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pln DIN plug 10
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# Projects... Theory... 

## and Popular Features ...

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The theme this month is Safety First!
Over the last few years gas has become the most popular source of energy for domestic users. In the form of propane, gas is also widely used in caravans and boats.

Leakage of gas through badly made connections or defective pipes is an ever present hazard particularly in occasionally used installations such as the holiday home or boat. There can be unsuspected dangers lurking in permanent dwelling places, as well, especially where the property is old and still has the original gas mains installation.

Many users of gas will welcome a device that gives warning if an accumulation of gas builds up. The nose is not always a dependable sensor and certainly not as sensitive as the solid state device which is the "nose" element in our Gas Sentinel.

The electricity mains supply also receives some of our attention this month. It is not always safe to assume that the mains supply outlets have been correotly wired during installation. Sadly many cases come to light where the live and neutral connections have been reversed and sometimes the earth connection omitted.

When moving into a property, the new occupier would be wise to check all outlets with our Mains Fault Indicator prior to plugging in any electrical equipment. This valuable gadget
is extremely simple and costs little to build.
From domestic establishments, fixed, floating or parked, let us now move outdoors and venture into another danger area-the road. And immediately we find a serious deficiency.
The motorist has his direction indicators, and rarely has to resort to hand signals. Most motorcyclists are similarly equipped. This leaves the push-cyclist practically alone, amongst all wheeled vehicle users, without the convenience and protection of illuminated signals to indicate his intentions to other road users.

This is something the cyclist can easily rectify for himself by building our Cycle Direction Flasher. Precise mechanical arrangements and installation details will depend upon the particular model of cycle, but the system described should be adaptable to individual needs without difficulty.

Safety First! The practicality of projects such as these, which enable the home oonstructor to help safeguard life and property, is one reason why electronics has become a great and worthwhile hobby.


Our May lssue will be published on Friday, Aprll 18. See page 261 for detalls.

## Readers' Enquirles

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WHEN riding a bicycle along the road being seen is as important as seeing. This is especially so at night. Another requirement is for the driver of the car behind to know of your intention to turn left or right.
Although there is an obvious need for turn indicators in this situation, few blcycles are fitted with them. The project preseated here fills this gap.
The circuit is based on a 555 timer 1.c. generating a square wave which flashes one of the two lamps accordIng to the setting of a switch. Because of Its 200 mA source ability it was deodded that the I.C. was capable of driving the lamps drectly although the bulbs used here have a slightly lower voltage rating than the battery to obtain Increased brightness of the bulbs.

## CIRCUIT DESCRIPTION

A 555 timer $1, c$, ICl is wired as an astable multivibrator wheh forms the heart of this crrcuit (see Fig. 1).

When power is applied to the ctrcult capactor Cl charges-up through external resistors R1 and R2. A voltage comparator on the chlp sets a flip-fiop in the 1.c. when the voltage on the capadtor reaches $2 / 3$ supply voltage.

At this point the transistor in the output stage (connected to pin 3) is driven high by the filp-flop and the capacitor begins to discharge through another resistor. As the voltage on the capactor passes below $1 / 3$ supply
voltage another comparator resets the flip-flop (pin 3 goes low) and the cycle begins again. The square wave thus produced is available at pin 3.

In the circuit for the Cycle Direction Flasher R1, R2 and C1 have been chosen to give a flash-rate of about $0.5 \mathrm{~Hz}-30$ flashes per minuteapproximately the rate of a car direction indicator.
The square wave from the 1.c. is linked to one pole of $S 1$. This switch is of the centre-off variety and when It is put Into elther of its on positions the square wave passes to the appropriate lamp which then pulses in sympathy with it.

The second pole of this switch applies power to the circuit whenever it is moved to elther of its "on" positions.


## CIRCUIT BOARD

Commence construction with the clrcult board. This consists of a plece of 0.1 Inch matrix stripboard 12 strips by 13 holes. A single mounting hole is frrst drilled in the position shown In Flg. 2. Remember to clean off any copper swarf from the edges with emery paper.

Fig. 1. Clrcult dlagram for the Cycie Dlrection Flasher,


Next, cut the copper strips as indicated in the diagram, using a spot face cutter or a hand-held twist drill.
Assemble the board beginning with the links and then the resistors, capacitor, and i.c. in that order, using a minimum of heat and solder for the i.c. in particular.

Use Veropins for external connections to the board.

## DIECAST BOX

Next prepare the box to take the circuit board, wires and switch. It is recommended that a diecast box be used here as these are more easily sealed against the elements than most plastics boxes.
It is best to drill one hole each for the five wires entering the box rather than one large hole as the entry points will later be sealed with epoxy resin. A bunch of wires will be more likely to come loose than a single wire.
Fix the circuit board in place using nuts, bolts and spacers, and seal the screw holes with epoxy resin. Flying leads or Veropins should be soldered to the board prior to fixing it into the box.

Wire the leads from the board to the switch and complete the interwiring of the circuit board and switch within the box.

## TERMINAL BLOCK

One of the 5 -way terminal blocks, TB1, is then mounted outside the box according to Fig. 2 with short wires leading to it from the box and longer ones to the indicator unit at the rear of the cycle.

In this way a larger box will not be needed and the epoxy seal of the wires will not need to be broken if the box has to be removed. The connections to the terminal block should not be duly affected by the weather if it is mounted upside-down.

## INSTALLATION

Mounting the box, battery and indicators onto the bicycle poses some problems. The box should be positioned on the handlebars or somewhere on the main frame where the switch is accessible.

Fixing the box in place is most easily accomplished by the method pictured in Fig. 3. Twin holes are drilled in the lid in which screws are placed with the heads inside the box. The lid is then held onto a member of the bicycle frame by a pipe-clip fitted over the screws and fastened with nuts and shakeproof washers.
If you have the appropriate equipment, you could of course tap the holes and mount the screws the other


Fig. 2 (above). Interior of the control unit showing the circuit board layout, board mounting and interior wiring.

Fig. 3 (left). View of the rear of the control unit showing fixing bracket.


Layout of components inside the control unlt.

## COMPONENTS

Resistors
R1 $10 \mathrm{k} \Omega$
R2 $33 \mathrm{k} \Omega$
R3 $220 \Omega$
All $4 W$ carbon $\pm 5 \%$
Capacitor
C1 $10 \mu \mathrm{~F} 16 \mathrm{~V}$ elect
Semiconductors
IC1 NE555 timer i.c.


Miscellaneous
S1 d.p.d.t. centre-off toggle
LP1,2 3.5V 150 mA M.E.S. bulbs
and panel lampholders (RS 565 -
226) (2 off each)
$81,2,31 \cdot 5 \mathrm{~V}$ SP11 type cell (3 off) TB1,TB2 5 -way screw terminal blocks (2 off)
Stripboard, 0.1 inch matrix, 13 holes $\times 10$ strips; diecast metal box: set of PP9 battery connectors; single screw terminal block: id inch plastic pipe; 90 degree eibows ( 2 off) i cllps ( 2 off): piece of wood for back plate; plastic end caps (2 off); 4 BA nut, bolt and spacer; interconnecting wire.


The box mounted on the handle-bars contains an electronic oscillator and a switch: the unit at the back contains the direction indicator lights and batteries. When the rider wishes to turn left or right he can indicate his intentions by moving the selector switch to the left or right position.
This has the effect of connecting power to the circuit from the batteries and routing a square wave which switches from full battery voltage to zero at a frequency of 0.5 Hz (that is, turns on and off once every two seconds), to the appropriate rear bulb.

Starting off with the positive connection, the end cap (which can be anything from a standard part to a plastic pill box) is drilled so that the battery connector stud protrudes through the hole. Small holes are also drilled in this to take the wires from the right lamp holder and the positive contact.
The positive clip from a set of PP9 battery connectors is glued in position in the end cap and a length of wire is soldered to the connector. Then the whole is glued into the end of the tube forming the centre section of the assembly.

The negative battery cap is prepared in much the same way but instead of gluing it in position, a loop of wire is passed through two holes and knotted as this is to be used as a draw wire when battery replacement becomes necessary.

## FINAL ASSEMBLY

Final assembly can now be started by first passing the wires of one of the bulb holders and that from the battery positive contact through the holes in the positive connector end cap. The common wire from the left lamp holder is then passed
way round. In this instance waterproofing is achieved with four fibre washers between the clip and the lid, and the screw heads and the clip.

## INDICATORS

Turning now to the indicators, these are built up from $1^{1_{4}}$ inch plastic waste pipe and fittings and the whole assembly is seen in Fig. 4.
This unit houses the indicator lamps LP1 and LP2, and also the batteries and is designed to bolt onto the back of the cycle above the rear mudguard. Some experimentation may be necessary as there are bound to be differences between different machines.

Referring to Fig. 4, assembly should start by soldering a piece of wire about 50 mm long onto each tag of the lampholders. If these wires have different coloured insulation this will be a great help in identifying them later on.
The lampholders are then glued in position in the elbows using "super glue" making sure that only the rear milled ring is glued and not the front retaining ring, see Fig $4(a)$. This front ring must be free in order to get at the bulbs in the lampholder.

## BATTERY HOLDER

The next stage is to assemble the battery holder. Basically this consists of the centre tube with caps at each end holding the contacts and some foam packing to ensure a tight fit.


CYCLE DIRECTION FLASHER



Completed control unit with terminal block glued to side.

## CYCLE DIRECTION FLASHER



Layout of components on the circuit board.


The wooden mounting block to which the rear indicator unit is attached and the clips used to secure it to the bicycle frame.
through the negative connector end cap and joined to the common wire of the other lampholder using a single screw terminal connector block.

The remaining wires are then passed back through the negative connector end cap and all the cables are brought out through a hole in the middle of the tube. The three
batteries are next pushed into the tube, positive terminal first. The negative connector end cap and the foam packing can now be inserted in position and the elbows pushed tightly onto the ends of the tube. They should not be glued as they will need to be removed in order to change the batteries.

The connecting wires are terminated on the painted wooden mounting block with the other 5 -way screw terminal block (TB2). The assembly needs now to be fitted with clips/ clamps to secure it to the bicycle frame. In the prototype plastic snap fixing pipe clips were employed to securely position the assembly on the saddle stem.
As cyanoacrylate glue is used throughout the usual precautions for this sort of adhesive must be followed.

## TESTING

When all wiring is completed the unit may be tested. Connect the battery (observe correct polarity) and the lamps if not already connected.

Moving Sl into either on position should cause the appropriate lamp to flash. If you wish to adjust the flash rate, change R1. Change R2 to change the length of time the lamp stays on for each flash.
Any malfunctions are most likely due to a flat battery, incorrect switch wiring, or wrongly orientated components.
Finally, when the unit is operating properly, seal the box completely. The switch is sealed with a rubber washer on the outside of the box.

Ensure that all wires to the box are sealed with epoxy resin, likewise with any screws in the box and lid. Sealing the lid is achieved by setting the lid flange in a liberal amount of non-hardening elastic caulking compound. Finally the switch is weatherproofed by covering with a rubber cup.

The Adventures of Tanty Bead



## By Dave Barrington

## Storage Cabinets

As this month's Square One concentrates on components, it seems appropriate to mention two new portable component storage cabinets..
A cabinet ideal for the storage of such items as resistors, transistors, i.c.s, capacitors, grommets and most small items is the latest product from Sumico.
Measuring $254 \mathrm{~mm} \times 203 \mathrm{~mm} \times 165 \mathrm{~mm}$, the cabinet is made from strong plastic and has 15 "see-through" drawers with drawer dividers. The top of the cabinet incorporates a recessed carrying handle.

A feature of the cabinets is that they can be interlocked together to form a semi-permanent system for the workshop. For further details of stockists and prices readers should write to Sumico Ltd. Dept EE, 7 Clarence Road, Clare, Sudbury, Suffolk, CO10 8QN.

The Partfolio 200 "cube" available from Toolrange Ltd., is an unusual folding component tray system which offers up to 30 separate compartments.

Rather like a collection of multi-shelf. letter trays linked together, the cube when opened out extends to 800 mm but when closed forms a 200 mm cube, with carrying handle.
The system is supplied with compartment dlviders and labels. Each individual tray measures $195 \mathrm{~mm} \times 95 \mathrm{~mm} \times$ 40 mm and has divider slots to enable different size compartments to be made up.

The Partiolio 200 is priced at $£ 17.50$ plus VAT and is available from Toolrange Ltd., Dept EE, Upton Road, Reading, RG3 4JA.


Toko transducers from Ambit.

## Piezo Ceramic Buzzer

A range of probably the smallest piezo ceramic sound transducers we have come across is now available from Ambit International. Being so small, not much larger than a 10 pence piece, these Toko transducers will make perfect hidden warning buzzers for simple alarm projects.
The buzzers are available as unmounted discs or encapsulated in plastic with mounting lugs. Operating from fairly low voltages one of the range, type PB-2720, needs as little as 1 mA drive current.
Suggested application and drive circuits is included in the product data which is available along with the devices from Ambit International, Dept EE, 200 North Service Road, Brentwood, Essex, CM14 4SG. No price was available at the time of going to press.

## CONSTRUCTIONAL PROJECTS

We cannot foresee many component buying problems this month but one or two special items need further mention.

## Gas Sentinel

The main item on our list is the Gas Sentinel and as far as we are aware the gas sensor transducer is only available from Watford Electronics, the main distributor for these devices. We understand that they are also prepared to supply a complete kit of parts for this project.

The components list calls for a mains transformer with a secondary rated at 9 V 1 A . However, the prototype unit used a tran sformer with two 9 V 400 mA secondaries wired in parallel and is available from Watford Electronics as type 182.

## Cycle Direction Flasher

The only item likely to cause any concern in the Cycle Direction Flasher is the plastic end caps. These are available from Home Radio (Components) Ltd., PO Box 92, 215 .London Road, Mitcham, Surrey, CR4 3HD.

The plastic elbows and tubes should be available from most DIY shops.

As far as we have been able to ascertain, the 3.5 V 150 mA bulbs appear to be only available from Maplin Electronics.

No problems should be enountered in obtaining components for the Mains Fault Indicator, the Auto Level Control or the Radio Control Charger Unit.

Finally, we include a list of components suppliers for the last six parts, including this month's experiments, for the Teach-In 80 series.


Fifteen drawer component cabinet from Sumico.

## SUPPLIERS OF KITS FOR TEACH-IN 80

These kits contain all items specified by Everyday Electronics (see below) but excluding batteries.

LIST A see October, 1979, page 634
LIST B see October, 1979, page 640
LIST C see April, 1980, page 253
All component requirements for the Teach-In 80 Series are covered by these three Lists.

LIST LISTS
C $A, B \& C$
SUPPLIER
Bi-Pak, Dept. EE, P.O. Box 6, Ware, Herts.
$£ 2.55 \quad £ 18 \cdot 00$
Electrovalue Ltd., Dept. EE, 28 St. Judes
Road, Englefield Green, Egham, Surrey.
Greenweld Electronics Limited, 443 Millbrook
Road, Southampton.
£2.75 £24.90

Home Radio, 234-240 London Road, Mitcham,
Surrey.
£3.00 £24.25
£7.50 £29•00
Magenta Electronics Limited, 98 Calais Road, Burton-on-Trent, Staffs.*
$£ 2.83 \quad £ 25.43$
A. Marshall (London) Limited, Kingsgate

House, Kingsgate Place, London NW6 4TA £4.03 £25.50
T. Powell, 306 St. Paul's Road, Highbury

Corner, London N.1.
£2.50 £22.50
All prices quoted are inclusive of VAT, postage and packing.
*Can also supply woodwork etc. for Tutor Deck, see advertisement.


This project describes the operation and construction of a simple, but very effective, automatic level controller or ALC. The device allows signals from a nominated source to be kept at a fixed volume when feeding a tape or amplifier system.

To appreciate the need for such a unit it is necessary to consider what happens when one makes a recording using a microphone feeding a tape recorder which has a manual record level adjustment.

When the recording is being made the level control must be adjusted to maintain correct modulation of the tape. Very loud sounds which occur could produce unpleasant overload distortion when the tape saturates magnetically. Then, on the other hand, very quiet sounds can be lost in the hiss of unmodulated tape if measures are not taken to increase the recording level.

Similar volume variations are experienced when using a public address or a discotheque microphone. The ultimate object of any of these systems is that information must be conveyed with the least disturbance to intelligibility, and the ALC helps to achieve this.

## PRINCIPLE OF OPERATION

The fundamental requirement of the ALC is that it must increase the amplification applied to low level signals and reduce the amplification applied to high level signals. The response of an ALC circuit in relation to a normal linear amplifier stage is shown in Fig. 1.

It can be seen that with the ALC connected the level of the input signal can vary quite considerably whereas the output level range is quite restricted.

The effect of reducing gain applied to high level input signals is called compression. And the opposite effect of increasing the
gain applied to the lower level signals is called expanding.

The unit described here performs both of the above operations so it could be called a compressorexpander (frequently called a compander). However the professional companders have many facilities which are required for use in broadcasting and recording studios. This unit cannot match these, but it performs the basic operation at low cost.


Fig. 1. Shows response curve of ALC in contrast to a linear gain amplifier.

A block diagram of the ALC and the circuit elements which are used to obtain the compression and expansion effects described above is shown in Fig. 2. It will be seen that a closed loop control system is employed, which means that the input of the system is controlled as a result of the output of the same control system.

