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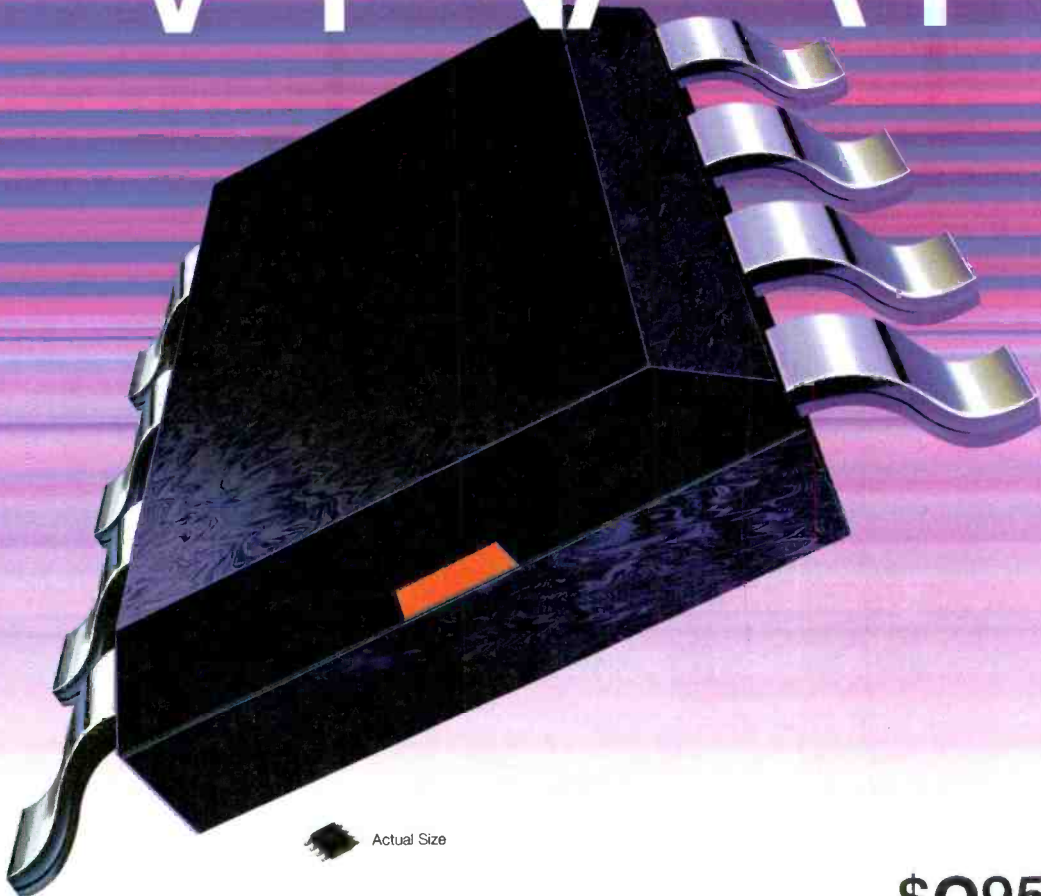
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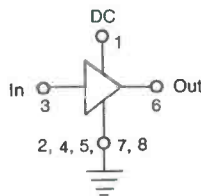
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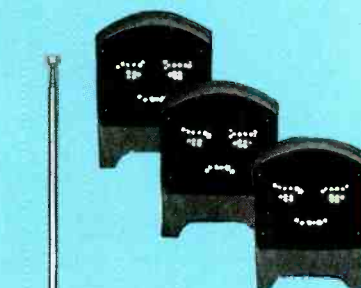
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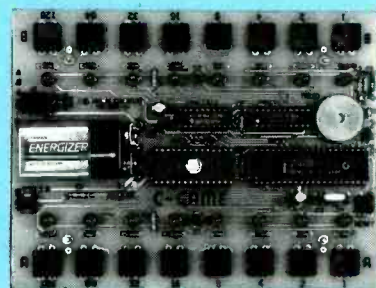
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## ON THE COVER



Although two-way amateur television (ATV) has been around for years, the prohibitive cost of the necessary equipment put it out of reach for most radio amateurs. But, thanks to recent advances in solid-state technology, prices for ATV components have dropped dramatically. This month, we show you how to take advantage of those affordable VCRs, camcorders, color TV receivers, and tiny video cameras by incorporating them into a mobile, battery-operated ATV station weighing less than five pounds. Four related ATV projects are presented: a complete ATV transceiver; a 5-watt, three-channel transmitter only; a  $\frac{3}{4}$ -watt, single channel Mini ATV transmitter; and the  $\frac{3}{4}$ -watt, single-channel "ATV Jr." (without audio capability). Turn to page 31.

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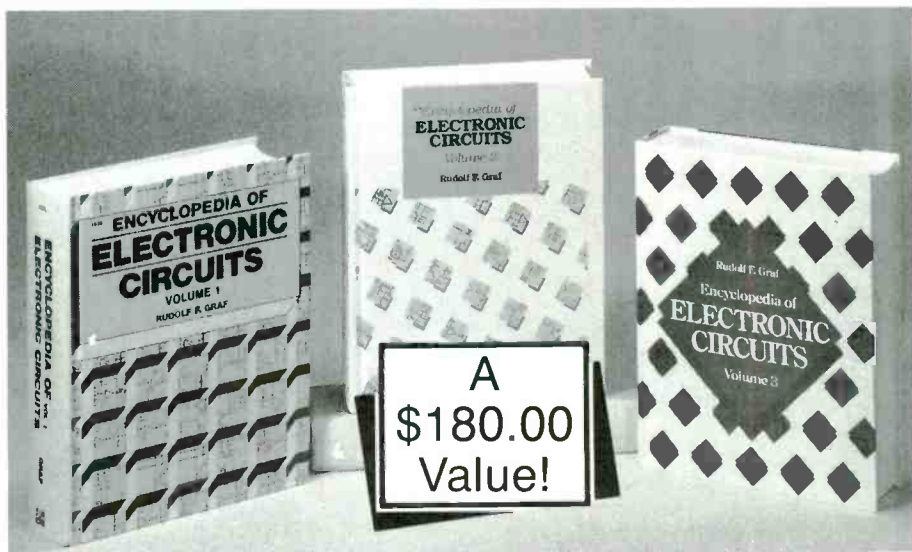
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July 1994, Electronics Now

# WHAT'S NEWS

*A review of the latest happenings in electronics.*

## Micromachined magnetic actuators

Photolithographic and micro-machining techniques permitted researchers at the Georgia Institute of Technology to form the tiny electrical windings and nickel-iron cores in low-voltage magnetic microactuators that do things their electrostatic counterparts can't do.

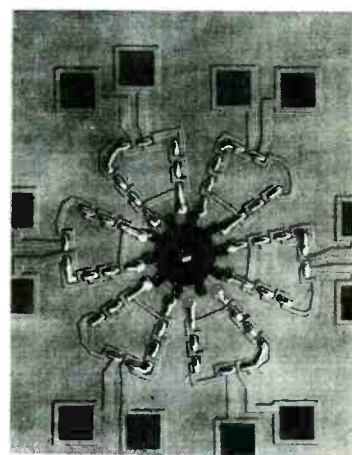
The microactuators are so small that they must be viewed under an electron microscope, as shown in Fig. 1. Georgia Tech scientists say the microactuators, made by techniques similar to those used in fabricating integrated circuits, could, for example, replace transistors for switching high-frequency signals, operate microscopic valves, and be components in microminiature voltage converters.

The low-voltage magnetic microactuators are said to be more compatible with existing micro-electronic circuits than electrostatic actuators. According to the researchers, electrostatic actuators depend on high voltages to generate the electrical charge differentials that draw the electrodes together to create the necessary actuating force.

The lower voltages of the magnetic microactuator make it less likely that it will cause the electrical arcs that could trigger an explosion where volatile gases or dust are present. They say the devices will also work in the human veins and arteries where blood conductivity would inhibit the generation of an electrostatic charge.

Magnetic microactuators also can generate more force than their electrostatic equivalents, although they are usually larger and draw more current. To surmount a major drawback of magnetic microactuators—high resistive loss—the Georgia Tech team is perfecting a device that can be switched by a single current pulse.

The researchers formed inte-



**FIG. 1—MICROMACHINED** microactuator made by integrated circuit fabrication techniques is examined under an electron microscope by Georgia Tech scientists, (left), and a microphotograph of a prototype planar, variable-reluctance magnetic micromotor (right).

grated electrical windings and a magnetic actuator that has its iron core wrapped around its windings. This contrasts with an earlier microactuator made by forming the iron core and electrical windings as separate components.

By integrating the tiny components, it is possible to produce multiples of one device simultaneously on the same substrate as is done with integrated circuits. As in IC fabrication, this technique would lower manufacturing costs. (See Fig. 1.)

Dr. Mark G. Allen, assistant professor in Georgia Tech's School of Electrical and Computer Engineering, said the number of devices that can be made at one time is only limited by the diameter of the substrate silicon wafer.

Several microactuator devices have been built and tested. Among them was a micro-relay that Dr. Allen believes could replace transistors as switches of high-frequency signals. "If you are trying to switch gigahertz-frequency signals for a microwave integrated circuit (MIC), a transistor is ineffective because of its leakage," he ex-

plained. "But if you had a microminiature version of the electromechanical relay with two conductor lines in contact until you move one away, you could switch the signal far more effectively."

## Plastic lithium-ion battery

A new, solid, rechargeable lithium-ion power cell that is as thin and flexible as a credit card, has been developed by Bell Communications Research (Bellcore, Livingston, NJ), the research arm of the regional Bell telephone operating companies.

The plastic cells can be stacked to form batteries for powering small, light, handheld portable telephones, pagers, laptop computers, and video games. Bellcore officials also believe that their new electrochemical technology can be scaled up to function as automotive batteries and even power electric cars.

According to Bellcore officials, the new cell is capable of offering equal or greater energy than the rechargeable cells it is intended to replace, and they are in cases which

*Continued on page 85*



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# VIDEO NEWS

What's new in the fast-changing video industry.

DAVID LACHENBRUCH

● **Home Digital VCR.** Fifty companies worldwide have agreed on specifications for all-digital consumer VCRs designed for standard TV formats—NTSC, PAL, and SECAM—and HDTV. Meeting in Tokyo, the Digital VCR Conference, organized last September, ratified earlier proposals and added some features. The specifications will be submitted to the International Electrotechnical Commission (IEC) for adoption as a world standard in an attempt to avert a standards battle in the future. The system is designed to record both analog and digital broadcasts as digital signals. The new digital video recorders, or DVRs, could be in stores as early as next year—initially at high prices. The first models in the U.S. are likely to be for standard (non-HDTV) broadcasts only.

One immediately noticeable feature of the new format is the cassette, which is considerably smaller than current VHS types. Two sizes are specified—one presumably for camcorders and the other for home decks. The smaller type is about the size of a digital audio tape (DAT) cassette. It measures 2.6×1.9×0.48 inches and is designed to record for 60 minutes in standard mode and 30 minutes in HDTV. The larger cassette is just slightly bigger than an audio-cassette box, at 4.9×3×0.57 inches; it can store 4½ hours of standard video, and half that amount of HDTV. The cassettes contain ¼-inch-wide tape with evaporated metal "or equivalent" coating. An optional feature of the cassette is a built-in IC memory for storage of a table of contents, recording dates, program title, and other information.

**The Specifications.** The system will use digital component recording for video. For all existing non-HDTV standards, the luminance sampling frequency will be 13.5 MHz, the video quantization will be 8 bits, and the video record-

ing frequency will be 25 megabits per second after bit-rate reduction. The audio track will use 48 kHz (18 bits) for two-channel recording, and 32 kHz (12 bits) for four-channel recording. Audio specifications are similar to those for DAT recording, and presumably were chosen to make digital copying difficult—although the specifications as released did not contain any specific mention of anti-copy system.

Tape speed for 60-Hz systems (such as NTSC) will be 18.812 millimeters per second; for 50-Hz systems (PAL, SECAM), 18.831 mm/sec. Discrete cosine transformation (DCS) will be used for video rate reduction. For high-definition systems, the video luminance sampling frequency will be 40.5 MHz; the video recording rate will be 50 megabits per second after bit rate reduction for both  $1125/60$  and  $1250/50$  systems. The tape will run at 27.594 mm/sec in both modes.

Detailed specifications are available for only one high-definition system—Japan's analog MUSE transmissions—because no country has yet adopted a digital HDTV system. However, the conference assigned working groups to develop detailed specifications for new HDTV systems—one for the Grand Alliance system now undergoing tests in the United States, and another for the proposed European digital HDTV system.

**How soon, how much?** Although industrial and broadcast versions of the new digital recorders could appear relatively soon, affordable consumer models could take quite a bit longer. One estimate is that the first versions will cost more than \$3000. JVC, the inventor of VHS recording and a member of the Digital VCR Conference, is trying to reassure the public that VHS will continue to live, particularly in view of the vast library of material already recorded on VHS. For the near term, JVC is pushing its compatible

analog HDTV recording system, W-VHS, which is already available in Japan for recording and playback of standard, widescreen, and HDTV signals. However, it seems unlikely to achieve any great popularity in the U.S. or Europe.

● **Tapeless recording.** Tape might not be the last word digital recording. The first no-moving-parts recorders for consumer use are beginning to appear. Norris Communications, of Poway, California, is planning the first deliveries this summer of a voice recorder that uses solid-state flash memory modules instead of tape. Initially, the "SoundClip" modules will have a playing time of 30 minutes, but Norris plans to extend that to 120 minutes and eventually to offer a music recorder. The initial solid-state digital voice recorder is a pocket device that will list for \$199.

In video recording, there are increasing warnings that the mechanical recording is doomed to disappear—just as the spinning disc and the mechanically rotated tuner disappeared from the television set. John Bermingham, vice president of AT&T's Advanced Communications Technologies Group, recently called magnetic media "an endangered species" and classified optical discs as merely a short-term interim replacement. Addressing a group of recording media executives, he forecast relatively rapid change to solid-state recording. With increasing sophistication of data-compression algorithms, denser and less expensive solid-state devices, and development of broadband communication into the home, mechanical recording is doomed, he said.

Microelectronics will make possible chips with "up to a billion components each" within about 15 years, Bermingham said. At some time in the future, "audio compo-

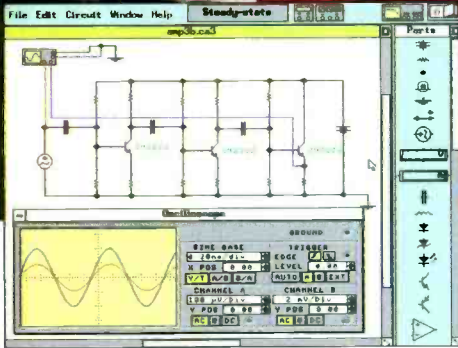
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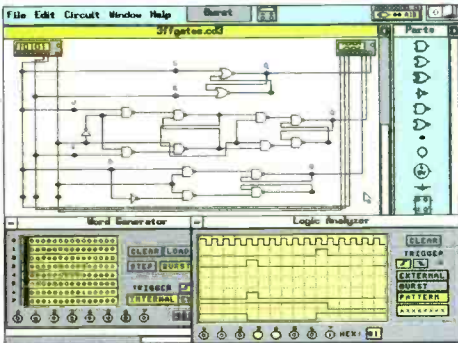
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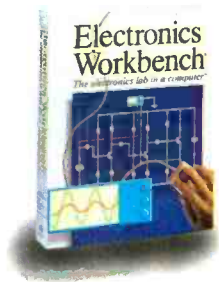
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### AM INTERFERENCE

I've put amplifiers and speakers in several rooms of my house, and they're all driven by line-level signals from a distribution amplifier in my living room. Everything works well except that I can always hear a local AM radio station from the speakers. Do you have any idea what's causing this, and can you suggest any solutions?—**B. Fishen, Albany, NY**

This kind of interference can be a real pain in the neck to eliminate since there are several factors that can cause it. I can make a few suggestions, but I'm willing to bet that you'll have to do a lot of work to make it disappear completely.

The problem you're having is that something in your system is acting as an antenna and introducing the AM signal into the input stage of your power amplifiers. The cable running from your distribution amplifier to the individual power amplifiers is probably a standard audio cable with a single conductor and a shield. If I'm right about that, you should replace it with two-conductor shielded cable and use the shield as a chassis ground.

The best way to find the source of your problem is to disconnect the inputs to the power amplifier and short them by connecting a short piece of wire from signal to ground at the back of the amplifier. If that kills the AM radio signal, you'll know that the cable from the distribution amplifier is acting as an antenna. That means you'll have to replace the wire connecting the two.

I suggest that you try replacing the cable by just placing it on the floor before you go to the trouble of routing it through the walls. If this solves the problem, you've got some rewiring to do. If you're still getting the AM signal, then the chances are it's sneaking in through the power line. Then only way to get rid of it is to use a power-line filter.

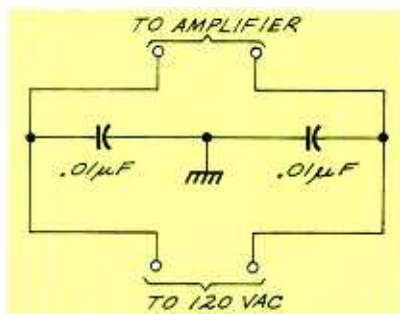


FIG. 1—BASIC AM TRAP. This trap can prevent AM signals in the AC power line from getting into audio equipment.

The schematic in Fig. 1 is a basic AM trap for the power line that I've used with success. Remember to follow proper safety procedures when you're working with 120 volts AC. Put the circuit in a plastic box and be sure to ground the trap properly. AM signals are really pervasive and hard to eliminate. If the filter shown here doesn't clean up the audio, try a commercial line filter as the next step.

### MCA TO ISA ADAPTER

I own an IBM PS/1 model 2121-E42 that has Micro Channel Architecture expansion slots on the motherboard. I would like to use some ISA (Industry Standard Architecture) cards in the computer since they're less expensive, and there's also a much larger variety of them available. I need information about the pin assignments for the Micro Channel Bus, and would like to know how I could make some kind of an adapter.—**R. Keats, Rexdale, Ontario**

In its short life, the PC industry hasn't had much time to generate the kinds of stories that go down in history, but IBM's switch to the Micro Channel Bus is certainly something that will be discussed in MBA classes for years to come.

When the original PC was developed in the early 80's, its bus allowed for expansion. The design of the PC followed the path pre-

viously taken by Apple and, before that, the older S-100 based computers. The motherboard carried the CPU, memory, and the circuitry to support expansion cards.

Although IBM also marketed software under its own name (most of it was licensed from other companies), it realized that its success depended on the creation of a third-party market that would make hardware and software for use with IBM personal computers. IBM published the specifications of the bus and made them available to any company that wanted to go into the business of making plug-in peripherals for the IBM PC. This was the same strategy that had been successful for Apple and others.

When the IBM-AT was developed around the 80286 processor, the bus was expanded to 16-bit width, and the specifications were again made available to anyone who wanted them. Both the 8- and 16-bit buses were far from perfect in terms of speed and signal availability, but they did provide a standard for the industry.

The bus was completely redesigned for 32-bit machines, and IBM started shipping computers with the Micro Channel bus. This was a good architecture that corrected the shortcomings found in the ISA standard, but the specifications and pinouts of the Micro Channel bus remained proprietary. If you wanted to make cards for the newer IBM PCs, you had to pay for the privilege.

This licensing and royalty requirement caused a lot of companies to stay away from the newer IBM PCs. Remember that when IBM switched to Micro Channel, the clone and compatible industry had taken on a life of its own. There was some confusion about a new standard but, after some time, the EISA (Extended Industry Standard Architecture) and VESA (Video Electronics Standards Association) standards

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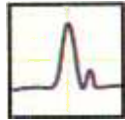
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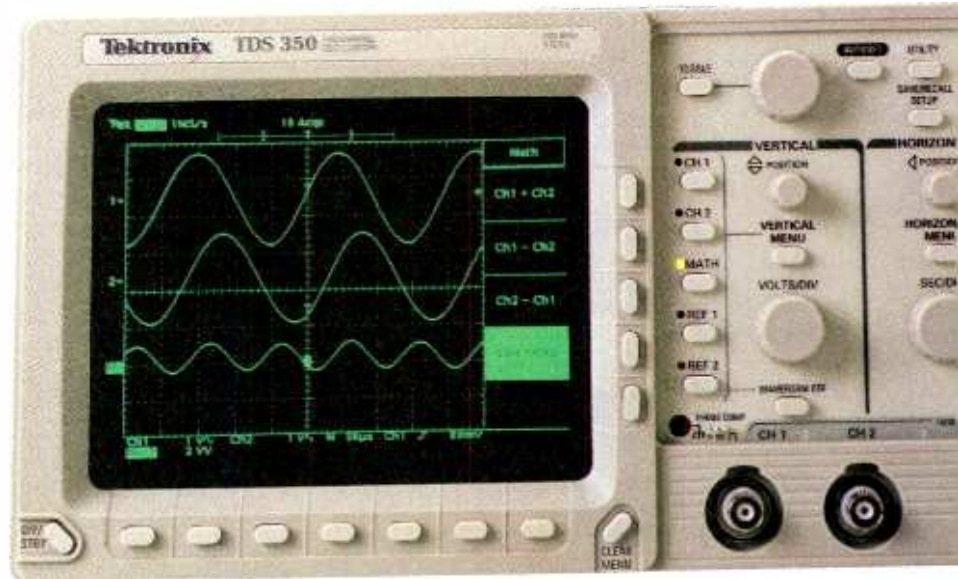
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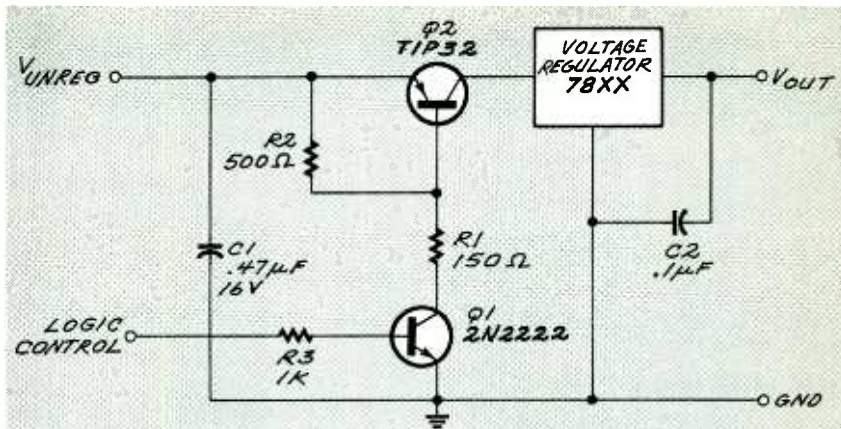
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**FIG. 2—TRANSISTORS CAN BE USED** to control any 78xx series regulator with logic signals. Both transistors are controlled by the logic level present at the base of Q1.

were developed, and the PC industry had a 32-bit standard of its own.

It's clear now that the Micro Channel Bus, no matter how good a bus it is, will remain exclusively IBM, and it's unlikely that it will be a standard for anyone but IBM. Since there are licensing and royalty fees that are associated with it, any third-party product made for the Micro Channel bus will necessarily be more expensive than a similar product made for the ISA bus. And, as long as the specifications for the Micro Channel bus remain proprietary with IBM, you won't be able to find the pin assignments in the reference section of your local library, or adapter cards on the shelves of your local computer store.

### REGULATOR SWITCH

**I'm using several 78xx series three-terminal voltage regulators in a circuit that I built, and I need a way to turn them on and off with logic level signals that are generated by another part of the circuit. I don't want to use a brute-force approach with relays, so please tell me how to do it with solid-state devices.—D. Ketting, St. Louis, MO**

There's no internal circuitry in the 78xx series devices that can turn them on and off. I don't know why you're against using relays but, since you are, you'll see it's also simple to control them with a transistor.

The schematic in Fig. 2 gives you the basic idea of how to control any of these regulators with logic signals. Both transistors are set up as simple switches, and their opera-

tion is controlled by the logic level present at the base of Q1. Whenever a high is presented to the base of Q1, the resulting low at its collector pulls enough current through R1 to turn on Q2. Using two transistors is a good idea because Q1 not only does the inversion needed to properly control Q2, but it also acts as a buffer to isolate the control logic from the power supply.

The component in the circuit whose value is critical is R1. It has to pass enough current to turn on Q2. However, it's easy to calculate the value for R1. You'll need about 50 milliamperes of current to turn on Q2, and the value of R1 can be determined from Ohm's law as follows:  $R1 = V_{UNREG}/50$  milliamperes. You can see from the schematic that all the regulator current must pass through Q2, so make sure you use a part that can handle whatever current your circuit is going to draw. It would be smart to heatsink Q2 as well.

### IS IT SAFE?

**I'm thinking of buying a larger hard drive for my computer, and am intrigued by the possibility of using disk-doubling software to let me increase the amount of storage. I could get 340 megabytes with a 170-megabyte drive, 420 megabytes from a 210-megabyte drive, and so on. Is this kind of software safe to use?—P. Murphy, Victoria, NJ**

Data-compression software has become really popular in the last couple of years, and will probably be used for years to come. Although

*Continued on page 82*

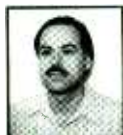
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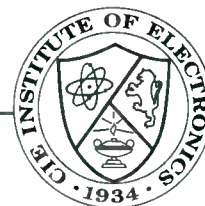


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# LETTERS

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## RADON MONITOR REVISITED

There were several errors in the article "Radon Monitor" published in the January and February 1994 issues of *Electronic Now*. In Fig. 4 (voltage tripler, Jan, p. 61) diode D2 should be reversed. In Fig. 10 (power supply, Feb, p. 70) resistor R3 should be 3.3-kilohms.

Almost any general purpose JFET can be substituted for the National Semiconductor J201 specified for Q1 in Fig. 2 (Jan, p. 58) provided the drain resistor is selected as described on page 62. For example, the 2N3819 (Radio Shack) will work if R1 is 510 ohms. However, the  $o_n$  resistance of some JFETs could be so low that it would cause excessive power drain.

In Fig. 6 (pulse-rate counter, Jan, p. 67), any matched general purpose JFETs can be substituted for the two 2N5566 JFETs, Q4-a and Q4-b, (including the 2N3819) without affecting temperature drift significantly. However, it might be necessary to substitute different values for resistors R10 and R13 to zero the meter properly if the JFETs are not closely matched.

Also in Fig. 6, one section of an LM324 quad op-amp (Radio Shack) used as a comparator can replace the LM392 specified. (Disable its unused sections by grounding their inputs.

It is not necessary to remove *all* of the plastic coating from the inside surface of the cathode sleeve: The sleeve is conductive enough to allow charge combination. Remove only enough to assure a sound high-voltage capacitor connection.

In response to a question about the effective volume of the beverage can chamber, it is considerably smaller than the physical volume of the can. The reason for this is:

Free electrons, from alpha particle ionizations, are repelled by the negatively charged cathode toward any relatively positive surface. The

anode wire collects only about one-quarter of those electrons because it is essentially at ground potential; most are attracted to the ends of the can, which are also at ground potential.

Alpha particle ionizations can occur anywhere within the chamber, but only those electrons released near the middle of the chamber are likely to be attracted to the anode wire. As a result, the can's volumetric efficiency is only about 25% or about one-quarter of its physical volume.

I gave a calibration constant of 1.9 for  $k/(n \times VE)$  in the article, but based on a year of additional field testing, I now believe that constant should be 2.1.

Experimenters should be sure to subtract the background (or outdoor air) count rate from the indoor rate when calculating actual radon concentration:

Radon (pCi/l) = 2.1 (indoor rate - outdoor rate)

I'll be happy to answer any further questions about the Radon Monitor from readers directly by mail. Please include a self-addressed, stamped envelope. PAUL NEHER  
1016 Engler Road  
Las Cruces NM 88005

## IMPROVING TECHNICIAN TRAINING

I read with great interest Larry Steckler's editorial in the March issue of *Electronics Now*. As an electronics engineering (laboratory) technician, there are a few points that I would like to contribute to the discussion.

In my college, certain basics, such as soldering techniques, wiring, and circuit layout (for prototype construction), were not taught. Teachers apparently thought that those skills would be taught in industry. But after graduation, I found that employers weren't annoyed that technicians weren't taught those skills in school.

I would very much like to see colleges take the approach that instructors are like supervisors at work, and the students must learn to function in the real world. A school environment, where there is less pressure, is the ideal place to teach students what the industry expects from them.

Most people in industry don't seem to know who (or what) they're hiring. Someone should clarify the difference for them between a factory technician (the person who specializes in troubleshooting, testing, and repair) and a laboratory technician (who can do basic design work, solder, and keep an engineering notebook).

I was trained as a laboratory technician. During my last year in college, my final exam required that I design and build simple circuit prototypes. That kind of exam encourages technicians to decide if they prefer to work in a laboratory or in a factory. Those who choose the laboratory are taught basic circuit design concepts.

Companies such as Motorola offer semiconductor data manuals to colleges free of charge. All an instructor need do is write to the company on college letterhead paper and specify the number and titles of the manuals he wants.

I would like to encourage more college instructors to do that. If the teacher explained to the students what components are available and how to work with actual component, their learning would be enhanced.

Students of electronics technology face two main stumbling blocks in school—lack of money for building circuit projects and lack of access to information about how to build them. If, at least, basic electronic components (such as standard resistors, logic-gate, and timer ICs) were made more readily available to students, I think that their learning would skyrocket.

It might take a combination of two



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approaches to get my ideas accepted. The first, borrowed from high-school lunch programs, is subsidies for students for buying components. The second would be for manufacturers to offer sample components to students free of charge. That policy would be good public relations, and the companies could write off the expense as advertising.

Along with the components made available at no cost to students, the manufacturers could include copies of any recently superseded data books that they would normally throw away.

By the way, what happens to all those outdated issues of electronics magazines that the newsstands don't sell? I'd suggest that they be shipped off to the electronics schools instead of being thrown away. Rather than take a loss for magazines that are not sold, the publisher could write off the expense as "educational assistance."

I'm sure there are plenty of other good ideas out there for encouraging electronic technician training, but I think these make a good start.

KLAUS SPIES

Niles, IL

### LCD PANEL REPAIR

In response to the Q&A inquiry titled "Dangerous Cleaner" (*Electronics Now*, February 1994), it might be possible to repair a broken LCD panel. If you can see the LCD segments while rotating a pair of polarized sunglasses over the display, it can probably be fixed easily.

Buy a low cost item with a small LCD display such as a game (about \$6) and remove the tin-oxide coated polarizing sheets from the front and back. Place the appropriate sheet in front of the LCD panel in the proper orientation, and you're set.

I repaired an LCD watch this way. Its polarization coating was partially removed because of a cracked crystal and exposure to steam.

RON DOZIER

Wilmington, DE

### IMPEDANCE MATCHING

I would like to respond to M. Bith's question that appeared in Q&A in April. Speaking from experience, I believe that Q&A's sugges-

tion—matching a low-impedance microphone to a high-impedance input—would give very poor results.

It is apparent that Mr. Bith is already experiencing hum as well as low-level output. The amplifier would raise the microphone's output level, but I believe the hum would be increased proportionally.

High-impedance microphones have two disadvantages. First, microphone lines tend to pick up 60-Hz hum, which can be induced in the microphone cable line and/or its extension. Second, long microphone lines will drastically reduce high-frequency response because of the effective capacitance between the center conductor and shield.

Both of those drawbacks are eliminated with low-impedance microphones having a balanced line input. Generally, that means the use of a microphone transformer. That transformer then accepts any induced voltage on one line and balances it out with an equal but opposite voltage on the other line.

Moreover, interconductor capacitance, while not reduced, has virtually no effect on the low impedance involved. Another approach takes advantage of the impedance switch found on most low-impedance microphones by allowing them to be switched to high. If that is done, use a single-conductor, high-impedance cable because has lower capacitance. I hope this suggestion helps.

DWIGHT EGGLESTON

Hendersonville, NC

### COMPLEMENTARY PAIR PREAMP

Thank you for presenting Ray Marston's article, "Audio Amplifiers" (*Electronics Now*, March 1994). I have long been interested in audio circuits, especially those containing discrete transistors. Over the years, I've enjoyed reading articles on this subject in *Electronics Now* and before that in *Radio-Electronics*.

However, I can't recall seeing my favorite audio preamplifier circuit before—the complementary pair shown in Fig. 1. Here are some of its benefits: high input impedance (approximately R1) and a low output impedance (significantly lower than

*Continued on page 82*

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# EQUIPMENT REPORTS

## BDM40 Benchtop Digital Multimeter

When performing benchtop troubleshooting or repair, it's best to use test equipment intended for benchtop use.

CIRCLE 14 ON FREE INFORMATION CARD



Most readers of this magazine are familiar with bench testing; it's an essential part of working with electronics. For infrequent testing, a handheld multimeter might be sufficient. However, anyone who is doing bench testing day-in and day-out needs test equipment better suited for benchtop use.

A handheld multimeter is the perfect tool for general-purpose testing both because of its versatility and portability. It can be a technician's "Swiss Army knife"—a real lifesaver for countless unexpected repairs. But you would never see an auto mechanic repairing a car with a Swiss Army knife—there are better tools for the job. Similarly, although a TV service center might have a few handheld multimeters in its equipment arsenal, you are sure to find benchtop test instruments being used for benchtop testing.

Benchtop test equipment is usually intended for making only a few specific kinds of tests. However, it is generally capable of making those measurements with greater accuracy and precision than handheld units. Traditional digital multimeter (DMM) functions are the measurement of AC and DC voltage, AC and DC current, and resistance. While some handheld units might boast ten times that number of features, the additional features usually lack the precision and operating range for professional work.

A person who uses a DMM every day wants a unit that's easy to position on a test bench and that stays

put. The unit should also have a display that's easy to read from as wide an angle as possible. The liquid-crystal display on a portable DMM conserves battery power, but it can be hard to see from wide angles. Because battery power conservation is usually not a concern at the test bench, power-hungry LED displays, which are much easier to see, are practical.

### The Wavetek BDM40

When buying a benchtop DMM it's a good idea to find one that strikes a happy median between price and performance—an example is the model *BDM40* from Wavetek Corporation (9045 Balboa Avenue, San Diego, CA 92123, 619-279-2955). This 4½-digit, true-RMS benchtop DMM has a list price of \$429.

The BDM40 can measure AC and DC voltage in five ranges to 1200 volts, AC and DC current in six ranges to 20 amperes, and resistance in six ranges to 20 megohms. It can also test diodes. Each measurement range has automatic polarity detection, overrange indication, and overload protection. All of the measurement functions are enabled by interlocking pushbuttons, and the LED display characters are a ½-inch high. A pair of test leads, two spare fuses, and an instruction manual are included in the price.

The BDM40 is housed in a rugged gray plastic case that measures about 10 inches wide by 12 inches long. The rubber-cushioned carrying handle also doubles as a bail that

locks into various positions making the DMM very easy to position. The power cord plugs into the back of the meter and, when not in use, can be wrapped around two plastic lugs molded onto the case. The back of the instrument, or the bottom depending on how you look at it, has two wide rubber feet that allow the DMM to stand in a vertical position.

### Measurements

Four input jacks are provided on the front panel: volt/ohm, common, and 2- and 20-ampere current. The test probes must be plugged into the different jacks, depending on whether current or voltage and resistance is to be measured. A red push-on, push-off switch turns the power on and off.

The DMM can measure AC voltage to 1000 volts in 200-millivolt, 2-volt, 20-volt, 200-volt, and 1000-volt ranges. The true-RMS function is pushbutton-enabled for AC and AC + DC coupled measurements. DC voltage measurements can be made in the same ranges up to 1200 volts.

Alternating and direct current (AC and DC) can be measured in 200-microampere, 2-milliamperere, 20 milliamperere, 200 milliamperere, 2-ampere, and 20-ampere ranges. Two current-input jacks are provided on the front panel of the unit; one is for measurements up to 2 amperes, and the other must be used for current measurements between 2 and 20 amperes.

Resistance can be measured in six ranges: 200 ohms, 2 kilohms, 20 kilohms, 200 kilohms, 2000 kilohms, and 20 megohms. In the first two ranges, the value of lead resistance will show up on the display.

The 4½-digit (20,000-count) display can register measurements from 0000 to 19999. The polarity of the input signal is indicated by the appearance of a sign on the left side of the display. The position of the

*Continued on page 77*

# Countersurveillance

**Never before has so much professional information on the art of detecting and eliminating electronic snooping devices—and how to defend against experienced information thieves—been placed in one VHS video. If you are a Fortune 500 CEO, an executive in any hi-tech industry, or a novice seeking entry into an honorable, rewarding field of work in countersurveillance, you must view this video presentation again and again.**



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**1-516-293-3751**

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*Wake up!* You may be the victim of stolen words—precious ideas that would have made you very wealthy! Yes, professionals, even rank amateurs, may be listening to your most private conversations.

*Wake up!* If you are not the victim, then you are surrounded by countless victims who need your help if you know how to discover telephone taps, locate bugs, or “sweep” a room clean.

There is a thriving professional service steeped in high-tech techniques that you can become a part of! But first, you must know and understand Countersurveillance Technology. Your very first insight into this highly rewarding field is made possible by a video VHS presentation that you cannot view on broadcast television, satellite, or cable. It presents an informative program prepared by professionals in the field who know their industry, its techniques, kinks and loopholes. Men who can tell you more in 45 minutes in a straightforward, exclusive talk than was ever attempted before.

## Foiling Information Thieves

Discover the targets professional snoopers seek out! The prey are stock brokers, arbitrage firms, manufacturers, high-tech companies, any competitive industry, or even small businesses in the same community. The valuable information they filch may be marketing strategies, customer lists, product formulas, manufacturing techniques, even advertising plans. Information thieves eavesdrop on court decisions, bidding information, financial data. The list is unlimited in the mind of man—especially if he is a thief!

You know that the Russians secretly installed countless microphones in the concrete work of the American Embassy building in Moscow. They converted

what was to be an embassy and private residence into the most sophisticated recording studio the world had ever known. The building had to be torn down in order to remove all the bugs.

## Stolen Information

The open taps from where the information pours out may be from FAX's, computer communications, telephone calls, and everyday business meetings and lunchtime encounters. Businessmen need counselling on how to eliminate this information drain. Basic telephone use coupled with the user's understanding that someone may be listening or recording vital data and information greatly reduces the opportunity for others to purloin meaningful information.

The professional discussions seen on the TV screen in your home reveals how to detect and disable wiretaps, midget radio-frequency transmitters, and other bugs, plus when to use disinformation to confuse the unwanted listener, and the technique of voice scrambling telephone communications. In fact, do you know how to look for a bug, where to look for a bug, and what to do when you find it?

Bugs of a very small size are easy to build and they can be placed quickly in a matter of seconds, in any object or room. Today you may have used a telephone handset that was bugged. It probably contained three bugs. One was a phony bug to fool you into believing you found a bug and secured the telephone. The second bug placates the investigator when he finds the real thing! And the third bug is found only by the professional, who continued to search just in case there were more bugs.

The professional is not without his tools. Special equipment has been designed so that the professional can sweep a room so that he can detect voice-activated (VOX) and remote-activated bugs. Some of this equipment can be operated by novices, others require a trained countersurveillance professional.

The professionals viewed on your television screen reveal information on the latest technological advances like laser-beam snoopers that are installed hundreds of feet away from the room they snoop on. The professionals disclose that computers yield information too easily.

This advertisement was not written by a countersurveillance professional, but by a beginner whose only experience came from viewing the video tape in the privacy of his home. After you review the video carefully and understand its contents, you have taken the first important step in either acquiring professional help with your surveillance problems, or you may very well consider a career as a countersurveillance professional.

## The Dollars You Save

To obtain the information contained in the video VHS cassette, you would attend a professional seminar costing \$350-750 and possibly pay hundreds of dollars more if you had to travel to a distant city to attend. Now, for only \$49.95 (plus \$4.00 P&H) you can view *Countersurveillance Techniques* at home and take refresher views often. To obtain your copy, complete the coupon or call.

**EN**

**CLAGGK INC.**  
**P.O. Box 4099 • Farmingdale, NY 11735**

Please rush my copy of the Countersurveillance Techniques Video VHS Cassette for a total cost of \$53.95 each (which includes \$4.00 postage and handling).

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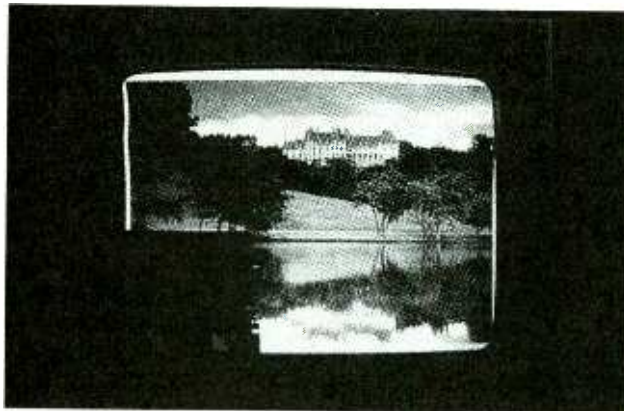
# NEW PRODUCTS

Use the Free Information Card for more details on these products.

## VGA-TO-NTSC CONVERTER.

The *VideoOut* plug-in card and software from *International Computers* allows the images on a computer screen to be displayed on a television monitor or be saved to videotape for a VCR. Capable of displaying text and graphics and both black and white and color screens, it can be used to create demonstration videotapes and instructional videos. *VideoOut* works on any IBM PC/XT/AT or compatible computer with a VGA display adapter. If the VGA card can send interlaced signals, *VideoOut* can display them on a television monitor in 480-line resolution. It will also work with non-interlacing VGA cards.

*VideoOut* includes a board that functions as a pass-through for the VGA video signals. A program remains resident until the hot key is pressed for start-up. The registers on the VGA card are reprogram-



CIRCLE 20 ON FREE INFORMATION CARD

med to convert the video signal to NTSC timing.

*VideoOut* supports both text and graphics modes. It contains a lookup table for determining the proper addressing and mode number for the VGA installed. It also identifies the specific board's manufacturer automatically.

The card is installed in the computer, and the cable from the VGA card is unplugged and plugged into the top connector of *VideoOut* card. The VGA cable provided is then

plugged between the VGA card and the bottom connector of *VideoOut*. An additional cable included connects the *VideoOut* card to the television, monitor, or VCR.

The *VideoOut* 4.2 x 4-inch plug-in board, two cables and connectors, user's manual, and software diskettes are priced at \$99.

**International Computers**  
12021 West Bluemound Road  
Wauwatosa, WI 53226  
Phone: 414-764-9000

slave outlet to control more than one appliance.

In the automatic position the *MasterSwitch* functions normally, but a manual position overrides the circuitry and turns on the slave outlet whenever desired. The maximum current rating for each outlet is 4 amperes (480 watts).

Plans, instructions and circuit board patterns for building your own *MasterSwitch* is priced at \$7.50. That Documentation with a printed circuit board is priced at \$14, and a kit with all documentation and parts is priced at \$39 plus \$4 S&H. A fully assembled and tested unit is priced at \$49 plus \$4 S&H. California residents add 8.25% sales tax.

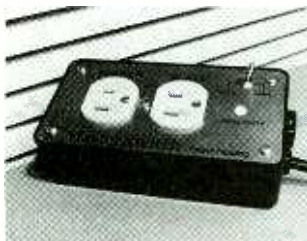
**Progressive Concepts**  
1313 North Grand Avenue  
Suite 291  
Walnut, CA 91789  
Phone: 909-626-4969

**12-DIGIT UNIVERSAL COUNTER.** *Hewlett-Packard* has increased the resolution of its universal-counter family by 12-digits per second with its introduction of the *HP 53132A* 225-MHz universal counter. It is able to make high-resolution measurements in a fraction of the time required by conventional counters. This feature can speed up product testing and troubleshooting in computer-controlled systems whose data transfer rate exceeds 200 fully formatted measurements per second.

In addition to typical universal-counter measure-

**AC SWITCHING DEVICE.** The *MasterSwitch* with master and slave AC outlets permits you to turn on your television with your remote control while it turns on your stereo or amplifier automatically. Now you can hear television sound through your stereo system with one convenient remote control setting.

Any electrical appliance plugged into the slave outlet will automatically switch on or off depending on the



CIRCLE 21 ON FREE INFORMATION CARD

on/off status of the device which is plugged into the master outlet. The current level threshold at which the slave outlet switches is ad-

justable with a sensitivity control. That control can cause the unit to ignore low current being drawn from the master outlet. The *MasterSwitch* also includes an auto/manual switch.

The *MasterSwitch* works in most situations where you want the on and off function of one or more appliances controlled by a master appliance. A three-way tap or a power strip can be plugged into the



CIRCLE 22 ON FREE INFORMATION CARD

ments, such as frequency, period, and time interval, the HP 53132A can measure pulse parameters, duty cycle, and frequency ratios. Built-in statistical and mathematical functions allow the user to display scaled measurement data. An optional third channel is available that can measure frequency up to 3 gigahertz.

Automatic limit testing permits the setting of upper and lower boundaries on any measurement. An analog display mode speeds testing by allowing users to see if a measurement falls within pass/fail limits.

The counter logs and flags out-of-limit conditions, and it can generate an output signal to trigger external devices when a limit is exceeded. A single keystroke recalls up to 20 different panel settings that were stored after the instrument was set up for a specific application.

A standard HP-IB port provides full SCPI-compatible programmability, and a standard RS-232 (talk only) interface provides printer support or data transfer to a computer through a terminal-emulation program.

The HP 53132A universal counter, complete with operating, service, and programming manuals and a power cord, is priced at \$2400.

**Hewlett Packard Company**  
3000 Hanover Street  
Palo Alto, CA 94304

### HIGH-BRIGHTNESS LED'S.

The red LED lamp in Rohm Corporation's SLA-570 Series provides luminous intensity of up to 2400 millicandelas (mcd) at 20 milliamperes, while a green LED lamp emits up to 750 mcd. Both LED lamps have 24° viewing angles. They are said to be suitable for illuminating airport terminal and stadium signs and theater marquees. Their use will avoid the cost and time required to replace incandescent lamps in those lighting applications.



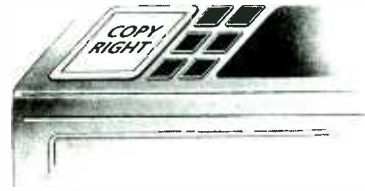
CIRCLE 23 ON FREE INFORMATION CARD

The red gallium phosphide LEDs have typical forward voltages of 1.75 volts, and they dissipate 100 milliwatts; equivalent values for green gallium aluminum arsenide LEDs are 2.3 volts and 75 milliwatts. Both are rated for 100,000-hour MTBF.

Red SLA-570 LEDs are priced at less than \$.07 each, and green LEDs are priced at less than \$.125 each when purchased in quantities of 10,000.

**Rohm Corporation**  
3034 Owen Drive  
Antioch, TN 37013  
Phone: 615-641-2020  
Fax: 615-641-2022

**UNDERWATER METAL DETECTOR.** The *Impulse* metal detector from Fisher Research Laboratory is intended for shoreline and underwater treasure hunting. Based on pulse induction (PI) circuitry, it has the ability to detect metal (in-



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#### RESTORE IT CORRECTLY

Doing it right with vintage audio gear.

#### EPROM PROGRAMMER

Put the IBM PC input/output breadboard to work.

#### CIRCUIT NOTEBOOK

All about low-voltage converter circuits.

☆ Plus additional interesting articles, columns and departments on topics covering theory and equipment servicing.

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**JULY 5, 1994**

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**CIRCLE 24 ON FREE INFORMATION CARD**

cluding gold and silver) in salt water and black sand. Both of those materials are seen as targets by most metal detectors.

The detector's transmission frequency is 5,333 pulses per second. A voltage-controlled oscillator provides audio target response through a piezoelectric headset. An LCD bargraph displays signal strength and battery condition. The detector can have an 8- or 10-inch spider coil with a 7-foot cable. Alkaline AA power cells provide up to 100 hours of service.

The *Impulse* can withstand depths up to 250 feet. It has two control knobs: a threshold tone control sets the tuner for maximum sensitivity, and a volume control, which is also an on/off switch, adjusts headset volume.

The *Impulse* underwater metal detector is \$900.

**Fisher Research Laboratory**  
Department EN

200 West Wilmott Road  
Los Banos, CA 93635  
Phone: 1-800-M-SCOPE-1

**INSULATED PROBES.** Oscilloscope probes from *ITT Pomona* are intended as replacements for factory-supplied probes for Fluke ScopeMeter 90 Series, Leader Model 300, and Hitachi 5025 handheld oscilloscopes.

The *6033 Scope Probe Kit* includes a paired set of *Model 6006* 10X probes (red and gray) with over-voltage protection to 360

volts rms. It is rated at 200 MHz, and includes fully insulated leads and an insulated BNC connector for direct interface.

Pomona has also introduced a new family of switchable (1X/10X) insulated probes that are sold separately. The *Model 6035* has a non-slip handle and a slide switch for the probe's attenuation range. A non-switchable *Model 6006* is also sold as a separate item.



**CIRCLE 25 ON FREE INFORMATION CARD**

The *6035* is priced at \$95 each, the *Model 6006* is priced at \$75, and *Model 6033* kit is priced at \$125.

**ITT Pomona Electronics**

1500 East Ninth Street  
Pomona, CA 91766-3835  
Phone: 909-469-2900  
Fax: 909-629-3317

**PC-BASED DATA-ACQUISITION AND PROCESS-CONTROL TOOL.** *TechnoView's*

*A/D Pods* combine the functions of a 7½ to 8½-digit voltmeter, a digital output card, and a multichannel personal computer-



**CIRCLE 26 ON FREE INFORMATION CARD**

based data-acquisition system. They were designed for use with bridge transducers that measure force, load, pressure, acceleration, flow, stress, and gain. The pods allow a sensor to be digitized and controlled over a serial RS-232 interface.

The A/D pods do not depend on amplifiers to permit the reading of low-level signals. An *A/D pod* is selected with a full-scale input voltage range that closely matches the output voltage range of the transducer. Each pod contains an A/D converter IC and voltage reference tuned to the required full-scale input range.

*A/D Pods* have full-scale inputs between 100 millivolts and 2.0 volts. The A/D IC offers  $\pm 18$  bits with 25 % overrange. The pod's *TVIHOST* data-acquisition software will run on computers with PC-DOS and Unix operating systems.

The *A/D Pod Senior* starter kit which includes eight *A/D Pods*, one PC-interface module, software, "C" driver source code, all necessary cables, and power supply is priced at \$6,495. The *A/D Pod Junior* starter kit which includes four *A/D Pods* is priced at \$4195.

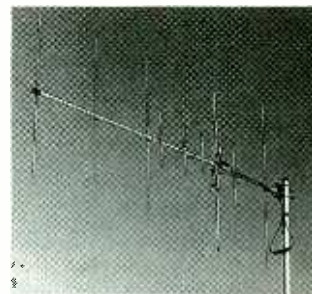
**TechnoView, Inc.**

98 Baycrest Court  
Newport Beach, CA 92660-2922  
Phone: 714-854-5559

**DUAL-BAND YAGI.**

*Cushcraft's A270-10S* dual-band Yagi array for two meters and 70 centimeters provides the gain and directional characteristics of a Yagi array with the convenience of a dipole antenna.

The boom for the *A270-10S* is six feet, two inches long, and weighs



**CIRCLE 27 ON FREE INFORMATION CARD**

less than two pounds. Because its wind load is only 0.725 square feet, light-duty rotors can be used. The antenna covers both the 144- to 148-MHz and 430- to 450-MHz bands.

The *A270-10S* yagi array is priced \$99.

**Cushcraft Corporation**

48 Perimeter Road  
Manchester, NH 03103  
Phone: 603-627-7877  
Fax: 603-627-1764

**DC POWER SUPPLY.** *B+K's*

*Model 1688* 3- to 14-volt DC power supply is intended to replace a 12-volt automotive battery for continuous duty operation. It can power mobile electronic equipment such as mobile cellular phones, car stereos, and amateur radios.

The *Model 1688* avoids concern for acid leaks from 12-volt automotive batteries, does not need recharging, and can tolerate short-circuited loads. It produces 35 amperes (nominal) and a maximum of 25 amperes at 13.8 volts DC, continuously, without overheating.

Output voltage of the



**CIRCLE 28 ON FREE INFORMATION CARD**



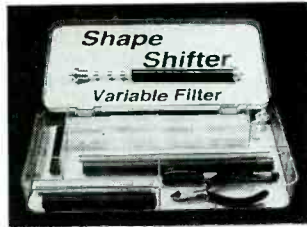
*Model 1688* can be varied from 3 to 14 volts DC. Current and voltage can be monitored simultaneously on separate analog meters. The outputs are fully isolated, so either output terminal can be floated or grounded.

The *Model 1688* DC power supply is \$299.

**B + K Precision Corp.**  
6470 West Cortland Street  
Chicago, IL 60635  
Phone: 312-889-1448  
Fax: 312-794-9470

outer conductor with removable SMA connectors.

The basic core has a characteristic impedance of 100 ohms. Transmission-line segments placed over the core provide characteristic impedances of either 50 or 20 ohms. The segments can form a stepped-impedance tubular filter. There can be from three to 11 segments. Each segment of transmission line is attached to the core with a special crimping tool.



CIRCLE 29 ON FREE INFORMATION CARD

Connections are electrically and mechanically

secure, yet can be reconfigured in minutes. Cut-off frequencies range from 500 MHz to 5.0 GHz with up to 11 sections. Typical insertion loss is 0.2 dB at 1 GHz and 1 dB at 5 GHz. Its maximum power requirement is 10 watts. All components except the core are reusable and they are designed to last for at least 100 filter responses. More than 50 cores are included.

The *Shape Shifter SL55* kit, including instructions and all necessary tools is priced at \$595.

**Gavewave**  
Division of Parkview R&D, Inc.  
565 Science Drive  
Madison, WI 53711  
Phone: 800-797-9283  
Fax: 608-238-5120

**SPECIALTY CABLE TESTER.**  
*L-com's* cable tester can test for continuity and iden-



CIRCLE 30 ON FREE INFORMATION CARD

tify any video or data cable equipped with nine-pin, D-type subminiature cable connectors.

Twenty LEDs verify cable continuity, open and short circuits between conductors, and shield ground. The tester has two modes: continuous scan and manual step scan.

The *D-Sub 9 Cable Tester* is priced at \$179.50.  
**L-com, Inc.**  
1755 Osgood Street  
North Andover, MA 01845  
Phone: 800-343-1455  
Fax: 508-689-9484

**LOW-PASS FILTER.** The *Gatewave, Shape Shifter SL55* adjustable low-pass filter is intended for laboratory use. It is sold as a kit with an assortment of transmission-line segments that are combined by sliding them onto a metal core which also serves as the center conductor. A tubular jacket forms the

## VIDEO NEWS

continued from page 8

nents and video players will be the same device," he added. They will be in "wallet-sized packages containing a digital recorder and player with 100 gigabytes of built-in memory as well as removable cards on which programs can be downloaded."

As envisioned by Birmingham, the recorder/player of the future "will be battery-powered, and have a small color viewing screen; it will go from home to car to pocket." It will be able to digitally copy any software from any electronic source, with "an embedded computer program" keeping track of copied material and routing royalties to the "appropriate copyright holders."

All conventional recording media, "even those newest technologies, still involve mechanical devices," Birmingham said, noting they are "conceptually identical to the tinfoil recorder Thomas Edison discovered in 1877."

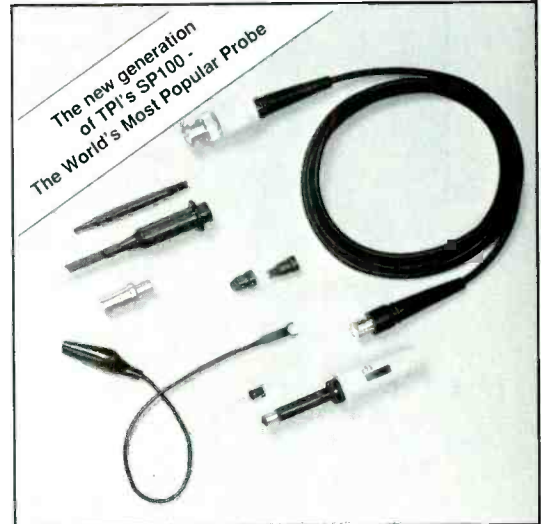
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CIRCLE 123 ON FREE INFORMATION CARD

www.americanradiohistory.com

# NEW LITERATURE

Use The Free Information Card for fast response.

**A Field Guide to Windows Icons: An Introduction to the Commonest Icons in North America;** by Patricia C. Hedtke and John V. Hedtke. Osborne McGraw-Hill, 2600 Tenth Street, Berkeley, CA 94710; Phone: 510-549-6600; Fax: 510-549-6603; \$7.95.

Learn the Windows operating system while laughing at the humor in this book that has a lighter look at Windows. By sending up the field-guide format familiar to bird-watchers, Windows learners at all levels of computer experience will be able to identify *iconus vulgaris* (common icons), *controllum panellum* (control panel) and *scribi microsoftii* (Microsoft Write).



CIRCLE 337 ON FREE INFORMATION CARD

Each entry includes the icon's common name followed by its Latin name, distinguishing marks, voice, a full description, and a single-sentence explanation of what the icon really does.

The book presents each common icon in its "natural habitat." The icon's attributes are examined, and its individual peculiarities are noted with a naturalist's eye for detail.

**JEDEC Style Integrated Circuit Package Trays;** 3M Electronic Products Division, 6801 River Place Blvd., Austin, TX 78726-9000; free.

This brochure describes 3M's full line of trays for transporting integrated circuits in quantity. The brochure discusses trays best



CIRCLE 338 ON FREE INFORMATION CARD

suited for high-, medium-, and low-temperature environments. All of the trays are designed to be compatible with JEDEC tray outline stacking dimensions, and they are made with dimensional tolerances that match those of the IC packages. 3M will design and manufacture non-standard trays to customer specifications.

This brochure includes product specifications, pictures of the trays, ordering information, and a chart presenting the properties of the plastic materials used in making the trays for customer selection.

**1994 Electronic Parts & Accessories Catalog;** Parts Express, 340 East First Street, Dayton, OH 45401-1257; Phone: 800-338-0531.

This 188-page catalog describes the Parts Express line of electronic components. The line



CIRCLE 339 ON FREE INFORMATION CARD

focuses on consumer-electronics products and hobbyist needs.

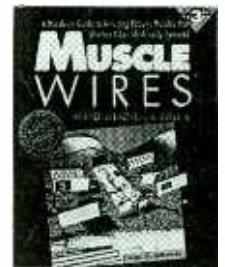
Among the products described in this 1994 catalog are speakers and audio accessories for home and car, audio products for home installation, professional audio equipment, and repair parts and accessories for CATV and VCRs. Other products available from Parts Express include telephone products, semiconductors, tools, chemicals, wire, connectors, computer accessories, and educational books and videos.

**Muscle Wires Project Book, Third Edition;** by Roger G. Gilbertson. Mondo-Tronics, 524 San Anselmo Avenue, No. 107, San Anselmo, CA 94960; Phone: 415-455-9330; Fax: 415-455-9333; \$17.95; book with Muscle Wires sample kit: \$34.95; book with Muscle Wires deluxe kit: \$59.95.

This book discusses Muscle Wires™, nickel-titanium filaments that shorten when they are electrically powered. When heated, they act like human muscles. This characteristic gives them the ability to lift weights that are

thousands of times their own weight. Until recently, these shape memory wires were little known outside of the scientific laboratory.

The author of this project book is the president of Mondo-Tronics, Inc., the company that manufactures Muscle Wires™. Mr. Gilbertson points out that they are now finding applications in teleoperated manipulators, mini- and micro-robotic devices, and heat-actuated tools. They can also actuate valves, relays, switches, circuit breakers, and temperature controlled devices.



CIRCLE 340 ON FREE INFORMATION CARD

The wires have been included in prosthetic limbs and heat-controlled medical instruments. Nevertheless, they are inexpensive enough to be suitable for animating dolls, toys, and puppets. When included in educational science kits and made available for home experimentation, they offer unlimited possibilities for amateur experimentation.

The author gives enough information in this book to permit the reader to design and build his own electromechanical and thermal-controlled devices with Muscle Wire™.

**DC/DC Converters Application Note. Conversion Devices, Inc., 15 Jonathan Drive, Brockton, MA 02401; Phone: 508-559-0880; Fax: 508-559-9288; free.**

This comprehensive, eight-page technical note from Conversion Devices discusses applications for DC/DC converters in many different circuit configurations. It also gives designers advice on how to avoid many common DC/DC application problems.



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The subjects in this application note include wiring and making connections, grounding, input circuits, output circuits, and the linking of multiple converters. Specific converter problems such as input transients and line drops are discussed. Circuit diagrams illustrate important technical points.

**Antennas and Techniques for Low-Band DXing: Your Guide to Ham Radio DXcitement on 160, 80, and 40 meters; by John Devoldere, ON4UN. The American Radio Relay League, 225 Main Street, Newington, CT 06111; Phone: 203-666-1541; Fax: 203-665-7531; \$20.**

This book offers the tips and techniques intended to improve the performance of amateur radio operators and help them win DXing contests. Entry-level amateurs as well as seasoned amateur operators alike can profit from the information given in this book to



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improve their on-the-air efficiency, whether they participate in DXing contests or not.

The topics discussed in DeVoldere's book include specific antenna systems that can improve station performance. Details about dipoles and vertical arrays are discussed. This guide has been updated regularly since it was first published in 1987. This latest edition has been expanded, and large sections have been rewritten to make them more valuable to a wider reader base.

The author has made use of the latest and most powerful computer analysis and modeling tools in the preparation of his section on antennas. A revised equipment review section includes recent product introductions. Another important addition is a directory of outstanding low-band DX'ers. The listing includes their scores, and describes the equipment and antennas they have.

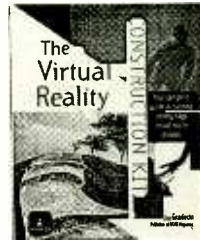
**The Virtual Reality Construction Kit; by Joe Gradecki. John Wiley & Sons, Inc., 605 Third Avenue, New York, NY 10158-0012; \$27.95.**

This book allows you to immerse yourself in the subject of virtual reality regardless of your level of training and experience with computers, programming or electronic circuits.

The author has included

detailed instructions for 18 inexpensive virtual-reality do-it-yourself projects. These range from adapting Nintendo PowerGloves and VictorMaxx 3D goggles, to building your own goggles, motion trackers, and 3D sound systems.

Gradecki's book includes a diskette containing all the software required to test, calibrate,



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and run the virtual reality projects discussed in the book. It includes virtual worlds, which are accessible with your mouse and computer monitor. Projects in the book include "duck and fire" a robot combat game that can be played over modems.

You can also play virtual reality racquetball in a realistic virtual-reality court and hook up a bicycle to your computer and pedal through a virtual park. Other adventures includes lifting marble slabs and columns to build an ancient Greek virtual temple. Those readers with C programming experience can make use of the information in the book to generate their own programs.

**1994 AUDIO DATA BOOK. Crystal Semiconductor Corporation, Literature Department, 4210 South Industrial Drive, Austin, TX 78744; Phone: 512-442-7555, ext. 254; free.**

This 1072-page data book from Crystal Semiconductors covers its com-



**CIRCLE 344 ON FREE INFORMATION CARD**

plete range of audio integrated circuits. It contains detailed product descriptions and discussions of circuit functions.

Among the topics covered in this data book in six product categories are: digital-to-analog converters, analog-to-digital converters, combined ADCs and DACs, digital signal processors and synthesizers, digital audio transmitters and receivers, and volume controls.

Data sheets are provided for 23 products, including 11 new to this edition, application notes, and reprinted articles from the Audio Engineering Society publications.

**Mastering Electronics Math, Second Edition; by R. Jesse Phagan. Tab Books Inc., Blue Ridge Summit, PA 17294-0850; Phone: 800-233-1128; \$17.95.**

This book was written as a guide to the understanding of the mathematics most widely used in electronics. It covers the practical calculations needed to design and troubleshoot circuits as well as test basic components.

Phagan has avoided the heavy theoretical approach taken in many mathematics books. His explanations and sample problems that illustrate each concept are

*Continued on page 83*

# What Do These Prestigious Companies Have In Common?

## Aerovox®

DC Film and RFI Suppression Capacitors, Aluminum Electrolytic and AC Oil Capacitors, EMI Filters

## AMP

Electrical/Electronic Connectors, IC Sockets, PCB Switches

## AMRAD Engineering, Inc.

Motor Run Capacitors, HID Lighting Capacitors, Power Factor Correction Capacitors



Miniature and Subminiature Coaxial Connectors and Cable Assemblies.

## AVAX CORPORATION

MLC, Tantalum and Thin Film Capacitors, Resistors, Networks, Integrated Passive Components, Trimmers, Oscillators, Resonators, Filters, Piezo Devices, and Connectors

## BERG ELECTRONICS

High Density and Industry Standard Connectors/Subsystems

## CAROL

CAROL CABLE COMPANY INC.

