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| Gnaramtaed |  |  |
|  |  |  |
| 879 | 4 | IN4007 Sil. Rec. diodes. 1,000 PIV lamp plastic |
| B89 | 10 | Reed Swltches, $1^{10}$ long. $\frac{1}{1}^{\circ}$ dla. High Speed P.O. type |
| B99 | 200 | Mixed Capacitors. Approx. quantity. Aounted by weight |
| $\mathrm{H}_{4}$ | 250 | Mixed Resistors. Approx. quantity counted by welght |
| H35 | 100 | Mixed Dlodes. Germ, Gold bonded, etc. Marked and Unmarked. |
| $\mathrm{H}^{38}$ | 30 | Short lead Transistors, NPN Silicon Planar type |
| H39 | 6 | Integrated Circults. <br> 4 Gates BMC 962, 2 Filp <br> Flops BMC 945 |
| H61 | 2 | Sil Power transistors comp pair BD131/132 |

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PNP. $A F$ and $R F$ 55p B66 150 Germanium Diodes 00 Min. olass type 00 glass equiv. to OA 200 55p OA202
55p
386100 Sil. Diodes sub. min.
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$20 \begin{aligned} & \text { Bri26/7 Type Sillcon } \\ & \text { Rectifiers } 1 \text { amp }\end{aligned}$
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| AD149 | 50 | BCY7: | 13D | LM309K | 0081 | 289 | -2N706 | 109 | 2N3203 |  |
| AD161 | 39p | RD194 | 80p | 1.87 | 0 Cs 3 | $25 p$ | 2N930 | $20 p$ | 2N4002 |  |
| ADl62 | 38 p | HD131 | 450 | MAT191250 | 0 Cl 40 | 65 | 2N987 | 45 | 2N- 4126 |  |
| AP117 | 20 p | BP115 | 22p | MJES40 50p | OC170 | 25 | 2N1132 | 45p | - $2 \times 4871$ |  |
| AP118 | 50p | BY180 | 835 | MJ K5920 65p | OC20 | 55 p | $2 \times 1304$ | ${ }^{23} \mathrm{p}$ | 2 NS 457 |  |
| AF139 | 389 | BF194 | 130 |  | 0 O 2 | 90p | 2N1613 | 20. | 25001 | 3.00 |
| AF18G | 40 p | BFX13 | 255 | $75 p$ | OCP71 | 100 | 2v1671 | 1.00 | 28026 | 8.90 |
| A SMa39 | 44 p | Brix 34 | 55p | WPFİS 46p | ORP12 | $55 p$ | 2N2147 | 750 | 28303 | 70 p |
| A8Y27 | 30 p | BFX88 | 20p | NET217450 | OR1'60 | 45p | 2N2160 | 69D | 40250 | 45 |
| RA115 | 10 p | BFY50 | 20 D | NKT40480p | P346A | 20p | $2 N 2928$ | 10 p | 40381 | 45 D |
| ${ }_{\text {BAX }}{ }_{\text {BCl }}$ | 5 D | BFY5! | 20 p | OA5 600 | THL209 | 86p | 2N3053 | $20 p$ | 40362 | 40 p |
|  | 15 p | BFY64 | 45p | 0481 10p | TIP29.4 | 49p | $2 \times 3054$ | 45p | 40408 | 60 p |
| BC109 | 15 p | BLY ${ }^{\text {BL }}$ S6 | 88.25 | OA200 ${ }^{\text {OD }}$ | TIP30A | 58p | 2N3055 | 45p | 40486 | 750 |
| BCl09C | 140 | 188X20 | 15D | OCI6 85p | TIPsiA | 74p |  | 50p | 40636 |  |
| $\mathrm{BClla}^{\text {che }}$ | 180 | BU105 | 2.20 | OC20 | TIP42A | 90D | 2N35.2 | 1.10 | 40430 |  |
| BC147. | 129 | Brion | 15p | 0C28 65p | T1843 | 265 | 2N3614 |  |  |  |
| BC169C | 14D | B | 15 | Cs |  |  |  |  |  |  |


| 2N3055 |  |
| :---: | :---: |
| 25 | ....47p ea |
| 100 | ....420 |
| 500 | 39p |
| 1000 | . . 340 |
| BY127 |  |
| 25 | ...12p ea |
| 100 | ...10p |
| 500 | 9p |
| 1000 | ... 8p |

ZENER DIODES $400 \mathrm{~m} / \mathrm{w}$ BZY88/ volt -33 volts 10 p each
$1 \cdot 3$ watts $5 \%$ MIniature Tubulars From $3 \cdot 3$ voli volt 18p each. 10 watts. Sing series 6.8 volts -
100 volts $5 \% ~ 40$ D each.

TRIACS - Stnd. mounting with access ories
3 AMP RANCE


NEW RANGES
BRIDGERECTIFIERS
FEATURES SMALL SIZE AND LOW COST Sizes. are approx. 250H/A QUARTER AMP
B025/05 50 PIV
PIP $\begin{array}{lll}8025 / 05 & 50 \text { PVV 18p } \\ \text { B025/10 } 100 \text { PIV }\end{array}$

 AMPS P.



## SILICON CONTROLLED

RECTIFIERS


Lenrys
 RRONS • Tools - valves poic cores mest Type of coumpieris

## TEST

## EQUIPMENT

MULTIMETERS
(carr. etc. 30p)
 OTHER EQUIPMENT

| $\begin{aligned} & \text { SE250B } \\ & \text { SE500 } \\ & \text { TE15 } \end{aligned}$ | Pocket Signal Injector Pocket Signal Tracer |  | $\begin{aligned} & 2.10 \text { carr. 15p } \\ & 1.70 \text { carr. } 15 p \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Grid Dip meter 440kHz- |  |  |
| E40 AC Millivoltmeter 1.2 mHz 18.95 carr. 35p |  |  |  |
| TE65 28 Range valve voltmeter 19.95 carr . 40p |  |  |  |
| TE20D 120kHz-500mHz RF Gensrator $1 \%$. 95 carr .40 p |  |  |  |
|  |  |  |  |
| TE22D $20 \mathrm{Hz-200kHz}$ Audio Generato |  |  |  |
|  |  | 18.85 | 40p |
| $\begin{array}{lll}\text { SE350A } & \text { Deluxe Signal Tracer } & \\ \text { SE400 } & \text { Voltsfohms/R-C sub.l } & \\ & \text { RF field/RF carr. }\end{array}$ |  |  |  |
|  |  |  |  |
| New Revolutionary Supertester 680R |  |  |  |
|  |  |  |  |
|  |  |  |  |
| $\square$ Elactronic volimeter 18.00 |  |  |  |
|  |  | Ampelamp | 11.95 |
| Temperature probe 11.95 |  |  |  |
| \% $17 \mathrm{l} \mathrm{l}^{3}$ Guass meter $\quad 11.95$ |  |  |  |
|  |  |  |  |
| Phase Sequence $\quad 5.95$ |  |  |  |
|  |  | HT Probe | 5.95 |
| Shunts 25;50/100A 4.50 |  |  |  |
|  |  |  | each |

A SELECTION OF INTERESTING ITEMS
C3025 Compact transletortester $6.30 \mathrm{p} \& \mathrm{p} 15 \mathrm{p}$ E1300 Mono mag. cart. preamp. $\quad 2.75$ p \& 15 p E1310 Stereo mag. cart. preamp. $4.97 p$ \& $p 25$ p Easiphone telephone amplifler $\quad 7-95 p$ \& p $25 p$ D1203 Teleamp. With PU coil 7.40 P \& 20 D Chattalle (latercomm. and chime 73.95 p ap 250 1 Kw Dimmerfcontroller $\quad 3.00 \mathrm{p} 1010 \mathrm{p}$ 1Kw Oimmerfcontroller $\quad 3.30 \mathrm{p}$ \& O 10 p 16" Twin spring unit Reverbs VHF 105 Aircraft Band Corrector $\quad 4.50 \mathrm{p} \& \mathrm{p} 15 \mathrm{p}$ 320054 Ch. mlc. mixer
320042 ch . Stereo mlxer 3.75 p \& $p 15 p$
$5.95 p \& p 13 p$
cuits

## BUILD THIS RADIO

Portable MW LW
radio kit using Mullard
RFIF module. Features extra selectivity. Slow molion tuning. Fibre glass PVC cabinet. 600 MW output. All parts £7: 98 (battery 22p). carr. etc. 320.
EXCLUSIVE: SPECIAL OFFERS MWILW CAR RADIO AKAI GXC40 + or - Earth with speaker Stereo cassette recorder. and firings. $£ 5 \cdot 50$ carr. $/$ £59.95 carrfoackg. 50 p .
Palr Akal ADM micropackg. 30p. Palr Akal ADM micro* 20p.
8 TRACK CAR STEREO In 5 WAVEBAND PORTABLE (- Earth) with speakers in TWIN SPEAKER RADIO. $\begin{array}{ll}\text { carr/packg. 400. } & \text { FM/MW/SW/AIRCRAFT- } \\ & \text { PUBLIC SERVICES. } £ 10.45\end{array}$ HANIMAX HC1000 Carripackg. 30p.
Batiery cassette recorder. PORTABLE CASSETTE
10-50 carrioackg. 25p. TAPEPLAYERfor car or carry around. ©7-25 carr/packg. 20p.
HANIMAX HC2030 corder. $£ 13.50$ carrjpackg. CALCULATOR WITH 30 p

## SPECIAL PURCHASES

AVOMETER MOVEMENTS AVO 8 or 950 mA MOVEMENTS Ex Brand New AVO's $£ 3$-50 UHF TV TUNERS CHANNELS 21 TO-64 Brand new transistorised
geared tuners for 625 LIne geared tuners for 625 L.Ine
 Receizer 20 p .

## EASY TO BUILD KITS BY AMTRON- <br> EVERYTHING SUPPLIED

Model No.
310 Radio control receiver
300 4-channel R/C transmitter
Superhet R/C receiver
AM signal generator
8 watt Amplifier
8 watt Amplifier
Stereo control unlt
Mono control unit
Power supply for 115
Power supoly for 120
Power supply for $2 \times 120$
Auto packing liaht
Mic. preamplifior
2 LF generalor $10 \mathrm{~Hz}-1 \mathrm{mHz}$
Sq. wave generator $20 \mathrm{~Hz}-20 \mathrm{Khz}$
SWR meter

NH-CAD Charter 1-2-12
Ni-CAD Charger 1 2-12v $0.25-0.1$ A
DC motor speed Gov.
Windscreen wiper timer
Acoustic switch
Metal Detector (electronics only)
Capacitive Burglar alarm
Delay car amp.
CAP. Discharge ignition for car englne (-Ve Earth)

$$
\begin{aligned}
& \text { Scopo Callbrator } \\
& \text { Level indicator, }
\end{aligned}
$$

555 120-160 mHz VHF timer
Photo cell switch
lity tester
ter
871 Shoto timer
235 Acoustic Alarm for driver
465 Quartz XTAL checker
320 Slgnal Injector
432 Testakit
670 Buffer Battery Charger
885 Capacittlve Contact Alarm
850 Electronic Keyer


ALL KITS OFFERED
SUBJECT TO
STOCK
AVAILABILITY
Prices correct at time of preparation without notice.

## BUILD THIS TUNER

MW/LW Radio Turner to use with any ampliffer. Features Mullard RFIF module Ferrlte aerlal, bullt All parts $£ 4 \cdot 85$, carr. $15 p$.
MULTI-USE \& RADIONIC KITS
10-1 10 Projects
$150-1150$ Projects
Telephone Communicator
$\left.\begin{array}{ll} \\ \times 20 & 20 \text { (Elec.) } \\ \times 20\end{array}\right\}$ Projects
(carr.packing 400)
All transistor circuits with hand books
All types offered subject to avallability. Prices correct at time of press $E$ a OE. $10 \%$ VAT TO BE ADDED TO ALL ORDERS. UK post ete. 15p per order unless stated.
EDGWARE ROAD, W2
SEE FACING PAGE FOR ADDRESSES

## YATES ELECTRONICS （FLITWICK）LTD

## DEPT．E．E．，ELSTOW STORAGE DEPT．

 KEMPSTON HARDWICK， BEDFORD．C．W．O．PLEASE．POST AND PACKING PLEASE ADD 10p TO ORDERS UNDER 2.
Catalogue which contains data sheers for most of the components listed will be sent free on request． 10p stamp appreciated．

## PLEASE ADD $10 \%$ VAT

## RESISTOAS

$\frac{1}{2}$ W Iskra high scabiltty carbon film－very low noise－capless construction． W Mullard CR25 earbon film－very small body size $7.5 \times 2.5 \mathrm{~mm}$ W $2 \%$ ELECTROSIL TRS．
Power
wates


DEVELOPMENT PACK
0.5 watt $5 \%$ Iskra resistors 5 off each value $4 \cdot 70$ to $1 \mathrm{M} \Omega$ ．
E：2 pack 325 resistors $22 \cdot 40$ ．E24 oack 650 resistors $64 \cdot 70$ ．

POTENTIOMETERS
Carbon track $5 k \Omega$ to $2 M \Omega$ ，log or linear（log $\ddagger W$ ，lin $\frac{t}{} W$ ）．
Single，12p．Dual gang（sterco）． 40 p．Single D．P．switch， 24 p．

SKELETON PRESET POTENTIOMETERS
Linear： $100,250,500 \Omega$ and decades co 5M $\Omega$ ．Horizontal or vertieal P．C． mounting（ 0.1 matrix）．
Subominiacure 0．1W．5p each．Miniature $0.25 \mathrm{~W}, 7 \mathrm{p}$ each．

## TRANSISTORS

| AC107 | 15p | AFI26 | 20p | BFII5 | 25p | $0 C 42$ | 12p | 2N3707 | 120 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ACI26． | 12p | AFI39 | 32p | BF173 | 20p | OC44 | $12 p$ | 2N3708 | 10 p |
| AC127 | 150 | AFI7B | 32p | BF177． | 28p | OC45 | 12p | 2N3709 | 11 p |
| AC128 | 15p | AFI80 | 40p | BF178 | 320 | OC70 | 12p | 2N3710 | 11 p |
| ACI31 | 12p | AFI81 | 40p | 8F179 | 32p | OC71 | 12p | 2N37！1 | 11 p |
| ACI 32 | 12p | BCl07 | 12p | BF180 | 32p | OC72 | 12p | 2N3819 | 32p |
| ACI76 | 15p | BCl08 | 12p | BFI81 | 32p | OC81 | 12p | $2 N 4062$ | 12p |
| ACl87 | 220 | BC109 | 12p | 8F194 | 14p | OC820 | 12p | 2N4286 | 20p |
| ACl88 | 22p | BC147 | 12p | BF195 | 14p | 2N2646 | 60p | 2N4289 | 20 |
| ADI40 | 50p | BC148 | 12p | BF197 | $15 p$ | 2N2904 | 20p | 40360 | $35 \%$ |
| ADI49 | 45p | BCI49 | 12 p | BF200 | 32p | 2N2926 | 10p | 40361 | 35p |
| AD161 | 33p | BC157 | 14 p | BFY50 | 20p | 2N3054 | 58p | 40362 | 40p |
| AD162 | 36 p | BC158 | 14 p | BFY 51 | 20p | 2N305S | 60p | 40408 | 40 p |
| AF114 | 20p | BCI59 | 14p | BFY52 | 20p | 2N3702 | 13p | $2 T \times 108$ | 15p |
| AFl15 | 20p | BC187 | 22p | BUY105 | 225p | 2N3703 | 12p | ZTX300 | 15p |
| AFl 16 | 20p | BDI31 | 75 p | OC26 | 45p | 2N3704 | 13p | ZTX302 | 20p |
| AFlil | 20p | BDI32 | 75p | OC28 | 50p | 2N3705 | 12p | ZTX500 | 15p |
| $A F I I B$ | 38p | BDI33 | 75p | OC35 | 50p | 2N3706 | $11 p$ | $2 \times 7503$ | 20p |

ZENER DIODES WIRE WOUND POTS．3W，10， 25 $400 \mathrm{~mW} 5 \% 3 \cdot 3 \mathrm{~V}$ to 30 V ，12p． 500 and decades to $100 \mathrm{k} \Omega, 35 \mathrm{p}$ ．

## DIODES

AECTIFIER BY127
IN4001
IN4002
IN4004
IN4006
IN4006
N4007

SLIDER POTENTIOMETERS
$86 \mathrm{~mm} \times 9 \mathrm{~mm} \times 16 \mathrm{~mm}$ ．length of track 59 mm SINGLE $10 \mathrm{~K}, 25 \mathrm{~K}, 100 \mathrm{~K}$ log．or lin． 40 p ． DUAL GANG．10K＋10K etc．log．or lin．60p KNOB FOR ABOVE，12p．
FRONT PANEL．65p．
18 Gauge panel 12 in $\times 4$ in with slots cue for use with slider pots．Grey or mate black finish com－ plete with fixings for 4 poss．