The gain element is a single stage transistor amplifier which has negative feedback-negative
feedback is a method of controlling the gain of an amplifier by feeding back a portion of the output such as to oppose the original signal. As more output voltage or current is fed back to the input of the amplifier the net gain is much less than normal, and the opposite is also true. The less feedback applied then the higher the gain of the amplifier stage.

The amount of feedback is variable and made dependent on the drain to source (channel) resistance of a field effect transistor. The channel resistance is dependant upon the voltage between the gate and source terminals of the f.e.t. What results is a simple voltage controlled amplifier.

## CONTROL VOLTAGE

To control the gain the output signal must be continuously monitored. An a.c. signal for gain control is derived through a buffer amplifier which then drives the a.c. to d.c. converter which comprises a pair of diodes D1 and D2 which form a voltage doubler circuit. The output from the circuit is a voltage, the value of which is proportional to the output signal level. The d.c. voltage would normally be changing all the time with the output signal but a storage capacitor allows an approximate average value to be obtained.
The actual storage time controls the time taken for the voltage controlled amplifier to restore to its maximum. In the prototype the

value of the storage time is controlled by a potentiometer in order to make the device suitable for various applications.

The source signal can be fed to a fixed low level input mic input, e.g. low impedance microphone, and the higher level signals can be fed to the higher level auxilliary (AUX) input which is connected to a variable attenuator. This control avoids the possibility of the device continuously compressing.

## CIRCUIT DESCRIPTION

The complete circuit diagram is shown in Fig. 3.

There are two inputs to the circuit as described but the circuit is so arranged that the level control is not connected when the low level input is used. This avoids unnecessary signal loss. This is achieved by wiring of the break action contacts of the low level input jack, SKl.

Under no signal conditions the f.e.t drain-to-source resistance has a low value of only a few hundred ohms and this with the low reactance of C3 shunts R3 thereby removing the a.c. feedback path for the amplifier. The amplifier stage consists of TR2 and its bias components, and with the feedback virtually removed the gain of the amplifier if fairly high.

Output from TR2 is fed to a second amplifier, TR3, which feeds
a.c. signals to the a.c. to d.c. converter. Diodes D1 and D2 form a rectifier and voltage doubler, and the output appears across C9. The value of this voltage is directly proportional to the amplitude or "loudness" of the source signal
and is negative with respect to the zero volt rail. This negative voltage is applied to TRI gate terminal. The more negative the gate voltage the higher the drain-to-source resistance becomes, thereby having less shunt effect on
Resistors

## COMPONENTS-…

| R1 | $1 \cdot 5 \mathrm{M} \Omega$ |
| :--- | :--- |
| R2 | $6.8 \mathrm{k} \Omega$ |
| R3 | $3.9 \mathrm{k} \Omega$ |
| R4 | $1.2 \mathrm{k} \Omega$ |
| R5 | $47 \mathrm{k} \Omega$ |


Potentiometers
VR1 $25 \mathrm{k} \Omega$ log. law VR2 $1 \mathrm{M} \Omega$ carbon lin. law
Capacitors

| C1 | $33 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. |
| :--- | :--- |
| C 2 | $3.3 \mu \mathrm{~F} 6 \mathrm{~V}$ elect. |
| C 3 | $100 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. |
| C 4 to C6 | $8 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. (3 off) |
| $\mathrm{C} 7,8$ | $100 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. (2 off) |
| C9 | $10 \mu \mathrm{~F} 10 \mathrm{~V}$ elect. |



Semiconductors
TR1 2N3819n-channel f.e.t.
TR2, 3 BC109 silicon npn (2 off)
D1, D2 1 N914 small signal silicon (2 off)

## Miscellaneous

S1 single-pole on/off toggle
SK1 switched jack socket
SK2, 3 mono jack sockets (2 off) or other sockets to suit equipment B1 9V PP3
Stripboard: 0.1 inch matrix size 19 strips $\times 31$ holes; connector to suit B1;4BA fixings; case: aluminium/vinyl clad steel size $152 \times 114 \times 44 \mathrm{~mm}$; screened cable; control knobs (2 off); connecting wire.


Fig. 3. The complete circuit diagram of the Automatic Level Control.

R3, increasing its negative feedback so reducing gain.

If the input signal falls to a low level, the voltage at the negative plate of C9 decays through VR2 and R10. The result is to restore the gain of TR1.

The time taken for the gain of the amplifier to restore is known as the recovery or release time. It is related to the discharge of C 9 and if the parallel resistance is reduced C9 will discharge quicker; VR2 allows this time to be varied from a few milliseconds to a few seconds.


## CONSTRUCTION

The prototype was intended to be a general purpose unit for use with anything and everything where such a device would be advantageous. The case used was fairly small but large considering the circuit simplicity, and readers may wish to use the circuit board alone and mount the device in the case of the equipment for which it was built. If this is so, VR1 and VR2 can be replaced by preset type potentiometers.

The components are mounted on a single piece of stripboard; Fig. 4 shows the layout of the components on the topside of the board. There are no breaks to be made on the underside.

The board as shown is mounted using a single fixing hole with a thick insulated washer to isolate the board from the case. When mounting the components observe the correct polarity for the diodes, electrolytic capacitors and in par. ticular the transistors.

Begin construction by mounting the resistors and capacitors followed by the semiconductors. Novice constructors are advised to use a heatshunt on the legs of the semiconductors to avoid thermal damage. Attach suitable lengths of flying lead to reach the chassis mounted components. Note that screened lead is used for some connectors.


 HOW IT WORKS


Electrical signals developed in the microphone are passed to the tape recorder via a low gain amplifier. The resulting amplifier output level is sensed by the automatic gain control circuitry which adjusts the gain of the amplifier in the required manner. Low level microphone signals are boosted whereas high level signals are subject to attenuation. In this way low level signals do not become overshadowed by inherent noise in the mic. system and high level signals are prevented from overloading the tape input which would otherwise cause distortion.



Prepare the case to accept the sockets, switch and potentiometer, secure these in place, and then wire up according to Fig. 4.

The prototype was designed for general purpose usage and the inputs were all standard jacks but by drilling the appropriate sized holes DIN, phono or banana sockets may be used.

Perhaps for the most versatile unit a selectable combination of sockets could be devised. Many microphones and guitars are connected to amplifiers and auxillary equipment by means of standard mono jack plugs and so SK1 could
be a jack socket whereas the auxilliary input, SK2, would be a DIN or phono.

The completed unit was mounted in a commercially available case with a black vinyl lid. This gave the unit a neat appearance. The battery requirement is furnished by a PP3 and the use of double sided adhesive tape provides adequate support.

## TESTING AND USE

Connect a microphone, low output type to SK1 or high output type to SK2, and the output of the


## AUTOMATIC LEVEL CONTROL



Fig. 4. Shows the layout of the components on the topside of the stripboard. In the prototype no breaks in the copper strips were found necessary around the single fixing-hole. Also shows full interwiring between board and case mounted components.

unit to an amplifier input. A headphone output facility on the amplifier will be particularly useful and would eliminate possible positive feedback during the setting up.
With the unit switched on speak into the microphone. It should be possible to shout and whisper without hearing any distortion.

By turning the release time control fully anticlockwise the gain of the unit will restore to its
maximum in a very short time. This will be perceived by an increase in background noise level.
If these results are not obtained then the wiring will have to be checked, particularly check for solder bridges on the circuit board. The 0.1 inch matrix stripboard is prone to short circuits through solder blobs bridging adjacent strips and care must be taken when soldering.

For high level signals SK2 input must be used and the attenuator adjusted to allow an undistorted output to be obtained.

For use with a tuner to record a programme onto tape, the high level input is used, and VR2 should be set to its midway position. This setting will prove to be adequate for both music of the pop and light variety and for talks and chat shows. However, where the music is much slower the recovery time can be much longer, which is achieved by advancing VR2 clockwise.

The input attenuator VR1 must be set to avoid excessive compression which will be evident by output volume reduction as the input reaches a high level.

A more compact version has proved particularly useful for the author when connected to the microphone circuit of a portable tape recorder. Then when the tape recorder was used for interview work, no adjustment of the microphone level was needed and the ALC was able to cope with the differing voice levels. For this type of application the unit needs a fast recovery time, i.e. VR2 fully anticlockwise.

## BOOK REVIEWS

TELEVISION \& RADIO 1980<br>\(\begin{array}{lll}Price \& £ 2 \cdot 50 \&<br>Size \& 230 \mathrm{~mm} \& 190 \mathrm{~mm}\end{array}\)<br>Publisher Independent Broadcasting Authority<br>ISBN 0900485345

ONCE again its a pleasure to read the "behind the scenes" stories of our independent television and radio services.

This year's edition gives a fairly concise guide to the many aspects of programming, technical developments and advertising controls; i.e. code of practice on what's acceptable and unacceptable material and details of better viewing and listening.

The handbook must be one of the very few publications that has not increased in price from last year and retained the same number of pages (224) and abundant illustrations. Unfortunately, the printing and visual appearance does not measure up to the high standards set by previous editions. However, the 1980 edition is still very good value for money.

Perhaps this criticism is a bit harsh and may be due to the growth in local broadcasting and trying to pack a "quart into a pint". Maybe, with the increasing growth and interest in local radio it's time a separate book dealing solely with radio was issued.

It seems paradoxical that having just read the section on their plans and optimisms for the 80 s , comes news that the proposed launching of the new channel may be delayed due to lack of funds.
D.G.B.

ELECTRONIC PROJECTS INDEX No. 21978

Compiler Price Size
Publisher £1.30 $297 \times 210 \mathrm{~mm} 48$ pages (Paperback) North Tyneside Metropolitan Borough Council, Libraries and Arts Dept., North Shields, Tyne and Wear ISBN 0142-1565

THIS is a guide to constructional projects published during 1978 in 16 well-known magazines which in total cover practically the entire field of di.i.y. electronics. It carries on (in the same style and format) from Electronics Projects Index 1972-1977 published at the beginning of 1979.
Projects are listed under 36 headings: an extensive list of subjects which itself is quite revealing as to the wide extent of electronics applications.
Individual entries give magazine title, issue and page numbers, then brief details including component complement and usually the form of construction e.g. P.C.B., Veroboard.
The largest section is Measuring and Test Instruments with 127 individual items listed, runners up being Music Effects and Musical Instruments ( 50 projects), Amplifiers (40), Automobile (37), P.S.U. (37), Games (34). Other subject groupings including Alarms, Calculators, Locks, Metal Locators, Receivers, Timekeeping, run to 30 or less projects each.
If this predominance of Test Gear and P.S.U. articles truly reflects the general demand, one is lead to the conclusion that the electronics constructor is essentially serious-minded and puts his working tools and instruments before all other kinds of projects.
F.E.B.


## By ADRIAN HOPE

## Breaking a Monopoly

The Post Office monopoly is now finally crumbling. Shortly after Sir Keith Joseph's historic statement promising a new era of freedom and enterprise for U.K. telecommunications, the Post Office issued a press release which was surprisingly not extensively reported. "From next year'", reads the press release "customers will be able to buy as well as rent telephone answering machines".
Until now, of course, anyone wanting to install a machine to answer their telephone and record messages has had to rent one from a Post Office approved supplier. These machines are remarkably complicated beasts. I know; I once bought a couple of ex-rental machines.

Over the last year, all manner of relatively inexpensive, but very efficient and electronically simple answering machines have been coming in from the USA either in traveller's suitcases or by bulk import for open sale in the increasing number of shops now offering "illegitimate" telephone gadgetry. It was a foregone conclusion that once the government had decided to chip away the Post Office monopoly telephone answering machines would be the first gadgetry to become legitimate for subscriber purchase and connection.

The government aims eventually to replicate the USA situation where the telephone company's monopoly ends at the front door, just like the gas, water and electricity supplies. But it will take time to make such a wholesale change and the use of "illegitimate" subscriber owned telephone answering machines is now so widespead that it's the obvious place to start with a change.

In some parts of the country the Post Office has already been recommending local suppliers of USA equipment when subscribers enquire about teleph one answering machines. The Post Office has put on a brave face about the official volte face over answering machines, claiming that rentals were previously required "so that the machines could easily be traced for modification when necessary" and that it's "progressive developments in the manufacture of these machines' ${ }^{\prime \prime}$ that have made possible a change in attitude. But the writing is now on the wall. Perhaps, appropriately, the new scheme comes into operation after April 1, 1980.

## Cordless Telephone

However, despite misleading publicity to the contrary, for the foreseeable future, you will not, repeat not be able to use cordless telephones. Advertisements have recently been appearing in the national press offering a cordless phone which is "easy to install",

The publicity material which is sent off to anyone who writes in for further details claims that "Following more press announcements on Sir Keith Joseph's plans for the Post Office services, we are giving you a great opportunity to be one of the first people to take advantage of this exciting new technology . . . our phones are easy to install and are completely compatible with the British system."
The cordless 'phone being offered for sale (at around £250) may well be easy to install and may well be completely compatible with the British telephone system, but it relies for its cordless connection on a radio link that is 100 per cent illegal under our old friend the Wireless Telegraphy Act 1949. This, of course, is the law which makes the use of CB sets illegal. The penalties for using a radio cordless telephone are in fact the same as for using a CB walkie-talkie: up to $£ 400$ fine and/or three months in jail.
In the USA such cordless 'phones are, like CB, legal. Moreover, there is no ban on importing them into the UK provided of course duty and VAT is paid. This is because those on sale in the UK work on the $1 \cdot 6-1 \cdot 8 \mathrm{MHz}$ and $49 \cdot 8-49 \cdot 9 \mathrm{MHz}$.
In an effort to curb the spread of CB, a 1968 modification to the W.T. Acts outlawed the importation of 27 MHz transceiver equipment. But this does not prevent the import of equipment operating on other frequencies. There is also nothing to prevent the advertisement or sale of such equipment.
But the acts do make it illegal to use such transceivers in the UK. What's more the Post Office can object to the connection of any unauthorised equipment to a subscriber's line, and if necessary disconnect at the exchange.
So although importing, advertising and selling a radio link wireless telephone is legally in the clear, the poor customer who pays his honest $£ 250^{\circ} 00$ is in anything but clover. He stands to have his telephone cut off by the Post Office and be fined and jailed into the bargain.

Incidentally, the public files of the British Patent Office reveals that one of the British Post Office's main suppliers, STC is now working on an infra-red linked cordless telephone. This will be both legal and much more secure in use.
Whereas a wireless link spreads signals at least 100 yards around the system and so enables anyone in that area to eavesdrop on telephone conversations (incidentally it also gives officialdom an easy opportunity to detect illegal use) the infra-red link won't stray outside the wall of the user's home.

## X-ray Time

Until a few years ago radiographers, who operate the $X$-ray examination equipment in our hospitals, grew tired of reassuring patients that there was no need to remove their wrist watches before examination. Now they are growing tired of saying just the opposite.
Many British hospitals are posting notices advising $X$-ray patients to remove their watches before examination. The turnaround dates back to a warning letter published in a medical journal.

Although ordinary mechanical hourand minute-hand watches are unaffected by $X$-rays, it seems that the same may not be true of electronic watches. There have now been several reports of digital watches stopping while the wearer is being $X$-rayed. Sometimes they start again. Sometimes they don't. In one case a watch simply skipped an hour.

A leading watch manufacturer quizzed on the problem has confirmed that the CMOS chips used in a digital watch certainly can be affected by high levels of radiation, and also intense magnetic fields. In some cases the chip recovers and in others simply stops working. But the simple truth is that no one really knows whether the relatively low levels of radiation used in hospitals for routine examinations are, or are not, significant.

Tests carried out have also been inconclusive because there are any number of different types of electronic watches, all with different thicknesses of shielding metal around the chip. Also there are all manner of different medical $X$-ray techniques, all involving a different dose on the patient's wrist.

## Play Safe

The manufacturer acknowledged that "there is still" somewhat of a grey area in CMOS technology" and it may well be years before enough incidents have been correlated to give a clear picture of the true situation. In fact, now that hospitals are "playing safe" and advising patients to remove their watches, we shall probably never know.

Similarly, we shall probably never now know whether there was any real basis in the suggestion of a tew years ago that high level $X$-ray inspection equipment at airports presented a risk to electronic equipment. The airlines have also "played safe" and there is now hardly an airport left in the world which uses high dosage baggage inspection equipment.

Anyone who constructs electronic prototype equipment, whether for a hobby or for business, would however be well advised to keep all chips well clear of $X$-ray radiation (and strong magnetic fields) until the matter is resolved.


T${ }^{\mathrm{HE}}$ transistor is undoubtedly the single most important device in electronics today. Although its actual operation is only fully understandable with a knowledge of advanced physics, we do not need to know exactly what is going on inside a device in order to make use of it.

The term transistor is today used to refer to many different types of device. There are bipolar transistors, field effect transistors (f.e.t.s.), unijunction transistors and many others. Each has its own special characteristics and is particularly suitable for specific applications.

The type of transistor with which we will be concerned in this part of the series is the bipolar type, the most common type of discrete transistor.

## THREE TERMINALS

All of the devices that we have looked at so far were relatively simple to understand since they had only two terminals. Any current entering. one terminal could only leave by the other terminal.

The first noticeable fact about transistors is that they have three terminals, so current entering any terminal could appear at either of the other terminals or, in fact, both.

