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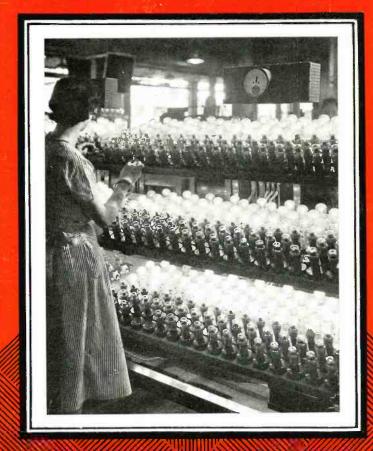
Television Apparatus

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Components

Tubes

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VOL. XIV

NO. 9



The Journal of the Radio and Allied Industries

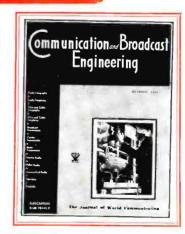
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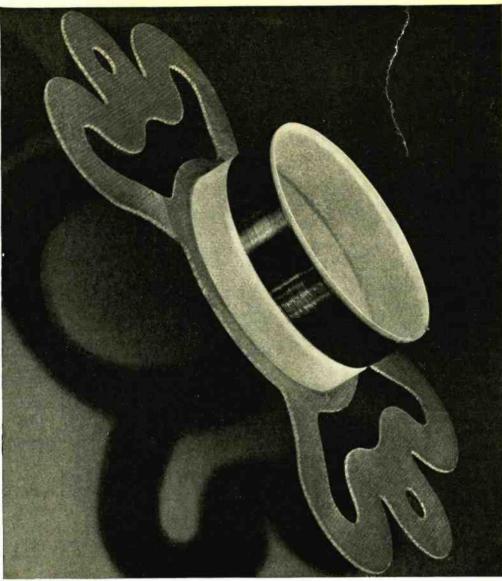
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RADIO ENGINEERING

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Vol. XIV

SEPTEMBER, 1934

Number 9

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RADIO INDUSTRY CODE

SPECIAL CONSIDERATION by the National Industrial Advisory Board of the RMA application for exemption from the electrical manufacturing code and a separate code for the radio industry has resulted in negotiations with NRA and between RMA and NEMA which are proceeding satisfactorily. Final action by the NRA is expected in September.

Independent code operation for the radio industry is the objective in the Washington negotiations. The National Industrial Advisory Board intervened in the NRA code proceedings instituted by the RMA, viewing the problem as an important matter affecting the two large industries, radio and electrical. The RMA code committee, headed by Captain William Sparks of Jackson, Michigan, and also a committee of NEMA, with NRA officials present. have been holding conferences with the National Industrial Advisory Board. These have delayed action both on the RMA proceeding and also on further revision of the electrical code.

BRYAN S. DAVIS
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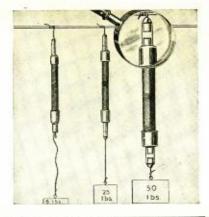
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"AD-A-SWITCH" was originated by Clarostat



SEPTEMBER, 1934

EDITORIAL

MANUFACTURING

RECEIVERS

PHILCO HAS STARTED high fidelity on its way. By this time the public is fairly well acquainted with the salient features of a high-fidelity receiver and will pattern their demands in accordance with their conceptions of what a modern receiver should be.

Unfortunately, the public may expect everything from soup to nuts in a single receiver, and grumble a bit if they do not get what they want. At the moment it is next to impossible to combine the true features of high-fidelity and all-wave reception into a single unit. There is no doubt, however, that it can be done in time. In the meantime, the manufacturer who wishes to offer both high-fidelity reception and all-wave reception, will do well to provide these features in separate units, or through the use of a built-in shortwave converter.

With the present popularity of all-wave receivers, and the probable popularity of high-fidelity receivers to a less marked degree, the usual necessity of perfection in design and manufacture arises. In both types of receivers closer tolerances appear necessary. The preciseness of design required in both instances also demands more rigid methods of factory testing and adjustment. All-wave and high-fidelity receivers call

All-wave and high-fidelity receivers call for components which will maintain their prescribed electrical and mechanical characteristics throughout the useful life of the receiver.

COMPONENTS

THE MANUFACTURERS OF radio-receiver components have made considerable progress in improving both the mechanical and electrical features of their products. Their research activities have increased over the past five years with the result that most component suppliers have not only contributed considerably to the improvement in receiver design, but likewise to a reduction in the cost of

finished sets—often at their own expense.

The problem of simplifying production operations is shared alike by the manufacturer and the parts supplier. For some years production men have directed their attention

production men have directed their attention to the simplification of actual fabrication in radio factories. Components have been grouped for the purpose of saving space, wire, supporting and anchoring devices, and for the purpose of reducing the number of

receiver-assembling operations.

There is considerable opportunity in the parts field for the development of entirely new components. The application of new materials and new tolerances are called for in the design of all-wave and high-fidelity receiver components. It may become desirable to revert to more expensive components, such as air dielectric condensers, to give accuracy and permanency of adjustment.

TUBES

THE 6-SERIES TUBES are now employed in the auto receiver, the universal, the all-wave receiver and the standard broadcast receiver. The field has practically standardized on this series and it appears that in the future the sale of the early 6-series, and the 2.5-series, will be entirely for replacement purposes.

In the case of ac-operated receivers, it is now general practice to employ one transformer winding for the filament of the rectifier tube, and a second winding for supplying the heaters of all other tubes. In a few cases, where an 84 rectifier tube is used, the job is done by a single heater winding. Since there are no high-current rectifier tubes of the indirectly-heated type, this simplification is restricted to small receivers and shortwave converters.

The new 6-series tubes are great space savers. The possibility of compactness is but one of their advantages. The small tube also permits a more sensible spacing of components and apportioning of vacant areas for the purpose of good ventilation and the isolation of high-frequency units from others operating at high temperature, without increasing manufacturing costs or adding materially to the size of the finished receiver.

Page 4

FIELD TESTED FOR TWO YEARS...

ANNOUNCED TODAY





VOLUME CONTROLS

IRC Volume Controls are a logical development of the IRC method of applying resistance coatings to insulating bases, used so successfully for years in the well-known Metallized resistors.

Nor is this their only recommendation. For two years prior to this general announcement, they have seen extensive service under all conditions of use in radio receivers produced by several manufacturers. Constantly increasing orders from these same firms tell their own story of quality coupled with sound economy.

The IRC Volume Control is especially designed to resist humidity. The resistance coating is permanently bonded at a high temperature, to a hard, moisture-proof base. Contact is made by three slider fingers that always follow the same course and which positively eliminate any jumps in resistance due to shifting of the points of contact. Wear is reduced

Write for Catalog M-26 describing this new IRC development in detail.

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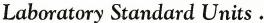
BY THE MAKERS OF METALLIZED, PRECISION AND POWER WIRE WOUND RESISTORS

SEPTEMBER, 1934

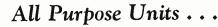
Page 5







The ultimate in perfection for those engaged in high fidelity reproduction and sound amplification, broadcast engineering, laboratory technicians and test equipment manufacturers. Housed in a high permeability iron casting which provides excellent electromagnet shielding, these efficient, long life audio transformers afford frequency characteristics of ± 1 db from 30 to 15,000 cycles.



A very reasonably priced high quality line of transformers and reactors ideal for public address, radio receiver, amateur broadcast and

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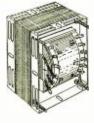
Portable Broadcast Units

In every respect the same high quality as the Laboratory Standard Line, they are identical castings. They meet the great demand for in design but are housed in small aluminum castings.



portability, high efficiency and low weight. Manufacturers and

These individual units are incorporated in radio receivers made by leading manufacturers, and are also widely used by enterprising service men. Their size makes them readily available for replacement work, especially where space is limited. All components are individually boxed in rugged containers, preventing damage in shipment or storage.



Special Units . . .

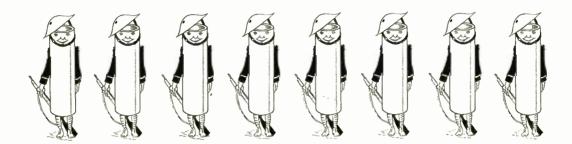
For those requiring special purpose transformers designed to meet any particular requirement, write us giving the specifications desired or describe your problem and we will gladly cooperate in solving it.

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RADIO ENGINEERING Page 6

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Standard ISOLANTITE standoff insulators used in transmitter construction.

radio Engineering

FOR SEPTEMBER, 1934

ENGINEERING INSPECTION

NOTES ON THE APPLICATION OF STATISTICAL METHODS TO PRODUCTION

By C. F. NORDICA

A UNIFORM PRODUCT is desirable if not essential to every manufacturer. In order to insure the required uniformity of a product it is customary to set up definite limits which the product must meet or which a specified portion of the product must meet. Regardless of the care taken with manufacturing processes or of rigorous inspection methods, it is known that no two units of any product will be identical. Such factors as wear of machines, lack of homogeneity of materials, humidity, temperature, and the psychological conditions of the manufacturing and inspection personnel, all contribute to lack of uniformity. Certain random variations are usually accepted as inevitable and it is customary to attempt to eliminate or reduce to a minimum only phenomena which produce irregular, cyclic, or secular trends in the product. In addition to maintaining a uniform product it is the duty of the inspection personnel to observe and trace to its source anything producing a definite trend in the product, as well as to segregate random or natural variations from those due to assignable faults in processes, materials, etc.

STATISTICAL INSPECTION METHODS

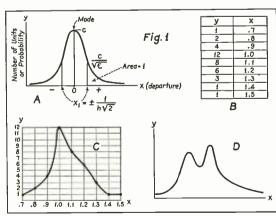
Inspection can be divided into two parts: first, gathering the data, and second, interpreting it. It is to the interpretation of the data that statistical methods can be usefully applied. In general there are two methods of rating a given characteristic of a product. The first is called the method of variables and consists of rating a product in terms of its variation from the desired value. The second is usually referred to as the method of attributes, and consists in rating a product as satisfactory or unsatisfactory. In numerous instances both may be employed on the same characteristic of a given product. As an example, suppose we are interested in the inductance of a coil. We can either measure the variation of the inductance of the coils from the assigned value or we can rate them as acceptable or non-acceptable as the inductance falls within certain specified limits. Again, every unit of a product may be measured, or only a selected number may be tested. The choice between inspecting each unit and sampling the product depends upon the effect of the inspection operations on the later characteristics of the product, upon the rigidity of the requirements and upon economic considerations.

A good example of a product requiring sampling inspection is the current rating of fuses. In this case the product is destroyed by inspection and inspection is called upon not only to determine whether the product meets the requirement, but also to find the most probable value for the normal rating of the product.

Inspection must be able to differentiate between natural or non-assignable variations and controllable or assignable variations. It is only by such methods of analysis that significant trends may be observed early and corrected. In order to do this it is customary to arrange inspection data in such form that significant trends may be readily observed.

PROBABILITY CURVES

When such data is plotted with the number of units having a given value as a function of the departure from some assigned value, a curve similar to the probability curve is usually obtained. Such a curve is shown in Fig. 1-A. This may be arrived at as follows: Suppose measurements were made at intervals of 0.1 henry on a series of 1.0-henry coils. Let the values of the table of Fig. 1-B represent the measured variations and Fig. 1-C the resulting curve. This gives a measure of the variation of the product. If the curve had the form shown in Fig. 1-D, however, it would be immediately



THE FREQUENCY POLYGON OR DEPARTURE CURVE.

SEPTEMBER, 1934

obvious that something was tending to make for a nonuniform product. This might be too large a diameter, too many turns, difference in winding tension, or difference in the incremental permeability of the core. Again, if the curves of several consecutive days' production were as shown in Fig. 1-E, it would be obvious that some definite factor or factors were tending to increase the value of the inductance. If the day-to-day curves had varied more or less uniformly about some one day's production, then random variations might account for it. If a persistent trend appears, however, it is usually due to some assignable phenomena.

