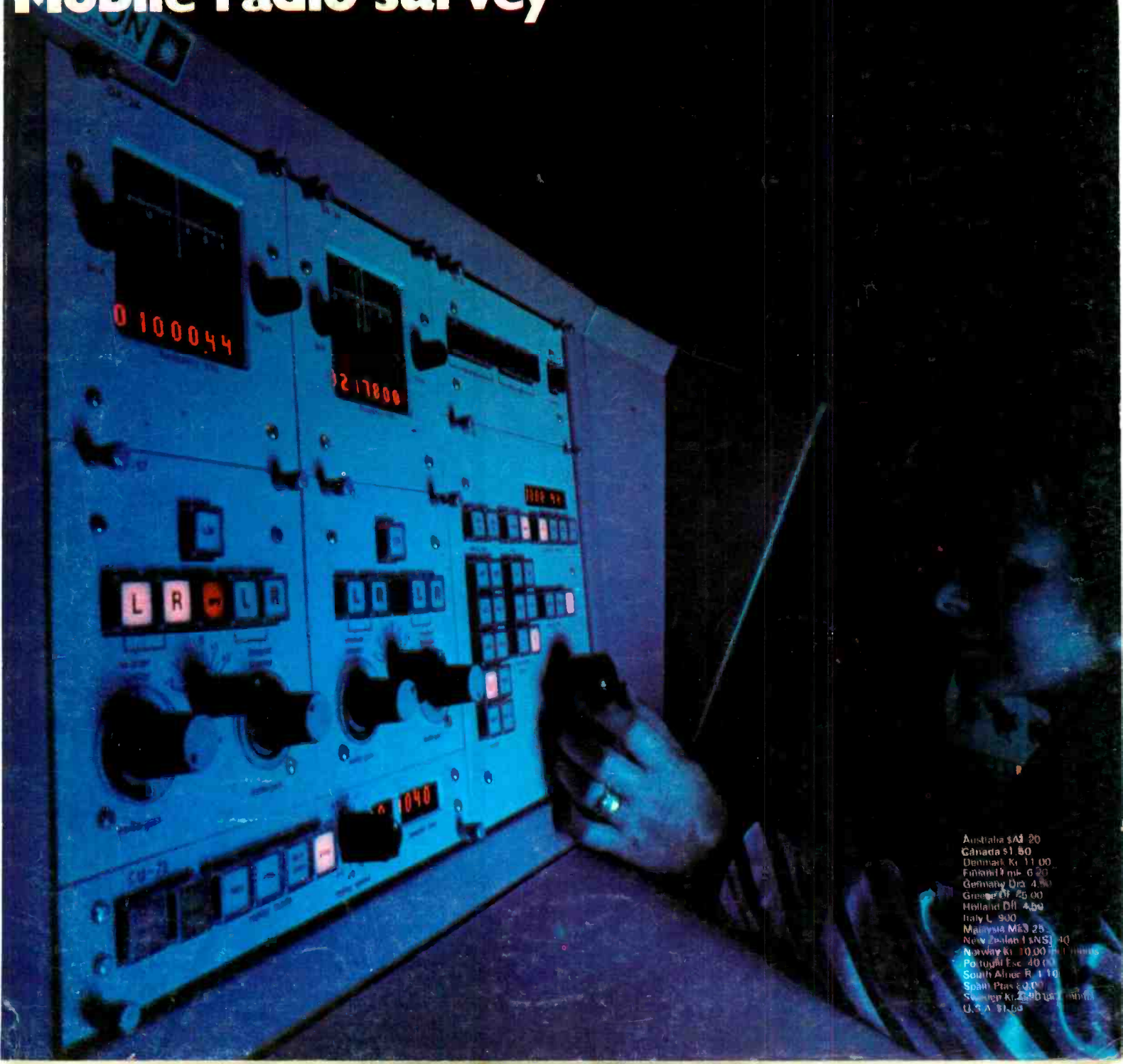


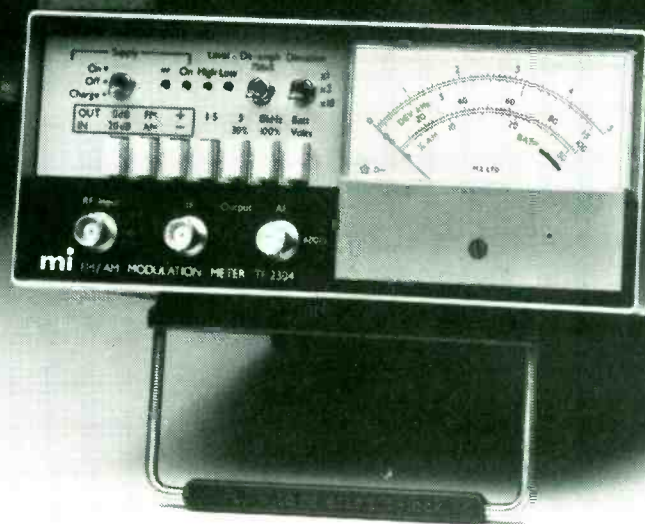
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NOVEMBER 1976 35p

Advanced preamplifier Mobile radio survey



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TF 2303 Compact and lightweight, this manual model is still preferred by many engineers for mobile radio testing on the bench or in the field. FM deviation and AM depth at carrier frequencies up to 520 MHz.

TF 2304 A low priced automatic with high performance. Automatic tuning and level setting with exceptionally good r.f. screening. Eight peak deviation ranges from 1.5 to 150 kHz and a.m. ranges at carrier frequencies from 18 to 1000 MHz.

TF 2300B A high-grade instrument with exceptional low noise performance, TF 2300B is often used as a standard for lower grade types. As a multipurpose instrument it can measure peak deviations up to 500 kHz (at modulating

frequencies up to 200 kHz) for carrier frequencies up to 1200 MHz. Applications include tests on mono and stereo broadcast transmitters, mobile radio type approval and f.m./a.m. production testing. Crystal oscillator **TK 2302** plugs into TF 2300B for extra low noise testing.

TF 2300BM series: A series of specials (e.g. for measuring a.m. on f.m.).

TF 2301A Fully programmable, for use in automatic test systems. Special peak detector designed to follow rapidly increasing or decreasing modulation depths. Deviation ranges 1.5 to 500 kHz and a.m. at carrier frequencies 4 to 1000 MHz.

Accessories A range of accessories specially designed to make your job easier includes a signal sniffer, power attenuators, termination unit, r.f. fuse unit and carrying cases.

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mi: THE MODULATION EXPERTS

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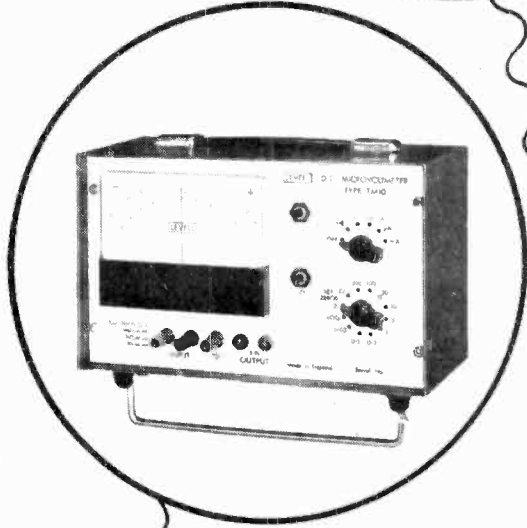
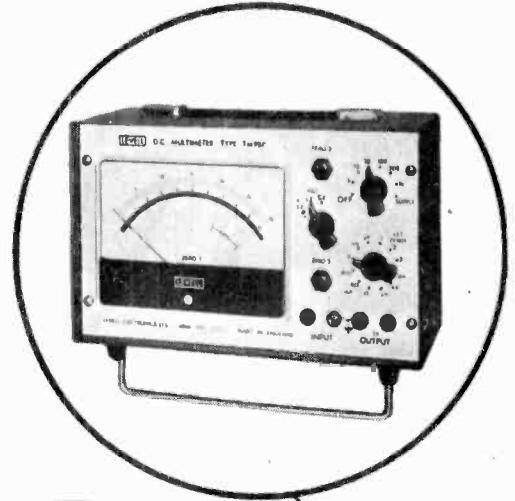
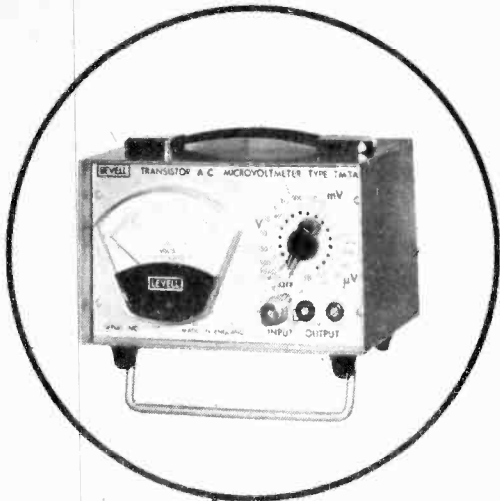
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WW-001 FOR FURTHER DETAILS

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A.C. MICROVOLTMETERS
VOLTAGE & dB RANGES: 15µV, 50µV, 150µV ... 500V.
 Acc. ± 1% ± 1% f.s.d. = 1µV at 1kHz — 100, — 90 ... +50dB
 Scale — 20dB / + 6dB rel. to 1mW / 600Ω.
RESPONSE: ± 3dB from 1 Hz to 3MHz, ± 0.3dB from 4Hz to 1MHz above 500µV. Type TM3B can be set to a restricted B.W. of 10Hz to 10kHz or 100 kHz.
INPUT IMPEDANCE: Above 50mV > 4 3MΩ < 20pf. On 50µV to 50mV > 5MΩ < 150pf.
AMPLIFIER OUTPUT: 150mV at f.s.d.
 type **TM3A** **£82** type **TM3B** **£92**

D.C. MULTIMETERS
VOLTAGE RANGES: 3µV, 10µV, 30µV, ... 1kV
 Acc. ± 1% ± 1% f.s.d. ± 0.1µV. LZ & CZ scales.
CURRENT RANGES: 3pA, 10pA, 30pA ... 1mA (1A for TM9BP)
 Acc. ± 2% ± 1% f.s.d. ± 0.3pA. LZ & CZ scales.
RESISTANCE RANGES: 3Ω, 10Ω, 30Ω ... 1 GΩ linear Acc. ± 1% ± 1% f.s.d. up to 100MΩ
RECORDER OUTPUT: 1V at f.s.d. into > 1kΩ on LZ ranges.
 type **TM9A** **£120** type **TM9BP** **£130**

BROADBAND VOLTMETERS
H.F. VOLTAGE & dB RANGES: 1mV, 3mV, 10mV ... 3V
 Acc. = 4% ± 1% f.s.d. at 30MHz. — 50dB. — 40dB. — 30dB to + 20dB Scale — 10dB / + 3dB rel. to 1mW / 50 Ω ± 0.7dB from 1MHz to 50MHz, ± 3dB from 300kHz to 400MHz.
L.F. RANGES: As TM3 except for the omission of 15µV and 150µV
AMPLIFIER OUTPUT: Square wave at 20Hz on H.F. with amplitude proportional to square of input. As TM3 on L.F.
 type **TM6A** **£130** type **TM6B** **£140**

D.C. MICROVOLTMETERS
VOLTAGE RANGES: 30µV, 100µV, 300µV ... 300V
 Acc. ± 1%, ± 2% f.s.d. ± 1µV. CZ scale.
CURRENT RANGES: 30pA, 100pA, 300pA ... 300mA
 Acc. ± 2%, ± 2% f.s.d. ± 2pA. CZ scale.
LOGARITHMIC RANGE:
 ± 5µV at ± 10% f.s.d., ± 5mV at ± 50% f.s.d., ± 500mV at f.s.d.
RECORDER OUTPUT: ± 1V at f.s.d. into > 1kΩ.
 type **TM10** **£75**

These highly accurate instruments incorporate many useful features, including long battery life. All A type models have 83mm scale meters, and case sizes 185x110x130mm. B types have 127mm mirror scale meters and case sizes 260x125x180mm.

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Prices include batteries and U.K. DELIVERY. VAT extra. Optional extras are leather cases and mains power units. send for data covering our range of portable instruments.



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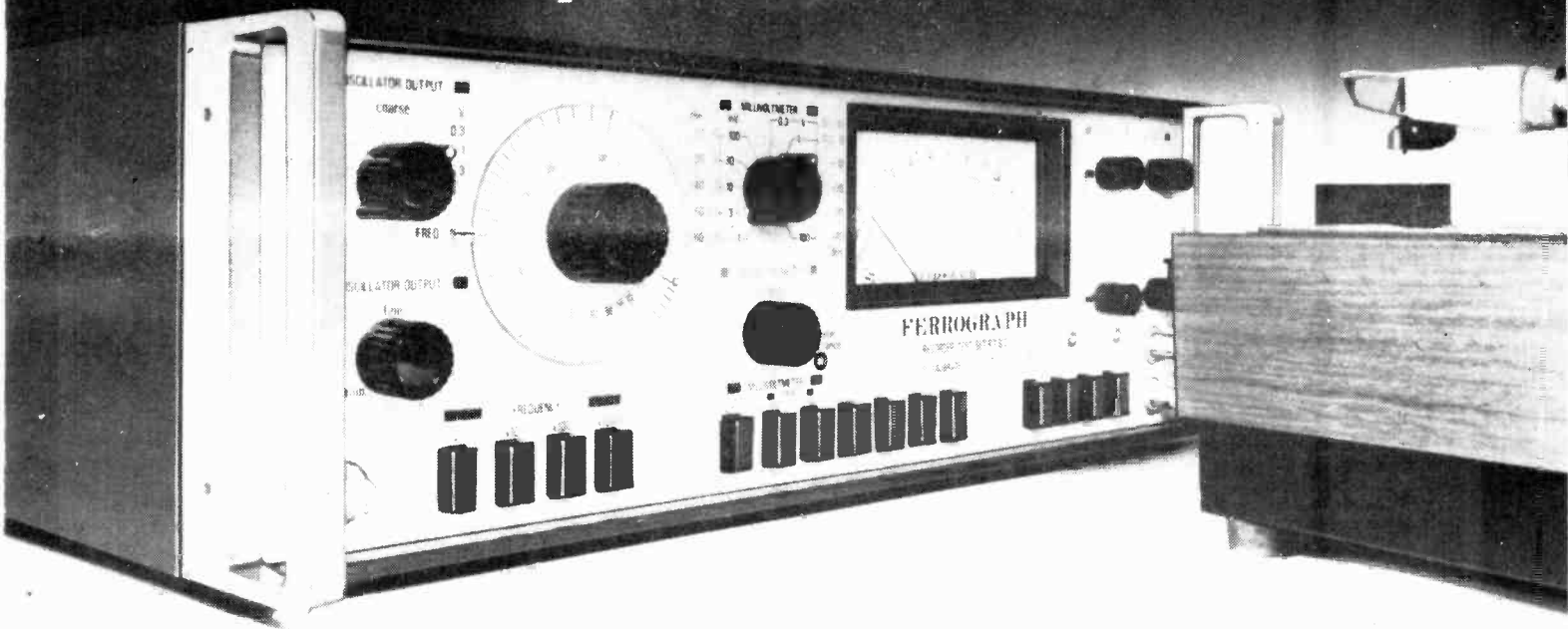
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How every hi-fi dealer can increase his sales and improve his service



The Ferroglyph RTS 2 is a complete, single-unit audio analyzer. Used by leading manufacturers and dealers throughout the world, it is the only single equipment available that can run exhaustive checks on hi-fi—including amplifiers, tape recorders, equalisers and mixers—making it an invaluable aid to sales and service.

Increase your sales!

By using the RTS 2 in your hi-fi store, your salesman can quickly prove to customers that the hi-fi system he is demonstrating is as good as it sounds. In a matter of seconds, up to ten different tests can be carried out, using just one pair of leads. (The push-button operation is so simple, even

unskilled staff can make accurate measurements.)

Result? The customer is reassured, confident he is getting value for money. So you sell more, more easily.

Improve your service!

But the RTS 2 is much more than a cost-effective sales aid. Used in your service department, it quickly identifies faults, making your after-sales back-up more efficient. And more profitable. You don't need a variety of incompatible test gear—so there are fewer connections, no hum-loops, no time-consuming frustrations. All of which means you save money.

The RTS 2 is an unbeatable demonstrator. It's so simple! And as test equipment, there's nothing faster.



Photograph by courtesy of Sowards & Rowling

Ferroglyph RTS 2

the complete, single-unit audio test set.



Wilmot Breeden Electronics
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- Send me more information about the RTS 2 audio test set
 I would like a demonstration. Phone me to arrange an appointment.

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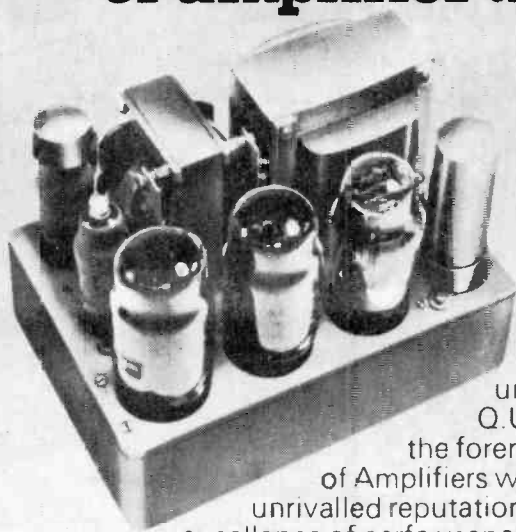
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The Acoustical Manufacturing Co. Ltd. have been designing and producing amplifiers since 1936 but it was not until 1951 that the Q.U.A.D. 1 was introduced, the forerunner of the Quad series of Amplifiers which have earned an unrivalled reputation for originality of design, excellence of performance and reliability in the ensuing twenty-five years.

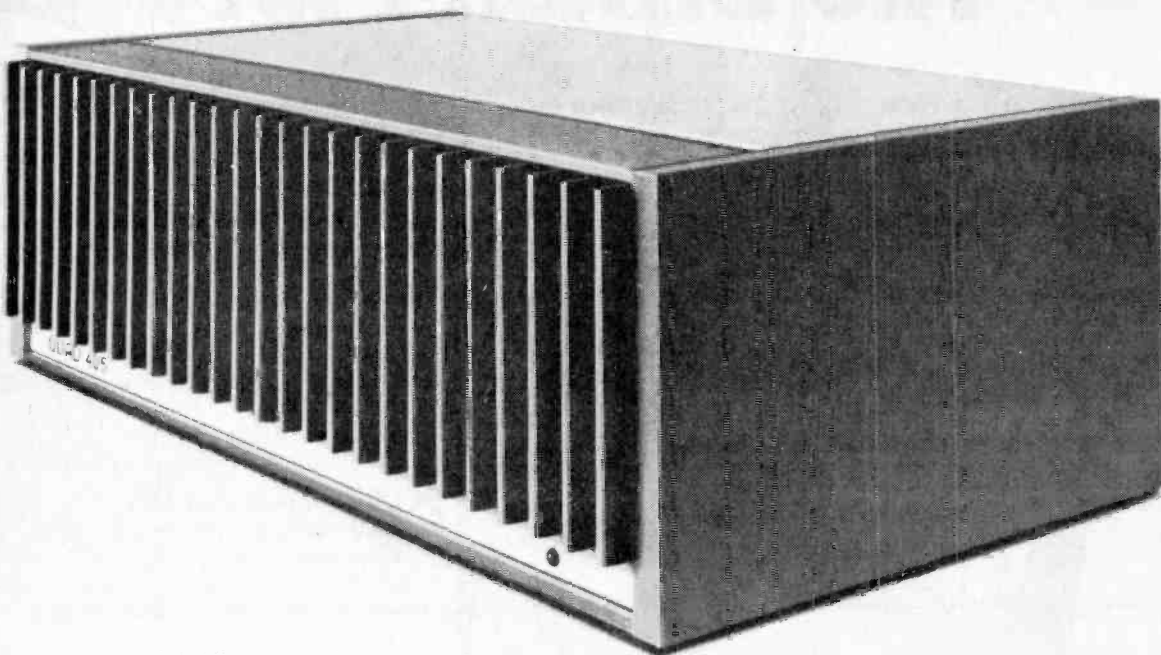
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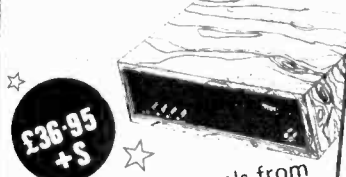
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TV sound only TUNER



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Picks up UHF signals from the transmitter and relays this through your hi-fi equipment.

Touch Activated Programmer MODULE

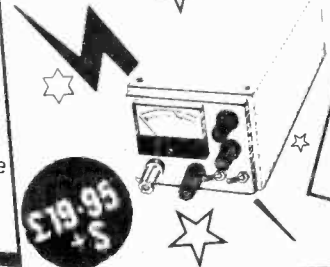


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0-30V and 0-1A with variable current limit.



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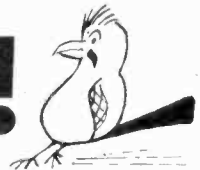
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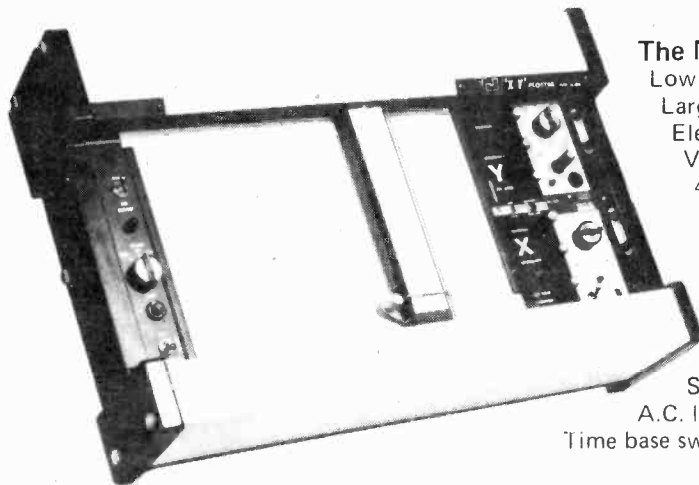
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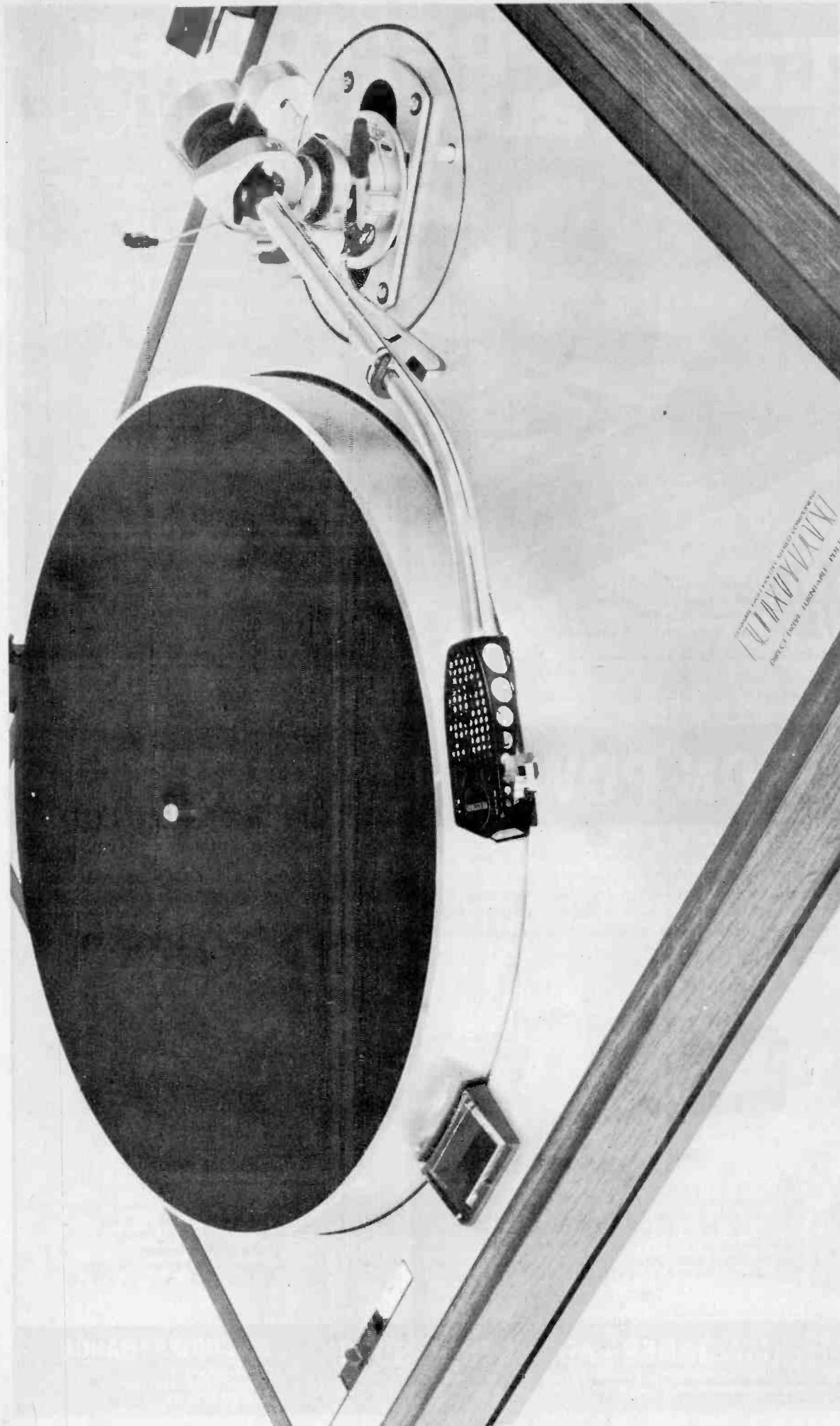
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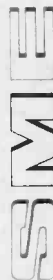
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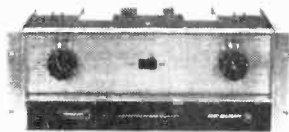
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AMCRON POWER AMPLIFIERS

The AMCRON range of DC-coupled power amplifiers are used by Government, and University, Research Departments as well as by Industry for a variety of applications ranging from Shaker, and Vibrator driving, to driving both AC and DC Motors, providing variable frequency power supply, or high voltage material testing. All models are DC-coupled throughout, with Intermodulation, and Harmonic Distortion below 0.05%, damping factor of at least 400 from DC to 1 kHz, and the ability to operate into load impedances from 1 ohm to infinity even into highly reactive loads.



M600



DC 300A



D150A

RMS power out	750 watts into 8 ohms 1,350 watts into 4 ohms
Power bandwidth	DC to 20 kHz + 1 db -- 0 db
Phase response	+ 0' -- 15' DC -- 20 kHz
Slew rate	16 V / usecond
Hum & noise	120 db below 600 Watts
Dimensions	19" std rack, 8 3/4" H, 16 1/2" Deep

500 watts rms into 2.5 ohms (1 chan)
DC-20kHz + 1 db -- 0 db
+ 0, -- 15' DC to 20kHz
8 volts per microsecond
At least 110db below 150 watts
19" Rackmount, 7" High, 9 3/4" Deep

200 watts into 2.5 ohms (1 chan)
DC-20 kHz + 1 db -- 0 db
+ 0', -- 15' DC to 20 kHz
6 volts per microsecond
At least 115 db below 90 watts
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Dear Wireless World Reader

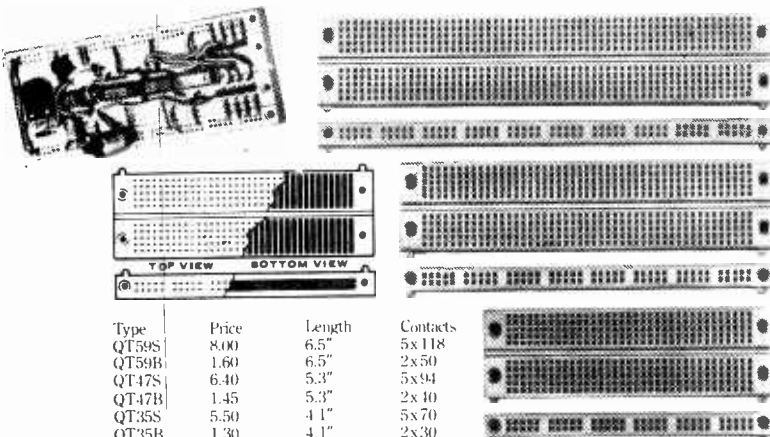
It is with great pleasure that I offer, for the first time in Great Britain, this selection of high quality test and circuit-building equipment. Continental Specialities has earned a high reputation in USA, and our goods are bought again and again, not only all over the States, but also in Canada, Australia and many other countries.

The reason for our success is simple. All our equipment is carefully designed to make life easy for the user, and then manufactured to a very high standard, to satisfy both the professional engineer and the enthusiastic hobbyist.

And at today's prices, we think the value is unbeatable.

QT Sockets

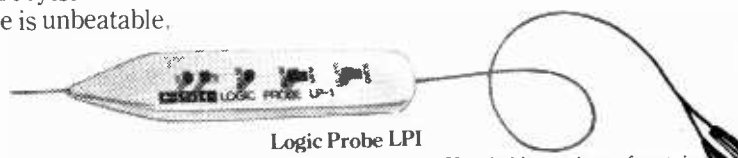
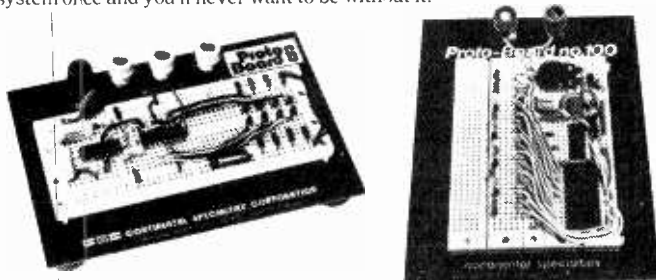
Circuit-building and testing at its easiest! Forget the soldering-iron; with these sockets and bus-strips you won't need it. Each socket is made up of rows of 5 contacts, connected transversely at the back, and each bus-strip has two rows of contacts, connected lengthways. You can plug in and out almost any component you can think of; DIL ICs (6-40 leads), TO5s, discretes with any lead diameter from .015 to .032 inch. Component interconnections are made with standard solid insulated wire. The contacts are solid Silver-Nickel alloy, with contact resistance only 0.4 milliohms, spaced at standard 0.1 inch pitch. The bodies are made of high-temperature plastic (so if you do decide to solder the heat won't hurt it); the reverse side, with the connecting strips, is covered by a peelable, tough vinyl insulation, and each socket unit has a snap-lock mechanism for easy mating to its neighbour.



Type	Price	Length	Contacts
QT59S	8.00	6.5"	5x118
QT59B	1.60	6.5"	2x50
QT47S	6.40	5.3"	5x94
QT47B	1.45	5.3"	2x40
QT35S	5.50	4.1"	5x70
QT35B	1.30	4.1"	2x30

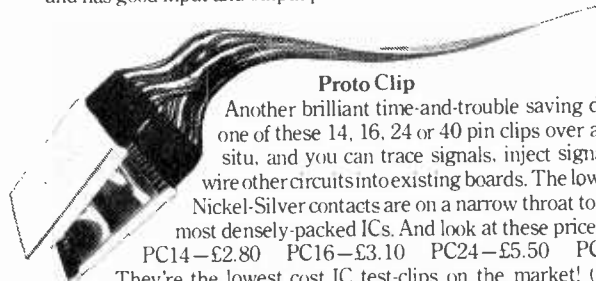
Proto Boards

Another great idea for easy circuit building, based on the QT socket and bus strip concept. These Proto Boards come as complete kits, which you assemble in a few minutes, ready for immediate use. PB6, £10.45, includes one QT47S socket and two QT47B bus strips, four 5-way building posts, a base-plate with rubber feet and all the necessary assembly hardware. PB100, £13.20, gives you two QT35S sockets, one QT35 Strip, two binding posts, base plate and assembly hardware. Try the QT and Proto Board system once and you'll never want to be without it.



Logic Probe LPI

A really low-cost, circuit-powered logic probe. Hardly bigger than a fountain pen, but amazingly versatile. It shows logic-state high, low or inoperative for any node of a TTL, HTL or CMOS device. (100KΩ input impedance). It detects and displays pulses as narrow as 50 nanosec. and level transitions (both +ve and -ve) at frequencies up to 10MHz, or even higher. (The pulse LED blinks continually 3 times a second for all input frequencies over 3Hz). And you can switch to memory, to store and display (until reset) single pulses, transitions or transients. LP1 works on any power supply, 5-15V, and has good input and output protection. Price £28.60.



Proto Clip

Another brilliant time-and-trouble saving device. Slip one of these 14, 16, 24 or 40 pin clips over a DIL IC in situ, and you can trace signals, inject signals or even wire other circuits into existing boards. The low-resistance Nickel-Silver contacts are on a narrow throat to fit over the most densely-packed ICs. And look at these prices:

PC14-£2.80 PC16-£3.10 PC24-£5.50 PC40-£8.90

They're the lowest cost IC test-clips on the market! (UK Patent Pending No. 33948/75).

How to Order

It's easy. Give us your name and full postal address, in block capitals. Clearly state the type-number, and quantity ordered for each item. Send ordinary UK bank cheque or international money order (from any post office) made out in UK currency. Goods will be despatched air mail, direct from factory; allow 2-3 weeks from posting your order. (All prices shown are in UK Pounds Sterling).

Type	£Price	QTY	TOTAL	Type	£Price	QTY	TOTAL
QT59S	8.00		£	PB-6	10.45		£
QT59B	1.60		£	PB 100	13.20		£
QT47S	6.40		£	PC 14	2.80		£
QT47B	1.45		£	PC 16	3.10		£
QT35S	5.50		£	PC 24	5.50		£
QT35B	1.30		£	PC-40	8.90		£
				LP 1	28.60		£

Name _____
 Address _____

Dealer enquiries invited. Note. Any UK taxes or duties chargeable are solely the responsibility of the buyer.

That's all for this month. But we'll send a catalogue full of good things to everyone writing to us, or you can use the enquiry service. Best wishes, and happy circuit-building!

Yours sincerely,



Continental Specialities Corporation, 44 Kendal St., PO Box 1942, New Haven, Connecticut, 06509 USA.

WW-029 FOR FURTHER DETAILS

ambit international

Coils, ICs for RF&AF, Tuners, Modules for AM FM & TV.

complete tuner kits

Larsholt Signalmaster Mark 8...the most stylish FM tuner kit that is available today. Suitable for even the relatively inexperienced in electronics construction, with clear and concise point-to-point details. Performance matches the excellent looks. £86.95

International Mark 2...A flexible system, with cabinet, chassis and panel designed to accommodate a variety of tuner electronics. The standard system is built around the Larsholt 7253 tuner set, includes two meters 6 preset stations, manual tune, balanced LED tuning, PSU etc. £65.00

The above tuners are supplied with prealigned RF and IF stages.

AM/FM...a new low cost MW/LW and FM stereo tuner, with muting, mechanical drive, teak effect cabinet. £41.95

TV sound...the 7700 TV sound module in a chassis and cabinet that matches the AM/FM tuner. £36.95

Please remember to include an extra £3 carriage on complete tuner kits.

Radio ICs	Misc. regs etc.	Transistors
CA3089E FM IF	1.94† 7805UC 5v 1A	1.55* ZTX107 0.14
CA3090AQ mpx	3.75† 78M12 12v ½A	1.20* ZTX108 0.14
MC1310P mpx	2.20† TDA1412	0.95* ZTX109 0.14
SN76660N FM IF	0.75 7815UC 15v 1A	1.55* ZTX212 0.16
TBA120AS FM IF	1.00 78M20 20v ½A	1.20* ZTX213 0.16
MC1350 AM/FM IF	0.70 78M24 24v ½A	1.20* ZTX214 0.16
HA1197 AM system	1.40 uA723 5-35v	0.80* ZTX413 0.18
TBA651 AM system	1.81 NE550A do.	0.80* ZTX551 0.18
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	LM3900 quad amp	0.68* BD165 0.50
	MC3401 do.	0.68* BD166 0.54
	8038 wave gen.	3.10* BD535 0.52
	NE555 timer	0.70* BD536 0.53
	NE560B PLL	2.50 BD609 0.70
	NE561B PLL	3.50 BD610 1.20
	NE562B PLL	2.50 40673 0.50
	NE565A PLL	2.50 MEM680 0.75
	NE566V VCO	2.55* BF256L 0.38
	NE567V tone trigger	2.50*

Tunerheads for VHF FM and UHF TV (All varicap types)

EF5800	6 circuit high quality 88-108MHz tunerhead	14.00
EF5600	5 circuit high quality 88-108MHz tunerhead	12.50
EC3302	3 circuit (same spec to LP1186) VHF tunerhead	5.50
5700	UHF TV tunerhead 38MHz IF with 4 way preset	8.00

Modules for IF, decoders etc. (Also available built & tested)

7020 kit	10.7MHz FM IF with mute, AFC, AGC, meter ops	5.25
7030 kit	10.7MHz linear phase low distortion FM IF	7.67
92310 kit	Stereo decoder with full pilot tone filtering (PLL)	5.35
93090 kit	Stereo decoder, low noise and distortion	6.40
7252	FM tuner set, built - 1uV in, Audio out with mute and all HiFi tuner features. Varicap tuned.(mono)	24.00
7253	FM tuner set, built 1.2uV in, stereo out, with mute and all Hi Fi tuner features. Varicap tuned.	24.00
71197 kit	Varicap tuned MW radio module. The best AM tuner, with 75dB AGC, 0.3% THD.	9.65
8001 kit	55kHz low pass, birdy, filter for stereo radio	1.75
2020 kit	TDA2020 stereo amplifier, with special heatsinks	9.35

Famous TOKO COILS, Mechanical filters, ceramic filters, chokes etc.

455/470kHz IF coils	0.30	M41T 4kHz/455kHz Mech filt.	1.65
(1st, 2nd & 3rd)IFTs	0.70	M71T 7kHz/455kHz Mech filter	1.65
10.7MHz IFTs	0.32	C455B 8kHz/455kHz ceramic filt	0.55
Variable signal chokes:		C455C 6kHz/455kHz ceramic filt	0.55
2mH, 23mH, 36mH, 7mH		C050D 6kHz/470kHz ceramic filt	0.60
11.75mH	0.33	CFS107 10.7MHz cer. FM filter	0.50
Fixed chokes: (uH)		SFE6.0 6MHz TV sound IF filter	0.80
1.0, 4.7, 10, 33, 47, 100,		3132A linear phase FM IF filter	2.25
22, 33, 470, 1000	0.16	SFD470B 470kHz ceramic filter	0.75

PLEASE REMEMBER TO INCLUDE VAT - thank you !!

If you have read this far, you probably appreciate that AMBIT tends to specialize in the areas of wireless and TV that most component sources do not include. Our catalogue and price list continue this theme with coils, linear ICs etc. Catalogue 40p, price list free with SAE. Post is 22p per order - unless otherwise stated.

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Cat. No.	Impedance Input	(O-HMS) Output	Turns Ratio Sec/Pr	Operating Level dBm at 50Hz	Frequency Response
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MU 7503	0.200 600	100k	10/23 1		
MU 7514	600	600/2.4k	1.1 1		
MU 7518	10k CT	10k	1.1 CT		
MU 7521	3.75/15	600 CT	6.32/12.64 1	16.5	± 0.5 dB 30Hz - 20kHz (± 1dB at 20kHz)
MU 7522	3.75/15	100k*	82/164 1		
MU 7524	150/600	600 CT	1/2 1		
MU 7525	600 CT	300/1.2k	1.1 1.41 CT		
MU 7530	10k CT	10k	1.1 CT	20	± 0.5dB 10Hz - 100kHz (± 1dB at 20kHz)
MU 7534	50/200	100k*	22.4/44.8 1		
MU 7566	600 CT	10k/2.5k	4.08/2.04 1		
MU 7567	600/150	50k	9.13/18.26 1		
MU 7582	200/50	600 CT	1.13/3.46 1	4.75	± 1dB 30Hz - 22kHz
VM 7461	15/3.75	600	6.35/12.7 1		
VM 7464	600/150	600	1/2 1		
VM 7466	600	10k/2.5k	4.14/2.07 1		
VM 7468	50/12.5	50k	32/64 1		

We would emphasise that the above is a representative selection only. Send for Brochure GT5 for complete listings. All units described are normally AVAILABLE FROM STOCK.

SPECIAL DESIGN SERVICE
If your requirements cannot be met by our standard range, then we will gladly design for your production needs.



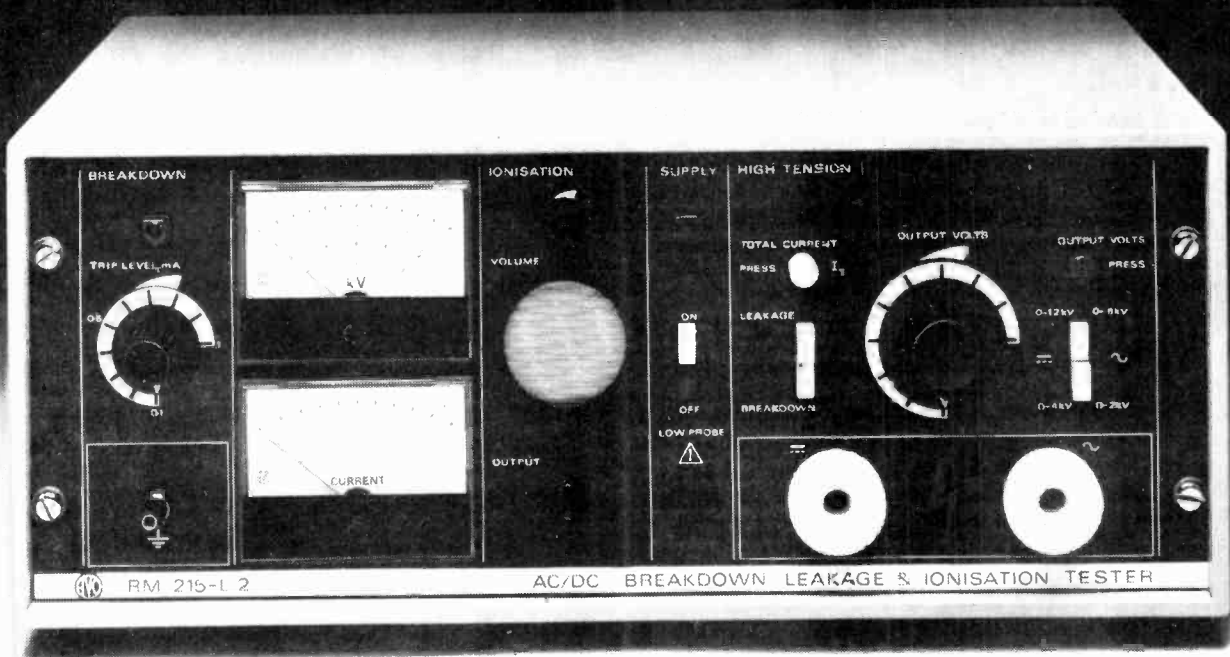
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Approved manufacturers of
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WW 11/76

WW-060 FOR FURTHER DETAILS



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The AVO Breakdown and Ionisation Tester RM215-L/2 is specifically designed to help solve all manner of quality control problems.

It measures resistive leakage current under both AC & DC voltage testing conditions as well as total AC leakage current. Test voltages up to 12 kV DC and 6 kV AC are continuously variable and breakdown current level is adjustable up to 1 mA. A built-in loudspeaker gives audible detection of ionisation and there are connections for earphone or an oscilloscope.

The circuit features low internal resistance yet at the same time limits the maximum output current, even at short circuit.

With the RM215-L/2 you can carry out general flash testing, measurement of breakdown voltage – even after breakdown – and the detection (and counting) of spurious flashovers.

Equally suited to both destructive and non-destructive testing, the RM215-L/2 is a piece of test equipment you cannot afford to be without. If you have some problems that need to be 'ioned' out, get in touch for full details.

APPLICATIONS

- Flash testing of electrical components.
- Measurement of breakdown voltage on electrical components and materials.
- Measurement of insulation resistance at high voltage.
- Measurement of d.c. leakage current.
- Measurement of a.c. leakage current and total current.
- Non-destructive insulation testing of materials and components.
- Detection of ionisation in electrical assemblies.

Designed to meet B.S., V.D.E. and I.E.C. Safety Requirements.



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Problem.

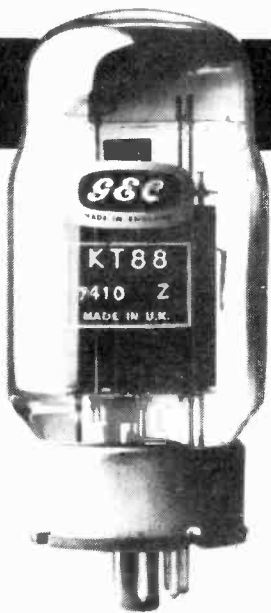
Where to obtain devices for push-pull audio power amplifiers which give good linearity and don't blow up on the slightest overload.

LAP81

Solution.

M-OV audio beam tetrodes. A pair of KT66s will give up to 50W and a pair of KT88s will give up to 100W.

And M-OV audio triodes, too: a pair of DA42s gives up to 200W and a pair of DA 100s gives up to 300W.



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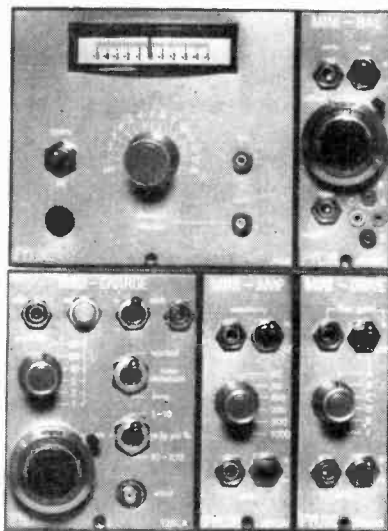
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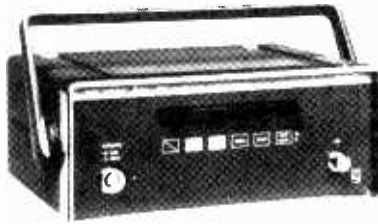
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PM5501 PAL TV Pattern Generator

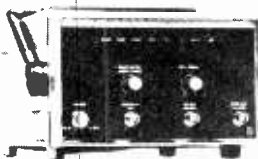
Extremely light, portable instrument for service in customers' home. 5 different test patterns for colour and black/white installation and service. RF output signal switchable: VHF Band III and UHF Band IV. 1 kHz tone for sound performance checks.

PM5509 PAL TV Pattern Generator

The ultimate in pattern generators. Full IF coverage; band I, III, IV and V. Electronic tuning with 5 preset channels. 10 test patterns (colour and black white). Adjustable chroma, burst and HF-amplitude. Special sync, video and VCR outputs.



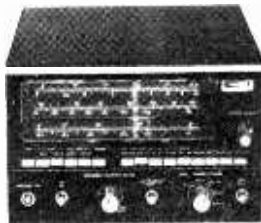
PM6456 FM Stereo Generator



Complete stereo signal. L & R signal. Internal L.F. modulation: 1 & 5 kHz. External stereo modulation possibility. X-tal controlled pilot. Adjustable multiplex signal.

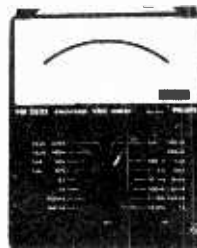
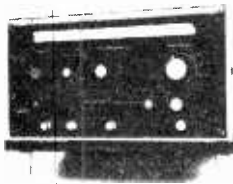
PM5324 HF Generator

Frequency range 100 kHz - 110 MHz. X-tal calibration. Special band spread ranges. High frequency stability. Electronically stabilised output max. 50 mVrms in 75 Ω. Facilities for internal and external AM and FM modulation.



PM5334 TV Sweep Generator

8 frequency ranges, 3 MHz - 860 MHz. Sweep width continuously adjustable over selected range. Sweep frequency adjustable, 8 - 50 Hz. One variable and 3 fixed markers. Signal frequency is accurate and thermally stable. Stabilised output into 75 Ω load.

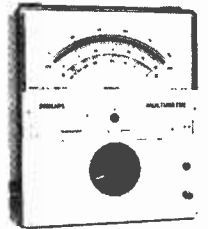


PM2503 Electronic Multimeter

AC DC voltage ranges 100 mV - 1 kV. AC DC current ranges 1 μA - 1 A. Resistance ranges 100 Ω - 10 M Ω. 2-3% accuracy on all ranges. Resistance measurements: unique linear scale. No zero adjustment necessary. Automatic polarity indicator.

PM2412 General Purpose Multimeter

DC voltage 300 mV - 1000 V. AC voltage 3 V - 600 V. DC current 10 mA - 6 A. AC current 100 mA - 6 A. (all values f.s.d.) Resistance 1 Ω - 10 M Ω. Tautband 40,000 Ω/V. suspension-type meter.



PM2513 Low Cost Digital Multimeter

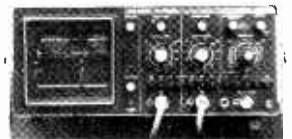
DC voltage ranges 0.2 - 1000 V. AC voltage ranges 0.2 - 600 V. AC DC current ranges 0.2 mA - 2 A. Resistance ranges 200 Ω - 2 M Ω. Full circuit protection. Provision for temperature measurements, -60 to 200 C.



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Comprehensive triggering facilities (Auto, AC, DC and TV) Large 8 x 10 div. screen Sensitivity 2mV/div Ergonomic styling and lightweight construction Single trace: PM3225. Dual trace: PM3226.

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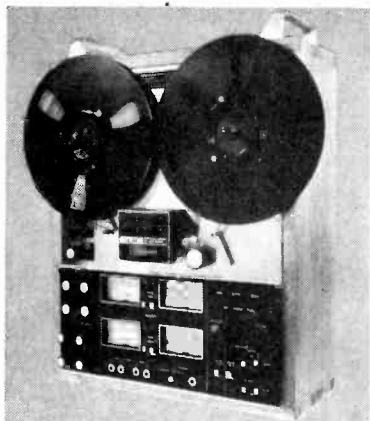
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TEAC

TEAC A3340(S) 4-CHANNEL RECORDER

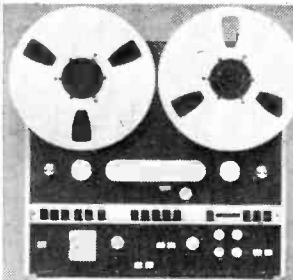


Industrial version upgraded to studio requirements, with increased signal to noise performance and improved reliability. Four totally independent channels each with sel sync, input mixing, switchable VU's and all the facilities for easy multitracking. This industrial model is in more studios than any other version.

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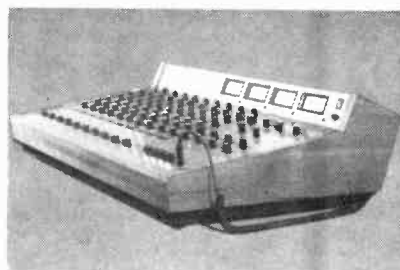
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EIGHT OUTPUT £1260

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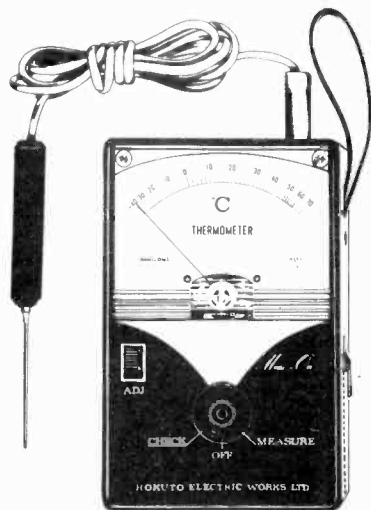
Industrial Tape Applications



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THE MODERN WAY TO MEASURE TEMPERATURE

A Thermometer designed to operate as an Electronic Test Meter. Will measure temperature of Air, Metals, Liquids, Machinery, etc., etc. Just plug-in the Probe, and read the temperature on the large open scale meter. Supplied with carrying case, Probe and internal 1 1/2 volt standard size battery.

Model "Mini-Z 1" measures from -40° C to + 70° C

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A continuously variable-frequency laboratory oscillator with a range 10Hz-1.00kHz, having virtually zero distortion over the audio frequency band with a fast settling time.

LDO3.B Low Distortion Oscillator, balanced output.

A LDO3 but fitted with an output amplifier and screened balanced transformer providing a 600 ohm floating / balanced output, and 150 ohms unbalanced output.

DMS3 Distortion Measuring Set (Illustrated)

Measures total harmonic distortion down to 0.001% speedily and accurately. Direct reading from calibrated meter.

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An accurate voltmeter with 16 ranges, 10µV-300V f.s.d. Average responding.

HSV2 High Sensitivity Voltmeter.

As HSV1 but true r.m.s. reading.

ANM1 Audio Noisemeter

An accurate voltmeter and noisemeter with 16 ranges, 10µV-300V f.s.d. Fitted weighting characteristics: Wide band, DIN Audio Band, IEC/DIN Curve 'A', and CCIR. Average responding.

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Full descriptive leaflets available from:

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WW1

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These modules are fully assembled, tested and guaranteed units, as featured in our tuner. Designed by experts in integrated circuit technology and applications, they represent the finest available modules, ideal for incorporation into top quality home built systems.

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M2 STEREO DECODER including L.E.D. indicator	£6.36
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All items (except M5) are available in kit form, or as individual I.C.s, P.C.B.s, etc.

Full metalwork and teak cabinet is also available to complete the finest tuner on the market today.

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If you are having trouble with our **original** design as in W.W. April/May '74, send S.A.E. for **FREE** corrections and diagnostic sheets, while stocks last.

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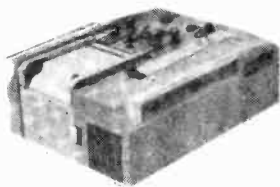


Fully illustrated leaflets describing the above modules are available for the asking.

A **booklet** is available for 50p (post free U.K.) Fully describing the completely **updated** tuner. Prices subject to 12.5% VAT and revision on 1st Nov.

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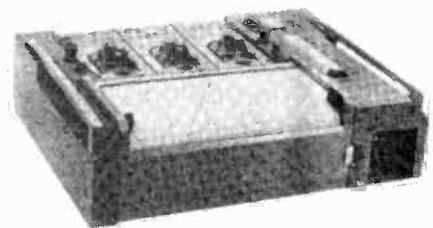
Made in USSR



Type H3020-1
Single pen

Specification

Basic error	2.5%
Sensitivity	8mA F.S.D.
Response	0.2 sec.
Width of each channel	80mm
Chart speeds, selected by push buttons	0.1-0.2-0.5-1-2.5- -5-12.5-25mm/sec.
Chart drive	200-250v 50Hz



Type H3020-3
Three-pen

Recording:

Syphon pen directly attached to moving coil frame, curvilinear co-ordinates

Equipment:

Marker pen, Timerpen, Paper footage indicator, 10 rolls of paper, connectors, etc.

Dimensions:

H320-1: 285x384x16.5mm
H320-3: 475x384x16.5mm

PRICE: H320-1 £108.00

H320-3 £160.00

Exclusive of VAT

Available for immediate delivery

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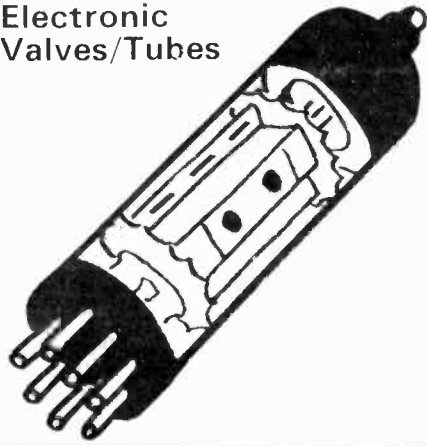
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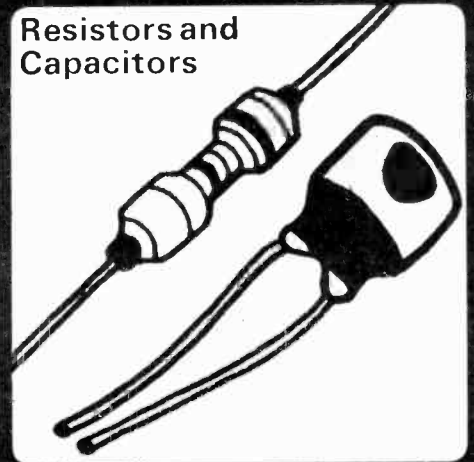
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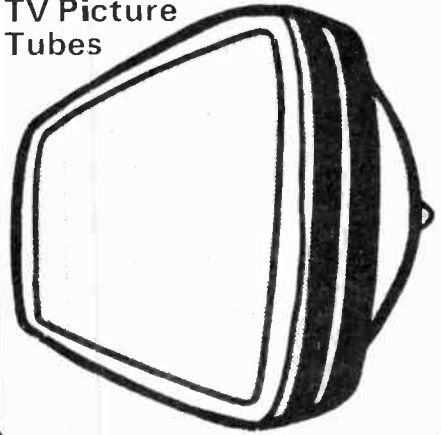
Electronic Valves/Tubes



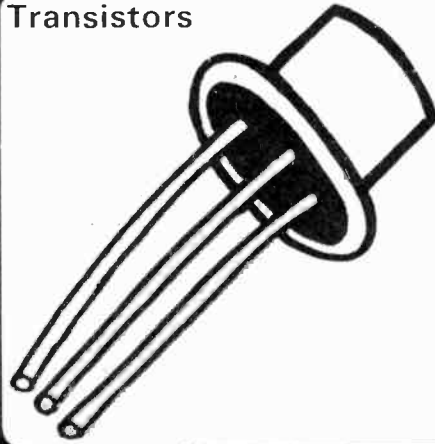
Resistors and Capacitors



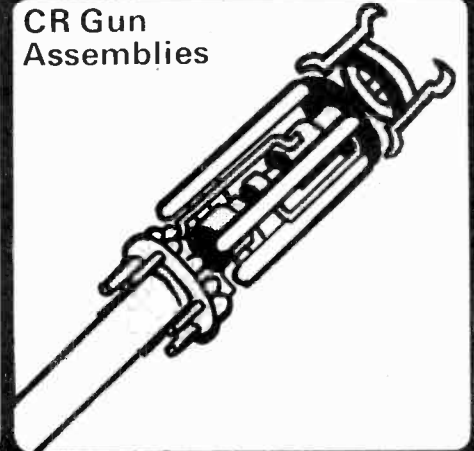
TV Picture Tubes



Transistors



CR Gun Assemblies

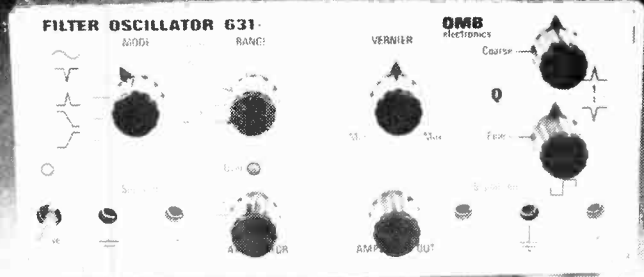


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Hi, Lo Pass	12 dB per octave
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631-0 1Hz to 100KHz 631LF-0.01Hz to 10 KHz

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 Telex: 848659.