To make any sense of transistors we must be quite sure
which terminals we are referring to, and to this end each is given a special name. The problem of lead identification on real transistors is complicated by the fact that there is a multitude of different packages in which the transistor chips themselves are mounted and enclosed.

Each type of transistor (by which we mean chip not package) has a unique code number ( $0 C 71$, $\mathrm{BCl} 08,2 \mathrm{~N} 3055$, etc) but different manufacturers may put the same type of chip in different packages.

The diagram in Fig. 7.1 shows the lead identification for some


Fig. 7.1. (a) and (b) show the circuit symbols for npn and pnp transistors respectively. (c) and (d) show the lead identification for two common types of translstor package. The packages are seen looking at the leads.
common transistor packages but, be warned: if you come across a transistor serial number that you have not met before, the only certain way to identify the leads is to check with published data, either in the form of transistor data books or tables which quite often appear in electronics magazines or, if this proves unsuccessful, direct from the manufacturer's own data.

The three leads are labelled emitter (e), collector (c), and base (b) and we must always make sure that the transistor is connected with these leads in the right place or damage could be done.

## GERMANIUM AND SILICON

There are two main types of material from which transistors are fabricated. The early transistors used germanium, a brittle white metal which is quite rare. Today's technology is centred around silicon, a non-metal with chemical properties quite similar to carbon. It soccurs naturally in abundance as silica (of which sand is the impure form).

The advances in recent years have been in ways of purifying the silicon and of growing very precise crystals. Whilst germanium transistors are still used to some extent in specialist applications, silicon is now used almost exclusively.

Silicon transistors have the advantage that they are much less prone to a destructive process known as thermal runaway which can destroy a transistor if the circuitry around it is not carefully designed.

The problem is that the leakage currents through germanium transistors could be quite high and these leakage currents increase dramatically with temperature. Since the increased current caused heating of the transistor there was a vicious circle (or, to give it its technical term, positive feedback) which eventually destroyed the device through overheating.

In silicon transistors the leakage currents are virtually negligible and so the heating effect which they produce are not of any importance.

The higher leakage currents through germanium also meant
that the circuitry around them was slightly more complicated, which is another factor in favour of silicon.

The symbol for the transistor (see Fig. 7•la and b) does not distinguish between the two types of transistor and so one must refer to transistor data to determine the material from which a particular transistor is made.

## PNP AND NPN

If we look at the diagram showing the internal construction of a transistor we will find that it is like the diode we looked at earlier with a $p$-n junction but another oppositely doped section has been added on the end.

The oppositely doped section can be added at either end (Fig. 7.2) thus producing two types of transistor: npn and pnp. The symbols for these two types is different, the arrow on the emitter lead being reversed.

It might be thought that simply adding another junction to the first would simply form a double diode as indicated in Fig. 7.3 and, up to a point this is so. If the emitter lead is left open circuit and the base-collector terminals only are used then we would have something that appears exactly like a diode. Similarly if the collector is left open circuit then the baseemitter behaves like a diode.

The interesting and useful thing is that when the base-collector junction is reverse biased then the forward current through the baseemitter junction is able to control the current through the collector. But not only does the base current control the collector current, we also find that only a tiny base current is needed in order to control quite large currents through the emitter.

So far the description has used fairly vague terms like "through" rather than "into" or "out of" and this is to keep the description applicable to both $n p n$ and pnp transistors.

## CURRENT AMPLIFIER

To sum up the operation of a transistor in one sentence we could say that a small current flowing into the base of a transistor controls a much larger current flowing into the collector. To put it


Fig. 7.2. The doping of the various sections of npn and pnp transistors. The arrows indicate the flow of conventional current through the two types when operated in their normal modes. In real transistors the base layer is very thin in relation to the collector and emitter sections.


Fig. 7.3. When viewed in isolation the base-emitter and base-collector sections of a transistor appear as diodes. it is when the base-collector junction is reverse blased and the base-emitter is forward biased that the transistor becomes interesting.
another way: the transistor is a current amplifier.
If we look back at the symbol for a transistor we see that the emitter lead has an arrow on it. This arrow indioates the direction of flow of conventional current when the transistor is used in its
normal operating mode. The direction of the arrow is used to differentiate between the $n p n$ and pnp types of transistor.
When one looks back at circuits from say fifteen years ago one finds that nearly all of them were built using pnp transistors. Today there is an overwhelming preponderance of $n p n$ transistors with pnp types only occurring occasionally. The change is not simply due to fashion it reflects changes in manufacturing technology.

## CURRENT GAIN

Since no current can "disappear" inside the transistor all current entering the device must appear as current leaving it. Thus we can say that the emitter current (that is current leaving the transistor) must equal the sum of the base and collector currents (those entering the transistor). Using mathematical notation :

$$
I_{\mathrm{e}}=I_{\mathrm{b}}+I_{\mathrm{o}}
$$

where $I_{e}$ is the emitter current, $I_{0}$ the base current and $I_{c}$ the collector current.
What can we deduce from this starting point? If the base current is zero (as will be the case when it is left open circuit) then the emitter current will be the same as the collector current. If the collector current is zero (collector open circuit) then the based current will be the same as the emitter current.


Some typical transistor packages (all to scale) with identification of leads or pins. The TO3 package is used for high power transistors, all other examples are small signal transistors.

There are two ways in which the emitter current can be zero: either $I_{\mathrm{c}}=-I_{\mathrm{b}}$ (the same current flows into the base and out of the collector) or both collector and base current are zero.

Let us connect up an actual circuit on the Tutor Deck to see exactly how the transistor (type $\mathrm{BCl} 08)$ behaves

The circuit is shown in Fig. 7.4 and it will be seen that we have connected the emitter of the transistor to the 0 V line and put a meter in the collector circuit which then goes up to +18 V . In the base of the transistor we have a resistor which can be connected to the 18 V line by pressing the switch $S 2$.

When the switch is not pressed we see that the current through the collector is virtually zero. The only current that is flowing is what is termed the "leakage current" and, for the BCl 108 , it can be taken as negligible.

When the pushbutton is pressed we see that the meter swings well over indicating a current into the collector of about two to 16 mA . How much current was flowing in the base when this current was flowing in the collector?

## BASE CURRENT

To work out the base current to a fair degree of accuracy we can make a few assumptions. The baseemitter junction is in effect a forward-biased silicon diode.

In the section of this series on diodes we noted that the forward voltage drop across a silicon diode never exceeded about 0.7 V . In fact, the assumption is perfectly valid for the transistor base-emitter junction.

Now 0.7 V is under five per cent of the supply voltage of 18 V so ignoring it will only introduce a five per cent error. The base current is therefore given (approximately) by the supply voltage divided by the base resistor (R1). This works out to be $18 \mu \mathrm{~A}$.

What we have been measuring is perhaps the most important characteristic of the transistor: its d.c. current gain. The current gain is defined as the collector current divided by the base current and it is given the symbol $h_{F \%}$ or sometimes $\beta$.

$$
h_{\mathrm{PE}}=\frac{I_{\mathrm{c}}}{I_{\mathrm{b}}}
$$

## PART 7 QUESTIONS

7.1. The arrow on the transistor symbol is on the:
a) emitter
b) base
c) collector
7.2. The gain (hFE) of a transistor is quoted as being 100. What is collector current at a base current of $10 \mu \mathrm{~A}$ :
a) $10 \mu \mathrm{~A}$
b) $100 \mu \mathrm{a}$
c) 1 mA
7.3. The collector current in a transistor is measured as being 10.4 mA whilst the emitter current is 10.6 mA . What is the $h_{\text {FE }}$ of the transistor:
a) 104
b) 52
c) 53

Now this figure depends to some extent on the collector current inquestion and tends to be lower at very low and very high currents than it is at medium currents. The terms "low", "high" and "medium" will vary from transistor to transistor, medium being between 1 and 10 mA for the BC108.

The manufacturer's data states that $h_{\text {PE }}$ can vary between 110 and 800 which is a very wide range. See if the transistor on which you are making the measurements falls within this range.

If we return to the first equation that we derived we can eliminate one of the terms, namely $I_{0}$ and get the emitter current in terms of the base current and $h_{\text {PE }}$.

$$
\begin{gathered}
I_{\mathrm{e}}=I_{\mathrm{c}}+I_{\mathrm{b}} \\
I_{\mathrm{e}}=\left(h_{\mathrm{FE}} \times I_{\mathrm{b}}\right)+I_{\mathrm{b}} \\
I_{\mathrm{e}}=\left(h_{\mathrm{FE}}+1\right) \times I_{\mathrm{b}}
\end{gathered}
$$

What this is saying is that the emitter current will be only different from the collector current by the magnitude of the base current and, since this is so small, it will be difficult to measure any difference between the two.

To check that the emitter current is as predicted, it might be thought that it is simply a matter of moving the meter to the emitter lead of the transistor, but doing this introduces a complication into the circuit which it is important to appreciate.

The meter itself (if by "meter" we take to mean the meter and its shunt resistor in parallel) has
7.4. $\mathrm{P}_{\text {tot }}$ (max) for a transistor is quoted as being 500 mW . When the collector to emitter voltage is 2.5 V what is maximum current that can be taken through the collector:
a) 200 mA
b) 500 mA
c) 100 mA
7.5. If $I_{c}$ (max) is 150 mA and $h_{\text {FE }}$ is $110-800$ what is the maximum base current that should be fed into the transistor assuming there is no limitation on the collector current:
a) 1.367 mA
b) $187.5 \mu \mathrm{~A}$
c) 1 mA

## PART 6 ANSWERS

6.1. b) 6.2 c) 6.3. c) 6.4 . b) 6.5 . a)
a resistance and thus any current that flows through it will produce a voltage drop by Ohm's Law. When it is placed in the emitter lead the emitter current which we are trying to measure will produce a voltage drop which effectively reduces the voltage across the base resistor R1.

We are expecting an emitter current of about 10 mA so what will be the voltage drop across the meter at this current? By application of Ohm's Law we find that it will be about $0 \cdot 1 \mathrm{~V}$. Fortunately this voltage is very small and it can again be ignored in comparison with the total voltage across the meter, transistor and base resistor (see Fig. 7.5).

As before, virtually no emitter current flows when the base is open circuit. When the button is pressed the reading on the meter should be indistinguishable from the previous reading, confirming the calculations.

## CONFIGURATIONS

What we have looked at in the previous section are the two most commonly used transistor configurations. They are given the names "common emitter" and "common collector" respectively. The adjective "oommon" is used to describe the terminal whose voltage is fixed either by connecting to the power supply rail or to some other invariant voltage.

## EXPERIMENT 7.1 : COLLECTOR V. BASE CURRENT

Components needed: BC108 transistor, $10 \Omega+W$ resistor, $1 \mathrm{M} \Omega+\mathrm{W}$ reslstor.


Fig. 7.4 (a)
Fig. 7.4 (b)
Fig. 7.4. (a). Circuit of Experiment 7.1 and (b) the layout of the components on the Tutor Deck.

The circuit for this experiment is shown in Fig.7.4a and the layout on the Tutor Deck in Fig.7.4b.
The meter on the Deck Itself can only measure current in the order of a few hundred microamps so a 10 ohm resistor (called a shunt resistor) is placed in parallel with it so that the resulting meter-resistor combination appears to be able to measure much higher currents.

Depending on the full scale current of the meter and its internal resistance, the effective full scale reading of the meter will vary but if both of these are known then the full scale current is given by

$$
I=\frac{R_{\mathrm{m}} \times I_{\mathrm{fsd}}}{10}+I_{\mathrm{fsd}}
$$



A typical $100 \mu \mathrm{~A}$ meter has an internal resistance of around 1700 ohms giving a full scale reading of just over 17 mA .

Note that the meter reads virtually zero when the base is open circuit.

EXPERIMENT 7.2: EMITTER CURRENT V. BASE CURRENT

## Components n eeded: as above

This is a repeat of the previous experiment except that the meter has been moved to the emitter lead of the transistor. See text for further description of this circuit. The clrcuit ls shown In Fig.7.5a and the layout on the Tutor Deck in Fig.7.5b.


Fig. 7.5 (a)


Fig. 7.5 (b)
Fig. 7.5 (a). Circuit of Experiment 7.2 and (b) the layout of the components on the Tutor Deck.

Components needed: BC108 transistor, $100 \mathrm{k} \Omega+\mathrm{W}$ resistor, $2 \cdot 2 \mathrm{k} \Omega+\mathrm{W}$ resistor, $220 \mathrm{k} \Omega \frac{1}{4} \mathrm{~W}$ resistor.


Fig. 7.6 (a)
Fig. 7.6 (b)
The circuit for this experiment is shown in Fig.7.6a and the Tutor Deck layout in Fig.7.6b.
Use the scale which we produced for the potentiometer in association with the $100 \mathrm{k} \Omega$ potentiometer on the Tutor Deck. The meter is used in this circuit as a voltmeter since a resistor has now been placed in series with it. The full scale reading of the meter will correspond with $220 \mathrm{k} \Omega \times \mathrm{I}_{\mathrm{fs}}$ (or about 22 V for a $100 \mu \mathrm{~A}$


Fig. 7.6 (a). Circuit of Experiment 7.3 and (b) the layout of the components on the Tutor Deck.
meter). The internal resistance of the meter is not important here as it will be small in comparison with the $220 k \Omega$ resistor.

Note down the meter readings for various settings of the potentiometer scale. These readings do not have to
be in volts, they can simply be in meter divisions; we are really just acquiring some figures for comparison with the next experiment. However, knowing that the meter is reading 22 V full scale gives a feeling for the sort of voltages we are looking at.

## EXPERIMENT 7.4: VOLTAGE AMPLIFICATION (EMITTER RESISTOR)

## Components needed: as above



Fig. 7.7 (a)
Fig. 7.7 (b)
The circuit of the next experiment is shown in Fig.7.7a and the layout in Fig.7.7b. This is very similar to the previous experiment but this should not mislead you into believing that the circuit behaves in the same way.
Taking a few meter readings for different settings of the potentiometer soon reveals that this circuit is much "better behaved" than the previous circuit in that the output tends to follow the setting of the potentiometer much more closely than in Experiment 7.3.


Fig. 7.7 (a). Circuit of Experiment 7.4 and (b) the layout of the components on the Tutor Deck.

The third configuration "common base" where the base is held at a fixed voltage and the collector current is used to control the emit-
ter current is not often encountered and so will not be described here.

## VOLTAGE AMPLIFICATION

We have seen how the transistor can be used to amplify a small current, but often we are more interested in amplifying small voltages. The first thing that we must do is convert the voltage that we wish to amplify into a current so that this can be fed into the base of the transistor.

The simplest way is to put a resistor of the appropriate value in series with the input voltage. This is possible but one must be very careful to make sure that whatever the input voltage, the transistor is operating as it should. We shall examine this problem in more detail when we look at the transistor as a linear amplifier.

To convert the output current into a voltage is much less of a problem although one must be clear about what effect this has on the operation of the transistor.

Fig. 7.6 shows a resistor (R2) inserted in the collector lead of the transistor. The meter has now

## ADDITIONAL COMPONENTS FOR PART 7 ONWARDS (LIST C)

Resistors
2 off 330 ohm 2 off 220 kilohm 2 off $2 \cdot 2$ kilohm 2 off 470 kilohm 2 off 22 kilohm 1 off 1 megohm
2 off 68 kilohm
All $\ddagger$ W carbon $\pm 20 \%$

## Capacitors

| 2 off | $0.01 \mu \mathrm{~F}$ polyester |
| :--- | :--- |
| 3 off | $0.022 \mu \mathrm{~F}$ polyester |
| 2 off | $10 \mu \mathrm{~F} 16 \mathrm{~V}$ (or higher) |
| , | electrolytic, axial lead |

Transistors
4off BC108 npn silicon bipolar
1 off $\quad$ BC178 pnp silicon bipolar 1 off 2N3819 $n$-channel f.e.t.

Integrated Circuits
1 off CA3140 linear MOS f.e.t. operational amplifier
1 off CD4024 (or HEF4024 or MC14024) CMOS 7 -stage binary counter
For details of suppliers of the above components see Shop Talk (page 241)
been moved out of the circuit and acts as a voltmeter since it has a series resistor. We are now using a potentiómeter to vary the base current of the transistor.

Note how the meter reading varies as the potentiometer is varied. The great trouble with this circuit is that the results will vary according to the gain of the transistor. In an actual circuit it would be very awkward if the gain of the transistor had to be selected for the circuit to work properly.

In Fig. 7.7 the resistor has been moved to the emitter. It turns out that the circuit behaves much more predictably now-we have somehow made the spread in gain of the transistor much less important. This is because we have produced what is called an "emitter follower" circuit. This will be examined more closely in Part 9, but you might try working out what is going on in this case.

## TRANSISTOR DATA

Table 7.1 shows transistor data as might appear in a catalogue. What do all the terms mean and why have these in particular been chosen?

The first column is the type of the transistor to which the following data refers. Only three are shown here, two low current type, one $n p n$ and one $p n p$, and one power transistor.

The next column shows the material from which the transistor is made and whether $n p n$ or $p n p$.

The next column gives a quick guide to any special features of the transistor, if there are any. The first two are simply general-purpose types with nothing special about them, whilst the 2 N 3055 is a high power type.

The next column gives a power rating of the transistor and is designated $P_{\text {tot max }}$. This is the total power that can be dissipated by the transistor without damage.