In arriving at the most probable value of some quantity such as the inductance of a coil or the capacity of a condenser, the same sort of measurements will be made on all or on a sample lot of the units. There are then three possible average values that may be assigned. First, the arithmetic mean; second, the mode or value which occurs most frequently; and third, the median, or central value, when the observations are arranged in order of magnitude. Thus, let a series of observations of a given characteristic of some product be as follows:

5, 6, 7, 8, 9, 9, 9, 10, 10, 10, 11, 11, 12, 13, 14, 15.

The arithmetic mean is: $\frac{168}{17} = 9.9$.

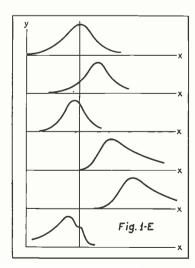
The mode is: 9.

The median value is: 10.

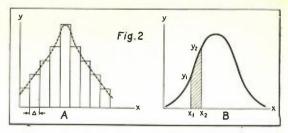
All three values are used to some extent in determining the most probable value although the arithmetic is probably the most generally useful. Had these observations been plotted as shown in Fig. 1 the modal value would have been that corresponding to the peak of the curve, while the median value would have been the value whose ordinate would divide the curve into two equal areas.

THE ERROR EQUATION

Now the curve of Fig. 1-A is represented by $y = c \, \epsilon^{-h^2 \, x^2}$ which is called the error equation from its association and use in determining the errors of observation, etc. This was first derived by Gauss and is a fundamental formula around which much statistical theory has been built. The quantity h is called the precision index and has to do with the precision of observations or the difference between successive departures from the modal value of the curve. Thus, large values of h indicate high precision or small incremental de-



PLOTTED CURVES OF SEVERAL DAYS' PRO-DUCTION, INDICAT-ING DEFINITE VARI-ANCES.



THE FREQUENCY HISTOGRAM AND FREQUENCY POLYGON.

partures. If these incremental departures are plotted as shown in Fig. 2-A, it may be shown that:

$$c = \frac{h \Delta}{\sqrt{\pi}}$$

from which we have the error equation reducing to:

$$y = \frac{n \Delta}{\sqrt{\pi}} e^{-h^2 x^2}.$$

One of the most important problems in statistical theory is to find the probability that a given observation will be between two given limits x_1 and x_2 . This may be obtained in terms of the precision index h, for the result sought is merely the sum of the probabilities of all observations between x_1 and x_2 which is:

$$Y = \frac{h}{\sqrt{\pi}} \int_{x_1}^{x_2} \varepsilon^{-h^2 x^2} \Delta = \frac{h}{\sqrt{\pi}} \int_{x_1}^{x_2} \varepsilon^{-h^2 x^2} \delta x$$
$$= \frac{h}{\sqrt{\pi}} \int_{0}^{x_2} \varepsilon^{-h^2 x^2} \delta x - \frac{h}{\sqrt{\pi}} \int_{0}^{x_1} \varepsilon^{-h^2 x^2} \delta x.$$

This expression has been termed the probability integral. Tables of the values of this integral are given in numerous reference works on the subject of statistics.

DERIVATION OF EQUATION

Gauss's derivation of the error equation is of interest in that it indicates the assumptions and boundary conditions necessary in arriving at this fundamental relation. Let q represent the unknown value of a quantity and let a series of n measurements be made upon it, n being assumed to be very large. Let the departures from the true value be $x_1, x_2 \dots x_n$. It is obvious that the probability of the occurrence of a departure x is some sort of inverse function of its magnitude. Designating the probabilities of these respective departures as y₁, $y_2 \dots y_n$, this fact may be expressed by:

$$y_1 = f(x_1)$$

$$y_2 = f(x_2)$$

$$y_n \stackrel{\cdot}{=} f(x_n).$$

It remains to determine the form of f(x). We do not know the true value q of the observed quantity, nor do we know the true departures x. We may, however, assume various tentative values of q and study the resulting tentative systems of departures, particularly with a view to selecting that one which seems most naturally distributed in accordance with experience. We are, therefore, seeking to find that system of values for xwhich as a whole has the greatest probability. Whence:

$$Y = y_1, y_2 \dots y_n = f(x_1) f(x_2) \dots f(x_n).$$

In order that the system of x shall have the greatest probability, the assumed value for q should be such that Y is a maximum. This condition is attained when:

$$\frac{\delta Y}{\delta a} = 0.$$

We therefore have:

$$\frac{\delta Y}{\delta q} = \frac{Y}{f(x_1)} \cdot \frac{\delta f(x_1)}{\delta q} + \frac{Y}{f(x_2)} \cdot \frac{\delta f(x_2)}{\delta q} + \dots = 0$$

$$\begin{split} &\frac{Y}{\delta\,q} \bigg[\frac{\delta\,f(x_1)}{f(x_1)} + \frac{\delta\,f(x_2)}{\delta\,f(x_2)} \ldots + \frac{\delta\,f(x_n)}{\delta\,f(x_n)} \bigg] = \\ &\frac{Y}{\delta\,q} \bigg[\delta\log\,f(x_1) + \delta\log\,f(x_2) + \ldots \delta\log\,f(x_n) \bigg] = 0. \end{split}$$

Replacing
$$\delta \log f(x)$$
 by $\phi(x) \delta x$ we have:
$$\phi(x_1) \frac{\delta x_1}{\delta q} + \phi(x_2) \frac{\delta x_2}{\delta q} + \dots \phi(x_n) \frac{\delta x_n}{\delta q} = 0.$$

designated by S_1 , S_2 ... S_n having definite fixed values, then the departures x are:

$$x_1 = S_1 - q$$

 $x_2 = S_2 - q$
 $x_n = S_n - q$.

From which:

$$\frac{\delta x_1}{\delta q} = \frac{\delta x_2}{\delta q} = \frac{\delta x_0}{\delta q} = -1.$$

Which reduces to:

$$\varphi(\mathbf{x}_1) + \varphi(\mathbf{x}_2) + \ldots \varphi(\mathbf{x}_n) = 0.$$

Assume that the resultant departure curve is symmetrical about the value q; that is, that the number of positive departures is equal to the number of negative departures for an infinite number of observations and that the algebraic sum of all departures is zero. We then have: $x_1 + x_2 + \dots + x_n = 0$. Now the last two equations are satisfied if:

$$\varphi(x_1) = Kx_1
\varphi(x_2) = Kx_2$$

$$\phi\left(x_{n}\right) = \mathrm{K}x_{n}$$

where K is a constant. To prove this let us add a finite quantity a to any one of the x's, say x', and subtract it from any other, say x'', This will not alter the conditions that: $x_1 + x_2 + ... x_n = 0$.

nor the condition that: $\varphi(x_1) + \varphi(x_2) + \varphi(x_n)$ =0

since by hypothesis these conditions are to be simultaneous. This necessitates the condition that:

$$\varphi(x') + \varphi(x'') = \varphi(x' + a) + \varphi(x'' - a)$$
or that:

 $\begin{aligned} & \left[\phi\left(x' + a \right) - \phi\left(x \right) \right] + \left[\psi\left(x' + a \right) - \phi\left(x' \right) \right] \\ & \text{Dividing through by } \alpha \text{ we have:} \\ & \phi\left(x' + a \right) - \phi\left(x' \right) - \phi\left(x'' - a \right) - \phi\left(x'' \right) \\ & - a \end{aligned} = 0.$

$$\frac{\varphi(x' + a) - \varphi(x')}{-} - \frac{\varphi(x'' - a) - \varphi(x'')}{-} = 0.$$

If α approaches zero this becomes as a limit:

$$\frac{\delta}{\delta x'} \varphi(x') - \frac{\delta}{\delta x''} \varphi(x'') = 0$$

or in general:

$$\frac{\delta}{\delta \mathbf{x}_n} \, \varphi \, (\mathbf{x}_n) = 0.$$

It follows at once that since the x's may be varied in any manner among themselves only so $x_1 + x_2 \dots x_n$ = 0 holds, that:

$$\frac{\delta}{\delta x} \delta (x) = K = constant.$$

Therefore, upon integrating, we have:

$$\varphi(x) = Kx + c.$$

But from $x_1 + x_2 + \dots + x_n = 0$ and $\phi(x_1) + \phi(x_2) + \dots + \phi(x_n) = 0$ jointly, it follows, since substitution in the latter gives:

$$K(x_1 + x_2 + \dots x_n) + nc = 0$$

that: $\varphi(x) = Kx$.

Now since

$$\varphi(x) \delta x = \delta \log f(x) = \delta \log y$$

then:

$$\delta \log y = Kx \delta x$$

Integrating:

$$\log y = \frac{1}{2} Kx^2 + c'$$
.

$$\text{Or} \colon y = \epsilon^{\frac{1}{2} \operatorname{K} x^2 + c'}$$

which is one form of the error equation. Now we have assumed that the larger the error the less likely it is to occur, whence the larger x the smaller y. From which it is obvious that K is a negative quantity. Replacing $\frac{1}{2}K^2$ by $-h^2$ and ε^c by the constant c, the error equation in its usual form results; thus:

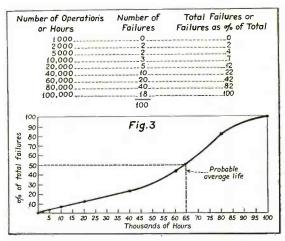
$$y = c \epsilon^{-h^2 x^2}$$
.

The bilateral symmetry of the function y is evident from the appearance of x in the second degree only. This indicates the equal possibility of positive and negative departures of the same magnitude. The function approaches zero as x increases in magnitude, which indicates that very large departures are extremely improbable. The derivatives of y are:

$$\begin{split} \frac{\delta \, y}{\delta \, x} &= - \, 2 \, ch^2 \, x \, \epsilon^{-h^2 \, x^2} \\ \frac{\delta^2 y}{\delta \, x^2} &= - \, 2 \, ch^2 \, \epsilon^{-h^2 \, x^2} \, [1 - 2 \, h^2 \, x^2]. \end{split}$$

$$\begin{split} \frac{\delta^2 y}{\delta \, x^2} &= - \, 2 \, \operatorname{ch}^2 \, \epsilon^{-h^2 \, x^2} \, [1 - 2 \, h^2 \, x^2]. \\ \delta \, y & \delta^2 y \\ \text{From this since} & \frac{\delta \, y}{\delta \, x} &= 0 \, \operatorname{and} \, \frac{\delta^2 y}{\delta \, x^2} < 0 \, \operatorname{when} \, x = 0 \end{split}$$

0, y is a maximum when x = 0. Which states that zero



CUMULATIVE FREQUENCY DISTRIBUTION CURVE.

departure has the greatest probability. We may now draw the curve of Fig. 2-B since the y intercept is the maximum value of y and equal to c at x = 0. And

$$1 - 2h^2 x^2 = 0$$
$$x = \pm \frac{1}{h\sqrt{2}}$$

we have the two points of inflection of the curve. The ordinate at the points of inflection is:

$$y = + \frac{c}{\sqrt{\epsilon}}$$

The quantity c represents the probability of zero departure.

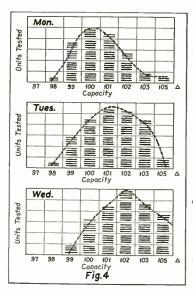
So far we have treated the departure x as a continuous variable which might have any value from zero to infinity. But to assume this would be to assume an infinitely minute graduation of the measuring scale. Thus the probability of any particular departure out of the infinity of possible ones would be infinitesimally small. It is thus apparent that the variable departure x instead of varying by infinitesimal increments δx does have finite discontinuities Δ , which represents the smallest fraction of a unit in which the measured results are expressed. The curve should therefore be represented as shown in Fig. 2-A, the width of the departure compartments being Δ and their height y. And:

$$\Sigma$$
 y = 1.

The curve of Fig. 2-A is usually called the frequency histogram, while that of Fig. 2-B is usually referred to as the frequency polygon.