Electronic and Electrical Wire and Cable and Power Supply Cords

## COLE FLEX

Tubing, Conduits, Hose, Sleeving, Splices, Insulation and Cable Harness Products, Power

## Communications Instruments, Inc.

CII Midtex

Relays and Solenoids

## COOPER

### Bussmann

Fuses, Fuseholders, Fuse Blocks, and Fuse Accessories

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Capacitors-Aluminum Electrolytics, Mica, AC Oil, Film, MICA Paper and Relays

A COMPANY OF



### Dale Electronics, Inc.

Resistors, Networks, Oscillators, Displays, Inductors, Thermistors, Connectors, & Transformers

## DI DANTONA INDUSTRIES, INC.

Batteries: Computer, Cordless Phone, Laptop, Scanner, Alarm and Medical  
Antennas: Cordless Phone and Scanner

## DEARBORN WIRE AND CABLE L.P.



## EATON

Eaton Corporation. Commercial & Military Controls Operation  
Switches, Relays, Displays and Keyboards



Quartz Crystals, Clock Oscillators, Surface Mount Products, Programmable Devices

## A GERNSBACK PUBLICATION

Electronics Now Magazine

## GUARDIAN

Relays and Solenoids

## KEMET

Electronics Corporation

Multilayer Ceramic and Solid Tantalum Capacitors

## KOA SPEER ELECTRONICS, INC.

Resistors, SMT Tantalum Capacitors Inductors, Resistor Networks, SMT Thermistors

## MALLORY

North American Capacitor Company  
Tantalums, Aluminums, Sonalaters® Ceramics, Films and AC's

## M-tron

Quartz Crystal Hybrid Oscillators

## muRata®

Fixed Ceramic Capacitors, Variable Capacitors and Resistors, Crystal Oscillators, Ceramic Filters, Resonators, EMI Filters, Hybrid Circuits and more.

## Panasonic Industrial Company

Resistors, Resistor Networks, Ceramic, Film, Electrolytic, Double Layer Capacitors, Potentiometers, Switches, Inductors, Filters, Resonators, Varistors, Thermistors

## Philips Components

Philips Electronics North America Corporation

Resistors, Ferrite Components  
Aluminum Electrolytic, Film & Ceramic Capacitors

They sell through distributors.  
They belong to the E.I.A.  
They belong on your vendor list.

## Quam

Loudspeakers and Commercial Sound Products

## ROHM

Rohm Electronics Division

Resistors, Ceramic Capacitors, Transistors/Diodes, Opto Components and IC's



Switches, Relays, Terminals, Indicator/Pilot Lights, LED Indicators, Test Clips, Test Leads, Cable Ties and Heat Shrinkable Tubing

A COMPANY OF  
**SPRAGUE**

Tantalum Capacitors, Wet & Foil Capacitors, Resistor Networks, Resistor Capacitor Networks, Filters

## Switchcraft

A Raytheon Company

Switches, Connectors, Jacks, Plugs, Jackfields & Audio Accessories, Cable Assemblies

Leadership in electronics is not just a matter of designing products better and manufacturing them better, but also of marketing them better. And the sponsors of this message understand that better service to customers requires effectively involving distributors as part of their marketing teams.

Distributor involvement means lower prices, quicker deliveries, better service over-all. The Buyer wins...the Seller wins.

Distributors help achieve marketing leadership. So does the manufacturer's involvement in the Components Group of the Electronic Industries Association. EIA fosters better industry relations, coherent industry standards, and the sharing of ideas, which helps one another and serves customers better.

In choosing your component supplier, look for the marks of leadership--

- availability through distribution
- membership in E.I.A.



Electronic Industries Association/Components Group  
2001 Pennsylvania Avenue, N.W.,  
11th Floor  
Washington, D.C. 20006  
Phone: (202) 457-4930  
Fax: (202) 457-4985

Committed to the competitiveness of the American electronics producer.

RADIO AMATEURS HAVE BEEN communicating with two-way television for years, but their equipment was so expensive that it cost more than most amateurs could afford. However, recent advances in solid-state technology have drastically reduced the prices of the necessary components for amateur television (ATV) and made them available to a far wider group of amateur operators.

Today, many key components in ATV systems that were once either prohibitive in cost or unavailable are now stock items. These include VCRs, camcorders, low-priced, quality color TV receivers, and solid-state video cameras. Credit-card-sized cameras based on charge-coupled devices (CCDs) are now available for less than \$200.

All of those components, together with the transceiver and transmitters described in this article, make the mobile, battery-operated TV station a reality. You can package a complete station in a case weighing less than 5 pounds that can easily be operated in the field.

In addition to two-way communications, the ATV projects presented in this article can be applied to radio-controlled model aircraft, boats, and cars. A transmitter and a small CCD camera placed in the vehicle act as "eyes" for the radio-controlled model; the view from the platform can be seen on a TV receiver. You can also build wireless video cameras, surveillance devices, and carry out unobtrusive nature studies. All this is possible with a package that fits in the palm of your hand and operates from AA power cells.

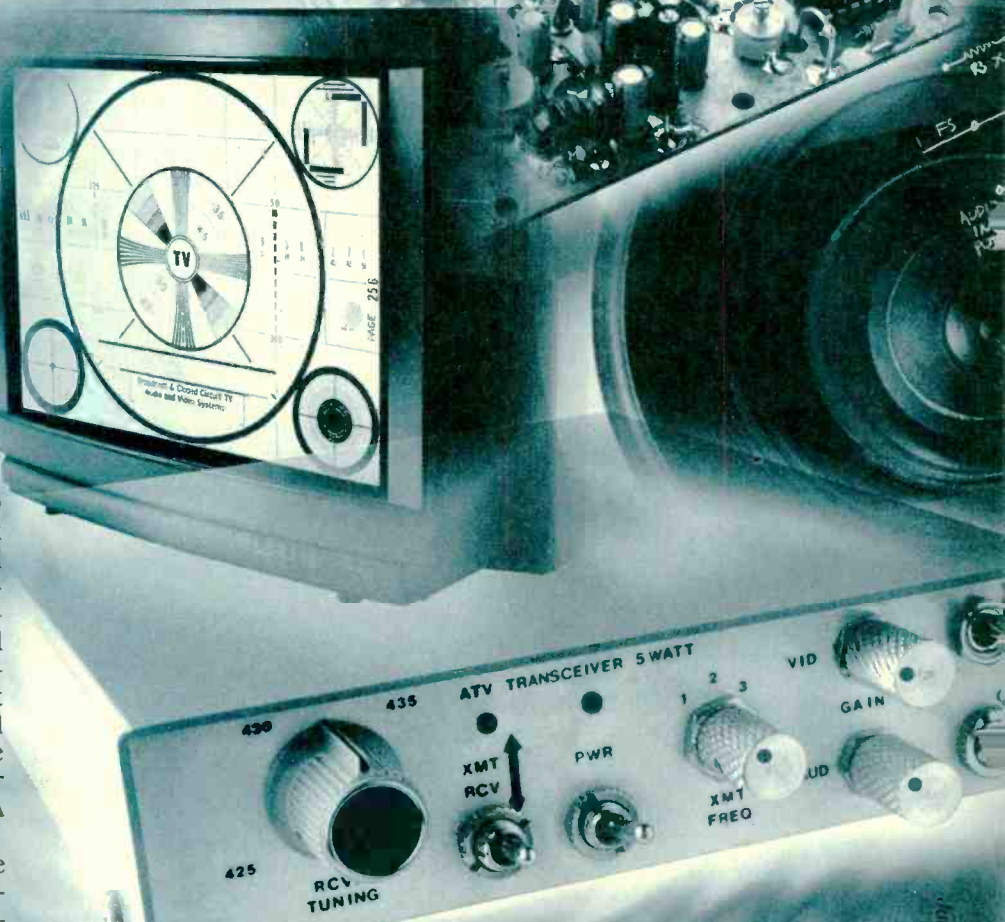
This is a two-part article; the first part describes the operation of the projects and the second part will cover the construction of them. There are four related ATV projects:

- Complete ATV transceiver with a 5-watt, three-channel transmitter, downconverter, line sampler, and RF switching relay
- 5-watt, three-channel transmitter only

# Build this Amateur TV Station

**Build your own two-way TV station that permits base and mobile operation.**

WILLIAM SHEETS AND RUDOLPH CHAIKIN



- 3/4-watt, single-channel Mini ATV transmitter

- 3/4-watt, single-channel ATV Jr. transmitter (it is the same as Mini ATV but without audio capability)

The first project is a complete two-way amateur TV station, with a three-channel transmitter, an integral receiving con-

verter, antenna relay, and test circuitry, all contained on a 3½ × 4-inch PC board. An integral heatsink that cools the RF power amplifier and modulator adds another ½-inch, making the overall size 4 × 4 × 1 inch.

Because some readers might want to build only the transmitter section, the PC board is de-

signed so that the receiving section (the downconverter), relay, and line sampler (the test circuitry) can be omitted. That will result in a three-channel, 5-watt ATV transmitter measuring only  $2\frac{1}{2} \times 4$  inches, including the heatsink.

The transmitter can be made even smaller if transmitter power less than 5 watts is acceptable. The low-power transmitter, which measures  $1\frac{3}{4} \times 2\frac{3}{4}$  inches, generates a 0.5 to 1-watt output, and is powered from an 8- to 14-volt source. Because it can be powered by a 9-volt battery, this smaller version is suitable for many applications in radio-controlled model aircraft, boats, cars, and robots. Its circuitry is similar to the 5-watt version except that it has no high-power RF amplifier and modulator. Table 1 lists suggested applications for the different ATV units.

A valid Technician Class amateur license (which does not require a knowledge of Morse code) is required to operate these transmitters legally in the United States. Also, you should know that it is illegal to transmit on commercial frequencies with these units. If you do not have a license, you can operate these transmitters only into nonradiating dummy loads for test purposes. However, you can legally construct these units and you can listen to the transmitter, but you will need a license to transmit. Outside the U.S., similar laws might apply—check the regulations of the country you are visiting. A no-code amateur license is suitable, and if you can construct these projects successfully, you should be able to pass the required exam for an amateur license easily. Call your local amateur radio club, or a licensed radio amateur for details. You can also write to the American Radio Relay League (ARRL), Newington, CT 06111 for details. (203) 666-1541.

ATV transmissions can be received on a standard TV receiver with a simple downconverter that converts signals in the 420 to 450 MHz band down to a suitable IF frequency. In the lower

TABLE 1—ATV APPLICATIONS

5-Watt Transceiver	ATV base station ATV portable and mobile operations ATV video handie-talkies
5-Watt Transmitter	ATV base with separate down converters
3/4-Watt Transmitter	R/C video links Surveillance applications Remote sensing Wireless cameras

VHF range, Channel 3 (60 to 66 MHz) or Channel 4 (66 to 72 MHz) are the IF frequencies most commonly used. A TV tuner usually can be modified to tune down to 420 MHz because all UHF TV tuners will tune as low as Channel 14 (470 MHz). Some cable-ready sets can also tune to certain UHF amateur frequencies. Channel 60 (cable), at 439.25 MHz, is the most commonly used amateur TV frequency. A downconverter provides the simplest approach, however. It can also be the most effective, because the downconverter can be made continuously tunable.

The projects to be described include relatively low-priced RF transistors characterized for 450-MHz operation to deliver 1 or 5 watts output. With a suitable antenna, a 30- to 40-mile range can be obtained, depending on factors such as height, terrain, local noise and interference levels, and path characteristics. A small antenna, such as simple 6-inch quarter-wave whip, will reduce the range. In general, simple antennas give unspectacular results. An efficient antenna at 450 MHz doesn't have to be large; a good Yagi antenna with over 10 dB gain need only be a few feet long.

The transceiver includes a three-channel 5-watt crystal-controlled transmitter that produces both picture and sound, a low-noise, tunable downconverter covering the 420 to 440 MHz ATV frequencies, a sampling circuit to monitor or test the transmitter output, and a changeover relay to perform antenna (RF) switching. The circuit draws less than 50 milliamperes when receiving and 800 to 900 milliamperes when transmit-

ting. Typically, the transmitter produces 6 watts peak output into a 50-ohms load.

### Circuitry

Figure 1 is the ATV transceiver block diagram. Notice that the transmitter section is enclosed in dashed lines. The crystal oscillator produces a signal of about 110 MHz. The exact frequency depends on the crystals installed. Any three crystals whose frequencies are within 2.5 MHz of each other are suitable. They will allow a 20-MHz frequency spread between the three output frequencies. A PIN-diode network (Q1, D1, D2, D3) selects the appropriate crystal.

A tuned network couples the oscillator's second harmonic to doubler Q2, which produces a 220-MHz output. That is coupled to a second doubler, Q3, which again doubles the frequency to 440 MHz and produces 50 to 75 milliwatts of RF energy. A double-tuned network couples this energy to Q8 which can produce nearly 1 watt of RF energy. In the  $\frac{3}{4}$ -watt transmitter, Q8 is the final RF amplifier. (It is labeled Q4 in that version.)

Amplifier Q8 drives Q9 to produce an output of about 6 watts during modulation peaks. Video modulator Q10 is in series with the collector voltage supply to Q8 and Q9. It modulates the  $V_{CC}$  supply to Q8 and Q9 with the video signal it receives from amplifiers Q6 and Q7. A small sample of the RF output voltage is rectified by D11 and fed to emitter-follower Q14. The output of Q14 is the modulation envelope of the transmitted signal. The envelope can be observed with an oscilloscope, or it can drive a monitor so that you can check picture quality.

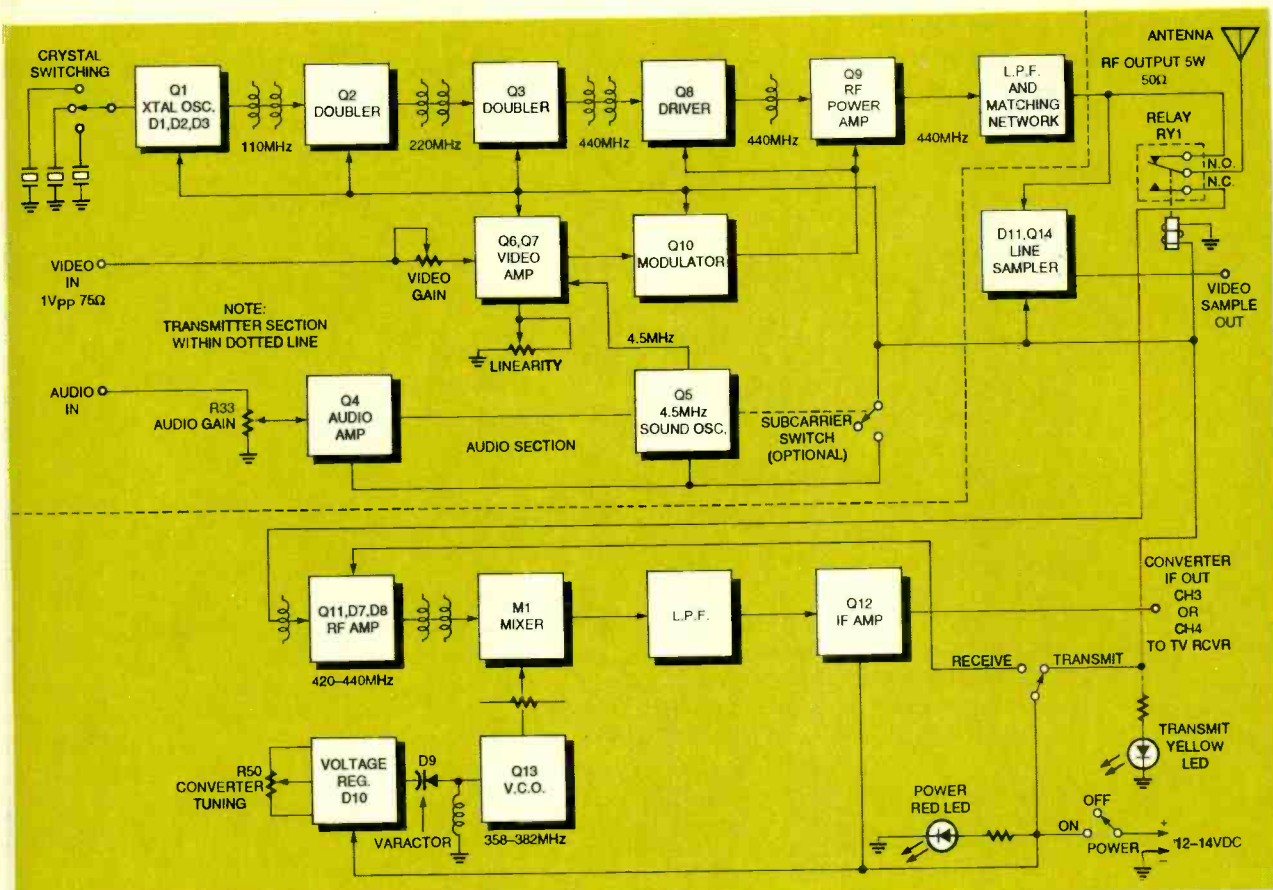


FIG. 1—ATV TRANSCEIVER BLOCK DIAGRAM. The transmitter section is enclosed in dashed lines.

The transmitter output is fed to relay RY1 which is activated by the transmitter  $V_{CC}$  line. The relay is used solely for RF switching. In the receive mode, the relay is de-energized and RF from the antenna is fed to down-converter RF amplifier Q11. The RF stage has a noise figure of less than 1 dB, a single-tuned input, and double-tuned output. Gain is about 20 to 23 dB. Signals from the RF amplifier are fed to double-balanced mixer M1 where they are mixed with the local oscillator (LO) signal from Q13. Voltage-controlled oscillator (VCO) Q13 has about a 15-MHz tuning range.

Varactor diode D9 is fed a bias voltage from tuning potentiometer R50. During transmit, DC voltage is removed from the RF stage. That reduces down-converter gain by about 50 dB. It also allows the downconverter to tune to the transmitted signal, which is useful for monitoring. The IF output of mixer M1 (60 to 72 MHz) feeds a lowpass filter that rejects UHF signals

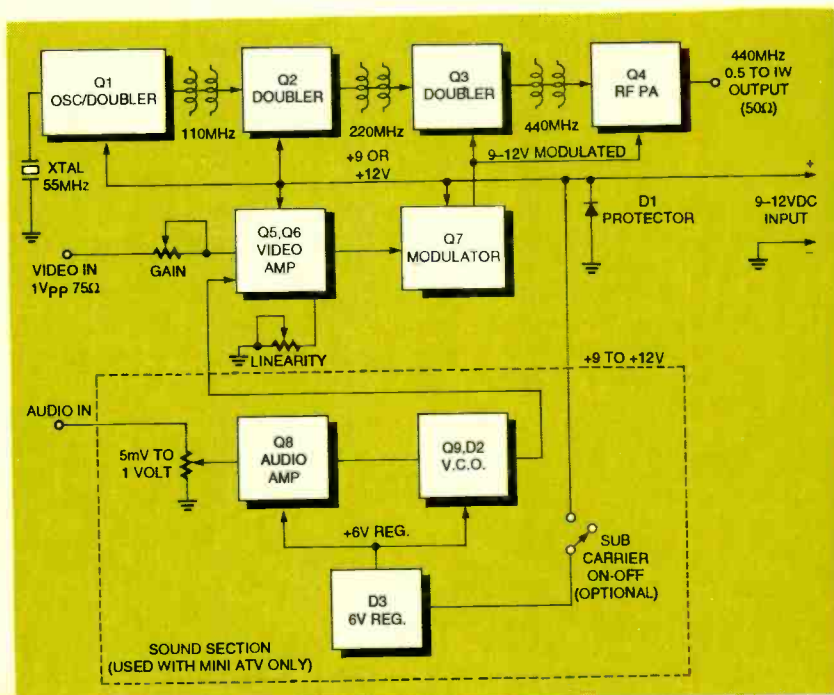
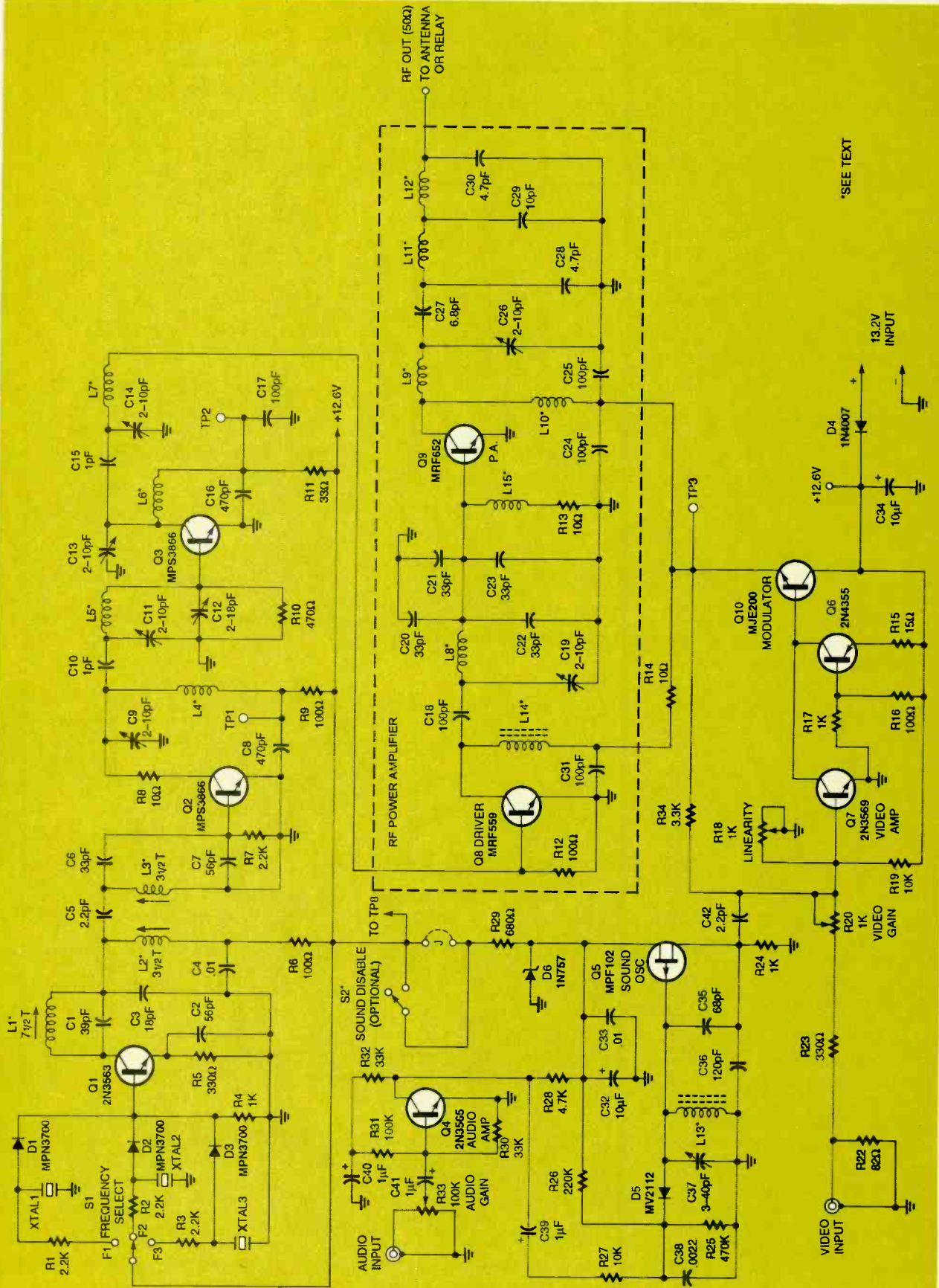


FIG. 2—BLOCK DIAGRAM OF THE 1/4-WATT UNIT. It is almost identical to the 5-watt version except that it has no 5-watt stage or crystal-switching circuitry.

above 100 MHz. IF amplifier Q12 has a 20 dB gain, and it provides an IF signal to drive a

standard TV receiver tuned to VHF Channel 3 or 4.

If audio transmission is also



34 FIG. 3—5-WATT TRANSMITTER. A 30- to 40-mile range can be obtained with a suitable antenna and favorable height, terrain, local noise and interference levels, and path characteristics.



desired, Q5 and D6 generate a frequency-modulated audio subcarrier at 4.5 MHz. The 4.5 MHz subcarrier is fed to video amplifier Q6-Q7, and it modulates the transmitted carrier. An optional subcarrier switch mutes the sound if desired. This feature is also useful for test purposes. The FM subcarrier produces a "fuzz" on the monitor waveform from Q14 if not turned off. The subcarrier can also generate colored stripes on the video from Q14 because of a beat with the 3.58-MHz color subcarrier. This occurs because some monitors do not have a sound trap in their video input circuits.

The  $\frac{3}{4}$ -watt version has a similar RF chain (see Fig. 2). Oscillator Q1 and doublers Q2 and Q3 are almost identical to those in the 5-watt version. Transistor Q4 serves as a power amplifier while Q5, Q6, and Q7 make up the video amplifiers and modulator, respectively. The main difference is in its lack of the 5-watt stage and crystal-switching circuitry.

A detailed circuit description of the 5 watt transceiver follows. Remember that the 5-watt transmitter is the transceiver without the downconverter, line sampler, and the RF relay. Also, much of the circuitry in the  $\frac{3}{4}$ -watt version is identical to the circuitry in the 5-watt unit, so only the 5-watt unit will be discussed here.

#### ATV transmitter

Figure 3 is the schematic for the 5-watt transmitter, Fig. 4 is the schematic for the Mini ATV, and Fig. 5 is the schematic for the ATV Jr. Transistor Q1, a 2N3563, forms part of the crystal oscillator. Depending on which of three crystals is selected by S1, a +12-volt bias is applied to R1, R2, or R3, which forward biases PIN diode D1, D2, or D3. The bias causes the PIN diode to appear as a resistance of a few ohms or less. Resistor R4 completes the path to ground and forms the bottom leg of a voltage divider, supplying about +3 volts bias to Q1's base. The corresponding crystal is connected to the base of Q1

### PARTS LIST—5-WATT TRANSMITTER

**All resistors are  $\frac{1}{8}$ -watt, 5%, unless otherwise specified.**

R1-R3, R7—2200 ohms  
 R14—10 ohms,  $\frac{1}{4}$ -watt  
 R4, R17—1000 ohms  
 R5, R23—330 ohms  
 R6, R9, R12, R16—100 ohms  
 R8, R13—10 ohms  
 R10—470 ohms  
 R11—33 ohms  
 R15—15 ohms  
 R18, R20—1000 ohms, potentiometer  
 R19, R27—10,000 ohms  
 R21—not used  
 R22—82 ohms  
 R25—470,000 ohms  
 R26—220,000 ohms  
 R28, R34—4700 ohms  
 R29—680 ohms  
 R30, R32—33,000 ohms  
 R31—100,000 ohms  
 R33—100,000 potentiometer  
 R34 (alternate value)—2200 or 3300 ohms

#### Capacitors

C1—39 pF, NPO  
 C2, C7—56 pF, NPO  
 C3—18 pF, NPO  
 C4, C33—0.01  $\mu$ F, disc GMV  
 C5, C42—2.2 pF, NPO (C42 alternates 1 or 3.3 pF)  
 C6—33 pF, NPO  
 C8, C16—470 pF, 20% disc  
 C9, C11, C13, C14, C19, C26—2–10 pF, trimmer (yellow body)  
 C10, C15—1 pF, NPO  
 C12—2–18 pF, trimmer (green body)  
 C17, C18, C24, C25, C31—100 pF, chip 60  $\times$  120  
 C20—C23—33 pF, chip 60  $\times$  120  
 C27—6.8 pF, NPO  
 C28, C30—4.7 pF, NPO  
 C29—10 pF, NPO  
 C32—10  $\mu$ F, 16 volts, electrolytic  
 C34—10  $\mu$ F, 16 volts, tantalum chip  
 C35—68 pF, NPO or SM  
 C36—120 pF, NPO or SM  
 C37—3–40 pF, trimmer (gray body)  
 C38—0.0022  $\mu$ F, 50 volts, Mylar  
 C39—C41—1  $\mu$ F, 35 or 50 volts, aluminum electrolytic

#### Semiconductors

D1-D3—Motorola MPN 3404 PIN diode (alternate MPN 3700)

D4—1N4007 diode  
 D5—Motorola MV2112 varactor diode  
 D6—1N757 diode  
 Q1—2N3563 transistor  
 Q2, Q3—Motorola MPS3866 transistor  
 Q4—2N3565 transistor  
 Q5—Motorola MPF102 FET  
 Q6—2N4355 transistor  
 Q7—2N3569 transistor  
 Q8—Motorola MRF559 transistor (alternate MRF627)  
 Q9—Motorola MRF652 transistor  
 Q10—Motorola MJE200 transistor

**Inductors (all coils wound on 8-32 mandrel unless noted—inductances below 50 nH are approximate and may vary  $\pm$  10nH)**

L1—125 to 300 nH (7 $\frac{1}{2}$  turns No. 22 enameled with Cambion Blue 8-32  $\times$   $\frac{1}{4}$  slug)  
 L2, L3—50 to 100 nH (3 $\frac{1}{2}$  turns No. 22 enameled with Cambion Blue 8-32  $\times$   $\frac{1}{4}$  slug)  
 L4—30 nH (4 turns No. 22 tinned)  
 L5—39 nH (5 turns No. 22 tinned)  
 L6, L8—5 nH ( $\frac{1}{2}$  turn No. 22 tinned)  
 L7—10 nH ( $\frac{1}{2}$  turns No. 22 tinned)  
 L9—7 nH ( $\frac{1}{2}$  turn No. 20 tinned, 0.375" dia.)  
 L10—40 nH (5 turns No. 22 tinned)  
 L11—20 nH (2 turns No. 20 tinned)  
 L12—12 nH (1 turn No. 29 tinned)  
 L13—11  $\mu$ H (12 turns No. 22 enameled on 0.375" toroid core)  
 L14—Bead choke, 43 matl  
 L15—part of R13  
**Other components**  
 XTAL1—54.90625 MHz crystal  
 XTAL2—54.25000 Mhz crystal  
 XTAL3—53.28125 MHz crystal  
 S1—SP3T switch and hardware  
 S2—SPST toggle switch

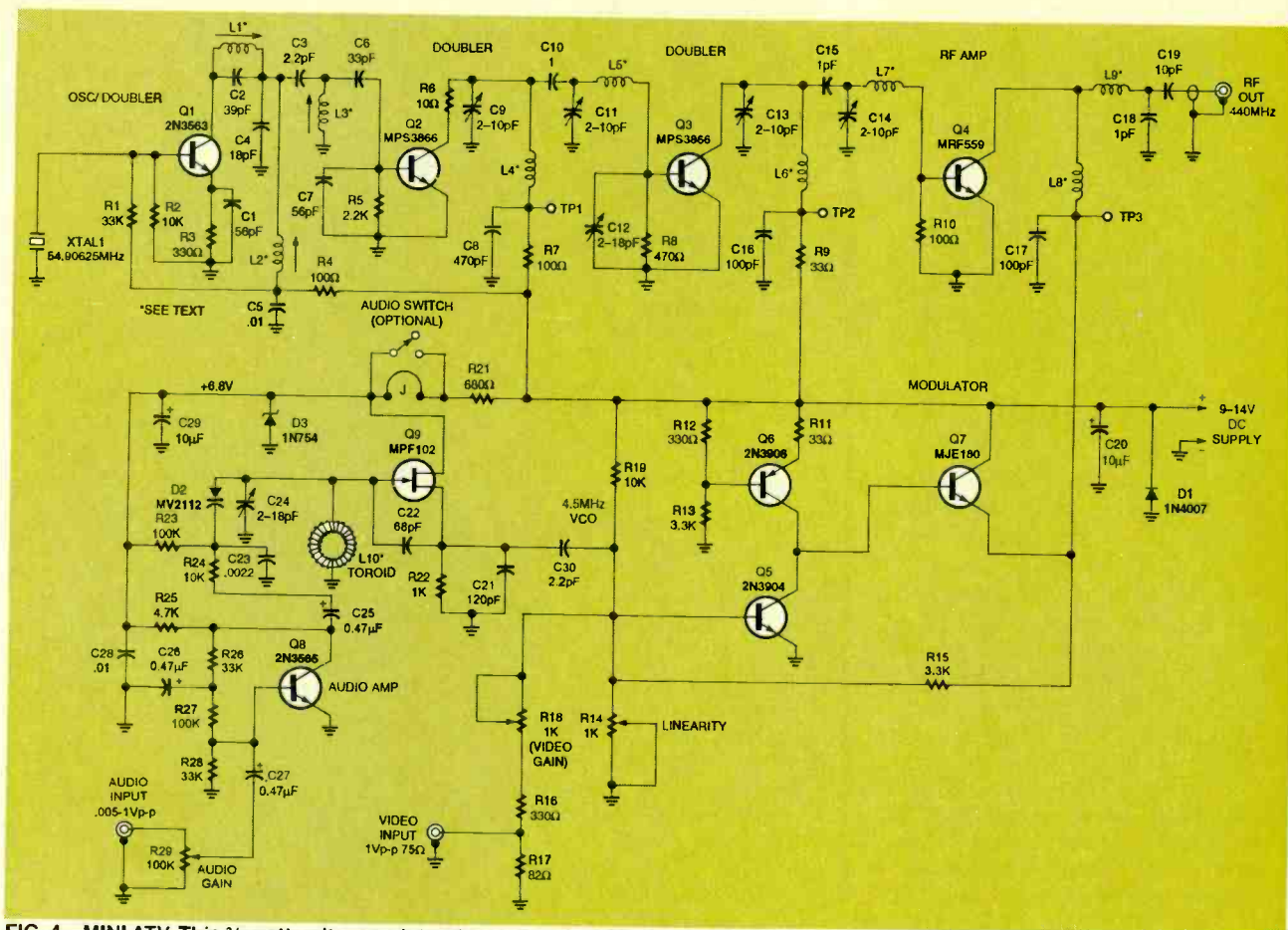
**Miscellaneous:** 2 RCA jacks, 1 female BNC, 1 power connector, 1 LED, 1 1000-ohm  $\frac{1}{4}$ -watt resistor, No. 22 enameled wire, No. 20 tinned wire, No. 22 tinned wire, No. 32 enamelled wire, heatsink material, 1 TO220 mica insulator, 5 No. 2  $\times$   $\frac{1}{4}$ " BHMS, 5 No. 2 nuts, 6 No. 4 locks, 1 No. 4  $\times$   $\frac{1}{2}$ " BHMS, 1 No. 4 nut, 1 No. 8 nut, 1 No. 8 lock, 1 No. 8  $\times$  1" BHMS (for use as coil form), transmitter PC board, power-amp PC board

through a PIN diode. In the  $\frac{3}{4}$ -watt version, R1 and R2 bias Q1's base to about +3 volts, and XTAL1 is connected between its base and ground.

At its series-resonant frequency, XTAL1 appears as a low impedance, effectively grounding the base of Q1. This forms a common-base oscillator at the crystal's series-resonant frequency. Frequency-selector switch S1 applies 12 volts to the selected crystal. Components L1

and C1 provide a high impedance load for the collector of Q1; L1 and C1 should be resonant at a frequency slightly higher than the crystal frequency (around 55 MHz or so). Because 55-MHz crystals are used, the oscillator frequency must be multiplied by 8 to obtain 440 MHz. While three doubler stages or a doubler and a quadrupler stage could do that, quadruplers are not usually efficient.

To minimize the number of



**FIG. 4—MINI ATV.** This  $\frac{3}{4}$ -watt unit, complete with audio capability is useful where size is a factor.

stages, the oscillator is made to act as its own doubler. This is done by placing a resonant circuit—L2 and C3—in series with the collector circuit, tuned to twice the crystal frequency. Capacitor C4 acts as a bypass capacitor. In the  $\frac{3}{4}$ -watt Mini ATV versions, the corresponding parts C4, L2, and C5 perform the same function. This circuit has a high impedance at 110 MHz, and it also appears as a very low impedance at 55 MHz. Similarly, L1-C1 appears as a high impedance at 55 MHz but a very low impedance at 110 MHz. Capacitor C5 couples 110 MHz energy to resonant circuit L3-C6-C7, which is tuned to 110 MHz. With this double-tuned circuit, a fairly clean 110-MHz signal is produced.

The RF voltage at the junction of C6, C7, and bias resistor R7 drives the base of Q2 (an MPS3866) fairly hard at 110 MHz. This results in a signal at the collector of Q2 that is rich in

harmonics. The collector of Q2 is connected to oscillation-suppressor resistor R8 and to resonant-circuit C9-L4-C8 tuned to 220 MHz. Components C13 and L6 select the 220-MHz component of the signal and couple it via C10 to another tuned circuit, C11-L5-C12, also tuned to 220 MHz.

Notice that test point TP1 is located at the "cold" side of L4 in both the 5- and  $\frac{3}{4}$ -watt ver-



**5-WATT ATV TRANSCEIVER.** This small package contains all the circuitry you'll need for transmitting, receiving, and downconverting a video signal complete with sound.

sions. It is the test point for measuring the DC current in the collector circuit of Q2. As more RF drive is applied to the base of Q2, more current is drawn by Q2. By monitoring the DC voltage drop across 100-ohms resistor R9 (R7 in the  $\frac{3}{4}$ -watt versions), it is possible to tune L1, L2, and L3 properly without detuning them. Adjust L1 to produce a voltage drop across R9, and then adjust L2 and L3 to maximize the drop, which can be as much as 4 to 5 volts DC. Base resistor R10 supplies 220-MHz bias to Q3 after RF rectification.

Transistor Q3 is driven hard, causing it to act as a highly non-linear amplifier. This stage draws 30 to 50 milliamperes of current. Tuned circuit C11-L5-C12 at the base of Q3 couples 220-MHz energy to Q3. Capacitor C10 couples the collector circuit of Q2 to the base of Q3. This provides a double-tuned circuit at 220 MHz, yielding good rejection

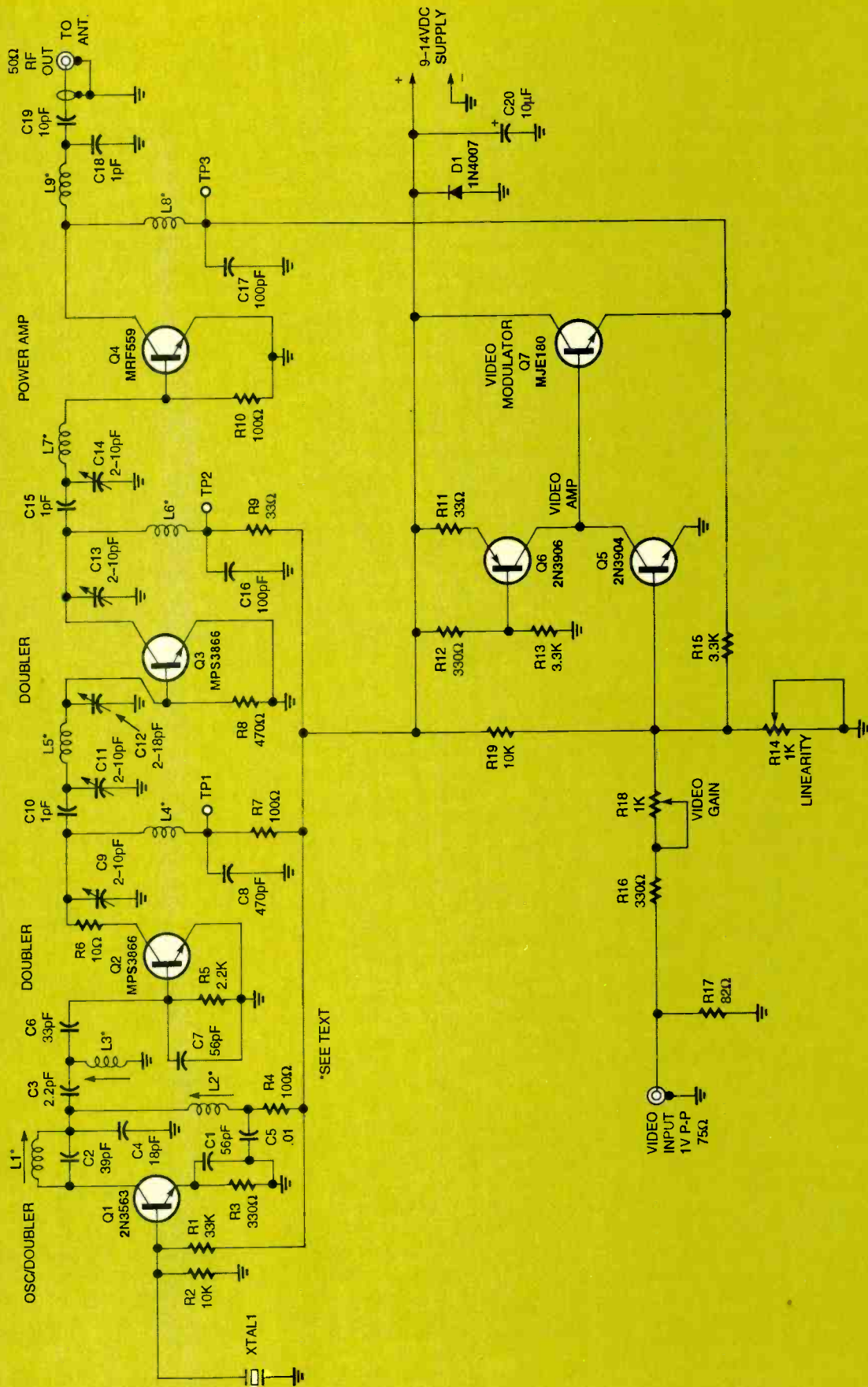


FIG. 5—ATV JR. If keeping cost as low as possible is of paramount concern, and audio output is not needed, build the ATV Jr.

## PARTS LIST—5-WATT TRANSCEIVER

All resistors are 1/8-watt, 5%, unless specified

R1—R3, R7, R49—2200 ohms  
R14—10 ohms, 1/4-watt  
R4, R17, R53, R55—1000 ohms  
R5, R23, R45, R47, R56—330 ohms  
R6, R9, R12, R16, R35, R36—100 ohms  
R8, R13—10 ohms  
R10, R41—470 ohms  
R11—33 ohms  
R15, R44—15 ohms  
R18, R20—1000 ohms, horizontal-mount potentiometer  
R19, R27, R46—10,000 ohms  
R21—not used  
R22—82 ohms  
R25, R39—470,000 ohms  
R26—220,000 ohms  
R28, R34, R42—4700 ohms (7× gain  
R34 = 3300 ohms, 5X gain R34 = 2200 ohms)  
R30, R32—33,000 ohms  
R31, R38, R51—100,000 ohms  
R33—100,000 ohms, horizontal-mount potentiometer  
R29, R43—680 ohms  
R37—47 ohms  
R40—220 ohms  
R48—6800 ohms  
R50—1000 ohms, thumbwheel potentiometer  
R52—470 ohms, 1/4-watt  
R54—3300 ohms (4700 ohms for normal use)

### Capacitors

C1, C53—39 pF, NPO  
C2, C7—56 pF, NPO  
C3, C52—18 pF, NPO  
C4, C33, C53—C55, C62, C67, C69, C70—0.01 μF disc GMV  
C5, C42—2.2 pF, NPO (alternate C42—1 or 3.3 pF)  
C6, C56—33 pF, NPO  
C8, C16—470 pF, 20% disc  
C9, C11, C13, C14, C19, C26, C43, C46, C57, C59—2–10 pF trimmer (yellow body)  
C10, C15, C60, C64—1 pF, NPO  
C12—2–18 pF trimmer (green body)  
C17, C18, C24, C25, C44, C45, C47—C49—100 pF, chip  
C20—C23—33 pF, 60×120 chip  
C27—6.8 pF, NPO  
C28, C30—4.7 pF, NPO  
C29, C65—10 pF, NPO  
C32, C63, C66—10 μF, 16 volts, electrolytic  
C34—10 μF, 16 volts, tantalum chip  
C35—68 pF, NPO or SM  
C36—120 pF, NPO or SM  
C37—3–40 pF, trimmer (gray body)  
C38—0.0022 μF, 50 volts, mylar  
C39, C40, C41—1 μF, 35 or 50 volts, electrolytic  
C50—0.6 pF (part of PC board)  
C57—6.8 pF, NPO  
C58—5.6 pF, NPO  
C61—100 pF, NPO  
C68—470 μF, 16 volts, electrolytic

**Inductors (all coils wound on 8-32 mandrel unless noted—inductances**

**below 50 nH are approximate and may vary ±10nH)**

L1—125 to 300 nH (7½ turns No. 22 enameled with Cambion Blue 8-32×¼ slug)  
L2, L3—50 to 100 nH (3½ turns No. 22 enameled with Cambion Blue 8-32×¼ slug)  
L4—30 nH (4 turns No. 22 tinned)  
L5—39 nH (5 turns No. 22 tinned)  
L6, L8—5 nH (½ turn No. 22 tinned)  
L7—10 nH (1½ turns No. 22 tinned)  
L9—7 nH (½ turn No. 20 tinned, 0.375" dia.)  
L10—40 nH (5 turns No. 22 tinned)  
L11—20 nH (2 turns No. 20 tinned)  
L12—12 nH (1 turn No. 29 tinned)  
L13—11 μH (12 turns No. 22 enameled on 0.375" toroid core)  
L14—Bead choke, 43 mall  
L15—part of R13  
L16—7 nH (½ turn No. 20 tinned)  
L17, L18—20 nH (2 turns No. 20 tinned)  
L19—75 nH (5 turns No. 22 enameled)  
L20—200 to 550 nH (11½ turns No. 22 enameled with Cambion Blue, 8-32×¼ slug)  
L21—8 nH (½ turn No. 20 square loop)  
L22—18 μH RF choke

### Semiconductors

D1—D3—Motorola MPN 3404 PIN diode (alternate MPN 3700)  
D4—1N4007 diode  
D5—Motorola MV2112 varactor diode  
D6, D10—1N757 diode  
D7, D8, D11—8200-2835 diode  
D9—Motorola MV2103 varactor diode  
Q1, Q12—2N3563 transistor  
Q2, Q3—Motorola MPS3866 transistor  
Q4—2N3565 transistor  
Q5—Motorola MPF102 FET  
Q6—2N4355 transistor  
Q7—2N3569 transistor  
Q8—Motorola MRF559 transistor (alternate MRF627)  
Q9—Motorola MRF652 transistor  
Q10—Motorola MJE200 transistor  
Q11—NEC 25137 or NEC 25139 FET  
Q13—Motorola MPSH81 transistor  
Q14—2N3904 transistor

### Other components

XTAL1—54.90625 MHz  
XTAL2—54.25000 MHz  
XTAL3—53.28125 MHz  
S1—2P3T switch  
S2—SPST toggle switch  
RY1—12-volt DIP relay  
M1—SBL-1 mixer

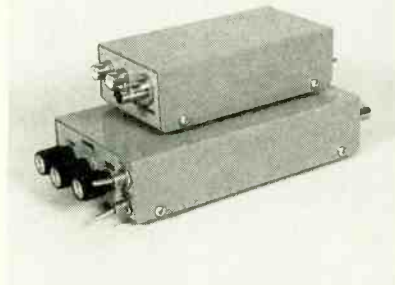
**Miscellaneous:** 2 RCA jacks, 1 female BNC, 1 power connector, 1 LED, 1 1000-ohm 1/8-watt resistor, No. 22 enameled wire, No. 20 tinned wire, No. 22 tinned wire, No. 32 enameled wire, heatsink material, 1 TO220 mica insulator, 5 No. 2×¼" BHMS, 5 No. 2 nuts, 1 12" teflon cable, 1 2" potentiometer shaft, 6 No. 4 locks, 1 No. 4×½" BHMS, 1 No. 4 nut, 1 No. 8 nut, 1 No. 8 lock, 1 8×1" BHMS (for use as coil form), transceiver PC Board, power-amp PC board

tion of unwanted frequencies. Adjust trimmer C12 for optimum matching to the base of Q3.

Capacitors C16 and C17 form a resonant circuit tuned to 440 MHz. Inductor L6 is a half-turn loop of No. 20 wire (about 0.006 microhenry). Capacitor C17 has a low impedance at 440 MHz, and C15 couples the 440-MHz energy to tuned circuits C14 and L7. At this point, about 50 to 75 milliwatts of RF energy at the transmit frequency (426 to 440 MHz) is available. The same RF exciter circuitry (Q1-Q2-Q3) is in both the 5- and 3/4-watt transmitters. Test point TP2 permits monitoring collector current of Q3 for tuning C9, C13, and C12. It is adjusted by peaking the three trimmer capacitors for a maximum current drain in Q3's collector. In the 5-watt version, Q8 and Q9 form a power amplifier. Resistor R12 provides self-bias for Q8, which receives base drive from tuned circuit C12-L7.

The collector circuit of Q8 consists of RF choke L14, bypass capacitor C31, and matching network C19 and L8. All bypass capacitors are ceramic chips. They are the only bypass capacitors that are both small and effective at 440 MHz. The collector of Q9 feeds matching network L9, C26, C27, C28, L11, C29, L12, and C30, which also acts as a lowpass filter. Harmonic output is a low 45 to 50 dB.

Transistors Q8 and Q9, which form the power amplifier assembly, are mounted on a separate heatsinked subassembly. Video-modulated DC is fed to



**5-WATT TRANSMITTER (bottom)** has audio output but it can't receive or down-convert video. **Mini ATV (top)** is a 1/4-watt unit that can transmit audio and video.

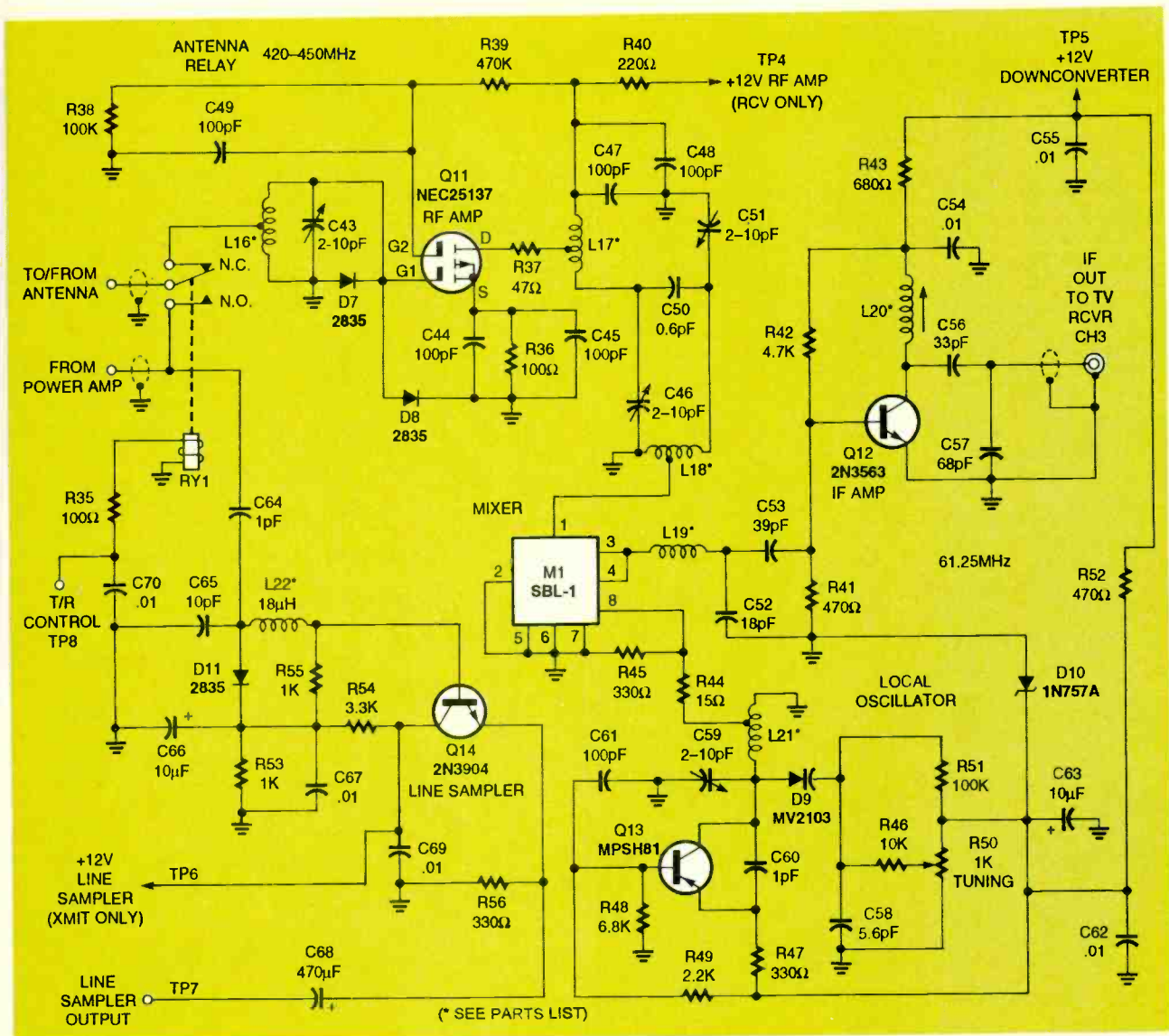


FIG. 6—DOWNCONVERTER, antenna relay, and line sampler. The downconverter consists of a tuned RF stage with a low-noise, dual-gate GASFET, a double-balanced diode mixer, an IF amplifier, and a varactor-tuned local oscillator.

### PARTS LIST—ATV JR.

All resistors are 1/8-watt unless otherwise specified

- R1—33,000 ohms
- R2, R19—10,000 ohms
- R3, R12, R16—330 ohms
- R4, R7, R10—100 ohms
- R5—2200 ohms
- R6—10 ohms
- R8—470 ohms
- R9, R11—33 ohms
- R13—3300 ohms
- R14, R18—1000 ohms, horizontal-mount potentiometer
- R15—3300 ohms (alternate 2200 to 4700 ohms)
- R17—82 ohms

#### Capacitors

- C1, C7—56 pF, NPO
- C2—39 pF, NPO
- C3—2.2 pF, NPO

- C4—18 pF, NPO
- C5—0.01  $\mu$ F, disc GMV
- C6—33 pF, NPO
- C8—470 pF, disc GMV
- C9, C11, C13, C14 2–10 pF trimmer (yellow body)
- C10, C15, C18—1 pF, NPO
- C12—2–18 pF trimmer (green body)
- C16, C17—100 pF, chip
- C19—10 pF, NPO
- C20—10  $\mu$ F, 16 volts, chip

#### Semiconductors

- D1—1N4007 diode
- D2—Motorola MV2112 varactor diode
- Q1—2N3563 transistor
- Q2, Q3—Motorola MPS3866 transistor
- Q4—Motorola MRF559 transistor
- Q5—2N3904 transistor
- Q6—2N3906 transistor
- Q7—Motorola MJE180 transistor

Inductors (all coils wound on 8-32  $\times$  1/4" form unless noted—inductances below 50 nH are approximate and may vary  $\pm$  10 nH)

- L1—125 to 300 nH (7 1/2 turns No. 22 enameled with 8-32  $\times$  1/4" Cambion Blue slug)
- L2, L3—50 to 100 nH (3 1/2 turns No. 22 enameled with 8-32  $\times$  1/4" Cambion Blue slug)
- L4—30 nH (4 turns No. 22 tinned)
- L5, L8—39 nH (5 turns No. 22 tinned)
- L6—5 nH (1/2 turn No. 22 tinned 0.375" dia.)
- L9—25 nH (2 1/2 turns No. 22 tinned)

#### Other components

- XTAL1—54.90625 MHz crystal
- Miscellaneous: ATV Jr. PC board, 8-32 screw for coil winding

## PARTS LIST—MINI ATV

All resistors are 1/8-watt unless otherwise specified

R1, R26, R28—33,000 ohms  
 R2, R19, R24—10,000 ohms  
 R3, R12, R16—330 ohms  
 R4, R7, R10—100 ohms  
 R5—2200 ohms  
 R6—10 ohms  
 R8—470 ohms  
 R9, R11—33 ohms  
 R13—3300 ohms  
 R14, R18—1000 ohms, thumbwheel trimmer potentiometer  
 R15—3300 ohms (alternate 2200 to 4700 ohms)  
 R17—82 ohms  
 R20—not used  
 R21—680 ohms  
 R22—1000 ohms  
 R23, R27—100,000 ohms  
 R25—4700 ohms  
 R29—100,000 thumbwheel trimmer potentiometer

### Capacitors

C1, C7—56 pF, NPO  
 C2—39 pF, NPO  
 C3—2.2 pF, NPO  
 C4—18 pF, NPO  
 C5, C28—0.01  $\mu$ F, Disc GMV  
 C6—33 pF, NPO  
 C8—470 pF, Disc GMV  
 C9, C11, C13, C14—2–10 pF trimmer (yellow body)  
 C10, C15, C18—1 pF, NPO  
 C12, C24—2–18 pF trimmer (green body)  
 C16, C17—100 pF, chip  
 C19—10 pF, NPO  
 C20—10  $\mu$ F, 16 volts, chip  
 C21—120 pF, NPO or SM  
 C22—68 pF, NPO

C23—0.0022  $\mu$ F, 50 volts, mylar  
 C25—C27—0.47 or 1.0  $\mu$ F, 35 volts, tantalum electrolytic  
 C29—10  $\mu$ F, 16 volts, electrolytic  
 C30—1 to 3.3 pF, NPO (1 pF, and 2.2 pF supplied in Mini-ATV kits—value determines sound subcarrier level)

**Inductors (all coils wound on 8-32  $\times$  1/4" form unless noted—inductances below 50 nH are approximate and may vary  $\pm$  10 nH)**

L1—125 to 300 nH (7 1/2 turns No. 22 enameled with 8-32  $\times$  1/4" Cambion Blue slug)  
 L2, L3—50 to 100 nH (3 1/2 turns No. 22 enameled with 8-32  $\times$  1/4" Cambion Blue slug)  
 L4—30 nH (4 turns No. 22 tinned)  
 L5, L8—39 nH (5 turns No. 22 tinned)  
 L6—5 nH (1/2 turn No. 22 tinned 0.375" dia.)  
 L9—25 nH (2 1/2 turns No. 22 tinned)  
 L10—11  $\mu$ H (12 turns No. 22 enameled on toroid)

### Semiconductors

D1—1N4007 diode  
 D2—Motorola MV2112 varactor diode  
 D3—1N754 diode  
 Q1—2N3563 transistor  
 Q2, Q3—Motorola MPS3866 transistor  
 Q4—Motorola MRF559 transistor  
 Q5—2N3904 transistor  
 Q6—2N3906 transistor  
 Q7—Motorola MJE180 transistor  
 Q8—2N3565 transistor  
 Q9—Motorola MPF102 FET

### Other components

XTAL1—54.90625 MHz crystal

**Miscellaneous:** Mini ATV PC board, 8-32 screw for coil winding form

**Note:** The following items are available from North Country Radio, PO Box 53, Wykagyl Station, New Rochelle, NY 10804-0053:

- 5-watt transceiver kit (contains PC boards, all parts that mount on them, chassis connectors suitable for basic operation, and three crystals for 439.25, 434.0, and 426.25 MHz)—\$179.00

- 5-watt transmitter kit (contains PC boards, all parts that mount on them, suitable chassis connectors for basic operation, and three crystals for 439.25, 434.0, and 426.25 MHz—downconverter and line sampler components and RF switching relay NOT included)—\$149.00

- 1/4-Watt Mini-ATV kit (contains PC board and all parts that mount on it with crystal for 439.25 MHz operation)—\$79.00

- 1/4-Watt ATV Jr. kit (contains PC board and all parts that mount on it and crystal for 439.25 MHz operation)—\$59.00

- Test Crystals (CH14, 15, 16, 17, 18, for test or export only—not legal for on the air transmission in the USA) and others for 434.0-, 427.75-, 426.25-, and 421.25-MHz are available—\$8.50 each, specify channel

- Other ATV kits for 440- and 915-MHz and CCD cameras are available—contact North Country Radio for details

- A complete catalog of kits is available from North Country Radio—send \$1.00 with a self addressed stamped (52 cents) envelope

Please include \$4.50 for the first item and add \$1.00 for each additional item for postage and handling. New York residents add sales tax.

L10 and through R14 to L14. Capacitors C24, C25, and C31 have low impedance at 440 MHz but high impedance at the higher video frequencies. The modulator must deliver video at 10 to

12 volts p-p into a 12-ohm load. This requires a power amplifier with a response from DC to 4 MHz. Modulator Q10 is installed on the same heatsink as Q8 and Q9.

A 440-MHz signal is fed through L7 to the base of Q8. About 0.5 to 1 watt of RF is produced by Q4, depending on the supply voltage. A matching network is formed by L9, C18, and C19. The network is broadband, and fixed tuning was found to be adequate. Notice that in the 3/4-watt version, the  $V_{CC}$  supply fed to Q4 is the only modulating source.

The video modulating circuit in both transmitter circuits is identical except for component values. Transistor Q10 is part of a feedback-pair video amplifier with Q7 acting as a video amplifier. Transistor Q6 supplies constant current to the base of Q10, assuring drive at peak voltages. This current produces a larger voltage swing than if a resistor were used in the collector of Q6.

The quiescent point (zero signal voltage) is set by the ratio of feedback-resistor R34 to linearity-control resistance R18, as well as gain-control potentiometer R20. Adjust R20 for maximum gain without white or black clipping, and adjust R18 to set the operating point. Input video should be between 0.7 to 1.5 volts p-p, negative sync.

## Audio

The audio channel (not used in the ATV Jr.) is basically the same in all versions. It consists of a preamplifier stage built around a 2N3565 (Q4) with a voltage gain of about +43 dB. In both 5-watt boards, audio is fed to gain-control R33 through coupling capacitor C41 to the base of Q4. Audio developed across R28 is coupled by C39 and R27 to varactor diode D5. The oscillator frequency is determined by L13 and the capacitance that shunts it. This is the series equivalent of C36 and C35, the input capacitance of Q5, trimmer C37, and the varactor diode capacitance.

Adjust the oscillator by setting C37 for operation at 4.5 MHz. When an audio signal is applied to the junction of C38, R25, R26 and D5, the effective capacitance of D5 varies with the instantaneous voltage across it. This response causes

*Continued on page 84*

# THE 'LED-HEAD'

**Build this amusing Electronic Face that appears to change mood when the LEDs that define its features are randomly switched.**

ROGER SONNTAG



HUMANS RESPOND TO CHANGES in the expressions on other human faces that reflect emotional state—happiness, anger, depression, boredom, and so on. Psychological studies have shown that people respond to those changes regardless of their gender, cultural background, race, or age difference.

Most people draw inferences (rightly or wrongly) about the mood of others by noticing relatively minor changes in facial features—the tilt of the eyebrows, the cast of the eyes, and the turn of the lips. The Electronic Face reproduces these effects symbolically with an array of 36 LEDs positioned to

represent a line drawing of the eyebrows, eyes, and mouth of a human face.

The LEDs on the circuit board are illuminated for varying lengths of time by oscillators set to change waveforms at different time intervals. These variations impart a randomness to the changes in facial expression. You'll find that this dynamic electronic display attracts a lot of attention—even from people who normally wouldn't pay much attention to electronic circuits.

Wear it around your neck on a cord, place it on your desk, or hang it up as decoration, and watch other people respond to its many changing faces. They'll be curious about it and want to know how and why the expressions change.

If you build the Electronic Face you'll learn about astable multivibrators based on Schmitt trigger inverters. The periods of the square-wave out-

puts of each oscillator can be set manually by adjusting trimmer potentiometers on the circuit board.

## How does it work?

Random triggering of the array of 36 LEDs arranged to outline eyebrows, eyes and mouth by Schmitt-trigger inverter oscillators can cause the face to smile, frown, move its eyes from side to side, and arch its eyebrows.

Figure 1 is an elementary schematic for each Schmitt trigger inverter circuit that is organized as an astable multivibrator to produce a variable square-wave output. A resistance-capacitance network consisting of a 1-megohm trimmer potentiometer in a feedback loop around the oscillator and a 47-microfarad capacitor from input to ground permit manually changing the RC time constant. This, in turn, changes the duty cycle of the output square wave. The trimmer is normally set at about its 500-kilohm mid-range position

Manually changing the trimmer's wiper position can change the frequency of the oscillator's square-wave output from 5 pulses per second down to once

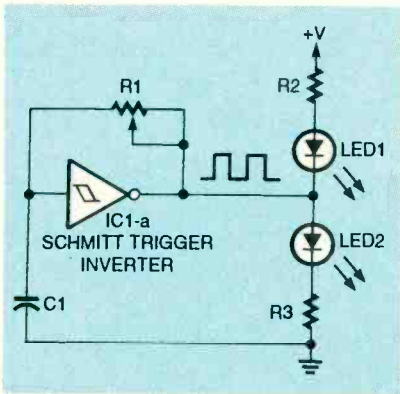


FIG. 1—BASIC CIRCUIT of the Electronic Face is a Schmitt trigger inverter with a feedback resistor and a capacitor to ground. The circuit sources or sinks LEDs.

### PARTS LIST

All resistors are ¼-watt, 10 %.

R1, R2, R5, R7, R14, R15—330 ohms

R2, R3, R6, R8, R12—220 ohms

R9, R10, R11, R13—680 ohms

R16, R17, R18, R19, R20—1 megohm trimmer potentiometer three-pin, PC mount, single-turn rotary unit.

#### Capacitors

C1, C2, C3, C4, C5,—47 μF, 10 volts, radial-leaded, aluminum electrolytic

#### Semiconductors

IC1—MC74HCT14 hex Schmitt trigger inverter, plastic DIP or equivalent (see text).