Now, the base current is usually very small as compared with the emitter or collector currents and the emitter and collector currents only differ by the base current.

The power dissipation of a transistor can thus be approximated by multiplying the voltage from collector to emitter by the current into the collector.

$$
\left.P_{\text {tot }}=V_{\mathrm{ce}} \times I_{\mathrm{c}} \text { ( approx. }\right)
$$

Thus the voltage across the collector to emitter times the collector current for a BC108 should not exceed 360 mW .

This does not imply that the current through the collector can be 360 mA if the collector to emitter voltage is $1 V$ as there is a limitation on the collector current and this is given in the next column headed $I_{c \text { max }}$.

The next column is headed $V_{\text {ceo max }}$ and this is read as the maximum collector to emitter voltage that the transistor can withstand with the base open circuit. This voltage is important as it limits the power supply rail which can be used with the transistor. It effectively says that a BC108 cannot be used with a voltage rail of more than 20 V unless special precautions are taken.

The next column is the maximum reverse voltage that the baseemitter junction can withstand without damage, assuming the collector is open circuit. Note that it is quite low and does not vary much between low current transistors such as the BCl08 and high power transistors like the 2 N 3055 .

In linear circuits one would not usually expect that voltages large enough to reverse bias the baseemitter junction will ever exist but in switching circuits one quite often finds large reverse voltages being potentially generated.

The column headed $h_{\text {FE }}$ gives the d.c. current gain of the transistor. The BCl08 and BC478 both have very high gains whilst the power transistor has a much lower gain.

The last column gives a frequency ( $f_{t}$ ) for each transistor which is that at which the gain of the transistor drops to unity.

It is an unpleasant fact of life that the gain of transistors drops off as the frequency of the applied voltage is increased.

Next month we will look at the use of transistors as switches.


IN this sixth and final part to the series we provide full details for the construction of the battery charger, which will be used to re-charge the Nicad batteries used in the transmitter and receiver, and also describe the setting up of the pulse width now that all the system equipment has been covered.

As with all projects of this size, there will be some constructors who will have problems of some form or other therefore information has been included to try and point the constructor towards the area where the fault may lie.

## BATTERY CHARGER <br> CIRCUIT

The charger unit described here for charging the batteries is of the constant current type, the circuit is given in Fig. 6.1.
The secondary of the mains transformer Tl provides 15 V which is
rectified by the bridge circuit composed of diodes DI-D4. The output is smoothed by Cl and the resultant 20 V d.c. applied to two separate constant current transistors TR1, TR2.
If we consider the transmitter section, the Zener D5 provides a reference voltage with Rl supplying the current through it. If D5 is 4.7 V
then the emitter of TRI is 0.7 V below this at 4 V , therefore this voltage across R2 will define a current through the emitter. With R2 being 82 ohms the current is approximately 50 mA .

This current as well as flowing through the batteries undergoing charge (via PLI) also flows through

Fig. 6.1. Circult of the battery charger.

 plug wiring.



Fig. 6.2. Circuit board (a) p.c.b. pattern, actual size (b) component layout on other side of board.

## COMPONENTS

## BATTERY CHARGER

Resistors

| Resistors | $2 \cdot 2 k \Omega$ | $\pm W \pm 5 \%$ |
| :---: | :--- | :--- |
| R1 | $22 \Omega$ | $+W \pm 2 \%$ |
| R2 | $82 \Omega$ | $+2 k \Omega$ |
| R3 | $2 \cdot 2 k \pm 5 \%$ |  |
| R4 | $180 \Omega$ | $W \pm 2 \%$ |
| R5 | $150 \Omega$ | $\frac{1}{2} W \pm 2 \%$ |

Capacitor
$\mathrm{C} 1 \quad 220 \mu \mathrm{~F}$ electrolytic 25 V

## Semiconductors

TR1, 2 2N3053 non (2 off)
D1-4 ZS170 or similar 0.5A rectifier (4 Off)
D5, 7 BZY88C4V7 4-7V Zener (2 off)
D6, 8 TIL220 l.e.d. (red) with mounting clips (2 off)

Miscellaneous
PL1 DIN plug 3.way
PL2 Plug-socket 2-way (SLM)
S1 Miniature s.p.d.t. switch
T1 Mains transformer. 0.240 V primary: 0.15 A 200 mA
Samos Case $100 \times 65 \times 50 \mathrm{~mm}$ (West Hyde). TO5 heatsinks (2 off). Grommet $\frac{3}{32} \mathrm{in}$. (2 off). Grommet $\frac{1}{4} \mathrm{in}$. internal dia. meter. Connecting wire
the series l.e.d. D6 which acts as an indicator to show that the batteries are in fact charging.
A similar circuit arrangement is provided for the receiver section. Here alternative charging currents are provided for by adjustment of TR2 emitter resistor. With S1 in the "High" position, R4 is in circuit, but when S1 is set to "Low" R5 is inserted in parallel with R4, thus reducing the effective emitter resistance. The "High" position current is 50 mA , to suit 500 mA and 600 mA cells. The "Low" position current is 22 mA to suit 225 mA and 300 mA cells. The receiver battery is connected via PL2.

Remember that when charging the current goes into the positive side of the cell so the positive side of the battery is connected to the +20 V line whilst the negative side goes to the l.e.d.

## CHARGER CONSTRUCTION

The charger construction is relatively simple and straightforward. The components for the p.c.b. should be inserted in their corresponding positions according to Fig. 6.2, and then the wires can be attached. The wires to the l.e.d.s, switch and transformer come off the component side whilst the outputs to the batteries come from the copper side.

The lid for the case is drilled as in Fig. 6.3 after which the l.e.d.s, switch and grommets can be inserted, making sure that the clips are used to hold the l.e.d.s in place.

Two holes should be drilled in the case base for the transformer, dependent upon its size, together with a hole in the case side large enough to accept the large grommet for the mains cable.

The plugs for the transmitter and receiver battery packs are attached as in Fig. 6.3 with the receiver plug having a length of sleeving over the soldered joints (see inset). When wiring up the switch make sure that it is connected correctly for the "High" and "Low" currents.

## TESTING

When construction is completed, one last overall check is always worthwhile. Plug the unit in and with the multimeter set to the 100 mA d.c. range connect across the output pins of the DIN connector and the meter should read around 50 mA . Then check the receiver side and the currents should measure 50 mA on the "High" range and 22 mA on the "Low".

If no current flows check the polarity of the l.e.d.s as these can be easily inserted the wrong way round. When the meter is connected and current flows the l.e.d.s should

TABLE 6.1
CHARGING TIMES

| Capacity <br> (mA H) | Charging <br> Current | Flat | 3 hrs. use | 2 hrs. use | 1 hr. use |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 225 | 22 mA | 14 | 12 | 10 | 5 | 2 Servo's + Rx |
| 300 | 22 mA | 18 | 12 | 10 | 5 | 2 Servo's + Rx |
| 500 | 50 mA | 14 | 10 | 8 | 4 | 2 Servo's + Rx |
| 500 | 50 mA | 14 | 14 | 10 | 5 | 4 Servo's Rx |
| 600 | 50 mA | 18 | 14 | 10 | 5 | 4 Servo's + Rx |
| 500 | 50 mA | 14 | 10 | 8 | 4 | Tx |
| 600 | 50 mA | 18 | 10 | 8 | 4 | Tx |

light up and on the receiver the "Low" range should produce an intensity slightly lower than for the "High" range.

## LENGTH OF CHARGE

Charging is usually carried out for a specified period of time dependent upon the capacity of the cells. Table 6.1 gives a rough guide to charging time against the state of charge, that is how long the battery has been used for and battery capacity. Although in the transmitter and receiver we recommend the use of 500 mA cells the other capacities are included for completeness and
because they are readily available to the modeller and may be purchased instead.

As seen from Table 6.1 we have given these recommended charging times for when the batteries are only partly discharged. These can be used regularly. However it is strongly recommended that at least once a month the batteries are given a full discharge followed by a full recommended charging period to ensure the life of the cells. It should also be pointed out that at the charging ourrents involved no damage is done to the cells should they be left on longer than the periods specified.

TABLE 6.2b
TRANSMITTER FAULT FINDING CHART
If there is plenty of r.f. present but no modulation the following chart may be of some use. All voltages are with respect to ground.

| Short b \& e of TR6 | r.f. | TR6 faulty |
| :---: | :---: | :---: |
|  | continues |  |
| r.f. disappears |  |  |
| Remove short on TR6 Short b \& e on TR1 | r.f. | TR1 faulty |
|  | continues |  |
| Check voltage IC3 pin 13 | $\checkmark$ low | R15 faulty |
| $\begin{aligned} & \text { approx. } \\ & 1 \cdot 2 \mathrm{~V} \end{aligned}$ |  |  |
| Check voltage IC3 pin 10 | $V$ high | R20 faulty |
| $\begin{aligned} & \text { approx. } \\ & 6.8 \mathrm{~V} \end{aligned}$ |  |  |
| Check voltage IC3 pin 5 | $V$ high | R13 faulty |
| $\begin{aligned} & \text { approx. } \\ & 1 \cdot 2 \mathrm{~V} \end{aligned}$ |  |  |
| Check supply and connections to all sticks |  |  |

## SETTING UP PULSE WIDTH

The procedure to be described here (as mentioned in the final paragraph of Part 2) is for those constructors who have no access to an osclloscope nor have any other R.C. equipment to make use of.

Up to this stage the constructor should have tuned up the transmitter and the receiver as described in Parts

2 and 3 and all that remains is to set up the pulse width. This is done by first choosing a servo and by removing the potentiometer body to find out where the wiper is and to mark its position on the output disc.
Now replace the pot body and rotate the output disc by hand so that the wiper is in the middle of the pot
track, and so has an equal distance to rotate in either direction to reach the end of the pot track.

With the sticks in the neutral position on the transmitter, plug the servo into the receiver and with both transmitter and recelver on, the servo should now rotate to some position at either side of its centre position. By adjusting VR7 (on the transmitter) the servo can be made to come back to this central position.

TABLE 8.2a
TRANSMITTER FAULT FINDING CHART
If it is not possible to tune VC1 and VC2 to get r.f. then the fault could be In one of many places. The foliowing sequence may be of some assistance. All voltages are with respect to ground.


TABLE 6.3
RECEIVER FAULT FINDING CHART

| SYMPTOM | CURE |
| :---: | :---: |
| 1. ICI pin 2 voltage low | (a) caused by shorted track <br> (b) C5 faulty or incorrect polarity <br> (c) check value of R1 <br> (d) IC faulty or incorrectly inserted |
| 2. TR1/2 emitter voltages incorrect | (a) too high-either collector/base short on track or faulty transistors(s) <br> (b) too low $\}$ suspect R8 or more probably a but(5) O.K. $\}$ base/emitter short in TR1 or TR2 |
| 3. Can IF transformer T3 low volts | (a) D1 incorrectly wired or faulty <br> (b) C11 incorrectly wired or faulty |
| 4. TR1/2 collector at low or 0 volts | (a) $\mathrm{T} 1 / \mathrm{T} 2$ windings open circuit |
| 5. A.G.C. supply (collector of TR3) low or at 0 volts | (a) D2 faulty or incorrectly inserted <br> (b) TR3 faulty |
| 6. TR3 base greater than 0.6 V | (a) D2 faulty or incorrectly inserted |
| 7. TR4 collector low or 0 volts | (a) D3 faulty or incorrectly inserted <br> (b) TR4 faulty |
| 8. TR4 collector very high | (a) check value of R13 <br> (b) both TR5 and TR6 faulty |
| 9. TR6 collector low | (a) check base TR5 is +1.3 V approx. If not check position, value and polarity of D3, R11 and C15. <br> (b) TR5 faulty |

TABLE 6.4
SERVO UNIT FAULT FINDING CHART

| SYMPTOM |  | FAULT | CURE |
| :---: | :---: | :---: | :---: |
| Servo hunts from side to side | (a) <br> (b) <br> (c) <br> (d) | Pot connected wrong way round <br> Poor wiper contact <br> Dirty or damaged pot <br> C2 wrong value or faulty | Swap round connections to pot ends (A \& B in Fig. 4.5) Remove pot body and very carefully bend the wiper contacts up Remove pot body and remove any signs of dirt DO NOT remove the lubricating grease on the surface. Inspect for damage and replace if necessary Replace C2 |
| Servo rotates continuously | (a) <br> (b) <br> (c) | Pot connections wrong way round <br> One of the pot connections open circuit R3 or R6 wrong value or open circuit | As (a) above <br> Re-solder both ends of each pot wire Check and replace as required |
| No movement from the servo at any time | (a) <br> (b) | Open circuit power leads <br> Motor connections open circuit or both shorted to case | Re-solder to connector and p.c.b. Check connections |
| Servo glitches at switch-on then no further movement | (a) <br> (b) | input lead open circuit <br> C1, or C3 or R1 faulty | Check connection <br> Replace components |
| Servo moves in one direction only | (a) <br> (b) | Blown output transistor Shorted connection to motor case or across p.c.b. gap | Replace transistor <br> Remove short |
| Servo overshoots its intended position | (a) | R4 or R6 too high value or open circuit | Check components and if O.K. lower value to $250 \mathrm{k} \Omega$ or even $220 \mathrm{k} \Omega$ if overshoot is bad |

By moving the relevant stick the servo should move giving a TOTAL movement of between 90 degrees with only full stick movement, and 90 degrees with full stick and trim movement. All the other servos will react in a similar fashion, however these do not have to be taken apart as only this first servo is used to set the gear up.

## FAULT FINDING

The faults to be described are the more common ones to be expected, generally from poor soldering rather than from faulty individual components. Obviously not all component faults can be described. However if you do suspect a component then the best advice would be to find someone who has access to an oscilloscope and practise your "crawling" to seek help.

The faults we have mentioned have been encountered during the development of the prototype, and its predecessors, and with duplicate systems that have been built by colleagues and friends of the authors.

If you do suspect a fault the first thing to do is to switch off and check the p.c.b. again. Feeling for a hot component is always a good start, then when all possible visual checks have been carried out make use of the fault finding tables.

There is one table for each individual part of the system, that is transmitter, receiver, servo and speed controller then one general table for the system as a whole.
Constructors who already have a R.C. system of some sort should make use of this to help locate faults. For example, use your transmitter with the E.E. receiver to check that the E.E. receiver is O.K.

## RECEIVER FAULT FINDING

Should the receiver take excessive current (normal current about 12 mA ) when connected to a $4 \cdot 8$ volt supply, there are four possible causes:
(1) Shorted track on p.c.b.
(2) Short in wiring or wiring loom to plugs etc.
(3) Capacitor Cl 6 faulty or incorrectly inserted
(4) Decoder IC2 faulty or incorrectly inserted.

The rest of the circuitry is isolated from the supply by the 100 ohm resistors R1 and R2 and any shorts after these resistors will show up in the d.c. voltage measurements as described in the receiver article (Part 3).
If however the receiver tunes up as described and the d.c. voltages are correct but the receiver will not drive a servo, the most likely cause is that the sync pulse from the transmitter is

not long enough to enable the sync pulse detector in the receiver to reset the decoder IC2.

The waveforms can be checked on an oscilloscope if one is available which will show that the collector of TR6 remains low all the time and that no sync pulse is present.

Whether a scope is available or not, try reducing R11 to 68 kilohms or shunt the present R11 with say 150 kilohms to obtain the same effect. This enables Cl5 to charge up more quickly, thus allowing the use of a shorter sync pulse.

Note: Whilst pulses appear at TR4 collector, capacitor C15 is discharged by each pulse via D3 thus ensuring TR5 remains off and TR6 on.
During the sync pulse time, Cl 5 charges up via R11 until sufficient voltage is available at TR5 base to turn it on. When TR5 turns on, TR6 turns off and its collector rises to +4.8 V thus resetting the decoder IC2.

If the sync pulse is too short Cl5 does not charge up sufficiently to turn on TR5, and hence TR6 collector remains low and no resetting of decoder IC2 occurs.

If this does not work and an oscilloscope is not available, try the following d.c. measurements with the transmitter on and in close proximity to the receiver.

## INTTIAL MEASUREMENTS

Collector TR3-typically +1V d.c.
under strong signal conditions).
Collector TR4-typically +4.2 V d.c.
Collector TR6--typically +2 V d.c.
If TR6 incorrect, switch off transmitter and check the sync pulse detector as follows:
Base TR5- +1.3 V approx.
Collector TR6-- +4.5 V approx.
Short out TR 4 collector to emitter.
Check TR5 base-less than 0.6 V -if not, D3 faulty or incorrectly wired.
Check TR6 collector-1V approx.-if not suspect TR5/TR6.
If the receiver voltages are incorrect but the board has no solder shorts, the possible faults are listed in Table 6.3 (note-transmitter off).

