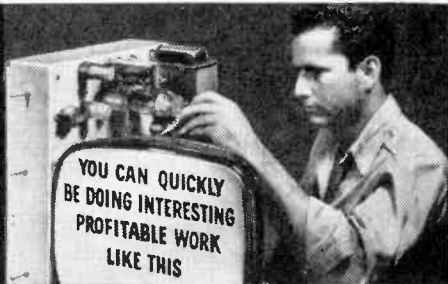
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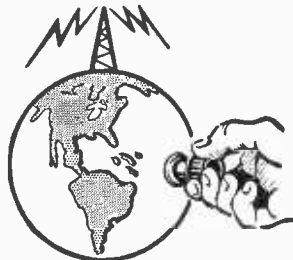
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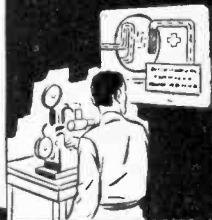
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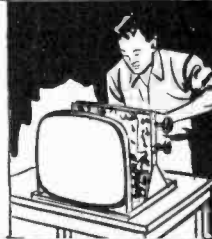
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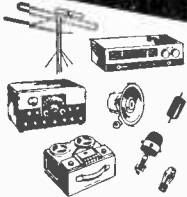
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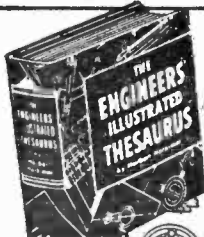
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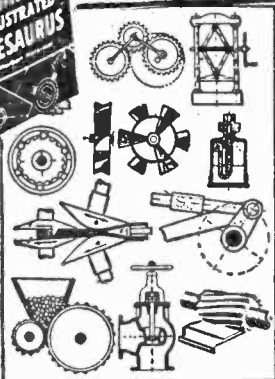
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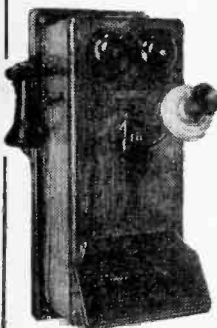
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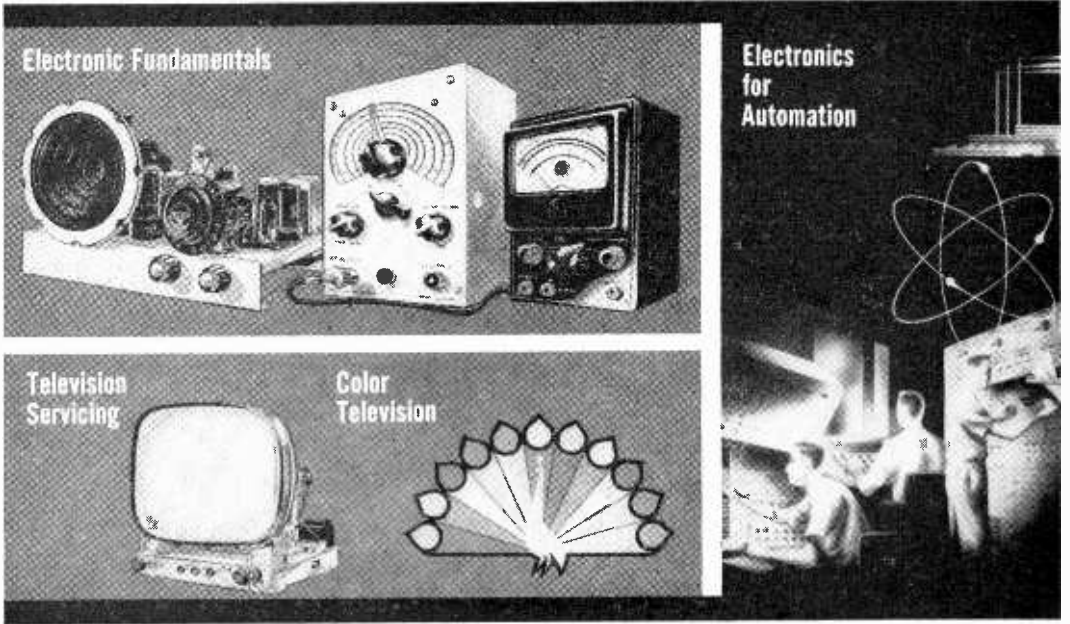


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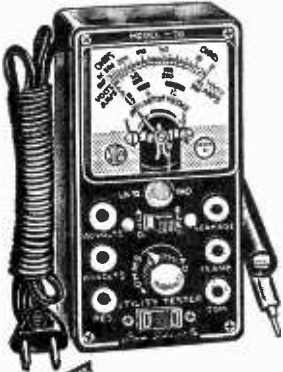
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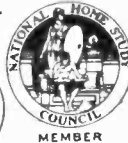
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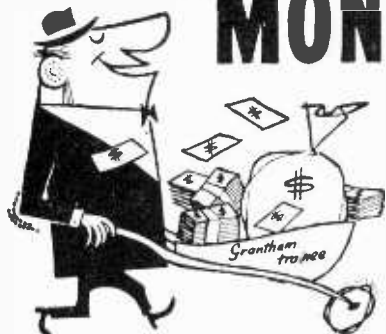
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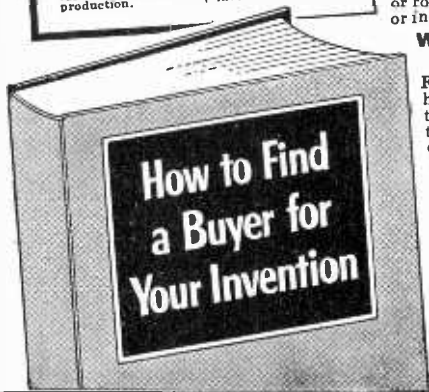
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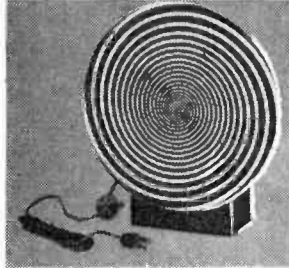
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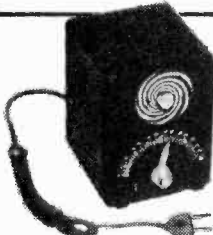
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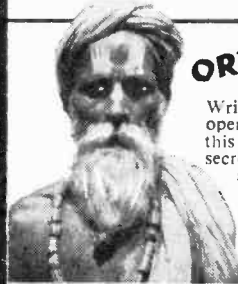
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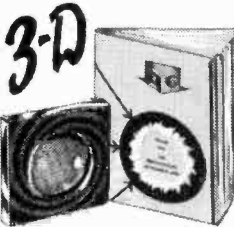
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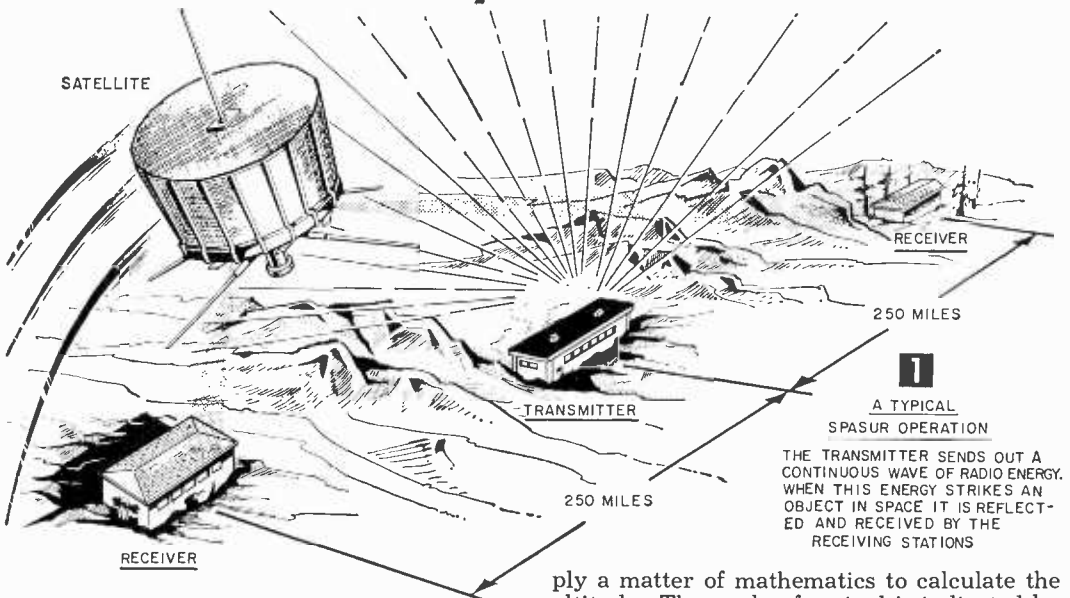
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SPASUR: New Eye On The Universe



JANUARY 1960. A dark satellite circles the Earth, its origin unknown. The space vehicle, transmitting no signal—at least no signal audible in the Western world—should have remained undetected, but didn't. Why not? The reason is SPASUR, a new electronic device built by Bendix Radio for the United States government.

Such an important new system should involve some sweeping new discovery—but that doesn't happen to be the case. SPASUR makes use of two very well known principles of radio reception, proving again that what man does with his discoveries is even more important than the discoveries themselves.

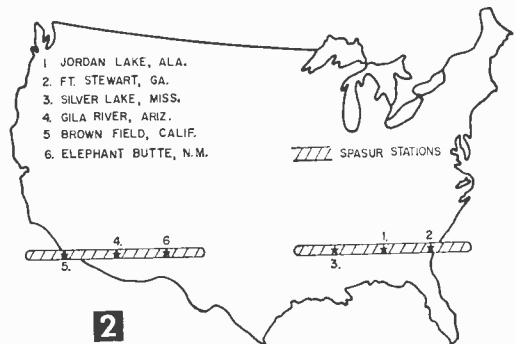
First part of the SPASUR system consists of a VHF transmitter fed into a non-directional antenna. VHF signals are not normally reflected back to Earth unless they happen to strike a solid object. This is precisely what happens when the SPASUR (SPAcE SURveillance) transmission strikes an object in space. Once the reflected signal is picked up by a properly equipped receiving station, position and attitude are determined.

Each SPASUR chain consists of a transmitter and two receiving locations, 250 miles either side of the transmitter. Thus the chain is spread out along a 500 mile strip (see Fig. 2). There are presently a pair of chains operating, centered on Jordan Lake, Alabama, and Gila River, Arizona. A satellite orbiting the Earth must eventually pass within range of at least one of these chains.

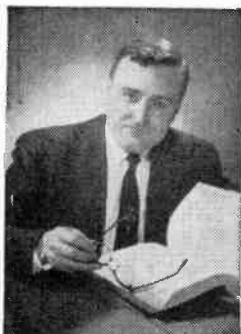
At a receiving station, the bearing is first taken and then the angle between signal and Earth is measured. From the latter, it is sim-

ply a matter of mathematics to calculate the altitude. The angle of arrival is indicated by the phase difference between two parallel antennas. Again this method is nothing new, it's been used for many years in short-wave research. However, when applied to SPASUR it is much more accurate since signals arrive via only one path while on short-wave multi-path reception is common.

The received data is fed into a computer and after three sightings both course and speed are revealed. Working with MINITRACK, another Bendix system which keeps tabs on broadcasting satellites, SPASUR provides a complete picture of "nearby" (near Earth) space activities.—C. M. STANBURY II



The approximate positions of the six stations of the U. S. Navy Space Surveillance detection net. The stations are divided into two complexes (eastern and western), each consisting of a transmitting station and two receiver stations. The stations are located along a great circle track between Fort Stewart, Georgia, and the Naval Air Station, Brown Field, just south of San Diego, California.



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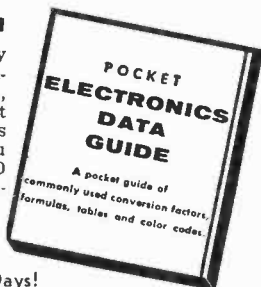
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Memorandum, 1915

Subject: Radio Music Box

David Sarnoff

In 1915, David Sarnoff was Assistant Traffic Manager of the Marconi Wireless Telegraph Company of America. In September of that year he sent to the Vice President and General Manager of the company the following memorandum:

"I have in mind a plan of development which would make radio a 'household utility' in the same sense as the piano or phonograph. The idea is to bring music into the house by wireless.

"While this has been tried in the past by wires, it has been a failure because wires do not lend themselves to this scheme. With radio, however, it would seem to be entirely feasible. For example—a radio telephone transmitter having a range of, say, 25 to 50 miles can be installed at a fixed point where instrumental or vocal music or both are produced. The problem of transmitting music has already been solved in principle and therefore all the receivers attuned to the transmitting wave length should be capable of receiving such music. The receiver can be designed in the form of a simple 'Radio Music Box' and arranged for several different wave lengths, which should be changeable with the throwing of a single switch or pressing of a single button.

"The 'Radio Music Box' can be supplied with amplifying tubes and a loud speaking telephone, all of which can be neatly mounted in one box. The box can be placed on a table in the parlor or living room, the switch set

accordingly and the transmitted music received. There should be no difficulty in receiving music perfectly when transmitted within a radius of 25 to 50 miles. Within such a radius there reside hundreds of thousands of families . . .

"The manufacture of the 'Radio Music Box' including antenna, in large quantities, would make possible their sale at a moderate figure of perhaps \$75.00 per outfit. The main revenue to be derived will be from the sale of 'Radio Music Boxes' . . ."

Hindsight tells us Marconi Wireless should have seized opportunity by the antenna. Instead, they ignored the memo. Five years later, after the Radio Corporation of America was organized, Sarnoff pulled his copy of the memo out of his files and revived his recommendation of 1915 in a report to Owen D. Young, Chairman of the Board of the new company.

Four weeks later, on March 3, 1920, Sarnoff was asked for an estimate of prospective radio business. He replied:

"The 'Radio Music Box' proposition . . . requires considerable experimentation and development; but, having given the matter much thought, I feel confident in expressing the opinion that the problems involved can be met. With reasonable speed in design and development, a commercial product can be placed on the market within a year or so.

"Should this plan materialize it would seem reasonable to expect sales of one million (1,000,000) 'Radio Music Boxes' within a period of three years. Roughly estimating, the selling price at \$75 per set, \$75,000,000 can be expected. This may be divided approximately as follows:

First Year	
100,000 Radio Music Boxes . . .	\$ 7,500,000
Second Year	
300,000 Radio Music Boxes . . .	22,500,000
Third Year	
600,000 Radio Music Boxes . . .	45,000,000

RCA's actual sales of "Radio Music Boxes" during the first three years of its activities in this field, were:

1st year 1922	\$11,000,000
2nd year 1923	22,500,000
3rd year 1924	50,000,000

Total \$83,500,000
Broadcasting had been born.



The serious young junior executive above is David Sarnoff as he looked 40 years ago; today he is RCA's Chairman of the Board of Directors and Chief Executive Officer.



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—	1AX2	.62	—	4CS6	.61	—	6AW8	.89	—	6DG6	.59	—	12AF3	.73	—	12CU5	.58
—	1B3GT	.79	—	4DE6	.62	—	6AX4	.65	—	6DQ6	1.10	—	12AF6	.49	—	12CU6	1.06
—	1DN5	.55	—	4DK6	.60	—	6AX7	.64	—	6DT5	.66	—	12AJ6	.46	—	12CX6	.54
—	1G3	.73	—	4DT6	.55	—	6BA6	.49	—	6DT6	.53	—	12AL5	.45	—	12DB5	.69
—	1J3	.73	—	5AM8	.79	—	6BC5	.54	—	6EU8	.79	—	12AL8	.95	—	12DE8	.75
—	1K3	.73	—	5AN8	.86	—	6BC7	.94	—	6EA8	.79	—	12AQ5	.52	—	12DL8	.85
—	1L6	1.05	—	5AQ5	.52	—	6BC8	.97	—	6H6GT	.58	—	12AT6	.43	—	12DM7	.67
—	1LN5	.59	—	5AT8	.80	—	6BD6	.58	—	6J5GT	.51	—	12AT7	.76	—	12DQ6	1.04
—	1R5	.62	—	5BK7A	.82	—	6BE6	.55	—	6J6	.67	—	12AU6	.50	—	12DS7	.79
—	1S5	.51	—	5BQ7	.97	—	6BF6	.44	—	6K6	.63	—	12AU7	.60	—	12DZ6	.56
—	1T4	.58	—	5BR8	.79	—	6BG6	1.66	—	6S4	.48	—	12AV5	.97	—	12EL6	.50
—	1U4	.57	—	5CC8	.76	—	6BH6	.65	—	6SA7GT	.76	—	12AV6	.41	—	12EL6	.50
—	1U5	.50	—	5CL8	.76	—	6BH8	.87	—	6SK7	.74	—	12AV7	.75	—	12E26	.53
—	1X2B	.82	—	5EA8	.80	—	6BJ6	.62	—	6SL7	.80	—	12AX4	.67	—	12F5	.66
—	2AF4	.96	—	5E08	.80	—	6BK7	.85	—	6SN7	.65	—	12AX7	.63	—	12F8	.66
—	3AL5	.42	—	5J6	.68	—	6BL7	1.00	—	6SQ7	.73	—	12AZ7	.86	—	12FM6	.45
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—	3AV6	.41	—	5U4	.60	—	6BN6	.74	—	6U8	.78	—	12BA6	.50	—	12SA7M	.86
—	3BA6	.51	—	5U8	.81	—	6BQ5	.65	—	6V6GT	.54	—	12BD6	.50	—	12SQ7GT	.74
—	3BC5	.54	—	5V6	.56	—	6BQ6GT	1.05	—	6W4	.57	—	12BE6	.53	—	12SN7	.67
—	3BE6	.52	—	5X8	.78	—	6BQ7	.95	—	6W6	.69	—	12BF6	.44	—	12SQ7M	.73
—	3BN6	.76	—	5Y3	.46	—	6BR8	.78	—	6X4	.39	—	12BH7	.73	—	12U7	.62
—	3BU8	.78	—	6AB4	.46	—	6BU8	.70	—	6X5GT	.53	—	12BL6	.56	—	12V6GT	.53
—	3BY6	.55	—	6AC7	.96	—	6BY6	.54	—	6X8	.77	—	12BQ6	1.06	—	12W6	.69
—	3BZ6	.55	—	6AF3	.73	—	6BZ6	.54	—	7AU7	.61	—	12BY7	.74	—	12X4	.38
—	3CB6	.54	—	6AF4	.97	—	6BZ7	.97	—	7A8	.68	—	12BZ7	.75	—	17AX4	.67
—	3CF6	.60	—	6AG5	.65	—	6C4	.43	—	7B6	.69	—	12C5	.56	—	17BQ6	1.09
—	3CS6	.52	—	6AH6	.99	—	6CB6	.54	—	7Y4	.69	—	12CA5	.59	—	17C5	.58
—	3CY5	.71	—	6AK5	.95	—	6CD6	1.42	—	8AU8	.83	—	12CN5	.56	—	17CA5	.62
—	3DK6	.60	—	6AL5	.47	—	6CF6	.64	—	8AW8	.93	—			—		
—	3DT6	.50	—	6AM8	.78	—	6CG7	.60	—	8BQ5	.60	—			—		
—	3Q5	.80	—	6AN4	.95	—	6CG8	.77	—	8CG7	.62	—			—		
—	3S4	.61	—	6AN8	.85	—	6CM7	.66	—	8CM7	.68	—			—		
—	3V4	.58	—	6AQ5	.50	—	6CN7	.65	—	8CN7	.97	—			—		
—	4BC5	.56	—	6AR5	.55	—	6CR6	.51	—	8CX8	.93	—			—		
—	4BC8	.96	—	6AS5	.60	—	6CS6	.57	—	8EB8	.94	—			—		
—	4BN6	.75	—	6AT6	.43	—	6CU5	.58	—	10DA7	.71	—			—		
—	4BQ7	.96	—	6AT8	.79	—	6CU6	1.08	—	11CY7	.75	—			—		
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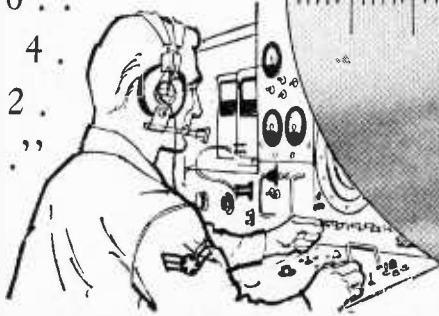
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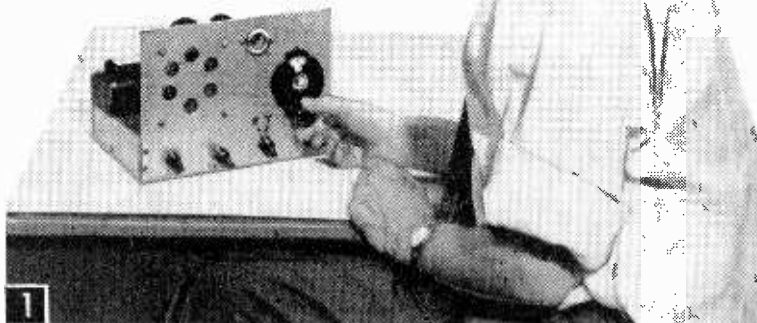
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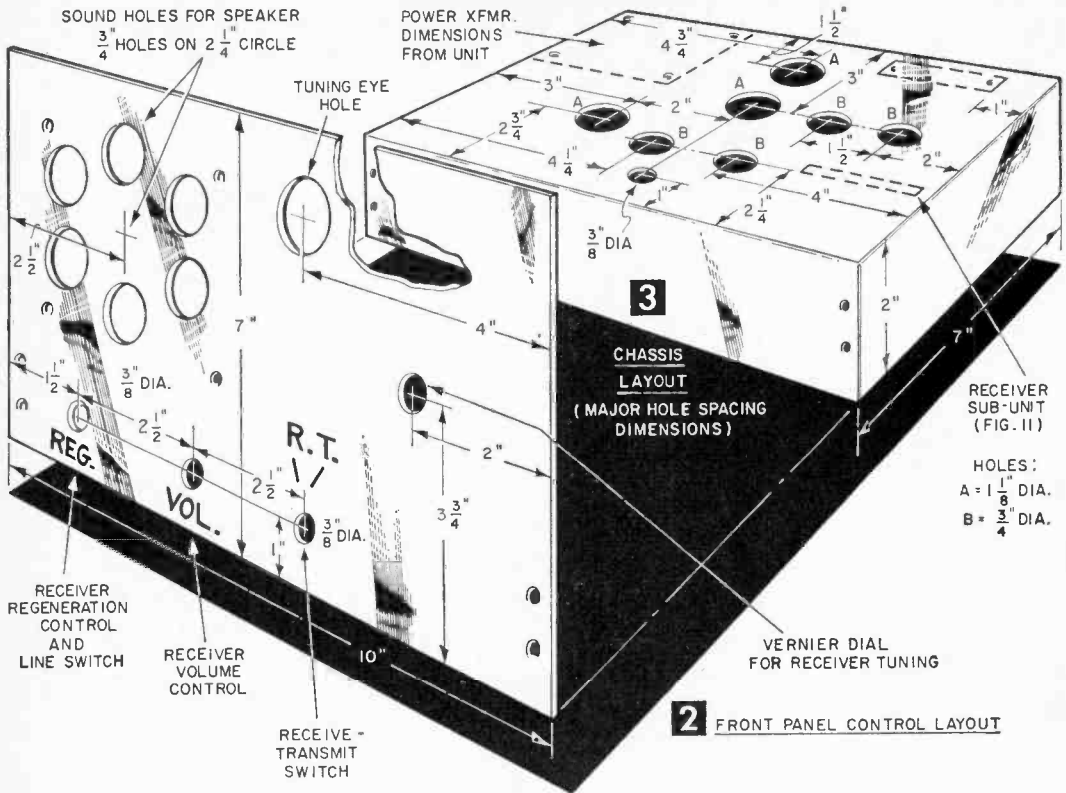
OPEN to holders of all classes of amateur license, the 144-megacycle, two-meter amateur band offers interesting possibilities to the experimentally inclined ham. This little rig provides an excellent starting setup, or a nice little extra rig.

Begin construction by drilling and punching the major holes in the front panel and chassis (Figs. 2 and 3). Mount the panel temporarily upon the chassis while drilling the holes for the two potentiometers and the Receive-Transmit switch. With all major holes drilled, mount the power transformer, then the rectifier tube socket and the Jones barrier terminal strip. Temporarily mount the regeneration control potentiometer upon the panel; it includes the On-Off power-line switch, which is wired-in immediately.

Now complete the power supply wiring (see Fig. 7) first connecting the transformer leads to the rectifier tube socket, then wiring in the 120-v primary leads. The electrolytic capacitors are held in place by their mounting brackets, as are the positive "hot" leads which are supported by a two-lug, insulated tie-point strip. Last of all, install and connect the filter choke. Ground one side of the 6.3-v heater winding and bring the other end out to one of the unused rectifier socket lugs, which will serve as a tie-point for connection to the heater of each of the tubes (except the rectifier, of course).

After you've wired and carefully checked the power supply, measure the resistance between the positive high-voltage terminal and ground. There should be more than 10,000 ohms. Less indicates a wrong connection, or short. When the high-voltage circuit has been checked out, connect the line cord to its terminals on the terminal strip and insert the rectifier tube in its socket. When the switch is turned on, the rectifier tube filaments should glow dull red and a dc voltage of at least 250 v (more won't hurt) should be observed from the positive terminal of the last filter capacitor to ground.

Audio Section. When the power supply is operational, remove the rectifier tube and line cord and fasten in the sockets for the audio frequency section, including the 12AT7, half of which is used for an AF amplifier. (The other half is the crystal oscillator, which is wired-in later.) The AF section includes one and one-half 12AT7's, and the 6V6GT. The 12AT7 sockets are mounted with 4-36 x 1/4-in. rh machine-screws and nuts. Be sure to put a soldering-lug under one of the mounting screws for each socket to provide a ground point for that part of the circuit. Pin No. 9 on each 12AT7 socket, and pin No. 7 on the 6V6GT are connected to the 6.3-v heater winding (ungrounded green lead) of the power transformer. Ground pins 4 and 5 on each 12AT7 socket, as well as the metal tube



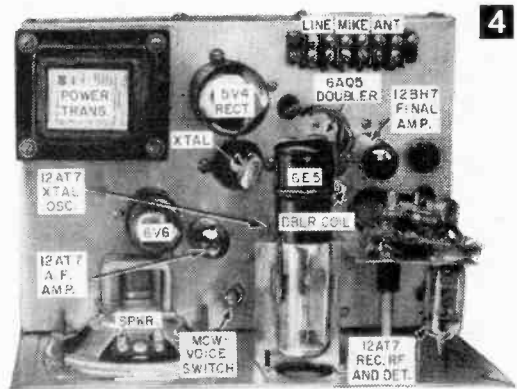
in the center. On the 6V6 socket, ground pins 1 and 2.

Work backwards from the output transformer through the 6V6 (see Fig. 6). Ground the "common" terminal on the output transformer secondary; leave the other secondary terminal alone for the moment. The output transformer is mounted with 6-32 *rh* machine screws and nuts. When the 6V6 has been wired, temporarily connect the loudspeaker (between unused secondary lead and ground), insert the 6V6 and rectifier tube, plug in line cord and turn on power. Both tubes should light and, when warm, a screwdriver touched to pin No. 5 (control grid) of the 6V6 should produce a characteristic clicky buzz in loudspeaker.

With the audio output stage connected and operating, unhook external connections, remove tubes, and wire the 12AT7 stage that feeds the signal to the 6V6. Use 2- and 4-point insulated tie-lugs as needed to hold small parts firmly in place by their leads.

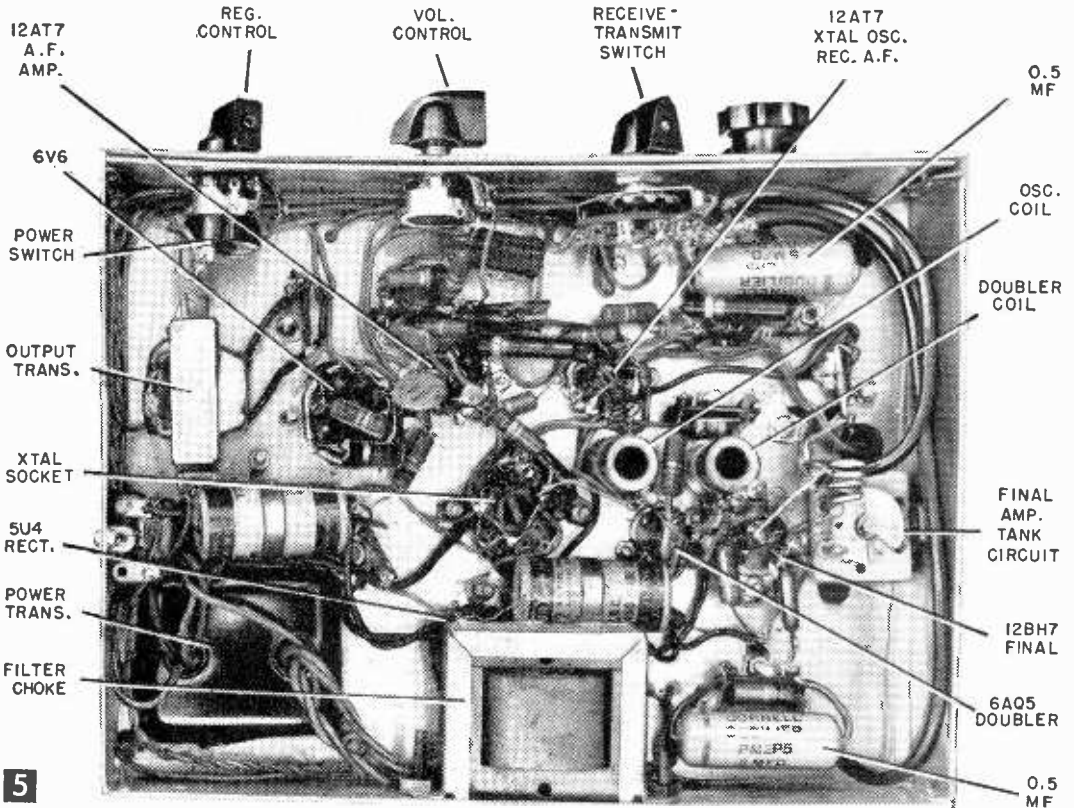
After you've wired and checked this next stage, put in tubes, re-connect speaker and plug in line. When all tubes are warm, carefully touch a screwdriver to the control grid terminal (pin No. 7) of the 12AT7. A much louder clicky buzz should be heard.

To complete further AF circuit wiring, you'll have to temporarily install both the



Receive-Transmit switch and the volume control potentiometer. Figure 8 shows connections for the non-shorting type R-T switch. Continue wiring by completing the 12AT7 amplifier stage that serves the receiver (see Fig. 9). Make all ground leads short.

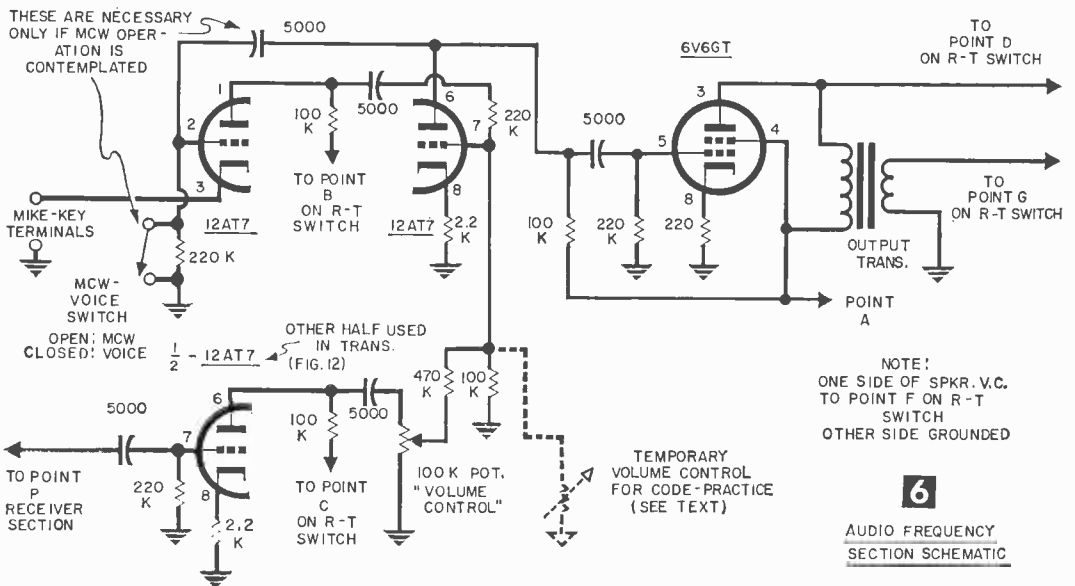
To test this stage, set up as previously described, throw the R-T switch to "Receive," and check for the characteristic buzz at the grid. Advance the volume control, of course. Because of the relatively high amplification involved here, it should be possible to hear a faint hiss of tube noise when the volume control is fully advanced.



Finish the AF section by wiring the 12AT7, "speech-amplifier" stage. This circuit contains the SPST toggle switch that converts it into an oscillating multivibrator for modulated CW work. When the switch is open the circuit acts as a multivibrator, or tone

generator. When closed, the stage becomes a grounded-grid amplifier for the mike.

Connect external connections, as previously described for testing, and insert all tubes involved. Connect a 220K resistor temporarily across the Mike-Key terminals on the termi-

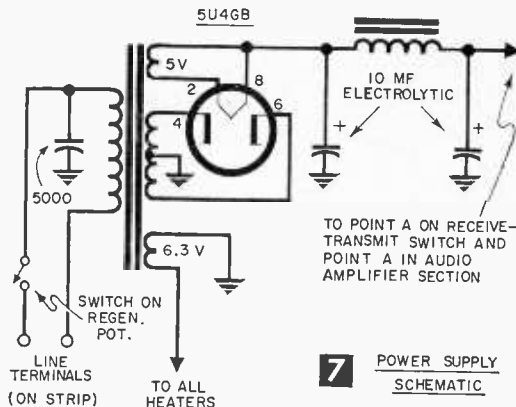


nal strip. When the toggle switch is in the open position, a loud, clean musical tone should emerge from the speaker. (Note that the volume control, since it is associated with the receiver only, does not affect the strength of the tone.)

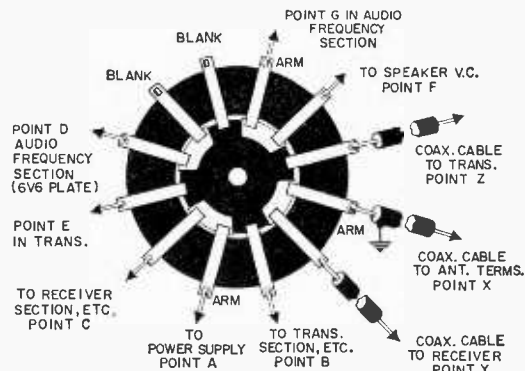
Throw the toggle switch into the closed position and connect a single-button carbon microphone (Type "F-1," from Telephone Engineering Company, Simpson, Penn., or other similar single-button carbon mike) to the microphone terminals. Now, the system should

MATERIALS LIST—2-METER STATION

No. Req'd	Description
1	2 x 7 x 10" aluminum chassis
1	7 x 10" aluminum panel
3	knobs for 1/4" shaft
1	National type BM dial
1	tuning eye assembly for 6E5 tube (includes bracket, socket and bezel)
1	PM loudspeaker, 4" size Jensen
1	2 3/4 x 3 1/2" aluminum sheet, for detector (see text)
3	octal plastic tube sockets, Amphenol
4	9-pin miniature sockets, high frequency plastic insulation, Amphenol
1	7-pin miniature socket, Amphenol
1	6-terminal Cinch-Jones barrier terminal strip
1	SPST toggle switch, H&H
1	100K linear-taper potentiometer & switch (Mallory)
1	500K audio-taper potentiometer (Mallory)
1	power transformer, Chicago-Standard Type PM-8408
1	filter choke, Chicago-Standard, Type C-1708
1	output transformer, Chicago-Standard, Type A-3823
2	10 mfd. electrolytic filter capacitors, 450 working volt, Mallory
2	0.5 mfd. paper capacitors, 200 working volt, Cornell Dubilier
3	Ohmite type Z-144, 2-meter RF chokes
3	National type XR-50 coil forms, with iron slugs
1	four-pole, double-throw, non-shorting wafer switch, Centralab No. 1409
1	15 mmf variable tuning capacitor, Hammarlund HF-15
1	15 mmf BUD variable tuning capacitor type MC-1850, with one plate removed (see text)
1	47 ohm, one-watt carbon resistor
8	100K one-watt carbon resistors
2	47K, one-watt carbon resistors
4	22K, one-watt carbon resistors
2	2.2K, one-watt carbon resistors
5	220K, one-watt carbon resistors (includes one extra for new operation)
1	220 ohm, one-watt carbon resistor
1	470K, one-watt carbon resistor
1	1K, one-watt carbon resistor
1	1 meg., one-watt carbon resistor
5	50 mmf, 600 W.V. disk-type ceramic capacitors
8	5000 mmf, 600 W.V. disk-type ceramic capacitors
2	5 mmf., 600 W.V. disk-type ceramic capacitors
3	1000 mmf., 600 W.V. disk-type ceramic capacitors
1	brass shaft coupling 1/4" to 1/8" shaft (female to female)
1	type 48, 2-volt, 60 ma dial lamp bulb (for tuning)
1	1N34 crystal diode, Sylvania
1	"overtone" crystal approximately 36 megacycles, Texas Crystal Co., River Grove, Ill.
1	If you are a General class operator, you may select a crystal anywhere between 36 to 36.975 megacycles. Novices and Technicians must select one between 36.25 and 36.75 Ma. If you wish a certain frequency within the 144-megacycle band, divide that frequency by four to get your crystal frequency. Ask for the adapters to adapt the pin diameter to fit octal sockets pins. Texas Crystal Co. will supply these gratis when requested in order.
1	line cord and plug
1 pc	plastic rod 1/4" dia., 3" long
1	5U4GB vacuum tube
1	6V6GT vacuum tube
3	12AT7 vacuum tube
1	6AQ5 vacuum tube
1	12BH 7 vacuum tube
1	6E5 vacuum tube
1	microphone, carbon, type F-1 (Telephone Engineering Co., Simpson, Penna.)
1	telegraph key (optional) Johnson Model 114-100
1	directional antenna for 144-Mc. amateur band, (the 5 element "Hi-Gain," or similar type is recommended.) With Co-axial transmission line and rotator
1	wire, rosin-core solder, screws, nuts, tie-points, etc.



7 POWER SUPPLY SCHEMATIC



8 BACK VIEW OF RECEIVE-TRANSMIT SWITCH (SWITCH SHOWN IN RECEIVE POSITION AS SEEN FROM BACK WITH CHASSIS INVERTED)

behave exactly like a good, low-power public-address amplifier. (Do not use a crystal or a dynamic mike.) Make sure the switch is in "transmit" position, before making these latter tests.

The unit as so-far constructed will serve very well as a code-practice oscillator with the toggle switch open, or as a small PA amplifier, with the switch closed. If it's too loud for you, connect a 50,000-ohm variable resistor from the grid of the last 12AT7 to ground (see Fig. 6). Varying this control will vary volume, but it may also have some effect upon the tone of the oscillation.

To use the audio system so-far constructed for a code practice oscillator, connect an ordinary telegraph key, in series with a 220K, one-watt carbon resistor to the Mike-Key terminals. The frame of the key should be connected directly to the grounded side, the 220K resistor in series with the other side. At full output, the signal is strong enough to serve a roomful of students; the volume may be reduced by the temporary volume control described above. Be sure the toggle switch is in the open position, and the R-T switch in the Transmit position, of course.

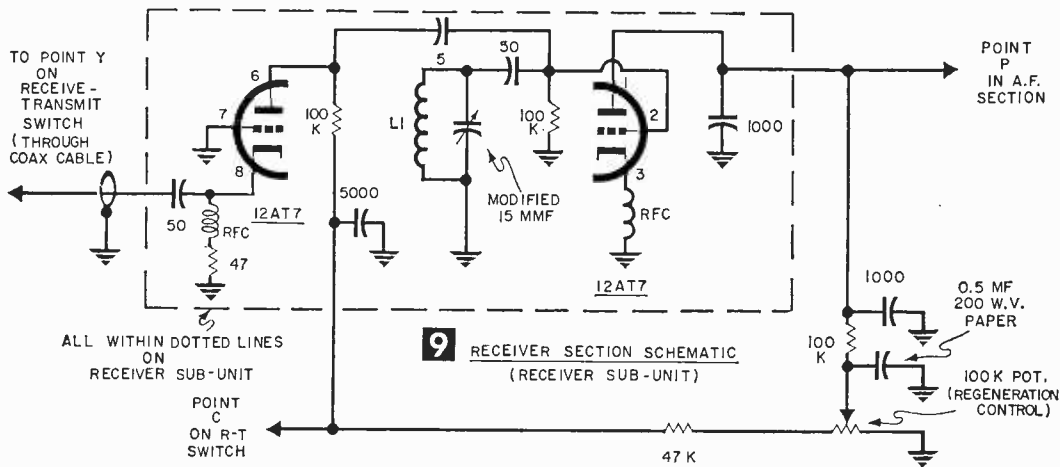
Receiver Section. Start by connecting the

regeneration control, 100K potentiometer and 47K voltage-dropping resistor, along with the 100K detector plate load resistor (see Fig. 9). These parts are installed beneath the chassis—using insulated tie-lugs where appropriate to hold the resistors firmly in place.

With this under-chassis receiver wiring done, drill and assemble the receiver sub-unit (Figs. 10 and 11). Since this receiver operates at the high frequency of 144-million cycles per second, short and direct leads are of paramount importance. This applies especially to grid, plate and bypass-capacitor leads. It is important to return cathode leads and high-frequency bypass capacitors in the same stage to the same ground where possible.

speaker. This hiss indicates *super-regeneration*, the condition for high sensitivity in a receiver of this type. By varying this control, it should be possible to increase the hiss level from zero to strong. Also, a super-regenerative condition should be possible over the entire range of the tuning capacitor.

When the receiver super-regenerates properly, check the tuning range with a grid-dip meter. My receiver covers from about 140 to about 150 megacycles, with the 144-148 megacycle amateur band falling between about 60% and 70% of maximum capacitance of the tuning capacitor. The exact tuning range is not critical as long as the 144-148 megacycle amateur band is conveniently included.



The 15 mmf Bud receiver tuning capacitor is modified by removing one of its rotary plates. Grasp one of the rotary plates firmly in the jaws of a long-nosed pliers, twist and pull, and the plate will slip cleanly out of its slot. This will leave one rotor and one stator plate. The two remaining plates should not scrape against each other. You may increase the band-spread (number of dial-degrees occupied by the amateur band) by cautiously bending the two plates away from each other. Do not make this adjustment, however, until the receiver is performing properly.

Wind coil L1 (see Fig. 13A) carefully and complete as much of the wiring as possible, before mounting the sub-unit upon the chassis. It is fastened in place with 6-32 rh machine screws and nuts. Next, connect heater, dc power, and signal output leads to the appropriate points under the chassis. Do not connect the antenna coaxial lead until later.

With the receiver wiring completed, insert tubes, connect loud speaker temporarily, and apply power. With the R-T switch at Receive, advance the volume control to full-on. Then slowly advance the regeneration control potentiometer. As this control is advanced, a loud, smooth hiss should be heard from the

Squeeze the turns of the coil together or spread them slightly for minor changes.

If you live in or near a large city, you should now be able to hear two-meter amateurs on the air within range when a good antenna is connected between the antenna input tie point and ground. In addition, police, taxicab dispatchers, and aircraft operating adjacent to the amateur band may be heard in many areas. If you have not yet installed a good two-meter antenna, a high, clear outdoor TV antenna may serve temporarily to test the receiver. (Install a knob temporarily on the capacitor shaft to aid in tuning. To use a TV antenna to test receiver, connect one of the lead-in line wires to the antenna input tie point, the other to chassis.)

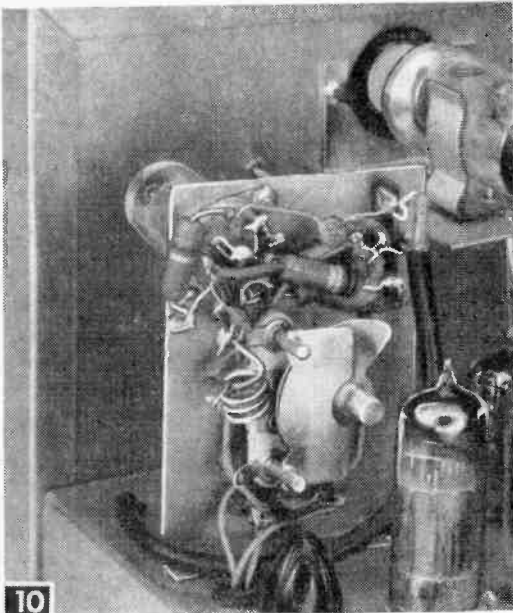
Transmitter. Start wiring with the crystal oscillator and work forward (see Fig. 11). The crystal plugs into any two alternate pins of the octal crystal socket; other unused pins may be used for tie-points for other circuits if desired. The crystal oscillator tube is the half of the 12AT7 that was *not* used for the AF amplifier circuit. The only critical part of the circuit is the coil, and this will cause no trouble if it is wound exactly as described in Fig. 13B.

After carefully checking the crystal oscillator circuit, proceed to the 6AQ5 frequency doubler stage. Again, this stage is straight-forward; only the coil being critical. Wind this coil exactly as shown in Fig. 13C, being careful to get the tap in the exact center. Ground the cathode and the screen bypass capacitor to the same point on the chassis, as close to the socket as possible. The 1K resistor should be fastened to a two-point insulated tie lug mounted close by the coil.

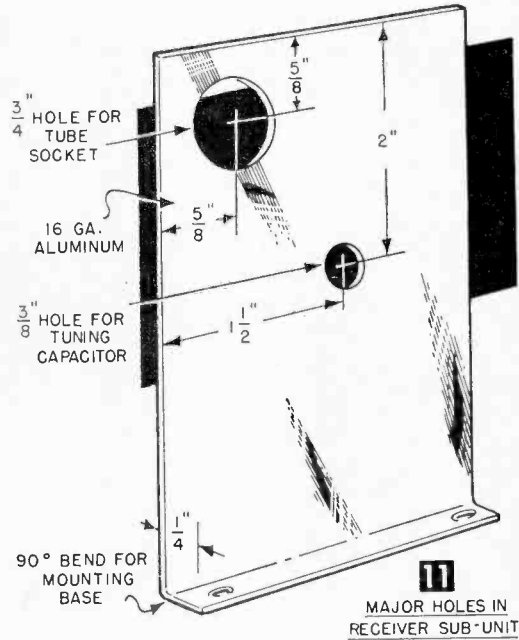
When this doubler stage is complete, wire the final amplifier stage. Although a frequency doubler, this circuit develops practically the same efficiency as a straight-through amplifier while at the same time avoiding the self-oscillation troubles which plague the lat-

stages is completed, insert tubes. Do not apply power yet, however. Instead, get your grid-dip meter, and carefully adjust each of the coils as closely as possible to its correct resonant frequency; 36 megacycles for the crystal oscillator, 72 megacycles for the doubler, and set the final tank to resonance at 144 megacycles. Be sure the tubes are in their proper sockets for this operation; their capacitance plays a big part in determining the resonant frequencies. If properly wound and installed, each of the coils should resonate at the correct frequency, with considerable extra slug-adjustment range available in either direction. The final tank coil may be adjusted by squeezing or spreading its turns.

When all coils have been pre-tuned, plug



10



11
MAJOR HOLES IN
RECEIVER SUB-UNIT

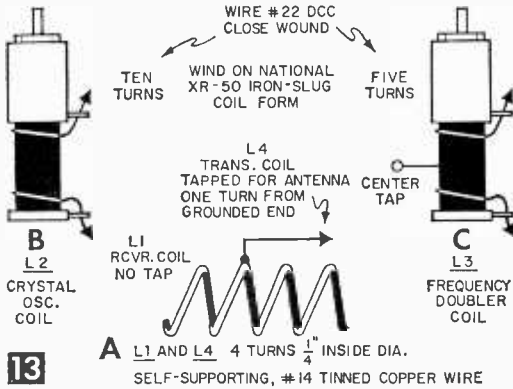
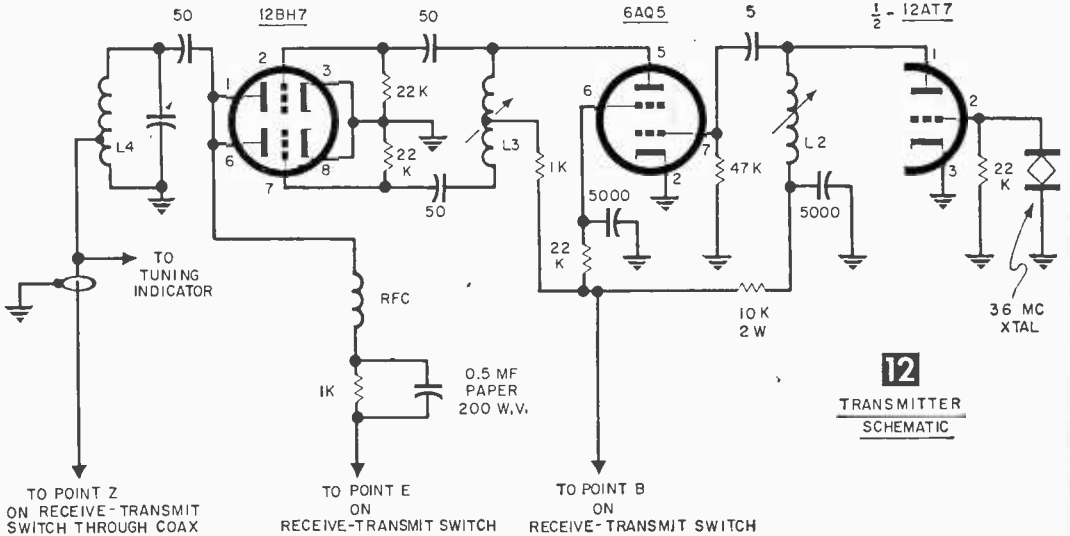
ter. Its push-push feature also helps to eliminate odd harmonics which could get into TV receivers and cause interference. The ordinary distortion-type frequency doubler, often used in simple VHF transmitter arrangements, provides none of this added spurious-harmonic suppression.

Again, since the output circuit is tuned to 144 megacycles, you *must* keep all leads as short and direct as possible. An extra quarter-inch of wire here can spell the difference between success and failure. Wind coil L4 exactly as shown in Fig. 13A and keep the leads short! Wire the entire final amplifier circuit carefully, but do not connect the antenna coax cable yet or the plus high-voltage lead. In the final stage, return all ground connections to the same point near the tube socket.

When the wiring of the transmitter RF

in the crystal, and apply power. Tune the grid dipper to 36 megacycles and immediately adjust the crystal oscillator coil for maximum oscillator output. If the crystal oscillator doesn't oscillate, recheck the wiring, and try another tube. When you find oscillation, screw the slug down until you get maximum output, then screw the slug out about three turns in the interest of stability and reliability of oscillation. Then immediately adjust the doubler coil slug for maximum output. Take a No. 48, or No. 49 dial light bulb (pink head) and solder a small loop of wire between its terminals. Then couple this loop closely about the doubler coil. If the doubler is operating properly, the lamp will light noticeably.

Now connect the positive high-voltage lead



to the final amplifier, apply power, and tune the final tank capacitor to maximum 144-megacycle output with the grid-dip meter. If you find plenty with the grid-dip meter, couple your "soup-loop" tuning lamp to the final coil and slightly re-tune. The bulb should glow brightly if the lamp is closely coupled. If you get weak, or no output, check the wiring again, or try another 12BH7 tube.

Now temporarily shut off power and plug-in the audio amplifier tubes. Connect your carbon mike to the *Mike-Key* terminals. Set the toggle switch to the closed position. Re-apply power and speak clearly into the mike. The bulb around the final amplifier tank should flicker markedly in step with your voice, indicating proper modulation.

The Finishing Touches. Pull out all tubes and remove all external connections. Mount the loudspeaker, the tuning-eye assembly, and the vernier dial upon the panel. Now remove the potentiometer and Receive-Transmit switch binding nuts and install the panel with the binding nuts and with self-tapping metal screws. Place knobs on potenti-

The VHF Amateur Bands

Today the VHF bands provide the greatest opportunity and challenge to the experimentally minded ham. These frequencies above 144 megacycles seem to be the only ones left wherein simple, low-powered equipment still can compete effectively against expensive, "store-bought" gear.

Nobody knows for sure the exact distance limitations on VHF communication. The first signal bounced off the moon by the U. S. Army back in 1946 was in the VHF range. On the other hand, it is the consistent, interference-free, short-haul communication, up to 50 miles or so, that is the operating bread-and-butter of the VHF amateur. Occasional long-distance spurts are to be considered as interesting diversions, rather than daily fare. Distance chasing, in itself, is not the whole of amateur radio. You'll have a lot of fun, face some stimulating problems, and meet some nice people on the two-meter band, believe me.

Those frequencies between 145 and 147 megacycles are available to both **novice** and **technician** class licenses, as well as the general-class operator. But do make sure that you have a license before you do any transmitting. "Citizens Band" license is **not** sufficient. You must have an **Amateur** license. (Write to the Federal Communications Commission office in the large city nearest you for details.)

In addition to the license, and to the usual hand tools owned by all radio experimenters, you should have available:

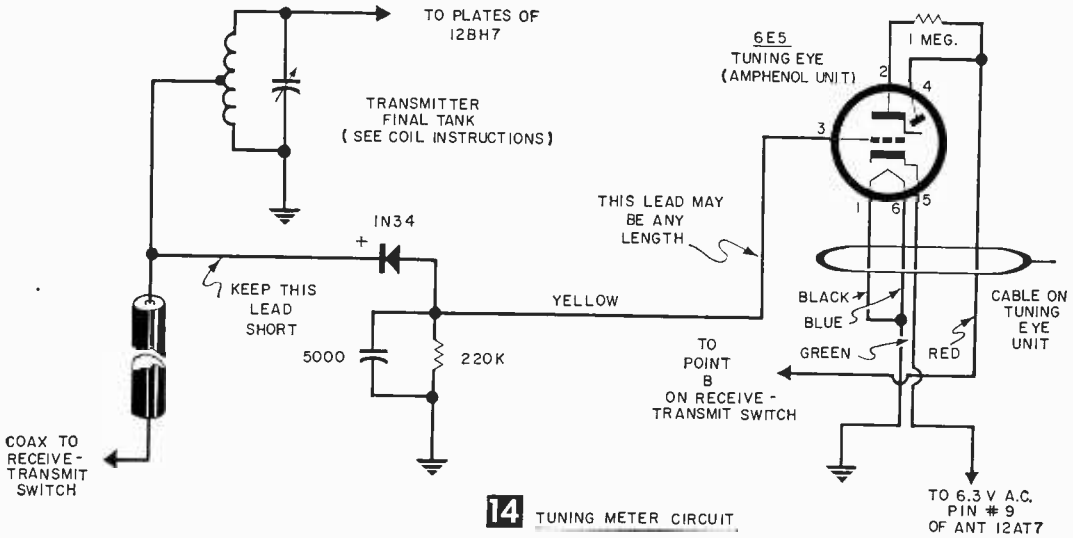
1) A good "two-meter beam," a directional antenna for the 144-megacycle band. Such an antenna is not expensive or unwieldy, in fact it is smaller than the usual outdoor TV antenna. A five-element antenna is sufficient, and can be purchased at a reasonable price from Newark Electric Co., Allied Radio, or any similar Amateur jobber.

You should equip your beam antenna with a suitable rotating-device, (one of those sold for TV antenna use will do very well) and you should get it as high above the ground as you can. A "quick and dirty" rule is that you can reliably work one mile of range per foot of antenna height (above average ground) beyond ten feet. In other words, this is your **consistent** communication range, in miles.

While you can make a number of contacts, particularly in the New York, New England, and Chicago areas, with a dipole in the attic, a good beam will do more for your morale than anything else.

2) A grid-dip meter. Stray capacitance and inductance being unpredictable in most cases, it becomes necessary to individually trim VHF tuned circuits by trial in nearly every case. The proper tool for establishing these resonant frequencies is the grid-dipper.

3) A volt-ohm-milliammeter.



ometer and R-T switch. Connect the receiver tuning capacitor to the vernier tuning dial with a piece of 1/4-in. fiber or plastic rod and a shaft coupling. A setting of zero upon the tuning dial should correspond to maximum capacity, lowest frequency.

Plug the 6E5 tuning-eye tube into its socket, and fit it into the clamp provided on its bracket. Bring the cable from the tuning eye socket through the chassis through a 3/8-in. hole with rubber grommet. Connect the black and blue wires of this cable to ground, the green wire to the 6.3-v heater supply, and the red wire to the positive high voltage.

Install the 1N34 crystal diode, the 5000 mf. capacitor, and the 220K resistor in the tuning meter circuit upon a two-lug insulated tie point, being careful to observe the polarity of the crystal diode. Install the diode-resistor assembly close to the final amplifier tank coil. Connect the yellow wire from the tuning eye tube to the ungrounded end of the 220K resistor as indicated in Fig. 14.

Now is the time to connect the receiver input and the transmitter output to the R-T switch through RG-59-U coaxial cable. Ground the outer sheath of each piece of cable firmly to the chassis at both ends of its run. The coaxial cable from the transmitter (center conductor) is tapped one turn from the grounded end of the final tank coil, L4, as shown in Fig. 13A. The receiver cable is run from the R-T switch to the input tie-point on the receiver sub-unit. Bring the cable up through a grommeted hole in the chassis. Next, run a piece of cable from the R-T switch to the antenna terminals on the terminal strip. Connect a short piece of wire—not over 1/2 in. long—from the center conductor of the coax cable (where it connects to the transmitter tank) to the tuning diode.

Finally, run the wire from the R-T switch

to one side of the speaker, passing it thru a de-burred 1/8-in. hole in the chassis. Ground the other speaker voice-coil lug.

Connect the power cord, and microphone to the proper terminals on the terminal strip. Then connect a No. 48 pilot lamp bulb across the antenna terminals. Apply power and, when the tubes are warm, throw the R-T switch to Transmit. The bulb should glow brightly and the tuning-eye should move toward closed position. (If it opens, reverse the connections to the 1N34.) Re-tune the final amplifier tank and buffer tank for maximum glow from the bulb. Note also that the eye closes most when the output is at a maximum. Speak into the mike and note the variation in bulb brilliance and eye closing as you speak, indicating proper modulation.

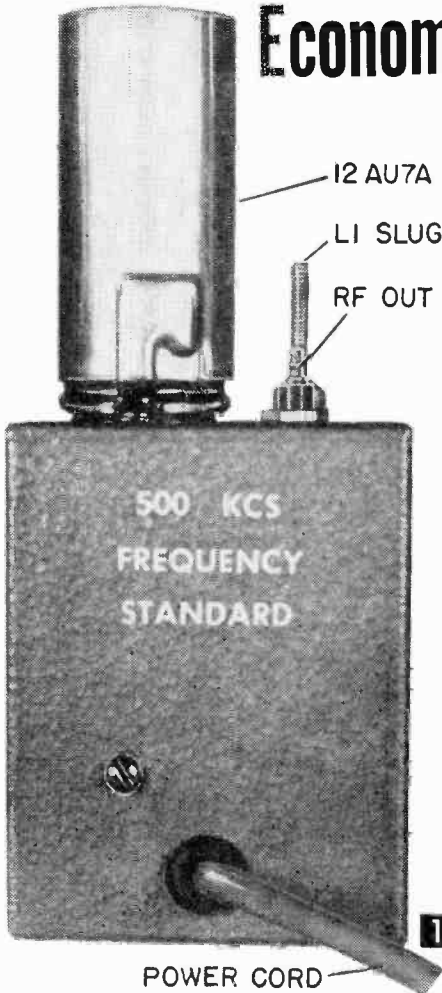
Now, remove the lamp bulb, and connect a 144-megacycle antenna system, preferably a good, high, beam antenna. Make sure the grounded terminal of the antenna feed coaxial cable is connected to the grounded terminal on the terminal strip. Throw the R-T switch to Receive and adjust regeneration for a smooth hiss. If there are any other two-meter amateur stations operating in your vicinity, you should hear them with no difficulty. Now throw the switch to Transmit position and adjust the final tank capacitor to close the eye as completely as possible. You're tuned-up and ready to go.

Novices learning the code, may wish to operate in the modulated code, MCW mode, which is legal in the 144-megacycle band. To use, throw the toggle switch into the open (MCW) position, and substitute a telegraph key, in series with a 220K resistor, for the microphone. Otherwise operation is identical to voice. The smooth, tone-modulated CW signal radiated can be read by other amateurs, regardless of the receiver employed.

Economy Frequency Standard

Here is a versatile frequency standard that the amateur, SWL, or experimenter can build in one evening for about five dollars

By JOE A. ROLF, K5JOK



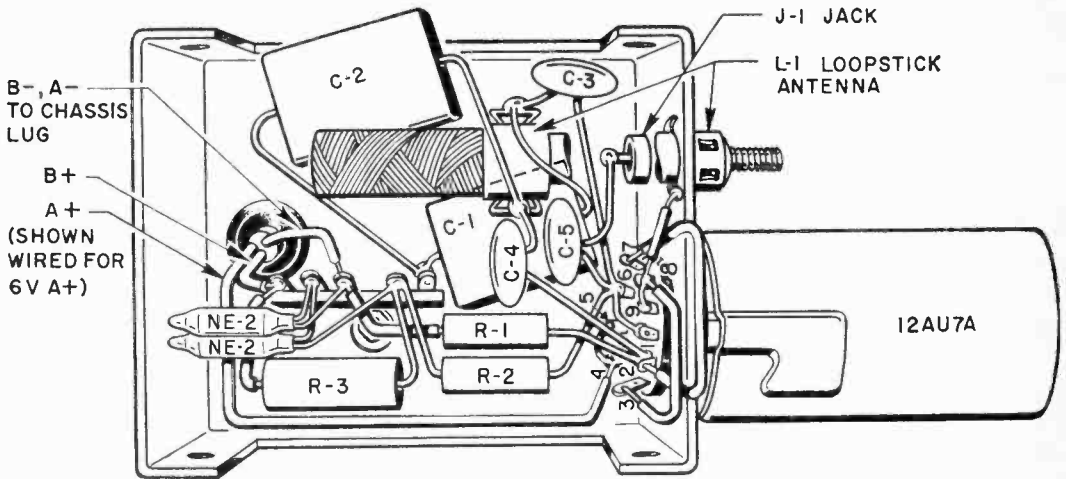
THIS compact frequency standard will enable you to calibrate your receiver and check its accuracy at will. It can also be employed as a beat frequency oscillator for receiving CW signals, and for other applications requiring a stable 400 Kc to 1200 Kc RF generator.

The circuit shown in Fig. 3 is a high-C Colpitts oscillator using a parallel connected 12AU7A. Excellent frequency stability is achieved by the use of a high-Q loopstick as tank coil and a large value of tank capacity. Two NE-2 neon lamps regulate the oscillator plate voltage for added stability. With rigid construction and good shielding, the circuit has negligible drift after initial warm-up.

For maximum compactness, the unit is constructed in a $1\frac{5}{8} \times 2\frac{1}{8} \times 2\frac{3}{4}$ in. Minibox (CU-2100). Construction details are shown in Figs. 2 and 4. The 12AU7A is mounted outside the cabinet to avoid heating frequency-determining components. The output jack, J1, and tank coil, L1, are mounted beside the tube socket. Inductance L1 should be securely mounted and reinforced with a bead of Duco cement to insure against possible vi-

1

Frequency standard is powered from an external source. Designed primarily for 500 Kc, it can be tuned from 400 Kc to 1200 Kc.

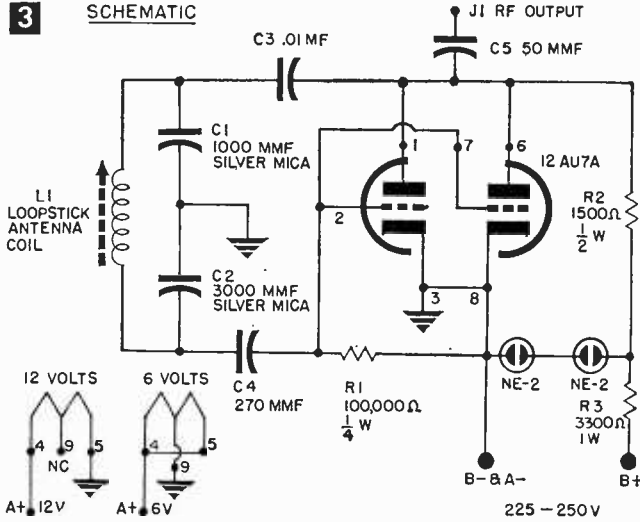


2 PICTORIAL

Components C3, C4, C5 and R1 are mounted to the tube socket beneath C1. Jack J1 is mounted behind L1.

3

SCHEMATIC



MATERIALS LIST—FREQUENCY STANDARD

Design.	Description
C1	1000 mmf silver mica capacitor
C2	3000 mmf silver mica capacitor
C3	.01 mfd disc ceramic
C4	270 mmf mica capacitor
C5	50 mmf mica or disc ceramic
J1	small feed-through insulator, coax jack, or phone tip jack
L1	ferri-loopstick antenna coil
NE-2	NE-2 neon lamp (two required)
R1	100,000 ohm, 1/4 watt resistor
R2	1,500 ohm, 1/2 watt
R3	3,300 ohm, 1 watt
1	Cu-2100 Minibox
1	12AU7A tube
1	3-conductor cable, length as desired
1	5-lug terminal strip
1	9-pin miniature tube socket
3	1/8 x 1/4" machine screws and nuts
1	1/8" rubber grommet
	tube shield, decals, etc.

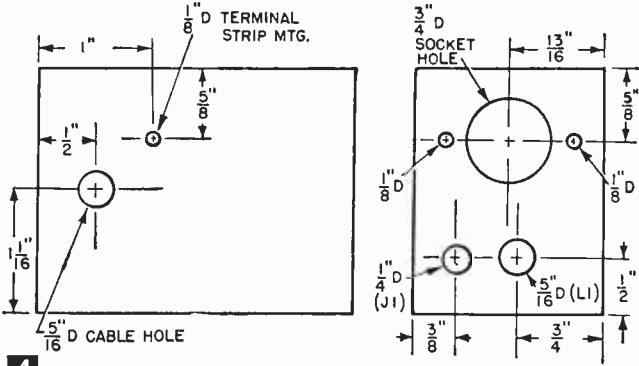
this switch can be included in the Minibox.

Adjustment of the slug on L1 permits the unit to be set at any frequency from about 400 Kc to 1200 Kc. This permits a number of applications, the most obvious, of course, as a 500 Kc or 1000 Kc frequency standard. When tuned to 500 Kc, useful harmonics will appear at 500 Kc. intervals up to about 15 Mc. Above 15 Mc, 500 Kc harmonics rapidly become too weak for easy receiver calibration and it is necessary to shift the standard's setting to 1000 Kc to get harmonics of useful amplitude above 35 Mc. The unit can be accurately adjusted to either frequency by zero beating WWV at 2.5 Mc, 5 Mc or 10 Mc.

4

FRONT SIDE

TOP



bration. Jack J1 may be a small feed-through insulator, miniature coax jack, or phone tip jack. Power is furnished by an external source and brought into the cabinet by a three-conductor cable.

It is important, from the standpoint of stability, that wiring be as rigid as possible. Connections between socket pins 2 and 7, and pins 1 and 6, should be made with heavy solid copper wire. Pins 3, 8, and 9 are grounded at the tube socket; other leads should be kept short and rigid to avoid vibration. Keep components away from L1 as much as possible and use quality silver mica capacitors for C1 and C2.

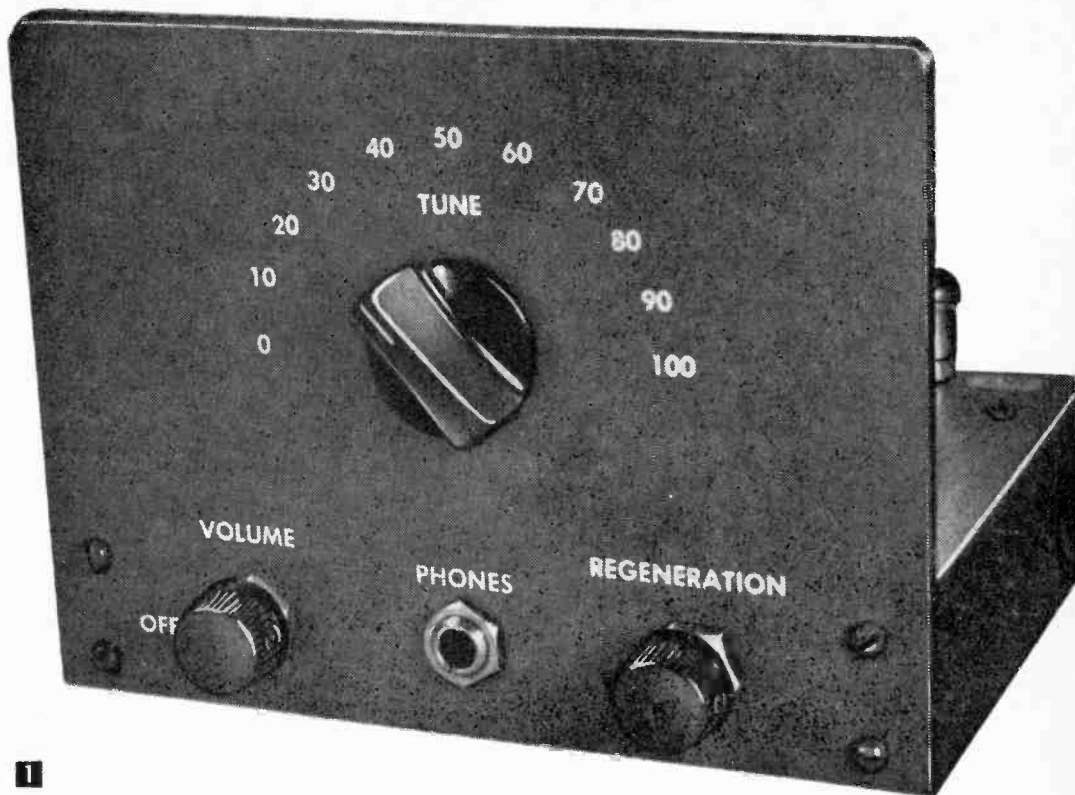
The oscillator is designed to operate with plate voltages from 225 to 250 v at about 15 ma. In most cases these voltages are available from the receiver with which this frequency standard will be used. Less than 225 v can be used if R3 is replaced with a 500 ohm, 1 watt resistor. Filament connections for either 6 or 12 v are shown in Fig. 3. The oscillator is turned on and off by a SPST switch in the external B-plus lead. If desired,

As a frequency standard, the unit is small enough to fit inside most receiver cabinets. In most cases, a short length of insulated wire connected to J1 and brought near the receiver input circuit will provide sufficient coupling.

However, you may find that with some receivers or with less than 225-v plate voltage, it may be necessary to connect the standard directly to the receiver antenna terminal with a 5-30 mmf mica capacitor.

Another useful application, for the SWL or amateur, is as a BFO (beat frequency oscillator) for 455-Kc IF receivers. The standard can be tuned to the IF frequency and connected to the grid or plate lead of the receiver's last IF stage with a 2 to 5 mmf capacitor for CW reception employing an all-wave set or an automobile receiver.

Note that Fig. 2 is shown wired for a 6-v filament supply, pin 9 of the 12AU7A grounded, pins 4 and 5 tied together. If you are using a 12-v filament supply, pin 9 will have no connection, pin 5 is grounded, and pin 4 is wired to the 12 volts (see Fig. 3).



Two-Tube Long Wave Receiver

This compact ac-dc receiver features good sensitivity, better than average selectivity, and simplified construction. It has an adjustable tuning range of 85 to 550 kc. and is easily modified for broadcast-band reception

By JOE A. ROLF, K5JOK

THE circuit of this economical receiver (see Fig. 4) employs two miniature high-gain TV tubes. The 6AN8 is a regenerative detector; the pentode section of the 6AU8 is an audio amplifier. The triode of the 6AU8 serves as an ac-dc type rectifier.

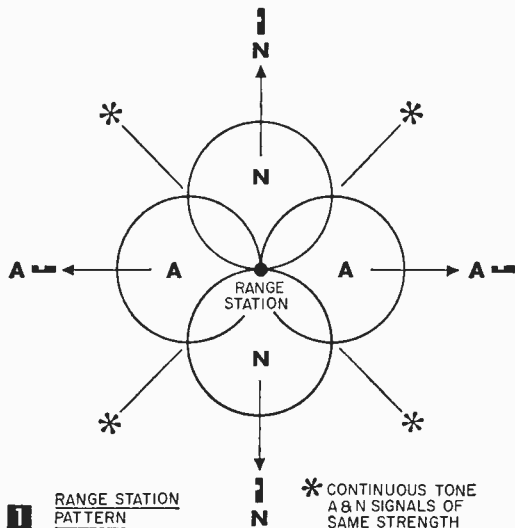
The heart of the circuit is the detector, a regenerative cathode-follower type commonly known as the "Regenode." If you're not familiar with this hybrid circuit, here's how it works: The pentode section of the 6AN8 is a conventional grid-leak detector, with the exception of the signal grid which is separated from the tuned antenna circuit by the cathode-follower connected triode section of the tube. This arrangement permits a degree of selectivity not possible with the detector

grid connected directly to the antenna circuit, since the signal-grid loads the tuned circuit and reduces its Q, or selectivity ability. The cathode-follower isolates the detector from its input circuit and allows a great improvement in selectivity. The circuit operates smoothly, is easily adjusted, and eliminates hand-capacity effects common to most regenerators. These advantages are particularly desirable in a LW receiver.

Since hand capacity does not affect operation, an all-wood chassis constructed with simple hand tools can be used. Chassis details are shown in Fig. 5. Large holes (for tube sockets and controls) can be made with a coping saw; fastener holes can be made with a hot ice-pick in the absence of a drill. A

What to Listen To on LW

The long waves provide up-to-the-minute reports on weather and flying conditions, code practice and some good DX



YOU'LL be pleasantly surprised at the number of interesting signals to be heard below the standard broadcast band, though at first they may sound like nothing but jumbled dots and dashes intermixed with weird howls and squeals. Careful listening, however, will reveal this apparent bedlam to be important communication services which make unusual listening and challenging DX.

The main divisions of the 10 Kc. to 535 Kc. band are shown in Table A. It is occupied mainly by aeronautical and marine services, although 150-535 Kc. is part of the standard BC band in Europe and Asia. However, without discounting the possibility of logging some of these BC stations, the marine and aeronautical stations are of prime interest to most LW listeners.

The most popular are the navigational aids, or radiobeacons, heard between 200 Kc. and 405 Kc. Some are marine beacons, others aeronautical. Both employ very slow amplitude modulated code and are easily distinguished from one another by their signals.

Marine beacons usually transmit their call signs continuously in an omni-directional pattern. In some cases the call, consisting of from two to four letters or numerals, is separated by a number of dashes. Many marine beacons can be heard constantly over a considerable range, while the less powerful can be logged at great distances under favorable conditions.

Aeronautical range stations transmit a combination A-N signal in a four-leaf pattern like that of Fig. 1. They identify themselves every thirty seconds and employ two pairs of antennas to obtain the four-leaf radiation pattern. The transmitter is operated continuously and is alternately switched between the two antenna systems so that an A (dit dah) is radiated in the directions marked A in Fig. 2, and an N (dah dit) in the directions marked N. Midway between the A and N patterns, the signals merge as a steady tone which aircraft follow to or from the station. If the pilot leaves this course, he will hear either the A or the N.

These radiobeacons offer an unlimited

metal chassis will afford more compact construction, but a wooden panel and cabinet should be used to avoid accidental grounding of the chassis.

Construction is not critical and will pose no difficulty if the general layout shown in Figs. 2, 3, and 5 is followed. Keep RF and AF leads separated and away from ac leads. This is best accomplished by wiring the filaments and power supply first, then the AF and detector stages.

Ground connections are made to solder lugs mounted to the socket and tuning capacitor fasteners. Components R4, R6, R9 and R10 mount on a 7-lug terminal strip at the rear underside of the chassis (see Figs. 3 and 4). The filter capacitor, C11, can be wedged between the 6AU8 socket and chassis leg, or secured with a mounting clip. Two sections of this capacitor are used in the power supply

filter, the third is used as a cathode bypass for the audio stage.

Other components under the chassis, except R3, C7 and C9, mount to respective tube sockets. Capacitor C9 is connected from J2 to the grounded terminal on R5. Resistors R3 and C7 connect to a machine screw and solder lug placed between L1 and C2. One lead of L2 connects to a solder lug on the same screw on the chassis top.

The antenna trimmer, C1, is secured by the antenna terminal mounting screw as shown in Fig. 3. This component requires only infrequent adjustment, but it can be mounted on the front panel for easier access, if desired.

Inductance L1, a standard TV replacement coil, is mounted last. Before inserting the core, as explained in the manufacturer's instruction leaflet, thread on the $\frac{3}{16}$ -in. mounting clip and remove $\frac{1}{2}$ in. from the slotted

TABLE A—LONG WAVE ALLOCATIONS

Frequency (Kc.)	Communications Service	Sunset Skip	Night DX
10-14	Radionavigation	none	4 am to 7 am
14-200	Fixed Public Services and Coastal-Marine CW		
200-283	Aeronautical Beacons and Communications		
285-325	Marine Radiobeacons		
325-405	Aeronautical Beacons and Communications	10 pm	7 am
405-415	Radio Direction Finding	to	
415-490	Coastal and Marine CW	2 am	
500	International Calling and Distress Frequency	2-4 hours after sunset	11 pm to 7 am
510-535	Misc. Radiobeacons		

Note: Frequencies between 150 Kc. and 535 Kc. also used by foreign BC stations.

TABLE B—STATION LISTS

The Airman's Guide	Superintendent of Documents, Washington 25, D. C. 25¢ per copy. A bi-weekly publication listing all U. S. aeronautical radio beacons.
Location Identifiers	Superintendent of Documents, Washington 25, D. C. \$1.50 for copy and one-year supplement service. General listing of all domestic beacons.
Broadcasting Stations of The World, Part 11, According to Frequency	Superintendent of Documents, Washington 25, D.C. \$2.00. Includes European LW broadcasting stations.
Air Navigation Radio Aids	Department of Transport, Air Service Branch, Ottawa, Ontario, Canada. Complete list of Canadian Radio Beacons, published every two months.
Radio Facility Charts—Caribbean & South America	ACIC, USAF, 2nd & Arsenal Streets, St. Louis 18, Mo. One year subscription \$3.50. Listing of Caribbean & South American beacons.
Radio Navigational Aids	Hydrographic Office, U. S. Navy. An annual publication listing worldwide marine beacons.
List of Coast Stations (4.10 Swiss francs)	Secretary General, International Telecommunications Union, Geneva, Switzerland. Very complete listings of worldwide stations.
List of Ship Stations (12.80 Swiss francs)	
List of Call Signs (21 Swiss francs)	

source of unusual DX. At first sight, these stations seem to offer poor DX since most are relatively low powered and have a daytime range of less than 200 miles. However, their range is greatly increased at night—best times for night DX are given in Fig. 1. These hours will vary somewhat with the seasons, with the choicest DX being heard from early fall to late spring.

Above 325 Kc. sunset skip is often heard for a half-hour during early darkness. Notable examples are PJG, 343 Kc. in the Netherlands Antilles; ASN, 350 Kc. on Ascension Island; and SWA, 406 Kc. from Swan Island.

Since beacons identify continuously or every thirty seconds, less than a minute is required to log a station. However, in order to determine the locations of the stations you

hear, you need a reference log listing the stations you are interested in. Such listings can be purchased (see Table B).

Range stations also transmit verbal weather reports for air fields in their area 15 minutes before and 15 minutes after the hour.

In addition to radiobeacons, many CW stations operate on long waves for maritime, aeronautical, and public service communication. For the CW enthusiast, these are interesting to copy and the slower stations, sometimes sending as slow as eight words a minute, provide plenty of code practice. Many good DX signals can be heard between 415 Kc. and 500 Kc., particularly on the 500 Kc. international calling and distress frequency. The frequencies below 200 Kc. are also widely used by public service and maritime CW stations.

end of the core adjustment screw, otherwise it will protrude below the chassis when the coil is mounted. Clamp the section to be removed in a vise and cut it off with a hacksaw, then cut a new screwdriver slot. Take care not to break or fracture the fragile ferrite coil.

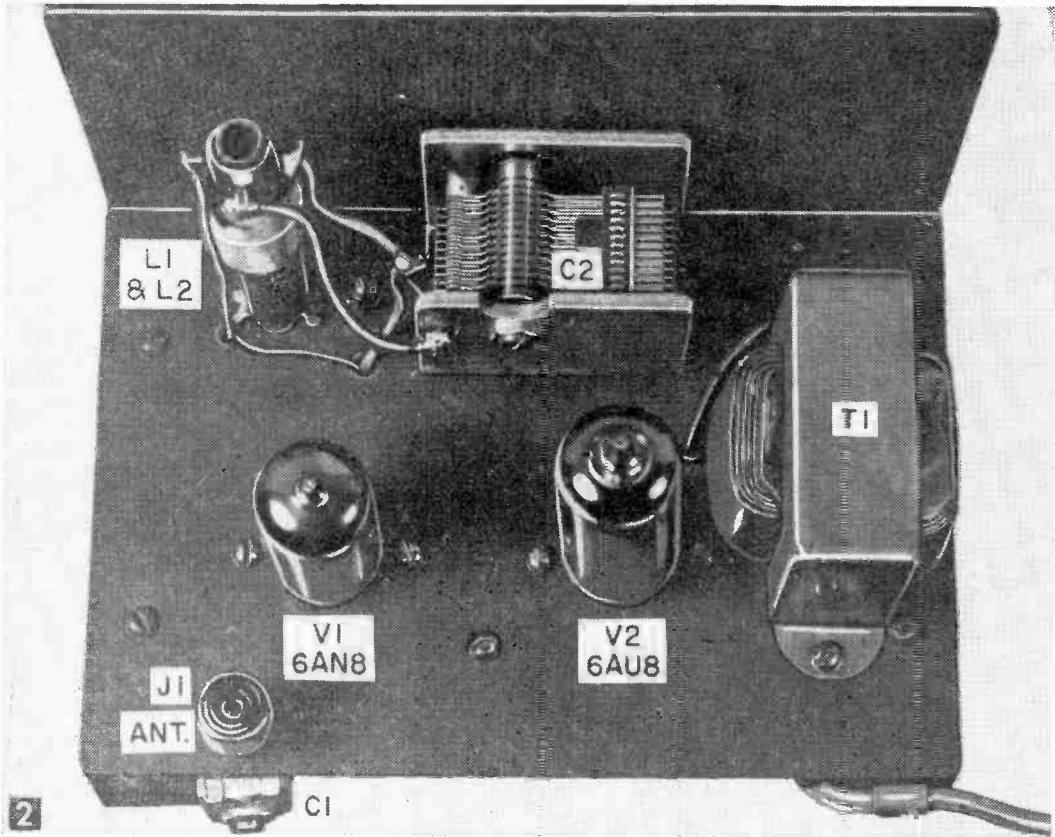
Inductance L2 consists of 35 turns of #26 (or smaller) enameled wire scramble-wound over a 1/16 in. ID tube which slides freely over L1. If not available, this form can be made by winding four or five layers of moist gummed tape, sticky side out, over L1. When dry, slip the tube off and trim to proper length with a razor blade. With L2 in place, secure L1 to the chassis with a bead of Duco cement.

For maximum sensitivity, the position of L2 on L1 should be adjusted for the individual receiver. This simple adjustment is well

worth the effort and can be made with a long antenna, 455 Kc signal generator, or a BCB receiver with a 455 Kc intermediate frequency. If possible, use a signal generator or BCB receiver, since this will permit adjustment of L2 and the core of L1 at the same time.

Short out L2 temporarily by connecting a short piece of wire from the R3-C7 solder lug to pin No. 7 of the 6AN8 socket. Turn the core adjustment screw full counterclockwise and connect the antenna, signal generator, or BCB receiver to the antenna terminal.

If a BCB set is used, tune to a strong BCB station and turn the set's volume down. Connect a short piece of insulated wire to your LW receiver antenna terminal and place it near the underside of the BCB set's IF tube socket or IF transformer to hear the 455 Kc IF signal of the BCB receiver.



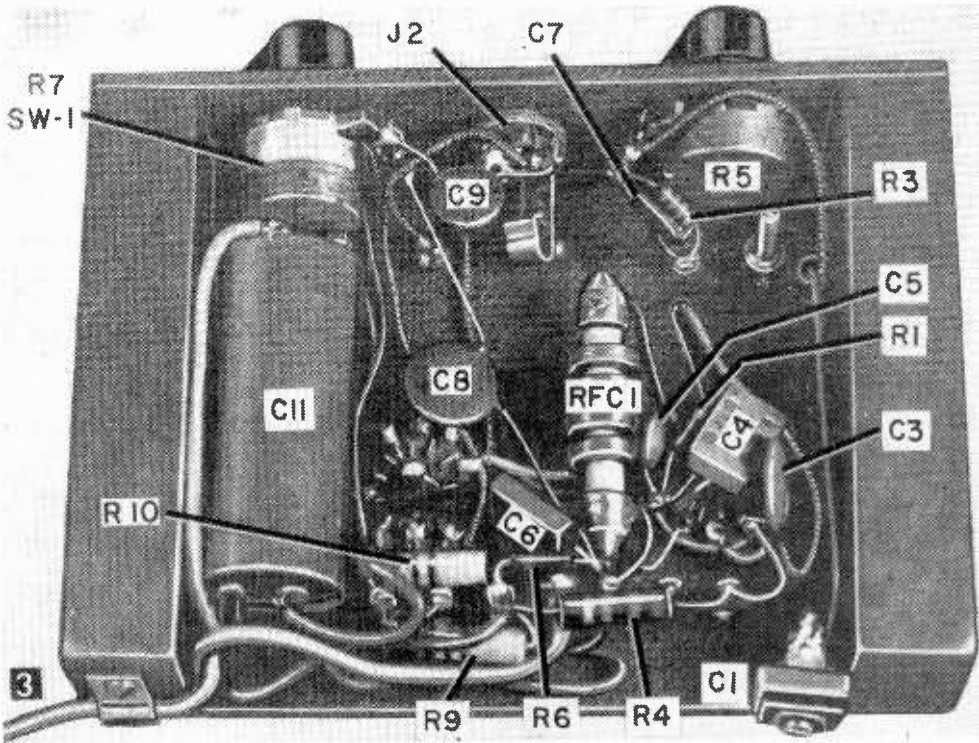
2
Topside of the receiver's Masonite chassis. The antenna coil, L1, is mounted so that its slug is adjusted from below the chassis.

MATERIALS LIST—LONG WAVE RECEIVER

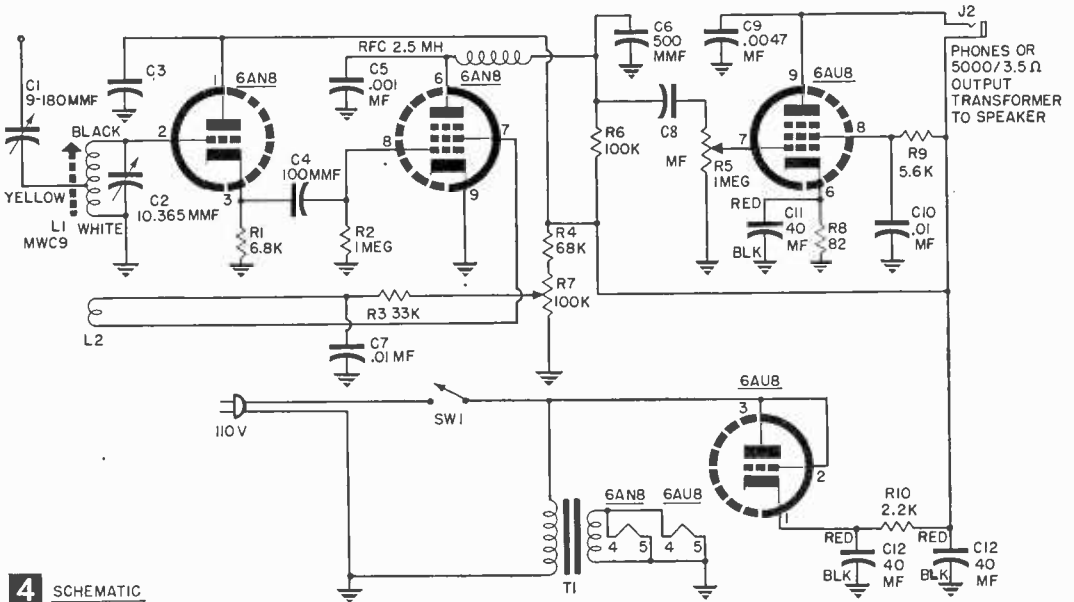
Desig.	Description	Desig.	Description
C1	9 to 180 mmf trimmer capacitor	R10	2.2 K, 1 watt
C2	10 to 365 mmf variable capacitor, standard single-gang TRF type	J1	antenna terminal post, or Fahnestock clip
C3	.01 mfd disc ceramic	J2	standard phone jack
C4	100 mfd mica	L1	Long Wave: Merit MWG-9 Width or Linearity coil, .3 to 12 ma., tapped (see text)
C5	.001 mmf disc ceramic		Broadcast: Ferri-loopstick BCB antenna coil (see text)
C6	500 mfd mica	L2	Long Wave: 35 turns #26, or smaller, enameled wire scramble wound on $\frac{7}{16}$ " ID x $\frac{3}{8}$ " form (see text)
C7	.01 mfd disc ceramic		Broadcast: 3 turns #26, or smaller, enameled wire on adjustable form (see text)
C8	.01 mfd disc ceramic	RFC1	2.5 mh. RF choke (National R-100, or equivalent)
C9	.0047 mfd disc ceramic	SW1	on R7
C10	.01 mfd disc ceramic	T1	filament transformer, 6.3 vct, 1.2 amp (S/anchor P-6134 or equivalent)
C11	40-40-40 mfd, 150 wv capacitor, 3-section electrolytic filter capacitor (Cornell-Dubilier BBRT 44415, or equivalent)	T2	optional—for speaker use only; 5000/3.2 ohm, 3 watt, 40 ma, output transformer. (Merit A-3025, or equivalent)
R1	6.8 K, $\frac{1}{2}$ watt resistor	W1	6AN8
R2	1 meg, $\frac{1}{2}$ watt	W2	6AU8
R3	33 K, $\frac{1}{4}$ watt	1 pc	$\frac{1}{8}$ x $4\frac{1}{2}$ x 6" Masonite (panel)
R4	68 K, 1 watt	1 pc	$\frac{1}{8}$ x 4 x 6" Masonite (chassis top)
R5	1 meg, $\frac{1}{4}$ watt volume control with SPST switch (Mallory U-53 Midgetrol with US-26 switch, or equivalent)	1 pc	pine strip, $\frac{3}{4}$ x $1\frac{1}{8}$ x 4" (chassis sides)
R6	100 K, $\frac{1}{2}$ watt	2 pcs	two miniature 9-pin tube sockets
R7	100 K, $\frac{1}{4}$ watt, volume control (Mallory U-41 Midgetrol, or equivalent)		hardware, power cord, dial, knobs, etc.
R8	82 ohm, $\frac{1}{2}$ watt		
R9	5.6 K, 1 watt		

With the volume control at maximum and the regeneration control set at half-scale, place the tuning capacitor about 85% open and turn L1's core clockwise until the 455 Kc signal is heard. Adjust the regeneration control for maximum volume and mark its position. This is the detector's most sensitive

point and will determine the position of L2. Remove the jumper across L2 and slide the coil up or down over L1 until regeneration (signal distortion) occurs just above the point previously marked on the regeneration control. If the detector fails to regenerate, reverse the leads on L2.



Under-chassis view, showing placement of components.

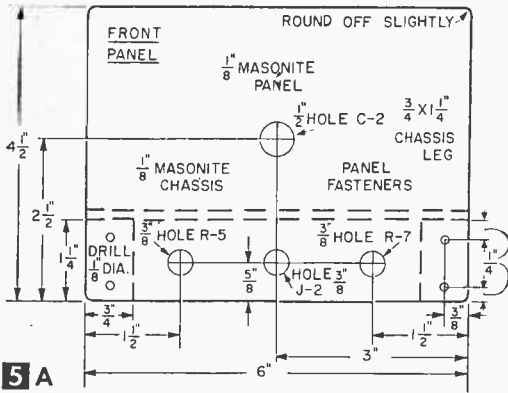


4 SCHEMATIC

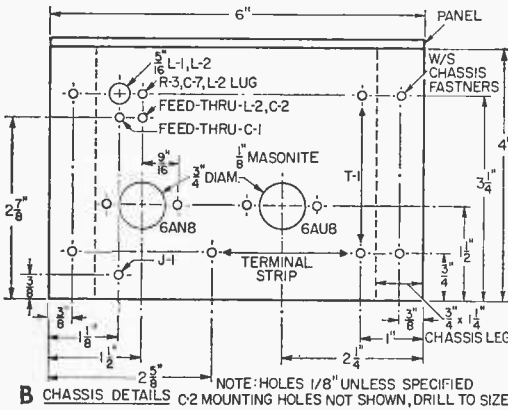
This receiver's tuning range, from 85 to 550 Kc, is covered in two adjustments of the core on L1. When set to receive 550 Kc at C2's minimum capacity, the receiver will tune down to about 200 Kc. The range from 85 to 200 Kc is tuned when the slug is almost fully inserted into L1. Overlap on both bands will

permit easy bandchanging once the operator is familiar with the stations heard around 200 Kc. On the lower band, L2 may require slight readjustment for best reception of weak signals.

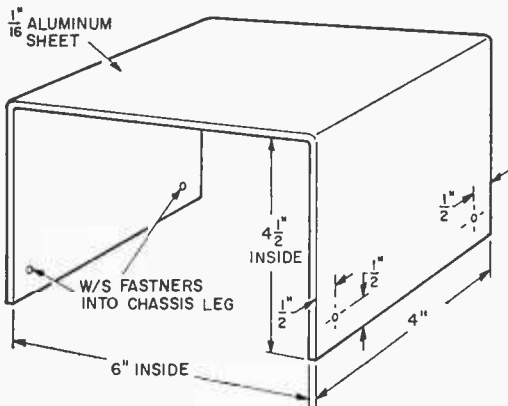
For CBB reception, a ferri-loopstick is used for L1. Inductance L2 consists of three turns



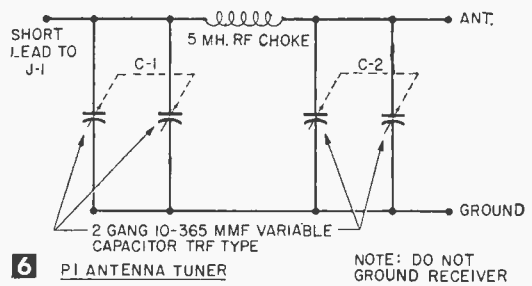
5 A



B CHASSIS DETAILS C-2 MOUNTING HOLES NOT SHOWN, DRILL TO SIZE



C OPTIONAL CHASSIS COVER



6 PI ANTENNA TUNER

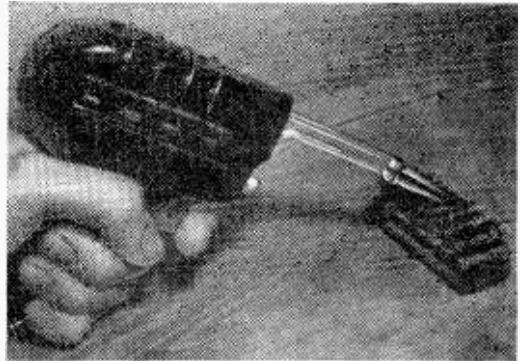
NOTE: DO NOT GROUND RECEIVER

interference can be minimized by reducing the antenna coupling or, in severe cases, by the use of the simple Pi antenna tuner (shown in Fig. 6). The tuner can be built on a small pine block. Adjust C1 and C2 for minimum CCB interference.

Four or five feet of hookup wire is sufficient antenna for CCB reception. The receiver will give good loudspeaker volume on the BC band and on the stronger LW stations. Due to the low power used by most LW stations, however, headphones are recommended for serious LW listening. For speaker operation plug a 5000-3.5 ohm, 3-watt, output transformer into J2.

Inverted Brush Cleans Gun's Tip

- To keep the tip of your soldering gun clean of scale, woodscrew-fasten a brass-bristle suede shoe brush to one end of your workbench. Wipe the soldering-gun tip across the brush occasionally to keep it clean for efficient soldering.—J.A.C.



Why Inside Gun-Tip Care?

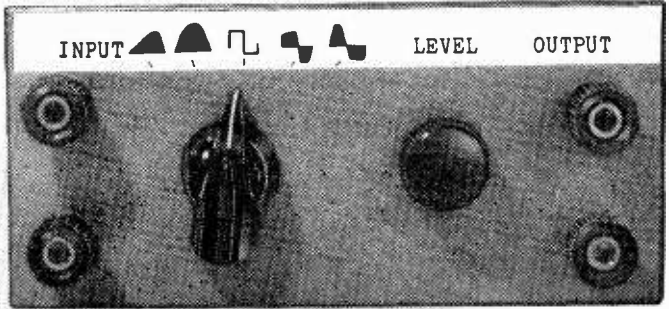
- To receive maximum soldering efficiency and long-tip life, be sure that cleaning and tinning operations of your soldering gun's tip also include the *inside* surfaces of the tip. A gun's tip that is maintained on the outside, but allowed to deteriorate on the inside, is sure to give lowered soldering efficiency and it will shorten tip life.

and adjustment is similar to that of LW operation. The lead from C1 should be connected to the grid end of the loopstick.

