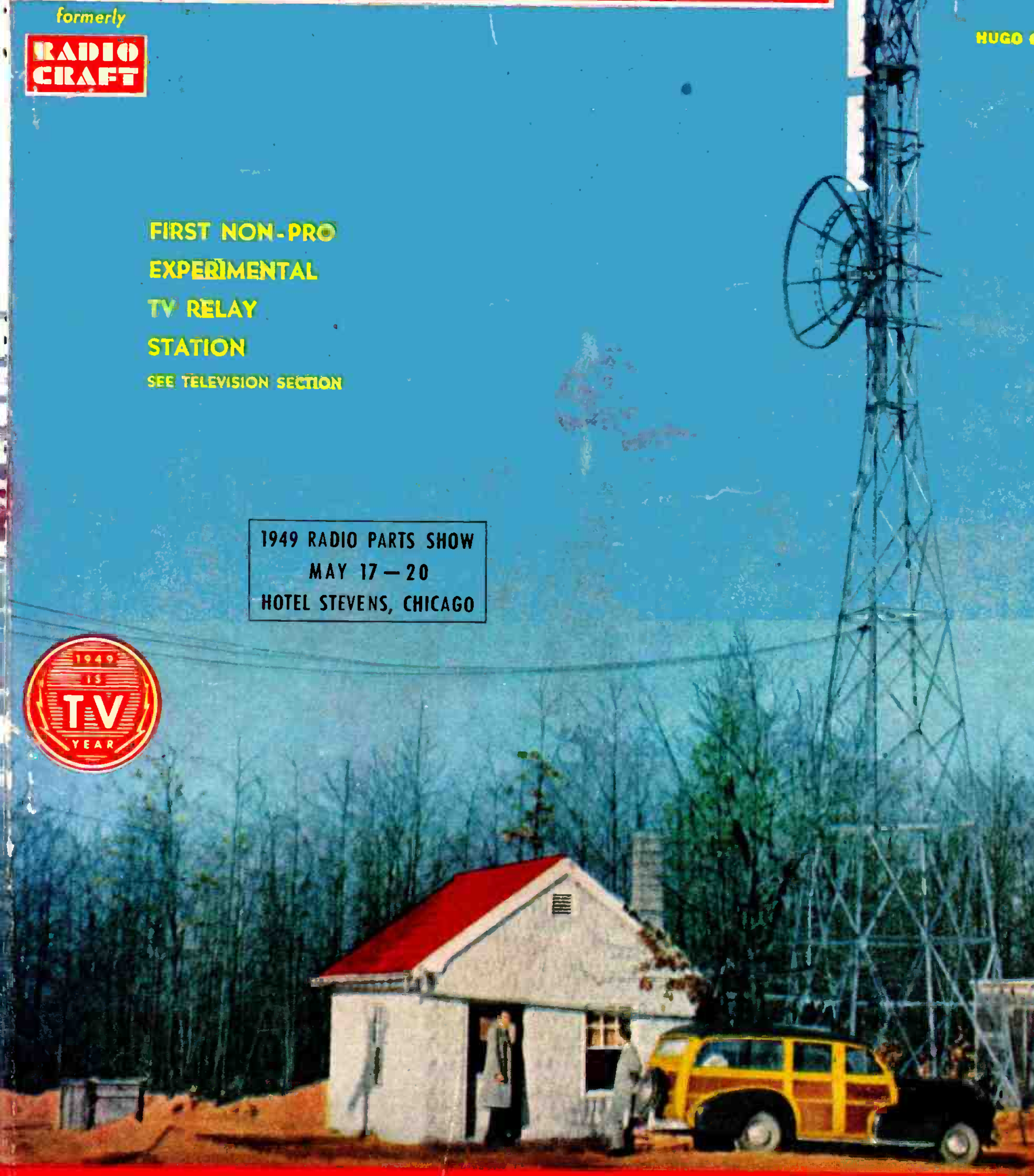
RADIO — ELECTRONICS

formerly RADIO CRAFT

IN THIS ISSUE
Eight-Tube Televiser
Survey of Multitesters

HUGO GERNSBACK, Editor



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Now the identity of "Madame X," the *unknown* in a long search for tone perfection, has been revealed. From this quest emerges a completely integrated record-playing *system* — records and automatic player — the first to be entirely free of distortion to the trained musical ear . . .

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ON THE COVER: Experimental Television Relay Station W3XBR: Dick Hughes and R. Barrett in front of the shack. Kodachrome by Avery Slack. See article on page 27.

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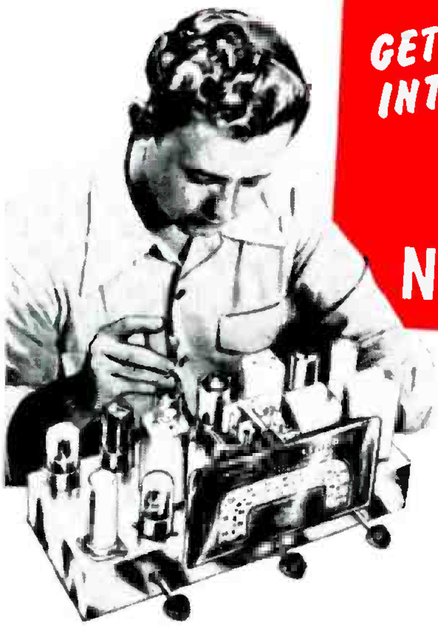

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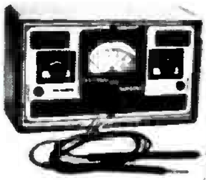

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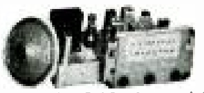

2-BAND $16.95

Kit Model 6-AC. A complete kit of parts, tubes and ready punched chassis (no cabinet) to build a fine 6-Tube AC transformer type radio. We furnish every piece as well as printed diagram and photo. Chassis size 14x 7½x7. 6-inch lighted slide rule dial. Receives broadcast and foreign short wave, (6 to 18 MC) 3 gang tuning condenser, pre-selection on both bands. 6V6 Output. This kit goes together like a manufactured radio. Made from parts intended for use by Detrola. Priced complete with tubes. Include postage for 16 lbs. Model 6-AC. Net $16.95.

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THEATRE QUALITY AMPLIFIER KIT $75.00 Value ONLY $24.95

Complete 15 watt true-fidelity audio amplifier kit. Response essentially flat from 20 to 17,000 cycles. Inputs for crystal mike and any phono pick up, crystal, magnetic or General electric variable reluctance. 3 tone controls and fader control. Merit high fidelity wax impregnated output, matches 4, 8, 16, 250 and 500 ohm line. Complete with 7 miniature tubes. (PP 6AQ5 in output.) Diagram, photo and assembly instructions. Ready punched chassis. Kit model ME 15R net $24.95. Lab. wired and tested $34.95. Speakers recommended, Altec 15-inch model 603B. Net $63.00.

Kit Model ME-34R, same as ME-15R, except has push-pull 6L6 Ouput tube. Giving 34 Watts of Audio. Weight 20 lbs. Net $34.95.

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PRK-24. Radio amp kit with 12 inch PM speaker. Weight 26 lbs.— $29.95.

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Model LP-CC8—Same as above only Dual speed with 2 pickups. $19.95.

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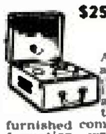
New, children's electronic player. Offered in kit form. Includes all material necessary. Attractive red plywood (not pictured) cabinet, self-starting phono motor and crystal pickup. 4x6" PM speaker and parts to build 70L7 amplifier. Diagram included. Stock No. LJ-1. Net Price $7.95.

4-TUBE T.R.F. KIT

BARGAIN SPECIAL $6.95

4 tube AC-DC. TRF radio kit. Ideal for students and beginners. Every part furnished to build this kit, including tubes, diagram and photos. Has Alnico V PM speaker and tubes. 12SK7, 12SJ7, 50B5 and 35W4. Plastic cabinet with airplane dial. Receives broadcast 550 to 1600 KC. This is the easiest type of radio to build. Kit Model TF-4. Weight 6 lbs. Net $6.95.

100 assorted ½ and 1 watt resistors all late production insulated type; assorted from low sizes to 10 meg. 100 for $1.49. Beldon 100 watt soldering iron—a $3.95 value for $1.95.



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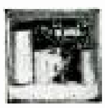

1½ Volt—90 Volt Vibrator Power Supply. Makes 1½ Volt portable radios work on 6 volt storage battery. Has 4 prong pack plug. Worth $10.00. Sale price $2.95. Stock No. X-VT. Weight 6 lbs.

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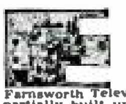

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If you want to play with Television here is a chance to get started.

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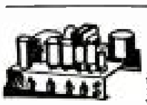
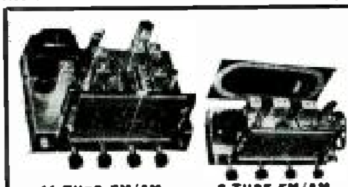
A complete Kit of parts to build a 5 Watt Audio Amplifier, for 110 Volt AC-DC operation. Inputs for mike and any phono pickup crystal or variable reluctance. Output transformer matches 4 to 6 Ohm voice coil. Has tone and fader controls. This is a complete Kit with ready punched chassis and easy to follow diagram. Everything furnished including tubes. 2—12AX7, 2—50B5, plus Selenium Rectifier. Offered at the usual price of a single output type Amp. Kit Model TM-4, weight 6 lbs. Net $6.95. Crystal Mike and desk stand $4.95 extra. 12 Inch PM Speaker $4.95 extra.



20-WATT AMP KIT $15.95 PUSH-PULL 6L6

A complete Kit of parts to build a high quality 20 Watt Audio Amplifier with full 135 Mill Power Transformer for 110 Volt AC operation. Inputs for mike and either crystal or variable reluctance pick ups. Tone and fader controls. Has heavy duty Universal Output Transformer to match any speaker. 4—8—16—250 and 500 Ohms. Ready punched chassis. Easy to follow diagram. Furnished with Tubes. 2—6L6, 2—7N7, 7Z4. Kit Model TM-20, weight 20 lbs. Net $16.95. Crystal Mike & Desk Stand $4.95 extra. Speaker recommended Model CR-13X $12.95 Extra.



11-TUBE FM/AM MODEL S-56..$59.50

8-TUBE FM/AM MODEL S-59..$39.95

HALLICRAFTERS

11-TUBE FM-AM CUSTOM REC. CHASSIS

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BANDSWITCHING TUNING TURRET made by Western Electric. Covers 4 bands above 100 MC. All coils wound with #14 silver-plated wire. Complete with tuning condensers and powerful electric driving motor. Diagram included. ONE OF OUR MOST TERRIFIC VALUES—ONLY $2.95.

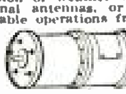
AUDIO AMPLIFIER—Brand new. Push-Pull stage triode amplifiers having 2 of the valuable and scarce ouncer type audio transformers that sell for over $10.00 each. Neat aluminum case, fully enclosed (largest dimension 6 inches). Perfect for intercom system, phono amplifier, mike amplifier or signal tracer amplifier for testing radio sets. A sensational bargain at only....$3.40 each

DUAL METER—One 50 uA and one 200uA movement in the same case. This meter is ideally suited for use as a combination modulation percentage and carrier shift indicator. If desired the movements may be removed from the case and used separately for voltmeters, ohmmeters, meters, etc. All meters are in perfect operating condition, but a few have cracked glasses. This super value costs only $1.95

$9.95 TAKES ALL THREE BIG BARGAINS "B"

HOME WORKSHOP AT BARGAIN PRICE. Accurate and precise 2 speed guaranteed hobby lathe, the essential machine for the home workshop. Sturdy enough for light production work or factory standby service. Supplied with 56" of belting for connecting to any available electric motor or power take-off. Also included in this unbelievable offer are such accessories as a ½" drill chuck with specially hardened tool steel jaws, a 4" electric furnace high speed grinding wheel, a cotton buffing wheel with a large supply of buffing compound, and a 4" steel wire scratch brush. Your cost $6.00. Sole export agent. Distributor inquiries invited.

SENSATIONAL, FASCINATING, MYSTERIOUS SELSYNS. Brand new Selsyns made by G. E. Company. Two or more connected together work perfectly on 110 V A.C. Any rotation of the shaft of one Selsyn and all others connected to it will rotate exactly as many degrees in the same direction, following unerringly as if the units were connected together by shafting instead of wire. This is true whether you twist the shaft of the master unit a fraction of a revolution or many revolutions. Useful for indicating direction of weather vanes, rotating directional antennas, or controlling innumerable operations from a distance. Complete with diagram and instructions. Per Matched Pair $4.95.



STROMBERG CARLSON

Power Switching Relay Box. Neat 3½x4x5½" Steel case with tight fitting cover finished in Stromberg's usual beautiful chocolate color crackle finish.........$1.00

SELENIUM RECTIFIERS

(May be used at any voltage lower than rating)

•1.2 ampere.......30 volt.......$ .90
(above can be paralleled for battery charging)

25 MA	50 Volt	$ .45
75 MA	120 Volt	.70
100 MA	120 Volt	.75
150 MA	120 Volt	.80
200 MA	120 Volt	1.05
250 MA	120 Volt	1.25

METER RECTIFIER—Full wave, may be used for replacement, or in construction of all types of test equipment—$1.25. Half Wave—90c.

CERAMIC INSULATED VARIABLE AIR CONDENSERS

350 mmfd, 5 gang—$1.95; 4 gang—$1.49; 3 gang—$1.29

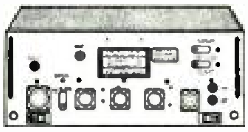
10 mmf	$.35—10 for $2.90	100 for $23.00
15 mmf	$.35—10 for $2.90	100 for $23.00
25 mmf	$.35—10 for $2.90	100 for $23.00
35 mmf	$.40—10 for $3.40	100 for $28.00
50 mmf	$.45—10 for $3.70	100 for $30.00
75 mmf	$.50—10 for $4.40	100 for $38.00
100 mmf	$.55—10 for $4.50	100 for $39.00
140 mmf	$.80—10 for $7.40	100 for $64.00
160 mmf	$1.00—10 for $8.50	100 for $70.00
2 Gang 140 mmf	$1.60—10 for $12.50	100 for $100.00

Butterfly condensers, rotor has double ball bearings and a ¼" shaft.

15 mmf. per section	$.50—10 for $4.50	100 for $40.00
30 mmf. per section	$.60—10 for $5.50	100 for $50.00
50 mmf. per section	$.70—10 for $6.50	100 for $60.00

Manufacturers and distributors write for prices on larger quantities. WE HAVE OVER 250,000 VARIABLE CONDENSERS IN STOCK.

BRAND NEW APN1 14-TUBE ELECTRONIC ALTIMETER



This famous 18x9x7 CAA approved unit, which weighs only 25 lbs. without plugs or cables, light enough for the smallest plane, cost the gov't $2000. and includes a transmitter, a receiver, all tubes, altitude indicator, altitude limit switch, and two easily installed 11" antennas. Working on the radar principle the receiver measures the absolute altitude from 3 to 4000 feet with precision enough for blind landings. In addition the altitude limit switch gives an alarm if the plane's height varies more than 10 feet from any readjusted value. This unit might also be used to warn boats of any obstacle that is on their course. 12V. $75.00. 28 volt model $45.00.

AT LAST YOU CAN AFFORD A LABORATORY STANDARD MICRO-VOLTER

78E Standard Signal Generator. 50 to 70 Mc. unmodulated or with 400 cycle modulation.

The famous Measurements Corp. Model 78E. 5 Tube Laboratory Standard Signal Generator (that sold new, FOB, Boonton, N. J., for $310.00 net), is available in perfect condition for 25 to 60 cycles, 115V AC operation. Until now this is the sort of top-flight lab equipment that discriminating buyers have only vainly hoped would be released at a bargain price. Worth every cent the manufacturer asks, but available FOB Buffalo while our limited supply lasts for only $79.95.

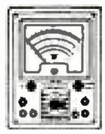
Such companies as Admiral Corp. and John Meck, Inc., have ordered from us and repeated many times on these 78 generators for use in their labs and production line testing.

Uses 1-9002, 1-7Y4, 1-VR 150-30, 1-7C7, and 1-7C5 tubes. Output continuously variable from 0 to 100,000 Microvolts.

VACUUM TUBE VOLT-OHM-CAPACITY METER

There are more features engineered into this all purpose instrument than in any other instrument on the market regardless of price. It was designed not only to meet present conditions but to be readily adaptable to future needs. At the sensationally low price of this precision instrument no school, plant, lab or service shop need deprive itself of the "new look" in measuring equipment. Here are a few of the many features of this outstanding meter:

- 5 inch easy to read meter.
- 6 DC voltage ranges from 0 to 1000 V (input resistance as high as 1 megohm per volt.)
- 5 AC voltage ranges from 0 to 1000 V (No dry disc rectifier to age and destroy the accuracy of this VACUUM TUBE VOLTMETER).
- 6 Resistance ranges from 2/10 ohm to 1000 megohms.
- 4 Capacity ranges from .000025 to 20 MFD.
- A zero center range for balancing FM discriminators.
- Isolating resistor built into probe.
- Sturdy natural finish hard wood case.



This outstanding development of one of the leading manufacturers of test equipment costs only $39.50 complete with all leads, as illustrated.

$7.05 TAKES BARGAIN "C"

(All three items below)

ALUMINUM GEAR BOX 18x8x7 that contains two powerful electric motors and two matched gear trains, 62 gears in all varying in size from ½ to 4 inches in diameter. This unit is readily converted to rotate in beam antenna or any other similar use..........$5.00

SIGNAL CORP INTER-CONNECTOR RELAY BOX 730A

This valuable unit, made by Bell, and more familiarly known by the U. S. Army designation BC616, is encased in a highly polished aluminum case 6¼x5¼x2½, and contains 150 mfd. of condenser capacity, sensitive relays, resistors, and terminal strips. Order several at the giveaway price of only..$1.95

REMOTE CONTROL UNIT—Aluminum case 4 x 3 x 2 containing 2 potentiometers, triple pole switch, 4 knobs, phone jack, gear mechanism and revolution counter. Including 8 prong JAN connector to fit box—$1.39.

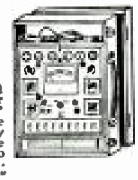
TOGGLE SWITCHES

Order Number		
SW-11	Single Pole, Single Throw	35c
SW-12	Single Pole, Double Throw	45c
SW-13	Double Pole, Single Throw	57c
SW-14	Double Pole, Double Throw	69c

COMPRESSED AIR INSTANTLY, ANYWHERE!!

Portable Air Compressor and storage tank. Ruggedly built of best materials using lifetime lubricated ball-bearing on connecting rod and oil impregnated main bearing on shaft. Unusual design forever eliminates valve trouble, the most common fault in air compressors. **PATENTED** unique air intake system increases efficiency tremendously over other compressors so that air output is much greater than that from larger compressors powered by heavier motors. Will deliver appr. 3500 cu. in air per min. at maintained pressure of 30 lbs., or will inflate a 90 lb. truck tire in less than 1 min. Complete with 100 lb. gauge, fingertip adjustment allows setting of output pressure at any value, which will automatically be maintained. Works from any ¼ HP. motor. Useful for spraying paints or lacquers, disinfectants, insecticides, annealing or brazing with natural gas, inflating tires, etc. Price $14.50 postage prepaid anywhere in U.S. Efficient adjustable syphon type spray gun complete with 12 ft. of 100 lb. tested hose for only $7.75 with pint container, also prepaid.

1949 MODEL MUTUAL CONDUCTANCE TUBE TESTER $52.95



No possibility of good tubes reading "Bad" or bad tubes reading "Good" as on dynamic conductance testers or other ordinary emission testers. Attractive panel and case equal to any on the market in appearance . . . Large 4½" meter . . . Calibrated micromho scale as well as a Bad-Good scale . . . Front panel fuse . . . Individual sockets for all tube base types—voltages from .75 volts to 117 volts and complete switching flexibility allow all present and future tubes to be tested regardless of location of elements on tube base . . . Indicates gas content and detects shorts or opens on each individual section of all loctal, octal and miniature tubes including cold cathode, magic eye and voltage regulator tubes as well as all ballast resistors. Name of the nationally known manufacturer withheld because of special price offer.

Model "C"—Sloping front counter case $52.95
Model "P"—Handsome hand-rubbed portable case.................. 57.95
Built-in roll chart with either of above $5.00 extra.

SENSATIONAL VALUE IN AC-DC POCKET TESTER

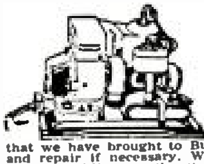
This analyzer, featuring a sensitive repulsion type meter housed in a bakelite case, represents the culmination of 15 years achievement in the instrument field by a large company specializing in electronic test equipment.

Specifications of the AC-DC Model Volt-Ohmmilliammeter:
AC Volts—0-25, 50, 125, 250
DC Volts—0-25, 50, 125, 250
Milliamperes AC—0 to 50
DC Milliamperes—0 to 50
Ohms Full Scale—100,000
Ohms Center Scale—2400
Capacity—.05 to 15 Mfd.

Total Price, prepaid anywhere in the USA—$7.00. Similar DC Meter, lacking the AC operated ranges of above, $5.50 prepaid.

OUR PE-109 DIRECT CURRENT POWER PLANT

This power plant consists of a gasoline engine that is coupled to a 2000 watt 32 volt DC generator. This unit is ideal for use in locations that are not serviced by commercial power or to run any of the surplus items that require 24-32v-DC for operation. The price of this power plant tested and in good condition is only $79.95 F.O.B. Buffalo, or we can supply in strictly "as is" condition for $58.95 F.O.B. New York City. These latter are exactly as received, in heavy steel-strapped gov't cases, and we are unable to determine if the individual units are new, or what the condition is if used, while the $79.95 are some of the same that we have brought to Buffalo for testing and repair if necessary. We do not recommend gambling on the "as is" condition, except for quantity purchasers. We can also supply a converter that will supply 110v AC from the above unit or from any 32v DC source for $12.95.



SAVE HOURS OF HARD WORK

. . . do the job in minutes with a BUFRAD Socket Hole Punch.

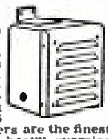
Cut clean accurate holes for sockets, plugs, connectors, etc. Cutting holes in radio chassis is simple as cutting butter with a hot knife with a BUFRAD punch. Just insert the punch in a ¼" hole and turn with an ordinary wrench. In a minute or less you can complete a job which often takes an hour with the old "drilling, reaming and filing" method. With BUFRAD punches you can make 13 different sizes of openings from ½" to 2¼" diameter.

½", ⅝", ¾", ⅞" Size................$2.08
1", 1 1/16", 1⅛", 1 5/32", 1 3/16" 1¼"........................ 2.42
1⅜", 1½"........................ 3.10
2¼"........................ 5.95

RHEOSTATS

200 ohm, 25 watt Clarostat heavy duty rheostat. The perfect size for tube testers, also useful in series with 110 volt line for controlling such units as electro-plating or model train power supplies, battery chargers, and for varying the speed of motors. Innumerable other uses. Regular price $5.20. Your cost 90c.

"P.M. SPEAKERS"



Latest type PM Speaker in a fully-enclosed finished metal cabinet. This speaker and case match communication receivers, and in addition make perfect intercom remote stations. Our price $4.50. Including output transformer $4.95

SPEAKERS—These PM speakers are the finest that are available. All have heavy oversize Alnico V magnets.

3½"	$1.15	6 for $6.60
4"	$1.15	6 for $6.60
5"	$1.10	10 for $9.50
6"	$1.50	6 for $8.70
6"x4" Oval	$2.10	6 for $10.80
7" (Car Radio Size)	$4.50	6 for $21.50
8" .....10 oz.	$3.95	6 for $20.50
8" .....21 oz.	$4.95	6 for $26.50
10" .....21 oz.	$5.50	6 for $30.00
12" .....21 oz.	$7.95	6 for $42.00

AUTO-TRANSFORMER—Steps up 110v, or steps down 220v to 110v—$1.95.

FIL. TRANSF.: 6.3v, 3 Amps.—$1.35; Universal Output Trans. 8 Watt—89c; 18 Watt—$1.29; 30 Watt—$1.69. **AUDIO TRANSFORMER:** S. Plate to S. Grid. 3:1—79c; S. Plate to P.P. Grids—79c; Heavy Duty Class AB or B, P.P. inputs—$1.49; Midget Output for AC-DC sets—59c; **MIKE TRANSFORMER** for T-17 Shure microphone, similar to UTC ouncer type—$2.00. Stancor SB or DB mike to line or grid—$1.95.

POWER TRANSFORMERS—Half-shell type. 110V, 60 cy. Centertapped HV winding. Specify either 2.5 or 6.3V filament when ordering.

For 4-5 tube sets—650V, 40MA, 5V & 2.5 or 6.3V........ $1.49
For 5-6 tube sets—650V, 45MA, 5V & 2.5 or 6.3V........ 1.75
For 6-7 tube sets—675V, 50MA, 5V & 2.5 or 6.3V........ 1.90
For 7-8 tube sets—700V, 70MA, 5V & 6.3 or two 2.5V........ 2.35
For 7-8 tube sets—700V, 70MA, 5V & 6.3 (25 Cycles)........ 3.60
For 8-9 tube sets—700V, 90MA, 5V-3A, 2.5V-3.5A, 2.5-10.5A........ 2.85
For 9-11 tube sets—700V, 5V & 6.3V-4A........ 2.85
For 9-15 tube sets—600V, 150MA, 5V & 6.3V........ 2.85

BUFRAD CAR-RADIO ANTENNA

BR1 BR2 BR3 BR4 BR5

All of our car radio antennas are made of triple plated Admiralty Brass Tubing, complete with low loss shielded antenna leads and high quality fittings.

SIDE COWL—BR-1, 3 sections extend to 66". Your price—single units—$1.60; in lots of 12—$1.35 ea.

SKYSCRAPER—BR-2 has 4 heavy duty sections that extend 98". This super-aerial must be seen to be fully appreciated. Your price—single units—$2.50; in lots of 12—$2.25 ea.

TILT ANGLE—BR-3, may be adjusted to all body contours, 3 sections extend to 66". Single unit price—$1.75; 12 lot price—$1.50 ea.

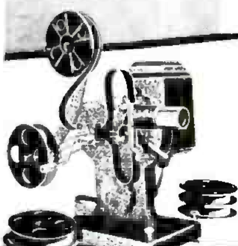
VERSATILE—BR-4, single hole fender or top cowl mounting may be adjusted to conform with all body contours, 4 sections extend to 56". Single unit price—$3.00; 12 lot price—$2.75 ea.

THE MONARCH—BR-5, single hole top cowl mounting, 3 sections extend to 56". Single unit price—$2.00; 12 lot price—$1.75 ea.

AFTER SEEING OUR ANTENNAS AND COMPARING, YOU WILL NEVER BUY ANY OTHER MAKE!

RADIOMEN'S HEADQUARTERS — WORLD WIDE MAIL ORDER SERVICE ! !

OSCILLO-SCOPE
MULTI-METER
R-F SIGNAL GENERATOR
6-TUBE RECEIVER



JOHN H. POTTS, engineer, editor, author, and publisher, died March 16, at the age of 56. A heart ailment was the cause of death.

Mr. Potts was a graduate of the University of Chicago, in which city he was born. He came to New York in 1918 and worked as engineer with RCA, General Electric, Westinghouse, and Sperry before entering the publishing field.

He was best known to engineers as editor and publisher of *Audio Engineering* and editor of its predecessor, *Radio.* To amateurs he was equally well known as the founder and publisher of the amateur magazine *CQ.*

DANGEROUS SURPLUS equipment is reported from Michigan, where the State Police have broadcast a warning that more than 1,000 war-surplus radio sets have been sold with detonators attached to them.

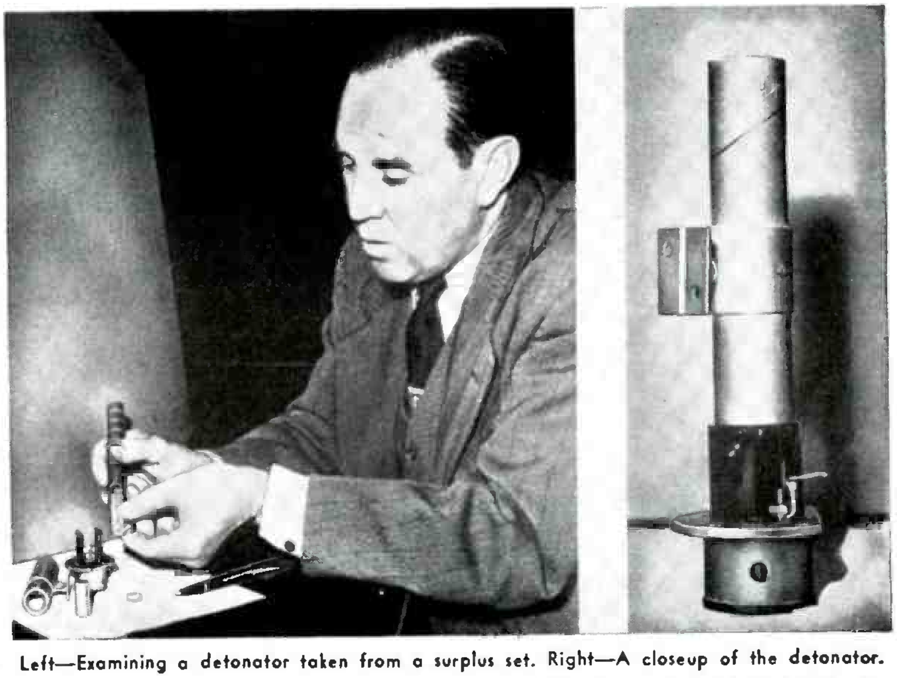
According to State Police Commissioner Donald S. Leonard, the sets are IFF models BC-647-A and BC-966-A. Some of them have tubes six inches long and three-quarters of an inch in diameter, containing a detonator cap and a quantity of TNT, the purpose of which was to destroy the set should the enemy attempt to open captured equipment to seek information about its construction.

How the sets got into the surplus market with their detonators in place is not known. There have been sporadic reports of single sets discovered with detonators intact, and Australian amateurs were warned a few months ago that a quantity of IFF transmitter-receivers already in their hands were dangerous and would blow up if any attempt were made to open them. The explosive charge is small, but quite sufficent to injure any would-be investigator very seriously.

TELEVISION ANTENNAS can be removed from apartment house roofs if they were not authorized by the landlord, an all-tenant jury ruled in New York last month.

Mrs. Estelle Sherer refused to pay her rent for two months because the landlord took down her TV antenna. The landlord tried to evict and Mrs. Sherer counter-sued for three times the value of her receiver, saying that the removal of the antenna was a "partial eviction." The superintendent had given his permission for the installation, she testified, but last December an official of the owner corporation removed it from the roof.

In charging the jury, the judge stated that the superintendent could not permit an antenna installation because he was not an officer of the corporation. Furthermore, he said, referring to Mrs. Sherer's claim of partial eviction, the roof was not a part of her rented premises, and therefore she could not be "evicted" from it.



Left—Examining a detonator taken from a surplus set. Right—A closeup of the detonator.

EDWIN H. COLPITTS, 77, retired vice-president of Bell Telephone Laboratories and inventor of the Colpitts oscillator circuit, died on March 6. Dr. Colpitts held 24 patents and was noted for his work with magnetic coils, his efforts in adapting electron tubes for long-distance telephone circuits, and his studies of capacity unbalance between adjacent telephone-line pairs.

Dr. Colpitts' telephone work began in 1899 when he joined the American Bell Telephone Company. He worked with the Armed Forces in both World Wars.

A. ATWATER KENT, at one time world's largest manufacturer of radio receivers, died in California March 4, at the age of 75. Atwater Kent's original radios were perhaps the only broadcast receivers ever to use "breadboard" mounting. Beautifully finished components were mounted above the board, and the wiring was carried in grooves on its underside. Turning to more conventional sets, he stepped his production up to a peak of 6,000 receivers a day, selling $60,000,000 worth of sets in 1929.

DR. HARVEY RENTSCHLER, retired director of the Westinghouse experimental laboratory at Bloomfield, N. J., died March 23 at his home in East Orange, N. J.

Dr. Rentschler had carried on experimental work with lamps and electronic tubes since 1917, when he joined the Westinghouse staff. Before that he had been a professor of physics at the University of Missouri for nine years.

He was the author of numerous contributions to scientific publications, chiefly on electronic tubes and electric lamps, and was the holder of more than 100 patents, most of them in those two fields.

Possibly Dr. Rentschler's best-known invention is the Sterilamp, the ultraviolet light that destroys bacteria in the air. Less well known, but even more spectacular, was his feat of refining the first uranium used in the development of the atomic bomb.

OBSOLESCENCE OF TV SETS will not be a problem, said Wayne Coy, chairman of the Federal Communications Commission last month. The statement was believed to be a reply to the many rumors that present television receivers would be useless in the near future if u.h.f. channels are adopted.

"The Commission would not be taking the time to revise the standards for the presently available service," said Mr. Coy, "if it had in mind eliminating in the near future the use of these channels for television service.

"I think this question of obsolescence of television receivers is something of a tempest in a teapot. I do not think that anyone buying a television set today has had a fraud perpetrated on them. I can assure them that wherever a television signal is available from a v.h.f. transmitter, their sets will render them fine service for many years and can be converted to render fine service for them if ultra-high frequencies are utilized. . ."

TELEVISION ANTIQUES are already in existence, it appears. Last month's National Antiques Show at Madison Square Garden in New York featured American items of every description—pre-revolutionary pottery, Pennsylvania Dutch cupboards, 19th century ball gowns, to mention a few items.

Right in the middle of the show, occupying its own small spot, was a 1938 RCA television receiver, one of the first commercial models made. Without radio or phonograph and able to tune only five channels, the 1938 set sold 11 years ago for $850, almost twice what a modern combination instrument would cost on today's market.

WINDOW TV ANTENNAS may become more widespread in New York City as the result of a ruling in Bronx Supreme Court last month. Joseph Einson, a tenant in an apartment house, was in court with landlord D. Greenstein, Inc., to determine whether Mr. Einson's window antenna—objected to by the landlord—should remain. Justice Eugene L. Brisach ruled that it might remain, provided the tenant obtained liability insurance ranging from $10,000 to $20,000 to protect the landlord in case of any accident attributable to the antenna.

WWVH is the call of the new Bureau of Standards station recently established on the Hawaiian island of Maui. Time and frequency standards are being broadcast experimentally on 5, 10, and 15 mc. As with WWV, the Bureau's main station in Beltsville, Md., WWVH is modulated with a standard 440-cycle A, as well as audio pulses at accurate 1-second intervals. The audio tone starts at the hour and continues for 4 minutes, followed by 1 minute of silence; this sequence is repeated throughout the hour. Greenwich Mean Time is given in code every 5 minutes. All transmissions are interrupted for about 4 minutes on the hour and half-hour and for about 30 minutes at 0700 and 1900 GMT.

Heathkit TEST


Heathkit engineer measuring frequency response and distortion of Heathkit Oscilloscope using Hewlett Packard Audio Generator and Distortion Analyzer.

1949 MODEL Heathkit VACUUM TUBE VOLTMETER KIT

Features

New 200 ua Meter.
24 Ranges.
New Accessory H.V. Probe makes Heathkit a kilovoltmeter. (Extra)
New Accessory RF Probe extends range to 100 megacycles. (Extra)

A new Model V-2 Heathkit VTVM with new 200 microampere meter, four additional ranges — full scale linear ranges on both AC and DC of 0-3 V., 10 V., 30 V., 100 V., 300 V. and 1,000 V. Accessory probe listed elsewhere in ad extends voltage range to 3,000 and 10,000 volts D.C. New model has greater sensitivity, stability and accuracy — still the highest quality features — shatterproof plastic full view meter face — automatic meter protection, push pull electronic voltmeter circuit, linear scales — db. scale — ohmmeter measures 1/10 ohm to 1 billion ohms with internal battery — isolated DC test prod for dynamic measurements — 11 megohm input resistance on DC — AC uses electronic rectification with 6H6 tube. All these features and still the amazing price of only $24.50. Comes complete with cabinet — panel — three tubes — new Mallory switches — test prods and leads, 1% ceramic divider resistors and all other parts. Complete instruction manual for assembly and use. Better start your laboratory with this precision instrument. Ship. Wt., 8 lbs.

$24.50

Heathkit 5" OSCILLOSCOPE KIT

Features

- Instant switching to plates or amplifier from front panel.
- Sweep generator supplying variable sweep 15 cycles to 30,000 cycles.
- All controls on front panel.
- Cased electrostaticly shielded 110 V. 60 cycle power transformer.
- AC test voltage on front panel.
- External synchronizotion post on front panel.
- Deflection sensitivity .65 V. per inch full gain.
- Frequency response ± 20% from 50 cycles to 50 Kc.
- Input impedance 1 Megohm and 50 MMF.

The Heathkit 5" Oscilloscope fulfills every servicing need. The husky cased power transformer supplies 1100 Volts negative and 350 Volts positive. Tubes supplied are two 6SJ7 amplifiers, 884 sweep generator, two 5Y3 rectifiers, and 5BP1 CR tube. Grey crackle aluminum cabinet and beautiful grey and maroon panel. Chassis especially designed for easy assembly.

An oscilloscope provides endless sources of experimentation in radio, electronics, medicine and scientific research.

Detailed instructions make assembly fun and instructive. Shipping Wt., 24 lbs. Express only.

$39.50 Nothing ELSE TO BUY

New Heathkit SIGNAL TRACER AND UNIVERSAL TEST SPEAKER KIT

$19.50 Nothing ELSE TO BUY

The popular Heathkit signal tracer has now been combined with a universal test speaker at no increase in price. The same high quality tracer follows signal from antenna to speaker — locates intermittents — defective parts quicker — saves valuable service time — gives greater income per service hour. Works equally well on broadcast — FM or TV receivers. The test speaker has assortment of switching ranges to match push pull or single output impedance. Also tests microphones, pickups — PA systems — comes complete — cabinet — 110 V. 60 cycle power transformer — tubes, test probe, all parts and detailed instructions for assembly and use. Shipping Wt., 8 lbs.

Heathkit RF SIGNAL GENERATOR KIT

$19.50 Nothing ELSE TO BUY

Every shop needs a good signal generator. The Heathkit fulfills every servicing need, fundamentals from 150 Kc. to 30 megacycles with strong harmonics over 100 megacycles covering the new television and FM bands. 110 V. 60 cycle transformer operated power supply.

400 cycle audio available for modulation or audio testing. Uses 6SN7 as RF oscillator and audio amplifier. Complete kit has every part necessary and detailed blueprints and instructions enable the builder to assemble it in a few hours. Large easy to read calibration. Convenient size 9" x 6" x 4¾". Shipping Wt., 4½ lbs.

Heathkit ELECTRONIC SWITCH KIT

DOUBLES THE UTILITY OF ANY SCOPE

An electronic switch used with any oscilloscope provides two separately controllable traces on the screen. Each trace is controlled independently and the position of the traces may be varied. The input and output traces of an amplifier may be observed one beside the other or one directly over the other illustrating perfectly any change occurring in the amplifier. Distortion — phase shift and other defects show up instantly. 110 Volt 60 cycle transformer operated. Uses 5 tubes (1 6X5, 2 6SN7's, 2 6SJ7's). Has individual gain controls, positioning control, and coarse and fine sweeping rate controls. The cabinet and panel match all other Heathkits. Every part supplied including detailed instructions for assembly and use. Shipping Wt., 11 lbs.

$34.50

Heathkit 3-TUBE ALL WAVE RADIO KIT

$8.75

An ideal way to learn radio. This kit is complete ready to assemble, with tubes and all other parts. Operates from 110 V. AC. Simple, clear detailed instructions make this a good radio training course. Covers regular broadcasts and short wave bands. Plug-in coils. Regenerative circuit. Operates loud speaker. Shipping Wt., 3 lbs.

HS30 Headphones per set	$1.00
2½" Permanent Magnet Loudspeaker	1.95
Mahogany Cabinet	2.95

The HEATH COMPANY
... BENTON HARBOR 20, MICHIGAN

EQUIPMENT must be good!

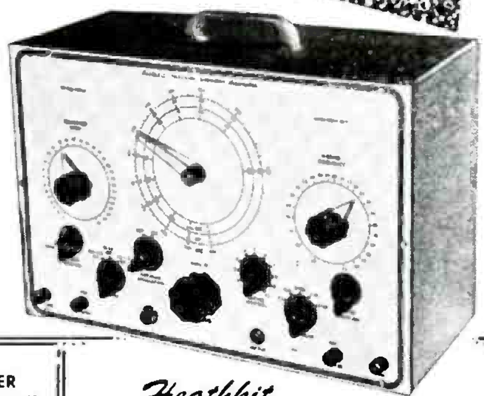
New Heathkit

TELEVISION ALIGNMENT

GENERATOR KIT

Everything you want in a television alignment generator. A wide band sweep generator covering all FM and TV frequencies — a marker indicator — AM modulation for RF alignment — variable calibrated sweep width 0-30 Mc. — mechanical driven inductive sweep. Husky 110 V. 60 cycle power transformer operated — step type output attenuator with 10,000 to 1 range — high output on all ranges — band switching for each range — vernier driven main calibrated dial with over 45 inches of calibrations — vernier driven calibrated indicator marker tuning. Large grey crackle cabinet 16-1/8" x 10-5/8" x 7-3/16". Phase control for single trace adjustment. Uses four high frequency triodes plus 5Y3 rectifier — split stator tuning condensers for greater efficiency and accuracy at high frequencies — this Heathkit is complete and adequate for every alignment need and is supplied with every part — cabinet — calibrated panel — all coils and condensers wound, calibrated and adjusted. Tubes, transformer, test leads — every part with instruction manual for assembly and use. Actually three instruments in one — TV sweep generator — TV AM generator and TV marker indicator. Also covers FM band. Deliveries start early in March. Order early.

$39.50



Heathkit

SINE AND SQUARE WAVE

AUDIO GENERATOR KIT

$34.50

Nothing ELSE TO BUY

Experimenters and servicemen working with a square wave for the first time invariably wonder why it was not introduced before. The characteristics of an amplifier can be determined in seconds compared to several hours of tedious plotting using older methods. Stage by stage, amplifier testing is as easy as signal tracing. The low distortion (less than 1%) and linear output (± one db.) make this Heathkit equal or superior to factory built equipment selling for three or four times its price. The circuit is the popular RC tuning circuit using a four gang variable condenser. Three ranges 20-200, 200-2,000, 2,000-20,000 cycles are provided by selector switch. Either sine or square waves instantly available at slide switch. All components are of highest quality, cased 110 V. 60 cycle power transformer, Mallory F.P. filter condensers, 5 tubes, calibrated 2 color panel, grey crackle aluminum cabinet. The detailed instructions make assembly an interesting and instructive few hours. Shipping Wt., 13 lbs.

110 V. A.C. MILITARY RECEIVER

POWER SUPPLY KIT

Ideal way to convert military sets. 110 V. 60 cy. transformer operated. Supplies 24 volts for filament — no wiring changes inside radio. Also supplies 250 V. D.C. plate voltage at 50-60 MA. Connections direct to dynamotor input. Complete with all parts and detailed instructions. Ship. Wt., 6 pounds.

$5.95

110 V. A.C. TRANSMITTER

POWER SUPPLY KIT

For BC-645, 223, 522, 274N's, etc. Ideal for powering military transmitters. Supplies 500 to 600 volts at 150 to 200 MA plate, 6.3 C.T. at 4 Amps., 6.3 at 4 Amps., and 12 V. at 4 Amps. Can be combined to supply 3-6-9-12 or 24 volts at 4 amperes. Kit supplied complete with husky 110 V. 60 cycle power transformer, 5U4 rectifier, oil filled condensers, cased choke, punched chassis, and all other parts, including detailed instructions. Complete — nothing else to buy. Shipping Wt., 22 lbs.

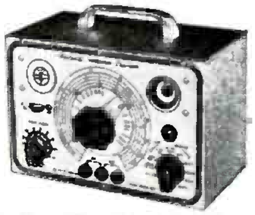
$14.50

Heathkit

CONDENSER CHECKER KIT

$19.50

Nothing ELSE TO BUY



Features

- Bridge type circuit
- Magic eye indicator
- 110 V transformer operated
- All scales on panel
- Power factor scale
- Measures resistance
- Measures leakage
- Checks paper-mica-electrolytics

Checks all types of condensers, paper-mica-electrolytic-ceramic over a range of .00001 MFD to 1000 MFD. All on readable scales that are read direct from the panel. NO CHARTS OR MULTIPLIERS NECESSARY. A condenser checker anyone can read without a college education. A leakage test and polarizing voltage for 20 to 500 volts provided. Measures power factor of electrolytics between 0% and 50%. 110 V. 60 cycle transformer operated complete with rectifier and magic eye tubes, cabinet, calibrated panel, test leads and all other parts. Clear detailed instructions for assembly and use. Why guess at the quality and capacity of a condenser when you can know for less than a twenty dollar bill. Shipping Wt., 7 lbs.

The HEATH COMPANY

... BENTON HARBOR 20, MICHIGAN


FLASH!
ELECTRONIC BARGAINS for EXPERIMENTERS and HOBBYISTS
ORDER NOW . . . ALL QUANTITIES LIMITED
POWER TRANSFORMER Specials
NO. 226. Primary 117V. 60 cycle. Secondaries supply 746 V.CT at 220 MA, 6.3V. at 4.5 A., and 5V. at 4A. Will handle 13 tube radio receivers. Supply is limited, order early. Shipping Weight 11 lbs. each.
$3.95 . . 3 for $9.95
BC 746 TUNING UNIT
NO. 257. Plug in transmitter tuning unit from army Walkie Talkie. Contains antenna and tank coils, tuning condenser, transmitting and receiving crystals. Ideal transmitter foundation. Shipping Wgt. 1 lb. Each $1.00
(Same as above except transmitter crystal in 80 meter amateur band $2.50 each)
PE101C BC645 POWER SUPPLY
NO. 273. Complete power supply for BC 645. Operates from 12 or 24 Volts. Supplies both AC and DC required. Shipping Wgt. 13 lbs. Each $3.95
T32 TABLE MICROPHONE
NO. 210. One of the Army's best. Built by Kellogg, ideal for factory call system, public address, amateur use. Brand new in original cartons. Add postage for 5 lbs. $2.95
T30 THROAT MICROPHONE
NO. 258. Makes excellent contact microphone for musical instrument or vibration pick-up. Shipping Wgt. 1 lb. $1.00 each
Extension cord with switch for above $ .50 each
DM 35 12 VOLT DYNAMOTOR
NO. 274. New input 12 Volt at 18.7 Amperes. Supplies 675V at 275 MA or ½ above voltage from 6 volts. Excellent for auto use. Shipping Wgt. 11 lbs. Each $7.50
MINIATURE ELECTRIC MOTOR
NO. 211. Tiny Delco motor only 1" x 1¼"x2" 10,000 RPM. Operates from 6 to 24 V. Excellent for models. Add postage for 1 lb. $2.95
BC731 CONTROL BOX
with Weston Model 476 AC Voltmeter
NO. 208. Excellent buy in motor control box. Size 8"x10"x5½". Contains Weston 0-150V. AC 3½" voltmeter, motor starting switch, 28 fuses all 30 Amp 110V. and 8 fuse holders. Fuses and holders alone worth the price. Shipping Weight 18 lbs. $7.95
HOME WORKSHOP GRINDER KIT
NO. 230. Easily assembled 110V AC or DC ball bearing fully enclosed motor from Army surplus dynamotor. Purchaser to make simple changes and shaft extensions, detailed instructions and all parts supplied. Motor approximately 5,000 R.P.M. Ideal for tool-post grinder, flexible shaft tool, model drill press, saw. Shipping Weight 6 lbs. $3.95
OUTPUT TRANSFORMER
NO. 227. Push pull 6V6's to 6 - 8 ohm voice coil excellent characteristics. 3 for $1.95
RCA SATURABLE REACTOR TRANSFORMER
NO. 246. New RCA No. CKV30531 AC current 750 MA DC current 2 Amperes. Rated 1.75 henries. Shipping wgt. 4 lbs. Each $1.00
METER SPECIAL
NO. 237. Brand new DeJur Model 312 0-800 M.A. D.C. Square 3" 0-10 M.A. basic meter with built in shunt. Probably the best buy ever offered in a surplus meter. Shipping Weight 1 lb. $2.95
COLLINS AUTOTUNE CONTROL HEAD
NO. 278. Brand new controls used on the ART/13, 100 Watt, Transmitter. Types 7, 8, 10, and 11 available. Get a spare while available as new cost is over $22.00 each. Shipping Wgt. 3 lbs. Price any type (mention when ordering). Each $4.50
12.6V POWER TRANSFORMER
NO. 247. New cased 110 V 60 cy. Power Transformer. Supplies 440V Ct. at 60 MA, 6.3V at 2A. and 12.6V at 1 Amp. Excellent for military sets. Shipping Wght. 6 lbs. Each. $1.95
HEARING AID HEADPHONES
NO. 216. The Army's best — eliminate flat ears and outside noise. Complete with transformer for conversion from low to high impedance. With cord and plug complete. Add postage for 1 lb. $1.00
300 MA SELENIUM RECTIFIERS
NO. 209. Rated 300 MA at 36 Volts, complete with mounting brackets. Shipping Wgt. 1 lb. 3 FOR $1.00
RCA INPUT TRANSFORMER
NO. 248. Heavy duty RCA No CKV-30529. Input has primaries 600 to 200 and 25 ohms secondary 250,000 ohms C.T. Shipping Wgt. 2 lbs. Each $1.00
BC 451 CONTROL BOX
NO. 236. Control box for 274N transmitters. Contains proper cw-voice switch, 4 channel switch, power switch, mike jack and telegraph key. Add postage for 2 lbs. $1.95
1N90 FEED THROUGH INSULATOR
NO. 276. Heavy duty feed through, 2" diameter 4" long, complete with brass hardware and gasket. Shipping Wgt. 2 lbs. 2 FOR $1.00
FEDERAL POWER TRANSFORMER
NO. 252. New cased 110V 60 cy. Power Transformer. Supplies 480V CT at 50 MA and 6.3 V at 2.1 Amps. A beautiful transformer. Shipping Wgt. 4 lbs. Each. $1.50
100 MA FILTER CHOKE
No. 641. Heavy 1.5 henry choke in drawn steel case, 50 ohm resistance, conservatively rated at 100 MA. Shipping Wt. 1 lb. 50c
MILITARY POWER TRANSFORMERS
NO. 229. Convert your military receivers without rewiring the filament. "A" type supplies 500 VCT at 50 MA, 5V. at 2A. and 24V. at ½ A. "B" type supplies 500 VCT at 50 MA, 5V. at 2A. and 12V. at 1 Amp. State whether A or B type desired. Shipping Weight 4 lbs. $2.95
1N86 STRAIN INSULATOR
NO. 277. Husky army type 1¼" diameter, 5¼" long. Brown porcelain. Shipping Wgt. 4 lbs. 4 FOR $1.00
FILAMENT TRANSFORMER
No. 922. 220V. 60 cy. primary supplies 12.6V. at 3.5 Amps, 15.6V at 1 Amp. Supplies 6.3 at 3.5 Amps and 7.8V. at 1. Amp from 110V. Shipping Wt. 8 lbs. $1.50
G.E. BC 306 ANTENNA TUNING UNIT
NO. 231. Matches any aerial to 150 Watt transmitter, used on BC 375. Brand new. Add postage for 20 lbs. $2.95
WALKIE TALKIE TRANSFORMER
No. 744. Carbon microphone input transformer and output to headphone transformer, all in one case, excellent for building your own. Shipping Wt. 1 lb. 4 for $1.00
PANEL METER
Burlington O-300 VAC Meter
No. 290. Model 32XA 3½" round AC Voltmeter 0-300 VAC full scale. Scale also calibrated 0-600V. Bakelite case. A beautiful meter in original carton. Shipping Wt. $3.95
LOW PASS FILTER UNIT
No. 637. 3000 cycle cutoff consists of 3 inductances and 4 capacitors in network, 500 ohms in and out. Excellent for clipping all frequencies above 3000 cycles. Drawn steel case, shipping Wt. 5 lbs. $2.50
DRIVER TRANSFORMER
No. 651. Couples 3000 ohm plate to push pull parallel grids hermetically sealed. Ship. Wt. 1 lb. $1.00
G. E. 1,000 VOLT 350 MA DYNAMOTOR
NO. 213. An ideal dynamotor for mobile operation in taxicabs, police cars, sound systems and amateur stations. Supplies above voltage from 12 Volts or 500V. at 350 MA from 6 Volts. Complete with starting relay, and fuses. New. Our Dynamotor A. Shipping Weight 72 lbs.
$5.95
FM PUSH BUTTON TUNER
NO. 224. Brand new ten push button tuning assembly from Army FM receiver. Contains 4 gang 100 MMF silver plated tuning condenser. Add postage for 10 lbs. $2.50 EACH
OUTPUT and MODULATION TRANSFORMER
No. 745. Companion transformer to above driver. A push pull output, 3000 ohms to 3.2 ohm voice coil, or to 1250 ohms at 80 MA. A high quality cased unit. Shipping Wt. 2 pounds. $1.00
HOW TO ORDER . . . GIVE PART NUMBER AND DESCRIPTION . . . ADD POSTAGE FOR WEIGHT SHOWN. NO ORDERS UNDER $2.00 . . . WE WILL SHIP C.O.D.
The HEATH COMPANY
. . . BENTON HARBOR 20, MICHIGAN

Radio Manufacturers Association has submitted to the Federal Communications Commission a formal set of recommendations for an expanded television service for present owners of television receivers, with future supplemental high-frequency broadcasting for additional areas. The 12 v.h.f. broadcasting channels now in use would be utilized and expanded as far as possible under the RMA program and future (u.h.f.) service and stations would have a minimum of overlap of v.h.f. areas, the RMA committee said.

