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JULY 1969

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PHOTO-ELECTRIC RECEIVER



REMOTE

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the CHROMATONE

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Lasky's Radio

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WITH AD-76K
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CARTRIDGE

AP75 3 speed single play deck with Synchro-Lab motor—offered with the outstanding AD-76K stereo magnetic cartridge



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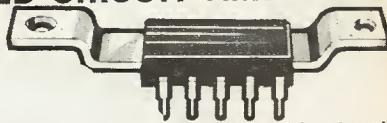
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EXCLUSIVE FIRST

PRESENTING THE IC-403
INTEGRATED CIRCUIT AMPLIFIER
MODULE
AVAILABLE
NOW!



Originally developed for computer and space projects these tiny modules—size only 25 × 10 × 5 millimetres—represent the most amazing breakthrough in circuit design since the introduction of the transistor. The actual circuit—no bigger than a pinhead—is encapsulated in solid plastic fused with the heatsink and connecting pins to make an almost indestructible unit. The IC-403 is an integrated power and pre-amplifier requiring only the addition of tone and volume controls, power source and speaker to form a complete audio amplifier of 3W output. There are many applications for this unique device, wherever high efficiency and ultra compact size is required, i.e. miniature P.A. and audio amplifiers, intercoms, electronic organs, tape recorders, etc., etc.

SPECIFICATION (ratings at 25°C): Output power typically 3W from 250mV input. Frequency response 20Hz to 80KHz ± 3dB. Power amp. distortion 0.3% (at 1W, 400Hz). Pre-amp. gain 24dB. Power amp. gain 26dB. Max. operating voltage 21V. Min. operating load 7.5 ohms. Noise level -75dB. Pre-amp. input imp. 23M/ohms. Pre-amp. and power amp. D.C. input current 50mA.

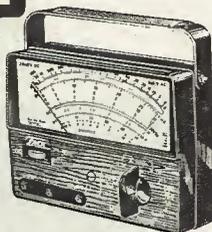
THE IC-403 IS AVAILABLE FROM STOCK EXCLUSIVELY FROM LASKY'S
—COMP. WITH INS. DATA AND SUGGESTED CIRCUIT APPLICATIONS

LASKY'S PRICE ONLY **52/6**

Post 2/6

TEST METERS TMK Model PL-436

20,000 O.P.V. Multitester for the amateur or professional. Features mirror scale and wood grain finish front panel. SPEC.: DC/V ranges: 0.6, 3, 12, 30, 120, 600V at 20K/O.P.V. AC/V ranges: 3, 30, 120, 600V at K/O.P.V. DC current: 50µA, 0.6, 60, 600mA. Resistance: 10K, 100K, 1M and 10M ohms end scale (5, 650, 6.5K and 65K ohms centre scale). Decibels: -20 to +57dB in four ranges. Operates on 2 × 1.5V U7 type batteries. Size: 5½ × 4½ × 2½ in. Complete with test leads, battery and instructions.



LASKY'S PRICE **£7.19.6**

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TTC Model C-1000

A really tiny 1,000 O.P.V. pocket multi-tester with "big" meter performance. Precision 2 jewel meter movement. Hand calibrated to ±3% accuracy on full scale of DC ranges. 4% on AC ranges. 2½ in. square meter. SPECIFICATIONS: AC/V ranges: 0-10, 50, 250, 1,000V at 1K/O.P.V. AC/V ranges: 0-10, 50, 250, 100V at 1K/O.P.V. DC current: 0-1-100mA. Resistance: 0-150K/ohms (3,000 ohms centre scale). Decibels: -10 to +22dB. Operates on one penlight cell. Two colour buff/green case—size only 3½ × 2½ × 1 in. Click stop range selection switch. Ohms zero adjustment. Complete with test leads, battery and ins.



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A portable radiogram of ultra slim "briefcase" proportions. Very smart impact resistant plastic cabinet with leather grain finish. The NRP-840 operates on 220/240V AC mains with built-in AC converter or 6 × 1½V (U2 type) batteries. The radio section covers full AM (medium band) 5,400-1,600Kc/s and Long wave 150-370Kc/s. MW reception through an internal ferrite aerial plus 7 section telescopic antenna for LW. The gram which are easily selected on a rotary control. Plays all sizes of records, 7, 10 and 12in. Lightweight spring loaded pickup arm with crystal cartridge automatically switches turntable off when in rest position. Supplied complete with mains lead, centre spindle adaptor, batteries and instructions. The ideal unit for your summer pleasure anywhere, anytime. Size: 13 × 9½ × 3ins. Available in black or red; please specify when ordering.



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a complete stereo system for 28 gns!



The new Duo general purpose two way system is beautifully finished in polished teak veneer, with matching vinyl grille. It is ideal for wall or shelf mounting either upright or horizontally. **SPECIFICATION:** Impedance 10 ohms. It incorporates Goodmans high flux 6 x 4in and 2 1/2in tweeter. Teak finish 12 x 6 1/2 x 5 1/2in. 4 guineas each, P. & P. 7/6. Garrard Changers from £7.19.6, P. & P. 7/6. Cover and Teak finish Plinth £4.15.0, P. & P. 7/6.

THE DUETTO 9 GNS

Integrated Transistor Stereo Amplifier + 7/6 P. & P.

The Duetto is a good looking quality amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more. **SPECIFICATION:** R.M.S. power output: 3 watts per channel into 10 ohms speakers. Input Sensitivity: Suitable for medium or high output crystal cartridges and tuners. Crosstalk better than 30dB at 1Kc/s. Controls: 4-position selector switch (2 pos. mono and 2 pos. stereo) dual ganged volume control. Tone Control: Treble lift and cut. Separate on/off switch. A preset balance control.

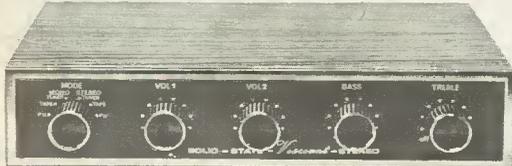
THE RELIANT

Solid State General Purpose Amplifier

6 1/2 GNS
+ 7/6 P. & P.



SPECIFICATION: Output: 10 watts into a 3 ohms speaker. Inputs: (1) for mike (10 m.v.). Input (2) for gram, radio (250 m.v.) individual bass and treble control. Transistors: 4 silicon and three germanium. Mains input: 220/250 volts. Size 10 1/2 x 4 1/2 x 2 1/2in. Price: 6 1/2 guineas in teak finished case. Less teak case 5 1/2 guineas. P. & P. 7/6. Mike to Suit: (Crystal) 12/6 + 1/6 P. & P. 8 x 5in speaker 14/6 + 3/- P. & P.



THE VISCOUNT 13 1/2 GNS

Integrated High Fidelity Transistor Stereo Amplifier + 7/6 P. & P.

SPECIFICATIONS: Output: 10 watts per channel into 3 to 4 ohms speakers (20 watts monaural). Input: 6 position rotary selector switch (3 pos. mono and 3 pos. stereo), P.U., Tuner, Tape and Tape Rec. Sensitivity: All inputs 100mV into 1.8M ohm. Frequency response: 40Hz-20KHz ± 2db. Tone controls: Separate bass and treble controls. TREBLE 13db lift and cut at 15KHz. BASS 15db lift and 25db cut at 60Hz. Volume controls: Separate for each channel. A.C. mains input: 200-240V. 50-60Hz. Size: 12 1/2 x 6 x 2 1/2in in teak finished case. Built and tested. P. & P. 7/6.

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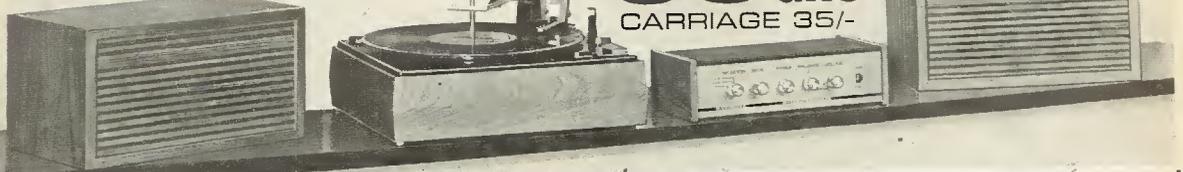
PREMIER RADIO

23, TOTTENHAM COURT ROAD, LONDON, W.1 Tel: 01-636 3451



COMPLETE STEREO SYSTEM

FOR ONLY **39 GNS**
CARRIAGE 35/-



The Premier Stereo System consists of an all transistor stereo amplifier, Garrard Model 2025 auto/manual record player unit fitted stereo/mono cartridge and mounted in teak finish plinth with perspex cover and two matching teak finish loudspeaker systems. Absolutely complete and supplied ready to plug in and play. The 10 transistor Amplifier has an output of 5 watts per channel with inputs for pick up, tape and tuner also tape output socket. Controls: Bass, Treble, Volume, Selector. Power on/off, stereo/mono switch. Brushed aluminium front panel. Black metal case with teakwood ends: Size 12" x 5 1/2" x 3 1/2" high (Amplifier available separately if required £14.19.6. Carr. 7/6).

WIDE RANGE OF HI-FI STEREO EQUIPMENT ON DEMONSTRATION

All leading makes available including Rogers Armstrong Dulci, Wharfedale, Goodmans, Goldring, Shure, etc. etc.

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1025 Stereo/Mono cart.	£7.19.6	
2025 Stereo/Mono cart.	£8.19.6	Teak Plinth with perspex cover as above £5.10.0.
3000 with STAICD Carriage 7/6 extra.	£9.19.6	
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AP75 less cart.	£19.0.0	Teak Plinth with perspex cover £7.10.0 Carr. 7/6 ex.
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SL95 less cart. £38.10.0.		Carriage 10/- extra.

GOLDRING RECORD UNITS

GL68 less cart. £22.7.0.	GL75 less cart. £35.15.5.
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Carriage 10/- extra.

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Post and Packing 1/6 each.		
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B.S.R. X3M (Mono compatible)		£1.18.5
B.S.R. X3H (Mono compatible)		£1.18.5
RONETTE 105 (Stereo)		£1.15.0
RONETTE 106 (Stereo)		£1.15.0
All complete with mounting brackets and instructions.		
Post and Packing 1/6 each.		

"PREMIER" TAPE CASSETTES



C60 (60 min.)	10/6
C90 (90 min.)	15/-
C120 (120 min.)	20/-

P. & P. 1/-.

CASSETTE HEAD CLEANER



Removes unwanted deposits from delicate tape heads. Fits all cassette recorders.
P. & P. 1/-.

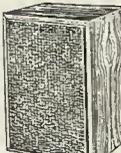


HI-FI STEREO HEADPHONES
Designed to the highest possible at standard. Fitted 2 1/2" speaker units with soft padded ear muffs. Adjustable headband. 8 ohm impedance. Complete with left, lead and stereo jack plug.
P. & P. 5/6.

MONO HEADPHONES 2000 ohm 14/6 P. & P. 2/6.
STEREO STETHOSCOPE SET Low Imp. 25/- P. & P. 2/-.
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Specially designed oiled teak cabinet with vynair front. Size 12 1/2" high 7 1/2" wide, 6 1/2" deep. Fitted 6 1/2" EMI 8 ohm Bass speaker with rolled surround and matching 3" EMI tweeter. Fully lagged.
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POCKET SIZE MODEL. With wide-angle, jewelled meter movement, ceramic long-life, low-loss switching, tough impact resisting case. Sensitivity 20,000 ohms/volt D.C. 10,000 ohms/volt A.C.
19 Ranges: 0.5-25-50-250-500-2500 volts DC. 0-10-50-100-500-1000 volts A.C. 0-50 uA-2.5 mA-250 mA D.C. 0-6000 ohms-6 megohms, 10u uf-0.001 mfd-1 mfd. -20 to +22dB. Complete battery, test lead and instructions.
£4.19.6 P. & P. 3/6.

WELLER SOLDERING TOOLS



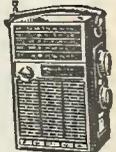
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PREMIER 33 GNS.
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FOUR STATION INTERCOM. Master unit and 3 slaves. Ideal for office and home. Complete with battery and connecting wire £7.19.6 P. & P. 5/6.

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TAPE SPOOLS 3" 1/-, 5", 5 1/2", 7" 1/8. TAPE CASES 5" 5 1/2", 7" 2/6.



Post and Packing 3" 1/-, 5", 5 1/2" 1/6, 7" 2/- (3 reels and over Post Free.)

sinclair

Z.12 - for all you want from any amplifier

The Z.12 is a most versatile integrated amplifier and pre-amp in which power, compactness and true high-fidelity standards are combined within a unit of very modest price. The most widely used unit of its kind in the world, the Z.12 has an output of 12W R.M.S. continuous sine wave (24W peak) or 15W music power (30W speak). It has Class B ultralinear output which can be fed into any loudspeakers from 3 to 15 ohms. (Two 3 ohm speakers can be used in parallel.) Frequency response—15 to 50,000Hz \pm 1dB; input sensitivity—2mV into 2 K Ω ohms. The Z.12 will operate from any power source between 6 and 20V d.c. As such,

a car battery or the PZ.4 are eminently suitable, giving much wider than usual scope in the applications to which the Z.12 may be put. As well as hi-fi, these include systems for P.A., electronic guitars, organs, intercom systems, laboratory, education or industry. You will find the Z.12 in use in such instances again and again. The Sinclair Z.12 is supplied ready built, tested and guaranteed, complete with manual of circuits and instructions for matching it to your precise requirements. Two may be used in stereo when, with the Stereo 25 and PZ.4 together with two Q.14s, you will have an ideal high fidelity assembly.

89/6

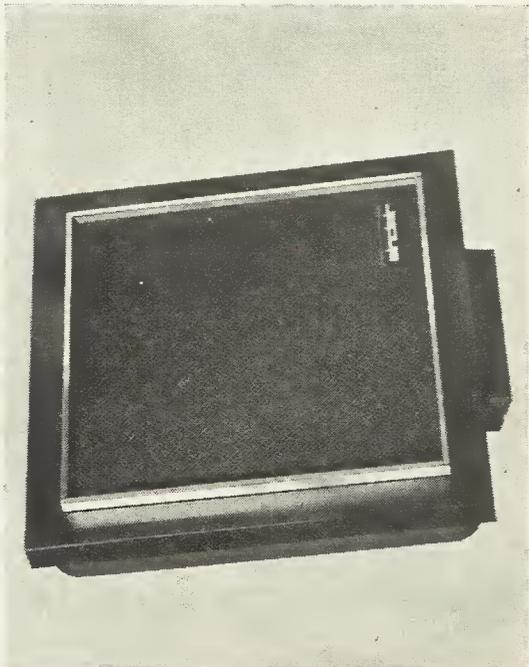
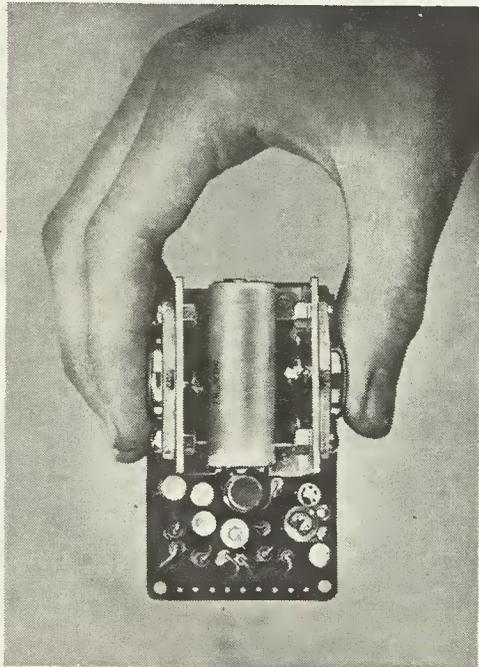
Q.14 - the unique loudspeaker

New materials and original design techniques have been used to produce speaker of fantastic quality at a most attractive price. Experts and reviewers have enthusiastically endorsed its performance. The shape and size of the Q.14 make it far more adaptable to its environment than is the case with conventionally styled speakers so that it is much easier to position this speaker in the room in which it is to be heard. The Sinclair Q.14 has a substantially flat frequency

response from 60 to 16,000Hz and outstandingly good transient response. It will comfortably handle up to 14W loading and is positively brilliant in stereo. Measuring 9 $\frac{1}{2}$ in square by 4 $\frac{1}{2}$ in deep, this loudspeaker is finished in matt black with solid aluminium bar trim. Try the Q.14 in your own home without delay. If you are not delighted with it, your money including cost of return postage to Sinclair will be refunded immediately.

£7.19.6

+ 2/11 P/T Surcharge



Stereo 25 de-luxe pre-amp/control unit

instructions manual provided gives matching details for pick-ups, shows how to connect up, etc. The front panel of the Stereo 25 is finished in brushed and polished aluminium embellished in black. The control knobs are in solid aluminium to match. Size 6½ x 2½ x 2½ in plus knobs. Supplied built, tested and guaranteed.

This is a very elegantly styled unit, which, although designed basically for use with the Z.12, is readily adaptable for use with any high quality power amplifier system. The switched input selector allows for Pick-up, Radio and Auxiliary and there are controls for bass cut and lift, treble cut and lift, volume and stereo balance. P.U. input is equalised to R.I.A.A. curve from 50 to 20,000Hz ±1dB and the

£9.19.6

PZ.4 - stabilised power supply unit

Designed specially to meet the power requirements for an assembly of two Z.12s and the Stereo 25, this heavy duty transistorized power supply unit has stabilised output of 18V d.c. at up to 1.5A. It is for a.c. mains operation 200/250V.

Supplied built, tested and guaranteed.

99/6

SINCLAIR MICROMATIC

Whether you buy your Micromatic in kit form or built ready for use, you must not deny yourself the thrill of owning this fantastically small British receiver. Smaller than a matchbox, it has power, range and selectivity that must be experienced to be believed. The high quality magnetic earpiece supplied with the set ensures excellent reproduction indoors and out. The Micromatic tunes over the medium waveband and has A.G.C. to counteract fading from distant stations. Bandpass tuning makes reception of Radio 1 easier; in fact you will find this set performing in some cases where other sets cannot be heard at all. The Micromatic is housed in a neat black case given an elegantly modern appearance by the attractive aluminium front panel and matching tuning control.

YOUR SINCLAIR GUARANTEE

Should you not be completely satisfied with your purchase when you receive it from us, your money will be refunded in full at once and without question.

FULL SERVICE FACILITIES AVAILABLE TO ALL PURCHASERS.

Goods sent post free in United Kingdom by surface mail. Air mail extra at cost.

Kit in fitted pack with magnetic earpiece, instructions and free solder

49/6 +11/6 P.T. Surcharge

Built, tested and guaranteed, inc. magnetic earpiece

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Mallory Mercury Cell type RM.675 (2 required) 2/9 each

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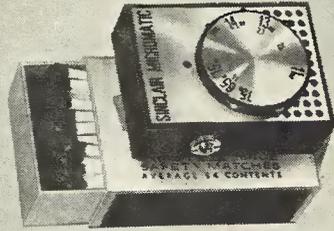
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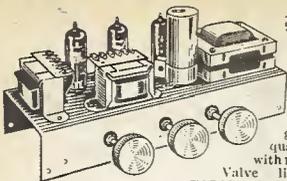
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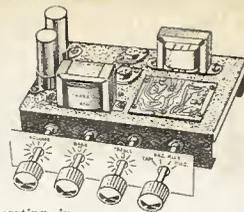
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Performance figures:
Sensitivity—PU1—50mV, 50K input impedance.
PU2—110mV, 1 meg input impedance.
Tape—110mV, 1 meg input impedance.
Radio—110mV, 1 meg input impedance.

Output power measured at 1Kc—6.2 watts RMS into 3 ohms, 5.8 watts RMS into 15 ohm. Overall frequency response 30c/s-18Kc/s: Continuously variable tone controls; Bass, +8db to -12db at 100c/s. Treble, +10db to -10db at 10Kc/s.

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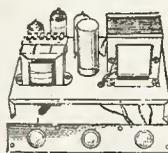
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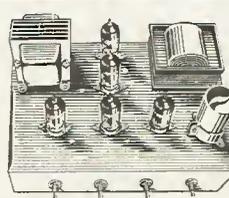
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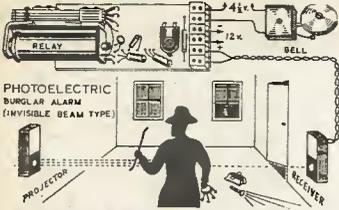
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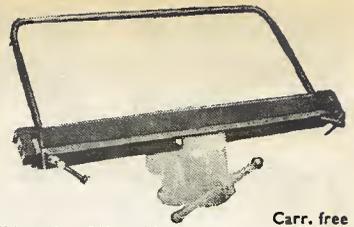
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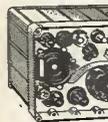
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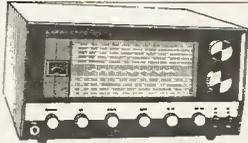
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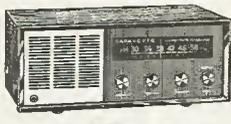
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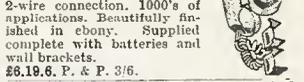
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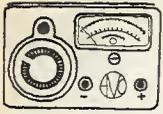
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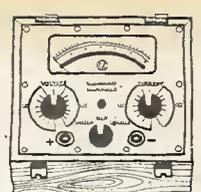
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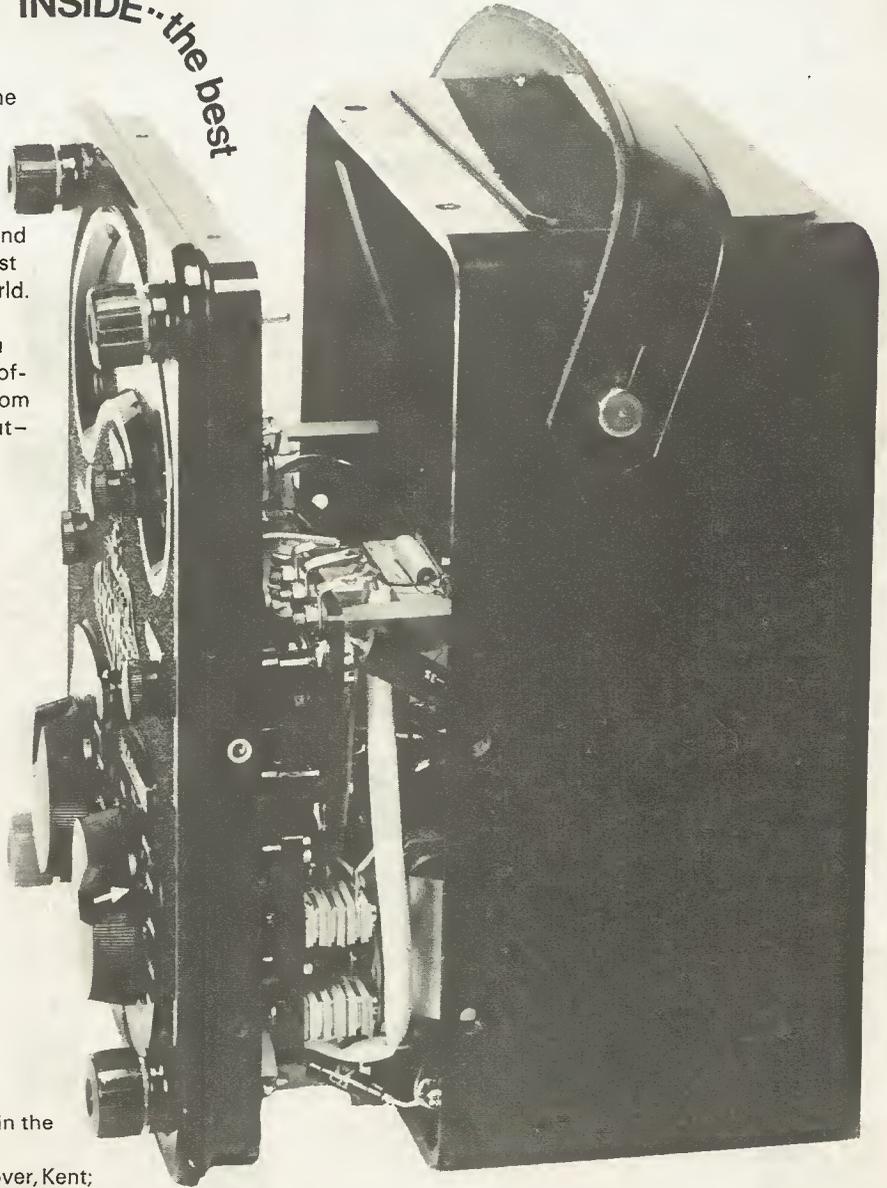


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A PLACE IN THE QUEUE

A TANTALISING profusion of new type semiconductors and other kind of circuit devices flow steadily from the component manufacturers. Tantalising, that is, to the amateur who reads accounts of these products and their capabilities, and likely effects upon future developments in electronic circuit design, but realises they are not likely to come his way for a long while, if indeed at all.

The recipients of these new products are of course the electronic equipment makers. The more exciting and trend-setting components usually are initially earmarked for the requirements of the armed forces (who, more often than not, have financed the original R and D work); then come the industrial users, and finally the mass consumer product market.

How does the amateur fare in this progressive dissemination of the latest advances in component technology? He has no officially recognised place in the queue, that much is obvious. But on the other hand a limited range of these devices do eventually find their way onto the retail market as branded items, often primarily intended as service replacements for the trade. An even wider variety of devices make their due appearance as unmarked "surplus" components. The manner of their distribution is somewhat devious, the name of the maker frequently not known and type number obscure. Availability of these supplies is fortuitous and dependent upon the caprices of mass production methods and professional user demand. Still to the amateur they are valuable, if not essential; and they are generally remarkably cheap.

Unfortunately, however, this has led to the amateur being stigmatised in some quarters as just a user of surplus components, with the inference that sub-standard or, at least, untested parts are good enough for him always—and for all purposes. This is unfair as a generalisation, and is demonstrably entirely untrue in very many cases. This kind of misrepresentation has harmed the image of the private enthusiast, and perhaps its most serious effect has been the obscuring of genuine contributions made by individuals towards extending the general usefulness of electronics for the ordinary person in every day life. Ideas of amateur origin have been adopted commercially on more than a few occasions, it is well to remember.

The component manufacturers could well ponder this and consider whether a wider range of their products could not be made available—via distributors—to the amateur fraternity. It must be in their interest to help sustain a body of individuals who are in tune with developing technology, although so often barred from useful active experimental work because of non-availability of vital parts.

F. E. Bennett—Editor

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*Our August issue will be published on
Monday, July 14*

OPTICAL REMOTE CONTROLLER

BY D. BOLLEN

A PERSON watching television, who is comfortably planted in a soft armchair, may be temporarily subjected to a sudden blast of energetic music. A possible cure for such a condition is to climb out of the armchair and adjust the television volume control, whereupon he might find himself straining forward to catch the whispered words of a particularly interesting but softly spoken personality.

Another case occurs where the discriminating viewer requires his picture to be as crisp as a good photograph, with correct contrast settings. As most television sets have inadequate black-level correction, a picture adjusted for a bright daylight scene will consist of pure white patches on a featureless black background when the shot changes to a night scene.

Clearly, some form of remote control is called for, which allows fine and continuous adjustment of a control within the set, without the inconvenience of a bulky screened cable draped across the room.

The optical remote controller described here uses a beam of modulated light, in place of interconnecting wires, to achieve a continuously variable and almost linear adjustment of a potentiometer setting in a remote receiver or instrument, situated at distances of up to 30ft away.

Although there are many possible applications for such a control, when it is used with a television set, the sound level can be increased, diminished, or turned off altogether, merely by rotating the knob on the transmitter or operating a switch.

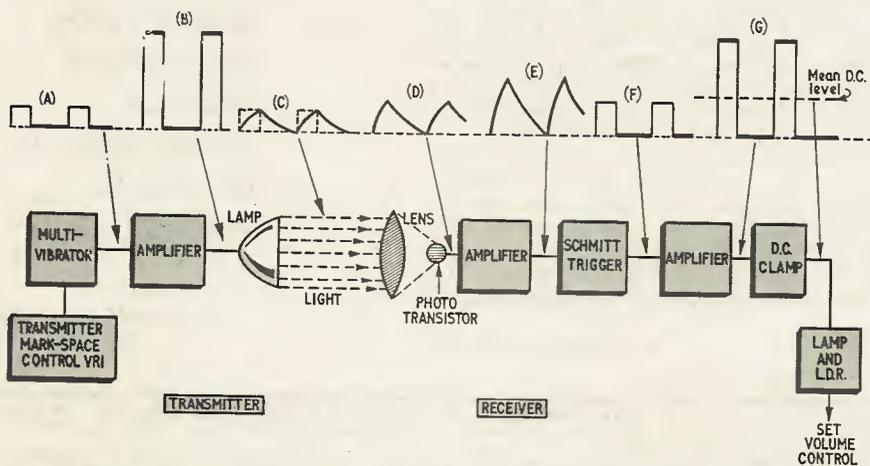


Fig. 1. Block diagram of the optical remote controller with transmission waveforms

Strong background lighting, whether from sunlight or from high powered mains bulbs, does not affect the operation of the controller.