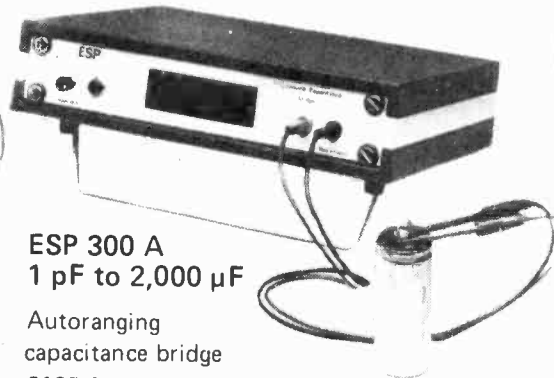
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ESP Capacitance measuring



ESP 100 A
1 pF to 10 μ F

Portable
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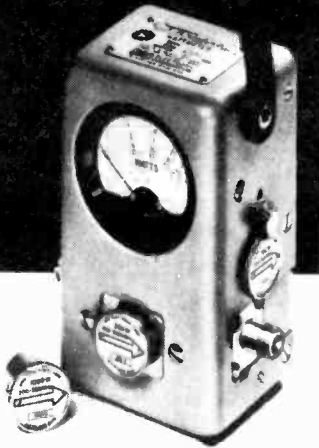
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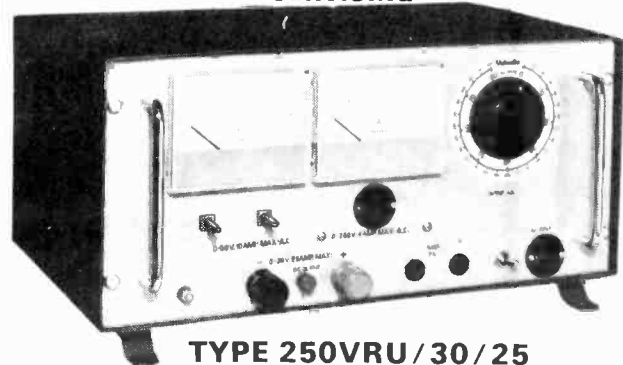
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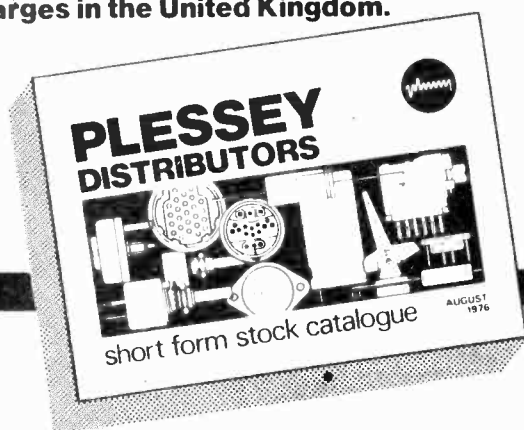
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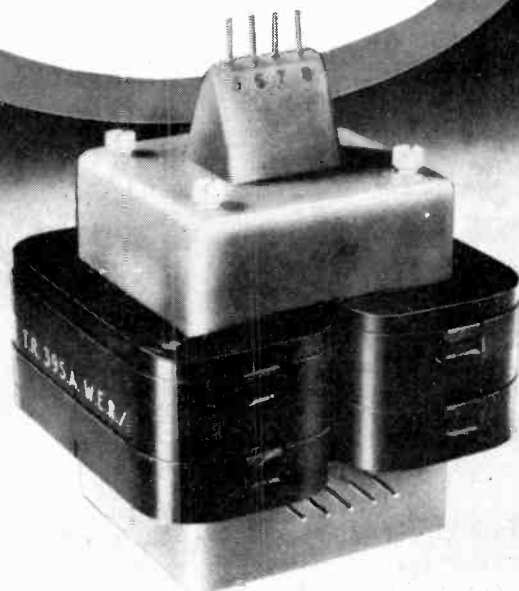
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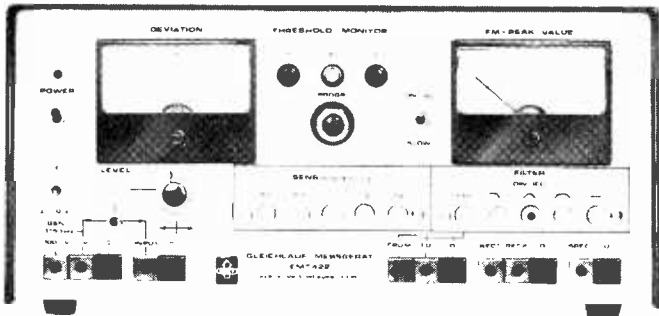
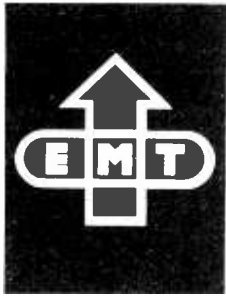
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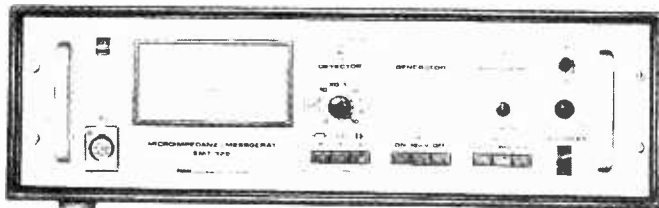


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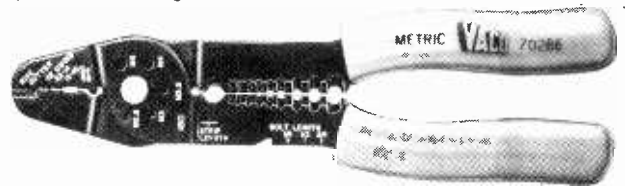
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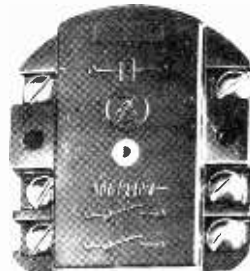
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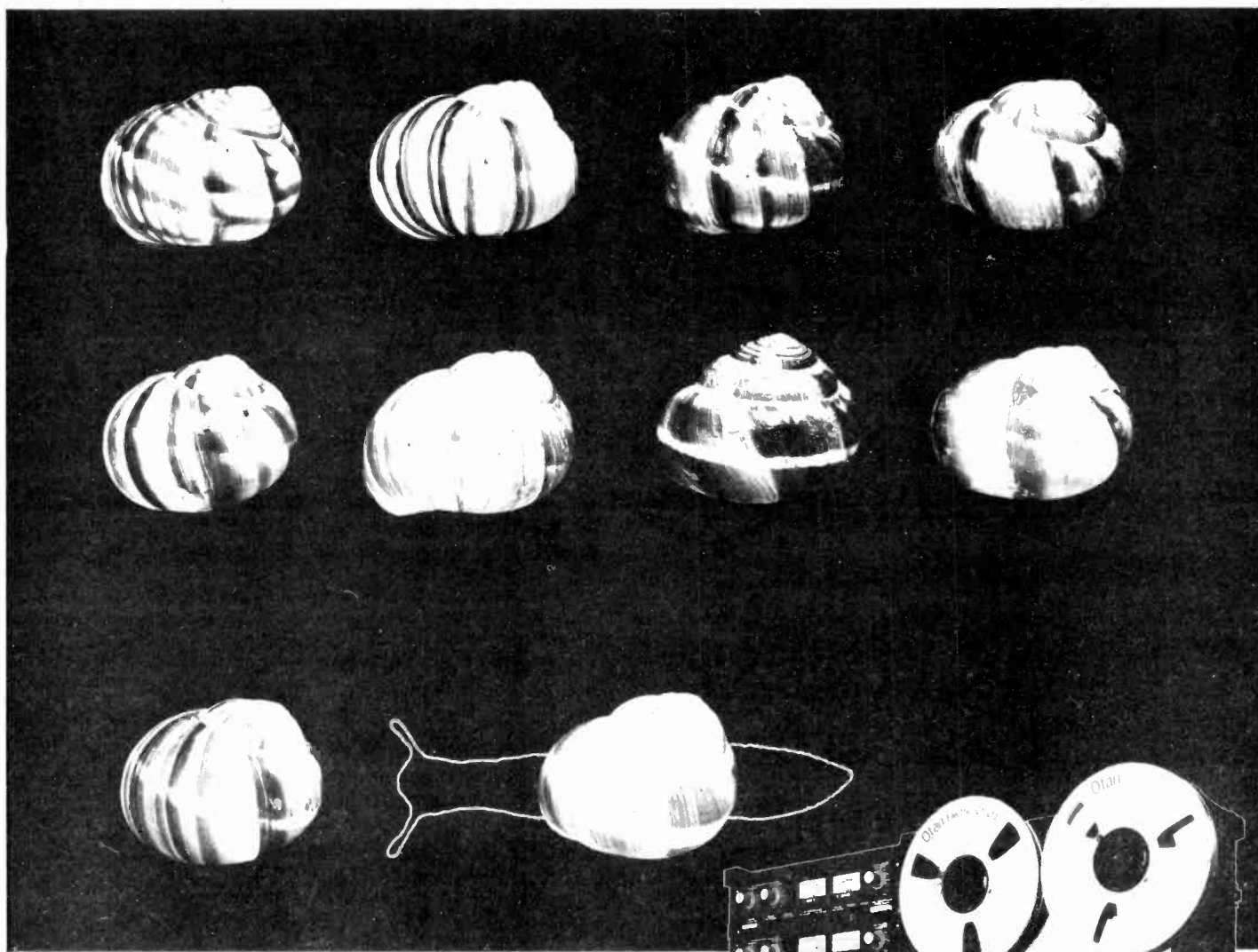
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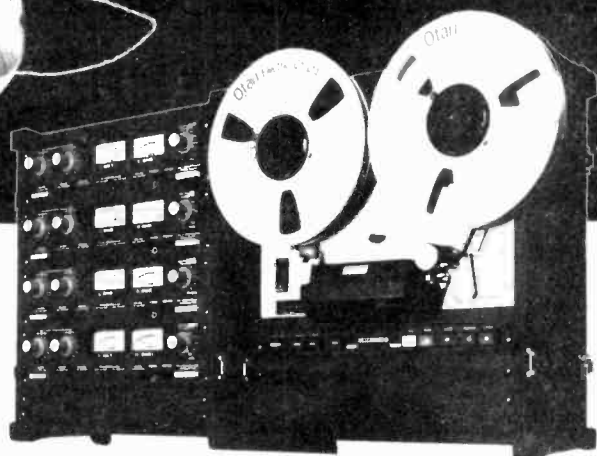
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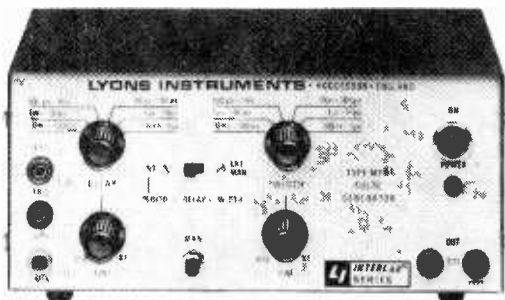
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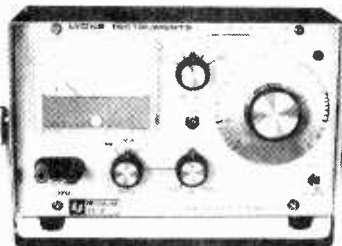


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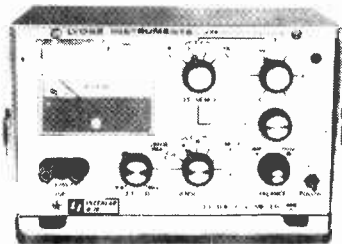
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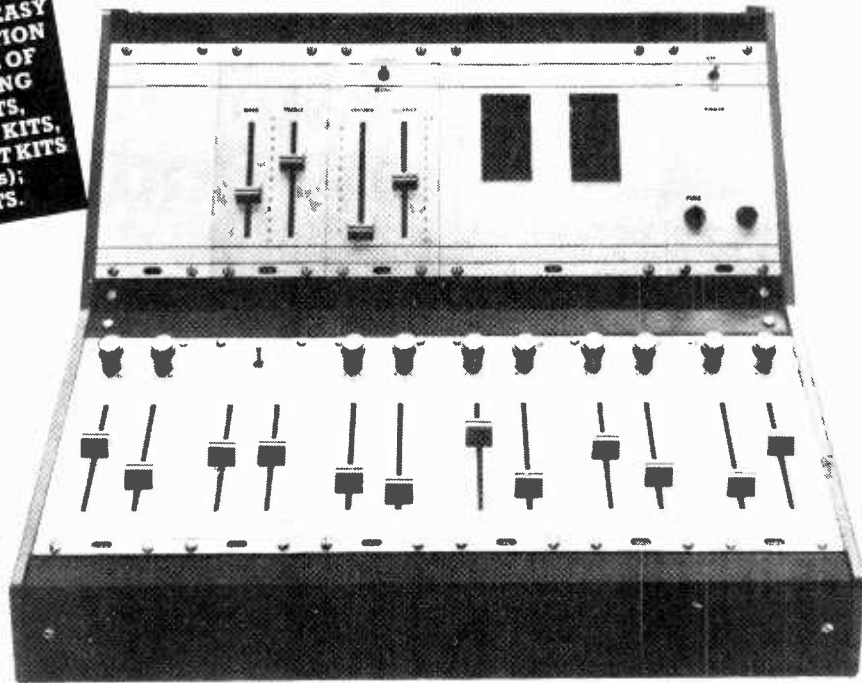
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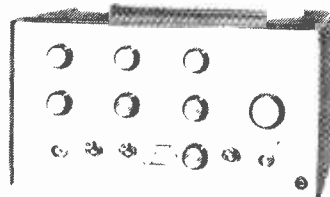
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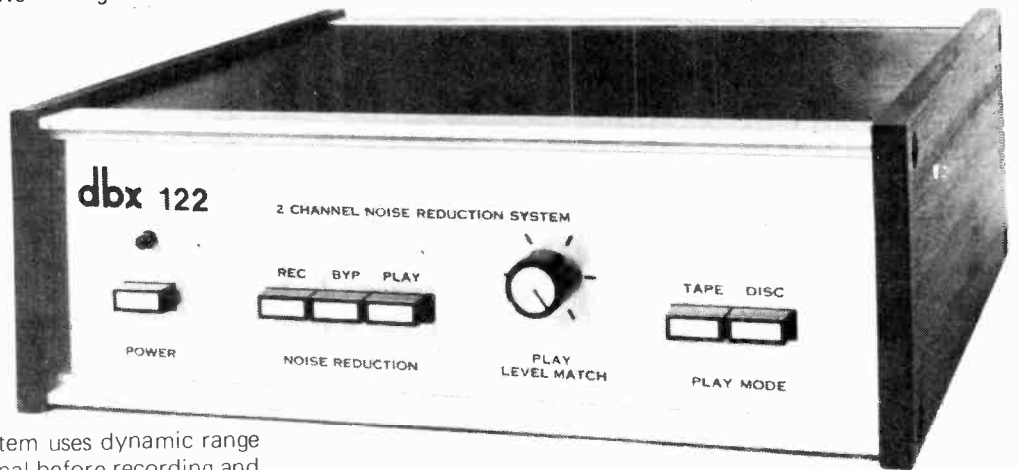
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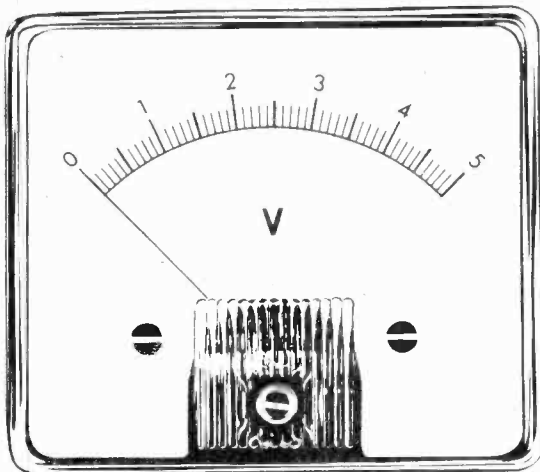
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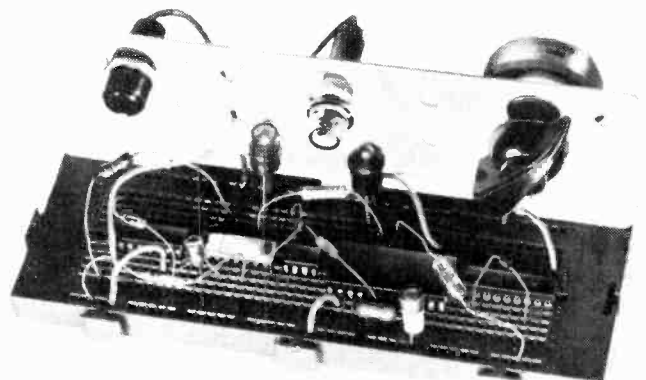
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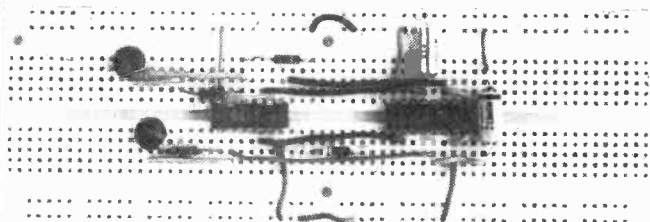
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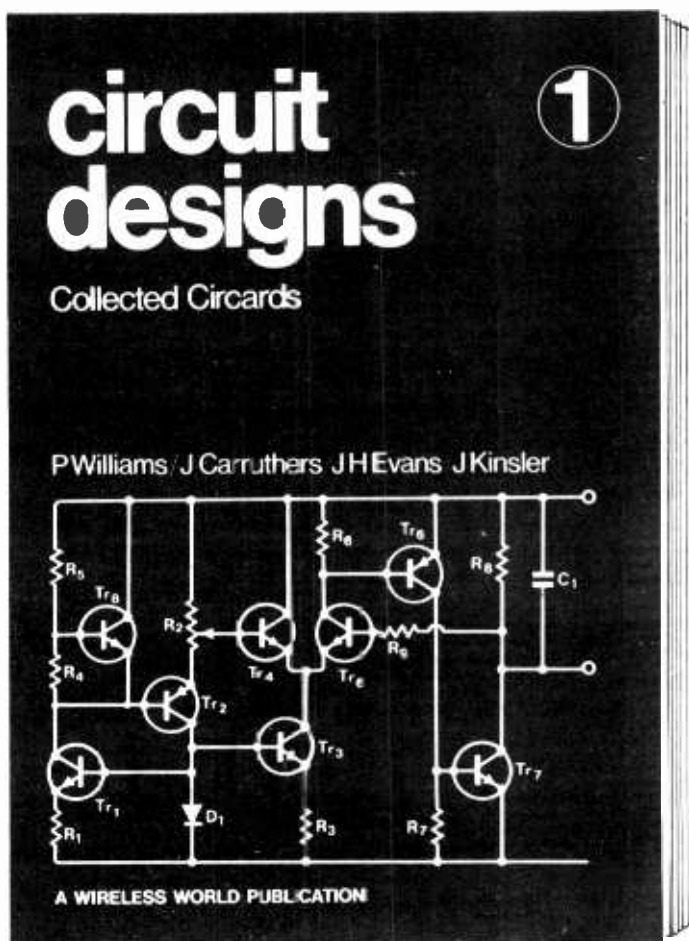
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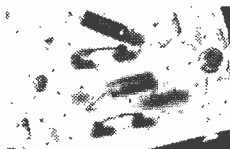
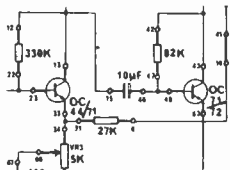
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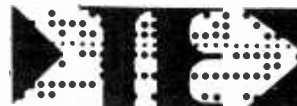
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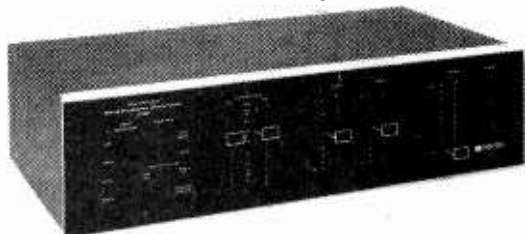
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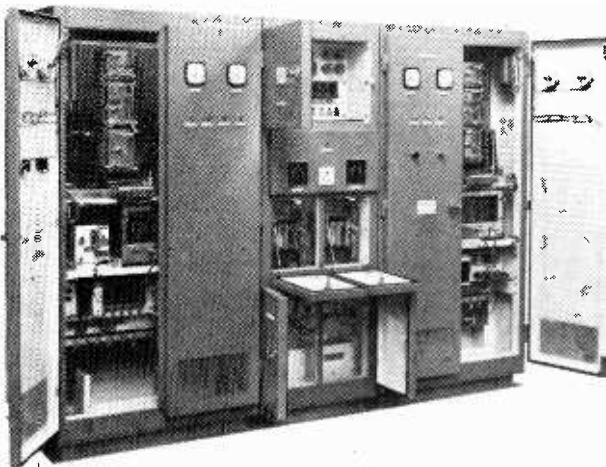
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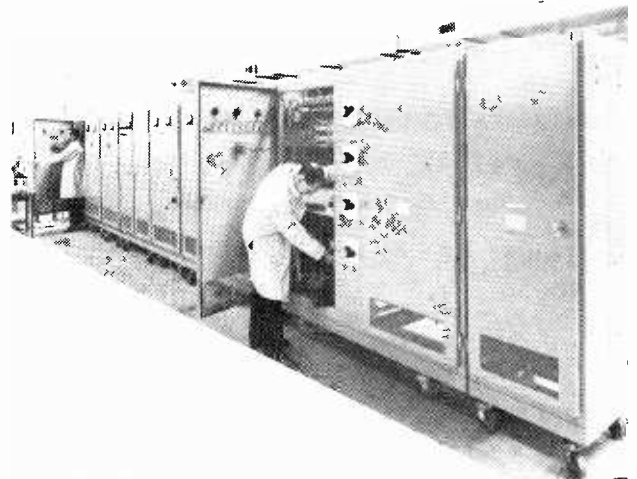
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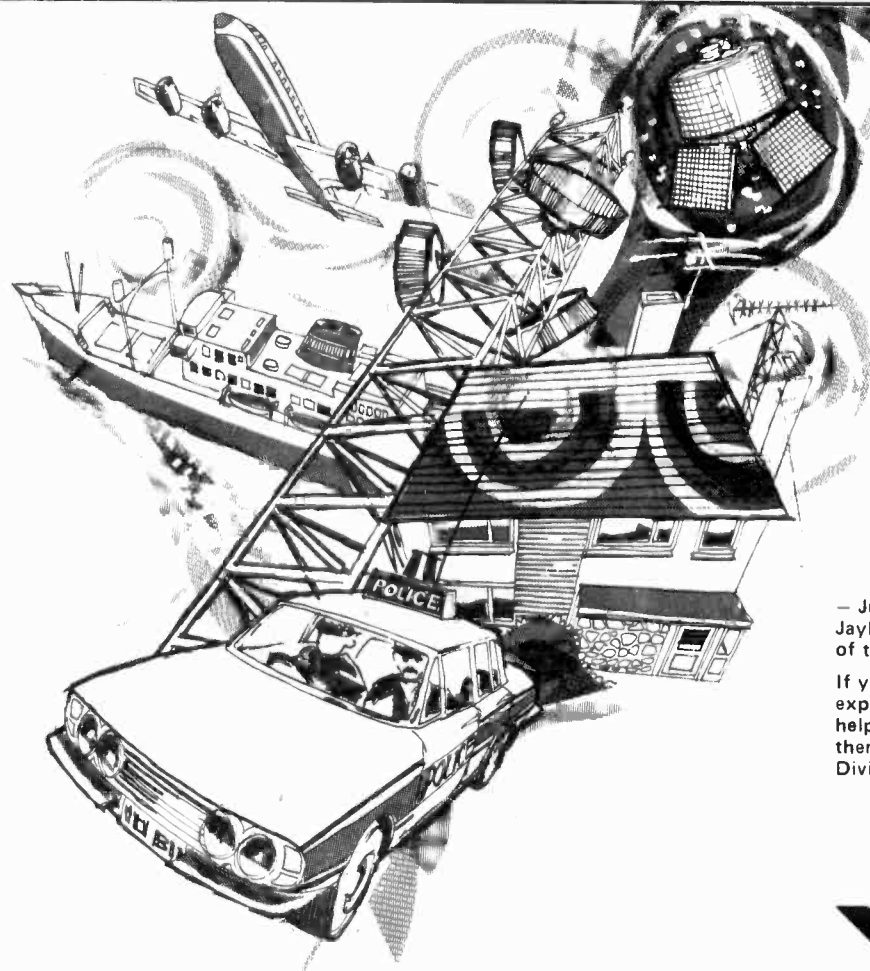
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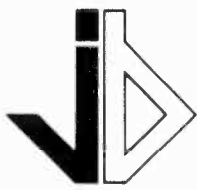


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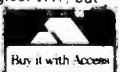
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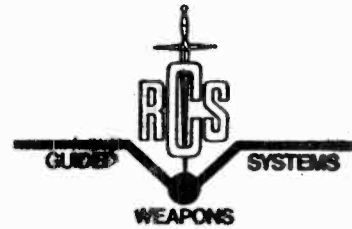
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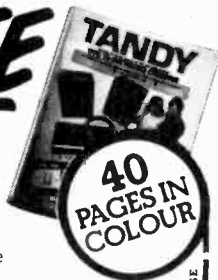
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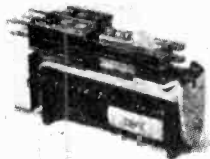
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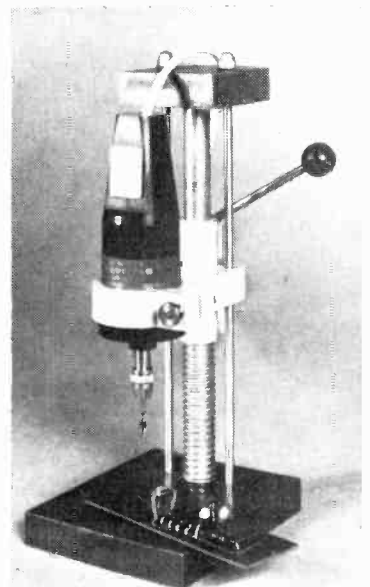
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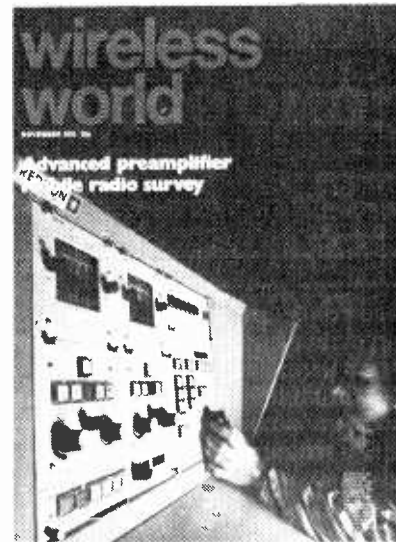
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Front cover shows part of a console of the Redifon Telecommunications CERES computer-assisted radio monitoring system and introduces the article on page 85.

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A cynic might say that people only co-operate reluctantly, from a realization of their own weakness. All the same, it's encouraging to be able to report on technical achievements that result from co-operation between different companies or organizations, especially when this co-operation crosses national frontiers. Whatever the motivation, one feels that successful co-operation is a worthwhile thing in itself and that the "brotherhood of man" is not after all just an empty phrase. Concorde is a case in point, regardless of the disagreements that attended the aircraft's development and the questions about its commercial viability. More recently this year we have seen a British firm, Marconi Elliott Avionic Systems, developing and supplying the flight control electronics for an American aircraft, the Boeing YC-14 military transport. Apart from individual projects, there are the continuous international technical programmes run by such organizations as the European Space Agency, CERN and EURO-COP-COST (European Co-operation and Co-ordination in Scientific and Technical research). The last-mentioned, for example, has a committee of fifteen members, including the British Post Office, studying the possibilities of radio communication at frequencies above 10GHz.

A characteristic of most of these international joint ventures and programmes is that they are set up between the industrialized, highly developed nations of the world. This is understandable since it is necessary for the partners to have comparable levels of technology, especially in "high technology" projects. But it is also one of the factors which tend to widen the gap between the rich countries and the poor countries of the world. The rich – those who have learned to apply science and technology to economic and social development – get richer and the poor remain poor. Although the developing countries support about two-thirds of the world's population, only two per cent of the world's total expenditure on research and development goes into them. Ninety per cent of the world's scientists and technologists work in the developed countries. So both talent and money are concentrated on solving the problems of the rich countries, and the gap between rich and poor becomes wider. It's a sad fact that the electronics industries of Western Europe and North America only "co-operate" with the developing countries to the extent of using them for cheap labour (particularly in consumer electronics) and as passive, dependent markets for their products.

The United Nations is concerned about this division among the world's people and has a committee that aims to help the developing countries to utilize modern science and technology, but so far it has achieved very little. Only when the individual national governments of the rich countries commit themselves to participate in an active way will there be any real co-operation between all the world's peoples.

Congestion in the shortwave bands

A topic for discussion at the World Administrative Radio Conference, 1979

by Jim Vastenhou, *Radio Nederland*

Shortwave broadcasting is of great significance to millions of people, who have to put up with a less perfect mass communication system than ours; without television and v.h.f.-f.m. broadcasting, no long wave, and only one or two transmitters within reach on the medium-wave band. It is this kind of situation that still prevails in large parts of the world, especially in Asia, Africa and to a lesser degree, also in South America. For these people, shortwave broadcasting may be their lifeline to the centres of civilization, to reliable and unbiased information, or simply to their own type of music or their own tongue.

The shortwave, or high-frequency (h.f.) range, running from 100-10 metres (3-30 megahertz), is the only portion of the electromagnetic spectrum which has the property of being able to propagate regularly over large distances, providing the frequency is properly chosen. Because of these propagational benefits the h.f. range is popular with many users: the aeronautical people, the maritime people, the amateurs, the armed forces, the national telecommunications administrations (PTT) and the international broadcasters, who value the ability to air their programmes (culture, political views), to compatriots overseas, seafarers and last, but not least, to people who might otherwise be denied free access to information. When you think about it for a moment, you will recognize one of the great values of shortwave broadcasting, namely, the possibility of being able to listen to different views on international affairs and of forming one's own opinion, a proven asset in periods of internal turbulence in a nation's existence.

Shortwave reception

However, it may be said that short waves are difficult, not least because propagation conditions tend to change with the hour of day and night, with the season, with the geographical location of the transmitter and the receiver, and periodically, over the so-called sunspot cycle. The varying propagation condi-

tions have led to the allocation of a number of shortwave broadcasting bands, the most important of which are:

49 metre band: 5.950- 6.020 MHz

41 metre band: 7.100- 7.300 MHz

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25 metre band: 11.700-11.975 MHz

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11 metre band: 25.600-26.100 MHz

Since propagation characteristics depend on the condition of the ionosphere, which in turn is dependent on many factors, one of which is the position of the sun at the point of signal impact, it can readily be understood that not all frequency bands are available for use all the time. In fact, the highest frequency band (11 metre band) is barely used at all at the moment: its usage is restricted to daytime periods under medium or high sunspot conditions. We shall have to wait a couple of years for such a situation to return, as we are at present in a low sunspot period. The solar cycle lasts about eleven years, with the maximum usually following the minimum in about four years.

After this brief look at the varying availability of the shortwave broadcasting bands it may be worth while to give some rules of thumb for those who want to listen to shortwave broadcasting stations. Generally speaking, the highest-frequency bands — 19, 16 and 13 metres — are valid for long-distance daytime propagation, between 2000 and 9000 km (1400-6000 miles). The longer wavelengths, such as 25, 31, 41 and 49 metres are either for short-distance daytime coverage, or for medium and long-distance night-time usage. A shortwave broadcasting band is, on the average, about 275kHz wide and the total available bandwidth for international shortwave broadcasts in Europe is 2350kHz or less than 10% of the entire spectrum. That is comparable to the frequency space allotted to the radio amateurs. Other users usually have more frequency space available and the fixed bands (used for point-to-point traffic by the telecommunications

authorities) top the list with 48% of the frequency space.

Channel width

A shortwave broadcasting station is allowed a total frequency occupancy of 10kHz. As the signal consists of a centre carrier frequency and two sidebands of equal width, it means that audio frequencies between, say, 30Hz and 5000Hz (5kHz) can be transferred from studio to receiver. The 10kHz width per channel rather limits the number of stations that can operate in a band. If we take the 25 metre band, the lowest usable channel is 11705kHz, the highest being 11970kHz. Keeping a channel separation of 10kHz to avoid mutual interference would leave us with 27 usable frequencies.

This is the theoretical minimum because, viewed on a world scale, it must be possible to achieve interference-free reception on more than 27 frequencies in the 25 metre band, e.g. by two widely separate transmitters operating on the same frequency to equally separate receiving areas and by using directional aerial systems. An example could be the BBC usage of a 25 metre channel to Africa, with a North American station broadcasting to either South America or the Pacific Area at the same time and on the same frequency (co-channel).

Separations of 5kHz are possible, if the frequency usage is coordinated properly between the users, or if geographically - separated properly, whether coordinated or not; this so-called interleaving is done on a large scale by shortwave broadcasters, as the frequency-separation of an adjacent 5kHz channel provides the extra interference protection that is needed in terms of signal-to-noise ratio, given a reasonable receiver selectivity.

So the frequency grid in the shortwave broadcasting bands is 5kHz, and an estimated 400 channels are available during favourable propagation conditions (high sunspot numbers). At present, at the minimum of the sunspot cycle, we are left with approximately 300 usable channels, and it is a

difficult task for the international shortwave broadcasters to service their respective target areas satisfactorily, not only because of the limitation of propagation towards the lower frequency ranges, but also because the number of shortwave transmitters is a multiple of the number of available channels and is growing continuously. The estimated number of shortwave transmitters operating in the world today is about 1500 and even if transmitters do have limited daily operating hours, the overload factor will still be more than 2. This means that in a particular spot on earth, at least two transmitters can be expected to be operating simultaneously on every available s.w. broadcast frequency — in Europe, there are periods when three or four broadcasters are on the same frequency simultaneously. The chart shows the state of the 25m band on June 4, 1976, on which the lines show stations heard.

Power race

Serious interference has resulted from this, and in trying to keep their services to the listeners at a reasonable level, shortwave broadcasting organisations have increased their transmitter carrier powers: 50kW was considered to be a reasonable power during the second world war, 100kW was considered "standard" in the fifties, and 250kW was introduced during the sixties, only to see the 500kW shortwave transmitter type emerging in the seventies. In terms of signal-to-noise (interference) ratio, the increase from 100 to 500 kW is only 7dB, but in terms of protection ratio it usually tips the balance at well above 20dB in favour of the high power station.

High-power shortwave transmitters are favourite items on the shopping list of nations that can afford them, and the order books of high power transmitter manufacturers show interesting delivery destinations: Libya, Iran, Brazil, Nigeria, Iraq, South Africa and Vatican City. Many responsible broadcasters feel that we must try to find a way out of this "power race", which leads to increasing cost for everybody concerned if they want to keep their services at an acceptable level. One way could be to set a maximum transmitter power by international agreement, but experience tells us that this idea is Utopian. It is impossible to enforce any international agreement made on a voluntary basis.

A solution?

An alternative may be to allocate more frequency space to the broadcasters, thereby decreasing the congestion in the s.w. bands and allowing everybody a reasonable breathing space. Assuming this to be possible, three other questions emerge: (1) how much new space is needed? (2) who will supply the additional frequency space? and (3) for how long will it remedy the situation? Apart

from these "technical" questions, there is the consideration that it would bring more fairness in the current situation. A number of countries (e.g. Albania, China, Egypt, Israel, Soviet Union and Vietnam) allow their international shortwave broadcasters to operate "out of band" in frequency ranges allotted to other services, whereas many other countries stick to the currently allocated s.w. broadcasting bands, thereby reducing their own technical effectiveness. So it is the feeling of many international shortwave broadcasters that they need more frequency space, since the present situation leads to continuously-deteriorating services where only the strongest broadcasters survive and, in the end, to organisations giving up, reducing listeners' choice and eventually detracting from the value of shortwave broadcasting itself.

Yet, the questions still stand, and they will undoubtedly form important topics at the next World Administrative Radio Conference, scheduled to start in September, 1979, in Geneva. This conference of the ITU (International Telecommunication Union), comprising the representatives of those countries which are members of the United Nations, will consider a reallocation of the radio spectrum, and many participants and frequency users have already been studying this subject for some time in preparation for the conference.

Many of them feel that the fixed services, to which almost half the spectrum space is at present allotted, could give up a reasonable portion, as new frequency space has become available for the fixed services through the telecommunications satellites and is still growing by extension into still higher frequencies. It is no secret that other frequency users, notably the maritime mobile services and the amateurs, also plan an extension of the frequency space allotted to them. On the other hand there is as yet no sign that administrations are willing to give up frequency space in the fixed bands voluntarily, although most of the traffic which used to be in the fixed h.f. bands has now been shifted to more reliable satellite communications, leaving registered frequencies unused for the time being.

If the conference can reach a *communis opinio* on the extension of the shortwave broadcasting bands at the expense of the fixed services, the questions of how much space and which bands remain. It is not possible to give a definite answer to these queries yet, but it seems reasonable to expect the broadcasters to want to double the available frequency space from 2350 to 4700 kHz. The feeling is that this could solve the problem of band congestion for a considerable time, perhaps 15 years, a period during which developments in the field of telecommunications will probably cope with future needs, either by the introduction of new receiving techniques or by a shift from h.f.

broadcasting to satellite broadcasting directly to the home. At the moment, however, this is all wishful thinking.

To conclude this survey, a few thoughts on the division of the extra frequencies. One of the apparently logical suggestions would be to extend the existing bands to cover some 550kHz instead of 275kHz, but that is not considered to be a good solution from the engineering point of view, because the congestion problems are more stringent in some bands than in others. It is especially the lower frequency ranges that need our particular attention, mainly for two reasons:

(1) the 49 metre band (6MHz) has turned out to be too short a waveband to cover nearby areas (200-1000 km) in the evening period during low or below-normal sunspot conditions. A longer waveband, probably in the vicinity of 4MHz is badly needed.

(2) The 49 metre band has been virtually the only frequency range that can be used during winter darkness conditions for east-west or west-east h.f. communications over long distances. The shortwave broadcasts from Europe to North America can serve as an example. The number of channels available in the 49m band has been inadequate to cope with the load of programmes from Europe alone, resulting in chaotic conditions. These could be avoided partly by a suitable extension of the 6MHz band, but many broadcasters feel that the 7MHz band (41 metres), now prohibited for broadcasting into the American region, should be made available to the broadcasters on a world-wide basis, just like the other broadcasting bands.

So, generally speaking, there is less need for band extension in the shorter wavebands than there is in the longer wavebands.

Let us hope that the delegates from the eighty or so countries broadcasting on the shortwave bands will have the wisdom to settle their differences at the 1979 WARC, differences which have been occupying them since 1933! It should be possible, now that technology has opened up new prospects for highly reliable point-to-point communications via satellite relays plus greatly expanded cable facilities. It would put an end to the power race and to the energy waste that goes with it, it would settle controversies on/out-of-band operation, and millions of listeners all over the world would benefit from it.

The above is the personal view of the author and does not necessarily reflect the views of the broadcasting organisation in which he is employed.

Advanced preamplifier design

A no-compromise circuit with noise gating

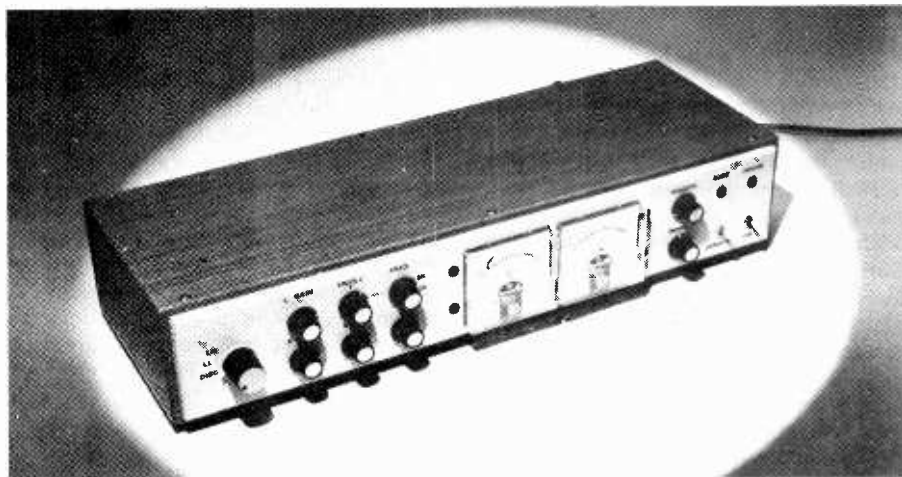
by D. Self, B.A., *Electrosonic Ltd*

This preamplifier design offers a distortion figure of below 0.002%, an overload margin of around 47dB, and a signal-to-noise ratio of about 71dB for the disc amplifier. A novel noise gate mutes the output when no signal is presented to the disc input and conversely, by using the subsonic information present on record pressings, eliminates the problem of muting low level signals.

This article describes a stereo pre-amplifier that equals or exceeds the performance of many of those available. The circuit incorporates a novel method of muting the signal path, when the disc input is quiescent, by using a noise gate that never mutes a wanted low-level signal.

Many of the important performance factors, such as signal-to-noise ratio, overload margin, and accuracy of the RIAA equalization, are essentially defined by the design of the disc input circuitry. This therefore merits close attention. The best attainable s/n ratio for a magnetic cartridge feeding a bipolar transistor stage with series feedback is about 71dB with respect to a 2mV r.m.s. input at 1kHz, after RIAA equalization. This has been clearly demonstrated by Walker¹. The equivalent amplifier stage with shunt feedback gives an inferior noise performance over most of the audio band due to the rise in cartridge source impedance with frequency. This limits the maximum s/n ratio after equalization to about 58dB. These facts represent a limit to what the most advanced disc input stage can achieve.

Overload margin appears to be receiving little attention. The maximum velocities recorded on disc seem to be steadily increasing and this, coupled with improved cartridges, means that very high peak voltages are reaching disc inputs. Several writers have shown that short-term voltages of around 60 to 80mV r.m.s. are possible from modern discs and cartridges, and higher values are to be expected. This implies that to cater for signal maxima, a minimum overload margin of 32dB with respect to



2mV r.m.s. at 1kHz is essential. Obviously a safety factor on top of this is desirable. However, most pre-amplifiers at the top end of the market provide around 35-40dB only. There are certain honourable exceptions such as the Technics SU9600 control amplifier which achieves an overload margin of 54dB, mainly by the use of a staggeringly high supply of 136V in the disc input amplifier. The Cambridge P50/110 series offers a margin in excess of 60dB by the artifice of providing unity-gain buffering, for correct cartridge loading, but no amplification before the main gain control. This allows the use of an 18V supply rail, but does limit the maximum s/n ratio.

The overload margin of a pre-amplifier is determined by the supply voltage which sets the maximum voltage swing available, and by the amount of amplification that can be backed-off to prevent overload of subsequent stages. Most pre-amplifiers use a relatively high-gain disc input amplifier that raises the signal from cartridge level to the nominal operating level in one jump. Low supply voltages are normally used which reduce static dissipation and allow the use of inexpensive semiconductors. The gain control is usually placed late in the signal path to ensure low-noise output at low volume settings. Given these constraints, the overload performance is bound to be

mediocre, and in medium-priced equipment the margin rarely exceeds 30dB. If these constraints are rejected, the overload margin of the system can be improved.

Two separate gain controls remove the most difficult compromise, which is the placement of the volume control. This approach is exemplified in the Radford ZD22 and the Cambridge P60 circuitry. One gain control is placed early in the signal path, preceded by a modest amount of gain. Cartridges of high output can be accommodated by the use of this first control. The second is placed late in the pre-amplifier and is used as a conventional volume control, see Fig. 1.

The other performance criterion which is largely defined by the disc input circuitry is frequency response, as defined by the accuracy of the RIAA equalization. Assuming that the relevant amplifying stage has sufficient open-loop gain to cope with the bass boost required, the accuracy of the equalization depends entirely on the time constants within the feedback loop. Careful design, and the use of close-tolerance components can assure an accurate response to within ± 0.2 dB from 30Hz to 20kHz.

Pre-amplifier distortion seems to have received little attention compared with that generated by power amplifiers, perhaps because the former has

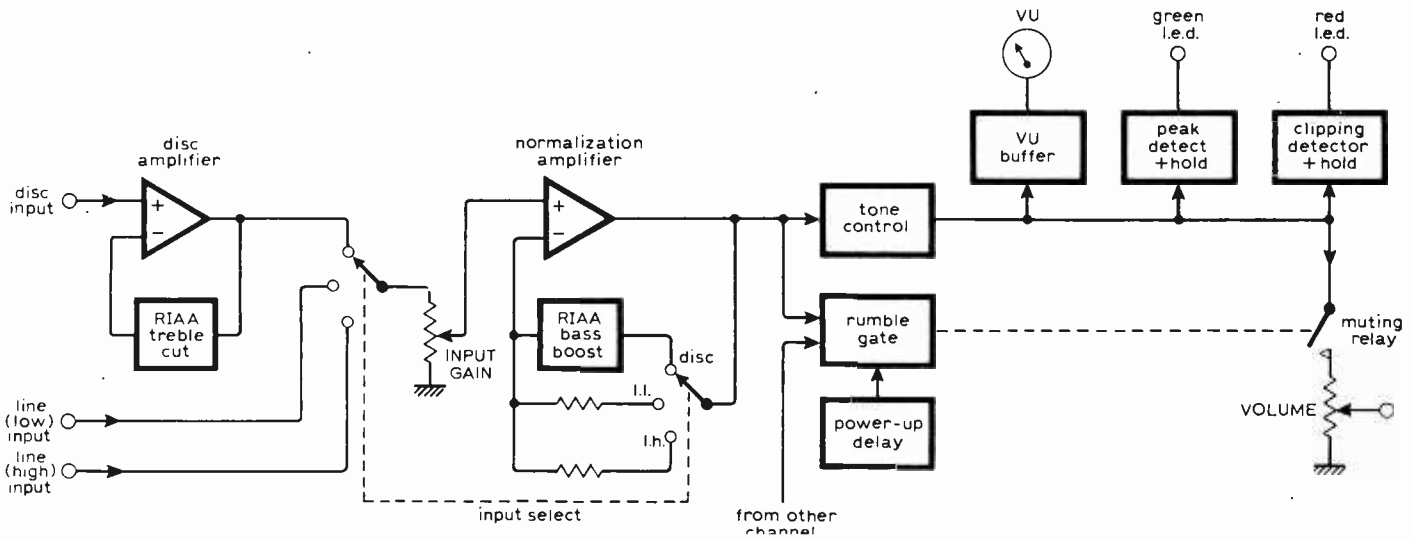


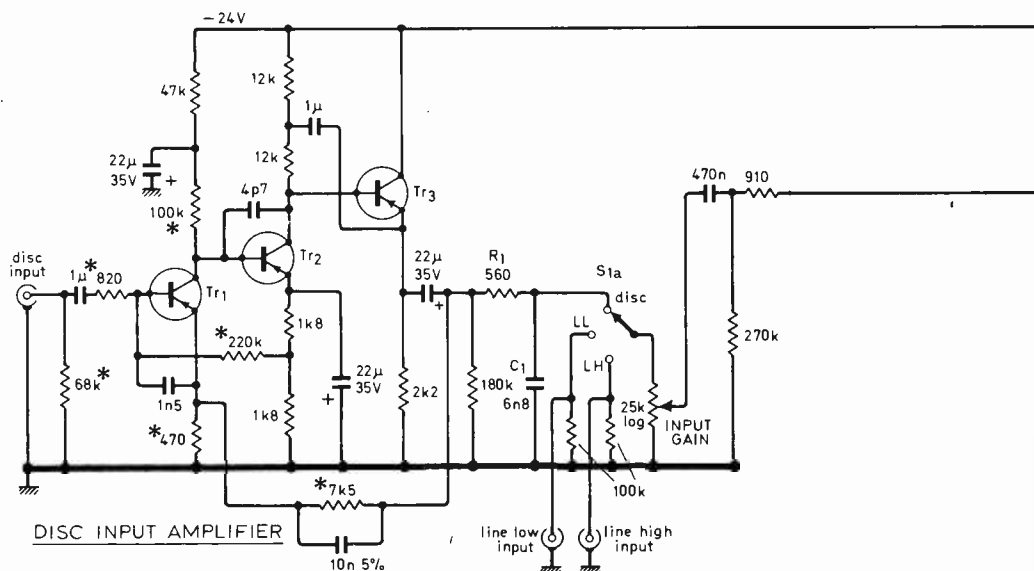
Fig. 1. Block diagram of the complete circuit. Two gain controls are used in the signal path to allow a substantial increase in overload margin.

The pre-amplifier is unmuted as soon as the stylus touches the disc, and muted about a second after it has been raised from the run-out groove. This delay can be made short because the relative quiet at the start of the run-out groove is sensed and stored. The rumble performance of the record deck is largely irrelevant because virtually all of the subsonic information is generated by disc irregularities.

Audio circuitry

A detailed block diagram of the pre-amplifier is shown in Fig. 1, and Fig. 2 shows the main signal path. The disc input amplifier uses a configuration made popular by Walker, but the

Fig. 2. Circuit diagram of the signal path. Constant-current sources are biased from a l.e.d./resistor chain for improved thermal stability.



traditionally been much lower. However, power amplifiers, with such low t.h.d. that the residual harmonics can no longer be extracted from the noise at normal listening levels, are now commonplace, particularly with the advent of techniques such as current dumping. This desirable state of affairs unfortunately does not extend to pre-amps, which in general produce detectable distortion at nominal operating levels, usually between 0.02% and 0.2%. In this design the t.h.d. at 1kHz is less than 0.002% even at 25dB above the nominal operating level of 0dBm. A Sound Technology 1700A distortion measurement system was used during development.

At this point it is convenient to consider the noise gate principle. When the pre-amplifier is being used for disc reproduction the output from each channel is continuously sampled to determine if a signal is present; if nothing is detected within a specified time interval, dependent on the previous signal levels received, the pre-amplifier is muted by the opening of a reed relay in series with the output signal path. This allows only power amplifier noise to reach the loudspeakers and considerably reduces the perceived noise generated by a quiescent sound system. Noise in the quiescent state is particularly noticeable when headphones are in use. The reed relay is also used to prevent switch-on transients from reaching an external power amplifier. So far this circuit appears to be a fairly conventional noise gate. The crucial difference is that signals from disc that have not been subjected to rumble filtering are always accompanied by very low frequency signals generated by record ripples and small-scale warps. Even disc pressings of the highest quality produce this subsonic information, at a surprisingly high level, partly due to the RIAA bass boosting. The l.f. component is often less than 20dB below the total programme level but this is quite sufficient to keep the pre-amplifier unmuted for the duration of a l.p. side.

collector load of the second transistor is bootstrapped. This increases the open-loop gain and hence improves the closed-loop distortion performance by a factor of about three to produce less than 0.002% at an output of 6.5V r.m.s. (1kHz). This stage gives a s/n ratio (ref 2mV) of about 70dB and a gain of 15 at 1kHz. This is sufficient to ensure that the noise performance is not degraded by subsequent stages of amplification. The maximum output of this stage before clipping is about 6.5V r.m.s. and the nominal output is 30mV r.m.s. Because this is the only stage before the input gain control, these two figures set the overload margin at 47dB. To ensure that this overload margin is maintained at high frequencies, the treble-cut RIAA time-constant is incorporated in the feedback loop. This leads to slightly insufficient cut at frequencies above 10kHz because the gain of the stage cannot fall below unity, and hence fails to maintain the required 6dB/octave fall at the top of the audio spectrum. This is exactly compensated for outside the feedback loop by the low-pass filter R₁ C₁, which also helps to reject high frequencies above the audio band.

For convenience I have referred to the next stage of the circuit as the normalization amplifier because signals leaving this should be at the nominal operating level of 0dBm by manipulation of the input gain controls. Separate controls are provided for each channel to allow stereo balance. A later ganged control is used for volume setting and causes no operational inconvenience. In the disc replay mode, the normalization amplifier provides the RIAA bass boost, by the feedback components $R_{2,3}$ and C_2 . Two line inputs are also provided; line low requiring 30mV and line high 100mV to give 0dBm from the normalization stage with the input gain control fully advanced. When these inputs are selected, the feedback networks are altered to adjust the gain and give a flat frequency response. Ultrasonic filters are incorporated to ensure stability and aid r.f. rejection. Capacitor C_3 in the feedback arm reduces the gain to unity at d.c. for good d.c. stability. If a fault causes the amplifier output to saturate positively the capacitor is protected by a diode which has no effect on the distortion performance.

The circuitry of the normalization amplifier is complicated because its performance is required to be extremely high. The harmonic distortion is far below 0.002% at the maximum output of

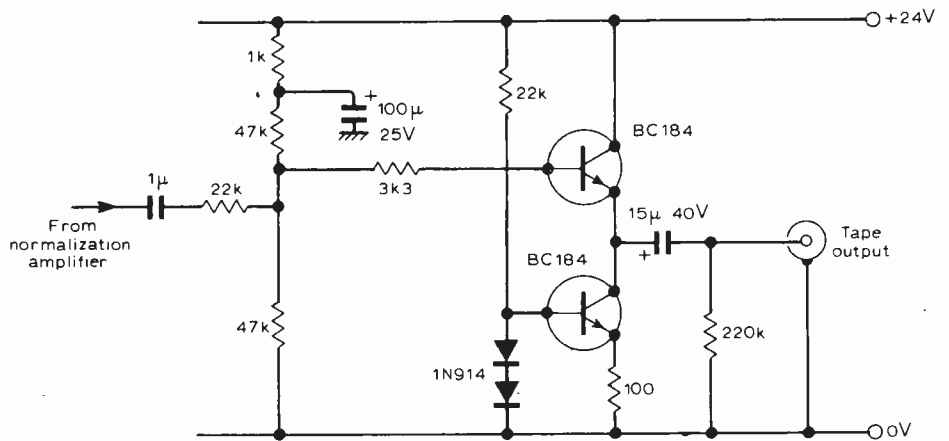


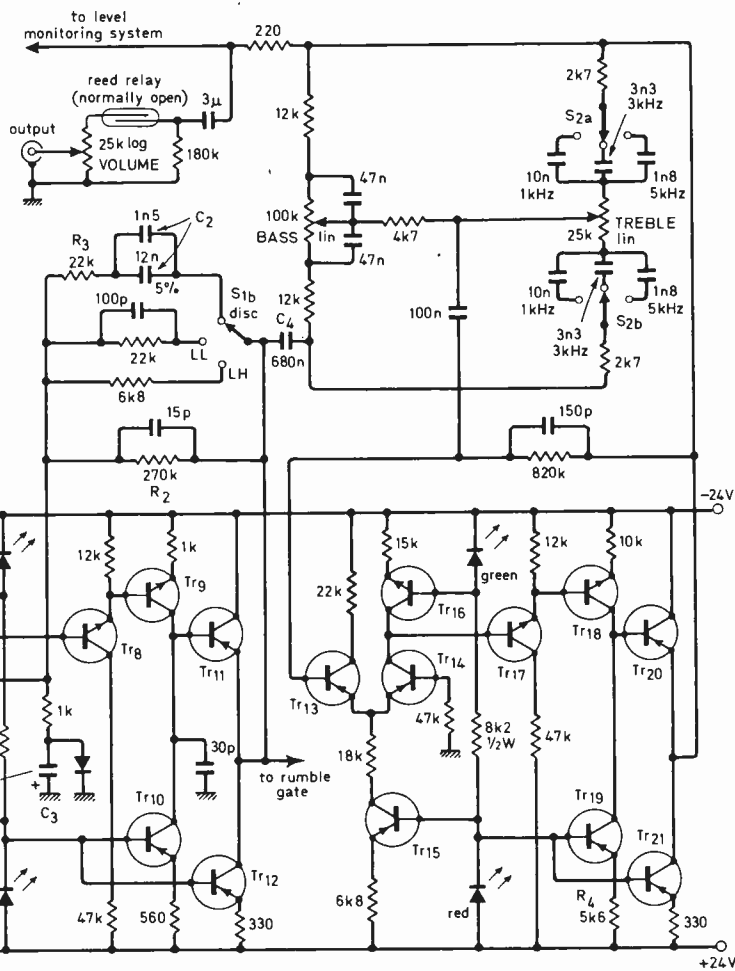
Fig. 3. Tape output circuit. The smallest allowable load impedance for an undistorted output is about $2.2k\Omega$. Line inputs of the pre amplifier are suitable for playback purposes.

14.5V r.m.s. which is 25dB above nominal operating level. This large amount of preamplifier headroom allows gross preamplifier overload before clipping. The input stage of the amplifier is a differential pair with a constant-current source for good common-mode rejection. The operating currents are optimized for good noise

performance, and the output is buffered by an emitter-follower. The main voltage amplifier, Tr_9 , has a constant-current collector load so that high voltage gain at low distortion can be obtained. This performance is only possible if the stage has very little loading so it is buffered by the active-load emitter-follower. The various current sources are biased by a l.e.d.-resistor chain because the forward voltage drop of an l.e.d. has a negative temperature coefficient that approximates closely to that of a silicon transistor V_{be} drop. Hence, this method provides exceptionally stable d.c. conditions over a very wide temperature range.