A high, long-wire antenna will give best all-round LW reception, though a short length of wire will give satisfactory local reception. Capacitor C1 should be adjusted for best reception on each band and the receiver should not be grounded.

In some localities, interference from strong CCB stations may be bothersome, a trouble commonly encountered with LW receivers having only a single tuned circuit. Such in-

This small grey box performs the electronic hocus-pocus that will convert sine waves into varied waveforms.



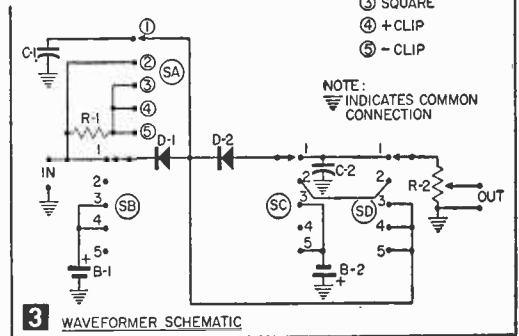
WAVEFORMER

This inexpensive instrument converts 60-cycle ac or audio generator sine waves to sawtooth, half-sine, clipped half-sine, and square waves

By FRANK WOODS, Jr.

- ① SAWTOOTH
- ② HALF SINE
- ③ SQUARE
- ④ + CLIP
- ⑤ - CLIP

NOTE: INDICATES COMMON CONNECTION



This waveformer is inexpensive (cost: less than \$5) and simple to construct. The waveforms generated by it can be used to drive sweep circuits, test amplifiers, check amplifier response, synchronize other equipment, and a host of other test and experimental jobs.

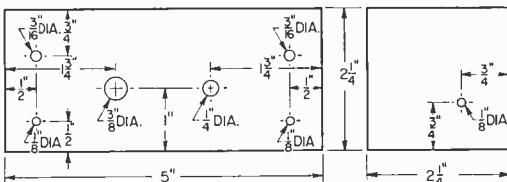
A sine wave is applied to the input terminals, and the switch next to the input terminals is set for the desired waveform; the level control is set for the desired output level. The desired voltage waveform will then be present at the output terminals on the right of the case. It's almost that simple.

Construction. Lay out the front half of the metal case as shown in Fig. 2. All components mount on this half of the case; the back is merely a cover. Mark hole starter marks on the case with an ice pick. Then, with the front and back of the case fastened together,

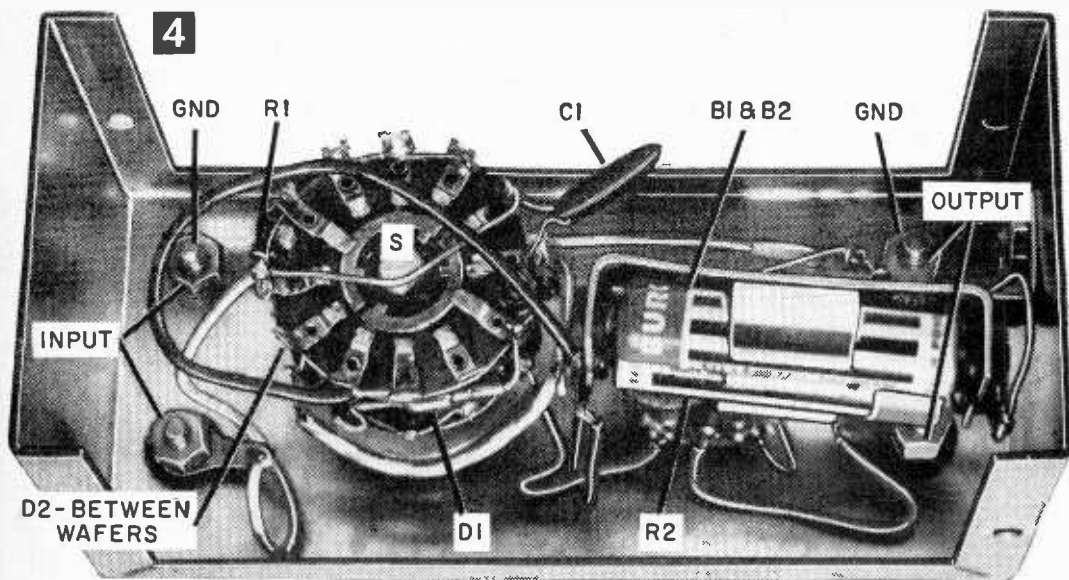
drill 1/8-in. holes for all positions. Separate the front and back of the case and enlarge the specified larger holes to the required dia. with a taper reamer. File the edges to remove burrs.

Saw the shaft of the switch to a length of 1/2 in. Saw the level control shaft to a length of 3/8 in. To avoid damaging switch and level controls, grip shafts in a vise when sawing. This prevents side pressure on bushings. Catch the switch or control when it is cut free from the shaft. The switch is ruggedly constructed, but it is subject to easy damage since its wafers are brittle.

Mount the input and output terminal binding posts. The bottom-chassis terminals are the common terminals; they make electrical contact to the metal case. The top-chassis terminals are insulated from ground by fiber washers between the binding post and the front of the case and between the retaining nut and the rear of the case, and by centering the binding posts. Note that the holes for the top binding posts are larger than those for the bottom. In the original model soldering lugs were used to permit soldering of binding post leads. A second nut on each binding post holds the soldering lug in place. But, the



2 PANEL LAYOUT



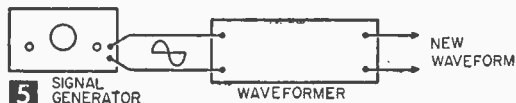
Component layout of Waveformer.

MATERIALS LIST—WAVEFORMER

Desig.	Description
R1	100K, 1/2 W carbon resistor 10% tolerance
R2	500K potentiometer (Lafayette VC-37)
C1, C2,	.1 mfd, 50 v ceramic capacitor (Sprague TG-P10)
S (A, B, C, D)	4-pole, 5-position switch (Centralab PA-1013)
D1, D2	1N54A diode (RCA)
B1, B2	penlite cell (Burgess #7)
	2-penlite cell holder (Lafayette MS-138)
	pointer knob (comes with switch)
	miniature knob (MS-185)
	binding posts (H. H. Smith 220R-red and 220B-black)
	2/4x2 1/4x5" metal box (Bud CU-2104)

soldering lugs are unnecessary since the connecting wires may be fastened between the two nuts.

Mount the switch and the level control on the case. Use retaining hex nuts on these controls behind the panel. Adjust to allow only enough of the control to protrude through the case to enable the hex nuts to be fastened on the front of the panel. Retaining washers between the rear retaining nuts and the rear of the panel will prevent the controls from slipping. At this point in the construction the components which fasten to the case are mounted—except for the battery holder.



When wiring, make connections to the switch so that they can readily be disconnected without damage. This approach will save you grief if you make a mistake in your wiring. Be very careful not to exert undue pressure on the switch terminals or you may twist them out of place or break a wafer.

Limit the length of time that you apply heat during soldering. The diodes in particular are susceptible to heat damage. Use a clean soldering iron capable of supplying a large amount of heat. A lot of heat applied for a short time will do a better soldering job with less chance of damage than a reduced amount of heat applied for a long time. Use *rosin core* solder only!

Figure 5, the circuit diagram, and Figure 4, a pictorial view, are used as a guide for wiring. Wire the switch first. Note that its sections are designated SA, SB, SC, and SD. Section SA is the lower half of the rear wafer; SB is the upper half of the rear wafer; SC is the lower half of the front (nearest the front panel) wafer; SD is the upper half of the front wafer. Connect the wires between terminals as shown and wire in components R1, D1, and D2.

Next, connect capacitors C1 and C2. Then connect the wires which run from the switch and capacitors to the terminals, level control and battery holder.

Now mount the battery holder and make connections to it. The battery holder is mounted with a small hardware bracket 3/8-in. wide with 1-in. and 5/8-in. sides. Solder-fill the battery holder eyelets which form the battery contacts to insure good connection to the batteries. Insert the batteries and fasten the knobs on the switch and level control. Fasten the back to the case. The markings for the front panel are made on a strip of paper 3/8 x 5 in.

Free-hand the waveform symbols which identify switch positions and fasten the strip to the front of the case with a 6-in. strip of cel-

lophane tape. You may have to realign the switch knob to match the waveform markings.

Operation. To use the waveformer connect a source of sine wave signals to the input terminals as shown in Fig. 5.

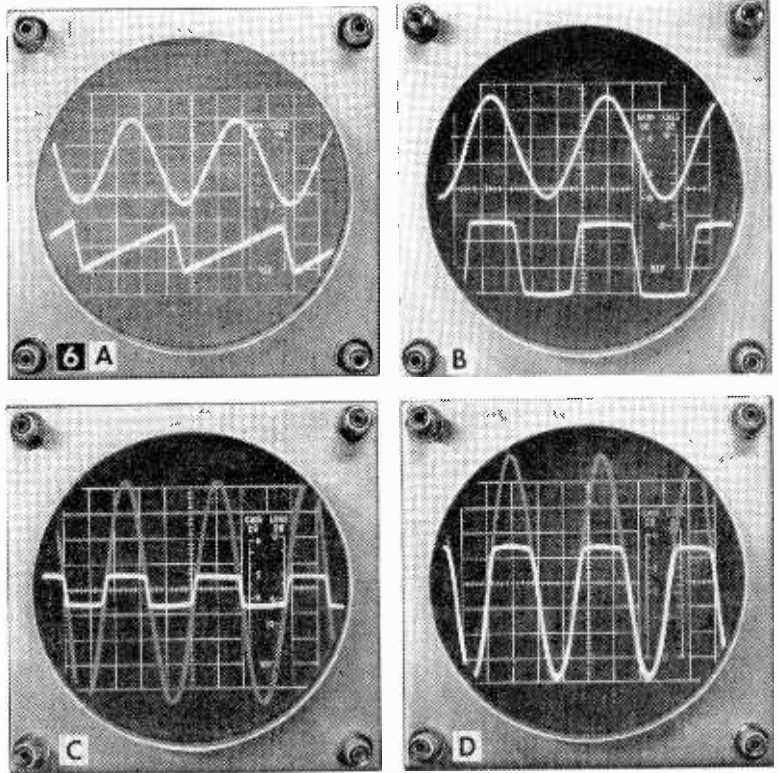
The signal generator may be a 6.3-v filament transformer (supplies 60 cycles only) or an audio signal generator such as the Heathkit AG-9 (frequency 10 cycles upward).

The Waveformer operates through a broad range of frequencies; principal limitations of frequency are imposed by the signal generator for most waveforms. A signal input level of 5 to 15 v is desirable to achieve the best waveforms.

Clean saw-tooth waveforms from about 10 cycles to about 10,000 cycles at .3 v will be produced by a 10-v sine wave. Clean clipped waves from 1.5 to several volts, with a frequency range from 20 cycles to over 20,000 cycles, can be expected.

Science Fair Demonstration. To demonstrate the performance of the Waveformer, a Heathkit AG-9 Audio Generator fed a sine wave to the Waveformer and to a Heathkit S-3 Electronic Switch. The output of the Waveformer was fed to the other set of Electronic Switch input terminals. The output of the Electronic Switch was connected to the vertical input of the oscilloscope. This arrangement permitted simultaneous viewing of the Waveformer input and output waveforms.

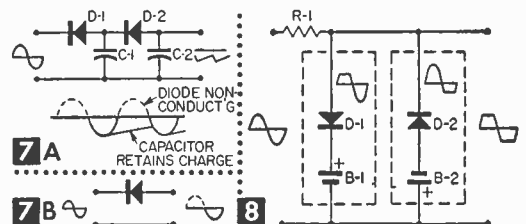
Figure 6A shows the waveform output with the Waveformer switch set for saw-tooth output. Figure 6B shows the output with the Waveformer switch set for square wave. In Fig. 6C the input and output waveforms are superimposed with gains adjusted to show how the Waveformer clips the sine wave. The "squareness" of the output waveform will depend on the magnitude of the input sine wave signals. With larger sine wave input signals, the clipping action produces "squarer" waves. Figure 6D shows the superimposed waveforms with the Waveformer switch set to one of the half-clip positions.

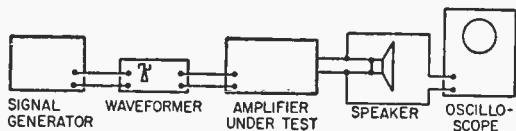


Simultaneous viewing of input to, and output of Waveformer. Explanation is given in text.

Principles of Operation. When the Waveformer switch is set to the sawtooth-wave position, the basic waveforming circuit connections are those shown in Fig. 7A. First consider only D1 and C1. Diode D1 passes only the negative portion of the sine wave. As the sine wave goes negative, capacitor C1 charges rapidly in the negative direction. This produces the steep portion of the curve. As the input signal falls from the negative peak to the zero line, the charge on C1 prevents further passage of current through D1 and capacitor C1 tends to discharge slowly through any load resistance connected across it. The use of D2 and C2 in the circuit improves the performance by providing additional storage and switch action.

When the switch is in the half-wave position the waveforming circuit reduces to that shown in Fig. 7B with diode D2 only in the





9 SET-UP FOR SQUARE WAVE AMPLIFIER TESTING

circuit. It passes only the negative half cycles.

With the switch in the square-wave position, the basic waveforming circuit is that shown in Fig. 8. As the input voltage builds up from zero, current flows through R1 to the output. But when the voltage becomes sufficiently high (greater than 1.5 v) to cause diode D1 to conduct, the current is shorted and the straight top of the wave results. As the voltage decreases toward the zero line, diode D1 ceases to conduct when the voltage to the anode becomes 1.5 v, and the return to zero portion of the waveform results. Diode D2 and bias battery B2 operate on the negative half cycle in the same way. Only R1, D1, and B1 or R1; D2 and B2 are connected in the circuit to produce the half-clipped sine waves.

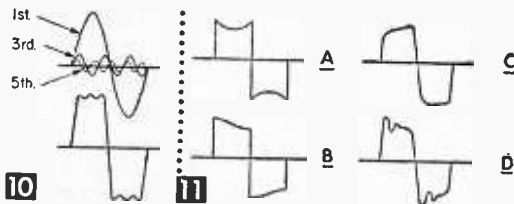
The level control R2 is a potentiometer which permits the setting of a desired output signal level. It is common to all switch positions.

The Waveformer is useful as a teaching tool to explain the operation of diodes, capacitors and pulse circuits, but it has more immediate practical applications. The sawtooth waveform may be used to provide sweep voltage for an oscilloscope. Some of the older inexpensive 'scopes employ sweep circuits that are extremely non-linear and tend to bunch a sine wave applied to the vertical input. If the sawtooth wave of the Waveformer is applied to the horizontal amplifier input of the oscilloscope, the linearity will be improved—if the amplifier has sufficient gain and frequency response.

The half-wave waveform may be used to drive a relay or any other dc device at a specified frequency. Of course, the device to be driven must be of sufficiently low power to allow operation with the signal generator used and the diode in the waveformer. The driven device cannot be operated at frequencies above those to which it can normally respond. The half-clipped sine waves may be used in similar fashion where an opposite "off bias" is desired.

Square-Wave Amplifier Testing. Clipped sine waves may be used to test audio amplifier frequency response. The square wave is applied to the input terminals of the amplifier and the waveform is observed on an oscilloscope connected across the output terminals of the amplifier (see Fig. 9).

A square wave contains a fundamental frequency sine wave and a large number of higher sine wave components. Figure 10

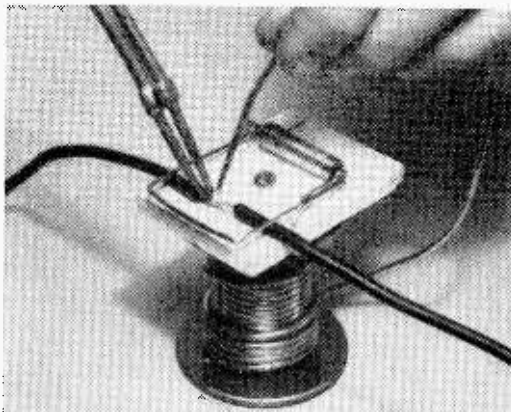


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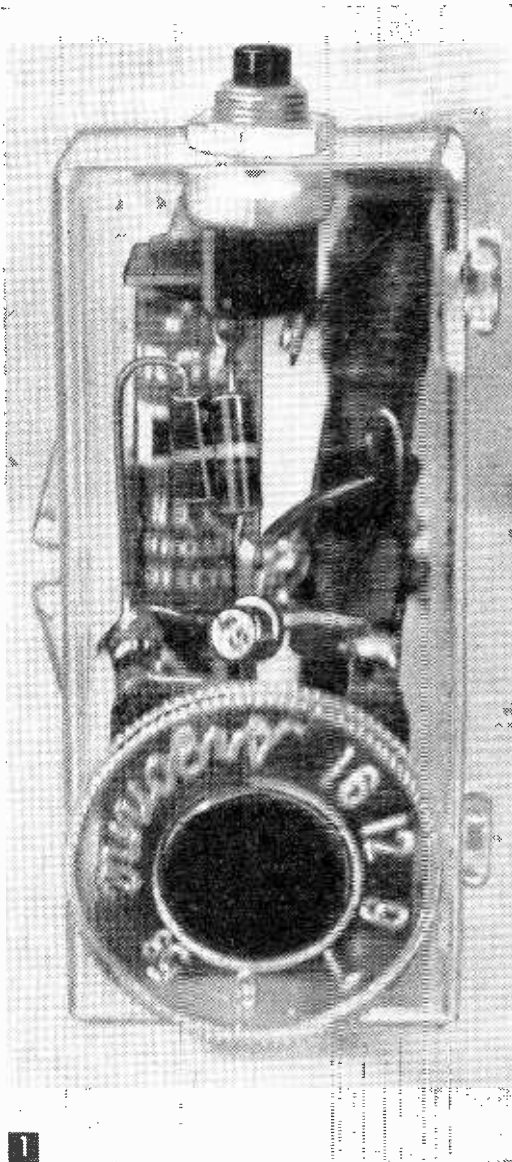
shows the fundamental frequency, the third harmonic, and the fifth harmonic, and how they combine to produce a waveform approaching a square wave. As more odd harmonics of proper phase and amplitude are added, the resulting waveform more nearly approaches a square wave.

Now, if a square wave is passed through an amplifier, amplifier defects will distort the waveform. Discrimination against frequency, and phase shift dependent on frequency (poor frequency response) will produce distinct distortions. If the response of the amplifier is poor at the fundamental frequency, the scope connected at the amplifier output will display a square wave with drooping midsections as shown in Fig. 11A. Phase shift is indicated by a waveform such as that shown in Fig. 11B. Attenuation and phase shift at high frequencies is indicated by an output waveform like that in Fig. 11C. Overshoot and ripples in the displayed waveform, as shown in Fig. 11D, are also indicative of high-frequency distortion. A pronounced high-frequency resonance in the amplifier under test will cause the overshoot to be further accented.

Mousetrap Third Hand



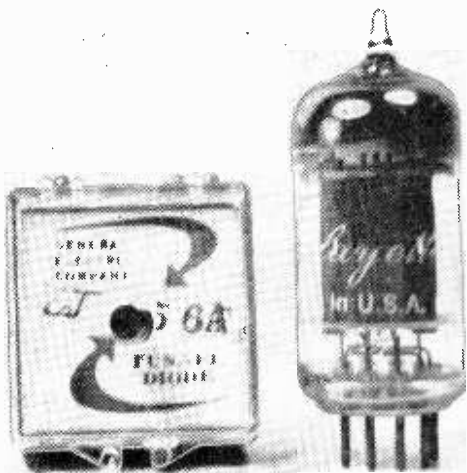
• Need an additional hand to hold small wires and parts while you solder them? To make certain an extra hand is always available when needed, mount the spring mechanism of a mousetrap on the top of your spool of solder as shown. Screw-fasten the mechanism to a tight-fitting cork inserted into the center of the spool.—JOHN A. COMSTOCK.



A simple demonstration construction project, this oscillator employs a tunnel diode which, even in its case (above right), is dwarfed by a vacuum tube.

THIS oscillator is one of the earliest tunnel diode construction projects designed for experimenters. It is an effective demonstration device, and it will attract attention by virtue of its simplicity and the fact that the tunnel diode is a novelty. For the builder, it is a painless introduction to the operation and use of the tunnel diode.

In July 1959 the General Electric Research Laboratory announced progress in the development of tunnel diodes, and offered them in limited quantities at \$75 per unit for labora-

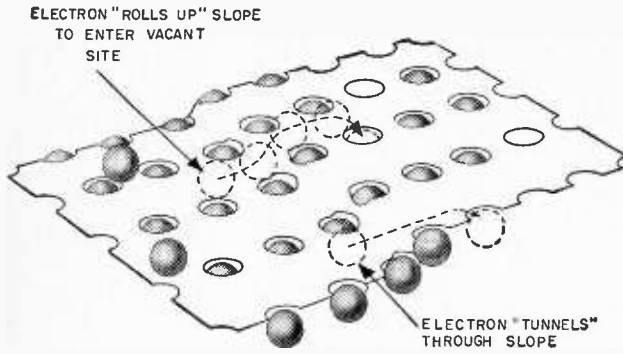


Tunnel Diode Broadcast Oscillator

The tunnel diode—newest member in the fast-growing family of semi-conductors—is giving its first cousin, the transistor, an inferiority complex. Here's a project which helps to explain why

tory use. Prices have been decreasing—thank goodness!—since that time and at the time this article goes to the printer are below \$10. Obtain one now, and get in on the ground floor of an exciting new electronic device. Within a year or two tunnel diode prices should have dropped to a dollar or two a unit, and you will have sufficient knowledge to build the many circuits that are possible with this device. The tunnel diode will be the subject of many science fair and engineering day displays, and it will soon be a common component in TV, communications, computer, and other electronic units.

The circuit of the tunnel diode oscillator



Here—in an extremely simplified diagram—is how the tunnel diode operates. Drawing represents a structure similar to a Chinese checkerboard, with one side slightly raised. Holes on the left side (which represent an n-type semiconductor) are filled with marbles, with a few left over and sitting on top. Right side (representing a p-type semiconductor) has a few holes vacant. The slope represents the potential barrier. A marble (or electron) from the left, can—after being given a push—enter a hole on the right side by rolling up the slope and dropping in. Or, without the push, it can miraculously “tunnel” through the board and appear in a hole. The former process is used in conventional diodes and transistors. The latter represents what happens in tunnel diodes.

THE tunnel diode was first reported by a Japanese scientist—Dr. Leo Esaki—in 1958. It takes its name from the phenomenon that makes its operation possible: quantum-mechanical tunneling.

As with transistors, it depends on the transfer of an electrical charge across a p-n junction, the region between a p-type semiconductor, which has an excess of positive carrier or “holes” (empty electron states), and an n-type, which has an excess of free electrons.

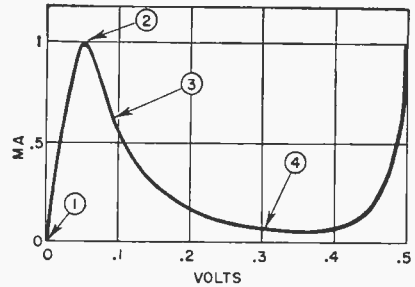
The opposite sides of this junction take on a charge which resists the movement of the “holes” and electrons across it. In the transistor, a charge carrier must be emitted into a region where its energy can be boosted by an outside voltage. It is then collected on an output electrode. The speed of this process is limited by the time it takes the charge carrier—having left the emitter—to traverse the control region and appear on the collector. This time limits the frequency at which the device can function and is quite long compared to, say, the time needed for a signal to travel an equivalent distance along a copper wire.

The quantum-mechanical theory says there is another way in which the particles can pass the barrier: an electron has a small, but definite possibility of disappearing from one side of the potential barrier and re-appearing simultaneously on the other—even though it does not have enough energy to surmount the barrier. It is as though the particles “tunnel” under the barrier, setting up almost instantaneous surges of current. Thus, in the tunnel diode, the signal moves with the same speed as it would in a copper wire—the speed of light.

The construction of a tunnel diode gives it some other

is shown in Fig. 2. Resistors R1 and R2 divide the voltage from the 1.5-v battery down to about 0.15 v, the approximate voltage for negative resistance operation of the tunnel diode. Resistors R1 and R2 were chosen so that R2 would be a fraction (about 1/10th in this case) of the tunnel diode negative resistance (which is about 150 ohms). Inductor L and

Unique Circuit Simplifier THE TUNNEL DIODE



TUNNEL DIODE
CURRENT-VOLTAGE CHARACTERISTICS

PTS ① TO ② - POSITIVE RESISTANCE
PTS ② TO ④ - NEGATIVE RESISTANCE
PT ④ ON — POSITIVE RESISTANCE

interesting characteristics. Its p-n junction is made of materials more heavily loaded—or doped—with impurities than conventional diodes, and made so that the barrier between p and n sections is extremely thin, less than a millionth of an inch thick.

So long as no outside voltage is applied across the p-n junction, there is no net current—since the electrons tunnel back and forth easily through the barrier in both directions. Apply a small voltage, however, and current appears. Add still more voltage, and current decreases. Add more, and current increases again.

In the range where an increase in voltage results in a fall-off of current, the tunnel diode is said to have “negative” resistance—making it suited for use as an amplifier or oscillator.

This negative resistance quality, combined with speed-of-light operation, makes possible a very high frequency response. Engineers confidently expect oscillation frequencies of more than 10,000 megacycles.

Some other outstanding features:

- It is smaller than a transistor and, because of its simplicity, ultimately will be just a fraction of its present size.

- It is affected very little by environment. The tunnel diode can operate at the near-absolute zero temperature of liquid helium or—at the other end of the thermometer—at temperatures up to 650° F, while conventional silicon diodes won't operate above 400° F.

- It has a low noise level, only parametric amplifiers and masers competing closely with it. And of these, only the tunnel diode can operate directly from a battery.

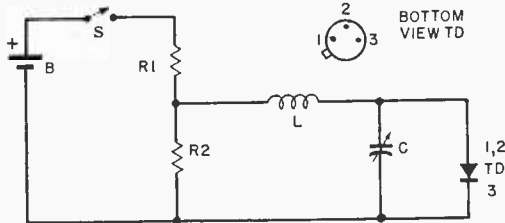
capacitor C form a resonant circuit that controls the oscillations of the tunnel diode, TD. (Several symbols for tunnel diodes have been suggested and are presently used by different manufacturers. The conventional symbol is shown in Fig. 2).

Correct polarity of the voltage applied to the diode is important—Be careful not to re-

MATERIALS LIST—TUNNEL DIODE OSCILLATOR

Desig.	Description
R2	27 ohm, 1/2 watt carbon resistor, 10%
R1	270 ohm, 1/2 watt carbon resistor, 10%
L	broadcast band ferrite loop antenna (Miller 6300)
C	365 mmf. miniature tuning capacitor (Lafayette MS-445)
TD	tunnel diode General Electric 1N2939 (ZJ56) or 1N2940 (ZJ56A)
S	miniature momentary contact switch (Grayhill 4001)
B	1.5 v. penlite cell (Burgess #7)
	penlite cell holder (Lafayette MS-137)
	1 x 1 3/16 x 2 7/8" plastic case (Lafayette MS-157)

Components for this project may be obtained from Lafayette Radio, 100 6th Avenue, New York 13, N. Y.



2 SCHEMATIC

Four holes are required in the plastic case. Start these holes with a heated ice pick. Capacitor C and the switch S are on the case centerline. The hole for the capacitor is 5/8 in. from the top of the case. The mounting hole for switch S is centered on the bottom side of the front half of the case. Locate the battery holder mounting holes by using the holder, against the back half of the case, as a guide. Enlarge the tuning capacitor and switch mounting holes to 5/16 in. dia. with a taper reamer. Wash the case with soap and water and rinse with clear water to remove fingerprints after all of the holes have been made.

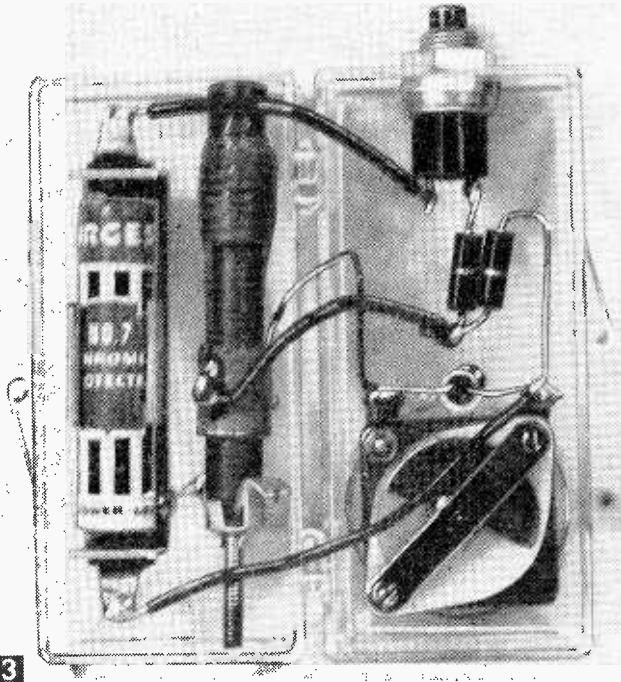
Mount the switch S, the capacitor C and the battery holder. Then wire the circuit. Use a hot, clean soldering iron and rosin core solder to make connections. Minimize the danger of heat damage to the tunnel diode by grasping the leads with needle nose pliers between the tunnel diode case and the connection point during soldering. When wiring is complete, insert the battery in the holder.

This oscillator operates in the broadcast band. To demonstrate its operation, tune in a relatively weak station on a broadcast receiver. Push the switch S on the oscillator. A momentary contact switch, it is "on" only when depressed. Hold the tunnel diode oscillator near the broadcast receiver antenna and tune C till a whistle is heard. At this point, the tunnel diode oscillator is tuned to the frequency of the received station.

The short length of wire furnished on coil L was removed, but if you have trouble picking up the signal on your receiver, simply connect a 6- to 8-in. length of wire at point A (Fig. 2) and provide a hole for it in the plastic case. This lead will act as a short antenna and provide better coupling of the signal to the receiver.

The unmodulated signal from this oscillator will not be audible in a receiver unless the receiver is tuned to a station. The oscillator signal beats against the received signal.

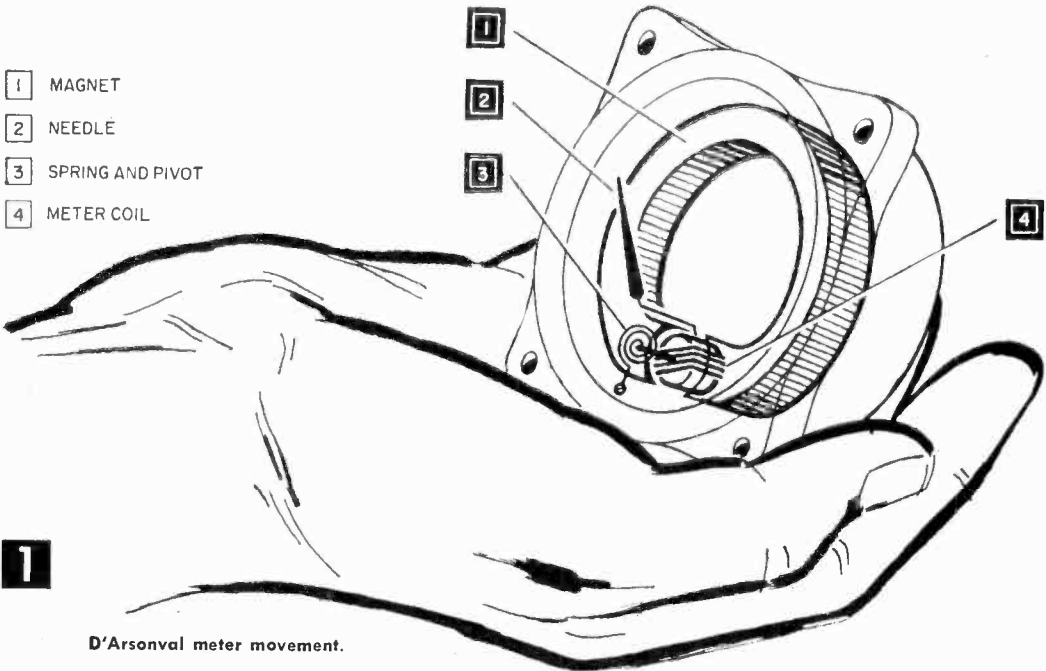
If you have difficulty check the battery voltage, and check capacitor C for a possible short. Remove the battery and the tunnel diode when checking any portion of the circuit with an ohmmeter. A change in the value of R2 may be required. Disconnect it and substitute a 100-ohm variable resistor. Adjust until unit operates, then disconnect and find value, and permanently install a resistor of this value for R2.—FRANK WOODS, JR.



3 Rear view of oscillator with case open.

verse it. The General Electric 1N2939, 1N2940, and 1N2941 (formerly designated as the ZJ-56 series) are housed in TO-18 cases and have the pin connections shown in Fig. 2. Note that leads 1 and 2 are both connected to the positive electrode.

The rear view of the tunnel diode oscillator with case open is shown in Fig. 3. Use Figs. 2 and 3 for guidance in assembling the unit and wiring it.



D'Arsonval meter movement.

Meters and Multimeters

By FORREST H. FRANTZ, SR.

THE type of meter we are concerned with has an electromagnetic mechanism known as a d'Arsonval movement. From it I'll show you how to make voltmeters and ammeters and ohmmeters.

How Meters Work. The d'Arsonval meter (Fig. 1) contains a permanent magnet, a coil that is free to rotate about its pivot axis, a needle attached to the coil and a spring that resists displacement of the coil from zero and tends to restore the coil to zero.

The torque that causes the coil to turn is developed when a current passes through the meter coil. The amount is proportional to the current passing through the meter coil. The coil and needle are supported by low friction bearings so that mechanical resistance is low. The pole pieces conduct the flux from the magnet poles and the circular iron core over which the coil rotates. This core and the curved pole piece faces assure that the magnet's flux is always cutting the coil windings at right angles.

The most common basic d'Arsonval meter movement is the 0-to-1 milliamperere dc meter.

Designing Your Own Meter Instruments. Assume for simplicity in the examples, that all of the work is being done with a 0-1 ma. meter. The resistance of the meter, if not

known, can be determined by the circuit of Fig. 2. Adjust pot R, which is connected as a high resistance rheostat, for full scale meter deflection. Connect shunt RS across the meter terminals, and adjust it until the meter deflection is reduced to half scale. The resistance to which RS is adjusted is the resistance of the meter movement. The resistance of RS may be measured with an ohmmeter or Wheatstone bridge.

Once you know the basic movement (I_m) and the resistance (R_m) of the meter, you can increase the current range with a shunt resistance (R_s in Fig. 3.). The value of the shunt resistance for a new range is determined using these formulas:

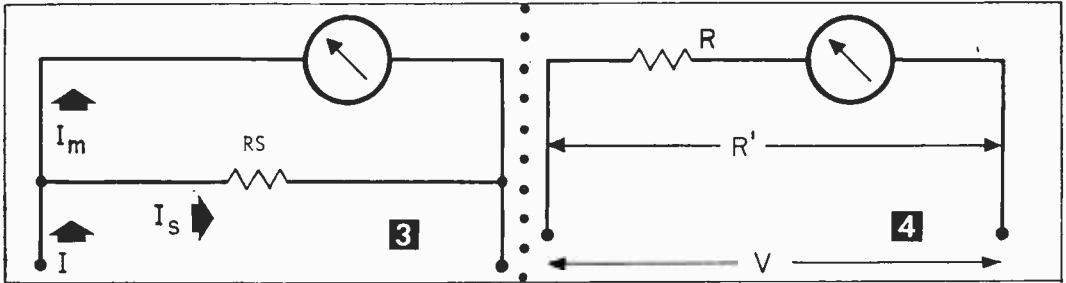
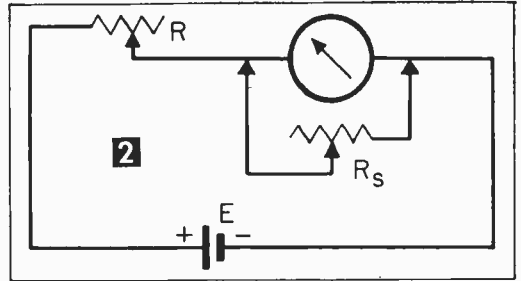
$$(a) I_s = I - I_m$$

$$(b) R_s = R_m \left(\frac{I_m}{I_s} \right)$$

You can buy a 1% shunt resistor, or you can make the shunt by winding insulated resistance or magnet wire on a form, such as a matchstick or a Bakelite bobbin. Or you can use a rheostat, adjust it to the proper resistance, and lock it with a cement seal between the shaft and bushing. Most shunt resistance values will be so low, though, that it's best to wind your own.

In designing an extended-range meter

- 2 Circuit for measuring meter resistance. With RS out of the circuit adjust R for full-scale meter deflection. Then connect RS across the meter as shown and adjust it till the meter reads half scale. The meter resistance is equal to the value to which R is adjusted.
- 3 Extending the range of a current meter with a shunt resistance.
- 4 Converting a milliammeter to a voltmeter with a series resistance.



using a basic meter movement, try to select a range that is a convenient multiple of the meter scale range. Multiples of 10 are best since you can read the meter directly, and have to supply only the decimal point. Two and five are the next best choices for scale number multipliers, and of course, multiples of 10 can be used with these also. (Same applies to voltmeters.)

The circuit for converting a milliammeter to a voltmeter is given in Figure 4. These formulas are used:

$$(a) R' = \left(\frac{V}{I_m} \right)$$

$$(b) R = R' - R_m$$

By connecting a switch (Fig. 5) you can make a multi-range voltmeter.

These current range extensions and voltmeter conversions are solved by applying Ohm's law. In the ammeter application of Fig. 3, the meter and shunt are in parallel. Thus, the voltage across the meter equals the voltage across the shunt. Therefore, the current through the meter times the meter resistance equals current through the shunt times the shunt resistance. And the current into the combination equals shunt plus meter current. The voltmeter arrangement of the second problem (Fig. 4) was based on the idea that the current through the shunt must equal the current through the meter, and the sum of the voltage drops across the meter and the series resistor equals the voltage drop across the combination.

What about measuring resistance with a meter? There are several approaches. The first (Fig. 6) utilizes an ammeter and a voltmeter to measure the current through, and the voltage across, an unknown resistance Rx. Then Rx is calculated from Ohm's law. For

example, if V is 4.5 v and I is .005 amp (5 ma.), using:

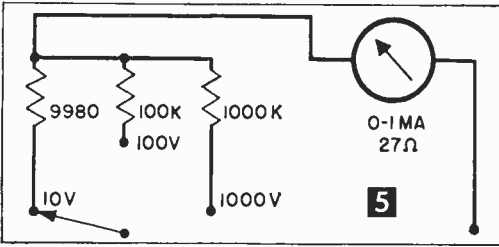
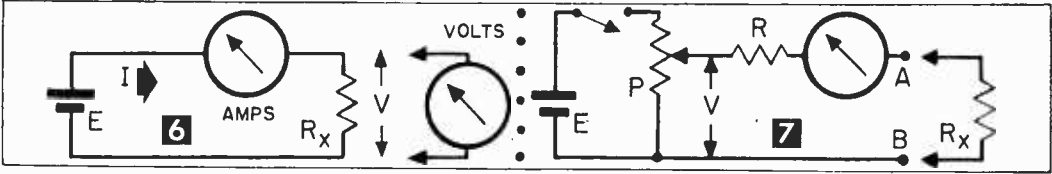
$$R_x = \frac{V}{I}. \text{ Then } R_x = \frac{4.5}{.005}, \text{ and } R_x = 900 \text{ ohms.}$$

This method is cumbersome, so let's see if we can get around it. If we know the voltage E of the battery, do we need to measure V? No, if Rx is much greater than the resistance of the meter measuring the current I. This leads us to the circuit of Fig. 7, where a pot P is employed to adjust the voltage V to a value around which we'll design our ohmmeter. Assuming that we'll use a 1-ma, 27-ohm meter movement, as before, we'll want the resistance of P to be about 500 ohms. This choice is made on the assumption that the current from the battery should be 10 or more times the current through the meter, for accurate results. The resistance across A and B is zero, if we short these terminals. Therefore the resistance of R and the meter should be 5v (the design voltage) divided by the meter current, .001 amp. Resistance R, therefore, is 5000 ohms, minus the meter resistance of 27 ohms, or 4973 ohms. Since 5000 and 4973 ohms differ by only about 1/2%, you can let R equal 5000 ohms without noticeable error. The ohms scale may be calculated in terms of the I scale on the meter by assuming different values of Rx using this formula:

$$I = \frac{V}{R + R_x}$$

Thus, Rx in ohms I in ma.

0	1.000
500	0.909
1000	0.832
2000	0.715
3000	0.625
4000	0.555
5000	0.500



5 A simple 3-range voltmeter. Resistance values were obtained by the method of Fig. 4 and rounded off to practical values.

6 Determining resistance by the volt-current (Ohm's law) method.

7 A simple ohmmeter circuit. In the example in the text, P is 500 ohms. For less critical zero adjustment, substitute (for P) a 100-ohm pot in series with a 400-ohm resistor.

8000	0.384
10,000	0.333
15,000	0.250
20,000	0.200
30,000	0.143
50,000	0.091
100,000	0.048
200,000	0.024

You can compute additional values yourself. Note that the half-scale meter deflection is equal to R for any meter combination which uses this arrangement. That's a handy piece of information for estimates, before you begin design. The ohm readings may be obtained using a table such as that above, or an ohms scale may be pasted on the meter glass. The switch S is turned on only when the ohmmeter is being used.

The potentiometer P may be made up of a 100-ohm pot in series with a 400-ohm, fixed resistance. This arrangement makes the zero resistance adjustment less critical. You can double battery life by doubling the value of P (use a 200-ohm pot and an 800-ohm resistance) with a decrease in accuracy that's negligible.

To convert a basic dc meter movement for ac measurements, rectifiers are used. Their difference in forward and back resistance is so great that we generally assume a rectifier acts as a switch. The rectifier circuit of Fig. 8A, not often used with meters, conducts during only half the ac input cycle. The full-wave half bridge of 8B passes current during all of the input cycle. A 2.7K resistor for each R works well with most germanium diodes. The output current is about 0.72 times the input current. The full bridge of Fig. 8C passes current during the entire input cycle also, but presents a greater output for a given input current. The output current is 0.9 times the input current.

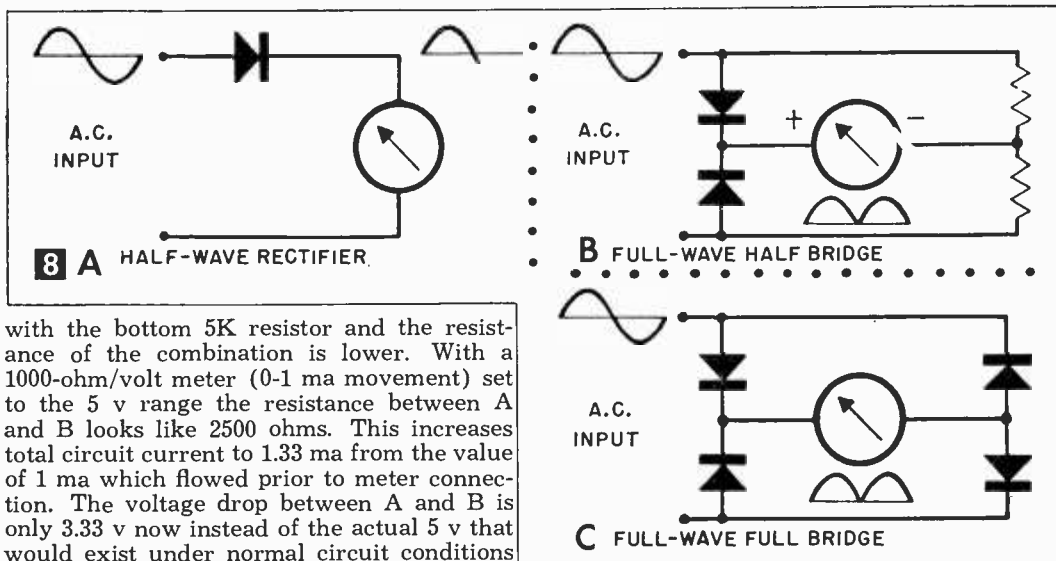
The rectifiers may be germanium diodes or copper oxide types. Germanium diodes are more readily available and cover a broader range of frequencies. The GE 1N64, Sylvania

IN34A and the Raytheon IN66 are suitable.

The shunt resistances for current meters and the series resistances for voltmeters of the ac variety may be determined in the same way as they were determined for dc instruments, but bear in mind that the transfer factor of the rectifier arrangement alters the value of the ac voltage required for full scale deflection, and that the apparent meter resistance is changed, too. Use the circuit of Fig. 2 for experimentation, considering the rectifier input terminals as the meter terminals and an ac voltage source instead of a battery to determine the apparent meter resistance. The current through the meter is the voltage across R divided by the resistance of R. Then, the formulas of Fig. 3 and 4 can be applied.

Multimeters. There are many meter kits available at low prices. They're called VOM (volt-ohm-milliammeter) or multimeter kits and are good for measuring ac and dc current and voltage, and for measuring resistance. Although many factors enter into the choice of a meter kit, the primary consideration is meter sensitivity: the number of ohms resistance that the meter movement and the series resistance present between the input terminals of the meter, divided by the corresponding voltage range. This is expressed in ohms/volt. This number is a function of meter movement current for full scale deflection. A 1-ma meter has a sensitivity of 1000-ohms/volt; a 200 microamp. meter has a sensitivity of 5000 ohms/volt; and a 50 microamp. meter has a sensitivity of 20,000-ohms/volt.

The sensitivity is important, because when you connect a voltmeter into a circuit to make a measurement, you're connecting a resistance across the circuit. If you connect too low a resistance across the circuit, you'll draw enough current from the circuit to get a wrong voltage reading. Figure 9 illustrates what can happen. When you connect the meter across AB, its resistance is in parallel



Meter rectifier circuits.

with the bottom 5K resistor and the resistance of the combination is lower. With a 1000-ohm/volt meter (0-1 ma movement) set to the 5 v range the resistance between A and B looks like 2500 ohms. This increases total circuit current to 1.33 ma from the value of 1 ma which flowed prior to meter connection. The voltage drop between A and B is only 3.33 v now instead of the actual 5 v that would exist under normal circuit conditions—a big error. However, if a 20,000 ohm/volt meter were used to make the measurement, the resistance paralleling R2 would be 100,000 ohms on the 5-v range, and the resistance between AB would be 4760 ohms. The total current through the circuit would be 1.023 ma, and the voltage between A and B would be 4.87 volts, very close to exact.

Using a Multimeter. My young son uses his meter to check the resistance of a toy motor. If it's open, the needle reads infinite resistance (no deflection). Sometimes he checks his toy motors by using them as generators, switching the meter to a low dc voltage or current range and looking for a meter deflection as he rotates the motor shaft.

The motor used as a generator with a meter indicating output voltage across or current through a resistance makes a good rpm indicator for lathes, drills, motors and engines (including cars). The same scheme may be used for a speedometer for bicycles or a child's wagon. Equipped with a propeller or vane that is outfitted to face into the wind or equipped with anemometer type cups, this same electrical arrangement may be used to measure wind speed. The hook-up of Fig. 10 may be used for any of these applications. The size of the series rheostat must be determined experimentally and may include a series resistance in the meter if you use the dc voltage range of a VOM for the meter. A more versatile approach is to use a dc current range.

Usually the pot adjustment can be made to calibrate the meter so the existing meter scale with a suitable fraction or multiple of 10 will provide the desired range of rpm or mph. Sometimes, though, you'll have to provide a paper and ink scale, and you'll have to figure out the mechanical coupling.

A multitester's ac volts range can be used

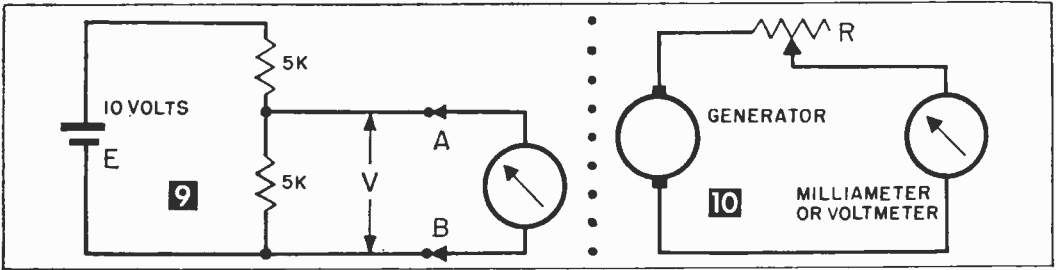
with an audio amplifier to produce an audio millivoltmeter, a sound survey meter or an applause meter (Fig. 11A). Figure 11B shows resistance-capacitance meter coupling, and 11C shows transformer coupling to the meter. You can rig up a calibration template for the amplifier volume control so you can use it as you'd use a range switch. You can use the meter's decibel or voltage scales.

The ac voltmeter ranges may be used to measure capacitance of paper, oil or mica dielectric capacitors. Use the circuit arrangement of Fig. 12. Adjust the pot till the voltages at A and B are equal. Then disconnect the pot and measure its resistance R. For the capacitance in microfarads, substitute the value of R in this formula:

$$C = \frac{1,000,000}{377R}$$

This circuit works best with higher ac voltages, but 30 v is the top, safe limit. (The voltages across C and R won't add up to the applied voltage.) Get the 60-cycle ac voltage from a transformer—either a filament transformer or a train transformer will do. And, don't use this arrangement to measure low-voltage electrolytic capacitors, or you may ruin them! You can use a 6.3-v transformer in the circuit to test electrolytic capacitors rated 100 v or more, without damage.

Beginners can use a meter to get a good understanding of electricity. Use it to find out: What happens when you connect batteries in series and parallel; what happens to the battery voltage when you decrease the resistance connected to it; what happens to the voltage and current when resistors are connected in series or parallel; how to apply

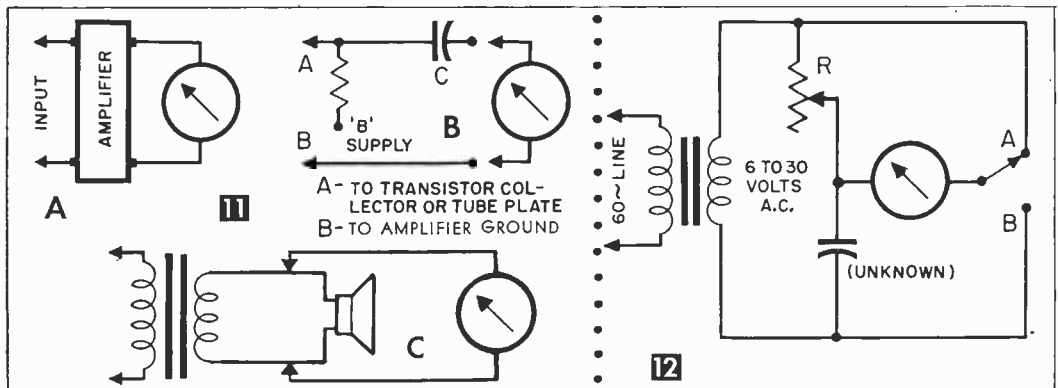


Ohm's law; the difference in the resistance of a light bulb before it's turned on and after it has been on a while. Incidentally, never use the ohms scales to measure resistance in a circuit under power. Always disconnect the voltage from the circuit before you measure resistance.

The resistance ranges may be used to check light bulbs and lamp wiring. If the ohmmeter needle deflects at all on the low ohm range, the bulb (or lamp wiring with a good bulb in the lamp and the switch on) isn't open and if the meter needle doesn't hit zero, the bulb or lamp isn't shorted. In the case of a table or floor lamp, if you get this kind of indication, everything's good, except that you're not sure that the switch will work. When you turn the switch off, the meter needle will return to its normal rest position if the switch is operating properly. This is the technique for trouble-shooting radios, electrical appliances and home and car electrical wiring.

Another example of the continuity check just outlined is locating tubes with open heaters in a radio or TV. If none of the tubes in an ac-dc (transformerless) radio light up when the radio is on, the probable cause of trouble is an open tube heater. An open tube heater will also cause a TV set to be inoperative, but won't necessarily prevent all tubes from lighting up. To check tube filaments for

11 Using an amplifier with an ac voltmeter as an audio millivoltmeter, sound survey meter or an applause meter (a); R-C coupling meter to amplifier (b); and meter-connected amplifier output transformer (c).



9 Illustrating how a low sensitivity voltmeter up-sets low current circuit operation and gives false readings (see text).

10 A toy motor used as a generator in this simple circuit has many practical uses. Determine R experimentally.

opens, use the ohmmeter test leads across the heater pins (power disconnected). The pin numbers may be obtained from tube manuals.

An ac voltmeter is useful in checking ac line voltages, transformers, circuit wiring, oscillator output, model railroad and toy circuits and for numerous other applications. The dc voltmeter is useful in checking batteries (check them for voltage with the normal load connected), checking dc power supplies, trouble-shooting in radios and car wiring, and for numerous other applications. You should have little difficulty in voltage measurement.

Current measurements are not used as commonly in routine trouble-shooting and experimenting, but are becoming more important with the advent of the transistor. The important thing to remember in making dc current measurements is that the meter is connected in series with source and load. That is, one of the leads connects to the source of voltage and the corresponding connecting point on the device that is receiving power. You might look at it as simply cutting one of the leads in the circuit and connecting the current meter to the lead ends that you've created. The microampere range on the meter is also useful as a current detector in Wheatstone bridge circuits.

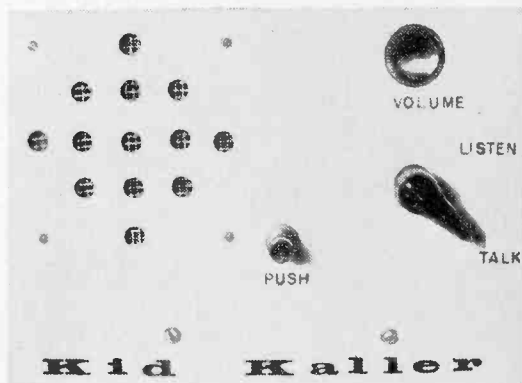
Kid Kaller

By HOMER L. DAVIDSON

WHEN the children are out playing, they can never be found when wanted. With this unit, however, simply by pushing in on a push-button switch you can call them. And then you can hear their reply or listen in on the outdoor happenings.

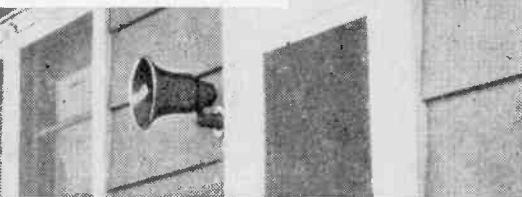
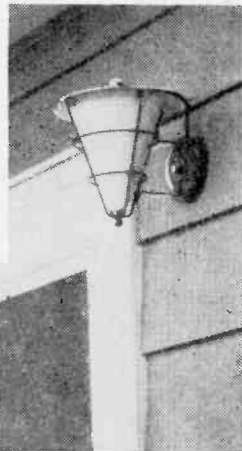
A DPDT two-position is used to switch from Talk to Listen position. A SPST switch of the momentary-hold type shuts the unit off. By using this type of a switch the battery will be on only when pushed, and outside noise will be present only when listening. The unit responds at once when pushed on, since there are no tubes to warm up.

Circuit Description. This inter-

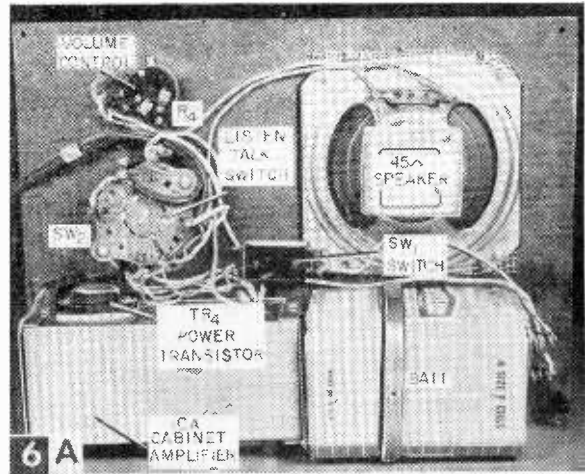
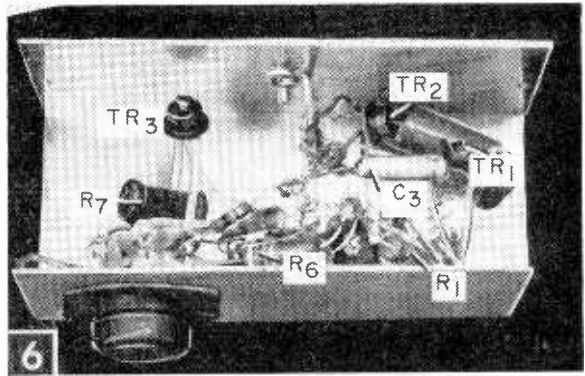
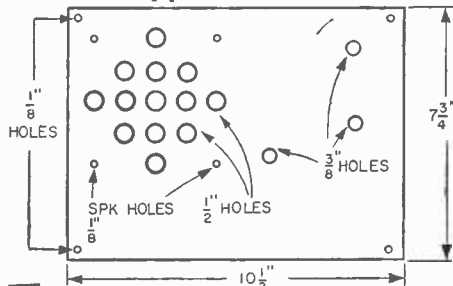
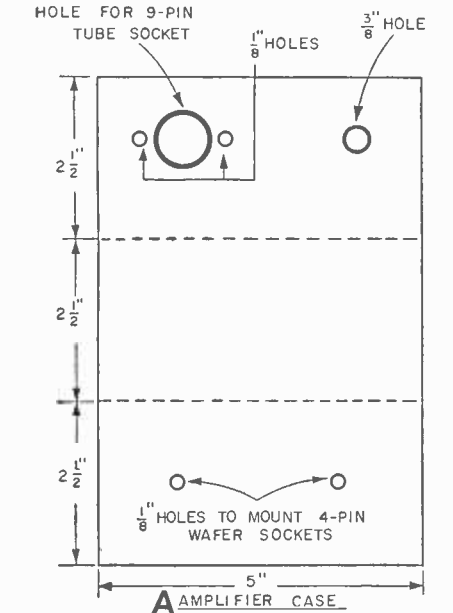
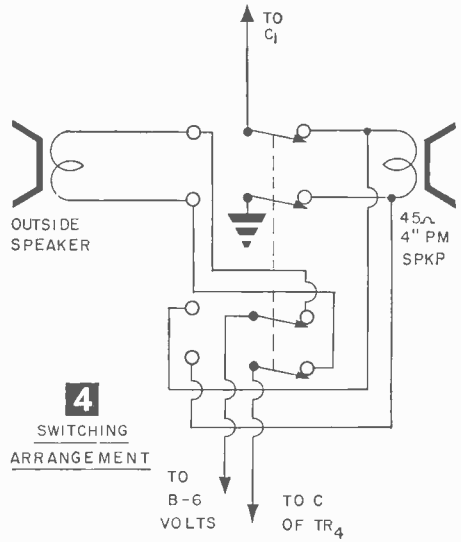
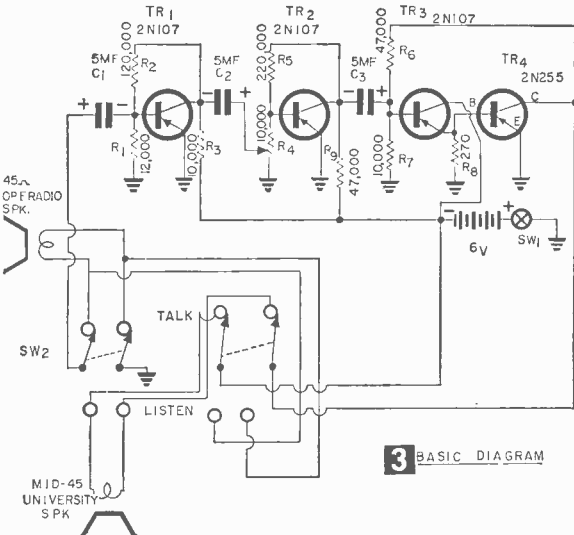


Kid Kaller can be installed in kitchen cabinet, as here, for instant communication outdoors.

Outside speaker can be located near back door, on post in yard or on garage.



com caller is built around four transistors. The first three are 2N107—PNP low-cost types. A 2N255 CBS power transistor is used in the output circuit for greater volume. From the input of the house unit a 45-ohm voice coil permanent magnet speaker is placed in the base circuit of the first cascade stage. This speaker, used as a microphone, is coupled to the base circuit through a 5 mfd electrolytic capacitor. The signal is amplified, then capacitively coupled to the second transistor stage through a small volume control that controls the output volume. Both emitters of the first two stages are grounded. A base resistor is tied to each collector terminal.



Amplifier and its case (6) and back view of complete unit (6A), except for outside speaker.

In the third audio stage the collector is tied directly to the battery, while the emitter terminal is wired directly to the base circuit of the power transistor. The base return

resistor is tied to the collector circuit of the power transistor. A 45-ohm, paging type speaker is switched into the output of the 2N255 collector circuit. As the output

MATERIALS LIST—KID KALLER

Desig.	Description
C1, C2, C3	5 mfd miniature elect. capacitors
R1	12,000-ohm, 1/2-watt carbon resistor
R2	120,000-ohm, 1/2-watt carbon resistor
R3, R7	10,000-ohm, 1/2-watt carbon resistor
R4	10,000-ohm I.R.C. volume control
R5	220,000-ohm, 1/2-watt carbon resistor
R6, R9	47,000-ohm, 1/2-watt carbon resistor
R8	270-ohm, 1/2-watt carbon resistor
TR1, TR2, TR3	2N107 GE transistors
TR4	2N255 CBS power transistor
SW1	SPST hold-type push switch
SW2	Rotary DPDT two-position switch
	Operadio 45-ohm 4" PM spkr. (microphone)
	Mid-45 University paging-type spkr. (outside)
	6-volt battery, lantern type

impedance of the power transistor is around 48 ohms, this insures a perfect match for amplification.

There will be no need for an output transformer in this type of circuit. The power or voltage to be applied to the circuit is furnished by a heavy duty lantern battery. Since the unit is used only intermittently, the battery lasts a long time.

Construction. Construct the amplifier inside an ICA aluminum case (see Materials List), or make your case, as shown in Fig. 5A, from thin-gage aluminum. Mount all 2N107 transistors directly on a three-lug terminal strip; the power transistor, in a standard 9-pin miniature socket insulated from the metal chassis (see Fig. 6A). There is no need to construct a heat sink for the power transistor since the unit is not on long enough to get warm.

Cut the front panel from hard-tempered Masonite and drill necessary holes before painting (see Fig. 5B). I used a white enamel spray paint so that the small unit would match the kitchen walls. The wire lead to the outside speaker can go directly through the wall through a small hole. Place colored putty around the hole so there will be no danger of weather damage.

Fasten the amplifier unit to the front panel with four small bolts and nuts and secure the PM speaker to the panel also. Mount the double wafer switch directly above the amplifier chassis (see Fig. 6A). A small metal bracket was constructed from aluminum stock to hold the lantern battery to the front panel. The switching circuit is shown in Fig. 4.

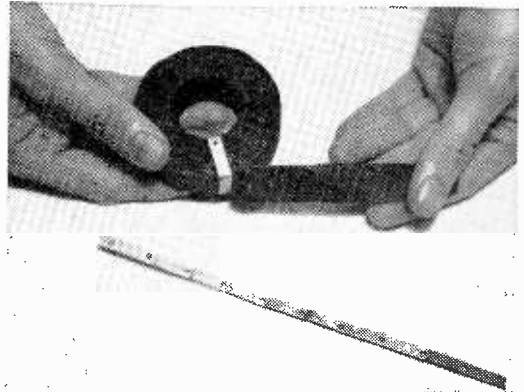
Operation. When the wiring has been completed and the unit installed, except for the outside speaker (which should be wired into circuit but not secured outside), push down on the switch and—with volume half-way up—feedback should occur between outside speaker and microphone speaker.

Then turn the switch to listen position and press the switch again. Again feedback should occur. If it does not, check the wiring of the double wafer switch. Now place the outside

speaker outdoors so that feedback will *not* occur with someone talking into the microphone speaker.

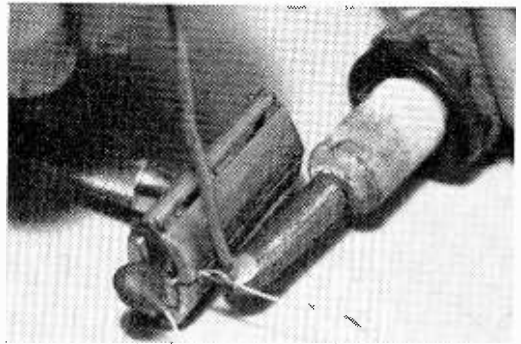
There are many uses for this small unit. The caller can be used as a regular intercom simply by placing a switch on the back of the volume control. Or the outside speaker can be placed on a post in the farm yard so the housewife can speak to her husband outside. Or you may be a rabid bird watcher. The outside speaker can be placed near a bird house and you can hear them while watching them.

Tape Cut-Off



- Rolls of plastic, rubber, and friction electrician's tape have no cutting blade to cut strips to length. A piece of metal cut-off blade removed from a wax paper box makes a good cutting edge. Simply cut off a length of blade that will fit loosely around the roll, overlap it on the inside and solder.—JOHN A. COMSTOCK.

Razor Shunts Iron Heat



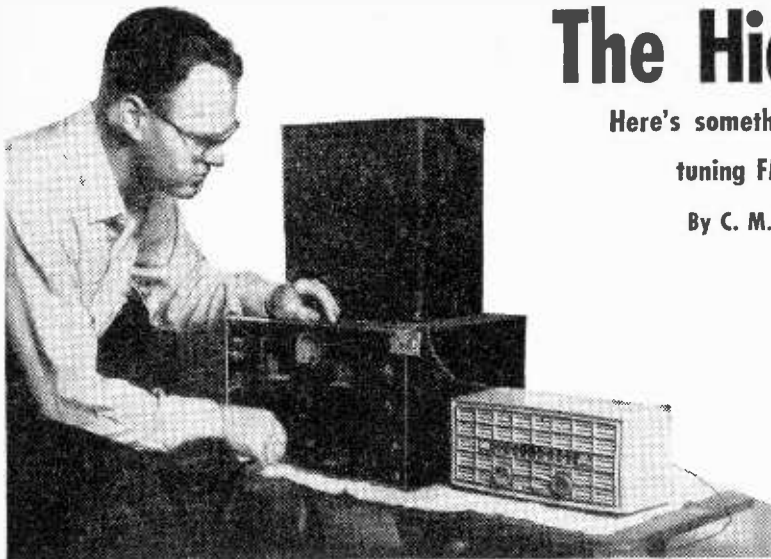
- That discarded razor can serve a useful purpose as a heat shunt when soldering radio parts leads. Clamp the razor over the lead and it will absorb the soldering heat that might otherwise damage or change the value of the radio part.

The Hidden DX

Here's something new in DX —

tuning FM subcarriers

By C. M. STANBURY II



The experimenter's DX special for hidden DX, consisting of a Hammarlund HQ 120 X and a Granco 780. Almost any combination of short-wave and FM receivers will do, but it is better if the SW set is equipped with band spread.

DO YOU own an FM receiver? Chances are pretty good you do, or could, because there are sets in the stores selling for as little as \$29.95. Second question, are you a DXer? If you are, then you're missing one tremendous bet on the FM band.

We're crazy? FM DX is a cross between that found on the Broadcast Band and VHF TV channels. However, DX listeners are missing some very rare catches between 88 and 108 mc, loggings which compare with the most unusual to be found anywhere in the radio spectrum. Hidden on the band are signals which the ordinary FM receiver will never pick up, which even local listeners will probably never hear. But if you have a short-wave receiver, you can. And at a distance, Rare enough for you?

Most of our readers will be familiar with one class of station in this "hidden" group, the satellites on 108 mc, but unless you have special equipment, these require a tremendous amount of patience. A much more inviting target are the *subcarriers* used for background music and storecasting. Believe it or not, such signals you will be able to detect (for DX purposes only), log and QSL with only a reasonable amount of effort.

How's it done? By using AM detection instead of FM. An FM detector measures the deviation between the frequency transmitted and the carrier frequency, subtracts them, and the result is an audio frequency. We have taken WSOM as an example, carrier frequency 105100 kc (105.1 mc). If the signal deviated to 105101 (or 105099) the result would be a 1 kc or 1000 cps audio note. However, should the deviation exceed 15 kc, it

would produce a supersonic audio note which your audio circuits would reject, no speaker could reproduce, and of course you couldn't hear it anyway. Thus WSOM may transmit background music around 105167 (the subcarrier) and no ordinary FM set could ever receive it.

But an AM receiver (detector) responds to variations in amplitude, and in this sense, not to frequency deviation. The subcarrier does produce amplitude variations. Thus if you could tune an AM receiver to 105167 it would pick up WSOM's subcarrier. The sounds would not be enjoyable listening but recognizable as music, and—more important from a DX standpoint—loggable.

But you don't have an AM receiver that will tune the FM band? You don't need one, the FM set will do it for you. Double talk? No.

An FM set receives a signal from the antenna, passes it through one stage of RF amplification (a few have two) then feeds it into a mixer tube where it's converted to an intermediate frequency, the most common of

QSL's received—

"Dear Mr. Stanbury:

"Thank you for your report on reception of WRRR located on Connecticut Hill, 9 miles, southwest of Ithaca, New York.

"The subcarrier you detected was our 67 kc multiplex subcarrier for background music . . .

"You may . . . be able to detect bursts of high frequency tone (19 kc to 29 kc) at station identification time and also our 45 kc telemetering frequency at odd intervals."

Northeast Radio Corporation

* * *

"Dear Mr. Stanbury:

"This will acknowledge your letter of 7 August 1959, relative to reception of radio signals from the Discoverer Satellite.

"Time, frequency and emission would certainly indicate that the signals you received were from the Satellite . . ."

From a Government Agency

CONFIRMING RECEPTION of	
the SUBCARRIER of	
W 5 0 M	SALEM, OHIO
KC/S 105167	DATE December 10, 1969
BY <i>C. S. Frank Ph Eng'r</i>	
<i>Thanks</i>	

QSL for an FM subcarrier. The card was prepared by the author to expedite verification.

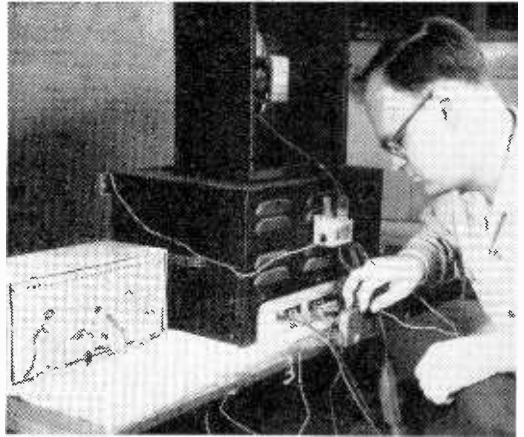
which is 10.7 mc. So far, simple. But what you may not know is that the mixer tube radiates a small portion of the signal at the IF frequency. Such radiation passes back into the antenna circuit. If a shortwave receiver is hooked up to the same antenna, there will be no difficulty picking up the FM signal at 10.7 mc (or whatever the IF is). Once you pick it up on your shortwave receiver, you will of course be using that all-important AM detection.

Now that we've reached the antenna, let's consider it a moment. Subcarriers usually produce weak signals. Thus your antenna must receive signals well from that direction. Which direction? Well, that depends upon which DX station you're after. In other words, your antenna must function in *all* directions. The best solution is a rotor, the kind used for TV antennas. But if you don't already have one, this is also the most expensive. A compromise would be the old fashioned long-wire.

Which brings us to a second use for the hidden-DX receivers: That very tough space reception. Most American satellites use either A1 (on/off) or F1 (frequency shift, in this case producing beep effect) modulation to identify their carriers. Both can be received much better on the narrow band set-up described here than on an ordinary broad-band FM receiver.

Now that the equipment is set, you're ready to use it. The first step would be to listen to one or more of your local FM stations so you become familiar with their sound when detected via AM. If you know one of them has a subcarrier, listen to it (look for a subcarrier when the orthodox programming is other than music). Among other things you will note that mixed with the background music will be transmissions from the standard carrier.

Finding a Subcarrier. The process is the same for both local and DX stations. Tune in the stations as well as possible on your FM set, then turn the volume down to nil (but not off). If your shortwave receiver is equipped with band spread, place it at the maximum



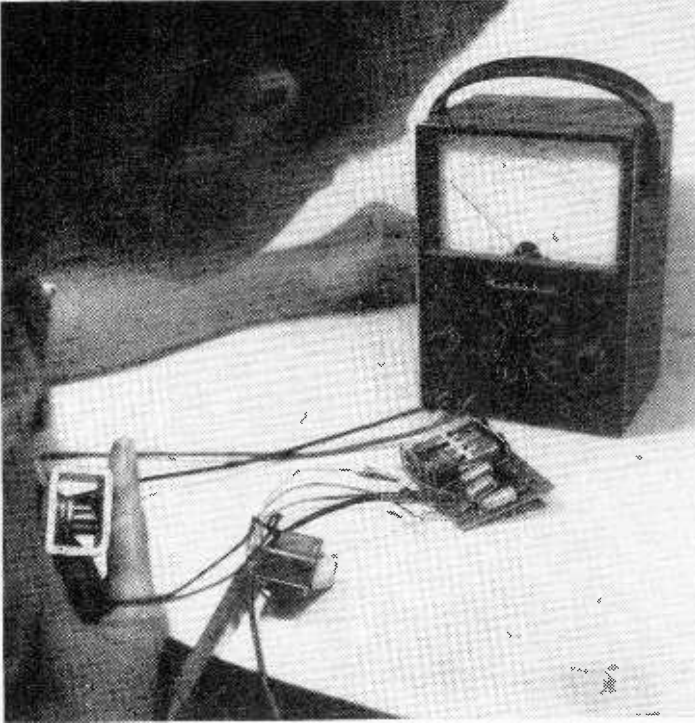
No internal adjustments are required on the rig, only a common antenna.

setting and find the carrier frequency on the main dial (around 10.7 mc or whatever the FM IF is). The carrier will be at the point of peak signal, but it can be found much more accurately by waiting for a moment of dead air (even while the announcer takes a breath). It will then appear as a distinctive hum at just one frequency. (In actual practice this extremely fine tuning is accomplished by a slight adjustment of the bandspread.) Once you find the carrier, look for the subcarrier with the bandspread. Assuming the station has a strong signal, if you fail to find it after a couple tries, place the bandspread at its lowest reading, retune the carrier via the main dial and start searching for your quarry again. If you don't have bandspread, tune in the standard carrier, note the frequency reading carefully, then tune back and forth for the subcarrier. When you find it, note that dial setting also.

Although these procedures sound complicated, they will—with a little practice—become simple routine and in the long run prove much easier than any haphazard approach.

Except for identification, which will be obtained from the normal FM transmission, you'll have to garner enough information from the subcarrier to authenticate reception of same. First item is frequency. If the subcarrier appears above the carrier on your shortwave receiver, it will actually be below it and vice versa. However the indicated frequency difference will be correct. Such readings should be as accurate as possible. A bandspread may be calculated via 31-meter SWBC images or more easily by using a 100 kc crystal calibrator. For space reception, pinpoint accuracy is absolutely indispensable.

Other verification data might include timing between records (to the second) and possibly song titles, although many stations keep no record of the latter, so don't depend upon it.



A speaker connected to the Hi-Qual Pre-Amp input can function as a mike sensitive enough to record heart beats.

Hi-Qual Pre-Amp

This preamp is inexpensive, easy to construct. It has a gain of about 500 flat from 10 cycles to 20,000 cycles. It may be used in apparatus requiring a quality pre-amplifier circuit, or as a laboratory tool

THE electronics and scientific experimenter frequently needs a high quality preamplifier. The preamp must have a low value of internal noise, hum, and hiss. It should have a reasonably high input impedance, high gain, and the gain should be relatively independent of the power supply voltage. The frequency response should be relatively flat over a wide range of frequencies, and distortion should be low.

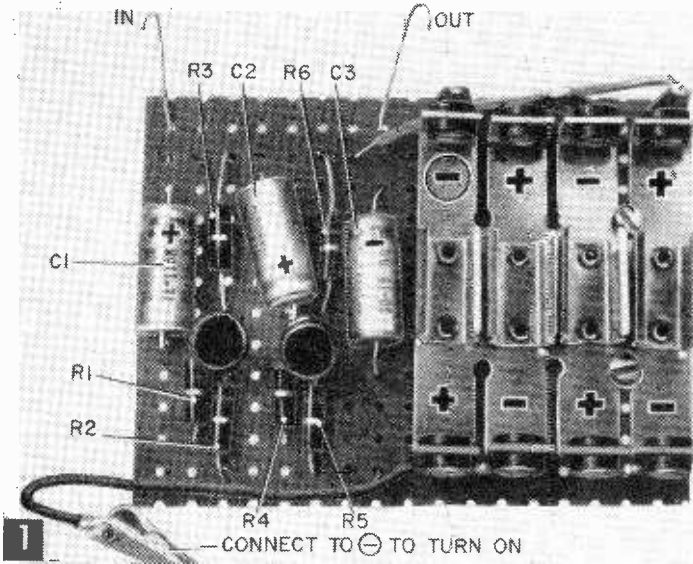
An amplifier that meets these specifications may be used as a phonograph, microphone, or tape recorder pick-up preamplifier. It may be used with a crystal detector tuner to drive a power amplifier for hi-fi listening. As a lab preamp a unit meeting the outlined specs can be used to detect small ac voltages, as a meter amplifier for a conventional meter, as a preamp for older, less sensitive oscilloscopes, and for a host of other uses.

The Hi-Qual Pre-Amp meets the specifications outlined, and it can perform the jobs outlined, plus numerous others. In addition to the characteristics mentioned below the title of this article, it is: 1) transistorized—uses two high gain GE 2N508 transistors; 2) dc operated from 6 v—no line cords to get in your way; 3) battery economy is good—requires less than 2 ma; 4) stabilized for variations in transistor characteristics and temperature; 5) handles inputs from zero to 3 millivolts with minimum distortion. The range may be extended by connecting a volume control in the input circuit (Fig. 4); 3 millivolts input produces a 1.5 v output; 6) input impedance is greater than 10,000 ohms; 7) compact construction— $\frac{3}{4} \times 2\frac{7}{16} \times 3\frac{3}{8}$ in. including self-contained battery (Figs. 1 and 2); 8) simple construction—can be built in about an hour with minimum chances of wiring mistakes; 9) flexible—can be built into other equipment or as a separate lab instrument and can be modified to meet varying requirements.

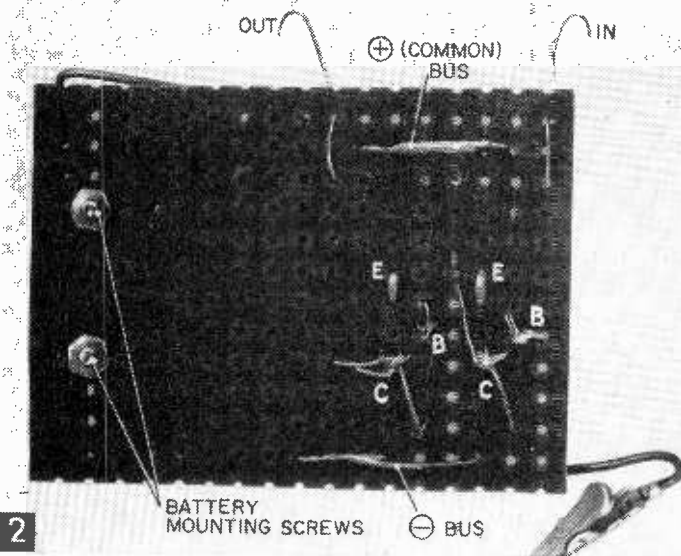
Construction. The top and bottom views of the completed amplifier are shown in Figs. 1 and 2; the circuit diagram is shown in Fig. 3. Using these as a guide, proceed as follows:

1) Drill two $\frac{1}{8}$ -in. dia. holes in the perforated board for the battery holder. There are four small perforations left between these two holes, and the two holes line up on the second row of perforations. Mount the battery holder and connect the terminals for series connection of the batteries. This is accomplished by turning the battery holder lugs till they contact each other, then soldering them together. Fill the inside eyelets of the battery holders which will contact the batteries with solder. This will minimize the chance of poor-contact or no-contact problems later.

2) Insert the transistor, resistor, and capacitor pigtailed through the appropriate board perforations. Note that one pigtail of R2 and



Top view of Pre-Amp.



Bottom view of Pre-Amp.

the collector pigtail of T1 both pass through the same perforation. The same applies to R1 and base T1; R3 and emitter T1. This also occurs for similar elements of T2 and the counterpart resistors. Be careful to position the capacitors with polarities as shown in Fig. 1.

3) The instructions which follow refer to connections made on the bottom side of the perforated board. Connect C1 (-) to junction R1-base T1. Solder and clip off the extra lead length.

4) Connect free end R1 and C2 (-) to collector T1. Solder and clip off extra lead length.

5) Solder R3 and T1 emitter junction; clip off extra lead length.

6) Connect free end C2 (+) to junction R4 and T2 base. Solder and clip excess.

7) Connect free end R4 and C3 (-) to junction R5 and T2 collector.

8) Solder junction R6 and T2 emitter; clip excess lead.

9) Bend free R3 and R6 pigtails against board and solder. Connect a 2-in. length of wire from this junction to the (+) battery holder terminal.

10) Bend free pigtails of R2 and R5 against the board and solder. Connect a 3-in. length of wire to this junction. Solder a Mueller Minigator clip to the other end of this wire. The clip is the On-Off switch for the amplifier. To turn the amplifier on, fasten the clip to the (-) battery holder terminal.

The clip lead switch may be replaced with a more sophisticated switch, but this isn't feasible unless the amplifier is housed in a case which has mounting space. The case may be the case which encloses another piece of equipment of which you want to make the preamp a permanent part, or the amplifier may be housed in its own case. The Lafayette MS-159 plastic case is a good fit, and there's room for a switch or control with switch.

The (+) pigtails of C1 and C3 are the "high" input-output terminals of the amplifier respectively. The

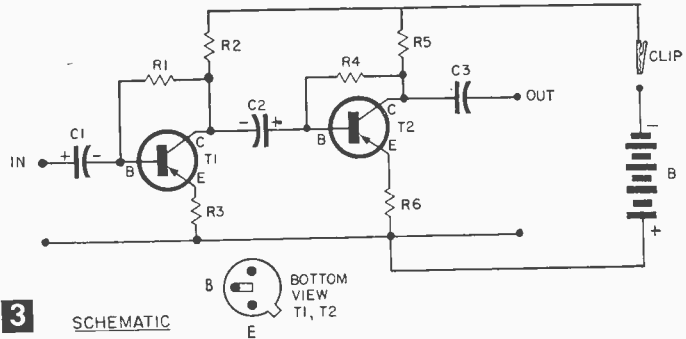
junction of R3 and R6 is the "low" common terminal for input and output. A lead may be soldered at this point for connection purposes. Minigator clips may be attached to these input-output leads, or other terminals of the user's choice may be provided.

A volume control or volume control with switch may be connected at the input of the amplifier as shown in Fig. 4. The amplifier will begin to distort when the input level exceeds 3 millivolts. The volume control divides higher voltage levels and can be set within

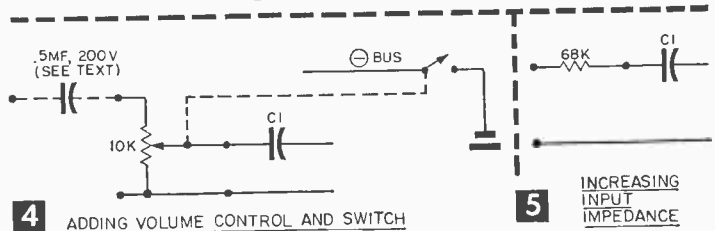
the amplifier input limits. The Lafayette VC-28 miniature control (10K with switch) is suitable for this application and will fit in the plastic case mentioned previously. The 0.5 mfd, 200 v capacitor shown in Fig. 4 should be used if the input signal contains a dc component.

However, if the dc voltage involved is greater than 200, a capacitor with a larger voltage rating must be used.

The input impedance of this high-quality pre-amplifier may be increased by connecting a 68,000-ohm resistor in series with the pre-amplifier's high input lead as shown in Fig. 5. This increases the unit's input impedance to approximately



3 SCHEMATIC



4 ADDING VOLUME CONTROL AND SWITCH

5 INCREASING INPUT IMPEDANCE

MATERIALS LIST—HI-QUAL PRE-AMP

Desig.	Description
R6	10 ohm, 1/2 watt, 20% carbon resistor
R3	100 ohm, 1/2 watt, 20% carbon resistor
R2, R5	2.7K, 1/2 watt, 20% carbon resistor
R1, R4	680K, 1/2 watt, 20% carbon resistor
C1	30 mfd, 15 v miniature electrolytic capacitor (Sprague TE-1158)
C2, C3	capacitor (Sprague TE-1158)
T1, T2	2N508 transistor (General Electric)
B	four 1.5 v penlite cells (RCA V50-74) battery holder (Lafayette MS-170)
	2 7/16 x 3 3/8" miniature perforated board (Lafayette MS-304)
	Minigator clip (Mueller 30)

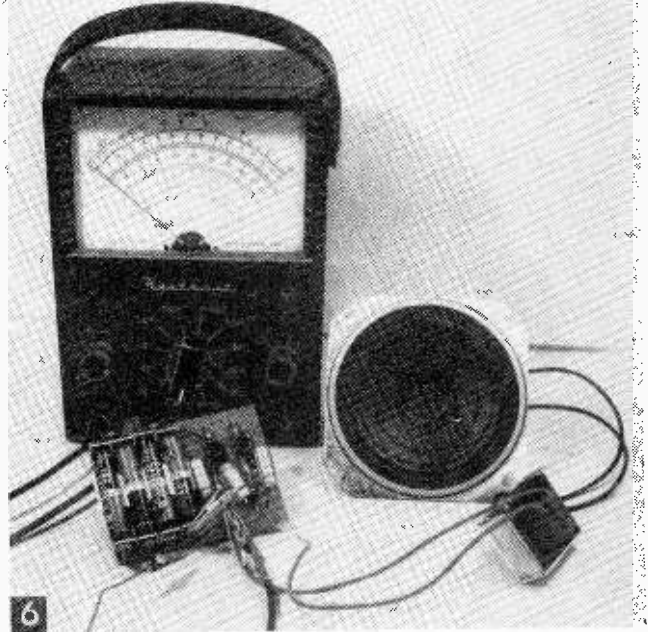
80,000 ohms (80K), adequate for most high-impedance sources. Of course, this results in a reduction of gain to approximately 1/8th of the previous 500 value.

As happens so often as to establish itself as a general rule, conflicting objectives of high voltage gain and high input impedance in transistor amplifiers must be accepted as a fact of life.

The preamp may be used as an amplifier for any reasonably sensitive low-voltage alternating-current meter or the low alternating-current range of a multimeter (Fig. 6). The Heathkit MM-1 Multimeter has a low range of 1.5 v which is ideally suited to this amplifier.

Meters with low ranges greater than that of Heath's MM-1 Multimeter may be used with the amplifier by using the scale only up to 1.5 v.

The preamp output may of course be used to drive an earphone or a power amplifier. The earphone arrangement might be used

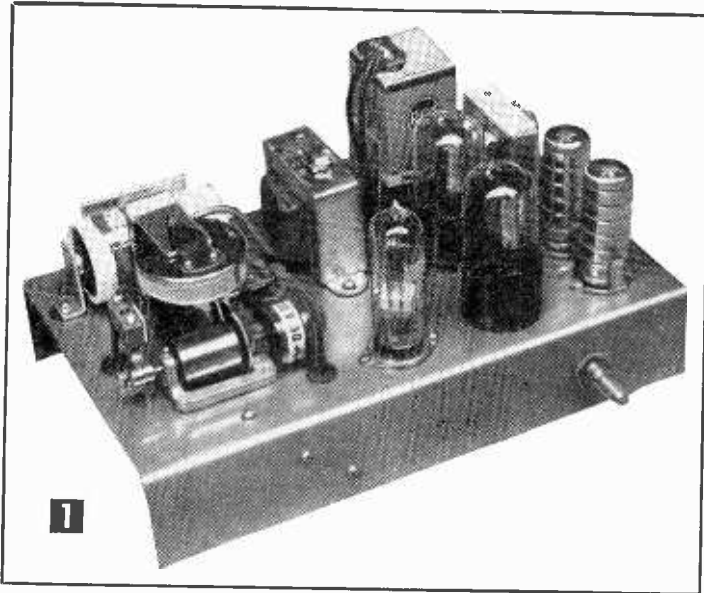


6 Hi-Qual Pre-Amp can be used with ac voltmeter to measure ac millivolts.

with the amplifier for signal tracing or it might be used in conjunction with a crystal radio input.

Another, but not quite so obvious application of the preamp capitalizes on the distortion created by overdriving. If a signal of 0.1 to 0.2 v is applied to the amplifier input, the output waveform will be clipped and will approach a square wave.—FORREST H. FRANTZ, SR.

A Musical Annunciator



With this device hooked into your front door-bell circuit, you substitute the soft, tinkling tones of a music box for the jangle of bell, rasp of buzzer or raucous cling-clang! of chimes

By HARTLAND B. SMITH, W8VVD

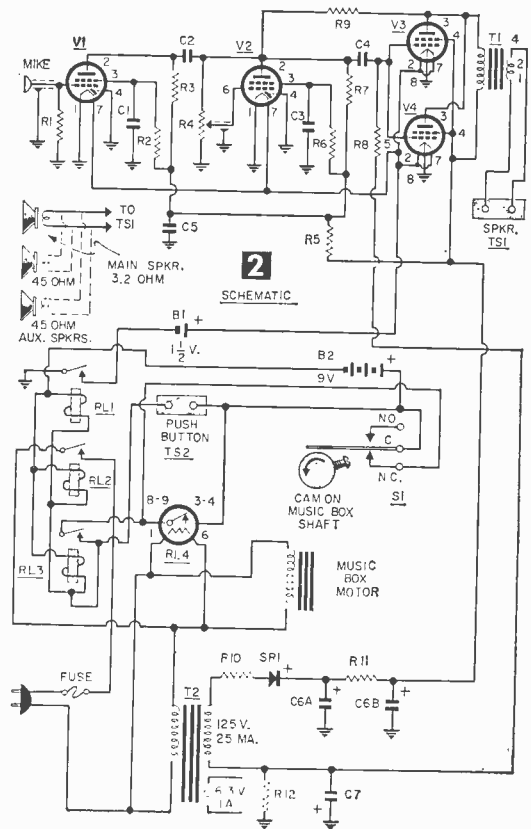
An electronically amplified Swiss musical movement (at left front) makes a pleasant door annunciator.

THE heart of this annunciator is its Swiss musical movement. Powered by a miniature 110-v, shaded-pole motor, this movement will play a 20-second excerpt from one of your favorite melodies. (The available tunes range from *Adeste Fideles* to the *Third Man Theme*, so you should have little difficulty in finding a composition to suit your taste.)

If this tiny music maker is to be heard throughout your home, however, some form of amplification must be employed—and the amplifier must be ready to operate the instant the front door button is pressed.

For economy's sake, no power should be drawn by the unit during standby periods. Consequently, heater-type vacuum tubes cannot be used. The choice, therefore, lies between battery tubes and transistors. Despite continued transistor price reductions, the capacitors, transformers, etc. needed for transistor circuitry are still relatively expensive. In contrast, the parts required for a vacuum-tube amplifier are quite reasonable and, in addition, many are likely to be found in the average experimenter's junk box. For this reason, the unit shown in Fig. 1 utilizes filament-type tubes rather than transistors.

An inexpensive high-output crystal lapel mike converts the sound produced by the musical movement into electrical impulses. These impulses are fed to the control grid of vacuum tube V1 (see Fig. 2). A dynamic mike cannot be employed at this point, be-



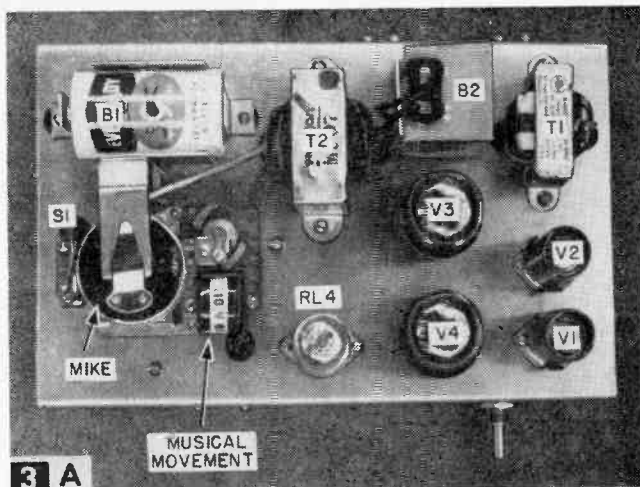
cause it would be sensitive to the hum resulting from the magnetic field that surrounds the motor. A vibration pickup mike, as used for electric guitars and similar musical instruments is also impractical, because of its sensitivity to the mechanical noises generated as the motor and its associated gearing operates.

Because of this mechanically generated noise, a relatively shockproof bracket (see Fig. 6) must be used to mount the mike. This bracket makes use of a small section of plastic sponge to deaden vibrations which would otherwise travel up the mount and excite the mike.

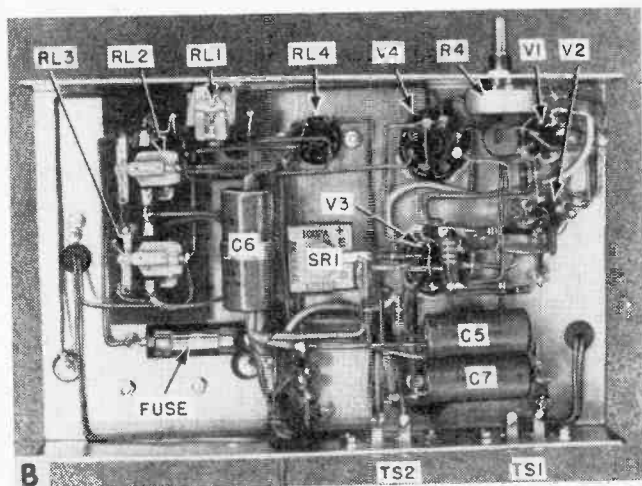
In most respects, the four-tube amplifier is of conventional design. Since the power capability of a single 3Q5GT is rather limited, two of these tubes are operated in parallel. The extra 3Q5GT provides a very useful increase in power output. Parallel, instead of push-pull operation was chosen because no phase inverter tube is needed and an inexpensive output transformer can be employed. Preliminary tests of the completed amplifier showed that its overall gain was so high that there was a tendency toward self-oscillation when the volume control was well advanced, but the addition of resistor R9 (see Fig. 2) provided sufficient inverse feedback to lower the gain and completely eliminate the oscillation problem. The use of inverse feedback also improved the frequency response and minimized distortion in the output stage.

When the annunciator is first plugged into the line, no power can be drawn because relay RL2 is open. However, as soon as the pushbutton is pressed current from the 9-v battery will flow through the coils of RL1, RL2, and RL3. Relay RL2 closes and applies 110 volts to the primary of T2, to the heater of delay relay (RL4), and to the motor of the musical movement. Relay RL1 closes and applies filament power to the tubes. The amplifier becomes operative at once and the tones of the musical movement are heard via loudspeakers placed in convenient spots throughout the home.

Relay RL3 also closes at the instant the button is pressed. The contacts of RL3—as long as RL4 or S1 remain closed—act as a short across the pushbutton. Thus, current continues to be supplied to the coils of RL1, RL2 and RL3 via the contacts of RL3, even



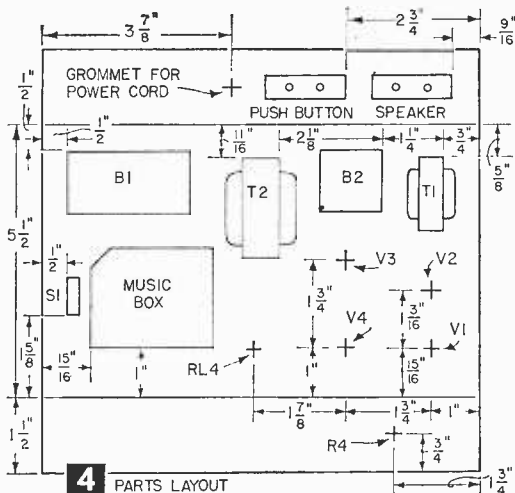
3 A Top-chassis (above) and bottom-chassis (below) views of annunciator circuitry.



after the visitor stops pressing the button.

As the unit operates, the heater in RL4 warms up. After a period of approximately 10 seconds, it becomes so hot that the bi-metal arm in RL4 bends far enough to open the normally closed contacts of this relay. At the moment, this action has no effect on the operation of the musical movement or amplifier because the points of RL4 are paralleled by those of S1, the miniature snap action switch operated by the cam on the shaft of the musical movement. As soon as the 20-second tune has been completed, the cam opens S1, breaking the current path from the 9-v battery to the coils of RL1, RL2 and RL3. The relays open and the entire unit shuts down until such time as it is reactivated by the push-button.

The cam on the music box is constructed from a short length of volume control shaft and a 6-32 machine screw (see Fig. 5). This



plus 6.3 v. Only half of the high-voltage secondary on the 62G008 should be employed with the center-tap going to R12 and one end of the high-voltage winding going to R10. Since the other end of the secondary and the 6.3-v leads are not required, clip them short and insulate with electrical tape.

