

electronics today

JANUARY 1978

INTERNATIONAL

40p

**Electronics In
Surveying**

Wireless Show Report

**Building And
Installing Our
Burglar Alarm**

**SPECIAL
GAMES ISSUE**

**Hammer Throw
Race Track
Calculator Games**



... NEWS ... PROJECTS ... MICROPROCESSORS ... AUDIO ...

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POLYESTER CAPACITORS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

POLYESTER RADIAL LEAD		FEED-THROUGH CAPACITORS	
10p	1p	10p	1p
15p	1.5p	15p	1.5p
20p	2p	20p	2p
25p	2.5p	25p	2.5p
30p	3p	30p	3p
35p	3.5p	35p	3.5p
40p	4p	40p	4p
45p	4.5p	45p	4.5p
50p	5p	50p	5p
55p	5.5p	55p	5.5p
60p	6p	60p	6p
65p	6.5p	65p	6.5p
70p	7p	70p	7p
75p	7.5p	75p	7.5p
80p	8p	80p	8p
85p	8.5p	85p	8.5p
90p	9p	90p	9p
95p	9.5p	95p	9.5p
100p	10p	100p	10p

ELECTROLYTIC CAPACITORS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

TANTALUM RADIAL CAPACITORS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

MYLAR FILM CAPACITORS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

CERAMIC CAPACITORS 50V	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

SILVER MICA CAPACITORS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

CERAMIC TRIMMER CAPACITORS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

MINIATURE TYPE TRIMMERS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

COMPRESSION TRIMMERS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

JACK PLUGS	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

DIN	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
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55p	5.5p
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65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

DO AXIAL (TV)	
10p	1p
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20p	2p
25p	2.5p
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35p	3.5p
40p	4p
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75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

PHONE	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

BANANA	
10p	1p
15p	1.5p
20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
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90p	9p
95p	9.5p
100p	10p

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25p	2.5p
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35p	3.5p
40p	4p
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40p	4p
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90p	9p
95p	9.5p
100p	10p

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85p	8.5p
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100p	10p

BANANA	
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20p	2p
25p	2.5p
30p	3p
35p	3.5p
40p	4p
45p	4.5p
50p	5p
55p	5.5p
60p	6p
65p	6.5p
70p	7p
75p	7.5p
80p	8p
85p	8.5p
90p	9p
95p	9.5p
100p	10p

SPECIAL XMAS OFFER

TV GAMES

- Olympic Kit £20.80
- Olympic Colour Kit £28.50
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- COLOUR ADAPTOR for existing Black & White Games £8.85
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- Sure Fire Rifle Kit for other makes £9.25
- (p&p insured add 48p)
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- IC AY.3-8500 £4.50
- IC AY.3-8550 £7.50
- IC AY.3-8600 £9.00

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14	50	110	99	78	145
14	50	116	90	48	160
14	50	121	20	27	185

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Vol. 7 No. 1

International

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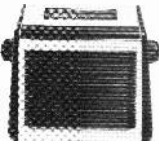
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EDITORIAL AND ADVERTISEMENT OFFICE

25-27 Oxford Street, London, W1R 1RF, Telephone 01-434 1781/2, Telex 8811896

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PAKS - PARTS AND MODULES

PANEL METERS

4" RANGE
Size 3 1/2" x 3 1/4" x 1 1/2"

Type	Price	Type	Price
AC-26	1.10	DC-26	1.10
AC-27	1.10	DC-27	1.10
AC-28	1.10	DC-28	1.10
AC-29	1.10	DC-29	1.10
AC-30	1.10	DC-30	1.10
AC-31	1.10	DC-31	1.10
AC-32	1.10	DC-32	1.10
AC-33	1.10	DC-33	1.10
AC-34	1.10	DC-34	1.10
AC-35	1.10	DC-35	1.10
AC-36	1.10	DC-36	1.10
AC-37	1.10	DC-37	1.10
AC-38	1.10	DC-38	1.10
AC-39	1.10	DC-39	1.10
AC-40	1.10	DC-40	1.10
AC-41	1.10	DC-41	1.10
AC-42	1.10	DC-42	1.10
AC-43	1.10	DC-43	1.10
AC-44	1.10	DC-44	1.10
AC-45	1.10	DC-45	1.10
AC-46	1.10	DC-46	1.10
AC-47	1.10	DC-47	1.10
AC-48	1.10	DC-48	1.10
AC-49	1.10	DC-49	1.10
AC-50	1.10	DC-50	1.10

2" RANGE
Size 2 1/2" x 1 1/2" x 1 1/2"

Type	Price	Type	Price
AC-51	1.10	DC-51	1.10
AC-52	1.10	DC-52	1.10
AC-53	1.10	DC-53	1.10
AC-54	1.10	DC-54	1.10
AC-55	1.10	DC-55	1.10
AC-56	1.10	DC-56	1.10
AC-57	1.10	DC-57	1.10
AC-58	1.10	DC-58	1.10
AC-59	1.10	DC-59	1.10
AC-60	1.10	DC-60	1.10
AC-61	1.10	DC-61	1.10
AC-62	1.10	DC-62	1.10
AC-63	1.10	DC-63	1.10
AC-64	1.10	DC-64	1.10
AC-65	1.10	DC-65	1.10
AC-66	1.10	DC-66	1.10
AC-67	1.10	DC-67	1.10
AC-68	1.10	DC-68	1.10
AC-69	1.10	DC-69	1.10
AC-70	1.10	DC-70	1.10

MR2P TYPE
Size 4x2x1/2 30mm

Type	Price	Type	Price
AC-71	1.10	DC-71	1.10
AC-72	1.10	DC-72	1.10
AC-73	1.10	DC-73	1.10
AC-74	1.10	DC-74	1.10
AC-75	1.10	DC-75	1.10
AC-76	1.10	DC-76	1.10
AC-77	1.10	DC-77	1.10
AC-78	1.10	DC-78	1.10
AC-79	1.10	DC-79	1.10
AC-80	1.10	DC-80	1.10
AC-81	1.10	DC-81	1.10
AC-82	1.10	DC-82	1.10
AC-83	1.10	DC-83	1.10
AC-84	1.10	DC-84	1.10
AC-85	1.10	DC-85	1.10
AC-86	1.10	DC-86	1.10
AC-87	1.10	DC-87	1.10
AC-88	1.10	DC-88	1.10
AC-89	1.10	DC-89	1.10
AC-90	1.10	DC-90	1.10

EDGEWISE
Size 3 1/2" x 1 1/2" x 2 1/2"

Type	Price	Type	Price
AC-91	1.10	DC-91	1.10
AC-92	1.10	DC-92	1.10
AC-93	1.10	DC-93	1.10
AC-94	1.10	DC-94	1.10
AC-95	1.10	DC-95	1.10
AC-96	1.10	DC-96	1.10
AC-97	1.10	DC-97	1.10
AC-98	1.10	DC-98	1.10
AC-99	1.10	DC-99	1.10
AC-100	1.10	DC-100	1.10
AC-101	1.10	DC-101	1.10
AC-102	1.10	DC-102	1.10
AC-103	1.10	DC-103	1.10
AC-104	1.10	DC-104	1.10
AC-105	1.10	DC-105	1.10
AC-106	1.10	DC-106	1.10
AC-107	1.10	DC-107	1.10
AC-108	1.10	DC-108	1.10
AC-109	1.10	DC-109	1.10
AC-110	1.10	DC-110	1.10

MINIATURE BALANCE/TUNING METER
Size 2 1/2 x 2 1/2 x 26mm

Type	Price	Type	Price
AC-111	1.10	DC-111	1.10
AC-112	1.10	DC-112	1.10
AC-113	1.10	DC-113	1.10
AC-114	1.10	DC-114	1.10
AC-115	1.10	DC-115	1.10
AC-116	1.10	DC-116	1.10
AC-117	1.10	DC-117	1.10
AC-118	1.10	DC-118	1.10
AC-119	1.10	DC-119	1.10
AC-120	1.10	DC-120	1.10
AC-121	1.10	DC-121	1.10
AC-122	1.10	DC-122	1.10
AC-123	1.10	DC-123	1.10
AC-124	1.10	DC-124	1.10
AC-125	1.10	DC-125	1.10
AC-126	1.10	DC-126	1.10
AC-127	1.10	DC-127	1.10
AC-128	1.10	DC-128	1.10
AC-129	1.10	DC-129	1.10
AC-130	1.10	DC-130	1.10

BALANCE/TUNING
Size 4 1/2 x 2 1/2 x 34mm

Type	Price	Type	Price
AC-131	1.10	DC-131	1.10
AC-132	1.10	DC-132	1.10
AC-133	1.10	DC-133	1.10
AC-134	1.10	DC-134	1.10
AC-135	1.10	DC-135	1.10
AC-136	1.10	DC-136	1.10
AC-137	1.10	DC-137	1.10
AC-138	1.10	DC-138	1.10
AC-139	1.10	DC-139	1.10
AC-140	1.10	DC-140	1.10
AC-141	1.10	DC-141	1.10
AC-142	1.10	DC-142	1.10
AC-143	1.10	DC-143	1.10
AC-144	1.10	DC-144	1.10
AC-145	1.10	DC-145	1.10
AC-146	1.10	DC-146	1.10
AC-147	1.10	DC-147	1.10
AC-148	1.10	DC-148	1.10
AC-149	1.10	DC-149	1.10
AC-150	1.10	DC-150	1.10

MIN. LEVEL METER
Size 2 1/2 x 2 1/2 x 26mm

Type	Price	Type	Price
AC-151	1.10	DC-151	1.10
AC-152	1.10	DC-152	1.10
AC-153	1.10	DC-153	1.10
AC-154	1.10	DC-154	1.10
AC-155	1.10	DC-155	1.10
AC-156	1.10	DC-156	1.10
AC-157	1.10	DC-157	1.10
AC-158	1.10	DC-158	1.10
AC-159	1.10	DC-159	1.10
AC-160	1.10	DC-160	1.10
AC-161	1.10	DC-161	1.10
AC-162	1.10	DC-162	1.10
AC-163	1.10	DC-163	1.10
AC-164	1.10	DC-164	1.10
AC-165	1.10	DC-165	1.10
AC-166	1.10	DC-166	1.10
AC-167	1.10	DC-167	1.10
AC-168	1.10	DC-168	1.10
AC-169	1.10	DC-169	1.10
AC-170	1.10	DC-170	1.10

Vu METER
Size 40x40x28mm

Type	Price	Type	Price
AC-171	1.10	DC-171	1.10
AC-172	1.10	DC-172	1.10
AC-173	1.10	DC-173	1.10
AC-174	1.10	DC-174	1.10
AC-175	1.10	DC-175	1.10
AC-176	1.10	DC-176	1.10
AC-177	1.10	DC-177	1.10
AC-178	1.10	DC-178	1.10
AC-179	1.10	DC-179	1.10
AC-180	1.10	DC-180	1.10
AC-181	1.10	DC-181	1.10
AC-182	1.10	DC-182	1.10
AC-183	1.10	DC-183	1.10
AC-184	1.10	DC-184	1.10
AC-185	1.10	DC-185	1.10
AC-186	1.10	DC-186	1.10
AC-187	1.10	DC-187	1.10
AC-188	1.10	DC-188	1.10
AC-189	1.10	DC-189	1.10
AC-190	1.10	DC-190	1.10

MINI-MULTI-METER
Size 80x24x29mm

Type	Price	Type	Price
AC-191	1.10	DC-191	1.10
AC-192	1.10	DC-192	1.10
AC-193	1.10	DC-193	1.10
AC-194	1.10	DC-194	1.10
AC-195	1.10	DC-195	1.10
AC-196	1.10	DC-196	1.10
AC-197	1.10	DC-197	1.10
AC-198	1.10	DC-198	1.10
AC-199	1.10	DC-199	1.10
AC-200	1.10	DC-200	1.10
AC-201	1.10	DC-201	1.10
AC-202	1.10	DC-202	1.10
AC-203	1.10	DC-203	1.10
AC-204	1.10	DC-204	1.10
AC-205	1.10	DC-205	1.10
AC-206	1.10	DC-206	1.10
AC-207	1.10	DC-207	1.10
AC-208	1.10	DC-208	1.10
AC-209	1.10	DC-209	1.10
AC-210	1.10	DC-210	1.10

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Type	Price	Type	Price
AC-211	1.10	DC-211	1.10
AC-212	1.10	DC-212	1.10
AC-213	1.10	DC-213	1.10
AC-214	1.10	DC-214	1.10
AC-215	1.10	DC-215	1.10
AC-216	1.10	DC-216	1.10
AC-217	1.10	DC-217	1.10
AC-218	1.10	DC-218	1.10
AC-219	1.10	DC-219	1.10
AC-220	1.10	DC-220	1.10
AC-221	1.10	DC-221	1.10
AC-222	1.10	DC-222	1.10
AC-223	1.10	DC-223	1.10
AC-224	1.10	DC-224	1.10
AC-225	1.10	DC-225	1.10
AC-226	1.10	DC-226	1.10
AC-227	1.10	DC-227	1.10
AC-228	1.10	DC-228	1.10
AC-229	1.10	DC-229	1.10
AC-230	1.10	DC-230	1.10

TRANSISTORS
BRAND NEW - FULLY GUARANTEED

Type	Price	Type	Price	Type	Price	Type	Price
AC-231	1.10	DC-231	1.10	AC-232	1.10	DC-232	1.10
AC-233	1.10	DC-233	1.10	AC-234	1.10	DC-234	1.10
AC-235	1.10	DC-235	1.10	AC-236	1.10	DC-236	1.10
AC-237	1.10	DC-237	1.10	AC-238	1.10	DC-238	1.10
AC-239	1.10	DC-239	1.10	AC-240	1.10	DC-240	1.10
AC-241	1.10	DC-241	1.10	AC-242	1.10	DC-242	1.10
AC-243	1.10	DC-243	1.10	AC-244	1.10	DC-244	1.10
AC-245	1.10	DC-245	1.10	AC-246	1.10	DC-246	1.10
AC-247	1.10	DC-247	1.10	AC-248	1.10	DC-248	1.10
AC-249	1.10	DC-249	1.10	AC-250	1.10	DC-250	1.10
AC-251	1.10	DC-251	1.10	AC-252	1.10	DC-252	1.10
AC-253	1.10	DC-253	1.10	AC-254	1.10	DC-254	1.10
AC-255	1.10	DC-255	1.10	AC-256	1.10	DC-256	1.10
AC-257	1.10	DC-257	1.10	AC-258	1.10	DC-258	1.10
AC-259	1.10	DC-259	1.10	AC-260	1.10	DC-260	1.10
AC-261	1.10	DC-261	1.10	AC-262	1.10	DC-262	1.10
AC-263	1.10	DC-263	1.10	AC-264	1.10	DC-264	1.10
AC-265	1.10	DC-265	1.10	AC-266	1.10	DC-266	1.10
AC-267	1.10	DC-267	1.10	AC-268	1.10	DC-268	1.10
AC-269	1.10	DC-269	1.10	AC-270	1.10	DC-270	1.10
AC-271	1.10	DC-271	1.10	AC-272	1.10	DC-272	1.10
AC-273	1.10	DC-273	1.10	AC-274	1.10	DC-274	1.10
AC-275	1.10	DC-275	1.10	AC-276	1.10	DC-276	1.10
AC-277	1.10	DC-277	1.10	AC-278	1.10	DC-278	1.10
AC-279	1.10	DC-279	1.10	AC-280	1.10	DC-280	1.10
AC-281	1.10	DC-281	1.10	AC-282	1.10	DC-282	1.10
AC-283	1.10	DC-283	1.10	AC-284	1.10	DC-284	1.10
AC-285	1.10	DC-285	1.10	AC-286	1.10	DC-286	1.10
AC-287	1.10	DC-287	1.10	AC-288	1.10	DC-288	1.10
AC-289	1.10	DC-289	1.10				

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The 450 Tuner provides instant program selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations any of which may be altered as often as you choose by simply changing the settings of the pre-set controls
Use with your existing audio equipment or with the BI-KIT'S STEREO 30 or the MK60 Kit etc. Alternatively the PS12 can be used if no suitable supply is available together with the Transformer T538.
The S450 is supplied fully built, tested and signed. The unit is easily installed using the simple instructions supplied.

- FET Input Stage
- VARI-CAP diode tuning
- Switched AFC
- Multi turn pre-sets
- LED Stereo Indicator

Typical Specification:
Sensitivity 3µ volts
Stereo separation 30db
Supply required 20-30V at 90 Ma max.



MPA 30

Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using the new M P A 30, a high quality pre-amplifier enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only. It is provided with a standard DIN input socket for ease of connection. Full instructions supplied.

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STEREO PRE-AMPLIFIER



PA 100 OUR PRICE £13.75

A top quality stereo pre-amplifier and tone control unit. The six push button selector switch provides a choice of inputs together with two really effective filters for high and low frequencies plus tape output.

MK 60 AUDIO KIT Comprising 2 x AL60's, 1 x SPM80, 1 x BTM50, 1 x PA100, 1 front panel and knobs, 1 kit of parts to include on/off switch neon indicator, stereo headphone sockets plus instruction booklet. **COMPLETE PRICE £36.00** plus 55p postage.

TEAK 60 AUDIO KIT Comprising Teak veneered cabinet size 16 1/2" x 11 1/2" x 3 1/4", other parts include aluminium chassis, heatsink and front panel bracket plus back panel and appropriate socket. **Kit PRICE £13.25** plus 85p postage.

- Frequency Response - 168 20Hz - 20KHz. Sensitivity of inputs:
1. Tape Input 100mV into 100K ohms
2. Radio Tuner 100mV into 100K ohms
3. Magnetic P U 3mV into 50K ohms
4. U input equalises to R1AA curve with 1dB from 20Hz to 20KHz
Supply - 70-35V at 20mA
Dimensions - 27mm x 89mm x 35mm

The AL30A is a high quality audio amplifier module replacing our AL20 & 30. The versatility of its design makes it ideal for record players, tape recorders, stereo amp, cassette and cartridge players. A power supply is available comprising a PS12 together with a transformer T538 also for stereo, the pre-amp PA12.

- SPECIFICATION**
- Output Power 10w R.M.S.
 - Load Impedance 8 to 16ohms
 - Sensitivity 100w for full output
 - Frequency Response 60Hz to 25KHz ± 2db
 - Supply 22 to 32 volts
 - Input Impedance 50K
 - Total Harmonic Distortion Less than 5% (Typically 2%)
 - Max Heat Sink Temp 80°C
 - Dimensions 90 x 64 x 27mm

ONLY £3.65



AL 60 25 Watts (RMS)

- Max Heat Sink temp 90C.
- Frequency response 20Hz to 100KHz
- Supply voltage 15-50V
- Thermal Feedback + Latest Design Improvements
- Load - 3,4,8, or 16 ohms
- Signal to noise ratio 80db
- Overall size 63mm x 105mm x 13mm.

Especially designed to a strict specification. Only the finest components have been used and the layout so state of the art, incorporated in this powerful 4 watt amplifier which should satisfy the most critical Hi-Fi enthusiasts.

£4.35

Stabilised Power Supply Type SPM80

SPM80 is especially designed to power 2 of the AL60 Amplifiers up to 15 Watts (R.M.S.) per channel simultaneously. With the addition of the Mains Transformer BMT80, the unit will provide outputs of up to 1.5A at 35V. Size 63mm x 105mm x 30mm. Incorporating short circuit protection.

Transformer BMT80
£5.40 + 86p postage

£3.75

Input voltage 15-20V A.C. Output voltage 22-30V D.C.
Output current 500mA Max. Size 60mm x 43mm x 28mm.
Transformer T538 £3.20

OUR PRICE
£1.30

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STEREO 30 COMPLETE AUDIO CHASSIS

7 + 7 WATTS
R.M.S.



P & P 45p
£16.25

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overvoltage will produce a high quality audio unit suitable for use with a wide range of inputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results this unit is supplied with full instructions, black front panel knobs, main switch, fuse and fuse holder and universal mounting brackets enabling it to be installed in a record player, cabinets of your own construction or the cabinet suitable for the beginner or the advanced constructor who requires Hi-Fi performance with a minimum of installation difficulty (can be installed in 30 mins).

TRANSFORMER £3.25 plus 50p p & p
TEAK CASE £5.45 plus 70p p & p

NEW PA12

Frequency Response 20Hz-20KHz (-3dB). Bass and Treble range, 12dB. Input Impedance 1 meg ohm. Input Sensitivity 300mV Supply requirements 24V 50ma. Size 152mm x 84mm x 32mm.

NEW PA12 Stereo Pre-Amplifier completely redesigned for use with AL30A Amplifier Modules. Features include on/off volume, Balance, Bass and Treble controls. Complete with tape output.

£6.70

PS12 Power supply for AL30A, PA12, SA450, etc

Input voltage 15-20V A.C. Output voltage 22-30V D.C.
Output current 500mA Max. Size 60mm x 43mm x 28mm.
Transformer T538 £3.20

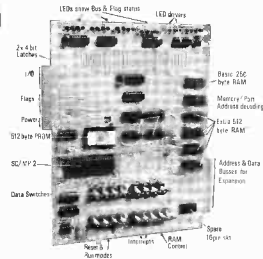
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Hemel Hempstead, HP3 9QR

CLOCK CHIPS & KITS

TYPE	SPECIAL FEATURES	£CHIP	£KIT
MM5309 7 seg	+ BCD RESET ZERO	8.53	12.50
MM5311 7 seg	+ BCD	4.26	8.00
MM5312 7 seg	+ BCD 4 DIGIT ONLY	4.26	8.00
MM5313 7 seg	+ BCD	6.50	
MM5314 7 seg	+ BASIC CLOCK	4.26	7.00
MM5315 7 seg	+ BCD RESET ZERO	6.50	9.00
MM5316 Non-mpu ALARM		7.50	8.00
MM5318 7 seg	+ SCD External digit select	12.19	
MM5371 ALARM	50 Hz	9.86	14.00
MM5378 CAR Clock	Crystal control LED	9.86	
MM5379 CAR Clock	Crystal control Gas discharge	5.60	9.00
MK5025 ALARM	SNOOZE	12.10	15.10
MK5039S UP	DOWN Counter — 8 Decade	9.00	12.50
MK5039S UP	DOWN Counter — HMMSS	12.10	15.10
MK5039T UP	DOWN Counter — MMSS 99	9.00	12.50
FCM7001 ALARM	SNZ CALENDAR 7 seg	9.00	
FCM7002 ALARM	SNZ CALENDAR BCD	9.00	
CT7003 ALARM	SNZ CALENDAR Gas discharge	9.00	
FCM7004 ALARM	SNZ CALENDAR 7 seg	9.00	12.50
AY5 1202 7 seg	4 digit	4.76	
AY5 1230 7 seg	ON and OFF ALARM	5.25	TBA

All above clock kits include clock PC board, clock chip, socket and CA3081 driver IC. MH15378 also includes crystal and trimmers. When ordering kit, please use prefix MHI, e.g. MHI 5309.

DISPLAYS

DL707, 704, 701 0 3"	1.70	Litronix class 2 product	
DL727, 728 721 0 5 1/2" (2 dig)	0.70	DL707E	0.85
	4.31	DL727E (2 dig)	2.00
DL747, 750, 746 0 6"	2.82	DL747E	1.80

MHI DISPLAY KITS

MHI707/4 digit 0 3"	7.60	MHI707E/4	4.30
MHI707/6	11.00	MHI707E/6	5.70
MHI727/4 0 5 1/2"	9.70	MHI727E/4	5.30
MHI727/6	13.80	MHI727E/6	7.20
MHI747/4 0 6"	11.40	MHI747E/4	7.20
MHI747/6	17.30	MHI747E/6	9.90

Any one or two of the above MHI display kits will interface directly with any of the MHI clock kits

CASES (with perspex screen)

VERO 1 8" x 5 1/2" x 3 1/2"	3.00	24 28 or 40 pin	0.60
VERO 2 6" x 3 1/4" x 2 1/4"	3.00	Soldercon strip kits 50 pins	0.30

SOCKETS

24 28 or 40 pin	0.60
Soldercon strip kits 50 pins	0.30

BITS & BYTES

74C00 Quad NAND	0.25	MM2102 2 1Kx1 RAM	2.11
74C04 Hex Inverter	0.25	MM2112 2 256x4 RAM	3.08
74C10 Triple NAND	0.25	MM74C920 256x4 CMOS RAM	
74C42 BCD Decoder	0.95		11.83
74C157 Quad Selector	2.25	XX2114 1Kx4 RAM	24.00
74C163 4 bit counter	1.15	MM17020 256x8 EPROM	11.90
74C164 PISO register	1.15	MM52040 512x8 EPROM	10.95
74C165 SIPO register	1.15	MM2708Q 1024x8 EPROM	31.15
74C173 3S Quad latch	0.95	EPROM prices for blank devices	
74LS139 Dual 2 4 Dec	1.50	ER3401 1024 x 4 EAPROM	28.85
DM8095 3S Hex buffer	1.75	MM5307AA Baud Rate Gen	12.68
DM8096 inv 8095	1.75	MM5303 (AY-5-1013) UART	6.34
DM811595 3S 6 bit buff	1.45	Xtal for 5307	TBA
DM81339 Dual 2 4 Dec	1.45	DM8578 Char Gen	15.20
DM81597 3S 4-3 buffer	1.45	(both CAB & BVFF avail.)	
DM81598 Inv 97	1.45		

CLOCK MODULES

LT601 Alarm Clock Module similar to MA1002	6.00
MTX1001 Transformer	0.25

OLDE CLOCKS

In kit form or built these clocks are based on designs hundreds of years old. Wood, stone and iron are used to reproduce authentic "olde worlde" wall clocks in full detail. The kits contain all you need including glass, screws etc. and very comprehensive instructions. Stones for weights are excluded. For coloured brochure please send 15p stamps

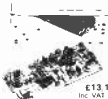
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HF 7948 FRONT END



£13.12
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TECHNICAL CHARACTERISTICS

Output terminal for digital frequency meter
Antenna impedance: 75 to 300 Ohms
Frequency ranges 87.5 to 104 MHz or to 108 MHz
Sensitivity 0.9 μ V 26dB signal to noise ratio \sim 75 kHz deviation Intermodulation 80dB Image rejection 60dB Tuning voltage 1V to 11V Total gain 33dB Intermediate frequency 10.7 MHz Power supply voltage +15V Power consumption 15mA Dimensions 104 x 50 mm

TECHNOLOGY

Double sided epoxy printed circuit board with plated through holes Dual gate effect transistors Silvered coils

FI 2846 IF AMP AND DECODER



£9.86
Inc VAT P&P

TECHNICAL CHARACTERISTICS

Intermediate frequency 10.7 MHz IF Bandwidth 280kHz Signal to noise ratio 70dB with 1mV input Distortion mono 0.1% stereo 0.3% Sensitivity 30 μ V up to the 3dB limit Channel separation 40dB at 1kHz Pass band 20 to 15 000Hz Rejection at 38 kHz greater than 55dB Am rejection 45dB De emphasis 50 to 75 μ s Pilot capture at 18kHz \pm 4% Channel matching within less than 0.3dB Output impedance 100 Ohms Output voltage 500mV Phase locked loop stereo decoder Output for LED VU meter Null indicator Outputs for AGC AFC and inter station muting Consumption 55mA LEDs extinguished 100mA LEDs illuminated Power supply 15V Dimens ons 195 x 76mm

CIRCUIT TECHNOLOGY

Epoxy printed circuit board Monolitic integrated circuits ceramic filter

ALS 1500 STABILISED POWER SUPPLY



£2.53
Inc VAT P&P

TECHNICAL CHARACTERISTICS

Output voltage 15V Max output current 500mA Thermal coefficient less than 1mV/C 15V power supply for modules HF 7948 and FI 2846 Supply protected against short circuit (power and current protection) Dimensions 65 x 55mm

TECHNOLOGY

Double sided epoxy circuit board Monolithic integrated circuit

OPTOELECTRONIC OPTIONS

£8.06
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LED VU-METER

Station strength indicator



£13.50
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ILLUMINATED POINTER

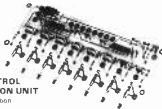
Station finder



£22.74
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FREQUENCY METER

Digital display of received station frequency



£8.77
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TOUCH CONTROL PRE-SELECTION UNIT

LED channel indicator



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KIT PRICE
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- Instantaneous Switching from 12/24 hour display



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Model 102

- Large red digits
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- 9min repetition
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COMPLETE KIT
£13.43
+ £1.07 VAT

Model 103

DIGITAL CAR CLOCK

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Swiss made 100% quartz case

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SITES

All games have superb plastic case. Are fully guaranteed and are beautifully packed in a presentation carton.
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Metac-Electronics & Time Centre

... news digest ...