After the normalization stage the signal is applied to a tone-control circuit based on the Baxandall network. The main limitation of the Baxandall system is that the turnover frequency of the treble control is fixed. In contrast, the bass control has a turnover frequency that decreases as the control nears the flat position. This allows a small amount of boost at the low end of the audio spectrum to correct for transducer shortcomings. The equivalent adjustment at the high end of the treble spectrum is not possible because boost occurs fairly uniformly above the turnover frequency for treble control settings close to flat. In this circuit the treble turnover frequency has been given three switched values which have proved useful in practice. Switch 2 selects the capacitors that determine the turnover point. The maximum boost/cut curves are arranged to shelve gently, in line with current commercial practice, rather than to continue rising or falling outside the audio range. In addition, the coupling capacitor C_4 has a significant impedance at 10Hz so that the maximum bass boost curve not only shelves but begins to fall. Full boost gives +15dB at 30Hz but only +8dB at 10Hz. The tone control system has a maximum effect of $\pm 14dB$ at 50Hz and $\pm 12.5dB$ at 10kHz.

The tone-control amplifier uses the same low distortion configuration as the normalization stage, but it is used in a virtual-earth mode. The main difference is that the open-loop gain has been traded for open-loop linearity by increasing the emitter resistor of the



NORMALIZATION AMPLIFIER

TONE CONTROL AMPLIFIER

main voltage amplifier from $1k\Omega$ to $10k\Omega$ thus increasing local feedback. Resistor R_4 has been increased to $5.6k$ to maintain appropriate d.c. conditions. This modification makes it much easier to compensate for stability in the unity-gain condition that occurs when treble-cut is applied.

Level detection circuitry

From the tone-control section the signal is fed to the final volume control via the muting reed-relay. Note that this arrangement allows the volume control to load the input of the external power amplifier even when the relay contacts are open, thus minimising noise. The signal level leaving the tone-control stage is comprehensively monitored by the circuitry shown in Fig.4. Each channel is provided with two peak-detection systems, one lights a green l.e.d. for a pre-determined period if the signal level exceeds 1V peak, and the other lights a red l.e.d. if the tone-control stage is on the verge of clipping. Each channel is also provided with a VU meter driver circuit. Transistor Tr_{22} forms a simple amplifying stage which also acts as a buffer. Voltage feedback is used to ensure a low-impedance drive for the meter circuitry. The first peak detector is formed by IC_1 and its associated components. When the voltage at pin 2 goes negative of its quiescent level by one volt, the timer is triggered and the l.e.d. turns on for a defined time. The relatively heavy l.e.d. current is drawn from an unstabilized supply to avoid inducing transients into any of the stabilized supplies.

The clipping detector continuously monitors the difference in voltage between the tone-control amplifier

output and both supply rails. If the instantaneous voltage approaches either rail, this information is held in a peak-storage system. Normally Tr_{24} and Tr_{25} conduct continuously but if the junction of D_1 and R_5 approaches the $+24V$ rail then Tr_{24} and hence Tr_{25} turn off. This allows C_5 to charge and turn on Tr_{26} , and Tr_{27} and hence the l.e.d. until the charge on C_5 has been drained off through emitter-follower Tr_{26} . If the measured voltage nears the $-24V$ rail, then D_1 conducts to pull up the junction of R_6 and R_7 , which once again turns off Tr_{25} . In this way both positive and negative approaches to clipping are indicated. This comprehensive level indication does of course add significantly to the task of building and testing the preamplifier. If desired, any or all of the three sections may be omitted.

Noise gate

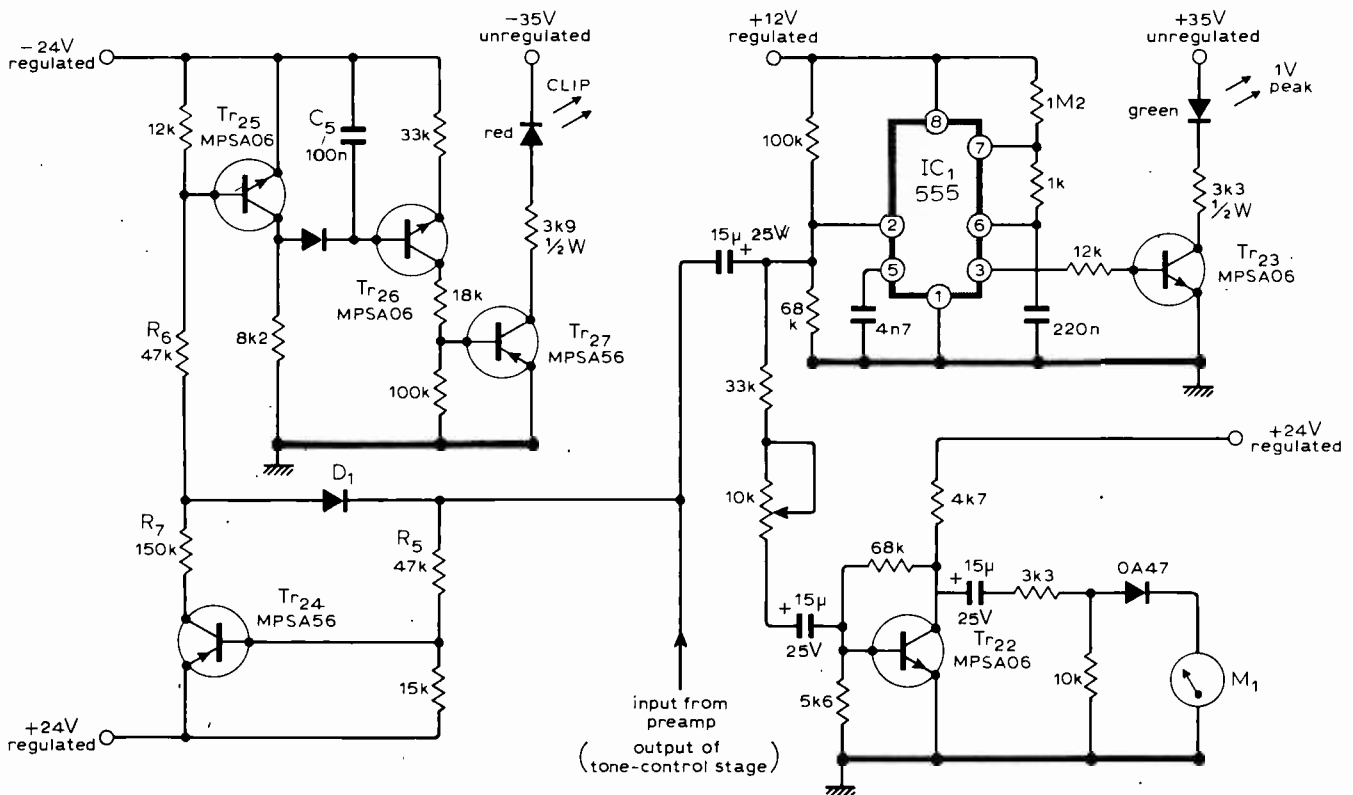
The final section controls the muting reed-relay. At switch-on, the $+12V$ rail rises rapidly until stabilized by the zener diode. Pin 2 on IC_4 is, however, briefly held low by C_6 , and the 555 is therefore immediately triggered to send pin 3 high. This saturates Tr_{28} which prevents Tr_{29} from turning on. At the end of the time delay, pin 3 goes low and relay driver Tr_{29} is no longer disabled.

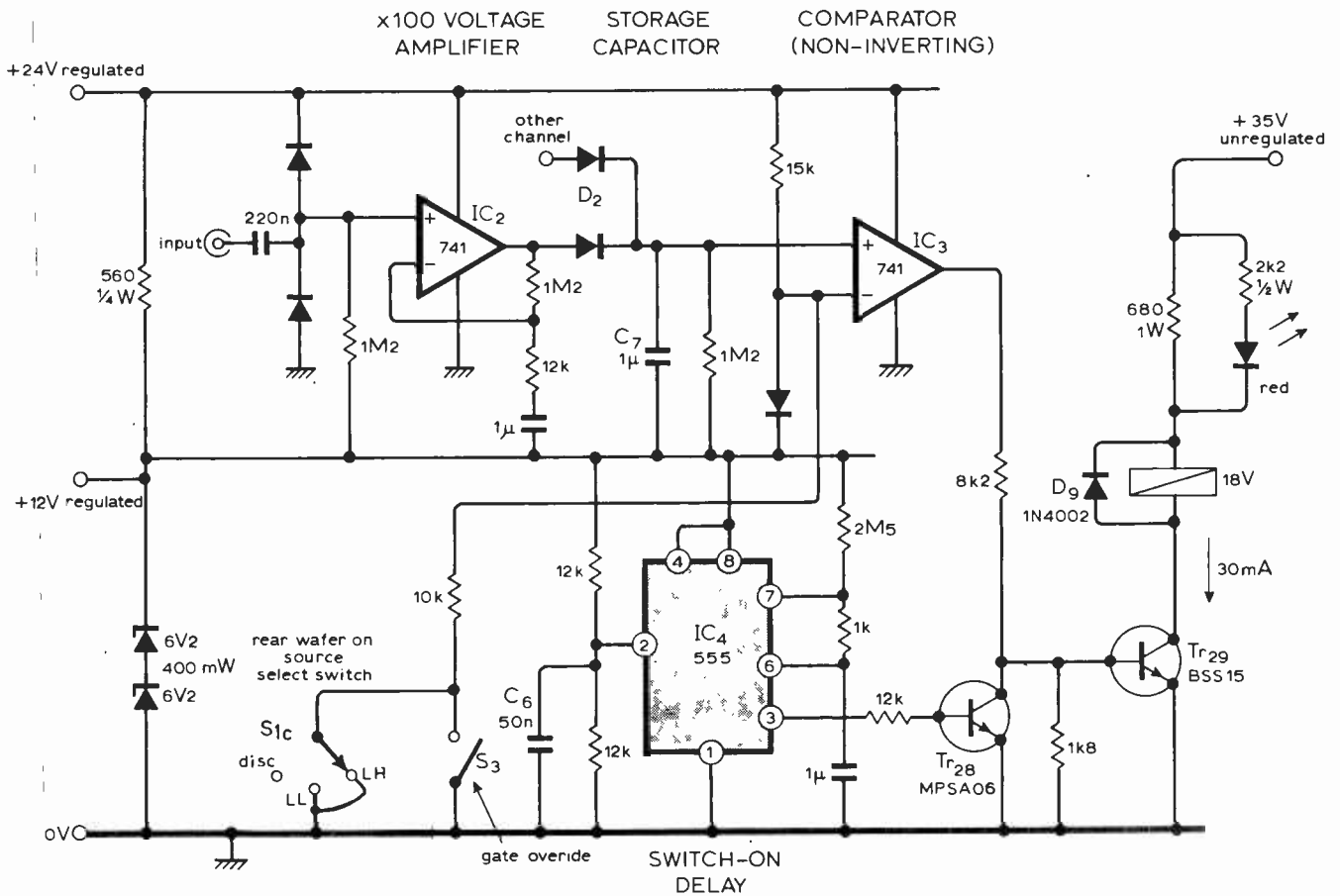
The noise gate uses two amplifiers with gains of about 100. These sample both channels at the output of the normalization stage and the inputs are clamped with diodes so that the norma-

lization amplifiers may use their full voltage swing capability without damaging the 741s. Due to their high gain, under normal signal conditions the op-amp outputs move continuously between positive and negative saturation which keeps the storage capacitor C_7 fully charged. In the silent passages between l.p. tracks the l.f. signal is not normally of sufficient amplitude to cause saturation but will usually produce at least $+3$ to $+4$ volts across C_7 which gives a large margin of safety against unwanted muting. To facilitate this the response of the amplifiers is deliberately extended below the audio band. When the stylus leaves the record surface and the l.f. signals cease, C_7 slowly discharges until the non-inverting input of comparator IC_3 falls below the voltage set on the inverting input. At this point the 741 switches and its output goes low to cut off the base drive to Tr_{29} , and switch off the relay. When the stylus is replaced on a record, the process takes place in reverse, the main difference being that C_7 charges at once due to the low forward impedance of D_2 . To prevent the relay sporadically operating when the preamplifier is handling signals presented through the line inputs, an extra wafer on the source-select switch is arranged to override the rumble-sensing circuit, and provide permanent unmute. This is achieved by pulling the inverting input of comparator IC_3 negative of the $+15V$ rail by the $10k\Omega$ resistor so that even when C_7 is fully discharged, IC_3 will not switch. In addition, S_3 provides a manual override for testing and comparison purposes.

The power supply is shown in Fig.6. Regulators are used to provide stabi-

Fig. 4. Level monitoring circuitry. Although three separate circuits are shown, these may be omitted as required.





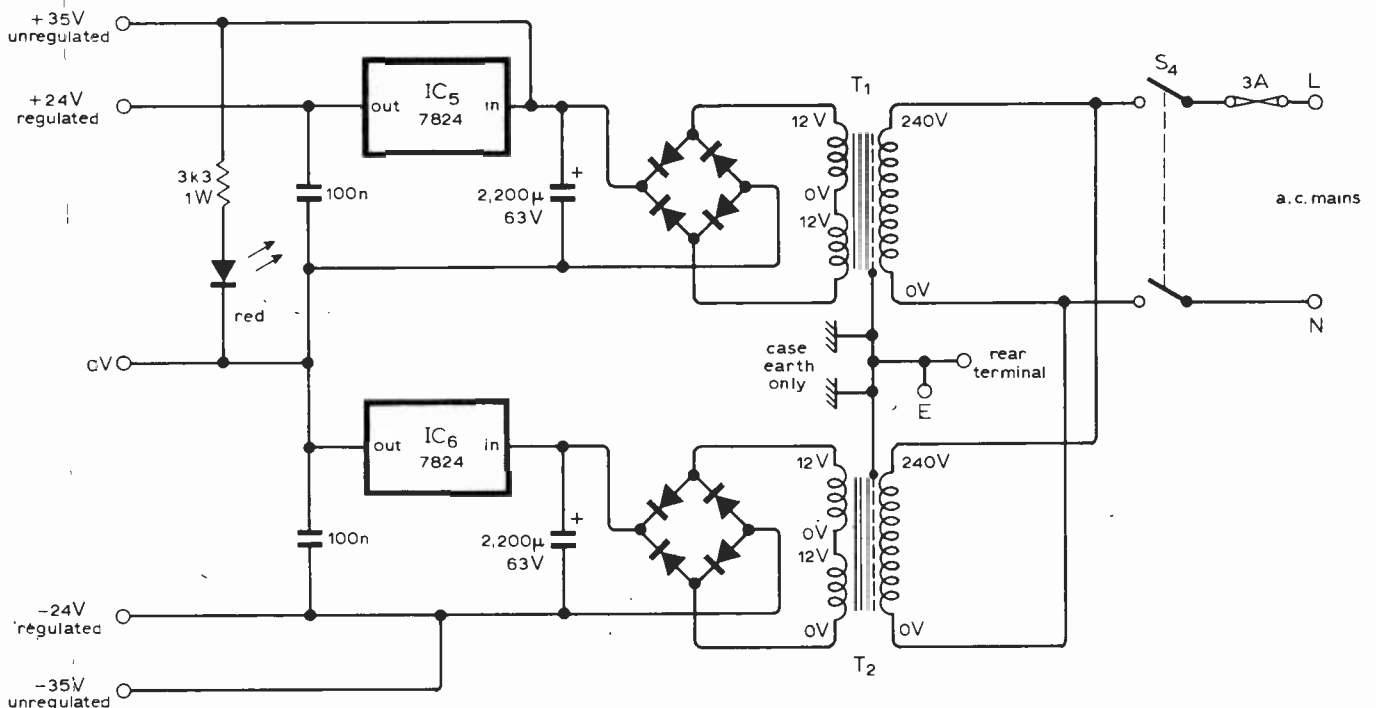
lized $\pm 24V$ rails. The unregulated supply rests at about $\pm 35V$. The signal circuitry has been designed to withstand $\pm 35V$ appearing on the supply rails, so that even in the unlikely event of both regulators failing, no further destruction will arise. Each regulator i.c. requires about $7cm^2$ of heat sink area.

Physical layout of the preamplifier is no more critical than that of any other piece of audio equipment. In general it is wise to use a layout that places the disc

input amplifier as close as possible to its input socket, and as far as possible from the mains transformer. Screened cable should be used between the disc input stage and its input socket, and between the final volume control and the output socket. The earthing requirements are straightforward and the circuit common 0V. rail is led from the input sockets through the signal path to the output volume control, and finally to the 0V terminal of the power supply. This arrangement minimises the possi-

Fig. 5. Noise gate and delay switch on circuitry. The noise gate is provided with an override switch for use with line input signals. The delay switch-on overrides all of the circuitry. Amplifier IC₂ is repeated for a stereo system.

Fig. 6. Power supply. Two regulator i.c.s are used which should be mounted on heat sinks.



Component notes

All unmarked diodes are 1N914 or equivalent.

Red bias i.e.ds are TIL209 or equivalent.

Green bias i.e.ds are TIL211 or equivalent.

Resistors marked with an asterisk should be metal oxide types

Tr_1 to Tr_6 and Tr_{13} to Tr_{15} are BCY71
 $Tr_7, 8, 9, 16, 17, 18, 22, 23, 25, 26, 28$ are
MPS A06.

$Tr_{10}, 11, 12, 19, 20, 21, 24, 27$ are MPS

A56

Tr_9 is BFX85 or equivalent.

The muting reed relay should be a 2 pole make type with an 18V coil. If a different coil voltage is used, the value of the dropper resistor should be adjusted.

The VU meter should have a 1mA movement.

If an internal diode and series resistor are fitted, the external components should be omitted.

Switch 1 (source select) is a 5 pole 3 way

Switch 2 (treble frequency) is a 4 pole 3 way

bility of spurious e.m.fs arising between stages. The only problem likely to be encountered is the formation of an earth loop when the preamplifier is connected to a power amplifier. Therefore, it may be satisfactory in a permanent installation to have the preamplifier circuitry connected to mains earth only through the signal lead to the power amplifier. The preamplifier case must of course be connected to the mains earth for safety reasons. It is preferable to define the potential of the preamplifier even if the power amplifier is disconnected. In the prototype the 0V rail was connected to the mains earth via a 22Ω resistor which stops the formation of an earth loop and prevents the signal circuitry from taking up a potential above earth due to leakage currents etc.

Testing is relatively straightforward, providing the preamplifier is constructed and checked stage by stage. Dynamic parameters such as t.h.d. are not accurately measurable without expensive test gear, but it has been found in the course of experimentation that if the d.c. conditions are correct then the various signal stages almost always show the desired a.c. performance. The non-signal circuitry should be relatively simple to fault-find. No problems should be encountered with the noise gate section which has proved to be very reliable throughout a protracted period of testing. The only preamplifier adjustment is for the VU meter calibra-

tion. This should be set to IV r.m.s. = 0VU, which is completely non-standard but very useful in terms of the dynamic range of the signal path. For normal operation the input gain controls should be set so that the meter indications do not exceed 0VU, to preserve a safety margin in the later stages. This completes the preamplifier design.

References

1. Walker, H.P. "Low-noise Audio Amplifiers", *Wireless World*, May 1972.

2. King, Gordon J. "The Audio Handbook", Newnes-Butterworth, 1975.

3. Heidenstrom, P.N. "Amplifier Overload", *Hi-Fi News*, December 1974.

Printed circuit boards

Wireless World has arranged a supply of glass fibre boards for the advanced pre amplifier. Two boards are available, one accommodates two audio channels, the other accommodates the stereo level detection and noise gating circuitry. The set of boards is priced at £7.00 inclusive. Available from M. R. Sagin at 11 Villiers Road, London N.W.2.

Literature Received

"Service planning and propagation" is No. 7 in a series of Technical Reviews from the IBA, which deals with the initial planning stage of new transmitters for sound and television broadcasting. Seven articles, concerned with service areas, field strength surveys, television microwave links and the business of negotiations with land interests are contained in the 64-page book, which is obtainable from Engineering Information Service, IBA, Crawley Court, Winchester, Hants SO21 2QA WW401

A cross-reference guide between CV, BS9000 and Nato semiconductors is available from Swift Hardman, containing currently-available types. Copies are obtainable from Semiconductor Sales Department, Swift Hardman Ltd, PO Box 23, Baillie Street, Rochdale, Lancs. WW402

A new GDS catalogue is now ready, containing lists and application information on a wide range of semiconductors, including Fetrons and integrated circuits. Components, tools and accessories are also covered and all prices are included. GDS Sales Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Berks SL1 3UZ WW403

We have received another weighty tome in the Eurolec series, this time No. 50, seventh edition of the guide to UK electronic components. In 507 pages, the book lists component manufacturers, importers and distributors, with company information and contracts, in both alphabetical order and by location. People in the industry are listed and there is a section in which associate companies are linked with their principals. A buyer's guide completes the book, which is available from Eurolec, Little Waltham, Chelmsford CM3 3NU, at £15.80 by post.

Modular telemetry outstations in the Serck Flex-C-Mos range are described in a four-page leaflet, from Serck Controls, Queensway, Leamington Spa, Warks. WW404

KGM have sent us a folder illustrating the principle behind the M-range edge-lit indicators. Characters of any form in sizes from 4mm to 150mm can be displayed. KGM Electronics Ltd, Clock Tower Road, Isleworth, Middlesex TW7 6DU ... WW405

"All in one package" is the title of an application booklet, produced by Marconi Instruments, on their TF2008 a.m./f.m. swept signal generator, which covers the frequency range 10kHz to 510MHz. Copies can be obtained from Publicity Department, Marconi Instruments Ltd, Longacres, St. Albans, Herts. WW406

A series of leaflets, produced by Omron, provides full electrical, mechanical and application information on the E3N range of photoelectric switches. The leaflets can be had from IMO Precision Controls Ltd, 349 Edgware Road, London W2 1BS. WW407

Counter/timers with maximum input frequencies of 32MHz to 1.2GHz are described in a brochure from RCS Electronics. Specifications of six instruments are included. Copies from 6 Wolsey Road, Ashford, Middx TW15 2RB. WW408

A list of UK-produced bibliographic data bases (abstracts, lists, reviews, information services, etc.) has been compiled by the British Library. The inventory is the basis of the UK contribution to the European information network and covers an enormous range of scientific and technical subjects. A subject index is provided. The "Inventory of bibliographic data bases produced in the UK" is available at £2.50 from Publications Ltd, British Library Lending Division, Boston Spa, Wetherby, West Yorkshire LS23 7BQ.

Ferranti have sent us leaflets on six new integrated circuits, an i.c. price list and an application report on the ZN417 analogue processor, which comprises three operational amplifiers and a voltage regulator in one package. The other i.c.s are the ZN1084E oscillator-divider timer, the ZN423T 1.26V reference source, the ZN10404 up/down counter, a gated linear amplifier, the ZN424, and an 8-bit a.-d./d.-a. converter type ZN425E. Ferranti Ltd, Electronic Components Division, Gem Mill, Chadderton, Oldham OL9 8NP. WW409

Technical Bulletin 7a-123 (UK) from Alpha Metals is entitled "Alpha M.E.G. Resin-based Solder Creams". The range of materials available is described, with methods of application and the removal of residues. The bulletin is obtainable from Alpha Metals Ltd, 457 Kingston Road, Ewell, Surrey ... WW410

News of the Month

More BBC surround-sound

The BBC has kept secret their use of the matrix H surround-sound encoding system for two concerts during the recent promenade series. The first occasion was the Salzburg Mass for eight choirs and orchestra from Westminster Cathedral, on August 5, and the second was the Beethoven "Emperor" Concerto and the Shostakovich Symphony No 10 from the Royal Albert Hall, on August 30.

In a statement issued on August 23, the BBC said that the H matrix had undergone "very rigorous testing and comparison with other systems already known to broadcasters and the public. The tests have been judged by panels of engineers, acoustic experts, musicians, and producers of all forms of radio programmes, and little doubt remains that the BBC's experimental matrix system . . . is superior for broadcasting to other systems tested." The BBC laid particular stress on its compatibility, which they say matrix H combines with "very good quadrasonic reproduction."

A panel of expert listeners compared it very favourably with normal mono and stereo reproduction of similar concerts, but none of the currently available decoders was suitable for use with the system. In any case, the BBC say their first priority is to extend v.h.f. and stereo services throughout the country: even though the stereo distribution network can carry matrix H two-channel signals without modification, "no regular quadrasonic service is envisaged at present."

The Corporation add that they are making the specification of the matrix available to members of the European Broadcasting Union and other interested professional bodies. A detailed article about the H matrix will appear in the *EBU Review* in October this year, but so far as is known the matrix conforms roughly to a phase-modified form of the Sansui QS system. As the BBC says, that does not mean that QS decoders will

operate satisfactorily with the H matrixed signal as input, and in any case most of the commercially-available circuits have been modified so extensively that they bear little relationship to their original forms of the early 70s.

First British and European microprocessor

The first microprocessor to be wholly designed, developed and manufactured in Europe is being produced in the UK by Ferranti at their electronic components factory at Oldham, Lancs. Called the F100-L, it is an advanced 16-bit computing device with typical instruction times of 3-4 μ s and the ability to handle up to 32,768 16-bit words of semiconductor or core memory. Unlike many microprocessors, which are based on m.o.s. technology, it has bipolar, non-saturating gates produced by Ferranti's well-established c.d.i. (collector diffusion isolation) process (see *W. W. Nov. 1971 issue*, p. 526). These are fast in operation, giving speed power products of less than 1 picojoule and propagation delays in the range 3 to 20 ns. The 7000 components of the device, which has 1500 gates, are on a 5.8mm square chip which is housed in a 40-pin dual-in-line package. Price of the device is £39 for quantities up to 100.

Development has been partly financed by the Ministry of Defence, so it is likely that the microprocessor will be used first in military applications. But Ferranti have set up a marketing unit to sell it to any equipment manufacturers, and it will become generally available on the market, together with a three-chip interface set, in early 1977. Considering the MoD sponsorship, and the fact that Ferranti itself is 50% owned by the Government (through shares held by the National Enterprise Board), the new microprocessor can be seen to a great extent as a venture of the British public.

ITT have also launched into the microprocessor market, which they say they expect to grow to £75 million in the UK in 1984 from its present £2 million. Next year, they say, it will be worth £7 million and in 1980 £25 million, of which they hope to capture at least £4 million.

The European market, at present worth £8 million, should be worth £100 million in 1980 and will grow by £100 million every two years to 1984. Their market projections appear to be based on internal information available in their British and European offices and on what happened to the i.c. market. ITT believe that all this growth will come from users who have never had anything to do with semiconductors before, never mind anything more complicated. They cite the motor

industry, washing machine makers and the control industry as examples of possible users of microprocessors. The consumer industry, they say, would tend to follow the industrial users, as has happened in the past. The non-electronic uses of microprocessors account for ITT's stress on educational programmes for potential users, and they are quoting training programmes at £45 a person a day for what would normally be a two- or three-day course.

First Dolby i.c. chip

Mullard's Signetics marketing group are now making available a Dolby B monolithic i.c. The chip is called the NE545B and, although working models have been made by Fairchild, Hitachi and National, this is the first to become commercially available. The others, say Dolby, may be ready towards the end of this year or early next year. The chips, whoever makes them, will not be generally available, and makers will only be able to supply those who already have a licence to make Dolby B processors.

Industry-oriented thin film research

Newcastle University's Electrical and Electronic Engineering Department is to get a £155,000 grant from the Wolfson Foundation for a four year programme of research devised jointly by the university and Welwyn Electric Ltd. In a statement, Welwyn said "There is an increasing danger that British industry's technology will fall behind that of other countries because of inadequate investment in research and development". There must be rapid development of commercial products which will stimulate production, particularly in high technology products.

The research will investigate thin films made from new alloys and deposited by various vacuum processes on to a variety of different substrates and the additional application of a range of post deposition treatments to improve electrical properties. "The work will be directed toward the development of improved precision resistors and resistive networks to be used in a variety of demanding applications where high accuracy and maximum stability are required in components of the smallest possible size." The project was one of the small proportion of applications that the Wolfson Foundation was able to accept from universities round the country. The research team will, according to Welwyn, collaborate closely with them to make sure the results of the research are rapidly exploited.

London's broadcasting convention

Although 2,500 or so delegates from 50 countries attended this year's International Broadcasting Convention in London in late September there was some feeling that there had been a lack of foreign interest. RCA, for example, had not exhibited, it was said because the extra business a stand might bring would not repay the cost.

The microprocessor has already found its way into broadcasting, and the IBA presented a paper on an m.p.u. based system design for measuring, monitoring and controlling transmitters. As in other applications, the microprocessor's use is a natural extension of the use of computers and minicomputers, and a natural result of the increasing use of unmanned transmitters. The microcomputer system developed by the IBA is based on the Intel 8080 eight-bit device, and they used a variety of modules for various functions. One application described was a visual display unit sub-system for an IBA Regional Operations Centre. The sub-system displays mimic diagrams to show the status of all stations equipped with telemetry within the region and to present priority alarm systems when fresh alarm conditions are reported. Teletext control and processing is another obvious application.

Some of this was mentioned in the television film based on the 1975/6 Faraday lecture and shown on independent television on the 21st anniversary of commercial television which, happily, occurred in mid-convention. Another development featured in the programme was that of a new generation of lightweight electronic television cameras. Electronic journalism, in fact, provided such interest at the convention that an electronic news gathering discussion session was full to overflowing and had to be continued on another day.

Thomson-CSF have produced a three tube Plumbicon camera which weighs 8lb and, with what used to be called a back pack — a title that hardly seems appropriate any more — a total of 11lb. The broadcast quality camera has been jointly developed by Thomson and CBS Labs, and is already in use on the CBS network. It is possible, though unlikely, that by the time the next IBC convention is held new cameras based on charged couple devices will be near pocket size.

According to a paper presented by G. M. Le Couteur of the BBC Research department, solid state image sensors will replace camera tubes in tv cameras in five to ten years, but "much work remains to be done before solid state area arrays can begin to be considered for use in broadcast cameras . . .

It should soon be possible to achieve devices with the necessary resolution for 625 line systems (572 by 572 elements absolute minimum) at the data rates required (11 MHz absolute minimum), but the difficulty in obtaining a uniform response free of blemishes on the large chip sizes required promises to keep the yield of perfect devices extremely low for many years."

The c.c.d. devices currently available had poor blue response and suffered from inconsistency between the spectral responses of nominally similar devices. This might be overcome by back imaging through a substrate of silicon only 20 μm thick, but producing and maintaining such a thin layer was a technique that had not yet been perfected. Semiconductor devices also had a high dark current, which reduced the dynamic range of the device. In the case of c.c.d. the dynamic range increased by an order of magnitude to 1000:1 when cooled from room temperature to -40°C , and some form of on-chip cooling might be essential.

"The scanning organisation within c.c.ds is not yet resolved. It seems that sensitivity, resolution, interface considerations and back imaging ability will result in a preference for the frame transfer mode in which the whole of the sensing section is involved in light collection."

"The future availability of sensors at other than unrealistically high prices may well depend on the ability of the broadcasters to meet the manufacturer at least part way by accepting a small number of blemishes and concealing them electronically."

The tendency for the convention to feature developments in television almost exclusively has continued, but the BBC showed a receiving system which reduces the interference previously experienced in the multiple use of radio microphones. Reflections of the radio waves from walls and studio equipment cause standing wave patterns which change as the performer moves round the studio, and the receiver may be in a null, causing muting of the sound signal. According to *BBC Engineering*, "BBC research engineers investigated r.f. propagation characteristics in studios and found that there was little or no statistical evidence for preferring any particular frequency band but that a four receiver diversity system could give complete coverage of the studio floor. The BBC radio microphone combines the weighted outputs of four independent receivers each connected to its own aerial located in different parts of the studio. Combining the outputs in this way achieves a better signal to noise ratio than simply switching to the optimum receiver-aerial unit and does not introduce switching transients."

If voltages from each receiver are detected and digitally coded at a sampling rate of 16.6kHz, the optimum audio contribution for any receiver

depending on the square of its aerial input voltage in relation to the sum of the squares of all the aerial input voltages. Multiplication, addition and division are then performed digitally to obtain a digital control signal for each weighting network. "Each weighting network is a multiplying digital to analogue converter. The audio output from each receiver passes through the multiplying d.a.c. and is attenuated by the correct amount for that instant. The four contributions are then added in an analogue adder to give the final output."

The continuing improvement in helical scan v.t.rs was illustrated by Ampex, who featured both a helical scan video timebase corrector and a model of a portable lin h.s. high band colour teleproduction recorder. The TBC1 timebase corrector is compatible, say Ampex, with all current h.s. v.t.rs and has been developed with, again, electronic news gathering in mind.

During start and bad error overload periods the TBC1 uses averaging correction to allow video signal to pass through the system. During normal running it switches automatically to line by line correction. Deliveries should begin, they say, towards the end of the year.

Judging by the murmur of disgruntled voices, it would have been better if Ampex had come clean and just discussed their AVR-3 quadruplex video tape recorder straightforwardly — by pretending to review video tape recording in their IBC paper, they were accused of "audience trapping." But they would surely have got the large audience anyway, such is the interest in their new machine. First shown at the NAB convention (report, page 75 June issue), the AVR-3 uses higher modulating frequencies (super high band) to place unwanted modulation products outside the video band. In addition, a pilot tone of 1.5 times the subcarrier frequency is recorded with all the errors of the video signal to allow automatic error correction. Colour velocity error and equalization are continuously corrected, virtually eliminating banding.

Effectiveness of this error correction depends on the out-of-band pilot having the same errors as the in-band video information, but as P. N. Kelly and C. E. Urban pointed out in their following LWT/BBC paper, cancellation will not always be complete because of the poorer signal-to-noise ratio at the pilot frequency.

This s.h.b. + pilot technique results in a picture quality at 7½in/s that is comparable with that from a conventional 15in/s machine. And to ease the AVR-3s acceptability, Ampex have made it dual band (conventional high band 15in/s can be second choice), with automatic sensing and switching to the appropriate band and speed on replay.

The LWT/BBC presentation — which included a split programme demonstration with the upper half of the picture

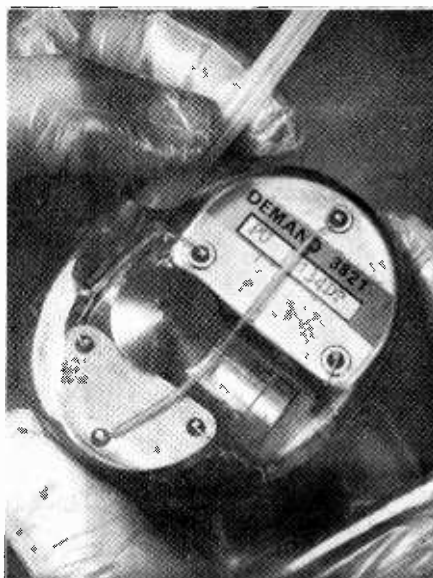
displaying normal 15in/s picture and the lower half from a machine modified for s.h.b. + pilot working at 7½in/s – admirably showed the capability of the technique over a number of tape generations. But it was a study of the potential savings in tape costs that occupied most of the paper. The authors said that although tape savings will be most beneficial to large organisations (the payback period being too long for organisations with a small number of v.t.rs), they are “by no means convincing.” Greater savings are likely to be had by changing to the 2-in segmented helical format, but this had disadvantages for organisations heavily committed to transverse recordings. “. . . a period of greater than five years is required to recover investment in equipment bought for transverse-track s.h.b. + pilot at 7½in/s” and could “only be justified when a machine replacement programme is necessary.” Further, it was very doubtful if even the largest organisation could justify this change for limited technological improvements alone.

The performance of s.h.b. + pilot at 15in/s, or segmented 2in helical machines for that matter, whilst representing a step forward has to be viewed against the “immaculate” results demonstrated by digital recording. “Broadcasters do not wish to find that a change of standards now prevents a real step forward in video and audio performance in several years’ time.”

Copsa anda computers

Police cars in the Rome force are being supplied with facsimile recorders which will receive and print out information from a central computer bank. The bank will contain details of all hospitals, fire departments, garages and other services in Rome's 10,000 streets, as well as records of police-car movements, operational data for special occasions, contingency plans for emergencies, and links to alarms in places like banks and museums. This information is made available to the police department's security, criminal and emergency sections via a number of video display terminals. Operators in those sections will be able to interrogate the database in the normal way, and the links to the high-risk alarms will indicate an emergency as it arises. Linked to the database is a microfiche retrieval system which enables a hard copy of graphical information to be obtained at police headquarters. It is this hard copy which can be transmitted via a radio link to the patrol cars, which will receive details of incidents from operators' terminals, having been allocated to these incidents automatically by the computer.

The £200,000 contract to supply the equipment has been won by Honeywell,



A nuclear battery at the core of a heart pacemaker. The device uses the heat from the radioactive decay of Plutonium 238 to generate electricity in a small semiconductor thermopile. The batteries, designed at Harwell, should last 20 years.

who supply a 716 minicomputer with 24 k words of main memory, a 7.5 million-word moving-head disk, four VIP7750 visual displays, paper tape equipment and interface equipment, and Muirhead, who supply a K400-MB/L facsimile scanner, K463 computer facsimile interface and 100 K460 B4 mobile facsimile recorders.

The equipment was originally developed for the Strathclyde Fire Brigade in Glasgow, a city which seems to suffer from an abnormally higher number of fires. Forty fire engines have been fitted with the Muirhead facsimile recorders linked by radio to twin Honeywell 316 minicomputers at divisional fire headquarters in Glasgow since the system was first put into operation in 1974.

The British police have, according to the Home Office, assessed the system by putting it on trial in Bristol and Sussex some years ago. More recently they set up a committee to study the use of facsimile devices but, according to the Home Office, they did not conclude that the use of mobile devices would be “cost effective”. Many police forces have installed video display units in stations so that, for example, they can obtain the whole past history of a motor car if they are provided with a registration number. This can then, of course, be relayed to patrol cars by radio telephone.

The national computer system for the British police has 300 SE Labs video terminals linked into a Burroughs computer. This provides ownership information and details of stolen vehicles and is about to be expanded to provide identification information on criminals, wanted persons and other police “operational data”. A contract

for a further 150 video display terminals has been placed with Delta Data Systems. The Home Office say, however, that individual police stations work on their own force-by-force computer system, not the national information data store.

● As a result of pressure from drivers of late night buses in London, buses are being fitted with radiotelephones. Redifon say they have just won a second contract to supply a further 600 telephones to the 208 already installed. Eventually some 6,000 buses will be at the end of a radiotelephone.

The London Fire Brigade are to get 500 u.h.f. hand-portable radio telephones from Burndept, who will supply two channel versions, one channel for single and one for two frequency working, or three channel units for supervisory officers with two single and one double frequency channel. Each fire engine will have a repeater to connect the hand units with the rest of the force via the main vhf network. A sub-audible tone makes sure that firemen can only activate the repeater on their own fire engine.

First p.c.m. relay

The first operational use of the BBC's prototype six-channel p.c.m. equipment was on August 22, when it was used to relay the first concert from the Edinburgh Festival. Although until now p.c.m. has been used to distribute programmes from the control centre at Broadcasting House to transmitters all over the country, via a 13-channel permanent pulse-code-modulated system, p.c.m. has not been used before to transmit an original signal from its source to the control centre. The point-to-point system developed by the BBC uses ten-digit words instead of the 13 used in the existing systems, since the existing systems use linear coding and the point-to-point system uses near-instantaneous digital companding (see *Wireless World* June 1975, p248). The 13 channel system therefore needs 487 kilobits per second per channel, giving an overall bit rate of 6336 kb/s, compared with only 341 kb/s per channel, totalling 2048 kb/s for the six channels, which coincides with the European standard first-order multiplex rate for digital transmission systems and the bandwidth of the links the Post Office is currently developing for digital transmission. Before developing near-instantaneous digital companding the BBC could only send four sound channels down such a link.

A paper in the *Japan Telecommunications Review*, published by the Nippon Telegraph and Telephone Public Corporation in July, describes a “High Quality Sound Program Digital Transmission System.” According to the authors, Tazaki, Matsumoto and Taka-

shima, four channels – in this case two stereo pairs – can be transmitted at a bit rate of 1.544 Mb/s, or 386 kb/s per channel. The system uses 13 bit linear coding, a seven-segment companding law, error correction, and a 32 kHz sampling frequency. While the coding is 13 bit linear, the transmission sample length is 11 bits plus a parity bit because of the digital companding law. The authors say that field tests have shown the system meets CCITT recommendation J21 and that, in subjective tests carried out with the Japanese Broadcasting Corporation (NHK) transmitting Jazz, a speech, an orchestra and a piano solo, scores of four or five on a five-mark scale were obtained on all programmes. Measurements showed that quantizing signal-to-noise ratios were less than 3 dB lower than the theoretical value, and the worst phase difference between channels was 3° at 14 kHz. "The system," the paper reports, "will be put into practical use in Japan in the near future." The development follows a rapid increase in the number of f.m. broadcasting stations in Japan.

Goodbye Goonhilly

Two new Post Office projects seem to demonstrate the diminishing importance of the once-famous earth station at Goonhilly Downs in Cornwall. The Post Office has placed a £6 million order with Marconi for an aerial at Madley, Herefordshire to take over the work of Goonhilly's Aerial One. The 32m dish will work to a satellite over the Indian Ocean and will handle all satellite communications between the UK and the eastern hemisphere between its coming into service in 1978 and the early 1980s. The Goonhilly aerial may eventually become an emergency standby. The new aerial is the first of three which may be needed at Madley early in the next decade, say the BPO.

The contract includes the dish, the aerial building, roadways, broadband transmitters and receivers, ground communications equipment and central and supervisory equipment. Although up to six aeriels could eventually be needed at Madley, the Post Office say they are limiting the first phase to three buildings and other site development work for three dish aeriels and associated equipment. "Today more than half of all telephone calls from Britain for places beyond Europe go by satellite. With an annual growth rate of more than 20%, international telephone calls are one of the fastest growing sectors of telecommunications. Last year, the number of calls rose from 78 million to more than 92 million. And, in the last eleven years, television transmission has grown from nine hours a year to well over 300 a year."

Goonhilly also provides 700 telephone

circuits to North America. On September 2 these were supplemented by TAT 6, the largest transatlantic cable laid to date, which is capable of carrying 4,000 simultaneous telephone conversations. The new cable runs from Rhode Island to St Hilaire, France. For contributing part of its cost of £100 million Britain will get 760 extra circuits between the UK and North America; these have been extended through northern France and over another new cable, also opened on September 2, supplementing the cross-channel microwave link.

TAT 6 is the ninth cable to be laid across the Atlantic since the first of only 36 channels in 1956. The previous largest cable was CANTAT 2 between Britain and Canada, completed in 1974 and providing 1,840 circuits. The cross-channel cable, on the other hand, is the first for 25 years. It has 2,500 circuits and is the first of two being provided jointly by the BPO and the French Ministry of Posts and Telecommunications. The second, to be built by ST & C, will carry 3,900 simultaneous conversations when it is brought into service in 1979. The microwave link these two cables replace now carries 5,500 calls, but the Post Office say that our communications with mainland Europe are doubling every four or five years.

The growth in telecommunications may be only one reason for these developments. It seems significant how much emphasis the Post Office's statements on these new routes stress the need to diversify our communications in case of "disruption." This may explain the apparently backward step of returning to a cable link between Europe and North America instead of launching new satellites. While satellites are expensive it may be that for some reason they have become more vulnerable. The Post Office's statement on the transatlantic cable says: "Because fishing fleets are exploiting ever deeper waters, the consortium decided to use armoured cable out to the edge of the European continental shelf. This makes TAT 6 the first submarine telephone cable system to have its armoured section laid to depths of up to 2,000m (1,000 fathoms)."

Hilltop profession?

Of 500 UK candidates whose entries for the two parts of the CEI exam were handled by the Institution of Electrical Engineers, 83 passed, according to the IEE's annual report for the year to March 31, 1976. Most, 463, took the part two examination. But the failure rate for overseas candidates was even higher. Of 717 entries, 489 for the part one exam, only 25 passed. The annual report, commenting on these results, said: "The success rate was about the same as in previous years."

More optical fibre trials

The Post Office has ordered 21 km of two strand optical fibre cable worth £76,000 from BICC to be used in assessing the BPO's experimental systems and equipment developed at its Martlesham Research establishment. An 8 Mbit/s 12 km link will be built between Martlesham and the Ipswich telephone exchange via a repeater at Kesgrave. Another cable, this time operating at 140 Mbits/s, will connect Martlesham and Kesgrave, a distance of 5 km.

As we reported in August, STC will conduct a field trial along the 9 km route between Hitchin and Stevenage with a 140 Mbit/s cable. In a recent article in *Electronics Weekly* Mr Peter Burke of ITT, STC's parent company, said that although optic cables were generally reliable and operated with particularly few servicing problems, "costs are high, depending a lot upon the specification but, for example, a 10 Mbit/s duplex link over 200m might cost £1,500, and a duplex colour TV link over 500m perhaps three times this." This had limited the number of applications of fibre-optic cable but costs were quickly coming down. He quoted a cost for a four fibre cable at about £6 per metre.

Yet Corning glass, who have had an agreement with BICC and Plessey for the use of Corning's Doped Deposit Silica process since 1973, claim that optical cabling is now competitive in price with conductors of high quality coaxial cables at a US price of \$1 a metre, and have offered to take production orders at ten cents per metre.

STC are understood to be reviewing their costs, however, and say that in any case the cost of the cable depends a great deal on its quality.

Their Hitchin-Stevenage link may be installed as early as March next year, they say. Meanwhile Rediffusion have installed 1.5 km of two strand BICC fibre optic cable to replace one which supplied television pictures to cable television subscribers near Hastings. The old cable had become silted and wet, say Rediffusion. BICC claim this is the first commercial order from the private sector.

Bell Labs and Western Electric are also evaluating fibre-optic communications systems in Atlanta and have installed 2,100 feet of half inch cable containing 144 lightguides around the laboratory. By joining various fibres at their ends transmission paths several miles long have been formed. The cable, say Bell, could carry up to 50,000 calls. Western Electric has put several million dollars into lightguide development since 1972. In 1975 Western supplied Bell Labs with 500 km of lightguide and the 1976 target is 1,500 km.

Continued on page 76

Letters to the Editor

SURROUND SOUND BROADCAST

I was very pleased to read in News of the Month, *Wireless World*, September 1976, your mention of Radio Clyde's quadrasonic broadcast. It was also nice to see publicity being given to Capital Radio on the first alleged "simulcast" on commercial television. However, I regret to inform you that the first simultaneous broadcast was by Radio Clyde and Scottish Television on the 14th October, 1975. This was on the occasion of Scottish Opera's first performance to mark the opening of their new opera house, the Theatre Royal. The broadcast, of *Die Fledermaus*, was covered by both companies in its entirety, live. Capital can possibly claim with Weekend Television the first simulcast where v.t.r.s were synchronized with multi-track sound recorders but, in my opinion, not the first simulcast.

John Lumsden,
Chief engineer,
Radio Clyde.

CITIZENS' BAND IN UK

I was saddened that the previously high standard of argument over the Citizens' Band issue should be lowered by the tone of the letter from Mr J. G. Kelly in your September issue.

Mr Kelly's personal opinions on the merits of other people's legitimate pastimes have no place in reasoned, logical argument. Indeed his whole letter reeks of the naivety and selfishness which he claims to find so distasteful in others. Fortunately he reveals his apparent lack of research into the subject, not only by missing the point of every correspondent he quotes, but also by not even attributing his helicopters to the correct author (May 1976).

As a professional communications engineer who has, at times, been involved in the design of modern digital radio control equipment, I can assure Mr Kelly that in such areas as spurious transmitter outputs and receiver bandwidths, RC equipment by necessity must exceed the relatively low standards set by CB manufacturers. Indeed, I note with some amusement that in the September issue, in the "World of Amateur Radio" column, that the FCC is proposing to clamp down on spurious local oscillator emissions on equipment working in the 26-28MHz region.

The domestic radio control industry supports seven major manufacturers, and two Japanese imports. This is a somewhat different balance to that normally found in the world's major CB markets.

However, despite all the foregoing I am in favour of establishing a Citizens' Band in the UK. It does perform a useful community purpose, especially in remote areas, but why must it be on 27MHz, when there are far more suitable frequencies available? It is not necessary to rob Peter to pay Paul, Mr Kelly.

Before long, the old 405-line television channels will be defunct. One such channel contains enough bandwidth for nearly *three hundred* CB channels, with all the advantages generally associated with v.h.f. operation. The main argument against such a plan is that all the currently available CB equipment is on 27MHz. However, it is also predominantly Japanese, and it would be extremely naive to believe that our manufacturers could compete with an industry that has successfully saturated the American market. By placing CB on v.h.f., as indeed the Americans are planning to do, our manufacturers would at least be placed on an equal footing.

Also in the September issue, Mr Flood makes the excellent point that in Germany, CB and RC coexist peacefully. This is largely because when 27MHz was opened up for CB use, the German authorities were very generous in the allocation of alternative frequencies in the 35 to 40MHz region, exclusively for radio-control. These frequencies are close enough to 27MHz to allow economic conversion of existing equipment. Look around, Mr Flood, and you will find very few people still using 27MHz RC gear because it is now completely impractical. Fortunately, the German authorities realised that whilst RC interference on CB is merely an annoyance, CB interference on RC is invariably disastrous. The modelling fraternity have an unsurpassed safety record in the field of outdoor leisure activities, and must be kept separate from CB if this is to be preserved.

P. Christy,
South Harrow,
Middlesex.

THE INVENTORS

For some time we have been investigating the possibility of establishing an innovations investment fund, the function of which will be to provide financial backing to new ideas and inventions.

John Dwyer's article in the August issue quite accurately identifies the difficulties faced by innovators and the attitude of the managers of conventional sources of finance to new technical and commercial ideas. Whatever the underlying motivation for these attitudes, and Dwyer points up most of these, the fact remains that the reason innovations are so seldom made into commercial ventures in the UK is the unavailability of finance. We believe that the principal reason behind this situation is that innovation involves speculative investment; speculative investment is akin to gambling, and gambling is something investment managers do not want to do. Their responsibility is protecting other people's money (private or public). As individuals, however, using our own money, we are prepared to gamble. Yearly the national

figures for betting, Premium Bonds, football pools etc. rise; yet no mechanism exists to enable the small gambler (speculative investor) to put his money into new ideas and into genuinely embryonic companies. The structure and objective of the fund we envisage will provide this mechanism and will provide the individual investor with the option of backing the innovation(s) of his choice, or of spreading his risk across a spectrum of innovations.

We believe that a fund of this type will not only benefit the speculative investor and innovator but will, more importantly, benefit the nation by making it possible for this country, as opposed to the USA etc., to gain from the commercial exploitation of our national inventive genius.

The setting up of the fund, however, poses numerous difficulties, one of which is the likely response of the public, and we should appreciate the opportunity of gauging this response by asking your readers to write to us (name and address is not necessary) indicating whether or not they would invest in such a fund and how much they would invest (from £5 upwards).

We must make it clear that at this point we are only conducting a survey. This is not an invitation to your readers to invest, nor is there any obligation on the part of those who write to us to invest in the fund, at any time, if and when it is established.

K. R. Williams,
J. Hempstead Associates Ltd,
33 Fortress Road,
London NW5 1AD

It is difficult to be called a genius (August issue, p.34), then to be publicly discussed and mentioned over the years without being offered the opportunity of expressing one's own view first hand, either to the establishment or to the public. There are, as I see it, four aspects to the matters with which I am involved and I believe that to others these four things are inextricably confused.

Firstly, there is my theory which has remained basically unchanged for the past seven years although I will admit that it was incoherently expressed at first. How can one learn to communicate in a particular language if the natives refuse to speak or even acknowledge one's presence?

Secondly, there is the experiment which I devised to test my theory. In essence this is the "Eiffel tower" gyroscope toy turned through 90 degrees to avoid the unwanted effect of gravity in the axis chosen for study. There is no doubt whatever that the centre of mass of the device moves along that axis without the presence of an impressed force acting along that axis. *That* is new science. A variant of this experiment was shown to my dear friend Eric Laithwaite and the centre of mass of the machine finished outside the original physical boundaries of the experiment. The original experiment was shown on "Tomorrow's World".

Thirdly, there are the attempts which have been made to turn the small and rather limited effect into a continuous and smooth one. Two have succeeded but in a pulsating rather than smooth manner. A vertical version was shown by Eric at the infamous (?) dissertation. The other, horizontal model, was shown by me to Rosser and Hawker Siddeley, who had the machine for about 18 months. Their technical report concludes:

"Within the confines of accepted classical mechanics, the proposed space drive will not convert angular momentum into linear momentum.

"It is undeniable that the apparatus demonstrated by Mr Jones translates along a near frictionless surface. This behaviour must be attributed to the necessarily limited build standard and test conditions. It is considered that a device constructed to higher accuracy and tested under controlled conditions would demonstrate a motion closer to that predicted i.e. zero net translation."

I now know that their first statement is true but why did they not reproduce the machine shown instead of one which conformed to their analysis? I freely admit that my first explanation for the machine was wrong but that does not alter the fact of the machine itself. This machine was also seen by a member of the "Tomorrow's World" staff who, picking it up, said "I feel it pulsing its way along through space" but that is subjective and therefore unacceptable to science. It is the attempts at smooth and continuous thrust which have so far failed, but remember that we venture unknown territory.

Fourthly, there is the attitude of the establishment which may be summed up by the phrase "but you must understand, it is only we who know about these matters". A further example lies with the German patent examiner. We visited Munich to argue our case, since the patent was to be rejected on the grounds of violating physical laws. Through much argument we almost gained our objective but in order to be certain a model was produced for demonstration. Upon seeing it the examiner stated "I now see that you violated the laws and must therefore reject on those grounds". When leaving the building I am pleased to remember that my good friend F. Cousins said "I know it was rejected but alongside those people I feel 14 feet tall".

Eric Laithwaite has demonstrated that he is able to carry a wheel (18lb) on a shaft (6lb) upon his little finger at arms length and cause the wheel to rise and fall, its axis remaining horizontal, at will. The engineers present suggested that either he was very strong, like his son Denis, or that the demonstration was "subjective experiment" and therefore not to be accepted.

I leave your readers to form their own conclusions.

It would seem that the establishment demands innovators at a time when the human species needs inventors.

Alex C. Jones,
M.V. "Juno",
Poole.

REPAIRING SEMICONDUCTORS

When an expensive power transistor ceased functioning for no obvious reason I decided I had nothing to lose by opening it up. I therefore sliced off the top surface of the T03 can to investigate. The hacksaw blade had just touched one of the connecting leads inside but it was clear that the cause of the failure was a flying lead from the transistor chip having become detached.

In the absence of an ultrasonic welding kit I investigated whether I could reconnect the loose lead and found to my surprise that the transistor terminal pad was quite easily solderable. I resoldered the loose lead, glued in the sawn-off lid with epoxy resin, and the transistor has been in service ever since.

Just recently I had a very expensive integrated circuit in a voltage regulator in an alternator which ceased to work correctly after someone, presumably accidentally, made a wrong connection. With nothing to lose, I used a thin-bladed knife to loosen the glue along three sides and to prise off the lid. Inside was an elegant array including what looked like a power transistor, a power diode, an integrated circuit chip, a capacitor, and what looked like several power resistors. Each of five main terminals had a flying lead of what looked like 10-amp fuse wire to a small pad in an insulated surface: all except one, that is. In the gel coating near the last pad there were a lot of black specks, which I assumed were the burnt-out remains of the fifth flying lead. Fortunately the circuit semiconductors and resistors showed no signs of overheating. I assume that this was due to the greater heat capacity produced by the components being closely bonded to the heat-sink. Once again I was able to tin the terminal pad and the terminal with a hot soldering iron and a piece of fuse wire to link the two. I then smoothed out the gel to protect against moisture. Evo-stik on the lid completed the repair and the unit is now back in its alternator and fitted in the vehicle.

Obviously not all transistors and i.c.s are worth attention when they fail. Of those which are worth attention some will be damaged beyond repair. But if the method can successfully repair a £15 i.c. or a £3 power transistor, and save the delivery time of weeks or months for some components, it is worth spending 10 minutes to have a look inside and another fifteen minutes to repair and put back together an expensive semiconductor device.

A. F. Jervis,
Bournemouth.

CURRENT-DUMPING AUDIO AMPLIFIER

The "distortionless" character of the current dumping (c-d) audio amplifier is said to be dependent on a bridge balance. Presumably, this balance is like any other circuit condition in that it can only be set up with a tolerance which can be made smaller as the cost of the arrangement increases.

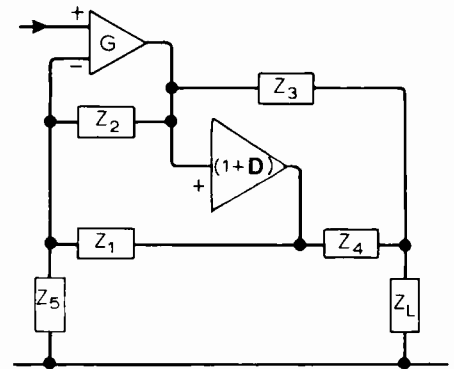
It therefore seems unrealistic to compare a theoretical balanced bridge with a practical conventional feedback arrangement (as some of your correspondents have done), to evaluate the distortion performance of the c-d circuit. A fairer approach would be to ask how badly the distortion performance of a practical c-d circuit, using reasonable techniques, would be affected by unbalances to be realistically expected, and how it would compare with the performance of a comparable conventional arrangement.

The two arrangements are directly comparable in principle. If for comparison we use a negative feedback arrangement around a distorting amplifier of gain $G(1+D)$ where G is a linear gain factor and D a distortion operator, we can take the closed-loop gain expression.

$$\frac{G(1-D)}{1+FG(1+D)} = \frac{G}{1+FG} \cdot (1 + \gamma D - \gamma n D^2 + \gamma n^2 D^3 \dots)$$

where F is the feedback fraction,
 $n = \frac{FG}{(1+FG)}$ and $\gamma = \frac{1}{(1+FG)}$, and derive an

expression of analogous form for the following c-d circuit configuration:



in which the class A amplifier is assumed linear with gain G , the current-dumpers unity gain with distortion $(1+D)$, and both amplifiers assumed to have zero output impedance.

The closed-loop gain is

$$\frac{L(1+\beta D)}{K^*(1+\alpha^* D)} = \frac{L}{K^*} [1 + (\beta - \alpha^*) D - (\beta - \alpha^*) \times (\alpha^* D^2 + (\beta - \alpha^*) \alpha^{*2} D^3 \dots)]$$

where $L = \frac{Z_1(Z_3+Z_4)}{Z_2 Z_4 + Z_2 Z_3}$, $\beta = \frac{Z_3}{Z_1+Z_2}$,

$\frac{1}{K^*} = \frac{G}{1+GK}$, $\alpha^* = \frac{\alpha GK}{1+GK}$, $\alpha = \frac{Z_2}{Z_1+Z_2}$

and $K = \frac{Z_3(Z_1+Z_2)}{Z_1 Z_2 + Z_2 Z_3 + Z_3 Z_1}$.