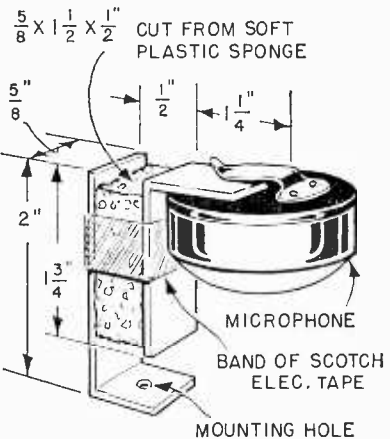
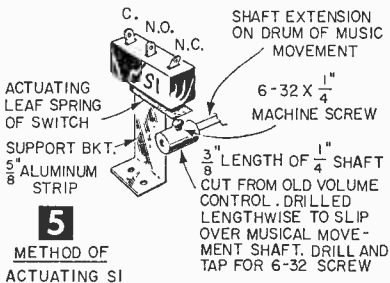
The two small batteries B1 and B2 are subjected to so little use in this particular device that they can be expected to have almost shelf life. Consequently, the battery cost per month will be insignificant.

Constructed on a 1 1/2 x 5 1/2 x 9-in. aluminum chassis, the amplifier is easy to wire since there is plenty of room between the components for the tip of a soldering iron. The armatures of the three small relays are directly connected to the frames. Therefore, RL2 and RL3 should be insulated from the chassis. Figure 3B shows how these relays are mounted on a thin sheet of Bakelite. Any easily worked plastic can be substituted for the Bakelite.

No knob is needed on the shaft of R4. Once the volume has been set to the desired level, no further adjustment is necessary. Battery B1 is kept in place with a home-made battery holder (or use a commercially built holder, such as a Keystone type 175). Two L-shaped brackets bent from small pieces of aluminum clamp battery B2 in position. Since the No. 5

cam must be so positioned that it actuates the lever of S1 when the tune on the barrel has been completed.

The power transformer T2 in Fig. 3A happens to be a surplus unit designed to provide 125 v at 25 ma and 6.3 v at 1 amp. A suitable substitute would be a Knight 62G008 which furnishes 125 volts each side of center-tap,



MATERIALS LIST—MUSICAL ANNUNCIATOR

Desig.	Description
R1, R6, R8	2.2 megohm, 1/2 watt (Allied 1MM000)
R2	1 megohm, 1/2 watt (Allied 1MM000)
R3, R7	220,000 ohm, 1/2 watt (Allied 1MM000)
R9	330,000 ohm, 1/2 watt (Allied 1MM000)
R10	75 ohm, 1/2 watt (Allied 1MM000)
R11	560 ohm, 1/2 watt (Allied 1MM000)
R12	330 ohm, 1/2 watt (Allied 1MM000)
R4	500,000 ohm volume control (Allied 29M773)
R5	33,000 ohm, 1 watt (Allied 1MM020)
C1, C2, C3, C4	.01 mfd. disc ceramic capacitors (Allied 11L437)
C5	12 mf., 150-v electrolytic capacitor (Allied 15L194)
C6	20-20 mf., 150 v electrolytic capacitor (Allied 15L247)
C7	100 mf., 15 v. electrolytic capacitor (Allied 16L236)
RL1, RL2, RL3	Sigma 11F-1000G-SIL SPDT Relay (Allied 75P068)
RL4	Amperite 115C10T miniature delay relay (Allied 75PP296)
T1	Stancor A-3822 4 watt universal output transformer (Allied 64G005)
T2	Knight power transformer 125-0-125 v, 25 ma; 6.3 v, 1 amp (Allied 62G008)
B1	1 1/2 v size D A battery (Allied 80J903)
B2	9 v battery VS-305 (Allied 80J838)
SR1	Federal 1002A, 65 ma. rectifier (Allied 4A606)
S1	Unimax USML SPDT Subminiature leaf switch (Allied 34B848)
TS1, TS2	2 screw terminal strip (Allied 41H505)
Mic	Crystal lapel Mike (Lafayette PA-9)
Battery Holder	for 1 size D cell (Lafayette MS-175)
Fuse	3AG 1/2 amp (Allied 52B232)
V1, V2	1U5 tube
V3, V4	3Q5GT tube
Musical movement	Reuge ELR 1.18 110 v, 60 cps with extended shaft. From Novelties of Distinction, 131 West 42nd St., New York 36, N. Y., or direct from the manufacturer, Reuge S.A., 26, Rue des Rasses, Ste. Croix, Switzerland.
	two octal tube sockets (Allied 40H058)
	one 9-prong miniature socket for RL4 (Allied 41H534)
	two 7-prong tube sockets with shield (Allied 40H194)
	two 13/4" tube shields (Allied 40H198)
	open-end chassis 1 1/2 x 5 1/2 x 9" (Allied 80P440)
	fuse clip (Allied 52B292)
	three terminal tie-point strip (Allied 41H501)
	5" loudspeaker, 3.2-ohm voice coil (Allied 81D617)
	wall baffle for 5" speaker
	wire, power plug, assorted 4-36 and 6-32 screws and nuts

6 SHOCK PROOF MOUNT FOR MICROPHONE

Components available from Allied Radio Corp., 100 N. Western Ave., Chicago 80, Illinois, and Lafayette Radio, 165-08 Liberty Avenue, Jamaica 33, New York.

pin on a 1U5 and the No. 1 and 6 pins of a 3Q5GT are not connected to elements within the tubes, those terminals on the sockets can be used as convenient tie points to support resistors and capacitors. Grid bias for the 3Q5GT's is obtained from the voltage drop across R12. Capacitor C7, the bias filter capacitor, must be wired with its positive terminal grounded.

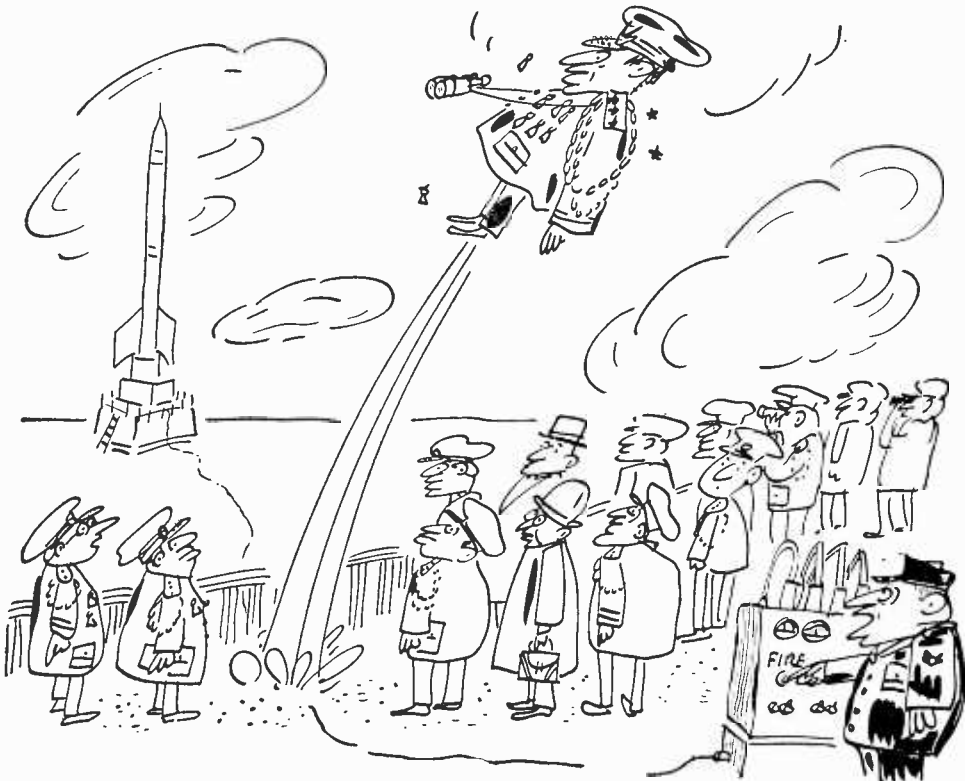
Locate the amplifier where output from the speakers cannot get back into the microphone to produce acoustical feedback—put it in the basement or, if you have no basement, in a utility room. Wherever you put the amplifier, make certain that it is out of reach of your youngsters. With the exception of the terminals on the motor of the musical movement, which ought to be insulated with electrical tape, all high voltages appear only on the under side of the chassis. A fuse has been included as a protection against overheating which might result from a shorted component.

Once it has been permanently installed, plug the amplifier into the power line and run a pair of wires from TS2 to a pushbutton near the front door. Run a second pair of wires from TS1 to the main speaker which may be a 4-in. or 5-in. unit with an impedance of 3.2 ohms. Mounted in a wooden baffle, this speaker can be placed at a convenient point in the most lived-in section of your

home.

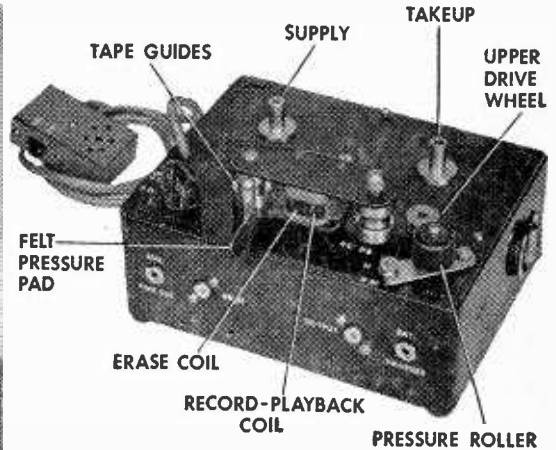
Overall volume in any one part of the house need not be high, since additional speakers can be placed in those areas where the sound of the main speaker does not penetrate adequately. These extra speakers can be wired in parallel with the main speaker as shown in Fig. 2. Since the desired volume level at remote locations will normally be less than that of the main speaker, intercom replacement units with 45-ohm voice coils will work effectively in these spots. Each intercom speaker will give adequate acoustical output to cover a room or two, but because of the relatively high impedances involved, even when several are connected in parallel, they will not seriously shunt the 3.2-ohm main speaker.

The electronically amplified music box, as a replacement for an ordinary door bell or chime has a number of important features, in addition to its basic one of providing pleasant music. Unlike the ordinary bell or solenoid-operated chime, it plays for a period of 20 seconds, whether or not the pushbutton is held down. The sound of a doorbell is usually of rather short duration and is often masked by noises around the house. On the other hand, the continued output from the music box tends to get through such distractions as children's voices, loud hi-fi's, clacking typewriters, pounding hammers, etc.





Standard flashlight batteries or the new, D-size, rechargeable storage batteries may be used in this instant-ready recorder. Its motor-driven fast rewind and erase features make it possible to use the same tape over and over. Depending on where you buy, and what you have on hand, drive parts should cost between \$40 and \$60. High precision is not required.



Miniature Tape Recorder

By JAMES E. PUGH

FLICK the mike switch and this battery-powered, 4-lb. midget starts recording immediately. There's no waiting for tube warm-up and no searching for an electrical outlet. And since playback speed is the standard $3\frac{3}{4}$ -ips used on home recorders, you can play your tapes with loudspeaker volume through a radio or hi-fi unit, instead of the combination mike-speaker; or—if more volume is required on playback—you can play them on any standard home-type recorder that has $3\frac{3}{4}$ ips speed. A built-in jack plug input also permits you to record voice or music directly from your radio or TV.

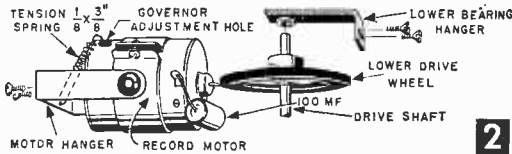
The switch on the mike case starts and stops the record motor. For dictation, you can wire in a 4-prong plug and foot switch for the convenience of a typist. If you need loud-speaker volume, feed the output into an amplifier, or use the input jacks on suitable radios, or the amplifier section of tape recorders.

Construction starts with the metal parts detailed in Fig. 6. First scribe lines at the desired points for cuts and saw and then clamp in a vise along the line, using a square to make sure that the metal is vertical to the vise jaws. Next, lay out the hole locations with scriber and center punch and, with the part held firmly in a drill press vise, start the holes with a $\frac{1}{16}$ -in center drill chucked in a drill press. Use oil and finish the holes to size with sharp drills. File the three notches in the forward-reverse idler lever, but leave the

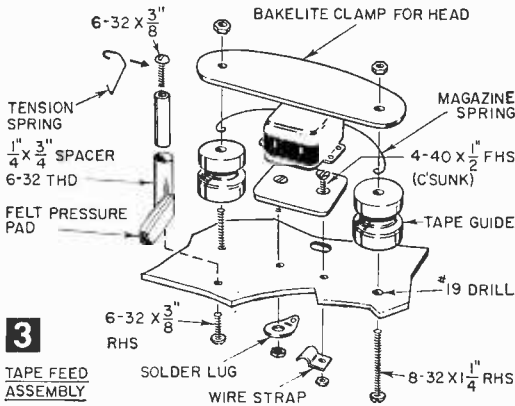
center notch slightly shallow, since it must be deepened later.

Locate the holes in the plastic case with a machinist square and scriber as in Fig. 7, and back up the plastic with a wooden block to prevent chipping when drilling. For the holes for the two tape spindles, use the metal bracket that goes inside the case as a template to assure matching center-to-center spacing. Countersink each hole requiring a Nyliner bushing inside the case and enlarge them with a tapered hand reamer just enough to obtain a free-turning fit with the shaft when bushing is installed. Each shaft must spin freely in its bushing for smooth tape motion, but it cannot be so loose that it wobbles. Nyliner bushings are split at one side to facilitate this kind of adjustment. Insert them by pressing the lower pointed end, of the bushing inward and spiraling clockwise into the hole with your fingers, working from the outside of the case, so the broad flange will be on top.

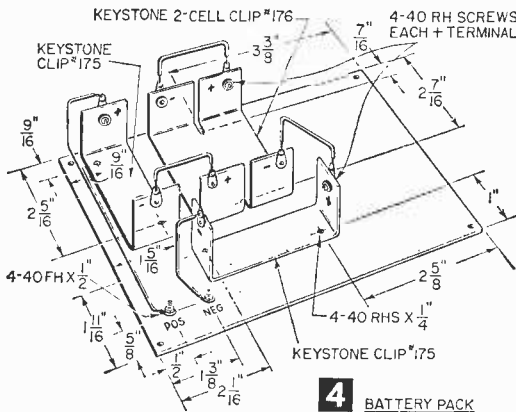
Next, make up the tape drive parts shown in Fig. 8. The three idler wheels must turn freely on their shafts. Mount the forward and rewind idler lever as in Fig. 9. Tighten the screw on the threaded shaft until the compression washer holds the shaft firmly, but not locked in place. Then, holding the first lock nut with a thin wrench to keep the shaft from turning, tighten the second lock nut. It should now be possible to slide the idler along the length of its slot without rocking.



Speed of the tape drive motor is reduced through a rubber rim idler wheel. A spring holds the motor shaft in contact.



Tape guides guarantee precise tracking of the tape across the recording head. Adjust felt-covered pressure pad so it lightly presses tape against the head.



Four rechargeable batteries (or four flashlight-type D-size dry cells) are mounted on the bottom panel.

After all tape drive parts are made and rotating parts operating smoothly, carefully remove the Nyliner bushings and clean all parts thoroughly. Then replace the bushings and coat the inner and flange surfaces with light machine oil.

Adjustment. Put the various shafts and wheels in place (Fig. 9) and tighten the wheel set screws allowing .001-.002 in. clearance between wheel and bushing flange. Oil the idler shafts and adjust, making sure that no oil gets on the rubber wheels or on the metal friction surfaces.

MATERIALS LIST—TAPE RECORDER

No. Req'd.	Size and Description Tape Drive Mechanism	Allied. No.
1	2 $\frac{5}{16}$ x 5 $\frac{1}{2}$ x 6 $\frac{3}{16}$ " black plastic case with panel	86P287, 86P289
1	2" O.D. takeup idler wheel (Walsco 1433)	43N388
1	2" O.D. rewind wheel (Walsco 1433)	
1	2" O.D. lower drive wheel (Walsco 1483)	SPECIAL
1	1" O.D. rewind idler wheel (Walsco 1450)	SPECIAL
1	3 $\frac{3}{4}$ " O.D. pressure roller (Walsco 1458)	SPECIAL
1	7 $\frac{1}{8}$ " dia. x 6" brass for hubs, wheels and tape guides	
1	3 $\frac{1}{8}$ " dia. x 12" drill rod for reel, drive and idler shafts	
1	1 $\frac{1}{4}$ " dia. x 3" drill rod for pressure and function lever shafts, function lever hub	
2	3 $\frac{1}{4}$ x 1 $\frac{1}{2}$ x 18" precision ground flat stock for hangers and levers	
2	spiral tension washers	
2	1 $\frac{1}{4}$ " dia. x 3 $\frac{1}{4}$ " 6-32 threaded bushings	
3	3 $\frac{1}{16}$ " I.D. 3L1-FF flanged Nyloners (Thomson Industries, Inc.)	
3	3 $\frac{1}{16}$ " I.D. 3L2-FF flanged Nyloners (Thomson)	
2	1 $\frac{1}{4}$ " I.D. 4L1-FF flanged Nyloners (Thomson)	
1	1 $\frac{1}{4}$ " I.D. 4L2-FF flanged Nyloners (Thomson)	
1	3 $\frac{1}{8}$ " dia. x 5 $\frac{1}{2}$ " tension spring (General Cement H420-F assortment)	SPECIAL
1	1 $\frac{1}{8}$ " dia. x 3 $\frac{1}{2}$ " tension spring (General Cement H420-F)	
4	1 $\frac{1}{2}$ " dia. rubber feet (General Cement H052-F assortment)	SPECIAL
Amplifier		
1	B1 battery pack consisting of 4 Sonatone rechargeable nickel-cadmium type S-103D batteries	
or 4	Eveready Type D99 leakproof flashlight cells	80J903
1	M1—6-volt rewind motor (Wilson's of Cleveland, Model 6-100)	
1	M2—6-volt DC record motor (Barber-Coleman BYQM 2022)	76P642
1	D1—3.9-volt voltage regulator Zener Diode (Texas Instrument 1N748A)	8E808
3	V1, V2, V4—2N217 PNP Transistor (RCA)	5E877
1	V3—2N647 NPN Transistor (RCA)	5E986
1	L1, L2—Record-PB-Erase head (Shure 815H)	65R584
1	Magnetic microphone, 1000 ohm (Shure MC11J)	SPECIAL
1	S1—SPST slide switch	34B422
1	S2—5-pole, 3-position wafer switch (Centralab PA-2015)	34B928
Capacitors		
5	C1, C2, C3, C5, C6—2uf, 8-v ultra-miniature electrolytic capacitors (Barco PT6-2)	10L660
1	C4—2uf, 75-v ceramic capacitor (Lafayette Radio C-616)	
2	C7, C9—100uf, 25-v ultra-miniature electrolytic capacitors	13L826
1	C8—150uf, 20-v ultra-miniature electrolytic capacitor	18L504
Resistors		
3	R1, R4, R6—3.3K, 1 $\frac{1}{2}$ -watt, 10% carbon resistors	1MM000
3	R2, R5, R10—72K, 1 $\frac{1}{2}$ -watt, 10% carbon resistors	1MM000
1	R3—4.7K, 1 $\frac{1}{2}$ -watt, 10% carbon resistor	1MM000
1	R7—5K miniature trimmer potentiometer (Bourns Wirewound Trimit 271)	31MM397
1	R8—10K, 1 $\frac{1}{2}$ -watt, 10% carbon resistor	1MM000
1	R9—3.3K, 1 $\frac{1}{2}$ -watt, 10% carbon resistor	1MM000
1	R11—150 ohm, 1 $\frac{1}{2}$ -watt, 10% carbon resistor	
1	R12—1.8K, 1 $\frac{1}{2}$ -watt, 10% carbon resistor	
Tape Cartridge		
4	1 $\frac{1}{4}$ x 3 $\frac{1}{4}$ " 6-32 threaded bushings (Newark Electric Co.)	
2	2 $\frac{3}{4}$ x 6 $\frac{3}{8}$ x 3 $\frac{1}{2}$ " thick Bakelite sheet	
6	.020 dia. piano wire	
1	3" reel of long play 1 mil tape	96R237
1	3" empty reel	
Hardware		
2	J1, J2—phono pin jacks (RCA)	46H213
2	J3, J4—sub-min phone jacks (Switchcraft 42A)	41H517
2	battery clips for 1 type-D cell (Keystone 175)	54J040
1	battery clip for 2 type-D cell (Keystone 176)	54J060

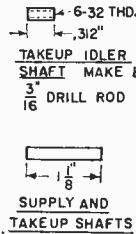
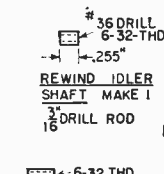
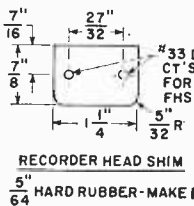
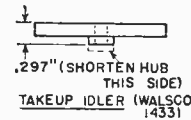
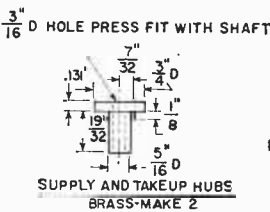
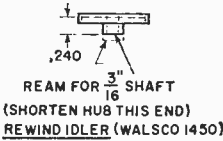
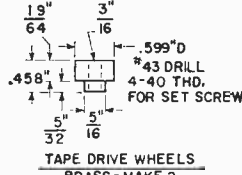
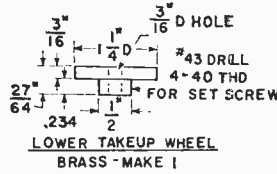
Hold the microphone about 8 in. from your mouth and speak in a normal voice. Play the recording back and adjust the tape pressure pad for maximum volume but be sure that it is not tight enough to drag on the tape. Now make another recording and, if it's weak, turn the volume control up 1/2 turn (clockwise) and try again. Repeat until the recording is of a suitable volume but not distorted from over-driving. Minor adjustments can now be made in the tape transport mechanism for smoothest recordings, and the recorder is ready to use.

How it Works. The tape feeds from the supply (left) reel across the first tape guide. From here it passes across the erase coil (on the right side of the head). The erase coil thus wipes off any previous recording before it reaches the record coil. The pressure pad holds the tape in contact with the head.

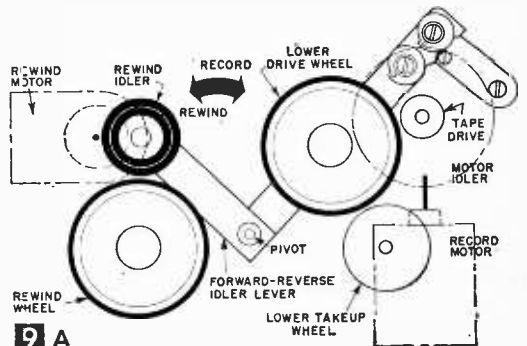
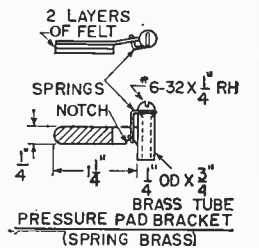
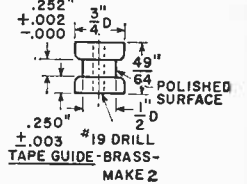
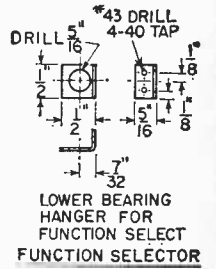
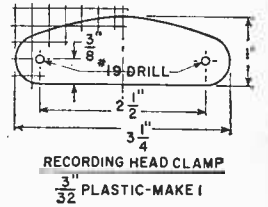
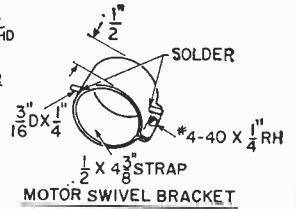
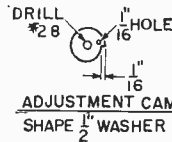
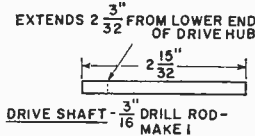
After the tape leaves the recording head it passes between the upper drive wheel and pressure roller and from here to the takeup reel. On playback the erase coil is disconnected by switch (S2) and the recorded signal on the tape energizes the record-playback coil which is now connected to the amplifier input. The amplified signal is fed to the magnetic microphone—now used as an earphone.

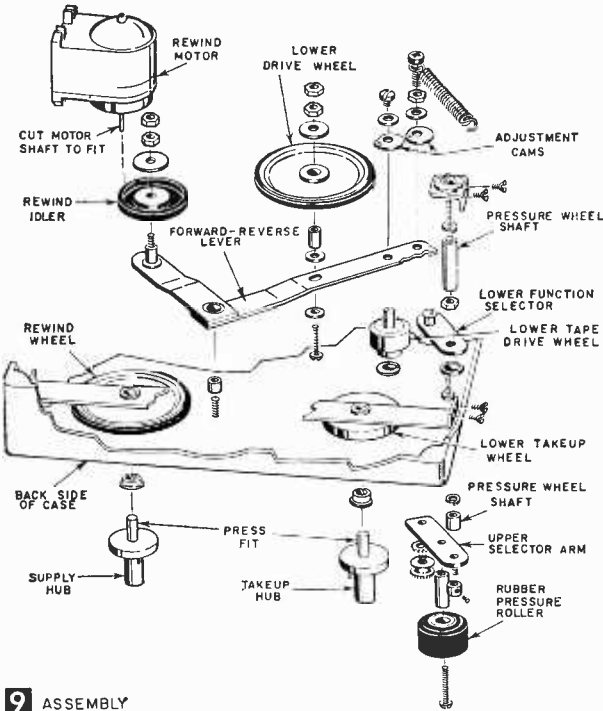
A simple three-stage common-emitter amplifier is used. The first two transistors are the PNP and the last the NPN type to allow the mike and record coil return leads to connect directly to common, on both record and playback, without using decoupling filters. High-frequency pre-emphasis is used on *Record* with flat response being used on *Playback* providing better quality with minimum distortion.

Motor noise is removed from the amplifier dc power source with V4, which acts as stable



8 TAPE DRIVE PARTS





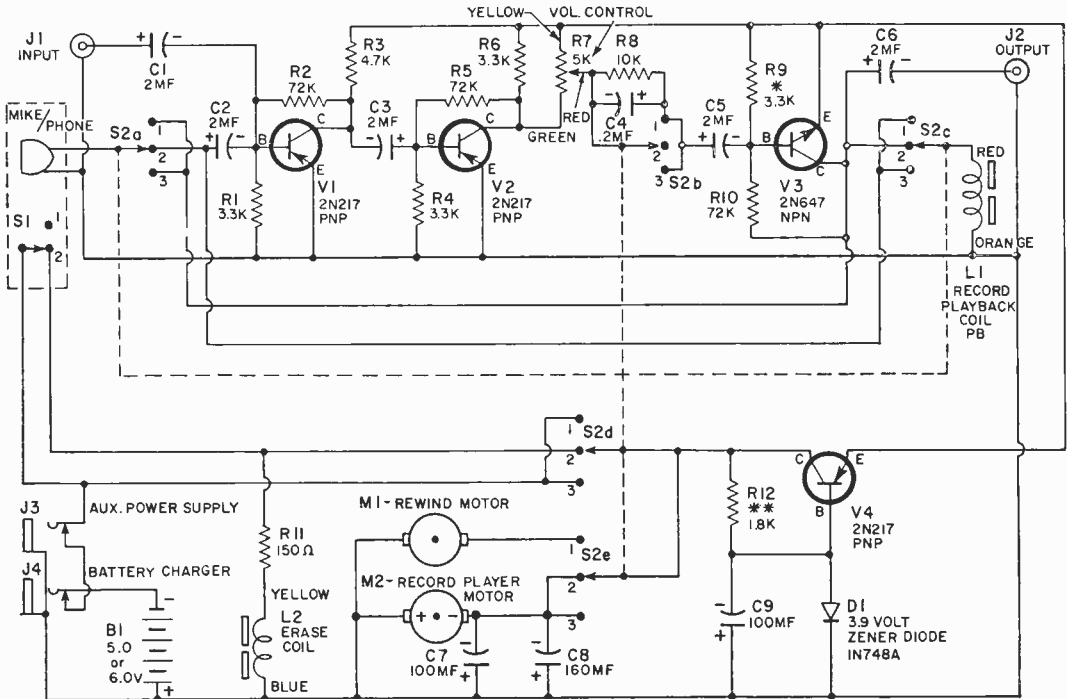
9 ASSEMBLY

voltage regulator. The voltage across the zener diode (D1) is constant at 3.9 as long as the input voltage does not fall below this value. Because this diode is in the base circuit, it determines the voltage output level at the emitter of V4. Since the base voltage is constant, the output voltage will thus be constant regardless of variations at the input (at V4 collector); therefore, variations due to motor noise will be filtered out.

Battery Notes. You can use either rechargeable Sonotone nickel-cadmium, or flashlight cells.

The nickel-cadmium cells provide nearly constant output voltage throughout their charge, whereas the flashlight cells drop off as they are used. Constant voltage is an advantage in maintaining motor speed; however, the 5-volt level approaches the lower limit for best governor operation.

The nickel-cadmium cells are slightly shorter than flashlight cells and a short 4-40 rh screw is threaded into the positive terminal of each battery clip to compensate for the difference (Fig. 4).



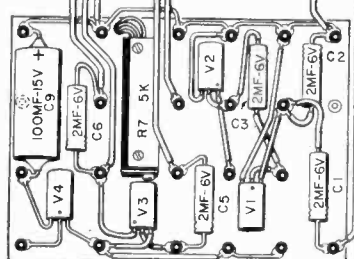
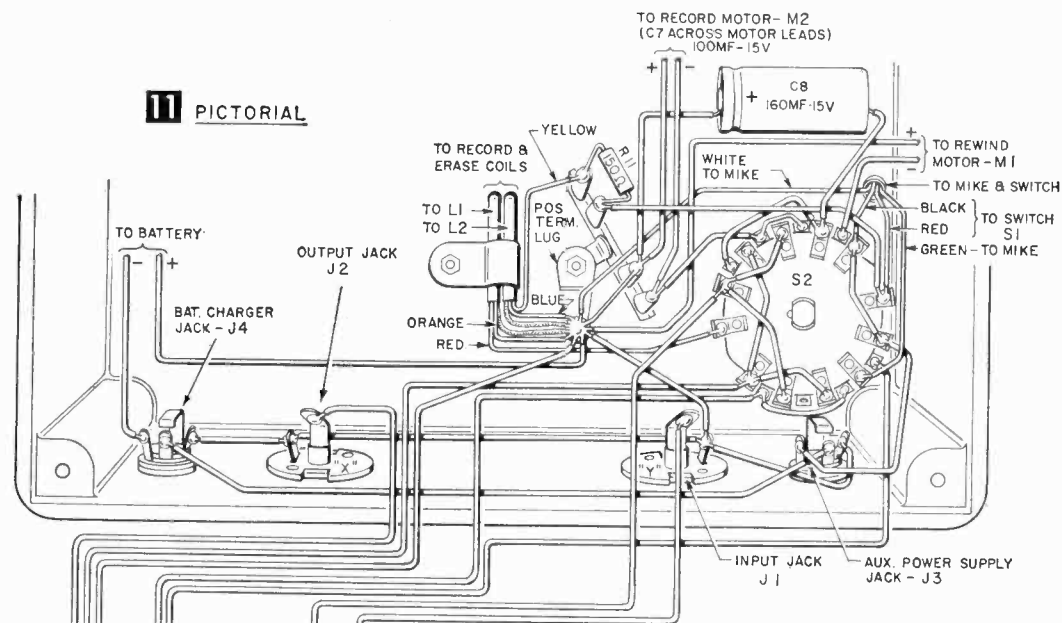
* ABOUT 3.3K. ADJUST FOR APPROX. .5MA. L1 CURRENT
 ** ABOUT 1.8K. ADJUST FOR APPROX. 1 MA. DIODE CURRENT
 OUTPUT FROM V4 EMITTER SHOULD BE ABOUT 3.9 VOLTS

SWITCH POSITIONS

- S1
 1 = OFF
 2 = RECORD
- S2
 1 = REWIND
 2 = RECORD / OFF
 3 = PLAYBACK

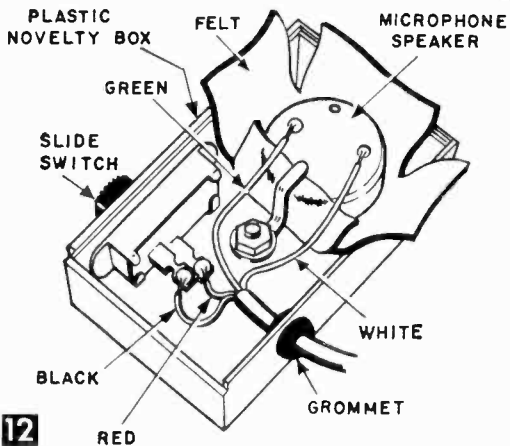
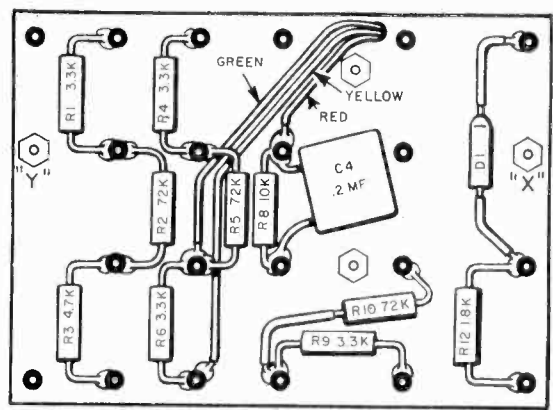
10 SCHEMATIC DIAGRAM

11 PICTORIAL



TOP VIEW OF TERMINAL BOARD

BOTTOM VIEW OF TERMINAL BOARD USE ACTUAL SIZE DRAWING AS DRILLING TEMPLATE

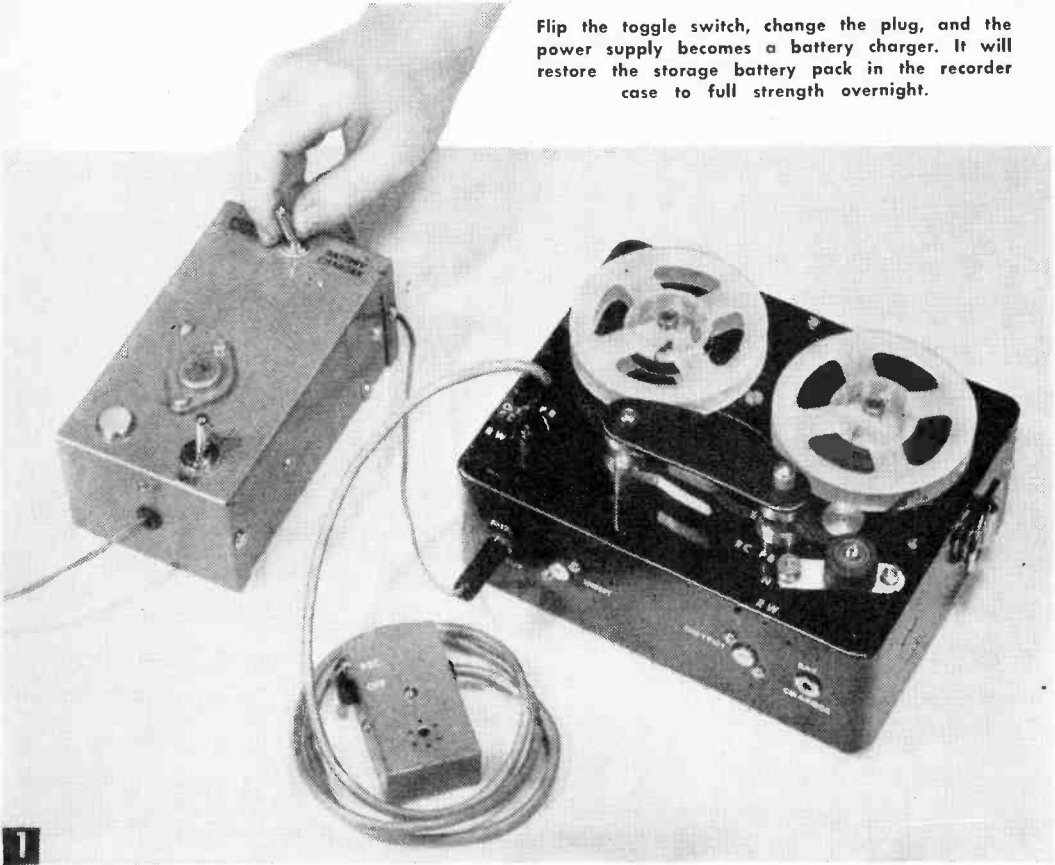


12

If you use flashlight cells, select Eveready Type D99, a leakproof type, to avoid damage to the recorder. Jacks are provided to allow recording an external signal; to feed the amplifier output to an external power amplifier; to connect an external power source such as a 6-volt automobile battery or an auxiliary ac power supply; and to connect the charger to the batteries. When the external power supply is connected, internal batteries are disconnected; when the charger is connected, amplifier and motors are disconnected.

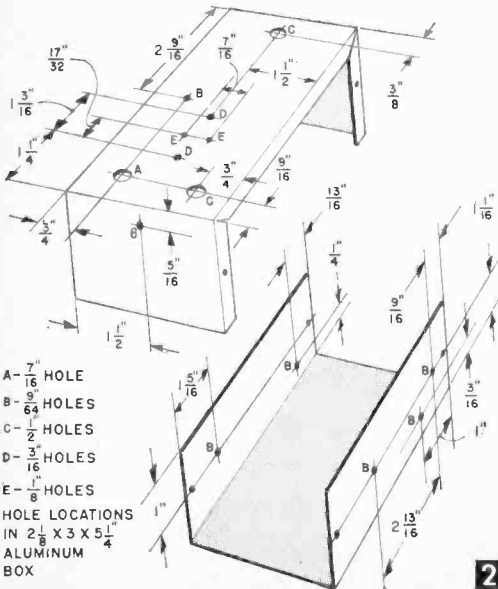
Accessories. The tape cartridge (Fig. 5), allows the recorder to be carried as a portable unit in any position. Plans for a separate power supply appear overleaf this handbook.

Flip the toggle switch, change the plug, and the power supply becomes a battery charger. It will restore the storage battery pack in the recorder case to full strength overnight.



Dual Purpose Tape Recorder Power Supply

By JAMES E. PUGH



DESIGNED as an accessory for the portable tape recorder, this combination power supply will either recharge the recorder storage batteries, or permit you to operate the recorder without batteries on house current.

The unit can double as an experimenter's power supply, and to charge miniature storage batteries used in other types of equipment, provided that the charging current (225 ma.) and the charging voltage (5.1, or 6.2-volt) are the same.

While the four *Sonotone* rechargeable batteries used in the portable tape recorder 5-volt power pack will operate continuously for many hours, they must be eventually recharged. This a-c power supply unit guarantees that you'll be able to use the tape recorder for continuous dictation or desk use, even though the batteries may be exhausted.

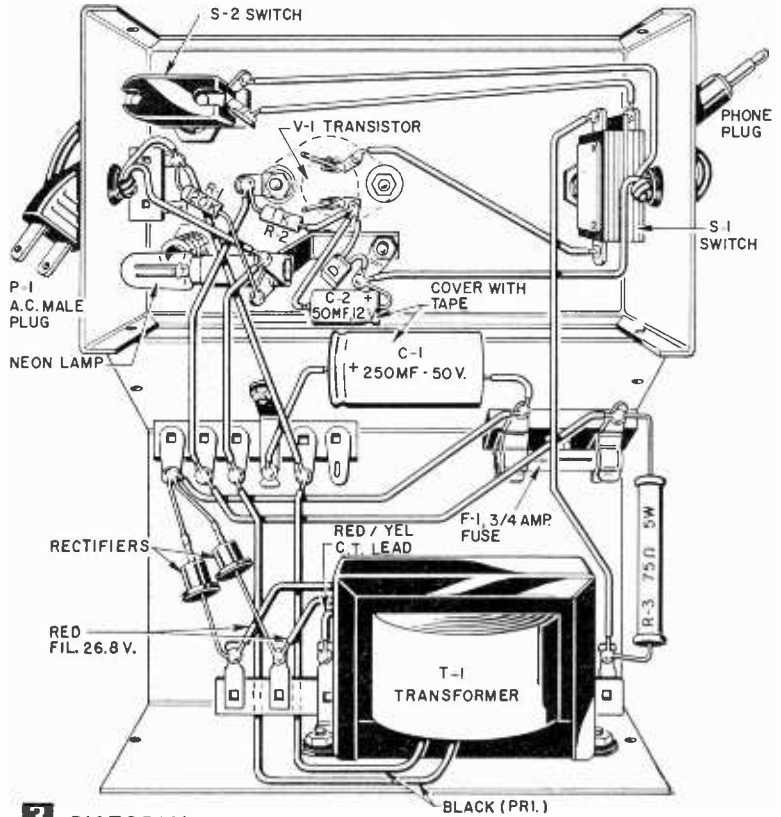
Begin construction by drilling all of the holes (Fig. 2) in the aluminum box. Wire the switches and other parts according to Figs. 3 and 4. Flexible #24 speaker cable is suitable for the a-c power cord and the connecting cord since the wattage of this unit is very low.

The power supply regulator, transistor V1, is mounted on top of the aluminum box to provide suitable heat dissipation. Drill the mounting holes in the box first, and then scribe the outline of the transistor case. Scrape away all paint within this outline to allow better thermal contact with the box; sand the surface smooth, and remove all burrs from the insulator holes to prevent puncturing the mounting insulator.

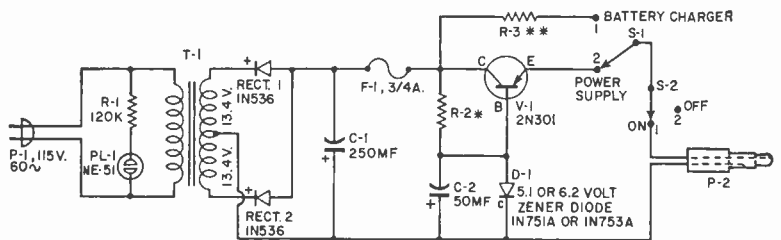
Make a thin mica mounting washer by scribing the transistor case outline on a piece of thin mica. Drill the two mounting holes, cut along the outline with sharp scissors, and then split the mica into thin layers about .002, or .003-in. thick. Coat both sides of the washer with light oil, and mount the transistor with 6-32 machine screws, washers, and nuts. Use an ohmmeter to make sure that the insulation between the aluminum box, and the transistor case is good.

Clip off the ends of one of the unused mica mounting washers, and use it as an insulator on the underside of the box. Make the emitter and base contactors from the contacts of a miniature 7 pin wafer tube socket. When soldering to the transistor contacts, remove the transistor to avoid heat damage. Mark the letters B and E near the base and emitter pins to identify them.

Transformer T1 steps the line voltage down to 13.4 volts a-c after which it is changed to d-c by the full wave rectifier consisting of



3 PICTORIAL



4 SCHEMATIC

* ABOUT 1000 Ω. FOR DIODE CURRENT OF 8 TO 10 MA. OUTPUT FROM V-1 EMITTER SHOULD BE APPROXIMATELY 5.1 OR 6.2 VOLTS (SEE TEXT)
 ** ABOUT 75 Ω FOR CHARGING CURRENT OF 200 TO 225 MA.

Rect. 1, and Rect. 2. Transistor V1 and Zener diode D1 form a voltage regulator that filters and maintains the output voltage at the desired level. The same kind of circuit was used in the motor noise filter of the recorder amplifier circuit.

The power supply output voltage should correspond closely to that of the batteries used so as to maintain more consistent motor speed. For example, with four 1.25-volt nickel cadmium cells, use a 5.1-volt Zener diode (IN751A). On the other hand, if you use four flashlight dry cells, 6 volts will result; therefore use a 6.2-volt zener diode (IN753A) for D1.

MATERIALS LIST
TAPE RECORDER POWER SUPPLY

No.	Req'd	Size and Description
1		D1—5.1 or 6.2-volt voltage regulator Zener Diode (Texas Instrument IN751A or IN753A, see text)
1		F1— $\frac{3}{4}$ ampere fuse, type 3AG; fuse holder (Littelfuse 3510011)
1		P1—a-c power plug
1		P2—sub-min phone plug (Switchcraft 750)
2		Rect. 1, Rect. 2—IN536 silicon rectifiers (RCA)
1		S1—SPDT toggle switch
1		S2—SPST toggle switch
1		T1—26.8 v., 1A. filament transformer (Triad F-40X)
1		V1—2N301 transistor (RCA)
1		PL1—NE-51 neon lamp
Capacitors		
1		C1—250uf, 50-v. electrolytic capacitor (Mallory TC-50025)
1		C2—50uf, 12-v. ultra-miniature electrolytic capacitor (Barco P12-50)
Resistors		
1		R1—120 K, $\frac{1}{2}$ w., 10% carbon resistor
1		R2—about 1K, $\frac{1}{2}$ watt, 10% carbon resistor (see Fig. 4)
1		R3—about 75 ohm, 5 w., resistor (Sprague 27E)
Hardware		
1		$2\frac{1}{8} \times 3 \times 5\frac{1}{4}$ " grey hammertone aluminum box (Bud CU-2106A)
1		On-off toggle switch plate
7 ft.		length 2-conductor chrome vinyl speaker cable (Belden 8782)
1		insulated tie point
1		miniature 7-pin wafer tube socket
1		pilot light socket, miniature bayonet (Dialco 720)
1		$\frac{1}{2}$ " pilot light jewel, white (Dialco 10006-435)
misc		rubber grommets, screws, nuts, solder lugs, mica, insulated, extruded washers, decals, plastic spray or lacquer, wire resin core solder
		Parts available from Allied Radio, 100 N. Western Ave., Chicago 80, Illinois

When charging the Sonotone batteries, resistor R3 bypasses the regulator circuit to provide a constant current. Between 200 and

225 ma. is required for proper charging. About 16 hours are required for a full charge at this rate, though the batteries may be left connected on charge for much longer time without harm.

The pilot light, indicating that the power supply or charger is ready for use, is lit whenever plug P1 is in the 115-volt socket, since the on-off switch does not control this part of the circuit.

When you connect the accessory unit (Fig. 1) to the recorder, always be sure that toggle switch S1 in Fig. 3 is thrown to the position corresponding to the jack to which the plug P2 is connected. When plug P2 is connected to the auxiliary power supply jack on the recorder, the internal battery pack is automatically disconnected. Be sure that S2 is at Off when connecting and removing plug P2. Also remove the plug from the charger jack when not charging to prevent the batteries from draining back into the charger circuit.

Polish "Locks" TV Adjustment

• When you've just finished making a critical adjustment on the service control of a TV set, "lock" the screw firmly against mechanical shocks by coating its threads with fingernail polish. If the control ever needs readjustment, a drop or two of fingernail polish remover will unlock it in a matter of seconds.—JOHN A. COMSTOCK.



D. Victor

"Lady wanted to know could we do anything with this. Hasn't made a move for two weeks."

The Typacode

By BERNARD DICKMAN

With the Typacode you can send Morse code as fast as you can type—whether you know the code or not. Thus, even a person who does not know Morse code can test you on your knowledge of it

WITH the Typacode, you press a button indicating the letter of your choice and this letter is automatically translated into the correct Morse code pulses. The number of words per minute you can send out with Typacode depends upon the speed of the motor you use to turn the shorting rotary switch, the "brain" of the device. Assuming five letters to the average word, a 100-rpm motor will permit you to send 20 words per minute; a 60-rpm motor, 12 words per minute, and so on.

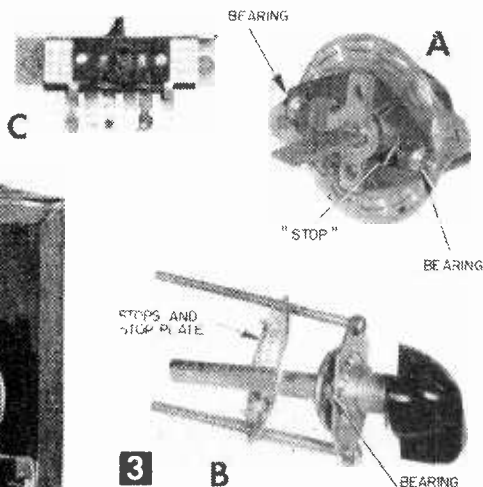
But motors aren't usually built to run that slowly, and a gear train is needed to reduce their speed (and increase their torque). I used a worm gear with an 80-tooth gear to get an 80:1 gear ratio and reduce the 6,000 rpm of the motor I used to 75 rpm. With my Typacode I can send about 15 words per minute. With speed reduced 80 times, torque is increased 80-fold, from 1.5 oz.-in. to 120 oz.-in. The motor I used consumes seven watts. The motor you use should have these approximate specifications in order to be able to turn the rotary switch. Most sewing machine or small fan motors are adequate, or try such a motor as the Hurst 60 rpm (RSM-60), Allied Radio catalog No. 76P862.



1

The number of words the device is capable of sending per minute may also be varied by the introduction of a variable voltage transformer to control the speed of the motor. This will help in adjusting word out-

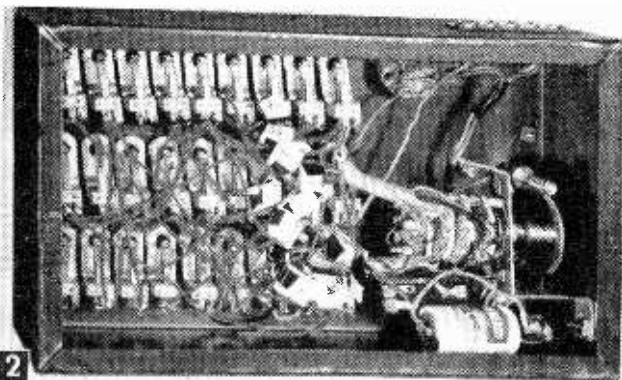
Standard rotary switch is shown in A; stop to be twisted off or bent down, bearings to be removed. In B is shown a miniature rotary switch. Its stop must be twisted off or bent down, or plate taken off; bearing to be removed. In C is shown an altered (as described in text) slide switch for slide-switch version of Typacode.



3

B

Bottom view of Typacode, showing tagged wiring.



2

put to the sender's typing ability and the auditor's understanding.

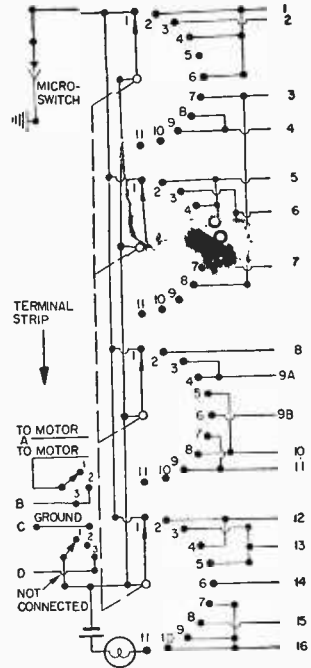
Construction. First remove the bearings which cause the rotary switch to click when turned (see Fig. 3). Pry them out with a screwdriver. Also, remove all of the "stops" which prevent the switch from turning continuously in one direction.

There are two basic versions of the device. One uses push-button, and the other uses spring-return slide switches. The spring-return slide switch version is somewhat cheaper, but a bit more difficult to operate. Choose the version you want to build (Figs. 1 and 2 show the push-button version), buy materials, and in either case, wire the shorting gang switch first (Fig. 5 for push-button unit, Fig. 6 for slide-switch unit).

If the gang switch is to be turned clockwise by the motor, Fig. 5 (and Fig. 6) is shown as one looks at the front of the switch. If, on the other hand, the switch shaft is to be turned counterclockwise, reverse the connections. That is, assume that the diagram shows the gang switch as you would look at it from the rear, and wire accordingly. (Remember that gears sometimes

ONE MAKE POS. EACH ON SW . . .	IS TO BE CONNECTED TO WIRE (S)	WITH MORSE CODE EQUIVALENT
A-----9A (SEE FIG. 8)	---	---
B-----1,15	----	----
C-----1,11	----	----
D-----1	---	---
E-----	---	---
F-----6,10	----	----
G-----5,7	----	----
H-----13,7	----	----
I-----2	---	---
J-----9,16	----	----
K-----1,7	----	----
L-----9,15	----	----
M-----5	---	---
N-----12	---	---
O-----5,3	----	----
P-----9,11	----	----
Q-----5,16	----	----
R-----9	---	---
S-----13	---	---
T-----8	---	---
U-----6,13	----	----
V-----3,13	----	----
W-----7,9	----	----
X-----1,4	----	----
Y-----1,16	----	----
Z-----5,11	----	----
PERIOD-----9A (HOLD FOR THREE FLASHES OF INDICATING LIGHT SEE FIG. 8)	----	----

4 CHART FOR WIRING PUSH BUTTON VERSION



5 WIRING OF PUSH-BUTTON VERSION (SEE FIG. 4)

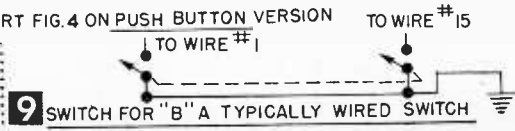
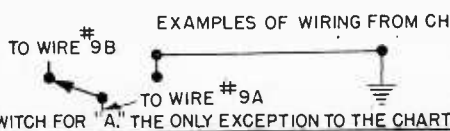
change the direction of rotation of the switch shaft.) For convenience, label the wires with tabs numbered as shown in the diagram. Allow approximately 5 in. of wire for connecting the rotary switch to the push-button or slide switches.

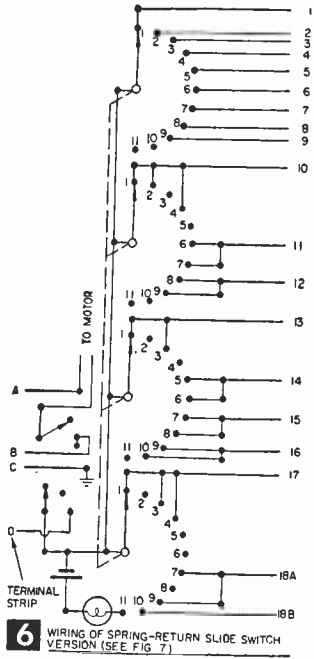
Now drill the holes in the chassis. Arrangement of the keyboard is left to the builder, but it will be found convenient to imitate that of the standard typewriter as closely as possible. Centers of holes for the Allied push-button switches are 3/4-in. apart in rows; the rows are spaced 2 in.

If you are using spring-return slide switches, adjust the sliding mechanism as shown in Fig. 3. Next, install the switches. There is a ground lug

MATERIALS LIST—TYPACODE
Push-Button Version

- | No. Req'd | Description |
|-----------|---|
| 18 | DPST normally open push button switches for letters B, C, F, G, H, J, K, L, O, P, Q, U, V, W, X, Y, Z and period (Allied 34 B 997) |
| 7 | SPST normally open push button switches for letters D, I, M, N, R, S, T (Allied 34 B 994) |
| 1 | SPDT push-button switch for letter A (Allied 34 B 996) |
| 1 | four pole, 12 positions per pole, shorting rotary switch (Only ten positions are needed for wiring; two extra needed for spacing between letters (Allied 34 B 906) |
| 1 | 3 x 7 x 12" chassis (Allied 80 PX 464). Only 7 x 8" is needed for push button keyboard, but since size of the motor will vary, the rest of the space needed is estimated with ample allowance for variations. |
| 1 | motor of the type specified in article and gear assembly * |
| 1 | 1 1/2 v. flashlight battery |
| 1 | indicator light assembly (Allied 52 E 475) |
| 1 | miniature bulb (Allied 52 E 330) |
| 1 | two-pole, 3 positions per pole, shorting rotary switch (Allied 34 B 303) |
| 1 | SPST normally open micro switch (Allied 35 B 028) |
- * Gears for either push-button or slide switch version are available from the Boston Gear Works with its main office at 14 Hayward St., Quincy 71, Mass. and offices throughout the country. Gear combinations are as follows:
 For a 100-1 gear ratio, a 100-tooth worm gear (Boston Gear G1023; hole dia 1/4") and a worm (Boston Gear HLSH; hole dia. 3/16") are needed.
 For an 80-1 gear ratio, an 80-tooth worm gear (Boston Gear G1022; hole dia 1/4") and a worm (Boston Gear HLSH; hole dia. 3/16") are needed.
 For a 60-1 gear ratio, a 60-tooth worm gear (Boston Gear G1024; hole dia. 1/4") and a worm (Boston Gear HLSH; hole dia. 3/16") are needed.
 1 coupling between motor and switch or gear assembly





6 WIRING OF SPRING-RETURN SLIDE SWITCH VERSION (SEE FIG. 7)

ONE MAKE POS EACH ON SW....	IS TO BE CONNECTED TO WIRE (S)
A	4, 13
B	6, 8, 10
C	9, 10, 11
D	6, 10
E	1
F	8, 13, 14
G	5, 7, 10
H	5, 7, 13
I	1, 3
J	11, 16, 17
K	10, 11
L	6, 8, 17
M	5, 10
N	10
O	5, 10, 15
P	9, 11, 17
Q	5, 10, 18
R	6, 17
S	5, 13
T	1, 2
U	13, 14
V	5, 13, 15
W	11, 17
X	6, 10, 12
Y	10, 11, 16
Z	5, 10, 18A

PERIOD-----13, 4
HOLD FOR THREE FLASHES OF INDICATING LIGHT)

7 CHART FOR WIRING SPRING-RETURN SLIDE SWITCH VERSION

then glued to the surface of the button. Complete the wiring, using the chart Fig. 4 for push-button switches or chart Fig. 7 for slide switches. The first column in the charts refers to the switch, the second to the labeled wire or wires which illustrate connections to switches.

Use. The micro switch is thrown when you want to indicate the end of a word; otherwise the letter "e", a short pulse, is automatically sent. This "e" is a simplifying factor in wiring, since all letters start with a pulse. This pulse is elongated for a beginning dash. The automatic "e" and micro-switch are eliminated on the spring return slide switch unit, the micro switch being comparable to a spacing bar.

On the terminal strip, terminals A and B connect to the power source for the motor (ideally a variable voltage transformer). Terminals C and D connect to the wires otherwise connected to the sending key of the buzzer, code practice oscillator, etc.

Turn the two-pole, three-position switch to the second position. The motor is on, but the unit is not capable of sending code. Next turn the switch to the third position. Each time the motor makes a revolution the bulb will light, and shortly after a short pulse will be sent (only on the push-button unit). Depress the micro "spacing" switch (on the push-button unit only); the bulb will still light, but no pulse will be sent.

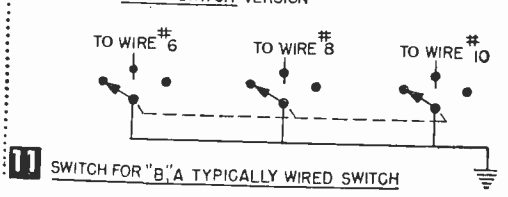
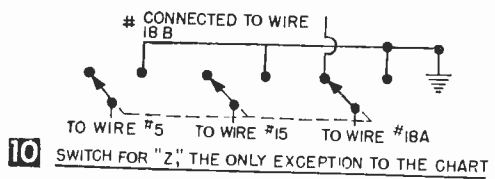
Directly after the bulb lights press the letter "a". A distinct "didah" will be heard. Release "a" and press "b" when the bulb lights again. Continue throughout the alphabet, checking against a standard table showing code equivalents for letters.

on the Allied push-button switches. Solder two different poles of each two-pole switch, and one pole of each one-pole switch to these lugs. This saves on wiring since now the poles on each switch are interconnected through the metal chassis. Otherwise (on slide switches) interconnect the different poles on each switch. The interconnected poles are referred to as "ground" and are connected to "C" on the terminal strip. Now install the motor, rotary switches, micro switch (this, only in push-button unit), bulb, and bulb socket, and letter the switches. For the push-button switches the letters were typed on a sheet of paper, punched out with a paper punch,

MATERIALS LIST—TYPCODE
Spring-Return Slide Switch Version

- | No. | Req'd | Description |
|-----|--|--|
| 2 | SPST | normally open spring return slide switch for letters E, N * |
| 11 | DPST | normally open spring return slide switches for letters A, D, I, K, M, R, S, T, U, W and period* |
| 13 | three-pole, single throw, | normally open spring return slide switches for letters B, C, F, G, H, J, L, O, P, Q, V, X, Y* |
| 1 | three-pole, double throw, | spring return slide switch for letter Z * |
| 1 | two-pole, three positions per pole, | shorting rotary switch (Allied 34 B 303) |
| 1 | 1 1/2 v. flashlight battery | |
| 1 | motor of the type specified in article, | and gear assembly |
| 1 | 7 x 12 x 3" chassis (Allied 80 PX 464). | Only 7 x 9 in. is needed for slide switch keyboard, but since size of the motor will vary, the rest of the space needed is estimated with ample allowance for the variations |
| 1 | four-pole, 12 positions per pole, | shorting rotary switch (Only ten positions are needed for wiring; two extra needed for spacing between letters (Allied 34 B 906) |
| 1 | miniature bulb (Allied 52 E 330) | |
| 1 | indicator light assembly (Allied 52 E 475) | |
- wire, solder, etc.
* The only spring return slide switch available was a 3-pole, double throw switch. (Allied 34 B 496). If a 3-pole push button switch is available, this device may be built using it.

EXAMPLES OF WIRING FROM CHART FIG. 7 ON SLIDE SWITCH VERSION



An Electronic Antenna Relay

For the amateur who still throws an antenna switch, this inexpensive electronic relay will do the job automatically on any band up to two meters, and it will increase the sensitivity of most receivers

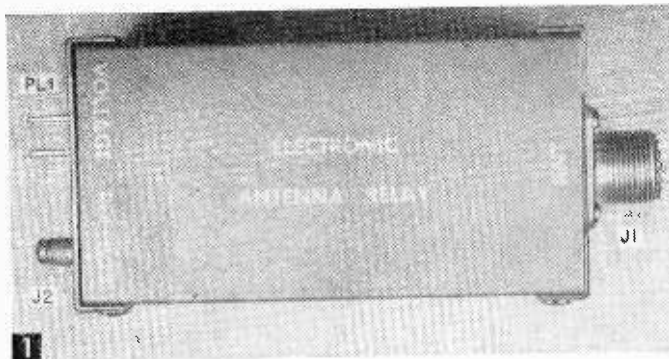
By JOE A. ROLF,
K5JOK

THE one-tube relay shown in Fig. 1 will handle up to 100 watts CW, or 85 watts phone. It is designed for use with any amateur antenna having an impedance of 25 to 300 ohms, and it permits instant CW break-in and greatly simplifies AM transmitter control. It also acts as a low-gain RF amplifier to improve receiver performance.

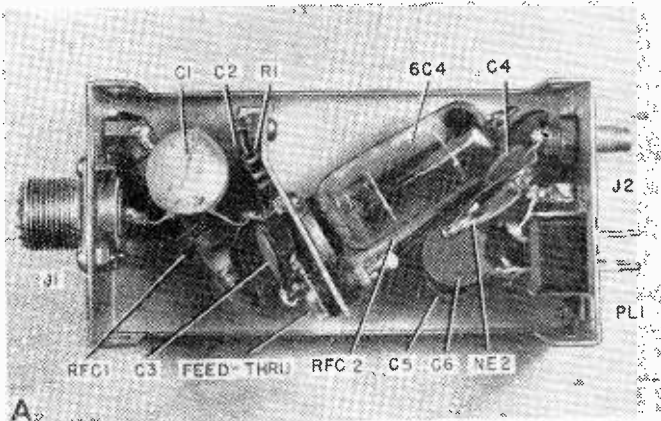
Figure 2 shows the circuit, Fig. 3 the connections to transmitter, receiver, and antenna. The T-R switch is inserted across the antenna feedline, in parallel with the transmitter. With the transmitter inoperative, the relay acts as a grounded-grid amplifier, allowing signals from the antenna to pass through to the receiver. When the transmitter is keyed, however, the relay's 6C4 is blocked and effectively isolates the receiver from the antenna.

The large biasing resistor R1 permits the 6C4 to conduct very weak RF signals to the receiver, while the strong signal from the transmitter creates a cut-off bias on the tube that prevents conduction to the receiver. Very little power is taken from the antenna since only a small amount of RF is required to block the 6C4.

The entire relay is built inside a 1½ x 2½ x 4-in. Minibox. For compactness and simplicity, the unit is powered by the station receiver or transmitter. A Cinch-Jones chassis plug receives the power cable; a miniature



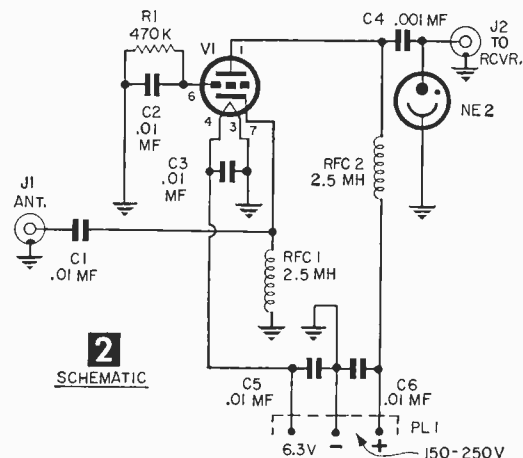
The completed electronic antenna relay, or T-R Switch, with the cabinet lid in place (above). This unit will permit instant break-in operation with CW transmitters of up to 100 watts input. It can also be used with phone transmitters running up to 85 watts. Interior of the relay cabinet showing construction and layout (below). The 6C4 is mounted on a small aluminum bracket (see Fig. 4) that also serves as a shield between the input and output components. The plate lead on the tube socket is brought through the bracket with a feed-through insulator.



coax antenna jack mounted beside it connects the unit to the antenna terminals of the receiver. A standard coax jack at the other end of the Minibox connects the unit to the antenna feedline. Construction and drilling details are shown in Fig. 4.

The author used a six-prong power plug (Cinch-Jones P-306-AB) on his unit to match an existing cable from his receiver. A three- or four-prong power plug can be used if desired. Also, if the builder prefers, phono jacks can be substituted for the coax antenna jacks—though coax jacks are recommended for high-frequency use to avoid losses and to insure adequate shielding.

The 6C4 is mounted on a small aluminum bracket (see Fig. 4) fastened to the bottom of the Minibox. The bracket is set at an angle



2
SCHEMATIC

MATERIALS LIST—ELECTRONIC ANTENNA RELAY	
Desig.	Description
C1	.01 mfd. 1.6 Kv disc ceramic or mica capacitor
C2, C3, C5, C6	.01 mfd. disc ceramic capacitors
C4	.001 mfd. disc ceramic capacitor
J1	Coaxial chassis jack and plug (Amphenol 83-1R and 83-1SP or equivalent)
J2	miniature coaxial chassis jack and plug (Jerrold C-52 and C-61 or equivalent)
NE-2	neon bulb
R1	470,000 ohm, 1/2 watt resistor
RFC1	2.5 mh, 125 ma RF choke (National R100 or equivalent)
RFC2	2.5 mh, 125 ma RF choke (National R100 or equivalent)
PL-1	Cinch-Jones 6, 4, or 3-prong chassis plug with matching socket
V1	6C4
1	9-pin miniature Bakelite or ceramic tube socket
1	miniature feed-through insulator, RF type
1	Bud CU 2102A Minibox, 2 x 1 1/2 x 4"
Misc	RG-58/U or RG-59/U coaxial cable (see text), 1 pc 1/16" aluminum, 2 x 2"; twelve 6-32 x 1/4" machine screws; nuts; solder lugs, etc.

to facilitate tube removal and to allow room for the power plug and associated components. It is important that the tube socket be Bakelite or ceramic to give good RF insulation.

For proper operation, it is also important to minimize capacitive coupling between the input and output sections of the circuit. The extra plate lug on the tube socket (pin 5) should be clipped off and pin No. 1 positioned to solder directly to a small feed-through insulator at the top corner of the tube bracket. If the relay is to be used on lower frequency bands only, a simple insulator can be made by passing a machine screw through a small rubber grommet. For high frequencies, the insulator should be a low-loss RF type.

The components in the input of the circuit, C1, C2, C3, R1 and RFC1, are mounted beneath the tube socket. The output components are mounted on the power plug side of the tube bracket. The tube mounting bracket acts as a shield between the input and output of the relay.

Choke RFC1 should be self-supporting, about 1/4 in. away from the sides of the cabinet. Choke RFC2 is insulated with a layer

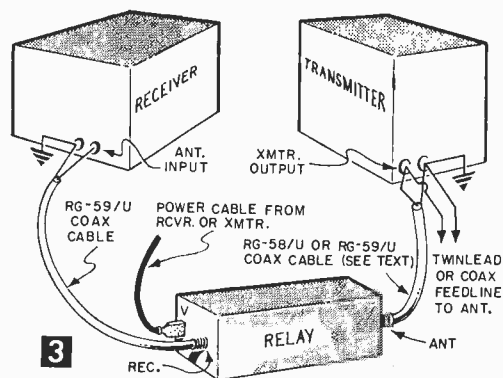
of tape or gummed paper to prevent accidental contact with the chassis and other components. Connect C3 from pin 4 of the tube socket to ground; C5 and C6 from their respective power socket pins to ground. These capacitors bypass any RF on the power cable to ground.

Power requirements for the relay are 6.3 v at 150 ma for filament supply, and from 150 to 250 v at about 25 ma for the plate. These voltages are obtainable from most amateur receivers and transmitters. Check the schematics of yours.

The relay is designed to work into an unbalanced transmission line (one lead grounded, the other hot), since most modern transmitters feature this type of output. If the antenna impedance is in the vicinity of 53 ohms, connect the relay to the antenna with type RF-58/U coaxial cable. Type RG-59/U coax can be used for ribbon or coaxial feedlines having impedances from 70 to 300 ohms. The cable from the relay to the receiver should be RG-59/U coaxial cable. In each case, the outside conductor of the cable is connected to the grounded antenna terminal, the inner conductor to the above-ground terminal.

The lead between the T-R Switch and the receiver should be as short as possible. The lead to the antenna can be as long as 3 ft. without noticeable effect and can be connected to the output terminals of the transmitter if a low-pass filter is not used in the transmission line. If a filter is used, connect the relay to the antenna side of the filter. With transmitters having coax output jacks, it is best to install a second jack in the transmitter for the relay and to make feedline connections inside the transmitter cabinet. This will reduce unwanted radiation and facilitate the use of different antennas if the transmitter is operated on more than one band.

Test the relay by first loading the transmitter to the antenna and then connecting the



3
CONNECTIONS TO RCVR., XMTR., ANT.

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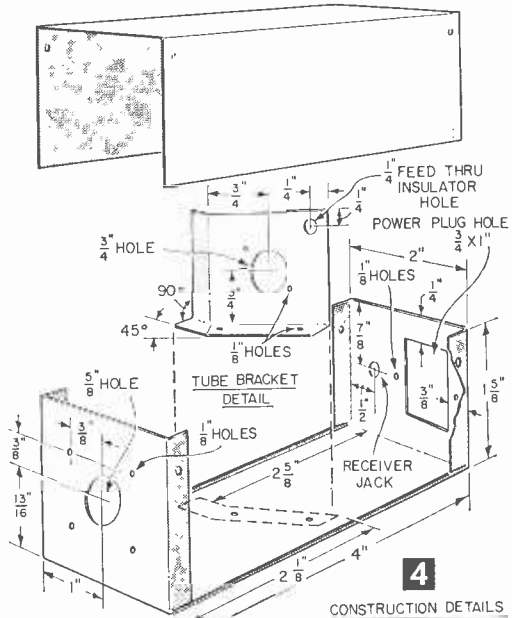
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4 CONSTRUCTION DETAILS

relay as shown in Fig. 3. The receiver should not be connected during initial tests. Apply power to the T-R Switch and reload the transmitter to the antenna. If the relay is working properly, the transmitter should require only slight readjustment, if any.

The neon bulb NE-2 is a safety device to indicate any dangerous amount of RF across the output terminals of the relay. If this bulb glows when the transmitter is keyed, it is an indication that the relay is not working properly. Check for a bad tube or wire-up.

If the unit is carefully constructed, only enough RF will reach the receiver to provide comfortable monitoring. If the receiver overloads while transmitting, it is probable that RF is entering the receiver through ventilation louvers or an exposed antenna connection (if the receiver has a terminal strip antenna post).

But a coax antenna jack and copper window screen taped over ventilation openings in the receiver cabinet will generally cure this. In some cases, shielding the transmitter cabinet will help. Another remedy for overloading on CW, or feedback on phone, is to reduce the receiver gain control when transmitting.

The cost of this simple electronic antenna relay is only slightly more than that of a good antenna relay, but this unit has the advantage of permitting switchless CW operation with a single antenna system. To transmit, just start keying and the receiver is automatically disconnected from the antenna. On phone, only one switch is needed to put the transmitter on the air.



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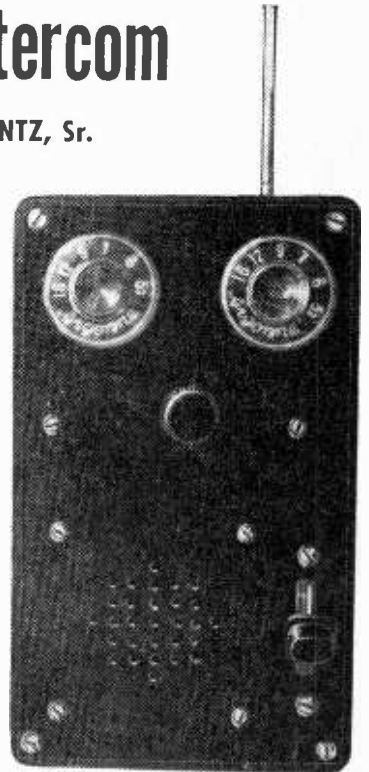
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A Portable Wireless Intercom

By FORREST H. FRANTZ, Sr.

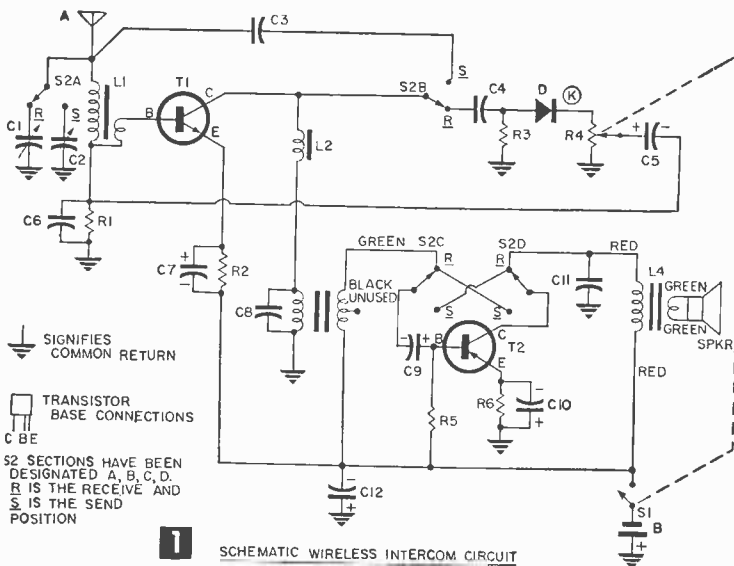


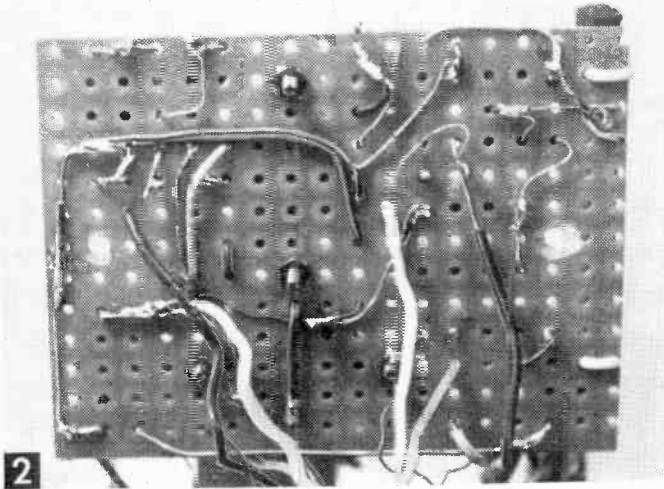
A neat, compact, two-transistor device, this portable intercom also functions as a broadcast band receiver.

This transceiver makes an excellent week-end construction project. It does not require a license!

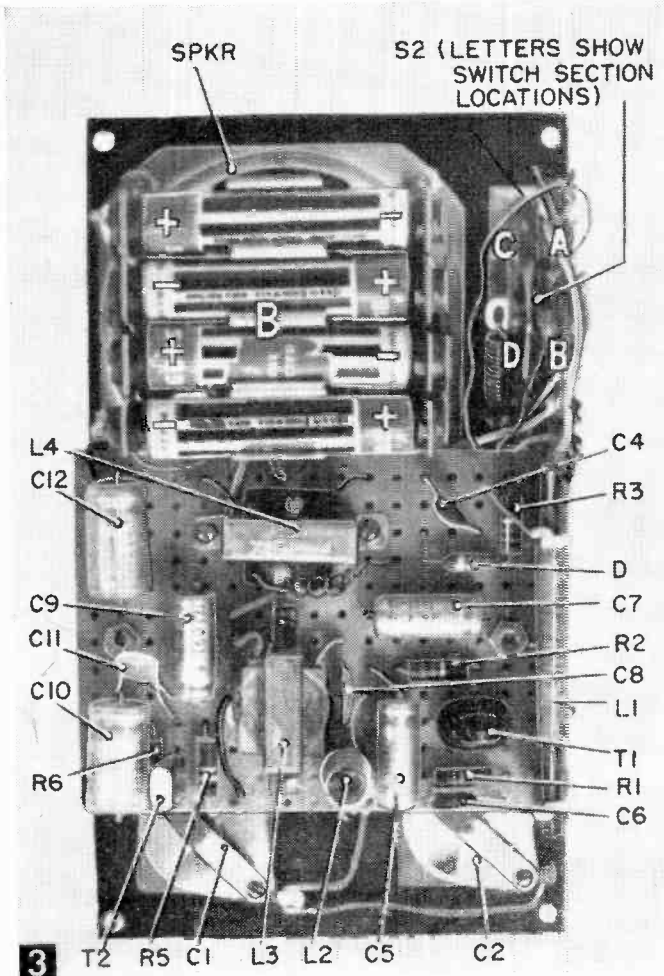
THERE'S no need to be stuck with intercom stations at fixed locations in your home. This portable wireless intercom can be carried wherever you wish to use it. It operates in the broadcast band under FCC limited radiation rules, and therefore does not require a license (limit communication distance to 75 ft.), and the receiver can be used for BCB reception. Components will cost between \$10 and \$15. For two-way communications, of course, you need two units. But with one unit you can indulge in one-way communication by using a broadcast receiver as the second station.

Trouble-Free Construction. The leads connecting to the Send-Receive switch, and those in the RF portion of the unit should be kept short and direct. When construc-





Circuit board wiring.



Parts call-out in case.

tion is completed, you may have to redress them to eliminate oscillation. First, remove antenna coil L1 from its Masonite mounting strip. Then cut shaft of volume control R4 to a length of $\frac{1}{4}$ in. Then turn connection of battery holder lugs over with pliers to form series connections and solder (see Fig. 3). Fill contact eyelets with solder.

Jumble-wind coupling coil L2 from 25 ft. of 7/41 litz wire on $\frac{3}{4}$ -in. length of $\frac{1}{4}$ -in. dia. ferrite core. Leave $1\frac{1}{2}$ in. connecting leads. Apply a coat of Duco cement to hold the windings in place. Clean and tin the ends of the leads.

Drilling and Cut-Outs. The circuit board as purchased is cut to correct size. Holes must be drilled in it as shown in Fig. 4. The front panel as purchased is cut to correct size and contains the four corner holes required to fasten it in the case. The other hole and switch cut-out locations are shown in Fig. 5. The cut-out for the Send-Receive switch is made by drilling a series of adjacent holes, finished with a keyhole saw and a file. The hole in the case for mounting the antenna is $\frac{1}{2}$ in. dia. placed 1 in. from the front and 1 in. from the right-hand side on the top of the case.

Front Panel Component Mounting. Mount C1 and C2. The dials are removed by loosening the knurled decorative head screws. These capacitors, because of their compact construction, sometimes develop shorts. Connect an ohmmeter across each of them in turn and rotate the shafts. If either of the capacitors is shorted, send it back to the supplier for replacement. *Don't* attempt a repair.

Mount the volume control (R4), the Talk-Listen switch (S2) and the loudspeaker (SPKR). Place the knob on R4 and the handle on S2. Fasten the 1-in. machine screws (which hold the circuit board in the final assembly) to the front panel.

Circuit Board Wiring. Mount transformers L3 and L4, and mount the antenna coil L1.

Fasten the coil with insulated hook-up wire or cord passed through the circuit board and tied around the coil. A few drops of Duco cement will hold it in place.

Using Figs. 1, 2, and 3 for guidance, wire the circuit board. Mount the components as required in the progress of the wiring. Note that most of the component pigtails pass through the circuit board. The pigtails are bent over and soldered together to form the circuit wiring. This produces a neat job, permits you to make short connections, and makes the compact size of the unit possible.

The leads which are to be connected between the circuit board and the panel wiring of the circuit board should be connected during the wiring of the circuit board. Leave these leads about 6 in. long and cut to length later when the wiring board and panel assemblies are integrated. Use wires of different colors and keep a record of the code to make integration of the circuit board and front panel easier.

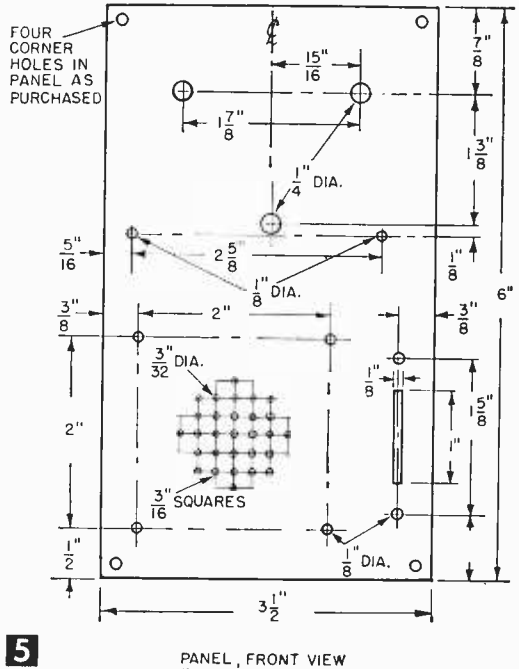
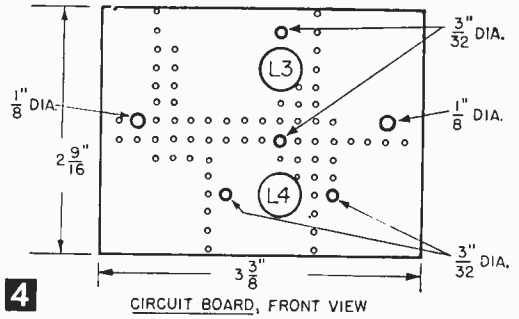
Front Panel Wiring. Wire R4-S, C1, C2 and the portion of the S-2 connections that do not tie into the circuit board wiring. The gimmick C3 is simply a piece of hook-up wire connected to S2 and twisted loosely around the lead from S2 to C2. Wire insulation acts as the dielectric. In making connections to S2, be careful to avoid bending or exerting undue pressure on the switch contacts and lugs. Also be cautious about exerting pressure on the switch wafer.

Mount the circuit board on the 1-in. machine screws provided on the front panel for this purpose. The nuts near the ends of these screws (Fig. 2) should be adjusted for correct spacing of the mounting board from the panel. Be sure that there aren't any shorts between the switch S1 and the circuit board. The lugs of S1 may have to be bent slightly to the side.

Make the interconnections between the front panel and the circuit board. The secondary of L4 connects to SPKR and several leads from the circuit board connect to R4-S1 and S2.

Mount the battery holder on the speaker magnet frame by passing a loop of wire around the holder and frame on each side of the magnet. Twist the ends together on the bottom side. A drop of Duco between the speaker and the battery holder will tend to make the mounting more solid. Connect the battery holder into the circuit. Insert the batteries in the holder, observing correct polarity. Then provide a lead from S2A to the antenna and place the assembly in the case. But don't fasten the four panel holding screws yet.

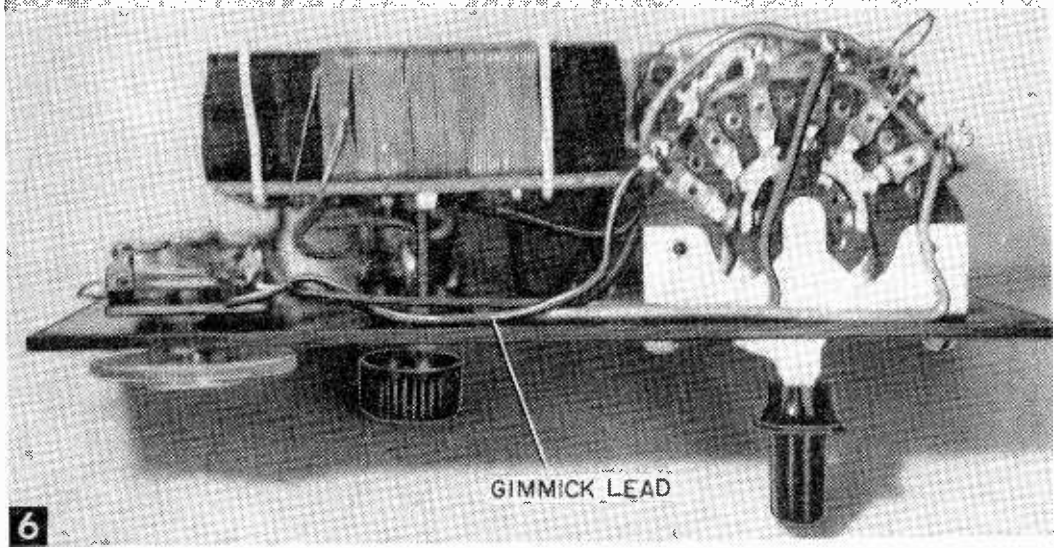
Testing Operation. Turn switch S1 on and turn R4 clockwise for maximum volume. Tune C1 to a local broadcast station. If you can't pick up a station, extend the antenna. If you still can't pick up a station (assuming



you're within 5 miles of a 250-watt station or within 10 miles of a 5 KW or more powerful station), recheck the wiring. Incorrect positioning of the S2C and S2D leads may cause audio feedback. To cure consistent squealing and whistling, redress these leads.

When you have broadcast reception, remove the set from the case and move the position of the lead on the antenna end of L1 relative to C4 for maximum gain at the high-frequency end of the broadcast band. Then decrease the volume control setting to about half of full setting. If the set squeals, decrease the coupling between the L1 lead and C4 till squealing quits.

Turn a broadcast receiver on and tune to a frequency at which you don't receive a broadcast station. Then, from a position near the receiver, with the intercom on and the antenna pushed down, push S2 to the send position. Adjust C2 till the intercom carrier comes in on the broadcast receiver. The



Side view of front-panel mountings.

coupling of gimmick C3 may have to be increased to attain a signal or decreased to minimize squealing and distortion at the receiver. Audio feedback due to coupling between intercom and receiver causes squeals also—but occurs only when receiver and intercom are within audible “hearing” distance.

The antenna may be extended to increase range, but don't open it far enough to permit reception beyond 75 ft. The intercom will function best for communication when held upright with the antenna vertical. It will function best as a broadcast receiver when the antenna loop is horizontal. It is extremely directional and selective in this plane.

MATERIALS LIST—WIRELESS INTERCOM	
Desig.	Description
R2, R6	270 ohm, 1/2 watt carbon resistor, 10%
R3	33K, 1/2 watt carbon resistor, 10%
R5	100K, 1/2 watt carbon resistor, 10%
R1	270K, 1/2 watt. carbon resistor, 10%
R4-S	10K miniature volume control with switch (Lafayette VC-28)
C3	gimmick (see text)
C4	100 mfd., 1000 v. ceramic capacitor (Sprague 5 GA-T1)
C6, C8, C11	.01 mfd., 50 v. ceramic capacitor (Sprague TG-S10)
C5, C7, C9	25 mfd., 6 v. miniature electrolytic capacitor (Sprague TE-1091)
C10, C12	100 mfd., 6 v. miniature electrolytic capacitor (Sprague TE-1102)
C1, C2	365 mmf. miniature variable capacitor (Lafayette MS-445)
T1	2N168A transistor (General Electric)
T2	2N407 transistor (Sylvania)
D	1N66 diode (Raytheon)
S2	4P2T spring return lever action switch (Centralab 1457)
L1	ferrite antenna loop coil (Miller 2004)
L2	25' 7/41 litz wire wound on 3/4" length, 1/4" dia. ferrite core. (Lafayette MS-331 is a 7 1/2" length of ferrite core and Belden 8817 is a 100' length of the wire)
L3	10K to 2K miniature driver transformer (Lafayette TR-96)
L4	2K to 10 ohm miniature output transformer (Lafayette TR-93)
SPKR	10 ohm, 2 1/2" loudspeaker (Lafayette SK-66)
A	miniature telescoping antenna (Lafayette F-343)
B	four 1.5 v. penlite cells, series connected (Burgess No. 7)
	battery holder (Lafayette MS-170)
	miniature knob (Lafayette MS-185)
	27 1/6 x 33 3/8" miniature perforated circuit board (Lafayette MS-304)
	2 x 3 3/4 x 6 1/4" Bakelite case (Lafayette MS-216)
	front panel for case (Lafayette MS-217)

Components for this project may be obtained from Lafayette Radio, 100 6th Avenue, New York 13, N. Y.

Operating Principles. The remote wireless intercom is an intercom that permits talk-and-listen operation with another unit without requiring connecting wires. The speaker functions as mike and speaker. Separate talk and listen tuning controls permit tuning to any desired frequency with easy switching from talk to listen without having to retune. To receive, C1 must be set for the frequency that C2 of a second intercom is tuned to in order to receive it. It is best to tune the two intercoms and then lock the capacitors. Don't depend on dial calibration to do the job.

The wireless intercom employs only two transistors and one diode. In the listen function T1 acts as an RF amplifier, and diode D1 rectifies the signal to provide an audio voltage signal. This signal is fed back through T1 which amplifies the signal again. Then the signal progresses to output stage T2 and the loudspeaker. The receiving circuit achieves considerable gain and selectivity with minimum equipment through the use of good components and the exercise of design innovations.

On the talk function, the coupling from the collector of T1 to the antenna and base of T1 is increased by C2 to produce broadcast frequency oscillation. The input and output connections to T2 are changed by S2 to make the speaker function as a mike and to make T2 function as a modulator for T1.

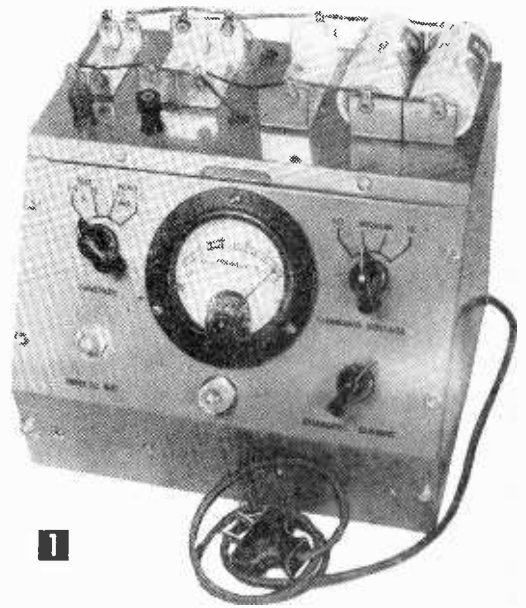
Dry Battery Tester-Charger

A single unit to test and charge flashlight, transistor radio and other small batteries

By W. F. GEPHART

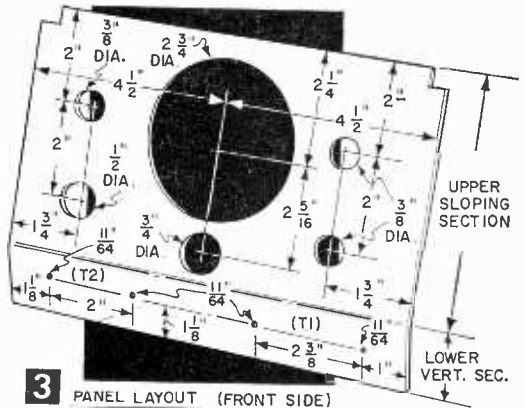
RECHARGING or boosting small dry batteries can be worthwhile if you have several flashlights, battery radios or other battery-powered equipment. Properly used, a charger can triple or quadruple the life of batteries, making the investment in a charger worthwhile. The unit shown in Fig. 1 also includes a tester to show when "recharging" is desirable. (Since dry batteries are essentially primary cells in which a chemical reaction takes place, true recharging is not possible. However, rejuvenation, which will extend the life of the cells, is possible. We'll call this recharging.)

Recharging must be done before the battery is completely exhausted. New batteries usually read about 1.5 v per cell (without load) on the average meter. Under normal load (about 25 ma for a battery made up of penlight cells, and about 150 ma for the larger flashlight batteries) the voltage of a fresh cell should not drop more than 10%. Thus, a type "D" flashlight battery in top condition ought to test at 1.5 v or better without load, and not less than 1.35 v with a 150



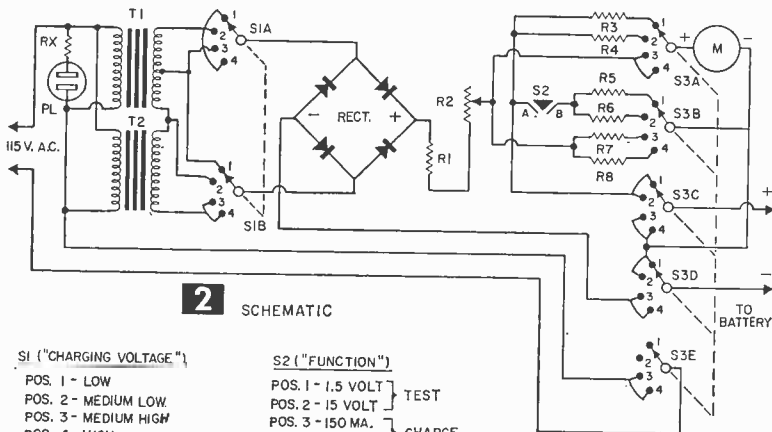
1

Overall view of charger. Battery clip arrangement may be varied to meet individual needs.



3

PANEL LAYOUT (FRONT SIDE)



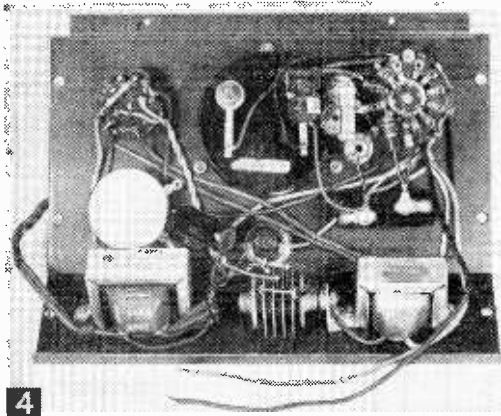
2 SCHEMATIC

S1 ("CHARGING VOLTAGE")
 POS. 1 - LOW
 POS. 2 - MEDIUM LOW
 POS. 3 - MEDIUM HIGH
 POS. 4 - HIGH

S2 ("FUNCTION")
 POS. 1 - 1.5 VOLT } TEST
 POS. 2 - 15 VOLT }
 POS. 3 - 150 MA. } CHARGE
 POS. 4 - 15 MA. }

ma load. When it drops below these levels, it should be recharged. Recharging is not too effective when the voltage (with or without load) is below two-thirds of the new-condition voltage.

Bear in mind, too, that the battery must be placed in service promptly after recharging. The shelf life of recharged batteries is short (probably due to the limited chemical action that takes



4 Inside view of unit. All parts are mounted on back of front panel.

place). Even so, the drop in voltage after charging is the greatest in the first 24 hours.

No one seems quite sure what actually happens in dry battery recharging, and some experimenters claim the best results with *ac* charging voltages, some with *dc*, and some with a combination. This unit uses unfiltered, fluctuating *dc*, which seems to give the best results in the shortest time. Filtered *dc* (secured by placing a large capacitor across rectifier output) seems to give about the same results, but requires a charging time of 12-20 hours.

Here are some results with unfiltered *dc* and an hour's charging time:

Type Battery & Service		Before Charge	Immediately After Charge	2-5 Days Later*
Two "D" Cells (Flashlight)	No Load	1.35 v	1.52 v	1.40 v
	Load	1.20 v	1.37 v	1.35 v
Three "D" Cells (Strobelight)	No Load	1.33 v	1.40 v	1.35 v
	Load	1.15 v	1.33 v	1.30 v
Two "C" Cells (Flashlight)	No Load	1.35 v	1.60 v	1.45 v
	Load	1.15 v	1.50 v	1.35 v
9 v Transistor# (Radio)	No Load	7.5 v	8.7 v	8.0 v
	Load	2.0 v	7.2 v	6.0 v

* shelf life time; not in service

charged at 9 ma; all others charged at 100 ma

We see that particularly in the case of the transistor battery, recharging is not too effective when the battery nears exhaustion. The charging rate must be fairly low, with a range of 5-30 *ma* recommended for batteries made up of penlight cells, and a range of 50-200 *ma* for the larger cells, such as "C", "D", and "A" cells.