HOW IT WORKS

The block diagram in Fig. 1 illustrates the sequence of operations. A square wave (A) is obtained from an astable multivibrator, which has a repetition frequency of about 25Hz, and a variable on-off or mark/space ratio controlled by potentiometer VR1.

The transmitter amplifier increases the amplitude of the waveform (B) to a level sufficient to drive a low consumption torch bulb. The bulb is mounted in a suitable reflector to throw a beam of light towards the receiver. Tungsten filament bulbs possess considerable thermal inertia, apparent even at 25Hz, and the original steep-sided square wave is degraded into the form of an exponential sawtooth.

Although the modulated light waveform (C) differs from the command signal, it still carries the necessary information. When shown on an oscilloscope, the relative positions of the peak and trough of the sawtooth will shift in sympathy with the on-off ratio of the square wave input signal, demonstrated by the diagram in Fig. 2.

Passing to the receiver (Fig. 1), a lens is used to focus light from the distant transmitter on to the sensitive area of a phototransistor. Signal (D) appears at the collector of the phototransistor and is amplified (E) to give reliable switching of a sensitive Schmitt trigger circuit.

The Schmitt performs the useful function of converting the sawtooth back to a square wave (F) closely resembling the multivibrator output in the transmitter. Once again, the signal is amplified to drive a torch bulb (G), but this time rectification and smoothing takes place so that the signal is converted to d.c.

Thus, the brightness of the receiver bulb will correspond to the mean d.c. level of (G), determined by the VR1 setting in the transmitter, and is virtually unaffected by distance of receiver from transmitter.

Finally, a light dependent resistor is arranged to pick up light from the receiver bulb and translate this to a resistance value. The l.d.r. forms one arm of a potentiometer so that the position of the sliding contact on VR1 in the transmitter is reproduced by the l.d.r. at the receiver output.

TRANSMITTER CIRCUIT

The transmitter circuit is given in Fig. 3. TR1 and TR2 form an astable multivibrator, with on-off timing set by C1, C2, and base bias resistors R2 and R3 in conjunction with VR1. Potentiometer VR1 serves to alter the base resistance in an equal and opposite manner and thus determines the on-off ratio of the multivibrator square wave output, without affecting repetition frequency.

The signal is then passed via limiting resistor R5 and capacitor C3 to the Darlington pair TR3, TR4. The transmitter bulb forms the collector load of TR4. DI helps to ensure a clean switching waveform at all input levels.

As the supply voltage is only 6V, and the bulb load resistance increases with current flow, additional protection against thermal runaway is not required.

When operating, the light output from the transmitter bulb will increase or diminish, depending on the setting of VR1, but the output signal does not change very much.

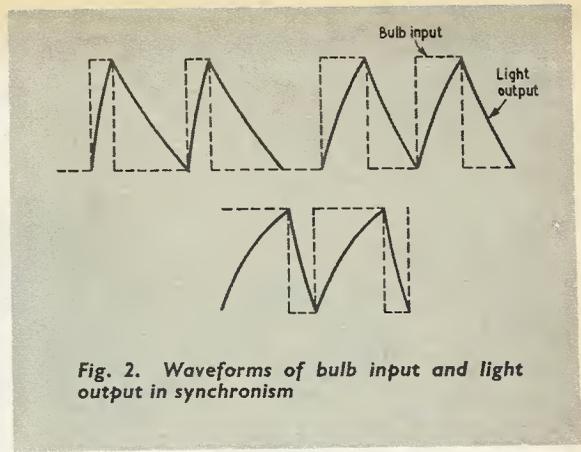
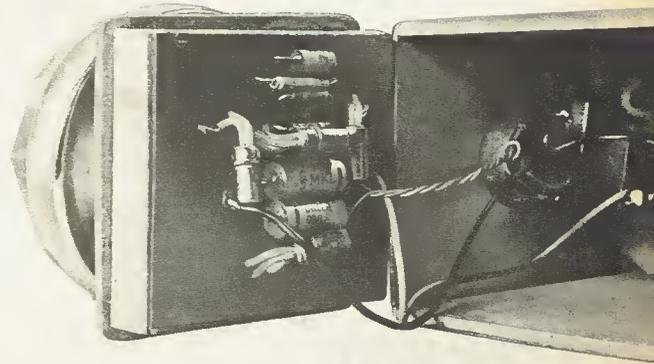


Fig. 2. Waveforms of bulb input and light output in synchronism



The transmitter case opened

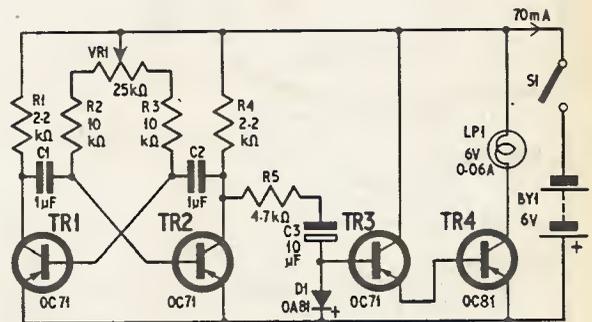


Fig. 3. Circuit diagram of the transmitter

It is important to distinguish between visible mean light level and the actual swing or change in output per cycle. The former is akin to a steady d.c. state and the latter may be likened to a.c.

The human eye is a poor instrument for measuring modulated light. However, as the working frequency is only 25Hz, there will be a noticeable flicker, but as only a dim light is radiated the effect will not be distracting.

With the battery specified, over 100 hours operation at the rate of four hours per day will be achieved. As an alternative, a small 6V motorcycle accumulator could be used.

TRANSMITTER CONSTRUCTION

The transmitter box is made up as shown in Fig. 4, from $\frac{1}{2}$ in plywood, with all joints epoxy resin glued. The rear cover can be provided with fabric or metal hinges and a fastener, to allow quick access for battery replacement. VR1 and S1 are mounted on the top face of the box; S1 is positioned as an end stop to prevent the battery sliding forward when the transmitter box is tipped.

The front cover, combining circuit panel and reflector unit, is made a tight push fit in the end of the transmitter box by means of a wooden flange constructed of $\frac{1}{2}$ in strips of thin plywood, this also acting as a mount for the circuit panel.

Reflector details are given in Fig. 5. A $2\frac{1}{2}$ in reflector assembly can be cut from the body of an inexpensive or old torch; the neck of the reflector housing is also cut, to make bend-over tabs.

The original reflector had a pre-focus bulb holder; packing was introduced to reduce the diameter of the holder so that m.e.s. bulb could be fitted. The bulb was held secure by the plastic threaded ring provided with the torch. If the reflector tends to revolve in its hole in the front cover, a dab of glue under the tabs will make it firm.

TRANSMITTER CIRCUIT PANEL

As there are no crossovers, the underside wiring diagram in Fig. 6 can be traced if an etched circuit panel is required. Alternatively, the transmitter circuit panel may be drilled and wired underneath with short lengths of single strand tinned copper wire. Also in Fig. 6 is the component layout diagram, including colour coded wiring from panel to S1, VR1, and LP1.

When the panel is completed, it should be tested, by connecting to LP1, VR1, S1, and to a 6V battery with a milliammeter temporarily in the negative lead. Current consumption will be found to vary as VR1 is rotated, but should not exceed 70mA.

The flicker rate, best observed out of the corner of one eye, should remain constant at all settings of VR1, irrespective of bulb brightness. The position of the bulb in the reflector is adjusted to throw an even patch of light, approximately 9in diameter, at a distance of roughly 9 feet.

RECEIVER CIRCUIT

A phototransistor is used in the receiver circuit of Fig. 7, to pick up the modulated light signal from the transmitter, but there is scope for experiment with other light sensitive devices. An l.d.r., such as the ORP60, can be wired in place of TR1 without further modification.

Although results will be inferior, both with regards to effective range and change of receiver output resistance, due to the lower sensitivity and slower time response of the ORP60, these disadvantages can be set against the higher cost of an OCP71.

A silicon photodiode was also tried, this time feeding straight into C2 with R1 omitted from the circuit. This gave a good time response but range was still poor. All the devices mentioned have a spectral response extending into the infra-red region and are a suitable match to a filament bulb.

Considering the circuit in Fig. 7, and bearing in mind the earlier diagram (Fig. 1) with its waveform sequence, TR2 amplifies the sawtooth signal from the collector of TR1, and passes it, via C3, to the input of Schmitt trigger TR3 and TR4. VR1 presets the Schmitt trigger level, and R4 might need some individual adjustment to bring the trigger level within the range covered by VR1.

The Schmitt itself is a sensitive version, responding to an r.m.s. input of less than 75 millivolts. Zener diode D1 is included to ensure stable operation over long periods, where fluctuations of supply voltage might interfere with VR1 trigger level setting.

With VR1 set to just bias TR3 off, TR4 is hard on, thus holding down the base of TR5 so that the bulb just glows dimly or not at all. VR2 adjusts the working point of TR6 and the current flowing through the bulb under static conditions.

On receipt of a signal, the Schmitt commences to switch, and feeds negative going pulses to the base of TR5, tending to switch TR5 on, depending on the on-off ratio of the command signal. Hence, the bulb will tend to glow more brightly while C4 acts to smooth signal pulsations, to prevent them being passed on to the l.d.r.

It will be seen that TR5 not only amplifies but also rectifies, and the bulb, coupled only by light to the l.d.r., provides a smooth, analogue function with no unwanted interaction. The l.d.r. resistance is wholly dependent on bulb brightness which, in turn, is determined by the signal from the transmitter.

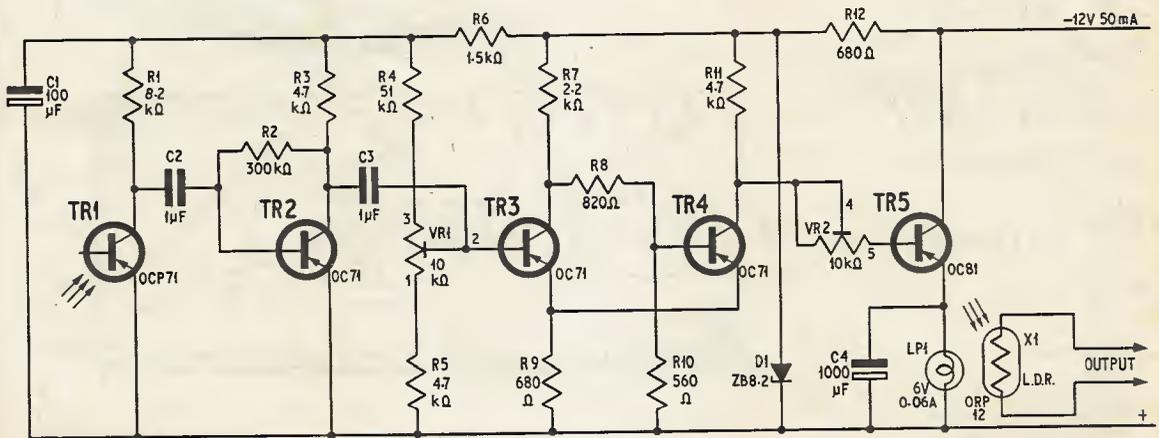


Fig. 7. Circuit diagram of the receiver

RECEIVER

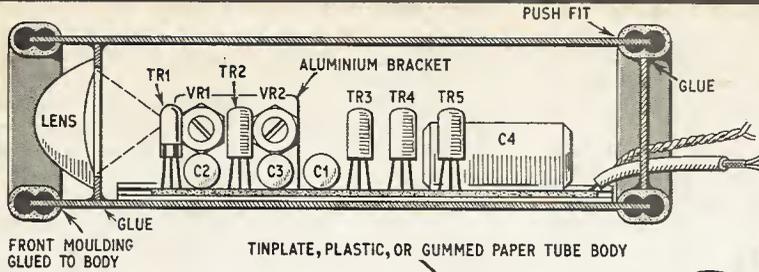


Fig. 8. Component panel mounted inside the receiver case

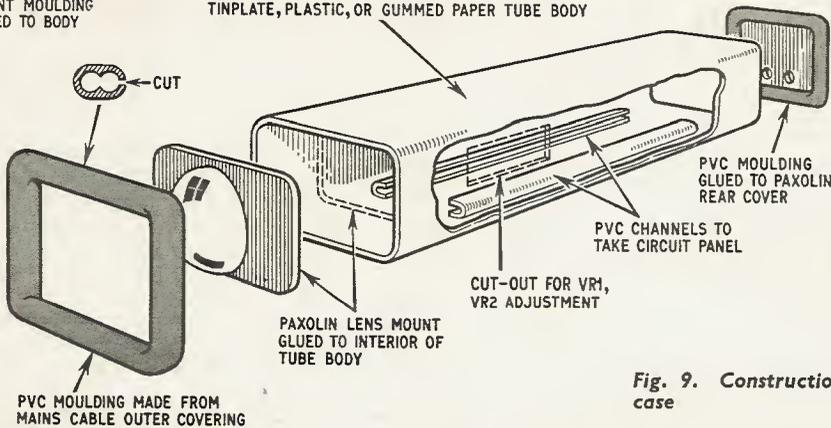


Fig. 9. Construction of the receiver case

COMPONENTS . . . RECEIVER

Resistors

R1 8.2k Ω	R7 2.2k Ω
R2 300k Ω	R8 820 Ω
R3 4.7k Ω	R9 680 Ω
R4 51k Ω	R10 560 Ω
R5 4.7k Ω	R11 4.7k Ω
R6 1.5k Ω	R12 680 Ω
All $\pm 10\%$, $\frac{1}{2}$ W carbon	

Potentiometers

VR1 10k Ω linear miniature carbon
VR2 10k Ω linear miniature carbon

Capacitors

C1 100 μ F elect. 15V
C2 1 μ F polyester 60V
C3 1 μ F polyester 60V
C4 1,000 μ F elect. 12V

Transistors

TR1 OCP71 (phototransistor)
TR2, TR3, TR4 OC71 (3 off)
TR5 OC81 or NKT271

Light Dependent Resistor

X1 ORP12

Diode

DI ZB 8.2 (8.2V) Zener diode

Lamp

LPI 6V 0.06A m.e.s.

Miscellaneous

Lens
S.R.B.P. panel
Twin screened cable
Mains cable covering

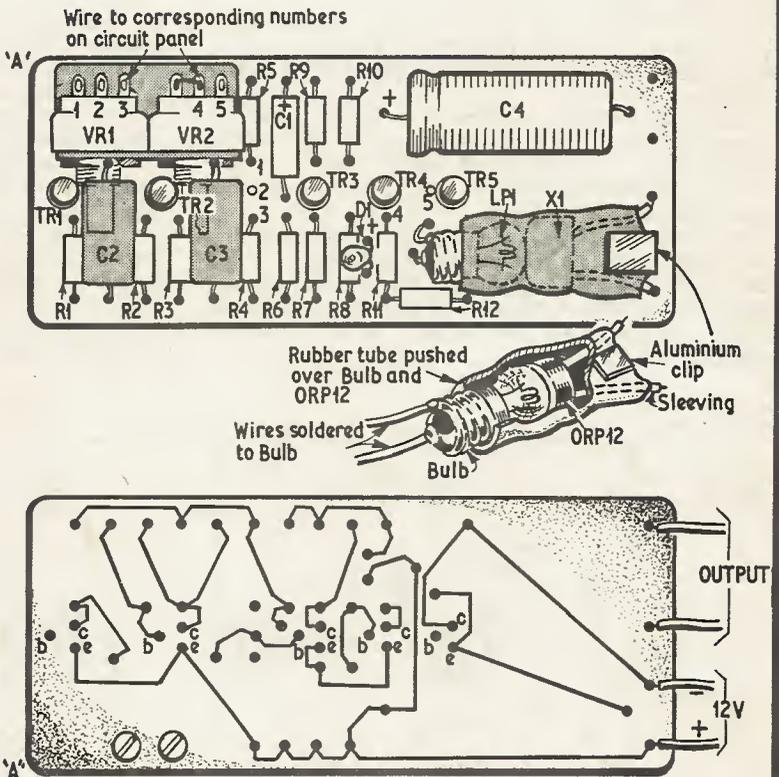
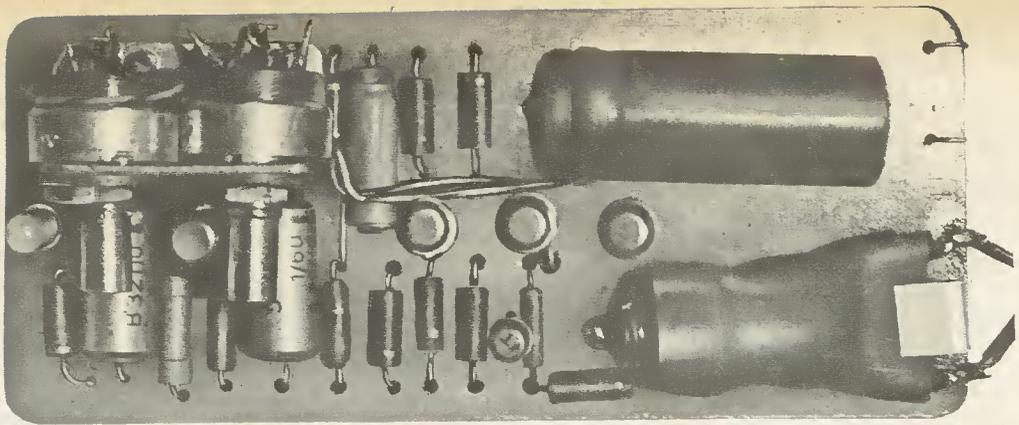


Fig. 10. Component layout and wiring of the receiver



The completed receiver panel

RECEIVER CONSTRUCTION

It is assumed that the receiver will take its supply from the equipment it controls, the requirement being a nominal 12 volts at about 50mA. Without a power pack, a compact form of construction can be used, and the receiver will be small and inconspicuous.

Fig. 8 gives a cross-section view of the receiver, while Fig. 9 shows the receiver case constructional details. The receiver panel slides along two runners made of p.v.c. taken from a short length of 5A house wiring cable; this ensures positive location and ease of focusing.

The lens is a "bull's eye lantern" type, with a short focal length. If other types are available, their focal length can be checked by focusing the image of a window upon a wall and noting the distance of the lens from the wall.

Obviously, the purpose of the lens is to focus a sharp image of the distant light source upon the sensitive area of the phototransistor. This is similar in effect to the use of a highly directional aerial in a radio receiver, increasing gain and reducing off-axis interference. For short ranges (not more than 9ft) the lens can be dispensed with, but the phototransistor must be hooded against stray light from mains bulbs.

The receiver tube body can be fashioned in several ways, the simplest being from stout gummed paper covered with self-adhesive plastic, but metal or some form of plastic moulding will obviously be much more durable. A circular hole is cut in the lens mount slightly smaller than the lens itself, the lens and mount being glued inside the tube body as shown.

P.V.C. cable covering is again used for the trim at the front of receiver box; this is glued in place. The rear cover is not glued to the tube body but is made a push fit, to facilitate easy removal and positioning of the circuit panel. Two holes are drilled in the paxolin part of the rear cover to take screened output cable and twisted supply leads.

RECEIVER CIRCUIT PANEL

The receiver panel construction follows the same lines as the transmitter panel, being either etched copper or wired underneath (Fig. 10). VR1 and VR2 preset potentiometers can be mounted, as shown, on a small aluminium bracket.

The lamp and I.D.R. assembly requires some explanation. A short length of thin rubber tubing, sometimes found on old capacitors, is pushed over the bulb to

exclude ambient light. After insulated sleeving is put on the I.D.R. leads, the I.D.R. is pushed into the other end of the rubber tube to make contact with the bulb.

A small clip, made from a piece of scrap aluminium, clamps the rubber tube around the I.D.R. leads and makes a lightproof seal. The clip is squeezed in place with a pair of pliers. Tinned copper wires are soldered to the body and centre contact of the bulb and are pushed through the circuit panel to hold the bulb-I.D.R. unit in place. The I.D.R. leads are terminated in a similar manner. As the bulb is very much underrated it is unlikely that it will ever need replacing until the glass becomes black with age.

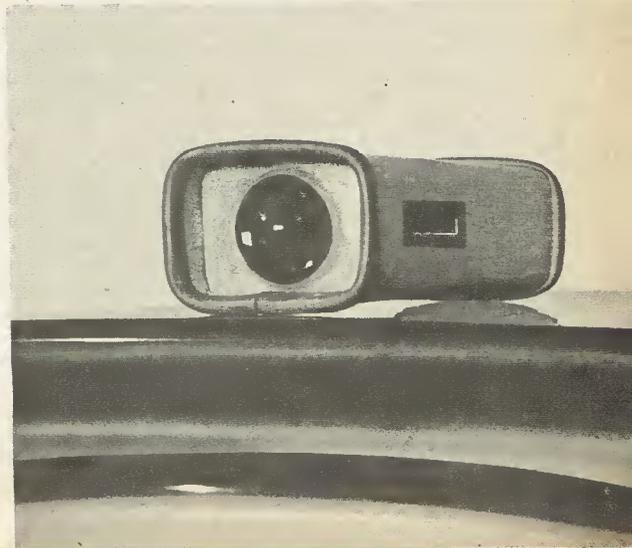
TESTS AND ALIGNMENT

When completed, the receiver panel can be tested in daylight, with a precautionary milliammeter connected in the negative supply lead. It is convenient to use a 12V battery for initial testing.

Connect an ohmmeter to the I.D.R. output terminals, and set VR2 near minimum resistance. Try the effect of rotating VR1; a position should be found where the circuit panel current consumption suddenly jumps up, and the ohmmeter pointer swings to indicate a low value of resistance.

Reset VR1 to just below this trigger point and VR2 so that the ohmmeter reads about 1 megohm. If it is

The receiver mounted on a television set



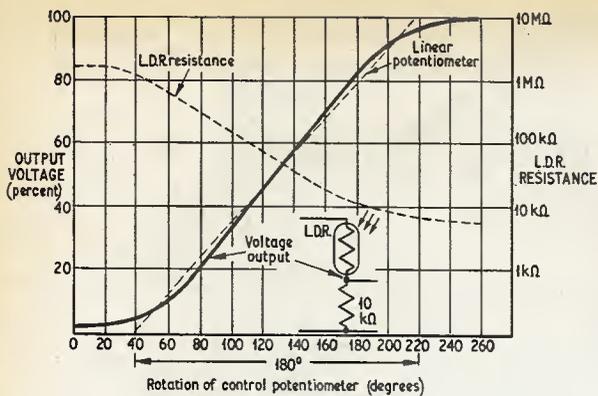


Fig. 11. Graph showing output controlled resistance for angular rotation of the transmitter control

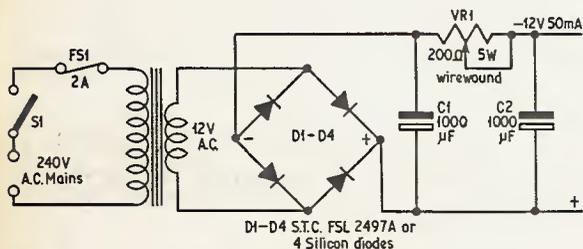


Fig. 12. Suitable power supply for controller receiver

found that nothing happens when VR1 is trimmed, adjust the value of R4.

Next, switch on the transmitter and point its beam at the phototransistor. The ohmmeter should show a resistance decrease. Rotate the transmitter control and observe the ohmmeter readings. Look for a smooth response and a minimum resistance of around 10 kilohms at the extreme setting of the transmitter control.

If all is well it will be found possible to set the receiver output for any value between, say, 10 kilohms and 100 kilohms from the transmitter.

At very short ranges the phototransistor may become saturated with light from the transmitter, especially when a lens is fitted, and this will diminish the coverage of output resistance swing. Depending on the required application and working range, VR1 and VR2 settings will determine the output characteristic.

As a guide, VR2 in the minimum resistance position will yield low values of output resistance to suit the low input impedance of transistor circuits. The high resistance position will give values suited to valve circuits, up to several megohms. VR1, once correctly adjusted, should not need readjustment, but this control is mainly responsible for high sensitivity with long range working.

OUTPUT CHARACTERISTIC

The graph in Fig. 11 gives a typical receiver output response. The dashed line shows the change of l.d.r. resistance plotted against angular rotation of the

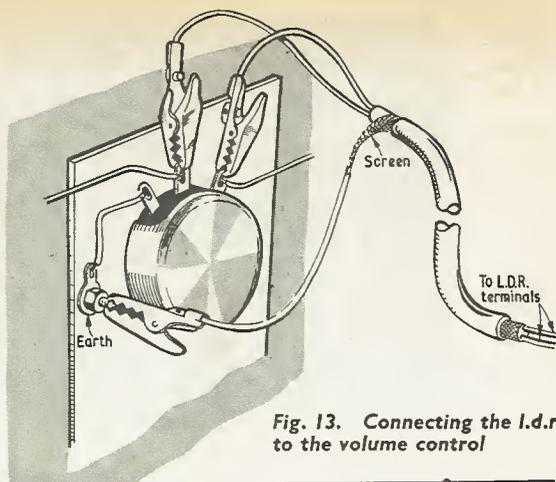


Fig. 13. Connecting the l.d.r. to the volume control

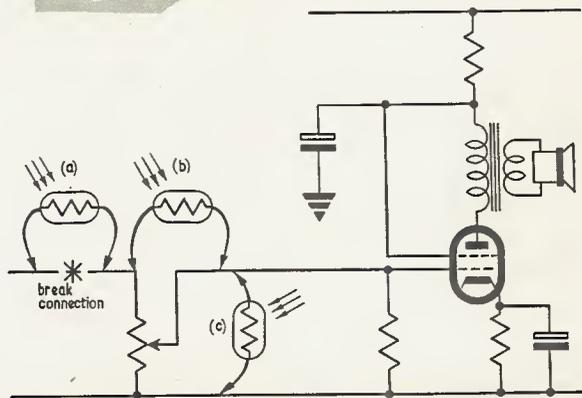


Fig. 14. Connections to volume control

transmitter control, and is seen to range from about 2 megohms to 8 kilohms. The solid line indicates the departure from true linearity with the l.d.r. connected in series with a 10 kilohm fixed resistor, as a potentiometer.

Although there is some flattening at both ends of the curve, the mid-position of rotation of the transmitter control yields a straight line very close to the ideal.

The lowest attainable l.d.r. output resistance will be slightly less than 1 kilohm, and the maximum resistance above 20 megohms, a range sufficiently large to control almost any apparatus function.

POWER SUPPLY

As the controller receiver has to draw its supply from the equipment it controls, arrangements must be made to secure a source of smoothed d.c. when operating mains powered equipment; a suitable circuit is shown in Fig. 12.

The method of obtaining low voltage a.c., prior to rectification and smoothing, will depend on the nature of the controlled equipment. Tappings can be taken from valve heater chains, and heater transformers, but if any doubt exists it is better to use a small 12V a.c. transformer, and rectifier, which can be fitted to a panel, along with the other components shown in Fig. 12. This power pack can be installed in a vacant corner of the controlled equipment.

The 200 ohm variable resistor serves the double purpose of smoothing resistor and output voltage adjuster.

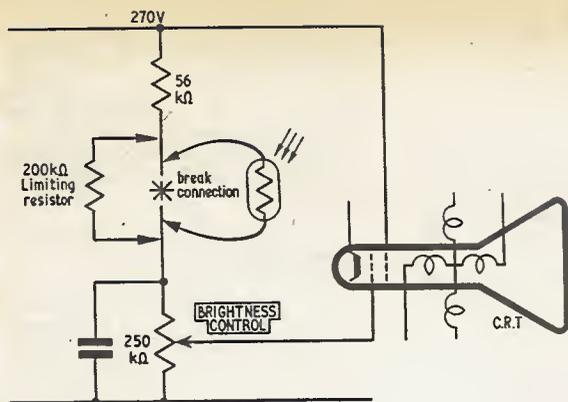


Fig. 15. Preferred connection to brightness control. SWITCH OFF MAINS SUPPLY WHILE CONNECTING AND BEWARE OF CHARGED CAPACITORS

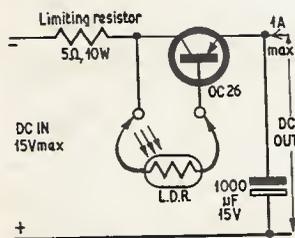


Fig. 16a. Remote controlled power supply

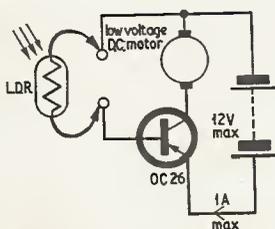


Fig. 16b. Remote motor speed control

SOME APPLICATIONS

Taking first the example of remote control of television or radio sound, crocodile clips can be fitted to the receiver I.d.r. screened lead, to facilitate a temporary connection to the television volume control (Fig. 13). This avoids making any permanent alterations to the television or radio set. The clips can be quickly removed at any time, but make sure there is no risk of accidentally shorting.