Table 6.4 continued

Servo sluggish
(a) TR3 or TR2 or both wrong way round
(b) R2 or C5 wrong value R4 or R6 too low in in value
(c) Motor or gearbox tight in its movement

Turn round transistors and replace Check values and change if required

Replace motor if it is a fauit, Grease gearbox (silicon grease only) and tighten screws carefully and not too tight

TABLE 6.5
SPEED CONTROLLER FAULT FINDING CHART

| SYMPTOM |  | FAULT | CURE |
| :---: | :---: | :---: | :---: |
| Notor runs but relay falls to changeover |  | Monostable pulse width wrong <br> Relay drive faulty | (1) Adjust VR2 <br> (8) Check connections around timing components R4, R5, C3. <br> (1) Check by shorting $c$ \& e of TR5 or TR4 to establlsh which is faulty |
| Relay changes over but motor fails to run <br> Neither relay or motor work |  | Relay contacts faulty <br> Motor faulty <br> Motor drive faulty <br> Drive battery flat <br> Battery connections faulty No Input signal to chip | (1) Clean and adjust contacts <br> (2) Check connections to contacts <br> (1) Check by disconnecting motor from speed controller and trying it on a battery <br> (1) Check by shorting c \& e of TR6 or TR7 to establish which is faulty <br> (1) Recharge <br> (1) Check and reconnect <br> (1) Try another channel on receiver to see if recelver is faulty <br> (2) Check wirlng to plug <br> (3) Check connections around C1 and pln 14 of IC |
| Motor runs in both directions at full speed but never stops |  | No deadband <br> Drive transistor short circuit collector-base or collector-emitter Pre-drive transistor short circuit collector base or collectoremitter | (1) Check deadband capacitor C4 <br> (1) Check by shorting b-e of TR7. If motor continues then TR7 faulty <br> (1) Check by shorting b-e of TR6. If motor continues then TR6 faulty |
| Motor runs in both directions at high speed but has a stationary position control stick |  | Expansion circuit faulty | (1) Check expansion capacitor C5 <br> (2) Check expansion resistors R3 in particular and potentiometer VR1 |
| Motor runs in "reverse" for forward movement of the control stick on transmitter | (a) | Pulse width change opposite from that required <br> o avoid excessive drain the transmitter and sp ovement of the vehicle ntroller is de-energised | either <br> (1) Reverse stick plug in transmitter <br> or <br> (2) Reverse connections to the motor <br> NB-DO NOT REVERSE <br> DRIVE BATTERY <br> POLARITY* <br> on the drive battery it is better to set eed controller such that the direction of is forward when the relay in the speed |

TABLE 6.6
OVERALL SYSTEM FAULT FINDING CHART

| SYMPTOM | Transmitter | AREA OF FAULT Receiver | Servo | CURE |
| :---: | :---: | :---: | :---: | :---: |
| One servo not functioning in one channel only | Open circuit lead or incorrectly wired plug or socket | Open circuit lead or incorrectly wired socket |  | Check wiring |
|  | Pot wiper open circuit on stick assembly |  |  | Using a meter on resistance range check that pot functions. If not then remove pot body and bend wiper in the case of the cermet pot |
|  | Connection between SK1 and IC1 open circuit |  |  | Check soldering and using meter check the offending resistor (R4-R10) |
| One servo not functioning on any channel |  |  | Fault on individual servo | Refer to servo chart |
| No movement of any servo on any channel | Crystal not fitted or damaged | Crystal not fitted or damaged |  | Insert or replace cyrstal |
|  | Wrong crystal i.e. receiver crystal in transmitter | Wrong crystal |  | Change around crystals |
|  | No transmitter output due to poor tuning | Poor tuning of receiver |  | Run through tuning-up procedures again |
|  | Incorrect wiring of channel plugs | Incorrect wiring of output leads | Incorrect wiring of plugs | Could be due to wiring the first plug or socket wrong from which the rest were copied, so check the wiring again |

## SOME FINAL POINTS

Having now completed the system with all parts functioning correctly it is now worth mentioning a few points in connection with the use of the equipment.

If you have used the Nicad batteries, always keep them well charged. In the case of dry batteries, carry a spare set around with you so that you are never stuck on a Sunday or an


Fig. 6.4. Typical servo linkages.
evening with a set of flat batteries. If you do not intend to use the equipment for a long period remove the dry batteries in case they leak and ruin the inside of the case.
The receiver should always be properly looked after and always mounted in foam rubber to absorb the shocks of bumps and crashes whether installed in boat, car or aircraft. With boats a watertight compartment is always useful. If you do have a bad crash check the equipment properly before you use it again, and in the case of the receiver giving it a tune-up will do no harm.

## SERVO LINKAGES

In the previous parts, mounting and positioning details have been outlined to give the newcomer an idea how to install the equipment. However, it must be borne in mind that the servos are very precise in their movement so always give them good linkages to the control function they are going to operate.

The ideal linkage, whether it is a pushrod, plastic "snake" or closed linkage, should have no slack in it, yet should not be tight enough to put a strain on the servo. These three types of linkage are shown in Fig. 6.4.

With these few hints we conclude, hoping that you have many enjoyable hours with your equipment, with as few mishaps as possible. Good luck and good flying, boating and driving.


# PRE-TUIED 4-5TATION RRDIO 

At.r.f. radio to receive Radios 1,2,3 and 4. These four stations are switch selectable thus eliminating the need for a tuning dial. Incorporates a loudspeaker.

## 50LID-5TRTE DURL LIIE CAIIE

Pit yourself against this electronic game playing computer.
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## LICHTS UARIIIL SVSTEII

This unit will sound a buzzer or flash a light to remind you that your lights are on when the ignition is turned off. Requires no setting or cancelling of switches. Includes a parking facility.


A very simple project designed to keep an "eye" on the state of your car battery. Fitted to the instrument panel, this unit will give continuous readout of battery voltage.

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## HAND HELD CASES

When recently faced with the problem of housing a transmitter for an ultrasonic remote control system, I found a very cheap, simple and attractive solution to the problem. This could be useful for many hand held projects.

A short length of $11_{4}$ inch diameter grey plastic waste water pipe was used in my project (there are other sizes) to hold at one end a PP3 bbattery held in place with foam plastic, with the circuit board, push button switch and the transducer at the other end. These were held in place with a more rigid foam plastic (the type sometimes used for packing i.c.s) and secured with Araldite. The case appearance can be further improved by the use of transfer lettering or paint.

Denis Williams,
Llandudno,
Gwynedd.

## CHANGING REED SWITCH ACTION

Reed switches have "normally open" contacts; "normally closed". types are unobtainable whilst changeover are not too easy to obtain and are much more expensive.

With reed coil switches it is possible to reverse normal action. All that is required is to put a suitable magnet outside the coil to cause the reed contacts to close. Current through the coil will now cause the reed switch to open. If it does not work one way, reverse the polarity of the current flow in the coil.
A. R. Smith,

Wallington,
Surrey.

## Morse Practice Oscillator

(February 1980)
Note that capacitor C1 should be connected to point B15 and not A15 as shown in Fig. 2.

## Simple S.W. Receiver

(February 1980)
We apologise for the following errors which appeared in the diagrams for the Simple S.W. Receiver.
In Fig. 3 from pin 1 of the coil holder the flying lead should go to 19 on the circuit board and not $\mathrm{H9}$. The flying lead from pin 4 should go to C1 alone and an extra flying lead should come from pin 3 to $E 9$ on the circuit board.
Fig. 4. Annotations SK1 and SK2 should be transposed. The flying lead from C1 should go to L1 pin 4 only.
Fig. 5. The flying lead from position E9 should be labelled L1 pin 3, not L1/C1. Capacitor C2 on board should be marked C5.


## STOCKING UP

Every constructor accumulates a E stock of components in a surprisingly short space of time. But when starting in this hobby, the question usually arises what kind of components should one obtain to form an initial stock.
Resistors, capacitors, transistors and diodes-these are the mainstay of electronic circuits. A carefully selected collection of such components will be a valuable working stock to draw upon whether for building projects or performing experimental "lash-ups".
This month we suggest a range of resistors that the new constructor should purchase.

The resistors listed in Table lare values that are most frequently encountered when building electronic circuits. They will satisfy possibly 75 per cent of needs.
A small number of additional components will usually have to be purchased to complete the complement of a given project. However with the majority of parts already in stock, construction work can often

be started on whilst awaiting the arrival of the additional "specials".

Some retailers offer discount rates for quantities of such small items as resistors and capacitors. This is another good reason for purchasing a fairly large selection.

The quantities against each type of component are the minimum it is suggested the new constructor should obtain. If resources permit, it would
be wise to multiply all these quantities by a factor of two or even five, say.

## CARBON RESISTORS

The cheapest kind of fixed value resistor is made of a carbon composition, or a carbon film. Physical size depends upon the wattage rating. Quarter watt resistors will suit many requirements. They measure about 8 mm in length and have a diameter of about $2 \cdot 5 \mathrm{~mm}$.
For our initial stock $1_{2}$ watt resistors (which measure about 10 mm by 3.5 mm diameter) might be the better choice. This size resistor can of course be used perfectly safely whenever ${ }^{1} 8,1_{4}$ or ${ }^{1} 2$ watt is actually called for in the Component List.

Carbon resistors do not have precise ohmic values, but are available with various percentage tolerances of the nominal value. For most purposes 5 per' cent resistors are ideal, and are readily available. (Higher tolerance resistors, such as 10 and 20 per cent, are also in fact suitable for many applications.)

TABLE 1
CARBON COMPOSITION OR CARBON FILM RESISTORS $\frac{1}{2} W \pm 5 \%$

| Ohms |  |  |  |  |  |  |  |  | Qty | Ohms | Qty |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 1 | 12 | 1 | Ohms | Qty | Ohms | Qty | Ohms | Qty | Ohms | Qty |
| 100 | 2 | 120 | 1 | 150 | 1 | 18 | 1 | 22 | 1 | 27 | 1 |
| 1 k | 2 | $1 \cdot 2 \mathrm{k}$ | 2 | $1 \cdot 5 \mathrm{k}$ | 2 | 1.80 | 1 | 220 | 2 | 270 | 1 |
| 10 k | 5 | 12 k | 1 | 15 k | 2 | 18 k | 1 | $2 \cdot 2 \mathrm{k}$ | 2 | $2 \cdot 7 \mathrm{k}$ | 1 |
| 100 k | 2 | $\cdot 120 \mathrm{k}$ | 1 | 150 k | 1 | 180 k | 1 | 220 k | 2 | 27 k | 2 |
| 1 M | 1 | $1 \cdot 2 \mathrm{M}$ | 1 | $1 \cdot 5 \mathrm{M}$ | 1 | $1 \cdot 8 \mathrm{M}$ | 1 | $2 \cdot 2 \mathrm{M}$ | 1 | $2 \cdot 7 \mathrm{M}$ | 1 |

## DICN PIDA \& FInN1Y...

## BY DOUG BAKER



WELL, HOW ABOUT THIS RATHER EXPENSIVE ONE SIR? IT GIVES THE HOURS MINUTES SECONDS, MONTHS, DATE, DAY AND THE exact time widen the next INSTALMENT IS DUE TO BE PAID.



MANy types of gas or fumes, if released and allowed to accumulate, are insidious killers; consequent explosions from large concentrations can wreck property and cause many thousand pounds worth of damage.

A small investment on this project could well prove to be money well spent. Whilst this device obviously cannot prevent leakages arising, it will detect the presence of a surprising variety of fumes and vapours, as well as common smoke, and will then relay a warning signal well before any dangerous accumulations can build up.

The unit has been designed to be flexible in its application and use. It can be either battery or mains powered.

## GAS DETECTED

The Gas Sentinel will detect the presence of domestic gas (methane) and Calor Gas (propane) the latter making it eminently suitable for use in boats and caravans when operated from a battery supply. Also, carbon monoxide, a constituent of smoke, will trigger the alarm giving the unit the additional feature of being. a fire detector. However, large volumes of smoke are required to trigger the alarm.

## REMOTE SENSING

Because the actual sensor is located remotely to the main unit, this means that the sensor can be mounted right in the heart of potential trouble spots (e.g. next to propane cylinders, alongside the gas cooker/fire) whilst the main unit and alarm can be positioned in any convenient place.
The Gas Sentinel employs a solidstate gas sensor device which makes the construction of a low-cost and easy-to-build gas detector a reality for the amateur enthusiast.

THE SENSOR
The sensor used in this project is from the TGS family. The family types differ in operating voltage as well as sensitivity to individual gases. Of these sensors, type TGS813 is used in this application. A diagram showing details of this appears in Fig. 1.
The TGS813 comprises a resin housing measuring 10 mm high by 17 mm diameter (excluding terminal pins). In the top of the housing is a very fine mesh window, with a smaller mesh window in the base. Standoffs are moulded into the underside, allowing gas and smoke to pass through the sensor.

Inside the housing is the sensor element, consisting of a ceramic tube with a semiconductor-material coating. Electrodes are taken from the sensor to terminal pins. The sensor is heated by a filament inside the


Fig. 1. Various details of the TGS 813 gas sensor.
tube; the increased temperature of the semiconductor improves the sensitivity and response time of the unit.

Connections for the electrodes and filament are taken to six external pins in the base: the sensor must always be used in conjunction with a special socket to which wires may be soldered. The base connections for the device are also given.

For practical purposes, pins 1 and 3 can be considered to be joined together, as can pins 4 and 6.
The maximum permissible circuit voltage is 24 V , and the filament is rated at 5 V 130 mA . Fig. 2 shows how the resistance of the semiconductor element alters with varying concenrations of several gases. The sensor will also respond to accumulations of smoke.

## CIRCUIT DESCRIPTION

The circuit diagram of the Gas Sentinel is shown in Fig. 3. Here two


Fig. 2. Graph showing the variation of sensor resistance with concentration of different gases reaching sensing element.


## HOW IT WORKS



Gas or other toxic vapours reaching the sensing element in the sensor affect its conductivity and causes the voltage level into the comparator to change. When this passes the set reference level, the comparator output turns on the latching electronic switch and sounds the alarms. The alarms continue to sound even if the gas concentration reduces, until manually reset.

The gas sensor itself requires a 5 V 150 mA supply for its heater filament, and this is provided by IC1, a 5 V 500 mA regulator fed from the 12V rail. The p.c.b. layout has been devised to suit the $\mu$ A78M05UC voltage regulator, so if an alternative type is considered the lead-out configuration must conform exactly with that shown.
In the mains version, the 12 V supply is unregulated, and in reality measured only $10-11 \mathrm{~V}$. The voltage available at the alarm output sockets was only 10 V . So if this outlet is used to drive a relay, ensure that it operates at 10 V .
Diode D9 indicates that power is being applied to the circuitry and should of course be on all the time that the unit is in use, whether mains or battery supply.
SGS1 is the gas sensor. Its resistive semiconductor element, $R_{\mathrm{g}}$, forms a potential divider with $\mathrm{R}^{2}$. As $\mathrm{R}_{\mathrm{s}}$ decreases, due to an increased concentration of ambient gas levels, the voltage at SGS1/R2 junction will be reduced.
This voltage is referred to the inverting input (pin 2) of IC2, an operational amplifier conneoted as a simple comparator. A variable resistor VRI determines the voltage at the non-inverting input (pin 3) of the comparator, and this voltage can be adjusted by rotating VR1 as necessary.

## COMPARATOR ACTION

The output voltage of the comparator depends upon the inputs at pins 2 and 3 of IC2. If the voltage at pin 3 exceeds that at pin 2 then the output goes high, being at a voltage almost equal to the positive supply rail. Similarly the output goes low if the two input voltages are reversed.

By varying the setting of VR1, the switching point of IC2 can be adjusted. The effect of this is to alter the sensitivity of the circuit, so that the alarm will sound at a required gas or smoke concentration.
Once pin 6 goes high-the sensor having detected gas at the necessary triggering level-then the Level indicator diode D6 will illuminate to show that the ambient gas level has reached a value determined by VR1. The l.e.d. will extinguish once the level drops again.
When the comparator output switches high, this is fed via attenuator R4 and R5 to the gate terminal of CSR1 causing the thyristor to turn on.
This device normally assumes a high resistance blocking state between anode and cathode, but will be triggered into a conductive state when a suitable signal is received at the gate.

Once conducting, the thyristor completes the circuit to the alarm l.e.d. and this illuminates.

## LATCHING ACTION

The alarm l.e.d. will continue to glow even if the output of IC2 falls and D 6 extinguishes. This is due to the latching action of the thyristor. The main characteristic of a thyristor is that once it is triggered into conduction, it will remain in this state until it is reset.

It can be reset by several methods. If power is removed temporarily from the circuit, once switched back on again it will resume its blocking state. Another means of resetting the thyristor is to short the anode to cathode. This is accomplished by temporarily closing S2. Once opened again, the thyristor will resume its high resistance state, unless a trigger signal is present at the gate in which
case the device will conduct once more.

Connected in parallel with the ALARM indicator is a miniature audible warning device, WDl. This consumes only 15 mA when operating, and provides an audible indicator that the gas level being monitored by SGSl has reached the required alarm level.

Provision has been made in this design for an external alarm to be connected at SK3 ( + ) and SK4 ( - ). This must be rated at 12 V 500 mA maximum (see later), and can take the form of a lamp, buzzer, relay, or combination of these.

If a relay is used, an e.m.f. suppression diode is required to short out any high reverse voltages which tend to appear across the relay coil just after power is removed from the relay; D8 accomplishes this.

## CONTROLS

Switch S2 has a dual function. Apart from resetting the thyristor as described earlier, it will also complete the circuit to the alarm. If closed, therefore, it will cause the alarm to operate, and this is useful in testing the external alarm set-up. S2 is a biased (spring-loaded) type so that it is normally open.