The RMA recommendations are:

1. Where practical without undue interference, utilize the 12 v.h.f. channels in those areas where stations are now operating or are under construction, and extend the use of these channels to other areas as soon as possible.
2. Utilize sufficient u.h.f. channels for monochrome television so that the cities capable of supporting television and not having any or adequate v.h.f. channels can have competitive service. In general, this would require a minimum of four stations per service area.
3. Arrange the assignments so that v.h.f. and u.h.f. coverage will have a minimum of overlap.
4. Release promptly a plan of allocation for the v.h.f. and allow this plan to be put into effect at once to permit the establishment of further v.h.f. stations even though the final allocation details for the u.h.f. assignment may not be complete at that time. The propagation data, including the advantages of synchronization, now available for the v.h.f. is adequate for preparation of such a v.h.f. allocation plan.
5. Provide that monochrome television in the u.h.f. channels shall use the same standards as those employed in the v.h.f. channels.

Radio Corporation of America announced a net profit of $24,022,047 in 1948. This is equal to $1.50 per common share, compared with a net profit of $18,769,557, equal to $1.12 per common share, in 1947, both after preferred dividends. The announcement was made in his annual report to stockholders by GENERAL DAVID SARNOFF, chairman of the board. Gross revenues in 1948 were $357,617,231 against $314,023,572 in 1947.

Oxford Electric Corporation of Chicago, maker of loudspeakers, announces that it has acquired a 50% interest in the Television Tube Research Laboratories of Clifton, N. J.

International Detrola Corporation reported to its shareholders a net profit of $1,000,858 for the first quarter of 1949. Stockholders, at their annual meeting, voted to change the corporate name to **Newport Steel Corporation.** In announcing the net earnings of the company and subsidiaries for the three months ended January 31, President C. RUSSELL FELDMANN compared them with net profit of $1,710,083 for the full year ended October 31, 1948, and with a net profit of $236,624 for the comparable quarter a year ago. The quarterly net profit equals 84 cents per share against $1.40 for all of the previous year.

Quarterly sales were $20,496,904 compared to $69,314,489 for all of 1948 and $18,312,613 for the comparable quarter of 1948.

Emerson Radio & Phonograph Corporation of New York reported net sales for the fiscal year ended October 31, 1948, of $30,926,842, as compared with $32,658,122 for the fiscal year of 1947.

The income of the company and its wholly owned subsidiaries for the fiscal year, before provision for federal income taxes, amounted to $3,825,369 as compared with $3,772,638 for 1947.

The Board of Governors of The Representatives, in preparation for the 1949 Radio Parts Manufacturers, Inc., trade show, held a special two-day meeting at the Stevens Hotel, Chicago, under the chairmanship of Irvin I. Aaron of Milwaukee. Other Board members present at the meeting were Samuel K. Macdonald of Philadelphia, Dan R. Bittan of New York City, and R. W. Farris of Kansas City, Missouri. National secretary-treasurer, L. C. McCarthy, was also on hand to give his preliminary report to the Board.

The Board unanimously approved a suggestion from the Industry Relations Committee that a Creed of Ethics be prepared and submitted for adoption by the entire organization at its annual delegates' meeting in Chicago, May 16. The Creed will establish national standards of practice and procedure for the first time in the history of The Representatives. It will also incorporate a summary of the principles and beliefs of members, all of whom are experienced sales representatives in the radio, electronic, and allied industries.

Stewart-Warner Electric of Chicago will introduce a 10-inch television set operating on d.c. only, in the New York market, thus eliminating use of an a.c. converter and also giving greater image stability. This was announced by E. L. TAYLOR, general sales manager.

Sonora Radio and Television Corp. of Chicago has filed a voluntary plan of reorganization in the U. S. District Court in Chicago. It is stated that the net worth of the company is $300,000 while the claims of creditors are $250,000.

Rauland-Borg Corp. of Chicago has purchased the sound division of the Rauland Corp. also of Chicago, now a wholly-owned subsidiary of Zenith Radio Corp.

The complete line of sound and amplifier products formerly manufactured by Rauland will be manufactured and sold by the new corporation.

SAVE and Be SAFE!

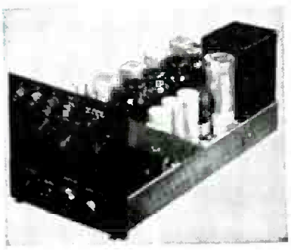
Buy Surplus & Standard Equipment with money-back guarantee at R & M RADIO

EXTRA TUNING UNITS

$2.50 each, FOB, Kingman, Ariz., or Arlington, Va.

Types in stock: TU 5-7-8-9-10-26.

Typical components: 2 vernier dials; 1 var. cap., 20-135 mmf.; 1 var. cap., 20-156 mmf.; 1 var. cap., 8-26 mmf.—neutralizing; 1 .00003-2000V cap., CD—Mica; 3 .00009-3000V cap., CD—Mica; 2 .0004-5000V cap., CD—mica; 3 .0001-3000V cap., CD—Mica; 2 4-position ceramic band switches; 2 RF chokes; 1 tank coil—ceramic form with tapped ant. coupling coil; 1 tank coil—ceramic form; 1 parasitic suppressor; 2 ceramic flex. couplings; plus banana jacks, stand-off insulators.



APN-4 RCVR—'SCOPE POWER SUPPLY

4 switch-selected screw-driver tuned RF channels; IF freq. 1050 kc. band-width 45-60 kc; RF freq. 16 2000 kc. Tubes: (2) 2Y2, (3) 6B4, (4) 6SK7, (1) ea. 5U4, 6SU7, 6SA7, 6H6, VR150. Makes fixed tuner for med. freq. police calls or PA system. Has power supply for 5" scope, with 400 cycle trans. Electronic-controlled low v. supply; delivers 260 vdc. 150 mils reg. to .01%. Power supply alone worth more than price **$8.95**

Buy it for conversion! Buy it to cannibalize!

Buy it to get on the air! It's the war-proved, versatile

BC-375-E

Quantity Limited

19.95

FOB KINGMAN, ARIZ.

Complete with
- tuning unit (TU-6)
- antenna loading unit
- dynamotor
- set of plugs
- all tubes
- wiring diagram and conversion data free

Complete conversion diagram included. Xmtr. designed to operate from 200 kc to 12 mc (less BC band). Equipped with antenna tuning unit BC-306-A—variometer and tap switch. Dynamotor (PE-73-C) complete with relay, fuses and filter.

INTER-COM

Factory Close-Out!

Brand New and Priced for Quick Clearance!

Limited Quantity **$14.95**

(List price $34.95)

Price includes master station, one remote, and 50' of wire. Rig it up as a "baby-sitter" with pick-up at baby's crib. Useful in office, or for instant contact with basement, garage, attic, kitchen. Simple to install—just plug it in to 110 v. AC or DC socket.

TRANSFORMERS

For converting SCR-274-N to 115 Volts AC.

No. 1 Power Transformer. Pri—115v 60 cycle; sec—500 CT .06 Amp. 24v ½ amp.
Price only $3.90

No. 2 Filament Transformer. Pri—115v 60 cycle; Sec. 1—14v 7½ amp.; sec. 2 14v 7½ amp. Series 28v 7½ amp. Parallel 14v 15 amp.
Price only $4.50

No. 3 Filament XMFR. Pri—115v 60 cycle; Sec. 24v 2 amps.
Price only $2.25

• Speakers—Brand New

Permanent Magnet

4"	$ 1.60
5"	1.85
12" Jensen in Metal Case	14.50

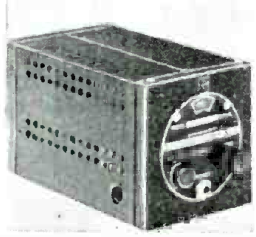
10% discount, purchase of 2 or more

Heavy Duty Transmitting Chokes

8 HY—500 MA—5000 V INS.
Price each $8.95

• Condensers—Fixed

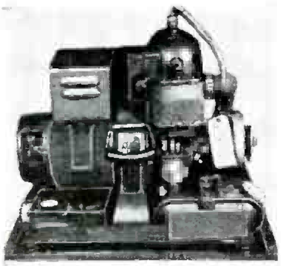
.05 Mfd. 600 Volts	$0.15
10 Mfd. 350 Volts	.69
15 Mfd. 150 Volts	.60
16 x 16 450 Volts	1.20
20 250 Volts	.69
40 150 Volts	.75
50 150 Volts	.69
150 25 Volts	.54
200 10 Volts	.45
8 x 8 Can. Electrolytic	1.50



BC 1206, LAZY Q FIVER

SINGLE SIGNAL RECEPTION **$9.95**

The littlest BIG BUY ever offered! A BC-1206 Setchell Carlson receiver will take the place of BC-453 (Lazy Q Fiver). We think it's even better. Here's why: Smaller—4" x 4" x 6⅝"; weighs only 3 lb. 14 oz. Less current drain. .75 amps at 24 v. DC. IF freq. 135 kc. A conventional superhet circuit is employed and is arranged so that AVC will prevent overloading on strong signals.



The Famous PUTT-PUTT

Gasoline Generator (HRU-28)

28 - 32 Volts D.C. ONLY **$74.50**

Single cylinder, 2-cycle gasoline engine with generator that is rated at 2,000 watts direct current. 70 amps. Has unlimited use around a farm; useful as field day power supply. More literature upon request.

DUAL POWER SUPPLY

SAVE YOUR BATTERY

Both for $8.95

$4.95 each

Use our dual dynamotors by wiring them in series and use one on receivers and both in transmitter. High voltage output 600 volts at 48 watts. Low voltage 300 volts at 24 watts.

Tubes (New, in Original Cartons). For the SCR-274-N Command Set & Others.

12A6	69c	OD3-VF150	75c
12SR7	69c	12SA7	69c
12K8	69c	77	59c
12SK7	69c	78	59c
12SF7	69c	89	59c
1625	89c	38322	$1.19
1626	79c	12J5-GT	69c
1629	89c		

ALL EQUIPMENT F.O.B.

R & M RADIO COMPANY

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The Radio Technician

. . . Good days are ahead for the radio servicing trade . . .

By HUGO GERNSBACK

SINCE 1929—for just 20 years—this magazine has conscientiously endeavored to serve the radio service technician. It will continue to do so in the future.

But as radio continued to change, so did the radio technician. In 1925 the man with a screwdriver and a pair of pliers had no particular difficulty in servicing radio sets. But as radio receivers became more complex every month, the service technician had to change as well. Servicing instruments came into wide vogue in the 30's, and their complexity increased to keep pace with the ever-changing radio picture.

Today—with television booming beyond our fondest expectation—the oldtime "serviceman" no longer can cope with the complexity of these new televisers.

Besides being a radio man he now also must be a television man, and if he has not had experience with television it means that he must learn the subject from the ground up.

For this reason and many others, it has been decided by RADIO-ELECTRONICS that beginning with this issue the old term "serviceman" be discontinued entirely, using in its place the more modern and appropriate term "radio technician."

RADIO-ELECTRONICS did not originate this term. It has been used in the radio manufacturing trade consistently for some time. We feel certain that the new—and better—term will enhance the standing of the present-day service technician a good deal in his community.

To borrow a very apt expression of Max F. Balcom, President of the Radio Manufacturers Association, in a recent talk:

"It means that the radio technician will be working on a much more costly product (televisers) than he has been in the radio field. . . . *It is like turning from repairing bicycles to servicing automobiles.*" The italics are ours.

With television now firmly established it would seem that great and profitable days are ahead for the servicing trade. Indeed it will be a small miracle if there can possibly be enough radio technicians to service all the new televisers by 1952. Here is the reason we see it that way.

There are now approximately 75,000 established radio technicians in this country. In many localities they have difficulty in servicing the 67 million radio sets now in use, *plus the over two million television sets* already installed. By the end of this year there will be at least three million television receivers in use. By the beginning of 1952, it is not only possible but very probable that there will be between 12 and 15 million televisers in the public's hands.

Unless there is a steady influx of new radio technicians, *who is going to service all of these receivers?*

What is needed at the present time—needed desperately—are trained—really trained—radio technicians who know television from A to Z. Look into any newspaper in the country where television programs are now being broadcast and note the help-wanted advertisements. These advertisements show that there is, even now, *a scarcity of good radio technicians who know their business.* This situation is certain to become more acute as time goes on.

The radio and television set manufacturers are fully aware of this situation and are now taking active steps to promote service meetings for radio technicians all over the country. They, however, deplore the fact that they are meeting with resistance and indifference from many radio technicians who do not attend these meetings in force. Regardless of who the manufacturer is, the service technician can gain a tremendous amount of knowledge by attending these meetings as they take place. No matter how busy he is, he should find time to attend these meetings which are now increasing rapidly in number all over the land.

Service technicians must follow certain routines in servicing televisers. These routines save a great deal of time. In other words, it is the old "know how." All these points are discussed in great detail at these service meetings, and any radio technician —no matter how good his knowledge—can enhance his standing by attending them. *They cost him nothing except his time.*

Another important matter that should be mentioned here is the following:

According to a countrywide survey made by the Broadcast Measurement Bureau, there were early this year 5,177,100 radios in the U. S. not in operating condition. That is a lot of receivers.

What have the radio technicians done to obtain this lucrative business now lying dormant? Apparently nothing.

Several radio manufacturers have investigated this condition and are ready to give the radio service technician not only hints, but also advertising suggestions that can be used locally to induce the owners of these old receivers to have them repaired and put into use again.

There is little question in our mind that there will be an extended radio servicing boom in the very near future. Are you ready for it?

Announcing
$100 PRIZE CONTEST

TELEVISION receivers can be made simpler. The number of tubes used in a modern televiser is reminiscent of the number of controls on broadcast receivers in the early '20's, when some of the best sets had close to a dozen knobs and dials.

The problems of simplification are complex, and well worth the attention of the most advanced experimenters in the art. To stimulate interest in this project, RADIO-ELECTRONICS is publishing below a description of a successful French televiser which uses only eight tubes besides the cathode-ray tube.

RADIO-ELECTRONICS now offers a cash prize of $100 for the best simple American televiser to be constructed under the following rules:

1. No fixed number of tubes is prescribed; but because the prize contest stresses simplicity, the receiver which uses the fewest number of tubes to accomplish given results will be rated highest. Televisers with more than 12 tubes (excluding rectifiers) will not be considered in this contest.

The cathode-ray tube and rectifier tubes (or selenium rectifiers) will not be considered tubes for the purpose of this count, but any crystal diode used in detector, limiter, and other circuits where a tube is commonly employed will be counted as half a tube.

2. *Only* photographs and description of the televiser are to be sent to RADIO-ELECTRONICS. If the editors wish to inspect the set, they will request it. Express charges both ways will then be paid by RADIO-ELECTRONICS.

3. To make construction simpler, and to focus attention on the main problem of simplification, it is not necessary that the televiser cover both television bands. A set which covers one band only will be judged against its competitors on the same band.

However, since the American tradition (unlike the European) has been to have the sound and vision receivers in one unit, *all receivers submitted must be capable of receiving both television sight and sound.* Loudspeaker results are not necessary; headphone output may be used.

4. All descriptions and photographs of the winning receiver will become the property of RADIO-ELECTRONICS, which will publish a descriptive article on the set at regular space rates. The set itself will remain the property of the builder.

5. If two or more televisers are judged worthy of a prize, identical $100 awards will be made for all accepted entries.

6. As it is the purpose of this contest to stimulate actual building of a special televiser, mere ideas and proposals, special circuit diagrams, patents, etc., are excluded from this contest.

7. Excluded from this contest are all employees of RADIO-ELECTRONICS and their relatives.

8. This contest closes at noon, September 1, 1949 (Eastern Standard Time), at which time all entries must have been submitted to RADIO-ELECTRONICS.

9. The judges of this contest will be the Editors of RADIO-ELECTRONICS and their findings will be final.

10. Announcement of the prize awards will be made in the January, 1950, issue of RADIO-ELECTRONICS. The prize or prizes will be paid on the publication date of the January issue of RADIO-ELECTRONICS.

Eight-Tube Televiser

THE construction of a television receiver is said to require time, a calibrated signal generator, and plenty of money, declares a writer in a recent French radio magazine. But he believes—and has constructed a televiser to prove his belief—that a set that does not cost an unreasonable sum can be built, and that its construction is not especially difficult.

The total number of tubes in the set, built by Pierre Roques—the French engineer who set out to prove that television sets can be simple—is eight! With this small number of tubes, the quality of pictorial reception is excellent, stability is satisfactory, and the sensitivity such as to receive transmissions from the Paris station in all parts of that city with an ordinary dipole antenna. The sole drawback, according to the constructor of this unique televiser, is the small image size. The tube is the equivalent of the American 3-inch size. The set does not have a sound channel.

While there are many differences between American and French television problems, notably the positive transmission and the fact that there is only one French station on the air, the Editors of RADIO-ELECTRONICS feel that there is much worthy of study in this simplified television circuit, and it is therefore reproduced below.

French television receiver

The televiser has eight tubes (plus the cathode-ray tube) which have the following functions:

1. A radio-frequency amplifier using two high-transconductance tubes, type EF51;
2. A detector using half of a 6H6;
3. A video frequency stage using an EF51;
4. A sync separator stage using the other half of the 6H6;
5. A line sweep comprising a triode-pentode ECF1 as multivibrator and half a 6N7 as a sweep amplifier;
6. A frame sweep using the other half of the 6N7 as a blocking oscillator synchronized by the 50-cycle line;
7. A low-voltage supply (300 volts) with a 5Y3-GB;
8. A high-voltage supply (1,000 volts) using a 6H6 as a voltage doubler;
9. A 7.5-centimeter (3-inch) cathode-ray tube.

The r.f. amplifier

The hookup of this section is very standard. The input circuit is designed to match a 72-ohm co-axial cable. The gain (contrast) control is the 5,000-ohm, wire-wound potentiometer P1, which varies the bias of the first r.f. tube.

Detection

The winding L4 inputs to the cathode of the 6H6, and the detected video signal appears between its plate and

Schematic of the French experimental television receiver which obtains excellent results with eight tubes (plus cathode-ray tube).

ground. This is applied to the video-frequency stage through a resistance of 500 ohms, which, with the input capacitance of the video tube, forms a filter which removes any residual radio frequency.

Video-frequency amplifier

Again we have a standard schematic. A high-frequency compensation coil is not used; with the small picture tube it is not necessary to amplify a wide band of frequencies.

The amplified video-frequency signal is then applied to the cathode-ray-tube control grid through a 0.1-μf capacitor of very high quality (1,500-volt test at least) and through another capacitor of the same quality to the sync separator half of the 6H6.

Sync separation

The signal on the cathode of the 6H6 is such that the sync pulses go negative and the video-frequency signals go positive. Thus no current passes through the diode except during synchronization. We find, then, at the plate negative pips which are sent on to the multivibrator.

To improve the output of this separator stage, the 6H6 plate is given a slight positive polarization.

Line sweep

The ECF1 is hooked up as a cathode-coupled multivibrator. The frequency is controlled by the 500,000-ohm potentiometer P2. The amplitude can be controlled by changing the resistance of the resistor shown as 100,000 ohms in the plate lead of the triode section.

A capacitance-type voltage divider (.0005 and .01 μf) permits obtaining the necessary voltage to apply to the sweep amplifier (one-half of a 6N7). The high grid resistance of this tube permits automatic biasing by inserting resistance in the cathode. The gain of the amplifier is controlled by adjusting the plate resistor (20,000 ohms) to a suitable value (see "Putting into Operation").

The cathode-ray-tube deflection plate D1 is connected to the plate of the triode section of the ECF1 through a capacitor of .005 μf. The plate D2 is also connected to the 6N7 plate through a capacitor of the same value.

Frame sweep

The second half of the 6N7 is hooked up as a blocking oscillator. The transformer has the following characteristics:

Secondary: 1,000 turns No. 30 enamel
Primary: 500 turns No. 30 enamel
Core: 2 x 4 centimeters square
(small filter choke or loudspeaker transformer).

The frequency is controlled by the 1-megohm potentiometer P3. Synchronization is effected by bringing the transformer to chassis through the intermediary of a resistance bridge connected between the filament (6.3 volts) and chassis. It is put into phase by varying the frequency potentiometer slightly, once it has been adjusted to 50 cycles per second.

The sweep amplitude is regulated by changing the value of the resistor (shown as 1 megohm) in the 6N7 plate. The sawtooth waves obtained are applied to the deflection plate D2 through a .01-μf mica condenser.

Medium-tension supply

An indirect heater tube 5Y3-GB is used, with a 300-0-300-volt transformer feeding its plates. The center point is returned to the chassis through a resistance of 300 ohms, thus supplying a voltage of –20 for the brightness control.

High-tension supply (1,000 volts)

The transformer has an output of 450 volts which is supplied to the 6H6, connected as voltage doubler. The rectified voltage of 900 is connected in series with the medium voltage supply of 300 volts, providing 1,200 volts. After filtering through the 100,000-ohm resistor, about 1,000 volts remains. The multivibrator and blocking oscillators are also supplied with this voltage.

Cathode-ray tube

A Philips tube of 7.5-cm diameter (DG 7) with green phosphor, its characteristics are:

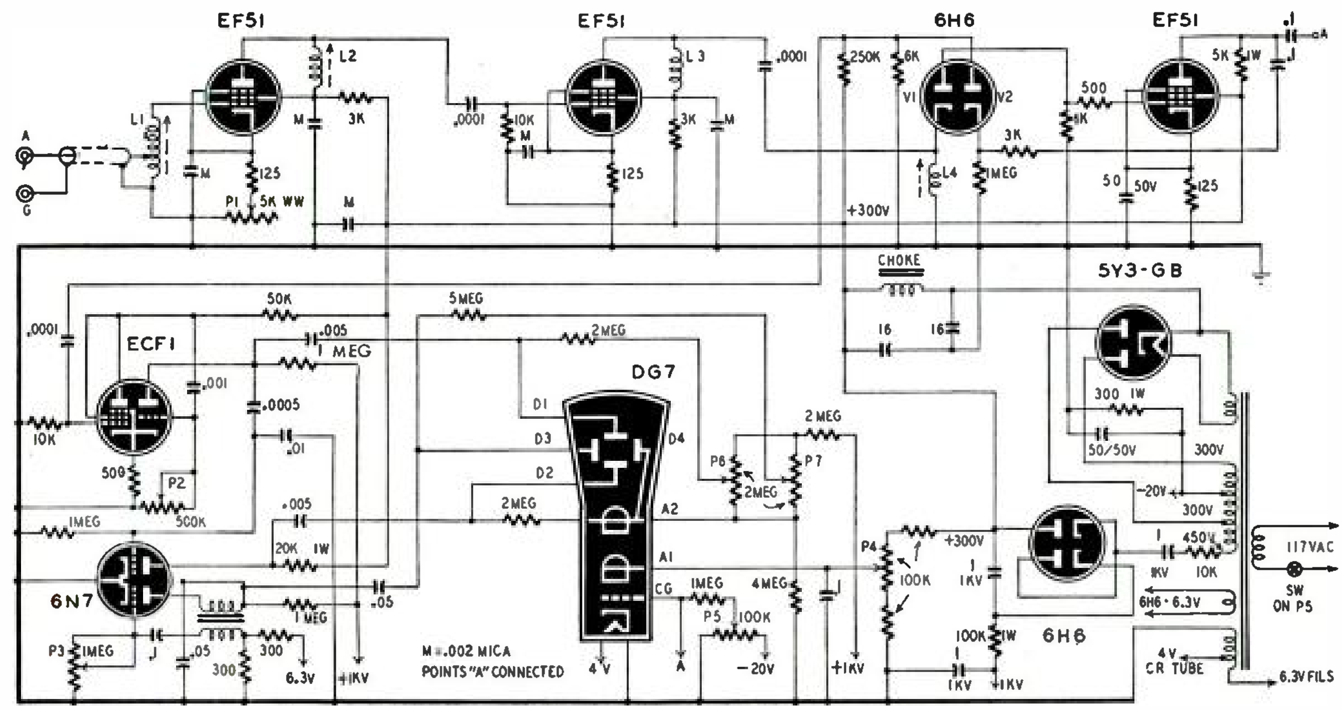
Filament: 4 volts, 1 ampere
Second anode: 600 volts
First anode: 150-200 volts, variable (focusing)
Control grid: variable, never positive (brightness).

The second anode voltage is obtained with a voltage divider which serves the vertical and horizontal hold-control system at the same time (P6 and P7 are two 2-megohm potentiometers). The focusing control is the potentiometer P4 (100,000 ohms) and the brightness control is P5 (100,000 ohms with switch), the switch being the on-off switch of the set.

Putting into operation

Putting the r.f. section into operation is a quick process. All that is needed, after checking the wiring and the voltages, is to attach the antenna.

If the windings are correct, images



should be received immediately (check with an oscilloscope connected to the control grid, for preference). Then adjust the cores of the r.f. coils for maximum reception, with potentiometer P1 in the position of maximum gain (shorted).

Flashes may then be seen in all directions on the tube screen. Working with the potentiometers P2 and P3 brings out the image and stabilizes it. The dimensions are regulated as follows:

1. Vertically (frame): Change the 1-megohm resistor in the 6N7 plate circuit.

2. Horizontally (line): Disconnect the capacitor in the D2 circuit and bring the sweep to half the desired dimension by changing the 1-megohm resistor in the ECF1 triode circuit. Reconnect the capacitor and adjust the 20,000-ohm resistor in the 6N7 plate circuit until the normal size is obtained.

The antenna recommended is a doublet with unbalanced lead-in. The co-ax should have an impedance of about 75 ohms.

Here, to conclude, are the power transformer specifications:

Primary: 110 volts, 0.5 ampere
Sec. 1: 5 volts, 2 amperes
Sec. 2: 300-300-450 volts (100 ma)
Sec. 3: 6.3 volts, 0.3 ampere (for 6H6 doubler)
Sec. 4: 6.3 volts, tapped at 4 volts, 3 amperes (filaments, including DG7).

Changes for U. S. standards

A few modifications may permit this circuit to be used as the basis for an experimental video receiver for use in this country. The first step is to revise the t.r.f. circuit. The EF51 is a variable-mu pentode designed for high-frequency service. This tube has a transconductance of 9,500 micromhos. No American tube can be used as a direct replacement, but the circuit can be modified to fit a number of our tubes. A 6AC7 can be used in this circuit (with a 300-volt B-supply) if a dropping resistor is used to limit the screen voltage to 150 when the plate is drawing 10 ma at 300 volts. This resistor will be in the order of 60,000 ohms. The cathode biasing resistor should be about 160 ohms, and the suppressor should be grounded directly to avoid instability and feedback. (For high-band use, a 6AK5 might give more gain than a 6AC7.) Coils L1-L4 for low band may be air-wound with about 3 turns of No. 14 wire with an inside diameter of ½ inch. The spacing between turns should be adjusted so the coils cover the desired range when tuned with 5-50-$\mu\mu$f, miniature air trimmers. The location of the antenna tap on L1 should be found by experiment. Commercial permeability-tuned coils such as the National AR-2 and AR-5 may be used.

The video detector V1, one half of the 6H6, develops a positive-phase output signal. This signal is reversed 180 degrees in its passage through the EF51 video amplifier. If this signal is applied to the grid of the C-R tube, the image will look like a photographic negative (the dark areas will be light and the light ones dark). This can be avoided by using two video amplifiers in cascade instead of a single stage. The same results can be obtained by reversing the connections to the video detector plate and cathode, though the first method has the advantage of providing extra amplification. The picture phase at the input of the sync clipper should be opposite to that at the input to the grid of the C-R tube, so the connections to the plate and cathode of V2 will also have to be reversed.

The ECF1 is a variable-mu pentode and triode similar to the 6F7 or 6P7. The pentode section of this tube is operated as a triode; therefore any number of dual triodes may be made to work equally well. The constants of the differentiating circuit, 10,000-ohm grid resistor, and .001-μf coupling capacitor may have to be juggled to provide proper separation of the horizontal sync pulses so they can control the horizontal multivibrator. Remember that the resistor in the differentiator circuit is also the grid leak of one section of the multivibrator.

The design data for the blocking transformer may prove suitable for constructing a unit to work at 60-cycles. However, it will probably be best to use a commercial vertical blocking transformer since they are available for less than $2.50.

The high-voltage power supply will depend on the C-R tube used. Such tubes as the 2AP1, 3BP1, 3EP1, 3KP4, etc., can be used. It is doubtful that the average builder will find a power transformer like the one shown in the diagram, but it is possible to connect the voltage doubler to one of the plates of the low-voltage rectifier rather than to a tap on the winding. A number of surplus radar and oscilloscope transformers are available and the experimenter will be able to find one of these to suit his needs. A small replacement power transformer may be used. One side of its high-voltage secondary may be grounded and the other end connected to the plate of a rectifier tube. The positive high voltage may be taken off its filament or cathode.

It may be necessary to bypass the r.f. amplifier filaments to ground with .0005-$\mu\mu$f mica or ceramic capacitors and to insert small u.h.f. chokes in the hot leads. These chokes may consist of 20-25 turns of No. 22 enamel wire wound on a 1-megohm, 1-watt resistor or other suitable form.

The 5Y3-GB is a Mazda tube directly replaceable, in this circuit, by a 5Y3-G or 5Y3-GT. Any rectifier tube having similar characteristics can be used.

This article, up to "Changes for U.S. Standards," was based on a translation of an article in the December 1948 issue of *T.S.F. pour Tous* (Paris).

BRIGHTER TELE IMAGES NOT ALWAYS BETTER

The answer to better video images is not to be found in merely increasing the brightness of the image, it was indicated by a paper presented at the Winter General Meeting of the American Institute of Electrical Engineers in New York, by Dr. P. C. Goldmark of the Columbia Broadcasting System.

Reporting on research into brightness and contrast in television, Dr. Goldmark said, "Contrast range is more important than mere brilliance, and contrast at moderate brightness is far more important to the eye than brightness applied indiscriminately. Increased brightness is of use to the eye only if it brings with it increased contrast.

"It is this increased contrast which assists the eye to see fine detail. If one wishes to see greater detail in a picture, one may increase the contrast, if possible, or move closer to it for a more detailed examination. The limit is set by the maximum possible picture brightness and the eye's resolving power.

"Several inherent properties of television make it difficult either to increase the brightness or view the picture from a closer range. The most basic limitation is that television's pictures are made up at approximately 500 horizontal scanning lines. Each line can show no detail along its height, but can show variations along its length. No matter how closely one looks at a television screen, or how bright it is, no detail smaller than a square area whose height is roughly that of a line can be perceived.

"One of the proposed solutions for producing adequate contrast range in television pictures suggested increasing the picture highlight brightness to a value many times above that of the surrounding brightness. This solution does not solve the problem because local illumination which is much higher than the general ambient illumination produces a sensation of glare, and glare reduces visual effectiveness. Experiments with visual acuity and with contrast recognition have shown that both reach their optimum for a given brightness when the surrounding illumination is about the same as the locally illuminated area.

"Many present day receivers," said Dr. Goldmark, "should not be viewed in rooms where the surrounding illumination is much in excess of 1 foot-lambert, otherwise the picture will suffer from inadequate contrast range. It is conceivable that commercially competitive direct-view receivers will some day be capable of furnishing a highlight brightness of 450 foot-lamberts. It is doubtful, however, that this would be a satisfactory solution, since viewing such a bright image without a correspondingly bright surrounding would be uncomfortable. Assuming that the presently used field repetition rate of 60 per second were employed, such a picture would also display objectionable flicker."

TELEVISION'S TRENDS

By DR. LEE deFOREST

THE first question I meet everywhere is: Do present tendencies indicate a material and permanent drop in receiver prices?

No marked falling off in the general price level need be expected so long as the present demand continues. As each new TV transmitter goes into operation, a new audience arises, of a size proportionate to that of the city or district involved. Until every town in the nation of 50,000 or more has its transmitter, any approach to saturation, with a resultant falling off of receiver demand, is most unlikely. Such considerations seem to postpone any very great price reduction for a long time to come.

Naturally the 7-inch and 3-inch sets will be even cheaper than they are today, because the relative merits of the 12-inch and 16-inch tubes are so convincing that the demand for the smaller sets, even with prices reduced, will diminish. And until the projection set has been materially improved, the brilliant, direct-view, large-tube set will continue in top demand.

We need not apprehend any changes from present RMA TV standards for a long time to come, such as may be required for the yet ill-explored u.h.f. bands. The industry today is too firmly founded, the television audiences already too vast and ever growing to permit the FCC to recommend or impose confusions of that nature.

This argues against expecting any radical changes in circuits. Simplified printed-circuit elements may be expected, and will somewhat reduce labor costs and speed up production. Multi-unit chassis will simplify service.

I think we shall see, ere long, rectangular, metal, pyramidal tube structures, involving, incidentally, a flatter glass screen surface. Without doubt, tube makers will solve the (apparently) difficult problem of the glass-metal rounded-corner seals which today are unsure against crack-strains. Such a tube, of 16 × 12-inch dimensions, giving us approximately 190 square inches of brilliant picture, and avoiding all huddling, should prove ideal.

For theater television, the FCC has found no specific place in the spectrum, but will give co-operative consideration to applications for experimental research involving intracity transmissions on frequencies between 480 and 920 mc, an allocation however, which can "be discontinued when needed for broadcasting!" In addition, experimentation with intra- and intercity relay of theater television programs may be authorized on six hyper-high bands, extending from 1,900 to 30,000 megacycles. Here, surely, is abundant opportunity for endless experimentation, with microwaves from 19 to 3 centimeters—not to mention the intracity possibilities of infra-red or ultra-violet light transmissions *without* consent of the FCC.

TV set is focal point of many present-day living rooms, will appear in most in the future.

It is clear that theater television in general will have no rosy path of progress, beset as it will be by unsolved problems of desirable tele programs, split-second time schedules, as well as mighty tough engineering. One basic change will be requisite: to double at least the present number of picture lines. A 525-line picture when blown up even to 18 × 12 feet resembles too unpleasantly a peepshow through a Venetian blind.

And after all, save for outstanding athletic events or a presidential inauguration (which we can all see in our homes), why should television attempt to compete with photographic projections which will always be inherently far superior? This talk of supplementing theater film reels by broadcast television pictures is the veriest twaddle, a fatuous dream.

In closing, a word regarding color. Elaborate and exceedingly costly experimentation, notably by CBS and RCA, has demonstrated that, given sufficiently high-frequency carriers and adequately wide video bands, good natural-color subjects can be transmitted. The appeal of such pictures in comparison to black and white is as compelling, as exciting, as that witnessed today in every cinema when a technicolor film is shown.

Unquestionably, therefore, we shall have color television. How soon is anyone's guess. Certainly not in two years, perhaps five. Whether this will be by so-called mechanical methods or "all-electronic" is still debatable. My own current experiments along these lines, while as yet not sufficiently far advanced to be definitely conclusive, give encouragment to the prospect of three-color-transmission *using our present black-and-white frequencies.* As of today, therefore, I see no necessity for restricting color to the u.h.f. ranges, with all the uncertainties involved—short transmission range, multiplied ghosts, obstructions, signal inaccessibilities, and so on.

Certain it is that the future, immediate and remote, of television is unlimited, eventful beyond our present imagination—and *glorious*, if we care to build it so.

All Channel TV Tuner

A TV front end can be constructed without any of the usual specially made coil or bandswitch assemblies

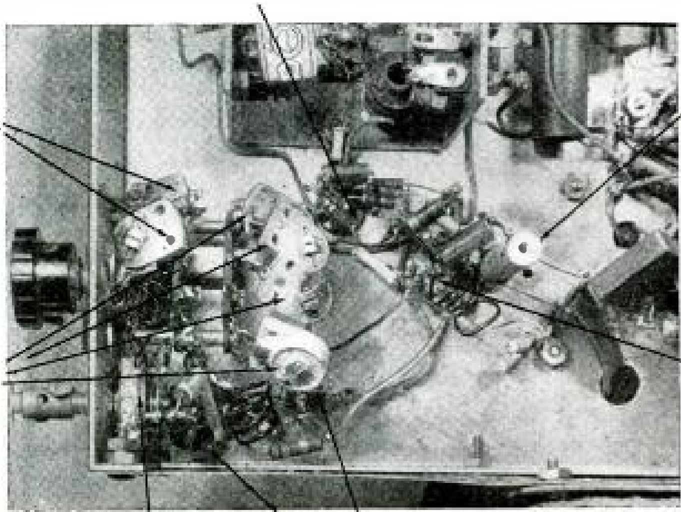
By E. J. SCHULTZ

ALTHOUGH there are a number of good television receiver kits and components available on the market, there are numerous constructors who, like the author, take pride in constructing their equipment without using manufactured assemblies. The average constructor will find that design and construction data on video i.f. amplifiers, detectors, sweep circuits, and video amplifiers have been published in a number of technical magazines and papers. Unfortunately, for us, little or no material is available on constructing or designing a TV front end for all channels. A number of commercial tuners have been described, but all these rely on special switches, turrets, or other components not readily available to the ordinary radio constructor.

Tuners usually present two problems: one is to make the oscillator work over the entire range, and the other is to track the mixer and antenna stages once the oscillator is working properly. The tuner described here was developed after weeks of experimenting with all types of circuits. Simple, it can be duplicated by almost anyone experienced with high-frequency circuits. It uses a channel-switching tuning system that can be made to work into almost any existing video i.f. circuit. It will work nicely with the video i.f. amplfier described on page 110 of the March, 1949, issue.

The circuit consists of a 6J6 broadband, grounded-grid amplifier with a cathode coil that is broadly resonant over the entire TV band. Its input circuit has an impedance of approximately 300 ohms on all TV channels. The plate circuit of the 6J6 is tuned and capacitance-coupled to the grid of the 6AG5 mixer. The oscillator is a 6C4 with its grid circuit tuned *above* the signal frequency and its cathode circuit loaded with an inductance. The plate is at ground potential for r.f. The oscillator and mixer grids are coupled to each other through stray capacitance and inductance.

The channels are selected with a 2-circuit, wafer-type rotary switch. One wafer switches small preset trimmer capacitors across the coil in the plate circuit of the 6J6, and the other shunts the oscillator coil with preset trimmers or small inductors. The capacitors lower the resonant frequency of L4 and the inductors raise it. Switch-tuning is advantageous in that it permits each channel to be aligned without disturbing the settings for other channels. A 2-plate midget and a 10-μμf capacitor are in series across the oscillator coil for fine tuning.



The parts are assembled in a compact mass under the chassis to eliminate long-lead trouble.

Construction

The channel-selector switch should be well constructed with good high-frequency insulation and good, clean, low-resistance contacts. A 7-position switch was selected for channel-switching since this is the maximum number of channels that will be assigned in any one area. If a builder is midway between the primary service areas of stations in two cities, a switch with more positions can be used. The position of the components is shown in the photographs. The oscillator grid and 6J6 plate circuits should be as close to the switch as components permit. In cases where leads must be long, make them out of heavy wire, as is usual in v.h.f. work.

The under-chassis photograph shows placement of the parts in the tuner circuit. The oscillator socket is hidden by components mounted on its terminals. It is mounted just back of the 2-plate midget capacitor used for fine tuning. The oscillator grid coil, L4, is the large one between L8 and L9. The shunt inductors L5, L6, and L7 are mounted directly on the channel-selector switch. L3, the tuned coil between the amplifier plate and mixer grid, is the heavy winding close to the antenna coil. Circuit operation may possibly be improved by locating this coil at the socket of the 6AG5.

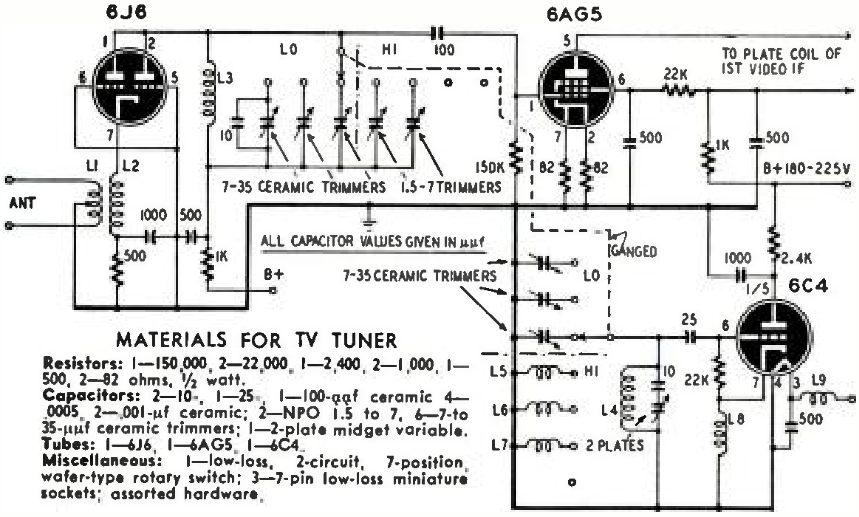
L1 has 6 turns interwound with L2, which has 12 turns on a ⅜-inch form. Both coils are closewound with No. 32 s.s.e. wire. L3 has 3½ turns of No. 14 enamel wound with an inside diameter of ½ inch and spaced to 1 inch long. The oscillator coil L4 consists of 2½ turns of No. 14 enamel wire spaced to ½ inch with a ½-inch inside diameter. L5, L6, and L7, the shunting inductors, are for channels 7, 11, and 13, respectively. They are self-supporting coils wound with No. 20 enamel wire to a ¼-inch inside diameter. L5 has 5 turns spaced to ½ inch, L6 has 3 turns spaced to ⅜ inch, and L7 has 2 turns spaced to ½ inch. L8 is a self-supporting coil made from 25 turns of No. 20 enamel wire close-wound on a ¼-inch form. L9 is 30 turns of No. 30 enamel wire close-wound on a 3/16-inch form. The specifications for L5, L6, and L7 are approximate. The exact number of turns and spacing will have to be determined for each individual layout. Coils can be wound for other channels by using cut-and-try procedure based on the data which has been given for channels near them.

Aligning the tuner

The tuner should be completed and connected to the i.f. system of a receiver before beginning the alignment procedure. Cut-and-try adjustments can be minimized by calculating the lowest oscillator frequency and adjusting L4 to approximately this frequency with an absorption frequency meter. The oscillator operates *above* the signal frequency, so its frequency can be found by adding the sound i.f. to the sound carrier frequency or by adding the video i.f. to the video carrier frequency.

The tuner can be aligned on a television signal or with an accurate signal generator. Set the channel-selector switch to the channel to be tuned in. Adjust the appropriate oscillator trimmer so the sound and picture come in together. Adjust the mixer trimmer for the best compromise between picture quality and maximum volume. If a high-band channel is being aligned, resonate the oscillator by varying the spacing between the turns of the shunt inductors. A tuning wand is useful in this operation because it indicates whether the turns should be squeezed together or spread apart. The vernier tuning control should be set at its mid-point when aligning each channel.

If it is impossible to peak the mixer coil on the highest channel, its trimmer may be replaced by a parallel inductor similar to the ones in the oscillator circuit.

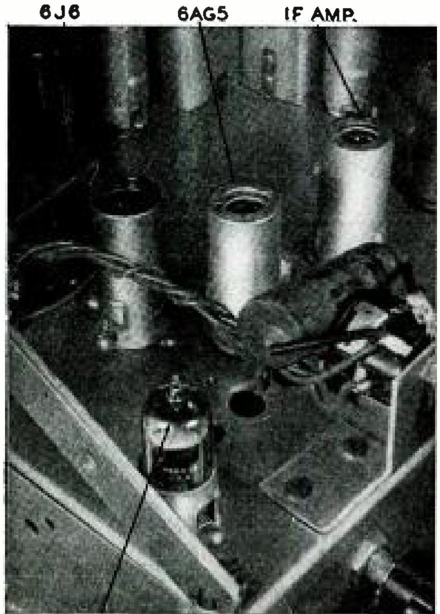


MATERIALS FOR TV TUNER

Resistors: 1—150,000, 2—22,000, 1—2,400, 2—1,000, 1—500, 2—82 ohms, ½ watt.
Capacitors: 2—10-, 1—25-, 1—100-μμf ceramic 4—.0005, 2—.001-μf ceramic; 2—NPO 1.5 to 7, 6—7-to 35-μμf ceramic trimmers; 1—2-plate midget variable.
Tubes: 1—6J6, 1—6AG5, 1—6C4.
Miscellaneous: 1—low-loss, 2-circuit, 7-position wafer-type rotary switch; 3—7-pin low-loss miniature sockets; assorted hardware.

The tuner precedes a 3-stage video i.f. amplifier followed by a detector and video amplifier driving a 7-inch picture tube. The set receives all New York City channels with satisfactory signal strength and picture quality when using an indoor antenna at Bayside, Long Island, approximately 15 miles from the stations.

Although not the ultimate in design, this tuner gives good results and will serve as a foundation for those constructors who design and build their own television receivers.



Top-chassis photo shows how tubes are placed.

TELEVISION NOTES OF THE MONTH

Channels for TV may number 50 to 70 if a u.h.f. band is adopted, FCC chairman Wayne Coy told a group of radio and advertising executives recently. "I hold the need [for additional channels] to be self-evident," Mr. Coy said in a speech in Boston. "How many channels it takes to satisfy that need I do not know. My present thinking is that 50 to 70 channels may be required." Adding his own predictions to those current recently about the fight for audiences between radio and television, Mr. Coy said, "As I see it, broadcasters who own television stations will gradually dispose of their radio stations and concentrate on television." This, he added, will be because advertisers do not like to spend their money with an organization which operates another simultaneous service competing for the same audience. He foresees, however, that aural broadcasting will remain important for specialized programs and that networks will soon be sending one type of program schedule to areas served by television and a different service to those where there are no television stations.

Six rules for visual comfort in viewing television were issued recently by the American Optometric Association. They are:

1. Make sure that your set is properly installed, with particular attention to the antenna, for clearest possible reception.
2. In tuning, adjust audio tone setting before turning the picture up to desired brilliance. Strike a comfortable balance between steadiness of image and brilliance. Either an unsteady image or too much light will result in visual discomfort.
3. Avoid both intense darkness and bright light in the room in which television is viewed. If the room is totally dark there will be too much contrast between the bright screen and its surroundings. If there are bright lights they will distract you from the screen. Mild, indirect light in the room is preferable.
4. Sun glasses should not be worn for televiewing because they adapt vision to unnatural conditions.
5. Avoid excessively long periods of close concentration on the television screen.
6. In case of discomfort, have your vision examined by a competent vision specialist and follow his advice. Many older persons who wear bifocal glasses may find neither segment suited to television viewing. They may be helped by special lenses prescribed for the proper distance.

Color television's usefulness in teaching medicine and surgery will be demonstrated at the annual meeting of the American Medical Association in Atlantic City in June, under a plan of Smith, Kline and French, Philadelphia pharmaceutical firm, and the University of Pennsylvania. Pickups will be made by CBS in cooperation with Zenith and Webster-Chicago. For four days, surgery and other procedures at the Atlantic City Hospital will be scanned and transmitted in color to 20 receivers in Convention Hall. The system used will be the CBS color-disc.

Students Build TV Transmitter

Full operation is expected late in the year.

By STEVE LAMOREUX

IDAHO STATE COLLEGE, by solving the TV parts bottleneck, is also solving that other television stickler—lack of trained men. And in so doing they have demonstrated that TV is still in the amateur's domain.

Plans drawn by a former civilian Navy electronics specialist, William Shiflett, have resulted in what would ordinarily be a million-dollar TV broadcasting setup. It is now being completed at the college for about $25,000 actual cost, including studio construction.

War-surplus radar parts, rebuilt by students to TV specifications, have been used for the college's 2P23 image orthicon cameras and estimated-100-watt-output transmitter. Completion is scheduled for June, 1949.

TV broadcasts are not the goal, although an experimental wired-TV show was produced in April, 1948. Trained technicians, scarce anywhere and especially in the West, are the school's product. About 20 per year are being turned out.

Some major components, such as the image orthicon tube, were bought commercially. The all-important tube was received in November, 1947, and the first experimental picture was produced a month later.

Shiflett's three-year course covers radio, electronics, and TV construction. Radio mathematics through calculus covers most of the book work.

In the third year, actual construction is undertaken. The experimental camera and transmitter are used for this purpose.

The gamble taken in attempting high-fidelity construction out of surplus materials has panned out. In April, 1948, the experimental camera produced a picture deemed the equal of that produced by most commercial stations now operating on the West Coast. Immediate construction of the operating station resulted. A thousand TV-hungry Westerners saw the one experimental showing.

The camera and assorted circuits—the sync board, shapers, and control amplifiers—were the first units built. A piece of cavity tuner was used as a window to hold the lens of the tube. Mounting and tripods for the cameras came out of radar sets. All camera-tube sockets and about 120 potentiometers were surplus. About 80% of tubes used were surplus, including high-gain 6AC7's and 6AG5's.

Resistors, capacitors, co-axial lines, and other shielded couplings all came from two carloads of "junk" received in 1945 and 1946 for no more money than freight cost.

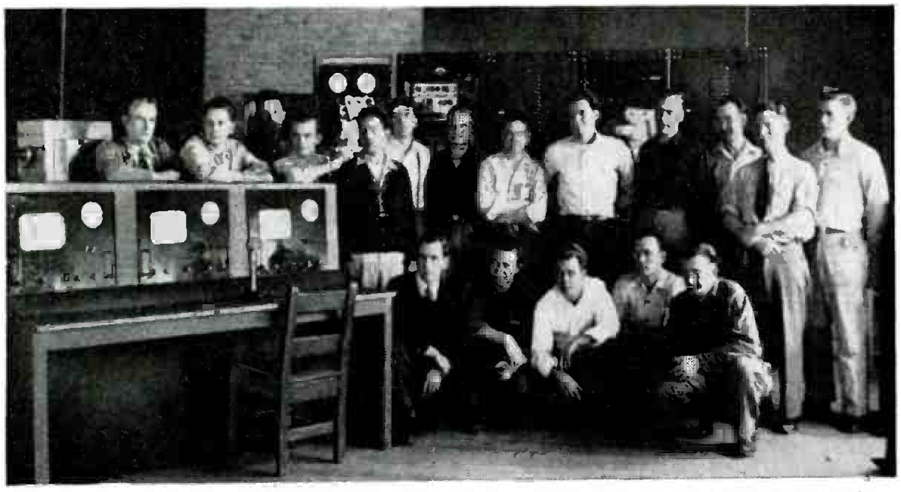
Timers, furnishing the six major pulses for control of all equipment, are completely GI, except for the chassis. Coils for broadband amplifiers were wound from what was at one time radar gear.

The shaper cost nothing except hours of hard work. Pulses do not vary over six parts in a million in width, or over six-millionth of a second in timing. Special oscillograph circuits were built to check pulses.

Rebuilt oscillator sections of the BC-688-A receiver, BC-689-A transmitter and other 500-mc gear form a good part of the video and sound transmitters.

Although present students are all veterans, the course will be open in 1949 to others. Shiflett thinks his successful experiment in salvage, science, and human relations shows that the war wasn't a complete loss.

William Shiflett, designer of the station, runs tests on the three-unit monitoring table.



Graduating electronics students at Idaho State College shown with the equipment they built.

Experimental TV Relay

Enthusiasts organize to help televiewers

LANCASTER, Pennsylvania, is only 65 miles from Philadelphia. But it is in a valley with a range of hills (the Welsh Mountains) between it and the city. What would be a "fringe area" is thus almost a "null area" because of these hills, and the few experimenters who purchased televisers and erected tall antennas reported the situation to be absolutely hopeless.

But the television experimenters refused to give up and sit quietly waiting for television to come to Lancaster. They went out and got it. Reception from Philadelphia is excellent on the Welsh Mountains. Television enthusiasts began to wonder about bending the rays from Philadelphia's television stations over the mountains and down into Lancaster.