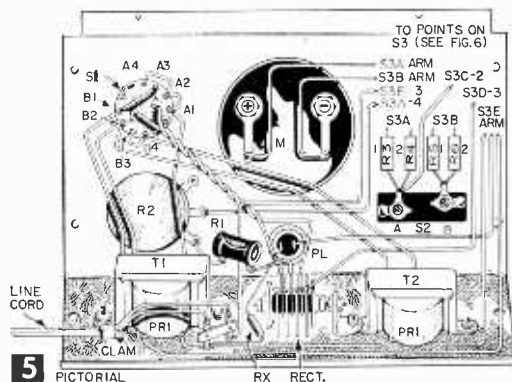
Schematic Fig. 2 shows that switch S_3 controls the function of the unit. On Positions 1 and 2, used for testing, proper meter multipliers are switched into the circuit for reading the battery voltages, and load resistors are cut in by pressing switch S_2 . When switch S_3 is on Positions 3 and 4, *ac* power is on, and the *dc* output is fed through the meter (with proper current shunts) to the

MATERIALS LIST—BATTERY CHARGER

Desig.	Description
Rx	56K, 1/2 watt (required only if not included in PL)
R1	20 ohm, 1 watt
R2	200 ohm, 4 watt potentiometer (Mallory M200PK)
R3	1500 ohm 1% precision (see text)
R4	15K 1% precision (see text)
R5	10 ohm, 1/2 watt
R6	330 ohm, 1/2 watt
R7	.66 ohm 1% precision (see text)
R8	7.14 ohm 1% precision (see text)
S1	two-pole, 4-position rotary switch (Mallory 3226J)
S2	SPST push button, normally open
S3	five-pole, 4-position rotary switch (Mallory 1335L)
T1	6.3v CT 1 amp filament transformer (Merit P-2944)
T2	6.3v 1/2 amp filament transformer (Merit P-2964)
Rect.	bridge-connected selenium rectifier: a-c input—15 v maximum, at 200 ma (Federal 1016)
PL	pilot light holder for NE-51 lamp (Dialco Series 95408X and 942208 have built-in resistor Rx)
M	0-1 milliammeter
	Steel cabinet, 6 1/2 x 7 1/4 x 9" (Bud C-1585), NE-51 lamp, 3 knobs, 2 binding posts, battery holders as desired, line cord, miscellaneous hardware

battery, with terminal polarity reversed. The proper charging voltage and current is selected by switch S_1 and rheostat R_2 . Two filament transformers, with their secondaries wired in series through S_1 , provide *ac* input voltages to the rectifier of 3.15, 6.3, 9.45, and 12.6, which are sufficient for all batteries up to 9 volts. Resistor R_1 is a limiting resistor to prevent the current from reaching excessive levels.

All parts (except battery holders and terminals) are mounted on the front panel of a small sloping-front cabinet, as shown in



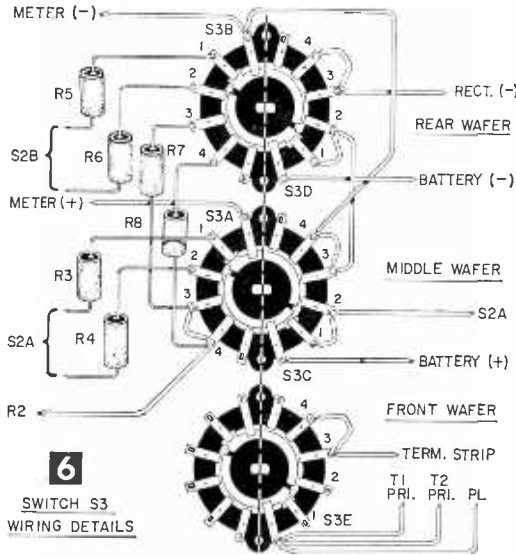
5

PICTORIAL

RX RECT.

Figs. 4 and 5. The layout for the panel is shown in Fig. 3, except for the meter mounting screw holes, which should be drilled to the meter being used.

The values shown for resistors R_3 , R_4 , R_7 and R_8 are applicable only to a 0-1 *ma* meter with an internal resistance of 100 ohms. This is a standard 1000 ohms/volt movement, but values for other meter movements can be calculated with the formulas top of opposite page for the ranges shown on Fig. 2:



6
SWITCH S3
WIRING DETAILS

$$R3 = \frac{15 - (I_m \times R_m)}{I_m} \quad R4 = \frac{15}{I_m}$$

$$R7 = \frac{I_m \times R_m}{.014} \quad R8 = \frac{I_m \times R_m}{.150}$$

I_m is the full scale deflection of meter in amperes, R_m is the internal resistance of meter in ohms.

Wire the primaries of the transformers and pilot light first. Then check polarity of the

secondary leads of the transformers so that series wiring will give 12.6 v. If the polarity is incorrect, the two secondaries will buck each other, and give no output voltage when wired in series. Complete the wiring.

The selection of the number and types of battery holders mounted on the cabinet will depend on individual needs. Two binding posts, wired in parallel with the battery holders, are also provided. Several sets of leads, using the most often needed battery plugs can then be used with the binding posts for those batteries that do not fit in the holders.

To use the unit, plug it in, turn S_1 to "Low", R_2 to full counterclockwise position, and S_3 to "15V Test." Put the batteries in the proper holder (or attach to leads), and switch S_3 to the appropriate scale and read the no-load voltage. Then press S_2 to read the voltage under load. Resistor R_5 provides a 150 ma load with 1.5 v, and R_6 provides a load of about 14 ma at 4.5 v, 18 ma at 6 v, and 27 ma at 9 v. Next, switch S_3 to the desired charging current range, and set the charging rate by adjusting S_1 and R_3 .

Generally, charging for an hour or two at the rates mentioned above will be effective. The rate may be increased, but under no conditions should the battery be permitted to get warm. Longer charging times can be used, with varying effectiveness, depending on the charging rate and battery condition, but the unit should be watched. Sometimes excessive charging, either in current rate or time, seems to break the cell down, and the current rises, increasing the damage.

Unscrewing the Inscrutable

Those Darn Decibels!

by Ol' Rock

Few terms are as frequently misused or widely misunderstood in electronics as is the *decibel*.

The decibel system merely *compares* signal power levels. Properly used, it makes possible a great simplification of arithmetic.

Decibels can be used to compare any two signal power levels of the same kind, in either an acoustical or electrical system. Or, one may compare the power of a given signal with a previously agreed-upon standard. When the signal being considered is compared to a similar, hypothetical, one-milliwatt signal, we speak of the "level" of the signal concerned, in DBM. Further, one may compare, in decibels, the strength of a given signal to that of the noise power in the same system—the "signal to noise ratio."

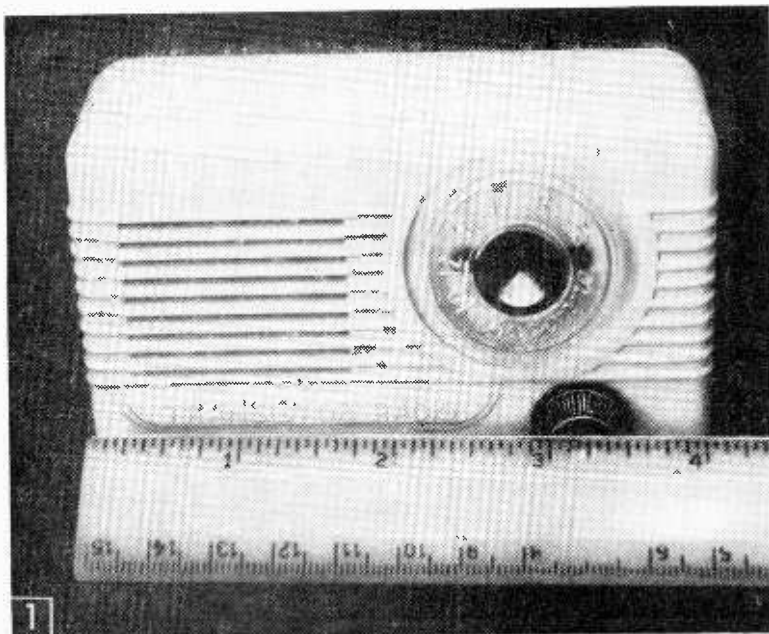
Let's get straight on the basic facts: First, the decibel measures *ratios*, that is, how many times greater or less-powerful is the signal concerned, as compared to the reference signal. Second, decibels are not measured upon an ordinary arithmetical scale, but rather upon what engi-

neers call a *logarithmic* scale. This is perhaps the most confusing point to the uninitiated. Twice as many decibels do *not* mean twice as strong a signal, for instance. Here's how a decibel scale works:

Ratio of Signal Power	DB Greater	DB Less
Signal powers equal	0 DB	0 DB
First signal twice as strong, or one-half as strong as the other	+ 3 DB	- 3 DB
First four times as strong or weak	+ 6 DB	- 6 DB
First ten times stronger or weaker	+10 DB	-10 DB
First 100 times greater or less	+20 DB	-20 DB
First 1000 times greater or less	+30 DB	-30 DB
First one million times greater or less	+60 DB	-60 DB

Any good electrical engineering reference book will show you how to obtain decibel values or corresponding power ratios for the intermediate values, such as -36 DB, +57 DB, etc.

A convenient feature of the decibel system is that amplifier gains and circuit losses, when each is expressed in DB, may be added and subtracted by simple arithmetic directly, to evaluate simply the performance of an entire communication system.

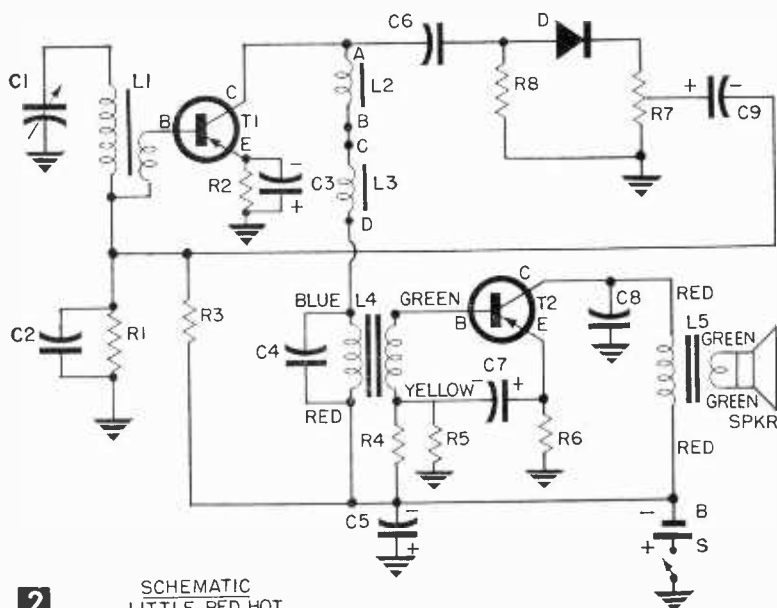


A set that's small but one that will scoop up rock 'n' roll from local broadcasters, commercials and all.

The Little Red Hot

This compact, attractive reflex receiver is so small it fits easily into pocket or purse

By FORREST H. FRANTZ, Sr.



SCHMATIC
LITTLE RED HOT

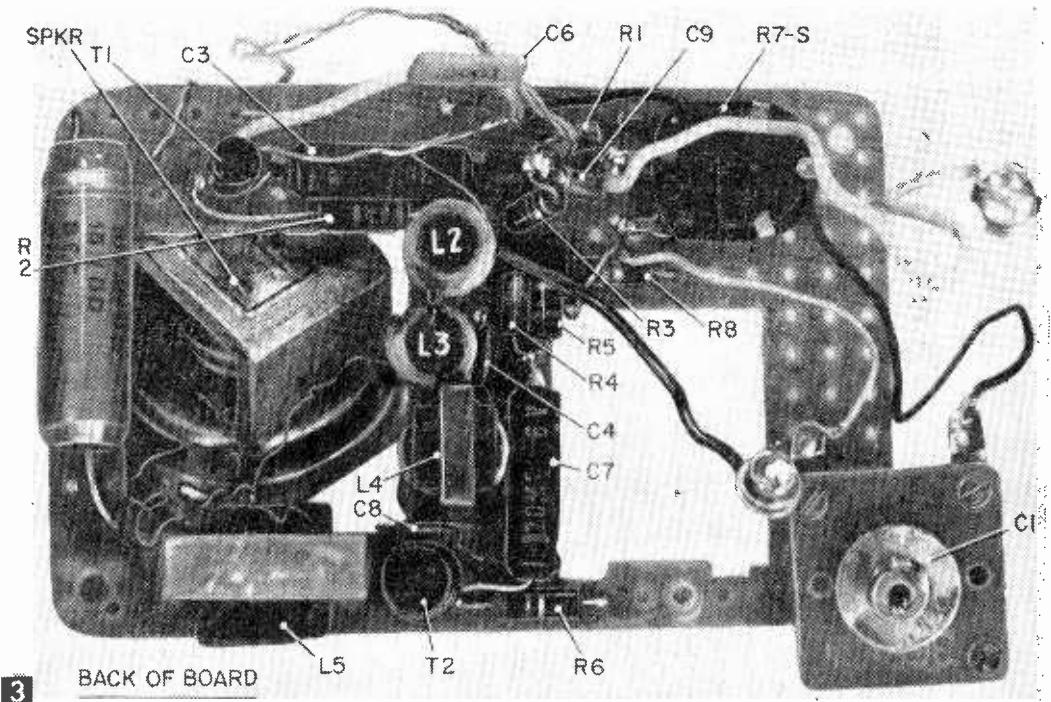
To get plenty of gain in the Little Red Hot transistor T1 (see Fig. 2) amplifies the signal twice, once while it is still RF and then again when it is AF after detection by diode D. The audio output of T1 is introduced to the base of transistor T2 through the audio driver transformer L4. The impedance match between T1 and T2 provided by L4 affords considerably more gain than you could expect from resistance-capacitance coupling.

Though not apparent from the circuit, and though not enough to make the set oscillate, there is positive feedback in the RF stage, resulting from the relative placement of the components in the case. This feedback feature and the high Q of the antenna coil (L1) make the set quite selective in spite of the fact that it has only one tuned circuit.

Cost of the components for the Little Red Hot will be a little over \$15. Construction time will vary with the builder's experience, but the compact construction makes this project a delightful experience in miniaturization.

Construction. The construction of this receiver may be accomplished most efficiently by pursuing the task in these phases:

- 1) Adapt parts.
- 2) Make the circuit board.



Back view before assembly.

- 3) Mount parts.
- 4) Wire the circuit board.
- 5) Complete wiring and assemble.
- 6) Test, adjust and debug.

Begin by cutting the volume control shaft to a length of $\frac{3}{8}$ in. Place the portion of the shaft to be eliminated in a vise and cut with a hacksaw. Now remove antenna coil L1 from its Masonite mounting board. Replace the paper tape around the coil ends to hold and protect the windings.

Make coils L2 and L3 using the data shown in the Materials List. Coat these coils with Duco cement to prevent unwinding of the turns.

The number of turns is not too critical, so if you slip a bit in counting them, don't worry about it.

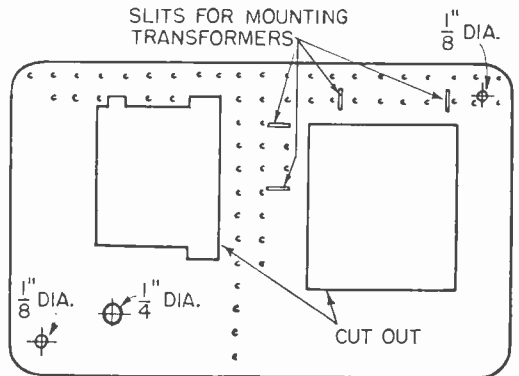
Next, place two layers of cellophane tape about $\frac{3}{8}$ in. wide around the edges of the speaker frame on the back of the speaker to prevent the speaker frame from shorting some of the receiver wiring which it would otherwise touch.

The circuit board is cut from a miniature perforated board according to the layout shown in Fig. 4. Speaker and tuning capacitor cut-outs are made by using the hacksaw blade removed from the saw frame. Starter holes can be made with drill and taper reamer. The slots for the transformers (L4 and L5) are also made with the hacksaw blade.

Drill a $\frac{1}{8}$ -in. starter hole for the volume

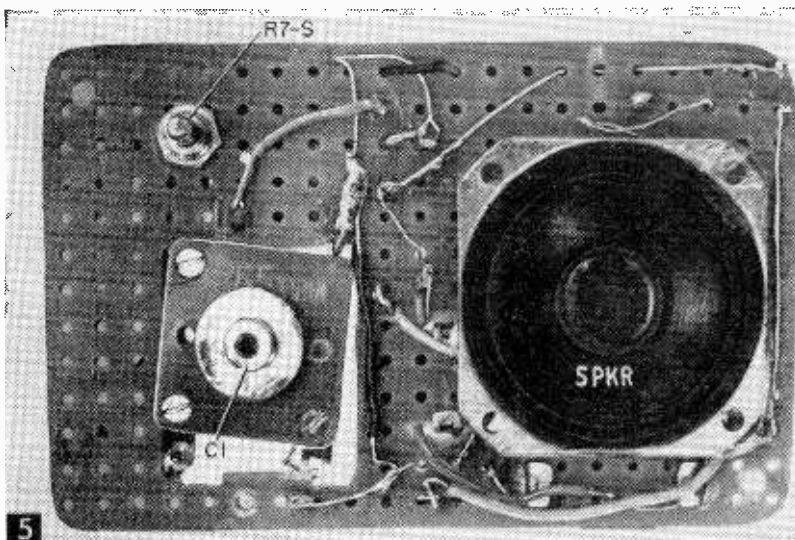
control shaft and ream to size, or simply drill using a $\frac{3}{8}$ -in bit. When cutting and drilling is completed, dress the edges of the board and the cutouts with a file.

Use Fig. 3 as a guide for mounting parts. Mount volume control-switch R7-S and transformers L4 and L5 first. The transformers are mounted by bending their mounting lugs down 90° so they can be inserted in the circuit board slits. With the transformer mounting lugs inserted in the circuit board slits, press the transformer against the board, and bend the lugs over on the front of the circuit board. Duco cement placed between the base



4

CIRCUIT BOARD LAYOUT—BACK VIEW



Front view of circuit board.

of the transformers and the circuit board will stabilize the mounting and may bail you out if you break a transformer lug in the mounting process.

Mount L2 and L3 by fastening with Duco cement, but go easy on the cement because you may have to loosen and re-orient these coils. The remaining components are mounted in the process of wiring the circuit board.

Desig.	Description
	1/2 watt carbon resistors, 10% tolerance
R6	100 ohms
R2	470 ohms
R5	2.7K
R1	10K
R4, R8	15K
R3	47K
R7-S	10K miniature volume control with switch (Lafayette VC-28)
C6	100 mmf. Mini Kap ceramic capacitor (Lafayette DM-101)
C2, C4, C8	.01 mfd. 75v. subminiature capacitor (Lafayette C-612)
C9	1 mfd., 6v. subminiature electrolytic capacitor (Lafayette P6-1)
C3, C7	30 mfd., 6v. miniature electrolytic capacitor (Lafayette CF-104)
C5	100 mfd., 15v. miniature electrolytic capacitor (Lafayette CF-126)
C1	365 mmf. miniature tuning capacitor (Lafayette MS-445, includes tuning dial)
L1	flat ferrite antenna loop coil (Miller 2004)
L4	10,000 ohm to 2,000 ohm subminiature transformer (Lafayette TR-98)
L5	2,000 ohm to 10 ohm miniature output transformer (Lafayette TR-93)
L2, L3	Coils L2 and L3 are jumble-wound with Belden 8817 litz wire on 1/4" dia. ferrite cores (saw or break off of Lafayette MS-331). Wind 25' of wire on a 3/4" length of core for L2, and 15' on 1/2" of core for L3
T1	2N412 transistor (RCA)
T2	2N321 transistor (GE)
D	1N60 diode (Raytheon)
SPKR	1 1/2" PM loudspeaker (Lafayette SK-61)
B	9v. transistor radio battery (Mallory TR-146R) volume control knob (Lafayette MS-185) miniature perforated board (Lafayette MS-305) case (Lafayette MS-424 ivory or MS-427 maroon)

All components for this project are available from Lafayette Radio, Dept. SM, 165-08 Liberty Avenue, Jamaica 33, New York.

The circuit board is wired by inserting component pig-tails through the perforations and making connections on the front of the board. Where several component pig-tails form a common junction, the pig-tails may be inserted in a common perforation. The connection routes on the front of the board are short enough in most cases to permit direct connection with component pig-tails.

Solder the connections as you go along. Use a hot clean iron and rosin core solder. Solder quickly. Miniature components, particularly transistors and diodes, may be damaged by soldering iron heat applied for too long a time. Be cautious about electrolytic capacitor and battery polarities in making connections.

Mount T2 first and then wire C3, C7, R5, R6, R4, and C5 into the circuit. Then wire R3, R1 and C2. The connection of C4, L2 and L3 follows. Don't cut L2 and L3 leads too short; you may have to reverse connections later.

Next, mount diode D and connect C6, R7, R8 and C9 into the circuit. Mount T1 and complete connections to L2. Mount and connect R2 and C3.

Now recheck the wiring for correctness and examine the circuit board for poor connections and shorts. Then attach leads for C1 and for battery connections. Solder battery connection lugs on the battery leads, connect C1, and connect the L5 secondary leads to the loudspeaker voice coil lugs. Connect L1 into the circuit.

Whether it is best to place the Little Red Hot in the case or leave it out for test, adjustment and debugging is a tossup. If you don't place it in the case, care must be exercised to prevent shorting of components, and the tuning capacitor (C1) is difficult to adjust. If you place the receiver in the case, you'll probably have to pull it out if there are difficulties.

To test, adjust, and debug, connect the battery to the set (if it's available, use another less expensive 9-v battery—six series-connected penlite or flashlight cells are fine—for first tests), turn the volume on, and tune for a station. If the set is insensitive over the entire broadcast band, interchange the A and D

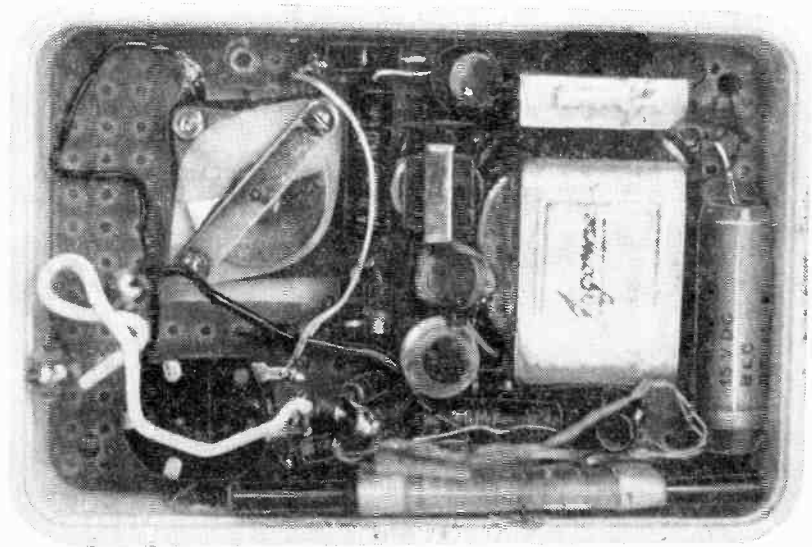
lead connections of L2-L3. Sensitivity should increase as L1 is moved toward the position approaching the "in-case" mounting relationship of L1 and L2-L3.

If the set is insensitive at one end of the band only, interchange L2's AB connections or L3's CD connections. Try the possible combinations till you arrive at the best results.

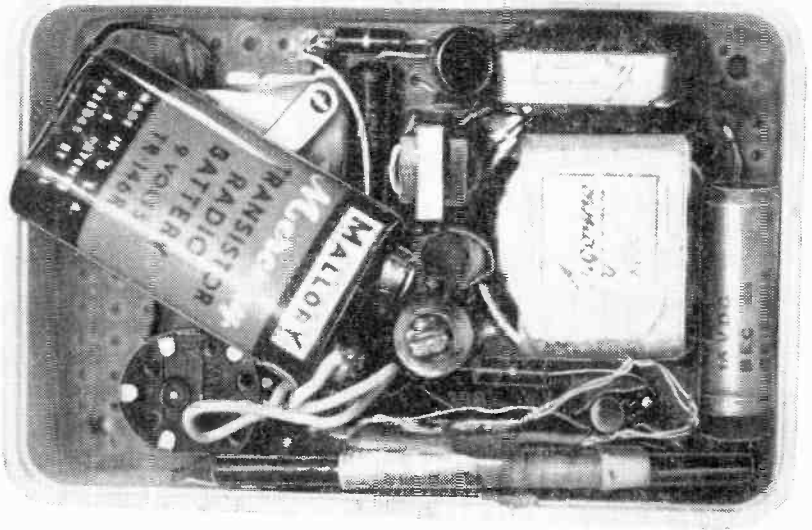
Next mount the set in the case and try it again. Slide L1 back and forth along the edge of the case till you get best sensitivity. It may be possible to reach a point where the set will oscillate (squeal). Simply change the position of L1 till the squealing stops.

The position of C6 relative to L1 influences sensitivity. The sensitivity of the set may also be increased by tilting L2 and L3 slightly from their vertical orientation relative to the circuit board if oscillations did not occur during the previous adjustment of the position of L1. Experiment with tilting to right and left with the set in the case. When optimum position is found, fasten L2-L3 in place permanently with cement, and fasten L1 against the side of the case with cellophane tape.

The circuit board assembly is held in the case with two machine screws. Pressure between the circuit board and the case holds the speaker in place. Position the speaker so that maximum cone area is visible through the cabinet speaker openings. Fasten C1 directly to the case with the two small machine screws provided with the capacitor for this purpose. Install the dial provided with the capacitor and fasten the volume control knob. Position the battery so the back of the case



6 A



B

Back view of entire assembly without (A) and with (B) battery.

can be snapped on. Insulate the battery lugs and any portion of the battery outer metal shell that might touch connections with cellophane tape.

The Little Red Hot will give you reasonable performance up to 10 or 15 miles from a broadcast station. It's extremely directive. A short (1 to 3 ft.) antenna lead connected to the junction of the C1 stator and the top of L1 will reduce this directivity.

Removing Enamel Wire Insulation

• To remove enamel insulation on magnet and hook-up wire quickly and cleanly, wrap a piece of sandpaper around the wire and give a twisting, rotary motion.—E. L. BURNER.

Underwater Intercom

This unusual intercom provides constant contact between boat and diver, amplifying your voice through a loudspeaker

By C. L. HENRY

DESIGNED for rough boat service or dockside operation, the amplifier of this intercom is transistorized for battery economy. Its simple circuitry and reliable operation make it ideal for Scuba divers, or even "hard hat" professionals.

The diver wears a throat mike and earphone (Figs. 1, 3). When he talks, his voice is amplified to speaker volume and can be heard by anyone within earshot on the boat or dock above. Unlike an ordinary telephone set, there is no push button or ringer, and the diver's hands are always free. Also, a special sidetone circuit enables him to hear his voice in the earphone and know that the surface is also hearing him.

At the "upstairs" end (Fig. 2) operation is ultra-simple, with a push-to-talk switch and

loudspeaker volume control as the only live controls. A separate volume control, R12, (Fig. 5B) is equipped with a Millen shaft lock so that the volume fed to the diver's earphone cannot be changed accidentally. Also, an auxiliary audio output jack enables you to connect in a remote speaker. One diver reported that this interphone, which uses less than \$20 worth of parts, paid for itself quickly in helping to salvage lost articles. It's fine for treasure hunting or coaching Scuba students and since the throat mike would enable it to work well in very noisy locations, it might have many uses on dry land as well.

Power for the microphone circuit is supplied by two D-size flashlight cells mounted inside the case. The 300-ma. amplifier requires an outside battery. You can use a lantern size dry cell, which will give you up to 15 hours of continuous operation, equal to many days of diving. Or, using the 6-12 volt selector switch, you can tap any convenient storage battery.

Construction. Begin by marking, drilling and punching all of the holes in the case, the front and back covers, Fig. 4 and in the internal chassis box (Fig. 6). Even though the case itself will be sealed later by rubber gaskets, it is necessary for salt water operation especially, to protect all metal surfaces against accidental wetting.

Coat the inside of the case and the surfaces of parts that you can't reach later with several layers of acrylic or silicone resin spray, which both insulates and provides corrosion resistance. Completely waterproof the speaker with 4 to 6 heavy coats of the plastic spray.

Wearing a waterproof earphone and throat mike, the diver is always in instant contact with the surface. The phone must be worn loosely to avoid unequalized ear pressure which could rupture the eardrum.





The diver's voice, at loudspeaker volume can be clearly heard on boat or dock. Man on surface presses push-to-talk button on top of amplifier case.

2

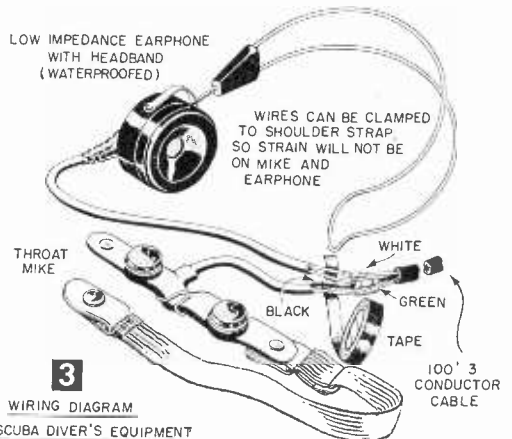
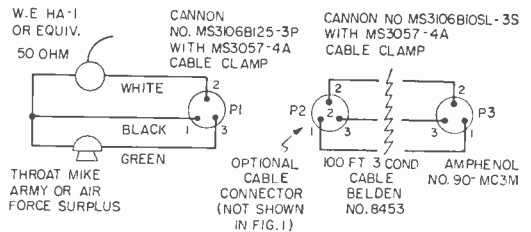
Next mount all the parts as shown in Figs. 5A, 5B, using lock washers or lock nuts. The transistors are located on the cover of a small 4 x 2 x 2 3/4-in. chassis box (Fig. 6) which in turn is mounted on the inside of the back panel of the amplifier case. Bolt the 2N155 transistor directly to the box, after scraping the box paint off to provide tight contact and effective heat dissipation.

Transformer T1 is mounted inside the chassis box along with the resistors and capacitors in the transistor circuitry. Positioning of parts is not critical, but keep the input and output circuits as far apart as possible, since feedback or whistling may occur if they are close enough to couple. Wire the transistor circuit (Fig. 5C) and then complete the rest of the amplifier, using color coded hook-up wire.

Now check your wiring carefully against the schematic. If the transistors are wired incorrectly, they will be ruined instantly when power is applied to the circuit. Complete construction by lacing the wiring carefully, and then coat the entire assembly (switch contacts protected temporarily with tape) with the waterproofing sprays mentioned earlier. Cut strips of rubber and cement them to the case to make a watertight gasket for the front and back panels.

How It Works. In the amplifier, two transistors are used to obtain a full 2-watt output with a carbon mike input. Mike power is supplied by two flashlight cells mounted inside the amplifier case. They will provide months of use. The diver's carbon mike is connected through a transformer, T1, and volume control R4 to the input of the first transistor, TR1, asylvania type 2N35. An NPN type, this transistor is operated in a common emitter type of circuit. Resistors R5 and R6 determine the bias or operating point of the transistor, and it requires about 4 ma collector current. The collector or output lead of the 2N35 is connected to the transformer T2. The winding of T2 is bypassed with C5 to correct the high frequency response of the amplifier. The secondary of T2 connects to the second transistor, TR2, a CBS type 2N155. Output of TR2 feeds to transformer T3 where the collector current

flows through the primary of T3 to the earphone. The primary of T3 is connected to the secondary of T2 through a capacitor C6. The primary of T3 is connected to the secondary of T2 through a capacitor C6. The primary of T3 is connected to the secondary of T2 through a capacitor C6.



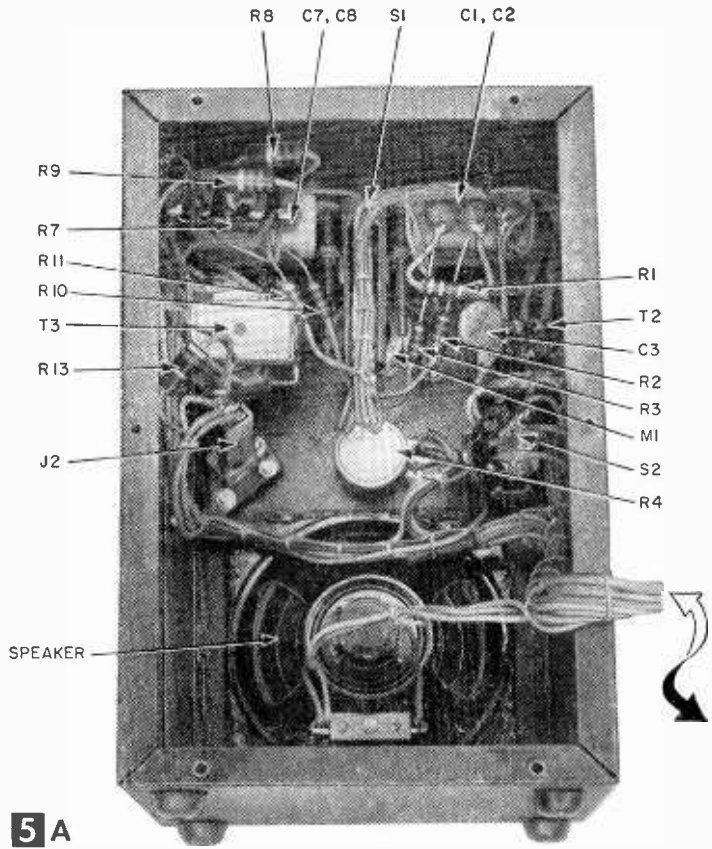
3 WIRING DIAGRAM SCUBA DIVER'S EQUIPMENT

is about 350 ma.

The 2N155 output circuit is unusual: in effect, it is a common emitter-type amplifier, with two feedback windings on T3 canceling each other to allow the 2N155 collector to be connected directly to chassis in order to provide an effective heat sink.

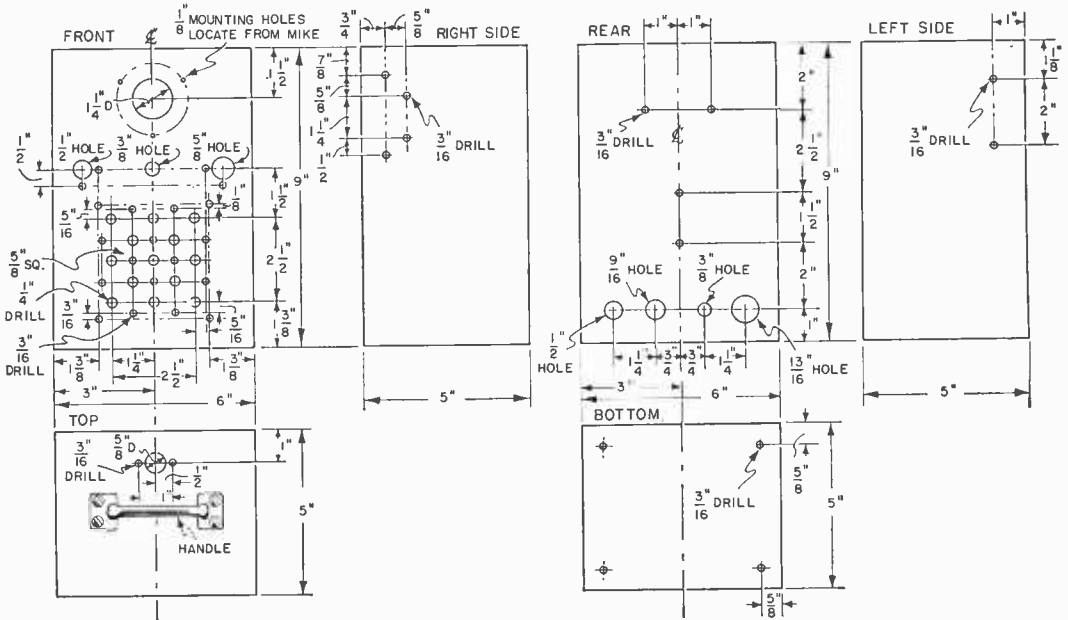
The T3 secondary is connected to the push-to-talk switch, and in normal position, through this switch to the loud-speaker mounted in the case. When the push-to-talk switch is pressed, the output of the amplifier output connects through the remote volume control, R12, to the diver's ear-phone. Capacitor C8 supplies a sidetone circuit which allows the diver to hear himself talk. When he can't hear himself, it warns him that there is no communication to the surface. If you want more sidetone, increase the size of this capacitor.

Water Proofing Mike and Phone. The amplifier Mike serves either the scuba or skin diver, or the hard-hat suit diving rig. Since the scuba diver must submerge with a tightly-fitting mouthpiece, speech in the ordinary manner would be impossible; hence a surplus throat

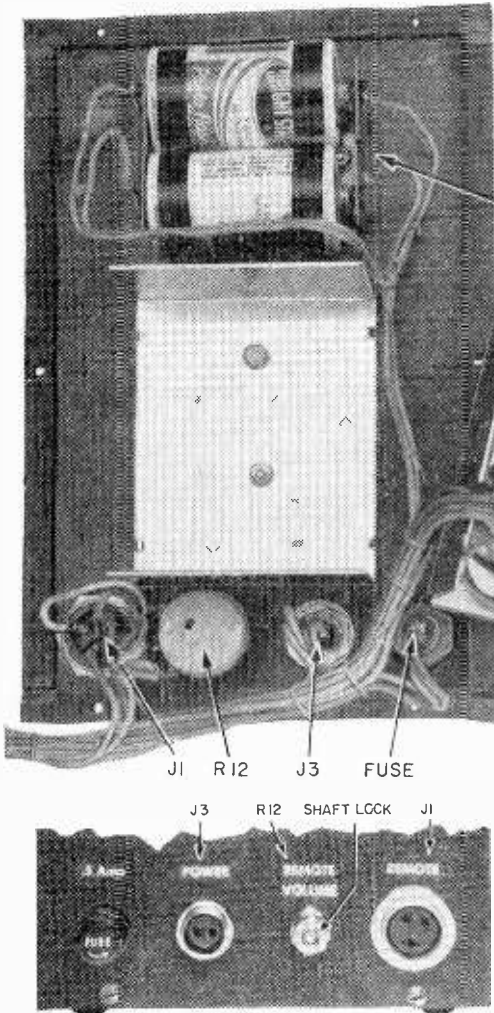


5A

Wiring inside the case is not crowded. Be sure to separate the input from the output circuit wiring to prevent audio howl. The speaker must be coated heavily with waterproofing spray.



Transistors are mounted on the top of the small circuit box cover. Make waterproofing gaskets for both front and back covers of 1/2-in. rubber strip.



5 B

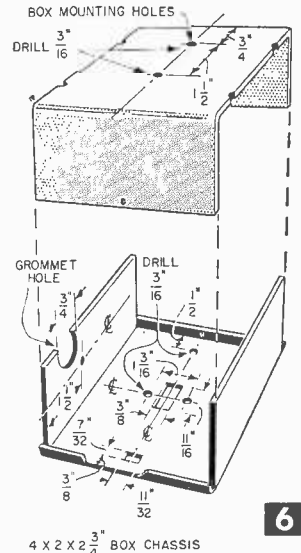
BATTERY HOLDER

R5 TR2 R6 T1

TR1 C5 C4 C6

RUBBER SEAL

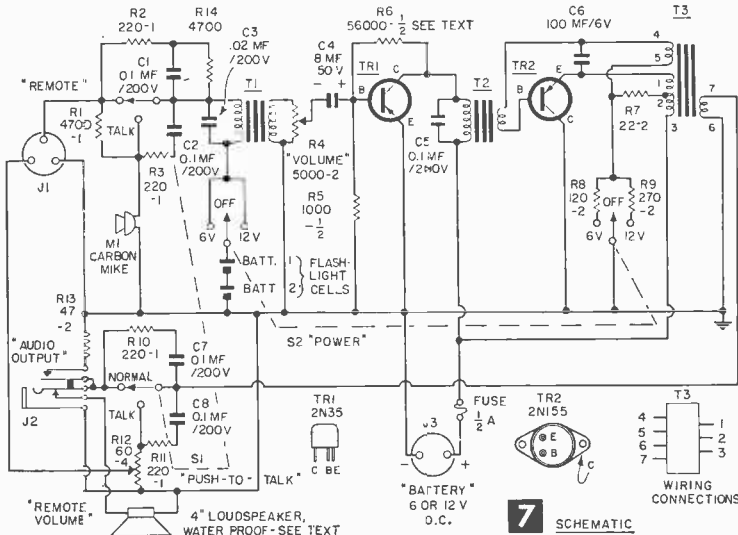
REAR VIEW



4 X 2 X 2 3/4" BOX CHASSIS

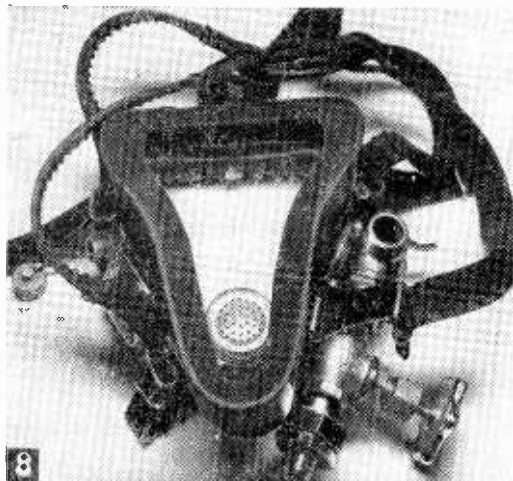
mike is used. Sound is picked up via throat contact and while the results are not hi-fi, a little practice makes simple words understandable. Seal the edge of the throat mike with *Scotchkote* (or equivalent) Electrical Coating.

Select an earphone of low impedance for greatest volume. Remove the diaphragm, spray it and the wiring, and then seal the entire assembly with plastic electrical tape covered with *Scotchkote*. For extreme depths, you may want to do some experimenting with the alternate method of drilling holes in the earphone case, and allowing water to enter and equalize pressure. Underwater, the earphone is almost as clear sounding as on dry land, since the short distance to the ear is not enough to muffle the sound. You can use an earphone clip, or attach both throat mike and earphone to an elastic headboard. One important caution: *When in the water, do not fit the head- phone tightly over the ear since pressure variations in descent can rupture your eardrum.*

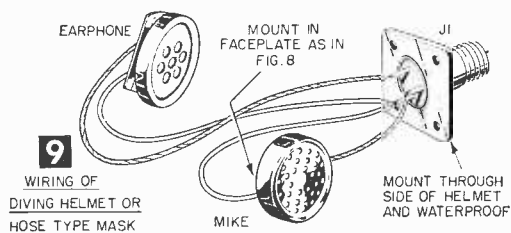
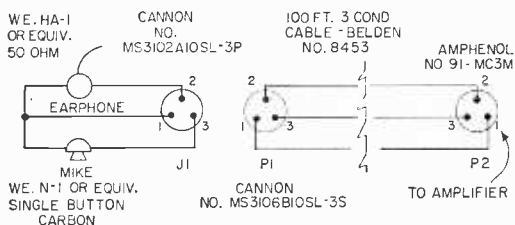


When in the water, do not fit the head- phone tightly over the ear since pressure variations in descent can rupture your eardrum.

Fig. 9 details the in-



This type of face mask connects to an air hose. Since the diver has no mouthpiece, the microphone can be installed near the bottom of the plastic faceplate.



WIRING OF DIVING HELMET OR HOSE TYPE MASK

stallation of a single button type microphone in the faceplate of the hard-hat diving rig. Waterproof the microphone, and install the earphone, also waterproofed, in the head covering of the suit. Both mike and phones are connected to the 3-wire cable with a surplus AN waterproof connector. Tape the cable directly to the air hose.

Connect the cable to the skin diver's mike and earphone directly—taping and covering the wire joint with Scotchkote. For extensive Scuba diving and exploration, a wire reel and about 150-feet of the 3-wire cable can be arranged for easy operation. Lines to several divers can be connected to the amplifier, simply by wiring in parallel.

If the Scuba diver needs complete freedom of movement, he can shed his phone, mike and cable, and tie it to an underwater marker

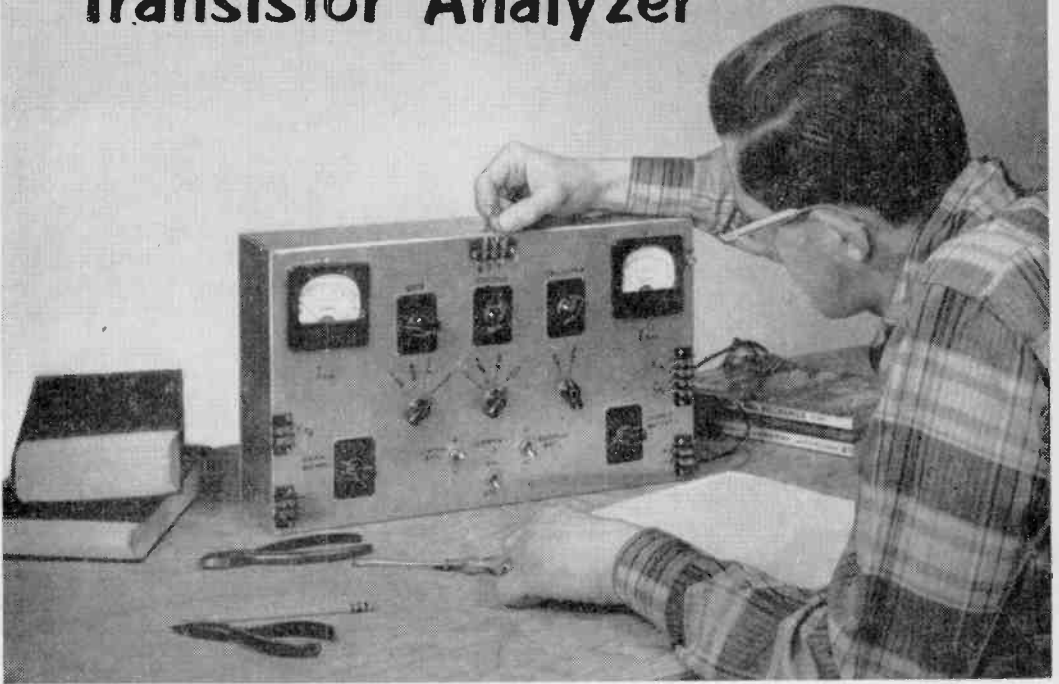
MATERIALS LIST—UNDERWATER TELEPHONE

No. Req'd	Size and Description
AMPLIFIER	
1	R1—4.7K, 1 watt, 10% carbon resistor
4	R2, R3, R10, R11—220 ohm, 1 watt, 10% carbon resistors
1	R4—5K, 2 watt, variable resistor (volume control) Ohmite type AB
1	R5—1K, 1/2 watt, 10% carbon resistor
1	R6—56K, 0 watt, 10% carbon resistor
1	R7—22 ohm, 2 watt, 10% carbon resistor
1	R8—120 ohm, 2 watt, 10% carbon resistor
1	R9—270 ohm, 2 watt, 10% carbon resistor
1	R12—60 ohm, 4 watt, variable resistor (remote volume control) IRC type 60
1	R13—47 ohm, 2 watt, 10% carbon resistor
1	R14—4.7K, 1 watt, 10% carbon resistor
5	C1, C2, C5, C7, C8—0.1 mfd., 200-volt paper capacitors
1	C3—0.02 mfd., 200-volt paper capacitor
1	C4—8 mfd., 50-volt electrolytic capacitor
1	C6—100 mfd., 6-volt capacitor
1	S1—Televex type 16006L, push-to-talk switch (Alternate Switchcraft 11006)
1	S2—Arrow-Hart and Hegeman bat handle toggle, type 82024-D
1	T1—transformer, Argonne AR-123
1	T2—transformer, Argonne AR-105
1	T3 transformer, Motorola type 25C536761 only (auto radio replacement) available Motorola parts distributors
1	TR1—Sylvania type 2N35 transistor, NPN
1	TR2—CBS type 2N155 transistor, PNP
1	M1—carbon microphone, Western Electric type F-1 or equiv.* (Surplus item available Columbia Electronics; 2251 W. Washington Blvd., Los Angeles, Calif.)
1	speaker, 4 in. PM type, cone speaker
HARDWARE	
1	J1—connector, 3 conductor, Amphenol type 91-PC3F
1	J2—telephone jack, Mallory type XP4B
1	J3—connector, 2 conductor, Amphenol type 80-PC2F
1	9 x 6 x 5" steel carrying case, Bud #CC-1095, black wrinkle finish, with handle
1	4 x 2 x 2 3/4" box chassis, LMB Model 102
1	fuse retainer, Buss type 342001
1	shaft lock for R12, Mallory type 12A1496
1	socket, transistor
1	battery holder, Keystone type
Misc.	plastic spray, rubber feet, mounting screws, nuts, lockwashers, decals
Unless indicated otherwise, all parts are available from Lafayette Electronics, 165-58 Liberty Ave., Jamaica 33, N.Y.	
PARTS FOR SCUBA OR SKIN DIVER	
1	microphone, throat type, Army or Air Force surplus, available from Roscoe Ward Bargain Bazaar, 3831 Hixson Pike, Chattanooga 5, Tenn.
1	headphone, 11 ohm, low impedance type, Western Electric HA1 or equal
1	P1—Cannon MS3106B12S-3P, with Cannon MS3057-4A cable clamp (optional)
1	P2—Cannon MS3106B10SL-3S, with MS3057-4A cable clamp (optional)
1	P3—Amphenol 91-MC3M
100 ft	3-conductor cable, rubber covered Belden 8453 with spool, or windup reel
PARTS FOR SUIT DIVER'S FACE MASK	
1	microphone—Western Electric type N1, single button carbon, 50 ohm*
1	headphone, Western Electric type HA1, or equal
1	J1—Amphenol MS3102A10SL-3P
1	P1—Amphenol MS3106B10SL-3S, with Cannon MS3057-4A cable clamp
1	P2—Amphenol 91-MC3M
100 ft	3-conductor cable, rubber-covered Belden 8453
* Telephone parts are also available from Telephone Repair and Supply Company, 1760 Lunt Avenue, Chicago 26, Ill.	

anchored in position. Brightly colored, it will be easy to find for use at any time.

Such a completed underwater intercom will add an immense safety factor for novice divers.

Transistor Analyzer



It's fun to build gadgets, but the serious experimenter soon realizes that this is but a preliminary to real electronic understanding. To master any branch of science, one must learn to take, graph, and analyze quantitative data. With this convenient transistor characteristics analyzer you do just that.

By C. F. ROCKEY

BLOCK diagram (Fig. 2) and schematic (Fig. 3) show how this transistor analyzer works. A relatively low-voltage dc source provides a "signal" which may be applied in either polarity to either the base or emitter circuit of the transistor under test. Likewise, a variable supply dc source may be connected at will to any electrode. Appropriate current-measuring instruments are associated with each source, and either positive or negative terminals of either source may be made the common point by grounding switches. All significant points of the circuit are brought out to terminal screws for convenient reading of all important circuit potentials. Thus voltage/current relationships in any parts of a three-terminal semiconductor element may be conveniently adjusted and measured. Two-terminal crystal diodes may also be studied by connecting to the two appropriate terminals.

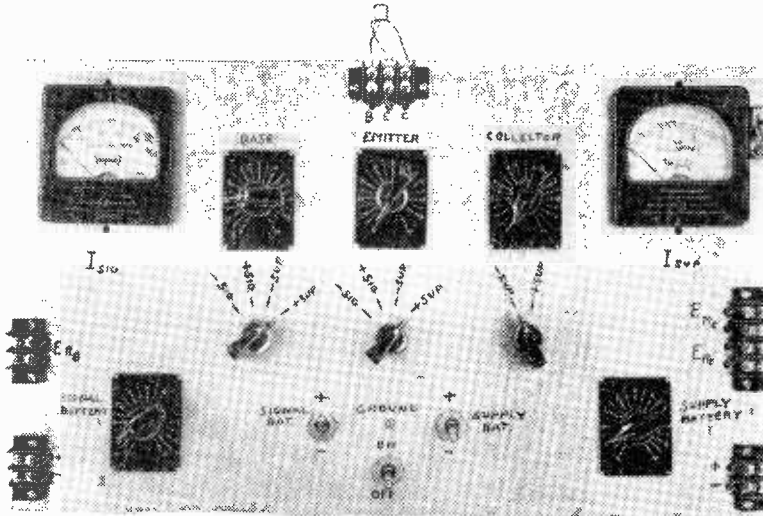
You can build this device easily in a couple of evenings. Total cost to build will be approximately \$50 (including batteries and at least one experimenter's transistor for dem-

onstration). You will also need a volt-ohm-milliammeter of the ordinary radio-servicing sort.

Constructing the Unit. Begin by drilling the major chassis holes (see Fig. 4). Any linear-taper, radio-replacement potentiometers of the right value may be used. They need not be equipped with switches. Multi-element function switches were used, even though so few positions were utilized, because these switches cost no more than those with fewer positions, and the manufacturer provides an adjustable stop so that the user may readily select as many positions as he needs; also, the additional switch positions provide for expansion as the transistor art advances. You may use appropriate switches you have on hand, but make sure that they are of the non-shorting type.

After drilling the major holes, drill chassis and mount the Cinch-Jones terminal strips using 6-32 steel machine screws and nuts. Then fasten into place each of the potentiometers and switches.

Solder each connection carefully with rosin-core solder, avoiding short-circuits between lugs or to the chassis. The exact order of the wiring is not critical; just be sure you



1 This analyzer provides maximum flexibility for quantitatively studying the dc and low-frequency interelectrode relationships of transistors.

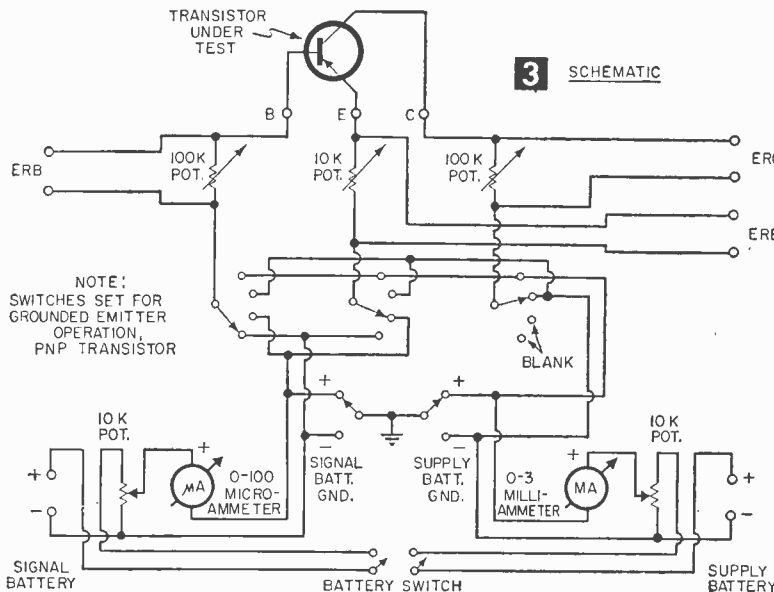
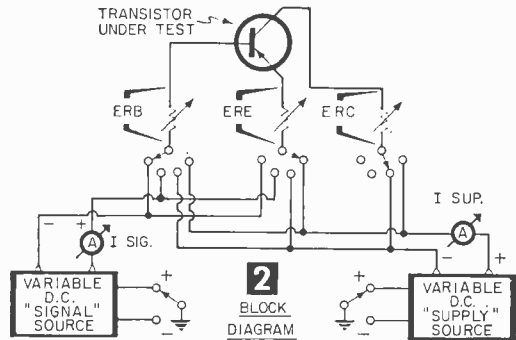
follow an orderly procedure, and check each step carefully.

Finally, install and connect the meters. Be sure to observe the little plus-sign, and polarize these correctly. When the meters have been installed, and the wiring checked, clean off the top of the chassis with carbon tetrachloride, or other grease solvent and mark the terminals and switch positions with a steel pen, using draftsman's ink. When the markings are complete and dry, give the chassis a coat of clear, water-white spray lacquer.

Using the Transistor Analyzer. Prepare the instrument for use by connecting a single 1.5-v flashlight battery to Signal Battery terminals, a 4.5- to 6-v battery to Supply Bat-

tery connections. Be sure to observe correct polarity. I recommend a 6-v "lantern battery," available at most large hardware stores, for the supply battery. Provide connections to it by soldering wires to the spring terminals usually used. Make sure the battery switch is in off position.

Next, connect the leads of the transistor you wish to examine to the terminals provided. Be sure to first ascertain whether it is a PNP or an NPN unit; incorrect information here will cause confusion in the measurements, and *may* re-



sult in transistor or meter damage.

Perhaps the most significant first determination that can be made is that of the grounded-emitter *current transfer characteristic*. This property clearly illustrates the control impedance property of the transistor, and thus its ability to amplify. In this measurement we hold the emitter-collector voltage constant, and vary the base current. The corresponding variations in collector current are then observed and tabulated.

Before turning-on the battery switch, set

MATERIALS LIST—TRANSISTOR ANALYZER

No. Req'd	Size and Description
1	aluminum chassis 4 x 10 x 17"
1	0 to 100 microammeter, Triplett Model 327
1	0 to 3 milliammeter, Triplett Model 327
1	DPST toggle switch
2	SPDT toggle switches
3	10K, wire-wound linear taper potentiometers, Mallory
2	100K, linear taper potentiometers, Mallory
3	non-shorting single deck rotary switches, Mallory, Number 1311-L
1	3 terminal, Cinch-Jones terminal strip
1	4 terminal, Cinch-Jones terminal strip
3	2 terminal, Cinch-Jones terminal strip
5	270° dial plates, Croname
8	bar knobs
1	Fahnestock clip
	6-32 machine screws, 1/2" long, steel hex nuts, steel for above, plastic insulated hookup wire, rosin core solder
Also needed for measurements, if not already on hand:	
1	1.5 v flashlight cell
1	6 v lantern battery
1	volt-ohm-milliammeter, or vacuum-tube volt-ohmmeter
1	experimenter's junction transistor

up the other controls as follows: For an NPN transistor (grounded emitter connection): Base selector switch, + sig; Emitter selector switch, - sup; Collector selector switch, + sup; Signal battery grounding switch, - ground; supply bat grounding switch, - ground.

For a PNP transistor: Base selector switch, - sig; Emitter selector switch, + sup; Collector selector switch, - sup; Sig bat grounding switch, + ground; Sup bat grounding switch, + ground.

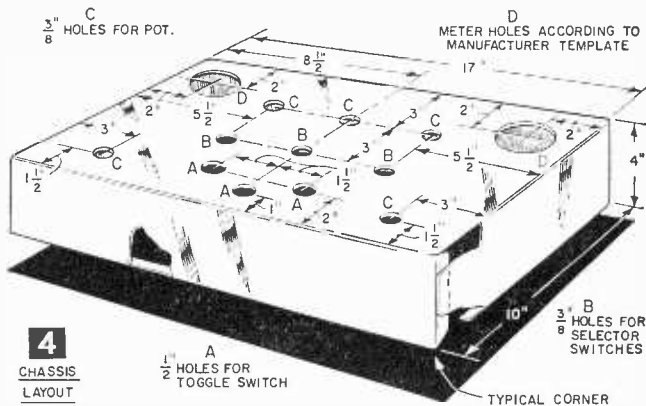
In either case, the potentiometers in series with each element of the transistor should be set to zero resistance position. Set both of the battery potentiometers to zero voltage position.

Now, using the 10-v (or similarly-scaled) range, connect a radio-serviceman's VOM or

VTVM from the collector to ground. Connection to the collector may be reached directly at the upper terminal of the pair marked ERC, and ground connection may be made to the Fahnestock clip.

Turn on the battery switch and adjust the supply battery potentiometer to 1.5 v from collector to ground. This may cause the Isig microammeter to read backwards. If it does, slowly advance the Signal battery potentiometer until it reads at zero. (This "back current" is due to normal interaction within the transistor.) After this change has been made you will probably have to reset the Supply battery pot to the correct voltage. (The input and output circuits of a transistor are interrelated, unlike those of a vacuum-tube at low frequencies which are isolated.)

With the collector voltage at 1.5 v and the base current (Isig) at zero, observe and tab-



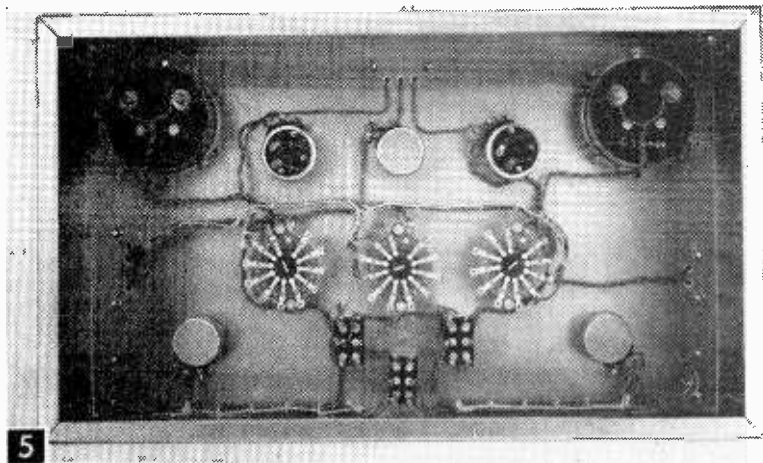
4 CHASSIS LAYOUT

ulate the collector current, which will be read from Isup, the 0-3 milliammeter. Now, keeping the collector voltage at 1.5 v. by adjustment of the Supply battery potentiometer, advance the Signal battery potentiometer to

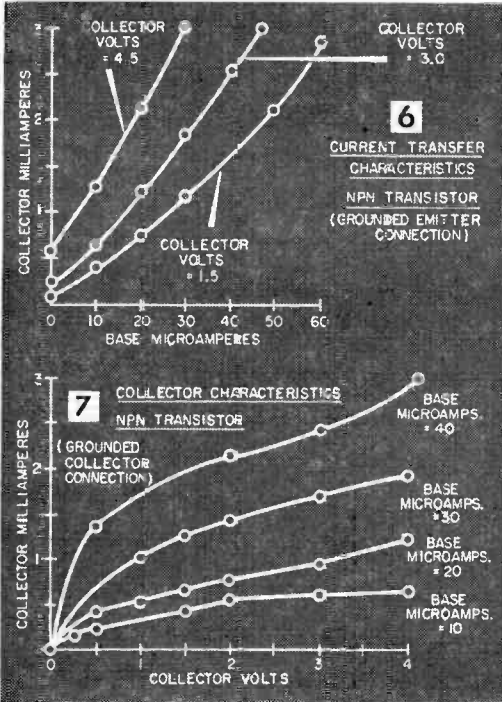
make the base current 5 microamperes. Jockey the two battery pots as necessary to achieve this condition. Again, observe and tabulate the collector current, Isup. Repeat, in 5 - microampere (base current) steps until the maximum collector current of 3 milliamperes is reached.

Be sure that the voltage from collector to ground remains at 1.5 v at the time each reading is taken.

When all of this data has been taken, plot it



5 Under-chassis view of completed analyzer.



in graphic form. It is customary to plot the independent variable, in this instance the base current, along the horizontal axis (abscissa) and the dependent variable, the collector current, along the vertical (ordinate) axis.

Figure 6 represents a set of curves taken in this manner using a popular brand of experimenter's NPN junction transistor. When completed, such a graph may give rise to a number of significant conclusions. One of these might be that since with an E_c of 4.5 v an approximate base current change of 12 microamperes gives rise to a collector current change of one millipere, or 1000 microamperes, this transistor provides a current amplification of about 80 times. Is there any doubt as to why such a transistor is useful in practical electronics?

Another useful transistor relationship is that between the collector current and the collector voltage, when the base current is kept constant (grounded collector connection). A family of such curves run by the author (using the same NPN unit) is shown in Fig. 7. The identical switch setup, as used for the transfer curves is used for this investigation. Such a family of curves is of first importance to an engineer, who must match a given transistor to a given load resistance, in a practical design problem.

With increasing experience in the use of this analyzer, a student may plan and execute many interesting measurements and experiments. Curves resulting from several such

TABLE A—SWITCH SETTINGS FOR TRANSISTOR CIRCUIT CONFIGURATIONS:

COMMON EMITTER:	NPN	PNP
Base Selector Switch	+sig	-sig
Emitter Selector Switch	-sup	+sup
Collector Selector Switch	+sup	-sup
Signal Battery Grounding	-ground	+ground
Supply Battery Grounding	-ground	+ground

Isig reads base current, Isup reads collector current. Load resistance provided by Collector series potentiometer.

COMMON BASE:	NPN	PNP
Base Selector Switch	+sig	-sig
Emitter Selector Switch	-sig	+sig
Collector Selector Switch	+sup	-sup
Signal Battery Grounding	+ground	-ground
Supply Battery Grounding	-ground	+ground

Isig reads emitter current, Isup reads collector current. Load resistance provided by Collector series potentiometer.

COMMON COLLECTOR:
Same as for common emitter, except that the load resistance is provided by the potentiometer in series with the Emitter.

investigations, as made by the writer, are shown in Figs. 8, 9, and 10. All of the usual transistor circuit configurations can be investigated by merely selecting the appropriate switch settings (see Table A).

Due to the non-uniformity of experimenter's-type transistors, you should not expect your measurements to agree with the author's. Corresponding curves should be of approximately the same shape, however.

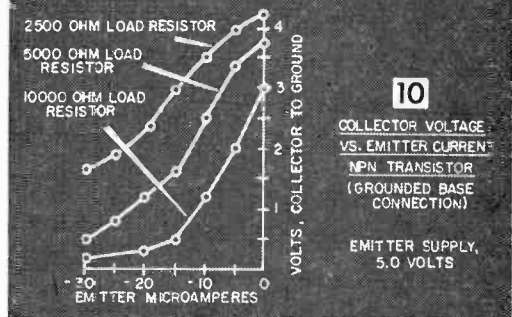
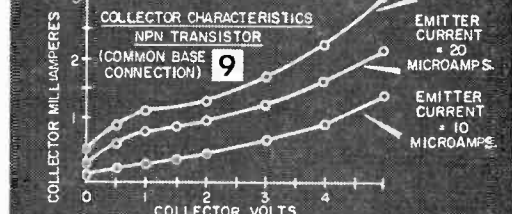
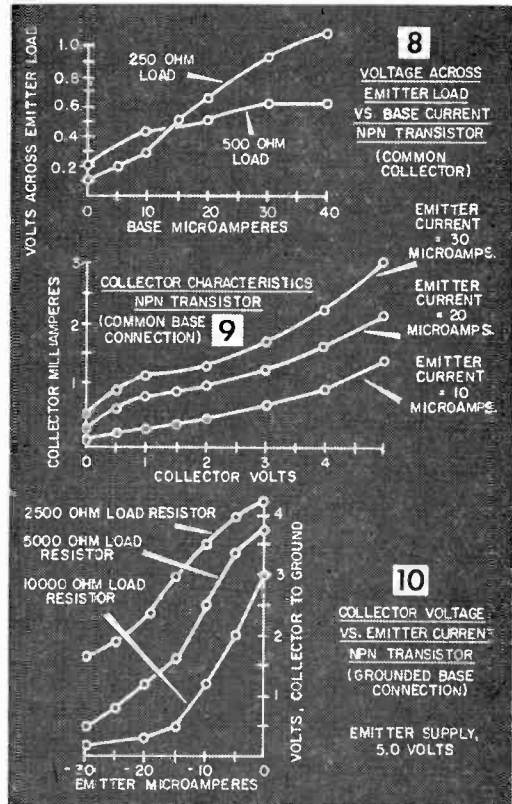
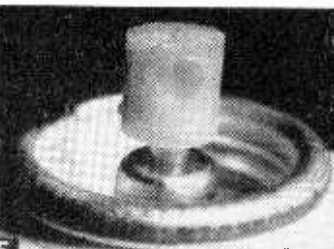
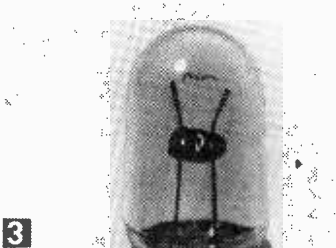
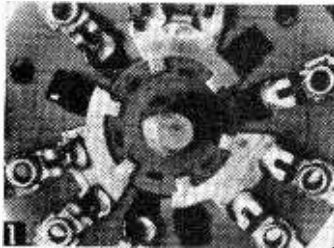


Photo Quiz

Turn a camera loose in a radio-electronic hobbyist's shop and it will come up with some odd-looking pictures. Do you have a good "eye" for solving photo quizzes? Write in the names of the objects in the spaces provided, then check your answers against those on page 122.

1. _____ 3. _____ 5. _____
 2. _____ 4. _____ 6. _____



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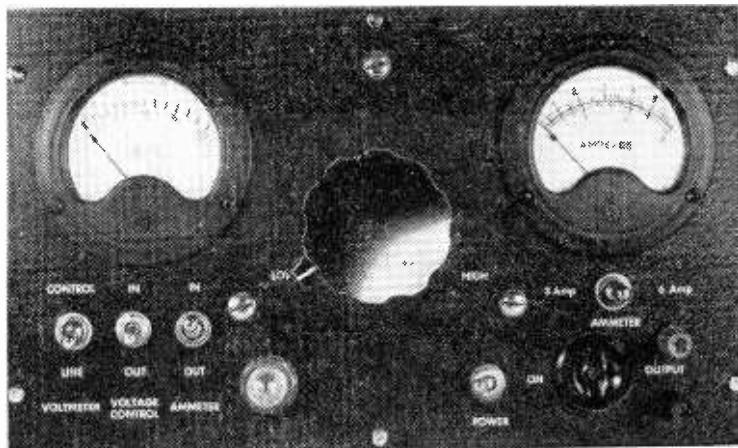
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1 Panel view of unit, showing parts placement, with voltage control knob in center.

AC Power Panel

Simple unit checks power input and furnishes various ac voltages

By W. F. GEPHART

Problem: A TV or radio set that goes bad only between 5:30 and 7:00 PM, or on rainy Monday mornings.

Problem: An electric motor that heats up excessively, even though the shaft turns freely.

Problem: Can a small radio output transformer be used as a step-down voltage transformer for a given load?

The solution to all of these problems lies in the metered variable-voltage power unit shown in Fig. 1. By reducing the normal line voltage to the TV set and radio (as happens when electric stoves create a peak load at dinner time, or when electric clothes dryers are being used on rainy Mondays), adjustments can be made to the set to provide proper operation at lower line voltages. By checking the current being drawn by the motor, evidence of shorted windings can be found. And by checking the current into the transformer as the voltage is increased, and comparing with its rating, its suitability for a given job can be determined.

There are many other uses for a high-powered, metered, variable ac power source in servicing work, appliance repair, and gen-

eral experimental work. By using surplus or imported meters, and adapting the common ac voltmeter to the more scarce ac ammeter, costs can be kept down to a reasonable figure. Excluding the cabinet, and by using 2½-in. meters, the unit shown can be built with surplus parts for less than \$20, as compared to nearly \$40 if built with new parts.

Basically, the unit consists of a variable voltage auto-transformer, an ac voltmeter and ac ammeter. Switches transfer the voltmeter connections, cut the ammeter and auto-transformer in and out of the circuit and (in the unit shown) provide two ammeter ranges. Figure 1 and the schematic (Fig. 2) also show a neon pilot light

MATERIALS LIST—POWER PANEL

(Applicable to unit shown in Fig. 1)

Desig.	Description
R1	56,000 ohms, ½ watt (not required if included in PL)
R2	27,000 ohms, ½ watt (see text)
T1	7.5 amp variable auto-transformer (Superior Electric 116U, Standard Electric 500BU or T51U, Ohmite VT-8, or surplus unit of desired ampere capacity)
T2	"Current Transformer" (see text)
S1	DPST toggle (see text)
S2	DPDT toggle (see text)
S3, S4	SPDT toggle, 3 amp
S5	SPST toggle, 3 amp
PL	neon pilot light holder (Dialco 95408X or equivalent)
M1	0-150 volt a-c meter
M2	low-range a-c voltmeter (see text)
S01	female panel receptacle (Amphenol 61-F1)
	6 x 7 x 12" cabinet (Bud CU-1124), binding posts (optional), plastic scraps, miscellaneous hardware

Some companies handling surplus material where auto-transformers and meters might be secured:

Advance Electronics, 6 West Broadway, New York 7, N. Y.
 Barry Electronics Corp., 512 Broadway, New York 12, N. Y.
 Columbia Electronics, 2251 W. Washington Blvd., Los Angeles 18, Calif.
 G & G Radio Supply, 51 Vesey Street, New York 7, N. Y.
 Hi-Mu Electronics, 133 Hamilton St., New Haven, Conn.
 Peak Electronics, 66 W. Broadway, New York 7, N. Y.
 Standard Surplus, 1230 Market Street, San Francisco 3, Calif.
 TAB, 111-WD Liberty Street, New York 6, N. Y.

Also refer to local Classified Telephone Directories under the headings of:

"Radio Equipment and Supplies"
 "Electronic Equipment and Supplies"
 "Surplus Materials"

and binding posts paralleling the outlet socket, neither of which is absolutely essential.

The only unusual item is the home-made "current transformer" (T2), the details of which are shown in Figs. 3 and 4. AC ammeters are scarce in surplus stocks, and since any ammeter's scale is non-linear, lower values are hard to read. Both of these problems are overcome by using a simple low voltage ac meter, the "current transformer," and multipliers to provide two or more ranges.

The transformer shown was made by wrapping insulated #14 wire around an old relay coil. The coil used was from a surplus relay, has a dc resistance of nearly 7000 ohms, and is about 2 in. long and of 1 in. dia. The #14 wire (top winding of T2 in Fig. 2) is in series with the power line through the unit, and current flowing through these turns of heavy wire induce a voltage in the relay coil, which deflects meter M2. The action is fairly linear, and the meter can readily be calibrated in amperes.

The meter used was a 0-2 volt ac meter. About 8 turns of #14 wire give a full-scale deflection (2 volts) when 3 amperes flow through the circuit. Smaller wire, with more turns, could be used to get greater deflection. For example, 3 amps flowing through the additional turns permitted by using #18 wire might give induced voltages of over 5 volts, permitting the use of a higher range voltmeter.

To make the transformer, first decide on the current to be required to give a full-scale deflection of the meter on the lowest range (if more than one range is desired). Then make a mounting for the relay coil on the back of the meter, as shown in Figs. 3 and 4. Temporarily connect the relay coil terminals to the voltmeter and solder one end of the heavy wire to the lug at one corner of the mounting plate. Wrap as many turns of heavy wire as

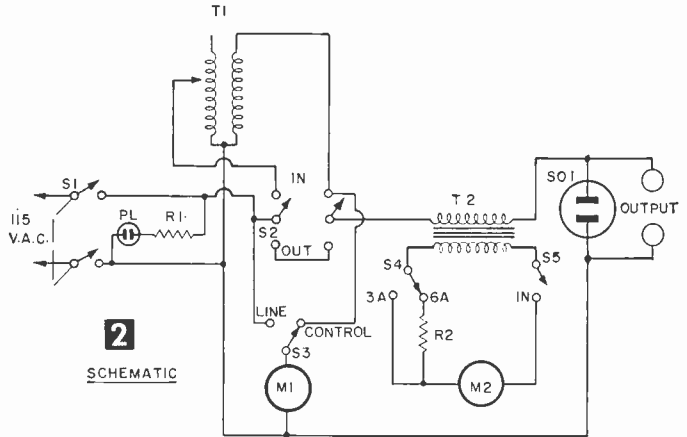
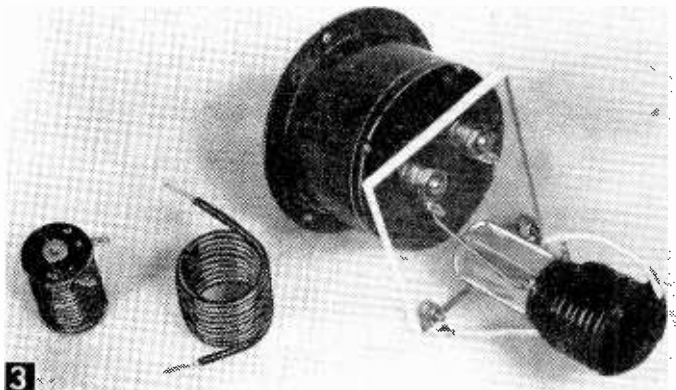


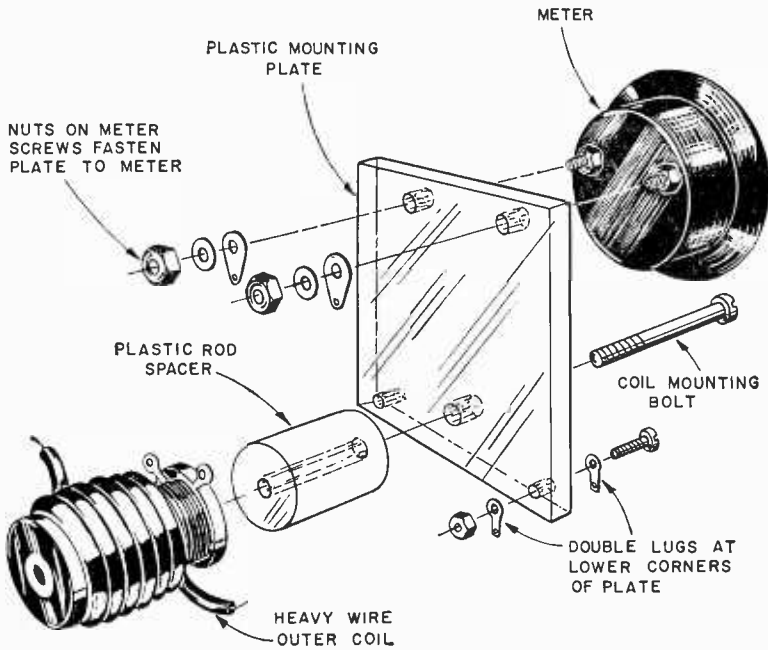
TABLE A—LIGHT BULBS REQUIRED TO GIVE SPECIFIC CURRENTS (at 120 volts)
 Note: The wattage rating of domestic lamps is usually quite accurate. Due to the combinations used for most readings, any inaccuracies tend to offset each other. However, only new or relatively new lamps should be used for the greatest accuracy.

FOR CURRENT (amperes)	WATTS REQUIRED	LAMPS REQUIRED (connected in parallel)
.125	15	15
.25	30	15 + 15
.5	60	60
.75	90	60 + 15 + 15
1.0	120	100 + 10 + 10
1.25	150	150
1.5	180	150 + 15 + 15
1.75	210	150 + 60
2.0	240	200 + 15 + 15 + 10
2.25	270	200 + 60 + 10
2.5	300	200 + 100
2.75	330	200 + 100 + 15 + 15
3.0	360	200 + 100 + 60
3.25	390	200 + 150 + 25 + 15
3.5	420	200 + 150 + 60 + 10
3.75	450	200 + 150 + 100
4.0	480	300 + 150 + 15 + 15
4.25	510	300 + 150 + 60
4.5	540	300 + 200 + 25 + 15
4.75	570	300 + 200 + 60 + 10
5.0	600	300 + 200 + 100
5.25	630	300 + 200 + 100 + 25 (minus 5W)
5.5	660	300 + 200 + 100 + 60
5.75	690	300 + 200 + 150 + 40
6.0	720	300 + 200 + 150 + 60 (minus 10W)

Lamps required to calibrate to 3 amperes: two 10 watt, two 15 watt, one 60 watt, one 100 watt, one 150 watt, one 200 watt
 Additional lamps required to calibrate to 6 amperes: one 25 watt, one 40 watt, one 300 watt.
 Four sockets will be maximum required for either calibration.



"Current transformer" and meter, showing at left the type of relay coil and heavy wire used.



4 CURRENT TRANSFORMER MOUNTING

possible around the relay coil (single layer) and hold the turns in place with a turn or two of plastic electrician's tape. Connect the coil of heavy wire in series with the load desired for full-scale reading (see Table A).

If the meter goes off-scale, reduce the number of turns of heavy wire by unwinding the free end of the coil, a turn at a time. Continue checking the meter reading, and as the exact full-scale point is approached, reduce the turns by half- and quarter-turns, to get the exact winding required to give full-scale deflection when the desired current is flowing. When this point is reached, tape the free end of heavy wire on the relay coil, and solder the end to the lug at the other corner.

If the full number of turns will not give full scale deflection for the desired current, these are several alternatives. One, use a meter of greater sensitivity; two, try winding a second layer of heavy wire; three, increase the current desired for full-scale deflection; and four, use smaller wire. The second layer of wire may reduce induced voltage unless wound carefully, and the use of smaller wire may be undesirable if it has insufficient current capacity for the full load required, particularly if several ranges are to be used.

In making the transformer mounting, make the plastic rod spacer as long as possible (within the limits of the cabinet chosen) to keep the relay coil away from the meter. This is particularly important if the meter is in a non-metallic case, as it reduces the possibility

of the magnetic field around the coil affecting the meter action.

To determine the multiplier used for the higher range (R2), use a variable resistance or resistance decade. Set the value high (50K or more), and connect the load required to give the desired deflection at full-scale on the higher range. The meter should read less than full-scale, and gradually reducing the resistance to the value required for full-scale deflection will give the multiplier (R2) value required.

To calibrate the meter, place the meter-transformer assembly in the panel (if a metal panel is used), and, using the lamp combinations shown in Table

A, note the meter readings on the existing scale at different current values, for both ranges (if more than one is used). In the unit shown, intermediate markings were not made up to 3 amps on the 6-amp scale, since those values would be read on the lower range.

There are definite reasons for the voltmeter switch (S3), the voltage control switch (S2), and the ammeter switch (S5). The voltmeter switch permits the voltmeter to be switched to read either direct line voltage or controlled voltage. The voltage control switch allows the control to be switched out of the circuit to permit measurement of current at direct line voltage, without "artificial" adjustment. The ammeter switch permits the ammeter to be switched out of the circuit when using devices that have a high starting current in excess of meter capacity, but a lower running current.

No dimensions are given, as they will vary with individual needs and the exact surplus parts secured. For most use, a 3-amp auto-transformer will do, as it will handle up to 360 watts, although a larger unit might be needed if much work is done with fractional horsepower motors.

Two-in. meters will do, although three-in. meter faces give longer scale length and only cost a dollar more at most surplus houses. Switches S1 and S2 must have a current capacity equal to the maximum to be handled by the unit; the others can be standard 3-amp switches.

R2 and R3 where the AF voltage is negative with respect to ground. This negative audio voltage, acting through L1 (low AF impedance) biases the tube automatically and causes it to act as an AF amplifier. The AF signal in the tube's plate lead is not affected by L3, nor is it transferred to L2. Nor is it grounded by C6. Instead, it appears across the primary of the audio transformer T1 to operate the speaker connected to the secondary winding.

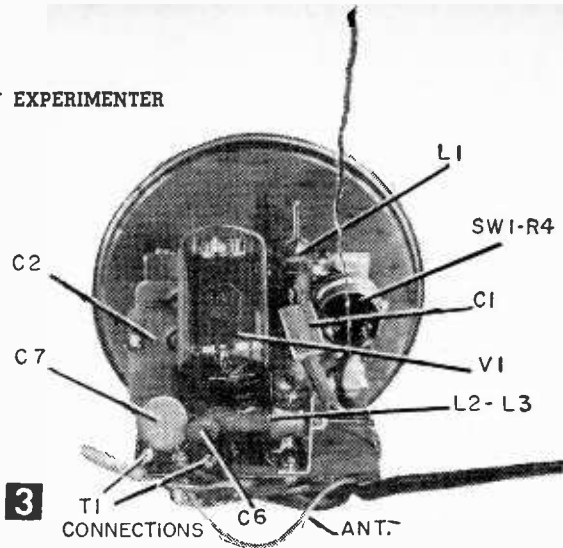
Construction. The receiver is built with the speaker and output transformer mounted in the bottom of the can and other components mounted on an L-shaped chassis which is fastened to the lid of the can by the volume control shaft and two machine screws. The chassis may either be of aluminum or sheet metal. Sheet metal will be somewhat harder to work, but will allow the builder to solder ground connections directly to the chassis without using solder lugs.

Form the chassis from a piece of material $3\frac{1}{4} \times 5$ in. bent to a right angle with sides measuring $2 \times 3\frac{1}{4}$ in. and $3 \times 3\frac{1}{4}$ in. The 2-in. side fastens to the lid with the other leg of the angle centered about $\frac{3}{4}$ in. from one edge of the lid. The $2 \times 3\frac{1}{4}$ -in. covers most of the lid to reinforce the thin material to which it is attached. The 3-in. leg is used for mounting the components.

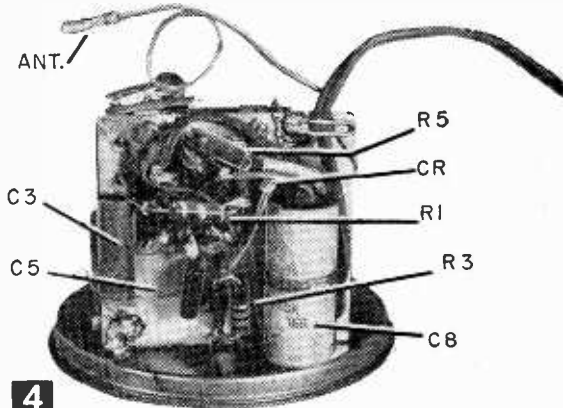
Tuning capacitor, C2 and volume control R4 are placed so that their shafts are centered in the lid. The tube socket is placed behind C2 as close as possible. Transformer L2-L3 is mounted horizontally next to the tube as shown in Fig. 3, while L1 is mounted in a vertical position between the tuning capacitor and volume control. A two-lug terminal strip on the top of the chassis, at the right rear edge, is used to connect the output transformer leads to the chassis. Capacitors C6 and C7 are also mounted on this strip.

Filter capacitor C8 is placed on the right underside of the chassis and next to it, toward the front, is a two-lug terminal strip for mounting R2, R3, and C5. The layout of the remaining components is not critical, but care should be taken that the lid will fit properly with everything mounted and that the grid and plate leads are separated as much as possible to avoid the possibility of feedback. It is particularly important that L1 and L2 be mounted at right angles to one another and separated as much as possible in order to minimize coupling.

The RF transformer L2-L3 is made by winding 75 turns of litz wire (obtainable from a discarded RF or IF coil) over the windings of a ferrite antenna coil. The added



3 Chassis for the receiver is an L-shaped bracket which fastens to the tobacco can lid. This photo shows the layout of parts on the topside of the chassis. Leads from the output transformer are soldered to the terminal strip at the rear edge.



4 Underside of chassis. Holes for bringing leads from the top of the chassis should be placed so that plate and grid leads are short and separated from one another.

winding should be secured with several coats of coil dope or finger-nail polish. The original winding is L2; the added winding, L3.

A 12-in. piece of hookup wire brought out of the cabinet with the power cord serves as an antenna lead-in to the chassis. A pin-jack from a discarded tube socket can be soldered to this wire and shielded with tape or plastic tubing to make a handy antenna jack.

Mount the speaker in the bottom of the can with four machine screws. Output transformer T1 can be mounted with screws or soldered in place. If the recommended speaker is not used, its replacement should not extend above the bottom of the can more than $1\frac{3}{4}$ in., otherwise the chassis may have to be made smaller.

Small holes in the bottom of the can serve as a speaker grille. Or, for better tone, cut a 4-in. dia. hole in the bottom with a sharp

MATERIALS LIST—TIN CAN RECEIVER

Desig.	Description
C1	100 mmf. mica capacitor
C2	365 mmf. variable (double-bearing replacement type) capacitor
C3	.05 mf. 200 WV midget tubular capacitor
C4	.001 mf. disc ceramic capacitor
C5	500 mmf. mica capacitor
C6	.001 mf. disc ceramic capacitor
C7	.005 mf. disc ceramic capacitor
C8	20-20 mf. 150 WV dual electrolytic (Cornell Dubilier BBRD 2215) capacitor
Cr	1N34 or CK-705 diode
L1	hi-Q ferrite antenna coil
L2	hi-Q ferrite antenna coil
L3	75 turns of litz wire wound over L2 (see text)
R1	56 ohm, 1/2 watt resistor
R2	22,000 ohm, 1/4 watt resistor
R3	1 megohm, 1/4 watt resistor
R4	1,000 ohm, 1/4 watt Volume control (with SPST switch)
R5	1,000 ohm, 1 watt resistor
Spk	4" PM replacement type speaker, 3.2-ohm coil (Jensen 4J6 or Cletron PM-4P2)
Sw1	SPST switch (on volume control R4)
T1	3,000/3.2 ohm, 3-watt output transformer
V1	117N7/GT tube

1 wafer or saddle-mount octal socket, 2 terminal strips (2-lug type), twenty 1/8 x 1/4" machine screws, 5' power cord with plug, 3/4 x 5" pc. of #16 or #18 ga. aluminum or sheet metal, 12" #8 copper wire, plain or tinned, solder & hook-up wire.

knife. But watch the sharp edges! When the mounting holes for speaker and output transformer have been drilled, plus a hole at one edge for the power cord, glue a piece of perforated cardboard over the bottom of the can to protect the speaker cone.

Then make three hairpin legs of #8 silvered copper wire formed into V shapes 1 1/4 in. high and soldered in place. For gold legs, use untinned copper wire that has been polished and given a coat of clear finger-nail polish to retard tarnishing.

With completion of chassis wiring and speaker mounting, bring the power cord and antenna lead through the hole in the bottom of the can and attach a power plug. Next, solder the output transformer primary leads to the lugs of the terminal strip at the rear of the chassis. These leads should be long enough to permit the chassis to be removed from the cabinet with the speaker in place.

To test the unit, use a long antenna. (The set should never be grounded or operated on a metal surface.) With an antenna connected, turn the set on and advance the volume control to maximum. Check and see if the filaments are lit before tuning across the band. If working properly, the receiver will receive stations clearly—or with a whistle. In either case, find a strong station at the high end of the band and adjust L2's slug for best reception. At some point of adjustment the audio will become distorted. Set the slug just below this point.

Because of the metal cabinet and the absence of a loop antenna, a short external antenna is necessary. For local stations, 4 ft. of hook-up wire is sufficient. For distant stations, a longer length strung around the room will do. When the set is working properly,

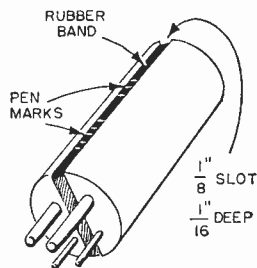
connect a short antenna and adjust L1 so that C2 tunes the entire broadcast band and then adjust the slug on L2 again for best reception. The receiver is now ready to be placed in its cabinet.

A small amount of regeneration requires the initial adjustment of L2 to avoid distortion or oscillation at the upper edge of the band. This also tends to make the receiver more sensitive on the high end of the band, but volume for all stations is nearly the same due to the AVC action of the audio bias. While not as selective, the receiver has better tone than most small table-models, despite the small speaker and tin cabinet. If poor selectivity is noticed when the set is operated near local, high-power stations, reduce the value of C1 by about half.

Note: To avoid the possibility of shock, either: 1) always plug the power cord into the 110-v outlet with the cabinet common to the ground side of the power line (this will also give best reception); or 2) completely isolate the line from the cabinet and chassis by making all ground connections to a terminal lug insulated from the chassis. Capacitor C4, however, should be grounded to the chassis to provide an RF return to the tuning capacitor frame.

Coil-Winding Tip

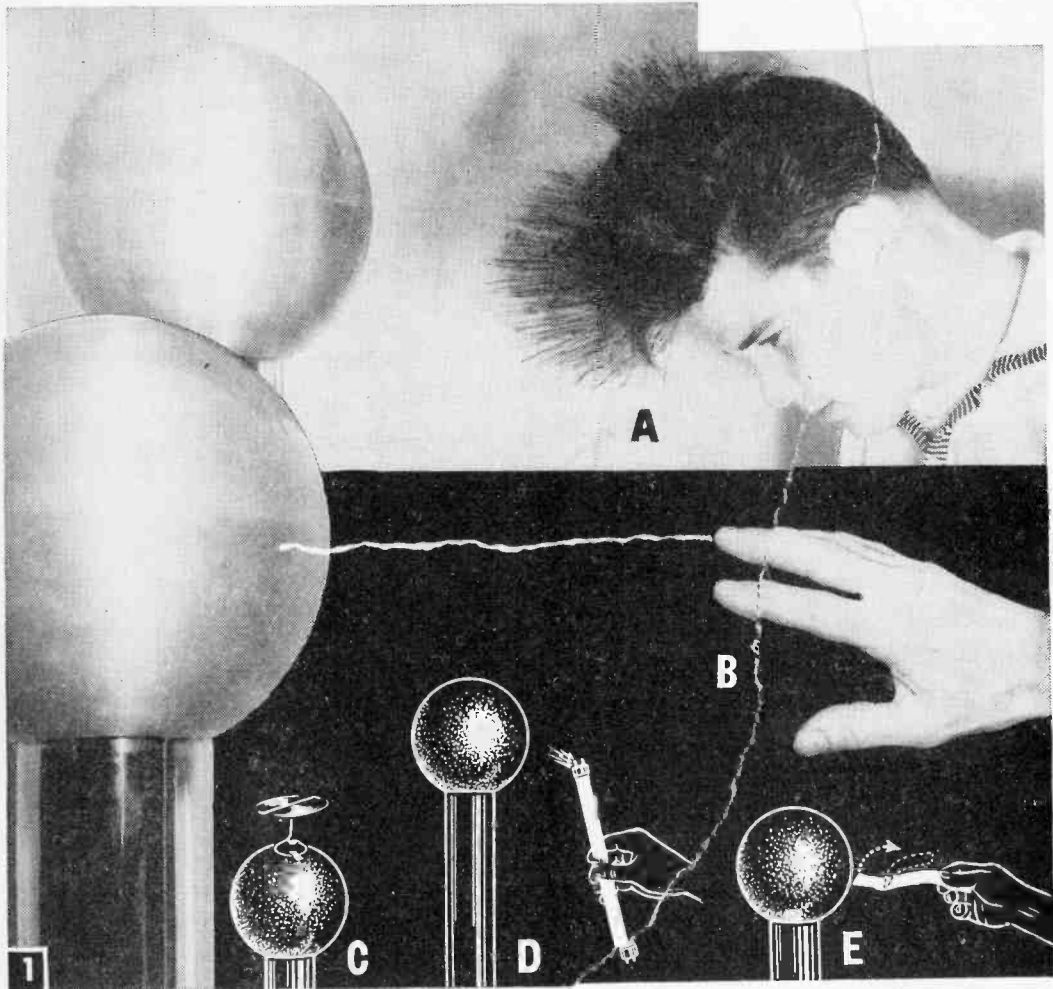
• Amateur radio operators who wind their own short wave coils know how difficult it sometimes is to properly space and anchor just a few turns of wire. The solution is to saw or file two opposite slots 1/8 in. wide and



about 1/16 in. deep on the top edge of the coil form. Place a wide, flat No. 32 rubber band in these slots and stretch it over the form and between two pairs of prongs. Fountain pen or ball pen marks are easily made on the rubber band, exactly where each turn of wire should pass. Draw the wire tightly to embed it in the insulating rubber and hold it neatly in place without the use of cement.

Invert Aerial to Speed Installation

• The neighbors may think you're crazy if you start the installation of a TV or radio aerial upside down, but doing this will help you to quickly and easily align a bracket on the edge of your house. By having the mast parallel a corner of the building, one of the windows, or some other vertical part, it is easy to sight the alignment while adjusting the mounting bracket. Then you need only reverse the mast to finish the job.



(A) Standing close to the sphere stands your hair on end and charges to tingle your scalp. (B) Blue flashes will jump to your fingers held 12 in. or more away. (C) Corona point discharge from the tips of a wire rotor spins it like a pin wheel. (D) When end of a fluorescent tube is held closely to sphere, small streamers of blue discharges burn from the lamp terminals and lamp lights. (E) Cloth strip shows electrostatic laws of attraction and repulsion. Tossing a strip of cotton cloth at sphere causes it to remain horizontal. When end touches sphere, it becomes charged to its polarity and is violently repelled.

Experimental Van de Graaff Generator

Develop up to 380,000 volts on the same principle as scuffing across a heavy rug

By HAROLD P. STRAND

YOU can build a simplified version of the electrostatic generator developed in 1931 by Dr. Robert J. Van de Graaff that aided in the development of the atomic bomb. The full-size generators produce several million volts on an aluminum sphere at the top of an insulated column.

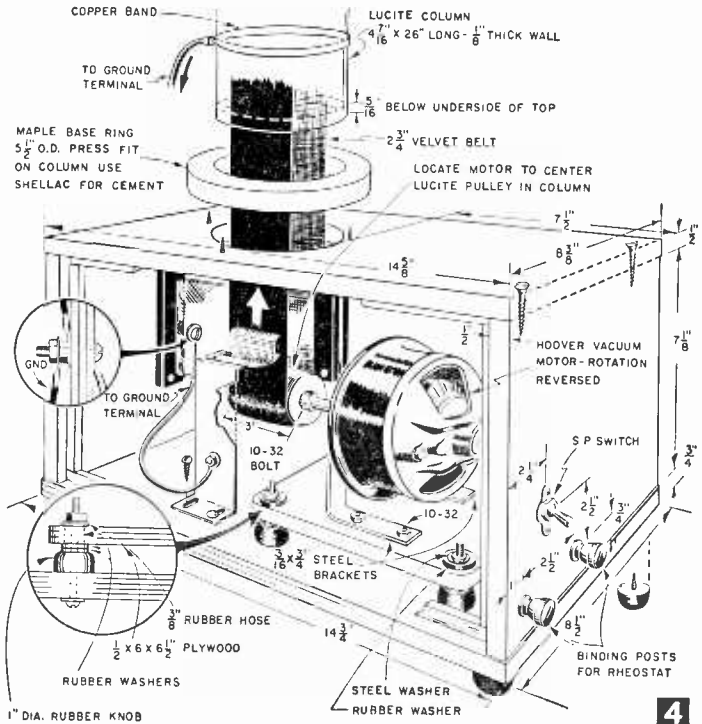
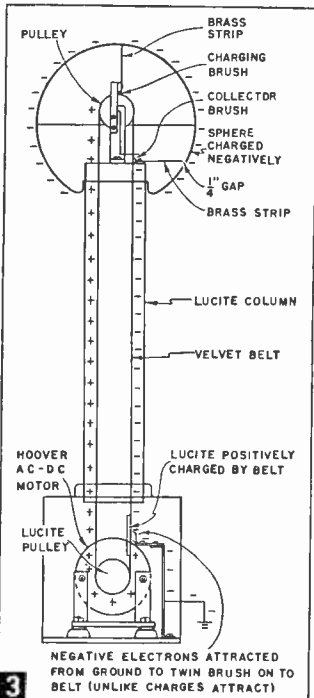
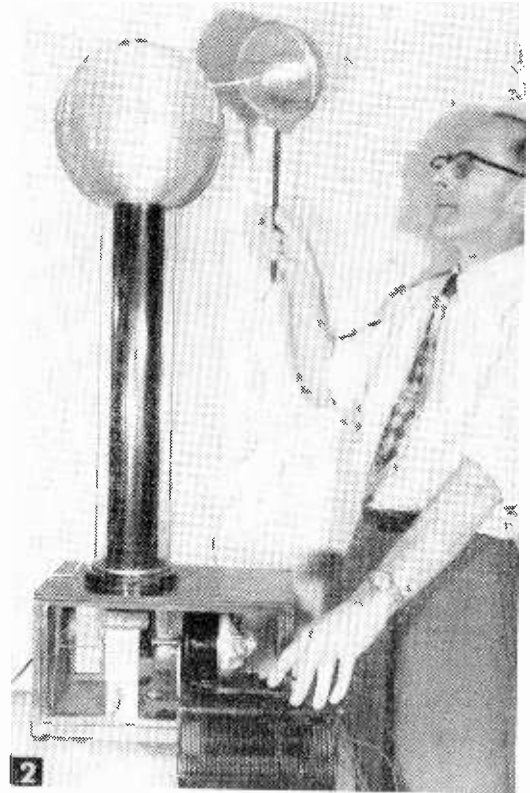
The small counterpart of these Van de Graaff generators will perform a variety of experiments (Fig. 1) and develop up to 380,000 volts under ideal atmospheric conditions. Dampness in the air reduces the efficiency of the unit causing leaks of the static charges from the belt, the column and the sphere to the air. When this unit was tested at the high-voltage laboratory of a large university in dry air, the short-circuit current was 18 microamps at the calculated voltage.