The muTE switch S3, if opened, silences the internal audible warning device WDl, and also removes power from the external alarm. This is necessary if the gas level is high for a long period of time.

Under these circumstances, the thyristor cannot be reset at S 2 until the gas level drops because a constant triggering signal is present at CSRl gate.

One could switch off the Gas Sentinel altogether, but this will not tell you when the gas level has dropped to below the triggering level. The most convenient course of action is obviously just to silence any audio alarms by opening S3. This will disconnect the external alarm

Rear view of prototype showing inlet/outlet sockets, fuse and internal alarm.


D6 to extinguish before resetting the alarm completely at S2. Switch S3 can then be closed once more. In practise this is a very neat solution.

The mute switch comes in handy when initially switching on the unit. During warming up, the resistance of the sensor temporarily drops to a low value ( 2 to 3 kilohms). The opamp detects this and triggers the alarm. The mute switch, if opened while sensor is warming up, will prevent any audio alarm sounding unnecessarily. Warming up, on the prototype, takes about 30 seconds, and the sensor is ready for use once the level l.e.d. has extinguished, the alarm has been reset and S3 has been closed.
The l.e.d., D5, fitted to the remote sensor case should always be illuminated when the unit is switched on. This shows that voltage is being applied to the filament of the sensor.

## PRINTED CIRCUIT BOARD

A professional finish, coupled with higher reliability, is achieved by using a p.c.b. to carry the complete circuit. This also makes for easier construction, and helps to ensure that the circuit will work first time.

The Gas Sentinel circuitry is very neatly accommodated in a Verobox Series II Casebox type 2066. This measures $155 \times 92 \times 52 \mathrm{~mm}$. It has one aluminium front panel which slots into a moulded bezel-type surround.

Any other plastic or metal case of suitable dimensions can be employed, but the specified box lends itself to compact construction and a professional appearance.
The remote sensor is mounted with its socket on a small Verobox type 1413E. This particular case measures $72 \times 47 \times 25 \mathrm{~mm}$ and is moulded in black ABS. Again, any other suitable box can be used. Details of construction of this are given later.


Straight-on view of completed unit.
as well as WD1, but D7 will remain alight. Then the user should wait for

## P.C.B. COMPONENT <br> ASSEMBLY

Construction should commence with the printed circuit board. This is shown full size in Fig. 4a. There are a few points to watch concerning what should otherwise be a straightforward assembly procedure. The layout of the components on the top side of the board is shown in Fig. 4b.

If the battery version is to be built, the bridge rectifier should be omitted and the battery supply wired up as indicated in Fig. 4c. Note the value of Cl .
IC2 is an 8 -pin di.i.l device and to make later replacement easier, should this prove necessary, it should be mounted in a suitable d.i.l. socket. This also prevents thermal damage arising during soldering.
The bridge rectifier specified here is a VM18 400 V 1A type. This is encapsulated in a 4 -pin di.i.l. package. Do not attempt to adapt a d.i.l. socket for use here, but solder it straight in, observing the d.c. polarity markings. Any other 1A type can be used if it is physically compatible with the p.c.b. It may be possible to bend the leads of the cheaper W005 device to make it fit the p.c.b., but ensure

## COMPONENTS - -

Resistors

| R1 | $220 \Omega$ | R5 | $820 \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $5.6 \mathrm{k} \Omega$ | R6 | $680 \Omega$ |
| R3 | $680 \Omega$ | R7 | $680 \Omega$ |
| R4 | $12 \mathrm{k} \Omega$ |  |  |
| All | fW carbon $\pm 5 \%$ |  |  |

## Capacitors

C1 $\quad 150 \mu \mathrm{~F} 12 \mathrm{~V}$ elect. (battery version) $2200 \mu \mathrm{~F} 16 \mathrm{~V}$ elect. (mains version)


C2 $\quad 1 \mu \mathrm{~F} 35 \mathrm{~V}$ tantalum
C3 $\quad 0 \cdot 1 \mu \mathrm{~F}$ polyester type C280
Semiconductors
D1-D4 VM18 1 A 400 V bridge rectifier (mains version) -see text.
D5 TIL220 red I.e.d.
D6 TIL223 yellow l.e.d.
D7 TIL220 red l.e.d.
D8 1N4001 silicon diode
D9 TIL221 green l.e.d.
IC1 $\quad \mu$ A78M05 5 V 500 mA voltage regulator i.c.-see text
IC2 741 differential op-amp 8 -pin d.i.l.
CSR1 C106D 4A 400V thyristor
SGS1 TGS813 semiconductor gas sensor (Watford)
Miscellaneous
VR1 $22 \mathrm{k} \Omega$ standard size preset potentiometer
S1 s.p. on/off toggle (battery version)
S2 d.p.d.t. sub-miniature toggle (mains version)
S3 s.p.c.o. sub-miniature biased off toggle
S3 s. s.c.o. sub-miniature toggle
FS1 1 A 20 mm fuse
SK1 TGS 6-pin socket
SK2 3-pin DIN socket
SK3 4 mm insulated (red)
SK4 4 mm insulated (black)
PL1 3-pin DIN plug to suit SK2
WD1 $\quad 12 \mathrm{~V} 15 \mathrm{~mA}$ audible warning device
T1 mains primary $/ 9 \mathrm{~V} 800 \mathrm{~mA}$ (or 1 A ) secondary or two 9 V 400 m A secondaries wired in parallel [latter, type 182 Watford] (mains version)
Printed circuit board: $66 \times 50 \mathrm{~mm}$; 8 -pin d.i.l. socket for IC2; 3-core miniature mains wire (connection to remote unit); mains cable (power to unit); small rubber grommet; nuts, bolts, washers; aluminium for IC1 heatsink; cases: Vero series II Casebox ( $65-2066$ A) (mains unit), Vero type 301 (74-1413-E) (remote unit); lens clips for panel l.e.d.s 2, red, 1 green, 1 yellow, self adhesive cabinet feet ( 4 off); 20 mm panel mounting fuseholder.


Fig. 4a. The master pattern of the p.c.b. underside shown full size. The black areas represent the copper remaining after etching.



Fig. 4b. The layout of the components on the top of the p.c.b. and wiring details to off-board components.

Fig. 4c. Shows modification to board layout, fuse and onoff switch for battery version.


Fig. 5. Dimension and drilling details for the regulator heatsink.


Fig. 6. Drilling information for the front panel, shown actual size for the specified case. Can be used as a template and/or front panel label.
that none of the leads can short circuit. The VM18 was used simply to make the p.c.b. copper track design slightly easier.
It is extremely important that the electrolytic smoothing capacitor Cl is soldered in the right way round. A radial lead (p.c. mounting) type is used, and the negative lead-out is clearly marked. Similarly, the tantalum bead capacitor has its polarity clearly marked, and this must be observed.

VRI is a standard-sized preset, and not the more usual subminiature component; the one used on the prototype has a plastic knob fitted which helps in adjusting this control.
Care needs to be taken to ensure that the semiconductors are not overheated during soldering. A small heatsink used on the lead being soldered will help prevent any damage arising. Also, note the base connections for ICl and CSR1. A chamfer on the plastic case identifies the output of the regulator and thyristor gate respectively.

ICl is best fitted with a small heat$\operatorname{sink}$ as seen in Fig. 5 to help dissipate heat generated by the regulator. The heatsink does not require a mica insulation kit. C1 and ICl are located closely together, but there should be enough clearance between the two. Note, however, that the heatsink is pointing to the perimeter of the p.c.b. and indeed overlaps it.

Check the completed printed circuit board for dry joints, reversed polarities of components, and adjacent tracks which may inadvertently have been abridged with solder.

## CASE COMPONENTS

Construction can proceed with the case. With this design, some care needs to be exercised to ensure that everything is going to fit into place. For example, the positioning of the p.c.b. within the case in relation to the switches on the front panel is very important. The components on the circuit board must not touch any of the wiring to the switch tags.

Drill the aluminium panel as illustrated in Fig. 6, and after this the panel may be lettered as desired.
As usual, use small rub-down lettering and then spray on two or three coats of protective lacquer. Take care not to get dust or fluff on to the varnish while it is drying. Alternatively, Fig. 6 may be cut out or copied and glued to the front panel. Now fit the front panel mounted components.

Before finalising the location of the p.c.b. within the case, it would be better to experiment with its position in relation to the mains transformer and assembled front panel. Similar care should be taken to make certain that the transformer will not touch any other parts once the case is closed up. The transformer used in the prototype had dimensions $50 \times 42 \times 44 \mathrm{~mm}$. Also it had two 9 V 400 mA secondary windings that were connected in parallel. In the diagrams, the secondary has been shown as a single winding having a current rating equal to 800 mA .



The completed control unit with top removed to show the close density of components.

On the bottom half of the case at the rear is mounted the 3 -pin DIN socket, fuseholder and mains cable inlet; this last hole should have a grommet fitted.

On the top half at the rear there are the two 4 mm sockets (SK3 and SK4) plus the audible warning device. The two sockets must clear the transformer completely when the case is fixed together. WDI requires a small hole nearby to enable the leads to pass through to the terminals of SK3 and SK4.

## INTERWIRING

There is quite a lot of interconnecting, to be carried out, and Fig. 7 gives details; 3 amp mains wire is suitable for the mains interwiring.

The earth input from the mains is connected to the metal bracket of TI with a solder tag under one of the transformer mounting bolts. The front panel is similarly earthed by placing a larger solder tag under one of the toggle switch nuts. The metal body of the DIN socket should also be earthed: an earth terminal tag may already be fitted to the socket, and this can be used.

The remainder of the wiring can be carried out with general purpose flexible hook-up wire. Try to use as many different colours as you can, in order to make subsequent checking and tracing easier.

Insulate any connections with p.v.c. sleeving as required. This is especially true of any mains voltage connections.

Readers may have noticed that the appearance of the front panel was improved by using "lens-clips" of the appropriate colour to mount the light-emitting diodes. Also, the rather small tangs of the toggle switches were made more manageable, and more attractive, by employing coloured push-on plastic caps.

## REMOTE SENSOR UNIT

The final part of construction is the remote sensor unit; Fig. 8 gives all necessary details. The socket for the sensor requires an 18 mm diameter hole to be cut: as this hole will still be visible once the socket is bolted in from behind, the cut-out should be as perfectly round as possible if a pleasing appearance is to be maintained.

In fact a perfect hole can be çut in the ABS plastic case using a Q-Max chassis cutter.
A cable length of 5 metres has proved successful, but it is anticipated that much greater lengths can effectively be used. Miniature 3-core mains cable is suitable for this.

It would be possible to mount the sensor on the main unit itself, thereby dispensing with the need for a remote unit. In this case, you would need to ensure that there is adequate clearance behind the socket once the unit was closed up, and the sensor would need to be mounted on top of the casebox.

A remote sensor, however, enables it to be positioned exactly as required, whilst the control unit can be in some other more convenient position (e.g. the bedside table).
Check over all wiring before proceeding to the next stage.

## TESTING AND SETTING UP

Insert IC2 into its socket if you have not already done so. Also plug the sensor into its socket on the remote unit (either way round will do).

The unit should not be plugged into the mains during these tests.

Before switching on, try to test that the completed model is earthed correctly. Using an ohmeter on a low ohms range, check:
(i) The resistance between the earth pin on the mains plug and transformer mounting bracket registers a very low resistance.
(ii) Similarly check that the front panel is correctly and soundly earthed.

Set VRI to middle position and S3 to mute (i.e. S3 open). Plug in and switch on. The green POWER ON l.e.d. should light, as should D5 on the remote unit.

After a few seconds the level and ALARM l.e.d.s should suddenly illuminate at the same time. This is perfectly in order and is attributable to the sensor warming up. This should be accompanied by the temperature of the sensor cell slowly rising.

Presently the lever indicator should extinguish, leaving the ALARM l.e.d. on. Close S3; this should cause the audible warning device to sound. Then operating S2 (TEST/RESET) should silence the buzzer and extinguish D7 (alarm).

Pressing S2 again should then operate the alarm circuitry once more, this time in the test mode.

One method of testing the sensor (without gassing yourself) is to pour a little lighter fuel or petrol on to a cotton wool pad and place this near to the sensor cell. Depending on the setting of VRI, the alarm should be triggered and the level l.e.d should illuminate.

The Gas Sentinel should then be operated for a few hours to make sure that everything is in order.

Over a period of about one week the sensitivity control, VRI, should be adjusted until the desired level of sensitivity is obtained. The reason for the extended period of adjusting is that false alarms may initially be given because, for example, very high levels of cigarette smoke may trigger the alarm. This tendency should eventually be cured by altering the setting of VRI accordingly until maximum sensitivity without false alarms is attained.

## LOCATION OF THE SENSOR

The gas sensors are affected by changes in humidity and ambient temperature. It is important therefore to position the remote unit away from direct heat (e.g. radiators, fires, lights, etc.) and also away from steam.

In use it is advisable to check occasionally to see that the mesh window of the sensor has not become blocked with dust or dirt, as this will impair its performance. Do not clean the mesh with any liquids or aerosols.

The life of the sensor is claimed to be approaching ten years under normal operating conditions. Should replacement prove necessary, this will be signified by much poorer response of the unit to the "lighter fuel" test mentioned above. Replacement of the gas sensor is a simple matter.

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# Everyday News 

## ELECTRONICS MAKES THE HEADLINES

At the BBC External Services the script of newn storles, talks and features (some 30 million of them in a year) are now distributed electronically to more than 200 outlets in Bush House, the London headquarters of the BBC's Overseas broadcasting.

The broadcasters, journalists and translators in the 38 different language sections at Bush House no longer have to wait, sometimes up to two hours, for the scripts to be copied and delivered by hand. Now they can get their stories in seconds from a visual display unit (VDU) or a printer, in their office.

At the heart of the Electronic Distribution System (EDS) are two mini-computers and an array of disc storage units. The scripts are written into the system on 64 VDUs in various parts of the building.
There are 39 VDUs in the central newsroom where journalists dictate their stories to copytakers who type them into the system. Once a story has been written, the journa lists can instruct the computer to direct it to specific language sections and, shortly after, it will be printed in their individual offices.

## The System

For the technically minded, the EDS is controlled by two General Automation 16/440 mini-processors. Both are in continuous operation and receive the same input, but only one of them provides any output. When a fault occurs, the standby processor is ready to take over immediately.

Each processor is asso ciated with a 2 -megabyte fixed-head disc and a 24-megabyte disc-pack drive. New material entered each day is "dumped" onto magnetic tape and later transferred to microfiche for archival storage.

Each of the 137 VDUs distributed around the building can undertake full text

editing, but only those in the news, talks and features areas are free to amend the stories in the central store. Hard copies can be demanded from 85 medium speed, 120 characters per second (c.p.s.), Lear Siegler 200 printers and 36 low speed

10c.p.s., Transtel printers.
The system can accommodate individual talks of up to half an hour, or about 5,000 words. A single story can take as many as 15 "pages" on a VDU, with each page accommodating up to 2,048 characters.

## Pay-TV

The Home Secretary, Mr William Whitelaw, MP, announced in the House of Commons that a consultation letter was being sent out inviting comments from both broadcasting authorities, film and cinema representatives and other interested parties on pay television pilot schemes over cable systems.
In reply to a written question from David Mudd, MP, the Home Secretary said on the basis of comments received he would then decide the circumstances and conditions in which subscription television might be authorised. He invited written comments by May 31 and said that in addition to those organisations specifically consulted, he would be pleased to receive comments from any other organisations or individuals who would like to send them.


## ELECTRONICS FOR TEACHERS

A four-day (March 31-April 3) and a one-week (July 14 to 18) course on Basic Electronics and Electronic Applications for Teachers is being run by Salford University. They are also offering a series of microprocessor courses from April 14 to 18.

For full details of all courses available, contact The Administrative Assistant (Short Course), Room 110, Registraur's Dept, University of Salford, Salford M5 4WT.
The Department of Electrical Engineering Science at Essex University will be holding its annual Electronics Summer schools for teachers during July 7 to 11. Three courses will be run simultaneously.

For further details contact the University of Essex, Department of Electrical Engineering Science, Wivenhoe Park, Colchester CO4 3SQ.

If you are one of those lucky people who happens to own an Apple Computer System and always had a yearning to write and play back your own synthesised music, then the latest plugin cards from Microsense Computers Ltd are for you.

Known as the ALF Music Synthesiser, the plug-in cards allow you to write your own synthesised music and play
it back through your hi fi.
The traditional music staves are displayed on the video monitor or TV screen and, using paddle controls, you simply enter each note directly onto the staves. Adjustment by pitch, envelope, decay, sustain and volume all within the full piano range of eight octaves (24 notes per octave) can be made.

Field tests of a viewdata system start in West Berlin and Dusseldorf this year. First reports indicate that the Germans are showing much greater interest than the British have shown for the BPO's Prestel equivalent.

## Comput-a-horse

The French state-owned horse-racing betting organisation is to install several thou sand betting terminals in cafes and bars throughout the country. These will enable punters to place their bets right up to the "off".
-ANALYSIS

## FADED IMAGE

The decade of the 1960s was one of glory for electronics. The transistor and microelectronics had arrived to pave the way for all sorts of technological miracles such as communications satellites and the ultimate triumph of the first men on the moon and their safe return to earth.