SIGN
OABS OA8S

## \section*{1250 V} <br> 1250 V 50 V 100 V 400 V

｜A

|  |  |
| :---: | :---: |
| 12p | SIGNAL |
| 7p | OA85 |
| 8p | OA90 |
| 8p | OA91 |
| 10p | OA202 |
| 10p | $1 N 4148$ |

$7 p$
$5 p$
$5 p$
$7 p$
$5 p$
$8 p$

| ALUMINIUM BOXES |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AB7 | $22^{\prime \prime} \times 5 t^{\prime \prime} \times 1 \frac{1}{\prime \prime}^{\prime \prime}$ | 50p | AB14 | $7{ }^{\prime \prime} \times 5^{\prime \prime} \times 2 \frac{1}{\prime \prime \prime}^{\prime \prime}$ | 84 p |
| AB8 | $4^{\prime \prime} \times 4^{\prime \prime} \times 1{ }^{\prime \prime}$ | 50p | ABI5 | $8^{\prime \prime} \times 6^{\prime \prime} \times 3^{\prime \prime}$ | 108p |
| AB9 |  | 50p | AB16 | $10^{\prime \prime} \times 7^{\prime \prime} \times 3^{\prime \prime}$ | 122p |
| ABIO | $4^{\prime \prime} \times 5$ n $^{\prime \prime} \times 1 \frac{1}{4}$ | 50\％ | A817 | $10^{\prime \prime \prime} \times 42^{\prime \prime} \times 3^{\prime \prime}$ | 108p |
| ABII | $4^{\prime \prime} \times 2{ }^{\prime \prime} \times 2^{\prime \prime}$ | 60p | AB18 | $12^{\prime \prime} \times 5^{\prime \prime} \times 3^{\prime \prime}$ | 1200 |
| AB12 | $3^{\prime \prime} \times 2^{\prime \prime} \times 1^{\prime \prime}$ | 44p | AB19 | $12^{\prime \prime} \times 8^{\prime \prime} \times 3^{\prime \prime}$ | 160p |


| HEATSINKS－REDPOINT |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 2W | 24p | 4W | 45p | TOS Clip | 5p | TOI Single | 5p |
| 3W | $36 p$ | SW | 60p | TOI8 Clip | 5p | TOI Double |  |

MULLARD POLYESTER CAPACITORS C296 SERIES $400 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F}, 0.0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 2 \frac{1}{2} \mathrm{p}, 0.0068 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}$ $0.015 \mu \mathrm{~F} \quad 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 3 \mathrm{p} .0 .047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 4 \mathrm{p}, 0.15 \mu \mathrm{~F}, 6 \mathrm{p} .0 .22 \mu \mathrm{~F}$ ．


MULLARD POLYESTER CAPACITORS C280 SERIES
250 V P．C．mouncing：0．01 $\mu \mathrm{F}$ ， $\mathrm{m}^{2}$ ． $0.02 \mu \mathrm{~F}$ ． $0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}$ ， $3 \frac{1}{2 p} 0.1 \mu \mathrm{~F}, 4 \mathrm{p} .0 .15 \mu \mathrm{~F} .0 .22 \mu \mathrm{~F}, 5 \mathrm{p} .0 .33 \mu \mathrm{~F}, 6 \frac{1}{2} \mathrm{p} .0 .47 \mu \mathrm{~F} .8 \div \mathrm{p} .0 .68 \mu \mathrm{~F} .11 \mathrm{p} .1 \cdot 0 \mu \mathrm{~F}$ ，
$\begin{array}{ll}\text { MYLAR FILM CAPACITORS IODV CERAMIC DISC CAPACITORS } \\ 0.001 \mu F, ~ & 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.02 \mu \mathrm{~F} . \\ \text { IOOpF to } 10.000 \mathrm{pF}, 20 \text { each．}\end{array}$ $0.002 \mu \mathrm{~F}, 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.02 \mu \mathrm{~F}$ ．

100 pF to 10.000 pF ， 20 each

## ELECTROLYTIC CAPACITORS


 $10040.150 / 25,22025,330110,47016-3,70,68,63,150 i 40,22040,33016,1000 / 4,10 \mathrm{p}$. $170 / 10.680 / 6-3,11 \mathrm{p} .100 / 63$ ． $150 / 63,220 / 63,1000 / 10,12 \mathrm{p} .47025 .680 / 16.1500 / 6 \cdot 3,13 \mathrm{p}$. $470 / 40$ ． $680,25,1000 / 16,1500 / 10,22006.3,18 \mathrm{p} .330 / 63.680 / 40,1000 ; 25,1500 / 16$. 2200／10．3300，6－3．4700／4，21p


## VEROBOARD

| 0.1 | 0.15 |
| :---: | :---: |
| $2 \frac{1}{7} \times 3 \frac{1}{2}$ ． $22 p$ | 16p |
| $2+\times 5$ 24p | 240 |
| $31 \times 32$ | $24 p$ |
| $34 \times 5$ 27p | 27p |
| $17 \times 2 \%$ 75p | 57.0 |
| $17 \times 3 \frac{1}{2}$ 100p | 78 p |
| $17 \times 5$（plain） | 82 p |
| $17 \times 34$（plain） | 60p |
| $17 \times 2 \frac{1}{\frac{1}{2}}$（olain） | $42 p$ |
| $21 \times 5$（olain） | 12p |
| $24 \times 33$（plain） | $11 p$ |
| Pin insertion tool 520 | $52 p$ |
| 5por face custer ${ }^{42 p}$ Pkt． 50 pins $20 p$ | 42p |


| JACK PLUGS AND SOCKETS |  |  |  |
| :--- | :--- | :--- | ---: |
| Standard screcned | $18 p$ | 2.5 mm insulated | $8 p$ |
| Standard insulated | $12 p$ | 3.5 mm insuiated | $8 p$ |
| Sterco screcned | $35 p$ | 3.5 mm screened | $13 p$ |
| Standard socker | $15 p$ | 2.5 mm sockek | $8 p$ |
| Stereo socket | $18 p$ | 3.5 mm socket | $8 p$ |

D．I．N．PLUGS AND SOCKETS
2 pin， 3 pin． 5 pin $180^{\circ}, 5$ pin $240^{\circ} .6$ pin
Plus i2p．Socker 8p
4 way screened cable， 15 pimerre．
BATTERY ELIMINATOR

$$
\begin{array}{llllllll}
\text { LARGE (CAN) ELECTROLYTICS } & & & \\
1600 \mu \mathrm{~F} & 64 \mathrm{~V} & 74 \mathrm{p} & 2500 \mu \mathrm{~F} & 64 \mathrm{~V} & 80 \mathrm{p} & 4500 \mu \mathrm{~F} & -16 \mathrm{~V} \\
2500 \mu \mathrm{~F} & 40 \mathrm{~V} & 74 \mathrm{p} & 2800 \mu \mathrm{~F} & 100 \mathrm{~V} & 62.60 & 4500 \mu \mathrm{~F} & 25 \mathrm{~V} \\
\hline 1.68 \\
2500 \mu \mathrm{~F} & 50 \mathrm{~V} & 58 \mathrm{p} & 3200 \mu \mathrm{~F} & 16 \mathrm{~V} & 50 p & 5000 \mu \mathrm{~F} & 50 \mathrm{~V} \\
\mathrm{El} & \mathrm{El} \cdot 10
\end{array}
$$ HIGH VOLTAGE TUBULAR CAPACITORS－ 1,000 VOLT

$$
\begin{array}{lllll}
0.01 \mu \mathrm{~F} & 10 \mathrm{p} & 0.047 \mu \mathrm{~F} & 13 p & 0.22 \mu \mathrm{~F} \\
0.022 \mu \mathrm{~F} & 12 \mathrm{p} & 0.1 \mu \mathrm{~F} & 13 \mathrm{p} & 0.47 \mu \mathrm{~F} \\
0.22 p
\end{array}
$$ POLYSTYRENE CAPACITORS $160 \mathrm{~V} 2 \frac{1}{2} \%$

10pF TO 1,000 DF EI2 Series Values．ip each．

## SMOKE AND COMBUSTIBLE GAS DETECTOR－GDI

The GDI is the world＇s first semiconductor that can convert a concentrasion of eas or smoke into an electrical signal．The sensor decreases ics electrical resistance when it absorbs deoxidizing or combustible gases such as hydrogen．carbon monoxide． methane，propane，alcohol，North Sea ras．as well as carbon－dust containing air or smoke．This decrease is usually large cnough to be utilized without amplification． Full details and circuiks are supplied with each detector．
Detector GDI．E2．Kis of parts for detecrors includinz GDI and P．C．board but excluding case．Mains operated derecror $\mathbf{8 5} \cdot \mathbf{2 0}$ ． 12 or 24 V batcery operated audibie alarm E7．30．As above for PP9 batiery．$£ 6.40$ ．
PRINTED BOARD MARKER
97p
Draw the planned circuit onto a copper laminate board with the P．C．－Pen，allow to dry，and immerse the board in the etchant．On removal the circuit remains in high relief．

METERS
1\}"Scale-500uA. ImA. $10 \mathrm{~mA}, 100 \mathrm{~mA}$
E1． 90

BULGIN MAINS CONNECTORS

| 3 Pin | $1 \frac{1}{2}$ A | Chassis Plug Line Socket | $\begin{array}{r} 10 p \\ 13 p \end{array}$ | 3 Pin | $1 \frac{1}{2} A$ | Chassis Socket Line Plug | $\begin{aligned} & 18 p \\ & 13 p \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 Pin | 3A | Chassis Plug line Socket | $\begin{aligned} & 10 p \\ & 14 p \end{aligned}$ | 3 Pin | 3A | Chassis 5ocker Line Plug | 21p |
| 3 Pin | 5A | Chassis Plup Line Sockex | $\begin{aligned} & 16 p \\ & 15 p \end{aligned}$ | 2 Pin | 5A | Line Pluz | 20p |


| THERMISTORS VA1005 VA1026 VA 1033 VA $1055 S$ VA 10665 VA1077 R53 | $\begin{array}{r} 15 p \\ 15 p \\ 15 p \\ 15 p \\ 15 p \\ 15 p \\ f 1.35 \end{array}$ |
| :---: | :---: |
| WAVECHANGE Ip 12 W .3 F 4 W ． | SWIT $\mathrm{p} 2 \mathrm{~W}$ |

ROTART MAINS SWITCH D．P．2A 32D

| LINEAR IC＇s |  |  |
| :--- | :--- | :--- |
| 709 | 14 pin DIL | $40 p$ |
| 741 | 8 pin DIL | $40 p$ |
| 741 | 14 pin DIL | $38 p$ |
| 723 | 14 pin DIL | $95 p$ |
| 747 | 14 pin DIL | $85 p$ |
| 748 | 8 pin DIL | $45 p$ |
| DIL Sockexs 14 pin and 16 pin $16 p$ |  |  |

## Understand Solid State Electronics?

Quite possibly you do it's also quite possible your knowiedge is not as broad as it might be and probably you're keen to fill in the gaps.
Whatever the extent of your knowledge in this fast-moving technology. it's a fair bet that this litzle book can help you find a few missing answers.
Designed for anyone who wants for needs) to understand how semiconductors work and how they work together in solid state electronic systems, this book takes the reader through a 12 -lesson, self-teaching course written in laymands language.
The course. complete with quizzes and glossaries covers basic theory and use of diodes, transistors, thyristors, optoelectronic .devices. It also covers logic and bipolar. MOS and linear integrated circuits.

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# everyday electronics 

## PLEASE HELP YOURSELF!

It is simple and inexpensive to make a start in the hobby of electronics. The bare essentials in equipment are a soldering iron, screwdriver, wire cutters, pliers, and a modest type of multimeter.

But let us be honest-it is hardly likely to stop just there! After completing a few simple projects the urge to delve progressively further and deeper into the subject comes quite naturally; to conduct experiments and try one's hand at circuit design, for example.

However, visions of the need for additional expensive equipment may cause some enthusiasts to hesitate and ponder over the probable financial outlay involved. Well, we have good and reassuring news in this connection. While many spare time activities do depend upon commercially made equipment that is often expensive, in the case of electronics "do-it-yourself" is doubly true! The most important circuit checks and measurements can be performed with instruments of a kind that the constructor can build himself-provided he is given full design details.
This month Everyday Electronics introduces the EE Test Gear Five, commissioned specially for our readers. Collectively, these five instruments will satisfy all the more usual requirements of the average constructor, experimenter, and designer. While a careful eye has been kept on the budget, these units have been designed to the highest professional standards.

This, then, is an opportunity for every reader to equip himself with a fine set of test gear-
instruments he will be proud to own and use and to show to his friends because they will demonstrate his own handiwork as a constructor. These five handsome instruments will transform the appearance of any "den" or private retreat, however modest. Their good looks are incidental however. The instruments are designed for serious work, not just to impress the visitorthough undoubtedly they will. With the EE Test Gear Five before him, the least pretentious of constructors will feel confident to tackle more ambitious projects and maybe venture into some experimental and design work in addition.

A word to the wise. All these instruments will have immediate and lasting value. So start building your collection this very month, with item number one-the Power Supply Unit.

Those more seasoned enthusiasts who already possess some items of test gear may well consider the merits of having a unified set of instruments with a common power supply linkage. Otherwise, one or more items of the EE Test Gear Five could be used to make up any deficiency in their existing equipment.

## OUR NEW PRICE

Soaring costs of materials, especially paper; have caught up with us. Regrettably we have to advise readers that as from next month the price of Everyday Electronics will be 20p.


Our March issue will be published on Friday, February 15

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[^1]
## EASY TO CONSTRUCT SIMPLY EXPLAINED

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[^2]For more details see page 105



Automatically switches on an auxiliary lighting system when mains supply fails

In these days of perpetual electricity failures it is convenient to have an auxiliary source of lighting in the home. It is mandatory that clubs and public areas have an emergency lighting circuit capable of running from a source independent from the mains.
The simple solution, in either case, is to have a circuit, or circuits, running 12 volt bulbs from an accumulator. This, however, requires that the accumulator is in a constant state of charge. This project is basically a battery charger that is used to keep the accumulator "topped up" but wired into it are two switchable output sockets for running auxiliary lighting and facility is built in for automatic change over to the emergency system, should the mains fail.

## CIRCUIT

The circuit is shown in Fig. 1. A tapped input mains transformer is used that gives a nominal output of 12 V r.m.s. ( 17 V peak) at up to 5 A . This is fed to a low voltage, high current bridge rectifier giving a full wave rectified output that is fed via a switchable series limiting resistor R2 and ammeter circuit to the terminals of the unit. The stand-by accumulator would be connected to these terminals.

With the series resistor in circuit charge current is limited to about 0.5 to 1 A (for trickle charge purposes) but when shorted out with S2 the circuit current is limited only by the internal resistance of the transformer, the resistance of the ammeter circuit and the state of charge of the accumulator. Current could be up to 5 A (and even greater). Should there be some major
fault with the accumulator or the output was shorted then current could exceed the 5A (maximum) and a fuse is inserted to prevent overheating ctc.

## LIGHTING CIRCUITS

The auxiliary lighting circuits are taken from the battery terminals via the relay contacts to switches S3 and S4 to output sockets on the front pancl. These circuits are connected on the front side of the same fuse. Because the relay (normally held in by the 12 V a.c. from the transformer) is connected with its "normally closed" contacts in the auxiliary circuit, current cannot flow through the bulbs unless the mains fails. When this happens the relay drops out and current from the battery flows the other way through the fuse into the auxiliary circuit. Thus both circuits are protected by the single fuse.

Some constructors may not wish to build in the automatic change over facility; in which case the auxiliary circuit ought to be separately fused.



## CURRENT

If the unit is to be run from the mains via a fused 13A plug there is no need for an internal fuse on the mains input but take note that this is essential if the unit is to be run from non-ring main domestic wiring (a 500 mA fuse is sufficient).

With this system the maximum output current to the bulbs is 5 amps (not displayed on the meter) thus the total power loading must not exceed 60 watts. In a domestic situation this is more than is necessary and in practice two circuits with a loading of 2 amps each is quite sufficient. Switches S3 and S4 allow selection of either or both external circuits in the usual way.

Remember that this unit provides high currents, consequently heavier gauge wire than usual should be used ( 10 amp rating preferably) for all internal and external connections (Fig. 2). It is particularly important to have this in mind if the equipment is to be permanently wired into a building's structure. If the wire is too light a gauge not only will you get excessive line voltage drops but the conductors could heat up and present a fire risk.