DEPARTURE VALUES

If a series of direct measurements be made upon a single quantity under constant conditions the result is a series of values each approximating the true value. However, no one of them is the true value and it therefore becomes a matter of judgment to select a value which will make the departures have a most natural distribution. The symmetry of departures from the true value has been shown to be symmetrical when the departures are due to natural causes. This leads at once to the axiom that the best value is probably the arithmetic



A GROUP OF THREE CAPACITY DEPART-URE CURVES; FOUR CHECKS PER SQUARE. mean. If the measured results be S_1 , S_2 , S_n and their arithmetic mean be m, then the departures from the

$$x_1 = S_1 - m$$

$$x_2 = S_2 - m$$

$$x_n = S_n - m$$

By summation we obtain.

$$\Sigma x = \Sigma m - n m = 0$$

which expresses the fact that the arithmetic mean of the results is the value with respect to which they are symmetrically placed; that is, the sum of the departures are equal to zero. From which it follows that in this case the arithmetic mean is the most probable value that can be assumed.

METHOD OF LEAST SQUARES

If this is true, then we should obtain a similar result by using the method of least squares. This principle may be stated as follows: The most probable value of a measured quantity that can be deduced from a series of direct observations, made under identical conditions, is that for which the sums of the squares of the departures is a minimum. Again, let the results of observations be $S_1, S_2 \ldots S_n$. If we designate the most probable value by m, then:

The probability of the occurrence of the assumed system of events is:

$$y_1, y_2 \dots y_n = c^n \epsilon^{-h^2 (x_1^2 + x_2^2 + \dots x_n^2)}$$
.

Now, if $y_1, y_2 \dots y_n$ is to be a maximum, then $x_1^2 + x_2^2 + \dots x_n^2$ must be a minimum. That is, m must be chosen so that $\sum x^2$ is a minimum in accordance with the principle just stated. Whence: $\Sigma x^2 = (S_1 - m)^2 + (S_2 - m)^2 + \dots (S_n - m)^2$

= minimum

and:

$$\frac{\delta}{\delta m} \sum x^2 = -2 [S_1 - m)^2 + (S_2 - m)^2 + \dots (S_n - m)^2] = 0 or: m = \frac{S_1 + S_2 + \dots S_n}{}$$

which is simply the arithmetic mean of the observations.

CUMULATIVE FREQUENCY DISTRIBUTION

So far we have confined the discussion to random observations due to natural or non-assignable causes. Consequently when the controllable variations are reduced to a minimum as they should be, then the above results apply. Now suppose we are to determine the probable life of a series of switches, or circuit breakers, or relays. Let the results be those given in the table of Fig. 3.

Probably the curve which reveals the most information is that shown in Fig. 3, in which the percentage of failures is plotted as a function of time or number of opera-This type of chart is usually referred to as a cumulative frequency distribution curve. The average life expectancy is then the ordinate corresponding to 50 per cent failure. This is an example of the use of sampling inspection of a given characteristic of the product.

Page 12

Suppose we are interested in variable condensers. Certainly one of the quantities which will be carefully scrutinized is maximum capacity. Suppose we decide that the value Δ or the steps in which we are interested, or which can be accurately measured, is 1.0 micromicrofarad. Then a chart such as that shown in Fig. 4 might be used and the inspector might simply draw a line in the proper column for each condenser. This results in a chart which can be observed even while the chart is still in the making, if desired. Moreover, it eliminates any re-arrangement of data for later analysis.

Distribution curves for different lots or different days can be readily examined without transcribing any of the data. A tendency for capacity to run toward the lower limit in condensers having plates accurately centered might at once point to plate material which is too thin, etc. This permits early correction of controllable errors, or early changes in design without a large waste of material or undue delay which might result if extensive analysis of inspection data were undertaken. Because of the immediacy of the data, departures from engineering specifications provided the supplier are instantly noted, with the result that the actual degree and nature of the departure can be transmitted to the supplier for correction without delaying the production line.

CHOOSING VALUE

Now assume that it was required to establish a capacity rating for a lot of fixed condensers. It is then required to establish a most probable value of capacity. Suppose the results are those given in the table of Fig. 5. While the curve is not symmetrical, it is still sensibly so. Had it been exactly symmetrical the three average values would be identical and we would know that the differences were due to random or non-assignable causes. Since it appears that manufacturing irregularities are actually playing a part, the mode would ordinarily be

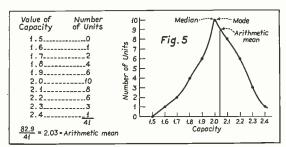


ILLUSTRATION OF USE OF FREQUENCY POLYGON IN DETERMINATION OF MOST PROBABLE VALUE.

chosen as the most probable value, since it occurs most frequently. The more unsymmetrical the curve the further the departure of the three average values and the more excuse there would be for using the modal value as the most probable value for the rating.

CONCLUSIONS

From the foregoing discussion it is evident that no two items of a given product can be identical and that attempts to reduce random variations due to nonassignable causes is more or less a waste of effort. It is therefore essential to determine which of the variations are due to controllable causes and which are not. In general we can expect random variations to obey the law of error distribution as derived by Gauss, knowing that this will produce a symmetrical series of results. It is therefore necessary to scrutinize carefully the unsymmetrical curves and by analysis eliminate the causes of irregularity in the product. One method of recording data in a readily usable form is illustrated. By the exercise of reasonable judgment and proper recording of inspection data it is therefore a reasonably simple matter to insure a stable and uniform product.

Weather-Report Receivers

INTERMEDIATE-WAVE radio receivers at filling stations and other points along highways to obtain weather information for motorists have been suggested by the Bureau of Air Commerce. Every hour from the 68 airways broadcast stations scattered throughout the United States along the Federal Airways System weather reports are sent out on the air to assist flyers, and small receiving sets with a range of from 200 to 400 kc could make this information available to motorists.

WEATHER BULLETINS

This service, if organized, could be made available to the transient motorist in the form of small bulletin boards to be placed in conspicuous places in service stations, bus stations, and local automobile clubs and associations on heavily traveled highways where an attendant could post the weather broadcasts as soon as they were sent out

on the air. This would be of particular importance in the more rugged and mountainous sections of the country, where a fog may mean delay, heavy rain, a washout, and a snow an impassable section of roadway. Using these proposed bulletins the motorist may take another route and avoid the possibility of these delays.

DATA BEING USED

Automobile test tracks and automobile clubs have already found this means of determining the weather very valuable, but this service has not yet been placed at the convenience of the casual motorist, the bus operator and the cross-country driver. Just as the airplane pilot depends on the weather reports to guide him through the skies, so will the automobilist depend on them in his selection of routes and the length of his day's travel.

It has been previously suggested by

the Bureau of Air Commerce that the automobiles themselves carry these receivers for the reception of this weather information. The service that would be offered by filling stations and other points where the motorist is likely to stop would include cars not equipped with radios.

NEW MARKET

There are literally thousands of service stations, filling stations and autocamps dotted along the principal highways of this country. The market appears to be sufficiently large to warrant the manufacture of inexpensive intermediate-wave receivers expressly for the purpose of picking up the weather information.

The radio service man is in a position to develop the market. It has been suggested that he do so in the September issue of Service.

Factory Processing of

By L. L. McMASTER, Jr.

COMMERCIAL ENGINEER

THE PROBLEMS INVOLVED in the activation of oxide-coated emitters are an endless source of trouble to factory engineers. At times the factory is suddenly plunged into an epidemic of low emission or slumping emission, only to run out of the trouble as quickly as it was encountered, the solution remaining a mystery. There is a cause for every effect. To find that cause as quickly as possible means a quicker solution of the effect. This theory is presented for the factory engineer. It is not offered as the latest theory on a question thus far unsatisfactorily answered; rather it is the result of considerable study of the literature plus practical experience.

Many theories have been advanced on emission from oxide-coated filaments. There have been many presentations in the literature both in this country and abroad and a study of these theories has led to a consolidation of many of the ideas suggested into a theory which has been found to be practical for the man responsible for the processing of tubes.

CHEMICAL REACTIONS

The chemical reactions involved may be represented by simple equations, the primary reaction being the breakdown of the carbonates into the oxides:

$$BaCO_{2} \xrightarrow{900 \text{ to}} BaO + CO_{2}$$

This reaction takes place during the breakdown of the carbonates on exhaust, though to various degrees. Frequently the secondary reaction is partially carried out during this period and is completed during aging. This secondary reaction is the vital part of the process. On it everything depends, such as stability of characteristics and emission life.

SECONDARY REACTION

The secondary reaction is the formation of metallic barium which produces the emission and is believed to be an equilibrium reaction:

$$2BaO \xrightarrow{\text{Further}} Ba \xrightarrow{} O \xrightarrow{} Ba + (?)O$$

The emission actually takes place from the metallic barium produced by the unsatisfied equation. If there is sufficient oxygen to satisfy the barium

there will be little emission, while if the reduction has been carried too far there will not be sufficient oxygen to carry on the continuous reaction with the excess barium. It is believed that the reaction itself is what keeps the barium on the surface of the cathode and is taking place continually, the barium never having enough oxygen to complete the reaction. This may be confirmed by the effect of further heat applied to the cathode. If there is incomplete breakdown, additional gas is introduced, while if there is insufficient oxygen, the barium will be vaporized giving short life and possibly secondary emission from the grid.

There is evidence that emission is from a monatomic film of barium, also that electrolysis within the coating is responsible for the phenomena. Evidence also shows that barium takes part repeatedly, moving toward the core in the form of barium ions which lose their charge and diffuse back as atoms. It has been shown that metallic barium evaporates from the surface and that the barium surface can be supplied through an external source.

PRODUCTION OF BARIUM

Most theories express the belief that emission is from the metallic barium though few offer an explanation as to how this barium is produced. It has been suggested that there are three possibilities:

1.—Thermal decomposition of the oxide.

2.—Chemical reduction.

3.-Electrolytic reduction.

In the opinion of the writer all three possibilities have a definite part in the activation. Heat alone will reduce the barium oxide while there is possible chemical reduction due to the reaction between the core material and the coating. The electrolytic reduction which takes place during aging is due to the application of the anode voltage. The ion bombardment dissociates or reduces the oxide carrying the secondary reaction to the necessary equilibrium.

ACTUAL PROCESSING

Let us now follow through actual processing, observing possibilities which might affect our goal of high emission plus long life. In the preparation of the coating solution we use a mixture of barium carbonate plus strontium carbonate. The reason for this is the activity of the barium, which if used alone would tend to form little pools of barium emission centers when activated, drawing the emission current from spots on the cathode which would tend to cause "hot spots," disturbing the equilibrium, vaporizing the emitter and in the case of a light filament causing burnout. The strontium, being less active, tends to smooth out the barium while itself a fairly good emitter.

BINDER MATERIALS

Some form of nitrocellulose binder is generally added. While to some the presence of carbon formed by the decomposition of the binder on exhaust is a source of worry it is rather quite beneficial as shown:

Actually, the presence of free carbon lowers the breakdown temperature of the carbonate as well as yielding carbon monoxide, a good reducing agent. Carbon is frequently added and while many engineers realize they get better results they do not like to admit they add carbon either directly or indirectly. Cases are known where 5% pure carbon is added to the coating solution; other engineers use turpentine inside the anode; another bombs carbonized plates before the cathode is heated, as it deposits a film of carbon on the cathode surface; and sugar has been added to the binder.

In the breakdown of the coating, if too much heat is applied it will be hard to start activation due to the fact that at the high temperatures its mechanically occluded or chemically combined gas is driven off. This is particularly true when an especially gas-free metal is used for the other elements in the tube.

AGING SCHEDULE

In establishing a "lighting up" or an aging schedule, the most common factors seem to be past experience, cut and try voltages, plus a leaning to some favored theory that the cathode should be flashed as high as the filament will permit, or that bombing should be just under the melting point of the anode or cage in the tube. An application of the "cause and effect theory" should enable us to line up a possible set of schedules which should be reasonably close, being corrected later for variations in conditions, equipment and machine speed.