The closed-loop gain expression is of similar form for both configurations, except that the distortion coefficient γ for the conventional arrangement is replaced by the difference $(\beta - \alpha^*)$ in the case of c-d.

It is apparent that the c-d as well as the conventional configuration produces high-order distortion as a result of applying feedback. But whereas with the conventional arrangement the distortion coefficient γ can only be minimised by raising G , the right-hand half of the bridge in the c-d configuration (theoretically) allows complete cancellation of the distortion by making $\beta = \alpha^*$ exactly. This balance equation expands to

$$\frac{1}{1+GK} + \frac{Z_1}{Z_2} = \frac{Z_4}{Z_3} \left(1 - \frac{1}{1+GK} \right)$$

and reduces to the familiar $Z_1 Z_3 = Z_2 Z_4$ as $G \rightarrow \infty$.

We can get a rough comparison between the performance of a slightly unbalanced c-d bridge and a conventional arrangement if we look at Mr P. J. Walker's article (Dec. 1975, p.562) and see that in the Quad 405 circuit the real parts of $Z_1/Z_2 + 1/(1+GK)$ and Z_4/Z_3 are of the order of 0.01. Assuming the bridge initially balanced, a perturbation of 5% in any of Z_1 to Z_5 or G leads to a residual $(\beta - \alpha^*)$ of

the order of 0.0005. Other things being equal, this indicates the same distortion performance as a conventional arrangement in which G is 10,000 and $FG = 2000$, i.e. $\gamma = 0.0005$. The difference is that the c-d configuration does not call for any particular value of amplifier gain or loop gain to reach this performance, provided the balance conditions are adjusted to take the finite G value into account. The Quad design appears to use values of the order of 1000 and 200. At the assumed 5% tolerance, therefore, the c-d configuration allows economy of amplifier gain and loop gain for the given distortion performance. This should evidently recommend itself as a worthwhile advantage, accompanied by fewer feedback loop stability problems.

However, other things may not be equal. The unbiased current-dumpers may generate more distortion than a conventional class-B transistor pair, thus calling for more accurate cancellation. 5% may not be an easily achievable tolerance for the bridge balance, particularly where Z_2 and Z_4 are reactive. It can be seen from the expanded balance equation that a finite G represents (from the point of view of bridge balance) a load resistance in parallel with Z_2 , so that even where Z_2 is purely capacitive, a resistor is needed in series with the opposite complementary arm L_4 . This balancing resistor is only a fraction of an ohm, so that its 5% tolerance will be in the order of milliohms, possibly comparable with wiring and joint resistances. Of course the accuracy of bridge balance also depends on the value of the amplifier gain G , not the best of well-defined or drift-free parameters in practice.

Furthermore, when reactive bridge arms are used, as seems essential in practice, unbalanced imaginary components of $(B - \alpha^*)$ may be present and do more harm than would appear likely from the high cut-off frequencies which the reactances introduce. As pointed out by Mr P. J. Baxandall (July 1976, pp 60-1), the amplification of a mid-frequency sinusoidal signal by the c-d arrangement requires handling of a non-sinusoidal and hence wide-band signal within the feedback loop. Thus reactance balance may turn out more critical than otherwise expected, and difficult to achieve where there is phase shift at high frequencies in the class A amplifier and hence an imaginary component of G to complicate the balance equation. Again, the output impedance of the dampers is unlikely to be negligible in relation to Z_4 .

It would be of interest to have some practical figures for the importance (or otherwise) of these expected sources of disturbance in the Quad commercial realization of this elegant new design. It is no doubt a worthwhile advance, but "distortionless"? The c-d circuit does away with the unattainable criterion of infinite loop gain for distortionless output, as with the conventional negative feedback arrangement, but replaces it with the equally unattainable criterion of perfect accuracy of bridge balance. The results of practical deviations from the theoretical requirements in the two cases are qualitatively the same
T. C. Stancliffe,
London S.W.6.

Mr Walker replies.

No indeed we don't claim to make distortionless amplifiers. The term – in so far as it has been used – is intended to indicate that there is a 'theoretically accessible' state where the output stage distortion will cancel

to zero, without calling upon infinite loop gain. Compared with straight overall feedback, the barriers preventing us reaching perfection are of a fundamentally different kind and, as Mr Stancliffe rightly points out, we want to know whether this change in kind can be applied to advantage in a practical amplifier. We have chosen to apply the technique to amplifiers with zero bias output stage because if we can overcome the fundamental problems of these amplifiers and raise their performance to impeccable standards then they emerge as essentially "right" and all the rigmarole of biasing becomes a thing of the past.

In a zero bias amplifier there is a no-man's land or backlash region between one output transistor turning off and the other turning on. It is to be hoped that the driver transistor transverses this gap as quickly as possible and to help it out it is usual to find a resistor bypassing the output stage so that there is some current to the load during this transition period. All such amplifiers suffer from the fact that the forward conductance during the transition is less than the forward conductance when one or other of the output transistors is operational, so that the whole transfer characteristic has a portion in the middle with a different slope to the remainder. In order to produce an acceptable standard of performance the bypass resistor is made as low as possible consistent with the driver's ability to supply the extra current required and heavy overall feedback is applied. Both of these manoeuvres reduce the change of slope in the transfer characteristic. There are several well respected and excellent commercial amplifiers of this type available, particularly in the high or "super power" class.

Current dumping is really a simple means of adapting such an amplifier whereby the two slopes are separately defined and can be made equal by the suitable choice of a few passive components. With Mr Stancliffe's criterion of a total error of 5% in these components the change of slope will be reduced 20 times without calling on any increase of feedback. Evidently the distortion will fall by a similar amount!

In practical amplifiers aimed at very low distortion there can be – and usually are – other factors which may determine a lower limit to the distortion. In all class B amplifiers, for example, parts of the circuit and power supply carry heavy current highly distorted signals (half sinewave for a single tone signal). The minutest coupling between these and other parts of the circuit which should be pure quickly builds in distortion which no amount of d.c. balancing will remove. Zero bias and c.-d amplifiers require parts of the circuit to have wide bandwidth and very fast slew rates which may not be fully achieved. Output transistors do not turn on or off as simply as one would wish.

These factors are really a matter of detail design and therefore difficult to quantify. Nevertheless, the 26dB (20 times) improvement is there for the taking and nearly for free. With care, most of it can be realised in a practical amplifier.

RECEIVING WEAK TV SIGNALS

I read with interest W. H. Jarvis's article (*Wireless World*, July 1976) on receiving weak TV signals. I was particularly intrigued by the attenuation found in wooded areas –

it might be instructive to look further into the mechanism of this. I think it likely that the main cause of attenuation is not scattering by the leaves but absorption due to the vertical conducting path provided by the sap, which rises in the spring as the tree comes to bud, and falls during the autumn as the tree begins to shed its leaves. If this is so, the increase in attenuation should be greater for vertically polarised signals, and should become apparent rather earlier than would be the case if the loss were purely due to scattering.

J. Sinclair Turnbull,
Glasgow.

Mr Jarvis replies:

Our experiments showed that scattering by foliage is unlikely to be the main explanation of the phenomenon. We suspect that the average conductivity of a wooded region is greatest in the vertical direction in all seasons, and that the rise and fall of sap with season makes very little difference to this conductivity.

Nevertheless we suspect some degree of loss due to scattering from foliage since, with a given aerial, IBA signals from Blackhill vary around 1 to 10 μ V in summer, and 10 to 50 μ V in winter. Several peaks and minima occur per minute, and the variation is deeper and more rapid in windy conditions. Presumably the IBA signals on 205MHz are more susceptible to scattering losses than those from the BBC (Kirk o' Shotts) on about 55MHz. Both signals reach us from almost the same direction, and have to diffract over a hilltop lined with conifers.

We have not noticed the correlation between sap rise and attenuation suggested by Mr Turnbull, but I am sure the possibility is worth pursuing.

It is a pity that foresters, mountain rescue teams, etc., are more or less obliged to use vertical polarisation for communication in areas such as ours!

STEREO IMAGES

In these questions of audibility of phase distortion etc. the writers do not consider that a stereo image produced by loudspeakers, or headphones does not behave as the original sound source does. If the listener moves his head to the right the stereo image also moves to the right. In reality the image should appear to move to the left. Surely this effect, which does not occur naturally, can only cause confusion in the direction sensing part of the brain, and blur the image produced.

P. J. Churchyard,
Grantham,
Lincs.

Audio moves

The tendency for Harman International to do their own marketing, pointed out in our news columns in August though denied by Harman, has been underlined by Metrosound's loss of the Ortofon agency. Ortofon was acquired by Harman in June. Metrosound have had the agency for fifteen years. Ortofon will now be sold through Harman's subsidiary, Tannoy Products Ltd at Canterbury Grove, London SE27. Shortly after the announcement, Lasky's announced that they would be stocking Harman Kardon equipment from September 27.

Mobile radio communication

V.h.f. and u.h.f. radio communication in the UK

by D. A. S. Drybrough, B.Sc., M.I.E.E., *Drybrough Communications Ltd*

It looks as if 1976 is a watershed year for mobile radio. Since its commercial inception soon after the second world war, speech has been the main vehicle for the conveyance of intelligence in these systems though data transmission, in the shape of selective calling signals, has been in minor use for many years. This year data does seem to be making significant progress, spurred on by the need for higher efficiency in the use of radio channels and the saving of manpower. Similarly, after a considerable period without changes to authorized channel bandwidths, there is now a move to narrower channels, at least in the lowest v.h.f. bands, affording more space for new users. To the same end, new methods of modulation are being investigated and field-tested. However, such new methods are unlikely to sweep away established modes in the very near future because of the high cost involved in any changeover.

Growth in the mobile radio services is shown in Fig. 1 which has been derived from official statistics, as recorded at the end of each year from 1950 to 1975. Sales and service records of the main manufacturers suggest that these figures are pessimistic, implying a good deal of unlicensed operation or unreported increases to initially small systems. The official statistics do not differentiate between a.m. and f.m., and so no comparison of the numbers of each type in use is possible. Statistics for the police and fire services are not available in the same form but their units total about 45% of those in use in the private services. The rate of growth for land mobile stations remained around 15% until about 1970 when it fell slowly to about 10%.

Despite a reduction in the number of large vessels registered in the UK in recent years, the number of maritime mobile private licences has risen by about 5% per annum, due mainly to the increasing use of mobile radio in small pleasure craft. From UK population statistics, it is estimated that the proportion of all UK registered motor vehicles fitted with mobile radio is about 1%. Similarly, the number of personal portables per head of adult

Mobile radio communication systems operating in the v.h.f. or u.h.f. bands are widely used in the UK for short-range services, particularly in the land mobile field. Developments in equipment and systems for such services are reviewed and selected units and installations briefly described. The design of selected sections of equipment and the estimation of range are discussed together with problems of frequency selection, interference and noise. The two widely-used systems of modulation are compared with recently-proposed types.

Fig. 1. Growth of land and maritime mobile radio services in the U.K. Comparing these official figures with manufacturers' records suggests a good deal of unlicensed operation.

male population is around the same percentage, having risen from virtually zero in 1963. Thus, penetration of the total vehicle and personnel markets is still small, even allowing for the high proportions of vehicles and people unlikely ever to require mobile radio. Saturation should not therefore be a factor adversely affecting growth for some time.

Except for the aero and parts of the land and maritime bands allocated to single frequency, mainly portable, services, main bands are divided into smaller sub-bands on a two-frequency, go-and-return, basis. Use of this method of frequency allocation, which at first sight looks wasteful except for full duplex systems, has contributed to efficient usage of the available frequency spectrum by minimizing interference at base stations.

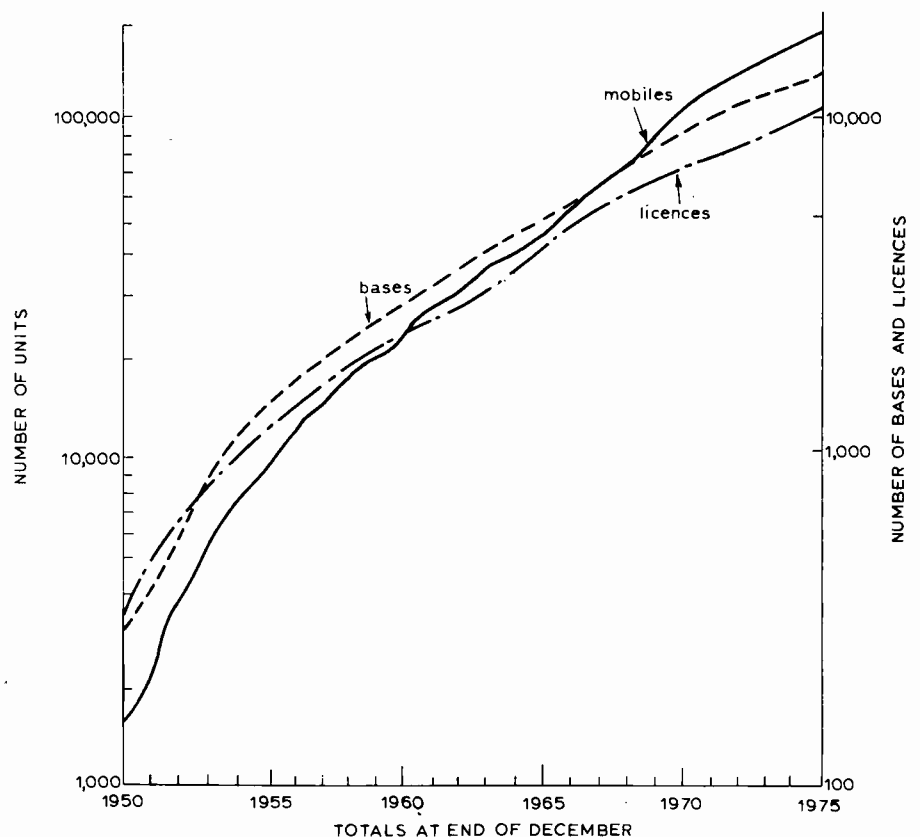


Table 1.

Frequency bands

The frequency bands normally available to the mobile radio services.

Low band	land services	71.5 to 88MHz
Police and fire bands		80 to 85MHz
		97 to 102MHz
Mid band	land services	105 to 108MHz
Aero band	aero services	108 to 136MHz
Mid band	land services	136 to 141MHz
Maritime band		156 to 165MHz
High band	land services	165 to 174MHz
u.h.f. band	land services	425 to 470MHz

Table 1 shows the frequency bands available for each type of service. The land mobile services use narrower channels in the main to accommodate larger numbers of stations than the other services. The ratio of base station numbers to total available channels has remained within the fairly narrow limits of about 8 to 17 and was about 11 at the end of 1975. Thus there is still some time available at the present rate of increase before the historical maximum of 17 per channel is reached. However, if no channel splitting or other means of increasing spectrum occupancy is adopted before the upper limit is reached in a few years time, then new slices of spectrum totalling about 44MHz would be required to reduce channel occupancy to the historical minimum of 8.

Channel widths have been reduced over the years from the very early values of 180-200 kHz to present standards of 12.5 kHz for land-mobile systems in the v.h.f. band and 25 kHz for most other channels. Acting on the advice of the Mobile Radio Committee, set up originally by the Postmaster General to study and report on fre-

quency-allocation problems, each reduction in channel width from 50 kHz downwards was accomplished by halving the width of existing channels and inserting new channels, centred at the edges of the old ones, thus retaining the possibility of continued operation by older equipment in the original channels if no interference were caused thereby. The changeover of equipment standards extended in each case over a period of five years but changes to 25 kHz in the 'high' v.h.f. band were begun before those to 50 kHz were completed. Some equipment in areas of low activity was not changed until obsolescence forced the purchase of new units to later standards. A proposal to split the u.h.f. 25 kHz channels into two was investigated in 1972 and rejected because of inadequate frequency stability of the equipment in use, and in immediate prospect, at that time. Recently, demonstrations of a.m. systems working in a channel width of 6.25 kHz have been given* but there is, as yet, no concerted agreement to move to these smaller widths.

Land mobile services

Commercial. The typical land mobile unit is a low-powered transmitter/receiver, operating in the two-frequency mode to a single, locally-controlled base station of similar power. It is powered from the 12-volt vehicle supply and operates in one of up to ten channels, pre-tuned and crystal-controlled. The transmitter output power is usually between 5 and 10 watts and the receiver can deliver an audio output power of 1 to 5 watts for an input of $1\mu\text{V}$ or slightly more. The whole unit is fitted in a small, well-designed case which can be mounted in a position easily accessible to the driver or pas-

* See page 57, September issue.

A. Public land mobile radiotelephone (Storno)

senger. A hand microphone, sometimes of the noise-cancelling type, is fitted with a press-to-talk switch and is used to modulate the transmitter. A coaxial cable couples the set to a vertical aerial, mounted as high as possible on a metal ground plane. Base stations are less standardized than mobiles but generally use the same r.f. units, mounted in a cabinet with local controls, microphone and loudspeaker. When the position of the base station is a poor one from the propagation point of view, extended or remote control units may be added to allow the base unit to be moved to a better site. Rented or private lines are then used to connect the radio equipment to the operating point. Higher-powered versions of these simple units may be installed when wide coverage is necessary. The average low-power system can cover about 2000km² and up to about 60 mobiles can be accommodated in one channel when unskilled operators are used at the base station, rising to over 100 for users such as taxis. U.h.f. installations differ from v.h.f. installations mainly in their aerial systems and channel widths. The operator generally notices a greater freedom from man-made noise, but a smaller coverage area with well-defined shadow areas where signals disappear.

Police and fire installations. The police and fire services use equipment basically similar to that in the commercial services but with additional facilities to suit their special needs. Multi-channel sets are standard for v.h.f. mobiles, ten channels being normal. Sets are specially designed for either a.m. or f.m., with easy conversion from 25 to 12.5 kHz channel width. A public address facility is also normal. The police and fire systems are generally large and complex, integrating the radio with telephone, telex, u.h.f. and other communication means in special control stations, each covering a county. Fire services have traditionally shared the police frequencies but are now tending to move to separate channels as traffic increases.

The police also operate short-range u.h.f. services, based on local, divisional or similar headquarters and used by policemen on the beat on foot or in Panda cars. In country areas, the v.h.f. and u.h.f. systems are linked to provide a wider coverage for the latter. Single channel (recently increased to three-channel) portable sets, fitted in small plastic cases are used and base stations are sited for just adequate coverage to these sets.

Other civil systems. The nationalized power industries make extensive use of mobile radio in large area systems with centralized control for general and emergency communications together with local control for normal working. Amplitude modulation is used in the mid-band. Equipment is similar to that



used in commercial services. Some large systems have multichannel radio links between sites and these carry both voice and data signals when necessary. Other large users are the ambulance services, transport services, water boards the Forestry Commission and county surveyors and engineers. The railways use short-range sets to cover shunting yards, station concourses and emergency operations and are planning a country-wide network. The Post Office have their own locally-controlled services to their vehicles and the airport authorities use mainly u.h.f. systems at the main airports for ground control, fire and safety services. Message-handling services operate widespread systems, linked via operators to the telephone system. Selective calling is widely used to minimise irritation and enhance privacy in mobiles and a paging service is sometimes offered as an adjunct to the full mobile radio system.

Mobile-v.h.f. public services. The Post Office operates several public mobile radio systems covering the more densely-populated regions of the UK. The first such system was installed in Lancashire in 1959 and was followed by a similar system in the London area. These systems have been brought up to date to provide a faster service to more subscribers and more areas have been added, each with a capacity of some thousands of mobiles. A public service is also available to shipping from stations located around most of the coast of Britain but no such service is available to aircraft.

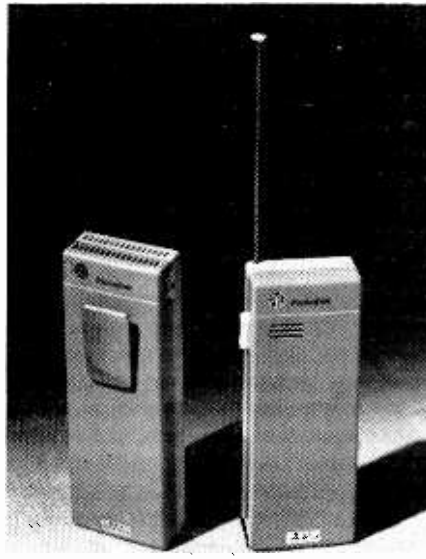
Maritime services

The equipment used in the normal commercial maritime v.h.f. services is basically similar to that used by the land services but may be fitted in more robust splashproof cases and is nowadays always f.m. Multichannel operation is normal and a low-power switch is mandatory to reduce interference in crowded estuaries and ports. Both single and two-frequency operation is possible and 25kHz channel widths are still in force.

In Britain, the coastguard service maintains constant watch on two v.h.f. channels with a wide coverage round the coasts. Rescue services are also co-ordinated on these channels which are shared with the pollution control service of the Department of Trade and Industry. Trinity House and equivalent controlling bodies for lighthouses and lightships use maritime sets in their more localized systems.

Aeromobile services

The major responsibility for providing services in the aeromobile frequency band rests with the CAA who provide communications to aircraft in flight over the whole of the UK flight information region through the National



B. UHF Pocketphone (Pye)

Air-Traffic-Services control centres at West Drayton (London Control), Prestwick (Scottish Airways) and Manchester (Manchester Control). Multiple a.m. base stations, usually with transmitters and receivers installed at separate sites spaced a few kilometres apart, transmit simultaneously on the spaced-carrier system to aircraft flying along controlled airways and advisory routes at altitudes between 900 and 14000 m, and down to ground level at airport terminal areas. Transmissions from the aircraft in reply are in the same channel, on a single-frequency-simplex basis, and are simultaneously received at the base stations from which they are relayed back to the control point where the best is selected.

The use of single frequency simplex working, following international agreement, has posed many problems in the design of stations and equipment and great care is necessary to avoid the generation of interference to low-level wanted signals when much stronger signals are present in nearby channels.

NATS also provides aeromobile communication facilities at the majority of airports not under their direct control. A small number of private systems, operating in the aeromobile band, are used for operational control purposes by the major operating companies. In some cases they are extensive and complex with links covering flight paths over the whole of Europe. The units fitted in civil aircraft are multichannel, auto-tuned transceivers, sometimes incorporating a frequency synthesiser instead of banks of crystals to cover the large number of channels now available at 25kHz spacing. Communication, once established, is assumed certain and the radio is operated by the crew using agreed standard codes to speed up messages and make full use of the channels available in each area.

Savings

The savings effected by the use of mobile radio vary greatly with the type of user, ranging from the saving of life in ambulance, fire and similar services, to a proportion, variously quoted as 10-20%, of the running costs of a transport system. Many services are now so geared to the use of radio for communications that they would collapse if the radio were removed. In such instances, the benefits of radiocommunication may not be immediately apparent to an accountant, but they are vital to the firm. The saving in expensive fuel imports should not be overlooked, since the better use of vehicles through closer control of routing and reduction in unprofitable journeys saves fuel, and Brinkley has estimated that the annual saving in the present cost of running the UK fleet of vehicles, excluding manpower costs, could be £80 million for a reduction of only 1% in distance covered. This greatly exceeds the total annual output of the mobile-radio industry and is a very cogent argument for more intensive use of its products.

Developments in design

There is no general agreement on the type of modulation to be used in the various mobile-radio services, although the available frequency bands and the range requirements are similar for many of them. In most cases today, the choice between the two main types, amplitude modulation and frequency modulation, is more likely to be made for historical than for technical or even commercial reasons, especially in the land-mobile services for which channel widths have been reduced to 12.5 kHz and much of the advantage in signal/noise ratio possible in wide-deviation f.m. systems has been lost. Amplitude modulation is used exclusively, by international agreement, for the aeromobile services and still preponderates in the v.h.f. land-mobile bands. Frequency modulation is used exclusively for the international maritime services and for the land u.h.f. services and is claimed to be on the increase in the land v.h.f. bands.

Despite these disagreements over type of modulation, designs for equipment for similar purposes are fairly uniform, with greater mechanical and presentation differences than circuit differences. Fairbairn reviewed design aspects in 1954, and the features he described then are, for the most part, valid today. Congestion has raised additional problems of selectivity and signal handling in receivers, shifting the emphasis from the maximum possible sensitivity to a compromise lower figure, influenced by problems of overload and linearity. New components have enabled designers to reduce size and weight and also power consumption dramatically, as shown in Fig 2. The frequency stability of oscillators has

been increased, allowing selectivity to become sharper and channel widths to be reduced, as shown in Fig. 3 and Table 2. Transmitter designs have not changed greatly except through the impact of transistors and, more recently, integrated circuits. Higher crystal frequencies are used, resulting in fewer spurious outputs while still achieving better frequency stability, and a choice of channels is now a standard facility, although the number is usually limited to 10 or less, spread over a comparatively narrow bandwidth, in land-mobile sets.

Prices for mobile-radio equipment have not risen as rapidly as prices in general, probably because of the economies made possible by the rising numbers in manufacture and by lower component costs.

Receiver design

The biggest change in receiver design since the early days has probably been the increase in selectivity, both in

Fig. 2. Dramatic reduction in power consumption (top), size and weight (bottom) of mobile radio units due to use of new components.

Curve

- (a) transmitter total battery drain – full output
- (b) total battery drain – receiver only
- (c) power to receiver (heater + h.t.) receiver only for 12.6V input
- (d) transmitter standby drain (heaters) for 12.6V input

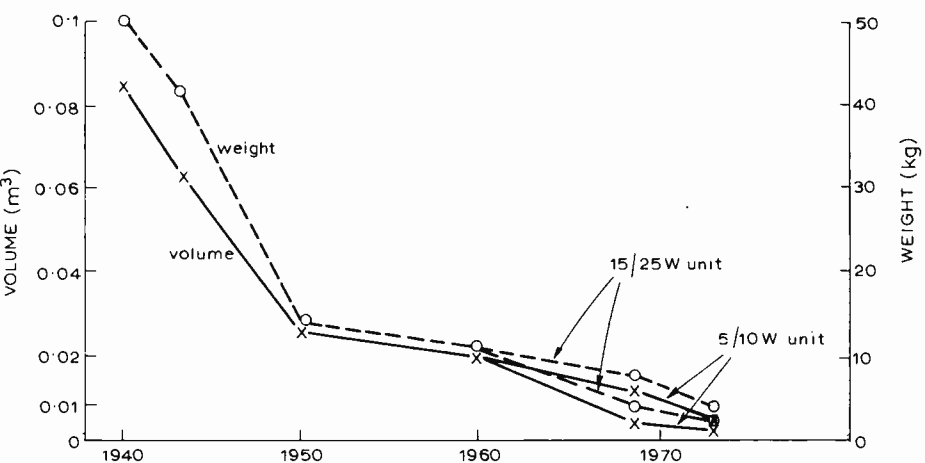
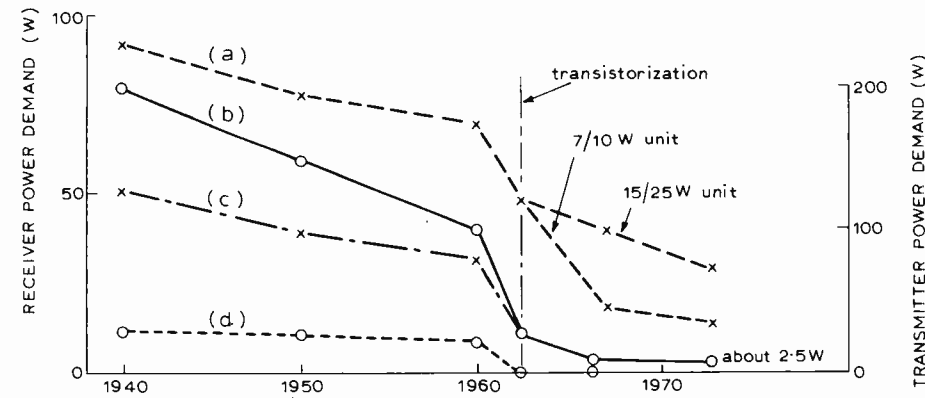


Table 2. Filter performance

Year	Channel width (kHz)	Bandwidth (kHz)				Filter type
		-6dB	-10dB	-40dB	-70dB	
1945	180/200	100	180	270	360	distributed LC
1950	100	50	105	170	240	
1955	50	27	35	45	55	block LC
1955	50	38*	45	50	65	block crystal
1960	25	17.5	20	25	35	block crystal
1970	12.5	8.5	10	12.5	17.5	block crystal
1980	6.25	5.0	5.5	6.25	8.0	

*Special wide-passband unit for area-coverage systems using spaced carriers

narrower passbands and in increased slope of the response outside the passband. Initially, conventional two-coil i.f. transformers were used. In 1954, block filtering at a low intermediate frequency of about 455 kHz was just coming into favour, enabling unwanted signals to be rejected early in the amplifying chain. Generally, bandwidths for the 50 kHz channel widths were about 27 kHz at 6 dB down with side slopes of about 5 dB per kilohertz. By 1966, these filters were being produced for 12.5 kHz channels with 6 dB bandwidths of 8 kHz and side slopes of about 14 dB/kHz. The low i.f. forbade adequate selectivity in a single superheterodyne configuration and double, or even triple, superheterodyne circuits had to be used, with first i.f. stages of about 10 MHz.

In the early 1960s, crystal filters operating at 10.7 MHz put in an appearance. Despite their high cost,

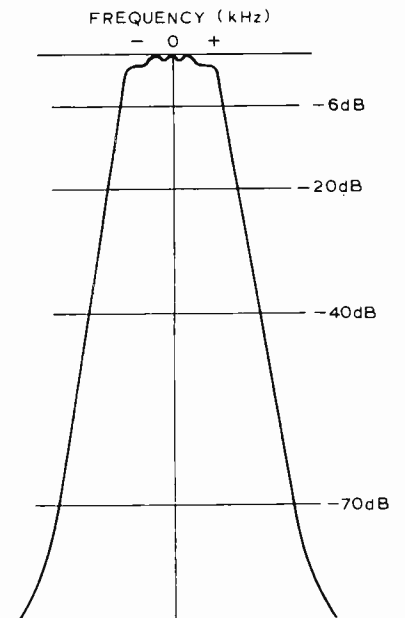


Fig. 3. Response curves relate to bandwidth figures given in Table 2.

they gained ground when it became possible to design high-gain transistor i.f. amplifiers for this frequency with good stability margins. Costs came down and the advantages in avoiding the need for a second frequency change, with its attendant increase in spurious responses and spurious emissions, and the deletion of a second crystal, increased their popularity until, by 1966, they were almost universal and were available in a wide range of performances and formats.

Selectivity, sensitivity and signal handling

In practical working conditions, many signals are delivered to a receiver by its aerial. Some may be many thousand times larger in amplitude than the wanted signal. In these circumstances it is useless to have a highly sensitive receiver unless its large-signal handling is such that it can reject the unwanted signals with minimum effect on the wanted signal. The required rejection is achieved firstly by inserting selective circuits at appropriate points in the receiver and then by careful choice of amplifying devices and control of stage gains so that overloading is kept low for all but saturation signals. Unfortunately,

ly high selectivity and good linearity for high level signals are incompatible with very good noise factors and low-cost components and the receiver designer has to compromise as best he can.

Mobile radio receivers are designed to operate in specified bandwidths within which must be accommodated the wanted carrier and its sidebands plus an allowance for transmitter and receiver frequency drifts and margins on the slopes of the selectivity curves sufficient to ensure adequate rejection of adjacent signals. This is generally accomplished by fitting crystal filters as early as possible in the receiver amplifying chain. Typical performance figures for such filters are shown in Table 2. Figures for a filter suitable for 6.25kHz channel spacing are also shown. This gives the same rejection of about 40dB at the channel edges with a passband for speech of 5kHz. This passband is too narrow for effective f.m. signals, at least those with both sets of sidebands, though the wider passband for 12.5kHz filters copes surprisingly well with f.m. having peak deviations of ± 2.5 kHz when theory predicts a poor result.

Additional selectivity must be provided earlier in the receiving chain to reject signals spaced further away from the wanted frequency, especially those at the unwanted responses of the mixer circuit. Such selectivity, however, must not be so sharp that the set cannot cover a reasonable spread of channels without re-tuning. Spreads of 1 to 2% are usually adequate and allow r.f. filters with rejections of about 50dB at spacings of $\pm 5\%$. This r.f. filtering also serves to reduce voltages at the aerial arising from the mixer injection signal and related frequencies.

Mixers and preceding r.f. amplifiers must be able to handle large signals reasonably linearly i.e. they must not change in gain when large, off-tune signals are applied to their input. In service, mobile radio receivers meeting the relevant performance specification should be able to receive a small wanted signal with little noticeable degradation in the presence of one or two unwanted

signals 70dB higher in level, spaced at least one channel width away.

Noise. Noise figures of 3dB or slightly less can be achieved economically in r.f. amplifiers but such figures are modified in practice by losses in aerial change-

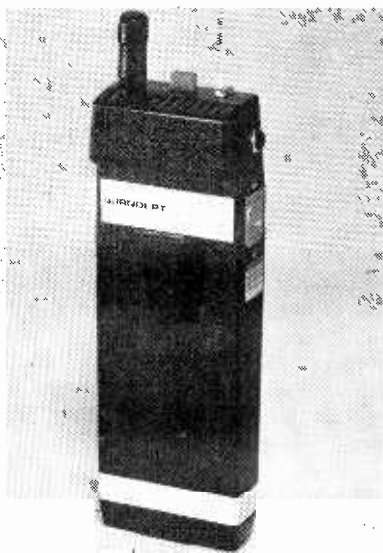
over circuits, input selective circuits and by external noise emanating from local sources such as ignition circuits and from more distant sources including the galaxy itself. An a.m. receiver with a typical overall noise factor of about 5dB would provide an output signal-to-noise ratio of about 12dB when fed with an input signal of $1\mu\text{V}$ e.m.f., modulated to a depth of 60%. For an f.m. receiver the output ratio would be about 20dB.

Noise originating in the supply line or in some inverter or stabilizing circuit in the radio unit itself can also be troublesome in audio stages. High acoustic noise levels can make operation very difficult, even with noise-cancelling microphones, because of its overloading effect on the voltage-limiting or a.g.c. circuits, widely used in transmitter audio amplifiers.

Frequency accuracy. Permitted frequency tolerances for transmitters and, by inference, for receivers are ± 1 kHz for base stations and ± 2 kHz for mobiles working in 12.5kHz channels in the high band. To achieve this order of stability over a long period demands great attention to the choice of crystal type and oscillator circuitry and components. Matters are made worse by the need to take up aging drifts and setting inaccuracies by a pulling circuit which, by its very nature, tends to add to frequency instability. Crystal ovens are not much favoured for increasing frequency stability because of their warm-up time and increased cost. Internally-mounted stabilising components can be used but are also expensive in multi-channel sets. The tighter frequency tolerances likely to be necessary for any method of channel width reduction may force a swing to synthesis from a single, very stable, crystal in place of separate crystals for each channel.

Transmitters. Overtone crystals operating in the range 40 to 100MHz have reduced the number of multiplying stages in transmitters in recent years but f.m. transmitters still require a relatively high multiplication factor to obtain a high enough frequency deviation at the output. The highest possible crystal frequency is always desirable, however, because of the reduced number and wider spacing of spurious outputs thereby obtained. Good power transfer between stages implies heavily-loaded interstage circuits and this has led to the use of fixed-tuned modules, covering a whole band with power gains of more than 15dB at u.h.f. and power outputs of up to 50 watts. Spurious harmonic outputs from transmitters must be reduced to $2.5\mu\text{W}$ or less and the power, due to unwanted sidebands and noise, in adjacent channels must not exceed a level about 60 to 70dB below the carrier level.

(To be continued)



C. Personal portable three-channel unit (Burndept)



D. Fireman's call unit (Pye)

E. Maritime mobile unit (Redifon)



Eddystone professional VHF receivers

Model 1990R

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Model 990R

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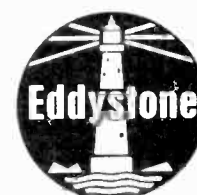
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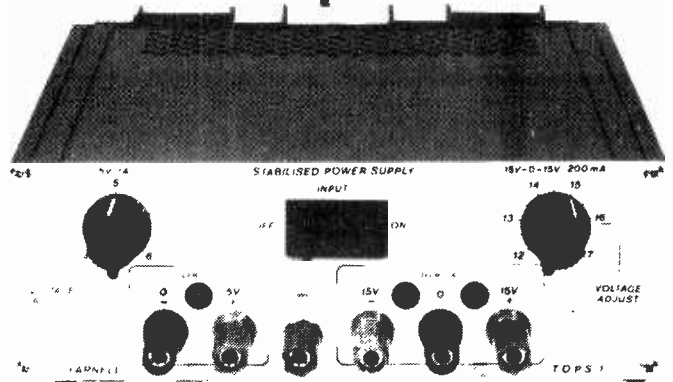
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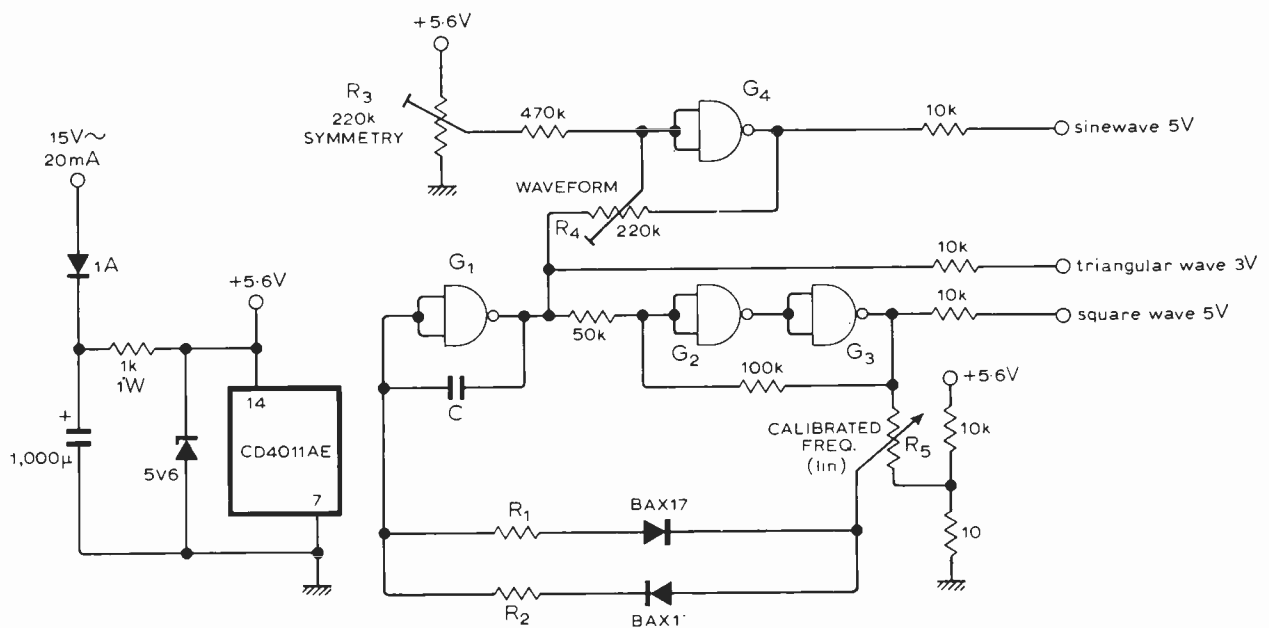
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Circuit Ideas

Single i.c. function generator

The c.m.o.s. nand gate CD4011 can be used as an operational amplifier with an open loop gain of ≈ 100 . The generator consists of an integrator G_1 with a variable delay-time, Schmitt trigger G_2 , G_3 , and a triangle to sinewave converter G_4 . The sine-wave approximation depends on the transfer function of G_4 and is calibrated by R_3 and R_4 . Sawtooth and pulse waveforms are obtained by choosing different values for R_1 and R_2 . Values of R_1 and R_2 may be varied between $10k\Omega$ and $10M\Omega$ while C can be between $100pF$ and $2.2\mu F$ (reversible). Typical oscillator frequency f is $\alpha/(R_1 + R_2)$. C hertz where α is the setting of R_5 . At the ends of the frequency range, however, waveform distortion and frequency deviation become significant. J. W. Richter, Backnang, Western Germany.



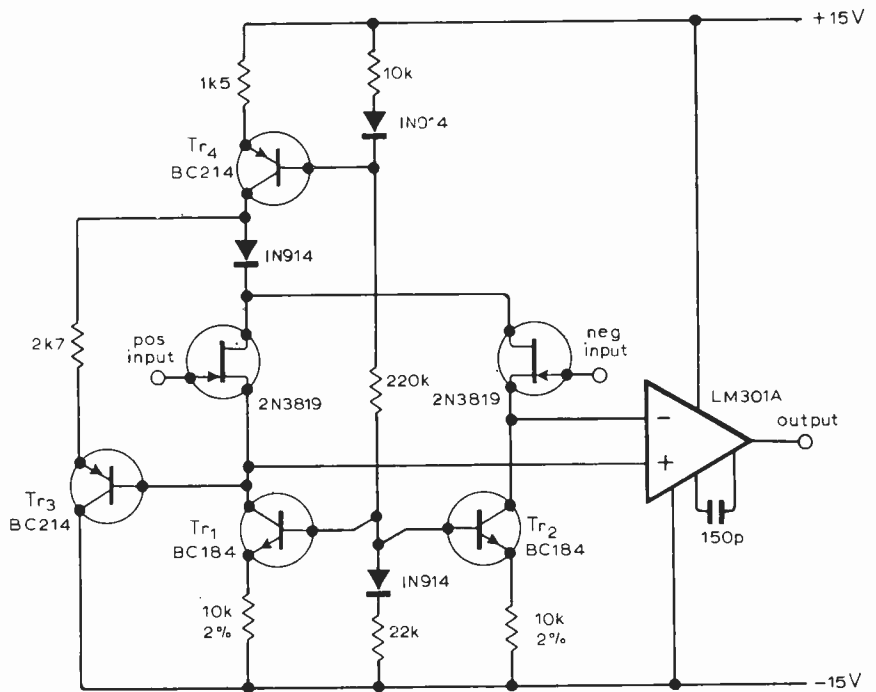
F.e.t.-input operational amplifier

For less than £1.50 this circuit offers the same input performance as the more expensive commercial units. Two f.e.t.s are used in a differential source-follower, operated at a constant source current of $200\mu A$ from Tr_1 and Tr_2 . Input leakage current is kept below $1pA$ by maintaining the drain-source voltages at $0.55V$. This value is kept constant by Tr_3 because the input common-mode voltage changes within its -13 to $+11V$ range. Tr_4 acts as a $600\mu A$ current source, its collector current being shared equally between the f.e.t.s and Tr_3 . A constant $200\mu A$ thus flows through the $2.7k\Omega$ resistor. This current

sets the V_{DS} voltage of the f.e.t.s. A diode is used to cancel the base-emitter voltage drift of Tr_3 .

Input offset voltage should be trimmed to zero by adding a resistor in the appropriate f.e.t. source, and matching the f.e.t.s will reduce thermal drift. Common mode rejection ratio can be $94dB$ if a resistor of adequate value (several $M\Omega$) is connected between one of the f.e.t. sources and ground. Input impedance of the circuit is greater than $10^{13}\Omega$.

Joel Setton,
Grenoble,
France.



Digital alarm clock

The MM5316 alarm clock i.c. is designed for use with either liquid crystal or fluorescent tube displays. The manufacturer, however, does not supply information for using i.e.d. displays. This circuit is similar to the manufacturer's but common anodes of display i.e.d.s go to V_{ss} rather than V_{dd} , and brightness is adjusted by R_1 . The power supply is non-critical because the 5316 does not require regulation. Diodes and batteries provide power in the event of an a.c. failure. The display is then blanked to extend battery life. The clock will not keep time without a.c. acting as a frequency element, but it is easier to reset the time and alarm after an interruption.

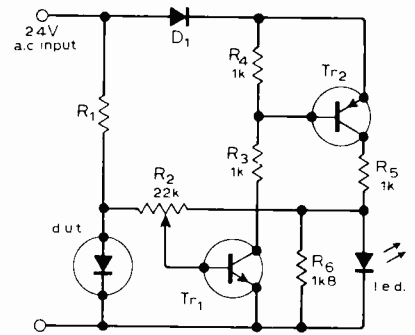
The alarm circuit is a conventional 555 multivibrator with a 100nF capacitor connected to the 1Hz output of the 5316. This produces a frequency shift warble on the output tone. Clock time is set by the fast and slow buttons, and time can be held by simultaneously pressing the seconds-display and slow buttons. Alarm time is set with the fast and slow buttons while depressing alarm-display.

M. F. Smith,
Department of Oceanography,
University College,
Galway.

Diode forward-voltage tester

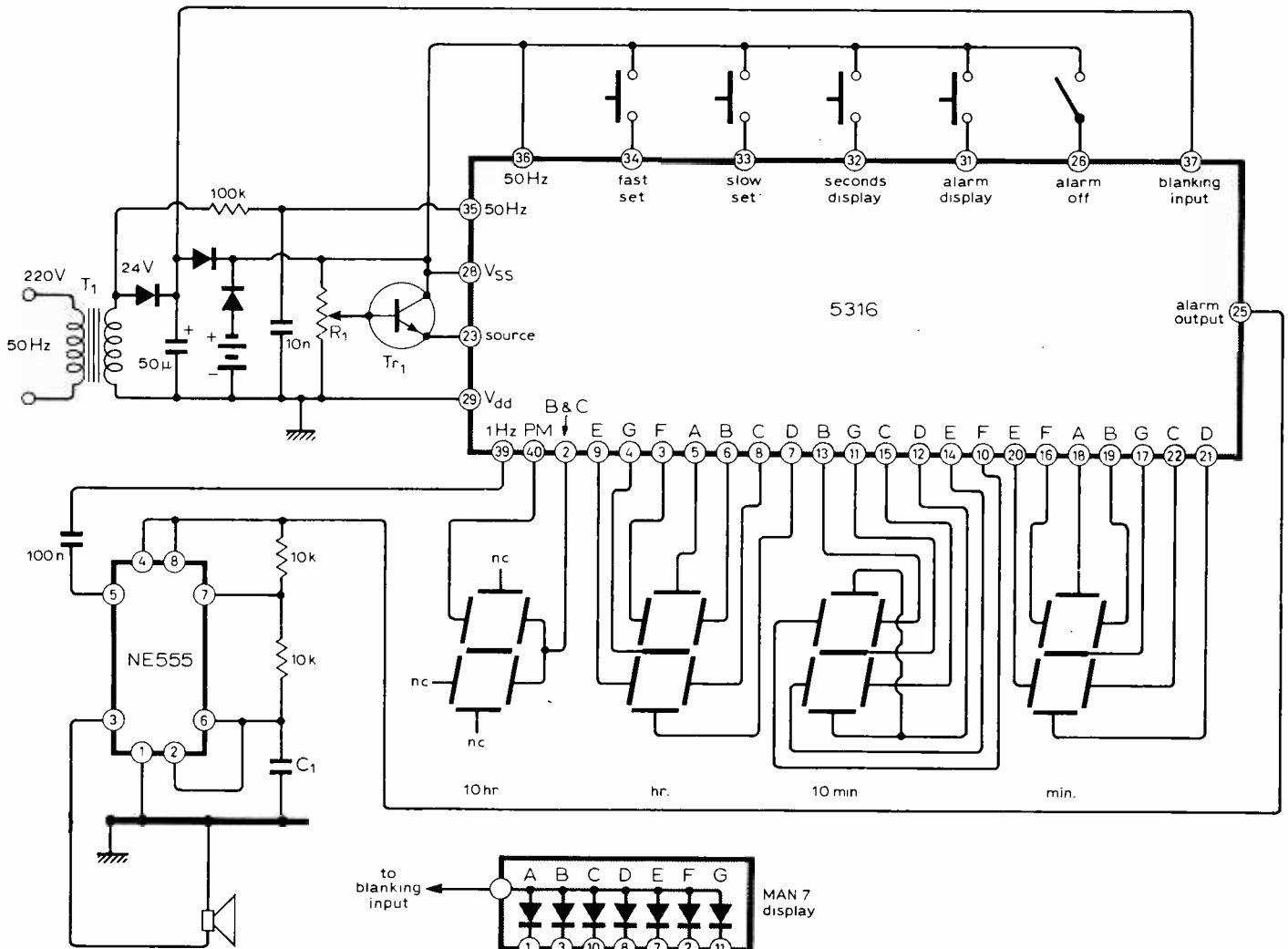
Many circuits use a diode in the forward voltage mode. This circuit enables diodes to be selected for forward characteristics using go-no go indication. The diode under test has a.c. passed through it via R_1 . On positive half cycles the diode is forward biased and D_1 passes voltage to the rest of the circuit. The diode's forward voltage drop across R_2 and R_3 causes a potential at Tr_1 base which can be adjusted. If this voltage is sufficient to turn Tr_1 on, then Tr_2 will also turn hard on to illuminate the i.e.d. and give positive feedback through R_2 . The i.e.d. will stay on for a half cycle.

The base-emitter junction of Tr_1 is used as a reference and is temperature sensitive but the diode offsets this. A complementary circuit can be made to measure the same diode on alternate half cycles. If an unmarked



diode is connected, one of the half cycles will be effective which will extinguish one i.e.d. to indicate a good diode and its polarity.

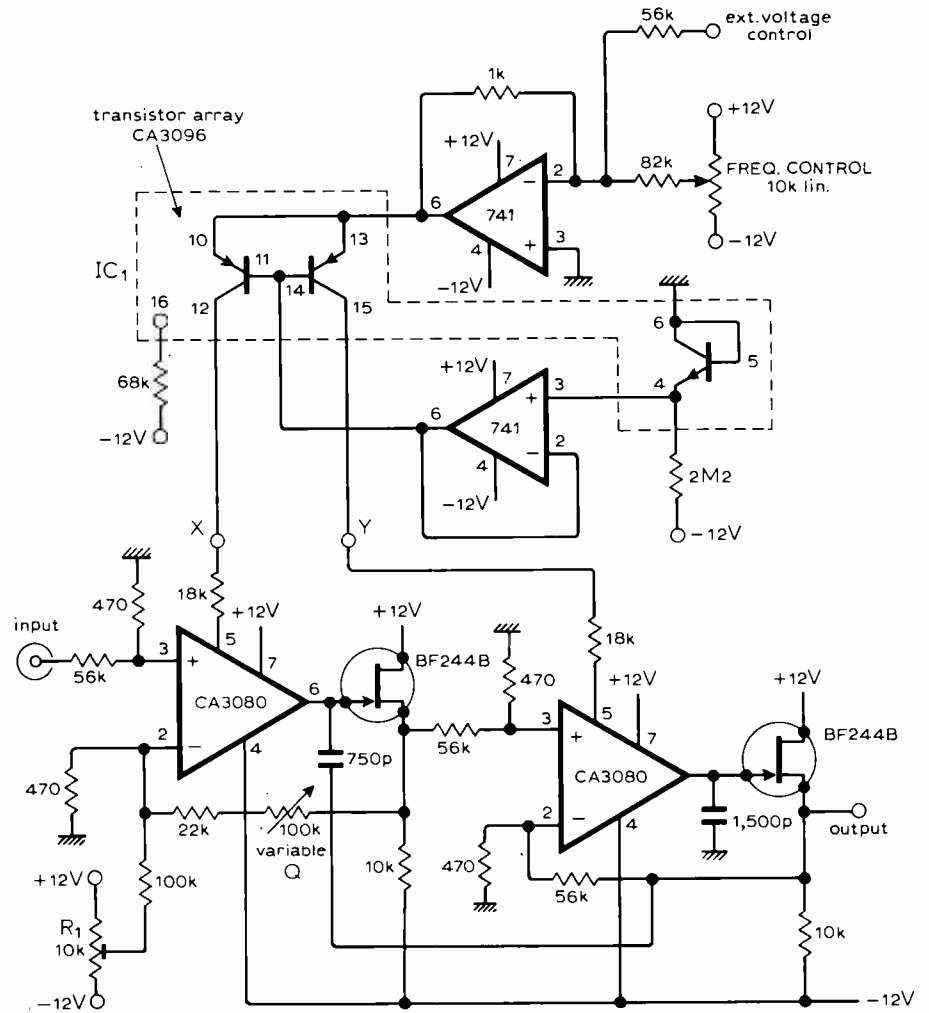
R. J. Torrens,
Scientronics,
Huntingdon.



Voltage/current controlled filter

The circuit shows a controllable filter, having a -12dB/octave roll off. Frequency range is 15Hz to 15kHz , this frequency being controlled by either a voltage or current. Voltage to current conversion is achieved with a logarithmic characteristic (IC_1); thus the filter frequency moves in octaves/volt rather than in Hz/volt . The CA3080 operational transconductance amplifiers are used to produce variable resistors. If just manual control of the cut off frequency is required, only the bottom half of the circuit is used by shorting points X-Y and connecting them to the wiper of a $10\text{k}\Omega$ log potentiometer between -12V and ground. If voltage control of the cut off frequency is required, the top half of the circuit is used. By using a transistor array, good matching and temperature stability is obtained. The separate transistor (pins 4, 5, 6) provides an offset bias voltage of the correct value and also a voltage to compensate for any temperature changes. The CA3080's may be selected for minimum d.c. offset change with respect to frequency control, or the offset may be nulled by R_1 .

T. Orr,
Putney,
London SW15



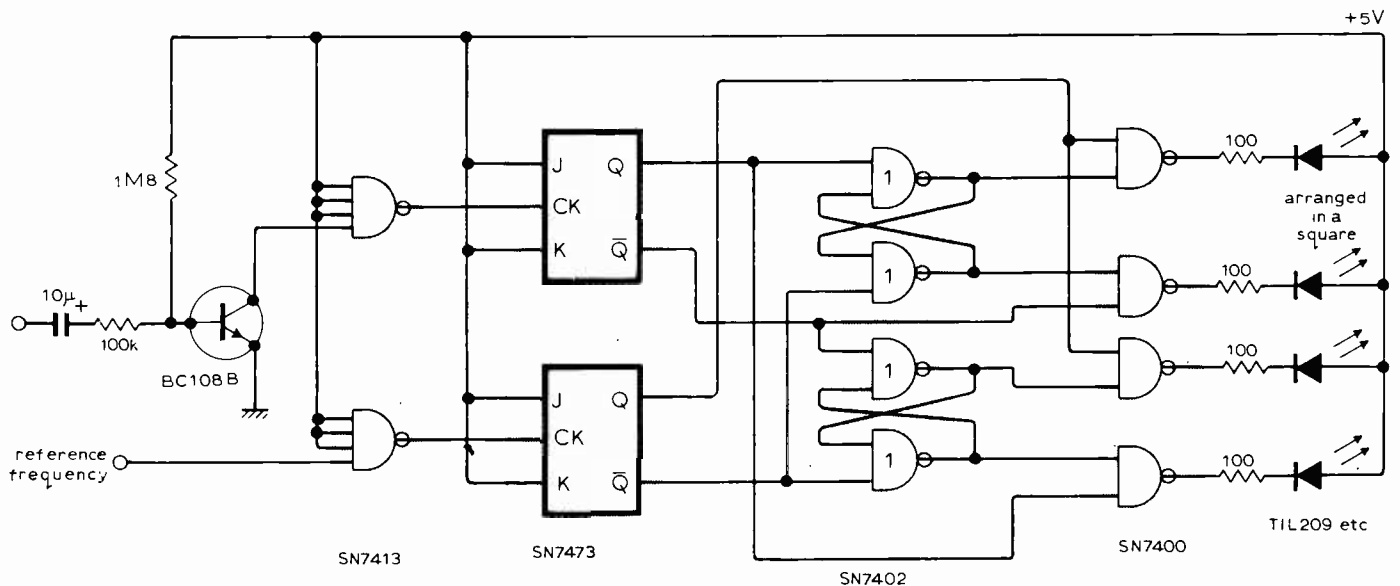
Beat-frequency indicator

By using four l.e.d.s arranged in a square, this circuit indicates whether an input frequency is above or below a reference frequency by the direction of apparent rotation. The circuit also accepts any shape of input or reference waveform. Schmitt triggers shape the input and reference waveforms to give rectangular pulses which the flip-flops divide by two, to produce square waves with mark-space ratios of half the original frequency. These are then

gated together to produce a rectangular pulse train whose mark-space ratio changes with the phase difference between the two square waves.

Provided that the input and reference frequencies are above about 50Hz , flashing of the l.e.d.s will not be noticeable, and they appear to brighten and dim in sympathy with the changing mark-space ratio. A rotating effect is achieved by arranging the logic to determine which waveform goes low

first before each pulse is produced, and then using this to decide which l.e.d. is lit. Rate of rotation will be half the difference between input and reference frequencies. If the rate of rotation is too fast it may be reduced by putting counters between the Schmitt triggers and their respective flip-flops. Input level should be above 200mV pk to pk. Craig Clapp, Southampton University.



World of Amateur Radio

Over 500 km on 10 GHz

The keen interest among a small but growing number of British amateurs in microwave operation has brought new successes in the exploitation of over-sea super-refraction modes on 10GHz. Following the 306km contracts between Holland and the Thames Estuary in July, a new "world record" has been set up by the Barry College Radio Society Microwave Group and George Burt (GM3OXX) for a two-way contact between G4BRS/P at Pendeen Watch, near St Ives, Cornwall (NGR SW 382 359) 130ft. a.s.l. and GM3OXX/P, Portpatrick, Scotland (NW 999 539) less than 30ft. a.s.l. The contact, made on August 14 between 1600 and 1900 GMT, was established directly on 10GHz without any lower frequency "talkback" contact and signals peaked to about 45dB above noise towards the end, although deep fading and drop outs were experienced throughout the period.

At G4BRS/P (operator Phil Schorah, GW3PPF) the equipment included a 4ft dish aerial with cutler feed, 15mW Gunn-diode transmitter and SIM2 mixer, two 40673 m.o.s.f.e.t. pre-amplifiers at 104MHz and a broadcast v.h.f./f.m. receiver using a deliberately misaligned circulator. Very little waveguide is used and the system provides duplex working with a common i.f.

At GM3OXX/P there was a 2ft dish aerial, 10mW Gunn-diode transmitter and SIM2 mixer into a home-made i.f. arrangement with a home-made transmit-receive waveguide switch.

A further but less consistent contact was made the following afternoon. British microwave enthusiasts are also anxious to investigate over-land ducts which are thought to be more common than usually suggested. A new 10.1 GHz beacon station, GB3LBH, is now operating from Romford, near London.