LED1—LED36—light-emitting diode, red, radial-leaded, T1 package (see text)

**Miscellaneous:** circuit board, red translucent plastic filter (see text); battery holder (see text); mounting board or case (see text), AC to DC adapter and coaxial jack (optional—see text); solder; fastening hardware

**Note:** The following options are offered by General Science and Engineering, P.O. Box 447, Rochester, NY 14603, 716-338-7001.

- Completely assembled and mounted circuit with filter, wall-outlet adapter, and matching jack—\$59.00

- Kit of parts including circuit board, all components, and filter, less case, and battery holder—\$24.00

- Wall outlet AC- to DC-adapt-er.—\$5.00

Money orders, Visa, or Master Card accepted. Add \$3.00 S&H. New York State residents add local tax.

every 50 seconds. Each circuit can source or sink current to turn on the LEDs.

Figure 2 is a schematic for the Electronic Face. Five of the six gates of IC1, a 74HCT14A CMOS hex Schmitt trigger inverter drive the LEDs by sinking or sourcing them. The shading indicates the positions of the 36 LEDs that define the eyebrows, eyes, and mouth of the circuit. The features will change at different rates when set by adjusting trimmer potentiometers R16 to R20.

Motorola offers an MC74HCT14A hex Schmitt trigger inverter IC, but any of the following can be substituted: Motorola MC74HC14A,

MC14584B or the Harris CD40106B. All of these parts have the same pinout diagram, and pins 3 and 4 are unused.

### Making the Face

An octagonal circuit board is recommended for the construction of this project. A foil pattern for this circuit board is included in this article, but a finished, trimmed and drilled board can be obtained from the source given in the Parts List as part of a kit.

Before inserting and soldering any components, decide how you want to mount the circuit board and whether you want to power it from four power cells or a wall outlet-

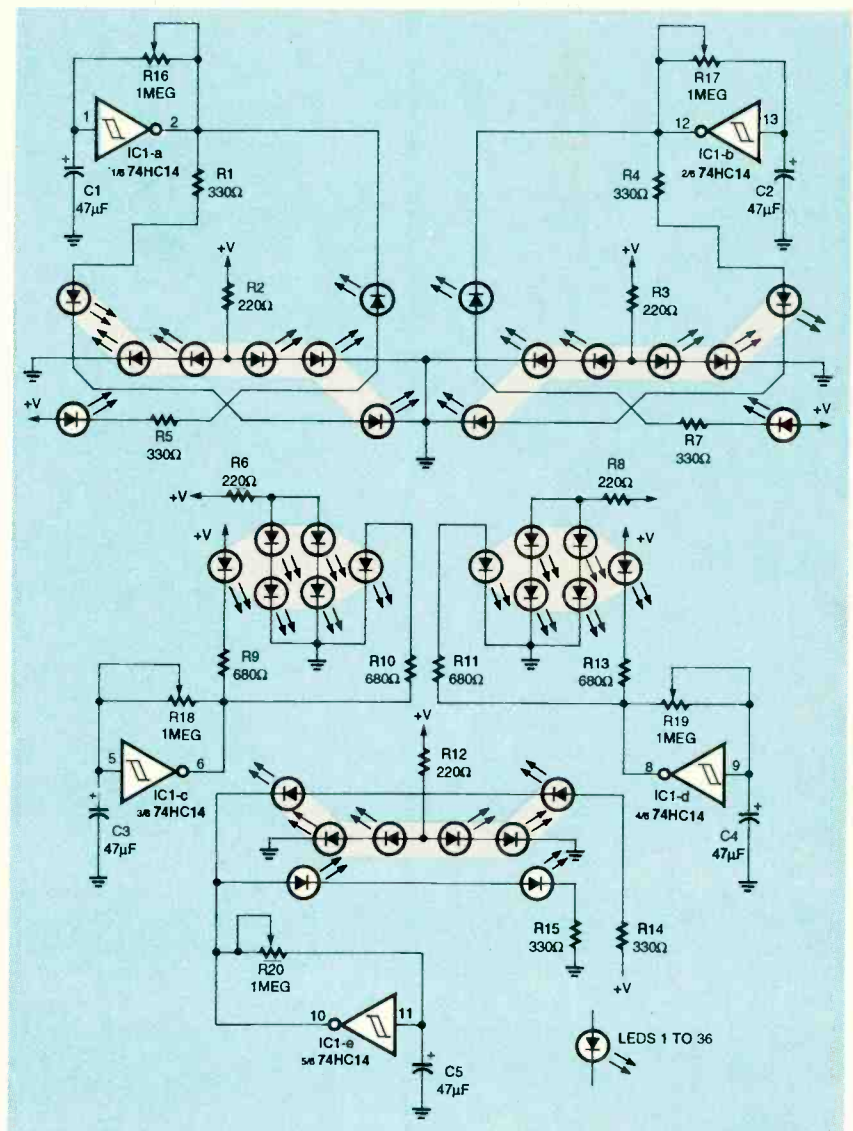


FIG. 2—SCHEMATIC FOR THE ELECTRONIC FACE. The shading defines the LEDs for each moving feature. Five of the six Schmitt trigger inverters in a hex IC illuminate the face LEDs to show mood changes.



mounted AC to DC adapter. Drill the clear mounting holes at the edges of the circuit board if you make your own.

Refer to Fig. 2 and component side parts placement diagram Fig. 3. Form and insert resistors R1 to R13 on the component side of the PC board and solder all leads with a soldering pencil with a fine tip set at a heat level satisfactory for melting rosin-core solder. Trim the leads close to the board.

Form and insert the leads of electrolytic capacitors C1 to C5 in the board, observing their correct polarities. Solder the leads and trim them close to the board. Insert trimmer potentiometers resistors R16 to R20, solder them in position and trim excess leads.

The LEDs to be soldered on the solder side of the board are specified as red, radial-leaded units in T1 cases. They might or might not have flat surfaces at their bases. However, even without the flats, the cathode lead is typically the shorter of the two. (The LED die is mounted on the cathode lead.) It is recommended that all LEDs be tested to see that they are functional with a suitable battery before they are inserted in the board.

Reverse the circuit board and this time refer to Fig. 2 and solder-side parts placement diagram Fig. 4. Insert the LEDs in the circuit board in clusters of six to eight, observing their correct polarities. Adjust the height of the LED bases about 1/4 inch above the board. Avoid bending the leads of the LEDs when inserting them. Solder those LEDs and trim their leads close to the board.

Continue inserting and positioning the LEDs in small clusters until all 36 have been soldered and trimmed. Then recheck their polarities to be sure that placement was correct. Note: the LEDs can be inserted from the component side and soldered on the foil side without changing the operation of the circuit, if you prefer.

Insert and solder IC1 on the solder (foil) side of the circuit board. Then recheck the complete board looking for solder

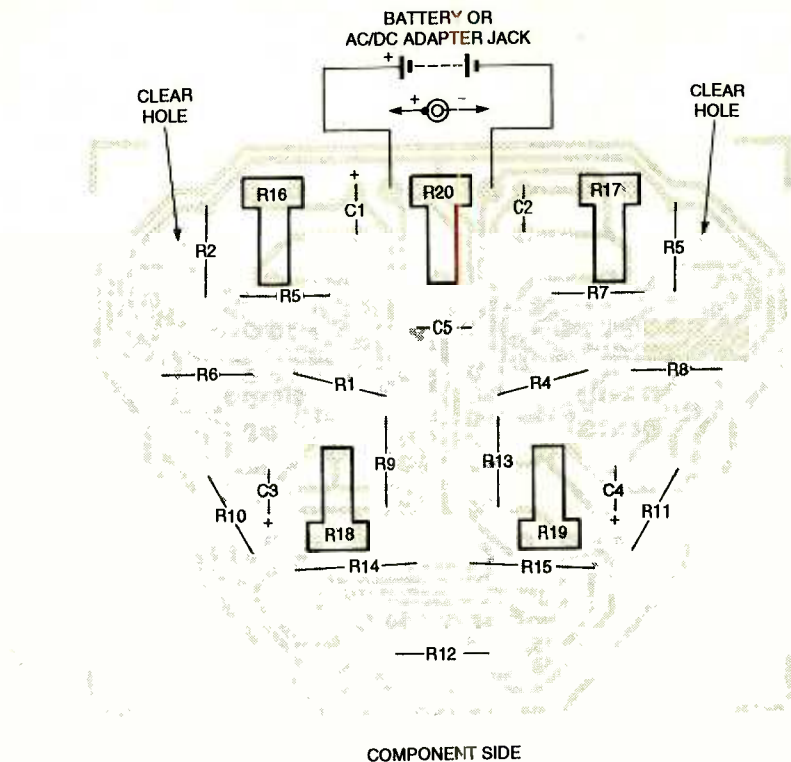


FIG. 3—COMPONENT SIDE PARTS PLACEMENT DIAGRAM for the Electronic Face.

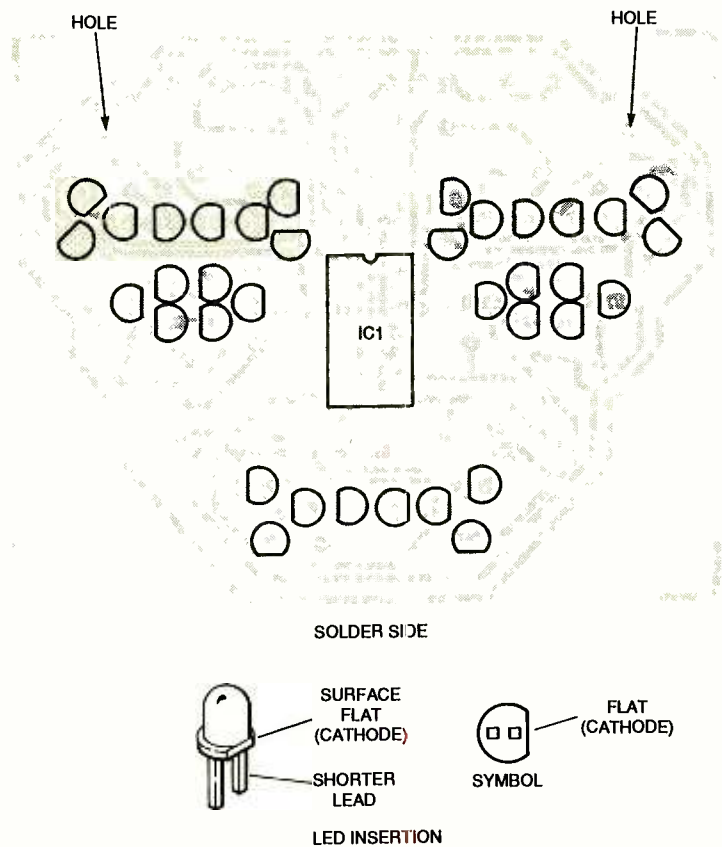
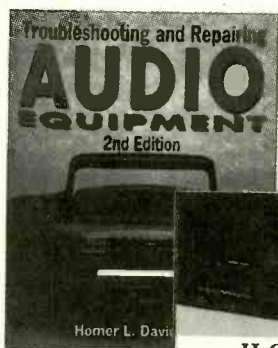


FIG. 4—SOLDER SIDE PARTS PLACEMENT DIAGRAM for the Electronic Face.

bridges or cold solder joints (dull gray). Make any repairs needed.

#### Circuit operation

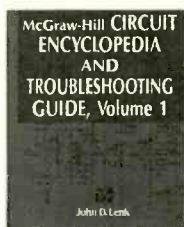
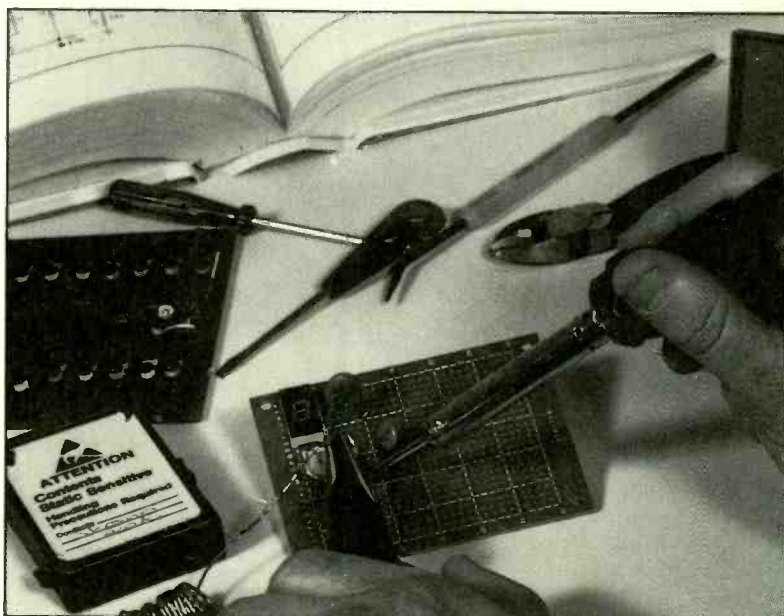
Adjust each of the trimmer potentiometers R14 to R17 with



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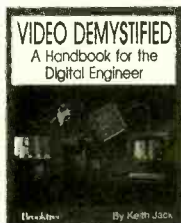
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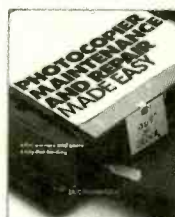
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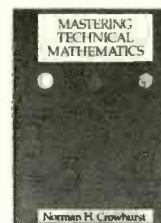
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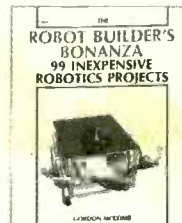
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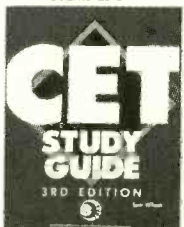
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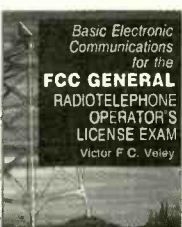
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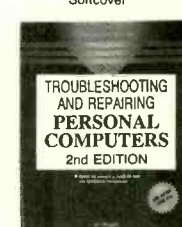
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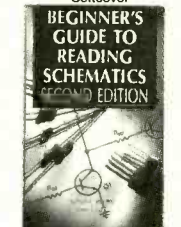
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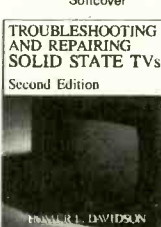
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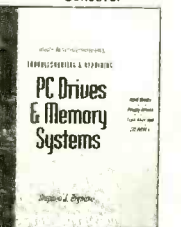
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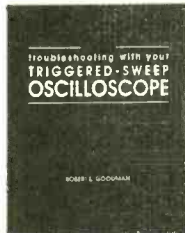
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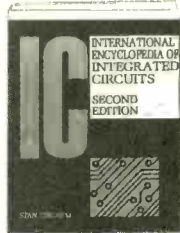
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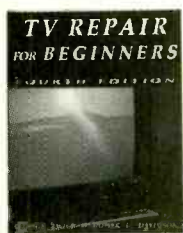
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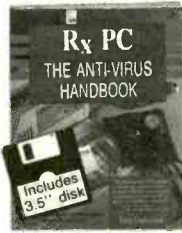
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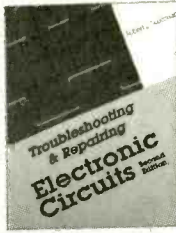
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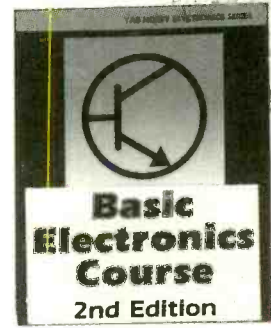
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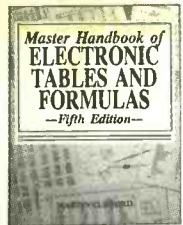
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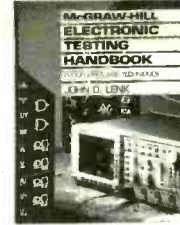
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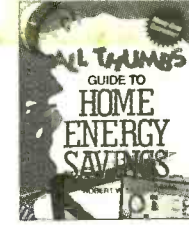
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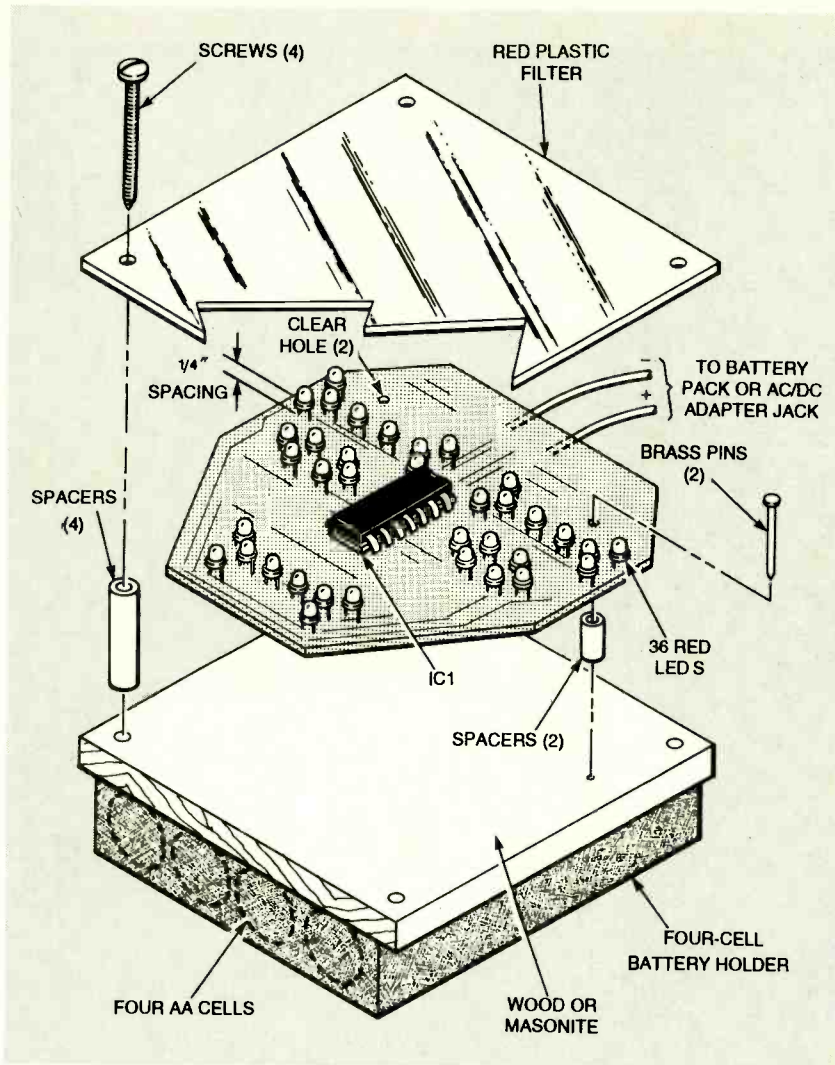
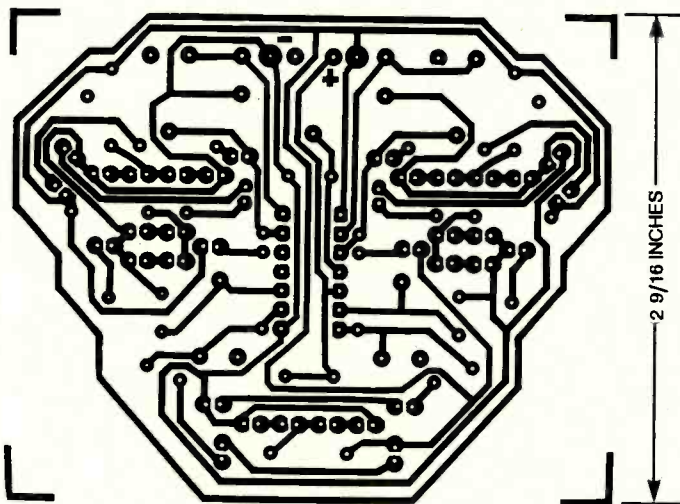


FIG. 5—MECHANICAL ASSEMBLY. The mounting board can be wood or even a suitable plastic case. The three parts are assembled with screws, nuts, pins and spacers.



FOIL PATTERN for Electronic Face.

an insulated tool and check to see that each Schmitt trigger oscillator section is switching. Then adjust the time constants

so that the "facial" pattern will change with reasonable frequency. A good place to start is with the following settings:

Feature	Time (seconds)
Eyes	2 to 3
Eyebrows	4 to 10
Mouth	8 to 15

### Packaging the circuit

Refer to the mechanical assembly diagram Fig. 5 for one possible packaging configuration. There are, however, many other possibilities. For the most effective display, it is recommended that the LEDs be covered with a red filter made from red-dyed transparent sheet plastic. The red filter screens out obvious variations in the brightness level of individual LEDs and masks the circuit components and circuit board traces that would otherwise be visible on the board.

If you want to power the face with batteries, obtain a battery holder for four AA cells (Radio Shack No. 270-383 or equivalent). Determine the lengths of the wires from the holder wires that you will need after you have decided how you want to mount the circuit.

Strip the ends of the insulated hookup wire from the holder, and solder the red wire in the hole marked + on the circuit board and the black (ground) wire in the hole marked -. The four AA cells will provide a DC voltage of about 5 volts for battery-powered circuit operation.

Alternatively, Electronic Face can be powered from a 120-volt AC to 6-volt DC wall-outlet adapter. This should be a UL Listed Class 2 transformer with a rating of 120 volts AC, 5 watts and an output of 6 volts DC at 150 to 200 milliamperes. The circuit board can be mounted on a square 1/8-inch plywood or Masonite of appropriate size to permit the circuit board to be sandwiched between the filter and substrate. Allow enough room for nuts, bolts and spacers near the edges if you elect to power the face from cells in a battery holder. If you use a battery holder, cement or bolt it to the underside of the mounting board.

Alternatively, you might want  
*Continued on page 90*

THIS ARTICLE CONTINUES THE relay switching circuit theme of last month by presenting a selection of practical control circuits for electromagnetic relays. Last month's article discussed the basic operating principles and application rules for four well-known relay classes—the electromagnetic relay (EMR), the reed relay, the solid-state relay (SSR), and the CMOS bilateral switch.

**High-impedance relays.**

Electromagnetic and reed relays are low-impedance, electromechanical devices whose typical coil impedance values range from tens to hundreds of ohms while input drive signal sources typically have much higher impedance values. Maximum power is transferred between the input drive signal and the relay coil when the source and load impedances are matched.

This is accomplished by inserting additional circuitry between the input drive signal and the relay coil. These circuits can be either a transistor stage or a transistor stage with one or more IC logic gates. Figures 1 to 4 show four different ways to boost the input impedance of a relay with transistors and logic gates.

Transistor Q1 in Fig. 1 is organized as a simple common-emitter amplifier that increases the effective sensitivity of the 12-volt coil of relay RY1 about one hundred times (e.g., the current gain of Q1 in this circuit is about 100). The introduction of this amplifier stage reduces

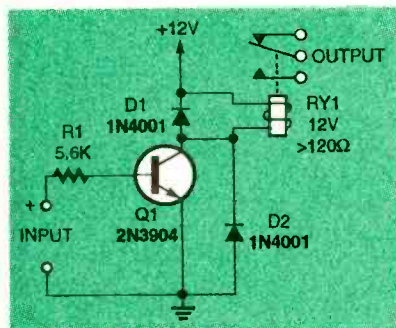
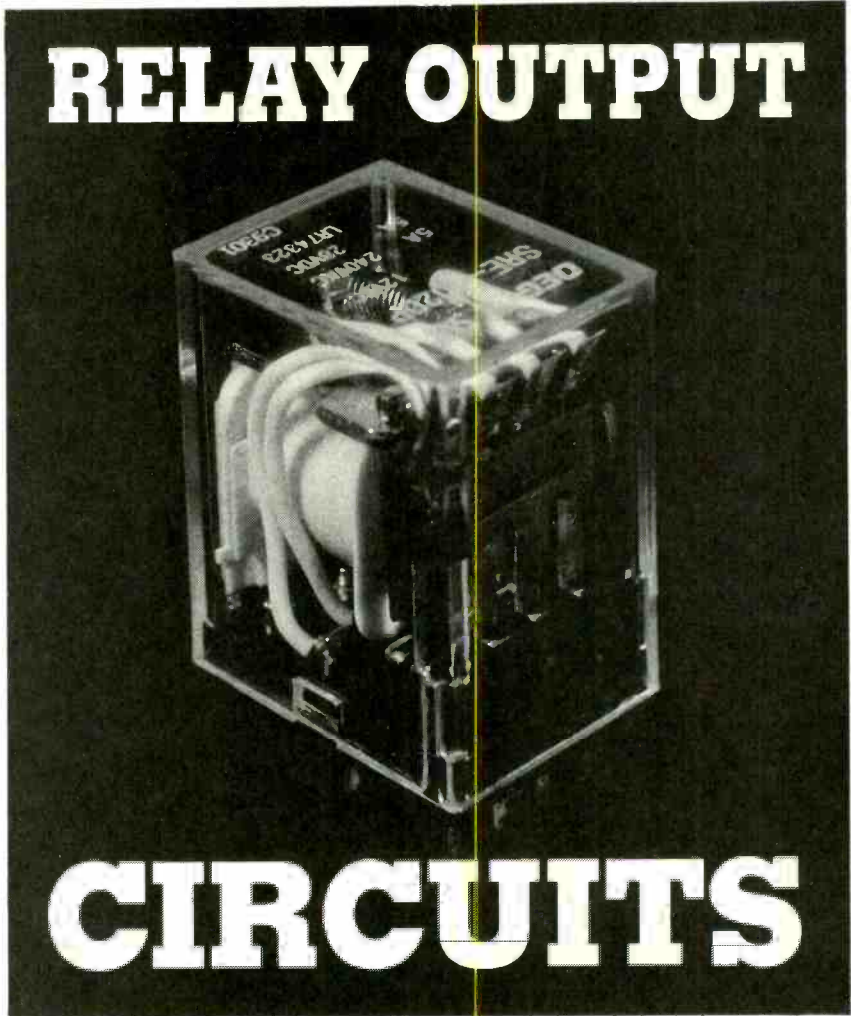


FIG. 1—NON-LATCHING TRANSISTOR-driven relay switching circuit.



**Learn to design transistorized circuits that can switch and time relay functions remotely with low-power input.**

relay sensitivity to a few volts. Resistor R1 puts safe limits on the input current to Q1, and it also determines the effective input impedance of the circuit. (The impedance is equal to the value of R1 plus about 1 kilohm.) Diodes D1 and D2 damp the coil's back EMF. (See last month's article.) The contacts of relay RY1 can control external circuitry.

Figure 1 is a schematic for a non-latching relay driver circuit. Relay RY1 is off when the input voltage is less than 600 millivolts and on when the input voltage exceeds a few volts. This driver circuit can be made self-latching by modifying it as

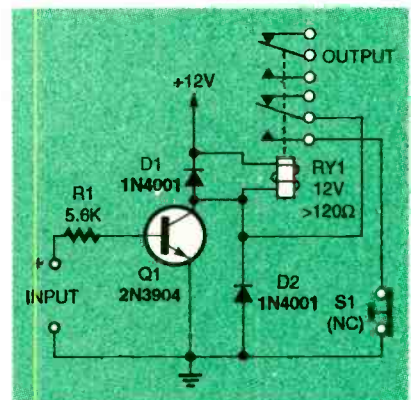


FIG. 2—SELF-LATCHING TRANSISTOR-driven relay switching circuit.

shown in Fig 2. Relay RY1 now has two sets of normally open (NO) contacts; the upper set is

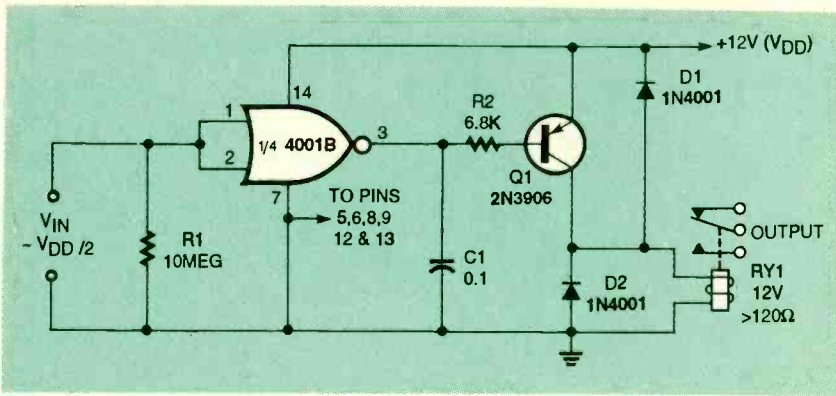


FIG. 3—HIGH-IMPEDANCE RELAY switching circuit.

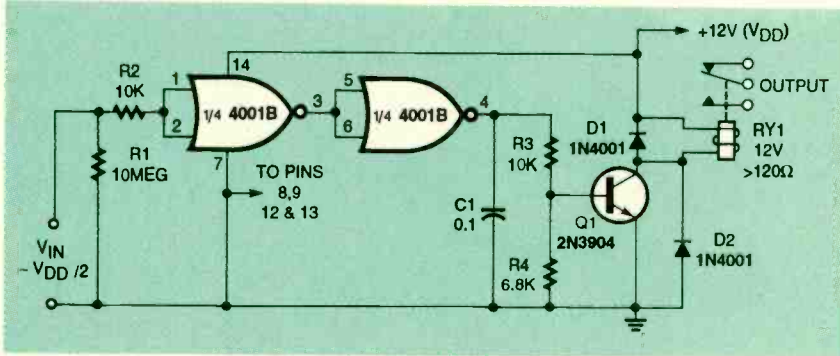


FIG. 4—MODIFIED HIGH-IMPEDANCE relay switching circuit.

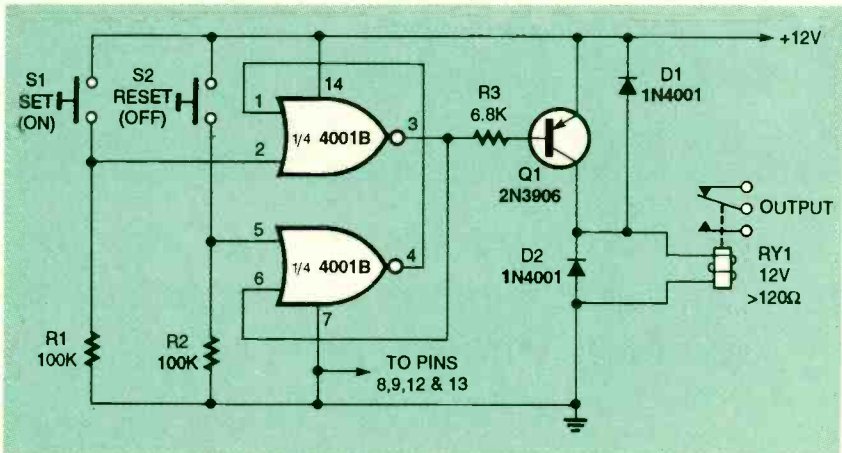


FIG. 5—BISTABLE RELAY SWITCHING circuit.

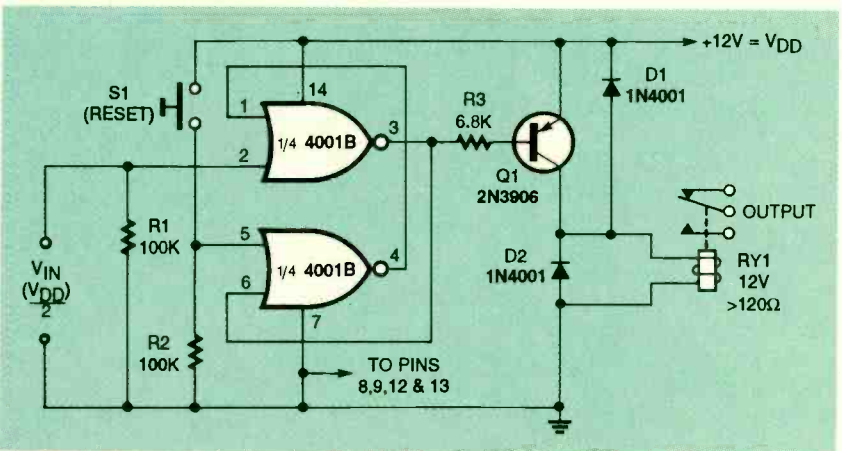


FIG. 6—SELF-LATCHING, HIGH-impedance relay switching circuit.

for the relay's output and the lower set is for latching. The latching set is in parallel with Q1, and it is actuated by normally closed (NC) switch S1.

As a result, these contacts bypass Q1 and self-latch RY1 after the relay has been initially energized. Once it has self-latched, the relay can be turned off again only by opening S1 or breaking the power connection.

The circuits of Figs. 1 and 2 have input impedances of only a few thousand ohms. If desired, the input impedance can be raised to 10 megohms or more by driving Q1 through a CMOS buffer stage as shown in Figs. 3 and 4. In these circuits, the CMOS buffer consists of one of four NOR gates of a CD4001B quad, 2-input NOR gate. The gate is wired as an inverter by short-circuiting its two input pins 1 and 2 together.

Figure 3 has only a single CMOS inverter stage. Consequently, to ensure that the relay turns off when the input voltage is low, transistor driver Q1 must be a PNP device, in this instance a 2N3906. In Fig. 4, two CMOS inverter stages are wired in series, so that the overall signal inversion is zero. Consequently, Q1 can be an NPN transistor such as the 2N3904.

It is worth noting in both Figs. 3 and 4 that the input impedance actually equals the value of resistor R1, and that the relay actually turns ON (or OFF) when the input signal exceeds (or drops below) about one half the supply voltage. This is the transition voltage for the CD4001B CMOS input gate. At that value the gate operates in the linear mode. Capacitor C1 inhibits any high-frequency or transient signals that might appear at the gate when the circuit is operated in the linear mode.

### Bistable circuits

A relay can be organized for bistable operation. In this mode it turns on and self-latches when a SET pushbutton switch is pressed, and it can be turned off again only by pressing a RESET pushbutton switch. Figure 5 is the schematic for a bistable relay switching circuit.

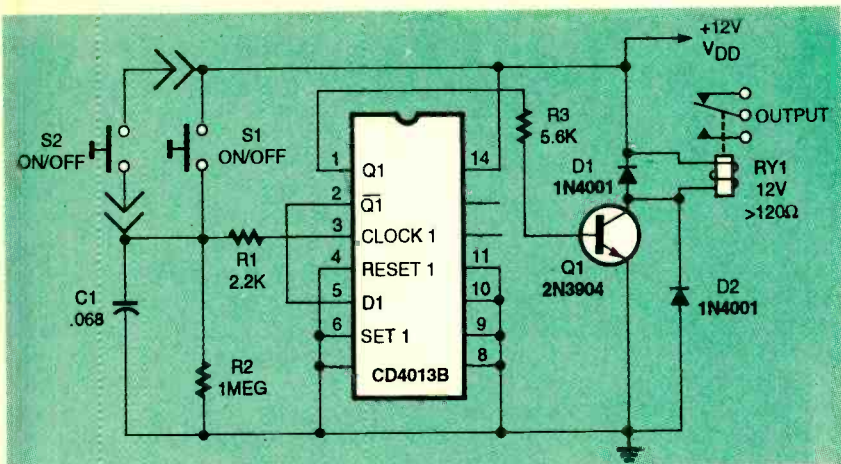


FIG. 7—PUSHBUTTON-OPERATED BINARY relay switching circuit.

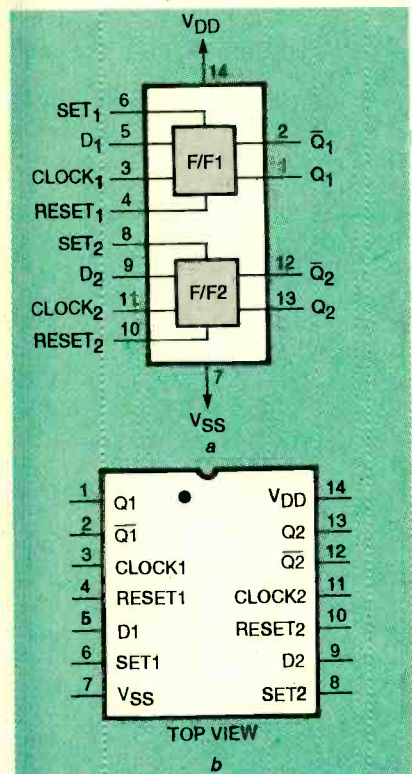


FIG. 8—CMOS DUAL D-TYPE FLIP-FLOP CD4013B: functional diagram (a), and pinout diagram (b).

In that schematic, two NOR gates of a CD4001B CMOS NOR gate are set up as a simple manually-activated bistable multivibrator. One of its outputs is connected to the relay coil through the Q1 common-emitter buffer stage. (Three other CD4000B series CMOS logic ICs are also specified in this article: CD40013B, CD40017B and CD4020B. All are offered by Harris Semiconductor and many other suppliers).

The circuit in Fig. 5 actually changes state as its SET or RESET input signal rises through the half supply voltage transition value of the CMOS gate. This response makes it easy to modify the circuit so that it acts as a self-latching, high-impedance relay, as shown in Fig 6.

The relay turns on and self-latches when the input voltage rises above the transition value; the relay can then be turned off only by removing or reducing the input voltage and pressing

the RESET switch. This circuit has an input impedance of 10 megohms.

Figure 7 shows another practical pushbutton-operated switching circuit. A single switch can turn the relay on and off, but many similar switches can be wired in parallel to permit the relay to be remotely controlled from many different locations. The relay changes state each time an input switch is pressed or released.

As a result, if the relay is initially on, it will turn off when any switch is pressed. But it can be turned on again when any switch is pressed after that. Therefore, the circuit exhibits a binary relay characteristic.

The circuit in Fig. 7 is designed around a CD4013B CMOS, dual D-type flip-flop IC whose functional and pinout diagrams are shown in Fig. 8. One flip-flop stage can be disabled by grounding its input pins, and the other flip-flop is configured as a divide-by-two circuit. This is done by shorting its Q and D1 pins together.

The input clock pulses to this divide-by-two stage must have rise times that are less than 15 microseconds; these are obtained by pressing one of the pushbutton switches. Each time the switch contacts are closed, capacitor C1 charges rapidly through the switch to provide the fast-rise time clock pulse.

Capacitor C1 then discharges slowly through R2 when the switch is re-opened. This response eliminates false triggering caused by switch bounce or

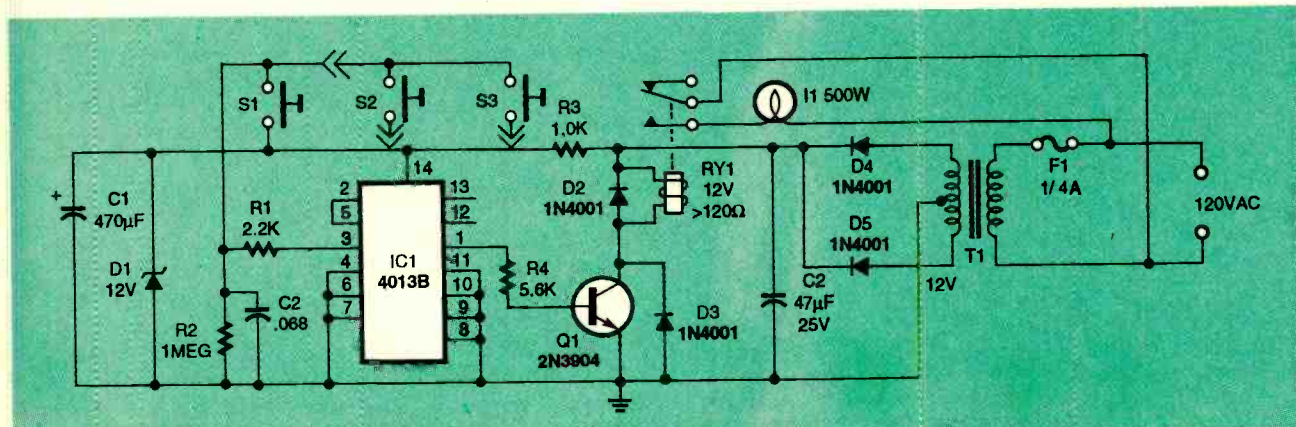


FIG. 9—MULTIPLE-INPUT, AC-LINE-powered binary lamp and relay switching circuit.

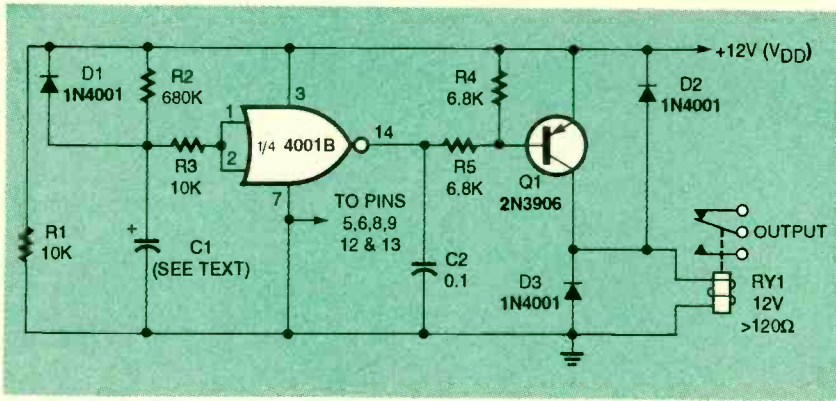


FIG. 10—DELAYED-TURN-ON RELAY switching circuit.

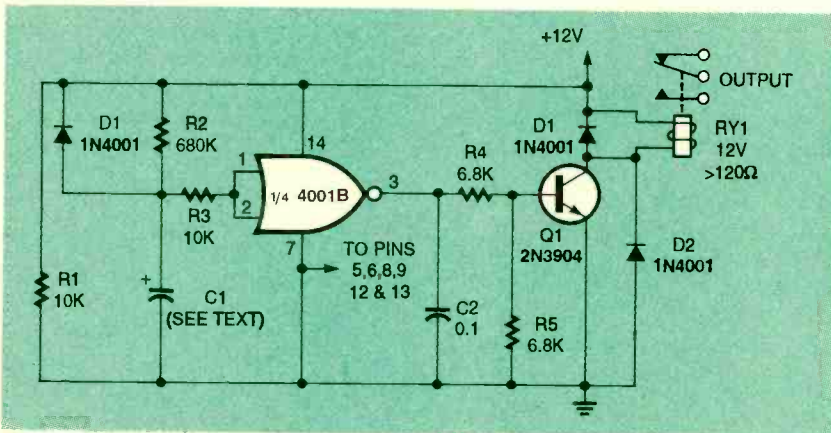


FIG. 11—AUTOMATIC TURN-OFF RELAY switching circuit.

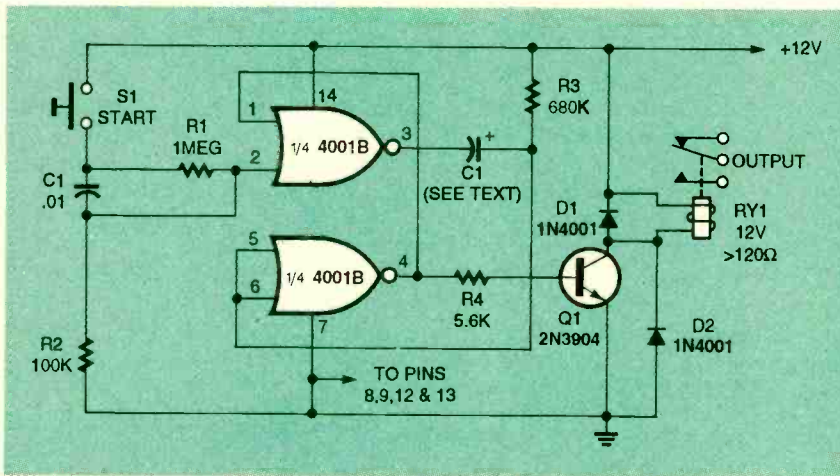


FIG. 12—ONE-SHOT MULTIVIBRATOR TIMER relay switching circuit.

chatter. As a result, transistor Q1 and the relay reliably change state each time a pushbutton switch is pressed.

The circuit illustrated in Fig. 7 will permit the relay to be actuated from many different locations. If this circuit is installed for use in a home or office it is recommended that approved switches suitable for use 120-volt AC operation be installed. Hall, landing, or cor-

ridor lights can be controlled from several different locations. Approved insulated twin-lead cable connecting the components can be concealed in the walls or along the baseboards.

Figure 8 shows the functional and pinout diagrams for the CMOS, dual D-type flip-flop. It consists of two identical flip-flops. Each flip-flop has independent DATA, SET, and CLOCK inputs and Q and  $\bar{Q}$  outputs.

In the light control application, the circuit should be powered from the 120-volt AC line. Figure 9 shows how the circuit in Fig. 7 can be modified to operate from the AC line. Transformer T1 must be selected to provide a 24-volt, center-tapped output at 100 milliamperes or greater.

### Timer circuits

Relays can be put to work in a wide variety of timer or time-delayed-switching applications with time delays from a fraction of a second to tens of hours. Figures 10 to 15 are practical examples of timing circuits for relay control.

Figures 10 to 12 show how CD4001B CMOS NOR gate ICs can produce time delays of up to several minutes with reasonable accuracy. The circuit in Fig. 10 offers delayed turn-on relay switching, and it operates as follows:

The CMOS gate is configured as a simple digital inverter. Its output is fed to the base of PNP transistor Q1 at the junction of resistor R5 and capacitor C2. The input to IC1 is taken from the junction of the time-controlled potential divider formed by resistor R2 and capacitor C1.

Before power is applied to the circuit, capacitor C1 is fully discharged. Therefore, the inverter input is grounded, and its output equals the positive supply voltage; transistor Q1 and relay RY1 are both off under this circuit condition.

When power is applied to the circuit, C1 charges through resistor R2, and the exponentially rising voltage is applied to the input of the CMOS inverter gate. After a time delay determined by the RC time constant values of capacitor C1 and resistor R2, this voltage rises to the threshold value of the CMOS inverter gate.

The gate's output then falls toward zero volts and drives transistor Q1 and relay RY1 on. The relay then remains on until power is removed from the circuit. When that occurs, capacitor C1 discharges rapidly through diode D1 and resistor R1, completing the sequence.



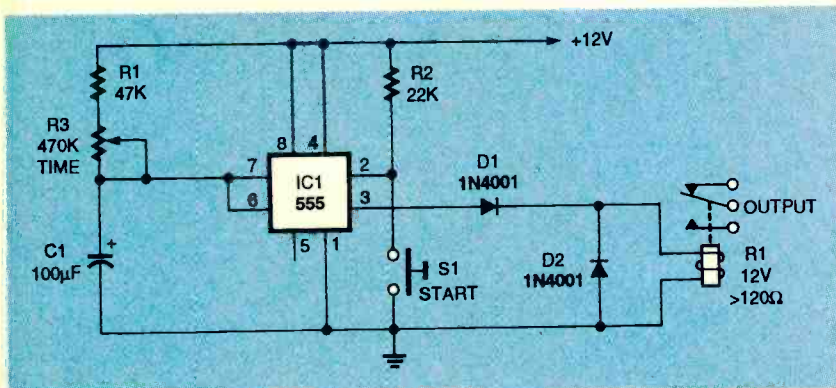


FIG. 13—SIMPLE 6-TO-60-SECOND timer relay switching circuit based on the 555 timer IC.

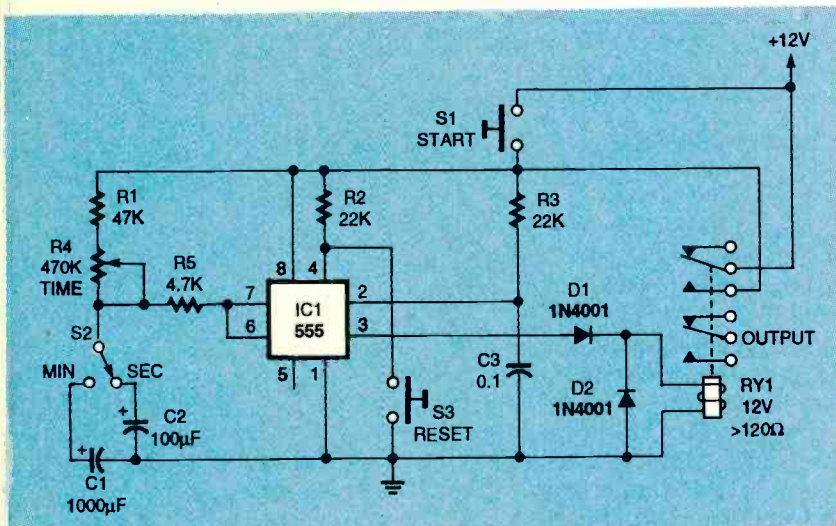


FIG. 14—TWO-RANGE 6-TO-60-SECOND and 1-TO-10 minute timer-relay switching circuit based on the 555 timer IC.

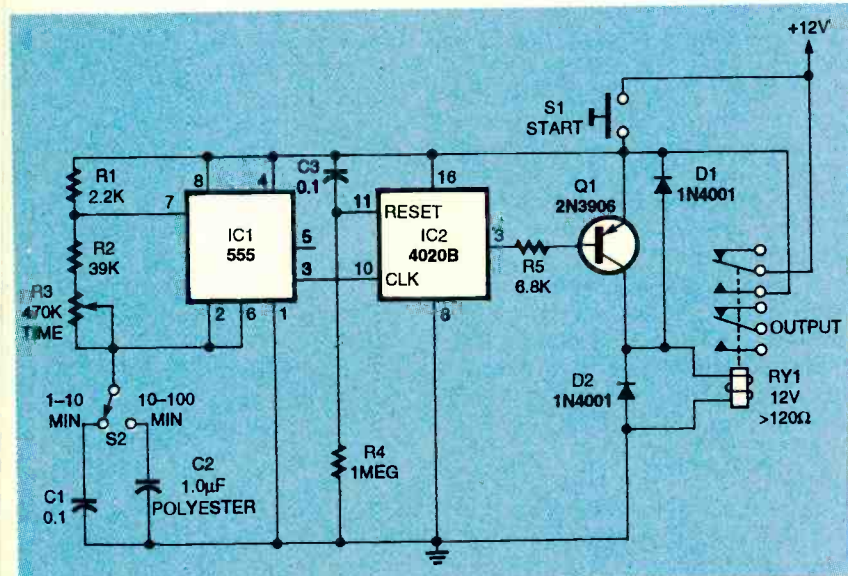


FIG. 15—TWO-RANGE 1-TO-10 MINUTE and 10-TO-100-MINUTE timer-relay switching circuit based on the 555 and 4020B ICs.

Figure 11 shows how the circuit function of Fig. 10 can be reversed so that the relay turns

on when power is applied but turns off again automatically after a preset delay. This re-

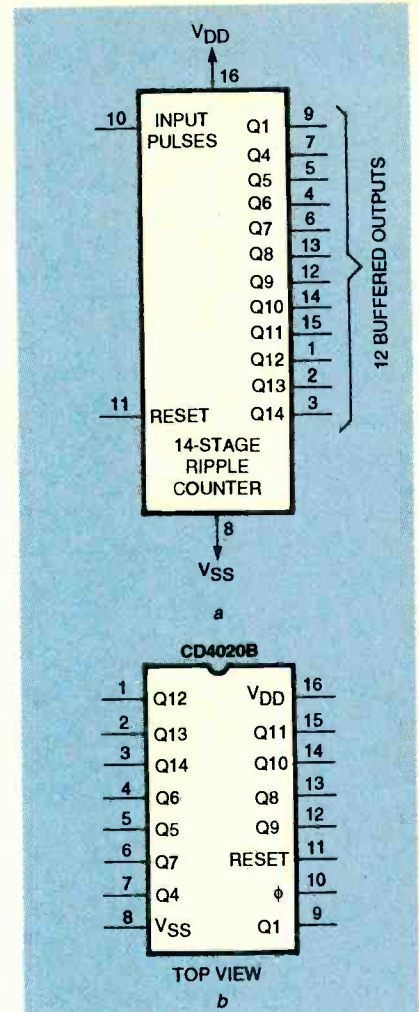
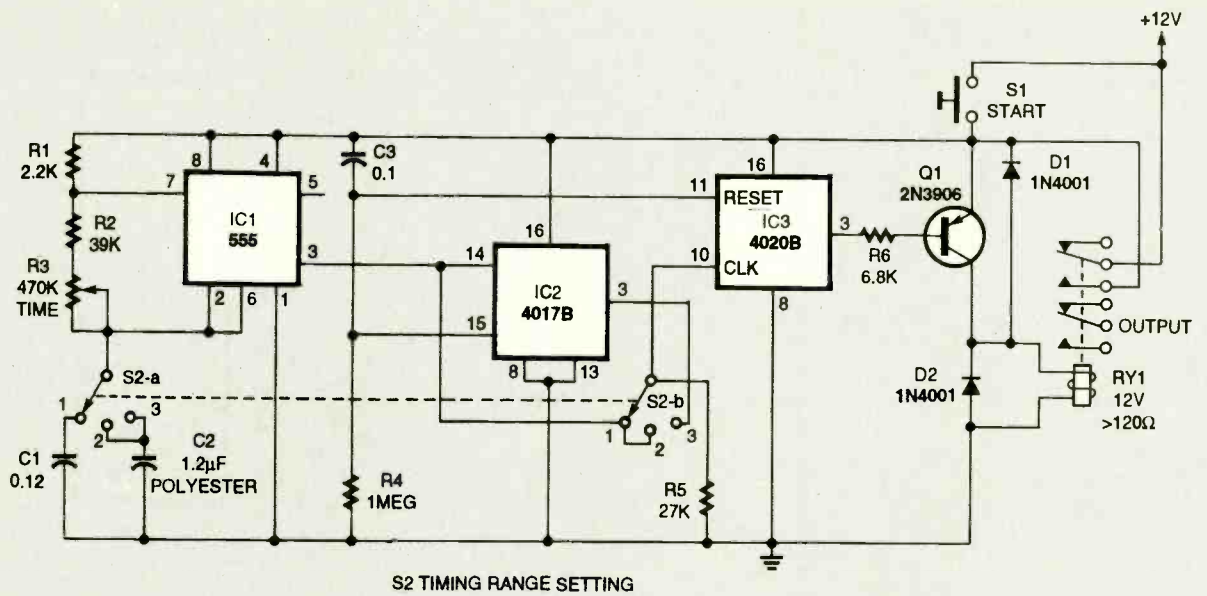


FIG. 16—CMOS 14-STAGE RIPPLE-CARRY binary counter CD4020B: functional diagram (a), and pinout diagram (b).

sponse is obtained by modifying the relay-driving stage for an NPN transistor.

It is worth noting that the circuits in Figs. 10 and 11 each provide a time delay of about 0.5 seconds for every microfarad in the value of capacitor C1. This permits delays of up to several minutes. If desired, the delay periods can be made variable by replacing resistor R2 with a fixed and a variable resistor in series whose nominal values are approximately equal to that of resistor R2.

Figure 12 shows how a pair of CMOS gates can form a push-button-activated one-shot multivibrator relay-switching circuit that provides delays up to several minutes with reasonable accuracy. The relay turns on as soon as START switch S1 is closed. However, it turns off



S2 TIMING RANGE SETTING

- NO. TIME  
 1) 1 TO 12 MIN  
 2) 10 MIN TO 2 HRS  
 3) 100 MIN TO 20 HRS

FIG. 17—WIDE-RANGE TIMER-RELAY switching circuit spans 1 minute to 20 hours in three ranges with a three-step, two-deck rotary switch.

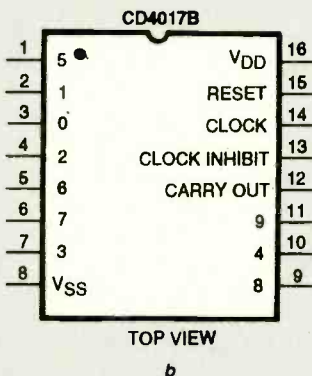
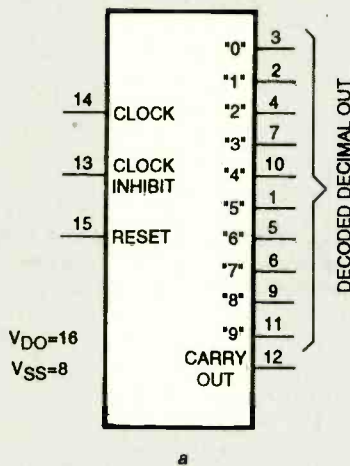


FIG. 18—CMOS FIVE-STAGE DECADE COUNTER CD4017B: functional diagram (a), and pinout diagram (b).

again automatically after a pre-set delay of about 0.5 seconds per microfarad of the value of capacitor C1. The two CMOS gates are configured as a manually-triggered monostable multivibrator whose output is fed to the relay through R4 and transistor Q1.

The circuits in Figs. 10 to 12 are all based on simple CMOS gates, and they are intended for applications where high timing accuracy is not required. Far greater timing accuracy can be obtained in circuits based on the 555-type timer IC. Figures 13 to 16 show four practical timer relay control circuits that include the 555 timer.

If you wish to learn more about how to apply the 555 timer IC (or brush up on what you do know), refer to previous articles in this series: page 58 of the September and page 69 of the October 1992 issues of *Electronics Now*.

Figure 13 is a circuit schematic for a simple 6 to 60 second timer-control circuit. The 555 IC is configured as a monostable multivibrator or a one-shot multivibrator. The circuit starts a timing cycle when START switch S1 is closed; relay RY1 is turned on immediately, and

electrolytic capacitor C1 starts to charge toward the positive power supply through 47-kilohm resistor R1 and 470-kilohm trimmer potentiometer R3.

The capacitor will continue to charge until, after a delay determined by the trimmer setting, C1 rises to two-thirds of the supply voltage. At that time, the IC1 changes state and the relay is turned off. The timing cycle is then complete.

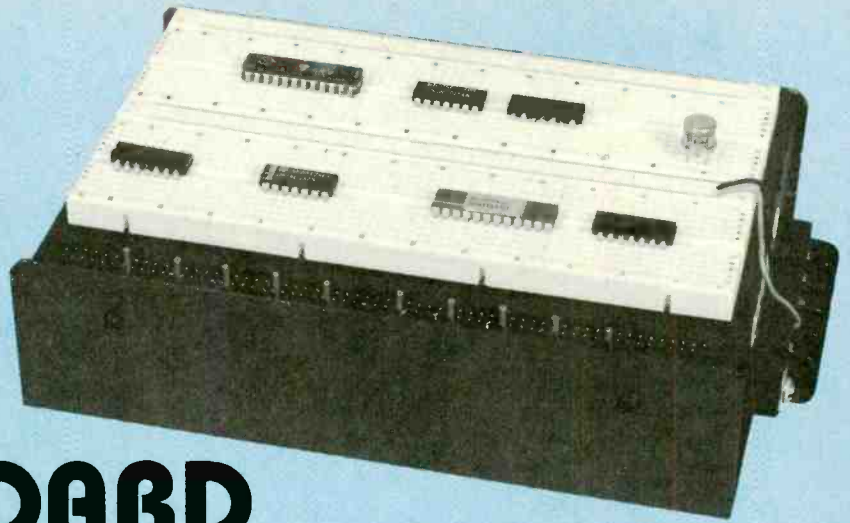
A shortcoming of the simple one-shot multivibrator relay control circuit in Fig. 13 is that it permanently draws current from the supply—even when the relay is off. Figure 14 is the schematic for a two-range timer circuit that overcomes this drawback. It is capable of timing over a range of 6 seconds to 10 minutes. The circuit operates as follows:

When START switch S1 is momentarily closed, a START pulse is sent to pin 2 of the IC1 through R3 and C3, and relay RY1 turns on. The control contacts then close, maintaining the power connections to the circuit when S1 is released. The circuit then runs through a timing cycle that is similar to the one described for Fig. 13. How-

Continued on page 90

**Putting last month's  
PC breadboard  
hardware to work.**

# BUILD THIS PC I/O BREADBOARD



**DAVE DAGE**

SOME PEOPLE MASTER HARDWARE, others master software—but few master both. Those who do, however, can expect great rewards. Last month's project was building the hardware: a PC interface card and a breadboard system with ten fully decoded and latched input/output (I/O) ports. This month's article is about the software required to make the hardware do something interesting. Along the way, you'll learn how to breadboard some hardware for demonstrating input and output capabilities, and you'll see software examples in three popular computer languages: BASIC, assembler, and C.

It will be helpful if you have had some experience with programming in at least one of those languages. But if not, don't worry—this presentation allows for inexperience. If you are just beginning to program, it's better to learn two—or more—languages at the same time. Most programming languages do the same things; learning several will help you place the statements and procedures of each in perspective.

## **Hardware setup**

To begin, breadboard the circuit shown in Fig. 1. The schematic specifies the resistor networks, a DIP switch, and LED bargraph indicator, but any discrete components that are elec-

trically equivalent can be substituted. Figure 2 shows how to mount the components on the breadboard.

The input circuit connects to port four, which appears at address 260 decimal (0104 hex) if you configured the interface card at the default base I/O port address. Resistors R2a–R2h pull all eight data lines low. By switching the poles of the DIP switch, you can pull each line high through resistors R3a–R3h.

The output circuit also connects to port four (260 decimal, 0104 hex). The output lines can drive each of the eight LEDs that are tied to ground through current-limiting resistors R1a–R1h. An LED will turn on when the associated data line goes high, and off when it is low.

Now let's see how to use the software to read the switches and light the lights. First I'll discuss the BASIC language, then assembler, and then C.

## **BASIC programming**

BASIC, as supplied with DOS, is an interpreted language. When you run a BASIC program, you are running the large BASIC.EXE program, which takes each statement one at a time, "interpreting" what it means, and then executing it.

As with any programming language, BASIC has advantages and disadvantages. BASIC's advantages include simple setup; most housekeep-

ing chores are handled for you automatically by the BASIC interpreter. In addition, testing and experimenting with BASIC is quick and easy because you can execute code in the immediate mode, rather than running "source code" through a program called a compiler.

BASIC also has disadvantages that include slow speed, awkward bit-level manipulation, and variables that are always global. An interpreted BASIC program is much slower than an equivalent compiled program in almost any other language. Bit-level manipulation can be troublesome for people who want to work directly with hardware. The problem with global variables is that simple typographical errors make it easy to create hard-to-debug problems, particularly in those large programs with lots of variables.

Despite those disadvantages, BASIC is ideal in situations where speed is not a requirement, the program is not large, and quick development and testing are paramount.

Listing 1 shows a simple BASIC program that will read the input port, transfer the data to the output port, and then repeat the process indefinitely. The overall effect of this program is that the switches directly control the LEDs. (Press Ctrl-Break when you've had enough.)

The objective of this program

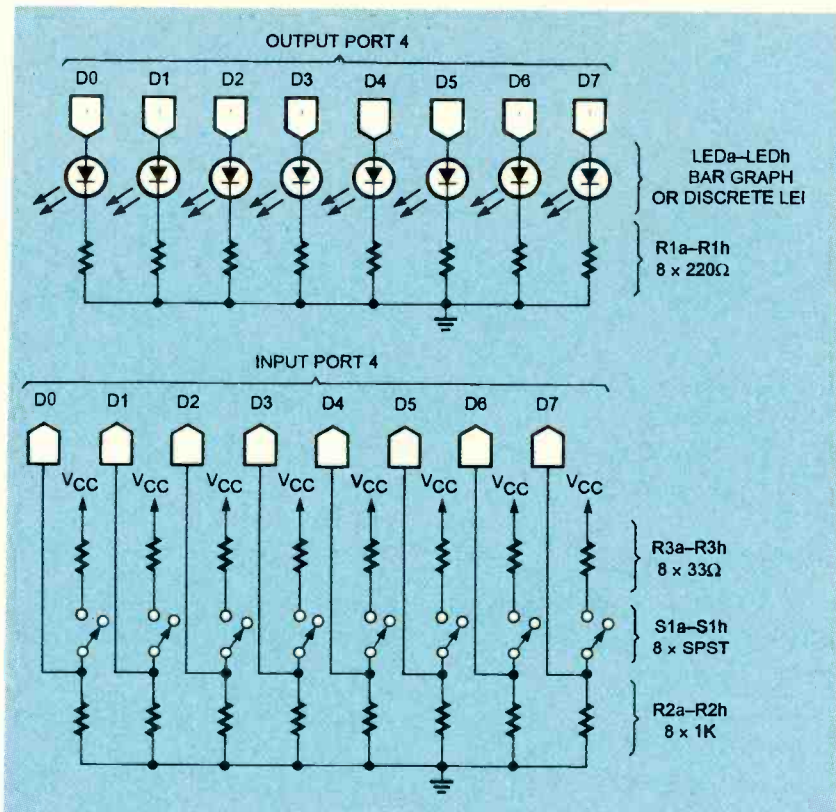


FIG. 1—SCHEMATIC DIAGRAM OF TEST CIRCUIT: The input port reads an eight-position DIP switch, and the output port drives an eight-LED bargraph.

is to show that the computer really controls the connection between the two ports. You could write a program that would switch a light on or off only after a password has been entered. Similarly, you could write a program so that the switch that controls a particular LED could be changed to control a completely different LED without rewiring the board. Try doing something like that without using software—it's next to impossible!

Another possibility would be to assign the input and output ports for completely separate purposes. For example, the DIP switch could serve as eight additional function keys for a special program, and the LEDs could function as a bargraph displaying, for example, the time remaining in some particular process.

