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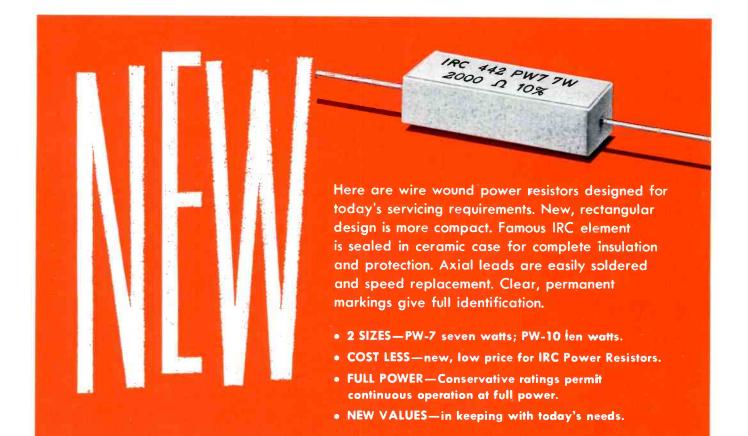


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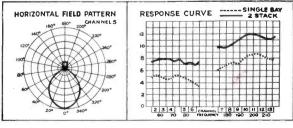
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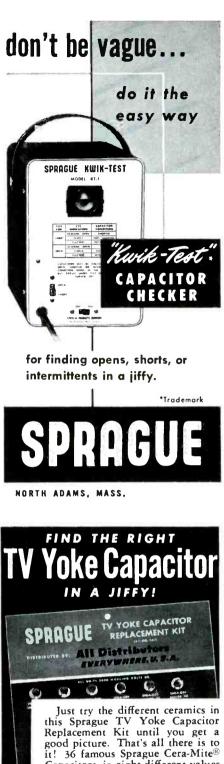


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CONTENTS

Capacitors			•			. James M. Foy 5
Color TV Training Series (Part VIII)						
Audio Facts			11			. Robert B. Dunham 11
Transistor Radios Are Here	2	\mathcal{L}^{2}				William E. Burke 13
Shop Talk						. Milton S. Kiver 15
A TV-Receiver Check Tube						W. William Hensler 17
Notes on Test Equipment						Paul C. Smith 19
Examining Design Features	0					Don R. Howe 21
Shop Tickets						. Henry A. Carter 25
The Garage-Door Opener						. Don R. Howe 27
In the Interest of Quicker Servicing	ŝ.	٢		4		Henry A. Carter and Calvin C. Young, Jr. 29
Dollar and Sense Servicing				G.		υ,
Stocking the Tube Kit					L.	
Photofact Cumulative Index No. 48 Covering Photofact Sets—Nos. 1-	263	In	clusi	ve		

SUBJECT REFERENCE

ANTENNAS AND ACCESSORIES	SERVICING
Antenna Response Curves 15	Garage-Door Opener, Perma-Power Model RC101
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27 76

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88

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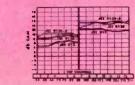
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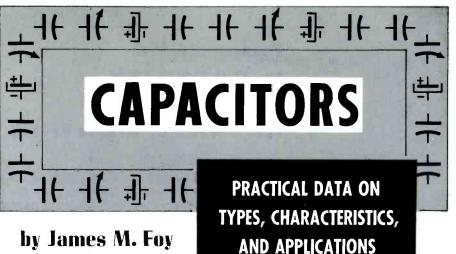
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With the exception of vacuum tubes, no other circuit element causes as much trouble as does the capacitor. Most of the troubles encountered in these units are shorts within the capacitor and leaky or open circuits between the plates. To a lesser degree, troubles will be caused by arcing and, in certain critical applications, by changes in capacity. In the following article dealing with the theory and construction of capacitors, an effort has been made to cover some of the points which may lead to a better understanding of these troubles and their causes. Although several different types of capacitors are used in radio and television circuits, some of these types are quite simple in construction and cause little trouble. Only the basic design and construction of these will be covered. Because the electrolytic capacitor is unique in its characteristics, the major part of this discussion will be confined to this type.

THEORY

In general, we can say that all capacitors are devices for storing static electricity. They are composed of two electrodes separated by a thin dielectric or insulating medium. The electrodes are usually constructed of metallic members or plates, and the dielectric may consist of gasses such as air; liquids such as mineral oil; or solids such as mica, glass, waximpregnated paper, and other materials. Fig. 1 is an example of a basic capacitor.

Capacitors are rated according to their voltage and capacity, with the voltage rating being the maximum amount of potential that should be applied across the plates. If a greater amount of voltage is used, arcing may possibly occur with a resultant breakdown of the insulation. This breakdown occurs when a spark jumps between the electrodes through a tiny flaw in the insulation. The heat generated by the spark burns out the insulation, and it becomes conductive. If the arcing is very severe, the heat may even become great enough to melt the foil of the plates and thus create a direct short circuit.

Capacity is a measure of the quantity of electricity that can be stored at a given potential. The unit of capacitance is the farad, which corresponds to one coulomb of electrical energy at one volt of pressure. (In actual practice, since the farad is too large a unit for practical use, capacitors are rated in microfarads or in micromicrofarads. A microfarad is one millionth of a farad, and the micromicrofarad is one millionth of a microfarad. The determining factor for capacity value will be discussed later in the article.) The relationship of capacitor charge can be expressed as:

Q = CE,

where

- C = farads,
- E = volts,
- Q = coulombs.

Thus, it is evident that the amount of charge in a capacitor is directly proportional to the applied voltage. From this relationship, we can see that when a direct current is applied to the

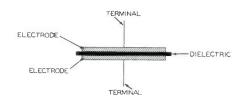


Fig. 1. Component Parts of Basic Capacitor.

plates of a capacitor, a static charge is established in the dielectric. This static charge rises until it is equal to the source voltage. When this point is reached, the source voltage is opposed by the electrostatic charge and there can be no further flow of current into or out of the capacitor unless the source voltage either rises or falls. If the source voltage rises above the electrostatic charge, additional current will flow until the charge again equals the applied voltage. If the source voltage falls below the electrostatic charge, current will flow from the capacitor into the circuit until the capacitor charge drops to a value equal to the applied or source voltage. Through utilization of this principle of charge and discharge, capacitors can be used as filters to smooth out ripple voltages; to block direct current; and to bypass alternating current wherever necessary.

Three physical factors govern the capacitance of a capacitor. The capacity is directly proportional to the area of the plates and inversely proportional to the thickness of the dielectric. This statement is easily proved when we look at the formula for computing the capacity of a simple capactior, such as the one diagrammed in Fig. 1. This formula is:

$$C = \frac{8.84 \times K A}{10^8 \times D},$$

where

C = capacitance in microfarads,

- K = dielectric constant for the dielectric being used,
- A = area of one side of one of the plates in square centimeters,
- D = thickness of the dielectric in centimeters.

When multiple plates are used to increase the capacity, a modification of the formula just given can be used. In this instance, we have:

$$C = \frac{8.84 \text{ x K A (n - 1)}}{10^8 \text{ x D}},$$

where

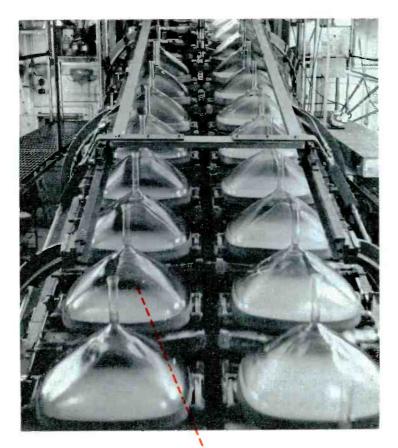
n = the total number of plates.

Thus, we see that the capacity of a capacitor will increase when the plate area is increased; it will also increase if the thickness of the dieelectric is reduced. This is an important point to be remembered.

* * Please turn to page 62 * *

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5



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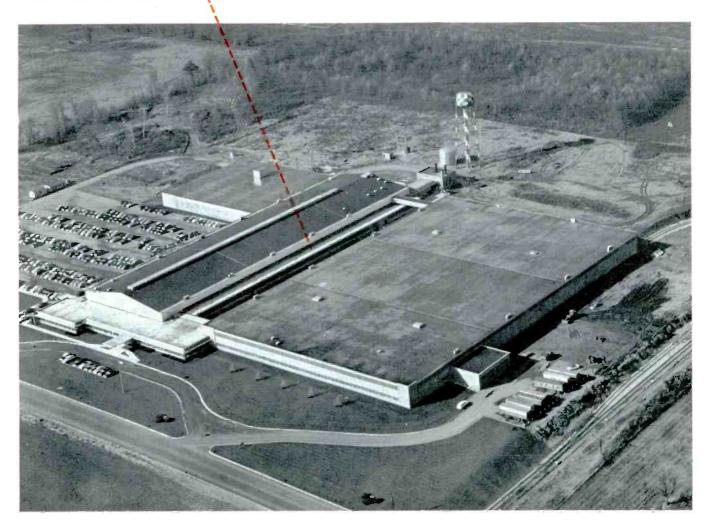


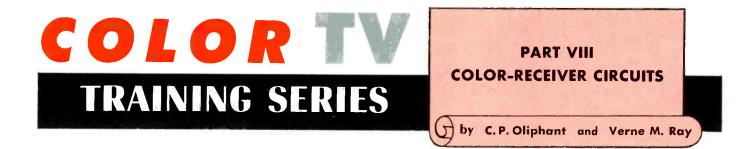
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Part VII of this Color TV Training Series covered the theory of synchronous demodulation and discussed the operation of two commercially used demodulator circuits. In this part, additional demodulator circuits will be discussed and the operational theory of the matrix section will be covered. Typical commercial matrix circuits will also be described.

Demodulator Using a Sheet-Beam Tube

The 6AR8 is a sheet-beam tube which contains double plates, a pair of balanced deflectors which direct the beam to either of the two plates, and a control grid to vary the intensity of the beam. Through the use of this tube, balanced output signals of both positive and negative polarities are developed, thus eliminating the need for phase-inversion stages after the chrominance signal is demodulated.

Shown in Fig. 7-27 is the physical structure of the 6AR8. Fig. 7-27A shows the schematic of the tube and the pin connections of each of the tube elements. Pins No. 1 and No. 2 connect to the deflector plates. Pin No. 3 is the accelerator terminal which is the third grid. Pins No. 4 and No. 5 are the heater connections, with pin No. 5 being the terminal for the internal shield and focus electrodes. The focus electrodes are shown as the second grid. Pin No. 6 is the terminal for the control grid. The cathode is pin No. 7, and the two plates are pins No. 8 and No. 9.

Fig. 7-27B is a cross-section drawing of the 6AR8. The electrons pass from the cathode to either of the two plates in the form of a planar beam or sheet; from this comes the name, sheet-beam tube. After being emitted from the cathode, the electrons are acted upon by the conventional control grid which controls the intensity of the beam. Next, the focus electrodes serve to converge the electrons into the required sheet beam. Then the beam of electrons is accelerated by the acceleration electrode and then is deflected to either of the two plates by the deflectors. The function of the internal shield is to suppress the interchange of secondary-emission electrons between the plates.

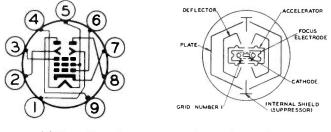


Fig. 7-27. Physical Construction of the 6AR8 Tube.

(A) Basing Diagram.

(B) Cross-Section Drawing.

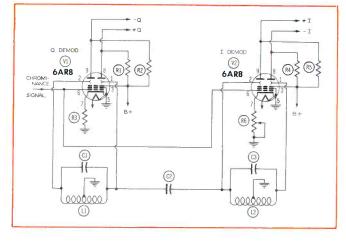


Fig. 7-28. Basic Circuit of Demodulators Using Sheet-Beam Tubes.

Under normal operation, positive DC voltages are applied to the accelerator and the plates. Signal voltages are applied to the deflectors and the control grid. The frequency of the signal voltages on the deflectors determines the rate at which the beam is switched from one plate to the other. The control-grid voltage varies the magnitude of the plate current. The 6AR8 can be compared to a voltage-controlled single-pole double-throw switch through which a current flows.

Shown in Fig. 7-28 is the basic diagram of two demodulator circuits using 6AR8 sheet-beam tubes. The chrominance signal is applied to the control grid of each stage in order to control the plate current in the demodu lators. Two CW signals are applied to the deflector plates of each demodulator, and two output signals from each stage are produced. The CW signal which is in phase with the Q vector is applied to terminal No. 2 of the Q demodulator. This will result in the tube current of the Q demodulator being deflected to plate No. 1 during the positive portion of the applied reference signal. On the other deflector plate of the Q demodulator, the CW reference signal is applied after it has been shifted 180 degrees. This shifting is accomplished by passing the reference signal through coil L1 and will result in the tube current being deflected to plate No. 2 during the time that the reference signal is positive; thus, the plate current is switched from plate to plate by the voltage applied to the deflectors. The rate at which the switching takes place is determined by the CW-signal frequency which is 3.58 megacycles. Since the frequency of the chrominance signal is the same as that of the reference signal, the current in the demodulator will be switched from plate to plate each half cycle (180 degrees) of the chrominance signal. This action produces a signal of positive polarity on one plate and one of negative polarity on the other plate.



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Cathode bias for the Q demodulator is provided by resistor R3. The accelerator anode is directly connected to the B_+ supply, and the plates are tied to B_+ through the plate-load resistors R1 and R2. The output from one plate of the Q demodulator is a negative Q signal, and the output from the other plate is a positive Q signal. The negative Q signal is present on plate No. 1, and the positive Q signal is present on plate No. 2.

The I demodulator is similar in operation to that of the Q demodulator. The CW signal fed to the deflectors is shifted the necessary 90 degrees by capacitor C2. The reference signal is fed to deflector No. 1 of the I demodulator at this phase and is shifted 180 degrees by coil L2 before being applied to deflector No. 2. This controls the deflection of the current in the I demodulator from plate to plate in the push-pull manner as it does in the Q demodulator.

The I demodulator has a variable cathode-bias resistor R6 which controls the gain of this stage so that the relative gains of the two demodulators can be adjusted. The accelerator anode of the I demodulator is tied directly to B+, and the plates are connected to B+ by resistors R4 and R5. The output of the I demodulator consists of a positive I signal which is present on plate No. 1 and a negative I signal which is present on plate No. 2.

The sampling process of the sheet-beam demodulator is similar to that of the demodulators previously discussed. In the other demodulators, the sampling time is very short; but in the sheet-beam demodulator, the sampling time is very long. The chrominance signal is sampled by the sheet-beam demodulators at four places instead of two, which is the case for the other demodulators. The chrominance signal is sampled during the positive and negative portions of its cycle. Whenever a chrominance signal contains both I and Q information, it is sampled twice by the I demodulator and twice by the Q demodulator. This way, an I signal of both polarities and a Q signal of both polarities are produced at the plates of the demodulators.

The sampling process of the sheet-beam demodulators is shown in Fig. 7-29 which illustrates three different conditions. Sine wave A represents the chrominance signal when it contains only Q information. Sine wave B shows the condition when only I information is present. During the time of sine wave C, both I and Q information are present in the chrominance signal.

During chrominance signal A, there would be an output signal from the Q demodulator but none from the I demodulator, since the chrominance signal is going through zero during the sampling time of the I demodulator. When sine wave B is being sampled, there would be an output signal from the I demodulator but none from the Q demodulator because the sine wave is passing through zero during the sampling time of the Q demodulator. In the case of chrominance signal C, there will be an output from both demodulators. A Q signal of both polarities and an I signal of both polarities will be produced.

Actually a sheet-beam demodulator can be looked upon as being two separate synchronous-demodulator stages in which one is being controlled by a positive reference signal and the other is being controlled by a negative reference signal. From two such demodulators, there would be an output signal of one polarity from one of them and an output signal of the opposite polarity from the other.

Diode Demodulators

A basic circuit employing diode demodulators is shown in Fig. 7-30. Two twin-diode tubes are employed

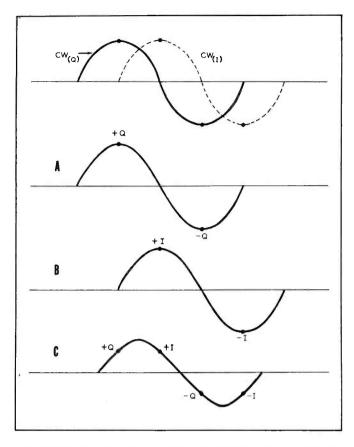


Fig. 7-29. Sampling Process of the Sheet-Beam Demodulators.

in this circuit. One pair of diodes is for the R - Y demodulator, and the other pair is for the B - Y demodulator. Each demodulator is connected so that one section will produce a rectified output voltage of positive polarity at its cathode, and the other section will produce a rectified output voltage of negative polarity at its plate.

In the R - Y demodulator, the chrominance signal is applied to the cathode of section A and to the plate of section B. The chrominance signal at the plate is 180degrees out of phase with the chrominance signal at the cathode. This phase reversal is due to the action of the

* * Please turn to page 33 * *

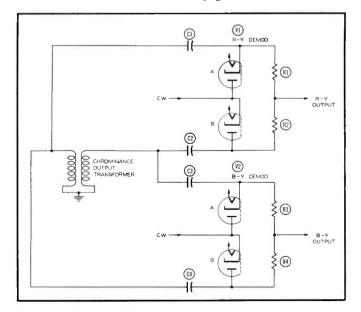


Fig. 7-30. Basic Diode Demodulator Circuit.



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RAYTHEON 3AL5 is a heater-cathode type double diode of miniature construction. Its principal ap- plication is as a diode detec- tor, automatic volume control rectifier, or as a low current power rectifier.	RAYTHEON 3AU6 is a heater-cathode type, sharp cutoff pentode of minia- ture construction designed for service as a high-fre- quency amplifier in radio and television receivers.	RAYTHEON 3BCS is a heater-cathode typer- sharp culoff pentode, of min- iature construction. Used as an RF amplifier and as a high- frequency, intermediate am- plifier.	RAYTHEON 3BN6 is a 7-pin miniature, heater- cathode type, sharp cutoff pentode. Designed to perform the combined functions of limiting and frequency dis- crimination in FM and TV re- ceivers.	RAYTHEON 3CB6 is a heater-cathode type sharp cutoff pentode of min- iature construction designed for use as an intermediate frequency amplifier, operating at frequencies in the order of 40 megacycles, or as an RF amplifier in VHF Television Tuners.
RAYTHEON 5AM8 is a diode pentode of minia- ture construction designed for use as a video detector and IF amplifier in television re- ceivers.	RAYTHEON 5AN8 is a medium-mu triode and a sharp cutoff pentode of min- iature construction designed to perform combined func- tions of a video detector or IF amplifier and sync separator.	RAYTHEON 5J6 is a heater-cathode type, double triode of miniature construction designed for mixer applications.	RAYTHEON 5U8 is a heater-cathode type tri- ode-pentode of miniature con- struction designed for use as an oscillator mixer.	RAYTHEON 654A is a heater-cathode type medium-mu, high-perveance triode of miniature construc- tion for use as a vertical de- flection amplifier in TV re- ceivers.
RAYTHEON 6SN7GTB is a dual triode designed for use as a combined vertical os- cillator and vertical deflection amplifier in television re- ceivers.	RAYTHEON 7AU7 is a heater-cathode type double triode of miniature construction designed for use as a resistance coupled volt- age amplifier, phase inverter, horizontal deflection oscilla- tor or vertical deflection os- cillator-amplifier in television receivers.	RAYTHEON 12AX4GTA is a heater-cathode type di- ode designed for use in Hori- zontal frequency damper service in television receivers.	RAYTHEON 12BH7A is a heater-cathode type medium-mu double triade of miniature construction de- signed for use as a vertical de- flection amplifier in television receivers employing "Series String" heater designs.	RAYTHEON 12BK5 is a miniature beam power pentode designed for use as a power output tube in radio and TV receivers.
RAYTHEON 12BY7A RAYTHEON 12L6GT s a heater-cathode type is a heater-cathode type between pentode of miniature con- truction designed for use as is a heater-cathode type s video amplifier. between pentode power ampli- fier. Generally used as an out- put tube in ac-dc receivers. RAYTHEON 12W6GT s a heater-cathode type between pentode designed for service as a vertical deflec- tion amplifier in TV receivers Ask your Raytheon Tube Distributor service as a vertical deflec- tion amplifier in TV receivers Service as a vertical deflec- tion amplifier in TV receivers Service as a vertical deflec- tion amplifier in TV receivers				

Receiving and Cathode Ray Tube Operations

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Kits for Constructing High Quality Preamplifiers and Amplifiers.

TRIAD KITS

Any one who wishes to construct his own audio equipment can have a lot of profitable fun while designing and building a preamplifier or amplifier, but a number of problems are usually encountered both before and after actual construction is in progress. These problems must be considered and solved if the desired results are to be obtained from the completed unit.

For instance, if the constructor wants to design and build a preamplifier, he must among other things decide how many inputs and outputs are required; what type of phono preamplifier circuit will be most suitable: which of the many methods of tone control should be chosen; what kind of output circuit will serve best in matching the unit to the rest of the equipment; and whether the unit should be self-powered or obtain its power from the power supply of the power amplifier. After these things have been decided and circuit components have been selected, these components must be mounted on a suitable chassis or in a cabinet or box before the preamplifier can be used properly with the rest of the audio system. Working

out a satisfactory layout of the parts and drilling, punching, or cutting the necessary holes in which to mount them can be time-consuming chores. Correct placement and proper mounting of the parts have a great influence upon the results to be obtained from the completed unit as well as upon its appearance and convenience of operation.

Most of the same problems will be encountered when the audio enthusiast constructs an amplifier. He must decide whether or not he wants preamplifier and control circuits included on the same chassis with the power amplifier, how much power output is desired, what output tubes and transformer will have to be used in the circuit selected, and what the power-supply requirements will have to be.

Now all of this can be a lot of fun and can serve as a challenge to any one with the ability and time to work out all of the design and layout details. The constructor who does not have the time or inclination to develop the equipment "from scratch" may find just what he is looking for in the Triad kits shown in Figs. 1 and 2.

by Robert B. Dunham

There are many advantages to be gained by using one of these kits. The circuits have been tried and proved, so the constructor knows what he is getting before he even starts construction, that is, if he will follow the detailed data furnished with the kit. A large-sized schematic; a pictorial drawing showing the actual layout, mounting, and point-to-point wiring of all components; and a detailed construction procedure are supplied with each kit. Also included is a complete and itemized parts list giving parts numbers and specifications of the parts recommended for use in the unit being constructed.

All appropriate transformers and chokes are supplied with each kit. A punched aluminum chassis, a gray enamel hammertone-finished front panel, and decals are added features.

* * Please turn to page 59 * *







Fig. 2. Triad HF-12 10-Watt Amplifier Kit.

January, 1955 - PF REPORTER



RCA WR-89A Crystal-Calibrated Marker Generator RCA WR-59C Television Sweep Generator

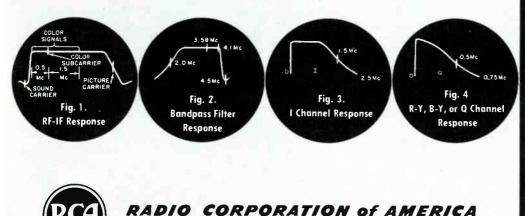
RCA WV-97A Senior VoltOhmyst®

In color receivers, all of the color information is contained in the region from about 2 Mc to 4.1 Mc on the over-all rf-if response curve, as shown in Fig. 1. Any loss of gain in this region will weaken the color signals. If the loss is appreciable, it may result in such effects as poor color sync, poor color "fit" (incorrect registration of color and brightness information on the kinescope), or cross-talk or color contamination between I and Q channels.

The rf-if amplifiers must be aligned correctly to provide flat response for modulating frequencies up to 4.1 Mc. The RCA WR-59C Sweep Generator and WR-89A Marker Generator provide the flatness of sweep output and crystal accuracy essential for aligning color circuits.

In color receivers, there are a number of video-frequency sections, including the video amplifier, the bandpass amplifier, the demodulator channels (see Figures 2, 3, 4), and the green, red, and blue matrix networks—including the adders and output stages. A flat video sweep extending down to 50 Kc is a necessity in checking or aligning the tunable bandpass filter and the I and Q filters. Late model RCA WR-59C Sweep Generators provide a flat video sweep extending down to 50 Kc. They also cover all rf and if ranges required for both color and black-and-white receivers.

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TEST EQUIPMENT

REMEMBER that the high voltage (up to 30,000 volts and more) must be set to the specified value before adjusting purity and comvergence. The RCA Volt-Ohmysts can be used with the RCA High Voltage Probe (WG-289 and WG-206 Multiplier Resistor) to measure dc voltages up to 50,000 volts.



Now off the press-RCA's new enlarged, 2nd edition of "Practical Color Television for the Service Industry." Price: \$2.00-from your RCA distributor.

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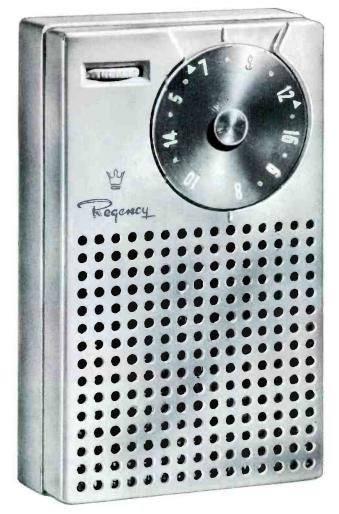
TRANSISTOR RADIOS are here

A DESCRIPTION OF THE REGENCY MODEL TR-1 POCKET RADIO

The advent of transistors into the commercial products which the service technician will eventually encounter has been predicted many times in the past several years. The volume production of the first of such items has recently been announced by Regency, a division of Industrial Development Engineering Associates, Inc., (I.D.E.A.) of Indianapolis, Ind. It is the Regency Model TR-1 completely transistorized pocket-sized radio receiver. Four transistors replace the four vacuum tubes commonly found in battery receivers.

Since Regency is located in the vicinity of our company, the author was priviledged in being allowed to examine several of these receivers in detail and in seeing the production line where the receivers are assembled. This article is presented as a preview of the circuitry used in the Model TR-1 so that the service technician can become somewhat familiar with the type of receiver which he may expect to encounter in the future.

BY WILLIAM E. BURKE



General Features

This receiver has been completely transistorized; in addition, it has been miniaturized to the point where it truly is a pocket-sized radio receiver. The dimensions of 5 inches by 3 inches by 1 1/4 inches are small enough so that the receiver conveniently fits into the pocket of a man's shirt. The size of the receiver can be judged from the fact that the picture in the heading of this article shows its actual size. The receiver

* * Please turn to page 55 * *

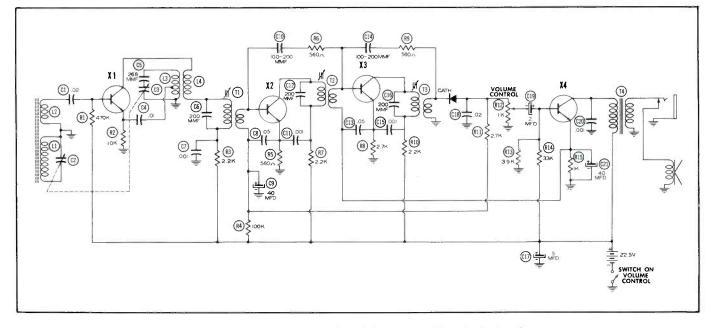
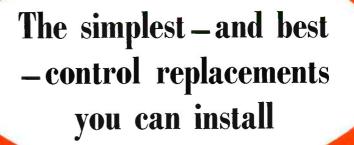


Fig. 1. Schematic of Regency Model TR-1 Pocket-Sized Radio Receiver.

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MILTON S. KIVER

President, Television Communications Institute

ANTENNA RESPONSE CURVES

Several months ago, some basic facts about antennas were discussed in this column. At that time, the reasons were given for the different lengths which may be encountered in antennas designed to operate on the same frequency. In this month's column we would like to probe deeper into the subject of antennas because of the particular importance of that portion of a receiving system.

A manufacturer likes to present his product in its most favorable light. Anyone who has done any buying is well aware of this practice. As part of the presentation, the manufacturer frequently uses engineering charts and data; and in order to judge these facts competently, the service technician must be capable of interpreting them correctly. There are a few pitfalls that he may encounter, and it might be of interest to see what these are.

One type of chart which is frequently included with technical equipment is a graph that depicts operating characteristics. For antennas, two typical response curves are shown in Fig. 1. Both reveal how the response of an antenna will vary with directional angle. Curves of this type are very common in antenna sales literature. These are further supplemented by data concerning such things as the materials used in the structure, the ease in mounting, and the gain to be expected.

Although nearly all response curves are smoothly drawn and symmetrically placed, as shown in Fig. 1. these are in reality only idealized. curves. It is more likely that an actual curve would appear as shown in Fig. 2, and eventhis would be true only under the specific conditions observed by the manufacturer intesting the array. If you erect the same array in some area where space is limited and where there are a number of nearby antennas and steel buildings, then the response curves can be modified to a remarkable degree. This is obviously not the responsibility of the antenna manufacturer: the problem, rather, must be faced by the technician.

Another fact, about which the technician should be cognizant concerning response curves, is the difference which the use of power or voltage units will have on the shape of the curve. In Fig. 1, we have two response curves; and if these are

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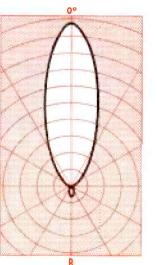


Fig. 1. Typical Antenna-Response Curves.

carefully examined, the conclusion is reached that the response of Fig. 1B is more desirable than the response of Fig. 1A. For one thing, the curve of Fig. 1B is narrower and therefore indicates better discrimination against undesired signals from directions adjacent to the direction marked zero degrees. Also, the rear lobe shown in Fig. 1B is smaller than that in Fig. 1A, and we would expect to have less rear-signal pickup on the second array. In view of these considerations, any technician faced with the choice of both antennas would undoubtedly tend to favor the second.

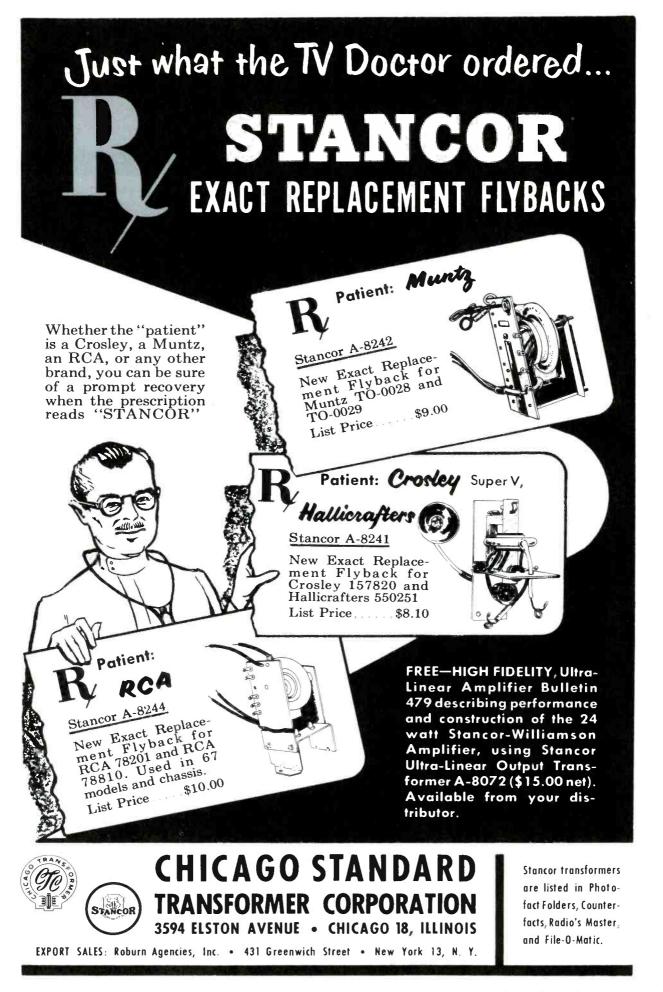
Unfortunately, neither antenna offers any more advantages than the other because both curves are for the same array! The reason the curves differ in appearance is that one is plotted in terms of relative voltage, whereas the other is fashioned by the use of relative power. To appreciate the reason why the change in units should make any difference, it must be recalled that power is proportional to the voltage (E) squared, or

power =
$$\frac{E^2}{R}$$

In the polar diagrams of Fig. 1, everything is expressed in relation to the maximum gain in the forward direction. This occurs at the point marked zero. If a point which is 30 degrees away from zero provides the antenna with only half the signal that it does at zero; then on the polar diagram using voltage values, the curve at 30 degrees will extend along its radial line only half the distance that it does at zero. On the polar diagram based upon power values, however, the amplitude at 30 degrees will be one half squared or one fourth the amplitude at zero. On a power plot, the curve will obviously be narrower and will seem to the

* * Please turn to page 70 * *

January, 1955 - PF REPORTER



Have you ever wished for a device that would permit the cabinetmounted picture tube to be left in the cabinet while the receiver is being serviced in the shop? Have you ever wished that you had a universal picture tube which could be inserted into any TV chassis while the set is being serviced? A TV-receiver check tube, now being manufactured by the Sylvania Electric Products Inc., fulfills these wishes.