Lancaster has plenty of television enthusiasts. One of the large plants of Radio Corporation of America is located there, and the town has a very high percentage of radio engineers and technicians in its population. A group of them met in April, 1945, to "find ways and means to bring television to the homes of Lancaster." They decided that a relay station on the Welsh Mountains, 15 miles away might be the best answer.

Inquiries showed that Philadelphia television stations would grant permission to relay their programs. The group of enthusiasts organized the Conestoga Television Association in September, 1945, and have worked steadily ever since "to bring television to the homes of Lancaster."

Result of the effort is experimental television station W3XBR, shown on our cover this month. During the winter of 1948-49 it made programs available on a more or less regular basis four nights a week. Quality of picture is usually equal to that in the best receiving locations, stability is excellent and there is little or no trouble from "snow" or man-made noise.

All work has been done on a strictly amateur basis. Members of the Association take turns in operating the station. But the Conestoga group do not use the word "amateur" in describing their activities. They point out that the word has a very definite meaning in the radio world, and that they are not hams, nor is their station licensed for operation on an amateur frequency. W3XBR is an experimental station, and the members who operate it have commercial licenses.

R. E. Barrett of the Conestoga Television Association at the W3XBR controls.

Transmitting equipment

The video transmitter operating on 600 mc uses four 2C43 10-watt lighthouse triodes, two in the oscillator and two in the final amplifier. The output is about 7 watts. The tubes are connected in a tuned-line circuit as shown in Figs. 1, 2, and 3. The lines are resonated by the shorting bars which slide along the plate and cathode lines. In addition, small split-stator capacitors, consisting of plates mounted on a shaft so they may be moved toward or away from the plate lines, act as vernier tuners on both the oscillator and the amplifier stages.

Oscillator and amplifier are identical with the exception of the oscillator feedback stubs, which extend from the cathode toward the grid of each oscillator tube through the copper chassis, which acts as a shield. Fig. 2 is a plan of the oscillator and Fig. 3 one of the amplifier. Thus the stubs appear in Fig. 2 only.

A number of modulation systems were tried. The transmitter was first grid-modulated with a low-power, 4-tube modulator which used receiving-type tubes and which connected to point B in Fig. 1. Modulation was about 50%. To approach 100% modulation, a much more ambitious circuit had to be designed. The present modulator has 5 stages feeding a power stage which consists of six 4E27/8001's in parallel. Their output goes to point A in Fig. 1. The circuits of the modulation amplifier appear in Fig. 4, and one of the six identical parallel sections of the modu-

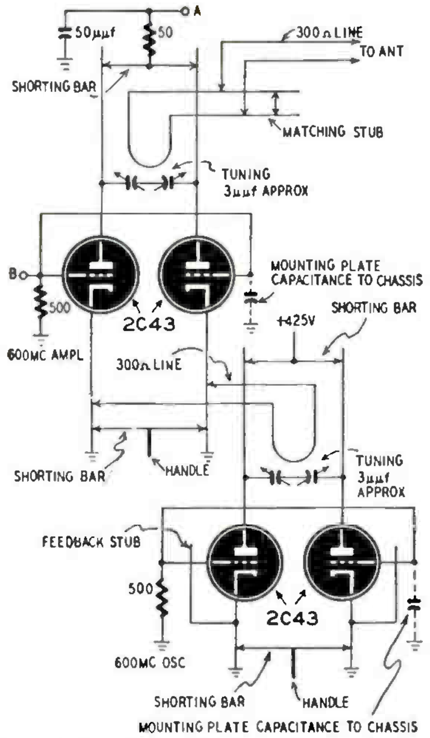


Fig. 1—Video transmitter uses four 2C43's.

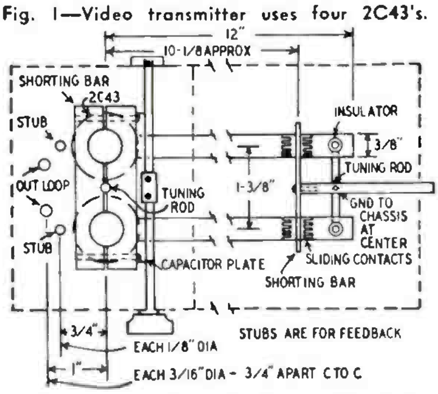


Fig. 2—Drawing shows oscillator construction.

lator final amplifier is shown in Fig. 5.

The sound transmitter is identical to the video transmitter illustrated in Fig. 1, having been originally constructed as the standby unit. In the earlier experimental stages, AM was used, but the modulation now follows standard television practice—frequency modulation with the sound r.f. at the standard frequency separation from the video signal. The sound transmitter is completely independent and has its own antenna.

Receiver converters

But getting the signals into Lancaster was only half the story. The 600-mc frequency for which the station was licensed had to be converted to one that could be picked up by a standard television receiver. This problem was solved with the experimenter's standby, surplus equipment. The former Navy radar receiver ASB-6 was adapted for the job. This versatile unit can be made into a converter that will either work from the u.h.f. band down to Channel 2, or will produce video signals directly with its own detector.

First stage of the converter (Fig. 6) is a 2C40 lighthouse tube. It feeds into an oscillator-mixer stage consisting of a pair of 955's, which brings the signal to 54 mc for the first i.f. section. This consists of two stages, and the 54-mc signal from it can be coupled into the antenna circuit of a standard TV receiver, whose Channel 2 circuits may have to be retuned slightly for best possible performance.

Better results can be obtained by heterodyning again and amplifying through another two i.f. stages at 16 mc, which in the ASB-6 is followed by a detector and one video stage. Since the converter problem has been solved by each member of the Association in his

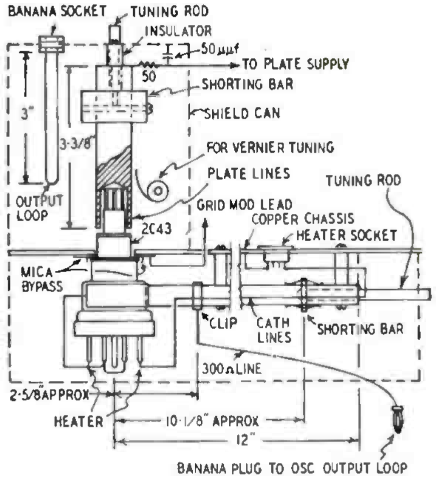


Fig. 3—A side elevation of the final stage.

own way, both of the systems mentioned in addition to a few variations are in use.

Antenna system

The mast which decorates this month's cover is a 65-foot tower originally built for experimental work by a windmill company. Receiving antennas increase the height another 13 feet, making 78 feet overall. Each receiving array is a pair of stacked Taco dipoles, one being

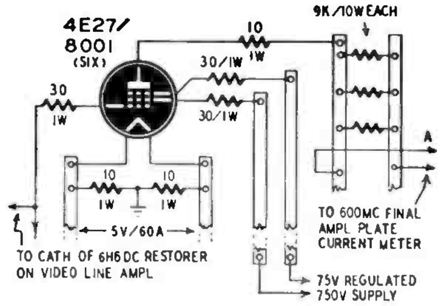


Fig. 5—Modulator has six parallel 8001 tubes.

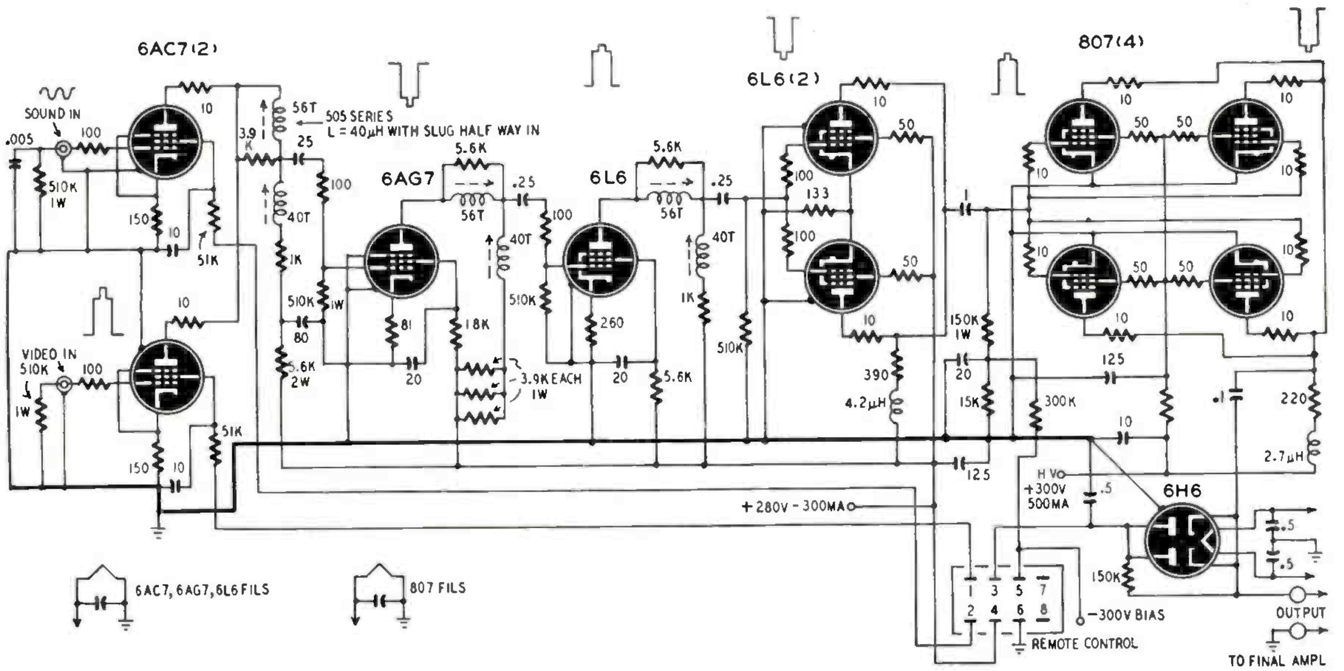


Fig. 4—A simple modulation circuit was tried at first but it was found that a more elaborate job was needed. This is the line amplifier.

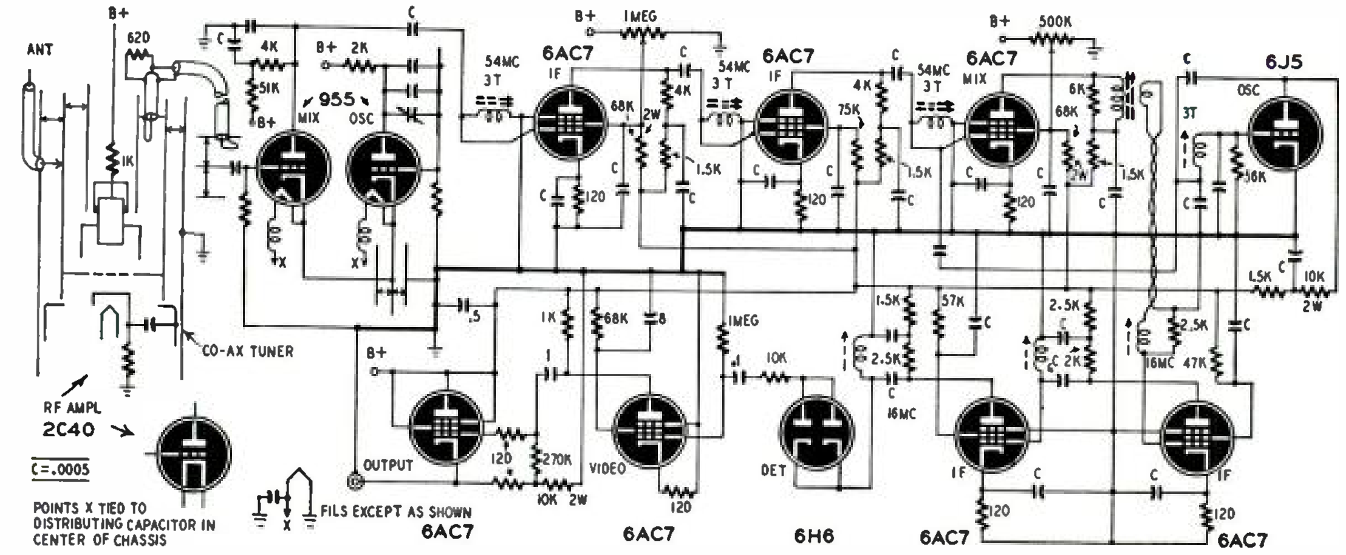


Fig. 6—A surplus ASB-6 radar receiver is used by most viewers to convert the 600-mc signal of W3XBR to one suitable for the TV receiver.

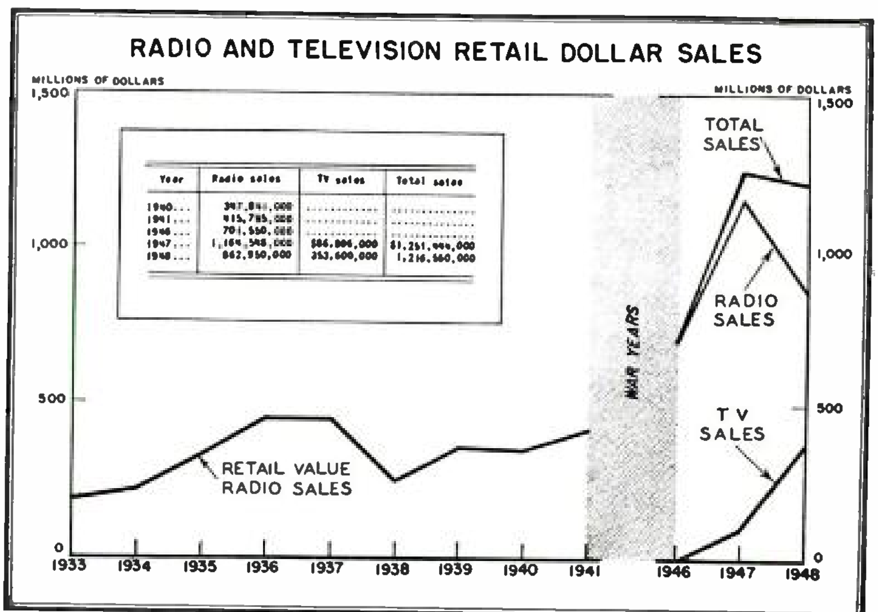
used for reception from WPTZ and one for WCAU. The two corner reflectors immediately below were originally for the sound and vision transmitting antennas. Now the video channel is transmitted from the large parabola below the reflectors, while four stacked vertical dipoles in one of the reflectors transmit the audio channel.

The television situation in Lancaster is a triumph of organized effort. Though any person who desires to receive the signals could do so simply by constructing a converter, without taking on the burdens of membership in the Association, there are no "pirates" and every televiewer is an active worker in the organization, doing such duties as his qualifications permit. The encouragement of outside organizations, notably the television stations in Philadelphia who permitted their programs to be relayed, and RCA in Lancaster, who loaned the new station much necessary material which might have been too costly to buy, also played an important part.

Lancaster expects a local commercial television station whose programs will probably start in June. How the long-distance relay will be affected is not known, but Association members are looking forward to the changed situation with interest. Will members who have been accustomed to receiving two stations be content with the single home-town program? And will the operators who have been spending their evenings on Welsh Mountain feel it worth while to continue to do so if television programs are otherwise available? Will W3XBR continue, cease, or change its form of operation? No one knows the answers, but all members of the Conestoga Television Association agree that the work up to the present has already paid off in satisfaction over a job well done, and in television training that could not have been so well obtained in any other, less practical way.

TV SALES TO REACH NEW HIGH IN 1949

TV RECEIVER SALES may bring as much income to radio manufacturers as sales of sound sets in 1949, according to a report released last month by the U. S. Department of Commerce. Written by James B. Forman and Charles P. Redick of the Department and entitled "Trends and Prospects in Radio and Television Receivers," the report relates that TV retail dollar volume amounted to less than 7% of total industry sales in 1947, but jumped to 30% in 1948. If the industry's objective of producing two million TV receivers in 1949 is realized, say the authors, the decline of radio sales and the growth of the television market may well cause a meeting or even crossing of the radio and TV lines on the sales chart shown. Aggregate sales of radio and TV receivers in 1949 is expected to approach the $1.2 billion reached in 1948, despite the approach to saturation in table-model radio receivers and the slump in radio-phonograph combinations caused by confusion over phonograph records.



Dept. of Commerce Chart. Source: Electrical Merchandising

The increase in the number of TV set makers is very marked. Before the war only one company was manufacturing televiewers; forty were in the business (or preparing to enter) in mid-1946 and 76 in mid-1948, all but 18 of whom are also active in radio.

Antennas For Television*

Part V—Higher gain and more directive patterns may be obtained by using parasitic arrays and stacking the elements

By
EDWARD M. NOLL
and
MATT MANDL†

THE presence of additional antenna elements increases the gain of simple and folded dipoles. Not only can the antenna system be made more sensitive in the direction of the station but also less sensitive in other directions, reducing the effects of noise and multipath signals. The poor sensitivity to waves arriving at odd angles improves the signal-to-noise and signal-to-interference ratios. It is important to realize, however, that the benefit of a higher-gain antenna can be realized only if antenna is properly matched to transmission line, transmission line matched to receiver (and of proper over-all length), and antenna positioned in the maximum field intensity of a space loop (see Part III, March issue).

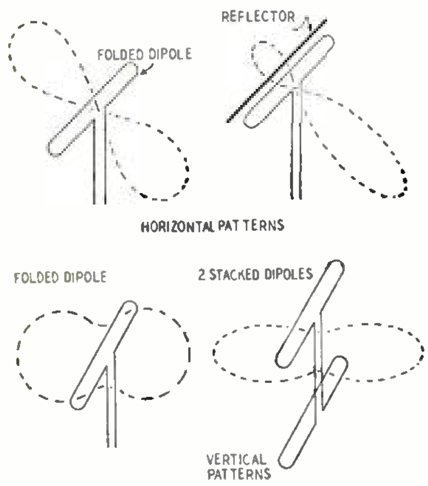


Fig. 1—Vertical and horizontal directivity.

Two factors which determine the gain and effectiveness of a directional antenna are horizontal and vertical directivity. Additional antenna elements, reflectors and directors, behind and in front of the dipole cause improved sensitivity in a given direction. There is less sensitivity to signals which arrive from other angles.

Limited improvement can also be obtained with elements positioned above each other. These so-called *stacked elements* determine the vertical directivity of the antenna system. Vertical and horizontal directivity patterns are shown in Fig. 1.

The vertical directivity of TV receiving-antenna systems should be practically parallel to the earth because television and FM waves are propagated as nearly parallel to earth as possible. The stacked system reduces the sensitivity of the antenna to noises which arrive from beneath the antenna. Thus the stacked antenna is, not only a bit more sensitive in the direction of the station, but assists in the rejection of high-angle radiation from below.

Parasitic elements

A properly matched dipole or folded dipole intercepts a specific section of the propagated wavefront and therefore receives a definite amount of energy. If the antenna has a resistive termination equal to its own radiation resistance, maximum energy will be transferred from it to the receiver. When the antenna is ideally matched, half of the total power intercepted is transferred to the load while the second half is re-radiated from the antenna.

Another antenna element is often introduced to intercept this re-radiated energy. This parasitic element, if spaced properly with respect to the driven element, transfers additional energy to the driven element in proper phase to reinforce the initial power intercepted. Under ideal conditions the presence of a driven element plus either a director or reflector increases signal intensity from 50% to 100%. The additional gain depends on the length of the parasitic element and a correct impedance match between the transmission line and the driven antenna, considering the effect of the parasitic element on the resistance of the driven antenna.

A reflector is 5% longer than the driven element and is placed a certain distance in back of it. Arriving waves strike the driven element which accepts part of the energy. A portion of the energy is re-radiated and moves on to the reflector. At the reflector there is almost complete re-radiation because the reflector is not terminated in a load; additional energy is transferred back to the driven element in the correct phase to reinforce the initial signal.

The director is shorter by 4% than the driven element and is a certain distance in front of it, that is, between the station and the antenna proper. The arriving wavefront strikes the director first. Again the combination of the arriving wavefront plus the re-radiation from the director produces an increased signal at the transmission line.

Element spacing

The spacing of the director and reflector from the driven element determines the gain and impedance of the antenna. For maximum gain it is customary to space a reflector 0.15 wavelength in back of the antenna and a director 0.1 wavelength in front of it (see Fig. 2). With this close spacing the antenna resistance is lowered substantially. When it is necessary to keep the antenna impedance relatively high, it is possible to space each parasitic element ¼ wavelength from the dipole. The gain is brought down somewhat, but reduction of impedance is not great.

Spacing	0.25λ	0.15λ	0.1λ
Reflector	82%	34%	19%
Director	71%	30%	19%
Both	41%	28%	7%

These figures show the resistance of a parasitic array as a percentage of the impedance of the dipole alone, for three different element spacings.

It is very important that the driven element be matched *exactly* to the transmission line if the full benefits of a directive antenna are to be obtained. Obviously, if multi-element arrays are to be used, a folded dipole is preferred over a straight dipole because of the much higher final resistance in the presence of parasitic elements, permitting the antenna to be matched more readily to a 300- or 75-ohm line. The resistance of a plain dipole drops to an exceedingly low value, which increases losses and complicates the matching problem. Furthermore, because of the inherently larger bandpass of a folded dipole, the array retains a substantial bandwidth despite the narrowing effects of the parasitic elements.

When a folded dipole is used, the

*From a forthcoming book: *Reference Guide For Television Antennas.*
†Television Instructors—Technical Institute, Temple University.

parasitic elements may still be simple, straight rods. They need not have the folded form. Element length is critical.

In checks made by the authors it was found that with reflector or director correctly cut (reflector 5% longer and director 4% shorter than driven element) some increase in signal strength was apparent when the parasitic element was spaced a quarter-wave, without giving consideration to impedance match. However, for the utmost improvement, the impedance match of antenna to transmission line was every

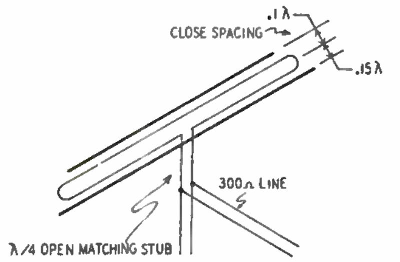


Fig. 2—Standard parasitic element spacing.

bit as important as the presence of the reflector or director.

Complete utilization of the gain added by the parasitic elements can be realized if a quarter-wave matching stub is used, as shown in Fig. 2. In this system an open quarter-wave stub is attached to the antenna and the transmission-line connections are moved up and down the stub until the peak signal point is obtained. If this method is used, a 300-ohm line can be matched to a dipole or folded dipole having one, two, or more parasitic elements. The system, of course, should be matched best for the weakest-signal frequency. A good match will then exist at the third-harmonic frequency.

In summary, the full effectiveness of the parasitic elements is obtained only with correct spacing, careful cutting of elements to correct lengths, and, above all, proper matching of the driven element to the transmission line, considering the change in antenna resistance caused by the parasitic elements.

To assist in finding the correct dimensions for the elements, and the spacings between them, a table has been compiled. It gives information for each channel as well as for compromise systems for high and low bands. Dimensions given for folded dipoles indicate the total length between one terminal and the other. Free-space dimensions for various parts of a wavelength are also given for use in obtaining proper stub lengths and spacings between elements. All of these dimensions are based on an air dielectric. When other than air is used (as in transmission through sections of line) the dimension given should be corrected by multiplying it by the velocity constant of whatever dielectric is used (see manufacturer's specifications).

Stacked arrays

If driven antenna elements are stacked vertically, antenna gain is somewhat increased because sensitivity

ANTENNA DESIGN TABLE

Channel	Center frequency	Dipole length	Reflector length	Director length	Folded dipole	Conical element	Free-Space Dimensions of Waves							Channel limits
							λ	λ/2	λ/4	0.1λ	0.15λ	3λ	10λ	
2	57	97.2	101	93.3	207	73.7	202	101	50.5	20.2	30.3	51.9	173	54–60
3	63	88	92.3	84.4	181	66.7	182.8	91.4	45.7	18.3	27.4	46.8	156	60–66
4	69	80	84.3	77	166	60.9	166.8	83.4	41.7	16.7	25	42.9	143	66–72
5	79	70	73.6	67.3	145	53.2	145.6	72.8	36.4	14.6	21.8	37.2	124	76–82
6	85	65.2	68.2	62.5	134	49.4	135.6	67.8	33.9	13.6	20.3	34.8	116	82–88
7	177	31.2	32.8	30	64.7	23.7	64.8	32.4	16.2	6.48	9.72	16.7	55.6	174–180
8	183	30.2	31.8	29	62.6	22.9	62.8	31.4	15.7	6.28	9.42	16.1	53.7	180–186
9	189	29.2	30.8	28.1	60.6	22.2	60.8	30.4	15.2	6.08	9.12	15.6	52	186–192
10	195	28.4	29.8	27.2	58.7	21.5	58.8	29.4	14.7	5.88	8.82	15.1	50.4	192–198
11	201	27.6	29	26.4	57	20.9	57.2	28.6	14.3	5.72	8.58	14.7	49	198–204
12	207	26.8	28.2	25.7	55.3	20.3	55.6	27.8	13.9	5.56	8.34	14.3	47.5	204–210
13	213	26	27.3	24.9	53.8	19.7	54	27	13.5	5.4	8.1	13.9	46.2	210–216
Low Band	71	78	81.9	74.9	161	59.1	166.3	83.2	41.6	16.1	24.2	41.7	138	
High Band	195	28.4	29.8	27.2	58.7	21.5	58.8	29.4	14.7	5.88	8.82	15.1	50.4	

All frequencies in megacycles; all dimensions in inches except 3λ and 10λ, which are in feet.

to waves traveling parallel to the earth is increased. Stacking two dipoles one-half wavelength apart increases voltage delivered to the transmission line by 40%, provided the system is properly matched. If the terminals of two driven elements are paralleled, net antenna resistance is halved.

Stacked antennas connected in phase have maximum sensitivity broadside, just as a single dipole. However, phase relation is affected by the feed system.

The two basic methods of feed are shown in Fig. 3. With the method of *a*, the signals picked up by the two dipoles are in phase, but the upper-dipole signal is reversed after it passes through the half-wave section of line. To correct this, the feeders must be transposed as shown. At *b*, signals from both dipoles travel the same distance before they meet and no correction is necessary.

A most important characteristic of the stacked antenna is its ability to reject noises arriving at other angles than broadside. For example, a signal arriving from beneath the antenna (street noises, etc.) would induce out-of-phase signals into the two elements (longer path to top antenna element) and signals would cancel at the point where the transmission line is attached. Thus the stacked antenna is particularly helpful in noisy locations.

The stacked array, in addition to contributing more gain, remains bidirectional, an advantage when reception from opposite directions is desired. Reflectors and directors can be used for each element of the stacked system, however, to make it unidirectional, with still higher gain in the chosen direction. Again proper impedance matching is essential, a matching stub doing wonders for any one stubborn station. Actually, because of the very limited additional gain acquired by stacking (only 40% for two stacked elements ideally matched), the rejection of noise should be the only reason for doing it. It was noticed that with a number of stacked systems, due to mismatch and nearness of the antenna to ground, signal strength increased when one driven element was removed. The effects of ground are evident when we consider that the nearer the stacked antenna is to ground (or to the grounded structure upon which it is mounted), the greater the ratio between signal contributed by the top element and that of the lower one.

A very simple system for approximately matching two stacked folded dipoles is the transposed-feeder method (Fig. 3-a). In a typical case, 300-ohm line was run to the lower element, connected, given a half-twist, and continued on to the top element. Spacing between the stacked elements should be 85 to 90% of a half-wave because of the velocity constant of the line. This system delivered a bit higher signal level than a center-feed system. Various element spacings—half-wave, quarter-wave, and eighth-wave—were tried with no apparent improvement.

Best results with a center-feed system (Fig. 3-b) were obtained when the

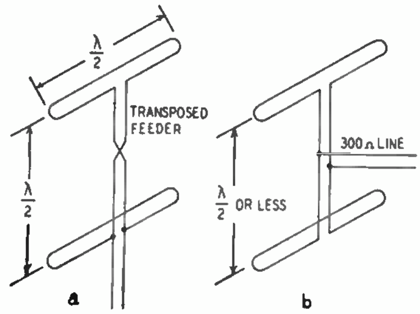


Fig. 3—Two way of joining stacked elements.

section of line between driven elements had a surge impedance which approximately matched the antenna to the center point of feed. For example, if two stacked folded dipoles are used, each has a 300-ohm resistance which should be transformed to 600 ohms at the point where the 300-ohm transmission line is attached. If the section between each antenna and the center feed point has a surge impedance of $\sqrt{300 \times 600}$ or about 420 ohms, it will act as a quarter-wave matching section. Element spacing did not appear critical from the signal-strength standpoint, although half-wave spacing gives the best noise cancellation.

In the next article of this series special antenna types will be discussed and comparisons made with conventional dipoles. An unusual high-directivity, high-gain antenna will be shown.

Electret Behavior

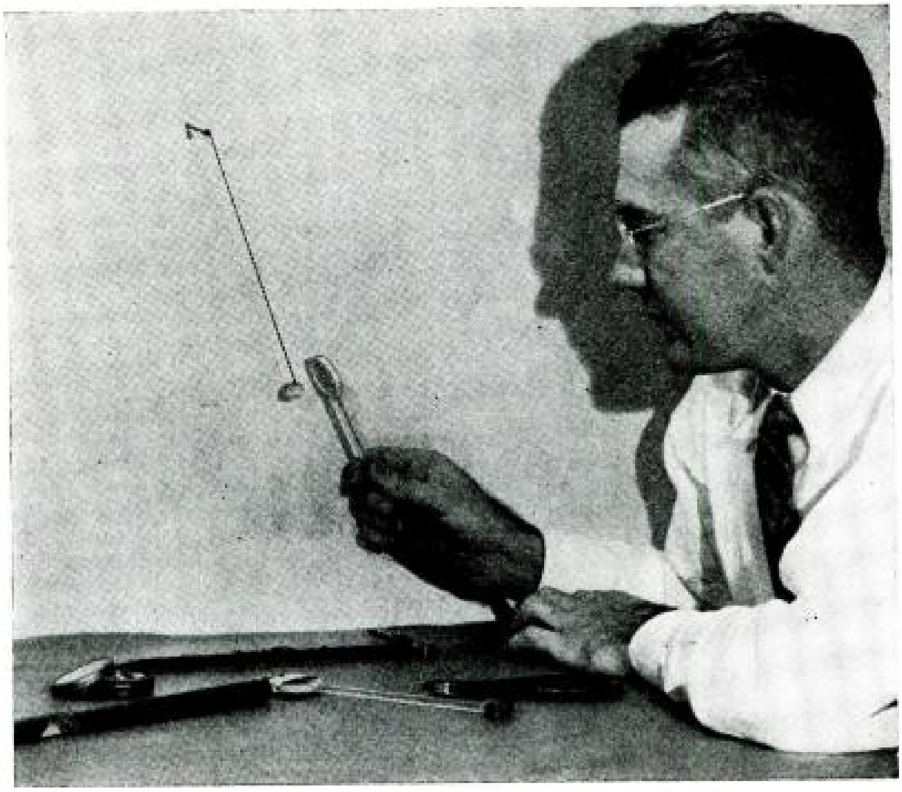
It is possible to evaluate electret behavior in spite of the dearth of theoretical knowledge prevailing

By EDWARD D. PADGETT

TO develop new industrial uses for the electret, the electronic technician should become acquainted with the properties of and the compounds that form electrets. As first shown by Mototaro Eguchi of the Higher Naval College of Tokyo, an electret is formed when certain dielectric materials solidify in a strong, externally applied electric field. The electric field causes the molecules of the dielectric to become oriented or polarized in the direction of the field. As the mixture solidifies, the polarized molecules are frozen into a fixed position. Events that occur inside the polarized dielectric cause the free charges that characterize an electret. At room temperature one electret surface has a positive electric charge and the other surface is charged negatively. Covering the electret with a metal-foil keeper preserves the charges indefinitely.

This electric charge property is related to the polar groups (—OH, —COOH) that occur in certain high-melting-point compounds. (Polar groups are groups of atoms with positive and negative electrical poles.) Mixtures of Carnauba wax and hydrogenated rosin (Hercules Staybelite resin) have polar groups and form electrets. Paraffin waxes have no polar groups and, in themselves, do not form electrets. However, paraffin waxes in mixture with Carnauba will form electrets because the Carnauba has polar groups.

Despite a lack of basic knowledge about the behavior of oriented polar compounds, practical information about electrets can be obtained from a number of experiments that can be made on the dielectric mixtures. Among the tests and analyses are potential-distribution curves inside the electret, x-ray diffraction patterns, cooling curves, and ammeter tests. The experimental results suggest the interesting hypothesis that the free charges on the surfaces of wax electrets are the result of *ionization* of some of the constituents in the wax. However, until new information about oriented polar compounds is available to support the experimental evidence, this hypothesis must not be regarded as a theory of electret behavior.



Edward Padgett, the author, shown experimenting with one of his electrets.

Andrew Gemant, one of the early electret workers, was the first (1935) to propose an ionization explanation. He inserted probes in the cooling Carnauba wax as an electret was being made. From the data he prepared curves of potential distribution inside the wax *versus* electrode distance (Fig. 1). He found that potential distribution was nonsymmetrical with respect to the two electrodes. The graph shows that the nonsymmetry becomes more pronounced as the wax temperature decreases. Gemant said this was due to different *ion mobilities* inside the wax; cation (positive ion) mobility was greater than anion (negative ion) mobility when the wax was in a molten or plastic condition (for wax temperatures down to 70 degrees C).

Professor Gemant hinted that this explanation might hold when the polarized dielectric was cooled to room temperature; for the solid wax he found a

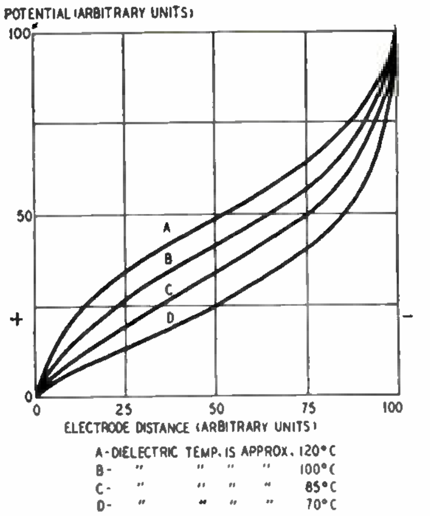


Fig. 1—Curves show potential distribution.

positive space charge at the cathode. Independent tests indicate that his explanation will hold when the wax is at room temperature. An X-ray analysis proves that when it is allowed to solidify in an externally applied electric field, Carnauba wax becomes polarized. In other words, the wax acquires an internal electric field of its own during the polarization process. When the wax is hard enough (cooled to room temperature), this internal field is retained indefinitely and can manifest itself long after the electret is removed from the making electrodes. If large enough, the internal field can ionize (or excite) certain contituents in the wax. The ions can migrate toward the polarized surfaces and form the free surface charges on the electret because of the internal field and a certain amount of ion mobility tends to manifest itself inside the wax.

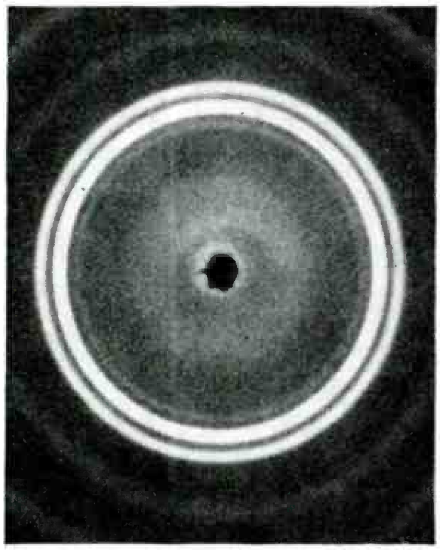


Fig. 2—Diffraction pattern of Carnauba wax.

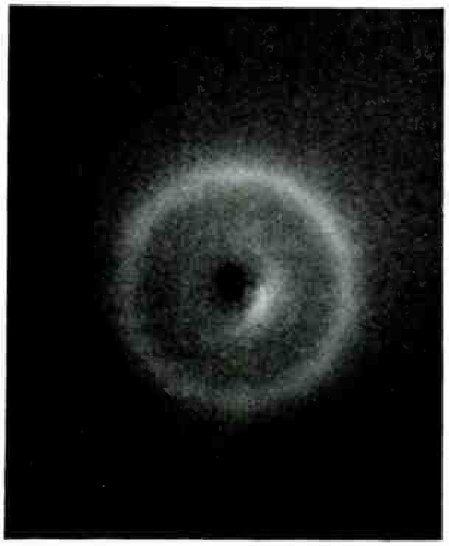


Fig. 3—Halo pattern from hydrogenated rosin.

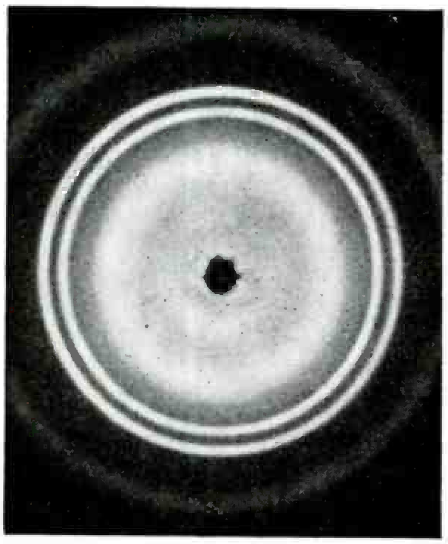


Fig. 4—Composite pattern of Figs. 2 and 3.

The electret is the electrical analog of the so-called permanent magnet. A keeper on a magnet maintains the direction of the internal magnetic field inside the iron, and the magnet keeps its pole strength indefinitely. The keeper on an electret maintains the direction of the internal electric field inside the polarized dielectric, and the electret keeps its free surface charges indefinitely. The precise mechanism of what happens inside the electret involves controversial and theoretical questions that will be answered when more information is obtained on the various phenomena involved.

If the keeper is removed from the electret, there is a reversal of the internal electric field. Experimental evidence indicates that this reversal is not instantaneous, but occurs instead in a series of jumps. This means that the decrease in the magnitude of free surface charge occurs in a series of jumps. The type of decrease indicates that there is either a rotation of the molecules, or changes in the distance between molecules or ions inside the electret. This is not a piezoelectric effect in the strict sense of the word—waxes are too soft, relatively, to show appreciable piezoelectric effects. Rather, it is an internal effect caused by oriented polar compounds. Additional knowledge about polar groups, concepts of quantum theory, and the number of degrees of freedom of atoms and molecules must be used to explain these jump effects more fully.

X-ray analysis

An externally applied electric field of between 5,000 and 10,000 volts per centimeter must be applied to the molten dielectric to produce satisfactory electrets. X-ray diffraction patterns prove the dielectric is polarized by this strong field. The patterns shown in this article were made with the k-alpha doublet from a copper-target X-ray tube operating for 20 minutes at 40 kv peak and 20 ma. The spot in the center of the pictures is due to the blocking out of the primary X-ray beam. These pin-hole patterns were taken by the writer in the X-ray laboratory of the University of Illinois.

The distance d between layers of a crystal is of the order of Angstrom units (1 A.U. = 10^{-8} cm). Since the wavelength L of X-rays is of the same order, a crystal acts on X-rays as a diffraction grating acts on light. Diffraction of X-rays is governed by the well-known Bragg equation, $nL = (2d)(\sin\theta)$. If a substance has a definite, repeating crystalline structure, X-rays will be diffracted in certain directions only, resulting in an X-ray pattern on a photographic film that is characteristic of the structure or substance. Organic compounds like Carnauba wax yield diffraction patterns that are clearly defined, smooth rings (Fig. 2). If the crystallites of a substance are very small and distributed in a random, nonrepeating manner, the X-rays will be scattered in all directions, resulting in diffraction patterns that are broad, diffuse halos. Compounds like glass and hydrogenated rosin yield these broad halos. Fig. 3 shows a halo from hydrogenated rosin. Note how it conforms to the description.

Any substance can be identified or "fingerprinted" by X-rays because it has its own characteristic diffraction pattern. If two substances are mixed together and there is a chemical reaction, an X-ray diffraction pattern will show new rings or lines because of the new compound formed by the reaction. Unpolarized *mixtures* of Carnauba wax and hydrogenated rosin show no new rings, hence, no chemical change is caused by mixing these two substances together. X-rays prove that mixtures of Carnauba wax and hydrogenated rosin

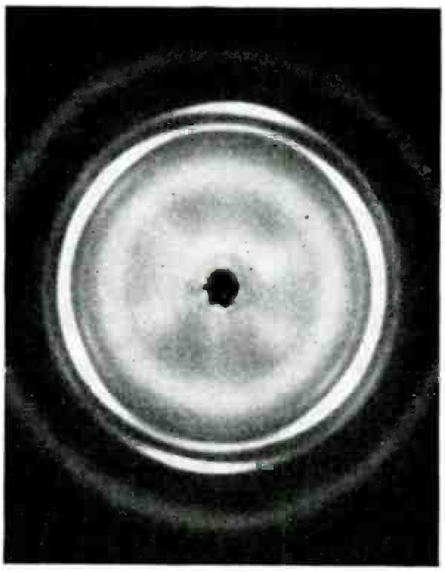


Fig. 5—Diffraction pattern of an electret.

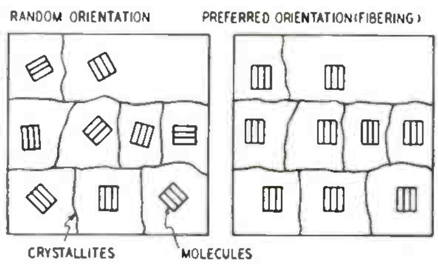


Fig. 6—Schematic illustration of fibering.

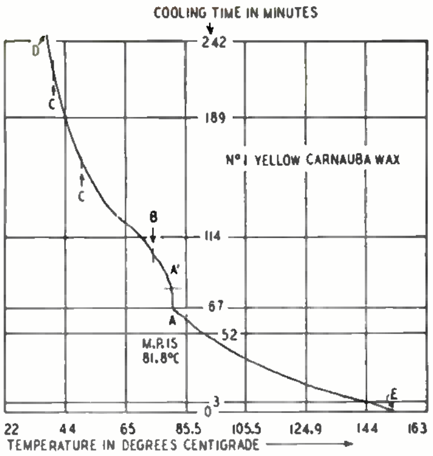


Fig. 7—Cooling characteristic of Carnauba.

are *physical mixtures*, not a new chemical compound. The diffraction pattern of the mixture merely shows a superpositioning of the individual patterns of the two substances. If Fig. 3 were added to Fig. 2, the resulting pattern would be identical to the diffraction pattern of the mixture (Fig. 4). In this photograph note the uniform photographic density of the closely spaced rings and the broad inner halo.

Fig. 5 is a diffraction pattern of an electret. Note the nonuniform photographic density of the rings and the broad inner halo. Such diffraction rings are characteristic of materials that show "preferred orientation" or fibering. In this instance the fibering is due to the polarization or orientation of the dielectric caused by the previously applied electric field from the power supply. Fibering means that an electret has a higher degree of orientation or organization than the unpolarized dielectric. Fig. 6 is a schematic illustration of fibering.

Other electret tests

In addition to the knowledge from the X-ray analysis, further information about electrets can be obtained from *cooling curves* of the dielectric mixtures. A copper-constantin thermocouple is inserted in the molten dielectric in a test tube. The thermocouple is connected to a recording potentiometer. The pen of this instrument draws cooling curves which show the time *versus* temperature relationships as the dielectric cools. (Discussions of the equipment used in testing electrets and photographs of the Leeds and Northrup recording potentiometer appeared in the April issue.)

Carnauba wax is crystalline in structure and is a unique solid solution of a homologous series of esters. Esters can have one or more *crystal transition* states. This means that at a certain temperature all the wax molecules are lined up in a certain direction and at a certain angle with respect to the vertical. In the region of the melting point the molecules line up vertically, like the pile in a rug. A change in crystal transition means that at a certain temperature all the molecules suddenly tip over at an angle with respect to the vertical. In the tipping over process heat energy is lost by the molecules. The energy loss is detected by the thermocouple and causes slight dips or bulges in the cooling curves. Thus point B in Figs. 7 and 8 is the center of a region of *crystal transition*. To see the bulges clearly, hold the paper parallel to the eye and sight along the curve. Irregular points like C on the graphs are due to the adjustment of the recording potentiometer.

When No. 1 yellow Carnauba wax cools in an oven, the curve of Fig. 7 is obtained. As the wax cools, it goes from a molten state (above 81.8 degrees C) through a vertical inflection point at 81.8 degrees (point A on the graph) into plastic and solid states (below 81.8 degrees C). In other words, from E to A on the cooling curve the wax is molten. At point A the wax cools through its melting point and begins to


This test tube was cracked when Carnauba wax was cooled in intense electric field.

solidify. At A' most of the wax is in a soft, plastic state. From A' to D the wax cools to solidification.

When Carnauba wax cools in an electric field, the curve is similar to that of Fig. 7 except for one important difference. This difference is that there is a slight lowering of the melting point of the wax. The electric field causes either preferred orientation of the wax or ionization of some of the constituents in the wax or both. In either case the wax takes energy from the applied electric field. Energy is taken gradually and in the melting point and crystal transition regions. This latter effect shows on a cooling curve only when the applied voltage is slightly greater than the breakdown strength of the dielectric. In this event arc-overs occur between the parallel-plate electrodes in the test tube. The voltage breakdowns in the wax occur with almost explosive noise and violence when the temperature of the cooling wax, as indicated by the lines drawn by the potentiometer pen, passes into the melting-point and crystal-transition regions. A test tube containing a thermocouple, brass electrodes, and Carnauba wax cracked by the application of the intense electric field during these tricky tests is shown in a photograph.

When Hercules hydrogenated rosin (Staybelite resin) is added to the Carnauba wax, the melting point of the mixture is lower. Also, the center of the crystal transition region (point B in the graphs) is at a lower temperature. This is shown in the cooling curve of a mixture of equal parts of Carnauba wax and hydrogenated rosin (Fig. 8).

Ammeter tests on wax electrets give useful information. Interestingly enough, pure hydrocarbons are essentially nonconductors of electricity in the molten state. A microammeter in the high-voltage circuit, when making an electret, shows currents of surprisingly large magnitude (approximately 400 microamperes or greater when the wax is at 90 degrees C). The specific resistance of Carnauba wax (considered as a mixture of hydrocarbon derivatives) is approximately 60×10^{13} ohm-centimeters at 30 degrees C. According to Ohm's law, currents measurable in micromicroamperes should flow through the dielectric. In practice, microamperes are observed. The large currents are due either to strong polar properties or to ionization of some of the wax components. These components are mixtures of esters of higher alcohols and acids, and impurities, such as inorganic salts, that are inherent in the wax. Undoubtedly, the ion currents contribute to the magnitude of the free surface charges on wax electrets.

In summation, then, a series of independent tests indicates that the electric charges on wax electrets are associated with the orientation of polar groups that occur in certain compounds. Unpolarized mixtures of Carnauba wax and hydrogenated rosin are physical mixtures. X-ray diffraction patterns prove that wax electrets consist of certain polarized dielectric materials.

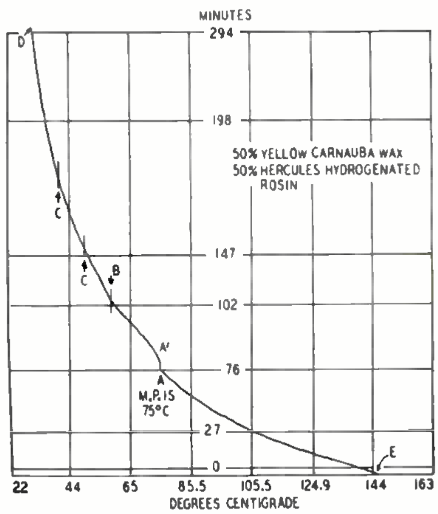
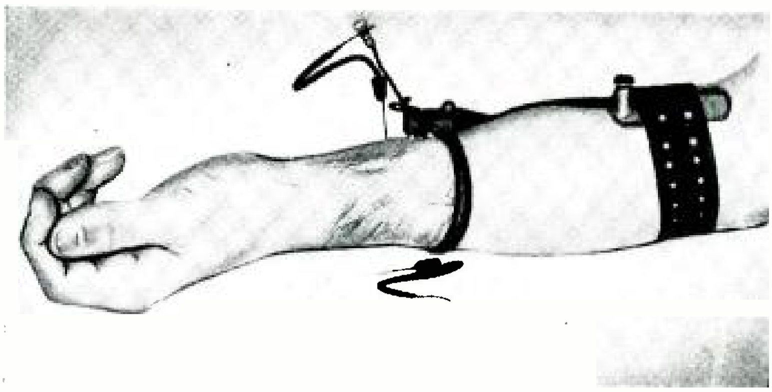


Fig. 8—How a Carnauba-rosin mixture cools.

ELECTRONICS IN MEDICINE



The insulated metallic needle is thrust into the arm. The bare tip picks up impulses.

Part VII—Devices to measure the activity of the muscle fibers

By EUGENE J. THOMPSON

ELECTROMYOGRAPHY is an electronic method of recording the electrical activity of muscles. Developed during the last war to study nerve injuries, it is now used to study diseases such as infantile paralysis.

The action potentials are picked up with a fine, metallic needle, thrust through the skin and into the muscle as in Fig. 1. The shaft of the needle is insulated, only the extreme tip remaining bare. This makes it possible to contact individual muscle fibers or collections of fibers known as a motor unit, which are controlled by only one nerve fiber.

The action potentials are measured with respect to a reference electrode placed on the skin nearby. A third, grounded electrode is attached to a distant, neutral part of the body to reduce stray electrical interference. The needle and reference electrode are connected to the input grids of a push-pull amplifier.

The action potentials are then amplified sufficiently to be seen or photographed with an oscilloscope and camera attachment and to be heard on a loudspeaker. The appearance and sound of the waveforms can be analyzed by an experienced electromyographer.

Individual muscle fibers emit small monophasic and diphasic transient discharges lasting 1 to 1.5 milliseconds at .01 to 0.3 millivolt. They appear in trains when the nerve supply to a muscle is destroyed, and have a crackling sound when heard on the speaker.

Motor-unit potentials last 5 to 7 milliseconds, range between 1 and 10 millivolts, and are di- or triphasic. A combination of motor units discharging simultaneously may produce amplitudes of 30 to 40 mv. Motor-unit potentials appear only when the muscle contracts, with a few exceptions. They sound like machine-gun fire.

The electromyograph recorder is composed of three major components:

1. A high-gain, low-noise-level, wide-range, calibrated, balanced, push-pull preamplifier, with built-in calibrator (Fig. 2);

2. A cathode-ray oscilloscope with photographic attachment, incorporating a nerve and muscle stimulator with variable duration and intensity (Fig. 3);

3. A combination mobile loudspeaker cabinet and table including the speaker, power amplifier, battery, and battery charger.

The preamplifier (Fig. 2) comprises three stages of push-pull, resistance-capacitance coupled voltage amplification. The advantages of the push-pull circuit in medical electronic equipment have been discussed in earlier articles. It is possible to obtain linear amplification of all input voltages between 10 microvolts and 100 millivolts by means of the balanced, tandem, 10-step attenuators R7, R8, R13, R14. Each attenuator has a loss of 3 db per step, making a total of 6 db per step for both stages. The frequency response is flat ±1.5 db from 10 to 4,000 cycles. The time constant is 0.1 second.

Extraneous electrical intereference is

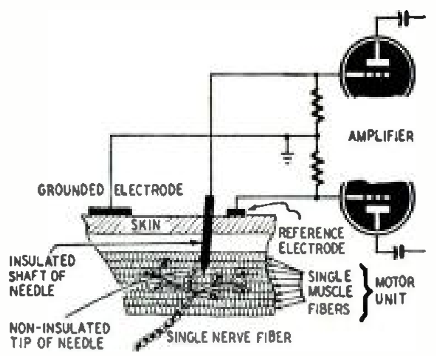


Fig. 1—Bare needle tip touches muscle fiber.