Of course, it's also possible to have some fun with the circuit. Listing 2 provides one example. (Depending on the speed of your computer, you might have to adjust the value of the time delay in line 190.)

### Assembly language programming

If BASIC represents one end of the programming-language spectrum, assembler or assembly language represents the other. Where BASIC is slow and cumbersome, assembler is quick and lithe. On the other hand, it's easy to perform tests and do experiments in BASIC,

#### LISTING 1—SIMPLE TEST PROGRAM

```
10 N = INP (260)
20 OUT 260, N
30 GOTO 10
```

#### LISTING 2—LEDSWING.BAS

```
100 REM * for ST-1. Purpose: walk a single bit back and forth for display on
110 REM * a LED bar indicator. Hardware: LED bar indicator, limit resistors.
120 REM * Note: TON (line 180) is loop delay, increase for faster cmprts.
130 REM *
140 REM * AO address output port, TON time LED is on, TOFF time LED is off.
150 REM *
160 CLS:REM START
170 INPUT " Enter output port address in decimal ";AO
180 TON=500 : REM increase to slow cycling. Try 500 to 5000.
190 FOR C=1 TO 7
200 OUT AO,2^C: FOR T=1 TO TON:NEXT T
210 NEXT C
220 FOR C=6 TO 0 STEP -1
230 OUT AO,2^C: FOR T=1 TO TON:NEXT T
240 NEXT C
250 GOTO 190
```

but assembler requires careful forethought in planning those tasks. However, it's easy to control the hardware in assembler.

Every microprocessor has its own assembly language. Intel's 80X86 family has one, Motorola's 68XXX family has another, and so on. Moreover, within a given microprocessor family, successive additions to the family usually call for new instructions specific to that more advanced device.

Some microprocessors have a single address space that is occupied by both system random-access memory (RAM) and I/O ports. Other CPUs have separate locations for memory and I/O. Intel CPUs, for example, have separate memory and I/O locations. In this architecture, the CPU and I/O devices share common address and data buses; separate CPU control signals determine whether a given operation occurs in an address space or an I/O space.

In the 80X86 microprocessor family, different instructions allow the transfer of one, two, or four bytes of data simultaneously between an I/O port and the CPU's accumulator, or A register. The CPU can specify which port participates in a transfer in several ways. In assembly language, the port can be selected by an *immediate value*, which is actually part of the instruction the CPU executes. Another way to select a port is to preload the DX register with the address of the desired port, and then execute a slightly different instruction.

Figure 3 shows the register model for the 8086 CPU. Later members of the Intel family ex-

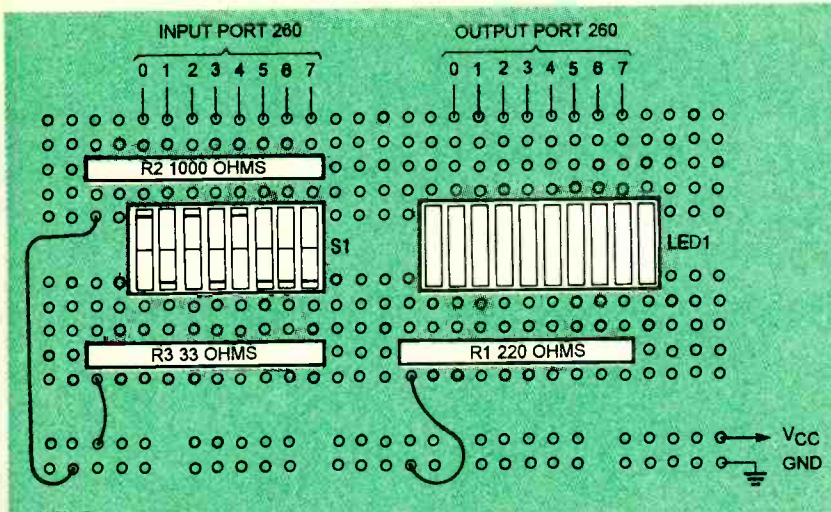


FIG. 2—PARTS PLACEMENT DIAGRAM for the test circuit. Parts placement is not critical; just be sure the power-supply polarity is not reversed.

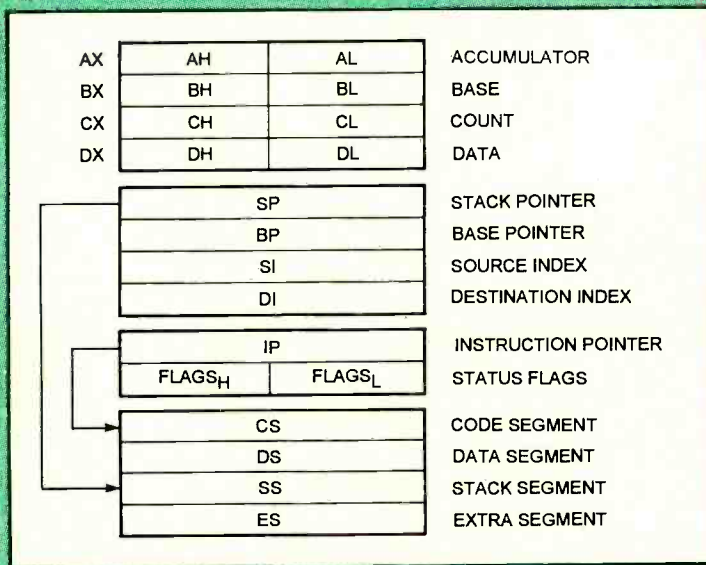


FIG. 3—INTEL MICROPROCESSOR REGISTER MODEL shows the 16-bit register format common to the 8088, 8086, 80186, and 80286 CPUs. The 386 and higher-level CPUs have 32-bit wide registers.

tend the architecture of the model, but all are backward compatible with it. Note that the main registers (AX, BX, CX, and DX) are 16 bits wide, but they can be addressed in 8-bit blocks: AL and AH (A low and A high), and so on. The 80386 and more powerful CPUs extend the concept to the 32-bit level.

The number of bits that can be transferred to or from an I/O port simultaneously depends on the CPU's capability, and on the interface hardware. This project's interface card works at the byte level, so only eight bits can be transferred at a time,

through the lower half of the accumulator, designated AL.

The assembly-language instructions for reading and writing a port specified by the DX register are, respectively, IN AL, DX and OUT DX, AL. Those instructions assemble to hexadecimal machine-code values EC and EE, respectively. At this time you should know how to build an assembly-language version of our earlier BASIC test program. See Listing 3.

The only difference between the BASIC program and the assembly program is that the as-

sembly program must preload the DX register with the desired hexadecimal port address. In Listing 3, the first instruction moves port address 0104h into the DX register. The second instruction transfers the data byte from the I/O port specified by DX into register AL. Then the CPU writes this same value back out to the same I/O port. Last, the program jumps back to line 2 to continue to the process indefinitely. Instead of using a GOTO statement with a line number, an assembly-language program uses labels such as "loop1" in the example.

To enter and execute an assembly-language program, you will need a program that can translate the assembler statements into machine code. This kind of program is called an assembler. A full-featured assembler such as MASM (Microsoft), TASM (Borland), or A86 (a shareware product by Eric Isaacson) will assign addresses to labels, keep track of data by name, and much more. However, for simple test programs, those programs are more comprehensive than necessary. For the purposes of this project, the DOS program DEBUG.COM will suffice.

### Debug

A version of DEBUG is packaged with every copy of DOS. Unfortunately, it's one of the most user-unfriendly programs ever written. To make things easy on yourself, set up a separate directory (or use a separate floppy disk) just for DEBUG and the assembly programs that you will write. DEBUG is normally installed in your DOS directory, so you should be able to run it directly from your test directory.

Now execute the program. You should see its prompt, a simple hyphen. Press "A" followed by Enter. This puts DEBUG into its Assemble mode.

### LISTING 3— ASSEMBLER TEST PROGRAM

```

mov dx, 104
loop1: in al, dx
out dx, al
jmp loop1

```

The program will display eight hexadecimal digits, divided into two groups of four separated by a colon. The value on the left is called the segment address, and the value on the right is called the offset address. The segment address, shown here as "xxxx" might vary from machine to machine; for small programs, its value doesn't matter. To determine the actual address associated with a segment:offset pair, multiply the segment by 16 (10 hex) and then add the offset. For example, hex address 2345:0006 = 23450 + 0006 = 23456.

The offset address, on the other hand, is critical. If you don't deliberately specify a value, DEBUG begins assembly at location 0100h (256 decimal). DOS allocates the first 256-byte block of memory within a given segment to store information about small COM programs of the kind being developed here. That block is a historical remnant from an earlier programming language, CP/M; it's officially called the PSP or Program Segment Prefix. Leave the PSP alone; don't try to place code or data there. (By the way, DOS's EXE file format does not use the PSP. In addition, COM programs are limited to 64K of code space, whereas EXE programs can be much larger.)

Intel CPUs have a set of registers called *segment registers*: code segment (CS), data segment (DS), stack segment (SS), and extra segment (ES). The segment registers typically function as indexes into various areas of memory. By default, DEBUG loads the current segment address into each of those registers.

Notice that the stack pointer (SP) is initialized at offset FFFE, and the instruction pointer (IP, also called the *program counter*) is set to offset 0100.

You now have a 64K block of memory ready for the entry of programs. Enter the code shown in Listing 4 at the DEBUG prompt.

Unfortunately, you cannot use symbolic addresses (e.g., the loop1 in the previous example) with DEBUG; you must enter

the actual CPU offset address. That's why you see jmp 0103 at offset 0105. After entering the final instruction, press Enter again, and you'll return to the DEBUG prompt.

Before running the program, save it. First name the program with DEBUG's "n" command:

#### LISTING 4—DEBUG PROGRAM SW2LED

```
-a100 <Enter>
xxxx:0100 mov dx, 104 <Enter>
xxxx:0103 in al, dx <Enter>
xxxx:0104 out dx, al <Enter>
xxxx:0105 jmp 0103 <Enter>
xxxx:0107 <Enter>
-
```

#### LISTING 5—DEBUG PROGRAM SW2LED2

```
mov dx, 104
loop1: in al, dx
out dx, al
shl al
jnc loop1
mov ah, 0
int 21
```

#### LISTING 6—C LANGUAGE PROGRAM

```
#include <conio.h>
main()
{
    int inp(unsigned), outp(unsigned, int);
    while(1)
    {
        outp(200, inp(260));
        _sleep(2);
        _asm int 21;
    }
}
```

-n SW2LED.COM <enter>  
Drive and path are optional, but for this project unnecessary, because the default directory has been specifically set aside for our test programs.

DEBUG's "w" command writes current memory contents to disk. However, you must specify the exact number of bytes in two registers: BX and CX. For anything less than 64 Kbytes, BX will contain zero and CX the remainder. The test program is only seven bytes long. So enter 0000 and 0007 into registers BX and CX as follows:

```
-r cx <enter>
CX 0000
:7 <enter>
-r bx <enter>
BX 0000
:<enter>
-
```

After you enter the first line ("r cx"), DEBUG displays the current value of CX and presents a colon (:) prompt. Enter 7 followed by Enter. Repeat the process with BX. To accept the currently displayed value, just press Enter.

The next step is to write the file to disk. Press "w" followed by Enter. Debug will respond with the number of bytes it is writing. Verify that the value displayed is correct:

```
-w <enter>
Writing 00007 bytes
```

Be certain the value is correct before proceeding—you'll see why in a moment. Now run the program by entering "g" (go) at the prompt. The hardware should respond just as it did with the BASIC program; cycling the DIP switch positions will cycle the corresponding LEDs.

There are, however, two major differences between the BASIC and the assembly program. The assembly program runs much faster, and pressing Ctrl-Break does not halt the program. With mechanical switches, the speed difference is insignificant, but if you are not able to stop the program and regain control, the only thing to do is reboot.

Now return to the test directory, load DEBUG, and reload the test program. Loading a file is a step that is opposite to writing it: first name it using "n," then load it using "l:"

```
-n SW2LED.COM <enter>
-l <enter>
```

How will you know that the correct program loaded? Try the unassemble command, "u." The assemble command used previously converts assembly-language instructions into hexadecimal bytes that are executed by the CPU, the unassemble command (sometimes called the *disassemble command*) converts hex bytes into assembly-language instructions that can be understood by people. Issue the following command to disassemble the test program:

```
-u 100 L7 <enter>
```

The "u" stands for unassemble, 100 is the starting address, and L7 instructs the program to

disassemble seven bytes beginning at that address.

DEBUG should display a list of program instructions identical to that in Listing 4.

### Graceful ending

For the final assembly-language exercise, the program is made a little more "intelligent." The program can be allowed to end gracefully, so you don't have to reset the computer to halt the program. One way of doing it is to use DIP switch position 8 as a "break" key. After each pass through the read-switches, write-LEDs loop, check switch 8. If it's on, end the program; otherwise continue.

The shift instruction provides a simple way to do this in assembly language. You will shift bit 8 out of the accumulator and into a special register called the *carry flag*. As its name implies, the carry flag is normally used for arithmetic instructions. But it's also useful for determining the flow of a program based on the state of some condition—for example, the on or off state of a DIP switch.

Listing 5 shows how all these instructions tie together. As before, preload DX with 0104h, input the byte from the port at that address, then write it back out. Now for a surprise. The "shl al" instruction causes the CPU to shift the contents of its AL register left one bit position, moving the most-significant bit into the carry flag. The following instruction tells the CPU to jump back to the input instruction (at address loop1) if the carry bit is not set—i.e., if the switch is off. If this is not done, the program executes a special pair of instructions that will return control to the calling program.

Following the procedure previously outlined, enter the program in DEBUG, and save it to disk with a new name (SW2LED2.COM). Remember that you must enter the address of loop1 with the hex address, not the symbolic constant. Other than that, the program's operation is straightforward.

With this introduction, you

should be able to read the documentation for DEBUG and learn how to use the rest of its commands. Although cryptic, DEBUG is a powerful tool for writing and debugging new programs and for exploring your computer system and its configuration. You might want to record all of the commands and parameters on a handy card for future reference.

The following information related to the speed difference between the assembler and BASIC versions of this program is interesting. On a standard 4.77-MHz PC, the BASIC program loop executes in about 2.25 milliseconds. By contrast, the assembler version takes about 9 microseconds. In other words, the assembly-language program ran about 250 times faster than the BASIC program!

### GLOSSARY OF TERMS

**Assembler**—A computer program that converts or translates assembly language source code instructions into machine language.

**Compiler**—A computer program or circuitry that translates a high-level language into an executable program in a single operation. See *assembler* and *interpreter*.

**Global variable**—A variable in a computer program that can be shared by any object or subroutine within the program.

**High-level language**—An application-oriented programming language, as distinguished from a machine-oriented programming language. It is also termed a *computer language*. Examples are BASIC and C.

**Interpreter**—A computer executive routine that translates a program in high-level language or code into machine language or code. Unlike a compiler, the interpreter translates and executes one line at a time. See *assembler* and *compiler*.

**Machine code**—Instructions executed by a computer processor. It is also called *machine language*.

**Machine instruction**—An instruction written in a programming language that a computer can recognize and understand without translation.

**Register**—A circuit in computers or other digital circuitry that holds data in binary format for process or transfer.

**Source language**—The language in which a problem is programmed for a computer. It must be translated into an object program in machine language by an assembler, compiler, or interpreter.

**Source program**—A program that is written in source language or code.

### C language programming

Earlier BASIC and assembler were defined as opposite ends of the programming-language spectrum. A broad range of other languages occupy positions all along that speed-performance spectrum. For example, C language has gained tremendous popularity during the past decade. Like BASIC, it is a high-level language, but it is really closer in many of its characteristics to assembly language. Indeed, C has been described as a "portable assembly language."

C is a compiled language like FORTRAN, COBOL, Pascal, and even some versions of BASIC. You start by writing source code that is similar to BASIC. However, C has no interpreter that runs it one line at a time. Instead, the source code is compiled into machine language that the CPU executes directly. As part of the compilation process, the compiler flags syntax errors (e.g., typos, undeclared variables, and misspelled language elements), that must be corrected before the machine code will be generated. Next, you have the option of linking the machine code with other predefined code libraries. When the process is complete, you will have a stand-alone file that will run from the DOS prompt.

Modern C development environments combine all the tools necessary for editing, compiling, and linking C code into a single, *integrated development environment* (IDE). The preeminent products in this category include Borland's Turbo C and Microsoft's Quick C. For entry-level programmers, an IDE is recommended. Even experienced programmers can significantly increase their programming productivity with an IDE.

Both Quick C and Turbo C include a special feature called *inline assembly*, which allows you to embed assembly-language programming instructions in the middle of a C program. Inline assembly thus gives you the best of both worlds: the low-level hardware

*Continued on page 89*

FOR AS LONG AS SHORTWAVE LISTENING has been popular, it has been difficult to match a random-length antenna to the typical 50- or 75-ohm input impedance of most radio receivers. The impedance of a random-length shortwave antenna can vary from a few ohms to several hundred ohms, depending

on frequency. Matching that impedance to the input impedance of a receiver is possible, but it can be complicated.

Many different active-antenna designs provide effective matching, but many people believe that active antennas never work satisfactorily. An active antenna is typically a single-stage, wideband amplifier with a gain from 5 to 8 dB and a noise figure from 3 to 8 dB, making it a device of questionable merits. While active antennas provide some gain, they can also add noise to the signal, especially a signal at a low microvolt level.

# TUNABLE SHORTWAVE ANTENNA

*Improve your shortwave reception with this tunable antenna.*

H.J. WECKE

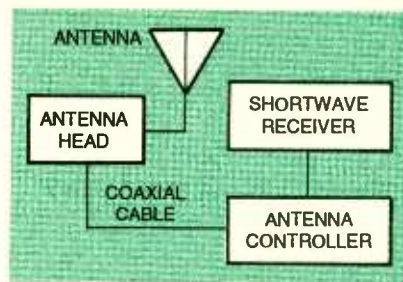
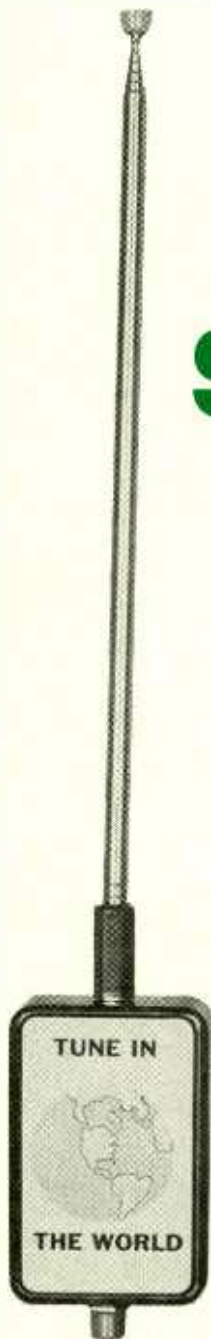


FIG. 1—THE TUNABLE SHORTWAVE antenna adds a tuned stage ahead of the 50- or 75-ohm input to your shortwave receiver.

Active antenna wideband amplifiers really lose out in the low microvolt region. The inherent noise usually kills a low-level incoming signal. Nearby transmitters might cause intermodulation in the active antennas as well. As a compromise solution, some older shortwave receivers had trimmer potentiometers on their front panels to provide impedance matches for the antenna at the received frequency. Sadly, modern receivers no longer have this control.

The author believed that a new method had to be designed to meet the following list of provisions:

- 1—No amplification should be needed, no noise should be generated, and no intermodulation should occur
- 2—It should have selectivity, but keep out strong adjacent signals
- 3—It should be small
- 4—It should be inexpensive, easy to build, and include only standard components

The solution was found by adding a tuned stage in front of the 50- or 75-ohm input to the shortwave receiver. A tuned stage has many advantages over the best wideband RF amplifiers, including preselection at resonance and elimination of both noise and intermodulation. The need for tracking the antenna from band to band is the only disadvantage this tuned stage has over a wideband active antenna. Several prototype antennas have been in service reliably for more than four years. They have been mounted on a balcony or a roof where they were exposed to a harsh climate. Figure 1 is a block diagram of the system.



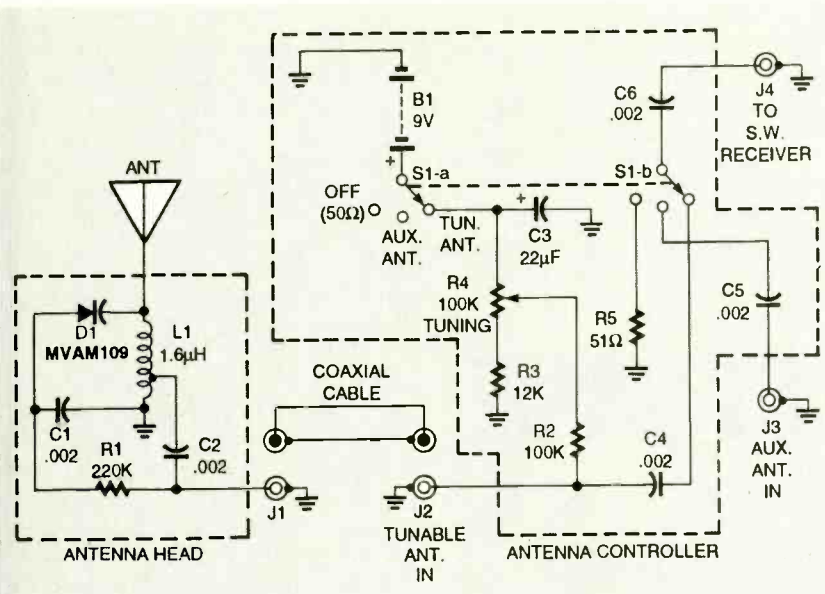


FIG. 2—TUNABLE ANTENNA SCHEMATIC. The variable element is Motorola MVAM-109 diode D1.

### Circuitry

Figure 2 is the schematic for the tunable antenna system. A single monopole antenna about 3 feet long was chosen. The antenna, which has a measured capacitance of approximately 10 picofarads, becomes part of the antenna-head circuit that feeds the antenna controller. The variable element of the antenna head is a Motorola MVAM-109 diode (D1). The inductor value required to cover the shortwave spectrum from about 6 MHz to 18 MHz was calculated to be 1.6 microhenries. The inductor can easily be wound by hand on a 0.25-inch diameter ferrite slug.

The MVAM-109 requires a tuning voltage from 1 to 9 volts DC at a low current. That is provided by 100-kilohm linear potentiometer R4 located in the antenna controller section. Switch S1, when in the "off" position, places a 50-ohm termination on the tuned output. The other two positions of S1 select either an auxiliary antenna input or the tuned antenna input. A length of coaxial cable terminated with suitable connectors connects the antenna head, which might be located outdoors, to the antenna controller, which should be located in a convenient place near your shortwave receiver.

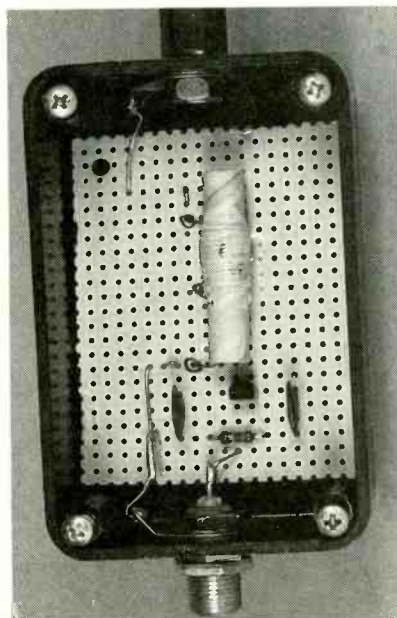


FIG. 3—THE ANTENNA SHOULD be mounted to the antenna-head case with a neoprene washer, and a bead of silicone sealant should be applied to the edge of the lid to keep out water.



FIG. 4—ANTENNA CONTROLLER unit. House the controller in a metal case to provide RFI shielding.

### PARTS LIST

All resistors are 1/4-watt, 10%, unless otherwise noted

- R1—220,000 ohms, 10%
- R2—100,000 ohms, 10%
- R3—12,000 ohms, 10%
- R4—100,000 ohms, linear potentiometer
- R5—51 ohms, 10%

#### Capacitors

- C1, C2, C4—C6—0.002 µF, ceramic
- C3—22 µF, 16 volts, electrolytic

#### Semiconductors

- D1—Motorola MVAM-109 varactor diode (nominal capacitance of 460 pF at  $V_R = 1.0$  V and  $f = 1.0$  MHz) or equivalent

#### Other components

- L1—1.6 µH (wind by hand, see text)
- J1, J2—panel-mount F connector
- J3, J4—any coaxial connectors suited to your needs

B1—9-volt carbon-zinc battery (do not use alkaline)

S1—2-pole, 3-position rotary switch (optional, see text)

Miscellaneous: Antenna, two cases, silicone sealer, coaxial cable, No. 26 magnet wire, 1/4-inch form with ferrite slug, 9-volt battery snap connector

Note: The following items are available from Wecke Associates, P.O. Box 3822, Ottawa, Canada K1Y 4M5:

- A kit consisting of D1, L1, and 6 mm bolt, nut, and solder lug to accommodate a 30-inch automotive whip antenna—\$6.00 + \$2.00 S&H
- Assembled and tested antenna controller, antenna head, and aluminum mounting bracket with U-bolts and battery (does not include whip antenna or connecting cables)—\$65.00 + \$5.00 S&H

Payment required in US dollars. Canadian customers please add appropriate provincial taxes. Allow 3-4 weeks for delivery.

### Construction

The antenna head can be hand wired on perforated construction board and installed in any weathertight case. Good, clean solder joints are important in the antenna head, which will probably be exposed to the weather. The layout of the parts and wiring is not critical—just avoid excessive lead lengths. The case selected for the prototype antenna head has an aluminum cover that can be used as a base for attaching a mounting bracket crafted from scrap aluminum. Coil L1 can be made by winding 16 turns of No. 26 magnet wire on a 1/4-inch diame-

Continued on page 90

ALTHOUGH PLAYING COMPUTER games can be a lot of fun, operating them teaches you very little about how they work. A good way to learn how electronic games work is to build your own. This article shows you how to build the C-Game, a two-

comfortable to use. A piezoelectric buzzer provides game sound effects.

### Features

The games and functions of the C-Game are selected by pressing one of the 16 pushbuttons after the device is reset. A new game can be selected at any

such as and, or, and exclusive-or. Finally, four non-game modes create sound effects and light-pattern displays.

### Circuitry

Figure 1 is the schematic of the C-Game. The circuit is designed around IC3, an 80C31 ROMless, CMOS version of Intel's 8051 8-bit microcontroller. The 80C31 has four 8-bit I/O ports (0 to 3).

Port 1 is connected to 16 pushbuttons, organized as two banks of eight (Bank-A and Bank-B). The 16 1N914 diodes (D1-D16) isolate each bank from the other. Each bank has one side of each pushbutton connected in common to one pin of Port 3 of the 80C31. These two pins (12 and 13, P3-2 and P3-3, respectively) enable the switch banks separately so that they can be periodically read under software control.

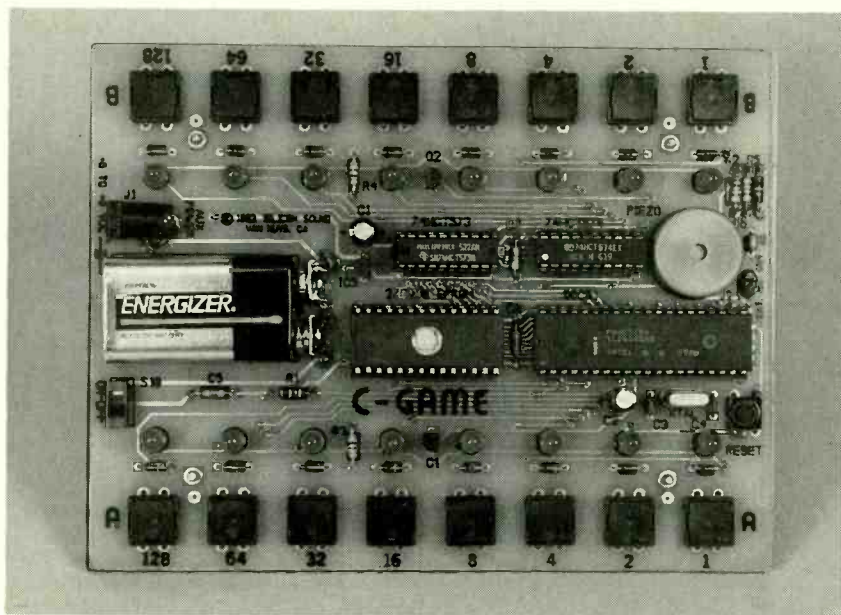
Port 0 of the microcontroller communicates with the 27C256 EPROM (IC1), where C-Game's software is stored. The address and data buses of the microcontroller are multiplexed. A 74HCT573 8-bit latch (IC2) is first strobed with the ALE (address latch enable) signal from the microcontroller, and the low-order address data is latched for the EPROM. The high-order address for the EPROM is output by port 2, pins 21 to 27. The EPROM is enabled by the microcontroller's PSEN (program store enable) line.

Port 0 also connects to IC4, a 74HCT574 8 bit D-type flip-flop that drives two banks of eight LEDs. Port 3 (P3-0 and P3-1) enables each bank separately through Q1 and Q2. Each bank is multiplexed under software control and is turned on approximately 50% of the time.

Port 3 bit-4 (pin 14) connects to a transducer. Components R5, R6, and C8 provide a signal through output jack J2 for connection to the line-level input of an external amplifier to produce a louder sound output.

At power up, C2 and R1 initialize the microcontroller. Reset switch S17 will reset the circuit to power-up conditions at any time. An oscillator is

# BUILD THIS COMPUTERIZED GAME



**Learn how electronic games work; then have fun playing one that you built.**

DAN RETZINGER

player game with a dozen different game modes. In addition to the 12 games, there are four other modes that let you generate sound effects and light-pattern displays.

The C-Game has 16 pushbuttons for player input, and it has 16 LEDs for display output. Eight LEDs and pushbuttons are arranged along each side of the device, making it convenient for two players to sit opposite each other while playing a game. The pushbuttons are installed with the same spacing as found on a standard computer keyboard, which makes them

time by pressing the reset switch followed by another pushbutton. Once a game is selected, the operation of all pushbuttons and LEDs are specific to that game.

Of the twelve games, three are reaction-time (who's quickest) competitions. Four games involve skill and thought, and two others are simple memory challenges. The C-Game also has two binary arithmetic contests in which you must add, subtract, divide, and multiply two binary numbers. (It's not as difficult as it sounds!) Another game performs logic functions

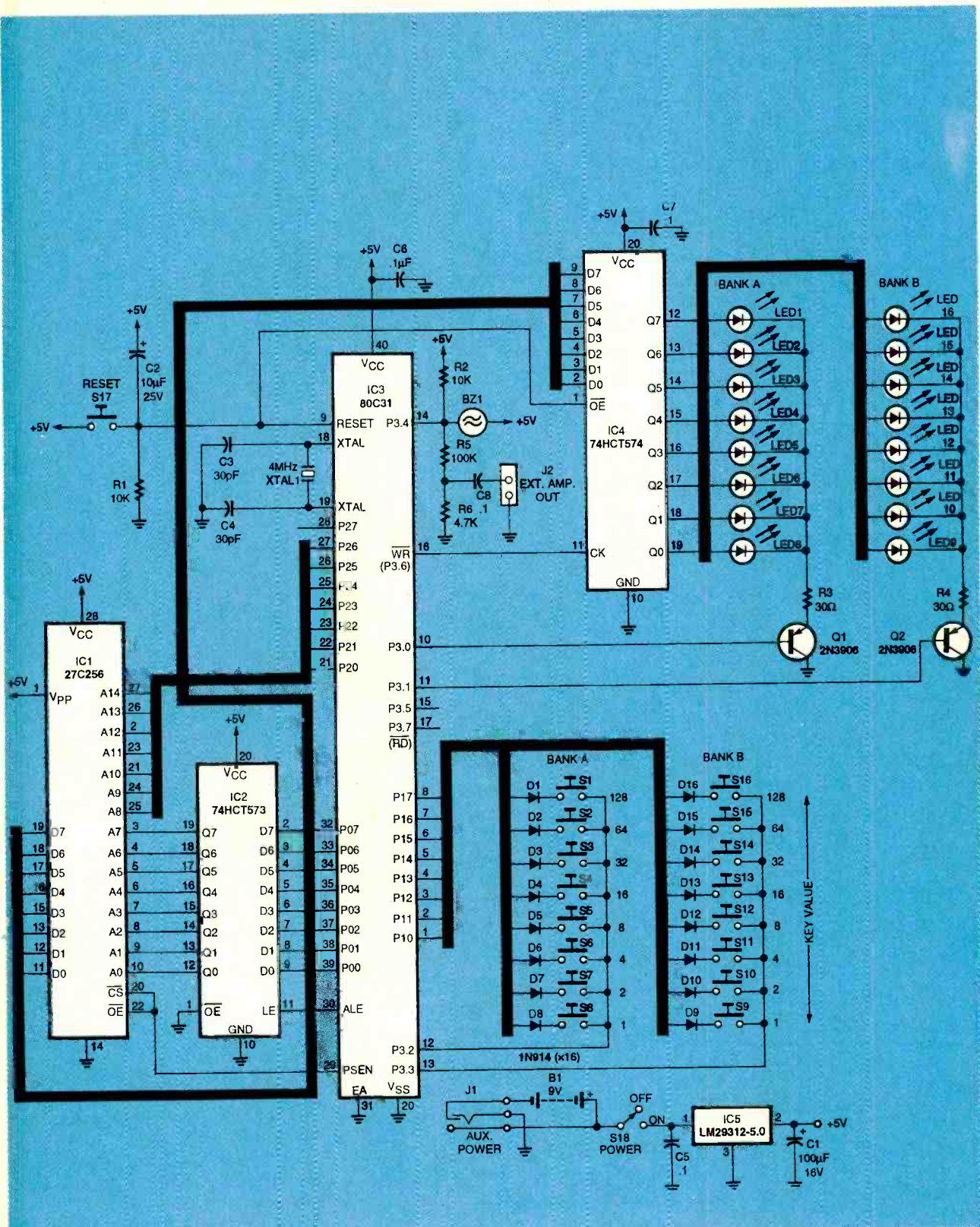
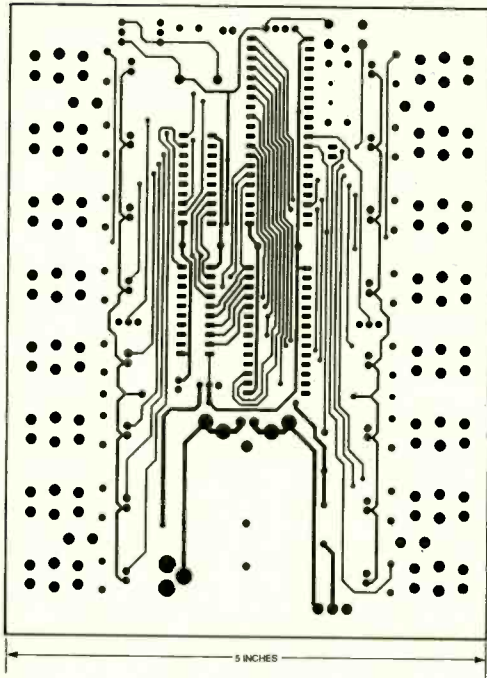


FIG. 1—C-GAME SCHEMATIC. The circuit is designed around an Intel 80C31 8-bit microcontroller.

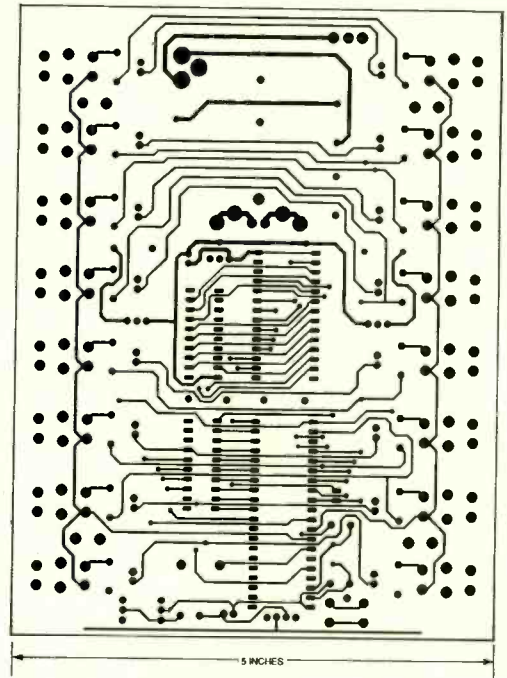
made up of a 4-MHz crystal (XTAL1) and two 30 pF capacitors (C3 and C4). An LM2931Z-5.0 low-dropout 5-

volt regulator IC5 will tolerate a reversed battery voltage of 15 volts without damage. The circuit is normally powered from a

9-volt battery, but power-input jack J1 can provide auxiliary power to the C-Game with any power adapter capable of supplying 6 to 9 volts DC at 100 milliamperes or greater.



COMPONENT SIDE OF THE PC BOARD.



SOLDER SIDE OF THE PC BOARD.

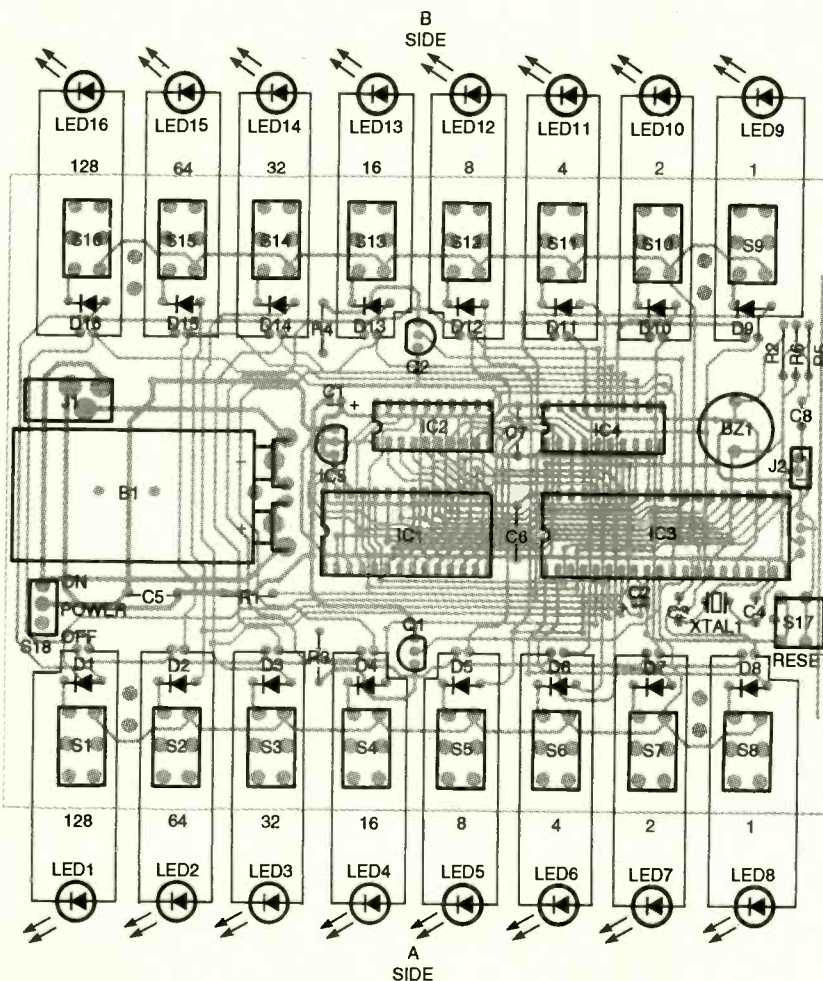


FIG. 2—PARTS-PLACEMENT DIAGRAM. Solder the 1N914 diodes first, then the resistors and capacitors.

Designing a battery-powered circuit with this many LEDs and components requires some special considerations. All ICs (except the regulator) are CMOS to conserve battery power—a non-CMOS 74LS574 would require approximately 27 milliamperes more current than the CMOS version, and the non-CMOS version of the 8031 microcontroller would need almost 100 milliamperes extra.

Second, the 80C31 is clocked by a 4-MHz crystal. Although most 80C31 controllers can operate at speeds up to 12-MHz, the lower speed keeps power consumption to a minimum. Current drain is directly related to the clock speed in this CMOS microcontroller.

Third, all LEDs in each bank share one common-cathode resistor (R3 for Bank-A and R4 for Bank-B), instead of one resistor per LED. That results in less current per LED if many LEDs are turned on, and more current per LED if fewer LEDs are turned on. When only one or two LEDs are on, current is limited by the 74HCT574. When more LEDs turn on, current is limited by R3 and R4. However, the change in brightness is barely noticeable with a differing numbers of LEDs on.

Activation Key

2 Player Game

1 Player Game

Game Title

TABLE 1—GAME INSTRUCTIONS

Score Displayed &amp; End

Activation Key	2 Player Game	1 Player Game	Game Title	Instructions	Score Displayed & End
A1	X		Who's Quickest #1	First player to press the key next to his lit LED gets a Point. Most points out of 20 wins.	X
A2	X		Road Kill	Most 'hits' (press key while LED on) out of 20 wins.	X
A4	X		Tennis	Press a key to send a ball (LED) to your opponent. Fewest misses (press key before time-out) out of 40 wins.	X
A8		X	Reaction Timer	Test your reflex time. Press a key to shut off the LED. Gives an average time for 10 hits.	X
A16	X		Race Around	"A" player sends LED counterclockwise, "B" player clockwise. If LED slips past you, other player gets a point.	X
A32		X	Binary Math	Use "A128" to enter your answer for add/sub/divide/multiply on two 14 bit binary numbers. "B" LED's show progress.	
A64		X	Binary Logic	Use key "A128" to enter your answer for and/or/xor/modulus on two 4 bit binary numbers. "B" LED's show progress.	
A128		X	Count to 64	Use key "A128" to repeatedly add original number shown until you've counted to 64 or greater. "B" side keeps your time.	X
B1	X		Who's Quickest #2	First player to press all lit keys gets a point. Best out of 20.	X
B2		X	Memory #1	A number will be shown. Use key "A128" to enter each number in the "sequence" correctly. 10 total in sequence.	
B4	X		Memory #2	Alternate play. Two players build and copy a sequence. 10 total.	
B8	X		Last Player Wins	Move lit LED (press a key) toward A1, then toward B128 any number of "jumps". Alternate play. Last player able to move wins. Score is accumulative game to game.	X
B16			Special Effects	Press any key or key combinations to generate steady tones.	
B32			" "	"A" key control pitch range, "B" keys control speed range of randomly appearing LED's and tones.	
B64			" "	Sixteen different sound effects, one per key.	
B128			" "	Sixteen different sound and LED patterns, one per key.	

NOTE 1: Press RESET, then any key (left side of chart) to start a game.  
NOTE 2: After a game terminates, pressing the key (other than RESET) will restart same game.

## PARTS LIST

## All resistors are 1/4-watt, 5%.

R1, R2—10,000 ohms  
R3, R4—30 ohms  
R5—100,000 ohms  
R6—4700 ohms

## Capacitors

C1—100  $\mu$ F, 16 volts, radial electrolytic  
C2—10  $\mu$ F, 25 volts, radial electrolytic  
C3, C4—30 pF, 25 volts, ceramic disc, 20%  
C5-C7—0.1  $\mu$ F, 50 volts, ceramic, axial, 20%  
C8—0.1  $\mu$ F, 50 volts, ceramic, radial, 20%

## Semiconductors

IC1—27C256 CMOS EPROM  
IC2—74HCT573 octal D-type CMOS latch  
IC3—80C31 CMOS microcontroller

IC4—74HCT574 octal D-type CMOS flip-flop

IC5—LM2931Z-5.0 low-dropout 5-volt regulator

D1-D16—1N914 diode

LED1-LED16—green light-emitting diode

Q1, Q2—2N3906, PNP transistor

## Other components

S1—S17—PC-mount pushbutton switch

S18—SPST PC-mount slide switch

J1—DC power jack, PC mount, 2.0mm pin

J2—2-pin molex header, 0.1-inch spacing

XTAL1—4-MHz crystal, HC-18 metal case

B1—9-volt alkaline battery

BZ1—piezo-alarm (murata-erie No. PKM22EPP-40)

**Miscellaneous:** PC board, 9 volt battery connectors (1 each, Keystone No. 593 and No. 594), six stick-on rubber feet, two 20-pin IC sockets, one 28-pin socket, and one 40-pin socket

**Note: The following items are available from Silicon Sound, PO Box 1694, Reseda, CA 91337-1694 (818) 996-5073:**

• Double-sided, silk screened PC board—\$35.00

• Programmed 27C256 EPROM—\$15.00

• Complete C-Game kit including all parts—\$79.00

• Assembled and tested C-Game—\$99.00

Please add \$3.50 for shipping and handling. California residents add 8.25% sales tax.

The circuit draws an average of 20 to 30 milliamperes, with a maximum drain of 65 milliamperes with all LEDs on. A 9-volt alkaline battery will last an aver-

age of 8 to 10 hours and a nickel-cadmium battery will last from 5 to 8 hours. Avoid 9-volt carbon batteries; even a fresh one can't deliver the C-Game's peak cur-

rent requirements. Supplying power through jack J1 eliminates the need for a battery. This is recommended if the game is played often.

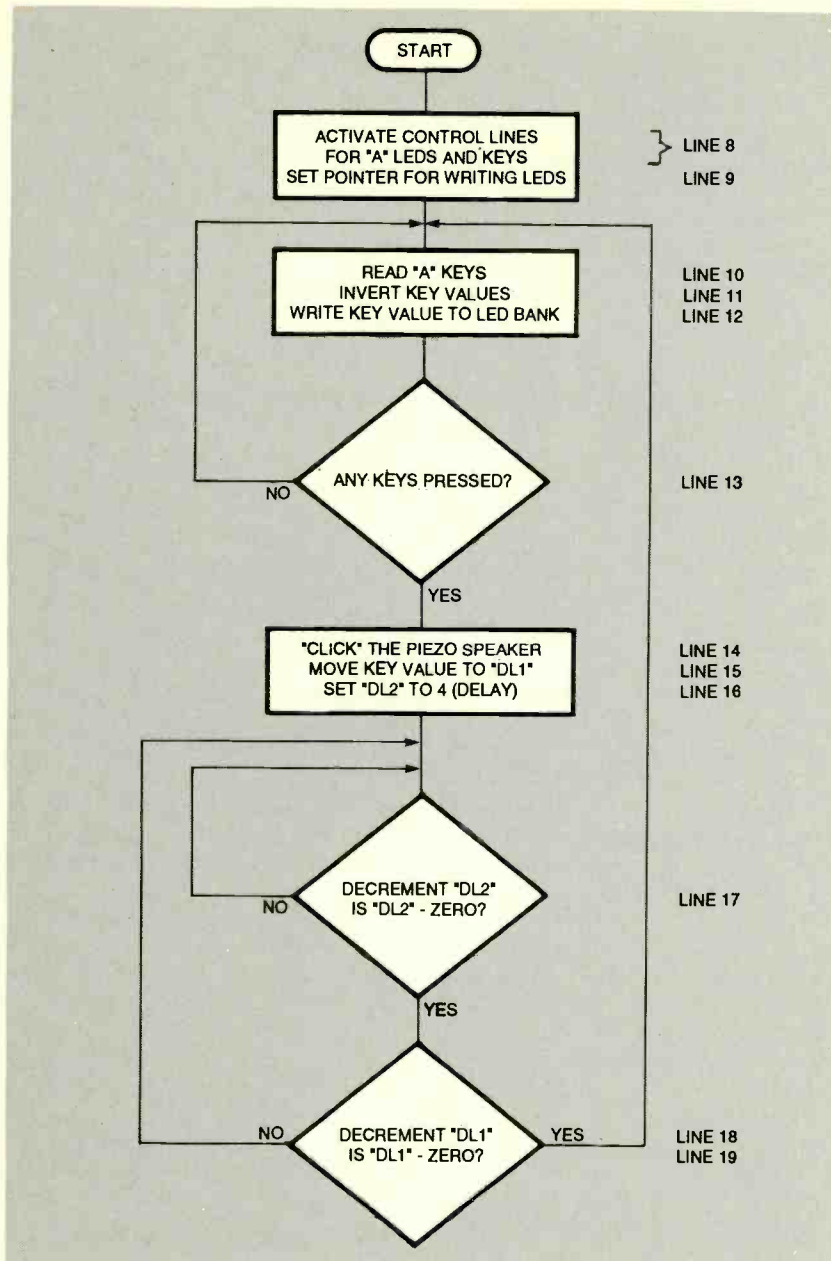


FIG. 3—THIS FLOWCHART details the operations performed in Listing 1.

### Construction

All of the necessary components including the PC board are available from the source given in the Parts List. Foil patterns are provided if you want to make your own PC board. Pre-programmed EPROMs are available from the source given in the Parts List, and the hex code is posted on the *Electronics Now BBS* (516-293-2283, V.32, V.42bis) as a file called CGAME.HEX.

Using Fig. 2 as a guide, solder the components in place beginning with the 1N914 diodes, re-

sistors, and capacitors. Next, install the sixteen LEDs flush with the PC board. Follow with the IC sockets, but do not install the ICs into their sockets until all other parts are installed.

To install the two battery connectors, align them by first snapping them onto a 9-volt battery. Be sure the battery polarity is correct. While holding the battery flush with the PC board, solder the battery connectors in place. Remove the battery after the clips are in place. Next, solder in the 16 pushbuttons, the power switch

and jack, transducer, crystal, and audio output jack.

Next install six rubber feet on the bottom of the printed circuit board. These will keep the cut leads of the components from damaging your table top while you play the game. Optionally, you might want to mount a sheet of plastic to the PC board's bottom side to keep the leads from scratching your fingers. Cut it to the same size as the PC board and fasten it with machine screws and spacers. One-sixteenth inch thick styrene or black ABS plastic works well. Finish up by installing the four ICs. The completed game is shown in the opening of this article.

### Checkout

Connect a 9-volt battery and turn on the power switch. You should first hear a short beep, then see the 16 LEDs light one at a time in a repeating counter-clockwise pattern. If nothing happens when power is applied, check to see that +5 volts is present at the output of IC5. Also check for +5 volts on each IC's power pin, and make sure each ground pin is at zero volts. Verify that none of the address or data lines are shorted to each other.

Check to see that each of the 16 pushbuttons work. To do this, you need to press the reset switch before pressing each pushbutton. At this point, don't try to play each game; just see that every pushbutton causes a distinct change in the game's behavior. (Note that you will hear a similar start-tone sequence after each game is selected, so wait long enough for a few LEDs to turn on.)

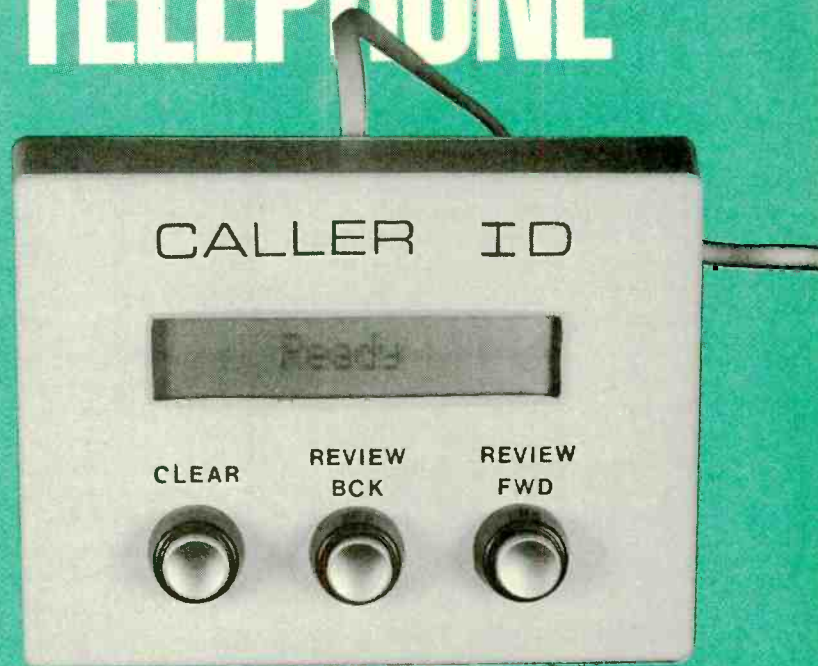
### The games

Table 1 shows a complete list of the 16 game functions. Notice the designations A1, A2, A4, etc., on the left side of the chart, which correspond to the key designations shown in Fig. 2. As an example of how a particular game is selected, if after pressing reset you press the "4" key on the "A" side, you will start the tennis game.

*Continued on page 70*

# TAKE BACK CONTROL OF YOUR TELEPHONE

**Upgrade the February 1994 Caller-ID project so it works with the calling-name delivery service.**



TERRY WEEDER

AN ARTICLE IN THE FEBRUARY 1994 issue of *Electronics Now* ("Take Back Control of Your Telephone") described the operation and construction of a calling number identifier or CDI. That circuit decodes the Caller ID data on the telephone line and displays the calling party's number. The subscriber feature that made this service possible is known as calling number delivery or CND. The service is probably available from your local telephone company for a small monthly fee.

This article describes an upgrade to that circuit which provides an additional service termed calling name delivery or CNAM. Be sure to reread the February article if you want to refresh your recollection of the details of that project before you add this upgrade.

The telephone companies use two different formats to send Caller ID to your home: single data message format (SDMF) and multiple data message for-

mat (MDMF). SDMF, described in the February article, works when an initial code of 04 (hexadecimal) is sent to your telephone to identify the data stream that follows as SDMF format.

### Single-data format

Figure 1 shows the order in which the data is sent with SDMF. The "message type" and "message length" are sent in binary code, while each character of the month, day, hour, minute, and telephone number are sent in standard 8-bit ASCII code. If the calling party's number is not available because it is outside your service area or originates from a phone where CND is not supported, the letter "O" is sent instead of a telephone number. If the calling party deliberately blocks the delivery of his number (done in most areas by pressing \*67 prior to making the call), the letter "P" will be sent instead of the telephone number.

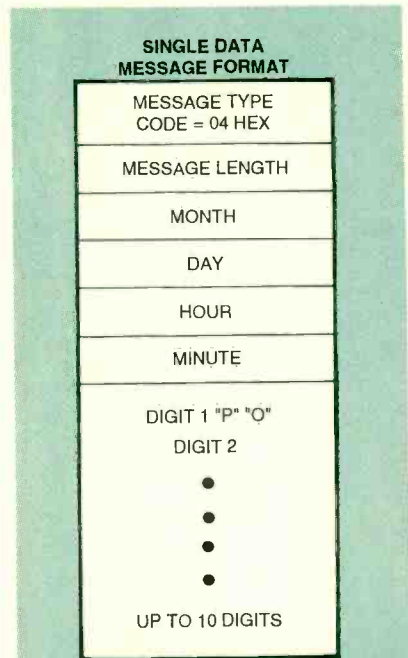


FIG. 1—A TYPE CODE OF 04 (hex) will precede the data in the single data message format (SDMF). This is the order in which each word will be sent in the SDMF format.

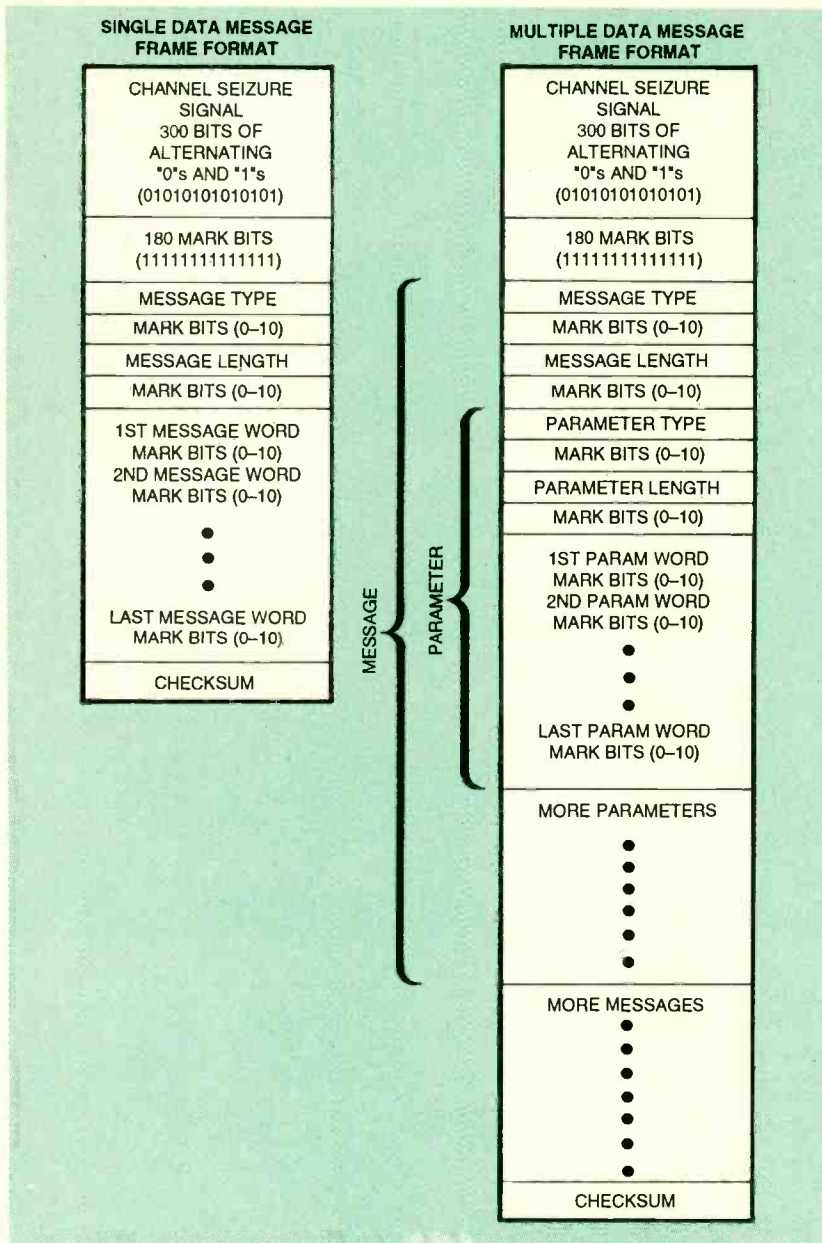


FIG. 2—DATA ARRANGEMENT IN THE SDMF frame as compared to the arrangement in the MDMF frame.

**Multiple-data format**

MDMF was invented to allow additions to be made to the data stream, including multiple blocks of data (messages) not necessarily related to each other. Bellcore (the Bell Communications Research Group) has suggested that SDMF might eventually be phased out in favor of MDMF.

Figure 2 shows how the structures of the two different formats coexist compatibly. The data associated with each MDMF message is divided into separate segments called pa-

rameters. For example, with CND, the information, date, and time are sent in a single segment, or parameter, and the calling number is sent in a second segment.

Each message can contain different kinds of segments in random order, depending on the service the customer has ordered. The last word to be sent is a checksum. Used for error detection, the checksum is the two's complement of the sum of the bits in *all* words in the data transmission.

The message-type word in the

MDMF that indicates transmission of CND and/or CNAM is 80 (hex). That's followed by a message-length word which is the sum of all the words in all the different parameters associated with the message. Figure 3 shows each parameter that can be included in the message, and the "type" codes that are used to identify each of the multiple parameters.

Notice that each parameter also has its own "length" word. The length word is important when designing a program that will decode the message. For example, if you want the program to look only for the name of the calling party, you would want it to ignore all other parameters that have the wrong type code. When receiving each type code, the length word indicates how many words the program will have to skip before the start of the next parameter in the message.

The parameters that will be included in the message depend on whether you subscribe to CND, CNAM, or both. In all cases, either the "Number" parameter or "Reason for Absence of Number" parameter will be

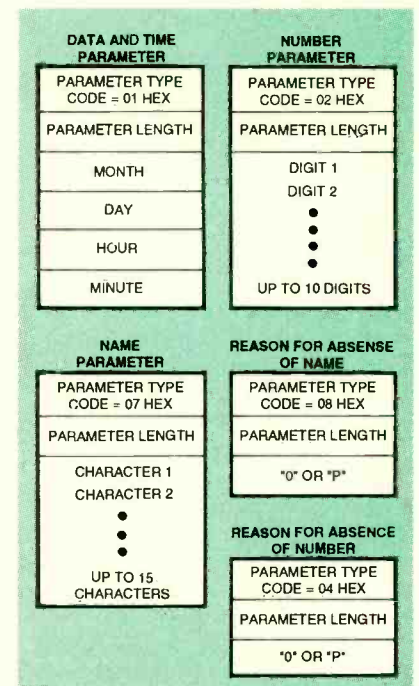


FIG. 3—MULTIPLE PARAMETERS are contained in the MDMF frame. Here's a list of those parameters with their identifying type codes.



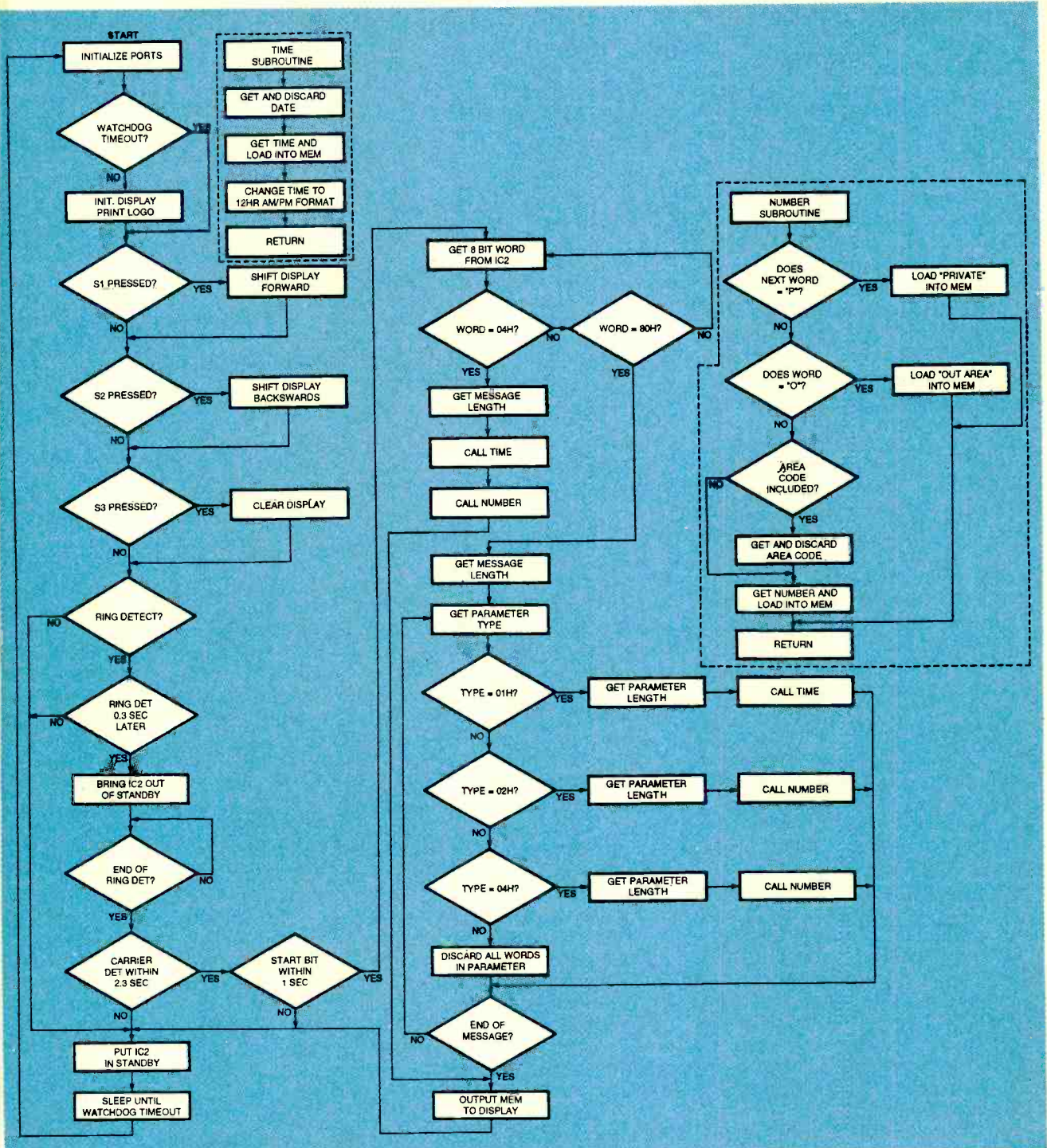


FIG. 4—FLOWCHART FOR THE UPGRADED VERSION of firmware for the PIC16C55 in the February 1994 Caller-ID project. This version is compatible with both SDMF and MDMF.

sent, but not both. The same applies to the "Name" parameter and "Reason for Absence of Name" parameter.

At the present time, the maximum number of characters in the name parameter do not exceed 15. That number is expected to increase some time in the future.

### Project upgrade

The original firmware written for the PIC16C55 microcontroller in the Caller ID project was configured to work with SDMF only. If you live in a calling area that supports MDMF and not SDMF (this can be determined by calling your telephone company).