When the intention is to install the controller as a permanent fixture, soldered joints are obviously to be preferred. Three different ways of connecting the I.d.r. to a typical audio output stage are shown in Fig. 14.

With the I.d.r. at point (a), in series with the input wire to the volume control, the signal may be fully attenuated. In position (b) the I.d.r. allows almost full control of volume, from a whisper to nearly maximum sound output, if the potentiometer in the set is initially set so that its slider is near the earthed end of the track.

The arrangement (c) works in reverse, that is, when the transmitter control is rotated towards the maximum position, the sound level will decrease.

The advantage with (b) and (c) connections is that the volume control can be used normally when the controller is inoperative, without disconnecting or shorting across the controller receiver output.

Fig. 15 gives a representative television brightness circuit; the important point to watch here is that the maximum dissipation of the I.d.r. is not exceeded. In

the case of the ORP12, absolute maximum ratings of 110V peak and 200mW are laid down by the manufacturer. About the only possible place for the I.d.r., therefore, is in series with the "live" lead to the brightness potentiometer, with a 200 kilohm limiting resistor placed in parallel with the I.d.r. (Fig. 15).

Preliminary checks should be made to see that the h.t. rail voltage is not more than, say, 290V, and the current to the brightness control does not exceed about 1mA. Since the ORP12 is commonly used where a television set already has an automatic brightness control, the manufacturer's circuits could be obtained as a guide to necessary modifications.

If automatic brightness is present in the receiver, it is a simple matter to connect the controller I.d.r. output leads in place of the existing I.d.r. terminals within the set. Remote volume control in transistor equipment would follow similar lines as with valve equipment.

The relatively low dissipation of the controller receiver output can be enhanced by using the I.d.r. to bias a power transistor. Two circuits are given in Fig. 16.

In the first case (Fig. 16a) an OC26 in series with a 15V maximum d.c. supply will permit remote control of output from 0 to 15V and 0 to 1A, depending on the load. Such a supply could form the basis of control of a wide range of devices or equipment.

In Fig. 16b an OC26 is again used for electric motor speed control and might be suitable for models, tape drives, and servo applications. With both circuits, the controller receiver can draw its supply from the common d.c. source, if this is 12V.

Proportional opto-electronic control of a servo, where the servo output shaft faithfully follows movement of the transmitter potentiometer spindle, is quite feasible, but such circuits are necessarily more complicated and are beyond the scope of this article.

FINAL SETTING-UP

If the controller receiver has a "bull's eye" lens, transmitter to receiver optical alignment can be observed visually, because the lens will act as a "cat's eye" reflector. Alignment is generally not critical, except at extreme range limits. It is sufficient, in most cases, for some light from the transmitter to fall on the phototransistor.

It is surprising, when working with modulated light, what small intensities are required for efficient operation. The procedure to adopt with final setting-up is as follows:

Align transmitter and receiver, set transmitter control to mid-way position and adjust VR2 in the controller receiver to obtain desired average sound volume. If VR1 in the receiver has been trimmed correctly, it should be possible to adjust the sound level from the transmitter.

Depending on how the I.d.r. is connected, the sound level may not quite drop to zero when the transmitter control is rotated to minimum, but it should be found that turning off the transmitter switch will cause a sharp reduction of the remaining sound.

If desired, the transmitter box can be mounted on a heavy base, by means of a locking ball-joint (such as is used with a camera tripod) to allow convenient optical alignment of the transmitter beam. Normally, though, a small table of suitable height will serve, or else the transmitter box can be clipped or fixed to the arm of a chair. Much will depend on the intended application and room layouts. ★

APOLLO II

Now that the final stage of the first *Apollo* programme reaches its climax with astronauts Neil Armstrong, Michael Collins and Edwin Adrian making ready for man's first landing on the Moon, a dream comes true. It is a far cry from Leonardo Da Vinci to the *Apollo's* lunar module and its complex back up systems.

The motivation for the ambition is still the same, to know more and more about man's environment. There will be many who have waited for this moment since schooldays as well as many who are still enjoying (or enduring) schooldays, when on July 16 the tall assembly from the *Saturn 5* rocket to the moon ship has its final moments of count-down. The work of its preparation on the site which began about the middle of April will again demonstrate the extent of technology's advancement.

SPACEWATCH

By Frank W. Hyde

It is planned that Armstrong and Aldrin the two astronauts chosen for the actual landing on the moon will spend about 22 hours performing their allotted tasks such as gathering moon-dust and samples of rock for analysis back on earth. In the meantime Collins will be circling the moon while waiting for the two "first men on the moon" to rejoin him for the journey back to earth. The first man in fact to set foot on the moon will be Armstrong and he will pass back to Aldrin, in the moon lander, a sackful of lunar dirt. This will make certain that even if the stay has to be cut short for any reason there will at least be a sample brought back.

There are indeed a number of problems involved, even in gathering samples, for the survival packs which the astronauts wear on their backs make them top heavy. Though the lunar gravity is but one sixth of that of the earth a fall could be dangerous. For this reason long tongs are to be used so that it will not be necessary for the astronauts to bend down. The setting up of the other equipment will require a hoist system for unloading as well as loading the mooncraft.

Among the experiments to be set up will be the solar wind probe, seismic unit, radioisotope thermal electric generator, superthermal ion detector, magnetometer and the central station for passing back to earth continuous information via the radio link set up. The unit is expected to continue to send back information for at least a year. Thus the time that the astronauts spend on the moon will be fully

occupied particularly if they are to attempt television pictures for transmission direct to earth.

The final touch down of the lunar module will come after the physical contact of the four foot long "cat's whiskers" (attached to the landing legs) with the surface of the moon which will result in the shutting off of the motor. The module will then drop under lunar gravity. The sequence of operation after separation from the command module is that the main motor between the landing legs is used to control the descent and is fired for brief periods to keep the craft on the correct course. This will bring the craft to within 500 feet of the surface of the moon and about 1,200 feet from the landing site. The speed at this point will be about 40 miles an hour forward and about 10 miles an hour downwards.

The crew will have two minutes or thereabouts to select the final landing site. The final control is then brought into operation by rockets at the four corners of the module to slow the descent to about 5 feet per second. After completing the tasks allotted the upper section of the lunar module will use its ascent engine to return to lunar orbit. This part of the mission will be computer controlled but the actual docking with the command unit will be manual. After transfer to the command module of men and materials the lunar module will be jettisoned and the three astronauts will begin the return journey to Earth. There are two "launch windows" for *Apollo 11* the first is July 15 to 22 and, if this is missed for any reason, another is available between August 13 and 21.

FUTURE MOON LANDINGS

There are to be nine future moon landings the final landing being sometime in 1972. They will be launched at the rate of two or three a year. The crew for *Apollo 12* have already been named and are all naval officers. Charles Conrad, Richard Gordon (these two are already veterans for they were both in Gemini crews) and Alan Bean, the third man for *Apollo 12* who is new to spaceflight missions. Conrad and Bean will land on the moon and spend about five hours there.

Though the actual landing site is not yet fixed it is not likely to be the same as *Apollo 11*. It is expected that a larger load of apparatus will be landed on the trip. Subsequent trips will take equipment to different points along the moon's equator and the lowlands and highlands will be explored.

NEW ORBITING OBSERVATORY

A *Nimbus* weather observatory has been launched which will enable more accurate weather predictions to be made up to two weeks in advance. The *Nimbus*, the most advanced weather craft so far built, is a butterfly shaped satellite which weighs 612 kilograms and is in an orbit which varies from 675 to 703 miles from earth. Its orbital time is 107.5 minutes. It is ten feet tall and is powered by solar panels and two new nuclear powered generators known as SNAP 19. These represent the first use of nuclear energy in space for civilian purposes.

In addition to the infra red sensors essential to weather forecasting *Nimbus* has very advanced television cameras which can take day or night pictures of cloud formations around the world. It will measure for the first time the atmosphere's temperature from ground to space, and also for the first time be able to interrogate other weather data gathering instruments such as ocean buoys, balloons, aeroplanes and ships and relay these data for processing.

Nimbus will take part in a large experiment by the U.S.A. known as BOMEX. Its object is to understand how the Sun features in the control of weather by the amount of water lifted from the oceans and distributed by wind currents round the world. An area of nearly 100 square miles east of Barbados will be explored by ten oceanographic ships, 24 aircraft, and dozens of balloons and buoys. The manpower will include some 1,500 scientists. The experiment is to last from May to July.

Included in the *Nimbus* tasks is one to track elk in Yellowstone Park. The animal carries a two-way radio round its neck.

Some of the "backroom boys" who have played an important part in making the *Apollo* lunar probe missions great successes



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A selection of readers' suggested circuits. It should be emphasised that these designs have not been proven by us. They will at any rate stimulate further thought. This is YOUR page and any idea published will be awarded payment according to its merit.

SIMPLE GUITAR TREBLE BOOSTER

AS SOME readers may know a basic treble boost unit consists of a preamplifier inserted between the guitar and amplifier which incorporates a high pass filter. This filter raises the response of the preamplifier to the harmonics of the guitar signal, producing a much higher pitched note.

Connecting the guitar straight through to the amplifier gives a rather flat sound lacking in the verve and impact sought by lead guitarists.

The primary windings of a valve output transformer are used as the filter in this design (the secondary winding not being used), see Fig. 1. The primary windings are connected across the input of the preamplifier. At low frequencies the impedance offered by the transformer is quite small and thus these notes are shorted to "earth" and not amplified. At high frequencies the impedance is large and the input signal is only slightly attenuated before amplification.

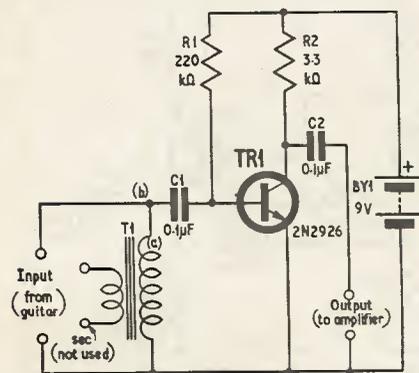


Fig. 1. Guitar treble booster circuit

The capacitor C1 serves as a d.c. blocking capacitor preventing the transformer windings shorting the base of the transistor TR1 to the negative supply line.

Any high gain *npn* silicon transistor may be used for TR1, suitable types being BC108, 2N1711, and 2N2926.

In the present design no control to regulate the amount of treble boost has been incorporated as this was thought unnecessary. If a control is required then a potentiometer, with a value of approximately 25kΩ, should be connected between point (a) and (b) in Fig. 1.

The preamplifier may be housed in its own case or built into the existing guitar amplifier. The type of battery used in the prototype was a PP3 type and should last for 100 hours depending on use.

S. J. Price,
Bristol.

VARIABLE WAA-WAA

I WOULD firstly like to recommend the excellent *Waa-Waa Pedal* circuit designed by B. H. Baily in PRACTICAL ELECTRONICS July 1968 issue. For anyone making this device I would like to suggest a useful addition.

By using the low frequency oscillator shown in Fig. 2, a continuous "waa-waa" effect can be produced at any desired speed.

The pedal controlled potentiometer VR2 in Mr. Baily's circuit is replaced by an *npn* silicon transistor, TR2, with its emitter connected to the negative line and its collector to the junction of C4 and C5. The base is connected to the output of the oscillator via a fixed 500kΩ resistor, R10, and a 1MΩ potentiometer (linear), VR3, which varies the effect from a "twangy" to a mellow "waa-waa". The capacitor C7 cuts out thump from the oscillator.

Component values are not critical and TR3 and TR4 can be almost any *npn* type, e.g., 2N1302. The transistor type for TR2 is more critical and a silicon type should be used, as the leakage current must be very small. If no meter is available to select a transistor with low leakage, complete the rest of the circuit first and then try several transistors to get best performance. Two types found suitable were BSY27 and BSY38.

The potentiometer VR4 varies the oscillator frequency from about 1 to 8Hz. It is connected so that it is turned fully anti-clockwise for minimum resistance, which then gives approximately linear frequency control.

The connections from C10 and C8 to C9 must be as direct as possible and not by wires longer than 2in.

M. P. R. Hamer,
Bath.

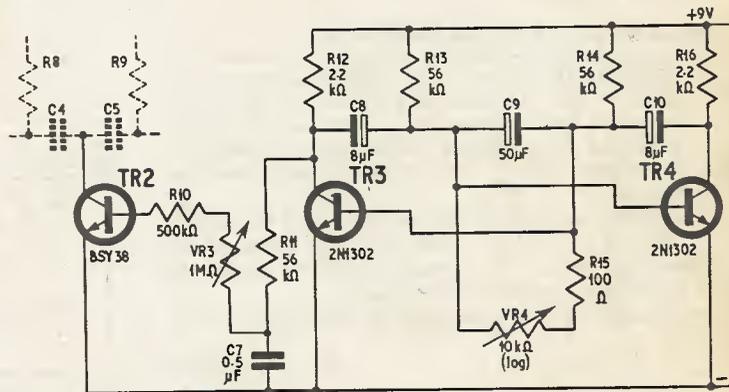


Fig. 2. Circuit diagram for variable "waa-waa" sound effect

BLOW OUT THE LIGHT

A REMARK made by the author of the *Sound Operated Switch*, March 1969 issue, spurred me into experimentation, and I have "developed" an advanced type of electronic candle.

In the circuit the base of TR5 is connected to the collector of TR4, so that with no input the bulb LP1 is on; when a signal is applied at the input the bulb is extinguished.

The original connection between TR5 collector and the negative supply is broken, and another NKT277 transistor (TR6) and a phototransistor (TR7) is inserted between these points as shown in Fig. 3.

The input transducer for the switch is a 200 ohm moving coil earpiece insert. The phototransistor TR7 is concealed behind the bulb, making sure that light can pass from the bulb to TR7 emitter.

When a lighted match or lighter is held near LP1 the light from the match falls on TR7 causing it to conduct, making TR6 base go more negative and causing it to conduct. If the ambient noise level is not too great TR5 will also be conducting and LP1 will light up. The light from this will fall on TR7 thus forming positive feedback and LP1 will stay alight when the match is removed.

To extinguish the bulb it is only necessary to blow on it, blowing on the input transducer at the same time.

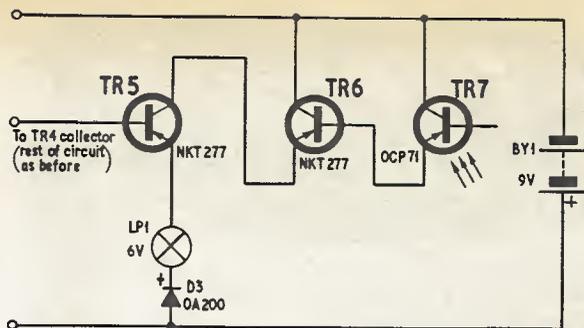


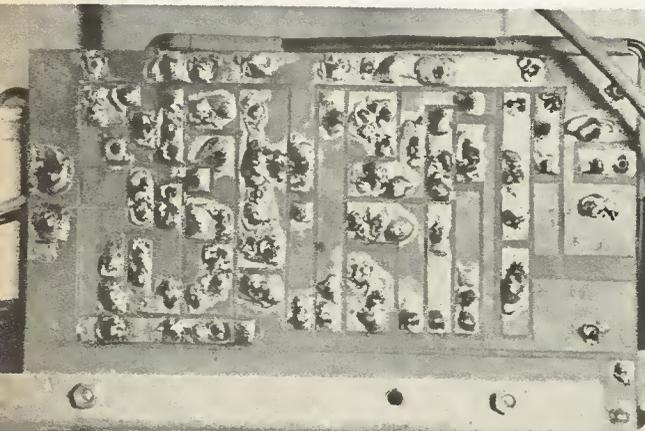
Fig. 3. Sound operated electronic candle

This will cause TR5 to switch off, extinguishing the bulb and thus interrupting the light to TR7 which remains off when the blowing is stopped.

Potentiometer VR1 should be adjusted so that ambient noise will not operate the switch. Also, TR7 should be positioned so that only light from the bulb, or match, will fall on the bulb. If the bulb still persists in lighting up when it is not intended to, a resistor should be placed between TR6 base and TR7 emitter.

T. J. Coombs,
Liss,
Hampshire.

PRINTED CIRCUITS



Underside view of a printed board for a 5 watt amplifier

QUITE a lot has been written recently about the awkward or risky techniques for making printed circuits. I have evolved a safe, simple and non messy method, using no paints or chemicals.

Once the chosen circuit wiring has been planned it should be drawn full scale on graph paper and taped to the copper side of the laminate board. Cut along the lines with a sharp knife to mark the copper and mark in the holes to be drilled. Remove the paper and now cut right through the copper foil. Next prise up the corner of each unwanted piece of copper and peel from the board.

Before drilling the holes, any rough edges of copper should be smoothed down. Once all drilling is completed the board is ready for soldering.

With a little care, strips of copper only 1mm wide can be removed, so the circuits can be really compact.

I have used this method successfully several times, the most complex circuit so far being a seven transistor 5 watt amplifier built on a board measuring 5in x 3in, see photograph.

J. Magee, Glasgow, S.2.

OSCILLOSCOPE PRE-AMPLIFIER

AN ADDITIONAL $\times 10$ on the y-scale of an oscilloscope is often desirable and the circuit in Fig. 4 was developed to fill this need. Noise is sufficiently low not to blur the trace and the frequency response is 50Hz to 9MHz ± 0.5 dB, wide enough for most low cost oscilloscopes.

The input impedance is 6k Ω at 1kHz and the maximum input signal is 0.5V peak to peak. The output impedance is 600 Ω . The pre-amplifier gives a gain of 20dB ($\times 10$) and current drain is 8mA.

The rise time t_r is ≈ 34 ns and the delay time t_d is ≈ 15 ns.

K. J. Matthews,
Seaford,
Sussex.

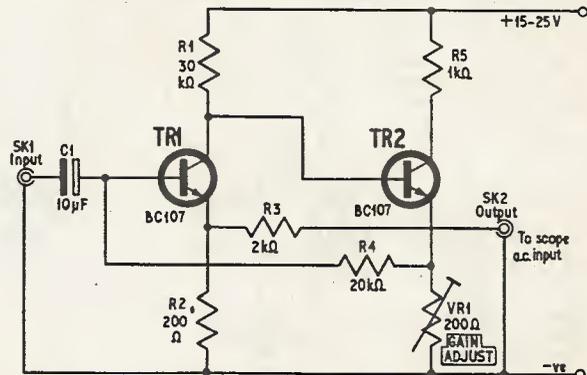


Fig. 4. Circuit diagram of the 20dB oscilloscope pre-amplifier

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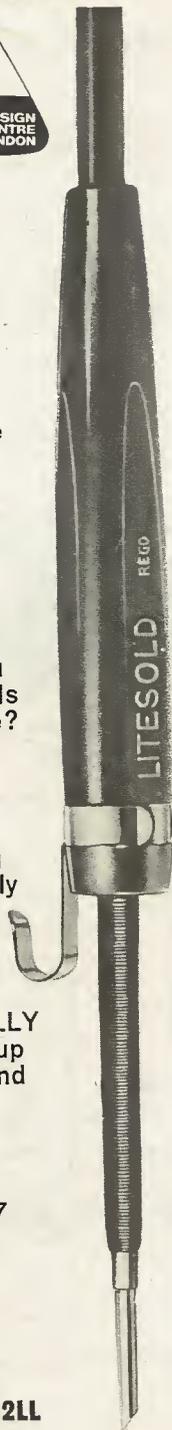
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Tel: Kelso 2369. Telex: 72192.

By Alan Douglas, Sen. Mem. I.E.E.E.

LAST month we completed the 12 oscillator units; now we go on to tackling the frequency dividers which will provide the rest of the pitches necessary, by division of the oscillator frequency in octave sub-multiples.

METHOD OF DIVISION

In Fig. 3.1 is given the block diagram of an oscillator and divider unit which shows how the note of B is successively divided to produce octave frequencies over seven stages of division.

The circuit of a divider unit is shown in Fig. 3.2. This consists of seven similar bistable generators which are in effect triggered switches; for if we consider the first divider, an incoming synchronising pulse from the

oscillator unit causes the circuit to change from one state to the other, that is one side fully conducting, the other side cut off.

One complete cycle of the bistable circuit occurs for every two input pulses so that the pulse repetition frequency of the output from either of the collectors is thus half that of the input frequency so that division by two has taken place, so producing the octave below the generator frequency which is taken off via C4 for subsequent routing to the manual contact assembly.

Each bistable stage continues this 2:1 square wave division as the synchronising pulses are maintained down the chain with the result that seven additional octave notes are generated in addition to the basic oscillator product.

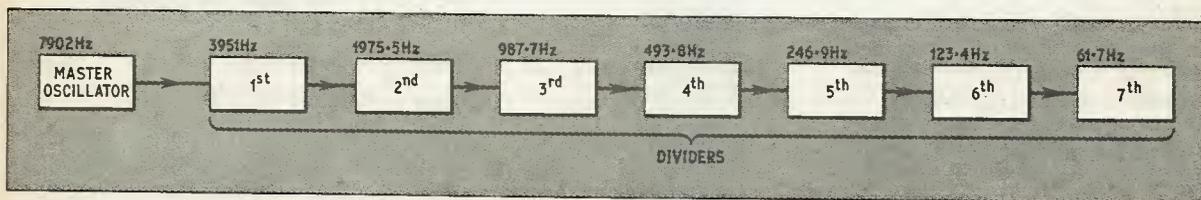


Fig. 3.1. Block diagram of an oscillator and divider showing how the note of B is divided into octave submultiples

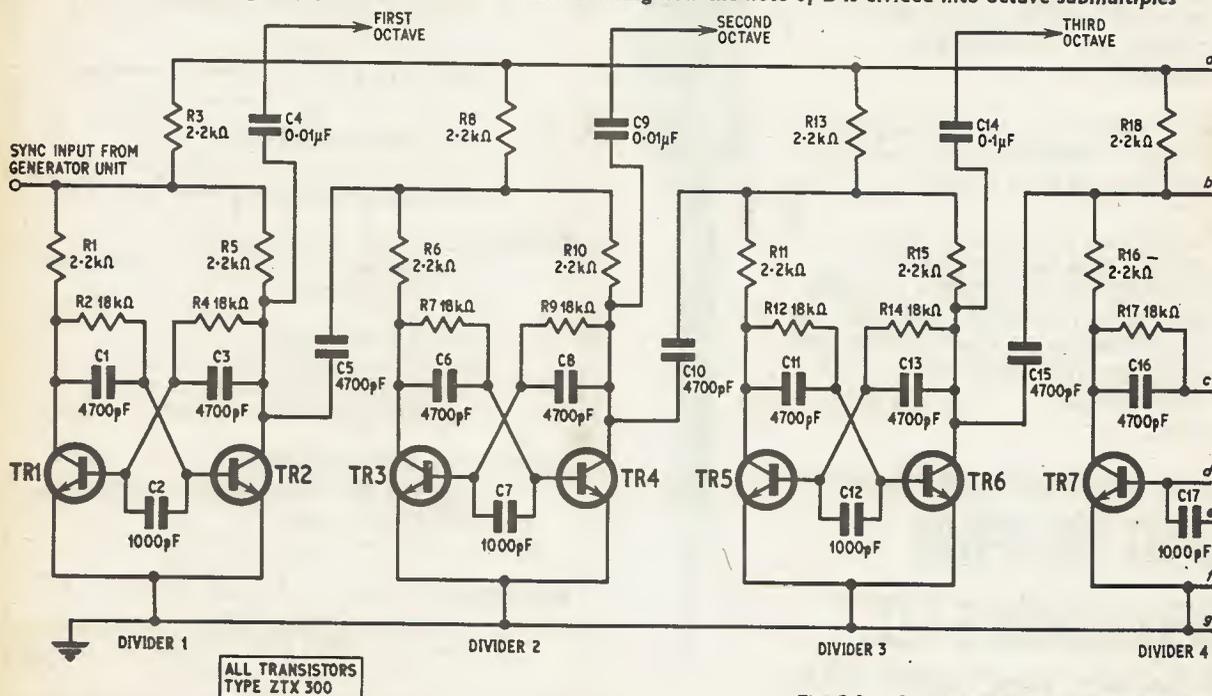


Fig. 3.2. Circuit diagram of a divider unit

DIVIDERS AND KEYBOARD WIRING

This series is expected to extend to 12 parts. Total cost of material for the organ is likely to be around £250

PRINTED BOARDS

Since the divider units are repetitive in their bistable complement, the choice of printed boards is an obvious one for a standardised assembly, as all component parts will fit in the same way on each board. Other advantages are the reduced risk of crosstalk and economy in the use of solder, a point sometimes overlooked.

Fig. 3.4 shows the etching and drilling layout for part of one divider board. Since the copper patterns for all seven stages are identical, only a section of the complete board is shown. However, a complete etched board is shown in the photograph.

For those constructors who do not fancy the prospect of etching boards, these can be obtained ready drilled from Mecelex Ltd., Whycliffe Mills, High Church Street, New Basford, Nottingham.

COMPONENT MOUNTING

In Fig. 3.3 is given the component layout for three bistables on the board section. Since the component assembly pattern for each stage is identical, with the exception of some of the output capacitors, the mounting and soldering of components can be swiftly completed.

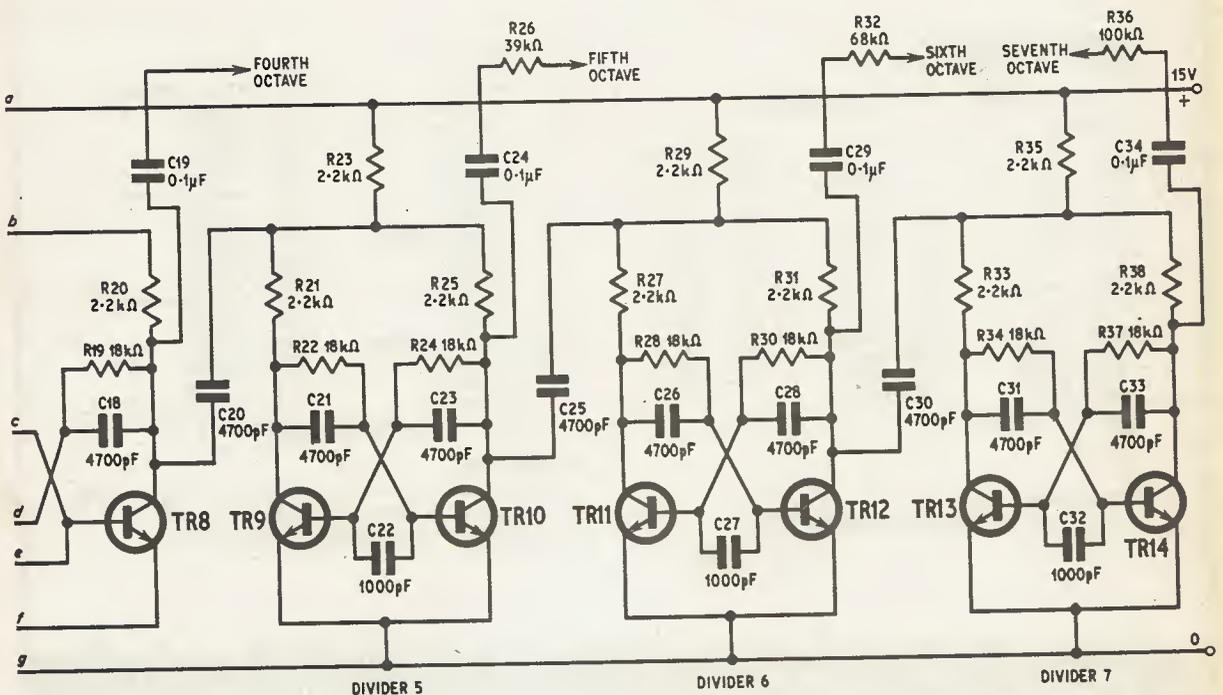
The accompanying photographs show a completely assembled board. Note here that one of the leads of the output capacitors is left to protrude for $\frac{1}{4}$ in of its length. This is to provide an anchorage for equalising resistors which will be attached later.

TESTING THE DIVIDERS

Last month we checked the oscillators with a 30,000pF capacitor across each of the coils. Now using one of these rough tuned oscillators we can check each divider in turn, taking the output from one stage at a time through a 100 kilohm resistor into a small amplifier and loudspeaker or high impedance headphones, which, of course, do not require the attenuating resistor.

If an oscilloscope is available the waveforms can be examined directly.

In making these functional checks the +15V supply from P.S.U.1 will feed both the oscillator and dividers. As an additional aid to smoothing a 1,000 μ F 25V electrolytic capacitor should be connected across the supply line and it is as well to retain this when assembling the tone generation system in the console.