This tube which is designated as a 5AXP4 is a 5-inch, round, magnetically deflected tube using electrostatic self-focusing. It is so designed that it can be inserted into any receiver which employs electromagnetic deflection. Since the tube has a focus system built into it, no focus mechanism needs to be used on the tube nor does the ion trap need to be installed while making tests on a receiver. The tube is so light that the voke of the receiver will very easily support the tube. The only electrical connections required are the highvoltage lead and the picture-tube socket of the receiver. The tube may be used in any receiver regardless of the deflection angle. When it is being used in a 90-degree deflection system, some oversweep of the tube face is experienced. This presents no problem, however, since the portion of the picture which is visible makes possible an accurate check on the operation of the receiver.

There are several advantages afforded by this tube. To illustrate how it can be employed as a servicing tool, let us point out a few of its applications. One of the most timeconsuming steps in the removal of a receiver from the cabinet is that of removing the cabinet-mounted picture tube. In many instances, several brackets are employed to hold the picture tube in the cabinet. The removal of these brackets not only takes considerable time but also exposes the picture tube to possible breakage. Since the TV-receiver check tube can be used in the shop as a substitute for the original tube in the receiver, it is not necessary to remove the large tube from the cabinet. After the receiver chassis and the deflection yoke have been removed from the cabinet, they can be taken to the service shop where complete analysis of the operation of the receiver can be made. The ease with which the yoke can be removed from the picture-tube assembly is illustrated in Fig. 1. The focus assembly is removed first, and the wing nut holding the deflection yoke is removed. The yoke can then be slipped off the neck of the tube, as shown in the illustration. After the receiver is placed on the bench in the service shop, the deflection yoke is

A TV Receiver Check Tube

The Uses of The New Sylvania 5AXP4 as a Servicing Tool

slipped over the neck of the check tube and the picture-tube socket and high-voltage lead are connected. A thorough analysis of the receiver operation can then be made. This procedure of leaving the picture tube in the cabinet can be followed in almost every instance except in those cases in which the picture tube itself is suspected. If, however, the trouble in the receiver is obviously not being caused by the picture tube, there is no need for its removal.

This suggests another application for the TV-receiver check tube. It is the use of the 5AXP4 as a substitute for the picture tube in the receiver to determine whether or not the original tube is operating properly. The substitution of the picture tube presents quite a problem in many service shops since it is not possible to stock all types of picture tubes.



by W. W. Hensler

Thus, when a tube is suspected of being defective, there may be no real means of verifying the suspicion unless another tube can be substituted. It is true that a test of the tube on a reliable picture-tube tester will indicate the condition of the tube in most cases; however, a more positive test is made through substitution. Since the installation of the 5AXP4 is a very simple one, the substitution tests can be made in a very minimum of time; and the results are very conclusive.

Another advantage offered by the 5AXP4 is brought about by its small size. Fig. 2 shows a receiver with a vertical chassis and its 17-inch picture tube mounted in place on the chassis. As can be seen in the photograph, the presence of the large tube

Fig. 1. Removing Yoke From the Neck of a Cabinet-Mounted Tube.



^{* *} Please turn to page 80 * *

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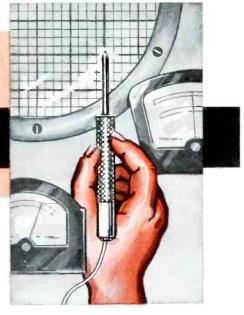
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PF REPORTER - January, 1955



TEST EQUIPMENT



Presenting Information on Application, Maintenance, and Adaptability of Service Instruments



Fig. 1. Hickok Model 755 Noise Generator.

Hickok Model 755 Noise Generator

The Hickok Model 755 noise generator pictured in Fig. 1 provides a convenient means for checking the noise figure in decibels of amplifiers or receivers that operate in the range of 10 to 250 megacycles. The benefits of increasing the sensitivity of a receiver for weak-signal reception can be nullified if the signal-to-noise ratio is lowered at the same time. Therefore, some way of determining the noise characteristics of the receiver or amplifier is necessary for proper evaluation of performance. Generally speaking, the lower the noise figure obtained by means of the Hickok Model 755 noise generator, the better the reception of weak signals by the television receiver.

The Model 755 noise generator is entirely self-contained and requires no external associated equipment for making the tests for the

noise figure. Three push buttons are provided for OFF, ON, or STAND-BY operation. A green pilot light indicates the STAND-BY condition, and a red pilot light indicates the ON condition. A four-position RANGE switch for the VTVM provides for selection of the proper range for the noise voltage being measured. A ZERO ADJUST knob is mounted directly below the RANGE switch and is also directly above the VTVM input terminals. On the front panel are mounted two meters, the one on the left for VTVM readings and the other for reading the noise figure in db. The noise-figure meter is calibrated with three scales which are marked with 50, 75, and 300 ohms respectively. The proper scale is selected to correspond to the impedance of the antenna input of the receiver being measured. An output control regulates the strength of signal supplied by the noise diodes of the instrument. This control has a spring return to prevent operation of the noise diodes at high output for any excessive period of time. The diodes are enclosed in

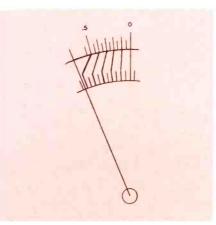


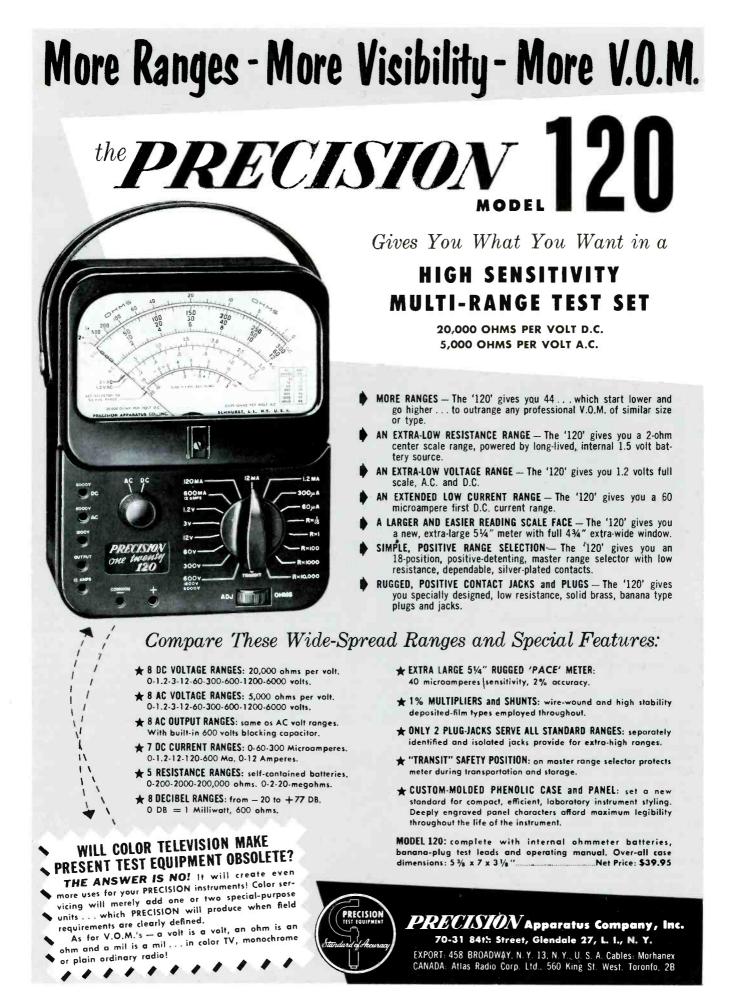
Fig. 2. Portion of the VTVM Scale on the Hickok Model 755 Noise Generator.

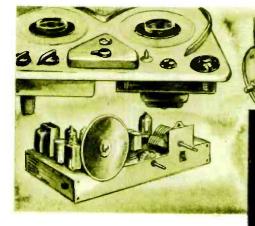
by Paul C. Smith

a small shielded box or head at the end of the output cable. Three binding posts on this head are provided for connecting to either 300-ohm or 75ohm antenna inputs. When the head is not in use, it can be stored in a receptacle on the front panel.

A noise reading is easily made in the following manner. After a short warm-up period for both the instrument and the receiver, the output of the generator is connected to the input terminals of the receiver. The proper binding posts on the head con taining the diodes are chosen to match the input impedance of the receiver. The VTVM section of the noise generator is connected across the videodetector load. The tube immediately preceding the video detector is removed from its socket, and the ZERO ADJUST knob is set for zero at the center of the meter scale. This adjustment cancels any contact potential present at the video detector. Then the video IF tube is replaced in its socket; and after it has warmed up, a deflection of the VTVM pointer will be observed. This deflection represents the noise generated internally within the receiver stages. The VTVM is calibrated with two scales, the lower one being an expanded version of the upper. At regular intervals along the dial, the calibrations of the upper scale are connected by diagonal lines to the corresponding calibrations on the lower. See Fig. 2. When the pointer reading for the upper scale has been noted, an output signal from the noise diodes is fed

* * Please turn to page 48 * *





CALTECH CHASSIS T1

The Caltech Chassis T1 shown in Fig. 1 demonstrates a departure from the more conventional practices of television-receiver construction. The chassis is positioned vertically, a condition which permits greater accessibility to the tubes for replacement purposes. This arrangement also permits the various controls to be mounted close to their associated circuits and still be accessible for adjustment.

One of the most outstanding features is the unitized construction employing printed circuits. The receiver is divided into subassemblies. These are mounted on a chassis base which contains the interconnecting wiring. A special plug-in arrangement is used so that the smaller units may be removed or installed very easily. One of the subassemblies is shown in Fig. 2. This particular one contains the horizontal-oscillator section. A top view showing the mounting of the components constitutes Fig. 2A. The printed-circuit wiring is clearly visible in the bottom view of Fig. 2B. The leads for most of the components are accessible from



10



Tuner

The tuner is a 12-position turret type. RF amplification is obtained by the use of a 6BQ7A tube connected in a cascode circuit. The mixeroscillator stage employs the two triode sections of a 6J6. The output of the tuner is fed to the 40-megacvcle IF strip.

Video IF

The video IF strip contains four stages of amplification. Each of these four stages employs a 6CB6. Interstage coupling is accomplished by inductive means. The secondaries of the IF transformers are shunted by resistances to obtain the desired bandpass. An interesting feature of the IF strip is the liberal use of traps. A total of five absorption traps are used.

A 1N60 crystal diode serves as the video detector. The resultant composite signal is then fed to the first video amplifier, a 6AU6. A parallel-resonant circuit tuned to 4.5 megacycles is contained in the cathode circuit of this stage, and the sound take-off point is located at the cathode. The amplified video signal is applied to the grid of the videooutput tube which is a 6AR5 or a 6AQ5. Cathode bias on this stage is adjustable by means of the contrast control. The output signal drives the control grid of the picture tube. One diode section of a 6AL5 is included in the picture-tube grid circuit to act as a DC restorer.

Sound

In the sound system, two stages of amplification precede the ratio detector. These two stages employ 6AU6 tubes and are transformer coupled. The signal from the un-

* * Please turn to page 68 * *



(A) Top View.



(B) Bottom View.

Fig. 2. Horizontal-Oscillator Subchassis in Caltech Chassis T1.

the top of the chassis in order to facilitate voltage and resistance checks.

The receiver is supplied with a remote-control head which permits changing channels and controlling the volume from a remote position.



Fig. 1. Caltech Chassis T].

January, 1955 - PF REPORTER



Ξ

Just 25 years ago this month, General Cement was little more than a hopeful gleam in its two founders' eyes. Yet such was their determination to bring quality, imagination and utility to the then infant radio service industry that today G-C is one of the best known names in radio—

Radio-

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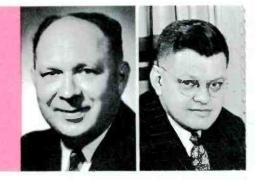
television—electronics. For this great acceptance, we of G-C are truly grateful and promise to maintain our reputation for manufacturing economically priced, top quality service aids . . . chemicals . . . tools . . . hardware . . . whether it's one item or several thousand!

Ε

DS

1930 Production Facilities 850 sq. ft.





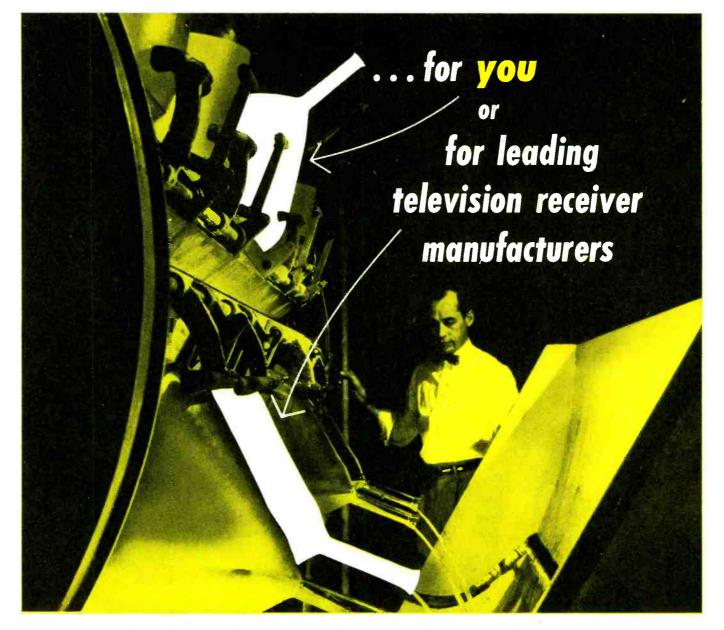
FOUNDERS...S. B. Valiulis, President, and R. G. Ellis, Secretary, Treasurer and General Sales Manager, founded G-C (General Cement Mfg. Co.) on January 6, 1930.





General Cement Mfg. Co.

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Du Mont name.

for new set performance.



Inquiries which we have received make it evident that there exists a need for a good shop-ticket design. Realizing that one ticket could not possibly fill the needs of all shops, we have tried to come up with two designs which should do the job for the majority. At any rate, we hope that the designs presented will aid the reader in making his own design if neither of these suit his specific needs or likes.

While it is true that several types of ready-made shop tickets are available many of these tickets do have deficiencies such as: not enough room to list all of the parts replaced and insufficient space for long serial numbers or for writing in longhand. They may, however, be considered satisfactory by some service shops, especially by those who have become accustomed to using them.

The views and suggestions that are set forth in this article are the results of a survey made of many TV and radio service shops, both large and small. As expected, the answers to the questions were many and varied. After all, there probably are no two repair shops anywhere that operate entirely in the same way; and the likes and dislikes of owners vary greatly. As a result of this survey, the shop tickets presented include items representative of the preferences most frequently expressed by shop owners.

The following is a list of items which might be placed on a shop ticket. Most of the readers will probably not want all of these; consequently, this list may be used more or less as a check list and perhaps may remind the reader of a few things that he had not thought about.

Space for Customer's Name and Street Address.

The identification of the owner of a set is certainly imperative, if no service-call slip is used other than

BY HENRY A. CARTER

the shop ticket itself. If a servicecall slip is also filled out, then at least the number of that call slip should be entered on the shop ticket.

Space for Customer's City and State Address.

The city and state information is not necessary unless the shop is part of a national organization or unless it does service work in several neighboring towns.

Space for Customer's Phone Number.

The phone number is added so that the customer may be called for a delivery appointment.

Spaces for Make, Model, and Serial Number.

Identification of the unit requiring service is of the utmost importance. The make of the unit and its model and serial numbers should be recorded on the shop ticket regardless of the type of ticket used. The model number is most often located on the cabinet and seldom on the chassis; therefore, the man making the pickup should record the model number on the ticket before he leaves the customer's home with the chassis. The model number will be a help to the shop technician when he starts looking for service literature.

Space for Pickup Date.

Knowing the date of pickup provides two advantages. First and foremost, it helps the service technician in the shop to decide which set gets first attention. Secondly, it is common knowledge that a customer loses his sense of time when he has to be without his television receiver; and he is apt to exaggerate when he calls to complain about the long wait. A record of the pickup date is helpful in such situations.

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Space for Delivery Date.

The delivery date is important when determing the expiration of a service guarantee in the case of a future call back.

Space for Complaint or Symptoms.

It is very essential to have all the data on the complaint or symptoms. This should include every detail that the service technician notices while attempting repairs in the home. The more he notes on the shop ticket, the quicker the shop man may be able to locate and correct the trouble.

Space for Promised Completion Date.

Entry of the date promised for completion of the work is entirely subject to the preference of the shop owner; but from our survey, we obtained the impression that it is not a good idea to promise a specific completion date except on very rare occasions when the technician knows without a doubt the cause of the trouble and is positive that the set can be returned by the promised time. Such an occasion might be when the chassis has to be taken in for the installation of a new picture tube and the technician knows that there is a replacement in stock at the shop.

Detachable Claim Check.

Some shops use customer claim checks, others do not. Both have valid reasons for their positions in this matter. The chief argument against the use of claim checks is that customers are prone to misplace them and are unable to present them when their sets are delivered. This situation is not a good one, because lost claim checks sometimes turn up later in the hands of unscrupulous individuals who try to make fraudulent claims against the service organization. The principal argument in favor of claim checks is that the customer is entitled to some kind of a receipt when his expensive set is taken out of his home. A receipt or claim check gives him more confidence in the service company.

Space on Claim Check for Receiver Serial Number.

Once in a while when a set is returned after repairs, a suspicious customer gets the idea that the set returned is not his. To guard against such misunderstandings, it is a good idea to jot down the serial number of the customer's set on his claim check (as well as on the shop ticket) before taking the set into the shop. Then

* * Please turn to page 82 * *

TV SUPPLEMENTARY SHEET F SYLVANIA ATALOG . TI CRIPTION LIST UP TO DATE DATA. ED UP TO DATE DATA. DATE CEDUIQ SUPPLEMENTARY SHEE DESCRIPTION 2 Meg. Q corbon \$1.25 120K Q corbon \$1.85 80 Q C.T. 2 1 2: 25 25 .25 HEET C LIST DESCRIPTION \$1.85 5000 Q 4W-W.W \$1.25 200 V. Q carbo \$1.23 5 Meg. Q carb \$1.2 Western MODEL & 2011858 For more profitable television servicing you need up-to-date 2011858 201185 2011850 2011856 replacement information.

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MOTOROLA

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the GARAGE - DOOR OPENER

by Don R. Howe

TECHNIQUES IN SERVICING AN ELECTRONIC DEVICE OF GROWING POPULARITY

An increase in the variety of items the service technician is called upon to repair requires that he become familiar with these items if he is to take full advantage of the additional business offered by their installation and repair. An example of such an item is the radio-controlled garage-door opener which is becoming very popular.

The Perma-Power Model RC101 is an example of one of the commercial garage-door openers now being marketed. The transmitter, receiver, and antenna associated with this model are shown in Fig. 1. The sizes of these units can be judged by their comparison with a ruler in the photograph. The following discussion of the Model RC101 covers only the units shown in the figure; it does not cover the mechanism which is used in conjunction with these units for raising and lowering the door.

Transmitter Unit

The transmitter shown in Fig. 1 is a tone-modulated, fixed-frequency unit operating at 27.255 megacycles. A crystal is used as the element which determines this frequency. Tone modulation of the RF carrier is provided. This modulation may be at any one of the ten available channel frequencies which are spaced logarithmically between 600 and 4700 cycles per second. The frequency-determining elements for the tone oscillator are contained in a plug-in unit which is easily inserted or removed from the trànsmitter. A similar unit is used in the receiver and will be described later in this article. The two plug-in units are shown in Fig. 2. The location of the plug-in unit which is installed in the transmitter and the placement of the major components may be seen in the top view (Fig. 3A) and in the bottom view (Fig. 3B).

A reference to the schematic diagram in Fig. 4 will show the circuitry employed in the transmitter. One tube, a 6U8 triode-pentode, is used. The triode section serves as the modulator, and the pentode section functions as the RF oscillator. The output of the modulator V1A modulates the screen of the RF oscillator V1B. A neon bulb is connected in the plate circuit of V1B and may be used to tune the plate tank circuit.

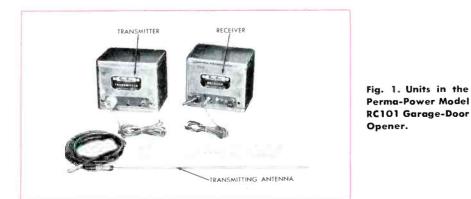




Fig. 2. Plug-in Tone Units for the Transmitter and Receiver.

The neon lamp also serves a secondary purpose. For maximum stability and ease of starting, the plate tank circuit should be resonant at a frequency slightly higher than the natural frequency of the oscillator. When the oscillator is quiescent, the neon lamp is not fired and the plate tank circuit is tuned to a higher frequency than the natural frequency of the oscillator. When the oscillator is operating, the neon lamp glows and the stray capacitance contributed by the neon lamp becomes greater. This additional capacitance then causes the tank circuit to resonate at a lower frequency, and the result is a more efficient circuit.

The B+ voltage for the transmitter is obtained from a vibrator type of power supply with selenium rectifiers connected in a voltagedoubler circuit. The transmitter is designed for operation on six volts. Operation from a twelve-volt source is possible by using the adapter available for this purpose.

The transmitter is normally installed in the engine compartment of the car, and the antenna is mounted under the splash pan behind the front bumper. The transmitter is conveniently attached to a base plate by four snap fasteners. This arrangement permits the transmitter to be removed from the automobile without the use of tools. The red lead from the plug on the transmitter is connected to a source of six volts DC. This connection must be made to a point where voltage is present only when the ignition switch is closed. This permits the filament of the 6U8 to be on whenever the ignition is on. The green lead from the plug is connected to the push button mounted on the dash. The closing of this switch supplies power to the vibrator and causes the transmitter to operate. The only adjustment that is necessary when installing the transmitter is the slug adjustment in the inductance L1. The slug in the tank coil L1 is adjusted for maximum brilliance of the neon bulb and is then turned counterclockwise for one

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^{* *} Please turn to page 84 * *



P CLAIMS GRANTED IN #2 609 503 -- #2 661.423 TV VIEWERS **OPENS NEW HORIZONS** TO

These are the reasons why the "Riviera" is by far the most powerful VH7 antenna on the market today!

I. Utilizes 16 elements 60" long, ½" diameter.

- 2. Utilizes a specially designed, extra low loss four conductor air-dielectric POLYMICALENE transmission line which has up to 50% less loss when wet than the finest conventional transmission lines.
- 3. The "Riviera" encompasses an electro-magnetic capture volume of well over 650 cubic feet, many times more than conventional antennas.
- The antenna works on the revolutionary principle that the approaching wave front is elliptically rather than horizontally polarized.
- 5. The new specially designed 9 position electronic orientation switch, aside from changing directivity, maintains a consistently better imped-ance match over the entire UHF-VHF spectrum.
- 6. The above features combine to give the "Riviera" antenna greater usable gain at the TV set antenna terminals than the best of any competitive antennas using rotor motors.

This new wonder antenna, called the "Riviera", is already making history. Beyond any question of a doubt, and on an unconditional money back guarantee, it will positively outperform in the field under actual installation conditions, any and all competitive antennas on the VHF channels, with or without rotor motors.





to-set Coupler * 2 Stand-offs, 71/2" * Complete instructions

The polar directivity response patterns show the major lobes of the "Riviera" antenna on VHF. It shows the fullness of coverage in all directions of this remarkable, patented an-tenna as it is 'turned'through each of the nine switch positions. Each degree of shading constitutes a different switch position. This excellent directivity response, which can be switched at will, plus the extremely high gains, clearly indicate why the Riviera is such a superior performer.





by Henry A. Carter and Calvin C. Young, Jr.

IN THE HOME

EQUIPPING THE SERVICE TRUCK

A very important part of any service business is the service vehicle which may be a panel truck, station wagon, vanette, pickup truck, sedan delivery, or a standard passenger car. The type of vehicle will be determined by the types of service rendered and by the financial status of the business. In television service the panel truck, sedan delivery, and station wagon are perhaps the most satisfactory vehicles for the service organization.

For the small shop, a station wagon is very practical since it may also be used by the owner as the family car. The panel truck is, in most cases, the best vehicle for service since it has ample room on the inside to carry even the largest television receivers. In fact, several receivers may be carried at one time. Along the sides of the panel truck there are rails to which large cabinets can be secured to prevent them from toppling over or shifting about and becoming damaged. The large, level top on the panel truck provides space on which ladders, antenna masts, and other long objects may be carried if a suitable rack is

employed. Shops which sell appliances or install antennas or do both will find the panel truck meets most of their requirements for a service truck.



Fig. 2. Containers for Small Parts.

There are some service organizations which do not sell appliances or make antenna installations. These shops may find the sedan delivery to be the ideal vehicle for them. This type of vehicle is smaller and more maneuverable than the panel truck and is usually easier to manage in traffic. If the large carrying capacity of a panel truck is not required, the sedan delivery will serve very well. In all cases, the needs of a particular

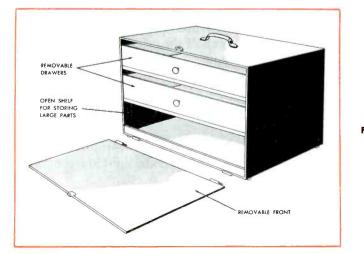


Fig. 1. Parts Caddy.

business should be carefully considered and the best vehicle for the intended use should be chosen.

The equipment and replacement parts carried in the service vehicle are also very important. Their choice will depend upon whether the service company does all phases of servicing such as television, radio, antennas, rotators, and all other allied electronic devices, or whether the service company specializes in television and radio service only.

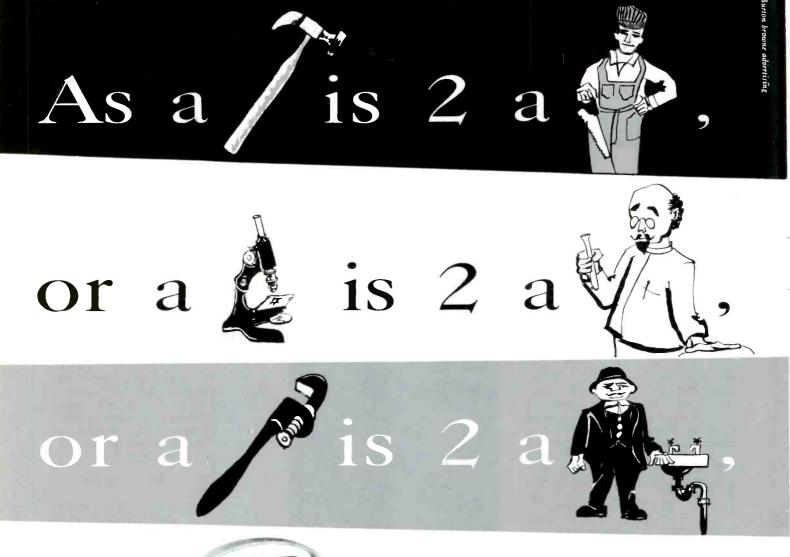
For TV and Radio Service

Service organizations which specialize in television and radio service should equip the service vehicle with certain basic pieces of test equipment and assorted replacement parts. A technician who is provided with a well-equipped service vehicle should be able to repair in the home, on an average, something over 90 per cent of all the sets he is called upon to service. If minor repairs are completed in the home, the bench technician will have more time to devote to those really difficult repair jobs. Minor repairs consist of replacing weak selenium rectifiers, faulty filament resistors, burnt resistors, shorted capacitors, faulty video-detector crystals, faulty highvoltage wiring, and other repairs of this nature. A service organization may elect to make such repairs in the home rather than to take a set into the shop just to replace a capacitor that is known to be bad or to replace a weak selenium rectifier. The time saved by performing these jobs in the home will more than make up for the difference in service charges.

The replacement parts for home service and the basic equipment given in Table I are needed in addition to the standard service tools and tube caddy normally carried by the technician. Although some of the items listed may already be carried in the

* * Please turn to page 75 * *

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MODEL 631 VOM-VTVM \$5950 NET

Recause—it's TWO-in-One for the price of one! It's a VTVM—It's a VOM with just the flip of a switch!

This one combination instrument will be the serviceman's most frequently used piece of test equipment. No need to invest in two separate testers when one will do his work at half the price-\$59.50 net.

Flip the switch, it's a V T V M (completely portable; battery operated—VTVM accuracy not subject to line voltage fluctuations — Input Impedance of 11 megohms).

Flip the switch and it's a **V** O M (with the sensitivity to match readings in all the service manuals— 20,000 ohms per volt DC, 5,000 ohms per volt AC).

Ranges entirely adequate for servicing needs. All 34 ranges selected by one knob control-minimizes incorrect settings and burnouts. Unbreakable clear plastic meter case front floods light on long, readable scales.

Triplett Model 631 is sold by leading distributors everywhere.



the

TRIPLETT ELECTRICAL INSTRUMENT CO., Bluffton, Ohio



TAPED CORRESPONDENCE. With tape recorders booming as a means of exchanging spoken messages rather than letters with correspondents all over the world, ingenious names have sprung up for the inevitable clubs of such enthusiasts. Here are a few: Tape Respondents International, The Voicespondence Club, World Tape Pals, Global Recording Friends, and Record-O-Club. It's one swell way to keep in practice with a foreign language that might otherwise become rusty through disuse.



TALKING BOOKS. If a mistake in pronunciation is made while reading a book for disk recording, the entire record must be done over. Knowing this, the reader is under tension and hence tends to make more mistakes than normal. Changing to magnetic tape cuts costs and eases the tension, because a fluffed sentence need simply be repeated. Later scissors and splicing tape will fix things in a jiffy.



TRAFFIC CONTROL. A new frequency just recently made available by the FCC will be used by Chicago police to send coded radio signals out to traffic lights. Purpose is to achieve synchronization of the lights along with different optimum timings for the morning and evening rush hours and with normal settings the rest of the day.

As a starter, eleven heavytraffic intersections will get antennas, receivers, decoders, and traffic-light controllers. Flans call for eventual radio control of 450 intersections at a cost of about \$480,000, as compared to \$3,375,000 for a comparable cable-control system.

ELECTRIC TYPEWRITERS "When I sat down to type, all the TV sets as far as half a mile away blanked out," is a story the wife of a good friend of ours can tell, now that the neighbors have been appeased and all is quiet again. To speed up the final typing of his book on TV servicing, our friend had rented an electric typewriter (\$25 per month). They're wonderful. Just barely touch the keys and the electric motor does the rest - and still more. The brushes on that motor apparently felt that they should tell the rest of the world about their work, because they surely radiated - on all TV channels. A complaint to the rental agency brought a second machine, which was just as bad. The third, a practically brand-new job, was all right in that it didn't bother the neighbors - just messed up his own TV set.