The originally programmed microcontroller will not work with this system. If you have a PIC16C55 programmed with the original version of the firmware, you can send it to the author at: PO Box 421, Batavia, OH 45103. He will exchange it for a PIC programmed to accept MDMF at no charge. You can also send him a 3½- or 5¼-inch

*Continued on page 88*

## COMPUTERIZED GAME

continued from page 66

The second column from the left in Table 1 shows the games that require two players. Typical play is with both players sitting opposite each other, each with both hands on the keys. Games checked in the third column can be played by one player, or alternately by two or more. Game titles are shown in the fourth column, and how-to-play instructions are shown in the middle of the chart.

Be aware that the numbers in the key designation (1, 2, 4, 8, 16, 32, 64, 128) also correspond to the bit values of an 8-bit binary number. It is important to know this when playing games A32, A64, and A128. Also, after many games terminate, the score will be displayed in binary on both sides of the board. For example, if after a game ends, LEDs A8 and A4 are lit, the score is 12 for the A side.

Four of the single-player games (A32, A64, A128, and B2) require that you "enter" an answer. During those games, pushbutton A128 acts as an enter key. First hold down a combination of A keys for your answer, then enter that answer by pressing key A128.

In two games, A32 and A64, two numbers will be shown in binary. The first number will be displayed with a corresponding "low" beep, followed by the second with a corresponding "higher" beep, then a pause. The numbers keep repeating. Those are the two numbers you need to work on in those games. The object of game A32 (Binary Math), for example, is to correctly add, subtract, divide, and multiply (in any order) the two 4-bit numbers shown. Each time you enter a correct answer (enter with key A128), two B side LEDs light up. After all eight B-side LEDs are lit, you win and the game ends.

In game B8 (Last Player Wins), the game will prompt the player whose turn it is by momentarily flashing all eight LEDs on that side. You then must move an LED by pressing

LISTING 1					
;EXAMPLE SOFTWARE LISTING FOR 80C31 C-GAME					
1					
2					
3	0030	DL1	EQU	30H	;VARIABLE, INNER DELAY
4	0031	DL2	EQU	31H	;VARIABLE, OUTER LOOP
5					
6	0000		ORG	0000H	;SET ORIGIN OF PROGRAM
7					
8	0000	75B0CA	START	MOV	P3,#0CAH ;ENABLE "A" KEY & LED BANKS
9	0003	900000		MOV	DPTR,#0 ;SET ADDRESS FOR LEDS
10	0006	E590	START2	MOV	A,P1 ;READ PUSHBUTTON KEYS
11	0008	F4		CPL	A ;MAKE LOWS TO HIGHS
12	0009	F0		MOVX	@DPTR,A ;WRITE TO LED'S
13	000A	60FA		JZ	START2 ;GO BACK IF NO KEYS DOWN
14	000C	B2B4		CPL	P3.4 ;TOGGLE PIEZO (ONE "CLICK")
15	000E	F530		MOV	DL1,A ;MOVE A TO DL1 VARIABLE
16	0010	753104	DELAY	MOV	DL2,#04 ;SET INNER LOOP TO 4
17	0013	D531FD	DELAY2	DJNZ	DL2,DELAY2 ;INNER LOOP
18	0016	D530F7		DJNZ	DL1,DELAY ;OUTER LOOP (KEY VALUE)
19	0019	80EB		JMP	START2 ;START OVER
20	001B			END	
Errors: None					

a key next to a lit LED to move it to an "empty" (non-lit) space. Either player can move any LED (in his turn), as long as it is in the direction of LED A1, and then finally in the direction of LED B128. The game won't let you make illegal moves. Once there are no more unlit spaces toward B128, the game is over. The last player to fill an empty space wins.

A few games are quite simple. They require only that a key be pressed when that side's corresponding LED lights. Games A1, A4, and A8 are three such games. When you are learning the C-Game, it is suggested you start with the games in the order shown in Table 1 (first A1, then A2, A3, etc.) as they are organized by order of difficulty.

The four "special effects" selections are included just for fun. When selected, C-Game produces random and pre-programmed LED displays and sound effects. In selection B16, the A-side keys and B-side keys each produce a separate tone; the frequencies are dependent on the keys held down. Selection B32 lights LEDs in a random pattern, with the A-side keys controlling the range of the tones, and the B-side keys controlling the overall cycling speed.

Refer back to Table 1 for more details about operating all of the games and functions. Don't be afraid to experiment and press the keys in any order you wish—you can't harm anything.

### Going further

For readers who want to program their own custom applications or games, a short assembly software listing is given in Listing 1. This program continuously reads the A-side keys and correspondingly lights the A-side LEDs while producing a tone from the transducer. The frequency of the square wave is directly dependent on the binary value of the keys that are pressed.

The flow chart, Fig. 3, details the operations performed in Listing 1. The line numbers in the flow chart correspond to the line numbers in the assembly listing.

Notice line 16 in the listing. The square wave's frequency is determined by the value placed in the "inner loop" (refer to the flowchart and also lines 16 and 17). By changing the value from 4 to some larger value, for example, the loop would require more time to decrement to zero, causing the overall range of frequencies of the square waves to be lower.  $\Omega$

**BE A GOOD  
NEIGHBOR**

Volunteer.

 American Heart Association

# HARDWARE HACKER

Second law violations, soliton wave rectifiers, a fine new CD-ROM directory, a Santa Claus machine update, and some unusual hacker opportunities.

DON LANCASTER

I just got a call from a graduate student who is certain that second law of thermodynamics has been proven wrong and he wanted to know what should be done about it. He said something about statistical thermal gradients nailing *Maxwell's Demon* in a driveby shooting. Naturally, the effect is purely theoretical. It is "too small to measure in the lab."

The second law says heat always *tends* to flow from a hot to a cooler body, but it does not say that it is impossible for heat to flow from a cool to a hot body.

Actually, our helpline hears about three second-law violations or so per month. So let's go over the rules one more time: True, the second law of thermodynamics ("you cannot break even") has never been proven. Moreover, it probably is *not* provable.

On the other hand, and *without exception*, every attempt to find any counterexample that would prove it wrong has utterly and totally failed—at least on the normal everyday scale of things. Literally billions of tests are unintentionally rerun day in and day out that overwhelmingly suggest that the law really is true. Congress is not expected to repeal the second law of thermodynamics any time soon.

If the grad student is convinced he is right, he has two options: He can go the *real science* or the *pseudoscience* route. By going the real science route, he has to create a simple and easily duplicated experiment that proves the effect conclusively to disinterested third parties. It must be done so that his explanation for what is happening seems to be the most probable and the most reasonable.

The results *must* stand up. After the results are independently duplicated and verified, then his paper

can be presented to a credible scientific journal for a peer review and publication.

By going the pseudoscience route, he can go to anyone in the pseudoscience industry press and get his paper instantly published. Or else he could pick slow news days in obscure rural newspapers for his coverage. Or he could go to even more obscure semi-scholarly foreign publications of questionable pedigree. But none of these alternate routes will look good on his resume.

I've just posted lots more information on exploring pseudoscience resources as NUTS26.PS on *GEnie* PSRT. Back to the real world...

## Solitons

Outside of a classic ghost town in Colorado's San Juan Mountains, there is an old free-hanging mining cable. This beast is nearly a mile long and over an inch in diameter. It leads us to some utterly fascinating real-world and real-time physics. If you grab this cable near the low end and shake it once, you can watch a solitary wave running up, reflecting, and returning several seconds later.

What is really amazing is that the solitary return wave is so violent that it will try to rip your arm right off the cable. Something unusual appears to be happening.

A century ago, a mathematician decided that certain solitary waves can indeed be special. He was riding his horse along a canal bank and was daydreaming about waves. A barge suddenly stopped and then launched a solitary wave. He immediately noticed that this wave was unique in that it kept going much farther than ordinary waves. In fact, he followed the wave for miles. After some analysis, he called this special type of wave a *soliton*.

Today, solitons are an incredibly

hot research topic. One application is in fiber-optic communications, where a soliton can go much further between repeating amplifiers. In fact, soliton fiber communication has been demonstrated over distances a third of the way around the earth with a 20-gigabyte data rate.

Why will any wave die out? There are three main reasons. First, the wave will *dissipate* when it does such things as flex a resisting cable or encounters air resistance. Dissipation ultimately transforms all of the wave energy into low-grade heat.

Second, portions of the wave will *reflect* whenever they encounter any changes in the media's impedance or uniformity. In the case of that San Juan cable, the end ring is something less than a perfect short circuit, so you don't get everything reflected back.

Finally, and most important for a soliton, the wave will *disperse* if the media lets higher frequency waves go by faster or slower than lower frequency ones. Usually, the wave energy "stretches out" over time.

Any waveform can be represented as a group of high-frequency and low-frequency components. If these ever get out of step, the wave shape will change drastically, as will its detectability.

A different name for one type of dispersion is *group delay distortion*. For instance, if the frequency for a one in a modem has more delay than the frequency for a zero, there might be a time when you get a one, a zero, *both*, or *neither* at the output. Obviously, "both" and "neither" are bad news when it comes to extracting useful information.

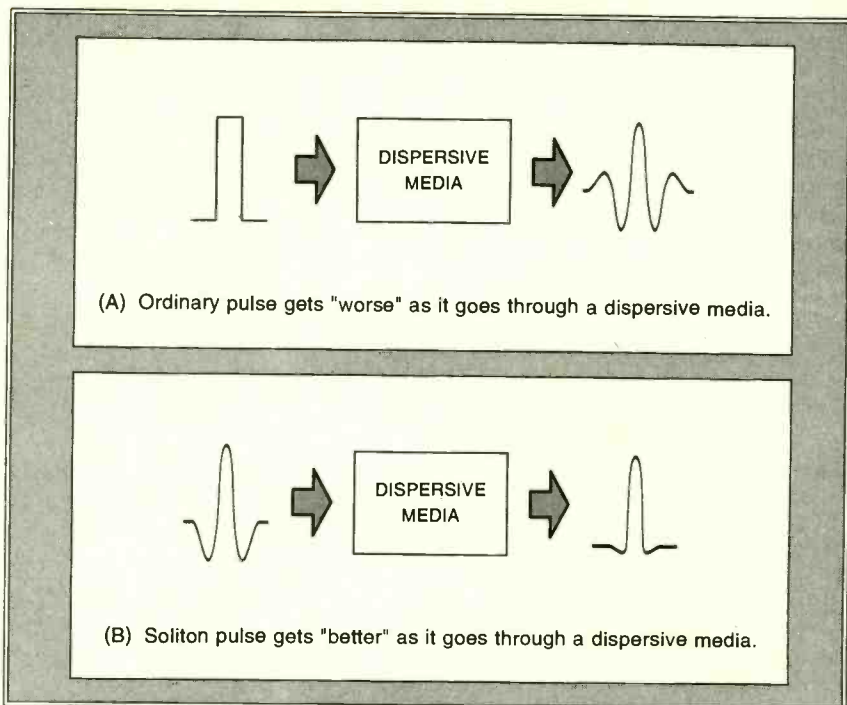
Figure 1 shows the essentials of solitons. An ordinary pulse that is sent through a dissipative media gets worse and harder to detect. A soliton that is sent through the

same media actually gets *better* and easier to detect. For the best results, the media has to be known, stable, and fixed in length. The soliton shape also has to be designed to match the media.

A soliton wave tries to *predistort* itself so that, by the time it is sent *through* the media to the intended receiver, the dispersion of the media and the "undispersion" of the initial waveform cancel out. The fast and later frequency components catch up with slow and early ones. The soliton wave in effect becomes self-reinforcing.

Bats and military radars depend on a more elaborate *chirp* scheme that works in more or less the same way as solitons. Send any swept FM signal through any media that has a linear delay versus frequency response, and you get a narrow and high-amplitude pulse out—Fourier transforms and all.

When you explore the literature, you will find 8,316 soliton papers on the *Dialog* information service alone! There are also dozens of textbooks available. Sadly, many are totally unreadable and involve horrendous math. I have posted a more or



**FIG. 1—SOLITONS** are a special class of solitary waveforms that can travel much farther than ordinary waves. They are now a very hot research topic.

less random and rather short sampling of information sources in Fig. 2. These sources and their end bibliographies should be enough to get you started.

Let me know if you find any favorite soliton tutorials on your own that are easy to understand. An *Incredible Secret Money Machine II* book will be sent for your trouble.

What good are solitons for hardware hackers? Well, obviously, they are a great subject for science fair projects, student papers, or even thesis topics. But there's a possible new use for solitons that just about anybody can explore, and for which hands-on backyard testing is more important than fancy math. It is one use that is guaranteed to get your feet wet, and that might make you some big bucks.

Simply answer this question: "Can solitons improve fire streams?"

Between spelunking, *tinaja quests*, and pecan harvests, I am also a city fireman. The deck gun on a pumper has an effective fire-ground range of slightly over 200 feet. There are times and places when that range just isn't enough. The solitons should be able to extend this range significantly.

Ideally, all of the solitons should

be generated through water pressure only, using some sort of bolt-on and pass-through flutterwumping adapter that is in series with the water supply.

But go ahead and use electronics or even high-pressure air to prove the idea works. Because of an exciting and an incredibly effective new foam firefighting technique, certain new pumpers now include a reliable compressed air supply.

Let me know what you can come up with here. Obviously, you can use an ordinary garden hose for all your initial tests. This subject appears to be an outstanding new hacker opportunity.

### Santa Claus machines

The science fiction authors called them *Santa Claus machines*. These magic boxes could run off a copy of anything—a BMW, a pastrami on rye, a new girlfriend, or a duplicate \$20 bill. It would start with either a sample or a set of software plans.

These days, crude approximations of the Santa Claus machine really do exist, and they are getting better every day. Today, these are often known as *desktop manufacturing* or else *rapid prototyping systems*. The pastrami on rye sandwich still leaves a distinctly acrylic after-

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- All-optical Waveguide Switching**, Stegeman, G.I. & Wright, E.M. *Optical and Quantum Electronics* V22, no.2, p95-122 March 1990 (62 refs).
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FIG. 2—SOME RECENT SOLITON REFERENCES. There are over 8000 more!

taste, but it definitely is low in fat and has zero cholesterol.

There are now a dozen approaches to Santa Claus machines, so I thought I would once again gather the names of several of the bigger players together into this month's resource sidebar. Most of the systems we'll look at are outrageously expensive—a house and two cars. But there is no reason why the whole kit and kaboodle of them can't be replaced with \$175 worth of hacker parts, bunches of time, and a lot of imagination. Some of the major approaches to Santa Claus machines are shown in Figs. 3 and 4. Here's a brief rundown:

**Direct toner method.** This one is the cheapest, the most accessible, and the most hacker friendly. But it is pretty much restricted to two-dimensional work such as making instant printed circuits, front panels, or dialplates.

With this method, you laser print the toner image onto a transfer sheet. The transfer sheet is placed in contact with your printed circuit board or whatever. Heat and pres-

sure is then applied. The toner transfers to the board and becomes the etch resist or the image.

The two leading suppliers of direct-toner materials are *DynaArt Designs* and *Techniks*, with the printed circuit supplies sold by *Kepto*.

**CAD/CAM.** This method has been around for a while. It works like an ordinary lathe or milling machine, machining materials to leave the desired object. The difference is software control. The machine is fed a set of plans in software form and it does the rest by itself. Low-end machines have only started to appear here. Although much lower in cost than old "industrial strength" machinery, they still remain obscenely overpriced for most hacker uses.

Typical low-end CAD/CAM suppliers include *Roland*, *Techno Isel*, and *Light Machines*. Other vendors advertise in such places as the *School Shop* and *Industrial Education* trade journals.

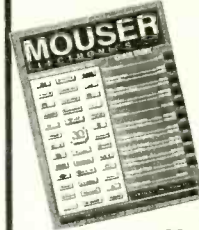
Custom CAD/CAM bits and pieces are available at *Stock Drive Products*. Two other material

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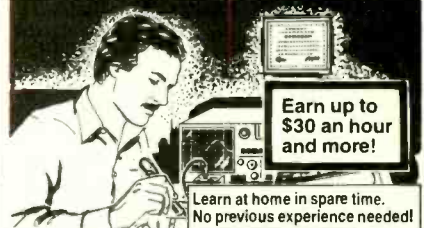
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sources are *MSC Specialties* and *McMaster-Carr*. *John Rees* offers a hacker version here that lets you use ordinary car alternators as power stepper motors.

A CAD/CAM prototyping system can be used with a machineable wax instead of metal or plastic. The wax can then become a pattern or a mold for your final product. This is easier on tools, and mistakes can be recycled. Wax is also a good material for practice. One source of machinable wax is *Freeman Supply*, while *Kindt-Collins* provides a wide range of industrial and artist waxes.

**Laser Blasting.** The medium power laser is one variation on CAD/CAM that is revolutionizing crafts, model making, and smaller part manufacturing. Parts are cut quickly, accurately, and splinter free. A 20-watt carbon-dioxide laser could be used for such tasks as the precision cutting of doll-house furniture or slicing up parts for model railroad structures. More information on power laser systems appears in *Industrial Laser Review*, while two hacker-friendly sources for lasers are *Meredith* and *MWK*.

**Water Knives.** Here an ultra high pressure water stream does all the cutting. My favorite demonstration is one of these chopping up a gooey piece of chocolate cake and a four-inch thick steel slab at the same time. *Flow International* is one source of equipment. *Haskell* makes the special pumps.

**Stereolithography.** The pioneer here is a company called *3D Systems*. With stereolithography, a vat of a liquid photopolymer is hardened one layer at a time by a scanning laser. The laser is lowered slightly as each new layer is finished so that the next layer can be hardened. The process is repeated until the part is completed. Virtually any shape can be made, including ones that are difficult to machine.

The photopolymers aren't all that different from the ones used in flexographic printing and rubber stamps. Two suppliers are *Merigraph* and *Grantham Polly-Stamp*.

**Selective Laser Sintering.** This is a rapid prototyping method that starts with a fine powder of wax, plastic, or even certain metals.

## NAMES AND NUMBERS

### Aero/Skyways

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### Buddy Products

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The laser selectively melts and bonds portions together in a thin layer by *sintering*. (Sintering is melting things just enough so that they stick together.) Then the part is lowered, more powder is leveled,

and a second layer is imaged, building up the desired prototype.

The final objects are often sturdy enough for use as actual production parts. Unlike stereolithography, the materials used are low-cost and non-hazardous. The laser is also cheaper because it emits infrared rather than ultraviolet light. *DTM Corp* in Austin seems to be the champion of selective laser sintering.

**Cubital Toner Imaging.** This method is related to the direct-toner method. An *unfused* toner laser image is contact-printed onto a photopolymer. After the uncovered photopolymer is hardened by exposure to ultraviolet light, the unhardened photopolymer is sucked up and recycled, as is the toner image. Voids are then replaced with a wax filling.

The surface is carefully milled flat and another layer is created. Unlike stereolithography, an entire layer rather than a single spot is formed at one time. Cubital toner imaging also requires far less photopolymer, since only a thin layer is used. First developed in Israel, one source is *Cubital America* and one service bureau is *Stature Machining Technologies*.

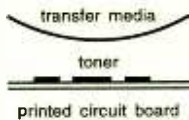
**Sticky Strings** This approach seems well suited for forming such hollow objects as shampoo bottles or similar packaging containers. The correct name for the process is *fused deposition modeling*, and *Stratasys* is its main source.

In use, a large reel of thermoplastic rod is unwound along a path. The rod is deposited at a temperature just hot enough so that the outside is liquid, causing it to stick to the previous layer of the pattern.

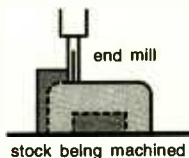
The results look sort of like corduroy, but you could trade off wire diameter against smoothness. A final polish or filler or solvent spray can improve the surface finish.

It appears to me that a hacker might easily fake this with a hot glue gun by substituting polyethylene for the glue sticks. One obvious use is custom cast house number or name plates.

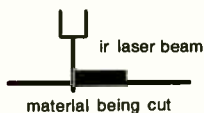
**Laminated Paper Shims.** This method works just like the contour lines on a topographical map. It is also known as *laminated object*



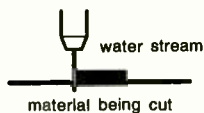
**DIRECT TONER METHOD** uses heat and pressure to transfer toner to a flat substrate for pc board etching or dialplate artwork.



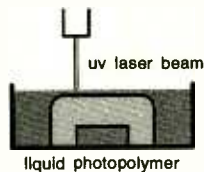
**CAD/CAM METHOD** uses a programmable lathe or milling machine to remove scrap from around the prototype object.



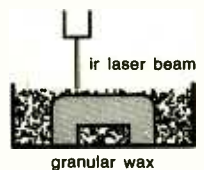
**LASER BLASTING METHOD** uses a medium to high power laser to physically cut out the parts to their desired shapes.



**WATER KNIFE METHOD** uses an ultra high pressure water stream to cleanly and quickly slice materials such as food or fabrics.



**STEREOLITHOGRAPHY METHOD** uses an ultra violet laser to selectively harden certain areas out of a liquid photopolymer.



**LASER SINTERING METHOD** will use an infrared laser to selectively bond certain wax, plastic, or metal granules.

FIG. 3—SOME CURRENT APPROACHES to Santa Claus machines.

manufacturing. At the present chosen elevation, a piece of adhesive-coated paper of the desired thickness is cut out with a laser.

The latest piece is then carefully aligned to the previous sheet and is then heat-set. This process repeats often enough to build up the desired part. A final surface coating can eliminate the individual steps.

Materials costs are exceptionally low, and only a low-power laser is needed. This method is particularly good for sand casting. One supplier of these systems is *Helisys*.

**Ceramic Shell Casting.** Originally developed at MIT, *Soligen* is now the leading proponent of this

method. A thin layer of ceramic powder is put down, and a scanning head with one or more inkjets passes over the powder, selectively applying a binder.

The part is lowered and the process is repeated, causing layer upon layer of binder to build up in the desired shape. The final shell can be directly used for the high-temperature casting of chrome alloys, aluminum, and even nickel. Hollow items can be made by building up integral cores.

**Wax Vacuuming** This is a new hacker concept that just might revolutionize jewelry and small art object creation. Picture a hypodermic-like

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needle that has a hot tip that can be moved along five or six mechanical axes.

The needle works its way around a block of wax, first melting and then vacuuming the molten wax away from the pattern. Curved needles can form the internal details or hard to access points. The intended use is for casting such things as class rings, and silver ornaments. *John Rees* is one source.

By the way, anytime you are using both X and Y motions, it pays to split up the problem. Move your tool in the X direction and your workpiece in the Y direction. This can convert a thorny two-dimensional problem into simpler one-dimensional ones.

For more information, a pricey industry newsletter called the *Rapid Prototyping Report* is available. *Batelle* does fancy research on rapid prototyping. Many ongoing Santa Claus machine developments are likely to appear in the *Machine Design* and *Design News* magazines.

### New tech lit

*Morph's Outpost on the Digital Frontier* is a unique new multimedia magazine in newspaper format. It offers the latest inside scoop on multimedia developer happenings.

Two other unusual magazines are *Skyways* and *WWI Aero* for those of you interested in early aviation.

From *Sony*, there's a new *Computer Audio & Video Multimedia* data book.

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*Buddy Products* offers Bakerizing in a can. You can spray this stuff on any laser-printed output and it will get blacker, smoother, and more durable. The resolution appears to improve and text becomes slightly bolder.

The spray is mostly methylene chloride, acetone, and some isobutyl acetate. It works like a champ. But use this spray outdoors only and watch out for fingerprints. No, it won't help direct-toner printed-circuit transfers much because of the residues it leaves.

The *Calculator Collector* is a new

labor-of-love newsletter published by the *International Association of Calculator Collectors*.

Lots of telecommunications books are offered by the *Telecom Library*. Some useful multimedia videotapes are sold by *First Light Video*.

The *Fluorescent Mineral Society* looks at rocks in the dark.

A fine catalog on moldmaking and casting materials is available from *Polytek Development*. A similar new catalog is available from *Burman Industries*, another special effects supplier.



## EQUIPMENT REPORTS

continued from page 20

decimal point is determined by the selected range. The LED display will flash when an overrange condition is encountered. If an illegal combination of front-panel switches is selected (for example, if DC volts and the 20-megohm range are selected at the same time), all of the decimal points will light.

The unit is said to be maintain its accuracy for at least a year. After that time, it should be calibrated. That one-year period also matches the limit of the manufacturer's warranty on the BDM40.

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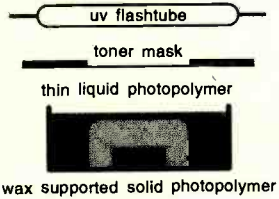
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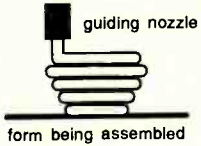
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<input type="checkbox"/> Bookkeeping	<input type="checkbox"/> Florist
<input type="checkbox"/> Child Day Care	<input type="checkbox"/> Secretary
<input type="checkbox"/> Medical Office Assistant	<input type="checkbox"/> Teacher Aide
<input type="checkbox"/> Legal Assistant	<input type="checkbox"/> Home Inspector
<input type="checkbox"/> Art	<input type="checkbox"/> Medical Transcriptionist
<input type="checkbox"/> Motorcycle Repair	<input type="checkbox"/> Real Estate Appraiser
	<input type="checkbox"/> Professional Locksmithing

Name \_\_\_\_\_ Age \_\_\_\_\_  
 Address \_\_\_\_\_ Apt. # \_\_\_\_\_  
 City/State \_\_\_\_\_ Zip \_\_\_\_\_  
 Phone ( ) \_\_\_\_\_

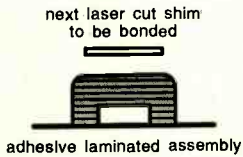
July 1994, Electronics Now



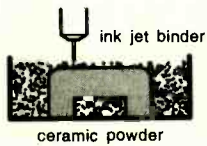
**CUBITAL TONER METHOD** transfers toner images a layer at a time to a wax supported and flat milled liquid photopolymer.



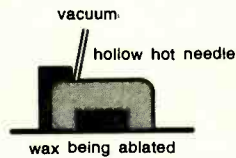
**STICKY STRING METHOD** uses a heated roll of plastic rod to bond to previous layers for bottles and hollow objects.



**SHIM LAMINATING METHOD** uses laser cut thin sheets of heat bonded paper to build up a composite object with low materials cost.



**CERAMIC SHELL METHOD** can selectively form ceramic powders by using an inkjet to apply suitable binding agents.



**HOT WAX VACUUM METHOD** uses a fine heated needle to remove unwanted portions of a wax block, leaving a pattern.

FIG. 4—ADDITIONAL APPROACHES to Santa Claus machines.

I've managed to get a great *GENie* deal specially for all you Hardware Hackers. Ten free hours with no first-month minimum. Just use the new JOINGENIE.DMD524 password that is shown in the *Need Help* box.

Be sure to type that HHH quickly after your communication program shows a connect. That is how *GENie* figures out your computer's baud rate and format.

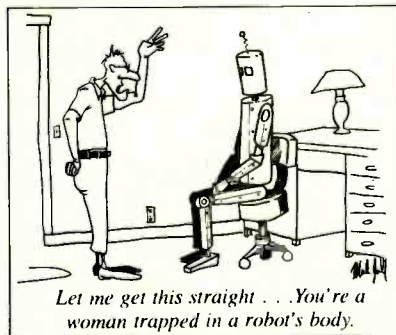
You'll find reprints of most of my previous columns and bunches of other unique stuff on *Genie's PSRT Roundtable*. But be sure to check out its RADIO, IBM, MAC, A2PRO, and DTP Roundtables as well. Look at the stock quotes on page 270 and the free DIALOG training area.

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Most items mentioned are found in the *Names & Numbers* or *Santa Claus Machine* sidebars. Be sure to check those first before calling our no-charge technical helpline.  $\Omega$



# AUDIO UPDATE

## Sound pressure level: damage/sonic realism

LARRY KLEIN

**R**egular readers of this column are probably aware of my strong interest in hearing preservation. Obviously, I'm swimming against the sonic tide, given the proliferation of killer car stereos, overdriven Walkmen, excessive concert-hall levels, and various other kinds of environmental noise. Recently, it all came home in an unexpected way.

One Friday during supper, my 10-year-old son announced that he'd like to attend the 5th-grade disco dance taking place in the middle-school cafeteria that evening. My wife dropped him off, and we looked forward to three or four hours of quiet, unsullied by various juvenile demands and the sounds of Sega. Alas, our dream of peace was not to be. About 30 minutes later, we got a phone call from Nathaniel asking to be picked up ASAP!

When he arrived home, Nathaniel said that the music was so loud it hurt his ears. My wife confirmed that the sound had indeed been very loud ("It must be 120 dB in there!"), and I thought it might be a good idea for me to visit the dance with my sound-pressure level (SPL) meter in hand.

Yes, things were pretty loud! At the rear of the room, opposite the platform where the DJ had set up his speakers, the measured SPL was about 95 dBA. At a distance of 10 feet in front of the speakers I measured a steady 110 dBA with the meter set to slow response. Wanting to protect whatever hearing I have left, I decided not to climb up on the platform with the speakers where a dozen or so kids were digging the vibes, literally.

Upset about the potential ear damage inflicted on my son's friends and classmates, I sought out the teacher in charge of the proceedings. I told him of my concerns, and suggested that he have the DJ turn down the level at least 15 dB. His response (delivered very po-



**Radio Shack's Model 33-2055 digital SPL meter was used to measure the sound-pressure level at a middle-school dance.**

lately) was: (1) He has been conducting these dances for eight years and there had never been any complaints about the sound level, and (2) if he turned the sound down too far the kids would revolt. I testily reaffirmed my point that at the existing sound levels there was a real risk of ear damage. I got nowhere and left vowing to continue the fight—but I wasn't quite sure how.

I found an unexpected and militant ally in a mother whose bright, musically talented daughter Katie is in the same grade as my son. I told her of my experience and provided some background articles on OSHA and hearing damage. She did some of her own research, became terribly concerned, and wrote a letter to the school principal outlining the situation and my SPL readings. She asked for a meeting with him and other concerned parties, including the members of the PTSA health committee.

### **The fuddy-duddy factor**

The meeting didn't go quite as I had hoped. I opened the proceedings by distributing background material and outlining my concerns and the reasons for them. I also made

the point that I've been a rock fan since the sixties. I had supplied sound equipment to a rock band, had permanent passes to the Fillmore East, the Cheetah Club, The Electric Circus, and Max's Kansas City Upstairs. In other words, I was not simply a gray-bearded fuddy-duddy complaining about the sonic excesses of our youth.

I was puzzled by the subsequent lack of support on the issue. The middle-school principal seemed mainly concerned that word of my measurements not get out to the parents. I don't know whether he envisioned hysterical reactions leading to lawsuits or simply felt that my fears of hearing damage were unwarranted. In any case, he said the older grades were having a dance the next Friday, and invited me to take more measurements.

I arrived there with Katie's mom, who had volunteered to take notes, a Heath real-time analyzer/SPL meter, a calibrated Radio Shack SPL meter—and earplugs. We found a different DJ with different equipment putting out a more moderate—but still too loud—sound level. The readings were a consistent 90 dBA at the back of the room, and about 5 dB louder up front. One of the chaperoning mothers accosted me, saying that she couldn't understand my point of view—would I rather have the kids wandering around out in the street than at the dance? Obviously, someone had spoken to her and probably to the DJ also.

Incidentally, the day after my initial meeting, I happened to run into Katie and one of her friends. I asked Katie how she enjoyed the dance, and whether the sound was okay. She said that when she left after three or four hours, she had felt a sort of pressure in her ears, but it was gone by the next morning. Her friend said that her ears were ringing after the dance, but her symptoms also faded by the next day.

When I happened to mention that to the principal, he appeared to be more upset by the fact that I had asked the question than by the kids' responses. Again, he strongly urged me not to talk to anyone about the situation.

There the matter rests for the moment. I've not yet passed on my new measurements, but I'm not at all hopeful about how gladly they will be received. To be continued ...

**Sonic reality**

Last weekend I attended a gospel-music concert given in a small auditorium. The room was packed and we were seated well toward the rear. Nevertheless, I was struck once again by the very audible (to me, at least) differences between live concerts and sound reproduced in the home.

As I see it, the essential purpose of high fidelity is to create the illusion of being in the presence of a live performance. Honest audiophiles are aware of how seldom that ideal is realized, despite their endless upgrading and tweaking. The dozen or so times that I've had a legitimate "I-am-there/they-are-here" experience with reproduced sound occurred when I was listening to: (1) binaural reproduction through headphones, (2) multichannel setups, or (3) stereo "venue-appropriate" reproduction.

Let me elaborate. Binaural reproduction of sound recorded with a microphone installed in a dummy head can be impressively realistic. When it's well done, there's no sense of the sound coming from the headphones; rather, one enjoys the audible illusion of being in a totally different sonic environment.

Multichannel sound can also be extremely realistic if the recording and playback are properly executed. I've heard a four-channel tape that transported me into the presence of an invisible, but wonderfully audible, grand piano. It was being played right over there! About 15 years ago, Acoustic Research demonstrated for me an experimental 16-channel setup that, in terms of I-am-there realism, left nothing to be desired. And I've heard other impressive multichannel demos dating back at least 25 years.

What do I mean by "venue-appropriate?" During the mid-sixties, when I was loosely associated with a rock band called the Group Image, I recorded a rehearsal at a friend's loft. My equipment consisted of two reasonably good mikes plugged directly into a Teac 10½-inch open-reel recorder, and a pair of good isolating headphones. Playback was provided by my friend's stereo system in the same room. After shifting around the band members and microphones for about 15 minutes, I finally achieved a reasonable stereo balance in the phones. I started the tape and went into the adjoining room to talk to my friend while the band and singer wailed on.

The band stopped for a break, but since I knew there was plenty of tape I didn't bother to switch the recorder off. I heard the band start up again doing the same number, and I wandered back to suggest they do something different. But I wasn't hearing the live band; they were playing back the rewind tape. And listening from the adjacent room through a wide doorway, I couldn't tell the difference! To say the least, I was flabbergasted. What I heard flew in the face of everything I had read about the deleterious effects of "doubled room acoustics"—which is what happens when the normal room reverberation caught on a recording is reinforced unnaturally by playback in the same room. Since I had the band at hand, I did some quick live-versus-recorded tests. Yes, there was a discernible difference during A/B comparisons, but from the next room A and B were equally "live."

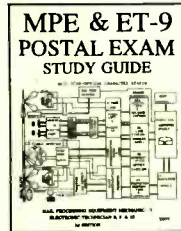
Over the years, I think I've been able to pin down the subjective differences between a live performance and a state-of-the-art commercial recording. For one thing, the extreme highs heard live have a crystalline quality that is almost always lost in reproduction. To my surprise, I can still hear that difference despite my age-induced high-frequency loss. But I believe there's a more important factor at play. I call it, for want of an established term, the Klein theory of sonic-venue appropriateness (SVA).

Somehow our ears find fault with  
*Continued on page 85*



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# DRAWING BOARD

This month we build the PLL section of our tachometer.

ROBERT GROSSBLATT

**B**efore I get started this month, there's some unfinished automotive-related business to take care of. Some months ago I mentioned that while two stroke engines had just about disappeared, they were still used in chain saws. I wondered if anyone out there knew the reason for that and, sad to say, I've gotten only one right answer in the mail so far. That's right, a lot of mail but only one correct answer.

To put the matter to rest, the reason that two-cycle engines power chain saws is simply because a chain saw has to be able to run upside down. It can't have an oil sump. During the more difficult maneuvers with the saw, the saw must be turned upside down. If it had a four-cycle engine, the oil would leave the sump bottom, the oil pump would run dry, and the engine would seize. Congratulations to John Lindsay of Paramus, New Jersey for providing the right answer. And now back to the tachometer.

Using a phase-locked loop as the basis for the tachometer does a lot to simplify the design of the circuit but, as I noted last month, it's not a totally trouble-free solution. Engine speed is never constant, and as rpm drops, the variations in engine speed become a larger and larger percentage of the mean speed. By the time it is returned to idle speed, the variation is often more than 10%. It can be even higher if the engine timing is off or something else isn't right with the engine.

This erratic behavior causes problems regardless of the design of the tachometer. It's especially a problem with a PLL-based design because the accuracy of the measurement and the stability of the output rely on the design of the loop filter. I'll go through a real example so you can see what I mean.

The first thing to do is determine the criteria for the design. You can change any of these things later on if you want.

1. The tachometer will read from 500 to 5000 rpm.
2. It will have a three-digit LED display.
3. It will update once a second.
4. It will work with any number of cylinders.

As I mentioned earlier, the heart of any PLL circuit is the design of the loop filter. To understand why, take a look at Fig. 1, the block diagram of a typical PLL. The output of a voltage-controlled oscillator (VCO) is routed to a phase detec-

tor. The phase detector compares the VCO's output with the input frequency and it outputs the difference between the two frequencies as an error voltage—the greater the difference, the higher the error voltage.

Feeding the error voltage back to the VCO forces the VCO to track the input frequency. The VCO output in a standard PLL circuit is a clean and squared-up version of the input frequency.

Any time you talk about comparing frequencies (or even voltages), two things have to be considered. The first one is a function of time. (How long should the sampling

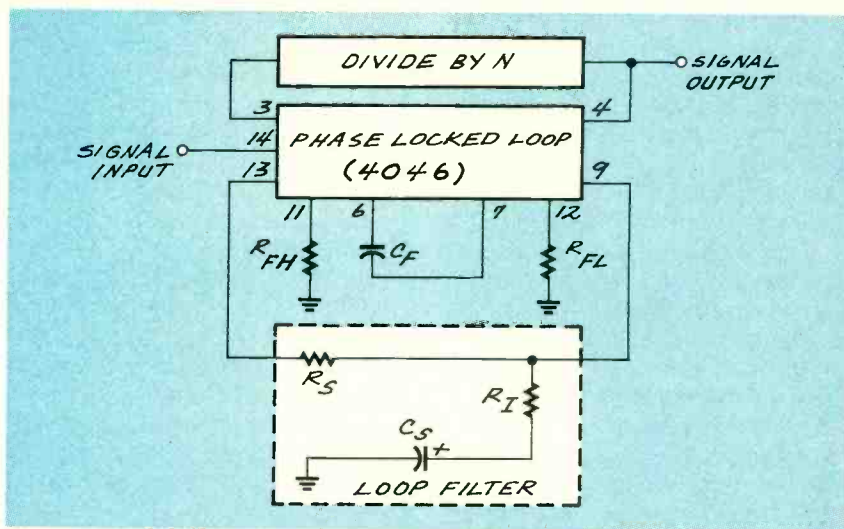


FIG. 1—THE HEART OF ANY PLL CIRCUIT is the loop filter.

# OF CYL	DEGREES/ SPARK	SPARKS/ REV	N
2	360	1	60
4	180	2	30
6	120	3	20
8	90	4	15

FIG. 2—THE SPARK RATE from the coil depends on the number of cylinders in the engine. For other engines, just divide the number of cylinders into 120 to give you the divide-by number for the PLL.

period be before the comparison is made?) The second is a function of inertia. (How quickly should the comparator respond to changes that show up during any particular sampling period?)

Those two factors are decided by the loop filter, which is why the filter is the most important part of the circuit. The loop filter in a 4046 is made up of just two resistors and a capacitor, but don't be fooled into

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taking these three components too lightly since they control the operation of the PLL. A poor design will make the tachometer worthless.

The PLL's sampling period is determined by the product of  $R_S$  and  $C_S$ , as shown in Fig. 1. If the RC period is too high, the tachometer will be sluggish, and if it's too low, the tachometer will be too erratic. The inertia of the loop is determined by  $R_I$ . If that value is too large, the tachometer will take a long time to reflect changes in the input frequency, and if it's too small, the tachometer will probably overshoot and will definitely oscillate around the input frequency.

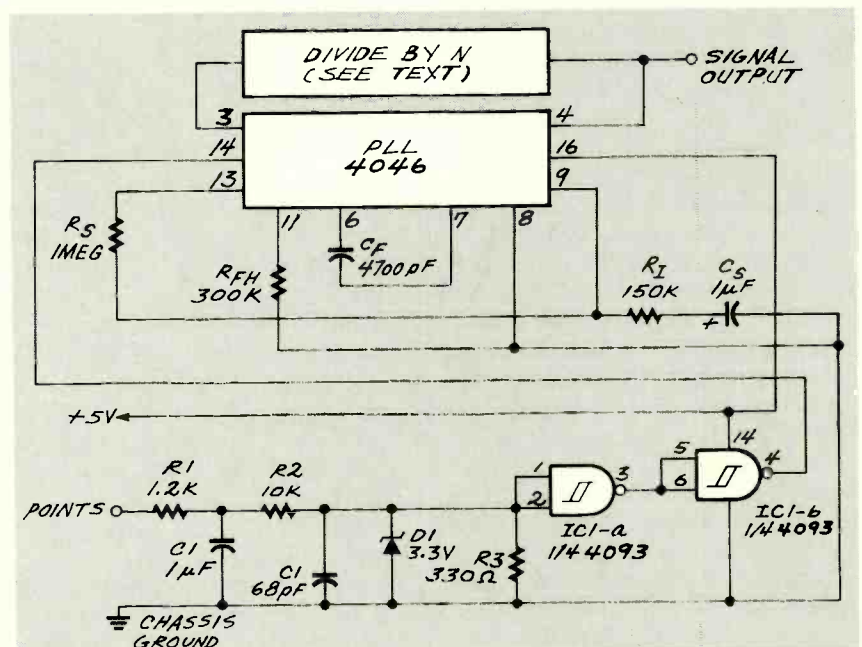
A divide-by circuit can be installed between the output of the VCO and the input of the phase detector to make the PLL even more useful. By raising the VCO center frequency to N times the expected center of the input frequency and dividing the VCO output by N before it gets to the phase detector, the VCO output can be made equal to a frequency that is N times the test input and is also locked to the test input.

This all sounds terrific but there's a catch: you have to decide what the center of the input frequency is going to be. Since the input frequency

I've been talking about is the signal from the ignition system, it's important to know what the expected spark rate from the coil is going to be. The tachometer is being designed to work with engine rpm's from 500 to 5000, and the rate of spark (from the coil, not to any particular plug) depends on the number of cylinders in the engine. I went

through this last time and I've summarized the results in the table of Fig. 2.

The tricky part of designing a tachometer with a PLL is to come up with the appropriate divide-by number for engines of different sizes. Since the circuit is counting sparks and its display should be updated every second, a conversion



**FIG. 3—THE FINAL CIRCUIT.** The loop component and VCO values are good starting points for the frequency range we agreed on.

factor that will translate the number of sparks per second into engine revolutions per second is necessary. The conversion numbers for various engine sizes are shown in Fig. 2, but if you have some other kind of engine (a five-cylinder Audi, for example), you can work out the conversion number yourself. To make things easier, just divide the number of cylinders into 120 and that will give you the divide-by number for the PLL.

Now all that's missing is the timebase for the counter and the display. Both of these sections are similar to things we've done many times before, and you should be able to design them with your eyes closed. If you keep notebooks (another thing I've talked about many times before and always encourage readers to do), you'll undoubtedly find loads of timebase and display circuits.

There are lots of ways to generate an accurate 1-hertz signal, but I think the easiest way is to use the 5369EST from National Semiconductor. A colorburst crystal connected to one end of the IC produces a 100-hertz signal out the other end. By adding a pair of 4017s to the circuit, a 1-hertz timebase for the tachometer can be produced at a very low cost.

Make sure you get the "EST" version of the 5369 chip (it produces a 100-hertz signal) rather than one with an "AA" suffix (it generates a 60-hertz signal). If all you can find is the AA version, you'll have to build a divide-by-60 circuit, but that should be no problem either—the two 4017's can divide by 60 just as easily as they can divide by 100. They just have to be wired differently.

The final circuit is shown in Fig. 3. It's a good idea to build the circuit and try it out before deciding that it's the one you want to use. The loop component and VCO values shown in the schematic are good starting points for the frequency range we agreed on, but you can play around with the values and try to tweak better performance out of the circuit. I don't think there's any way to completely avoid jitter at low engine rpm, but that's something you should determine for yourself at your own testbench.

Remember that the VCO's cen-

ter frequency is set by the capacitor straddling pins 6 and 7, and the upper frequency is set by the resistor between pin 11 and ground. An offset frequency can be added by putting a resistor between pin 12 and ground. If you leave out that last resistor, the VCO's minimum frequency will be 0. You can make a much more intelligent estimate of the starting component values by going through the manufacturer's data sheet.

Once you have the circuit assembled, connect an oscilloscope to the output and watch the waveforms as you experiment with different loop-filter component values to stabilize the tachometer output. If you see a lot of wild swings on the scope, chances are the PLL is going out of lock. If the scope shows that the PLL response is too sluggish, you'll have to change the components to reduce the loop settling time as was disclosed.

When we get together next time I'll work out the details of a second approach to tachometer design. I'll also put together a display circuit that can be used for both tachometer circuits.  $\Omega$

## Q&A

*continued from page 12*

the increase in storage space that you can obtain with compression software depends on the kind of files you have on your hard disk, there's no doubt that the software works.

The heart of this type of software is the real-time compression and decompression algorithms that write and read to the hard disk. In the early days of disk doublers, the software would occasionally cause errors that resulted in the loss of data but, these days, the whole operation is virtually invisible. The technology has improved to the point where the data is just as safe as it would be if the doubling software were not used.

Just about the only disadvantage to disk compression is that you never know for sure exactly how much room is left on the drive. That's because some kinds of data can be

compressed more efficiently than others. Text and data files can often be squeezed down to 10% of their original size, while executable and other binary files can be compressed only by about 30% or so. The claim of being able to double disk space is a statistical expectation, and not always a measurable reality. But as long as the algorithms are stable and the compression schemes are reliable, it would seem that the increase in storage space is well worth the cost of the software—usually less than \$100.  $\Omega$

## LETTERS

*continued from page 18*

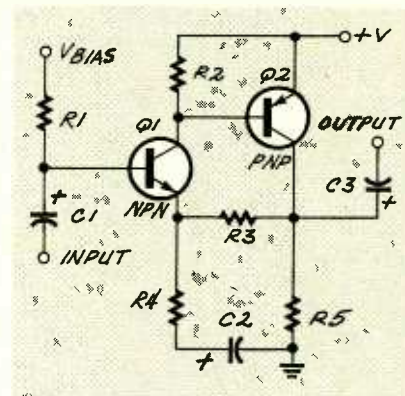


FIG. 1.

R5). The input stage collector current is easily set by R2, and the output stage collector current is easily set by R5.

The output stage operates as a current source, offering excellent power supply rejection. AC current gain is easily set with ratio of resistance values for R3 and R4. The circuit is independent of transistor characteristics, and is simple enough so that it is likely to work the first time you power it.

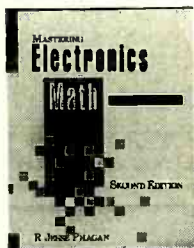
You listed no references in the article so I would like to contribute two titles: *The RCA Audio Amplifier Manual* (APA-551, 1979) is quite detailed on both with discrete components and IC's. Jack Darr's *Electric Guitar Amplifier Handbook* (Sams 21443, 1977) is even more comprehensive. It includes detailed schematics and servicing tips for various circuits.

MARK WILLIAMSON  
Rockford, IL

## NEW LITERATURE

continued from page 29

clear. He tells the reader when and why certain kinds of math are needed to solve electronics problems. The answers to all of the sample problems are given in an appendix.



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Included in this math book are explanations of scientific and engineering notation, sine waves, transformers, inductors and capacitors, time constants,

and resistance-capacitance waveshaping. This second edition has been improved with new graphs, drawings, and four new chapters covering the math related to multimeters, oscilloscopes, transistors, and computer numbering systems.

**Microterminal Catalog.** Burr-Brown Corporation, 6550 South Bay Colony Drive, Tucson, AZ 85706-7148; Phone: 800-328-2526; Fax: 602-741-4240; free.

Microterminals are small, rugged units designed as operator interface/control panels and data-collection terminals. This 12-page catalog from Burr-Brown contains product specifications, pictures, and information on key features and applica-



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tions for the microterminal product line. Discussions of accessories and peripherals are also included. The Microterminals are available in a wide variety of cases, functions, keyboards, and displays.

**Can We Talk?** Kepeco, Inc., Attn: Mrs. Alexandra Dunleavy, 131-38 Sanford Avenue, Flushing, NY 11352; Phone: 718-461-7000; Fax: 718-767-1102; free.

This six-page, four-color brochure describes Kep-

co's line of digitally controlled power supplies. It details the various communication and control options offered with Kepeco's series MBT 360-watt, instrumentation-grade, voltage-current stabilizers.

The units permit communication over the IEEE-488 bus through a two-wire serial bus that can link up to 27 units to a host



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PC, or it can communicate with an RS-232 interface.  $\Omega$

## MEASURING NI-CAD RESISTANCE

Q&A's reply to T. Ng, who asked in the February Q&A column about measuring the internal resistance of nickel-cadmium cells and batteries, was long on sarcasm and short on solid technical fact. Although Q&A apparently does not agree, the internal resistance of a battery is one of its critical specifications.

That resistance determines the battery's terminal voltage versus load current characteristic. Therefore, it determines how much current can be drawn from the battery without an objectionable drop in voltage. That resistance also determines the external voltage that must be applied to the terminals of the battery to force a given current through it for recharging.

Furthermore, Q&A's procedure for computing the internal resistance is incorrect. In general, the proper procedure requires two loads. It is easily developed by referring to the simple schematic Fig. 2.

In that diagram,  $V_b$  is the internal or open-circuit voltage of the battery, and  $R_b$  is its internal resistance.  $R_L$  is an arbitrary load

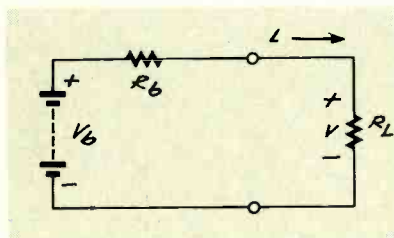


FIG. 2.

resistance, and  $V$  and  $I$  are the circuit's terminal voltage and current, respectively.

With basic circuit analysis, it can be seen that for any  $R_L$ :

$$V_b = V + R_b I.$$

For a specific load resistance,  $R_{L1}$ , the relationship becomes:

$$V_b = V_1 + R_b I_1.$$

Where  $V_1$  and  $I_1$  are the values of  $V$  and  $I$  for this load.

Similarly, for another specific load resistance  $R_{L2}$ , the relationship is:

$$V_b = V_2 + R_b I_2.$$

Equating the right-hand sides of the last two equations and solving for  $R_b$  give the desired result:

$$R_b = (V_2 - V_1) / (I_1 - I_2).$$

Thus, the internal resistance of the battery is the ratio of differences in voltage and current for the two loads.

Mathematically, the values of  $R_{L1}$  and  $R_{L2}$  are arbitrary, so one is free to choose them based on practical considerations. One convenient choice is to set an open circuit as one of the load conditions—say, resistor  $R_{L1}$ .

As a result, the corresponding current  $I_1$  is zero and the corresponding voltage  $V_1$  is  $V_b$ , the open-circuit voltage of the battery. Another choice is to set values of  $R_{L1}$  and  $R_{L2}$  that approximate the actual load anticipated for the battery. By doing that,  $R_b$  is computed as a small-signal value at the nominal operating point of the battery. DONALD M. KELLER, Ph.D., P.E. Blacksburg, VA

## ANTENNA BOOSTER CORRECTIONS

In the article "Tunable FM Antenna Booster" (May 1994, *Electronics Now*), resistor  $R1$  in Fig. 3 (Parts Placement, p. 50) should terminate on pad 3. Also  $Q1$  and  $Q2$  are specified correctly in Fig. 2 (amplifier schematic, p. 50) but incorrectly in the Parts List. Both are 2N3904 NPN transistors.  $\Omega$

## AMATEUR TV STATION

*continued from page 40*

the oscillator frequency to change about 20 kHz per volt of applied signal. About 2 to 2.5 volts p-p is required for 25-kHz deviation of the 4.5-MHz subcarrier. About 6 to 7 millivolts of audio signal is required at the base of Q4 to obtain full deviation (25 kHz).

The FM 4.5-MHz subcarrier is taken from the source of Q5 through C42. The value of C42 sets the subcarrier level; C42 also removes the DC level present at this point. If it were not removed, it might change the effective Q point of the video amplifier. The audio subcarrier is fed to the video amplifier Q7 where it is mixed with the video signal. This design makes a separate sound transmitter/RF system unnecessary.

If desired, optional switch S2 can be inserted in series with R29 to disable the audio subcarrier. This is often done in ATV work, where a separate audio link (such as a 2-meter FM) might be used instead. With this modification, it will not be necessary to turn on the video transmitter to talk, and it is useful during test and setup procedures. If S2 is not needed, install the jumper across the switch pads on the PC board.

The Mini ATV has the same audio circuitry as the 5-watt transmitter circuit with one exception. The Mini-ATV requires 9 volts to operate, so the 9-volt regulator D6 in the 5-watt version is replaced with a 6-volt diode (D3) in the Mini-ATV. Also, the varactor diode (D2 in the Mini ATV) is biased to the full 6-volt regulated voltage, through R23. The ATV Jr., of course, has no audio channel so there are no audio components on the PC board.

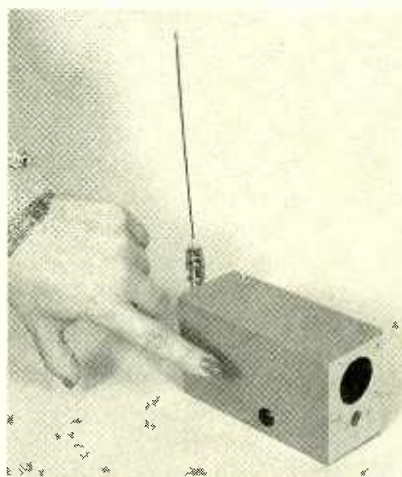
### Downconverter

The downconverter, antenna relay, and line sampler section of the 5-watt transceiver are shown in Fig. 6. If you are building only a transmitter, you can skip this section. The downconverter consists of a tuned RF

stage with a low-noise, dual-gate GASFET, a double-balanced diode mixer, an IF amplifier, and a varactor-tuned local oscillator.

Signals from the antenna pass through relay RY1 to a tap on antenna coil L16. The coil is tuned to signal frequency (420 to 440 MHz) by trimmer C43. Diodes D7 and D8 protect the gate of RF amplifier Q11 from excessive RF levels that might damage it. Transistor Q11 is biased to about 10 milliamperes drain current.

Capacitor C50, a value of about 0.6 picofarads, built into the PC board layout, couples RF into the tuned circuit consisting of C51 and L18. A tap on L18



**THIS ATV UNIT contains a built-in CCD camera module and rechargeable battery pack. It's a hand-held wireless TV transmitter in itself.**

can match the input impedance of double-balanced mixer M1 to the tuned circuit. Mixer M1 is fed with a local-oscillator signal of about +7 to +10 dBm (500 to 700 millivolts). Oscillator transistor Q13 is biased by R47, R48, and R49. The collector circuit consists of oscillator inductor L21, trimmer capacitor C57, and varactor diode D9, in series with 5.6-picofarad capacitor C58. The DC bias is applied via R51, R46, and potentiometer R50.

The setting of R50 determines the bias on D9 (from +1 to +9V). It tunes the LO frequency from 350 to 380 MHz; this will provide 60 to 72-MHz IF frequencies over the input signal range of 420 to 445 MHz.

This corresponds to channel 3 or channel 4 (VHF TV) so that a standard TV receiver can serve as an IF amplifier and display monitor for the transceiver.

Components D10, R52, C62 and C63 provide a regulated 9-volt DC source for the oscillator, and C60 provides feedback. The LO signal is fed to mixer M1 through R44 and R45 from a tap on L21. The IF signal is taken from pins 3 and 4 of M1 through lowpass filter L19 and C52, and coupling capacitor C53. The IF amplifier Q12 is biased by R43, R42, and R41. Coil L20, C56, and C57 are resonant at the IF frequency, and they match the collector circuit of Q12 to 50 to 75-ohm loads.

The downconverter has separate supply lines for the RF amplifier (TP4) and the mixer-LO-IF section (TP5). During transmit,  $V_{CC}$  is removed from the RF amplifier (Q11 and associated components), but the mixer-LO-IF is still functional. This allows the operator to pick up some transmitted signal with the downconverter and see it on the receiver—a handy feature for verifying transmission. The downconverter gain is cut from about 33 dB in its receive mode to about a 10 to 20 dB loss. If the downconverter feature is not needed and you want to disable it completely, the downconverter mixer-LO-IF lead (TP5) can be fed from +12-volts in the receive-only mode, as in the RF amplifier.

To monitor transmission quality, a line sampler circuit is included. This circuit samples the transmitted RF signal, demodulates it, and feeds the detected (demodulated) video to an emitter-follower output buffer and then to an output jack. Refer to Fig. 6. Capacitors C64 and C65 form a capacitive voltage divider across the RF power amplifier output line. About 1.5 volts of RF signal is available from the divider. Diode D11 is an envelope detector that produces a negative video signal. The video is fed through RF choke L22 to the emitter of Q14. The detected video appears across R56.

The base bias of Q14 is set at



about +3 volts through resistors R54 and R53 and bypass capacitors C66 and C67. Because Q14 is an emitter-follower, a low impedance video output is produced. Capacitor C68 couples video to the line sampler output jack. Sufficient output (about 1.5 volts) is available to drive most monitors. If more or less output is desired, change C65 to 6.8 or 15 picofarads, respectively. If a variable output is needed, substitute a trimmer with a value of 5 to 20 picofarads in place of C65. (This change was not found to be necessary in the prototypes.)

Relay RY1, a DIP reed relay, is activated through R35 and bypass C42 by voltage from the transmit supply lead. The relay has about 0.7 to 0.8 dB loss, but switching RF at 440 MHz at a reasonable cost is not easy. The relay can be omitted, and the RF output from the transmitter and the RF input to the down-converter could be brought out to separate jacks.

### Next month

That's all for this month. If you want to build any ATV unit, collect all the parts you'll need for the unit you want to build. Next month's article will tell you how to build the ATV circuits.  $\Omega$

## AUDIO UPDATE

continued from page 79

reproduced sound whose recorded acoustics are at odds with the acoustics of the room in which it is being reproduced. It just doesn't sound live. The sound is a lot more realistic when we are listening binaurally through headphones—which means no listening-room acoustics—when the listening-room acoustics are swamped out by multiple channels, or when the recording is played back in the same room it was made.

In any case, listen to some live, minimally-amplified performances against the best recorded material at hand. What differences do you hear? I would be interested to know if you think my SVA theory holds water.  $\Omega$

## WHAT'S NEWS

continued from page 6



FIG. 2—PROTOTYPE, PLASTIC, rechargeable lithium-ion battery is held by Bellcore scientist Jean-Marie Tarascon.

weigh half as much. Moreover, they say lithium-ion technology poses none of the environmental problems of the most commonly used rechargeable cells and batteries based on nickel-cadmium or lead-acid chemistry.

"This is the first plastic, solid-state rechargeable battery," says Jean-Marie Tarascon, leader of Bellcore's battery team. "It does not contain such toxic metals as lead, cadmium, mercury, or cobalt.

What's more, no liquid will leak out if the battery is cut or punctured; this makes it safer to install and use." The new power cell is a refinement of one announced by Bellcore in late 1992, which had a liquid electrolyte.

The new solid form of lithium-ion cell consists of five active layers encased in a metallized plastic bag that keeps out contaminants. Reading down from the positive side they are an aluminum mesh, a plastic anode layer containing manganese oxide (the positive pole), and then a layer of plastic that appears solid. It is actually a porous plastic structure impregnated with liquid electrolyte. Below that is the plastic cathode layer containing carbon (the negative pole), and at the bottom is copper mesh. The manufacturing process calls for fusing the layers together with heat.

When the power cell is being charged, lithium ions from the anode pass through the electrolyte layer and collect on the cathode. The reaction is reversed when current is being drawn from the cell: current flows across the terminals in the opposite direction.

According to Bellcore, their lithium-ion cell has twice the energy density of a nickel-cadmium (Ni-Cd) cell and 40% more than a nickel-metal hydride (Ni-Mhd) cell. Each cell produces a nominal voltage of

Continued on page 89

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# COMPUTER CONNECTIONS

And then there were none.

JEFF HOLTZMAN

This year is shaping up as an eventful one for the computer industry. So far, several new technologies have been introduced, and several significant business events have occurred. Those events that happened in the first quarter of 1994 will have a dramatic, long-term effect on the computer industry:

- Apple introduced the first PowerPC-based Macintoshes.
- AMD, NexGen, Cyrix, and IBM intensified the assault on Intel's dominance of the microprocessor market.
- Intel retaliated by introducing enhanced versions of its 486 and Pentium CPU's.
- Novell initiated a buyout of WordPerfect.

## PowerPC

PowerPC is an overloaded term that can mean: 1) A microprocessor, 2) A family of microprocessors, 3) A member of IBM's RS/6000 workstation family, 4) A personal computer made by IBM, 5) A personal computer made by Apple (which calls its version Power Macintosh, shown in Fig. 1).

PowerPC started out not as a microprocessor, but as a multi-chip central processing unit (CPU) complex used by IBM in its RS/6000. When IBM, Apple, and Motorola teamed up in 1991, one of their prime objectives was to build a single-chip version of that RS/6000 processor, then dubbed the PowerPC. Power, by the way, is IBM's acronym for "performance optimization with enhanced RISC." RISC is also an acronym; it stands for reduced-instruction-set computing. In stark contrast to RISC, CISC stands for complex-instruction-set computing. To understand the difference between these terms, see the sidebar "RISC vs. CISC."

Who needs PowerPC? And why?



FIG. 1—APPLE'S NEW POWERPC-BASED MACINTOSH line introduces RISC-level performance at desktop prices. SoftWindows technology from Insignia Solutions lets DOS and Windows programs run in emulation mode at 486/25 speeds.

Many analysts believe that Apple needs a RISC processor because the Motorola 680X0 microprocessor family (on which Apple's computers are based) simply ran out of steam. Without going RISC, Apple would be stuck in a dead end—or it would be faced with the prospect of moving to the Intel (or some other) platform. (That's a tactic Apple is pursuing anyway, just in case). Similarly, if Motorola were going to stay in the microprocessor market in a serious way, it would need something new.

IBM's reason for joining the PowerPC partnership is less clear. The company has a close relationship with Intel, including manufacturing rights for the 486. (IBM builds enhanced versions of the 486 and sells them as parts of both boards and systems.) Some industry observers have suggested that IBM joined the PowerPC partnership because it desperately wants to dethrone Microsoft, particularly in the operating-system market.

The PowerPC could do that because one of its key technical and marketing features is emulation technology that allows DOS, Windows, and Macintosh applications to run as-is on PowerPC machines.

Both IBM and Apple are promoting the idea that RISC provides enhanced performance, lower cost, and backward compatibility. At one time, the PowerPC triumvirate seemed to be promoting the idea that a PowerPC is a PowerPC—in other words, that compatibility would extend across the major players' product lines. It now appears that such is not the case. IBM's PowerPC boxes will run DOS and Windows software through emulation. They will also run native versions of AIX (IBM's version of Unix) and OS/2. IBM's PowerPCs won't run Apple's System 7 software or any applications written for that operating system.

Similarly, Apple's PowerPC boxes will run DOS and Windows software through emulation. They

will also run existing System 7 applications under emulation, and they will run rewritten System 7 applications in native PowerPC mode.

In both cases, the DOS/Windows emulation software is expected to provide performance equivalent to a low-end 486—but both performance and reliability remain to be seen. Many people, including myself, question whether success is possible with either. IBM, for example, has had problems keeping OS/2 compatible with successive releases of Windows. Moreover, with Chicago looming just over the horizon, IBM seems to be in for even more trouble, especially now that it no longer has rights to Windows source code.

Who will buy PowerPC boxes?

From the Apple point of view, it appears likely that the company will have no trouble converting its existing user base. Those users can benefit immediately from the extra performance that native PowerPC applications will provide, particularly for advanced graphics and multimedia development. Apple is going after the PC market as well.

Apple executives have vowed to maintain Power Mac prices several hundred dollars below those of comparable Pentium boxes. Apple can do this because a PowerPC processor can be manufactured for (by one estimate) as little as 20% of the cost of a Pentium CPU. Nonetheless, Apple will find the PC market a tough sell. This market still views Apple with suspicion. Why change

hardware platforms? Is there any compelling application software? In my view, without good answers to those questions, Apple will find it tough going indeed.

From the IBM point of view, the company will have no trouble establishing PowerPC in the RS/6000 market. But IBM has also revealed plans to conquer the mainstream desktop PC market. In fact, IBM has established a separate PowerPC division whose charter is just that. Doing so, of course, pits that division against IBM's Personal Computer Co., still the largest maker of Intel-based PCs in the world.

And where is Microsoft in all of this? Quietly porting all of its major applications to run on both IBM and Apple PowerPC boxes. In addition, Microsoft is also porting its software into a Unix-like operating system, Windows NT, to run on IBM's box. In other words, regardless of who wins the hardware wars, Microsoft seems to have all bets covered.

### RISC vs. CISC

Until March 1994, all PC's, Macintoshes, Amigas, Ataris, Apple II's, Commodores, Sinclairs, and CP/M machines were based on CISC processors. By contrast, all engineering workstations, such as those built by IBM, Digital, Hewlett-Packard, Sun, and Silicon Graphics were based on RISC processors.