## INSTALLATION

When installing the equipment make sure the accumulator is in a well ventilated area because hydrogen and oxygen are liberated during charging-a localised build up of these gases could cause an explosion if exposed to a naked flame. Ideally it should be contained in a wooden (frost protected) box outside.
The charger unit should be as close as possible to the accumulator but for convenience it is more likely that the latter would be indoors, nevertheless keep the leads to the accumulator as short as possible. The longer they are the heavier gauge they ought to be to prevent line drop.

When charging a badly exhausted accumulator it is best to charge at the trickle rate for an hour or two before changing to full rate-other-

Fig. 1. Complete circuit diagram of the Emergency Lighting Unit.

## Components . . . .

## Resistors <br> R1 $22 \Omega 2 \mathrm{~W}$ (see text) <br> R2 $2.2 \Omega 5 \mathrm{~W}$ <br> SHOP <br> taik <br> Capacitor

C1 $1,000 \mu \mathrm{~F}$ elect. $25^{\circ} \mathrm{V}$

## Semiconductors

D1 1N4001
D2) $5 \mathrm{~A}, 24 \mathrm{~V}$ silicon bridge rectifier (AEI
D3 type PM7A6) or equivalent wired group
D4 of 5 A rectifiers ( 4 off )
Switches
S1 Two pole 3 A 240 V on/off toggles. S2 3 (Both poles shorted together for S2, 3 S3 and 4)

## Miscellaneous

ME1 5A moving iron meter
RLA1 6 V coil, 260 hms with 5 A changeover contacts (see text)
LP1 240V neon indicator-incorporating limiting resistor
T1 Mains transformer. Primary 0-210, 230, 240, 250. Secondary 12 V at 5A (Douglas type MT 85AT)
FS1 Bulgin panel mounting fuse holder and 5 A fuse
SK1/2 2 plug socket pairs for auxiliary circuits (5A capacity)
SK3/4 2 red, 1 black 5A screw terminals
2 large crocodile clips for accumulator. Heavy gauge insulated wire, 3 core mains lead, grommet and cable clamp. Case approx. $200 \mathrm{~mm} \times 150 \mathrm{~mm} \times 150 \mathrm{~mm}$.

## EMERGENCY LIGHTING UNIT



Fig. 2. Layout and wiring of the Emergency Lighting Unit.
wise currents in excess of 5 amps might be drawn．Use can be made of the tapped mains input of the transformer（if such a transformer


The completed unit with front panel removed to show construction．Relay types may differ from that shown in the photograph．
has been used）to slightly increase or decrease the maximum charging rates．The output of 12 V r．m．s．assumes the supply is connected to the input tapping of the same magnitude（e．g． 240 V ）． If，however，you connect 240 V across the 210 V tappings the output voltage will increase by about 15 per cent．Connecting to higher voltage tappings will reduce the output voltage and hence the charge current．Should the maximum charge current be higher than required a $0-5$ or 1 ohm resistor（ 5 watt）should be inserted between S2 and FS1 at point A（Fig 1）．

## COMPONENTS

Finally，some points about the construction and availability of components．The diode bridge must be capable of passing 5 amps ．If you cannot obtain the one specified you can make one up using discrete stud rectifiers（of 5 amps rating each）which are easily obtainable．They should， however，be bolted onto a panel of insulating material prior to fixing in the cabinet．

The relay might present some problems but a variety will do here．Ideally an a．c． 12 V coil relay with 5 amp low voltage rating contacts should be used straight across the transformer＇s secondary，but relays with a．c．coils are not very common．The prototype used a 6 V d．c．relay that had a coil resistance of 26 ohms．The d．c． drive is provided by rectifier D1 and the current （from the 12 V source）is limited by R1 which should be of 2 watts rating， Cl prevents chatter of the relay contacts．If you locate a 12 V d．c．coil relay with 5 amp contacts Rl can be omitted．

Because of problems in locating or making low value shunt resistors for a milliameter a 5 amp moving iron meter was used as a current monitor．Moving coil meters of the same full scale reading could be used just as effectively but are likely to be more expensive．

## What do youknow？

TERMS
Explain the following terms as used when dis－ cussing electronic circuits or phenomenon．
1 Direct Coupling
2 Bandwidth（applied to a receiver）
3 Sensitivity
4 Modulation Depth
5 Bias



## ANSWERS

## 

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# Tgxilit FOR BECHWERS W ELECTROIVCS... THEORV AND EXPERMEVTS 

TUTOR: PHIL ALLCOCK*

## LESSON 5 The Transistor

So far we have mentioned the relationship that exists between the base, collector, and emitter currents of an $n p n$ transistor and have examined the current/voltage characteristic for the emitter/base junction.

## TRANSISTOR CHARACTERISTICS

Manufacturers often publish other characteristics such as the variation of $I_{c}$ with $V_{c e}$. Such a characteristic is illustrated in Fig. 5•1. Each curve shows the variation of $I_{c}$, as $V_{\text {ce }}$ is varied, for a constant value of base current $I_{l}$.


Fig. 5.1. Variation of $I_{c}$ with $V_{\text {ce. }}$
The curves usually relate to a "typical" device and the values for a particular transistor may differ considerably from the published curves since the parameter $\beta$ has a wide spread. However, the curves are useful in that they illustrate several important features of the transistor.

The first point is that for $V_{\text {ce }}$ values greater than about one volt the collector current is almost constant for a given value of $I_{\mathrm{l}}$. The collector current does rise slightly as can be seen from the $I_{b}=100 \mu \mathrm{~A}$ curve. The current $I_{e}$ rises by a small amount, shown as $\Delta I_{\mathrm{c}}$, as $V_{\text {cc }}$ increases from 1.0 to $5 \cdot 0$ volts. For a typical device this current change might be about 40 to $100 \Perp \mathrm{~A}$. Note
that the collector current for this curve would be about 10 mA , if we assume that $\beta$ is 100 , since we saw last month that $I_{c}=\beta I_{b}$.
Although a change of $100 \mu \mathrm{~A}$ seems quite large when compared to the base current of $100 \mu \mathrm{~A}$ it represents only one per cent of the total collector current. Consequently for most purposes we can assume that $I_{c}$ is independent of the voltage $V_{c o}$ if $V_{\infty}$ is at least one volt. (For power transistors the change in $I_{c}$ can be much larger and may have to be considered.)

## GAIN

The second point which is illustrated by the characteristics is that $\beta$ does vary somewhat with $I_{c}$. If $\beta$ was constant, each increase of say $100 \mu \mathrm{~A}$ in $I_{\mathrm{b}}$ would produce a definite change in $I_{c}$, equal to $(100 \beta) \mu \mathrm{A}$. The changes in collector current can be read off the characteristics by measuring the spacing of the curves at a given $V_{\text {ce, }}$, say 1 volt, whilst noting the corresponding changes in base current for the curves used. For example at $V_{\mathrm{ct}}=1.0$ volt, changes of $100 \mu \mathrm{~A}$ in $I_{b}$, over the range 100 to $400 \mu \mathrm{~A}$, give collector current changes represented by the lengths $A, B, C$. If these lengths are unequal then $\beta$ is varying as $I_{c}$ rises.

Some manufacturers give a separate curve to show this effect and a typical curve would appear as in Fig. 5.2. The parameter plotted is usually $h_{\mathrm{fc}}$ which is similar to $\beta$ and is actually a measure of the change in collector current for a small change in base current. The curve shows that $h_{\text {fe }}$ falls at low and high currents. Since the manufacturing spread for $\beta$, and hence $h_{\mathrm{re}}$, is already large this variation of $h_{\mathrm{fe}}$ with collector current is not important uuless a wide variation of $I_{\text {. }}$ occurs in the circuit used. This situation does occur with "large signal" circuits such as power amplifier output stages.

It is worth noting that some transistors are designed to give reasonably high $h_{\text {fe }}$ values down to collector currents of $1 \mu \mathrm{~A}$. Others have their


Fig. 5.2. Typical variation of $h_{\mathrm{fe}}$ with $/ \mathrm{c}$ best performance at high currents and for power transistors it may be necessary to ensure that reasonable values of $h_{4}$ are still obtained at currents of several amperes.

## SATURATION

A third and very important feature of the transistor is illustrated by considering point $P$ in Fig. 5.1. Notice that at low $V_{\text {ce, }}$ less than one volt typically, all the curves tend to merge into one line. This is the saturation region of the transistor, so called because at points such as $P$ the collector voltage is almost zero and the current in the colector reaches a saturation level above which it cannot rise.

If the transistor is made to operate at point $P$ any increase in base current above $200 \mu \mathrm{~A}$ will have virtually no effect. The collector current has saturated and the additional base current simply flows via the emitter/base junction. Obviously the relation $I_{\mathrm{c}}=\beta I_{\mathrm{b}}$ no longer holds since $I_{1}$, can have any value above $200 \mu$ A without $I_{c}$ changing. To realise the full implications of this situation consider the circuit shown in Fig. 5.3.

If $I_{\mathrm{c}}$ was zero one would have $V_{\mathrm{ce}}=9 \mathrm{~V}$ (switch Sl open). By closing the switch any base current up to about 1 mA can be provided by adjusting VR3. The resistor R1 limits the maximum base current to a safe value. As the base current is increased from zero the collector current, equal to $\beta I_{b}$, also increases and the voltage $V_{c e}$ falls due to the increasing voltage drop across the collector resistor R2. If we could make $V_{\text {re }}$ fall to zero the maximum current in R2 would be

$$
I_{e}(\max )=\frac{9(\text { volts })}{1(\mathrm{k} \Omega)}=9 \mathrm{~mA}
$$



Fig. 5.3. Circuit for testing saturation.

Any attempt to force $I_{c}$ higher than this must fail. If the transistor has $\beta=100$ the base current corresponding to this maximum collector current will be $9 / 100 \mathrm{~mA}=90 \mu \mathrm{~A}$. If the base current is made larger than this value the "excess" simply flows via the base/emitter junction but does not give rise to any additional collector current. The transistor is said to be saturated.

The collector voltage never falls to zero in practice and so the manufacturer quotes a typical saturation voltage called $V_{\text {ce }}(s a t)$. The corresponding base and collector currents are usually specified and for the BC107 transistor the specification sheet gives:
$V_{\text {ces }}($ sat $)$ at $I_{\mathrm{C}}=10 \mathrm{~mA}, I_{\mathrm{h}}=0.5 \mathrm{~mA}=250 \mathrm{mV}$ (max.) $V_{\text {ec }}$ (sat) at $I_{\mathrm{c}}=100 \mathrm{~mA}, I_{\mathrm{b}}=5 \mathrm{~mA}=600 \mathrm{mV}$ (max.). These are maximum values for any sample of the BC 107 transistor, typical values for the same current levels are 90 mV and 200 mV respectively. The variation of $V_{\text {se }}$ as VR3 is rotated clockwise is shown in Fig. 5.4. (The letters $J, H, G$, identify the connections to the 100 kilohm potentiometer (VR3) as shown in the Tutor Board article [Oct. 73 ] page 534).


Fig. 5.4. Variation of $V_{c e}$ with setting of VR3.
This lettering will be helpful as our circuits become more complex and is used in this month's tests. The potentiometers can be left permanently fixed to the tutor board with the 100 ohm control on the left hand side, the 5 kilohm control in the centre and the 100 kilohm control adjacent to the switch.

## THE COLLECTOR/BASE JUNCTION

The collector/base junction is similar to the emitter/base junction since it involves the transition from the base $p$ material to the $n$ material of the collector (for an $n p n$ device). In the circuits so far discussed this junction has been reverse biased since the collector ( $n$ region) has been made positive with respect to the base. The only exception to this condition is when the transistor is saturated. In this state the voltage $V_{\text {ce }}($ sat $)$ is less than the corresponding base/ emitter voltage which is known as $V_{\text {br }}($ sat $)$.

The situation is illustrated in Fig. 5.5 for both (a) saturated and (b) non saturated conditions. Note carefully that the collector base diode is forward biased under saturated conditions but reverse biased under normal conditions. The base/emitter diode is forward biased for both saturated and non saturated states.


Fig. 5.7. Simple current generator.
Fig. 5.5. (a) Saturated and (b) non satürated conditions.

## TRANSISTOR LEAKAGE CURRENTS

Early germanium transistors had leakage currents which were often significant and these had to be considered when designing circuits. Nowadays the modern silicon planar types have very low leakage and for most general applications the leakage can be neglected. Leakage currents increase with temperature however and silicon power devices can exhibit appreciable leakage if operating at junction temperatures of say 100 degrees Centigrade or more. The two most common leakage currents are $I_{\text {roo }}$ and $I_{1 \ldots 0}$ and are illustrated in Fig. 5.6.

Current $I_{\text {ree }}$ is always considerably greater than $I_{\text {rbe }}$ since the leakage current is forced to flow via the emitter/base junction and this gives rise to extra current by virtue of the basic transistor action. The relationship between $I_{\text {cbo }}$ and $I_{\mathrm{mo}}$ is shown in Fig. 5.6 but note that the $\beta$ value is for very low current operation and may be much smaller than the specification value.

## JUNCTION VOLTAGE RATINGS

The collector/base junction, like any diode, can only withstand a certain voltage in the reverse-bias condition. The value depends on the external circuit conditions at the base/emitter junction. For the BCl 107 , the absolute maximum voltage between collector and base, with the emitter left open circuit, is 50 volts. The corresponding limit for the emitter/base junction (also with reverse bias and with the collector


Fig. 5.6. Illustration of leakage currents.
open circuit) is only 6.0 volts. These ratings are known as $V_{\text {cloo }}$ (max) and $V_{\text {etoo }}(\max )$ respectively. (See table of parameters in last month's Teach-In '74, page 24).

## CONSTANT CURRENT GENERATION

The ideal voltage source is easy to understand since present-day batteries approach the ideal very closely. To be ideal the voltage at the battery terminals must be independent of the current taken. An alternative, which can be very useful, is a current generator which has the property of supplying a constant current, independent of the load voltage. A transistor can be used to make a practical current generator which will operate over a restricted voltage range and one possible circuit is shown in Fig. 5.7.

The resistor R1 allows current to flow via the Zener diode D1 which keeps the voltage across R2 constant since $V_{\text {be }}$ is almost constant for a given transistor emitter current. The current $I_{\text {e }}$ through R2 must be given by
$I_{\mathrm{e}}=\frac{V_{\mathrm{z}}-V_{\mathrm{bc}}}{R 2}$ where $V_{\mathrm{x}}$ is the breakdown voltage of the Zener diode used.

When a load is connected to the terminals $A, B$ the current flowing will be the collector current of the transistor which is almost exactly equal to $I_{c}$ (actually $x I_{\mathrm{e}}$ ) providing the voltage across $A, B$ is small enough to avoid saturation of the transistor. To illustrate the action of the circuit it is instructive to calculate the circuit currents and voltages using some of the techniques so far covered in this series. Let us assume that $\mathrm{RI}=1$ kilohm, $E=9$ volts, $\mathrm{R} 2=$ 10 kilohm and $V_{x}=4 \cdot 7$ volts. The calculations can then proceed as follows:-
(i) Voltage across $\mathrm{R} 1=(9-4 \cdot 7)=4 \cdot 3$ volts.
(ii) Current in $\mathrm{Rl}=4 \cdot 3 / 1000 \mathrm{~A}=4 \cdot 3 \mathrm{~mA}$.
(iii) Assume $V_{\text {be }}=0.6$ volts, then
(iv) Voltage across R2 $=(4 \cdot 7-0 \cdot 6)=4 \cdot 1$
(v) Current in R2 $=4 \cdot 1 / 10,000 \mathrm{~A}=410 \mu \mathrm{~A}$.

To prevent saturation occurring (which would give incorrect operation of the current generator) it is necessary to restrict the voltage be-


Fig. 5.8. Behaviour of constant current generator.
tween $A$ and $B$ so that the transistor collector base junction never becomes forward biased Taking $V_{\text {et }}=0$ as the limiting condition this
implies that the maximum voltage across $A, B$ must be limited to the voltage drop across R1 i.e. $4 \cdot 3$ volts. Since $I_{c}$ and $I_{r}$ are almost equal the maximum resistance of the load connected to $A, B$ must be approximately $4 \cdot 3 / I_{\mathrm{e}}(\mathrm{mA}) \times 1,000$ i.e. $10 \cdot 5$ kilohms. Consequently a fixed current of about $410 \mu \mathrm{~A}$ will flow through the load connected at $A, B$ for all load resistance values in the range 0 to 10.5 kilohm approximately. Higher resistance values cause the constant current action to fail and the load current then falls below $410 \mu \mathrm{~A}$, as shown in Fig. 5.8.