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Thermionic Emitters

 Detailing the problems involved in the activation of oxide-coated emitters with data on the reduction of "low-emission" productions.

It should be kept in mind that the formation of metallic barium by the reversible equilibrium reaction is what controls the electron emission. Every action which helps to set up this reaction should be considered, while any action which will upset the proper balance of barium and oxygen should be avoided. Let us first consider the effect of bombarding before breaking down the coating. With freshly fired parts, or with parts of a metal having a low occluded gas content, this is not vital. If, due to circumstances, mounts have been exposed to air, permitting absorption or oxidation, the bombing is an advantage as any oxygen will be released into the bulb without affecting the carbonates in the coating. If Svea Metal parts are used, the oxides are absorbed into the surface of the metal. eliminating any danger of poisoning the emitter at a later stage. Pre-bombing should be regarded as a precautionary measure.

The following position is the proper place to start the primary breakdown reaction. As to an initial flashing, it is a matter of opinion, some preferring it, others not. In the opinion of the writer it should be avoided as it tends to liberate carbon dioxide so rapidly as to disturb the bond and loosen the coating. If a porous coating is desired, it should be sprayed on in such a manner during the cathode preparation.

LIGHTING SCHEDULE

The actual lighting schedule depends entirely on conditions and is practically never the same for any two machines or with any two engineers. From the standpoint of production it is an advantage to process the emitter as far as possible on the pumps while to obtain the highest degree of activation requires an ion bombardment internally. In consideration of this fact, aging is recommended. It is generally conceded that carbon dioxide plays a very important part in the activation of the emitter. If this be the case, care should be taken not to carry the primary breakdown too far on the pumps as there will be no residual gas to be ionized by the application of anode voltage on aging. This gas may be from two sources, either breakdown of the carbonates, or from absorbed gas in the parts not completely removed during bombing. If the parts contain little occluded gas, or are completely degassed on bombing, the supply has to be from the further breakdown of the carbonates. This is the better practice as oxygen as well as carbon dioxide may be released from the parts, poisoning the emitter. In view of that fact, too high a lighting schedule should be avoided and a flashing position be used initially on aging.

GAS EFFECT ON AGING

The effect of gas on the aging of the tube offers an interesting phenomenon . . . one not too well understood. It is believed that the application of an anode voltage ionizes the gas present and that the ion bombardment dissociates or reduces the barium oxide, carrying the secondary reaction to the desired equilibrium if properly controlled. If the quantity of gas is excessive, sputtering will be observed. This sputtering is evidently due to positive ions formed by collision with electrons in inert gases and is to be avoided as it tends to actually knock pieces of the coating loose. The control of the amount of carbon dioxide present during aging is both critical and important.

SALVAGING LOW EMITTERS

Another problem faced by the tube engineer is recovery of low emission tubes containing cathodes which have a coating of a light gray or brown color. This color is thought by many to be impurities, possibly carbon from decomposed binder. This material is probably barium peroxide (BaO2). It is formed by the action of oxygen on barium oxide, is gray to brown in color, and breaks down at a relatively low tentperature. It is frequently observed up and down the cathode opposite the grid support wires and sometimes even the grid turns may show by faint lines on the coating.

The control grid, because of the shielding action of the other elements, receives little heat during bombardment on the pumps. Any gas absorbed by

the grid will, therefore, be likely to be driven off during aging when the grid is heated by internal electron bombardment. If this gas is oxygen, and because of the closeness to the cathode, reaction takes place which forms barium peroxide on the cathode at points nearest the control grid. In addition to this there is oxygen provided to satisfy the free barium on the emitter surface, upsetting the equilibrium, and driving the reaction one way to form the inactive barium oxide thus poisoning the emission.

FLASHING

It is well known that flashing these tubes will bring back the cathode to the white color. This is not sufficient alone. If the cathode is heated to a temperature sufficient to break down the peroxide, oxygen is given off which may be taken up by reflashing the getter while the cathode is thus heated, after which the cathode should be flashed or put through the regular aging. Tubes treated in this manner will often give fairly good life.

INCREASE IN AMATEURS

EVIDENCING THE ever-widening interest in amateur radio throughout the United States, its territories and possessions, records just compiled by the Federal Communications Commission disclose that there were 46,390 valid amateur station licenses in existence at the close of the last fiscal year, June 30, 1934.

During the year 8,782 new station licenses were issued and there were 12,-279 modifications, reissues and renewals.

Authorizations as amateur operators totaled 16,686; operator license endorsements for higher privileges 209; duplicates of lost or destroyed licenses 161, and special authorizations 15, making a grand total of 38,132 authorizations issued during the year, or well over 100 per day, relating to amateurs alone.

Applications for amateur operator station licenses pending July 1, 1933, were 497, while 33,184 were received during the fiscal year. Of the total, 21,672 were approved; 8,211 were returned, or referred; 3,631 applicants failed to pass required examinations, and 11 were denied formally, leaving 156 cases pending at the close of June 30, 1934.

Return of applications occurred for many reasons such as lack of citizenship, alien control of premises and misconception of the proper use of an amateur station. Many others had only formal defects, curable by amendment of applications.

1933 CENSUS of Radio Manufacturers

RADIO APPARATUS AND PHONOGRAPHS to the value of \$112,279,565 (at f.o.b. factory prices) were made in the United States in 1933 by establishments engaged wholly or principally in these lines of manufacture, according to a preliminary tabulation of data collected in the Biennial Census of Manufactures taken in 1934, released by Director William L. Austin, Bureau of the Census, Department of Commerce. This is a decrease of 40.2 per cent as compared with \$187,717,880 reported for 1931, the last preceding census year. The decrease in wage-earner employment was much less pronounced, however—only 11.4 per cent, from 36,490 in 1931 to 32,339 in 1933.

(Continued on page 22)

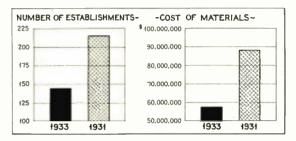


Table 1.-Summary for the Industry: 1933 and 1931

1933	1931	Per cent of increase (+) or decrease
Number of establishments 145		(-) -33.2
Wage earners (average		-33.2
for the year) ¹	36,490	-11.4
Wages ² \$29,124,981	\$35,145,577	-17.1
Cost of materials, containers, fuel, and purchased electric energy ² \$57,483,028 Products, total value ² \$118,273,470	\$88,402,858	-35.0
Radio apparatus and		
phonographs\$112,279,565	\$187,717,880	-40.2
	\$4,479,966	
Custom, repair and	. , ,	•
contract work \$1,303,390	\$944,999	+37.9
Value added by manufac- ture ³ \$60,790,442	\$104,739,987	-42.0

³Not including salaried officers and employees. Data for such officers and employees will be included in a later report. The item for wage earners is an average of the numbers reported for the several months of the year. In calculating it, equal weight must be given to full-time and part-time wage earners (not reported separately by the manufacturers), and therefore it exceeds the number that would have been required to perform the work done in the industry if all wage earners had been continuously employed throughout the year. The quotient obtained by dividing the amount of wages by the average number of wage earners cannot, therefore, be accepted as representing the average wage received by full-time wage earners. In making comparisons between the figures for 1933 and those for 1931, the possibility that the proportion of part-time employment was larger in one year than in the other should be taken into account.

²Manufacturers' profits or losses cannot be calculated from the census figures because no data are collected for certain expense items, such as interest, rent, depreciation, taxes, insurance and advertising.

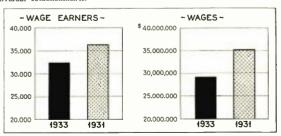
"Value of products less cost of materials, containers, fuel, and purchased electric energy.

Table 2.—Radio Apparatus and Phonographs—Production, by Kind, Quantity and Value: 1933

	Number	Value
Radio apparatus and phonographs made in the radio and phonograph industry, value		\$112,279,565
Receiving sets, complete (cabinet, chassis, speaker, and tubes):		
speaker, and tubes): Number reported	2 451 112	66,839,828
Number not reported, value		2,161,587
For the home, total	2,788,467	53,837,362
Covering standard broadcast band-		
Socket-power operated—Factory price—	404,839	3,400,240
Over \$11, but not over \$30	1,877,166	31,550,623 12,217,077
Over \$30	1,877,166 305,726 92,284	12,217,077 1,922,647
Not over \$11. Over \$11, but not over \$30. Over \$30 Battery operated (excluding batteries) Extending beyond standard broadcast	, _,	2,520,017
socket-power and battery operated (excluding batteries)	108,452	4,746,775
Automobile sets (excluding those for police use)		
Power-operated, including all accessory equipment—Factory price—		
Not over \$22	443,301	7,519,948
Over \$22	219,344	5,459,246
All other sets (including those for police use) ²		2,184,859
Receiving tubes, total	57,042,409	24,197,086
For Replacement, total	34,965,113	15,308,022
Rectifiers (intended primarily for use with receiving sets)		
With receiving sets)	4,864,120	1,967,594
Other (including television-neon and other converters)	30,100,993	13,340,428
For initial equipment, total Rectifiers (intended primarily for use	22,077,290	8,889,064
with receiving sets)	5,736,584	2,157,984 6,731,080
Transmitting tubes, value	(1)	937,213
Light-sensitive (all sizes, all purposes); other, primarily for industrial control		
apparatus; and rectifier tubes other than		
for use with receiving sets2, value	(1)	141,470
Transmitters (including all associated equip- ment):		
Broadcast type, aircraft and ship trans- mitters ²		
Other transmitters for use at fixed locations	108 74	970,035 296,473
Phonographe and accessories		
Phonographs for mechanical or electrical reproductions of records, not including dictating machines ² , value		
dictating machines ² , value	(1) (1)	301,436 2,562,08? 272,284
Needles, value	(1)	272,284
Miscellaneous:	30.092	1,407,650
Receiving set chassis for sale separately as such	25,725	378,371
Loudspeakers for sale separately as such.		
value	(1) (1)	2,797,048 198,858
Microphones (all types), value Other apparatus and products (including dictating machines) ² associated with radio	. ,	
and phonograph equipment, and products		
not reported by kind, value	(1)	8,818,144

¹Data incomplete.

²Figures combined to avoid disclosing approximations of data for individual establishments.



Insulated Wire and Set Production

BY RAYMOND G. ZENDER

LENZ ELECTRIC MANUFACTURING CO.

THE ELECTRICAL characteristics of textile-insulated wire will depend largely on; the kind of fibre, the chemical nature of the insulating materials, the atmospheric conditions under which it is used and the effects of aging.

CHEMICAL ANALYSIS

There are several ways in which electrical leakage can take place in insulated wire but the most important is surface leakage and electrolytic action, present in impure textiles and inferior impregnating compounds when hygroscopical. The electrolytic action will depend largely on the chemistry of the insulating materials and the humidity to which it is subjected.

In laboratory tests the author has found that impurities in the form of salts of potassium and sodium found in unwashed textiles have the most damaging effect on insulation resistance. When insulated wire is placed in a humid atmosphere, small beads of water form on the surface. If exposed for some time, the beads of water spread out and unite to form a continuous film, and during this time water is absorbed by the insulation. This water in turn dissolves the soluble chemicals and electrolytic action takes place. The film of water, together with the soluble salts, form a network of conducting paths on the surface of the insulation.

Insulated wire used in high-frequency circuits, exhibits losses which change with the temperature of the insulation, frequency and applied voltage. In all cases, the radio-frequency phase difference was found to increase after a sample had been subjected to

TABLE NO. I

Insulation: 2 Cotton Braids Waxed

At 74° F. 90% R.H.
for 100 Hours.
Insulation Res.
0.29 Meg. per ft.
Moisture Absorption 0.94%
Power Factor
6.63%

Average voltage breakdown at room tem-

Note: In each of the three Tables, insulation and voltage breakdown measured on one-foot samples immersed in mercury. Moisture absorption by weight. Power factor measured at 1000 kc. (Tests conducted by A. R. McLellan, Consulting Engineer.)

perature: 1925 volts.