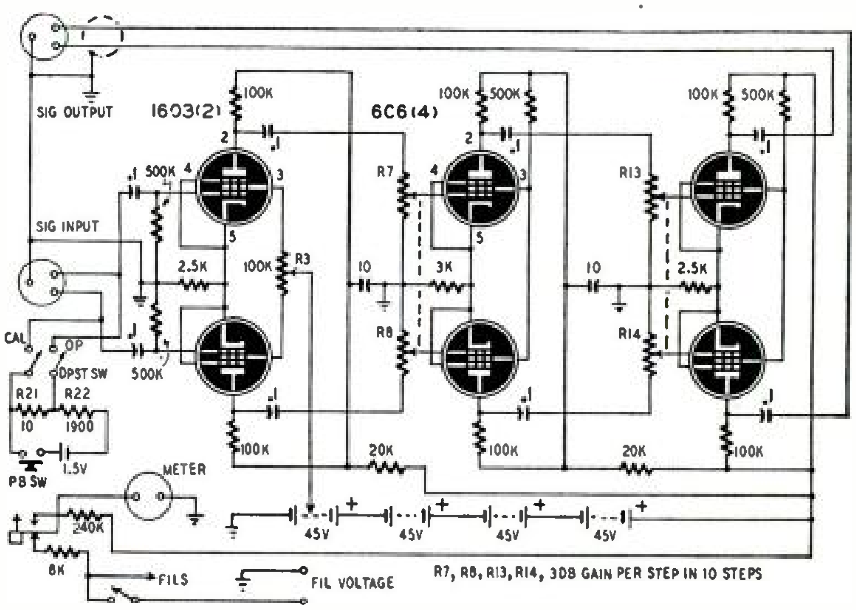


Fig. 2—This high-gain, low-noise, wide-range amplifier magnifies muscle action potentials.

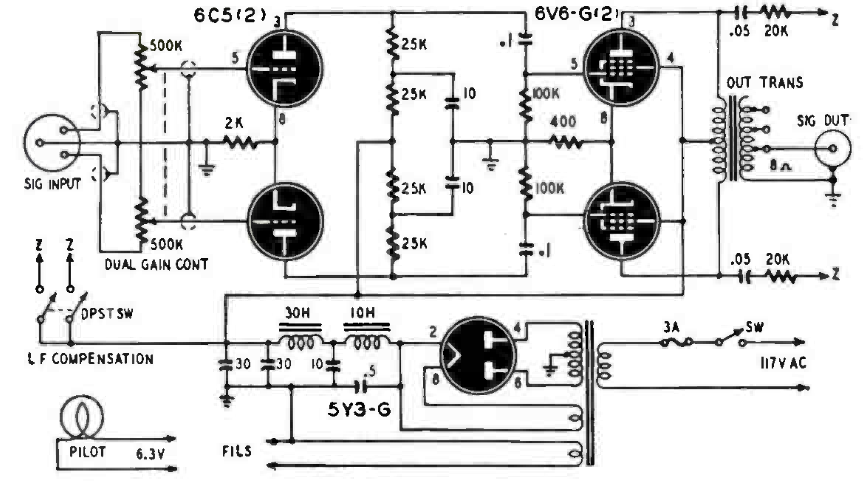
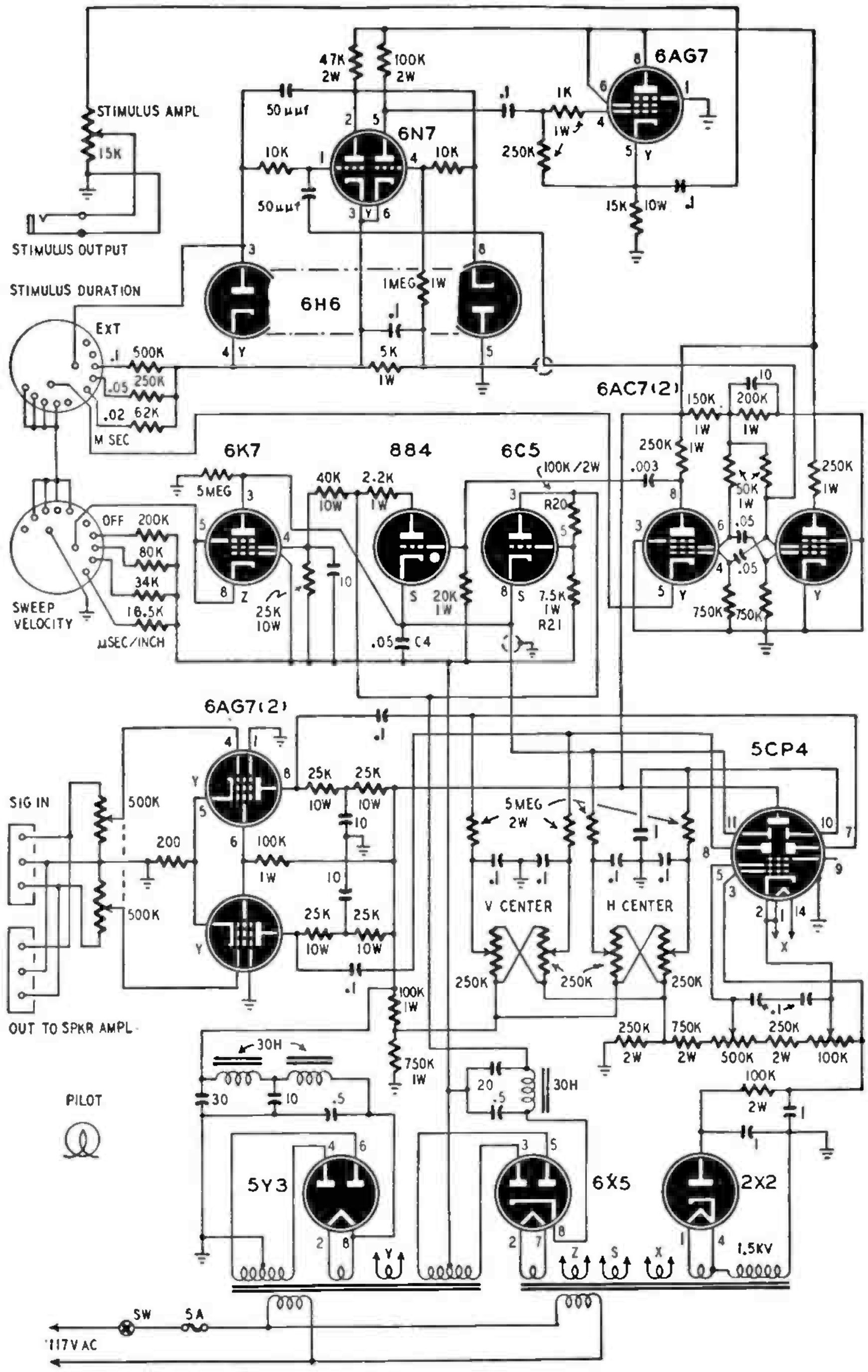


Fig. 4—The power amplifier. Listening to the impulses, the physician's diagnosis is aided.



reduced without shielding by the screen-grid-balancing potentiometer R3. Inasmuch as such interference appears principally as a grid-ground signal, R3 can be varied to make the undesirable signals of equal amplitude. Since they are already 180 degrees out of phase, they cancel. Mechanical tube noises are reduced by using 1603's (non-microphonic 6C6's) in the first stage. These are mounted in rubber-cushioned ceramic sockets. Precision wire-wound resistors in the first stage plus careful shielding reduce inherent noise still further.

The calibrator circuit consists of a 1.5-volt battery, R21, R22, and a push-button. When the OP-CAL switch is thrown to CAL, depressing the CAL button introduces an 0.8 mv square-wave pulse. The oscilloscope vertical gain control can then be adjusted to secure the desired deflection.

The output of the preamplifier is fed into the vertical deflection amplifier of the cathode-ray oscilloscope (Fig. 3). This consists of two 6AG7 beam-power tubes which, because of their high transconductance and high plate current, deliver a high voltage across a low plate-load impedance. This produces linear deflection, because the beam goes off the face of the 'scope before the tubes are driven past the linear portion of the characteristic curve.

The sweep generator employs an 884 thyratron, 6K7 constant-current pentode, and a 6C5 limiter. Normally, the 884 thyratron is biased to cutoff, and is prevented by the 6C5 limiter, connected in parallel with it, from flashing or conducting. However, a simple positive pulse from the multivibrator raises the grid bias of the thyratron, causing it to conduct, charging C4. This is then discharged at a linear rate through the 6K7 constant-current pentode. When the potential across C4 drops to a low value, the grid of the 6C5 limiter is driven positive with respect to the cathode (since the cathode is made more negative than the bias impressed on it by R20 and R21). As a consequence, the 6C5 conducts heavily, preventing further conduction of the thyratron until the next positive trigger pulse arrives from the multivibrator.

The multivibrator consists of two 6AC7 pentodes in which the screen grids are used as plates for the switching action. The circuit provides positive pulses for triggering the sweep generator and negative pulses to trigger the muscle and nerve-stimulator circuit. The frequency is set at 7.5 cycles.

The square-wave pulse from the appropriate plate of the multivibrator is passed through a differentiating network to produce the sharp, positive trigger pulse for the sweep generator. The negative trigger pulse is obtained from the grid of the nonconducting tube of

Fig. 3—The muscle impulses show up on this oscilloscope for visual evaluation. The same unit furnishes potentials for stimulating the nerves and muscles with currents of variable intensity in pulses of adjustable duration.

the multivibrator as its voltage suddenly swings negative.

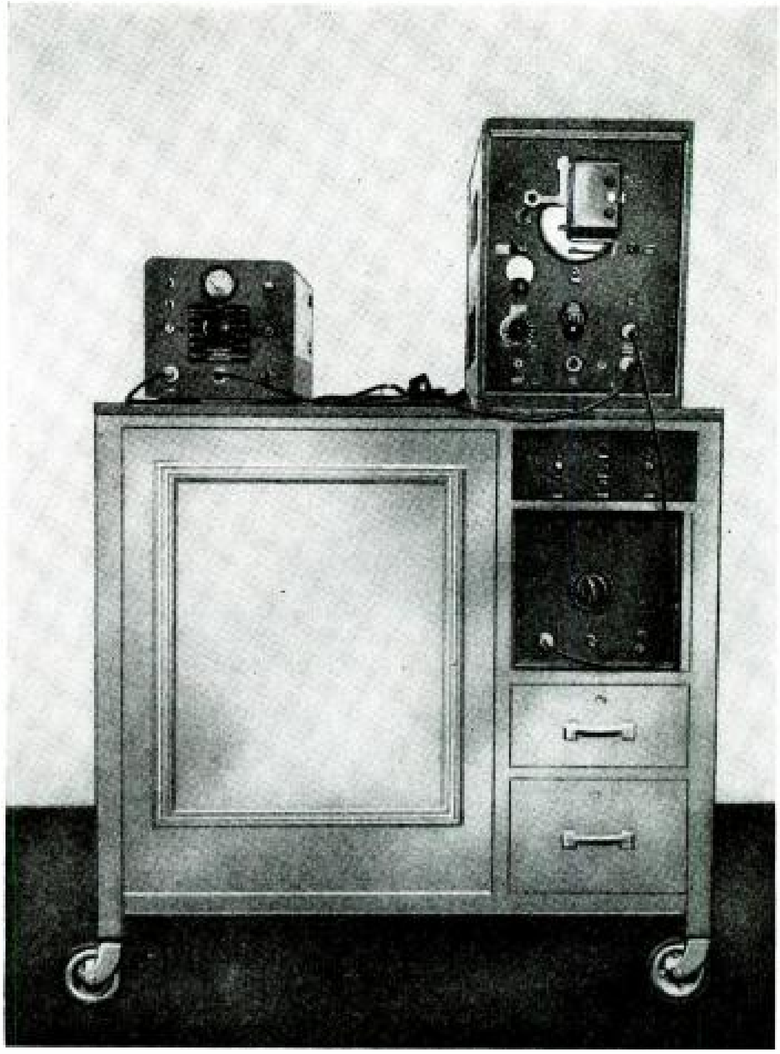
The output of the stimulator circuit is a negative square-wave pulse with a recurrence frequency of 7.5 cycles. The duration may be set at 1, 0.5, and 0.2 millisecond, and the amplitude varied from zero to —90 volts.

The stimulator is composed of a 6N7 one-shot multivibrator triggered by the negative pulse described above. The output, a negative square wave, is passed through the 6AG7 cathode follower. This arrangement minimizes distortion of the square-wave stimulus.

The 6AG7, which is normally conducting heavily, is made to conduct less by the negative square-wave input from the 6N7. The fall in current in R41 results in a negative square-wave output. The duration of the stimulus is kept constant by the 6H6 duration limiter which stabilizes the grid-voltage excursions of the two triode sections of the 6N7.

The power amplifier (Fig. 4) is a two-stage, resistance-capacitance-coupled circuit, with frequency compensation in the plate of the first stage. The output is flat from 10 to 10,000 cycles, but the lows may be accentuated and the highs attenuated by switching in the low-frequency booster. The output is 6 watts undistorted. Careful attention to power-supply design is responsible for the extremely low hum level of the instrument.

With the exception of Fig. 1, all illustrations for this article are presented by courtesy of Dr. H. H. Jasper.



This is the electromyograph diagrammed and described on the preceding pages.

NEW RADIATION DETECTOR

A new electronic scintillation counter was developed recently by Dr. George B. Collins, head of the Physics Department of the University of Rochester, N. Y.

Scintillation was the first method used by atomic physicists to count radioactive particles. Using a microscope, the scentists counted the tiny flashes of light that are made by the particles as they hit a fluorescent screen. When the Geiger counter and other detectors were invented, the scintillation method, which was extremely tedious, was dropped.

Dr. Collins, however, has made the scintillation counter completely automatic. A small block of anthracene (a coal-tar product) is placed on the end of a quartz or Lucite rod. The flashes of light produced by the anthracene when it is bombarded by radioactive particles are "piped" through the rod to a multiplier phototube which produces electrical impulses and passes them along through an appropriate amplifier to a counter.

According to Dr. Collins, scintillation counters can count faster than Geiger counters. They are more sensitive to hard gamma rays and the choice of phosphor (anthracene or other) can determine the device's relative sensitivity to alpha and beta particles. The light-conducting rod allows the phosphor to reach into tight places.

FIRST AMERICAN PORT TO GET RADAR

Though England is the world's first nation to have installed a port radar system ("Radar Eyes Bring Safety to Fog-Bound Liverpool," RADIO-ELECTRONICS, December, 1948), the U.S. will not be far behind in furnishing radar protection to marine traffic. This country's initial installation was authorized recently by the Board of Harbor Commissioners of Long Beach, Calif. Equipment for the installation will be furnished by the Sperry Gyroscope Co.

A radar scanner atop a 120-foot steel derrick at the end of a pier in Long Beach's Outer Harbor will transmit to the operator in the pilot house the position of every ship in the San Pedro Bay area within a distance of 10 miles. The radar operator will inform ships of their exact positions by two-way radio, even in the midst of the heavy fog banks which roll in from the sea. Harbor pilots will carry portable equipment for communication with the radar operator, and pilot boats will have permanent installations. With radar and the two-way radios, it will be possible to direct any vessel safely through the entrance in the breakwater system to any desired berth.

The procedure employed during bad weather will be similar to the Ground-Controlled Approach method used with aircraft. With the aid of a mobile radar station, aircraft are "talked down" in the GCA system—ground observers watching the radar 'scope know the plane's position and tell the pilot by radio every few seconds exactly what to do to maintain proper approach.

The Long Beach ship radar will operate with approximately the same procedure, except that the radar station will be fixed. Like GCA, the port radar will be accurate to within 50 feet. The shore operator will be able to act only in an advisory capacity, as all responsibility for control and direction of the ship rests with the pilot.

Because of its novelty, the system will be operated at first on an experimental basis, but it is expected to prove so vital that all major American ports will follow Long Beach's pioneer example.

Build A TRANSISTOR

Experiments show that the average experimenter can construct a crystal amplifier from parts of 1N34's

End plug at right holds the two catwhiskers.

By RUFUS P. TURNER, K6AI

SINCE the sensational announcement of the crystal triode, or transistor, several months ago, radio experimenters have been waiting impatiently for manufactured versions of this device. We have communicated with several manufacturers known or expected to be planning transistor production, but have obtained no commitments as to a date on which crystal triodes might be expected to appear on the market. In the meantime, a few brave souls have made simple experimental transistors for the prime purpose of doing a little advance playing with the gadget; most builders, however, have complained of electrical instability and lack of mechanical ruggedness.

The author has constructed several transistors employing various mechanical arrangements. Although the electrical behavior of some of the models was interesting and quite satisfactory, all suffered more or less from mechanical delicacy. In each case, the germanium wafer and the two S-shaped, pointed, tungsten whiskers required were obtained by disassembling two 1N34 crystal diodes. One whisker is obtained from each diode, and one germanium wafer is left over for experimentation. The 1N34 undoubtedly has been the source of parts for all home-made transistors built up to this time.

Without going into the theory of transistor operation in this article, we show the basic arrangement of a crystal triode as an amplifier in Fig. 1. An oscillator circuit also can be made by introducing feedback between the output and input portions of the triode circuit. From this drawing, it may be seen that the transistor is simply a two-whiskered crystal unit. The *emitter* whisker is biased with a low positive voltage and is comparable to the control grid of a triode tube. The *collector* whisker receives a much larger negative voltage from a B-battery and is comparable to the plate of a tube. The germanium wafer, commonly referred to as the *crystal*, is comparable to the cathode of a tube. In order to obtain transistor action (that is, to have the emitter voltage control the collector current in much the same fashion as the grid voltage of a tube controls the plate current), the two whiskers must touch the germanium surface firmly at points ex-

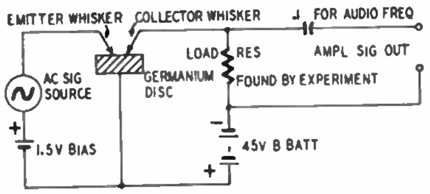


Fig. 1—This is a basic transistor amplifier.

tremely close to each other (.002-inch separation is the figure that has been published widely). The job of mounting the two whiskers as close together as this, so that their tips do not touch each other but still press down upon the germanium surface, is the formidable mechanical obstacle which most experimenters have found.

Recently, Ralph Jacobson, WØYEE, produced a mechanically rugged transistor for the author's experiments, using 1N34 parts. It is the novel, easily duplicated construction of this unit which is described here.

Construction

Fig. 2 is an exploded view, showing how the various parts of a 1N34 have been utilized in construction of the crystal triode.

The 1N34 consists of two threaded brass end plugs which are screwed into opposite ends of a small ceramic tube. The tungsten whisker is soldered to one of these plugs and rests upon the surface of the germanium wafer. The wafer is soldered to the end of a brass pin passed through a central hole in the other end plug and held by a setscrew. These parts are all shown, ready to go together, in Fig. 2. After adjustment at the factory, the ceramic tube is filled with wax. This wax has been injected through a hole in the side of the ceramic tube; this hole served previously for an access point through which the whisker could be moved about to various spots on the germanium surface during electrical adjustment.

After obtaining two 1N34's, the first step in the construction of the triode is carefully to pick out the sealing material which plugs the hole in the ceramic tube of each unit. This may be done with a needle, being cautious not to dig any deeper into the unit than the thickness of the ceramic wall. The next

Five simple tools used in making transistors.

step is slowly to melt out the wax by heating the entire unit. Hold it high over a low flame. Make no attempt to rush this operation. The wax will run out through the side hole. After the wax has been expelled, the tinned ferrules which hold the pigtails may be peeled off the end of each unit with the aid of diagonal cutters. This will expose the two brass end plugs which then may be unscrewed.

After removing the end plugs, unsolder the whiskers from their plugs and bathe them in carbon tetrachloride. The next step requires painstaking care: saw one of the whisker plugs vertically in half, using the thinnest obtainable jeweler's saw blade, to obtain the two separated halves shown as parts A and C in Fig. 2. Solder one whisker to each half. The tungsten wire is a little tricky to solder and may require acid soldering flux. If the latter is used, wash the finished job thoroughly in strong soapy water, give several rinsings in clear water, then dry the parts and bathe them in carbon tetrachloride. Next, using Duco cement, fasten the two halves of the split end together with an insulating separator (part B in Fig. 2) made from Lucite or Plexiglas 1/64 inch thick. Be careful to keep the threads of the split plug aligned. Then, with a needle, toothpick, or slender tweezers, bend the tips of the whiskers together until they have the smallest separation without actually touching each other. It will help to use both a magnifying glass and continuity meter in this operation.

Screw the two-whiskered plug back into one end of the ceramic tube, and the germanium-holding plug F into the other end. Using a magnifying glass

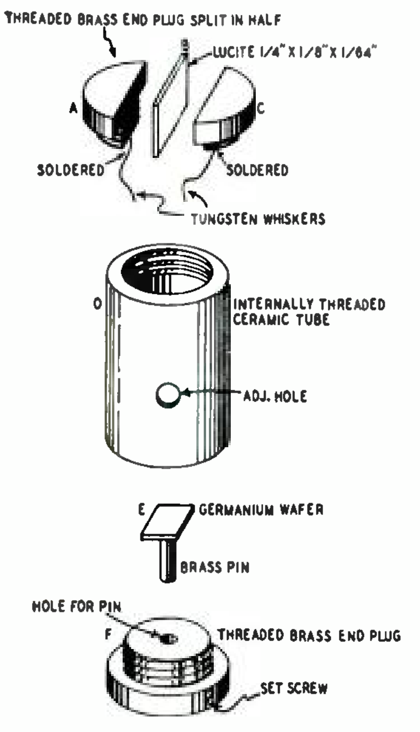


Fig. 2—Exploded view shows transistor parts.

(or the naked eye if yours is that good), look through the tube hole to see whether the whiskers are both in contact with the germanium surface and also whether threading in the germanium plug has twisted them. If the whiskers are twisted or are touching each other, separate them with a needle or toothpick inserted through the hole. If they are spread too far apart, push them closer together with the needle. If the whisker tips are not in contact with the germanium surface, loosen the setscrew in the germanium end plug and cautiously push the end of the germanium pin inward by means of a pin inserted into the center hole of the plug, until contact is made. Then retighten the setscrew.

The final step is to solder a wire pigtail lead to each half of the split whisker plug (A and C in Fig. 2) and also to the germanium plug F. The soldering operation must be completed quickly in order not to melt the solder holding the whiskers or damage the germanium wafer.

Throughout the construction, take care not to handle the germanium wafer or the whiskers with the fingers any more than is absolutely necessary. If there has been excessive handling, both the whiskers and the germanium wafer should be bathed in carbon tetrachloride or lacquer thinner.

Fig. 3 shows how the completed transistor assembly appears in cross section. Letter symbols are the same as those in Fig. 2. The photographs also show constructional details.

Adjustment

After the unit has been assembled, set up the test circuit shown in Fig. 4, and test the crystal triode according to the following procedure. Either half of the split end plug may be chosen as emitter or collector.

1. With switch S2 open, close switch S1. The emitter current, read with milliammeter M1, should not exceed 20 ma and undoubtedly will be in that neighborhood at the outset.

(The 20-ma emitter current is very much greater than the figures commonly published. These range from a fraction of a milliampere to 1 or 2 ma. Transistors made by different experimenters vary widely for reasons still unknown. The performance of transistors made by readers therefore may be entirely different from that of the one described here; the difference should be no cause for discouragement or alarm but should, instead, prove to be a strong incentive for experimentation.—*Editor*)

2. Open S1 and close S2. The collector current, read with milliammeter M2, should not exceed 0.5 ma.

3. If emitter or collector current is in excess of the values given, reverse the emitter and collector terminals and repeat steps 1 and 2. If the currents still are excessive, unscrew the germanium end plug, loosen the setscrew, and rotate the germanium pin to expose new surface points to the whiskers. Reinsert the end plug, respace the whiskers if necessary, and repeat the tests.

4. When approximately correct emitter and collector currents are obtained, label the emitter and collector terminals by marking the whisker end of the ceramic tube.

Check the transconductance of the triode in this manner:

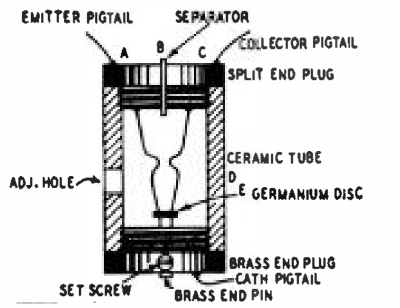


Fig. 3—Cross-section of finished transistor.

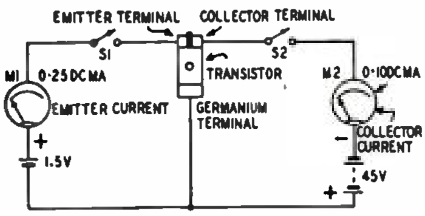


Fig. 4—Test circuit reveals characteristics.

1. Close switch S2 and record the reading of milliammeter M2 as I1.

2. Leaving S2 closed, close S1, noting the new reading of milliammeter M2. Record this second M2 deflection as I2.

3. The transconductance in micromhos is

$$\frac{1{,}000\,(I_2 - I_1)}{1.5}$$

The builder should aim for the highest transconductance he can obtain with a given germanium wafer. Magazine articles have reported transconductances as high as 15,000 micromhos. The author has found that transconductances of 1,000 to 3,000 (comparable to such tubes as the 6J5, 6SQ7, 6T7, etc.) may be obtained readily with little or no adjustment on a transistor of the type described in this article. Rotating the germanium wafer to expose better spots to the two whiskers has yielded transconductances a little higher than 5,000, but the author has not exceeded that figure.

After all adjustments are completed, the side hole in the ceramic tube should be closed with a small piece of Scotch tape. We do not recommend filling the interior of the unit with any of the waxes ordinarily available to the home experimenter.

Some question is apt to arise as to capacitance between the two halves of the split whisker plug. The author checked this and found it to be 2.45 $\mu\mu f$ in his unit at a test frequency of 1 mc. This is comparable to the grid-plate capacitance in a corresponding triode tube, smaller, in fact, than in such triodes as 6J5, 6SL7, 6SN7, etc. It should cause no trouble.

Photoflash Unit For Your Camera

A voltage-doubler saves space and weight in this useful photographer's aid

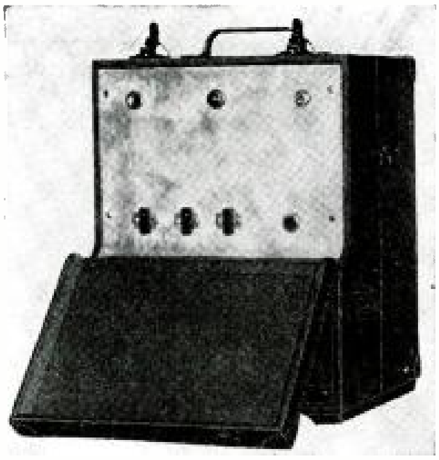
By W. C. BROWN *

SEVERAL years ago the writer built an electronic flash oufit for his own use. While it gave excellent service, it was far bigger and heavier than necessary, and as time went by the desire for a more convenient unit grew.

No small amount of thinking and innumerable paper sketches finally resulted in a mental picture of what the new unit should be like. Remembering that electronic components are almost always rated for continuous duty and that the duty cycle in electronic flash service is very low, a few rough calculations showed that components with very low ratings were ample. This reasoning even applied to capacitors, although not to the same extent as to transformers, rectifiers, and resistors.

War-surplus components are generally of excellent quality and attractively priced. But they are heavy. All the transformers listed in advertisements and having the desired secondary voltage delivered 100 ma or more. You simply don't carry such a transformer around in your pocket; and since light weight was a requirement, these transformers were ruled out. Further meditation provided more answers: If a light-weight transformer delivering 2,000 volts d.c. at the rectifier output is not available, why not voltage-double from a light-weight, lower-voltage transformer?

A capacitor connected across an unloaded d.c. circuit will charge to the full *peak* voltage across the circuit, and an *unloaded* voltage doubler will have exactly $2\sqrt{2}E_{rms}$ across its output. In a photoflash unit previously sketched out, the flashing capacitors also served as part of the voltage doubler so they would charge to twice the transformer peak secondary voltage. Using a 900-volt transformer this gives $2(1.414 \times 900) = 2{,}545$ volts.

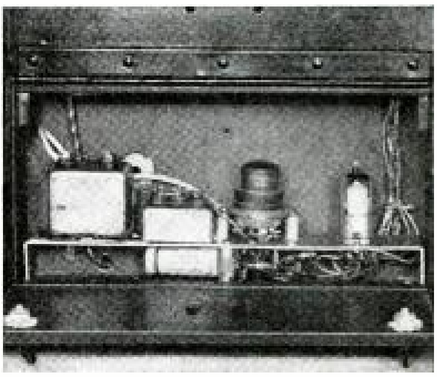


Frequency meter case contains the power supply for the flash unit. Three receptacles for flash guns are shown; the author later added two more, as the circuit diagram shows. The panel is mounted on ¾-inch spacers to make room for the energy-storage capacitors within.

Now the foregoing is true only where there is no loading on the circuit and the back-resistance of the rectifier is infinite. Neither condition applies in the unit described here; and since the back-resistance of dry-disc rectifiers is relatively low, the voltage across the capacitors in this unit turns out to be only about 2,000. But that is plenty.

If thermionic rectifiers are used, the output voltage will approach the 2,500-volt figure because of their high back-resistance. In such a case, for the welfare of the capacitors, it is suggested that a 700- or, at the most, a 750-volt transformer be used.

Having decided upon a voltage doubler, the next question was the type of rectifier to be used. After considering all the factors of weight, cost, and life, dry-disc rectifiers were selected over vacuum tubes with the necessary two filament transformers. There is very little choice, however, and two tubes (2X2's) and two filament transformers may be used in place of the dry-disc rectifiers used by the writer. It might be added that the thermionic-rectifier system will cost a little less and weigh a little more than the dry-disc type. The schematic is shown. The next problem was where to obtain the parts. The advertisements of dealers in surplus materials revealed that almost all of the needed components were listed. The writer used two 15-µf and two 10-µf capacitors wired to give two 25-µf units for the energy-storage capacitors. These fit very nicely into the case used. Subsequently, regular 24-µf photoflash capacitors were found in the surplus market. While these are made for 2,000-volt photoflash service, they have stamped on the case "24 MFD—1500 VDC Work—3000 VDC Peak." The dealers apparently feel that it would be unethical to advertise them for 2,000-volt photoflash service when they are plainly marked for 1,500 working volts. So they won't be found in the adver-



The trigger circuit installed in the lower front compartment of the case. The 6H6 was later replaced with two selenium rectifiers to give enough capacity for five flash tubes.

*Signal Corps Engineering Laboratories, Fort Monmouth, N. J.

tisements as photoflash capacitors, but they are intended for such service and will last for a long time.

The case used was intended for the BC-221 frequency meter. The canvas cover and all internal fittings and hardware except three items were removed. The angle brackets in the upper compartment for mounting the panel were left in, as was the partition separating the upper and lower compartments and the partition separating the lower compartment into two parts. The outside of the case was given a coat of flat black lacquer and waxed when dry. The result was a neat and attractive unit.

The power supply was mounted on a U-shaped chassis and fitted into the large lower compartment. This chassis contains the power transformer, the 10-µf voltage-doubler capacitor, the rectifier, the 6.3-volt transformer for all heaters and the pilot light, and a terminal strip for connection to the other chassis. The writer fastened the power transformer and the 10-µf capacitor by using a length of flexible No. 14 wire with spade bolts on each end. This makes a flexible U-clamp, and two of these for each component will hold it very firmly to the chassis. The chassis was held in by drilling and tapping 8-32 holes in the lips of the chassis and then drilling matching holes in the side of the case. Flat-head 8-32 screws were used to hold the chassis positively in place.

The trigger circuit is also mounted on a U-shaped chassis with 1-inch lips. The 2D21 was chosen instead of the 0A5 solely because of cost. The 2D21 and its filament transformer are surplus items, and together cost less than the non-surplus 0A5.

In operation this circuit is simple. The grid of the 2D21 is normally biased beyond cutoff; but when the synchronizing contacts on the camera are closed, the grid is made positive. The tube immediately fires and capacitor C discharges through the tube and the trigger transformer T in the cathode circuit. This pulse in the trigger-transformer primary induces a 12-15-kc pulse in its secondary, which is connected to the flash-tube grid, and causes the flash to fire.

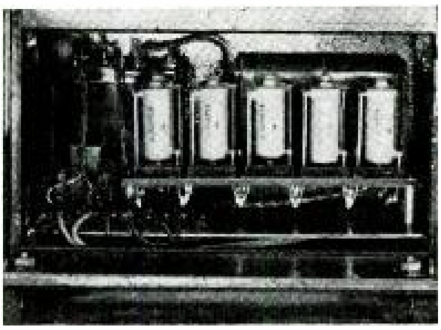
C is, of course, essential, and without it, the circuit won't work. This is due to the high IR drop that would exist across R the instant the 2D21 started to conduct. This drop would be so high that the plate voltage on the tube would immediately drop below the firing voltage when the tube started conducting. C thus provides a low-impedance power source for the 2D21 during the short period of time necessary to generate the trigger pulse. It, of course, recharges between flashes.

The trigger transformers used are model-gas-engine ignition coils. Several manufacturers are now building small transformers for this service and they will serve just as well as the small ignition coils. Shown alongside the main unit schematic is a schematic of one flash-tube unit with its wiring. The trigger transformer is mounted directly on the back of each reflector.

The plate voltage for the 2D21 could be taken from a voltage divider across the B-supply. This would load the doubler still further and lose a few more volts in the output. With 117-volt, 50-ma selenium rectifiers and electrolytic capacitors as cheap as they are, it was decided to double the 117-volt supply and provide a separate power supply for the trigger circuit. As indicated in the diagram, the trigger circuit will simultaneously fire as many as five flash tubes. The circuit is, of course, a simple voltage doubler; but remember—the selenium stacks are insulated for only approximately 130 volts, and in this circuit voltages as high as 250 appear between the rectifier plates and ground. Be sure to insulate the rectifiers from the chassis when mounting them. Small ceramic standoffs are suggested. The photograph of the trigger circuit components shows the 6H6 originally used; the selenium rectifiers were added later to increase the number of flash tubes that could be triggered.

The four units comprising the 25-µf energy-storage capacitors (which are also part of the voltage-doubling circuit) are mounted in the upper compartment of the case. We do not know whether two of the regular photoflash capacitors available as surplus will fit in, but one of them definitely will. If two will not fit, the reader can mount one or both right on the light standard. The diagram shows that while only two capacitors are in the circuit, three extra outlets are provided on the panel for remote flash lamps with their own 25-µf capacitors. This procedure eliminates the IR drop of a long lead to the flash tube and avoids the inductance and capacitance effects of a 10- or 15-foot piece of co-axial cable.

Remember that all exposed high-voltage leads should be of flexible co-axial cable. An insulation breakdown will result only in a short across the output of the unit and never endanger anyone coming in contact with the leads. All wire carrying high voltage within the unit should be made with hookup wire insulated for 5,000 volts.



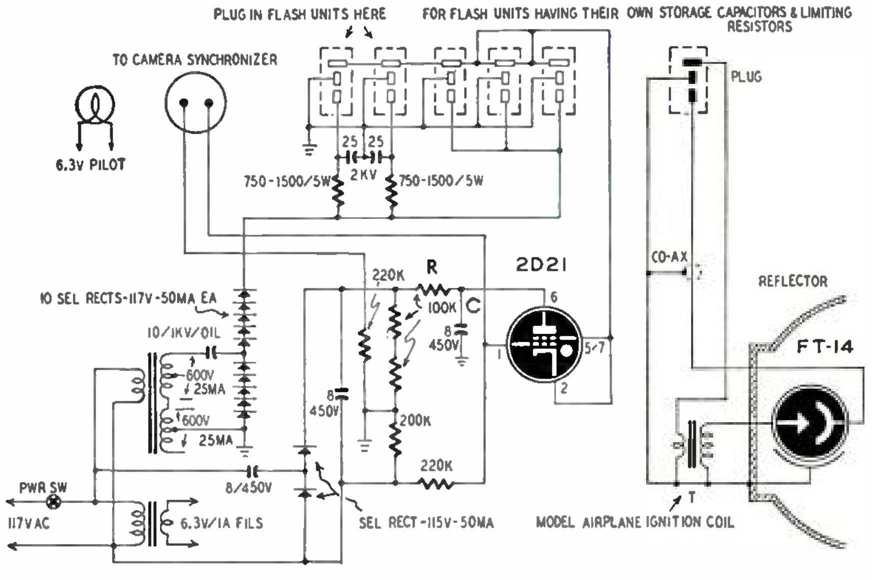
Dry-disc rectifiers in lower rear compartment.

The photographs show the completed unit in operating condition. Note that the panel is flush with the face of the top compartment. The panel-mounting brackets left in the case will recess the panel if it is mounted directly on them. With the panel recessed, there is not enough clearance between it and the capacitor bank for the panel-mounted components. Using a ⅛-inch aluminum panel, ¾-inch spacers will bring it exactly flush and provide sufficient clearance for the switch, pilot light, receptacles, and so on.

This equipment has been in use for some time, and its performance equals any seen by the writer from commercial units costing $150 to $250. It will handle five lights giving 12,000,000 peak lumens each. And the total cost is less than $30.00.

MATERIALS FOR PHOTOFLASH UNIT

Resistors: 3—100,000, 1—200,000, 2—220,000 ohms, ½ watt; 1—750-1,500 ohms, 5 watts.
Capacitors: 3—8 µf, 450 volts, electrolytic; 1—10 µf, 1 kv, oil-filled; 2—25 µf, 2 kv.
Tubes: 1—2D21, 1—6H6, 1—GE FT-14.
Transformers: 1—6.3-volt, 1-ampere; 1—900-volt, 25-ma or equivalent.
Miscellaneous: 1—model-gas-engine ignition coil; 12—117-volt, 50-ma, dry-disc or selenium rectifiers; 1-5—flash-lamp assemblies; 1—miniature 7-pin tube socket; 1—s.p.s.t. toggle switch; 3—3-connection female, polarized panel receptacles, insulated for high voltage; 1-3—male plugs to fit; 1—6.3-volt pilot-lamp assembly; 1—case; necessary hardware.



Complete schematic diagram of the flash unit. Use high-voltage cable for ignition circuits.

Telephone Lines in Broadcasting

Part II — Maintenance, attenuation, noise, and communication problems

By LEIGH L. KIMBALL*

THE first part of this article (April issue) explained methods of equalizing telephone lines used for carrying broadcast programs. The broadcast engineer must also be familiar with the techniques of measuring noise and loss on these lines and with maintenance procedures.

Line loss depends on loop makeup (sizes of wires used), equalization applied, and length. It is more easily measured than calculated. It is also affected by line terminal impedance, which may or may not be equal to the input and output impedances of the loss-measuring equipment. Therefore, a definition of line loss which takes operational mismatch into account must be used. It is as follows for 600-ohm program equipment:

The difference between the reference power level which a generator of 600 ohms internal resistance will deliver to a 600-ohm resistive load, and the level received in a 600-ohm measuring set at the line output terminals when the generator is connected to the line input terminals, is the line loss.

Note that any impedance mismatches are conveniently taken care of by such a definition. It is important to eliminate impedance mismatch as a factor in loss measurement because line terminal impedances vary widely. The arrangement used for frequency-response measurement (Fig. 2 in April article) is also ideal for loss measurement. The measuring set may simply be a calibrated amplifier used for presetting programs.

Noise

All telephone lines are subject to a certain amount of induced cross-talk interference. Cross talk may come from several sources—dial systems, teletype machines, tone and d.c. telegraph, special high-frequency ringing systems, and faulty voice circuits, to list a few. Objectionable hum on the line is usually an indication of an unbalance or a long, unterminated branch somewhere in the circuit.

Unusually long lines are, of course, especially subject to cross talk. As the audio signal travels down a long line, it may be attenuated to a relatively low level. However, the induced noise tends to remain more or less constant along the line. The result may be a small signal-to-noise ratio. To combat this situation, the highest permissible power level should always be delivered to the line. The maximum levels which have been agreed upon[1] are:

Program material ....8 VU
Sustained test tones........0 VU
400- or 500-cycle tone for program level setting..............8 VU
(VU=db above 1 mw.)

The +8-VU level for program transmission has been set as high as possible to give the broadcaster the best signal-to-noise ratio consistent with proper cross-talk protection to other services handled through the telephone exchanges.

Other solutions are available to the broadcast engineer having trouble with line noises. An audio booster or repeater amplifier may be installed at an intermediate point on the line to restore the program level before it drops down into the noise. Where the line length is not excessive, but noise is giving trouble, it may be necessary to move the radio-loop pair to another point in the telephone cable (or cables) of which it is a part. The usual practice is to move it 25 pairs away from the point where it is giving trouble.

The VI pad

An attenuation pad is not necessary between the amplifier and the line to maintain frequency response; it would have absolutely no effect on the over-all response if the pad were the same as the amplifier's internal impedance.

However, the pad *is* necessary to make the volume indicator at the line input read accurately and to provide the correct meter damping on program material. The damping factor is especially important when several V.I.'s in a system must be co-ordinated. An attenuation pad between the amplifier and line as shown in Fig. 1 will reduce V.I. error which could result from connecting the V.I. directly across the line. This is important because telephone-line terminal impedances vary over a wide range and the standard V.I. is designed to have the proper damping and power calibration when connected across an amplifier and load, both of which have an impedance of 600 ohms. The pad is also extremely important if a bridging amplifier is connected across the output of the line amplifier, as line capacitance will probably reduce the high-frequency output of the line amplifier even if the line is perfectly equalized at the far end. The capacitance effect at the sending end can be eliminated from the bridging amplifier by isolating the line by means of a 600-ohm pad. A 6-db pad usually gives sufficient isolation to make the amplifier load look like 600 ohms over the audio range, but 8 to 10 db may be desirable when equalizing by method 1 in Fig. 6 of the April article, in which case the input impedance of the line may be several thousand ohms at medium audio frequencies. However, excessive attenuation only increases amplifier distortion if the correct power level to the line is maintained.

Telephone communication

Communication between the remote point and the studio is essential for program production. There are several ways of maintaining it. Telephone com-

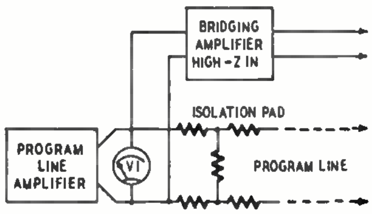


Fig. 1—Isolating pad for volume indicator.

munication may be carried on *via* the program loop itself. This is certainly desirable economically, and is often sufficient for small stations. Modern control consoles of the type usually employed by small stations have elaborate provisions for talk-back and cueing to remote points, and these should be used whenever possible.

When a greater degree of reliability and flexibility is required, a PL (private line) to the remote point may be hired to parallel the program loop. The PL may be another loop of the same high quality as the radio circuit, or it may be (and usually is) a less expensive line designed primarily for telephonic communication. In the latter case, there may be loading coils left in the line, but even so, the PL will put the show on the air (which, after all, is the main

* Chief Engineer, WASH-FM.

commercial consideration) should the regular program loop fail.

Several telephone arrangements are possible for PL work, and the best one depends upon the individual case.

Line maintenance

Certain procedures of routine line maintenance will pay big dividends as program insurance.

1. An early-morning check of all lines which will be used during the day.
   a. Resistance and noise check is sufficient on most lines. In this case, all lines are permanently terminated in 100,000 ohms, used only for the resistance check.
   b. A round-robin check is most satisfactory when a one-way amplifier has been installed on the program line at an intermediate exchange because of extreme line length. In this case, the PL and radio circuits must always be connected together by the remote operator after finishing his program. A standard tone or program material may then be fed down the PL from the studio to return *via* the program loop.
2. A complete check of frequency response, loss, and noise should be made on all lines once a month, especially those lines which are seldom used but may be called up on short notice. A calibrated amplifier or standard transmission set is invaluable in making these checks.

Fig. 2—Form for telephone line information.

3. Loop numbers are very important to the broadcast engineer. They should always be obtained at the time of line installation, as the loop number designates the whole circuit in the records of the telephone company. Should there be trouble on a circuit, the Wire Chief in the first exchange on the faulty loop should be called. The first piece of information he will require is the *loop number*. As some lines may pass through several exchanges, any information about a line is very helpful in an emergency. A sample form page for keeping line records is shown in Fig. 2. One such page should be kept for each line; the result will be a whole notebook full of valuable information.

Coupling Capacitors Can be Troublemakers

By JOHN T. BAILEY

MANY readers may have wondered why the writer felt it necessary to include a 200-megohm range in the novel ohmmeter described in the April issue of RADIO-ELECTRONICS. There are many important reasons why no modern service shop is complete without such a high-range instrument.

In present-day circuits 10-megohm resistors are commonly used as grid resistors in low-level audio stages, with tubes such as the 12SQ7, 12AT6, and many others. The resistors develop bias, and they cannot be measured without a high-range meter. Even higher-value resistors are used for grid bias in hearing-aid and subminiature-tube circuits.

Probably the most extensive use of a 200-megohm range is for checking d.c. leakage resistance of capacitors other than the electrolytic types. A good paper capacitor will have a resistance above 300 megohms, though in many applications a lower resistance is immaterial. However, there are numerous instances where high resistance is required.

Coupling between audio stages is one important instance, as shown by C in Fig. 1. This capacitor sometimes gets fouled with dust and dirt and develops a low resistance over its exterior surface. Extremes of temperature as encountered in auto radios cause expansion and contraction of the inside foils and eventually low-resistance paths, besides other defects. Since these coupling capacitors have high d.c. potentials across them at all times, they act as bleeders when low in resistance and divert small currents through the following stage's grid resistor, thus producing a voltage opposite in polarity to that stage's grid bias. Hence, the following stage's grid bias is reduced and more plate current flows, causing the tube to operate under incorrect conditions. Many a tube has gone soft and had to be replaced because of a leaky capacitor coupling its grid to the plate of a preceding stage.

Furthermore, the increased plate current causes the tube to operate at a higher temperature and this increases the amount of grid current flowing, which also reduces the negative grid bias. Therefore, when using output tubes such as the 25L6, 50L6, 117P6, and so on, a low-value grid resistor is recommended to limit the undesirable accumulated voltages developed by the faults just mentioned.

Another capacitor which has no plate voltage across it, but which can cause plenty of trouble, is the coupling capacitor C in Fig. 2, from the volume-control tap to the grid of a 12SQ7 tube in a typical diode-detector-a.v.c.-first-audio circuit. When this capacitor's resistance drops, even if it is no lower

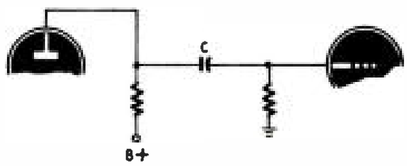


Fig. 1—Capacitor C becomes voltage divider.

than 50 or 75 megohms, the set will overload on strong signals. This is because the volume control will have an a.v.c. potential of possibly —25 volts d.c. across it on a strong signal. This 25 volts is shunted by the leaky capacitor of, say, 50 megohms in series with the following tube's grid resistor of 10 megohms, with the grid connected to the common junction. Hence, the grid gets a negative bias equal to 1/6 of 25 volts ($10/10 + 50 = 1/6$) which is sufficient to cut off the plate current of a high-mu triode.

A word of advice: check all coupling capacitors with a *high-range* ohmmeter and replace all which test under 100 megohms. It is amazing how many capacitors in midget sets have low re-

12SQ7

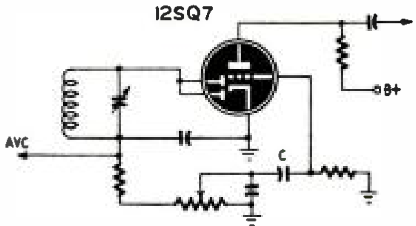


Fig. 2—Troubles start when C gets leaky.

sistance values. And how the distortion can be cleaned up and the output increased by replacing them! But don't expect to find these offenders with an ohmmeter range of less than about 200 megohms because 100 megohms, even on a 200-megohm range, is in the crowded portion of the scale.

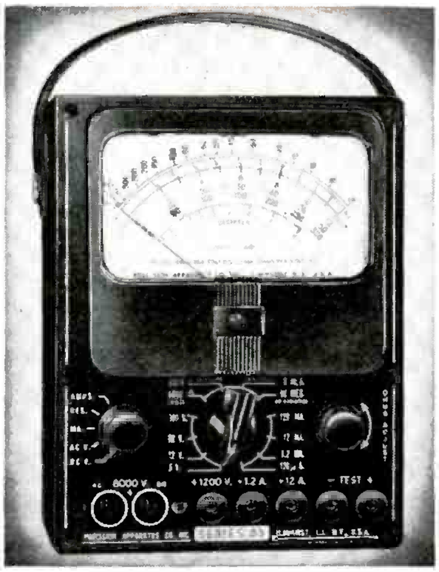
Survey of Multitesters

By RUFUS P. TURNER

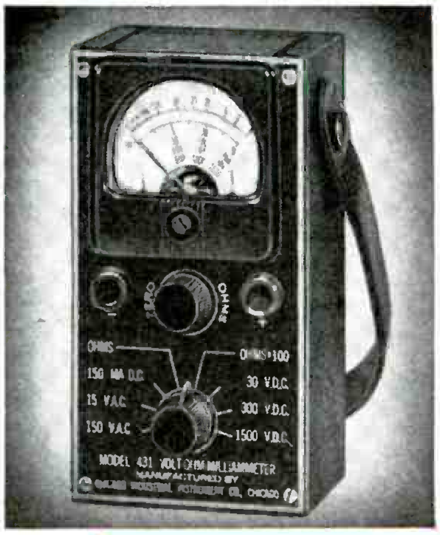
and

ROBERT F. SCOTT

The Hickok Model 435 measures a. c. at 5,000 ohms per volt.



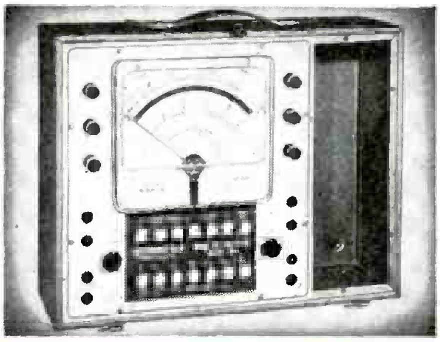
The Precision Series 85 is a good all-purpose instrument.



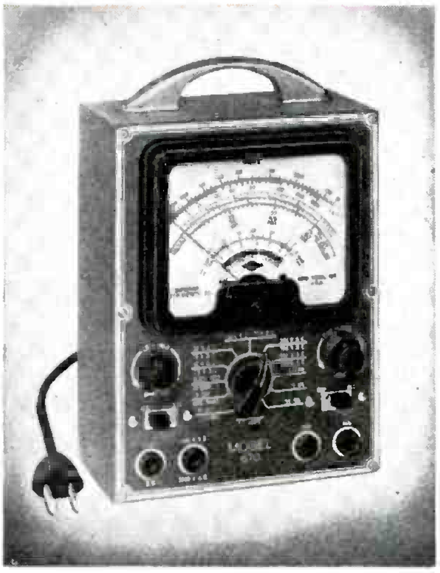
A low-cost meter is Chicago Industrial Instrument's 431.

The Model 630 (Triplett) measures currents as low as 1 μa.

Popular with hams and service technicians — the Simpson 260.



Supreme 644, a deluxe instrument with 98 different ranges.



Superior's Model 670 is popular with radio service technicians.

A common sight on many service benches is Radio City's 488.

Electrical specifications of popular multitesters—still the most valuable radio service instruments

THE nonelectronic volt-ohm-milliammeter, commonly called the "v.o.m.," long has been considered the foundation instrument for all radio test benches. This meter is the basic test tool which the new radioman buys first and is apt to use more frequently than any other piece of gear in the shop. It is versatile and can be used under a variety of work conditions. It is especially long-lived—as long as the user does not set it on the 10-ma range and put 100 volts across it!

Modern volt-ohm-milliammeters provide a.c. and d.c. voltage coverage sufficient for all usual receiver and transmitter measurements. The average resistance range is somewhat better than in pre-war models. Very nearly all the new meters check d.c. amperes, as well as milliamperes and—in some cases—microamperes. Only a few measure a.c. milliamperes and amperes, but this is not ordinarily necessary in radio servicing.

The prices range somewhat higher than in earlier models. (The average price of thirty current models is $39.)

The accompanying table lists information on most of the popular models. Technicians can use the data for guidance in selecting a new meter.