John Markus

Unbelieving, the owner of the typewriter agency took one of the machines to his own home. Now he's looking for some other kind of business to get into.

Properly connected filter capacitors and proper maintenance on the machines will stop such radiation, but it has to be done at the factory level. Once you've determined that the typewriter is the source of interference, break the news to your customer and get out quickly. This policy, incidentally, applies to a good many other man-made-interference complaints as well.

TUBES. The next time it takes five minutes to get a tube out from a too-crowded location, give a thought to the radar service technician. It requires just about half an hour to replace a magnetron in a radar receiver-transmitter unit because of the resonant cavities associated with the tube.

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Editor-in-Chief, McGraw-Hill Radio Servicing Library

EYE CATCHER. When business trips take us to a new town, a flip through the pages of its classified telephone directory gives a quick picture of business and industry there. In Pittsburgh this fall, the ad that really caught our attention was headlined "STOP AND THINK BEFORE YOU TINKER.'' Combined with a little cut showing the man of the house getting ready to attack his ailing TV set, it effectively gets across the idea that fixing a set is a job for a trained service technician. Though it's just a one-column ad 21/2 inches deep, we're sure it's pulling business for Chuck Barofsky who runs Chuck's TV & Radio Service at East Liberty, Penna.



CHILDREN'S HOUR. In Britain where there is only one television station per city, the 5 to 6 p. m. Children's Hour is followed by a long black-out until the weather forecast comes on at 7:25. When Television Digest's editor asked a top BBC official why they went off the air right at the peak of their viewing audience, he replied; "So that the mothers may prepare dinner and put the children to bed without any distraction from TV." The children "have had it." If they know the screen is dark, they make no fuss about staying up for more.

What peace that must be - no supermen or rustlers to interfere with the enjoyment of the evening meal! With Britain as a precedent, we wonder if we could get by with hooking up a time clock that would also darken our screen during that magical hour '' Between the dusk and the daylight, when the night is beginning to lower.'' Just wishfulthinking - this is America where the kids run the family and the good wife is on their side in any showdown over TV.

* * Please turn to page 54 * *

BRAND FEATURES

THAT MAKE TRIO THE LEADER IN '55



Thick-wall, exfra-sturdy 11/4" diameter Booms. Nothing approaching them for strength! Now used on **ALL** low-band yagis.



This revolutionary clamp permits instant Hip-out assembly, permanent alignment with ultra strength. Nothing stronger — nothing faster! Insta-Lok employed on **ALL** TRIO Antennas that have parasitic elements.



New "VARI-CON" HEAD

Four Hi-strength aluminum adjusting arms. Interlocking Butterfly sections. Heavier snap-action spring assembly. The "Vari-Con" is the only antenna with spring dampeners to lessen vibration and breakage. The "Vari-Con" head also used on the popular TRIO 88 Series.



New MINIT-UP CONICAL HEAD

Swing out element mounting plates, fan out elements into snap-fastenings and it's set! Used throughout conical line_a

New MYCASTYRENE INSULATORS USED THROUGHOUT TRIO LINE



Color TV Training Series

(Continued from page 9)

transformer at the take-off point of the chrominance signal. The reference signal from the color-sync section is applied to the plate of section A and to the cathode of section B. The output of the R - Y demodulator is present at the junction of resistors R1 and R2.

The B - Y demodulator is connected in a manner similar to that of the R - Y demodulator. The chrominance signal is applied to the cathode of section A and to the plate of section B of the B - Y demodulator. The signals present at these points are displaced by 180 degrees. The B - Y reference signal is applied to the plate of section A and to the cathode of section B. The output of the B - Y demodulator appears at the junction of resistors R3 and R4.

The magnitude of the output signal from each demodulator is dependent upon the amount of conduction by each section of the demodulator. Whenever the conduction of each section is equal, the output will be zero. For example, when both sections of the R - Y demodulator are conducting equally, a positive voltage will appear at the junction of R1 and the cathode of section A because of the positive charge on C1. A voltage of the same magnitude but of opposite polarity will appear at the junction of R2 and the plate of section B because of the negative charge on C2. Since the charges on C1 and C2 are equal but of opposite polarity and since both C1 and C2 are returned to ground through the chrominance output transformer, a zero voltage is present at the junction of the equal-value resistors R1 and R2. This condition would exist when there is no chrominance signal at the input. Under the same conditions, the B - Y demodulator would perform in the same manner.

Let us now investigate the action of the diode demodulators during the time that a chrominance signal is being received. For example, let us assume that a chrominance signal which is lagging the R - Y reference signal is present at the cathode of section A of the R - Y demodulator. The action of both demodulators is shown by the waveforms in Fig. 7-31. The first pair of waveforms shows the action of section A of the R - Y demodulator. The sine wave marked P is the reference signal at the plate, and the one marked K is the chrominance signal at the cathode. The conduction time is during the period that the plate is more positive than the cathode and is represented by the shaded portion between the sine waves.

The second pair of sine waves in Fig. 7-31 shows the action of section B of the R - Y demodulator. The reference signal appears at the cathode of this section and is represented by the sine wave marked K. It is the same signal that was present at the plate of section A. The other signal of the second pair of sine waves is the chrominance signal and is marked with a P, since it appears at the plate of section B. This chrominance signal is 180 degrees out of phase with that previously discussed, since it is taken off at the transformer secondary. The conduction time of section B is the shaded portion between the two sine waves.

It can be seen that section B conducts more than section A. This will cause the charge on C2 to be greater than that on C1; and because the charge on C2 is negative, a negative voltage is present at the junction of R1 and R2.

The third pair of sine waves in Fig. 7-31 shows the action of section A of the B - Y demodulator. The chro-

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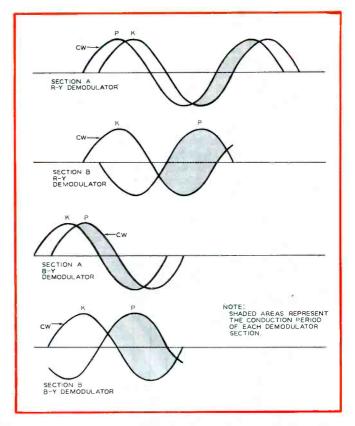


Fig. 7-31. Illustration of Conduction Period of Each Demodulator When the Chrominance Signal Lags the R-Y Reference and Leads the B-Y Reference by 45 Degrees.

minance signal is sine wave K, and it appears at the cathode of section A. This chrominance signal is at the same phase as that at the plate of section B in the R - Y demodulator. The other sine wave of the third pair is the B - Y reference that appears at the plate of section A. This reference signal is advanced 90 degrees in relation with the R - Y reference signal. The conduction time of section A of the B - Y demodulator is during the shaded portion of the third pair of sine waves in Fig. 7-31.

The fourth pair of sine waves in Fig. 7-31 represents the action of section B of the B - Y demodulator. In this section, the chrominance signal is applied to the plate and the reference signal to the cathode. Sine wave P is the chrominance signal and is at the same phase as the signal that appears at the cathode of section A in the R - Y demodulator. Sine wave K is the reference signal. The conduction time of section B of the B - Y demodulator is represented by the shaded portion between the two sine waves.

Section B of the B - Y demodulator conducts a greater amount than section A; as a result, there is a greater charge on C4 than on C3. Therefore, the instantaneous output voltage of the B - Y demodulator will be negative in polarity.

For the case just assumed, the chrominance signal lagged the R - Y reference signal by 45 degrees and it led the B - Y reference signal by 45 degrees. The instantaneous output voltage of each demodulator was found to be of negative polarity.

Let us assume that the chrominance signal leads the R - Y reference signal by 45 degrees and leads the B - Y reference signal by 135 degrees. The conduction period of each section of the R - Y demodulator and the B - Y demodulator is illustrated in Fig. 7-32. By inspection of the first two pairs of sine waves, it can be seen

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More Efficient: DUAL RANGE THEATER TYPE SYS-TEM permits uncompromising design of the "woofer" and "tweeter" sections for greatest efficiency. Hear it penetrate noise with remark-able fidelity and intelligibility.

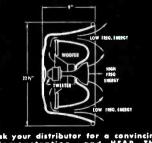
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Response 7	0-15,000 eps
Power	
Coposity	25 watts
Impedance	8 ohms
Dispersion	120 degrees
Mounting	
180° adju	stable "U" bkt.
Dimensions	
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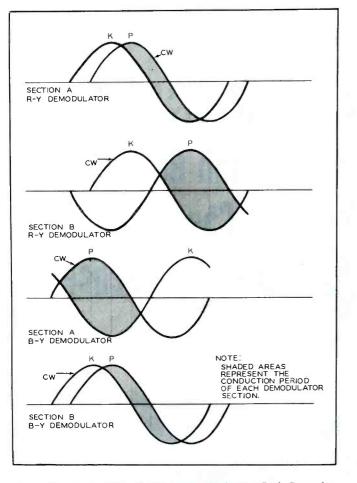


Fig. 7-32. Illustration of Conduction Period of Each Demodulator When the Chrominance Signal Leads the R—Y Reference by 45 Degrees and Leads the B—Y Reference by 135 Degrees.

that section B of the R - Y demodulator conducts more than section A. This will produce an instantaneous voltage of negative polarity at the output of the R - Y demodulator.

The B - Y demodulator will produce an instantaneous output voltage of positive polarity, as can be seen from inspection of the last two pairs of sine waves in Fig. 7-32. Section A of the B - Y demodulator conducts more than section B; thus, the charge on C3 will be greater than that on C4, and the resultant output voltage will be positive.

Let us investigate what happens when the chrominance signal is in phase with the R - Y reference signal. Under this condition, there must be maximum output from the R - Y demodulator and zero output from the B - Y demodulator. The illustrations in Fig. 7-33 show that this is true. There will be no output from section A of the R - Y demodulator, since the chrominance signal is in phase with the reference signal. In section B of the B - Y demodulator, conduction is at maximum because the chrominance signal has been changed in phase by 180 degrees. Maximum output will appear at the junction of R1 and R2, under this condition.

The third and fourth pairs of sine waves in Fig. 7-33 show that the conduction of section A of the B \sim Y demodulator is equal to the conduction of section B. The charges on C3 and C4 are equal, and the output of the B \sim Y demodulator will be zero the same as if there were no chrominance signal present.

The vector relationship of the conditions previously discussed is represented in the vector diagram of Fig. 7-34.

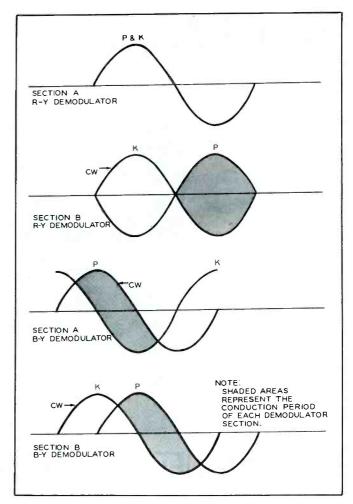


Fig. 7-33. Illustration of Conduction Period of Each Demodulator When the Chrominance Signal Is in Phase With the R-Y Reference.

The first condition in which the chrominance signal lagged the R - Y reference signal and led the B - Y reference signal by 45 degrees is represented by the vector marked chroma 1. A chrominance vector at this position on the phase diagram would represent a color near magenta. This chrominance signal contains a positive R - Y signal and a positive B - Y signal. These are the polarities of the R - Y and B - Y signals when chroma 1 is transmitted.

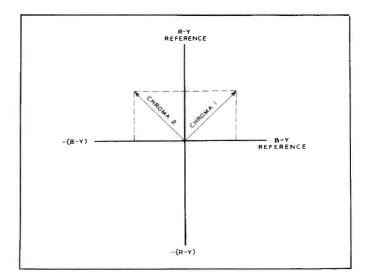


Fig. 7-34. Vector Relationship of the Chrominance Signals With the Reference Signals.

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ACITORS

Sangamo's line of TV Replacement Electrolytics has been and still is the most complete in the industry. It is constantly expanded to include all the new sizes used in the latest model television receivers of all major set manufacturers.

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Sangamo Type PL Electrolytics are used as original equipment by all major manufacturers—they are *exact* replacements—they assure long life and dependable performance at 85° C and under conditions of high surge voltages and extreme ripple currents.

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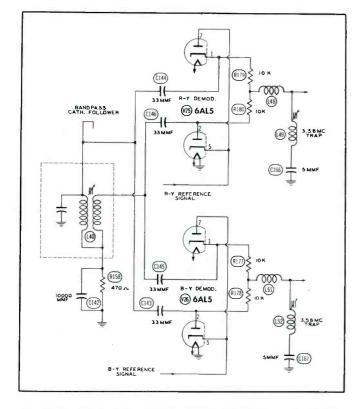


Fig. 7-35. Diode Demodulator Circuit in the Motorola Model 19CT1 Color Receiver.

The vector marked chroma 2 represents the second condition in which the chrominance signal led the R - Y reference signal by 45 degrees and led the B - Y reference signal by 135 degrees. This vector represents a yelloworange color and contains a positive R - Y signal and a negative B - Y signal. These are the polarities of the R r Y signals and B - Y signals when chroma 2 is transmitted.

The R - Y and B - Y demodulators can be made to produce an output signal of a positive or a negative polarity, depending upon which is desired. Whenever an output signal of a positive polarity is wanted, the demodulator is made to demodulate on the negative reference axis. When one of a negative polarity is desired, the demodulator is made to demodulate on the positive reference axis. Such was the case for the demodulation process previously discussed — modulation was performed on the positive reference axis.

The circuits of diode demodulators that are used commercially are shown in Fig. 7-35. This circuit is employed in the Motorola Model 19CT1 color receiver. Two 6AL5 tubes are used in the demodulator stages. V25 is the R - Y demodulator, and V26 is the B - Y demodulator. The operation of these demodulators is the same as that discussed for the basic circuit in Fig. 7-30. These are R - Y and B - Y demodulators which are of negative polarity; that is, they demodulate along the positive reference axes and produce output signals that are reversed in polarity from the polarities used for modulating the chrominance signal at the transmitter. By passing these signals of negative polarity through an amplifier stage, they are inverted and then become signals of positive polarity.

This concludes the discussion of the demodulation process and the demodulator circuits in color receivers. In this discussion, we have been concerned with the chrominance signal as a modulated signal. We have taken this signal, demodulated it, and changed it into color-difference signals. From this point on, in the discussion of the color-receiver circuits, we will be concerned with these color-difference signals.

THE MATRIX SECTION

At this point in the discussion of color-receiver circuits, three video signals have been described. These are the luminance signal and the two color-difference signals at the output of the chrominance demodulators. It is the function of the matrix section to combine these three signals in the correct proportions so that three color signals are produced. These color signals are then amplified and applied to the picture tube where they represent the hues of an image in terms of red, green, and blue. The block diagram shown in Fig. 8-1 illustrates the

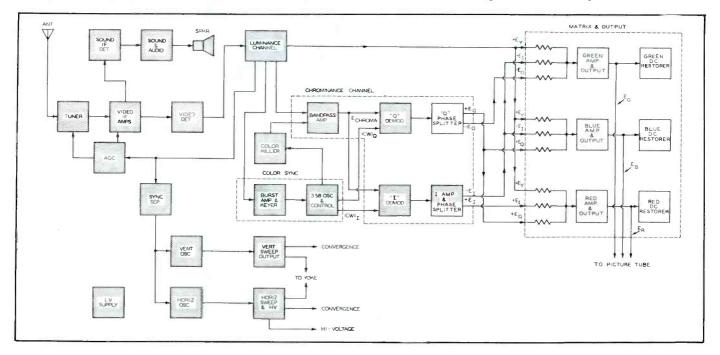
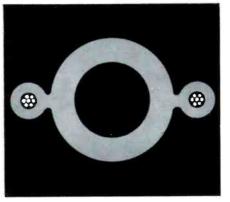


Fig. 8-1. Partial Block Diagram of a Color Receiver Showing Sections Previously Discussed and Those to Be Covered

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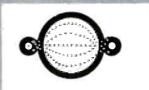
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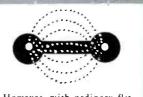
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stages which perform this function. The shaded blocks represent the sections previously discussed in the Color TV Training Series.

In order to understand how the colors are reproduced, it is necessary to know something about the picture tube. The tube used in the basic color receiver is known as the tricolor kinescope. Three separate electron guns are incorporated in this type of tube in order to accommodate the three color signals. The coating on the face of the tube consists of phosphor dots which are arranged in triangular groups of three. One dot in each trio emits red, one emits green, and one emits blue light.

When operating properly, the electron beam from the red gun activates only the red dots, the beam from the blue gun activates only the blue dots, and the beam from the greengun activates only the green dots. The phosphor dots are closely spaced so that when more than one dot in each trio is activated, the total light emission will blend to form one color. For example, when the light emissions from all three phosphors are equal, the screen appears white. If the red and green phosphors emit equal light, the resultant hue appears to be yellow. The blending into a single hue of the color dots on the picture-tube screen is based upon the principle that the human eye cannot resolve the separate colors at normal viewing distance. As a result, the total light emitted from the dot combination appears as a single color.

The foregoing information should be helpful in understanding the requirements of the matrix section. A detailed discussion of the picture tube will be presented later in the Color TV Training Series.

In order to produce the colors of an image correctly, the matrix section must fulfill certain conditions. For instance, when a fully saturated red portion of the image is to be reproduced, the instantaneous amplitude of the video signal that is applied to the red gun must be at its maximum value and the amplitude of the signals applied to the green and blue guns must be zero. During the time when a fully saturated green is to be reproduced, the amplitude of the signals applied to the red and blue guns must be zero and that applied to the green gun must be at its maximum value. The blue signal must be at maximum and the red and green signals at zero when a fully saturated blue is being reproduced. If white is to be reproduced, the amplitude of all three of the color signals must be at maximum, because white contains all colors.

During the transmission of a composite color signal, the content of the Y, I, and Q signal voltages at the transmitter is known to be:

$$EY = .30E_R + .59E_G + .11E_B,$$
 (4)*

$$E_{I} = .74(E_{R} - E_{Y}) - .27(E_{R} - E_{Y}),$$
 (8)*

$$E_Q = .48(E_B - E_V) + .41(E_B - E_V).$$
 (9)*

From these equations, it can be determined that:

$$E_{R} = .96E_{I} + .63E_{Q} + 1.00E_{Y},$$
 (13)

$$E_{\rm B} = -1.11E_{\rm I} + 1.72E_{\rm Q} + 1.00E_{\rm Y}, \qquad (14)$$

$$E_G = -.28E_I - .64E_Q + 1.00E_Y$$
, (15)

where

 $E_{\mathbf{R}},\ E_{\mathbf{B}},\ \text{and}\ E_{\mathbf{G}}$ represent the desired red, blue, and green signal voltages which are to be applied to the

picture-tube guns. The mathematical proof for these equations is presented in the footnote. $^{1} \ \ \,$

It can be seen that the voltage combinations needed to produce the color signals consist of plus and minus values of E_I and E_Q . The plus and minus signs designate the polarities of the signal voltages. For instance, the minus sign in the expression -.28E_I indicates an I signal which has a negative polarity. When no sign is used, the polarity is considered to be positive.

Let us suppose that the color-bar pattern shown at the top of Fig. 8-2 is used as the transmitted image. If all of the colors are fully saturated, the relative amplitude of the I, Q, and Y signals used in the make-up of the composite signal at the transmitter will be as shown below the bar pattern. The amplitude of the luminance signal during the reproduction of a white of full brightness is considered as the standard for unity; therefore, E_Y is shown to have an amplitude of 1.00 during the transmission of the white bar.

The amplitudes of the luminance signal and the color-difference signals during the transmission of the color-bar pattern shown are based on this unity figure. For example, when the image is a fully saturated red, the the amplitude of E_I is .60; the amplitude of E_Q is .21; and the amplitude of E_Y is .30. If the color of the image is changed to green, the amplitude of E_I becomes a negative .28; the amplitude of E_Q becomes a negative .52; and the amplitude of E_Y becomes .59. If the polarity of the E_I or E_Q signal is inverted (as through an amplifier stage), the positive levels become negative and the negative levels become positive. The negative polarities of E_I and E_Q are also shown in Fig. 8-2 to provide a convenient reference for the reader.

¹The content of the I and Q signals is known to be:

$$E_{I} = .74(E_{R} - E_{Y}) - .27(E_{B} - E_{Y}),$$
 (8)*

$$E_Q = .48(E_R - E_Y) + .41(E_B - E_Y).$$
 (9)*

If both sides of equation 8 are multiplied by .41 and if both sides of equation 9 are multiplied by .27, then:

$$.41E_{I} = .30(E_{R} - E_{Y}) - .11(E_{B} - E_{Y}),$$

 $.27E_Q = .13(E_R - E_Y) + .11(E_B - E_Y).$

Adding the foregoing equations, we arrive at:

$$.43(E_R - E_Y) = .41E_I + .27E_Q$$

de by .43, and solve for
$$E_{\mathrm{R}}$$
:

Divid

$$E_{\rm R} - E_{\rm V} = .96E_{\rm I} + .63E_{\rm Q}$$

$$E_{\mathbf{R}} = .96E_{\mathbf{I}} + .63E_{\mathbf{Q}} + 1.00E_{\mathbf{Y}}.$$
 (13)

By substituting this value of $E_{\rm R}$ in equation 8, we find:

$$E_{I} = .74(.96E_{I} + .63E_{Q}) - .27(E_{B} - E_{Y}).$$

From the foregoing equation, EB may be found:

$$E_{\rm B} = -1.11E_{\rm I} + 1.72E_{\rm Q} + 1.00E_{\rm Y}.$$
 (14)

It was shown in Part III of the Color TV Training Series that:

 $E_{G} - E_{Y} = -.51(E_{R} - E_{Y}) - .19(E_{B} - E_{Y}).$

Substituting values of $E_{\mathbf{R}}$ and $E_{\mathbf{B}}$ from equations 13 and 14, we find:

$$E_{C} - E_{V} = -.51(.96E_{I} + .63E_{O}) - .19(-I.11E_{I} + 1.72E_{O}).$$

Solve the foregoing equation for E_G :

$$E_{G} - E_{Y} = -.49E_{I} - .32 E_{Q} + .21E_{I} - .32E_{Q},$$
$$E_{C} = -.28E_{I} - .64E_{Q} + 1.00E_{Y}.$$
(15)

^{*}Equations 4, 8, and 9 were presented in Fart III of the Color TV Training Series which appeared in the August 1954 issue of the PF REPORTER.

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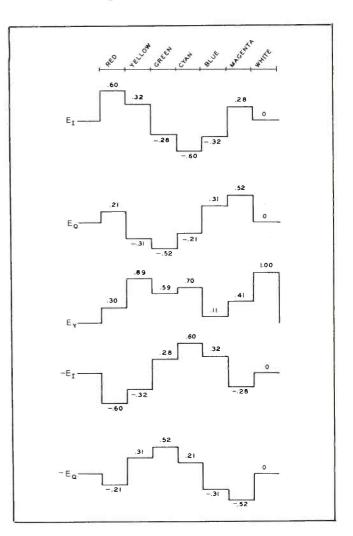


Fig. 8-2. Video Signals Developed in a Color Receiver During a Color-Bar Transmission.

During the scanning time of the red bar, the amplitudes of the I, Q, and Y voltages that are combined in the red matrix section have a ratio of .57 to .13 to .30, respectively. Since the addition of these amplitudes totals unity, the amplitude of the red signal is at maximum when red is being reproduced. If the same procedure is followed for all seven bars, it will be seen that the red signal will also be at maximum during the reproduction of yellow, magenta, and white. The instantaneous amplitudes during the scanning time of green, cyan, or blue will add up to zero; therefore, the red signal does not contribute to the reproduction of these colors.

The voltages determined by equation 14 are graphically shown in Fig. 8-4. These values are combined in the blue matrix section to produce the blue-signal voltage. The addition of instantaneous amplitudes shows E_B to be at maximum for cyan, blue, magenta, and white; and E_B is at zero for red, yellow, and green. This is the desired result, since ${\rm E}_{\rm B}$ contributes to the colors which contain blue and does not contribute to the colors which are void of blue.

The values of the three signal voltages applied to the green matrix section were obtained from equation 15 and are shown in Fig. 8-5. The green signal represented by E_G is obtained by adding the instantaneous values of these three signals. The resultant signal is shown to have a maximum amplitude for yellow, green, cyan, and white. This indicates that the green signal contributes to the reproduction of each of these colors. E_G is at zero amplitude during the scanning time of red, blue, and magenta; therefore, the green-signal voltage does not contribute to these colors.

A comparison of the three color-signal voltages shows how the individual color bars are produced on the viewing screen. During the scanning time of the red bar, the red signal is at maximum and the blue and green are

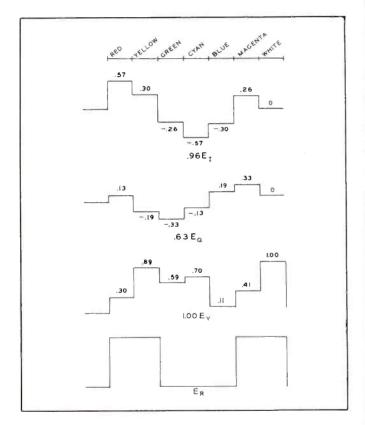


Fig. 8-3. Specific Amplitudes of E_1 , E_0 , and E_Y Needed to Produce the Desired Red-Signal Voltage.

at zero. Only the red phosphor is illuminated, and a saturated red is produced on the screen. When the yellow bar is being scanned, both the red and green signals are at maximum and the amplitude of the blue signal is at zero. The red and green phosphors are both activated; however, the eye cannot see these colors separately. Instead, the total light emitted appears to be yellow. Cyan is produced when the light emissions from the blue and green phosphors are equal. When the light outputs from the red and blue phosphors are equal, the eye will see a fully saturated magenta.

The only time when all three color signals are at maximum is during the reproduction of white. This is to be expected, since white contains all colors. It is interesting to note that during the scanning time of the white bar, the amplitudes of E_I and E_Q at the input of the matrix sections are at zero. The amplitude of the E_Y signal is

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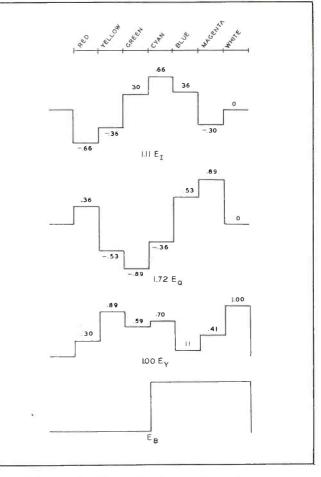


Fig. 8-4. Specific Amplitudes of E_1 , E_2 , and E_Y Needed to Produce the Desired Blue-Signal Voltage.

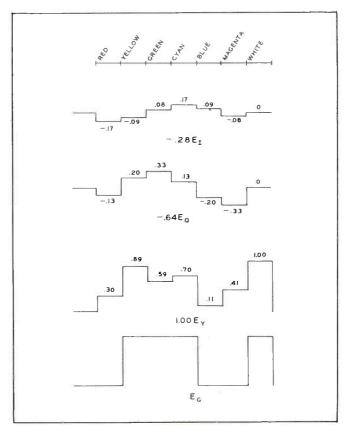


Fig. 8-5. Specific Amplitudes of $E_1,\,E_0,\,and\,E_Y$ Needed to Produce the Desired Green-Signal Voltage.

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at maximum in each case, which indicates that white is represented by the luminance signal only.

Theory in Practical Application

Now that the purpose of the matrix is known, let us examine some actual circuits. The schematic drawing shown in Fig. 8-6 shows the matrix circuit used in the RCA Victor Model CT-100. The triode sections of two 6AN8 tubes are used as phase splitters. A negative polarity of E_Q from the output of the Q demodulator is applied to the grid of V10B. As a result, a positive polarity of E_{Q} is available at the plate of this stage; whereas, a negative polarity of E_Q is obtained from the cathode. Since the polarity of the I signal from the I demodulator has been reversed through the I amplifier stage, the signal at the grid of V32B has a positive polarity. The polarity of E_I at the plate of this stage is negative, and the polarity at the cathode is positive. During a typical colorbar transmission, these signal voltages are like those shown by the waveforms in Fig. 8-7.

Refer to Fig. 8-6, and note that the positive E_{Ω} signal is fed to the red and blue matrix circuits and that the negative ${\bf E}_Q$ signal is applied to the green matrix. The negative ${\bf E}_I$ signal is fed to the green and blue matrix networks, and the positive E_I signal is applied to the red matrix. A positive E_Y signal from the output of the luminance channel is applied equally to all three matrix networks. Note that the signals applied to each matrix network have the proper polarity to produce the three color signals. Now, let us see how the specific amplitudes of E_I , E_Q , and EY are obtained.

The E_Y signal is applied to each of the matrix circuits through R239, R250, and R261. All three of these resistors are equal in value; therefore, if the grid resistance to ground at each amplifier stage is assumed to be the same, the amount of Y voltage to each of these stages will be the same. The amplitude of the chrominance signal at the output of the bandpass amplifier will have a fixed relationship with the luminance signal. This is because the contrast adjustment which controls the gain of the bandpass amplifier is ganged with the contrast adjustment which controls the gain of the luminancechannel output.

The amount of chrominance signal which is applied to the synchronous detectors can be varied through the use of the color-saturation control. Since this control will vary the amplitude of the E_I and E_Q signal outputs, it can be adjusted so that the amplitude of the negative E_Q signal at the input of the green amplifier has the desired relationship to the $E_{\mathbf{Y}}$ signal at this point (see Fig. 8-5) . The amplitude of the positive E_Q signal is determined by the gain of V10B and by the value of the load resistor R223. The value of R223 was selected so that the amplitude of the positive $\boldsymbol{E}_{\boldsymbol{Q}}$ signal at the input of the blue amplifier has the desired relationship to the E_{Y} signal (see Fig. 8-4).

The gain control in the cathode circuit of the I amplifier (not shown) can then be adjusted for the desired amplitude of the positive ${\bf E}_{I}$ signal at the input of the red amplifier. The amplitude of the negative E_I signal at the plate of the I phase-splitter stage will then depend on the gain of V32B and the value of the plate-load resistor R237. The value of R237 is such that the amplitude of the negative E_I signal has the desired amplitude at the input of the blue amplifier.

A certain amount of the negative ${\bf E}_{I}$ signal is also required at the input of the green amplifier; however, the amplitude of the signal at the plate of the I phase splitter

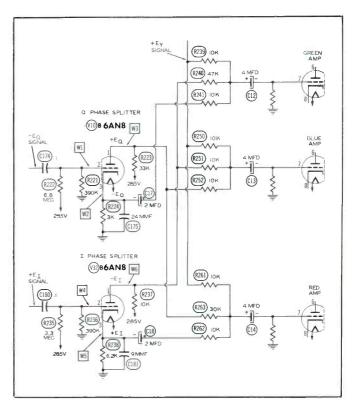


Fig. 8-6. Matrix Circuit Used in the RCA Victor Model CT-100 **Color Receiver.**

is more than four times the desired amount. The 47Kohm resistor R240 and the resistance from the grid of the green amplifier to ground form a voltage-divider network. The same is true for the 10K-ohm resistor R251 and the resistance from the grid of the blue amplifier to ground. It was originally assumed that the resistance from grid to ground was equal at each amplifier stage; consequently, the amount of negative E_I signal developed across the grid resistance of the green amplifier will be much less than that developed at the input of the blue amplifier. The value of R240 was chosen so that the voltage division would produce the correct amount of negative E_I at the input of the green amplifier.