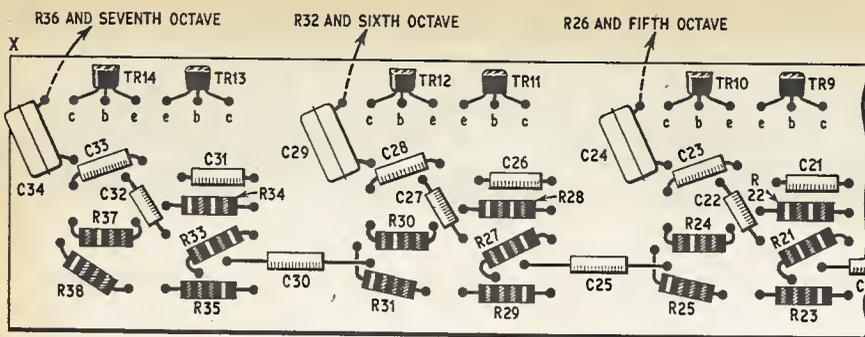


Fig. 3.3. Component layout on top side of divider board. Three stages are shown; the complete board can be seen in photo at the bottom of the page

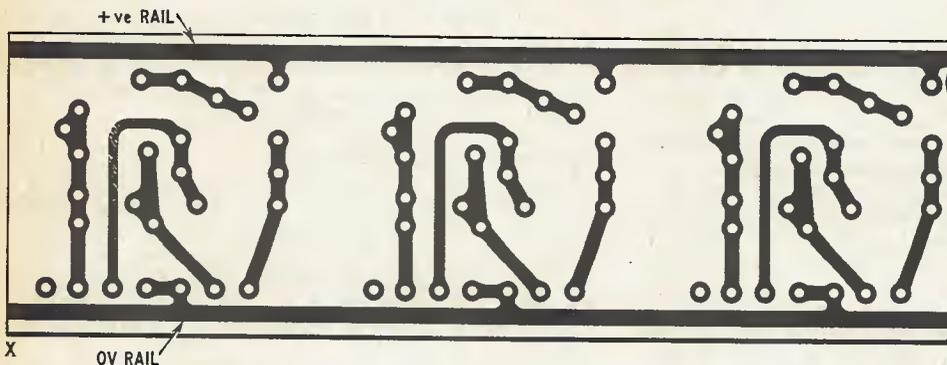
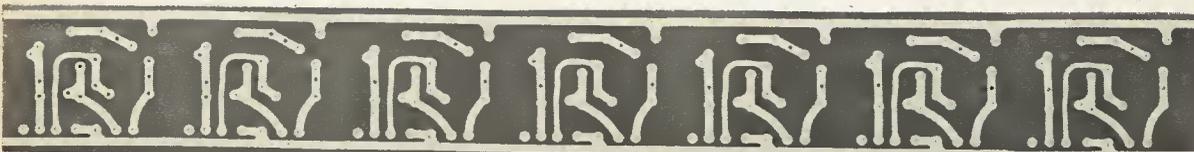


Fig. 3.4 (below). Printed circuit for divider unit board. Three stages only are shown full size, the pattern being repeated to cover seven stages in all. See photograph below



COMPONENTS . . .

DIVIDER UNIT (12 REQUIRED)

Resistors

R1	2.2k Ω	R14	18k Ω	R27	2.2k Ω
R2	18k Ω	R15	2.2k Ω	R28	18k Ω
R3	2.2k Ω	R16	2.2k Ω	R29	2.2k Ω
R4	18k Ω	R17	18k Ω	R30	18k Ω
R5	2.2k Ω	R18	2.2k Ω	R31	2.2k Ω
R6	2.2k Ω	R19	18k Ω	R32	68k Ω
R7	18k Ω	R20	2.2k Ω	R33	2.2k Ω
R8	2.2k Ω	R21	2.2k Ω	R34	18k Ω
R9	18k Ω	R22	18k Ω	R35	2.2k Ω
R10	2.2k Ω	R23	2.2k Ω	R36	100k Ω
R11	2.2k Ω	R24	18k Ω	R37	18k Ω
R12	18k Ω	R25	2.2k Ω	R38	2.2k Ω
R13	2.2k Ω	R26	39k Ω		

All 10%, $\frac{1}{2}$ watt carbon

Transistors

TR1-TR14 ZTX300 (Ferranti) (14 off)

Capacitors

C1	4,700pF	C18	4,700pF
C2	1,000pF	C19	0.1 μ F polyester
C3	4,700pF	C20	4,700pF
C4	0.01 μ F polyester	C21	4,700pF
C5	4,700pF	C22	1,000pF
C6	4,700pF	C23	4,700pF
C7	1,000pF	C24	0.1 μ F polyester
C8	4,700pF	C25	4,700pF
C9	0.01 μ F polyester	C26	4,700pF
C10	4,700pF	C27	1,000pF
C11	4,700pF	C28	4,700pF
C12	1,000pF	C29	0.1 μ F polyester
C13	4,700pF	C30	4,700pF
C14	0.1 μ F polyester	C31	4,700pF
C15	4,700pF	C32	1,000pF
C16	4,700pF	C33	4,700pF
C17	1,000pF	C34	0.1 μ F polyester

All polystyrene unless otherwise stated.

Miscellaneous

Copper clad board 14 $\frac{1}{2}$ in \times 1 $\frac{1}{2}$ in. Stranded core single p.v.c. wire in colours as required
Material for board retaining bars (see text)



If any one of the bistables fails to divide, it is almost certainly a faulty transistor which needs to be replaced.

BOARD RETAINING BARS

The long narrow shape of the divider boards was decided on because there is a convenient place for the 12 sets on the left-hand side of the console kneeboard which isolates them from possible power line effects.

Referring to the rear view photograph of the console given in last month's article, it will be seen that these boards are held in place by four slotted hardwood bars. Details of two bars with a pair of boards in position are given in Fig. 3.5.

The two bars "b" should be attached to the kneeboard by way of the fixing screw and separated by a distance of $13\frac{1}{2}$ in (measured from inner edge of bars). Using a $\frac{3}{16}$ in drill, pilot holes can be made for screwing in the $3\frac{1}{2}$ in lengths of 2 B.A. brass rod. Bars "a" are drilled to just clear the threads of the rods so that these are a push fit. The retaining nuts can be loosely threaded on at this point, but the boards should not be positioned as some further wiring has to be done.

EQUALISING RESISTORS

Now, in all bistable systems the lower notes tend to be louder than the upper ones. The dividers amplify as well as divide, at least they pass through the condition when they amplify during the switching period. So we have to reduce the lower octaves somewhat to prevent the sound from being bass heavy.

With individual contacts and precious metal busbars, it is easy to cut the bars and introduce resistors as required. But with the flat graphited bars used in the Harmonics keyswitches, it is not so easy and the method of holding the bars in slotted plastic blocks does not encourage much alteration, so we add equalising resistors to some of the divider outlet capacitors as follows:

- The seventh octave outlets, 100 kilohms.
- The sixth octave outlets, 68 kilohms.
- The fifth octave outlets, 39 kilohms.

All of these being $\frac{1}{2}$ watt, 10% types.

In addition, there might be one or two other dividers which tend to be too loud and may need the odd resistor of values in the range 27, 33 or 39 kilohms, to equalise. This cannot be predicted and might not occur.

COLOUR CODED OUTLETS

Naturally with so many tone outlets to consider, we must adopt a colour coding system, and this can be based on the international resistor colour code.

The wiring colour code that will apply to each oscillator and divider board is as follows:

Generator output F	black
1st octave	brown
2nd octave	red
3rd octave	orange
4th octave	yellow
5th octave	green
6th octave	mauve
7th octave	white.

Underside of divider board showing soldered connection. Note protruding output capacitor wires to which equalising resistors are attached where required

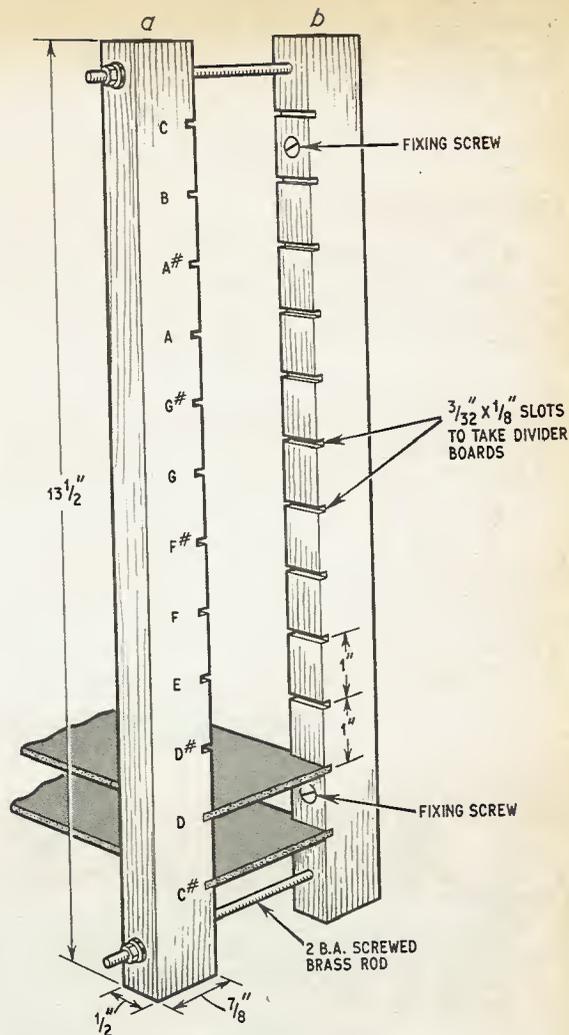
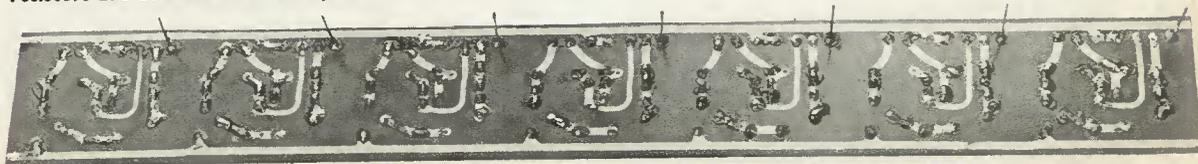


Fig. 3.5. Retaining bars "a" and "b" for divider boards
Note signs are added to bar "a" to aid in board identification when oscillators are tuned

It is important, when making up the cable forms, to keep each set together in a bunch and tie a small label to each bunch with its note sign, otherwise they will all look the same and will have to be sorted out all over again.

MOUNTING OF OSCILLATORS

To ascertain the correct lengths of the black leads from the oscillator outputs F to the keyboard, these oscillator units should now be mounted in their final position.

First make up a wood shelf 21in × 4in × 1/4in. This should then be fixed to the rear keyboard support rail using angle brackets (see photograph below). Six oscillators are attached to the shelf by screws. The remaining six are angularly disposed along the console side, to the fore of the divider bars.

tone ROUTING

To connect the tone sources to the keyboards involves three processes. Firstly connect the dividers to the upper keyboard; then connect from the upper to the lower one; and finally connect again to the upper one to extract the pedal notes which run from 32.7Hz to 349.2Hz.

Fig. 3.6 gives the frequency breakdown of the tone generation system. It will be noted that the highest frequency is B at 7,902Hz. Since there are 12 notes in the octave, we cannot divide 12 into 61 to include top C, and as this note is rarely used it is thought better to ensure generation of bottom C 32.7Hz which is often required.

PITCH PAD WIRING

If we refer to Fig. 2.1 showing the printed circuit of the upper contact assembly, we can see the 16ft wiring pads starting at bottom C on the lower extreme left of

the board. The first octave here has no coupler connections to the 8ft row, so we start by taking the white wire from the C divider and soldering it to the extreme left-hand pad. Then we take the white wire from the C sharp divider and solder it to the C sharp pad next to the C; and so on using all the white wires from the different dividers.

When we get to B, we start again with the mauve wire from the C divider, then the mauve wire from the C sharp divider and so on.

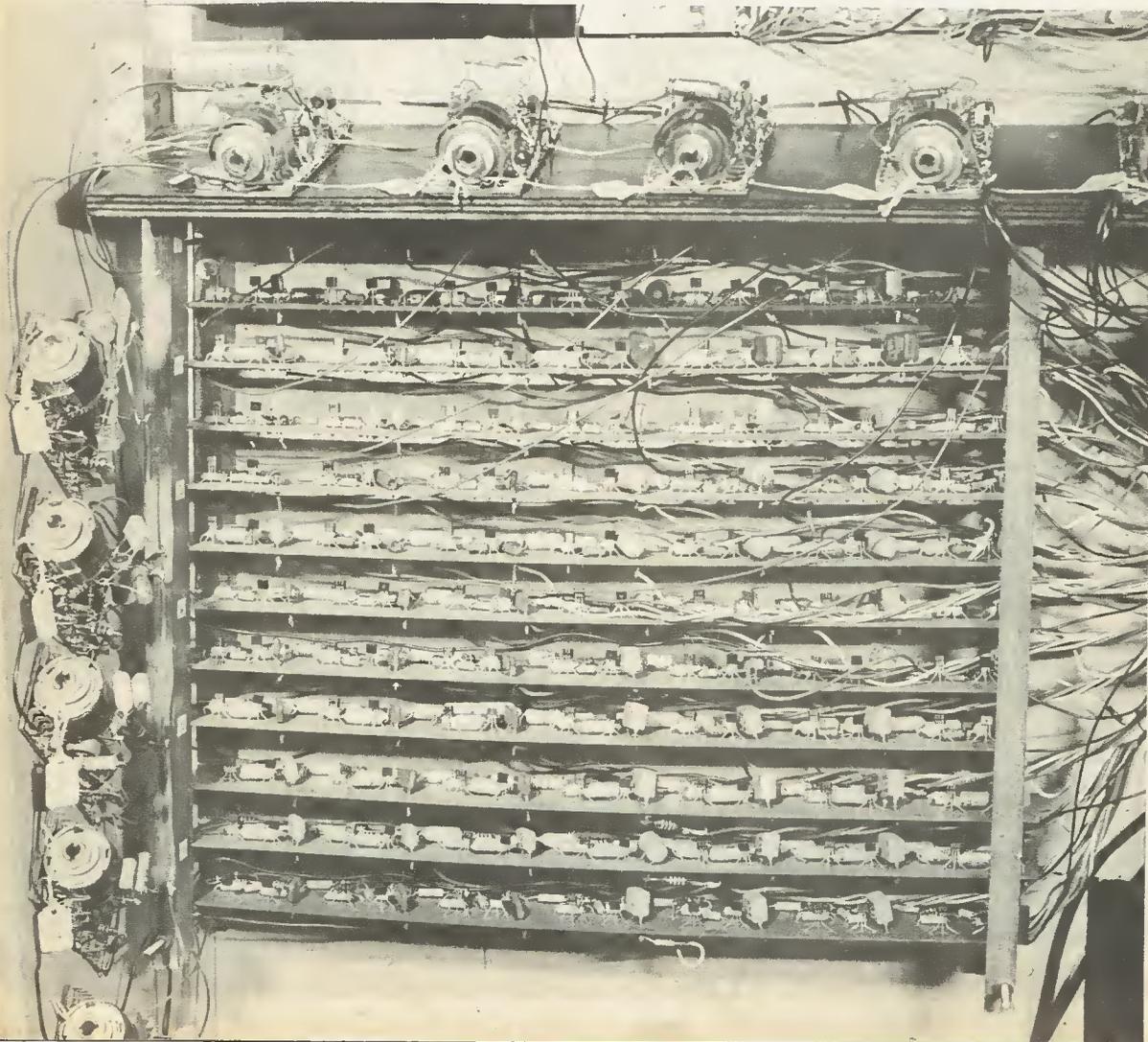
Eventually we come to the end of the 16ft pitch row of pads and at this point we go back one octave and solder to the 8ft pads above.

When we come to the end of the 8ft we again go back one octave and use the 4ft pads. In the end we find we have wires left over for the 2ft pads and if all that has gone before is correctly carried out, all of these remaining wires will be black.

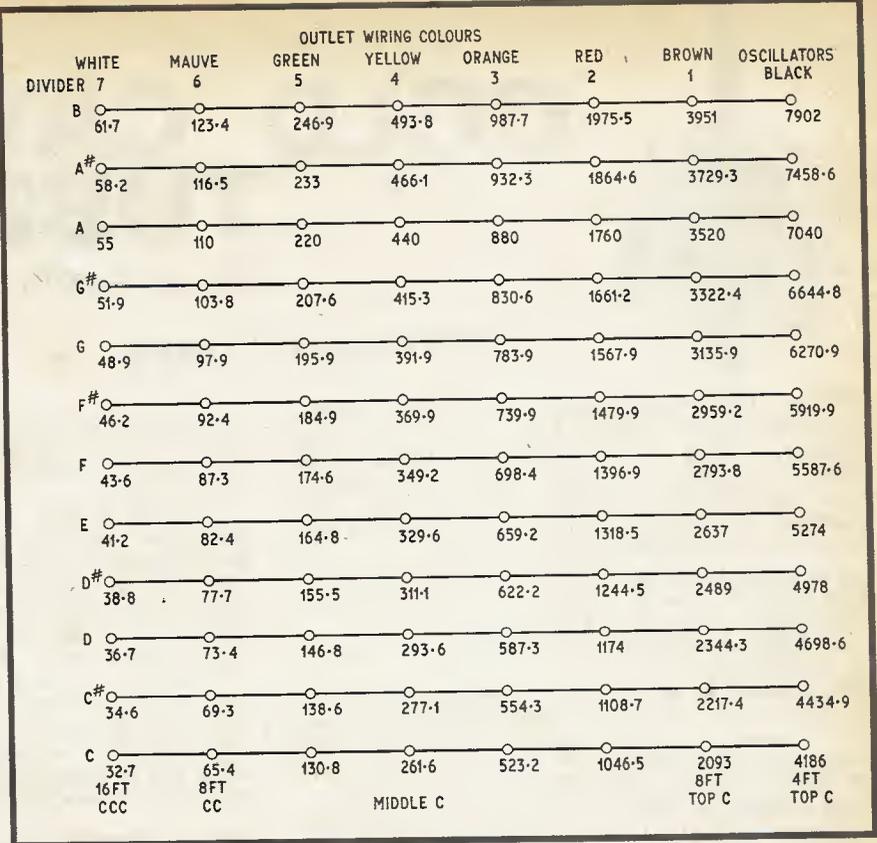
Considerable care should be exercised in soldering to these printed circuit boards and *only* resin as a flux can be used. Excessive heat will affect the bond between the copper and the laminate, so make sure the iron is hot and complete the joints quickly.

If further clarification of this wiring is required, a diagram of a complete printed board can be obtained by purchasers of the manual contact assemblies from Harmonics Ltd.

Oscillators and dividers shown wired and in position. Note equalising resistors on divider board underside.



This shows how the complete tone generation system is evolved from the 12 fundamental frequency oscillators. These frequencies are divided down in their octave sub-multiples through the 12, seven octave dividers each of these being identified by their preceding note sign B, A sharp, etc. The frequencies given in Hertz are only to one place of decimals, the lowest being 32.7Hz and the highest 7,902Hz, these constituting the frequency limits of the organ. The pedal frequency range extends from 32.7Hz to 349.2Hz. When wiring from the dividers to the printed circuits of the manual contact assemblies, this chart should be used.



BUSBAR OUTLETS

The tone signals fed into the upper manual are automatically distributed to the proper busbars by the printed wiring.

The busbar outlets are coloured: blue for 16ft, grey for 8ft, yellow for 4ft and red for 2ft. There is also a black earth wire at each end which is most important.

WIRING TO LOWER MANUAL

Now, the problem is to cross connect the upper tone inlets to those of the lower manual. This is in fact easy, since it merely means looping across from A to A, B to B, etc., along the whole keyboard. For this we need stranded core single p.v.c. wires in the following colours:

C	black	F sharp	light blue
C sharp	brown	G	dark blue
D	red	G sharp	mauve
D sharp	orange	A	grey
E	yellow	A sharp	white
F	green	B	pink.

Attach about a foot of each colour to the lower manual pads using the upper manual printed circuit board as a guide. These wires are now brought out past the springs at the rear. If the lower keyboard is placed in position and the top one laid on its back, connections to the latter can be easily made.

There are two busbar pitch outlets; 8ft and 4ft, the wires being identified by the colours: grey for 8ft, yellow for 4ft and black for earth.

PEDAL CABLES

Before putting the upper keyboard back on its supports the pedal cables must be attached. There is a

small problem here because we must only attach as many wires as there are pedal key contacts.

If the full 30 wires were soldered on and it was decided to use a short compass pedalboard of 13 notes, the wires not used would certainly pick up hum and noise. We will assume, however, that the full 30 notes are to be used and here once more we need the 12 core cable.

The wire lengths to be used should be in the order of 3ft to span from the keyboard to the pedal plug position.

WIRING TO UPPER MANUAL

There are two and a half octaves of pedal notes at 16ft pitch plus one extra at 8ft; but as the tone networks are different for each of these, they must be wired separately.

For the 30 16ft notes we go back to the 16ft wiring pads of the upper contact assembly (see Fig. 2.1). Using the 12 note colour code as before, connect a black lead to the extreme lower left 16ft pad, then brown to the pad adjacent and so on until all 30 wires are connected.

For the 8ft notes we do exactly the same but starting one octave higher up, that is the 13th pad along on the 16ft row or the second C from the left.

At this point, if all soldering is secure both keyboards can be screwed into position on the support rails. Be sure none of the busbar outlet wires are trapped between the keyboards and their wooden supports or that the switch plungers do not catch on any of the wiring and fail to return.

Next month we start construction of the amplifier and power supply units.

To be continued

Part
THREE

COLD CATHODE TUBES

By J.B.Dance M.Sc.

TRIGGER TUBES

Cold cathode trigger tubes are basically very similar to cold cathode diodes, but contain an additional electrode known as the trigger or starter. This electrode can be used to initiate a discharge between the main anode and the cathode, but once the main discharge has started, it will not be affected by any variations of the trigger electrode potential. The main discharge can be extinguished only by a reduction of the main anode to cathode potential. The symbol for the trigger tube is shown in Fig. 3.1.

A trigger tube may be considered as a double diode, the trigger being one of the anodes and the cathode being common to both anodes. The trigger to cathode gap and the main anode to cathode gap each have their own striking and maintaining voltages, those for the trigger electrode normally being much lower than those for the main anode, since the trigger to cathode gap is much smaller than the main anode to cathode spacing.

Trigger tubes can replace valves and transistors in many types of switching circuit, but cannot operate at such high speeds. The trigger electrode is used as a high impedance input electrode; whilst its function is to initiate conduction, it has no effect on the main gap current of a conducting tube.

In many circuits trigger tubes are operated with a main anode voltage greater than the main anode maintaining voltage but less than the main anode striking voltage. No main gap current will therefore flow at first.

If, however, the potential of the trigger electrode is now increased, the trigger to cathode gap will strike as soon as the potential across it reaches the trigger striking voltage.

The ions formed in the trigger discharge are so numerous that a space charge of positive ions is formed in the region of the cathode and this results in the main gap striking voltage being lowered almost to the maintaining voltage of this gap. The main gap therefore strikes, since the potential applied across it is greater than its maintaining voltage.

Some trigger tubes have twin trigger electrodes. In such tubes conduction in the main gap can be initiated by a discharge from either trigger to the cathode. Such tubes are used in reversible counting circuits which will either add or subtract and in other circuits where two isolated inputs are required.

RELAY OPERATION

A circuit designed by Ericsson Telephones for the operation of a relay, from an input which cannot supply much power, is shown in Fig. 3.2. The tube employs a priming anode to ensure prompt striking; it is connected to the 10 megohm resistor in the circuit shown. The electrode connected to the junction of R4 and R5 is a shield anode; tubes employing a shield anode can control more power, since a higher anode voltage can be employed before the trigger electrode loses control.

The Elesta ER21A trigger tube for a.c. operation

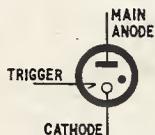


Fig. 3.1. Graphical symbol for a cold cathode trigger tube

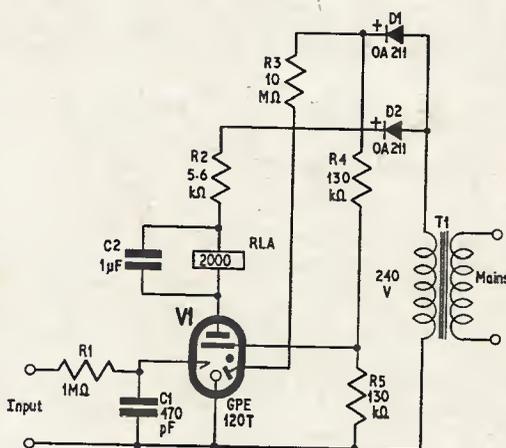


Fig. 3.2 The trigger tube used to operate a relay

In the circuit in Fig. 3.2, the alternating mains supply voltage is half wave rectified and is applied to the circuit without being smoothed so that conduction in the trigger tube will cease when the power supply voltage falls towards the end of a half cycle. If a smoothed power supply voltage is used, some means of extinguishing the discharge in the tube would be needed, since the charged smoothing capacitors would tend to hold the tube on.

When the input potential is raised above the trigger striking voltage, the trigger gap strikes and the main gap will also pass a current as soon as a positive going half cycle of the power supply reaches the anode. The relay therefore closes if the input potential exceeds the trigger striking voltage of $123.5 \pm 2.5V$. The capacitor connected across the relay keeps the latter energised during the half cycles when the tube is non-conducting; it therefore prevents the relay from "chattering".

since the relay contacts RLA1 are now open. However, when the level does reach the upper contact, the trigger voltage will fall and the relay will be de-energised. This will result in the pump which is forcing more liquid into the tank ceasing to function. The contacts close again and the level must now fall below the level of the tip of the lower probe before the motor is switched on again.

It can be seen that the use of the two contacts at different levels prevents the pump from being switched on and off too frequently as the level changes slightly.

TIMING CIRCUITS

A timing circuit will cause a relay to operate or produce an output pulse at a certain preset time after an input pulse has been applied to the circuit. The timing interval may range from a small fraction of a second to many hours. Such circuits are widely used in industrial

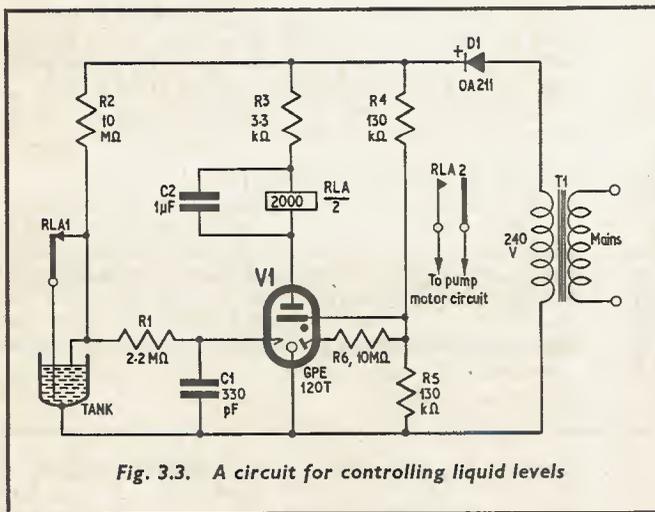


Fig. 3.3. A circuit for controlling liquid levels



The Cerberus GR44 trigger tube; this tube has twin trigger electrodes and a priming anode

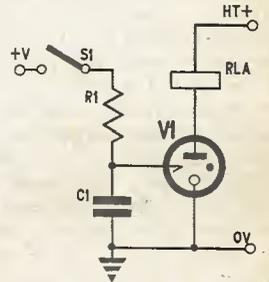


Fig. 3.4. A basic timer circuit

LEVEL CONTROL

The application of the circuit in Fig. 3.2 to the control of liquid levels in a metal tank may be illustrated by the circuit in Fig. 3.3. The liquid must have at least a limited conductivity.

The relay contacts RLA1 are closed when the relay is not energised. The 10 megohm resistor forms a potential divider with the resistance of the liquid between the probes and the tank. If the conductivity of the liquid is adequate to ensure that the resistance between the probes and the tank is much less than 10 megohms, the trigger electrode voltage will be only a little above the cathode potential and the tube will not pass a current. The relay will therefore remain de-energised.

When liquid is taken from the tank and the level falls below that of the tips of both probes, the latter will no longer be in contact with the liquid. The trigger voltage will therefore rise and the tube will fire, the main gap conducting in the half cycles when the anode is positive with respect to the cathode. The relay therefore operates and contacts RLA1 open. The relay may be used to switch on an electric motor (by means of an additional pair of relay contacts RLA2) which pumps more liquid into the tank.

When the liquid rises, the circuit will not be affected until the level reaches that of the tip of the upper probe,

automation systems, but are also useful as photographic timers in the home.

Trigger tube timing circuits depend on the time taken for a capacitor to charge through a resistance for their operation. The basic circuit is shown in Fig. 3.4. When a voltage V is applied to the resistor $R1$ by the closure of the switch $S1$, the capacitor $C1$ begins to charge. The tube fires when the voltage across C becomes equal to the striking voltage of the tube used.

The capacitor charges exponentially from zero to the voltage V . It can be shown that the voltage V_c across the capacitor at a time t after the application of the voltage V is given by the equation:

$$V_c = V(1 - e^{-t/RC})$$

The tube will fire when the voltage V_c becomes equal to the trigger striking voltage, V_s . This occurs after a time t where

$$t = RC \log_e \left\{ \frac{V}{V - V_s} \right\}$$

The product RC is known as the time constant of the circuit; R is in megohms and C is in microfarads.