Awajiya has become the third Japanese hi-fi company to open showrooms in London. The new premises are at 56-58 Brunswick Centre, just off Russell Square, which itself is quite close to Tottenham Court Road (just turn right at 11 o'clock and keep going straight) and right into Russell Square.

The idea of such a place is to allow people to inspect the goods without the usual hi-fi shop hand sale. Sony started the idea in Regent Street some time ago, but to get a place like this, of Awajiya on Regent Street would cost a fortune. It is massive! Certainly worth a look around if you are wandering the length of Tottenham Court Road in search of some hi-fi. In addition to

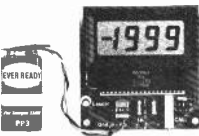
displaying the entire range, the showroom sells the specialised Awajiya accessories which might not be available elsewhere.

Also from Awajiya is the brand new cassette deck which to us represents the endstop (at present!) in cassette technology. The machine is designed for the 4000Hz and can be adjusted to obtain the optimum from any brand of tape, by the way within 10 seconds! Sample procedures align the heads and set the bias via a special test head. The machine is far too complex to describe here, so, looking at it in more detail elsewhere, is this issue? Awajiya Sales and Service, Brunswick Centre, Bloomsbury, London WC1.

A new hand-operated coaxial cable stripper has been introduced by AB Engineering Company under the model number COAX 1. Simple hand pressure ensures accurate stripping of television and communications and other coaxial cables up to 7.5 mm diameter. The

tool incorporates four apertures offset to a common cutting blade which provide Aperture one—Strips to outer insulation Aperture two—cuts through the sheath and strips the insulation leaving a 7 mm or 12 mm length Aperture three—strips the dielectric Aperture four—cuts through the cable.

Further details may be obtained from AB Engineering Company, Apem works, St Albans Road, Watford, Herts.



Linear Electronics have introduced a 3½ digit DPM (with 0.5 digit crystal display) the new meters have the features of auto polarity into zero, 0.1% accuracy, etc. Available with an I.S.D. of 999 mV or 1999 mV. The new 15000 ohms input from a single supply—can be used at 5.12 V D.C. The low power consuming from 1750 fully 1 mA current drain) makes them ideal for use in portable instruments.

It is claimed that a PP3 battery would last several months operation in normal use.

Calibration is set by an on board 120 ohm preset with over range input indicated by suppression of the last three digits. Programmable L.H. display mode and input impedance switch) than 10 Ohms. Levels are also available.

Linear Electronics Limited, P.O. Box 12, Module House, Billingsley, Essex CM12 9QA.

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...news

The first Commodore TV game is titled TV 3000H and can be played by up to four players. The usual four games are available:

- Football (Two or four players),
- Tennis (Two or four players),
- Squash (Solo or two players),

and Target Shooting

Other Features

On Screen Scoring shows the score after every point and three realistic sounds help to add realism to the game. (To save battery costs a mains adaptor is provided, included in the price)

The game is colour and auto speed up of the ball is also included. The TV 3000H is covered by a one-year guarantee and is available at a RRP of £39.95 (including VAT and adaptor). A price which can be assembled into a rink for use with two large games is available as an optional extra at £12.95 (including VAT). Commodore Business Machines (UK) Ltd, 446 Bath Road, Slough, Berks SL1 6BB.

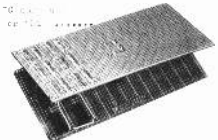
...news

A new Passive Infra Red Intruder Detector is now available from Photon. The unit consists of a solid state passive infrared sensor which views an area through a seven facet optical system. When the sensor detects an infrared emission (see the human body) passing across the optical system a relay system is activated to trigger any type of alarm system. Two conditions must be satisfied with before the relay operation takes place: the heat emission and movement; and therefore false alarms will not occur from static hot bodies such as radi-

ator electric fires etc.

The unit is normally fitted on a wall some 3 metres above ground level (the area of coverage is up to a distance of 12 metres).

The main use for the device is to protect specific high risk areas of a building and as the unit does not emit any signal (such as ultrasonic or microwave detectors do) it can be used in areas with large glass surfaces or light-tight partitions without suffering problems. Photon Controls Ltd, Unit 18 Hanger no. 3, The Astro Dome, Ford, Ayrshire, W. Sussex.



A new circuit board, designed for the book, which has been introduced by Vero Electronics Limited, designated V-Q (Vero Quad).

Primary design considerations were to produce an economical board capable of accepting any component, but especially integrated circuits — regardless of pin spacing. V-Q has a 0.1" matrix and a layout sheet with a 1" grid of the copper pattern is packed with every board. Up to twenty one 14 or 16 pin IC's can be accommodated on the board, which measures 147 mm (5 1/2 x 73 mm (2 9/16").

The order code for V-Q is 01-0044C and it is available from retail shops and mail order houses at around £0.90. Vero Electronics Limited, Retail Dept, Industrial Estate, Chandler's Ford, Hampshire, SO5 3ZR.

digest...



Drop in or

An initial release of funds totalling £374 million for the full development of the initial ECS (European Communications Satellite) has been made by the European Space Agency.

ECS will be a fully operational European regional satellite communications system and will be capable of carrying out an efficient proportion of future European telephone, telex and TV traffic. The first ECS will be placed in geostationary orbit in 1983 by the European Ariane launcher and it is planned that this should be followed by three more between then and 1990. The launches will be made from the equatorial site at Kourou in French Guiana. M.K. Ltd (now known as Spideley Dynamics Ltd, Manor Road Hatfield Herts



.....

We have just received our copy of Watford Electronics latest stock list. It's not really as extensive but it is very comprehensive and would certainly have covered us with what we've had to do elsewhere.

Active component stock is particularly good and the prices near competition with the best. Watford are working on a 20 per cent discount which will be in and soon apparently. In the meantime, the stock list makes a very useful addition to the 2000.

Watford Electronics, 33C (old) Road, Watford, Herts.

THE DYNAMIC DUO



The C15/15 is a unique Power Amplifier providing Stereo 15 watts per channel or 30 watts Mono and can be used with any car radio or tape unit. It is simply wired in series with the existing speaking leads and in conjunction with our speakers S15 produces a system of incredible performance.

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...news



Staff Vacancies

ELECTRONICS TECHNICIAN

We need someone for the ETI Project Team. Applicants must be capable of and enjoy firstly hand building prototypes from supplied circuits and then converting the proved circuit into a well built prototype.

Skills necessary are a good standard of workmanship, a high electronic and mechanical aptitude and examples of previous work must be available for examination. Ability to design PCB layouts would be an advantage though limited experience in this area should not preclude candidates from applying.

The majority of the work is in building up but it will be necessary to co-operate with the other editorial staff both with design and with the paper-work needed to produce the project in the magazine.

The job is in our workshop at our Oxford Street premises. Salary will depend upon skills and experience but will be in the range £2,800 absolute minimum to £3,000 for someone bringing additional skills to the team.

EDITORIAL ASSISTANT FOR ETI AUSTRALIA

An additional staff member is needed in Sydney Australia to work on ETI OZ. This position is only being advertised here at

digest....

„Irad“ in Germany.....

A new edition of ETI starts this month — Elrad in Germany. The name Elrad itself means nothing and is simply an amalgamation of electronics and radio. It is being published by Heinz Hesse in Hanover and is edited by Udo Wittig shown with pipe in the photograph examining a publicity leaflet with the advertising and production managers.

Following German tradition, the first issue is number zero and given away. This came out in November and the front cover is shown on the left.



with ETI

at this stage so we are serious about seeking applicants.

We are seeking a young person — probably under 25 — who is genuinely interested in electronics. We are not specifically seeking someone with journalistic experience as this is far easier learnt than for a journalist to learn electronics. The work is extremely varied but much of the work is preparing the work of others for the magazine so some writing is also involved. Formal qualifications in electronics are not as important as interest in the field.

Initially the successful applicant will work on the British editor for initiation and work experience. After a set factory trial period, the successful applicant will go to Sydney. It is a permanent position. A stipend is a long wage similar to English money and only other relevant formal qualifications in Australia are considered higher than those prevalent in the UK.

For more particulars apply in writing to Hulver Mudgehead, Editor, ETI Magazine, 75/77 Oxford Street, London, W1R 1RF, giving details of education, knowledge, experience, age, marital status and any other relevant formal qualifications. Applications should reach us as soon as possible. Interviews will be held in London in early January.

ETIPRINTS

Yes folks, it's you the readers at home whose vote really counts (we mean that most sincerely) and your vote is that ETIPRINTS should become a regular part of our readers' services. The response to ETIPRINTS 001 has been overwhelming so that we have decided to make this new method of PCB production a regular ETI feature.

In case you have missed out on ETIPRINTS thus far, they are a complete PCB pattern already to rub down in seconds. The patterns are produced from our original artwork so that the results they produce are nice and sharp.

We think that ETIPRINTS are such a good idea that we have patented the system (Patent numbers 1445171 and 1445172).

Until now the only ETIPRINT available has been 001 but this month we publish two further sheets 002 and 003 featuring projects from this and last month's issues.

Details of ordering the ETIPRINTS are shown below.



Let down the ETIPRINT and rub over with a soft pencil until the pattern is transferred to the board. Peel off the backing sheet carefully making sure that the resin has transferred. If you've been a bit careless there's even a repair kit on the sheet to correct any breaks!

ORDER TODAY

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ETI MAGAZINE,
25/27, OXFORD STREET, LONDON, W1R 1RF

75p

 Inc. VAT and P & P

Please indicate clearly the ETI PRINTS you require. Those available at present are:

- 001 With patterns for spirit clock board A and the compander from Nov 77 plus the spirit level three channel tone control and the digital thermometer from Oct 77.
- 002 With patterns for hammer throw and race track from Jun 78 plus the freeracer alarm from Dec 77.
- 003 With patterns for the burglar alarm from Jan 78 plus clock board B and the tee monitor from Dec 77.

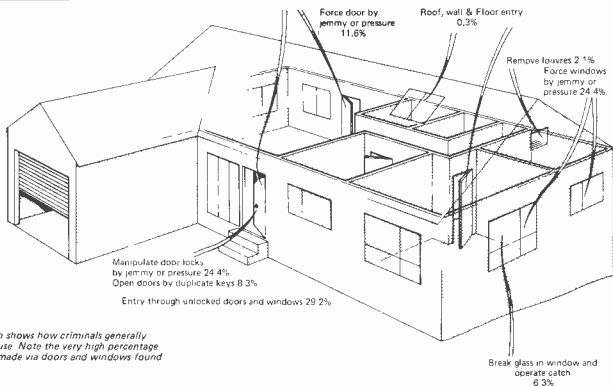


Fig 2

This sketch shows how criminals generally enter a house. Note the very high percentage of entries made via doors and windows found unlocked.

Vibration sensors may be used to protect large areas of glass but these are prone to false triggering during thunderstorms etc.

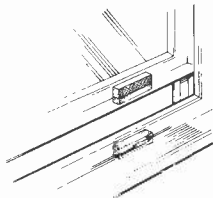
Many other types of intruder sensing devices may also be included in the system. Pressure mats for example can be placed under carpets in strategic passageways — or even under the door mat. The mats contain a large number of normally open contacts some of which will be closed when the mat is trodden on. The system can also include more sophisticated intruder detectors such as infra-red type sensors.

The intruder alarm itself should be reasonably accessible to people entering and leaving the premises via a silent entry door but will be hidden from the sight of an intruder. The alarm's output stage should be a relay which latches when an alarm signal is received.

Warning Devices

For household use a good quality 12 Volt bell should prove an adequate warning device. Being mechanically resonant, bells have a very high conversion efficiency.

Fig 3 Set the reed switch into the window frame and the magnet into the moving part



in fact, the average bell draws less than 500 mA at 12 V yet can be heard several hundred metres away.

Good sirens can be heard well over a few kilometres away but they draw a lot of current and cost more than a good bell. Small cheap sirens cannot be recommended.

If at all possible, householders should make mutual arrangements with neighbours to contact the police if the alarm is heard. Similar arrangements should also be made so that neighbours can switch off the alarm when the police arrive.

An alarm which resets after a period of time silencing the bell or siren, is a useful device that will be much appreciated by the neighbours. Care must be taken to ensure however that the alarm when triggered and reset still provides some measure of protection to the property.

Whatever the warning device chosen, it should be mounted unobtrusively high up in an inaccessible place. The leads to the device should be of an adequate gauge to avoid any voltage drop associated with a long

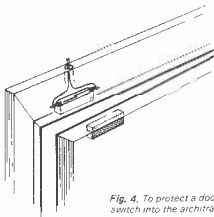


Fig 4. To protect a door set the reed switch into the architrave

HOUSE ALARM

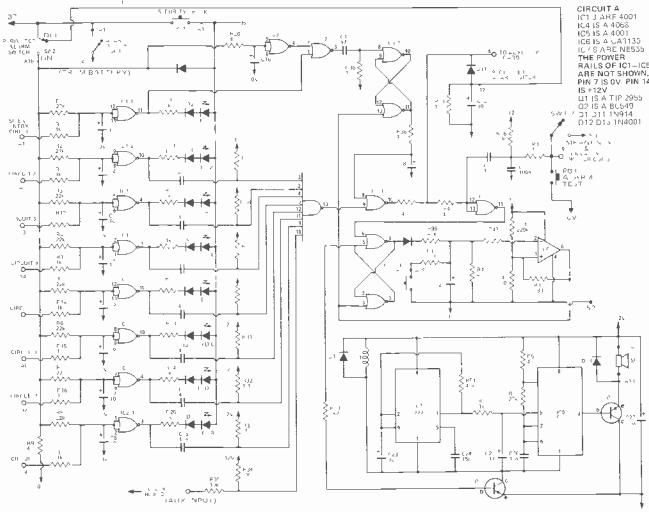


Fig 5 Circuit diagram of the A board

run. The wires should be concealed from view. We strongly recommend that a separate 12 V battery be used in any burglar alarm. This should be checked at regular intervals to ensure it is still in good condition and should be replaced as a matter of course when it has been in service for a period of one year.

Alarm Unit

The specification of our alarm unit is shown in Table 1. From this one can see that the alarm has seven 'normally closed' circuits (A2-AB) plus a silent entry circuit (A1) which allows about 30 seconds on entry to turn the alarm off. This feature also gives a 30 second delay between turning the alarm on and the sensors being armed, this allows time to leave the house.

It is possible to connect two or more alarm switches in series for each external circuit but if so doing ensure that any such series-connected switches are grouped together.

The reason for providing a number of separate alarm circuits is to do with the problems involved with resetting a triggered alarm mentioned above. Most alarms work on a system where all the windows and doors have normally closed reed switches all wired in series so that opening any one breaks the loop and sets the alarm off. The alarm then rings for ten minutes and

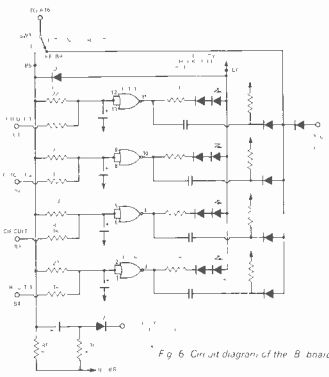


Fig 6 Circuit diagram of the B board

HOW IT WORKS

UNLIKE SOME ALARMS that use a single sensing loop with all the switches wired in series, this design features a number of different alarm groups. These are broken down into two groups designed for normally closed (N.C.) switches — Perimeter Group (inputs A₁-B₁) and Internal Group (inputs B₂-B_m) — together with one group for normally open (N.O.) switches (inputs to A₂).

The inputs to each of the circuits described above have their own input circuitry.

PERIMETER CIRCUIT

The normally closed sensors associated with the perimeter circuit (inputs to A₁-A₂) are connected to the circuitry around IC₁ and IC₂.

These ICs are Quad NOR gates which, in this application, are configured as inverters. The sensors are connected to the inputs of these gates via the resistors R₁₀/R₁₁. With the sensor switch closed the output of the associated IC will be high. If the switch is opened the output will go low as the inputs to the gates are then tied high via resistors R₁₂-R₁₄. R₁₅ is included to ensure that the inputs to the CMOS ICs are terminated under all conditions. The capacitors C₁-C₃, together with the resistors R₁₀/R₁₁, provide a filter to ensure that transients on the input lines do not trigger the alarm.

In each output of IC₁ and IC₂, there is a LED which is connected to the Security Check Button (PB₁). Upon operation of this button power is supplied to the LEDs which will light if the IC they are connected to has a low output, i.e. the input is triggered. The diodes in series with the LEDs are necessary because of the low reverse voltage breakdown of the LEDs. Diode D₁ supplies power to the input circuitry during the security check. The input A₁ provides the silent entry feature and is described below.

The other sections A₂-A₄ have their outputs fed via an RC network, which generates a negative pulse upon triggering, to one of the inputs of IC₃. Thus if any of the inputs are triggered a positive pulse at the output of IC₃ will result.

SILENT ENTRY CIRCUIT

With the silent entry circuit a 30 second delay due to R₂₀, C₁₀, and IC₄ overrides the output of IC₂ immediately after the alarm has been energised. After this time if the input is triggered the output of IC₃ will go high having been inhibited from doing so until now by the high output of IC₄, and will toggle the RS flip flop formed by IC₅ and IC₆, taking the output of IC₃ high. After another 30 second delay due to R₁₆, C₂, the input to IC₃ will be high and its output low.

TRIGGERING CIRCUIT

The same output results if one of the other inputs is triggered and the output of IC₃ goes high momentarily.

This output is used to toggle, via IC₇, the RS flip flop formed by IC₅, which is used to control the alarm and resetting circuitry described below.

IC₇ also has two other inputs. The first, consisting of the network R₁₇, C₃, and D₁. This circuitry disables the alarm function when the Perimeter Switch is in the off position and for a short period of time after the switch is moved to the on position by holding the input of IC₇ high. This prevents spurious triggering.

The second input to IC₇ is from the normally open input (A₂), as well as the emergency and alarm test switches. If any of these switches are taken low a negative going pulse is coupled to IC₇ to trigger the alarm. These functions operate even if the perimeter sensors are off. This input can be

used for emergency inputs such as fire alarms.

OUTPUT

The positive going pulse at the output of IC₃ sets the RS flip flop IC₅, IC₆, and in this triggered state IC₅ output is low and IC₆ is high.

The delay circuitry uses a CA3130 (IC₈) configured as a comparator. IC₈ is normally charged to +10V until the flip flop is triggered allowing it to discharge via R₂₁. When the voltage on C₁₁ has fallen to about 20mV (the level set by R₂₂ and R₂₃ on the non-inverting input of IC₈) the output of the IC will go high resetting the flip flops formed by IC₅, IC₆, and IC₇. IC₈ R₂₄ is included in the feedback loop to provide some hysteresis.

The output device can either be a relay or siren circuit. We have provided for both options. The siren output is formed by two 3535 one operating at a high frequency and driving the speaker via driver transistor Q₁ and the other at about 2Hz which is used to modulate the frequency of the first.

The relay and 3555s are energised when Q₁ is turned on by the high output of IC₅, as the flip flop is set.

Addition circuits can be added in blocks of four at a time (as Board B) and connected to the Aux input.

AUXILIARY BOARD

The circuitry of board B is almost identical to that of Board A. The main difference is that the negative going outputs of each IC are ORED using diodes D₂-D₄ as opposed to a logic gate.

This board can only be energised if the perimeter board is powered up. The capacitor C₁ together with R₁₀ and D₂ provide a short positive going pulse upon switch on to disable the main alarm for a brief period of time.

resets. If, however, the window, as is likely, is still open, the alarm must be turned off completely to prevent it continuing to ring.

This is the reason that our alarm does not use a single loop but has a number of alarm groups. Further, the alarm is triggered only by a change of state in any of its alarm loops. Thus if the alarm is triggered by the change of state in any of its sensing loops when a window, say, is open it will not be retriggered when after a period of time it resets and the window is still open. This affords some protection to the premises under these conditions.

We have provided a test button so that a check on the security of the house can be made before the alarm is set, indicating immediately which window or door is open.

As well as the external circuits the system has provision for connecting a number of internal circuits. These may be actuated by normally closed switches — or which case they should be connected to B1-B4 — or by normally open sensors connected to A9.

It may well be worth considering installing a series of emergency push buttons. Such switches should be mounted on the architraves of the front and rear doors or in a readily accessible position near the doors. They enable the occupant to set off the alarm if a caller forces his way into the house when the door is opened.

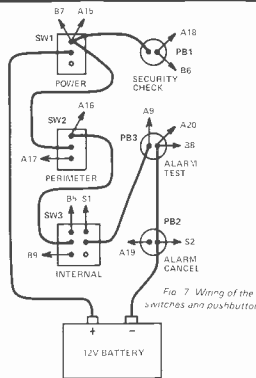
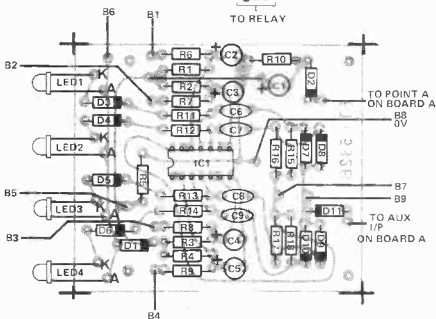
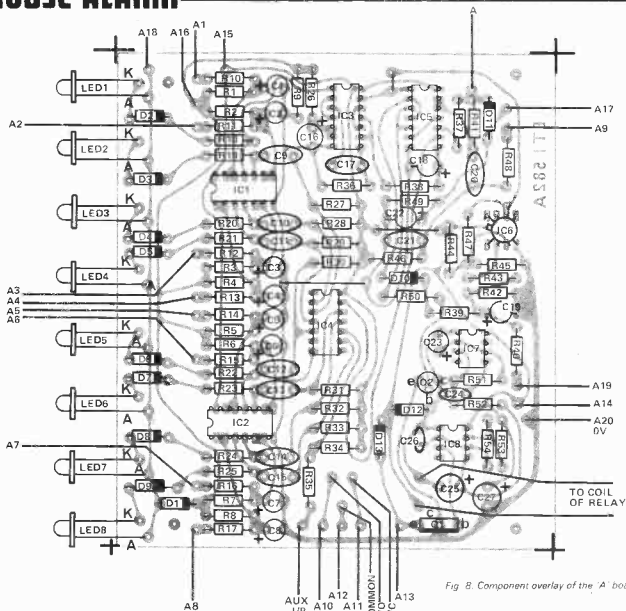


Fig. 7. Wiring of the switches and pushbuttons.

HOUSE ALARM



Although this is not a common event, emergency switches provide elderly or timid people with a feeling of security.

Use good quality bell pushes for these circuits and connect them to the A9 inputs on the circuit board.

Fire Alarms

Fire sensors may be wired across the A9 input. The actual fire sensors should be mounted in the ceilings of rooms in which there is a fire hazard — kitchen, living room, rooms with electrical or heating appliances or where people smoke (don't forget the bedroom if you've a habit of smoking in bed!). Sensors should also be installed in the roof of the garage especially if this is attached to the house — the laundry, workshop etc.

Construction

Due to the number of components, it is recommended that the unit should only be built using the PCBs shown here.

Assemble the components, watching the connection of all the polarised components. Also solder the CMOS ICs last and then solder pins 7 and 14 first. This allows the protection diodes inside the IC to be effective. The LEDs should be mounted parallel to the PCB as shown in the overlay as these have to protrude through holes in the chassis.

Boxing of the alarm unit is largely a matter of choice. Our layout can be seen in the photographs. Note that we did not fit a key switch to our alarm, but installed it in a locked cupboard which could also be used for the storage of valuables.