SYMBOLS

*—Alternating current ranges
1—Resistance range can be extended with external batteries
2—Same ranges available at 1,000 ohms/volt
3—1.2-, 30-, 60-, and 120-ampere external shunts available
4—1-, 5-, 10-, 25-, 50-, 75-, and 100-ampere shunts available
5—25-, 50-, 75-, and 100-ampere shunts available
6—Meter has output ranges same as the a.c. volts ranges

Manufacturer and Model	D.c. volts	A.c. volts	Direct current	Resistance	Other functions	Case (in.) weight	Scales	Control
Chicago Industrial Instrument Company Model 421[6]	0–7.5–15–150–750–1,500 1,000 ohms/v	0–7.5–15–150–750–1,500 1,000 ohms/v	0–7.5–75 ma	0–5k–500k ohms		H: $5\frac{7}{16}$ W: $3\frac{9}{16}$ D: 3 4 lbs	3 2.2 in.	toggle switch; jacks
Model 431	0–30–300–1,500 2,000 ohms/v	0–15–150– 1,000 ohms/v	0–150 ma	0–3k–300k ohms		H: $5\frac{5}{16}$ W: $2\frac{15}{16}$ D: $2\frac{1}{2}$ 4 lbs	3 1.6 in.	rotary switch; jacks
Model 450A	0–5–10–50–100–500–1,000 1,000 ohms/v	none	0–1 ma	0–5k–50k–500k ohms		H: $3\frac{5}{16}$ W: $2\frac{7}{8}$ D: $2\frac{1}{2}$ 12 oz	2 1.7 in.	rotary switch; jacks
Model 458	0–5–10–50–500–2,000 1,000 ohms/v	0–12.5–25–125–250–1,250 1,000 ohms/v	0–1–10–100 ma; *0–2.5–25–250 ma	0–1k–200k ohms; 0–2 megohms	—5 to +55 db	H: $10\frac{1}{8}$ W: $6\frac{3}{4}$ D: $5\frac{1}{2}$ 8 lbs	5 3.1 in.	rotary switch; jacks
General Electric Company Model UM-3	0–2.5–10–50–250–1,000–2,500 2,000 ohms/v	0–2.5–10–50–250–1,000–2,500 1,300 ohms/v	0–1–10–100 ma; 0–1–10 amps	0–1k–100k ohms; 0–1 megohm[1]	—12 to +55 db (5 ranges)	H: 9 W: 10 D: $4\frac{5}{8}$ $9\frac{1}{4}$ lbs	5	rotary switch; jacks
Model YMW-1A[6]	0–2.5–10–50–250–1,000 20,000 ohms/v	0–2.5–10–50–250–1,000 1,000 ohms/v	0–50 µa; 0–0.5–5–50–500 ma	0–2k–200k ohms; 0–20 megohms	—4 to +62 db (5 ranges)	H: $10\frac{1}{4}$ W: $9\frac{3}{4}$ D: 4 9 lbs	5 $4\frac{1}{2}$-in. meter	rotary switch; jacks
Hickok Electrical Instrument Company Model 435[6]	0–2.5–10–50–250–1,000–5,000 20,000 ohms/v	0–2.5–10–50–250–1,000–5,000 5,000 ohms/v	0–50 µa; 0 2.5–10–50–250ma; 0–1 amp	0–10k–100k ohms; 0–1–10 megohms	—30 to +55 db (5 ranges)	H: 6 W: $8\frac{1}{4}$ D: $4\frac{1}{4}$ $6\frac{1}{2}$ lb	5	rotary switch; jacks
Precision Apparatus Company, Inc. Series 40[6]	0–3–12–60–300–1,200–6,000 1,000 ohms/v	0–3–12–60–300–1,200–6,000 1,000 ohms/v	0–0.6–6–60–600 ma	0–5k–500k ohms; 0–5 megohms	—26 to +70 db (6 ranges)	H: $6\frac{1}{4}$ W: $3\frac{3}{4}$ D: $2\frac{1}{2}$	4 3-in. meter	rotary switch; jacks
Series 80[6]	0–6–12–60–300–1,200–6,000 1,000 ohms/v	0–6–12–300–1,200–6,000 1,000 ohms/v	0–0.6–6–60–300 ma; 0–1.2–12 amps	0–1k–100k ohms; 0–1–10 megohms	—20 to +70 db	H: $7\frac{1}{8}$ W: $5\frac{1}{2}$ D: 3	4 $4\frac{5}{8}$-in. meter	rotary switch; jacks
Series 85[6]	0–3–12–60–300–1,200–6,000 20,000 ohms/v	0–3–12–60–300–1,200–6,000 1,000 ohms/v	0–120 µa; 0–1.2–12–120 ma; 0–1.2–12 amps	0–6k–600k ohms; 0–6–60 megohms	—26 to +70 db	H: $7\frac{1}{8}$ W: $5\frac{1}{2}$ D: 3	4 $4\frac{5}{8}$-in meter	rotary switch; jacks
Series 847-P[6]	0–3–6–12–60–300–600–1,200–6,000 5,000 ohms/v	0–3–6–12–60–300–600–1,200–6,000 1,000 ohms/v	0–0.3–1.2–3–30–300–600 ma; 0–1.2–12 amps	0–2k–20k–200k ohms; 0–2–20–200 megohms		H: $8\frac{1}{2}$ W: $7\frac{1}{2}$ D: 3	4 $4\frac{5}{8}$-in. meter	P.B. switch; jacks
Series 858-P[6]	0–3–6–12–60–300–600–1,200–6,000 20,000 ohms/v	0–3–6–12–60–300–600–1,200–6,000 1,000 ohms/v	0–60–120 µa; 0–1.2–12–120–600 ma; 0–1.2–12 amps	0–6k–60k–600k ohms; 0–6–60–600 megohms	—26 to +70 db	H: 9 W: 10 D: $4\frac{1}{2}$	4 $4\frac{5}{8}$-in. meter	P.B. switch; jacks
Series 866	A panel-mounting instrument with electrical specifications of Series 847-P. 9-inch meter and controls on 19-inch panel.							

Manufacturer and Model	D.c. volts	A.c. volts	Direct current	Resistance	Other functions	Case (in.) Weight	Scales	Control
Radio City Products Model 447A[6]	0–5–50–250–500– 2,500 1,000 ohms/v	0–10–100–500– 1,000 1,000 ohms/v	0–1–10–100 ma; 0–1–10 amps	0–10k ohms; 0–1 megohm[1]	—8 to +55 db	H: 5⅛ W: 8⅝ D: 3⅛ 2¾ lbs	4 3-inch meter	rotary switch; jacks
Model 449[6]	0–5–50–250– 1,000 5,000 ohms/v	0–5–50–250– 1,000 1,000 ohms/v	0–0.5–50–250 ma; 0–1 amp	0–2k–20k–200k ohms; 0–2 megohms	—6 to +52 db	H: 6 W: 3 D: 2¼ 2 lbs	4 3-inch meter	jacks
Model 488A[6]	0–3–12–60–300– 600–1,200–6,000 20,000 ohms/v	0–3–12–60–300– 600–1,200– 6,000 1,000 ohms/v	0–60–300 μa; 0–3–20–120–600 ma; 0–12 amps; *0–3–6–12 amps	0–3k–300k ohms; 0–30 megohms		H: 11⅝ W: 9¾ D: 6⅛ 10 lbs	4 4½-in. meter	rotary switch; jacks
Simpson Electric Company Model 221 (Roto-Ranger)	0–2.5–10–50– 250–1,000–5,000 20,000 ohms/v	0–2.5–10–50– 250–1,000– 5,000 1,000 ohms/v	0–100 μa; 0–10–100–500 ma; 0–10 amps	0–2k–200k ohms; 0–20 megohms	—10 to +52 db	11½ lbs		rotary switch; jacks
Model 240	0–15–75–300– 750–3,000 1,000 ohms/v	0–15–150–750– 3,000 1,000 ohms/v	0–15–75–300– 750 ma	0–3k–300k ohms		H: 5⅞ W: 3 D: 2 2½ lbs	3 3-inch meter	rotary switch; jacks
Model 260[6]	0–2.5–10–50–250– 1,000–5,000 20,000 ohms/v	0–2.5–10–50– 250–1,000– 5,000 1,000 ohms/v	0–100 μa; 0–10–100–500 ma; 0–10 amps	0–2k–200k ohms; 0–20 megohms	—10 to +52 db (5 ranges)	H: 7 W: 5¼ D: 3⅛ 3½ lbs	5 4½-in. meter	rotary switch; jacks
Supreme Instruments Corp. Model 542[6]	0–6–50–150– 300–1,500 5,000 ohms/v	0–6–30–150– 600 5,000 ohms/v	0–0.3–6–30–150 ma	0–2k–20k–200k ohms; 0–2 megohms	—6 to +50 db (4 ranges)	H: 5⅞ W: 3 1/16 D: 2⅛ 2 lbs	3 3-inch meter	slide switch; jacks
Model 632[6]	0–5–25–100–250– 500–1,000– 5,000 1,000 ohms/v	0–5–25–100– 250–500–1,000– 5,000 1,000 ohms/v	0–5–25–100–250– 500 ma; 0–1 amp	0–2k–20k–200k ohms; 0–2–20 megohms	—10 to +49 db (5 ranges); 0.1 to 400 μf	H: 11¾ W: 8½ D: 4¾	5	rotary switch; jacks
Model 640[6]	0–5–25–100–500– 1,000–5,000 20,000 ohms/v[2]	0–5–25–100– 500–1,000–5,000 1,000 ohms/v	0–100 μa; 0–10–100–500 ma	0–2k–200k ohms; 0–20 megohms	—10 to +49 db (4 ranges)	H: 7½ W: 5 D: 3	4 4-inch meter	rotary switch; jacks
Model 644[6]	0–5–25–100–500– 1,000–5,000 20,000 ohms/v[2]	0–5–25–250– 500–1,000–5,000 1,000 ohms/v	0–5–25–100–500 ma; 0–1–10–50 amps; *0–1–10–50 amps	0–0.5–5–500– 5k–500k ohms; 0–5–50 meg- ohms	—10 to +69 db (6 ranges)	H: 11 W: 15 D: 6¾	4 7-inch meter	P.B. switch; jacks
Superior Instruments Company Model 670[6]	0–7.5–15–75– 150–750–1,500– 7,500 1,000 ohms/v	0–15–30–150– 300–1,500–3,000 1,000 ohms/v	0–1.5–15–150 ma; 0–1.5 amps	0–500–100k ohms; 0–10 megohms	—10 to +58 db; .001 to 4 μf; 1.75 to 8,000 henries	H: 7½ W: 5½ D: 3	7	rotary switch; jacks
Model 770	0–7.5–15–75–150– 750–1,500 1,000 ohms/v	0–15–30–150– 300–1,500 1,000 ohms/v	0–1.5–15–150 ma; 0–1.5 amps	0–500 ohms; 0–1 megohm		H: 5⅞ W: 3⅛ D: 2¼	3	rotary switch; jacks
Triplett Electrical Instrument Company Model 625-NA[6]	0–1.25–5–25–125– 500–2,500 20,000 ohms/v; 0–2.5–10–50–250– 1,000–5,000 10,000 ohms/v	0–2.5–5–10–50– 250–1,000–5,000 10,000 ohms/v	0–50 μa; 0–1–10–100 ma; 0–1–10 amps (all ranges at 250 mv)[3]	0–2k–200k ohms; 0–40 megohms	—30 to +70 db (6 ranges)	H: 5½ W: 6 D: 2½ 3 lbs	4 (mirror) 6-inch meter	rotary switch; jacks
Model 630[6]	0–3–12–60–300– 1,200–6,000 20,000 ohms/v	0–3–12–60–300– 1,200–6,000 5,000 ohms/v	0–60 μa; 0–1.2–12–120 ma; 0–12 amps (at 250 mv)[3]	0–1k–10k ohms; 0–1– 100 megohms	—30 to +70 db	H:7½ W: 5½ D: 3¼ 4 lbs	5 5½-in. meter	rotary switch; jacks
Model 666-HH	0–10–50–250– 1,000–5,000 1,000 ohms/v	0–10–50–250– 1,000–5,000 1,000 ohms/v	0–50 μa; 0–10–100–500 ma; 0–10 amps (at 250 mv)[4]	0–2k–400k ohms		H: 5⅞ W: 3 1/16 D: 2 9/16 1 lb	3 3-inch meter	rotary switch; jacks
Model 2405-A[6]	0–10–50–250– 500–1,000 20,000 ohms/v	0–10–50–25– 500–1,000 1,000 ohms/v	0–50 μa; 0–1–10–50–250 ma; 0–10 amps *0–500 ma; 0–1–5–10 amps	0–4k–40k– ohms; 0–4– 40 megohms	—10 to +55 db (5 ranges)	H: 10 W: 10 D: 5¾ 11 lbs	4 6-inch meter	rotary switch; jacks
Weston Electrical Instrument Company Model 772	0–2.5–10–50–250– 1,000; 20,000 ohms/v[2]	0–2.5–10–50– 250–1,000 1,000 ohms/v	0–0.1–1–10–50– 250 ma; 0–1–10 amps	0–3k–30k ohms; 0–3– 30 megohms	—14 to +54 db (5 ranges)			

Novel Bridge Rectifier Circuit

by H. B. CONANT *

FOR many years, two-section instrument rectifiers have been used with two resistors in a bridge circuit to produce full-wave rectification. To my knowledge, however, no one has ever suspected that a *single*-section rectifier and *three* resistors could also be made into a full-wave rectifier.

Thinking about rectifier circuits in general one day, I found myself considering the single-rectifier, three-resistor scheme. I drew the diagram shown here.

Because current relationships in bridge circuits are complex, I omitted the meter at first and calculated the potential difference developed between points B and D during each alternation. According to theory, if a potential difference exists and a meter is connected between two points, current must flow through the meter.

A value of 1,000 ohms was given to each resistor. The resistance of the rectifier was taken as 200 ohms in the forward direction and 30,000 ohms in the inverse direction. An a.c. voltage is applied to terminals A and C. For clarity of explanation, consider this to be 10 volts and terminal A to be the reference or "ground" point of the circuit throughout the discussion.

Taking the first alternation, during which terminal A may represent the negative and terminal C the positive side of the input signal, terminal D has a potential of +5 volts because R2 and R3 are equal. Since current is passing through the rectifier in the forward direction, its resistance is effectively 200 ohms. The voltage at terminal B is then $\frac{200 \times 10}{1{,}000 + 20} = +1.67$ volts. Obviously, terminal D (at +5 volts) is more positive than terminal B with respect to the reference point, terminal A. The voltage difference between terminals B and D is 3.33 volts. No matter what the a.c. input voltage, terminal D, on this alternation, will always be 33.3% of the input voltage *more positive than terminal B.*

Now let us consider the opposite alternation. This time terminal C is negative and A is positive. Terminal A is still the zero reference point to which all voltages are referred.

Again D is at 5 volts, but this time it is *negative* with respect to A. Since the inverse resistance of the rectifier is 30,000 ohms, the voltage at terminal B is now $\frac{30{,}000 \times 10}{30{,}000 + 1{,}000} = -9.67$ volts with respect to terminal A. With terminal D at —5 volts, terminal B is obviously much more negative than D. In other words D is *still positive with respect to B!* The difference is 4.67 volts, meaning that, on this alternation, D will always be 46.7% of the input voltage more positive than B.

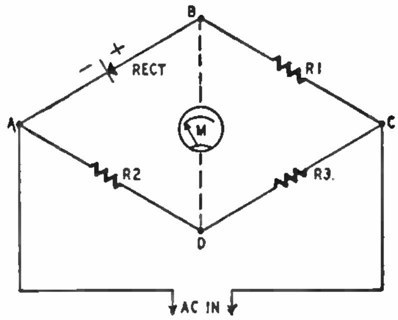
The voltage differences between B and D on the two alternations, as has been shown, are not alike—46.7 volts in one case and 33.3 volts in the other. This will, of course, give a distorted rectified d.c., but the interesting point is that the d.c. is actually greater when current is passing through the rectifier in the *inverse* direction. The same d.c. can be obtained on both alternations if the values of the resistors are changed appropriately.

After all these calculations were made, an actual circuit was connected up and the output of terminals B and D was fed to a 'scope. The full-wave pulsating d.c. showed up clearly, with alternate half-waves slightly different in height.

Next a 1-ma meter was connected across B and D, as shown by dotted lines in the diagram. A sensitivity of 400 ohms per volt was obtained.

Further calculations showed that for optimum results R1 should be equal to 12 times the rectifier's forward resistance, and R2 and R3 should be five times the rectifier resistance.

Two important apparent advantages are: No inverse current can flow through the meter (this is not the case



This bridge operates with just one rectifier.

with a four-rectifier bridge), and the rectifier is so placed that damaging it with voltage overloads is extremely unlikely.

(The only possible objection to this ingenious circuit is that its resistance will undoubtedly be higher than that of a four- or even two-rectifier arrangement. It is, of course, less sensitive. These points may or may not be important in any particular application.—*Editor*)

"My husband is a bug on shortwave listening."

*Conant Electrical Laboratories, Lincoln, Nebraska

Radio Set and Service Review

The Air King A725 wire recorder has many applications

This 21½-pound recorder is well-balanced and easy to carry.

THE development and production of low-cost wire recorders has done much to popularize the use of these devices in business, industry, schools, and homes. Most of the machines can record for periods up to an hour on a single spool of wire so the number of applications is limited mainly by the imaginations of the users.

Invalids, shut-ins, and other persons who would normally have "pen pals" have begun to use wire recorders as a means of communication. They record their messages on spools of wire and mail them to the addressee. After playing the recording on his machine, the addressee erases the wire and records his own message before returning the spool. This method of communication has become so popular in some circles that the word *wiresponding* has been coined to mean communication by magnetic wire.

Many shut-ins find wire recordings have a much more personal touch and are less tiring than writing letters, so the use of wire recorders has enabled them to enlarge their circle of friends. There are some shut-ins who, unable to leave their homes, have a friend or member of their family take the wire recorder to various parties, banquets, and other festive occasions. The recorder is set up in some out-of-the-way place and the microphone placed where it will have the greatest pickup. In this way, the shut-in is able to gather from the recordings much more of the festive gayety and feeling than he possibly could from a verbal report.

The new Air King Model A725 wire recorder, designed for home and semi-professional use, is one of the few complete units costing less than $100.00 (slightly more west of the Rockies). It handles standard spools of wire for recording up to 1 hour. The wire speed is approximately 2 feet per second for recording and playback. The rewind ratio is about 6 to 1.

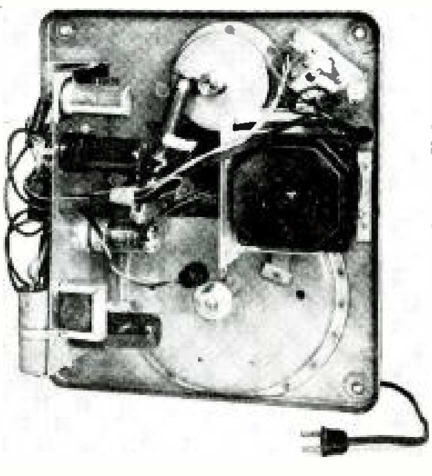
There are only three controls. They are the combined volume control and on-off switch, the RECORD-PLAY switch, and the SELECTOR switch. The recorder is equipped with a hand-held crystal microphone with a 10-foot cable that plugs into the center of the control panel (see front-view photograph). A jack on the left side of the panel is for connecting a radio tuner, phonograph, or other high-level signal source. A neon recording-level indicator is on the right side of the panel. It operates when the machine is recording. The SELECTOR in the upper right-hand corner controls the speed and direction of the wire during record, playback, and rewind operations by varying the ratio of the friction-drive drums in the mechanism. The SELECTOR is coupled to two slide switches; one applies power to the drive motor in the PLAY, RECORD, and REWIND positions. The other turns on the bias-erase oscillator when the selector is in the RECORD position. A simple press-to-release lock prevents the operator from unintentionally throwing the selector to RECORD while playing a record.

The circuit of the recorder appears in Fig. 1. It consists of a 1280 (non-microphonic 14C7) microphone amplifier, 6AQ6 voltage amplifier, and two 50L6-GT's as power amplifier and oscillator.

The unit has an interesting compensating circuit that attenuates the bass during recording and attenuates the highs during playback. This circuit and that of the level indicator are shown in Fig. 2. The RECORD-PLAY switch S1 is a 6-circuit, 2-position unit. Three of its sections are used in the circuit of Fig. 2. In RECORD, the voice coil (terminals 2 and 4 on the recording head) is capacitance-coupled to the plate of the 50L6-GT power amplifier through C9 and R13. C9, R13, and the low-impedance voice coil form a voltage divider with the maximum voltage being developed across the voice coil at the higher frequencies.

In the PLAY position, one section of S1 grounds C9 through R13 while another section shunts C8 across R13, reducing the high-frequency response.

The level indicator is biased almost to the ignition point by a voltage developed across R11 when S1 is set to RECORD. Audio voltage from the power amplifier is sufficient to make the lamp light on modulation peaks when the volume control is set to the correct level. The lamp is shorted by a section of S1 on PLAY.



A view of the chassis and driving mechanism.

When S1 is in the RECORD position, it also:

1. Disconnects the loudspeaker and loads the secondary of the output transformer T1 with a 3.2-ohm dummy-load resistor;
2. Connects the microphone to the input of the 1280;
3. Completes the cathode return of the 50L6-GT oscillator through S5 (when the selector is rotated to RECORD);
4. Grounds one side of the output winding of the oscillator transformer T2 to complete the path to the erase and bias coil (terminals 2 and 3) in the recording head.

When the recorder is used for playback, S1, in addition to the functions mentioned, also:

1. Connects the voice coil of the speaker to the secondary of output transformer T1;
2. Connects the voice-coil in the recording head to the input of the 1280 voltage amplifier;
3. Opens the cathode circuit of the 50L6-GT oscillator.

This recorder is easy to thread and simple to operate. One of the most annoying characteristics of it—and other wire recorders—is that the wire tends to break at the slightest provocation. When it does, it is likely to tangle and kink badly. In such cases, it is difficult to gather the loose ends of the wire and tie them without getting more knots and kinks into the wire. An automatic shut-off S3 stops the motor at the end of the play, record and rewind operations but does not operate when the wire breaks.

The quality of reproduction is by no means high but is suitable for many purposes. Amateur radio operators can make records of rare dx contacts and play them for skeptical visitors and members of the local radio club. Parents sometimes find it difficult to get children to study their lessons when study-hours conflict with a favorite broadcast. These parents can record the programs and permit the children to play them at a more convenient time.

The A725 uses a transformerless power supply with one side of the line and B-minus connected to the chassis through a 0.1-μf capacitor. Although there is no direct connection between the line and chassis, the *chassis is hot* when the ungrounded side of the line is connected to B-minus.

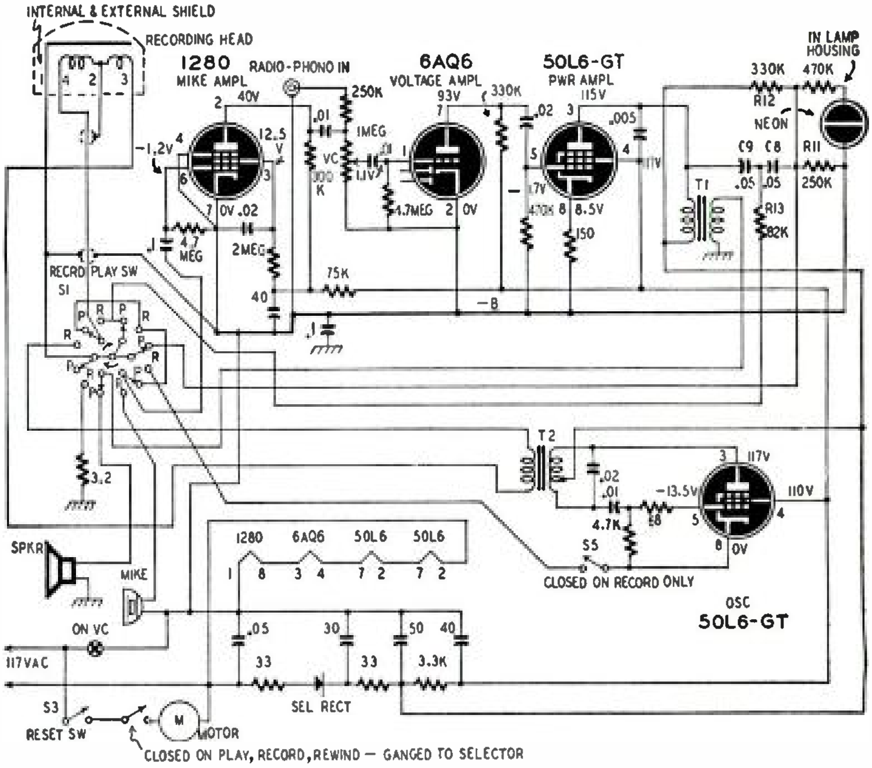


Fig. 1—The circuit of this recorder is simple when compared to some professional models.

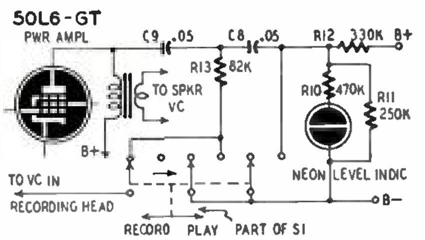


Fig. 2—A novel tone-compensating network.

SERVICE NOTES ON SOME PHILCO SETS

By W. G. ESLICK

Here are some hints for technicians on repairing and improving several frequently encountered models of Philco receivers.

Models 46-1201, 1203, 48-1253, 1260: Replace the oscillator coil with one not having a capacity winding. Use a 47-$\mu\mu$f capacitor between the coil and the 7A8 oscillator grid. Shunt a 10-$\mu\mu$f negative-temperature-coefficient capacitor across the oscillator tuning capacitor.

Models 46-200, 201, 202, 203, 420, 421, 250: If the oscillator is not stable at the low frequencies, change the oscillator grid-leak resistor from 47,000 to 120,000 ohms.

Model 46-480: If there is oscillation when the set is switched to FM, install a 240-$\mu\mu$f capacitor across C316, which can be found by tracing the wire from pin 3 of the 6H6 socket, through a 33,000-ohm resistor, to pin 1 on the band-switch. From here C316 (.01 μf) goes to ground.

To prevent oscillator drift on the same model when the push-buttons are used, replace C412 (485-$\mu\mu$f silvered mica capacitor) with a ceramic capacitor of the same value. Replace C413 (285 $\mu\mu$f) in the same manner. Both are across push-button oscillator coils.

To prevent drift and failure of the 7F8 in the 46-480, remove the 1-megohm resistor which goes from the 7F8 mixer cathode to B+. Change R300 (4,700 ohms, in the 7F8 plate circuit) to 47,000 ohms.

Model 46-120: If the set lacks pep, the second i.f. transformer may be bad due to heat from the tubes. Replace it with a Philco part No. AD-1024.

Model M8 Record Changer: If the changer keeps cycling, check the spring on the retractable segment of the cam gear. If the spring is broken, replace the whole gear. If not, and if the segment is not binding, bend the little "ear" that stops the trip plate; it probably does not come over far enough to lock the segment. Be sure the little copper vane is at about a 40-degree angle when on trip.

Sets using 50A5 and 50X6: Replace the 50A5 if the tone is "mushy." If the 50A5 was shorted, replace the 50X6 as well. Check both voltage-doubling capacitors in the 50X6 circuit and all bypass and coupling capacitors.

1941 models using "beam-of-light" phonograph, 7B5 oscillator, and 7Y4 rectifier: Replace the 7B5 with a 7A5 and the 7Y4 with a 7Z4. This will make the beam light brighter and give more volume. Replace the two .01-μf coupling capacitors in the circuit of the 41 output tubes, regardless of test results.

Fundamentals of Radio Servicing

Part IV—Capacitance

By JOHN T. FRYE

EVERY electrical circuit, whether it be a 1-inch length of wire or a cross-country telegraph line, has three "built-in" electrical properties: resistance, inductance, and capacitance. The first two of these we have already encountered in previous chapters; now we are ready to grapple with the third.

Capacitance is like discarded chewing gum; you may find it almost anywhere. *Any time you have two electrical conductors separated by a nonconducting medium, you have a capacitor;* and a capacitor is to capacitance what a doghouse is to a dog; it is where you normally expect to find it. By the light of this definition, you can see that your pocket watch and the furnace in the basement below form a capacitor; so does a clothesline and the antenna

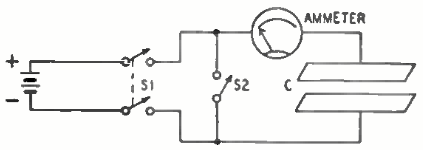


Fig. 1—Test setup shows capacitance effects.

stretched above it; so does a moisture-bearing cloud and the earth beneath.

In this free or "stray" state, capacitance is of little or no value; in fact it is often a nuisance. But when it is controlled and "lumped" in definite units, it is every bit as important to electricity as are resistance and inductance.

In its "cultured" state, capacitance comes in the packaged form of *condensers*, the common name for *capacitors*. There is a wide variety in the form and material used in such condensers; but before we start studying these practical units, let us see how a simple basic capacitor operates. Once we grasp how it works, we shall know how all capacitance units function.

Take a good look at Fig. 1. Here we have a capacitor C, consisting of two parallel flat metal plates with an air space between them. Switch S2 connects across these plates. The double-pole switch S1 permits us to connect the battery directly to the plates. An ammeter, an instrument for indicating both the intensity and direction of any electrical current passing through it, is inserted in the lead going to the top plate of the capacitor.

To begin, let us say that S1 is open and that we have momentarily closed S2 and then reopened it.

Now, suppose we close switch S1. As we do so, the ammeter pointer flips over and then drops back to zero, indicating that a momentary current passed through it. Next, let us open S1 so as to disconnect the battery. What happens? Nothing; the ammeter pointer does not budge. But, suppose we now close 2. As we do so, the ammeter needle flicks again, but in the opposite direction, indicating a reverse flow of current.

Paradox or sense?

Several questions should be pulsing through your head at this point: Why did current flow in this circuit when we connected the battery? There was no complete circuit, for the plates of the condenser were separated by insulating air. After the current started flowing, why did it stop? Where did the current come from that caused the meter to flick when we closed S2? It could not come from the battery, for that had already been disconnected.

The explanations, as usual, go back to electron theory. The momentary closing of switch S2 before we connected the battery allowed any excess of electrons on either capacitor plate to flow through the switch and balance the electron distribution. At the instant the battery was connected, however, the positive terminal put a strong "come hither" on the negative electrons of the top plate, and they surged through the wire and the ammeter to that terminal, causing the ammeter to register their passage as they did so. At the same instant, the pent-up excess of electrons on the negative terminal of the battery rushed out on to the bottom plate of the condenser like school kids spilling out on the playground at recess. The result of this simultaneous "push-pull" action was to leave the top plate with a deficiency of electrons, giving it a strong positive charge, while the lower plate was strictly "Standing Room Only" with electrons and so had a negative charge.

As more and more electrons left the top plate and crowded on the lower plate, the charges on the two plates increased *in opposite directions* until the difference between them was exactly equal to the difference in potential between the two terminals of the battery. At this point, the electrons stopped flowing, because the pushing and pulling force of the charged plates exactly balanced the equal and opposing forces of the battery terminals.

Nothing happened when we opened S1, for there was no path by which the excess of electrons on the lower plate could reach the electron-hungry upper plate. Since this state of unbalance still existed, a voltage equal to that of the battery still was present between the plates, even though the battery itself had been disconnected.

The instant we closed S2 we provided the needed connecting path, and the displaced electrons rushed through it and through the ammeter to the upper plate. Since this time the electrons were flowing *to* the upper plate instead of *away* from it—as they were when the battery was first connected—the ammeter pointer moved in the opposite direction. As soon as the electrons were once more evenly divided between the two plates, they ceased to flow; and we were right back to the point we were before we started charging and discharging the capacitor.

We might have made one other experiment: When we had the battery connected to the capacitor (S1 closed), if we had slid a sheet of glass between

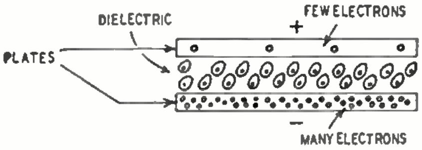
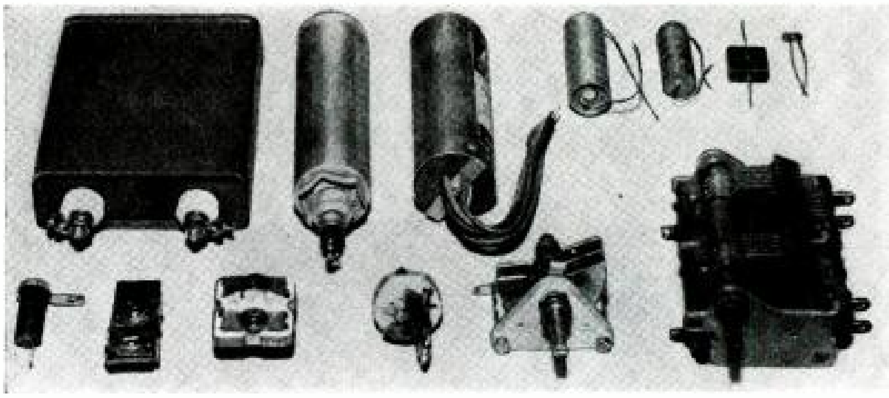


Fig. 2—Capacitor plates after being charged.

the plates, we should have noticed that the ammeter pointer flicked again, indicating that more charge was moving into the capacitor. When we removed the glass, the pointer would have moved in the opposite direction, showing that this new additional charge had moved back out of the capacitor. An explanation of why the material used as the insulating medium of a capacitor (it is called the capacitor dielectric) affects the charge the capacitor will take will be given a little later.

It is apparent that a capacitor is a device for storing an electrical charge. The measure of its ability to do this storing is its *capacitance*. The amount of the charge stored depends upon how many electrons we can force to leave the top plate and congregate on the bottom plate. We know that the more voltage we have in our charging battery, the more power we have to do this forcing; so it should not come as a surprise that the unit used to measure the capacitance depends both on the number of electrons stored and the voltage necessary to do the storing. This unit is called the *farad*. One farad is the capacitance of a capacitor *in which a coulomb* (6.28×10^{18} *electrons) of electricity is stored when an* e.m.f. *of 1 volt is applied*. This unit is too large for practical use; so the *microfarad* (μf), a millionth part of a farad, and the *micromicrofarad* (μμf), a millionth part of a microfarad, are always used in radio.



These capacitors illustrate the many types the technician will encounter in his servicing.

The "why" of capacitance

We have explained *what* happens when a condenser is charged, but we have not explained *why*. Truth to tell, the pundits of electronics tend to take refuge in such phrases as "it is believed," "the theory is held," and "we may assume" when they go to talking about this subject; but here is what is generally thought:

A charged capacitor looks like Fig. 2, in which the ellipses between the plates represent, in a greatly exaggerated form, the out-of-round orbits of the electrons of the dielectric atoms in their paths about their respective positive nuclei. The orbits are out-of-round because of the attraction of the positively charged upper plate and the repulsion of the negatively charged lower plate. Were the electrons of the dielectric free to move, they would go straight to the positive plate; but since they are tightly bound, the best they can do is deviate slightly from their normal circular path.

When these orbits are comparatively easy to push out-of-round, their counter-repelling action on the electrons trying to muscle their way on to the negative plate will be comparatively weak, just as a weak spring puts up a feeble resistance to being compressed; consequently a large number of electrons can force their way onto the plate. The capacitance of the capacitor will be larger than it would be with a dielectric material in which the electron orbits were harder to distort. In the latter case, since the dielectric electrons would stubbornly refuse to budge from their orbits, the electrons trying to wedge their way on to the negative plate by distorting these orbits would be rebuffed, and the storage ability would be lessened.

We could increase the capacitance by using a thinner slice of dielectric material, allowing the plates to come closer together. This would reduce the total number of the repelling dielectric electrons and so permit more electrons to collect on the negative plate of the condenser.

It is evident, then, that we can increase capacitance in three different ways:

(1) We can increase the size of the active portion of the plates. The active portions of the plates are the portions that are directly opposite each other and with the dielectric material squarely between them. Increasing the size of these portions means that we have more electrons to draw from the positive plate and more room on the negative plate to store them. When you remember that the resistance of the electrons of the dielectric material is "softened up" by the *double* action of the lower and upper plates, working as a combined pushing and pulling team, you can see why only the portions of the plates considered active have much effect on the capacitance.

(2) We can reduce the thickness of the dielectric material as discussed above.

(3) We can use a dielectric material whose electron orbits are more easily distorted.

The effect that the dielectric has on the capacitance is called the *dielectric constant* of the material and is expressed by the symbol K. Air is assigned a K of 1, and all other materials are compared with this. For example, replacing the air dielectric of a given capacitor with mica will multiply its capacitance about 5 to 7 times; so we say that mica has a K or dielectric constant, of 5-7. In the same way glass has a K of 4.5-7, and some rutile ceramics have a K of 90-170. No wonder the little cusses can pack so much capacitance in so small a space!

An ideal capacitor would be one with insulation so perfect that absolutely no current could leak across from one plate to the other; but ideal capacitors are like ideal picnics—they are never quite realized. We have *no* perfect insulators, and there is always *some* leakage. A capacitor with high leakage current is said to have a *high power factor;* just remember that in capacitors power factors are like living costs—the lower, the better.

If we keep increasing the voltage across the plates of a capacitor, we eventually reach a point where the current will break through the dielectric and destroy it (unless, of course, it is air). Increasing the thickness of the dielectric will make this breakdown voltage higher, but it will also reduce the capacitance. Most capacitors used in radio work carry, in addition to their capacitance value, a marking indicating the maximum voltage with which they are to be used. These voltage ratings may vary all the way from a half-dozen volts to several thousand for various applications.

The picture shows the wide variety of capacitors used in radio work. In the next chapter we will take up the actual construction of capacitors, the good and bad points of each type. We will also find out why it is necessary to have so many different forms of capacitors when they all operate on the same basic principle.

If you are impatient to get to this discussion of the practical aspects of capacitor construction, just remember that unless you have a good, firm grasp of the theory of operation, you will have a hard time understanding *any* type of construction, whether it be an internal combustion engine or a baby's three-cornered pants!

AUTOTRANSFORMER

While converting a 110-volt a.c.-d.c. radio to operate on 220 volts a.c., I was unable to get a suitable step-up transformer or line-cord resistor. I took an old power transformer with a burned out primary and connected the 220-volt line across the ends of the high-voltage secondary. The radio was connected between the center tap and one side of the winding. I have used this method with good results for some time.

D. E. O'N. WADDINGTON.
Natal, South Africa.

(When selecting a transformer for such service, be sure to select one with a secondary capable of carrying comparatively heavy current. The same setup can be used for operating 220-volt equipment from 117-volt a.c. lines, that is, for stepping voltage up.—*Editor*)

Television and FM Alignmen


McMurdo Silver Model 911 generator.

How to align television and FM receivers, using a modern sweep generator and 'scope

By
DOUGLAS H. CARPENTER*

THE modern television receiver imposes many new service problems that have no counterparts in the more familiar AM practice. Aligning TV sets requires specialized apparatus with which the average service technician has had little experience.

Television, without a doubt, will be the major broadcasting field within a very few years; the wise technician is the one who is now preparing to be a part of this lucrative industry. There are only three things that he must possess: a thorough knowledge of TV receivers, modern service equipment, and a knowledge of how to use this equipment intelligently.

Reference to the schematic (Fig. 1) indicates the essential circuits of a TV alignment instrument. Two 12AT7 twin-triodes are used as reactance modulator, fixed-frequency oscillator, variable-frequency oscillator, and mixer. The reactance modulator causes the frequency of the "fixed" oscillator to shift around its center frequency when a modulating voltage is applied to the reactance modulator grid. The linear variation of the fixed oscillator (the amount that the carrier may be shifted in either direction) is controlled by the setting of P1, the sweep-control potentiometer. We have, therefore, a fixed oscillator whose frequency may be swept or frequency-modulated some 10 mc at the maximum setting of P1. The amount of carrier swing is shown directly on a scale.

The output of the fixed oscillator is taken from across the cathode resistor R2 and fed to the grid of the mixer tube through the coupling capacitor C8. The output of the variable-frequency oscillator is also fed to this mixer grid through the 10-$\mu\mu$f capacitor. The mixer tube operates as a cathode follower, its cathode load being the output control P2. Both the sum and difference frequencies generated by the mixing of the two oscillators are available across P2.

The frequency of the fixed oscillator in the McMurdo Silver Model 909 and 911 sweep generators is set at 114 mc. The variable-frequency oscillator in both instances covers the range of 37 to 112 mc. For this discussion the Model 909 may be considered similar to the 911, with the exceptions that the 911 contains the crystal marker circuit (a 12AU7), and the phasing control (P3), shown in Fig. 1.

The frequency range produced by the mixing of the variable and fixed oscillators is a continuous 2 to 226 mc, directly calibrated in three scales on the main vernier tuning dial. The first range of 2 to 77 mc is produced by the difference between the two oscillator frequencies. The second or middle scale, calibrated 60 to 154 mc, is the second harmonic of this difference frequency. The sweep width in this instance is double that obtained on the 2-77-mc range. The outer scale, calibrated from 151 to 226 mc, represents the sum frequency generated by the mixing.

When two high-frequency oscillators are mixed to produce a low-frequency output, it is extremely difficult to keep the lower frequency accurate. Drift in either oscillator which is only a small percentage of its fundamental frequency may show up as a large error when translated to the low-frequency mixed output. It is for this reason that manufacturers advocate the use of marker signals accurately to trace out pattern

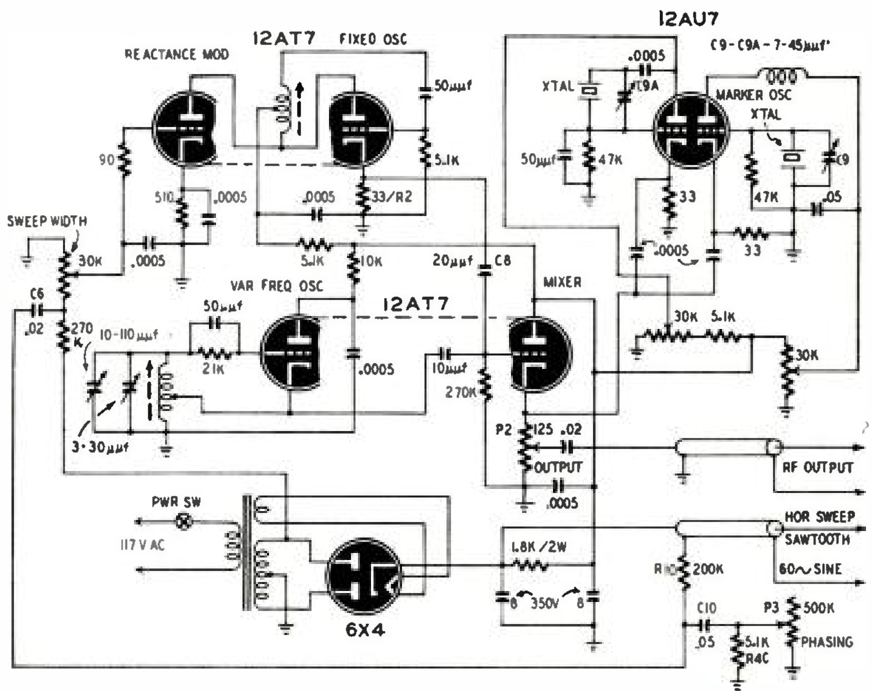


Fig. 1—Schematic of the 911. The instrument includes marker oscillator and sync outputs.

*Chief Engineer, McMurdo Silver Co.

response and to determine TV frequency and bandwidth. Some manufacturers have gone so far as to use dials that cannot be read closely enough for alignment work, thus forcing the technician to use a separate marker system. The only method of avoiding the use of a separate marker is to recheck dial calibration against known sources and compile a chart of the most-used points. Although such a system may be used with relatively narrow passbands such as with FM, i.f. and discriminator patterns, it is definitely not applicable to video i.f. work. For this reason the marker system and phasing control have been incorporated in Model 911. Both Models 909 and 911 may be used for either FM or TV alignment, but the 909 requires a separate external marker system to determine the exact frequency and bandwidth of TV patterns. This marker may be any test oscillator of the correct frequency and necessary accuracy. The Model 911 is an "all-in-one" instrument incorporating a dual crystal-marker system as well as a phasing control used to produce a single image when inspecting asymmetrical passbands such as video i.f. responses.

FM and TV receivers may be aligned rapidly with either instrument. The important points with an FM receiver are the i.f. and discriminator patterns. The table has been prepared as a quick reference guide. It assumes that phasing control is used in television alignment. The phasing control circuit incorporated in Model 911 can be copied, and built externally or into the 909, as the technician prefers. The phasing network consists of C6, C10, R10, R4c, and P3. The only connection that has to be changed in the 909 is the shield braid of the horizontal synchronizing cable. In manufacture this was connected internally to ground. It must be disconnected and utilized as the means of obtaining the 60-cycle phased voltage through C6. It serves as the output line for this voltage, and a phone tip may be connected to the output end of the cable braid to allow convenient connection to the 'scope binding post. The phasing network may be built in a few minutes, and all components are common in any radio shop.

It will be noted in Fig. 1 that two separate types of 'scope-control voltages are available from Model 911. These two voltages are provided to accomplish direct control of the beam through the horizontal amplifier for two different conditions. When the sweep generator is used to inspect a symmetrical passband, the output connection labeled SAWTOOTH is connected to the high side of the horizontal amplifier. No separate ground connection need be provided for the control voltages in any case, as a ground is made automatically when the 'scope's vertical amplifier input is connected to the receiver. Symmetrical passbands include FM-receiver i.f. and discriminator responses, and sound channels of television sets. The control voltage provided in this case is a 120-cycle sawtooth that is in phase with the reactance-modulator sweep voltage. Since the fixed oscillator is swept with a 60-cycle sine wave, the sweep rate is twice this, or 120 sweeps per second. If the coarse frequency control of the 'scope is turned to OFF and the 120-cycle sawtooth voltage is used for direct control through the horizontal amplifier, mirror-image responses will be observed.

This means that two response curves will be seen, one the actual response, the other the same curve backward. To illustrate this, assume a very distinct asymmetrical i.f. response as shown in Fig. 2-a. (This is never obtained in practice but it makes a good illustration because the upper- and lower-frequency slopes are obviously different.)

The sawtooth voltage sweeps the cathode beam to the right in 1/120 second. The first half-cycle of the 60-cycle-modulated generator output passes through the i.f. amplifier under test in 1/120 second. Therefore, on the first half of the modulator cycle, the actual amplifier response curve is shown on the oscilloscope screen.

Now, in the second half-cycle of modulation, the generator output is swept over the same frequency range, *but from high to low frequency—backward.* The 120-cycle sawtooth, however, again traverses the screen *in the same direction as before,* toward the right. The beam spot is being pushed to the right, but its vertical deflection is governed by the amplifier response curve *in reverse* because the modulator is making the frequency decrease rather than increase as it did on the first half-cycle. The result is that the *reversed* picture of the amplifier response will appear on the screen. It will be exactly where the actual response appeared during the first half-cycle if the center of the response is at the center frequency of the FM generator. Since the two are being traced at a comparatively high rate of speed, the eye sees both the actual and reversed curves simultaneously. The two are superimposed, reversed—or mirror—images of each other as the drawing (Fig. 2-b) clearly indicates.

(Continued on following page)

ALIGNMENT TABLE

Alignment	Generator connections	Oscilloscope connections	Oscilloscope control voltage	Notes	Response
FM discriminator (ratio-detector type)	converter grid	junction of discriminator-transformer tertiary winding and de-emphasis network	120-cycle sawtooth	substitute 1½-volt flashlight cell for 3-8-µf stabilizing capacitor; receiver oscillator shorted	Fig. 4
FM oscillator	antenna post	as for i.f. alignment	"		Fig. 3
FM r.f.	"	"	"	adjust for maximum amplitude	Fig 3
FM i.f. (limiter-discriminator type)	each i.f. grid in turn	across first-limiter grid resistor	120-cycle sawtooth	short receiver oscillator	Fig. 3
FM discriminator	converter grid	ungrounded discriminator cathode	"	"	Fig. 4
FM i.f. (ratio-detector type)	each i.f. grid in turn	junction of discriminator-transformer tertiary winding and de-emphasis network	"	disconnect 3-8µf stabilizing capacitor; receiver oscillator shorted	Fig. 3
TV video i.f.	each i.f. grid in turn	across video second-detector load resistor	60-cycle sine	adjust phasing control for single image; employ markers to establish correct bandwidth	Fig. 5
TV oscillators	antenna posts	not used	not used	set generator to center of sound channels; adjust trimmers for loudest 120-cycle sweep tone at speaker	
TV r.f.	antenna posts	across second-detector load	60-cycle sine	see text	Fig. 6

Suppose now that the amplifier being tested is an FM i.f. Ideally, the curve should be symmetrical—the slope on both high- and low-frequency ends should be the same. As the correct adjustments are made in the set to achieve symmetry, the actual and image slopes on one side will tend to approach each other, the more slanting one becoming steeper and the more vertical one becoming more gradual. The same will occur on the other side. When the upper- and lower-frequency slopes are exactly equal, and the center frequency of the passband is the same as the center frequency of the generator, the actual and mirror-image curves will coincide and only one curve will be seen.

This type of response is desired in the alignment of FM receivers. If the output cable labeled 60-CYCLE SINE is used for direct control through the horizontal amplifier, one image will be observed when the phasing control is properly adjusted. It is of little value to obtain one image of a symmetrical passband because the advantage of visual comparison of opposite sides is lost. It would also be confusing to have a mirror-image response of an asymmetrical pass band (such as a video i.f.) because opposite sides of the pattern should have different slopes and trap responses. For this reason two distinct types of control voltages are made available to satisfy the two entirely different conditions. When using Models 909 and 911, the time base of the 'scope is turned off, and no additional 'scope adjustments are necessary.

Alignment procedures

Here is a typical alignment procedure using the 911. Reference to the table will simplify the explanations.

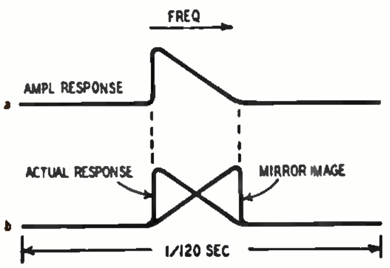


Fig. 2—An example explains the mirror image.

To align an FM receiver it is first necessary to short out the receiver oscillator. The sweep-generator output clips are connected from the last i.f. grid to ground. The 'scope coarse frequency control is turned to OFF. The 120-CYCLE SAWTOOTH cable is connected to the high side of the 'scope's horizontal amplifier. Connect the vertical amplifier across the first limiter grid resistor. When appropriate sweep is applied, the mirror-image response of Fig. 3 will be obtained. The last i.f. trimmers are adjusted so that the two patterns coincide. This procedure is repeated, connecting the generator in turn to each preceding i.f. grid and finally to the converter grid.

Without changing the dial setting of the sweep generator, connect the 'scope vertical amplifier to the ungrounded discriminator cathode. Adjust the discriminator trimmers until a symmetrical pattern like that of Fig. 4 is obtained. If the FM receiver employs a ratio detector, simply follow the instructions given in the table for this case.

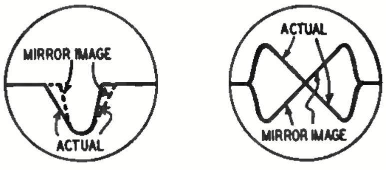


Fig. 3 (left) and Fig. 4 (right)—FM receiver i.f. and discriminator oscilloscope patterns.

The next step is to adjust the oscillator and r.f. sections. The receiver oscillator is restored and the generator connected to the antenna binding posts. The 'scope's vertical amplifier is again connected across the first-limiter grid resistor (in the case of ratio-detector receivers follow the table). The generator dial is set to the appropriate r.f. alignment frequency, and the oscillator trimmer adjusted to give the superimposed i.f. patterns. The r.f. trimmers are next adjusted for maximum amplitude.

The problems encountered in video i.f. alignment are entirely different. Here we are dealing with a passband some 4 mc wide as well as with adjacent trap circuits which must be set up properly. Reference to Fig. 5 reveals that this pattern is not symmetrical. For these reasons it is desirable to observe only one image on the 'scope screen. The output cable labeled 60-CYCLE SINE is connected to the high side of the 'scope's horizontal amplifier. The vertical amplifier is connected across the video second-detector load resistor. The generator output clips are connected from the last video i.f. grid to ground. The phasing control is adjusted to obtain a single image. If this control is not adjusted properly, a double image will be observed, resembling somewhat the mirror-image effect described before.

The output of the generator is progressively moved, stage by stage, from the last i.f. grid through to the converter. Exact responses specified by the manufacturer must be duplicated in each stage. For stagger-tuned systems this cannot be overemphasized. A variation in the pattern response of any single stage could result in a loss of picture contrast and quality.

The 5-mc crystal marker is next turned on. The variable amplitude control of this oscillator (30k in the schematic of Fig. 1) is adjusted to give a convenient-sized pip on the pattern. This pip is a harmonic of the 5-mc oscillator, and in the case of a standard i.f. will lie at 25 mc. If the pip appears at the proper point in the over-all response, the initial alignment procedure may be considered correct.