The high voltages generated are not usually dangerous, although you can feel a good sting if sparks jump to your fingertips when held too close to the ball. There is no electrical power

supplied to the belt; it picks up charges as the velvet rubs over plastic. Static charges on the surface of the plastic are positive and attract negative charges from the ground through a brush near the bottom end of the belt. These negative charges are carried upward on the moving belt, picked off by one of the two brushes in the top and carried to the surface of the sphere through the corona gap. The other brush is called the charging brush because it insures a positive polarity of the belt on the way down (Fig. 3). After a few minutes of operation, voltage builds up on the sphere to the maximum possible with the insulation provided and atmospheric conditions present. The model stands 39½ in. high and only weighs 18 pounds. The only requirement for operating it is a 115-volt a-c or d-c outlet for the motor.

An inexpensive motor for driving the belt can be salvaged from an old Hoover vacuum cleaner. A slide-wire resistor or rheostat controls the speed to around 3000-4000 rpm. These motors are usually available at repair shops for \$5 or \$6 and develop about ¼ hp. Be sure to select one with tight bearings that runs fast, smooth and without excessive sparking. It's a good idea to disassemble the motor, clean out dirt and old oil first. While the armature is out, turn the threaded end of the shaft to a ¼-in. diameter (Fig. 5). To reverse the direction of rotation to drive the vel-

Table-top Van de Graaff throws heavy, noisy discharge to hand electrode up to 5 in. or thinner discharges up to 8 or 10 in. This model simulates the full-size generators that helped in atomic research.



3

4

A plywood cabinet encloses the motor and the base of the plastic column (Fig. 4). The motor mounts on two angle brackets bent up from $\frac{3}{16}$ x $\frac{3}{4}$ -in. mild steel or aluminum. Make a base for the motor from $\frac{1}{2}$ -in. birch plywood and mount it on large rubber knobs at the four corners to reduce vibration and to allow the belt to be tightened by compressing the rubber. Adjust compression on rubber mounts to align pulley.

A turned hardwood ring with its inside diameter of about $\frac{7}{16}$ in. should be a tight fit around the Lucite column. Shellac or varnish makes an effective cement to hold the column in the ring. A flat copper wire (salvaged from the field winding of an old automobile starter) around the column keeps lower end of unit at ground potential.

The lower belt pulley mounts directly on the end of the motor shaft (Fig. 5). Turn a slight crown on the solid Lucite pulley to help keep the belt centered. Turn the center rod parts from brass stock and assemble pulley to the end of the motor shaft with set screw. Turning and center hole boring must be done accurately.

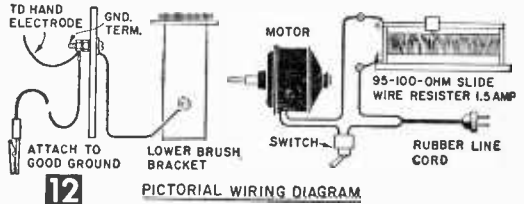
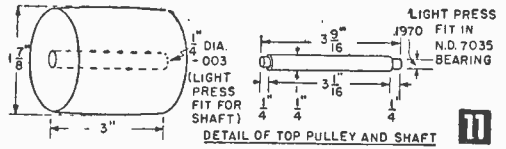
A bent-up piece of .064 aluminum supports the ground inductor brush (Fig. 6). Two pieces of copper screening, $\frac{1}{32}$ -in. mesh, give numerous arcing points and are adjusted with screws to about $\frac{1}{8}$ in. from the moving belt after it is in place.

A piece of Lucite sheet must be fitted inside the cabinet so the back of the belt rubs it (Fig. 7). Fit the Bakelite supports after the belt is in place.

When you complete the base cabinet, mount the driving motor, lower brush pickup and pulley, you're ready to add the top pulley assembly, make the belt and top sphere.

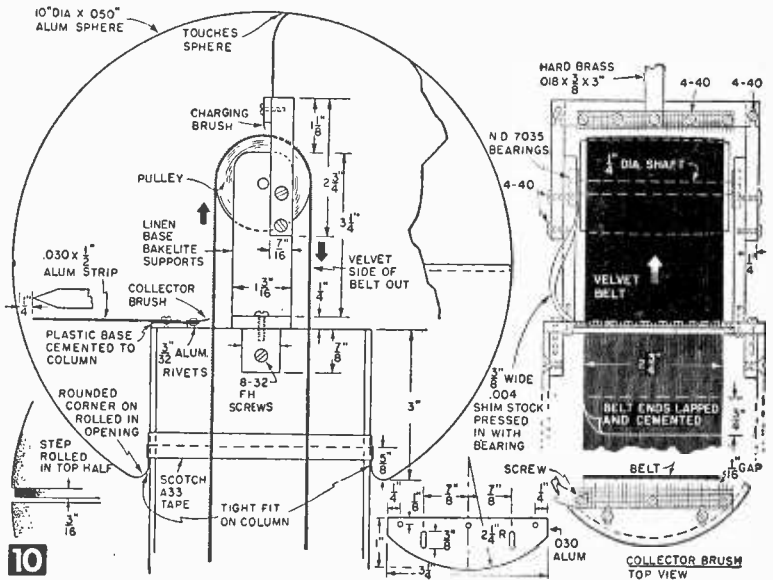
The top pulley and brush collector assembly inside the aluminum sphere mounts on two chunks of paperbase Bakelite screwed and Pliobond cemented to the inside of the Lucite column (Fig. 10). These blocks are curved to fit the column and must be mounted directly opposite each other and centered. The vertical U-supports that hold the top pulley must be bored for a press fit with the bearings. Use a $\frac{3}{4}$ -in. end cutting bit or end mill .0003-.0006 in. undersize in a drill press to bore out for the bearings. Or you may use a single lip type wood boring bit without a threaded center worm in a drill press if well sharpened.

Bore a $\frac{1}{4}$ -in. center hole about .0003 in. undersize in the piece of 2-in. dia. Lucite to be used for the top pulley for a press fit with the $\frac{1}{4}$ -in.



shaft, or you can drill a full-size $\frac{1}{4}$ -in. hole and turn a slightly oversize steel shaft for a press fit in the hole (Fig. 11). Cut bearing seats on the ends of the shaft for a light press fit in the bearings. Use the lathe cut-off tool to indicate length of the shaft, remove from lathe and remove the excess length; file ends smooth. Now, cut a piece of aluminum foil long enough to wrap around the pulley and lap $\frac{1}{16}$ in. Pliobond to pulley.

To assemble the upper pulley unit, press the bearings on the ends of the pulley shaft, then press the Bakelite side supports over the outer race of the bearings. The U-supports and the cross piece must be centered so the pulley is di-



rectly over and in alignment with the bottom pulley. A plumb bob or weight on a string helps to align the pulleys vertically, but be sure the bottom assembly is resting level. After locating the U-supports, screw them to the Bakelite cross piece and screw the cross piece to the blocks at the top of the column. The top pulley assembly will be removed later to slip on the belt.

MATERIALS LIST—VAN de GRAAFF GENERATOR

- Clear Lucite
 1 tubing 26" long x 4 1/2" dia. x 1/8" wall. May come about 4 7/16" diameter actual measurement, column
 2 solid rod stock 3" long x 2" dia., pulleys

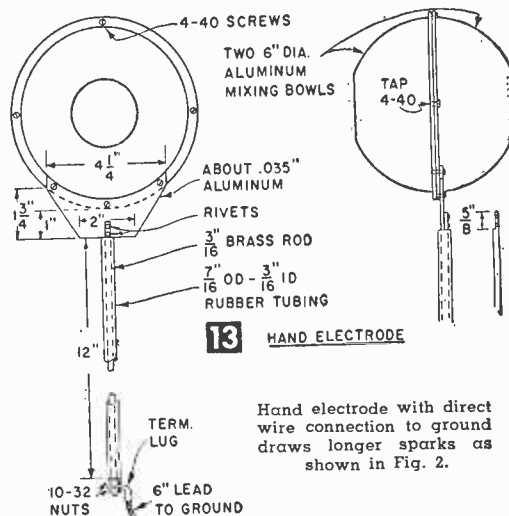
- Natural paper base Bakelite
 1 1/2 x 3/4 x 3 7/8" (Friction piece support in base)
 1 1/4 x 5/8 x 2 1/2" (Friction piece support in base)
 1 1/8 x 5/8 x 2 1/2" (Friction piece support in base)
 Forest Products Company Inc., 131 Portland St., Cambridge, Mass. will supply the above material postage paid to any part of the U.S.

- 1 1/16 x 2 x 6 1/2" alum. brush bracket (base)
 1 .032 x 1 3/8 x 2 3/4" alum. alloy (top of bracket)
 2 3/16 x 3/4 x 5 1/2" mild steel motor angle brackets
 1 9/16" dia. x 1 7/16" brass lower pulley
 1 5/8" dia. x 1 3/4" brass lower pulley
 1 1/2" 8 3/8 x 14 5/8" birch plywood, cabinet
 2 7/8 x 8 3/8" birch plywood, cabinet
 1 fir plywood 3/4 x 8 1/2 x 14 3/4" base
 8 ft 3/8 x 3/8" hardwood strip stock

Miscellaneous

- 4 rubber knobs or feet
 4 rubber knobs about 3/4 to 1" diameter for motor base
 1 universal motor from an old Hoover vacuum cleaner
 1 3 x 4" copper screening, preferably 1/2" mesh
 1 flat copper wire from the field coil of an old auto starter, about 24" long, ground band around column

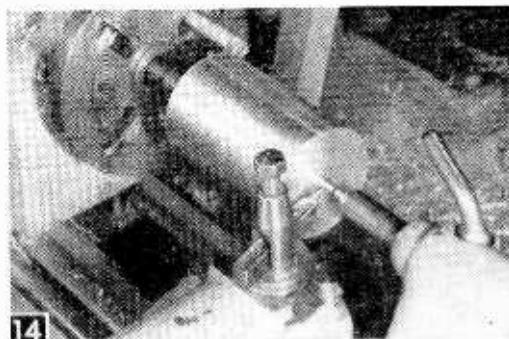
- | No. | Size and Material | Use |
|--|---|---|
| 1 | 1/8 x 1/2 x 4 1/4" sheet Lucite | top brush strip |
| 1 | 1/8 x 3/4 x 3 1/4" sheet Lucite | brush base in top |
| 1 | 1/4 x 1 1/4 x 4 1/2" paper base Bakelite | top support |
| 2 | 1/4 x 1/8 x 2 3/4" paper base Bakelite | side support blocks, top edge of column |
| 2 | 1/4 x 3/4 x 7/8" paper base Bakelite | pulley supports |
| 2 1/4 x 1 3/16 x 3 1/4" linen base Bakelite (Forest Products Company Inc., 131 Portland St., Cambridge, Mass. will supply the above material postpaid to any part of the U.S.) | | |
| 1 | 1/4 dia x 4 1/2" cold rolled steel | top pulley shaft |
| 1 | .030 x 1 x 3 1/4" sheet aluminum | side collector brush base |
| 1 | .030 x 1/2 x 3" sheet aluminum | corona gap strip |
| 2 | 6" dia mixing bowls aluminum | hand electrode |
| 1 | .050 x 1 3/4 x 4 1/4" sheet aluminum | handle support, hand electrode |
| 1 | 10" dia sphere, .050 alum. (available from Robert Towne, 49 Abbott Ave., Everett, Mass., \$8.25 ppd. in U.S.) | |
| 1 | .018 x 3/8 x 3" hard brass sheet | connecting strip |
| 1 | .003 or .004 x 3/8 x 4" shim stock | jumper to pulley |
| 1 | slide wire resistor or a rheostat 95-100 ohms, 1.5 to 2 amps | |
| 1 | S.P.S.T. toggle switch | |
| 1 | 2 3/4" wide x 6' long velvet ribbon | belt |
| 2 | New Departure ball bearings #7035 (Available from Bearings Specialty Company, 665 Beacon Street, Boston, Mass.) | |
| 1 | 3/16 dia x 13" long steel or brass rod | handle for hand electrode |
| 1 | 3/16 I.D. x 1/2 O.D. x 12" long rubber tubing | handle for hand electrode |
| misc. wire, stain, shellac, screws, nuts, etc. | | |
| heavy duty aluminum foil, Pliobond cement | | |



sembly at the two #6-32 screws and slip the unit through the loop of the belt. Tightening the base nuts maintains the reasonably tight tension required. When the belt is running straight and true, adjust the plastic piece in the base and fit the ground brush in place.

In case you have difficulty keeping the belt running true, there are several ways to correct misalignment. Thin shims of cardboard under either base end of the top pulley support or tightening front or rear motor bolts allow considerable adjustment. For further adjustment, the holes in the cabinet base can be slotted to permit shifting the motor as required.

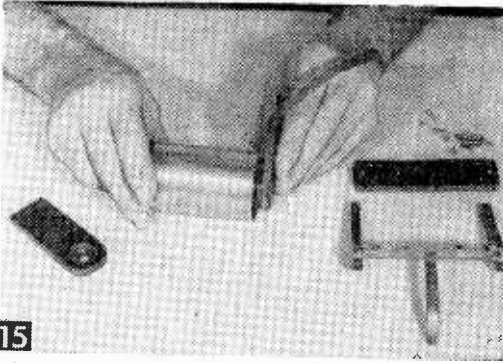
The aluminum sphere is a metal spinning made according to Fig. 10. You should be able to have a local metal-spinning shop do the job for you, if not, you can get a sphere by mail from the source indicated in the Materials List. When spinning the turned-in neck that should fit tightly over the top end of the column, avoid any sharp corners or the built-up energy from the sphere will leak away. The seam between the two halves of the sphere should form a smooth joint to eliminate any edges where energy can leak off.



Machining shaft to be a light press fit in New Departure ball bearings 7035.

Velvet ribbon for the belt may usually be obtained from a large department store. You'll need about 6 ft. of 2 3/4-in. ribbon of any color. To determine the exact length, run a string over both pulleys and allow about 3/4 in. for lapping at the joint (Fig. 10). Apply a generous coating of Pliobond cement to both surfaces to be joined and clamp between two pieces of wood in C-clamps. Be careful not to allow cement outside of the lap area, or it will be difficult to separate from the wood later. Let the lap set overnight.

To install the belt, remove the top pulley as-



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A strip of .003-in. brass shim stock is pressed in with bearing at left side (facing collector brush). After starting the bearings in their holes, an arbor press can be used to seat them. Note other top end parts.

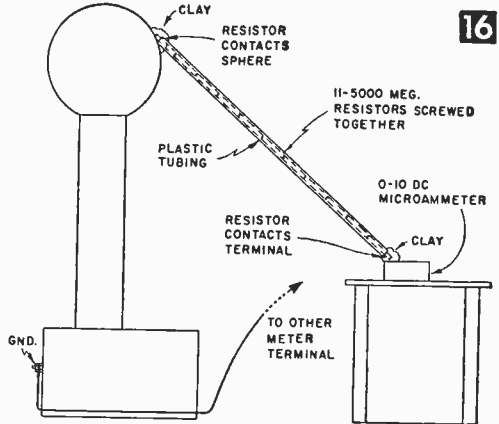
When the bottom half of the sphere is adjusted, fit the brush collectors and the spark gap strip at the top (Fig. 10). The wiring diagram (Fig. 12) shows the necessary connections with the slide-wire resistor or rheostat in the circuit to control the motor's speed.

When all parts are assembled and you're ready to make the initial test, run the motor up to about 3000 rpm with the top half of the sphere off. After a few minutes, you should be able to draw short sparks to your finger at the belt in the region between the brushes if the generator is working right. Possible causes for non operation may be that the plastic sheet in the base is not in full contact with the belt or too much humidity.

A final test is to set the half-sphere on top and connect a d-c microammeter between the sphere's surface and the ground terminal. A small chunk of modeling clay will plaster the top lead to the sphere's surface. Start the motor and, after a few moment's operation, you should read 15-20 microamperes, the short-circuit current of the unit.

To test the voltage output of the generator, connect a string of eleven 5000-megohm special high-voltage resistors (Type BBV, available from Resistance Products Co., Harrisburg, Pa.) by screwing their ends together (Fig. 16). Connect the series resistor string to one terminal of a 0-10 d-c microammeter away from the generator, using modeling clay to hold it in constant contact with meter terminal. Attach other end of the resistor string to the sphere with clay. Enclose the resistors in a tube of plastic or other insulation. The other terminal of the meter is connected to the ground terminal of the generator. You might be able to test your generator in a nearby university or electrical testing laboratory which would probably have the special resistors and microammeter.

When you complete the voltage test set up, run the motor at about 3000 rpm for a few minutes to allow voltage to build up on the sphere. Depending upon the humidity conditions in your test room, you should be able to read from 6 to 8 microamperes. If the meter's needle fluctuates wildly, it probably indicates the plastic piece is



Set up of resistors and microammeter for checking voltage of generator. It will vary with humidity.

not making full contact with the back of the belt. Good contact between the sphere's surface and the resistor string and at the meter is also important for correct readings.

When you read the current on the meter, calculate the voltage using Ohm's law ($E = I \times R$, where E represents voltage, I the current in amperes and R the resistance in ohms). One micro-ampere is one millionth of an ampere, so 7 microamperes becomes .000007 amperes. One megohm equals 1,000,000 ohms and 55,000 megohms converts to 55,000,000,000 ohms. Completing the calculation shows the voltage at a current reading of 7 microamperes is 385,000 volts.

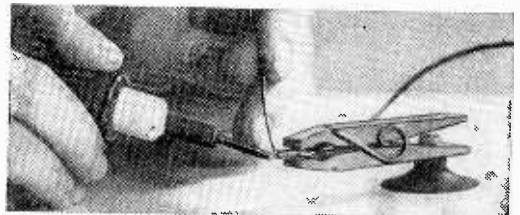
The hand electrode (Fig. 13) capacitor aids in experimenting with the Van de Graaff generator. It should be possible to get satisfactory discharges at speeds as low as 1000 rpm.

Foil Aids Set Alignment

- To avoid interference, it is common practice to stop a superhet's oscillator before aligning the intermediate-frequency amplifiers. A simple way to do this, is to wedge a piece of aluminum foil between the plates of the oscillator's tuning capacitor. When the dial is rotated, the foil between the rotor plates makes contact with the stator plates and "kills" the oscillator.

The Radioman's Third Hand

- A wood clip-type clothespin fastened to tabletop by a suction cup makes a handy holder for soldering of eyelets, terminals and lugs.

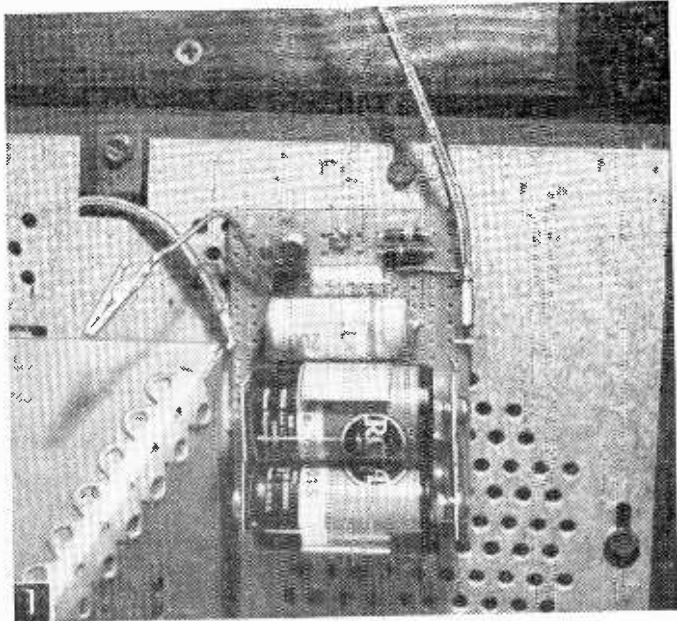


16

Build An Emitter Follower!

You can couple low-impedance devices to high-impedance circuits with this emitter follower. The unit can be built in a few hours for about \$3

By FORREST H. FRANTZ, Sr.



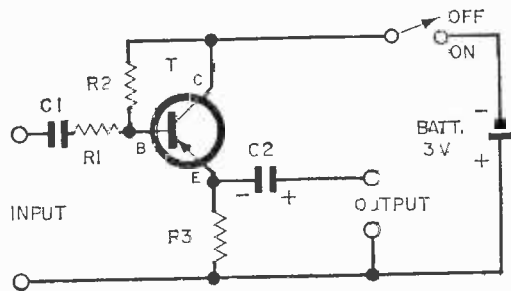
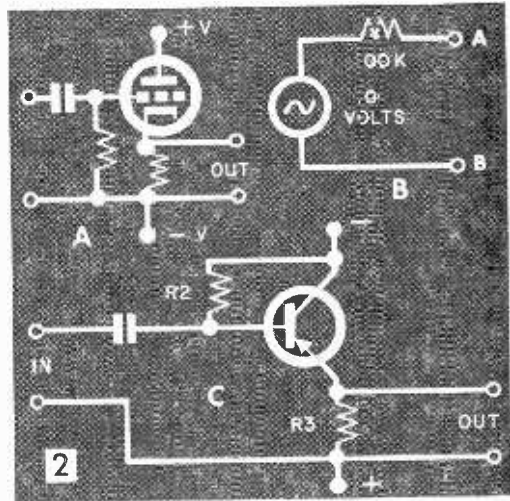
An emitter follower can be used to connect the audio of a radio or TV set to a hi-fi amplifier. If back of set is metal, insulate back of emitter follower.

ELECTRONIC experimenters and hi-fi enthusiasts frequently need to connect a low-impedance load to a high-impedance output. Typical applications are coupling a low-impedance microphone or phono pick-up, or using a low-impedance meter to measure voltages in a high-impedance circuit. An emitter follower will do the job.

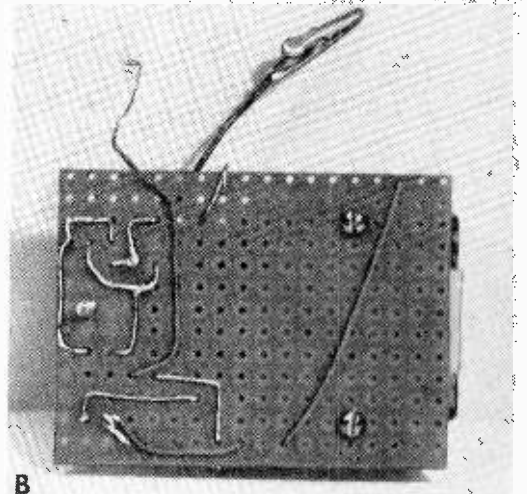
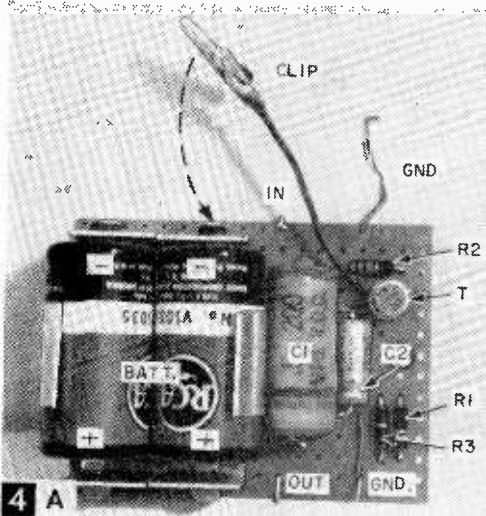
Sometimes the problem of coupling high impedance devices separated by considerable distance crops up because the capacitance between the connecting wire center lead and shield is sufficiently large to affect the frequency response of the system. If an emitter follower is connected in the line, the problem can be licked.

The emitter follower described in this article is relatively small in spite of the fact that no special effort was made to miniaturize it. Flashlight batteries were employed as a power source to obtain operating economy. The current drain on these batteries is less than 1 milliamper.

The emitter follower is the transistor equivalent of the vacuum-tube cathode follower. The voltage gain of a cathode follower is approximately unity. A simplified vacuum tube cathode follower circuit is shown in Fig. 2A. The input impedance of a cathode follower is high (several megohms), but the output impedance is low (several hundred ohms). Thus, if a low-impedance device such as the ac voltmeter section of a multimeter is to be used to measure ac voltage in a high-impedance circuit, it can be connected to the output terminals and the



3 SCHEMATIC



Front (A) and back (B) views of follower's parts placement and wiring.

input terminals of the cathode follower become high-impedance input terminals for the meter. Probe leads connected to these input terminals can be connected across high-impedance circuits without loading them significantly.

If, on the other hand, the low-impedance ac voltmeter section of the multimeter were placed across a high-impedance circuit, the circuit would be—for all practical purposes—shorted, and the voltage indicated on the meter would be very low. In addition to causing a low meter reading, the near-short circuit would affect the operation of the circuit under test. An example will illustrate this more clearly:

Assume that the voltage across terminals A and B in Fig. 2B is to be measured. If a meter with 5K impedance (1000 ohms per volt set to the 5-volt scale) is connected across terminals A and B, it will measure $5/(100 + 5)$ or $1/21$ of the 10 volts. However, if the meter is connected to the output terminals of the cathode follower, and the input terminals of the cathode follower are connected across terminals A and B, the meter will read nearly 10 volts. Assuming the input impedance of the cathode follower to be 10 megohms, the voltage across the cathode follower input is $10 \times 10/10.1$, which is nearly 10.

The cathode follower unfortunately has the drawbacks associated with a vacuum-tube circuit: high voltage supply requirements, wasted power and large size.

An emitter follower is free of these drawbacks, but there are some differences between it and the cathode follower. The circuit of a simplified emitter follower is shown in Fig. 2C. The input impedance of this emitter follower would be approximately equal to beta times R3, if R2 were not present. The

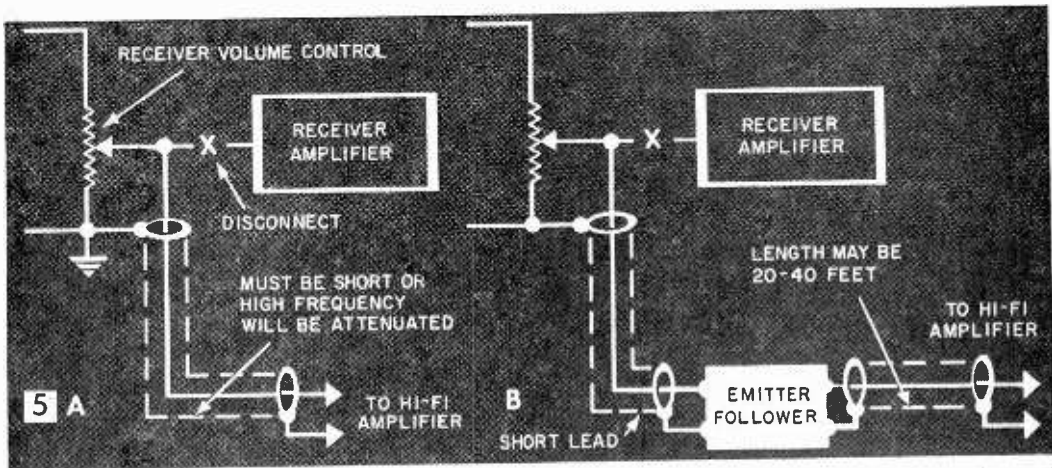
MATERIALS LIST—EMITTER FOLLOWER	
Desig.	Description
R3	2.2K, 1/2 watt carbon resistor
R2	220K, 1/2 watt carbon resistor
R1	470K, 1/2 watt carbon resistor
C1	.5 mfd., 200 v paper capacitor (Sprague 2EP-P50)
C2	30 mfd., 15 v miniature electrolytic capacitor (Sprague TE-1158 Litt'l Lytic)
B	two 1.5-v flashlight cells (RCA VS035 or Burgess No. 1) two cell battery holder (Lafayette MS-174) 27/16 x 33/8" miniature perforated board (Lafayette MS-304)
T	minigator clip (Mueller 30) 2N362 Raytheon transistor (or any PNP transistor, see text)

Components may be obtained from Lafayette Radio, 165-09 Liberty Ave., Jamaica 33, New York.

beta of the transistor is the current gain, and for the better audio driver transistors, beta is around 100. Then, if R3 is 1K, the input impedance of the emitter follower would be about 100K if R2 could be neglected. But R2 acts in shunt with the input signal, and therefore if R2 is about 200K (this is a practical approximation), the input impedance would be about 67K.

It might seem that the input impedance could be increased considerably by increasing R3. Suppose R3 were 10K. Then, if R2 could be neglected, the input impedance would be 1 megohm! Now, assuming that R2 can be 1 megohm, the input impedance becomes 1/2 megohm or 500K. Unfortunately, the size of the battery must be increased (greater voltage required) to use such values. Furthermore, the previous 1K output impedance has been increased to about 10K. This is a relatively high impedance in itself.

The Circuit that was chosen for the practical emitter follower described in this article is shown in Fig. 3. This circuit contains the compromises between voltage and circuit values that produce a high ratio of input to output impedance and relatively good frequency response. Resistor R3 was chosen as



2.2K; R2 was chosen as 220K. A series resistance R1 was added to increase the input impedance. In the original model, this resistor was 470K. The input impedance of the amplifier without this resistance was about 100K with a gain of unity. With R1 in the circuit and equal to 470K, the voltage gain was about 1/6, and the input impedance was about 570K. If R1 is 100K, the input impedance is about 200K, and voltage gain is about 1/2.

If a lower beta transistor such as a Raytheon CK722 or a GE2N107 is substituted for the higher beta 2N362 used in the original model, the input impedance of the emitter follower without R1 in the circuit will decrease to about 40K. Now if R1 is made equal to 40K, the input impedance of the unit will be 80K and the voltage gain will be 1/2. If R1 is 200K, the input impedance will be 240K and the voltage gain will be 1/5. It is easy to see that any PNP transistor that you might have will work in this circuit, but some performance is lost with lower beta transistors.

The front and back views of the emitter follower are shown in Fig. 4. The emitter follower is constructed on a perforated Bakelite board. The on-off switch is a Minigator clip which is connected to the unconnected battery holder lug to turn the emitter follower on. Two flashlight cells connected in series furnish the 3 volts required to power the emitter follower. The input capacitor C1 is 200-v paper capacitor which permits connecting the emitter follower to vacuum-tube circuits. The output capacitor C2 is a 30 mfd. electrolytic capacitor rated at 15 v. If you intend to couple into a circuit that has high voltage present, a higher voltage rating is required for this capacitor, but most circuits that you'll couple to won't have high voltage present.

To construct the emitter follower, drill the two battery mounting holes and the third mounting hole. This third hole has been provided to allow the emitter follower to be

bolted down on other electronic equipment for permanent or semi-permanent installation.

Next, mount the battery holder. Then place all of the parts on the board as shown in Fig. 4 by inserting the pigtails through appropriate holes in the board. Then turn the board over and use Figs. 3 and 4 to guide you in wiring. Most of the connections are made with the pigtails of the component parts. The pigtails are bent against the board, and wherever a connection is to be made, the wires are run against each other and soldered.

Input and output terminals consist simply of pigtail or wire ends to which Minigator clip leads may be connected on the original model. If you wish, you may provide wire leads with clips on the ends, or you may provide terminals on the model. The input leads should be shielded. Output leads must not be shielded unless a long length of connecting wire is involved.

The emitter follower will permit two high-impedance devices that are separated by a great distance to be connected together without high frequency attenuation. You might, for example, wish to use an inexpensive table radio as a tuner with a hi-fi amplifier since the tone quality of most inexpensive radios is quite poor. If you disconnect the radio audio amplifier from the center lug of the volume control and run a shielded lead to the amplifier as shown in Fig. 5A, you've converted the radio into a tuner for your hi-fi amplifier.

But, if the shielded lead is over, say, a foot or two long, it will attenuate the high frequencies due to the inherent capacitance of the shielded lead required to minimize ac hum voltage pick-up. If the capacitance of the shielded lead was in parallel with a low impedance such as that of the emitter follower output, the frequency response would remain relatively flat. Such an arrangement is shown in Fig. 5B.

Magic Light Bulb

THIS 60 watt Mazda bulb, removed from a light socket, glows when held in the fingertips or mouth, and when placed on a suspended pane of glass. Of course, it takes a little doctoring to make it work this way. First remove the "in-nards" from a burned-out 60 watt frosted bulb. With pliers, crush the black composition at tip of lamp base (Fig. 2). Shake out composition and remove brass button. With brass shell opening clear, insert plier handle and tap sharply, thus breaking off glass stem inside lamp (Fig. 3). Pull out glass stem and burned out filament through open-

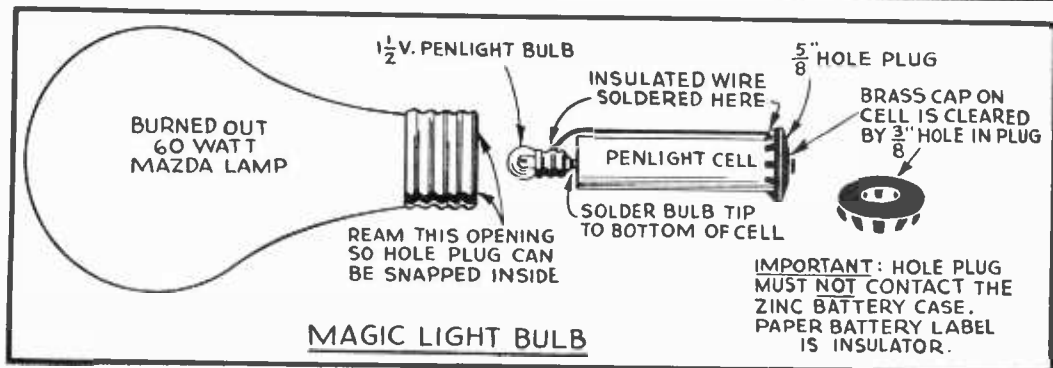
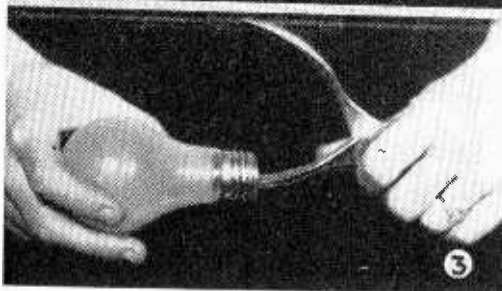


ing in bottom of brass screw base (Fig. 4).

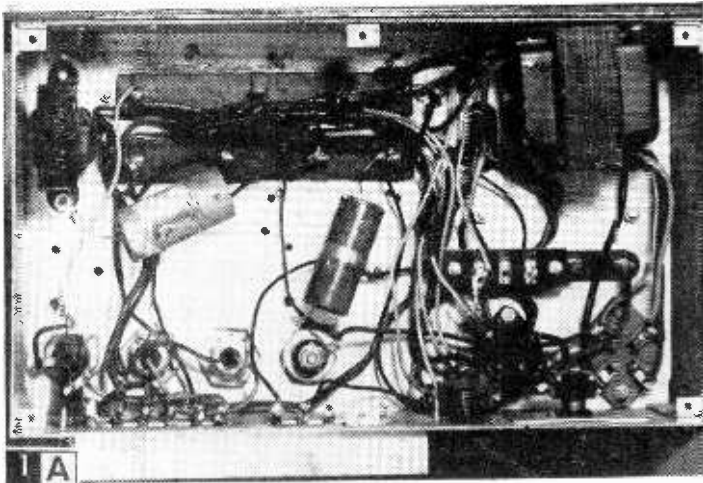
Obtain an anodized hole plug at an auto accessory or radio supply store, and a 1½ volt penlight bulb and a penlight battery. Cut a ⅜ in. hole in the hole plug. Insert pen-cell into plug, brass tip down. Solder tip of bulb to bottom of battery. Connect thin insulated wire from brass shell of penlight bulb to brass shell of hollowed out Mazda bulb. Ream base with closed scissors to admit battery and insert penlight cell assembly into bottom of lamp base (as shown in drawing).

So trick will look natural, insert bulb into a lamp which has been disconnected from the house current. When occasion arises, remove bulb from socket,

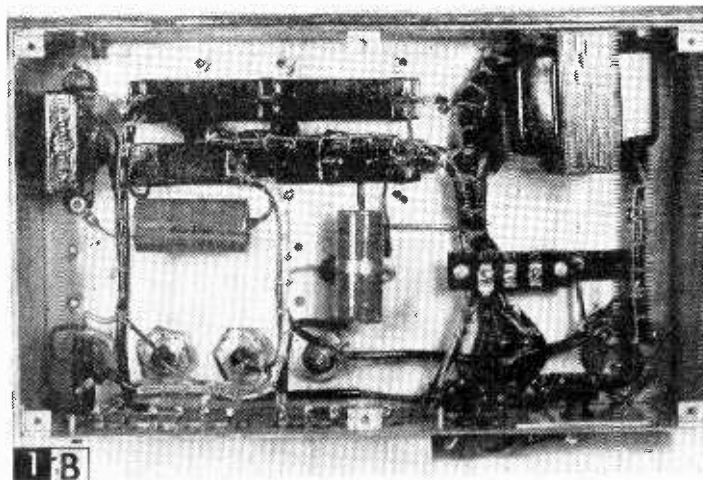
and hold it in your fingers. Press a dime, small paper clip or pin concealed in your hand against bottom of bulb. This completes circuit from center cap of inverted pen cell to outer brass shell of Mazda lamp and bulb lights up. A paper clip concealed under tongue may be used to light the bulb when held in the teeth. To light bulb in porcelain cleat socket with no connections and resting on a suspended pane of glass (Fig. 1), simply previously short-circuit the two screw terminals on socket with a piece of fine wire.—
R. R. DOISTER.



Professional Electronic Wiring



A general-purpose power supply is shown scramble-wired above. While it works, it looks bad and is difficult to troubleshoot. The same power supply is shown cleaned up below. An even more workmanlike job would have resulted if the builder had been willing to rewire the unit completely.



By HOWARD S. PYLE

WHETHER you build hi-fi or amateur radio equipment, you want gear you can point to with pride. What you are building is something which you expect to be more or less permanent. If and when you have occasion to abandon it, you can ask, and receive a far better price if your wiring, as reflected by your terminal connections and other circuitry, are of professional appearance and workmanship. Fig. 1A shows a "hay-wire" method of termination; Fig. 1B is the professional version. Which of the two

would attract *your* cold, hard cash.

Figures 2, 3, 4 and 5 illustrate the method of accomplishing the professional touch shown in Fig. 1B. A final touch of spit-and-polish can be given by applying a generous coating of clear lacquer (such as Fuller's ANL-232 "Synalac") over wire, sleeving and number tape.

A slack loop consists of nothing more than an excess wire length of 2 or 3 in. at the terminal, where it is formed into either a horseshoe or a complete circle. Use a 1/2-in. or 3/4-in. wooden dowel to form your circles. Slack loops serve two purposes: they provide sufficient slack in the wire to permit rerouting it to an adjacent terminal in the event of later modification in circuitry and they provide for re-termination to the same terminal without a short splice in case a wire breaks at a lug or soldered connection.

Shielded wire, one or more insulated conductors enclosed in a cross-hatch weave of tinned copper, is used in both radio and audio frequency applications to prevent stray radiation of RF fields and to avoid pick-up of ac hum and similar disturbing influences on audio leads. Grid wiring to vacuum electron tubes is particularly susceptible to such undesirable influences which then are amplified in the tube; microphone wiring should *always* be in shielded conductors. Frequently the shield itself is used with microphones of the "push-to-talk" variety with a built-in switch. The shield then becomes common and forms part of both the switch and microphone circuits.

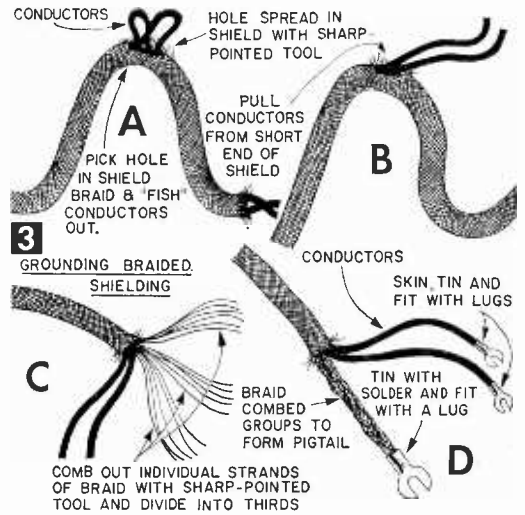
Before the advent of plastic insulated conductors, it was possible, by skillful handling, to run a small solder "collar" around the

end of the shielded braid—even include a short length of wire in the collar which could be used to terminate the shield on a chassis ground-point. This is still possible when the conductors themselves are fabric insulated, but not so with plastic which will melt completely with application of sufficient heat to the shield to permit a hot solder joint.

The answer? Well, if the shield is merely to be ended or tied-off without grounding, put a drop of liquid solder or aluminum (both applied cold) on the end of the braid and form it smoothly with your fingers to make a solid collar. Such a collar will set up hard in a few minutes and requires no heat, hence there is no damage to insulation. I use either Warner's Liquid Solder or Duro Liquid Aluminum.

As an alternate method of avoiding fray at the end of shielding, you can pinch the shield between spaghetti sleeving. The sleeve that goes over the conductors, the inner sleeve, should be a snug fit, and still capable of being pushed up *under* the shield braid; the outer sleeve must be of an inside diameter which will permit sliding over both the shielded braid and the spaghetti on the conductors.

Suppose, however, that you do have to ground the shield at either or both ends. Liquid solders are a mechanical binder only and should not be relied on for electrical connections. A far better method is to form a pig-tail directly with the end of the braid itself. This can be done neatly and effectively by following the steps illustrated in Fig. 3. First, push the shield back up the wire to form a bulge or hump in the shielding by working the braid apart. Using the same tool, pick the conductors out of the shielding, one at a time in small loops. Once you have them within easy finger grasp, withdraw them completely from the short end of the

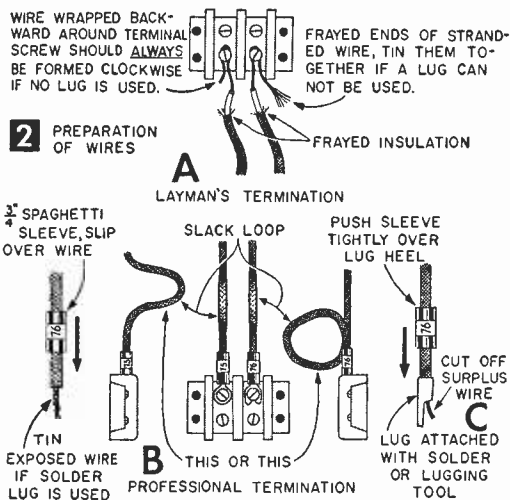


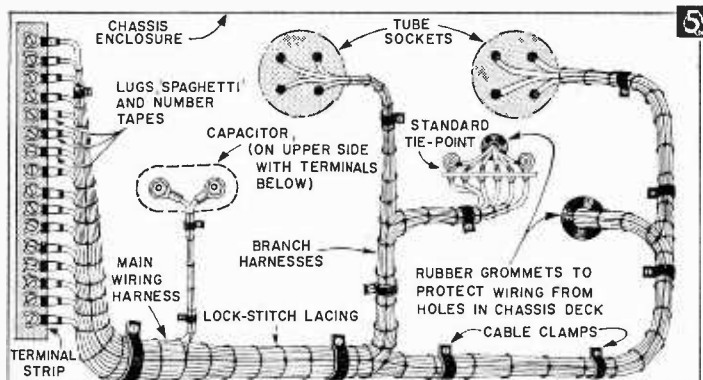
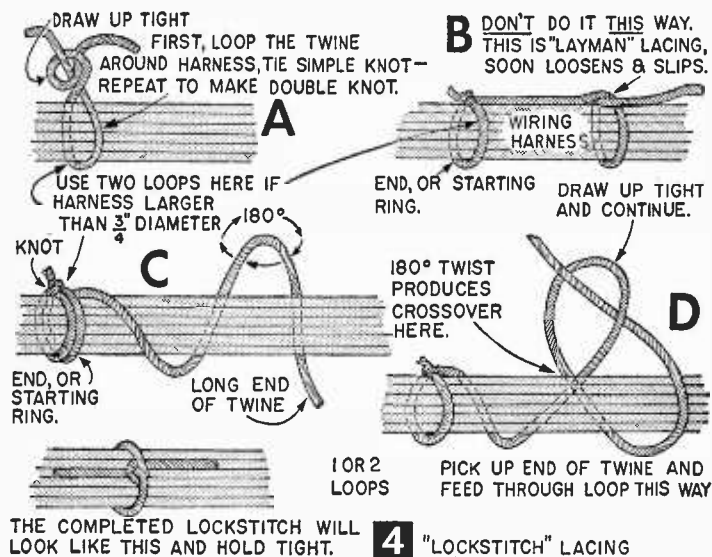
shield.

Next, separate the wires of the shield which will form the short pig-tail by using the pick or a nail to unbraids the web. Divide the resulting individual wires into approximate thirds and braid them tightly like a small girl's hairdo. Seal the end of the pig-tail with a spot of hot solder and fit it with a lug, either the solder type or solderless, as you prefer.

Cabling and Lacing. In forming your wiring prior to cabling and lacing, do not attempt to run wires from point-to-point by the shortest route. Except in a few isolated instances (high-frequency carriers, for example), whether a wire is 5 in. long or 7 in. long is of no consequence. Using that reasoning, you will be able to form your wires to follow the line of the chassis, making short, rounded 90° turns at the corners and at branches leaving the main cable harness. If, by extending some individual wire for a few inches you can include it in a main cable harness, do so. If you are careful to use shielded wire wherever the schematic you are working from specifies, or, if not so designated, wherever you are carrying radio or audio frequency such as microphone and speaker leads and wiring to the grid circuits of vacuum tubes, you'll have no trouble. See that all such shielded wires are solidly grounded to the chassis at both ends either by the pig-tail method of Fig. 3 or by small wiring clamps screwed to the chassis.

Now to the actual cabling and lacing. Obviously if you are to run in one harness a number of wires that will terminate at scattered points, each wire will be of a different length. Be sure that each is long enough or you'll have the tedious job of unlacing all of your harness to replace the short wire. You can cut to exact length when you come to the point of actual termination but better to





begin by making each wire a few inches longer than necessary.

In some instances you can completely pre-form your harness, including the lacing, right on the bench and have it fall in proper place in your chassis. Where chassis layout makes such pre-fabrication of a harness impossible, it will be necessary to place each individual wire in proper position in the chassis, routing each one carefully alongside the others with which it is to be cabled and making the final termination at each end. Hold the bundle in place temporarily with a few ties here and there to maintain the final harness form. Then, when all wiring for that particular harness run is complete, lace it in place in the chassis.

One tip on pre-fabrication: use different color wires for ready identification individually at each end of the harness. If your available wire stock is insufficient to permit this color coding, mark both ends of each wire with adhesive number tapes or tags. Some craftsmen

prefer to "ring out" each individual wire with a buzzer or an ohmmeter as a double-check, when terminating.

Professional practice dictates the use of "lock-stitch" which, while really simple, almost defies written description (see Fig. 4). Start your lacing about an inch from the main termination point of your harness . . . a connection block for instance. If it is a harness of relatively few small wires, space the twine rings around the harness about $\frac{1}{2}$ in. apart. If it is a larger number of heavier wires, 1-in. spacing will be adequate. Multi-wire harnesses of more than 1-in. cross-section can be laced every 2 in., but if 6-cord lacing twine is used it should be doubled for added strength.

A good rule to follow is to space the twine rings for a distance about equal to the dia. of the bundled harness and use the twine doubled on any harness over 1 in. Tie-off the ends, both at the starting point of the lacing and at completion, with an ordinary square knot, double tied.

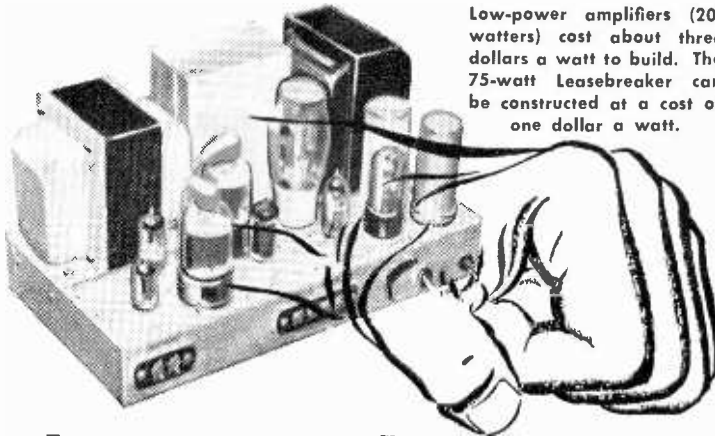
Chassis wiring by the cabled and laced method does not mean that all wires of the harness will terminate in the same area at each end.

There will be considerable branch wiring from the main harness trunk. As your lacing progresses, you reach various points where one or more wires leave the harness to connect to an adjacent component.

At this point, wrap the twin ring twice around the main harness and bend the wires leaving the harness 90° toward the terminals to which they will connect. Then proceed with your lacing to the next branch. This will result in a tapered harness (see Fig. 5).

Answers to Photo Quiz on Page 103

1. Rotary wafer switch.
2. Roll of electrician's rubber tape.
3. Pilot lamp.
4. TV lead-in stand-off insulator.
5. Top of spray can of service chemical.
6. Diagonal cutters.



Low-power amplifiers (20-watters) cost about three dollars a watt to build. The 75-watt Leasebreaker can be constructed at a cost of one dollar a watt.

little job with enough wallop to enable anyone to break his lease by popular request within three minutes! Whether or not that is your projected use for it, this amplifier will deliver—subject to rising costs and picking up a few good buys—one watt of power per dollar of construction cost.

It is an engineering maxim that when cost is an object, no element of a system should be unduly stronger, or unduly weaker, than any other. There is no sense in paying for performance that cannot be utilized. At the outset, we gained considerable simplification in design by deciding that the amplifier would be used only to handle program material and not sinusoidal signals. This is a compromise that has been used for years in the design of modulators for high power AM transmitters.

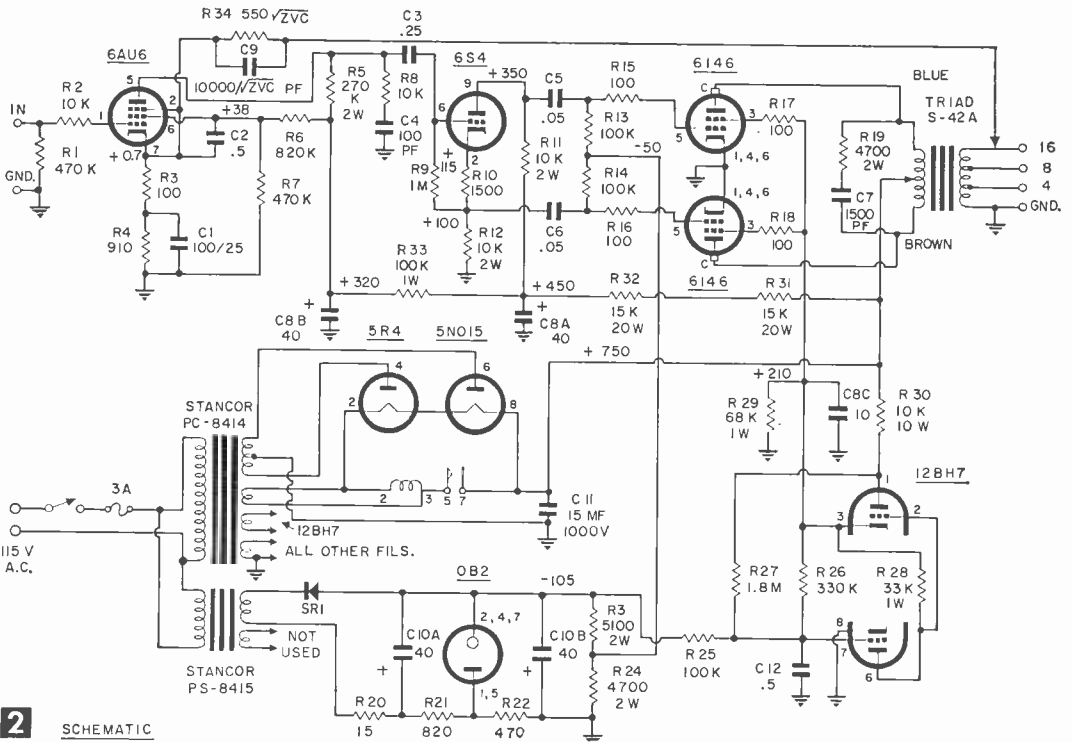
Since a sine wave contains much more average energy than does program material of the same peak amplitude, it is permissible to use much lighter components than would

The Leasebreaker

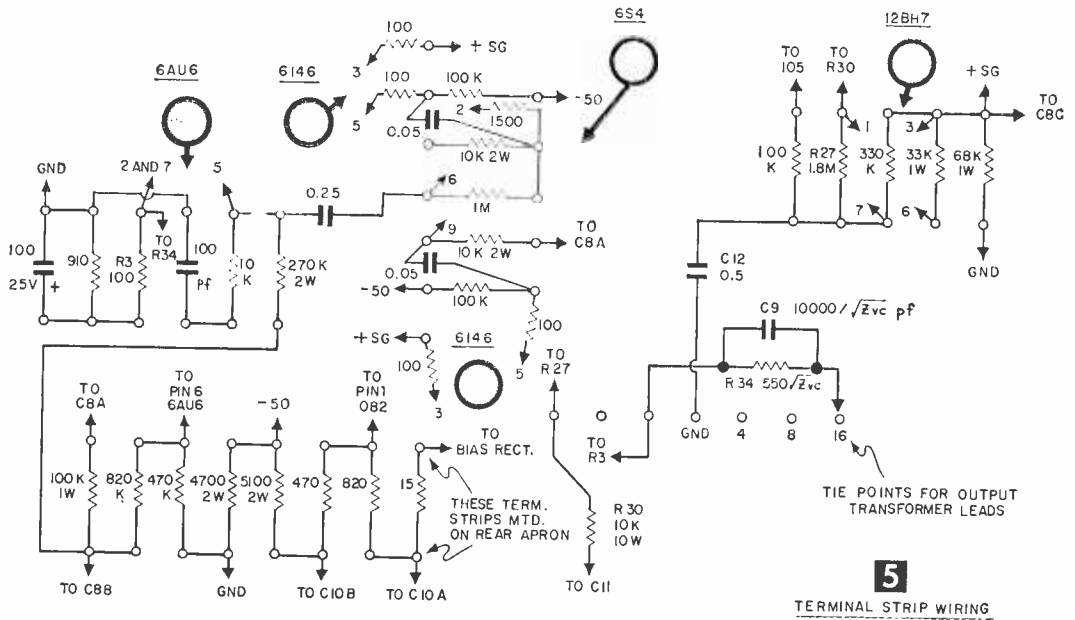
Not the perfect amplifier—that hasn't been built—but an outstanding bargain in high-power amplifiers. Net price, including tubes, is \$75—or a dollar per watt

By LEE/SHERIDAN

WHEN we decided we needed a new amplifier we knew we wanted the greatest possible power output per dollar of cost. What we achieved was a dandy



2 SCHEMATIC



between heater and contacts. We preferred the octal-based relay to the miniature for this job because the octal socket provides a longer flashover path to ground than does the miniature.

A simple bias supply is provided with a configuration which permits use of a dual 40 mfd can. An OB2 glow tube holds the bias voltage constant. With the values shown, it draws about 10 mils. Some selection of the 5100 and 4700 ohm resistors may be needed to get just exactly minus-50 volts at the tap, and these should be 2-watt units for best temperature stability.

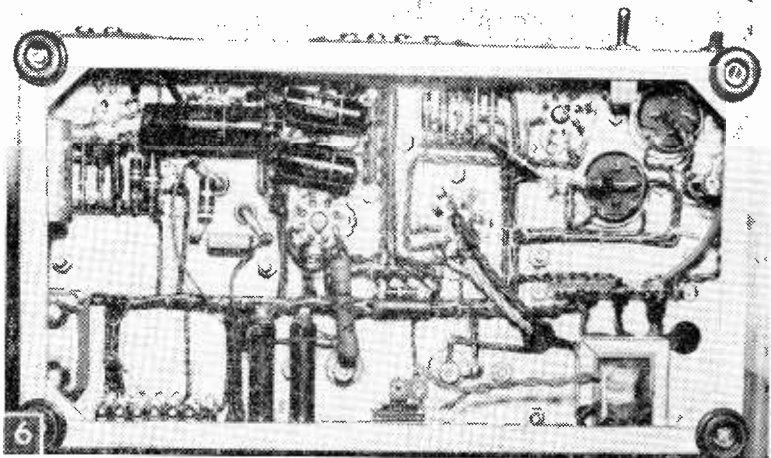
Screen regulation is an absolute necessity if maximum power is to be developed. We blithely started with VR tubes and encountered trouble! By the time the screens are stabilized the tubes are beyond their ratings when there's no signal. And there is also considerable additional heat dissipation.

So we cast about for a simple solution and came up with that shown in Fig. 2. Note that the conditions which increase the screen drain also pull down the supply voltage considerably, due to the poor high-voltage regulation.

The 12BH7 is a husky

twin triode, designed for use as a TV vertical deflection amplifier, with a 500-v plate voltage rating and a permissible dissipation of 3.5 watts per section. The two sections are connected in series, with the upper as pass tube and the lower as dc amplifier. The control voltage divider is returned to the minus-105-v bias supply, to keep the dc amplifier grid near ground, yet allow large swings.

In operation, this has proved an excellent little regulator, its output voltage being the same at full output as at zero signal, with a rise of about 10 v in the middle range. Initially, the output voltage had a tendency to drift with changes in line voltage, but the addition of R26 reduced this drift to an acceptable range. Correction is not complete, of course, because the dc amplifier does not have sufficient gain.



Bottom-chassis view of the Leasebreaker. (Photo was taken before addition of C12.)

Construction. We constructed The Leasebreaker compactly on a 2 x 7 x 13-in. chassis, and the large transformers and filter capacitor must butt against each other in order to fit (see Figs. 1, 3 and 4). Tubes and electrolytic capacitors are placed along the front, the 6146's being staggered, rather than side by side, to reduce the heat problem.

A neat terminal board effect is achieved through the use of Cinch-Jones 2000 series terminal strips mounted in parallel pairs (See Fig. 5). For the input stage, we used 2006's; a 2005 and 2007 for the phase inverter, 2005's for the screen regulator, and 2008's for mounting miscellaneous power supply resistors. This scheme is a real space saver, since tube sockets may easily be straddled.

The two 15K 20-watt dropping resistors are mounted with long screws through the back apron of the chassis. Be sure to use an insulated shoulder washer here and several insulated flat washers on each end!

Cinch type 2C7 sockets were used for the two electrolytic cans. Note that the outer contacts are tied together to make maximum use of contact area. The bias supply capacitor should be provided with an insulated sleeve, since its can is negative with respect to the chassis.

A double ground system is used to avoid hum troubles, for the charging current through the 15 mfd capacitor is quite high and can easily give trouble if it gets into a common ground bus. For this reason, a power supply ground is made right at the negative terminal of the 15-mfd capacitor to which transformers, electrolytic capacitors and 6146 cathodes are returned. A separate signal ground is made at the input terminals, to which all other grounds are returned through separate ground wires.

Good quality steatite sockets should be used, at least for the rectifier and delay relay, since these parts carry the full 750 volts.

Use an aluminum chassis, be-

MATERIALS LIST—LEASEBREAKER

Design.	Description
T1	45000 ohms plate-to-plate to 4, 8, 16 ohms (Triad S-42A)
T2	600-0-600v, 220ma; 5v, 3a; 2 x 6.3v, 3a (Stancor PC-8414)
T3	115v. 15ma; 6.3a, 0.6a (Stancor PS-8415, Triad R-54X)
V1	6AU6
V2	6S4
V3, V4	6146
V5	5R4
V6	0B2
V7	12BH7
V8	Amperite 5N015
SR1	50 ma, 115-v selenium rectifier
C1	100 mfd, 25-v electrolytic
C2	0.5 mfd, 600-v bathtub or 0.5 mfd, 400-v molded paper tubular
C3	0.25 mfd, 600-v molded paper tubular
C4	100 mmfd mica
C5, C6	0.05 mfd, 600-v molded paper tubular (matched, if possible)
C7	1500 mmfd, mica
C8	40-40-10 mfd, 450-v electrolytic (Mallory FP 376.8)
C9	10000/√Zvc mmfd
C10	40-40 mfd, 450-v electrolytic (Mallory FP-238)
C11	15 mfd, 1000-v oil
C12	0.5 mfd, 200-v molded paper tubular
(All resistors 1/2 watt 10% unless otherwise indicated)	
R1	470 k
R2	10 K
R3	100
R4	910, 5%
R5	270 K, 2 w
R6	820K
R7	470 K
R8	10 K
R9	1 meg
R10	1500 w
R11, R12	10 K, 2w matched
R13, R14	100 K matched
R15, R16,	100
R17, R18	4700 2w
R19	15
R20	820
R21	470
R22	5100, 2w, 5% } see text
R23	4700, 2w } see text
R24	100 K
R25	330 K
R26	1.8 meg
R27	33 K 1w
R28	68 K 1w
R29	10 K 10w
R30	15 K 20 w
R31, R32	100 K 1w
R33	550 √Zvc
R34	
Miscellaneous	
2	Millen #36002 ceramic plate caps
1	SPST toggle switch
1	extractor fuse holder
1	3AG, 3-amp fuse
2	Cinch #2008 terminal strips
2	Cinch #2007 terminal strips
2	Cinch #2006 terminal strips
3	Cinch #2005 terminal strips
3	Cambridge Thermionics #X2006 (or equivalent) insulated terminals
1	2 x 7 x 13" aluminum chassis
2	7-pin miniature tube sockets
2	9-pin miniature tube sockets
4	octal tube sockets
2	Cinch #2C7 FP capacitor sockets
1	Eby #56-2 (or equivalent) screw terminal strip
1	Eby #56-4 (or equivalent) screw terminal strip
1	hook-up wire, rosin solder, misc. hardware

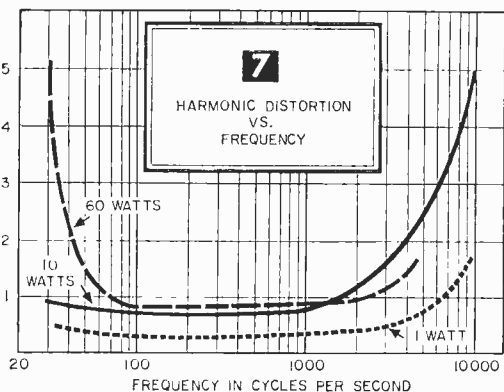
cause the high heat conductivity of the metal makes the whole chassis surface available as a radiator. While heat dissipation of this amplifier is considerably below that of most others in its power class, its compact design does keep the dissipation per unit volume fairly high. For this reason, The Leasebreaker should never be enclosed in a small space.

Testing. With the 5R4 removed, a dummy load connected and the feedback loop open, the first job is to adjust the bias. Select 4700 and 5100 ohm resistors so that the bias is minus-50 volts. If necessary, other resistors can be shunted across one or the other for vernier adjustment.

Next, if a milliammeter is available, check the current drawn by the 0B2, which should be around 10 mls. Variation of R21, an 820-ohm resistor, can raise or lower this as desired.

To set the screen voltage, replace the 5R4 and turn on the power. The high voltage at the 15-mfd capacitor should be around 750 v. Now check screen voltage. If it is not in the range of 200-215 v, shunt one of the resistors in the control voltage divider. Shunting R27 reduces the screen voltage; shunting R25 increases it. Use high values for the first try; the circuit is quite sensitive.

When screen voltage is set, the various other voltages can be checked. A VTVM should be used to measure the 6AU6 plate and screen. If results are



satisfactory, feed a 400-cycle test signal into the input and turn up its level. The amplifier should deliver 75 watts (33 v rms into a 15-ohm load) just at the clipping level as seen on a scope.

As regards the feedback loop, if the output transformer primary leads have been connected as indicated, and if the manufacturer is uniform in attaching leads to the windings, the feedback should be negative. With the oscillator providing the 400-cycle test signal set for low output, watch the output signal on a scope while touching a 22K resistor across the feedback terminals. If the output decreases, the feedback is indeed negative and the proper feedback resistor may be installed. If the output increases, reverse the output transformer primary leads and try again. It is wise to use the 22K resistor for the initial test so that if the feedback happens to be positive, the amplifier will be spared the burden of violent oscillation. Resistor R34 and capacitor C9 are chosen according to voice coil impedance (see Materials List); but explicitly:

Voice Coil Impedance	R34	C9
16 ohms	150 ohms	2500 mmf
8 ohms	200 ohms	3600 mmf
4 ohms	270 ohms	5000 mmf

With the feedback loop closed, a frequency response run at a level of about 1-v output may be made. The amplifier should be down about 0.5 db at 20 and 20,000 cycles, and should fall continuously outside of those points as discussed previously.

Note particularly—this amplifier is intended only to be flat to 20 kc, not to 100 kc! People accustomed to 100-kc bandwidth and a fancy square wave response will be disappointed by this—but our aim was a stable amplifier. This type of response is the price of using a cheap output transformer. Similarly at the low end—but it should be noted that smoothly falling response below 20 cycles is beneficial in attenuating rumble from turntables.

In checking the power output, the amplifier

should deliver 65 watts at 30 cycles and 75 watts at 40 cycles and above, at the clipping level and just before noticeable flattening appears on the scope. Full power should not be run continuously above 5000 cycles since the network across the output transformer primary begins to absorb power and the 4700 ohm resistor R19 will "head west" in a big hurry.

Instead, make quick checks at 10 and 15 kc by turning up the oscillator for no more than a second or two, reading the meter and immediately turning down the oscillator. Power should be 65 watts at 10 kc and 40 watts at 15 kilocycles.

This drooping power response does no harm to program material where the vast bulk of power lies below 1000 cycles, and the amplifier will break up at low frequencies long before the point where high-frequency power will endanger the 4700-ohm resistor.

The Leasebreaker may be used with any standard pre-amplifier, although we don't recommend that the preamp power be drawn from the amplifier, as it is very difficult to provide sufficient plate supply decoupling to make the system really stable at sub-audible frequencies. Either the preamp should be self-powered, or a separate power supply should be built for it. Voltage gain from input to 16-ohm output is 20, hence 1 v in will produce 25 watts—a sensitivity of the same order as any usual home music amplifier.

Internal impedance as measured at the 16-ohm output tap is 1.3 ohms, resulting in a damping factor of 12, which is adequate for restricting speaker hangover. Total hum and noise output with the input shorted is less than 5 millivolts at the 16-ohm tap, or better than 75 db below 60 watts output. This is predominantly power-supply ripple due to imbalance in the output tubes, but 5 millivolts of hum is so low as to be barely audible a foot from a good speaker.

Harmonic distortion was measured as a function of frequency for several power levels and the results were about what might be expected.

The low-level distortion is higher than that in units of the Williamson type, but not seriously, since any reasonable amplifier distortion pales into insignificance compared to that contributed by even the best of speakers. The curves (Fig. 7) show the usual rise at the ends of the range, the low end curve at 60 watts being due to the onset of core saturation. The high end rise, however, is only of academic interest since the 10- and 60-watt power levels will never be reached by program material at frequencies above 1000 cycles.

If you haven't seen curves like Fig. 7 before, be advised that the usual practice of using only mid-band frequencies in distortion ratings tends to make an amplifier look better than it really is.

Radio Tuner for Child's Phono

Your child can have his phono and radio, too—
all in one package

By HOMER L. DAVIDSON



Enjoyment is doubled with the addition of a radio tuner to a child's record player.

THIS tiny RF tuner can easily be attached to the young fry's record player, converting it to a radio receiver. The tuner consists of a tuned input stage with a small, variable capacitor. The separated signal is then rectified to audio power and amplified by a small transistor. From here the signal is applied to the pick-up arm and then amplified by the phono-amplifier itself.

Circuit. The RF signal is picked up from a small lead that should be clipped to an outside antenna for best results. For local stations, a bed spring or metal window frame will pick up enough signal to drive the loudspeaker. A small ferrite coil with a tunable slug and a variable capacitor separates the stations. The slug can be tuned in or out to separate several local stations if one (or more) seems to bother the desired station.

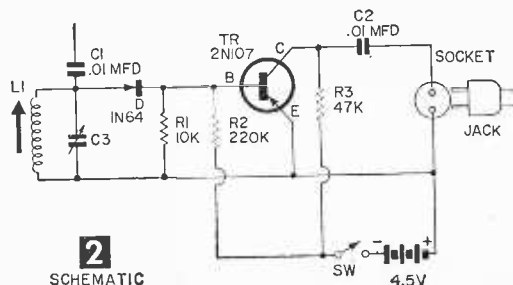
A fixed crystal diode detects the audio signal, which is then amplified by the 2N107 transistor. The transistor was added here to help amplify the weak detected signal, as some of the cheaper record players have only one amplifying tube. Since all phonographs have their own volume control, there was no need to place one upon the small tuner. Also, most record players have a tone control, but most radios do not.

A small, fixed capacitor couples the audio signal to the phono pickup arm. It is best to first remove the record player arm from the phonograph before wiring up the male jack.

Be careful not to damage the crystal cartridge by rough handling. Generally, a small pin or swivel screw holds the pickup arm to the horizontal swivel bracket. Remove this, and the arm can be taken off. Be sure to unsolder the two small wires that go from the amplifier to the pickup arm.

Phono Arm Repair. Drill a $\frac{1}{8}$ -in. hole in the middle of the phono pickup arm. This hole should not be drilled too far back on the arm because of the sharp angle in lifting the arm before the male plug is inserted into the radio tuner. Two small, flexible wires are soldered to each terminal and brought out so they can be soldered to the crystal cartridge connection. Do not solder these connections until they are pulled off the cartridge. Heat will sometimes damage the crystal cartridge. Place the connections back on the cartridge, and the arm is ready to go. Now remount the phono arm in its original position. All that you're doing is making a simple way to plug the phono amplifier into the radio tuner box.

Battery and Cabinet Construction. If your case is large enough, use two penlite cells in series or an Eveready 4.05 v. (E133) or an RCA 4.5 v. battery. Since my plastic case was only $1\frac{1}{4} \times 1\frac{1}{2} \times 2\frac{1}{4}$ in., I had to devise a smaller battery: Three small button mercury cells were used to furnish 4.5 v. of collector voltage. These batteries are the size of small buttons, and being so small, must be mounted in such a way that good contact is made. Cut the closed end from the zinc casing of a small penlite cell to a length of $\frac{3}{4}$ in. Clean out all loose carbon and residue from the inside of the cell. Cut a piece of thin cardboard long enough to just meet the ends when inserted inside of the penlite zinc case. Drop a small



MATERIALS LIST—CHILD'S PHONO-RADIO

Desig.	Description
C1, C2	.01 mfd flat ceramic capacitors
D	1N64 xtal fixed diode
C3	365 mfd miniature variable capacitor (Lafayette MS-274)
L	ferrite coil (Lafayette MS-11)
R1	10,000 ohm resistor, 1/2 watt
R2	220,000 ohm resistor, 1/2 watt
R3	47,000 ohm resistor, 1/2 watt
SW	SPST switch (Lafayette VC-42 or equivalent to fit case—such as Cutler-Hammer's type 8098-K3, Allied 348510)
TR	GE 2N107
Batt	4.5 v (see text)
plug	miniature plug (Lafayette MS-284)
jack	miniature jack (Lafayette MS-283)
	plastic cabinet (Lafayette MS-298 or other)

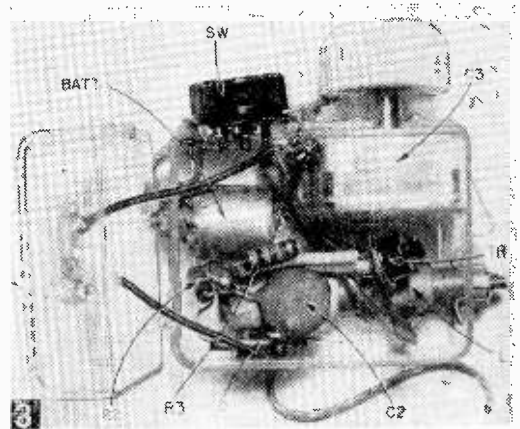
shiny split lock washer into the bottom of the case, and insert the first button battery. Insert all three batteries, observing correct polarity. The batteries will fit snugly, and should be pressed together as tightly as possible.

The center contact connector and mounting screw are bolted to a small fiber washer (see Figure 5). Use the smallest bolt and nut combination here, so that they do not touch the crimped sides.

Place the washer and bolt into the top of the battery. While pressing down on the bolt, crimp the edges of the zinc case over the top of the insulated washer. Be very careful not to touch the center post to the crimped edge, as this will short out the newly constructed battery. The little battery is ready to mount with its own mounting screw.

The plastic case I used was the container from an Argonne (Lafayette) interstage transformer. Any plastic box at least 1 1/8 in. high, but not too high to fit under the pickup arm can be used. If no other box is available, you will have to use Lafayette's MS-298 (1 1/8 x 3 1/8 x 3 7/8 in.). Drill holes for the ferrite coil assembly, variable capacitor and on-off switch. Mount the female plug atop the case. You can use the tip of the soldering iron to make the larger holes in the plastic, as long as you don't hold the iron to the case too long.

After all the holes are drilled, the large components are mounted. First, the capacitor and switch are mounted, then the battery.



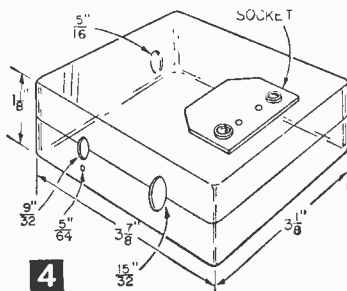
Parts layout of the RF tuner in a tiny 1 1/4 x 1 1/2 x 2 1/2 in. box. Any case you have available may be used (see text).

Before mounting the ferrite coil, solder the diode and resistor into place, and solder two small pigtails to each side. This will save a lot of close soldering down inside the case. The small resistor, capacitors and transistor can be soldered as they are mounted. While the lid is open, solder two small flexible leads to the female plug and to its corresponding circuit. The unit can now be wired. Be sure the battery polarity is observed.

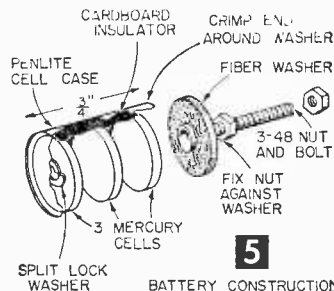
The unit is placed directly under the pickup arm and plugged into it. Turn the record player on, and let the tube heat up a few seconds. Hook an outside antenna or long wire to the small antenna wire. Then, turn on the radio-tuner. If there is hum, reverse the ac plug on the phono.

Surprising results were obtained with the small radio-tuner on local and distant stations. The batteries should last a long time, as only 1/5th of a milliamperere is pulled from them.

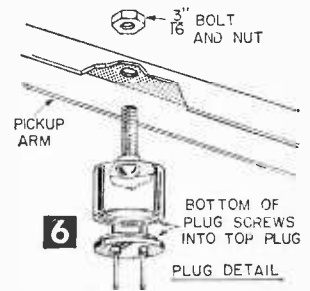
The small plastic case can now be bolted to the phonograph mounting board. Always turn the batteries off when only the record player is being used to play records. The pickup arm mounting holder can be removed or re-mounted closer toward the turntable if so desired.



4



5



6

ELECTRON TUBE ANAGRAM

Although transistors are rapidly replacing electron tubes in many applications, tubes still perform jobs that transistors cannot handle. This anagram puzzle pertains entirely to electron tube terminology.

Can you correctly fill in all the empty blocks with the correct words, letters, symbols and abbreviations? When you have the blocks all filled, check your solution with the correct one on page 152.

By JOHN A. COMSTOCK

ACROSS:

- 1) Seven-element electron tube.
- 4) A _____ cutoff tube is one in which the control grid spirals are uniformly spaced.
- 7) A gain compensating vacuum tube circuit (abbr.).
- 10) A straight line drawing across a series of plate current-plate voltage curves.
- 11) A _____ tron is a five-element tube having two plates.
- 15) Output power (abbr.).
- 16) Target (abbr.).
- 18) A vacuum tube circuit that sets up and maintains sustained oscillations. (abbr.).
- 19) A tube in which the electron stream is concentrated or "focused" for greater amplification.
- 20) To reduce this, some tubes have a center-tapped filament.
- 21) Unit of current usually applied to electron tubes. (abbr.).
- 22) A floating grid.
- 24) A cathode-ray tuning indicator tube is sometimes called a "magic-_____."
- 25) A tube noise effect that limits high amplification.
- 27) Negative potential applied to a control grid.
- 28) Interelectrode capacitance between grid and plate (letters symbol).
- 30) Part of a CRT tube.
- 32) _____ uration is the point reached when current is

maximum obtainable by increasing plate voltage or cathode temperature.

- 33) Particles heavier than electrons that are harmful to a CRT tube's screen.
- 35) A variable resistor used in many vacuum tube circuits (abbr.).
- 37) An electron tube's signal input element.
- 41) Electron flow effect in an electron tube.
- 44) The "at-rest" potential applied to tube elements.
- 46) Unit of conductance.
- 48) A cathode that emits electrons when struck by light rays.
- 49) Heater tap for pilot lamp (letters symbol).
- 51) _____ = $R_p \times G_m$ (supply missing term).

52) The alkali earth metal introduced into a vacuum tube to remove residual gas.

53) $u = \frac{dEp}{?}$ (supply missing term).

DOWN:

- 1) A _____ -wave rectifier has only one plate.
- 2) Electron receiving element.
- 3) $u = \frac{?}{dEg}$ (supply missing term).
- 5) A _____ ode tube is one having a total of six elements.
- 6) The ratio of a small change in plate voltage divided by a small change in plate current (letters symbol).
- 7) A particular vacuum tube element.
- 8) A tube envelope designation (abbr.).

9) Electron tube emitting element (abbr.).

12) Plate potential (letters symbol).

13) The name of the grid that was added to triodes in 1929.

14) _____ = $\frac{dIp}{dEg}$ (supply missing term).

17) The name of Lee de Forest's triode tube.

19) The ones used on most octal tubes are of Bakelite.

23) A unilateral vacuum tube circuit (abbr.).

26) Made to determine whether or not a tube is good.

29) Tube connectors.

31) Plate capacitance letters symbol.

34) A tube's second grid (abbr.).

36) A tube base having eight equally spaced pins and a central aligning key.

38) A _____ cutoff tube is sometimes called a "supercontrol" tube.

39) The vacuum tube invented by Fleming.

40) A tube that doesn't contain gas (abbr.).

41) C-bias voltage (letters symbol).

42) Cathode current (letters symbol).

43) An inert gas used in some gaseous electron tubes.

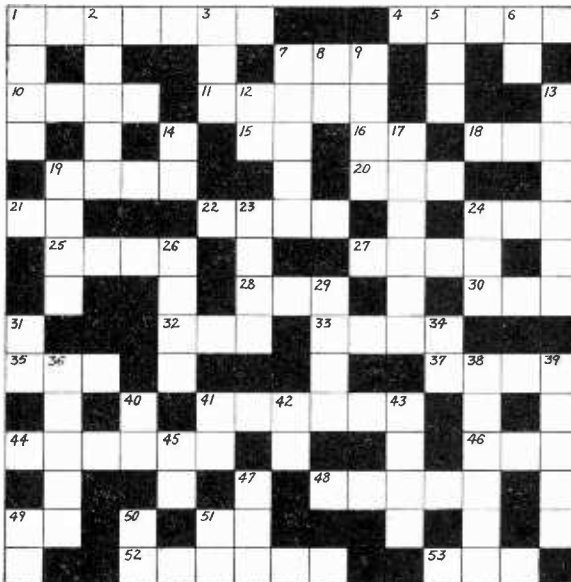
45) Plate current flow (letters symbol).

47) A remote _____ off tube is a variable μ tube.

49) Heater mid-tap (letters symbol).

50) Grid conductance (letters symbol).

51) Shell designation: metal tube (letters symbol).



What to Listen for on Short Wave

Fall & Winter 1960

By C. M. STANBURY II

WINTER on short wave presents a paradox, an important one for the listener. As you probably know, ionization (caused when ultra violet radiation from the sun passes through the atmosphere) is responsible for both the reflection of radio waves back to earth (essential for distant reception) and the absorption (weakening) of radio waves, especially frequencies below 7000 kc. Also commonly known, during winter with shorter days and rays from the sun received more obliquely, ionization is reduced, signals are stronger, and reflection from the ionosphere should decrease at higher frequencies. The latter is *not* true. Frequencies above 15 mc are normally reflected by the F2 layer, the uppermost portion of the ionosphere, and reflection in this region is actually improved as the earth approaches its winter solstice, the point in the earth's orbit when it is closest to the sun. Why? We don't know and neither does anybody else. Some researchers have linked this phenomenon with temperature but the theory appears to have holes in it.

In any case, the result is a broader range of usable wavelengths with both higher and lower frequencies open. However, there is a second factor to consider, sunspots. Ionization, reflection and absorption all vary directly with the number of "spots" on the sun and right now we have a dropping count. Result, the higher frequencies will be slightly poorer than last winter, but low frequencies will be better. Add to this little or no static on downstair channels and you have prospects for an excellent short wave season.

We should say excellent for the serious listener. If you read the article *Tune In On The World* in Radio-TV Experimenter #565, you may recall that I suggested that one way to know other countries was to listen in on local broadcasts intended only for the area from which they originate. This is usually not easy. But many countries do use the lower short wave frequencies for such purposes, particularly in the tropics and in such a country as Russia where one transmitter must cover a good many square miles of sparsely populated territory. Of course you'll still face a language barrier. Which leaves the music. However this is sometimes more revealing than words particularly when the words are propaganda while the music is not too polished folk music.

With reception of local broadcasters as



Verification card from Radio Clube de Mocambique, a semilocal (regional) broadcaster heard throughout the World on 11760 kc. However, as indicated on reverse side of card, this QSL is for reception on the Broadcast Band during the peak period for lower frequencies, 1953-55. Winter 1960 will represent the very early stages of another such period.

МОСКОВСКОЕ РАДИО

Адрес: Москва, Радио Тел. № _____

Moscow, USSR
July 24, 1958

G.M. Stanbury II
Box 218
Crystal Beach, Ontario,
CANADA

Dear Mr. Stanbury,

Thank you very much for your reception reports on our Sputniks.

Enclosed please find a verification card as well as a Sputnik badge, as a souvenir.

Under separate cover, we are sending you a copy of the magazine "Soviet Union" in which you can find the information about Sputnik III.

Hoping to hear from you again,

Sincerely yours,
E. Stepanov
(Luena Stepanova)

RADIO MOSCOW
North American Service

Verification letter for Sputniks I and III (no longer broadcasting) heard at 20.005 mc.

the goal, frequencies below 7000 kc. become all important and a dropping sunspot count can be nothing but good news. How far has it dropped? Well, the count has a long way to go but even in April two stations in the 120 meter band, H13C (2440 kc, La Romana, Dominican Republic) and Radio Martinique could be heard throughout the eastern United States.

International Broadcasting. If you're new to short wave listening, or you just plain want to listen and keep DXing down to minimum, then the International Bands, 31 through 13

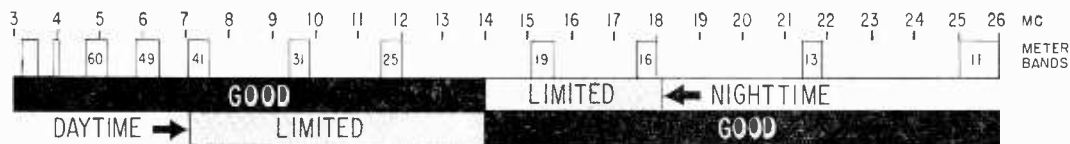


TABLE A: BEST BANDS BY NIGHT AND DAY

meters (see Table A) will interest you most. That boost in the F2 layer will certainly make things better than in the summer. But reception will be slightly poorer than last winter.

The 13 meter band will be open many days to all parts of the world with north and south paths having an edge. Europe will be best during daylight hours on the 19 and 16 meter bands and then at night on the 31 and 25 meter bands. Africa will follow a roughly similar pattern. The 19 and 16 meter bands may remain open the first few hours of darkness with both Europe and Asia received. Such a path will occasionally hold up most of the night with the 25 meter band providing an alternate band for evening reception of the Orient. During the hours after midnight both 25 and 31 meters will produce signals

from Asia and the Pacific. Technically this would be the best time for such listening but most broadcasts to North America are made during the more convenient evening hours: Thus 19, 25 and 31 become bands for all parts of the world with the latter pair most dependable.

Possibly you gathered from these predictions the increasing importance of 31 meters. As the sunspot count continues to drop it will become almost irreplaceable in international broadcasting. Unfortunately, it may have to be replaced. Crowding on this band is fast reaching an intolerable saturation, even for the comparatively hardy SWL. As an example, listen to the 15 kc spread between 9585 and 9600. During the evening we have no less than 5 transmitters in this tiny portion of the radio spectrum, Radio Canada (CKLP), Radio

Nederland, Radio Cultura de Bahia (ZYN 29), Radio Moscow, Radio Republik Indonesia (YDF6) and the British Broadcasting Corp. (GRY). Of this group, ZYN29 and YD F6 would be the newer, and it is this continuous stream of new tropical stations coming on the band which is mainly responsible for such overloaded channels. Of course they have as much right here as any other country.

The International Telecommunications Union is taking steps to alleviate this situation but the ITU does not have enforcement powers.

If the malady is not cured, or at least arrested, broadcasters will either have to concentrate on 25 meters, in which case that band might soon look like 31, or switch their programs to less advantageous afternoon periods.

TABLE B—GOOD SHORTWAVE LISTENING

COUNTRY	FREQUENCY IN KC/S	TIME* (EST)	STATION AND DETAILS
WINDWARD ISLANDS	3365, 15085 5010	1600-2115 1600-1730	West Indies Broadcast Service. Here we have the happy circumstance of a semi-local broadcaster using an international band (after 7:30). This one intended for the Caribbean Federation (British West Indies) features a variety of local programs which are a blend of British, Caribbean and American cultures.
MOZAMBIQUE	11760	2230 until fadeout	Another semi-local program in international territory. This will give you a good idea what the English and Afrikaan (Dutch) of Central and South Africa consider entertainment. Programs do not include news. Reception will be best on the Pacific Coast.
CONGO REPUBLIC	11725	2100-2145	Radio Brazzaville. African news from a French point of view. Also French music and French lessons.
ISRAEL	9008 (or 9725)	1530-1600	Kol Israel (or Kol Zion), Zionist picture of Near East news, limited amount of folk music.
SWITZERLAND	11865, 9535 and 6165	2030-2215 and 2315-2400	Swiss Broadcasting Corporation. Neutral international news (government) followed by democratic West European viewpoint from Swiss newspapers. Has sunspot report once a month.
NETHERLANDS	15220 (or 16 meters) 11755 and 9590 (or 9715)	1615-1705 2130-2210	Radio Nederland. Most interesting features here are international news and topical talks.
GREAT BRITAIN	Several frequencies throughout the bands	1600-2200	General Overseas Service, British Broadcasting Corporation. Good example of conservative British programming and thought.
JAPAN	17855, 15235 and 11705	1930-2015	Radio Japan. Features on Japan and a limited amount of Japanese folk music.
AUSTRALIA	11710 11810	0714-0845 1014-1145	Radio Australia. Most important feature here is news from the fifth continent. Remainder of program is primarily entertainment.
ARGENTINA	9690 (or 15345)	2200-2300 and 0000-0100	R.A.E. Compare the polished Argentine music with the more interesting Latin varieties easily heard on 49 and 60 meters.

* Time is given on the 24-hour clock. 1200 is 12 noon, 1300 is 1 pm, 2400 is midnight, and so on. In other words, for times past noon subtract 1200 to get Eastern Standard Time.

† Frequencies listed in brackets are alternate possibilities. If you fail to hear a program on the channels listed first, try these.

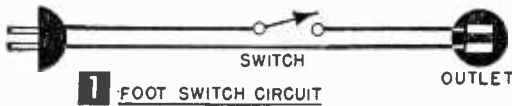
Handy Foot Switch

A FOOT switch on your table saw or drill press may limit the damage that can occur in the event of an accident. A foot switch comes in handy at the telephone to mute a blaring radio or near your easy chair to kill TV commercials. There are uses for the foot switch in the kitchen, too.

There are several types of switches that may be employed for foot switch duty. Several commercial foot switches, some of them in the form of a mat, are available. But these switches are rather expensive. You can make your own from inexpensive basic switch units, enabling you to choose according to your power and function requirements.

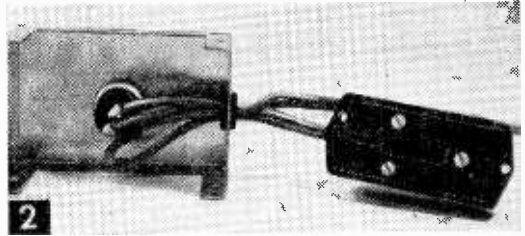
You'll want either a positive action switch, which remains on once you switch it, or a momentary contact switch, which is only on when you hold it on. A positive action switch may be desirable for a foot switch for your wife's electric mixer; a momentary contact switch is desirable for power tools since the natural tendency in an emergency is to release the switch.

Power handling ability is important too. Switches are rated by volts and amps rather than by watts. To determine the amperage of an appliance, divide the wattage of the device by the voltage, usually about 120. Thus, the switch required for a 600 watt appliance must have at least a 5 amp. rating at 120 v. Another point to remember is that switches

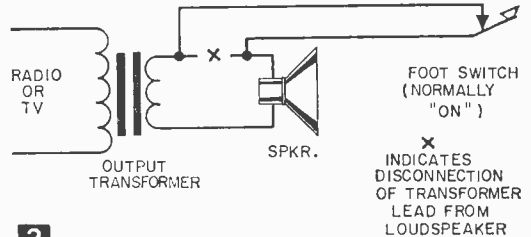


are rated for resistive loads. Devices which involve coils or capacitors (for example, anything containing a motor) usually demand currents in excess of the current computed by this method. It's usually desirable to use a switch that can handle more current than the controlled appliance requires.

The circuit for a practical foot switch is shown in Figure 1. The SPST switch is connected in one side of the ac line. A plug is provided for easy connection to any ac outlet. A receptacle is provided so that the switch may be used to control any or several appliances. The back view of the unit is shown in Figure 2. The switch is housed in a small metal box. A 1/2-in. hole drilled in or near the center of the front side of the box is required for the switch. A 3/8-in. hole is needed in the end of the box for the line cord. Insert a rubber grommet in the end hole. Double a convenience outlet extension cord on itself near the outlet end, and push the doubled end



Chassis view of switch before attaching back.



3 SPEAKER MUTING FOOT SWITCH

Speaker muting foot switch. X indicates disconnection of transformer lead from loudspeaker.

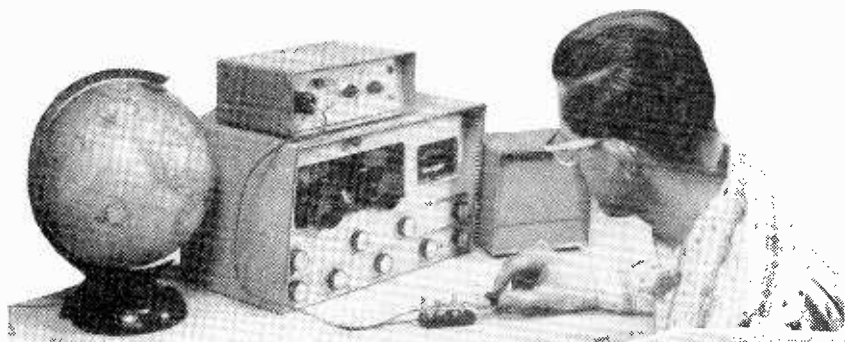
through the grommet into the metal box. Mount the switch, separate the parallel conductors, and connect them and solder. Wrap tape around the cord next to the grommet on the inside of the metal box as a strain relief. The box may be fastened to the floor with four small brackets attached to the sides. The connection to the line and to a specific power tool can be made permanent, too. If current exceeds 5 amps, a permanent installation is desirable.

Several switches are listed in the materials list. Pick the one that suits your function and current requirements. Note that you can obtain a normally on switch which will turn off when you place your foot on it. This type of switch placed near the phone with radio or TV set connected to the outlet is handy for turning either of these blaring contraptions off during a phone conversation. An alternate scheme which utilizes a normally on switch to mute the audio on a TV set from your easy chair during commercials is shown in Figure 3. In this case the switch is connected in the speaker coil circuit and does not control high voltages or currents.—FRANK WOODS, JR.

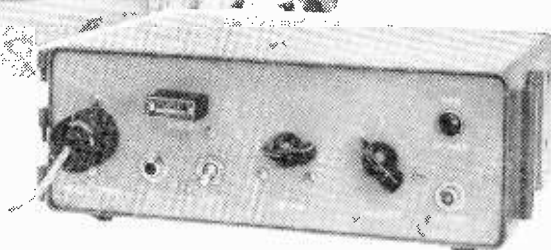
MATERIALS LIST—FOOT SWITCH

No. Req.	Description
1	switch, either a momentary contact type, such as 1/2 amp. normally off (Grayhill 4001) or 1/2 amp. normally on (Grayhill 4002) or 10 amp. normally off (Grayhill 2201) or 10 amp. normally on (Grayhill 2202) or a positive contact type, 4 amp. push on-push off (Carling 110-SP).
1	3/4x2 1/8x1 5/8" metal box (Bud CU-2101)
1	convenience outlet extension (electrical or variety store)

Transmitter for the Novice



Novice transmitter shown here atop a Knight-Kit receiver, is powered by an external power supply, permitting fixed or mobile use. Inset shows closeup of transmitter face.



By ALICE ROLF, KN5SEL

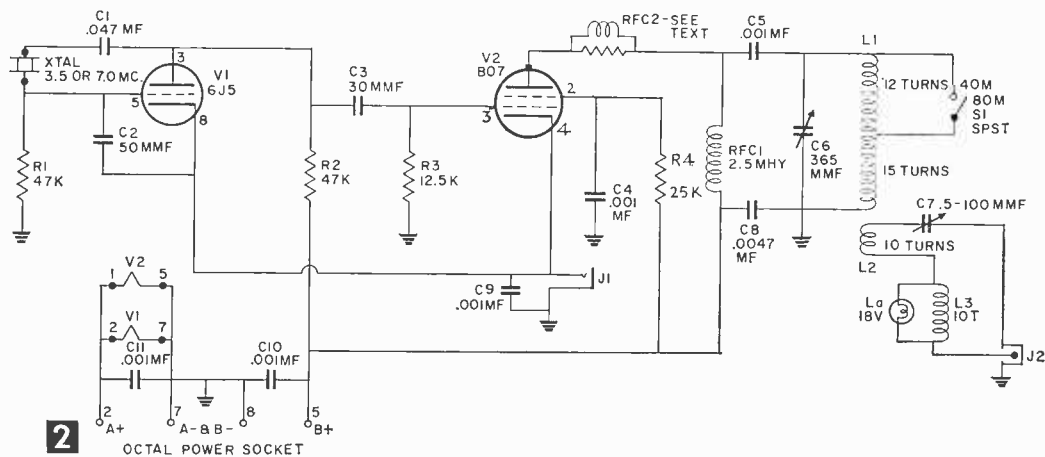
HERE'S a compact 75-watt transmitter that even a Novice YL can build. In fact, a Novice XYL did build it after her husband drilled the panel and took over as babysitter. The rig puts out a good signal on 40 and 80 meters, featuring bandswitching, and can be used either at home or in the car with a suitable power supply.

The two-tube circuit shown in Fig. 2 fits into a U.S. Army 30 cal. ammunition tin, available at surplus stores. The 3¼ x 6¾ x 10¼-in. cabinet is modern enough to enhance any shack, and small enough to fit comfortably under the dash of even a foreign car. If an ammo tin is not available, the circuit can easily be enclosed in a small commercial

metal cabinet available from radio supply houses.

The transmitter is built in a 5¾ x 9¾-in. hardboard chassis, with a 3¼ x 10½-in. metal panel bracket-attached. Use two brackets of any convenient size and sturdy enough to support the panel, which extends about ¼-in. below the Masonite.