Security Sense

May we say again that the installation of an alarm should only be part of a co-ordinated campaign to dissuade burglars. Details of the various precautions that can be taken were detailed in our feature last March. Your local Crime Prevention Officer will also be prepared to give help on most matters of security.

ETI

PARTS LIST

BOARD A RESISTORS all 1/2 W 5%

R1-8,54	22k
R9,37,39,41,46,51,53	47k
R10,25,48,52	1k
R26,38,42	4M7
R27-34,36,43,49	1M
R35	10k
R40	100R
R44	220k
R45,47	680R
R50	2k2

CAPACITORS

C1	33u 16 V electrolytic
C2-5	10u 16 V tantalum
C6-9	47n polyester

SEMICONDUCTORS

IC1	CD 4001
D1-11	1N914
LED1-4	.2" type LED

MISCELLANEOUS PCB as pattern.

GENERAL FOR BOARDS A & B, SWITCHES

SW1	SPST toggle switch
SW2	SPDT toggle switch
SW3	DPDT toggle switch
PB1-3	single pole press to make push type.

MISCELLANEOUS

Case to suit, 12 V battery (HP1 or 2 X 991) terminal strip.

CAPACITORS

C1-8,16,18,22,23	10u 16 V tantalum
C9,15,17	47n polyester
C19	22u 16 V tantalum
C20,21	100n polyester
C24,26	15n polyester
C25,27	100u 16 V

SEMICONDUCTORS

IC1,3,5	CD 4001
IC4	CD 4068
IC6	CA 3130
IC7,8	555
LED1-8	.2" type LED
Q1	TIP 2955
Q2	8C109
D1-11	1N914
D12,13	1N4001

MISCELLANEOUS

PCB as pattern, 12 V 1B5R relay.

BOARD B

RESISTORS all 1/2 W 5%

R1,4	22k
R5,10	47k
R6,9,11,14	1k
R10	47k
R15-18	1M

SPECIFICATIONS

Types Of Inputs

Silent entry
Perimeter circuits
Internal circuits
Emergency circuits

Silent Entry

Single circuit,
30 s exit delay,
30 s entry delay.

Perimeter Circuits

7 circuits, N/C contacts,
can be expanded in units of 4.

Internal Circuits

4 circuits, N/C contacts,
can be expanded in units of 4,
Any number of N/O circuits.

Emergency Circuits

Any number of N/O circuits.
These circuits are active even if perimeter and internal circuits are switched off.

Current Drain And Battery Life (Type HP1 or similar)

Emergency only	2.5 mA (4000 hours)
Alarm active	9 mA (2000 hours)
Alarm sounding	500 mA (10 hours)

Alarm Time

12 minutes.

HOUSE ALARM

BUY LINES

The components for this project should be available from most suppliers Watford, Marshalls Maplin etc., or, probably, from most local shops. The Siren used is a matter of choice but please make sure it's up to the job.

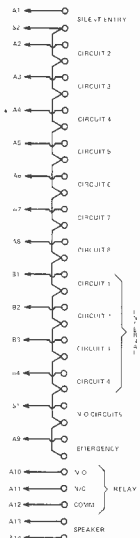


Fig 10 Connection of the rear terminal block

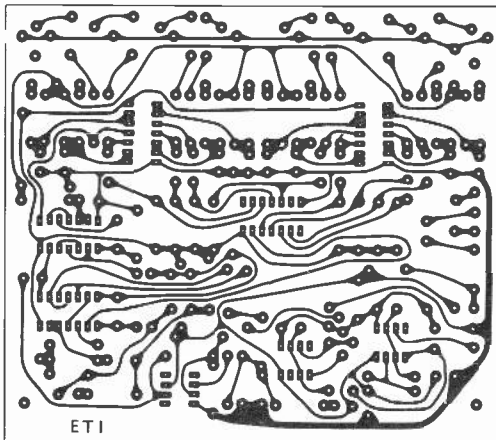


Fig 11 PCB foil pattern of A board shown full size (130 x 115mm)

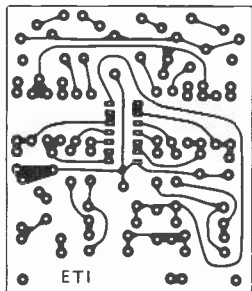
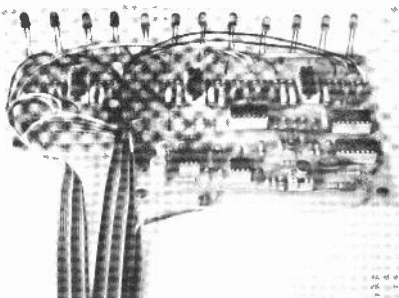


Fig 12 PCB foil pattern of B board shown full size (75 x 65mm)



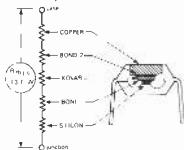
SOC20.



The most powerful Monolithic IC amplifier in the world.

20 watts output (continuous sine wave) . . .
Less than 0.2% total harmonic distortion at *all* powers,
all frequencies . . .
And totally electronically indestructible!

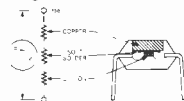
Until recently, all monolithic IC chips suffered from two basic design weaknesses. First, thermal runaway causing heat to build up as current increased, and second, short circuiting.



Standard plastic package with copper slug

Until the SOC20 IC chip! This extraordinary new power amplifier chip is uniquely designed to improve thermal dissipation. It also has two separate built-in circuits, one of which measures on-chip temperature. If this should rise above 150°C the output transistors are switched off thus preventing thermal runaway.

And short circuits? The other circuit continuously monitors both current and voltage. If the product of current and voltage rises above a critical level, the



SOC20 plastic package with chip directly soft soldered to copper slug

drive is adjusted to bring the transistors within safe operating limits.

The amplifier can drive speakers of any impedance – maximum power will only fall outside the recommended 4 Ω – 8 Ω range.

And *any* pin on the chip may be shorted to *any* voltage in the system for *any* length of time – and *no* damage will occur!

Superb quality . . . extraordinary power

The SOC20 isn't only safe – it's also extraordinarily sophisticated. Total harmonic distortion is less than 0.2% at all powers and all frequencies – and in normal use is well below 0.1%.

If power is at a premium, use two SOC20 amplifiers in 'Full Bridge' to give over 40 watts continuous into 8 Ω speakers.

The SOC20 is naturally guaranteed unconditionally for one year. Although with the SOC20's unique patented design, we think you'll have little cause to make use of any guarantee!

Specification

Maximum supply voltage
 ± 22 V (44 V total)
Output power
20 watts continuous 4 Ω or 8 Ω
Open loop gain
100 dB
Supply voltage rejection
50 dB
Input noise voltage
4 nV
Number of transistors
18

Supplied with free printed circuit board, heat sink mounting bracket, comprehensive instructions, and suggested applications.

The SOC20 will work on any supply from 12–44 volts and therefore can be used for in-car as well as domestic applications. Apart from its obvious audio uses the fact that it is DC coupled throughout makes it ideally suited for servo systems – in radio-controlled models for example.

Incorporate the SOC20 in your equipment today!

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Please send me _____ (qty)
SOC20 Monolithic IC Amplifiers
(£4.95 each or £7.95 per pair,
inclusive of p&p and VAT at 8%)

I enclose cheque/money order/
postal order for £ _____

Name _____

Address _____

(PLEASE PRINT)

ETI

TRANSFORMERS

Panel Meters, Bridge Rectifiers, Power Supply Units
Multimeters - Semi Conductors - Timers - Safeloc

Miniature & Sub Miniature

Volts	Mills-amps	Ref No.	£	P&P
1	20	4	1.85	70
1.5	1A	212	2.60	85
50/4	10	13	1.85	43
C 2419	600/33	23E	1.95	70
C 69 C 89	50/500	47	2.35	51
7F 40 4 4	1A	208	3.50	55
50/12	200/200	24E	1.95	42
7F 2 2	300/300	214	2.35	70
20/12	700/DC	21	3.10	40
0-15/20	5/20	18	2.06	4.20
0.15/27	5/2	205	2.65	70
0.15/27	5/2	205	2.65	70
0.15/27	5/2	205	2.65	70

12 AND/OR 24 VOLT

Pin 220 240 volts

Amps	Price	£	P&P
1.5	0.25	1.11	1.95
2	0.5	2.13	2.30
4	2	3.75	74
6	3	7.0	85
8	4	10.8	6.25
10	5	12	8.95
12	6	16	7.85
15	8	17	8.25
20	0	11	12.75
30	2	8	16.80
60	30	27.6	22.90

30 VOLT Pin 220 240V

See 0 12 15 20 24 30.

Amps	Ref No.	£	P&P
1.5	112	2.45	70
1.5	79	3.09	70
2	3	4.80	85
3	20	5.80	110
4	21	6.85	110
5	51	7.75	100
8	17	9.90	100
15	48	11.36	130
10	39	12.00	130

CATALOGUE 30

Please add .AT 3 P 8

Buy direct and see facilities

available

Trade and Location A/E/eng

50 VOLT Pin 220 240V

See 0 15 20 24 40 50V

Amps	Ref No.	£	P&P
2.5	102	3.20	70
0	103	4.20	85
7.0	104	6.10	100
4	105	7.85	100
1	106	8.60	110
1.5	107	14.95	130
8.0	108	16.75	150
10.0	119	20.50	150

50 VOLT Pin 220 240V

See 0 24 30 40 18 80V

Amps	Ref No.	Price	P&P
3	24	3.40	70
1.0	126	4.65	85
4.0	127	6.50	100
4.0	128	8.15	110
4.0	123	11.25	130
5.0	40	11.80	130
8.0	120	14.75	140

AUTO TRANSFORMERS

Pin 1 Pin 2 Tap 0.115 210 40V

VA	Ref No.	£	P&P
20	113	2.25	70
15	4	3.50	70
15	4	5.25	85
15	4	10.00	110
0.15 210 220 240			
40	14	7.15	70
50	6	10.75	130
100	8	17.00	140
Auto 15 10 2000 3000 4			

HEATING ISOLATING ICenters Tapped

& Sintered

Pin 120 240 300 20 240.

VA	Ref No.	Price	P&P
10	121	5.75	55
15	122	6.40	70
20	123	10.00	110
250	52	11.95	130
15	15	14.45	140
100	20	35.00	3.0

54a Monner Street
Horne Bay Kent
Horne Bay SA58B

BAYDIS

ELECTRONIC SURVEY

THE PRACTICAL ASPECT of a professional surveyor's job requires measurement of the size, shape and position (relative to other such defined shapes) of pieces of land ranging from the small household plot to the size of a country. It may also involve the application of the same methods for the measurement of large manufactured objects, such as buildings, bridges and other engineered structures. Such tasks commonly require measurement of distances and lengths ranging from a few metres to thousands of kilometres to precisions as small as a millimetre and angles to precisions down to less than an arc second.

Combinations of length and angle measurements, on a basis of measurement using triangles, are used in various ways to define shape and size. Definition of direction, with respect to North, and with respect to a level surface or a vertical plane also enters into a surveyor's daily needs.

In many cases, for reasons of convenience the measurements made are not quite those actually needed. Conversion or correction is required and as the mathematical process must be performed within 5 to 7 decimal figures of precision, the calculations needed can become tedious. As an example, when measuring the distance between two pegs in sloping ground it is the horizontal distance to a point vertically above the pegs that is often needed. The distance measured in practice is more often than not the slope distance between the actual position of the pegs.

Enter electronics

Until the 1950s the most precise method for measuring long lengths used a steel-tape hung in catenary, this method having developed from the less accurate chain of iron links. Another optical method, called tachometry, used the telescope of the theodolite

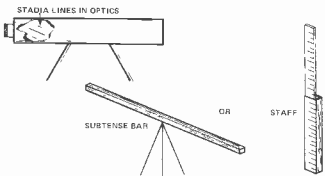


Figure 1 Using a telescope to determine range by tachometry

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ELECTRONICS IN SURVEYING

Ranging

Microwave methods: A continuously generated UHF signal, which is typically generated today by a Gunn diode oscillator, is sent from a small reflector or horn to a second unit placed at the other end of the distance to be determined. Phase difference between sent and returned signals provides a measure of distance in terms of the velocity of electromagnetic wave propagation in free-air conditions.

Accuracy is limited in all EDM (electronic distance measurement) methods by the knowledge of the refractive index of the air path. This limits all methods to around a 2 parts per million error in determining distances which range from 100 m to 50 km.

The first systems required the operator to learn a quite complicated procedure of use. Today the latest models provide digital readout, a voice channel to the person at the other station and, in some cases, an output compatible with digital data storage and processing systems. A modern microwave EDM unit is shown in Fig. 2.

The design and construction of microwave systems follow established radio communication practice using mixing techniques and special tone pattern generation. More detail on these methods is available in the "further reading" list given at the end of this review.

Electro-optical modulation: In these an optical carrier beam is modulated by altering the intensity of the carrier or its angle of optical polarization. The modulated beam is transmitted from a high-quality optical telescope to the far station where it is reflected back to the sender by one or more corner-cube reflectors. Fig. 3 shows the schematic of a Geodimeter model 6A.

Various sources of radiation are used in the models marketed. Originally a tungsten lamp or mercury discharge lamp was employed. Later improvements to range were provided by the use of helium-neon C.W. laser sources. Lasers also provided better utility in daylight conditions. The Mekometer method uses a pulsed Xenon gas source. The shorter distance modern units usually use a laser-diode source of infra-red radiation.

The kind of electro-optical technology involved in the manufacture of an I-R ranger is seen from the schematic of the optical system of the Hewlett-Packard 3820A provided here as Fig. 4.

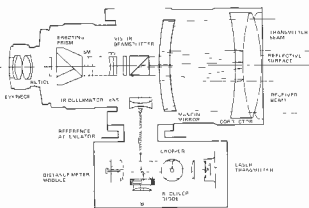


Figure 4. Electro optical rangiers require sophisticated manufacture to extreme provisions. This schematic is of an I-R laser diode instrument.

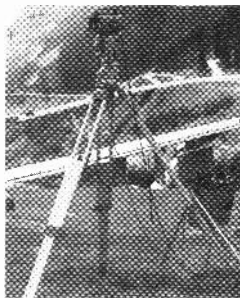


Figure 5. The Wild DL10 Distomat is an I-R ranger that fits on to a conventional theodolite.

Tacheometry: Basically the angle subtended between a fixed interval bar of scale unit is used to determine range by redirecting the theodolite from end to end of the target interval. The alternative is to observe the interval of a graduated staff seen within the angle defined in the field of view of the telescope by two parallel lines appearing in that field of view.

A variation is possible in which the optics of the telescope are altered geometrically at the operator's control.

This method of ranging is simple in principle, but needs many geometric corrections in practice for the subtended interval is rarely geometrically square and central with the telescope. Corrections are needed to change slope to horizontal and vertical distances and to allow for the fact that the observed interval is not square to the observer.

Many of the new electronic methods are called 'reducing tacheometers'. These, it seems, are not true tacheometers in the traditional sense, but are in reality rangiers to a point target.

Automatic angle measurement

The period 1950-65 was one in which extensive development of automatic angle measurement methods took place as part of numerically-controlled machine-tool development. Many methods of producing an electronic signal equivalent to angular rotation were invented.

Around 1960 several of the instrument designers in Europe began to apply these methods to surveying instruments so that the scales of a theodolite could be read automatically providing digital readout and automatic data reading.

Angular encoders for this task must provide circle subdivision to at least 21600 increments (1 arc minute) in a small diameter.

Of the wide range of angular encoder types invented optical methods have been adopted in electronic theodolites. Optical encoders may be of the incremental kind in which a pulse is produced and counted for each minimum resolvable increment of angular movement, the pulse being added or subtracted for the appropriate sense of direction. The alternative is to use a disk on

which a digital code pattern is manufactured. This is called the absolute method, for there is no chance of pulse loss or gain due to noise, power-supply failure does not destroy the value.

Incremental methods use simpler to make measuring gratings because they need only identical lines ruled radially. A much higher density of lines is possible by this method than is economically available with the absolute scale. The absolute scale is more costly to make and read than the incremental version.

In practice experience has shown that a hybrid system is the best to use, one in which an absolute encoder disk scale provides the coarse-position component of the readout, a finer ruling incremental scale providing the less significant digits, usually by way of an analogue subdivisional method that interpolates between the rulings.

The future

In the world of large commercial manufacture, new ideas are slower to reach the market place than they are to realise. Over the next decade a number of

improvements and alternatives should emerge.

Study of the time taken to set up a theodolite or level shows that the initial levelling procedure takes a significant time to achieve. Hewlett-Packard have recognised this and provided a partial solution to the user. Using electro-optic sensing of a plane surface, defined by a mercury pool, two-axis correction signals are produced that compensate for the not quite truly vertical central axis. The operator needs only to level the instrument within crude limits using a small circular bubbly level. The next stage must surely be to provide automatic levelling servos that set the instrument orientation regardless of gross misadjustment of the tripod top. This is straightforward to design — it is a matter of cost and time being available.

The next time-consuming task is to acquire the target and set the telescope fiducial mark on it so that the angles can be read out. In many cases the target is identified by a special mark or pattern to make it easier to find. The next logical move is to have the theodolite or level automatically seek out the target, locking on to it. Once acquired the scale values would be read automatically.

Another development that may replace the theodolite in many applications is a technique called chronometric angle measurement. In this method a rapidly spinning mirror causes a photo-detector to see established targets in sequence. The time between the sources is a measure of angle if the rate of rotation is known. Simple arithmetic establishes that the precision of timing available today is able to provide second of arc accuracy. There are no scales to read in the method. This concept was explored and an instrument built in Germany a decade ago. Perhaps the surveying instrument makers have a prototype ready to market now — such information is hard to establish in this highly competitive field of sophisticated instrumentation.

ETI

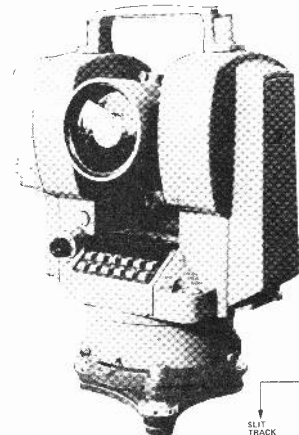
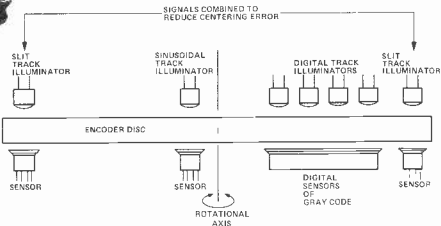


Figure 6 The 3820A electronic Total Station is an example of the more sophisticated electronic surveying instruments. Like some others, it contains a microprocessor that does the tedious calculations required, and the extra computing power available is used to correct readings for such variables as out of vertical of the instrument.

Figure 7 Cross section of reading heads that sense the angle in the HP 3820A Total Station.



Further reading

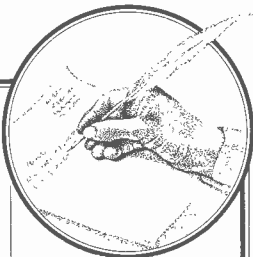
"Surveying by A Barnister and S Raymond Pitman 1977, contains a quite up-to-date chapter on electronic methods. It does not, however, discuss such concepts as electronic theodolites and instruments having micro processors in them.

"Electromagnetic Distance Measurement" by C. D. Burnside Crosby, Lockwood Staples provides detail.

Hewlett Packard Journal issues describe the theory, operation and construction of their Total-Station instrument in considerable depth. Most companies marketing this kind of equipment are able to provide reprints of papers describing the use of their products.

LETTERS

"Replies by
Bright Spark"



Contributions to this page are invited from all our readers. If you wish to make a point—this is the place to do it. All contributions to this section should be intended for publication. Please mark your envelopes 'LETTERS PAGE'.

ANNUAL ENQUIRY

Dear Sir,

In an advert in one of your magazines there is one book 'Arc Welders Annual', I wonder if there is an Arc Welders Monthly magazine please let me know if there is and if your com-



pany publish it. If they don't would you be so kind as to tell me the address of the company that does publish it.

F.Q.
Eire

Excuse me . . . erm . . . I don't know how to tell you this but that was a cartoon i.e. a joke — mind you the magazine displayed beneath Arc Welders would be sure of one reader should it ever appear.

BLOB BOARDS

Dear Readers,

If you are following the series 'Digital Electronics by Experiment' in Electronics Today International, you will have found the boards differently laid out to a ZB 81C. The author of the series used pre-production samples of ZB 81C Blob Boards and these were slightly different to the production models.

The only difficulty that this should cause with the series is in the construction of the voltage stabilizer cu-

cut, and we suggest the following modifications:-

USE bus-bar J for the regulated supply, linking to bars I and 34.

USE bus-bar K for unregulated input and O for negative line, Link O to 141.

USE line 151 in place of line N.

USE line 161 in place of line M.

For the remaining projects, use the boards supplied with the letters on top and the numbers down the left hand side.

We regret the inconvenience caused and now hope that you can still enjoy the series of articles

P. I. B

P. B. Electronics (Scotland) Ltd.

AND THE SAME TO US.....

Dear Sirs,

Can you imagine the chagrin you poor correspondents must feel at the nasty replies to their letters printed in the November issue? This letter is directed at you, the staff of ETI, so that you may share the experience.

You may be expert at plagiarising and paraphrasing but you do not actually know any basic theory do you? Original thoughts must be as scarce as butterflies at the offices at ETI.

One should, of course, suffer fools gladly but the mendacity, jealousy and spite of the aspiring intellectual makes him hard to bear — and when he pours malicious scorn on those only slightly more naive than himself a rebuke is in order. How different is the humble simplicity of the true scientist, whose virtue lies in his readiness to admit that there are things he doesn't know.

The copy you produce, redolent of third-form wit, parading knowledge lifted verbatim from the manufacturers' handouts—the ponderous puns, the gaffes, the howlers, the malapropisms, the spelling mistakes does nothing to justify the superiority you so obviously feel.

R.S

Piddlehinton

Ouch!

BLOOMING SPELL

Dear ETI,

I see the little homepride men have struck at the I.F.I offices!

You keep on spelling fluorescent as flourescent . . . an' my dikshunary don't agree!

D.J.

Chelmsford

We've downgraded the typist for that. Cos graded brains make finer flour!

POINTING OUT

Dear Sir

Although full of admiration for the November cover, I feel there is more than meets the eye behind the Special Offer.

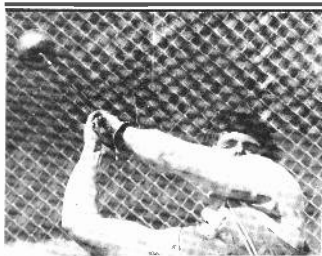
There are in fact two points I should like to see raised, however, as this may be physically impossible perhaps the offer could be moved to another page?

W.T.W.

Hednesford



Oh yeah? What size plastic mac do you take then?



HAMMER THROW

An exciting game of skill and luck that will help pass those long and lonely winter evenings.

IF, LIKE MOST of the ETI staff, you have more brains than brawn, and would not boast about the quality of either, it is likely that the mere thought of swinging a massive weight around your cranium is enough to strain your bodily systems. This probably means — and we are sorry if this comes as a disappointment — that your chances of selection for the Olympic hammer throwing team are, shall we say, nil.

Some may say that this is a pity as the sheer thrill of an event such as the hammer throw is probably very stimulating to those chunky brutes that are lucky enough to be able to take part. This is where we come to the rescue with our armchair version of the game. We think it has a number of distinct advantages over the real thing. One of these is that anyone, from an anemic sparrow upwards, can play the game. A second being that it is nowhere near as messy if, when playing in your lounge, you get things wrong.

The game, as can be seen from our photographs, has a front panel with a circle of sixteen LEDs together with a spot of eight LEDs at a tangent to the circle.

To play, after pressing reset, firmly press the play button. The LEDs in the circle will light one at a time simulating a spot of light moving in a circle. At the same time a distinctive, not to say

loud, sound will be generated.

The spot will at first travel slowly round the circle, but will soon begin increasing in speed until it is travelling quite fast.

The object of the game is to release the play button at the instant that the 'top' LED of the circle is lit. If successful the line of LEDs will light to indicate your score, the faster the spot was moving when you scored the more will be your score. If you miss, the circle of LEDs will continue to rotate at the same speed as they were when you played.

Big Ones And Little Ones.

A game will consist of, say, eight rounds — the score from each being added to the last. At the end of a game the person who scored the most is the winner. The skill comes in deciding whether to go for a number of low scores that are relatively easy to get, or for a few big ones.

As befits the design of a project of this nature we were in convivial mood and pleasant surroundings when we first discussed the game. We produced the first design sketch (well a few lines on a beer mat — yes in the pub again) which used digital devices. Upon seeing this some likely person said that he thought most games featuring LEDs designed over the past few years should

generically be called "spot the 4017".

Our initial reaction was to defend our design but a moment's thought showed that he had a point — the 4017 CMOS counter is over used when it comes to games. At this stage we decided to rise to the occasion and produce the game using an all analogue approach.

The result can be seen in the circuit diagram. We are pleased with this circuit. It uses some unusual ICs and features a number of interesting circuit blocks — and of course there is not a 4017 in sight.

Construction

Construction of the game is greatly simplified if the PCBs are used. Three boards are required, one for the power supply, one for the display, and finally the main control board. Begin by building and testing the power supply. Take care to ensure that all components are mounted as shown in our overlay.

Next assemble the control and display boards. These carry a large number of components and mistakes made during assembly can be difficult to trace later — so take care at this stage. Do not insert the link between IC2/4 and IC9 at this stage.