TABLE NO. 2

Insulation: 2 Silk Wraps Plus 1 Cotton Braid Waxed

At 74° F. 90% R.H. for 100 Hours. Insulation Res. 513 Megs. per ft. Moisture Absorption 0.94%. Power Factor 6.93% Average voltage breakdown at room tem-

TABLE NO. 3
Insulation: 2 Wraps Cellulose-AcetateTreated Textile Plus ! Cotton

Braid Waxed

perature: 2100 volts.

At 74° F. 90% R. H. for 100 Hours. Insulation Res. 1792 Megs. per ft. Moisture Absorption 0.94% Power Factor 6.68%. At 120° F. 38% R. H. for 100 Hours. Insulation Res. 2083 Megs. per ft. Moisture Absorption Infinity. Power Factor 0.15%.

Average voltage breakdown at room temperature: 2800 volts.

 The importance of adequate insulation for wire used in radio receivers cannot be overemphasized. This article covers recent research into this subject



RAYMOND G. ZENDER.

high humidity, and it was found to decrease upon expelling the moisture by heating. Note power factor difference in the accompanying Tables. Impregnating the textile insulation with a high-dielectric wax compound reduced this effect.

Insulated wire, used in auto-radio sets and home sets, is subject to contamination in the form of dust and dirt containing electrolytic impurities. Auto sets are subject to the oxides of sulphur and carbon which react with the surface film of water on the insulation to form solutions of sulphuric and carbonic acids. This condition has also been found in home radio sets that have been operated adjacent to large industrial factories.

Therefore, those impregnating compounds should be accepted which do not soften at operating temperatures and which do not break down at these temperatures to form any of the series of weak organic acids which create electrolytic action.

The reader will note that the tests shown in the tables were run under two different atmospheric conditions; first, the extreme, and secondly, what is to be conceived as set-operating temperature. In comparing the results it will be noted that the best results, shown in Table No. 3, were obtained on the combination of two wraps of cellulose-acetate-treated textile plus one cotton braid, waxed.

In the selection of proper insulation for hook-up wire, four essential dielectric characteristics should be considered, namely: insulation resistance. power factor, voltage breakdown, and moisture absorption.

ELECTRICAL ANALYSIS

The growing demand for better hook-up wire in radios, necessitated by high-gain r-f systems and shortwave receivers, calls for a new type of

(Continued on page 22)

SEPTEMBER, 1934

Design .. Notes And

SHORT-CUT FOR DETERMINING OPERATING CONDITIONS OF POWER OUTPUT TRIODES

THE APPROXIMATE operating conditions for output triodes can be readily obtained by graphical methods. In the following notes prepared by the Engineering Department of RCA Radiotron Co., Inc., the Power Output Rule is described and simple formulas are given for obtaining the operating current, bias, and load for both single and push-pull triodes. Other formulas are included for converting power output, load, and plate current from one set of plate voltage conditions to another. These formulas are based upon the assumption that the E_e = 0 curve of the plate family follows the three-halves power

POWER OUTPUT RULE

The Power Output Rule (frequently referred to as the Distortion Rule) is used to obtain the plate load and the corresponding power output. This rule was first described by K. S. Weaver in QST of November, 1929. It is the doublescaled rule illustrated in Fig. 1. L1 and L2 have a ratio of 11 to 9, since this is the ratio corresponding to 5% distortion. The zero of the rule is placed at the point on a plate family corresponding to the values of plate voltage and plate current or grid bias under consideration. The slope of the rule is then adjusted so that the reading of the rule at one extreme of the assumed grid swing is the same as that at the other extreme of the grid swing. The slope of the rule when so adjusted corresponds to the load line for 5% distortion.

SELECTION OF THE LOAD FOR A SINGLE-TRIODE OUTPUT TUBE

The plate circuit load for a triode is determined from its plate characteristics curves. If the operating point I. of Fig. 2 is known, the distortion rule can be used directly to obtain the load. If I. is not known, it can be determined from the simple relation, $I_o = \frac{1}{4} I_m$. I_m is obtained by drawing a vertical at the desired operating plate voltage and extending the E. = 0 curve until it intersects the vertical line. One quarter of this value, Im, locates Io, the operating point. The Distortion Rule is then applied with its zero placed at I, and adjusted until L1 reads for the intersection with the zero bias the same as L2 reads for the intersection with the curve for twice the operating bias. The slope of this line represents the load resistance.

The power output can be obtained from the formula:

$$P = \frac{(I_{\text{max}}, \dots I_{\text{min.}}) \ (E_{\text{max}}, \dots E_{\text{min.}})}{8}.$$

LIMITATIONS OF METHOD

The only limitation to the general use of this method is that conditions should not be chosen which exceed recommended maximum plate dissipation of the tube. The best guide to this value is the product of the maximum recommended plate voltage and the maximum recommended plate current. When a value of I. giving too high a tube plate dissipation is obtained, I. should be arbitrarily lowered to bring the plate dissipation within limits. Tubes such as the 112-A, 71-A, 45 and 2A3 are generally operated with control-grid voltages somewhat greater than the theoretical bias value for their maximum plate voltage rating in order that plate dissipation may be kept down. The operating points (I. values) obtained by this method will be found to check the established operating points for types 10, 31, 50 and 89 with triode connection, and to be fairly close for the 112-A and the 71-A. Some readjustment of the grid bias is required for the 45 and 2A3 when used above 180 plate volts.

CONVERSION FORMULAS FOR SINGLE AND PUSH-PULL TRIODES

When a set of conditions for single or push-pull operation of power triodes is known and when operation under some other plate voltage condition is desired, the power output, load resistance, and plate current can be quickly computed by means of the following conversion formulas:

For power output P=A (E) $^{5/2}$ where

P = the power output for the new operating conditions,

A = the power output for the old operating conditions,

E = the ratio of the old and the new plate voltage.

For load resistance $R = B(E)^{-1/2}$ where

R = the load resistance for the new operating conditions,

B = the load resistance for the old operating conditions,

E = the ratio of the old and the new plate voltage.

For plate current $I_b = C (E)^{3/2}$ where

 $I_b =$ the plate current for the new operating conditions,

C = the plate current for the old operating conditions,

E = the ratio of the old and the new plate voltage.

The practicability of these formulas is shown by the example of a triode-connected 89 given in the accompanying table:

Plate Volts Grid Voits Plate Milliamperes Plate Load (chms) Power Output (watts)	183 22.5	version Factors 1.39° 1.39 (1.39) ³ / ² (1.39)-1/ (1.39) ⁵ / ²	
*250/180 == 1.39.			

For filament types of tubes, such as the 10, 45, 50, 71-A, and 2A3, the plate characteristics curves are given for de filament excitation, although operating characteristics are generally shown for ac filament excitation. For these types, conversion calculations are made on a de excitation basis. To adjust ac excitation bias values to corresponding devalues, reduce the de values by ½ the peak value of the rms filament voltage. To adjust de values to ac values, add ½ the peak value of the rms filament voltage to the de value of grid bias.

LIMITATIONS OF FORMULAS

The conversion formulas are accurate except for over-biased operation. Thus, for the 45 and 2A3 at voltages greater than 180 volts, these conversion formulas can not be used unless adjustment is made to keep plate dissipation within limits.

SELECTION OF LOAD FOR TRIODES IN PUSH-PULL

To obtain the proper load for triodes in push-pull, the relation $E=0.6\ E_{\circ}$ is used (see Fig. 3). Plate characteristics curves for the triode are required. An operating plate voltage E_{\circ} is then selected. A vertical is erected at $E=0.6\ E_{\circ}$ and the intersection of this vertical with the $E_{\circ}=0$ curve determines one end of the load line. The other end is at E_{\circ} , the operating plate voltage. The slope of this line multiplied by four is the correct value of plate-to-plate load for two triodes operating in a Class A push-pull amplifier. Thus, for the 45 (see Fig. 3), the plate-to-plate load is equal to

$$\left(\frac{250-150}{0.096}\right) \times 4$$
, or 4160 ohms.

This simple method for determining the plate-to-plate load is applicable to all power-output triodes. The oper-

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COMMENT . . Production

ating point can be anywhere between the bias voltage specified for single-tube operation and the bias voltage obtained by taking one-half of the control-grid bias at plate current cut-off for a plate voltage value of 1.4 Eo. Fig. 3 shows the plate family of a 45 tube. The recommended operating point as a single triode is - 50 volts. The maximum bias that can be used without departing from Class A operation is - 55 volts. Plate current cut-off at 1.4×250 volts, or 350 volts, occurs with a control-grid bias of -110 volts. One-half of this value is -55 volts, the maximum bias. Operation beyond this value of grid bias will be accompanied by rectification and will no longer be representative of a Class A amplifier.

POWER OUTPUT FORMULA FOR PUSH-PULL TRIODES

The method just described of determining the plate-to-plate load also makes it possible to determine the power output for push-pull triodes by means of the following simple formula:

$$P = \frac{I_m E_o}{5}$$

Thus, for the 45's of Fig. 3, power output is equal to

$$\frac{0.096 \times 250}{5}$$
, or 4.8 watts.

RCA-955 (ACORN TYPE) TUBE

RCA RADIOTRON will soon announce the acorn-type tubes, which were designed some time ago for use in connection with equipment operating at ultra-high frequencies.

The acorn-type tubes have been developed for the use of experimenters and amateurs and are not considered in any way as an addition to the standard line of receiving tubes. No doubt these tubes will eventually find general use. In the meantime there is much to be learned about their capabilities and the fact that they are to be made available for experimental purposes will expedite individual research.

CHARACTERISTICS OF TUBE

The 955 tube may be used as an amplifier, a detector or an oscillator. The tubes will oscillate at frequencies up to 600 megacycles, or approximately 0.5 meter.

The essential characteristics are as follows:

241101101
Heater Voltage6.3 volts
Heater Current0.16 amp
Plate Voltage (max.) 180 volts
Grid Voltage5 volts
Plate Current (max.)4.5 ma

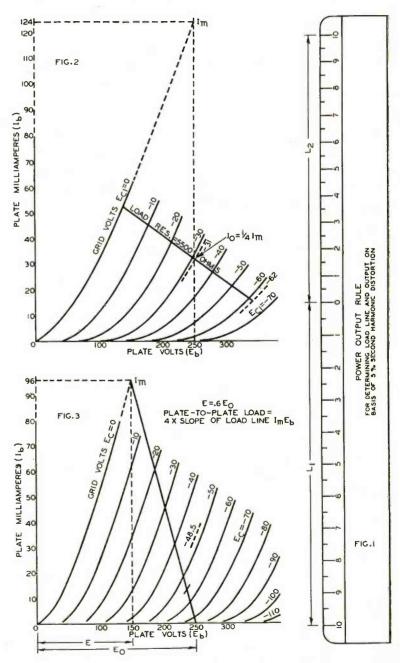
Mutual Conductance.....2000 m-mhos Amplification Factor 25

Plate Resistance 12,500 ohms

Mechanical and electrical features which permit unusual applications rather than the features which would make the tube suitable for use in commercial production receivers, have been

stressed. These features provide considerable latitude to the experimenter.

No attempt should be made to solder connections to the electrode leads of the tube, since soldering usually results in breaking the glass envelope of the tube. The r-f ground must be extremely good at ultra-high frequencies.



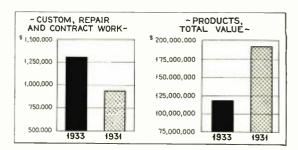
1933 CENSUS of Radio Manufacturers

(Continued from page 18)

1933 PRODUCTION TOTALS

The more important items which contributed to the production total for 1933 are as follows: Radio receiving sets for the home (except combination radio and phonograph units), 2,788,467, valued at \$53,837,362; combination radio and phonograph units, 30,092, valued at \$1,407,650; all other receiving sets (including automobile and aircraft sets), \$15,164,053; receiving tubes for initial equipment, 22,077,296, valued at \$8,889,064; receiving tubes for replacement, 34,965,113, valued at \$15,308,022; phonographs (not including dictating machines), \$301,436; records and blanks, \$2,562,082.