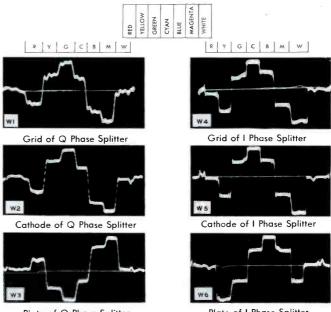


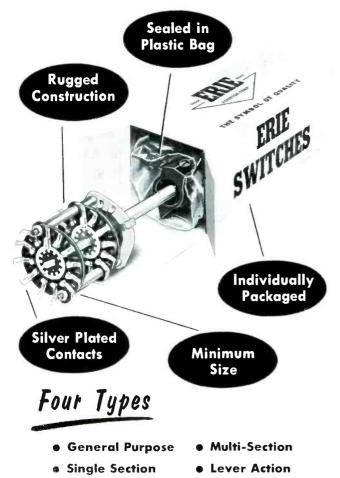
Plate of Q Phase Splitter

Plate of I Phase Splitter

Fig. 8-7. Signal Voltages Present at the I and Q Phase-Splitter Stages During the Transmission of the Color-Bar Pattern Shown.

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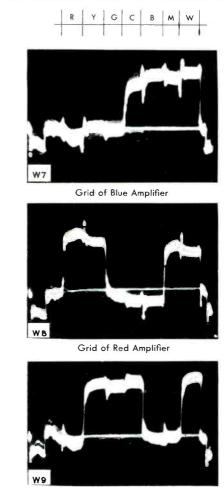
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In actual practice, proper matrixing in this receiver can be accomplished by adjusting the hue, contrast, color saturation, and I gain controls. The grid resistance at each of the amplifier stages is a common load for the



Grid of Green Amplifier

Fig. 8-8. Color-Signal Voltages at the Input of the Matrix Amplifiers When the Circuits Are Correctly Balanced.

three signals applied to each matrix circuit. For this reason, a change in one signal amplitude will affect the amplitude of the other two signals across the same load circuit. As a result, the foregoing adjustments must be repeated several times before the matrix circuits are balanced.

Following this procedure, a color-bar signal is fed into the receiver; and the controls are adjusted while observing the results on an oscilloscope. When the blue signal is balanced, as shown by waveform W7 in Fig. 8-8, the red and blue signals should then appear as shown in waveforms W8 and W9. These two signals will automatically balance when the blue signal is correctly adjusted, since a prearranged relationship exists between the three matrix circuits. It can be seen that these three wave forms conform to the requirements for proper color reproduction.

Cathode-Follower Matrix Circuit

The circuit drawing in Fig. 8-9 shows the matrix circuits used in the Arvin Model 15-550. The demodulator action is essentially the same as that described for the other receivers; however, the phase of the Q reference signal is such that a positive Q signal is available at the output of the Q demodulator stage. A negative I signal is produced in the output of the I demodulator stage. These signals are applied respectively to the grids of the G - Y and the R - Y matrix amplifiers.

These two stages function as cathode followers; consequently, positive Q and negative I signals are developed across the common cathode resistor R214. This combination of signals is applied to the cathode of the B - Y matrix amplifier. The signals will experience no polarity inversion through this stage; therefore, positive Q and negative I signals are produced at the output of V35B. These signals are of the proper polarity to produce a positive B - Y signal.

A positive Q signal is applied to the grid and a negative I signal is applied to the cathode of the G - Y matrix amplifier. The polarity of the Q signal is reversed through this stage; however, the polarity of the I signal is not inverted. A negative I and a negative Q signal appear at the output of this stage. These are the necessary polarities for producing a positive G - Y signal.

The specific amplitudes which are developed in the output of each of the matrix amplifiers are governed by the various bias levels on these stages. The relative signal amplitudes obtained from the demodulator stages and the plate voltages applied to the matrix amplifiers are also important factors in this operation. The values chosen for the parts in the matrix circuit are such that the proper amplitude of the I and Q signals are combined to produce the ghree color-difference signals.

Video peaking is provided for each of the colordifference signals in the plate circuits of the matrix amplifiers. Since the DC component is lost when the signals are applied through the coupling capacitors, DC restoration is provided. The color-difference signals are then fed to the respective control grids of the picture tube.

A previous section of this series discussed a luminance channel which provided at the output a negative Y signal. It can be seen that the circuit in Fig. 8-9 utilizes such a signal. By applying a positive color-difference signal to a grid of one of the guns in the tricolor picture tube and a negative Y signal to the cathode of the same gun, the matrix operation is completed. This can be more clearly understood if it is considered that a negative signal at the cathode of a tube will provide the same action as a positive signal of the same amplitude applied to the grid.

Matrixing in the R-Y, B-Y Receiver

The schematic diagram in Fig. 8-10 shows the matrix circuit used in the Westinghouse Model H840CK15 color receiver. The fact that this receiver demodulates along the R - Y and B - Y axes simplified the matter of combining signals. An R - Y signal and a positive EY signal are combined at the input of the red amplifier, and a B - Y signal and a positive E_Y signal are combined at the input of the blue amplifier.

It has been mathematically proved that a G - Y signal can be formed by combining a negative R - Y and a

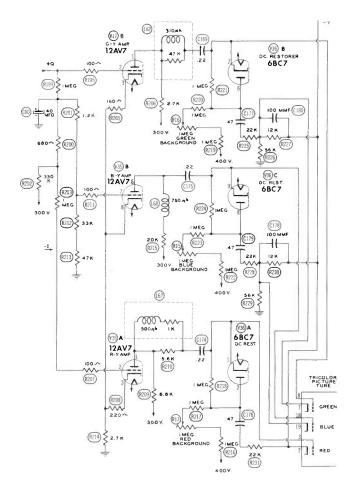


Fig. 8-9. Matrix Circuit Used in the Arvin Model 15-550 Color Receiver.

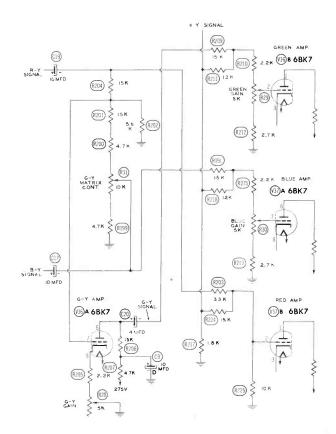


Fig. 8-10. Matrix Circuit Used in the Westinghouse Model. H840CK15 Color Receiver.

negative B - Y signal in the ratio of .51 to .19. This receiver combines positive values of R - Y and B - Y in the proper ratio to produce a negative G - Y signal which is then applied to the grid of the G - Y amplifier. As a result, the signal voltage available at the plate of this stage is a positive G - Y. This signal is combined with a positive E_V signal at the input of the green amplifier.

In order to reproduce the three color signals properly, the luminance and color-difference signals must be combined in a specific ratio. For a given amplitude of the luminance signal, the amplitudes of the R - Y and B - Y signals can be adjusted through the use of the color saturation and B - Y gain controls (not shown in Fig. 8-10). The G - Y matrix control can be adjusted for a ratio of R - Y and B - Y which will produce a negative G - Y signal. The gain control in the cathode circuit of the G - Y amplifier can be adjusted so that the proper amplitude of G - Y voltage is combined with a given amount of positive E_Y signal.

AMPLIFIER AND OUTPUT STAGES

The analysis of the matrix circuit used in the RCA Victor Model CT-100 color receiver assumed that the grid resistances of the amplifier stages were equal. As seen in Fig. 8-11, this is not actually the case, because the grid-load circuits of the blue and green amplifiers are shunted by the blue and the green gain controls. The reason for this is that in order to produce the same light output from all three phosphors, more signal voltage is required to excite the red phosphor than is required to excite the blue and green phosphors. The blue and green gain controls are used to adjust the amplitudes of the signal voltages so that the emissions from the three phosphors are equal.

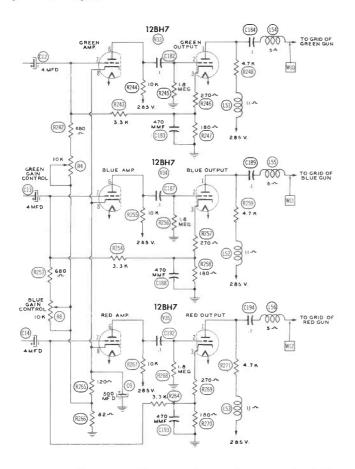


Fig. 8-11. Matrix Amplifier and Output Stages in the RCA Victor Model CT-100 Color Receiver.

The ratios of the voltages in the individual matrix circuits are not affected by the adjustment of these controls. That is, if the blue gain control is varied, the amplitudes of the I, Q, and Y voltages which are developed in this grid circuit will vary; but the percentage of change in each signal is the same, and the ratio between each signal amplitude and the total amplitude does not change.

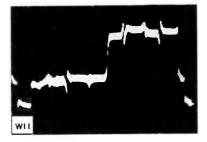
Further examination of the circuit shows that degenerative feedback is applied from the cathodes of the output stages to the grids of the amplifier tubes. The 470-mmf capacitor in each cathode circuit causes the degeneration to be greater at the low frequencies. These capacitors also cause the gain through the output stages to be greater at the higher frequencies. The gain of each color signal is thereby stabilized over the video-frequency range. Shunt and series peaking are provided in order to maintain uniform video response. The signals at the grids of the red, blue, and green guns during a typical color-bar transmission are shown by the waveforms in Fig. 8-12.

DC RESTORATION

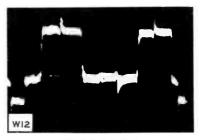
The DC component of three color signals has been blocked by the coupling capacitors between the various amplifier stages. If the correct DC level is not restored, these signals will not accurately reproduce the background illumination. Instead, the background illumination will be represented by the average amount of voltage of the AC signals.



Signal at Green Gun



Signal at Blue Gun



Signal at Red Gun

Fig. 8-12. Color-Signal Voltages at the Control Grids of the Tricolor Kinescope During a Color-Bar Transmission.

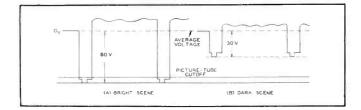


Fig. 8-13. Loss of the DC Component in the Video Signal,

The drawing shown at A in Fig. 8-13 is representative of a scene which has a high-brightness level. The brightness control has been adjusted so that picture-tube cutoff is just above the blanking level. If a signal representing a low-brightness scene is now transmitted, a condition like that shown at B will exist. The average bias on the picture tube does not change; consequently, the background illumination is still the same. In addition, the blanking level will not reach the cutoff level of the picture tube, and the retrace lines may be seen in the picture.

The desired condition at the grid of the picture tube is illustrated in Fig. 8-14. The sync tips are shown to be clamped at a predetermined DC level so that cutoff is effected by the blanking pedestal regardless of the peakto-peak amplitude of the signal. It can be seen that the average voltage at the grid of the picture tube will be equal to the DC clamping level plus the average voltage produced by the AC signal.

One method of obtaining the foregoing condition is through the use of the circuit shown in Fig. 8-15. This circuit is used in the RCA Victor Model CT-100 color receiver to restore the DC level to the red signal. The restoration circuits for the blue and green signals are identical to the one shown. If no signal is present at the output of V35B, the voltage at the plate is approximately 215 volts. Let us assume that the brightness control has been adjusted so that the potential at the plate of V36C is a positive 20 volts with respect to ground. This voltage will also be present at the cathode and at the top side of R277; consequently, C194 and C195 will each be charged to a potential of 195 volts. The polarity of these charges will be as shown in the drawing. Since the diode will conduct only from cathode to plate, the voltage at the negative side of these capacitors can increase but cannot decrease.

Let us suppose that the signal representing a bright scene in Fig. 8-13A is present at the plate of V35B. During the negative excursions of the signal, the voltage at the positive side of C195 will decrease by 60 volts. The voltage at the negative side of this capacitor will try to decrease by the same amount; however, this action causes

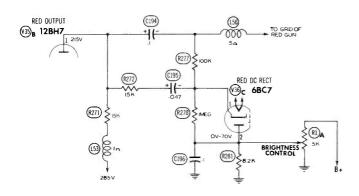


Fig. 8-15. DC-Restorer Circuit Used in the RCA Victor Model CT-100 Color Receiver.

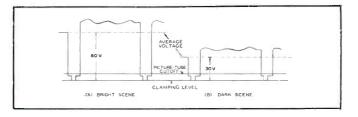


Fig. 8-14. Video Signals With the DC Component Restored.

the diode to conduct, and the charge across C195 is reduced by 60 volts.

When the signal at the plate of V35B goes in a positive direction, C195 will try to charge to a higher value; however, the time constant of C195 and R278 is nearly 800 times the scanning time of one horizontal line. As a result, the charge across C195 will remain fairly constant until the brightness level of the scene changes. The voltage at the negative side of the capacitor will follow the signal variations at the positive side; consequently, the voltage at the grid of the red gun will have an average value which is equal to the average value of the signal plus the voltage at the plate of the diode. The negative peaks of the signal are clamped at the DC level determined by the setting of the brightness control. Note that this condition conforms with that shown at A in Fig. 8-14.

Let us see what happens to the same circuit when the signal representative of a dark scene is being received. During the negative excursions of the signal, the voltage at the plate of V35B will decrease by 30 volts. The voltage at the negative side of C195 cannot decrease, so the potential across the capacitor is reduced by 30 volts. (The discharge path is through the diode.) The result of this action maintains the voltage on the negative side of C195 at the DC level determined by the setting of the brightness control during the time that the signal at the plate of V35B is at a maximum negative level.

When the signal goes in a positive direction, C195 tries to charge to a higher level but does not have sufficient time to do so. (The signal is positive for approximately 60 microseconds; whereas, the time constant of C195 is 47,000 microseconds.) As long as the brightness level of the signal remains the same, the charge across C195 will be held at a relatively constant level. When the signal at the plate of V35B traverses from the negative side of C195 will increase by the same amount. As a result, the negative peaks of the signal at the charge of the signal at the charge by the same amount. As a result, the negative peaks of the signal at the charge at the signal at the charge by the signal at the cathode of the diode are clamped at a specific DC level, as shown at B in Fig. 8-14.

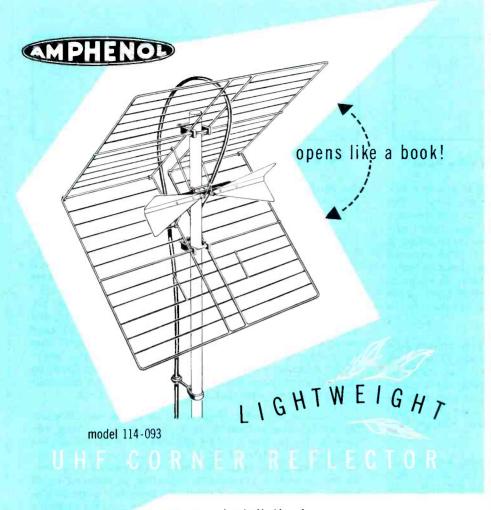
The 15K-ohm and 100K-ohm resistors R272 and R277 isolate the clamping action of the diode from the plate circuit of V35B. The charging and discharging action across C194 is much the same as that across C195, since C194 is essentially connected in parallel with C195.

As mentioned previously, a DC-restoration circuit is employed in the grid circuit of each of the guns. The plates of all of the DC-restorer diodes are connected together so that all three signals will be clamped at the same level.

In the next issue, we will begin the discussion of the color-picture tubes and will discuss their associated convergence circuits.

In order to give the reader an opportunity to test himself on the material in this issue, we are including on the insert a few questions that are answered in this discussion.

BY C. P. OLIPHANT and VERNE M. RAY



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Notes on Test Equipment

(Continued from page 19)

into the receiver by rotating the output control in a clockwise direction. The VTVM pointer will move across the scale; and when it has reached the mark on the lower scale which corresponds to the one noted previously on the upper scale, the noise figure of the receiver can be read on the db meter. The noise generator is so designed that, for the conditions just mentioned, the signal fed in from the diodes is just enough to double the noise power at the video detector.

For those readers who may wonder why the instrument is set up to operate in this manner (that is, through a doubling of the noise power). the following explanation is offered. The noise factor (NF) of an amplifier can be defined as the actual noisepower output that is due to input resistance and amplifier noise divided by the noise-power output that is due to input resistance only. This relationship can be conveniently referred to the amplifier input terminals in terms of the rms noise current of a noise diode. If the noise source is matched to the amplifier input throughout the bandwidth of the amplifier, the noise factor may be found from the following expression:

$$NF = \frac{.02 IR}{n-1}$$

where

I = noise-diode current in ma,

R = amplifier input impedance,

n = noise power from the amplifier when the diode is on divided by noise power from the amplifier when the diode is off.

By adjusting the output of the noise diode until the receiver output doubles, n can be made equal to 2; and n - 1, of course, becomes 1. The meter which measures diode current I can then be calibrated to read the noise factor directly; and since by definition the noise factor is a power ratio, the scale divisions can be in decibel units.

Contrast the method which uses the Hickok Model 755 to determine the noise figure with another method that is sometimes used to evaluate how well a receiver will pick up weak signals. First, the antenna terminals are shunted with a resistor of value equal to the input impedance of the receiver (usually 300 ohms). An AC VTVM is connected across the point

PF REPORTER - January, 1955

of signal input to the picture tube, and the reading is noted. The contrast control should be at maximum setting for all readings. If the reading is greater than 3.33 volts rms, the receiver sensitivity is reduced to obtain this reading by applying the necessary amount of fixed bias to the AGC line. In a receiver which employs keyed AGC, the AGC section should be disabled unless fixed bias is applied as just mentioned. The receiver check should be made with the tuner set to that channel on which it is expected to receive the weakest signal, and the fine tuning must be accurately adjusted. This can be accomplished by applying a sweep signal to the antenna terminals at the channel frequency and an RF marker signal at the exact frequency of the channel video carrier. A scope connected across the video detector will then display the over-all response of the receiver, and the fine tuning should be adjusted to place the marker at the point recommended for correct alignment. This will usually be at 50 per cent in the video slope of the curve.

After the receiver tuning has been correctly adjusted in this manner, the sweep generator is removed and the marker signal alone is applied. This signal is maintained at its previously determined frequency and is modulated 30 per cent with an audio signal. The generator used for the marker signal must be one which has an accurately calibrated attenuator. The level of output from the generator. is adjusted to obtain a 20-volt peak-to -peak reading of the audio modulating signal on the VTVM which is connected to the modulated element of the picture tube. This level of output will provide a relative evaluation of the ability of the receiver to pick up weak signals.

The choice of the 3.33-volt and 20-volt standards in the foregoing procedure is based on the following reasoning. A 20-volt peak-to-peak signal at the picture tube is generally considered to be the minimum for an acceptable picture. Satisfactory synchronization will usually be obtained for a value even lower than this; therefore, the picture guality can be considered as the limiting factor. A one-to-one ratio of signal to noise is also generally accepted as the minimum for acceptable viewing, and this would mean that the noise peaks should be limited to 20 volts or less. The average reading for random noise with 20-volt peaks is about 3.33 volts, as read on the AC rms scale of the VTVM. Therefore, a 3.33-volt rms noise reading and a 20-volt peak-topeak signal indicate that the signal-to -noise ratio is established at a value of one to one. This value satisfies the



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minimum conditions for acceptable picture quality.

It can readily be seen that the foregoing procedure is rather involved when compared to the direct approach afforded by the noise generator. In addition to the ease with which the noise generator may be operated, another advantage of the instrument is the fact that the noise figure is obtained without regard to the response characteristics of the receiver.

Manufacturers of receivers and amplifiers should find an instrument of this type useful in checking the noise characteristics of their products. Large service shops, particularly those in fringe-reception areas, should also find use for this instrument. For example, a receiver may be brought into the shop with the complaint that there is excessive snow in the picture. A check may reveal that the set does not have abnormally low sensitivity. This would indicate that some stage is introducing an unusual amount of noise.

Any circuit component can be suspected of contributing excessive noise. Resistors and capacitors can become noisy in time, and this noise will be especially noticeable if the components are in a part of the circuit where the B_+ voltage is applied. More often than not, a noisy tube may be the offender, and this can be easily checked by substitution.

In the majority of cases, the input stages of an amplifier will contribute much towards a high noise level because any noise developed in them undergoes a higher amplification than noise introduced at later stages. The following example will serve to illustrate how the selection of tubes for the tuner section of a receiver may lower the noise figure of the entire receiver. A receiver was checked using the Model 755 noise generator and was found to have a noise figure of 16.5 db. The tuner employed a 6J6 mixer-oscillator tube. Three new 6J6 tubes were substituted and the results are shown in the following table.

TUBE	Noise Figure (db)	Triode No. 1 (µ mhos)	Triode No. 2 (μ mhos)
1	16.5	2500	2100
2	15.0	5000	5000
3	12.5	3900	4700
4	11.5	4600	4600
-			

The No. 1 tube was in the set originally and was also the one which gave the highest noise figure. As a matter

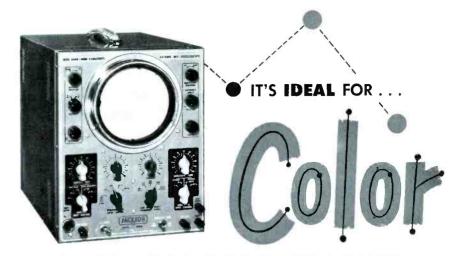
of information, the tubes were checked for transconductance in a tube checker to see if that tube characteristic might bear any relation to the noise figure. It can be seen that the No.1 tube was considerably weaker in transconductance than the others. A value of 3.000 micromhos was listed as normal on the tube checker. The No.4 tube afforded an improvement of five db in the noise figure. No apparent relation between the transconductance and the noise figure could be seen. All these tests were made inside a screen room in order to exclude outside noise. When a test was made outside the screen room, the noise figure using the original 6J6 jumped from 16.5 db to over 19 db which is the maximum indicated on the scale of the db meter. Incidentally, although a screenroom would be desirable for exact measurements, a relative comparison between receivers can be made without the use of a screen room. No attempt was made to check the sensitivity of the receiver while substituting tubes to lower the noise figure; however, a decrease in the noise figure will usually be accompanied by an increase in sensitivity.

In checking a variety of receivers, the technician might find that representative noise figures would fall into the following ranges: 9 to 16 db for receivers with pentode tuners and three to four IF stages, 6 to 14 db for receivers with cascode tuners and three to four IF stages. Individual receivers in each group might occasionally give an even lower figure. A noise figure near the upper limits of these ranges should lead the technician to suspect that some improvement might be obtained either by tube substitution or by other means such as realignment.

It is quite possible that noise may be originating within the receiver in sources other than the amplifier circuits being measured. Such sources could be a high-voltage supply with corona leakage, a sweep circuit that is disturbing the video stages, or other sources having RF leakage or hum coupling. Fossibly noise measurement can be used as an aid in determining if this type of noise is present and in tracking it down. If the technician is unable to lower the high noise figure in a receiver by working with the RF and IF stages, he should check to see whether these other sources are contributing to the noise in the set.

Locating Hard-to-Find Tube Shorts

While checking a tube recently for suspected shorts, we accidentally came upon a procedure which might prove helpful in some of those stub-



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pull horizontal amplifiers have a sensitivity for all applications of 0.40 RMS volts per inch. Vertical Input Impedance-1.5 megohms,

shunted by 20 mmf. Direct to plates balanced 6 megohms, shunted by 11 mmf.

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Model CRO-2 Oscilloscope	. \$225.00, net
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REMOT-O-MATIC SALES, INC. 8747 Sunset Boulevard • Los Angeles 46, California born cases. Usually, the procedure in checking a tube with any make of tube checker is to check first for shorts and then, if none are found, to proceed with a merit check and other tests. This precludes the risk that a shorted tube might damage the tube checker if other checks were made before the shorts test.

Some shorts will not show up unless the tube is at a high operating temperature like that attained during actual use. A shorts test is usually performed with only the filament voltage applied for tube operation. (A voltage is also applied to make the shorts indication, but this does not contribute towards heating the tube.) The tube temperature can be raised considerably by the following procedure. First, make the shorts test as a safety precaution; then, if no indication is obtained, make the merit test, prolonging it somewhat more than necessary for the actual reading. Immediately, before the tube has a chance to cool, make another shorts test. The added heat may be sufficient to cause the short to appear. and thus it can be located. Some tube checkers are designed so that it is possible to make a quick change from a shorts test to a merit test. On other checkers, this change may require a little more time.

The above procedure might prove helpful in checking for gas in tubes, because this condition is one which is also aggravated by heat.

Calibrating the Hickok Model 690 Crystal-Controlled Marker Calibrator

Recent correspondence indicates that some technicians may be a little uncertain concerning the exact location of the proper calibration points when calibrating the Hickok Model 690 marker calibrator on the lowest range (4.25 to 11 mc). This uncertainty arises from the fact that apparently two peaks of electric-eye closure are obtained within a fraction of a megacycle of each other at the calibration points. This aspect of calibration is covered briefly in the Hickok manual of operating instructions, Note 1, page 3. When the technician understands fully the significance of these indications, it will be seen that calibration is extremely accurate

Calibration of the instrument is accomplished through the use of a 2.5-mc crystal furnished with the Model 690, or a crystal of the technician's own choosing can be used in one of the spare positions. When the 2.5-mc crystal is used, the marker signal can be calibrated at all points which are multiples of 2.5 mc. These points are indicated by indentations on the dial scale.

Signals from the crystal oscillator and the RF variable oscillator of the instrument are applied to a mixer stage and heterodyned together. The result is an audio beat difference, and this difference is fed to a twostage audio amplifier having a gain of approximately 800. The amplified audio beat difference is then applied to a diode rectifier and filter stage with the result that a filtered DC out put is available for the grid of the tuning-eye tube. Application of this DC voltage causes the tuning eye to close to a certain extent, depending upon the setting of the sensitivity control of the indicator. The audio amplifier has a normal audio response which falls off at the high-and lowfrequency ends. Above and below these points, the beat frequency will have little effect on the eye. When the generator is tuned to approach the calibration point, a high beat frequency is obtained first; and this is gradually lowered in frequency as the tuning continues. When the generator tuning reaches the exact point of calibration, the beat frequency has fallen to zero; and further tuning in the same direction will cause the beat frequency to rise and go through all the previous frequencies but in reverse order.

A graph of the audio-amplifier response to the beat frequency might appear somewhat as in Fig. 3. Since the response falls off at the extreme high and low audio frequencies, there

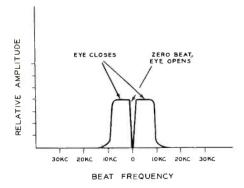


Fig. 3. Response of the Audio Beat-Frequency Amplifier in the Hickok Model 690 Marker Calibrator.

will be a dip in the response at the zero-beat point with a peak occurring on either side. This graph could also serve to represent the DC voltage applied to the tuning eye, with the two peaks representing closure of the eye and the dip representing the open condition. The entire range of response of the audio amplifier extends from approximately 10 kc on one side through zero beat to approximately 10 kc on the other side. The RF generator must betuned through approximately 20 kc to cover this range.

On the low-frequency range (from 4.25 to 11 mc) of the generator, this 20-kc tuning is covered by a very small rotation of the tuning control; therefore, slow and careful tuning is necessary to set the control to zerobeat position. On the high-frequency ranges, the tuning is even sharper; and the only visible indication of zero beat will be a faint flutter of the eye as the generator is tuned through the point of minimum shadow angle. In either case, the flutter or opening of the eye between the two peaks of eye closure indicates the exact center of the calibration point; and it is to this point that the generator should be tuned for calibration purposes.

RECENT RELEASES

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Frequency-compensated attenuator.

Seven-inch cathode-ray tube.

Other specifications include vertical impedance of one megohm and 26 mmf and horizontal impedance of one megohm and 53 mmf. Provision is made for internal or external synchronization of either positive or negative polarity. Horizontal and vertical amplifiers are push-pull.

Over-all dimensions are 17 1/16 inches high by 11 3/8 inches wide by 19 1/2 inches deep. Weight is 43 pounds.

Sylvania Type 301 Polymeter

This Type 301 vacuum-tube voltmeter is a recent addition to the line of polymeters made by Sylvania Electric Products Inc. Among its

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features are: a 7-inch meter movement illuminated for viewing in poorly lighted locations, 17-megohm effective input resistance, peak-to-peak scale for measurement of complex waveforms, shielded AC lead, screw-on connectors, and a patented linearity circuit for greater scale accuracy.

The following scales are provided for each of the indicated functions:

Peak-to-peak meter, 6 ranges from 0 to 2800 volts.

AC voltmeter, 6 ranges from 0 to 1000 volts.

DC voltmeter, 6 ranges from 0 to 1000 volts.

Ohmmeter, 6 ranges from 0 to 1000 megohms.

DC ammeter, 6 ranges from 0 to 10 amperes.

Decibel meter, 6 ranges from -20 to +61.4 decibels.

The input impedances are:

AC ranges, 2.7 megohms shunted by 40 or 125 mmf when using the shielded lead.

DC ranges, 17 megohms including one megohm in the probe.

Over-all dimensions are 83/4 inches wide by 11 3/16 inches high by 6 15/16 inches deep. Weight is 12.5 pounds.

Accessories supplied with the Sylvania Model 301 are:

One DC test probe.

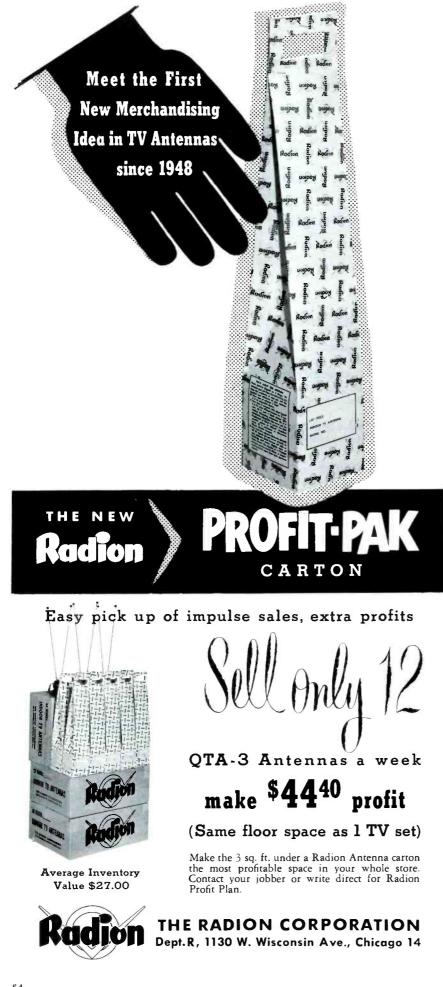
One shielded AC-volt, DC-current, and ohms test lead.

One common test lead.

Sylvania Type 302 Polymeter

The Sylvania Type 302 is a deluxe version of the Type 301 polymeter and includes all of its features. An additional feature is the inclusion of an RF probe which is an integral part of the new Type 302. This probe is of the vacuum-tube type and is equipped with a shielded cable and a coaxial connector. Spring clips provide for convenient mounting of the probe on the front panel when the probe is not in use.

PAUL C. SMITH



Dollar & Sense Servicing

(Continued from page 31)

TV IN BOOTHS. From a Washington news letter, we learn that a restaurant in Paramus, N. J., practically in our own back yard, has installed TV sets in individual booths. Half a dozen phone calls failed to locate the restaurant, but we still like the idea. Here's why.

For booths a 10-inch screen is ideal, since viewers are close up. What better use could there be for those 10-inch trade-ins gathering dust in your back room or basement. You'd have to catch the restaurant at remodeling time, or talk them into moving the booths out from the wall far enough to accommodate the depth of the sets. Some may prefer outright sale, with or without a yearly service contract; whereas others might prefer leasing at so much a month including service.

Don't go into something like this too fast, however. Remember that the sets will have to bring the restaurants enough EXTRA business to give enough extra profit to pay for what you charge for the sets. You've gotta be prepared to show that these sets will pay for themselves and then some in a place that probably has one big set over the bar already.

Perhaps coin-in-the-slot attachments for the sets will be the answer in some places; you can buy these quite reasonably now and then from such surplus firms as Herbach and Rademan Inc., 1204 Arch St., Phila.7, Pa. Ask toget on their mailing list for monthly catalogs, if you're not already getting them. The bargains are mixed in with items of regular price so you'll have to hunt.