It is best to test the boards before mounting them in the case, as it is difficult to get to some of the devices when the boards are in their final

HAMMER THROW

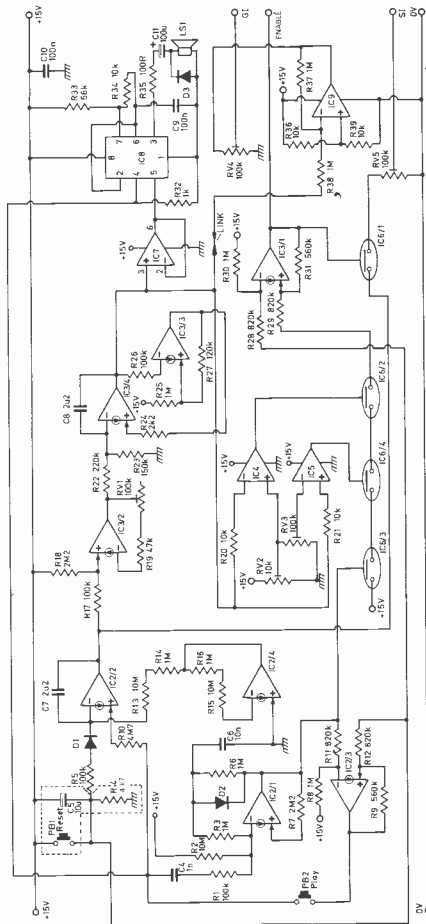
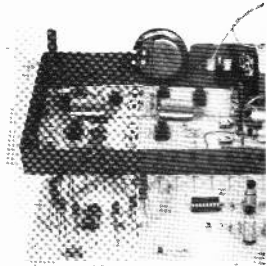


Fig. 1 Full circuit diagram of the hammer throw. For IC pin outs see Fig. 10



positions. We used a sloping front Vero box to house our game and the general layout adopted can be seen from our photographs.

Setting Up

There are five preset potentiometers on the board and all must be correctly set up before the game can be played.

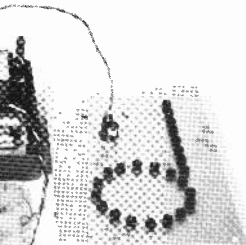
The first adjustment to be made is to RV4. To calibrate this control first press the reset button and then the play button for a few seconds. At this stage a sound should be heard from the speaker and the game display LEDs should be seen flashing. Adjust RV4 until the LEDs produce a continuously rotating spot of light. The speed at which the circle of light rotates can be adjusted by RV1.

The next operation is to set up the score display. To accomplish this, press reset and then operate the play button until the spot of light is rotating at maximum speed. Release the play button and enable the score display by applying a positive pulse (from supply) to the junction of R29 and IC6. RV5 should now be adjusted so that the seventh score LED is just extinguished and the eighth lit.

The final adjustments concern the 'window' discriminator. To make this adjustment R38 (the end remote from IC9) should be connected to the slider

BUY LINES

Some of the ICs used in this project may be unfamiliar but they are stocked by most of the larger component stores. Some of the high value resistors may also prove elusive, but again, if they are not available at your local shop try the advertisers in this issue.



of RV2 Adjustment of RV2 should illuminate successive LEDs of the game display. RV2 should be set to the point at which the top LED just extinguishes and the LED to the left just lights.

Now connect the input of IC9 to the slider of RV3. Adjust this pot so that the top LED just extinguishes and the LED to the right is just on.

This completes the adjustments and the link omitted during construction, should now be fitted.

Now is the time to get in training and, if you're good enough, you may yet make it to Moscow.

ETI

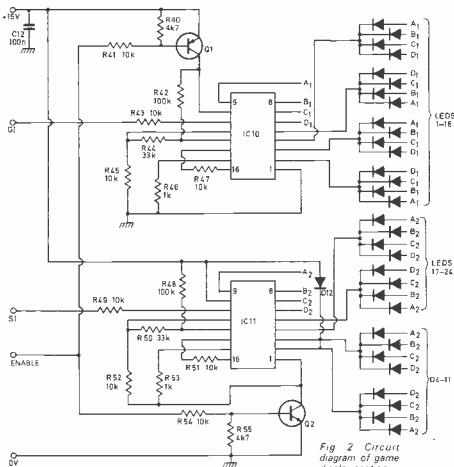


Fig 2 Circuit diagram of game display section

PARTS LIST

RESISTORS all 1/2W 5% unless stated

R1,5,17,26,42,48	100k
R2,13,15	10M 1/2W 10%
R3,6,8,14,16,25,30,37,38	1M
R4,40,55	4k7
R7,18	2M2
R9,31	560k
R10	4M7
R11,12,28,29	820k
R20,21,34,36,39,41,43,45,47,49,51,52,54	10k
R22	220k
R23	150k
R24	2k2
R27	120k
R32,46,53	1k
R33	56k
R35	100R
R44,50	33k
R19	47k

POTENTIOMETERS

RV1,3,4,5	100k min hor trim
RV2	10k min hor trim

CAPACITORS

C1	1000u	25 V electrolytic
C2	220n	polyester
C3	470n	polyester
C4	1n	polystyrene

C5	10u	25 V electrolytic
C6	10n	polyester
C7,8	2u2	polyester
C9,10,12	100n	polyester
C11	100u	25 V electrolytic

SEMICONDUCTORS

IC1	78L15A
IC2,3	LM3900
IC4,5,7,9	741
IC6	CD 4016
IC8	555
IC10,11	UAA 170
Q1	BC212L
Q2	BC184L
D1,2,3,4-12	1N914
LEDs 1-24	.2" type
BR1	4 pin DIL TYPE 0.9 A 400 V (from R S Stockists)

TRANSFORMER

T1	240 V - 15 V 6VA
----	------------------

LOUDSPEAKER

LS1	G.P O type insert
-----	-------------------

SWITCHES

PB1,2	Push to make
SW1	SPST toggle

CASE

	Vero type 65-2523
--	-------------------

MISCELLANEOUS

	Flex, PCBs as patterns, LED mounting clips, fuse and holder to suit,
--	--



Fig 3 Foil pattern of power supply board shown full size (120 x 45 mm)

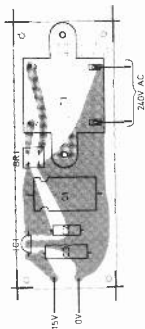


Fig 4 Component overlay of PSU mains earth is connected to T1 by a solder tag under the mounting bolt. The transformer's screen should also be connected to earth

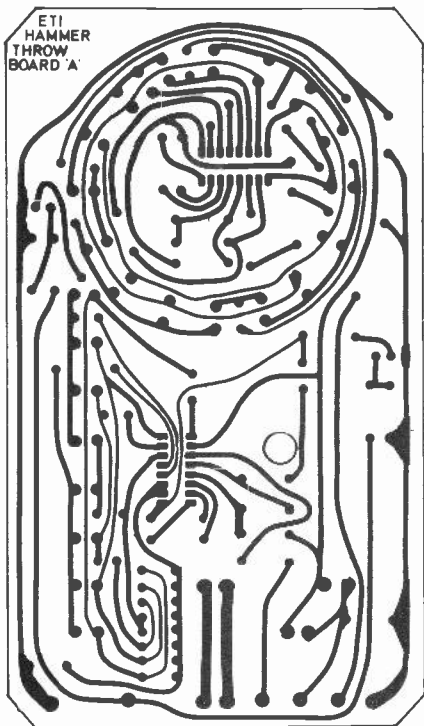
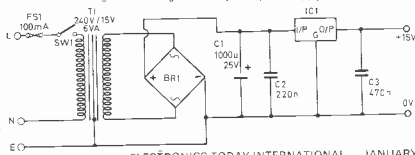


Fig 5 Full size (160 x 110 mm) foil pattern of display board

Fig 6 Circuit diagram of the game's power supply



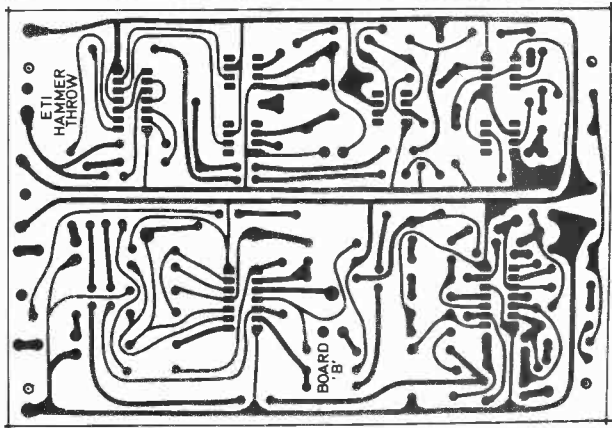


Fig. 7. Full size foil pattern of main control board (160 x 110 mm)

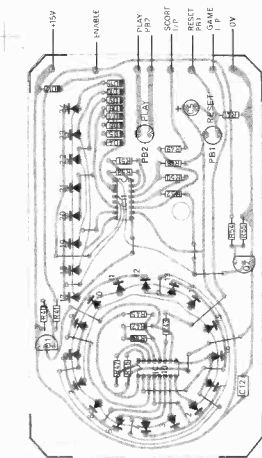


Fig. 8. The overlay for score board

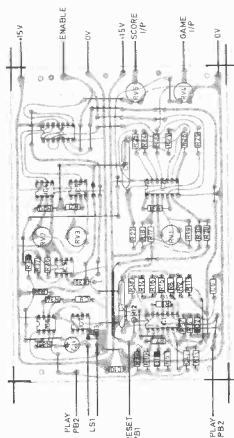


Fig. 9. The overlay for the control board

HAMMER THROW HOW IT WORKS

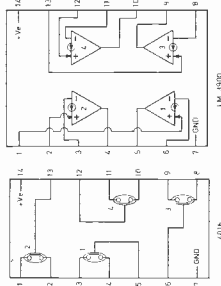
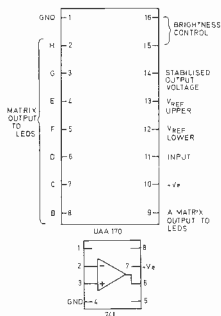
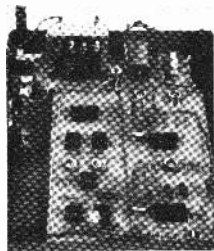


Fig. 10 Pinouts for the integrated circuits used in the hammer throw



The circuit may be broken down into a number of major blocks — viz the display sections for both game and score, a voltage controlled oscillator, a ramp and hold circuit whose output controls the oscillator, a 'window' discriminator, a sound generating circuit and finally a power supply. As well as these major blocks there are also a number of latches, buffers and switches that are necessary for circuit operation.

The block diagram shown in Fig 11 shows most of the circuit blocks and, together with the circuit diagram, should be read in conjunction with this how it works.

SYSTEM OPERATION

The game display is based on a UAA 170 IC. This device is used for driving LED displays and when connected to a line of sixteen LEDs will illuminate any one of these depending on the magnitude of the analogue voltage applied to its input. For the game display we need to produce the effect of a spot of light moving in a circle. To achieve this we arranged the sixteen LEDs in a circle and feed a sawtooth waveform into the UAA 170. A moment's thought will show that this will produce the desired effect.

In order to make the display rotate slowly at first, but speed up as play proceeds, we made the sawtooth generator voltage controlled. The control voltage is produced by a ramp and hold circuit which is reset to zero at the start of play, but begins to ramp up, thus increasing the sawtooth's frequency as play continues. When the play button is released, the voltage reached is held by the ramp and hold configuration until it is reset. This voltage is used for score purposes as described below.

The game requires that if at the instant of releasing the play button, the 'Top LED' of the game display is lit, a score is indicated, the magnitude of the score being proportional to the speed at which the circle of LEDs was moving at the instant of release. From the description of the game display it will be seen that in order to light a specific LED the voltage input to the display driver must lie within a specific voltage range. Thus in order to detect whether or not the 'top' LED is on we must look at the output of the sawtooth generator (this is input to UAA170) and decide whether it lies within the range that will light the specific LED at the instant the play button is released. The circuit that accomplishes this is the 'window' discriminator.

This is formed from two voltage comparators together with two analogue switches. Detailed action is described below, but briefly the circuit, when fed with the sawtooth output, will provide an indication whenever this waveform passes through an (adjustable) 'window' voltage range.

At the instant that the play button is released a short pulse is produced from a monostable. If this pulse is coincident with an indication from the window circuit that the top LED is on we must arrange to indicate a score.

The score must be proportional to the speed of the LED circle which is in turn proportional to the voltage level reached by the ramp and hold circuit. Thus, to produce a score, we feed the output from the ramp and hold, via an analogue switch to a second UAA 170. This second display consists of eight LEDs in a line.

This completes a brief description of circuit action; we shall now deal with each block in more detail.

RESET CIRCUITRY

The game is initiated by operation of the reset button (PB1). This zeros the ramp and hold circuit described below, as well as setting latch 1 IC2/3 and resetting latch 2 IC3/1. Latch 1 enables the play button when its output is high (set) — latch 2 enables the score display when low ('reset') the game display when high (set).

Each latch is set on two of the amplifiers of an LM 3900 Quad Norton amplifier package. This device is unusual in that instead of amplifying the difference in voltage applied to its input terminals it amplifies the difference in input current.

The + and - inputs of these Norton amplifiers are both clamped to one Diodo Drop above ground and thus all input voltages must be converted to currents (by resistors) before being applied to the inputs. This is the basis for the current Mode (Norton) type of operation.

In operation the current flowing into the + input must equal that flowing into the - input, the difference between the current demanded at the current provided by an external source must flow in the feedback circuitry.

Operation of both latches is the same and we shall only describe the action of latch 1.

Assuming that the latch output is low (the latch is reset) the current injected into the - input of IC2/3 will ensure that the output remains low. If now sufficient current is injected into the + input the output voltage will rise as the device attempts to reduce the input current differential to zero. Positive feedback via R9 will enhance this action and cause the amplifier to latch high. This is because the current injected into the + input via R9 in this case is greater than that into the - input due to R8. A positive pulse via R11 to the - input will however once again bring the output low.

C5 and R4 ensure that when power is first applied the game is reset.

RAMP AND HOLD

The ramp and hold action is provided by IC2/2 and IC2/4. A positive voltage via R5 and D1 causes the output to ramp down while a similar voltage via R10 causes the output to ramp up. The reset button causes the downward ramp while play causes an upward ramp.

In any sample and hold application a very low input bias current is required if the hold period is to be stable. The existence of matched amplifiers within the LM3900 allows one amplifier to bias another.

In operation the LM 3900 requires a bias current to be applied to its - terminal IC2/4 has its + terminal grounded and feedback applied via R15 and R16. The output voltage of this device will attain a level such that the current fed back via these resistors is equal to the bias current demanded by the input. This same current will flow via R13 and R14 into the - input of IC2/2 reducing the effective bias current of this amplifier to almost zero. D1 isolates this bias current from the rest of the input circuitry.

If now a positive current is injected into the - terminal, the output voltage will fall as it attempts to feedback a current of this value in order to reduce the input current differential. This constant current across C7 results in a linear voltage ramp appearing across C7 into the + terminal causing a positive going ramp to the - terminal a negative going ramp.

The rate at which the voltage across C7 changes is proportional to the value of the

constant current supplied which is in turn proportional to R5 and R10. As R5 is some 40 times larger than R10, the ramp down (reset) is far quicker than the ramp up.

The output from the ramp and hold circuit is fed, via IC6/1 to the score display and via IC3/2, a non-inverting scaler, to the sawtooth VCO.

NON-INVERTING SCALER

The scaler is required because the output from the ramp and hold configuration can vary over nearly the whole supply voltage whereas the VCO requires only small voltage swing to provide the required frequency change.

The scaler is based on another Norton amplifier arranged as a non-inverting amplifier feedback is applied via RV1 and R19 and output is fed to a potential divider formed by R22 and R23 and thence to the VCO.

VOLTAGE CONTROLLED SAWTOOTH OSCILLATOR

The VCO is formed by IC3/3 and IC3/4. Action of IC3/4 is much the same as that of IC2/2 described above. The special input bias circuitry is not required as there is no hold requirement.

IC3/3 acts as a comparator and circuit action is as follows: while the output of IC3/4 is high and ramping down (input to - terminal) the current into the - input of IC3/3 due to R26 is greater than that to its + terminal due to R25 - its output is thus low.

As the output of IC3/4 ramps low however, there comes a point where this situation is reversed. The output of IC3/3 goes high. This state being maintained by positive feedback via RT and injects a large current into the + input of IC3/3 as R7 is much smaller than R25.

The output of IC3/4 thus goes high, restoring current flow via R26 and starting the cycle again.

By varying the current injected via R22 the time taken for the output of IC3/4 to ramp down to the point at which the comparator triggers is lessened. This results in an increase in the frequency of the sawtooth.

The output from the VCO is fed to the game display section R77, to the 'window' discriminator formed by ICs 4 and 5 and via IC7 to the sound generator IC8.

WINDOW DISCRIMINATOR

The window discriminator is formed by two comparators IC4 and IC5 and two of the analogue switches in IC6.

Operation is as follows: If we assume that the output of the sawtooth VCO is high and ramping down the voltage on the - input of IC4 will be higher than that on the + input (a reference level established by RV2) and its output will be low. The output of IC3 will be high as the input to its + terminal is higher than that to its - input.

As the voltage ramps down, a point will be reached where the output of IC4 goes high as the voltage at its - input falls below that set by RV2 at its + terminal. At this stage the outputs of both IC4 and IC5 are high, as IC5 has not switched. As the voltage continues to ramp down, however, the voltage on IC5's + input falls to a point below that on its - input and the output of this IC goes low.

Thus the outputs of both ICs will be high for a small range of input voltages (the window) defined by the difference in voltage between the sliders of RV2 and RV3.

The outputs of these ICs are fed to the inputs of two analogue switches. A positive voltage applied to these switches turns them 'on'.

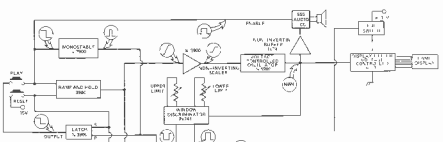


Fig 11 Block diagram of the hammer throw game

Thus during the window a signal path exists from the input of IC6/4 to the output of IC6/2.

MONOSTABLE

The monostable is formed by IC2/1. This produces a short positive going pulse upon receipt of a negative spike produced by the release of the play button.

Current injected into the - terminal via R3 will normally hold the output low, however a negative pulse applied via C4 and R1 will 'rob' this current from the input and causes the output to go high.

RT latches the gate in this state after the negative pulse is removed. At this stage C6 begins charging, feeding back an increasing amount of current to the - input as the voltage at the junction of R6 and R3 rises.

There comes a point when this current is greater than that fed back via R22 and the output returns low. Diode D2 rapidly discharges C6 to provide reliable re-triggering.

The leading edge of the output pulse is coincident with the release of the play button. This pulse is used to turn on analogue switch IC6/3. It will be remembered that if the voltage of the VCO is within the 'window' at this point - switches IC6/4 and IC6/2 will also be on. This allows the supply voltage input to IC6/3 to set latch 2 and thus initiate the required actions, i.e. blank game display, enable score display, etc.

The monostable also resets latch 1. IC2/3 to remove supply from the play button, this prevents cheating.

GAME DISPLAY

The output of the sawtooth VCO is fed via an inverting buffer, IC9, and a potential divider, RV4, to the input of IC10 a UAA170. The input circuitry of this device consists of a series of differential amplifiers with one input of each connected to the input terminal (pin 11) via an emitter follower. The other input of each is connected to a point in a potential divider chain consisting of equal value resistors. The differential amplifiers thus operate as analogue voltage comparators and as the input exceeds the reference voltage of a particular comparator, the output of that comparator will change state.

To reduce the package pin-out the LEDs of the display are not driven individually but are arranged in a four by four matrix pattern controlled by the row and column outputs of the UAA170 (A-D and E-F respectively). By enabling the appropriate row and column output any one of the sixteen LEDs may be selected. The matrix outputs are controlled by the internal logic of the UAA170.

The resistor chain R42, R44 and R45 sets up the reference voltage inputs of the device. The voltage on pin 12 establishes

the lowest voltage to which the UAA170 will respond. If the input voltage is below this point the first LED of the display remains lit. As the voltage rises above this level the first LED is turned off, the second on - as the input rises the spot moves up the chain, until the voltage reaches that set on pin 13. This is the maximum voltage to which the display responds and if the input is taken above this level the last LED remains lit.

In addition to defining the indication range the voltage between pins 12 and 13 determines the abruptness of transition between any two LEDs. With this difference set to IV4 the light point glides smoothly along the scale with increasing voltage difference the passage becomes more abrupt until at 4V the light spot jumps from one LED to the next. We have set this voltage to a point between the two extremes.

The resistors R46, R29 and R47 control the brightness of the display Q1 supplies power to the display and is driven from latch 1. IC2/3. This you will recall is reset, i.e. its output is low, at the start of a game. A low voltage applied to Q1 via R41 turns this transistor on and enables the display. The latch is returned high at the end of a game this turns Q1 off and blanks the display.

SCORE DISPLAY

The score display is formed by a second UAA170 (IC10). Much of the circuitry is the same as that of the game display except that we only wish to display eight LEDs. The diodes from unused outputs to the +VE supply act as 'dummy' LEDs, restricting the display to eight LEDs, you could use LEDs for extended scoring - but a larger box is needed. This display is powered by Q2 which is again fed from the output of latch 1 (IC2/3). This time however, the display is blanked, Q2 on, when the latch is low and enabled, Q2 on, when the latch output is high.

SOUND GENERATOR

The sound is generated by IC8 an NC555 operated in an astable mode. The reset pin(4) is normally held low by R32 and hence circuit action is inhibited. A positive voltage applied from latch 1 via the play button enables the sound during the game.

The output is frequency modulated by applying the output of the sawtooth VCO, via buffer IC7 to provide the necessary low impedance drive, in the voltage control input (pin 5) of IC8.

RACE TRACK



WE BET YOU'LL HAVE FUN WITH THIS GAME

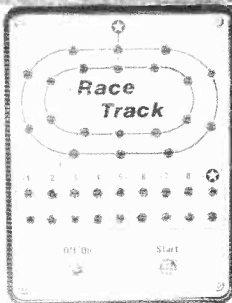
THE DESIRE TO place bets upon almost any event, from the outcome of the big race at Newmarket to the likelihood of life on other planets, is a deep seated one in many of the inhabitants of these islands. That old joke about the guy who bet his friend a couple of quid that he can give up gambling for a week would not be amusing, but for the fact that it were so near the truth.

Three Way Bet

Bets fall into a number of different categories. They may be made on disagreements of fact ('I bet mine's bigger than yours'), about events capable of being modified by skill or lack of it ('I bet I can get mine further than yours'), or bets made upon random events (The mind boggles!).

It is this latter type of bet, the toss of a coin, cut of a card or spin of a roulette wheel, that is probably the most popular form of gambling amongst groups of people, our race track game provides an exciting means of indulging in this type of activity.

The game is really a development of the well known 'heads or tails' type of game, but whereas most games of this sort are visually unexciting, the race



track game more than makes up for any shortcomings in this area!

They're In The LED

When the game's reset button is pressed all the LEDs are off and the 'horses' line up at the starting post. Now is the time to choose a horse and place bets if you wish.

Releasing the button starts the action with the circles or LEDs representing the 'horses' starting to flash as first one horse then the other takes the lead. As each horse completes a lap the appropriate lap LED lights. The first horse to cross the finish line lights his 'win' LED and halts the racing horses. If lady luck did not smile on you this time, pressing the reset button gives her, and you, another chance.

Construction

Mount all the components on the PCB as indicated in our overlay diagram. We recommend that sockets are used for ICs 1-6 as these are CMOS devices and should not be placed in circuit until all constructional work is complete. The LEDs are hard wired to the PCB and the interconnection information is given in Tables 1 and 2. Note that LEDs 37 and 38 have their cathodes taken to 0 V via R6 and R7 and not directly to ground as the rest.

The value of R1 should be selected to give the best display on the race track. A value somewhere between 4M7 and 10M should suit.

Now is the time to turn on, place your bets and probably loose your shirt.

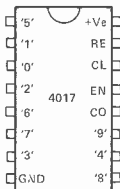
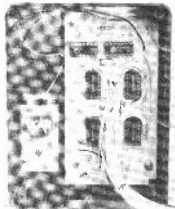


Fig 1 Pin-out for 4016 IC



The photograph of the game shown left shows the general method of construction used in the prototype. Connection details for the wires between the board and front panel are shown in Tables 1 and 2.

HOW IT WORKS

The circuit uses two oscillators each based on two of the NOR gates in the 4001 Quad NOR CMOS packing. One of these (IC1/3 and IC1/4) runs at a high frequency and its output is fed to the input of one half of a 4013 Dual D type flip-flop. The device divides the output of the high speed oscillator by two and provides two signals that are 180° out of phase at its Q and Q outputs. These signals enable either IC3 or IC5, the ICs being enabled if their enable input is held low.

The second oscillator based on IC1/1 and IC1/2 runs at a lower speed and is arranged to provide a non-unity mark space ratio, in fact a very short "high" output followed by a much longer "low".

This non-unity mark space ratio is achieved by the inclusion of D1 in the oscillator's timing network. This second oscillator can be gated on and off by signals to be described below.

Circuit action is as follows: PBI is closed and this resets all the counters to zero as well as inhibiting the slow running oscillator. Upon releasing PBI, IC3 or IC5 will be clocked as the first positive pulse is generated by IC1/1 and IC1/2. Which counter is incremented will depend upon the state of IC2's outputs.

In general as the two oscillators are out of phase the counters will appear to be clocked in a random manner. A further random element is introduced because

while a 4017 is normally clocked with positive going pulses at the clock input with enable held low, it is possible for it to be clocked with a negative going pulse at enable while clock is high. Thus occasionally IC2 will act as a clock.

At the end of a lap a pulse is generated from the carry out (CO) output of either IC3 or IC5 and is used to advance the lap counters (IC4 and IC6).

The game ends on the ninth lap when the '9' output of either lap counter goes high. This turns on either Q1 or Q2 and in turn lights the appropriate win LED. The signal from either '9' output is ORed by diodes and this signal used to halt the game by disabling the slow running oscillator.