The industry, as defined for census purposes, embraces establishments engaged wholly or principally in the manufacture of radio apparatus, phonographs and parts and accessories for either or both.



Summary statistics for 1933 in comparison with 1931 are presented in Table 1, and detailed production statistics for 1933 are given in Table 2. All figures for 1933 are preliminary and subject to revision.

AUDIO-FREQUENCY TESTING

(Continued from page 16)

added to that produced by the attenuation network in all cases to obtain the total network loss. The loss increases with the ratio of impedances, and may be calculated from the following expressions:

$$\begin{bmatrix} \sqrt{\frac{R_{\text{A}}}{R_{\text{N}}}} + \sqrt{\frac{R_{\text{A}}}{R_{\text{N}}}} - 1 \end{bmatrix}$$

HUM MEASUREMENT

With an ac-operated amplifier set up in the gain test, other pertinent data may be obtained. The hum level may not only be noted but, in addition, the relative components of hum frequency may be approximately evaluated. It often-times happens, especially in pushpull amplifiers, that the observed hum with no signal is quite permissible due to cancellation in the output circuit with well balanced tubes, but when the amplifier is excited the tone is garbled by the unbalanced condition that obtains during a portion of the audio cycle. A transmission test for hum is especially desirable for the detection of the latter condition.

With the amplifier set-up in the circuit of Fig. 2, a normal input voltage is applied at a frequency differing from 60 cycles by a small amount, say, one-half to one cycle. The output meter will indicate this beat and swing slowly between certain limits on the scale and the amplitude is a qualitative indication of the 60 cycle component of hum. In the same way the 120 cycle and higher harmonics can be evaluated. By learning the relative amplitudes of the various hum frequencies in a qualitative way much of the probable cause of the hum

in the design is indicated. The method can be arranged, of course, to provide quantitative results, (See Suits, *Proceedings* I.R.E.) but the application suggested is probably sufficiently indicative of the true operation of the amplifier for most purposes.

OTHER AUDIO MEASUREMENTS

The basic principles of gain measurements as outlined above may be applied to all sorts of audio-frequency equipment. Telephone lines are measured with the line substituted for the amplifier shown in Fig. 2. Usually individual volume indicators are employed at the sending and receiving ends of the line. The attenuation network at the line input is not always necessary.

The beat-frequency oscillator and auxiliary equipment is indispensable in overall tests of sound reproducing equipment of all types.

INSULATED WIRE CHARACTERISTICS

(Continued from page 19) insulation to meet the requirements. In the accompanying Tables are characteristics of various combinations and types of textile-insulated hook-up wire, including results of tests on a most recently developed and, incidentally, highly efficient insulation, as shown in Table No. 3.

UNDERWRITERS' VIEWPOINT

Through the courtesy of the Underwriters' Laboratories, the writer is privileged to set forth other interesting information. As is generally known, the Underwriters are chiefly concerned with those destructive hazards that may create property damage or personal injury. Consequently, their interest centers on component parts and their

proper assembly into complete units functioning efficiently with wide safety margins.

They specify that insulation must withstand a breakdown test involving a potential of three times the maximum open-circuit voltage to which wires are subjected. Therefore, since the average peak voltage in most radio circuits is 500 volts, it follows that any combination of insulations shown in the breakdown tables will suffice. However, insulation resistance, power factor and moisture absorption must also be considered for efficient performance.

The following information taken from the published pamphlet entitled "Underwriters' Laboratories Requirements for Power-Operated Radio Receiving Appliance," dated April, 1933, shows the attitude and refinement of these laboratories on temperatures to which several types of insulation may be subjected:

"Materials will be considered adversely affected if temperatures higher than the following are attained:

90° C.—On conductors having fiberous textile materials such as cotton, silk, etc.

90° C.—On conductors having slow-burning insulation.

49° C.—On conductors having rubber insulation."

I. R. E. FALL MEETING

THE ANNUAL FALL meeting of the Institute of Radio Engineers will be held in Rochester, N. Y., November 12, 13, 14, 1934. This is one of the highlights of the year and every engineer should plan to attend.

An outstanding program has been arranged. There will be the usual Technical Sessions and Engineering Exhibits.

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NEWS OF THE INDUSTRY

SVEA METAL ENGINEER

The Swedish Iron & Steel Corporation,
17 Battery Place, New York City, suppliers of Svea Metal for internal vacuum tube parts, announced the engagement some time ago of Mr. Lauren L. McMaster, Jr., as Chief Engineer.



L. L. McMASTER, JR.

Mr. McMaster is a chemical engineer with five years experience in two of the major radio tube plants where he has been in constant contact with all phases of factory management. He has likewise done considerable research work on oxide

considerable research work on oxide coated cathodes and made a careful study of the processing of tubes in production.

Since his association with the Swedish Iron & Steel Corporation, Mr. McMaster has been successful in solving many of the problems which have arisen in connection with the application and use of Svea Metal in the electronic tube field.

AIR EXPRESS RATE REDUCTIONS

Substantial rate reductions in air express Substantial rate reductions in air express handled over a nationwide network of commercial airlines by Railway Express Agency, became effective August 15, according to J. H. Butler, General Manager. Outstanding reductions permit air express shipments of packages weighing 34 lb., or less, at the flat rate of 85c, regardless of distance carried. The corresponding charge for one pound shipment is \$1. Minimum for one pound shipment is \$1. Minimum charges previously ranged up to \$1.80. General lowering of tariffs affects particularly the lighter-weight shipments, which now the lighter-weight shipments, which now constitute the greatest percentage of pack-ages handled over the airlines. Yet new low rates also provide for air shipment of packages weighing up to 25 lbs. between cities 149 air miles apart, at a cost of \$1, including special pick-up and delivery.

SPANGLER APPOINTED SALES MANAGER

John M. Spangler, who as "Jack" Spangler is personally known to hundreds of officials and salesmen throughout the country in the railroad, electrical, hardware, radio and automotive fields, has been made

general sales manager of National Carbon Company, Inc.,

The promotion is the latest of a series of advances which began almost with Mr. Spangler's initial connection with the National Carbon Company in 1915. Previous to that, he had devoted two years, following his graduation from Penn State College, to railroading with the New York Central, where he was connected with the signal department, chiefly in Albany and Rochester, N. Y.

MAJOR ARMSTRONG WITH

MAJOR ARMSTRONG WITH COLUMBIA UNIVERSITY Major Edwin Howard Armstrong has been appointed professor of electrical en-gineering in Columbia University, it is an-nounced by President Nicholas Murray

Major Armstrong, carrying on a notable Columbia tradition, will direct instruction in radio communication and high frequency research in the Hartley laboratories, the scene of Prof. Michael I. Pupin's triumphs in electrical transmission and of his own early efforts in the development of the vacuum-tube oscillator, which revolutionized radio.

INCREASE IN SHOW ACTIVITY

A listing of the more important industrial and trade shows, issued recently in a Bulletin of the Exhibitors Advisory Coun-Gilletin of the Exhibitors Advisory Coun-cil, revealed the fact that more shows and expositions have been held during the first six months of 1934 than were scheduled over a similar period in 1933. In addition the Council, through its trade association and show management con-

tacts, has learned that show promoters and trade groups sponsoring shows are anticipating a larger number of exhibitors and more responsive attendance at their shows scheduled this Fall and next Spring.

EARPHONE-MIKE FOR TRANSCEIVERS

Universal Microphone Co., Inglewood. Cal., will soon manufacture a combination earphone-microphone to be used on the new five-meter transceivers. It will weigh approximately nine ounces.

BOOK ON APPLICATION OF NICKEL

A new booklet on the applications of Monel Metal, Nickel, and Nickel-clad steel has been issued by the Technical Service Department of the International Nickel Company. It has been prepared especially for users of industrial processing equip-

Besides giving data on the physical and mechanical properties of these materials, the booklet contains considerable miscellaneous information, including instructions on the selection of suitable welding rod and other details on fabrication. Copies will be supplied without charge on request to the Editorial Department. The Interna-tional Nickel Company, Inc.

NATIONAL UNION DIRECTORS

NATIONAL UNION DIRECTORS
ELECT OFFICERS
S. W. Muldowny, Chairman of the
Board of National Union Radio Corporation, announced this week that, at a meeting of the Board, held at New York City
on July 31st, Mr. H. A. Hutchins, National Union General Sales Manager, was

made Vice President, as was Mr. George Ernst, who has held the position of General Superintendent of factory operations. Another election at the same meeting elevated Dr. Ralph E. Myers to the First Vice Presidency. Dr. Myers has heretofore held the title of Vice President in charge of manufacturing and engineering. Mr. H. R. Peters remains as President.

ZENDER MADE RMA CHAIRMAN OF WIRE GROUP

Raymond G. Zender, Sales Manager of Lenz Electric Manufacturing Company, has been appointed RMA Chairman of the Wire and Transformer Coil Group. It is Mr. Zender's intention to work towards standardizing on color coding and various constructions of lead wires during the time of his chairmanship.

ALLEN-BRADLEY APPOINTS NEW CLEVELAND MANAGER

R. J. Roy, formerly Cleveland branch manager for the pump and electrical de-partment of Fairbanks, Morse & Company, was recently appointed district manager of the Allen-Bradley equipment in the Cleveland, Pittsburgh, and Cincinnati territories.

SIPP JOINS BURGESS

Mr. E. A. Sipp, until recently Manager of the Lighting Division of Pyle-National Company, has become associated with the management of the Burgess Battery Company and C. F. Burgess Laboratories, Inc.



E. A. SIPP.

Mr. Sipp will maintain his headquarters in the offices of the Burgess organizations at 111 West Monroe Street, Chicago, Illi-

LINCOLN TO BE N. E. E. HEADQUARTERS

Hotel Lincoln is to be official headquarters for the delegates to the National Elec-trical Exposition at Madison Square Gar-den September 19-29, 1934. The Lincoln

(Continued on page 24)

SEPTEMBER, 1934

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will take a progressive and important step by being probably the first hotel to exhibit

at a trade show.

The hotel will exhibit the equipment of one of its typical two-room suites in the section adjacent to the broadcasting stu-dios on the Exposition Floor of Madison Square Garden.

Many rooms at the Lincoln will be set aside for private showing of various electrical companies, who will repeat last year's special sales campaign at that hotel during the trade show.

NEW KENYON CLASS A-B AMPLIFIER KIT The Kenyon Transformer Co., Inc., 840 Barry St., New York City, has introduced a unit designed to act as a public-address amplifier capable of delivering either 18 or 36 watts power output. This output is achieved by using either push-pull Class A-B 45s or push-pull parallel Class A-B 45s in the output stage. By unique type of chassis construction, using one chassis for the audio channel and one chassis for the power channel, it is possible to change this amplifier from an 18-watt amplifier to a 36-watt amplifier by merely installing two

tubes, two transformers, and a filter re-

actor. The mechanical construction of the chassis also permits the operation of the amplifier as a rack and panel unit, or as a table mount unit. In the past on rack mount amplifiers built on a chassis, it was necessary to remove the amplifier chassis from the panel before the amplifier wiring became accessible. With the new units it is only necessary to remove four 10-24 screws to remove the panel. When the panel is removed, the chassis is held in place to the rack by an additional four screws which have no connection whatsoever with the panel. Thus, when the panel is removed

A common voltage amplifier is used for either the 18- or 36-watt condition. This amplifier consists of a pair of 77 pentodes operating push-pull impedance coupled to a pair of push-pull 76 tubes. The overall gain is said to be 80 db. Despite the high gain of the voltage amplifier, it is said the hum level has been kept down to 50 db with respect to full power output. Microphonic noises which might otherwise be transmitted through the amplifier by the 77 or 76 tubes have been eliminated by mounting these voltage amplifier tubes in a phosphor bronze spring suspension.

all wiring is exposed.