A simple timing circuit designed by Ericsson Telephones is shown in Fig. 3.5. A stabilised source of

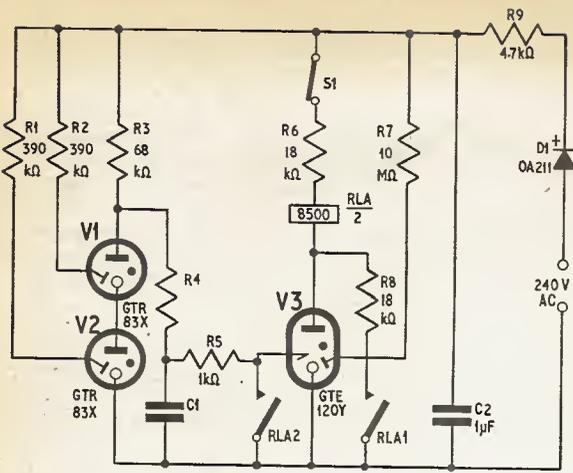


Fig. 3.5. Simple timer using a relay that operates at 4.5mA

voltage is used to supply the trigger resistor and capacitor to prevent mains voltage variations from affecting the duration of the timing intervals. When the mains voltage is first applied to the circuit, the capacitor C1 begins to charge through the resistor R4. After a time equal to $1.28RC$ seconds the tube will fire and the relay will close.

Contacts RLA2 close and discharge C1 via the 1 kilohm resistor and contacts RLA1 close so that the relay energising current no longer flows through the trigger tube. The circuit will be reset and the relay de-energised when the reset switch S1 is opened or when the mains supply is interrupted. The electrode

connected to the 10 megohm resistor is a priming anode.

A more sophisticated version of this timer, which will provide a wide range of time intervals, is shown in Fig. 3.6. The circuit is basically similar to that in Fig. 3.5, but the time interval may be pre-selected by means of a six-position switch S1 together with the two-position switch S2 and the potentiometer VR1 connected to S1. The approximate time intervals obtained are shown in Fig. 3.6, but these will be affected by component tolerances.

The principle of operation is the same as that of the circuit in Fig. 3.5. The circuit in Fig. 3.6 may be supplied from a source of alternating voltage in the range 200 to 225 volts if the 1.2 kilohm resistor in the h.t. line is shorted out.

This circuit can be used in a photographic enlarger timer (Fig. 3.7). The contacts marked RLA3 are an additional set of normally closed contacts on the relay of the Fig. 3.6 circuit. When the photographer is ready to commence the exposure, he closes the switch S4 and the enlarger lamp is illuminated. This action also applies the mains voltage to the timer circuit. After the pre-set time interval, the relay is energised and contacts RLA3 open, thus ending the exposure.

It is now only necessary to open the switch S4 in order to prepare the equipment for use again.

LIGHT OPERATED RELAY

The circuit in Fig. 3.8 (published by the Cerberus Company) enables the relay to be energised when a beam of light falls on the cadmium sulphide photoconductive cell X1. The GR16 trigger tube is designed for operation from either a.c. or d.c., therefore no rectifier is required in the power supply line. The tube has an internal shield electrode which should be biased appropriately.

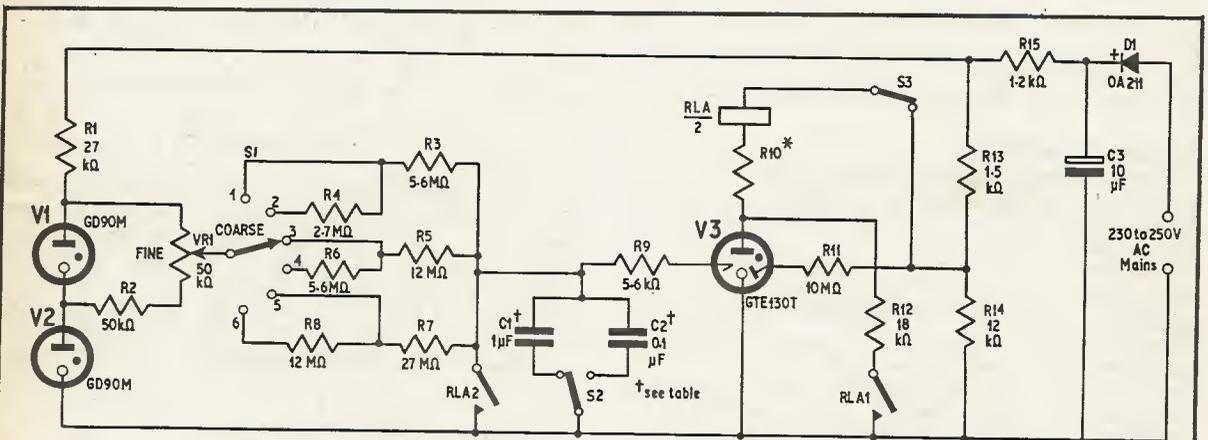


Fig. 3.6. A more comprehensive timer with range switches. The value of R10 is equal to 4 kilohms minus the relay resistance. The relay must operate at a current of less than 13mA

Table 3.1

Switch position	Time (seconds)		Switch position	Time (seconds)	
	C1	C2		C1	C2
1	1.0	10	4	3.1	31
2	1.5	15	5	4.8	48
3	2.1	21	6	7.0	70

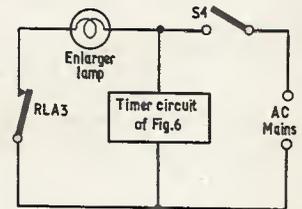
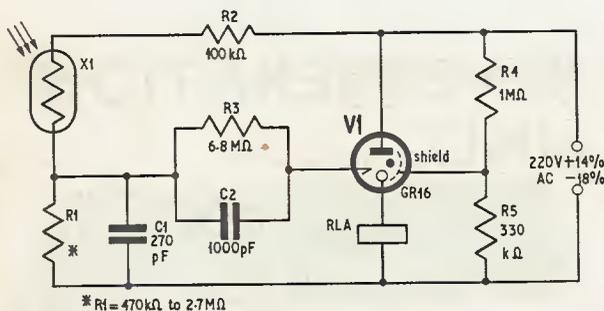


Fig. 3.7. The circuit in Fig. 3.6 can be used with a photographic enlarger

When no light falls on the photoconductive cell, its resistance will be high compared with the resistor R1, therefore the potential of the trigger electrode is not very different from the cathode potential. If a beam of light falls onto the photocell, the resistance of the cell falls from some megohms to a much lower value (typically, a few hundreds of ohms). The voltage drop is now occurring mainly across the resistor R1, so a relatively high voltage is applied to the trigger electrode. The tube therefore fires on those half cycles of the mains potential which result in the anode being positive. If the light beam is now removed, the trigger tube no longer fires.

The optimum value of the resistor R1 depends on the sensitivity required and on the type of photoconductive cell being employed. Typical values for R1 are within the range 470 kilohms to 2.7 megohms. The relay used contains a number of shorted turns so that it can be operated from a pulsed current without chattering.

There is a difference between the light intensities at which the relay is just de-energised as the light intensity slowly falls and that at which it will be just energised as the light intensity rises again. This has the advantage that it prevents the circuit from repeatedly switching itself on and off if there are some relatively small alterations of the light intensity. Such repeated switching would be undesirable if the unit were used to control street lighting or to switch the lighting on in an office.



* R1 = 470 kΩ to 2.7 MΩ

Fig. 3.8. Trigger tube can also be used in light sensitive circuits

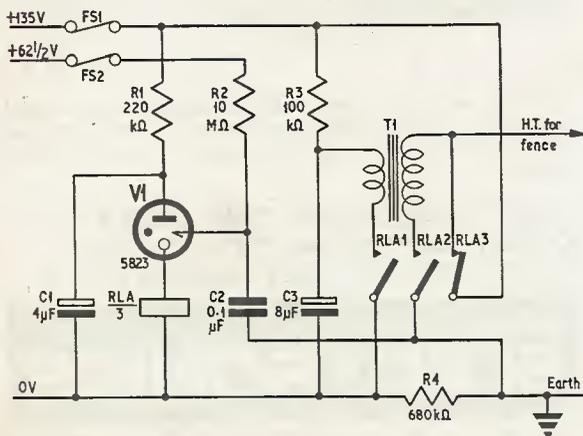


Fig. 3.9. An electric fence high voltage supply

If a circuit is required in which the relay will open when the photocell is in darkness, it is only necessary to interchange the resistor R1 and the photocell, the 100 kilohm resistor R2 being omitted. As in the case of the circuit of Fig. 3.8, there will be a switching interval between the light intensity at which the relay is energised and that at which it will be de-energised.

ELECTRIC FENCE CIRCUITS

A simple electric fence circuit using a high current cold cathode diode was discussed last month. A further circuit using a trigger tube (designed by the Philips Company) is shown in Fig. 3.9. A single pulse is applied to the electric fence when an animal touches the it.

No current is taken from the power supply except during the time an animal is in contact with the fence. If the insulation of the fence with respect to earth is good (over ten megohms), two small 62½ volt batteries will last at least one season, since the time for which current is being taken from the batteries is a very small fraction of the total operating time. The circuit uses the Philips/Mullard 5823 cold cathode trigger tube which contains a coated cathode; an equivalent type is the Z900T.

In the circuit in Fig. 3.9, a relay with two pairs of normally open contacts (RLA1 and RLA2) and one pair of normally closed contacts (RLA3) is required. The transformer is a valve output transformer.

When a resistance (normally that of an animal) is placed between the fence and earth, a current flows from the battery through this resistance and returns to the battery via resistor R4. The voltage thus developed across the latter resistance adds to that already present at the trigger electrode of V1 and causes the tube to fire. This causes C1 to discharge and a current passes through the relay. The contacts RLA1 and RLA2 therefore close, whilst contacts RLA3 open. Capacitor C3 discharges through the primary winding of transformer T1 and contacts RLA1, thus resulting in the generation of a pulse of about 2,800 volts across the secondary winding; it is this pulse which is applied to the fence.

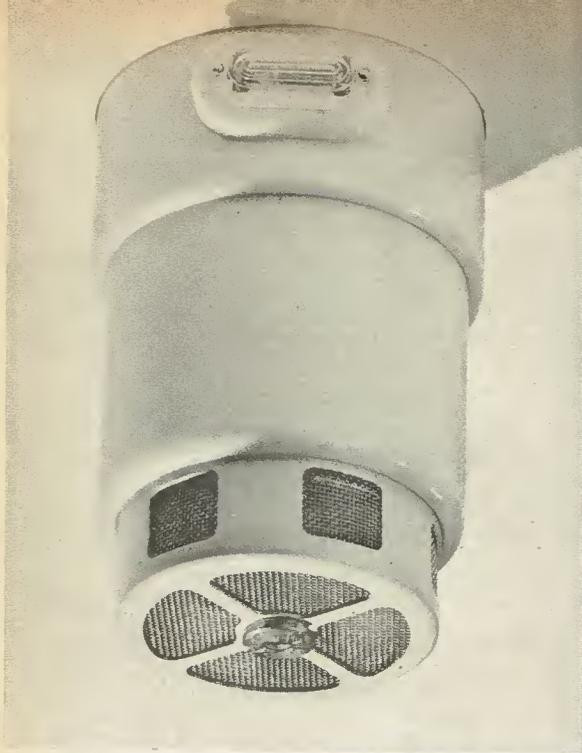
The tube ceases to conduct after a period of about 3 milliseconds and the relay is de-energised. The contacts then return to their quiescent position and the capacitors are charged via the appropriate resistors.

It is recommended that the insulation resistance between the fence and earth should be at least six megohms, since both the battery life and the pulse frequency are affected by inadequate insulation. If the insulation resistance is smaller than this recommended value, it may be necessary to reduce the value of R1 to prevent the circuit from operating continuously even if no animal is in contact with the fence.

COUNTING CIRCUITS

Trigger tubes can be used for counting electrical pulses. Counting circuits are widely used in industry (for example, for counting the number of articles coming off a production line), in electronic instruments such as digital voltmeters and in instruments used in nuclear physics. However, the use of trigger tubes for counting is now less common than it was some years ago.

The most common type of trigger tube counting circuit employs a ring of ten trigger tubes, one of the tubes conducting at any one time. The tube which is conducting emits a red glow and this indicates the number of pulses which have been counted by the



The Minerva ionisation chamber smoke detector. This unit is mounted on the ceiling and gives early warning of fire. A trigger tube is employed to operate a relay

circuit. If the zero tube is initially glowing and an input pulse is received by the circuit, the succeeding tube will fire (thus indicating that the circuit has made one count); the previously glowing zero tube will then be extinguished. The next pulse will result in the tube which indicates the digit two glowing.

This process continues, the glow passing step by step around the ring of tubes until, at the tenth pulse, the zero tube again conducts. At this instant an output pulse is provided which can be fed to another group of ten tubes which counts the number of tens. This latter group of ten tubes will provide an output pulse for each hundred pulses applied to the first ring. Thus forty tubes (four rings of ten tubes in each) can be used to count up to 9,999.

Other types of trigger tube counting circuit have also been used, including binary systems and the so-called biquinary counters which employ a ring of five combined with a ring of two; in the latter system a scale of ten can be constructed using only seven trigger tubes.

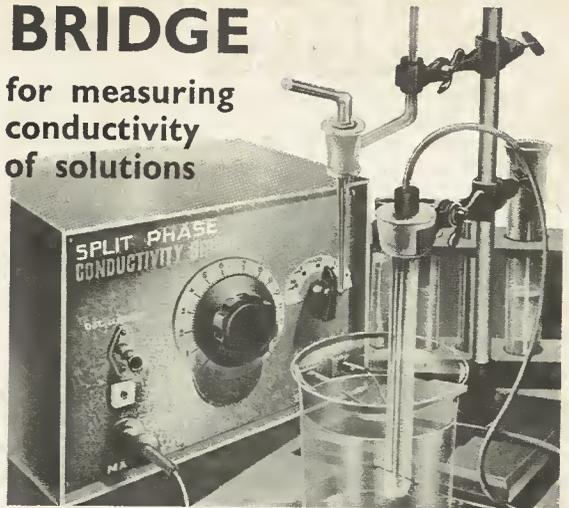
OTHER USES

Trigger tubes are used for a wide variety of other purposes. They may, for example, be used in a type of voltage stabilising circuit, which provides a stabilisation of a few per cent at output currents of up to some tens of milliamps. They are also widely used in industrial automation. A particularly interesting use of a special electrometer low current trigger tube is in ionisation smoke detectors. These detectors, which are normally ceiling mounted, will give an early warning of invisible smoke particles before a fire has done an appreciable amount of damage. They are widely used for protecting computers, nuclear reactors, and art treasures.

Next month: Arc discharge tubes

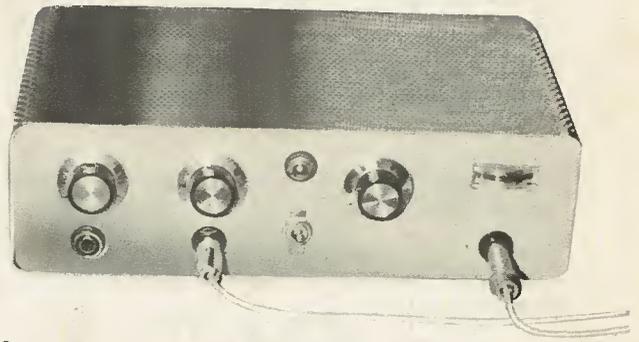
CONDUCTIVITY BRIDGE

for measuring conductivity of solutions



A new design based on a split phase circuit. This provides a higher degree of accuracy than more conventional instruments based on the Wheatstone bridge. A valuable asset for the chemistry laboratory.

SPRING LINE REVERBERATION UNIT



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MARKET PLACE

Items mentioned in this feature are usually available from electronic equipment and component retailers advertising in this magazine. However, where a full address is given, enquiries and orders should then be made direct to the firm concerned.

PHOTO WATCHDOG

Now that the holiday period has begun, many readers will be thinking of ways of making their homes secure during their vacation. One of the more obvious methods is to convince the would-be intruder that the house is occupied, and so deter his intrusion.

A photo-electric switch particularly suitable for deterring burglars is now being produced by Andrew Stephens (1947) Co., 61 Dickson Road, Blackpool, Lancashire. This switch operates from a.c. mains and can handle up to 6 amps. The switch automatically switches any lights on at night and off at daybreak, so creating the impression that the house is occupied at all times, particularly during the evenings when the intruder is most likely to pay a visit.

The circuitry is contained in a weatherproof housing with a fixing bracket and consists of a highly sensitive photocell and a specially designed bimetal relay.

The switch can be used on any landing or porch, in the garage, as a child's nightlight, and possibly used for automatically switching on a small electric fire (1kW) in a bedroom.

SHORT-CIRCUIT DETECTOR

Detecting and localising short-circuits in any cable form is always a bugbear that causes time consuming delays in servicing work, and any apparatus that eases this problem is always to be welcomed. To help relieve this problem I.T.T. Modular Electronics Division (formerly known as S.T.C.) is now marketing a Swiss short-circuit detector in the U.K.

It is claimed that the detector localises short-circuits rapidly and enables these particular faulty cables to be identified from among many others. Also, it is claimed that concealed cable runs, in pairs, can be traced in concrete to a depth of 30cm.

The detector comprising a probe, transistor amplifier and headphones, operates in conjunction with a transistor oscillator generating a fixed frequency of approximately 1,400Hz. The oscillator is attached to the cable run; the probe is then moved along the cable, being kept as close as possible and with its axis in the direction of the magnetic field, detecting the oscillator output tone in

a pair of headphones. When the short-circuit is reached the tone falls away to practically zero, indicating the point of failure in the cable.

Two output voltages are available from the oscillator, for use as determined by the nature of the short circuit path. The loudness of the tone in the headphones can be adjusted to suit aural conditions.

The I.T.T. short circuit detector costs £25 17s 6d; the oscillator can be provided as an extra at £12 12s. Both units are available through I.T.T. Electronic Services, Edinburgh Way, Harlow, Essex.

CONNECTORS

The 159 series of multi-way connectors from Painton Co. Ltd., has now been modified and redesigned to give better and more robust working. The solder tag connections have been modified and the mouldings improved to give greater resistance to any displacement due to vibrations.

The connectors are manufactured with 7 to 71 poles and a descriptive leaflet number PS10 is available from Painton Co. Ltd., Kingsthorpe, Northampton.

One of the ideal applications for these connectors will be to connect the P.E. Organ foot pedals to the main console.

SWITCH KIT

Intended mainly for engineers, but ideal for experimenters and educational laboratories is the Print Switch kit from Plessey. Practically any multiple arrangement of rotary switching can be set-up, and pre-production samples made in a very short period of time.

The switch consists of a special printed circuit wafer, lightweight

rotor, precious metal faced contacts and an arrangement of dual compression springs and rollers for indexing. The printed circuit wafer allows numerous switch configurations to be obtained by simply removing any unwanted interconnections with a special hand tool, provided with the kit. Contacts press-fit into the moulded rotor in one of 12 switch positions, the assembly being attached to the board by a retainer. Side plates up to 10in depth are available and will accommodate wafers at multiples of 0.2in pitches.

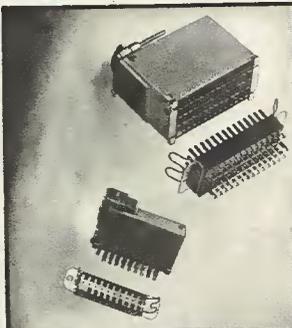
The kit is packaged in a case with full instructions and cost approximately £35. Further details of the PrintSwitch kit can be obtained from Plessey Co. Ltd., Professional Components Division, Abbey Works, Titchfield, Hampshire.

NEW ADDRESSES

The well-known component specialists Home Radio have moved into larger premises just a short distance from their original shop in Mitcham. The name of the business has at the same time been changed to Home Radio (Components) Ltd.

With more space at their disposal, an even larger range of components can now be stocked and no doubt this expansion will be reflected in the next issue of their catalogue. Personal shoppers and mail order shoppers should note the new address: Home Radio (Components) Ltd., 234-240, London Road, Mitcham, Surrey.

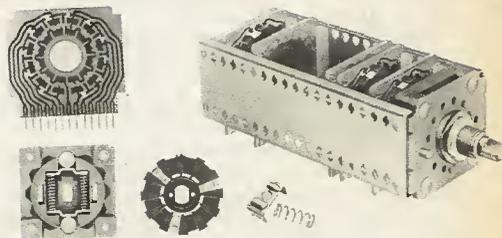
Another company which has also moved house due to recent expansion is S.D.C. Products (Electronics) Ltd. All future orders for their well-known "breadboard" systems should now be addressed to S.D.C. Electronics (Sales) Ltd., 34, Arkwright, Astmoor Industrial Estate, Runcorn, Cheshire.



Painton multi-way connectors



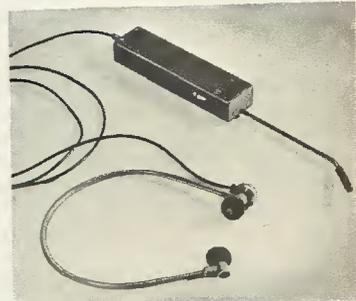
Photo-electric switch made by Andrew Stephens



PrintSwitch from Plessey Components Division



I.T.T. Oscillator and short-circuit detector





BOOK REVIEWS

VHF-UHF MANUAL

By G. R. Jessop, C.Eng., MIERE, G6JP
Published by the Radio Society of Great Britain
244 pages, 9½ in × 6½ in. Price 21s

THE interest of amateur radio enthusiasts in the v.h.f. and u.h.f. fields is ever growing and, with the increasing "overcrowding" of the lower frequency bands, this trend is very likely to continue.

Much of the equipment employed by amateur operators using these bands is home constructed and this book has been published with the intention of giving "a wide range of material for each of the bands, so the constructor has a selection of designs from which to choose—together with a suitable amount of basic information on general matters."

The result is a concisely written manual which covers a wide range of basic information such as; propagation and the effects of weather; details of equipment for mobile users; single sideband equipment; a comprehensive chapter on various aerials, giving polar diagrams, discussing feeders, impedance matching and giving constructional details.

The final chapter is entitled "Aerial Test Gear and Accessories" and comprises such items as reflectometers, power meters, grid dip oscillators and power supplies.

Both transistor, valve and hybrid circuits of transmitters and receivers are given and layout diagrams and photographs of equipment are shown.

In all a manual that no operative v.h.f. or u.h.f. amateur should be without—a worthy addition to the range of RSGB publications.

M.K.

POPULAR ELECTRONICS AND COMPUTERS

By F. G. Rayer, A.I.E.R.E.
Published by Arco Publications Ltd.
190 pages, 8½ in. × 5½ in. Price 36s

THE choice of title for this book is perhaps unfortunate, because the only part describing computers is chapter nine (16 pages), and even then in such condensed elementary detail to be hardly worth advertising in the title at all.

A larger part is devoted to radio in its many facets, about which the author is best known. Indeed, he has written other books on this subject.

No newcomer to electronics can complain of a lack of books on basic theory, and it is becoming all too common for electronics and radio books to be prefaced by several chapters of the same kind of details, from atoms to amplifiers, from electrons to a.c. theory. This one does not deviate from this course, and one is led to ask how much are we really getting for our money on popular electronic circuits and computers.

All the more puzzling is the cramming of a wide range of subjects in only 190 pages, none of which is really given justice in its description. Had the first 72 pages of basics been dropped, the space could have been more usefully spent on more satisfying descriptions of the other subjects, not least being the computer section.

M.A.C.

MEETINGS

INSTITUTION OF PHYSICS AND THE PHYSICAL SOCIETY

LONDON

July 2-4. Conference on *Lasers In Medicine*, Chairman Prof. O. S. Heavens, at The Medical School of Middlesex Hospital, London, W.1.

Further details, time of conference and registration forms available from The Meetings Officer, 47, Belgrave Square, London, S.W.1.

SOCIETY OF ELECTRONIC AND RADIO TECHNICIANS

EVESHAM

July 4-7. Symposium on *Maintenance In Electronics* at Wood Norton Hall, Evesham.

The inclusive charge for this residential symposium is fifteen guineas for members and nineteen guineas for non-members. Further details and registration forms are available from the Secretary, Faraday House, 8-10, Charing Cross Road, London, W.C.2.

LONDON RADIO CONTROLLED MODELS SOCIETY

LONDON

July 10, 7.30 p.m. *General Discussion*, at The Two Chairmen, Dartmouth Street, London, S.W.1.

Further details from the Secretary, H. C. Farley, 24, Dacre Crescent, Kimpton, Hitchin, Herts.

INSTITUTION OF ELECTRICAL ENGINEERS

WARWICK

July 8-10. Conference on *Measurement Education*, at University of Warwick.

Further details, time of conference and registration forms available from The Secretary, I.E.E., Savoy Place, London, W.C.2.

MULLARD MEETINGS

The 1969/70 season of Mullard meetings for the radio and television trade opened at Southampton on May 5. This year's talk is devoted to integrated circuitry. Between now and the end of April 1970 it will be given at 76 centres in the U.K.

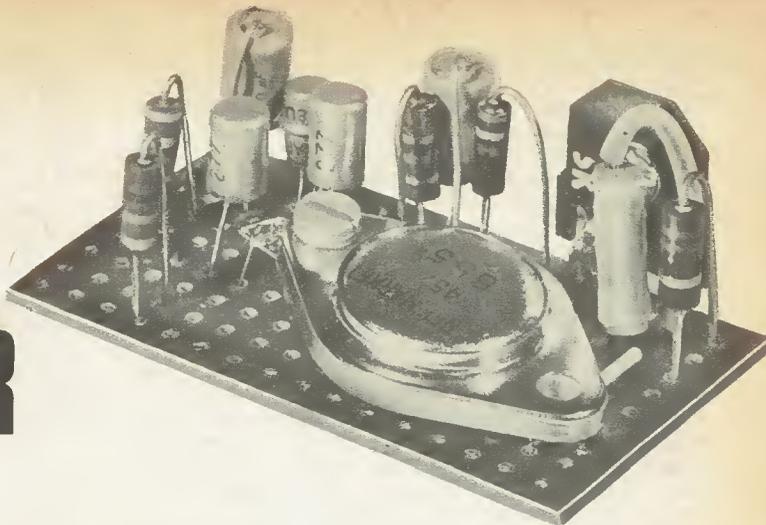
Apart from members of the retail trade, these meetings are attended by representatives of many other branches of the electronics industry, students from technical colleges, and also amateurs who are interested in the latest technical developments.

The programme for June and July is as follows:

- June 17. Five Bridges Hotel, Gateshead, Durham.
- 18. County Hotel, Carlisle, Cumberland.
- 23. Grosvenor Restaurant, Glasgow.
- 25. George Hotel, Edinburgh.
- July 1. City Cafe, Londonderry, N. Ireland.
- 3. The King George VI Youth Centre, Belfast, N. Ireland.
- 9. Dolphin Hotel, Swansea.
- 10. Park Hotel, Cardiff.

All meetings commence at 7.45 p.m. and readers wishing to attend any of these meetings should apply for tickets to Mr Ian Nicholson, Films and Lectures Organisation, Mullard Ltd., Mullard House, Torrington Place, London, W.C.1.

SERIES VOLTAGE REGULATOR



THIS unit gives a stabilised output voltage from an unstabilised input. The output can be varied between approximately 7 and 12 volts, at currents up to approximately 400mA, or up to 1A if the output transistor is mounted on a heat sink.

The unit may be used on its own, or made up into a bench mounted variable voltage stabilised supply, or it may be built into additional equipment, such as test gear. As well as giving a stabilised output, the unit acts as a smoothing circuit, giving a considerable reduction in ripple from the unstabilised input.

BASIS OF OPERATION

When discussing voltage regulators, it is advisable to lead up to the final circuit in a number of progressive stages, and this approach will be adopted here.

A very simple form of voltage stabiliser is shown in Fig. 1a. Here, the circuit consists simply of a limiting resistor (R_1) wired in series with a Zener diode (D_1). The unstabilised input is applied across this combination, and the stabilised output is taken from across the Zener diode.

This circuit has a number of applications, but suffers from severe disadvantages: the output power is very limited (unless large—and expensive—Zener diodes are

used); the output voltage is not variable; the output voltage varies (by a small amount) with changes in input voltage.

Fig. 1b shows an improvement on this basic circuit. Here, TR_1 is wired as an emitter follower, with its base fed from the stabilised Zener diode output. The emitter of an emitter follower tends to "follow" very closely the voltage on its base; thus, the voltage on the emitter of TR_1 tends to remain almost the same as that across the Zener diode, irrespective of the current flowing in TR_1 emitter. R_z , in the emitter of TR_1 , represents the output load seen by this regulator.

This circuit has the advantage that the output power is handled by TR_1 , and negligible power need be handled by the Zener diode D_1 . Disadvantages are: the output voltage is not variable; the transistor has an output impedance of several ohms, so that the output voltage will vary by a certain amount with the output current; and the output voltage is not fully stabilised.