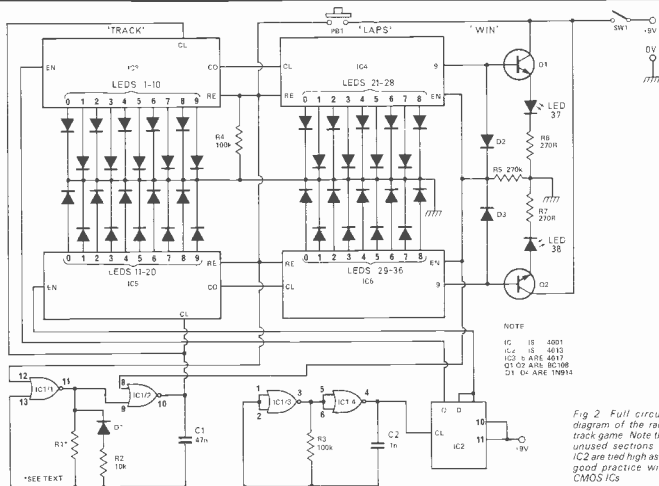


Fig 2 Full circuit diagram of the race track game. Note the unused sections of IC2 are tied high as is good practice with CMOS ICs.

TABLE 1
CONNECTIONS TO IC3 (5)

PIN	LED (ANODE)
1	6 (16)
2	2 (12)
3	1 (11)
4	3 (13)
5	7 (17)
6	8 (18)
7	4 (14)
9	9 (19)
10	5 (15)
11	10 (20)

TABLE 2
CONNECTIONS TO IC4 (6)

PIN	LED (ANODE)
1	25 (33)
2	21 (29)
4	22 (30)
5	26 (34)
6	27 (35)
7	23 (31)
9	28 (36)
10	24 (32)

BUY LINES

There should be no problem getting any of the components for this project. The ICs should be available from people like Lynx, Maplin, Watford and Marshalls. The main thing is to try and get a quantity discount on the thirty eight LEDs needed.

PARTS LIST

RESISTORS (all 1/4 W 5%)

R1	* see text
R2	10k
R3,4	100k
R5	270k
R6,7	270R

CAPACITORS

C1	47n polyester
C2	1n ceramic

SEMICONDUCTORS

IC1	4001
IC2	4013
IC3-6	4017
Q1,2	BC108
D1-3	1N914
LED1-38	TIL209 red

SWITCHES

PB1	Push to make type
SW1	SPST toggle

MISCELLANEOUS

Battery clip, flex, PCB as pattern, case to suit.

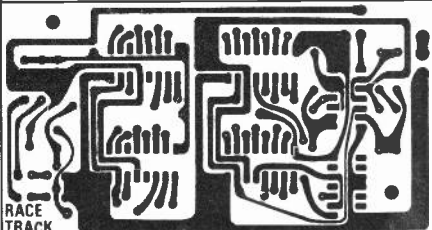


Fig 3 Full size (115 x 62mm) foil pattern

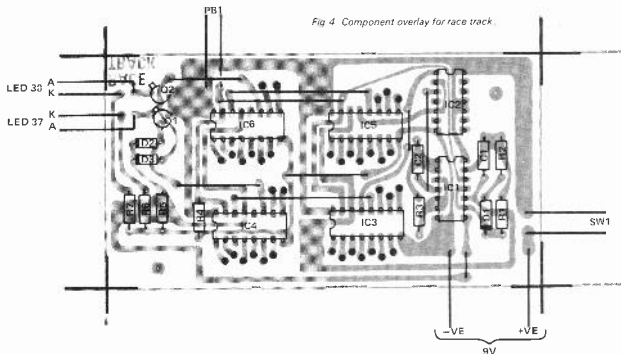


Fig 4 Component overlay for race track

SUREFIRE

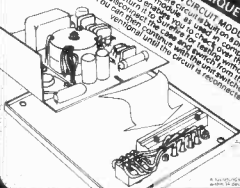
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Gaps?

Gaps?

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P/P & Ins. £1.00



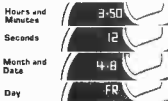
The Golden Dot is truly an entirely new standard for timepiece craftsmanship. Never before has there been an electronic Quartz watch so whisper thin that its profile challenges the breadth of its elegant mesh band.

If you have ever wished to wear a piece of contemporary sculpture, elegant and deserving of museum recognition, The Golden Dot is a beautiful choice. We cannot stress strongly enough how fine this electronic digital watch is. We can only urge you to wear it for 10 days at our expense.

A technology so new it defies comparison. Beneath the wafer thin styling of this remarkable timepiece is the most advanced solid state technology ever crafted for an electronic watch. Notice that there are no obtrusive buttons to interrupt the graceful lines of the watch itself and it is accurate to seconds.

The circuitry of the Golden Dot is so unique that a soft fingertip touch of the Golden Dot instantly beams easy to read LED display onto the watch face.

Six Function Performance



This wafer thin Golden Dot watch has a mesh casing with simulated gold finish and matching mesh bracelet designed for him and her.

Wear it for 10 days.

You just cannot believe the luxury of the Golden Dot until you have worn it. Until you have experienced its featherweight comfort and have enjoyed the compliments it generates. We are so certain that you will be satisfied that in addition to the One Year warranty we are offering a 10 day money back guarantee if you are not entirely satisfied.

Telephone orders 01-455-9855

Please send me Golden Dot Watch(es) on 10-day trial. I enclose cheque/P/O for £. Charge to me through Access A/C No.

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Complete kit with pre-built search coil

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The computer is a true thinking machine utilizing artificial intelligence and programmed to adapt to all strategies of the game. The computer has an aggressive offense, yet understands defence. It plays a running game, block, hit and run game, semi-back game, backgame, blot hitting contest and bear-off strategies.

A novice can learn the game of backgammon and an intermediate player should be able to greatly improve his game.

Always ready to play an exciting game to match your novice to master level of skill using artificial intelligence programmed for all strategies. This advanced state of the art electronic product uses microprocessors and memory technology that verifies every move, even recognises an illegal move and generates a random roll of the dice. Play against the computer by yourself, with couples or conventionally Handsome charbrown compact 12 3/4" x 7 1/2" x 1 1/2" impact resistant plastic unit shipped with carrying case, simple instructions, 30 men and 2 spares. Ideal personal or business gift to challenge and improve a player's game. 12 months' warranty. Please allow 2-4 weeks' delivery.

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SAE for data sheets
Export enquiries welcome

You may think your conversation is private but

WALLS HAVE EARS

There appears to be little control in Britain over the manufacture and sale of bugging devices. ETI has been investigating the current situation.

IT WILL COME as a big surprise to most readers that bugging is not in itself a criminal offence. Plant an RF bug in an office during working hours, listen in on highly confidential discussions and the worst that you'll be got for — if you're caught — is operating a transmitter without a licence. Technically you could also be had for listening to 'an unauthorised transmission' but we know of no such prosecutions.

Top secret, illustrated export catalogue details 20 ready built security devices: automatic surveillance receiver, beam microphone, miniature radio, telephone override device (industry harmonics etc), electronic microscopes and many more.

The Younger Committee on Privacy which reported in 1972 quite rightly recommended that bugging in any form should be an offence, in itself, but it has not yet been acted upon.

How serious is bugging?

In researching this feature we found ourselves continually coming up against stony silence — few people are prepared to discuss the subject and none would agree to having their comments personally attributed. Try

to talk to a company that's advertising bugs and ten-to-one he'll tell you he's now stopped, but he will supply you with equipment to 'sweep' your office (the technical term for finding other people's bugs).

It is possible to get some idea of the scale of things however. There are about ten companies in Britain openly advertising bugs — most of them appear to be very small. Even so this indicates that sales are unlikely to be worth less than £100,000 a year and since bugs are cheap, literally thousands are sold every year.

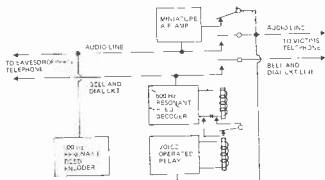
Most technical publications (this includes ETI) refuse to accept advertisements for these devices on

the grounds that they are undesirable, not because we are not allowed to.

Where are these bugs used then? We suspect that the overwhelming number are bought as toys and not for any devious purpose but this still leaves probably several hundred that are bought for their stated purpose of listening in on other people's business.

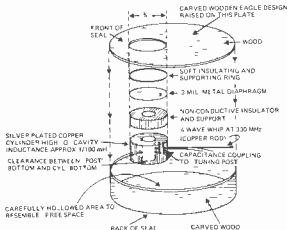
UNSCRAMBLER SUPER SALE Our famous Code-Breaker works with all scanners and tunes all scramble frequencies only £99.95 COD s (501) £109.95. Mail orders to [redacted]

The vast majority of businesses are operated decently and honestly but in every sphere it is very useful to know



Arrangement of an infinity transmitter used to eaves drop on sounds in a room thousands of miles away using the telephone as the microphone.

Exploded view of the US Great Seal presented to the American Embassy in Moscow in 1945. This ingenious device was passive in operation and could not be detected by most of today's anti-bugging equipment. When you appreciate that this was devised 33 years ago it makes one wonder how sophisticated modern-day intelligence equipment must be.



WALLS HAVE EARS



This telephone insert looks pretty standard. In fact it contains an FM radio transmitter with a range of several hundred metres

risks to a company initiating bugging are enormous. Middlemen are almost always used

Superbug, not just another bug, high sensitivity FM transmitter, with 20 mile range, 500 mW, tinier than matches, 5 miles range (battery), 100% reliable (not 99.99% for use), best value available, see for details.

Sweeping

Many if not most of the companies selling bugs will also supply sweeping equipment — after all a radio signal is easier for someone close to the transmitter to pick up than it is for someone a hundred metres away — or is it? First you don't know what frequency it's operating on. It could in theory be from 50 kHz (though the antenna would be a problem) up to several hundred megahertz. OK, use an untuned circuit but then what do you do about regular radio and TV

broadcasts? If you set the frequency of the bug close to that of a powerful FM station it's difficult to sort out the two

The makers of the equipment are highly secretive about their techniques and not one would discuss technicalities, they claimed, perhaps with some justification, that if you know how the sweeping is done, it's all the easier to use a technique which won't be picked up. We believe many of them employ a howl-round technique — put a receiver near a bug and you'll set up an audio/RF loop which will go into oscillation

Micro transmitters, receivers, electronic substations, etc., complete range of professional equipment available, send 4/10p stamp for fully illustrated catalogue, local agents in many areas.

International Espionage

Although companies will normally keep quiet about attempts to bug them, Governments delight in exposing the failed attempts

The American Embassy in Moscow recently announced that they were being subjected to extremely high



A small bug openly advertised in Britain. Claimed to have a range of 200 metres with a 50-hour battery life, it retails for under £40



The size of this bug can be judged from the PP3 battery plug. It is claimed to have an output of 300 mW which the makers claim is good for 5 miles and can be supplied with any frequency, in the range 84-150 MHz. We have no way of verifying these claims. Price is about £16

power, high frequency radio signals. It was of such a magnitude that it was even suggested that it was an attempt deliberately to make the staff ill. It is now thought far more likely that the RF signals were being used to recharge batteries in bugs within the building

In 1945, as a gesture of good will the Russians presented the US Embassy in Moscow with a beautiful wooden carving of the US Great Seal. After several years it was discovered that this had built into it a wonderfully simple bug. Inside the seal was a copper cavity coupled to an antenna, one end of the cavity was covered by a thin metal diaphragm

The bug was activated by an external RF signal (in fact 330 MHz) — this made the cavity resonate but the diaphragm caused the reradiated signal to be modulated and this to relay conversations near the Seal. This could still have been in operation

DISSECTING A BUG

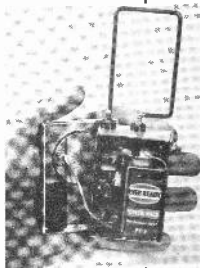
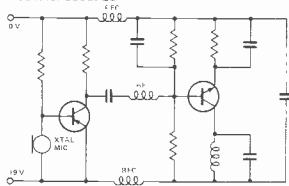
THE RF BUG shown in the photograph is a home-brew one that came into ETI's possession. The circuit was openly published in a British book a few years ago — we show the circuit as well although we have not nor will we provide any component values. (Since there are several variables we do not suggest you 'suck-it-and-see')

Although a DIY circuit, it would seem that virtually all the smaller or simpler bugs are of similar complexity or even similar circuitry

This bug operates anywhere in the 87 MHz-108 MHz range and despite the simplicity and low battery drain (only a few milliamps) it will transmit a fair quality signal for several hundred metres in most areas and at least 30 metres even in heavily built-up areas

with steel-frame buildings like city centres

The microphone will pick up normal speech at 10 metres quite easily. The performance, frankly, is worrying — because of the effectiveness — and the unit can be built for about £3!



Complete circuit of a VHF bug which can be built for only a few pounds

if some British technicians had not stumbled across the signal by accident. A thorough subsequent 'sweep' of the US Embassy brought to light no less than 60 other devices!

It is hardly surprising that British Intelligence Services are involved as well. The Russian Embassy in London moved a year or so ago and when access to the building became possible it could be seen the lengths to which the Russians went to prevent eavesdropping, even to having built a room within a room. Various bits of information have leaked out that Intelligence Services were directing a low power laser at the window glass; this would then have been slightly modulated by the sound inside the room and the reflection picked up could detect this.



One of the techniques which has recently come to light is that of 'RF flooding' of a telephone. Even when the phone is on the hook, the RF can 'jump' the contacts. This is then modulated by the microphone and can be picked up. As it can only be used with single lines, a switch-board defeats this technique.

The other phone tapping technique, the 'infinity transmitter' is also made useless with a switch-board. Many company executives use direct lines for security whereas the switch-board itself is a pretty good defeat against some techniques.

Transistorised transmitters (not licensable in UK); outstanding range, easy-to-use size include microphones, PCB and all electronic components. All VHF/FM tunable 70-150 MHz. Power 300mW. 400 yards, only 100mW. Price £12.95. 250mW 1,500 yards, 500mW, 300mW, 3 miles. Other kits available, including test ear-piece, switching and entertainment studio. Send two for use for detailed price list to: info@electronics-today.com

Equipment Available

Laws in many countries have failed to keep pace with technology but it is ironic that most of the really sophisticated equipment being made originates in the US — the very place

ARE YOU BEING BUGGED?

THE BIGGEST PROBLEM facing someone wishing to bug another is gaining access. Breaking and entering is obviously criminal but a bug can be installed literally in one minute if some risk of the device being discovered is acceptable. Unless the villains have access to a building during building or decorating work, problems in siting the bug are real — well-concealed hiding places are usually bad for picking up sound. Favourite sites reported to us are in low pressure air-conditioning vents and behind radiators — another one is on sticky pads under a desk, somewhere which would not be noticed for years.

A simple search is best and most bugs will be discovered unless a true expert has been employed. The extent of telephone bugging is unlikely to be high — access is so difficult that only the Intelligence services will be able to handle this. In any case electronic telephone scramblers can overcome this. If you regard yourself as a candidate for bugging, check the credentials of Post Office engineers if you haven't called them in yourself. But don't be fooled by the novelists who seem to insist that 'two ominous clicks' after the telephone is lifted at a certain indication that there is an unwanted listener on the line.

with the strictest laws against bugging and phone tapping. This could be because the problem there is greater but no amount of legislation is going to prevent the availability of equipment — the profits are too great.

UNSCRAMBLE CODED MESSAGES from Police, Fire and Medical Channels. Same day service. Satisfaction guaranteed.

The range of equipment is so varied and the interest so keen that in the Spring of 1977 a full scale exhibition of both bugging and anti-bugging devices was held in West Germany — a country which



A real spy kit advertised for 'the professional'. A 6-channel transmitter operating on VHF or short wave is supplied — there is a matching receiver. Also included is a cassette recorder mains operation facilities

incidentally bans sales . . . except if it is marked as 'Export Only'. It's surprising how many retail outlets regard themselves in this field!

The Future

However superior anti-bugging equipment becomes, the number of ways of eavesdropping electronically is so varied and the techniques developed for keeping the devices undiscovered so ingenious, it seems that bugs and bugging are not likely to become any less of a problem.

Legislation may not stop bugging but it can raise the risk factor to such a level that those practising it will think carefully.

ETI

MICRO ELECTRONIC TRANSMITTER

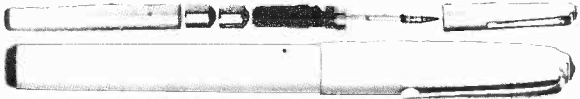
Receive on a VHF Radio. A must for Security, entertainment, warning alarm or listening to bird songs, etc. The smallest transmitter available, only 2" x 1". Can pick up and transmit voices and minute sounds. Range 500 yards plus. Works anywhere, in a hand of driver, on 12v PP3 batteries (long life). Completely self-contained, conditioned printed circuit. To operate works on no other connections. Used world wide. Guaranteed. Latest model now developed.

Transmitter
If required, suitable pocket receiver
Mail order welcome.

Send 2/10p stamp for Catalogue of Many similar devices. Licence not available in UK.

ETI is not prepared to answer any queries, for whatever reason, on the circuit components or as to the availability of the equipment shown in this feature.

At first sight an ordinary pen but look closer. Despite its size it has everything incorporated and will put out a signal over 100 metres for three days on one set of batteries



electronics today

international

What to look for in the February issue: On sale January 6th

IB Metal Locator Mk 2

The photo shows our Mk. 1, published a year ago but we've taken this design a stage further.

The Mk 1 was one of the most popular projects ever published, probably because the early builders were able to demonstrate the exceptional performance to others.

We've looked at every aspect of the design and have come up with an improved version which we are sure is going to be of interest to practically everyone.

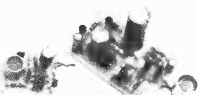


ETI

goes technical colour!

The next issue of ETI will have several pages in 4-colour. At this stage it's only an experiment but you can be sure that if it's in the electronics or publishing field, ETI is way ahead of the competition.

Ultrasonic Switch



This project describes both transmitter and receiver and unlike most can be modulated. The basic project in the February issue enables you to control a relay remotely from a very small transmitter — and no licensing problems!

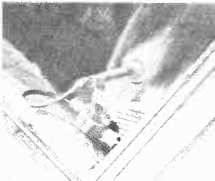
LIGHTNING

A flash of lightning rarely lasts more than a second but the power is immense. The current can reach tens or even hundreds of thousands of amps and potentials are believed to be about 10^8 or 10^9 volts: no wonder Frankenstein's monster sat up!

How lightning occurs and what happens at the ground is far more involved than you'd think. In the next issue Prof. W. R. Lee of Manchester University explains just how dangerous it is.



Electronics & your water supply



Sounds dull? Not a bit of it. As in most fields, electronic measurement of all sorts of parameters is now widespread. Dr Sydenham describes how transducers ensure that our drinking water is monitored.

ETI Cover Price

Sorry folks — up we go to 45p from the February issue. We hope you'll still consider us worth it. You may have noticed that recent issues have been 100 pages and although many are accounted for by ads, the editorial pages have increased appreciably.

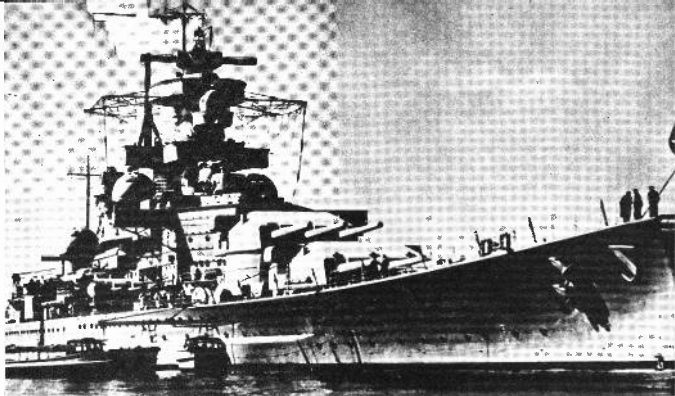
Accentuated Metronome

Not just yer tick, tick, tick but a tick, tick, tock. Don't follow? Well, musical times (eg 3-4 time) are more complex than the regular metronome can cope with — next month's project explains.

Articles mentioned here are in an advanced state of preparation but circumstances may affect the final contents.

OP-AMPS

Following Tim Orr's very popular series on Active Filters, we've twisted his arm to cover OP-Amps in the same way. The feature will not only give the theory but will be heavily spiced with usable circuits.



PUZZLE OF THE DRUNKEN SAILOR

THE MODEL REPRESENTS a ship which has four navigation lights on the port (left) side and four on the starboard (right) side. Unfortunately, a drunken sailor installed 4 green lights in the sockets on the port side and four red lights on the starboard side -- which, as everybody knows, is the wrong way round. Everybody knows too that you don't have four navigation lights on each side -- but never mind that, this is a puzzle.

And the puzzle is to get all the green lights on to the starboard side, and all the red lights on to the port side -- where they belong. That would be easy if you just unplug them and swap

them around, but the rules of the game are that:—

- only one lamp can be moved at a time;
- a lamp can be moved only along the black line and must be put into a vacant socket at the end of the move,
- a lamp can be moved as far as desired on any move, including going round corner;
- a lamp cannot jump over another lamp.

Well that's the puzzle. If you think it's easy -- try it. Just draw the lines on a sheet of paper, use dots for the sockets and use 4 5c and 4 2c coins as lamps.

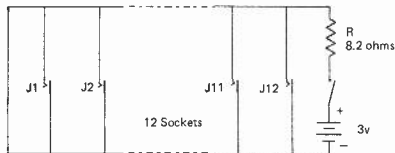
Actually that's all you really need for the puzzle, but to make it more attractive and electronic we used red and green LEDs which light up in the sockets.

Construction

The circuit of course is simple -- just 12 audio sockets connected in parallel, a 3 volt battery, a current limiting resistor, a switch and 8 LEDs which can be plugged in.

The prototype was constructed in a plastic box measuring 140 x 100 x 75 mm with an aluminium panel. Any box about that size would do; construction is not critical.

Circuit diagram Fig 1: The value of current limiting resistor R should be found by trial to keep total battery drain to about 100 mA.




PARTS LIST

RESISTOR
8R2 ½ W (see text)

LEDS
4 Red (TIL 209 or similar)
4 Green (TIL 209 or similar)

MISCELLANEOUS
2.5mm jack socket (12 off)
2.5mm jack plugs (12 off) (see text)
On/off switch (any type)
Hook-up wire
Box to suit
Battery (3 V)

WHAT THE CRITICS SAY ABOUT ETI'S FUN NEW SPECIAL

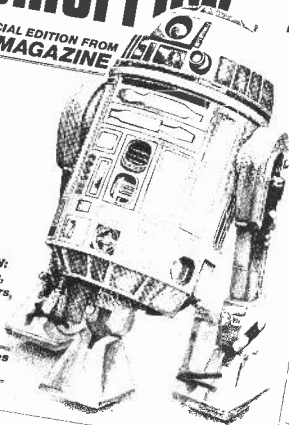


ARNOLD SKULFINGTON
I built the timer, the morse oscillator, the buzz game and the temperature alarm — all using the same PCB design. I really liked the pictures of the ETI staff, I've cut them out and stuck them on my bedroom wall (where the dartboard used to be). I want to learn more electronics so I can build a robot like R2, the internal pictures of the Star Wars robots are really good in Jim Perry's big feature on Star Wars. I asked my uncle to get me one of those futuristic calculators that Halvor Moorshead talks about, but he said that they won't be invented for a couple of years yet!

Apologies to Roy Pullen for messing around with his cartoons, you can see the full glorious, unexpurgated versions in Electronics Tomorrow

electronics tomorrow 75p

A SPECIAL EDITION FROM ETI MAGAZINE



WHAT'S HAPPENING IN:
Projects, MPUs,
Hi-Fi, Calculators,
Video, Audio...

**Behind the scenes
of STAR WARS**



JACK WURTFANGLER
Ron Harris's report from the future has given me many new ideas for developing my hi-fi system — but I disagree with his views on valves, surely valves will never be replaced! After reading Angus Robertson's feature on the future of video I'm thinking of installing a video complex in with my hi-fi — which is based on the system shown in the audio section.



GERRY LEWINKLE
I don't know when I'll find time to build the CMOS switched amp, but I've already started on the power supply — my old one just blew up! The cartoons by Roy Pullen are great, and all those gadgets for building projects (the ones Jim Perry talks about) are going to make electronics a lot more fun.

JASPER OATS
When I convert my TV to a display for my computer (as described in this far-out special edition), what will I do with all the print-out I've got lying around? If Gary Evans is right with his predictions about MPUs, I'll be able to build my own Star Wars robot in about a year's time. With the tips I picked up from Clive Sinclair (wasn't it good of ETI to send Steve Braidwood and Halvor Moorshead to interview him for us), I'll take on the Yanks and Japs with my own robot company — Oats Robotics

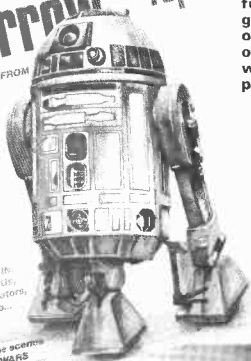


ELECTRONICS TOMORROW

On sale now at your friendly newsagent or direct from ETI for £1 inclusive of p&p. Send cheque or postal order (payable to Electronics Today International) to Electronics Tomorrow, ETI Magazine, 25-27 Oxford Street, London W1R 1RF

electronics tomorrow 75p

A SPECIAL EDITION FROM
electronics today



WHAT'S
HAPPENING IN:
Projects, MPUs,
Hi-Fi, Calculators,
Video, Audio...

Behind the scenes
of STAR WARS

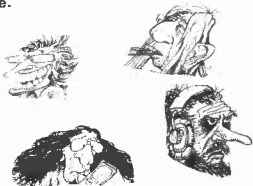


Inside Star Wars — The inside story from the most successful film ever made. Not due for release until later this month, ETI staff travelled to Canada to preview it for Electronics Tomorrow readers. Plus R2-D2 and fellow robots exposed — detailed internal shots show how they were made.

Calculators Of The Future — In the last 5 years prices have dropped and complexity has risen, we don't think prices will drop much further — but the facilities offered will become mind boggling! Halvor Moorshead designs a new model for 1979 and talks about the generation to follow — some manufacturers may think we've been at their research files!



Electronics Tomorrow is the latest fun-packed special from ETI magazine. Available at your newsagent — or direct from ETI. Here are just some of the features, for more details see what the critics say on the opposite page.