VETERAN WIRELESS OPERATORS ASSOCIATION NEWS

GEORGE H. CLARK "Radio's Toastmaster"

Graduated an Electrical Engineer by the Massachusetts Institute of Technology in '03—with John Stone Stone in Boston for five years as Radio Engineer—entered active duty in Navy Department at Washington in 1908 and advanced to the office of Expert Radio Aide—joined the Marconi Wireless Talia Aide of Expert Radio Aide—Joined the Marconi Wireless Telegraph Company of America in 1919—became the Showman of Radio for RCA in 1921—awarded medal at Sesquicentenial in Philadelphia for "excellent historical display"—and throughout that period to the present functioning as Radio's Toastmaster at dinners and banquets giving thumbnail sketches of radio developments and its associated aspects, George H. Clark has been conspicuously active. Organizing and bringing together remotely associated interests in the radio art and industry, he is known from coast to coast. He has helped promote many successful social functions through which the personnel of the radio industry has become better acquainted to the advantage of their respective business enterprises.

Despite the prominence of his activities he remains the easily approachable acquaintance and friend of all. He is the unspoiled "Man With the Hoe," ever thinking of the other fellow and his inter-ests. The V. W. O. A. is proud of his record as Vice-President, Director and Chairman of many committees, but as Toastmaster at our Annual Banquets he

has excelled.

His name is a by-word in radio circles, known everywhere—for hasn't he toured every neck and corner of the country as the "RCA Showman"? Yes, and he is known in other countries, too. His first big engineering job following the termination of his Navy service at the conclusion

of the war, was the construction of the two big radio stations in Venezuela.

Marconi in Italy knows him as "George". Radio men in other countries have become familiar with the far-reaching cry for obsolete radio equipment to complete the only Radio Museum of note, of which he is Curator.



G. H. CLARK Vice-President

To the veteran wireless men the name of this distinguished pioneer engineer symholizes much more than a personage of world-wide fame. He is one of the mainstays of the Veteran Wireless Operators Association. He loves what the organization stands for. He has done much for it is the poor and today to it done the it in the past and today he is doing still more.

There is an exhibit at the Century of Progress Exposition in Chicago which

graphically portrays the quarter-Century of Progress in the development of radio. George Clark designed it and during the Exposition, as visitors come and go, George will be found near it ready to greet veteran and novice in the art of radio with equal pleasure.

"CHINA SKYWAYS"

The return address on the envelope is Foreign Y. M. C. A., 150 Bubbling Well Road, Shanghai, China. The letter is signed by Wm. W. ("Flying Bill") Ehmer, the original "WE" for that was his sign on the air lanes twenty years back. "WE" is a true veteran radio operator but during recent years has confined his activities to piloting. He holds a Commercial Transport Pilot's license and is at present engaged in blazing new trails for China Airways Federal, Inc., throughout China. He writes, in part, as follows:

"By the way, chop suey is a food that very few folks eat out here when they visit a Chinese restaurant. There are so many other nice foods that chop suey takes a back seat. It takes considerable experience to order correctly, and after a year I get my soup last or in the middle

year I get my soup last or in the middle of the meal and am beginning to think it is some sort of 'Chinese' custom.

"Our flying on the Canton line has been temporarily suspended until we receive the new planes which have been ordered. We get some very bad weather on the Shanghai-Canton route. In one season we encounter had force at the other statements. season we encounter bad fogs on the northern end and heavy squalls on the southern and central sections with heavy monsoon winds which bucks us going and helps us coming back. However, in the other season we have only a dozen or more typhoons and frequent thunderstorms to

"To overcome these conditions we are getting faster ships and putting in more radio stations. We always had radio at every stop but there was no way of obtaining information on conditions in between; thus, if conditions at the point of departure and the destination were favorable, the plane would leave. We are at able, the plane would leave. We are at present installing stations in between stops, especially in the worst weather sectors, so that a plane's pilot will know what to expect at all times. At present I am preparing to put in a 100 watter in a little lighthouse in the middle of Hangchow Bay. I am temporarily handling radio installa-tions. We use all English speaking Chinese operators and they are quite

capable.
"We are also getting radio direction finders out here. The type used will be a compared extractions and take stationed at the ground stations and take bearings on planes on wavelengths of 187 to 197 meters. Good results have been obtained

thus far.

"Have met many operators and exoperators in these parts. The ex-operators are generally sound-motion-picture or broadcast men. George F. Shecklen, one of our members, represents RCA here. Best regards to all." "WE"

MEETING

The next regular meeting of the membership of the Veteran Wireless Operators Association will be held at 6 PM Wednes-Association will be need at 0 Faw vectors day evening, October 10th, 1934, at Daniel's Grill, 94 Chambers Street in the City of New York. Plans for a Fall Smoker as well as other plans for our winter activities will be discussed at this meeting. We urge the attendance of our membership to this, the first meeting after the summer vacation.



THE New weston model 681

Here is a tube checker and merchandiser that will help you make friends . . . help build your business. It does a thorough test job, and does it in a manner that is impressive and convincing to your customers. The design and color scheme are compelling; and the large 9" meter, set at an easy reading angle, gives direct indication of tube conditions in understandable terms.

And Model 681 has been designed and engineered to end obsolescence worries. Twenty-five sockets are provided in the panel with seven spares for use when and if new tubes are developed. It not only tests all present 4, 5, 6 and

large and small 7 prong tubes but also makes individual tests on each section of all double and triple plate combinations. It makes a complete inter-element short test, a high resistance cathode leakage test, and a mutual conductance test on all tubes.

Dealers, jobbers and engineers who have seen Model 681 have voiced their enthusiasm. All agree that its many outstanding features make it the greatest value available in tube checkers. You will want all the facts. Mail the coupon today . . . Weston Electrical Instrument Corporation, 612 Frelinghuysen Avenue, Newark, New Jersey.

WES	TON	MRA.
7.	1	
Naaio	Instrum	rents

WESTON	ELECTRIC	AL INST	RUMENT	CORPORATION
612 Freli	inghuyser	Avenu	e, Newa	rk, N. J.
Send bu	lletin on	Weston	Radio	Instruments.

Nanie	 	
Address	 	
C: 1 C: .		

Purchasing Guide

The following pages contain information which it is believed will be of value to executives, engineers and purchasing agents. The companies listed are recognized sources of supply whose products thru past and present acceptance and use by the radio and allied industries, have achieved a reputation for merit and satisfactory performance.

In presenting this information, Radio Engineering

assumes no responsibility for omissions. We have tried to give comprehensive and accurate information. We have tried to make the information usable and as complete as possible. If we have unintentionally overlooked or omitted information, we'll be only too glad to have it brought to our attention and will make any needed additions in a following issue of the publication.

For the purpose of brevity and convenience, the listings are grouped in rather broad classifications which include groups of related materials or components. See Index below.

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TUBE MACHINERY	38	Solder Stop Nuts
TUBE PARTS AND MATERIALS — Including Wire	38	Tape
		m

OUR READERS ARE CORDIALLY INVITED TO COMMUNICATE WITH US AT ANY TIME CONCERNING PRODUCTS WHICH THEY ARE INTERESTED IN PURCHASING. WE WILL BE GLAD TO GIVE PROMPT, UNBIASED INFORMATION REGARDING SOURCES OF SUPPLY.

Broadcasting and Public Address Equipment Amplifiers, Attenuators, Crystals, Decade Boxes, Microphones, Mixers, and Miscellaneous Equipment

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Los Angeles, Calif. Microphones of All Kinds. New York Office: 27 Park Place, N. Y. C.

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PRODUCTS Microphones.

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PRODUCTS

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Standards.

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SEPTEMBER, 1934

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FEDERAL TELEGRAPH CO. 200 Mt. Pleasant Avenue, Newark, N. J. Transmitting Tubes.

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Assistant Chief Engineer......P. L. Tourney

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159 East Elizabeth Street, Detroit, Michigan.

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HEINTZ AND KAUFMAN, LTD.

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HYGRADE SYLVANIA CORPORATION (See page 36) Electronics Department, Clifton, New Jersey

PRODUCTS

Radio Transmitting Tubes, Phototubes, Industrial Power Tubes, Radio Transmitters. Special Radio Receivers, Sound Amplifiers, Broadcast Speech Equipment, Custom-Built Electronic Devices.

INT'L BROADCASTING EQUIPMENT CO.

3112 W. 51st Street, Chicago, Ill. Frequency Monitors—Amplifiers.

(Continued on page 28)

Page 27

Broadcasting and Public Address Equipment (Continued)

(Continued from page 27)

JENKINS & ADAIR, INC.

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JENKINS & MILER & SOUND & TELEVISION CORP. -Sound Equipment. Philadelphia, Pa. Amplifiers, Sound Equipment.

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The M. Simons & Sons Co., 25 Warren St., New York, N. Y.
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L. M. Wood, Wood & Anderson Co., 915 Olive St., St. Louis, Mo.
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Clawson, care Harry W. Gebhard, 55 Kilby St., Boston, Mass.

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SOUND SYSTEMS, INC.

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PRODUCTS

Crystal Microphones. P. M. Dynamic Speakers. Amplifiers and Control Equipment for Rack and Panel Mounting. Precision Equipment for Special Uses. Special Systems for Dance Bands, Funeral Parlors. School and Hospital, Sound and Centralized Radio. Hotel Systems. Hearing Aids. Turntables. Transformers. Crystal Pickups, High-Fidelity Units.

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For all other Western Electric equipment, the distributor is the Graybar Electric Company through their branches.

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HAMMARLUND MFG. CO. (See page 27) 424 W. 33rd Street, New York City.

MEISSNER MFG. CO. 522 S. Clinton Street, Chicago, Ill.

SICKLES COMPANY

300 Main Street, Springfield, Mass.

PRODUCTS

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P. Mack, 1603 So. Michigan A.ve., Chicago, Ill.
G. O. Tanner, 345 Fourth St., Pittsburgh, Pa.

Ad. Auriema, Inc., 116 Broad St., New York, N. Y.

Condensers, Fixed. Dry Electrolytic, Wet Electrolytic, Mica and Paper

ACME WIRE COMPANY (See page 40)

New Haven, Connecticut. Paper Condensers and Condenser Parts.

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P. R. MALLORY & CO. 30:9 E. Washington Street, Indianapolis, Ind. All types. MICAMOLD RADIO CORP. 1087 Flushing Avenue, Brooklyn, N. Y. All types.

Page 28

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WIRE SHEET ROD

FANSTEEL . . . best source of supply

Fansteel Molybdenum is always of exceptional purity and meets exacting specifications for dimensions and physical characteristics. It is the result of 15 years' specialization in this field.

Fansteel Molybdenum is made from start to finish in the Fansteel plant at North Chicago, Illinois. This insures prompt deliveries and facilitates furnishing any type of wire, sheet or rod to meet your particular requirements.

Fansteel Tantalum has unusual advantages for tube parts and is available in sheet, rod and wire in all commercial Sizes

Fansteel Tungsten wire, sheet and electrical contact points are supplied in a wide variety of sizes and types.

Samples, prices and data will be promptly furnished to manufacturers.

Fansteel Products Co., Inc. NORTH CHICAGO, ILL.

NOW-perfect reception on all modern automobile radios with these new STACKPOLE specialties

For smoother and more perfect auto radio reception, Stackpole announces 3 timely improvements of interest to all radio engineers. . . . {1} The new Spark Plug and Distributor Type Auto Spark Suppressors; (2) The New Paper Type Radio Volume and Tone Control, and (3) Stackpole Fixed Resistors.