This improved circuit can be made to give a variable output voltage by wiring a variable resistor (VR_1) across the Zener diode, as in Fig. 1c, and connecting the base of TR_1 to the moving arm of VR_1 . The main disadvantage of this modified circuit is that the output impedance is still quite high.

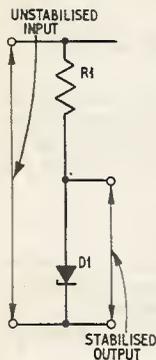


Fig. 1a. Basic regulator circuit

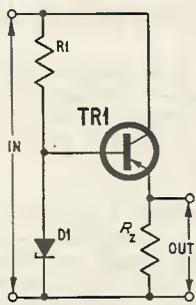


Fig. 1b. Higher output basic regulator

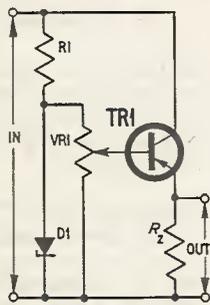


Fig. 1c. A variable version of 1b

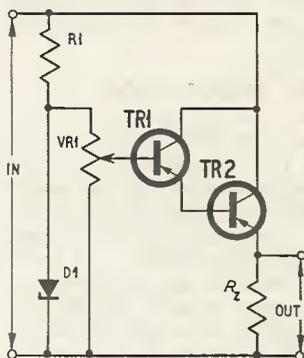


Fig. 1d. Series regulator using a super-alpha pair

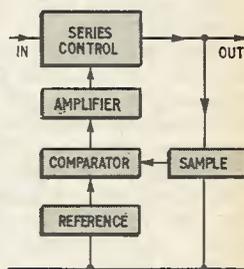


Fig. 1e. Block diagram of a feedback system for voltage regulation

Resistors

- R1 3.3k Ω
- R2 1.8k Ω
- R3 22 Ω
- R4 6.8k Ω
- R5 1k Ω $\frac{1}{4}$ W to 220 Ω 1W (see text)
- All $\pm 10\%$, $\frac{1}{4}$ W carbon except where stated

Potentiometer

- VR1 5k Ω skeleton pre-set

Capacitors

- C1 50 μ F elect. 15V
- C2 16 μ F elect. 15V
- C3 50 μ F elect. 15V

Semiconductors

- TR1 NKT277
- TR2 NKT277
- TR3 NKT405
- DI Any 6.8V Zener diode

Miscellaneous

- Veroboard
- 4B.A. fixings
- P.V.C. covered wire

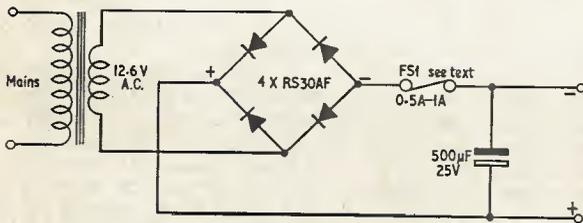


Fig. 4. Circuit of a suitable power supply for use with the series voltage regulator

just slightly warm under any given set of operating conditions, the design is satisfactory. Using a heat sink of about 7in \times 7in, currents up to 1A can be handled.

If the unit is to be used under constantly loaded conditions, R5 can be left out of the circuit. When the regulator is to be used only occasionally as a general purpose power supply under variable load conditions, R5 can be made 1 kilohm. If the unit is to be made into a general purpose bench mounted power supply, R5 should be made 220 ohms or less.

USING THE REGULATOR

The unit is perfectly simple to use, it being necessary merely to connect an unstabilised 18V supply to the input and take the stabilised output from the lead connected to TR3 emitter.

The input voltage is in no way critical, as long as it is a few volts greater than the required stabilised voltage. The input voltage does not have to be particularly well smoothed.

As a safety precaution, a fuse should be inserted in the unstabilised supply circuit. The fuse should be 500mA maximum if the power transistor is to be mounted on the Veroboard panel, and 1A if TR1 is to be mounted on a heat sink. A suitable circuit for the unstabilised power supply is shown in Fig. 4. ★

NEWS BRIEFS

Fifteenth International V.H.F.-U.H.F. Convention

THE FIFTEENTH V.H.F.-U.H.F. Convention was held on April 26 at the Winning Post Hotel, Whitton. The Convention, organised by the RSGB, was attended by some 260 members—a slight increase on last year's attendance.

An exhibition of home constructed equipment was the centre-piece in the "display" hall and this was surrounded by various commercial firms' stands and a selection of RSGB publications which included the new V.H.F.-U.H.F. Manual (see *Book Reviews*).

During the afternoon some seven lectures were held in rooms adjoining the display and later in the evening the convention dinner was served in the largest of the rooms. During the after-dinner speeches, members of the RSGB were urged by Colonel I. St. Q. Severin O.B.E., of the Cabinet Office, to "use or lose" those frequency bands allotted them by the GPO. The Convention closed with the presentation of the V.H.F. Committee Cup to Mr D. Dall G5AHK for his entry in the amateur constructed equipment display, and the G5RV Trophy to Mr R. Ham BRS15744.

Transducer Equipment for N.A.S.A.

THE National Aeronautical Space Administration have recently ordered 40 channels of transducer equipment from the Wayne Kerr Corporation in the U.S.A.

The system is positioned in the instrument capsule of the Saturn Rocket being used in the Apollo programme and will measure the position of vital components to within a few millionths of an inch. The eight measurement channels will relay vital mechanical information back to earth whilst the rocket is in orbital flight.

Design Awards Presented Aboard QE2

HIS Royal Highness The Prince Philip, Duke of Edinburgh, presented the 1969 Council of Industrial Design Awards, together with his own prize for Elegant Design, on board the new Cunard *Queen Elizabeth 2* at Southampton on Thursday, May 29.

The photograph below shows a "Vision Comparascope", made by Vision Engineering Ltd., being used for inspecting a printed circuit panel. The Comparascope is the winner of this year's Capital Goods Section and is designed to compare the object to be checked with a master. Images of the two objects (that being checked and the master) are accurately superimposed on one another in such a way that the operator sees in sequence the master object and the object being checked. Thus any difference between the two "winks" at the operator as it appears and disappears.



Report from AUSTRALIA

BY D. F. MOODY



WHO wants to be taught by T.V.? I must admit that the thought does not appeal to me at all. I remember my school days with a sort of "glow"—that warm, learned feeling when staying behind to talk over a particularly interesting topic, with the chalk dust lingering in the air. Where would all this be with teaching machines and educational television?

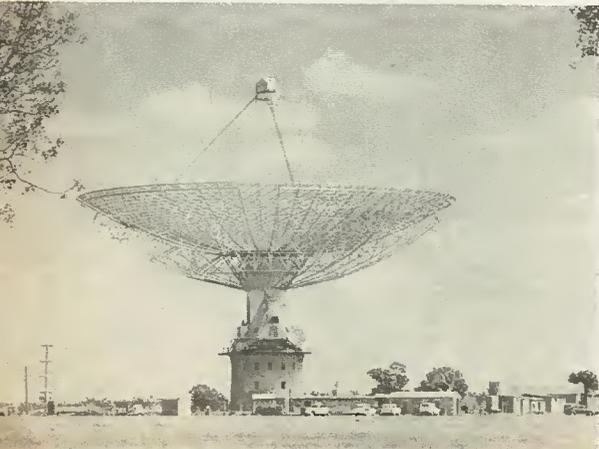
OUTBACK RADIO

The facts are though that here in Australia, and all over the world, there is a growing teacher shortage, classes are getting bigger and more unmanageable, and educational authorities are looking to electronics to solve their problems for them. I gather that it will not be long now before all the colleges of London University will be hooked up into a common closed circuit television network.

In Australia, remoteness rather than overcrowding is more of a problem, and this is overcome by the use of radio as much as possible. For example the University of New South Wales has recently begun transmitting lecture material through its own radio station to registered students in remote areas. Of course, the "outback" has had a radio system operating for over thirty years now. The system—The Royal Flying Doctor Service—is well known, and covers an area of over 1½ million square miles and, from fourteen base stations, provides the isolated communities of this area with a medical, educational and social service.

Probably the medical service is the more commonly known one outside of Australia. The Darwin radio station, for example, transmits medical schedules twice each day. In these "medical skeds", a doctor prescribes treatments to patients scattered over thousands of square miles, with aircraft standing by to bring to hospital those too ill for distant treatment.

The New South Wales radio telescope, one of many situated throughout Australia, used for satellite tracking and space communications



There are nearly 6,000 homestead transceivers and, in communities where it is not possible or desirable for children to be sent away to school, these sets are used in the so-called "Schools of the Air". A typical set up is with about seventy transceivers hooked up together through a base station. Thus the teacher at the base station is able to talk to all the seventy or more children at once, and they are able to talk back, both to the teacher and to one another. These radio lessons are also supplemented by correspondence courses.

These transceivers (which are locally known as "pedal radio" from the early form of set which was powered by a pedal) also provide isolated homesteads with some form of community life, with such organised activities as "Brownies of the Air", and a daily "galah" or gossip session for the womenfolk.

Although this network is of vital importance to the lives of the outback inhabitants, it is only a drop in the ocean compared with the other uses of the radio spectrum. But surely it would be most satisfying to Marconi's ghost to find that here true use is being made of radio communication for the benefit of man. I don't know what he would think if the use of his invention was solely limited to supplying entertainment for the over indulged masses.

SPACE IN AUSTRALIA?

Sure there is space in Australia! It is some 20 times the area of the U.K. and has only 20 per cent of the population.

However, the sort of space I'm referring to is deep space, and it may not be realised that Australia has a growing interest in this activity. Apart from the planned radio-telescope, which will be one of the largest in the world, Australia has six NASA space-tracking and communication stations, which places her second only to the United States.

Concerned mainly with tracking, reception, and command signalling of satellites and deep-space probes, these stations provide NASA with essential elements of their world wide Space Tracking and Data Acquisition Network (STADAN). They are staffed by Australians, and require a total of 800 engineers, technicians and supporting staff.

Why is Australia so interested in satellite technology? Because it holds the solution for providing Australia with high capacity international telephone and television links, and for providing the sparsely populated areas with a television service, when direct transmission from satellites to home receivers becomes a practical proposition. It would then be possible to provide an educational television service to everyone in Australia, no matter where they lived.

Who would want to be taught by television? I guess I would.

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For 12 to 16 ohms—Price 20/-, p.p. 2/-.

★ SPRING REVERBERATION UNITS

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Model **HR162**, 8in overall, 35-40msc delay, Price £6.10.0.

★ GRID DIP METER

All transistor grid dip meter, absorption wavemeter and osc. detector. Frequency range 440kc/s to 280Mc/s in 6 coils. Uses 3 transistors plus diode with 500µA meter. Internal battery. **TE15, Price £11.10.0.**



★ FIELD STRENGTH METER

Covers 1-250Mc/s. Switches for model control and any application requiring peaking of transmitters and oscillators. 100µA meter. Complete with aerial. **FS1, Price 45/-.**



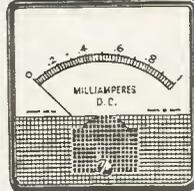
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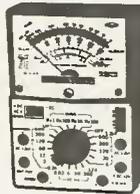
TO3 SCOPE £35, p.p. 10/-.

★ QUALITY PANEL METERS

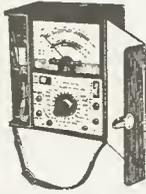


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65 Series. Face size 86 x 78mm (3½ x 3in). 50µA, 62/6; 100µA, 52/6; 200µA, 47/6; 500µA, 45/-; 1mA, 5mA, 10mA, 50mA, 37/6 each. "S" meter, 1mA, 42/6. Other ranges and sizes available. Complete list on request.

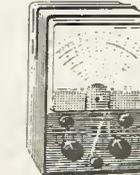
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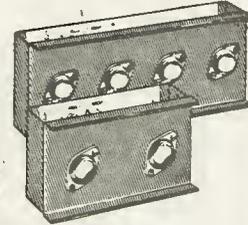
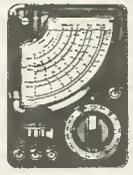


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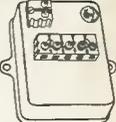
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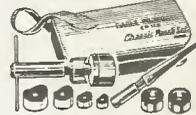
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EXPERIMENTS WITH THE OPERATIONAL AMPLIFIER

By G. K. FAIRFIELD

Part 2 Measuring small currents and voltages, waveform generators

LAST month's article discussed the theory of the operational amplifier and suggested a few uses of the device concerned with the measurement of component values. Due to its very high input impedance the operational amplifier can also be adapted for the measurement of very small currents and voltages.

MICROVOLT/MICROAMP D.C. METER

The d.c. measuring circuit is given in Fig. 2.1. For high accuracy the two resistors R1 and R2 should be high stability types having an accuracy of ± 1 per cent.

With input circuit A the instrument behaves as a millivolt meter having a full scale sensitivity of ± 3 mV. The sensitivity can be decreased by a suitable setting of potentiometer VR1.

Since a standing d.c. is often superimposed on small changes of voltages we require to measure then a backing-off potentiometer VR3 is included. This allows a very small current $\pm i$ to be applied to the summing junction of the amplifier via a high resistance R3 which will be sufficient to back off any small d.c. present at the input terminals.

Where the operational amplifier used is itself subject to a small voltage offset, or d.c. drift, then the adjustment of VR3 will enable this to be compensated. The positive and negative supplies (which are not at all critical) can be obtained from the operational amplifier power supply.

For use as a microammeter, input circuit B is used. This permits full-scale measurements of 0-30m μ A at its maximum sensitivity. This circuit requires rather more components than those discussed last month, but its construction is considerably quicker than its conventional counterpart for this order of sensitivity.

Of course, when measuring such small electrical values it is necessary to avoid 50Hz mains pick-up at the input. Consequently screened leads are recommended up to the input of the amplifier including the leads to the input attenuators.

OSCILLOSCOPE ACCESSORIES

Accurate mixing of several signals can be made using an operational amplifier with several input resistors as shown in Fig. 2.2. This technique is useful to determine the time coincidence of two waveforms, such as the incidence of a repetitive fault in the television scanning circuit, and to show its relationship with its synchronising waveform.

The identification of the separate waveforms, when they are added together in this way, is facilitated if one of these is made negative so that the output of the operational amplifier represents the difference and not the sum of the two waveforms.

With triggered oscilloscopes it is often required to commence the scan at a time when a waveform reaches a pre-determined voltage value. Assuming that the

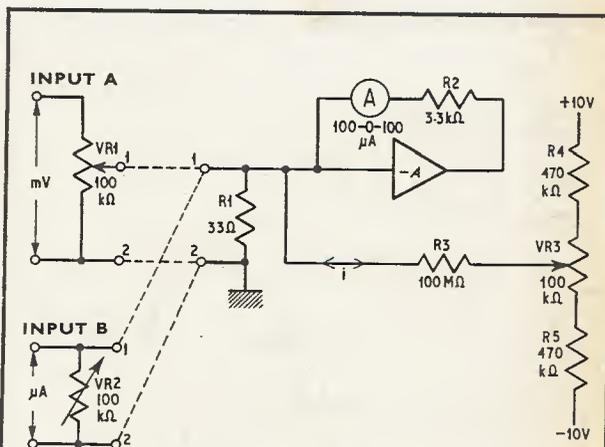


Fig. 2.1. D.C. meter for measuring microvolts and microamps

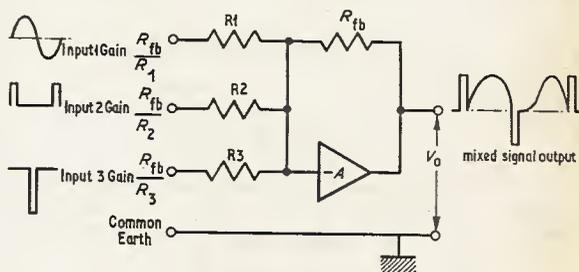


Fig. 2.2. Oscilloscope mixer amplifier circuit

oscilloscope needs a positive trigger pulse (which is generally the case) then the circuit to achieve this is given in Fig. 2.3.

As long as V_1 is very much greater than V_2 then the output of the operational amplifier is negative and the scope is not triggered. As soon as the trigger voltage V_2 reaches the value set by V_1 then a positive output level is obtained.

By using an operational amplifier with no feedback resistance as shown then its high gain will cause a very sharp transition between negative and positive output voltages to be obtained. This will provide a very definite triggering level for the oscilloscope.

TIMING DELAY CIRCUIT

A time delay circuit is often required in electronic equipment—a common example is a photographic process timer to fix the period of exposure during the printing process. Once again an operational amplifier can be made very quickly into a time delay circuit. In addition to the amplifier, a fixed resistor, a capacitor, a potentiometer, a low current relay and a starting switch (which may be included in the photographic or other equipment are required). The very simple circuit is shown in Fig. 2.4.

The potentiometer VR1 is set at the delay value required. Switch S1 is then opened and the capacitor C1 is charged from the operational amplifier power supply at a rate determined by the value of R_1C_1 and the setting of potentiometer VR1. After a given time t the

operating voltage for the relay is reached and its contacts are closed to control the desired apparatus. The time delay is given by

$$t = R_1C_1 \frac{V_r}{V_s} \text{ seconds}$$

In order to obtain some practical delay figures, let us assume that a 50V relay is available. The actual voltage is not important providing the current it draws does not impose too great a load on the operational amplifier. Generally the amplifier will be able to supply a current of about 10 to 20mA.

With C1 fixed at $1\mu\text{F}$ (paper) and R_1 $1\text{M}\Omega$, then the rate of rise of voltage across the relay will be 10V per second with the potentiometer set at maximum. Therefore the minimum delay will be $50/10 = 5$ seconds.

As the setting of VR1 is reduced then the delay is lengthened up to a maximum of about 250 seconds. The longest delay obtainable will depend on the stability of the amplifier and the leakage of the capacitor. Table 2.1 shows how the time delay range varies with the time constant (R_1C_1 value).

Table 2.1: TIME DELAY VALUES

Delay range (seconds)	R_1	C_1
0.5– 25	$100\text{k}\Omega$	$1\mu\text{F}$
5 – 250	$1\text{M}\Omega$	$1\mu\text{F}$
50 – 2,500	$1\text{M}\Omega$	$10\mu\text{F}$

Mathematically we can describe this circuit as an integrator.

Again assuming

$$i_i = 0$$

then

$$i_s = V_s/R_1 \text{ (see Part 1).}$$

The output voltage developed across C_1 as a result of its charge Q is:

$$V_o = \frac{Q}{C_1} = \frac{1}{C} \int i_s dt$$

Substituting for i_s we obtain

$$V_o = \frac{1}{R_1C_1} \int V_s dt$$

Differentiating

$$\frac{dV_o}{dt} = \frac{V_s}{R_1C_1}$$

Thus the delay t , for a given relay voltage V_o is

$$t = \frac{V_o}{V_s/R_1C_1}$$

SQUARER

The operational amplifier can permit a number of interesting waveform generators to be constructed which are useful for triggering or experimental work.

Let us consider first the squaring of the output of a sine wave oscillator. For this we need two germanium or silicon diodes, a fixed resistor, two potentiometers and the operational amplifier. The circuit is given in Fig. 2.5.

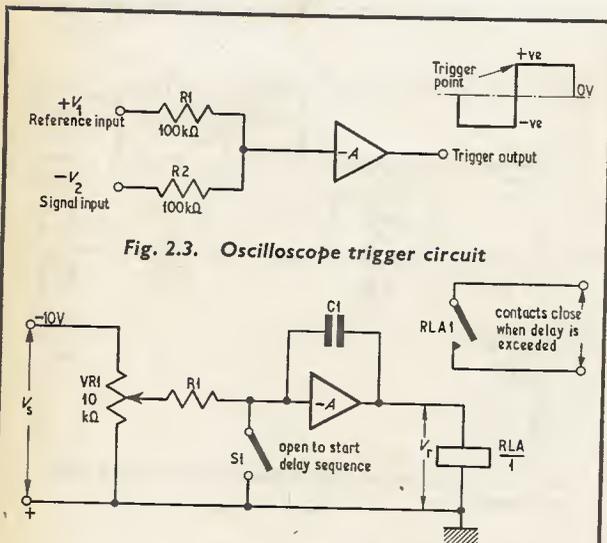


Fig. 2.3. Oscilloscope trigger circuit

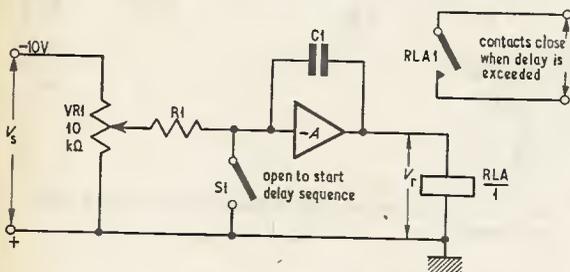


Fig. 2.4. Time delay circuit

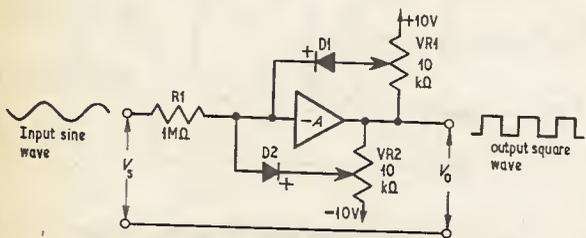


Fig. 2.5. Waveform squaring circuit

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A 6 Germ. V.H.F. PNP T0-1 = AF116-7, KNT667, 2G417	£3.10	£15	£25	£200
A 7 Assorted Germ. A.F.-R.F. PNP mixed cans, general purpose	15s.	£2.10	£4	£32
A 8 Germ. A.F. 50-2 PNP = 2G371-89, ACY27-31, OC71-75	£2	£7.10	£12.10	£100
A 9 Sil. Alloy PNP T0-5 = 2S301-5, BCY17-29, BCY30-34	£2	£7.10	£12.10	£100
A 10 Sil. Alloy PNP 50-2 = 2S321-325, OC200-205	£2	£7.10	£12.10	£100

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 - SN7430N—3-input Positive NAND Gate
 - SN7440N—Dual 4-input Positive NAND "Power" Gate
 - SN7450N—Dual EXCLUSIVE-OR Gate with Expander Inputs
 - SN7451N—Dual EXCLUSIVE-OR Gate
 - SN7472N—Master-slave J-K Flip-flop
 - SN7473N—Dual Master-slave J-K Flip-flop
 - SN7474N—Dual Latch
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BC109	2N697	2N1613	2N3707	2N3391
BFY50	2N706	2N1711	2N3711	T1544
BFY51	2N708	2N2904	25102	2N2906
BFX84	2N929	2N2905	25103	2N2907
BFX86	2N930	2N2924	25104	2N2696
BFX88	2N1131	2N2926	25732	2N3702
				2N3703

From Manufacturers' Over-runs—Unmarked Plastic and Metal cases. Devices similar to above Nos.

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AC126	ACY27	NKT141	NKT713	OC82	2G382
AC127	ACY28	NKT142	NKT773	2G301	2G399A
AC128	ACY29	NKT212	OC44	2G302	
AC130	ACY30	NKT213	OC45	2G303	
ACY19	ACY31	NKT214	OC71	2G308	
ACY20	ACY34	NKT215	OC72	2G371	
ACY21	ACY35	NKT271	OC75	2G374	

1/6 each

POWER TRANSISTORS

OC25	OC35	NKT403	AS217	5/-
OC26	AD130	NKT404	T13027	each
OC28	AD140	NKT405	T13028	
OC29	AD149	NKT452	T13029	

Manufacturers' Surplus Germ. A.F. All similar to above.

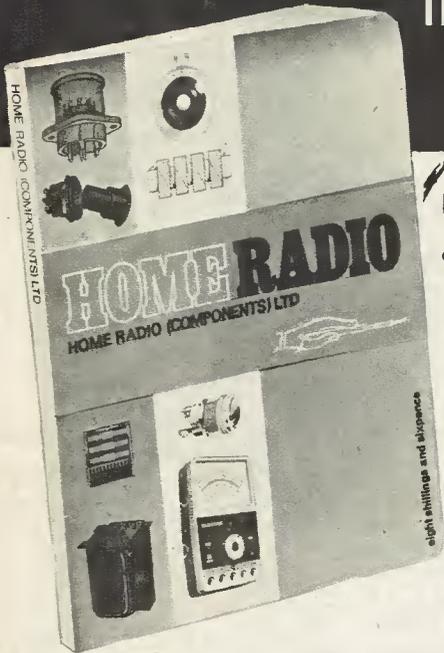
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Type No.	PIV	Each
IN4001	50	1/3
IN4002	100	1/6
IN4003	200	2/-
IN4004	400	2/9
IN4005	600	3/3
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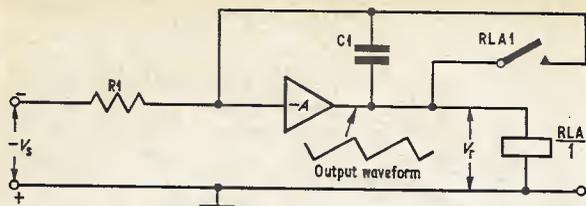


Fig. 2.6. Sawtooth waveform generator

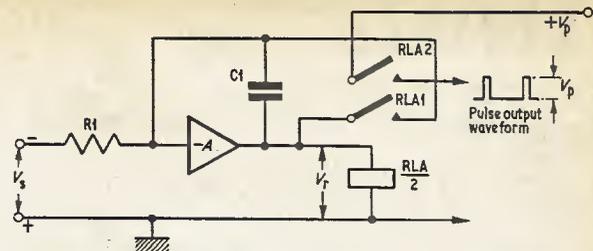


Fig. 2.7. Pulse generator

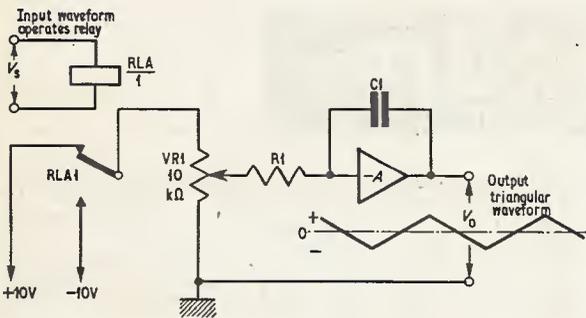


Fig. 2.8. Triangular waveform generator

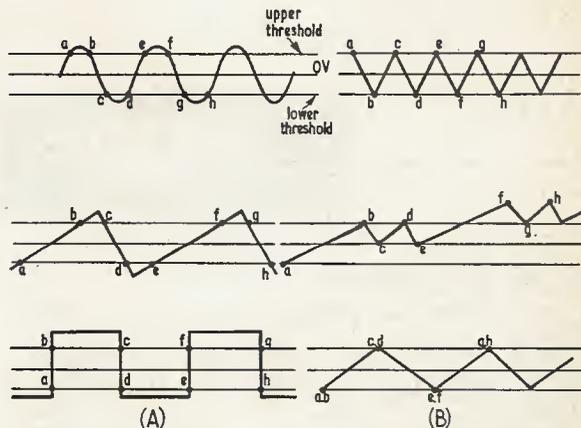


Fig. 2.9. Input and output waveform for the circuit in Fig. 2.8. Input waveform is shown left (A), and output waveform from amplifier is shown right (B)

The two potentiometers are set to give the required amplitude of the square waveform. The input sinusoidal waveform must have an amplitude greater than this.

The action of the diodes effectively prevents the output from becoming greater in amplitude than the setting of the potentiometers, since when either diode conducts, a low feedback resistance (actually the forward impedance of the diode) is shunted across the operational amplifier. As shown by the equation for gain derived in Part 1, the overall gain falls to a very low value indeed.

If a symmetrical waveform is not required it is easy to arrange either a positive or negative going square wave to be produced by setting one of the potentiometers to zero.

This same circuit could also be used to clamp a given incoming signal to a particular level set by VR1 or VR2.

SAWTOOTH WAVEFORM

To generate a free-running sawtooth waveform a capacitor, resistor, and a low current relay can be connected to the operational amplifier to form the circuit given in Fig. 2.6.

The operational amplifier with its feedback forms an integrator circuit and the value of the time constant determines the frequency of the sawtooth waveform, given by

$$f = \frac{V_r}{V_s C_1 R_1} \text{ Hz}$$

where R_1 is in megohms, C_1 in microfarads, and the input V_s and relay V_r voltages are in volts.

When a negative voltage V_s is applied to the input of the circuit, capacitor C_1 begins to charge through the input resistance R_1 . As it does so the voltage across the capacitor begins to increase and the feedback action works to slow down the rate of charge.

Consequently, instead of a non-linear (strictly speaking, an exponential) voltage change appearing across the capacitor, and hence the amplifier output, a very linear rise of voltage is obtained. This is because the reduction of charging current exactly cancels out the non-linearity.

When the output voltage reaches the relay operating voltage then the capacitor is short-circuited by the action of the relay contacts and the cycle repeats once more, when the voltage across the capacitor becomes zero again.