ETI Types — Graphically portrayed by Roy (you name it, I'll draw it) Pullen, this pen-in-cheek feature takes a look at the beginner, project builder, audio man and the MPU addict.

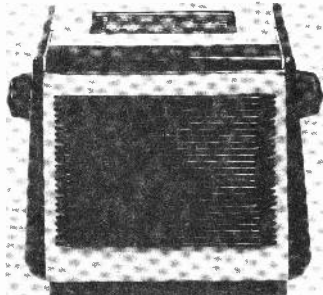
The ETI Story — In the beginning there was no ETI and there was a great wailing from the electronics enthusiasts of the world. Then Modern Magazines said 'Let there be ETI' and there was great rejoicing — read about the history of ETI and see the staff in action (downing pints) with a selection from our scrapbook.



The Sinclair Story — Steve Braidwood and Halvor Moorshead went off (tape recorder, at the ready) to get Clive Sinclair's true life confessions — exclusively for Electronics Tomorrow readers. The man who brought you the world's smallest television talks about his past failures (and successes!) and the possibilities for the future — gripping stuff!

wireless show

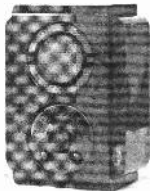
Pete Scott, our visiting Australian hi-fi editor, took a wander through the hallowed halls of the Victoria and Albert Museum to cast his eyes over the vintage radios displayed therein and bring us this report on the ancestors of the 'trannie'.



Decca Deccette 1953 A 4-valve battery portable, using miniature valves of superhet design and with (detachable) mains eliminator base



Left Ekco model SH25 from 1932 and on the right the UAW7B five years older



Left to right A 1948 GEC 4 Marconiphone Personal (would you believe) set (1947) out

THE NOSTALGIA TRIP of 1977 is undoubtedly the 'Wireless Show' at the Victoria and Albert Museum until December 11. The show, which consists of a fine collection of British radio receivers from a period which could loosely be called the 'valve era' is the most comprehensive survey of historical radio receiving sets ever compiled.

Scope

The 130 classic receivers have been chosen as a representative selection of equipment produced between the early 1920s — when regular public broadcasts commenced in Britain — to 1956, when the era could be said to have ended with the introduction of the first British transistorised portable radio.

The show is necessarily restricted in scope by the available space and so does not attempt to give a completely balanced view of the thirty years it covers. Items such as the combined radio-gramophone, or the larger combined radio-TV, are not included. It is also obvious that the exhibits of the larger floor-standing consoles have been limited to allow a greater overall diversity.

Table-standing valve sets — every home used to have one — form the dominant section of the show, but older visitors will have their memories stirred by the earlier units with their free-standing horn speakers.

Background

The choice of 1922 as the starting point is not random even though a great number of the major innovations in the wireless field had already taken place by that time. Marconi had filed his first world patent in 1896, transmitted over the Atlantic in 1901, and speech had been broadcast by Fessenden in 1903.

The first broadcast of speech across the Atlantic had been achieved in 1916, using a transmitter comprising some 300 valves, and the first practical use of superhet techniques for speech broadcast across the Atlantic was made in 1921.

About this time wireless was being used only by experimenters and enthusiasts, who tended to construct their own receivers, although it was estimated that there were some 500 companies manufacturing components in Britain alone.

Wireless at this stage was not used for 'passive entertainment' in Britain, although America was being served by several hundred transmitters — largely unregulated. However, with the formation of the British Broadcasting Company, set up in 1922 to organise regular entertainment programmes through a network of eight transmitting stations, wireless began to have a less esoteric appeal.

So the starting point for the Wireless Show represents the time at which radio started to become a popular commodity. The growth rate in the industry from this time was extremely rapid, as was public acceptance.

The Technical Side

For those interested in the changing technology the show is an interesting aid to tracing technical developments through the thirty years preceding Britain's first transistor radio.

Immediately obvious features include the rapid improvement in tuning facilities, the fight for higher selectivity as the number of transmitters escalated, and the move from battery operated sets (or combined battery/ac) to ac only as more houses were wired up, and then the move back to battery power as portability became a desirable feature.

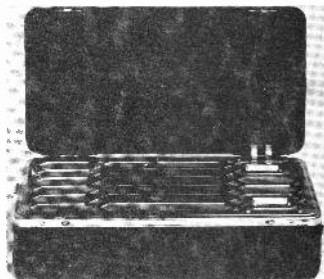
Even the gimmicks and convenience features, such as the 'magic eye', introduced as technological advances slowed in the late thirties, prove fascinating.

Stylistically

The main purpose of the exhibition at the Victoria and Albert, however, is to show the changing styles in the presentation and appearance of radio receivers through the chosen period. Styles that moved from the ornate — almost ornamental — crystal sets of the very early days through to the receivers with intricate wooden cabinets and then to the architect-designed, sculpted-plastic 'creations' which eventually proved too much for the woodworking craftsmen, but which were dropped in post-war austerity.

The show, produced by the V&A in association with the British Vintage Wireless Society, is well worth a visit by anybody who ever built a crystal set. It will give many memories for older visitors and gives a fascinating insight into the background and formative years of radio in this country.

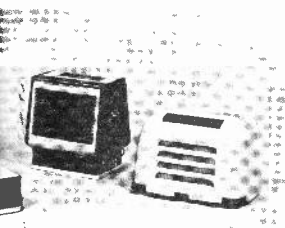
ETI



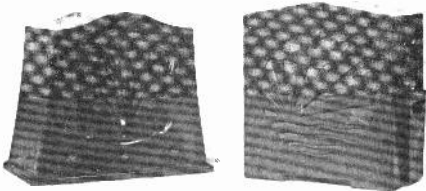
The vastly expensive (£15 19s 6d) Marconiphone personal receiver in close up



Superhet from 1932 and Ekco 3 valve design, could be battery run



friend the Decca gram and a 1950 design by Lawrence Griffin



Marconiphone 1932 model 42 on the left of the Pye MM from the same year

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The TL080 family of BIFET operational amplifiers provides an ideal combination of high-impedance JFET inputs with a low-distortion bipolar output circuit. Quality performance in the TL080 family is achieved without complex circuitry.

TL080 family circuit description

The following sections should be read in conjunction with Fig. 1, the basic schematic for one channel.

Bias circuits

EFT Q16, zener D2, transistors Q14/Q15 and resistor R6 establish the bias currents for the input differential amplifier and the second gain stage. Epitaxial FET Q16 provides a fixed current to D2 establishing 5.2V on the base of Q15. The resulting 317 μ A collector current of Q15 flows through Q14 and sets the current levels in Q1 and Q9.

Resistor R1 causes 196 μ A current in Q1 that is divided between the input stage JFETs Q2 and Q3. The second gain stage bias current, about 600 μ A, is derived from E9.

Input circuit

Input JFETs Q2 and Q3 operate into the active load circuit consisting of Q4, Q5 and Q7. Current imbalance and input offset voltages may be adjusted on the TL081 and TL083 through connections to the emitters of Q6 and Q7. External offset controls for the TL080 connect to the collectors of Q6 and Q7. The C1 compensation capacitor is internal on the TL080, TL082 and TL083, and TL084. For the TL080 connections for external compensation are provided which allow user adjustment of AC characteristics.

Ion-implanted input devices provide very high input impedance, controlled pinch-off voltage for maximum common-mode input range, and matched characteristics for control of the input offset voltage. JFET inputs also allow adequate drive to the second stage resulting in maximum output peak-to-peak capability and wide power bandwidths.

Output stage

Q10 and Q11 provide Class AB bias to the output transistors Q12 and Q13. This allows near zero crossover distortion and produces a low total harmonic distortion at the output. The simplicity of the output circuit results in minimum silicon area requirements, keeping manufacturing cost down while maintaining quality performance. R2, R3 and R4 form the output short-circuit protection network.

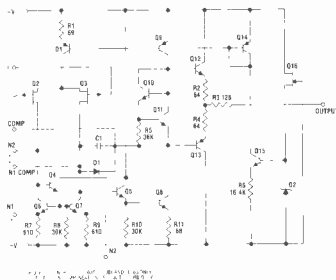


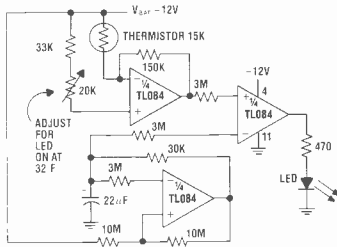
Fig. 1 Schematic diagram for TL080 family

Second stage

Drive from the input stage is single-ended from the collector of Q7. D1 provides a clamping action across Q5 and Q8, preventing saturation

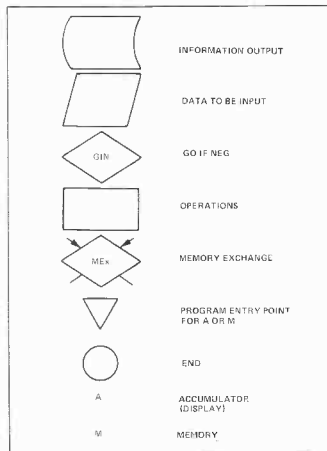
of Q8 and excessive current in Q5. Q5 and Q8 form the high-gain second stage. The second stage output, collector of Q8, drives the output stage consisting of bias transistors Q10 and Q11, and output drivers Q12 and Q13.

Icy Road Warning Indicator



SOFTWARE GAMES

These games for the Sinclair Programmable were submitted by Mr P Cornes of Crewe in Cheshire. A flow chart is given with each listing, so that owners of different machines have a head start in producing a program for their machines.



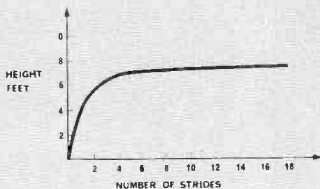
Object — To simulate a show jumping course in such a way that:—

1. The player enters a guess as to how many strides of acceleration he thinks will be required by a horse to clear a fence H feet high.
2. The player is given an indication of right and wrong guesses.
3. The players total score is made available to him at the end of the game.
4. The players score is made dependent on the value of his guesses and on his successfully clearing the fences.

Execution —

```
O/A/V/sto/A/V/goto/0/0/
input H fence 1/RUN/input strides/RUN/right-wrong
input H fence 2/RUN/input strides/RUN/right-wrong
input last H/RUN/input strides/RUN/right-wrong
A/V/Rcl/score.
```

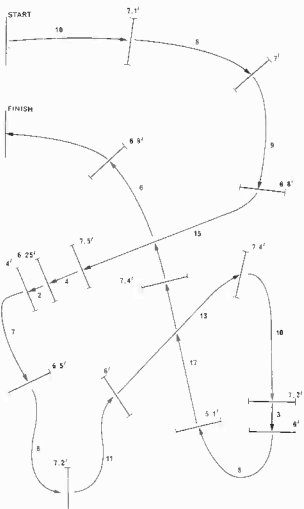
The biggest problem with this program was trying to find a realistic relationship between the number of accelerating strides input and the height that these strides would enable a horse to jump. The following curve shows the sort of relationship that is required.



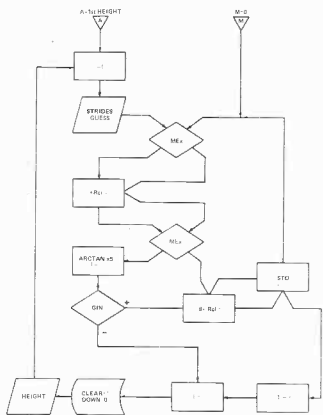
As you can see from the curve the extra height that the horse can jump decreases as the number of strides increases, such that after a certain point no increase in height is gained by increasing the number of strides. This is the sort of curve you would expect in reality. I have simulated this curve by using the arctan function. The tan of an angle can take any value between zero and infinity so the arctan of any number between zero and infinity has a radian value between 0 and 1.57 and you will find that taking the arctan of any number greater than about twenty gives approximately 1.57 as an answer. The only thing to be done now is to scale the arctan values up to give a reasonable range of heights, to do this we multiply by five.

Looking at the plan of the course you will see the path connecting the fifteen fences together. The number alongside each fence is its height (H) and the numbers on the paths between the fences are the distances in strides to each fence. If you input these numbers as your guesses

HORSE JUMPING GAME



Above a suggested course for the horse race game. All the fence heights are given in feet, and the number of strides between the fences



VALUE -VE FOR
FENCE CLEARED
+VE FOR FENCE
DOWN

INPUT STRIDES

UPDATE SCORE
WITH STRIDES
INPUT

CALCULATE
HEIGHT FROM
STRIDES
INPUT

UPDATE SCORE
WITH FENCE
DOWN/PENALTY

FENCE CLEARED/
DOWN DISPLAY
1 = CLEARED
0 = DOWN

INPUT HEIGHT

-	F	06
I	6	01
Stop	0	02
▼	A	03
ME	5	04
-	E	05
Rel	5	06
-	-	07
▼	A	08
ME	5	09
▼	A	10
arctan	9	11
x	-	12
#	3	13
S	5	14
-	-	15
I	6	16
-	-	17
▼	A	18
Gr	1	19
3	3	20
2	2	21
#	3	22
B	9	23
-	E	24
Rd	5	25
-	-	26
Stop	2	27
#	3	28
I	1	29
-	F	30
-	E	31
#	3	32
I	1	33
-	-	34
Stop	0	35

then you are guaranteed to clear the fences but you will find that it is possible to clear most of the fences in less strides than shown.

Your score is calculated by totalling all your guesses round the course and by adding a penalty of nine points for each fence you do not clear. You should consider yourself to be disqualified if you knock down more than four fences.

If you clear every fence in the minimum number of strides you will end with a score of ninety-five but you should consider a score of one hundred and ten or less as good.

When you master this course it is a simple matter to change the heights of the fences and this creates your own course but remember that no fence should exceed 7.6 feet in height or you will not clear it.

UNIVERSAL RANDOM NUMBER GENERATOR—FOR GAMES

Object — To generate a random number of any required length up to eight digits in such a way that each digit can take any value from N to M.
OR generate single random numbers with values from K to L.

OR play an ESP game such that the player has the opportunity of entering a single digit number before the calculator generates a random number, both digits being displayed at the end of the run for comparison and statistical purposes.

Execution 1 —

Any number between 0 and 1
 $\Delta \nabla / \text{Sto} \Delta \nabla \Delta \nabla / \text{goto} 0/0/ \text{f} / \text{ce} /$
 RUN/random digit/ if you require a two digit random number then press RUN again and a second random digit will be displayed alongside the first, a three digit random number, press RUN a third time etc

When you have a random number of the required length and wish to generate another number press the clear button followed by RUN/random digit/ etc. . . .

Execution 2 —

Any number between 0 and 1
 $\Delta \nabla / \text{Sto} \Delta \nabla \Delta \nabla / \text{goto} 0/6/ \text{f} / \text{ce} /$
 RUN/random number/
 RUN/random number/
 RUN/random number/ etc

Execution 3 —

Any number between 0 and 1
 $\Delta \nabla / \text{Sto} \Delta \nabla \Delta \nabla / \text{goto} 0/0/ \text{f} / \text{ce} /$
 Your guess/RUN/random number and your guess
 Your guess/RUN/random number and your guess
 Your guess/RUN/random number and your guess

With the program as it stands the variables take the following values:—

$$N = K = 1$$

$$M = L = 6$$

Obviously with these values the program can be used to simulate the throwing of dice with executions 1 or 2.

When you come to change the variables you should do it in the following way:—

Executions 1 and 3

Chose a value for N between 0 and 10 (integer).
 Chose a value for M and 9 (integer).
 Replace lines 9 and 10 with the value of M - N.
 Replace lines 29 to 31 with the value of N - 1 (including sign).
 Run as per execution instructions.

Execution 2

Chose a value K between 0 and 10 (integer).
 Chose a value L between K and K + 99 (integer).
 Replace lines 9 and 10 with L - K.
 Replace lines 29 to 31 with K - 1 (including sign).
 Run as per execution instructions.

With a moments thought you will see that there are one hundred and one uses for this program, a few of these are given below.

Slot Machine

Use execution 1 with N = 1 and M = 4 and score wins according to the following table.

Display	Win
111	10
222	10
333	10
444	10
221	5
331	5
441	5
11	4
1	2

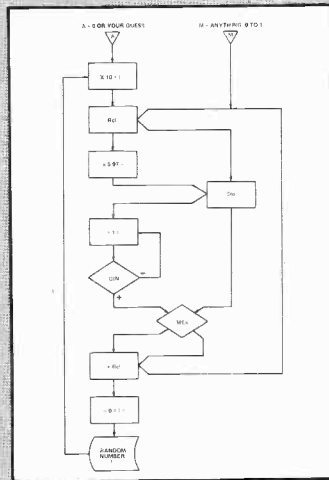
With the values of win shown, the program gives a 95% pay-out.

Race

Use execution 2 with K = 1 and L = number of players (say four). Run the program and each time a number comes up enter a one in the table shown, in the next empty square down, underneath the number displayed. The first player to fill the column below his number is the winner.

Battle

Use execution 3 with N = 0 and M = 5. Each player takes it in turn to enter his own number (one to five) and run the program. When the display appears subtract the smaller digit from the larger and then add the larger digit to this answer. The player with the highest number at the end of the round wins the round. The first player to win five rounds wins the game.





CUTS CARD

Designed by John Miller-Kirkpatrick

LAST MONTH WE completed the description of the System 68 TTY card and described a simple cassette interface circuit that could be used in conjunction with this card. This month we begin describing what is probably the most popular means of encoding data in a form suitable for storage on magnetic recording tape — the CURS format. CUTS stands for Computer Users Tape System and is also sometimes referred to as Kansas City Format.

CUT Above The Rest

Figure 1 shows the basic specification of the CUTS system. From this it can be seen that a serial data stream of eight bits has a number of control bits added to it, much as a TTY has similar control information added to its output. The reason for these additional controls were dealt with in the first part of the TTY interface published in November last year.

Figure 1 also shows that the CUTS

specification calls for a logic '1' to be recorded as eight cycles of a 2 400 Hz tone and a logic '0' as four cycles of 1 200 Hz. These tones have been selected as being suitable for recording on most tape systems and are also easily derived from the master 4 800 Hz clock present in standard UART systems.

The circuit diagrams of the decoder are shown in Figs. 2 and 3. These two circuit blocks replace the equivalent sections of the TTY interface circuitry to provide a complete CUTS encoder/decoder, all memory decoding and UART configuration being identical to that of the TTY card.

Next month we shall deal with the construction of the CUTS card as well as dealing with the necessary software. We shall also deal with means of providing additional RAM and PROM for the System 68.

Before winding up this month however, may we go on to discuss an interesting area of software.

Assemblers and Disassemblers.

An assembler is a program which allows instructions to be entered in a coded form which are converted by the program into a machine code form. Large programs cannot be written without an assembler or similar program to help with address and branch decoding. A disassembler works the other way round, if you feed it with a machine code program it will attempt to convert this back into the coded form used by the assembler. This is useful for documenting programs which have been written originally in machine code.

Mr. G. L. Evans of South London (not our G. Evans) has sent us an example of a routine written in Assembler for use in a disassembler. We hope that Mr. Evans will send us further details of his Disassembler as it progresses. If anybody has a small Assembler we would be very interested in that as well.

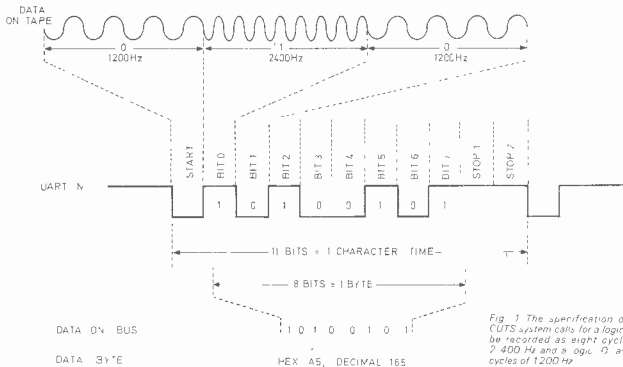


Fig. 1 The specification of the CUTS system calls for a logic '1' to be recorded as eight cycles of 2 400 Hz and a logic '0' as four cycles of 1 200 Hz.

CUTS CARD

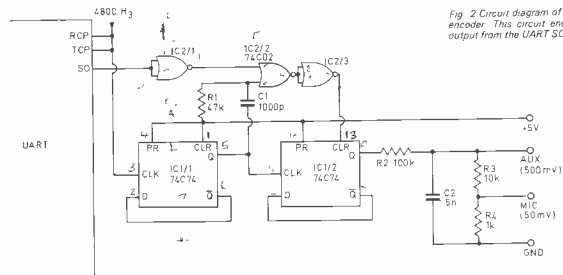


Fig 2 Circuit diagram of the CUTS encoder. This circuit encodes the output from the UART SO output

HOW IT WORKS

Much of the circuitry of the CUTS encoder is exactly the same as that used for the TTY interface described in the November 1977 copy of ETL.

The CUTS format calls for a byte of data to be recorded as a START bit (logic '0') followed by eight data bits with the end of a word being signified by two STOP bits (logic '1'). The setting up of the UART's control registers to conform to this specification was dealt with in the December issue of ETL.

With a data rate of 300 baud each bit time will be equal to sixteen pulse times of the UART transmit clock (4 800 Hz). We require that a logic '1' be recorded as eight pulses of 2 400 Hz and a logic '0' be recorded at four pulses of 1 200 Hz.

ENCODER

The circuit of the encoder is shown in Fig 2. As mentioned above, this circuitry replaces the circuitry associated with the SO output of the UART shown in the TTY interface.

The 4 800 Hz TCP clock is input to one half of the 74C74 Dual D flip-flop

where it is divided by two to provide a 2 400 Hz signal with a 50% duty cycle.

This signal is fed to the clock input of the second half of the 74C74 and, via C1 to the input of IC2/2 a 74C02 NOR gate.

Circuit action is as follows. When SO is low and we require a 1 200 Hz signal, the inverted SO output is fed to IC2/2. A glance at the truth table for a NOR gate will show that the output from this gate must then be low. This output is inverted by IC2/3 and the resultant high applied to IC1/2's CLR input. This input is active low and the clear is thus disabled. This means that IC1/2 will act as a divide by two element producing the required waveform. If now SO goes high, a low is input to IC2/2 after inversion. Reference should be made to Fig. 4 to make the following description easier to follow.

The signal at the C1/R1 junction consists of a series of negative spikes co-incident with the trailing edge of the 2 400 Hz signal at IC1/1's Q output. With a low applied via the inverter, to the other input of IC2/2, the output of this gate will be a series of short positive going pulses, which after inversion, are used to reset IC1/2.

As the 74C74 clocks on the positive edge

of the clock input from IC1/1's Q output but is reset on the negative edge of the same signal, the output of this IC becomes the required 2 400 Hz signal.

The 2 400 Hz or 1 200 Hz output from IC1/2 is fed via a filter formed by R2 and C2 to the AUX output and via an attenuator, R3 and R4, to the MIC output.

The filter is necessary to convert the square wave logic signal to a waveform more suitable for recording on tape.

DECODER

Figure 3 shows the circuit of the decoder, which again, is used to replace the equivalent circuit block on the TTY card.

The output of the recorder is squared up and brought to TTL levels by Q1 and IC2/4. It is then applied to IC3/1, one half of a 74123 dual triggerable monostable. This device has its stable period set to a time that is longer than the period of a 2 400 Hz signal, about 550 μ s is the best. If we now assume that the signal from the tape is of 2 400 Hz, when the first pulse reaches the 74123 its output goes high for 550 μ s. As the input is 2 400 Hz however, after some 417 μ s, the device is retrigged. Therefore with an input of 2 400 Hz the Q output will remain high.

If, however, the signal is replaced by a 1 200 Hz output from the recorder, the Q output will still go high for 550 μ s, but as retrigging will not take place for at least 830 μ s, the Q output will consist of 550 μ s, logic '1' pulses with logic '0' pulses in-between.

The output from the monostable is input as data to the D flip-flop IC4/2. The clock signal for this device is the 1 200 Hz or 2 400 Hz input to the 74123. The D flip-flop is triggered from the low to high transition of this waveform and thus if the signal is 2 400 Hz implying that the Q output of IC3/1 is at '1', the output of IC4/2 will also be at logic '1'. If however the input is at 1 200 Hz, at the moment of clocking, the Q output of IC3/1 will be low, thus the Q output of IC4/2 is also low. The waveforms shown in Fig. X help explain this action.

The Q output of IC4/2 is fed to the SI input of the UART thus completing the recovery of data.

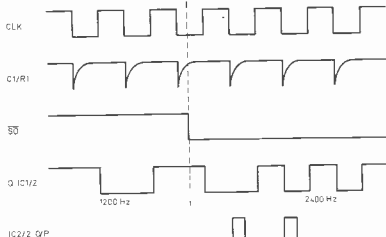


Fig 4 Diagrams showing the various waveforms present in the encoding circuit

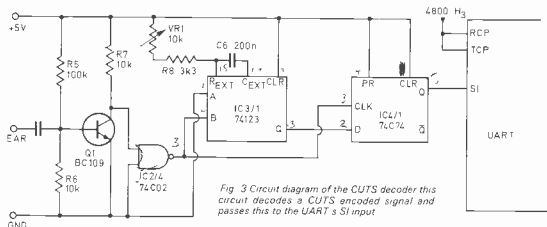


Fig. 3 Circuit diagram of the CUTS decoder this circuit decodes a CUTS encoded signal and passes this to the UART's SI input

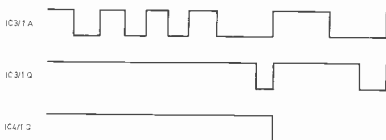


Fig. 5 Diagram showing the various waveforms present in the decoding circuit

SYSTEM CLOCKS

The receive clock pulse RCP used in the decoding operation is the same as that used in the transmit mode (TCP). In order to justify the use of the same clock for both operations we need to study the operation of the UART and do some straightforward arithmetic. (For a full explanation of the terms used below see the UART data sheet published in November 77's ETI).