FOLLOW THE LEADER. When RCA needed half a dozen special new electronic assemblies in a hurry to meet opening dates for a new Cinemascope feature, their industrial TV system saved the day by eliminating training time entirely. A camera was mounted in position over a workbench where a specialist assembled the needed unit, and six receivers were placed on production benches right in front of the other workers. Each watched the screen and followed the movements of the leader while listening to his verbal instructions, completing the job in time to make the deadline.

JOHN MARKUS

PF REPORTER - January, 1955

Transistor Radio Is Here

(Continued from page 13)

complete with battery weighs only 12 ounces. The case is made of polystyrene plastic and is available in a variety of colors. The schematic of the Model TR-1 is shown in Fig. 1 and should be of real interest.

Technical Features

The assembly process starts with the printed-circuit board shown in Fig. 2. This board serves as the chassis of the receiver. All of the components are mounted on the board, and all connections are soldered simultaneously in one dipping operation.

Converter Stage

The antenna in the Model TR-1 is in the form of a coil which has a ferrite core providing a tuned circuit of high Q. Hand capacitance has very little detuning effect on this coil, and the receiver is not exceptionally directional; these are two good

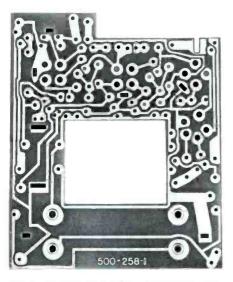


Fig. 2. Printed-Circuit Board Used in the Regency Model TR-1.

features in a portable receiver of such a small size. A low-impedance winding on the antenna coil couples the received signal to the base of the converter transistor. Like the three other transistor stages in the receiver, the converter stage is biased in such a way that the input impedance is low (about 500 ohms).

The oscillator injection voltage is derived from a tuned circuit which is inductively coupled to a coil in the collector circuit. The entire converter stage is similar in operation to the vacuum-tube converter circuit shown in Fig. 3, a circuit which has been used in conventional receivers. As in any superheterodyne receiver,

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the IF transformer accepts the proper frequency from among the multitude of frequencies in the output circuit of the converter and passes this frequency to the first IF stage.

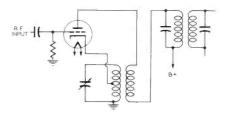


Fig. 3. Equivalent Vacuum-Tube Converter Circuit.

IF Stages

The IF transformers used in this receiver are of the tuned-primary, untuned-secondary type; and they resonate at 262 kc. The secondaries are wound with very few turns so that proper matching to the low input impedances of the IF transistors is obtained. The primary of each transformer is paralleled by a capacitor of fixed value, and variable tuning is accomplished with the threaded iron core.

The two IF stages are almost identical, and they are both connected as grounded-emitter circuits. Since the three-element transistor is the analogue of the triode vacuum tube, and since triodes must be neutralized when they are used at other than audio frequencies, the two IF transistors must also be neturalized in order to prevent stray oscillations. In this receiver, the neutralization of each stage is accomplished by a series capacitor-resistor combination which feeds a portion of the output signal back to the input of the stage.

Only the first IF stage is controlled by AVC. This is derived from the output of the diode detector, is filtered, and is then supplied to the base of the transistor in the first IF stage. When the received signal increases, the negative AVC voltage which is fed back to the base of the first IF transistor increases and reduces the gain of this stage. The opposite condition prevails when the signal strength decreases.

The second IF stage derives its base bias from the emitter of the audio output transistor. The bias resistor in the output-emitter lead is bypassed by a large value of capacitance in order to stabilize the voltage across the resistor. This voltage is further bypassed by an .05-mfd capacitor and is fed to the low side of the secondary of transformer T2. A resistor in the emitter lead of each of the IF transistors develops a voltage which biases the emitter properly. The diode-detector stage, in which the manufacturer uses either a Raytheon CK706A or a Tungsol TS117 crystal diode, is connected directly to the volume control. The low resistance (1,000 ohms) of this control is necessary for a proper impedance match to the input of the audio transistor.

Output Stage

The output transistor is connected in a grounded-emitter circuit, and bias for the emitter is obtained by a series resistor. Bias for the base is obtained by a voltage divider from the positive line. These two bias arrangements assure that variations in ambient temperature and in battery voltage will not adversely affect the operation of this transistor. The collector impedance of this transistor is approximately 10,000 ohms, a value considerably lower than that which is characteristic of most transistors of this general type.

The output transformer matches the 10,000-ohm impedance of the output transistor to the 12- to 15-ohm impedance of the speaker. The speaker, which is only 2 3/4 inches in diameter, provides reasonable fidelity and volume for so small a unit. A hearing-aid type of earphone is available as accessory equipment for the Model TR-1, and the earphone plug can be inserted into a small jack on the side of the receiver. The speaker is silenced when this plug is inserted into the jack.

Power Supply

The entire power requirements for this receiver are fulfilled by one hearing-aid battery that provides 22.5 volts. The current drain from this battery is only 4 ma when a local station is being received, and the life expectancy of the battery is rated at 20 to 30 hours depending upon frequency and duration of use.

One important fact to remember is that it is physically possible to reverse the battery when inserting it into the clips. Warnings are given about this in the literature accompanying the receiver and inside the receiver case. The transistors will not be harmed by a reversal of battery polarity; but the electrolytic capacitor connected between the positive battery lead and ground will be damaged if the battery is reversed.

A photograph of the receiver shown in Fig. 4 has been included to give a general idea of the way the components have been mounted. Note in particular the small size of the IF transformers, audio output transformer, and the tuning capacitor. The

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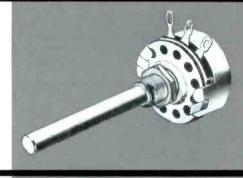
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Complete Public Address System catalog available upon request. Simply check Bogen number on Catalog & Literature Service post card in rear of magazine. use of these miniature components together with the use of transistors instead of tubes contribute to the compactness of the receiver.

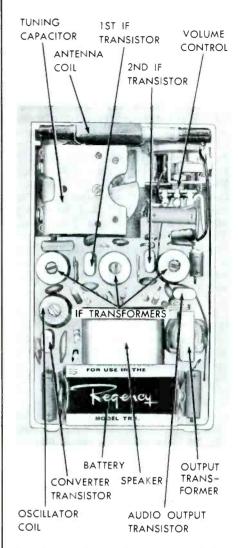


Fig. 4. Rear View of Regency Model TR-1 Showing Layout of Components.

We want to acknowledge the very kind cooperation of the Regency Division of I. D. E. A., Inc., in supplying information for this article and in making it possible for us to view the units in production.

WILLIAM E. BURKE

EDITOR'S NOTE: For those who would like to review general transistor theory, it is suggested that reference be made to "The Transistor Story, Parts I and II," which appeared in the September -October 1953 and in the Febru ary 1954 issues of the PF INDEX, predecessor of the PF REPORTER.

Audio Facts

(Continued from page 11)

The sectional chassis is unique and convenient in that, besides being prepunched, many of the components can be mounted and partially wired on the separate sections before the chassis is completely assembled.

The chassis furnished with the Triad HF-3 preamplifier kit is shown assembled in Fig. 3. The decals have been applied, but no components have been mounted.

Preamplifier and Equalizer Kit

The schematic of the selfpowered preamplifier which can be constructed with the Triad HF-3 preamplifier and equalizer kit is shown in Fig. 4.

Any one of the four inputs provided for convenient and flexible operation can be connected into the



Fig. 3. Triad HF-3 Chassis Assembled With Decals Applied.

circuit by the input selector switch. The two phono inputs (magnetic and crystal) channel the signal through the preamplifier section. The two halves of the 12AY7 tube V1 operate as a two-stage phono preamplifier with an equalizing network which is controlled by the 9-position record compensation switch connected between them. Correct compensation for satisfactory reproduction from most any record can be obtained by selecting the proper playback curve from the nine different ones provided by the record compensation switch. The tuner and microphone inputs are

channeled around the phone preamplifier section by the input-selector switch and connected directly to the volume control R1.

All signals are amplified by the first section of the 12AU7 tube V2 and then fed into the second section of V2 which is the tone-control stage. The degenerative tone-control circuit provides a wide range of boost or droop of both high and low frequencies. A flat frequency response is maintained when the tone controls are set in mid-position because this point on both controls is effectively at signal (AC) ground potential, and no boost or droop is produced. If R29 and R30 are equal in value, the signal voltages at opposite ends of R2 and R3 are equal but are of opposite polarity.

When the movable contact of R3 is moved to the end of the control connected to the plate of V2, maximum bass droop will be produced. If the control is turned to the end connected to the cathode, L1 will be shunted across R29 and maximum bass boost

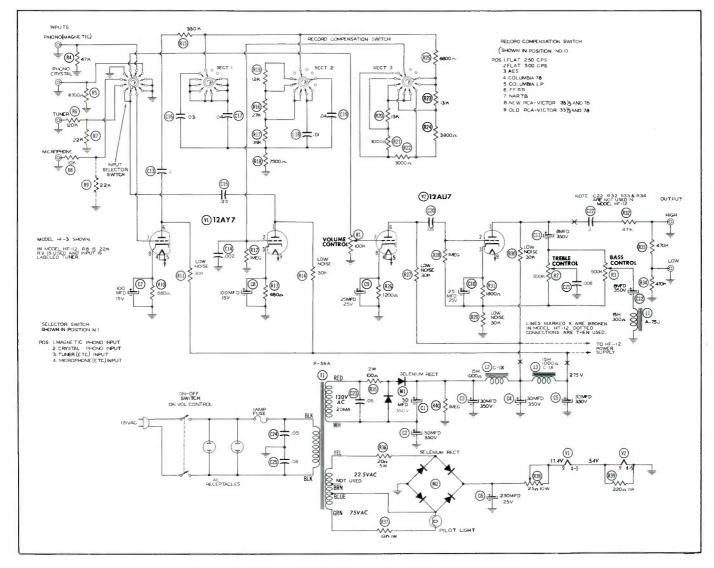


Fig. 4. Schematic of the Triad HF-3 Preamplifier and Equalizer Kit.



Service men go for Walco's packaged phonograph needle replacement plan because it's so easy to understand and put to work. No headaches trying to figure out which needle for which cartridge-two easy guides figure for you. And you don't have to be a salesman to sell replacement-even to sell profitable diamond needles-Walco sells 'em for you, by proven methods learned in our long experience as leaders in the replacement needle industry-and as originators of the modern jewel tip needle. See how the Walco plan stacks up 8 ways better to help you service and sell:

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3 10-SECOND GUIDE—to most popular replacements. Nome of phono is all you need!

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When you need in the second second

7 RECORD SPINDLE CARDS—They tell the customer you've replaced a needle and how long it will wear —then urge him to re-order.

8 NATIONAL ADVERTISING—building your customer's confidence in Wolco and in you for replacing with Wolco. Ads in High Fidelity, Saturday Review and other record-minded magazines.

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SEND FOR WALCO'S CATALOG 600 TRADE NAME OF ELECTROVOX CO., INC. Leaders in Replacement Needles 60 Franklin Street, East Orange, N. J. will be obtained. The same effect will be produced on the treble response if the treble control R2 is moved in a similar manner. The 8-mfd electrolytic capacitors C11 and C12 prevent the DC from flowing to ground.

Personal experience with this type of tone control has convinced us that the objections raised against the use of inductors in tone-control circuits can be discounted. We have never been troubled with such things as transient distortion and instability caused by the presence of an inductor in the tone circuit. Hum pickup is no problem when a unit such as the A-75J tone choke with its 45-db shielding and hum-bucking construction is used. Sufficient signal is available at the output of this preamplifier and equalizer to operate any amplifier used in the usual audio system.

A selenium rectifier M1 operating in a voltage-doubling arrangement and the filter formed by C3, C4, C5, L2, and L3 supply the well-filtered B+ voltages. The full-wave bridge type of selenium rectifier M2 and filter capacitor C6 supply DC for heating the tube filaments. Voltage adjustments can be made by moving the slider on the adjustable resistor R38. The R-56A power transformer T1 was designed for this type of application where selenium rectifiers are employed.

A 10-Watt Amplifier Kit

The preamplifier section of the Triad HF-12 10-watt amplifier kit is identical to the HF-3 preamplifier and equalizer kit except for the common power supply. Since they are similar, the data covered in the discussion on the HF-3 preamplifier will not be repeated here. A schematic of the HF-12, less the preamplifier section, is shown in Fig. 5.

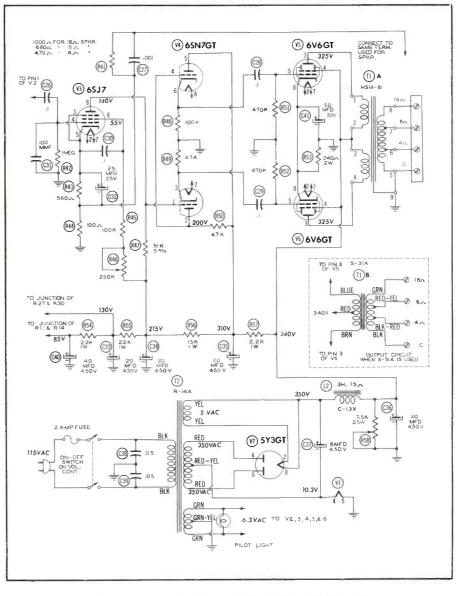


Fig. 5. Schematic of the Triad HF-12 10-Watt Amplifier Kit.

The layout of parts and controls of the HF-12 amplifier kit, which is a single unit, follows the same general pattern as that used in the HF-3; but a slightly larger (8-inch by 12-inch) chassis is used. The output from the preamplifier section feeds into the grid of the 6SJ7 (V3) which is in the first stage of the power-amplifier section. The potentiometer in the screen circuit of V3 serves as a balance control and is adjusted to obtain the correct bias on the phaseinverter stage V4 which is coupled directly to the plate (pin No. 8) of V3.

The phase inverter is cathodecoupled to the push-pull 6V6GT output stage. Note that C28 and C29 are the only coupling capacitors used in the power-amplifier section. Negative feedback is provided by the connection of C27 and R41, in parallel, from the secondary of the output transformer T1 to the junction of R43 and R44 in the cathode circuit of V3.

The schematic shows the Triad HSM-81 output transformer connected as T1 (A) and the Triad S-31A output transformer connected as T1 (B) in the partial schematic. This is done because the HF-12 kit can be obtained with any one of four different output transformers supplied as follows:

KIT	TRANSFORMER	OUTPUT (ohms)
HF-12	S-31 A	16/8/4
HF-12A	HSM-81	16/8/4
HF-12B	S-32A	500/250/125
HF-12C	HSM-82	500/250/125

The power supply is conventional in most ways. Probably the most unusual feature is the manner in which DC is supplied to heat the filament of the 12AY7 tube V1. The heater (pins 4 and 5) of V1 is connected into the negative return lead of the highvoltage supply. The amount of current flowing through the heater of V1 can be adjusted by moving the adjustable contact on the bleeder resistor R58.

The Triad HF-18 and HF-40 are also available in kit form. These kits feature the same type of assembly and mechanical construction methods used in the HF-3 and HF-12 kits.

The HF-18 kit contains the basic parts for constructing a conventional Williamson amplifier using KT66 (or 5881, 807, 1614, or 6L6) output tubes. An audio output of 16.5 watts is obtained with triode operation, or an output of 20 watts is obtained when the screens of the output tubes are connected to screen taps on the primary of the output transformer.

КІТ	TRANSFORMER	OUTPUT (ohms)
HF-18	S-148A	16/8/4
HF-18A	HSM-189	16/8/4
HF-18C	HSM-190	500/250/125

A 40-watt amplifier suitable for use in auditoriums or theaters can be constructed from the basic components furnished in the HF-40 kit. This high quality of amplifier features 6146

KIT	TRANSFORMER	OUTPUT (ohms)
HF-40	S-42A	16/8/4
HF-40A	HSM-94	16/8/4
HF-40C	HSM-95	500/250/125

output tubes and a regulated power supply.

ROBERT B. DUNHAM



Capacitors

(Continued from page 5)

We have mentioned dielectric constant, and this can be considered to be the third determining factor of capacitance. Specifically the derivation of this factor lies in the nature of the material that is used as a dieelectric, and the dielectric constant can be stated as the ratio between the capacity of a capacitor using a given material as the dielectric and the capacity of a capacitor of equal plate area but using air as a dielectric. The formula given for this is:

$$K = \frac{C_S}{C_a},$$

where

- C_{S} = the capacity with the material in question,
- C_a = the capacity with air as a dielectric.



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We do not have to concern ourselves with this formula other than to know what is meant when we refer to dielectric constant. We should know that this constant is a variable which depends upon the composition and purity of the material used, that it is affected somewhat by temperature, and that it will vary to a certain extent with the frequency of the applied voltage. A table of constants of dielectric strength for the most commonly used materials can be found in almost any of the electrical engineering handbooks, should this information be desired.

TYPES

All capacitors are roughly classfied as to whether they have a fixed or variable value. These terms are self-explanatory; but if we want to give a more definite explanation, we can define a fixed capacitor as one in which the plates are permanently positioned in relation to each other and in which the capacity remains constant. If the plates can be moved relative to one another or if the dielectric can be displaced to change the capacitance, then the capacitor is said to be variable.

Capacitors are also designated according to the dielectric that is used. For this reason we have capacitors which are known as mica, ceramic, and paper capacitors. If we investigate further, we find that the mica capacitors have metal-foil plates separated by thin sheets of mica insulation. For silvered mica capacitors, the metal-foil is eliminated and a silver coating is deposited directly on opposite sides of the mica sheets to serve as electrodes. Almost without exception, this type of capacitor is enclosed in a molded-bakelite cover as protection against dirt and moisture.

The insulation between the plates of a ceramic capacitor is composed of a special ceramic material. The procedure is to mold this material into a thin rectangular wafer, a cylinder, or a disc and bake until it becomes very hard. Each side is then coated with a thin film of silver, and these sides act as the plates. Leads are soldered to crimped-on end terminals or directly to the silver, and the entire unit is covered with an insulating covering.

Paper capacitors are the most common of all the capacitor types. They are constructed with thin strips of metal foil as plates and use one or more thicknesses of wax-impregnated paper as insulation. A foil strip is placed between two paper strips, and the combination is then wound into a

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tight roll in order to occupy a minimum amount of space. This roll is then inserted in a tubular cardboard or metal container. In some cases, the capacitor is enclosed in a housing of molded plastic.

The capacity of paper capacitors can be increased in several different ways. The foil area can be increased by widening or lengthening the roll with a corresponding increase in overall size, or a thinner paper insulation can be used. When the thickness of the insulation is decreased, the capacitor will break down more easily; consequently, this method of increasing capacity is limited to the lower voltage ratings.

Paper capacitors are also made with a metallic film deposited on one side of each paper strip so that the films on alternate strips act as the electrodes. This type is referred to as a metalized-paper capacitor and has the advantage of being somewhat self-healing although, as will be seen later, it is inferior to the electrolytic capacitor in this respect. Self-healing is possible because the thin metalized coating burns away when a short occurs, leaving in the electrode a bare spot which tends to isolate the flow of current. Fig. 2 is a photograph showing examples of the capacitor types that have just been discussed.

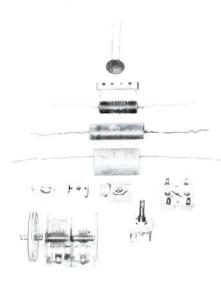


Fig. 2. Common Types of Capacitors.

ELECTROLYTIC CAPACITORS

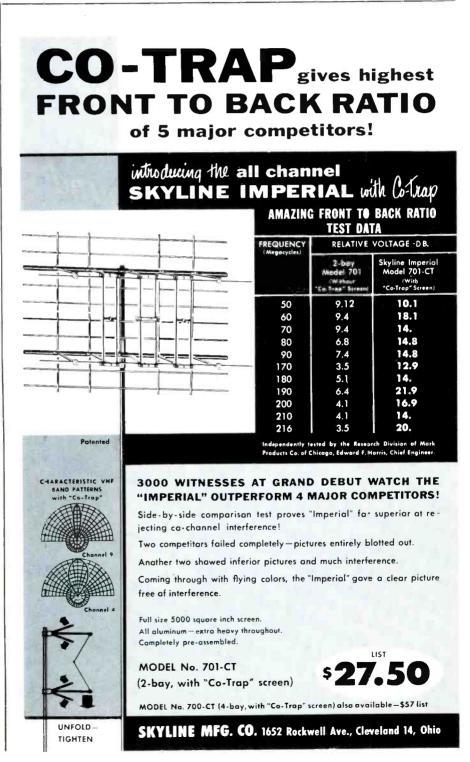
The component parts of an electrolytic capacitor are essentially the same as those in any capacitor. It has electrodes and a dielectir c medium between them. It also performs the basic function of storing and releasing static electricity. Electrolytic capacitors do possess some functional and structural differences which warrant placing them in a class of their own.

January, 1955 - PF REPORTER

We have said that when mica is used as a dielectric, the capacitor is known as a mica capacitor; when ceramic is used, it is called a ceramic capacitor, and when paper is used as a dielectric, we refer to it as a paper capacitor. This terminology would lead us to believe that in an electrolytic capacitor, the electrolyte is the dielectric. Such is not the case. Actually, the electrolyte in an electrolytic capacitor serves as an ionconducting medium and as one of the electrodes. The dielectric material or medium is an extremely thin oxide film which is deposited on the anode or positive plate.

Oxide Film

The exact nature and composition of the film which forms the dielectric are not too well-known; but this is not too important, since the formation and action of this film are understood and can be explained in rather simpleterms. One characteristic of aluminum and a few other metals is that they will acquire a nonconducting film of metallic oxide



when they are inserted into an electrolyte and when current is caused to flow from the electrolyte to the metal. This film will oppose the flow of current. If two pieces of aluminum are inserted into the proper electrolyte and if a difference of potential is applied between them, a high current will flow at the instant that the voltage is applied. If the voltage is left on, the current will gradually taper off until little or no current is flowing in the circuit. This process is known as "forming," and the action takes place while the film is being established on the plate to which the

positive potential is connected. The film that is formed retards the flow of current in one direction only. If the polarity of the applied voltage is reversed, high current will again flow. From this, we can see that the film acts as an insulation only as long as the polarity of the forming voltage is maintained. This is the reason that, with most of the electrolytic capacitors we use, we must be careful to adhere to the proper polarity when connecting them into a circuit.

The dielectric constant of the film which is formed will vary with



the magnitude of the forming voltage. In other words, for a given plate area, a capacitor formed at a low voltage will have a higher capacity than one with the same plate area but formed at a higher voltage. It is easy to understand that the higher voltage will form a thicker film; and since capacity is inversely proportional to dielectric thickness, the capacitor that is formed at the highest voltage would have the lowest value of capacitance. There is, moreover, a limit to the voltage at which these capacitors can be formed without increasing the dielectric thickness to such a point that the principal advantage (large capacity) of the electrolytic type is lost. Thus, we seldom find electrolytic capacitors which operate above 600 volts; and when we desire to use them for higher voltage ratings, it is necessary to connect two or more units in series.

The electrolyte that is used determines another characteristic of the electrolytic capacitor, inasmuch as it governs the maximum voltage at which the film can be for med and maintained. This holds within a fairly rigid limit. If a potential of more than 300 volts is applied to a capacitor using an electrolyte rated at 300 volts, the film may be punctured and in severe instances permanently damaged. When the surge voltage of a capacitor is rated at 400 volts, this means that the maximum momentary voltage that can be applied without puncturing the dielectric film is 400 volts.

Leakage Current

There will be small imperfections in any of the oxide films; and because of this, there will be a small amount of current flowing at all times. This is referred to as "leakage current." For a good quality electrolytic, it is very small, probably some fraction of one milliampere. The exact value of the leakage is determined by the condition of the film on the plate and the length of time that the capacitor has been without a polarizing voltage. Because the film tends to deteriorate when the capacitor is not used, a certain amount of time is required to form the film again after the capacitor has been stored or left idle. This will also apply to a new unit that has never been used. As an illustration, leakage current was taken on a new 40mfd, 250-volt capacitor that had been in stock for an undetermined length of time. A potential of 250 volts DC was applied to this capacitor, and the leakage current was recorded for the length of time necessary for the current to level off and reach a normal

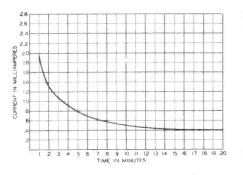


Fig. 3. Graph of Leakage Current Versus Re-Forming Time for a New 40-Mfd, 250-Volt DC Capacitor.

value. The leakage current versus time is shown in the graph of Fig. 3.

After a capacitor is put into use and the necessary time has elapsed, the leakage current will remain fairly constant unless the applied voltage exceeds the forming voltage. When the forming voltage is exceeded; the leakage current will exhibit a sudden and great rise in value. The exact amount of the forming voltage is seldom known, but it is safe to assume that it will be at some value slightly above the rated maximum voltage of the capacitor. In order to see just how sharp this rise of current could be, another series of tests were made. The same 40-mfd, 250-volt capacitor was used; but in this case, the test started with 100 volts of applied volt age and the potential was gradually increased to a value of 350 volts. The leakage current was recorded for each step of the increase. If the resultant graph shown in Fig. 4 is analyzed, it can be seen that the current remained practically constant over the range from 100 to 200 volts. Between 200 and 240 volts, there was an increase from .1 to .3 ma; but from 240 to 350 volts, the leakage current jumped from .3 ma to 6 ma, or an increase of 2,000 per cent. A close examination of the graph will show that the current began a really notice-

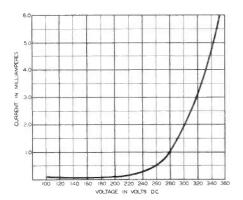


Fig. 4. Graph of Leakage Current Versus Applied Voltage for a New 40-Mfd, 250-Volt DC Capacitor.

able rise at 250 volts, which was the voltage rating of the capacitor. All of this shows that it is necessary to keep the applied voltage at or below, preferably below, the rating of the capacitor. If a capacitor is operated above it's voltage rating, the life of the unit will be materially reduced.

Construction

In the physical construction of an electrolytic capacitor, the true cathode is the electrolyte; the oxide film is the dielectric; and the anode or second electrode is the metallic member on which the film is formed. A second metallic plate is required in order to establish a good electrical contact with the electrolyte. In practice this is called the cathode, although it serves primarily to distribute the current into the electrolyte. For the purpose of explanation, we will follow this accepted terminology and refer to the second plate as the cathode. Almost without exception, the anode is constructed of aluminum; and in most cases the cathode is also, although the aluminum used in the cathode construction is usually a cheaper grade. In some instances, such as in the wet electrolytic capacitor where the can serves as the cathode, an aluminum-plated or a copper can may be found.

The electrolyte that is used in electrolytic capacitors can be either in a liquid or paste form. If it is a liquid, the capacitor is a wet electrolytic capacitor. If the electrolyte is a paste pressed into paper, gauze, or other absorbent material, then it is a dry electrolytic capacitor. Both of these capacitors operate in a similar manner, and each possesses certain advantages. The dry electrolytic capacitor will not spill nor leak and may be mounted in any position and in any type of container; whereas, with the wet capacitor, there is always a possibility of leakage resulting in a partial or complete loss of the electrolyte. In a dry electrolytic capacitor, the electrolyte offers a high resistivity which makes it simple and easy to mount more than one capacitor in one container in order to conserve space. With wet capacitors, the possibility of stray currents through the low-resistance electrolyte makes much more difficult the mounting of several sections in one container, especially if we desire a considerable potential difference between them. As a rule, the leakage current of a wet electrolytic capacitor is greater than that of the dry type, but it will have better self-healing properties.

Fig. 5 is a diagram which shows the basic components of the polarized electrolytic capacitor. As is shown in the diagram, this type of capacitor has



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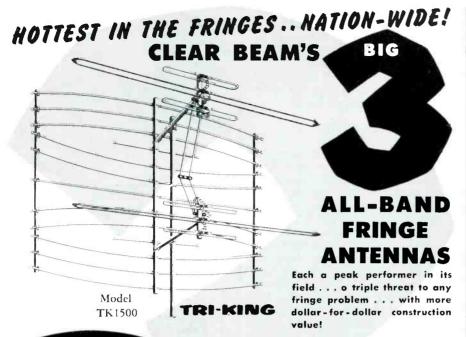
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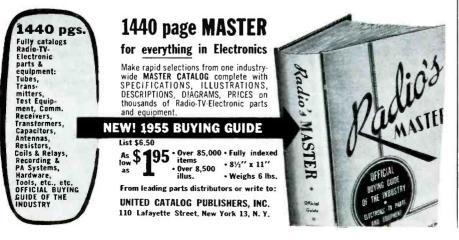
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an insulating film deposited on only one of the electrodes so that the current is restricted in one direction only. Most of the capacitors in use will be of this type. However, there

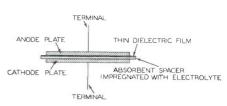


Fig. 5. Component Parts of a Polarized Dry-Electrolytic Capacitor.

are cases in which nonpolarized AC electrolytic capacitors are used, mostly for rather special applications such as the starting capacitor for a capacitor-start motor. Since, in all probability, a large number of this type will not be encountered, few details will be necessary regarding its construction and characteristics. The major difference between this capacitor and the polarized electrolytic is in the electrodes, both of which are provided with dielectric films. The film on each electrode is effective only during the half cycle when the electrode is positive. During the negative half of the cycle, the dielectric properties are reduced to a small value

Advantages

There are several inherent advantages, along with some severe disadvantages, of the electrolytic capacitor over the nonelectrolytic type. Foremost among the advantages is the large value of capacity that can be provided by an electrolytic capacitor of a given physical size. This is. possible because the thickness of the dielectric is not limited as it is in the other types. As has been pointed out, the capacity of a capacitor is dependent upon the area of the plates and upon the dielectric constant of the dielectric used; and it will increase with a decrease of the dielectric thickness. With the nonelectrolytic capacitor, this dielectric thickness is the governing factor which limits the capacity that can be obtained without increasing the plate area so much that the finished capacitor is too large for practical use. For example, ina paper capacitor, it is difficult to make insulating paper thinner than 0.0003 inch; hence, it is the usual procedure for the manufacturer to use at least two sheets of insulation in order to avoid shorts that are caused by un avoidable pinholes and to conductive particles in the paper. Even if a chance were taken and only one layer of paper were placed between the foils of a capacitor, thus limiting it to low voltage use, the absolute minimum spacing would be 0.0003 inch. This

would set the limit to the capacitance per unit area for this type of dielectric, no matter how low the voltage rating of the unit.

With an electrolytic capacitor, this limit does not apply. The dielectric film is formed electrochemically on the electrode, and its thickness can be controlled down to less than one-millionth of an inch. Since the forming voltage controls the dielectric thickness, a variation of this voltage will produce capacitors with wide capacitance and voltage ratings; and all of these capacitors could be housed in cans of the same dimensions. The enormous difference in capacitance between electrolytic and nonelectrolytic capacitors can be seen when we consider that an electrolytic capacitors can be seen when we consider that an electrolytic capacitor designed for use in a unidirectional circuit and rated as 2,000 mfd at 5 to 10 volts can be housed in a container of approximately 5 cubic inches; whereas, a nonelectrolytic capacitor of the same voltage rating and occupy ing the same space will have a capacitance of only a few microfarads.

We have already mentioned that certain types of paper capacitors are self-healing, within limits. We have also seen that the dielectric film of an electrolytic capacitor is formed by a chemical action on the plate when voltage is applied and current flows. This forming action of electrolytic capacitors makes them far superior inself-healing properties to any of the nonelectrolytic capacitors, since they will tend to heal themselves by reforming the film as long as there is a direct-current voltage applied. This does not mean that these capacitors cannot be permanently damaged. If the electrolyte-impregnated material of the dry electrolytic capacitor is repeatedly punctured, it will lose its insulation qualities and a continuous short results. However, the wet electrolytic capacitor with its liquid electrolyte will practically always heal itself after a brief surge of current or a momentary overload.