The highest frequency of operation is limited, of course, by the speed of response of the relay. Modern relays are capable of operating in as little as one millisecond so that frequencies of several hundred hertz can be generated in this way.

PULSE CIRCUIT

This sawtooth generator circuit is very adaptable and with the additional pair of contacts on the relay the same circuit can be made to provide a series of narrow pulses, one each time the relay is momentarily operated, and of amplitude V_p volts, at the output (see Fig. 2.7). The fixed d.c. supply is switched by contacts RLA2.

TRIANGULAR WAVEFORM

The integrator circuit can be used to provide a triangular output waveform from almost any shape of input signal. The circuit is given in Fig. 2.8.

The input signal is applied to a low current relay shown in the diagram. This relay will be operated when the input signal exceeds the operating voltage of the relay.

A changeover pair of contacts are required to change the input voltage to the integrator from positive to negative whenever the relay is energised. Consequently the capacitor is alternatively charged in opposite directions as the relay changes. This results in a linear rise and a linear fall of voltage at the output as described in the previous section.

If the input signal is twice the amplitude of the relay operating voltage then a symmetrical triangular waveform is generated as shown in Fig. 2.8. The amplitude of the triangle is set by potentiometer VR1 since this controls the rate of rise of the charge applied to the capacitor.

The waveform of the signal input voltage operating the relay is unimportant as long as it is able to exceed the relay operating voltage during some part of its voltage excursion. A 50Hz signal from the mains would be quite adequate and result in a triangular waveform of this frequency. A number of different input waveforms are shown in Fig. 2.9 with their resulting triangular output waveforms.

Next month: Further applications and operational amplifier circuit design.

NEWS BRIEFS

The Late John Clarricoats, O.B.E., G6CL

A WELL-KNOWN personality in the radio amateur world, John Clarricoats, joined the Radio Society of Great Britain in 1925, was elected honorary secretary in 1930 and became the full-time secretary in 1932, a post which he held until his retirement in 1963. He died March 1969.

During his term as secretary "Clarry", as he was known by his many friends, was greatly in demand as a guest speaker at local RSGB group functions. He also did much to explain the purpose of the amateur radio movement to the general public and served on numerous bodies including the IARU. He was awarded the O.B.E. in 1955 and was elected an honorary member of the RSGB in 1963.

Mains Colour Code Changes

ON July 1 the colour coding of three-core mains cables is to be changed to comply with the new International Standard. The present coding of green for earth, black for neutral, and red for live on a.c. mains will become:

- LIVE—Brown
- NEUTRAL—Blue
- EARTH—Yellow and green stripes

In spite of what many consider to be an illogical move, there are reasons for the new choice. The new earth colours can be picked out easily in poor light or by the colour blind; the other two are sufficiently separated in the colour spectrum for one to be lighter than the other.

It is also claimed that blue and brown are the only colours which do not fade when impregnated in p.v.c. and are also cheap.

It is expected that by Spring 1970 it will be illegal to sell appliances with the old colour coded cables, although this has yet to be established.

Computer Controlled Telephone Exchange

A COMPUTER-CONTROLLED telephone exchange system, believed to be unique anywhere in the world, is being developed by Plessey Telecommunications Group under a multi-million pound programme spread over the next few years.

Other computerised or stored programme control (SPC) systems under development are based on a massive centralised processor—similar to a computer—which

signals instructions to the telephone switching equipment. This method can increase costs substantially when, in order to guard against breakdown, a second or even a third standby processor needs to be installed.

Plessey plans to overcome these problems by introducing a system incorporating a plurality of smaller processors which will not only reduce capital cost but will also make the system more flexible and easier to extend.

Radar Systems

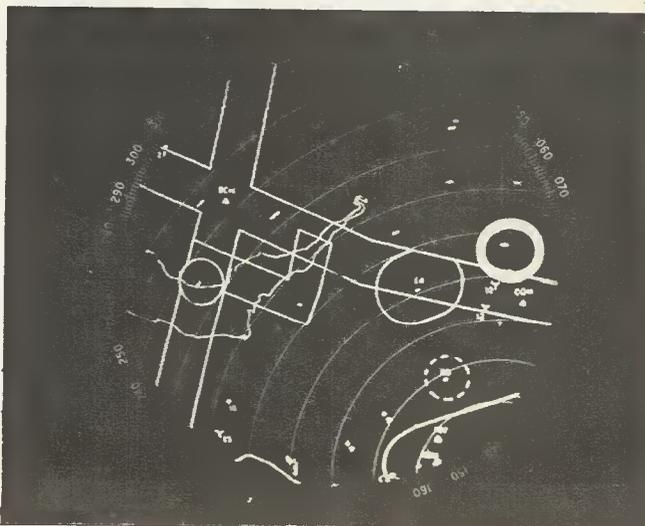
TWO NEW Plessey radar systems have been introduced recently. They are the WF44—an advanced meteorological radar—and the AR-5—a 23cm air surveillance system.

Orders for the type WF44 have been placed by the Australian Department of Supply for use by the Commonwealth Bureau of Meteorology, Melbourne.

The new radar is designed to operate in both windfinding and weather-watching roles.

Two type AR-5 radars have been ordered by the Board of Trade for installation at Burrington, Devon, the key West Country station in the chain providing en route cover for the UK's national air traffic control system.

The AR-5 can provide range cover of 200 nautical miles or more and height cover up to 80,000 feet. Shown below is a photograph taken from the screen of the prototype AR-5 installed at Plessey Radar's test and demonstration site at Cowes, Isle of Wight. The white circle encloses Concorde 002 during its maiden flight.



NEW PRICES ON NEW COMPONENTS

RESISTORS

High stability, carbon film, low noise. Capless construction, molecular termination bonding.
Dimensions (mm): Body; $\frac{1}{4}$ W; 8 : 2.8
 $\frac{1}{2}$ W; 10 : 4.3

Leads;		35			
10% ranges; 10 Ohms to 10 Megohms (E12 Renard Series)		5% ranges; 4.7 Ohms to 1 Megohm (E24 Renard Series)			
Prices—per Ohmic value.					
$\frac{1}{4}$ W	10%	each	10 off	25 off	100 off
$\frac{1}{4}$ W	10%	2d	1/6	3/3	10/4
$\frac{1}{4}$ W	5%	2 $\frac{1}{2}$ d	1/9	3/8	11/8
$\frac{1}{4}$ W	10%	2 $\frac{1}{2}$ d	1/9	3/8	11/7
$\frac{1}{4}$ W	5%	3d	2/-	4/-	12/10

CAPACITORS

Subminiature Polyester film, Modular for P.C. mounting. Hard epoxy resin encapsulation. Radial leads.
 $\pm 100\%$ tolerance.

100 Volt Working.				
Prices—per Capacitance value (μ F)				
0.001, 0.002, 0.005, 0.01, 0.02	each	10 off	25 off	100 off
0.05	6d	4/3	8/4	30/-
0.1	8d	6/-	12/6	41/8
0.2	10d	7/1	15/6	51/8
0.5	1/2	10/-	20/10	68/6
	2/-	17/6	37/6	125/-

Polystyrene film, Tubular, Axial leads.
 $\pm 5\%$ or $\pm 1\mu$ f tolerance.

Unencapsulated.				
160 Volt Working.				
Prices—per Capacitance value (μ F)				
10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82, 100, 120, 180, 220, 270, 330, 390	each	10 off	25 off	100 off
470, 560, 680, 820, 1,000, 1,500	5d	3/7	7/9	24/-
2,200, 3,300, 4,700, 5,600	6d	4/-	8/8	26/8
6,800, 8,200, 10,000, 15,000	7d	5/-	10/10	33/4
22,000	8d	6/-	13/-	40/-
	9d	6/9	18/-	45/4

Polystyrene film, Tubular, Axial leads. Professional Grade. Hard Epoxy Resin encapsulation.

100 Volt Working.				
$\pm 1\%$ tolerance.				
Prices—per Capacitance value (μ F)—except where stated				
100, 120, 150, 180	each	10 off	25 off	100 off
220, 270, 330, 390, 470, 560, 680, 820	1/3	10/2	21/2	64/6
1,000, 1,200, 1,500, 2,200, 2,700	1/6	10/8	23/1	71/-
3,300, 3,900, 4,700, 5,600	1/9	14/1	29/11	92/-
6,800, 8,200, 10,000, 12,000	1/9	15/2	31/-	96/-
15,000, 18,000	2/-	15/11	32/10	101/-
22,000, 27,000	2/3	17/3	32/10	107/4
33,000, 39,000	2/6	20/1	34/9	115/-
47,000, 56,000	2/9	22/1	37/10	133/9
68,000	3/-	24/9	43/6	147/4
82,000	3/3	26/1	47/10	165/4
0.1 μ F	3/6	27/5	53/8	173/9
0.12 μ F	3/9	30/3	59/4	182/8
0.15 μ F	4/3	34/2	65/10	202/-
0.18 μ F	5/-	37/10	73/7	228/-
0.22 μ F	6/-	47/-	81/11	252/3
0.27 μ F	6/9	53/9	101/10	313/4
0.33 μ F	7/3	58/10	116/8	358/4
0.39 μ F	7/9	65/-	126/11	390/-
0.47 μ F, 0.5 μ F	9/9	75/2	140/10	433/4
			137/7	500/-

POTENTIOMETERS (Carbon)

Miniature, fully enclosed, rear tags, carbon brush wiper. Long life, low noise. Body dia., $\frac{1}{2}$ in. Spindle, $\frac{1}{16}$ in. $\frac{1}{4}$ W at 70°C. $\pm 20\%$ $\frac{1}{4}$ M, $\pm 30\%$ $\frac{1}{2}$ M Lin. 100 Ohms to 10 Megohms, Log. 5 Kohms to 5 Megohms.
Prices—per ohmic value.

GANGED STEREO POTENTIOMETERS (Carbon)				
$\frac{1}{4}$ W at 70°C. Long Spindle.				
Logarithmic and Linear: 5k + 5k to 1M + 1M.				
Prices per ohmic value				
	each	10 off	25 off	100 off
	8/-	70/-	162/6	575/-

SKELETON PRE-SET POTENTIOMETERS (Carbon)

High quality pre-sets suitable for printed circuit boards of 0.1in. P.C.M. 100 Ohms to 5 Megohms (Linear only).
Miniature: 0.3W at 70°C. $\pm 20\%$ below $\frac{1}{4}$ M, $\pm 30\%$ above $\frac{1}{4}$ M. Horizontal (0.7in. \times 0.4in. P.C.M.) or Vertical (0.4in. \times 0.2in. P.C.M.).
Subminiature: 0.1W at 70°C. $\pm 20\%$ below 2.5M, $\pm 30\%$ above.
Prices—per ohmic value

Miniature (0.3W)	each	10 off	25 off	100 off
Subminiature (0.1W)	1/-	8/9	18/9	66/8
	10d	7/1	14/7	46/8

JACK PLUGS

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 $\frac{1}{4}$ in. Type SE/P1. Side-entry version of type P1.
 $\frac{1}{4}$ in. Type P2. Standard. Unscreened. Unbreakable moulded cover.
 $\frac{1}{4}$ in. Type P3. Tip-Ring-Sleeve Stereo version of Type P1.
 $\frac{1}{4}$ in. Type P4. Tip-Ring-Sleeve Stereo version of Type P2.
3.5mm Type P5. Standard. Screened. Aluminium cover.
3.5mm Type P6. Standard. Unscreened. Unbreakable moulded cover.
Prices—

	each	10 off	25 off	100 off
P1.	3/-	26/8	62/6	233/4
SE/P1.	3/6	30/10	66/8	280/-
P2.	2/6	23/4	54/2	200/-
P3.	6/6	60/-	137/6	500/-
P4.	6/2	56/6	127/6	455/-
P5.	2/2	19/2	43/9	158/4
P6.	1/8	15/-	33/4	116/8

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$\frac{1}{4}$ in. Type S3. Stereo version for use with P3 or P4 plugs.
 $\frac{1}{4}$ in. Type S5. Standard. Moulded body. Chrome insert.
3.5mm Type S6. Standard. Moulded body. Chrome insert.
Available with make or break contacts on Tip, Ring and Sleeve.
Prices—

	each	10 off	25 off	100 off
S3	3/3	30/-	68/9	250/-
S5	2/9	25/-	56/8	216/8
S6	1/6	13/4	33/4	100/-

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10V	4	16	32	64	125
16V	2.5	10	20	40	80
25V	1.6	6.4	12.5	25	50
40V	1	4	8	16	32
64V	0.64	2.5	5	10	20
Price	1/4	1/3	1/2	1/-	1/1

Small (all values in μ F)					
4V	800	1,250	2,000	3,200	
6.4V	640	1,000	1,600	2,500	
10V	400	640	1,000	1,600	
16V	250	400	640	1,000	
25V	160	250	400	640	
40V	100	160	250	400	
64V	64	100	160	250	
Price	1/6	2/-	2/6	3/-	

POLYESTER CAPACITORS (Mullard)

Tubular, 10%, 160V: 0.01, 0.015, 0.022 μ F, 7d. 0.033, 0.047 μ F, 8d. 0.068, 0.1 μ F, 9d. 0.15 μ F, 11d. 0.22 μ F, 1/- 0.33 μ F, 1/3. 0.47 μ F, 1/6. 0.68 μ F, 2/3. 1 μ F, 2/8.
400V: 1,000, 1,500, 2,200, 3,300, 4,700pF, 6d. 6,800pF, 0.01, 0.015, 0.022 μ F, 7d. 0.033 μ F, 8d. 0.047 μ F, 9d. 0.068, 0.1 μ F, 11d. 0.15 μ F, 1/2. 0.22 μ F, 1/6. 0.33 μ F, 2/3. 0.47 μ F, 2/8.
Modular, metallised. P.C. mounting, 20%, 250V: 0.01, 0.015, 0.022 μ F, 7d. 0.033, 0.047 μ F, 8d. 0.068, 0.1 μ F, 9d. 0.15 μ F, 11d. 0.22 μ F, 1/- 0.33 μ F, 1/5. 0.47 μ F, 1/8. 0.68 μ F, 2/3. 1 μ F, 2/9.

SEMICONDUCTORS: OA5, OA81, 1/9. OC44, OC45, OC71, OC81, OC81D, OC82D, 2/- OC70, OC72, 2/3. AC107, OC75, OC170, OC171, 2/6. AF115, AF116, AF117, ACY19, ACY21, 3/3. OC140, 4/3. OC200, 5/- OC139, 5/3. OC25, 7/- OC35, 8/- OC23, OC28, 8/3.

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High quality. Rear tags. Long spindle, $\frac{1}{8}$ " Dia.
1p/12w, 2p/6w, 3p/4w, 4p/3w, 2p/3w.
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	each	10 off	25 off	100 off
All Types	4/6	38/4	83/4	283/4

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0.1 Matrix: 3 $\frac{1}{2}$ in \times 2 $\frac{1}{2}$ in, 4/- 5in \times 2 $\frac{1}{2}$ in, 4/6. 3 $\frac{1}{2}$ in \times 3 $\frac{1}{2}$ in, 4/6. 5in \times 3 $\frac{1}{2}$ in, 5/3.

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THE CHROMATONE

BY M. J. HUGHES M.A.

A mains powered sound operated lighting effects unit, that can provide up to 2kW of light power

A RECENT series in this magazine (**Sound Light and Colour*) described several lighting effects that can be used in conjunction with music either to intensify or complement the listeners' enjoyment. One such system used audio signals from the music to control the intensity of coloured lamps mounted on a display panel.

The Chromatone works on exactly the same principle but instead of using transistors to drive low voltage bulbs, thyristors are used to operate mains driven bulbs allowing up to 750 watts of light power on each colour channel. The unit to be described has three colour channels thus, when loaded to capacity, can deliver more than 2 kilowatts of light power—more than sufficient to light even the largest domestic room and many medium sized clubs.

The unit is highly compact and portable as well as being versatile on its input requirements; it will operate effectively from small transistor radios, hi-fi record players, commercial tape recorders, electric guitars and electronic organs. Being portable it is admirably suited to "pop" groups who wish to augment their music with constantly changing floodlights.

OVERALL SYSTEM

Fig. 1 shows the full circuitry of the equipment which is most logically divided into three sections:

- (1) A matching preamplifier having a low impedance input which allows the unit to operate from any extension speaker terminals from 3 to 15 ohms without applying load to the existing speakers in circuit.
- (2) A simple RC tone separator circuit roughly splitting the input signal into three channels—low, middle and high frequencies.
- (3) Three identical but separate integrators and thyristor firing circuits.

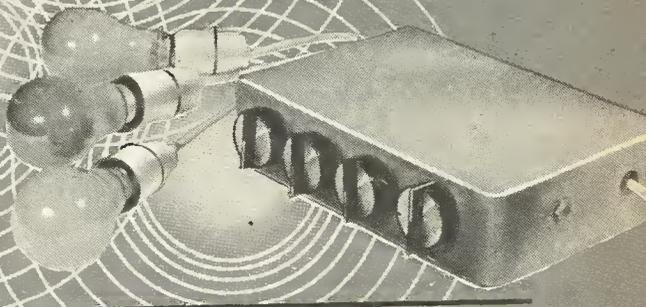
The thyristors specified have peak voltage ratings of 400 volts and can supply up to 3 amps each. They are

used to drive conventional tungsten filament bulbs and, as the circuit stands, are not suited to running fluorescent lamps. As the controlled lamps are constantly switching on and off it is suggested that normal domestic bulbs be used and special purpose high power lamps such as photo-floods or quartz iodine bulbs avoided. Any number of lamps can be wired in parallel on each channel provided the total power does not exceed 750 watts per channel.

CIRCUIT DESCRIPTION

The circuitry used is rather unconventional and for this reason it is important that the constructor reads this section carefully before embarking on any work (by so doing he will probably save himself much time and trouble).

In order to fire the thyristors it is necessary for the whole of the tone separator, integrator and firing circuits to be strapped to the "neutral" side of the mains. At the same time it is absolutely essential that the input circuit be isolated and capable of being earthed for safety reasons. Isolation is provided by a conventional 3 ohm valve output transformer (T2) con-



*The series on *Sound Light and Colour* appeared in the August to November 1968 issues; unfortunately these issues are now unobtainable.

nected so that its 3 ohm winding forms the collector load of TR1 (Fig. 1). As the common emitter line of the firing circuit cannot be connected to the earth line of the preamplifier, two separate power supplies *must* be used.

The power requirements for the preamplifier are comparatively crude and are provided by T3—a 6.3V heater transformer—through a low voltage silicon diode D2. First order smoothing is provided by C1. The input signal from an extension speaker socket is applied to the base of TR1 through a 25 ohm gain control. By normal audio standards this stage produces considerable distortion but this is of no detriment to the final effect, therefore it was decided to keep this stage as simple as possible. *To ensure safety in operation it is essential to earth the emitter line of the preamplifier.*

Tone separation is obtained very simply by three separate gain controls each of which has a crude filter circuit. The controls adjust the amount of signal applied to each filter which provide top cut (for bass), top cut and middle pass (for the mid-audio frequencies) and top pass for the higher frequencies. Accurate frequency separation is not possible with this simple layout and there is considerable overlap between the

channels, but in order to keep the size, weight and cost low it was felt desirable to omit inductive tuning.

Experimenters might like to substitute their own tone circuits which could be of the *EC* type described in the *Sound Light and Colour* series. If *LC* tuning is attempted it should be pointed out that the inductance of the isolating transformer will significantly alter the characteristics of subsequent filters. In practice the overlap of frequencies did not prove as great a disadvantage as one might imagine owing to the fact that each channel's sensitivity can be set independently by VR2, 3, and 4, thus compensating to a large extent for this defect.

The output from each filter is applied to the base of a transistor (TR2, 3 and 4 respectively) in each of three thyristor firing circuits shown in Fig. 1.

INTEGRATOR CIRCUIT

It is worth describing the circuit of the integrator in a little more detail because the transistors are used in a rather unconventional fashion. Fig. 2 shows a single integrator connected to the trigger of a thyristor (SCR1).

To make a thyristor fire, the trigger electrode must be driven approximately 3 volts positive with respect to the

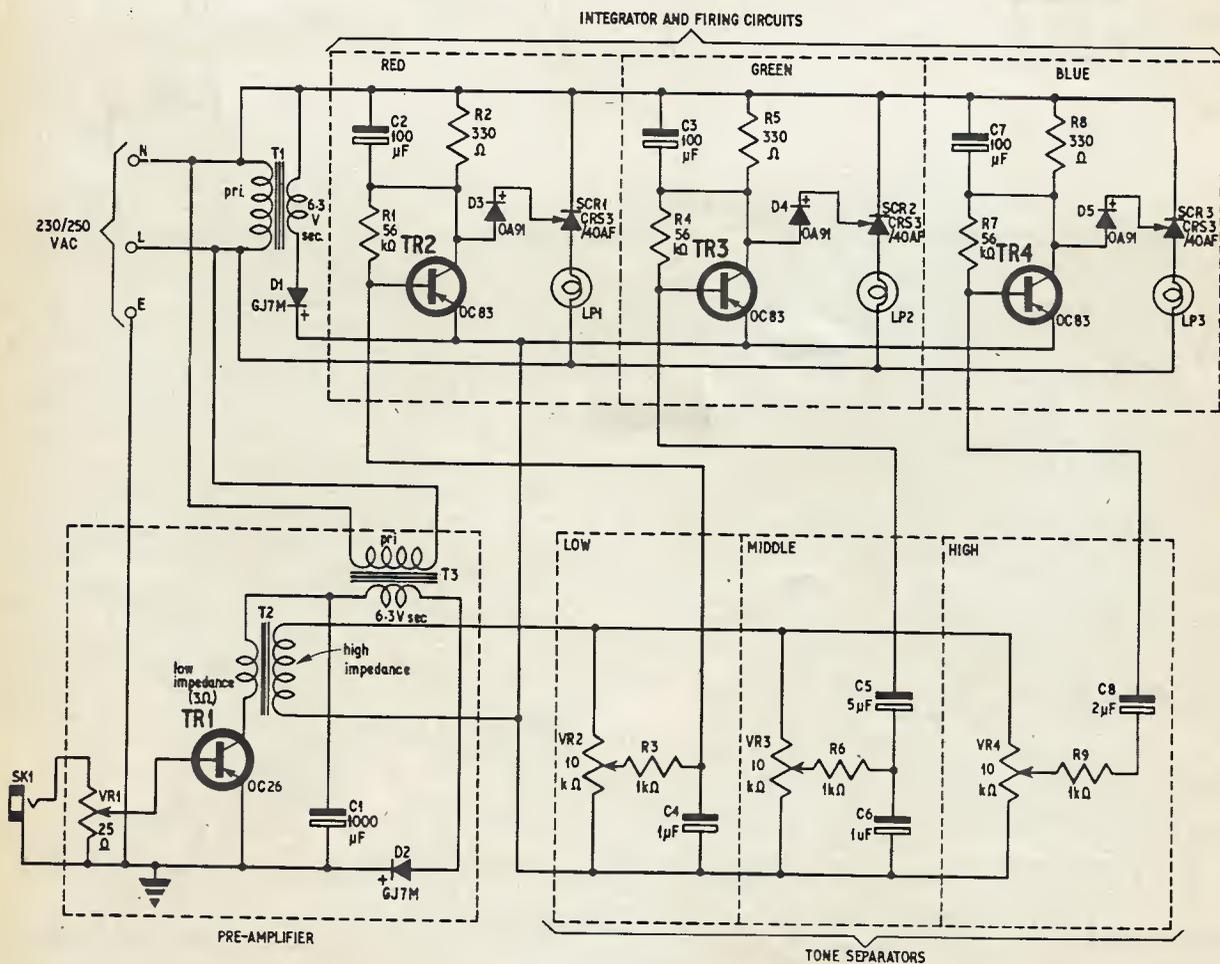
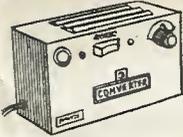


Fig. 1. The complete circuit diagram of the Chromatone

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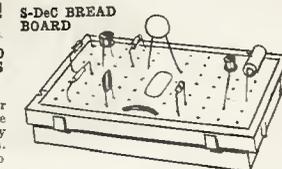
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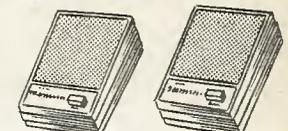
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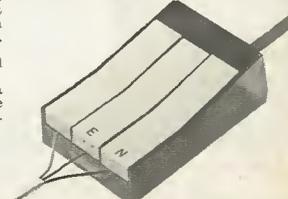


For table or wall mounting. Smart two tone grey cases size 3 1/2 x 1 1/2 in. Complete with lead, staples and 9V battery. 55/- P. & P. 3/6.

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Ideal for model makers, record players, tape decks, etc.

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One mains "Keynector" instantly and safely connects electrical appliances to mains supply without the use of a plug. A number of appliances may be used simultaneously up to the full 13 amp rating of this device. A red light glows when "live". The "Keynector" is fused and has its own robust switch which is interlocked to prevent connections when "live". Invaluable to handymen, servicemen, demonstrators, etc.

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For measuring alpha, beta and Ico factors of transistors also for checking germanium and silicon diodes. Internal 9V battery. Wide reading scale. Moulded case size 7 x 4 1/2 x 3 1/2 in. Ranges: Alpha 0.7-0.9967; Beta 0-300; Ico 0-50-5,000A. Diode test: forward and reverse internal resistance. Resistances: 200 ohm-1 megohm. Complete with connectors and instruction booklet. £7.19.6. P. & P. 3/6.

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J1003	5"	Long Play PVC	900ft	10/-	P. & P. 1/8
J1004	5"	Double Play Poly	1200ft	15/-	P. & P. 1/8
J1005	5 1/2"	Long Play PVC	1200ft	12/6	P. & P. 2/-
J1006	5 1/2"	Double Play Poly	1200ft	12/6	P. & P. 2/6
J1007	7"	Standard Play PVC	1800ft	22/6	P. & P. 2/-
J1008	7"	Long Play PVC	1800ft	17/6	P. & P. 2/6
J1009	7"	Double Play Poly	2400ft	25/-	P. & P. 2/6
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E.1311. PHONO PRE-AMPLIFIER. Size 2 x 1 1/2 in. Built-in R.I.A.A. characteristics enabling low output magnetic pick-up cartridges to be amplified up to 1 volt. Input 100Kohm: Gain 28dB: Max. output 3V: Max. input 50mV. Distortion 0-15% (at 1V level). Power supply 9-12V. 29/6. P. & P. 2/-.

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E.1315. ELECTRONIC ORGAN TONE OSCILLATOR. Used in conjunction with an organ keyboard, variable resistances and a 9 volt power supply, this module acts as the oscillator unit for an electronic organ. Tone Frequency: 200-1,000Hz: Output 80mW: Current 15mA. 25/- P. & P. 2/-.

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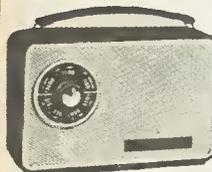
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THE MAGNIFICENT ROAMER 7

SEVEN WAVEBAND PORTABLE

7 FULLY TUNABLE WAVE BANDS—MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Extra Medium waveband provides easier tuning of Radio Luxembourg, etc. Built in ferrite rod aerial for Medium and Long Waves. 5 Section 22in chrome plated telescopic aerial for Short Waves—can be angled and rotated for peak S.W. listening. Socket for Car Aerial. Powerful push-pull output. 7 transistors and two diodes including Micro-Alloy R.F. Transistors. Famous make 7 × 4in P.M. speaker. Air spaced ganged tuning condenser. Volume/on/off control, wave change switches and tuning control. Attractive case with carrying handle. Size 9 × 7 × 4in approx. First grade components. Easy to follow instructions and diagrams make the Roamer 7 a pleasure to build.

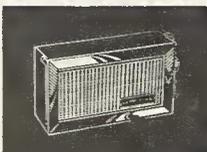
Total building costs Parts price list and easy build plans 3/7/6 (FREE with parts).
£5.19.6 P. & P. (FREE with parts).
 Personal Earpiece with switched socket for private listening, 5/- extra.



"NEW LOOK" MELODY SIX MED. AND LONG WAVES. WITH SPEAKER AND EARPIECE

6 transistors and 2 diodes. Push-pull output, tuning condenser, high "Q" ferrite rod aerial, 3 1/2in speaker, and personal earpiece with switched socket for private listening. 6 1/2 × 4 × 2in. Total Building Costs 69/6. P. & P. 4/3.

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POCKET FIVE

MED. and LONG WAVES AND TRAWLER BAND to approx. 50 metres. WITH SPEAKER AND EARPIECE. 5 transistors and 2 diodes, ferrite rod aerial, tuning condenser, moving coil speaker, etc. 5 1/2 × 1 1/2 × 3 1/2in. Total Building Costs 44/6. P. & P. 3/6. Plans and Parts list 1/6 (free with parts).



TRANSONA FIVE

MED. AND LONG AND TRAWLER BAND to approx. 50 metres WITH SPEAKER AND EARPIECE. 5 transistors and 2 diodes, ferrite rod aerial, tuning condenser, volume control, moving coil speaker, 6 1/2 × 4 1/2 × 1 1/2in. Total Building Costs 47/6. P. & P. 3/6. Plans and Parts list 1/6 (free with parts).