Figure 6 shows the timing of the UART in receive mode, the data presented to the UART by the CUTS decoder is shown as SI. If we assume that the UART is looking for a START bit then it will recognise the transition of SI from high to low as a possible

START bit. It now waits for eight pulses of its 4 800 Hz clock and then samples the SI line at what should be the mid-point of the START bit. If SI is high at this time then the START bit logic is reset and the UART waits for another high to low transition of SI. If SI is low at the sample time then the UART accepts this as a valid START bit and proceeds to sample the SI line every sixteen pulses of the 4 800 Hz clock. After inputting the correct number of data bits the UART looks for a valid STOP bit (logic 1) at which time it transfers the data and any error conditions to the output registers and signals DAV (Data Available) to the MPU. The MPU accepts the data and status words and resets the DAV line to indicate accept-

ance to the UART which by now is looking for the next valid START bit.

The ideal sampling pulse is shown as Fig. 6A, two worst cases are shown as Figs. 6B and 6C. In these worst case conditions it is assumed that the 4 800 Hz clock used as TCP is also being used as RCP and thus the only variations possible are phase change and frequency change. The phase change problem is overcome inside the UART and thus does not concern us here. The frequency change can only be due to changes in tape speed between recording and playback as the 555 timer used as a 4 800 Hz oscillator is independent of voltage variations in the power supply. If we examine sample pulse train B we can see that the data is being input at a faster rate than expected and as a result the sample pulses end up very close to the end of data bit seven time. As the sample pulse is set during the START bit as being the eighth pulse and the START bit is seven during the fifteenth pulse time of the input data it must change by seven pulses in eight bits (8 x 6 pulses). This can be worked out to an error variation of:-

$$\frac{7}{8 \times 16} \times 100 \text{ percent}$$

$$= 5.46\%$$

On a tape recorder of a reasonable specification this level of tape speed tolerance will not occur and thus the 4 800 Hz TCP can also be used as the RCP clock.

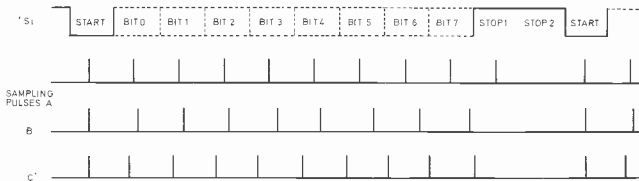


Fig. 6 Diagram showing the effect on the sampling pulses generated by the UART with a difference between TCP and RCP. A shows the ideal sampling pulse (TCP = RCP). B shows TCP - RCP while C shows TCP <- RCP

TECHNICAL BO

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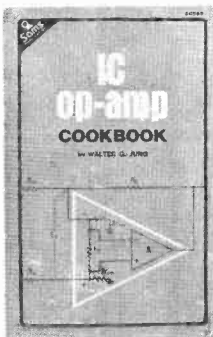
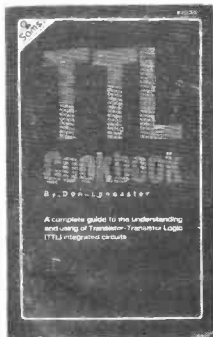
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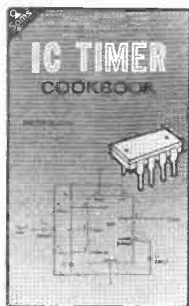
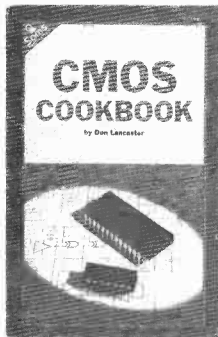
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DIGITAL ELECTRONICS

BY EXPERIMENT

PART 4

IN THIS PART of our series we shall look into sequential logic by using the 7400 IC.

Set the IC up on the board to make a circuit using two of the logic gates as shown in Fig. 1. The gate with its output taken to the LED should have its spare input marked R, while the spare input to the other gate should be marked S.

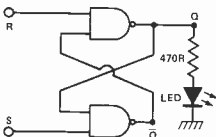


Fig. 1 Cross coupled NAND gates forming an R-S flip-flop

This circuit is a flip-flop, as you may have guessed from the cross-section of inputs and outputs. Complete the table shown in Fig. 2, and note that the output for R = 1, S = 1 is not the same in each case.

Sequential Logic

The R-S flip-flop, as this is called, is an example of a sequential logic circuit, in which the output depends on the sequence of signals at the input—in other words, the state of the output depends on the previous signals as well as the present ones. Strictly speaking this circuit is more of a latch, a circuit which temporarily stores an output while both inputs are high. Note that in normal use, we want two outputs Q and \bar{Q} to be complementary (\bar{Q} is always the inverse of Q) so that the input R = 0, S = 0 must not be used, since this gives $Q = \bar{Q} = 1$.

In logic circuits, clocked flip-flops are much more common. A clocked flip-flop changes state only when a

R	S	Q
0	1	
1	1	
1	0	
1	1	

Fig. 2 Part truth table for R-S flip-flop. When you complete the table taking readings from your lab-board circuit, be sure to work through each state in sequence

timing, or clock pulse is received. This is done by combining the flip-flop action with gating so that the signal inputs have no effect until the gating (clock) pulse arrives.

One type of clocked flip-flop is the D-type, and a typical truth table is shown in Fig. 3. In this type of circuit the signal (0 or 1) which is present at the D (for Data) terminal is transferred to the output at the clock pulse, and remains unchanged until the data changes and the clock pulse arrives.

Clocked Flip-Flop

The type of flip-flop chosen for this board is the J-K flip-flop. This is a more versatile device which combines clocking with gating to achieve a wide range of actions. On the type we have chosen, the SN7476, the action is the type known as "Master-Slave", which means that the input signals are accepted on the leading edge of the clock pulse, but the outputs do not change until the trailing edge comes along. This avoids problems which would occur if outputs were connected back to the inputs, as we shall see later.

The J-K flip-flop has five inputs and two outputs. The inputs are labelled J, K, Clock, Set and Reset (the Reset is sometimes called clear, and the Set terminal is sometimes called preset). The outputs are Q and \bar{Q} , with \bar{Q} always

D SIGNAL	Q BEFORE CLOCK	Q AFTER CLOCK
0	0	0
0	1	0
1	0	1
1	1	1

Fig. 3 D type flip flop and truth table. Note that, unlike the R-S flip flop, changes take place only when the clock pulse arrives

the inverse of Q. We shall check the action of the J-K flip-flop using signals generated on the board.

From previous work you should have available one section of the 7414 connected as a low speed oscillator. This provides an ideal slow clock pulse, and you should already have an LED connected to the output of the 7414 to monitor this pulse.

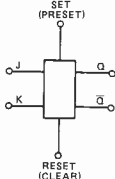


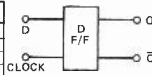
Fig. 4 J-K flip flop symbol

Double Flip-Flops

The connection diagram of the 7476 is shown in Fig. 5. From this you will see that the 7476 contains two J-K flip-flops which are completely independent. For the first series of practical exercises we shall use only one half.

Solder connections from pin 13 of the 7476 to earth, and from pin 5 to the +5 V line. Now solder an insulated wire connection from the clock oscillator output to pin 1 of the 7476, so that flip-flop number 1 is activated.

Connect pins 4 and 16 to earth so that J = 0 and K = 0, and connect switches so that the reset pin (pin 3) and the set pin (pin 2) can be connected momentarily to earth as needed. The



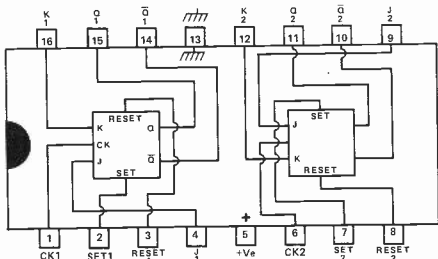


Fig. 5 Pinout of the SN7476 dual master-slave J-K flip flop

circuit is now as Fig. 6, and the appearance of the board is shown in Fig. 7.

Now connect a resistor from pin 15 (Q) to a spare pad, and an LED from the spare pad to earth. This LED will indicate the state of the output from the flip-flop at Q.

Switch on, and look at the LED. Using the SET switch, set the output to give logic 1 (This happens when the SET switch is returned to 0, whatever the clock pulse is doing at the time). When the switch is changed back again, does the output change at once? Or when a clock pulse arrives?

These changes and others to follow may be easier to observe if the clock pulse is very slow, and a 1 000 μ F, or greater, capacitor may be used in the oscillator circuit. Later, a "debounced" switch will be used.

Complete the sequential truth table, in which Q_{n-1} is the value of Q just before the clock pulse arrives, and Q_n is the value of Q just after the end of the clock pulse (the 1 to 0 change). Can you decide when the change, if any, occurs? Is it on the leading or the trailing edge of the clock pulse?

Now, switch off, and disconnect one end of the link between K pin (pin 16) and earth, so allowing K to float to 1. Now we have J = 0 and K = 1. Switch

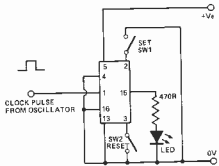


Fig. 6 Circuit for checking J-K action, see text for details

and observe the output. Change the output by using a switch (which one will you use SET or RESET?). Does the clock pulse affect the output after the switch has been returned to normal?

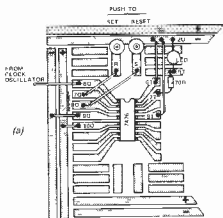


Fig. 7 (a) The layout on the board, with the LED in position
(b) Form of part truth table

Switch off again and reverse the connections so that J = 1 and K = 0, and repeat your readings. Enter all the readings on the sequential truth table of Fig. 8.

J=0 K=1	
Q_{n-1}	Q_n
0	0
1	1

J=1 K=0	
Q_{n-1}	Q_n
0	1
1	0

J=1 K=1	
Q_{n-1}	Q_n
0	1
1	0

Fig. 8 Remaining truth tables for J-K action

From these exercises you will have found that the action of the J-K flip-flop can be controlled by the J and K inputs, which act to force the output to either 1 or 0 when the clock pulse arrives. The SET and RESET pins act independently of the clock, making the output go to 0 or 1, and holding it there until the reset or set voltage rises to 1 again, when the next clock pulse will cause whatever output is forced by the J and K voltages.

Toggleing

With the power off, disconnect the wires from both J (pin 4) and K (pin 16). Switch on again, and observe both the output and the clock LEDs. Now complete the truth table of Fig. 8 (c). In this arrangement the J-K flip-flop is acting as a divide-by-two stage, for there is one complete output pulse for each two complete input pulses — we say that the flip-flop is *toggleing*. At any time during this action, the output may be forced to 1 or 0 by the action of the SET or RESET pins, but it will revert to the toggling action when the SET or RESET is released.

Try applying a clock pulse obtained from a switch, as in Fig. 9 (a). Wire the switch to the board and replace the connection between the 7414 clock generator and the flip-flop with a connection from the switch output to the flip-flop clock input. Turn on the 5 V supply, and use the switch as a slow clock generator. You will probably find that the output is erratic, sometimes seeming not to change the output when the switch is operated.

This is caused by switch contact bounce.

De-Bounce De Switch

With power off, rewire the switch with a resistor and a capacitor to one of the spare sections of the 7414, as shown in Fig. 9 (b). This is a simple de-bouncing circuit.

Solder a resistor and an LED to the output of the 7414 in the usual way to show the state of the clock pulse, and connect the output also to the clock input of the 7476. You should find that the action is perfect, and the very slow clocking which is now possible will show that the changes which take place at the output do so when the clock pulse goes low, that is, from 1 to 0.

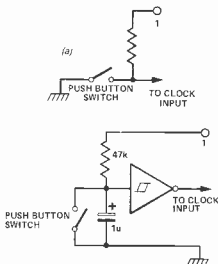


Fig 9 (a) Using a push-button switch as a clock pulse supply
(b) A debounced switch circuit

Note that other flip-flop types may not have the same sequence of actions. Some, for example, are edge triggered, meaning that all the flip-flop action takes place on the leading edge of the clock.

When you are using flip-flop circuits, you must be careful to use the same type of flip-flop as that specified, since circuits which suit one type may not suit another. In particular, the 7476 "Master-Slave" type of flip-flop has a particularly complex action.

In essence, the action is that on the leading edge of the clock, the information which is present (1 or 0) at the J and K inputs is stored and once the clock pulse has reached its 1 value, these inputs are reached out, meaning that changes in J and K will now have no effect. At the trailing edge of the clock pulse, the flip-flop action takes place to change the output. The reason for this construction is that several types of circuits, some of which we shall build in this series, use feedback connections between the output of the flip-flop and its J or K inputs.

If all the action of the flip-flop,

Fig 10 Truth table for J-K flip flop

(a) Complete truth table

J-K FLIP-FLOP

INPUTS		OUTPUT	
J	K	Q BEFORE CLOCK	Q AFTER CLOCK
0	0	0	0
0	0	1	1
0	1	0	0
0	1	1	0
1	0	0	1
1	0	1	1
1	1	0	1
1	1	1	0

happened at the leading edge of the clock, such feedback would cause indeterminate action — any change in Q would cause a change in J or K, which might cancel the effect on Q, and the flip-flop would probably oscillate at the high frequency. Because of the Master-Slave action, this does not happen — the changes in Q happen at the trailing edge of the clock pulse, by which time the J and K inputs are locked out and their voltages cannot affect the action until the leading edge of the next clock pulse.

Investigation

You should already have one section of the 7414 set up as a high frequency oscillator with earphones, or similar, to detect the output note. What is the effect of leading the output of the 7414 oscillator to the clock terminal of the 7476 with J = 1 and K = 1? Listen to the output wave from Q and compare it with the signal from the oscillator.

Can you now design an "octave" oscillator? This circuit will use a single oscillator, but its output will be alternately at oscillator frequency, then at half oscillator frequency (one musical octave below) according to the input to the gate. The gate input could then be obtained from another slow oscillator.

Finally, Fig. 10 (a) shows the complete truth table for the 7476. Fig. 10 (b) shows a changes truth table, in which the settings of J and K to produce certain changes (or non-changes) are listed. In the last table, X means "don't care", signifying that the value may be 1 or 0, and the action will be the same. Check that this last table agrees with the full table of Fig. 10 (a).

You may want to copy these tables, since we shall refer to them several times in Part 5 of this series.

ETI

READERS FOLLOWING THIS SERIES SHOULD REFER TO THIS MONTH'S LETTERS PAGE FOR DETAILS OF SOME APPARENT CHANGES TO THE BOARD USED IN THESE ARTICLES. WE APOLOGISE FOR ANY CONFUSION THIS MAY HAVE CAUSED.

To be continued.

(b) Shortened truth table for changes only

J	K	Q _{n-1}	Q _n
0	X	0	0
1	X	0	1
X	1	1	0
X	0	1	1

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A RECENT heated discussion between several hi-fi enthusiasts here brought to light several interesting points. The first was the number of similarities which exist between the fairer sex and hi-fi equipment!

Think we're joking eh? Well consider: both tend to dominate the room they're situated in. Both are capable of generating very high sound levels, but will stay absolutely silent if turned off or ambient conditions are not favourable to smooth operation. Upkeep on both is horrendously expensive, and requires constant purchase of software (wear) and cleaning materials.

In fact the only major difference detectable occurs when the specimen blows a fuse. One variety refuses to make a sound, while the other demonstrates incredible slew-rate and reaches 200 dBA in a microsecond.

Class E Birds?

Be that as it may, our German edition has sent us news of the missing E amplifier configuration. We shall assume here that you've all read the article on class G in the last issue. If you haven't... go directly to jail, do not pass GO, do not collect £200. As you now know then Hitachi

attempted to call their Dynaharmony circuit class E when it first appeared, but found that classification already reserved.

And now we know who by: Arcus. Their DPA 320, shown in Fig 1, is a 200 W RMS per channel power amplifier—class E. Basically this configuration would appear to be a digital system, using pulse width modulation to control the output transistors.

A 100 kHz square wave is generated within the amplifier by means of a crystal-locked oscillator, and integrated to produce a triangular wave.

This wave is then superimposed on to the incoming music signal, this being put through a very fast A-D converter, the end result of all the logic circuitry producing a pulsewidth modulated square wave. Fig 2 shows a sine wave with the square wave produced by the logic alongside. The square wave is now used to switch the output transistors on and off very rapidly, the on time depending on the widths of the incoming pulses.

In this manner the music signal is reproduced, but theoretically without the inherent faults of the transistors affecting it. Using the output stage like a switch is not new — Quad's 405 current dumper does this, but in a different manner.



Fig 1 The Arcus DPA 320 power amp. Producing some 200 W per channel this digital design is claimed to be totally free of crossover distortion, TID and all other bipolar amp vices!

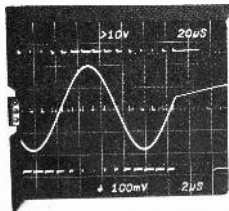


Fig 2 A sine wave and its equivalent pulsewidth modulated square wave. In a class E power amp this would hopefully induce the output stages to reproduce the sine wave!

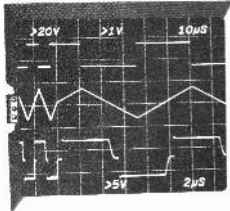


Fig 3 The middle trace is the triangle produced by the 100 kHz square wave signal within the DPA 320. This triangle is then superimposed on the digitised music signal to control the power switch output pair.



Spray now, play later — Sound Guard takes your highs to a ripe old age

To keep operation symmetrical the transistors are not pushed totally into saturation and this allows 'recovery' from each switching operation to occur more rapidly. Contrast this to class D switching amps which operate by completely saturating the output pair in turn. Class E is 10 times faster to 'recover'.

Those interested in further details can look up the patent on the process (No 1444201) or contact Arcus direct in Germany (*Don't mention the war!*) at: Elektroakustik GmbH, Teiltower Damm 283, 1 Berlin 37, Postfach 370 370.

Don't Wear It — Spray It!

An interesting spin-off from the space programme is to be marketed in Britain by Pysler Ltd. Called Sound-Guard the product is a spray preservative for LPs. (Just around this point in the proceedings all the usual spectres of gunged-up records and glue-ridden styli ploughing through seas of dust attracting *substances* should leap into the enthusiast's mind. They don't? . . . Sorry!)

The compound was originally produced by NASA as a dry lubricant for use in conditions of hard vacuum and high temperatures. Development has now taken it into the form of a liquid spray.

This is applied to the LP surface, and immediately polished up. A coating five millionths of an inch thick is apparently formed across the record and groove walls. The basic property of Sound Guard is that it will not bond to itself, so that once applied a build up on the surface is just not possible, thus alleviating the horrors associated with such an occurrence.

Benefits claimed are a cancellation of increase in harmonic distortion due to wear, reduction of surface noise generated by stylus wear, and a preservation of high frequency response by protection of the delicate groove modulations for those frequencies.

To The Test

To test these assertions, we decided to set up an A/B comparison on a Sound-Guard treated LP. This was achieved by purchasing from our local record emporium two (different) LPs in as good a condition as could be managed

(after several return trips to dispose of copies with extra radial grooving) and recording these at 15 ips.

One LP was then treated with the fluid, simply by spraying on and rubbing well in with the pad provided. No trouble here — once buffed up properly no audible deterioration could be detected, and certainly the noise level was not affected. Nothing appeared round the stylus either!

So far, so good.

Both records now went into the collection as normal, and were played over a period of about a month, no special care being taken to differentiate them from any other LP other than noting when each was put under the needle.

The test was called to halt when we ran out of time on this report. Things were evened up so that the test side of each had been played the same number of times, thirty-one in fact. Yes we *do* play a lot of records.

Masterful Comparison

Each could now be compared with the master tape made at the time of purchase, and the by now obligatory listening panel was assembled to haggle over results. This time however no haggling was necessary, and the results could be unanimously agreed. The Sound Guard treated LP had definitely 'held' the high frequencies better than the untreated record.

On direct comparison with the tape, there was no doubt whatsoever that the treatment had preserved the frequency response to a clearly audible degree. Most people do not realise how quickly extreme high frequencies are worn off an LP, even at low tracking weights. Our tests were conducted at 1.2 g and so heavier weights would presumably show benefits earlier and to a greater extent.

For The Record

No conclusions could be drawn, however, as to whether Sound-Guard had achieved a favourable result with regard to surface noise—both LPs were still in excellent condition. As it is, we have no hesitation in recommending Sound-Guard as a worthwhile addition to the audiophile's armoury, it's worth its cost if it only prolongs the life of two LPs after all and one bottle does 25. Price: Full kit (see photo) £4.99. Refill £3.25 (inc. VAT). Pysler Ltd., Fircroft Way, Edenbridge, Kent.

Aiwa The Lads

And so to our main news this month, a cassette deck with several important differences. Recent models from such noteworthy manufacturers as Nakimichi, Sony, Technics and Aiwa have shown a search for something other than that last few kilohertz at the top of the range. And now Aiwa have come out with the AD 6800 which they themselves consider "as far as one can go with cassettes," and have equipped the machine with the facilities to let you know just how far that is!

Bias Your Opinions

With all the various tape formulations on the market today the age old compromise inherent in not optimising a particular machine's bias for a particular brand is becoming ever more irksome. While being fairly satisfactory in general there is no flexibility in this system at all, and no user control since such adjustment has always had to be done by a dealer. All the user could do was to set a single three position switch to 'Fe-Cr', 'CrO₂' or 'LH'.

What has been needed, and Aiwa have now provided (else we would not be rambling on about it) is some simple user controlled system to set up the machine for any brand of tape desired, and obtain the maximum fidelity from it. Let's face it at 4.8 cm/sec and 1/4in wide we need all the help we can get. Too high a bias current results in high frequency roll-off and increased distortion, and a balance has to be achieved.

On the 6800 the facilities to optimise bias are built-in oscillator, test head, switched meters with filter, azimuth adjustment and two three-position switches for bias and equalisation, backed up by the three 'fine adjust' bias controls. All this must add a considerable amount to the cost of the machine, and shows how seriously Aiwa take the cassette. (Wonder if they'll come up with an Elcaset?)

Self Satisfied Unit

Before we move on to show how the bias adjustments are made, and what effect they have on performance, let's consider the rest of what the AD-6800 has to offer. The finish is superb, and the controls are smooth and positive. Everything about it looks — and probably is — very expensive.

The meters are a revelation in themselves. Two needles, peak and VU reading, are provided for each channel with excellent ballistics. The peak reading facility really is peak reading, not some cheap approximation, and is switchable from peak reading to peak hold, or even to off if you feel like.

The hold facility makes setting up to record very easy. Just lock the hold on, and advance the record level until the needles move onto the level you want to set at. No getting eye-jump trying to watch cavoring little needles avoiding 0 VU, and much improved recording as result.

Even loading this animal is different. In short you don't — it does it itself. Press the open key and the door swings up and over in an almost seductively damped manner. Facing you now is the cassette carrier. Put the tape in and give it a gentle push (or close the door) and the machine jumps to life, takes the carrier out of your hand and locates the cassette itself, all with a mechanical whirr of efficiency. Now I know it's only a little motor set to activate upon movement of the carrier, and I know it's silly and probably a gimmick — but it's still beautiful!

When the 6800 arrived here for review it was hours

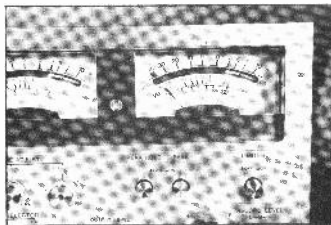
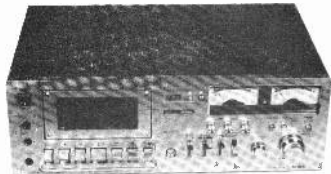


Fig 1 The twin needles meters show clearly the peak facility is on here, and the reading is thus of the highest level which passed through the circuit on the last segment



before we could actually play anything on it, since the entire office staff from receptionist to technician insisted on having a play with the loader. On a practical note, the auto-load does mean that the tape itself is less liable to be mishandled and the drive mechanism can be mounted further into the case with all the attendant advantages of dust avoidance. A conveniently placed head cover makes cleaning easy.

Reviewing Review

Another very useful facility is the review/cue mode. With the 'FWD' key depressed operating rewind reverses the tape direction as normal, but leaves the head in contact with the tape so that an audio signal at reduced level, appears at the output. Very handy for locating the end of tracks on recordings. The fast 'FWD' keys work in a similar manner to allow you to 'CUE' up quickly to the end of a piece. If used continually no doubt head wear would be accelerated, but Aiwa contend that for the amount of use the facility will see in terms of playing time such additional wear will be negligible and well worth the facility. In our opinion a fully justified contention.

Finding Your Type

Using the bias tuning is simplicity itself. Let the machine load a cassette (don't fight it — use it) put it into the record mode, with input selector at Test and Dolby off

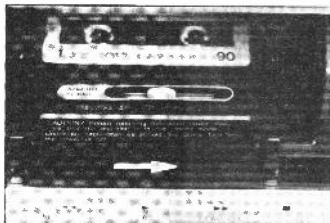


Fig. 2 The azimuth adjust control within the cassette compartment. This is used in conjunction with the 8kHz oscillator and the right hand meter in obtaining maximum level and hence correct alignment.

This allows the internal oscillator to put its signal onto the cassette. Both meters now deflect. The right channel meter indicates 8 kHz level, and the left 400 Hz. The test head itself is aligned by adjusting the slider inside the cassette compartment for maximum 8 kHz level.

To optimise the bias set the coarse control to the correct formulation, and adjust the fine control until both meters read as equal as possible. It takes longer to describe all this than it does to do it, and just to make it even easier, the fine control you should be using is illuminated as soon as the coarse bias is set. CrO₂ switching is automatic.

Aiwa intend all this to be used to obtain a flat frequency response by setting equal levels at 400 Hz and 8 kHz. Of course if the tape type in use sounds a little 'dead' at the top end, you can always leave a few dB extra on that meter.

We tried the 6800 on a whole range of cassette types from TDK SA to BASF LH Super taking in CrO₂ and FeCr on the way. Results with all tape types were first class, but even using the fine tuning, the 6800 seems to display a preference for TDK Super Avilyn. Results with this tape were the best we have ever heard from a cassette deck, the sound displaying a clear and open nature with little of the usual stricture associated with the medium.

Ferry Chrome Carried?