Examining would-be amateurs

The Radio Amateurs' Examination, set by the City and Guilds of London Institute, was introduced in the UK in 1946 and at first many ex-servicemen and others were able to claim exemp-

tion. From 1920-1939 the only formal examination was a Morse test, though technical reasons for wanting an "experimental" licence had to be given. It is debatable whether the RAE has really raised the technical standard of the British amateur, though it has deterred the dabblers (who might have become competent by "learning by doing"). It sets a hurdle of variable height that brings some down with a bump and gives others a feeling that the licence is not to be taken lightly. But one wonders how often the average amateur uses in practice the elementary formulae and alternating current theory that he or she mugged up for the exam.

But at least the RAE syllabus and questions do have a working relationship with amateur radio. A more difficult problem, as the Australians have discovered recently, is to set a suitable standard for novice licences. They opted for multiple-choice techniques giving four answers to each question. But then, as *Electronics Australia* has revealed, inspiration seems to have run out.

For example: "an audio amplifier will give the best response when operated: class A; class AB; class B; or class C?" A question surely more likely to be fought out in the correspondence columns of *Wireless World* than by a novice.

Or how about: "Which method of coupling, when used in an audio amplifier, would have the best frequency response: RC coupling; transformer coupling; direct coupling; choke coupling?" Shades of the 1931 edition of the *Admiralty Handbook of Wireless Telegraphy!*

Or consider: "It is required to increase the power output of a transmitter by 3dB. The power would then be increased by: 4 times; 6 times; 8 times; doubled?" The correct answer is the only one that does not make a sentence – but, that apart, should one expect a would-be novice to be familiar with decibel notation? It is not in the RAE syllabus for Class A or B licences.

Amateur radio is a service of self-training: new recruits should be keen to learn, know how to avoid causing interference and how to check their transmitter; and know the regulations. With examinations like the one set for Australian novices it is no wonder that many hobbyists are attracted to the concept of the Citizens' Band!

Among the places where RAE courses are available (apart from those given last month) are: Bangor; Bedford; Birkenhead; Borehamwood; Brentwood; Bridgnorth; Burgess Hill; Colchester; Crawley; Doncaster; Dudley; Enniskillen, Framwellgate Moor; Harrow; Heanor; Huddersfield; Knottingley; Langley; Leeds; London—Acton, Chingford, Holloway, Ilford, Islington and Paddington; Loughborough; Manchester; New Ollerton; Newcastle-upon-Tyne; Princess Risborough; Redruth; St Ives; Scunthorpe; Sheffield; Southend-on-Sea; Stockport; Wembley

and Wigan. Advanced courses include those at: Langley, Leeds, London (Islington).

In Holland the first examination for the introductory D-licences attracted 1150 candidates of whom 652 passed; 500 sat the second examination.

Intruders

Direction-finders placed an extremely powerful amateur-bands intruder (apparently some form of ionospheric sounder) – radiating about 10 pulses a second on about 14,215kHz but spreading ± 100 kHz or more – in the Gornel area of Byelo-Russia or Ukraine. The monthly summaries of the IARU Region 1 Intruder Watch typically list some 500 or 600 stations heard operating within amateur bands, often half of them in the 14MHz band. But undoubtedly the most serious intruders, apart from the Russian pulses, are normally the high-power broadcasting stations and associated Russian and Bulgarian jammers, which include deliberately over-modulating stations between 7000 and 7100kHz. China, Albania and Egypt appear the most persistent offenders.

In brief

The Derby society reports a "first" for the GB2RS news bulletins with bulletins read on successive Sundays by "YL" operators – Mrs Ann Buckley, G4EYL and Mrs Jenny Shardlow, G4EYM . . . The fifth National Amateur Radio and Electronics Exhibition, organized by the Amateur Radio Retailers Association, is being held at the Granby Halls, Leicester, on October 28, 29 and 30 . . . The RSGB has announced that an International Radio Communications Exhibition and Convention will be held at Alexandra Palace, North London on May 6 to 8, 1977. The convention will cover h.f., v.h.f. and microwaves and there will be a dinner and dance . . . The Scandinavian 432MHz beacon stations OZ2UHF, SK6UHF and LA1UHF have been received in Aberdeen . . . The first u.h.f. repeater in the London area, GB3HR at Bushy, is in operation and a u.h.f. repeater (GB3CB) has now been licensed for the Birmingham area . . . The Cornish v.h.f. beacon station, GB3CTC, has been testing new equipment on 144.914MHz with 75 watts e.r.p. omnidirectional . . . The Home Office has temporarily suspended the issue of special-event "GB" licences . . . The BBC's World Radio Club has enrolled its 30,000th member . . . The 1976 National Field Day was won by the Glenrothes club with the Channel Contest Group in second place and the "restricted" section won by the Rascal Amateur Radio Group . . . the v.h.f./u.h.f. field day was won by the March club . . . An NRRL report states that there are 3863 licensed amateurs in Norway and society membership has increased from 2525 to 2680.

PAT HAWKER, G3VA

Optical fibre communication

Sub-systems for field demonstrations — 1

by M. M. Ramsay, A. W. Horsley and R. E. Epworth *Standard Telecommunication Laboratories Ltd*

In 1966 Hockham and Kao¹ described the possibility of an optical communication system using single-mode fibre waveguide as the transmission medium. Such systems would have enormous information carrying capacity, and if attenuations down to 20dB/km could be achieved they would have clear economic advantages over coaxial cables for wideband long-haul applications. At the time, the 20dB/km target seemed highly optimistic, and there were a number of other technology breakthroughs which needed to be established, such as uncooled c.w. semiconductor lasers, before such systems could become a reality.

All these breakthroughs have been achieved, and subsequently confirmed, by several independent groups of researchers. Furthermore, the 20dB/km target, which once seemed so distant, was passed with relative ease, and attenuations of around 3dB/km have now been demonstrated in high silica fibres. If such fibres can be produced routinely in quantity and can be incorporated into practical cables with only modest loss increases, then, even ignoring the plethora of military and other non-PTT applications which look increasingly attractive, a very much broader range of systems than was originally proposed will be viable, particularly in view of the rising cost of conventional materials.

More recently, therefore, the emphasis of the work has shifted towards consolidating research results and tackling the many engineering problems which will have to be solved before optical fibre systems become a reality. This type of work requires a different approach from the earlier research, and is best carried out using a model system approach, where the assumption is made that a demonstration will be held in a typical PTT environment. This ensures that adequate account is taken of the myriad of practical problems which occur with real systems in a field environment, but often cannot be predicted from experimental work in the laboratory.

The PTT situation chosen was that of the British Post Office as this is best

Progress in research contributing to the realisation of an optical-fibre communication system has been rapid. Long-lived, room temperature, c.w. semiconductor lasers are being tested. Several techniques have been shown to be capable of producing multimode or monomode fibre waveguides on a routine basis with attenuation well below 10 dB/km. Fast, reliable silicon avalanche photodiodes are available commercially. Connectors for single-fibre waveguides have been produced with 1-2 dB/km loss and splices with much lower attenuation. Complete analogue and digital laboratory systems have been shown at many conferences and exhibitions. From a position of such strength in the realm of research, it would seem that a wide range of targets would be set for a field trial. However, the introduction of an optical-fibre communication system into an existing network is possibly a more far-reaching step than any that has been taken since the inception of these networks. Because of this, a great deal of engineering confidence has still to be established. A large-scale field demonstration (see August issue, page 70) could achieve this, but many sub-systems must be engineered before this can be held. With careful design, such a demonstration will assist in determining the targets to be set for a field trial.

known to us. Had the original expectations of Hockham and Kao been only barely realized, the choice would have been simpler, because only at very high bit rates would any economic advantage over coaxial cables have been expected. In fact, we can select from a very wide range of systems from 2Mbit/s to 560 Mbit/s which are all feasible and all economically advantageous in the appropriate PTT environment.

It is still too early for PTTs to know definitely which systems they will wish

to procure and install in quantity, and it would require a prodigious and unjustifiable expenditure of resources to cover all possibilities. Fortunately, the problem is not as difficult as it seems at first sight. The solution is an integrated but flexible field demonstration programme, designed to provide sufficient practical information to a broad range of systems, not just the specific one tested, for a PTT administration to see in the work done sufficient justification and technical content to commission a full-scale field trial for whatever type of system turns out to be most appropriate for its needs.

This article describes work being carried out to produce the key sub-systems which will enable realistic field demonstrations to be mounted, thus paving the way to field trials of optical fibre communication systems.

Present status

From many aspects the present time may be regarded as a watershed in optical fibre communication. Progress in most of the lines of research contributing to the realization of a communication system has been extremely rapid, and in several instances confidence is growing that today's results are the harbingers of future progress. We have sufficient confidence now to plan the first steps in engineering aimed ultimately at full-scale field trials. However, before we can examine this new realm, we review the present research status in more detail.

A recent review of propagation in optical fibre waveguides² illustrated the progress that has been made during the last few years in building up an understanding of the dispersive and radiative loss mechanisms in dielectric waveguides. A further review³ considered the various manufacturing technologies that have been developed, all of which are capable of producing low-loss fibre waveguides: in particular those involving high-silica-content glass give total attenuations below 10dB/km on a routine basis.

Provided that all the relevant physical parameters can be established, there are

several methods of fibre transmission analysis available which cover a wide range of complexity and accuracy^{4,5}. The physical parameter proviso is far from being a trivial one, although considerable insight can be obtained into the behaviour of optical fibre waveguides by analytical means.

Most of the current methods used to manufacture low-loss fibre waveguides are capable of producing single or multimode guides. In either case the waveguide design may use a simple or multi-layer cladding. In the case of multi-mode guides, a graded-index profile can be used to reduce the dispersion of group velocity of the various propagating modes. The optimum profile can be computed for any particular materials and wavelengths⁶ and gives a dispersion of under 100 picoseconds/km for $\Delta n/n = 1\%$, where n is the refractive index; but the best experimental results are still about an order of magnitude greater. Modal dispersion of below 1ns in 1km of fibre waveguide has been demonstrated, but only in cases where either the fibre aperture was not fully illuminated⁷ or mode mixing due to residual or applied strain, or other waveguide inhomogeneities, was present^{8,9}.

Cabling. Apart from the mechanical problems obviously present when cabling optical fibre waveguides, the essential requirement is that the fibre waveguides must remain in a strain-free condition. The effects of an inadequate cabling technology can be quite dramatic. Even comparatively small amplitudes of microbends, a few microns amplitude for instance, can lead to hundreds of dB/km attenuation if the mechanical wavelength is particularly unfortunate¹⁰. However, these problems can be overcome and several designs have been shown to be capable of producing cables having an overall attenuation around 10dB/km, and which can be installed in conventional ducts.

Jointing. Both demountable connectors and permanent splices have been demonstrated in many laboratories. Particular splicing techniques involve fusion in low-melting-point glasses, cementing or fusing in accurate capillaries, V-groove alignment or three precisely machined pins. Alternatively, adjustable splices can be made with fibres mounted in eccentrically machined holders. All these techniques have involved losses of only a small fraction of a dB and some have already been demonstrated in the field¹¹. Connector design has concentrated on modifications to existing electrical connectors which enable the fibres to be accurately aligned when the connectors are coupled. Attention to mechanical tolerances has enabled losses to be reduced to a few dB with 30 μ m core fibre waveguides and correspondingly lower losses for larger cores.

Optical sources. Although low-bit-rate systems of modest repeater section could be made to operate with conventional light emitting diodes of the kind now commercially available, such systems could hardly be said to stretch the technology of fibre optic communication. Also, although rapid progress is being made with various miniature neodymium lasers, these all require external modulators and must still be regarded as firmly in the realm of research. We can therefore confine our attention to high-intensity light-emitting diodes and semiconductor injection lasers, both of which can be modulated directly by control of their current drive. Both have reached their most advanced state of development using GaAs and/or Ga_xAl_{1-x}As and hence emitting in the spectral range 800 to 900nm. Both are capable of continuous operation at room temperature.

Emission at longer wavelengths, in the range just beyond 1 μ m, would be attractive for two reasons. The first is that the basic scattering mechanisms reduce at longer wavelengths and many fibre waveguides also show lower absorption. The second reason is that there is a much lower dispersion of group velocity due to the material¹². This last-mentioned attraction is most pressing for l.e.ds as the combination of material dispersion and their wide spectral width of 20-80nm could well impose the bandwidth limitation in system design.

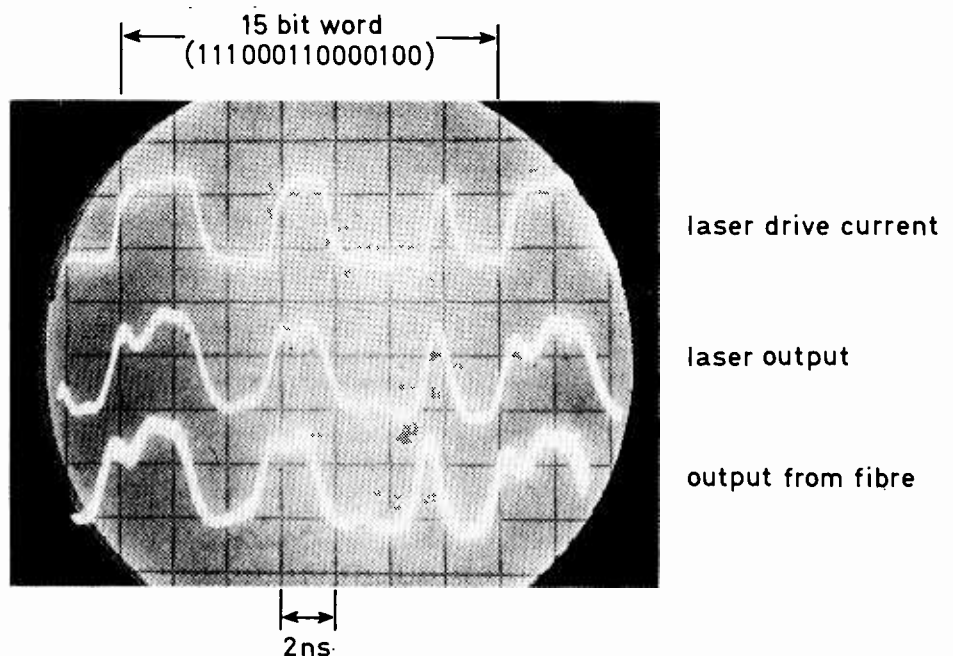
Light-emitting diodes in Ga_xIn_{1-x}As systems are being investigated to exploit these advantages¹³ and initial

results are encouraging. From an engineering standpoint l.e.ds offer one outstanding advantage in that they already have a demonstrable life of well over 10 000 hours. Disadvantages arise from their large spectral width, from the isotropic emission of radiation and hence low coupling efficiency to optical fibre waveguides; and from the fact that even small-area l.e.ds designed to launch light into a single multimode fibre have sufficient reactance associated with junction capacitance and an inherent radiative lifetime that makes modulation difficult at over 100Mbit/s when operated at high intensity.

Launching efficiency can be improved and the limitations due to spectral width overcome by using lasers. Most commercially available lasers have a broad contact and emit over a junction width of over 100 μ m. Under these circumstances there is little prospect of providing an adequate thermal path away from the junction and operation must be limited to less than a 30% duty factor. Striped contact mesa techniques and proton bombardment have all been used to confine the current and emission to a narrow region¹⁴. These are becoming commercially available. Continuous operation at room temperature can be effected by any of these techniques, and, when the change in refractive index at the boundary of the active region is small, single transverse mode operation can be obtained. Under these circumstances reasonably efficient launching is possible even with single-mode optical fibre waveguides.

Lifetime has long been the major problem with semiconductor lasers, but rapid strides have recently been made and many institutions now report lifetimes of several thousand hours, with best results of well over 10 000 hours and extrapolations being made to around 100 000 hours¹⁵.

Fig. 1. 1 Gbit/s single-mode fibre. Laser current, laser light output and fibre output after light has been transmitted through nearly 1km of single mode fibre.



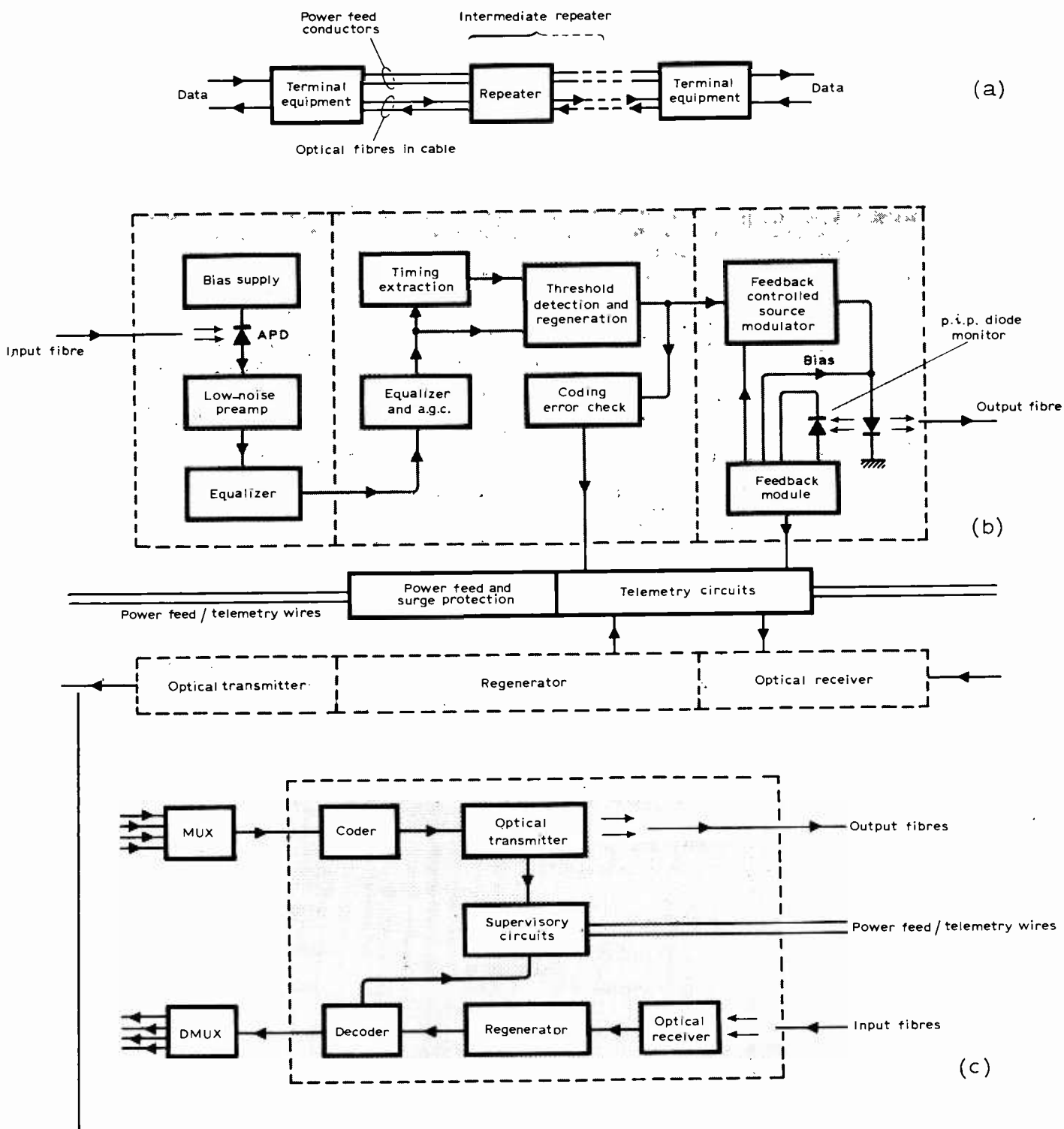


Fig. 2. Overall system block diagram (a) wherein initial system repeater spacing is expected to be 3km. Repeater block diagram (b) shows optical receiver, regenerator and transmitter. Degraded pulse received after transmission is amplified, reshaped and retimed before retransmission. Terminal block diagram (c) shows multiplexing of incoming signals prior to transmission and regeneration and demultiplexing of received signals together with testing equipment and subcircuits.

Detectors. Fortunately, adequate silicon avalanche photodetectors have always been available commercially¹⁶. Although these detectors may not be optimum and — for some applications packaging deficiencies have been apparent — they have enabled laboratory systems to be constructed with a signal-to-noise penalty of only 5-6dB. Continuing research and new experimental techniques will enable this margin to be narrowed even further.

Systems. Practical considerations rule out heterodyne detection, so attention can be confined to direct detection. Also, two-channel systems show a very minor return at best for the additional complexity¹⁷, and can be ignored. Quantum noise, dark current noise and

leakage noise are all manifest as a shot noise characterized by Poisson statistics. With proper system design these will dominate the receiver thermal noise

and quantum noise should form the largest element. Design principles to ensure this are well understood¹⁸ and theoretical consideration has been given to other aspects of system design, particularly to optical fibre systems¹⁷.

Many systems have already been demonstrated on a laboratory basis and scale. Pulse-code modulated systems with bit rates ranging from 6.3 to 400Mbit/s have been described¹⁹, and transmission has been reported through nearly 1km of single-mode fibre from a $Ga_xAl_{1-x}As$ injection laser directly modulated at 1Gbit/s²⁰; see Fig. 1. Pulse analogue and amplitude modulation systems have also been described, but as regeneration is not possible and as carrier signal-to-noise ratios are inadequate for transmission through many

repeater sections, these cannot be considered for PTT applications. Nevertheless, virtually the entire range discussed in the introduction has been covered by present-day laboratory demonstrations.

Overall system design

A field demonstration study is not a prototype system, but a means of collecting the maximum engineering information possible on optical fibre systems under normal operating conditions. The scale must be sufficient to achieve this goal, and will involve a complete, self-contained, two-way system, operating through at least two intermediate repeaters, with both test equipment and partially equipped multiplexers at the terminals.

In view of the rapid advances in the state-of-the-art, flexibility is desirable; spending time and effort on sophisticated and supposedly ultimate solutions, in areas where the scarcity or transience of available data preclude this, is not. A modular approach is essential to maximize the commonality of equipment between terminals and repeaters. Design of the individual modules requires special attention to give scope for later modifications or experiments.

A key decision concerns the bit rate. A good choice is 140Mbit/s which, though not the highest rate which could be demonstrated, enables a searching test of possible exposures to be carried out, corresponds to an economically attractive slot in many PTT networks, and will yield much data relevant to lower bit rate systems.

There are also a number of subsidiary decisions on the system and component details which have to be made, and in the following sub-sections these are discussed with reference to the system and sub-system block diagrams shown in Fig. 2.

Sources and detectors. It seems highly likely that gallium arsenide directly modulated light sources will prove adequate for all but the very highest bit rates. For PTT systems the laser will generally have an advantage, particularly at higher bit rates, because considerably more power can be launched into a suitable fibre, from the dispersion point of view, and the extra repeater spacing potential is economically very desirable. The possible exception is at low bit rates, for example 2Mbit/s, where, because large-core, high-numerical-aperture fibres can be used, the laser may have no advantage.

The choice of detector lies between two silicon devices whose responses are well-matched to the gallium arsenide sources: the p-i-n diode and the avalanche photodiode (a.p.d.). With special high-impedance preamplifier techniques the performance of the p-i-n diode may be comparable with the a.p.d. at low bit rates; but at higher bit rates

the a.p.d. has a clear advantage since its internal multiplication provides lower noise gain than have available preamplifiers. Avalanche photodiodes have, however, been unpopular as they require voltages of typically 80-200V and are reputedly difficult to drive.

The best choice for a field demonstration at the present time is expected to be c.w. lasers and a.p.ds and as they will almost certainly eventually emerge as the preferable devices for most PTT applications and because they enable more ambitious systems, in terms of repeater spacing and bit rate, to be evaluated. This in turn will enable more comprehensive data, more closely relevant to an economically realistic system, to be accumulated. The choice can be made with confidence since c.w. lasers with more than adequate lives for such a demonstration are already available and, as will be described in part two, elegant solutions to the problems, real or supposed, of incorporating both devices in practical subsystems are being developed.

Fibre type. The choice of fibre lies between single-mode fibre, with a simple or multilayer cladding, and multimode fibre with step or graded index. Single-mode fibre is in many ways the best understood; it is convenient to make and has the highest bandwidth. However, it does pose jointing problems which, while doubtless being soluble in the long term, are truly formidable in the short term. Step index multimode fibre seems limited in PTT applications to low bit-rates (2Mbits/s and possibly 8Mbit/s). Graded-index multimode fibre is the most interesting possibility. It is certainly suitable for very much higher bit rates than step index fibre and, depending on how precisely the index profile can be maintained on a repeatable basis, it may prove adequate for any likely first-generation system. On the evidence available so far, jointing difficulties appear comparable with step-index fibre of equivalent core size. There are admittedly numerous unknowns associated with this fibre, but in view of its promise it seems the natural choice for a field demonstration. Its performance when produced in pre-production quantities can then be evaluated in an installed, jointed cable in a practical environment.

Coding. In conventional p.c.m. wire line systems a line code is selected that avoids the transmission of d.c., ensures adequate timing content and allows in-traffic monitoring. The last two requirements are common to an optical system, but as we do not have positive and negative light pulses available, the best method of implementation might be different. The present codes used for conventional wire line systems have evolved only as a result of considerable practical experience, and obviously it is not possible to predict what codes will eventually prove the most effective and

efficient in optical systems. There is no point in going to a complicated code until more practical information is available on how optical systems behave and some of the key components develop. This point is illustrated by the fact that any system chosen today would almost certainly be some type of binary code. But even this broad choice could be proved wrong; with the improvement of lasers and the associated driving techniques based on optical feedback described in part two, ternary operation is quite feasible and could be used if it proves advantageous. The natural choice for this trial is therefore a code which satisfies the basic requirements and is simple to implement. Such a code, which would also be compatible with an adaptive equalization scheme, is described in part two.

Power feeding. Possibly the greatest problem unique to optical fibre systems is power feeding, and the optimum solution will differ depending on the type of system and country of installation. For instance, at the lower bit rates it may prove possible in some areas to achieve wide enough spacings for repeaters to be located in, or close to, buildings with existing dependable supplies. In general, however, power feeding along the route is likely to be necessary unless small, efficient, cheap and utterly reliable independent sources become a reality.

It therefore seems prudent to consider in detail route power feeding in any field demonstration, and this can be done either by incorporating conductors into the cable or by laying a parallel separate power feed cable. Unfortunately, either would largely negate the electrical isolation advantage of optical transmission systems. The parallel power feed obviously could be used, but would prove little. Because an integral power feed cable has certain advantages in accommodating route growth and supervision requirements it seems best to use a field demonstration to make a practical evaluation of this technique.

Supervision. In a conventional wire line system the transmission line itself is used not only for power feeding but also as a low-loss supervisory circuit. An all-optical supervisory channel could be devised, but would add significantly to overall system complexity, and probably require amplification at each repeater. If power feed conductors are included in the fibre cable it is obviously attractive to use these for the supervisory channels for at least an interim solution. We also have to consider what supervisory information has to be handled. As with coding, the ultimate supervisory solution cannot be foreseen, particularly as more practical evidence is needed of which parameters should be monitored in an optical system. Indeed, the whole supervision philosophy might be different from a

conventional system. It is certainly desirable to avoid the need for any special remote monitoring of the source parameters. It is preferred to rely on optical-feedback-controlled driving techniques which, with the continuously improving source-life characteristics, should provide the best solution to the problem of supervision.

Equalization. The problem of providing equalization in optical systems is basically different from conventional systems in two main respects. Firstly, optical detectors are square-law devices and hence phase information is lost on detection. Secondly, the source of dispersion in a fibre arises from a radically different mechanism from the skin effect in wire cables, and its magnitude, though smaller, is generally far less predictable and reproducible.

As a consequence of the first point, electrical equalization is relatively less effective compared with conventional systems, causing one to examine whether optical or pre-detector equalization might be feasible. In principle it could be applied to multimode fibres because the angles at which rays emerge from the fibre serve to label the individual groups of modes, each with its own characteristic velocity, and some method of delay compensation²¹ could be applied. It seems unlikely that this would be effective in a practical PTT system, since even with almost perfect fibres the spacings are so long that significant mode mixing will occur, probably further enhanced by joints and microbends. We are thus forced back to electrical equalization, requiring the use of a fibre which introduces relatively little dispersion.

The situation is simpler for single-mode fibres, where the propagation delay correlates directly with the transmitting wavelength, and in principle several optical equalization schemes should be effective. At present this is largely of academic interest as the dispersion of these fibres is so low with single-mode sources that bit-rate-distance products up to tens of Gbit km/s could be transmitted without the need for equalization.

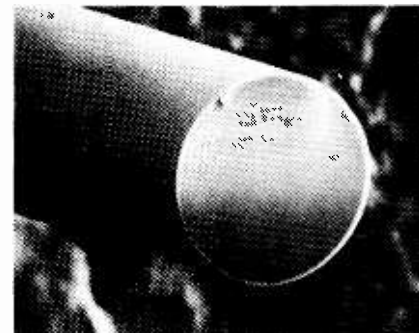
The second point makes it difficult to design the equalization at all, but a prime requirement at this stage is obviously flexibility.

A further point is that in conventional systems, because the amount of equalization required is related to the total attenuation, it is practicable to have an adaptive equalization system. In fibre systems there is no such simple relationship, but with the appropriate choice of coding, an adaptive system as described in part two should be possible, and would obviously be very desirable. Thus, although it may not be practicable to incorporate an adaptive system into the main hardware, it should certainly be possible to use a field demonstration system to evaluate the practicability of building adaptive equalization into a future system.



(a)

Silica fibre of 150µm diameter broken by hand (a) and broken by machine (b).



(b)

The propagating medium

The medium for propagation in a field demonstration involves not only the fibre waveguides themselves but also the cabling, the jointing and the installation techniques. Although these techniques are subjects of study in their own right, certain aspects are intimately bound up with the planning of an optical fibre field demonstration and cannot be divorced from it.

Fibre fabrication. In view of the preferred repeater spacing and capacity arrived at earlier, the wide choice of materials and technologies outlined can be narrowed. First, when allowance is made for additional losses in cabling and splicing, sufficiently low attenuations can be obtained when using high-silica-content glasses. Again, an accurately graded profile can most easily be obtained using chemical vapour deposition. These techniques are flexible and we can contemplate changes in waveguide design or the carrying through of more than one design, provided that the external diameter, stiffness, mass, and other physical properties of the total waveguide are not altered to an extent that could be significant in the cabling processes. It would then be possible to change to single-mode guide for instance at a late stage in the preparation of a field demonstration.

At present most of the available fibre waveguides are the by-products of research programs aimed at the elucidation of many of the remaining problems. As such it is hardly possible to consider the yield and how this can be scaled up. During the preparation for a field trial, though, it will be essential to concentrate on a few uniform products of high consistency. One of these could well be a graded-index fibre with a core diameter somewhere between 30 and 100µm with a gradation of the form:

$$n_r = n_1 [1 - (\Delta n/n) (r/a)^\alpha] \text{ within the core,} \\ \text{and } n_r = n_2 [1 - \Delta n/n] \text{ in the cladding.}$$

It would be reasonable to aim for $\Delta n/n > 1\%$, giving a minimum pulse

dispersion of below 100ps/km when the exponent α is exactly the optimum. A practical pulse dispersion figure may well be an order of magnitude higher due to small errors in α , but may be reduced by mode mixing. The optimum occurs close to $\alpha=2$ for a $\text{GeO}_2/\text{SiO}_2$ core and an operating wavelength near to 850nm. The overall diameter of such a fibre could well be between 100 and 150µm, as this offers a good compromise for cabling purposes. Having chosen such a product many of the parameters will have to remain fixed, and in some respects further research which will point to better designs must be ignored. In part this accounts for engineering margins which may look rather conservative when one considers the rapid progress in this field during the last few years.

On the basis of such a fibre waveguide and the machinery in current use³, fibre could be produced in batch lengths between 2 and 5km. Two or more batches could be produced per day; but, if the yield is to be high, very close control will be required on all parameters at every stage. In the deposition stage, the mass flow of each gas and the temperature of the reacting zone must not only be closely controlled but must be very uniform throughout every pass. Again, during the collapsing stages temperature and traversing speed must be accurately controlled. In this way a very uniform preform can be obtained. This can be pulled into a homogeneous fibre waveguide, but careful control of temperature and profile in the pulling zone is essential. Also, inadvertent changes in pulling speed must be avoided, but judicious use of feedback control from fibre diameter monitoring can be used on this last parameter to improve the uniformity of the product.

Connectors and splices. Joints will be required at each source and detector. Demountable couplings will be required at the transmitter, receiver, and every intermediate repeater. In addition, if we accept the hypothesis that the cable is to be installed in conventional British Post Office ducts, splices will be needed at intervals of between 100 and 500m. Also, allowance must be made for at least two other splices per fibre per repeater section, to take account of accidents during cable manufacture or

installation. Although some prefabrication may be possible, the bulk of the splicing operation will have to be performed in the field.

No real problems are anticipated for the joints between waveguide and detector. High transmission efficiency should be obtained between a small laser source and graded index fibre of the proposed design. However, if the energy is launched with isotropic distribution, as it would be from a light-emitting diode for instance, 25% of that launched will be in leaky modes⁹. Improvement is possible with a laser source. As demountable connections occur comparatively seldom, a loss of up to 1dB can be tolerated, but loss at splices should be about 0.1dB and must not be above 0.25dB. This implies that variations in core diameter should be below 1.0%, and lateral tolerances or eccentricities below 3.5% of the core diameter for good splices with a graded-index fibre.

Further information is required on the effect of such splices on modal dispersion. A large amount of mode mixing is introduced at an inaccurate splice, and in the initial stages this could aid the establishment of modal equilibrium. Beyond that the effects of such perturbations are difficult to predict. If single-mode fibre is required, suitable waveguide design can raise the core diameter to values where the above tolerances can be met², but other techniques can be used to aid splicing. Localized reduction in the normalized frequency of the fibre waveguide spreads the electric field and reduces the effect of lateral displacement. This can be effected in the field with multicomponent glasses by pulling down the fibre, but a suitable technique is difficult to envisage in silica.

Quality assurance. Measuring techniques are largely diagnostic and involve considerable effort in measurement and analysis. With a highly uniform product such time-consuming processes will not be required after the manufacturing procedures have become firmly established. From this point measurements can be geared to quality assurance and will fall into manufacturing and field categories.

In manufacturing, routine measurements⁴ of fibre geometry, core profile and refractive index difference, will be required. These can all be obtained by interference microscopy of a section of fibre²², or by reflection measurement using a laser scan²³. Attenuation measurements will be required but not as a complete spectral scan. The attenuation at the operating wavelength is of obvious importance, but other wavelengths will have to be monitored to keep a check on known potential deficiencies. For instance, measurements at 630nm will indicate when problems from drawing-induced colouration are being encountered²⁴. Dispersion measurements are also

required to monitor uniformity and residual stresses. Steps must be taken to ensure that there are no stresses applied to the fibre during this measurement. Possibly the most sensitive indication of inhomogeneities is the length to modal equilibrium, determined by a shuttle pulse technique.

In the field, measurements of attenuation can be comparatively simple as effects will probably be gross. A portable instrument suitable for carrying out such measurements has been described²⁵. More important will be the effects of installation on dispersion. Fortunately, these are most likely to increase the bandwidth of the propagating medium. Two basic methods are available for making these measurements in the field. A portable apparatus for carrying out frequency domain measurements on the transfer characteristic of the waveguide has been demonstrated²⁶. This has the advantage that coaxial cable engineers are familiar with the technique and existing systems are specified in this way. However, pulse dispersion measuring apparatus could be made simpler and automatic analysis and presentation in terms of transfer characteristic provided.

(To be concluded.)

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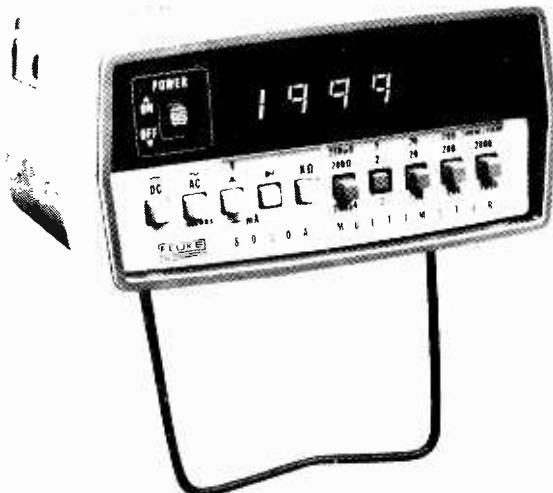
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Earthing, shielding and filtering problems

3—Pick-up problems in electrically-adverse environments

by R. C. Marshall, M.A., M.I.E.E. *Xerox Research (UK) Ltd*

Case 6

Situation: Subassembly amplifier.

Symptom: Hum or high frequency signals, which may have been demodulated by non-linearity due to overload, appear at the output. In some cases these vary if people or non-ferrous objects move nearby.

Problem: Stray capacitance from input to other circuits or objects, or wiring acting as an antenna.

Cures: Reduce source resistance; increase source capacitance; or reduce amplifier bandwidth.

Put a grounded non-ferrous shield or box around the input circuit. The situation is very likely that of Fig. 4(b) (September) and the same cautions apply.

Ensure that there are no nearby ungrounded conductors such as spare cores in multicore cables or structural hardware.

Comments: A closely related problem is that due to stray capacitance from a supply transformer secondary to ground. Despite the existence of the usual electrostatic shield a spurious current can flow along power supply output wires, as shown in Fig. 6(a).

Problems resulting from ineffective or insufficient grounding, shielding or filtering are not easily anticipated or understood, yet this is one of the least-taught aspects of the electronic engineer's art. Difficulties arise from components not shown on circuit diagrams, modes of operation not contemplated by the designer and, worst of all, several such modes operating at the same time. Cure of one mode may not eliminate the symptom — only when all spurious couplings are removed at the same time will correct operation occur. This month, the problem of obtaining good performance in electrically adverse environments is considered. Hence, the major effects are capacitive and electromagnetic pickup. Some precautions are so simple that they should be taken as a matter of course.

The principal component of C in a conventional transformer is between the inner end of the secondary and the electrostatic shield. It can therefore be minimized at near-zero cost by turning the secondary winding inside out, with one of the centre-tap points next to the

shield as shown in the winding section Fig. 6(b). Alternatively, a second shield may be used, connected to the output, as in Fig. 6(c).

These precautions are usually required only if the supply frequency is high or the load at a high impedance to ground. However, if the return resistance is open circuit, in Fig. 6(a) a potential appears on the load even if it is switched off by the switch shown. This can result in damage to semiconductor devices in the load if it is then serviced with a grounded soldering iron.

In the real world completely isolated pieces of electronics such as case 6 are rare, so consider next case 7.

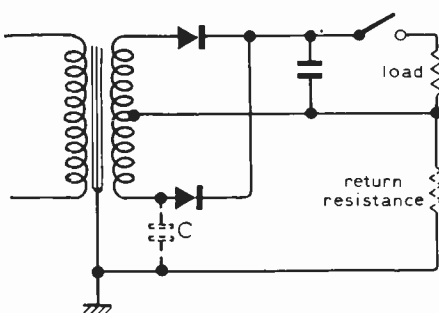
Case 7

Situation: Subassembly with various cables from it.

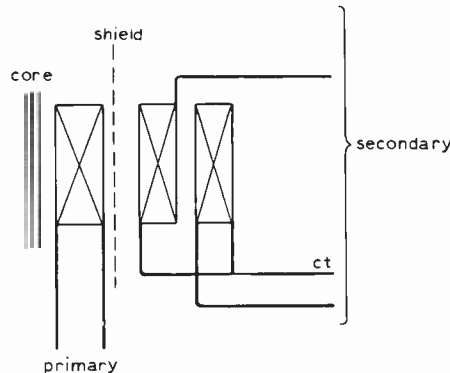
Symptom: Switching clicks or radio frequency signals appear despite all the cures so far suggested.

Problem: Interference is conducted along cables, incoming, outgoing, or power supply and thence coupled through real or stray circuit elements into the circuit. Interference may appear on these cables by direct con-

Fig. 6 (a)



(b)



(c)

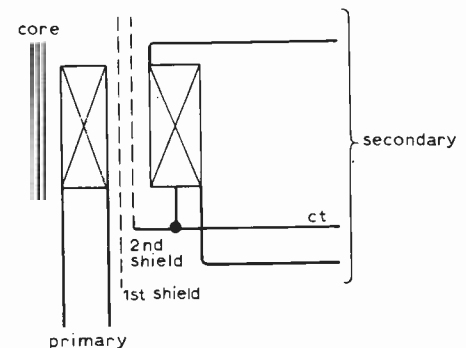
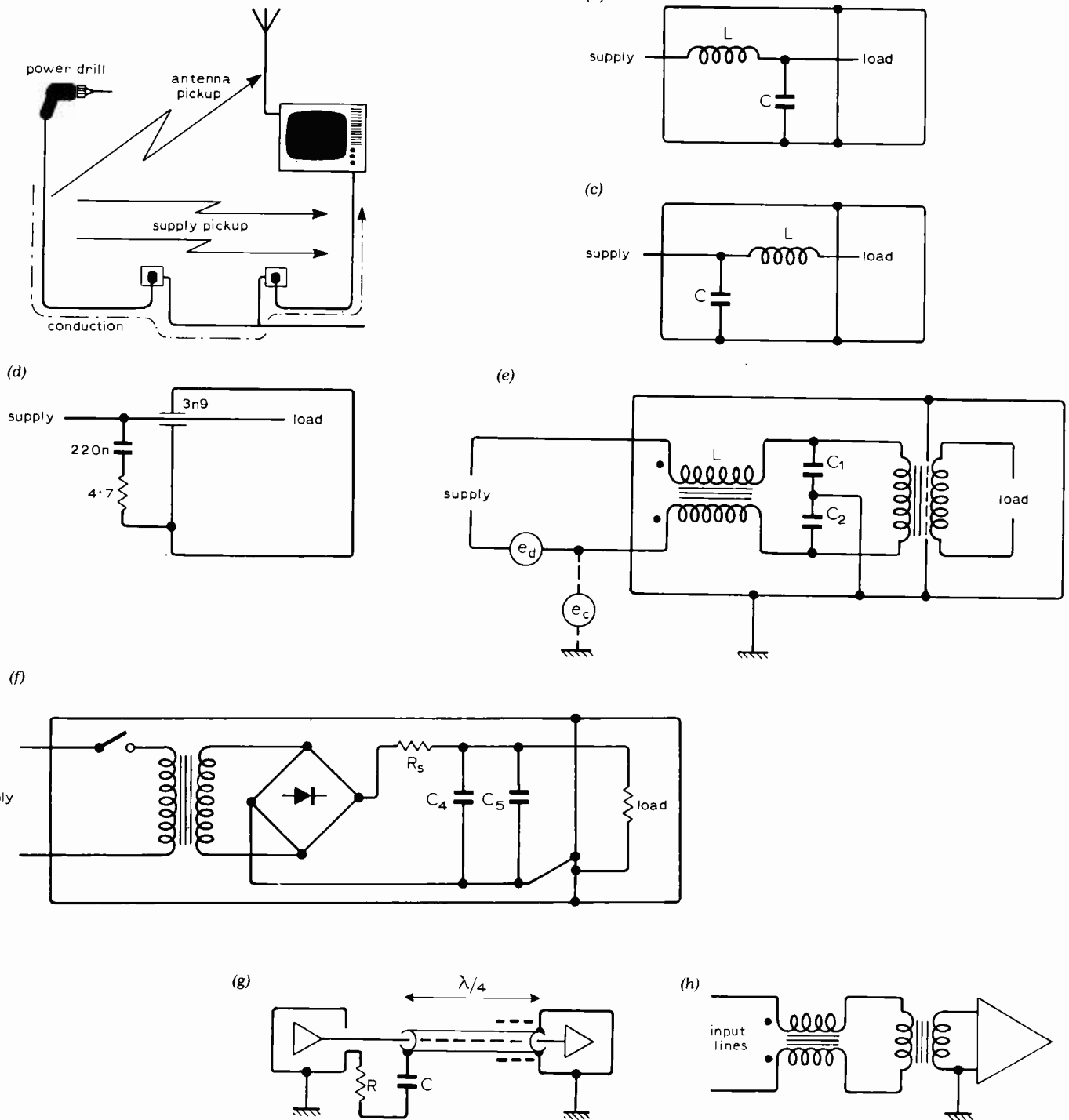


Fig. 7 (a)



duction from other apparatus⁵, or by pickup onto the cable acting as an antenna. Fig. 7(a) shows a typical situation.

Cures/Preamble: The working environment is usually defined by explicit specifications only in military situations⁶ although maximum emission from electronic equipment is defined by a variety of national and international standards. Generally these limit conducted interference from apparatus to 1 to 6mV per 10kHz bandwidth in the h.f. range, but allow rare clicks up to 1V. The commercial radiation environment will depend on the proximity of both deliberate transmitters and unintended sources such as r.f. welders and fluorescent lamps, and

in the absence of direct information can only be assumed to lie somewhere between 1mV and 100mV/metre/kHz. White noise signals increase as the square root of bandwidth, so that one hundred times greater signals will appear in a 10MHz bandwidth system. With single-frequency signals it is just the probability of their occurrence that increases. The choice of design figure requires knowledge of the working environment and of the consequences of trouble; occasional clicks in a programme of music are acceptable, but occasional corruption of a computer program is not.

Susceptibility to an r.f. interference field depends on cable length in relation to the wavelength of the interfering

signal, reaching a maximum at a quarter wavelength, and thereafter fluctuating between this value and zero due to cancellation. To assess pickup, first ascertain the maximum frequency to which the system will respond, then calculate the quarter wavelength. If the cable lengths associated with the system are shorter than this, the voltage pickup will be given by $length \times field$, and, very approximately, will be frequency independent. If the cable lengths are much longer, the pickup will be that corresponding to a quarter wavelength, and will thus increase at lower frequencies.

Actions: Shorten cables.

Output, control and power cables for example should be arranged so that

they cannot couple interference into more sensitive circuits. Use isolated transformer windings and careful layout. Ensure that out-of-band signals cannot be coupled from output to input via negative feedback components. Though not strictly interference, bias voltage at the output of a magnetic tape record amplifier is such an out-of-band signal.

Filter power and control cables where they pass through the shield box wall. The design of filters for this purpose is overshadowed by the uncertainty as to terminating impedance, for this will vary with frequency and application. This results in apparently anomalous behaviour, as a shunt capacitor alone is useless as a filter element if the source impedance is zero, but effective if the source impedance is high. The reverse is true of a series element, such as an inductor, so the two should always be used in combination, as in Figs. 7(b) & (c).

Current flowing through C in Figs. 7 (b) & (c) will add to the circulating current in the ground wire and make the problem of case 3 in Part I worse. This can be avoided, though probably only at high frequencies, if the capacitor is on the load side as in Fig. 7(b). If greater series-mode attenuation is required, filters with three to six elements are used. Very low impedance to the correct ground point is essential; special capacitors are usual⁷.

Resonance of the filter due to the mismatch is a problem which can be avoided by deliberately adding loss to the elements⁸. A simple example of this is encountered in the distribution of low voltage supplies to a number of separately shielded stages using feed-through capacitors for high-frequency decoupling⁹. If low-frequency decoupling is provided by a larger capacitor in parallel, its lead inductance will form a parallel resonant circuit with the feed through at some higher frequency. This can be damped by the use of a series resistor as in Fig. 7(d).

The inductor L has to carry the circuit current without saturation of its core. If the current is appreciable, then inductor bulk and cost will be appreciable too. Economies can be made where the go and return wires run together, for most interference will be common mode, that is between the wires taken together and ground as shown by the generator e_c in Fig. 7(e) Here the sense of the two identical windings on L is such that the supply current does not magnetise the core, so it can be smaller. Consequently, the inductor has no effect on the differential mode interference voltage e_d — this will be attenuated only by the supply impedance and C_1 in series with C_2 . On the other hand common-mode voltage such as will predominate from radiation pickup and ground potential differences will be attenuated by L and C_1 in parallel with C_2 .

Low-cost precautions: Use as filters

components already required for other purposes, by careful choice of configuration and layout. For example, in Fig. 7(f) the on/off switch shares a compartment with the supply transformer so that supply wiring is well away from the load. The resistor R_s is required to limit peak diode current, and together with the transformer leakage reactance it forms the series element of a filter. The electrolytic reservoir capacitor C_4 acts as shunt element, augmented at high frequencies by the ceramic capacitor C_5 .

Choose the input circuit configuration for minimum pickup. The situation is like that of Fig. 2 (August), the only difference being that the e.m.f. JK arises from a different source: the effect of C_3 is greater at high frequencies so that balanced cable becomes more desirable, and skin effect may effectively separate currents on the inside and outside of the shield so that coax acts as triax.

If the input cables are of appreciable length and particularly at those frequencies where they are an odd number of quarter-waves long, the proposal in Fig. 3(b) (August) is unsatisfactory, as the resulting resonance gives the ungrounded end of the shield a very high impedance, and consequently high potential. These resonances can be damped by loading the outside of the cable with lossy ferrite rings at the grounded end (where the shield current is highest), or by providing shunt damping at the ungrounded end, (where the voltage is highest). Both techniques are illustrated in Fig. 7(g). They have the merit of converting unwanted r.f. energy into heat, rather than reflecting it.

If the subassembly is a receiver, it will have an antenna cable which can often be balanced as in the previous paragraph, but cannot be filtered quite as easily as a power lead! Often there are electronics that can be driven into non-linearity prior to the bulk of the selective circuits. Interference then intermodulates the wanted signal, and no amount of subsequent filtering will remove it. The cure is to design carefully the distribution of gain and selectivity in a receiver, and, in particular, to avoid the use of wide-band preamplifiers¹⁰.

As indicated in Part I (August), balanced inputs distinct from the ground connection are desirable. However, at high frequencies balance becomes increasingly difficult to maintain, and the dominant need is to minimize the common-mode potential by multiple grounding of all box and cable shields using as many parallel paths as possible to lower the reactance. In a sense this is the opposite of the low-frequency technique — changeover should be at a frequency somewhere between 50kHz and 1MHz — but both can be combined if twinaxial or triaxial cables are used as in Fig. 5(c), (September), or if a cable shield is grounded only at r.f. by a capacitor (as in Fig. 7(g)

if $R=0$). A method of improving the r.f. performance of balanced inputs is the common-mode choke¹¹, already mentioned in connection with power supplies. It is only effective at high frequencies, and is usually used in conjunction with other balancing devices, that take over at low frequencies, as in Fig. 7(h).

Sometimes it is possible to eliminate interference at source, though this is usually difficult and time-consuming. The suppression of thermostat contacts or vehicle ignition systems¹² are examples of this.

Next article discusses the effects of purely magnetic pickup.

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Announcements

Customs and Excise have issued a VAT leaflet correcting their earlier list of electronic components attracting a VAT rate of 12½% as opposed to 8%. The substance of the change is that only plastic encapsulated Zener diodes (Section K, sub-section iv) attract the higher rate of 12½%.

BASF (UK) have moved their offices from Knightsbridge to Haddon House, 2-4 Fitzroy Street, London W1P 5AD.

CBS have ordered two automatic Tachos 12 cassette loading machines from Hayden Laboratories for CBS's Aylesbury factory. The Tachos 12 loads up to 50 cassettes at four a minute, say Hayden, and is the fastest yet developed. This is their first sale in the UK.

Continued from page 50

A prejudice against engineers

The child who intends to become an engineer "will be fortunate if any of the teachers in his science sixth have any but the remotest contact with engineering." This assertion was made by Sir John Baker in a presidential address at the opening of the 138th annual meeting of the British Association for the Advancement of Science. "The child will spend some of his leisure listening in, watching television or reading the newspaper. The media do give some time and space to engineering achievement but without exception, whether it is successful space travel or winning oil from the North Sea, it will be described as another 'triumph for science'. It would not be surprising if even the brightest child became confused."

Sir John's explanation was that scientists had continued to cultivate their political influence despite successful pleas for government money to carry out fundamental research. The money had led to "an extraordinary era" which was "unplanned and influenced by unrelated and largely fortuitous factors; unrelated but in their cumulative effect disastrous to the economic health of the country." The unrelated factors included the loose use of ill-defined terms, where the once honourable title "Engineer" became "Scientist" or "Technologist", the development of television and other popular means of communication and the great explosion in higher, particularly university, education.

The opportunities that existed after the war for rebuilding our industrial and engineering base had not been grasped. Quoting former president Sir Alec Cairncross in 1971, he said: "Post war discussion was dominated by what were thought to be the achievements of science in wartime. In fact these achievements were in large measure the achievements of scientists rather than of science and, what is more, scientists acting as technologists, that is, helping to produce military hardware. The necessary scientific knowledge was largely available before the war; it was the engineering know-how that had to be created."

He did not believe that the reason for the lack of status of engineering could be laid entirely at the door of human snobbery. Cambridge University, after all, had produced more graduates who had read engineering than any other subject, certainly any other science subject, but it was frightening that in the last three years the proportion had dropped to below 9%. Nevertheless, he thought it possible that a mistaken idea of status and glamour could have been

produced by the expansion in higher education, and the susceptibility of school children to the influence of their teachers and the mass media, "all of whom had somewhat distorted ideas about science and engineering or, at least, about the respective roles of the people they described as 'scientist' and 'engineer'."

The result of all this has been, he said, that scientists have had little or no direct effect on society, since the scientists, having themselves been deceived, took little or no part in what had been regarded as engineering work, and carried on with perpetuating their own kind and increasing their facilities, "believing that this would enrich us all."

The engineer as presently defined had to work under more pressing restraints: "The public have been so pampered for generations that they take our engineering marvels for granted. They no longer realise that the machines and structures on which they depend, the kidney machines that keep some of them alive, the complex equipment we sell abroad to pay for our food, must all be conceived, designed in every minutest detail, fabricated to fine limits from the right materials, put together and then they must work. . . . The demands, intellectual and in every other way, of the engineer's work are of a higher order than those facing the scientist". If we failed to attract into engineering a far greater proportion of those with outstanding ability "we will not survive as an effective people." He confessed he was "irritated" with industry and the professional engineering institutions for not being more active in putting their own house in order, and "with the individual engineer for his smugness in not lifting a finger to raise his own status."

Medical research

When the first Spacelab flight is made in the early autumn of 1980, launched by NASA's Space Shuttle, it should be carrying an electrophoresis experiment. Electrophoresis is the movement of suspended particles under the influence of an electric field and the movement of such biological particles is a widely used aid in medical diagnosis, particularly of cancer and heart disease, and in immunology. The technique is used to separate some of the rare elements from transfusion blood but, on earth, the separation is limited by gravitational effects. In space the process could be made much more efficient.

The British Aircraft Corporation say they and Electronic & Space Systems have completed a study for the European Space Agency of the feasibility of developing a general purpose floating zone electrophoresis experiment which could be carried up with Spacelab. The

technique has been developed by the Protein Fractionation Centre of the Scottish Blood Transfusion Service at Edinburgh, under the leadership of the centre's scientific director, John Watt. The British Aircraft Corporation have been studying ways of putting the biological samples into spacelab, and building the necessary control equipment.

Further notes on the self-setting time code clock

The following list of corrections and explanations will be helpful to readers of the time code clock articles in the August, September and October issues.

Receiver Fig. 1.

The ten turn potentiometer can be a 200 or 500 ohm cermet type. Signal strength meter movement should be 100 μ A f.s.d. The capacitor across T₁ primary should be 4,700pF not 47n.

Decoder Fig. 4.

The capacitor across pins 10 and 11 of IC₇ and C₂ should be non polarized types. IC_{12b} is half of a 7420 and not a 7470 also, pin 11 should be pin 13. Emitter resistor of Tr₅ should be 4k7 and not 47k Ω as shown. The resistor on pin 2 of IC_{9d} is 1k Ω .

Seconds counter Fig. 6.

The transistor on pin 5 of IC₁₅ and Tr₉ are both BC182 types. IC₁₇ is a 7400. Two gates are marked IC_{17a} but pins 11, 12 and 13 should be 17d. C₄ and the capacitor between pins 10 and 11 of IC₁₅ are both tantalum. On the last-mentioned the positive end goes to pin 11. The pin numbering of the 747 displays is incorrect. Connections as shown in Fig. 11 should be followed.

GMT to BST converter Fig. 9.

The i.c. numbering does not follow on from previous diagrams. IC₂₃ is a 7400, IC₂₄ a 7408, IC₂₅ a 7432, IC₂₆ a 7486, and IC₂₇ is a 7240.

Components list

IC marked SN7412N should be 74121.

Because the op-amps in the receiver are used with an unconventional supply it is possible that IC₃ will not fall below 2V in the no signal condition. This produces a permanent a.g.c. voltage on the emitter of Tr₁ and, hence, a reduction in gain. Several popular brands have been tried successfully in the design but Texas types are recommended throughout. Alternatively, the bias on Tr₁ can be altered to increase the base voltage to around 3V.

Alive and just kicking

The state of audio as seen from Harrogate

The audio market would still appear to have life in it, and although views among exhibitors at Harrogate's Audio 76 exhibition in September were mixed, most might agree with the exhibitor who said: "In spite of inflation and all the rest of it, I wouldn't be very surprised if we had a very good year."

It seems clear that the public is becoming more discerning, paying less attention to either specifications or the exhortations of more or less trustworthy reviewers and more to the evidence, however wilful, of their own ears. Money that would once have been spent on radiograms is buying music centres, and the music centres are becoming more refined. Aiwa may claim that they were the first to produce a "true hi fi" music centre with Dolby noise reduction but Dolby, without which neither multitrack recording at one end or the consumer cassette explosion at the other could have happened, is, it seems, no longer enough. Next year a Dbx option will be available on at least one cassette deck as well as Dolby, and BASF, most of whose machines are made by Aiwa, are already offering DNL and Dolby on the 8200 stereo cassette deck.

Connected with these additions, ironically, is some movement away from cassettes. Dbx, for example, can be used with records as well as tape, and one exhibitor remarked: "A lot of people start off with a cassette deck but within six months they want a record deck." Part of the reason, he said, was that cassette prerecorded material quality was so poor, but in any case the choice of material on cassette was still limited.

One consequence of the music centre and cassette boom has been the proliferation of tape coatings. The extent of the problem was made clear in an article in September's *Practical Hi Fi & Audio*. That some tapes give better results than others is beyond doubt, but the customer has to use different tape bias for most of them. In addition, the man who sets up his machine for the tape he thinks preferable is unlikely to be able to hear the prerecorded material he wants on tape, adding to the slight tendency to move back to disc: BASF,

for example, said there were only about two dozen titles on Ferrochrome. Pyral, who have just introduced the Optima pure microferric tape to complement their Maxima, which has a slight doping of cobalt, claim to be conducting market research to discover what machines the public are using and on what settings, presumably so that they can design a tape to suit. While this a novel approach perhaps things are bad enough as they are.