Disadvantages

To offset these advantages, several disadvantages are apparent in an electrolytic capacitor. We have already shown that the leakage current in this type of capacitor is great, much more than with the nonelectrolytic type. This is equivalent to saying that the insulation resistance per microfarad is less. We know that the insulation resistance for a nonelectrolytic capacitor may be hundreds, even thousands of megohms per microfarad; whereas, in an electrolytic capacitor, this resistance usually amounts to only a few megohms. Because of this, the loss due to power factor in the former type is much less than it is in the electrolytic capacitor. For example, the power factor of a waxed-paper capacitor is usually less than one per cent, while it is several per cent for the best electrolytic capacitor and may even run as high as 10 per cent.

In addition, the temperature characteristics of the electrolytic capacitor are inferior to those of any of the other types; since the capaci tance, power factor, and leakage current are all affected by temperature. At very low temperatures, the capacitance may be reduced to a fraction of its normal value; and at high temperatures, the leakage current is so great that it may lead to complete failure of the unit. The wet electrolytic capacitor will become inoperative if the electrolyte freezes, although it will return to a near normal condition after it has regained its normal temperature.

The application possibilities of electrolytic capacitors are especially limited because of their low power factor. The low power factor of the capacitor causes a high I²R loss within the capacitor. Whenever power is dissipated in this manner, heat will be generated and will cause a weakening of the dielectric. The leakage current will increase because of the loss of dielectric, and more heat will be generated. This cycle of events is cumulative and can lead to an eventual failure of the unit. For this reason, the use of electrolytic capacitors should be avoided where ambient temperatures are excessive or the alternating-current component is high. The latter condition is apt to generate more heat than is permissible. As a general rule, if a nonpolarized electrolytic capacitor is used with pure alternating current, the operation should be limited to intermittent service in order to allow for cooling between cycles.

Service and Testing

Almost all of the electrolytic capacitors that service technicians will encounter will be of the pelarized or unidirectional type. With few exceptions, they will be dry electrolytic capacitors and may be either the multiple- or single-section, metalcan type or the tubular, paper type.

Occasionally, it will be necessary to replace an upright can type, which is mounted on the top of the chassis, with a tubular capacitor that must be attached to the underneath

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side of the equipment. This usually happens because the technician does not have an identical replacement unit and does not want to wait while ordering one. Whatever the reason, when the occasion does arise we should remember that electrolytic capacitors are sensitive to heat; and care should be taken to make sure that the replacement is mounted in as cool a place as it is possible to find. Avoid placing these capacitors near voltagedropping resistors, voltage-dividing networks, and other parts which emit considerable heat. Because of its metal housing, the can type of unit will dissipate more heat than will the tubular capacitor. Should these units be operated at excessive temperatures. their life will be shortened, regardless of capacity and voltage ratings.

Because of their high leakage current and high capacitance values. electrolytic capacitors are not so easily tested for faulty operation as are some of the other types of capacitors. While an ohmmeter check will show when a capacitor is shorted, excessive leakage current cannot be determined with this method. Probably the best test for these units is to replace them in the circuit with capacitors of equal or slightly greater values. In order to save time on this operation, some service technicians prefer to have units equipped with alligator clips for this purpose. Then it is a simple matter to disconnect one lead of the suspected capacitor and clip the replacement into the circuit. An adequate selection of capacitors for testing purposes would probably include those with an 80-mfd, 150-volt; a 50-mfd, 150-volt; a 20mfd, 450-volt; and a 10-mfd, 450volt rating. If these capacitors are equipped with clips and kept on hand, it is possible to check quickly and accurately by substitution practically all of the electrolytic capacitors in use. These test capacitors should be replaced periodically with fresh capacitors, lest they lose too much of the oxide film and develop excessive leakage current. Another solution would be to place them periodically across a direct-current voltage for periods of 10 or 15 minutes.

The information herein given has been more or less general in nature. However, it is hoped that it will give the service technician a better understanding of capacitors, particularly electrolytic capacitors and their limitations and applications.

JAMES M. FOY

Examining Design Features

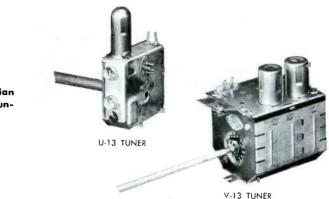
(Continued from page 21)

balanced ratio detector is coupled to the grid of the 6AU6 audio amplifier. Feedback from the output stage is applied to the cathode of the first audio amplifier. Amplification in the audio output stage is accomplished by a 6AR5 or a 6AQ5 tube.

AGC

A system of keyed AGC is used in this receiver. The keyer tube is a 6AU6. The signal from the plate circuit of the first video amplifier is applied to the grid of the keyer by DC coupling; consequently, B+ voltage will be present on this grid. In order to reduce the potential existing between the grid and cathode of the keyer, the cathode is returned to a source of B+. The AGC voltage is developed and filtered in the conventional manner and is then applied to the first and second IF amplifiers. AGC for the tuner is delayed by application of a positive potential. A clamper is employed to prevent the AGC voltage to the tuner from becoming positive.

Fig. 3. Sarkes Tarzian U-13 and V-13 Tuners.



Sync

A composite signal from the output of the first video amplifier is fed to the 6AU6 sync separator. The output signal resulting from the action of the sync separator is coupled to the 6C4 phase inverter. The inverter stage provides sync signals of opposite polarities for use in the sweep systems. One signal is taken from the cathode circuit and fed to the vertical-sweep section. Since two signals of opposite polarity are required in the horizontal section, one signal is taken from the cathode circuit of the 6C4 and one is taken from the plate circuit.

Vertical Sweep

The sync signal from the phase inverter is fed through an integrator network before application to the vertical multivibrator. The cathodecoupled multivibrator circuitry employs a 12AU7. Two controls are associated with this stage, namely, the height control and the verticalhold control. The vertical output tube is a 6W6GT with its cathode bias adjustable by means of the vertical-



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linearity control. A signal is taken from the vertical-output transformer and applied to the cathode of the picture tube to accomplish retrace blanking.

Horizontal Sweep

Two signals of opposite polarity are taken from the sync separator and applied to the horizontal-phase comparator. The two diode sections of a 6AL5 are used in this application. A signal from the horizontal-output stage is also applied to the 6AL5. The output of the phase comparator is applied to the horizontal multivibrator as a correction voltage. A 6SN7GT is used in the 'horizontal-multivibrator circuit. The output of this stage drives the 6AU5GT horizontaloutput tube. High-voltage rectification is obtained by the use of a 1B3GT. Damper action is furnished by a 6W4GT.

Power Supply

The power supply consists of a 5U4G rectifier connected in a conventional circuit. A series of dropping resistors are used to provide the outputs of 320, 250, and 150 volts. The power supply may be operated by a local or a remote switch. The remote switch actuates a 6-volt AC relay which connects the power line to the power-transformer primary. A separate transformer is used to supply the 6 volts for the relay. The use of 6 volts for the remote switch eliminates the need of running the line voltage to the remote switch.

SARKES TARZIAN TUNER UV-13

The Sarkes Tarzian Model UV-13 tuner is a combination of the V-13 VHF tuner and the U-13 UHF tuner. The two tuners shown in Fig. 3 are mounted coaxially and plug into each other. The tuners feature solderless pin connections for all leads in order to permit easy removal of the tuners from the receiver. Tuning of the UV-13 is accomplished by three concentric knobs. This arrangement eliminates the use of extraneous gears, pulleys, and dial cords. The combined UHF and VHF tuners from a unit comparable in size to con-

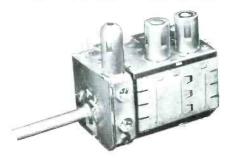


Fig. 4. Sarkes Tarzian UV-13 Tuner.

ventional VHF tuners. This is shown in Fig. 4. Another feature of this tuner is the simplicity with which the UHF tuner may be added in the field. NTERNATIONAL

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The V-13 is a switch type of tuner covering channels 2 through 13. The RF amplifier is a 6BZ7. The oscillator-mixer section employs a 6U8. The V-13 is designed for use with a 41-megacycle IF strip.

The U-13 is a continuous tuner covering channels 14 through 83. The oscillator employs a 6AF4. A crystal diode serves as a mixer. Tuning of the UHF circuits is through the use of capacitance-tuned resonant cavities.



Fig. 5. Setchell-Carlson Model 552 TV Receiver Showing Chassis Mounted Above the Picture Tube.

SETCHELL-CARLSON MODEL 552

Ease of servicing is reflected in the design of the Setchell-Carlson Model 552 television receiver. The receiver is constructed on small subchassis which are plugged into a base containing the interconnecting wiring. This is similar to the system employed in previous Setchell-Carlson receivers. A unique method has been employed for mounting the chassis in the cabinet. The chassis is mounted above the picture tube. The top of the cabinet is hinged so that it may be raised as shown in Fig. 5. When this is done, the top of the chassis is completely exposed to provide access to the plug-in subchassis and the tubes. This greatly facilitates removal and replacement of these items and should prove particularly beneficial for servicing in the customer's home.

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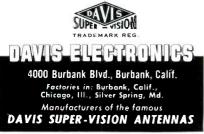
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IMMEDIATE DELIVERY



Shop Talk

(Continued from page 15)

unwary eye to indicate greater directivity.

That which is true of the forward lobe is just as true of the backward lobe. On a power curve, any lobes to the rear - representing the tendency of the antenna to pick up rear signals - will appear smaller than they would on a voltage plot. But since television receivers utilize the signal voltage rather than the

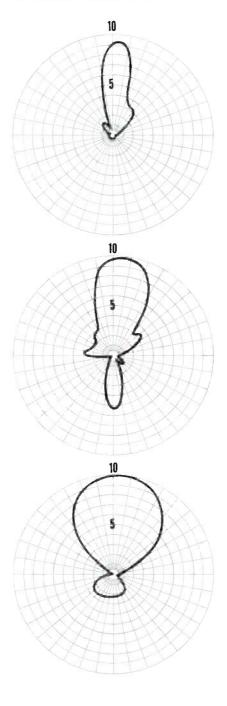


Fig. 2. Response Curves Which Are More Indicative of Actual Antenna Operation Than Those in Fig. 1.



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APPLICATIONS

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APPLICATIONS

APPLICATIONS • DYNAMIC CONVERGENCE—vertical and hori-zontal test and adjustment • DC CONVERGENCE —test and adjustment • DEFLECTION COIL— positioning for best convergence • BEAM MAGNETS—alignment for best convergence • DYNAMIC PHASE ADJUSTMENT—vertical and horizontal • FOCUS—test and adjustment of DC and dynamic focus • TROUBLESHOOTING of all circuits affecting convergence • LINEARITY —test and adjustment of horizontal and vertical sweep linearity sweep linearity



signal power, it is the voltage curve with which we are concerned.

In view of the foregoing discussion, it can be appreciated why most antenna manufacturers present their polar response curves in power form unless otherwise indicated. There is, of course, nothing harmful in this practice; but too often the service technician who is unaware of the differences between voltage and power curves is misled.

While we are on the subject of antennas, it might not be amiss to consider them in the light of color television. As most readers of the PF REPORTER know, the color portion of the signal resides principally at the upper end of the channel bandpass. In addition to the color sidebands, there is also the color-subcarrier burst which can be considered even more important than the sidebands. Whereas it is possible to lose some but not all of the color in a picture when portions of the sidebands are lost, it is impossible to develop and maintain a suitable color picture when the color burst is lost. The NTSC color system is based on the arbitrary use of a color reference signal which is called the color burst. This burst may be considered the "key" which unlocks the information contained in the chrominance signal. Once the key is lost, automatic color synchronization in the receiver becomes impossible. It is thus of the utmost importance that the key be retained.

Let us see what difficulties the antenna may present in this respect. The amount of signal which an antenna develops at any one frequency not only depends upon the direction in which the antenna is pointing but also upon the gain of the antenna at that frequency.

Typical gain curves versus frequency for a widely used VHF antenna are shown in Fig. 3. Both the high and low bands are included; and as we examine these curves, we see that there is a considerable variation in gain, particularly across the low band. Notable in this respect are channels 2, 5, and 6. On the high band, gain is fairly uniform with the principal exception of channel 13.

For most uniform results in color reception, the gain curve should be as flat as possible. Desirable limits of variation should not exceed 10 per cent or 1 db. With this in mind, let us return to the curves of Fig. 3. Channels 3 and 4 conform very nicely because the gain varies less then 1 db from one end of the channel to the other. On channels

5 and 6, there is almost a 2 1/2-db or 3-db variation from end to end of each channel; and furthermore, the high end of the band where the color information is contained receives the least amount of gain. This would work to the detriment of the color signal; and it is entirely possible that although black-and-white reception would be enjoyable, color would not. This condition could be further aggravated by additional attenuation in the antenna system or the receiver. One reduction by itself, unless excessive, will seldom prove fatal; but the combined effects of several could.

The situation on channel 2, where there is a 2-db variation, is still not so bad as it is for channels 5 and 6. For one thing, the color signal is on the rising side of the curve. Secondly, the curve tends to flatten out somewhat near the high end of the channel, and this is also desirable. Hence, one would expect to obtain good color reception on channel 2, all other factors being equal.

On channel 13, there is an intermediate situation which approaches that of channel 6. The high end of the band is down, but the drop is not excessive.

It is needless to say that yagis and other high-gain, sharply directional arrays are especially critical in regard to color reception. Substantial attenuation of the high video frequencies may pass unnoticed on a black-and-white set; but since these high frequencies carry color information during color transmission, loss of color may occur in a color receiver.

The antenna is not the only component in the antenna system. Present, too, are RF boosters and dis-

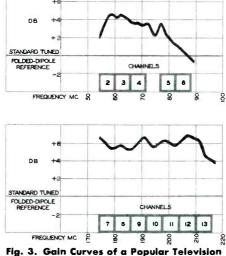


Fig. 3. Gain Curves of a Popular Television Antenna.

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tribution amplifiers. Any attenuation inflicted by these items will add to antenna loss, and the total may suppress the color signal below the point of usability. Particular caution will have to be observed in tuning RF boosters. If the passband of a booster is too narrow, the booster will have to be replaced with one possessing a wider-channel response. This situation has already been encountered in apartment-house distribution systems.

Contrary to the idea expressed in some ads which have appeared in technical magazines, our belief is that an antenna by itself cannot be responsible for the loss of color. The trend in recent years has been toward use of antennas with characteristics that have been fairly uniform over individual channels. High gain achieved at the expense of bandwidth has been made more or less unnecessary by the increase in broadcast power and the marked improvement in receiver sensitivity. Hence, the antenna might be a contributing factor to color deficiency, but it is seldom the sole factor. This means that a technician, answering a complaint of no color, will have to possess some means of checking over-all color performance of the set. One approach to this problem is by means of a color-bar generator. This can be connected to the set; and if a full color picture is not obtained, it can be presumed that the set is not func tioning normally. Trouble is then indicated in the set, and it is probable that the antenna system is not at fault. In the absence of this information, it could very well be that the service technician will needlessly attempt repairs to the antenna before he discovers his error.

REVIEW

The trend toward the use of more completely automatic machinery in the fabrication of electronic devices has spread from radio sets totelevision receivers. In Admiral's latest black-and-white television sets, fully half of the tubes operate in printed circuits which were partially or fully constructed without the assistance of human hands. When a trend is thus so firmly established and shows every indication of gather ing even greater acceptance than it has at present, then it is time for the technicianto become as familiar with the techniques of servicing these circuits as he is with the systems which have been used up to the present time.

Admiral has recently released a 6-page manual, No. S559, which is entitled '' Printed Circuits — Service and Repair.'' In it, the technician will find full servicing instructions



not only for Admiral printed circuits but for many other printed circuits wherever found. In this review, we will attempt to cover the highlights of the practices outlined in this publication.

The first item of interest to the technician is, ''What tools will I need specifically for printed circuits?'' In the manual, eight items are listed. These are:

1. Low-wattage soldering iron with a small point or wedge. (The rating of the iron should not exceed 35 watts.)

2. Small wire brush, such as a suede shoe brush.

3. Low-temperature 60/40solder with a rosin core. (This is made with 60 per cent tin and 40 per cent lead. Ordinary solder is 40 per cent tin and 60 per cent lead. The latter is not recommended.)

4. Diagonal wire cutters and long-nosed pliers.

5. Thin-bladed knife.

6. Small wire pick or soldering .

7. Clear lacquer and brush or Krylon acrylic spray.

8. A solvent (such as Xylene, lacquer thinner, or denatured alcohol) for silicone resin.

The reason for some of the special tools can be found in the precautions which should be observed when servicing. For example, overheating should be avoided because it can cause the bond between the laminated plastic board and the copper foil to break. The copper foil represents the wires of the circuit, and any break in foil continuity will have the same effect circuit-wise as a severed conductor. If soldering becomes necessary, it should be done carefully; and any excess solder should be brushed away with the small wire brush.

Items 4, 5, and 6 in the foregoing list are designed to help in the removal of circuit components such as resistors, capacitors, coils, and transformers. One of the features of printed circuits is compactness, and sharp-edged tools make the job of repair that much easier.

After a solder connection has been made, a coat of lacquer or Krylon should be applied over the area to prevent dust or moisture from causing short circuits. Initially, when the chassis was constructed, it received



'America's Most Complete Wire Line"

USING DIAGONAL WIRE CUTTERS AS SHOWN, CUT LEAD AS CLOSE AS POSSIBLE TO DEFECTIVE COMPONENT

Fig. 4. Cutting a Defective Resistor Free of the Printed-Circuit Board. (Courtesy of Admiral Corp.)

a coat of silicone resin as a protective coating. In repair, the resin must be removed and then subsequently replaced with a coat of lacquer or Krylon. If the Krylon spray is used, it will be necessary to cover the tops of the tube sockets and the ground connections of the chassis with masking tape to prevent the contact surfaces from becoming coated.

Note that because of the protec tive coating, a probe with a needle point should be used for circuit checking. The varnish coating must be penetrated to make the desired contact.

The major portion of the manual is devoted to specific instructions for replacing various components. The most important features will be summarized to indicate the best procedure to follow.

1. Capacitors, Resistors, Couplates, and Peaking Coils.

In the replacement of component parts, it is desirable not to have to unsolder the component leads where they make connection to the printed wiring. Toward this end, if the leads from the defective part are long enough, cut the leads where they enter the component. See Fig. 4. Clean off the ends of the remaining leads. Then make a small loop in each lead of the replacement component and slide the loops over the remaining leads of the part removed. Finally, make a secure solder connection using as little solder and as little heat as possible. Too much heat may cause the original lead to fall out of the board and complicate the replacement job.

If the original component does not present sufficient lead length, then

it is suggested that the defective part be cut in half. Then cut through each half of the unit until it is broken away from its lead. See Figs. 5 and 6. By performing this procedure carefully, enough extra lead (inside the component) will be gained to permit a secure connection to the replacement part.

The remaining alternative is used when the part is so mounted that neither of the foregoing methods can be employed. Then it becomes necessary to unsolder the defective unit and the following shows the best way to accomplish this.

Heat the connection on the wiring side of the board with the small soldering iron. Brush away the solder



Fig. 5. Cutting a Defective Resistor Apart. (Courtesy of Admiral Corp.)

when it becomes melted. See Fig. 7. Then insert a knife blade between the wiring foil and the bent-over component lead and bend up the lead. Apply the iron again, and wiggle the compo-



Fig. 6. Removing Resistor From Leads. (Courtesy of Admiral Corp.)

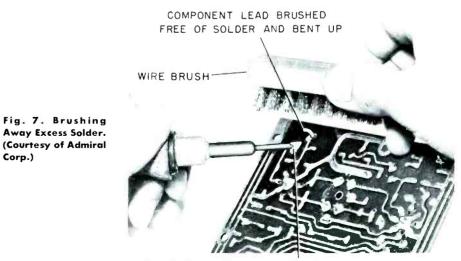
nent until the lead can be pulled back through the chassis board. Remove any small particles of solder imbedded in the silicone resin by using a clean cloth dipped in solvent.

The replacement part is next placed in position, and its leads are passed through the same holes used by the original part. If a thin film of solder remains over the hole, heat the area; and then push through the leads from the replacement unit.

Cut off any excess lead length, and then bend the remaining lead ends over the copper foil. Solder carefully using the low-temperature 60/40 solder. Finally, cover with a coat of lacquer.

2. Coil Replacement.

The removal of one coil and the substitution of another does not present any unusual problems because



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MDDEL No.	TYPE	LIST Price	OUTPUT Level	MIN. NEEDLE FDRCE	RESPONSE TO	NET WT.	SHURE NEEDLE ND.
W78‡	Crystal	\$5.55	4.0V or 2.0V	1 oz.	6,000 c.p.s.	Dual-Weight 25 grams or 12 grams	None

Dual-Weight, Dual-Volt Cartridge. Has weight slug secured by shrink-on band. With lead weight, net weight of curridge is 25 grams. If 12 gram weight is desired, the shrink-on band can be cut off and the lead weight removed. In addition Model W78 has capacitor, furnished as accessory. Without capacitor output is 4.0 volts; with capacitor output is 2.0 volts.

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Admiral does not bend over the terminal lugs of these components against the foil. Thus, heat the coil lugs, one at a time, and gently wiggle the coil back and forth until the unit can be pulled free of the board. Then the replacement is inserted and its terminal lugs resoldered in position. All excess solder should be brushed away.

3. Tube Sockets.

A tube socket is a component which requires a major operation for removal, and accordingly considerable space is devoted to it in the Admiral service manual. The exact approach is governed by the particular placement of the socket — whether it is mounted on the wiring side or on the component side of the board. In either instance, the general approach is as follows.

First, break all connections to each of the socket lugs by carefully heating each in turn, and then brush away all excess solder. A knife blade will assist in separating leads from lugs where these are physically joined together.

The same treatment is accorded grounding lugs, if these are present and used. (The tube sockets are of the miniature type with an additional grounding lug extending to the tubular center shield at the bottom of the socket.) The grounding lug is generally the last item to be unsoldered; and as the heat melts the solder, the socket is gently lifted away from the board. Then the area left by the socket is cleaned free of solder particles, and the replacement socket is carefully placed in position. Its lugs are then bent over and soldered.

On some boards, the sockets are mounted upright on the wiring side; consequently, tube-pin numbers must be counted in a counterclockwise di rection. The clockwise direction is the usual practice when the socket is viewed from the bottom.

By now, the major aspects of working with printed circuits should be quite evident to the reader. Work carefully using as little heat as possible, remove all excess solder quickly and completely, and use new solder as sparingly as if it were rationed. Never use too large an iron.

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Quicker Servicing

(Continued from page 29)

tube caddy by some service technicians, these items could very well be carried in the service truck; and the space in the tube caddy could be filled with parts and tools that are more frequently used.

For maximum convenience and portability, most of the listed parts

TABLE I

EQUIPMENT AND PARTS FOR SERVICE TRUCKS USED ONLY IN TV AND RADIO SERVICE CALLS

Equipment

- 1. VOM.
- $2. \ {\tt Cross-hatch\,linearity\,generator}.$
- 3. Tube checker, if desired.
- Five-inch TV-receiver check tube 5AXP4. (See ''A TV Receiver Check Tube,'' an article in this issue.)
- 5. Small hand drill and drill bits.
- 6. Extension leads for yoke, picture tube, high voltage, and other uses deemed necessary.
- 7. Solder gun and solder.

Parts and Materials

- 1. Seldom-used tubes that are not in the tube caddy and extras of the often-used tubes.
- 2. Selenium rectifiers: at least two of each of the 300-, 350-, and 400-ma sizes.*
- Negative-temperature-coefficient resistors. These have applica tions in the filament and B+ circuits in GE and other receivers.*
- 4. Crystal diodes, video-detector type.
- 5. Resistors: 1/2-, 1-, and 2-watt, assortments.
- 6. Capacitors:
 - a. Molded-plastic tubulars (MPT),600-voltassortment.
 - b. Disc-ceramic assortment.c. Mica and ceramic tubular
 - assortment, for critical sync and coupling applications.
 - d. Universal-mount type of high-voltage filter capacitors: 500 mmf, 20-30 kv.
- 7. High-voltage wire, tape, and spaghetti.
- 8. Replacement anode leads.
- 9. Krylon spray.
- 10. Assorted wire and spaghetti of the standard type.
- 11. Replacement AC interlocks.
- 12. Assorted screws and washers.
 - a. Sheet-metal, self-tapping screws.
 - b. Machine screws and nuts.
 - c. Flat and lock washers.

*PF REPORTER, July 1954, p. 23.

and equipment may be stored in a large additional caddy. A unit, similar to the one shown in Fig. 1, with several drawers and a removable side would probably be the best type for this application.

Small plastic containers or empty 35-mm film cannisters, such as those shown in Fig. 2, may be used to hold the small parts. These containers may be stored in the drawers of the caddy. The larger parts and

TABLE II

EXTRA EQUIPMENT AND PARTS FOR SERVICE TRUCKS USED IN MAKING ANTENNA SERVICE CALLS

Equipment

- 1. Portable field-strength meter (desirable especially for the oneman operation).
- 2. Sound-powered phone set.
- 3. Two or three-section extension ladder.
- 4. Large cutters and pliers to handle guy wires.
- Crimping tool for chimney straps.
 Device for measuring wire length
- (a small hand unit).
- A set of wrenches for work on antenna towers and rotators; 3/8-inch to 1-inch open-end or box-end type. (It may be advisable to have two of each of the 7/16-, 1/2-, 9/16-, and 3/4-inch sizes.)
- 8. Adjustable wrench for odd-sized nuts and bolts.
- 9. Light oil for rotator motor bearings.
- 10. Lubriplate for rotator gears and thrust-bearing assemblies.
- 11. Mineral-spirit solvent to clean rotators.
- 12. Pan to hold solvent for cleaning parts.
- 13. Brush for cleaning.
- 14. Aluminum paint.
- 15. Paint brush.
- 16. Rags for wiping.

Parts and Materials

- 1. Antenna lead-in wire.
- 2. Guy wire.
- 3. Rotator-control wire with 4 and 8 conductors.
- 4. Chimney mount and universal mount.
- Assorted hardware such as guywire eyes; screw eyes; turn buckles; guy rings; and assorted nuts, bolts, and washers.
- 6. Antenna masts: 5- and 10-foot sections.
- 7. Replacement elements for conical antennas.
- 8. Ground wire and ground rods.
- 9. Lightning arrestors.
- 10. Standoff insulators.



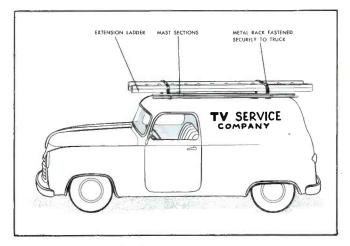


Fig. 3. Top Carrier for Service Truck.

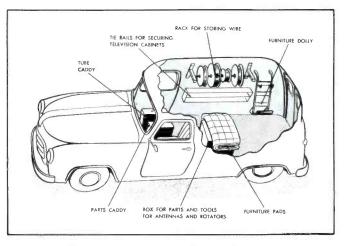


Fig. 4. Inside Layout of Service Truck.

tubes may be stored in the open-shelf compartment below the drawers.

To insure that the parts caddy is always fully stocked, the parts that are taken out should be replaced each day. The parts lists on the service tickets may be used for this purpose. An inventory of the parts caddy should also be made weekly since there may have been occasions when replacement parts were not available on the day they should have been restocked. A weekly inventory before going to your distributor will insure that the parts caddy will be kept completely equipped.

For Antenna Service

The shops which service and install antennas and rotators as well as television and radio sets will find it helpful to outfit the service truck or trucks so that any type of call can be completed without having to use haste in assembling the ladders, wire, hardware, and equipment needed for the installation or repair of antennas. The equipment and materials which will, for the most part, be satisfactory for making service calls for antenna and rotator repairs are presented in Table II.



Although there are numerous items of equipment and material, most of them are not bulky; and if they are properly stored, they will actually occupy only a small part of the area in a service truck. The extension ladder and mast sections of antennas may be carried on a suitable rack which can be fastened to the top of the service truck. See Fig. 3. The balance of the tools and materials may be stored on the inside of the service truck.

A rack for spools of antenna wire, rotator wire, guy wire, and any other type of wire needed can be constructed. By using large washers and lengths of garden hose between each wire spool, a minimum of noise will be generated by rattling of the wire reels or spools during transit.

By combining the equipment and material given in the two foregoing lists, a service organization can equip a service truck for complete service.

To assist service technicians and organizations in equipping a service vehicle, a sample layout of the inside of a fully equipped service truck is shown in Fig. 4. This layout should prove to be very effective, but many variations which would work equally as well are possible. Therefore, this layout is intended only to serve as a guide and to give you ideas about equipping your present or proposed service truck.

As mentioned before, a properly equipped service truck is a very valuable part of the service organization and can do much toward reducing your operating costs and increasing customer satisfaction with on-the-spot service.

IN THE SHOP

Since high-fidelity audio systems have gained so much popularity

PF REPORTER - January, 1955

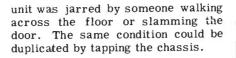
recently, many new models of AM-FM tuners and audio amplifiers are being produced. These employ circuits that are more complicated than those found in the average five- or six-tube AC-DC receivers. Examples of such circuits are: special phase inverters, feedback circuits, and tone-control systems. A technician not accustomed to working with these circuits may run into some difficulties. For that reason, it was considered a good idea to point out some of the possible troubles which may and occasionally do occur. These troubles will be covered in much the same manner as the troubles in television receivers were covered previously in this column.

First of all, it may be well to point out one very important aspect connected with the servicing of highfidelity equipment. The technician should learn to be very critical of the quality of performance of such equipment. If his ear is not able to detect slight distortions in the output signal. he should use test equipment which will detect distortions of this nature. An intermodulation meter, a squarewave generator, and an oscilloscope are instruments which can be very useful in the servicing of high-fidelity audio systems. If a shop does much work in this field, it would not take an instrument such as an intermodulation meter long to pay for itself.

The following four problems should serve as examples of the kinds of trouble which may be encountered in high-fidelity equipment. These particular problems could be found and corrected with ordinary test instruments. Problem No. 1 illustrates an intermittent condition of an unusual nature; problem No. 2 shows a case of trouble in the tuning-eye circuit; whereas, problems No. 3 and No. 4 have to do with tone-control difficulties.

Problem No. 1

The unit in question was an AM-FM tuner and amplifier. The complaint was that the sound quits momentarily, particularly when the



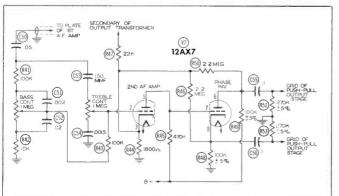
After the tubes had been checked and found to be in good condition, an insulated probing tool was used to move components in an effort to localize the source of trouble. If the sound could have been made to quit for a longer period, the technician would have been able to locate the trouble by signal tracing. Since this was not the case, however, he was obliged to use the probe.

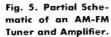
Note the partial schematic which is shown in Fig. 5. It was found that the movement of capacitor C50 caused the sound to quit; therefore, one end of the capacitor was disconnected, and a capacitor checker was used to check it. Tests showed that it was good even when moved about. The capacitor was then soldered back into the circuit so that further tests could be made.

One lead of an ohmmeter was placed at the junction of C50 and R41, and the other lead was connected to the chassis. The capacitor was moved again, and the meter suddenly dropped to a reading of zero. An examination of the circuit wiring did not disclose any short circuits between the leads from these components and the chassis.

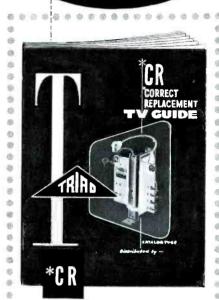
Once again, C50 was disconnected. This time it was removed from the circuit completely, and a through examination was made of the capacitor itself. The source of trouble was found to be a small piece of metal which projected through the coating at the outside edge of the capacitor. This had been intermittently touching the chassis and shorting the signal. A file was used to remove this piece of metal, and the set returned to normal operation.