Next month we shall describe several useful circuit applications using the components covered in Teach-In ' 74 to date. These circuits will be treated experimentally and use most of the ideas so far presented.

## TUTOR BOARD EXPERIMENTS

## Test No. 15

This test is based on the circuit shown in Fig. 5.3. Plan a neat layout for the Tutor Board and then wire up the components to match the circuit. Note that the switch only controls the connection of the lower 4.5 V battery. Wire up the circuit for the $0-10 \mathrm{~V}$ voltmeter in the usual way and connect the voltmeter to the points indicated on the diagram as XX. Observing polarity! With this connection the voltmeter will register the voltage $V_{\text {cr }}$ for the transistor off.

Set the 100 kilohm control VR3 fully anticlockwise so that the slider H is at end J. Close the switch. Slowly increase the voltage fed to the transistor base by rotating VR3 clockwise whilst observing the meter. Verify that the voltage $V_{\text {cr }}$ varies as indicated in Fig. 5.4. Estimate the value $V_{c e}$ (sat) for the transistor used. (The value may be difficult to read accurately since the meter deflection will be very small.)

Switch off the base supply and change the 1 kilohm collector resistor to 10 kilohm. Repeat the test and notice that a smaller rotation of VR3 is now required to give saturation. Why is this so? It is helpful in this test to make pencil marks corresponding to the knob pointer positions at which conduction starts and saturation commences. These marks can be removed with a pencil rubber when the test is complete.

## Test No. 16

This test uses two BCl 107 transistors to produce a very sensitive current detector. The circuit is quite straightforward and is shown in Fig. 5.9. The circuit should be built on the Tutor Board and VR1 set to the mid-point of its rotation to give a resistance of approximately 50 ohms between points $B$ and $C$. Check the connections of both transistors carefully as an incorrectly wired circuit could cause damage.

The points $X, Y$ can be the test probes normally used for the voltmeter. If the probes
are not touching each other, the lamp should be off when the switch is closed. Pick up the probes, one in each hand and make a contact between the metal (nail) and the skin. The lamp should light due to the small current that flows via the "skin resistance" of the user. Experiment to see how many people you can connect "in series" between $X$ and $Y$ whilst still operating the light. With high $\beta$ transistors the lamp should light even if the resistance between $X$ and $Y$ is as high as 10 million ohms and for transistors with $\beta=500$, resistances of 100 million ohms can be detected.

The sensitivity of this circuit can be reduced if necessary by connecting the 100 kilohm potentiometer as a variable resistor, across the base/emitter connections of transistor TR2 (shown dotted). The lower the setting of this resistance, the lower the sensitivity will be. With zero resistance the lamp may not light at all, since only the collector current of TRI can now flow via the lamp. (TR2 must now be off since its base-emitter junction is shorted out by the zero resistance and no part of the emitter current of TR1 can flow into TR2 base.) This connection of two transistors, without the 100 kilohm potentiometer, behaves like a single transistor having a very high $\beta$ of 10,000 or


Fig. 5.9. Circuit for Test No. 16.

ANLONE who has tried to produce a continuous slide show for an exhibition or at home, has met the problem that most of the timing devices available on the market are not repetitive but merely time an interval from when the button is pressed after which they operate a set of contacts and they have to be reset before they will go through the cycle again. All of which means that they are not of any use for continuous slide show operation. Fortunately it is not difficult to build a repetitive timer at a reasonable cost.

The circuit described here is very simple, and is one of the many variations of the simple astable multivibrator; no relay driver was found to be needed making the finished design very economic on components.

The projector for which the prototype was designed to be used, was a Kodak Carousel which required to have a set of contacts made together for about a quarter of a second to cause the slide mechanism to operate. This contact is made by means of the relay contacts when the relay is activated in the circuit. The relay needs

# SIIDE PROJECTOR TIMER <br> BYC.G. GAMMANS 

to be a $6-9 \mathrm{~V}$ type with a coil resistance of at least 185 ohms and one set of normally open contacts.

## CIRCUIT

The complete circuit diagram of the Slide Projector Timer is shown in Fig. 1 and is seen to be a simple astable multivibrator, of variable frequency and mark/space ratio, loaded with relay RLA. Only the "space" part of the periodic time of the cycle is variable.


Fig. 1. The complete circuit diagram of the Slide Projector Timer.

The projector, to operate, uses the fixed timing interval ie. the "mark" and this is set at the required 0.25 seconds by the "mark" timing components R2 and C1.
The "space" part of the multivibrator cycle ie. time between relay contact "makes", is variable by adjusting VR1 which, together with C2 and R1 forms the timing components. Adjusting VR1 allows the time between "makes" of the relay contacts to be adjusted from one second to 20 seconds. Increasing VRI increases the time interval between "makes" and thus between slide changes.
When S1 is switched to the on position, TR1 turns on hard (saturates) with TR2 off (not conducting) and virtually the whole supply appears across the relay coil causing the relay contacts to close for 0.25 scconds. After this time. TR2 switches on and TR1 off-astable action-and the relay contacts oper and remain open for a time determined by VR1 setting. After this set time intervat the cycle is repeated until turned off at Sl
To hold a slide in position for longer than that available from the unit, Sl should be switched off for as long as required. Longer delays may be obtained by increasing the values of C 2 and/ or VRI
The unit will run for many hours powered by a PP3 battery.

## Components....

Resistors
R1 1.8kI
R2 3.9k:1
R3 $1 k$ :!
All $\div W$ carbon - $90 \%$

Potentiometer VR1 100 k ! carbōn lin. TAT

## Capacitors

C1 $64 \mu \mathrm{~F}$ elect. 9 V
C2 $1000, \mathrm{~F}$ elect. 9 V

## Serniconductors

TR1 2N2926G npn silicon
TR2 2N2926G npn silicon
D1 OA91. 1N4148 or similar

## Miscellaneous

RLA Any $6-9 \mathrm{~V}$ relay with coil resistance 185!? or greater and one set of normally open contacts
B1 9 V PP3
S1 d.p.s.t. toggle or slide
Veroboard, 18 holes $\times 26$ strips 0.1 in. matrix; battery clip; aluminium for case; two core cable for connecting unit to projector; knob.

## CONSTRUCTION

The prototype unit was built on a piece of $0 \cdot$ lin matrix Veroboard size 18 holes by 26 strips. The layout of the components on the topside of the board is shown in Fig. 2; there are no breaks in the copper strips on the underside.

Commence construction by drilling the fixing hole at location P11 and then mount and solder the link wires, resistors and capacitors as shown.

Next construct the aluminium case to the dimensions given in Fig 3, and assemble the components VR1, RLA, S1 and B1 as indicated. Now solder flying leads of sufficient length to the component board. The transistors should now be soldered in position and a heatshunt used to prevent thermal damage.

Secure the component board in position in the case with 4BA nut bolt and spacer and then wire up the flying leads to the other components as detailed in Fig. 3. Finally, solder the output lead from one set of normally open contacts and S1b, and pass out through the case via a rubber grommet. The length of this lead will depend on the desired distance of the unit from the projector. If desired, this lead can be made detachable by using a two pin plug and socket.

## TESTING

Check out the circuit for wrong/omitted connections. solder bridges between copper strips, transistor connections and diode and capacitor polarities. If satisfied, turn VR1 fully anti-clockwise and switch on with projector not connected. The relay should click over once every second or so. Turning VRl clockwise should increase the time between clicks; the fully clockwise position should produce one click every 20 seconds or so. If this does not happen, recheck for faults.
lf all is well. the lid may be screwed in place. A piece of foam plastic glued to the inside lid will hold BI in place.

## IN USE

Locate the slide change contacts in the remote operating box of the slide projector and connect the two wires from the timer unit in parallel with the slide change contacts.

Switch on the slide projector and set it up as you would normally then switch on the Slide Projector Timer. Set the slide changing speed, then switch off the slide timer and reset the slide cassette to the first slide required. Switch on the Slide Projector Timer when you wish the show to begin. If during a display you want to hold the show at the slide on the screen, then it is necessary to switch off the timer.
If the magazine of the projector is one of the round types, then with the timer running, the show will go on until you switch off.


# SEMICONDUCTOR PRIMER 

By A.P. STEPHENSON

## 3 <br> - PN JUNCTION ACTION

" $p$ " material contains positive holes which can move around freely within the crystal. These can be considered as "little white balls" which possess a positive charge.
" $n$ " material contains electrons, which can be treated as "little black balls". If these two materials are joined (in a special way) a $p m$ junction is formed, Fig. 3.1.

Assume a battery is connected as in Fig. 3.2. No current flows because the holes and electrons are simply pulled away from the junction. leaving an area in between which is an insulator (because there are no charges left).

Now consider Fig. 3.3. This time, the holes and electrons are pulled across the junction, and a steady curient flows round the circuit. The directional arrows are in opposite directions but the effect is additive since holes are $+v e$ and electrons-ve.


Fig. 3.1. Schematic of a $p n$ junction.

Fig. 3.2. A reversed biased pn junction.

## 4 : CONSTRUCTION OF A TRANSISTOR

A transistor comprises two pn junctions forming a "sandwich". There are two ways of forming such a sandwich: (a) pnp (b) npn. These are illustrated in Fig. 4.1

The three wires connected are named as follows:

The base is the middle fayer connection.
The emitter is one of the ends.
The collector is the other end.
The symbols for the two kinds of transistor are given in Fig. 4.2.

The emitter arrow points in direction of conventional current, i.e. positive to negative. Emitter arrow is INWARDS for pnp. Emitter arrow is OUTWARDS for $n p n$.


Fig. 4.1. Schematic sandwich construction of transistors.


Fig. 4.2. Circuit symbols for $p n p$ and $n p n$ transistor types.

## 5 : THE "TWO DIODES" CONCEPT

A transistor is basically two pn-junction diodes back to back, Fig. 5.1.

Assume the middle connection (the base) is left "up in the air", no current can flow due to the opposing effect of the two diodes, Fig. 5.2.

Suppose the base is now returned, via a resistor, to the collector rail. The bottom diode is now forward biased and the top diode is still reverse biased, which is the correct way to operate all transistors.

Note that in both cases the boltom diode is forward biased and is therefore dropping about 0.6 volts (assuming a silicon transistor).


Fig. 5.1 The back to back diode representation of a transistor.
Fig. 5.2 (left). No current flows under these conditions.


THE replacement of the therinionic valve by the transistor and the fien effect transistor enabled the size of electroaic equipment to be reduced by a very large factor. The development of integiated circuits during the 1960's has carabled a further large reduction in the size of squipment ta-be effected.
An integrated circuit tan contain large numbers of diodes, transistors, field effect transistors, resistors and capacitors formed by a photographic technique on a single minute silican chip. Iategrated tircuits are often called monolithic circuits because they are formed on a single piece of silicon.

## SOME APPLICATIONS

The replacement of numerous discrete components by a small integrated circuit confers a number of advantages. The reduction in size is important and useful in most applications, but in some fietris it is essential.

For example it is easy to incorporate a thousand transistors and other components on a very small silicon chip; the resulting intecezated circuit can be used in a wrist watch employing a quartz crystal electronic oscillator to provide an accuracy of about one minute per fear or less ( 12 seconds oer year in the case of the Omega "Megaquartz"). A circuit with a thousand separate (or "discrete") components could not possibly be incorporated into a miniature wrist watch.

## SPACE RESEARCH

Another field where integrated circuits have proved to be of vital importance is that of space research. The reduction in weight and volume achieved by the use of these components instead of separate transistors has made the modern

# Introduction 

 to INTEGRATED CIRCUITS (1) By J.B.DANCE m.sc. sophisticated signalling and control systems possible. Satellites can now be equipped with miniature computers containing numerous integrated circuits.The modern computer employs very large numbers of integrated circuits so that an enormous number of components can be connected together in a relatively small space. This has enabled much more powerful computing systems to be made than would have been practicable with discrete components.

## ADVANTAGES

The advantages achieved by the use of integrated circuits are not limited to the saving in space thereby obtained. In the manufacture of an integrated circuit all of the internal connections are automatically made by the photographic techniques used in production. In these days of extremely high labour costs, this enables a great saving to be made on the manufacturing costs.


An example of the use of integrated circuits for a computer core memory.

The price of many of the cheaper integrated circuits is about the same as that of about three cheap transistors. Many types of integrated circuits are available for less than 11 , even though they contain some hundreds or thousands of separate components. The cost of designing and setting up the equipment used to manufacture integrated circuits is very high, but once the equipment has been set up, the cost of producing each additional component is very low.
The price of any one type of integrated circuit is therefore dependent more on the expected demand for that component rather than on the complexity of the device concerned. Indeed, most integrated circuits employ more components than a similar circuit using discrete devices, partly because additional components can be added with only a very small rise in the manufacturing cost.

## DISADVANTAGES

There are two main disadvantages in the use of integrated circuits instead of discrete devices, but these disadvantages tend to apply only in certain specific applications.

In general, circuits which must operate at extremely high frequencies employ discrete components, since it is difficult to manufacture integrated circuits which can operate at some thousands of megahertz.

The other disadvantage is that when one has mass produced, cheap integrated circuits available, one cannot alter the internal design of the integrated circuit to suit one's particular application. In other words, one loses some of the versatility of circuit design when one replaces discrete components with integrated circuits. Nevertheless, this very loss of versatility implies that the circuit designer is relieved of much of the detailed design work of individual stages.

In general, each type of integrated circuit is normally produced for a fairly definite type of
application for which it can be sold in large numbers. It is uneconomical to produce integrated circuits which will not be sold in very large numbers. Some types are designed for audio amplification applications, others for use in television receivers and others for the counting of electrical pulses, but some comprise a high gain amplifier which can be used in a fairly wide variety of applications.

## EARLY HISTORY

Various attempts were made to miniaturise - circuits during the last war, but the first type of device which one might really call an integrated circuit was developed in 1958 by Texas Instruments Ltd. This consisted of a number of resistors and transistors which were produced by diffusing impurity elements into a single chip of silicon.

Many types of integrated circuits were developed in the early 1960 's. The well known silicon planar process developed by the Fairchild Company in 1960 provided a great boost to the industry, since it is the process by which almost all modern integrated circuits are produced.
The first types of integrated circuits were used mainly in the military and computer fields, but their use has spread and one can now find them in the radio and television fields where costs are most competitive. It is generally cheaper to employ a mass produced miniature integrated circuit than to pay labour charges for people to wire up and test discrete circuits.

## APPEARANCE

A transistor normally has three connections, and seldom more than four. Most integrated circuits need more connections than this owing to their complexity. However, the first integrated circuits were produced by various transistor manufacturers and they naturally fitted their products into the type of cases they had been using for transistors.

An integrated circuit before encapsulation.


One type of integrated circuit employs the normal TO-5 type of transistor encapsulation, but there are typically six or eight leads coming out of the base instead of the three or four of the normal transistor. The leads are arranged in a circle. Such integrated circuits can dissipate only about one watt of power. Some high power integrated circuits employ the diamond shaped TO-3 type of encapsulation (as used for many high power transistors), but there may be a number of connecting wires arranged in a circle coming from the base of the device.

One of the most common types of encapsulation used for integrated circuits at the present time is the dual-in-line package (see Fig. 1). This usually consists of a rectangular plastic or ceramic package with two separate rows of connection pins, one row being fitted on each side of the package. Some types of dual-in-line integrated circuits have eight pins (two lines of four pins each), but the most common


A small part of the production area for 7400,12 Ces at ITT Semiconductors.
types of integrated circuit have 14 pins (two lines of 7 pins each). Types with 16 pins are common (for example, certain types of counters), whilst some types of dual-in-line integrated circuits have still more connections.

Some types of integrated circuit are available both in the TO-5 type of encapsulation and as dual-in-line devices. The latter are usually very slightly cheaper than the same devices in a TO-5 type of encapsulation.

## SOCKETS

A transistor is normally soldered directly into the circuit in which it is to be used. Integrated circuits can also be soldered directly if a suitable circuit board is employed, but it is not easy to unsolder and change devices having a large number of connections. It is therefore common practice to use integrated circuits in suitable
sockets. This also avoids possible damage to the integrated circuit by the voltage spikes occurring on an unearthed soldering iron or by overheating during soldering by an inexperienced person.

Sockets are available for integrated circuits having the TO-5 type of encapsulation and also for those employing the dual-in-line encapsulation. In the latter case, sockets are available with 8,14 and 16 connections and possibly for other numbers also. An integrated circuit with 8 connections, can, incidentally, be fitted into a dual-in-line socket which has 8,14 or 16 connections.