The next step is to adjust the trap circuits. The 5-mc oscillator is turned off and the 1-mc oscillator employed. A series of pips 1 mc apart will be observed across the i.f. response. One of these will lie at the same spot as the 5-mc pip previously observed. It is then a simple matter to count down or up from this reference pip to determine exact bandwidth and frequency.

The trap circuits are next adjusted in relation to the 1-mc pips. The two marker oscillators should not be used simultaneously, nor need they be. Unless the two oscillator harmonics are exactly equal, an audio voltage is created by the difference. The audio voltage will show up on the pattern unless a filter is employed between the generator and the 'scope. This is not harmful in any way. The oscillators may be brought to zero beat by adjustment of C9 and C9a. The oscillators can be referred to WWV at 5 mc.

All that has been done with these crystal oscillators may be accomplished by the serviceman's own test oscillator, if it can be calibrated accurately, and Model 909.

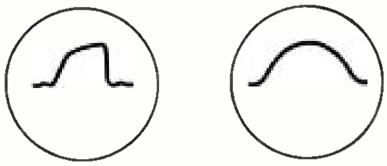


Fig. 5 (left) and Fig. 6 (right)—Video i.f. and television r.f. patterns on 'scope screen.

The next job is to set the oscillator and r.f. sections for all channels. The oscillator is restored to operation and the generator connected to the antenna posts. The receiver is set to the highest channel, and the fine frequency control adjusted half way. The generator is set to the center of the *sound channel* and the oscillator adjusted until the 120-cycle sweep signal is heard in the receiver loudspeaker. All channels are set in this manner, working from the highest to the lowest frequency.

R.f. sections usually require little or no adjustment. Most modern TV receivers employ preset coils, and do not rely on capacitive or inductive compensation. The turns are set at the factory; and if the set is functioning satisfactorily, it is better not to attempt adjustment.

If the set employs capacitive or inductive (slug) compensation, connect the generator to the antenna posts. Connect the 'scope vertical amplifier across the second-detector load, and the 60-cycle control voltage to the high side of the horizontal amplifier. Again one image of the video i.f. response will be observed when the generator is set to the appropriate r.f. channel. The compensating trimmer for the r.f. coil is now adjusted carefully for a slight increase in the height of the image. Start at the highest channel and work down.

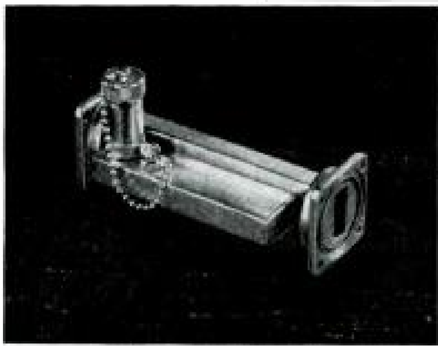
The table can be used as an alignment reference when using either the instruments described or similar apparatus.

MICROWAVES

Part II—An introduction to standing waves, cavity resonators, and representative examples of u.h.f. plumbing

By C. W. PALMER

Photos courtesy DeMornay-Budd



For extracting samples of energy traveling in either direction along a waveguide, directional couplers are needed.

IN Part I of this series we considered a number of the practical factors governing the use of waveguides for ultra-high-frequency transmission and reception.

The use of parallel-wire and co-axial transmission lines becomes impractical above approximately 3,000 mc because of the greatly increased losses as frequency rises. For example, RG/8U co-axial cable, which has a loss of 0.13 db per 100 feet at 1 mc and 2.1 db at 100 mc, has a loss of 18 db at 3,000 mc; and RG/58U cable, which has a loss of 0.24 db per 100 feet at 1 mc, has losses of 4.1 db at 100 mc and 34 db at 3,000 mc. A glance at Fig. 1 shows how loss increases with frequency for these two popular cables.

This explains why such a wide interest has been displayed by u.h.f. investigators in the development of waveguides. The loss in 1 x ½-inch waveguide for frequencies from 6,500 to 12,500 mc was shown in Part I of this series. It drops from 80 db per 100 feet at 6,500 mc to 30 db at 12,500 mc. Similar values of attenuation are found for other sizes of waveguide for their optimum frequency ranges. Also, the waveguide will carry much higher power than co-axial conductor without arcing over.

A waveguide can be used at any frequency above its cutoff point, but a certain band of frequencies is transmitted with the least loss. This is due to the "skin" resistance on the inside of the waveguide, which increases with frequency. Since the penetration of radio-frequency currents into the surface of a conductor (in this case the inside wall of a waveguide) is inversely proportional to the frequency, it follows that at frequencies above some critical point there will be an increase in loss. Table I shows the skin penetration and resistance of some commonly used waveguide electroplating and fabricating metals—the five most commonly used in waveguide construction.

Standing waves

Standing-wave ratio is a term often heard where transmission lines as well as waveguides are concerned. If a length of waveguide is provided with movable ends so that it becomes a closed container, it will resonate at a particular frequency just like a tuned circuit consisting of a coil and capacitor. This is because the voltages are reflected by the end plates and reinforce the applied voltage at one and only one frequency. At this frequency the reflected voltages combine with the applied voltage and thus increase the original voltage at one point in the cavity (where we place the pickup dipole or loop).

This subject of standing waves in transmission lines and waveguides is so important in the practical application of microwave plumbing that it is well for us to spend some time on the subject.

Let us look at Fig. 2 which shows a rope secured to a stationary hook and

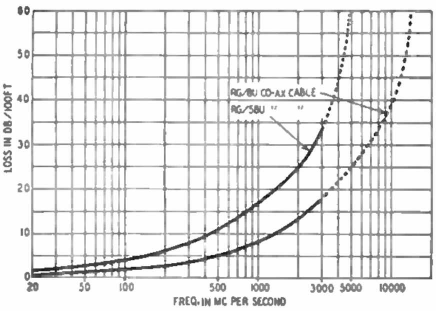


Fig. 1—Graph shows losses in co-axial cable.

TABLE I

R. F. RESISTANCE AND SKIN PENETRATION

Depth of current penetration is given in millionths of a meter (.001 mm).

	100 mc		1000 mc		10,000 mc	
Metal	Ohms	Depth	Ohms	Depth	Ohms	Depth
Silver	.0025	6.5	.008	2.0	.025	.65
Copper	.0026	6.6	.0083	2.1	.026	.66
Gold	.0032	8.2	.0103	2.6	.032	.82
Aluminum	.0034	8.6	.011	2.7	.034	.86
Brass	.005	12.6	.016	40	.05	1.26

swung back and forth to provide a wave motion. If the rope is held at the correct tension and swung back and forth rhythmically (simulating waves of oscillating or alternating voltage), modes will be formed as shown by the cross-over of the solid and dotted lines where the rope remains stationary while other parts of the rope move back and

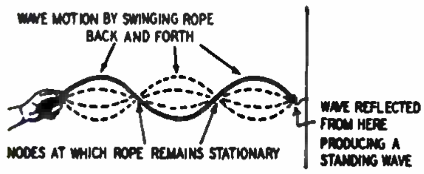


Fig. 2—Swinging rope forms loops and nodes.

forth. This is caused by the wave reflected by the stationary end of the rope producing a standing wave in the motion of the rope.

Now if we have a transmission line of two infinitely long parallel wires connected at one end to a source of r.f. power, as shown in Fig. 3-a, the r.f.

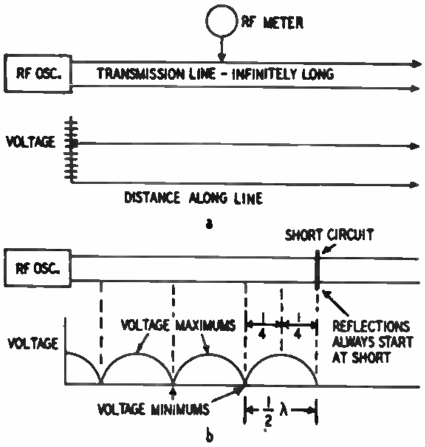


Fig.—3 Standing waves form on shorted line.

voltage will travel along the line with no reflections and there will be no standing waves; but if we provide a short circuit across the line at some point as at b, reflections will occur, with resulting standing waves, voltage maxima and minima along the line at intervals.

If a resistance connected across the transmission line matches the characteristic impedance of the line (depending on the space between the wires and their size), the outgoing signal from the source is completely absorbed by the load and there are no reflections or standing waves. This is usually desirable in connecting a signal source to a load (as in connecting a transmitter to an antenna) since the maximum amount of power is delivered by the source to the load.

When the load is resistive and matched to the impedance of the line, the voltage is essentially the same all along the line; the length of the line is not critical. The impedance is uniform along the line and is equal to its characteristic impedance. The standing-wave ratio is extremely low and there is, therefore, a maximum transfer of energy.

If the load is not matched to the line or is reactive instead of resistive, the signal is reflected back from the load. The standing-wave ratio is high, and the voltage varies greatly from one half-wave position to the next. The length of the line is critical, and there is a loss of power.

All these characteristics of transmission lines with respect to standing waves also apply to waveguides, though the method of determining the standing-wave ratio and correcting for a mismatch or high standing-wave ratio is different.

In waveguides, standing-wave ratio is checked by means of a special section of guide having a narrow slot cut parallel to the axis of the guide (located at the maximum of the electrostatic field). A probe with a crystal detector and a d.c. microammeter is used to indicate the presence of standing waves. The photograph shows a slotted waveguide section that can be used to measure standing-wave ratio, impedance, and frequency.

Cavity resonators

In waveguides all the old circuit quantities, such as inductance, capacitance, resistance, reactance, etc., have their place and usefulness, though their forms are different from those found in lower-frequency work.

A piece of waveguide of the correct length, with the ends closed off, can be used just as are the more common coil and capacitor for a tank or resonant circuit, displaying all the characteristics of a coil-and-capacitor combination without actually containing either coil or capacitor.

The resonant cavity can perhaps be better understood by looking at the sketches in Fig. 4. At a is the usual coil-and-capacitor parallel-resonant circuit. As the frequency is increased, the number of turns on the coil is decreased until eventually only a single turn is required. This is shown at b. Now to reduce the inductance further, several

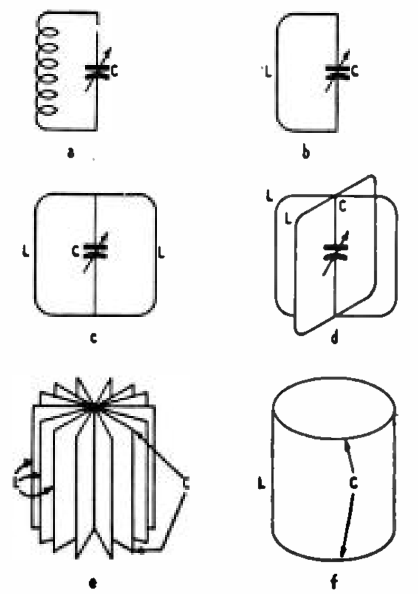


Fig. 4—The evolution of a cavity resonator.

coils are connected in parallel as at c and d. It will be remembered that the inductance of two coils in parallel is less than either coil individually. By adding an infinite number of single-turn coils in parallel, a closed chamber or resonant cavity results as shown in e and f.

Strictly speaking, we should not use the term inductance in a resonant cavity, as the resonance is a result of reflection of radiated waves in such phase as to reinforce their potential. However, this approach does make it easier to understand how a cavity can be tuned to a given frequency.

A rectangular cavity can be resonated at several frequencies by changing the mode. You will remember that we explained the electrostatic and magnetic modes of transfer of energy in waveguides and that, for each mode, one dimension of the guide controls the lowest or cutoff frequency. The choice of mode was made by the type and location of the insertion and pickup probes. The same conditions occur in cavity resonators as in waveguides, in this respect.

In Fig. 5 dimension a, b, or c may be made to control the resonant frequency by changing the position or type (dipole or loop) of the coupling and pickup devices. For any one mode, two side walls control the frequency, and the other walls control the Q or merit factor of the resonator.

In tuned circuits of the coil-and-capacitor variety used at lower frequencies, Q figures up to several hundred are typical. For cavity resonators, Q factors in the *tens of thousands* are not uncommon. In this respect the cavity

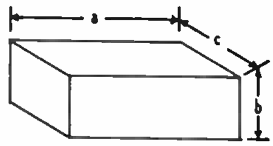


Fig. 5—The critical dimensions of a cavity.

resonator is different from and much more efficient than a low-frequency tuner.

Types of resonators

Cavity resonators take a number of different shapes and forms other than the simple rectangle shown in Fig. 5. For example, some vacuum tubes used for microwaves—notably reflex Klystrons—include a resonant cavity as part of their build-up. The grids form one boundary of the cavity, and the cylindrical bellows is another of the elements from which the output is taken. Figure 6 shows the cross sections of a number of different types of cavity resonators, including the basic principles of the reflex Klystron and Magnetron tubes to be discussed in detail in the next article of this series.

The size and shape of the cavity determine the frequency of oscillation. If the cavity is too small or too large, it cannot resonate at a given frequency; but if it has the correct dimensions, high-amplitude waves are built up be-

tween the reflecting walls. As in waveguides, cavity resonators have different modes of resonance. One pair of opposing walls becomes the frequency-controlling mechanism, while the others affect the impedance and Q of the unit.

Cavity resonators may be tuned by moving the side walls in or out, or tuning slugs may be inserted, as shown in

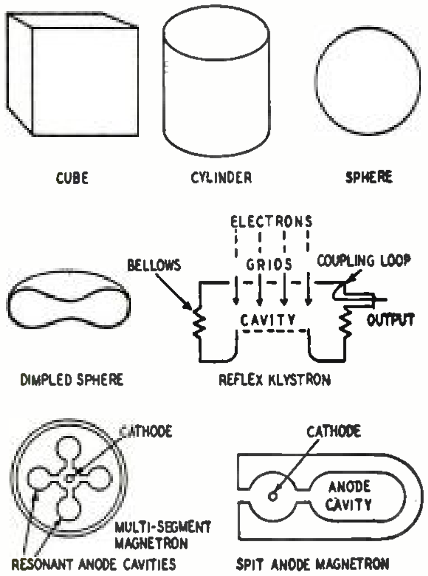


Fig. 6—Resonant cavities take various forms.

Fig. 7, to increase or decrease the frequency. The tuning slugs consist of metal rods that may be moved into or out of the cavity. If the slugs are located in the path of the electrostatic field (depending on the mode), the frequency decreases as the slugs are inserted. If they are inserted in the electromagnetic field, the frequency increases. This is because inserting the slugs in the electrostatic field shortens

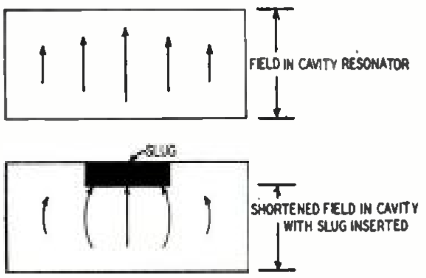


Fig. 7—This cavity may be tuned with a slug.

this field, which is similar to increasing the capacitance of a tuned circuit. Conversely, inserting the slugs in the electromagnetic field decreases that field, which is the equivalent of lowering the inductance.

Samples of waveguide plumbing

We have touched on a number of the factors controlling the individual pieces of apparatus comprising a microwave waveguide setup, but so far we have not pieced them together to form a circuit. Let us look at Figs. 8 and 9. Here we have two setups used for testing purposes. They serve as examples of how the pieces of apparatus are linked together to propagate waves.

Figure 8 shows an oscillator, such as a Klystron or Magnetron, coupled to the following five pieces of apparatus in turn:

1. An impedance meter which consists of a length of waveguide with a longitudinal slot in one wall in which a rod or probe connected to a crystal detector and a d.c. microammeter can be moved.
2. An impedance transformer consisting of a length of waveguide with impedance-adjusting slugs or stubs which change the amount of power reflected back toward the source, thus introducing standing waves of controllable amounts to change the effective impedance.
3. A directional coupler which permits a small sample of the wave to be taken off through a side path without affecting the propagation of the main wave through the guide, except for introducing a certain amount of attenuation. This sample wave is fed through a waveguide or co-axial line to a frequency meter where its frequency can be determined by measuring the distance between the high-voltage or high-current points.
4. Another directional coupler feeding into a power meter or wattmeter permits the power transmitted through the waveguide to be measured. This power meter may be a bolometer or temperature-sensitive resistance element, a power bridge, a water load, or other power indicators (which we will take up in a succeeding article);
5. Last in the circuit is the termination or power-absorbing device, which is used to dissipate the power from the oscillator without radiating it and without introducing reflections that would affect the operation of the measuring devices by introducing a high standing-wave ratio in the line.

This circuit is used to measure the effect of a changing load impedance on the amount of useful power propagated through a waveguide, as, for instance, in changing the antenna of a microwave transmitter.

Fig. 9 shows another test setup for measuring the amount of reflection introduced by a section of waveguide over a wide range of frequencies. Here a Klystron oscillator is amplitude-modulated by a square-wave oscillator and fed into the test circuit, which comprises:

1. A variable attenuator for controlling the power from the Klystron and isolating it from the test setup;
2. A tee section of waveguide coupled to a frequency meter;
3. An impedance meter with slotted wave guide;
4. The section of waveguide under test;
5. A power termination.

The impedance meter is used here to measure any reflection that occurs when the section of guide under test is inserted, over that measured when the termination is coupled directly to the impedance meter. This test is made at a series of frequencies.

In these two examples of waveguide plumbing a number of new items have been described in a rather sketchy manner in order to show the over-all result of applying apparatus to a circuit for a specific purpose. Each of these items will be taken up in turn and described in greater detail in succeeding parts of this series, so that we can build up a working knowledge of the devices and how to use them.

One of the greatest stumbling blocks in the path of microwave development for many years was the inability of ordinary vacuum tubes to either amplify or oscillate successfully at frequencies in the thousands-of-megacycles region. Several factors were responsible. Interelectrode capacitances negligible at more amenable frequencies became prohibitively high at microwaves; leads from the elements to the pins made highly effective—and damaging—inductances; insulation losses and grid emission made u.h.f. oscillation impossible. And perhaps most important, the time required for electrons to reach the plate from the cathode—transit time—became comparable to the period of a single cycle. As a result, the upper oscillation limit of ordinary tubes was between 150 and 175 mc.

How entirely new principles were conceived and developed to achieve amplification and oscillation at frequencies considered impossible of attainment a few years ago will be discussed in Part III of this series. For the technician and experimenter unfamiliar with microwaves, the descriptions of the Megatron, the orbital beam tube, the Klystron, and the Magnetron will open new and exciting fields for thought and experimentation.

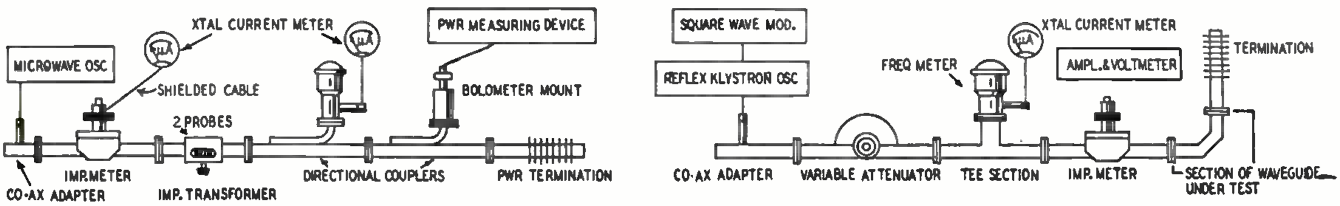


Fig. 8 (left) and Fig. 9 (right)—Two representative circuits using waveguide plumbing illustrate how various components may be combined.

Audio Impedance Matching

Part III—How to calculate loads and construct output transformers

By WALTHER RICHTER*

IN the preceding part of this article (March issue) we laid down the specifications for matching transformers, as far as the impedance transformation is concerned. We shall now see how these transformers can be constructed or picked out from a number of available units. We shall take two examples, a transformer to make a 20-ohm voice coil look like 53.4 ohms, and a multitap matching unit.

The impedance transformation ratio is equal to the square of the turns ratio. The turns ratio required for an impedance transformation is therefore equal to the square root of the impedance ratio. To make 20 ohms look like 53.4 ohms requires an impedance transformation ratio of 2.67. The square root of this is 1.63. This is the turns ratio of the required transformer.

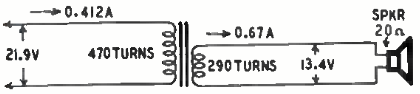


Fig. 1—Specifications, standard transformer.

But the turns ratio does not completely describe a transformer. We also must know how much voltage will be applied across the primary terminals, its frequency, and how much current will flow in the windings. The voltage across the 16-ohm winding of the output transformer, with the 30-watt amplifier operating at full power and properly loaded, was calculated at 21.9 volts (see March article). This voltage applied to 53.4 ohms results in a current of 0.412 ampere. The voltage on the 53.4-ohm secondary will be 13.4 volts (using the turns ratio of 1.63) and the current will be 0.67 ampere. Fig. 1 shows the specifications of the transformer.

While space does not permit a detailed discussion of transformer design, we can give enough information to permit the sound man to make such a transformer on short notice.

As far as wire size is concerned, it is common practice in the design of small power transformers to allow approximately one circular mil per milliampere; in audio work this is more than ample, since most of the time transformers run considerably below full output. A standard wire table shows that No. 24 wire will be satisfactory for the primary and No. 22 wire for the secondary. Larger wire for one or both windings (provided there is sufficient space for the required number of turns) will, of course, be more satisfactory.

The number of turns required depends on the cross-sectional area of the core, the maximum flux density decided on, and the lowest frequency at which the transformer must operate. The formula on which all turns calculations are based is

$$E = 4.44 \times \phi \times n \times f \times 10^{-8} \text{ volts,}$$

where

ϕ is the maximum amplitude of the alternating flux pulsating through the coil, in maxwells or magnetic lines;

n is the number of turns;

f is the lowest desired frequency.

If we wish to find the number of magnetic lines necessary to induce 1 volt in a single turn, we simply solve this formula for ϕ, substituting 1 for E, 60 cycles for f, and 1 for n. The result is 375,000 lines. This is one of the handiest figures to keep in mind, because all transformer calculations become easy with the aid of it.

The relation may be stated in words as follows: If we wish to apply or induce in a single turn 1 volt at a frequency of 60 cycles, a magnetic flux must pulse through it with a peak value of 375,000 lines. For any other frequency, this value of 375,000 lines must be increased or decreased in the inverse ratio of the desired frequency to 60 cycles. Thus, if we wish to go down to 30 cycles per second, a magnetic flux with a peak value of 750,000 lines is required through one turn to induce 1 volt.

A practical problem

Let us assume now that we have available a core with E-shaped laminations, with a center leg ⅞ inch square With the laminations built up in a square stack, the cross-sectional area of the core will be 0.765 square inch. Because of the insulating varnish, only about 95% of this area, or 0.7 square inch, is actually iron.

The maximum magnetic flux which this core can carry is equal to the maximum permissible density in lines per square inch times the cross-sectional area of the iron. In power-transformer design, even for small ones, densities of 60,000 to 75,000 lines per square inch are not uncommon. Such high values require fairly large magnetizing currents, however, which should be avoided in audio transformers. The density should preferably be kept at a lower value, perhaps 50,000 lines per square inch. This multiplied by the area of 0.7 gives 35,000 lines as the maximum flux which should be permitted to pulsate through the core. But, since at 30 cycles it takes a flux of 750,000 lines to produce 1 volt in 1 turn, a flux of 35,000 lines will produce 35,000/750,000 = .0465 volt. This is consequently the voltage per turn; the primary winding, which is to operate with 21.9 volts, must therefore have 21.9/.0465 = 470 turns, while the secondary side will have to have 290 turns.

It remains to be checked whether this amount of copper can be accommodated within the window. If not, the stack height must be increased, which increases the maximum flux the core can carry and consequently increases the volts per turn, with a corresponding reduction in the number of turns required; or the next larger size of lamination may be used.

The amount of copper and the space required for it can be considerably reduced if an autotransformer is constructed. In addition, since 100% coupling exists at least between parts of the primary and secondary of an autotransformer, it has better high-frequency response and better regulation than a two-winding transformer. The fact that in an autotransformer there is no isolation between the primary and secondary is of no consequence in the case of a matching transformer of the type discussed here.

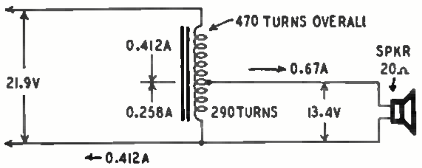


Fig. 2—An autotransformer may save space.

The two-winding transformer shown in Fig. 1 can be converted to an autotransformer simply by making the secondary winding part of the primary winding, so to speak. The transformer will then consist of the single winding of 470 turns, tapped at 290 turns (Fig. 2). The current which will flow in that part of the coil which is common to the primary and secondary circuits will be the algebraic sum of the two currents shown in Fig. 1. Since the direction of the current flowing in the secondary winding of a transformer is opposite to that of the current flowing in the primary winding, the algebraic sum will be only 0.258 ampere in the part of the winding common to both the primary and secondary. This permits the reduction of the wire size of this part of the

* Engineering and Development Dep't, Allis-Chalmers Mfg. Co.

winding; in this case No. 26 wire would be large enough. The arrangement will result in a considerable reduction in the space requirement for the windings, compared to the two-winding transformer shown in Fig. 1. The superiority of the autotransformer is quite important when the turns ratio is between 2 to 1 and 1 to 1. For higher turns ratios, such as 10 to 1, the saving in space is not very significant.

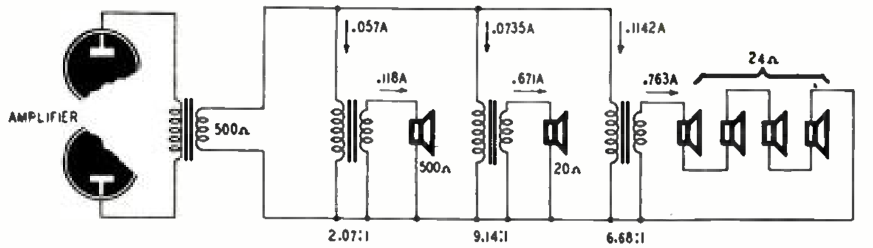


Fig. 3—This separate-transformer hookup can be matched back to tubes or line transformer.

Matching six speakers

As the second design example a single transformer matching all the speakers shown in the March article to the 500-ohm line will be discussed. It was calculated that the 500-ohm speaker taking 7 watts, the 20-ohm speaker taking 9 watts, and the four series 6-ohm speakers taking 3.5 watts each had to appear to the 500-ohm tap on the output transformer as 2,140, 1,670, and 1,070 ohms, respectively. These are impedance ratios of $2140/500 = 4.28$, $1670/20 = 83.5$, and $1070/24 = 44.6$. The square roots of these figures give us the turns ratios 2.07, 9.14, and 6.68, respectively.

A common matching transformer supplying power to all the speakers is again best designed by considering it as the composite of three individual transformers. In Fig. 3 are shown the three individual transformers with the ratios just calculated. The current in the secondary windings will be the primary current divided by the turns ratios.

The primary windings of all three transformers are in parallel with the same voltage across them. If the transformers were constructed with cores of identical size, the number of primary turns would all be the same. The three windings can just as well be placed on a single core, making one winding out of them, and increasing the wire size. The combined primary current is 0.245 ampere, for which No. 26 wire will be satisfactory.

Since the finished transformer must handle 30 watts, we will need a fairly large core, especially if the frequency response is to be good down to 30 cycles. Suppose we can lay our hands on some E-shaped laminations with the center leg 1¼ inches wide. Following the procedure outlined in the preceding example and assuming a square stack, the voltage which a single turn can produce at 30 cycles, with the density in the iron not exceeding 50,000 lines per square inch, will be .099, or roughly 0.1 volt. This will require 1,225 turns for the primary winding for the 122.5 volts which will appear across the 500-ohm primary at 30 watts.

Instead of providing three separate secondary windings, as shown in Fig. 3, we can use the autotransformer, simply providing one continuous winding, tapped at places corresponding to the turns ratios given in Fig. 3. Since the various parts of this continuous winding carry different amounts of current, they may be wound with different sizes of wire, unless the window in the laminations is sufficiently large to accommodate one continuous winding of the largest wire required. The specifications for the complete matching transformer, based on a 1¼ x 1¼-inch stack, are shown in Fig. 4. The reader should have no difficulty convincing himself that this is simply the result of superimposing upon each other all the windings shown in Fig. 3. The currents in the various sections of the transformer, also indicated in Fig. 4, are found by superimposing the current values shown in Fig. 3.

The calculations can be checked for accuracy. The total ampere turns in a transformer—assuming zero d.c. magnetizing current, as we have done in this example—must come out as zero. Multiply the current in each section by the number of turns in this section, adding those in a downward direction and subtracting those in the opposite direction. A correct design will result in zero, within the limits of the accuracy of the calculations.

If the 1¼-inch laminations happen to be of one popular (the "scrapless") type, the window for the coil will be found to have dimensions of ⅝ x 1⅞ inches. This will be ample to accommodate the windings without having to cut each size wire down to the exact requirement given by the current flowing in it. The 183 turns carrying the heavy currents may be wound of No. 19 wire and can be accommodated in five layers. The remaining 1,042 turns can be accommodated in 11 layers of No. 26 enameled wire. If wound reasonably tight, the finished winding will fit nicely into the available space.

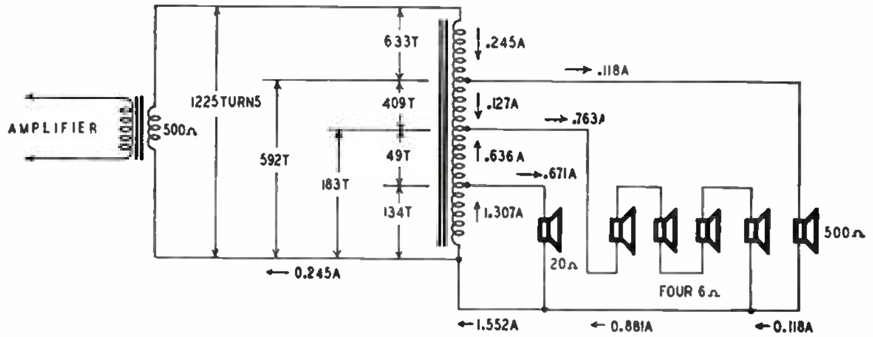


Fig. 4—How the several speakers of Fig. 3 can be fed from a single output transformer.

Changing the load

Will it be permissible to disconnect any one of the speakers with an on-off switch? Naturally, that will mean that the total load presented to the amplifier is not 500 ohms any more. But as pointed out in past articles, the notion that the amplifier will then furnish distorted output is unfounded, provided we see to it that it does not have to furnish more voltage or current than the rated values. The removal of part of the load will cause a rise of voltage; and if the amplifier happened to be operating at full-rated voltage before, it will now operate with a voltage beyond its rating. The input signal must therefore be reduced, so that the total output voltage will not exceed 122.5 volts. If this precaution is taken, there is no objection to removal of part of the load.

The necessity of readjusting the input signal can be avoided by replacing the speaker which is to be taken out of service by a dummy load resistance equal to the voice-coil impedance which was removed. This will of course require a double-throw switch.

The designers of negative-feedback amplifiers often demonstrate with pride the fact that they can connect an 8-ohm speaker to either the 4-ohm, 6-ohm, or 20-ohm tap without noticeable change in volume. If the feedback voltage happens to be taken from the output terminals, such a performance is not at all surprising, since the feedback is essentially a device to keep the output voltage constant regardless of any changes which may have taken place in the amplifier; and a change of the output tap can of course be considered as a change in the over-all amplification from the input terminals to the output terminals. Such a demonstration is quite misleading, because it usually is not made under maximum output conditions. If it is, it will become quickly apparent that, feedback or no feedback, distortion will set in earlier if the load does not have the value recommended by the manufacturer for the particular type of tube used in the output stage.

SWEEP GENERATOR

Precision Apparatus Co., Elmhurst, N. Y.

Series E-400 offers wide- and narrow-band sweep selection for FM and television alignment. Frequency coverage is continuous from 2 to 240 mc in five

bands. Sweep ranges are 0-1 and 0-10 mc. A direct-reading dial has two-color scales; a vernier reads to 1 part in 1500.

TAPE RECORDER

Crestwood Recorder Corp., Chicago, Ill.

The MagicTape recorder has a two-channel feature which allows recording of a full hour's material on a standard half-hour tape. Frequency range is from

50 to 8,000 cycles. Rewind time is less than 1½ minutes for a half-hour reel. The unit is portable, weighing 25 pounds, including microphone and an extra reel of tape.

NEON PILOT LIGHT

Industrial Devices, Inc., Edgewater, N. J.

The Tiny-Glow, a rugged and dependable pilot light consisting of a neon lamp encased in a chrome-plated housing, may be used over a range of 75 to

250 volts and is guaranteed for a minimum of 10,000 hours' use. Power consumption is about 0.1 watt. It is said to operate more reliably under vibration than spring-contact lamp assemblies because all connections are firmly soldered.

KEYING RELAY

Sigma Instruments, Inc., Boston, Mass.

Type 7 J0Z is a sensitive, polarized keying relay for measuring high-speed telegraphy, measuring 1⅛ inches square by 2⅜ inches high when seated. Hermetically sealed, it fits on an octal tube socket. It is serviceable up to 250 w.p.m.

INK RECORDER

Sound Apparatus Co., Stirling, N. J.

Model FRA is a fully automatic recorder which plots a curve of any changing quantity that can be converted into an a.c. or d.c. voltage. Measuring ranges may be selected and recorded on either a logarithmic or linear scale. Typical applications are in sound, strain or pressure, and r.f. field-strength measurements.

The instrument is available in 56 double chart speed combinations from 45 inches per minute to ½ inch per hour and for frequencies from 2 to 200,000 cycles. It is supplied with a standard 10½-inch relay-rack panel, by which it may be mounted in any standard relay rack.

KILOVOLTMETER

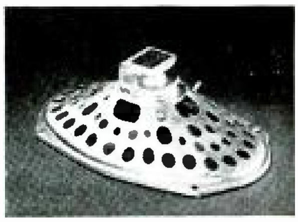
Bradshaw Instruments Co., Brooklyn, N. Y.

Model 4,000 is designed to measure television and X-ray voltages up to 50,000 d.c. It has a 20 μa meter and an input impedance of 1,250 megohms. Basic sensitivity of the instrument is 50,000 ohms per volt. For safety, all voltages are dissipated in the polystyrene probe, test leads are shielded, and the shields are connected together. A NORMAL-REVERSE key is provided so that the probe may be used regardless of the polarity of the voltage being measured.

REPLACEMENT SPEAKER

Quam-Nichols Co., Chicago, Ill.

Model 69A2 Adjusto-Cone speaker is designed for replacement in automobile receivers. Because of its shallow



construction, it will fit most auto receivers, regardless of make, so that the technician need stock only the one type for most cars.

MOBILE AMPLIFIER

Newcomb Audio Products Co., Hollywood, Calif.

Model E-10-M is a rugged low-cost amplifier usable on either 6-volt d.c. or 117-volt a.c. Power output is 10 watts with less than 5% distortion; frequency response ranges from 50 to 10,000 cycles. Five tubes are used, a 6SC7, a 6SF5, two 6V6-GT's, and a 6X5 GT.

A standby switch is included to save battery power when the amplifier is used intermittently.

TV TRANSFORMERS

Chicago Transformer Division Essex Wire Corp., Chicago, Ill.

A new line of transformers for television receivers is now available from stock for manufacturers and technicians. Included are power, vertical blocking-oscillator and vertical scanning output transformers and a horizontal scanning output transformer.

SERVICING MIRROR

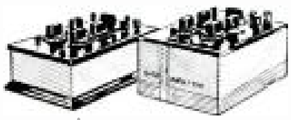
Federal Engineering Co., New York, N. Y.

Many television service technicians feel that only a giraffe is built for the job of adjusting the rear-panel controls of a receiver for the best picture. Neck craning is eliminated by the Picture-Vu, a portable mirror and its collapsible metal stand. The stand is unfolded and set on the floor in front of the receiver. The unbreakable 14 x 10-inch mirror is removed from its cloth bag and hooked to the stand. The technician makes his adjustments in comfort, watching the reflection in the mirror.

WHEATSTONE BRIDGE

Leeds & Northrup Co., Philadelphia, Pa.

The Enclosed Switch Wheatstone bridge, offered previously in a mahogany case, is now housed in a gray, baked-enamel, metal case. Other instruments made by this company will change from wood to metal boxes as soon as engineering is completed.



RECORD PLAYER

Scott Radio Laboratories, Inc. Chicago, Ill.

The three records now available—Columbia's 33 1/3-r.p.m. LP, Victor's 45-r.p.m., and the 78-r.p.m. standard—may be played on this assembly. Two pickups are provided, one for the slow-speed and the other for standard discs. Standards are played automatically, the others manually. A brass collar which may be slipped over the spindle provides for the 1½-inch center hole of the Victor records. The player is an adaptation of the Thorens changer, made in Switzerland and widely used in Scott radio-phonographs. The turntable is governor-controlled.

RECORD CHANGER

Farnsworth Television & Rado Corp., Fort Wayne, Ind.

The new record changer will play all three sizes—12-, 10-, and 7-inch—records automatically, with intermixing of 10- and 12-inch discs permissible. Two speeds are provided, 78 and 33 1/3 r.p.m., each of which is automatically switched in when the correct pickup is inserted. The standard and micro-groove pickups are easily exchanged.

INPUT TRANSFORMER

United Transformer Corp., New York 13, N. Y.

A new transformer designed to match a low-impedance (50 500 ohm) microphone or pickup to a grid is equipped with built-in phone plug and jack. The transfomer is plugged into the micro

phone or phono jack on the amplifier, and the cable from the mike or pickup is plugged into the transformer. Frequency range of the transformer is 50-10,000 cycles, and hum picup is low.

MICROPHONE STAND

Electro-Voice, Inc., Buchanan, Mich.

Model 432 microphone stand, built in three sections, can be used as a banquet stand, set at choir height, or extended to full height for standing speakers. The unit is easily portable, but stable. It has the "red button" height control, which allows change of height without necessity for twisting lock-fittings.

CUEING DEVICE

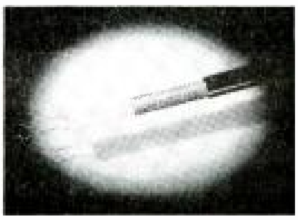
Amplifier Corp. of America, New York, N. Y.

The E-Z-Cue tape and wire indexer is a counter actuated by rotary motion. A flexible shaft extension is placed over the spindle of either the supply or the take-up reel of almost any wire or tape recorder. The counter registers the number of revolutions so that any section of the wire or tape may be identified and located. Average accuracy is within about 1 second on standard spools.

SHIELDED LINE

Federal Telephone and Radio Corp., Clifton, N. J.

A new 300-ohm, balanced, shielded line minimizes noise, ghosts, and snow



on the television screen due to transmission line pickup, often eliminating the need for more elaborate antennas. The K-III line has two inner conductors—crimped at intervals to keep it rigid with respect to the inner tube of insulating material—a shield, and an over-all covering.

ISOLATION UNITS

Chicago Transformer Division,
Essex Wire Corp.,
Chicago, Ill.

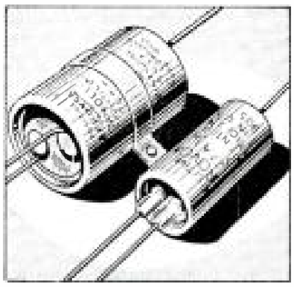
Three new isolation transformers with 50, 150, and 250 volt-ampere ratings are available. They are suitable

for adjusting line voltage or isolating a.c.-d.c. chassis from the line for safety. Secondaries will provide 105 or 125 volts for testing, as well as the standard 115.

ELECTROLYTICS

Aerovox Corp.,
New Bedford, Mass

Stud terminals are used in place of the usual rivet terminals in the new PRS midget dual electrolytic capacitors. These allow a reduction of as much as 40% in the size of the capacitors. Diameters of the new Dual Dandees range from 11/16 to 1 1/16 inches against a previous single size of 1 1/16 inches. Illustration shows new and old types.



PRECISION RESISTORS

Welwyn Electronic Components, Inc.,
New York, N. Y.

New "cracked carbon" resistors manufactured in England are being introduced in this country. The resistance element is a homogeneous film of pure carbon deposited on a porcelain tube. The resistors are unusually stable, according to the maker, and may be expected to adhere to their 1% tolerance throughout their service life. Two- and five-percent tolerances are also available; all may be had in ¼-, ½-, 1-, and 2-watt sizes.

MOBILE CONVERTER

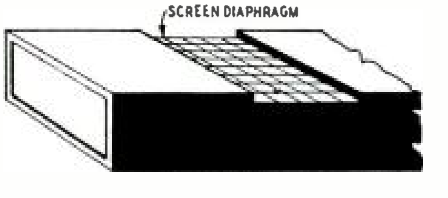
Gonset Co.,
Burbank, Calif.

Model 3-30 is a compact converter which, when used with an automobile broadcast receiver, allows reception of signals between 3 and 30 mc. The converter is powered by the supply in the auto set. A switch on the panel connects the regular car antenna to either the converter or the receiver. A bandspread dial permits logging.

MICROWAVE MEASUREMENT

Patent No. 2,453,533
Lowell E. Norton, Princeton Junction, N. J.
(assigned to Radio Corp. of America)

When a waveguide carries microwave energy, its opposite faces are oppositely charged. Therefore these walls attract each other. If a small section of wall is removed and a fine screen substituted, a relatively large physical displacement occurs.



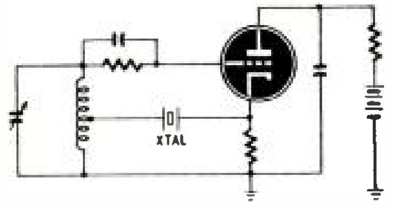
The screen should be light and resilient. It may have about 1,000 conductors per linear inch, and may be constructed by photodeposition. This screen portion acts like a diaphragm. Its displacement is maximum if the microwave energy is modulated or keyed at the resonant frequency of the diaphragm.

The screen carries a tiny mirror which throws light upon a photocell. Displacement of the diaphragm modulates this beam. Photocell output is amplified and indicated on a meter. A direct power reading is obtained when the instrument is calibrated.

CRYSTAL OSCILLATOR

Patent No 2,452,951
Donald E. Norgaard, Scotia, N. Y.
(assigned to General Electric Co.)

The series resonant frequency of a crystal governs the oscillations in this circuit. Holder capacitance and air gap have negligible effect. Plate and filament voltages also have comparatively little effect.



The crystal is connected in series with the coil tap and controls the feedback. Maximum feedback occurs with minimum impedance, that is, at the series resonant frequency of the crystal. This results in a more stable and precise oscillator than is usually obtained.

SECRET TRANSMISSION

Patent No. 2,455,443
David Sarnoff, New York City
(assigned to Radio Corp. of America)

This system preserves the secrecy of messages by using arbitrary symbols instead of letters, and transmitting by facsimile or television. The symbols are chosen for distinctiveness so that they can be recognized even if portions are lost due to noise or interference.

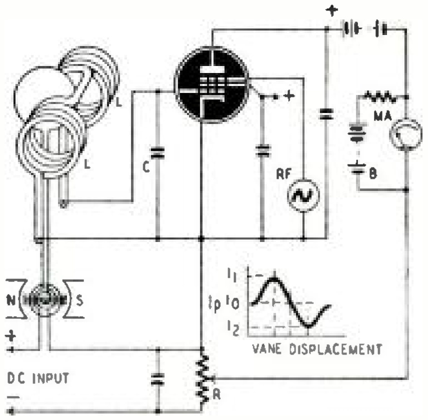
The code governing these symbols may be changed as often as necessary to insure secrecy. At the transmitting end, the teletypewriter may use a conventional keyboard with ordinary letters, but the corresponding symbols are printed. At the receiving end the machine prints letters but the keyboard may be marked with the corresponding symbols. If desired the receiving machine may be operated automatically by the incoming signals.

WEAK-SIGNAL AMPLIFIER

Patent No. 2,446,390
Karl Rath, New York, N.Y.
(assigned to Radio Patents Corp.)

Because of tube noise and other limitations it is very difficult to amplify a weak d.c. voltage such as is obtained from a thermocouple. However, sufficient *current* output may be available to deflect a meter. In this invention the signal is used to deflect a sensitive galvanometer and modulate an r.f. voltage. The r.f. is easily amplified and then detected.

Referring to the diagram, the d.c. signal is connected to galvanometer G and resistor R in series. The meter pointer moves a metal vane between coils L. The coils and condenser C are tuned to approximately the same frequency as the r.f. voltage applied to the suppressor of the tube.



When a weak d.c. signal is applied, the resonant frequency of LC is changed because the vane is displaced. The average plate current then increases or decreases, as shown by the curve. If the galvanometer needle is deflected in one direction, for example, the current may rise from I_0 to I_1. For a change in the opposite direction, there may be a drop from the normal current to I_2. This change may be amplified in further stages before detection, although in this schematic only one tube is used.

The plate current flows through MA, a recording or indicating meter, and then through part of R. This plate current may be several times greater than the original signal; but, by adjusting R, it is made to balance out the original. After each displacement the vane tends to return to its original position until there is another change in the input.

Battery B is used to balance out the static plate current I_0 so that MA indicates zero with no input.

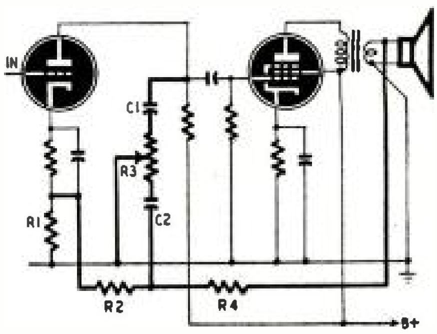
TONE CONTROL

Patent No. 2,444,076
Pierre Visschers, Antwerp, Belgium
(assigned to Int'l Standard Electric Corp.)

This tone control is used with a negative feedback circuit.

C1 and R3 are the high-frequency control components. As the movable arm is adjusted toward the upper end of R3, more high frequencies are bypassed through C1 to ground. Therefore the over-all h.f. response of the amplifier becomes weaker.

The negative feedback circuit from the speaker is composed of R1, R2, and R4. When the movable arm of R3 is adjusted toward its lower end, more highs are bypassed from the negative feedback line through C2 to ground. Then the degenerative effect is greater at low frequencies and highs are effectively boosted.



MONEY BACK GUARANTEE—We believe units offered for sale by mail order should be sold only on a "Money-Back-If-Not-Satisfied" basis. We carefully check the design, calibration and value of all items advertised by us and unhesitatingly offer all merchandise subject to a return for credit or refund. You, the customer, are the sole judge as to value of the item or items you have purchased.

BUILD YOUR OWN OSCILLOSCOPE and V.T.V.M. and *SAVE!!*

5″ OSCILLOSCOPE KIT

Indispensable for AM, FM, and Television. Horizontal sweep circuit 15 to 30,000 cycles. All controls on front panel. Linear sweep with 884 gas triode. Graph screen for measuring peak to peak voltage. Frequency response of horizontal and vertical amplifiers from 50 cycles to 50 Kc. Input impedance 1 megohm and 50 mmfd. Etched panel for long life. Tube complement: 2-6SJ7, 2-5Y3, 1-884, 1-5BP1. Provision for external synchronization, test voltage and intensity modulation. Deflection sensitivity: .30 volts per inch full gain. Detailed instructions and pictorial diagrams included. Operates from 105/-130 V.A.C. 50/60 cy. Nothing else to buy!

$39.95

VACUUM TUBE VOLTMETER KIT

THE MOST USEFUL TOOL ON THE RADIO BENCH!

D.C. and A.C. ranges 0-5, 10, 100, 500 and 1000 volts. Ohm-meter ranges from .2 ohms to 1,000 megohms in steps of Rx1, Rx10, Rx1000, Rx10,000 and Rx1 megohm. Db scale from —20 to +55 Db in 5 ranges. Diode A.C. rectifier. Large rugged 4½″ meter with all A.C. and D.C. readings on one simple scale. 1% accuracy. Complete tubes and test prods. Nothing else to buy!

$23.95

THE NEW MODEL 670

SUPER METER

SUPER METER. A Combination VOLT-OHM-MILLIAMMETER plus CAPACITY REACTANCE, INDUCTANCE and DECIBEL MEASUREMENTS.

D.C. VOLTS: 0 to 7.5/15/75/150/750/1500/7500. **A.C. VOLTS:** 0 to 15/30/150/300/1500/3000 Volts. **OUTPUT VOLTS:** 0 to 15/30/150/300/1500/3000. **D.C. CURRENT:** 0 to 1.5/15/150 ma.; 0 to 1.5 Amps. **RESISTANCE:** 0 to 500/100.000 ohms. 0 to 10 Megohms. **CAPACITY:** .001 to .2 Mfd., .1 to 4 Mfd. (Quality test for electrolytics.) **REACTANCE:** 700 to 27.000 Ohms; 13.000 Ohms to 3 Megohms.

INDUCTANCE: 1.75 to 70 Henries; 35 to 8,000 Henries.

DECIBELS: —10 to +18, +10 to +38, +30 to +58.

The model 670 comes housed in a rugged, crackle-finished steel cabinet complete with test leads and operating instructions. Size 5½″ x 7½″ x 3″.

$28.40 NET

The New Model 770 — An Accurate Pocket-Size

VOLT-OHM MILLIAMMETER

(Sensitivity: 1000 ohms per volt)

Features:

Compact-measures 3⅛″ x 5⅞″ x 2¼″. Uses latest design 2% accurate 1 Mil. D'Arsonval type meter. Same zero adjustment holds for both resistance ranges. It is not necessary to readjust when switching from one resistance range to another. This is an important time-saving feature never before included in a V.O.M. in this price range. Housed in round-cornered, molded case. Beautiful black etched panel. Depressed letters filled with permanent white, insures long life even with constant use.

Specifications: 6 A.C. VOLTAGE RANGES: 0-15/30/150/300/1500/3000 volts.
6 D.C. VOLTAGE RANGES: 0-7½/15/75/150/750/1500 volts.
4 D.C. CURRENT RANGES: 0-1½/15/150 Ma. 0-1½ Amps.
2 RESISTANCE RANGES: 0-500 Ohms. 0-1 Megohm.

The Model 770 comes complete with self-contained batteries, test leads and all operating instructions.

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THE NEW MODEL 777

20,000 OHMS PER VOLT!!

TUBE & SET TESTER

Tube Tester Specifications:

★ Tests all tubes including New Miniatures, etc. Also Pilot Lights. ★ Tests by the well-established emission method for tube quality, directly read on the scale of the meter. ★ New type line voltage.

V.O.M. Specifications:

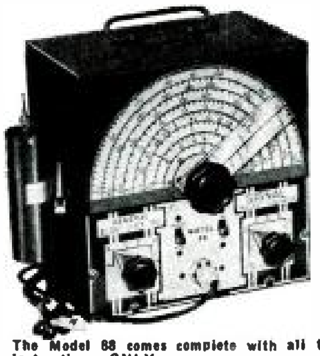
* **D.C. VOLTS:** (at 20,000 Ohms Per Volt), 0 to 7.5/15/75/150/750/1,500 Volts.
* **A.C. VOLTS:** (At 10,000 Ohms Per Volt), 0 to 15/30/150/300/1.500/3.000 Volts.
* **D.C. CURRENT:** 0 to 1.5/15/150 Ma. 0 to 1.5 Amperes.
* **RESISTANCE:** 0 to 5.000/50.000/500.000 Ohms. 0 to 50 Megohms.

Model 777 operates on 90-120 volts 60 cycles A.C. Housed in beautiful hand-rubbed cabinet. Complete with test leads, tubes, charts and detailed operating instructions. Size 13″ x 12½″ x 6″.

$59.95 NET

The Model 88 — A COMBINATION

SIGNAL GENERATOR AND SIGNAL TRACER



*Frequency Range: 150 Kilocycles to 50 Megacycles. *The R.F. Signal Frequency is kept completely constant at all output levels. *Modulation is accomplished by Grid-blocking action which is equally effective for alignment of amplitude and frequency modulation as well as for television receivers. *R.F. obtainable separately or modulated by the Audio Frequency.

Signal Tracer Specifications:

*Uses the new Sylvania 1N34 Germanium crystal Diode which combined with a resistance-capacity network provides a frequency range of 300 cycles to 50 Megacycles.

The Model 88 comes complete with all test leads and operating instructions. ONLY

$28.85 NET

20% DEPOSIT REQUIRED ON ALL C.O.D. ORDERS

GENERAL ELECTRONIC DISTRIBUTING CO.

DEPT. RC-5, 98 PARK PLACE, NEW YORK 7, N. Y.