Drill all the panel holes before fastening the panel to the chassis. The power socket, key jack, band switch, tuning capacitors, dial light jewel, and antenna jack mount on this panel, the remainder of the components mount on the chassis. The 807 socket mounts on an aluminum bracket 1¾-in. high at the right-rear of the chassis, leaving plenty of



MATERIALS LIST—NOVICE TRANSMITTER

Desig.	Description	Desig.	Description
C1	.047 mfd 200 wv tubular	R1	47,000 ohm, 1/2 watt
C2	50 mmfd mica	R2	47,000 ohm, 1 watt
C3	30 mmfd mica	R3	12,500 ohm, 10 watt
C4	.001 mfd 1 kv, disc	R4	25,000 ohm, 10 watt
C5	.001 mfd 1.5 kv tubular	S1	SPST toggle switch (Arrow-Hart & Hegmen #20994NV)
C6	365 mmfd single gang broadcast type variable (Philmore)	V1	6J5 vacuum tube
C7	5-100 mmfd variable (Bud MC 1873)	V2	807 vacuum tube
C8	.0047 mfd 1 kv, disc	Xtal	80- or 40-meter crystal—for Novice band 3750 KC to 3800 KC (80 M) or 7150 to 7200 KC (40 M)
C9	.001 mfd, 1 kv, disc	20	6-32 x 1/4" machine screws and nuts
C10	.001 mfd, 1 kv disc	10	#8 terminal lugs
C11	.001 mfd, 1 kv, disc	2	single lug terminal strips
J1	phono jack, single circuit (Mallory)	1	dial lamp jewel
J2	miniature coax jack	1	ceramic octal socket (6J5)
L1	27 turns #22 enameled close wound on 1" form, tapped 15 turns from bottom	1	5-prong socket (807)
L2	10 turns #22 enameled close wound over top half of L1	2	octal wafer sockets (xtal and power sockets)
L3	10 turns #22 or #18 enameled close wound 1/2" form	1	octal plug (for power cable)
La	#1455 18-V pilot lamp	1 pc	hardboard 3/4 x 5 x 10" (chassis)
RFC 1	2.5 mhy, 100 ma RF choke (National)	1 pc	1/16" steel or aluminum 3/4 x 10" (panel)
RFC 2	parasitic choke or 5 turns #22 or #18 enameled wound on 50-ohm, 1-watt resistor	6 ft	4-wire rubber insulated cable (insulated for 1000 volts)

room for the 807. Place the tank coil between the panel and the 807 (Fig. 3).

Mount the socket for the 6J5 on the left side of the chassis. Clip the mounting saddle of the socket away with a pair of snips and drill holes in the hardboard so that the socket solder lugs extend through the chassis. These holes are aligned by first drilling the key hole for the key pin of the 6J5. Put a drop of finger-nail polish on the pins of the 6J5 and press it against the chassis with the key in the drilled hole. The polish will mark hole locations. After drilling, press the lugs into the holes until the socket is flush with the chassis. Bend the lugs back so that they lock the socket in place.

Mount the remainder of the components on #8 terminal lugs which are fastened to the hardboard by 6-32 x 1/4-in. machine screws—except for the two connections of RFC1. This choke is mounted on two single lug terminal strips in order to isolate the high RF potentials from the metal cabinet. Parts layout is not critical, but should be similar to that shown in Fig. 3.

Extend a length of #12 wire across the front of the chassis and ground it to the panel for a ground bus bar. Connect the 807 mounting bracket to this bar. All ground leads should be connected to this bus, the panel, or the 807 mounting bracket.

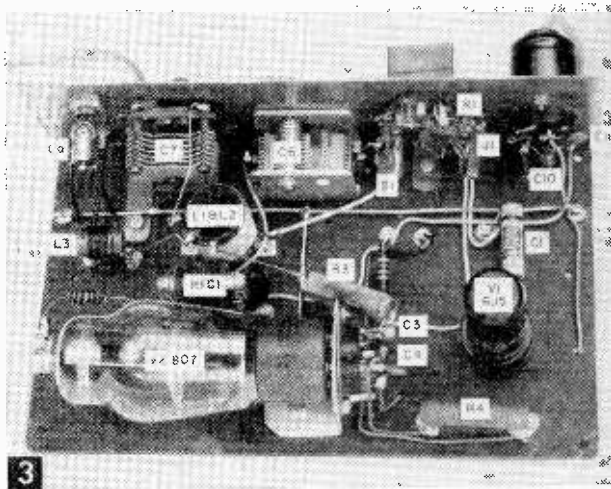
Connect the leads to the 6J5 socket and bring them to the top of the chassis through holes drilled around the tube socket. Indicator lamp terminals must not be grounded; they are supported by two pieces of solid wire.

Coils L1 and L2 are #22 enameled copper wire wound in a 1-in. dia. form. This form can be a commercial unit with mounting brackets, or a cardboard or plastic tube 1 1/2-

in. long. L1 is wound with the connection for C5 at the bottom of the form, nearest the chassis, and the ground connection at the top.

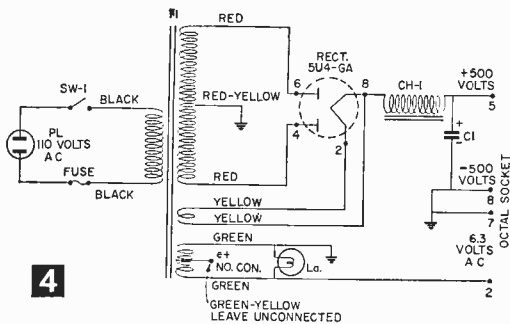
The tap for the bandswitch is placed 12 turns from the bottom of the coil. Twist the wire into a loop for the bandswitch connection and wind the other 15 turns. Coil L2 is wound over the top of L1 between the bandswitch tap connection and the top of the form. Wind it over a layer of Scotch tape with the connection to C7 at the top of the form.

Coil L3 consists of 10 turns of #22 or #18



Components are mounted on terminal lugs, the 807 socket is mounted on an aluminum bracket and the 6J5 socket mounts similar to sockets in printed circuitry. A wafer-type octal socket is used for the crystal.

enameled wire close-wound on a 1/2-in. form; RFC 2 can either be a commercial parasitic choke of five turns of #22 or #18 enameled wire wound on a 47 ohm, 1-watt resistor. For the antenna jack (J2 in Fig. 2) use a miniature connector jack of a coax type.



4

Power supply for novice transmitter.

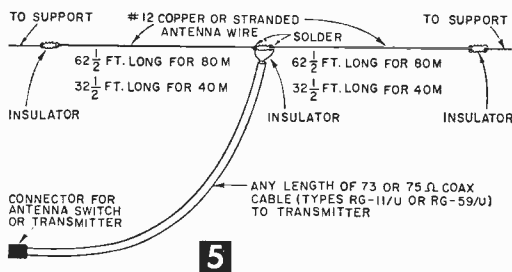
POWER SUPPLY PARTS LIST

Desig.	Description
C1	12 mfd. 700 W.V.D.C. electrolytic capacitor (Cornell Dubilier BRH 712, or equiv.)
CH1	7 or 8 hy. 200 to 250 ma. filter choke (Thordarson 20C56, or equiv.)
Fuse	3 amp fuse, with holder
La	#47 pilot lamp, with holder
PL	Line cord, heavy duty
SW1	SPST switch (On-Off switch)
T1	1200 volt c.t. @ 200 to 260 ma. power transformer with 5 volt, 3 amp, winding; 6.4 volt, 3 amp, winding. (Stacor PC-8414, or Burstein-Applebee Co., Kansas City, special #3B164, or equiv.)
Rect	5U4-GA tube
Misc:	2 octal sockets, chassis, mounting screws, etc.
Note:	BA #3B164 transformer has 350 volt tap, at 10 ma, and 5 volt, at 2 amp., windings in secondary. These should be left unconnected if the unit is used.

Use a 3- or 4-wire cable to connect the transmitter to the power supply. The power supply should be capable of delivering from 500 to 750 *v* at 150 *ma* for plate voltage, and 6.3 *v* at 1.2 *amps* filament voltage. For fixed use, an inexpensive full-wave rectifier circuit will work. For mobile work use a dynamotor or heavy duty vibrapack. At 500 *v*, the input will be about 50 watts; with 750 *v*, about 75 watts. A power supply circuit which will serve well is shown in Fig. 4.

Test the Unit on a non-metallic surface before putting it in the cabinet. Plug in the power cable, key, and a 40- or 80-meter crystal. Switch the bandswitch to the band the crystal operates in. Remove the 807 and turn on the power supply. After the tubes have had time to warm up, key the transmitter and listen for the oscillator signal with a shortwave receiver. If nothing is heard, check the oscillator wiring and try a smaller value for C2.

If the oscillator is working, turn off the power supply and insert the 807. If the power supply does not have a bleeder resistor, short the B-plus to ground before replacing the 807 or handling the chassis to avoid shock. Connect a 60-watt light bulb to the antenna terminals and again turn on the power. Place C7 at about half scale and rotate C6 while holding the key down.



5

Antenna recommended for use with novice transmitter. Should be as high and clear of obstacles as possible. Solder inner conductor of coax cable to one side of center insulator, and outer conductor to other side. Tape cable to insulator to relieve strain on soldered joints. Ground outer conductor of cable at the transmitter.

With C6 at about half scale, the indicator lamp and the 60-watt lamp will show some sign of output. Adjust C6 and C7 until the indicator lamp (La) glows brightest. Check the plate of the 807; if it is red, replace C3 with a 50 *mfd* capacitor. This will increase the drive from the 6J5 and allow the final tube to run cool.

If available, a grid-dip meter (or an absorption frequency meter) should be used to check the transmitter's frequency and harmonic output at twice the crystal frequency, and to note the keying characteristics. If carefully constructed, the rig will be clean.

After the transmitter has been tested, place it in the cabinet. Before doing this, however, drill a number of 1/2-in. holes in the rear of the cabinet and directly above the 807 tube location for ventilation. Then cement a piece of thin Bakelite plastic or three or four layers of "Saran Wrap" to the bottom of the cabinet to insulate the screw heads and 6J5 socket lugs from the cabinet's metal bottom. Secure the unit in the cabinet with two small wood screws on the underside which fasten into the Masonite chassis. Cement rubber feet on the cabinet to avoid scratching surface on which unit stands.

The transmitter will work with most types of popular amateur antennas. We had good results with the antenna rig shown in Fig. 5. The ground lead of the antenna connection should be connected to a good ground. Capacitors C6 and C7 are adjusted until the indicator glows brightest. At this point the transmitter is loaded, and with a good antenna, is capable of working just about any station within range that can be heard on either 80 or 40 meters.

On 80 meters, the daytime range is 50-75 miles and night range is 800-900 miles with 40 to 75 watts input. On 40 meters, with the same input, daytime range is about 200 miles, night range is several thousand miles.

Amplification Amplification Amplification

The simple "control-impedance" principle explains this vital, modern process

By C. F. ROCKEY

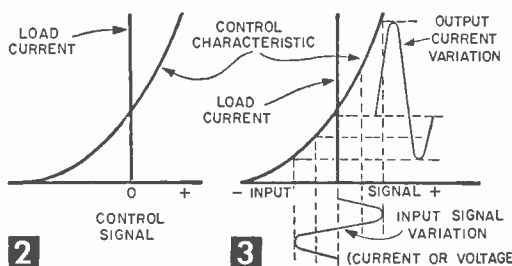
NOT all amplification is electronic. Fundamentally, amplification is any process in which a great amount of power is controlled by a lesser amount. The throttle valve of an automobile, through which the full power of a several hundred *hp* engine is controlled by the touch of a toe, is a crude amplification system.

Because electronic amplification first found wide use in radio, however, this process is firmly linked with electronics in most people's minds. Although technicians frequently speak of "current amplification" or "voltage gain," the most fundamental form of amplification is *power* amplification:

$$\text{Power Amplification} = \frac{\text{Power Output}}{\text{Power Input}}$$

Power Output refers to the large amount of power being controlled; Power Input, the much smaller amount of power that does the controlling. Often, in industrial usage, the power input may be called the "control signal." Both quantities in the fraction may be in ergs per second, joules per second, kilocalories per second, horsepower, or other power units, but *watts* or *kilowatts* are most widely used in electrical systems. Since both numerator and denominator must be expressed in the same units, it is seen that power amplification is a dimensionless, "pure ratio," without units in itself.

Power amplification is considered most fundamental here because neither current nor voltage amplification can occur without the simultaneous occurrence of power amplification. This is the case in the vacuum tube, the transistor, the magnetic amplifier, and all other true amplifying devices used today. For instance, although a transformer can readily step up electrical voltage, it does so at the expense of a proportionately decreased amount of available current. Therefore the power available for exerting any useful func-



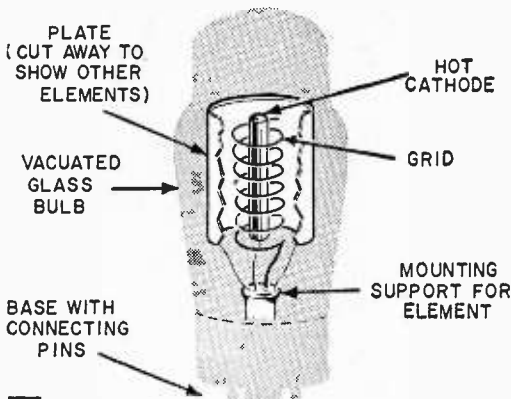
tion has not been increased, and in practice it is usually decreased slightly. Thus a transformer, in itself, is not an amplifier.

The basis of all amplification is control. No amplifier generates power, it merely makes it possible for a small amount to control a large amount. Thus the essence of an amplifier is what engineers call a *control impedance*, a device whose ability to pass electric current is at the direct command of a small control signal—a relatively small electrical current or voltage. In Fig. 1 the input control signal is shown as an alternating voltage generator and the supply voltage as a direct-current source, but this is by no means always the case. Amplifiers may be made to work with either *ac* or *dc* signals or supply sources. All that is needed fundamentally is an input or control signal, a control impedance, a relatively large power source, and a load. The *load* (represented in Fig. 1 as a resistor) may be an electric motor, solenoid coil, transformer, lighting circuit, loudspeaker, radio transmitting antenna, heating coil, or any other device capable of applying electrical power to a useful function.

The high-energy source in the output circuit of an amplifier causes a steady current to flow through the control impedance and load, normally, even when no control signal exists at the input terminals. When the input control signal, either voltage or current as the case may be, increases, it decreases the opposition which the control impedance offers to the flow of current from the high-energy source, and more current flows through it and the load. The load then consumes more power, normally, in proportion to the input signal. If the control signal decreases to zero, the current supplied to the load decreases to its resting value.

Now, should the control signal reverse in





4

polarity, it will increase the opposition to current flow in the load circuit, causing the load to consume less than the resting current value. The control signal at the input terminals directly regulates the internal opposition to current flow by the control impedance. Since the power supplied to the load is the product of the current flowing through it times the voltage across it, changing its current supply directly affects the power consumed by the load. And because the load current is a function of the input control signal's intensity and polarity, power amplification is the result.

The **control characteristic** is a graph (or curve, as engineers call it) relating output or load current to input signal magnitude. Although the control characteristic of tubes, transistors, or magnetic amplifiers may be quite irregular in practice, it is represented in Fig. 2 as a smooth, gradually curving line. The output current magnitude is found on the vertical, the control signal magnitude on the horizontal line.

To show how an engineer uses the control characteristic to predict the behavior of a control impedance as an amplifying device, a hypothetical alternating-control signal is projected in Fig. 3 upon the characteristic curve's horizontal axis.

Note in Fig. 3 that there is a specific value of load current for each instantaneous value of control signal magnitude. Thus the output or load current is under constant, direct control by the input signal. And, since the output or load power may be large in comparison with the input signal (sometimes several hundred times larger), we have true *amplifying* action.

The exact shape of the control characteristic may be of the utmost importance to the engineer. For instance, where voice, television, or music signals are being amplified, it is essential that this curve be a nearly straight line. Otherwise, the output current will not resemble the input signal, it will be

distorted. In certain scientific or industrial applications, accurate reproduction of the input signal by the output current is not necessary, and more efficiency can be secured by purposely distorting it. Then a highly curved control characteristic is advantageous. Other problems, such as feedback from the output to the input of the system may sometimes arise to complicate the designer's plans for a successful amplifier.

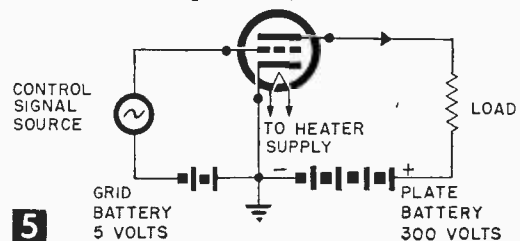
The earliest, highly successful control impedance applied to electrical amplification—the device still called “the king of amplifiers”—is the three-element vacuum tube. First made for “wireless detection” by Dr. Lee DeForest in the early 1900's, the vacuum tube was the amplifier until 1947.

The **triode vacuum tube** consists first of all of a bulb full of nothing; that is, an evacuated envelope. Placed within this envelope is an electrically heated wire or metal tube called the cathode. When heated to a red, or higher temperature, the cathode boils off millions of negatively charged electrons. Surrounding the cathode is a spiral of wire called the grid. Finally a (frequently) cylindrical electrode, called the plate is mounted coaxially with the cathode and grid, and outward from the latter, as shown in Fig. 4.

Vacuum tubes of myriad shapes and sizes have been made and used since about 1908, but the one diagrammed in Fig. 4 illustrates the principle as well as any. The connections of a basic triode vacuum-tube amplifier circuit are diagrammed in standard schematic symbols in Fig. 5. For simplicity, batteries are shown as the *dc* supply sources, but they are seldom used in modern practice. Instead, an electronic power supply, operating from the commercial power line is most often substituted. Basic principles remain the same.

When the cathode of the vacuum tube is heated, clouds of electrons collect about it. When a positive potential (positive with respect to the cathode) is placed upon the plate, the negatively charged electrons are attracted to it, and current flows between cathode and plate, around through the load and plate battery and back to the cathode. These electrons must, however, pass between the wires of the grid enroute to the plate.

Normally, the grid is connected to a slightly negative *dc* potential, and this causes it



5

THE HYBRID COIL

One most interesting modification of the amplifier exists. Although it is an old idea, comparatively few people are aware of it.

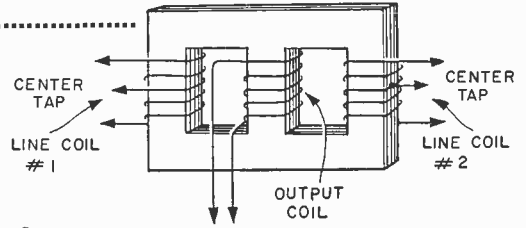
As everyone knows, telephone signals lose their "kick" rapidly as they travel down the line. After traversing about 30 miles of ordinary cable pair, the voice signals have been reduced to one-thousandth of their original strength. Thus, amplification becomes necessary to long-distance telephony.

But the telephone is a two-way device. Mrs. Smith in Boston wants both to talk and to listen to Mrs. Brown in San Francisco. In fact, both ladies are often talking at the same time. How can we arrange a two-way amplifier that will amplify the signals equally well in both directions without complex switching, and without getting the signals mixed up?

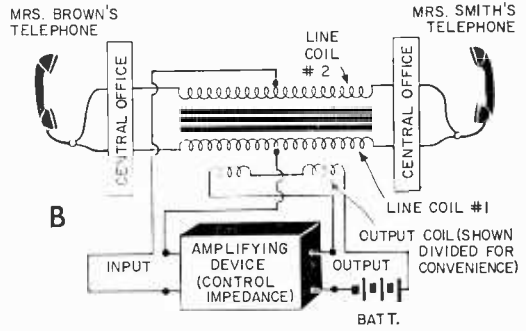
The answer lies in a special kind of transformer called a hybrid coil (see Fig. A). Two identical, carefully balanced coils, the line coils, are connected in series with the two wires of the line. A third winding, the output coil, is arranged to couple its magnetic field equally into both of the line coils. The output coil is connected to the output terminals of the amplifying device, which may be either a vacuum-tube or a transistor. The input terminals of the amplifier are connected to the two center-taps of the two line coils (see Fig. B).

The two line coils have small resistance, about that of a mile or two of line, so the signal can pass through them with little loss. And since the input of the amplifier is connected to the two center taps, it is effectively connected across the line. Thus the voice signals from either Mrs. Brown's or Mrs. Smith's phone will be fed equally well into the amplifier.

These signals act to vary the battery current in the output circuit via the control impedance. Therefore, a greatly enlarged replica of either or both voice currents flows through the output winding of the hybrid coil. These strong voice currents cause a changing magnetic flux to pass through both line coils in the right direction,



A GENERAL ARRANGEMENT OF A HYBRID COIL



thus inducing a large voice voltage back into the line. This greatly-amplified signal propagates down the line in both directions, giving both parties the benefit of the boost.

Because the input of the amplifier is connected to the exact center of each of the coils, and since half of the signal is sent each way down the line, the amplifier's output voltage is cancelled out at its own input terminals. Thus, when things are adjusted properly, the voice signals may be amplified many times without annoying "singing," or feedback.

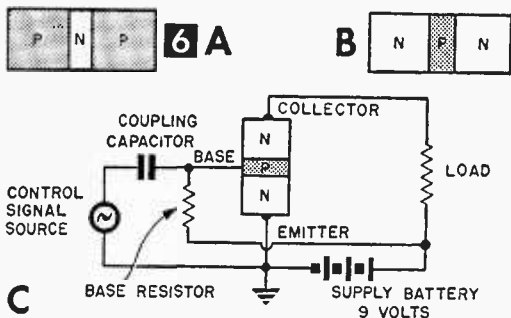
to have a definite repulsive effect upon the electrons. The control-signal voltage source is connected in series with the grid battery so that its variations will add to and subtract from the negative, fixed grid voltage. Thus the signal voltage will make the grid instantaneously more or less negative with respect to the cathode. When the grid becomes less negative, it repels the electrons less strongly, and the cathode-plate-load current increases. When the signal makes the grid more negative, it repels more electrons, reducing the load current. Thus the triode vacuum tube acts as a control impedance whose internal opposition to load current flow is at the command of the grid voltage.

Like all practical devices, the vacuum tube can develop "indigestion" which interferes with its action under some circumstances. To avoid this, more grids have been added which, when properly connected, vastly improve its universality. Also, vacuum tubes ranging from pea-size (for hearing-aids and microwave use) to 100-kilowatt giants have been built and are in use as amplifiers on all sorts of jobs today. They're made of metal, glass and special ceramics. Vacuum tubes are shot into outer space on satellites, and are operating miles beneath the surface of the ocean as

transoceanic cable amplifiers. They work.

The Transistor. In 1947, after countless hours of cogitation upon solid-state physics, quantum mechanics, statistical theory, and (possibly) voodoo, Drs. Bardeen and Brattain, of the Bell Telephone Laboratories brought forth a remarkable new control impedance called the *transistor*. Unlike the vacuum tube, the transistor makes use of conduction through a special kind of solid substance called a semiconductor instead of through a vacuum. The stuff most of the practical ones are made of today is element No. 32, *germanium*, an element recovered as a by-product from the combustion of certain coals.

When it's pure, germanium is an almost perfect insulator. But when the minutest whiff of indium, arsenic, gallium, aluminum, or certain other elements are added, it becomes a semiconductor. By adding the right stuff, in the right amount, one may make at will two different types of semi-conducting germanium, either N-type, or P-type. An N-type germanium conducts practically like copper does, that is, by means of free electrons which may move about inside the crystal. The P-type, however, is missing a few electrons which it should normally contain. These missing electrons, called *holes*, can



gized, it causes an alternating signal current to flow between the base and emitter connections of the transistor. We recall that an alternating current can flow readily through the coupling capacitor, but that this capacitor acts as an open circuit for unvarying, dc battery current. Thus the capacitor prevents the generator from short-circuiting the base resistor, while allowing the ac control signal current to flow with relative ease.

From one point of view, we may think of the base section acting something like a semi-permeable wall, allowing electrons to pass through it in proportion to the base-emitter current. When the signal source current acts in such a direction as to add to the steady base current, its permeability is increased, and more current can flow from the emitter to the collector through the load. On the other hand, when the signal current subtracts from the battery current from base to emitter, base permeability decreases, the collector-load current is forced to decrease in proportion. Thus the load current is at the direct control of the base current from the signal source; the transistor, like the vacuum tube, acts as a true control impedance. And since the magnitude of the base signal current change is always much less than the corresponding load current change, transistors are effective amplifiers.

It is most important to observe here that, while the vacuum tube and the transistors are both control impedances, and thus amplifiers, they differ drastically in one important operational aspect. Whereas the vacuum tube is a voltage-controlled impedance, the transistor is a current-controlled device. Thus, while these two devices may often do similar jobs, they are by no means interchangeable, either in theory or in practice.

Both the vacuum-tube and the transistor have particular amplifying jobs to do at which each excels. At present, high-quality vacuum tubes are relatively inexpensive, easy to manufacture on a mass scale uniformly, and operate well when the control signal changes rapidly with time, that is, at high frequencies. On the other hand they are relatively bulky, mechanically fragile, and require excessive operating power in the form of cathode-heating requirements.

The transistor is exceedingly compact, operates well with a low-voltage supply source, requires no heating power, and laughs at mechanical shock that would shatter a vacuum tube. But, transistors are exceedingly difficult to manufacture to within close tolerances. Every production run includes a high percentage of rejects which do not meet government and commercial standards. (These culls are what you and I buy for experimenter's projects today, unless we pay over \$5 per unit.) Furthermore, transistors are extremely subject to quick and fatal elec-

move around inside the crystal and conduct electricity too. However, since they're "missing electrons," they're positively charged particles and move in the opposite direction through the system. But they still conduct, nevertheless.

The art of semiconductor fabrication has advanced so far as to allow different zones of the same chunk of germanium to be made into either N- or P-type material. In fact, such technique is necessary in the routine fabrication of a modern transistor. A modern "junction" transistor, the presently most common and practical type is made of a small bar of germanium about $\frac{1}{8}$ in. long and about $\frac{1}{16}$ in. square. This little bar is divided into three alternate zones of P- and N-type material. The finished bar is sealed in a neat case, for convenience and security.

As Figs. 6A and 6B show, two types of junction transistors are thus possible—PNP and NPN. Both operate upon the same basic theory, the main difference being in the polarity of the supply voltages.

Fundamentally, in schematic terms, an NPN transistor is connected into its most generally practical amplifier circuit in the manner shown in Fig. 6C. The magnitude of the voltages and current shown apply to the typical experimenter's transistor. Power transistors are made which are capable of dealing with much greater voltages and currents when necessary.

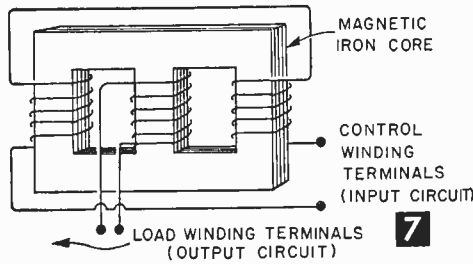
Connections made to the ends of the bar of N-type germanium are designated the *emitter* and the *collector*, while the thin layer of P-type material in the center of the bar is called the *base*. In normal operation an electron current of about one milliampere flows from the grounded side of the supply battery into the emitter end of the transistor and up toward the base. Here, within the transistor, it divides, about 95% of it flowing through the entire bar and into the load through the collector connection. The remaining 5% flows out of the base connection, through the base resistor, and back to the positive terminal of the battery. This is the resting state of the circuit.

When the control signal source is ener-

trical damage if wrongly connected or allowed to become too warm. Truly effective high-power or high-frequency transistors remain extremely expensive, if indeed they are available to ordinary mortals at all, while vacuum tubes capable of supplying hundreds of watts at hundreds of megacycles may be bought over the counter for a few dollars almost anywhere.

Magnetic Amplifiers: While the vacuum-tube or transistor is still necessary for amplification of signals which change magnitude appreciably in less than one-thousandth of a second, slower signals may be effectively handled by the *magnetic amplifier*.

This interesting device depends for its operation upon the fact that an iron-alloy core, similar to that used in transformers, can, so to speak, pass only a limited number of mag-

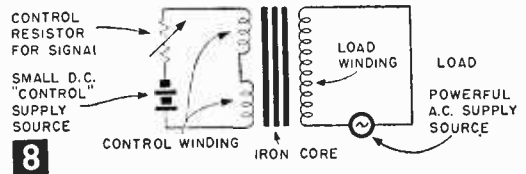


BASIC ARRANGEMENT OF SIMPLE MAGNETIC AMPLIFIER

netic force (flux) lines per square-inch of cross-section area. When such a core has been filled with magnetic flux it becomes very difficult to force any more to pass through it.

The heavy alternating current to the load is made to pass through the load winding (see Fig 7), while a small, possibly slowly changing unidirectional (*dc*) control current passes through the control windings. Because the two control windings consist of the same number of turns effectively wound in *opposite* directions, the heavily load current induces equal but opposite voltages into each winding, which thus effectively cancel-out in the control circuit. By this means, effective electrical isolation is maintained between control and load circuits. On the other hand, the control currents may still magnetize the core, and exert control action.

A more easily understood schematic diagram of a simple magnetic amplifier circuit is shown in Fig. 8. Assume that the control resistor is of such high resistance that negligible current flows through the control winding. The *ac* load current then flows through the load winding, developing a large and constantly changing magnetic field within the iron core. This continually changing magnetic field induces an *opposing ac* voltage back into the turns of the load winding. This opposing, self-induced voltage subtracts from the *ac* generator voltage, thus, reducing the



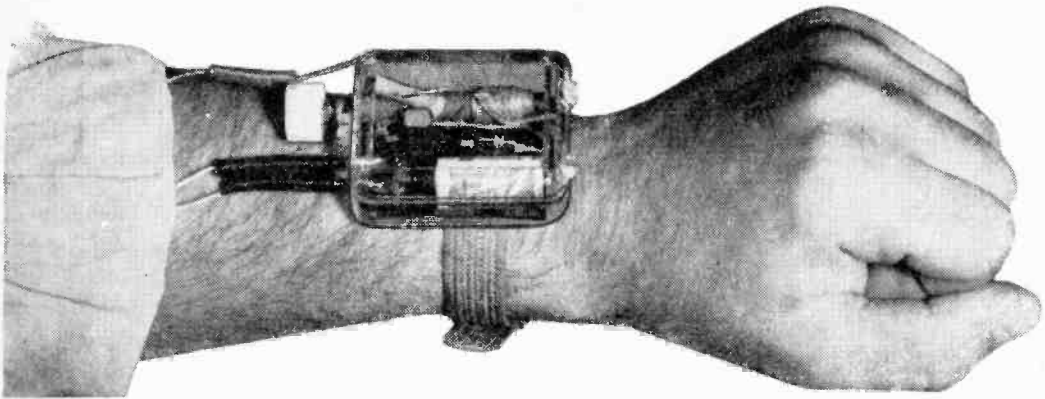
current in the load circuit to a small number of amperes. In other words, the load winding acts as an efficient "choke coil" in the *ac* load circuit, opposing the flow of current therein.

But now let us pass a small current through the control windings. This current now adds a second set of magnetic flux lines to those present due to the load current. But, as we have just said, the iron core can only contain a certain maximum number of total magnetic lines. Since an appreciable amount of the core's magnetic capacity is now being used by the *dc* control flux, the *ac* load current can no longer produce as great a changing field within the core as formerly. Since the opposing voltage induced within the load winding is directly proportional to its own changing field, and this must be appreciably less than formerly, the load winding's "choking" effect is less, allowing more load current to flow.

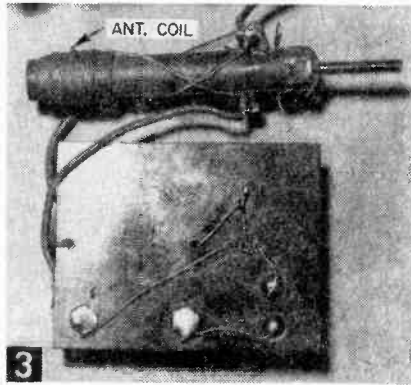
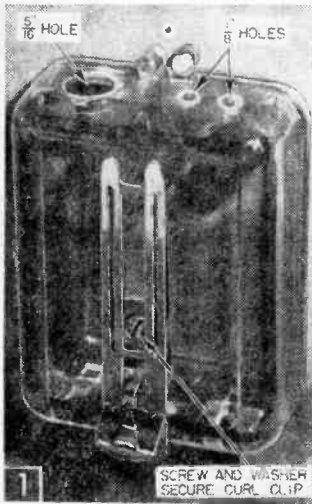
Increasing the steady current further leaves still less "space" within the core for the changing flux about the load coil, so the choking-effect of the latter is reduced still further. Finally, we may increase the control winding current to the point where it almost fills, or "saturates" the iron core. Then, even though the *ac* load current is still changing as rapidly as before, it can produce little or no changing flux within the coil.

Thus we see that the magnetic amplifier is really nothing but a variable choke coil, whose current-opposing effect is at the direct control of a small direct current in the control windings. Though relatively slow in response, it is a powerful amplifier, finding much use in multi-kilowatt applications. By its use, thousands of horsepower involved in the rolling-mills of a large steel plant may be perfectly synchronized and controlled in an automatized steel-plate production system.

Of course, numerous improvements are possible, and are frequently applied in magnetic amplifier practice. By inserting a rectifier, or electrical "one-way valve" between the control source and the control windings, a magnetic amplifier may be made to amplify low-frequency *ac* control signals. Also, a feedback circuit by which some of the output power is reapplied to the input circuit, may improve the action and response-speed of the device. Where its inherent slowness is not a disadvantage, the magnetic amplifier is certain to find increasingly wider use, since it is the simplest, longest-lived (practically immortal), most rugged high-powered amplifier we have available at present.



WRIST RADIO



Left, the versatile curl clip is fastened to the case with screw and washer. Holes in end of case are for phone clips and antenna coil. Above, underside of chassis. Virtually all wiring is done with pigtail leads of circuit components.

lighter, than a diminutive hearing aid whose manufacturer advertises his unit as tiny enough to be hidden in milady's hair. Only slightly larger than a book of paper matches, it still has up to twice the volume and selectivity of ordinary transistor or transistor-diode circuits.

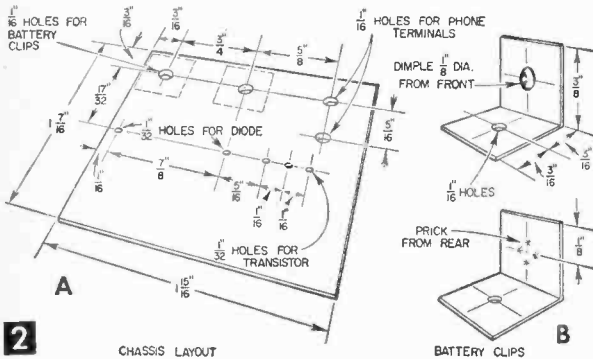
In spite of its tiny dimensions, all parts for the set are readily available. The polystyrene plastic case you'll find on the "Cosmetics" counters of any dime store. There also you'll find the versatile clip which attaches to the case. The trade name is "Lady Ellen Curl Clips." Get the 1 $\frac{1}{8}$ -in. size.

For the chassis, we used a 1 $\frac{1}{16}$ x 1 $\frac{15}{16}$ in. piece of linen impregnated Bakelite. Thin fiber or cardboard can also be used. Lay out and punch the $\frac{1}{16}$ in. holes (Fig. 2A) with a paper punch and pierce the $\frac{1}{32}$ in. holes for diode and transistor with a needle. If you use cardboard for the chassis, dip it in shellac, remove and allow to dry after making mounting holes. Repeat if necessary to give the cardboard the stiffness that fiber or Bakelite has.

Insert the germanium diode and transistor "pigtail" leads into their mounting holes and bend to right angles on the underside of the chassis (Fig. 3).

This gives rigidity to circuit components without resorting to ultra-miniature clips and sockets.

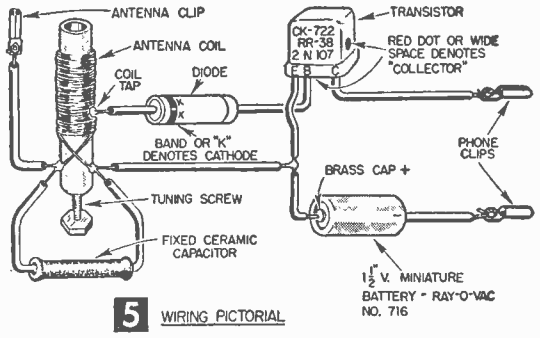
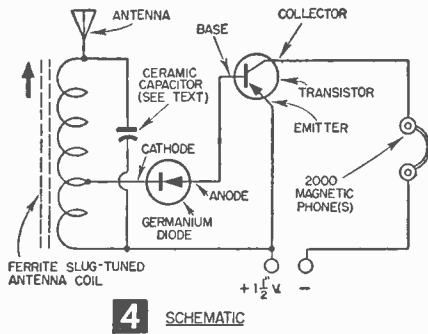
Make the battery clips from strips of brass, copper or tinplate as in Fig. 2B. To hold the brass cap end of the battery securely, dent or dimple one of the clips with a $\frac{1}{8}$ -in. flat punch, or



2

CHASSIS LAYOUT

THIS super-small set can—honestly—be called a *Wrist, Clip-On, or Pendant Radio*; its minute size lends itself to these applications without forcing the name upon it as is done so often with sets that should have been labeled *Pocket Radios Only*. It's one-third smaller, and 75%



MATERIALS LIST—WRIST RADIO

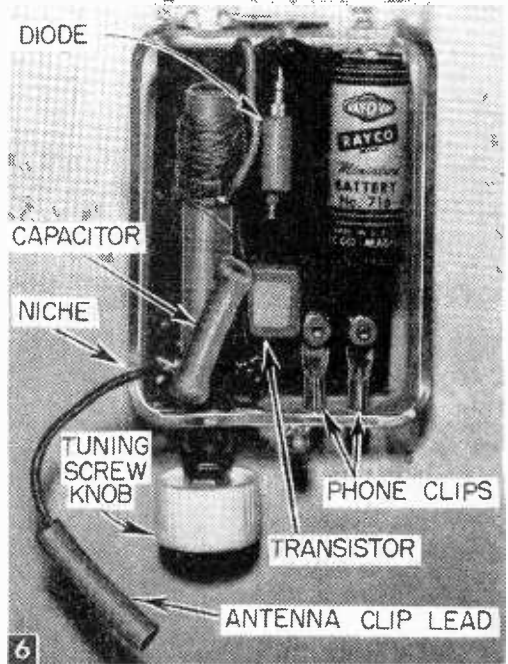
- | No. | Description |
|-----|--|
| 1 | Plastic utility box, 2 1/8 x 1 3/4 x 7/8 in. |
| 1 | General purpose diode (1N34, 1N66, 1N48, or 1N65) |
| 1 | Transistor (CK-722, RR-38 or 2N107) |
| 1 | Ferrite antenna coil (Miller, Stanwyck, Grayburne, etc.) |
| 1 | Ceramic fixed capacitor (120 mmf. to tune 1590-880 kc.; 220 mmf. to tune 880-550 kc.) |
| 1 | Pair standard magnetic headphones, or miniature earphone (D.C. resistance should be 2000 ohms minimum) |
| 1 | Miniature flashlight battery (Ray-O-Vac #716 or any other size "N" 1 1/2 v. cell. If mercury type cell should be used, note that cap is minus, not plus as with regular batteries) |
| 3 | Tube pin contacts salvaged from octal wafer socket |
| 5 | 2-56 x 1/8 in. brass machine screws and nuts |
| 1 | 4-40 nut or 4-40 knob for tuner screw |
| 1 | Small alligator clip (or "frictional" paper clip) |
| 1 | 3 ft. length light, flexible hook-up wire |
| 1 | "Lady Ellen" curl clip, 1 7/8" size |

machine screw. To prevent the smooth, zinc shell end of the battery from sliding out of position, pierce the other clip with a prick punch or nail. Fasten the battery clips to the chassis with 2-56 machine screws and nuts not more than 1/8 in. long and the phone clips with 2-56 screws.

The set uses either standard-size or hearing-aid-size magnetic phones. Standard-size phones have cords fitted with tips, but with the miniature phone you'll have to add them. To do this, carefully remove about 1/4 in. of the insulation from the cord to expose its tinsel conductors. Then place a common pin parallel with the tinsel conductors, and bind pin and tinsel together with a single strand of ordinary stranded fixture wire, snip off the protruding end of the pin and solder.

Suppose you use standard-size phones—then what about the jacks we used? Well, these are nothing more than the pin clips used in cheap octal wafer tube sockets. A 5¢ socket yields 8 of them if you don't have an old socket from which you can salvage the 3 used in this project. If your standard-size phone tips don't fit, simply compress the clips with a pliers until they do.

Except for the coil connections, wire all components on the underside of the chassis with the transistor and diode pigtail leads (Fig. 3); separate hook-up wire is not required. When soldering to the screw terminal points, use a thumbnail-size wad of wet cleansing tissue pressed over the pigtail lead so that heat is not



Set with case open. It measures only 2 1/8 x 1 3/4 x 7/8 in.

transmitted up into the diode or transistor. Just as soon as the solder sets, move the wad over the hot connection so that it will cool rapidly. This protects transistor and diode from damage. Electrical connections are shown in Fig. 4; physical connections, in Fig. 5.

In order to provide the most efficient match between the high-impedance resonant circuit of coil and capacitor and the low-impedance diode detector—which, in turn, feeds into the low impedance transistor—the ferrite slug-tuned antenna coil is tapped 16 turns from the outside end of the winding. Using the coil shown in Fig. 3, which has a progressive type winding, you needn't count off turns; just unwind 21 inches of wire. This is equal to 16 turns. Carefully scrape off the cotton insulation and form a small loop, then rewind the coil wire as closely as possible into its original space and pie-layer arrangement and reconnect the end of the coil to the terminal lug. No great harm will result,

however, if you "scramble wind" the turns back on the coil form.

With two short lengths of light stranded, plastic-covered hook-up wire, connect one coil lug and the tap to chassis components. With a third length, connect the inside coil lug to another octal socket clip. This is the antenna connection. A 3 ft. length of wire fitted with a small alligator clip and brass weatherstrip nail or phone tip attaches to it. Removed from the set when not in use, this type of antenna eliminates dangling wires.

A fixed ceramic capacitor connected across the coil lugs completes the wiring. Its value will depend upon stations operating in your area. If stations tune in between 1590 and 880 kc., the value of the capacitor should be about 120 mmf. To tune from 880 kc. to the top of the dial, 550 kc., use 220 mmf. Solder a 4-40 brass nut to the end of the threaded coil slug, or a small bakelite knob with a 4-40 lock nut, to turn the coil's tuning slug in and out.

When testing the set before installing in its case, attach the alligator clip to the finger stop or metal box of your telephone. If wiring is correct, and the correct size capacitor for your area is across the coil, you may find that powerful local stations are so loud that the earphone is overloaded and reception distorted. If this happens, remove the alligator clip from the phone. The volume will still be loud, but the set will be free of distortion—and quite selective.

Try the antenna clip on metal lamp bases, screens, bedsprings, etc., but you will probably find you can let it hang free and still get good reception.

With the set tested, it's ready for mounting in the case. Drill two $\frac{1}{8}$ -in. holes for the phone clips and a $\frac{5}{16}$ -in. hole for mounting the tuning coil (Fig. 1). Drill a $\frac{1}{4}$ -in. hole in the back of the case for securing the curl clip and slip a $\frac{5}{16}$ -in. dia. washer over a 2-56 screw and clamp the clip between washer and case. The chassis with its wiring friction-fits in the case.

The antenna lead passes through a niche filed between case lid and cover. (Fig. 6.) When not in use, it's tucked inside. Since the case is transparent, a snapshot, colorful floral print or decal can be inserted under the lid when the set is used as a Pendant Radio. There is a $\frac{1}{8}$ -in. hole in the curl clip to which either a ribbon or chain may be attached. As a Wrist Radio, a plain leather strap is all that is required—the set clips to the strap—and as a Clip-On Radio, it clips to tie, shirt pocket, belt.

We've obtained fair results with an aluminum-foil-lined hat as a walking antenna, receiving 50 kw. stations located 20 airline miles away. For so tiny a receiver, mobility is asking a lot, but in many areas this stunt is possible. Note that no ground connection is required for normal reception. In remote areas, of course, a ground may be connected to the battery's minus terminal.—THOMAS A. BLANCHARD.



I don't object to your doing-it-yourself—but I do draw the line at growing your own needles!

Code Practice Oscillators

The article describes two code practice oscillator kits that are easy to build, instructive, and inexpensive

CODE practice oscillators are comparatively simple electronic devices. The simplest use only a single transistor or tube. The output is an audible tone, generally between 400 and 2,000 cycles per second, which the user can hear in an earphone.

The Lafayette KT-72 kit is available for \$2.99 from Lafayette Radio, 165-08 Liberty Avenue, Jamaica 33, New York. It comes complete with key, but the head-phone must be bought separately. The Knight 83Y239 kit is available from Allied Radio, 100 N. Western Avenue, Chicago 80, Illinois, for \$3.95. The key and the head-phone are not included in the kit and cost \$3.33 more.

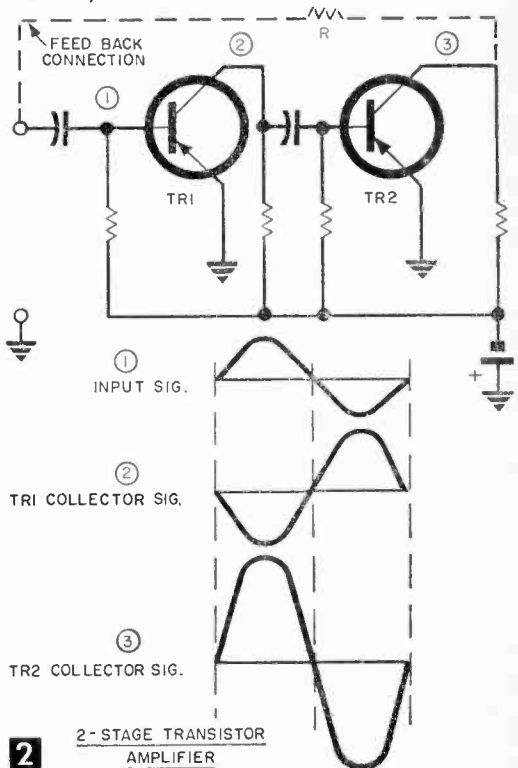
Theory. A small signal voltage at the input to the base of the first transistor shown in Fig. 2 will produce a larger signal at the second transistor (TR2) output. Now even if there's no signal at the input of the amplifier, there's still a very small signal at the first transistor collector made up of noise generated within the transistor and the circuit components. This noise is amplified by the second transistor.

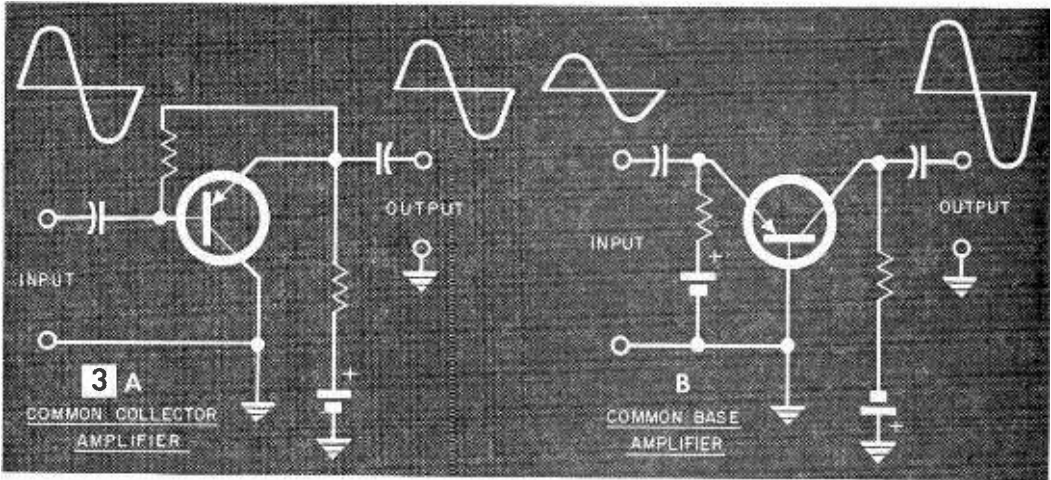
If we were to feed the output of this amplifier back to its input (through a resistance to keep the low-impedance input from partially shorting the higher impedance output), this noise would pass through the amplifier. It would again appear at the output—amplified this time—and it would continue to recirculate in this way until it was prevented from becoming any louder by the value of battery voltage and the parts values employed in the circuit.

Did I intentionally use two transistors to illustrate this? Yes. The transistor circuit configuration used in the circuit of Fig. 2 is called a common emitter circuit because one battery terminal and one input terminal (indicated by the ground symbol) are connected to the emitter. The amplifier in Fig. 2 consists of two cascaded common emitter connected transistors.



The Lafayette Transistor Code Practice Kit completed.





The common emitter circuit configuration is more popular than the common collector and the common base circuits shown in Figs. 3A and 3B because the common emitter circuit has greater power gain and because only one battery power supply is required to operate it. But the common emitter circuit inverts the signal (see Fig. 2). Thus, if we fed some of the output of a single transistor back to its input, the signal would subtract and cancel the tendency to oscillate. This type of feedback is described as degenerative.

However, if two of these transistor stages are cascaded, the signal will be inverted a second time, and when a portion of the output is fed to the input of this two-stage amplifier, the signals are in phase. This results in the build-up required for oscillation.

If a resonating circuit consisting of an inductance (a pair of headphones in the case of this code practice oscillator) and a suitable capacitance *ac* voltage divider combination for feedback is provided, one transistor will produce oscillations. In this case the LC (inductance and capacitor) combination tends to oscillate at a given frequency depending on the product of their values. But the internal *dc* resistance of the headphone windings dissipates energy, and the combination needs a recurring kick of energy—from somewhere—for continued oscillation.

A single transistor can furnish the kick. This type of oscillator is generally known as a Colpitts oscillator, and this circuit is utilized in the Lafayette KT-72 code practice kit. The circuit is shown in Fig. 4.

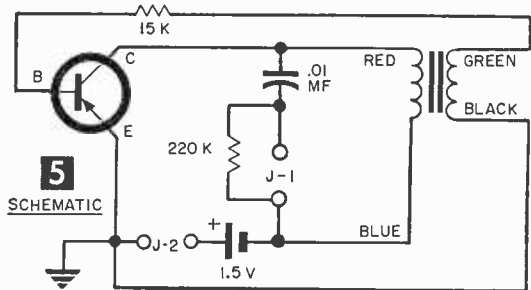
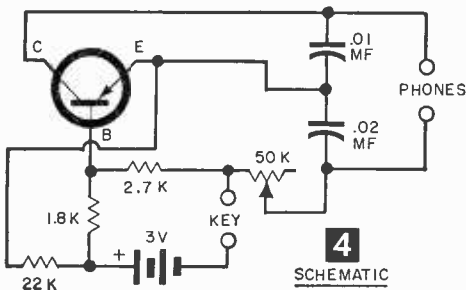
The oscillator circuit of the Knight kit also utilizes a resonant LC circuit, but in this case, feedback is introduced with a transformer. The circuit is shown in Fig. 5.

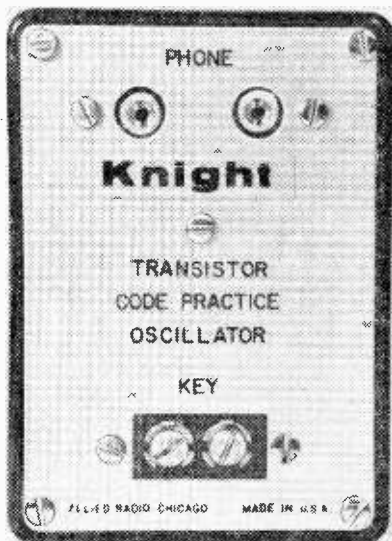
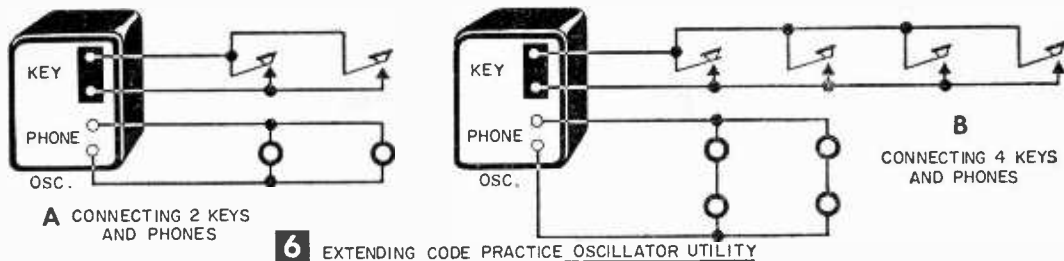
The instructions which come with the Lafayette code practice oscillator kit include a step-by-step wiring sequence. Many of the connections are made without any soldering and rely instead on screws and nuts and Fahnestock clips.

The components are mounted on a perforated Masonite board before any wiring is attempted. The shaft for the volume control must be cut to about 3/8-in. length before it is inserted in the volume control. The 50-K volume control is connected as a rheostat (only two terminals are used) instead of as a potentiometer (where three terminals would be used).

The Knight transistor code practice oscillator kit fits in a compact Bakelite case 1 5/8 x 2 7/8 x 4 in. with an aluminum front panel. It operates from a single 1 1/2-v penlite cell. Terminals for connecting key and headphones are provided on the front panel.

The parts in both kits are covered by a





7

Front-panel view of the Knight Transistorized Code Practice Kit.

standard RETMA 90-day warranty. Any defective parts will be replaced within 90 days provided the damage was not due to carelessness or abuse. Each of the suppliers will troubleshoot your kit for a nominal cost if you can't make it work yourself, but the chance that you'll have trouble with either is very small.

Almost any kind of magnetic headphones of 1,000 ohms or greater impedance may be used with either oscillator. Lafayette recommends a single headphone which may be ordered from them as AM-15-1 at \$1.18. Allied recommends a unit which sells for \$1.08 (59Y112, their catalog number). The key for the Knight Kit may be Allied's 76 PO53 at \$2.25 or Lafayette's MS-309 at \$1.25.

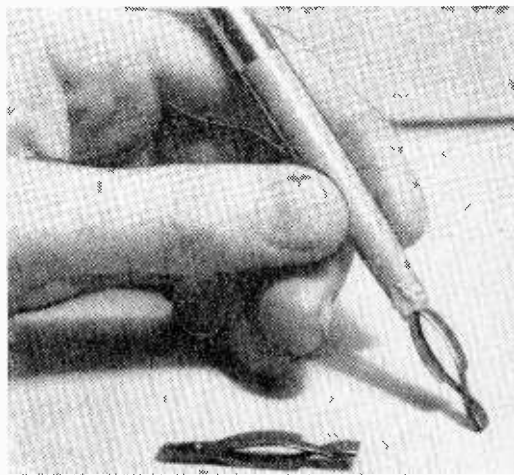
If you wish to use either code practice oscillator with another person, another key and headset may be added as shown in Fig. 6A. If you wish to get as many as four people into the circuit, connect the keys in parallel and the headphones in series-parallel as shown in

Fig. 6B. This kind of operation is a lot of fun and it will help you and your friends learn the code faster.

In comparing the two kits, I find it difficult to recommend one over the other. The Knight Kit is simpler to construct and can be built in less time. It is housed in a very attractive functional package. The Lafayette Kit, on the other hand, is less expensive and it includes the key.—F.H.F.

Soldering "Pen" Absorbs Heat

- Soldering iron heat can ruin transistors and other small electronic parts, unless you use a heat sink. Pliers are often too bulky and heavy for the job, especially in the corners of chassis wiring, or working on minia-



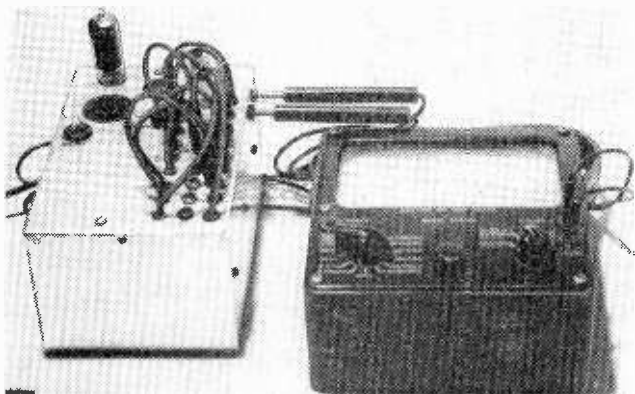
turized circuits. Remove the ink cartridge from an old ball point pen, and saw off the tip about 1/2-in. from the end. Then heat the back end of a Mueller #88 test clip and force it into the pen handle. A drop of cement completes this handy tool.

Draftsman's Tape Holds Tight

- Draftsman's tape makes an excellent "third hand" to hold electronic components together during assembly or soldering. Due to its high insulation, the tape can be left on permanently, or can be peeled off easily.

—J. A. McROBERTS

Adapter Unit Checks Tubes With Your Multimeter

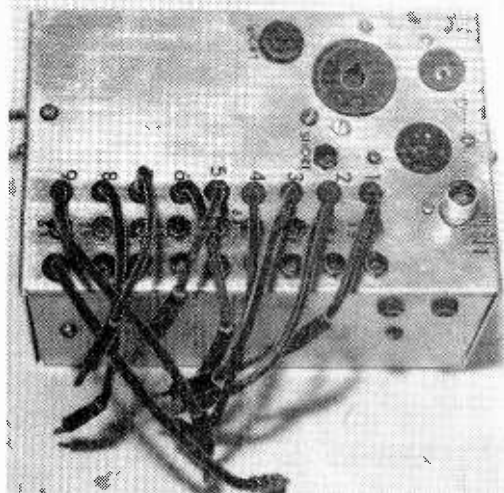


This adapter unit enables you to check tubes with your volt-ohmmeter, makes a fine filament source for experimental setups, and provides multi-ac taps for measurement and calibration work

Figure 2A shows the filament continuity test in schematic form. If a neon tube is connected to an appropriate voltage source, through a tube filament, it will glow brightly. If the filament is open, the neon tube will stay dark. Similarly, if any of the elements are shorted, and the neon tube is connected through both of them to its source, it will glow again brightly (Fig. 2B). Usually we are interested in shorts to cathode, because they are the most commonly found shorts in tubes.

When a tube is in good condition, the cathode is capable of emitting all the electrons which can be demanded by plate and grid voltages. Actually, the cathode can deliver many more electrons, but there is a finite limit, the saturation current. When a vacuum-tube cathode starts to deteriorate, the first indication is a drop in saturation current. Thus by testing what the saturation current is, we can pretty well determine the condition of the tube. We do this by tying the cathode to ground, heating the filament normally, and applying an ac voltage to all the other elements together. Then we measure the current through the tube, this is the emission test. (See Fig. 3.) Since this measured emission current is the total of that received by all of the elements, when we remove one of them from the circuit, there will be a slight drop in current. Not much, but enough to be perceptible and enough to indicate whether the element in question is open. The recommended *maximum* time to take a reading is three seconds.

Multimeter Requirements. The schematic is shown in Fig. 4. The transformer for the adapter unit is a tube checker transformer with many voltages tapped off. The tapped voltages are supplied to jacks. There are five jacks to a red lead; these supply ac to the elements of the tube under test. There are three black pin-jacks; these are grounded.



Adapter unit at left above (and below) used with volt-ohmmeter for checking tubes.

By TOM JASKI

THE most common and one of the simplest tube tests which can give reasonably reliable information about a vacuum tube is the emission test. Together with tests for continuity of the filament, shorts and opens of the elements, these are the tests that are made when you take your tube to a service shop for a free tube test, and these are also the tests which you perform on do-it-yourself tube testers. With the unit described here and with your volt-ohmmeter you can make these tests yourself.

One of these must be used for one side of the filament, one for the cathode and one is a spare in case you want to ground the suppressor grid also. There are two jacks for the meter, one red for the positive prod, one black for the negative meter prod. The neon tube circuit was shown in Fig. 2. Each lead of the group of nine flexible black leads with phone tips on the ends is connected to a numbered pin on the tube test socket S. Lead one connects to all the #1 pins, lead two to all the #2 pins, etc. These are plugged into the appropriate jacks when you are using the unit.

The meter must have at least a 100 ma scale and preferably a higher one. If your multimeter does not have a scale as high as 100 ma, make a shunt to use with whatever scales you have. If you have only an ordinary 1 ma meter, you can use this provided you make a shunt for it which has a resistance of $\frac{1}{100}$ th of the meter internal resistance, for the 100 ma range, or $\frac{1}{1000}$ th for the 200 ma range. The reason your meter needs these high ranges is that the saturation current of cathodes is considerable, in some cases over 200 ma. (In regular emission tube checkers, this is com-

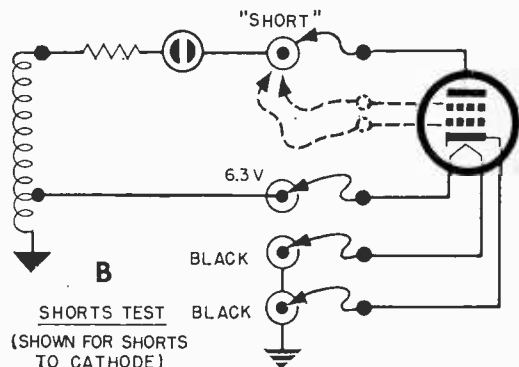
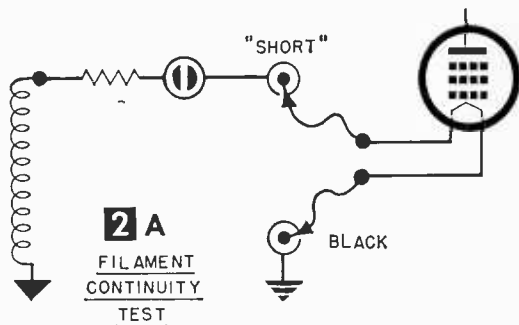


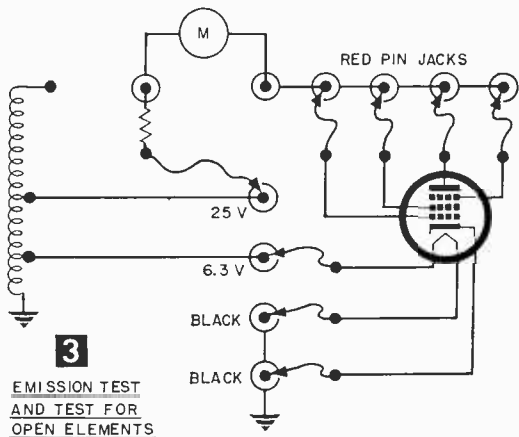
TABLE A

EMISSION CURRENT AND TEST VOLTAGE OF REPRESENTATIVE TUBES

For other tubes, refer to tube manual. Similarity for emission test can be judged from maximum dissipation, maximum plate current and voltage or max. cathode current.

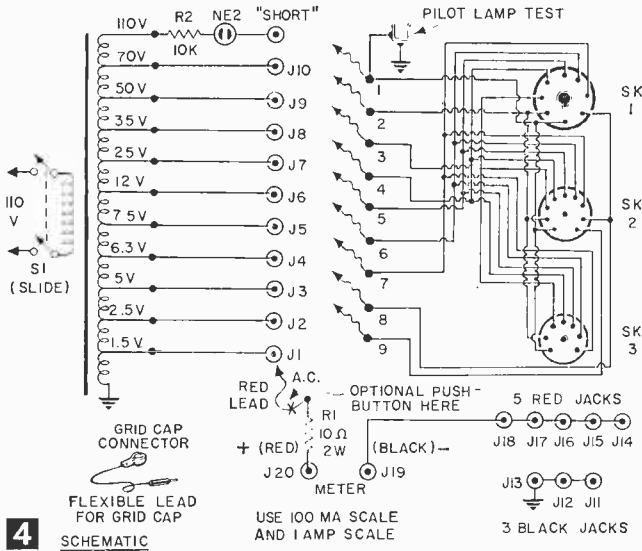
(For dual tubes, the figures refer to each section separately with the other section unconnected.)

Type	Test Voltage	Current (ma)
5U4G	70	180
5Y3	70	60
5Y4	70	65
5Z3	70	70
6AG5	25	65
6AH6	12	70
6AK5	25	65
6AL5	12	50
6AQ5	35	80
6AU6	12	60
6BA6	12	40
6BC5	12	70
6C4	25	65
6J6	25	40
6L6	50	200
6SL7	25	50
6SN7	25	75
6V6	35	90
6X4	50	100
6X5	50	90
12AU7	25	75
12AX7	25	50
12SN7	25	80
25L6	35	160
25Z3	35	150
25Z6	35	140
35L6	25	140
35W4	25	140
35Z3	25	140
50B5	35	160
50C3	35	140
50L6	25	180



pensated for by a dc voltage circuit which counteracts the deflection of the meter.)

Plug in the adapter unit, but do not yet turn it on. Find the base connections of the tube you wish to check from a tube manual. (Electronic supply stores have good tube manuals available for from 25¢ to 75¢.) Plug one of the filament terminals into a black pin-jack, the other into the appropriate voltage jack. For split filament tubes, use the entire filament. For example a 12AX7 can be used on 6.3 and 12.6 v, but in this case you would use the 12.6-v tap and apply it to either pin #4 or pin #5, with the other one connected to the ground jack. Next, determine what the cathode is. On 7-pin miniature tubes, for ex-



ample, it will usually be either pin #2 or #7. Plug it into a black pin-jack. If the suppressor grid is internally tied to the cathode, ignore its pin # lead. If it isn't, plug it into a red jack.

Now plug all the remaining element leads which are appropriate into red jacks. Of course on a 7-pin tube you will have two unused leads. If a tube socket has no connection to, say, pin #6, this lead will not be used. Hang the leads away from the box, in case there is an internal connection in the tube.

Insert the meter prods, and make sure the meter is at least on the 100-ma range. Observe meter polarity. (Note that so far we have done nothing with the red lead which supplied ac to the red jacks.) Turn the unit on, and let the tube warm up for about a minute. Then select the proper ac voltage and plug in the red tip to that particular jack. In table A, a representative group of tube types are listed, together with the voltage which should be used to test them and the current the meter should read for a good tube. Tubes which belong to the same family can be found in your tube manual. For example a 12AY7 is tested with the same voltages as a 12AU7, draws a bit more current.

As soon as you plug in the red lead, read the meter and unplug it again. Don't leave the red lead connected any longer than necessary. If you don't want to plug and unplug a hot lead, build in a normally open "test" pushbutton so that this lead can be plugged in ahead of time and pushed on as needed.

If the tube reads the approximate current listed in Table A, or a value you calculate must be about right from similar tube listings, it passes the emission test. If it reads only 60% of these values, the tube is doubtful. If it reads only 50%, reject the tube.

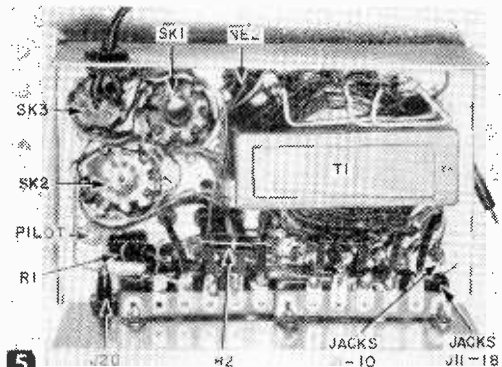
Construction. Front panel layout is shown

in Fig. 1; internal construction in Fig. 5. The flexible leads are anchored on the tie-point strips, so they won't pull out. You could solder them directly to one of the tube sockets, but then they must be made longer. There is nothing critical about the layout, just make sure the leads are long enough to reach all of the jacks. A bayonet type socket is included for testing pilot lamps. If you expect to check other types of tubes, with different bases, there is nothing to keep you from including as many different kinds as are available—simply use a larger box.

The shorts and filament continuity tests have not been discussed in detail, but once you know how to set up a tube for the emission check, it is obvious from Figs. 2A and B what must be done for the others. Simply plug in the appropriate leads, one at a time on the shorts test. Don't be alarmed if the neon tube glows slightly when you test the cathode to filament short (which is done by simply plugging the cathode lead in the "short" jack). There is always some leakage between cathode and filament, and only if the tube lights up brightly should the tube be rejected.

MATERIALS LIST—ADAPTER UNIT

No. Req'd	Description
1	transformer (T1) Stancor P-1834-3—tube checker transformer (or equivalent)
1	octal socket
1	7-pin miniature socket
1	9-pin miniature socket
21	phone-tip jacks
10	phone tips
1	resistor, (R1) 10 ohms, 2 watts
1	resistor, (R2) 10,000 ohms, 1/2 watt
1	pilot lamp socket, bayonet type
1	NE2 neon lamp
1	DPST slide switch (S1)
1	grid-cap connector
3 ft	extra flexible test lead
2	5-point tie-point strips
1	3 x 4 x 6" box
	hardware, wire and solder, decals
1	pushbutton switch for "Test" (optional)



Under-chassis view of adapter unit.

One-String Electric Guitar

How one string and an earphone make music for you

BY ART TRAUFFER

MELLOW, rich and vibrant are the tones produced by this experimental unit. It can be built in an evening, and will play notes ranging through 1½ octaves.

Ordinarily, the magnets in an earphone cause the diaphragm to vibrate, making sound. This instrument uses the same principle in reverse: when the steel string (Fig. 1) vibrates, voltage induced in the coils produces a musical tone when fed through an amplifier. You can plug the unit into the phono jack of a radio, TV set, phono amplifier or tape recorder, and when you move the sliding block (Fig. 2), the pitch of the note varies as you pluck the string.

Cut a piece of straight 1 x 2-in. lumber about 28-in. long. Sand it perfectly smooth (the block must slide easily), and then give it two coats of varnish or shellac. About 1 in. from each end center the 1¼-in. long rh wood screws. These screws allow for height adjustment and their slots support the string above the board.

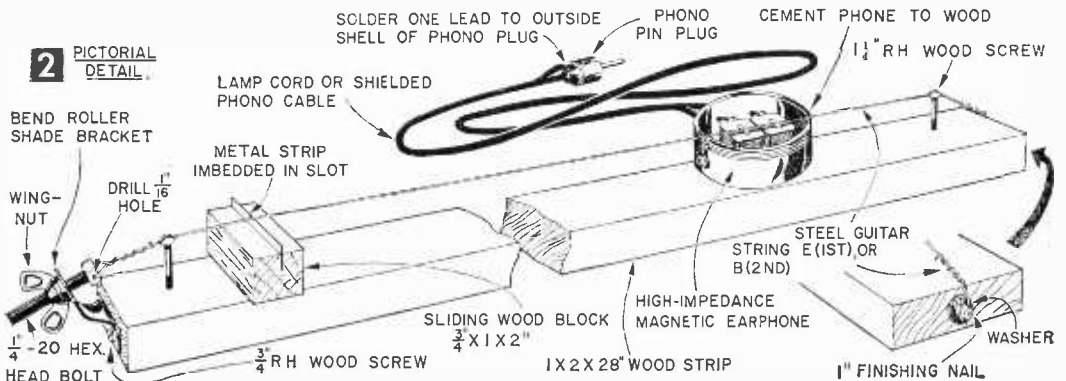
You can use either a "B" or "E" steel string. Obtainable in any music store, these strings are the two highest pitched strings on a standard 6-string guitar. Usually they are



1 Connect the one string electric guitar to the phono plug of your amplifier, radio, TV set, or tape recorder. Be sure that your set is properly grounded for safety.

supplied with a loop or factory made collar at one end. Fasten this to one end of the board, with the nail and washer assembly shown in Fig. 2.

The tie post which holds the other end of the string is made of a roller window shade mounting bracket. Drill the center hole out to ¼ in., bend the bracket as in Fig. 2, and



MATERIALS LIST—"ONE-STRING ELECTRONIC GUITAR"

Amt.	Description
1	1 x 2 x 28" hardwood strip
1	1 x 3/4 x 2" wood block
1	metal strip 1/2 by 2"
2	1 1/4" x 8 rh wood screws
2	3/4" x 5 rh wood screws
1	1/4"-20 wing-nut
1	1/4 x 20 x 1" brass bolt, hex-head
1	roller-shade bracket
1	1" finishing nail, or fh nail
1	3/8" dia. washer
1	high-impedance magnetic earphone (1,000—2,000 ohm, higher ohmage preferred)
5 ft	lamp cord, or shielded phono or mike cable
1	phono pin plug
1	Gibson steel guitar string (E or B)

mount it on the end of the board with two 3/4-in. rh wood screws. Now drill a 1/16-in. hole for the string through the head of a 1/4-20 x 1-in. hex-head screw.

The pickup is made of a discarded earphone of high impedance, between 1,000 and 2,000 ohms dc resistance, and with magnet coils in good working condition. Remove the outside screw cap and the metal diaphragm disc. Then cement, or screw the phone onto the wood board about 5-in. from one end. If your earphone has cord terminals on the back side, you may have to cut grooves in the board for the cord. This connecting cord can be made of ordinary lamp cord, with a phono-pin plug soldered at one end. However, if you find later that there is objectionable hum pickup, you may have to substitute shielded phono or mike cable.

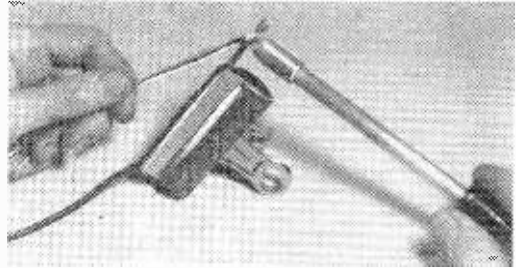
Make the sliding wood block 1 in. wide by 3/4 in. high and about 2 in. long. With a thin-bladed hacksaw, cut the slot in the top to accept a thin strip of sheet metal.

Stretch the strings over the heads of the supporting screws, thread the end through the hole and twist the end securely. Turn the wing nut slowly until the string is taut enough to produce a medium pitch. For best results the space between the string and the tops of the magnets should be as small as possible, but not so the string hits the phone when it is plucked. Plug the phono tip into the jack of your hi-fi amplifier, a radio, TV or recorder. The instrument is now ready to play.

Safety note. In most types of ac-dc radios (having no power transformer), the chassis is hot and hence, if the power is not polarized, the string of the instrument could also be "hot," and serious electrical shock could result. Be cautious about using this instrument on, or near damp floors, or near radiators, etc., and if in doubt, have your phono input jacks checked for safety by a radio serviceman.

How It Works. In theory, this one-string "guitar" works like a musician's electric guitar with magnetic pickup. When the steel guitar string vibrates in the magnetic field of the earphone pole pieces, the string

cuts the lines of force between the poles and induces a small e.m.f. (electromotive force) in the coils. This e.m.f. is amplified by an audio amplifier, or by the audio section of a radio or TV, and then reproduced by a loud-speaker. The tone you hear depends on the rate of vibration of the string. A 1000 c.p.s. tone means that the string is vibrating 1000 times per second. The amplitude of the tone depends on the strength of the strings vibration, the gain of the audio amplifier, and on the spacing between the string and the magnets.

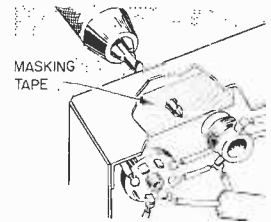


Clamp Holds Wire for Soldering

• When tinning the tips of electric wires and soldering on lugs, use a large paper clamp to hold the wire still and keep it from rolling while you touch the iron and solder to the wire's tip.—JOHN A. COMSTOCK.

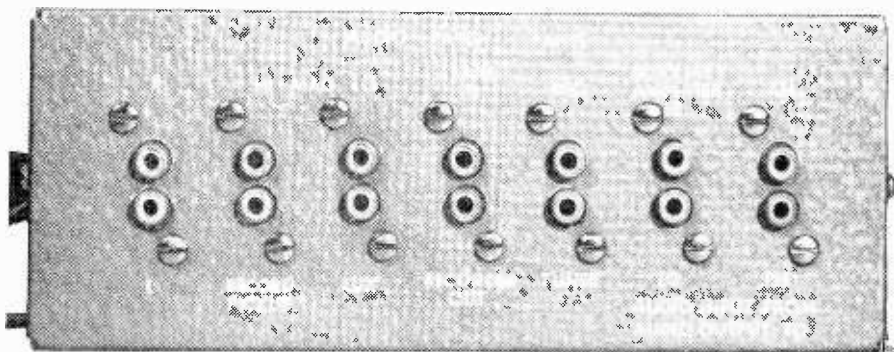
Drilling Chassis Holes

• When drilling holes in the metal chassis of electronics gear, there's a good possibility that some of the metal chips will fall between contact points on the underside of the chassis and cause a short circuit. To prevent this, apply a wide strip of masking tape to the underside of chassis where the drill will come through, to catch and hold the chips. Once the hole has been drilled, remove the tape, being especially careful not to spill the metal chips.



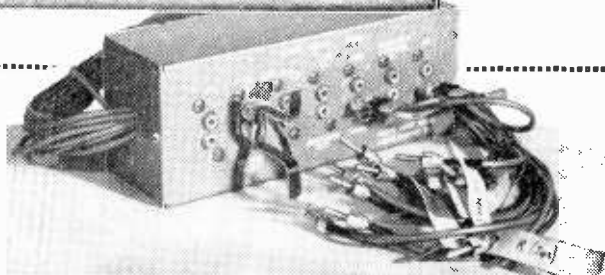
**SOLUTION TO
ELECTRON
TUBE
ANAGRAM
Page 130**





1

The far-flung connections made by the connectors in the foreground of the photo at right are all brought into one plane for easy handling in the patch-panel. A patch plug and patch cord are shown plugged in to connect inputs of one unit to outputs of others. On the chassis, lettering stands for: R and L, stereo head; HI and LO MAG., AUX, TAPE IN, MIC., and TUNER, terminations found on rear panel of a DB-110 amplifier; AM and FM are tuner outputs, as is RECORDER OUT; RECORD PICKUP jack connects to monaural disc head; AUXILIARY AMPLIFIER, HI and LO refer to inputs of a second amplifier for stereo; AUDIO INPUT FROM and AUDIO OUTPUT to refer to color coding that simplifies making connections.



Audio Patch-Panel

Build this \$10 version of a broadcast station patchboard to broaden the use of your hi-fi components

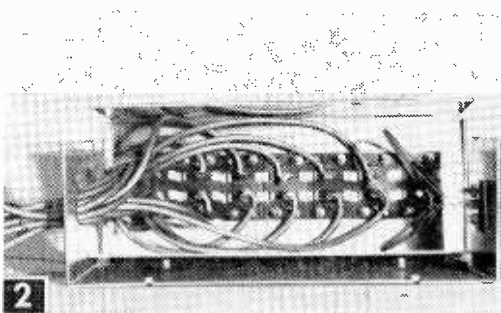
BY DON SCHROEDER

EASY to wire in an evening, this audio patch panel will enable you to set up practically any combination of audio components without delay, and without fumbling for matched cords and connectors.

For many years, audio engineers have used patchboards to quickly connect combinations of equipment in broadcast stations, recording studios, and theatres. These panels offer not only convenience, but a complete variety of possible combinations. But the broadcaster has a great advantage over the hi-fi enthusiast in that most of his lines are low impedance and thus less vulnerable to screaming or hum.

This article describes an easily assembled high-impedance patch panel that will greatly facilitate the connection changes required for straight play-back of records, dubbing discs onto tapes, or any other connection it might be desirable to make. With it, all inputs become accessible in one location, eliminating the need to pull amplifiers off shelves or out of cabinets to get access to rear or underside terminals. It also simplifies the adapter fitting problem that plagues most audiophiles because all changes are made with RCA type plugs.

Construction. The patch panel shown in Fig. 1 was designed for use with a Bogen DB-110 amplifier. It therefore includes all those jacks that are present on the back of that model amplifier. It will probably be necessary to change these to suit your particular amplifier. The important thing to bear in



Interior wiring is not difficult and is further simplified by the use of double jacks. All shields are grounded in the box but only one is grounded at the plugs going to any one unit, to avoid ground loops and hum. Two pairs of jacks are connected together at the right. These take care of the tuners which usually come equipped with an output cord.

Portable Radio-Phonograph

Here's a transistorized radio and phonograph turntable that operates off batteries. You can take it, and use it, anywhere

By HOMER L. DAVIDSON



In the home, on the beach, in the air, overseas—wherever you happen to be or go, this radio-phono combination can go with you.



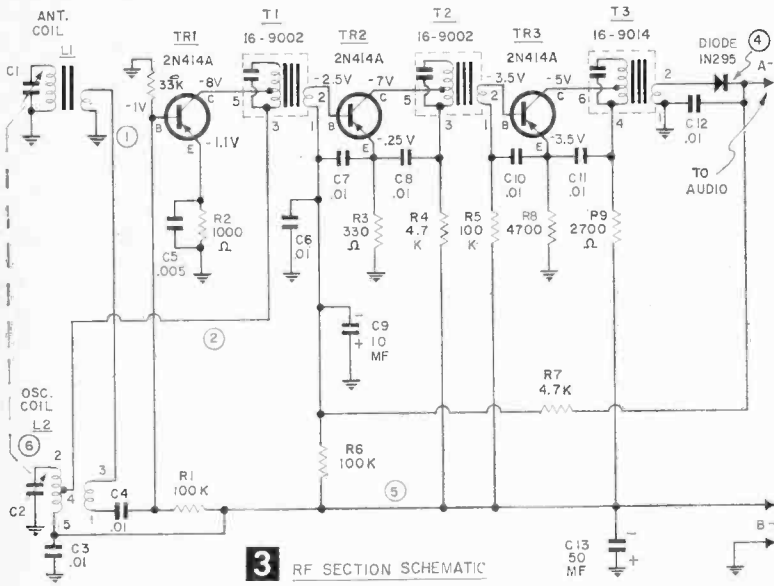
Belling and catch on case are available in dime stores.

THE RF section of the radio circuit of this portable consists of three RF transistors and a fixed diode rectifier (see Fig. 3). Transistor TR1 is the oscillator mixer stage, TR2 and TR3 are IF amplifiers. The intermediate frequency is 445 kilocycles. This IF signal is rectified to audio frequency by the fixed crystal diode.

A 3 x 11-in. printed circuit board is used as a subchassis for the RF and audio circuit (see Fig. 5 for RF section

MATERIALS LIST—PORTABLE RADIO-PHONOGRAPH

Desig.	Description	Desig.	Description
RF SECTION			
C1, C2	Variable capacitor, RF section 6.3 to 123.1 mfd; osc. section 5.7 to 78.2 mfd—Lafayette MS261	R3	330 ohm, 1/2 watt resistor
C3, C4, C6, C7, C8 C10, C11, C12	.01 mfd disc capacitors	R4, R7, R8	4.7k ohm, 1/2 watt resistor
C5	.005 mfd disc capacitor	R9	2700 ohm, 1/2 watt resistor
C8	10 mfd 25 v elec. capacitor	R10	33k ohm, 1/2 watt resistor
C13	50 mfd 25 v elec. capacitor	L1	ant. loop, 700 mh (Lafayette MS-264)
R1, R5, R6	100k ohm, 1/2 watt resistor	L2	osc. coil (Lafayette MS-265 or equiv.)
R2	1000 ohm, 1/2 watt resistor	T1, T2	Meisner 16-9002 455 kc IF transformer
C14	8 mfd 25 v electrolytic capacitor	T3	Meisner 16-9014 455 kc output IF transformer
C15	.05 mfd 200 v paper capacitor	TR1, TR2, TR3	Raytheon 2N414A transistors (PNP)
R10	10k volume control, with sw	diode	Raytheon 1N295 fixed diode
R11	470k ohm, 1/2 watt resistor	AUDIO SECTION	
R12	12k ohm, 1/2 watt resistor	T5	AR119 Argonne output transformer PRI 500 ohm C. T.; sec. 3.2 ohm
R13	3000 ohm, 1/2 watt resistor	SW1	SPST switch on rear of R10
R14	68 ohm, 1/2 watt resistor	Batteries	9-volt (Eveready #276 or equiv.)
R15, R16	10 ohm, 1/2 watt resistor	Spk. jack	standard female phono jack
TR4	2N107 GE transistor (PNP)	1	pickup arm and crystal (PK-89 phono arm and cartridge, Lafayette)
TR5, TR6	2N188 GE transistor (PNP)	1	6-volt phono motor, 45 rpm, 33 1/3, 16 rpm (Lafayette)
T4	AR109 Argonne transformer driver PRI 10,000 ohm; sec. 2000 C.T.	SW2	rotating DPDT switch
PRINTED CIRCUIT			
1 pt.	PE-5 liquid etchant	1	6-volt battery (Eveready #409 or equiv.)
1	XXXP copper laminated board (3 x 11" cut from 12" piece)	1 roll	PRLT ball point pen tape resist



3 RF SECTION SCHEMATIC

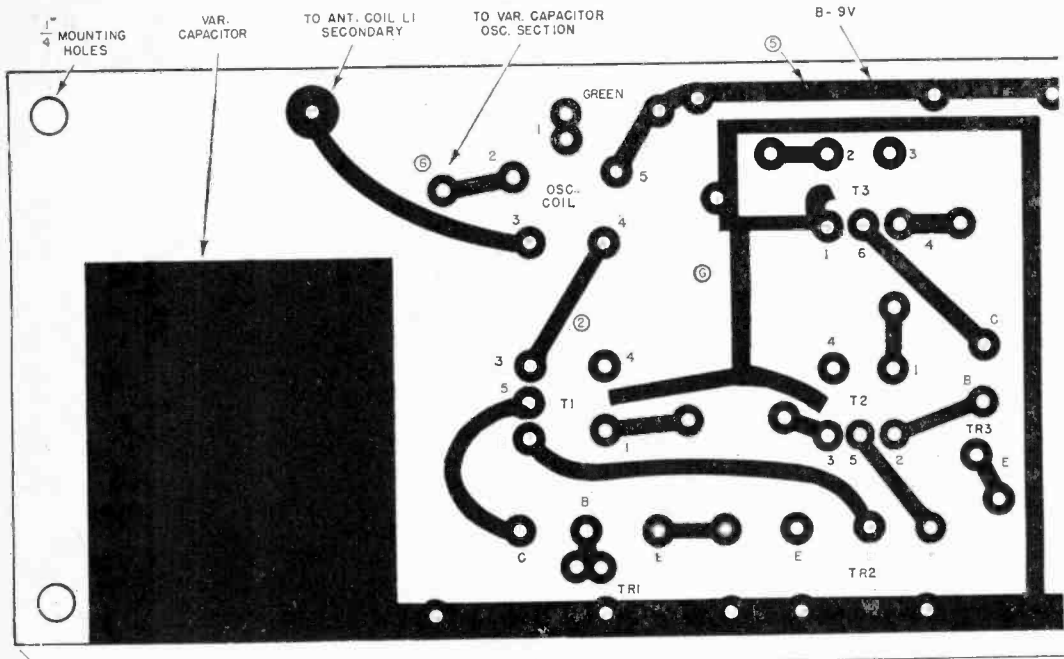
switched into the phono-graph circuit, with a separate battery for this circuit since the radio operates off 9 v.

Printed Circuit. Wash the copper side of the PC board with soap and water, and then trace on it the RF and audio circuits through carbon paper. Unroll resist tape and apply, using a sharp pocket knife to cut all corners. Dots can be made with a ball-point resist paint by simply pressing down on the ball point of the pen.

When the circuits have been completely laid out on the printed board, pour enough etching solution into a

and Fig. 6 for audio section portions of the PC board). The audio circuit consists of an audio amplifier with a volume control in the base circuit of TR4. The last two audio stages are operated push-pull for greater amplification. This little portable has two 5 x 7-in. PM speakers in the output and pulls only 10 ma with full volume. A 6-v phono-motor is

tray to sufficiently cover the board. The solution should be agitated or rocked back and forth to quicken the etching process. It will take about one hour to complete the process. Wash the finished board in cold-running water, wash out the etching tray or dish, and pour the remaining solution back into the bottle. It can be used again. Remove the tape



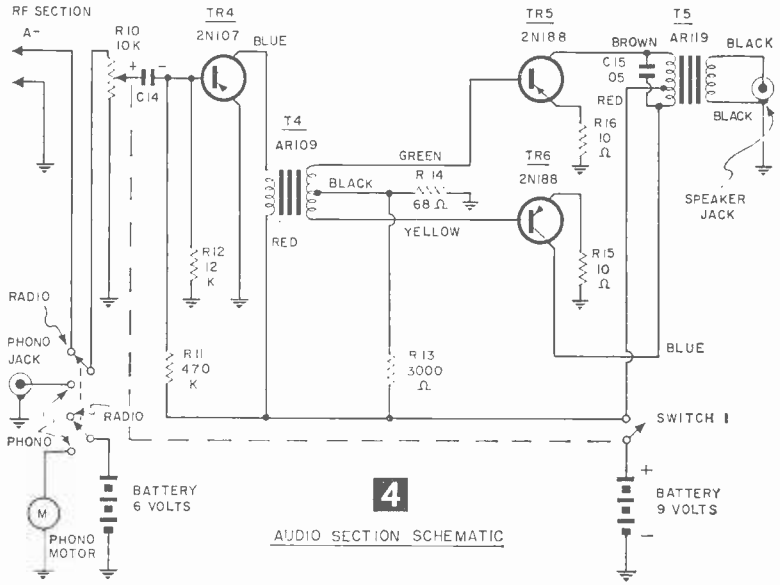
(ACTUAL SIZE)

5 RF SECTION P.C. (SEE FIG. 3)

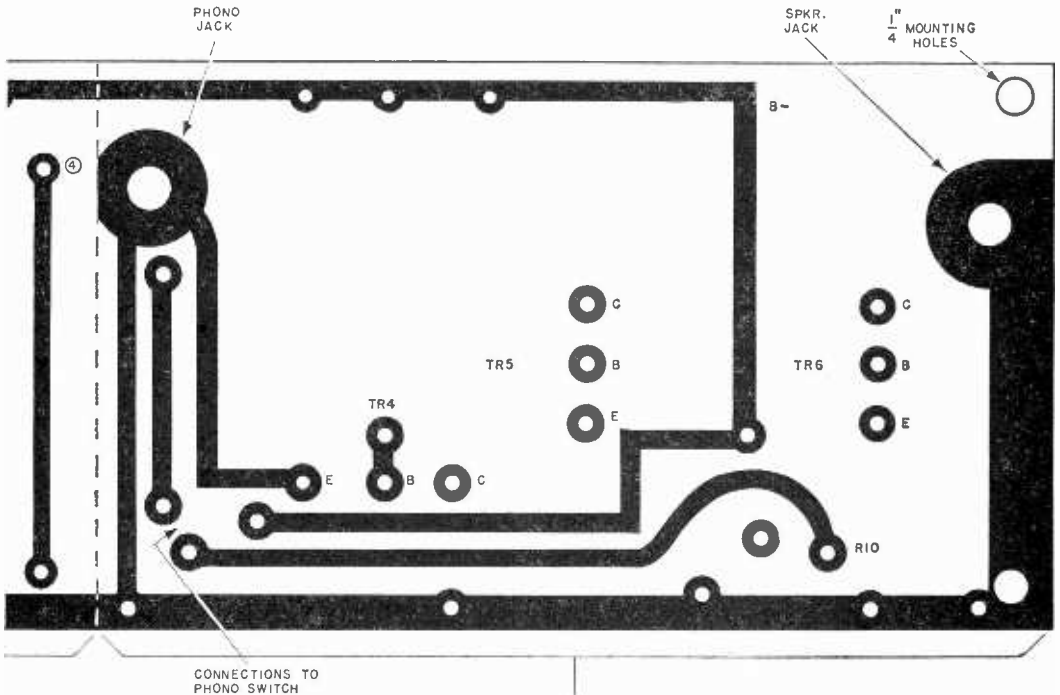
and pen resist paint. Now drill all holes in the printed circuit board before mounting any parts. A very small drill should be used for all small parts such as resistor, capacitors, and transistor wires. The phono and speaker jacks take 3/8-in. dia. holes. At the two ends of the printed circuit board drill 1/4-in. holes for mounting the PC board on the wooden cabinet.

Mounting Components.

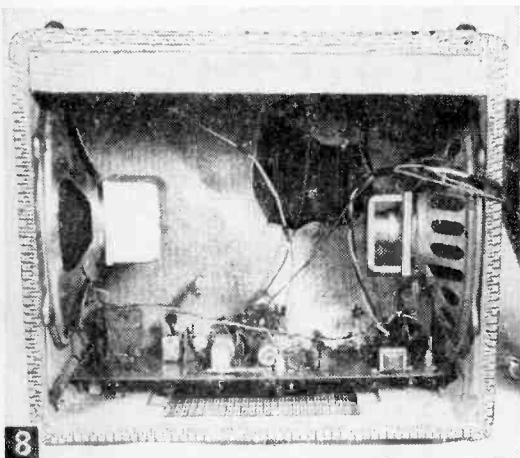
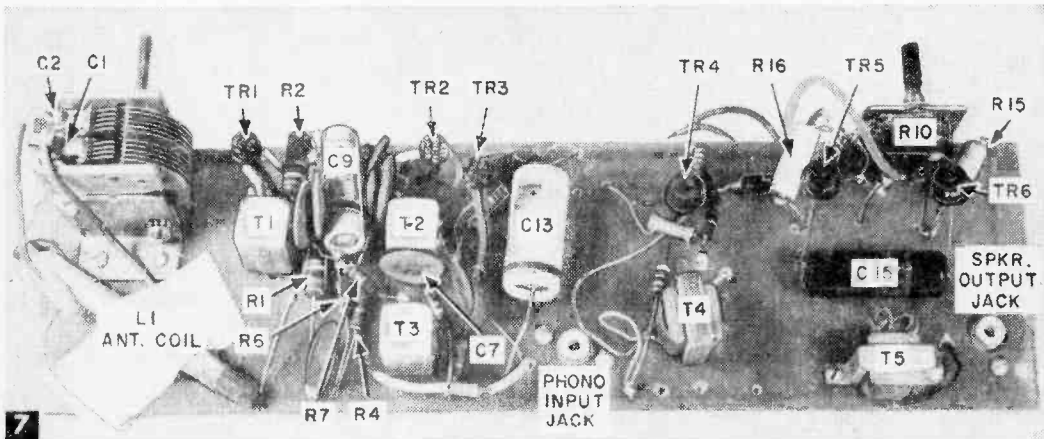
All the small parts are mounted as they are wired into the circuit. Wait until the last thing to solder to the circuit so that excessive heat on a given point will not ruin them. The variable capacitor and volume control are bolted to the printed chassis, as are the phono and speaker jacks. The small antenna is temporarily taped to the printed board while alignment and mounting is done (see Fig. 7). If you have a signal generator, you already know how to



do the IF and RF receiver alignment. (See "How To Align Superhet Circuits," p. 66, *Radio-TV Experimenter*, No. 559, 75¢ from *Science and Mechanics*, 450 East Ohio Street, Chicago 11, Ill.) If not, the local radio and television shop can easily do a professional job of alignment of the small portable receiver.



6 AUDIO SECTION P.C. (SEE FIG. 4)

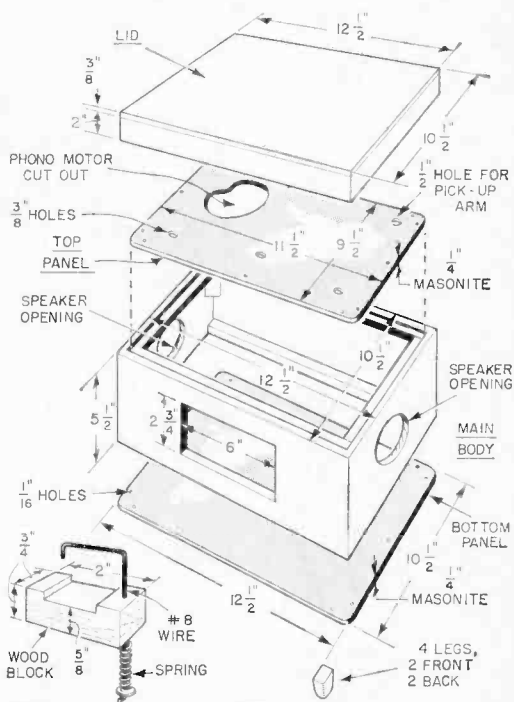


Looking up into cabinet. Speakers mount at opposite ends of case.

Test the audio portion of the printed circuit board first. Do all alignment and testing of the chassis before it is mounted in the cabinet. Turn the switch on and the volume up half-way, and plug the crystal pickup arm into the audio phono jack. A noise should be heard. Rub your finger over the needle and a scratchy sound will be audible. The radio portion can be checked by simply turning the switch to the radio position, and aligning first the IF stages with a signal generator, then the RF section.

Cabinet Construction. After the receiver and phonograph printed circuit board has been thoroughly tested it is ready to be mounted into the cabinet. The cabinet can be made from 3/8-in. plywood. If you already have a case, be sure it is large enough to take both chassis and speakers.

The speakers mount at the ends of the cabinet (see Fig. 8). A piece of 1/4-in. Masonite was cut and drilled for the top panel to



9 PHONO ARM HOLDER

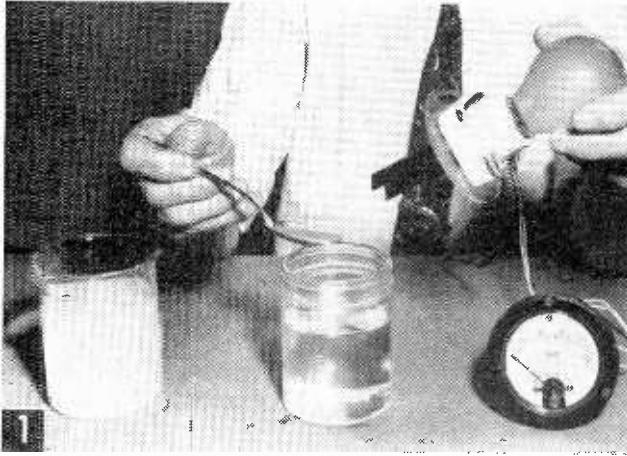
10 CABINET CONSTRUCTION

hold the record player and phono pickup arm, and another piece of 1/4-in. Masonite was cut and drilled for the bottom, as in Fig. 10.