Great care should be taken when one is inserting and removing dual-in-line integrated circuits into or from their sockets, since the pins can be badly bent (even if reasonable care is taken) when the integrated circuit fits tightly into a new socket. If one attempts to remove an integrated circuit of the dual-in-line type from


Fig. 1. Dual-in-line packages, these examples have 16 pins.
its socket and it does not come out easily, a thin, small screwdriver slipped under the device will greatly assist in removing it without any damage. If, however, the pins of the device are bent, they should be carefully straightened or "dressed" with pliers and/or forceps.

## TYPES

Integrated circuits are employed for so many purposes that it is possible only to give some general indications of some of the more common types of application in this article. Audio amplifiers will be considered in most detail, since they are the type of integrated circuit which is most likely to be of interest to the amateur enthusiast.

The first types of integrated circuit to be developed were digital types which operate by the switching of transistors in them. These tran-
sistors are either fully conducting or switched off at any one time; any states of partial conduction do not occur for more than a very short time.

Digital integrated circuits became commercially available in large numbers around 1964. They are widely used in computers and for complex logic applications. They can be used in counting circuits. Metal oxide semiconductor techniques (M.O.S.T.s) are much used in digital applications with integrated circuits, since very economical devices can be produced. However, they are not yet widely used in other types of circuit.

Digital integrated circuits can be employed in industrial logic control. As an extremely simple example, one may employ a digital logic circuit to ensure that a machine will operate only if the cooling water is flowing or if an airblower is switched on and if there are enough metal parts at the input and if a bath is within certain temperature limits.

The amateur enthusiast may meet digital integrated circuits in calculators, but such projects are fairly complex. In general, the average amateur will be more interested in other types of integrated circuit, so the digital types will not be discussed further here.

## LINEAR INTEGRATED CIRCUITS

In linear circuits the currents and voltages can have any values between certain limits, the output being in some way related to the applied input. Suitable linear integrated circuits offer the designer ready made high gain amplifiers, etc.

They were initially rather expensive and designers were not familiar with them; they have therefore been used in large numbers only during the past five years or so. The price of linear integrated circuits has fallen rapidly and they may become cheaper still as time passes and more of them are used.

## OPERATIONAL AMPLIFIERS

Operational amplifiers were originally high gain amplifiers using discrete components. They were mainly used to carry out mathematical operations (such as subtraction, integration, etc.) in analogue computers-hence their name. They are coupled so that they can handle steady signals (even signals of zero frequency) as well as alternating inputs.

Operational amplifiers are now produced as integrated circuits. They have a multitude of applications and the properties of the circuits in which they are used can be greatly altered by using various resistors and capacitors in the input and feedback circuits of the amplifiers.

General purpose operational amplifiers form a natural field for the use of integrated circuits.


Pre-testing of integrated circuits at Mullard's. Silicon slices are being electrically checked.

Some thousands of types of operational amplifier are now available.

## THE "709"

The first type of general purpose operational amplifier to be produced in quantity was the Fairchild $\mu$ A709. This type is now available from many manufacturers. For example, Texas Instruments market it under the type number SN72709, Motorola under the number MC1709, National Semiconductor under the number LM709, Newmarket Transistors as LIC709 and Mullard-Philips as the TAA521, etc. Some manufacturers offer two type 709 amplifiers in a single 14 pin dual-in-line package; one example is the Motorola MC1437 and MC1537 dual amplifiers.

A transistor of a certain type number from one manufacturer will satisfactorily replace a transistor of the same number produced by another manufacturer. However, in the case of integrated circuits, one cannot necessarily replace one device by an equivalent device of another manufacturer. This is due to the complexity of the circuits and the impossibility of specifying all of the parameters of a device in a data sheet. However, expert circuit designers take such factors into account.
Next month we shall be looking at some particular linear integrated circuits.


We are beginning to receive a number of letters from readers complaining about long delays in the supply of components from retailers. Unfortunately these delays are often unavoidable and are due to the manufacturers not being able to supply the retailers. Quite often the retailer can find no alternative supply and cannot obtain a definite commitment on when he will receive the goods.

A recent instance of this problem was experienced in this office. We were trying to obtain some low value, high wattage resistors for a future project and one supplier quoted 63 to 64 weeks delivery-some time in 1975!

## Emergency Lighting Unit

The basically very simple Emergency Lighting Unil could be very useful indeed both for supplying light and of course for charging car batteries which are bound to be stretched to the limit supplying power during emergencies. If the petrol shortage gets worse it may be worth using the car baltery for lighting most of the time-however we will be looking at petrol economy, so watch out for some petrol saving devices.

Getting back to the components needed for the lighting unit, provided a battery is available, most of the components are straightforward with some alternatives being given in the text. The relay may take a bit of looking for, but almost any 12 V or less type will work provided the contacts are rated at $5 \mathrm{amps}-$ the coil resistance does not matter 100 much and there are a number of different types with coils of about 200 ohms that should suit.

Unfortunately the case we show is not. available but most suppliers sell a range of cases and any one that is big enough will do.

## Power Supply Unit

The first of the EE Test Gear Five; the Power Supply Unit will be of immediate interest to the more serious constructor and, as with all the instruments in this serics is a very useful and "professional" piece of equipment. Most of the parts will be readily
available, the transformer and the 10 ohm potentiometer should be available from the larger suppliers. Miniature switches were used on the prototype but these are expensive and normal toggle types are suitable.

The cases used for the Test Gear Five are made by Olsen Electronics Lid., and are available from them for $£ 3.45$ including postage, packing and V.A.T.

The case used is a type 25A with louvres; this case is very well made and very strong, it also gives a good appearance to the finished unit. Cases are available in light green, dark green, blue and silver grey and front panels in light green, cream or white. Our prototypes used dark green cases and cream front panels and look very smart (see front cover). Olsen are at 5 Long Street, London E.2.

The knobs used on the front panel are available from Re-an Products, Burnham Road, Dartford, Kent.

## Slide Projector Timer

Relays and cases are items that are often discussed in this article and this once again applies with the Slide Projector Timer. In fact the relay can be almost any type that will work on 9 volts and most suppliers should be able to find something to suit. Virtually the same words can be used when referring to the case, there are a number of types available and any that is big enough will do.

A handy tool 1 have made to extract integrated circuits. and other components from circuit boards without damage. It is made from 3 mm brass rod which will spring back when released, the rod is bent into an inverted " $V$ " shape and about 10 mm is bent inwards at each end and then filed down to a taper keeping the bottom as horizontal as possible.
The tapered ends are inserted under each end of the integrated circuit and a slight pressure is applied to the sides of the brass rod, heat is then applied to the pins on the underside of the circuit board and as the solder melts the integrated circuit will lift out because of the tapered prongs.
R. Linklater,

Aldershot, Hants.
Instead of using enamel paint as a p.c. board resist I used nail varnish which has several advantages.
(1) It takes less time to dry.
(2) It is difficult to remove the paint while wet if a mistake is made, but with nail varnish it dries quickly and can be removed with the special remover.

[^3]
# POUER SUPPLY UNIT 

## Stabilised variable voltage from O-20V with current limit control up to 0.5A.

APOWER supply is a key component in any electronic circuit. Although one may use batteries in a finished project, they are not flexible enough to provide variable voltages needed while designing and testing a new circuit. Additionally, this unit supplies power for other instruments in the E.E. Test Gear Five series.

This unit has been designed to satisfy the essential requirements of a home constructor's workshop at a reasonable cost. It provides a stable, well regulated, low ripple output, and incorporates a variable current limit. The voltage may be continually varied from zero to 20 V , and the current limit set within the range 50 mA to 0.5 A . The output current or voltage is indicated on a meter. Limiting the supply current at 0.5 A protects the unit from damage arising from a short circuit.

## DESIGN PRINCIPLES

The block diagram, Fig. 1, outlines the bāsic principles of the circuit.

The power scurce provides a rectified, smoothed, d.c. voltage to the other circuit blocks. The Zener diodes provide a 30 V source for the

differential amplifier, and a 25 V source for the voltage selector. The 25 V source covers the range from $-3 \cdot 3 \mathrm{~V}$ to +22 V to ensure that the output voltage will swing from zero to 20 V .

The differential amplifier compares the voltage from the voltage selector with the voltage at the output of the supply. The signal which appears at the output of the differential amplifier is proportional to the difference between the two inputs and this signal controls the regulation circuit which in turn controls the output voltage.

This feedback loop will force the output voltage of the supply towards the voltage set at the voltage selector. This circuit arrangement produces a supply having good regulation and low ripple, while allowing the output voltage to be set at any desired level between zero and 20 V .

Fig. 1. Block diagram of the Power Supply Unit.



Fig. 2. The complete circuit diagram of the Power Supply Unit.

## CIRCUITRY

The circuit diagram for the Power Supply Unit is shown in Fig. 2. The power source comprises a $25-0-25 \mathrm{~V}$ transformer, a diode bridge (D1-D4), and capacitors Cl and C 2 , an arrangement which gives two voltage sources, 38 V being produced across each capacitor.

The Zener diodes give 30V across D5 and D6 to supply the differential amplifier, and a more accurate supply of 25 V across D7 and D8 for the voltage selector. Resistors R1-to R4 limit the current through the Zener diodes.

The potentiometer VR1 acts as a voltage selector, while the differential amplifier ICl consists of a 741 and ancillary components. Components R5 and C3 form a filter to reduce noise. Resistor R6 increases the output impedance of the 741, which is normally 75 ohms and R7 is a current limiting resistor, through which the output voltage is sampled.
The regulator circuit consists of TR1, R8, R9 and TR3 connected as a darlington pair. This may be considered as one transistor with very high gain. Because of this the darlington transistor has a low base current with high collector current, so the arrangement reduces the drain on the 741 .

When the sample voltage drops below the reference voltage, the output on the 741 rises, and this increases the base current of the darlington pair. The collector/emitter voltage of

TR3 falls and the output voltage increases until the sample voltage is the same as the reference voltage. If the output voltage is greater than the reference voltage, the effect is reversed.
The output voltage will always take up the potential of the reference voltage.
Components TR2, RIO and VR2 form the current control and current limit. With VR2 set to zero ohms, and with 0.5 A flowing through R7, the voltage drop across R7 amounts to 0.5 V . This is sufficient to turn on transistor TR2 and bring the base of TRI to the output potential. This cuts off TR1, and hence TR3, so the output current is limited to 0.5 A .

By increasing the resistance between base and emitter of TR2, with VR2, the current limit may be reduced to below 50 mA .
The meter circuit has been designed for a meter having ImA full scale deflection and an internal resistance of 105 ohms. Voltage is measured directly across the output via the 20 kilohm resistor, R12, so that full scale deflection represents 20 V .

Current is measured by reading the voltage across RIl, so that 0.5 A current gives half scale deflection on the meter.

## CHOOSING COMPONENTS

In the prototype it was decided to use an inexpensive 50 V , centre tapped, half-ampere
transformer, and this allowed the prototype Power Supply Unit to reach its specified voltage and current output with normal mains supply.

If the mains supply falls appreciably below 240 V , the poor regulation of an inexpensive transformer may affect the output. If it is intended to make regular use of the unit near to its limits, a better quality transformer should be considered.

A half-amp diode bridge package with reverse voltage of 100 V is used to provide rectification. Four diodes in a bridge arrangement could be used as an alternative, provided that they are each rated at half-amp, and have a reverse voltage of at least 40 V .

Transistor TR2 is a BCl 82 , but any small, silicon $n p n$ transistor having a maximum $V_{c e}$ greater than 50 V may be used in this position.

All resistors used are ${ }^{1_{4}}$ watt types or greater. The capacitors are all electrolytic and it is important to ensure that you use capacitors with working voltages equal to or greater than the values given.

## METER

The meter must give full scale deffection for 10 mA or less. If this current is called $I_{\text {tsd }}$ and the resistance of the meter is called $R_{\mathrm{m}}$, then the product, $I_{\mathrm{fs}} \times R_{\mathrm{m}}$ must be less than one volt.

To choose resistors R11 and R12 the formula $R_{s}=\frac{V_{\mathrm{fsd}}}{I_{\mathrm{tad}}}-R_{\mathrm{tn}}$ was used where $R_{\mathrm{s}}$ is the series resistance, see Fig. 3.

Output voltage is measured via R12 and $V_{\text {rssi }}$ is 20 V . Output current is measured across R10 and via R11, and $V_{\text {tsd }}$ is one volt.
So, $\mathrm{R} 11=\frac{1}{I_{1 \mathrm{sd}}}-R_{\mathrm{m}}$ and $\mathrm{R} 12=\frac{I_{\mathrm{fd}}}{20}-R_{\mathrm{n}}$
The closest resistance in the list of preferred values should be chosen.


Fig. 3. Current flow in the meter circuit.

## CONSTRUCTION

The prototype Power Supply Unit was housed in a commercially available steel cabinet with remor eable front and rear panels but any robust case available will do as long as it is metallic,

Components are mounted on the case parts
itself and on a piece of $0 \cdot 1$ in plain matrix board. Veropins are used to anchor some components on the topside of the board and insulated wire to make the interconnections on the underside of the board.
The top and underside of the component board are shown in Fig. 4. Begin by drilling the four fixing holes near to each corner and then insert the Veropins as indicated.

Next insert the integrated circuit holder and then position and solder the bridge rectifier, resistors and capacitors, paying special attention to polarities, and then wire up the underside as shown keeping the connecting wires as short as possible. The transistors and diodes should be soldered in position next and a heatshunt, such as a pair of pliers, should be used when doing so otherwise heat from the soldering iron may damage these components.

The back panel should be prepared next and the power transistor TR3 mounted in place. Insulating bushes and mica washer must be used. Now mount the component board to the back panel with four 4BA nuts, bolts and standoff spacers and then wire the board to TR3. The back panel acts as a heatsink for TR3.

The next step is to cut and drill the front panel to take the components ME1, VR1, VR2, S1, S2, LP1 and the three terminal connectors SK1, SK2 and SK3 as shown in Fig. 4, and then secure these components in position.

The smoothing capacitor Cl should now be fixed to Tl by means of the capacitor clip as shown in Fig. 6. This assembly should now be placed in position inside the case and suitable holes marked and drilled in the case base through which the transformer can be secured with 4BA nuts and bolts.

Place the front and rear panels on the work bench with Tl between them and wire up according to Figs. 4 and 5. The three core mains cable should be fed in through the panel via a rubber grommet; the other end should terminate in a fused mains plug.

Thoroughly check out your wiring before finally assembling in the metal case.


Photograph of completed component board.

## POWER SUPPLY UNIT



Fig. 5. Component positioning and wiring up on the front panel.



Fig. 6. Wiring up details on primary and secondary windings of T1.

## CHECKING OUT

Set VR1 fully anti-clockwise and VR2 fully clockwise, S2 to the voltage mode and then plug into the mains and switch on at Sl. The neon indicator lamp should light. Now turn VRl in a clockwise direction and the meter needle should move across the scale, reading 20 volts with VR1 in the fully clockwise position. Turn VRI back to read zero volts and switch off.

Connect a 12 volt bulb, six watts or less-i.e. the bulb takes 0.5 A or less-across the output
terminals SK2 and SK3. Now turn VR1 clockwise until a reading of 12 volts shows; the intensity of the bulb increases from zero.

Leave VR1 set at this level and switch S2 to the current monitoring mode, and take the reading from the lower scale, it should be $0-5 \mathrm{~A}$. Turn VR2 in an anticlockwise direction and the intensity of the bulb should decrease showing that the current through the bulb is being limited to the value shown on the meter.

With VR2 set to limit at about $250 \mathrm{~mA}(0.25 \mathrm{~A})$. switch $\$ 2$ back to the voltage mode, the meter

## Components . . . .

| Resistors |  |  |
| :--- | :--- | :--- |
| R1 | $680 \Omega$ |  |
| R2 | $2.4 \mathrm{ks} \Omega$ |  |
| R3 | $390 \Omega$ |  |
| R4 | $390 \Omega$ |  |
| R5 | $22 \mathrm{k} \Omega$ |  |
| R6 | $5 \cdot 1 \mathrm{ks} \Omega$ |  |
| R7 | $10 \mathrm{k} \Omega$ |  |
| R8 | $27 \Omega$ |  |
| R9 | $240 \Omega$ |  |
| R10 $1 \Omega$ |  |  |
| R11 $910 \Omega \Omega$ |  |  |
| R12 $20 \mathrm{k} \Omega$ |  |  |
| All $\frac{1}{4} \mathrm{~W}$ carbon $\pm 5 \%$ |  |  |

## Potentiometers <br> VR1 $50 \mathrm{k} \Omega$ linear carbon <br> VR2 $10 \Omega$ linear

## Capacitors

| C 1 | $1000 \mu \mathrm{~F}$ | 40 V | elect. |
| :--- | :--- | :--- | :--- |
| C 2 | $100 \mu \mathrm{~F}$ | 40 V | elect. |
| C 3 | $10 \mu \mathrm{~F}$ | 25 V | elect. |
| C 4 | $100 \mu \mathrm{~F}$ | 25 V | elect. |

## Semiconductors

| TR1 | 2N3053 silicon npn |
| :--- | :--- |
| TR2 | BC182 silicon npn or similar |
| TR3 | 2N3055 silicon npn |

D1-D4 $\frac{1}{2}$ A 100 P.I.V. bridge rectifier or equivalent
D5 BZY88/24 400 mW Zener
D6 BZY88/5V6 400 mW Zener
D7 BZY88.22 400 mW Zener
D8 BZY88/3V3 400 mW Zener
IC1 741 differential operational amplifier, 8 -pin d.i.l

## Miscellaneous

## T1 240 V primary 25-0-25 0.5A second-

 aryME1 1 mA d.c. meter type S.E.W MR38P or similar
LP1 panel mounting mains neon with built-in resistor
S1 mains on/off slide or toggle
S2 d.p.d.t. toggle or slide
SK1, 2, 3 insulated screw terminals, black green red ( 1 off each colour) Plain matrix board $0.1 \mathrm{in} .28 \times 28$ holes; Veropins; capacitor clip to suit C1; mica washer and insulating bushes for TR3; 4BA nuts bolts and washers and four 4BA standoff spacers; length of three-cored mains cable. Case, metal approx. $165 \times 115 \times 115 \mathrm{~mm}$.