How do RISC and CISC differ? RISC is based on a variation of the 80/20 rule. This rule assumes that most software spends 80% of its time executing only 20% of the available instructions. RISC processors attempt to optimize the performance of that 20%, and to keep chip size and cost down by eliminating the other 80%. RISC does in software what CISC does in silicon.

RISC processors are marked by the following characteristics: They have fewer than 150 instructions, and most instructions execute in a single processor cycle. They have many CPU registers and high clock rates. They provide instruction pipelining for simultaneous instruction fetching, decoding, and program execution.

RISC processors have a relatively small number of transistors, which contributes to their low cost. CISC processors, on the other hand, have a larger instruction set, fewer CPU registers, lower clock rates, larger numbers of transistors, and higher prices.

The division between RISC and CISC—both architectures and markets—was crystal clear until Intel

released the 486. Intel touted it as having RISC-like features (primarily pipelining and single-cycle execution of simple instructions). In terms of performance, the Pentium is even more RISC-like, but not in terms of underlying complexity, which translates into higher cost. RISC purists strongly object to calling any member of the 80X86 family RISC-like. Regardless, Intel evidently found RISC alluring enough as a marketing concept to start using it several years ago.

The PowerPC, however, is a true RISC processor—the first one designed specifically for the high-volume personal computer market. It represents the most serious attempt in the industry to wrest control over microprocessors and operating systems from Intel and Microsoft, and to transfer that control to the Apple, IBM, and Motorola partnership.

The PowerPC microprocessor is really a family of processors that includes four members, the 601, 603, 604, and 620. The 601 is the only version shipping now. It provides Pentium-level performance, but uses less power and costs less. The 603 is a low-power version for laptop computers.

The 604, which should be released in about a year, will offer twice the performance of the 601. Following that will be the 620, which if it meets current design goals, will provide truly unprecedented power for a desktop system.  $\Omega$

### Long term considerations

Hypothesize for a moment that in ten years we'll all be running RISC processors. Who'll make the chips? Who'll make the operating system?

The mainstream PC market (Intel + DOS/Windows) has one more stop—the final stop—on the highly-coupled CPU/OS line: Chicago. Chicago is going to be a better Windows than Windows. It will have a Macintosh-like user interface, along with a robust, OS/2-like, 32-bit, preemptive multitasking architecture. It will run only on Intel CISC chips. It will be highly compatible with existing DOS/Windows software.

Two or three years will probably pass before Chicago achieves the market penetration that Windows 3.1 currently enjoys. During that time, Microsoft is expected to be developing and enhancing the next version of Windows, currently code-named Cairo. Cairo will subsume everything currently part of DOS, Windows 3.1, Windows NT, and Chicago. Cairo will also be a portable operating system capable of running on Intel, PowerPC, and numerous other RISC processors. All of Microsoft's applications will also be portable among these different processors.

## TAKE BACK CONTROL

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Against this backdrop, consider Apple and IBM with their respective PowerPC boxes and operating systems. Apple has always played to the leading-edge graphics, publishing, and multimedia markets, and it seems likely that Apple's PowerPC will provide a smooth transition for those groups now. IBM, on the other hand, has no captive market that it can develop. Whatever PowerPC gains IBM is likely to make must come at the expense of the mainstream market, the workstation market, or Apple's loyal followers.

As I see it, IBM's only hope is the mainstream market. Apple followers are unlikely to convert *en masse*. Even if IBM somehow magically converted the entire workstation market, it would still be a relatively small fraction of the mainstream desktop market.

PowerPC boxes are going to appear to the PC market just as PS/2 and OS/2 1.0 did: proprietary, closed architectures foisted for no apparent reason on a market with no compelling need. Perhaps IBM will build dual-processor PowerPC machines (with the second processor an enhanced 486). It might have standard ISA/VESA/PCI buses so that existing high-volume, low-cost peripherals will be compatible. The problem is that a dual-processor PC will be expensive. Nevertheless, IBM probably knows better than any other PC manufacturer how to manufacture efficiently, so it might be able to keep costs in line.

In short, the PowerPC is going to help keep Apple afloat. In the near term, IBM can be expected to throw lots of money into this project, but it might pay off by the time the market moves to Cairo, which is expected to run on any and all processors. By that time, the market will have coalesced into just a few high-volume hardware manufacturers, and just a few high-volume software publishers.

### CPU Wars

The introduction of numerous 486 clones has forced Intel to be more competitive, and that benefits consumers tremendously. Pentium-based systems now sell for well un-

der \$3000. Systems that a year ago were high-end 486 systems now sell for under \$2000.

Intel is not standing still, however. Intel recently introduced enhanced versions of both 486 and Pentium chips. The Pentiums include 90- and 100-MHz models, which are clock-tripled 30- and 33-MHz units, respectively.

Intel's DX4 CPU's are interesting devices, perhaps even more interesting than the Pentiums. Judging from the name, you might expect that they are clock-quadrupled, but they are not. They are clock-tripled, and pick up additional speed through a larger cache (16 kilobytes) than prior 486's (8 kilobytes). There are several versions: a 100-MHz model that runs on either a 33- or 50-MHz bus; a 75-MHz model that runs on a 25-MHz bus, and an 83-MHz model that runs on a 33-MHz bus. The latter uses a  $2.5 \times$  clock for internal operations. The DX4s combine Intel's most advanced architectures, including 3.3-volt operation, 5-volt tolerant input buffers, a larger cache, and Intel's SL technology, which provides a power management mode that is important in laptops and other applications where energy conservation is critical.

### Business evolution

Novell, the largest network software company, bought WordPerfect, the market leader in word processing. Novell also bought Borland's Quattro Pro spreadsheet. So what? The deal shows just how scared software firms are of total domination by Microsoft. Look at another recently forged big-name alliance: Adobe (of PostScript fame) and Aldus (of PageMaker fame).

Now those two companies fit together. They're in the same business. They have the same customers. But Novell and WordPerfect? Look at it another way; see Table 1. In terms limited to the raw technologies available to them, the deal puts Novell and Microsoft on roughly equal footing. Now look at the Lotus column; there's a big gap at the top. Now look at the IBM column. There's a big gap in the middle. Hmmm. . . . Remember you read it here first!  $\Omega$

IBM-compatible disk, and he will return a copy of the source- and object-code files for the updated version.

The author has written another version of the firmware for the same project that will display the name of the calling party instead of the number. This is for readers who live in areas where the CNAM feature is available. Also note that the new code is available on the *Electronics Now BBS* (516-293-2283, v.32, v.42bis) as a file called CID2.ZIP.

Figure 4 is the flowchart for the updated version of the firmware. Notice that there are two separate paths, depending on whether the data is found to be SDMF or MDMF.

The program also has a few improvements. A provision has been made to determine if the area code is included in the message. (Although it's rare, one local telephone company decided to leave out the area code in its message stream.) So that the project will work with short initial ring pulses, the valid ring-detect has been decreased from 0.5 second to 0.3 second. To support longer pauses between the ring pulse and the data stream, 0.8 second has been added to the time the program is allowed to wait for a carrier detect after receiving a ring pulse.

In the original project, the channel-seize signal occasionally bled through on the data pin of the MC145447 microcontroller. Provisions have been included in the new program to fix that problem.  $\Omega$

### REFERENCES

1. Bellcore "Voiceband Data Transmission Interface Generic Requirements" Technical Reference TR-NWT-000030
2. Bellcore "Calling Number Delivery" Technical Reference TR-NWT-000031
3. Bellcore "Calling Name Delivery Generic Requirements" Technical Reference TR-NWT-001188

## PC I/O BREADBOARD

continued from page 59

access features of assembly, with the high-level control and error checking features of C. (Note that Turbo C requires a separate product, Turbo Assembler, to make use of inline assembly; Quick C has everything you need built in.)

The final example, Listing 6, is a Quick C version of the switches-in, LEDs-out program. The first line of the program instructs the compiler to include a standard library of functions for controlling the keyboard and screen. Every C program has a *main* function, which begins on the next line. Within the main function, two integers are defined: *inp* and *outp*. They correspond to the input port and the output port, respectively. It will loop forever (or until someone presses Ctrl-Break) reading the input port,

writing that value to the output port, and then checking for a key press entry through DOS.

The call to DOS has interesting features. The purpose of DOS function 11 (0Bh) is to report if a key press entry is waiting. When engaged in that function, it checks for a Ctrl-C or Ctrl-Break; either will terminate the program.

### Wrapping up

The full potential of the computer (PC or mainframe) can be realized only with effective supporting software. Your success in any technical field today requires that you have a working

### ORDERING INFORMATION

The following items are available from DAGE SCIENTIFIC, P.O. Box 144, Valley Springs, CA 95252, (209) 772-2076:

- Complete kit including manual and all parts (model ST-1)—\$119
- Set of 2 PC boards and manual (model ST-2)—\$40

All orders add \$3.95 shipping and handling. CA residents add sales tax.

knowledge of software. This has been a brief, and it is hoped, painless introduction to programming. You've seen that assembly language offers power and speed, but it requires a lot of planning and intimate knowledge of its host microprocessor to be used effectively. BASIC, on the other hand, is easy to learn and use, but it suffers from low speed, and is burdened with antiquated language constructs. For many people, C is the ideal compromise. It allows low-level access to the hardware when you need it, while simultaneously providing all the advantages of a high-level language. C is, however, more difficult to write (and read) than BASIC.

In the next part of this article, you will learn how to put the hardware and software to work in a practical project: a flexible, configurable EPROM programmer. The control software is in BASIC.  $\Omega$

## WHAT'S NEWS

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3.8 volts, compared with the 1.2 volts of the other cells.

The solid lithium-ion cells can be stacked and connected together to produce batteries with higher voltages. Because the cells are thin and flexible, they can be formed into prismatic batteries of almost any shape needed. The battery form would not be restricted by the cylindrical shapes typical of other rechargeable cells. Bellcore says that its lithium-ion cells can be discharged and charged several hundred times with less capacity loss than the other rechargeable cells.

Lithium-ion batteries with liquid electrolytes have been on the market for only about two years, but they are still developmental models for limited applications. Japan started a national project to develop distributed lithium-ion battery storage technology in 1992.

### Automated hotel check-ins

Hyatt Hotel Corporation expects

that its "Touch and Go Check-In" machine will do for hotels what the automatic teller machine (ATM) did for banking. The check-in machine, which looks and works like an ATM, allows guests with reservations and credit cards to bypass lines at the front desk and check themselves



AN AUTOMATED HOTEL registration machine, part of Hyatt Hotel's Touch and Go Check-In system, speeds up guest registration and checkout.

into their rooms directly.

Two machines are now being tested at the Hyatt Regency O'Hare hotel in a Chicago suburb and the Hyatt Regency Atlanta in Atlanta, with an eye toward their eventual use chain-wide.

Upon arrival, a guest inserts his credit card into the machine. This causes his previous room, bed, and other check-in selections to appear on the machine's monitor for his approval. When this procedure is complete—typically in less than 90 seconds—the machine dispenses one or more room keys and a printed "passport" containing the room number.

At check-out time, the guest can use the machine to approve and pay for room charges that are displayed on screen. When that transaction is complete, the machine prints out a receipt.

Hyatt Hotel plans to expand its Touch and Go Check-In program to other hotels this year. A future service that could possibly be performed by the machine would be interactive participation in the selection and the making of reservations for local restaurants.  $\Omega$

## TUNABLE ANTENNA

*continued from page 61*

ter form. Place a tap at the second turn from the grounded side of the coil, and insert a ferrite slug in the form. Coat the finished coil with clear nail polish or lacquer before soldering it into the circuit.

An F connector was installed at the bottom side of the antenna head for connecting the coaxial cable that runs between the head and the controller. The antenna itself should be mounted to the antenna-head case with a neoprene washer to keep water out of the unit. For the same reason, apply a bead of silicone sealant around the edge of the lid. The finished antenna head is shown in Fig. 3.

On the antenna-controller section, two-pole, three-position rotary switch S1 allows tuning, the use of an auxiliary antenna, or the ability to switch the unit off entirely. A two-position switch can be substituted if you do not want an auxiliary antenna. Also, because current consumption is so low, the switch can be omitted and the battery left in the circuit permanently where it might attain its rated shelf life. Use shielded cable to connect components S1, R4, and J2-J4 to the rest of the circuit.

Do not use an alkaline 9-volt battery because it could provide too much current for proper operation. Instead, install a carbon-zinc battery. Warning! Do not take the required 9-volt power from the internal circuitry of your shortwave receiver, even if the antenna controller is built into the receiver. House the controller in a metal case, because it will provide the best RFI shielding. Figure 4 shows the prototype controller.

When the unit is completed, allow a "burn-in" period for the tuning diode. Perform burn in by installing a battery, turning the unit on, and allowing the silicon crystal structure of the diode to settle with a few hours of operation. That step proved to be necessary for many of the units built.  $\Omega$

## THE LED-HEAD

*continued from page 48*

to mount the circuit board in a suitable plastic box. The size of the box will, of course, be determined by your choice of power—battery or adapter. If you use the four cells, you can mount the holder in the bottom of the box; if you choose an adapter, mount the jack on the side of the box.

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## RELAY OUTPUT CIRCUITS

*continued from page 54*

ever, the period is determined by the switch position to either electrolytic capacitors C1 (minutes) or C2 (seconds), until the relay turns off.

At that time, the control contacts reopen and break the power connections to the circuit. The timing cycle is then complete. This circuit can be turned off part way through its timing cycle by pushing RESET switch S3.

Standard aluminum electrolytic capacitors have very wide capacitance tolerance values (typically -50% to +100%). Moreover, they exhibit relatively large and unpredictable leakage currents. Consequently, their use in simple circuits such as those shown in Figs. 13 and 14 make them unsatisfactory for precise timing of relay contact functions. Also, they are unable to time periods longer than about 15 minutes.

Figures 15 and 17 show two accurate, long-period relay timer-control circuits whose functions do not depend on electrolytic capacitors. Film dielectric capacitors have been substituted. In both of those circuits, IC1 is configured as a free-running astable multivibrator.

In Fig. 15 schematic, a two-range, 1 to 10 minute and 10 to 100 minute relay timing control circuit, the astable frequency is divided down by IC2, a CD4020B CMOS, 14-stage, ripple-carry binary divider. Consequently relay RY1 turns on as soon as switch S1 is closed, and it turns off again when the 8192nd astable pulse arrives. This provides time periods from 1 to 100 minutes, depending on the position of switch S2.

Figure 16 shows the functional and pinout diagrams of the CD4020B 14-stage binary counter. All counter stages are master-slave flip-flops. The state of a counter advances one count on the negative transition of each input pulse, and a high level on the RESET line resets the counter to its all zeros state. All inputs and outputs are buffered.

The Fig. 17 circuit is similar to that of Fig. 15 except that an additional decade-divider stage is substituted for position 3 of switch S2. This gives a maximum division ratio of 81,920, making it possible to time for periods of up to 20 hours. This circuit is found in battery chargers and area security lighting systems with time-controlled turn-off.

Figure 18 shows the functional and pinout diagrams of the CD4017B decade counter IC, a five-stage Johnson counter with 10 decoded outputs. Inputs include a CLOCK, a RESET, and a CLOCK INHIBIT signal.

Time-delay relays are coil and contact EM relays with built-in timing circuits that delay contact openings or closings for a preset interval. The time delays are generated by an internal RC circuit or by counting cycles on a 50- or 60-Hz AC power line. The time delays are set with either a knob or a DIP switch on the relay.  $\Omega$

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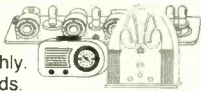
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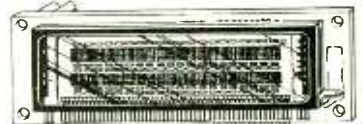
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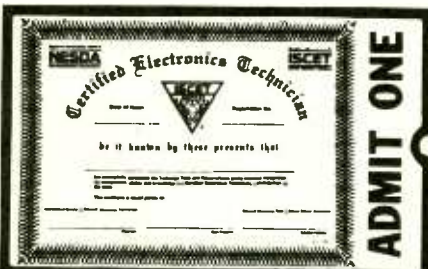
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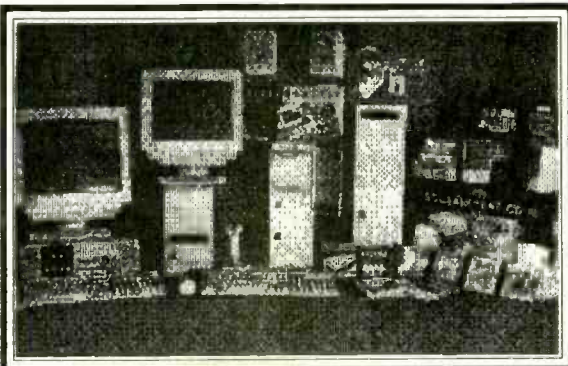
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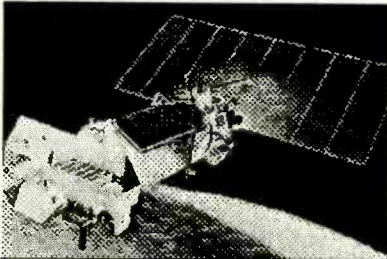
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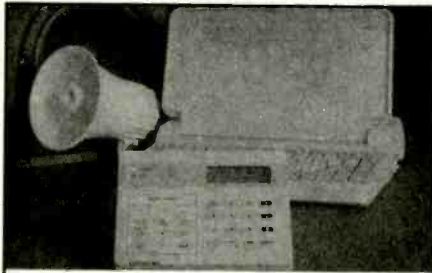
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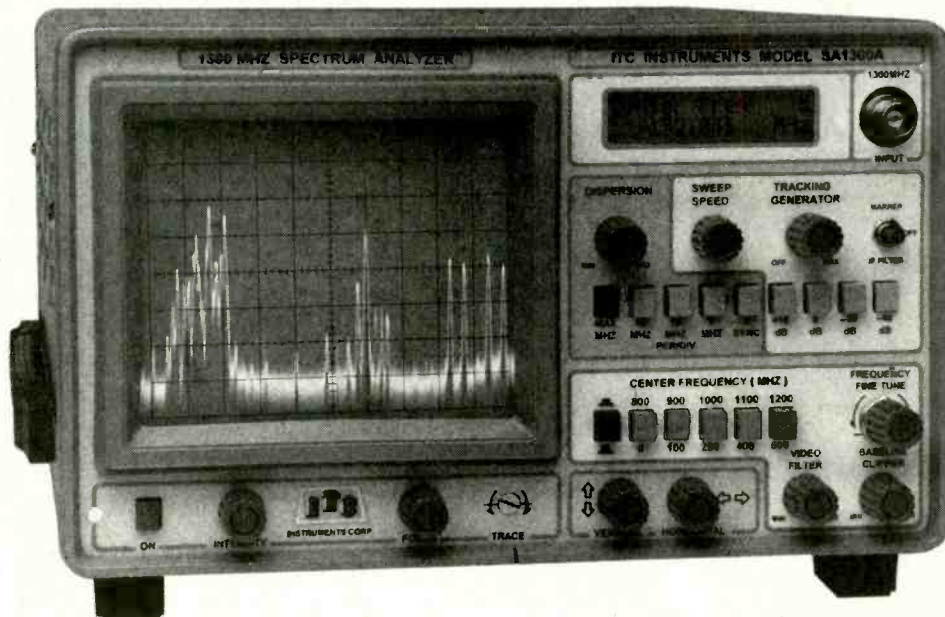


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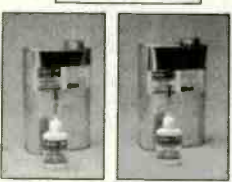
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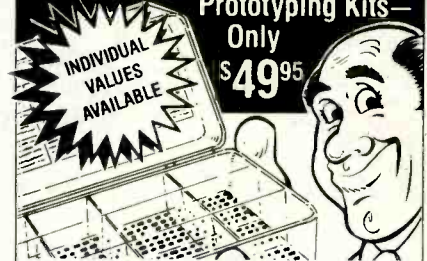
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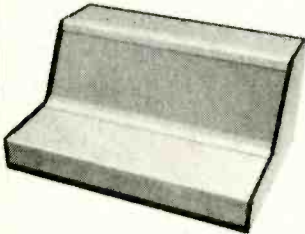
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**DUAL SLOPE METAL CABINETS**

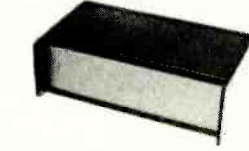
MODEL	DESCRIPTION	PRICE
MAJOR DIM.	SECONDARY DIM.	
W x D x H (inches)	W x D x H (inches)	
DS-1	4 x 6 x 4 x 12 x 19 x 2.4 x 1.8	59.00
DS-2	6 x 6 x 4 x 12 x 19 x 2.4 x 1.8	83.25
DS-3	8 x 6 x 4 x 12 x 19 x 2.4 x 1.8	67.50
DS-4	10 x 6 x 4 x 12 x 19 x 2.4 x 1.8	71.50
DS-5	12 x 6 x 4 x 12 x 19 x 2.4 x 1.8	76.00
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DS-8	6 x 8 x 6 x 2 x 3.1 x 3.5 x 1.9	73.00
DS-9	8 x 8 x 6 x 2 x 3.1 x 3.5 x 1.9	78.00
DS-10	10 x 8 x 6 x 2 x 3.1 x 3.5 x 1.9	82.75
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2RU7	19 x 7 x 3.5	35.25
2RU10	19 x 10 x 3.8	37.50
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MC-5A	6 x 4 x 3	20.95
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MC-8A	6 x 7 x 4	23.15
MC-9A	8 x 7 x 4	25.75



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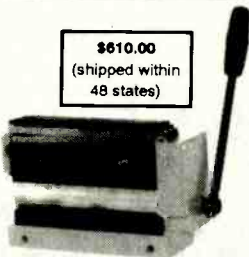
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3RU10 HD	19 x 10 x 5.25	121.00
3RU14 HD	19 x 14 x 5.25	134.00
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4RU10 HD	19 x 10 x 7.0	129.00
4RU14 HD	19 x 14 x 7.0	134.00
5RU7 HD	19 x 7 x 8.75	126.00
5RU10 HD	19 x 10 x 8.75	133.00
5RU14 HD	19 x 14 x 8.75	143.00

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PUNCH 8	13/16" ROUND	12.95
PUNCH 9	7/8" ROUND	12.95
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PUNCH 11	1-1/16" ROUND	13.95
PUNCH 12	1-1/8" ROUND	13.95
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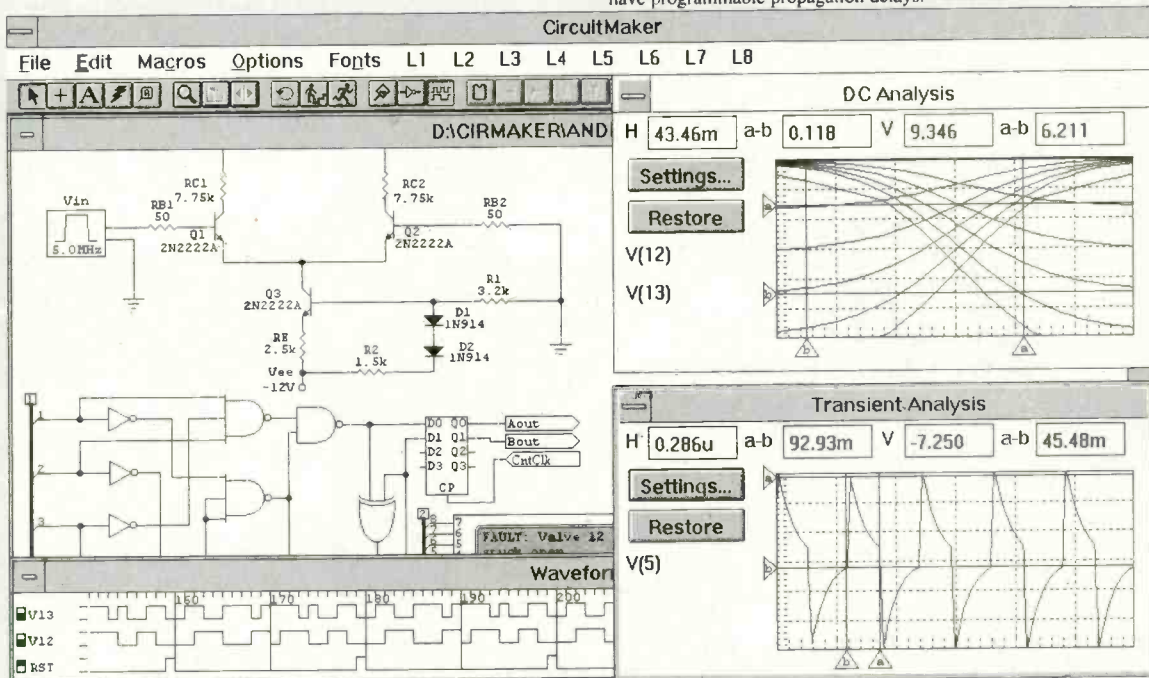
**CircuitMaker's** analog simulation results are shown in graph windows that provide powerful, interactive analysis options. You can plot multiple waveforms by clicking on the desired nodes and can select linear or logarithmic axes. Horizontal and vertical cursors facilitate quick and accurate measurements. You can also zoom in on any portion of the graph to obtain additional detail.

**Electronics Workbench** offers a single, small scope or Bode plot instrument window. The windows are not sizeable and only two waveforms can be plotted at a time. EWB has a single measurement cursor and provides no direct way to read results from the instruments.

### Superior Digital Simulation

**CircuitMaker** has an exclusive Trace feature where the state of every node is indicated in color as the simulation runs. You can monitor as many waveforms as your screen will allow, set edge or level breakpoints for analysis, and interactively see the state of any node by touching the logic probe to it. The data sequencer provides 1024 words of pattern data. Additional digital instruments include ASCII and HEX input keys and an ASCII display. CircuitMaker includes tri-state devices and devices have programmable propagation delays.

**Electronic Workbench** has no interactive logic probe or Trace capability and no Hex or ASCII keys. Their "word generator" is limited to 16 words. EWB does not have tri-state devices and digital devices do not have programmable propagation delays.



### Comprehensive Device Libraries

**CircuitMaker** includes libraries containing programmable, TTL, CMOS, generic analog and digital devices, and many powerful I/O devices. With CircuitMaker's macro function you can quickly and easily create your own functional devices and symbols. Now that's giving you the tools you need to get the job done right!

**Electronics Workbench** ships with only 17 digital devices. If you want additional devices you pay extra.

Comparison based on CircuitMaker 2.0 for Windows and Electronics Workbench 3.0 for Windows. All product and company names are trademarks of their respective owners.

### High-Performance Schematic Capabilities

**CircuitMaker** puts you in control of your schematic with SmartWires<sup>™</sup>, bussing, page connectors, and rubberbanding. You can label devices and pins, add fully stylized multi-line text, and create a parts list or netlist. With the Macro feature you can add user defined symbols to your device library.

**Electronics Workbench** dictates wire placement to you. EWB limits your overall "workbench" layout to 1 x 2 pages. EWB has no bussing, page connectors, pagebreaks, print scaling, labeling, free text fields, netlisting, zoom, undo, and no Toolbar or Toolbox.

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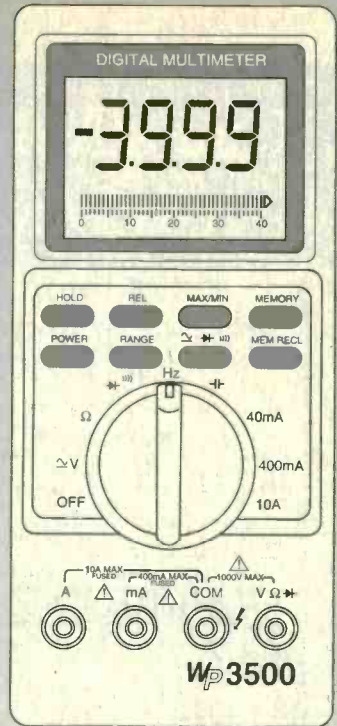
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**Shoreline**  
INSTRUMENTS

- 2000 Count Digital Display
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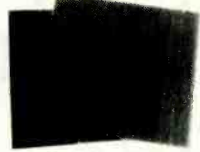
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**TOTAL COST FOR SHIPPING OF ANY ONE, OR AS MANY OF THE FOLLOWING ITEMS BY AIR MAIL IS \$15**

**ALL PRICES ARE IN U.S. DOLLARS**

\*\*\*\*\*  
\* **FIBRE OPTIC TUBES** \*

**UNIVERSAL SOLAR CHARGER KIT**

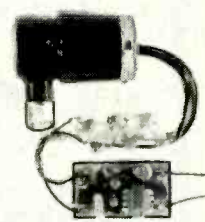


Two 6" x 6" amorphous glass solar panels, and a PCB and all on-board components kit for a solid state inverter. In normal sunlight, the combination can deliver a charging power of over 1.4 Watts into 5-12V batteries. EG 6V-230mA, 9V-150mA, 12V-120mA. The glass panels need to be terminated and have their rear waterproofed. Simple to do, instructions included.

**\$20**

For the two panels, PCB and components, terminating clips and the instructions.

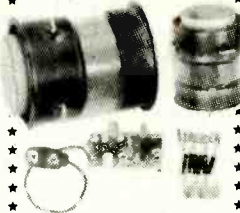
**IMAGE INTENSIFIER TUBE AND SUPPLY**



These are the key components needed for making a PASSIVE NIGHT VIEWER. The small prefocussed Russian image intensifier tube only requires a low current EHT power supply to make it operational, which we provide in kit form. Draws 20mA from a small 9V battery. With a suitable low light objective lens (not provided) the resultant viewer will produce useful pictures in sub-moonlight illumination, and it can also be IR assisted. **INCREDIBLE PRICE:**

**\$105**

for the Russian image intensifier tube and an EHT power supply kit! All that is needed to make a complete passive night viewer is a lens, an eyepiece, a 9V battery, a case and a switch. We can supply a matching lens and eyepiece. **\$68 for the pair.**



These US made tubes are "pulls" from equipment, in excellent condition. Have 25/40mm diameter, fibre-optically coupled input and output windows. The 25mm tube has an overall diameter of 57mm and is 60mm long. The 40mm tube has an overall diameter of 80mm and is 92mm long. The gain of these is such that they would produce a good image in approximately 1/3 moon illumination when used with suitable "fast" lens, but they can also be IR assisted to see in total darkness. The superior resolution of these tubes would make them suitable for low light video preamplifiers, wild life observation, and astronomical use. **INCREDIBLE PRICES:** Each of the tubes is supplied with a 9V-EHT power supply kit. **INCREDIBLE PRICES:**

**\$85** For the 25mm intensifier tube and supply.

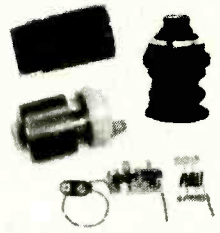
**\$130** For the 40mm intensifier tube and supply.

Three of these tubes can be cascaded to make a very high gain image intensifier! We should have a kit and instructions available to make these. Approximately \$195 for 25mm and \$320 for 40mm, three stage kits. Resellers enquiries welcome.

**MISCELLANEOUS ITEMS COMPONENTS AND KITS**

- High Voltage Diodes 8KV-3mA, \$0.80; 10KV-20mA, \$1.40
- High Voltage Disc Ceramics: 0.01uF-3KV, \$0.80; 0.01uF-5KV \$1.30, 1000pF-15KV, \$3.50
- Electric Fence Kit: PCB and components, \$28. Garage-Door-Gate Remote Control Kit: Tx \$13; RX \$56. Laser Beam Communication Kit TX, RX, plus IR Laser, \$39.
- Plasma Ball Kit: PCB and components kit, needs only bulb \$18
- IEC Extension Leads: 2 meters long \$3.50 High Intensity Led's: 550-1000mCD output of 20mA, 5mm diameter, 10 for \$2.80.
- Triacs: 60A-600V Stud mounted THOMPSON type T6AL606 \$7.20.
- Ultrasonic Transducers: Murata brand (Japanese), 40KHz TX-Rx Pair, \$1.50

**IR "TANK SET"**

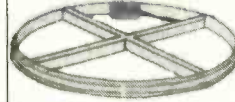


**ON SPECIAL** is a set of components that can be used to make a very responsive Infra Red night viewer. The matching lens tube and eyepiece sets were removed from working military quality tank viewers. We also supply a very small EHT power supply kit that enables the tube to be operated from a small 9V battery. The tube employed is probably the most sensitive IR responsive tube we ever supplied. The resultant viewer requires low level IR illumination. Basic instructions provided

**\$85**

For the tube, lens, eyepiece and the power supply kit. When ordering specify preference for a wide angle, or a telescopic objective lens.

**MIRACLE TV ANTENNA KIT**

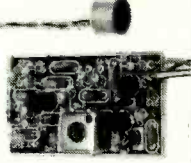


This combination of proven circular antenna design, and a wideband low noise amplifier produces remarkable results on VHF, UHF, and FM frequencies. Based on an IC with 20dB of gain, a bandwidth of 2GHz and a noise figure of 3dB. Can be used as a masthead amplifier on existing antennas. The cost of the complete kit of parts for the masthead amplifier PCB and components, the power and signal combiner PCB and components, a balun core and the tinplate for the antenna is priced at only:

**\$18**

Requires a DC supply (Plugpack etc.) 7V-20V DC at approximately 25mA. Extra reinforcement for the tinplate antenna is also required.

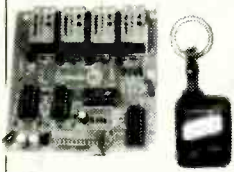
**FM TRANSMITTER KIT - MKII**



This low cost FM transmitter features pre-emphasis, high audio sensitivity as it can easily pick up normal conversation in a large room, a range of well over 100 meters, etc. It also has excellent frequency stability. Specifications: Tuning range: 88-108MHz. Supply voltage 6-12V, current consumption @ 9V: 3.5mA, Pre-emphasis: 7.5uS, Frequency response: 40Hz to greater than 15KHz, S/N ratio: Greater than 60dB, Sensitivity for full deviation: 20mV, Frequency stability with extreme antenna movements: 0.03%, P.C.B. dimensions: 1" x 1.7". Construction is easy and no coil winding is necessary. The coil is preassembled in a shielded metal can. The double sided, solder masked and screened PCB also makes for easy construction. The kit includes a PCB and all the on-board components, an electret microphone, and a 9V battery clip.

**\$8**

**FOUR CHANNEL UHF REMOTE CONTROL KIT**



Features a 3 channel transmitter which is small enough to fit onto a key ring. The fourth channel can be accessed by a second transmitter. For example each of the two transmitters could have two common channels and one individual channel. The compact receiver employs a ready made and predigined (304MHz) UHF receiver "front end" module. Over 100 meters range, has 12A SPDT relay contact outputs, has a user programmable security code with 6561 combinations, easy to construct, is expandable, etc. Transmitter: \$13. Receiver: \$46. **TWO TRANSMITTERS AND ONE RECEIVER: \$68**

The operating frequency of the system is adjustable but you should check local regulations with regards to using this very low power remote control system.

**FM TRANSMITTER MK1 KIT**



This unit has most of the features of our FMTXMK2 transmitter, but is much smaller. The complete transmitter PCB (Miniature microphone included) is the size of a "AA" battery, and is powered by a single "AA" battery. We use a two "AA" battery holder (provided) for the case, and a battery clip (shorted) for the switch. Estimated battery life is over 500 hours!! **SAME PRICE AS OUR FMTXMK2:**

**\$8**

**PASSIVE NIGHT VIEWER**



This is a completed commercial monocular hand held night viewer, that employs an image intensifier tube. The viewer is of a USSR military standard (model T3C-2), and will produce useful images in very low ambient light. Has adjustable low light objective lens, adjustable eyepiece, and is supplied with a carry case.

**\$280**

**SOLID STATE "PELTIER EFFECT" COOLER - HEATER**

These are the major parts needed to make a solid state thermoelectric cooler - heater. We can provide a large 12V-4.5A Peltier effect semiconductor, two thermal cut-out switches, and a 12V DC fan for a total price of:

**\$32**

We include a basic diagram - circuit showing how to make a small refrigerator - heater. The major additional items required will be an insulated container such as an old portable cooler. Two heatsinks, and a small block of aluminium.

**INFRA RED FILTER**

A very high quality IR filter and a RUBBER lens cover that would fit over most torches including MAGLITES, and convert them to a good source of IR. The filter material withstands high temperatures and produces an output which would not be visible from a few meters away and in total darkness. Suitable for use with passive and active viewers.

**\$11**

For the filter and the rubber lens cover.

All our kits are provided with high quality fibreglass, silk screened and solder masked, printed circuit boards

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- OPTREX 1x16 "Backlit"-DMC 16187-  
8 Bit ASCII Input Dim. 3 1/4x1 3/8x9/16  
Char. Height. 11" ..... **\$9.95**
- OPTREX 1x20-DMC 20171-8 Bit ASCII Input  
Dim. 7 9/16x1 9/16x1/2 Char. Height. 42" ..... **\$9.95**
- OPTREX 2x40-DMC 40218-8 Bit ASCII Input  
Dim. 7 9/16x1 9/16x1 3/32 Char. Height. 19" ..... **\$9.95**

**VERY EASY TO INTERFACE TO ALMOST ANY MICROPROCESSOR!!!!!!**

## STEREO AUDIO AMP

This 20 watt per channel, open frame, stereo audio amp comes completely assembled and tested. It also includes a self contained plug-in power supply. Less than .1 % distortion for you real "audio buffs". You supply the speakers and we will supply some of the cleanest audio you have heard. Unit includes volume, tone, and balance controls. Front panel measures 9"x3".

**A steal at ..... \$12.95**

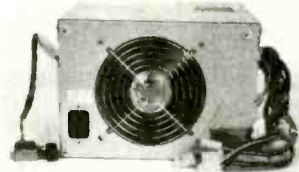


## SWITCHING POWER SUPPLIES

### DELTA Switching Power Supply

Heavy duty switcher—A full 280 watts completely enclosed w/fan—UL and CSA approved— + 12V @ 7 amps— + 5V @ 37 amps  
-5V @ .75 amps—  
-12V @ .75 amps.  
Measures 8 1/2"x  
5 15/16"x7 3/8"

**\$17.95**



## SIRENS

Simply apply 12 volts to this little baby, then you had better hold your ears. Very loud!

**\$5.95**

Great for car and intrusion alarms



## DTMF

- SSI-202 Decoder **2.25**
- 8870 Decoder **2.25**
- 5087 Generator **2.00**
- 5089 Generator **1.25**

## UART

- NS16450 ..... 6.50
- 16550 ..... 10.95
- TR1602B  
(COM 2017) .... 1.75
- IM6402 +5v High speed  
AY5-1013 pin out 2.45
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- 2016-2KK8 200 n.s. .... 1.00
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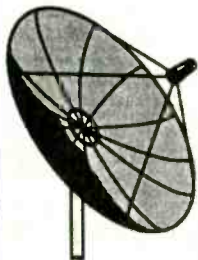
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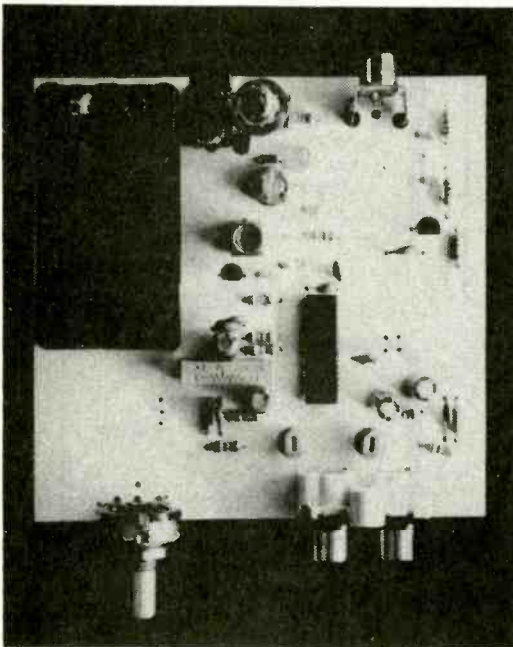
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By Staff Writer

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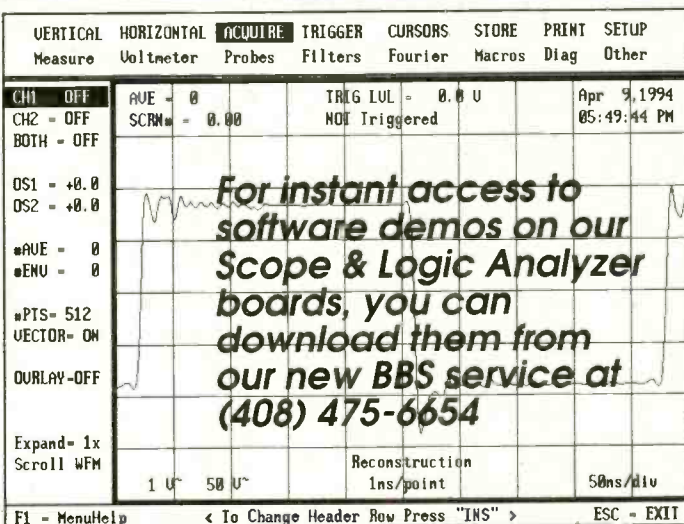
These boards have completely independent vertical channels, each with their own 25 or 40 megasample/sec 8-bit A/D converter, 32K static ram, and 10 vertical gain settings (in 1,2,5 steps). This gives you the same high performance whether you are using one channel or multiple channels simultaneously. Also, in addition to 27 timebase settings (in 1,2,5 steps), there is a user programmable mode for sweeps as slow as 1 month/division.

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Maximum Digitizing Rate						
(two channel simultaneous)	40 Ms/sec	40 Ms/sec	25 Ms/sec	25 Ms/sec	40 Ms/sec	40 Ms/sec
Time Base Range	5ns-2sec/div	5ns-2sec/div	5ns-2sec/div	5ns-2sec/div	5ns-2sec/div	5ns-2sec/div
Maximum Time Resolution	1ns	1ns	4 ns	4ns	1ns	1ns
Vertical Resolution	8-bit	8-bit	8-bit	8-bit	8-bit	8-bit
Vertical Sensitivity	5mV-5V/div	5mV-5V/div	10mV-10V/div	10mV-10V/div	5mV-5V/div	5mV-5V/div
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	74197	.85	74LS166	65	74S23	35	74F257	79	74HC157	49	LM555	59	CA3130	89	2764	3.95	78L29	59	4N29	79
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	74200	.40	74LS170	69	74S26	35	74F260	69	74HC160	69	LM555	1.59	CA3160	1.09	2768A	4.50	78L29	59	4N32	79
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	74207	.40	74LS177	49	74S33	35	74F267	69	74HC167	69	LM555	1.09	CA3167	1.99	2768A-2	3.75	78L29	59	4N39	79
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	74210	.40	74LS180	49	74S36	35	74F270	69	74HC170	69	LM555	1.09	CA3170	1.99	2768A-2	3.75	78L29	59	4N42	79
	74211	.40	74LS181	49	74S37	35	74F271	69	74HC171	69	LM555	1.09	CA3171	1.99	2768A-2	3.75	78L29	59	4N43	79
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	74215	.40	74LS185	49	74S41	35	74F275	69	74HC175	69	LM555	1.09	CA3175	1.99	2768A-2	3.75	78L29	59	4N47	79
	74216	.40	74LS186	49	74S42	35	74F276	69	74HC176	69	LM555	1.09	CA3176	1.99	2768A-2	3.75	78L29	59	4N48	79
	74217	.40	74LS187	49	74S43	35	74F277	69	74HC177	69	LM555	1.09	CA3177	1.99	2768A-2	3.75	78L29	59	4N49	79
	74218	.40	74LS188	49	74S44	35	74F278	69	74HC178	69	LM555	1.09	CA3178	1.99	2768A-2	3.75	78L29	59	4N50	79
	74219	.40	74LS189	49	74S45	35	74F279	69	74HC179	69	LM555	1.09	CA3179	1.99	2768A-2	3.75	78L29	59	4N51	79
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	74221	.40	74LS191	49	74S47	35	74F281	69	74HC181	69	LM555	1.09	CA3181	1.99	2768A-2	3.75	78L29	59	4N53	79
	74222	.40	74LS192	49	74S48	35	74F282	69	74HC182	69	LM555	1.09	CA3182	1.99	2768A-2	3.75	78L29	59	4N54	79
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	74224	.40	74LS194	49	74S50	35	74F284	69	74HC184	69	LM555	1.09	CA3184	1.99	2768A-2	3.75	78L29	59	4N56	79
	74225	.40	74LS195	49	74S51	35	74F285	69	74HC185	69	LM555	1.09	CA3185	1.99	2768A-2	3.75	78L29	59	4N57	79
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	74231	.40	74LS201	49	74S57	35	74F291	69	74HC191	69	LM555	1.09	CA3191	1.99	2768A-2	3.75	78L29	59	4N63	79
	74232	.40	74LS202	49	74S58	35	74F292	69	74HC192	69	LM555	1.09	CA3192	1.99	2768A-2	3.75	78L29	59	4N64	79
	74233	.40	74LS203	49	74S59	35	74F293	69	74HC193	69	LM555	1.09	CA3193	1.99	2768A-2	3.75	78L29	59	4N65	79
	74234	.40	74LS204	49	74S60	35	74F294	69	74HC194	69	LM555	1.09	CA3194	1.99	2768A-2	3.75	78L29	59	4N66	79
	74235	.40	74LS205	49	74S61	35	74F295	69	74HC195	69	LM555	1.09	CA3195	1.99	2768A-2	3.75	78L29	59	4N67	79
	74236	.40	74LS206	49	74S62	35	74F296	69	74HC196	69	LM555	1.09	CA3196	1.99	2768A-2	3.75	78L29	59	4N68	79
	74237	.40	74LS207	49	74S63	35	74F297	69	74HC197	69	LM555	1.09	CA3197	1.99	2768A-2	3.75	78L29	59	4N69	79
	74238	.40	74LS208	49	74S64	35	74F298	69	74HC198	69	LM555	1.09	CA3198	1.99	2768A-2	3.75	78L29	59	4N70	79
	74239	.40	74LS209	49	74S65	35	74F299	69	74HC199	69	LM555	1.09	CA3199	1.99	2768A-2	3.75	78L29	59	4N71	79
	74240	.40	74LS210	49	74S66	35	74F300	69	74HC200	69	LM555	1.09	CA3200	1.99	2768A-2	3.75	78L29	59	4N72	79
	74241	.40	74LS211	49	74S67	35	74F301	69	74HC201	69	LM555	1.09	CA3201	1.99	2768A-2	3.75	78L29	59	4N73	79
	74242	.40	74LS212	49	74S68	35	74F302	69	74HC202	69	LM555	1.09	CA3202	1.99	2768A-2	3.75	78L29	59	4N74	79
	74243	.40	74LS213	49	74S69	35	74F303	69	74HC203	69	LM555	1.09	CA3203	1.99	2768A-2	3.75	78L29	59	4N75	79
	74244	.40	74LS214	49	74S70	35	74F304	69	74HC204	69	LM555	1.09	CA3204	1.99	2768A-2	3.75	78L29	59	4N76	79
	74245	.40	74LS215	49	74S71	35	74F305	69	74HC205	69	LM555	1.09	CA3205	1.99	2768A-2	3.75	78L29	59	4N77	79
	74246	.40	74LS216	49	74S72	35	74F306	69	74HC206	69	LM555	1.09	CA3206	1.99	2768A-2	3.75	78L29	59	4N78	79
	74247	.40	74LS217	49	74S73	35	74F307	69	74HC207	69	LM555	1.09	CA3207	1.99	2768A-2	3.75	78L29	59	4N79	79
	74248	.40	74LS218	49	74S74	35	74F308	69	74HC208	69	LM555	1.09	CA3208	1.99	2768A-2	3.75	78L29	59	4N80	79
	74249	.40	74LS219	49	74S75	35	74F309	69	74HC209	69	LM555	1.09	CA3209	1.99	2768A-2	3.75	78L29	59	4N81	79
	74250	.40	74LS220	49	74S76	35	74F310	69	74HC210	69	LM555	1.09	CA3210	1.99	2768A-2	3.75	78L29	59	4N82	79
	74251	.40	74LS221	49	74S77	35	74F311	69	74HC21											

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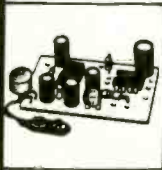
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## SUPER SNOOPER BIG EAR

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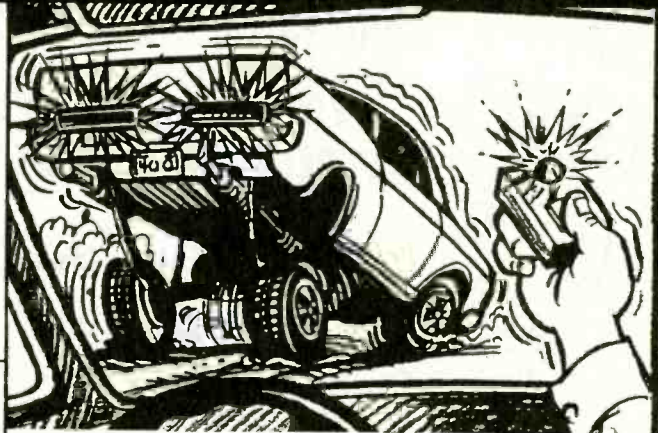
away. The BIG EAR can be hidden about anywhere. Makes an ultra-sensitive intercom. Can be used as a 1.5W AMP. We supply a mini-electret mike in the kit. 1"x1.75" 6 to 12VDC AA-1 **\$10.95**



## PHONE TRANSMITTER

Small but mighty, it fits anywhere. Phone line powered, never needs batteries. Transmits both sides of a phone conversation loud and clear, wireless, to any FM radio at great distances. Variable tunes from 70MHz TO 130MHz FM. You can also use it as a speaker phone. Size .5"x1"

TEL-B1 **\$12.95**



**THE ZAPPER** activates any radar detector within 3/4 of a mile. Check the brake lights of that sports car that just went by 90 miles an hour. Back off those 18 wheelers trying to eat your back bumper. Put the fun back in driving. THE ZAPPER is a 10GHz amateur transmitter the size of a cigarette pack, operates on a 9v battery, when the button is pushed, brake lights and radar detector light the skies. Complete with the rules of the new ROAD WARRIOR GAME... TROLLING FOR TAIL LIGHTS, America's fastest growing highway participatory sport. **Built \$49.95 Kit \$39.95**



## PHONE RECORDING SWITCH

This phone line powered switch is small enough to be installed anywhere. Every time the phone is picked up the recorder will record both sides of the conversation automatically. Use it in your office to record all phone calls so you don't lose important information. 1"x.6"

TEL-SW1 **\$12.95**



## STROBE LIGHT

If you need an attention getter, warning light, or flashing light for model airplanes, then this kit is for you. Use it as an emergency light for your auto, radio tower, even use it on your bicycle. Has a variable flash rate. Size 3.5"x1.8" operates on 6 or 12V DC only.

ST-1 **\$9.95**

**DIGITAL THERMOMETER**  
The DT-3 kit will turn your digital volt meter into an accurate digital thermometer with .1 degree resolution. Measures temperature from -40F to 250F degrees. It has a remote sensor 25" SQ. and can be mounted many feet away from the meter. Size 1.5x1.2" 9vDC  
DT-3 **\$8.95**

**CAPACITANCE METER**  
This kit will turn your digital volt meter into a capacitance meter. Turn that junk box of unmarked capacitors into a fortune of usable parts. Measures capacitors from <2.2pF to 2.2uF. 1.75"x2" 9vDC  
CA-1 **\$12.95**

**VOLTAGE MONITOR**  
This kit has 7 multi-colored leds to monitor your 12, 8, or 5V DC systems. Build it to work in 1v, 1/2v, or 1/4v steps. Great for nicad packs, autos, boats, mobile homes, or battery chargers. P.C.B. 1.3"x2.7"  
VM-1 **\$7.95**

**BLINKEY LIGHT**  
This kit is perfect for decorating hats, name badges, & model trains. Add a box, set it on the dash of your car, use it as an auto burglar alarm. Comes with 2 alternate flashing leds. Size .5"x.5" 9 to 12VDC  
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FOR CHANNELS 2 thru 22 ONLY  
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This VOX circuit can be used to operate a tape recorder, ham radio, CB radio, or turn on an alarm. The VOX-1 kit has 100MA of output. That operates a relay, light, motor, or ? What could you do with a sound activated switch? Size 1.5"x1.3" 7.5 TO 18VDC  
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Ideal for preamp for scanners, hand held radios, frequency counters. Amplifies low level (weak) signals. If the signal is extremely low 2 amps can be used in series. 1MHz TO 2.5MHz @ 2.8dB nf 1dB compression = +0 dBm gain: 1MGHz-20dB to 2.5GHz-6dB Requires 12VDC @ 16Ma  
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**TY-25 ▲** Super fast acting relay protects speakers against destructive DC voltages. Can connect directly to a power amplifier or can use a separate power supply. Has a 3 second turn-on delay to avoid turn-on thumps. (1 lb.)  
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**1R-503 ▲▲** It is short circuit proof and has overload protection. Output voltage is variable over a range of 0-50 volts. Current limit trip is adjustable up to max of 3A. May use Mark V #002 transformer. (1 lb.)  
 Kit: \$ 17.75



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**TY-2 ▲ (1 lb.)** This unit drives 6-40 watts fluorescent light for portable and emergency use. Works from a 7.2-16 VDC battery. Includes a "Hi-Efficiency Switching Mode IC Driving Circuit" suitable for use with different lights.  
 Kit: \$ 11.97



### 120-250W MOSFET POWER MONO AMPLIFIER AF-2 (6 lbs.) ▲▲

Power Output: 250W into 4 ohms RMS(42VX2 6A transformer is used). 120W into 4 ohms RMS(33VX2 4A transformer is used). Frequency Response: 3Hz-22,000Hz. THD: <0.03%. Signal to Noise Ratio: 91dB. Sensitivity: 1V RMS at 47k. Load Impedance: 4 or 8 ohms. Power Requirement: ±46VDC 4A or ±60VDC 6A. May use Mark V model 012 Transformer. Suggested Capacitor 10,000uf 100V Model 019. Suggested Metal Cabinet LG-1925.



Kit: \$ 89.80 Asmb.\$ 114.80

### 300W HIGH POWER MONO AMPLIFIER TA-3600 (5 lbs.) ▲▲▲

Power Output: 300W into 8 ohms RMS. 540W music power into 8 ohms. Frequency Response: 10Hz-20KHz THD: < 0.05%. Sensitivity: 1V RMS at 47K. Power Requirement: 60 to 75 VDC at 8A. May use Mark V Model 007 or 009 Transformer. Suggested Capacitor: 10,000uf80-100V Model 019 Capacitor. Suggested Metal Cabinet LG-1925.



Kit 85.00  
 Asmb.\$ 110.00

### 120W + 120W PRE & MAIN STEREO AMPLIFIER TA-800MK2 (4 lbs.) ▲▲

Power Output: 120W into 4 ohms RMS. 72W into 8 ohms RMS. Frequency Response: 10 - 20 KHZ. THD: < 0.01%. Tone Control: Bass ±12dB, Mid ±8dB, Treble ±8dB. Sensitivity: Phono Input, 3mV into 47K. Line, 0.3V into 47K. Signal to Noise Ratio: 86dB. Power Requirement: 40V DC @ 6A. May use Mark V Model 001 or 008 Transformer. Suggested Metal Cabinet Model LG-1924.



Kit: \$ 63.92 Asmb. \$ 73.95

### 80W + 80W PURE DC STEREO MAIN POWER AMPLIFIER TA-802 (4 lbs.) ▲▲

Power Output: 80W per channel into 8 ohms. THD: < 0.05%. Frequency Response: DC to 200 KHZ, -0 dB, -3dB @ 1W. Power Requirement: 30V AC X 2 @ 6A. May use Mark V Model 001 or 008 Transformer. Suggested Capacitor 8,200uf 50V Model 017. Suggested Metal Cabinet LG-1924



Kit: \$ 45.94  
 Asmb. \$ 59.72

### 30W + 30W PRE & MAIN STEREO AMPLIFIER TA-323A (1 lb.) ▲

Power Output: 30W into 8 ohms RMS per channel. THD: < 0.1% from 100 HZ to 10 KHZ. Sensitivity: Phono 3mV @ 47K. Tuner, Tape 130mV @47K. Signal to Noise ratio: 80dB. Power Requirement: 22 to 36V AC, 3A. May use Mark V Model 002 Transformer. Suggested Cabinet LG-1684.



Kit: \$ 29.50 Asmb. \$ 38.50

### METAL CABINETS

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 Kit: \$ 73.00



### 3½ MULTI-FUNCTION LED DPM ▲▲

**SM-43 (1 lb.)** AC/DC Voltage range: 1mV-1000V. Thermometer range :0-100C. DC current range: 1 microamp - 2 amp. Capacitance range: 1pf to 2 microfarads. Frequency Counter: 10HZ-20KHZ. Max indication ±1999. Power Supply: 5-6V DC, 200ma. Asmb.: \$ 43.00  
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MFM/RLL, IDE or Floppy .....\$1.00  
Serial Link Cable  
To link two computers for data transfer. Ends. Can be DB9 to DB9 or DB9 to DB25 .....\$9.95

## CHIPS & ROMS

### Processors

80287-8 .....\$19.00  
V20-8 .....\$2.00 V28-10 .....\$6.00  
MC68030-16 .....\$39.00  
MC68882-16 .....\$39.00  
16550 (Enh.serial port chip) \$13.00

### RAM

4116, 4164 or short lead 41256 -12 or -15 .....50¢  
41024 (1 Meg x 1) or 44256 .....\$3.00  
256x8 -15 SIMM...\$3.00 / -12...\$4.95  
256x9 SIP -12 .....\$5.95  
256x9 SIMM -80 .....\$8.00

### Batteries

1/2 AA size, 3.6V lithium .....\$4.95  
AT Type "plug in" 3.6V or 6V \$6.95

## EPROMs

2716 or 2732 .....75¢  
2764 .....\$1.00  
27128 .....\$1.50  
27256 .....\$2.00  
27512 .....\$2.50  
271000 (32 Pin) .....\$4.00  
27010 .....\$6.00

### Microcontrollers

8748 .....\$4.00  
8749 .....\$6.00  
8751 .....\$9.00

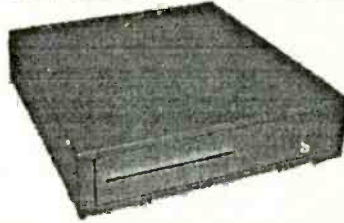
## FLOPPY DRIVES

Used 360K 5.25" Drive .....\$14.95  
Used 1.2 Meg 5.25" HH .....\$35.00  
IBM PS/2 720K Drive OEM for IBM, Mitsubishi Part.....\$59.00

## Fujitsu Cash Drawer.

Hooks up to any receipt printer w/parallel I/O. RJ45 Has check "deposit" slot in front of drawer.

**\$75.00**



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## SPECIALS

Dexxa Hand Scanner 300dpi  
**\$59.00**

XT System Refurbished  
Mono Monitor 360K Drive  
**\$95.00**

AT System • Mono Monitor  
8 Mhz • 1024K • 1.2M Drive  
**\$159.00**

## Monitors

9" Composite "Box" type cabinet. Green screen. Good for security monitor. Input for 75Ω (standard) or High impedance .....\$35.00  
Color Composite Monitor. Not suitable for 80 column text but can be used for computer games, Nintendo, as a video monitor. Some have sound input also. Specify .....\$69.00  
Used/Refurbished Mono. DB9.....\$35.00

## Computer & Drive Cases

Desktop XT/AT Case & 150W P/S Turbo Switch & LED, 2 Exposed HH drive bays .....\$29.00  
External Floppy Drive Case. Holds two HH drives or one FH drive. With Power Supply .....\$19.00  
External MFM/RLL HH HD Case Holds HH 5.25" Hard disk .....\$19.95  
Open face SCSI Case & P/S. For SyQuest or CD ROM. Two 50 Pin Centronics Connectors .....\$45.00  
External SCSI Case & P/S For 5.25" or 3.5" HH Drive. Two 50 Pin Connectors & ID Selector .....\$45.00  
Full height SCSI Case & P/S. Holds 2 HH Drives or 1 FH .....\$65.00  
External CD ROM Drive Case 36 or 40 Pin CD ROM Drives. To install a CD on your system externally.....\$45.00

## Peripheral Cards & Accessories • Keyboards

AT Floppy, Serial & Par Controller .....\$9.95  
AT IDE HD Controller .....\$9.95  
Mono/Parallel Port .....\$9.95  
Universal Video Card. 8 Bit  
CGA/EGA/VGA .....\$39.00  
Full Length CGA w/RCA out.....\$14.95  
EGA Card .....\$29.00  
101 Keyboard (NEW) .....\$29.00  
5 Pin kybd to PS/2 adapter .....\$2.95  
16 Bit Backplane board .....\$10.00  
Microsoft InPort Mouse Card (only) .....\$19.00  
Winning Wordperfect 5.1 in 5 hours! .....\$9.95  
AT 2 Meg Mem. Exp Card w/2 Meg .....\$39.00  
101 XT/AT Keyboard .....19.00  
Keyboard Wrist Pad .....\$1.95

## KESTOR SOLDER \$4.95 EA.

Alloy	Dia.	Flux	Core
Sb5	.025	282	66
Sn60	.031	282	66
Sn60	.020	282	66
60/40	.031	331	40
Sn63	.031	282	66

\* CA Residents please add 7.75% Sales tax. • Minimum shipping & handling charges \$5.00. (This covers most orders) • Warranty: Used/Refurbished products have a 90 day warranty • ALL Returns must have an RMA #, call before shipping back to us. • No Returns without an invoice. Shipping & Handling charges are non-refundable • 20% Restocking charge. applies to products purchased in error & incompatibility problems. • School & University Purchase Orders accepted, others on AOC only. • Prices and availability subject to change at anytime without any notification whatsoever. • Some Products are refurbished product.

CIRCLE 282 ON FREE INFORMATION CARD

# Parts Express

International Inc.

## 1" Titanium Dome Tweeter

Features a ferro fluid cooled Kapton voice coil and a rubber surround. Very natural sounding high frequency reproduction with extended response to 30KHz.

- Power handling: 50 watts RMS/75 watts max
- Voice coil diameter: 1"
- Impedance: 8 ohms
- Frequency response: 2500-30,000 Hz
- Magnet weight: 5.3 oz.
- Fs: 1000 Hz
- SPL: 93 dB 1W/1m
- Net weight: 1 lb.



#EN-275-050 .. \$17<sup>50</sup> (1-3) ... \$15<sup>80</sup> (4-UP)

## 10" Treated Paper Cone Woofer

This 10" woofer features a non-pressed, polymer laminate cone and a rubber surround. Well suited for applications where a high level of performance is desired, but at a reasonable price. Aluminum voice coil and vented pole piece.

- Power handling: 70 watts RMS/105 watts max
- Voice coil diameter: 1-1/2"
- Impedance: 8 ohms
- Frequency response: 30-2,800 Hz
- Magnet weight: 20 oz.
- Fs: 31
- SPL: 91 dB 1W/1m
- Vas: 4.1 cu. ft.
- Qts: .35
- Qes: .39
- Qms: 3.69
- Xmax: .27 in.
- Net weight: 4 lbs.



#EN-295-260 \$29<sup>80</sup> (1-3) ... \$26<sup>90</sup> (4-UP)

## 12" Musical Instrument Speaker

Ribbed paper cone with treated cloth accordion surround. Vented pole piece for heat dissipation and reduced distortion. Perfect replacement for many P.A. and musical type speakers.

- Power handling: 150 watts RMS/200 watts max.
- Voice coil diameter: 2 inches
- Impedance: 8 ohms
- Frequency response: 50-5000
- Magnet weight: 50 ozs.
- Fs: 50 Hz
- SPL: 96 dB 1W/1m
- Vas: 3.56
- Qts: .43
- Qes: .49
- Qms: 3.62
- Xmax: .129
- Net weight: 10 lbs.
- Manufacturer model number: A30GC50-52FQ.



#EN-290-142 .. \$49<sup>80</sup> (1-3) ... \$45<sup>50</sup> (4-UP)

## 3M Super 77 Spray Adhesive

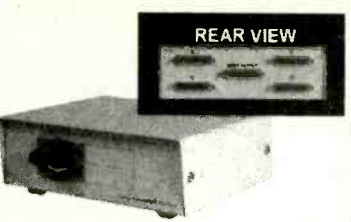
A high tack, fast drying transparent adhesive to permanently attach carpeting, cloth, foils, foams, etc. to wood, metal, painted or unpainted surfaces. High initial "grab" with sufficient time to position materials. 24 oz. can with two spray head actuators (wide and round).



#EN-340-255 ..... \$9<sup>95</sup> (1-11) ..... \$7<sup>95</sup> (12-35) ..... \$7<sup>50</sup> (36-UP)

## RS-232 A-B Switch

Fully shielded, steel enclosed data switch with gold plated female connectors. All 25 pins switched through. High reliability rotary type switch. Compact size. Anti-skid rubber feet. Boxed. Can be used to switch multiple printers or computers. 1 year guarantee. Net weight: 1-3/4 lbs.