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MED. LONG AND TRAWLER BAND. 7 transistors and 2 diodes. 3in speaker, 2 R.F. stages, push-pull output, etc. 7 1/2 × 5 1/2 × 1 1/2in. Total Building Costs 89/6. P. & P. 4/6. Plans and parts list 2/- (free with parts). Personal Earpiece with switched socket for private listening, 5/- extra.

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 6 WAVEBANDS—MW1, MW2, SW1, SW2, LW AND TRAWLER BAND. 6 transistors and 2 diodes. Ferrite rod and telescopic aeriels. 3in speaker. Top grade components. Size 7 1/2 × 5 1/2 × 1 1/2in. Total Building Costs 79/6. P. & P. 4/6. Plans and parts list 2/- (free with parts).

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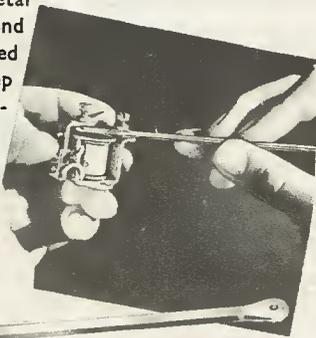
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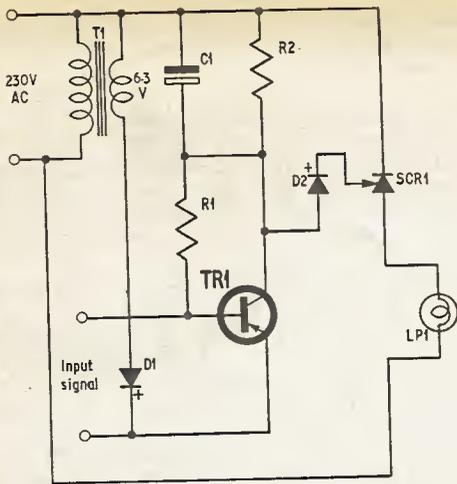


Fig. 2. Circuit of a single integrator connected to the trigger of a thyristor

anode, and the driving source must be capable of delivering at least 20mA into the trigger. Once triggered the thyristor will continue to conduct as long as it is passing a current in excess of its holding current (about 25mA) between its anode and cathode. As soon as this holding current falls below the threshold the thyristor will turn off and will not conduct again unless the triggering condition is repeated.

When operating on 50Hz mains the applied voltage passes through zero 100 times a second, and hence, to keep the thyristor conducting, it is necessary to re-trigger for every cycle (if we were using a full wave bridge it would be necessary to trigger every half cycle).

Triggering therefore has to occur in synchronism with the applied voltage and in normal lamp dimmer circuits this is carried out by applying a small proportion of the applied voltage to the trigger.

Conventional dimming is obtained by changing the phase of the trigger voltage relative to the applied voltage so that the thyristor will fire during a comparatively short period of the half cycle. Phase shift is obtained in a manually operated lamp dimmer by adjusting the value of a resistor in an RC circuit.

Referring now to Fig. 2, we have replaced the variable resistor in the manual system with a transistor (TR1). Because the trigger of the thyristor must receive a synchronous 50Hz pulse, it is necessary to power the transistor with single wave rectified un-smoothed a.c. supplied by T1 through D1. Although the circuit is live to mains, the voltages across the circuit never exceed the 6.3V supplied by T1.

The voltage across R1 and collector/emitter of TR1 oscillates between 0 and 6.3V in exact phase relationship with the full 230V across the thyristor and the lamp. This phase relationship can only be obtained if the correct end of the secondary winding of T1 is linked to the live mains line—if the link was made to the wrong end the power to the drive circuit would be 180 degrees out of phase.

With no signal applied to the base of TR1 the transistor is effectively a very high resistance and the potential difference across R1 at any part of a half cycle is zero, thus the trigger to anode voltage of the thyristor is also zero. If a negative going signal is applied to the base the collector/emitter resistance of TR1 falls roughly in proportion to the amplitude of the applied signal and C1 starts to charge through TR1 towards the voltage set by the potential divider formed by TR1 and R2. It will take a finite time for C1 to charge and this is again dependent on the instantaneous resistance of TR1 and on the value of the capacitor.

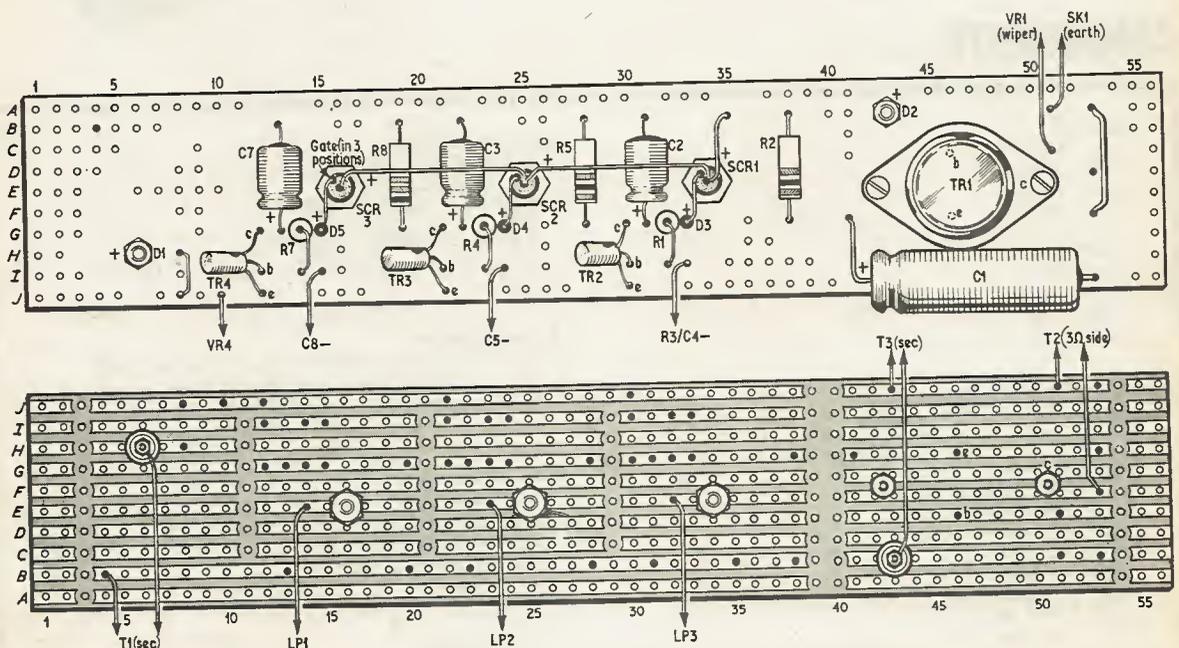


Fig. 3. Circuit board layout and wiring details

The values of C1 and R1 have been chosen so that the average integration time for the capacitor to charge to 3 volts is approximately 5 milliseconds. This naturally has considerable dependence on the input signal and has been taken into account, so that, with the master gain control (VR1) set midway, an input signal from a medium volume loudspeaker will operate the unit correctly.

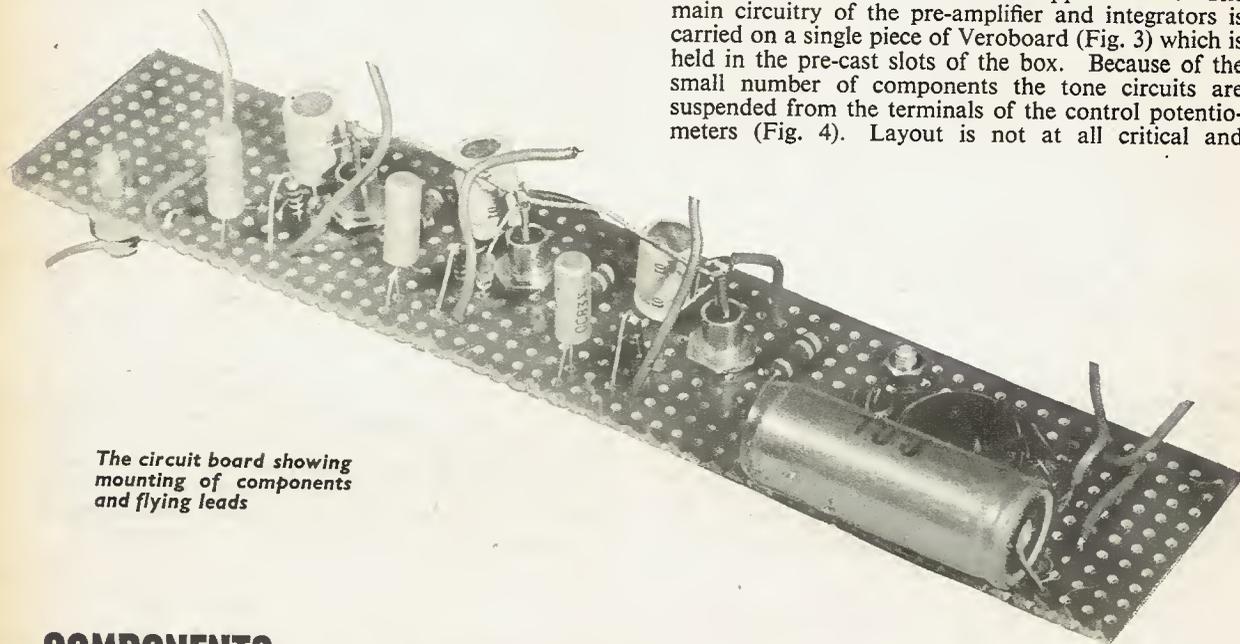
With an average integration time set for 5ms, C1 will reach 3V approximately half way through a half cycle; when this moment is reached the thyristor fires thus lighting the lamp for the remainder of that half cycle. If the input signal increases in amplitude the integration time becomes less, and the thyristor will fire earlier thus

passing more energy to the lamp and effectively increasing its brightness; for lower level audio signals the converse happens.

CONSTRUCTIONAL DETAILS

All components are readily available, and there are no critical values. The power transformers are conventional 6-3V heater types. The only point to watch is that the isolating transformer T2 will really isolate; hence it is best to use one that has been designed for use in valve circuits.

The unit is housed in a die cast box measuring $8\frac{3}{8}$ in \times $5\frac{3}{8}$ in \times $2\frac{3}{8}$ in. The transformers used conveniently mount along one side of the box and all four gain controls are mounted on the opposite side. The main circuitry of the pre-amplifier and integrators is carried on a single piece of Veroboard (Fig. 3) which is held in the pre-cast slots of the box. Because of the small number of components the tone circuits are suspended from the terminals of the control potentiometers (Fig. 4). Layout is not at all critical and



The circuit board showing mounting of components and flying leads

COMPONENTS . . .

Resistors

- R1 56k Ω
- R2 330 Ω
- R3 1k Ω
- R4 56k Ω
- R5 330 Ω
- R6 1k Ω
- R7 56k Ω
- R8 330 Ω
- R9 1k Ω
- All $\pm 10\%$, $\frac{1}{2}$ W carbon

Potentiometers

- VR1 25 Ω , 3W wirewound
- VR2, 3, 4 10k Ω log (3 off)

Capacitors

- C1 1,000 μ F elect. 15V
- C2 100 μ F elect. 15V
- C3 100 μ F elect. 15V
- C4 1 μ F elect. 15V
- C5 5 μ F elect. 15V
- C6 1 μ F elect. 15V
- C7 100 μ F elect. 15V
- C8 2 μ F elect. 15V

Semiconductors

- DI, 2 GJ7M (or any 15 p.i.v., 1A silicon rectifier) (2 off)
- D3, 4, 5 OA91 (3 off)
- TR1 OC26
- TR2, 3, 4 OC83 (3 off)
- SCR1, 2, 3 CRS3/40AF (3A, 400 p.i.v.) (3 off)

Transformers

- T1, 3 Mains transformer, sec 6-3V at 1A (2 off)
- T2 Midget choke type (Radiospares) or any 3 Ω valve output transformer

Miscellaneous

- SK1 jack socket
- Die cast box ($8\frac{3}{8}$ in \times $5\frac{3}{8}$ in \times $2\frac{3}{8}$ in)
- Bayonet bulb holders (3 off)
- Control knobs (4 off)
- Veroboard
- Mains lead
- Grommets
- 4B.A. fixings

RADIO STETHOSCOPE

Easiest way to find fault—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio, TV, amplifier, anything—complete kit comprises two special transistors and all parts including probe tube and crystal earpiece. 29/6—two at a set instead of earpiece 11/extra—post and ins. 2/9.

MINIATURE WAFER SWITCHES

2 pole, 2 way—4 pole, 2 way—3 pole, 3 way—4 pole, 3 way—2 pole, 4 way—3 pole, 4 way—2 pole, 6 way—1 pole, 12 way. All at 3/6 each. 36/- dozen, your assortment.

WATERPROOF HEATING ELEMENT

26 yards length 70W. Self-regulating temperature control. 10/- post free.

BATTERY CHARGER FOR NICADS

This is in plastic case, size 5 1/2 x 4 1/2 in. approx. All wired up with 3 core output lead and 3 core mains input lead. Contains mains transformer with 40v. 250mA secondary and standard 200/240 primary. Also contains full wave bridge rectifier, neon indicator, wired up with resistors to charge 2 Nicad batteries simultaneously. Charge rates of 50mA and 25mA respectively. Batteries up to 30 volts may be charged. Price 39/6 each, plus 3/6 postage and insurance.

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Making a power pack for amplifier or other equipment? These transformers have normal mains primaries (230/40v.) and isolated secondaries two types (1) 12v. 500mA at 3/6; (2) 15v. 500mA at 8/6.

FP3 ELIMINATOR. Play your pocket radio from the mains. Save 5s. Complete component kit comprises 4 rectifiers—mains dropper resistances, smoothing condenser and instructions, only 6/6 plus 1/- post.

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16mm. Made by the Swiss company, Kern Paillard. Year 1:28 f=75mm. Brand new in leather case 339, which is less than half current list price.

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MAINS TRANSISTOR POWER PACK

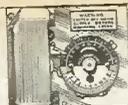
Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500mA (Class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP8, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only 16/6, plus 3/6 postage.

16 RPM GEARED MOTOR

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Made by Smiths these are AC mains operated, NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. 2 completely adjustable time periods per 24 hours, 5 amp changeover contacts will switch circuit on or off during these periods. 59/6, post and ins. 4/6. Additional time contacts 10/- pair.

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CONTROL DRILL SPEEDS



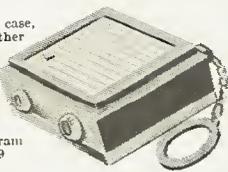
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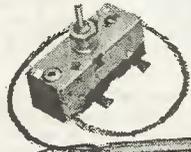
CASSETTE LOADED DICATING MACHINE for only 99/6

Battery operated and with all accessories. Really fantastic offer a British made £31 outfit for only 24.19.6, brilliantly designed for speed and efficiency—cassette speed and normal spools, drops in and out for easy loading—all normal functions—includes: stethoscopic earpiece—crystal microphone has on/off switch—telephone pick-up—DOXYT MISS THIS UNREPEATABLE OFFER—SEND TODAY 24.19.6 plus 7/6 post and insurance. Foot switch 18/6 extra. Spare Cassettes at 4/6 each, three for 10/-.



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This has a sensor attached to a 15A switch by a 14in. length of flexible capillary tubing—control range is 20°F to 150°F so it is suitable to control soil heating and liquid heating especially when in buckets or portable vessels as the sensor can be raised out and lowered into the vessel. This thermostat could also be used to sound a bell or other alarm when critical temp. is reached in stack or heap subject to spontaneous combustion or if liquid is being heated by gas or others means not controllable by the switch. Made by the famous Teddington Co., we offer these at 12/6 each. Postage and insurance 2/9.



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Made by the famous meter company Chamberlain and Hookham, these have a normal mains 200-240V motor which drives a ratchet mechanism so geared to give one ratchet action per minute on a wheel with 60 teeth thus a complete revolution of the cam takes place in one hour. The cam operates 8 switches (6 changeover and 2 on/off thus 480 circuit changes per hour are possible). Contacts, rated at 15 amps have been set for certain switch combinations but can, no doubt, be altered to suit a special job. Also other switch wafers or devices can be attached to the shaft which extends approximately one inch. 47/6. p. & ins. 4/6.

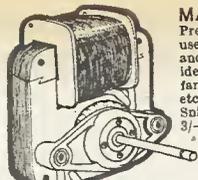


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FULL FI 12 INCH LOUDSPEAKER. This is undoubtedly one of the finest loudspeakers that we have ever offered, produced by one of the country's most famous makers. It has a die-cast metal frame and is strongly recommended for Hi-Fi and Rhythm Guitar and public address. Flux Density 11,000 gauss—Total Flux 44,000 Maxwells—Freq. response 30-10,000 c.p.s.—specify 3 or 15 ohms—Main resonance 60 c.p.s.—Chassis Diam. 12in.—12 1/2in. over mounting lugs—Baffle hole 1 1/2 in. Diam.—Mounting holes 4, holes—1/2 in. diam. on pitch circle 1 1/2 in. diam.—Overall height 6 1/2 in. A 26 speaker offered for only 23.9.6 plus 7/6 p. & p. Don't miss this offer. 15in. 30 watt 27.19.6.



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MAINS MOTOR

Precision made as used in record decks and tape recorders—ideal also for extractor fans, blower, heater, etc. New and perfect. Snip at 9/6. Postage 3/- for first one then 1/- for each one ordered. 12 and over post free.

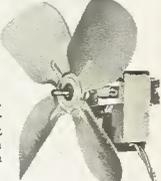
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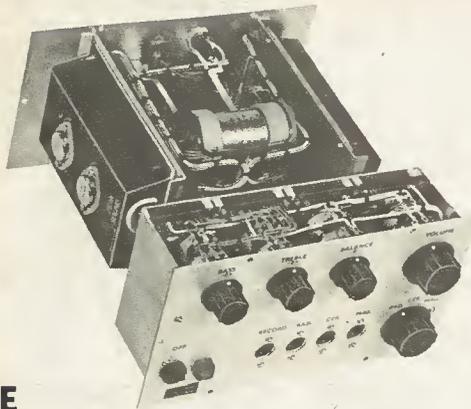
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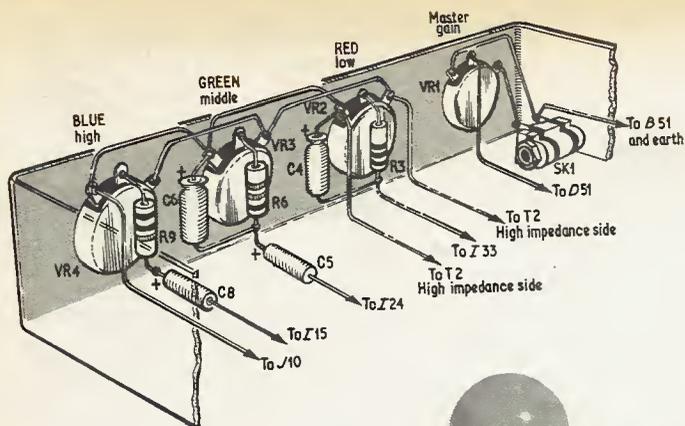
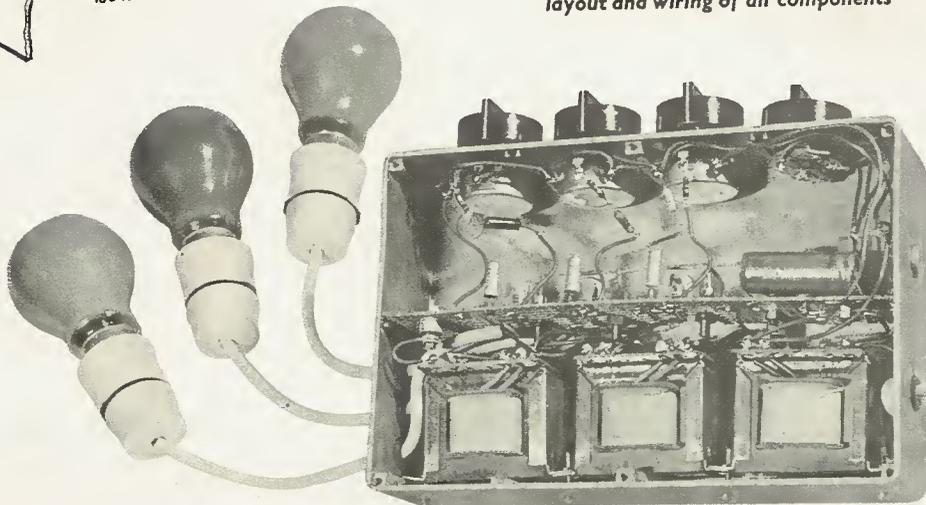


Fig. 4. Layout and wiring details of the four gain controls and filter circuits

The complete Chromatone showing the layout and wiring of all components



readers could use any type of enclosure provided it can be adequately earthed or similarly protected in case the insulation of T2 should break down.

Output connections to the three lamp channels are provided by flying leads terminated with standard bayonet bulb sockets. Panel mounting sockets could be used if desired, but should be capable of carrying 230V at 3A. The prototype was designed to run from a fused 13A plug, and therefore an integral fuse was omitted; for safety's sake a built-in fuse must be fitted if the unit is to be used without a fused plug.

No details of fixing holes are given as these will vary according to the types of component used by the constructor. Work should begin by drilling all holes in the box, and grommets inserted in all those holes carrying inlet or outlet leads. All components should then be wired in to the Veroboard as shown in Fig. 3. The final stage of assembly is to wire up the transformers and gain controls to the Veroboard (Figs. 4 and 5). When connecting the transformers, try to ensure that the linked ends of primary and secondary of T1 are both "starts"; this will ensure that phasing is correct.

OPERATION

When the wiring is complete, connect the input jack socket (SK1) to the extension speaker terminals of a record player or radio, plug three different coloured lamps into the bayonet sockets (it is suggested that red be used with the low frequency circuit, green for the middle, and blue for the high). Turn all gain controls to minimum and plug the unit into the mains. None of the lamps should light under this condition. Next set

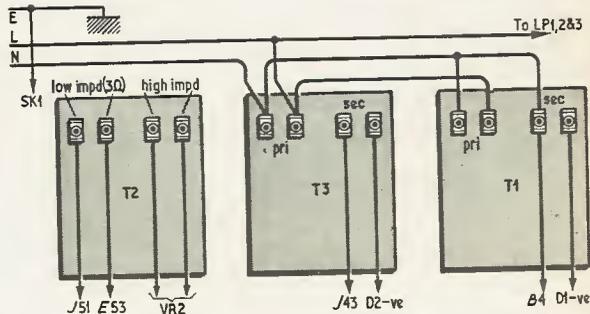


Fig. 5. Wiring details of transformers showing mains input lead

the volume of the record player to a comfortable listening level and turn VR2, 3 and 4 to midway positions. Slowly turn up VR1 and if all is correct one or all of the lamps should begin to light up in time with the music. If on advancing all controls to maximum none of the lamps light, and the circuit has been checked for errors, it is more than probable that the phasing is wrong. This is simply remedied by reversing the connections from the secondary of T1.

When the lamps are working satisfactorily the overall sensitivity of the unit can be set by VR1 and any personal choice of light balance can be set by adjusting the tone gain-controls relative to each other. ★

Readout —

A SELECTION FROM OUR POSTBAG

correspondents wishing a reply must enclose a stamped addressed envelope

I.C.'s for the public

Sir—As suppliers of integrated circuits advertising in PRACTICAL ELECTRONICS, we were somewhat disconcerted to read the letter from Mr Robson (*Readout*, May 1969) expressing his opinion that i.c.'s are not for the public at large. We note that Mr Robson offers no reasons for his "down" on i.c.'s and we would be interested to read his other letter to which he refers.

It has been our experience that i.c.'s are indeed for the public as evidenced by the fact that we find people who have bought them frequently come back for more. Surely, from the experimenter's point of view, the i.c. is no more nor less than just another semiconductor, but admittedly a much more sophisticated one than a single transistor for example.

Most manufacturers produce comprehensive data sheets which include a circuit diagram of the device, and often examples of applications, giving the average enthusiast all the information he needs for many hours of experimenting.

D. E. Johnston,
Director,
Kinver Electronics Ltd.,
Stourbridge.

Cost of i.c.'s

Sir—I was surprised to find in the May edition of PRACTICAL ELECTRONICS two letters objecting to integrated circuits. Labelling the letter concerning the radio repairing a problem relating to "I.C." even if the latter was in inverted commas is a bit unfair. The use of the word module in the letter suggests that either a hybrid circuit was used or simply normal circuitry enclosed in some impregnable material such as Araldite. As an engineer working on the circuit development of integrated circuits, I can say that to the best of my knowledge the average cost of an integrated circuit for a radio is certainly not in the

region of pounds trade price. Such a circuit contains all the circuit functions of a radio, bar the decoupling capacitors and passive tuning components. I.C.'s for the domestic market, like present transistors, are almost certain to be plastics or ceramic encapsulated by all manufacturers; the most likely configuration is the dual in line package, which should be easily removable with the help of a specially shaped soldering bit—a matter of half a minute's work?

I would be interested to see Mr James Robson's objections to i.c.'s. All i.c. circuits can of course be implemented in ordinary discrete circuitry, but i.c.'s I would think are far easier to use and make the whole system much neater. I have for instance just made a system that produces a 1.5 volt "ramp" formed of 512 discrete steps. This required only three, ten lead TO5 cans and about 20 resistors. Each TO5 can is the equivalent of three clockable flip-flops plus an AND gate. I admit that at the present time it is probably cheaper for the amateur to build such a system of discrete components, but I would suggest that within the next few years, i.c.'s will make it possible for the ambitious person to build himself a desk top calculator (probably to be used more by his children for homework) a project a little daunting in discrete components.

... and electronic dice

I also have a suggestion for Mr Brian Dellow regarding an electronic dice. The difficulty here as I see it is the production of a random sequence. A pseudo-random sequence could be produced entirely digitally, but the system would be rather complex in order to beat people with exceptionally good memories. An alternative would be to use an analogue source of noise, such as a noisy transistor, amplify the noise, filter it and feed the filtered signal onto the input of a squaring stage to produce a pulse output. The output could then be decoded serially to produce a decimal number from a binary sequence, or perhaps three filters of different values could be used to produce a

parallel output. The outputs could be decoded with a simple diode matrix and fed to six bulbs via amplifiers.

P. Cranswick,
Swindon,
Wilts.

Electronics instructor!

Sir—Our Youth Club is most interested to make contact with amateur electronics clubs and enthusiasts in this area in order to form a section within the Club.

Our members have recently indicated a great deal of interest in forming their own group to build radio and electronic systems but, of course, they desire to receive instruction from a person who has experience and knowledge of this sort of interest.

I would be most grateful if you were able to give me contacts who would be able to help us in this present situation.

Brian Gouldman,
Youth Leader,
Liverpool Jewish Youth Centre,
Harold House,
Dunbabin Road,
Liverpool L15 6XL.

Electronic club wanted

Sir—I have been asked for names and addresses of any local clubs or societies concerned with do-it-yourself electronics. I shall be grateful for any help you can give.

Ealing Borough Librarian,
Technical Library,
Acton Library,
High Street,
London, W.3.

NOTICE

ARSENIDE DIODES GO UP

With reference to an editorial note in *Readout* last April, Messrs Proops Bros. inform us that the current price of the gallium arsenide light source type MGA100 is 35s. This is an increase of 6s 6d on the advertised price prior to December last and which we unsuspectingly quoted. We are also asked to state that the MGA100 is a new production item.

Thus dashed for the moment, it seems, is the earnest hope expressed on that occasion for an early downward trend in the cost of infra-red devices.—Ed.

OLRUS ELECTRONICS LTD

As we have had a number of complaints concerning the service provided by this Company, readers are asked to get in touch with me before dealing with it.

EDITOR.

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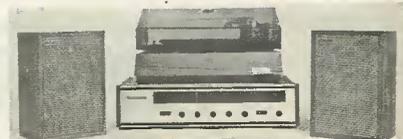
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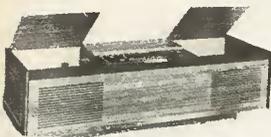
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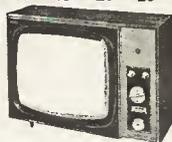
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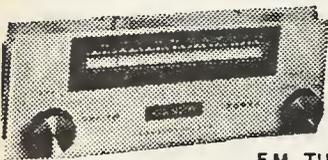
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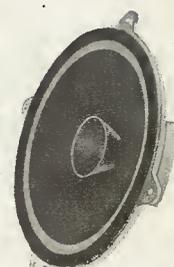
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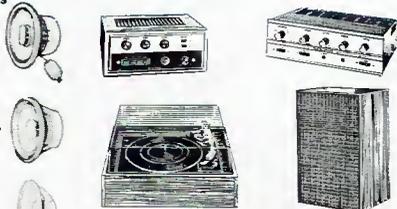
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