FM Set Installed in Car

An FM installation in your car can give you better sound, less noise

By MAX ALTH

THE shape of FM things to come was outlined in miniature by Andrew's Radio Service Company of Yonkers, N. Y., when Andy, at the behest of Harry Taubin, of the Bronx, installed an FM tuner in the latter's '47 Buick.

While this is by no means the first FM installation in a car, this is the first FM *broadcast receiver* installation of which this writer has heard. The forecast is that auto radios of the near future will incorporate an FM band, or even possibly be designed for FM reception only.

The results, Mr. Taubin relates, are satisfactory. The quality of reception is very good in town, and is satisfactory up to about 35 or 40 miles from the city, at which distance ignition noise begins to compete with the signal. However, Mr. Taubin could not drive very much further from town without losing considerable AM signal, either. It is only the fact that there are other AM stations along the way that enables him to receive AM programs over a greater road distance than FM signals. When FM stations increase in number, as they are doing right along, it is conceivable that FM auto receivers will supplant AM sets entirely.

FM reception in the city is considerably superior to AM reception, Mr. Taubin reports. Noise is less, sound quality is better and—this is, of course, a personal point of view—the FM programs are better.

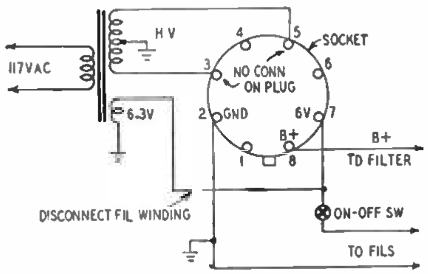
The installation consists of a converted Meissner 8C FM tuner feeding the audio section of the Buick auto receiver.

Surprisingly enough, the regular AM antenna already installed in the car is used. The only change is a reduction in antenna length for FM use. It has been found that maximum FM signal is picked up with the antenna extended half way. Since there is sufficient AM signal strength in the city, the antenna is left half extended all the time the car is in town, for reception of both AM and FM.

Converting tuner and receiver

The conversion of the FM tuner from 117 volts a.c. to 6 volts d.c. is simple. The 6X5 rectifier tube is removed; the transformer and power wiring are left in place for future use.

An octal plug is wired to the car radio. Ground is connected to pin 2, the high side of the 6-volt battery to pin 7, and B-plus to pin 8. When this plug is inserted into the tuner's 6X5 socket, filament and plate voltages are furnished the tuner, as shown below. Disconnect the high side of the tuner's filament transformer from the filament circuit. Remove the on-off switch (part of the tuner's volume control) from the transformer primary and connect it in the filament circuit, as in the diagram. Disconnect the shielded wire leading to

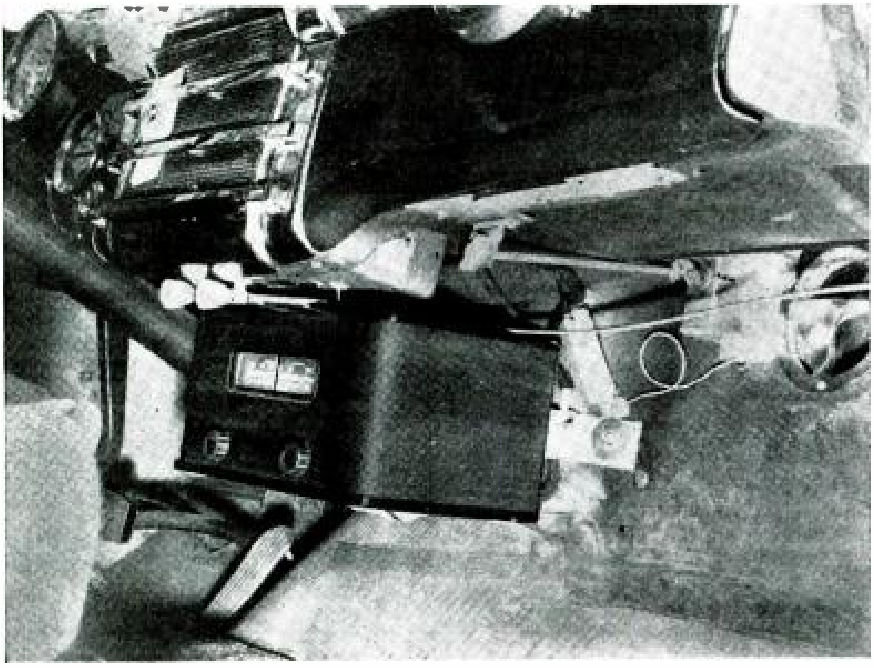


Power cable plugs into original 6X5 socket.

the grid of the 6C4 output tube from the arm of the volume control and solder it permanently to the high side of the control so that volume will always be maximum.

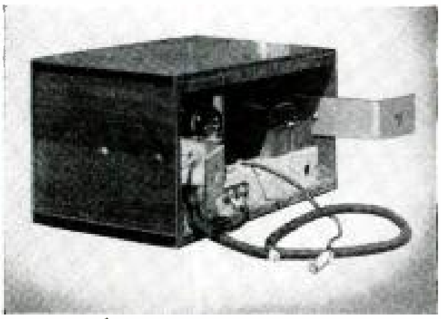
The tuner is mounted in the car by means of two home-made metal brackets. These are bolted to the fire wall of the car and to the sides of the wood cabinet that houses the tuner. The cabinet is strong enough for this purpose. A hole is drilled in one of the brackets, and an antenna-change-over toggle switch is mounted here. A receptacle for the plug on the end of the antenna lead-in is mounted next to the switch, and a length of shielded antenna wire is run from the switch to the AM-set antenna input.

A hole is drilled in the side of the AM set, through which the power leads to the tuner are brought. The AM detector output is disconnected from the volume control and connected to one end contact of a toggle switch. A lead is run from the other end contact through a length of shielded wire to a female bayonet socket. This takes the FM audio output *via* the plug that comes with the tuner. The center contact is wired to the a.f. amplifier of the AM set. The toggle switch is mounted on the side of the AM set, permitting the AM audio amplifier to be connected to either the FM or the AM signal. The volume control of the AM set, up on the dash of the car, controls the volume of either.



The tuner is mounted beneath the regular car radio where the driver can easily adjust it.

To operate the AM receiver, the set is turned on, and the audio and antenna toggle switches are thrown to the AM side. The on-off switch turns the tuner filaments off, as they are not used.



Brackets and antenna switch on tuner's rear.

To receive FM programs, the filaments are turned on and the two toggles thrown to FM. The AM receiver must, of course, be on, as well, as its A.F. section is used.

Little difference in signal strength is found when the antenna is adjusted for the various frequencies on the 88-108-mc FM band.

NBC SYNCS CARRIERS

The first use of carrier synchronization for television stations was announced recently by David Sarnoff, chairman of the board of RCA and the National Broadcasting Company. Stations WNBT and WNBW, New York and Washington outlets of the network, both operate on channel 4. In some locations between the two transmitters, viewers get co-channel interference, due largely to the slight difference in frequency of the two carriers. Even though crystal-controlled, this slight difference is inevitable at television frequencies. The beat effect usually destroys reception from both stations. It appears on the screen as horizontal black and white sound bars.

The problem of keeping the frequencies of the two transmitters precisely equal is solved by synchronization. Two sync units are used, one at WNBW in Washington, the other at RCA Laboratories in Princeton, N. J., between New York and Washington.

Receivers set up in Princeton compare the frequencies of WNBT and WNBW. Information about the difference between the two is translated into variations in the frequency of a 1,000-cycle tone, which is transmitted by telephone line from Princeton to New York. The audio frequency variations (± 300 cycles) are used to control WNBT's frequency, keeping it in exact step with that of WNBW.

Though synchronization of television carriers is a recent development, some AM stations have been operated on this basis for many years. Television engineers hope that the new technique will hasten the end of the freeze on TV station allocations; one of the main reasons for the stoppage was that a study had to be made of co-channel interference to determine future allocation policies.

European Report

By Major Ralph W. Hallows

RADIO-ELECTRONICS LONDON CORRESPONDENT

HOW loud do you like your radio to be? Most people, I suppose, would reply something like this: "If I'm *listening* to a program, I want music to come through loud enough to sound real. Speech from the loudspeaker should have about the same sound level as the voice of a friend talking to me in the room where the radio set is used. But if the radio is just providing a background of which I'm pleasantly conscious though I'm not actively listening, then the volume I want from the loudspeaker is quite low." Fine! But the radio engineers who design our receivers do so first by spoiling vast areas of paper by covering them with figures and mathematical signs. There are no combinations of signs and figures which of themselves indicate "friend talking," or "room where the radio set is," or "loud enough to sound real," or "quite low." What the designing engineer wants before his paper-spoiling activities start are just cold, hard decibels! And, if asked to state his preference in terms of decibels, the ordinary listener might well reply that he couldn't see how the lady who painted her face, fell out of a window, and was eaten by dogs came into the question at all. What had Jezebel to do with radio reception anyway?

The BBC recently set some of its engineers the task of finding out and measuring the various degrees of loudness preferred by several different kinds of people, ranging from transmitting engineers and professional musicians to ordinary listeners of both sexes, all types, and all ages. The results were embodied in a report by two of them, T. Somerville and S. E. Brownless, which contains a good many surprises. The measurements are stated in decibels above a reference level of 10^{-16} watts per square centimeter. From practical experience of their likes and dislikes I expected to find that broadcasting engineers preferred loud reception. They do; on the average they prefer all sorts of programs to come in at a level 13 db above that which best suits the ordinary listener: engineers +88 db, listeners +75 db. Musicians also like more volume than most of us do, but here the difference is smaller—only 80 db against 75 db. What does surprise me is that among ordinary listeners, a very large number of whom were tested, men like more volume than women and advancing years causes a preference for smaller and not greater volume. Taking the mean of the combined measurements for both sexes on symphonic music, light music, and speech, the 15-year-olds like +76 db; the 25-year-olds, +75 db; the 35-year-olds, +74 db; the 45-year-olds, +73.5 db; the 55-year-olds, +73 db; and the 65-year-olds, only +70 db.

"Singing" TV antennas

Though it was unusually mild, the past winter was a very windy one in Britain and many folk who installed TV had considerable annoyance from the loud and incessant singing noise due to the vibration of tubular dipole antennas. Probably some of you in the States have had the same trouble. Here's a remedy recommended by one of our firms specializing in TV antennas, which is very effective, as I can testify personally. It's very simple, like so many good things. All you need to do is pack the tube with sawdust for about 12 inches on either side of the supporting arm. And that is easily done without dismantling the antenna. Remove the plugs at the ends, then push down as much sawdust as is needed. Push down also a wad of rags at each end to keep the sawdust in place. Replace the original plugs and there you are. No antenna so treated can keep you awake at nights by singing and whining as the wind makes it vibrate.

British TV progress

Speaking of TV calls to mind the fact that there are now over 100,000 televisers operating in British homes. That figure may not seem very large to you; but remember that we have still only one transmitting station in action. Recall, too, that less than two years ago the number of owners of TV receivers was not more than 18,500, as I reported in these notes. You'll see that television is going ahead pretty fast here. The reason why there are not more televisers in use is not that people are coy about buying them; it is simply that for several reasons the supply from the manufacturers can't keep pace with the demand from would-be owners. That may seem absurd to you, but it isn't so strange as it looks at first sight. A very considerable proportion of our radio manufacturers' output consists of radar and radio navigational aids for shipping and for commercial planes (that's one reason why there's a shortage of cathode-ray tubes for televisers), and another big proportion has to be devoted to gear which has been made for export.

There are whispers that a battery-operated receiver is soon to be on the market here. It's still all very hush-hush, and I can't get authentic details; but a little bird tells me that high-efficiency superhet circuits, some novelties in time-base makeup, and the use of a small electrostatic C-R tube enable it to give results with a surprisingly modest number of tubes and no out-of-the-way drain on A- or B-batteries. Well, here's hoping!

Broadcast antennas classified

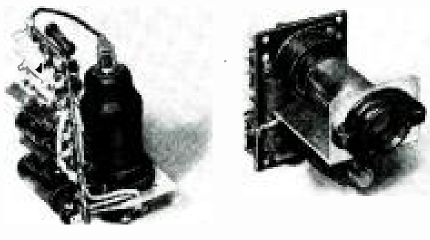
A useful piece of work has been done lately by our Radio Component Manufacturers' Federation in classifying three types of antenna commonly used for broadcast-band reception and working out a figure of merit for each. They did not find it possible to do anything about outdoor antennas of the T or inverted-L types, since these vary so much in effective height, location, insulation, shielding, and so on. For similar reasons the antenna slung indoors in the attic or fixed round a picture rail doesn't lend itself to classification. But outdoor rod antennas are being used more and more and with them a broad classification, based on the performance to be expected, is possible. The radio dealer can be given figures which enable him to tell a customer with fair certainty which kinds of antennas will and will not give the most satisfactory results.

The drawing shows the three chief types of rod antennas. Those in class A are from 10 to 20 feet in length with their tops not less than 50 feet from the ground; for class B, lengths are usually below 15 feet, and maximum heights 25 feet; the class C antenna is fixed to the window ledge of a ground-floor room and is seldom over 10 feet long or 12½ feet in maximum height. The figure of merit for class A is 1.5; for class B, 0.75; and for class C, 0.075. Assuming that the minimum signal input needed for the broadcast receiver is 1 millivolt, the type of antenna required can be worked out with something like certainty, provided that the field strength of the weakest station to be received is known or can be measured. Multiply the field strength in millivolts per meter by the figure of merit and the answer is the input in millivolts to be expected. So long as this comes to 1 or more the antenna in question will do what is needed. Any of the three types, for instance, is suitable for field strengths over 14 mv; class A or class B will give good reception on field strengths above 1.4 and below 14 mv, though class C will not; below 1.4 mv only class A will do, and it can be relied on for field strength down to about 1400 microvolts per meter.

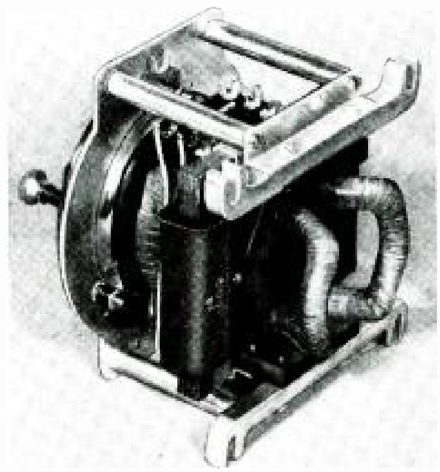
FRENCH RADIO COMPONENTS

THESE three photos, contributed by Mr. E. Aisberg, editor of the French magazine *Toute la Radio*, show the most interesting pieces exhibited at the annual French Parts Show (Exposition de la Pièce Détachée). A striking feature of the show, reports Mr. Aisberg, is the large number of prefabricated tuning assemblies. These pretuned assemblies are used by technicians to construct custom-built receivers, which are much more common in France than in the United States.

These miniature tuning assemblies include all r.f. and oscillator coils for three frequency bands. The main control operates a movable iron core. Matchbox points up the small size.



These are assemblies for small test instruments. At the left, a 1000-cycle oscillator for use as a bridge signal source; at the right is an electron-ray balance or null indiator.



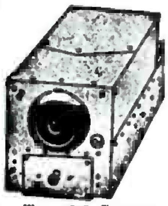
Focus and deflection coils for a CR tube.

Not only are assemblies for receivers sold, but also prefabricated assemblies for test instruments, and even one for a magnetically deflected television tube. Apparently the French radio technician also constructs televisers for himself and others.

The test-instrument assemblies pictured indicate that he may also be inclined to roll his own meters of various types.

HAMS! EXPERIMENTERS! LOOK AT THESE TERRIFIC BUYS!

ARMY AIRCRAFT RECEIVER—BC-946-B



Covers 520 Kc to 1500 Kc Broadcast Band. 6 Tubes: 3—12SK7, 1—12SR7, 1—12A6, 1—12K8. Designed for dynamotor operation; can be easily converted to 110 volt or 32 volt use. Two IF Stages. Three-gang tuning con. BRAND NEW, in sealed carton, with tubes and instruction manual, less dynamotor **$24.50**

Dynamotor DM-32A $2.95

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BC-645 XMTR RECEIVER
15 Tubes 435 To 500 MC

BRAND NEW!

$11.95 each

The electronic equipment that saved many lives in the war. Set can be modified to use for 2-way communication, voice or code, on following bands: ham band 420-450 mc, citizens radio 460-470 mc, fixed and mobile 450-460 mc, television experimental 470-500 mc. 15 tubes (tubes alone worth more than sale price!): 4—7F7, 4—7H7, 2—7E6, 2—6F6, 2—955 and 1—WE316A. Now covers 460 to 490 mc. Brand new BC-645 with tubes, less power supply in factory carton. Shipping weight 25 lbs.

PE-101C DYNAMOTOR for above BC-645 .... **$2.95**

UHF ANTENNA ASSY. for above BC-645 .... **$2.45**

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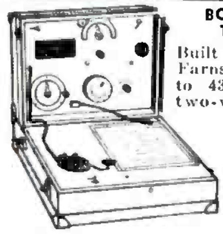
Receives A-N beam signals, operates on 24-28 V DC. 5 Tubes: 3—14H7, 14R7, 28D7. Tunes 195 to 420 Kc. Size 4"x4"x6¾" wide. 4 lbs. In original carton. BRAND NEW **$7.95**

BC148 RECEIVER-TRANSMITTER



Built for Sig. Corps by Farnsworth. Range 3960 to 4360 Kc. Complete two-way communications. Operates on batteries or hand generator. CW operation, handkey on base. Entire unit in two hinged parts. (Xmtr & Rcvr. and Battery compartment) closes down to 15½"x14½"x8½" overall. Less tubes and batteries. Operating instructions included. Used, clean. Each **$5.95**

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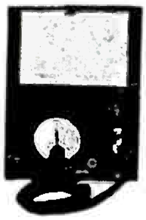

Excellent for measuring DC voltages, bias voltages, or checking polarity of DC voltages. Designed originally for telephone and teletype voltage measurements. With adaptor plug, schematic, metal carrying case. Batteries not needed for operation. Your cost, only **$5.95**

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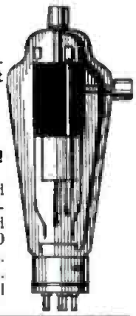
Brand New MERCURY RECTIFIER



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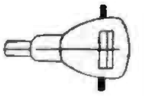

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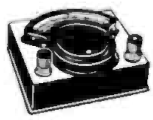

A terrific buy! 3½" easy reading scale. 75 divisions. Black plastic case 4½"x5¼"x2¼". Rubber covered test clip leads plus black metal carrying case with hinged cover. **Brand New.** Wonderful for automotive, battery charging, general test work. Value $25. All yours for only **$3.99**

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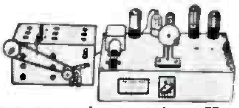

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Genuine Sig. Corps Mike, 200 ohm, single button, has press-to-talk switch, 4-ft. rubber cable, amphenol plug. Beautiful satin chrome finish. BRAND NEW..... **$2.25**

SELSYN 2J1G1

Operates from 57½ V 400 cycles. Suggested wiring for 110 V 60 cycle included. Used, tested.

Price per pair...... **$3.50**

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Type EE8—Talk as far as 17 miles. Dependable 2-way communication at low cost. Ideal for home, farm, field. Up to six phones can be used on one line. Each phone complete with ringer. Originally cost gov't. $39.90 each.

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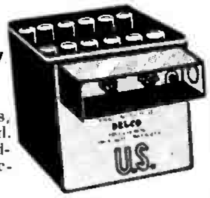
Please include 25% Deposit with order—Balance C.O.D. MINIMUM ORDER $3.00. All Shipments F.O.B. Our Warehouse N.Y.C.

G & G GENUINE MAJESTIC **RADIO PARTS SERVICE**
53 VESEY STREET • NEW YORK 7, N.Y.

TERRIFIC VALUE 24-VOLT STORAGE BATTERY, BRAND NEW 17 AMP. HRS.



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WILLARD 2-VOLT STORAGE BATTERY
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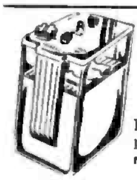
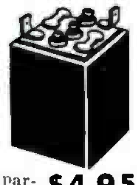


Exact replacement for GE portables—brand new. Each...... **$1.95**

GOULD 6-VOLT STORAGE BATTERY



Navy Standard, Black Rubber Case. BRAND NEW. 15 Amp. Hour Rating **$4.95**

WILLARD 6-VOLT STORAGE BATTERY

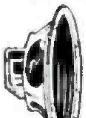
Similar to above but in transparent plastic case. Real value at... **$4.95**

1-QUART BOTTLE BATTERY ELECTROLYTE

Made by Willard, for above storage batteries, 1 qt. sufficient for two 2-volt cells. Hermetically sealed. SPECIAL, per qt. bottle **$1.25**

7-PRONG 2-VOLT RADIO VIBRATOR for Portable and Farm Sets Replacement for GE LB 530.......... **$1.65**

LOOK AT THESE PM SPEAKER BUYS!



Alnico V, 4" PM, less trans.	$1.30
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Alnico V, 8" PM, less trans.	2.75
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Alnico V, 12" PM, less trans.	4.95
Alnico V, 6" PM, with trans.	2.35
Alnico V, 8" PM, with trans.	3.25
Alnico V, 10" PM, with trans.	4.65
6V6—Midget Output Trans.	42c
50L6—Midget Output Trans.	42c
ACDC—Chokes	32c

Wonderful Condenser Buys!
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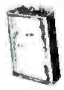
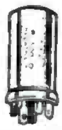
All Brand New—Perfect—Standard Makes



.1 mf 400V..14c	4.0 mf 600V.79c
.5 mf 600V..17c	3-3 mf 600V.88c
2.0 mf 600V.34c	.25 mf 600V $1.79
1.0 mf 1000V.49c	8 mf 1000V 2.25
1.0 mf 1500V.69c	

FP TYPE FILTER CONDENSERS
Standard Makes—Brand New



30 mfd 50 V	12c
100 mfd 50 V	17c
40/40/20 mfd 150/150/20 V	35c
8 mfd 500 V	38c
16 mfd 500 V	49c
8x8 mfd 500 V	59c
20/20 mfd 450/25 V	59c
30 mfd 350 V	55c

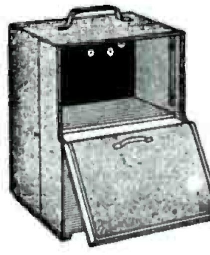
TUBULAR 50+30 Mfd 150V NEW..........lots of 12, 19c ea.

20 Mfd 200 V INVERTED CAN SCREW MT 29c

4/3 Mfd 400/475 V Round Metal Can Com neg 39c

60 Mfd 110 V 60 cy. AC motor start Cond. round metal can 99c

FREQUENCY METER CABINET

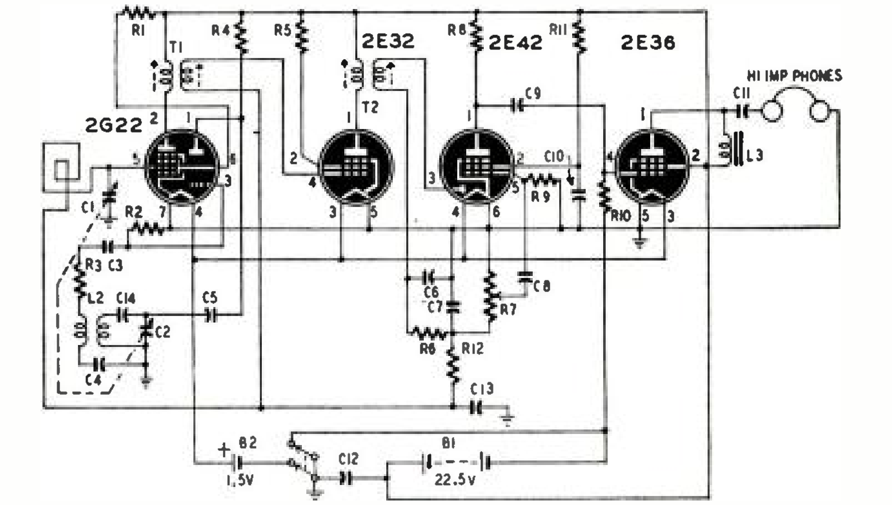


For BC-221 Series freq. meters. BRAND NEW! 3 compartments. Massively built. 14½x10¼x10". Value $20.00. Complete with canvas cover for both ends. Yours for only **$3.95**

SUBMINIATURE-TUBE RECEIVER

? *Please give me a diagram for a small receiver using subminiature tubes.—H.J.W., Sea Cliff, N. Y.*

A. The receiver shown in the diagram uses four subminiature tubes operating with a 22.5-volt B-battery. The converter is a 2G22, the i.f. amplifier is a 2E32, and the 2E42 is used as second detector and first audio. The 2E36 output amplifier plate circuit uses an audio choke (almost any value will do) as a load so that d.c. can be kept off the phones. This will be useful if crystal phones are used. Because the 2E32 is a sharp-cutoff tube, the a.v.c. will not be as effective as in some receivers, but it will be of some help.

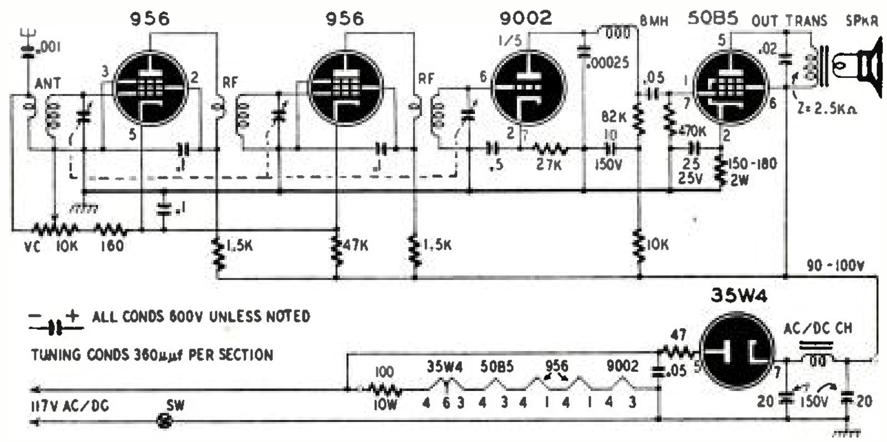


R1, R5—15,000 ohms, ½ watt
R2, R6—47,000 ohms, ½ watt
R3—100 ohms, ½ watt
R4—27,000 ohms, ½ watt
R7—1-megohm potentiometer
R8—1 megohm, ½ watt
R9—10 megohms, ½ watt
R10—5 megohms, ½ watt
C1, C2—365-μμf, 2-gang tuning capacitor
C3, C6—100-μμf mica
C4, C10, C13—.03-μf, 150-volt paper
C5—.001-μf, 150-volt paper
C7—50-μμf mica
C8, C9—.01-μf, 150-volt paper
C11—0.1-μf, 150-volt paper
C12—10-μf, 50-volt electrolytic
C14—250-μμf mica
L1—broadcast loop antenna
L2—broadcast oscillator coil
L3—audio choke
T1, T2—456-kc i.f. transformers
B1—22.5-volt battery
B2—1.5-volt battery
SW—d.p.s.t. toggle switch

T. R. F. SET WITH ACORN TUBES

? *Please show a design for a t.r.f. broadcast-band receiver using five miniature tubes.—C.F.M., Brooklyn, N. Y.*

A. The complete circuit is given in the schematic. The antenna and r.f. coils are standard commercial broadcast units. Low-priced surplus acorn tubes are used in r.f. and detector stages.



FIXED-TUNED CONVERTERS

? *Please print a circuit of a fixed-tuned converter for use with my standard automobile receiver. I want to cover the 4.5- to 5.5-mc and 8.5- to 10.5-mc bands by using the tuning control on the receiver.—E.A., East London, South Africa.*

A. Fixed-tuned converters usually have a stable oscillator and a bandpass input circuit that covers a given band of frequencies. The oscillator signals beat with signals in the passband of the input circuit to produce heterodyne or beat notes within the tuning range of the receiver. It is very difficult to design a suitable bandpass circuit to operate over the bands you want to cover. Furthermore, the beats between the desired signal and the fixed oscillator must fall within the tuning range of the receiver. A 3.9-mc fixed oscillator will produce 600- and 1,600-kc heterodynes when mixed with 4.5- and 5.5-mc signals, respectively. These signals are within the broadcast band so they can be received on a broadcast set. The weak point in this setup is the bandpass circuit, which must be 1 megacycle wide.

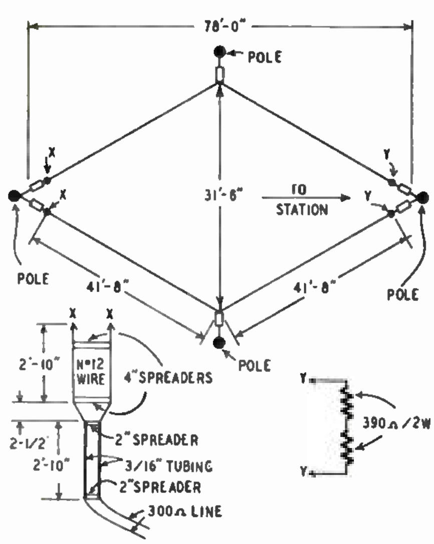
A 7.9-mc fixed oscillator will beat against an 8.5-mc signal and produce a 600-kc heterodyne, and against a 9.5-mc signal to produce a 1,600-kc heterodyne. The receiver would have to tune from 600 to 2,500 kc to cover the 8.5- to 10.5-mc band with a fixed tuned converter.

I suggest you use a tuned converter and use the receiver as an i.f. stage. The circuit shown on page 36 of the April, 1948, issue of RADIO-CRAFT can be modified to meet your needs. The transformer in the plate circuit of the 6K8 should be tuned to 600 kc or some quiet spot on the low-frequency end of the broadcast band. The oscillator padders and trimmers should be adjusted so the oscillator and antenna circuits track over the tuning range. Narrow segments of any band can be covered with a bandspread control consisting of ganged 35- or 50-$\mu\mu f$ capacitors connected across the main tuning capacitors.

RHOMBIC FOR LOW-BAND TV

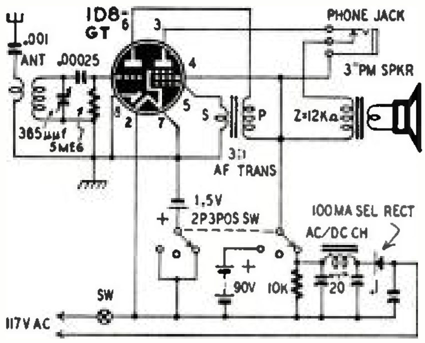
? *Please outline a horizontal rhombic antenna suitable for receiving TV stations on channels 3 and 5. This is to be used with a receiver with 300-ohm antenna input terminals.—J.W., Randolph, Wis.*

A. The sketch shows a rhombic suitable for any low-band station. This antenna should be terminated with two 390-ohm 2-watt metallized resistors. A matching section composed of two 34-inch lengths of No. 12 wire spaced 4 inches apart and two 34-inch lengths of 3/16-inch tubing spaced 2 inches apart. The sections are connected with 2 inches of No. 12 wire. The tubing connects to standard 300-ohm line.



1-TUBE RECEIVER

Using only one tube, this receiver operates from 117 volts a.c. or d.c. or from batteries. A 1.5-volt filament battery is used at all times. A two-circuit, three-position rotary switch selects battery or line operation. In the center position of the switch the set is turned off entirely.

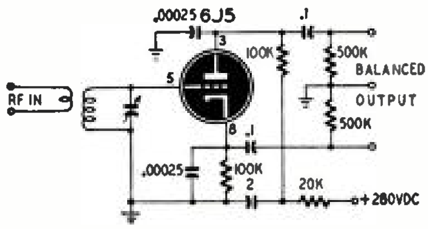


The circuit is a grid-leak detector operating directly from the standard antenna coil. A 100-ma selenium rectifier is used in the a.c.-d.c. power supply. A small PM speaker is built into the set, but a circuit-transfer phone jack provides for headphones. When they are plugged in, the speaker goes off as in most communications receivers.

An antenna is necessary for best operation. An automobile whip works nicely but almost anything will be satisfactory.—JOHN S. ZVERLOFF

BALANCED DETECTOR

Some audio amplifiers which have push-pull from beginning to end give excellent results. It occurred to me that a balanced AM detector would work better with these amplifiers than the usual single-ended one. It would require no phase inverter and would have the inherent advantages—distortion cancellation and so on—of any balanced circuit.

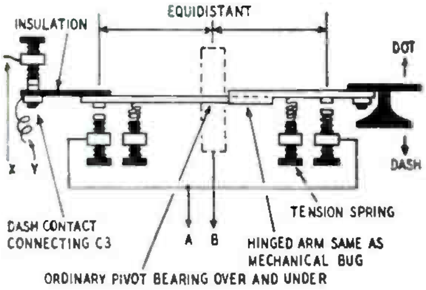


The diagram shows the best one found so far. It is an infinite-impedance detector with the load divided between plate and cathode circuits. Because the infinite-impedance characteristic makes for a minimum load on the tuned circuit, selectivity is often enough to allow omission of an r.f. amplifier stage. In my location, four high-power stations can be separated without any difficulty with only a 6SK7 feeding the detector.—FRANK S. GUE

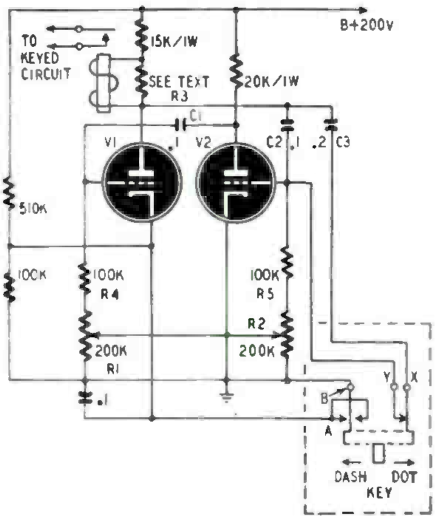
(The circuit looks useful, but may not be as selective as suggested. Two of the Edmonton stations have 5 kw, one 1 kw, and only one 50 kw of power.—*Editor*)

AN AUTOMATIC BUG

The electronic keyer described in the magazine *Break-In* (New Zealand) is simple and easy to build and operate. The schematic and construction details for the key are shown. After constructing the unit and key, adjust R1 and R2 so their full resistance is in the circuit. Apply power. V1 should be cut off and the relay open. Throw the key to DOT position. The voltage should be equal on the plates of V1 and V2. If it is not, substitute other 0.1-μf capacitors for C1 and C2 and other 100,000-ohm resistors for R4 and R5 until the plate voltages are equal *while making dots*. When this is done, the length of the dots and the spacing between them will be correct for standard sending.



Move the key to DASH. This places C3 in parallel with C2 and causes the relay to stay closed for three times the length of one dot. Check this by measuring plate voltages. One section should drop by one-third and the other increase by one-third the resting plate voltage. Adjust the value of C3 until this condition is met.



Speed is increased by decreasing the values of resistors R1 and R2 simultaneously.

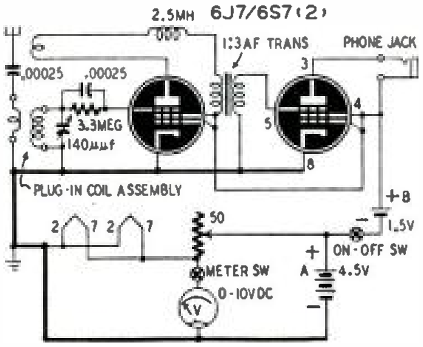
The keyed circuit is controlled by a sensitive relay with normally-open contacts. R3 should have a resistance about ten times the resistance of the relay coil. V1 and V2 may be any receiving-type twin-triode with separate cathodes or two separate triodes.

The key can be made in any convenient form. It can be built around a discarded "bug." Contacts common to A-B should be open and the X-Y contacts closed when the arm of the key is in the normal position.

LOW-VOLTAGE RECEIVER

This receiver operates with a B-voltage of only 1.5 and A of 4½.

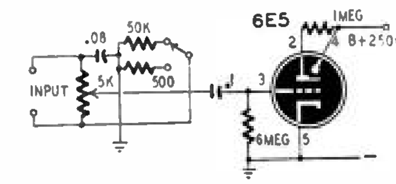
To make the tubes operate with the low plate and filament voltages, the suppressors are used as control grids and the control grids are tied to the screens. Standard plug-in coil assemblies are used.



The 0-10 voltmeter is used to keep check on the condition of the A-battery. The 50-ohm rheostat should be adjusted for whatever filament voltage gives the most efficient operation. The original receiver used 6J7's; but if 6S7's are available they should be used, as their 0.15 ampere filament current is only half as great.——*John S. Zverloff*

AUDIO FREQUENCY METER

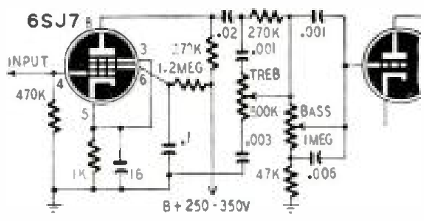
The audio frequency meter shown in the diagram measures tones from 4 to 40,000 cycles. It is a simple bridge circuit with one reactive arm to make it frequency sensitive. The indicator is a 6E5 electron-ray tube. The potentiometer should be linear. It can be calibrated with a standard audio-frequency oscillator. If no oscillator is available. a microphone and amplifier—with known frequency sources such as a frequency record, tuning forks, or pitch pipes—may be used to obtain a fair calibration curve.



To measure the frequency of a tone, feed it to the input terminals, *neither of which can be grounded.* Adjust the calibrated potentiometer for widest shadow angle on the 6E5.——*D. Bosman*

AUDIO EQUALIZER

The equalizer shown in the diagram will boost or attenuate bass and treble. There is no interaction between the controls. Because of the 6SJ7, there is considerable gain, and therefore the unit may be used as part of the low-level section of an amplifier.——*Leon Medler*



GETTING STARTED ON 160

Now that a portion of the 160-meter band is to be opened to amateurs, many of them are looking for ways of getting their rigs into operation on this band with the least amount of trouble. A frequency-halving circuit and a method of loading short antennas for 160-meter operation, described in *QST*, will permit hams with 80-meter crystals to get on 160 without buying new ones or putting up another antenna.

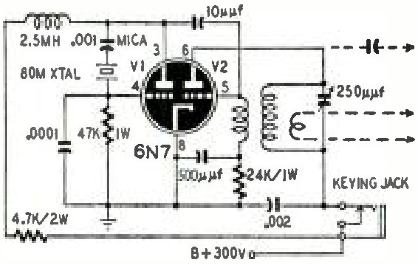


Fig. 1—160-meter exciter uses 4-mc xtals.

The frequency-halving oscillator is shown in Fig. 1. It consists of a Pierce oscillator V1 controlled by an 80-meter crystal and of a tuned-plate self-excited oscillator V2 operating in the 160-meter band. The v.f.o. locks in with a submultiple of the crystal and is stabilized by it.

The plate coil has 38 turns of No. 20 d.c.c. wire, close-wound on a 1¼-inch form; and the grid coil has 24 turns of No. 26 d.s.c, close-wound at the bottom end of the plate coil.

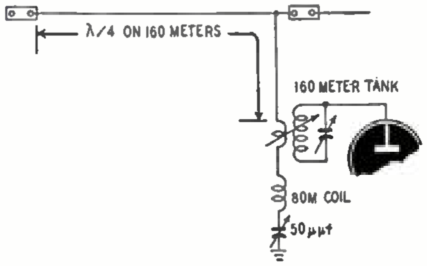


Fig. 2—Loading the 80-meter Zepp on 160.

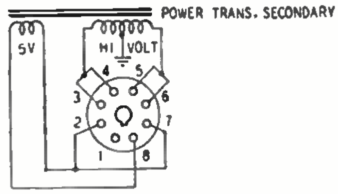
The output is sufficient to excite almost any of the beam-power tubes normally used in crystal oscillators. The unit can be coupled to the grid of the crystal oscillator, in the rig, through a blocking capacitor or through link coupling.

CAUTION: It may be necessary to experiment with the value of the 10-μμf capacitor between the grid of V2 and the plate of V1. If the coupling is too loose, the oscillators will not lock; if it is too tight, the crystal frequency may vary when the variable oscillator is tuned. Adjust this circuit while monitoring the signal.

Fig. 2 shows how an 80-meter Zepp can be used on 160. The feeders are tied together at the transmitter end. Almost any antenna can be used if the sum of the feeder and radiator lengths approximates one-quarter wavelength on 160 meters. The system is tuned by an 80-meter coil and a 50-μμf variable capacitor in a series resonant circuit. The plate spacing of the capacitor should be sufficient to prevent breakdown.

RECTIFIER TUBE SOCKET

A rectifier tube socket connected as shown will accommodate any of the following tubes without a change in wiring: 5R4-GY, 5T4, 5U4, 5Z4, 5V4, 5W4, 5Y3, 5Y4. This is a useful idea

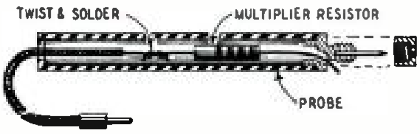


for the amateur or experimenter who has a number of surplus tubes to use as replacements.

E. E. BALDWIN,
Grand Island, Neb.

EXTENDING VOLTMETER RANGE

Many owners of multimeters sometimes have to measure voltages higher than their meters ordinarily will handle. A simple way to extend meter range is to use a test prod with a multiplier resistor built into it. A standard ½-watt resistor can be inserted in the handle of most test prods, as shown in the drawing.



All the information necessary for choosing the correct resistance value is the sensitivity of the meter in ohms per volt, usually given in the maker's instruction book. If the meter has a sensitivity of 1,000 ohms per volt, for example (this is usual), and you want to extend the 300-volt range to read 600 volts, multiply the difference between the old and desired full-scale readings (600 — 300 = 300) by 1,000 (300 × 1,000 = 300,000). For best accuracy, the 300,000-ohm resistor used should have a tolerance of no more than ± 1%. To make the original 300-volt range read 900 volts, use a 600,000-ohm resistor; and so on.

If you choose even multiples of the existing meter scales, you can read the higher values simply by multiplying. For instance, if the 300,000-ohm resistor is used with the 300-volt scale to read a maximum of 600 volts, just multiply any reading by 2. For 900 volts maximum, multiply by 3.

DON HUTCHINSON,
Troy, N. Y.

(If you use multipliers to read voltages around 1,000 or more, be sure to get a high-voltage probe, one with sufficient insulation to protect you from arc-overs and breakdowns.—*Editor*)

SOLDERING TIPS

It is a good idea to have a number of different-sized and -shaped tips for your soldering iron to take care of fine and coarse jobs and to get into otherwise inaccessible places.

A small depression, large enough to

hold a drop of solder, in one surface of the iron is useful for transferring solder to hard-to-reach connections.

N. SCHVEDMAN,
Kew Gardens, N. Y.

COLOR CODING

Applying spots of colored paint to resistors and terminals in a chassis is often useful for coding. Instead of a brush, use a pipe cleaner. It does not have to be cleaned when the color is to be changed. All that is necessary is to clip off the end that has been dipped in the paint.

O. C. VIDDEN,
Fertile, Minn.

TEMPORARY CONNECTORS

Small steel springs are very useful on the experimenter's bench for making temporary connections between wires. The ends of the two pieces (or more) of wire can be inserted between the coils. If the spring is close-wound, it will grasp the wires tightly.

The connections can be insulated quickly by slipping a small length of rubber tubing over the spring and wires.

G. GARVIN,
South Bend, Ind.

PICK-UP TOOL

A wooden rod about ¼ inch in diameter and having a blob of wax firmly stuck on the end is very useful for picking up small parts in inaccessible places or starting nuts in cramped quarters.

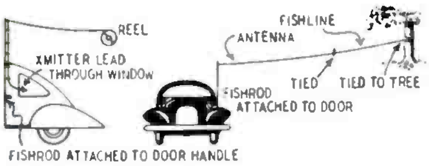
AUGUSTINE MAYER,
Tiffin, Ohio

LONG-WIRE ANTENNA

I carry a 40-80-meter transmitter in my car and frequently must erect a long-wire antenna. To simplify erecting and taking down the antenna I use a deep-sea fishing rod and reel.

A good length of strong fishing line is wound on the reel first. Then the end of a 134-foot length of phosphor-bronze (surplus) antenna wire is tied to the end of the line and wound on the reel.

On arrival at a location, I dismount the reel from the rod and tie the rod to the side of the car (see drawing).



The end of the wire is passed through the top guide of the rod, through subsequent guides, and into the car window. Then, walking backward, I carry the reel, letting the wire pay out.

Eventually the wire is all unreeled and I tie the fish line to a tree. The line acts as an end insulator. To fold up and move on, the process is simply reversed.

R. L. BRIDGES, W6PMU,
Los Angeles, Calif.

World-Wide Station List

By ELMER R. FULLER

WITH the issue we are again printing the Station List after an absence of two months. An FM Station List appeared in the February issue and a list of television stations in March. A list of Canadian FM stations is printed this month, on page 85.

Incidentally, many dx reports have been received on FM. Possibly more significant are the occasional dx television reports. These are necessarily rather rare, since few people with television sets are to be found in regions remote from broadcasters. However, the television frequencies are inherently better suited for distance reception, and as television sets become more numerous, we are likely to hear more about television reception over distances of several hundred miles. We are very anxious to obtain verified reports of such long-distance reception, and especially of repeated reception of television programs at distances of 200 miles and more.

Freq.	Station	Location and Schedule
2.500	WWV	WASHINGTON, D.C.: U.S. Bureau of Standards; continuous, day and night
3.310	YV1RO	TRUJILLO, VENEZUELA: 1700 to 2130
3.370	YV1RT	MARACAIBO, VENEZUELA: 1730 to 2230
3.400	YV5RW	CARACAS, VENEZUELA: 0530 to 0800; 0955 to 1430; 1530 to 2130
3.420	YV2RC	MERIDA, VENEZUELA: 1800 to 2130
3.440	YV1RU	MARACAIBO, VENEZUELA: 0530 to 0830; 1030 to 2230
3.460	YV4RP	VALENCIA, VENEZUELA: 1730 to 2130
3.480	YV4RQ	PUERTA CABALLO, VENEZUELA: 1700 to 2130
3.480	ZQI	JAMAICA, BRITISH WEST INDIES: 1600 to 1730; 1930 to 2200
3.490	YV3RS	BARQUISIMETO, VENEZUELA: 1630 to 2130
3.500	YV5RX	CARACAS, VENEZUELA: 0930 to 1400; 1530 to 2230
3.510	YV6RC	BARQUISIMETO, VENEZUELA: 1800 to 2130
3.530	YV5RS	CARACAS, VENEZUELA: 0530 to 2230
3.910	ZQP	LUSAKA, NORTHERN RHODESIA: 0400 to 0530; 1000 to 1200
4.750	YV1RV	MARACAIBO, VENEZUELA: 0930 to 2130
4.780	YV4RO	VALENCIA, VENEZUELA: 1630 to 2130
4.780	HJAB	BARRANQUILLA, COLOMBIA: 1700 to 2255
4.810	YV1RL	MARACAIBO, VENEZUELA: 0530 to 2230
4.810	HJBB	CUCUTA, COLOMBIA: 1700 to 2200
4.820	XEJG	GUADALAJARA, MEXICO: 2200 to 2400
4.820	HJED	CALI, COLOMBIA: 1900 to 2300
4.830	YV2RN	SAN CHRISTOBAL, VENEZUELA: 1100 to 2130
4.340	YV1RZ	VOLERA, VENEZUELA: 1030 to 2145
4.850	HJCA	BOGOTA, COLOMBIA; 1900 to 2200
4.860	PRC5	BELEM, BRAZIL: 0600 to 0700; 0900 to 1100; 1530 to 2000 except Sundays
4.880	HJFH	ARMENIA, COLOMBIA: 0600 to 2200
4.890	HJCH	BOGOTA, COLOMBIA: 1800 to 2200
4.900	ZOH	COLOMBO, CEYLON: 0000 to 0330; 0445 to 1145: 2100 to 2145
4.920	CR7BU	LOURENCO MARQUES, MOZAMBIQUE; 1000 to 1600
4.920	YV5RN	CARACAS, VENEZUELA: 0600 to 2230
4.940	HJCW	BOGOTA, COLOMBIA: 0645 to 1115; 1600 to 2315
4.950	HC5HC	RIOBAMBA, ECUADOR: 1800 to 2300
4.950	ZQI	JAMAICA, BRITISH WEST INDIES: 1600 to 1730
4.960	HJAE	CARTAGENA, COLOMBIA: 1600 to 2230
4.990	YV3RS	BARQUISIMETO, VENEZUELA: 1630 to 2130
5.000	WWV	WASHINGTON, D.C.: U.S. Bureau of Standards; continuously day and night
5.020	YVRO	CARACAS, VENEZUELA: 2000 to 2230
5.870	HRN	TEGUCIGALPA, HONDURAS: 0800 to 1000; 1300 to 1500; 1800 to 2300
5.880	ZRK	CAPETOWN, SOUTH AFRICA: 0315 to 0915: 1200 to 1600
5.940	RV15	MOSCOW, U.S.S.R.: 0300 to 0930; 1530 to 1820; 2100 to 0015
5.970	HJV	VATICAN CITY; 1345 to 1515
5.970	HC1QRX	QUITO, ECUADOR; 0700 to 0815; 1200 to 1400; 1800 to 2300
5.980		ANDORRA: 0600 to 0830: 1300 to 1900
5.890	OAX4Z	LIMA, PERU: 1630 to 2330
5.910	OZX4V	LIMA, PERU: 1800 to 2400

Freq.	Station	Location and Schedule
5.950	HH2S	PORT-AU-PRINCE, HAITI: 0600 to 0815; 1100 to 1300; 1730 to 2130
5.970	HI2T	CIUDAD TRUJILLO, DOMINICAN REPUBLIC: 1900 to 2400
5.980	LRSI	BUENOS AIRES, ARGENTINA: 1800 to 2300
5.980	XGOA	NANKING, CHINA: heard at 0600
6.000	ZFY	GEORGETOWN, BRITISH GUIANA: 2100 to 2200
6.000	CFCX	MONTREAL, CANADA: 0700 to 2315
6.000	HP5K	COLON, PANAMA: 0730 to 2300
6.000	HHYM	PORT-AU-PRINCE, HAITI: 1200 to 1400; 1830 to 2100
6.000		NOUMEA, NEW CALEDONIA: 0345 to 0500
6.000	HJKD	BOGOTA, COLOMBIA; 1900 to 2300
6.010	OQ2RC	LEOPOLDVILLE, BELGIAN CONGO: 1200 to 1300
6.010	CJCX	SYDNEY, NOVA SCOTIA: 0530 to 2200
6.020	XEUW	VERA CRUZ, MEXICO: 2100 to 2300
6.020	PGD	HILVERSUM, NETHERLANDS: 1745 to 2330; Tues., 0300 to 0130; Wed. & Sat., 1030 to 1200; 1600 to 1730
6.030		MOSCOW, U.S.S.R.: 0000 to 0500
6.030	CFYP	CALGARY, CANADA: 0730 to 0100
6.030	HP5B	PANAMA CITY, PANAMA: 1800 to 2300
6.040		RANGOON, BURMA: 0600 to 1115
6.040	COBF	HAVANA, CUBA: 0800 to 2300
6.040	XETW	TAMPICO, MEXICO: 0745 to 0045
6.040	WRUS	BOSTON, MASSACHUSETTS: Mexican beam, 1900 to 2230
6.060		TANANARIVE, MADAGASCAR: 1330 to 1400
6.060		TETUAN, SPANISH MOROCCO: 0230 to 0300; 1330 to 1500
6.060	KNBA	DIXON, CALIFORNIA: Hawaiian beam, 0130 to 1005
6.070	CFRX	TORONTO, CANADA: 0600 to 2345
6.080	CKFX	VANCOUVER, CANADA: 0930 to 0300
6.080	MUNICH III	MUNICH, GERMANY: 1100 to 1700
6.090	LRYI	BUENOS AIRES, ARGENTINA: 0645 to 2200
6.090	CBFW	MONTREAL, CANADA: 0730 to 1915; 2000 to 2400
6.090	ZYB7	SÃO PAULO, BRAZIL; 1600 to 2150
6.100	VUD3	DELHI, INDIA: 1200 to 1245
6.100		WARSAW, POLAND: 1100 to 1800
6.100	PRE9	FORTALEZA, BRAZIL: 0900 to 1200; 1600 to 1900
6.100	WKLS	KURE, JAPAN: 1630 to 2030
6.110	GSL	LONDON, ENGLAND: 2300 to 0215; 1615 to 1745
6.120	HP5H	PANAMA CITY, PANAMA: 0630 to 2400
6.130	XEUZ	MEXICO CITY, MEXICO: 1100 to 0400
6.130	CHNX	HALIFAX, NOVA SCOTIA: 0700 to 2300
6.130	COCD	HAVANA, CUBA: 0700 to 2400
6.140	HJDE	MEDELLIN, COLOMBIA: 1100 to 2300
6.150	GRW	LONDON, ENGLAND: 1515 to 1600; 2000 to 2215
6.150	CKRO	WINNIPEG, CANADA: 0600 to 0200
6.150	EQB	TEHERAN, IRAN: 0930 to 1400; 2230 to 2315
6.150	TIRH	SAN JOSE, COSTA RICA: 2130 to 2100
6.150	CS2WD	LISBON, PORTUGAL; 1330 to 1800
6.160	HCKJ	BOGOTA, COLOMBIA: 2000 to 2300
6.160	CBRX	VANCOUVER, CANADA: 0900 to 0200
6.160		MUNICH, GERMANY: 0000 to 0300 or later
6.160	HHCM	PORT-AU-PRINCE, HAITI: 0630 to 0930; 1200 to 1430
6.160	HER3	BERNE, SWITZERLAND: 0245 to 0715; 1200 to 1700; 2030 to 2230
6.180		STUTTGART, GERMANY: 2300 to 0330; 0430 to 0715; 0900 to 1630
6.200	HJCT	BOGOTA, COLOMBIA: 1000 to 1400; 1800 to 2315
6.200	YV6RD	CIUDAD BOLIVAR, VENEZUELA: 1700 to 2315
6.200	FK8AA	NOUMEA, NEW CALEDONIA: 0200 to 0400; 0130 to 0500
6.220	CE622	SANTIAGO, CHILE: 0630 to 2330
6.230	HRD2	LA CEIBA, HONDURAS: 1200 to 1400; 1900 to 2300
6.330	COCW	HAVANA, CUBA: 0600 to 2400
6.240	HJCF	BOGOTA, COLOMBIA; 1700 to 2300
6.240	HIIN	CIUDAD TRUJILLO, DOMINICAN REPUBLIC: 1600 to 2230
6.250	YSUA	SAN SALVADOR, SALVADOR: evenings till 2400
6.280	HCJB	QUITO, ECUADOR: 1800 to 2100
6.310	HIIZ	CIUDAD TRUJILLO, DOMINICAN REPUBLIC: 1600 to 2255
6.360	HRPI	SAN PEDRO SULA, HONDURAS: 1100 to 1415; 1800 to 2330
6.370	CSX	LISBON, PORTUGAL; 1230 to 1800
6.400	CR5AA	PRAIA, CAPE VERDE ISLANDS: 1530 to 1700
6.400	HHCN	PORT-AU-PRINCE, HAITI: 2000 to 2200
6.450	COHI	SANTA CLARA, CUBA; 0630 to 2400
6.510	CP40	COCHABAMBA, BOLIVIA: 1930 to 2200
6.620	TG2	GUATEMALA CITY, GUATEMALA: 0730 to 0900; 1800 to 2300
6.760	YNDS	MANAGUA, NICARAGUA: 0800 to 1000; 1700 to 2330
6.770	CP49	LA PAZ, BOLIVIA: 0700 to 0900; 1100 to 1200; 1930 to 2100
6.770		SINGAPORE, MALAYA: 0330 to 1200
6.850	YNOW	MANAGUA, NICARAGUA: 2000 to 0100
6.910	YNQE	MANAGUA, NICARAGUA; 1300 to 2300
6.920	FZK6	DAKAR, FRENCH WEST AFRICA: 1330 to 1700
6.980		MOSCOW, U.S.S.R.: 1600 to 1745; 2315 to 2345
6.980	FO8AA	PAPEETE, TAHATI; Tuesdays, Wednesdays, Fridays, Saturdays, 2230 to 0030
7.010	XPSA	KWEIYANG, CHINA; 2330 to 0030; 0430 to 0900

OPPORTUNITY AD-LETS

Advertisements in this section cost 25c a word for each insertion. Name, address and initials must be included at the above rate. Cash should accompany all classified advertisements unless placed by an accredited advertising agency. No advertisement for less than ten words accepted. Ten percent discount six issues, twenty percent for twelve issues. Objectionable or misleading advertisements not accepted. Advertisements for June, 1949, issue, must reach us not later than April 21, 1949.
Radio-Electronics, 25 W. Broadway, New York 7, N. Y.