With FeCr tape it was necessary to tune considerably from brand to brand, but once achieved the correct setting delivered a very good recorded performance. The results with CrO₂ tapes were frankly disappointing. The sound never approached that of the SA recordings, and some difficulty was experienced in following through the setting-up procedure. We feel this is a minor drawback however, in view of the outstanding qualities displayed with both FeCr and Super Avilyn, and the excellent LH results.

Without doubt the bias controls of the AD6800 added considerably to the unit's versatility and allowed wide variety of cassette tapes to give of their best. The variation in sound quality with tuned settings is surely to be expected, after all some tapes are better than others! If you are looking for a machine that takes cassettes seriously, and are prepared to pay for it (in the

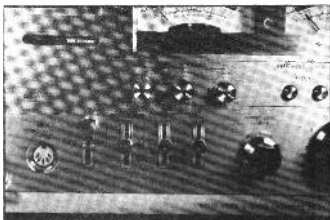


Fig. 3 Close-up of the clever bits. Above the general input controls can be seen the bias fine adjust control which allows tuning up for each tape formulation available. The control (to be used) is illuminated once the input is set to Test.

region of £400) then this unit merits top place on the shopping list. It costs a great deal of money, but has much to offer in return.

Manual Labour

In conclusion this month, one parting shot across the bows of the Japanese giants — Aiwa included. The standard of the instruction manual with the AD 6800 is typical of such publications — abominable! Production and layout are nicely done, but the English — oh the English! It's been said before and now we've said it again. Please please please someone somewhere convince the powers that be and get the instructions up to the unimpeachable standards of the hardware.

ETI

SPECIFICATION

Frequency Response	According to DIN 45 500 LH tape 25–15,000 Hz CrO ₂ tape 25–17,000 Hz Fe-Cr tape 25–18,000 Hz
SN Ratio	According to DIN 45 500 64 dB (Fe-Cr tape DOLBY NR ON)
Wow & Jitter:	According to DIN 45 500 0.1%
Tape Speed	4.8 cm/sec. (1-7/8 ips)
Revolutions:	90 sec. (C-60)
1-1/2 I.D. 1-mc	90 sec. (C-60)
Bias Frequency	100 kHz
Motor	38 pulse FG Servo Motor
Tape Head	Cartridge Guard Head (FGH)
Distortion:	0.9% (400 Hz) 0 VU, Fe-Cr (r tape)
Input levels	Microphone sensitivity 0.25 mV impedance 200R to 10 k
1 mc	sensitivity 50 mV impedance over 50 k
DIN	sensitivity 0.1 mV/k impedance 3 k
Output levels	Line: 0.775 V (0 VU) optimal load impedance over 50 k DIN 0.775 V (0 VU) optimal load impedance over 50 k Headphones load impedance 8R to 150R
Power Consumption	20 Watts
Dimensions	450 W, 162 H, 335 D (mm)
Weight	10 kg

microfile

This month Gary Evans takes the hard work out of finding a way of producing cheap hard copy, at some new educational items from Heathkit and how to nobble your AGC which can give trouble with digital signals.

May I begin this month by asking you a question? Yes? — No, hold on! that was not the question that comes next

Heath CUTS

If I were to ask you if you would be interested in an impact printer that produced copy with a thirty-six alpha-numeric character set on eight inch-wide paper with sixty characters per line and five lines per inch for less than a hundred pounds, what would be your answer? If it's No then suppose I threw in a keyboard which was capable of generating seven bit ASCII codes with parity? Still No? Well let's also throw in a UART making the terminal TTY or CUTS compatible. If you're not yet sold on this device what about reducing the price to less than ninety pounds? If having read this far and still not become very interested in the specification evolving I can only assume that you mistook this column for news about a new item for your tool-box (shades of needle file?)

Why have I dreamt up this machine that would answer most micro users' prayers? Well the answer is that it is no dream. I have been sent details of just such a device, the DTS 77 data terminal. I shall try to get hold of one of these beauties and tell you all about it when I do. In the meantime further details may be obtained from:—

**Heath E & M,
26 Broad Street,
Lyme Regis,
Dorset.**

Heath Kits

A few months ago I mentioned that Heathkit had launched the H8 personal computing system, in the US. This interesting piece of hardware is yet to make it across the great divide but rumours have it that the middle of next year should see its UK launch. Microprocessors do, however, have a foothold in the range of kits that Heath offer on the UK market. The microprocessor flag is being waved (set) by Heath's microprocessor course and computer Trainer package (Heath references FE 3401 and ET 3400 respectively).

These follow the lines of their by now familiar to connoisseurs of the Heath range continuing Education Series. The format of these courses follows the same basic pattern of providing a 'learning program' which is a comprehensive set of notes dealing with the theory of the subject to be covered — in addition practical experiments are described in the text. These experiments can be carried out with the 'trainer' that is designed to complement each learning program. These trainers incorporate a breadboard area together with all the components necessary to carry out the experiments described.

At the end of each section a self-evaluation quiz allows one to assess the progress that one has made during each unit of study. Until recently the courses covered basic AC and DC theory plus Semiconductor Principles and a Digital Techniques course.

The MPU course is the latest addition to the range and looks as if it could be a good way of getting to grips with Micros. I have not yet managed to get my hands on one, but from the photos and description shown in the new Heath catalogue, it looks good.

Based on the good old 6800 supported by a 1K ROM monitor, with 256 byte RAM plus other components and breadboard area, Heath say it should prove a valuable teaching aid. It should provide a means of gaining familiarity with machine language programming, hardware I/O interfacing, micro theory and design applications.

With data input via a hex keyboard and display of data plus address on seven segment LEDs, to use the trainer is easy. It is an expensive item and has limited applications — in that it cannot be easily expanded to form part of a larger system. It was not designed for this latter role however and should together with the learning program provide very valuable hands-on experience. For further details of these new items from Heath see their new catalogue. For a copy of this contact Heath at:—

**Heath (Glous) Ltd
Gloucester
GL2 6EE**

A Corrupting Influence

Referring to a past microfile last month I mentioned the SERT MPU lectures at Kent University during late September. Lack of space last month prevented me from saying much about it — and it looks as if much the same thing has happened this month! So just another titbit from the event.

The idea came from R. A. Smith of Essex University and concerns the use of low-cost cassette recorders

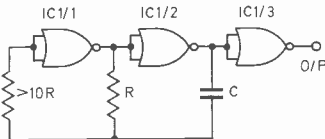


Fig 1. Circuit of oscillator to produce signal suitable for disabling AGC circuits. Select R and C to give frequency of about 18KHz ($t = 2.2RC$)

when recording data output from a micro system. It is a technique to overcome one of the problems often associated with this type of recorder — namely unwanted action of AGC circuits.

In the less costly recorders these AGC circuits, ideal for recording speech, often cannot be switched out of the signal path. When recording any form of digital data the action of such a circuit will be to corrupt it. Consider for example a gap in the recording. The AGC will increase the gain of the input signal, thus increasing the likelihood of noise or transients upsetting the recording.

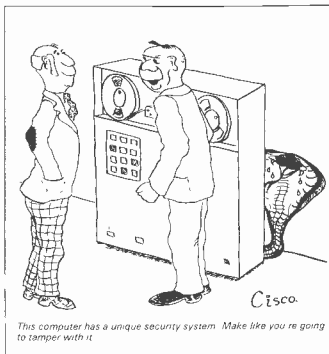
Now we get to the clever bit — by superimposing a continuous HF signal on the, usually, LF data signal the action of the AGC can be nullified. How? Well, we arrange for the HF signal to be outside the response of the tape, usually not much more than a few KHz on the cheaper machines, but within the response range of the AGC processor.

Thus the AGC circuits 'think' that there is a continuous high level present at the input and keep the recorders gain constant.

A simple CMOS oscillator can provide the required bias signal, and be mixed with the data just before being fed to the recorder.

A simple idea that should improve the performance of these low-cost storage systems.

ETI



This computer has a unique security system. Make like you're going to tamper with it.

WE'RE OUT TO FINISH YOU OFF!

Rapitape *
eti PANEL TRANSFERS

WOOD MAGS PPH no 1

GOOD AND PROPER!

... or at least your projects. If there is one thing which is impossible to do at home is lettering front panels to professional standards. At least until now. If you cast your eyes right a while you'll see our new panel transfers sheet, which has been carefully designed to allow you to do exactly that.

The transfers are easily rubbed down, and the two sheet set contains a mass of lettering and —uniquely— control scales for both rotary and slider pots.

Each sheet measures 180mm X 240mm and comes packed flat in a stiff cardboard envelope 'no' protection. There should be enough, for dozens of projects here - and the longer you wait the worse they'll look!

Send £1.75 (includes VAT and postage) for the two-sheet set to:
Panel Markings
ETI Magazine,
25-27 Oxford Street,
London W1R 1RF.

ELECTRONICS TOMORROW

by John Miller-Kirkpatrick

JUST A COUPLE of weeks to Christmas and you haven't yet thought what you would like Father Christmas to bring you in your stocking this year? Its time to leave extra large hints lying around, if you feel like dabbling with your TV games unit try leaving this article in a place where Father Christmas is sure to find it!

Christmas Colouring Kit.

If you have one of the black and white TV games based on the GIAY-3-8500 TV games chip you can now upgrade it to colour. Watford Electronics have a kit to upgrade this type of unit to give effects such as a green court, red boundary and score, yellow left bat and blue right bat. The kit includes a UHF modulator so that you can plug the game into the aerial socket of your TV. If your game was built from a kit which never quite worked then this add-on might be just the excuse to dig it out of the 'not quite completed' projects pile. If you still don't feel like trusting your ability to build such a unit you will be pleased to hear that Watford can supply it built, tested and even installed in your own game. For details see their advertisement.

Other Upgrades and add-ons

Another way to improve your TV games unit is to change the chip for the AY-3-8550 which gives additional horizontal bat control together with a few other improvements. The chip is pin compatible with the AY-3-8500 and requires only an additional potentiometer in each hand control to complete the modification.

Alternatively you could start almost from scratch with the AY-3-8600 chip which gives a total of eight games including Gridball, Hockey and Basketball. The AY-3-8550, AY-3-8600 and PCBs, kits, etc are available from Telecraft, for further details see their advertisement.

Add-on Music.

If you already have enough of the above modifications or think that they will only cover Christmas day and you are looking for something to occupy you on Boxing Day then how about making out a list of components for 'Father Christmas' to enable you to experiment with this idea?

The TV games chips described use something like a 2MHz oscillator to generate all of the timing signals including sync. If this oscillator were also divided by

about 4 and gated so that it was enabled only inside the 'court' or visible signal time of a TV game then it should be possible to divide up the court into several horizontal sections. If the sync signals are counted (and reset during court) then the court can be similarly broken up into several vertical sections. A little additional logic will allow you to display several 1 in or so squares on your TV screen. With your colour modulator kit you can also define the colours of the squares and define how the colours are allowed to change.

Now all you need is an audio signal, a bit of filtering, a few BC109s and suddenly you have your own multi-option fourth TV channel. For additional mind-bending experiences try adding the TV games signals and your generated music signals to give a multicoloured court!

1978

1978 will bring some pleasant surprises in the TV games business with some cassette or cartridge units already available. At first there will be a great divide in the market between GRAPHICS games such as those already available and BASIC games played in question and answer form. Eventually these will become combined in some really interesting TV games units — stay tuned to ETI for more information!

Software Made Simple

I have been involved in writing a lot of software for various applications over the past few months and I thought that some of the techniques I use might be of interest.

First of all get yourself a hardback or loose-leaf notebook of a reasonable size to write down all of your attempts — there is nothing worse than having to rewrite a routine from scratch because you have lost the cigarette packet which had the original notes on the back.

Decide roughly what the routine will do, a rough flowchart plus an idea of any fixed stack assignments, sub-routines, etc. Convert this to a first draft machine code listing with notes and labels but leave plenty of room for additional, insertions and changes. Looking at some of my roughs and comparing them to the finished product it seems that nearly every other line has alterations.

Having decided what you think the machine code should be sit down at your MPU and try it. For most sub-routines you will probably have to set up a calling routine to test it, this routine simply sets up any parameters used by the sub-routine and then calls the routine. Do not bother to enter more than about 10 instructions at a time because the likelihood of having to shift them all is very high. At a convenient point enter an instruction to generate a Software Interrupt so that the MPU will perform the code entered so far and then return to a routine which will allow the results so far to be checked. In most 6800 systems this will be a 3F instruction.

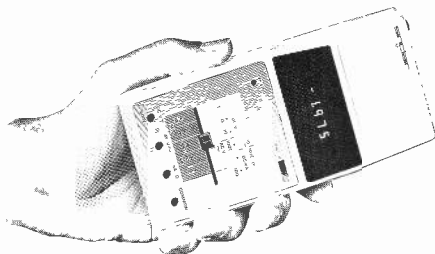
If the results so far are those expected then another 10 instructions can be entered and another 3F instruction inserted etc etc. Any changes to the original coding should be made to your original notes immediately after the change has been verified on the MPU.

Branches to parts of the routine which are not yet coded are easily handled by branching to a 3F instruction or back into a loop until the condition changes. This allows one side of the branch to be coded before attempting to do the other.

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The Sinclair PDM35.

A personal digital multimeter for only £29.95



Now everyone can afford to own a digital multimeter

A digital multimeter used to mean an expensive, bulky piece of equipment.

The Sinclair PDM35 changes that. It's got all the functions and features you want in a digital multimeter, yet it's neatly packaged in a rugged but light pocket-size case, ready to go anywhere.

The Sinclair PDM35 gives you all the benefits of an ordinary digital multimeter – quick clear readings, high accuracy and resolution, high input impedance. Yet at £29.95 +8% VAT, it costs less than you'd expect to pay for an analogue meter!

The Sinclair PDM35 is tailor-made for anyone who needs to make rapid measurements. Development engineers, field service engineers, lab technicians, computer specialists, radio and electronic hobbyists will find it ideal.

With its rugged construction and battery operation, the PDM35 is perfectly suited for hand work in the field, while its angled display and optional AC power facility make it just as useful on the bench.

What you get with a PDM35

- 3 1/2 digit resolution
- Sharp, bright, easily read 11 D display, reading to ± 1999
- Automatic polarity selection
- Resolution of 1 mV and 0.1 nA
- 0.0001 Ω
- Direct reading of semiconductor forward voltages at 5 different currents
- Resistance measured up to 20 MΩ
- 1% of reading accuracy

Operation from replaceable battery or AC adaptor
Industry standard 10 MΩ input impedance

Compare it with an analogue meter!

The PDM35 10% of reading compares with 3% of full scale for a comparable analogue meter. That makes it around 5 times more accurate on average.

The PDM35 will resolve 1 mV against around 10 mV for a comparable analogue meter – and resolution on current is over 1000 times greater.

The PDM35 DC input impedance of 10 MΩ is 50 times higher than a 20 kΩ 1-volt analogue meter on the 10 V range.

The PDM35 gives precise digital readings. So there's no need to interpret ambiguous scales, no parallax errors. There's no need to reverse leads for negative readings. There's no delicate meter movement to damage. And you can resolve current as low as 0.1 nA and measure transistor and diode junctions over 5 decades of current.

Technical specification

- DC Volts (4 ranges)**
Range: 1 mV to 1000 V
Accuracy of reading $10^0 \pm 1$ count
Note: 10 MΩ input impedance
- AC Volts (40 Hz-5 kHz)**
Range: 1 V to 500 V
Accuracy of reading $10^0 \pm 2$ counts
- DC Current (6 ranges)**
Range: 1 nA to 200 mA
Accuracy of reading $10^0 \pm 1$ count
Note: Max. resolution 0.1 nA
- Resistance (5 ranges)**
Range: 1 Ω to 20 MΩ
Accuracy of reading $15^0 \pm 1$ count
Also provides 5 junction-test ranges

Dimensions: 6 in x 3 in x 1 1/2 in.

Weight: 6 oz.

Power supply: 9V battery or Sinclair AC adaptor

Sockets: Standard 4 mm for resilient plugs

Options: AC adaptor (or 240 V 50 Hz power De-luxe padded carrying case w/let, 30 kV probe)


The Sinclair credentials

Sinclair have pioneered a whole range of electronic world-firsts – from programmable pocket calculators to miniature TVs. The PDM35 embodies six years' experience in digital multimeter design, in which time Sinclair have become one of the world's largest producers.

Tried, tested, ready to go!

The Sinclair PDM35 comes to you fully built, tested, calibrated and guaranteed. It comes complete with leads and test probes, operating instructions and a carrying w/let. And getting one couldn't be easier. Just fill in the coupon, enclose a cheque (PO for the correct amount – usual 10-day money-back undertaking, of course) and send it to us.

We'll mail you your PDM35 by return! Sinclair Radionics Ltd, London Road, St Ives, Huntingdon, Cambs. PE17 4HH, England Regd No 699183

To: Sinclair Radionics Ltd London Road Selby - Harrogate Cumbria PE17 4HH	
Please send me <input type="checkbox"/> by PDM35 x	
9 £33.00 inc. 240V-51 and 65P P&P	
Name	_____
Address	_____
<input type="checkbox"/> by De-luxe padded carrying case x £3.00 inc VAT and P&P each	
<input type="checkbox"/> by AC adaptor x for 240V 50Hz power 0.2300 inc VAT and P&P each	
<input type="checkbox"/> Enclose cheque (PO made payable to Sinclair Radionics Ltd for _____ £ _____) to indicate total amount	
<input type="checkbox"/> Fund, please, if I am not completely satisfied with my PDM35. I may return it within 10 days for full cash refund.	
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tech-tips

Digital Echo Unit

J. A. Murdie

The Digital Echo Unit described below may be constructed on standard Euro card PCBs with 31 way connectors, and utilizes the cheap 2102 1K static RAM, of which from any amount from (say) 32-64K may be used to achieve a (continuously variable) delay of up to a second. The delay time is of course directly proportional to the amount of memory used. There are three PCB designs used: Fig. 1: Input/Clock board (1 off), Fig. 2: Output/Control board (1 off), Fig. 3: 8K Memory Board (max. 8 off).

Dealing with the input board first, it may be seen that the 555, 7476 and 7408 constitute a non overlapping two phase clock whose outputs are 'Enable Read' (ER), and 'Enable Write' (EW). During the write phase a bit is taken from the digitized input and fed to the 'Data Write' (DW) line. The AD converter used is the FX209 which was featured in the ETI June 1976 Data Sheet. The bits created are placed in the memory location addressed by the 12 bit counter ('Bit Address'), on this board and the 4 bit counter on the Output/Control board ('Block Address').

When the ER line goes high a bit is taken from the memory address pointed to by the counters with the 4 bit value produced by the Hexadecimal Priority encoder (Delay Switches) being added to the block address. Thus the 'distance' between the write and read 'heads' may be altered to place them any number of blocks apart, and thus create a choice of 16 basic delay lengths. The bit read is placed on the DR line and is then converted to an analog value by the DA converter. Note that some of the output may be fed back to the input ('Regen') to create multiple echo effects.

After this sequence of a write and a read cycle the bit/block address is incremented by one so a succession of bits may be placed in memory by input, and read from the memory by the output. The rate at which this sequence occurs is controlled by the clock rate of the 555 astable, and thus this not only controls the delay time as do the delay switches, but also the quality of the sound reproduced as this independent on the number of samples taken

per second in the digitizing process. The device may be set up to digitize the analog input at a maximum of 125 K

bits/second — which is quite adequate for (say) an electric guitar which requires a bandwidth of some 10 KHz.

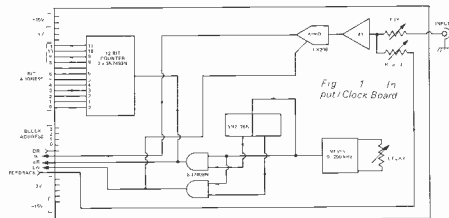


Fig 1 Input/Clock Board

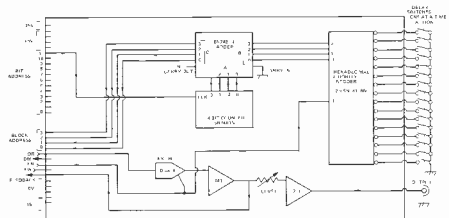


Fig 2 Output/Control Board

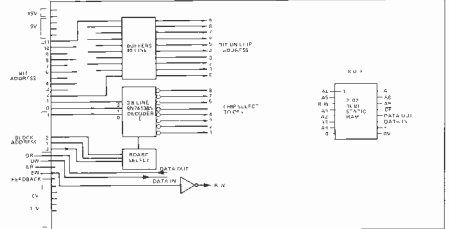


Fig 3 8K Memory Board

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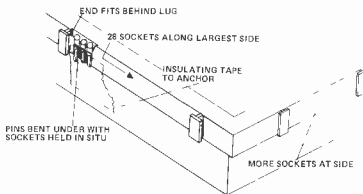
Dec-ed Out

D. F. Tranter

When using S-Decs to test circuits, one often finds that several groups of the Dec contacts are taken up for one common connection, particularly the contacts which run to the battery connections.

In order to extend the capacity of a single S-Dec I fit a row of sockets along each of the two Dec sides which have lugs for connecting to other Decs, using the lugs as end fixing points.

If the sockets are bent and a strip of insulating tape used to anchor the lower



ends, one gets a reasonably robust fitting which greatly extends the capacity of the Dec.

The lug recesses along the other two sides can also be used for attaching more rows of sockets.

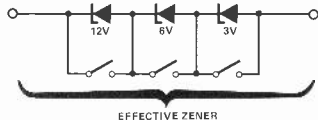
The Multi-zener

R. N. Soar

This is an application of zener diodes based on the binary system. In the example shown three zener diodes are used 3 V, 6 V and 12 V (ie. 3.0 V, 6.2 V and 12 V) plus three S.P.S.T. switches. In the 'on' position of a switch the diode is short circuited. In the 'off' position the diode is in circuit. Thus the effective diode by suitable

operation of the switches is 3, 3+6, 3+12 etc ie. 3,6,9,12,15,18,21 volts. By the addition of the next in the

series 24 V and another S.P.S.T. switch the range is 3,6,9,12,15,18,21,24,27, 30,33,36,39,42,45 volts.



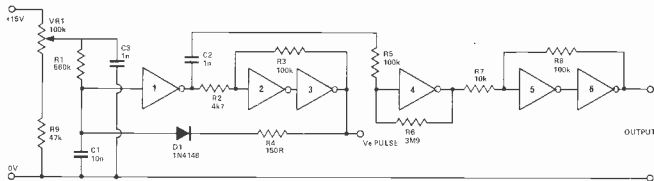
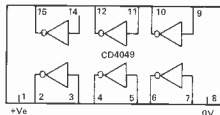
Cheapo VCO

A. J. Richardson

This circuit provides a cheap solution to a non precision voltage controlled oscillator. C1 charges towards the voltage set on VR1 until inverter 1 output goes low whereupon the output of inverter 3 goes low and discharges C1 via D and R4. Inverters 2 and 3 form a Schmitt trigger circuit with positive feedback supplied by R3. Inverter 4 forms a linear amplifier with its gain

set by the ratio of R5 to R6 which squares up the signal appearing on inverter 1 output. The signal is further squared up by the Schmitt trigger action of inverters 5 and 6 to provide a square wave of approximately 50% duty cycle at the output of inverter 6. With the values shown a frequency range of at least 100 Hz to 15 kHz is guaranteed with VR1 but other ranges can be covered with suitable values of R1 and C1. The circuit works well at lower supply voltages but the frequency range covered for a given set of com-

ponents may be slightly less. If a square wave is not required a negative pulse of approximately 200 nS is available at the output of inverter 3 thus enabling two VCOs to be built with one chip.



Phaser Mod

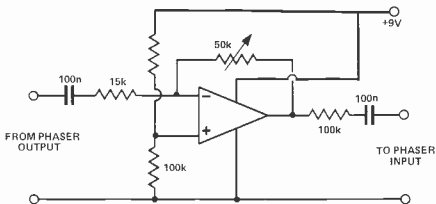
M. Headey

I constructed a simple variable gain op amp inverter and connected it between the output and the input.

When the feedback amp was switched into circuit the effect was dramatic. The phaser sounded much deeper.

The modification is simple enough and though can be adjusted to feedback (audio) level, sounds very good if the gain is kept down.

The circuit as shown gives very good results although you may be able to suggest some component value changes.

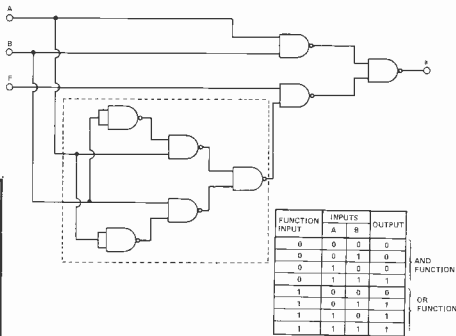


Programmable Gate

P. Mead

The Programmable Gate is a gate which converts an AND gate to an OR gate by applying a logic '1' on the function input.

The logic design uses 8 x 2 input NAND gates. The number of gates may be reduced by replacing the 5 NAND gates enclosed by the dotted line, with a 2 input exclusive OR, such as the TTL 7486.



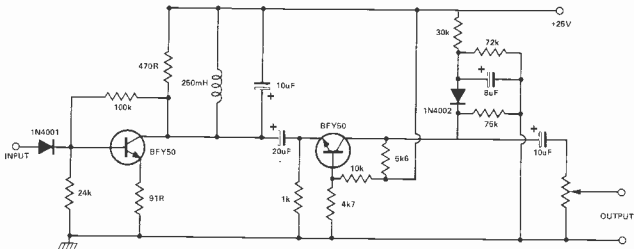
5mS Delay Unit

C. S. Rushton

The circuit shown will produce a delay of 5 mS from input to output with good correlation between amplitudes over a dynamic range of approximately 40 dB.

The circuit consists of four main sections: an input buffer, a damped resonant RLC circuit, a non-inverting amplifier and a clamping circuit.

The delay can be modified within reasonable limits by adjustment of the RLC network.



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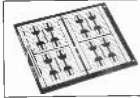


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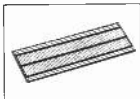
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