Mention of this trouble has been made to point out that there can occur in these instruments the same odd defects that occur in television receivers. The problem emphasizes





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the importance of physical inspection as an early step in any troubleshooting procedure.

Problem No. 2

This trouble developed in an AM-FM tuner unit which employed a tuning-eye indicator. The circuit which was involved is shown in Fig. 6. The symptom was an absence of indications on the tuning eye during the reception of AM signals. The eye operated properly for FM reception. When the technician began checking the instrument, he noticed that there was also a loss of AVC action during AM reception.

The first step toward locating the trouble was to try substituting the 6U5 tuning eye. When this failed to help, a check of the operating voltages on the tube was made. The voltages on pins 2 and 4 were normal, but the grid voltage on pin 3 measured a negative 0.8 volts and did not change when the set was tuned through the AM band. Upon checking the circuit, it was found that the eye obtained its grid signal from the AVC line. The AVC voltage was checked, and it also remained steady when the set was tuned from station to station. In this manner, the trouble was localized to the AVC line

Tracing the circuit in Fig. 6, the technician saw that the AVC voltage during AM reception is obtained across the detector load resistor R35. The signal developed by this resistor is filtered by R54 and is fed to the IF tubes and to the grid of the tuning eye.

A check with a voltmeter showed that signal voltage was present across R35; therefore, the chief suspect was logically resistor R54. An ohmmeter measurement showed that R54 was open. Replacing this resistor returned the set to normal operation.

The significance of this problem is that it shows the value of step-bystep logical reasoning that is based upon a knowledge of circuit theory and operation and upon the wise use of test instruments.

Problem No. 3

The treble control in the amplifier under investigation did not seem to have as much effect over its entire range as it should. It reduced the high frequencies only slightly at its minimum setting. Normally, this control can cut out the high frequencies almost completely when it is turned all the way down. In the

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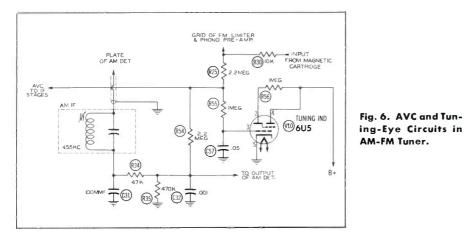
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amplifier shown in the schematic of Fig. 5, the tone-control circuit is a part of the input to the second audio amplifier. This circuit will be used as the reference in our discussion of this problem.

In checking the operation of the controls, the technician noticed that the bass control seemed to function properly. This fact indicated that the trouble must be somewhere in the treble-control portion of the tonecontrol network. The theory of operation of the treble control is given in the following paragraph.

The coupling capacitor C53, with a value of 150 micromicrofarads, offers a very low impedance to the higher audio frequencies. C54 has a value of .0015 microfarads and is also a low-impedance path for high frequencies. Hence, for these high audio frequencies, the bottom tap of the treble control is effectively at AC ground potential. The high frequencies are developed across the one-

megohm control and are tapped off as wanted.

The technician checked the control and the two capacitors individually, and he found that C54 was open. This condition accounted for the abnormal operation of the treble control. It can be seen that, without C54 in the circuit, the voltage-dividing property of the treble control is greatly lessened by the fact that resistors R43 and R42 improperly constitute a branch of the dividing network.

Problem No. 4

The schematic in Fig. 5 can be used to illustrate this problem. The symptom was that the bass control was acting abnormally. Instead of varying the bass response as it should, the bass control was changing the volume as if it were a volume control. The action of the treble control seemed normal, and so did that of the regular volume control

which is situated ahead of the first audio amplifier. This volume control is not shown in the schematic of Fig. 5. Trouble was indicated in the bass section of the tone-control circuit.

The action of the bass control can be explained as follows. Note the two capacitors C51 and C52 across the bass control. These capacitors offer a high impedance to the bass frequencies and a low impedance to the higher audio frequencies. The result is that the low bass tones are developed across the one-megohm control and are tapped off as desired. Because of the shunting effect of capacitors C51 and C52 at the middle and high frequencies, the load presented by the bass-control circuit at these frequencies should remain relatively constant despite changes in the setting of the control. In other words, when it is operating normally, the bass control should not act like a volume control.

When the individual components in the bass-control circuit were tested, C52 was found to be open. With this defect in the circuit, varying the bass control caused the portion of the control between the arm and the bottom tap to appear as a variable impedance at all frequencies. Hence, the bass control actually changed the volume level in the output.

This problem was an interesting one and was characteristic of the type of problem that may be encountered in the tone-control circuits of an amplifier.

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A TV-Receiver Check Tube

(Continued from page 17)

causes some difficulty in making voltage measurements at the tube bases. This is particularly true of the tubes mounted near the deflection yoke and those mounted underneath the picture tube. If the 17-inch tube is removed from the chassis and the 5AXP4 tube is substituted for it, all of the tube sockets are readily accessible. This is illustrated in Fig. 3, which shows the same chassis with the check tube mounted in position. Although it is possible to service the receiver with the picture tube removed from the chassis, certain symptoms which might be exhibited by the picture tube during the servic ing procedure would not be present with the tube removed. Since the small check tube does present a picture, any symptoms which are exhibited while making voltage measurements or performing waveform analysis might present information that would be useful in servicing the set.

Fig. 4 shows the tube being mounted in a TV chassis. The size of the tube can be noted by comparing it with the technician's hands. After

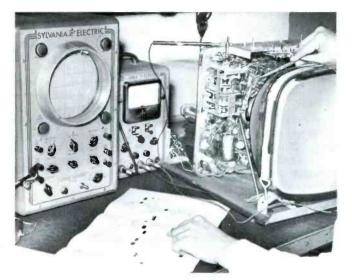


Fig. 2. Measuring Voltages on a Vertical-Chassis Receiver.

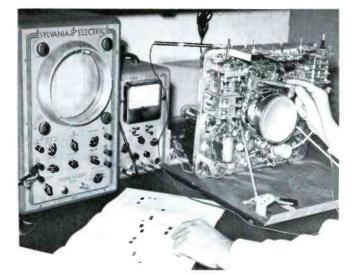


Fig. 3. TV-Receiver Check Tube Mounted in a Vertical-Chassis Receiver.



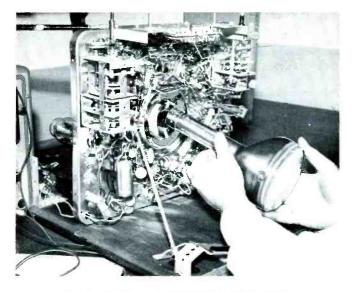


Fig. 4. Installing the 5AXP4 in a TV Receiver.

the tube is inserted in the yoke, several methods may be employed for holding it in position. Probably the simplest method involves the use of a centering-magnet assembly such as that employed on many picture tubes. The centering magnets are removed from the assembly so that they will not affect the operation of the tube. Fig. 5 shows such an assembly after the centering magnets have been removed. These assemblies are readily available at parts distributors.



Fig. 5. A Centering-Magnet Assembly With the Centering Magnets Removed.

and they work very satisfactorily in holding the 5AXP4 in position. To use this assembly, slide it over the neck of the tube after the tube has been inserted in the yoke and move the assembly forward on the neck of the tube until it comes in contact with either the chassis or the back of the yoke, whichever the case might be. Fig. 6 shows the assembly in position. There is sufficient tension to prevent the tube from sliding forward, and it is thus held in position.

The 5AXP4 can be mounted permanently in a box with a deflection yoke mounted on its neck for use as

a test assembly in the service shop. Such an assembly would be extremely helpful in shops that specialize in the servicing of a particular type of receiver. If such is the case, the voke leads can be extended and terminated with the proper plug so that it can be plugged into the receiver under test. It should be pointed out that such an arrangement would not be completely universal, since the variation in the inductances in the horizontal and vertical windings of the yoke vary considerably among receivers. One means of overcoming this would be to mount the tube permanently in a box so that the neck of the tube is free from any mounting brackets. The yoke of the receiver under test can then be quite easily slipped over the neck of the tube, and the servicing can be efficiently performed. Of course, it would be necessary to provide for extension of the high-voltage lead as well as the leads to the base of the tube, but this presents no great problem.

As was stated previously, the 5AXP4 is self-focusing and therefore does not require any external focus assembly. In those receivers which have the focus assembly mounted directly to the yoke in such a way that it cannot be removed, some defocusing of the picture will be experienced. It is usually not so severe, however, that it prevents satisfactory operation of the tube.

The characteristics and ratings of the 5AXP4 are such that it works equally well over a wide range of voltage inputs. This makes the tube a truly universal unit. The quality of picture which is obtainable through the use of a 5AXP4 is illustrated in Fig. 7. It should be pointed out at this time that final linearity adjustments should be performed on the picture tube which is installed permanently



Fig. 6. Modified Centering Assembly in Place on the Neck of the Tube.

in the receiver. However, approximate adjustments can be made while the 5AXP4 is mounted in the chassis. Only slight touch-up adjustments are then required when the large tube is reinstalled.

Normally, a picture tube would not be considered as a tool; but the 5AXP4 is just that. During certain tests, it can provide very conclusive results which heretofore have been a sort of hit-and-miss proposition.



Fig. 7. Test-Pattern Display on the 5AXP4 Mounted in a Receiver Having 90-Degree Deflection.

This is particularly true when the tube is used to substitute for a suspected picture tube. The use of the 5AXP4 eliminates the necessity for removing cabinet-mounted picture tubes, and thus considerable time is saved. Because of its small size and weight, the 5AXP4 can be used in place of the large picture tube to make the receiver chassis lighter and more manageable during the servicing operation. The use of the 5AXP4 lessens the implosion hazard and eliminates any risk of damage to the customer's picture tube.

These are only a few of the many applications for the 5AXP4 tube. Its versatility will undoubtedly result in its application in an even greater number of servicing operations.

W. WILLIAM HENSLER

Shop Tickets

(Continued from page 25)

when the set is returned and the customer claims it is not his, let him check the serial number himself.

Space for Technician's Initials.

Most of the technicians interviewed in our survey seemed to approve of this entry when the ticket is used in shops where there are more than two men. It seemed to be the general consensus of opinion that the technician who makes the service call should first initial the shop ticket when he removes the set so that he can be assigned the return job. The shoptechnician should initial the ticket in case the man who delivers the set has some question about the job and also in case the chassis has to be returned to the shop for additional work.

Space to List Tubes and Parts Used and Their Prices.

It goes without saying that the parts used must be listed on the shop ticket regardless of the type of system used. In addition, the prices of the parts may be recorded on the ticket if it is to be used as the bill or income record.

Space for Description of Labor Performed and the Labor Charge.

If the ticket is not to be used as a bill, the shop technician can use this space to enter the length of time he works on the set and possibly a brief word or two about the nature of the repair. If the ticket is to serve as a bill or income record, the labor charge is entered in place of the time spent on the job.

Space for Pickup and Delivery Charge.

If it is standard procedure for the company to make a separate charge for pickup and delivery and if the shop ticket acts as the bill or income record, the job of making out the ticket would be simplified if a special space on the ticket were set aside for the charge made for pickup and delivery.

Tickets Numbered in Sequence.

If the shop tickets are used as service-call slips, they should be printed with consecutive numbers. On the other hand, if they are to be used in conjunction with regular

	\odot	
	TICKET NO.	
ADDRESS		
PHONE NO		
MAKE & MODEL		
SERIAL NO		
SYMPTOMS		
ABOR TIME		

Fig. 1. Simple Shop Ticket to Be Used for Chassis Identification.

service-call slips, they can be given the same number as the call slip. In the latter case, there should be a specific space allocated on each sec-



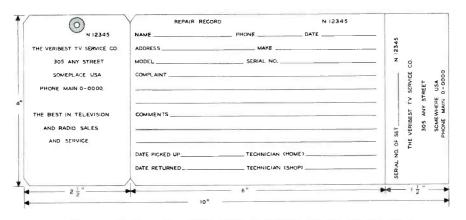


Fig. 2A. Front Side of Shop Ticket With Record Section Suitable for Filing.

tion of the shop ticket for the insertion of such a number.

Size of Ticket.

The size of the ticket will naturally depend upon the quantity of information that you wish to use on it. The size also depends upon the manner in which the shop tickets are to be used; that is, if they are to be discarded when the set is fixed or if they are to be kept as a record. If the latter is the case, it would be advisable to have them made in a handy size for filing. One size of file card is 3 by 5 inches; however, if many items are to be recorded on these tickets, this size is too small. A much more appropriate size for the main section of the ticket would be 4 by 6 inches. It may cost a little more to have this size printed, but the larger size would be well worth the additional expense.

Space for Purchase Date of a Set in Warranty.

The purchase date of a customer's set is important in computing the warranty status of parts. For shops which engage in a considerable volume of warranty work, it might be advantageous to provide a space on the shop ticket for the date of purchase or for the date of warranty expiration. In other cases, it should not be necessary to set aside a special space for this information. The warranty status can be indicated in the space provided for listing the parts replaced.

Space for Expiration Date of Service Contract.

In shops that do a great deal of service business on the contract basis, space can be set aside on the shop ticket for any necessary data concerning the customer's service contract.

Sample Tickets

With these ideas and suggestions to go on, two types of shop tickets have been developed. The first design, which may be seen in Fig. 1, is a simple shop ticket. It is intended to be used by shop personnel to identify chassis and to have something on which the parts used and the work done can be listed. Once a set has been returned to the home, the ticket may be removed and discarded. In other words, this simple shop ticket is to be used when there is no desire to keep the ticket for a record.

In order to simplify this ticket further, the customer identification can be left off if a system is employed whereby the chassis is identified by the call-slip number which is placed on the shop ticket in place of the reg-

WORK DONE		
PARTS USED		
	_	

Fig. 2B. Back Side of Shop Ticket Shown in Fig. 2A.

ular printed number. The chief advantage in having the name and phone number of the owner on these tickets is for the convenience of the shop man if he finds it necessary to call the customer about the set.

The more elaborate ticket shown in Fig. 2 is designed to serve a broader purpose. It has three sections: a customer's claim check, a file card, and a shop identification tag.

The first section is the customer's claim check. It contains the name, address, and phone number of the shop as well as a ticket number corresponding to the numbers on the other two sections. It also provides a space for the technician to write the serial number of the chassis before removing it from the home. We believe that this is good for customer relations. It will most assuredly put a stop to accusations that the wrong set was returned. Such erroneous claims, incidentally, do happen occasionally.

The center section measures 4 by 6 inches, which is a file-card size. This means that it is a good size for filing as a permanent record. This size is also large enough for all the necessary information without having the writing too small to be legible. While on the subject of keeping records, it is suggested that a service record be kept on shop work and on service calls completed in the home. This may best be done by using the main section of the shop ticket to record all the information from the completed service call and by filing the card section along with the regular shop tickets at the end of the day. This makes a much better filing system, since a card is much easier to file than the slip of paper that is usually used as a service-call slip. The file provides complete records as well as a complete mailing list which may be used for any type of mail advertising.

The third section of the shop ticket may be removed from the chassis and tied to the back of the cabinet when the set is reinstalled in the customer's home so that he has your shop name and phone number handy the next time he needs service.

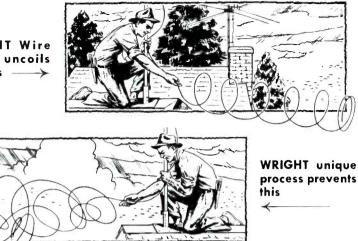
It is our belief that this shopticket design will fill the needs of the average radio and television service shop; however, for those who desire a slightly different design, some items can be eliminated and others added to suit the individual shop.

HENRY A. CARTER

January, 1955 - PF REPORTER

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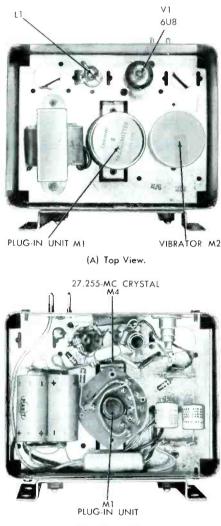
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The Garage-Door Opener (Continued from page 27)



(B) Bottom View.

Fig. 3. Transmitter in the Perma-Power Model RC101.

quarter of a revolution to resonate the circuit at a frequency slightly higher than that of the oscillator. No attempt should be made to alter the length of the antenna lead. Particular care should be taken to see that the leads to the transmitter do not interfere with the normal operation of the automobile.

Servicing of the transmitter is not difficult, and the normal troubleshooting procedures may be used. If trouble is experienced with an installation, one of the first checks to be made is to see if the neon bulb on the transmitter glows when power is applied to the unit. If the neon bulb does not glow and the vibrator supply seems to be operating, a slight readjustment of the slug in L1 may cause the transmitter to operate. The 6U8 is most easily checked by substitution. The antenna and its connecting cable may be checked when these preliminary

tests do not isolate the trouble. This may be done by unplugging the antenna cable and tuning L1 for an indication. Failure of the neon bulb to ignite when the antenna is disconnected isolates the trouble to the transmitter, and the transmitter may be removed from the automobile for more thorough testing.

A rapid and efficient check of transmitter performance may be made with the aid of a communication receiver tuned to 27.255 megacycles. This method also permits an audible indication of the modulation on the RF carrier and is very useful for this reason.

Bench servicing of the transmitter involves the usual procedure of checking voltages and resistances. A grid-dip meter is a very useful item when servicing transmitters. The resonant frequency of the tank circuit in the RF oscillator may be determined very easily by using this instrument. When checking the RF oscillator, the crystal should not be overlooked as a possible source of trouble. The griddip meter is of value in testing the crystal for activity. It is necessary to remove the crystal from the transmitter for this check. When removing or installing the crystal, care should be taken not to damage it as a result of the heat generated by the soldering operation; moreover, the crystal should not be subjected to excessive shock. After the crystal has been removed, a small loop made from hookup wire is connected across the leads from the crystal. The grid-dip meter is inductively coupled to this loop and tuned through 27.255 megacycles. If the crystal is good, a dip should occur at the resonant frequency. The grid-dip meter should be tuned very slowly, because the high Q of the crystal causes a very sharp dip on the meter.

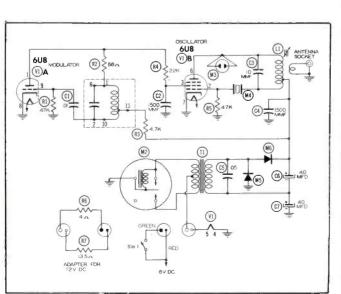
The modulator is of such a nature that it should not prove difficult to service. The operation of the modulator may be checked by connecting an oscilloscope to the screen grid of the RF oscillator and by checking for the presence of the tone signal. No attempt should be made to service the plug-in unit used in the modulator circuit. If the unit is defective, a replacement unit should be obtained from the manufacturer.

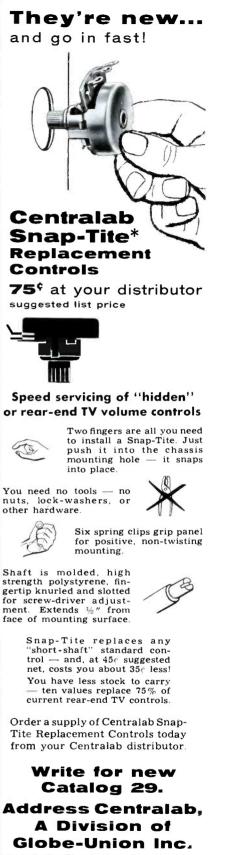
The power supply in the transmitter employs conventional circuitry and may be serviced in the same manner as any vibrator type of power supply.

Receiver Unit

The Model RC101 receiver used in conjunction with the aforementioned transmitter employs two 6U8 tubes and operates from a self-contained AC power supply. The major components and the parts placement may be seen in Fig. 5, which shows a top and a bottom view of the unit.

The receiver is tuned during manufacture to a frequency of 27.255 megacycles. The control relay in the receiver will not operate, however, unless the received signal is modulated at the correct frequency. As previously mentioned, the frequency of the tone modulation on the RF carrier is chosen by means of a plug-in unit in the transmitter. The receiver also has a similar unit which must correspond in frequency to the unit in the transmitter. The chance of the door mechanism being actuated by an unwanted signal is virtually eliminated by this system. In order to understand how this is accomplished, we shall investigate the receiver circuitry by means of the schematic diagram in Fig. 6.

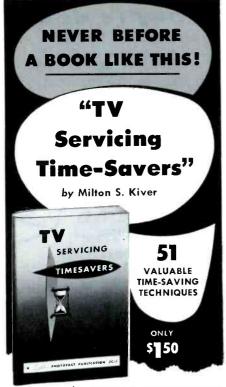




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Fig. 4. Schematic DiagramoftheTransmitter in the Perma-PowerModelRC101.



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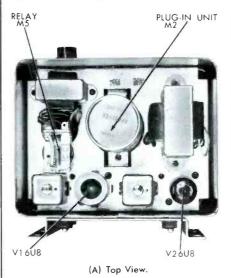
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A sensitivity control R1 is provided for adjusting the input to the first stage of amplification. The first stage employs the pentode section of a 6U8. Tuned circuits are used at the input and output of this stage. Gain of the amplifier is controlled by the application of AVC.

The second stage of amplification also employs the pentode section of a 6U8. The schematic shows that this stage is connected as a reflex amplifier. The signal at the plate of this stage is a 27.255-megacycle signal containing the tone modulation.



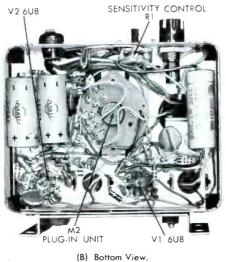


Fig. 5. Receiver in the Perma-Power Model RC101.

This signal is applied to a detector circuit employing a 1N64 germanium diode. The output of the detector is applied to the grid of the reflex amplifier V2A through R10. The amplified tone signal is taken from the screen grid which acts as the plate of a triode. The use of a reflex amplifier permits the pentode to serve the dual purpose of amplifying the 27.255-mc signal and of amplifying the tone signal as well. The output of



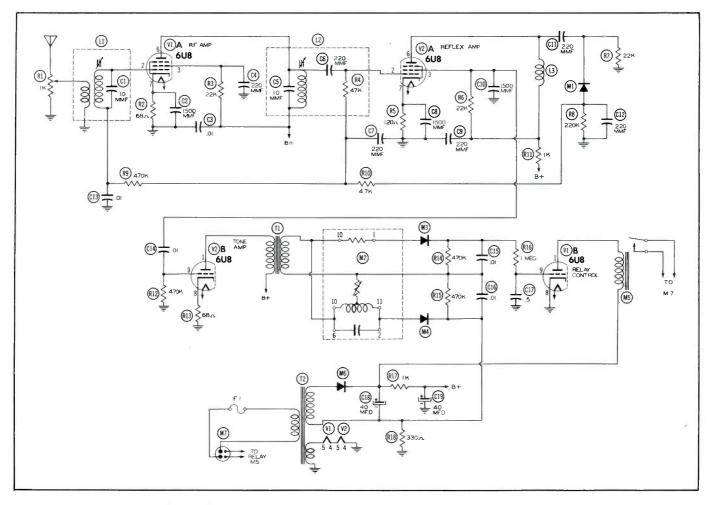


Fig. 6. Schematic Diagram of the Receiver in the Perma-Power Model RC101.

the detector is filtered by resistor R9 and capacitor C13 and is used as AVC on the first amplifier V1A.

The tone signal from the screen grid of V2A is fed through capacitor C14 to the grid of the triode section V2B where it is again amplified. The output of this stage is transformer coupled to the decoding network which contains the plug-in unit. It is necessary at this point to consider the triode section V1B. With no output from the decoder unit, the triode is cut off by the application of a negative voltage taken across resistor R18. During th is quiescent state, no plate current will flow and the contacts on relay M5 are open.

The plug-in unit is used in conjunction with two minature selenium rectifiers and contains two channels. One channel is merely resistive and has no frequency-selective circuit. The other channel is a band-stop circuit tuned to the frequency of the tone signal.

If a signal other than the proper tone signal is applied to the decoder network, very little attenuation is offered in either channel of the plug-in unit. The two outputs of the rectifiers M3 and M4 will then combine across resistors R14 and R15 in such a manner that the bias on the grid of the triode V1B will not be appreciably affected, and the tube will remain cut off.

If, however, the frequency of the signal is the same as the resonant point of the band-stop filter, a much larger output is obtained from the resistive channel than from the bandstop channel. The voltage developed across resistor R14 will cancel the bias on the triode grid, and the tube will conduct. Current then flow s through the relay, and the relay contacts close. The door-opening mechanism is activated by the closed contacts of the relay.

In order to reduce the risk of actuating the relay by a momentary signal occurring at the tone frequency, resistor R16 and capacitor C17 are used to form a time delay of approximately one-half second.

In trouble shooting the receiver, it is convenient to isolate the trouble to a particular stage first. This may

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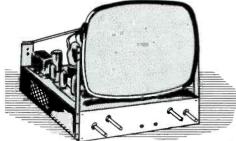
be done with the use of an audio signal generator and an RF signal generator.

The tone amplifier, the decoder network, and the relay-control stage may be easily checked by connecting an audio generator to the grid of V2B and applying a signal at the proper tone frequency. If this is done, the relay should close. Tuning of the audio generator to either side of the tone frequency should cause the relay to open. The triode section of the reflex amplifier may be checked in a similar manner by connecting the generator to the grid of V2A.

The over-all performance of the receiver, as well as the RF amplifiers and detector, may be checked by feeding into the receiver at the antenna terminal a 27.255-megacycle signal that is modulated at the tone frequency. An audio generator tuned to the tone frequency can be used to modulate the signal from the RF generator.

DON R. HOWE

Stocking the Tube Kit



A suggested list for stocking the tube kit appeared in the January 1954 issue of the PF INDEX. Since that time, some variations have occurred in the tube complements of television receivers. These variations should be reflected in the stock of tubes carried in the tube kit. It is for this reason that a revised list has

SUGGESTED MINIMUM STOCK REQUIREMENTS FOR DELUXE OR STANDARD TUBE KITS

been prepared. Chart I contains the list for the deluxe kit. A tube list for the standard kit is shown in Chart II.

As color television receivers become more prevalent, additional tube types will have to be carried by the service technician. Among these are the 3A2, 3A3, 6AN8, 6BC7, 6BY6, 6CL5, and 6BD4 tubes. The development of new tubes for use in series-string circuits will also be reflected in the types of tubes carried in the tube caddy. When the receivers using these tubes become more popular, the service technician may augment his tube stock with the appropriate types. The series-string tubes used in current models are listed in Chart III.

CHART I

Tube Complement for the Deluxe Kit

TUBES TYPES	TV MC	DELS 52-55	TUBES TYPES	TV MO 46-55		TUBES TYPES	TV MC 46-55		TUBES TYPES	TV MC 46-55	DE LS 52-55	TUBES TYPES	TV MC 46-55	DDELS 52-55
10000			2105	2	2	6BK5	1	1	6S4	1	1	12AU7	2	0
1B3GT	3	3	6AQ5	2	2		1	1		1	1		3	2
1X2A	2	2	6AQ7GT	1	,	6BK7A	2	2	6SL7GT	1	1	12AV7	1	1
5U4G	4	4	6AS5	1	1	6BL7GT	1	1.	6SN7GTA	4	4	12AX4	.1	1
5V4G	1	0	6AT6	1	1	6BN6	1	1	6SQ7(GT)	1	1	12AX7	1	1
5Y3GT	2	1	6AU5GT	1	1	6BQ6GT	3	3	6T4*	1	1	12AZ7	0	1
6AB4	1	1	6AU6	4	3	6BQ7A	2	3	6T8	2	2	12BH7	1	1
6AC7	2	2	6AV5GT	1	1	6BZ7	1	1	6U8	1	1	12BY7	1	-1
6AF4*	2	2	6AV6	2	2	6C4	2	2	6V3 (A)	1	1	12SN7GT	1	1
6AG5	2	1	6AX4GT	1	1	6CB6	3	4	6V6GT	2	2	25BQ6GT	1	1
6AG7	1	1	6AX5GT	1	1.	6CD6G	2	2	6W4GT	3	3	25L6GT	1	1
6AH4GT	1	1	6BA6	1	1	6CL6	0	1	6W6GT	1	1	25W4GT	1	1
6AH6	1	1	6BC5	2	1	6CS6	1	1	6X5(GT)	1	1	5642	2	2
6AK5	1	1	6BE6	1	1	6J5(GT)	1	1	6X8	1	1			
6AL5	2	2	6BG6G	2	2	616	3	3	6Y6G	î	1			
6AN4*	1	1	6BH6	1	0	6K6GT	2	1	12AT7	2	2			

*For UHF areas



Tube Complement for the Standard Kit

TUBES TYPES	TV MC 46-55		TUBES TYPES	TV MC 46-55		TUBES TYPES		DDELS 52-55	TUBES TYPES	TV MC 46-55		TUBES TYPES	TV MC 46-55	
1B3GT	2	2	6AN4*	1	1	6BG6G	1	1	6J6	2	2	12AT7	1	1
1X2A	1	1	6A Q5	1	1	6BK5	1	1	6K6GT	1	1	12AU7	1	1
5U4G	2	2	6AQ7GT	1	1	6BK7A	1	1	6S4	1	1	12AV7	1	1
5 V 4 G	1	0	6AS5	1	1	6BL7GT	1	1	6SL7GT	1	1	12AX4	1	1
5Y3GT	1	1	6AT6	1	1	6BN6	1	1	6SN7GTA	2	2	12AX7	1	1
6AB4	1	1	6AU5GT	1	1	6BQ6GT	1	2	6SQ7(GT)	1	1	12AZ7	0	1
6AC7	1	1	6AU6	2	2	6BQ7A	2	2	6T4*	1	1	12BH7	1	1
6AF4*	1	1	6AV5GT	1	1	6BZ7	1	1	6T8	1	1	12BY7	1	1
6AG5	1	1	6AV6	1	1	6C4	1	1	6U8	1	1	12SN7GT	1	1
6AG7	1	1	6AX4GT	1	1	6CB6	2	2	6V3 (A)	1	1	25BQ6GT	1	1
6AH4GT	1	1	6AX5GT	0	1	6CD6G	2	2	6V6GT	1	1	25L6GT	1	1
6AH6	1	1	6BA6	1	1	6C L6	0	1	6W4GT	2	2	5642	2	0
6AK5	1	1	6BC5	1	1	6CS6	1	1	6W6GT	1	1			
6AL5	1	1	6BE6	1	1	6J5(GT)	1	1	6X8	1	1			

*For UHF areas

CHART III

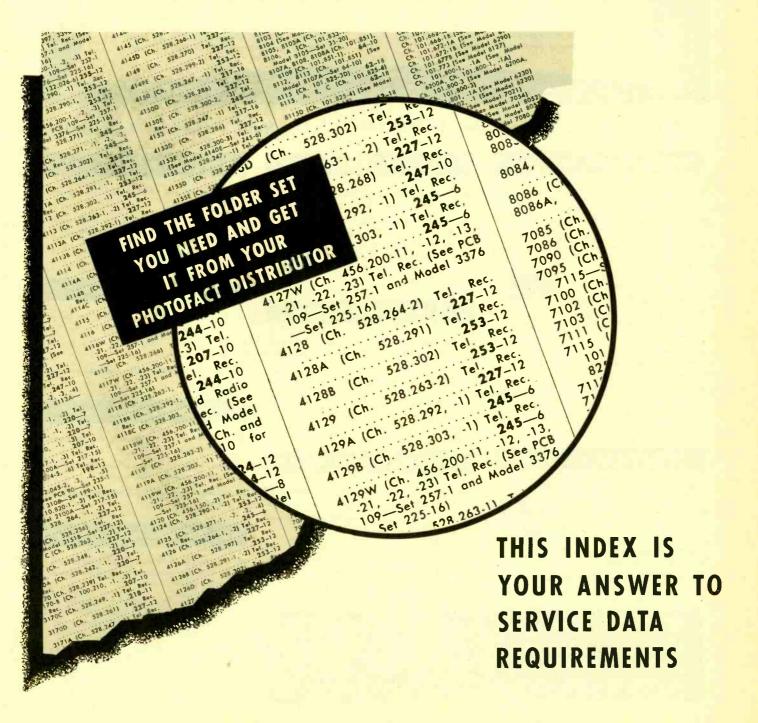
Tubes Appearing in Series-String Receivers

TUBES TYPES	TV MODELS 46-55 52-55								
2AF4		4BQ7A		516		12BQ6GT		25C D6G	
3BC5		5AM8		5U8		12CU6			
3BN6		5AN8		5X8		12L6GT			
3C B6		5AV8		6AW8		12W6GT			

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- 3. Diagrams are clear, large, extremely easy to read
- 4. Wave forms are shown right on the TV schematics for quick analysis by 'scope.
- 5. Voltages appear on the schematics for speedy voltage analysis.

matic.