One cassette machine producer, NEAL, said that often the customer was sold tape that needed a great deal more bias current than the machine he had bought was able to deliver: "The effect is to exaggerate high frequencies. They say, 'You might get an increased high frequency response,' but of course you will, because the machine is under-biasing the tape."

Neal is a good illustration of how useful the tape cassette has become in fields other than hi fi. NEAL make a four-channel machine which is used for instrumentation and data recording, though the cassette is mostly a secondary medium in many cases, providing a quick reference to the highlights of a data sequence. One example was e.c.g. recording in hospitals. Two tracks are used for data, one for a time track and one for a spoken commentary, perhaps by a surgeon who interprets the data tracks.

Some British manufacturers, who may have an axe to grind, think the public is tiring of flashy dials and knobs and moving towards a simpler, more elegant — not to say more "British" — approach. One said that although British equipment once looked old-fashioned it had now become more

attractive. The evidence for this seems slender, unless you are prepared to attach importance to good but unrepresentative amplifiers such as that made by Naim which have no tone controls at all.

The amount of available power from amplifiers seems still to be increasing. Many manufacturers thought that this had been one of the effects of greater use of i.c. technology and of a continuing tendency to inefficiency in loudspeakers. Integrated circuits make the initial design easier, and therefore cheaper, they make servicing easier, and larger output stages can be put in the same amount of space that used to be occupied by all the electronics from preamp stage onwards.

The public, if they are aware of the new technology, seem less impressed by the letters "i.c." than "f.e.t.", but they do want higher power. So that while "i.c." occurs rarely as a sales point Trio, for example, make special mention of their "complementary Darlington power blocks," which include the output transistors, driver stages and input stages to the power section in the form of a differential amplifier. Marantz are also plugging their use of complementary output stages and lower feedback, leading they say to less transient distortion, and direct coupling. Trio also claim to have compensated for power surges on one channel causing temporary stereo image shifts by building separate power supplies for each channel, though how much this worries most listeners remains to be seen. One device that seems to have been taken up by audio manufacturers in no small way is the l.e.d. "People like to see flashing lights," said one exhibitor, and typical applications are those like the "tape run" indicator on the NAD 900 cassette deck. Like most machines of its type it had front loading and two large VU meters.

One reason for the growth of music centres has been that it is only the enthusiast who is prepared to make separate decisions about each component of the audio system and then undertake to match and connect them all up, so that while the music centre market is moving upwards in quality there is still a gap, though a smaller one, between than and what most regard as the hi fi market.

One of the most difficult matching problems for the non-technical buyer appears to be the power amplifier and the speaker. It has often been argued



Signalmaster 8, an unusual tuner design available as a kit from Doran electronics at around £100.

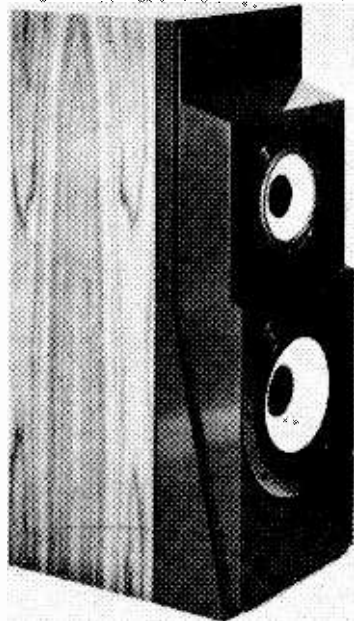
that the best way round this is to combine the two, and Alice (Stancoil) have gone one better than previous attempts by using the current dumping circuit technique developed by the Acoustical Manufacturing company, probably the most significant, if not the only development in audio this year.

Alice emphasise that the speaker amplifier is as suited to domestic as professional use, though the name "Quality Assessment Monitor," abbreviated to QAM, and the fact that the IBA were involved in its design may intimidate some punters. The amplifier feeds 100W into a four unit loaded bass reflex speaker designed by Peter Keeley. It can be used with any preamplifier, though the tendency for manufacturers to produce integrated power and preamplifiers restricts the customer's choice a little. Alice are bringing out their own preamplifier, the PSC1, with a number of features which make it more flexible than most: to name but three, the pickup amplifier is mounted in a plug-in module which can be detached, placed near the signal source, and connected to the control unit via an extension lead; many of the outputs are duplicated on phono and Cannon connectors; and there is a separate 10W amplifier for headphones.

Other manufacturers have said that the combined speaker and power amplifier has the disadvantage that it needs a separate mains lead (to which Alice reply that so does an electrostatic), and that it can be often difficult to service, since a fault cannot so easily be partly diagnosed, as is often done, over the phone. That the customer must decide for himself when he hears the Alice combination. One trade comment was: "The public is not ready for an integrated speaker. I'd like to do it that way — it's the proper way to design the beast, but they're not ready for it yet."

There were some other interesting views on how closely the trade and press were in touch with public taste. For example, Audiomaster, Rogers and Chartwell are all producing the LS3/5A under licence from the BBC. Those who have heard the speaker say that it is a remarkable piece of design, and it becomes even more impressive, it appears, when compared with others in a blindfold test where all the speakers in the comparison are behind an acoustically transparent curtain.

Yet the very combination of qualities that make the speaker such an advance — its good sound combined with its small size — appear to be responsible for a certain prejudice against it. Among reviewers who are not accustomed to quite such good performance from such a small speaker the tendency is to allow its smallness to prejudice their assessment of its performance. Some dealers have had to be convinced that such a small speaker is worth its £140 or so, not because the public wouldn't pay that much but because of their own assessment of the product:



Leak 3080 loudspeaker, one of the 3000 series referred to in the text.

Allan Coleman of Audiomaster said: "Dealers still equate size with price. In that respect the public is ahead of the dealers." They were coming round, though, he said, and in two months Audiomaster had built up a dealer list of 45.

Another example of under-rating the intelligence of the customer was Dual's misplaced assumption that potential customers might be impressed by their playing records upside down. Fortunately such imbecilities were not much in evidence on other stands.

Indeed, anyone who imagines that the public will swallow anything put in its trough would do well to note the neglect of quadraphony. Four-channel sound is bedridden, and its illness may be terminal. Already manufacturers who provide four channel options are either building in decoders switchable to more than one system or, like Marantz, offering extra plug-in units according to which system the customer prefers. A similar example of resignation to the inevitable was Shure's decision to market their M24H cartridge on the basis that it was suited to CD4, SQ, QS, or two channel stereo, and surely there is no more eloquent description of the state of things than Sansui's demonstrating four channel amplifiers through only two sets of speakers. Sansui's man explained that they had been unable to get a large enough room in time for the exhibition. "We felt that it's got to be demonstrated in a large room, and in any case there's a continuous demonstration at our Lon-

don showroom." He felt that public interest in four channel was still strong, and would be further stimulated by the BBC's H matrix tests. Back at Shure, though, it was pointed out how very few four channel records were yet available, and how the one they were playing cost £7.

On the other hand the demand for direct drive turntables has been strong, despite the feeling of some parts of the industry that it has been the result more of a skilful marketing exercise on the part of the Japanese manufacturers than of any intrinsic merit in the technique. "We've had a look at direct drive," said Connoisseur, "but we can see no real advantage apart from the fact that people are asking about them. They have fewer moving parts and so they should be quieter, but price for price we think our BD1 has the advantage. We think you can get greater reliability using a belt drive with a simple synchronous motor."

The periodic urge to counteract real or imaginary defects in speakers has also reasserted itself. Last season the talk was of linear phase and a number of manufacturers have climbed aboard the bandwagon but, as with Doppler distortion before it, what once seemed to be the hidden key to making loudspeakers sound less like themselves has turned out to offer less than was originally claimed for it. At times it seems that speaker makers suffer from the delusion that, if only they can find it, one discovery is more likely to produce the perfect speaker than the tedious business of moving by small steps towards eliminating imperfections.

To be fair, Rank, for example, would not claim that the use of "time delay compensation" is any such panacea, and their description of the new Leak 3000 range of speakers indicates a step by step approach in more senses than one. But then they could hardly claim that for a technique which would seem to differ little from the linear phase approach: because of the different sizes, depths and positions of the low, mid and high frequency units the points of origin of the different frequency sounds are not equidistant from the listener. Rank have therefore stepped the baffleboard and mounted the different units on each of the steps. This, they say, improves the depth and transparency of the sound image even when listening to one speaker.

This year there seemed to be only one recurring theme in the conversation of those on the stands, but it had nothing to do with new techniques or equipment. The trade seems unhappy about both the number and content of hi fi publications. It is assumed that the magazines ought to exist for the benefit of the trade rather than the readers to whom these journals claim to provide information. Perhaps it is a fallacy that those magazines ought to make some effort to dispel, if it is not already too late. JTD

Digital wristwatch

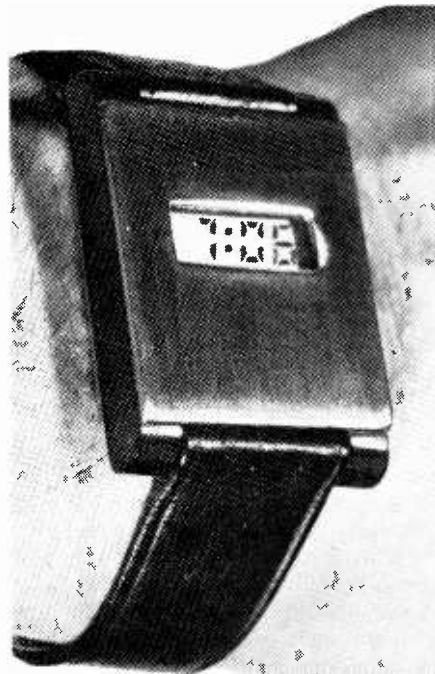
2—Case construction and assembly

by P. A. Birnie

The prototype watch was enclosed in a case simply made from a piece of perspex and two plates of stainless steel. The perspex plate holds the completed module, the two mercury cells, and setting switches. Fig. 15 shows the sizes of holes to be cut in the $\frac{1}{4}$ in perspex plate and care should be taken over the cutting of both the mercury cell and module holes. The diameter given for mounting the mercury cells should be used for cutting the holes rather than using a cell as a template since the tolerance in cell size could result in replacement cells not fitting the enclosure. The module itself should be used as a template when cutting the large rectangular hole so that a smooth sliding fit is achieved to allow the module to be pressed against the front plate when the back plate is screwed on.

Some explanation is required of the method of making and operating the setting switches S_1 and S_2 since they are not switches in normal terms but rather raised contact areas which are shorted to the case by a convenient metal object e.g. a pen or a paper clip. Fig. 15 shows the position of the two domestic pins which form the setting contacts, effectively hidden by the watch strap when the watch is worn. The precise positions of the watch strap peg holes and setting contacts depend on the strap to be used and for this reason the front-back position of these holes is not given. If a metal watch strap is to be fitted then care must be taken that under normal conditions of usage i.e. wear and repeated removal, the strap cannot accidentally short the setting contacts. Whichever type of strap is used, the setting contacts should be kept as far as possible from the back of the enclosure to prevent problems with moisture and general accumulation of foreign matter.

Drilling the small post and terminal holes may pose problems due to the relatively poor availability of drills of the required diameter but from past experience a hot pin will create neat holes which in any case are masked by the strap and so need not mar the finished appearance of the watch. Before gluing the contact pins into the perspex, a slot should be cut to allow wires to be soldered on to the inner ends



of the pins without interfering with the module — the position of this slot is shown in Fig. 15.

The battery connections comprise the final parts of the design and these are made from four scraps of 1mm single-sided printed circuit board. Each piece is cut to 8mm diameter and then sanded down to be a loose fit in the battery holes. Using a damaged scrap of gold-plated edge connector as a source, a piece of gold-plated copper is soldered on to each of the contacts taking great care to keep solder away from the gold surface of the contact. A short length of miniature flexible wire is soldered on to each contact ensuring that when the cell sits on the contact, it can only touch the gold-plated area otherwise corrosion of the cell case will quickly take place. The cell manufacturers recommend the use of Austenitic 18/8 stainless steel, nickel-plated stainless steel or Inconel as contact materials but as these are not readily available, the above method was felt to be equally good. It is now necessary to cut some

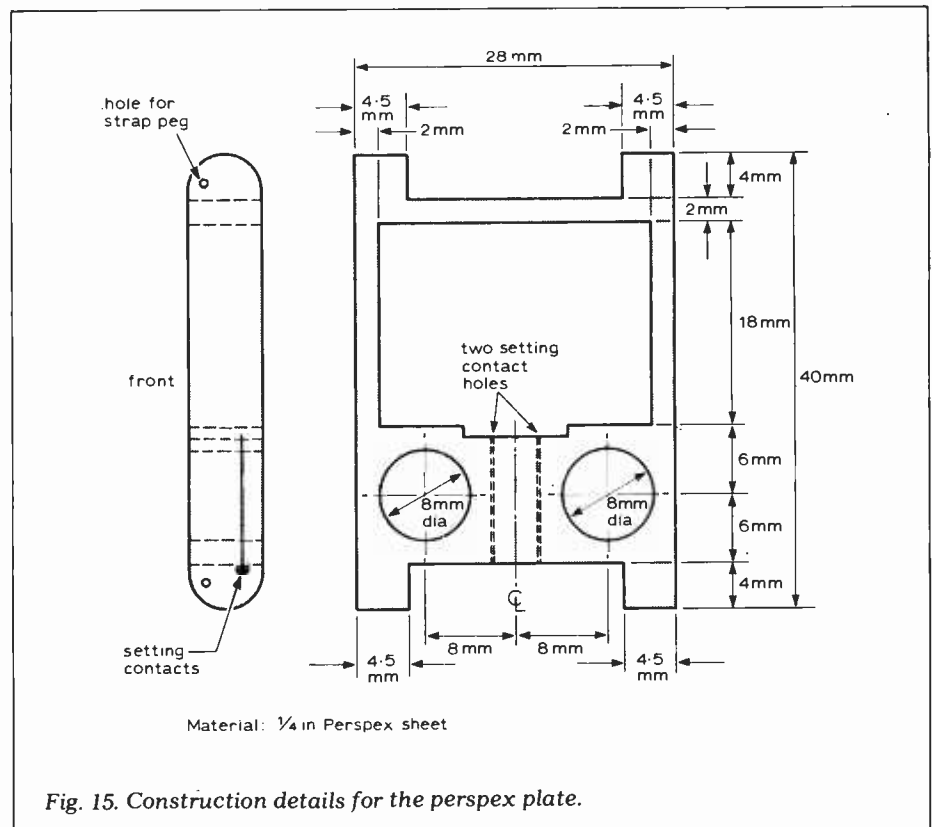
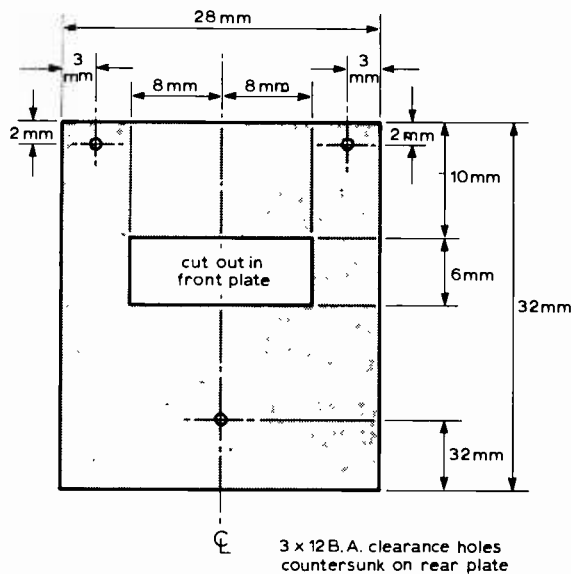


Fig. 15. Construction details for the perspex plate.



Material: 1mm stainless steel sheet

Fig. 16. Dimensions for the front and rear plates. Note that the holes are only drilled in the rear cover.

small grooves in the perspex to allow the four battery wires access to the module space while still keeping a flush finish to the perspex block and this is easily done using a small file.

Turning now to the front and back plates—these were cut from 1mm stainless steel in the prototype and Fig. 16 shows their dimensions. The back plate should be used as a drilling template when drilling the three fixing holes in the perspex block, and both back and front plate should then be rubbed down using very fine wet-and-dry abrasive paper until a pleasant surface finish is achieved and all surface defects are removed. It is as well to rub down all surfaces and edges of these plates paying particular attention to the inner surface of the front plate where this will contact the display, to ensure that no burrs exist which may cause sealing problems later. Having drilled the three 12BA holes in the perspex block, it is necessary to fit nuts to the front face of the block by drilling slightly undersize holes in the top of the block and then carefully pressing into these holes 12BA nuts, using a hot soldering iron.

Final assembly

The front plate and block should be roughened with a small file where they are to make contact with one another and then both should be thoroughly cleaned in hot, soapy water. After securing the two front battery contacts in position, the 12BA fixing screws are screwed into the perspex block until they are flush with the front face, and their ends covered with a small blob of silicon grease to prevent the threads

being Araldited in position! The front plate can now be glued on to the perspex block, ensuring that a good seal is obtained round the periphery and that the plate is absolutely square with the block. When the glue has dried, any excess should be removed and the perspex block polished up using fine wet and dry sandpaper followed by "Brasso" or "T-Cut" car bodywork cutting fluid. The last-mentioned will allow a very good surface finish to be achieved on the body of the watch.

Assembly of the complete watch can be started by smearing a thin film of silicon grease on the reverse of the front plate — later to act as a moisture seal on the display front. The display is placed into the display mount in the completed module and this is placed into the cavity in the watch body. The four battery wires can be trimmed and soldered in place, not forgetting that a link is needed between the V_{DD} land and the earth area by the trimmer, and in addition a single strand of bare tinned copper wire should be soldered to this earth area, later to be sandwiched between the case back and perspex block to earth the back of the watch. To allow the case and plate to come together, this wire should be partially recessed into the block — taking care that it is sufficiently proud to cause a connection to be made.

The last connections to be made are between the setting contacts and S_1 and S_2 lands. When these are completed, and after a careful check of wiring, the batteries can be placed into the holders. Before screwing the back into position, three scraps of dense foam rubber are

placed above the module and battery contacts so that when the case back is screwed on, they press the module and display together and ensure a good battery contact is made. A smear of silicone grease round the sealing parts of the perspex block will ensure a watertight enclosure and after applying this, secure the back by means of the three countersunk-head 12BA screws.

The watch should now be "running" and can be set to the correct time by reference to the table in part 1. If a faulty display is given, the rubber placed between case back and module should be increased in thickness until a good display is obtained.

Announcements

Farnell have formed Farnell Audio Visual Ltd to separate their A-V activities from the domestic consumer business. Managing director is A. E. Long, and the new company will operate from Kenyon Street, Sheffield.

German power semiconductor makers Semikron International have formed a South African subsidiary at Koedoespoort, near Pretoria, headed by Ignalus M Burger.

Pye subsidiary Newmarket Transistors Ltd have appointed representatives in Denmark, Italy and South Africa. Tage Schouboe of Kobenhavn, Denmark, will market thick film devices, and Syscom Elettronica of Milan and TV Engineering (Pty) Ltd of Doornfontain, Johannesburg, will sell thick film and discrete devices.

Power supply makers Coutant are selling through component distributor Celdis. An agreement effective October 1 makes Celdis Coutant's first appointed distributor for the SU series of plug-in power supplies, the first in a range of power supply components. Celdis now have a stock of £15,000 worth of units.

Microprocessor manufacturers Zilog have appointed Cramer Components as exclusive distributors in the UK and Ireland. Cramer handle AMD, Motorola and Texas m.p.u.s. but say that the Zilog franchise is complementary. Cramer are based at Uxbridge Road, Ealing.

The Ministry of Defence has ordered equipment for pre-flight testing digital airborne navigation sets worth £250,000 from G & E Bradley. The equipment will be used on new Tacan and DME systems as well as the older Tacan equipment used in all NATO aircraft.

Zoom Television have been acquired by Plantation Holdings, parent company of Television International for an initial payment of £200,000 and further payments of £57,000 in each of the next two years, all the shares to be acquired immediately.

F. W. O. Bauch Ltd of Boreham Wood became sole agents for Britain and Ireland of Revox hi fi equipment and ancillary products from September 1. Bauch have expanded the staff by 17 to deal with the pre and after sales service requirements of the agreement. The previous agents with C. & E. Hammond, one of whose staff has joined Bauch.

Radcomex 76

RSGB revives amateur radio exhibition

After a period of eight years the RSGB re-introduced their three-day Radio Communication Exhibition, once held annually in London. The exhibition was held at the Alexandra Palace from July 30 to August 1, and visitors to the exhibition, many of whom had been waiting enthusiastically for the "capital city" event, were in for a surprise. The exhibition space was occupied by recruiters such as the RSGB, AMSAT-UK and the London UK-FM group, together with second-hand stalls, components stands and displays by kit manufacturers. Whilst it can be argued that such a mix is no bad thing on the basis of encouraging home-construction amongst amateurs who are becoming increasingly dependent on ready-built commercial equipment, there was nevertheless a great deal of surprise at the absence of the black-box merchants.

An explanation for the shortage of major traders was given by an RSGB representative, in the form of copies of a minute passed on June 6 at a meeting of the Amateur Radio Retailers Association (ARRA), and claimed by the Exhibition Organiser, J. Hitchins, to have been posted to potential exhibitors to the RSGB event about a month later. The section of the minute highlighted in the RSGB explanation was a resolution proposed by W. Lowe of Lowe Electronics. This stated that any dealer attending any major exhibition in 1976 would not be invited to the 1976 Leicester Exhibition, and that dealers who had already paid for space at another major exhibition could have that cost deducted from their fee for the Leicester Exhibition on production of a receipt and their non-attendance at the other exhibition. This ARRA extract had been sent out, unsigned, under the name and address of the Secretary of the ARFA, Tom Darn G3FGY, who is also a regional representative of the RSGB. The RSGB rightly pointed out that the recommendation made by the ARRA did not mean that a trader would be barred from any other major exhibition, but that they would have to write in and apply to take part.

Not surprisingly, many of the visitors to the exhibition felt that they had been let down by the major traders, who had

apparently "blackd" the exhibition (see Pat Hawker's comments, October issue), and many made up their minds to boycott the Leicester Exhibition, to be held October 28-30.

In 1968 the RSGB decided that they would not hold any more exhibitions in London due to the great expense involved and the fall-off in attendance.

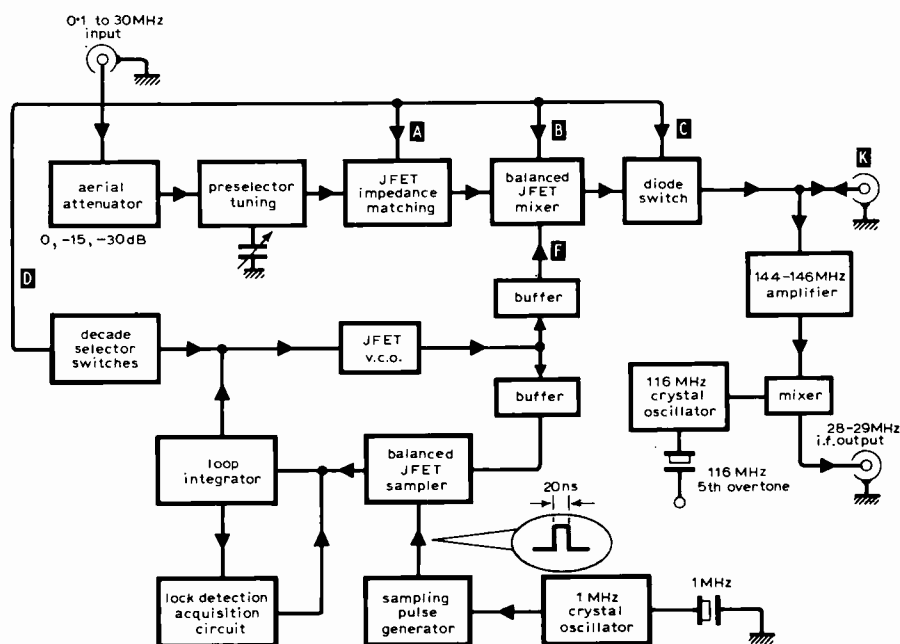
In 1972, the ARRA was formed at a meeting of thirteen traders, who became the founder members. The Association decided to support radio rallies with a view to protecting traders from being exploited by exhibition organisers, attendance at such rallies being considered as an aim of the Association. It also decided to hold an

annual exhibition to replace the RSGB exhibitions, the first taking place at Granby Halls, Leicester, in 1972. In 1975, at the Woburn Abbey rally in August and at the Leicester Exhibition in October, the idea of reviving the RSGB Exhibition was canvassed amongst the traders who, at that time, were in support of the idea in the knowledge that it was to be a one-day rally.

Following this favourable response from the traders the society decided to hold a three-day exhibition instead and informed prospective exhibitors of their intentions, with application details for stand space, in February this year. According to representatives of the traders and the ARRA, most of the major traders replied to the effect that they could not attend because they would not be able to allocate resources to mount a three-day exhibition in London, particularly since at the time proposed they would be well advanced in their preparations for the Leicester Exhibition, which is an established event in their calendar. The ARRA also pointed out that the London exhibition coincided with the peak holiday period when staffing is more difficult to arrange and when, in their view, interest in amateur radio is at its lowest ebb.

It is at this stage that the story begins to turn sour with accusations directed toward both organisations. The ARRA believed that the RSGB were continuing to give the impression that the major traders would be at the London event, knowing that they would not — the only evidence of this is in the surprise expressed by the visitors. Another accusation was that the RSGB had approached certain Japanese manufacturers with suggestions that the boycotting was by their UK traders only. The RSGB, on the other hand, felt that their prospective exhibitors were being pressured not to attend their exhibition, especially after repeated

Block diagram of the Datong model UC/1 up-converter — a general-coverage add-on unit for amateur-bands-only receivers. Frequencies are selected, in 1MHz bands, using two sets of decade switches which control the voltage at D. One set of switches selects tens-MHz and one selects units-MHz. Socket K acts as either the 144-145MHz i.f. output of the 2-metre (144-146MHz) converter input. Point F appears to the balanced mixer as a local oscillator providing 144-115MHz, on 1MHz steps, from the synthesizer.



attempts to talk to the ARRA secretary proved fruitless. South Midlands Communications were one company who initially decided to go to the RSGB event and then changed their minds after, as their representative stated, they were pressured into backing out.

The question which many visitors asked was why the ARRA did not inform the traders of the outcome of the June meeting until July. Tom Darn, representing the ARRA, said that initially he was not going to act publicly on the decision outlined in the minutes, but later he considered it his duty to give traders, who had perhaps hastily committed themselves to the two events, an easy and economical way out of the situation.

As these points can be argued almost indefinitely, it is probably better to accept that the ARRA and the RSGB, who undoubtedly have a great deal of respect for one another, have both acted improperly at some stage in the events preceding the exhibition. Priority must now be given to arranging a meeting between the two organizations to ensure that this unfortunate and unhealthy situation can never happen again.

With both organizations equally determined to continue with their own events (the RSGB are planning an International Radio Communication Exhibition and Convention at Alexandra Palace in May 1977) the next few years will show if the two exhibitions can co-exist, and whether the RSGB can show that the difficulties experienced in 1968 have been overcome.

Low-cost silent r.t.t.y.

Increased interest in any radio amateur field is usually followed by commercial offerings of "black boxes" in place of "knife-and-fork" constructions, and r.t.t.y. communication is no exception.

H.B.R. Electronics were showing a r.t.t.y. video display unit which, with a video monitor and signal source, offers silent monitoring of teleprinter signals. Using this device, messages can be displayed on either a standard 625-line TV monitor, a modified TV set, or a standard TV set with a u.h.f. modulator fitted. The display has a format of seven lines each of 32 characters, allowing readability at a distance of several yards on a 12in screen. As fresh information is received it is written on the last line of the display. When the screen is full all of the lines are moved up one space and the top line is removed. Line feed and carriage return commands in the received signal are ignored by the unit, which generates its own for maximum display utilization, but may be displayed if required. A letter shift code may be inserted at any time. The video output is a composite 1V pk-pk signal, for 75 Ω matching, with internally generated sync pulses. The input accepts Murray (Bandot) code (t.t.l. levels) at speeds of 45, 50, 57 or 74 bauds, a variation of $\pm 7\%$ on the data rate being allowable.

Circuit operation is briefly as follows: the serial input is converted to a parallel form in a shift register and is decoded into an a.s.c.i.i. (American standard computer information interface) code via a r.o.m. This data is stored in a 256 x 6 r.a.m. and read out via a character generator r.o.m. and parallel-to-serial shift-register.

A permanent record of received signals may be taken, using a domestic tape recorder as a back-up store, by recording the audio tone from the receiver. The TD224, which measures 12 x 12 x 3 $\frac{1}{2}$ in, has a power requirement of 15W from an 8 to 15V d.c. or mains supply.

Who needs a g.c. receiver?

Of particular interest was the model UC/1, a prototype shown by Datong Electronics Ltd of Leeds, which converts any existing amateur-bands-only receiver having a coverage of 28-29 or 144-145MHz, into a general coverage receiver of equivalent performance. This unique up-converter, as it is called, was designed by D.A. Tong G8ENN to make available a low-cost alternative to the high-performance g.c. receiver.

The device, which simply connects in series with the aerial lead to the main receiver, gives complete coverage from 60kHz to 30MHz in thirty 1MHz bands selected by two decade switches. To ensure that 2-metre band frequencies do not pass through to the outputs of the unit a 40MHz low-pass filter is used at the aerial input. The unit also adds 2-metre coverage to 28-30MHz receivers. This is done by selecting number 11 on the 'units' decade-switch (see block diagram) causing the voltages at D, A, B and C to go low, disabling the cascode impedance-matching and mixer sections and opening the diode switch, converting the unit into a conventional 2-metre converter.

Design techniques, using e.c.l., t.t.l., c.m.o.s., bi-mos and matched-dual j.f.e.t. circuitry, have ensured that the performance of the complete receiving system is limited mainly by that of the associated receiver and not by the add-on unit. To achieve this, performance factors such as the noise figures, sensitivity, gain distribution, overload properties, intermodulation have been optimized and synthesizer noise sidebands have been minimized. For example, the use of a quartz crystal-controlled frequency synthesizer makes the overall frequency stability equal to that of the basic receiver; instead of conventional tapped r.f. coils the UC/1 uses two encapsulated r.f. inductors for each of the six preselector bands, eliminating a tuning adjustment, saving space and removing the possibility of drift due to moving slugs. The unit, which is stabilized and only requires a 9 to 20V 100mA supply, is protected against

destruction due to accidental transmission by back-to-back diodes capable of withstanding 10W continuously.

Price is expected to be considerably cheaper than a g.c. receiver offering an equivalent performance.

Satellite news

A slide and tape show on the AMSAT (UK) stand gave comprehensive details of the Oscar amateur-satellite series.

Although the Oscar 6 satellite has been operational for four years, it is still managing to transmit better signals, on the 2-to-10m mode, than Oscar 7, which has been operational for only two years. However, latest news from the telemetry beacons on Oscar 6, which send down real-time teletype c.w. data detailing conditions on the satellite, is that its capacity to hold charge in its batteries is now being seriously affected by environmental conditions.

Throughout a single year the satellite receives varying amounts of sunlight, depending on the earth's position in relation to the sun, and the battery suffers in different ways during both the maximum and minimum conditions. For example, in July this year Oscar 6 was receiving a minimum of sunlight and, to conserve battery charge levels, it was necessary to observe strict operating schedules. By February 1977 the satellite will receive a maximum of sunlight and due to its inability to dissipate heat high temperatures will be reached. If the temperature reaches the critical level at which the ageing Nicads cease to function, the satellite may have to be taken out of service.

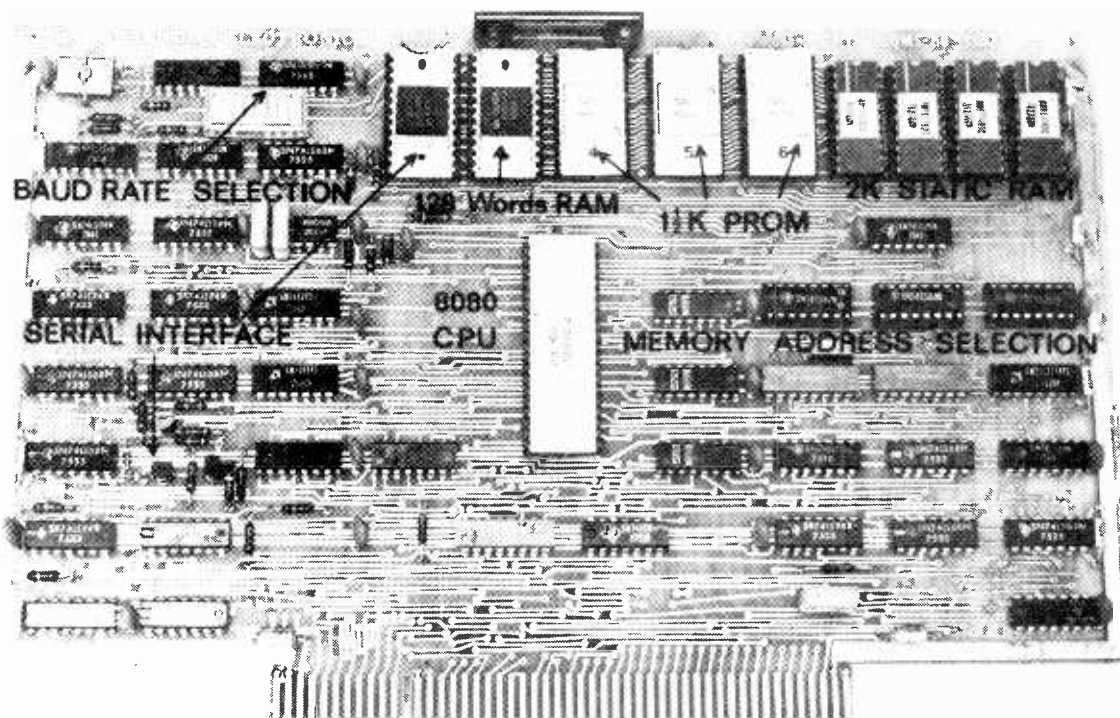
Another problem being experienced by Oscar 6 is that of ionization caused by the high radiation received during the satellites passage through the inner Van Allen belt, resulting in degradation of the depletion layers in the silicon planar transistors.

Design and construction work by AMSAT groups throughout the world is still continuing for the phase III plans for future Oscar satellites. Among these is the v.h.f./u.h.f. microprocessor-controlled stabilized spacecraft which is planned to have an elliptical orbit. This spacecraft should be capable of providing long distance communication for long periods for 70% of the earth's surface and 95% of the world's radio amateurs.

Since Oscar 6 has already exceeded its planned one-year lifetime by almost a factor of four, and it is doubtful whether the phase III Oscar will be launched before 1978, it is likely that the next satellite will be a 2-to-10 mode set to replace this heavily used satellite. This would permit Oscar 6 to be used for special purposes during its remaining operational life. The replacement satellite will probably be almost a duplicate of Oscar 6 but will contain a greater number of solar cells to ensure continuous operation.

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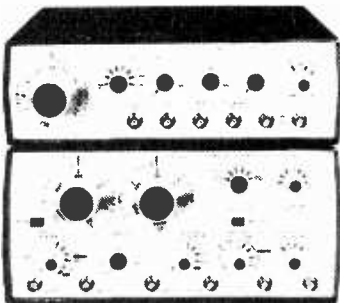
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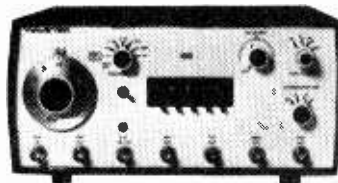
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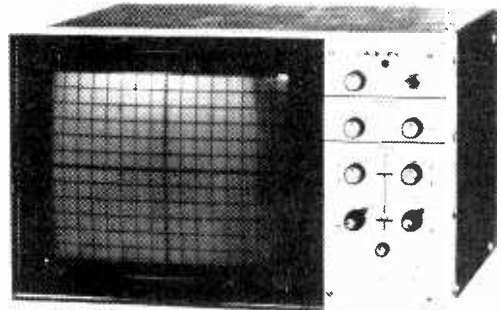
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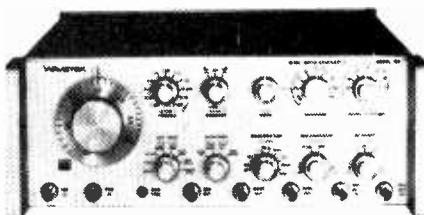
180 Sweep/Function Generator.
185 LIN/LOG Sweep Generator.
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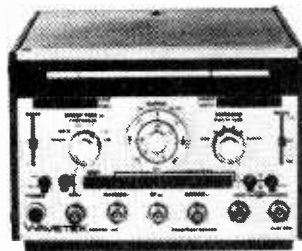
171 Synthesizer/Function Generator.
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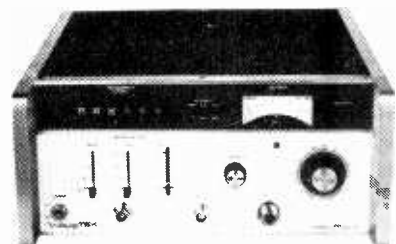
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Using a computer to augment the work of operators

by Stuart Faulkner and Hugh Letheran *Redifon Telecommunications Ltd*

From the earliest days of radio communication the need has existed to monitor the man-made signals present in the radio spectrum. Broadcasting authorities may wish to monitor the news broadcasts of other authorities as part of their news collecting activity. Post Office authorities may wish to monitor licensed users in their territory in order to maintain control of quality in accordance with ITU, CCIR and other international regulations. Military organisations may wish to monitor the radio activities of other powers. While the reasons for monitoring vary widely, the basic problems involved are the same for all users. Each monitoring operator is attempting to locate and intercept interesting traffic in an increasingly congested radio spectrum in which most of the signals he receives are either uninteresting or merely noise. For every wanted signal there may be hundreds of uninteresting ones. This is particularly so in the now very overcrowded h.f. band from 1.5 MHz to 30 MHz.

The technique currently employed by monitoring stations throughout the world is almost without exception based upon a well tried method which has been in use for many years. This is a one man — one receiver situation in which the operator spends his time searching the r.f. spectrum with a continuously tunable general purpose receiver in the hope of making an interesting interception. There are variations of this approach. For example, it is possible, and common practice, for an operator to have at his disposal two receivers. One is used for searching while the second remains tuned to a known interesting frequency. A further variation is called the master-slave technique. In this method a group of operators works together. The master operates a fast tuning-sweep receiver with an associated panoramic display unit. When he locates a signal of interest he "farms out" this intercept to one of the slaves, who tunes to the appropriate frequency and does the monitoring on a conventional general purpose continuously tunable receiver.

None of these techniques overcomes

the fundamental problem of serious overcrowding of the h.f. radio spectrum. An operator searching through a mass of noise and unwanted signals covering a large frequency band in order to tune in possibly weak wanted signals faces a soul destroying, time consuming and very boring task. Experience shows that the problem is not overcome by use of a swept receiver and panoramic display unit. Most operators open up the sweep until the panoramic display unit is showing only a very narrow band within the h.f. range. The reason is, quite simply, that the operator is confused by the mass of signals appearing on a display unit if the sweep covers a larger band.

In addition to the problems of confusion and tedium described above, the "classical" monitoring techniques suffer from another major disadvantage. They are profligate in their use of both operators and receivers and are consequently very expensive. In the one man — one receiver situation, the operator for much of his time is not receiving an interesting signal. In the master-slave situation, the slaves spend much of their time actually doing nothing while the master carries out his search. In either case this inefficiency leads to the use of very large numbers of operators and receivers in order to achieve the required coverage and number of intercepts.

Recent developments

During the last few years there have been two developments which have caused users to reconsider their approach to monitoring and have resulted in Redifon Telecommunications Limited developing equipment which employs a fundamentally different, and superior, approach. First, the existing pool of highly skilled operators has begun to dry up and it is proving difficult to find replacements. The classical method of monitoring is, after all, a very boring occupation. Secondly, we have seen the development of two important new pieces of equipment: the fast switching digitally synthesised receiver and the small, inexpensive minicomputer. Using these two basic

tools, our company has developed CERES — a Computer Enhanced Radio Emission Surveillance system.

During 1972 one of our customers asked us to take a look at the problem of the increasing cost and reduced availability of operators. As we have already seen, conventional systems tend to leave their operators idle for much of the time. Clearly if one operator could control more than two receivers, say four, a marked improvement in efficiency would result. Fewer operators would be needed, and, since they could be used more efficiently, fewer receivers, to achieve the same result. In fact, using our new system it is possible to achieve improvements in efficiency of as much as 50%. The principle is to use a computer to augment the activities of the operator in such a way as to release him from the necessity to perform routine, repetitive tasks. Men and computers each have their areas of special aptitude. A man is very good at recognising and interpreting signals — speech, morse, telegraphy, etc. A machine has limited capacity for these tasks and to perform them at all must be prohibitively large, complex and expensive. On the other hand, a machine performs repetitive functions extremely well: it does not get bored, it does not forget. Once programmed to perform a certain series of operations in a certain order at a certain time, a computer can be totally relied upon to do so.

The receiver

The CERES system combines the special aptitudes of operator and computer in such a way as to leave the operator to perform those tasks he can do best while making the computer perform the routine, repetitive functions. This is possible because of the special characteristics of fast switching digitally synthesised receivers. A synthesised receiver can be made to cover the h.f. spectrum from 1.5 MHz to 30 MHz in increments chosen by the designer. The synthesiser of the receiver used in the system switches in 10Hz increments throughout the range and employs fully electronic switching. Because the switching is digital and electronic it is,

readily suited to remote control and to computer control.

The receivers in the system are subject to computer or manual control at the choice of the operator. It is extremely important that the "feel" of the receiver to the operator, although he is actually operating the remote control unit of a digitally controlled receiver, should be identical with the "feel" of a normal, tunable receiver. In other words, when adjusting the tuning control of the receiver, the operator should experience precisely the same response as he would if using v.f.o. of a standard variable oscillator controlled receiver. This is achieved by the use of a digital optical shaft encoder. A continuously rotatable knob on the receiver control panel, while looking and "feeling" exactly like a v.f.o. tuning knob, in fact generates a train of pulses. It rotates a disc around the edge of which, in the plane of the disc, are a series of radial lines, giving alternate opaque and translucent areas. Light is directed through the outer portion of the disc and a light sensitive diode on the obverse side receives a series of light pulses when the disc rotates, thus generating a chain of digital electronic information on tuning rate, shift and direction.

Since receiver tuning is not truly continuous but simulated continuous tuning by digital control in 10Hz steps, the control of tuning by a computer is quite easy. In fact a 56-bit serial synchronous word with a bit rate of 19,200 bauds is used in the system to control antenna selection, bandwidth, a.g.c. time constant and frequency.

The minicomputer

We have said that two important new pieces of equipment are necessary to this monitoring system. The first is a receiver as described above. The second is the minicomputer. A large number of

proprietary minicomputers are now on the market and selection is uncritical. In general, a particular model will be chosen to suit customer considerations such as availability of local maintenance facilities, previous experience of the same model or maker, etc. The basic parameters which the computer must have as its minimum specification are: 16-bit word length; a central processor with a 32 thousand word main store; a store cycle time of less than 1 microsecond; an instruction time of less than 2 microseconds; and two exchangeable disc store units of at least 1 million words each.

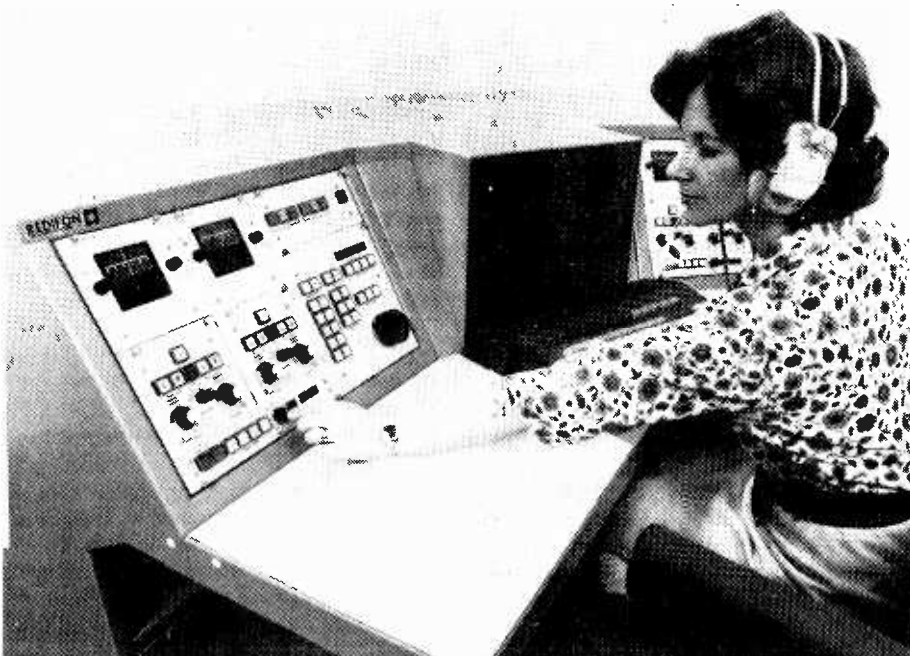
The console

The console, shown in Fig. 1, enables one operator to control four receivers with assistance from the computer. A block diagram showing the signal and control paths associated with one of the receivers is shown in Fig. 2. The operator has access to any one of the four receivers at a time for manual control, the remaining three receivers simultaneously continuing to obey the computer. The functions available for manual control are set out below. The controls for these functions are located in a manual control unit seen on the left of Fig. 1.

Aerial selection. Eight push button switches permit selection of aerials by means of a digitally controlled aerial selector switch panel. This panel is located in the receiver rack, remote from the console.

Bandwidth. A series of six push button switches permit selection of i.f. bandwidth from 100Hz to 12kHz.

Fig. 1. This console enables one operator to control four receivers with assistance from the computer.



A.g.c. time constant. Two push button switches select long or short time constants.

Tuning. As described earlier, the receiver is manually tuned by means of an optical shaft encoder. In addition to the control knob associated with the encoder, the manual control unit contains three push button switches permitting tuning rate selection. These control the rate of shift in receiver frequency as the tuning knob is rotated at a constant speed. In this way the operator is provided with the choice of rapid manual sweep or relocation to a new working frequency on the one hand or fine tuning on the other.

Receiver selection. Four push button switches enable the operator to select manual control of any one of the four receivers at a time.

Frequency readout. The operating frequency of the receiver under manual control is displayed on a digital l.e.d. display. Revertive signalling is used so that the displayed frequency is the actual tuned frequency of the receiver.

Visual tuning aid. For use in conjunction with the controls located in the manual tuning unit, four visual tuning aids are provided (see Fig. 2), one dedicated to each receiver and indicating at all times the state of this receiver. The visual tuning aid employs a c.r.t. display for tuning indication and precise frequency measurement. Although the unit displays received signals as vertical lines on a c.r.t., it is not a sweep panoramic display unit. A received signal appears on the c.r.t. screen as a vertical line with amplitude proportional to signal strength and horizontal position proportional to its frequency difference from the receiver tuned (nominal carrier) frequency.

By tuning the signal exactly to the centre of the c.r.t., as indicated by a vertical calibration line, the signal frequency may be read off to an accuracy of 20Hz on a l.e.d. display located immediately below the c.r.t. In the case of signals such as frequency shift keyed r.t.t.y. two (or possibly four) signals will appear on the screen. By tuning each in turn to the centre line and reading off the frequencies, the shift may be calculated, by subtraction, to an accuracy of 40 Hz.

The c.r.t. displays, in addition to the signal, a Lissajous figure in the form of a rotating ellipse. This is an aid to exact tuning. As the receiver is tuned towards the signal frequency in 10Hz steps, the Lissajous figure will continue to rotate until the 10Hz step is reached which brings the receiver to within 5Hz of the signal frequency. At this point the figure will cease to rotate, exhibiting only a wobble if modulation is present. At this point the vertical signal line on the c.r.t. will be seen to be at the centre of the graticule.

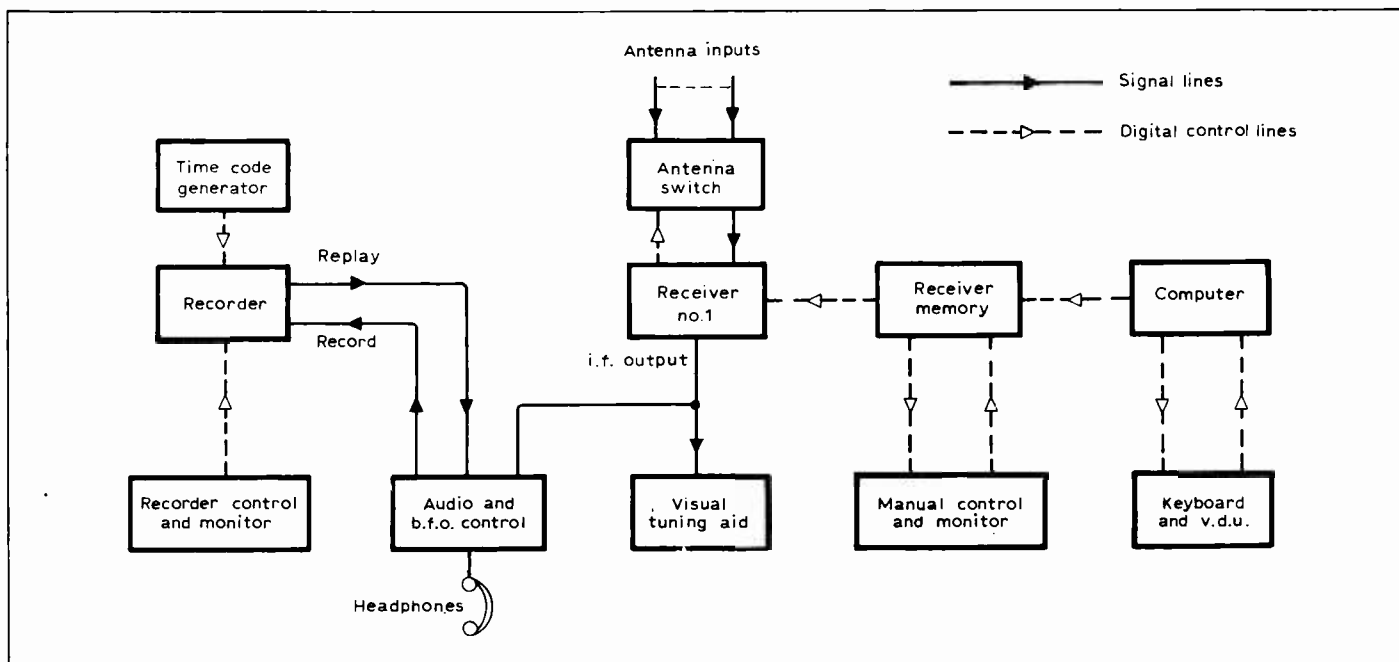


Fig. 2. Simplified diagram showing signal and control paths associated with one of the receivers controlled by a console. The lower row of blocks are units contained within the console; the upper row are units in remote equipment racks.

Computer control

All of the receiver manual control functions described above may also be controlled by the computer. Each receiver is controlled by a memory which passes a continual stream of digital serial command data to the receiver and to the manual control unit (as status information). Each memory is accessed by both the computer and the manual control unit. The operator has access to the memory, via the manual control unit, at all times except for the intervals of around 2.4ms when a command from the computer is being fed in. Although during these intervals the computer takes priority, they are too brief for the operator to become aware of them as he operates the manual controls.

The memory stores one set of commands, which the receiver always obeys. Each new command, whether from the manual control unit or the computer, replaces the existing command of the same function in the memory. All command and revertive information data is constantly repeated in an uninterrupted data stream of 19,200 bauds bit rate.

Visual display unit

The console contains a visual display unit and associated keyboard. The keyboard is a standard computer operator's typewriter capable of 30 characters per second, and is used both to command and interrogate the computer and as a typewriter in transcribing to hard copy interesting information received by the system. The commands typed on the keyboard and responses from the computer are displayed on the visual display unit.

The following are some of the functions which the operator can perform using the keyboard and visual display unit (note that in this context a "task" is a programme of work carried out by a receiver or receivers): Assignment of

automatically controlled tasks to specific receivers; monitoring of tasks while they are being performed; interruption or modification of tasks; transcription of data and storage of transcribed data; printing of edited transcribed data, from the disc store onto hard copy; transfer of tasks from one operator to another to ease peak workload situations; creation of new tasks, entering all the required parameters and control functions, etc.

Information handling

Those parts of the system so far described are concerned with receiver control and thus with the ability of the system to make interceptions of r.f. signals. Of equal importance is the handling of the received information. Intercepted signals are demodulated in the audio and b.f.o. control unit shown in Fig. 2. Four such units are housed in the console underneath the visual tuning aids and, like the visual tuning aids, each is dedicated to one of the four receivers. The system is primarily concerned with reception of double sideband speech (A3) and morse (A1) signals, although other types of modulation can be accommodated, for example single sideband speech (A3J), FSK (F1), etc.

Audio signal routing

Each operator is provided with a headset so arranged that he can listen to the audio signals from all four of his receivers simultaneously in any combination he chooses, in either ear. In other words, the output of any number

of his four receivers can be routed to either earpiece, quite independently.

The audio signals are routed by push button switches on the audio and b.f.o. control unit front panel. Each unit contains two switches marked L and R associated with the left and right hand earpieces. When a switch button is depressed the audio signal from the associated receiver is routed to the left or the right hand earpiece, as selected. If several receiver outputs are selected simultaneously, the audio outputs are mixed and heard together in the selected earpiece. Each audio signal is independently level controlled by an audio gain control on the audio and b.f.o. control unit. The audio routing system thus allows the operator total flexibility to choose his method of operation. For example, he may wish to route one important signal to one ear, possibly for immediate transcription, while listening to all three other receiver outputs in the other ear in case an interesting signal should appear.

A tape recording system is provided and is described later. The facility to route taped audio signals is provided, in exactly the same way as for the demodulator outputs, by a similar group of controls on the front of the audio and b.f.o. control unit. Taped and receiver output signals can be mixed. An operator therefore has the facility to transcribe to hard copy a taped signal while continuing to monitor live signals.

B.f.o. tone and on/off controls are located on the front of the audio and b.f.o. control unit so that the operator can receive morse (A1) signals at whatever audio pitch he prefers.

Automatic signal recognition

Another facility provided by the audio and b.f.o. control unit is the selection of signal recognition. By depressing a front panel switch the operator activates a circuit capable of simple signal recognition. When the recogniser is

activated it causes a light to flash in the selector switch on the audio and b.f.o. control unit, causes an l.e.d. to flash beside the visual display unit and produces an audio tone which appears on one track of the tape system.

Tape recorders

Each console contains two tape recorder control units. These are each associated with one digitally controlled tape recorder, located remotely in the receiver racks. The tape recorder itself is a highly specialised unit developed to meet the specific demands of the monitoring system. Control is by means of a bit synchronous 36-bit serial word at a bit rate of 19,200 bauds. Each recorder is provided with four tracks, two of which are occupied by the audio output from two of the four receivers. (Hence the need for two recorders and two tape recorder control units per console.) The remaining two tracks, of each recorder, are occupied by the output of a time code generator and the signal produced by the signal recogniser. The recorders are of the continuous loop type with separate and independent record and replay heads. Sufficient tape in a cassette is provided for 60 minutes of recording time at a tape speed of 15/16 of an inch per second.

Both manual and computer control of the tape recorders is available. Control is provided of record; replay forward; replay reverse; replay speed from 0.6 to 10 times record speed; stop and auto scan. In the last-mentioned mode the recorder replays at ten times record speed in a search for signals from the signal recogniser on the fourth track.

The facility can be provided of re-recording on to a separate reel-to-reel recorder and of remote transcription by other operators.

The facility is thus provided of recording and replaying simultaneously and at different speeds from one tape. The operator in transcribing can return to a part of the recorded message which he has missed, possibly in order to listen to another interesting signal on another receiver, without interrupting the continuing recording of the incoming signal. The presence of the time code signal enables the operator to read off the time at which any signal was recorded. This information, together with the amount of tape still available for recording, is displayed on the front panel of the tape recorder control unit by l.e.d. display.

Using the system

It is worthwhile looking in general terms at the use of the above capabilities in a complete monitoring system, possibly containing several consoles and a large number of receivers.

The first important point to note is that the receiving and recording systems and the computer are all capable of remote control. This is no accident, but

an essential characteristic of a system capable of dual control, by an operator and a computer. It does, however, provide a second major advantage in that it permits the receiver, recorder and computer racks to be remotely located in a separate room from the control console. In this way, the particular environmental requirements of man and machine can be separately catered for.

A typical monitoring station would have an operations room containing only consoles, operators and supervisors. The consoles would be arranged in groups of six with a seventh console of different design for a supervisor overseeing the activities of the six operators. Each group of seven consoles would share a computer and work would be distributed evenly between the operators, ensuring maximum use of facilities and minimum fatigue.

Each operator's console is fitted with a signal activity display unit. This indicates to the supervisor the status of all four receivers in a console in terms of whether they are in use or idle. The supervisor can thus see at all times which operators have spare capacity. A button on the signal activity display unit permits each operator to call the supervisor in emergency by activating audible and visual alarms on the supervisor's console.

Because all of the routine activities of a group of consoles are controlled by a single computer, switching of complete tasks from one operator to another or others is simple and extremely rapid. In a properly designed system with a well chosen quantity of consoles, no overloading ever occurs, even though large savings in operators and equipment are made in comparison with a conventional system.