Photograph of completed unit and front panel, removed.
reading, now from the top scale should still be at 12 volts.

If a lower wattage bulb is used, say three watts, ie. current consumption of 0.25 A , then in the above test, turning down the current limit control, VR2, would have no effect on the intensity of the bulb until the current is limited to less than $0 \cdot 25 \mathrm{~A}$.

## USING

When using the Power Supply Unit to power a device, the maximum current likely to be required by the device should be estimated and the current limit control set to this value. In this way damage to the device is kept to a minimum should there be a fault. Even if there is a short circuit in the device being powered, the maximum current that can flow into it will have been limited by VR2.

There is a third terminal, SKI connected to earth, so it is possible to earth either side of the power supply output as required.
It is recommended that when in use all connections to the output sockets be made and checked before switching on the unit.


MANY who take up electronics as a hobby, become "hooked on it" if you will forgive the argot. However, when you consider that there are so many less useful or interesfing things that could claim your money and attention, this must count in it's favour. If you do reach that stage, you will probably find you are placing regular weekly or monthly orders with your suppliers. In which case, I would suggest that you approach them, with the idea of opening an account. I don't think the mail order firms, would raise any objections.

Of course it would be wisest not to broach the subject, until you have been one of their "cash customers" for a few months. This will give them confidence, and they will also be able to assess your value to them as a client. They may want references, this is usual procedure, but I am sure you will know plenty of people who will vouch for you.

It helps considerably, if your referees have a status, such as, bank manager. doctor, vicar, or school teacher. You may have the
payment card of a completed hire purchase transaction, this is often acceptable evidence of your credit worthiness.

## Advantages

Consider the advantages of a monthly account. You can order at will, either by post or telephone, and just one cheque or postal order at the end of each month will settle your debt, (this in itself can show quite a saving in the cost of cheques and postal orders). In our company (due perhaps to my enthusiasm) we went overboard for this scheme.

I had an Answerphone installed on a special ex-directory line, (thus enabling our customers to place orders at any time during the 24 hours). Apart from the convenience, it meant that they could use the telephone at the reduced rates. I also provided them with order forms and prepaid envelopes.

## 'C' for Charlie

For the benefit of the telephone users, I sent them a letter, telling
them what to do and what to avoid. I even sent them a copy of the international air alphabet. I think you know the type of thing. I believe it started in World War 1, with "C for Charlie," "D for Don", "B for beer" etc. Now it is much more sophisticated, and to give you a small sample, " $G$ " "H" "L" "K", would become "golf" "hotel" "Lima" "kilo."

## Miss-understanding

When I first introduced it, it led to an amusing incident. The excellent young lady, who runs the whole scheme in her spare time takes the orders off the telephone machine each morning.

This particular morning, she came to me in great consternation, "Ere this bloke must be orf his chump, 'E wants to order a hotel an' a golf course!" I quickly told the poppett that we were not going into the real estate business, and explained to her, how it came about. Since then all has been plain sailing.

Finally, if any of my fellow sufferers (I mean of course component retailers) would like any advice on running these accounts, just contact mc, and, as they say in the Times personal column, they will learn something to their advantage, to say nothing of their customers.

Iuside... next month's I5SUE


# Ruminations <br> By Sensor 

## Watts to do!

In the midst of the energy crisis there seems little to be cheerful about; the prospect of cold homes, long bus queues in snow filled streets and a bowl of cold gruel for supper, scarcely gladdens the heart.
But the electronics man can feel smug if not snug in the knowledge that the transistor circuits can run on a small battery for many hours. When the power is "on" the whole family can gather round the hot soldering iron while construction of the latest project continues and thus avoid any waste of heat.
I remember warming my hands on the valves of a radar set, during a power crisis many years
ago, and a keen fisherman I knew put this waste heat to good use in rather unusual circumstances. One of the women in the factory had bought some bacon during a lunchtime shopping trip and had discovered that it contained some maggots. She was quite justifiably complaining to her workmates about this unhappy state of affairs when the fisherman overheard her remarks. He paid her for the bacon and put it into a piece of equipment for the afternoon where it was kept at an ideal temperature for the maximum production of fat maggots! I felt that this incident represented a variation on the "one man's meat is another man's poison" theme.

## Waste Not

The early computers used a considerable amount of power but most of it was dissipated in heat. It was usual to fit refrigeration equipment to all but the smallest computer in order to
keep the temperature down to within the operating limits of the components and to avoid the operators having to work stripped to the waist.
Even at a more humble level the domestic radio and television produced an appreciable amount of heat; my father used to raise boxes of tomato seedlings on top of the television very successfully but if you try it be very carefnl when watering them (see next month's propagator article-ed.).
I have often felt that man is guilty of a prodigous waste of heat which is pushed out into the atmosphere, poured into rivers and into the sea with no real attempt to extract the energy which has been put into it at such cost. It has been cheaper to throw away heat than to try to conserve it but the trend towards dearer fuel must change all that. Unfortunately we cannot get back all that has been lost over the years; the best that we can do is to put our house in order now, before it is too late.


## Electrolytic Capacitors

Are there any rules that limit the use of electrolytic capacitors in a circuit?

Provided one side of the capacitor is always positive with respect to the other then you can use an electrolytic. Even if you have an alternating voltage on one side provided it is set off by a d.c. level so that the peak a.c. levels do not reverse the
applied polarity then you can still use an electrolytic but you miust make sure that the a.c. component of the signal does not cause the capacitor's "ripple current rating" to be exceeded. With small signal coupling capacitors (between stages) this is not likely to be a problem but it could be in the case of power supply smoothing.
You must however remember that most electrolytics are "leaky" and this would preclude their use in some circuits.

## Capacitor Voltage

Why do capacitors have a voltage rating? Is it very important and can you use devices having different ratings from those specified?
Any capacitor - when boiled down to its fundamental principle of operation is made up of a number of electrodes separated from each other by a very thin insulator-known as a dielectric. This can be plastic (polyester or polystyrene) ceramic, paper, air or a chemical electrolytic. Any insulating substance can prevent d.c. current flow but only when the voltage across it is limited to below its breakdown voltage; this is dependant on its nature and its thickness. Breakdown occurs
by a spark jumping across between the electrodes and through the dielectric. Not only can this permanently damage the capacitor but it can ruin the operation of the circuit.

The voltage rating for a capacitor is the maximum voltage (whether d.c. or peak a.c.) that you can apply across the device before this breakdown occurs. Sometimes there are differences in level between the peak a.c. value and d.c. value for a given capacitor. Obviously is is a very important parameter. You can, however, always use a capacitor having a higher voltage rating than is specified in a components list.

##  <br> MARCH ISSUE

Lighting cuts neean't be such a problem with the car battery powered FLUORESCENT LAMP INVERTER

Improve the performance of your car with the SCORPIO MK. 2 IGNITION SYSTEM-for 6 V and 12 V systems

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| AE2 | Pre-amplifier | 1.26 |
| AE3 | Diode-reciver | 2.00 |
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\section*{3/ CARRY OUT OVER}

40 EXPERIMENTS ON BASIC ELECTRONIC CIRCUITS \& SEE HOW THEY WORK, including:
valve experiments. transistor experiments amplifiers. oscillators, signal tracer. photo electric circuit. computer circuit. basic radio receiver, electronic switch, simple transmitter, a.c. experiments. d.c. experiments, simple counter. time delay circuit, servicing procedures.

This new style course will enable anyone to really understand electronics by a modern, practical and visual method-no maths, and a minimum of theory-no previous knowledge required. It will also enable anyone to understand how to test, service and maintain all types of electronic equipment, radio and TV receivers, etc

\title{
DEMO CRRCUITS (12) By MIKR Huches \\ The AND Gate
}

This month's circuit is shown in Fig. 12.1 and you would be excused if you felt, at first glance, that it was so simple it hardly warranted a special article to describe its function.
However, it is a most important circuit and crops up over and over again-usually hidden away within a more involved system. Because of its simplicity and the fact that it is seldom described in detail when embodied within a more complicated circuit we felt that we had better do the honours to the diode AND gate.
To understand its function, imagine you are in a car on a gated mountain road; it is impossible for you to progress along the road unless someone opens the gate-your progress is under the control of a third party!
Conversely, the third party could deliberately impede your passage by refusing to open the gate. This is a direct comparison with this month's circuit which has the same effect on electrical signals as the mountain gate had on the car. This is how the circuit gets its name.

\section*{EXPERIMENT}

To see this effect wire up the circuit of Fig. 12.1 and connect point \(B\), with a temporary lead, to the +4.5 V rail. Connect a meter, set to volts, between point \(C\) and ground and then alternately connect point \(A\) to +4.5 V and then to ground with a flying lead.

By varying the voltage at \(A\) in this manner you are simulating a square wave and you will see that the voltage measurement at the output, point \(C\), follows the waveform you are putting in at \(A\). When \(A\) is connected to ground do not expect to see zero volts at point \(C\) because you must remember there are forward voltage drops across the diodes to consider. By keeping input \(B\) connected to +4.5 V you are, in effect opening the gate to allow the signals from \(A\) to pass through.

Now connect point \(B\) to ground and you will find that the output \(C\) drops to nearly zero and stays there irrespective of any signal you apply at \(A\)-grounding point \(B\) shuts the gate.

Yon may have noticed that while doing this
you can have the gate open by leaving input \(B\) disconnected; you can therefore consider this to be a "spring loaded" gate which-in the absense of any positive action to keep it closed (grounding point \(B\) )-will always swing open.

\section*{CIRCUIT ACTION}

Let's see why this effect takes place. We shall assume that we are using "digital" signals at inputs \(A\) and \(B\); this means that the voltages we supply will be either the full supply voltage \((+4.5 \mathrm{~V})\) or ground ( 0 V ).
Imagine that both inputs are shorted to ground; both the diodes D1 and D2 will be forward biased and current will flow down R1 and through the diodes and we will get a voltage at \(C\) that corresponds to the forward voltage drop of the silicon diodes (about 600 mV ).
Leave \(B\) connected to ground and imagine \(A\) connected to \(+4 \cdot 5 \mathrm{~V}\). The voltage at \(A\) is more positive than the voltage at \(C\) so \(D 1\) will be reverse biased and hence will not conduct; D2, on the other hand, is still forward biased and the output will stay at nearly zero. Reverse the connections between \(A\) and \(B\) (so that \(B\) is now going to +4.5 V with \(A\) to ground) and you have exactly the same set of circumstances as before -the voltage at \(C\) stays low.

If, however, both \(A\) and \(B\) are connected to +4.5 V (or, for that matter, are left disconnected) no current can flow through R1-except for the minute amount taken by the meter-and the voltage at \(C\) will rise to about \(+4 \cdot 5 \mathrm{~V}\).
Fig. 12.1. The basic AND gate and the truth table
\begin{tabular}{|c|c|c|}
\hline \multicolumn{2}{|c|}{ INPUTS } & OUTPUT \\
\hline\(A\) & \(B\) & \(C\) \\
\hline\(O V\) & \(O V\) & \(O V\) \\
\hline\(+4.5 V\) & \(O V\) & \(O V\) \\
\hline\(O V\) & \(+4.5 V\) & \(O V\) \\
\hline\(+4.5 V\) & \(+4.5 V\) & \(+4.5 V\) \\
\hline
\end{tabular}



Fig. 12.2. Test circuit for the gate
Notice that we have described every possible permutation of applying either 0 V or +4.5 V to both inputs-four possibilities in all-and in only one of these possibilities did the output go to +4.5 V . This occurred when both \(A\) and \(B\) were connected to +4.5 V -strictly speaking we should not consider any cases of the inputs being disconnected.

Because the output will go to a high voltage only when both outputs are connected to a high voltage shows us why the gate is called an and gate. It takes \(A\) and \(B\) to be at high levels to make \(C\) go to a high level!

\section*{TRUTH TABLE}

The combinations of the input conditions and the resulting output conditions can best be seen in the form of a table-Fig. 12.1. This is called a truth table. Imagine column \(A\) as being a signal and column \(B\) a control voltage. You can see that the voltages applied to \(A\) appear at the output when \(B\) is +4.5 V but the input signal is inhibited from appearing at the output when \(B\) is at \(0 \mathrm{~V} ;+4.5 \mathrm{~V}\) at \(B\) opens the gate while 0 V closes it!

\section*{DIGITAL GENERATOR}

As an extension of the experiment you can generate a real electronic digital waveform for input \(A\) by using a slow running astable multivibrator as shown in Fig. 12.2. Check with the voltmeter that you are getting a repetitive waveform at point \(A\) and then measure what you get at output \(C\) when \(B\) is firstly connected to +4.5 V and then to ground.

You might think that connecting point \(B\) to ground in some way stops the multivibrator operating; this is not so and you can check this by returning the voltmeter to point \(A\). The two diodes are acting as a control gate for the multivibrator's signal.

\section*{ALARM}

Finally, and to remove the need for mechanical intervention, we can use an electronic signal as the control. A simple circuit is shown in Fig. 12. 3. Basically we have a multivibrator operating at an audio frequency and a photocell driving a transistor as a control source.

When the photocell is dark, the voltage at the collector of TR3 is high and this effectively applies +4.5 V to input \(B\)-the signal from the audio source can thus pass through the gate into the loudspeaker driver and we hear an audio tone. When light falls on the cell base current passes into TR3 and the voltage at its collector falls virtually to zero; this closes the gate and the audio tone stops.

If you had this circuit set up with a torch beam illuminating the cell there would be no tone from the loudspeaker until the light beam was interrupted-perhaps by someone walking through a door-and then you get an audible alarm.

\section*{Next part: The series resonant filter}

Fig. 12.3. Simple electronic circuit to demonstrate the function of the AND gate


\title{
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\title{
COUHTOERHITV By GEORGE HYLTON
}

\begin{abstract}
"Why is it that you don't get a shock if you touch the neutral terminal of the mains? After all, this terminal is negative half the time and positive half the time, so if you don't get a shock when it's negative then you should get one whèn it's positive. Also, why is it that if you connect a voltmeter between the neutral and earth terminals you get a small voltage reading?"
\end{abstract}

An enquiring mind is a great thing, and can lead to important discoveries. Benjamin Franklin, flying his kite in a thunderstorm, proved that thunderclouds are electrically charged and so gained evidence that lightning is electrical.
The next chap to try the experiment discovered that it could be dangerous. He was electrocuted. Which is by way of saying, please, please don't play about with the mains.
Even if what you do should be safe, in theory, as in this case, there's no guarantee that it will be safe in practice. Electrical wiring in the house has been known to have the polarities reversed, the earth connection omitted, and so on.

\section*{BRITISH SYSTEM}

For the benefit of foreign readers whose mains system may be different from ours, the standard British housc wiring system provides \(240 \mathrm{~V}, 50 \mathrm{~Hz}\) outlets at sockets which take three-pin plugs.

One pin is connceted to the local, domestic earth (often a metal water pipe where it enters the ground). Another is the neutral side of the mains, earthed at the power station or distribution transformer. The third is the live or non-earthy side of the mains. The system is shown in Fig 1, which is simplified in that it glosses over the fact that the distribution cables are usually made to carry more than one "phase" and so have more than two conductors, but the general idea is correct.

In order to receive a shock from the mains, it is necessary to connect your body between the
live and neutral terminals, directly or indirectly.