#EN-130-010 ..... \$10<sup>50</sup> (1-2) ..... \$9<sup>95</sup> (3-UP)

## High Voltage Capacitor Kit



This 85 piece kit contains a selection of 250, 350, and 450 volt electrolytic capacitors. 5 pieces each of 1, 2.2, 3.3, 4.7, 6.8, 10, 22uf and 2 pieces each of 33, and 47uf, 250V radial caps. 5 pieces each of 1, 2.2, 3.3, 4.7, 10uf and 2 pieces each of 22, 33uf, 350V radial caps. 5 pieces each of 1, 2.2, 4.7uf and 2 pieces of 10uf, 450V radial caps. Over \$62.00 wholesale cost if purchased individually. Net weight: 1 lb.

#EN-020-950 ..... \$49<sup>95</sup> EACH

## 22 Amp Power Supply

The perfect test bench power supply. You can run just about any 12 VDC powered product without worrying about overloading the supply. Highly regulated IC and transistor circuitry with built in crowbar protection alarm. Dual metering for voltage and current. Output adjustable between 10-14 VDC. Adjustable output current for testing amplifiers. 2 year warranty.

**Specifications:**

- Output voltage ..... 10-14 VDC
- Output current (cont) 22 amps
- Output current (surge) 25 amps
- Dimensions ..... 9"x5"x11"
- Net weight ..... 19 lbs



#EN-120-504 \$139<sup>95</sup> (1-3) ... \$129<sup>80</sup> (4-UP)

## Strobe Flasher

Weatherproof red strobe flasher. Includes 9/16" mounting stud and foam gasket. Operating range 6-12 VDC. 2-3/4" (W) x 1-5/8" (dia). Net weight: 1/4 lb.



#EN-335-123 .. \$12<sup>50</sup> (1-3) ... \$11<sup>25</sup> (4-UP)

## Technicians' Turntable



Turntable to speed repair of VCRs, TVs and more. Allows technician to easily turn unit for convenient repair. Dimensions: 20" W x 15" D x 1-1/8" H. Black pebbled surface. Includes 4 anti-skid adhesive feet. Net weight: 9 lbs.

#EN-360-427 ..... \$28<sup>50</sup> EACH

## Multi-Speaker Distribution Box



This multi-speaker distribution box features metal construction, inputs for left and right channels, and 8 set of speaker outputs. Color coded, spring loaded pushbutton terminals accept 12 to 22 gauge wire. Built in impedance protection can be switched in or out. Power handling capacity: 300 watts (impedance protection switched off), 150 watts (impedance protection switched on). Black color. Made in the U.S.A. Dimensions: 19"W x 3-1/2"H x 2-1/4"D. Net weight: 2 lbs.

#EN-300-600 ..... \$149<sup>80</sup> EACH

## Center Off Toggle

DPDT center off toggle switch. 6A, 125VAC. (1/2" mount.)



#EN-060-087 . \$17<sup>5</sup> (1-9) . \$1<sup>50</sup> (10-UP)

## Deluxe TV Wall Mounting System

Deluxe wall bracket features heavy duty, all steel construction and the platform is adjustable from 12-1/4" to 16-3/4". Has 4 pivoting points and swivels 180 degrees for a variety of viewing angles. 60 lb. capacity. White enamel finish. Must be mounted directly to studs. Net weight: 9 lbs.



#EN-240-772 .. \$36<sup>50</sup> (1-3) ... \$32<sup>80</sup> (4-UP)

## F-59 Deluxe Connector

Popular connector for cable TV systems. Full attached ferrule for hex crimp. Securely holds RG-59 cable.



#EN-090-355 .. 29¢ (1-49) ..... 22¢ (50-UP)

## Mag-Lite Focusable Flashlight

These high tech flashlight from Mag-Lite are constructed of rugged aircraft aluminum for shock resistance and are anodized inside and out to guard against corrosion. High intensity light beam can be easily focused from a flood to a spot. Rubber "O" rings provide excellent moisture resistance. The sealed switch is self cleaning to eliminate oxidation and to ensure high reliability. Don't settle for imitations. See why most police and fire departments across the country use Mag-Lite! Includes spare krypton lamp. Lifetime manufacturer warranty. Designed and manufactured in the U.S.A.



Part #	Description	Price (1-3)	Price (4-9)	Price (10-UP)
EN-361-510	2 D-cell black	\$22.90	\$20.50	\$19.50
EN-361-515	2 D-cell red	22.90	20.50	19.50
EN-361-520	3 D-cell black	23.90	21.45	19.95
EN-361-525	3 D-cell red	23.90	21.45	19.95
EN-361-530	5 D-cell black	25.95	23.50	21.90
EN-361-535	5 D-cell red	25.95	23.50	21.90
EN-361-540	Mini AAA cell black	11.50	9.95	9.25
EN-361-545	Mini AAA cell red	11.50	9.95	9.25
EN-361-550	Mini AAA cell blue	11.50	9.95	9.25
EN-361-555	D-cell wall mount brackets	5.20	4.70	3.95

## Cabinet Carpet

This high quality carpet conforms easily to sharp corners because it has no stiff backing. You can also stretch it to cover irregular shapes. This is the covering of choice for car, stage, and amplifier cabinets. Carpet is strong, yet easy to cut with knife or scissors. Adhere with spray adhesive or latex contact cements. Provides protection and good looks. Sold by the linear yard. 54" wide.



#EN-260-765 Dark Charcoal  
#EN-260-767 Medium Grey  
#EN-260-768 Jet Black

Per Linear Yard, 36" x 54" ..... \$4<sup>50</sup> (1-49 YDS) ..... \$3<sup>25</sup> (50 YDS-UP)

Parts Express  
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Dayton, Ohio 45402  
Local: 513-222-0173  
FAX: 513-222-4644

•30 day money back guarantee •\$20.00 minimum order •We accept Mastercard, Visa, Discover, and company C.O.D. orders •24 hour shipping •Shipping charge = UPS chart rate + \$1.50 (\$4.00 minimum charge) •Hours 8:30 am - 7:00 pm ET, Monday - Friday •9:00 am - 5:00 pm Saturday. Mail order customers, please call for shipping estimate on orders exceeding 5 lbs. •Foreign destination customers please send \$6.00 U.S. funds for catalog.



# Parts Express

International Inc.

## Teac Floppy Disk Drives

High quality disk drives made by Teac. Standard putty color. High density 3-1/2", 1.44 MB and 5-1/4", 1.2 MB.



- (3-1/2" drive)  
**#EN-130-530 .. \$59<sup>90</sup> EACH .. \$55<sup>80</sup> (2-UP)**  
 (5-1/4" drive)  
**#EN-130-532 .. \$69<sup>90</sup> EACH .. \$64<sup>95</sup> (2-UP)**

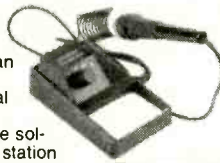
## The Ultimate Test CD

The Ultimate Test CD was designed for use by both the audio amateur and the professional sound engineer. This CD can be used to test CD players, speakers, amplifiers, and for tuning instruments. The manual is written in easy to understand English and takes you step-by-step through each track of the CD and explains its purpose. The Ultimate Test CD is a necessary tool for anyone who is serious about quality audio sound.  
**#EN-510-100 ..... \$7<sup>95</sup> EACH**



## Ungar UTC SS

The Ungar UTC SS is an economical dual wattage soldering station for use in the home, shop or at work. Dual temperature capability makes it ideal for surface mount components. Station includes an iron holder, and tip protects electronic components from static discharge. UL listed. Net weight: 2 lbs.  
**#EN-372-060 ..... \$59<sup>90</sup> EACH**



## Head/Disc Cleaner

Head and Disc Cleaner is a CFC free cleaner which will remove carbon deposits, metallic oxides, dirt, dust and other contaminants from magnetic heads. Non-flammable Head and Disc Cleaner has superior cleaning properties compared to freon blends and is safe on most plastics. HCFC blend. 6 oz. liquid.



- #EN-341-075 ..... \$3<sup>80</sup> (1-11) ..... \$3<sup>40</sup> (12-23) ..... \$3<sup>25</sup> (24-UP)**

## Drive Belt Kit

We've selected 18 of our most popular VCR, cassette and turntable belts to include in this kit. 87 belts total, five each of 17 square belts from 2.3" to 13.2" for VCRs and cassettes, and 2 each of the 23.6" turntable belt. Have the belt you need in stock when you need it. A \$50.00 value. Net weight: 1/4 lb.



- #EN-400-910 ..... \$29<sup>95</sup> KIT**

## 3 In 1 Universal Remote

This remote will operate any remote controlled cable box, TV or VCR at just a fraction of the cost of a factory replacement! This unit is already preprogrammed to include the most common codes. It is attractively styled, durable, and easy to set up and operate. The manufacturer even offers a toll free consumer help line to answer questions and provide customer assistance. Requires 2 AAA batteries (not included).



- #EN-180-565 .. \$12<sup>50</sup> (1-9) .. \$9<sup>95</sup> (10-UP)**

## Designing, Building, And Testing Your Own Speaker System

Completely revised and updated to reflect the latest trends in audio technology, this edition of David B. Weems' best-seller will guide do-it-yourselfers through the building and testing of low-cost speaker systems that rival the most expensive units on the market. 224 pages. Copyright: 1990. Third edition. Net weight: 1 lb.  
**#EN-500-021 ..... \$16<sup>95</sup> EACH**



## Speaker Surround Repair Kits

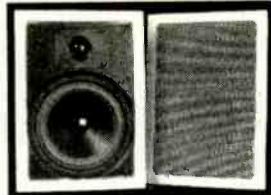
Don't throw away expensive loudspeakers just because the foam surround has dry rotted, or has been punctured. With these new repair kits from Parts Express, you can save BIG bucks by repairing the foam surround and avoid costly loudspeaker replacements. The kit includes 2 pair foam surrounds (except for the 15" kit which includes one pair), a plastic syringe filled with 25cc of adhesive (specially formulated for various speaker cone materials), 5 foam swabs for application of glue, and complete repair instructions.



Part #	Size	Price (1-3)	Price (4-UP)
EN-260-920	8" kit	\$19.95	\$17.95
EN-260-925	10" kit	20.50	18.50
EN-260-930	12" kit	21.90	19.90
EN-260-935	15" kit	22.90	20.90

## 6-1/2" Two-Way System

The basis of all architectural audio systems. This is our most popular in-wall. The perfect system for main and/or surround speakers. Easily installed in any 2 x 4 or larger wall. Retrofit design allows installation in new or existing walls in minutes. Features high quality crossovers and premium drivers that can outperform the name brands.  
**Specifications:** 6-1/2" poly woofer with a 10 oz. magnet, 1" field replaceable soft dome tweeter. Integral 2-way crossover with pushbutton wire terminal. 8 ohm impedance. Frequency response: 40-20,000 Hz. 40 watts RMS/80 watts max power handling capability. Sensitivity: 90 dB 1W/1m. Dimensions: 8-1/2" (W) x 12" (L) x 3-1/2" (D). Net weight: 9 lbs. per pair.



- #EN-300-036 ..... \$249<sup>95</sup> (SUG. LIST) ..... \$124<sup>90</sup> (1-3 PRS) ..... \$112<sup>95</sup> (4 PRS-UP)**

## Kester "44" Solder

Kester "44" rosin core solder is designed for electronic and electrical work. It uses a fast acting, instant wetting, non-corrosive, and non-conductive flux for faster soldering and a strong, long lasting bond.



Part #	Alloy Lead/Tin	Spool	Dia.	Price (1-3)	Price (4-UP)
EN-370-080	60/40	1 lb.	.031"	\$10.95	\$9.95
EN-370-090	60/40	1 lb.	.050"	10.95	9.95
EN-370-098	60/40	4 lb.	.031"	43.80	39.50
EN-370-072	63/37	1 lb.	.020"	13.60	12.25
EN-370-074	63/37	1 lb.	.031"	11.50	10.50

## Magnetizer/Demagnetizer

Handy device to magnetize (or demagnetize) screwdrivers, tweezers, and various other tools.



- #EN-360-700 .. \$9<sup>90</sup> (1-9) ..... \$8<sup>90</sup> (10-UP)**

## 36 Piece Precision Driver Set

Contains 6 individual kits. Each Moody kit contains locking, chuck type, knurled steel handles and 5 interchangeable ends. The set includes: Slotted Screwdriver Kit (.040", .055", .070", .080", and .100" slotted blades), Cross Driver & Awl Kit (1 awl plus, .055"/1.4mm/#000, .080"/2.0mm/#00, .100"/2.5mm/#0, and .125"/3.2mm/#1 cross recess blades), Hex Driver Kit (.035", .050", .062", .078", and .093" hex blades), Torx® Driver Kit (T-6, T-7, T-8, T-9, and T-10 Torx blades), Socket Wrench/Nut Driver Kit (5/64", 3/32", 7/64", 1/8", and 5/32" socket wrenches), and Open End Wrench Kit (7/64", 1/8", 5/32", 3/16", and 1/4" open end wrenches). Includes black leatherette case.  
**#EN-361-215 \$65<sup>90</sup> (1-3) \$59<sup>90</sup> (4-UP)**



## 12V, 15 Ah Battery

Save big on this rechargeable lead acid battery. Has many uses: computer back-up upgrade, alarm back-up battery, garden tractor starter battery, and more. Sealed in a high impact polystyrene case. Bolt and nut type terminals. Dark blue color. Dimensions: 7"W x 6-1/2"H x 2-15/16"D. Net weight: 14 lbs. Limited availability.



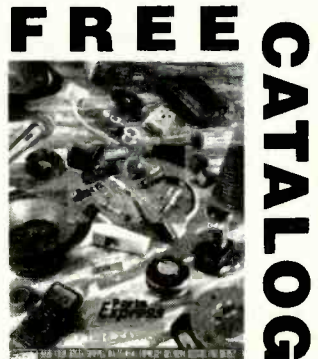
- Compare to  
**#EN-149-100 ..... \$60<sup>00</sup> ..... \$29<sup>95</sup> (1-4) ..... \$24<sup>95</sup> (5-UP)**

## Chamois Swabs

Genuine sheepskin swabs for cleaning delicate video and audio heads. Chamois leaves no residue. 10 pieces per package. Reusable.



- #EN-200-028 \$2<sup>95</sup> (1-9PKGS) \$2<sup>60</sup> (10PKGS-UP)**



Parts Express  
 340 East First St.  
 Dayton, Ohio 45402  
 Local: 513-222-0173  
 FAX: 513-222-4644

CALL TOLL FREE  
**1-800-338-0531**

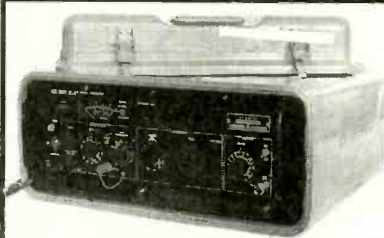
# Davileys CORP.

13406 Saticoy Street  
North Hollywood, CA 91605-3475



Price: \$395.00

**TEKTRONIX 528 SOLID STATE  
N.T.S.C. WAVEFORM MONITOR**

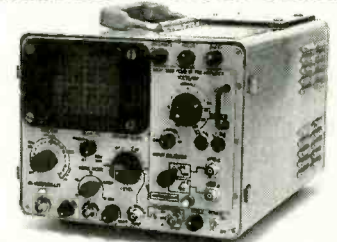


**HEWLETT PACKARD 8640B-OPT 323  
SOLID STATE SIGNAL GENERATOR**

(w/o synchronizer) Frequency range: 450 KHz to 512 MHz, to 1100 Mhz with external frequency doubler option supplied. Ten Frequency bands in octave increments from 500 KHz; band 11 for doubler use. Accuracy: 6 digit LED read out. Stability: < 1000 ppm. Output power: -145 dBm to +10 dBm (0.013 V to 2 V) into 50 Ω. Impedance is 50 Ω, VSWR < 2.0 on 2 V and 1V range < 1.3 on other ranges >. Modulation: Internal AM, FM and PM, external AM, FM and PM. Pulse frequency: 0.05 to 5 kHz. General: Power Requirements: 100, 120, 220, 240 V, 48 hz to 420 hz, 2 amps. Size: 6" (H) x 19" (W) x 13 1/4" (D). Wt. 60 lbs. Includes ruggedized case and manual.

Price: \$795.00

Current Hewlett Packard Prices: \$12,050.00



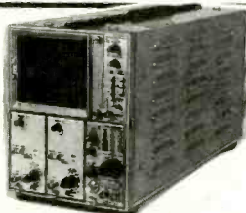
**AN/USM-117 TRANSISTORIZED  
DC-6, MHz OSCILLOSCOPE**

Specifications: CRT Size: 2 1/2" x 2" - Vertical Bandwidth: DC-6 MHz - Sweep Ranges: .1 microsecond div. to 1 sec. - Horizontal Bandwidth: DC:500 Hz - Power Input: 115V/50-1000 Hz/1 Ph - Dimensions: 8" x 9 1/4" W x 18 1/2" D (including front cover) - Weight: 23 lbs. complete. Price: \$135.00

NEW

**AN/URM-120 50 OHM  
THRU-LINE RF WATTMETER**

Frequency range: 2MHZ to 1000MHZ. Power range: 10 Watts to 1000 Watts. USWR ≤ 1.08 to 1. Uses three plug-in coupler elements, (included). CU-753 2 to 30 MHz 50 to 100 Watts CU-754 25 to 250 MHz 10 to 500 Watts CU-755 200 to 1000 MHz 10 to 500 Watts Connector: Type N. Case included. Size: 7" W x 6 5/8" H x 7 1/2" D Weight: 6.5 lbs. Price: \$285.00



**TEK MODEL 7603N**

Oscilloscope: Mil Spec AN/USM-281C, 8 x 10 CM display, 100 mHz response which accepts standard 7000 series Plug-Ins. Vertical Plug-In: 2 ea. 7A15 (AM-6565), frequency BW 75 mHz, maximum sensitivity 5mV/DIV. Horizontal Plug-In: 1 ea. 7B53 (TD-1085), triggering to 100 mHz, minimum, sweep-time 50 NS/DIV, has delayed sweep capacity. Includes cover probes accessories. Price: \$495.00



**COLLINS HF8050 SOLID STATE  
SYNTHESIZED RECEIVER**

Freq: 250KHZ to 29.99999MHZ; 10HZ steps thumb wheel tuning. Modes: SSB, USB, LSB, CW, AM. B.W.: 2.7KHZ, 16KHZ. Sensitivity: 0.7MV 10dB S+N/N. Computer controllable. Squelch. Power: 103 to 127U, 47 to 63HZ/207 to 253V, 80 watts. Size: 7"H x 19" x 20.9"D. Wt: 42 lbs.

Price: \$2500.00

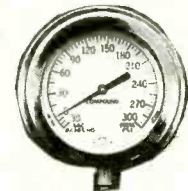


Collins 651S-1 synthesized, solid state HF receiver, AM, CW, SSB, FM, ISB. Freq: 250 KHz to 29.9999 MHz. 1MHz, 0.1MHz, 100 CPS steps. IF filters: 16MHz, 6MHz, 3MHz, 2.7 MHz, 0.5 MHz, No 0.2. Input power: 115/230v, 47 to 63hz, 70 to 110 watts. Price: \$1,895.00



**HP MODEL 606B**

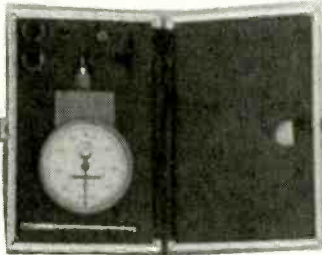
Signal Generator: Later version of 606A. Frequency range of 50 KHz to 65 MHz in size bands; accuracy ± 1%. Output level is continuously adjustable from 0.1uV to 3V into 50 resistive load. Modulation level of 0 to 95% on TV attenuator range and below, 0 to at least 20% on 3V range. Price: \$375.00



**GENUINE U.S. NAVY**

-30 vacuum to +300 PSI Bronze Encased Gauge. 5 1/4" diameter 1/4" male NPT.

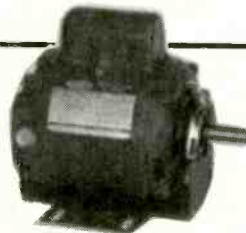
New Price: \$85.00



**JONES INSTRUMENT TACHOMETER**

Centrifugal Mechanical tachometer. Measures RPM scale to 500 RPM. Coupling shaft 1/8". Accessories: various size rubber tipped drive couplings.

New Price: \$75.00



**DAYTON CAPACITOR MOTOR**

5K504 1/2HP capacitor start 1725 RPM 115V, 60HZ, 1PH. Sleeve bearings rubber mounted open, dripproof thermal protection nema 56 frame 5/8" dia. shaft 3/16" shaft HT.

New Price: \$75.00



**ITT UHF POWER AMPLIFIER AM6155/  
GRT-22**

Frequency range: 225 MHz K 399.95MHz. Power Output: 50 watts. Impedance: 500ΩHMS. Modulation range: 90% ± 10%. Power Req: 105/120V/210/240 at 47 to 420 HZ, 610 watts max. Size: 5 1/4" H, 17 3/4" W, 18 1/2" D at 70 lbs.

Price: \$300.00

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**(800) 235-6222**

**FAX (818) 787-4732**

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Fluke 721A	Lead Compensation	500.00
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Fluke 895A	Differential Voltmeter	350.00
Fluke 931PB	True RMS Voltmeter	400.00
Fluke 1953A	Frequency Counter	450.00
Fluke 6160A	Frequency Synthesizer	650.00
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GE 1620A	Capacitance System	2,000.00
HP 203A	Function Generator	400.00
HP 334A	Distortion Analyzer	600.00
HP 853A	Display	2,000.00
HP 1725A	Scope, 275MHZ	700.00
HP 1740A	100MHZ Scope	500.00
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HP 3456A	Digital Voltmeter	900.00
HP 3575A/001	Phase Gain Meter	900.00
HP 3575A/002	Phase Gain Meter	1,000.00
HP 4800A/4801A	Vector Impedance Meter	450.00
HP 4815A w/Probe	Vector Impedance Meter	800.00
HP 5340A	Frequency Counter, 10HZ to 18GHZ	1,000.00
HP 5328A w/OPT 011	Counter, DC to 100MHZ, 9 digit	450.00
HP 606B	Signal Generator	350.00
HP 3325A	Synthesized Function Generator	2,000.00
HP 3330B	Automatic Synthesizer	800.00
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HP 4935A	Transmission Test Set	1,500.00
HP 4940A	Transmission Test Set	600.00
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TEK 465 w/DM44	Scope, 100 MHZ	650.00
TEK 465B OPT05	Scope with TV, 100 MHZ	850.00
TEK 520A	NTSC Vectroscope	1,000.00
TEK 576	Curve Tracer 220W	1,800.00
TEK 7A13	Differential Comparator LED	400.00
TEK 7A22	Differential Amplifier	500.00
TEK 7A24	Amplifier	500.00
TEK 7A29	Plug-In, 1GHZ	750.00
TEK 7B15	Time Base	500.00
TEK 7B53A OPT05	Plug-In	300.00
TEK 7CTIN	Curve Tracer, 0.5W	400.00
TEK 7D20	Programmable Digitizer	1,500.00
TEK 7L5/L3	Spectrum Analyzer	2,200.00
TEK 7L13	Spectrum Analyzer, 1KHZ to 1.8 GHZ	2,850.00
TEK 1480R	Waveform Monitor	1,000.00
TEK 2901	Time Mark Generator	350.00
TEK 7844	Dual Beam Scope, 400MHZ	750.00
Velonex 510	Transient Generator	1,000.00
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Jerrold 550: Scientific Atlanta (Blk) with and without volume, Zenith type or refurbished Slimline with new battery.

All of the above \$11 \$10 \$9 Call Call

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THERE MAY BE NO RESTOCKING ON THESE ITEMS.

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CONVERTERS W/BUILT-IN DESCRAMBLER IN CONVERSION MODE

1 5 10 20 100

Scientific Atlanta 8500/321 w/Remote Jerrold and SA compatible \$110. \$105. \$100. N/A N/A

Scientific Atlanta 8530/320 w/Remote Jerrold and SA & SA dropfield compatible \$125. \$118. \$114. N/A N/A

CONVERTERS/DESCRAMBLERS RAW

Jerrold jSX-3-DIC 36 Ch. 80% plus test good \$14. \$12. \$9. Call Call

STRAIGHT CONVERTERS ONLY

CONVERTERS W/BUILT IN DESCRAMBLER IN CONVERSION MODE

Scientific Atlanta 8530/330 Basic SA & SA dropfield (Advanced SA) 6 db type Jerrold & Hamlin type compatible \$135. \$125. Call N/A N/A

Panasonic Ch 3 w/Volume & new Remote, Feature packed \$55. N/A N/A N/A N/A

DECODERS ONLY

Jerrold SB3-DIC General Instrument original equipment Ch 3 w/xfmr/.

Raw tested and guaranteed \$19. \$16. \$14. \$12. \$9.50

Positive Traps Ch 2,3,4,16,23 \$10. \$9. N/A N/A N/A

REMOTES ONLY - All remotes come with new batteries.

Panasonic original \$9. \$8. Call Call N/A

Oak & Hamlin \$9. \$7. \$6. Call N/A

Pioneer original type with Universal Programmable TV function (for 5\_\_ & 6\_\_ series) New \$12. \$10. Call Call N/A

CONVERSION KITS & CHIPS

Zenith ZLI, 8500 310,320, 410, 420 Starcom 6 (not BB) \$12. \$10. \$9. \$8. Call

Tocom 5503 VIP, 5507, 5507VIP (no 2R series) \$10. \$9. \$8. \$6. Call

Scientific Atlanta 8570,8580, 8590 & 8600 (40 pin micro controller) \$45. \$39. Call Call N/A

MISCELLANEOUS

Zenith LED displays \$3. \$2. \$1. Call N/A

Zenith Remote Sensor Module \$5. \$4. \$3. \$2. \$1.

Zenith Slimline Remote, front bezel inlay \$1. Call Call Call Call

Zenith Cosmetic Repair Parts Call Call Call Call Call Call for specifics

Zenith decoder board 165 type tested and guaranteed \$19. \$15. \$12. Call Call

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If you plan to steal cable, do us both a favor, don't waste your dime and my time!!! Because Z-Mann Cable Supply does not assist any company or any individual in this illegal activity!

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- DESCRAMBLERS
- CONVERTERS
- COMBINATION UNITS

**WE'LL BEAT ANY PRICE!**

## LATEST DESCRAMBLER MODELS

Add On Descrambler for all JERROLD Systems (Except Base Band) Guaranteed to Work Anywhere Coast to Coast (Model JD-3)

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Add On Descrambler For All PIONEER Systems. Guaranteed to Work Anywhere Coast to Coast. (Model PD-3)

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**BRAND NEW  
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### SCIENTIFIC ATLANTA 8580

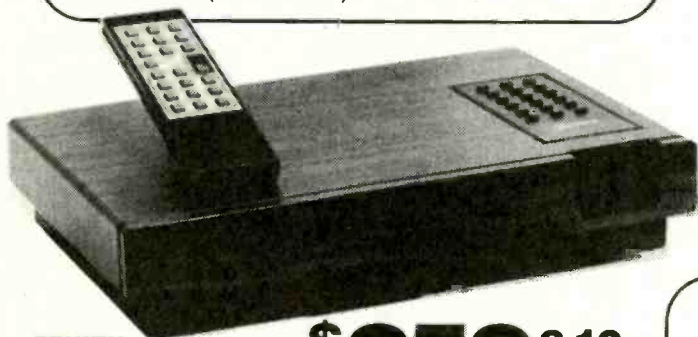
#### Features

- Wireless Remote Control
- Favorite Channel Recall
- Parental Lockout

**\$259** 6-10

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### ZENITH

#### Features

- Wireless Remote Control
- 550MHz (99 Channel) capacity
- Volume Control
- Parental Lock-Out
- Programmable Favorite Channel Memory

**\$259** 6-10

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## ADD ON DESCRAMBLERS

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FTB-3	49.00	39.00
TVT OR TBI	55.00	47.00
SA-3	59.00	49.00
KN12-3	59.00	49.00
MLD1200-3	49.00	39.00

## CONVERTERS

	1-5	6-10
PANASONIC 1453G	79.00	69.00
JERROLD DQN7-3	75.00	65.00
STARGATE 2001	75.00	65.00

Call for other models



**DPV7 & DBB7  
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Fully operating system independent diagnostic software.

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MICRO-SCOPE Universal Computer Diagnostics was developed to satisfy the expanding need for accurate system diagnosis in the rapidly growing desktop computer market.

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- MEMORY TEST—"Micro-Scope" 5.0 has no limitations as to the size of memory it can accurately test. Micro-Scope now also tests VIDEO MEMORY (up to 2 MB)!!
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- AUTOMAPPING—Automatically bad sector maps errors found on hard disks.
- IRQ DISPLAY—Shows bits enabled in IRQ chip for finding cards that are software driven. (Network, Tape Backup, etc.)
- IRQ CHECK—Talks directly to hardware and shows I/O address and IRQ of devices that respond.
- SECTOR EDITOR—Allows the editing of any sector of floppy or hard disk media (even track 0).
- AND MUCH MORE...We don't have enough space here for everything this software can do!



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The only Power-On Self-Test card you need to debug any "dead" PC!

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"This is the only card that will function in every system on the market. The documentation is extensive, and not only covers the expected POST Codes for different BIOS versions, but also includes a detailed reference to the bus signals monitored by the card." —Scott Mueller from his globally recognized book, 'Upgrading & Repairing PCs, Second Edition'

- Includes pads for voltmeter to attach for actual voltage testing under load.
- 4 LEDs monitor +5vdc -5vdc +12vdc -12vdc.
- Monitors Hi & Lo clock and OSC cycles to distinguish between clock chip or crystal failure.
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- Monitors memory write/read to distinguish between address line failures and memory chip failures.
- Monitors ALE for proper CPU/DMA operation.
- Monitors Reset to determine if reset is occurring during POST, indicating short.
- Monitors progress of POST without POST codes.
- Reads POST codes from any IBM or compatible that emits POST codes. ISA/EISA/MCA.
- Compatible with Micro Channel computers.
- Dip switch allows easy selection of I/O ports to read.
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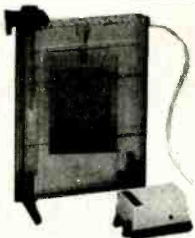
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## ETCHING TANK

This attractive injection moulded designed tank is ideal for etching your PCBs. It includes a thermostatically controlled glass heater, electric agitator and PCB hanging accessories. Measuring graduations are included. Maximum PCB size is 160mm x 250mm or 200mm x 250mm w/o heater. Typical etching time is 4 minutes.

CAT NO DESCRIPTION PRICE  
ET10EN Etch Tank System \$48.00



## ETCHING CHEMICALS FERRIC CHLORIDE

A dry concentrate that mixes with water to make 1 pint of etchant, enough to etch 400 sq. inches of 1oz board.

CAT NO DESCRIPTION PRICE EACH  
ER-3EN Makes 1 pint \$3.50 \$2.75



**DEVELOPER** This product is used as the developer on our positive photo-resist printed circuit boards. Includes instructions. 50 gram package, mixes with water, makes 1 quart.

CAT NO DESCRIPTION PRICE EACH  
POSDEVEN Positive Developer \$ .95 \$ .80 \$ .50

## POSITIVE PHOTO RESIST PRE-SENSITIZED PRINTED CIRCUIT BOARDS

These pre-sensitized printed circuit boards are ideal for small production runs. They provide high resolution and excellent line width control. High sensitive positive resist coated on 1oz. copper foil allows you to go direct from your computer plot or art work layout. No need to reverse art.



### Single-Sided, 1oz. Copper Foil on Paper Phenolic Substrate

CAT NO	DESCRIPTION	PRICE EACH		
		1	10	50
PP101EN	100mm x 150mm/3.91" x 5.91"	\$2.55	\$1.90	\$1.70
PP114EN	114mm x 185mm/4.49" x 7.28"	2.98	2.45	1.98
PP152EN	150mm x 250mm/5.91" x 9.84"	5.40	3.98	3.60
PP153EN	150mm x 300mm/5.91" x 11.81"	6.15	4.48	4.10

### Single-Sided, 1oz. Copper Foil on Fiberglass Substrate

CAT NO	DESCRIPTION	PRICE EACH		
		1	10	50
GS101EN	100mm x 150mm/3.91" x 5.91"	\$ 3.90	\$2.98	\$2.60
GS114EN	114mm x 185mm/4.49" x 7.28"	4.80	3.49	3.20
GS152EN	150mm x 250mm/5.91" x 9.84"	8.69	5.98	5.78
GS153EN	150mm x 300mm/5.91" x 11.81"	10.20	7.20	6.80

### Double-Sided, 1oz. Copper Foil on Fiberglass Substrate

CAT NO	DESCRIPTION	PRICE EACH		
		1	10	50
GD101EN	100mm x 150mm/3.91" x 5.91"	\$ 5.07	\$3.68	\$3.38
GD114EN	114mm x 185mm/4.49" x 7.28"	5.95	4.29	3.99
GD152EN	150mm x 250mm/5.91" x 9.84"	10.47	7.39	6.98
GD153EN	150mm x 300mm/5.91" x 11.81"	11.95	8.69	8.30

## 486 CPU COOLER

*Increase Performance! Prolong Life!*  
**COOL IT!** With our easy to install miniature CPU Cooler Fan. This kit includes an omni-directional heat sink, long-life, low noise, DC fan with ready to go power hook-up. The best low-cost, high add-on value investment you can make!

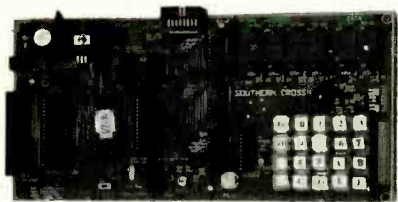
**PERFORMANCE** Typical 80486-33MHz CPU surface temperature reduces from approximately 79°C to approximately 48°C. Typical 80486-50MHz CPU surface temperature reduces from approximately 95°C to approximately 54°C.

CSI PART# PRICE  
CC-M3EN \$15.95 \$ 5 \$14.95



## WANT MORE INFO ON THE SOUTHERN CROSS?

Use our FaxBack Automated Document Retrieval System. Dial 1-800-662-5426 (602-834-1005 in AZ) and select document #5025 on your push-button phone. You'll receive an article reprint from Australia's "Silicon Chip" magazine, reviewing the Southern Cross SBC. This is a free service available 24-hours a day. Don't forget to have your FAX# handy.



## THE SOUTHERN CROSS

**A Single Board Z-80-Based Computer**  
Here is a single board computer designed especially for the 1990's generation of students. With a series of add-on boards, smart sockets, fully commented monitor & an intelligent EPROM emulator, it can teach many aspects of micro-processor & micro-controller techniques of programming.

The Southern Cross SBC is designed to teach beginners modern code development techniques as well as assembly language. Start with machine language using the on-board

21 hex digit keypad, then progress to using a PC Assembler provided with many program examples. Serial download assembled program from PC to Southern Cross. Serial interface provided.

Simple, but powerful monitor program fully annotated. Learn to use parts of it in your own programs by 'system calls' & using a 'header file'.

Learn how to single step through your program to find errors. Both hardware & software single stepping provided & explained.

We do not fill the User Manual with pages of theory. Go straight to program examples. Starts from a very basic level anyone can follow.

The Southern Cross system includes:

- All CMOS IC's
- Hardware speed control
- 8K EPROM
- 64K RAM
- 4.00MHz Z80
- 10 year RAM backup with optional DS1213B
- Calendar/time access & RAM backup with optional DS1216B
- 9-15V AC/DC Single-sided PCB 9.75" x 5.15"

Two add-on boards available. Relay Board to connect to real world of lights & motors and 8 x 8 LED module Board to write moving displays.

SC1EN Southern Cross Kit	\$145.00
SC2EN Assembled	\$185.00
SC4EN 8 x 8 Board	\$49.00
SC3EN Relay Board-1 relay	\$27.00
SC13EN Kit to complete relay board-7 relays plus components	\$19.95
DS1213BEN SmartSocket	\$18.00
DS1216BEN SmartWatch	\$36.00

### Intelligent Eprom Emulator

Full explanation of how to construct & use it. Uses 5 IC's & 8748 uC. Emulates 8K, 16K & 32K EPROM. Recognizes binary & Intel hex files in software. Connects to printer port 1 or 2 on a PC. Reset sent in software before file transfer. /F switch fills unused emulated ROM with any hex byte. Powered from target system. Cables included. Small 4.5" x 2.3" double-sided, PCB with overlay. Many examples provided on floppy disk.

SC5EN Kit	\$79.00
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### EDUCATIONAL PROJECT KITS

These kit designs are fully tested & guaranteed to work! They are designed to provide educational value as each kit includes complete documentation, a schematic diagram and a short discussion on the theory. All of the circuit boards are made from 1.6mm fiberglass. They have been silk-screened on the top to aid in component placement and the backs have been soldermasked to aid in soldering. The solder pads and traces are on the large side to help withstand rough handling.

- High Quality Educational Project Kits
- Excellent Documentation
- Each Kit Includes a Schematic Diagram
- A Circuit Description and Theory Discussion Included
- PCB's are Rugged 1.6mm Fiberglass
- PCB's are Silk Screened on Top to Aid in Component Placement
- PCB Pads & Traces are Oversized to Protect Against Rough Treatment
- Faulty Components will be Replaced FREE of Charge

#### Three Digit Panel Meter and Counter Module

Basic low cost counter. Two or more counter modules may be plugged together with 6-pin sockets & harness provided. Uses a single-unit 3-digit LED display. Built around the 14553 & 14551 chips. Box & battery provided. The separate COUNTER MODULE shows how to use the Kit as a counter. Has COUNT & RESET switches with debounce circuit built in to eliminate problems from noisy switches. 9V battery operation.

CAT NO PRICE  
KIT 1EN \$19.95

#### Introduction to a Power Supply

Batteries soon become an expensive way to power your electronic kit and electronic games. This is a basic power supply using two 7805 regulators. Input up to 20V AC from a transformer or power pack. Two regulated outputs—fixed 5V, the other variable. Box provided. Good introduction to electronics.

CAT NO PRICE  
KIT 4EN \$12.77

#### Introduction to LM3909. Continuity Tester & Long Life Flasher

Most ICs operate in the 4V to 40V range. The LM3909 from National Semiconductor changed this. Two PCBs supplied. A 1.5V D cell will flash an LED for over two years. Use as an imitation car alarm. A second PCB connects the chip as a 1.5V continuity tester. Seven pages of documentation provided from National Semiconductor.

CAT NO PRICE  
KIT 11EN \$9.95

#### Sound Activated Switch for Tape Recorder

Can be adjusted to turn on your tape recorder through its REMOTE plug. Has feedback and delay circuit for robust operation. Very sensitive. Proven circuit. Needs 6V plug pack for most stable operation.

CAT NO PRICE  
KIT 13EN \$9.95

#### 6V Tape Switch for Telephone

Record your phone conversations. Turns tape recorder on when the handset is lifted. Easy to connect to your phone line. Plugs into REMOTE & MIC jacks of your tape recorder. Best for 6V tape recorders. Educational Kit, not for illegal use.

CAT NO PRICE  
KIT 15EN \$9.95

#### FM Telephone Transmitter

Miniature transmitter which attaches in series to one of the two lines to your telephone. Transmits over 200 meters to an ordinary FM receiver. Transmits further if the FM receiver is near the phone line. Tune with ceramic trim cap. Uses the phone line as an aerial and power source. Not for illegal use.

CAT NO PRICE  
KIT 16EN \$8.95

#### Logic Probe

This is the most important piece of equipment for testing and measuring digital equipment. It is usually used in fault finding and testing, but can also assist in design work and to find out how digital equipment works. Switch for either TTL or CMOS. Our own modern design using a PUT. Includes detection circuit for very fast pulses. Gives visual (3 LED's) and audio (piezo buzzer) response.

CAT NO PRICE  
KIT 24EN \$10.88

#### Fiber Optic Audio Link

Allows you to send sound through plastic 1mm fiber optic cable. Matched transmitter/receiver pair from Motorola. Two circuit boards with a microphone at one end and a speaker at the other. 14 feet fiber optic cable supplied. Will work over 200 meters.

CAT NO PRICE  
KIT 26EN \$29.00

#### Two Stage FM Transmitter

Our most powerful FM 'bug' to date. A two stage FM transmitter with an RF transistor (2N3563 or ZTX320) in its output stage. 9V operation. On/off switch mounted on the PCB.

CAT NO PRICE  
KIT 32EN \$9.95

#### General Purpose 4-1/2 Digit Frequency Counter with LCD

General Purpose 4-1/2 Digit Counter uses Harris 7224 IC. Full instructions INCLUDING the 7224 data sheet is included. All pins from the 7224 are brought out for easy access. Directly drives an LCD (provided). This project is a building block that you can use as part of a larger project. The LCD section can be cut away and connected by a flat ribbon cable. The Kit has its own 5V regulated supply on board for the 7224, allowing a relatively wide range of voltage inputs from +6V to 10V. The Harris 7224 counts up to 15MHz, guaranteed, 25MHz typical.

CAT NO PRICE  
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#### Intro to Microcontrollers

Learn to program microcontrollers without going to technical college. This Kit introduces the Motorola 68HC705K1, an 8 bit, 16-pin microcontroller released in 1992. The Kit is a down counter from 60 or 90 seconds with beeps every 10 seconds. All the software code is supplied and fully explained. See how easy it is to change the time and beep settings by simple changes in the software program. You can judge for yourself how using micro-controllers is a huge advance over using logic ICs. On/off switch and pull-down resistors on input lines are all built into the K1 and are under software control. 9V battery powered.

All the information about how to continue learning to program these "computers-on-a-chip" is supplied. The tools to program the K1 are available at very low cost (under \$200) from Motorola. The K1 is the simplest 8-bit microcontroller available.

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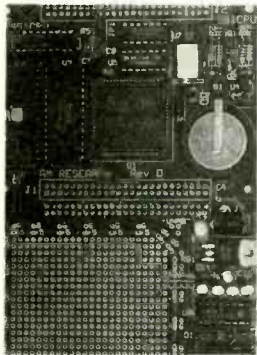
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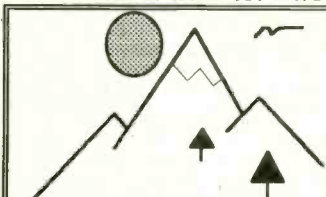


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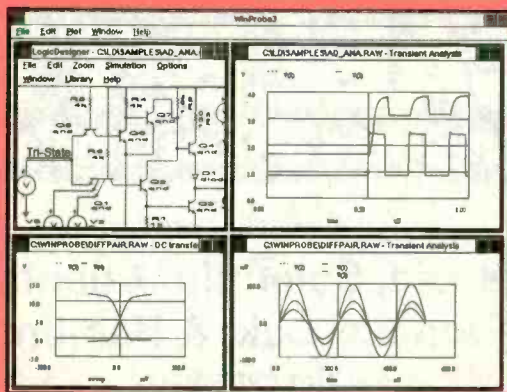
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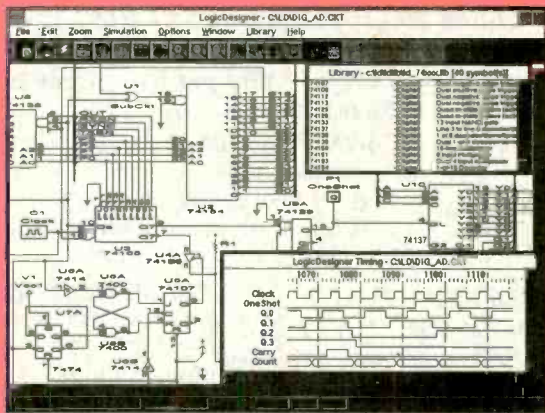
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### INFRA-RED TRANSMITTER / RECEIVER KIT \$5.50

Originally a remote control alarm panic button, this set includes two hand-held IR units, modification instructions to make either unit a receiver, an IR transistor, a resistor, and two 9 volt batteries, (one of those great moments when you find out batteries are included, huh!) Just add a bell or buzzer, a relay, or whatever you want and create your own remote control IR unit. You also get an added bonus, each unit includes stickers like the ones alarm companies put on the windows of protected houses, (you know, this house is protected by...)  
Makes a great single function remote control!

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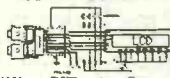
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There is a small prototyping area with space for connecting signals and extra components, and it runs on 5-12 VDC or a 9-volt battery! Multiple stamps can even be networked!!! The BASIC stamp is \$39.00 and the BASIC stamp developer kit (which includes 1 stamp plus all the hardware, software, and literature necessary to program a stamp) is \$138.00.

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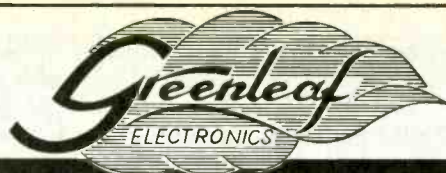
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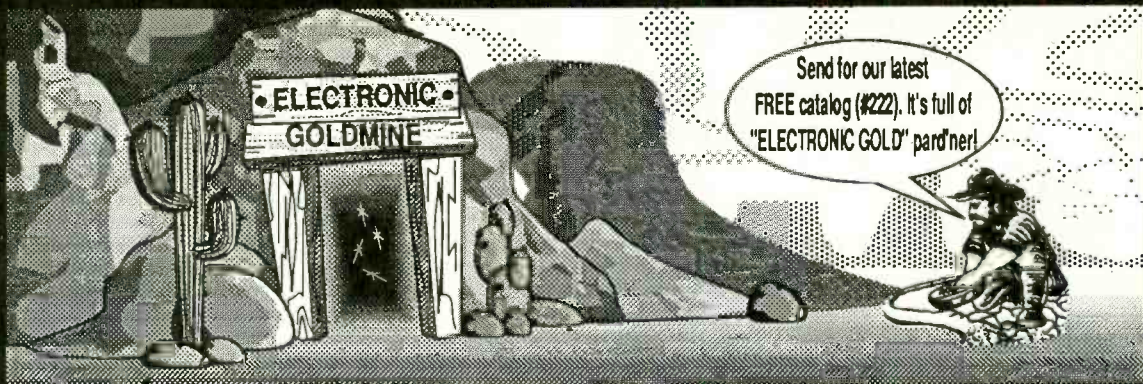
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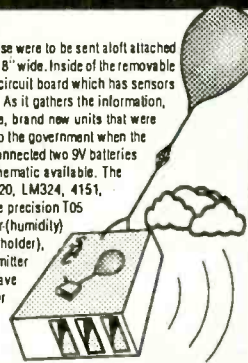


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MAIN BOARD AND NOSE CONE



G5058 \$8.95

### PERSONAL PERFORMANCE MONITOR/HEART PULSE SENSOR

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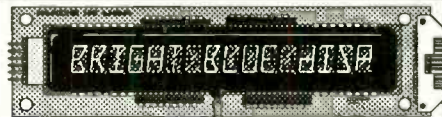


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79¢

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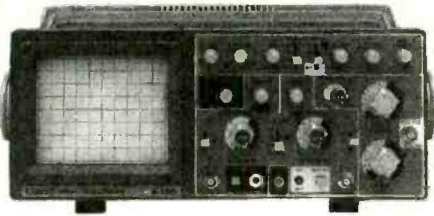
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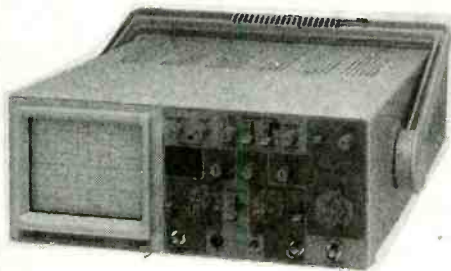
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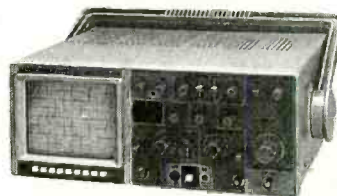
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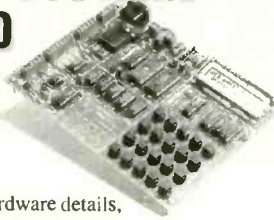
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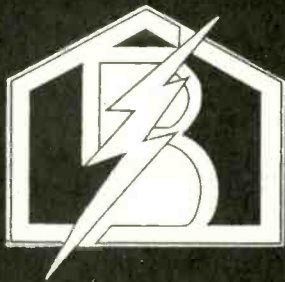
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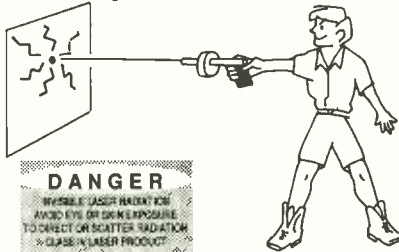
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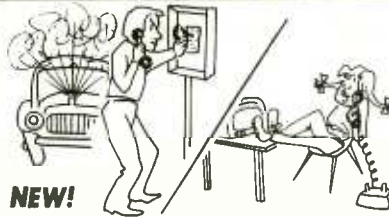
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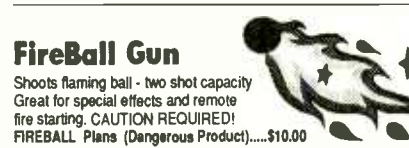
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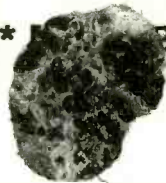
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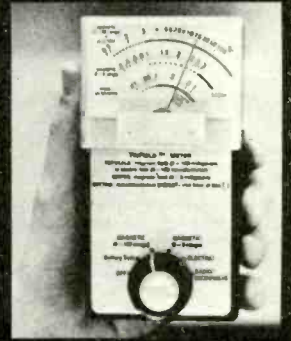
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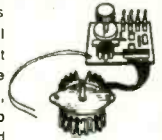


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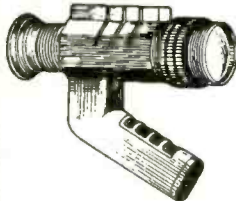


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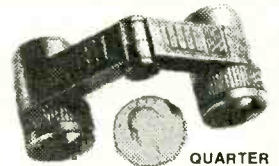


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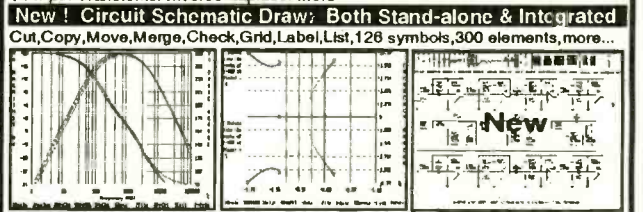
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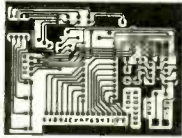
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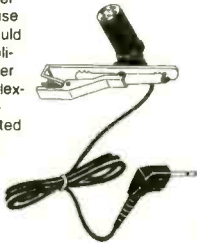
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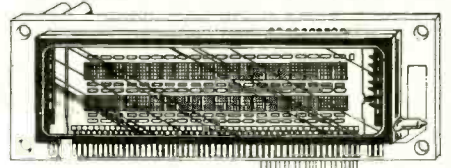
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## Futaba # M202SD08GL

Two rows of 20 characters displayed in a 5 X 7 dot matrix. Bright green 5 mm X 3.5mm characters. On board CPU, driver and DC-DC converter simplifies hook-up and interfacing. Operates on 5 Vdc. Displays 215 different characters including alphanumeric and other symbols. ASCII configuration. Module overall dimensions: 6.1" X 1.7" X 0.7" thick.

These displays were modified somewhat from original specifications and we do not know the exact nature of the modifications. They work fine in the test mode, but we don't know if the original interface is the same. We supply a data/ hook-up sheet for the pre-modified device which, hopefully, provides most of the information necessary to use the display.

## VACUUM FLUORESCENT DISPLAY



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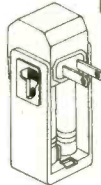
- 200 MV full scale sensitivity
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  - Decimal point selectable
  - 13 mm figure ht.
  - Automatic polarity indication
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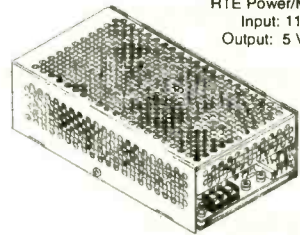


SANYO# NC-452  
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Magnet o.d. 1.35"



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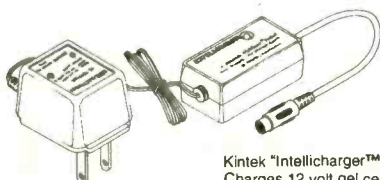
Mabuchi # RS-380PH  
Operates smoothly on 6 to 20 Vdc.  
3,200 RPM @ 12 Vdc (no load).  
1.15" diameter X 1.7" long.  
0.1" diameter shaft.

**\$2.50**  
each



CAT# DCM-47

## GELL CELL BATTERY CHARGER



Kintek "Intellicharger™"  
Charges 12 volt gel cell

lead-acid batteries of 1.6 amp/hours or greater. Charger circuit regulates current, providing more current to low cells and gradually ramping down current as battery approaches full capacity. Bi polar LED glows red when battery is taking a fast charge and green when battery is ready for use. Batteries can be left on charger indefinitely. Originally designed to charge a particular phone battery, the output cord on this device terminates with a 5 pin DIN plug which can easily be replaced with connectors more suitable to your particular application. You will need to open the case, clip-off the DIN cord and reconnect desired output cord.

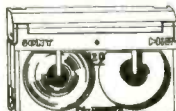
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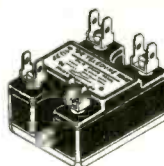
probably originally designed for 9 Vdc use, but they operate well on 6-12 Vdc. They accept color video and audio, and a selector switch is provided for output to channel 3 or 4. Easy to hook-up. Requires a 6-12 Vdc power supply or wall transformer and a connector to interface with your audio/video source. Output is an RCA jack. Hook-up instructions included. 3" X 1.47" X 0.75".

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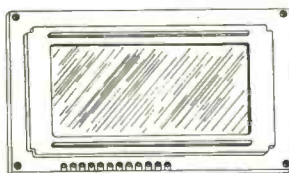


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## 240 X 128 DOT LCD

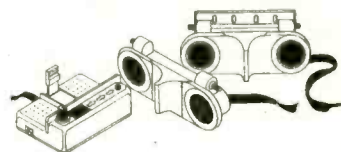


Optrex# DMF660N-S 240 X 128 dot LCD module with on-board drivers. Will display graphics, figures and characters. Module size: 5.68" X 4.1" X 0.5" thick. Viewing area: 4.1" X 2.52". Dot size: 0.4mm X 0.4mm. High contrast, wide viewing angle. Low voltage drive and low power consumption. Uses fitting controllers LSIMS6255, HD64646, SED1330, SED1351. Includes hook-up instructions and specs.

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CAT# LCD-15

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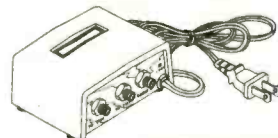
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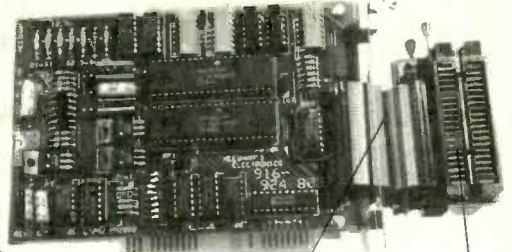
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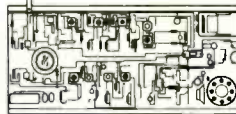
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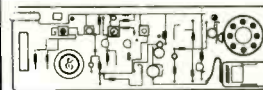
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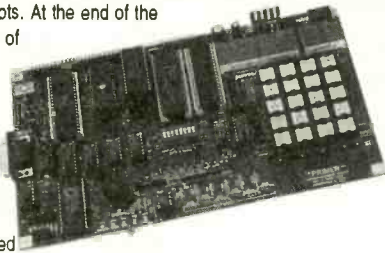
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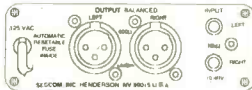


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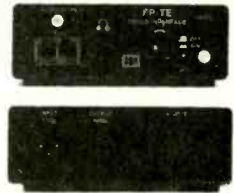


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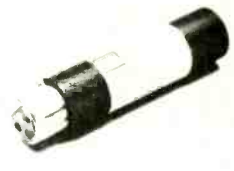


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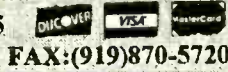
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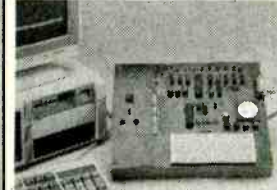
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## DC POWER SUPPLY



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**PS-305D \$399.95**

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**#202(8203) \$499.95(\$549.95)**, triple outputs, dual 0-30VDC/0-3A(5A), fixed 5VDC/3A, independent tracking operation, constant voltage and current.



## RF SIGNAL GENERATOR

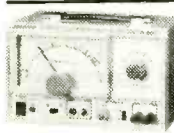


**SG-4160B \$119.00**  
100KHz-150MHz up to 450MHz on 3rd harmonics, 6 ranges, AM modulation.  
**RF OUTPUT:** 100mVrms to 35MHz

**MODULATION:** INT. 1kHz, EXT. 50Hz-20KHz.  
**AUDIO OUTPUT:** 1KHz, 1Vrms.

**SG-4162AD \$229.95**, with Freq. Counter 10Hz-150MHz for internal & external source.

## AUDIO GENERATOR

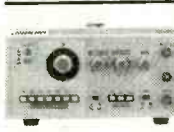


**AG-2601A \$119.00**  
10Hz-1MHz, 5 ranges  
**OUTPUT LEVEL:** sinewave 0-8Vrms, square 10Vp-p.  
**OUTPUT IMPEDANCE:** 600 Ohm.  
**DISTORTION:** <0.05%

500Hz-50KHz, <0.5% 50KHz-500KHz.

**AG-2603AD \$229.95**, with Freq. Counter 10Hz-150MHz for internal & external source.

## FUNCTION GENERATOR



**FG-2100A \$169.95**  
0.2Hz-2MHz in 7 ranges; Sine, Square, Triangle, Pulse & Ramp  
**OUTPUT:** 5mVp-p-20Vp-p, 1% distortion.

**PCF:** 0-10V control freq. to 1000.1.

**FG-2102AD \$229.95**, generates signals same as FG-2100, 4-digit counter display, TTL & CMOS outputs, 30ppm+/-1 count accuracy.

**FG-2020B \$169.00**

0.5Hz-500KHz, Sine, Square, Triangle.

**(FG)2103 \$329.95**, Digital sweep generator, 0.5Hz-5MHz in 7 ranges.

**OPERATING MODE:** sweep, AM, gated burst, VCG.

**FREQ. COUNTS R:** Internal 5Hz-5MHz

External 5Hz-10MHz

## SWR/RF POWER METER



**310 \$89.95**  
**FREQ RANGE:** 1.8-150MHz  
**RF POWER:** 0-4W/20W/200W

**SWR MEASUREMENT:** 1.0 - ∞, 4W minimum

**ACCURACY:** 5%-10%

**INSERTION LOSS:** 0.3dB

**INPUT/OUTPUT IMPED.:** 50ohm, SO-239 plugs

**320 \$89.95**, 130-520MHz

**330 \$129.95**, 1.8-520MHz

**SWR-3P \$26.95**

1.7-150MHz, RF Power: 0.5-10W, 0.5W-100W.

**SWR-2P \$22.95**, 1.7-30MHz, RF Power: 0.5-10W.

**PM-330 \$149.95** 1.8-500MHz, 0.5W/20W/120W



## STEREO MODULATOR

**AG-2011A \$549.00**

**RF SECTION:** CARRIER: 98MHz±/-2MHz

**OUTPUT:** 10mV, 1mV & 0.1mV

**COMPOSITE SIGNALS:**

**PILOT:** 19KHz±/-2KHz, 0.8Vrms

**INT. MODULATION:**

400KHz, 1KHz±/-1%

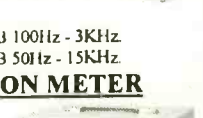
1Vrms, distortion: < .5%

**L-R SEPARATION:** >50dB.

**EXT. MODULATION:**

**FREQ.:** 50Hz-15KHz

**L-R SEPARATION:** >45dB 100Hz - 3KHz



>35dB 50Hz - 15KHz.

## AUTO DISTORTION METER

**DM-3104A \$799.95**

**MEASUREMENT:**

**RANGE:** 0.01%-30%

0.1/0.3/1/3/10/30% full scale.

**FREQ.:** 400Hz±/-10%

1000Hz±/-10%(HPF).

**INPUT:** 3mV-100V, ratio measuring 20dB.

**AUTO SWITCHING RANGES:**

Fundamental Freq. = (fo)±/-10%.

Fundamental Rejection: >-80dB at (fo)±/-5%

>-70dB at (fo)±/-10%

**HARMONIC ACCURACY:** ±/-5dB, 1.8(fo)-20KHz

## FREQUENCY COUNTER

**FC-5250C \$119.95**

**FREQUENCY RANGE:**

10Hz-220MHz;

(HF) 10Hz-20MHz,

(VHF) 10MHz-200MHz

**GATE TIME:** 0.1 & 1sec.

**INPUT SENSITIVITY:** 35mV 10Hz-200MHz

**INPUT IMPED.:** (HF) 1MOhm, (VHF) 50Ohm.

**MAXIMUM INPUT:** 10Vp-p.

**FC-5260A \$139.95**

10Hz-600MHz

**FC-5270A \$159.95**

10Hz-1300MHz

**FC-5600B \$329.00**

10Hz-600MHz

**(FC)5700B \$329.95**, 10Hz ~ 1.3GHz

## SIGNAL TRACER/INJECTOR

**SE-6100 \$134.95**

**TRACER:**

Gain Max. 60dB

**ATTENUATION:**

0/20/40/60dB

**INPUT IMPED.:** 100KOhm

**OUTPUT IMPED.:** 600Ohm, **SPEAKER:** 8 Ohm.

**INJECTOR:** Freq. 1KHz Squarewave, Output

Level. Continuously variable 0-4.5Vp-p.

## COLOR PATTERN GEN.

**CPG-1366A \$159.95**, VHF NTSC.

## GRID DIP METER



**DM-4061A \$99.95**  
1.5-250MHz, 6 bands,  
6 plug-in coils, 2 transistor,  
and 1 diode.

**MODULATION:** approx. 2KHz Sinewave

**CRYSTAL OSCILLATOR:** 1-15MHz

**POWER SUPPLY:** 9VDC.

## AM/FM SWEEMAR SCOPE



**SM-6225B/C \$1999.95**

**FREQ RANGE:**

420-490KHz(AM),

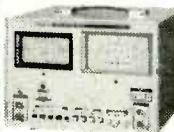
10-11.4MHz(FM).

**ACCURACY:** +/- 0.1%

**MARKER:** (AM)455KHz, +/-5KHz, +/-10KHz,

(FM)10.7MHz, +/-7.5KHz, +/-150KHz.

## WOW-FLUTTER METER



**WF-3103 \$699.95**

**FREQ. RANGE:**

3KHz±/- 10% JIS/CCIR

3.15KHz±/-10% DIN.

**MEASURE RANGE:**

0.03/1/3/3% full scale.