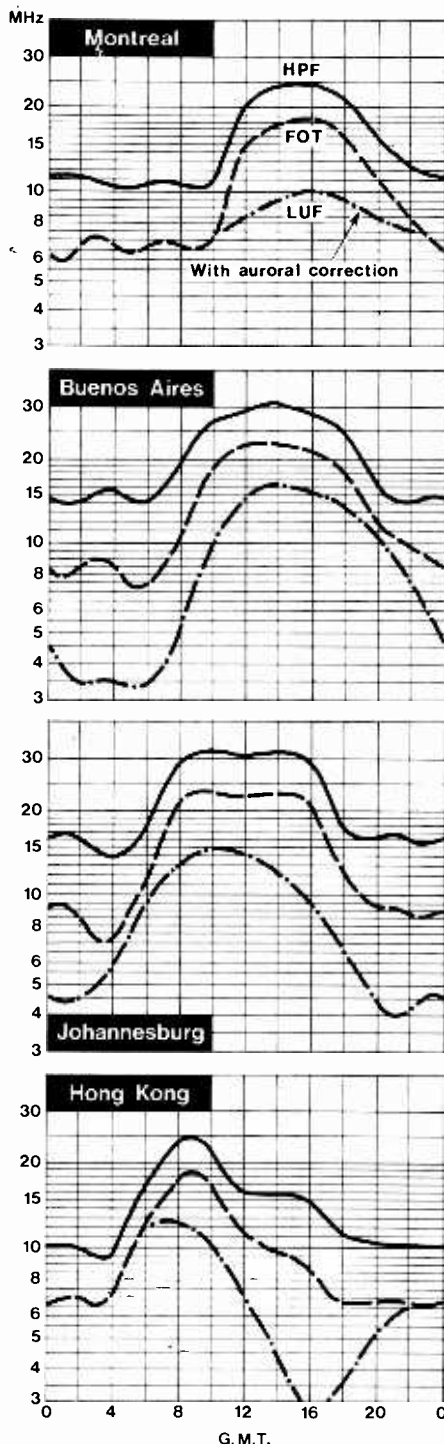
The equipment racks are normally located in a separate room in a suitably controlled environment. They are thus accessible for routine maintenance and for repair by non-security cleared engineering staff without such staff having access to secure material. For this purpose, the tape machine and computer hard copy outputs may be located in a separate secure area.

Because the entire system is operated in conjunction with perfectly standard digital computers, there is no reason why the system's computers cannot "talk to" other computers. The monitoring system can therefore be readily linked to other computer controlled systems such as direction finding networks. Largely automatic interception and direction finding facilities capable of giving pinpoint locations of signal sources within a few seconds are available from a combined CERES and computer controlled d.f. system. A conventional monitoring system is entirely incapable of this facility.

HF predictions

The seasonal feature of high values of daytime FOTs and HPFs is clearly illustrated by this month's charts. Daytime here means the period during which the whole of the path is in daylight; thus Hong Kong, for example, being a long path to the east of London, is in daylight for a few hours only, 0700 to 1100 GMT or 1600 to 2000 Hong Kong time.

Whereas FOTs and HPFs apply for both directions of a path, LUFs are shown for reception in the UK only. This is because LUF is dependent on noise level at the receiving site and atmospheric noise level variations are systematic with local time.



New Products

Communications teaching kit

Feedback Instruments Ltd have extended their Teknikit tutor series to include a communications kit. The TK295 kit, number 4 in the series, provides a method of teaching the basic principles of communication to students of all grades from technician to graduate. The twelve modules supplied with the kit include a signal source, an amplifier, a detector, a balanced modulator, filters, a ring bridge, tuned circuits, a crystal unit, an aerial unit and a miniature speaker. Experiments which can be performed with this kit include studies of the balanced modulator, other methods of a.m., a.m. detection, a complete a.m. system, frequency modulation and f.m. detection. A student's manual and an instructor's manual, accompany the kit providing comments and explanations for these and other experiments. The kit requires external power supplies and

a ferro-magnetic assembly frame. Feedback Instruments Ltd, Park Road Crowborough, Sussex TN6 2QR.

WW301 for further details

Filter/oscillator instrument

A versatile technique for obtaining active filter transfer functions using only low gain inductive circuitry has enabled OMB Electronics to produce a low cost hi-fi measuring instrument suitable for spectrum analysis, noise analysis, frequency response checking and cross-talk measurements. The 631 filter/oscillator has 12dB/octave low-pass and high-pass modes, a filter accept mode, having a variable Q factor from 2 to 100, and an oscillator mode. A frequency range extending from 0.1Hz to 100kHz enables the instrument to virtually eliminate any interfering frequency in the audio spectrum. In the filter reject mode the instrument can achieve over 80dB, and typically 100dB, rejection of a fundamental, enabling distortion products of 0.001% to be measured by a suitable r.m.s. voltmeter. OMB Electronics, Riverside, Eynsford, Kent DA4 OAE.

WW302 for further details

Constant-current h.v. supply

A high-voltage power supply, the Model 820, is designed to give a constant current output at up to 30kV for electrophoresis and similar applications. The unit uses h.f. conversion to generate high-voltage low-ripple d.c. power without the hazard of high

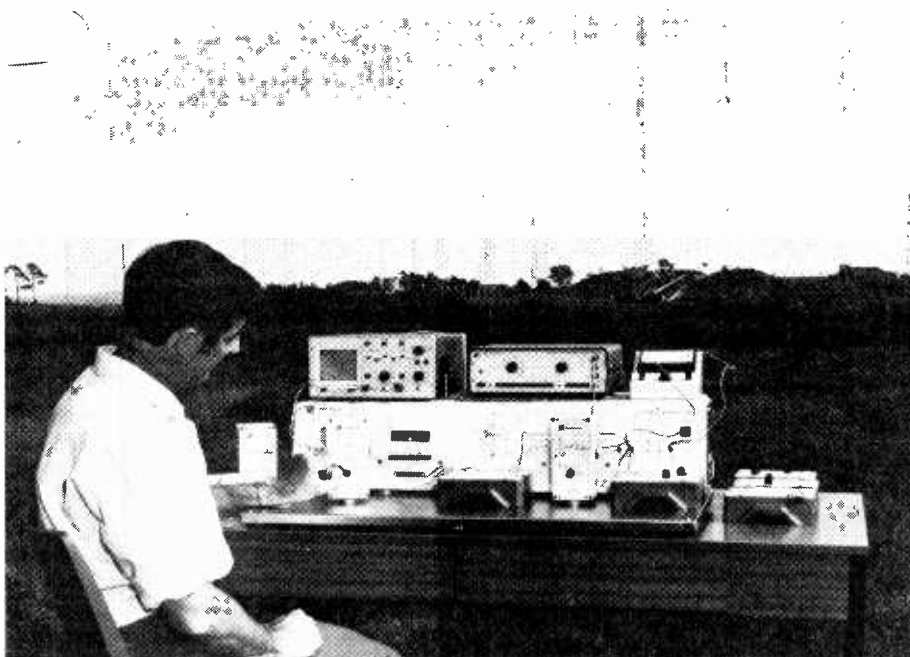
energy storage in the output filter circuit. Current stability is better than 0.1% of the set current, which is variable between 10 and 500 μ A. The output can also be stabilized in the constant-voltage mode which is variable between 0.1 and 30kV. An overvoltage trip prevents excessive output if the load becomes open circuit in the constant-current mode, while an overcurrent trip and a fuse give protection against overloads or short circuits in either mode. Brandenburg Ltd, High Voltage Engineering Division, 939 London Road, Thornton Heath, Surrey CR4 6JE.

WW303 for further details

Teletext decoder

The Spectrum Telefax Decoder TFX-32, from Spectrum Laboratories Ltd, has all the standard features for receiving Ceefax and Oracle and offers optional facilities for decoding the Viewdata service. The hand-held control keypad, which includes a remote TV receiver on/off switch, may be replaced by an optional ultrasonic cordless unit. Unusual features include roll, with pages changing continuously, and a time display which can be inserted into the top right of any TV programme. This decoder is priced at approximately £300 and may be built-in to a receiver or mounted externally, Spectrum Laboratories being able to advise and supply the necessary circuitry and information for the conversion of most TV receivers. This deluxe version also incorporates sound muting, continuous page header movement and upper/lower case selection. A standard teletext decoder is also available. Spectrum Laboratories Ltd, 32 Royal Avenue, Chelsea, London SW3.

WW304 for further details



WW301



WW302



WW303

Cable-tie mounts

Low profile cable-tie mounts, available from Panduit Ltd, are suitable for use in securing wires where the minimum of space is available. The mounts, which are made from natural nylon, are available with No. 2 (3/32in diam.), No. 5 or No. 8 screw holes, types LPMM-S2, LPMM-S5, or LPMM-S8 respectively. Types LPMM-S2 and LPMM-S5 are designed for use with miniature cross-section ties and type LPMM-S8 is suitable for miniature, intermediate and standard cross-section ties. Panduit Ltd, Sittingbourne Industrial Park, Unit 22a, Crown Quay Lane, Sittingbourne, Kent. **WW305 for further details**

Digital multimeters

Two compact digital multimeters have been made by Fluke International Corporation. Type 8030A has been designed for service and maintenance applications and is believed to be the first 3½-digit instrument to offer features such as true r.m.s. voltage and current measurements, in addition to facilitating the testing of diodes. The diode measurement feature permits the forward drop across a diode or transistor to be checked with the semiconductor junction biased at 1mA. The 8030A provides voltage, current and resistance measurement, each in five ranges. Direct voltage measurement ranges from 200mV full scale to 1,100V full scale, at an accuracy of $\pm 0.1\%$ of reading + 1 digit; true r.m.s. voltage measurement from 200mV full scale to 750V full scale, to an accuracy of $\pm 0.5\%$ of reading + 2 digits and 200 μ A full scale to 2A full scale in true r.m.s. to an accuracy of $\pm 1\%$ reading + 2 digits for most ranges. Resistance measurements

from 200 Ω to 2M Ω full scale can be made to an accuracy of $\pm 0.4\%$ of reading + 1 digit with the exception of the 2M Ω range which has an accuracy of $\pm 0.6\%$ of reading + 1 digit.

Type 8040A is a 4½-digit multimeter which offers the same ranges as the 8030A with the exception of the resistance range which measures 200 Ω to 20M Ω . The 8040A does not contain a diode test facility but offers greater accuracies due to the additional decimal digit available on each range. This model also has autoranging and auto-zero features.

Both meters use large l.e.d. displays, with hoods for bright conditions, and are designed to withstand overloads occurring in normal use, and transients up to 6kV, 10 μ s duration, across their inputs. Optional extras include temperature, h.v. and r.f. probes, a current transformer, rechargeable cells and a mains adaptor. Prices are from £139. ITT Instrument Services, Edinburgh Way, Harlow, Essex.

WW306 for further details

Vitreous-enamel resistors

A range of high power-to-size ratio resistors has been introduced by Welwyn Electric Ltd. The Series 1900 resistors are wirewound and elliptical in cross-section and can be obtained with fixed, tapped or adjustable windings in a range of terminations and with mounting devices for stacking. Resistance values range from 1 Ω to 24k Ω and are rated from 23 to 56W at 20°C. Resistors in the Series 1900 range are designed to withstand high mechanical and heat shock loads, making them suitable for

pulse applications. The elliptical cross-section permits the resistors to be mounted in positions where space is limited. Welwyn Electric Ltd, Bedlington, Northumberland, NE22 7AA. **WW307 for further details**

R.f. shielding door seals

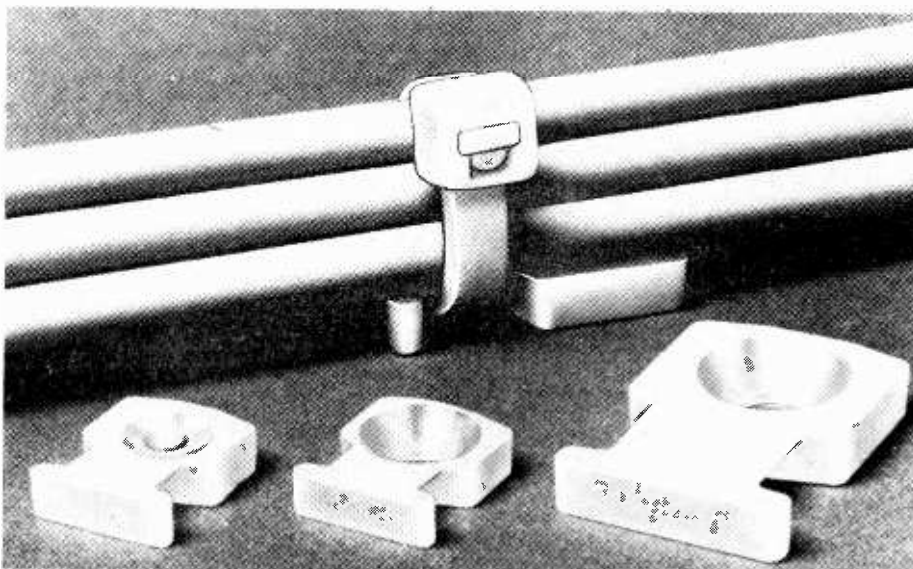
Knife-edge r.f. sealing is now available for Belling-Lee's range of single and double r.f.-shielded doors. The knife-edge principle reduces the force required to open and close the doors and the finger contacts, which provide electrical continuity between the walls of the shielded room and the door, are less susceptible to damage because they are concealed in a recess. Given shielding of appropriate performance the seals offer a high level of attenuation at both high and low frequencies. For example, tests on a complete shielded enclosure gave 60dB down at 1kHz, 100dB down at 10kHz and in excess of 125dB down from 100kHz to at least 10GHz. Belling & Lee Ltd, Great Cambridge Road, Enfield, Middlesex, EN1 3RY.

WW308 for further details

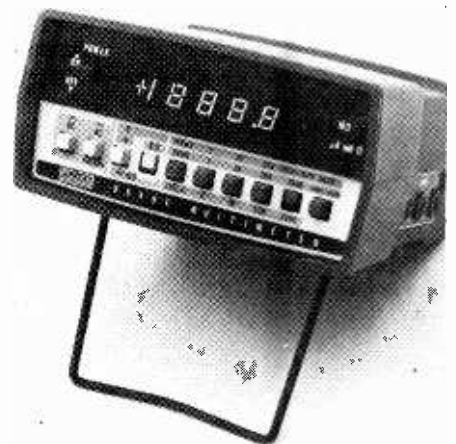
Miniature rotary switches

Rotary switches, in the MR and SSR series, have been designed for applications where space and reliability are major considerations. The switches, from Waycom Limited, have body diameters of no more than 16mm and are rated at 0.5A at 240V r.m.s. and 1A at 12V d.c. Switching actions ranging from 1-pole 10-way to 4-pole 2-way in the MR series and 1-pole up to 12-way to 4-pole up to 3-way in the SSR series, are all break-before-make. Waycom Ltd, Wokingham Road, Bracknell, Berks.

WW309 for further details



WW305



WW306

Miniature multimeter

A hand-held digital multimeter, which is essentially a self-contained probe, is being produced by Kane-May of Welwyn Garden City. The meter uses a p.m.o.s. analogue-to-digital converter chip, in which the charge-balancing technique is employed. Current from the measured source is taken to the inverting input of a feedback integrator, while current pulses are fed to this virtual-earth point in opposition. The number of pulses required to prevent the integrating capacitor charging is counted and displayed. The rest of the circuitry is contained in c.m.o.s. chips.

The meter is battery-powered and is provided with a charger. It can be held and controlled by one hand, the controls consisting of a "press-to-read" button and five function buttons. The intention is that the unit should be used in this way, but a cradle is supplied for bench use, in which condition the display is continuously illuminated.

Briefly, the specification is as follows: direct voltage 2-1000V fullscale ($\pm 0.6\%$ of reading ± 1 digit), alternating voltage 2-700V r.m.s. full-scale ($\pm 2\% \pm 1$), direct current 2A ($\pm 0.6\% \pm 1$), alt. current 2A ($\pm 2\% \pm 1$) and resistance $2k\Omega - 2M\Omega$ full scale. Input impedance is $10M\Omega$ and 20pF. The current ranges represent an advance in this type of equipment. Kane-May Ltd, Burrowfield, Welwyn Garden City, Herts AL7 4TU.

WW310 for further details

Function generators

Two function generators, models G430 and G432, have been manufactured by

Metronex of Poland. Model G430 provides a source of sine and square wave signals at frequencies from 1Hz to 1MHz in six switchable ranges, and is designed for general-purpose laboratory or field applications. The sinusoidal signal is continuously variable from 0 to 10V r.m.s. and the square-wave signal from 0 to 20V pk-pk. Switched attenuator steps of 0, 20, 40 and 60dB are provided with sine-wave distortion less than 0.3% in the range 100Hz to 20kHz, 0.1% in the range 20Hz to 100kHz and 1% in the range 1Hz to 1MHz. The rise and fall time of the square-wave slope is less than 50ns. Model G432 is a precision generator providing square, triangle and sine waveforms over the range 1Hz to 1.1MHz in six ranges. Prices at time of going to press were £95 for the G430 and £115 for the G432. Electronic Brokers Ltd, 49/53 Pancras Road, London NW1 2QB.

WW311 for further details

Plug-in crystal displays

The IEE-Polaris range of liquid crystal displays consists of 3½, 4, 4½, 5, 6 and 8 digit displays, a 12-hour clock and 16-segment alphanumeric field-effect crystal displays. Two types of display are available, a reflective model for ambient lighting and a transmissive model for backlighting. Uniformly spaced integral contact clips solder directly to p.c.bs or may be inserted into strip sockets on 0.1in centres. The 0.12in (max) thick displays, which are compatible with c.m.o.s. and m.o.s. i.cs and drivers, have low power requirements, typically 2.5 to 24µW for all segments,

and offer wide viewing angles (up to 110°), 20:1 contrast ratio, and an average operating life of 50,000 hrs at -20 to +60°C. The segmented characters are available in five heights from 0.4 to 1.0in. Industrial Electronic Engineers Inc., 7720-40 Lemona Avenue, Van Nuys, California 91405, U.S.A.
WW 312 for further details

Digital stopwatch

The ET105 from Siliconix is a hand-held battery-powered stopwatch intended for all applications from sport to process control. This model measures time up to 59 minutes and 59.9 seconds in one-tenth second intervals, and has controls for start/stop and time-in/time-out. A quartz crystal is used for accuracy and the digital readout is viewed on an i.e.d. display. Three heavy-duty batteries are claimed to provide 12 hours continuous operation and the watch, which measures approximately 4½ × 2½ × 1½in, weighs only 6oz. Newitt & Co. Ltd, 81 Goodramgate, York YO1 2LU.

WW313 for further details

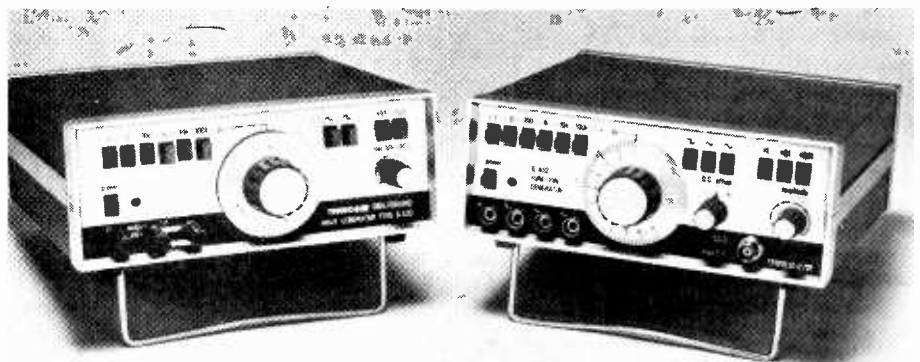
Turns-counting dial

A ⅜in diameter 15-turn counting dial, the H507, has white markings on a black background for good legibility. The dial, which has 50 divisions per turn, has a readability of 2 parts in 1000 over 10 turns, a minimum torque of 350g-cm with the brake engaged, and a mechanical life of 10,000 cycles. The standard model weighs 7g and can be mounted directly to a ¼in potentiometer shaft with no backlash. Bourns (Trimpot), Limited, Hodford House, 17/27 High Street, Hounslow, Middlesex, TW3 1TE.

WW314 for further details



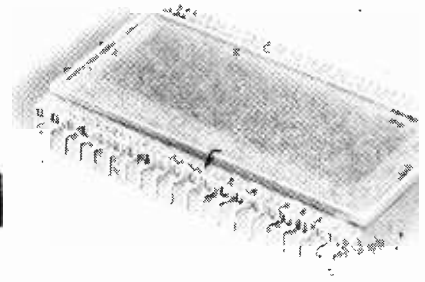
WW310



WW311



WW312



Precision capacitors

A family of precision Teflon capacitors, available from Perdix Components Ltd, covers the range 500pF to 4 μ F in tolerances of 1%, 0.25% and 0.1% using extended-film and metallized-film constructions. The capacitors, which operate over a temperature range of -55 to +200°C, have a cyclic stability of less than 0.02%, a temperature coefficient of 100ppm/°C and a minimum insulation resistance greater than 10¹⁴ Ω up to 1.0 μ F. Standard voltage ranges are available up to 600V, with no derating within the full temperature range. Other characteristics include a dissipation factor better than 0.02% and a dielectric absorption of less than 0.02% at 25°C. Perdix Components Ltd, 98 Crofton Park Road, London S.E.4.

WW315 for further details

Miniature soldering iron

The model CX soldering iron, from Antex, has a leakage current of less than 3 μ A, making it safe to use on delicate integrated circuits and other semiconductors. This model, which is made on the same principle as the Antex model X25, has a ceramic shaft inside a stainless steel shaft. The element, rated at about 17W, is wound on a former and inserted inside the ceramic shaft to give maximum heat-transfer to the soldering bit which slides over the steel shaft. A breakdown voltage in excess of 4000V a.c. has been achieved with this construction. A range of six bits is available with tip sizes ranging from 1 to 6mm giving tip temperatures varying from 300 to 380°C. The iron, which measures 19.5cm and weighs 40g, conforms with BS3456 and is available for 220-250V or 100-120V, a.c./d.c. Antex Electronics, Mayflower House, Plymouth, Devon.

WW316 for further details

Piezo-electric horns

The principle of operation of a piezo-electric horn unit is based on an electrical signal being applied to a crystalline structure to produce a mechanical displacement. These units can be used as tweeters without the use of crossover networks, necessary with moving coil tweeters, because the crossover is inherent in the physical characteristics of the crystal structure. The horn unit, or units, can be connected across existing speaker systems as long as the output of the driving amplifier is within the rating of the units. Types suitable for p.a. applications include the highly directional 3 $\frac{1}{2}$ in KSN6005A horn and the wide-dispersion 3 $\frac{1}{2}$ in KSN6006A horn. The 3 $\frac{1}{2}$ in KSN6011A and the 2 $\frac{1}{2}$ in KSN60010A types are piezo-electric tweeters suitable for audio applications. Instead of horns, the tweeters have cones directly driven by the crystals. 2 \times 5in wide-dispersion horns, suitable for both p.a. and audio applications, are also available. Prices are from £2.75

Solid State Devices

Names of suppliers of devices in this section are given in abbreviation after each entry and in full at the end of the section.

depending upon type and quantity. Soundout Productions Ltd, 91 Ewell Road, Surbiton, Surrey KT7 9AH.

WW317 for further details.

Silicon rectifiers

A series of high-voltage high-current silicon rectifiers has been made available by Semtech Corporation. The rectifiers, designated KW-PAC, are mass produced for economical military, industrial and commercial applications and can be mounted in either an air or oil environment. Peak inverse voltages range from 3 to 72kV, average rectified currents from 3 to 12A, and the single-cycle surge currents are 150, 300 or 600A. The rectifiers measure 1in thick \times 4in wide \times 4.8 to 20.8in long.

WW318

Bourns

Infrared l.e.d.

The Xciton XC1209 l.e.d. has a typical output radiation power of 1.5mW centred at 940nm. Maximum power dissipation at 25°C is 75mW, and the maximum forward direct current is 50mA. The device measures 0.16in diameter \times 0.210in high and is suitable for alarm or fire protection systems.

WW319

Distronic

Multiplexers

The HI506 and HI507 are 16 and dual-8 channel multiplexers, equivalent to the Siliconix DG506 and DG507. Harris Semiconductors Ltd, who manufacture the devices, claim that the access times of 300ns and typical on-resistances of 170 Ω , varying only 6% between channels on any one device, are a significant improvement on the Siliconix devices. The devices, which are t.t.l./c.m.o.s. compatible, require no pull-up resistors and are latch-up proof, are in 24 d.i.l. packages and have overvoltage protected digital inputs.

WW320

Memec

4-amp Darlington transistors

Six complementary power transistors, from Motorola Ltd, are designated BD775, 777 and 779 (n-p-n) and BD776, 778 and 780 (p-n-p) and are intended for general-purpose applications. Characteristics include a current-gain-bandwidth product of 20MHz, h_{fe} typically 1400 at an I_{cc} of 2A, V_{ce} breakdown voltages of 45V for BD775 and 776, 60V for BD777 and 778, and 80V for BD779 and 780, and a total power dissipation of 15W at 25°C.

WW321

Motorola

Opto-isolators

Optically coupled isolators in the NSL150 and 250 ranges use gallium arsenide infrared l.e.ds and phototransistors to achieve isolation voltage ratings of 1500 and 2500V respectively. Insulation resistance is greater than 10¹¹ ohms, the direct current transfer ratio is up to 20%, and the turn on/off time is typically 2 μ s. All the devices have a temperature range from -55 to +100°C and are housed in the six pin d.i.l. package.

WW322

National Semiconductors

Gunn oscillators

The SSG0101-0126 family of Gunn oscillators has been added to the range of microwave sources available from Solid State Technology Inc., and covers the frequency range 5 to 18GHz. Each unit can deliver more than 100mW with harmonic rejection better than 30dB (measured with C-weighting) and with a temperature stability of $\pm 0.002\%$ /°C. These oscillators are designed to provide low-cost simulation sources for radar and communication applications. Optional isolators, oven and voltage regulators are also available.

WW323 **Tony Chapman Electronics**

Power switching transistor

The DTS-515 series of n-p-n switching transistors comprises five devices all offering a continuous collector current of 10A. Maximum V_{CBO} ratings range from 300 to 700V and current gains are between 15 and 80. Typical turn off time for the devices is 250ns, and the power dissipation is 125W. All devices are housed in the TO-3 package.

WW324

Walmore

Bourns (Trimpot) Ltd, Hodford House, 17/27 High Street, Hounslow, Middx TW3 1TE.

Distronic Limited, 50/51 Burnt Mill, Elizabeth Way, Harlow, Essex.

Memec Ltd, The Firs, Whitchurch, Aylesbury, Bucks HP22 4JU.

Motorola Ltd, York House, Empire Way, Wembley, Middx HA9 0PR.

National Semiconductors Ltd of Canada, Stamford House, Stamford New Road, Altrincham, Cheshire WA14 1DR.

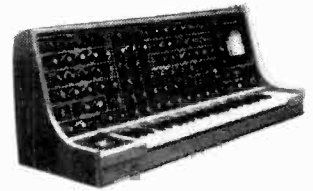
Tony Chapman Electronics Ltd, 80A High Street, Epping, Essex CM16 4AE.

Walmore Electronics Ltd, 11-15 Betterton Street, London WC2H 9BS.

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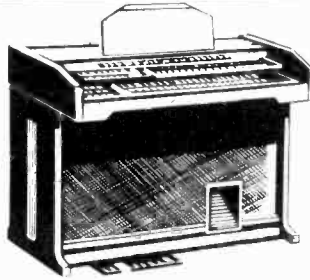
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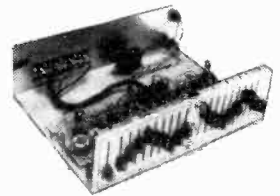


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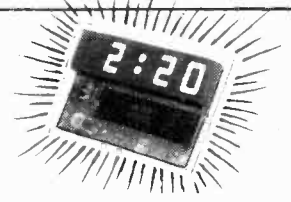
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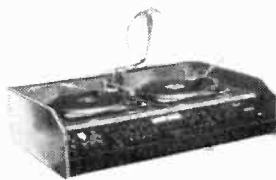
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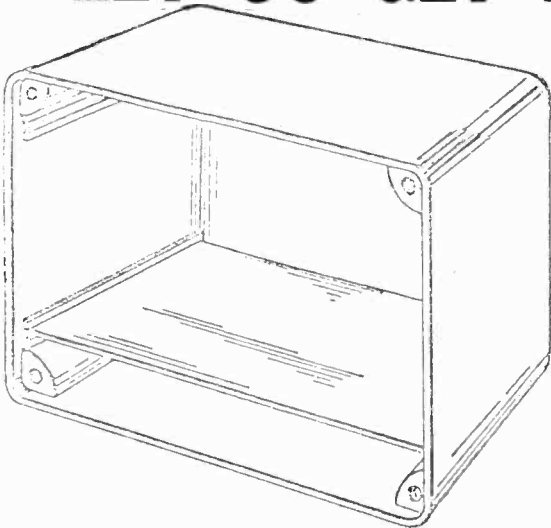
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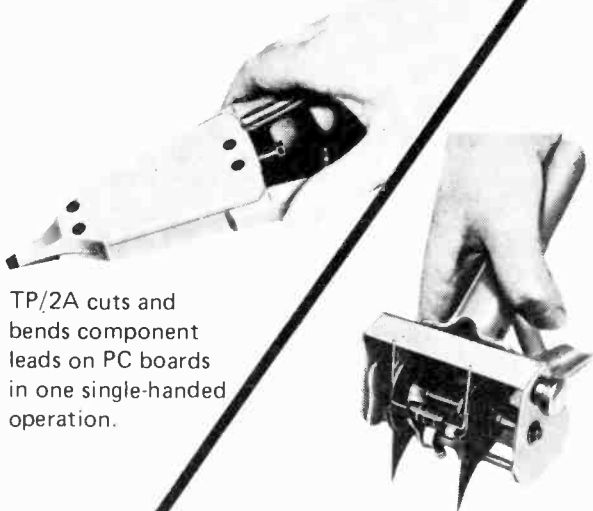
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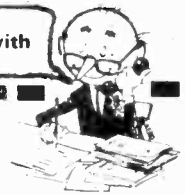
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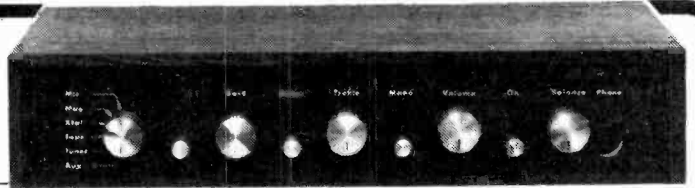
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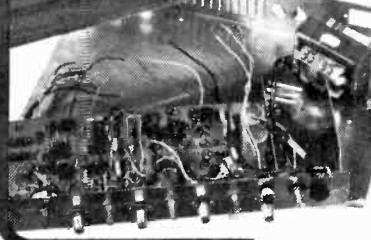
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VALUE



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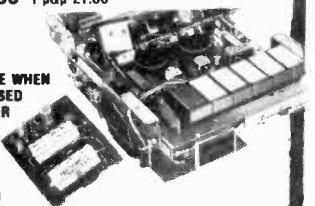
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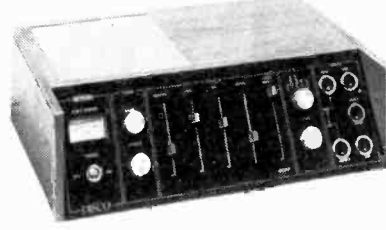
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When you are looking for a good speaker, why not build your own from this kit. It's the unit which we supply with the above enclosures. Size 13" x 8" (approx.) EMI woofer, 3¼" (approx.) tweeter, and matching crossover.

£7⁵⁰ + p & p £1.50
PER SET

Power handling capacity 15 watts rms, 30 watts peak.

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For extra power, choose this super RT-VC kit! EMI 13" x 8" (approx.) triple-laminate-coned woofer with massive 5" (approx.) magnet, plus 5" (approx.) mid-range unit with concentric 2" parasitic tweeter and 2¼" (approx.) magnet. Complete with circuit diagram and crossover components.

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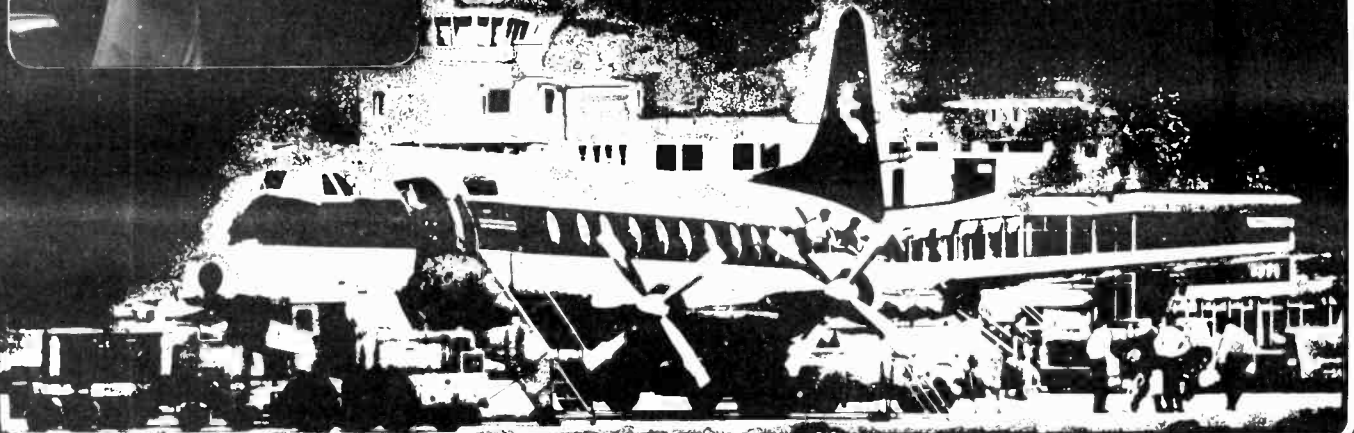
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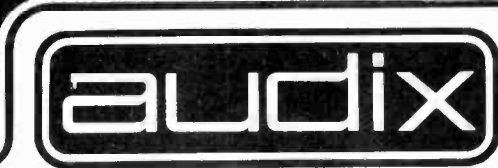
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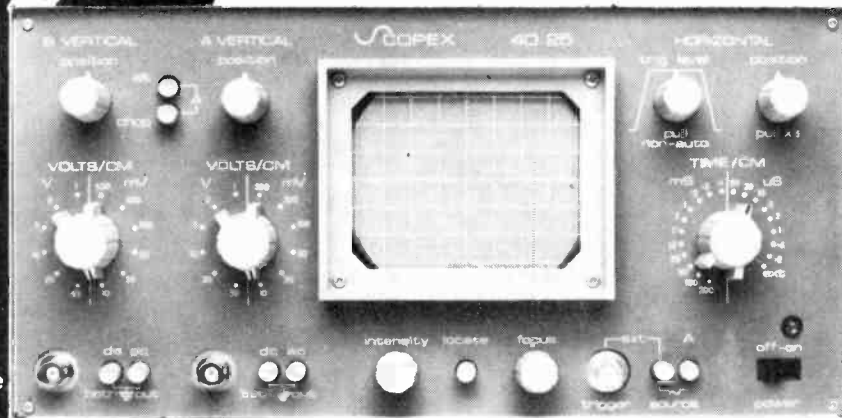
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Ditton 11	150	210	130	10W	16Ω	85dB	40-20,000 Hz
Ditton 15	140	220	130	10W	16Ω	85dB	40-20,000 Hz
Ditton 33	160	250	140	10W	16Ω	85dB	40-20,000 Hz
Ditton 44	160	250	140	10W	16Ω	85dB	40-20,000 Hz
Ditton 25	180	280	150	10W	16Ω	85dB	40-20,000 Hz
Ditton 66	180	280	150	10W	16Ω	85dB	40-20,000 Hz
UL 6	200	310	170	10W	16Ω	85dB	40-20,000 Hz
UL 8	190	280	150	10W	16Ω	85dB	40-20,000 Hz
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Type	Price (p)	Type	Price (p)
BD132	39	BF338	34
BD133	45	BF355	50
BD135	29	BF457	37
BD136	30	BF458	37
BD137	30	BF459	38
BD138	33	BFT42	35
BD139	37	BFT43	35
BD140	39	BFX29	29
BD144	£1.99	BFX84	29
BD160	£1.65	BFX85	30
BD181	80	BFX86	28
BD182	90	BFX88	25
BD183	80	BFY50	19
BD184	£1.10	BFY51	19
BD222	47	BFY52	20
BD225	47	BFY90	£1.10
BD232	50	BR100	32
BD233	43	BR101	38
BD234	49	BRC4443	80
BD235	49	BRY39	38
BD236	53	BSY52	30
BD237	49	BT106	£1.20
BD238	55	BT108	£1.50
BDX32	£2.40	BT116	£1.25
BDY20	80	BU105/02	£1.60
BF115	38	BU108	£1.80
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BF158	20	BU204	£1.80
BF160	35	BU205	£1.67
BF167	24	BU206	£1.95
BF173	25	BU208	£2.20
BF178	33	BU208/02	£2.75
BF179	38	BUY69B	£2.50
BF180	31	BUY69A	£2.65
BF181	37	E1222	38
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BF183	30	MJE520	44
BF184	29	2N696	30
BF185	30	2N706	15
BF186	26	2N3053	20
BF194	8	2N3054	65
BF195	8	2N3055	55
BF196	10	2N3702	12
BF197	11	2N3703	12
BF198	23	2N3704	10
BF199	25	2N3705	10
BF200	28	2N3706	10
BF218	40	2N3819	38
BF224	20	2N5296	40
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BF258	26	R2008B	£1.90
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BF336	37	RCA16334	80
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Type	Price (p)	Type	Price (p)
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S6080 A KIT	£4.90	TIP41A	60
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TIP31A	52	TIS91	27

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Type	Price (p)	Type	Price (p)
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BA155	15	IN6C/OA91	7
BAX13	6	IN914	6
BAX16	6	IN4001	4
BY126	11	IN4002	5
BY127	10	IN4003	5
BY199	25	IN4004	5
BY206	17	IN4005	5
BY238	25	IN4007	6
BYX10	14	IN4148	4

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EHT Multipliers

Type	Order Code	Price
Thorn 950 MK II 1400	D101P	£2.07
Thorn 1500 3 stick	D102Y	£1.98
Thorn 1500 5 stick	D103G	£2.17
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Rank Z 718	D106A	£1.54
Thorn 3000/3500	D107J	£5.34
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New Mono Tubes

Screen Type	Equivalent	Price
12" Toshiba E2117A	TMT 31/10L A31 250W	£17.75
14" Toshiba M6529 FZP	TMT 34/10L	£17.95
20" A50-140W	CME 2013	£15.50
24" A61-140W	CME 2413	£17.30

New Colour Tubes

Screen Type	Equivalent	Price
19" A49-191X	A49-192 and A49-120X	£57.70
20" 510DJB22	A51-110X	£61.35
22" A56/120X		£61.50

Aerial Accessories

Type	Price
Coax Plugs	each 10.5p
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Superverters with variable gain	each £15.95
Superverters with variable gain and frequency	each £17.45
Broad Band Amplifier	each £16.50

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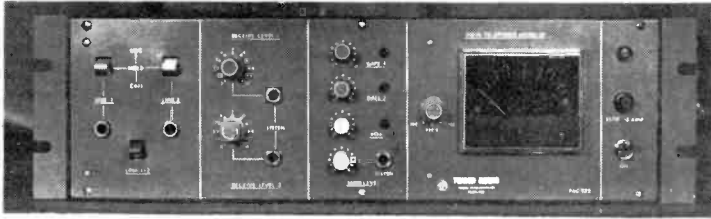
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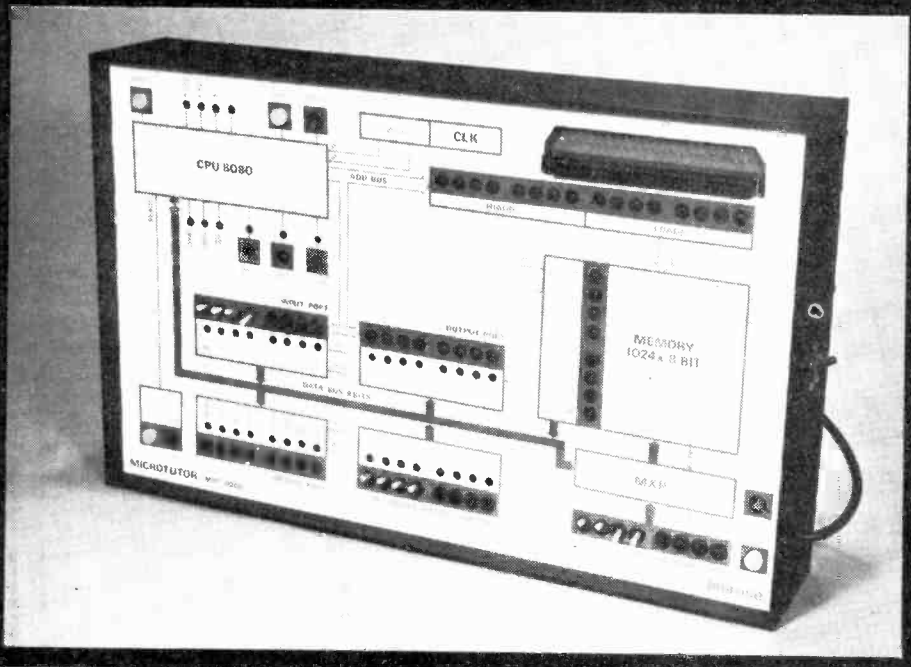
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WW — 093 FOR FURTHER DETAILS

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On the contrary, the clear six-LED display tells you at a glance the polarity of the device (NPN, PNP, N-channel, P-channel) and for out-of-circuit tests whether it is bipolar, depletion FET, or enhancement FET.

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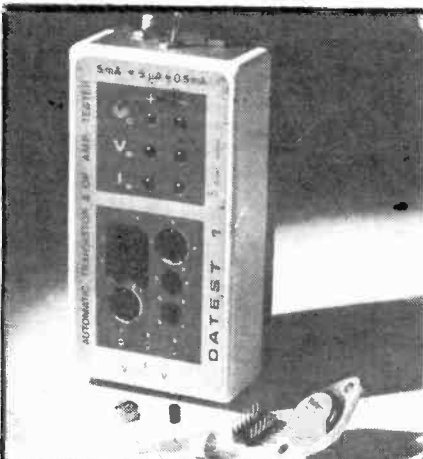
DATEST 1 with its advanced four i.c. and six transistor circuit (part appl. for) rapidly pays for itself in skilled man hours saved and in expensive mistakes avoided. For complete user confidence DATEST 1 even stops working abruptly and gives a special display when battery voltage has dropped to too low a value.

DATEST 1 is available now and comes complete with battery, easy-to-use probes for in-circuit tests, and detailed handbook. Write for full details or send now for your own "time saver". Price: £49 plus 8% VAT, cash with order.

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15 — 240 Watts!

HY5 Preamplifier

The HY5 is a mono hybrid amplifier ideally suited for all applications. All common input functions (mag Cartridge, tuner etc) are catered for internally, the desired function is achieved either by a multi-way switch or direct connection to the appropriate pins. The internal volume and tone circuits merely require connecting to external potentiometers (not included). The HY5 is compatible with all I.L.P. power amplifiers and power supplies. To ease construction and mounting a P.C. connector is supplied with each pre-amplifier.

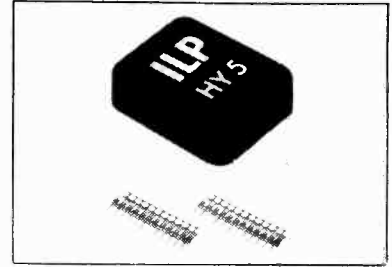
FEATURES: Complete pre amplifier in single pack. Multi function equalization. Low noise. Low distortion. High overload. Two simply combined for stereo.

APPLICATIONS: Hi-Fi. Mixers. Disco. Guitar and Organ. Public address.

SPECIFICATIONS:

INPUTS: Magnetic Pick-up 3mV. Ceramic Pick-up 30mV. Tuner 100mV. Microphone 10mV. Auxiliary 3 100mV input impedance 47k Ω at 1kHz.
OUTPUTS: Type 100mV. Main output 500mV R.M.S.
ACTIVE TONE CONTROLS: Treble \pm 12dB at 10kHz. Bass \pm at 100Hz.
DISTORTION: 0.1% at 1kHz. Signal Noise Ratio 68dB.
OVERLOAD: 38dB on Magnetic Pick-up. **SUPPLY VOLTAGE:** 16-50V.

Price £4.75 + 59p VAT P&P free.
HY5 mounting board B1 48p + 6p VAT P&P free.



HY30 15 Watts into 8 Ω

The HY30 is an exciting New kit from I.L.P. it features a virtually indestructible I.C. with short circuit and thermal protection. The kit consists of I.C. heatsink P.C. board 4 resistors 6 capacitors, mounting kit together with easy to follow construction and operating instructions. This amplifier is ideally suited to the beginner in audio who wishes to use the most up to date technology available.

FEATURES: Complete Kit. Low Distortion. Short Open and Thermal Protection. Easy to Build.
APPLICATIONS: Updating audio equipment. Guitar practice amplifier. Test amplifier. Audio oscillator.

SPECIFICATIONS:

OUTPUT POWER: 15W R.M.S. into 8 Ω . **DISTORTION:** 0.1% at 15W.
INPUT SENSITIVITY: 500mV. **FREQUENCY RESPONSE:** 10Hz-16kHz \pm 3dB.
SUPPLY VOLTAGE: 18V.

Price £4.75 + 59p VAT P&P free.

**Available
Ex-stock**

HY50 25 Watts into 8 Ω

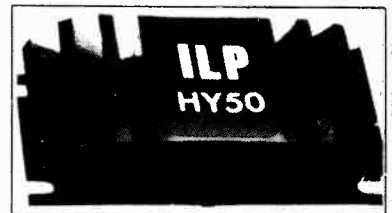
The HY50 leads I.L.P.'s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World.

FEATURES: Low Distortion. Integral Heatsink. Only five connections. 7 Amp output transistors. No external components.

APPLICATIONS: Medium Power Hi-Fi systems. Low power disco. Guitar amplifier.

SPECIFICATIONS: **INPUT SENSITIVITY:** 500mV.
OUTPUT POWER: 25W RMS into 8 Ω . **LOAD IMPEDANCE:** 4-16 Ω . **DISTORTION:** 0.04% at 25W at 1kHz.
SIGNAL NOISE RATIO: 75dB. **FREQUENCY RESPONSE:** 10Hz-45kHz \pm 3dB. **SUPPLY VOLTAGE:** 25V. **SIZE:** 105 50 25mm.

Price £6.20 + 77p VAT P&P free.



HY120 60 Watts into 8 Ω

The HY120 is the baby of I.L.P.'s new high power range designed to meet the most exacting requirements including load line and thermal protection this amplifier sets a new standard in modular design.

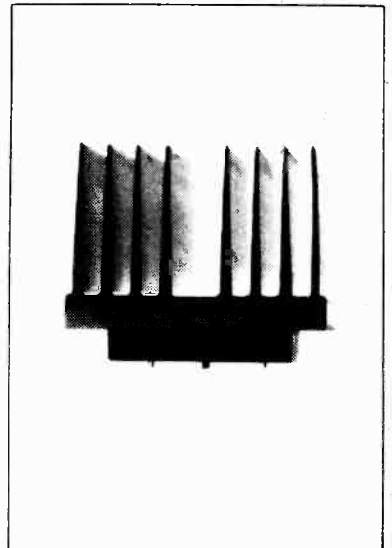
FEATURES: Very low distortion. Integral heatsink. Load line protection. Thermal protection. Five connections. No external components.

APPLICATIONS: Hi-Fi. High quality disco. Public address. Monitor amplifier. Guitar and organ.

SPECIFICATIONS:

INPUT SENSITIVITY: 500mV.
OUTPUT POWER: 60W RMS into 8 Ω . **LOAD IMPEDANCE:** 4-16 Ω . **DISTORTION:** 0.04% at 60W at 1kHz.
SIGNAL NOISE RATIO: 90dB. **FREQUENCY RESPONSE:** 10Hz-45kHz \pm 3dB. **SUPPLY VOLTAGE:** 35V.
SIZE: 114 50 85mm.

Price £14.40 + £1.16 VAT P&P free.



HY200 120 Watts into 8 Ω

The HY200 now improved to give an output of 120 Watts has been designed to stand the most rugged conditions such as disco or group while still retaining true Hi-Fi performance.

FEATURES: Thermal shutdown. Very low distortion. Load line protection. Integral heatsink. No external components.

APPLICATIONS: Hi-Fi. Disco. Monitor. Power slave. Industrial. Public Address.

SPECIFICATIONS:

INPUT SENSITIVITY: 500mV.
OUTPUT POWER: 120W RMS into 8 Ω . **LOAD IMPEDANCE:** 4-16 Ω . **DISTORTION:** 0.05% at 100W at 1kHz.
SIGNAL NOISE RATIO: 96 dB. **FREQUENCY RESPONSE:** 10Hz-45kHz \pm 3dB. **SUPPLY VOLTAGE:** 45V.
SIZE: 114 100 85mm.

Price £21.20 + £1.70 VAT P&P free.

HY400 240 Watts into 4 Ω

The HY400 is I.L.P.'s 'Big Daddy' of the range producing 240W into 4 Ω ! It has been designed for high power disco or public address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to lead the market as a true high power high fidelity power module.

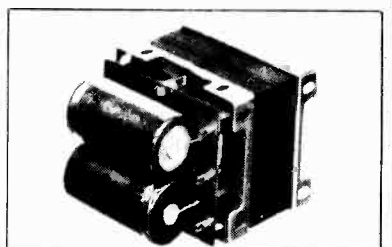
FEATURES: Thermal shutdown. Very low distortion. Load line protection. No external components.

APPLICATIONS: Public address. Disco. Power slave. Industrial.

SPECIFICATIONS:

OUTPUT POWER: 240W RMS into 4 Ω . **LOAD IMPEDANCE:** 4-16 Ω . **DISTORTION:** 0.1% at 240W at 1kHz.
SIGNAL NOISE RATIO: 94dB. **FREQUENCY RESPONSE:** 10Hz-45kHz \pm 3dB. **SUPPLY VOLTAGE:** 45V.
INPUT SENSITIVITY: 500mV. **SIZE:** 114x100x85mm.

Price £29.25 + £2.34 VAT P&P free.



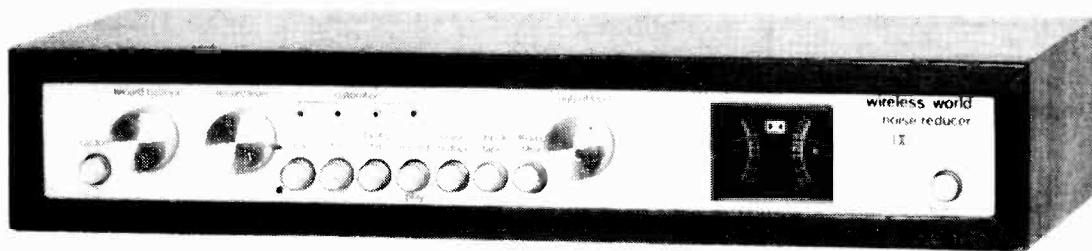
POWER SUPPLIES

PSU36 suitable for two HY30's £4.75 plus 59p VAT P. P. free.
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We are proud to announce the latest addition to our range of matching high fidelity units.

Featuring:

- switching for both encoding (low-level h.f. compression) and decoding
- a switchable f.m. stereo multiplex and bias filter
- provision for decoding Dolby f.m. radio transmissions (as in USA)
- no equipment needed for alignment
- suitability for both open-reel and cassette tape machines
- check tape switch for encoded monitoring in three-head machines

The kit includes:

- complete set of components for stereo processor
- regulated power supply components
- board-mounted DIN sockets and push-button switches
- fibreglass board designed for minimum wiring
- solid mahogany cabinet, chassis, twin meters, front panel, knobs, mounting screws and nuts

Typical performance

Noise reduction: better than 9dB weighted

Clipping level: 16.5dB above Dolby level (measured at 1% third harmonic content)

Harmonic distortion 0.1% at Dolby level typically 0.05% over most of band, rising to a maximum of 0.12%

Signal-to-noise ratio: 75dB (20Hz to 20kHz, signal at Dolby level) at Monitor output.

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30mV sensitivity.

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Please add VAT at 12% unless marked thus*, when 8% applies
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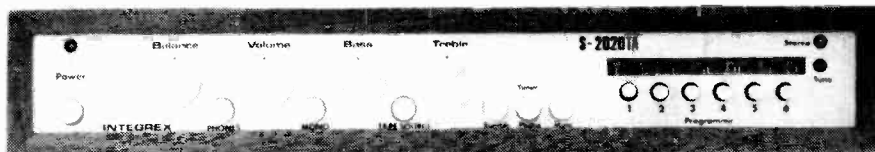
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A high-quality push-button FM Varicap Stereo Tuner combined with a 24W r.m.s. per channel Stereo Amplifier.

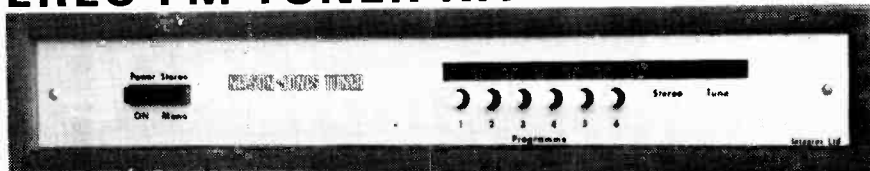


Brief Spec. Amplifier: Low field Toroidal transformer, Mag. input, Tape In/Out facility (for noise reduction unit, etc), THD less than 0.1% at 20W into 8 ohms. Power on/off FET transient protection. All sockets, fuses, etc., are PC mounted for ease of assembly. Tuner section: uses 3302 FET module requiring no RF alignment, ceramic IF, INTERSTATION MUTE, and phase-locked IC stereo decoder. LED tuning and stereo indicators. Tuning range 88—104MHz. 30dB mono S/N @ 1.2 μ V. THD 0.3%. Pre-decoder 'birdy' filter.

PRICE: £53.95 + VAT

NELSON-JONES STEREO FM TUNER KIT

A very high performance tuner with dual gate MOSFET RF and Mixer front end, triple gang varicap tuning, and dual ceramic filter / dual IC IF amp.



Brief Spec. Tuning range 88—104MHz. 20dB mono quieting @ 0.75 μ V. Image rejection — 70dB. IF rejection—85dB. THD typically 0.4%. IC stabilized PSU and LED tuning indicators. Push-button tuning and AFC unit. Choice of either mono or stereo with a choice of stereo decoders.

Compare this spec. with tuners costing twice the price

Mono £29.15 + VAT

With ICPL Decoder £33.42 + VAT

**With Portus-Haywood Decoder
£35.95 + VAT**

STEREO MODULE TUNER KIT

A low-cost Stereo Tuner based on the 3302 FET RF module requiring no alignment. The IF comprises a ceramic filter and high-performance IC Variable INTERSTATION MUTE. PLL stereo decoder IC. Pre-decoder 'birdy' filter



Sens. 30dB S/N mono @ 1.2 μ V
THD typically 0.3%
Tuning range 88—104MHz
LED sig. strength and stereo indicator

PRICE: Mono £26.85 + VAT

Stereo £29.95 + VAT

S-2020A AMPLIFIER KIT

Developed in our laboratories from the highly successful "TEXAN" design. PC mounting potentiometers, switches, sockets and fuses are used for ease of assembly and to minimize wiring. Power 'on/off' FET transient protection.



Typ Spec. 24+24W r.m.s. into 8-ohm load at less than 0.1% THD. Mag. PU input S/N 60dB. Radio input S/N 72dB. Headphone output. Tape In/Out facility (for noise reduction unit, etc.). Toroidal mains transformer.

PRICE: £31.95 + VAT

ALL THE ABOVE KITS ARE SUPPLIED COMPLETE WITH ALL METALWORK, SOCKETS, FUSES, NUTS AND BOLTS, KNOBS, FRONT PANELS, SOLID MAHOGANY CABINETS AND COMPREHENSIVE INSTRUCTIONS

BASIC NELSON-JONES TUNER KIT £14.28 + VAT
BASIC MODULE TUNER KIT (stereo) £16.75 + VAT

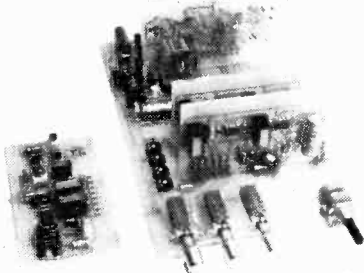
PHASE-LOCKED IC DECODER KIT £4.47 + VAT
PUSH-BUTTON UNIT £4.50 + VAT

PORTUS-HAYWOOD PHASE-LOCKED STEREO DECODER KIT £8.00 + VAT

HART ELECTRONICS

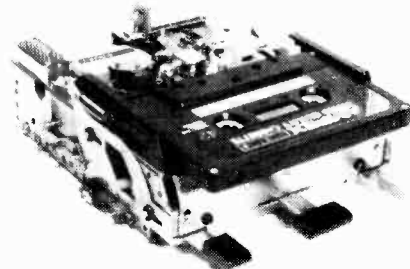
The Only Firm for Quality Audio Kits

J. L. Linsley-Hood High Quality Cassette Recorder



Master Board with one Replay Amp removed

As these circuits in recent issues of "Wireless World" are capable of such an excellent performance we feel that it is not sensible to sacrifice this potential by designing a kit down to a price. We have therefore spent a little more on professional hardware allowing us to design a very advanced modular system. This enables a more satisfactory electrical layout to be achieved, particularly around the very critical input areas of the replay preamps. These are totally stable with this layout and require no extra stabilising components. Many other advantages also come from this system which has separate record and replay amps for each channel plugging in to a master board with gold plated sockets. The most obvious is the reduction of crosstalk and interaction which could cause trouble on a single plane board, with our modular system the layout is compact but there is no component crowding. Testing is very easy with separate identical modules and building with the aid of our component-by-component instructions is childishly simple, but the finished result is a unit designed not to normal domestic standards but to the best professional practice.



LENCO CRV CASSETTE MECHANISM

High Quality, robust cassette transport for Linsley Hood Recorder. Features fast forward, fast rewind, record, pause and automatic cassette ejection facilities. Fitted with Record/Play and Erase Heads and supplied complete with Data and extra cassette ejection spring for above horizontal use. Ex-stock £19.10 + £2.38 VAT

- 71x Complete set of parts for Master Board, includes Bias oscillator, Relay, Controls, etc £9.83 + £1.23 VAT
- 72x Parts for Motor Speed and Solenoid Control for Lenco CRV Deck. £3.52 + 44p VAT
- 73x Complete set of parts for stereo Replay Amps and VU Meter Drive. £8.02 + £1.03 VAT
- 74x Complete set for Stereo Record Amps £6.64 + 83p VAT
- 75x Complete set of parts for Stabilised Power Supply including special Low Hum field Mains Transformer. This unit is a separate 3.5" x 5" PCB designed so that the motor control board fits above it to save space. £8.29 + £1.03 VAT
- 700M. VU Meters Individual high quality meters with excellent ballistics and built-in illumination. £6.48 + 81p VAT PER PAIR.