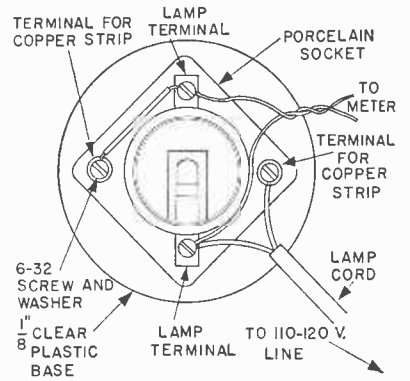
Cover the cabinet with plastic grille cloth, stapling it to the case. Apply glue around the speaker holes before stapling. Both Masonite panels and the top phono-lid were sprayed with red enamel paint.

The small batteries were bracketed to the bottom Masonite panel. A small wooden block and No. 8 wire form a holder (see Fig. 9) to secure the phono arm to the cabinet when transporting this portable.

Measuring the Conductivity of Liquids

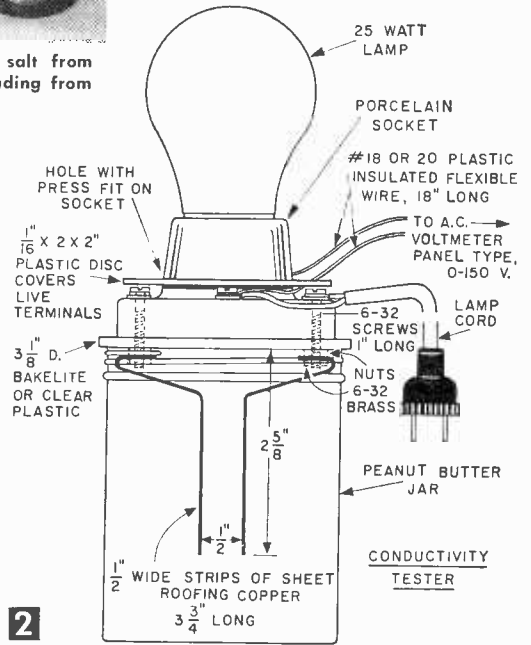


1 Adding a teaspoonful of saturated solution common salt from beaker at left to test jar of water, upped voltmeter reading from 10 to 112.

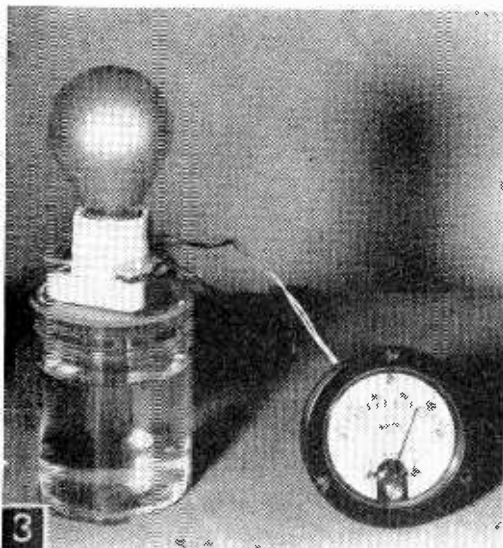


SOME liquids conduct electricity better than others. You can test this fact with the setup shown in Fig. 2. Two strips of sheet copper secured to the underside of a plastic disc are immersed in the liquid to be tested. A meter connected across the lamp terminals indicates voltage applied to the lamp.

With this setup, we found, for example, that the voltmeter registered 10 volts with pure water in the peanut butter jar. We then



2



3 Teaspoonful of saturated bicarbonate of soda resulted in a lighted lamp and 108-volt reading.

added one teaspoonful of a saturated solution of common salt to the pure water (Fig. 1). The voltmeter reading jumped up to 112 volts, and the lamp burned brightly. No wonder medical technicians use salt-soaked pads when attaching various types of electrical equipment to the body!

Figure 3 shows an experiment using a teaspoonful of bicarbonate of soda from a saturated solution placed in a fresh jar of water. Here the voltmeter registers 108 volts, as against 112 for salt.

Figure 4 shows how a teaspoon of vinegar results in 58 volts to the lamp, indicating conductivity better than water but not nearly

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'couple-two' circuit provides up to 5 db gain (per set) as an amplified two-set coupler

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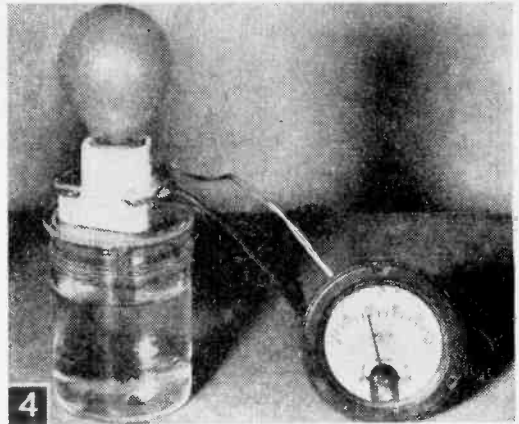
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9 Alling Street, Dept. RX-60, Newark 2, N. J.

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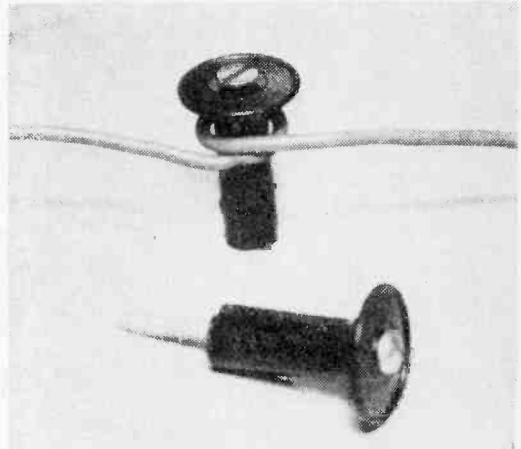
Teaspoonful of vinegar produced reading of 58 volts.

so high as either salt or soda.

For accurate comparisons, use the same quantity of each additive, e.g. a teaspoonful. You'll find salammoniac (ammonium chloride) similar to salt in conductivity. A few drops of dilute sulphuric acid (battery acid) will show a surprising degree of added conductivity to water.

Caution: Do not try any but aqua solutions—an inflammable liquid could easily be touched off in contact with the copper electrodes. Also, don't leave your test setup plugged in, or out where youngsters can poke around its live terminals under the plastic guard ring.—HAROLD P. STRAND.

Film Spools As Wire Stand-Offs



• Those plastic spools that 120 film comes wound around can be made into low-loss, no-cost stand-off insulators for wires such as radio lead-in. Cut the spool in half, drill a hole through the inside and insert a long wood-screw. Wrap one turn of the wire around the insulator near the flange as shown.



WHITE'S RADIO LOG

An up-to-date broadcasting directory
AM, FM, TV and Short-Wave Stations

Vol. 37 No. 2

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U. S. and Canadian AM Stations by Frequency

U.S. stations listed alphabetically by states within groups, Canadian stations precede U.S. Abbreviations: Kc., frequency in kilocycles; W.P., watt power; d—operates daytime only. Wave length is given in meters

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
540—555.5			WSAU Wausau, Wis.	5000		WSHE Raleigh, N.C.	500d		KFXM San Bernardino, Cal.	1000	
CBK Regina, Sask.	5000d		560—535.4		WKBN Youngstown, Ohio	5000		KCSJ Pueblo, Colo.	1000		
KVIP Redding, Calif.	1000d		CFRA Ottawa, Ont.	5000	WNAX Yankton, S.Dak.	5000		WDLF Panama City, Fla.	1000		
KFMB San Diego, Calif.	5000		CJKL Kirkland Lake, Ont.	5000	WFAA Dallas, Tex.	5000		WPLD Atlanta, Ga.	5000		
WGTO Cypress Gardens, Fla.	5000d		CFOS Owen Sound, Ont.	1000	WBAP Ft. Worth, Tex.	5000		KID Idaho Falls, Idaho	5000		
WDAK Columbus, Ga.	5000		WOOF Dothan, Ala.	5000d	KLUB Salt Lake City, Utah	5000		WFLK Lexington, Ky.	5000		
KBRV Soda Springs, Idaho	5000		KSFO San Fran., Calif.	5000	KVI Seattle, Wash.	5000		WEEI Boston, Mass.	5000		
KWMT Ft. Dodge, Iowa	1000d		KLZ Denver, Colo.	1000	WMAM Marinette, Wis.	250		WKZO Kalamazoo, Mich.	5000		
WDMV Pocomoke City, Md.	1000d		WQAM Miami, Fla.	5000	580—516.9			WOW Omaha, Nebr.	5000		
WBIC Islip, N.Y.	250d		WIND Chicago, Ill.	5000	CJFX Antigonish, N.S.	5000		WROW Albany, N.Y.	5000		
WONG Canonsburg, Pa.	250d		WMIK Middlesboro, Ky.	5000	CKEY Toronto, Ont.	5000		WGTM Wilson, N.C.	5000		
WDXN Clarksville, Tenn.	1000d		WGAN Portland, Maine	5000	KRPD Ft. William, Ont.	3000		KUGN Eugene, Ore.	5000		
WRIC Richlands, Va.	1000d		WHYN Springfield, Mass.	1000	CKUA Edmonton, Alta.	1000d		WARM Scranton, Pa.	5000		
			WMIC Monroe, Mich.	5000d	CKY Winnipeg, Man.	5000d		WMBS Uniontown, Pa.	1000		
550—545.1			WEBC Duluth, Minn.	5000	WABT Tuskegee, Ala.	5000		KTBC Austin, Tex.	5000		
CFNB Fredericton, N.B.	5000d		KWTO Springfield, Mo.	5000	KTAN Tucson, Ariz.	5000		KSUB Cedar City, Utah	1000		
CFBR Sudbury, Ont.	1000		KMON Great Falls, Mont.	5000	KMJ Fresno, Calif.	5000		WLVA Lynchburg, Va.	1000		
CFLN Three Rivers, Que.	250		WGAI Elizabeth City, N.C.	1000	KUBC Montrose, Colo.	5000		KHQ Spokane, Wash.	5000		
CKPG Prince George, B.C.	250		WFL Philadelphia, Pa.	5000	WGAC Augusta, Ga.	5000		600—499.7			
KKEN Anchorage, Alaska	5000		WIS Columbia, S.C.	5000	KFXD Nampa, Idaho	5000		CFCF Montreal, Que.	5000		
KOY Phoenix, Ariz.	5000		WHBQ Memphis, Tenn.	5000	WILL Urbana, Ill.	5000d		CFCH North Bay, Ont.	1000		
KAFY Bakersfield, Calif.	1000		WHDQ Beaumont, Tex.	5000	KSAC Manhattan, Kans.	5000		CFQC Saskatoon, Sask.	5000		
KRAI Craig, Colo.	1000		KPQ Wenatchee, Wash.	5000	WIBW Topeka, Kans.	5000		CJOR Vancouver, B.C.	5000		
WGGA Gainesville, Ga.	5000		WJLS Beckley, W.Va.	5000	KALB Alexandria, La.	5000		CKCL Truro, N.S.	1000		
KMVI Wailuku, Hawaii	1000		570—526.0		WTAG Worcester, Mass.	5000		WRB Enterprise, Ala.	1000		
KFRM Concordia, Kansas	5000d		CKEK Cranbrook, B.C.	1000	WAGR Lumberton, N.C.	5000		KCLS Flagstaff, Ariz.	5000		
WBCI Columbus, Miss.	1000		CKCQ Quessel, B.C.	1000	WHP Harrisburg, Pa.	5000		KFCV Redding, Calif.	1000		
KSD St. Louis, Mo.	5000		CJEM Edmundston, N.B.	1000	WKAQ San Juan, P.R.	5000		KFSD San Diego, Calif.	5000		
KOPR Butte, Mont.	1000		WAAX Gadsden, Ala.	5000	KOBH Hot Springs, S.Dak.	500d		WFCQ Bridgeport, Conn.	1000		
WGR Buffalo, N.Y.	5000		KCNO Alturas, Calif.	1000	WRKH Rockwood, Tenn.	1000d		WFDQ Jacksonville, Fla.	5000		
WDBM Statesville, N.C.	500d		KLAC Los Angeles, Calif.	5000	KDAY Lubbock, Tex.	500d		WMT Cedar Rapids, Iowa	5000		
KFYR Bismarck, N.Dak.	5000		WGMS Washington, D.C.	5000d	WCHS Charleston, W.Va.	5000		WYFE New Orleans, La.	1000d		
WKRC Cincinnati, Ohio	5000		WACL Waycross, Ga.	5000	WKTY LaCrosse, Wis.	5000		WFST Caribou, Maine	5000d		
KOAC Corvallis, Oreg.	5000		KYKB Paducah, Ky.	5000	590—508.2			WCAO Baltimore, Md.	5000		
WHLM Bloomsburg, Pa.	5000		WVMI Biloxi, Miss.	1000d	CFAR FlinFlon, Man.	1000		WLST Escanaba, Mich.	1000d		
WPAB Ponce, P.R.	5000		KGRT Las Cruces, N.Mex.	1000d	CKAR Huntsville, Ont.	1000		WTAC Flint, Mich.	1000		
WPAW Pawtucket, R.I.	1000d		WMOA New York, N.Y.	5000	CKRS Jonquiere, Que.	1000d		KGEZ Kalispell, Mont.	2000		
KCBS Midland, Tex.	5000		WSYR Syracuse, N.Y.	5000	VOCM St. Johns, N.F.	1000d		WCVP Murphy, N.C.	1000d		
KTSA San Antonio, Tex.	5000		WWNC Asheville, N.C.	5000	WRAG Carrollton, Ala.	1000d					
WDEV Waterbury, Vt.	5000				KBHS Hot Springs, Ark.	5000d					
WSVA Harrisonburg, Va.	5000										

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	
WSJS	Winston-Salem, N.C.	5000	WESC	Greenville, S.C.	5000d	CBL	Toronto, Ont.	50000	WJAT	Swainsboro, Ga.	1000d	
KSJB	Jamestown, N.D.	5000	KSXY	Dallas, Tex.	1000	WBAM	Montgomery, Ala.	50000d	WXIC	Iowa City, Iowa	1000d	
WFRM	Gaudesport, Pa.	1000d	670-447.5			KUEP	Phoenix, Ariz.	1000d	WRUS	Russellville, Ky.	1000d	
WAEI	Maryager, P.R.	1000	WMAQ	Chicago, Ill.	50000	KBIG	Albany, Calif.	1000d	WBOK	New Orleans, La.	1000d	
WREC	Memphis, Tenn.	1000	680-440.9			KCBS	San Francisco, Calif.	50000	WCCM	Lawrence, Mass.	1000d	
WED	El Paso, Tex.	5000	CHFA	Edmonton, Alta.	5000	KSSS	Colorado Springs, Colo.	1000	KREI	Farrington, Mo.	1000d	
KERB	Kermit, Tex.	1000d	CHLO	St. Thomas, Ont.	1000	KVFC	Cortez, Colo.	1000d	KDBM	Dillon, Mont.	1000d	
KTBB	Tyler, Tex.	1000	CJWB	Winnipeg, Man.	1000	WKIS	Orlando, Fla.	5000	WKDN	Camden, N.J.	1000d	
610-491.5			CKGB	Birmingham, Ala.	1000d	KYME	Boise, Idaho	5000	KJEM	Oklahoma City, Okla.	250d	
CHNC	New Carlisle, Que.	5000	KNBC	San Fran., Calif.	50000	WVLN	Olney, Ill.	250d	KPQD	Portland, Ore.	1000d	
CJAT	Trail, B.C.	1000	WPIN	St. Petersburg, Fla.	1000d	KBOE	Oskaloosa, Iowa	250d	WCHA	Chambersburg, Pa.	1000d	
CKKL	Thompson, Man.	1000	WCTT	Corbin, Ky.	1000	WNOB	Newport, Calif.	1000d	WDSG	Dillon, S.C.	1000d	
CKTB	St. Catharines, Ont.	5000	WCBM	Baltimore, Md.	10000	WFRB	Frostburg, Md.	250d	WTAO	Cambridge, Mass.	250d	
WSGN	Birmingham, Ala.	5000	WNAE	Lawrence, Mass.	50000	KPBM	Carlsbad, N.Mex.	1000d	KDDH	Dumas, Tex.	250d	
KAFL	Lancaster, Calif.	1000	WDBC	Escanaba, Mich.	1000	WGSN	Huntington, N.Y.	1000d	KBUH	Brigham City, Utah	250d	
KFRK	San Francisco, Calif.	5000	KFEQ	St. Joseph, Mo.	5000	WMBL	Morehead City, N.C.	1000d	WVSV	Crewe, Va.	1000d	
WKOR	Miami, Fla.	5000	WNRN	Singhanton, N.Y.	1000	WPAQ	Mount Airy, N.C.	1000d	WKEE	Huntington, W.Va.	1000d	
WDEB	Pensacola, Fla.	5000	WRVM	Rochester, N.Y.	250d	KRMG	Tulsa, Okla.	5000	WDUX	Waupaca, Wis.	1000d	
WCEH	Hawkinsville, Ga.	5000d	WPTF	Raleigh, N.C.	50000	WBSJ	Santurce, P.Rico	1000d	810-370.2			
WRUS	Russellville, Ky.	5000d	WIRJ	Butler, Pa.	250d	WBAW	Barnwell, S.C.	500d	CFAX	Victoria, B.C.	1000d	
KDAL	Duluth, Minn.	5000	WAPA	San Juan, P.Rico.	10000	WIRJ	Humbolt, Tenn.	250d	KGO	San Francisco, Calif.	50000	
WDAF	Kansas City, Mo.	5000	WMP5	Memphis, Tenn.	10000	WJIG	Tullahoma, Tenn.	250d	WABW	Annapolis, Md.	250d	
KOJM	Havre, Mont.	1000	KENS	San Antonio, Tex.	50000	KTRH	Houston, Tex.	50000	KCMO	Kansas City, Mo.	50000	
WGR	Manchester, N.H.	5000	KOMW	Omaha, Wash.	10000	750-399.8		WGY	Schenectady, N.Y.	50000		
KGGM	Albuquerque, N.Mex.	5000	690-434.5			WSB	Atlanta, Ga.	5000	WKB	New York, N.Y.	1000d	
WPS	Charlottesville, Va.	5000	CBV	Vancouver, B.C.	10000	WBMD	Baltimore, Md.	1000d	WCCB	Rocky Mount, N.C.	1000d	
WTVN	Columbus, Ohio	5000	CBF	Montreal, Que.	50000	KMMJ	Grand Island, Neb.	1000	WEDD	McKeesport, Pa.	1000d	
WIP	Philadelphia, Pa.	5000	WVOK	Birmingham, Ala.	50000d	WHEB	Forsyth, N.H.	1000	WKVM	San Juan, P.R.	25000	
KILT	Houston, Tex.	5000	KVNA	Flagstaff, Ariz.	1000	WED	Durham, N.C.	250d	820-365.6			
KVNU	Logan, Utah	1000	KEVT	Tucson, Ariz.	250d	KXL	Portland, Ore.	1000	WAIT	Chicago, Ill.	5000d	
WPSL	Roanoke, Va.	5000	KBA	Benton, Ark.	250d	WPD	Clarkburg, W.Va.	1000d	WIKY	Evansville, Ind.	250d	
KEPR	Kennecik, Wash.	5000	KAPI	Pueblo, Colo.	250d	760-394.5		WOSU	Columbus, Ohio	5000d		
620-483.6			WADS	Ansonia, Conn.	500	KGU	Honolulu, Hawaii	10000	KIKI	Honolulu, Hawaii	5000	
CFCL	Timmins, Ont.	10000	WAPD	Jacksonville, Fla.	25000d	WJR	Detroit, Mich.	5000	WFAA	Dallas, Tex.	2500	
CKCK	Regina, Sask.	5000	KULA	Honolulu, Hawaii	10000	WCPS	Tarboro, N.C.	1000	WBAP	Ft. Worth, Tex.	50000	
KTAR	Phoenix, Ariz.	5000	KBLI	Blackfoot, Idaho	1000d	770-389.4		830-361.2				
KWES	Hanford, Calif.	1000d	KGCF	Coffeyville, Kans.	10000	KUOM	Minneapolis, Minn.	5000d	WCCO	Minneapolis, Minn.	50000	
KWSD	Mt. Shasta, Calif.	1000d	WITX	New Orleans, La.	50000	WCAL	Northfield, Minn.	5000d	KBA	Kennett, Mo.	5000d	
KSTR	Grand Junction, Colo.	5000d	KSTL	St. Louis, Mo.	1000d	WCB	Fort Worth, Tex.	1000d	WVVC	New York, N.Y.	1000d	
WSUN	St. Petersburg, Fla.	5000	KRCD	Princeton, Ore.	1000d	WAB	San Antonio, Tex.	5000	840-356.9			
WTRP	LaGrange, Ga.	1000d	KUSD	King Hill, S.Dak.	1000d	WBC	Albuquerque, N.Mex.	5000	WKAB	Mobile, Ala.	1000d	
KWAL	Wallace, Idaho	1000	KHEY	El Paso, Tex.	10000	WAB	New York, N.Y.	5000	WKNB	New Britain, Conn.	1000d	
KMNS	Sioux City, Iowa	1000	KPET	Lamesa, Tex.	250	KXA	Seattle, Wash.	10000	WHAS	Louisville, Ky.	1000d	
WMT	Louisville, Ky.	5000	KZEY	Tyler, Tex.	250d	780-384.4		WVPO	Stroudsburg, Pa.	250d		
WLBZ	Bangor, Maine	5000	WCYB	Bristol, Va.	10000d	WBBM	Chicago, Ill.	50000	850-352.7			
WJDX	Jackson, Miss.	5000	WNNT	Warsaw, Va.	250d	WJAG	Norfolk, Neb.	1000	CKVL	Verdun, Que.	50000	
WVNI	Newark, N.J.	5000	WELD	Fisher, W.Va.	500d	WCKB	Dunn, N.C.	1000d	CKRD	Red Deer, Alta.	1000	
WHEN	Syracuse, N.Y.	5000	700-428.3		WCKB	Dunn, N.C.	1000d	WYDE	Birmingham, Ala.	1000		
WDNC	Durham, N.C.	5000	WLW	Cincinnati, Ohio	50000	KSPI	Stillwater, Okla.	250d	KOA	Denver, Colo.	50000	
KGW	Portland, Ore.	5000	710-422.3		WARK	Arlington, Va.	1000d	WRUF	Gainesville, Fla.	5000		
WYWB	Greensboro, Pa.	1000	CJSP	Leamington, Ont.	1000d	CBY	Corner Brook, N.F.	1000	WEAT	W. Palm Beach, Fla.	1000	
WCAY	Caeco, S.C.	5000	CFRG	Lambourgh, Sask.	5000d	CKMR	Newcastle, N.B.	1000	KIM	Hew, Hawaii	1000	
WATE	Knoxville, Tenn.	5000	CKVM	Ville Marie, Que.	1000	CKSO	Sudbury, Ont.	1000	WHDH	Boston, Mass.	50000	
WKFT	Wichita Falls, Tex.	5000	WKR	Mobile, Ala.	1000	WTUG	Tuscaloosa, Ala.	1000	WKBS	Muskegon, Mich.	1000	
WCAX	Burlington, Vt.	5000	KMPC	Los Angeles, Calif.	50000	KEE	Tucson, Ariz.	1000	KFUD	St. Louis, Mo.	5000d	
WNNR	Beckley, W.Va.	1000	KICN	Denver, Colo.	5000	KDAN	Eureka, Calif.	5000d	WKIX	Raleigh, N.C.	10000	
WTMJ	Milwaukee, Wis.	5000	WGBS	Miami, Fla.	50000	KABC	Los Angeles, Calif.	5000	WJW	Cleveland, Ohio	5000	
630-475.9			WROM	Rome, Ga.	1000d	WLBE	Leesburg, Fla.	1000	WEEU	Reading, Pa.	5000	
CFCO	Chatham, Ont.	1000	KEEL	Shreveport, La.	10000	WPFA	Pensacola, Fla.	1000d	WRAP	Norfolk, Va.	5000	
CHLT	Sherbrooke, Que.	10000	WHB	Kansas City, Mo.	50000	WQXI	Atlanta, Ga.	5000	KTAC	Tacoma, Wash.	1000	
CHY	Charlottetown, P.E.I.	10000	WOR	Newark, N.Y.	50000	WQX	Cairo, Ga.	1000	860-348.6			
CJET	Smith Falls, Ont.	5000	DZRH	Manila, P.I.	1000	WXXX	Colton, Kans.	5000d	CJBC	Toronto, Ont.	50000	
CKRC	Winnipeg, Man.	5000	WKBJ	Mayaguez, P.Rico	1000	WAKY	Louisville, Ky.	5000	WHRT	Hartsville, Ala.	250d	
CKRO	Kelowna, B.C.	1000	WTPR	Parris, Tenn.	250d	WRUM	Rumford, Me.	1000	WAMI	Opp, Ala.	1000d	
CKYL	Pace River, Alta.	1000	KGNC	Amarillo, Tex.	10000	WSGW	Saginaw, Mich.	1000	KIFN	Phoenix, Ariz.	1000d	
WAVU	Albertville, Ala.	1000d	KURV	Edinburg, Tex.	50000	KGHL	Billings, Mont.	5000	KOSE	Oseola, Ark.	1000d	
WJDB	Thomasville, Ala.	1000d	KIRO	Seattle, Wash.	50000	WNNY	Watertown, N.Y.	1000	KTRF	Warren, Ark.	250d	
KJNO	Juneau, Alaska	1000d	WDSM	Superior, Wis.	5000	WLSV	Wellsville, N.Y.	1000	KWRB	Modesto, Calif.	1000d	
KYMA	Magnolia, Ark.	1000d	720-416.4		790-379.5		WTFN	Thomasville, N.C.	1000d	WKCO	Knoxville, Tenn.	250
KIDD	Monterey, Calif.	1000	WGN	Chicago, Ill.	50000	CKMR	Newcastle, N.B.	1000	WDM	Atlanta, Ga.	5000	
KHOW	Denver, Colo.	5000	730-410.7		CBY	Corner Brook, N.F.	1000	WERG	Douglas, Ga.	1000d		
WMAL	Washington, D.C.	5000	CJNR	Blind River, Ont.	1000	CKMR	Newcastle, N.B.	1000	WMRI	Marion, Ind.	250d	
WSAV	Savannah, Ga.	5000	CKAC	Montreal, Que.	50000	CKSO	Sudbury, Ont.	1000	KWPC	Muscateine, Iowa	250d	
KIDO	Boise, Idaho	5000	CKDM	Dauphin, Man.	1000	WTUG	Tuscaloosa, Ala.	1000	KOAM	Pittsburg, Kans.	10000	
WLAP	Lexington, Ky.	5000	CKLG	N. Vancouver, B.C.	10000	KEE	Tucson, Ariz.	1000	WSON	Henderson, Ky.	500d	
KTIB	Thibodaux, La.	500	KFKD	Anchorage, Alaska	10000	KOSY	Toxarkana, Ark.	1000	WQAF	Waukegan, Ill.	500d	
WJMS	Ironwood, Mich.	1000	WJMW	Athens, Ala.	1000d	KDAN	Eureka, Calif.	5000	WWSB	Gt. Barron, Mass.	250d	
KDWB	St. Paul, Minn.	5000	KNBY	Newport, Ark.	1000d	KABC	Los Angeles, Calif.	5000	WUBJ	New Urm, Minn.	1000d	
KXOK	St. Louis, Mo.	5000	WKTG	Thomasville, Ga.	1000d	WLBE	Leesburg, Fla.	1000	WFMG	Forest, Miss.	5000	
KGVV	Belgrade, Mont.	1000d	KBLR	Goodland, Kans.	1000d	WPFA	Pensacola, Fla.	1000d	WMO	Fairmont, N.C.	1000d	
KLOA	Reno, Nev.	5000	WFMW	Madisonville, Ky.	250d	WQXI	Atlanta, Ga.	5000	WALO	Homestead, Pa.	250d	
KLEA	Livingston, N.Mex.	5000	WMTV	Vanceville, Ky.	1000d	WQX	Cairo, Ga.	1000	WTLF	Philadelphia, Pa.	250d	
KRY	Hickory, N.C.	1000d	KTRY	Bastrop, La.	250d	WXXX	Colton, Kans.	5000d	WLBG	Laurens, S.C.	1000d	
WMFD	Wilmington, N.C.	1000	WARB	Covington, La.	1000d	WAKY	Louisville, Ky.	5000	WVVC	New York, N.Y.	1000d	
WEIL	Scranton, Pa.	500d	WMMS	Bath, Maine	500d	WRUM	Rumford, Me.	1000	WMTS	Murfreesboro, Tenn.	250d	
WPRO	Providence, R.I.	5000	WACE	Chicopee, Mass.	500d	WSGW	Saginaw, Mich.	1000	KFTS	Ft. Stockton, Tex.	250d	
KGFX	Pierre, S.Dak.	250	KWR	Warrenton, Mo.	500d	KGHL	Billings, Mont.	5000	KPAN	Hereford, Tex.	250d	
KMAC	San Antonio, Tex.	5000	KWOA	Worthington, Minn.	1000d	WNNY	Watertown, N.Y.	1000	KSA	Nacogdoches, Tex.	1000d	
KGDN	Edmunds, Wash.	1000d	KURL	Billings, Mont.	500d	WLSV	Wellsville, N.Y.	1000	KONO	San Antonio, Tex.	5000d	
KZUN	Opportunity, Wash.	500d	WDDS	Oneonta, N.Y.	1000d	WTFN	Thomasville, N.C.	1000	KWHO	Salt Lake City, Utah	1000d	
640-468.5			WFMC	Goldsboro, N.C.	1000d	CKSO	Sudbury, Ont.	1000	WEVA	Emporia, Va.	1000d	
CBN	St. John's, N.F.	10000	WHS	Shelby, N.C.	1000d	WTUG	Tuscaloosa, Ala.	1000	WOAY	Oak Hill, W.Va.	10000d	
KFI	Los Angeles, Calif.	50000	WHRW	Bowling Green, Ohio	250d	WNNY	Watertown, N.Y.	1000	WVFX	Milwaukee, Wis.	250d	
WQI	Ames, Iowa	5000	KBOY	Medford, Ore.	1000d	WLSV	Wellsville, N.Y.	1000	870-344.6			
WHLO	Akron, Ohio	1000	KNBY	Newport, Ark.	1000d	WQAF	Waukegan, Ill.	500d	KIEV	Glendale, Calif.	250d	
WNAD	Norman, Okla.	1000d	WKTG	Thomasville, Ga.	1000d	WQXI	Atlanta, Ga.	5000	KAIM	Kaimuki, Hawaii	1000	
650-461.3			KBLR	Goodland, Kans.	1000d	WQX	Cairo, Ga.	1000	WWL	New Orleans, La.	50000	
KPOA	Honolulu, Hawaii	10000	WFMW	Madisonville, Ky.	250d	WXXX	Colton, Kans.	5000d	WKR	E. Lansing, Mich.	5000d	
WSM	Nashville, Tenn.	50000	WMTV	Vanceville, Ky.	1000d	WAKY	Louisville, Ky.	5000	WGTU	Ithaca, N.Y.	1000d	
KROT	Baytown, Texas	250d	KTRY	Bastrop, La.	250d	WRUM	Rumford, Me.	1000	KJFM			

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
880—340.7			920—325.9			960—312.3			990—302.8		
WCBS New York, N.Y.	5000		CJCH Halifax, N.S.	10000	WGOV Valdosta, Ga.	5000	7400	5000	CKNW New Westminster,	5000	
WRRZ Clinton, N.C.	10000		CJCI Woodstock, N.B.	1000	KB01 Boise, Idaho	5000	7400	5000	CKNW Brit. Columbia	5000	
WRFD Worthington, Ohio	5000		CJCN Windham, Ont.	2500	WAAF Chicago, Ill.	10000	7400	5000	CFPL London, Ont.	10000	
890—336.9			930—322.4			970—309.1			1000—299.8		
WLS Chicago, Ill.	5000		WCTA Adalusia, Ala.	5000	WVBF Troy, Ala.	5000	7400	5000	WCFB Chicago, Ill.	5000	
WHNC Henderson, N.C.	10000		WWRW Russellville, Ala.	10000	WVBF Troy, Ala.	5000	7400	5000	WNOX Knoxville, Tenn.	10000	
KBYE Okla. City, Okla.	10000		KAR Little Rock, Ark.	5000	WVBF Troy, Ala.	5000	7400	5000	KWAM Memphis, Tenn.	10000	
900—333.1			940—315.6			1010—296.9			1000—296.9		
CKTS Sherbrooke, Que.	1000		WMEG Eau Gallie, Fla.	10000	WJAN Ishpeming, Mich.	5000	7400	5000	CBX Edmont, Alta.	5000	
CHML Hamilton, Ont.	5000		WGST Atlanta, Ga.	5000	WKHM Jackson, Mich.	1000	7400	5000	CFRB Toronto, Ont.	5000	
CHNO Sudbury, Ont.	10000		KAHU Wainhau, Hawaii	10000	KOOK Billings, Mont.	5000	7400	5000	KVNC Winslow, Ariz.	1000	
CJBR Rimouski, Que.	10000		WMOK Metropolis, Ill.	10000	KJLT No. Platte, Nebr.	5000	7400	5000	KLRA Little Rock, Ark.	10000	
CJVI Victoria, B.C.	1000		WBAA W. Lafayette, Ind.	5000	WNTA Newark, N.J.	5000	7400	5000	KLRA Little Rock, Ark.	10000	
CJBI Prince Albert, Sask.	10000		WFEN Philadelphia, Pa.	5000	WREB Buffalo, N.Y.	5000	7400	5000	CKCH Hilo, Hawaii	5000	
CJGX Yorkton, Sask.	10000		WTOW Whitesburg, Ky.	10000	WRCS Ashokic, N.C.	10000	7400	5000	KAYT Rupert, Idaho	10000	
WATV Birmingham, Ala.	10000		WBOX Bogalusa, La.	10000	WHT Center, Tex.	10000	7400	5000	WMAY Springfield, Ill.	10000	
WGOK Mobile, Ala.	10000		KTCO Jonesboro, La.	5000	WVFL Tampa, Fla.	5000	7400	5000	WAVE Louisville, Ky.	5000	
W0ZK Ozark, Ala.	10000		WPXI Lexington Pk., Md.	5000	WVFL Tampa, Fla.	5000	7400	5000	KSVA Alexandria, La.	10000	
KCPBR Fairbanks, Alaska	10000		WMPL Hancock, Mich.	10000	WVFL Tampa, Fla.	5000	7400	5000	WCSH Portland, Maine	5000	
KHOZ Harrison, Ark.	10000		KDHL Faribault, Minn.	10000	WVFL Tampa, Fla.	5000	7400	5000	WAMD Aberdeen, Md.	5000	
KBIF Centerville, Calif.	10000		KWAD Wadena, Minn.	10000	WVFL Tampa, Fla.	5000	7400	5000	WESO Southbridge, Mass.	10000	
WJWL Georgetown, Del.	10000		KRAM Las Vegas, Nev.	10000	WVFL Tampa, Fla.	5000	7400	5000	WJAN Ishpeming, Mich.	5000	
WJWN Belle Glade, Fla.	10000		KOLO Reno, Nev.	10000	WVFL Tampa, Fla.	5000	7400	5000	WKHM Jackson, Mich.	1000	
WMOP Ocala, Fla.	10000		KQEO Albuquerque, N.Mex.	10000	WVFL Tampa, Fla.	5000	7400	5000	KOOK Billings, Mont.	5000	
WCGA Calhoun, Ga.	10000		WTTM Trenton, N.J.	10000	WVFL Tampa, Fla.	5000	7400	5000	KJLT No. Platte, Nebr.	5000	
WCRY Macon, Ga.	2500		WKRT Cortland, N.Y.	10000	WVFL Tampa, Fla.	5000	7400	5000	WNTA Newark, N.J.	5000	
WJIV Savannah, Ga.	10000		WGHO Saugerties, N.Y.	5000	WVFL Tampa, Fla.	5000	7400	5000	WREB Buffalo, N.Y.	5000	
KSIR Wichita, Kan.	10000		WBBB Burlington, N.C.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WKYW Louisville, Ky.	10000		WMI Columbus, Ohio	5000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WLSI Pikeville, Ky.	10000		KGAL Texas, Oreg.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
KREH Oakdale, La.	2500		WKVA Lewistown, Pa.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WCME Brunswick, Maine	2500		WIAR Providence, R.I.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WATC Gaylord, Mich.	10000		WTND Orangeburg, S.C.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
KTIS Minneapolis, Minn.	10000		KEZU Rapid City, S.Dak.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WDDT Greenville, Miss.	10000		WLIV Livingston, Tenn.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
KFAL Fulton, Mo.	10000		KELP El Paso, Tex.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
KSKK Columbus, Nebr.	10000		KECK Odessa, Tex.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WOTW Nashua, N.H.	10000		KTLD Las Vegas, Nev.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WBRV Beaverville, N.Y.	10000		KITN Olympia, Wash.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WSPN Saratoga Springs, N.Y.	2500		KKLY Spokane, Wash.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WAYN Rockingham, N.C.	10000		WMMN Fairmont, W.Va.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
WIAM Williamston, N.C.	10000		WOKY Milwaukee, Wis.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVFL Tampa, Fla.	5000	
KFNW Fargo, N.Dak.	10000		930—322.4			970—309.1			1000—299.8		
WAND Canton, Ohio	5000		CJBC Saint John, N.B.	5000	KROF Abbeville, La.	10000	7400	5000	WVSC Somerset, Pa.	2500	
WFRO Fremont, Ohio	5000		CFCA Edmonton, Alta.	10000	WBOC Salisbury, Md.	5000	7400	5000	WVSC Somerset, Pa.	2500	
WCPA Clearfield, Pa.	10000		CJON St. John's, N.F.	10000	WFGM Fitchburg, Mass.	10000	7400	5000	WVSC Somerset, Pa.	2500	
WFLN Philadelphia, Pa.	10000		WETO Gadsden, Ala.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
WKXV Knoxville, Tenn.	10000		KTKN Ketchikan, Alaska	10000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
WCOR Lebanon, Tenn.	5000		KKPR Douglas, Ariz.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
KALT Atlanta, Tex.	10000		KHJ Los Angeles, Calif.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
KMCO Comroe, Tex.	5000		KIUP Durango, Colo.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
KFLD Floyd, Ohio	5000		WKSJ Milford, Del.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
KCLW Hamilton, Tex.	5000		WJAX Jacksonville, Fla.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
WAFG Staunton, Va.	10000		WKXY Sarasota, Fla.	10000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
KUEN Wenatchee, Wash.	500		WGRB Bainbridge, Ga.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
WATK Antigo, Wis.	2500		WTRD Quincy, Ill.	5000	WVFL Tampa, Fla.	5000	7400	5000	WVSC Somerset, Pa.	2500	
910—329.5			940—319.0			1010—296.9			1000—296.9		
CJDU Drumheller, Alta.	1000		CBM Montreal, Que.	5000	7400	5000	7400	5000	7400	5000	
CJLV Lindsay, Ont.	1000		CJGX Yorkton, Sask.	10000	7400	5000	7400	5000	7400	5000	
CFB Ottawa, Ont.	5000		CJJB Vernon, B.C.	10000	7400	5000	7400	5000	7400	5000	
CJFK Kamloops, B.C.	10000		KFRE Fresno, Calif.	50000	7400	5000	7400	5000	7400	5000	
CJRL Rogers, B.C.	10000		WINZ Miami, Fla.	50000	7400	5000	7400	5000	7400	5000	
KPHO Phoenix, Ariz.	5000		WMAZ Macon, Ga.	50000	7400	5000	7400	5000	7400	5000	
KLCN Blytheville, Ark.	5000		WMIX Mt. Vernon, Ill.	10000	7400	5000	7400	5000	7400	5000	
KAMD Camden, Ark.	1000		KIDM Iowa Falls, Iowa	10000	7400	5000	7400	5000	7400	5000	
KDEO El Cajon, Calif.	1000		WYLD New Orleans, La.	10000	7400	5000	7400	5000	7400	5000	
KEWB Oakland, Calif.	5000		WGRL Bend, Oreg.	10000	7400	5000	7400	5000	7400	5000	
KOXR Oxnard, Calif.	5000		WESA Charleroi, Pa.	250	7400	5000	7400	5000	7400	5000	
KOPF Ft. Ord, Calif.	5000		WIPR San Juan, P.R.	10000	7400	5000	7400	5000	7400	5000	
WHAY New Britain, Conn.	10000		KIXZ Amarillo, Tex.	10000	7400	5000	7400	5000	7400	5000	
WPLA Plant City, Fla.	10000		950—315.6			1010—296.9			1000—296.9		
WGAJ Valdosta, Ga.	5000		CNKN Campbellton, N.B.	5000	7400	5000	7400	5000	7400	5000	
WAKO Lawrenceville, Ill.	5000		CKEB Barre, Ont.	5000	7400	5000	7400	5000	7400	5000	
WSUI Iowa City, Iowa	5000		WRMA Monticello, Ala.	5000	7400	5000	7400	5000	7400	5000	
WCLS Baton Rouge, La.	1000		KXJK Forrest City, Ark.	5000	7400	5000	7400	5000	7400	5000	
WABI Bangor, Maine	5000		KJFA Ft. Smith, Ark.	1000	7400	5000	7400	5000	7400	5000	
WDFD Flint, Mich.	5000		KAHJ Auburn, Calif.	10000	7400	5000	7400	5000	7400	5000	
WCOC Meridian, Miss.	5000		KIMN Denver, Colo.	5000	7400	5000	7400	5000	7400	5000	
KOYN Billings, Mont.	10000		WFBF St. Walton Sch., Fla.	10000	7400	5000	7400	5000	7400	5000	
KYSS Missoula, Mont.	10000		WLOF Orlando, Fla.	5000	7400	5000	7400	5000	7400	5000	
KBIM Roswell, N.Mex.	5000		WGTA Summerville, Ga.	10000	7400	5000	7400	5000	7400	5000	
WLAS Jacksonville, N.C.	10000		960—312.3			1010—296.9			1000—296.9		
KCJB Miami, N. Dak.	10000		CFAC Calgary, Alta.	10000	7400	5000	7400	5000	7400	5000	
WFB Midland, Ohio	10000		CHNS Halifax, N.S.	5000	7400	5000	7400	5000	7400	5000	
KGLC Miami, Okla.	10000		CKWS Kingston, Ont.	10000	7400	5000	7400	5000	7400	5000	
KURY Brookings, Oreg.	500		WBIR Birmingham, Ala.	5000	7400	5000	7400	5000	7400	5000	
WAVL Apollo, Pa.	10000		W0ZK Ozark, Ala.	10000	7400	5000	7400	5000	7400	5000	
WGBI Scranton, Pa.	10000		KHOZ Harrison, Ark.	10000	7400	5000	7400	5000	7400	5000	
WSBA York, Pa.	10000		KBIF Centerville, Calif.	10000	7400	5000	7400	5000	7400	5000	
WPRP Ponce, P.R.	5000		WJWL Georgetown, Del.	10000	7400	5000	7400	5000	7400	5000	
WDBI Bangor, Me., S.C.	5000		WJWN Belle Glade, Fla.	10000	7400	5000	7400	5000	7400	5000	
WJCH Wisconsin City, Tenn.	5000		WMOP Ocala, Fla.	10000	7400	5000	7400	5000	7400	5000	
WEPF S. Pittsburg, Tenn.	5000		WCGA Calhoun, Ga.	10000	7400	5000	7400	5000	7400	5000	
KNAF Fredericksburg, Tex.	10000		WCOR Lebanon, Tenn.	5000	7400	5000	7400	5000	7400	5000	
KRID McAllen, Tex.	1000		KALT Atlanta, Tex.	10000	7400	5000	7400	5000	7400	5000	
KRRV Sherman, Tex.	1000		KMCO Comroe, Tex.	5000	7400	5000	7400	5000	7400	5000	
KALL Salt Lake City, Utah	10000		KFLD Floyd, Ohio	5000	7400	5000	7400	5000	7400	5000	
WBRJ White River Junction, Vermont	10000		KCLW Hamilton, Tex.	5000	7400	5000	7400	5000	7400	5000	
WRNL Richmond, Va.											

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
KCHI	Chillicothe, Mo.	250d	KFBI	Wichita, Kans.	1000d	KSEN	Shelby, Mont.	1000	WENC	Whiteville, N.C.	1000d
KCFJ	Festus, Mo.	5000d	KHMO	Hannibal, Mo.	5000	KDEF	Albuquerque, N. Mex.	1000d	KEYD	Oakes, N. Dak.	1000d
KRVN	Lexington, Nebr.	2500d	KHFE	High Point, N.C.	5000	WUW	Wichita, N.Y.	5000	WVAR	Cleveland, Ohio	5000d
WINS	New York, N.Y.	5000d	WDAI	Memphis, Tenn.	5000d	WBAG	Burlington, N.C.	1000d	WEST	West, Ohio	250d
WBZ	Albany, N.C.	1000d	KOPY	Alice, Tex.	1000	WGBR	Goldsboro, N.C.	5000	KGYN	Guyton, Okla.	1000d
WELS	Kinston, N.C.	1000d	WKOW	Madison, Wis.	1000d	WCUE	Akron, Ohio	1000d	WJUN	Mexico, Pa.	250d
WIOD	New Boston, Ohio	500d				WIMA	Lima, Ohio	1000	WRIB	Providence, R.I.	1000d
WITT	Lewisburg, Pa.	250d	1080-277.6			KNED	McAlester, Okla.	1000	WALD	Waterboro, S.C.	1000d
WHIN	Gallatin, Tenn.	1000d	CHED	Edmonton, Alta.	1000d	KAGO	Klamath Falls, Oreg.	5000	WFWL	Camden, Tenn.	250
WORM	Savannah, Tenn.	250d	KSCD	Santa Cruz, Calif.	1000	WHUN	Huntingdon, Pa.	1000d	WCPH	Etowah, Tenn.	1000d
KBUY	Amarillo, Tex.	5000	WHFE	High Point, N.C.	5000	KWPA	New Kensington, Pa.	1000d	WHEY	Millington, Tenn.	250
KMLW	Marlin, Tex.	250d	WTRC	Memphis, Tenn.	5000	WVAV	Waynesville, N.C.	1000	KLBS	Livingston, Tex.	250d
WELK	Charlottesville, Va.	250d	WKLO	Louisville, Ky.	5000	WRNO	Orangeburg, S.C.	5000	WVLT	Weatherford, Tex.	250d
WLEV	Madison, Va.	1000d	WKOJ	Owosso, Mich.	250d	WYVC	Rock Hill, S.C.	1000d	WLSB	Big Gap, Va.	1000d
WCST	Berkeley Springs, W. Va.	250d	WYSL	Kenmore, N.Y.	1000d	WSNW	Seneca Township, South Carolina	1000d	WFAJ	Falls Church, Va.	1000d
WSPT	Stevens Pt., Wis.	1000d	WEWO	Laurinburg, N.C.	1000d	WAPO	Chattanooga, Tenn.	5000	KASY	Auburn, Wash.	250d
			KWJJ	Portland, Oreg.	1000d	WCRC	Morristown, Tenn.	1000			
1020-293.9			WEFP	Pittsburgh, Pa.	1000d	WTAW	Bryan, Tex.	1000d			
KPOP	Los Angeles, Calif.	5000	KRLD	Dallas, Tex.	5000d	KCCZ	Corpus Christi, Tex.	1000d	1230-243.8		
WCIL	Carbondale, Ill.	1000d				KIZZ	El Paso, Tex.	1000d	CFWC	Chamrose, Alta.	1000
WFEO	Peoria, Ill.	1000d	1090-275.1			KJBC	Midland, Tex.	1000d	CFHC	Cherokee, Man.	250
KDKA	Pittsburgh, Pa.	5000	CHEC	Lethbridge, Alta.	5000	KPNG	Port Neches, Tex.	1150	CFKL	Schefferville, Que.	250
			CHIC	Brampton, Ont.	1000	KOLJ	Quanah, Tex.	500d	CFGR	Greenville, Sask.	500
1030-291.1			CHRS	St. Jean, Que.	250	KOFE	Pullman, Wash.	1000d	CFYT	Dawson City, Yukon T.	100
WBZ	Boston, Mass.	5000d	KTHB	Chile, Chile	1000d	KAYO	Seattle, Wash.	5000	CBQJ	Belleville, Ont.	250
WBZA	Springfield, Mass.	1000	WCRA	Emingham, Ill.	250d	KAYO	Vancouver, Wash.	1000d	CFPA	Port Arthur, Ont.	1000
KOB	Albuquerque, N. Mex.	1000d	KNWS	Waterloo, Iowa	1000d	WELC	W. Va.	1000	CKLD	Theftord Mines, Que.	250
KCTA	Corpus Christi, Tex.	5000d	WBAL	Baltimore, Md.	5000d	WAXX	Chippewa Falls, Wis.	5000d	CKCP	Port Arthur, Ont.	1000
			WILD	Boston, Mass.	1000d	WISN	Milwaukee, Wis.	5000	VOAR	St. John's, Nfld.	100
			WMUS	Muskegon, Mich.	1000d				CKVD	Val D'Or, Que.	250
			KING	Seattle, Wash.	5000d				WAUD	Auburn, Ala.	250
1040-288.3									WJBB	Haleyville, Ala.	250
KHVV	Honolulu, Hawaii	5000	1100-272.6			WJDD	Chicago, Ill.	5000d	WBHP	Huntsville, Ala.	250
WHO	Des Moines, Iowa	5000d	KFAX	San Francisco, Calif.	1000d	KSL	Salt Lake City, Utah	5000d	WTAJ	Taladega, Ala.	250
KIXL	Dallas, Tex.	1000d	WLBK	Carrollton, Ga.	250d				WTBC	Tuscaloosa, Ala.	250
			WHLI	Hempstead, N.Y.	1000d				KIFW	Sitka, Alaska	250
1050-285.5			WYVA	Cleveland, Ohio	5000d	1170-256.3			KSUN	Bisbee, Ariz.	250
CFGP	Grande Prairie, Alta.	1000d	KYFA	Bethlehem, Pa.	250d	CFNS	Saskatoon, Sask.	1000	KAAA	Kingman, Ariz.	250
WBSB	St. Boniface, Man.	1000d				WCDF	Montgomery, Ala.	1000d	KRIZ	Phoenix, Ariz.	250
CJIC	Sault Ste. Marie, Ont.	250	1110-270.1			KCBQ	San Diego, Calif.	5000d	KCON	Conway, Ark.	250
CHUM	Toronto, Ont.	5000	CFML	Cornwall, Ont.	1000	KLOK	San Jose, Calif.	1000d	WVAV	Waynesville, N.C.	1000
WRES	Alexander City, Ala.	1000d	CFTJ	Gait, Ont.	250	KOHO	Honolulu, Hawaii	1000d	KBTM	Jonesboro, Ark.	250
WCR1	Scottsboro, Ala.	250d	KRLA	Pasadena, Calif.	1000d	WLBH	Mattoon, Ill.	250d	KGEE	Bakersfield, Calif.	250
KVVM	Show Low, Ariz.	250d	WALT	Tampa, Fla.	1000d	KSTT	Davenport, Iowa	1000d	KWTC	Barstow, Calif.	250
KVLC	Little Rock, Ark.	1000d	KIPA	Hilo, Hawaii	1000	KVOD	Tulsa, Okla.	5000	KIBS	Bishop, Calif.	250
KOFY	San Mateo, Calif.	1000d	KWAB	Chicago, Ill.	5000d	WLEO	Ponce, P.R.	250	KXO	El Centro, Calif.	250
KWSO	Waco, Calif.	1000d	KARL	Omaha, Nebr.	5000d	KPUG	Bellingham, Wash.	1000	KDAC	Fort Bragg, Calif.	250
KLMO	Longmont, Colo.	250d	WBT	Charlotte, N.C.	5000d	WVVA	Wheeling, W. Va.	5000d	KGJF	Las Vegas, Calif.	250
WJSB	Crestview, Fla.	1000d	KBNB	Bend, Oreg.	5000				KPRL	Paso Robles, Calif.	250
WIVY	Jacksonville, Fla.	1000d	WNAR	Norristown, Pa.	500d				KRDG	Redding, Calif.	250
WHBO	Tampa, Fla.	250d	WJAP	Caguas, P.R.	250	1180-254.1			KWG	Stockton, Calif.	250
WRMF	Titusville, Fla.	5000	WHIM	Providence, R.I.	1000d	WLDS	Jacksonville, Ill.	1000d	KEXO	Grand Junction, Colo.	250
WJAZ	Albany, Ga.	1000d				WHAM	Rochester, N.Y.	5000d	KLVC	Leadville, Colo.	250
WAUG	Augusta, Ga.	1000d	1120-267.7						KZA	Fueblo, Colo.	250
WBE	Marietta, Ga.	500d	WUST	Bethesda, Md.	250d	1190-252.0			KGEE	Sterling, Colo.	250
WIN	Courier D'Alene, Idaho	250d	KMOX	St. Louis, Mo.	5000d	KEYZ	Anaheim, Calif.	1000	WINF	Manchester, Conn.	250
WDE	Desatur, Ill.	1000d	KCLE	Cleburne, Tex.	250d	KBA	Valle, Calif.	1000	WGGG	Gainesville, Fla.	250
KNCO	Garden City, Kans.	1000d	1130-265.3			WOWO	Flag, Wyo.	5000d	WONN	Lakeland, Fla.	250
WZIP	Covington, Ky.	1000d	CKWX	Vancouver, B.C.	5000d	WANN	Annapolis, Ind.	1000d	WMAF	Madison, Fla.	250
KLPL	Lake Providence, La.	250d	KSDO	San Diego, Calif.	5000	WKOK	Framingham, Mass.	1000d	WMBF	New Smyrna Bch., Fla.	250
KCIJ	Shreveport, La.	250d	KWKH	Shreveport, La.	5000d	WLOB	New York, N.Y.	1000d	WNVY	Pensacola, Fla.	250
WQMR	Silver Sprng., Md.	1000d	WCAE	Detroit, Mich.	5000d	KEX	Portland, Oreg.	5000d	WCNH	Quincy, Fla.	250
WQAG	Ann Arbor, Mich.	1000d	WDGY	Minneapolis, Minn.	5000d	KLIF	Dallas, Tex.	5000d	WJNO	W. Palm Beach, Fla.	250
KLOH	Pigeonst., Minn.	1000d	WNEW	New York, N.Y.	5000d				WBLA	Augusta, Ga.	250
WACR	Columbus, Miss.	1000d	1140-263.0			1200-249.9			WBLD	Dalton, Ga.	250
KSIS	Sedalia, Mo.	1000d	CKXL	Calgary, Alta.	1000d	WDAI	San Antonio, Tex.	5000d	WXLJ	Dublin, Ga.	250d
KRBO	Las Vegas, Nev.	500d	KRAK	Stockton, Calif.	1000d	1210-247.8			WFOM	Marietta, Ga.	250
WBNC	Conway, N.H.	1000d	WMI	Miami, Fla.	1000d	WCNT	Centralia, Ill.	1000d	WSOK	Savannah, Ga.	250
WSTN	Baldwinsville, N.Y.	250d	KGEM	Boise, Idaho	1000d	WKNX	Saginaw, Mich.	1000d	WYAX	Waycross, Ga.	250
WSEN	Massena, N.Y.	5000d	WSIV	Pekin, Ill.	1000d	WADE	Wadesboro, N.C.	1000d	KBAR	Burley, Idaho	250
WGM	New York, N.Y.	250d	KLPR	Oklahoma City, Okla.	1000d	WAVI	Dayton, Ohio	250d	KORT	Grangeville, Idaho	250
WHL	Farmville, N.C.	250d	WITA	San Juan, P.R.	500	WCAU	Philadelphia, Pa.	5000d	KRXK	Rexburg, Idaho	250
WFC	Franklin, N.C.	500d	KSDO	Silver Falls, S. Dak.	1000d	1220-245.8			WJBC	Bloomington, Ill.	250
WLN	Lincolnton, N.C.	1000d	KORC	Mineral Wells, Tex.	250	CJOC	Lethbridge, Alta.	1000d	WDU	W. Va.	250
WWGP	Sanford, N.C.	1000d	WRVA	Richmond, Va.	5000d	CJRL	Kenora, Ont.	1000	WHCO	Sparks, Nev.	250
KCCO	Lawton, Okla.	250d	1150-260.7			CKEK	New Glasgow, N.S.	250	WJOB	Hammond, Ind.	250
KFMJ	Tulsa, Okla.	1000d	CKSA	Lloydminster, Alta.	1000	CKCW	Moncton, N.B.	1000	WSAL	Logansport, Ind.	250
KEDS	Pendleton, Oreg.	1000d	CHSJ	Saint John, N.B.	5000	CISS	Cornwall, Ont.	1000	WTCJ	Tell City, Ind.	250
KUEE	Springfield, Oreg.	1000d	CKOC	Hamilton, Ont.	5000	CKSM	Shawinigan, Quebec	1000	WBOW	Terre Haute, Ind.	250
WOT	Butler, Pa.	250d	CKX	Brandon, Man.	5000	WEZB	Birmingham, Ala.	1000d	KFJB	Marshalltown, Iowa	250
WLVC	Williamsport, Pa.	1000d	CKTR	Three Rivers, Que.	5000	WPRN	Butler, Ala.	1000d	WHOP	Hopkinsville, Ky.	250
WMSPT	Sparta, Tenn.	1000d	WBCA	Bay Minette, Ala.	1000d	KVSA	McGehee, Ark.	1000d	WMLF	Pineville, Ky.	250
KLEN	Killeen, Tex.	250d	WGEA	Geneva, Ala.	5000	KIBE	Palo Alto, Calif.	1000d	KLIC	Monroe, La.	250
KWLD	Liberty, Tex.	250d	WJRD	Tuscaloosa, Ala.	5000	KFCG	Denver, Colo.	1000d	WJBW	New Orleans, La.	250
WGAT	Gate City, Va.	250d	KCKY	Coolidge, Ariz.	1000	WTTT	Arlington, Fla.	250d	KSLO	Opelousas, La.	250
WBRG	Lynchburg, Va.	1000d	KXLR	No. Little Rock, Ark.	5000	WKBX	Kissimmee, Fla.	250d	WDCY	Calais, Maine	250
WCMS	Norfolk, Va.	1000d	KFSG	Los Angeles, Calif.	2500	WFEC	Miami, Fla.	1000d	WTH	Baltimore, Md.	250
KNBX	Kirklinburg, Wash.	1000d	KRKD	Los Angeles, Calif.	5000	WCLB	Camilla, Ga.	250d	WCUM	Cumberland, Md.	250
WCFP	Parisburg, W. Va.	1000d	KJAX	Santa Rosa, Calif.	5000	WPLB	Rehoboth, Ga.	250d	WMNB	No. Adams, Mass.	250
WECL	Eau Claire, Wis.	1000d	KGMC	Englewood, Colo.	1000d	WSFT	Thomasboro, Ga.	250d	WESX	Salem, Mass.	250
WLIP	Kenosha, Wis.	250d	WDEL	Wilmington, Del.	5000	WLPO	LaLle, Ill.	1000d	WNEB	Worcester, Mass.	250
KWIV	Douglas, Wyo.	250d	WNBW	Daytona Beh., Fla.	1000d	WKRS	Waukegan, Ill.	1000d	WJEF	Grand Rapids, Mich.	500
			WTMP	Tampa, Fla.	5000d	WLSM	Salem, Ind.	1000d	WIKB	Iron River, Mich.	250
1060-282.8			WFPM	Fort Valley, Ga.	1000d	KJAN	Atlantic, Iowa	250d	WVFC	Waynesville, N.C.	1000d
CFNC	Calgary, Alta.	1000d	WJEM	Valdosta, Ga.	1000d	KOFO	Ottawa, Kans.	250d	WSOO	Sit. Ste. Marie, Mich.	250
CJLR	Quebec, Que.	5000	KANI	Oahu, Hawaii	1000d	WFKN	Franklin, Ky.	250d	WSTR	Sturgis, Mich.	250
KPAY	Chicago, Calif.	1000d	WGH	Marion, Ill.	5000d	KBOL	Bossier City, La.	250d	WLLK	Cloquet, Minn.	250
WNDE	New Orleans, La.	5000d	WKW	Des Moines, Iowa	1000	WLB1	Denham Springs, La.	250d	KYSM	Mankato, Minn.	250
WHFB	Benton Harbor, Mich.	1000d	KSAL	Salina, Kans.	5000	WSME	Sanford, Maine	1000d	KWFO	Winoona, Minn.	250
WMAP	Monroe, N.C.	250d	WMST	Mt. Sterling, Ky.	500d	WBCH	Hastings, Mich.	250d	WCMA	Carthage, Miss.	250
WCWM	Canton, Ohio	1000d	WLOC	Mumfordsville, Ky.	1000d	WAVN	Stillwater, Minn.	1000d	WHSY	Hartiesburg, Miss.	250
WRCV	Philadelphia, Pa.	5000d	WJBO	Baton Rouge, La.	5000	WMDC	Hazlehurst, Miss.	250d	WSSO	Starkville, Miss.	250
			WGHM	Shohegan, Maine	5000d	KBHM	Branson, Mo.	1000d	WAZF	Yazoo City, Miss.	

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
1290—232.4			CJRH Richmond Hill, Ont.	1000	WEBY Milton, Fla.	5000d	WAGN Menominee, Mich.	250	WAGN Menominee, Mich.	250	
CFAM Altona, Man.	5000		WHEP Foley, Ala.	1000d	WMEN Tallahassee, Fla.	5000d	WMBN Petoskey, Mich.	250	WMBN Petoskey, Mich.	250	
CKSL London, Ont.	5000		WJAM Marion, Ala.	5000d	WMET Dublin, Ga.	5000d	WEXL Royal Oak, Mich.	250	WEXL Royal Oak, Mich.	250	
WTHG Jackson, Ala.	5000		WKBJ Mesa, Ariz.	5000	WEAW Evansville, Ill.	1000d	KDLM Detroit Lakes, Minn.	250	KDLM Detroit Lakes, Minn.	250	
WMLS Sylacauga, Ala.	1000d		KBOB Meyer, Ark. Ga.	1000d	WMOH Monmouth, Ill.	1000d	WEVA Weaverville, N.C.	250	WEVA Weaverville, N.C.	250	
KEOS Flagstaff, Ariz.	1000		KWBK Oakland, Calif.	1000	WRRR Rockford, Ill.	1000d	KROC Rochester, Minn.	250	KROC Rochester, Minn.	250	
KUCB Tucson, Ariz.	1000		KTRB Taft, Calif.	400d	WJPS Evansville, Ind.	5000	KWLM Willmar, Minn.	250	KWLM Willmar, Minn.	250	
KDMS El Dorado, Ariz.	5000d		KFKA Greeley, Colo.	1000	KWWL Waterloo, Iowa	5000	WJMB Brookhaven, Miss.	250	WJMB Brookhaven, Miss.	250	
KUOA Sitom Strgs., Ark.	5000d		WICH Norwich, Conn.	1000	KFH Wichita, Kans.	5000	WAML Laurel, Miss.	250	WAML Laurel, Miss.	250	
KHSL Chico, Calif.	5000		WUOC Deland, Fla.	5000d	WMOR Morehead, Ky.	1000d	KXED Mexico, Mo.	250	KXED Mexico, Mo.	250	
KPRG Gilroy, Calif.	1000d		WUOC Wauchula, Fla.	5000	KVLD Lafayette, La.	1000	KSMO Salem, Mo.	250	KSMO Salem, Mo.	250	
KPTO San Bernardino, Calif.	5000		WBRO Waynesboro, Ga.	1000d	WASR Harvey de Grace, Md.	1000d	KICK Sidersville, Mo.	250	KICK Sidersville, Mo.	250	
WCLS Hartford, Conn.	5000		WBWK West Point, Ga.	1000	WCRB Waltham, Mass.	1000	KCAP Helena, Mont.	250	KCAP Helena, Mont.	250	
WTUX Wilmington, Del.	1000d		KWTR Twin Falls, Idaho	1000	WTRX Flint, Mich.	1000	KPKR Livingston, Mont.	250	KPKR Livingston, Mont.	250	
WTMC Ocala, Fla.	1000		WISH Indianapolis, Ind.	5000	WL0L Minneapolis, Minn.	5000	KATL Miles City, Mont.	250	KATL Miles City, Mont.	250	
WSCM Panama City Beach, Fla.	5000		KOKX Keokuk, Iowa	1000	WCRR Corinth, Miss.	5000	KQTE Missoula, Mont.	250	KQTE Missoula, Mont.	250	
WIRK W. Palm Bch., Fla.	5000		WTTL Madisonville, Ky.	5000d	WJPR Greenville, Miss.	1000d	KFGT Fremont, Nebr.	100	KFGT Fremont, Nebr.	100	
WDEC Americus, Ga.	1000d		WDOC Prestonsburg, Ky.	5000d	WDAL Meridian, Miss.	1000d	KGFV Kearney, Nebr.	250	KGFV Kearney, Nebr.	250	
WCHK Canton, Ga.	1000d		KIKS Sulphur, La.	500	KUKU Willow Springs, Mo.	5000d	KSID Sidney, Nebr.	250	KSID Sidney, Nebr.	250	
WTOC Savannah, Ga.	1000d		KUZN W. Monroe, La.	1000d	KGAK Gallup, N. Mex.	5000	KBRK Las Vegas, Nev.	250	KBRK Las Vegas, Nev.	250	
WBCS Watatulo, Idaho	1000d		WLOB Portland, Maine	1000d	KEVW New York, N.Y.	5000	KBET Reno, Nev.	250	KBET Reno, Nev.	250	
WIRL Peoria, Ill.	1000d		WLRB Springfield, Mass.	5000	WPOW New York, N.Y.	5000	WDCR Hanover, N.H.	250	WDCR Hanover, N.H.	250	
WBFL Benton, Ky.	1000d		WKMH Dearborn, Mich.	5000	WDSO Oswego, N.Y.	1000d	WMID Atlantic City, N.J.	250	WMID Atlantic City, N.J.	250	
KJEF Jennings, La.	1000d		KRBI St. Peter, Minn.	1000d	WHAZ Troy, N.Y.	1000	KNDE Aztec, N.M.	250	KNDE Aztec, N.M.	250	
WHGR Houghton Lake, Michigan	5000d		WXXX Hattiesburg, Miss.	1000d	WFIN Findlay, Ohio	1000d	KSIL Silver City, N. Mex.	1000	KSIL Silver City, N. Mex.	1000	
WNIL Niles, Mich.	5000		KFSB Joplin, Mo.	5000	KVOV Wellston, Ohio	5000	WMB0 Auburn, N.Y.	250	WMB0 Auburn, N.Y.	250	
W01A Saline, Mich.	5000		KFBB Great Falls, Mont.	5000	KPOJ Portland, Ore.	5000	WENT Groversville, N.Y.	250	WENT Groversville, N.Y.	250	
KRBD Benson, Minn.	5000		WJLK Asbury Park, N.J.	250	KCPA Spokane, Wash.	5000d	WJOC Jamestown, N.Y.	250	WJOC Jamestown, N.Y.	250	
W01E Batesville, Miss.	1000d		WJAM Camden, N.J.	250	WZLF Zionsville, Ind.	1000d	WUSJ Lockport, N.Y.	250	WUSJ Lockport, N.Y.	250	
KALM Thayer, Mo.	1000d		WVLP Mt. Kisco, N.Y.	1000d	WVIC Erie, Pa.	5000	WMSA Massena, N.Y.	250	WMSA Massena, N.Y.	250	
KGVO Missoula, Mont.	5000		WVTP Utica, N.Y.	1000	WLAT Conway, S.C.	5000d	WALL Middletown, N.Y.	250	WALL Middletown, N.Y.	250	
KOIL Omaha, Nebr.	5000		WICE Asheville, N.C.	5000	WFBC Greenville, S.C.	5000	WIRY Plattsburg, N.Y.	250	WIRY Plattsburg, N.Y.	250	
WKNE Keene, N.H.	5000		WKTG Charlotte, N.C.	1000	WAEW Crossville, Tenn.	1000d	WJRI Lenoir, N.C.	250	WJRI Lenoir, N.C.	250	
KSCR Socorro, N.M.	5000		WTKI Durham, N.C.	1000	WTR0 Dyersburg, Tenn.	5000	WOXF Oxford, N.C.	250	WOXF Oxford, N.C.	250	
KRBD Benson, Minn.	5000		KNOX Grand Forks, N.Dak.	5000	KMIL Cameron, Tex.	5000	WOOW Washington, N.C.	250	WOOW Washington, N.C.	250	
WNBF Binghamton, N.Y.	5000		WFRB Albany, N.Y.	1000d	KSWA Graham, Tex.	1000d	WGNI Wilmington, N.C.	250	WGNI Wilmington, N.C.	250	
WHKY Hickory, N.C.	5000		KNPT Newport, Ore.	5000	KIRB Kirby, Tex.	1000d	WAIR Winston-Salem, N.C.	250	WAIR Winston-Salem, N.C.	250	
WEYE Sanford, N.C.	1000d		WBFD Bedford, Pa.	1000d	KDOK Tyler, Tex.	1000d	KGPC Grafton, N.D.	250	KGPC Grafton, N.D.	250	
WOMP Bellaire, Ohio	1000d		WGSA Ephrata, Pa.	1000d	WBTM Danville, Va.	1000d	WANC Ashland, Ohio	250	WANC Ashland, Ohio	250	
WHIO Dayton, Ohio	5000		WNSA Warren, Pa.	5000d	WESR Tasley, Va.	1000d	W01B Athens, Ohio	250	W01B Athens, Ohio	250	
KDMA Pendleton, Ore.	1000d		WDKD Kinross, S.C.	5000d	KFKF Bellevue, Wash.	1000d	WIZE Springfield, Ohio	250	WIZE Springfield, Ohio	250	
K01L Portland, Ore.	1000d		WDD0 Chattanooga, Tenn.	5000	WETZ New Martinsville, West Virginia	1000d	WSTV Steubenville, Ohio	250	WSTV Steubenville, Ohio	250	
WTRN Tyrone, Pa.	1000d		WDXI Jackson, Tenn.	5000	WHBL Sheboygan, Wis.	1000	KIHN Hugo, Okla.	250	KIHN Hugo, Okla.	250	
WICE Providence, R.I.	5000		WBNT Oneida, Tenn.	1000d	KOVE Lander, Wyo.	1000	KOXY Okla. City, Okla.	250	KOXY Okla. City, Okla.	250	
W01G Sumter, S.C.	1000d		KZIP Amarillo, Tex.	1000d	1340—223.7		KL0D Corvallis, Ore.	250	KL0D Corvallis, Ore.	250	
WATO Oak Ridge, Tenn.	1000d		WRR Dallas, Tex.	5000	CFGB Goose Bay, Nfld.	250	KFIR Nor Bend, Ore.	250	KFIR Nor Bend, Ore.	250	
KBLT Big Lake, Tex.	1000d		KOYL Odessa, Tex.	5000	CJAF Cabano, Que.	250	WFBG Altoona, Pa.	250	WFBG Altoona, Pa.	250	
KIVY Crockett, Tex.	5000		KUBO San Antonio, Tex.	5000d	CFSL Weyburn, Sask.	250	WCVI Connellsville, Pa.	250	WCVI Connellsville, Pa.	250	
KRGY Wesley, Tex.	5000		WEEL Fairfax, Va.	1000	CFYK Yellow Knife, N.W.T.	150	WSAJ Grove City, Pa.	100	WSAJ Grove City, Pa.	100	
KTRN Wichita Falls, Tex.	5000		WGRY Newport News, Va.	5000	CHAD Amos, Que.	150	WKRZ Oil City, Pa.	250	WKRZ Oil City, Pa.	250	
WPVA Colonial Hgts., Va.	5000d		WAGY Prosser, Wash.	1000d	CJLS Yarmouth, N.S.	250	W01H Philadelphia, Pa.	250	W01H Philadelphia, Pa.	250	
WAGE Leesburg, Va.	1000d		WIBA Madison, Wis.	5000	CHRD Drummondville, Que.	250	WRAW Reading, Pa.	250	WRAW Reading, Pa.	250	
WV0W Logan, W. Va.	5000		1320—227.1		CJQC Quebec, Que.	250	WBRE Wilkes-Barre, Pa.	250	WBRE Wilkes-Barre, Pa.	250	
WMIL Milwaukee, Wis.	1000d		CHQM Vancouver, B.C.	1000d	KIKR-I Parry Sound, Ont.	250	WPPA Williamsport, Pa.	250	WPPA Williamsport, Pa.	250	
WSCP Sparta, Wis.	1000d		CKEC New Glasgow, N.S.	1000	KX0X Woodstock, Ont.	250	WGRF Aquadilla, P.R.	250	WGRF Aquadilla, P.R.	250	
			CKSO Sorel, P.Q.	1000	KWUL Cullman, Ala.	250	W01K Charleston, S.C.	250	W01K Charleston, S.C.	250	
			CKKW Kitchener, Ont.	1000	WJ0I Florence, Ala.	250	W01R Rock Hill, S.C.	250	W01R Rock Hill, S.C.	250	
			WAGF Dothan, Ala.	1000	W01J Florence, Ala.	250	WSSC Sumter, S.C.	250	WSSC Sumter, S.C.	250	
			WENN Birmingham, Ala.	5000d	W01K Selma, Ala.	250	KJIV Huron, S.D.	250	KJIV Huron, S.D.	250	
			KBLN Yuma, Ariz.	5000d	W01B Sylacauga, Ala.	250	KRSD Rapid City, S.Dak.	250	KRSD Rapid City, S.Dak.	250	
			KRWL Fort Smith, Ark.	5000	KIBH Seward, Alaska	250	W01C Cleveland, Tenn.	250	W01C Cleveland, Tenn.	250	
			KRLW Walnut Ridge, Ark.	1000d	KIKO Miami, Ariz.	250	W01R Columbia, Tenn.	250	W01R Columbia, Tenn.	250	
			SHS Hemet, Calif.	500	KNOG Nogales, Ariz.	250	W01V Greenville, Tenn.	250	W01V Greenville, Tenn.	250	
			KUCE Oceanside, Calif.	500	KZ0K Prescott, Ariz.	250	W01N Knoxville, Tenn.	250	W01N Knoxville, Tenn.	250	
			KCRA Sacramento, Calif.	5000	KBTA Batesville, Ark.	250	W01M Memphis, Tenn.	250	W01M Memphis, Tenn.	250	
			KAVI Rocky Ford, Colo.	1000d	KBRB Springfield, Ark.	250	W01D Wichita, Tenn.	250	W01D Wichita, Tenn.	250	
			WATR Waterbury, Conn.	1000	KENL Arcata, Calif.	250	KWKC Abilene, Tex.	250	KWKC Abilene, Tex.	250	
			W01A Hollywood, Fla.	1000d	KMAB Fresno, Calif.	250	KAND Corsicana, Tex.	250	KAND Corsicana, Tex.	250	
			WJHP Jacksonville, Fla.	5000	KSFE Needles, Calif.	250	KSET El Paso, Tex.	250	KSET El Paso, Tex.	250	
			WNEG Topeka, Kan.	1000d	KATY San Luis Obispo, Calif.	250	KDUB Lubbock, Tex.	250	KDUB Lubbock, Tex.	250	
			WKAN Kankakee, Ill.	1000d	KIST Santa Barbara, Calif.	250	KRBA Lurkin, Tex.	250	KRBA Lurkin, Tex.	250	
			KMAQ Maquoketa, Iowa	5000	KW01 Watsonville, Calif.	250	KYKM Monahans, Tex.	250	KYKM Monahans, Tex.	250	
			KLWN Lawrence, Kans.	5000	KDEN Denver, Colo.	250	KOLE Port Arthur, Tex.	250	KOLE Port Arthur, Tex.	250	
			WBRT Bardstow, Ky.	1000d	KVRH Salida, Colo.	250	KTXL San Angelo, Tex.	250	KTXL San Angelo, Tex.	250	
			KVGO Mayfield, Ky.	1000d	KW02 New Haven, Conn.	250	KVIC N. of Victoria, Tex.	250	KVIC N. of Victoria, Tex.	250	
			WHLH Homer, La.	1000d	W00K Washington, D.C.	250	WTWN St. Johnsbury, Vt.	250	WTWN St. Johnsbury, Vt.	250	
			W01S Salisbury, Md.	1000d	WTAN Clearwater, Fla.	250	WKEY Covington, Va.	250	WKEY Covington, Va.	250	
			W01C Lansing, Mich.	5000	WR0D Daytona Bch., Fla.	250	W01P Hopewell, Va.	250	W01P Hopewell, Va.	250	
			W01J Marquette, Mich.	1000	WDSR Lake City, Fla.	250	W01Q Hot Springs, Va.	250	W01Q Hot Springs, Va.	250	
			W01C Houston, Miss.	5000d	W01Y Marianna, Fla.	250	KAGT Anacortes, Wash.	250	KAGT Anacortes, Wash.	250	
			WR0J Picayune, Miss.	5000d	W01B Palm Beach, Fla.	250	KPKW Pasco, Wash.	250	KPKW Pasco, Wash.	250	
			KX0L Clayton, Mo.	1000d	WNSM Valparaiso-Nieville, Fla.	250	KAPL Raymond, Wash.	250	KAPL Raymond, Wash.	250	
			K01T Scottsbluff, Nebr.	5000	W01A Athens, Ga.	250	KMEL Wenatchee, Wash.	250	KMEL Wenatchee, Wash.	250	
			W01G Hornell, N.Y.	5000	W01E Atlanta, Ga.	250	WHAR Clarksburg, W. Va.	250	WHAR Clarksburg, W. Va.	250	
			W01C Forest City, N.C.	5000	W01B Augusta, Ga.	250	W01N Montgomery, W. Va.	250	W01N Montgomery, W. Va.	250	
			W01G Greensboro, N.C.	5000	W01C Columbia, Ga.	250	W01E Welch, W. Va.	250	W01E Welch, W. Va.	250	
			W01G Minot, N.Dak.	1000d	W01B Lyons, Ga.	250	W01Y Ladysmith, Wis.	250	W01Y Ladysmith, Wis.	250	
			W01K Lancaster, Ohio	1000d	W01F Tifton, Ga.	250	WRIT Milwaukee, Wis.	250	WRIT Milwaukee, Wis.	250	
			KW0E Clinton, Okla.	1000d	KPST Preston, Idaho	250	W01F Wis. Rapids, Wis.	250	W01F Wis. Rapids, Wis.	250	
			W01P Allentown, Pa.	5000	W01Y Decatur, Ill.	250	K01B Laramie, Wyo.	250	K01B Laramie, Wyo.	250	
			W01P Pittsburg, Pa.	5000	W01L Joliet, Ill.	250	KW0R Worland, Wyo.	250	KW0R Worland, Wyo.	250	
			W01C Scranton, Pa.	1000	W01B Bedford, Ind.	250					
			W01R Rio Piedras, P.R.	5000	W01C Elkhart, Ind.	250	1350—222.1				
			W01C Columbia, S.C.	1000	W01B Muncie, Ind.	250	CH0V Pembroke, Ont.	1000	CH0V Pembroke, Ont.	1000	
			K01E Sioux Falls, S.Dak.	5000	KROS Clinton, Iowa	250	CJDC Dawson Creek, B.C.	1000	CJDC Dawson Creek, B.C.	1000	
			KW0N Kingsport, Tenn.	5000d	KL01 Estherville, Iowa	250	CHGB St. Anne de la	1000	CHGB St. Anne de la	1000	
			W01R Manchester, Tenn.	1000d	K01N Kansas City, Kans.	250	PK02 Pocatello, Que.	1000	PK02 Pocatello, Que.	1000	
			W01G Colo. City, Tex.	1000d	K01K Pittsburg, Kans.	250	CKLB Oshawa, Ont.	1000d	CKLB Oshawa, Ont.	1000d	
			W01C Houston, Tex.	5000	W01C Pittsburg, Kans.	250	CKEN Kentville, N.S.	1000d	CKEN Kentville, N		

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
KRNT	Des Moines, Iowa	5000	KCRV	Caruthersville, Mo.	10000	WKRR	Murphy, N.C.	10000	WBNY	Buffalo, N.Y.	250
KMAN	Manhattan, Kans.	5000	KXLF	Butte, Mont.	5000	WEED	Rocky Mount, N.C.	5000	WELM	Elmira, N.Y.	250
WLou	Louisville, Ky.	5000	KAWL	York, Nebr.	5000	WADA	Shelby, N.C.	5000	WSLB	Ogdensburg, N.Y.	5000
WSMB	New Orleans, La.	5000	WFEE	Manchester, N.H.	5000	KLPM	Minot, N.Dak.	5000	WOTT	Watertown, N.Y.	5000
WDEA	Ellsworth, Me.	10000	WALK	Patchogue, N.Y.	5000	WOHP	Bellevue, Ohio	5000	WBMA	Beaufort, N.C.	5000
WHMT	Howell, Mich.	500	WSAY	Rochester, N.Y.	5000	WMPO	Middleport, Pa.	5000	WGBG	Greensboro, N.C.	250
KDFO	Ortonville, Minn.	10000	WLTC	Gastonia, N.C.	10000	WFMO	Youngstown, Ohio	10000	WDXB	Hamlet, N.C.	250
WCMP	Pine City, Minn.	10000	WTAB	Labor City, N.C.	5000	KSCM	Enid, Okla.	5000	WSIC	Statesville, N.C.	250
WKOD	Kosciusko, Miss.	5000	KFJM	Grand Forks, N.D.	5000	KCLM	Salem, Oreg.	5000	WHCC	Waynesville, N.C.	250
KCHR	Charleston, Mo.	10000	WSPD	Toledo, Ohio	5000	WLAN	Lancaster, Pa.	1000	KEYJ	Jamestown, N.Dak.	250
KBRX	O'Neill, Nebr.	10000	KAST	Astoria Oreg.	1000	WHPB	Belton, S.C.	5000	WPAY	Portsmouth, Ohio	250
WLNH	Laconia, N.H.	5000	WOTR	Corry, Pa.	1000	WCSC	Charleston, S.C.	5000	KWON	Bartlesville, Okla.	250
KABQ	Albuquerque, N.M.	5000	WPZA	Pottstown, Pa.	10000	WTJS	Jackson, Tenn.	10000	KTMK	McAlester, Okla.	250
WCBA	Corning, N.Y.	10000	WKMC	Rochester Sprgs., Pa.	10000	KULP	El Campo, Tex.	1000	KNOR	Norman, Okla.	250
WRNY	Rome, N.Y.	5000	WIVV	Vieques, P.R.	1000	KBCB	Waxahatchie, Tex.	5000	KWIN	Windsor, Oreg.	250
WHIP	Moorehead, N.C.	5000	WDEF	Chattanooga, Tenn.	10000	KLGN	Logan, Ark.	10000	KOMB	Comb Grove, Oreg.	250
KQDI	Bismarck, N.D.	5000	WDXE	Lawrenceburg, Tenn.	10000	WEAM	Arlington, Va.	10000	WEST	Easton, Pa.	250
WAOC	Akron, Ohio	5000	WRGS	Rogersville, Tenn.	10000	WWOOD	Lyndburg, Va.	5000	WIET	Erie, Pa.	250
WCHI	Chillicothe, Ohio	5000	KOKE	Austin, Tex.	10000	KLOQ	Yakima, Wash.	1000	WHGB	Harrisburg, Pa.	250
KRHD	Duncan, Okla.	250	KFRQ	Longview, Tex.	1000	1400—214.2			WIAC	Johnstown, Pa.	250
KTLQ	Tahlequah, Okla.	10000	KUKO	Post, Tex.	5000	CKBC	Bathurst, N.B.	250	WKBI	St. Marys, Pa.	250
WORR	York, Pa.	5000	KSOP	Salt Lake City, Utah	10000	CKGY	Sault Ste. Marie, Ont.	250	WRAX	Williamsport, Pa.	250
WDAR	Darlington, S.C.	5000	WBTN	Bennington, Vt.	5000	CJFR	Riviere-du-Loup, Que.	1000	WPCP	Clinton, S.C.	500
WGSW	Greenwood, S.C.	10000	WHEE	Martinsville, Va.	10000	CKRN	Rouyn, Que.	250	WCOS	Columbia, S.C.	1000
WRKM	Cartersville, Tenn.	5000	KPWS	South Hill, Va.	10000	CKSN	Swanton, Sask.	5000	WGTN	Georgetown, S.C.	250
KTXJ	Jasper, Tex.	10000	KPOB	Quincy, Wash.	10000	WXAL	Demopolis, Ala.	250	WTHE	Spartanburg, S.C.	250
KCOR	San Antonio, Tex.	5000	WMOO	Moundsville, W.Va.	10000	WFPA	Ft. Payne, Ala.	250	WJZM	Clarksville, Tenn.	250
WBTL	Bedford, Va.	10000	WCCN	Neillsville, Wis.	5000	WJHD	Homewood, Ala.	250	WHUB	Cookeville, Tenn.	250
WNVA	Norton, Va.	5000	KVVO	Cheyenne, Wyo.	1000	WJHO	Opekela, Ala.	250	WSLB	Copper Hill, Tenn.	250
WAVY	Portsmouth, Va.	5000	1380—217.3			KSEW	Sitka, Alaska	250	WHPA	Kingsport, Tenn.	250
WPDOR	Portage, Wis.	10000	CFDA	Victoriaville, Que.	1000	KCLF	Clifton, Ariz.	250	WGAP	Gap, Tenn.	250
			CKPC	Brantford, Ont.	10000	KXIV	Phoenix, Ariz.	250	WKT	Shelbyville, Tenn.	250
			CKLK	Kingston, Ont.	6000	KTUC	Tucson, Ariz.	250	KRUN	Baillinger, Tex.	250
			WGYV	Greenville, Ala.	10000	KVOY	Yuma, Ariz.	250	KBYG	Big Spring, Tex.	100
			KDXE	N. Little Rock, Ark.	10000	KELD	El Dorado, Ark.	250	KUNO	Corpus Christi, Tex.	250
			KBVM	Lancaster, Calif.	10000	KCLA	Clarks Bluff, Ark.	250	KILE	Nr. Galveston, Tex.	250
			KGMS	Sacramento, Calif.	1000	KRWY	Wynne, Ark.	250	KGLV	Greenville, Tex.	250
			KSBV	Salinas, Calif.	5000	KBEA	Beaufort, Calif.	250	KRFJ	Jacksonville, Tex.	250
			KBYW	Modesto, Calif.	10000	KREO	Indio, Calif.	250	KEYE	Perryton, Tex.	250
			KRCK	Ridgecrest, Calif.	10000	KSDA	Redding, Calif.	250	KVOP	Plainville, Tex.	250
			KGB	San Diego, Calif.	1000	KSPA	Santa Paula, Calif.	250	KDWT	Stamford, Tex.	250
			WDRR	Hartford, Conn.	5000	KHOC	Truckee, Calif.	1400	KTEM	Temple, Tex.	250
			WOB	Jacksonville, Fla.	5000	KUKI	Ukiah, Calif.	250	KTFB	Texarkana, Tex.	250
			WKAT	Miami Beach, Fla.	5000	KONG	Visalia, Calif.	250	KXIX	Paris, Tex.	250
			WDD	Sanford, Fla.	5000	KRND	Delta, Colo.	250	WDOT	Burlington, Vt.	250
			WINT	Winter Haven, Fla.	10000	KBZZ	La Junta, Colo.	250	WINA	Charlottesville, Va.	250
			WAZA	Bainbridge, Ga.	10000	WSTC	Stamford, Conn.	250	WLOW	Portsmouth, Va.	250
			WLAW	Lawrenceville, Ga.	10000	WILL	Williammante, Conn.	250	WHLF	So. Boston, Va.	250
			WLBK	DeKalb, Ill.	5000	WFLT	Lt. Lauderdale, Fla.	250	WINC	Winchester, Va.	250
			WVMC	Mt. Carmel, Ill.	5000	WIRA	Ft. Pierce, Fla.	250	KRSC	Othello, Wash.	250
			KXGI	Ft. Madison, Iowa	10000	WRHC	Jacksonville, Fla.	250	KTNT	Tacoma, Wash.	250
			KSCJ	Sioux City, Iowa	5000	WPRY	Perry, Fla.	250	WBOY	Clarksburg, W.Va.	250
			KBTO	El Dorado, Kans.	5000	WRSS	Safford, Fla.	250	WRON	Roneeverte, W.Va.	250
			WFLW	Monticello, Ky.	10000	WCSA	Alma, Ga.	250	KWKW	Wheeling, W.Va.	250
			KDBC	Manchester, La.	10000	WNEK	Macon, Ga.	250	WBTH	Williamson, W.Va.	250
			KVIM	New Iberia, La.	10000	WMAF	Moultrie, Ga.	250	WATW	Ashland, Wis.	250
			KTLD	Talulaha, La.	5000	WCOH	Newnan, Ga.	250	WUJZ	Eau Claire, Wis.	250
			WBBB	Dundalk, Md.	5000	WGS	Savannah, Ga.	250	WRJN	Racine, Wis.	250
			WLYN	Lynn, Mass.	10000	KART	Jerome, Idaho	250	WRDB	Reedsburg, Wis.	250
			WKMI	Kalamazoo, Mich.	5000	KRPL	Madrid, Idaho	250	WRIG	Wausau, Wis.	250
			KLRS	Mountain Grove, Mo.	10000	WDS	Champaign, Ill.	250	KATI	Casper, Wyo.	250
			WNJ	Newton, N.J.	1000	WEGA	Evansville, Ind.	250	KODI	Cody, Wyo.	250
			WVZ	Vineland, N.J.	1000	WBAT	Marion, Ind.	250			
			WKOP	Binghamton, N.Y.	5000	KCOG	Centerville, Iowa	100			
			WMNS	Olean, N.Y.	10000	KVFD	Fort Dodge, Iowa	250			
			WCHL	Chapel Hill, N.C.	10000	KVOE	Emporia, Kans.	250			
			KEYZ	Williston, N.D.	5000	WHS	Hays, Kans.	250			
			WSAI	Cincinnati, Ohio	5000	WCYN	Cynthiana, Ky.	100			
			WVOW	Woods County, Ohio	10000	WELI	Elizabethtown, Ky.	250			
			KUIK	Hillsboro, Oreg.	10000	WFTG	London, Ky.	250			
			WMCK	McKeesport, Pa.	10000	WFRP	Hammond, La.	250			
			WPPA	Pittsville, Pa.	10000	KAOK	Lake Charles, La.	250			
			WELP	Easley, S.C.	10000	WGL	Galveston, La.	250			
			WLCM	Lancaster, S.C.	10000	WIDE	Biddeford, Maine	250			
			WNAH	Nashville, Tenn.	10000	WALN	Baltimore, Md.	250			
			KRAY	Amarillo, Tex.	5000	WWE	Fall River, Mass.	250			
			KACT	Andrews, Tex.	10000	WLLH	Lowell, Mass.	250			
			KWBA	Baytown, Tex.	10000	WHMP	Northampton, Mass.	250			
			KRYS	Corpus Christi, Tex.	5000	WELL	Battle Creek, Mich.	250			
			KXOL	Ft. Worth, Tex.	5000	WHDF	Houghton, Mich.	250			
			WBOB	Galax, Va.	10000	WMAB	Munising, Mich.	250			
			WHBG	Harrisburg, Va.	5000	WSAM	Saginaw, Mich.	250			
			KFRD	Grand Coulee, Wash.	10000	WSJM	St. Joseph, Mich.	250			
			KMO	Tacoma, Wash.	5000	WTCM	Traverse City, Mich.	250			
			WHJC	Matawan, W.Va.	5000	KYCL	Longview, Minn.	250			
			WVOW	Raywood, W.Va.	10000	KMHL	Marshall, Minn.	250			
			WBAY	Green Bay, Wis.	5000	WMIN	Mpls. St. Paul, Minn.	250			
			WISV	Viroqua, Wis.	5000	WHLB	Virginia, Minn.	250			
			WMNE	Menomonee, Wis.	10000	WBIP	Booneville, Miss.	250			
			KVRS	Rock Springs, Wyo.	10000	WNA	Grenada, Miss.	250			
						WFOR	Hattiesburg, Miss.	250			
						WQSS	Jackson, Miss.	250			
						WMB	Macon, Miss.	250			
						KFRU	Columbia, Mo.	250			
						KSIM	Sikeston, Mo.	250			
						KTTS	Springfield, Mo.	250			
						KXGN	Glendive, Mont.	250			
						KABR	Great Falls, Mont.	250			
						KCOW	Albany, Nebr.	250			
						KLIN	Lincoln, Nebr.	250			
						KBMI	Henderson, Nev.	250			
						KWNA	Winnemucca, Nev.	250			
						WTSL	Hanover, N.H.	250			
						KGFL	Roswell, N. Mex.	250			
						KTRC	Santa Fe, N. Mex.	250			
						KCHS	Truth or Consequences, N. Mex.	250			
						KTNN	Tucumcari, N. Mex.	250			
						WOND	Pleasantville, N.J.	250			
						WABY	Albany, N.Y.	250			

1360—220.4

WWWB	Jasper, Ala.	10000	CFDA	Victoriaville, Que.	1000
WMFC	Monroeville, Ala.	10000	CKPC	Brantford, Ont.	10000
WELR	Roanoke, Ala.	10000	CKLK	Kingston, Ont.	6000
KRUX	Glendale, Ariz.	5000	WGYV	Greenville, Ala.	10000
KLYR	Clarksville, Ark.	5000	KDXE	N. Little Rock, Ark.	10000
KFA	Helena, Ark.	5000	KBVM	Lancaster, Calif.	10000
KVY	Modesto, Calif.	10000	KGMS	Sacramento, Calif.	1000
KRCK	Ridgecrest, Calif.	10000	KSBV	Salinas, Calif.	5000
KGB	San Diego, Calif.	1000	KBYW	Modesto, Calif.	10000
WDRR	Hartford, Conn.	5000	WAMS	Wilmington, Del.	10000
WOB	Jacksonville, Fla.	5000	WLIZ	Lake Worth, Fla.	5000
WKAT	Miami Beach, Fla.	5000	WVXQ	Ormond Beh., Fla.	10000
WDD	Sanford, Fla.	5000	WLCY	St. Petersburg, Fla.	5000
WINT	Winter Haven, Fla.	10000	WAOA	Atlanta, Ga.	5000
WAZA	Bain				