\section*{DIRECT AND INDIRECT}

A direct connection is what you get if you touch the "live" terminal with, say, one finger and the "neutral" with another. This is not pleasant. In particular, if the two fingers are on different hands, the resulting arm-to-arm current passes through your heart, which is a pretty good way of killing yourself.

The indirect connection is nearly as bad. It happens when you touch the "live" terminal only, but when your body is also in some way connected to the earth.

Since the mains "neutral" is also connected to earth, the circuit is complete and you get a shock. With 240 V to drive the current, the earth connection to your body needn't be very good. Standing on a concrete floor in leather-soled shoes may provide a low enough resistance for a lethal shock, while most homes contain a wealth of earthed objects such as water pipes, taps, gas pipes, central heating radiators and so on.

\section*{NO SHOCK}

I know: I haven't answered the questions yet. Well, the answer to the first one can be seen from


Fig. 1 Domestic mains supply from power station.

Fig. 1. Touching the "neutral" alone, even if you are earthed, doesn't permit current to flow between "live" and "neutral", via your body, so, no shock. The polarity of the voltage at the neutral terminal swings positive and negative with respect to the live terminal but it's always the same as that of the earth terminal, since both neutral and earth are connected to the earth, one at the power station and the other at the local water pipe or whatever.

Since both these terminals are earthed, there can be no voltage difference between them, Or can there? Yes, there can, because they are not connected to the earth at the same place: the earth connections may be miles apart.

\section*{VOLTAGE DROP}

This leads to the answer to the other question, which is, really: how can there be a voltage difference between two terminals, each earthed? In Fig. 1, the cable between power station and home is shown as having no resistance. But real cables, however thick, do have some resistance. Since a mains distribution cable may be carrying thousands of amperes even a few thousandths of an ohm resistance can cause an appreciable voltage drop.

In the case of the neutral side of the cable, this voltage drop is earthed at the power station but not at the home end. The home end can therefore be-a few volts above local earth potential, and this is one cause of the small voltage which our reader measured between local earth and neutral terminals.

"Better check your construction of that indicator audible warning-it's just failed the noise test."


\section*{P.C. Construction}

Wishing to construct the Train Controller as described in Everyday Electronics Vol. 2 No. 9 September, ' 73 , I decided to have a go at making my own printed circuit as per instructions in Vol. 2 No. 6. June '73. I'm afraid that I have lost count of the number of chemists that I called on to try and get the ferric chloride and have come to the conclusion that there must be an easier way to carry out this project. One chemist told me that there was no such animal as ferric chloride in powder or crystal form and that it existed only in liquid form.
In the end I managed to purchase a do-it-yourself kit (in which the f.c. was a liquid) but as I would like to be able to purchase the necessary chemicals separately I would welcome your comments generally.
I note that in the process of etching on copper that nitric acid is used. Although more care would have to be exercised when using acids it might prove easier to obtain and I would enquire if this is a suitable alternative
By the way, I feel that the estimated cost of \(£ 3 \cdot 15\) for the cost of parts for the controller was a bit conservative. I purchased most of the bits and pieces from Henry's Radio, and the balance from a component shop in Brighton, and they came to a lot more than \(£ 3 \cdot 15\). If A. J. Dunn managed to build his for \(£ 3 \cdot 15\) then he was very lucky.

I look forward to receiving your reply and thank you for providing such an interesting mag. each month.
N. C. Langridge, Littlehampton, Surrey
G. F. Milward of 369 Alum Rock Road, Birmingham B8 3DR can supply \(1_{2} l b\) packs of. ferric chloride (in crystal form) for 50p including post and packing. A dilute solution of nitric acid can
be used provided the resist can withstand it-nail varnish is quite good!

The price for the controller was obtained by pricing components from suppliers catalogues. One of our advertisers is supplying a kit of parts for the same price.

\section*{Soldering Competition}

Many thanks for your letter dated September, 1973 and your kind congratulations accompany:ing a most attractive and useful runner-up prize

The competition has given me great pleasure and I would like to say that I whole-heartedly agree with the final order selected by the judges for the first prize. They obviously gave the competition considerable thought

May I also take this opportunity to congratulate you on your very fine publication, which I always find most interesting, stimulating and educational.
J. W. Berry,

Bury St. Edmunds.

Many thanks for the safe receipt of my prize from the recent soldering competition in Everyday Electronics.
Congratulations are really all due to Everyday Electronics which I have taken ever since the first issue. Before chis, I did not have the vaguest idea about electronics or solderiag.

Being a midd'e aged spinster with no male friends or relatives connected in a:iy way with electronics I have. learned all I do know on the subject through your pages. It is the lucid way in which processes are explained, together with the detailed diagrams and clear photographs, which I have found so easy to follow, which has enabled me to learn as much as I have. (To my wondering surprise.)

The excellent book about soldering is just what I needed and is going to be so useful. I didn't have a wire stripper either, so that also will be very acceptable, even though I have acquired the knack of stripping with side cutters!

Incidentally, I have never ever won any kind of prize in my life before. Maybe electronics has brought some luck at last!
Thank you again for the gifts and for an excellent magazine, and for the happy hours that will ensue from both.

> Connie Wade Leeds.

\section*{Price}

As a schoolboy I am rather annoyed at the letter in the December E.E. which said that your projects are within the scope of the pocket money of the schoolboy enthusiast. This is not true. the average schoolboy only gets at the least 30 p pocket money which is hardly enough for your projects. I have made one of your projects which the approximate cosl was 45 p (Neon Novelty with two lamps). It cost me a total of 105p which 1 could only afford because it was Easter.

David Hooton,
Rushden, Northants.

\section*{Spiders At Work}

Re. your December issue Ruminations, spiders are used by man to spin their webs to suit our purposes. Selected spiders are made to spin a thread onto special frames, which are then stored until needed to be used as graticules (crosswires) in certain optical instruments. An example of this application was shown on BBC's "Animal Magic" some weeks ago, when a spider was shown working for man at the York factory of Vickers Instruments, the "end" result being used in the repair of a theodolite.
C. Long,

Leeds.

\footnotetext{
Please note: we can only answer readers letters concerning published articles. not commercial equipment or modifications to circuits. Please include an s.a.e. for a reply.
}


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\section*{COMPONENTS}

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}

\author{
POWER SUPPLY UNIT FEB. 14 \\ SLIDE PROJECTOR TIMER FEB. 74 \\ SEE COST \\ FETSET JAN. 74 \\ £2.00 \\ TREMOLO DEC. 73 \\ WAA-WAA \\ SEPT. 73 \\ £1.50 \\ BETA FUZZ-TREBLE JAN. 73 \\ £1•50 \\ (For Beta Fuzz-Treble, Component board components only.
}

BETA TRANSFORMER
£1•85

\section*{MAIL ORDER ONLY S.A.E FOR ALL ENQUIRIES}

\section*{CTPRTNRIIE MK II \\ ELECTRONIC IGNITION KIT}

\section*{COMPRISES}

Everything:-
Ready Drilled Case and Meralwork. Cables, Coil Connectors, Silicon Grease. Printed Circuit Board, 5 year guaranteed components and a lull 8 -page instruction leaflet.
WHEN COMPLETE THE UNIT CAN BE FITTEDTO YOUR CAR IN ONLY IS MINUTES USING THE STANDARD COIL AND CONTACT BREAKER POINTS: TO GIVE YOU:-
Instant all weather starting. Up to \(20 \%\) fuel saving, Longer bateery life, Higher top speed. Faster acceleration. Spark plugs last about five time longer. Misfire due to contact breaker. bounce electronically eliminated. Purer exhaust emission resulting in less air pollution, Contact breaker burn eliminated. Suitable for all perrol engines up to 8 cylinders

PRICE ONLY \(£ 12.65\)
Ready Bult Unit \(£ 14.85\)
Unic for Motor.
Cycles with twin coils
and twin C.B. Points \(\mathbf{£ 1 9 . 8 0}\)
(prices include VAT and post
Please staze whether Positive or negative earch unirs are required when ordering. \& packing).
(NOT AVAILABLE IN KIT FORM)
SEND FOR YOUR UNIT OR FULL
BROCHURE NOW
FROM
ICE ELECTRONIC SYSTEMS DEPT E.E.
114 PARK FARM ROAD
BIRMINGHAM B43 7QH

\section*{Introducing the new}


Following the successful merger in 1972 of

\section*{LASKYS RADIO LTD. \& G. W. SMITH \& CO. (RADIO) LTD} the U.K's two leading audio retailers through Audiotronic Holdings Ltd the final phase of the integration has now been completed. One retail company trading under the name of "Laskys" has been formed to bring you a wider choice of equipment, highly competitive prices and a better than ever service.

LASKYS RANGE-We stock the widest range of the best equipment in the U.K. and probably the world, backed by accessories,tapes and cassettes, components and other electronic equipment

\section*{LASKYS BRANCHES-}

We have 24 branches throughout London and the provinces each holding a comprehensive range and our staff will be pleased to demonstrate and advise on your choice of equipment

LASKYS PRICES-()ur enormous purchasing power together with reduced administration costs enables us to offer you the most competitive prices to be found in the UK.


LASKYS GUARANTEE-All equipment purchased from us is offered with a full 12 months guarantee including parts and labour.

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\section*{14 ALL PRICES EXCLUDE VAT}


\section*{U4323 MULTIMETER}
 60/150i600mA
1.5/5A AC. \(0 / 200 / 3 * / 30 \mathrm{k}\) ohms. DC sccuracy 18. AC \(1.5 \%\). Knite edga pointer, mirror seale. Complete with
sturdy metal carrying case, lands and sturdy metar OUR PRICE E9.75 P\&P 25p


\section*{}
 Current: \(0.06 i 0.61\)
\(6 / 60 / 600 \mathrm{~mA} D \mathrm{C}\). \(0.3 / 3 / 30 / 300 \mathrm{~mA} A\)
Resistance: \(0.06 f\) Resintance: \(6 / 6 / 20 / 60 / 200 \mathrm{k}\) ohma/2 Mohrras
Eattery operated. Supplied complate Eattery operated. Supplied complate with probes, leads and stoe earrying
case Size: \(115 \times 285 \times 90 \mathrm{~mm}\).
OUR PRICE 10.50

Model 449A In Circuit
TRANSISTOR TESTER
Checks trut AC,
Beta inlour Chick
ICO. Checks diodes in out. Checks SCR
etc. Erta H1 \(10-500\)
\(10.2-50,1 C O-0-\) \(202-50.1 C 0\)
5000 VA .220 :
240 ac ope
OUR PRICE \(\mathbb{1} 17.50\) F\&P 25p

\section*{MOOEL 500 \\ 

MODEL CTOBOEN
 50,25017000/
 \(1000 / 5000 \mathrm{~V}\) AC
\(0 / 50 \mathrm{Al} 1 / 10 /\) 100/500mA/10A
 \(20 \mathrm{Meg}-20\) to +50 dB OUR PRICE E13.95

PEP 35p

\section*{KAMODEN 360 MULTIMETER}

High sersitivity;
DC \(100 \mathrm{kohm} / V\)

\section*{A}
A. Current S00mA/IOA. 1/10/100 ohmis 1/10/100k ohms
 10/100M ohms
Decibels -20 to
+62 dB , Battery opersted. Size: \(180 \times\) \(140 \times 80 \mathrm{~mm}\).
test losds
Etc.
OUR PRICE E13.95 P\&P 25p

\section*{HIOKI MODEL 700X \\  \(300 / 600 / 1200 \mathrm{VAC}\).
\(15 / 30 \mathrm{~A} / 3 / 6 / 30 / 60\) \(150 / 500 \mathrm{~mA} / 6 / 124 \mathrm{DC}\) 63 dE.}

OUR PRICE £14.95

\section*{S100TR MULTIMETER}

TRANSISTOR TESTER
100,000opv. Mirtor
protection. o/0.12/ \(0.6 / 3!12 / 30 / 120 /\)
\(600 V\) DC. \(0 / 6 / 30 /\) 1201600 V AC. \(0 / 12 / 600 \mathrm{~A} A / 12 f\)
\(300 \mathrm{mAC12A} D C\) \(0 / 10 \mathrm{k} / \mathrm{I} \mathrm{Me} / \mathrm{g}\) 100 Mieg. -20 to 50 dB .
\(0.01-0.2 \mathrm{MFD}\).
Transisior tester measures Ajphz, Bera and ico. Compiest.
batteries-and lesós. OUR PRICE £14.95
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\section*{KAMODEN HM720B FET VOM}
\(180 \times 80 \times 40 \mathrm{mim}\).
OUR PRICE \(£ 15.00\) P\&P 200
U4317 MULTME TER

\section*{10
\(k\)
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8}
 \(0.5 / 2.5 / 10 / 25 / 50 / 100 / 250 / 500 / 1000\)
00 C
\(0.5 / 25 / 10 / 25 / 50 / 100 / 250 /\)


 Battury operated. Size: \(210 \times 115 \mathrm{x}\)
gomm. Supplied in carrving cass complete with lead. OUR PRICE E15.00 P\&P 200
KAMOOEN 72200 Mulfiteste:

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OUR PRICE £16.95 P\&P 30p

\section*{37OWTR MULTIMETER}

Features AC currant
rantus 20000 opv.
 \(250 / 500 / 1000 \mathrm{~V}\) 250/25/10/50/250/
\(500 / 10000 / 4 C\) \(500 / 1000 V\)
\(0 / 5001 / 1 / 101100\) mA/110A OC
\(0 / 100 \mathrm{~mA} / 110 \mathrm{~A}\) AC. \(0 / 5 \mathrm{~F} / 50 \mathrm{k} / 500 \mathrm{k}\) \(5 \mathrm{Meg} / 50 \mathrm{M} 90\)
Decibels: -20 to +62 dB OUR PRICE E17.50 P\&P 25p
TMK MOOEL 117 FET
ELECTRONIC VOLTMETER
Buttery operated.
11 Mieg inpu:,
z.
rangos Large \(4 \times\).
mirror scale. Size:
mirror
\(149 \times 11760 \mathrm{~mm}\).
\(0.3-120000 \mathrm{DC}\). 3.3-12000V DC.
\(3-300 \mathrm{~V}\) FMS AC. 8-800V P.P. 12 12 mA Risisimice


12 to 2000 Monms. Decibuss: -20 to
 OUR PRICE E17.50 PEP 200

\section*{TE65 VALVE VOLTMETER}

28 range \(D C\) vors
\(1.5-100 \mathrm{~V} . \mathrm{AC}\)
volss \(1.5-1500 \mathrm{~V}\).
1.50ts \(1.5-1500 \mathrm{~V}\).
viscistance up to
.