12B8 & 25B8 TUBES. ADAPTER UNIT USING 2 miniature tubes (6AT6 & 6BA6 for 12B8, and 12AT6 & 12AB6 for 25B8). Takes less space than original tube—nothing else to buy—just plug in & it works. Money-back guarantee. 12B8 or 25B8 unit complete: $2.49 each. 10 units for $22.50. Send 25% deposit, balance C.O.D. Write for free parts catalog. COMMERCIAL RADIO, 36 Brattle St., Boston, Mass.

BARGAINS: NEW AND RECONDITIONED HALLICRAFTERS, National, Collins, Hammarlund, Meissner, RME, other receivers, tuners, television receivers, transmitters, etc. Wholesale prices. Terms. Shipped on trial. Liberal trade-in allowance. Write. Henry Radio, Butler, Missouri and 11240 West Olympic, Los Angeles, California.

AMATEUR RADIO LICENSES. COMPLETE THEORY preparation for passing amateur radio examination. Home study and resident courses. American Radio Institute, 101 West 63rd St., New York City. See our ad on Page 94.

BARGAIN HUNTING? RADIO SERVICEMEN WRITE. Sensational catalog. Henshaw Radio Supply, 3619 Troost, Kansas City 3, Missouri.

RECORD CHANGER PARTS for leading makes of changers. We ship everywhere. Mail orders invited! FRIEND'S Wholesale Distributors, 106 North Sixth Street, Philadelphia 6, Pa.

WANTED: Salesmen to sell Nationally Advertised Brand Radio Tubes to Dealers and Servicemen at liberal discounts. Good Commissions Paid. c/o Radio-Electronics, P. O. Box RE-32, 25 W. Broadway, New York 7, N. Y.

MAGAZINES (BACK DATES)—FOREIGN, DOMESTIC, arts. Books, booklets, subscriptions, pin-ups, etc. Catalog, 10c (refunded). Cicerone's, 863 First Ave., New York 17, N. Y.

SELECTED GROUP OF MEN, GRADUATES OF WELL-known trade school, desire employment in Radio Field. Will travel anywhere. Qualified in radio servicing, installation, test instruments, circuit operation, etc. Contact Placement Dept. Eastern Technical School, 888 Purchase Street, New Bedford, Mass.

WE REPAIR ALL TYPES OF ELECTRICAL INSTRUMENTS, tube checkers and analyzers. Hazleton Instrument Co. (Electric Meter Laboratory), 140 Liberty Street, New York, N. Y. Telephone—BArclay 7-4239.

LANCASTER, ALLWINE & ROMMEL, 436 BOWEN Building, Washington 5, D.C. Registered Patent Attorneys. Practice before United States Patent Office. Validity and infringement Investigations and Opinions. Booklet and form "Evidence of Conception" forwarded upon request.

TELEVISION, RADIO, TUBES, PARTS. SEND FOR free bargain list. Hallmark, 592A Communipaw, Jersey City, New Jersey.

RADIOMEN, SERVICEMEN, BEGINNERS — MAKE more money, easily, quickly. $250 weekly possible. We show you how. Information free. Merit Products, 216-32L 132nd Avenue, Springfield Gardens 13, New York.

EVERYONE CAN MAKE EASY MONEY INSTANTLY! Radio training unnecessary. Top-quality—quick selling—new plastic scientific Television Filter made specifically for TV! 100% profit, sells for $2.00, costs $1.00, up to 12" picture. Send $1.00 for sample. Money-back guarantee! Start earning extra money today! APSCO, 544 Sixth Ave., New York, N. Y.

Send for 30 Years Proved Radio Repairing Simplified System; $1.00. Box 178E, Lake Hiawatha, New Jersey.

HEARING AIDS—Reconditioned. Make wonderful miniature radios. $20.00 complete with cords, earphone. Shelby Instrument, 321 West 7th St., Long Beach, Calif.

ALUMINUM TUBING, ANGLES, SHEETS AND FITTINGS. Write for list. Willard Radcliff, Fostoria, Ohio.

RADIO TUBES, ALL POPULAR TYPES $37.00 FOR 50. Reliable Tube Co., O'Neill, Nebr.

ELECTRONICS KIT Builds AC-DC voltmeter, oscillator, electric eye. $2.95 complete. Literature Free. Precise Measurements Co., 942E Kings Highway, Brooklyn, N. Y.

ANY RADIO-ELECTRONICS TEXT BOOK RENTED—1-2c per day. Address: TBRA, 780 East 214th St., New York, N. Y.

For Sale—Best radio-refrigeration shop in Ozarks, sportsman's paradise. Wilson Radio, Thayer, Missouri.

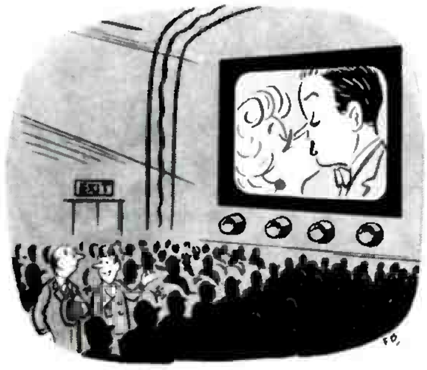
27 years experience radio repairing. Simplified system. No calculations. No formulas. Total price $2.00 postpaid or COD. Moneyback guarantee. Ross Radio, 14615 Grand-river, Detroit 27, Mich.

Heath's Vacuum tube voltmeter, new, wired, complete, ready to use, accurate, best looking meter on market $45.50. Ernest Santalla, 42-35 64th Street, Woodside, N. Y.

PHONOGRAPH RECORDS CHEAP. CATALOGUE. Paramount, BJ-313 East Market, Wilkes-Barre, Penna.

TELEPHONE DIALS. NEW AUTOMATIC ELECTRIC standard AK-11 $5.25 postpaid. Used N-E Type-1 Rebuilt $2.25. Re-adjusted $1.25 postpaid. Kissel Electric Products, 431-C Sherman, Galion, Ohio.

Freq.	Station	Location and Schedule
7.100		BISSAU, PORTUGUESE GUIANA; 1345 to 1730
7.120	GRM	LONDON, ENGLAND; 1145 to 1215; 1445 to 1715; 2330 to 2345
7.130	VQ6MI	HARGEISA, BRITISH SOMALILAND; 0800 to 1030; 1200 to 1300
7.150	XGOY	CHUNGKING, CHINA: 0530 to 0730; 0745 to 0945; 1000 to 1045
7.160	KWS4	VIENNA, AUSTRIA; 2345 to 2030
7.220		SINGAPORE, MALAYA: 2330 to 0130
7.250	PJCI	WILLEMSTAD, CURACAO: 1130 to 1230; 1630 to 2130
7.250	MUNICH II	MUNICH, GERMANY: Balkan beam, 1100 to 1700
7.260	GSU	LONDON, ENGLAND; 2315 to 2330; 2345 to 0130; 1000 to 1700
7.230	JLW	TOKYO, JAPAN: Home Service, 0300 to 0900; 1600 to 1800; 2200 to 0230
7.290	VUD3	DELHI, INOIA: 0800 to 1100; 1730 to 1825; 2100 to 2300
7.290	ZOY	ACCRA, GOLD COAST: 1045 to 1300
7.300		MOSCOW, U.S.S.R.; 1100 to 1615
7.310	YSN	SAN SALVADOR, SALVADOR: 1300 to 1500; 1900 to 2300
7.410	PSTA2	SAO PAULO, BRAZIL: except Saturdays and Sundays, 1800 to 2000
7.570	EAJ43	SANTA CRUZ, CANARY ISLANDS: 0730 to 0900; 1230 to 1700
7.850	ZAA	TIRANA, ALBANIA: 1300 to 1700
7.850	SUX	CAIRO, EGYPT; 1400 to 1920
7.920	HLKA	SEOUL, KOREA: 0250 to 0830; 1630 to 1850; 2100 to 2400
7.950		ALICANTE, SPAIN: 0700 to 1000; 1400 to 1800
7.950		DOUALA, CAMEROONS: 1300 to 1500
8.030	FXE	BEIRUT, LEBANON: 0000 to 0115; 0515 to 0800; 1030 to 1600
8.700	COCO	HAVANA, CUBA: 0800 to 0100
8.830	LOCQ	HAVANA, CUBA: 0700 to 0100
8.950	COKG	SANTIAGO, CUBA: 0600 to 2300
9.030	COBZ	HAVANA, CUBA: 0700 to 0100
9.080	CNR3	RABAT, MOROCCO: 0145 to 0500; 1315 to 1900
9.160	CR6RB	BENGUELA, ANGOLA: 1330 to 1430
9.210	HI2G	CIUDAD TRUJILLO, DOMINICAN REPUBLIC: 0530 to 0830; 1300 to 1530; 1700 to 1845
9.230	COBQ	HAVANA, CUBA: 0800 to 1200; 1730 to 2330
9.270	COCX	HAVANA, CUBA: 0700 to 0030
9.330		SOFIA, BULGARIA: 2300 to 0100; 0530 to 0700; 1100 to 1330; 1400 to 1545
9.370	EAQ	MADRID, SPAIN: 1330 to 1600; 1830 to 2200
9.380	COBC	HAVANA, CUBA: 0700 to 2400
9.380	OTC	LEOPOLDVILLE, BELGIAN CONGO: 0000 to 0200; 1100 to 1500
9.420		BELGRADE, YUGOSLAVIA: 0000 to 1230; 1630 to 0845; 1000 to 1015; 1110 to 1125
9.440	FZI	BRAZZAVILLE, FRENCH EQUATORIAL AFRICA: 0000 to 0230; 1100 to 1630; 1700 to 2030
9.460	TAP	ANKARA, TURKEY: 1000 to 1015; Sun., Mon., Thurs., 1530 to 1545
9.470	CR6RA	LOUANDA, ANGOLA: 0115 to 0230; 0630 to 0715; 1400 to 1530
9.470		WILLEMSTAO, CURACAO: 1400 to 1600
9.480		MOSCOW, U.S.S.R.: 0600 to 0900
9.500	XEWW	MEXICO CITY, MEXICO: 0800 to 0200
9.500	OIX2	LAHTI, FINLAND: 0350 to 0730; 1000 to 1600; 2300 to 2100
9.510	JLG2	TOKYO, JAPAN: 0300 to 0830
9.520	VLW7	PERTH, AUSTRALIA: 0530 to 1030; 1600 to 1000
9.520	ZRG	JOHANNESBURG, SOUTH AFRICA: 0300 to 1045
9.520	OZF	COPENHAGEN, DENMARK: 1900 to 2030
9.520	SEAC	COLOMBO, CEYLON: 1930 to 1200
9.530	WGED	SCHENECTADY, NEW YORK: South American beam, 1900 to 2230
9.530	SBU	STOCKHOLM, SWEDEN: 2000 to 2100
9.540	VLR	MELBOURNE, AUSTRALIA; 0800 to 0915; 0930 to 1000; 1245 to 1415
9.540	LKJ	OSLO, NORWAY; 0125 to 0230
9.540	MUNICH II	MUNICH, GERMANY: East European beam, 1100 to 1700
9.540	CJCA	EDMONTON, CANADA: 0815 to 0200
9.550	XETT	MEXICO CITY, MEXICO: 0700 to 0100
9.550		PARIS, FRANCE: 2100 to 2130



"We had to fake a Television effect to make folks feel at home."
Suggested by H. Roesler, Milwaukee, Wis.

Freq.	Station	Location and Schedule
9.560		KOMSOMOLSK, U.S.S.R.: 2100 to 2400
9.560		VIENNA, AUSTRIA: 0000 to 0200; 0400 to 0830;; 1000 to 1600
9.570	KWID	SAN FRANCISCO, CALIFORNIA; Chinese beam, 0700 to 1000
9.570	WRUW	BOSTON MASSACHUSETTS: South American beam, 2000 to 2200
9.570	KWIX	SAN FRANCISCO, CALIFORNIA: Alaskan beam, 2215 to 0345
9.580	GSC	LONDON, ENGLAND: 1330 to 1315; 1430 to 1530; 1600 to 1615; 1815 to 2030
9.580	VLH3	MELBOURNE, AUSTRALIA: 0345 to 0830; Sat., 0245 to 0900; Sun., 0330 to 0830

CANADIAN FM STATIONS

While Canada has not yet started its television efforts in earnest, FM in the Dominion is advancing. The following list of Canadian FM stations enumerates all those in operation as of February 21, 1949. It includes those which are owned by the Canadian Broadcasting Corporation (the four in Montreal, Toronto, and Vancouver, and CBO-FM in Ottawa) as well as privately owned outlets. There are 22 altogether, which is twice the number in operation in April, 1948. All stations are operating with a nominal power of 250 watts except for CFPL-FM, London, which uses 3,000.

CITY	CALL	FREQUENCY
	ALBERTA	
Edmonton	CKUA-FM	98.1
	BRITISH COLUMBIA	
Vancouver	CBR-FM	105.7
	MANITOBA	
Winnipeg	CJOB-FM	103.1
	NEW BRUNSWICK	
Saint John	CHSJ-FM	100.5
	NOVA SCOTIA	
Halifax	CHNS-FM	96.1
Sydney	CJCB-FM	94.9
	ONTARIO	
Fort William	CKPR-FM	94.3
Hamilton	CHML-FM	94.1
Kingston	CKWS-FM	96.3
Kirkland Lake	CJKL-FM	93.7
Kitchener	CKCR-FM	96.7
London	CFPL-FM	93.5
Ottawa	CBO-FM	103.3
Ottawa	CFRA-FM	93.9
Sarnia	CHOK-FM	97.5
Sault Ste. Marie	CJIC-FM	100.5
Timmins	CKGB-FM	94.5
Toronto	CBL-FM	99.1
Windsor	CKLW-FM	93.9
Woodstock	CKOX-FM	106.9
	QUEBEC	
Montreal	CBF-FM	100.7
Montreal	CBM-FM	95.1

Suggested by:
E. A. Conklin, Denver, Colorado

"So that's what you mean by 'point to point testing,' eh?"

Stuart Hall Frank has been elected president of Major Television Corporation of New York. He was formerly president of Steinhardt & Kelly. Other officers elected are **Irving Ross**, vice-president and sales director; **Michel E. Macksoud**, vice-president and chief engineer; **Warren Kessler**, vice-president; **Henry Weintraub**, treasurer; and **Charles J. Hyman**, secretary.

H. G. Kronenwetter, former advertising production manager of the Radio Division, has been appointed manager of advertising production for the Lighting, Fixture, Lamp, Radio, Electronics, and International Divisions of Sylvania Electric Products, Inc., according to an announcement by Terry P. Cunningham, director of advertising.

O. K. Lindley has been appointed assistant sales manager, communications products, for the Specialty Division of the General Electric Company at Electronics Park, Syracuse, N. Y., according to an announcement by H. W. Bennett, manager of sales for the division. He will be responsible for those communications products designed for other than home use, such as the FM bus receiver equipment and the single sideband selector.

Charles P. Baxter has been appointed assistant general manager of the RCA Victor Home Instrument Department of Camden, N. J. He will assist Mr. Henry G. Baker, general manager of the department, in the administration of sales, engineering, design, purchasing, and manufacturing operations.

Mortimer W. Loewi, executive assistant to **Dr. Allen B. Du Mont**, assumed directorship of the Du Mont Television Network. He replaces Lawrence Phillips who is leaving Du Mont to operate his own management consultant business. Mr. Loewi has been active in the development of Allen B. Du Mont Laboratories, Inc., since the company's inception.

Dr. Hans Kohler, formerly a member of the Research Laboratories of the Signal Corps, has been appointed to the staff of the National Bureau of Standards, where he will do theoretical work in the Electronics Division.

G. W. DeSousa has been appointed staff assistant to **J. M. Lang**, divisions manager of the General Electric Company's Tube Divisions at Schenectady, N. Y.

L. S. Thees has been appointed general sales manager of the RCA Tube Department, it has been announced by L. W. Teegarden, vice-president in charge of technical products, RCA Victor Division, Harrison, N. J., of the RADIO CORPORATION OF AMERICA.

Formerly manager of equipment sales of the RCA Tube Department, Mr. Thees will now coordinate and direct all the sales activities of the department, including equipment and renewal sales. Products of the Tube Department include tubes, electronic components, tube parts and machinery, batteries, test equipment, and accessories.

Charles Roberts has been appointed advertising and promotion manager of AIR KING PRODUCTS COMPANY, INC., of Brooklyn, makers of radio, television, and electronic apparatus. Mr. Roberts was formerly sales promotion manager of Zenith Radio Corporation of New York.

Henry P. Kalmus, formerly a member of the research laboratory of the Zenith Radio Corporation, has been appointed to the staff of the NATIONAL BUREAU OF STANDARDS. Mr. Kalmus will conduct investigations in advanced electronic techniques in the Bureau's Ordnance Research Laboratory.

Dr. B. H. Alexander, formerly professor of metallurgy at the Carnegie Institute of Technology, has joined the staff of the Metallurgical Research Laboratories of SYLVANIA ELECTRIC PRODUCTS, INC., Bayside, N. Y.

Dr. Alexander will head a group of scientists engaged in fundamental studies of the physics of metals, aimed at gaining a better understanding of the basic principles governing the behavior of these materials. Among the elements of interest are tungsten, germanium, titanium, nickel, cobalt, and many others which are important to the performance of radio and electronic tubes and incandescent and fluorescent lamps.

Dr. J. R. Dedrick, formerly associate professor of powder metallurgy at the University of Cincinnati, has been appointed section head of the advanced development group at the metallurgical research laboratories of SYLVANIA ELECTRIC PRODUCTS, INC., according to an announcement by W. E. Kingston, manager of the laboratories. Dr. Dedrick will have charge of the group doing work of a research nature but dealing with problems important to commercial products.

.... DETROLA CHANGERS

Sometimes these record changers stop after completing half of the change cycle. Replacement of the faulty spring drive belt with a similar one is not effective because the spring soon stretches. Instead, use a rubber belt, such as General Cement's No. 20 Phono Drive.

JOHN STROLE,
Weehawken, N. J.

.... AIR KING MODEL 4705

If a set is noisy, has excessive hum, and crackles when the cabinet is tapped, check the points where ground connections are made to the chassis. Very often the soldering may not be perfect and the connections develop a high resistance. The cure is to connect all these points together with hookup wire.

ANTON E. SPERLING,
Ft. Meade, Md.

.... INTERMITTENT PORTABLES

In areas where line voltage varies from 115 to 90 volts, portable sets which are intermittent when operated on a.c. can usually be cleared up by replacing either the oscillator tube, the rectifier, or the power-supply filter capacitors. An autotransformer is very useful in determining whether low line voltage is really the cause of the trouble.

THOMAS D. BICHLER,
Tucson, Ariz.

.... SILVERTONE 4566

If the set is dead from approximately 750 kc up, check for an open .0041-μf capacitor between oscillator trimmer and ground. Replace it with a .005-μf unit.

HURLEY D. ROBINSON,
Pullman, W. Va.

.... TUNABLE HUM

When tunable hum is found in a.c.-d.c. receivers, try adding a 0.1-μf capacitor in parallel with the one across the power line.

ALAN SMITH,
Shaftsbury, Vt.

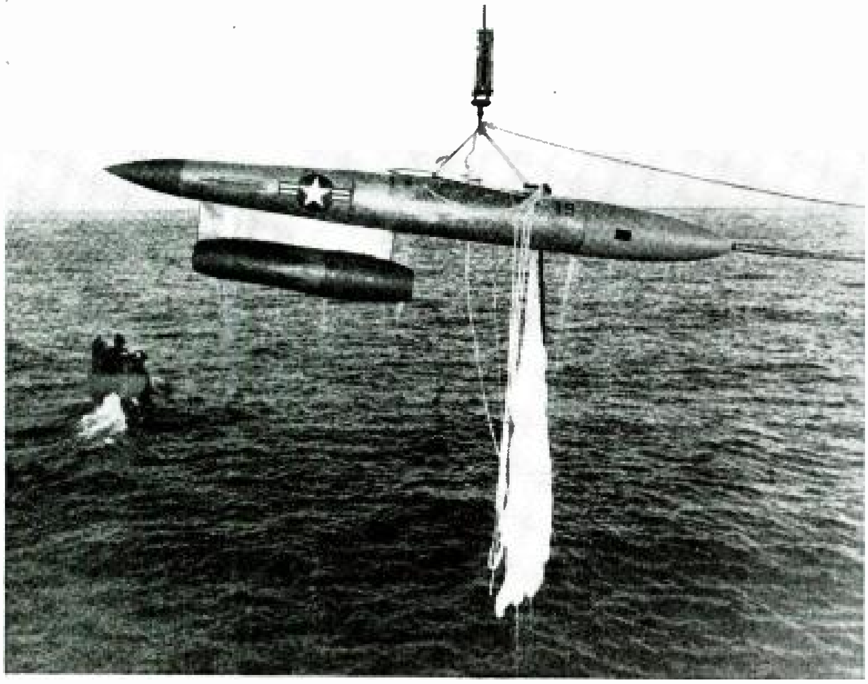
.... SCRATCHY TUNING

If cleaning a tuning capacitor does not clear up the scratchy sound heard when tuning, the shaft may not be making good contact with the frame. Remove the bearing and shaft and clean with carbon tetrachloride. Lubricate with graphite.

A. G. SANDERS,
Miami, Fla.

"What! Another Soap Opera?"
Suggested by J. F. Dunnett, Vancouver, B.C., Canada

RADIO-CONTROLLED AIRCRAFT



(U.S. Navy photo)

U.S. Navy's newest aircraft used for testing ram-jet engines, the PV-N-2 (Gorgon IV), is radio-controlled. Photo shows craft being taken from water after the end of a test flight. The craft may be controlled completely by radio while in flight; after the fuel runs out a parachute is released and the Gorgon floats down to the water. It is retrieved by a crane

FUTURE AIR TRAVEL SAFER

Travel by air in 1964 will be at least as safe, reliable and automatic as train travel is today, D. W. Rentzel, U. S. Administrator of Civil Aeronautics told the recent Institute of Radio Engineers convention in New York. According to Mr. Rentzel, the typical flight of 15 years hence will be much like this:

The pilot's landing time will be reserved for him before he leaves his port of departure. A dial on his board will tell him how many minutes or seconds he is ahead or behind schedule, so that he can regulate his speed.

A pictorial presentation of everything around him will appear on a television screen in the cockpit. He will thus be able to see other planes, obstructions, and even storms which are near him.

A railroad-like radar "block system" will assure that he is in safe air space—free from collision danger—at all times.

Telemetering systems will show ground controllers the readings on all the plane's instruments. Any variation from the conditions noted by ground instruments will be noted and warnings flashed to the pilot.

If the pilot wishes to change altitude or flight plan, he will query ground stations by pressing a button, and transmit his new plan to a calculating machine, which will check its practicability and flash approval or disapproval in a fraction of a second.

SWEDES PHOTOGRAPH SUN

Photographs of the sun taken in Sweden and transmitted to this country by radiophoto, whenever the sun is obscured in New York, are making it possible for RCA Communications, Inc., to continue without interruption its daily forecasts of sunspot activity, General H. C. Ingles, president, announced last month. Observations of solar disturbances and the calculation of their effect on shortwave transmission have been carried out by RCA for several years. The information provides advance warning of magnetic storms and permits rerouting of radiotelegraph traffic to circuits outside the areas affected.

Until recently, General Ingles stated, forecasts of radio conditions have depended upon success in "shooting" the sun through a refracting telescope installed atop the RCA Central Radio Office at 66 Broad Street, New York. But a recent prolonged cloudy period revealed the need for a supplementary source of data in emergencies, and led to the present cooperative arrangement with the Royal Board of Swedish Telegraphs in Stockholm and the Stockholm Observatory in Saltsjobegen, Sweden. When observation by RCA in New York is impossible, a photograph of the sun, taken by Dr. Yngve Oehman, in charge of solar work at the Stockholm Observatory, is transmitted to New York by radiophoto to take the place of the local observation.

Radio Thirty-Five Years Ago
In Gernsback Publications

HUGO GERNSBACK
Founder

Modern Electrics	1908
Electrical Experimenter	1913
Radio News	1919
Science & Invention	1920
Radio-Craft	1929
Short-Wave Craft	1930
Wireless Association of America	1908

Some of the larger libraries in the country still have copies of ELECTRICAL EXPERIMENTER on file for interested readers.

MAY 1915 ELECTRICAL EXPERIMENTER

Tuning Coil Sliders, by Edward Minnis
A Solderless Detector Cup, by Godfrey Rigby
Wireless Telephony and Telegraphy on Union Pacific, by Frank C. Perkins
A Novel Detector Stand
A New Wireless Valve
A Rotary Switch Tuning Coil
Variable Condenser Switch, by Max Epstein
The D. C. Arc for Wireless Telegraphy and Telephony
Improved Conical Tuning Coil
Novel Wireless Telephone Microphone
Universal Crystal Detector, by W. H. Hale
The Galvanometer as a Radiation Indicator for Radio Transmitters, by William H. Dettman
A Radio Blocking Condenser, by Percy M. Roope
A "Wireless" Menu

BRITONS COMMENT ON BILL

The British government has proposed to solve the problem of man-made r.f. noise by passing a bill making unsuppressed noise sources cause for legal action against the owner. An apt comment, headlined "More Dinned Against than Dinning," is this letter to the *London Times*, quoted in the *Scottish Radio Trade Digest*:

Sir,—What irony if a man is compelled to fit a gadget to suppress an electric fire (electric heater—*Ed.*) or a water-heater from interfering with the wireless opposite or upstairs which is blaring uninhibited and unashamed!

A. G. MORRIS.

The *Digest* itself had this to say:

A point about the Wireless Telegraphy Bill about which there appears to be considerable feeling is the fact that there is no compulsion on manufacturers of apparatus causing or capable of causing interference with radio, to fit suppressors.

It has been pointed out that a lot of appliances which can cause interference do not in fact do so for several reasons, and secondly that the incorporation of a suppressor raises the cost. . . .

So does the provision of adequate insulation, but no one would argue that an appliance capable of killing the user of it does not necessarily do so.

The fact is that all new electrical equipment should be suppressed, and manufacturers should be made to produce interference-free products.

THINKS PEDRO MISLEADING

Dear Mr. Shunaman:

This will acknowledge, with my thanks, the return of the negative which pictured one of the simple decommissioning devices used in our survey last year.

I acknowledge, too, the January issue of your publication which contains, on page 54, a story titled "The Impeded Double-Cross."

The article, in my opinion, renders a serious disservice, not only to the honorable element in the radio service industry, but to those legitimate agencies of business with whom they are co-operating to improve the ethical standards of the industry.

The distortions, both of fact and technique, which occur in "The Impeded Double-Cross" may result in some confusion in the minds of your readers. I am sure that the majority of them feel, as we do, that these occasional airings have been good for the industry as a whole, because they have paved the way for the establishment of uniform standards of practice and improved customer relations.

Is it possible that the clamor of the guilty few has made a louder noise in your editorial offices than the resultful efforts of the ethical many who are quietly working to maintain the integrity and dignity of the industry?

G. H. DENNISON
General Manager
Better Business Bureau
of Pittsburgh, Inc.

OUR REPLY

Dear Mr. Dennison:

I am at a loss to understand your reaction to "The Impeded Double Cross." I have re-read the article carefully and failed to find any "distortions" either of fact or technique. I would appreciate your calling to my attention any distortions of fact. I feel myself a competent judge of technique, but would also like to hear any comments from your technical contacts concerning supposed "distortions of technique."

I realized from your rather puzzled

WE PAID $1.85 TO $9.50 TO HAVE THESE PRONGS CLOSED.

One of the Pittsburgh BBB's faulty circuits.

RADIO-ELECTRONICS prints several radio cartoons every month. Readers are invited to contribute humorous radio ideas which can be used in cartoon form. It is not necessary that you draw a sketch, unless you wish.

earlier letters that you were not quite clear as to our objections to the type of investigation carried out in Pittsburgh, and felt that the story would clear you up. Now I am not sure what the situation is. It seems possible that you either feel that we object to investigations *per se;* or that you feel that the kind of gimmicking described in "The Impeded Double Cross" is a fair test of an auto mechanic's honesty or ability; or that you may have fallen into that error common to all of us in believing that a given method must be all right simply because you used it.

We are not opposed to investigations. What we oppose is investigations carried on with the help of "gimmicks" or artificial, atypical faults which do not fall within the technician's normal experience, and consequently cause him extraordinary amounts of time and labor to discover.

You will remember that I asked you before: why not get radio service technicians to put the receiver into condition for an investigation; put into it genuine defects like broken-down filter capacitors, burned-out coils and shorted bypass capacitors.

I also pointed out—to head off any argument that similar results might follow a genuine, as would be produced by a "gimmicked", investigation—that just such genuine investigation had taken place. It was conducted by the former New York newspaper *PM* with the object of ascertaining what shops they could recommend to readers. A genuinely faulty radio was found for the test. Before taking it to the first shop, it was examined by a technician, Herbert Roth of the Electronic Corporation of America, who discovered that one section of an electrolytic capacitor was partially open, the set was out of alignment, needed cleaning, and had a burned-out pilot lamp and a line cord broken at the plug. Thus both the gimmick and the almost equally bad trivial complaint were avoided.

The investigation was made in 1946, a wartime shortage year. Yet the highest quotation received was in the order of $8. Only two of the 10 shops canvassed gave an incorrect diagnosis, and of the ten shops, six were recommended by the paper. The recommendation took into consideration such points as price (highest price by a recommended shop was $7.10, lowest $4.75), guarantee, and apparent ability to deliver a good job, as well as honesty.

So you can see that there is a difference between an investigation made with genuine faults and a "gimmicked" one. I mentioned this investigation to you in my letter of May 19, 1948, but you did not refer to it later.

We agree with you that honest, competent investigations might well be "good for the industry as a whole" but have pointed out in articles and editorials that "gimmicked" investigations have harmful features which may neutralize any good done. And it is not the "guilty few" who object strenuously. They would be at as great a disad-

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To help supply this needed manpower, the Milwaukee School of Engineering has expanded its radio and television courses. Now you can get complete practical, technical training in the MSOE laboratories. *This is not just a serviceman's course.* It prepares you for a career in all of the technical phases of television and radio.

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Police, Taxi-Cab and Railroad Receiver Serviceman

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• Heating	• Refrigeration, Heating and Air Conditioning	

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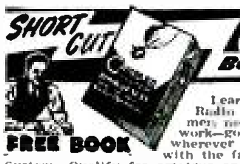
Lincoln Engineering School, Box 931-RE-5, Lincoln 2, Neb.

vantage faced with a legitimate investigation as with an incompetent one. It is definitely the ethical man who feels that his profession has been represented in an incorrect light.

We do not wish to be critical of any action that has already been taken. The Pittsburgh investigation, whatever its faults, produced positive results. Our object is to attempt to persuade you of the reasonableness of our position at least to the extent that, to quote my letter of April 29, 1948, "if other Better Business Bureaus contact you in regard to tests of this type that you advise them to use genuine defective sets or to create genuine defects in the set rather than use 'gimmicks' which cannot give an exact idea of how the repairman would work on a genuinely defective set."

I regret that we have not up to the present been able to convince you of the importance of that one point, as I had hoped that the Pedro story would make the matter abundantly clear to any layman who, while having little knowledge of radio, might be better informed about motor cars and would have sufficient inductive ability to follow the analogy.

FRED SHUNAMAN
Managing Editor



LICENSING TECHNICIANS

Dear Editor:

I am glad to see that Mr. Joseph Amdy was interested enough in licensing (even though opposed to it) to state his views in the January issue. Among other things he says, "Licensing of other trades and professions has not eliminated these evils—there are still worthless and gyp doctors, lawyers, and so on."

There *are* unscrupulous and incompetent people in other businesses and professions. But how many more would there be if there were no licenses? At present anyone can call himself a technician and set up shop. If he is dishonest or ignorant, nothing can be done about it; but if he had a license, it could be revoked and he would go out of business.

My experience has been that mechanics, carpenters, and painters are on the average pretty straightforward businessmen. My experience with radio technicians has been that many are incompetent and dishonest.

If we can have licensed electricians, we can have licensed radio technicians.

WILLARD MOODY,
New York, N. Y.

STATIONS NOT OFF CHANNEL

Dear Editor:

In "European Report" in the January issue of RADIO ELECTRONICS there appeared this statement: "The report on frequency measurements during a recent month, for instance, shows that though 181 European stations deviated by less than 5 cycles from their allotted frequencies, there were 84 whose frequency wanderings exceeded 25 *kilocycles!* In the first class there were 17 French stations and in the second 11."

In the interests of truth as well as the honor of European broadcasting, I must point out that this is a grave error. It is possible that someone accidentally wrote "25 kilocycles" instead of "25 cycles." Our organization possesses a checking center in Brussels for measuring the frequencies of European broadcasting stations. Out of the 400 stations here, not over 20 deviate more than 100 cycles and these 20 are very-low-power transmitters reconstructed after the war as makeshifts. A very large proportion of the stations satisfy the conditions laid down at Atlantic City. Finally, we have never come across a single case of deviation of as much as 500 cycles. There is no French station which deviates more than 50 cycles and most have a stability better than 5 cycles.

We agree that there should be something like a European FCC—allowing for certain differences in the European situation from that in the U.S. It seems to me, however, that there are much more exact and substantial arguments to back this up than the frequency instability mentioned in your article.

H. ANGLES D'AURIAC,
International Broadcasting Organization.
Brussels, Belgium

ADVERTISING INDEX

MAY 1949

RADIO SCHOOL DIRECTORY
(Pages 94-95)

RADIO ENGINEERING, by E. K. Sandeman. Published by John Wiley & Sons, Inc., New York. 5½ x 8¾ inches, 775 pages. Price $6.50.

The author, a former BBC engineer, describes his own book beautifully in the following, taken from the introduction:

"The writer has an infallible method of dealing with all mathematical descriptions. He glances at the type of mathematics involved, and if it is of a type that he can understand, there is evidently no point in reading it. He therefore looks at the conclusions reached to see if they are presented in a useful form. If they are not, the treatise is not very much use anyway! If, on the other hand, the mathematical argument is incomprehensible, there is also no point in reading it. But provided the problem is clearly formulated and the conclusions are clearly stated in explicit form, they may still be of full value to the practical man if he is capable of substituting in a simple formula."

Mr. Sandeman has taken his own admonition deeply to heart. A knowledge of garden-variety algebra and logarithms will carry any reader through the book, even though the pages are sprinkled very liberally with formulae. The point is that each formula is solidly useful for solving one of the intensely practical problems that working radiomen run up against. Wherever there is a chance of obscurity, a sample problem is cited and solved before the reader's eyes.

And yet this *is* an engineering book. It gives the basic facts of electronic life—and in detail. It is thoroughly useful to designers and equally helpful to those who must adjust and service anything from a home receiver to a high-power transmitter.

Many engineering books present theory alone, leaving the reader to correlate this with practice as best he can. Mr. Sandeman has presented all the theory —but he is apparently aware that electronic apparatus exists "in the flesh" as well as on paper!—*R.H.D.*

ATOMIC ENERGY, by Karl K. Darrow. Published by John Wiley & Sons, Inc., New York. 5½ x 8½ inches, 80 pages. Price $2.00.

Dr. Darrow, a noted physicist, has assembled this book from four lectures he gave at Northwestern University in 1947. As a consequence, the style is conversational; with the author's facility for creating mental pictures and his logical, from-the-ground-up approach, this is one of the few books on nucleonics which need not be "waded" through. In fact, it's hard to put down.

The lecturer assumes that the audience has practically no knowledge of even the electron theory. Yet, slowly, surely, and inevitably, he guides his hearers through the complexities leading to the release of nuclear energy. All the basic qualitative (and even a little quantitative) information is given, spiced with history and background.

The book will qualify no one for a degree in nuclear physics, but 76 pages after he begins, the reader will find himself in possession of a larger number of well integrated atomic facts than he would ever have thought possible.

—*R.H.D.*

PRACTICAL TELEVISION SERVICING, by J. R. Johnson and J. H. Newitt. Published by Murray Hill Books, Inc., New York. 6 x 9 inches, 334 pages. Price $4.00.

After opening the book with a basic discussion of television fundamentals, the authors proceed to discuss the television receiver by breaking it down into its r.f., i.f., detector, sweep, video, power supply, and C-R tube circuits, discussing each section in great detail. By so doing, they cover each section of the receiver along with its particular servicing problems without relying on previous discussions or those to come later in the book.

In their discussion of antennas and wave propagation they describe the various types of TV antennas, their characteristics, and the types of transmission lines that may be used under different conditions with advantages and drawbacks of each type.

The section on receiver installation alone is well worth the price of the book to the average service technician or installation man. The authors go into considerable detail on the problems of antenna placement and mounting; supplementing their material with photographs and drawings. One chapter is devoted to the requirements and operation of test equipment for TV receiver servicing. This section ties in nicely with the following discusions on wiring techniques, trouble-shooting, case histories, and common defects which are often found by the technician in TV receivers.

The book concludes with an appendix of tables providing such information as frequencies of TV channels, intermediate frequencies used in many commercial sets, oscillator frequencies for given i.f. channels, characteristics of common transmission lines, and a ten-page glossary of television terms.

"Gosh! My Wife!!"

Suggested by Jack C. Thurston, El Centro, Calif.

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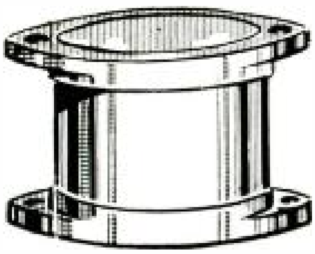
PARTS SHOW VISITORS:

Be sure to visit our tremendous showrooms at 320 N. LaSalle St. Thousands of electronic components conveniently displayed.

SPECIAL LOW PRICES FOR IMMEDIATE SALE AND DELIVERY

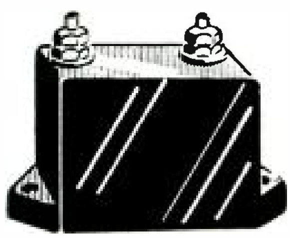
We have literally hundreds of thousands of these top quality standard type transmitting mica condensers in stock for immediate delivery at a fraction of their original cost. Every condenser is brand new and carries the name of a fine nationally known manufacturer.

Despite the unusually low prices, these mica condensers, like all Wells Components, are fully guaranteed. Be sure to order sufficient quantities for your requirements.

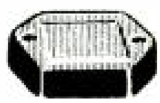


STYLE "AA"

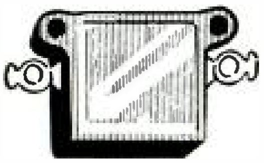
STYLE "A"



STYLE "B"



STYLE "C"



STYLE "D"

Cap. Mfd.	Wrkg. Volts	Mfr. Leg.	Price Each:
STYLE "AA" CONDENSERS			
.02	3000	2	$4.50
.04	1000	2,7	3.50
STYLE "A" CONDENSERS			
25mmfd	10000	8	$1.65
STYLE "B" CONDENSERS			
.00003	2000	2	$0.70
.000047	3000	1	.80
.00005	3000	2,9	.75
.00007	1140	6	.70
.00009	3000	2,7,9	.75
.000091	3000	7	.80
.0001	3000	2,7,9	.80
.000107	3500	1	.85
.00011	3000	8	.95
.00137	3000	2	.95
.000175	1500	8	1.00
.0002	1430	6	1.00
.0002	3000	7,8	1.00
.0002	5000	1,8	1.05
.00025	5000	7	1.10
.0004	3000	2,7	.95
.0004	5000	2,7,8	1.10
.0004	6000	1	1.55
.0005	2000	7	.95
.0005	3000	3	1.00
.00051	3000	7	1.00
.00055	3000	7	1.10
.0006	2500	7	1.05
.0006	5000	8	1.15
.000625	3000	7	1.05
.0007	3000	7	1.05
.00075	2500	2	1.05
.00075	5000	8,9	1.15
.0008	3000	7	1.00
.0008	5000	2,8	1.15
.001	4500	2,9	1.25
.001	5000	7,8	1.30
.0011	5000	2,7	1.35
.00125	2000	7	1.10
.0014	5000	2	1.35
.0015	3000	7	1.10
.0024	3000	8	1.15
.0025	2000	1,2,7	1.10
.00275	2000	1,7	1.10
.003	2000	7	1.20
.004	3000	2,8	1.50
.005	2000	2	1.40
.005	5000	6,8	1.70
.006	2500	7	1.30
.006	3500	8	1.45
.0068	3000	8	1.40
.008	3000	7,8	1.45
.01	2000	1,2,3	1.55
.01	1000	7	1.35
.02	600	7	1.30
.02	2000	2,8	1.60
.024	1500	3	1.60
.033	1500	3,7	1.60
.056	1000	3,7	1.70
.06	1000	8	1.70
.1	1000	8	1.75
STYLE "C" CONDENSERS			
.000005	2500	2	$0.40
.00005	600	7,8	.30
.0001	600	2,7	.25
.0001	1200	7	.35
.0001	2500	4,7,8	.40
.0002	600	2,7,9	.25
.0002	2500	7	.40
.00024	2500	7,8	.45
.00025	2500	2	.45
.0003	2500	7	.45
.00039	2500	7	.50
.0004	2500	2,7,9	.45
.0005	600	1,7	.35
.0005	1200	2,7	.40
.0005	2500	1,2	.45
.001	1200	2,7,8	.40
.001	2500	6,7	.55
.001	3750	7	.85
.0011	600	2	.35
.002	600	7	.35
.002	1200	2	.45
.002	2500	1,2,8	.55
.002	3500	8	.80
.0022	2500	7	.60
.003	600	8	.40
.0035	2500	7,9	.60
.0039	2500	2	.60
.004	2500	2,7	.60
.0045	600	8	.40
.0046	500	9	.45
.0047	2500	8	.65
.005	600	2	.35
.005	1200	7,8	.45
.005	2500	7,8	.60
.0051	1200	7	.45
.0051	2500	7,8	.65
.0056	2500	8	.65
.006	600	7,9	.40
.006	2500	7	.65
.0068	1200	7	.60
.007	600	8	.35
.0075	1200	2	.55
.009	600	9	.50
.01	600	2,7,8	.40
.01	1200	3,7,8	.45
.01	2500	7,8	.60
.0115	600	8	.40
.013	1200	3	.55
.015	1200	7	.55
.015	2000	8	.60
.015	2500	7,8	.60
.0175	1200	2	.55
.02	600	7	.35
.02	1200	7	.45
.022	1200	7	.45
.025	600	8	.35
.03	600	6	.35
.03	1200	2,8	.50
.033	600	7	.35
.033	1200	8	.50
.04	600	7,8	.35
.073	250	8	.40
STYLE "D" CONDENSERS			
.00004	600	7	$0.20
.00005	1200	1,7,9	.25
.00005	2500	2,8,9	.30
.0001	600	9	.20
.0001	1200	7,8	.25
.00015	2500	2,6	.35
.00024	2500	6	.35
.00025	1200	6,8	.25
.00025	2500	6,8	.35
.0005	1200	7	.30
.00051	2500	1	.35
.0007	600	2	.25
.001	600	2,8	.25
.001	1200	6,8,9	.35
.001	2500	6,8	.40
.0011	2500	8	.40
.002	600	1,2,9	.25
.002	1000	8	.30
.002	1200	6,7,8	.35
.002	1250	1	.35
.002	2500	8	.40
.0022	1200	8,7	.30
.0022	2500	8	.40
.0025	600	2	.25
.0025	1200	1	.30
.0027	600	1	.25
.003	600	2	.25
.003	1200	6,7,8	.30
.0033	1200	6	.30
.004	1100	8	.35
.004	1200	7,8	.35
.004	2500	9	.45
.0044	600	8	.25
.0047	2500	6,8	.40
.005	600	2,6,7	.25
.006	600	1,2	.25
.01	600	2,7,8	.30
.01	1200	6,7,8	.40
.01	1250	1,6,9	.40
.01	2500	2,8	.50
.02	600	2,6,8	.25
.022	600	7	.25
.025	1200	7	.35
.027	600	7	.25
.03	600	2,8	.25
.05	600	7	.30

Manufacturers' Legend:

1—Aerovox; 2—Cornell Dubilier; 3—Faradon; 4—General Electric; 5—Illinois; 6—Mica-Mold; 7—Sangamo; 8—Solar; 9—Sprague

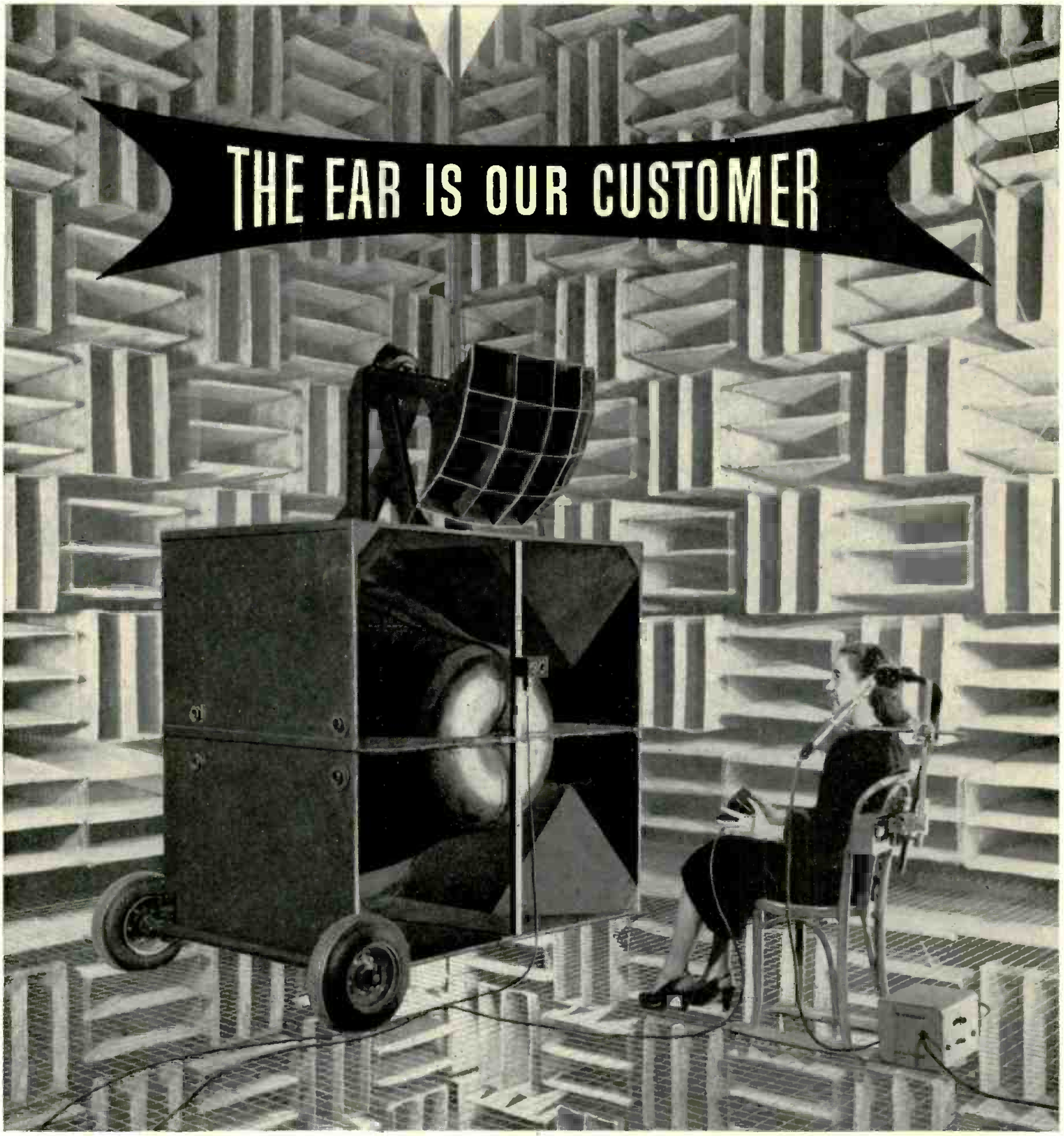
This is only a partial listing. Write or wire for information on types not shown and for receiving set micas and silver micas.

We advise distributors to order immediately from this ad. Our standard jobber arrangement applies.

Manufacturers and Distributors: Write for our complete Mica Condenser Listing No. 103A.

WELLS SALES, INC.

320 N. LA SALLE ST. DEPT. Y, CHICAGO 10 ILL.


THE EAR IS OUR CUSTOMER