ALL PARTS ARE POST FREE

Please send 9 x 4 SAE for lists giving fuller details and Price breakdowns.
A suitable Metalwork and Front Plate will be available soon

Penylan Mill, Oswestry, Salop

Personal callers are always welcome, but please note we are closed all day Saturday

MUIRHEAD D-658 18" MUFAX CHART TRANSMITTERS (Model GA). Further details on request. For 110/250v a.c. operation £325.00

MEGGER (Record): 500 volts £20.00 £1.00 post

MEGGER (Evershed Vignoles): 250 volts £17.50 £1.00 post

R216 Receiver MANUAL (photostat copy): £1.50 inc. post

RACAL I.S.B. ADAPTOR RA-95A: £65. Carr. £2.

MUIRHEAD ATTENUATORS: 75 ohms 0.8 Mc/s 3V MAK 3 ranges 0.5, 0.25, 0.50 DB £3.00 + 75p post.

CREED MODEL 75 TELEPRINTER: Receiver only £30.00. Carr. £3.

EDDYSTONE TELEPRINTER ADAPTOR TYPE 937: £45. Carr. £1.

WILD BARFIELD ELECTRIC FURNACE MODEL CCI.22X: With ether indicating temperature controllers Model 990. 0-1400° C. £250. Carr. £5.

CAPACITOR: 10mfd 20Kv working. £35.00 each. Carr. £5.00

POWER UNIT TYPE 234: 200-250v a.c. input, 250-0-250v d.c. @ 100mA and 6.3v @ 4 amps output. £7.50 each. Carr. £2.00.

REDIFON TELEPRINTER RELAY UNIT No. 12: ZA-41196 and power supply 200-250v a.c. Polarised relay type 3SEITR. 80-0V 25mA. Two stabilised valves CV 286. Centre Zero Meter 10-0-10. Size 8in. x 8in. X 8in. New condition. £104 Carr. 75p.

SOLARTRON PULSE GENERATOR TYPE G1101-2: £75.00 each. Carr. £2.00.

TELEPRINTER TYPE 7B: Pageprinter 24V d.c. power supply, speed 50 bauds per min. second hand cond. (excellent order) no parts broken. £20 each. Carriage £3.

AUTO TRANSFORMER: 230V 50c/s. 1000 watts. Mounted in strong steel case 5" x 6 1/4" x 7". Bitumen impregnated. £12.00. Carr. £1.50.

CRYSTAL TEST SET TYPE 193: used for checking crystals in freq. range 3000-10,000KHz. Mains 230V 50Hz. Measures crystal current under oscillatory conditions and the equivalent resistance. Crystal freq. can be tested in conjunction with a freq. meter. £25. Carr. £1.50.

SOLARTRON VARIABLE POWER UNIT S.R.S. 1535: 0-500 volts at 100 mA and 6.3 volts C.T. 3 amps d.c. 110/250 volts a.c. input. £18.50. Carr. £1.50.

CATHODE RAY TUBES. 5" screen, type CV-1536. £4.00 + £1.00 post. Type 95J20 square face 5" x 3" £7.50 + £1.00 post.

PULSE GENERATOR PG21: Pulse width variable 15nS to 200msec in 7 ranges. Delay variable 40nS to 200msec with respect to sync pulse output in 7 ranges. Jitter less than .1%. Repetition rate 1Hz to 10MHz in 7 decade ranges. 20MHz available in double pulse mode. Pulse mode: normal, square wave and double pulse. 240v a.c. As new condition. £125.00. Carr. £2.00.

CLASS 'D' WAVEMETER NO. 1: Crystal controlled heterodyne frequency meter covering 2-8 MHz. Power supply 6V d.c. Good secondhand condition. £8.50. Carr. £1.50.

All U.K. orders subject to Value Added Tax

PRECISION PHASE DETECTOR TYPE 205: Freq. 0.1-15MHz in 5 ranges. Variable time delay microseconds 0-0.1c. 115V input. £55 each. Carr. £1.

RING TOROIDAL DUST CORES: Size 2 1/2" outside 1 1/4" inside 5/16" thick. Box of two £1.00. Post 30p.

MUIRHEAD PHASEMETER TYPE D729: A.M. £95.00. Carr. £3.00.

CT.420 SIGNAL GENERATOR: 200-8000c/s Variable tuning. Two fixed frequencies 9000 and 10,000. Internal calibrator 100 & 500 c/s. £75 each carr. £2.

NOISE GENERATOR TF-1106: Frequency 1 to 200 Mc/s Direct noise factor calibration. Output impedance 70 ohms £65 each. Carr. £1.50.

MW-59 UNIVERSAL KLYSTRON POWER SUPPLY: £85. Carr. £3.

TF-1278/1 TRAVELLING TUBE WAVE AMPLIFIER: £125. Carr. £2.

BPL A.C. MILLIVOLTMETER TYPE VM.348-D Mk. 3: 2 millivolts-2 volts. 6 ranges. £30. Carr. £1.

CAWKELL REMSCOPE TYPE 741: Memory scope. 'as new' cond. £150.00.

MANSON SYNTHESISER Q115-URC: 2-30 mc/s. £175.00.

FIREPROOF TELEPHONES: £25.00 each. carr. £1.50.

POWER UNIT: 110/230 volts a.c. input. 28 volts d.c. at 40 amps output. £30.00 each. Carr. £3.00.

BACKWARD WAVE OSCILLATOR TYPE SE-125: 6.3 heater. 105V Anode. 7.9mA. Mnfr. Watkins & Johnson. £85 each. Carr. £1.

X-BAND MODULATOR CALIBRATOR TYPE MC-4420-X: Mnfr. James Scott. £125 each. Carr. £1.

SMOOTHING UNIT (for the above): £10.00 each. carr. £2.00.

ROTARY INVERTERS: TYPE PE.218E — input 24-28V d.c. 80 Amps. 4,800 rpm Output 115V a.c. 13 Amp 400 c/s. 1Ph. P.F.9. £20.00 each. Carr. £2.50.

FREQUENCY METER BC-221: 125-20,000 Kc/s complete with original calibration charts. Checked out, working order. £21.00 + £1.50 carr.

RECTIFIER UNIT: 200-250v a.c. input, 24v d.c. @ 26 amps output continuous rating. £35.00 each. Carr. £5.00.

EVERSHED SAFETY OHM. METER: Max 10Ma. Test pressure 30v. Complete in leather case. £25.00 each. post £1.00.

FYLDE AMPLIFIERS TYPE 154 BDM: Rack mounted 3v d.c. and power supply FE.500 TP. £65.00. carr. £2.00.

AUTOMATIC VOLTAGE STABILIZERS: Input 207-242v a.c. Output 230v a.c. at 2.80 amps. £17.50, carriage £1.50.

ANTENNA MAST 36ft.: Aluminium. diameter at base 3" tapering to 2" at top. complete with red hazard lights, stays, guys, etc. Normally used with direction finding equipment. Approx. weight 3cwt. £95.00 each. carriage rates on request. With rotating Antenna suitable for 200-400 mHz. £15.00 extra.

BURGLAR ALARM BELL: 6-8v. d.c. £3.00. £1.00 post.

Carriage quotes given are for 50-mile radius of Herts.

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It's the cat's whiskers!



wireless world

A fascinating excursion into the past. The author has unearthed some 400 trade names from the crystal set days, along with nearly 200 manufacturers—giving the name of the set, technical description and original price. He also reviews the first days of broadcasting and looks at the difficulties experienced by crystal set users. Concise information and over 40 illustrations make this book a valuable work of reference as well as a rare piece of nostalgia for collectors.

VINTAGE CRYSTAL SETS 1922-1927

£2.50 from bookshops

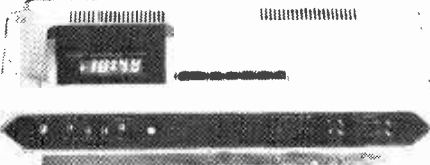
£2.80 inclusive direct from Wireless World, Room 11, General Sales Dept., IPC Business Press Ltd., Dorset House, Stamford Street, London SE1 9LU

Name

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VCS

UNIQUE STEREO ELECTRONIC CLOCK RADIO



£39.90
inc. VAT
P&P £1

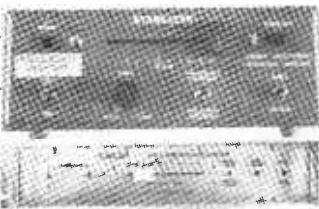
THE REALTONE F4 AM FM STEREO CLOCK RADIO has a unique design. It features an accurate digitron (green) clock incorporating a dimmer control which can be used as a night light or adjusted to a pleasant soft glow. It has a stop watch facility and can be set to display HRS / MINS or MINS / SECS and can be programmed to wake you up to the alarm and/or stereo music. The radio has an FM multiplex Stereo system with AFC (automatic frequency control) which allows drift free reception and incorporates two balanced high fidelity speakers. The wake up / sleep control has its own memory and can be set for up to 59 mins duration.

ALSO THESE SCIENTIFIC CALCULATORS AVAILABLE:

TEXAS SR56 @ £57.95, SR52 @ £199, PC100 Printer for SR52/SR56 @ £175, SR51A @ £47.95, T130 @ £15.95, REALTONE SC6010 @ £50 (13 Memories) SC60 @ £36 (3 memories), CBM4100R @ £36.95, 414BR @ £26.95, ROCKWELL 44RD @ £18.80, 64RD @ £23.90, HP 21 @ £56.25 @ £94.25C @ £155.27 @ £127.67 @ £336.91 @ £320.97 @ £580.201P (Programmable 11 mem, 127 Steps) - £49.95, AL10 @ £16.95, AL8 @ £13.95, FX19 @ £16.95, FX102 @ £19.95 All prices inc. VAT P&P 50p. S.A.E. for full details.

C.W.O. TO: KRAMER & CO., 9 October Place, Holders Hill Road, London NW4 1EJ
01-203 2473. Telex 888541. Attn: KRAMER

STABILIZER



+ 5Hz Fixed Shift Circuit Boards for WW July 1973 article.

Small enough to be built inside the cabinets of many amplifiers

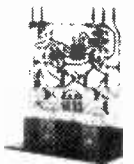
Complete kit and board £24 including PSU & mains transformer DESIGNER Board built and aligned £31 APPROVED

CASH WITH ORDER less a UK POST FREE ADD VAT at 8

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PROFESSIONAL POWER AMPLIFIER MODULES



FEATURES :
SHORT & OPEN CIRCUIT, IMPEDANCE OVERLOAD, MISMATCH AND THERMAL PROTECTION. ONLY 5 EXTERNAL CONNECTIONS REQUIRED.
FULL 2 YEAR GUARANTEE.

•NEW•100w MODEL

	JPS 80 price (£18.75)	JPS 100 price (£23.50)	JPS 150 price (£29.65)
Power Output	70watts RMS 7.6 ohms	110 watts RMS 7.5 ohms	170 watts RMS 7.5ohms
Frequ. Response	10-30 kHz - 0.5dB	10-30 kHz - 0.5dB	10-30 kHz - 0.5dB
Slewing Rate	7.3V per microsec.	8V per microsec.	8.4V per microsec
T.H.D.	0.05% @ 1kHz	0.05% @ 1kHz	0.05% @ 1kHz
Damping Factor	200	400	400
Hum & Noise	115dB below 70 watts	115dB below 110 watts	115 dB below 170 watts
Input Sensitivity	0dB(0.775V) 70 watts	0dB(0.775V) 110 watts	0dB(0.775V) 170 watts
Input Impedance	47k	47k	47k
Power Requirement	± 35Volts	± 45Volts	± 55 Volts
Overall Dimens.	5.8" Long x 3" Wide x 1" High.	5.8" Long x 3" Wide x 1" High	4.8" Long x 3" Wide x 1" High Heat Sink 6" x 5" x 1"

For industrial usage the frequency response of the amplifiers can be extended down to DC + 0dB-0.2dB Input Impedance & Sensitivity can be modified to suit particular requirements.

POWER SUPPLIES

PS100 powers 1 JPS 100 price £14.10 PS60 powers 1 JPS60 price £12.30
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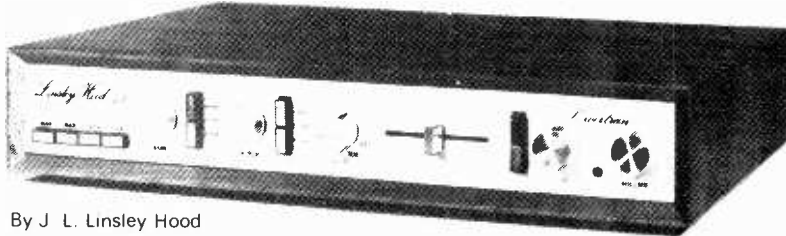
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POWERTRAN ELECTRONICS

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HI-FI NEWS 75W/CHANNEL AMPLIFIER



By J. L. Linsley Hood

- | Pack | Price |
|--|--------|
| 1. Fibreglass printed-circuit board for power amp | £1.15 |
| 2. Set of resistors, capacitors, pre-sets for power amp | £2.15 |
| 3. Set of semiconductors for power amp | £6.50 |
| 4. Pair of 2 drilled, finned heat sinks | £1.10 |
| 5. Fibreglass printed-circuit board for pre-amp | £1.75 |
| 6. Set of low noise resistors, capacitors, pre-sets for pre-amp | £3.40 |
| 7. Set of low noise, high gain semiconductors for pre-amp | £2.40 |
| 8. Set of potentiometers (including mains switch) | £3.15 |
| 9. Set of 4 push-button switches, rotary mode switch | £4.50 |
| 10. Toroidal transformer complete with magnetic screen/housing primary: 0 117-234 V; secondaries: 33-0-33 V, 25-0-25 V | £10.95 |

- | Pack | Price |
|--|-------|
| 11. Fibreglass printed-circuit board for power supply | £0.85 |
| 12. Set of resistors, capacitors, secondary fuses, semi-conductors for power supply | £4.60 |
| 13. Set of miscellaneous parts including DIN sockets, mains input socket, fuse holder, inter-connecting cable, control knobs | £5.95 |
| 14. Set of metalwork parts including silk screen printed fascia panel and all brackets, fixing parts, etc. | £7.50 |
| 15. Handbook | £0.30 |
| 16. Teak cabinet 18.3" x 12.7" x 3.1" | £9.85 |

2 each of packs 1-7 inclusive are required for complete stereo system. Total cost of individually purchased packs £93.75

Designed in response to demand for a tuner to complement the world-wide acclaimed Linsley Hood 75W Amplifier, this kit provides the perfect match. The Wireless World published original circuit has been developed further for inclusion into this outstanding slimline unit and features a pre-aligned front end module, excellent a.m. rejection and temperature compensated varicap tuning, which may be controlled either continuously or by push button pre-selection. Frequencies are indicated by a frequency meter and sliding LED indicators, attached to each channel selector pre-set. The PLL stereo decoder incorporates active filters for 'birdy' suppression and power is supplied via a toroidal transformer and integrated regulator. For long term stability metal oxide resistors are used throughout.

NEW KIT! LINSLEY-HOOD CASSETTE DECK



A full kit has been prepared for this excellent new design. The above illustration is of Mr. Linsley-Hood's own unit but the Powertran kit is, though not identical, very similar and of course in the same cabinet (that used for the outstandingly successful 75W Linsley-Hood Amplifier design).

- | Pack | Price |
|--|--------|
| 1. Stereo PCB (accommodates 2 rep. amps, 2 rec. amps, 2 meter amps, bias/erase osc. relay) | £3.35 |
| 2. Stereo set of capitors, M.O. resistors, potentiometers for above | £9.80 |
| 3. Stereo set of semiconductors for above | £8.90 |
| 4. Miniature relay with socket | £2.45 |
| 5. PCB, all components for solenoid, speed control circuits | £3.20 |
| 6. Goldring Lenco mechanism as specified | £19.10 |
| 7. Function switch, knobs | £1.60 |
| 8. Dual VU meter with illuminating lamp | £7.20 |
| 9. Toroidal transformer with E.S. screen prim. 0-117V, 234V, Sec. 15V | £4.45 |

- | Pack | Price |
|---|-------|
| 10. Set of capacitors, rectifiers, I.C. voltage regulator for power supply (Powertran design) | £2.80 |
| 11. Set of miscellaneous parts, including sockets, fuse holder, fuses, interconnecting wire, etc. | £2.50 |
| 12. Set of metalwork including silk screened fascia panel, internal screen, fixing parts, etc. | £7.10 |
| 13. Construction notes | £0.25 |
| 14. Teak cabinet 18.3" x 12.7" x 3.1" | £9.85 |
- One each of packs 1-14 inclusive are required for complete stereo cassette deck. Total cost of individually purchased packs £82.95

SPECIAL PRICE FOR COMPLETE KITS £78.50

Further details of above given in our FREE LIST

Portugal Mozambique Belgium Sumatra

In Hi-Fi News there was published by Mr. Linsley-Hood a series of four articles (November, 1972; February, 1973) and a subsequent follow-up article (April, 1974) on a design for an amplifier of exceptional performance which has as its principal feature an ability to supply from a direct coupled fully protected output stage, power in excess of 75 watts whilst maintaining distortion at less than 0.01% even at very low power levels. The power amplifier is complemented by a pre-amplifier based on a discrete component operational amplifier referred to as the Liniac which is employed in the two most critical points of the system namely the equalization stage and tone control stage, positions where most conventional designs run out of gain at the extremes of the frequency spectrum. Unusual features of the design are the variable transition frequencies of the tone controls and the variable slope of the scratch filter. There is a choice of four inputs, two equalized and two linear, each having independently adjustable signal level. The attractive slimline unit pictured has been made practical by highly compact PCBs and a specially designed Toroidal transformer.

FREE TEAK CASE WITH FULL KITS
KIT PRICE ONLY £73.90

WIRELESS WORLD FM TUNER



- | Pack | Price |
|---|-------|
| 1. Fibreglass printed board for front end IF strip, demodulator, AFC and mute circuits | £2.15 |
| 2. Set of metal oxide resistors, thermistor, capacitors, ceramic preset for mounting on pack 1 | £4.30 |
| 3. Set of transistors, diodes, LED, integrated circuits for mounting on pack 1 | £5.25 |
| 4. Pre-aligned front end module, coil assembly, three section ceramic filter | £8.50 |
| 5. Fibreglass printed circuit board for stereo decoder | £1.10 |
| 6. Set of metal oxide resistors, capacitors, ceramic preset for decoder | £2.60 |
| 7. Set of transistors LED, integrated circuit for decoder | £2.90 |
| 8. Set of components for channel selector switch module including fibreglass printed circuit board, push-button switches, knobs, LEDs, preset adjusters, etc. | £8.80 |

- | Pack | Price |
|--|-------|
| 9. Function switch, 10 turn tuning potentiometer, knobs | £5.30 |
| 10. Frequency meter, meter drive components, fibreglass printed circuit board | £9.45 |
| 11. Toroidal transformer with electrostatic screen, Primary: 0-117V-234V | £4.45 |
| 12. Set of capacitors, rectifiers, voltage regulator for power supply | £2.95 |
| 13. Set of miscellaneous parts, including sockets, fuse holder, fuses, inter-connecting wire, etc. | £1.50 |
| 14. Set of metal work parts including silk screen printed fascia panel, acrylic silk screen printed tuning indicator panel insert, internal screen, fixing parts, etc. | £7.50 |
| 15. Construction notes (free with complete kit) | £0.25 |
| 16. Teak cabinet 18.3" x 12.7" x 3.1" | £9.85 |

One each of packs 1-16 inclusive are required for complete stereo FM tuner. Total cost of individually purchased packs £76.85

FREE TEAK CASE WITH FULL KITS
KIT PRICE ONLY £66.75

PRICE STABILITY!

Order with confidence! Irrespective of any price changes we will honour all prices in this advertisement for two months from issue date provided that this advertisement is quoted with your order. E&OE VAT rate changes excluded. All components are brand new first grade full specification devices. All resistors (except where stated) are low noise carbon film types. All printed circuit boards are fibre-glass, drilled, roller tinned and supplied with circuit diagrams and construction layouts.

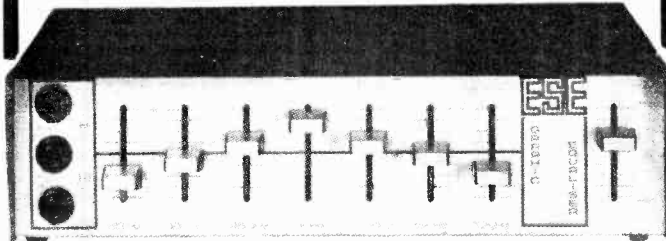
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DEPT. WW11

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No more annoying amplifier noises — just clear, true sound! Frequencies from 60 Hz to 10 kHz!

Cut or boost each frequency by maximum of 15 dB!

Hi and lo gain inputs.

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Try it and you'll buy it — it will change your concept of sound.

Trade enquiries welcomed.

Condensed Technical Spec Max. output: terminated to 600Ω, 10 dB> 1.6 volts peak to peak, 2.5 volts R.M.S.

Signal to noise ratio: input terminated with 47K resistor. All filters at max. better than -70 dB.

Frequency response: All filters at central better than ± 2 dB.

Filter slope: Better than ± 13 dB per octave.

Filter ranges: Max. ± 15 dB at 60, 180, 480 Hz, 1, 2, 4, 5 and 10 kHz.

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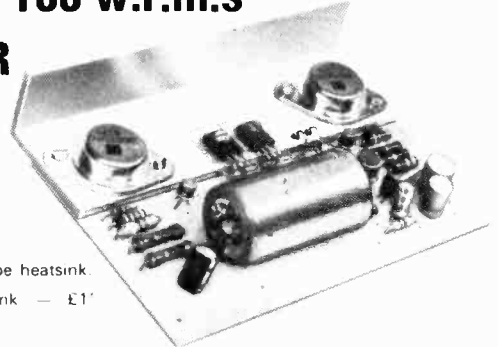
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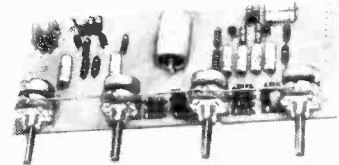
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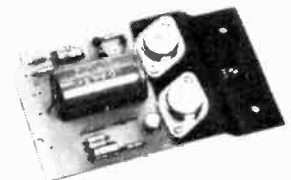
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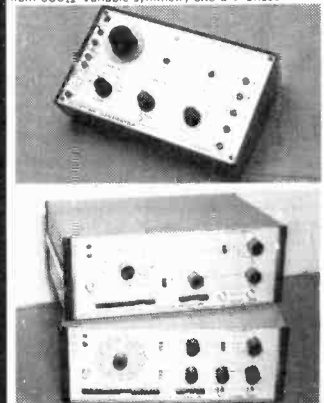
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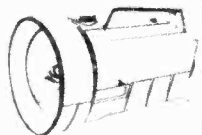
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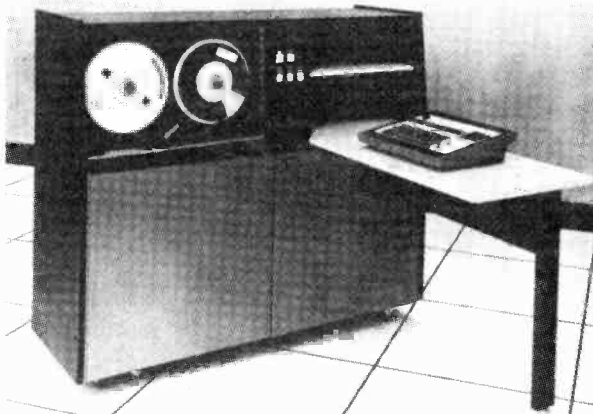
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Table listing digital displays and LEDs like DL704, DL707, DL747, DL750, etc., with prices.

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Table listing thyristor types like 8A, 1A, 4A, etc., with prices.

TRIACS (PLASTIC TO-220 PKG ISOLATED TAB)

Table listing triac types like 10A, 15A, 20A, etc., with prices.

74 TTL mixed prices

Table listing 74 TTL logic components like 7400, 7401, 7402, etc., with prices.

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Table listing linear ICs like LM307, LM390, LM392, etc., with prices.

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Fane Crescendo 15, 8 or 15 ohm	£49.95
Fane Crescendo 18, 8 or 15 ohm	£67.95
Fane 807T 8" d/c, rolls/s, 8 or 15 ohm	£5.18
Fane 801T 8" d/c roll/s 8 ohm	£8.96
Goodmans 8P 8 or 15 ohm	£6.20
Goodmans 10P 8 or 15 ohm	£6.50
Goodmans 12P 8 or 15 ohm	£14.95
Goodmans 12P-D 8 or 15 ohm	£16.95
Goodmans 12P-G 8 or 15 ohm	£16.50
Goodmans Audiom 200 8 ohm	£13.46
Goodmans Axent 100 8 ohm	£7.60
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Kef T27	£5.18
Kef T15	£6.25
Kef B110	£6.75
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Richard Allan Twinkit each	£13.46
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Richard Allan Triple, each	£25.16
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Richard Allan RA8 kit, pair	£37.80
Richard Allan RA82 kit, pair	£59.40
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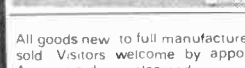
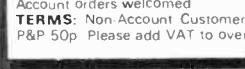
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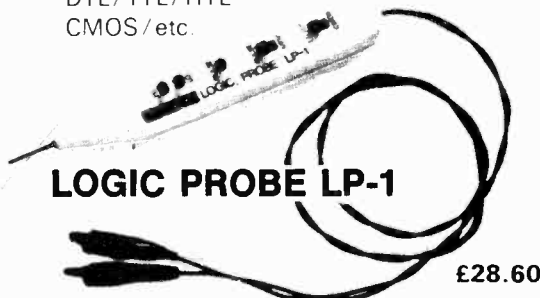
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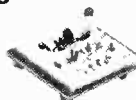


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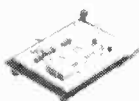
PB-6
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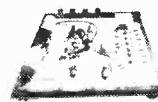
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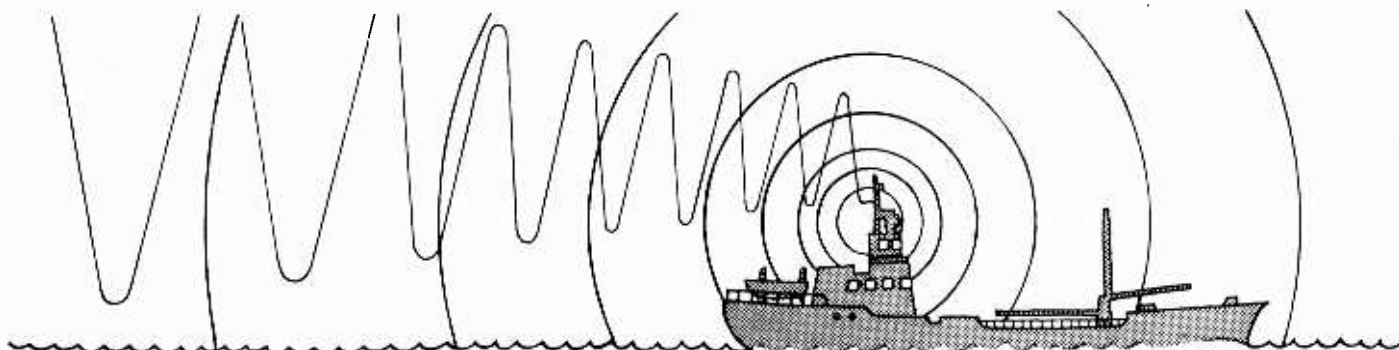
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Advertisements accepted up to 12 noon Monday, October 4, for the November issue, subject to space being available.

DISPLAYED APPOINTMENTS VACANT: £6.50 per single col. centimetre (min. 3cm);
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BOX NUMBERS: 45p extra. (Replies should be addressed to the Box Number in the advertisement, c/o Wireless World, Dorset House, Stamford Street, London SE1 9LU.)
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p.a. is payable. You'll also receive an allowance for shift duties which at the maximum of the scale averages £900 a year and there are opportunities to earn overtime. There's a good pension scheme, sick pay benefits and prospects of promotion to senior management.

Right now we have a few vacancies at some of our coastal radio stations, so if you're 19 or over, preferably with sea-going experience, write to: ETE Maritime Radio Services Division (L690), ET 17.1.1.2., Room 643, Union House, St. Martins-le-Grand, London EC1A 1AR.

Post Office Telecommunications

TELEVISION SYSTEMS AND RESEARCH

require additional

ENGINEERS

for the installation and maintenance of equipment in the UK and overseas. Successful applicants must have at least two years' practical experience in installations or maintenance of electronic equipment, and a sound knowledge of television principals. They will be based at our Richmond branch and will operate primarily in the South East of England with opportunities for short term visits to overseas installations. Salary in the region of £3,000 per annum plus a bonus and lunch allowance scheme. A company estate car will be provided.

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(6255)

AMPEX

Due to expansion of activities we are currently seeking a highly experienced

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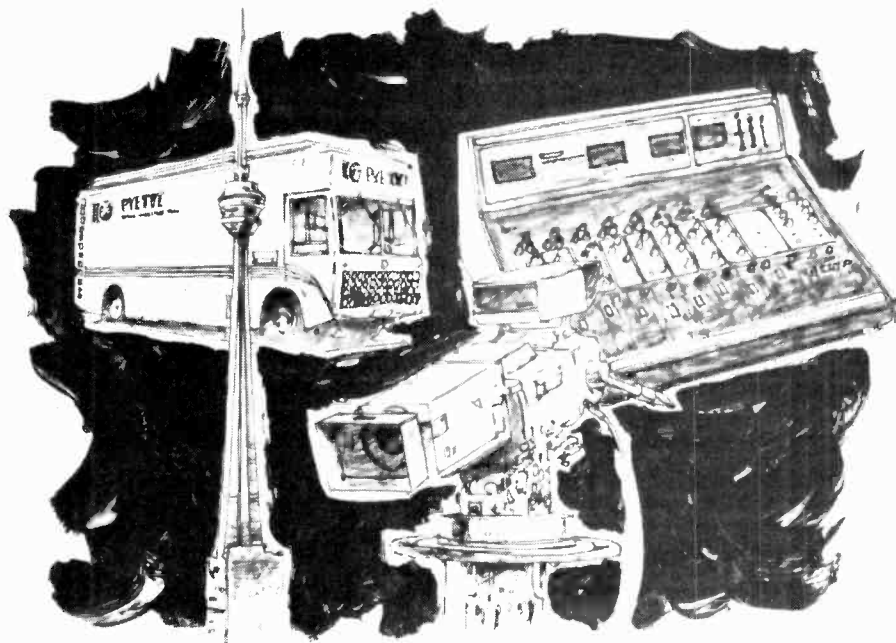
for our Systems Group in Reading. The successful applicant would work with a team of three engineers whose task is to prepare Proposals based on a customer's specification. The Proposal would contain a comprehensive description of the system required, an equipment list, drawings and quotation. It is essential that applicants have operational experience in TV studios and mobiles, also that they are familiar with the characteristics of video and audio switches, lighting, power and air conditioning in mobiles, etc. Some short term travel abroad may be involved in cases where direct contact with customers is necessary, either to define their requirements or to present the Proposal.

We offer an interesting and varied job in a pleasant atmosphere. Salary will be commensurate with experience and ability. Please call Proposals Manager, Maurice Nash, on telephone number (0734) 85200 extension 247, or send your application to **The Personnel Manager, AMPEX ELECTRONICS LTD., 72 Berkeley Avenue, Reading RG1 6HZ, quoting reference "Systems".**

(6263)

Our success opens up new opportunities for you

Pye TVT Limited is an international leader in broadcasting engineering. We took colour TV to ZANZIBAR – the very first colour service in the whole of Africa. In OMAN we were awarded probably the largest single broadcasting contract ever placed – a complete radio and TV *turnkey* project. Other successes in CANADA, the FAR EAST and many other parts of the world open up new, rare opportunities for *you*.



SENIOR STUDIO INSTALLATION ENGINEER

The job involves the supervision of all aspects of installation testing and commissioning of professional colour TV broadcast studio projects on site to ensure that specifications are met and standards strictly maintained. Reporting to the Installations Supervisor or Site Engineer, you will control all subordinate engineering grades, fitters, wiremen and sub-contract labour. You should therefore be prepared to spend periods of up to 4 months abroad. Candidates, who should have H.N.C. or an equivalent qualification will be expected to be fully conversant with the installation and testing of modern generation TV studio equipment and have good leadership and organisational qualities.

STUDIO PLANNING ENGINEER

Your responsibilities will include the preparation of documents and drawings relating to the design of studios. This will involve the preparation of schematics and building lay-outs.

A working knowledge of TV studio operation and maintenance is required and a full City & Guilds Technological Certificate or H.N.C. is necessary. Recent attendance at a BBC or ITV Studio Training Centre or practical experience of studio planning and installation is desirable.

The successful candidate will be adaptable, self-motivated, and prepared to spend short periods abroad.

Attractive salaries are offered and Company benefits include good catering facilities, staff shop, pension fund and an active sports and social club. Assistance with relocation expenses is given in approved cases. Apply to: David Barnicoat, Personnel Officer.

SENIOR TRANSMITTER SYSTEMS TEST ENGINEERS

The job requires the ability to align TV transmitter systems and to demonstrate that they meet their specifications. This entails the use of a wide range of equipment in the video, audio, digital and R.F. fields. You should be self-motivated and have at least two years' experience of testing or commissioning U.H.F. or V.H.F. high power TV transmitters. Ideally you will have H.N.D., or equivalent. The ability to work with customers' engineers of various nationalities is essential. Some training of customers and assistant engineers may occasionally be required. A clean driving licence is essential and you should be prepared to make occasional visits to installations abroad.

SYSTEMS TEST ENGINEERS

The job is to ensure that the specified technical performance of a system is actually achieved, and this requires the ability to work on a wide range of equipment in the video, audio, digital and R.F. fields. The successful candidate will have had experience of the maintenance and testing of broadcast systems, or detailed experience in a particular product area, and will ideally have H.N.C./H.N.D. or equivalent. The ability to work with the minimum of supervision and with customers' engineers of various nationalities is essential.



Pye TVT Limited

PO Box 41 Coldhams Lane Cambridge CB1 3JU
Tel. Cambridge (0223) 45115 Telex 81103

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ELECTRONIC TEST ENGINEERS

At M.E.L., part of the Philips Concern, we develop and manufacture sophisticated Electronic Equipment for the British Services and overseas markets.

We are currently recruiting Test Engineers at all levels, but have specific vacancies for the following personnel:-

PROJECT TEST ENGINEERS

to work on Clansman - a new range of tactical radio systems for the British Army and export markets.

We require a Senior Engineer to build up a team of Test Engineers involved in fault-finding on the High Power Clansman System. The successful applicant should have had previous experience of supervision and of working on high voltage radio frequencies.

We are expanding a team of engineers who give technical advice to the various test sections within the Radio Department. Two Engineers are needed to prepare and plan test schedules and associated equipment to finalised stages ensuring production target achievement.

A background in modern medium frequency radio communication is desirable

SENIOR TEST ENGINEER

to work in our Automatic Telegraph Systems Project Group at Whyteleafe, Surrey, engaged in the production of sophisticated message handling systems for the Royal Navy.

Applicants should have previous experience in MOS and TTL logic systems, power supply and general analogue techniques.

We offer progressive salaries, annual bonus and pension schemes, staff restaurant and shop and at least 22 days annual holiday. M.E.L. is located in Crawley, an expanding new town in the middle of Sussex, midway between London and Brighton. There is ample opportunity for both house rental and purchase within the area. We will give you generous assistance in your relocation to this attractive part of Sussex. If interested, please write or telephone for an application form to:- C. Marks, Personnel Officer, The M.E.L. Equipment Company Limited, Manor Royal, Crawley, Sussex. Telephone Crawley 28787.

(6205)

M E L

KING'S HEALTH DISTRICT
Department of Biomedical Engineering
Dulwich Hospital

ELECTRONICS TECHNICIAN

required to join the department of Biomedical Engineering, to assist research groups within the department with the design, development and maintenance of electronic signal processing equipment, using analogue digital and radio-frequency techniques.

Applicants should possess an HND or equivalent in electronics as a minimum. Additional industrial experience would be an advantage.

The post is tenable for 1 year in the first instance but is renewable up to a maximum of 3 years. Initial salary will be within the range of £2808-£2922 including London Weighting allowance and salary supplement commensurate with experience and qualification. Application, giving details of age, qualifications and experience together with the names of two referees.

Application forms available from the Personnel Office, King's College Hospital, Denmark Hill, London SE5 9RS. Tel. 01-274 6222. Ext. 2753 (Medical Staffing) should be completed and returned by 27th October, 1976.

(6193)

Medical Research Council requires
an
ELECTRONICS TECHNICIAN

for the construction and repair of electronic instruments and for the maintenance of a Linear Accelerator. A degree or HNC in relevant subject is required. Salary, according to age (limit age 25) and experience, in the range £2511-£2790 plus London Weighting.

Apply, giving full particulars, to the Director, MRC Cyclotron Unit, Hammersmith Hospital, London W12 0HS (tel. 01-743 4594, ext. 103).

6199

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Immediate vacancies exist in most areas for engineers qualified to BSc/HNC/C&G with analogue, digital or R.F. experience.

Phone or write

APEX PERSONNEL
800 FULHAM ROAD
LONDON S W 6

01-731 4353

6220

Audio Engineer

An opportunity has arisen within our Company for an experienced Audio Engineer. Applicants should have C & G Radio and Television and at least 4 years' experience in the Audio Engineering Field. Age 24+.

This vacancy is in our modern workshops located at Slough. We can offer the successful applicant an attractive salary plus all the benefits associated with a major international Company. Please apply for Application form to

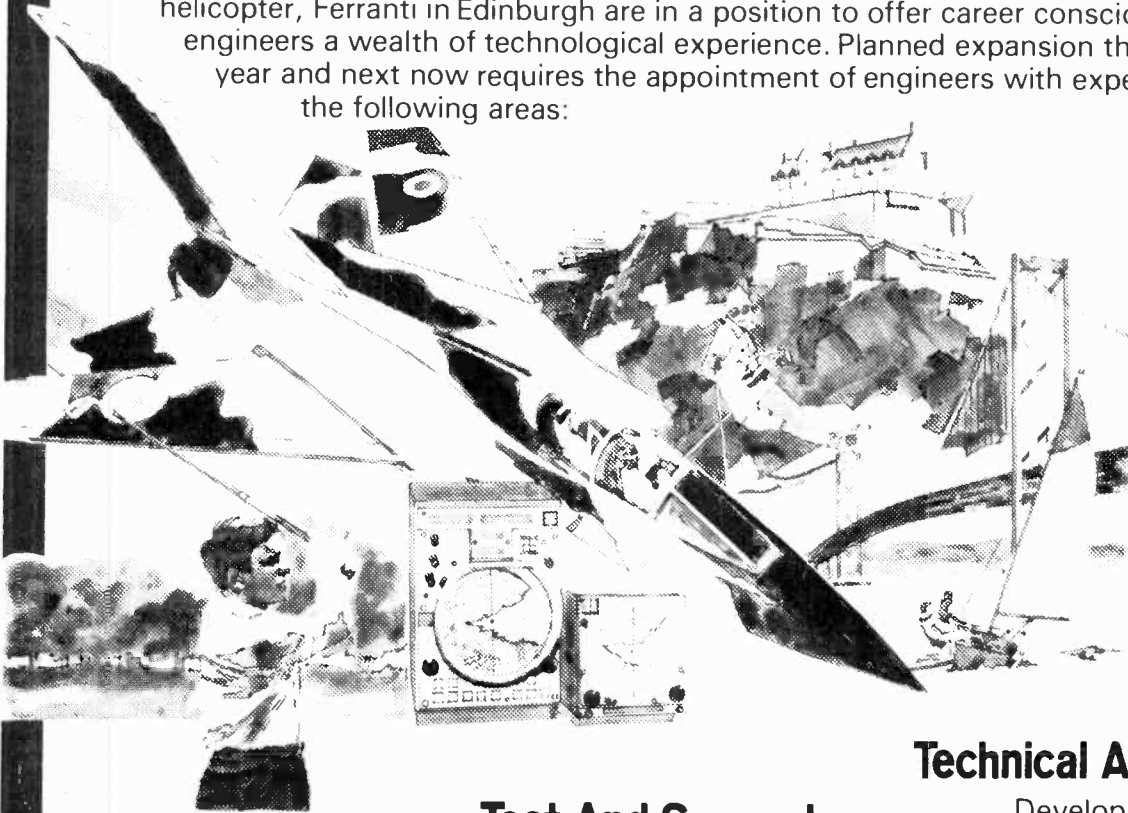
Mrs. E. M. McClure, Personnel Officer
AEG Telefunken (UK) Ltd, Bath Road, Slough, Berks.
Tel. Slough 872350

6194

AEG

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With contracts for a variety of advanced avionic projects in the Tornado (MRCA), Sea Harrier, Nimrod Mk2, Mitsubishi FS-T2, Jaguar and the naval Lynx helicopter, Ferranti in Edinburgh are in a position to offer career conscious engineers a wealth of technological experience. Planned expansion through this year and next now requires the appointment of engineers with experience in the following areas:



Design/Development

Opportunities exist for electronic and mechanical engineers with qualifications ranging from HND to Honours degree to join our design teams involved in airborne radars, laser range finding and target seeking equipments, inertial navigation systems and their associated test gear.

Test And Support

To support our design teams we need engineers with qualifications from C & G to HNC, preferably with Test and Quality Assurance experience.

They will become involved in a range of work covering automatic test equipment, fault diagnosis and building special-to-type test equipment.

Technical Authors

Development across all our projects requires parallel expansion in our Technical Publications Group.

Experienced technical authors will find the close association with project design particularly stimulating and for engineers keen to embark on such a career this is an opportunity to train in one of the most authoritative technical writing teams in the country.

Salaries are negotiable. The Company operates a contributory pension and life assurance scheme and incoming employees will qualify for housing under the Scottish Special Housing Association scheme.

Apply in writing, quoting reference WW/5, with particulars of qualifications and experience to:

Staff Appointments Officer,
Ferranti Limited, Ferry Road,
Edinburgh EH5 2XS.

FERRANTI

UNIVERSITY OF GLASGOW ELECTRONICS TECHNICIANS

Applications are invited for vacant electronics posts in the following departments:

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Grade 7 to supervise a departmental workshop, responsibility for design development and construction of prototype electronic apparatus for chemical applications/maintenance of existing equipment, experience in both digital and analogue electronics. Ref. No. 3861 FH.

DEPARTMENT OF NATURAL PHILOSOPHY

Grade 6, electronics technician for maintenance and repair of the scanning and measuring projector attached to computer. Ref. No. 3862 FH.

KELVIN LABORATORY, EAST KILBRIDE

Grade 5, electronics technician for electron linear accelerator, electrical and mechanical testing of magnets; experience with high current power supplies or large electro-magnets an advantage. Grade 2B electronics technicians to assist in general maintenance; Grade 2B, operators for electron linear accelerator, experience in operation of radar or similar equipment an advantage (no formal qualifications required). Ref. No. 3863 FH.

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Grade 3, technician for variety of techniques in connection with medical ultrasonics. Ref. 3864 FH.

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Grade 5, applications of the latest techniques in electronics to the solution of problems in medical research and teaching/design, build and maintain electronic equipment. Ref. No. 3865 FH.

VETERINARY REPRODUCTION & SURGERY AT GARSCUBE

Grade 2B, electronics/physiological measurement. ref. No. 3866 FH.

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Grades 5, 4 & 3, technicians experienced in modern circuitry and instrumentation to assist in development, maintenance and testing of equipment for research. Ref. No. 3867 FH.

There is a Non-Academic Staff Pension Fund and holiday entitlement is 29 days per year (inclusive of 8 public holidays).

Salary ranges and minimum qualifications are
 £3354 - £3810 + £312 HNC with over 10 years' experience for Grade 7
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 £2439 - £2895 + £312 ONC with 7-9 years' experience for Grade 5
 £1860 - £2343 + £312 ONC with 3-5 years' experience for Grades 3 & 2B

Applicants should send details of age, qualifications and experience to the Personnel Officer, University of Glasgow, Glasgow G12 8QQ, from whom further particulars may be obtained.

(6241)

THE PAPUA NEW GUINEA UNIVERSITY OF TECHNOLOGY DEPARTMENT OF ELECTRICAL & COMMUNICATION ENGINEERING TECHNICAL INSTRUCTOR

DUTIES: Teaching of technical subjects in the Communications Diploma course and to assist in the general development of the course, training aids and laboratories

QUALIFICATIONS: Applicants should have experience in the tele-communications field. Experience in training personnel to technician or technician engineer level is desirable and applicants should themselves be qualified to at least technical engineer level. Specialist experience in one or more of the following fields would be an advantage: Line Transmission, Telephony, Telegraphy, Broadcasting. Salary Range K8663-9613 (Currently 1 Kina equals 74 1/2p as at 13/10/76).

Allowances additional to salary are payable as follows: Married K2 300 per annum Single K1 300 per annum. In certain circumstances a child allowance of K156 per annum is also payable. An educational allowance and additional fares may be provided for children educated away from their parents' place of residence. Other benefits include furnished housing (hard goods only) supplied at nominal rental, leave fares to place of recruitment Australia each alternate year and six weeks annual leave. Superannuation benefits apply in most circumstances. Study Leave of six months will accrue after five semesters of service. Appointment will be on a contract basis for a minimum of three years in the first instance. The University reserves the right not to appoint or to appoint by invitation.

Applications in duplicate should include particulars of age, nationality, marital status, family if any, qualifications, experience, present post, the names and addresses of three referees from whom confidential enquiries can be made and should reach the Registrar, The Papua New Guinea University of Technology, P.O. Box 793 LAE, PAPUA NEW GUINEA, before 1 December, 1976. A copy of the application should be sent to Association of Commonwealth Universities (Apps) 36 Gordon Square London WC1H 0PF, from whom general information may be obtained.

6218



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(6229)

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ELECTRONICS TECHNICIAN in Department of Engineering Production, University of Birmingham. Analogue and digital circuit development, computer interfacing, instrumentation, machine-tool control. Do you have substantial experience or two or more of these plus initiative and self-motivation. Do you enjoy varied work in a small team? Salary scale £2,751-3,207 p.a. Ref 173/C/269. Application forms from Assistant Secretary, Personnel Office, University of Birmingham, P.O. Box 363, Birmingham B15 2TT. (6195)

Television International

TELEVISION INTERNATIONAL, the largest broadcast facilities company in Europe, has vacancies for

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experienced in the operation and maintenance of Philips VCR and Sony U Matic machines

The work is contained within a broadcast environment, and every encouragement will be given to the successful applicants to progress to the operation and maintenance of broadcast videotape equipment.

Salary, according to experience ranging from £3,171 - £4,608, plus £433 London Weighting.

The company gives a colour incentive bonus in addition to a service incremental scheme.

Applications in writing to Harold Gray, Head of VTR Engineering, Television International Operations Limited, 9/11 Windmill Street, London W1P 1HF.

(6253)

**LINCOLNSHIRE AREA HEALTH
AUTHORITY
NORTH LINCOLNSHIRE DISTRICT
ST. GEORGE'S HOSPITAL
Long Leys Road, Lincoln
Area Medical Physics Service**
Tel: Lincoln (0522) 29921, ext. 7122.
Ref: SGH 27

TECHNICIAN GRADE III

in the Area Medical Physics Department at the above hospital.

Applicants should be prepared to join a small team undertaking technical support of electro-medical and laboratory equipment, including planned preventive and breakdown maintenance. The work will also involve collaboration with Electrical Engineers and Physicists on varied development projects.

Qualification to HNC standard is required, together with a minimum of 3 years' practical experience. Experience of mini-computer operation would be an advantage.

Salary: According to the scale £2784 to £3630 per annum, plus £312 per annum non-enhanceable supplement. Single accommodation may be available.

Further informal details from Mr. S. N. Mukherjee, Area Physicist-in-Charge, Medical Physics Department.

Written application, giving full details and names and addresses of two referees to: District Personnel Officer, Lincolnshire Area Health Authority, North Lincolnshire District, 1 St. Anne's Road, Lincoln.

Closing date: 29th October, 1976.

(6200)

UNIVERSITY OF LIVERPOOL ELECTRONICS TECHNICIAN

required to service a wide range of electronic equipment and develop new instrumentation in the Department of Organic Chemistry. Several years' experience as an electronics engineer and at least ONC (or equivalent) are essential. HNC preferred. Salary within a range up to £3762 p.a. (under review) according to qualifications and experience. Application forms may be obtained from the Registrar, The University, P.O. Box 147, Liverpool L69 3BX. Quote Ref. RV/888/WW. 6219

UNIVERSITY OF ABERDEEN

TELEVISION SERVICE

TELEVISION ENGINEER

Applications are invited for a new post of TELEVISION ENGINEER in the University's Television Service required for expansion of the Service, particularly in the medical field.

Applicants should be professionally qualified television engineers with considerable experience of operations and maintenance of colour television origination and recording systems. A knowledge of television studio lighting would be an advantage. Normal colour vision is a requirement.

Salary on scale £5214-£6446 with appropriate placing.

Further particulars from The Secretary, The University, Aberdeen, with whom applications (2 copies) should be lodged by 4 November, 1976.

(6231)

**UNIVERSITY OF
EXETER
DEPARTMENT OF
PHYSICS**

Applications are invited for the post of

ELECTRONICS TECHNICIAN

Duties will involve repair and recalibration of commercially produced instruments and construction testing of prototype equipment in a well-equipped Electronics workshop.

Applicants should be experienced in the repair of transistor circuitry and be prepared to extend their knowledge to integrated circuits. An interest in Audio Recording would be an advantage.

The appointment will be made on the scale for Technician Grade 3, salary £2,325-£2,655 per annum.

Applications in writing giving full personal particulars, qualifications and experience and the names of two referees should be sent to the Personnel Officer, University of Exeter, Exeter EX4 4QY by 21st October, 1976. Please quote reference number 1/79/5075.

(6232)

unilever research

Analytical Chemistry

The Unilever Colworth/Welwyn Laboratory is the largest food research centre in Western Europe, situated in the pleasant North Bedfordshire countryside.

The following vacancy exists for a Graduate in a Section that provides analytical chemistry support to most projects in the Laboratory, and many manufacturing companies on a world-wide basis.

INSTRUMENTATION — DATA PROCESSING ENGINEER

This job (Ref. CWA328) is concerned with the design, construction and commissioning of instruments and interfaces, mainly associated with techniques used by Analytical Chemists. The job-holder will work with another Engineer, and will be required to translate paper designs into working prototypes.

Skills: A working knowledge of both digital and analogue circuits, along with a high level of constructional ability. This will also call for preparation of printed circuit artwork and an aptitude for light mechanical work.

Qualifications: A Degree or H.N.C. in Electronics plus at least two years' relevant, preferably industrial, experience.

Salary Scale: £3,000, depending on age and experience, up to £3,962.

Interested applicants should write for an application form (quoting reference number CWA328) to:

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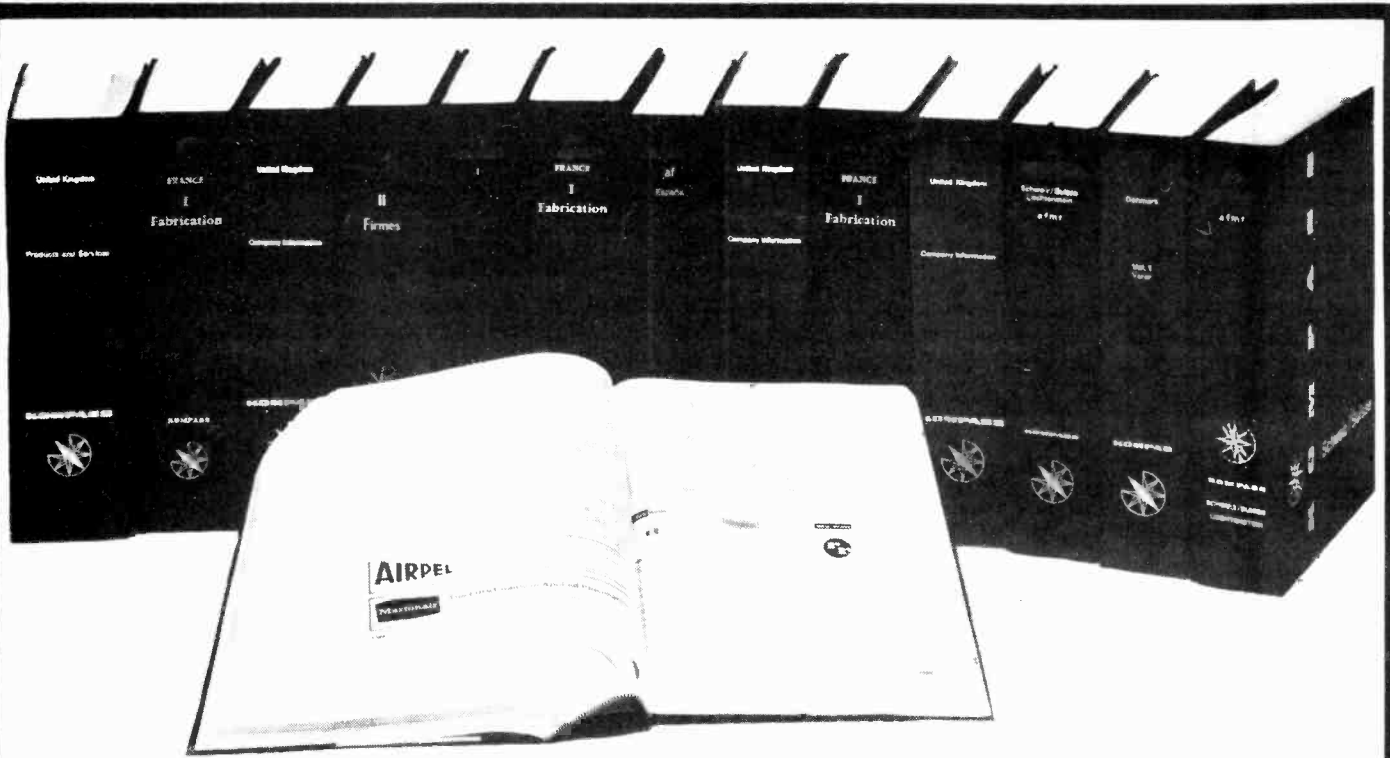
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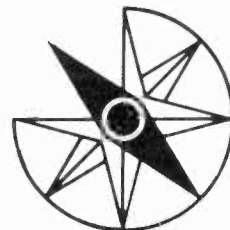
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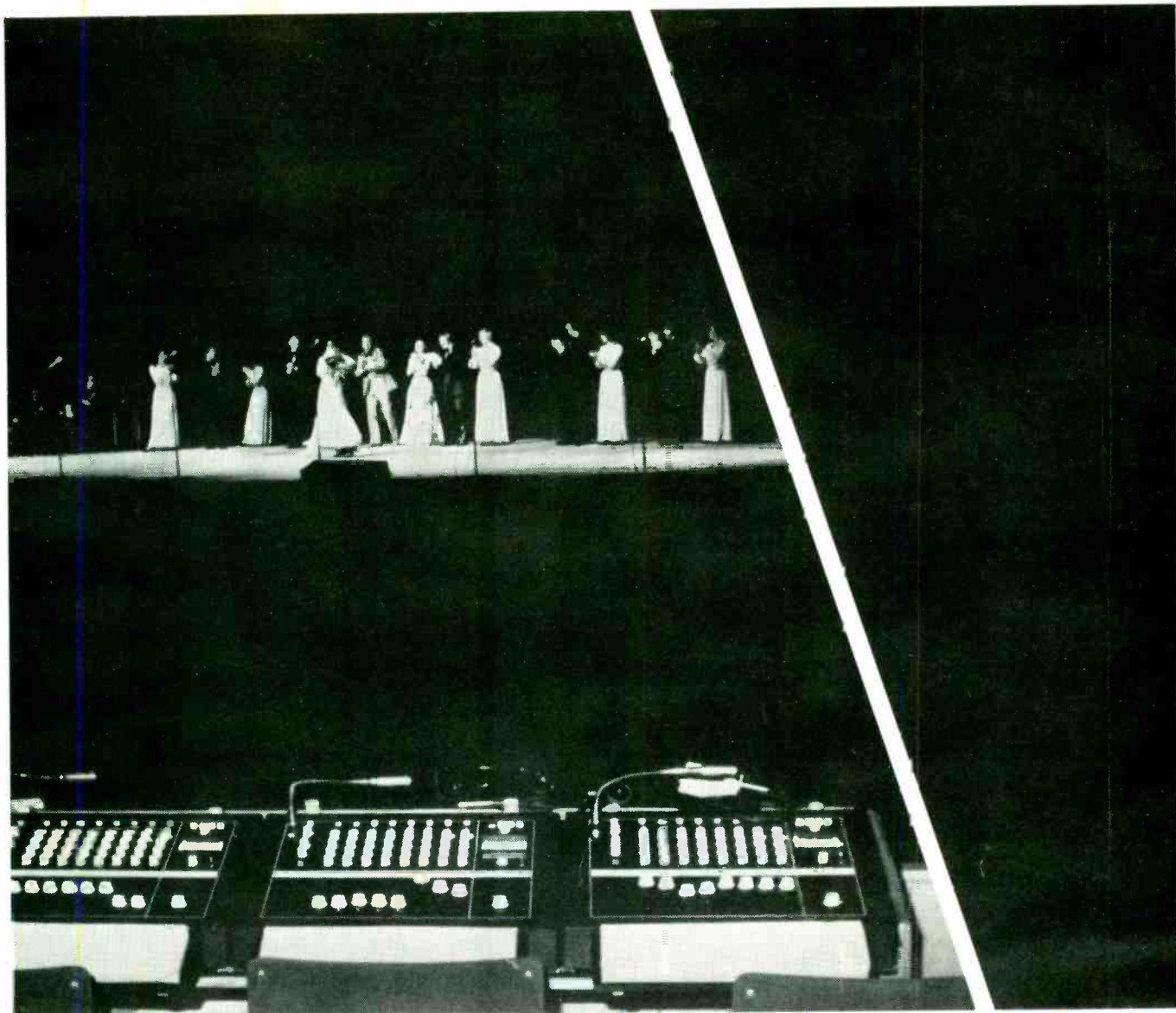
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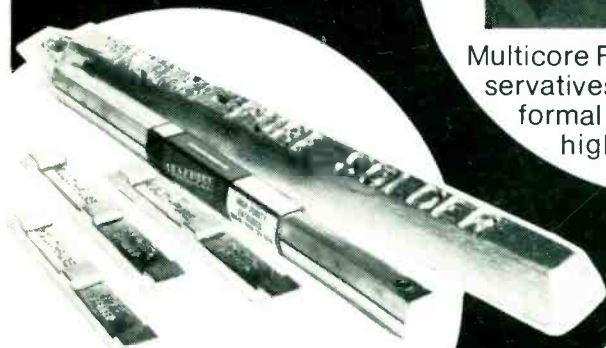


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