But microelectronics could be applied in other ways and at the start of the 1970 s electronics started hitting the headlines in an entirely different way. In 1972 the news of "dirty tricks", the attempted electronic bugging of the Watergate building in Washington was the start of the biggest political upset for years

By the late 1970s the microchip, the latest electronic miracle, was already being branded as "a menace". And in the first month of the present decade there was uproar over the revelation that the British Post Office has a modern centre for phone-tapping

The new British phone-tapping complex has been represented as particularly sinister simply because it is modern. It is said to have a capacity (not actual usage) of 1,000 lines which is not very many for a population of 55.8 million using 22 million telephones. But, horror of horrors, worse is to come. It is alleged that tape transports are voiceoperated, that individual callers can be electronically recognised through their voice-prints, and that conversations can be automatically printed out in hard copy.

If true, then the Post Office Engineering Department deserves congratulations. How splendidly efficient compared with old-fashioned methods of shorthand writers with earphones clamped over their ears, chain-smoking while waiting for calls. If eavesdropping is necessary in the interests of the community (and it always has been) the new and better method is no more sinister in principle than the old.

There is plenty of room for debate on the microchip. But, apart from purely technical merits, not on the chips themselves. How they are applied is a human problem. The chip itself is neutral and harmless.

Brian G. Peck

## CB NEWS

The British authorities are delaying any decision on authorising $C B$ radio for the time being, contenting themselves with the announcement that whatever future decisions are made, 27 MHz operation will be out, thus diseotraging potential users from wasting their money buying equipment for that band.

Meantime, the Irish Gov ernment has banned CB radio and warned both dealers and the public that illegal usage will lead to prosecutions.

A National Committee for Legalisation of Citizens Band Radio has been formed in an effort to focus attention on the growing numbers of people calling for the introduation of CB in the UK.

The new National Committee, under the chairmanship of Lewisham councillor Theo Yard, will pool together the efforts of CB clubs around the UK. Theo Yard commented, "Our aim is the establishment of a legal CB system in the UK as soon as possible."

## SINCLAIR STRIKES AGAIN!

Clive Sinclair, of pocket calculator and microtelevision fame hit the headlines again last month when his firm, Sinclair Research, announced the arrival of their new baby-the $\mathbf{Z X 8 0}$ personal computer.

This "pint-sized" machine (it is small and light enough to be carried in your brief-case) is a powerful, full facility computer and costs under £100; the kit is $£ 20$ cheaper. This remarkable price has been made possible by the dramatic
 reduction in component count, a tenth of most other comparable performance computers by application of new design techniques, a super ROM and touch sensitive keyboard. The keyboard has single-stroke keyword entry which eliminates the need for much tiresome typing. The ZX80 plugs into a standard TV (to produce a black-onwhite display) and is powered by an external 9 V supply via a suitable mains adaptor.

## MICRO SHORTAGE HITS RETAILERS

Next time you try to order certain i.c.s you may be in for a surprise. A recent survey of some of the larger component retailers has revealed a considerable shortage of logic devices, especially in the CMOS and 74LS ranges. Prices and deliveries are uncertain and the inevitable black market is blossoming.

This shortage of microchips is not particularly new nor is it confined to the retail end of the market. However, semiconductor users supplied through electronics industry distributors (and this includes most retail outlets) are hardest hit. Delivery times of six to nine months are not uncommon and some retailers are still waiting for January shipments.

The enormous increase in demand for computer based products has, to some extent, taken the industry by surprise and has contributed greatly to the present shortage in production. Companies placing orders for "safety-first" reasons have also been criticised.

There is, however, some comforting news for the hobbyist. Component shortages tend to move in cycles and many suppliers believe it is only a matter of time before the i.c.s become plentiful again. Whether this is true or not, only time will tell, but it is significant to note that major companies such as ICL remain concerned about future supplies.

## CURTAIN CALL

Poland is now the 91st country which Britain's phone users can now dial direct.

One of the places that can be dialled direct is the 16th century royal capital of Krakow where Pope John Paul was cardinal archbishop.

Over 15,000 calls a month are received from Poland and about the same number are made from Britain.

## Golden Oldies for Video

The RCA company has acquired 12 classic Charlie Chaplin films and five NBC specials, including "Victory at Sea", for its catalogue of video disc programmes. They also have an option on the original 26 episodes of the World War II television epic.
Some 300 titles are planned in the first year after the RCA "SelectaVision" video disc appears on the market in the early part of 1981.


A standard mains outlet has $L$ (Live), $N$ (Neutral) and $E$ (Earth) sockets. Power for appliances is obtained from the $L$ and $N$ sockets, but the Neutral is at low potential relative to earth, so $L$ and $N$ will not be interchangeable. The Earth is used to ground the metalwork of appliances, or act as a conductor for fault current which will result in the Live circuit being interrupted.

When an appliance is correctly connected by means of a 3-core cable, maximum safety is obtained for the user. Short circuits from $L$ to $N$, or $L$ to $E$, will result in the fuse in the live ( $L$ ) circuit blowing or operation of a trip, so that the appliance is not dangerous to handle.

Proper protection is not obtained if $L$ and $N$ circuits are reversed at the outlet, or Neutral or Earth omitted. The fault indicator plug described here shows the situation when wiring is correct at the outlet, and also four fault conditions. Some of the latter, and especially an omitted earth, can be dangerous for the user.

## CIRCUIT AND OPERATION

The circuit diagram for the Mains Outlet Fault Indicator is shown in Fig. 1. The neons LP1 and LP2 receive current through their series limiting resistors R1 and R2. Resistor R3 is from $L$ and $N$ in the plug to allow a path to LP2 in case of an "open circuit Neutral".

When the plug is inserted into a mains outlet socket, a correctly wired output will pass current via R1 to illuminate LP1; LP2 remaining off. An output with the Live


Fig. 1. Circuit diagram for the Mains Fault Indicator.


Fig. 2. Layout of components and wiring.

## COMPONENTS

Resistors
R1, 2, $3270 \mathrm{k} \Omega$ or $330 \mathrm{k} \Omega$ to suit neons (3 off)
$\pm W$ carbon $\pm 5 \%$
Miscellaneous
LP1, 270 to 90 volt wire-ended neons (2 off)
FS1 2A or 3 A fuse
Standard flat pin 13A type plug
Approx cost 30.90

Guidance only
20.90 (see page 241)
lead disconnected (open circuit) will be obvious by both LPl and LP2 failing to light.

If the Live and Neutral mains wiring have been reversed this will allow current, via R2, to illuminate LP2; LP1 remaining off. A complete lack of an earth connection will be indicated by both neons being alight, current flowing via R1, LP1, LP2 and R2.

If an open circuit Neutral is present current will pass through R1 to LP1, and R3 and R2 to LP2. In this condition both neons will be illuminated.

The only correct indication is LP1 ON and LP2 OFF, see Table 1. Any other indication means that the outlet must be fully investigated, by a qualified electrician, before using it.

## PLUG ASSEMBLY

A standard flat pin 13A plug is used to house the components and the positioning and wiring is shown in Fig. 2. Grip a stout wire in the $E$ terminal of the plug and solder one end of both neons to this. Twist one end of R1 and R3


Mains Fault Indicator with cover removed. One end of R3 should be covered with insulating sleeving to avoid shorting to the heavy gauge wire.
connecting leads together, and fold over to give more grip, and secure with the $L$ terminal. Similarly secure R2 and R3 at the N terminal. Resistor R1 is then soldered to LP1 and R2 to LP2.

To avoid any possibilities of short circuits when wiring, particularly to the heavy gauge earth wire, it is recommended that the leads from the neons and one end of R3 ( $N$ terminal) be insulated with plastics sleeving.

Keep the neons about as high as the fuse, with electrodes horizontal. Fit a 2 A or 3 A fuse. The


Front cover of the plug showing viewing windows and suitable lettering indicating lamp state for correct conditions at outlet.
flexible cord securing grip is removed and the mains cable inlet hole blocked with a wooden plug cemented in.
Drill viewing holes about 6 to 9 mm in diameter directly over LPI and LP2 in the plug cover and cement pieces of transparent material over these holes inside the cover before replacing it.

## TESTING

The fault indicator can be tested by inserting it in a socket which has a 3 -core cord and plug, and simulating the faults listed in the operating conditions table at the plug. Remove the plug from the wall outlet before removing its cover or changing connections to it.

Table 1: Operating Conditions

| OUTLET | LP1 | LP2 |
| :--- | :--- | :--- |
| Gorract |  |  |
| (Current via R1 to LP1) | ON | OFF |
| Live open circuit <br> (No current to LP1 or LP2) | OFF | OFF |
| Land $N$ reversed |  |  |
| (Current via R2 to LP2) | OFF | ON |

No Earth
(Current via R1, LP1, LP2, R2)
$\begin{array}{lll}\text { Noutral open circut } & \text { ON } & \text { ON } \\ \text { ON } & \text { ON }\end{array}$ (Current via R1 to LP1, and via R8 and R2 to LPR)

To test outlets, insert the plug in the usual way. Only LP1 should light. In other cases a qualified electrician should look at, test and correct the circuit or plug connections, as necessary.

If the indication is correct at a wall outlet but not when an extension lead is added for remote use, connections at the extension plug and socket need to be examined. I


## Yes Dearl

I have just been watching a film called "The Stepford Wlves". For the beneft of those of you who do not know the story, it is about a quiet American town in the backwoods, where all the men have disposed of their wives and replaced them with exact replicas. Externally they are identical to the originals, but inside they are all wires, chips and various other electronic devices.

They are, needless to say all very beautiful but have the advantage that they can be programmed to enjoy housework, and always do their husbands slightest bidding without argument. It set me thinking, "an unusual occurrence", and $I$ thought just imagine this happening. You could build your own dolly bird, make her beautiful, curvaceous, like any film star and she would hurry to obey your slightest whim.
I was just about to write to Everyday Electronics to ask when they were going
to publish an article, on how to construct your very own sweetle pie, when wiser thoughts prevailed. Would I really prefer this lovely pneumatlc creature that hasn't the word "No" in her vocabulary to my present model, who, when I say I can't take her out, trles the effect of bouncing crockery off my head?
Such is the perversity of human nature, that I know in advance the answer would be "No". That I think is the weakness in the story. I think it could have been made into a hilarious comedy with all the models going wrong and running amok but the producers tried to treat it seriously and it wouldn't stand up to such treatment. However, it left me wondering if one day all this may be feasible, if so । shall look at electronics with renewed interest.

## Mail Order

Now, before I'm reminded that I am not employed as a film critic, let me hurriedly return to my brief. I was most annoyed to see the postal rates put up
yet again. We absorbed the last one without passing the increase on to our customers but there is a limit, after which we have no option but to try and recoup some of the increase. I feel it is particularly hard on the electronic constructors, who are dependent on mail order for so many of their supplies
The only advice I can offer, is to take advantage of suppliers offering a fixed postal rate, as many of us do, and send fewer, but larger orders. I belleve some retailers actually offer to send goods post free, if the order Is over a certaln value.

## A Good Connection

My regular readers may recollect that about two or three years ago I was very scathing about the fact, that the good old Bulgin P73 Mains Socket was suddenly condemned, by the madarins of the common market as unsafe. Consequently Messrs. Bulgin had to derate it from 250 volts a.c. down to 50 volts d.c.
I was therefore delighted when I saw that a well known and respected component supplier, had found a way round it. In the preamble to the description they simply say "These plugs are not suitable for making external mains connections to equipment for domestic use as defined in The Electrical Equip. ment (Safety) Regulations 1975". After which they proceed to rate them as before at 250 volts a.c. at 5 amps .

This means that you and I can carry on using them in the same way as before, and a good thing too, because when all is said and done, the P73 is a very useful and robust mains connector.

# RADIO WORLD <br> By Pat Hawker, gзva 

## Long-range VHF

Almost everyone who listens at all regularly on v.h.f.-broadcast or amateur stations-soon becomes aware of the marked extension to the distances over which signalstravel during "tropospheric" weather conditions; and also (during summer months in the UK) during the seemingly random "Sporadic E" conditions. Fresh light on both these phenomena has been reported recently.

The presence of water vapour at heights up to about $6,000 \mathrm{ft}$ combined with the existence of a "temperature inversion" (i.e. the air becoming warmer instead of cooler with increasing height) results in the bending and ducting of v.h.f. signals. Such conditions occur often in periods of fine warm anticyclonic weather and also during the misty days of late autumn and spring.

A good 'tropo opening' is regarded as bad news by broadcast engineers since it brings a big increase in the number of complaints of "patterning" on TV pictures or break-through of foreign languages on sound; but the same conditions are warmly welcomed by amateurs who find they can then make contact with stations as much as four times farther away than in "normal" conditions. On 144 MHz British amateurs have made contacts of some $2,000 \mathrm{~km}$; and on 432 MHz up to about $1,500 \mathrm{~km}$ although these distances are exceptional.
Much less known is the fact that tropospheric ducting is not confined to v.h.f./ u.h.f. signals but can also enhance ground wave signals on frequencies between $20-30 \mathrm{MHz}$ (and possibly sometimes even on much lower frequencies). It has been shown that over a 235 km sea path, signals may become as much as 20 dB stronger than normal when there is super-refraction or tropospheric ducting.

At the other end of the frequency scale, at $10,000 \mathrm{MHz}_{\text {, }}$ sea-path ducting has enabled British amateurs to span the distance from St. Ives, Cornwall to Portpatrick, Scotland using extremely low power (a few milliwatts). This was achieved in August 1976 but it has had a rather unexpected result: with an "over 500 km " record achieved, enthusiasm for further tests appears to have declined and the 10 GHz "record" has now passed to Italian amateurs who last year exceeded 600 km in the more favourable Mediterranean climate where super ducts form more readily than in our turbulent weather.

The other phenomenon, Sporadic E , is at last becoming more fully understood. Amateur observers and scientists over the past two years have produced fairly positive evidence linking Sporadic E with tiny metallic particles from burned out meteors and meteorites.

These particles become caught up in wind shears in the upper atmosphere, some $50-60$ miles above the Earth, becoming lonised from the action of the Sun to form highly reflective layers that
descend slowly as the day progresses. This has the effect that signals from about 20 to 100 MHz (and occasionally extending as high as the 144 MHz amateur band) can be received at good strength over distances up to about 1,000 miles.
Sporadic E layers thus seem to be basically metallic and are not layers of ionised gases as are the other layers of the ionosphere on which short-wave propagation depends.

## 3D for TV?

With many engineers in many countries working on ways in which television broadcasting could be extended, there is still doubt as to the most likely outcome. One possibility is the introduction of a second sound channel with better "separation" than is possible with the conventional pilot-tone stereo system used for sound radio.

The second channel could be used for stereo, or as a second-language channel, or possibly even as an additional radio broadcast channel. For instance some engineers believe we could consider using the line sync periods for carrying sound since it is now possible to build receivers with very stable line oscillators that need only an occasional sync pulse to keep in step with the studio cameras.
Then again, there is still interest in the idea of three-dimensional (3D) television which would give a better illusion of solidity, particularly if this could be achieved without the viewer having to wear special coloured glasses. In a recent English-language broadcast from Radio Moscow it was stated that 3D TV is being studied in Leningrad and has already been introduced for closed-circuit applications in order to provide better remote-handling instruments in nuclear plants. But apparently 3D TV for the home is not being given priority, although it was claimed that one such system had been tested some years ago and had proved to be quite effective for black-and-white pictures but attention has now turned to colour.
A number of inventors have described 3D TV systems in the UK but I do not feel there is much chance of any of these being adopted in the foreseeable future.
Another idea being proposed is multifocus photography in connection with TV film cameras, and a computer-aided system with digital processing was described recently at the National Film Theatre. Those of us present at that meeting came away disappointed that no firm evidence was presented to show that these ideas have reached the stage where real results can be demonstrated or what, even if the system proves technically feasible, would be the cost of introducing such a process.
A big advantage would be that the viewer would not have to change his set, as for most other possible innovations.

## Radiophone services

Citizen's band was originally introduced in the USA to appeal to people who, having no special technical interest in radio communication, nevertheless felt a need to have two-way communication facilities in their vehicles; in fact a sort of - poor man's London Radiophone service.

The Post Office system, of course, has many more features than CB and is tied in with the normal telephone service. "Selective calling" techniques mean that a user is alerted to receive only calls specifically intended for his "number" and the use of various automatic channelling systems and multiple base stations is all intended to provide a first-class, if rather expensive, public service throughout the London area

How effective is the system at present? Can a user, who will have paid some $£ 1,500$ for equipment from one of the three "approved" manufacturers, pays about £15 a quarter to the Post Office plus 25p per call, be reasonably sure of receiving and making calls whenever he wants to?

It would seem, from a report by lan Priest, G8PML in the newsletter of the UK FM Group (London) that the system works-but only "with a lot of luck and a great deal of difficulty". Outgoing calls from mobiles seem reasonably easy; the main problem is that the system tends to become overloaded at some times of the day and then the user, when called, finds he cannot seize a free channel, sometimes for as long as 20 minutes or soby which time his caller is likely to have given up and rung off.

The answer would seem to be that the Post Office needs much more "channel space" in other words a bigger chunk of the radio spectrum; and again that would allow them to reduce the two years or so "waiting period" for would-be subscribers. But is this practicable? One has the feeling that with any reasonable number of channels, the extra subscribers would soon be experiencing similar problems of overload.