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
KBAL	San Saba, Tex.	5000	1440	—208.2		WMJQ	Iron Mtn., Mich.	250
KNAL	Victoria, Tex.	500	CFCP	Courtenay, B.C.	1000	WJBM	Jackson, Mich.	250
WRIS	Roanoke, Va.	5000	WHHY	Montgomery, Ala.	5000	WKLA	Ludington, Mich.	250
WKBB	LaCrosse, Wis.	5000	KFOK	Scottsdale, Ariz.	5000	WHLB	Port Huron, Mich.	250
WKYO	Sheridan, Wyo.	1000	KOKY	Little Rock, Ark.	5000	KAE	Alexis, Minn.	250
1420—211.7								
CKPT	Peterborough, Ont.	1000	KVON	Napa, Calif.	500	KBMU	Bemidji, Minn.	250
CJMT	Chicoutimi, Que.	1000	KPRO	Riverside, Calif.	1000	KBNW	Breckenridge, Minn.	250
CKOM	Saskatoon, Sask.	5000	KCOY	Santa Maria, Calif.	1000	WELY	Ely, Minn.	250
WACT	Tuscaloosa, Ala.	5000	WBIS	Bristol, Conn.	5000	KFCM	St. Cloud, Minn.	250
KHFF	Pierra Vista, Ariz.	1000	WABR	Winter Park, Fla.	5000	WROX	Clarksdale, Miss.	250
KPOG	Pocahontas, Ark.	1000	WWCC	Bremen, Ga.	1000	WCJU	Columbia, Miss.	250
KSTN	Stockton, Calif.	1000	WGJB	Brunswick, Ga.	1000	WAKS	Wasson, Mo.	250
WIS	Old Saybrook, Conn.	5000	WZBJ	Williamsburg, Ky.	5000	WOKK	Meridian, Miss.	1000
WBRO	Bradenton, Fla.	1000	WPRS	Paris, Ill.	5000	WNAT	Natchez, Miss.	250
WBFB	Delray Beach, Fla.	5000	WQEM	Quincy, Ill.	1000	WROB	West Point, Miss.	250
WSTN	St. Augustine, Fla.	1000	WRCK	Rockford, Ill.	1000	WMBH	Joplin, Mo.	250
WAVO	Avondale Estates, Ga.	5000	WPGW	Portland, Ind.	5000	KIRX	Kirksville, Mo.	250
WRBL	Columbus, Ga.	5000	KCHE	Cherokee, Iowa	5000	KOKO	Warrensburg, Mo.	250
WLET	Toccoa, Ga.	5000	KJAY	Topeka, Kans.	5000	KXFN	West Plains, Mo.	250
WNET	Murphysboro, Ill.	5000	WKLX	Paris, Ky.	5000	KXBL	Bozeman, Mont.	250
WIGS	Michigan City, Ind.	1000	WZLJ	Williamsburg, Ky.	5000	KUDI	Great Falls, Mont.	250
WOC	Davenport, Iowa	5000	KJMB	Monroe, La.	5000	KLLM	Missoula, Mont.	250
KJCK	Junction City, Kans.	1000	WJAB	Westbrook, Me.	5000	KVCK	Wolf Point, Mont.	250
WTCR	Ashtland, Ky.	5000	WAAB	Worcester, Mass.	5000	WKBE	Beatrice, Nebr.	250
WHBN	Harrodsburg, Ky.	5000	WBCM	Bay City, Mich.	1000	KCSR	Chadron, Nebr.	250
WVJ5	Owensboro, Ky.	1000	WCHB	Inkster, Mich.	1000	KONE	Reno, Nev.	250
KPEL	Lafayette, La.	1000	KEVE	Golden Valley, Minn.	5000	WKXL	Concord, N.H.	250
WB5M	New Bedford, Mass.	1000	KEVV	Milville, N.J.	1000	WFGP	Atlantic City, N.J.	250
WPSK	Pittsfield, Mass.	1000	WBAB	Baytown, Tex.	5000	WCTC	New Brunswick, N.J.	250
WAMM	Flint, Mich.	500	WJNL	Niagara Falls, N.Y.	1000	KLOS	Albuquerque, N.Mex.	250
KTOE	Mankato, Minn.	5000	WBLA	Elizabethtown, N.C.	1000	KLMX	Clayton, N.Mex.	250
WSUH	Oxford, Miss.	1000	WBUY	Luxington, N.C.	5000	KOBE	Las Cruces, N.Mex.	250
WQBC	Vicksburg, Miss.	5000	KILO	Grand Forks, N.D.	1000	KENM	Portales, N.Mex.	250
KBTN	Neosho, Mo.	5000	WHHH	Warren, Ohio	5000	WHDJ	Hartford, N.Y.	250
KOOO	Omaha, Nebr.	5000	KMED	Medford, Ore.	5000	WHOL	Olean, N.Y.	250
WACK	Newark, N.Y.	5000	KODL	Dayton, Ohio	5000	WKIP	Poughkeepsie, N.Y.	250
WLNA	Peekskill, N.Y.	1000	WCDC	Carbondale, Pa.	5000	WKAL	Rome, N.Y.	250
WMYN	Mayodan, N.C.	500	WGCB	Red Lion, Pa.	1000	WATA	Boone, N.C.	250
WGAS	S. Gastonia, N.C.	5000	WGRB	Greenville, S.C.	5000	WGNK	Gastonia, N.C.	250
WYOT	Wilson, N.C.	1000	WZYY	Cowan, Tenn.	1000	WHVH	Henderson, N.C.	250
WHK	Cleveland, Ohio	5000	WHDH	McKenzie, Tenn.	5000	WHKP	Hendersonville, N.C.	250
KTAS	Hobart, Ohio	1000	KFDA	Amarillo, Tex.	5000	WHIT	New Bern, N.C.	250
KYGB	Coos Bay, Ore.	5000	KF5S	Corpus Christi, Tex.	1000	WJER	Dover, Ohio	250
WCOD	Coatesville, Pa.	5000	KDNT	Denton, Tex.	1000	WMOH	Hamilton, Ohio	250
WCEJ	DuBois, Pa.	5000	KEXL	Livingston, Tex.	1000	WMOG	Sandusky, Ohio	250
WEUC	Ponce, P.R.	1000	WKLK	Blacksburg, Va.	5000	WALD	Walden, N.H.	250
WCRE	Cheraw, S.C.	1000	WHIS	Bluefield, W.Va.	5000	KGFF	Shawnee, Okla.	250
KABR	Aberdeen, S.D.	5000	WJWR	Morgantown, W.Va.	5000	KSIW	Woodward, Okla.	250
WEMB	Erwin, Tenn.	5000	WJPG	Green Bay, Wis.	5000	KWRO	Coquille, Ore.	250
WKSJ	Pittsfield, Tenn.	1000	1450—206.8			KROE	Eugene, Ore.	1000
KFYN	Bonham, Tex.	2500	CBG	Gander, Nfld.	250	KFLW	Klamath Falls, Ore.	250
KTRE	Lufkin, Tex.	1000	CFAB	Windsor, N.S.	250	KBLM	La Grande, Ore.	250
KGNB	New Braunfels, Tex.	1000	CFJR	Brockville, Ont.	1000	WPTD	Portland, Ore.	250
KPEP	San Angelo, Tex.	1000	CHEF	Grandy, P.Q.	1000	WLEU	Erie, Pa.	250
WWSR	St. Albans, Vt.	1000	CJOY	Guelph, Ont.	250	WDAD	Indiana, Pa.	250
WDDY	Gloucester, Va.	1000	WDNG	Annisston, Ala.	250	WPAM	Pottsville, Pa.	250
WVJL	Waxhaw, Va.	1000	WYAM	Bessemer, Ala.	250	WMPST	So. Williamsport, Pa.	250
KITI	Chelalis, Wash.	5000	WDIG	Dodan, Ala.	250	WMAJ	St. Johns, Pa.	250
KUJ	Walla Walla, Wash.	5000	WFUN	Huntsville, Ala.	250	WJFA	Washington, Pa.	250
WPLY	Plymouth, Wis.	5000	WFLU	Muscogee, Ala.	250	WNEL	Cagus, P.R.	250
1430—209.7								
CKFH	Toronto, Ont.	5000	WLYC	Muscle Shoals City, Ala.	250	WWRI	W. Warwick, R.I.	250
WFHK	Pell City, Ala.	1000	KLAM	Corordova, Alaska	250	WQSN	Charleston, S.C.	250
KHBM	Monticello, Ark.	1000	KAWT	Douglas, Ariz.	250	WCRS	Greenwood, S.C.	250
KAMP	El Centro, Calif.	1000	KNOT	Prescott, Ariz.	250	WMYB	Myrtille Beach, S.C.	250
KARM	Fresno, Calif.	5000	KOLD	Dothan, Ala.	250	WBF5	Hartselle, S.Dak.	250
KALI	Pasadena, Calif.	5000	KHOG	Fayetteville, Ark.	250	KYNT	Yankton, S.Dak.	250
KOSI	Aurora, Colo.	5000	KENA	Mena, Ark.	250	WLAR	Athens, Tenn.	250
WDFB	Homestead, Fla.	5000	KYOR	Blythe, Calif.	250	WOGA	Chattanooga, Tenn.	250
WPCF	Panama City, Fla.	5000	KPAL	Palmdale, Calif.	250	WDSG	Dyersburg, Tenn.	250
WGFS	Covington, Ga.	1000	ICTP	Porterville, Calif.	250	WLAF	LaFollette, Tenn.	100
WRCD	Dalton, Ga.	1000	KSAN	San Francisco, Calif.	250	WQSS	Murfreesboro, Tenn.	250
WWGS	Tifton, Ga.	5000	KROG	Rosora, Calif.	250	KRAC	Beaumont, Tex.	250
WCNY	Ottawa, Ill.	5000	KVEN	Ventura, Calif.	250	KBEN	Carrizo Sprgs., Tex.	250
WIRE	Indianapolis, Ind.	5000	KYGA	Yuba City, Calif.	100	KCTI	Gonzales, Tex.	250
KASI	Ames, Iowa	1000	KGIU	Alamosa, Colo.	250	KMBL	Juniper, Tex.	250
KNRC	Morgan City, La.	5000	KYVY	Greeley, Colo.	250	KCVL	Lampasas, Tex.	250
WNAV	Annapolis, Md.	1000	WABJ	Bridgeton, Conn.	250	KMHT	Marshall, Tex.	250
WHIL	Medford, Mass.	5000	WILM	Wilmington, Del.	250	WCMB	McCombs, Tex.	250
WION	Ionia, Mich.	5000	WOL	Washington, D.C.	250	KNET	Palestine, Tex.	250
WBRB	Mt. Clemens, Mich.	5000	WWBJ	Brookville, Fla.	250	KSNY	Snyder, Tex.	250
WLAU	Laural, Miss.	5000	WMFJ	Days Beach, Fla.	250	KURA	Moab, Utah	250
WIL	St. Louis, Mo.	5000	WSKP	Miami, Fla.	250	KEYY	Provo, Utah	250
WNRJ	Granville Island, Nebr.	1000	WBSR	Pensacola, Fla.	250	KDXU	St. George, Utah	250
WNER	Newport, Nebr.	5000	WSPB	Sarasota, Fla.	250	WSNO	Barre, Vt.	250
WNEE	Endicott, N.Y.	5000	WSTU	Tallahassee, Fla.	250	WWSA	Brattleboro, Vt.	250
WNNC	Morgantown, N.C.	5000	WTNT	Tallahassee, Fla.	250	WFTR	Fort Royal, Va.	250
WROX	Roxboro, N.C.	1000	WGPC	Albany, Ga.	250	WREL	Lexington, Va.	250
WFOB	Fostoria, Ohio	1000	WBHF	Cartersville, Ga.	250	WVMA	Martinsville, Va.	250
WCLT	Newark, Ohio	5000	WCON	Connelia, Ga.	250	WLPM	Suffolk, Va.	250
KALV	Alva, Okla.	5000	WKEU	Griffin, Ga.	250	KBKW	Aberdeen, Wash.	250
WKTL	Tulsa, Okla.	5000	WVGS	Millersville, Ga.	250	KCLX	Claxton, Wash.	250
KGAY	Salem, Ore.	5000	WCCF	Waynesville, Ga.	250	KCSO	O'Connell, Wash.	100
WYAM	Altamoa, Pa.	5000	WVLD	Valdosta, Ga.	250	KONP	Port Angeles, Wash.	250
WFRK	Franklin, Pa.	1000	KEOK	Payette, Idaho	250	KAYE	Puyallup, Wash.	250
WBLR	Batesburg, S.C.	5000	KEWP	Keeney Falls, Idaho	250	WPAR	Parkersburg, W.Va.	250
WATP	Marion, S.C.	1000	WHFC	Cietero, Ill.	100	KFIZ	Fond du Lac, Wis.	250
KBRK	Brookings, S. Dak.	1000	WKEI	Kewanee, Ill.	100	WDLB	Marshfield, Wis.	250
WENO	Madison, Tenn.	1000	WVCS	Springfield, Ill.	250	WFPF	Port Falls, Wis.	250
WHER	Memphis, Tenn.	1000	WANE	Ft. Wayne, Ind.	250	WRCO	Richland Center, Wis.	250
KSTB	Breckenridge, Tex.	1000	WASK	Lafayette, Ind.	250	KBBS	Buffalo, Wyo.	250
KKSJ	Gladewater, Tex.	1000	WAOV	Vincennes, Ind.	250	KWRL	Riverton, Wyo.	250
KCOH	Houston, Tex.	1000	KPQJ	Cedar Rapids, Iowa	250	1460—205.4		
KLO	Ogden, Utah	5000	KWBW	Hutchinson, Kans.	250	CKRB	Villo St. Georges, Quebec	10000
KBRC	Mt. Vernon, Wash.	5000	WTOG	Cambellsville, Ky.	250	CJNB	N. Battleford, Sask.	10000
WEIR	Weirton, W.Va.	1000	WPKX	Manchester, Ky.	250	WFHM	Culman, Ala.	5000
WBEV	Beaver Dam, Wis.	1000	WPAD	Paducah, Ky.	250	WPNX	Pezy City, Ala.	5000
1480—202.6								
WABW	Mobile, Ala.	5000	KSIG	Crowley, La.	250	WTRH	Panama Beach, Fla.	5000
KHAT	Phoenix, Ariz.	1000	KNOC	Natchitoches, La.	250	WYZE	Atlanta, Ga.	5000
KGLU	Safford, Ariz.	500	WNPS	New Orleans, La.	250	WRDW	Augusta, Ga.	5000
KTCM	Berryville, Ark.	1000	WRKD	Rockland, Maine	250	WTHI	Terre Haute, Ind.	1000
KIEM	Eureka, Calif.	5000	WTKT	South Paris, Maine	250	WRSW	Warsaw, Ind.	500
KYOS	Merced, Calif.	5000	WTBO	Cumbyland, Md.	250			
KWIZ	Santa Ana, Calif.	1000	WMAS	Springfield, Mass.	250			
KTUX	Pueblo, Colo.	1000	WATZ	Alpena Township, Mich.	250			
WAFG	Armadillo, Fla.	1000	WHTC	Holland, Mich.	250			
WPEZ	Cocoa, Fla.	1000						

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
KLEE	Ottumwa, Iowa	500d	KTRR	Rolla, Mo.	250	KGBT	Harlingen, Tex.	5000d	WYTI	Rocky Mount, Va.	1000d
KLEO	Mission, Kans.	1000d	KDRO	Sedalia, Mo.	250				WEER	Warrenton, W.Va.	500d
KLEO	Wichita, Kans.	5000	KBOW	Butte, Mont.	250				WAPL	Appleton, Wis.	1000d
WKOA	Hopkinsville, Ky.	1000d	KBOA	Omaha, Neb.	250	1540—195.0					
WNKY	Neon, Ky.	1000d	WLDB	Atlantic City, N.J.	250	ZNS	Nassau, B.W.I.	5000	1580—189.2		
WTLO	Somerset, Ky.	1000d	KRSN	Los Alamos, N.Mex.	250	KPDL	Los Angeles, Calif.	1000d	CBJ	Chicoutimi, Que.	1000d
KJOE	Shreveport, La.	1000d	KRTN	Raton, N.Mex.	250	WSM	Flushing, Ill.	1000d	WHB	Talladega, Fla.	1000d
WSAR	Fall River, Mass.	5000	WCSS	Amsterdam, N.Y.	250	WBNL	Boonville, Ind.	250d	KPCA	Marked Tree, Ark.	250d
WMAX	Grand Rapids, Mich.	1000d	WBTA	Batavia, N.Y.	250	WLOI	LaPorte, Ind.	250d	KDFD	Van Buren, Ark.	1000d
WIOS	Tawas City, Mich.	1000d	WKNY	Kingston, N.Y.	250	KXEL	Waterloo, Iowa	5000d	KWIP	Merced, Calif.	500d
KAUS	Austin, Minn.	1000d	WIKY	Malone, N.Y.	250	KLKC	Parsons, Kans.	250d	KDAY	Santa Monica, Calif.	5000d
KGGX	Sidney, Minn.	1000d	WOLF	Watkins, N.Y.	250	WDOO	Wheaton, Md.	250d	KPIK	Colorado Sprgs., Colo.	5000d
KLMS	Lincoln, Neb.	1000d	WSSB	Drumham, N.C.	250	WPRR	Albany, N.Y.	5000d	WWIL	Ft. Lauderdale, Fla.	1000d
KWEW	Hobbs, N. Mex.	5000	WFLB	Fayetteville, N.C.	250	WIFM	Elkin, N.C.	2500d	WGRC	Green Cove Springs, Fla.	1000d
WLEA	Hornell, N.Y.	1000d	WLOE	Leaksville, N.C.	250	WABC	Cleveland, Ohio	1000d	WIOK	Mouth Dora, Fla.	500d
WHOM	New York, N.Y.	5000	WRNB	New Bern, N.C.	250	WJMI	Philadelphia, Pa.	5000d	WRFB	Tallahassee, Fla.	1000d
WREM	Remsen, N.Y.	1000d	WRMT	Rocky Mount, N.C.	250	WPTS	Pittsburg, Pa.	1000d	WCLS	Columbus, Ga.	1000d
WYRN	Charlotte, N.C.	1000d	WZPT	Salisbury, N.C.	250	WPME	Punkstutawney, Pa.	1000d	WBLA	Gainesville, Ga.	5000d
WYMS	Louisburg, N.C.	500d	KQVC	Knoc Valley City, N.Dak.	250	WADK	Newport, R.I.	1000d	WDQN	Quoin, Ill.	250d
WHBC	Canton, Ohio	5000	WJED	Chillicothe, Ohio	250	KCUL	Ft. Worth, Tex.	1000d	WBBA	Pittsfield, Ill.	250d
WCIN	Cincinnati, Ohio	1000d	WMBX	Cleveland Hghts., Ohio	250	KGBC	Galveston, Tex.	1000d	WKID	Urbana, Ill.	250d
WTRA	Latrobe, Pa.	500d	WQHI	E. Liverpool, Ohio	250	WTKM	Hartford, Wis.	500d	WCNB	Connersville, Ind.	250d
WDAS	Philadelphia, Pa.	5000	WMOA	Marietta, Ohio	250				WJVA	South Bend, Ind.	1000d
WISL	Shamokin, Pa.	1000d	WRRN	Marion, Ohio	250	1550—193.5					
WLOK	Memphis, Tenn.	5000d	WRRW	Chattanooga, Tenn.	250	CBE	Windsor, Ont.	1000d	WAWW	Washington, Ind.	250d
KBOX	Dallas, Mont.	1000d	KWBX	Muskogee, Okla.	100	WAAY	Huntsville, Ala.	5000	WCH	Chattanooga, Tenn.	1000d
KCLV	Pasadena, Tex.	1000d	KBKR	Baker, Oreg.	250	KOBY	San Fran., Calif.	1000d	KWNT	Davenport, Iowa	500d
KVFR	Springfield, Vt.	1000d	KRNR	Springburg, Oreg.	250	KENT	Shreveport, La.	1000d	KDSN	Denison, Iowa	500d
WBLE	Richmond, Va.	5000	KBZY	Salem, Oreg.	250	KRES	St. Joseph, Mo.	5000	WAXU	Georgetown, Ky.	250d
WLEE	Richmond, Va.	5000	WESB	Bradford, Pa.	250	WLOA	Bradock, Pa.	1000d	WMTL	Leitchfield, Ky.	250d
WBLU	Salem, Va.	5000d	WAZL	Hazleton, Pa.	250	WBSA	Bennetsville, S.C.	1000d	WPKY	Princeton, Ky.	250d
KVAN	Camas, Wash.	1000d	WARD	Waynesboro, Pa.	250				KLUW	Haynesville, La.	1000d
KKAG	Lakewood, Wash.	1000d	WAGL	Lancaster, Pa.	250	1560—192.3					
WISM	Madison, Wis.	1000d	WBCB	Levittown, Pa.	250	CFRS	Simcoe, Ont.	250d	WGFC	Bradbury Hghts., Md.	1000d
			WMRF	Levittown, Pa.	250	KPMC	Bakersfield, Calif.	1000d	WOWE	Akron, Mich.	250d
			WMGW	Meadville, Pa.	250	WBYS	Canton, Ill.	250d	KDOM	Windom, Minn.	250d
			WNBT	Wellsboro, Pa.	250	KSWI	Council Bluffs, Iowa	5000	WAMY	Amory, Miss.	5000d
			WMDD	Fajardo, P.R.	250	WXDR	Paducah, Ky.	1000d	WGLC	Centerville, Miss.	250d
			WGGD	Chattanooga, Tenn.	250	WQXR	New York, N.Y.	5000d	WESY	Leland, Miss.	1000d
			WRRB	Greenville, S.C.	250	WTNS	Coshocton, Ohio	1000d	WPMP	Pascagoula, Miss.	1800d
			KORN	Mitchell, S.Dak.	250	WTOD	Toledo, Ohio	1000d	KBIA	Columbia, Mo.	250d
			WOPI	Bristol, Tenn.	250	WKCG	Chickasha, Okla.	1000d	KNIM	Maryville, Mo.	250d
			WDXB	Chattanooga, Tenn.	250	WENA	Bayamon, P.R.	250d	WCRV	Washington, N.J.	5000d
			WJLM	Lewisburg, Tenn.	250	KHBR	Hillsboro, Tex.	250d	KHAM	Albuquerque, N.Mex.	1000d
			WDXL	Lexington, Tenn.	250	1570—191.1					
			KNOW	Austin, Tex.	250	CHUB	Nanaimo, B.C.	1000d	WPAC	Patchogue, N.Y.	5000d
			KIBL	Beaville, Tex.	250	CFRY	Portage la Prairie, Manitoba	250d	KZKY	Albamar, N.C.	250d
			KBST	Big Spring, Tex.	250	CBI	Sidney, N.S.	1000d	WYCN	Cheney, N.C.	1000d
			KHUZ	Borger, Tex.	250	CFOR	Orillia, Ont.	1000d	WKVK	Columbus, Ohio	1000d
			KNEL	Brady, Tex.	250	WCRL	Oneonta, Ala.	250d	KLTR	Blackwell, Okla.	250d
			KSAM	Huntsville, Tex.	250	WRWJ	Selma, Ala.	1000d	WCQY	Columbia, Pa.	500d
			KVOZ	Laredo, Tex.	250	KBRI	Brinkley, Ark.	250d	WANB	Waynesburg, Pa.	1000d
			KZLN	Littlefield, Tex.	250	KBT	Fortyford, Ark.	250d	WBPD	Orangeburg, S.C.	250d
			KPLT	Paris, Tex.	250	KRKC	King City, Calif.	250d	WYCL	York, S.C.	250d
			KGKB	Tyler, Tex.	250	KCVR	Lodi, Calif.	1000d	WLIJ	Shelbyville, Tenn.	1000d
			KVVC	Vernon, Tex.	250	KACE	Riverside, Calif.	1000d	KGAF	Gainesville, Tex.	250d
			KVOG	Oden, Utah	250	KLOV	Loveland, Colo.	250d	KTRU	Rusk, Tex.	1000d
			WIKI	Newport, Vt.	250	WTWB	Auburndale, Fla.	1000d	KWED	Shamrock, Tex.	1000d
			WCVA	Culpeper, Va.	250	WJPE	Fernandina Beach, Fla.	1000d	KEVA	Shamrock, Tex.	1000d
			WVAB	Hampton, Va.	250	WJAE	Ward Ridge, Fla.	250d	WILA	Danville, Va.	1000d
			WKBO	Bremerton, Wash.	250	WEAS	College Park, Ga.	250d	WPUV	Pulaski, Va.	5000d
			KLOG	Kelso, Wash.	250	WGRS	Millen, Ga.	1000d	WTTN	Watertown, Wis.	250d
			KENE	Toppish, Wash.	250	WKOZ	Alton, Ill.	1000d			
			KTEL	Wallis Walla, Wash.	250	WFRF	Freeport, Ill.	1000d	WATM	Atmore, Ala.	5000d
			WHMS	Charleston, W.Va.	250	WBEE	Harvey, Ill.	1000d	WANA	Tusumbia, Ala.	5000d
			WTKS	Charmont, W.Va.	250	WTAY	Robinson, Ill.	1000d	KPB	Pine Bluff, Ark.	1000d
			WLOH	Princeton, W.Va.	250	WILF	Frankfort, Ind.	250d	KLIV	San Jose, Calif.	1000d
			WGEZ	Beloit, Wis.	250	WOWI	New Albany, Ind.	1000d	KUUV	Ventura, Calif.	1000d
			WLXC	LaCrosse, Wis.	250	KMCD	Fairfield, Iowa	250d	WBRV	Waterbury, Conn.	5000d
			WIGM	Madford, Wis.	250	KIFJ	Webster City, Iowa	250d	WILZ	St. Petersburg Beach, Fla.	1000d
			WOSH	Oshkosh, Wis.	250	KNDY	Marysville, Kans.	250d	WELE	S. Daytona Bch., Fla.	1000d
			KIML	Gillette, Wyo.	250	KWSK	Pratt, Kans.	250d	WALB	Albany, Ga.	1000d
			KRT	Thermopolis, Wyo.	250	WKKS	Vancaburg, Ky.	250d	WLFA	Lafayette, Ga.	5000d
			KGOS	Torrington, Wyo.	250	WABL	Amite, La.	500d	WNMP	Evanston, Ill.	1000d
						KLLA	Leesville, La.	250d	WAIK	Galesburg, Ill.	5000d
						KMAR	Winnboro, La.	500d	WGEE	Indianapolis, Ind.	5000d
						WAGE	Townson, Md.	1000d	WPGO	Mt. Vernon, Ind.	500d
						WPEP	Taunton, Mass.	1000d	KWBG	Boone, Iowa	1000d
						WFRD	Grand Rapids, Mich.	1000d	KVGB	Grand Bend, Kans.	500d
						WMRS	Morris, Minn.	1000d	WDEW	Lebanon, Ky.	1000d
						KUNA	Winnona, Miss.	1000d	KEVL	White Castle, La.	1000d
						KLEX	Lexington, Mo.	250d	WTVB	Coldwater, Mich.	5000d
						WFLR	Dundee, N.Y.	250d	WDOG	Marine City, Mich.	1000d
						WBZ	Fredonia, N.Y.	250d	WOKJ	Jackson, Miss.	1000d
						WUBA	Siler City, N.C.	1000d	KDEX	Dexter, Mo.	1000d
						WHOT	Campbell, Ohio	250d	KPRS	Kansas City, Mo.	1000d
						WCLW	Mansfield, Ohio	250d	WEHH	Elmira Heights, N.Y.	500d
						WPTW	Piqua, Ohio	250d	WNYS	Salamanca, N.Y.	1000d
						KTAT	Frederick, Okla.	250d	WGTC	Greenville, N.C.	5000d
						KOLH	Pryor, Okla.	1000d	WNOS	High Point, N.C.	1000d
						KQHS	Forest Grove, Oreg.	1000d	WAKR	Akron, Ohio	500d
						KOHU	Hermiston, Oreg.	1000d	WRSB	Hillsboro, Ohio	500d
						WBUX	Doylstown, Pa.	1000d	KHEN	Henryetta, Okla.	500d
						WLBX	Latrobe, Pa.	1000d	KTIL	Tillamook, Oreg.	250d
						WMLP	Milton, Pa.	1000d	WXRF	Guyayama, P.R.	1000d
						WFGN	Gaffney, S.C.	250d	WCBG	Chambersburg, Pa.	5000d
						WLSL	Loris, S.C.	1000d	WEEZ	Chester, Pa.	1000d
						WHLP	Centerville, Tenn.	1000d	WYNG	Warwick, R.I.	1000d
						WELB	Cleveland, Tenn.	1000d	WABY	Abbeville, S.C.	1000d
						WVGL	Ringlet, Tenn.	1000d	WACA	Camden, S.C.	1000d
						KVLG	La Grange, Tex.	250d	KCCR	Pierre, S.Dak.	1000d
						KZOL	Mulshoe, Tex.	250d	WJSO	Jonesboro, Tenn.	5000d
						KTER	Terrell, Tex.	250d	WDBL	Springfield, Tenn.	1000d
						KWIC	Salt Lake City, Utah	5000d	KGAS	Carthage, Tex.	1000d
						WSWV	Pennington Gap, Va.	1000d	KERC	Eastland, Tex.	500d
									KINT	El Paso, Tex.	1000d

Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.	Kc.	Wave Length	W.P.
KYOK	Houston, Tex.	5000	KLAK	Lakewood, Colo.	1000	KVI	Vivian, La.	500d	KUSH	Cushing, Okla.	1000d
KCBZ	Lubbock, Tex.	1000	WKEN	Dover, Del.	1570	WIKX	Rockville, Md.	1000	KASH	Eugene, Oreg.	1000
KBUS	Mexia, Tex.	1000	WKTX	Atlantic Beach, Fla.	1000d	WBOS	Brookline, Mass.	5000	WHOL	Allentown, Pa.	500d
KDOD	Sinton, Tex.	1000d	WKWF	Key West, Fla.	500	WTYM	East Longmeadow, Mass.	5000d	WEZN	Elizabethtown, Pa.	500d
WEZL	Richmond, Va.	5000d	WHEW	Riviera Beach, Fla.	1000d	WHRV	Ann Arbor, Mich.	1000	WFIS	Fountain Inn, S.C.	1000d
KTIX	Seattle, Wash.	5000d	WOKB	Winter Garden, Fla.	1000d	WTRU	Muskegon, Mich.	5000	WGSU	N. Augusta, S.C.	500
WSWV	Platteville, Wis.	1000d	WCCA	Atlanta, Ga.	1000d	WKDL	Clarksdale, Miss.	1000d	WHBT	Harriman, Tenn.	5000d
WTRW	Two Rivers, Wis.	1000d	WGCA	Chicago Hgts., Ill.	1000d	KATZ	St. Louis, Mo.	5000	WKBJ	Milan, Tenn.	1000d
KCHY	Cheyenne, Wyo.	1000d	WMCW	Harvard, Ill.	500d	KTTN	Trenton, Mo.	500d	KBBB	Borger, Tex.	500d
			WBTO	Linton, Ind.	500d	KNCY	Nebraska City, Nebr.	500d	KWB	Brownsville, Tex.	1000
			WARU	Peru, Ind.	1000d	WONG	Oneida, N.Y.	1000d	WHL	Midland, Tex.	1000
			KLGA	Algonia, Iowa	5000d	WURL	Woodside, N.Y.	5000	KCFH	Cuero, Tex.	500d
			KCRG	Cedar Rapids, Iowa	5000	WGIV	Charlotte, N.C.	1000d	KMAE	McKinney, Tex.	1000d
			KMDO	St. Scott, Kans.	5000	WIDU	Fayetteville, N.C.	1000d	KOGT	Orange, Tex.	1000
			WNES	Central City, Ky.	500d	WFRS	Reidsville, N.C.	1000	KBBB	Centerville, Utah	1000d
			WSTL	Eminence, Ky.	500d	WFSK	W. Jefferson, N.C.	1000d	WHBF	Virginia Beh., Va.	1000d
			KFNV	Ferriday, La.	1000d	WBLV	Springfield, Ohio	1000d	WOL	Wheeling, W. Va.	5000d
			KLFT	Golden Meadow, La.	1000d	WTFE	Tiffin, Ohio	500d	WCWC	Ripon, Wis.	5000d

U. S. and Canadian AM Stations by Location

Abbreviations: C.L., call letters; Kc., frequency in kilocycles; N.A., network affiliation—A: American Broadcasting Co., C: Columbia Broadcasting System, Inc.; M: Mutual Broadcasting System; N: National Broadcasting Co., Inc.

Location	C.L.	Kc.	N.A.	Location	C.L.	Kc.	N.A.	Location	C.L.	Kc.	N.A.	Location	C.L.	Kc.	N.A.
Abbeville, La.	KROF	960		Abbeville, S.C.	WAND	970		Abbeville, S.C.	WAND	970		Abbeville, S.C.	WAND	970	
Abbeville, S.C.	WAND	970		Aberdeen, Md.	WMPA	1240		Aberdeen, Miss.	KABR	1220		Aberdeen, S.Dak.	KSDN	930	A
Aberdeen, Md.	WMPA	1240		Aberdeen, S.Dak.	KABR	1220		Aberdeen, Wash.	KBKW	1450		Aberdeen, Wash.	KBKW	1450	
Aberdeen, Miss.	KABR	1220		Aberdeen, Wash.	KBKW	1450		Abilene, Tex.	KNIT	1320		Abilene, Tex.	KNIT	1320	
Aberdeen, S.Dak.	KSDN	930	A	Abilene, Tex.	KNIT	1320		Abingdon, Va.	WBBI	1230		Abingdon, Va.	WBBI	1230	
Aberdeen, Wash.	KBKW	1450		Abingdon, Va.	WBBI	1230		Ada, Okla.	KADA	1230		Ada, Okla.	KADA	1230	
Aberdeen, Wash.	KBKW	1450		Ada, Okla.	KADA	1230		Auel, Ga.	WAAG	1470		Auel, Ga.	WAAG	1470	
Abilene, Tex.	KNIT	1320		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Abilene, Tex.	KNIT	1320		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Abingdon, Va.	WBBI	1230		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Abingdon, Va.	WBBI	1230		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Ada, Okla.	KADA	1230		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Ada, Okla.	KADA	1230		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Auel, Ga.	WAAG	1470		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Auel, Ga.	WAAG	1470		Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
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Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
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Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
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Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A	Adrian, Mich.	WABJ	1490	A
Adrian, Mich.	WABJ	1490	A	Adrian, Mich.											

Location	C.L. Kc. N.A.	Location	C.L. Kc. N.A.	Location	C.L. Kc. N.A.	Location	C.L. Kc. N.A.
Black River Falls, Wis.	WVIS 1260	Butler, Pa.	WBUT 1050	Chatham, Ont.	CFCO 630	Colonial Heights, Va.	WPVA 1290
Blackfoot, Idaho	KBL 690	Butte, Mont.	WBOR 1490 C	Chattanooga, Tenn.	WOPA 1450 M	Colorado City, Tex.	KVMC 1320
Blackstone, Va.	WKVL 1440		KOPR 550 M		WDFE 1370 N	Colo. Sprngs., Colo.	KRDO 1240
Blackwell, Okla.	KLTR 1580		KXLF 1370 N		WDDO 1310 C		KPIK 1580
Blakely, Ga.	WBKB 1260	Cabano, Que.	CJAF 1340		WDXB 1490		KVOR 1300 C
Blind River, Ont.	CJNR 730	Cadillac, Mich.	WATT 1240 M	Cheboygan, Mich.	WCBY 1240		KSSS 740 M
Bloomington, Ill.	WJBC 1230 A	Caguas, P.R.	WNEL 1450	Chickawago, N.Y.	WCOB 1230	Columbia, Ky.	WAIN 1270
Bloomington, Ind.	WTTS 1370		WRDL 1450	Chehalis, Wash.	KITI 1420	Columbia, Miss.	WCJU 1450 M
Bloumsburg, Pa.	WPCN 930		WFO 1430	Chelan, Wash.	KOZI 1220	Columbia, Mo.	KFRU 1400 A
Bluefield, W.Va.	WHIS 1440 N	Cairo, Ga.	WGRA 790	Cheraw, S.C.	WCRE 1420		KBIA 1580
	WKOY 1240 M	Calais, Maine	WKID 1490	Cherokee, Iowa	KCHE 1440	Columbia, Pa.	WCOS 1580
Blythe, Calif.	KYOR 1450 A	Caldwell, Idaho	WQDY 1230 N	Chester, Pa.	WEEZ 1590	Columbia, S.C.	WCOS 1400
Blytheville, Ark.	KLCN 1310	Calera, Ala.	WBYE 1370		WVCH 740		WVLC 1560 N
Boaz, Ala.	WAVC 900	Calixto, Calif.	KICG 1430 A	Chester, S.C.	WVCH 1490		WNCS 1320 C
Bogalusa, La.	WKD 1490 N	Calgary, Alta.	CFAC 960	Cheyenne, Wyo.	KFCB 1240 A		WNOK 1230 C
	WBOX 920 C		CFCN 1060		KCHV 1590	Columbia, Tenn.	WOIC 1470
Boise, Idaho	KBOL 1140 M		CKXL 1140		KVVO 1370 M		WMCP 1280
	KGEM 1140 M	Calhoun, Ga.	WCGA 900	Chicago, Ill.	WAFF 950		WKRM 1340
	KIDO 630 N	Camas, Wash.	KVAN 1480		WAIT 820	Columbus, Ga.	WAKO 540 N
	KYME 740	Cambridge, Md.	WCEM 1240		WBEM 800		WRB 420 C
Bonham, Tex.	KFYN 1420	Cambridge, Mass.	WATA 1240 A		WCFI 1000		WGBA 1270 M
Boone, Iowa	KFNB 260	Cambridge, Ohio	WILE 1270		WCRW 1240		WLSL 1580
	KWBG 1590	Camden, Ark.	KAMD 910		WEDC 1240		WOKS 1340
Boone, N.C.	WATA 1450	Camden, N.J.	WCAM 1310		WGES 1390	Columbus, Ind.	WCSI 1010
Boonville, Ind.	WBNI 1450	Camden, S.C.	WKDN 800		WGN 720 M	Columbus, Miss.	WAGR 1050
Boonville, Mo.	KWRT 1370	Camden, Tenn.	WFWL 1220		WIND 560		WCB 55 C
Booneville, Miss.	WBIP 1400	Camden, Tex.	KMIL 1220		WJH 1160	Columbus, Nebr.	KJSK 900
Booneville, N.Y.	KWB 900	Camilla, Ga.	WCLB 1220		WLS 890 A	Columbus, Ohio	WBNS 1460 C
Borger, Tex.	KHUZ 1490 M	Campbell, Ohio	WHOT 1570		WMAQ 670 N		WCOL 1230 A
	KBBS 1620	Campbellsville, Ky.	WTOC 1450		WMBI 1110		WMNI 920
Bossier City, La.	KBCL 1200	Campbellton, N.B.	CKNB 950	Chicago Hgts., Ill.	WBSC 1240		WOSU 820
Boston, Mass.	WBZ 1030	Camrose, Alta.	CFCW 1230	Chickasha, Okla.	KWCO 1560		WOT 1580
	WCOP 1150	Canon City, Colo.	KRLN 1400 M	Chico, Calif.	KWCO 1290	Civilville, Wash.	KCVL 1270
	WILD 1090	Canonsburg, Pa.	WONG 1430		KPAY 1060	Commerce, Ga.	WJJC 1270
	WNAC 890	Canton, Ga.	WCHK 1290	Chicopee, Mass.	WAGE 730	Concord, N.H.	WKXL 1450 C
	WEZE 1260 N	Canton, Ill.	WBYB 1560	Chicoutimi, Que.	CBJ 1580	Concord, N.C.	WEGO 1410
	WEEI 950 C	Canton, Miss.	WDOB 1370		CJMT 1420	Concordia, Kans.	KNGK 1390
	WHDH 890	Canton, N.C.	WWIT 970	Childress, Tex.	KCTX 1510		KFRM 550
	WMEX 1510 M	Canton, Ohio	WAND 900	Chillicothe, Mo.	KCHI 1010	Conneaut, Ohio	WVLC 1490
	WORL 950 M		WCMW 1060	Chillicothe, Ohio	WBCH 1350	Connellsville, Pa.	WCVI 1340
Boulder, Colo.	KBOL 1490		WHBC 1490	Chilliwack, B.C.	KCHW 1270	Connersville, Ind.	WCNB 1580
Bowie, Tex.	KBAN 1410	Cape Girardeau, Mo.	KFVS 960 A	Chipley, Fla.	WBGC 1240	Conroe, Tex.	KMCO 900
Bowling Green, Ky.	WKCT 930 A		KGMO 1220	Chippewa Falls, Wis.	WAXX 1150	Conway, Ark.	KCON 1230
	WBGJ 1340	Carbondale, Ill.	WCIL 1020		WBCR 1260	Conway, N.H.	WBNC 1050
	WLBJ 1410 M	Carbondale, Pa.	WCIL 1440	Christiansburg, Va.	WBEC 1260	Conway, S.C.	WLAT 1330 M
Bowl, Green, Ohio	WHRW 730 N	Caribou, Maine	WFST 600	Christiansburg, Va.	WBEC 1260	Cookeville, Tenn.	WKVC 140 C
Bozeman, Mont.	KXXL 1450 N	Carlisle, Pa.	WFLY 960	Church Hill, Tenn.	WMCH 1260	Coos Bay, Oreg.	KOOS 1230 M
	KBMN 1230	Carlisle, N.Mex.	KPBM 740	Churchill, Man.	CFCH 1230		KYNG 1420
Bradbury Hgts., Mo.	WLOA 1550	Carmel, Calif.	KRML 1410	Cicero, Ill.	WHFC 1450	Copper Hill, Tenn.	WLSB 1400
Bradbrook, Fla.	WTR 1490	Carmi, Ill.	WROY 1450	Cincinnati, Ohio	WCKY 1530	Coraque, Oreg.	KWRO 1450
Bradenton, Fla.	WBRD 1420	Carrizo Springs, Tex.	KBEN 1450		WCIN 1480	Coral Gables, Fla.	WVCG 1070
	WESB 1490 M	Carroll, Iowa	KCIM 1380		WKRC 1230	Cordoba, Ga.	WJMJ 690 M
Bradford, Pa.	KNEL 1490	Carrollton, Ala.	WRAG 590	Clanton, Ala.	WKFL 980	Cordova, Alaska	KLAM 1450
Brady, Tex.	KLIZ 1380	Carrollton, Ga.	WABC 1240	Claremore, Okla.	KWPR 1270	Corinth, Miss.	WCMA 1230
Brainerd, Minn.	KGMC 1060	Carson City, Nev.	KPTL 1300	Claremont, N.H.	WTSV 1230	Cornelia, Ga.	WCOS 1450
Brampton, Ont.	CKX 1150	Cartersville, Ga.	WBHF 1450 M	Claremont, N.V.	WBY 1400 N	Corning, Ark.	KCCB 1250
Brandon, Man.	KBHM 1220	Carthage, Ill.	WCAR 990	Clarksburg, W.Va.	WJAR 1340 M	Corning, N.Y.	WCBA 1350
Branson, Mo.	KBHM 1220	Carthage, Mo.	KDMO 1490		WPDX 750	Cornwall, Ont.	WCLI 1450 A
Brattleboro, Vt.	WTSB 1450	Carthage, Tenn.	WRKM 1350	Clarksdale, Miss.	WROX 1450 M		CJSS 1220
Brawley, Calif.	KROP 1300 A	Carthage, Tex.	KGAB 1590		WKDL 1600	Corona, Calif.	CFML 1110
Brazil, Ind.	WITE 1300	Caruthersville, Mo.	KCRV 1370	Clarksville, Ark.	KLYR 1360	Corpus Christi, Tex.	KCTA 1030 M
Brockenridge, Minn.	KDMW 1450	Casa Grande, Ariz.	KPIN 1260	Clarksville, Tenn.	WJZM 1400 M		KCTT 1150
Brockenridge, Tex.	KSTB 1430	Casper, Wyo.	KATI 1470 C	Claxton, Ga.	WCLA 1470		KEYS 1440
Bremen, Ga.	WWCC 1440		KVOC 1230 A-M	Clayton, Mo.	WCLM 1320		KRYS 1360 N
Bremerton, Wash.	KBRO 1480	Cayce, S.C.	WCAY 520		KFOU 850		KSIX 1230 A-C
Brenham, Tex.	KWHI 1280	Cedar City, Utah	KSUB 590 C	Clayton, N.Mex.	KLMX 1450	Corry, Pa.	WOT 1370
Breward, N.C.	WPNF 1240 M-N	Cedar Rapids, Iowa	KCRG 1600 M	Clearfield, Pa.	KWAO 900	Corsicana, Tex.	KAND 1340
Brewton, Ala.	WBEJ 1240 M		KPIG 1450	Clearwater, Fla.	WLAN 1340	Cortez, Colo.	KVFC 740
Bridgeport, Conn.	WIGC 800 M	Cedartown, Ga.	WGAA 1340	Cleburne, Tex.	KCLE 1120	Cortland, N.Y.	WKRT 920
	WNAB 1450 A	Center, Tex.	KDET 950	Cleveland, Ga.	WRWH 1380	Cortland, N.Y.	KOAC 550
	WSNJ 1420	Center, Tex.	KGEB 1570	Cleveland, Miss.	WCLD 1490	Cortland, N.Y.	KFJL 1240
Bridgewater, N.S.	CKBW 1000	Centerville, Tenn.	WHLP 1570	Cleveland, Ohio	WKW 400		KLOD 1340
Brigham City, Utah	KBHU 800	Centerville, Utah	KBBC 1600		WKW 400	Coshocton, Ohio	WTNS 1560
Brighton, Colo.	KBRN 890	Centralia, Ill.	WCNT 1210		WRE 1300	Cottage Grove, Oreg.	
Brinkley, Ark.	KBIA 1570	Centralia & Chehalis, Wash.	KLA 1470		WGR 1220 C		KOMB 1400
Bristol, Conn.	WBIS 1440	Centreville, Miss.	WGLC 1580	Cleveland, Tenn.	WJH 1340 M	Coudersport, Pa.	WFRM 600
Bristol, Tenn.	WQPI 1490 N	Chadron, Nebr.	KCSR 1450		WCLF 1570	Council Bluffs, Iowa	KSWI 1560 M-A
Bristol, Va.	WCYB 690 A	Chambersburg, Pa.	WCHA 800		WVLE 1410	Courtenay, B.C.	CFCP 1440
	WFHG 980 M		WCBG 1590		WJMB 1490	Courtenay, Ga.	WGFS 1430
Brockton, Mass.	WBET 1460	Champaign, Ill.	WCBS 1400 C		WVLE 1410	Covington, Ky.	WZIP 1050 M
Brockville, Ont.	CFJR 1450	Chanell Hill, N.C.	WCHL 1360		WJMB 1490	Covington, La.	WAB 730
Broken Bow, Nebr.	KONI 1280	Charleroi, Pa.	WESA 940		KCLF 1400 A	Covington, Tenn.	WKBL 1250
Brookfield, Mo.	KGHM 1470	Charles City, Iowa	KCHA 1580		WCFV 1230	Covington, Va.	WKCY 1340 A
Brookhaven, Miss.	WCHJ 1470	Charleston, Ill.	WEIC 1270		WHOU 1520	Cowan, Tenn.	WVLC 1440
	WJMB 1340 M	Charleston, Mo.	KCHR 1350		KROS 1340	Craig, Colo.	KRAI 550
Brookings, Oreg.	KURY 910	Charleston, S.C.	WCSC 1390 C		KROS 1340	Cranbrook, B.C.	CKEK 570
Brookings, S.Dak.	KBRK 1430		WPAJ 1340 A-M		KDKD 1280	Crane, Tex.	KCRN 1380
Brookline, Mass.	WBOS 1600		WQSN 1450		WRR 880 A	Crescent City, Calif.	KPLY 1240
Brooklyn, N.Y.	WPOW 1330	Charleston, W.Va.	WCWA 1400		KWQE 1320	Creston, Iowa	KSIB 1520
Brooksville, Fla.	WVJB 1450	Chattanooga, Tenn.	WCHS 580 C		WPCC 1400	Crestview, Fla.	WCNU 1010
Brownfield, Tex.	KTFY 1300		WHMS 1490 A		WVLE 1230		WVLC 1560
Brownsville, Tex.	KBOR 1600 A		WKAZ 950 N		KVLR 1240	Crewe, Va.	WSVS 800
Brownwood, Tex.	KBWD 1380 M		WTIP 1240 M		KCHV 970	Crockett, Tex.	KIYY 1290
	KEAN 1420 A		WCER 1390		KBX 1470	Crookston, Minn.	KROX 1260
	WGA 1400 A		WBT 1110 C		WCOJ 1420	Crossett, Ark.	KAGH 800
Brunswick, Ga.	WMOG 1490		WAYS 610 A		WKGO 860	Crossville, Tenn.	WAEW 1530
	WCME 900		WGVA 1600		WZZR 1480	Crowley, La.	KSJ 1450 M
Brunswick, Maine	WCME 900		WHTC 1310		WRKT 1300	Cuero, Tex.	KCFH 600
Bryan, Tex.	KORA 1240 M		WIST 930 M		KODI 1400	Cullman, Ala.	WFMH 1460
	WTAW 1150		WSOC 1240 N		KVIN 1210	Culpeper, Va.	WCVA 1490 M
Buffalo, N.Y.	WBEN 930 C		WVOK 1490		KZIN 1050 A	Cumberland, Ky.	WCPM 1280
	WBNY 1400	Charlottesville, Va.	WCHV 1260 A		KGFF 650 A	Cumberland, Md.	WCUM 1230 C
	WEBR 970 M		WELK 1010		KVLS 1590	Cushing, Okla.	KUSH 1600
	WGR 550		WINA 1400 M		WTVB 1590		
	WKBW 1520 N	Charlottetown, P.E.I.	CFCY 630		KCLX 1450		
	WWOL 1120 A	Chase City, Va.	WMEK 980		WDEA 1570		
Buffalo, Wyo.	KBBS 1450						
Burford, Ga.	WDMF 1460						
Burbank, Calif.	KBIA 1490						
Burley, Idaho	KBAR 1230 A-M						
Burlington, Iowa	KBUR 1490 A						
Burlington, N.C.	WBBS 920 M						
	WBAG 1150						
Burlington, Vt.	WCAX 620 N						
	WDOT 1400						
	WJOY 1230 A						
Burns, Oreg.	KRNS 1230						
Butler, Ala.	WPRN 1220						

Location	C.L. Kc. N.A.	Location	C.L. Kc. N.A.	Location	C.L. Kc. N.A.	Location	C.L. Kc. N.A.
Lancaster, Calif.	KAVL 610	Lock Haven, Pa.	WPBZ 1280 M	Marinette, Wis.	WMAM 570 N	Midland, Tex.	KCRS 550 A
Lancaster, Ohio	KBVM 1380	Lockport, N.Y.	WUSJ 1340	Marion, Ala.	WJAM 1310	KJBC 1500	KWEL 1600
Lancaster, Pa.	WHOK 1820	Lodi, Calif.	KCVR 1570	Marion, Ill.	WGGH 1150	KWBJ 1600	KWBJ 1600
Lancaster, Pa.	WGAL 1490 N	Logan, Utah	KVNU 610 M	Marion, Ind.	WBAT 4400 A	Miles City, Mont.	KATL 1340 M
Lancaster, S.C.	WLAM 1360	Logan, W.Va.	WLBG 1230 M	Marion, N.C.	WBRM 1250	Millford, Del.	WKBS 930
Lander, Wyo.	KOVE 1330 M	Logansport, Ind.	WVOW 1290	Marion, N.C.	WBRM 1490 A	Millford, Mass.	WMRC 1490
Landry, Ala.	WRLD 1490 A	Lompoc, Calif.	WSAL 1280 M	Marion, S.C.	WMBT 1430 A	Millidgeville, Ga.	WGSV 1450 M
Lansford, Pa.	WLSH 1410	London, Calif.	KNEZ 960	Marion, Va.	WMEV 1010 A	Millen, Ga.	WGVS 860
Lansing, Mich.	WLS 1320	London, Ky.	WFTG 1400	Marked Tree, Ark.	KPCA 1580	Millington, Tenn.	WHY 1220
Lapeer, Mich.	WJIM 1240 A-N	London, Ont.	CFPL 980	Marksville, La.	KAPB 1370	Millville, N.J.	WMVB 1440
LaPorte, Ind.	WMPC 1290	Long Beach, Calif.	CKSL 1290	Marlborough, Mass.	WSRO 1470	Milton, Fla.	WEYB 1330 M
Laramie, Wyo.	WL01 1540	Long Beach, Calif.	KFOX 1280	Marlin, Tex.	KMLW 1010	Milwaukee, Wis.	WSRA 1490
Laredo, Tex.	KOWB 1340 M	Longmont, Colo.	KGER 1390	Marquette, Mich.	KDMJ 1320 M	WMLP 1570	WMLP 1570
LaSalle, Ill.	WLPO 1220	Long Prairie, Minn.	KELY 1400	Marshall, Minn.	KMT 1400 A	WFOX 1250 M	WFOX 1250 M
LaSarre, Que.	CKLS 1420	Longview, Tex.	KFRD 1370 A	Marshall, Mo.	KMMO 1300	WRIT 3400	WRIT 3400
LasCruces, N.Mex.	KOBE 1450	Longview, Wash.	KLUE 1280	Marshall, N.C.	WMMH 1460	WISN 1150 A	WISN 1150 A
Las Vegas, Nev.	KGRT 570	Lorain, Ohio	KEDO 1400 A	Marshall, Tex.	KMHT 1450	WMIL 1290	WMIL 1290
Las Vegas, Nev.	KENO 1460 A	Lorain, Ohio	KBAM 1270 A	Marshalltown, Iowa	KFBZ 1230	WOKY 920	WOKY 920
Las Vegas, Nev.	KLAS 1230 C	Louis, S.C.	WWIZ 1380 A	Marshallfield, Wis.	WDLB 1450	WTMJ 620 N	WTMJ 620 N
Las Vegas, Nev.	KRAM 920 M	Los Alamitos, N.Mex.	WLSJ 1570	Martin, Tenn.	WTIG 980	Mineral Wells, Tex.	KORC 1410
Las Vegas, Nev.	KRBO 1050	Los Angeles, Calif.	KABC 790 A	Martinsburg, W.Va.	WEPM 1340	Minneapolis, Minn.	WFCY 1150
Las Vegas, Nev.	KFUN 1230 A	Los Angeles, Calif.	KFI 640 N	Martinsville, Va.	WHEE 1370	Minneapolis, Minn.	WCCO 830 C
LaTrobe, Pa.	WSHH 1570 M	Los Angeles, Calif.	KHJ 930 M	Marysville, Calif.	KMYC 1410 M	Minden, La.	WL03 1380
LaTrobe, Pa.	WTRA 1480	Los Angeles, Calif.	KFSG 1150	Marysville, Kans.	KNDY 1570	Mineral Wells, Tex.	WMIN 1400
LaTuque, Que.	CFLM 1240	Los Angeles, Calif.	KFVB 980	Marysville, Mo.	KNIM 1580	Minneapolis, Minn.	WDFW 1130
Laurel, Miss.	WAML 1340 N	Los Angeles, Calif.	KGFI 1230	Marysville, Tenn.	KWCA 1400	Missoula, Mont.	WTCN 1280 A
Laurel, Miss.	WNSL 1250	Los Angeles, Calif.	KFCF 1390	Mason City, Iowa	KRIB 1490	Missoula, Mont.	KTIS 900
Laurens, S.C.	WLBG 860	Los Angeles, Calif.	KKAC 1390	Massena, N.Y.	KSMN 1010	Minot, N.Dak.	KUDM 770
Laurinburg, N.C.	WEWO 1080	Los Angeles, Calif.	KKAY 570	Massena, N.Y.	WMSA 1340 A	Minot, N.Dak.	KLPM 1390 M
Lawrence, Kans.	KFKU 1250	Los Angeles, Calif.	KMPK 710	Massillon, Ohio	WSTS 1050	Mission, Kans.	KQDY 1320
Lawrence, Kans.	KLWN 1320	Los Angeles, Calif.	KNX 1070 C	Massillon, Ohio	WTFG 980	Mission, Kans.	KCBK 1480
Lawrence, Mass.	WCOM 900 M	Los Angeles, Calif.	KPOL 1540	Matane, Que.	CKB 1250	Missoula, Mont.	KIRT 1580
Lawrenceburg, Tenn.	WDXE 1490	Louisburg, N.C.	KPOP 1020	Matawan, W.Va.	WHIC 1360	Missoula, Mont.	KGYO 1290 C
Lawrenceburg, Tenn.	WLAW 1360	Louisville, Miss.	KRKO 1150	Mattison, Ill.	WLBH 1170	Missoula, Mont.	KXLL 1450 N
Lawrenceville, Ill.	WAKO 910	Louisville, Miss.	WYRN 1480	Mayaguez, P.R.	WAEI 600	Missoula, Mont.	KQTE 1340 M
Lawton, Okla.	KSWO 1380 A	Louisville, Miss.	WAYE 970 N	Mayfield, Ky.	WKJB 710	Missoula, Mont.	KYSS 910
Lawton, Okla.	KCCO 1050	Louisville, Miss.	WYFV 790 M	Mayfield, N.C.	WMYN 1320	Moab, Utah	KORR 980
Lawton, Okla.	KLVC 1230	Louisville, Miss.	WHAS 840 C	Mayfield, N.C.	WNGD 1320	Moab, Utah	KURA 450
Leadville, Colo.	WL0E 1490 M	Louisville, Miss.	WKLO 1080 A	Mayfield, Ky.	WFTM 1240 M	Mobile, Mo.	KNCM 1230
Leadville, Colo.	WLOE 1490 M	Louisville, Miss.	WINN 1240	Mayfield, N.C.	WFTM 1240 M	Mobile, Ala.	WALA 1410 N
Leaksville, N.C.	CJSP 1410	Louisville, Miss.	WKYV 900	Mayfield, N.C.	WFTM 1240 M	Mobile, Ala.	WABB 1480 A
Leaksville, N.C.	WLOE 1490 M	Louisville, Miss.	WLOU 1350	Mayfield, N.C.	WFTM 1240 M	Mobile, Ala.	WGGK 900
Leavenworth, Kans.	WLBW 1590	Louisville, Miss.	WLSM 1270	Mayfield, N.C.	WFTM 1240 M	Mobile, Ala.	WGOB 840
Lebanon, Ky.	KLWT 1230	Louisville, Miss.	WLTG 1570	Mayfield, N.C.	WFTM 1240 M	Mobile, Ala.	WKRQ 910 C
Lebanon, Mo.	KGAL 920	Louisville, Miss.	WLVG 1570	McAllen, Tex.	KNEE 1560	Mobile, Ala.	WMOZ 960
Lebanon, Pa.	WLBW 1270	Louisville, Miss.	WLVG 1570	McCamery, Tex.	KCMR 1450	Mobile, Ala.	KOLY 1300
Lebanon, Pa.	WCBR 900	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Modesto, Calif.	KTRB 860
Leesburg, Fla.	WLBE 790 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Modesto, Calif.	KBEE 970 A
Leesburg, Fla.	WBI 1410	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Modesto, Calif.	KFTV 1350 A
Leesville, La.	WAGE 1290	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Modesto, Calif.	WGU 1230
Leesville, La.	KLLA 1570	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KVKM 1340 M
Leitchfield, Ky.	WMTL 1580	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBAF 1300
Leland, Miss.	WESY 1580	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KCKW 1220
LeMars, Iowa	KLEM 1410	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KRMO 990
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WBAM 1330
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WRE 1490
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KMLB 1440 A-N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KLIC 1230 M
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KNOE 1390
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WMIC 560
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WMAP 1060
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WEKZ 1268
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVAP 1600
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WHYY 1440 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WMGY 800
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WRMA 950
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVON 1340 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KHBM 1430
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WFLW 1360
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKBM 1490
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WSKI 1240 A
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBF 690
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBN 940 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CFBC 600 A
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CJAD 800
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CJMS 1280
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKGC 730 C
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKRM 980
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KLU 580
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WPFL 350
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVAP 1600
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WHYY 1440 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WMGY 800
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WRMA 950
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVON 1340 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KHBM 1430
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WFLW 1360
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKBM 1490
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WSKI 1240 A
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBF 690
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBN 940 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CFBC 600 A
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CJAD 800
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CJMS 1280
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKGC 730 C
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKRM 980
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KLU 580
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WPFL 350
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVAP 1600
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WHYY 1440 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WMGY 800
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WRMA 950
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVON 1340 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KHBM 1430
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WFLW 1360
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKBM 1490
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WSKI 1240 A
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBF 690
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CBN 940 N
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CFBC 600 A
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CJAD 800
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CJMS 1280
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKGC 730 C
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	CKRM 980
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	KLU 580
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WPFL 350
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WVAP 1600
LeMars, Iowa	WJRI 1340 M	Louisville, Miss.	WLVG 1570	McComb, Miss.	WHNY 1250 A	Monahans, Tex.	WH

Location	C.L.	Kc.	N.A.	Location	C.L.	Kc.	N.A.	Location	C.L.	Kc.	N.A.	Location	C.L.	Kc.	N.A.
Shreveport, La.	KANB	1300		Suffolk, Va.	CHNO	900		Trinidad, Colo.	WTTM	920	N	Wallace, Idaho	KWAL	620	M
	KCIJ	1050		Sulphur, La.	WHPM	1450	A	Troy, Ala.	KCRT	1240	M	Wallace, N.C.	WLSE	1400	
	KEEL	710		Sulphur Sprgs., Tex.	KIKS	1310		Troy, N.Y.	WTFB	970	M	Walla Walla, Wash.	KHIT	1320	
	KENT	1550	M	Summerside, P.E.I.	KSST	1230			WHAZ	1330			KUJ	1420	M
	KJOE	1480		Summersville, Ga.	CJRW	1240			WTRY	980			KTEL	1490	A
	KOKA	980		Sumter, S.C.	WGTA	950		Truckee, Calif.	WFLG	290		Walnut Ridge, Ark.	KRLV	1320	M
	KRMD	1340	A	Sunbury, Pa.	WFIQ	290		Truro, N.S.	WSSC	1340	A	Walsenburg, Colo.	KFLJ	1380	
Sidney, Mont.	KWKH	1130	M	Sunnyside, Wash.	WVCO	1240	C	Truth or Consequences, N.M.	WVCO	1240	C	Waterboro, S.C.	WALD	1220	M
Sierra, Nebr.	KSID	1340	A	Superior, Nebr.	KREW	1230		Tryon, N.C.	WWTN	1580		Waltham, Mass.	WCRB	1390	
Silver City, Ariz.	KHFH	1420	A	Superior, Wis.	KRFS	1600		Tucson, Ariz.	WTKA	1400	A	Walton, N.Y.	WDRB	1370	
Sikeston, Mo.	KSIM	1400		Susanville, Calif.	WDSM	710	N		KAJR	1490		Ware, Mass.	WDA	1270	
Siler City, N.C.	WNCA	1570		Suswainboro, Ga.	WQMN	1320			KCFE	790		Warner Robbins, Ga.	WARE	1250	M
Siloam Sprgs., Ark.	KUQA	1290	M	Sweetwater, Tenn.	KSUE	1240			KCUB	1290	N	Warren, Ark.	KWRF	860	
Silsbee, Tex.	KKAS	1340		Sweetwater, Tex.	WDEH	800			KEVT	690	N	Warren, Ohio	WVHH	1440	
Silver City, N.M.	KKIL	1340	C	Swift Current, Sask.	KXOX	1240			KMOP	1330		Warren, Pa.	WNAE	1310	
Silver Sprgs., Md.	WQMR	1050		Sydney, N.S.	CKSW	1400			KTKT	960		Warrensburg, Mo.	KOKO	1450	
Simcoe, Ont.	CFRS	550			CBZI	1570			KOLD	1450	C	Warrenton, Mo.	KWRE	730	
Sinton, Tex.	KTOD	1590			CJCB	1270			KTNM	1400	M	Warrenton, Va.	FEER	1570	
Sioux City, Iowa	KSCJ	1360	A	Sylacauga, Ala.	WFEB	1340	M	Tucumcari, N.Mex.	KCNM	1400	M	Warsaw, Ind.	WRSW	1480	
	KMNS	620		Sylvania, N.C.	WFLS	1290		Tulare, Calif.	KCNM	1400	M	Warsaw, Va.	WNNT	690	
	KTRI	1470		Sylvania, Ga.	WWSY	1490		Tulia, Tex.	KGEN	1370		Warwick-E.Greenwich, R.I.	WYNG	1590	
Sioux Falls, S.Dak.	KISD	1230		Syracuse, N.Y.	WHEN	620	C	Tullahoma, Tenn.	KTUE	1260		Wasco, Calif.	KWSD	1050	
	KIHO	1270			WFBL	1390	A	Tulsa, Okla.	WJIG	740		Washington, D.C.	WCMS	570	
	KS00	1140	A		WVDR	1260	M		KAKC	970			WOL	1450	M
Sitka, Alaska	KIFW	1230	C-A		WOLF	1490	A		KRMG	1300			W00K	1340	
	KSEW	1400			WYAB	570	N		KTUL	1490	C		WVDC	1260	
Skowhegan, Maine	WGHM	1150		Tabor City, N.C.	WYR	1490	A	Tupelo, Miss.	KV00	1170	N		WRC	980	N
Smithfield, N.C.	WMPM	1270		Tacoma, Wash.	KMO	1360			WEL0	580	M	Washington, Ga.	WTOP	1500	C
Smiths Falls, Ont.	CJET	680			KTAC	850			WTUP	1490	A	Washington, Ind.	WAME	1560	
Snyder, Tex.	KSNY	1450	M	Taft, Calif.	KTKR	1310			WJRD	1390		Washington, Ind.	WVMS	1580	
Socorro, N.Mex.	KSRC	1290		Tahlequah, Okla.	WJHB	1300			WACT	1420		Washington, N.C.	W00W	1340	
Soda Sprgs., Idaho	KBRV	540		Talladega, Ala.	WNUZ	1230	M		WTUG	790			WRRF	930	A
Somerset, Ky.	WFSF	1240	M	Tallahassee, Fla.	WMEN	1330			WTBC	1230	M	Washington, Pa.	WJPA	1450	M
	WTLO	1480			WFRB	1580			WVNA	1590		Washington Court House, Ohio	WCHO	1250	
	WVSC	990			WTAL	1270			WVNB	1270	N	Waterbury, Conn.	WBRY	1590	C
Sonora, Calif.	KROG	1450			WTLS	1300			WVNL	1590			WVCO	1240	M
Sorel, P.Q.	CISD	1320		Tallahassee, Ala.	WTNT	1450	A-M		WVNL	1590			WVDE	550	M
So. Bend, Ind.	WVNDU	1490		Tallulah, La.	WALT	1110			WVNL	1590		Waterbury, Vt.	KXEL	1540	A
	WJVA	1580	M	Tampa, Fla.	WDAE	1250	C		WVNL	1590		Waterloo, Iowa	KNWS	1090	
	WSBT	960	C		WFLA	970	N		WVNL	1590			KWVL	1390	M
	WES0	970			WBBO	1050			WVNL	1590		Watertown, N.Y.	WOTT	1400	
	WHLF	1400	A		WTMP	1150			WVNL	1590			WVNY	790	C
South Daytona Beach, Florida	WELE	1590			WWSL	1300			WVNL	1590		Watertown, S.Dak.	KWAT	950	M
So. Gastonia, N.C.	WGAS	1420		Tarboro, N.C.	WCPB	760			WVNL	1590		Watertown, Wis.	WTTN	1580	
So. Paris, Mo.	WKTO	1450		Tarpon Sprgs., Fla.	WDCL	1470			WVNL	1590		Waterville, Me.	WTVL	1490	A
So. Pittsburg, Tenn.	WEPG	910		Tasley, Va.	WESR	1330			WVNL	1590		Watsonville, Calif.	KOMY	1340	
So. St. Paul, Minn.	WISK	630	M	Taunton, Mass.	WPEP	1570			WVNL	1590		Wauchula, Fla.	WALU	1310	
So. Williamsport, Pa.	WMPT	1450		Tawas City, Mich.	WIOS	1480			WVNL	1590		Waukegan, Ill.	WVNS	1220	
	WHCO	1230		Taylor, Tex.	KTAE	1260			WVNL	1590		Waukegan, Wis.	WVNS	1220	
Sparta, Ill.	WHSI	1050		Taylorville, Ill.	WTIM	1410			WVNL	1590		Waupaca, Wis.	WVNS	1220	
Sparta, Tenn.	WSPR	1290		Tell City, Ind.	WTCJ	1230			WVNL	1590		Wausau, Wis.	WVNS	1220	
Spartanburg, S.C.	WTHA	1400	M	Temple, Tex.	KTEM	400			WVNL	1590			WVNS	1220	
	WTRD	910	N	Terre Haute, Ind.	WBOW	1230	N		WVNL	1590			WVNS	1220	
	WSPA	950	C		WMFT	1300			WVNL	1590			WVNS	1220	
	KICD	1240			WTHI	1480	C		WVNL	1590			WVNS	1220	
Spencer, Iowa	KGA	1510	A	Terrell, Tex.	KTER	1570			WVNL	1590			WVNS	1220	
Spokane, Wash.	KLYI	1230		Texarkana, Ark.	KOSY	790	M		WVNL	1590			WVNS	1220	
	KPEG	1380		Texarkana, Tex.	KCMC	1230	A		WVNL	1590			WVNS	1220	
	KHQ	590	N		KFTS	400			WVNL	1590			WVNS	1220	
	KHJ	920	C		KFTS	400			WVNL	1590			WVNS	1220	
	KXLY	920	C		KFTS	400			WVNL	1590			WVNS	1220	
	KGFS	1330			KFTS	400			WVNL	1590			WVNS	1220	
Springdale, Ark.	KGRS	1340	A		KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Ill.	WCVS	450	A-M		KFTS	400			WVNL	1590			WVNS	1220	
	WMAY	970	N		KFTS	400			WVNL	1590			WVNS	1220	
	WTAX	1240	C		KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Mass.	WBZA	1030			KFTS	400			WVNL	1590			WVNS	1220	
	WHVN	560	C		KFTS	400			WVNL	1590			WVNS	1220	
	WMAS	1450	M		KFTS	400			WVNL	1590			WVNS	1220	
	WSPR	1270			KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Mo.	KGBX	1260	N		KFTS	400			WVNL	1590			WVNS	1220	
	KICK	1340			KFTS	400			WVNL	1590			WVNS	1220	
	KTTS	1400	C		KFTS	400			WVNL	1590			WVNS	1220	
	KWTO	560	A		KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Ohio	WIZE	1340			KFTS	400			WVNL	1590			WVNS	1220	
	WVLY	1600			KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Ore.	KEED	1050			KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Tenn.	WDBL	1590			KFTS	400			WVNL	1590			WVNS	1220	
Springfield, Vt.	WCFR	1480			KFTS	400			WVNL	1590			WVNS	1220	
Springhill, La.	KBSF	1460			KFTS	400			WVNL	1590			WVNS	1220	
Spruce Pine, N.C.	WTDE	1470			KFTS	400			WVNL	1590			WVNS	1220	
Stamford, Conn.	WSTC	1400			KFTS	400			WVNL	1590			WVNS	1220	
Stamford, Tex.	KDWT	1400	A		KFTS	400			WVNL	1590			WVNS	1220	
Starks, Fla.	WRGR	1490			KFTS	400			WVNL	1590			WVNS	1220	
Starkville, Miss.	WSSO	1230			KFTS	400			WVNL	1590			WVNS	1220	
State College, Pa.	WMAJ	1450	M		KFTS	400			WVNL	1590			WVNS	1220	
Statesboro, Ga.	WVNS	1240			KFTS	400			WVNL	1590			WVNS	1220	
Statesville, N.C.	WVNS	1240			KFTS	400			WVNL	1590			WVNS	1220	
Stauton, Va.	WDBM	1400			KFTS	400			WVNL	1590			WVNS	1220	
	WVNS	1240	A		KFTS	400			WVNL	1590			WVNS	1220	
Stephenville, Tex.	WVNS	1240			KFTS	400			WVNL	1590			WVNS	1220	
Sterling, Colo.	KGEC	1230			KFTS	400			WVNL	1590			WVNS	1220	
	KOLR	1490			KFTS	400			WVNL	1590			WVNS	1220	
Sterling, Ill.	WSDR	1240			KFTS	400			WVNL	1590			WVNS	12	

Location	C.L. Chan.	Location	C.L. Chan.	Location	C.L. Chan.	Location	C.L. Chan.	
Harrisonburg	WSVA-TV 3	KIRO-TV	7	Huntington	WHTN-TV 13	Milwaukee	WISN-TV 12	
Lynchburg	WLVA-TV 13	KOMO-TV	4		WSAZ-TV 3		WMVS-TV *10	
Norfolk	WTAR-TV 3	KHQ-TV	2	Oak Hill	WOAY-TV 4		WTMJ-TV 4	
Petersburg	WXEX-TV 8	KREM-TV	6	Parkersburg	WTAP-TV 15		- WX18 18	
Portsmouth	WAVY-TV 10	KXLY-TV	4	Wheeling	WTRF-TV 7	Wausau	WSAU-TV 7	
Richmond	WRVA-TV 12	KTNT-TV	11			Whitfish Bay	WITI-TV 6	
	WTVR 8	KPEC-TV	56	WISCONSIN				
Roanoke	WDBJ-TV 7	KTWV	13	Eau Claire	WEAU-TV 13	WYOMING		
	WLSL-TV 10	KIMA-TV	29	Green Bay	WBAY-TV 2	Casper	KTWO-TV 2	
WASHINGTON					WFRV	5	Cheyenne	KFCB-TV 5
Bellingham	KVOS-TV 12	KNDD-TV	23		WKBT	8	Riverton	KWRB-TV 10
Everett	KBAS-TV 16	KNBS	22	La Crosse	WHA-TV *21			
Pasco	KEPR-TV 19	WEST VIRGINIA						
Seattle	KCTS-TV 9	Bluefield	WHIS-TV 6	Madison	WISC-TV 3			
	KING-TV 5	Charleston	WCHS-TV 8	Marinette	WKOW-TV 27			
		Clarksburg	WBOY-TV 12		WMTV 33			
					WMBV-TV 11			

Canadian Television Stations

Location	C.L. Chan.	Location	C.L. Chan.	Location	C.L. Chan.	Location	C.L. Chan.
ALBERTA				MANITOBA			
Calgary	CHCT-TV 2	Brandon	CKX-TV 5	ONTARIO			
Edmonton	CFRN-TV 3	Winnipeg	CBWT 13	Barrie	CKVR-TV 3	Clermont	CFCV-TV-1 75
Lothbridge	CJLH-TV 7	NEW BRUNSWICK				Estouart	CJES-TV-1 70
Medicine Hat	CHAT-TV 6	Moneton	CKCW-TV 2	Elk Lake	CFCL-TV-2 2	Jonquiere	CKRS-TV 12
Red Deer	CHCA-TV 6	Saint John	CHSJ-TV 4	Hamilton	CHCH-TV 11	Matane	CKBL-TV 9
BRITISH COLUMBIA				NEWFOUNDLAND			
Dawson Creek	CJDC-TV 5	Argentia	CJDX-TV 10	Kenora	CBWAT 8	Montreal	CBFT 2
Kamloops	CFCR-TV 4	Corner Brook	CBYT 5	Kingston	CKWS-TV 11		CBMT 6
Kelowna	CHBC-TV 2	Grand Falls	CJCN-TV 3	Kitchener	CKCO-TV 13	New Carlisle	CHAU-TV 5
	CHGP-TV-1 72	St. John's	CJON-TV 6	London	CFPL-TV 10	Quebec	CFQM-TV 4
Oliver	CHBC-TV-3 8	Stephenville	CFSN-TV 8	North Bay	CKGN-TV 10		CKMI-TV 5
Penticton	CHBC-TV 13	NOVA SCOTIA				Rimouski	CJBR-TV 3
Vancouver	CBUT 2	Halifax	CBHT 3	Peterborough	CHEX-TV 12	Rouyn	CKRN-TV 4
Vernon	CHBC-TV 7	Inverness	CJCB-TV-1 6	Ottawa	CBOT 9	Sherrbrooke	CHLT-TV 7
Victoria	CHEK-TV 6	Liverpool	CBHT-1 12	Port Arthur	CFJG-TV 2	Three Rivers	CKTM-TV 13
LABRADOR				New Glasgow	CFCY-TV-1 7		
Goose Bay	CFLA-TV 8	Shelburne	CBHT-2 8	Sudbury	CKSO-TV 5		
		Sydney	CJCB-TV 4	Timmins	CFCL-TV 6		
		Yarmouth	CBHT-3 11	Toronto	CBLT 6		
				Windsor	CKLW-TV 9		
				Wingham	CKNX-TV 8		
				PRINCE EDWARD ISLAND			
				Charlottetown	CFCY-TV 13		

World-Wide Short-Wave Stations

Most international broadcasting is done within frequency limits agreed upon at international conventions. These frequency ranges are listed here, at the right, expressed both in frequency and by meter bands (wave-length).

Reception in the various bands varies according to the time of day and season of the year. Reception in the 60, 49 and 41 meter bands is best at night during the winter months. Reception in the 31 and 25 M. bands is best at night, but all year. Reception in the 19, 16, 13 and 11 M. bands is best during the day, also at night during the summer in the 16 and 19 M. bands.

Abbr.: AIR—All India Radio; RAI—Radiotelevisione Italiana; RTF—Radiffusion Television Francaise; VOA—Voice of America; RFE—Radio Free Europe. • denotes stations beaming evening (U.S.) broadcasts to the U.S., † morning or afternoon broadcasts.

Kcs. Call and Location	Kcs. Call and Location	Kcs. Call and Location	Kcs. Call and Location
4630 HGGBI, Quito, Ecu.	4945 HJCV, Bogota, Col.	6020 Amman, Jordan	6120 BBC, Limassol, Cyprus
4765 HJEF, Cali, Col.	4945 Paradys, So. Afr.	6020 Kiev, Ukrainian S.S.R.	6130 Port Moresby, New Guinea
4770 ELWA, Monrovia, Lib.	4950 Dakar, Mali Fed.	6025 Kuala Lumpur, Malaya	6130 Madrid, Spain •
4770 YVMW, Punto Fiji, Ven.	4950 YVMN, Coro, Ven.	6025 Hilversum, Neth.	6135 HRMF, La Ceiba, Hond.
4775 Libreville, Gabon Rep.	4955 CR6RZ, Luanda, Ang.	6030 Baghdad, Iraq	6135 Papete, Tahiti
4780 YVLA, Valencia, Ven.	4960 YVQA, Cumana, Ven.	6035 Rangoon, Burma	6135 Singapore, Sing.
4790 YVQN, Puerto La Cruz, Ven.	4970 YLKK, Caracas, Ven.	6035 HRTL, Tegucigalpa, Hond.	6140 HCOVS, Azuques, Ecu.
4795 Rangoon, Burma	4975 Yaounde, Cameroun	6037 TIFC, San Jose, C. R.	6140 VLW6, Perth, Aus.
4805 ZY8B, Manaus, Braz.	4990 Lagos, Nigeria	6037 Monte Carlo, Mon.	6145 Algiers, Algeria
4810 YVMG, Maracaibo, Ven.	4990 YVMQ, Barquisimeto, Ven.	6040 HJLB, Ibaguete, Col.	6147 PRL9, Rio de Jan., Braz.
4830 YVOA, San Cristobal, Ven.	5010 HCRGX, Quito, Ecu.	6045 YDF, Djakarta, Indon.	6150 VLR6, Melbourne, Aus.
4835 HJKE, Bogota, Col.	5010 St. George, Grenada, B.W.I.	6045 HOU31, David, Pan.	6150 BBC, London, Eng.
4840 YVGI, Valera, Moz.	5020 HJFW, Manizales, Col.	6050 HCB, Quito, Ecu.	6155 AVDA, Cap Haitien, Haiti
4845 HJGF, Bucaramanga, Col.	5020 NIAMEY, Niger Rep.	6050 BBC, London, Eng.	6155 VOA, Salonika, Greece
4850 YVMS, Barquisimeto, Ven.	5030 YVMK, Caracas, Ven.	6055 HJEX, Cali, Col.	6160 FEN, Tokyo, Japan
4870 Cotonou, Dahomey Rep.	5040 YVMA, Maracaibo, Ven.	6055 JOZZ, Tokyo, Japan	6160 RAI, Caltanissetta, It.
4880 YVKF, Caracas, Ven.	5045 Lome, Togo	6065 XEXG, Leon, Mex.	6165 HER3, Bern, Switz. •
4885 Dakar, Mali Fed.	5050 YJGD, Caracas, Ven.	6065 Hoby, Sweden	6165 XWV6, Mexico City, Mex.
4895 PRFB, Manaus, Braz.	5075 HJCK, Bogota, Col.	6070 Soňa, Bulgaria	6165 Saigon, Vietnam
4898 HJAG, Barranquilla, Col.	5075 HRN, Tegucigalpa, Hond.	6070 BBC, London, Eng.	6170 BBC, Limassol, Cyprus
4900 YVKP, Caracas, Ven.	5940 Moscow, U.S.S.R.	6075 Norden, Ger.	6170 Cayenne, Fr. Guiana
4905 HRQN, Puerto Cortes, Hon.	5952 TUNA, Guatemala, Guat.	6080 ZLT, Wellington, N.Z.	6175 RTF, Paris, France
4910 HCIMI, Quito, Ecu.	5954 TIQ, Puerto Limon, C. R.	6082 OAX4Z, Lima, Peru	6180 BBC, London, England
4910 Conakry, Guinea	5960 HJCF, Bogota, Col.	6085 Munich, Ger.	6185 HBT, Bogota, Col.
4915 Accra, Ghana	5965 YNNW, Granada, Nic.	6090 VL16, Sydney, Aus.	6190 VOA, Munich, Ger.
4920 YLM4, Brisbane, Aus.	5980 TGAR, Guatemala, Guat.	6090 Luxembourg, Lux.	6190 HJA, Vatican City
4920 YVKK, Caracas, Ven.	5981 Georgetown, Br. Guiana	6090 XECMT, C. El Mante, Mex.	6195 HJEZ, Cali, Col.
4930 HCIR, Quito, Ecu.	5982 AVB, Port-au-Prince, Haiti	6095 ZYB7, Sao Paulo, Braz.	6195 HRD2, La Ceiba, Hond.
4935 HJLF, Ibaguete, Col.	5990 Andorra, Andorra	6100 VOA, Munich, Ger.	6195 Pyonyang, N. Korea
4940 Abidjan, Ivory Coast	5990 TGJA, Guatemala, Guat.	6100 Belgrade, Yugo.	6200 H1ZLR, C. Trujillo, D.R.
4940 YVMO, Barquisimeto, Ven.	5995 Fort-de-France, Mart.	6103 Peking, China	6200 AVHVR, Port-au-Prince, Haiti
	6002 AVEC, Cap Haitien, Haiti	6105 XEQM, Merida, Mex.	6215 Pyonyang, N. Korea
	6005 RIAS, Berlin, Ger.	6105 Tunis, Tunisia	6225 Peking, China
	6006 THBG, San Jose, C. R.	6110 BBC, London, Eng.	6305 Andorra, Andorra
	6010 XEOL, Mexico City, Mexico	6115 ZYC7, Rio de Jan., Braz.	6327 GOCF, Havana, Cuba
		6115 Khabarovsk, U.S.S.R.	6345 Ulan Bator, Mong.
		6120 LRXI, Buenos Aires	

Kcs. Call and Location

6373 Lisbon, Port.
 6790 BC, Limassol, Cyprus
 7105 Madrid, Spain
 7110 VOA, Colombo, Ceylon
 7140 BBC, London, England
 7115 Rabat, Morocco
 7115 RFE, Germ.
 7120 BBC, London, England
 7120 BBC, Singapore
 7125 Warsaw, Poland
 7140 Monte Carlo, Monaco
 7145 BFE, Ger.
 7150 Khabarovsk, U.S.S.R.
 7160 RTF, Paris, France
 7160 VOA, Tangier, Mor.
 7165 RFE, Germ.
 7170 Algiers, Alg.
 7180 Baghdad, Iraq
 7185 BBC, London, Eng.
 7200 BBC, London, Eng.
 7200 R. Malaya, Sing.
 7200 Omdurman, Sudan
 7205 VOA, Salonika, Gr.
 7210 BBC, London, Eng.
 7210 Dakar, Mali Fed.
 7210 Khabarovsk, U.S.S.R.
 7220 VLD7, Melbourne, Aus.
 7220 Budapest, Hung.
 7230 BBC, London, Eng.
 7235 Taipei, Taiwan, China
 7235 VOA, Munich, Ger.
 7240 RTF, Paris, France
 7250 BBC, London, Eng.
 7255 Sofia, Bulg.
 7260 Saigon, Vietnam
 7270 Motola, Sweden
 7270 Magadan, U.S.S.R.
 7275 RAI, Rome, It.
 7280 Teheran, Iran
 7280 HVJ, Vat. City
 7285 Ankara, Turk.
 7290 RAI, Rome, It.
 7295 Makassar, Celebes
 7295 RFE, Ger.
 7320 BBC, London, Eng.
 7398 Damascus, U.A.R.
 7505 Peking, China
 7650 YNMS, Leon, Nie.
 7670 Sofia, Bulg.
 7850 Tirana, Alb.
 8002 Beirut, Leb.
 8000 HCJ63, Zamka, Cuba
 9009 Te Aviv, Israel
 9026 COBZ, Havana, Cuba
 9065 Peking, China
 9110 Leopoldville, Congo
 9360 Madrid, Spain
 9360 COBC, Havana, Cuba
 9360 Alma Ata, Kazakh S.S.R.
 9385 Leopoldville, Congo
 9410 BBC, London, Eng.
 9440 CP38, La Paz, Bol.
 9458 Peking, China
 9500 XEWW, Mexico City, Mex.
 9500 Magadan, U.S.S.R.
 9500 Moscow, U.S.S.R.
 9505 PRB22, Sao Paulo, Braz.
 9505 Rabat, Mor.
 9505 HOLA, Colon, Pan.
 9510 Peking, China
 9510 VOA, Courier, Rhodes
 9515 RAI, Caltanissetta, It.
 9515 Ankara, Turkey
 9520 Colombo, Ceylon
 9520 Copenhagen, Den.
 9520 VOA, Salonika, Gr.
 9520 OAX8E, Iquitos, Peru
 9523 Paraguay, S. Afr.
 9525 BBC, Singapore
 9525 JOB9, Tokyo, Japan
 9525 Warsaw, Poland
 9530 COCO, Havana, Cuba
 9530 VOA, Munich, Ger.
 9530 AIR, Delhi, India
 9530 VOA, Courier, Rhodes
 9530 YVMZ, Maracaibo, Ven.
 9535 Lagos, Nigeria
 9535 VOA, Manila, P.I.
 9535 HER4, Bern, Switz.
 9540 ZL2, Wellington, N.Z.
 9540 Warsaw, Poland
 9540 Omdurman, Sudan
 9545 YS43, Curitiba, Braz.
 9545 HED5, Bern, Switz.
 9550 Prague, Czechoslovakia
 9550 AIR, Bombay, India
 9550 OAX1Z, Tumbes, Peru
 9555 CPB, La Paz, Bol.
 9555 BBC, London, Eng.
 9555 XETT, Mexico City, Mex.
 9560 RTF, Paris, France
 9560 Tokyo, Japan
 9563 OAX4R, Lima, Peru
 9565 YK33, Recife, Braz.
 9565 Radio Liberty, Ger.
 9565 Khabarovsk, U.S.S.R.
 9570 Bucharest, Rom.
 9575 YZ27, Rio de Jan., Braz.
 9575 Taipei, Formosa
 9575 RAI, Rome, Italy
 9580 VLA9, Melbourne, Aus.
 9580 BBC, London, Eng.
 9585 ZYR56, Sao Paulo, Braz.
 9585 RTF, Paris, France
 9588 Peking, China
 9590 Djakarta, Indon.

Kcs. Call and Location

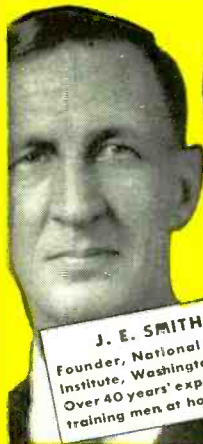
9590 Hilversum, Neth.
 9590 Bucharest, Rom.
 9595 JO23, Tokyo, Japan
 9598 CE960, Santiago, Chile
 9600 BBC, London, Eng.
 9605 Cologne, Ger.
 9607 Athens, Greece
 9610 VLX9, Perth, Aus.
 9610 OLS, Rio de Jan., Braz.
 9610 Oslo, Norway
 9610 OAX8C, Iquitos, Peru
 9615 VOA, Tangier, Morocco
 9620 ZYR88, Sao Paulo, Braz.
 9620 Peking, China
 9620 VOA, Tangier, Mor.
 9620 Saigon, Vietnam
 9625 Brazzaville, Equat. Un.
 9625 BBC, London, Eng.
 9625 OAX8K, Iquitos, Peru
 9625 Moscow, U.S.S.R.
 9630 CR6RL, Luanda, Ang.
 9630 VLG9, Melbourne, Aus.
 9630 RL, Rome, Italy
 9630 Komsomol, U.S.S.R.
 9635 ZYR83, Aparecida, Braz.
 9635 VOA, Munich, Ger.
 9635 Lisbon, Portugal
 9640 BBC, London, Eng.
 9640 Cologne, Germany
 9640 Accra, Ghana
 9640 HLBK, Seoul, Korea
 9640 Moscow, U.S.S.R.
 9645 TIFC, San Jose, C.R.
 9645 HVJ, Vatican City
 9650 BBC, Limassol, Cyprus
 9655 Radio Free Europe, Ger.
 9660 LRX, Buenos Aires, Arg.
 9660 VLB9, Brisbane, Aus.
 9660 Radio Liberty, Ger.
 9660 Teheran, Iran
 9660 Komsomol, U.S.S.R.
 9665 Moscow, U.S.S.R.
 9667 Hargeisa, Somalia
 9667 TGN4, Guatemala, Guat.
 9670 COCQ, Havana, Cuba
 9670 Prague, Czechoslovakia
 9675 BBC, London, Eng.
 9675 RTF, Paris, France
 9675 JOB9, Tokyo, Japan
 9675 Warsaw, Poland
 9680 VLBH, Melbourne, Aus.
 9680 XEQQ, Mexico City, Mex.
 9680 VOA, Tangier, Mor.
 9680 Parady, S. Afr.
 9685 Algiers, Algeria
 9690 LRA, Buenos Aires, Arg.
 9690 BBC, London, Eng.
 9690 BBC, Singapore
 9700 Sofia, Bulgaria
 9700 Rabat, Morocco
 9705 Kabul, Afghan.
 9705 Brussels, Belg.
 9705 AIR, Delhi, India
 9705 Radio Free Europe, Port.
 9710 BBC, London, Eng.
 9710 RAI, Rome, It.
 9715 Hilversum, Neth.
 9715 Radio Free Europe, Ger.
 9720 Parady, S. Afr.
 9725 Te Aviv, Israel
 9725 RFE, Ger.
 9725 BBC, Singapore
 9730 Brazzaville, Equat. Un.
 9730 Leipzig, G.D.R.
 9730 DZH7, Manila, P.I.
 9735 Peking, China
 9735 BBC, London, Eng.
 9735 Cologne, Germany
 9735 AIR, Madras, India
 9740 VOA, Tangier, Mor.
 9742 LRS1, Buenos Aires, Arg.
 9745 Brussels, Belg.
 9745 HCJB, Quito, Ecu.
 9745 Ankara, Turk.
 9750 Moscow, U.S.S.R.
 9750 BBC, London, Eng.
 9750 Radio Free Europe, Port.
 9750 Khabarovsk, U.S.S.R.
 9755 YZW23, Goiania, Braz.
 9755 RTF, Paris, France
 9755 Saigon, Vietnam
 9760 BBC, London, Eng.
 9760 Hanoi, N. Vietnam
 9765 Moscow, U.S.S.R.
 9770 Brazzaville, Equat. Un.
 9770 BBC, London, Eng.
 9775 Moscow, U.S.S.R.
 9785 Cairo, U.A.R.
 9800 Peking, China
 9800 Moscow, U.S.S.R.
 9805 Cairo, U.A.R.
 9825 BBC, London, Eng.
 9835 Budapest, Hung.
 9835 Hanoi, Vietnam
 9850 AIR, Delhi, India
 9860 Peking, China
 9870 Djakarta, Indon.
 9885 Bengazi, Libya
 9915 BBC, London, Eng.
 9973 Peking, China
 10355 Hanoi, Vietnam
 10355 Alma Ata, Kazakh S.S.R.
 11290 Peking, China
 11570 Moscow, U.S.S.R.
 11600 Peking, China
 11630 Moscow, U.S.S.R.

Kcs. Call and Location

1650 Peking, China
 1665 Cairo, U.A.R.
 1675 Peking, China
 1675 Karachi, Pak.
 1680 BBC, London, Eng.
 1685 HVJ, Vat. City
 1680 Moscow, U.S.S.R.
 1700 RTF, Paris, France
 1705 OAI9, Moscow, U.S.S.R.
 1705 Horby, Sweden
 1705 Moscow, U.S.S.R.
 1710 VLB11, Melbourne, Aus. †
 1710 AIR, Delhi, India
 1710 WBOU, New York, N.Y.
 1715 VOA, Munich, Ger.
 1715 Moscow, U.S.S.R.
 1717 Athens, Greece
 1720 Brazilia, Brazil
 1720 BBC, Limassol, Cyprus
 1725 Brazzaville, Equat. Un.
 1725 Prague, Czechoslovakia
 1725 BBC, Singapore
 1730 Hilversum, Neth.
 1735 Rabat, Morocco
 1735 Moscow, U.S.S.R.
 1740 VLB11, Melbourne, Aus.
 1740 CE1174, Santiago, Chile
 1740 Peking, China
 1740 VOA, Tangier, Mor.
 1745 RFE, Germ.
 1750 Moscow, U.S.S.R.
 1750 FEN, Tokyo, Japan
 1755 RFE, Port.
 1755 Hilversum, Neth.
 1755 Komsomol, U.S.S.R.
 1760 VLB11, Melbourne, Aus.
 1760 VOA, Munich, Ger.
 1760 VOA, Tangier, Mor.
 1760 Lourenco Marques, Moz.
 1760 Hanoi, N. Vietnam
 1765 ZYB8, Sao Paulo, Braz.
 1765 Berlin, E. Germany
 1770 Colombo, Ceylon
 1770 BBC, London, Eng.
 1775 ZY228, Rio de Jan., Braz.
 1775 Moscow, U.S.S.R.
 1780 BBC, London, Eng.
 1785 Djakarta, Indon.
 1785 VOA, Tangier, Morocco
 1790 BBC, London, Eng.
 1790 VOA, Manila, P.I.
 1790 Moscow, U.S.S.R.
 1795 Cologne, Germany
 1795 Djakarta, Indon.
 1800 BBC, London, Eng.
 1802 Warsaw, Poland
 1805 RAI, Rome, It.
 1805 VOA, Courier, Rhodes
 1810 VLB11, Melbourne, Aus. †
 1810 RAI, Rome, It.
 1810 Amman, Jordan
 1810 Bucharest, Rom.
 1810 Horby, Sweden
 1815 Madrid, Spain
 1820 Peking, China
 1820 BBC, London, Eng.
 1820 XEBR, Hermosillo, Mex.
 1825 ELWA, Monrovia, Lib.
 1830 WRUL, Boston, U.S.A.
 1830 Moscow, U.S.S.R.
 1835 Algiers, Alg.
 1840 VOA, Tangier, Morocco
 1835 CXA19, Montevideo, Urug.
 1840 Prague, Czechoslovakia
 1840 VOA, Tangier, Mor.
 1840 Lisbon, Port.
 1840 Khabarovsk, U.S.S.R.
 1840 Hanoi, N. Vietnam
 1845 RTF, Paris, France
 1845 Karachi, Pak.
 1850 Sofia, Bulg.
 1850 AIR, Bombay, India
 1850 Oslo, Norway
 1855 Brussels, Belg.
 1855 Radio Free Europe, Ger.
 1855 DZH8, Manila, P.I.
 1860 Peking, China
 1860 BBC, London, Eng.
 1860 Moscow, U.S.S.R.
 1865 PRAB, Recife, Braz.
 1865 VOA, Tangier, Mor.
 1865 HER5, Bern, Switz.
 1865 Tunis, Tun.
 1870 Moscow, U.S.S.R.
 1875 ZYN32, Salvador, Braz.
 1875 VOA, Colombo, Ceylon
 1875 VOA, Tangier, Mor.
 1880 BBC, London, Eng.
 1880 XEHB, Mexico City, Mex.
 1885 Peking, China
 1885 Karachi, Pak.
 1885 Radio Free Europe, Ger.
 1890 Moscow, U.S.S.R.
 1895 Dakar, Mali Fed.
 1895 VOA, Tangier, Mor.
 1895 VOA, Manila, P.I.
 1900 Bucharest, Rumania
 1900 CXA10, Montevideo, Ur.
 1900 Moscow, U.S.S.R.
 1905 RAI, Rome, Italy
 1905 WDS1, New York, U.S.A.
 1910 BBC, London, Eng.
 1910 Budapest, Hungary
 1910 Bangkok, Thai.
 1915 HCJB, Quito Ecu.
 1915 Hilversum, Neth.
 1920 RAI, Paris, France

Kcs. Call and Location

11920 DXF2, Manila, P.I.
 11920 WLW0, Cincinnati, U.S.A.
 11925 ZYR78, Sao Paulo, Braz.
 11925 HLK6, Seoul, Korea †
 11925 Wawsaw, Pol.
 11925 Moscow, U.S.S.R.
 11930 BBC, London, Eng.
 11930 BBC, Singapore
 11935 Radio Liberty, Ger.
 11940 CE1190, Valparaiso, Chile
 11940 JOB11, Tokyo, Japan
 11945 Peking, China
 11945 BBC, London, Eng.
 11945 Cologne, Germany
 11950 Warsaw, Poland
 11950 Jidda, Saudi Arab.
 11950 Moscow, U.S.S.R.
 11955 BBC, London, Eng.
 11955 BBC, Singapore
 11960 CE1196, Santiago, Ch.
 11960 Moscow, U.S.S.R.
 11965 Radio Liberty, Ger.
 11970 Caracas, Ven.
 11972 Brazzaville, Equat. Un.
 11975 Peking, China
 11975 Moscow, U.S.S.R.
 11985 Moscow, U.S.S.R.
 11986 ELWA, Monrovia, Lib.
 11985 Prague, Czechoslovakia
 12000 Moscow, U.S.S.R.
 12010 Hanoi, Vietnam
 12020 AIR, Delhi, India
 12020 Moscow, U.S.S.R.
 12040 BBC, London, Eng.
 12050 Cairo, U.A.R.
 12085 BBC, London, Eng.
 12085 Radio Free Europe, Port.
 15030 Peking, China
 15060 Peking, China
 15070 BBC, London, Eng.
 15085 Grenada, Windward Is., BWI
 15095 Peking, China
 15100 Moscow, USSR
 15105 YZ32, Rio de Jan., Braz.
 15105 AIR, Delhi, India
 15110 BBC, London, Eng.
 15110 Moscow, USSR
 15115 HCJB, Quito, Ecuador
 1515 Peking, China
 15120 Colombo, Ceylon
 15120 RAI, Rome, Italy
 15120 Warsaw, Poland †
 15120 HVJ, Vatican City
 15125 ZYN31, Salvador, Brazil
 1515 Prague, Czechoslovakia
 15125 Seoul, Korea
 15125 VOA, Manila, P.I.
 15125 Lisbon, Portugal
 15130 RTF, Paris, France
 15130 VOA, Manila, P.I.
 15130 KCBR, Delano, Calif.
 15130 WBOU, New York, USA
 15130 Moscow, USSR
 15135 PRB23, Sao Paulo, Braz.
 15135 JOB15, Tokyo, Japan
 15135 Radio Free Europe, Port.
 15140 Peking, China
 15140 BBC, London, Eng.
 15140 AIR, Delhi, India
 15140 Komsomol, USSR
 15145 ZYK33, Recife, Brazil
 15145 Radio Free Europe, Port.
 15148 CE1515, Santiago, Chile
 15150 Djakarta, Indonesia
 15150 Lourenco Marques, Moz.
 15150 Lisbon, Portugal
 15150 Moscow, USSR
 15153 OAX4T, Lima, Peru
 15155 ZYB9, Sao Paulo, Brazil
 15155 Karachi, Pakistan
 15155 VOA, Manila, P.I.
 15155 WBOU, New York, USA
 15155 Moscow, USSR
 15160 VLA15, Melbourne, Aus.
 15160 RTF, Paris, France
 15160 XEWW, Mexico City, Mex.
 15160 Ankara, Turkey
 15160 Moscow, USSR
 15165 ZYN7, Fortaleza, Braz.
 15165 Copenhagen, Denmark
 15165 Damascus, UAR
 15170 Tromso, Norway
 15170 OBX4C, Lima, Peru
 15170 Radio Free Europe, Port.
 15175 Peking, China
 15185 Oslo, Norway
 15180 BBC, London, Eng.
 15180 AIR, Delhi, India
 15180 Moscow, USSR
 15185 VOA, Manila, P.I.
 15185 Radio Free Europe, Port.
 15185 WDS1, New York, USA
 15195 Brazzaville, Congo Rep.
 15190 Helsinki, Finland †
 15190 Komsomol, USSR
 15190 Moscow, USSR
 15195 Prague, Czechoslovakia
 15195 Radio Free Europe, Ger.
 15195 Ankara, Turkey
 15200 Parady, S. Africa
 15200 WDS1, New York, USA



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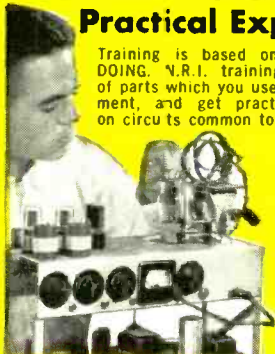


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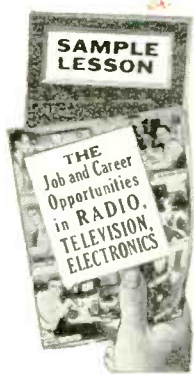
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