**ACCURACY:** +/-5%.

**WF-3105A \$799.95**, Digital.

**FUNCTION:** LIN/WOW/F/Flutter/WTD.

**FREQ CNTR:** 10Hz-9.99MHz

**INDICATION:** CCIR/DIN/JIS.

## AM/FM STD SIGNAL GEN.

**SG-4110A \$1999.95**

**FREQ:** 100KHz-110MHz

**DISPLAY:** 6-digit LED

**RESOLUTION:**

1001Hz (100-34.99MHz), 1KHz (35MHz-110MHz)

**ACCURACY:** <+/- (5X10-E5 +/-1 count)

**OUTPUT RANGE:** -19dBu, -99dBu, 1dB step

**IMPEDANCE:** 50Ohm VSWR 1.2.



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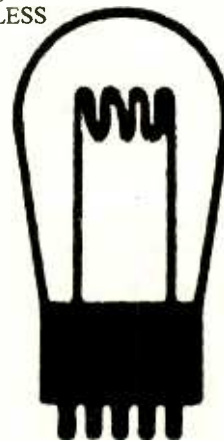
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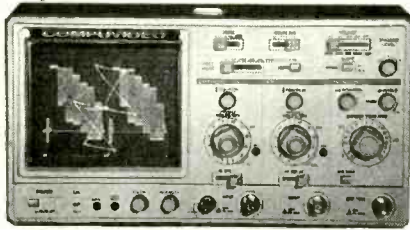
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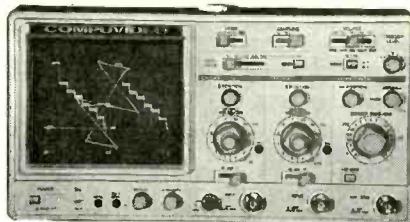
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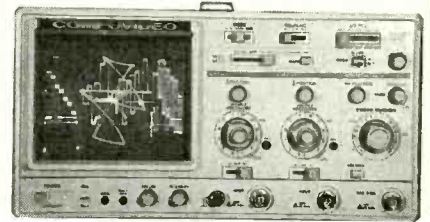
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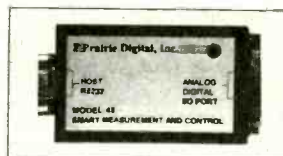
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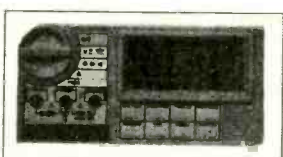
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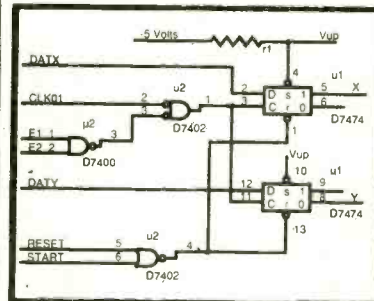


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Peak Hold  
Auto power off  
Ruggedized case.  
Rubber Holster \$8.00  
Temperature probe \$7.00



**DMM 21 \$74.95**

Inductance: 1μH-40H  
Capacitance: 1pF-200 F  
Frequency: 1Hz-1MHz  
Volt, amp, ohm, diode, continuity  
3999 count display  
TTL logic, HFE  
Peak hold  
Ruggedized case  
Rubber holster \$8.00

**Fluke Multimeter**  
Fluke 12 \$84.95  
Holster C-10 \$10  
Fluke 70 II \$67.5  
Fluke 73 II \$94  
Fluke 75 II \$129  
Holster C-70 \$16  
Fluke 77 II \$149  
Fluke 79 II \$169  
Fluke 29 II \$169  
Fluke 83 \$225  
Fluke 85 \$259  
Fluke 87 \$287  
Fluke 97  
Scope Meter \$1785

Full line of DMMs, economy, compact, ruggedized, solar cell, automotive, heavy duty, industrial starts from \$15.95



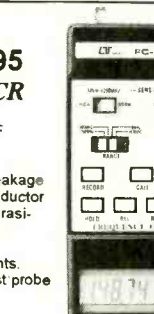
**LCR Meter 131D \$229.95**

**Most Advanced LCR**  
Dual display: L/Q or C/D  
Inductance: 0.1μH-1000H  
Capacitance: 0.1pF-10,000μF  
Impedance: 1mΩ-10MΩ  
0.7% basic accuracy  
Dissipation factor & Q factor  
Serial & parallel mode  
Relative mode for comparison and to remove parasitics  
Statistics, tolerance,  
Best for design, incoming testing & production  
SMD and chip component test probe \$25.00



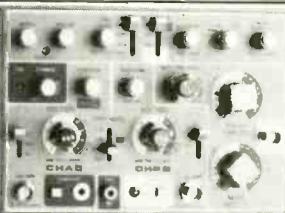
**LCR Meter 814 \$189.95**

**Best Resolution LCR**  
Inductance: 0.1μH-200H  
Capacitance: 0.1pF-20,000μF  
Resistance: 1mΩ-20MΩ  
1% basic accuracy  
Dissipation factor indicates leakage in capacitor and Q factor in inductor  
Zero adjustment to reduce parasitics from test fixture  
Best for high frequency RF and surface mount components.  
SMD and chip component test probe \$25.00, Deluxe carrying case \$5.00



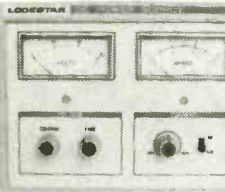
**Frequency Counter FC-1200 \$129.95**

Frequency: 0.1Hz-1.25GHz  
Display: 8 digit LCD  
Period: 0.1μs-0.1s  
Records: Max/Min/Average  
Data hold, relative mode  
Telescoping antenna \$8.00  
Deluxe case \$5.00  
**Also Available:**  
AC/DC clamp meter, Light meter, Thermometer, pH meter, High voltage probe, Digital caliper, Anemometer, Electronic scale, Force gauge, Tachometer, Stroboscope, Humidity & EMF adapter, Sound level meter, Frequency counter, SWR/field strength/power meter, Dip meter

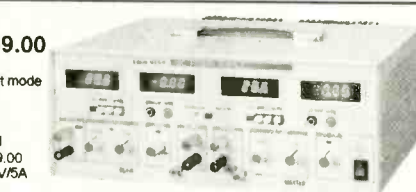


**20 MHz Oscilloscope with Delay Sweep PS-205 \$429.95**  
Dual Trace, Component test, 6" CRT, X-Y Operation, TV Sync, Z-Modulation, CH2 Output, Graticule Illum, 2 probes each has x1, x10 switch. Best price with delay sweep.  
PS-200 20 MHz DUAL TRACE \$339.95  
PS-400 40 MHz DUAL TRACE \$494.95  
PS-405 40 MHz DELAY SWEEP \$569.95  
PS-605 60 MHz DELAY SWEEP \$769.95  
Scope Probe: 60MHz x1, x10 \$13, 100MHz x1, x10 \$22

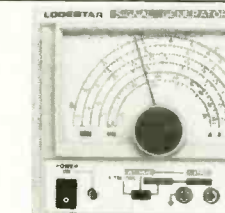
**20 MHz Digital Storage Oscilloscope DS-203 \$729.95**  
Switchable between digital and analog modes  
2 K word per channel storage  
Sampling rate: 10 M sample/sec  
8 bit vertical resolution (25 Level/div)  
Expanded Timebase 10ms/div - 0.5 s/div.  
Refresh, Roll, Save all, Save CH2, Pre-Trig  
Plotter Control  
250MHz x1, x10 \$29, 250MHz x100 \$39



**DC Power Supply PS-303 \$159.00**  
**0-30 VDC, 0-3A output**  
Constant voltage & constant current mode  
0.02% + 2mV line regulation  
0.02% + 3mV load regulation  
1 mVrms noise and ripple  
Short circuit and overload protected  
PS-8200 with digital voltmeter \$179.00  
Also available: 30V/5A, 60V/3A, 60V/5A, 16V/10A, 30V/10A



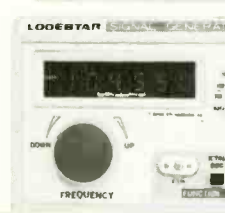
**DC Power Supply Triple Output PS-8202 \$499.95**  
Two 0-30 VDC, 0-3A outputs  
One fixed 5VDC, 3A output  
Capable of independent or tracking operation  
Constant voltage and constant current mode  
Four digital meters for volt and current display  
Excellent regulation and low ripple  
Short circuit and overload protected  
Also available: 30V/5A triple output \$549.95  
Dual tracking 30V/3A, 30V/5A, 60V/3A, 60V/5A



**RF SIGNAL GENERATOR SG-4160B \$119.00**  
100 kHz-150MHz sinewave in 8 ranges  
RF Output 100mVrms to 35 MHz  
Internal 1kHz, External 50Hz-20kHz  
AM modulation  
Audio output 1 kHz, 1 Vrms

**AUDIO GENERATOR AG-2601A \$119.00**  
10Hz - 1MHz in 5 ranges  
Output 0-8Vrms sinewave  
0-10Vp-p squarewave  
Synchronization: ±3% of oscillation frequency per Vrms  
Output distortion:  
0.05% 500Hz - 50kHz  
0.5% 50Hz - 500kHz  
Output impedance: 600 ohm

**FUNCTION GENERATOR FG-2100A \$169.95**  
0.2 Hz - 2 MHz in 7 ranges  
Sine, square, triangle, pulse and ramp  
Output: 5mV-20Vp-p  
1% distortion, DC offset ± 10V  
VCF: 0-10V control frequency to 1000.1



**RF SIGNAL GEN./COUNTER SG-4162 AD \$229.95**  
Generates RF signal same as SG-4160B  
Frequency counter 1Hz - 150 MHz for internal and external source  
Sensitivity <50mV

**AUDIO GEN./COUNTER AG-2603AD \$229.95**  
Generates audio signal same as AG-2601A  
Frequency counter 1Hz-150MHz for internal and external sources  
Sensitivity <50mV

**FUNCTION GEN./COUNTER FG-2102AD \$229.95**  
Generates signal same as FG-2100A  
Frequency counter 4 digits  
Feature TTL and CMOS output  
**SWEEP FUNCTION GEN./COUNTER \$329.95**  
0.5Hz to 5 MHz in 7 ranges  
Sweep: Linear 10:1/Log 10:1 20ms to 2s  
AM Modulation  
Gated Burst, Voltage Control Generator  
Generator Control Voltage & 6 digit counter  
1Hz-10MHz for internal & external sources

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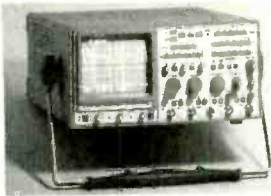
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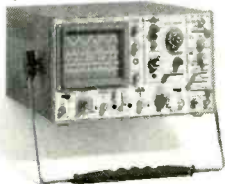
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### 100 MHz Cursor Readout Scope 4 ch, 8 traces OS-6101 \$1,499.95



- \* 4 independent channels, 8 traces
- \* Time / Voltage cursor measurement
- \* ALT triggering function for 4 ch.
- \* Sweeps to 2ns/div, Delayed Sweep
- \* TV Sync., Ch. 1 output, Z-axis input
- \* 2 probes(x1, x10)

### 100 MHz Scope, 4ch. 8 traces Best value all purpose scope OS-6100B \$1,329.95



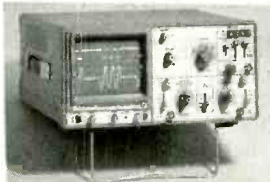
- \* 4 channels, 8 traces
- \* High sensitivity 500µV/div
- \* Sweeps to 2ns/div, Delayed sweep
- \* 20 kV accelerating voltage
- \* TV sync., Z-axis input
- \* A and B gate output
- \* Best price 100 MHz scope
- \* 2 probes(x1, x10)

### 50 MHz Triggering Oscilloscope OS-653 \$699.95



- \* Dual Channel
- \* Hold Off Function
- \* Delayed Sweep
- \* Built-in Delay Line
- \* TV Sync
- \* ALT Triggering
- \* High sensitivity 1 mV/div
- \* Trigger level lock function
- \* Z-axis input, CH1 output
- \* 2 probes(x1, x10)

### 20 MHz Oscilloscope OS-622B \$344.95



- \* Dual trace, X-Y operation
  - \* TV Sync., Z-axis input, CH1 output
  - \* High sensitivity 1 mV/div
  - \* Trigger level lock
  - \* 2 probes (x1, x10)
- |                                       |           |
|---------------------------------------|-----------|
| OS-645B - 40 MHz Cursor readout.....  | \$ 734.95 |
| OS-625B - 20 MHz Cursor readout.....  | \$ 549.95 |
| OS-623B - 20 MHz w/Delayed Sweep..... | \$ 449.95 |
| OS-935 - 5 MHz One channel.....       | \$ 209.95 |

### DC Linear Power Supplies Single Output



- \* Constant voltage and constant current mode
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- \* Current regulation ≤0.2%
- \* Low ripple and noise
- \* Overload and reverse polarity protection
- \* Features 2 analog or 1 digital meter(PS series)  
2 analog or 2 digital meters(PR series)

PS-1830 : (0-18V, 0-3A).....	\$194.95
PS-1830D : Digital Display.....	\$204.95
PS-1850 : (0-18V, 0-5A).....	\$204.95
PS-1850D : Digital Display.....	\$229.95
PS-3225 : (0-32V, 0-2.5A).....	\$199.95
PS-3225D : Digital display.....	\$219.95
PS-6010 : (0-60V, 0-1A).....	\$199.95
PR-1810H : (0-18V, 0-10A).....	\$329.95
PR-3060 : (0-30V, 0-6A).....	\$299.95
PR-6030 : (0-60V, 0-3A).....	\$299.95
PR-6030D : Digital Display.....	\$399.95

### Triple Output DC Power Supplies



- \* Two variable 0-30VDC, 0-3A outputs
  - \* One fixed 5VDC, 3A output
  - \* Auto tracking
  - \* Auto serial and parallel operation
  - \* Constant voltage and constant current mode
  - \* Continuous/dynamic load can be selected
  - \* Features 4 analog or 2 digital displays
- |                                 |          |
|---------------------------------|----------|
| PC-3030 : (0-30V, 0-3Ax2).....  | \$479.95 |
| PC-3030D : Digital display..... | \$509.95 |

### Programmable DC Power Supplies



- \* High stability, low drift, 4 digit display
  - \* Front/rear output-sense switch selectable
  - \* Auto step running w/timer settings
  - \* 100 point programmability (PPS series)
  - \* 50 point programmability (PPT series)
  - \* Auto serial and parallel operation (PPT series)
  - \* Auto tracking (PPT series), IEEE-488.2 and SCPI compatible command set (optional)
- |   |           |
|---|-----------|
| PPS-1860G: (0-18V, 0-6A).....                 | \$999.95  |
| PPS-3635G: (0-36V, 0-3.5A).....               | \$999.95  |
| PPS-6020G: (0-60V, 0-2A).....                 | \$999.95  |
| PPT-1830G: (0-18V, 0-3Ax2, 0-6V, 0-5A).....   | \$1299.95 |
| PPT-3615G: (0-36V, 0-1.5Ax2, 0-6V, 0-3A)..... | \$1299.95 |

### Digital Display Function Generator FG-8016G \$239.95



- \* Frequency Range: 0.02Hz to 2MHz
- \* Three Instruments in one: Function generator, Pulse generator & Frequency counter.
- \* Sine, Triangle, Square, TTL Pulse and CMOS output
- \* Built-in 6 digit counter with INT/EXT function
- \* 1000:1 tuning range
- \* Variable DC offset control

FG-8015 Function Generator	
* 0.02Hz-2MHz (No Counter).....	\$189.95
FC-8131 Intelligent Counter 1.3GHz.....	\$469.95
FC-8270 Intelligent Counter 2.7GHz.....	\$599.95
UC-2010G Universal Counter.....	\$289.95

### Digital Multimeter & C Meter DM-8034(3½ digits) \$179.95



- \* 8 Function, AC/DC voltage, AC/DC current, resistance
  - \* Built-in C meter, diode test and audible continuity check
  - \* High voltage 1000V and 20A range
  - \* 0.5% basic accuracy
- |                                      |          |
|--------------------------------------|----------|
| DM-8040 (3½ Digits, True RMS)        |          |
| * Measures ACV to 50 kHz.....        | \$339.95 |
| DM-8055 (5½ Digits).....             | \$649.95 |
| * 0.006% basic accuracy              |          |
| * 1µV, 1mΩ, 1nA resolution           |          |
| * dBm measurement                    |          |
| * Auto range, relative mode, Max/Min |          |
| DM-8055G(5½ Digits, GPIB).....       | \$889.95 |

### Model DM-392 (3½ digits) \$109.95



- \* Auto/Manual ranging(38 ranges)
- \* 42 Segment analog bar graph
- \* Data Hold/Min-Max memory /Relative mode
- \* Auto power off
- \* Overload protection
- \* Audible continuity check
- \* Diode test
- \* Capacitance: 1pF-40µF
- \* Frequency: 0.1Hz-1MHz
- \* 20 Amp range
- \* Double high energy fused (1A, 20A)
- \* 0.3% DCV accuracy
- \* AC True RMS (DM-394 only)

DM-351 3½ Digits w/Continuity, Auto Off.....	\$54.95
DM-352 3½ Digits, Cap. Freq. hFE, 20 Amp.....	\$79.95
DM-353 3½ Digits, Cap. Freq. Temp. hFE.....	\$84.95
DM-391 3½ Digits, Auto, Cap. Freq. Min/Max.....	\$99.95
DM-392 3½ Digits, Hold, Min/Max 20Amp.....	\$109.95
DM-393 3½ Digits, Peak, Logic, hFE, Freq.....	\$119.95
DM-394 3½ Digits, TRMS, Same as DM 392.....	\$129.95

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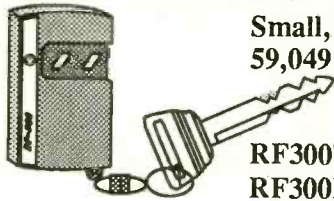
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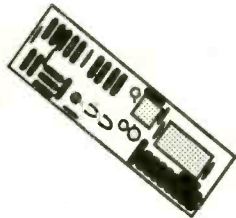
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# Miniature Transmitters and Receivers



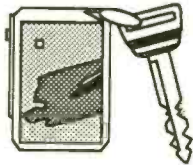
Small, Attractive, High End Quality, 2 Channel 318 MHz Transmitter  
59,049 Settable Codes, 120'-300' Range, 1-1/4" x 2" x 9/16", Assembled

	Qty	1	5	10
RF300T 150' Range Transmitter		24.95	19.95	15.95
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Small, High End Quality, 2 Channel Receiver for the RF300 Transmitters  
1-1/4" x 3-3/4" x 9/16" PCB w/ .1" spaced pads for standard connectors  
Input: 8-24 vdc Output: Gated CMOS Momentary and Latching Lines

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RF300PA Pre-Amplifier. Doubles Range		14.95	11.95	9.95



Small, Economical, Single Channel Transmitter and Receiver Set  
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RF60 Transmitter and Receiver Set		24.95	19.95	14.95

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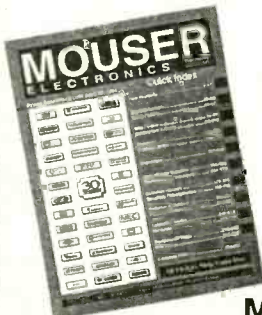
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TEK 475 200 MHz Dual Channel Oscscope	\$750.00
TEK 485 350 MHz Dual Channel Oscscope	\$950.00
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TEK 7B15 1 GHz Delaying Time Base	\$600.00
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HP 8080A 1 GHz Dual Channel Pulse Gen	\$1,400.00
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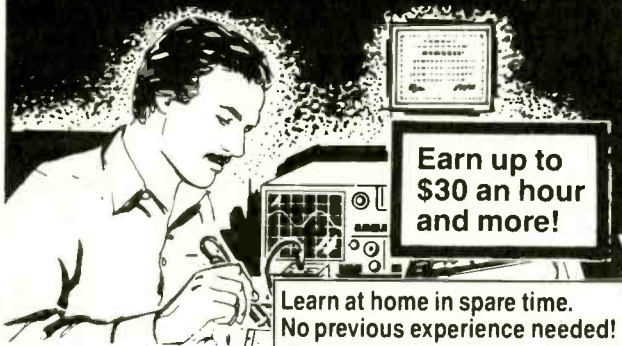
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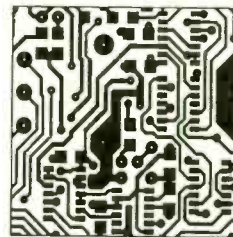
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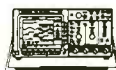
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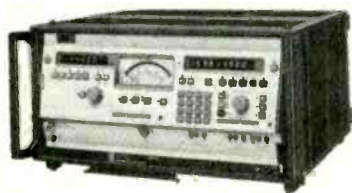
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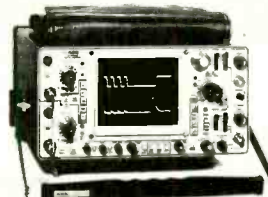
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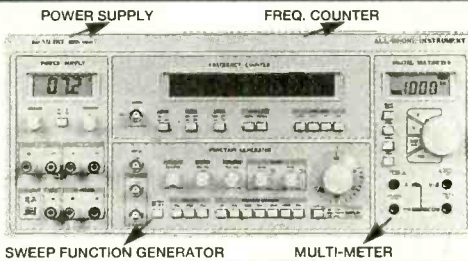
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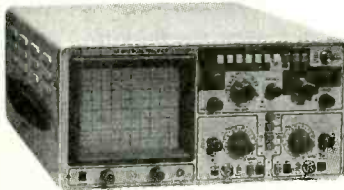
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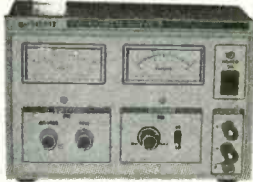
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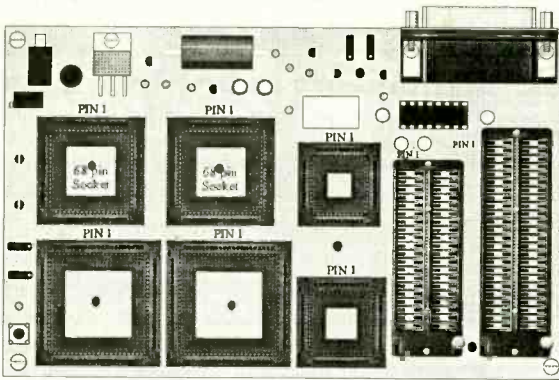


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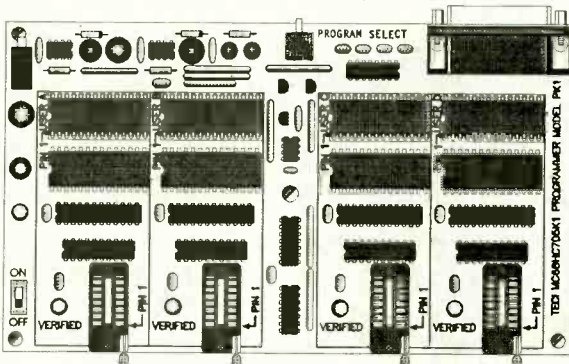
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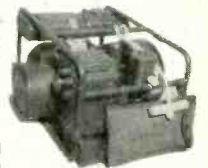


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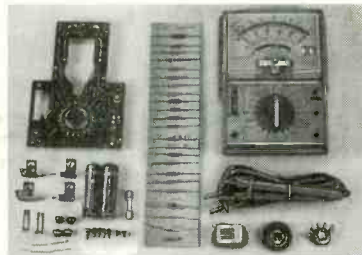
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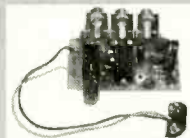


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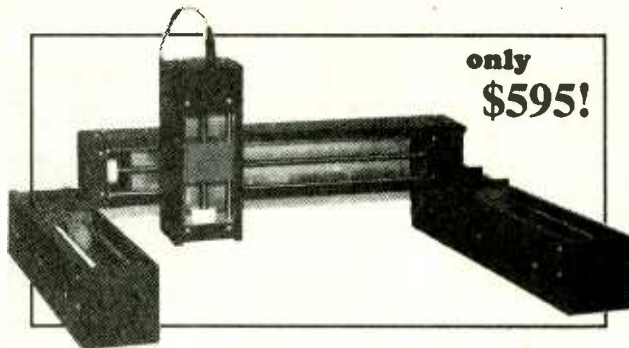
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## Total Coverage Radios

### TR1000XLT

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1000 Channels

500KHz to 1300MHz coverage in a programmable hand held. Ten scan banks, ten search banks. Lockout on search and scan. AM plus narrow and broadcast FM. Priority, hold, delay and selectable search increment of 5 to 995 KHz. Permanent memory. 4 AA ni-cads and wall plus cig charger included along with belt clip, case, ant. & earphone. Size: 6 7/8 x 1 3/4 x 2 1/2. Wt 12 oz. Fax fact document # 205



### TR 2500

\$449.00

2016 Channels  
1 to 1300MHz  
Computer Control

62 Scan Banks, 16 Search Banks, 35 Channels per second. Patented Computer control for logging and spectrum display. AM, NFM, WFM, & BFO for CW/SSB. Priority bank, delay/hold and selectable search increments. Permanent memory. DC or AC with adaptors. Mtng Brkt & Antenna included. Size: 2 1/4H x 5 5/8W x 6 1/2D. Wt. 1lb. Fax fact #305



### TR980

\$299.00

125 Channels  
5MHz to  
1300MHz

Most Economical receiver in its class, offers AM, NFM Wide FM, modes. 5KHz increments. Delay & hold & Search. Cell Lock NiCads, chgr & whip ant. Size: 5 7/8H x 1 1/2W x 2 D. Wt 14oz.



### NEW TR1500

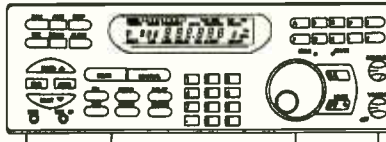
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Full Coverage with SSB  
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100KHz to 2060MHz. Ten scan banks, ten search banks. Search lock and store. BFO. Antennas. AM/NFM/WFM. Selectable increments. Tons of features, small size: 5 7/8 x 1 1/2 x 2. Wt 14 oz. Fax fact document # 250



## Continuous Coverage



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Bearcat 2500XLT hand held.....\$349.95

Bearcat 8500XLTC mobile.....\$389.95

Bearcat 890XLTB mobile.....\$259.95

25-1300MHz, 500 ch. in 8500, 400 in 2500. 890 has 200 ch & 29-956MHz. All cell locked. Features include turbo scan, VFO, search and store, Priority, LCD display, and more. Fax Facts 474, 475, 476

## Mobile Scanners

Bearcat  
760XLTM  
\$219.95  
100 Channel  
800 MHz



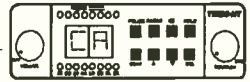
Five banks of 20 channels each. Covers 29-54, 118-174, 406-512 and 806-954MHz (with cell lock). Size: 4 3/8 x 6 15/16 x 1 5/8. Weight: 4.5lbs. Fax fact document #550

Bearcat  
560XLTZ  
\$99.95  
16 Channel  
10 Band



Compact, digital programmable unit covers 29-54, 136-174, and 406-512MHz. Size: 7 3/8 x 2 1/2 x 15/8. Wt: 2.5lbs. Fax fact #560

Trident  
TR-33WL  
\$299.00



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Sangean ATS-808.....	\$179.95
Sangean ATS-606.....	\$149.95
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## Hand Held Scanners

### Bearcat 200XLTN

\$209.95 200 Channels 800 MHz

Ten scan banks plus search. Covers 29-54, 118-174, 406-512 and 806 956MHz (with cell lock). Features scan, search, delay, 10 priorities, mem backup, lockout, WX search, keylock. Includes NiCad & Chgr. Size: 1 3/8 x 2 11/16 x 7 1/2. Wt. 32 oz. Fax Facts # 450



Bearcat 100XLTN 100Ch H/L/U..... \$159.95

Bearcat 70XLTP 20Ch H/L/U..... \$139.95

Bearcat 55XLTR 10 Ch H/L/U..... \$ 99.95

Coverage of above hand helds is: 29-54, 136-174, 406-512 except 100 which also adds 118-136 Air Band. Fax facts #475

## Table Top Scanners

Bearcat 855XLTE 50Ch w/800.....	\$159.95
Bearcat 142XLM 10Ch H/L/U.....	\$ 84.95
Bearcat 147XLJ 16 Ch H/L/U.....	\$ 89.95
Bearcat 172XM 20Ch H/L/U/Air.....	\$124.95
Bearcat 210 16Ch H/L/U/Air.....	\$129.95

Coverage of above units is: 29-54, 136-174, 406-512, plus Air in 172 and 210 and air plus 800MHz in the 855. Fax facts #675

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\$209.95



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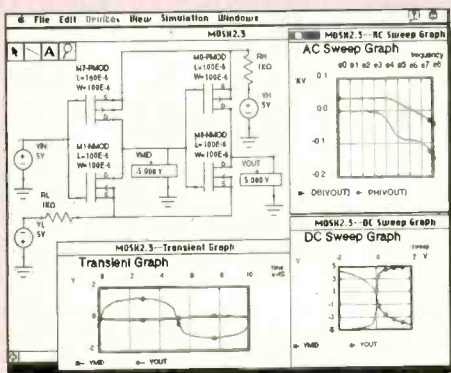
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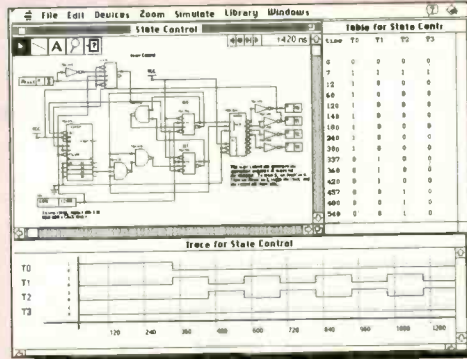
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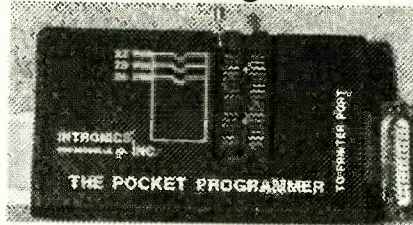
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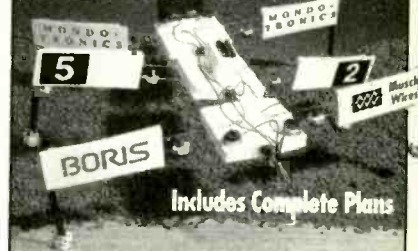
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### How strong are Muscle Wires?

This varies with the wire's size. A single wire can lift from 35 to 930 grams (over 2 lbs)! For more strength, use several wires in parallel.

### How fast can Muscle Wires activate?

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### Flexinol Muscle Wire Specifications

Wire Diameter (μm)	50	100	150	250
Resistance (Ω/m)	510	150	50	20
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### How much power do Muscle Wires need?

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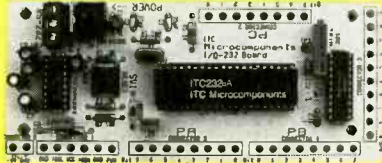
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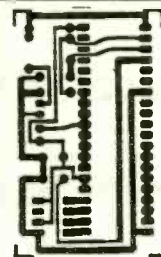
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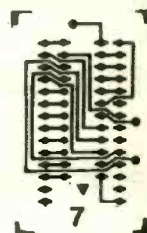
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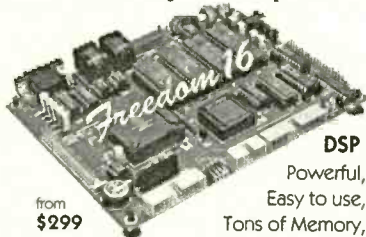
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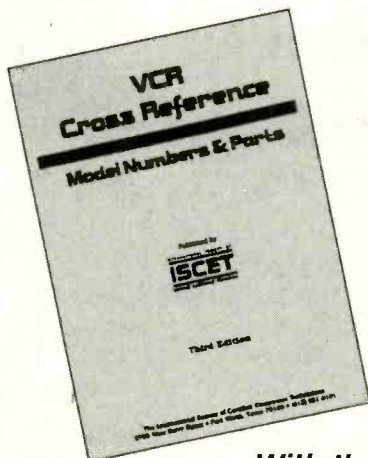
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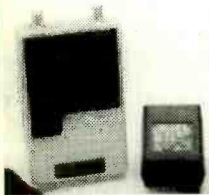
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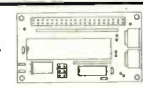
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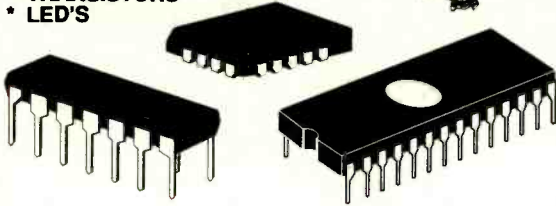
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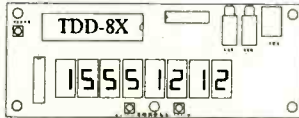
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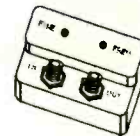
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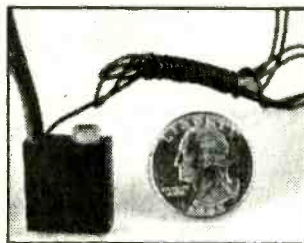
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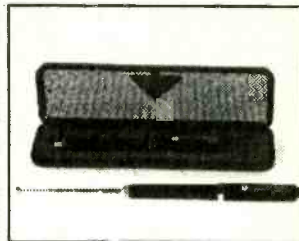


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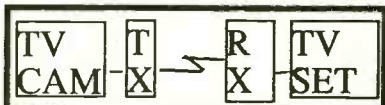
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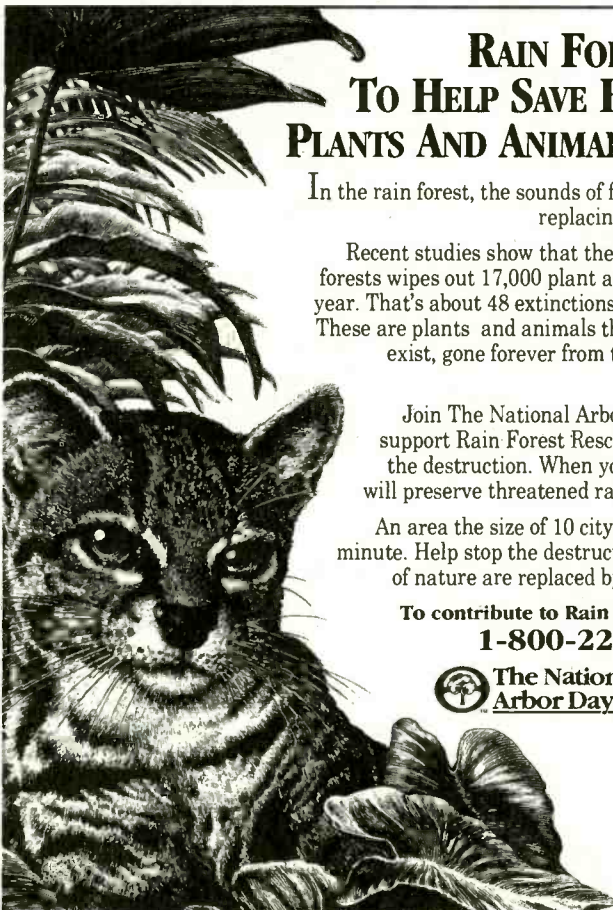
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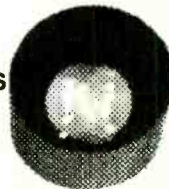


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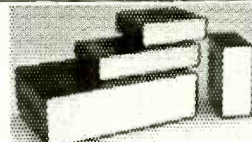
**BOOM  
MIKE**

Electret condenser type. This versatile microphone can be wired for Handy Talkie, telephone, base station, aircraft radio, CB radio, motorcycle intercom, etc. An earphone or miniature speaker may be installed in either or both muffs. The microphone unit can be easily removed and installed on another headset or helmet. (92A001) **\$4.95**

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**STEEL ENCLOSURES**

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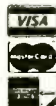
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141T/8552A/8553, SPECT ANAL, 1KHZ-110MHZ	1800.00
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141T/8552A/8555, SPECT ANAL, 10MHZ-18GHZ	2250.00
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1722B, 275 MHz PORTABLE O'SCOPE	900.00
1740A, 100 MHz PORTABLE O'SCOPE	600.00
1741A, 100 MHz PORTABLE O'SCOPE	800.00
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204C, AUDIO OSCILLATOR, 4Hz-10MHz	250.00
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3312A, 13 MHz FUNCTION GENERATOR	800.00
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3403C, TRMS DMM, 3.5 DIGIT, 1.6Hz-10kHz	450.00
3406A, BROADBAND SAMPLING VOLTMETER	800.00
3437A, HIGH SPEED SYSTEM DMM, 1000 R/SEC HPIB	350.00
3440/3444A, DIGITAL MULTIMETER	75.00
3455A, 6-1/2 DIGITAL MULTIMETER	700.00
3467A, LOGGING MULTIMETER, 4.5	1000.00
3469B, MULTIMETER, DIGITAL/ANALOG READOUT	275.00
3490A, DMM, 5 DIGIT	275.00
3555B, TRANSMISSION & NOISE MEASUREMENT SET	200.00
3581A, WAVE ANALYZER, 15 Hz-50 kHz	1200.00
3581C, SELECTIVE VOLTMETER, 15HZ-50KHZ	1500.00
3582A, SPECTRUM ANALYZER, .02Hz-25.6Hz	5000.00
3586B, SELECTIVE LEVEL METER	1000.00
3702A, IF/BB RECEIVER	2000.00
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431, POWER METER	75.00
431B, POWER METER	100.00
431C, POWER METER	150.00
432A/478A, PWR MTR, 0.01-10 GHz, -20 dBm TO +10 dBm	300.00
435A, POWER METER	450.00
435A/8481B, PWR MTR W/SENSOR, 1 mW-25 W, 0.01-18 GHz	1325.00
436A/03/002 DIGITAL PM w/ HPIB	\$900.00
436/8484 DIGITAL PM/SENSOR	\$1500.00
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4800A/4801A, VECTOR IMPEDANCE METER, 5 Hz-500 kHz	550.00
491C, AMPLIFIER, TWT, 2.4GHZ, 1W 30DB GAIN	2000.00
4935A/003, TRANS TEST SET, AC & BATT. PWR	1250.00
5004A, SIGNATURE ANALYZER w/ PROBES	250.00
5245L, 50MHz FREQUENCY COUNTER	75.00
5246L, FREQUENCY COUNTER	75.00
5253B, FREQUENCY CONVERTER, 18GHZ	350.00
5300B/5305B, MEASURING SYSTEM	450.00
5302A, UNIVERSAL COUNTER, 50MHZ	150.00
5305B/5300B/001, 1.3 GHz COUNTER WITH TCXO REF	450.00
5312A, HP-1B INTERFACE	100.00
5314A, 100 MHz/100 nS UNIVERSAL COUNTER, PORTABLE	250.00
5315A, UNIVERSAL COUNTER	500.00
5326C, UNIVERSAL COUNTER, 50MHZ	100.00
5328A, TIMER/COUNTER, 500MHZ, DUAL CHANNEL	250.00
59500A, MULTIPROGRAMMER INTERFACE	500.00
6110A, 3000V AT 6mA DUAL POLARITY POWER SUPPLY	275.00
6111A, PRECISION POWER SUPPLY, 0-20V, 0-1A	275.00
6130B, BIPOLAR DIGITAL PROG. POWER SUPPLY, +/-500A	600.00
6131B, CVCC, PROG., +/-100@5A	1500.00
6186B, DC CURRENT SOURCE, TO 300V, 100mA	450.00
6200B, 40V/20V AT 0.3A/0.6A CVCC POWER SUPPLY	200.00
6201, 0-20V, 0-1.3A, THREE UNITS	175.00
6255A, DUAL DC POWER SUPPLY, 40V AT 1.5A	450.00
6264B, 20V AT 20A CVCC POWER SUPPLY	500.00
6267B, 0-400 AT 10A CVCC POWER SUPPLY	700.00
6282A, 10V AT 10A CVCC POWER SUPPLY	275.00
6284A, 0-20V DC AT 3A DC POWER SUPPLY	275.00
6291A, 40V AT 5A CVCC POWER SUPPLY	375.00
6299A, 100V AT 750mA CVCC POWER SUPPLY	275.00
6439B, 0-60V DC AT 15A DC	600.00
6448B, 600V AT 1.5A CVCC POWER SUPPLY	700.00
652A, AUDIO OSCILLATOR, 10Hz-10MHz	275.00
6824A, POWER SUPPLY/AMPLIFIER, 50V 1A	300.00
6940B, MULTIPROGRAMMER	500.00
6942A, MULTIPROGRAMMER	1500.00
775D, DUAL DIRECTIONAL COUPLER, 450-950MHZ	250.00

8080A/8091A/, 1 GHz CLOCK GENERATOR	950.00
809B/806B/444A, SLOTTED LINE SYSTEM, 2-12.4 GHz	135.00
8405A, VECTOR VOLTMETER, 1-1000 MHz	600.00
8407A, NETWORK ANALYZER, 0.1-110 MHz	300.00
8411, HARM FREQ CONV, OPT 018, 0.11-18.0GHZ	725.00
8411A, FREQ CONV for 8410, 110MHz-12.4GHz	500.00
8411A/018, FREQ CONV for 8410, 110MHz-18GHZ	725.00
8412A, PHASE MAG. DISPLAY for 8410	400.00
8413A, PHASE GAIN INDICATOR for 8410	150.00
8414A, POLAR DISPLAY	275.00
8418A, AUX. DISPLAY HOLDER	200.00
8443A, TRACKING GEN/COUNTER, LED DISPLAY	700.00
8444A, TRACKING GENERATOR, 0.5-1300 MHz	800.00
8445B, AUTOMATIC PRESELECTOR	700.00
8447A, AMPLIFIER, 0.1-400 MHz	300.00
8552A, IF SECTION	500.00
8552B, IF SECTION, SWITCH DISP. MODES	750.00
8553B, RF SECTION, 0-110 MHz	500.00
8553L, SPECTRUM ANALYZER-RF SECTION	350.00
8554B, RF SECTION, 0.1-1250 MHz	800.00
8555A, RF SECTION, 10 MHz-18 GHz	800.00
8556A, LF SECTION, 20 Hz-300 kHz	500.00
85B, COMPUTER	350.00
8614A, SIGNAL GENERATOR, 0.8-2.4 GHz	375.00
8620A/8621A, SWEEP OSC. SYSTEM 0.1-4.2 GHz	600.00
8620C/011, SWEEP OSCILLATOR MAINFRAME, HPIB	550.00
86222A, RF PLUG-IN, 0.1-2.4GHZ	400.00
86222B, RF PLUG-IN, 0.1-2.4GHZ	1700.00
86222B/002, RF PLUG-IN, 0.01-2.4 GHz	1800.00
86230B, RF PLUG IN, 1.8-4.2 GHz	400.00
86240B, 2-8.4GHZ PLUG	200.00
86241A/001, RF PLUG IN, 3.2-6.5 GHz	400.00
86245A, RF PLUG-IN, 5.9-12.4GHZ	250.00
86260A, RF PLUG-IN, 12.4-18GHZ	800.00
8640B, SIGNAL GENERATOR, 0.5-512 MHz, AM/FM	1400.00
8683B, SIGNAL GENERATOR, 2.3-6.5 GHz	4000.00
8740A/H18, TRANSMISSION TEST UNIT, DC-18 GHz	100.00
8742A, REFLECTION TEST SET	500.00
8745A, S-PARAMETER TEST SET, 0.1-2.0GHZ	675.00
9278A, PLOTTER	125.00

## TEKTRONIX

1240, LOGIC ANAL W/ 2 D2 CARDS, 36 CHANNEL	1000.00
1241/D2/D2, LOGIC ANAL, 36 CHAN, 50 MHz, CLR DISP	2000.00
144, NTSC TEST SIGNAL GENERATOR	700.00
147, NTSC TEST SIGNAL GENERATOR	\$600.00
184, TIME MARK GENERATOR	50.00
2213, 60MHz DUAL CHANNEL O'SCOPE	\$600.00
2215, 60MHz DUAL TRACE O'SCOPE	\$800.00
2235, 100MHz DUAL CHANNEL O'SCOPE	\$1200.00
2245, 100MHz, CH 34 for DMM MEASURE	\$1700.00
2246, 100MHz 100MHz ON SCREEN DMM	\$1900.00
2445, 150MHz CURSORS	\$2500.00
2465, 300MHz 4 CHANNEL O'SCOPE	\$3500.00
434, STORAGE O'SCOPE, 25MHZ	500.00
465B, 100MHz DUAL VERT./TIME O'SCOPE	675.00
466, 100 MHz VERT./TIME STORAGE O'SCOPE	1100.00
475, 200 MHz DUAL CHANNEL O'SCOPE	750.00
475A, 250MHz DUAL CHANNEL O'SCOPE	825.00
485, 350 MHz DUAL VERT./TIME O'SCOPE	900.00
491, SPECTRUM ANALYZER, 10 MHz-12.4 GHz	950.00
492, SPECTRUM ANALYZER, 50 kHz-21 GHz	\$950.00
528, TELEVISION WAVEFORM MONITOR	500.00
5440/D40, 50 MHz THREE SLOT FRAME	225.00
577/D2, CURVE TRACER	1505.00
5A22N, DIFFERENTIAL AMPLIFIER	400.00
7623A, MULTIMODE STORAGE O'SCOPE, 100MHz	375.00
7633, 100 MHz STORAGE, 1000cm/uS WRITING	600.00
7704, 150MHz, FOUR SLOT FRAME	250.00
7704A, 250 MHz FOUR SLOT FRAME	325.00
7834, 400 MHz STORAGE, 2500 cm/uS WRITING	750.00
7834, 400 MHz SYS, W/(1)7A24,(1)7A26,(1)7B80,(1)7B85	1150.00
7844, 400 MHz DUAL BEAM FRAME	900.00
7904, 500 MHz FOUR SLOT FRAME	450.00
7904, 500 MHz SYS, W/(1)7A19,(1)7A26,(1)7B80,(1)7B85	1000.00
7A13, DIFFERENTIAL COMPARATOR, LED DISPLAY	400.00
7A14, CURRENT PROBE AMPLIFIER, 120MHZ	175.00
7A18, 75 MHz DUAL TRACE AMP	100.00
7A19, 600 MHz AMP	250.00
7A24, 400 MHz DUAL TRACE AMP	450.00
7A26, 200 MHz DUAL TRACE AMP	200.00
7A29, 16Hz VERT. PLUG	800.00
7A42, 4 CHANNEL LOGIC TRIG. VERT. AMP., 350MHZ	1500.00



# ELECTRONICS BROKERS


7B10, DELAY TIME 2ns/2s/DELTA TIME.....	350.00	INTERSTATE P24, PULSE GENERATOR.....	300.00
7B15, DELAY TIME 2ns/2s.....	400.00	KAV 1/432D, ATTENUATOR.....	75.00
7B53A, 100 MHz DUAL TIME BASE.....	200.00	KAV 30-0, ATTENUATOR.....	125.00
7B80, 400 MHz DELAYED TIME BASE.....	200.00	KEITHLEY 225, CURRENT SOURCE.....	350.00
7B85, 400 MHz DELTA TIME DELAYING TIME BASE.....	250.00	KEITHLEY 230, PROGRAMMABLE VOLTAGE SOURCE.....	875.00
7B92A, 500 MHz DUAL TIME BASE.....	450.00	KEITHLEY 260, NANOVOLT SOURCE.....	300.00
7D01, LOGIC ANALYZER PLUG.....	200.00	KEITHLEY 261, PICOAMPERE SOURCE.....	350.00
7D02/PM111, LOGIC ANALYZER W/6809 POD.....	450.00	KEITHLEY 705/2x7158, LOW CUR SCANNING SYS, GPIB.....	500.00
7D10, DIGITAL EVENT DELAY.....	200.00	KEPCO BOP-72-1.5M, 72V AT 1.5A BP OP AMP/PWR SUP.....	400.00
7D13, 3-1/2 DIGIT DMM.....	125.00	KEPCO BOP-72-5M, 72V AT 5A BP OP AMP/PWR SUP.....	600.00
7D15, 225 MHz UNIVERSAL COUNTER/TIMER.....	300.00	KEPCO JOE, 36-3MVP, 36V AT 3A CVCC METERED SUP.....	300.00
7D20T, PROGRAMMABLE DIGITIZER.....	2500.00	KEPCO JOE, 100-2.5MVP, 1000 AT 2.5A CVCC MTR SUP.....	500.00
7M11, DELAY LINE.....	150.00	KEPCO JOE, 15-6MVP, 15V 6A.....	150.00
7S11, SAMPLING UNIT.....	400.00	KEPCO JOE 55-10M, 55V AT 10A CVCC POWER SUPPLY.....	350.00
7S12/S6/S52/7603, TDR SAMPLING SYSTEM W/S6, S52.....	1950.00	KIKUSUI 5509, O'SCOPE, 15MHz, 4 CH.....	250.00
7T11, SAMPLING SWEEP UNIT.....	900.00	KIKUSUI 5513, O'SCOPE.....	200.00
AM501, OPERATIONAL AMP.....	100.00	KIKUSUI COS6100, 5-CHANNEL 100 MHz O'SCOPE.....	525.00
DC5009/01, PROG 135 MHz UNIV CTR, TCXO.....	750.00	LEADER 480-U71, TV-VIF PLUG IN UNIT.....	300.00
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DC503A, 125 MHz UNIVERSAL COUNTER.....	500.00	LH RESEARCH 137A, PULSE GEN, 125MHz-10Hz.....	300.00
DC504, COUNTER/TIMER, 1Hz-80MHz.....	185.00	MAGNAVOX T-23893, CHART PRINTER.....	200.00
DC505A, 225 MHz UNIVERSAL COUNTER.....	250.00	MARCONI 2304, MOD METER.....	400.00
DC509, 135 MHz UNIVERSAL COUNTER/TIMER.....	700.00	MARCONI 2337A, AUTOMATIC DISTORTION METER.....	400.00
DD501, DIGITAL DELAY.....	350.00	MARCONI TF2300B, AM/FM MOD METER.....	500.00
DM501, DMM MODULE, 4.5 DIGIT DISPLAY.....	275.00	MARCONI TF2370/TK, SPECTRUM ANAL., 0-1250 MHz.....	3000.00
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DM501A, MULTIMETER, 4.5 DIGIT.....	300.00	MEASUREMENTS CORP 80, SIGNAL GENERATOR.....	300.00
DM502, MULTIMETER, 3.5 DIGIT.....	175.00	MICRO TECHNICAL INDU 358 THERMO PROBE.....	400.00
DM502A, MULTIMETER, 3.5 DIGIT.....	225.00	MICROTREL SG800, SWEEP SIGNAL GEN 1GHz-18GHz.....	3000.00
FG501, 1 MHz FUNCTION GENERATOR.....	250.00	MILLIVAC 828A.....	300.00
FG502, 11 MHz FUNCTION GENERATOR.....	250.00	MILLIVAC MV-823B-S1, RF MILLIVOLTMETER, 10 kHz-1.2 GHz, 1mV-10V, W/ADAPTERS.....	375.00
FG503, 3 MHz FUNCTION GENERATOR.....	250.00	PHILLIPS 3226, O'SCOPE.....	300.00
FG504, 40 MHz FUNCTION GENERATOR.....	900.00	PHILLIPS 5512, NTSC TV PATTERN GENERATOR.....	250.00
P6015, 1000X 40kV PROBE, AC/DC.....	300.00	PHILLIPS PM2454B, AC MILLIVOLTMETER.....	200.00
PG501, 50 MHz PULSE GEN.....	300.00	PHILLIPS PM3225, O'SCOPE.....	300.00
PG508, 50 MHz PULSE GEN.....	500.00	PHILLIPS PM6302, RCL BRIDGE.....	250.00
PS501, POWER SUPPLY.....	100.00	PHILLIPS PM6611, UNIVERSAL COUNTER.....	250.00
PS501-1, 0-20V PRECISION POWER SUPPLY.....	150.00	POWER DESIGN 2005A, PREC PWR SRCE, 20V, 500mA.....	200.00
PS5010, PROGRAMMABLE TRIPLE POWER SUPPLY.....	750.00	POWER DESIGN 2K-10, 0-2000V 0-10mA CV PWR SUP.....	200.00
PS503A, DUAL POWER SUPPLY.....	250.00	POWER DESIGN 6050A, UNIV DC SOURCE, TO 60V, 5A.....	200.00
RS103N, RACK MOUNT O'SCOPE.....	200.00	RACAL-DANA 1250, UNIV SWITCH CONTROLLER.....	300.00
SC502, DUAL TRACE O'SCOPE PLUG, 15MHz.....	475.00	RACAL-DANA SERIES 6000, MICROPROCESSING DMM.....	350.00
SC504, 80 MHz O'SCOPE.....	475.00	RACAL-DANA SERIES 9000, TIMER/COUNTER 9 DIGIT.....	250.00
SG502, AUDIO OSCILLATOR.....	300.00	RADIO RESEARCH 41, AM/FM SIGNAL GENERATOR.....	200.00
		RADIOMETER COPENHAGE SMG1 STEREO GEN.....	500.00
		RFL INDUSTRIES 829G, AC/DC CAL STANDARD.....	1700.00
		SHIBASOKU AS9538, MPX TV SOUND SIGNAL GEN.....	600.00
		SLAUGHTER 103-2.5J, 2.5 KVAC HIPOT.....	300.00
		SLAUGHTER 205, MEGOHMMETER 20,000 MEG ELEC.....	200.00
		SYSTRON-DONN 6244A/011, 4.5 GHz PORT CTR, W/30 PPB/MNTH OXCO.....	1500.00
		SYSTRON-DONNER 712-2A/809-A, SPECT ANAL.....	700.00
		SYSTRON-DONNER M107, PREC DCV SRCE, 0-1kV/50mA.....	1500.00
		TAUTRON MB-1A, PCM ERROR RATE MEAS RECEIVER.....	300.00
		TAUTRON MB-302, BERT REC.....	300.00
		TAUTRON ME-1, PSEUDO RANDOM DATA RATE MOD.....	250.00
		TAUTRON ME-302, DATA RATE EXTENDER.....	300.00
		TAUTRON ME-502, DATA GENERATOR.....	400.00
		TAUTRON MN-302, BERT TRANSMITTER.....	500.00
		TAUTRON MS-2, UHF PULSE SOURCE.....	600.00
		TAUTRON MX-302, CRYSTAL CLOCK SOURCE.....	700.00
		TEXSCAN 7271.....	250.00
		TEXSCAN WB713, 0-950MHz SWEEP GENERATOR.....	500.00
		THERMOTRON 012005, TEMP LIMIT CONTROL.....	150.00
		TI XDS.....	500.00
		VALHALLA 4440, DMM, AC/DC, V&C, 2K-20M OHMS.....	75.00
		VALHALLA SCI 2000-1, AUTORANG DIG WATT-AMM.....	750.00
		VU-DATA PS933, w/975, MINI O'SCOPE w/ COUNTER.....	500.00
		VU-DATA PS950, w/975, MINI O'SCOPE w/ COUNTER.....	700.00
		WANTABE SR6312, CHART RECORDER.....	500.00
		WAVETEK 1002, SWEEP SIGNAL GENERATOR.....	500.00
		WAVETEK 116, 1 MHz FUNCTION GENERATOR.....	225.00
		WAVETEK 134, SWEEP GENERATOR.....	300.00
		WAVETEK 1402A, VHF SWEEP GENERATOR FOR USE w/1502, 1-300MHz.....	700.00
		WAVETEK 1701, UHF/VHF SWEEP GENERATOR.....	1500.00
		WAVETEK 180 2 MHz SWEEP/FUNCTION GENERATOR.....	250.00
		WAVETEK 1801A, SWEEP GEN, 1-950 MHz, 75 OHMS.....	500.00
		WAVETEK 182A, 4 MHz FUNCTION GENERATOR.....	275.00
		WAVETEK 184, 5 MHz SWEEP/FUNCTION GENERATOR.....	325.00
		WAVETEK 185, 5 MHz LIN/LOG SWEEP/FUNCT GEN.....	375.00
		WAVETEK 2001A, SWEEP/SIGNAL GEN, 1-1400 MHz.....	650.00
		WAVETEK 3000, SIGNAL GENERATOR, 1-500MHz.....	200.00
		WAVETEK 51, UHF PROGRAMMER FOR USE w/1502.....	250.00
		WESTON ELECTRICAL IN 759 FOOT-LAMB METER.....	150.00

## MISCELLANEOUS

AMBITROL 4005, PWR SUP, 0-40VDC, 0-500MA.....	175.00
ANRITSU ML422B/31, SELECTIVE LEVEL METER.....	1100.00
B&K PRECISION 1850A, FREQ. COUNTER 512MHz.....	175.00
BAFCO 920A, FREQUENCY RESPONSE ANALYZER.....	750.00
BIOMATION KD101-D, LOGIC ANALYZER.....	400.00
BLUE MPR-336E-MPI, ENV. CHAMB w/ CTR SRVOCORDR.....	3000.00
BOONTON 92BD, DIG RF MV METER, 10KHz-1.2GHz.....	700.00
BOONTON 93A, TRMS VOLTMETER, 10 Hz-20 MHz.....	125.00
CLIMET CI-3100, OPTICAL PART. TRANSDUCER.....	250.00
DANA 9000, MICROPROCESSING TIMER/COUNTER.....	300.00
DELTRON SP, CVCC, 10V, 5A, METERED PWR SUP.....	75.00
DELTRON SP, 40V, 5A, CVCC METERED PWR SUP.....	150.00
E.S.I. SP-2534, 4-1/2 DIGIT LCR METER, GPIB.....	1000.00
EIP 451, MICROWAVE PULSE COUNTER.....	2000.00
FLUKE 1722, IEEE 488 CONTROLLER.....	750.00
FLUKE 1910A, 125 MHz COUNTER/TIMER.....	175.00
FLUKE 1920A, FREQUENCY COUNTER, 520MHZ.....	250.00
FLUKE 1952B, COUNTER/TIMER, TCXO, 2 CHAN.....	250.00
FLUKE 1953A/02, UNIV TIMER/COUNTER 2 CHAN.....	350.00
FLUKE 4265A, BIN PROG PRECISION PWR SUP.....	250.00
FLUKE 6011A, FREQ. SYN. 10MHz-11MHz, 1Hz RES.....	2000.00
FLUKE 750A, REFERENCE DIVIDER.....	900.00
FLUKE 8000A, DMM, 3.5 DIGITS, 5 FUNCTIONS.....	175.00
FLUKE 8120A, DMM.....	200.00
FLUKE 845AR, HIGH IMPEDANCE VOLTMETER.....	300.00
FLUKE 8600A, DMM, 4.5 DIGIT, 5 FUNCTION.....	200.00
GENERAL MICROWAVE 460B-10, 3 HEADS.....	350.00
GENERAL MICROWAVE 476, POWER METER.....	150.00
GOULD 816, DUAL PIN PORT RECORDER.....	350.00
GUILDLINE 91540, TRANSVOLT 4890 STAND CELLS.....	750.00
HARRISON LAB 6206A, POWER SUPPLY.....	40.00
HITACHI V-151F, PORT. O'SCOPE.....	600.00
HITACHI V-212F, PORT. O'SCOPE.....	700.00
HONEYWELL 1858/700, OSCILLOGRAPH.....	2000.00
IBM SYSTEM 9000, CONTROLLER.....	3000.00
INTERSTATE F31, 3 MHz FUNCTION GENERATOR.....	300.00
INTERSTATE F72, 20 MHz PULSE FUNCTION GEN.....	450.00
INTERSTATE P23, PULSE GENERATOR.....	200.00


# ACCORD ELECTRONIC SYSTEMS, INC.

## RADIAL ELECTROLYTIC CAPACITORS



1uF	25V	.04
2.2uF	25V	.04
3.3uF	25V	.04
4.7uF	25V	.04
6.8uF	25V	.04
10uF	25V	.05
22uF	25V	.05
33uF	25V	.06
47uF	25V	.06
100uF	25V	.08
220uF	25V	.08
330uF	25V	.09
470uF	25V	.09
1000uF	25V	.22
2200uF	25V	.42
3300uF	25V	.53
4700uF	25V	.91

## RADIAL MONOLYTIC CAPACITORS




.001uF	50V	.05
.0022uF	50V	.05
.0047uF	50V	.05
.01uF	50V	.05
.022uF	50V	.05
.047uF	50V	.05
.1uF	50V	.05
.22uF	50V	.12
.47uF	50V	.17

## CERAMIC DISC CAPACITORS




10pF	50V	.05
22pF	50V	.05
27pF	50V	.05
33pF	50V	.05
47pF	50V	.05
68pF	50V	.05
82pF	50V	.05
100pF	50V	.05
120pF	50V	.05
150pF	50V	.05
180pF	50V	.05
220pF	50V	.05
270pF	50V	.05
330pF	50V	.05
470pF	50V	.05
1000pF	50V	.05
2200pF	50V	.05
3300pF	50V	.05
4700pF	50V	.05
.01uF	50V	.05
.022uF	50V	.05
.047uF	50V	.05
.1uF	50V	.05

## DIPPED TANTALUM CAPACITORS



1uF	25V	.14
2.2uF	25V	.14
10uF	25V	.25
22uF	25V	.52

## DIODES



### 1 AMP RECTIFIER

1N4001	50V	.03
1N4004	400V	.04
1N4007	1KV	.05

### 3 AMP RECTIFIER

1N5401	100V	.06
1N5404	400V	.07
1N5408	1KV	.08

### 6 AMP RECTIFIER

6A10	100V	.19
6A100	1KV	.22

### 1 AMP SCHOTTKY

1N5817		.20
1N5818		.23
1N5819		.25

### 3 AMP SCHOTTKY

1N5820		.40
1N5821		.46
1N5822		.50

## GERMANIUM

1N34A		.10
1N60		.10
1N270		.17

## SWITCHING

1N914		.025
1N4148		.025

### 1 W ZENER DIODE

1N4728	3.3V	.07
1N4729	3.6V	.07
1N4730	3.9V	.07
1N4731	4.3V	.07
1N4732	4.7V	.07
1N4733	5.1V	.07
1N4734	5.6V	.07
1N4735	6.2V	.07
1N4736	6.8V	.07
1N4737	7.5V	.07
1N4738	8.2V	.07
1N4739	9.1V	.07
1N4740	10V	.07
1N4741	11V	.07
1N4742	12V	.07
1N4743	13V	.07
1N4744	15V	.07
1N4745	16V	.07
1N4746	18V	.07
1N4747	20V	.07
1N4748	22V	.07
1N4749	24V	.07
1N4750	27V	.07
1N4751	30V	.07
1N4752	33V	.07
1N4753	36V	.07
1N4754	39V	.07
1N4755	43V	.07
1N4756	47V	.07
1N4757	51V	.07
1N4758	56V	.07
1N4759	62V	.07
1N4760	68V	.07
1N4761	75V	.07
1N4762	82V	.07
1N4763	91V	.07
1N4764	100V	.07

## TRANSISTORS

2N2222A		.22
2N3055		.65
2N3904		.05
2N3906		.05
2N4125		.09
2N4126		.09
2N4401		.05
2N4403		.05
2N5086		.09
2N5087		.08
2N5088		.08
2N5089		.09
2N5209		.09
2N5210		.09
2N5400		.12
2N5550		.12
2N5551		.09
MJE3055T		.65
MPSA-05		.10
MPSA-10		.12
MPSA-13		.15
MPSA-14		.15
MPSA-42		.14
MPSA-44		.22
MPSA-56		.10
MPSA-63		.45
MPSA-92		.10
MPSA-93		.15
MPSH-10		.10
PN2222A		.05
PN2907A		.05
TIP31		.42
TIP41		.48
TIP122		.52
TIP125		.55

## VOLTAGE REGULATORS

7805		.48
7812		.48
7905		.48
7912		.48
78L05		.35
78L12		.35
79L05		.35
LM317T		.68
LM350T		2.05

## INTEGRATED CIRCUITS

CD4001		.29
CD4011		.29
CD4013		.37
CD4017		.37
CD4028		.37
CD4049		.29
CD4051		.63
CD4066		.35
CD4069		.29
LM311		.43
LM324		.47
LM339		.47
LM358		.47
LM386		.67
LM393		.37
LM555		.43
LM556		.47
LM741		.37
MC1458		.43
LM1488		.47
LM1489		.47
TIL111		.35

## IC SOCKETS


	LOW PROFILE	MACHINE SCREW	WIRE WRAP
8 PIN	.04	.16	.32
14 PIN	.08	.28	.56
16 PIN	.10	.32	.64
18 PIN	.11	.36	.72
20 PIN	.12	.40	.80
24 PIN	.15	.48	.96
28 PIN	.17	.56	1.12
32 PIN	.20	.64	1.28
40 PIN	.24	.80	1.60

## DIP SWITCHES




4 POS.	.68
6 POS.	.77
8 POS.	.80
10 POS.	.95

## TOGGLE SWITCHES




SPDT	.62
SPDT center off	.73
DPDT	.69
DPDT center off	.86

## PUSH BUTTON SWITCHES




fits in a 1/4" hole	
Normally open	.29
Normally closed	.30

## BRIDGE RECTIFIER



IN LINE BODY	
RS101 1A-50V	.60
RS106 1A-800V	.93
3N256 2A-400V	.95
TL400 4A-50V	.65
TU600 6A-50V	1.02
TU800 8A-50V	1.33

## 8 PIN DIP BODY



DF005M 1A-50V	.25
DF10M 1A-1KV	.52

## ROUND BODY



W04M 1A-400V	.35
2W10M 2A-1KV	.50

## SQUARE WIRELEADS

TB305 3A-50V	.53
TB805 8A-50V	.93

## SQUARE TAB LEADS

TB151 15A-100V	2.30
TB352 35A-200V	2.68

## CRYSTALS

1.8432 MHZ	.89
2.0000 MHZ	.74
3.5795 MHZ	.74
3.6864 MHZ	.74
4.0000 MHZ	.74
4.9152 MHZ	.74
5.0688 MHZ	.74
7.3728 MHZ	.74
10.000 MHZ	.74
11.000 MHZ	.74
11.059 MHZ	.74
12.000 MHZ	.74
14.3181 MHZ	.74

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1.44M 3.5" WHITE FACE	
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10uF	25V	.10
22uF	25V	.14
47uF	25V	.16
100uF	25V	.19
220uF	25V	.27
470uF	25V	.35
1000uF	25V	.45
2200uF	25V	.89

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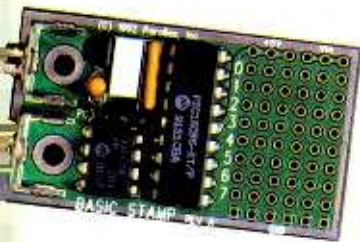
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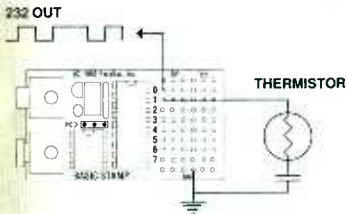
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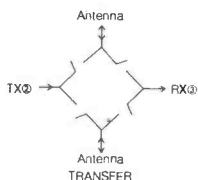
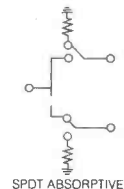
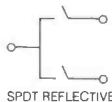
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