1000 M Megohms.
\(200 / 240 \mathrm{AC}\)
operation. Comb.
pleat wift probe
and instructions.
BUR PRIGE 17.50 Additiond
RF \(£ 2.12, ~\)
HV
52.50

TE4O HIGH SENSITIVITY AC VOL TMETER 10 Meg input
10 ranges \(0.001 /\)
\(0.03 / 0.1 / 0.3 /\) \(10.03 / 0.1 / 0.3 / 1\)
\(1 / 3 / 11 / 30 / 100 /\)
501

 supplied brand
new complate with leads and


QUR PRICE E17.50 PRP 25p
KAMODEN HMG500
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Range 0- 1,000 \\
Megohms, 500 V \\
Battery operated meter \(4 \times 4 x^{\prime \prime}\). \\
Complete with doluxe earring cass, battories and instructione OUR PRICE 19.95
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TMK LAB TESTER
100.0000pv. 6
couie Buzxer
tort circuit
theck

OC Votss \(0.5 / 2.51\)
10/50/250/1000V

current \(10 / 100 \mathrm{u} / 10\)
\(10 / 100 / 500 \mathrm{~mA} / 2.5 / 10 A\). Resistence: \(1 \mathrm{k} / 10 \mathrm{k} / 100 \mathrm{k} / 10 \mathrm{Meg} / 100 \mathrm{Mleg}\) ohms
Decibets: -10 to +49 dE . Plastrc care
 OUR PRICE E19.95 P\&P \(25 \rho\)

MODEL U4311 Sub-standard
Multi-range Volt-Ammeter Sbnsitivity 330
\(0 \mathrm{Hmm} / \mathrm{V}\) otr AC OhmiV oit AC and DC.
Atcuracy 0.5
DC. \(1 \%\) AC.
Sci leng Scile length:
165 mm .
\(0 / 300 / 750 \mathrm{~A}\) \(1.5 / 3 / 7.5 / 15 /\)
\(30 / 75 / 150 / 300\) \(30 / 75 / 150.300\)
\(750 \mathrm{~mA} / 4.5 / 3 /\)
7.5ADC. O/3/
\(7.5 / 15 / 30 / 75 /\)
\(150 / 300 / 750 \mathrm{~mA}\)

1.5/3/7.5A AC.
\(0 / 75 / 150 / 300 / 750 \mathrm{mV} / 1.5 / 37.5 / 15 /\) \(30 / 75 / 150 / 300 / 750 \mathrm{~V}\) DC. O/750mV/ A.5/3 /7.5/15/30/75/150/300/. Aspp-
AC. Automatic cart out device. Supp lied complete with test lesds, manual and test certificatex.
OUR PRICE \(£ 49.00\) P\&P 500

\section*{AT201 Decade \\ ATTENUATOR}

Frequency rtang 0-
200 khz . Artenuator
\(0-111 \mathrm{~dB}, 0.1 \mathrm{~dB}\)
steps. Impedance 600 ohms. ingut

OUR PRICE E12.50 P8P 37p
TEIGA TRANSISTORISEO
SIGNAL GENERATOR


ARF 300 AF/RF SIGNAL
GENERATOR
All transistorised portable AF sino
wwite 1810220
KHz AF square
wave 18 Hz to 800 k
Hz . Output Squara/
Sipe wove 10 V .
P.PRF 100 KHz to
200 MHz . Output
1 maximum.
with instructians and lasds.
OUR PRICE E79.95 50p
Everyday Electronics, February 1974


SKYFON 100 mW
OUR PRICE E24.95 per pair P302 Two Channel 300 cmw OUR PRICE E 52.50 per pair P1003 Three Channel I Watt OUR PRICE \(£ 71.25\) per pair P\&P 50p per peir
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\hline \(25 \times \mathrm{A}\) & - & - & - & - & - & £4.60 & - & - & - & - & - & - & \\
\hline 50uA & 5255 & 5270 & E3.50 & £3.70 & \(\underline{4.40}\) & E3.55 & 23.50 & E4.15 & 1280 & 123.05 & \(\pm 3.40\) & \(\pm 3.75\) & 66.90 \\
\hline 100uA & \(\underline{22.45}\) & ¢2.60 & E3.00 & E3.15 & £4.25 & ¢3.00 & E3.40 & E3.95 & \(\underline{52.75}\) & \$3.00 & E3. 35 & E3.60 & E6.40 \\
\hline 200uA & £2.40 & E2.50 & - & \(\pm 3.05\) & E4:05 & - & - & - & £270 & E3.00 & \(\pm 330\) & E3.40 & - \\
\hline 500uA & ¢2.25 & £2.45 & £2.65 & 22.75 & E3.90 & ¢2.70 & E3.05 & \(E 3.70\) & 5255 & 12.95 & E3.15 & E3.20 & \\
\hline 50.0-50uA & ¢2.50 & ¢2.85 & £3.05 & E3.15 & 14.25 & ¢3.05 & E3.40 & 183.95 & 12.80 & 23.05 & \(\pm 3.40\) & 53.60 & 156.40 \\
\hline 100-6-100ua & ¢2.40 & E2.50 & \(\pm 2.95\) & £3.10 & £4.05 & E3.00 & 23.30 & E3.90 & \(\underline{52.75}\) & 23.00 & E3.35 & 43.50 & - \\
\hline 500.-500uA & E2.25 & E2.40 & - & E2.60 & E3.90 & \(E 2.60\) & - & - & - & - & - & - & - \\
\hline 1 mA & £2.25 & £2,40 & E2.50 & \(\underline{2.60}\) & \$3.90 & E2.60 & £3.00 & \%360 & 82.60 & 12.90 & 53.10 & 53.20 & - \\
\hline 1-0-1mA & \(\underline{52.25}\) & - & - & - & £3.90 & E260 & - & - & - & - & - & - & - \\
\hline 2 ma & E2.25 & - & - & - & & - & - & - & - & - & - & - & - \\
\hline 5 mA & \(\underline{2.25}\) & E2.40 & F2.50 & \(\underline{260}\) & E3.90 & 52.80 & - & - & 52.60 & 22.90 & \(\underline{3.10}\) & - & - \\
\hline 10 mA & E2.25 & E2.40 & E2.50 & £2.60 & E3.90 & 12.80 & - & - & 18260 & \(\underline{290}\) & ¢ 7.10 & - & - \\
\hline 20 mA & \(\underline{22.25}\) & - & - & - & - & - & - & - & - & - & - & - & - \\
\hline 50ma & £2.25 & \(\underline{42.40}\) & E2.50 & £2.60 & 53.90 & 82.60 & - & - & ¢2.80 & 12.90 & 23.10 & - & - \\
\hline 100 mA & £2.25 & £2.40 & ¢2.50 & E2.60 & \(E 3.90\) & \(\underline{52.60}\) & - & - & 182.60 & E2.90 & £3.10 & - & - \\
\hline 150 mA & \(£ 2.25\) & - & - & - & - & - & - & - & - & - & - & & \\
\hline 200ma & \(£ 2.25\) & & & & & & - & - & - & - & - & - & - \\
\hline 300 mA & \(\underline{525}\) & - & - & & - & - & - & - & - & - & - & - & - \\
\hline 500 mA & ¢225 & £2.40 & £2.50 & 5260 & E3.90 & \(\underline{\text { E2.60 }}\) & - & & 82.60 & E2.90 & ¢3.10 & - & \\
\hline 750 mA & \(\underline{2} .25\) & & - & - & - & - & - & - & - & - & - & - & - \\
\hline 1A DC & ¢2.25 & 22.40 & \(\underline{4.50}\) & £2.60 & E3.90 & \(\underline{2} .60\) & £3.00 & E3.60 & 18230 & 22.90 & E3.10 & - & 25.85 \\
\hline 2A DC & 52.25 & & - & - & - & E2.60 & - & - & - & - & - & - & \\
\hline 5A DC & ¢225 & E2.40 & 22.50 & ¢2.80 & E3.90 & \(¢ 2.60\) & £3.001 & E3.60 & E2.80 & E290 & 53.10 & - & 15.95 \\
\hline 10a DC & \(\underline{C 2} 25\) & - & - & ¢2.60 & - & - & - & - & E2.80 & E2.90 & E3.10 & - & - \\
\hline 15A DC & £2.25 & - & - & E2.50 & E3.90 & E2.60 & - & - & - & - & - & - & - \\
\hline 20A DC & E2.25 & - & - & E2.60 & - & - & - & - & - & - & - & - & - \\
\hline 30A DC & - & - & - & £2.80 & E3,95 & 12.60 & - & - & & & & & \\
\hline 50A DC & - & - & - & \(£ 2.90\) & - & £2.60 & - & - & - & - & - & - & - \\
\hline 3V DC & ¢2.25 & - & - & - & - & - & - & - & - & - & - & - & - \\
\hline \(5 V\) DC & - & & - & 12.60 & - & \(\underline{22.60}\) & - & - & ¢2.60 & E2.90 & E3.10 & - & 25.95 \\
\hline 10 V DC & \(¢ 2.25\) & E2.40 & E2.50 & £2.60 & E3.90 & \(\underline{1260}\) & - & - & £2.60 & - & £3.10 & - & E5.95 \\
\hline 15 V DC & ¢2.25 & - & - & - & - & - 1 & - & \(\square\) & - & - & & - & 55.95 \\
\hline 20V DC & \(¢ 2.25\) & £2.40 & £2.50 & 82.60 & E3.90 & \(£ 2.60\) & E3.00 & £3.60 & - & £2.90 & ¢3,10 & - & E5.95 \\
\hline 50 V DC & 12.25 & E2.40 & E2.50 & 82.60 & E3.90 & \(\underline{2.60}\) & E3.00 & £3.60 & 12.60 & E2.90 & E3.10 & - & 25.95 \\
\hline 100 V DC & ¢2.25 & - & - & - & - & - & - & - & - & - & - & - & - \\
\hline 150 V DC & \(£ 2.25\) & - & - & 2260 & E3.90 & \(\underline{22.60}\) & - & - & - & - & - & - & - \\
\hline 300V DC & £2.25 & E2.40 & E2.50 & 82.60 & E3.90 & ¢2.60 & E3.00 & 33.60 & 22.60 & E2.90 & E3.10 & - & 55.95 \\
\hline 500V DC & 8225 & - & - & - & - & - & - & - & - & - & - & - & - \\
\hline 750 V DC & ¢225 & - & - & - & - & - & - & - & \(=\) & - & - & - & - \\
\hline 15 V AC & ¢2.30 & £2.45 & £2.60 & £2.80 & £2.95. & - & - & - & ¢2.70 & E3.00 & £3.30. & - & - \\
\hline 30 V AC & - & - & - & - & - & £2.65 & - & - & - & - & - & - & - \\
\hline 50 V AC & £2.30 & - & - & £2.80 & & £2.65 & - & - & - & - & - & - & \\
\hline 150 V AC & f2.30 & - & - & £2.80 & - & £2.65 & - & - & - & - & - & - & - \\
\hline 300 V AC & E230. & \(\underline{545}\) & E2.60 & 22.80 & 83.95 & E2.65 & E3.00 & £3.70 & \(£ 2.70\) & £3.00 & £3.30 & E3.25 & - \\
\hline 500 V AC. & £2.30. & - & - & £2.80 & - & £2.65 & - & - & - & - - & - & - & 7 \\
\hline S Minter 1mA & £230 & £2.50 & E2.60 & ¢2.85 & £3.90 & - & - & - & - & \(\stackrel{-}{-}\) & - & - & - \\
\hline VU Mener & \(¢ 2.65\) & \(£ 2.70\) & E3,60 & E3.70 & £4.55 & £3.65 & £3.70 & 14.30 & 12.00 & £3.15 & E3.50 & E3.85 & - \\
\hline IA AC & - & 5240 & £2.50 & £2.60 & E3.90 & ¢2.60 & - & - & - & - & - & - & - \\
\hline 5A AC & - & 52.40 & £2.50 & \$2.60 & 83.90 & E2.50 & - & - & - & - & - & - & - \\
\hline 10A AC & - & \(E 2.40\) & £2.50 & £2.60 & \(\pm 3.90\) & £2.60 & - & - & - & - & - & - & - \\
\hline \(20 A A C\) & - & E2.40 & C2. 50 & E2.60 & \(\pm 3.90\) & \(£ 2.60\) & - & \(\rightarrow\) & - & - & - & - & - \\
\hline 30A AC & - & E240 & E2.50 & 82.60 & \(\pm 3.90\) & \(£ 2.60\) & - & - & - & & - & - & \\
\hline 50A AC & - & - & 亏 & - & - & ¢260 & \(\stackrel{-}{+}\) & - & - & - & \(=\) & - & - \\
\hline 50mA AC & - & - & - & £2. 50 & - & - & - & - & - & & & - & - \\
\hline 100 mA AC & - & - & - & ¢2.601 & - & - & - & - & - & - & - & - & - \\
\hline \(200 m A A C\) & - & - & - & 82.60 & - & - & - & - & - & - & - & - & - \\
\hline 500 mA AC & - & - & - & E2.60 & - & £2.60 & - & - & - & - & - & - & - \\
\hline 50 mV V DC & - & - & \(\because\) & - & - & E2.90 & - & \(\llcorner\) & - & - & - & - & - \\
\hline 100 mV DC & - & - & - & - & - & £2.90. & - & - & - & - & - & - & \(-\) \\
\hline 500 mA 5 SA DC & - & - & - & - & - & - & - & - & - & - & - & - & E7,00 \\
\hline 1/15A DC & - & - & - & - & - & - & - & - & - & - & - & - & \(\underline{7.00}\) \\
\hline 5/15V DC & - & 1- & - & - & - & - & - & - & - & - & - & - & \(\underline{7.00}\) \\
\hline SJ50Y DC & - & - & - & - & - & - & = & - & - & \(\cdots\) & - & \(\cdots\) & \(\underline{27.00}\) \\
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\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Fiont & Panal Hole & Fixing & & Front & Panel Hole & Fixing \\
\hline \(42 \times 42 \mathrm{~mm}\) & 32 mm din & 4 studs & Model SWi00 & \(100 \times 80 \mathrm{~mm}\) & E5man dia. & 4 studs \\
\hline \(50 \times 50 \mathrm{~mm}\) & 38 mm dia. & 4 studs & Model SO460 & \(59 \times 46 \mathrm{~mm}\) & 38 mm dia & 4 studs \\
\hline \(60 \times 60 \mathrm{~mm}\) & 48 mm dia. & 4 studs & Model SD640 & \(85 \times 64 \mathrm{~mm}\) & 45 mm dia. & 4 studs \\
\hline \(86 \times 78 \mathrm{~mm}\) & 57 mm dia & 4 studs & Madel SOB30 & \(110 \times 83 \mathrm{~mm}\) & 58 mm dia. & 4 studs \\
\hline \(120 \times 110 \mathrm{~mm}\) & 98 mm dia. & 4 studs & Model PE70 & \(90 \times 34 \mathrm{~mm}\) & \(70 \times 3 \mathrm{imm}\) & 2 holes \\
\hline \(80 \times 80 \mathrm{~mm}\) & 64 mm dia & 4 sturs & \multicolumn{4}{|l|}{\multirow[t]{2}{*}{Modai ED 107 Size: \(100 \times 90 \times 150 \mathrm{~mm}\) high inciuding terminals.}} \\
\hline \(80 \times 80 \mathrm{~mm}\) & 65 mm dia. & 4 studs & & & & \\
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POWER RHEOSTATS High quality ceramic
conscruction. Wind ingse mbedded in vitrocous enamel. Heary duty brush wiper. Contimuous ayailiblo eme ftock
Sinple hole fixing. X" diameter shatse Bulk quantiting susilabie. 25 WATT 10/25/50/100/250/500/ 1000 Ohme E1.15 P\&P 15p 50 WATT 10/25/50/100/250/500/ 1000/2500/5000 Ohms £1.62

P\&P10D
100 WATT 1/5/10/25/50/100/250/ E2.34

P\&P 15 \(p\)
YAMABISHI VARIABLE VOLTAGE TRANSFORMERS
 Variable output 0-260V MDOEL SZGO GENERAL PURPOS BENCH MOUNTING


AUTO TRANSFORMERS
O/155/250V. Stop up or step down.
\begin{tabular}{rrr} 
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The veraatlijty of their design makes theto ldeal for ure in recard players, tape recorders, stereo amplifiers and cassetle and cartridge tape players in the car and at home.
\begin{tabular}{|c|c|c|}
\hline Parameter & Conditions & Performance \\
\hline HARMONIC DISTORTION & \(\mathrm{Po}=3\) WATTS \(\mathrm{f}-1 \mathrm{KHz}\) & 0-25\% \\
\hline LOAD IMPEDATCE & - & \(8-16 \Omega\) \\
\hline INPUT LMPEDANCE & \(t=1 \mathrm{KHz}\) & \(100 \mathrm{k} \Omega\) \\
\hline PREQUENCY RESPONSE CE SdB & Po-2 WATTS & \(50 \mathrm{~Hz}-25 \mathrm{KEz}\) \\
\hline BENEITIVITY for MATED O/P & V8=25V. \(\mathrm{Rl}-8 \Omega \mathrm{f}=1 \mathrm{KHz}\) & 75 mV . BMs \\
\hline DIMENBIONS & & \(3^{\prime \prime} \times 21^{\prime \prime} \times 1^{\prime \prime}\) \\
\hline \multicolumn{3}{|l|}{The above table relates to tbe ALIO. AL20 and AILSO mudiles. The following table outlines the difierencex in their working conditionk.} \\
\hline Paramoter & ALIO AL20 & AL30 \\
\hline Maximam Supply Voltage & \(2 \overline{6}\) & 30 \\
\hline \begin{tabular}{l}
Power output for \({ }^{2} \%\) T.I.D. \\
\((\mathrm{BL}=8 \Omega \mathrm{f}=\mathrm{i} \mathrm{KHz})\)
\end{tabular} &  & 10 wates a 318 3 1 n . \\
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\end{tabular}

\section*{AUDIO AMPLIFIER \\ MODULES}

AL 10. 3 watts RNIs iL 30 . 10 watte RAS

\section*{POWER SUPPLIES}

P8 12. (Use with AL10 \& ALw0) \&PM 80. (Use with also AL 30 \& \(88 p\) PRONT PANERS SP 12 with knobe 3.25

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The FA 12 pre amplifier has been designed 20 match into most budget stereo yystems. It is compatible with the AL 10. AL 20 and AL 30 audio porer amplifers and it can be supplied from their wewociated power enpplies, There are two stereo inpurn, one bas been deaigned for use vith *Ceramic cartridges while the auxillary input will aust most tisagnetic cartridges. Full details are giren in the apecification table. The fow controls are, froan left to right: Volume and onfoff switch. balarice bass and treble. Size \(152 \mathrm{mma} \times 84 \mathrm{~mm} \times 35 \mathrm{~mm}\).

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