Eliminate Ignition Interference with the New STACKPOLE CARBON AUTO SPARK SUPPRESSORS



Designed especially to effectively suppress the high voltage discharge of automobile ignition on any car, Stackpole Suppressors consist of a resistor unit molded into a bakelite housing with connections molded into the bakelite at the same time . . . assures a solid, unified structure unaffected by heat, high humidity, vibration or rough usage. Direct electrical contact made from terminal to resistor element, eliminating troublesome steel wool and springs. Note cuts D and E above. Standard units have resistance value of 5,000, 10,000 and 20,000 ohms.



- The bakelite hub, which carries the contact, fully insulates the moving contact and resistance element from bushing and shaft... very necessary in a great number of applications.
- The Switch-Operating cam, is fastened directly to the bakelite hub and therefore, fully insulated from the resistance element.
- Uniform contact Pressure is maintained by a specially designed coil spring carried within the bakelite hub—always maintains the correct contact Pressure.
- The newly designed contact maintains a true line contact with the resistance element, thus eliminating any possibility of noise due to contact resistance.
- resistance. New type "P" resistance element made by depositing carbon on high grade paper. Element is fired at high temperature making it permanent and unaffected by changes of humidity and temperature.

Stackpole Fixed Molded Carbon Resistors

Non-inductive ... unaffected by humidity ... the standard of comparison in the radio and electrical fields ... designed for voltage reducers, cathode bias resistors, orld leaks and suppressors, tube plate loads and all radio and audio circuits.

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TOBE DEUTSCHMANN CORP.
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81 Prospect Street, Brooklyn. N. Y.

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OAK MFG. CO.
308 W. Washington Street, Chicago, Ill.
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Abrasive Products and for Waterproohing Fabrics.

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Synthane Laminated Bakelite, Sheets, Rods, Tubes, Fabricated Parts, Stabilized Gear Material.
Synthane Corporation has devoted itself exclusively to the production of laminated bakelite. The plant itself was laid out and built in 1929 to the requirements of laminated bakelite manufacture. This also guided the selection of equipment and, in several instances, machines were specially designed and constructed that would definitely contribute to a better and more uniform product. Enlarged in 1934. Facilities for machining and assembling laminated bakelite parts on a production basis are now available to manufacturers. EXECUTIVES

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Fixed Radio Resistors, Spark Plug Suppressors, Bradleyometers, and other Variable Resistors, Filament Rheostats, Adjustable Grid Leaks, Relays, and a complete line of Industrial Electric Controlling Apparatus, such as Motor Starters, Controllers, Contactors, Relays, etc.

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GOAT

TUBE PARTS



PRODUCTS

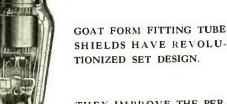
TUBE SHIELDS





GOAT QUALITY PARTS IM-PROVE TUBE PERFORM-ANCE.

WE MANUFACTURE AT MOD-ERATE PRICES AND IN UN-LIMITED QUANTITIES PARTS FOR ALL STANDARD RE-CEIVING TUBES, AND ALSO HAVE FACILITIES FOR PRO-DUCING SPECIAL PARTS FOR CATHODE RAY RECTIFIERS, POWER TUBES, X-RAY TUBES, ETC.



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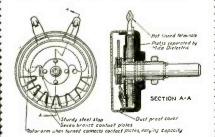
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Over 100 Manufacturers Use



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They afford an unequalled smooth tone taper from treble to bass between 7 variable capacity steps. Compact, accurate and very reasonable in price, they cut space requirements and assembly costs, and no condenser need be added. That is why more than 100 leading receiver and sound equipment manufacturers specify Octave Tone Controls.

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Standard shaft ½" long, bushing ½" long, ½" diameter. Standard capacity range from 50 M. MFD. to .006 MFD. (Other capacities available from almost zero to .02 MFD.) Dimensions: 1½" diameter by 11/16" deep. Controls furnished with or without power switch. (Special shafts available to specifications.)

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 F.M.C. porcelain case fixed condensers were designed to meet the demand for rugged commercial units of exceptional quality. Yet they are priced low enough to warrant their use in even the cheapest receivers.

Study these F.M.C. features . . . compare these new units on a quality and price basis.

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- Climatic conditions, heat and cold, cannot effect them. They are moisture proof, very rugged, and compact.
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EXPORT

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Eric Resistor, Ltd., Waterloo Road, Cricklewood, London, England.

FILTERMATIC MFG. CO.

6913 Ditman Street, Philadelphia, Pa.

PRODUCTS Condensers.

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Harry Fox, 1157 South Hill St., Los Angeles, Calif.
L., W. Nutt Sales Co., 618 Dayton Industries Building, Dayton, Ohio.
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HARDWICK, HINDLE, INC.
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INTERNATIONAL RESISTANCE CO.

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I.R.C. Fixed and Variable Resistors, I.R.C. Volume Controls and Potentiometers, I.R.C. Motor-Radio Suppressors, I.R.C. Precision Wire Wound Resistors, I.R.C. Heavy Duty Power Wire Wound Resistors. Metallized Resistors.

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St. Louis, Missouri.
New Orleans, La.
Atlanta, Ga.
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New York City, N. Y.
Pittsburgh, Pa.

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International Resistance Co., Italy. Other Offices in Australia, New Zealand, South America, Mexico and most countries.

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3029 E. Washington Street, Indianapolis, Ind.

MICAMOLD RADIO CORP. 1087 Flushing Avenue, Brooklyn, N. Y.

THE MUTER CO. (See page 30) 1255 S. Michigan Avenue, Chicago, Ill.

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E. J. Fenton, 1775 Broadway, New York City.
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Jeffries & Hartweg, 916 Packard Bldg., Philadelphia, Pa.
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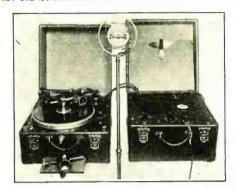
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Page 33

Sockets, Dials, etc. (Continued)

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Dynamic Speakers, High-Fidelity Speakers and Permanent Speakers as Standard Reproducing Equipment in All Makes and Types of Radio Broadcast Receivers, Public-Address Installation. Sound Distribution Systems, and Kindred Apparatus. Also Wet and Dry Electrolytic Capacitators of All Kinds for Use in Radio Broadcast Receivers, Radio and Line Wire Transmitting Stations, Motor Starting and Control Apparatus, and Industrial Applications.

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Air Column Horns, Electro-dynamic Speakers, High-frequency Speakers, Public Address Equipment.

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Radio Transformers, Neon Transformers, Stepdown Transformers, Voltage Adjustors, Spark Plug Testers, Ozone Devices.

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Vice President.....J. A. Comstock
Purchasing Agent.....J. A. Comstock

Purchasing Agent......J. A. Comstock

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F. C. Somers, 2004 Grand Avenue, Kansas City, Mo.
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L. G. Cushing, 9 South Clinton Street, Chicago, Ill.
Harry C. Harrison, 409 South 7th St., St. Louis, Mo.
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PRODUCTS Amplifiers, Transformers and Reactors.

President.....F. P. L. Kenyon Sales Mgr......Paul R. Fernald
Chief Engineer....Edward J. Friebele
(Continued on page 36)

RADIO ENGINEERING

Page 34

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FOR HOME SETS and AUTO RADIOS







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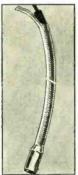
BATTERY ADAPTER CABLE

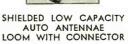
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SEPTEMBER, 1934

Transformers and Chokes (Continued)

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R. E. Stemm, 28 East Jackson Boulevard, Chicago, Illinois.
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James Millar, 316 Ninth Street, N. E., Atlanta, Georgia.
Conrad R. Strassner, 160 South Hobart, Los Angeles, California.
Arnold Sinai, 341 Tenth Street, San Francisco, California.
G. O. Tanner, 345 Fourth Avenue, Pittsburgh, Pennsylvania.
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President Allen R. Du Most Scale Management of Cathode Scale Managemen

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General Manager.....H. C. Holmes

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W. Stuart Canton, 70 Arnold Avenue, Edgewood, Rhode Island.

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American Radio Corp.. 175 Rue Blomet, Paris. France.

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GENERAL RADIO CO.
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INTERNATIONAL RESISTANCE CO. (See page 32)
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WESTINGHOUSE ELEC. AND MFG. CO.
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PRODUCTS

Receiving and Transmitting Tubes of all Types, Photo Cells, Broadcasting Equipment, Police Radio Equipment, Incandescent Lamps.

(Continued on page 38)

Page 36

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- * Low loss at radio frequencies
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SEPTEMBER, 1934

Tubes (Continued)

(Continued from page 36)
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400 Madison Avenue, N. Y.

RCA RADIOTRON COMPANY, INC.

201 North Front Street, Camden, N. J.

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Receiving Tubes, Transmitting Tubes, Cathode-Ray Tubes, and Amateur

Receiving Tubes, Transmitting Tubes, Latnode-Ray Lubes, and Annatcu Radio Tubes.

RCA Radiotron Company, Inc., was incorporated as a subsidiary of Radio Corporation of America, January 1, 1930, to take over the manufacturing activities of General Electric Company and Westinghouse Electric and Manufacturing Company, and the commercial activities of Radio Corporation of America, relating to vacuum tubes and other apparatus in the field of radio.

In November, 1932, a unification of the sales direction of RCA Radiotron Company, Inc., and E. T. Cunningham, Inc., was effected and the same progressive program has since been applied to both brands of radio tubes.

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EXECUTIVES
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N. A. Woodford, Export Sales Manager, Camden, N. J.

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Newark, New Jersey.

WESTINGHOUSE ELEC. & MFG. CO.

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WESTERN ELECTRIC CO. (See page 28)

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... Plates, Segments, Rings, Tapes, Tubes, Washers



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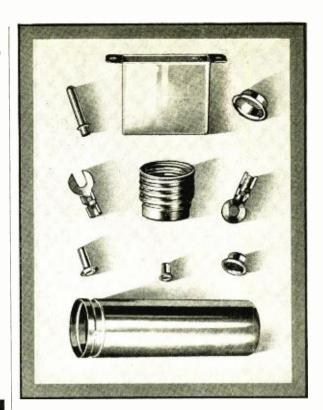
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SYRACUSE ORNAMENTAL COMPANY

Syracuse, N. Y.

Ceramics

AMERICAN LAVA CORP. (See page 38)
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ERIE RESISTOR CORP.

SEPTEMBER, 1934

Page 41

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SHAKEPROOF LOCK WASHER COMPANY

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PRODUCTS
PRODUCTS

PRODUCTS

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Page 42

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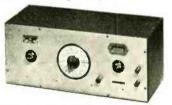
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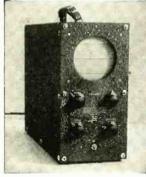
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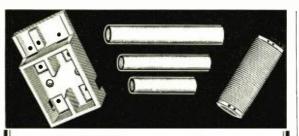
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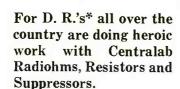




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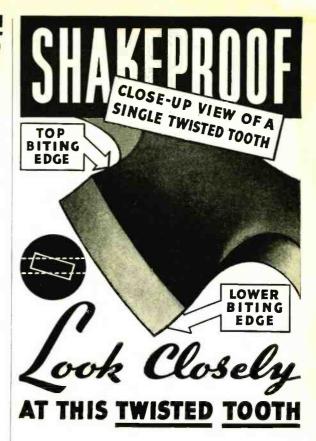


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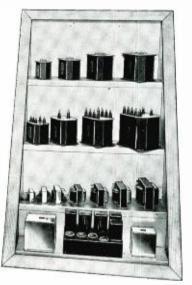


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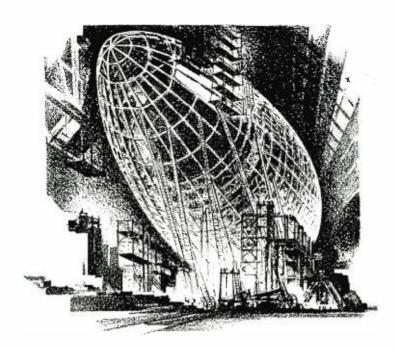
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