## Radio Antarctic

The Racal Company tells me that more than 100 tonnes of equipment and sup-plies-including high-frequency radio equipment-is being flown over the Antarctic permafrost for members of the Transglobe Expedition in the mountains of the Borga Massif.

The expedition, which recently arrived in the Antarctic under the leadership of Sir Ranulph Fiennes, will camp for the Antarctic winter before pushing on to the South Pole and then on round the world by its polar axis. The expedition by six men and one woman will last some three years using Land Rovers, an adapted trawler and powered sledges.

The radio network is being established at a cost of some $£ 130,000$. Much will depend on the skill of Giles Kershaw who will make the airlift in a light aircraft. The company say "Should anything go wrong the members of the team would be left without adequate supplies during the worst part of the year. One hundred per cent reliable radio communications are essential."
Radio communication near the Poles is often very far from being reliable due to the difficult propagation conditions, so we had better keep our fingers crossed.

## You will not be too late

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MINI-MULTI TESTER

By Harry T. Kitchen

## Discipline

"What", you may well ask, 'has discipline to do with our workshop?', A great deal as I intend to explain if you read on.
Most of us are gullty of a lack of discipline in our lives, and this can insinuate itself Into our hobby unless we make a determined effort to maintain some form of discipline. Such an effort is well-worth while since it enables us to make the most of our limited time; this increased efficiency manifests itself as improved output, and hence pleasure.
Discipline begins with keeping a clean, tidy workshop. Let us now explore the extension of discipline to the keeping of records of your activities, particularly if you are well advanced, and hence have more to forget. Remember that memory is a most unreliable assistant-well, mine is, to be honest.

## Note Carefully

Notes of your experiments, of circuits built - successfully or otherwise - will prove invaluable since you can learn from your own mistakes by back-tracking, as a source of future inspiration, guidance, and as a means of easing trouble-shooting if necessary. A good stout A4 sized note book is not expensive, and is large enough to record most circuit details; if the circuit is too large, it is usually possible to break it down into sections.
Record also all relevant calculations, however elementary, all voltages and currents, the effects of circuit changes, in shorteverything. By doing so you will build up an invaluable diary of your workshop activities. In time it is quite possible that you will be able to guide others who may be struggling or have done something wrong in their constructional activities.

You should aiso keep a record of ideas for future action, matters that you have read about, and so on. It is debatable whether you should use two note books, one for current projects, the other for future projects. It depends on your ambitions and the scale of your activities. I personally use two such note books; one an A4 for current work, the other an A5 in which I make notes of articles that I think that I may wish to refer to later.

## Stock Control

In an earlier article I covered the purchasing of components. If your activities are modest, then you will probably have no problem keeping an eye on your stocks. If on the other hand you are into constructional work in an ambitious way, then it. is worth thinking about some form of "stock control", as this will enable you to check on your existing stock and to update it if necessary.
Again, a note book is handy and you can allocate pages to different components and the quantity in stock. As the stocks are used up you alter the quantities until
a time arrives when re-ordering is necessary. I would suggest that re-ordering is effected before you actually run out of any component.

This method also has the advantage that it high-lights components that are much used, as well as those that are littleused or used not at all.

## Experimental Aids

Under the somewhat non-committal heading of experimental aids come all sorts of things that are difficult to classify, are perhaps unheard of outside professional circles, but which make the life of the experimenter that bit easier. These can be either home-made or bought-out.

An extremely useful piece of equipment is the old-fashioned "bread board", literally a piece of board onto which all the components were attached as best possible. A modern equivalent that I myself used was a piece of s.r.b.p. board onto which turret tags were rivetted at intervals of $\frac{1}{4} \mathrm{in}$. Components went on one side, connections on the reverse.

A similar board could be built using 0.1 in matrix plain, pierced, board using Vero pins or similar. The ultimate, manufactured version, is the T-Dec and its variants, and exceedingly useful 1 find them, though I do on occasion find myself short of room and wishing for another board to slot in.

## Breadboards

Breadboards, home-made or manufac tured, provide you with the facility of trying out circuits before plunging into the traumas sometimes associated with building a circuit untried. This applies particularly to home-grown circuits, since you have the facility of changing components with relative ease.

Breadboards have one or two snags, though, and it is as well to consider these. The circuit, or rather the components comprising it, is strung out somewhat, and this is unavoidable to some extent.
With r.f. or high gain circuits feedback may be a problem. Also, the final layout, be it p.c.b. or matrix board, may not have quite the configuration that it had whilst strung out on the bread board; you may now have feedback that you didn't with the bread board.

## Connecting Leads

A usefui adjunct to the bread board is a. set of connecting leads. These take various guises, but are in essence varying lengths of connecting wire, typically 14/ 0076 or its metric equivalent, with crocodile clips, banana plugs, and the like to terminate them.

Large and small croc clips, large and small banana plugs, in all possible combinations; you will need them all, so useful are they for connecting to power supplies, meters, other boards, and so on.

## Substitution Boxes

Resistance and capacitance substitution boxes seem to have gone out of fashion, yet I wouldn't be without mine. Built many years ago, the resistance range covers 100 hms to 10 meg ohms in six swltched decades using the normal E12 range of $\frac{1}{2}$ watt 5 per cent carbon film resistors.

The capacitance box covers from $0 \cdot 1 \mu \mathrm{~F}$ to $1000 \mu \mathrm{~F}$. Up to $2 \cdot 2 \mu \mathrm{~F}$ the capacitors are polyester; over thai electrolytic; voltages cover 400 V (polyester) to 16 V (electrolytic).

Such boxes are not by any means difficult to build, nor expensive.

Switching offers resistor/capacitor values and their multipliers. For instance, the basic resistance range covers 100 hms to 91 ohms, the next is 100 hms to 9100 hms and so on, with one switch selecting the value, the other the multiplier. Similarly with the capacitance box.

The latter is of somewhat less use, certainly on the electrolytic side due to the wide tolerance of such capacitors, typically -50 per cent to +100 per cent. Below $0 \cdot 1 \mu \mathrm{~F}$ stray capacitance tends to nullify the usefulness. Even so, a capacitor substitution box serves as a very usefui "pointer"' towards the required value.

## Restrictions

In using such boxes, it is essential to remember that resistors have wattage restrictions, capacitors voltage restrictions. What this means is that you must not gaily place them in positions where the makers of the resistors and capacitors did not intend them to go.
Do so and you may be amazed at the amount of smoke a resistor exudes, or the amount of foil in an electrolytic capacitor!

"I'll try this silic and chips I've heard so much about"

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## BOOK REVIEWS

ELEMENTS OF ELECTRONICS-BOOKS 1, 2 and 3

Author
F. A. Wilson

Price
Size Publisher ISBN £2. 25 each

Bernard Babani
0900162821 (Book 1)
$180 \times 108 \mathrm{~mm} 200$ pages (approx.) each

090016283 X (Book 2)
090016284 X (Book 3)

NE of the latest additions to electronios eduoation literature is this set of books, described by the publishers as an "on going series of books aimed at the absolute beginner"

The uiltimate aim of the series is to enable anyone to have an inexpensive but comprehensive introduction to modern electronics although on the evidence of the first three volumes you would have to wade through nearly three books of theory before you even approached modern electronic techniques.

That apart, volume 1 gives a good grounding in basic eleotrical theory which is later expanded to include a.c. theory in Book 2. The electronios proper really starts in Book 3. Entitled "Semiconductor Technology", it concentrates on transistor theory although there are also short sections on logic i.c.s. and op.amps.

Generally speaking, presentation is quite good although it is let down from time to time by poor drawing and inconsistencies in the text that didn't ought to be there book of this kind.

## QUESTIONS AND ANSWERS-

 INTEGRATED CIRCUITSAuthor<br>Price<br>£1-55<br>Publisher<br>ISBN<br>R. G. Hibberd<br>$165 \times 110112$ pages<br>Newnes Technical Books<br>0408.004665

THE concept of presenting information in question and answer form is not new. A great number of educational aids and instruction manuals have been written in this style with varying degrees of success and this book certainly ranks amongst the more convincing.

In any publication of this sort the selection and order of questions is all important and here R. G. Hibberd has apparently been very successful.

Each question prepares the reader for the next (with one or two exceptions), and the accompanying artwork is particularly crisp and clear especially for the small page size.

The book, which is not in fact new but a revised edition of an older publication, answers a number of general questions on i.c. technology as well as more specific points on the separate chip families-linear, mos, digital, bipolar, etc. There are new sections on cmos, nmos, and vmos technologies and microprocessors are looked at for the first time.
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\section*{The Extra Ordinar Experiments of Proiessor Evnest <br> by Anthony John Bassert <br> |n Last month's issue, the Prof. left

his visitors Tom, Maurice and Bob, trying to solve the problem of what happens to the trigger-points of a Schmitt trigger when control potentiometers are used to move the two trigger-points closer together until the point of zero hysteresis is reached, and passed. Maurice has been tackling the problem by mental concentration and deductive reasoning.

## MENTAL APPROACH

After some careful consideration of the factors involved, Maurice announced:
"As the controls are adjusted to give less and less hysteresis, the circuit will respond to smaller and smaller signals, until eventually as the point of zero hysteresis is approached, it should become possible for the circuit to be triggered by really minute signals. It seems to me that the sensitivity of the circuit would approach infinity, and its behaviour would also come to approach that of an "infinite gain amplifier".
"Prof., is it really possible to obtain such a high performance from such a simple two-transistor circuit?
"I think that Bob is in the process of finding out-and he is certainly looking very excited about it".

## PRACTICAL APPROACH

Whilst Maurice had tackled the problem mentally by use of reasoning, Bob had used a practical


Fig. 1. Experimental Schmitt trigger circuit.
approach and built up a special experimental Schmitt Trigger circuit (Fig. 1).
He set VR3 so that its wiper was near to the end of the track conneoted to the emitter of TR1, and VR2 so that its wiper was near to the collector of TR1. Now by connecting a multimeter to indicate the voltage at the collector of TR2, and moving the wiper of VRI back and forth a few times, Bob found the two trigger points.
At one point of adjustment of VRl the collector voltage of TR2 suddenly became high (about 9 volts) and at the other point it suddenly fell to about 3 volts. A guitar signal fed to the input from a pre-amplifier sounded very harsh and crackly at first, but as Bob carefully adjusted VR2 so that the trigger-points came closer together, there came a point where a less crackly but intensely "fuzzy" sound was produced.

\section*{HELIUM BALLOON RADIO

## HELIUM BALLOON RADIO AERIAL

At one point of adjustment of VR1 and VR2, the circuit became very sensitive to the slightest vibration of the guitar strings, and also began to pick up radio signals, so I decided to test it as a radio receiver. I launched the Prof's. Helium Balloon Radio Aerial.
"Wow, Bob, What's that?" Tom asked.
"Look outside, Tom you'll see it", Bob replied.
"It is a long piece of aerial wire carried up by a gas-filled balloon. With this it is easily possible to receive a wide range of radio frequencies, and I thought that, with a sensitive receiving circuit it might be possible to receive radio signals from space".

As Bob manipulated a tapped tun-ing-coil and a tuning capacitor a huge variety of radio signals could be heard from the loudspeaker of the audio amplifier, but he could not tell Maurice which of these signals might have come from outer space!

## PASSING POINTS

"What I still would like to know" Maurice told Bob, "is what exactly happens when you adjust VR2 so that trigger points coincide, then pass each other?"
"That's easy," Bob replied. "The Schmitt trigger effect disappears and the circult becomes a high-gain
amplifier. As the wiper of VR2 approaches closer to the positive supply connection, the gain becomes lower and lower. By adjusting the wiper of VR1, two points can still be found; these are the positive saturation points of the amplifier beyond which it will not amplify any further in a positive direction, and the negative saturation point beyond which it will not amplify any further in a negative direction.
As VR2 is adjusted back down towards the point of zero hysteresis or backlash the gain rises and the two saturation points approach closer together until a point of very high gain is reached, and as VR2 is adjusted beyond this, two trigger-points appear, and we have our Schmitt effect again!"

## HIGH GAIN

"It is fascinating to think that you can obtain enormously high gain from a couple of cheap transistors in such a simple circuit!" The Prof. observed, and whilst Bob and Maurice were contemplating the possibilities of this for all sorts of oscilloscopes, amplifiers and signal detectors, the Prof. walked off with the electric guitar which Bob had been using to test his Schmitt trigger fuzz circuit!

A few moments later their contemplations were interrupted by some extraordinary guitar sounds which, al-
though very fuzzy, seemed to be also extraordinarily rich and full in tonal character.

## SPLITTER BOX

It was Tom, playing the guitar through a number of fuzz boxes all at once. The guitar was plugged into a signal splitter box from which a number of jack leads took the signal to the various fuzz boxes, each of which was plugged into a different amplifier.

There were both valve amplifiers and transistor amplifiers, so that "valve sound" was mixed with "transistor sound" and together with the different effects of the various fuzz boxes this contributed to the extraordinarily rich and full sound of the guitar which Tom was happily playing.
"Now with many fuzz box circuits the main problem is circuit noise. They produce just the sound the guitarist wants whilst he is playing, but during any pause or quiet spot in the music a loud hiss can be heard. This can be remedied by a circuit known as a "noise drive gate" whose function is to act as an attenuator, preventing the passage of this annoying hiss when the guitarist is not playing.


Fig. 2. Noise drive gate circuit.
The attenuator circuit will open its "gate" to let the sound through whilst the guitarist is playing, then quickly shut it again to cut out the hiss when he is not playing. Many commercial noise-drive gates are expensive, but here is a circuit (Fig. 2) which can easily be built in a very small space and will fit into most fuzz boxes. The control input of the noise gate is derived from the first or second pre-amplifier stage of the fuzz box; a suitable connection point can easily be found on most fuzz boxes, usually at the collector of the transistor.

From this control input signal the circuit, after adjustment of the sensitivity control, will very rapidly detect whether or not the guitar is playing, and the attenuator circuit then quickly either shuts off or lets through the signal."

To be continued


## BOOK REVIEWS

## ELECTRONICS-LEVEL 3

| Author | B. F. Gray |
| :--- | :--- |
| Price | $£ 4 \cdot 95$ |
| Size | $215 \times 140 \mathrm{~mm} 201$ pages |
| Publisher | Longman |
| ISBN | 0582411351 |

Ask any student what he wants out of a textbook and he will probably tell you that it should be clearly written, well set out, contain few irrelevancies and of course be inexpensive. In an already overcrowded market such as educational publishing, mistakes can be very costly, although in this case the author has avoided most of the major pitfalls.

This is the last in a series of three electronics texts and is written specifically for students studying the TEC Level III Electronics syllabus. However other readers who are fascinated by the theory behind many of their favourite projects need not be put off, as good presentation and a well thought out text make even the more extreme parts palatable.

Topics covered include f.e.t.s, voltage amplifiers, noise, feedback, oscillators and op-amps, and the book closes with a chapter on the ubiquitous microprocessor. Worked examples are included at all stages and only a rudimentary mathematical knowledge is assumed.

MICROPROCESSORS FOR HOBBYISTS

| Author | Ray Coles |
| :--- | :--- |
| Price | $£ 2.95$ (Limp Covers) |
| Size | $230 \times 155 \mathrm{~mm} 85$ pages |
| Publisher | Newnes Technical Books |
| ISBN | 0408004142 |

THis is a very good introduction to the microprocessor, that chip which yesterday was an esoteric subject but is now part of everyday technology. It is based on a series of articles published in Practical Electronics three years ago-and one of the first comprehensive popular technical accounts of the microprocessor to be written for the non-professional.

It says much for Mr Coles early perceptivity of (1) the microprocessor's potential power and influence and (2) the bewilderment this new development would cause to non-experts that his text is just as fresh and relevant today. It deserves the more permanent form and the chance to reach an even wider readership that this new presentation now affords.

The MPU chip, programming techniques, and peripheral chips are explained. Then come sections on home computers and software which will be valuable to the wouldbe computer owner. The extensive glossary explains those buzz terms peculiar to the world of microelectronics and computing.

Written primarily for the electronics enthusiast, the book will also be of assistance to the non-electronics person who is interested in computing but wishes also to obtain an insight into what lies behind the keyboard.

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| 4037 | ${ }^{90} \mathrm{p}$ | 7403 | 10p | 14 p | 7476 | 25p | 30p | 74190 | 69p | 78p | NE555 | 22 p |  | ARTS |  |  | pin 9.0p | TIP 41 | 50 p | 52p | 58p |
| 4040 | 55 p | 7404 | 10p | $14 p$ | 7480 | 35p |  | 74191 | 69p | 90p | NE556 | 50p |  | R16028 | 63 | 16 p | pin 10.0p | TIP 42 | 45p | 48 p | 59p |
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| 4043 | 30p | 7407 | 24p |  | 7483 | 45p | 58p | 74194 | 55p |  | NE567 | 100p |  |  | 9 p |  |  | 2N3054 |  |  | 33p |
| 4044 | 50 p | 7408 | 10p | 14 p | 7485 | ${ }^{60 p}$ | ${ }^{68 p}$ | 74195 | 48p | 60p | LM382 | 110p |  | Green | 11p |  | enerator for | BC108 |  |  | 7 p |
| 4046 | 75p | 7409 | 10p | 18p | 7486 | 20p | 30 p | 74198 | 49p | 78p | CA3080 | 68p |  | ellow | 11p |  | ARCH project | BC107 |  |  | 7p |
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