- 7. Transformer winding resistances appear on the schematic.
- 8. Schematics are keyed to photographs and parts lists,

FULL PHOTOGRAPHIC COVERAGE

- 9. Exclusive photo coverage of all chassis views is provided for each receiver.
- 10. All parts are numbered and keyed to the schematic and parts lists.
- 11. Photo coverage provides quicker parts identifications and location.
- 12. Photo coverage helps identify burned-out or missing parts.

ALIGNMENT INSTRUCTIONS

- 13. Complete, detailed alignment data is standard and uniformly presented in all Folders.
- 14. Alignment frequencies are shown on radio photos adjacent to adjustment number —all alignment adjustments are keyed to schematic and photos.

TUBE PLACEMENT CHARTS

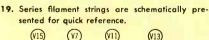
15. Top and bottom views are shown. Top view is positioned as chassis would be viewed from back of cabinet.

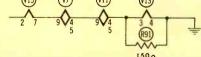
6AU6

- 16. Blank pin or locating key on each tube is shown on placement chart.
- 17. Tube charts include fuse location for quick service reference.

TUBE FAILURE CHECK CHARTS

18. Shows common trouble symptoms and indicates tubes generally responsible for such troubles.





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COMPLETE PARTS LISTS

- 20. A complete and detailed parts list is given for each receiver.
- 21. Proper replacement parts are listed, together with installation notes where required.
- 22. All parts are keyed to the photos and schematics for quick reference.

FIELD SERVICE NOTES

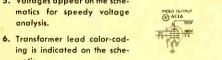
- 23. Each Folder includes time-saving tips for servicing in the customer's home.
- 24. Valuable hints are given for quick access to pertinent adjustments.
- 25. Includes tips on safety glass removal and cleaning.

TROUBLE-SHOOTING AIDS

- 26. Includes advice for localizing commonly recurring troubles.
- 27. Gives useful description of any new or unusual circuits employed in the receiver.
- 28. Includes aids, hints and advice for each specific chassis.

OUTSTANDING GENERAL FEATURES

- 29. Each and every PHOTOFACT Folder, regardless of receiver manufacturer, is presented in a standard, uniform layout.
- 30. PHOTOFACT, is a current service-you don't have to wait a year or longer for the service data you need. PHOTOFACT keeps right up with receiver production.
- 31. PHOTOFACT gives you complete coverage in both TV and Radio-to serve every Technician.
- 32. PHOTOFACT maintains an inquiry service bureau for the benefit of its Service Technician users.



Cumulative Index to PHOTOFACT FOLDERS

No. 48 · Covering Folder Sets Nos. 1 through 263 · World's Finest Electronic Service Data

HOW TO USE THIS INDEX

To find the PHOTOFACT Folder you need, first look for the name of the receiver (listed alphabetically below), and then find the required model number. Opposite the model, you will find the number of the PHOTOFACT Set in which the required Folder appears, and the number of that Folder. The PHOTOFACT Set number is shown in bold-face type; the Folder number is in the regular light-face type. **IMPORTANT-1.** The letter "A" following a set number in the Index listing, indicates a "Preliminary Data Folder." These folders were designed to provide immediate basic data on TV receivers. Many of these were later superseded by regular Photofact Folders. In those cases where short production runs and/or limited distribution prevented availability of a sample chassis the "A" designation has been retained.

2. Models marked by an asterisk (*) have not yet been covered in a standard Folder. However, regular PHOTOFACT Subscribers may obtain Schematic, Alignment Data or other required information on these models without charge by supplying make, model or chassis number and serial number. (When requesting such data, mention the name of the Parts Distributor who supplies you with your PHOTOFACT Folder Sets.)

3. Production Change Bulletins contain data supplementary to certain models covered in previously issued PHOTOFACT Folders, and are listed in this Index immediately preceding the listing of the original coverage of the model or chassis. These Bulletins should be filed with the Folders covering the models to which the changes apply.

Bit No. Bit No. <t< th=""><th>Set Folder</th><th>Set Folder</th><th>Set Folder</th><th>Set Folder</th><th>Set Folder</th></t<>	Set Folder	Set Folder	Set Folder	Set Folder	Set Folder
Ch-1 Marcine 1001 Biology 1722	No. No.		No. No.		No. No.
ADMARKA (Alley use Batter) 171:	ADAPTOL				
Const. 10170. 33-34 Single Const. 10170. 33-34 Single Const. 1021. 3312000 Sec. 1021. 332200 Sec. 10		Chassis 19H1, 19K1 (Also see PCB 112-Set 263-1)	19F1C)		 Models 24C15, 24C16, 24C17 (See Ch. 20B1)
Const. 10170. 33-34 Single Const. 10170. 33-34 Single Const. 1021. 3312000 Sec. 1021. 332200 Sec. 10	Changer Listing)	Chassis 19N1 (See PCB 78—Set	Model T2226 (See Ch. 19F1)	Model 6P32 (See Ch. 6E1, 6E1N)	 Models 24R11, 24R12 (See Ch.
 Chami and C. Journell, 2021 (Jack Constrainty, 2024). Second 2023 (Jack Constrainty, 2024). Sec	Chassis ULSK1	 Chassis 19T2, 19T2A (See PCB 112) 	22A3AZ)	(See Ch. 6Q1)	Models 24X15, S, 24X16, S, 24X175
 Chami and C. Journell, 2021 (Jack Constrainty, 2024). Second 2023 (Jack Constrainty, 2024). Sec	Chassis 1HF1	-Set 263-1 and Chassis 1981-	Models T2237Z, T2239Z (See Ch. 22427)	Model 6R11 (See Ch. 6R1)	(See Ch. 20X1)
Came of the construction Came of	Chassis 3A1	Chassis 20AI, 20B1 (Also see PCB)	•Model T2242 (See Ch. 19K1)	Ch. 3A11	Ch. 20A1)
 Chemi and J. (1997) Chemi and J. (1997)<	Set 126-11	23-Set 140-1) 77-1 Chassis 2042 20427 256-2	Models 4D11, 4D12, 4D13 (See Ch. 4D1)	Models 6RT41, 6RT42, 6RT43 (See Ch 5B1 Phone)	 Models 26R11, 26R12 (See Ch. 21B1)
Community 1281 and 76 B - 25 m (1) 1281 and (1) 1281 and (1) 1281	Chassis 4A1	• Chassis 20D2	Models 4H15, 4H16, 4H17 (A or B)		• Model 26R25 (See Ch. 24H1)
Chamie and international inter	Chassis 4D1 49—1	126-1 and PCB 26 Set 146-11	(See Ch. 2041) • Models 4H15, 4H16, 4H17, 4H18,	Model 6RT44 (See Ch. 7B1)	Model 26R26 (See Ch. 24H1)
Commit dati	Chassis 4H1	117_2	4H19 (S or SN) (See Ch. 30B1)	Models 6511, 6512 (See Ch. 651)	Model 26R26A (See Ch. 21B1)
Case: 41 100-10 -0.0001 3021 3021 3021 3021 3021 3021 3021	Chossis 431, 4K1	126-1 and PCB 26—Set 146-1)	Ch. 20B1)	Model 6T02, 6T04 1-20	Model 26R35A (See Ch. 2181)
Commit day 100	Chassis 4R1	Charrie 20X1 20X1 100 1	Models 4H115, 4H116, 4H117 (S or SNI) (See Ch. 30B1)		Model 26R36 (See Ch. 24H1) Model 26R364 (See Ch. 21B1)
Chemis 44 141 1	Chassis 451	Chossis 2021 (Also see PCB 7-Set	Models 4H126A, B, C, CN (See Ch.	Model 6711 (See Model 6702-Set	Model 26R37 (See Ch. 24H1)
Chemi 43,, 191-2 130 and 140 and 150 and	Chassis 4W1	Charle 2141 (Ales and BCB 23	All (1120 is or SN) (See Ch.	1-20) Model 6T12 (See Ch. 4A1)	Model 26837A (See Ch. 2181) Models 26X35, 26X36 (See Ch.
Chang, 39) (Sar, Mardial 2023) (Sar, Sar, Sar, Sar, Sar, Sar, Sar, Sar,	Chassis 5A3	Set 140-1)	3081)	Model 6144A (See Ch. 781)	24D1)
Commit 33, Amaze F2-7 Chammit 31, Ch. 7100 (Alice mar PC) Amaze first Alice	Chassis 5B1 (See Model 6T02—Set	Chassis 21B1 (Also see PCB 25—Se 144-1 and PCB 79—Set 220-1)	Model 4H137 (S or SN) (See Ch.	Models 6V11, 6V12 (See Ch. 6V1) Models 6W11, 6W12 (See Ch. 6W1)	Models 26X36A5, 5 (See Ch. 21E1) Model 26X37 (See Ch. 24D1)
Chemi 391.4 1447 Chemi 391.4 14447 Chemi 391.4 1447 Chemi 391.4 1447 Chemi 391.4	Chassis 5B1 Phono. 4-24	118-2	30B1)	Models 6Y18, 6Y19 (See Ch. 6Y1)	 Models 26X45, 26X46 (See Ch.
Ceneri 307 114-7 Ceneri 307 200 / 105 / 107 / 1	Chargie SBIA 18 1	25-Set 144-1) 118-2	2081)	Ch. 6B1}	 Models 26X55, 26X56, 26X57 (See
Commi 327 137-2 Product At1455, N [See Ch. 2001] Models (76.3, 76.3) / (5.3, 76.3) / (5.3, 76.3) / (5.4, 76.3) Models (76.3, 76.3) / (5.3, 76.3) / (5.4, 76.3) Commi 327 137-2 Commi 327 N [See Ch. 2001] Models (76.3, 76.3) / (5.3, 76.3) / (5.3, 76.3) Models (76.3, 76.3) / (5.3, 76.3) / (5.3, 76.3) Models (76.3, 76.3) / (5.3, 76.3) / (5.3, 76.3) Models (76.3, 77.6)	Chassis 5C3	• Chassis 21E1 (See Ch. 21D1-Set	Models 4H145S, SN (See Ch. 30B1) Models 4H146A B. C (See Ch.	Models 7C61, 7C62, 7C62-UL (See	Ch. 24D1) Models 26X55A 26X56A 26X57A
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5D2	Chassis 21F1, 21G1 (Also see PCB	2081)	Model 7C62A (See Ch. 6M1)	(See Ch. 21D1)
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5E2	30—Set 156-2 and PCB 46—Set 180-1)	 Models 4H1465, SN (See Ch. 30B1) Models 4H147A, B (See Ch. 20B1) 	7C1)	Ch. 24D1)
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5E3	Chassis 21H1, 21J1 (Also see PCB	Models 4H1475, SN (See Ch. 30B1) Models 4H1554, B (See Ch. 30B1)	Model 7C63A (See Ch. 7C1)	Models 26X65A, 26X66A, 26X67A
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5G2	Chassis 21K1, 21L1 (Also see PCB	Models 4H155S, SN (See Ch. 30B1)	Ch. 7E1)	• Models 26X75, 26X76 (See Ch.
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5J2	46_Set 190.11 135-7	Models 4H157A, B (See Ch. 20B1) Models 4H156A, B (See Ch. 20B1)	Model 7C73 (See Ch. 9A1)	24D1)
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5K1	Set 156-2, PCB 46-Set 180-1	Models 4H156S, SN (See Ch. 20B1)	7G16 (See Ch. 7G1)	21D1)
Chantis Still Sp- Tig_1 Pril Stree Tig_1 Pril Stree Sp- Tig_1 Pril Stree	Chassis 5M2	and Ch. 21F1Set 135-2) Chassis 21P1 21Q1 (Also see PCB)	 Models 4H1575, SN (See Ch. 3081) Models 4H165A, B (See Ch. 2081) 	Models 7P32, 7P33, 7P34, 7P35 (See Ch. 5H1)	Models 27K12 (See Ch. 21F1) Models 27K15 A B 27K16 A B.
Chanis 31/1 1921 1921 1921 1921 1921 1921 1921 1	Chassis 5R1	30—Set 156-2 and PCB 46—Set	Models 4H1655, SN (See Ch. 30B1)	Models 7RT41, 7R242, 7RT43 (See	27K17, A, B (See Ch. 21F1)
Chansis Sull Fig 2	Chossis 5R2		2081)	Models 7T01, 7T01M-U1, 7T04,	27K27, A, B (See Ch. 21F1)
Chemis 327 204-2 177-21, 17 177-21, 177-21, 177-2 2011, 117-23, 217, 272-14, 2012,		Chassis 21X1, 21X2 (See PCB 62-	Models 4H166S, SN (See Ch. 301B1) Models 4H167A B C. CN (See Ch.	7T04-UL (See Ch. 5N1) Model 7T06 (See Ch. 4B1)	Models 27K35 & B 27K36 A B
Chessis 641 (58e Model 4701-59r L19) Chessis 642 (58e Ch. 421) Chessis 642 (58e Ch. 422) Chessis 642 (58e Ch. 422) Chessis 643 (58e Ch. 422) Chessis 641 (58e Ch. 421) Chessis 641 (58e Ch. 581) Chessis 641 (58e Ch. 1971) Chessis 641 (58e Ch. 1971) Chessis 641 (58e Ch. 1971) Chessis 641 (58e Ch. 1971) Chess		177-2)	20B1)	Model 7110 (See Ch. 5K1)	Models 27K46, A, B (See Ch. 21F1)
Chassis 64.2 10.3 Chassis 62.4 Chassis Chassis <thchasis< th=""> <thchasis< th=""> <thchasis<< td=""><td></td><td>• Chassis 2121, 2121A 177-2 • Chassis 2121, 2121A 177-2</td><td></td><td>Model 7112 (See Ch. 481) Models 7114, 7115 (See Ch. 5K1)</td><td>Ch. 21F11</td></thchasis<<></thchasis<></thchasis<>		• Chassis 2121, 2121A 177-2 • Chassis 2121, 2121A 177-2		Model 7112 (See Ch. 481) Models 7114, 7115 (See Ch. 5K1)	Ch. 21F11
Chemis 681 48-2 chemis 722 201-2	1-19)	• Chassis 22A2, 22A2A	Model 4T11 (See Ch. 4T1) Model: 4W18 4W19 (See Ch. 4W1)	Models 8C11, 8C12, 8C13 (See Ch. 30A1 and Ch. 8C1)	Model 27M12 (See Ch. 21X2)
Chassis 621, dEIN General 641, dEIN	Chassis 6A2		Models 4X11, 4X12 (See Ch. 4X1)	Model: 8014 8015 8016 8017	Ch 21F1)
Chassis 621, dEIN General 641, dEIN			Models 4X18, 4X19 (See Ch. 4X1) Models 5A32/12, 5A32/15, 5A32/	(See Ch. 8C;) Models 8D15, 8D16 (See Ch. 8D1)	Models 27M35, 27M36 (See Ch. 21F1)
Chanis 2Ani 23-1 Chanis 2Ani 180-2 Chanis 2Ani 22-1 Model 521, 5E2, 5E23 (See Ch. 2H1) Model 521, 5E2, 5E23 (See Ch. 2H1) Model 522, 5E23 (See Ch. 2H1) Model 522, 5E23 (See Ch. 2H1) Chanis 601 78-1 Chanis 221, 221, 222-2 Model 521, 5E2, 5E23 (See Ch. 2H1) Model 521, 5E2, 5E23 (See Ch. 2H1) Model 522, 5E23 (See Ch. 2H1) Chanis 601 74-1 Chanis 221, 221, 221, 221, 222-2 Model 551, 5E2, 5E23 (See Ch. 521) Model 521, 5E2, 5E23 (See Ch. 2H1) Chanis 601 74-1 Chanis 321, 221, 221, 221, 222, 222, 223, 223,	Chassis 6E1, 6E1N	•Chassis 22E2	16. 5A33/12. 5A33/13, 5A33/10	Model 8RP46 (See Ch. 3A1)	B Hodels 20115 20116 2017 (See
Chossis & M2 (See Ch. 612—Set 140-2) Chossis 21M, 22M, 222 - 222-2, 222 Chossis 21M, 22M, 222 - 222-2, 222 Chossis 21M, 22M, 22M, 22M, 22M, 22M, 22M, 22M,	Chassis 6J2		Models 5D31, 5D32, 5D33 (See Ch.	9B1)	Ch. 24F1) Model 29X25 (See Ch. 24F1)
Chasis 601 78-1 Chasis 601 78-1 Chasis 601 70-1 Chasis 601 71-1 Chasis 761 25-2 Chasis 761 56-1 Chasis 761 56-1 Chasis 761 56-1 Chasis 761 56-1 Chasis 761 56-2	Chassis 6M1	• Chassis 22M1		Models 9E15, 9E16, 9E17 (See Ch.	Model 29X25A (See Ch. 21H1)
Chasis 601 78-1 Chasis 601 78-1 Chasis 601 70-1 Chasis 601 71-1 Chasis 761 25-2 Chasis 761 56-1 Chasis 761 56-1 Chasis 761 56-1 Chasis 761 56-1 Chasis 761 56-2		• Chossis 22N2	5E2)	Models 12X11, 12X12 (See Ch.	Model 29X26A (See Ch. 21H1)
Charsii & Still 107-1 Charsii & Still 107-1 24H1 Alto tee PCB 9	Chargin 4(0) 79 1		6 6 2 1	2021) Models 14R11, 14R12 (See Ch.	Model 29X27 (See Ch. 24F1) Models 30A12, 30A13 (S or SN)
Chassis 721 192-2 Chassis 3081, 30C1, 30D1, 71-2 Models 12222, 122, C22227, C22227, C22272, C2226, C22272, C2226, C22272, C22272, C2226, C22272, C2226, C22272, C22272, C2226, C22272, C2272, C226, C22272, C2272, C226, C22727, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C2272, C226, C2272, C226, C2272, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C226,	Chassis 651	Chassis 24D1, 24E1, 24F1, 24G1,	Models 5E38, 5E39 (See Ch. 5E3)	2071)	(See Ch. 30A1)
Chassis 721 192-2 Chassis 3081, 30C1, 30D1, 71-2 Models 12222, 122, C22227, C22227, C22272, C2226, C22272, C2226, C22272, C22272, C2226, C22272, C2226, C22272, C22272, C2226, C22272, C2272, C226, C22272, C2272, C226, C22727, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C2272, C226, C2272, C226, C2272, C2272, C226, C2272, C226, C2272, C226, C2272, C226, C2272, C226,	Chassis 6V1	114-1	Models 5G21, 5G21/15, 5G22,	• Model 15K21 (See Ch. 2011)	Ch 30411
Chossis 7C1 25–2 Chossis 7C1 36–1 CU2272, See Ch. 22832 Sign 2, 22832, CU2272, See Ch. 22832 Sign 2, 22832, CU2272, See Ch. 22832 Sign 2, 22832, See Ch. 30C1, S. SN, 30C185, SN, 30C1	Chassis 6Y1	• Chassis 30A1 57—2	5G22/15, 5G23, 5G23/15 (See	Model 16M12 (See Ch. 21X1) Models 16R11 16R12 (See Ch.	 Models 308155, SN, 308165, SN, 308175, SN (See Ch. 3081)
Chasiis 721 36-1 CD22/22 [See Ch. 2282] CD22/22 [See Ch. 2282] Model: 7283] Model: 7283] <td>Chassis 781</td> <td>Models CU2225Z, CU2226Z,</td> <td>Models 5J21, 5J22, 5J23 (See Ch.</td> <td></td> <td>Models 30C155 SN 30C165 SN</td>	Chassis 781	Models CU2225Z, CU2226Z,	Models 5J21, 5J22, 5J23 (See Ch.		Models 30C155 SN 30C165 SN
Chorsis BCI [See Ch. 80]-Set d7-1] Models (22232, C2227, C2227, (See Ch. 22A32] Models (22232, C2227, C2227, (See Ch. 22A32] Models (22232, C2227, (See Ch. 22A32] Models (22232, C2227, (See Ch. 22A32] Models (2223, C2227, (See Ch. 22A32] Models (See Ch. 2A32] Models (See Ch. 2A33] Models (See Ch. 2A31] Model (See Ch. 2A31]	Chossis 7E1	Model C2216Z (See Ch. 20A2Z)	Models 5K11, 5K12, 5K13, 5K14	(See Ch. 1981)	Models 30F15, A, 30F16, A, 30F17,
Chorstis BD1 67-1 0Model (22364 (See Ch. 2072) 0Model (22364 (See Ch. 19F1B) 0Model (See Ch. 2182) 0Model (See Ch. 211) 0Model (See Ch. 2011) 0Model	Chassis 8C1 (See Ch. 8D1—Set	• Models C2225Z, C2226Z, C2227Z	(See Ch. 5K1)	Models I/KII, I/KI2 (See Ch.	A (See Ch. 20A1)
Chossis 981 49-2 (See Ch. 2282) • Models FU22102, FU2217Z, FU2218Z (See Ch. 2282) • Models FU2210Z, FU2217Z, FU2218Z (See Ch. 2282) • Models FU22122(See Ch. 2021) • Models FU2212(See Ch. 2021) • Models FU2212(See Ch. 2021) • Models FU2210 FU2211 See Ch. 1981 • Models FU2211 See Ch. 1981, 1981C • Models FU2212(See Ch. 2021)	Chossis 8D1 67-1	 Model C2236A (See Ch. 20A2) 	5L2)	Model 17K16 (See Ch. 21F1)	20Z1)
Charsit 10AH 23-20 Cise CL: 223/21 Cise CL: 223/21 Model 5521AN (See CL: 5C3) Model 5521AN (See CL: 5C3) Model 5521AN (See CL: 5C3) Model 5522AN (See CL: 5C3) Model 522AN (See CL: 5C3) Model 52AN (See CL: 5	Chassis 9A1	• Model C2246 (See Ch. 19F1B)	Model 5R10 (See Ch. 5R1)	•Models 17K21, 17K22 (See Ch. 21F1)	
Charsit 10AH 23-20 Cise CL: 223/21 Cise CL: 223/21 Model 5521AN (See CL: 5C3) Model 5521AN (See CL: 5C3) Model 5521AN (See CL: 5C3) Model 5522AN (See CL: 5C3) Model 522AN (See CL: 5C3) Model 52AN (See CL: 5	Chassis 981	(See Ch. 22B3Z)	Models 5R11, 5R12, 5R13, 5R14	Models 17M15, 17M16, 17M17 (See	•Models 32X35, 32X36 (See Ch.
100-11 13HF1, 1HF1, 1HF1, 11, 1232 25B-2 Choasis 19B1 (Also see PCB 112— Set 2d3-1) 13HF1, 1HF1, 11, 1232 25B-2 Choasis 19B1 (See PCB 112— 20Ac) Model 52(15, 25C) Choasis 19B1 (See PCB 112— 210—2) Model 122232 (See Ch. 2262) Choasis 19B1 (Sie PCB 112— 210—2) Model 122232 (See Ch. 2262) Choasis 19B1 (Also see PCB 112— 210—2) Model 122232 (See Ch. 2262) Choasis 19B1 (Also see PCB 112— 210—2) Model 122232 (See Ch. 126) Choasis 19B1 (Also see PCB 112— 210—1) Model 122232 (See Ch. 126) Choasis 19B1 (Also see PCB 112— 210—1) Model 122232 (See Ch. 19B1) Model 532 (See Ch. 19B1) Model 532 (See Ch. 19B1) Model 532 (See Ch. 19B1) Model 542 (See Ch. 2011) Model 532 (See Ch. 19B1) Model 542 (See Ch. 2011) Model 532 (See Ch. 19B1) Model 611 (See Ch. 572) Model 532 (See Ch. 19B1) Model 611 (See Ch. 6C1) Model 52 (See Ch. 19B1) Model 611 (See Ch. 6C1) Model 52 (See Ch. 19F1) Model 6121 (See Ch. 10A1) <td< td=""><td>Chussis TOAT</td><td> Models F2216Z, F2217Z, F2218Z (See Ch. 22A37) </td><td>Model 5521AN (See Ch. 5C3)</td><td>Models 19A11S, SN, 19A12S, SN</td><td>2021) Model: 34815 A 34816 A (See</td></td<>	Chussis TOAT	 Models F2216Z, F2217Z, F2218Z (See Ch. 22A37) 	Model 5521AN (See Ch. 5C3)	Models 19A11S, SN, 19A12S, SN	2021) Model: 34815 A 34816 A (See
100-11 13HF1, 1HF1, 1HF1, 11, 1232 25B-2 Choasis 19B1 (Also see PCB 112— Set 2d3-1) 13HF1, 1HF1, 11, 1232 25B-2 Choasis 19B1 (See PCB 112— 20Ac) Model 52(15, 25C) Choasis 19B1 (See PCB 112— 210—2) Model 122232 (See Ch. 2262) Choasis 19B1 (Sie PCB 112— 210—2) Model 122232 (See Ch. 2262) Choasis 19B1 (Also see PCB 112— 210—2) Model 122232 (See Ch. 2262) Choasis 19B1 (Also see PCB 112— 210—2) Model 122232 (See Ch. 126) Choasis 19B1 (Also see PCB 112— 210—1) Model 122232 (See Ch. 126) Choasis 19B1 (Also see PCB 112— 210—1) Model 122232 (See Ch. 19B1) Model 532 (See Ch. 19B1) Model 532 (See Ch. 19B1) Model 532 (See Ch. 19B1) Model 542 (See Ch. 2011) Model 532 (See Ch. 19B1) Model 542 (See Ch. 2011) Model 532 (See Ch. 19B1) Model 611 (See Ch. 572) Model 532 (See Ch. 19B1) Model 611 (See Ch. 6C1) Model 52 (See Ch. 19B1) Model 611 (See Ch. 6C1) Model 52 (See Ch. 19F1) Model 6121 (See Ch. 10A1) <td< td=""><td>Chassis 19A1 (Also see PCB 5—Set</td><td>• Model F2226 (See Ch. 20A2)</td><td>Model 5S22AN (See Ch. 5C3)</td><td>(See Ch. 19A1)</td><td>Ch. 20V1)</td></td<>	Chassis 19A1 (Also see PCB 5—Set	• Model F2226 (See Ch. 20A2)	Model 5S22AN (See Ch. 5C3)	(See Ch. 19A1)	Ch. 20V1)
Chorsis 1981C (See PCB 112—Set 240—2) 200.21 Model TU2232 (See Ch. 22G2) Model SATA, 5X12, 5X13, 5X14 Model 20X132 (See Ch. 20X1) Model SATA, 3X36A, 36X37 (See Ch. 5X1) Set 263-1) 228321 Model TU22327 (See Ch. 122G2) Model SATA, 5X22, 5X23 (See Ch. 22G2) Model SATA, 5X22, 5X23 (See Ch. 22G1) Model SATA, 5X22, 5X23 (See Ch. 22G1) Model SATA, 5X22, 5X23 (See Ch. 22G1) Model SATA, 5X23, 5X24, 5X24, 5X24, 5X24 (See Ch. 20X1) Model SATA, 5X23, 5X24, 5X23 (See Ch. 22G1) Model SATA, 5X36A, 36X37 (See Ch. 22B31) Charsis 19F1, 19F1, 4 (Alio see PCB 76 112—Set 263-1] 20832(See Ch. 19F1), 11812 (See Ch. 19F1) Model SATA, 5A2, 6A23 (See Ch. 201) Model SATA, 5A2, 6A23 (See Ch. 201) Model SATA, 5A2, 6A23 (See Ch. 201) Set 210_2) Model TU2211 (See Ch. 19F1A, 19B1C) Model SATA, 5A2, 6A23, 4See Ch. 201) Model SATA, 5A2, 6A23 (See Ch. 201) Model SATA, 5A2, 6A23 (See Ch. 201) Set 210_2) Model TU2211 (See Ch. 19F1A, 19F1) Model SATA, 5A2, 6A23, 4See Ch. 201) Model SATA, 5A2, 6A23, 4See Ch. 201) Model SATA, 5A2, 6A23, 4See Ch. 201) Set 210_2) Model TU2211 (See Ch. 19F1A, 19F1) Model SATA, 5A2, 6A23, 4See Ch. 201) Model SATA, 5A2, 6A23, 4See Ch. 201) Model SATA, 5A2, 6A23, 4See Ch. 201) </td <td>Chossis 198) (Also see PCB 112-</td> <td>15HF1, 4HF1, 1HF1)258-2</td> <td>Model 5712 (Ch. 571)</td> <td>Models 20X11, 20X12 (See Ch.</td> <td>Model 36R37 (See Ch. 21C1) Model: 36R45 36R46 (See Ch.</td>	Chossis 198) (Also see PCB 112-	15HF1, 4HF1, 1HF1)258-2	Model 5712 (Ch. 571)	Models 20X11, 20X12 (See Ch.	Model 36R37 (See Ch. 21C1) Model: 36R45 36R46 (See Ch.
263-1 and Chassis 1981—Set 210-2) Model 10/2/32 (See Ch. 2262) Model 10/2/32 (See Ch. 2262) Model 20/136 (See Ch. 2071) Model 10/2/32 (See Ch. 2262) Model 20/136 (See Ch. 20/1) Model 20/136 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1) Model 20/13 (See Ch. 20/1)	Set 263-1)	Models K2216A, K2217A (See Ch. 20A2)	Models 5W11, 5W12 (See Chr. 5W1)	20X1)	21C1)
• Chosisi 197(1 (Alto see PCB 112_ Set 263-1) • Modelis 1022362, TU22372 (See Ch. 2282) • Modelis 20223 (See Ch. 2282) • Modelis 20223 (See Ch. 2282) • Modelis 20223 (See Ch. 2282) • Modelis 3722 (See Ch. 2282) • Modelis 3722 (See Ch. 282) • Modelis 3723 (See Ch. 282) <t< td=""><td>263-1 and Chassis 19B1-Set</td><td>• Model TU2232 (See Ch. 22G2)</td><td>(See Ch. SAI)</td><td>Model 20X136 (See Ch. 20Y1)</td><td>Models 36X35, 36X36, 36X37 (See Ch 24E1 and Ch 582)</td></t<>	263-1 and Chassis 19B1-Set	• Model TU2232 (See Ch. 22G2)	(See Ch. SAI)	Model 20X136 (See Ch. 20Y1)	Models 36X35, 36X36, 36X37 (See Ch 24E1 and Ch 582)
Chosisis VEI Allos tes PCB 7654 Models 1181, 11812 (See Ch. 1981) Models 37715, A, B. Syr16, A, B. 219-11 203203	210-21	 Models TU2236Z, TU2237Z (See Ch. 	Models 5X21, 5X22, 5X23 (See Ch.	Models 20X145, 20X146, 20X147	•Models 36X35A, 37X36A, 36X37A
Chossis i yE1 (Also isee PCB 76—Set 2012) Or 1981 Cl Or 1981	Set 263-1)	22B3Z)		Model 22X12 (See Ch. 20Z1)	(See Ch. 24E1 and Ch. 5D2)
112Set 263-1		or 1981C)	Models 6A21, 6A22, 6A23 (See Ch.	Models 22X25, 22X26, 22X27 (See	(See Ch. 21G1 or Ch. 21Q1 and
Chasis 19F1B, 19F1C (See FCB 112 —Set 23-1 and Chasis 19F1B, 19F1C (See FCB 172) Model 122112 (See Ch. 19F1A or 19F1B) Order 3212 (See Ch. 19F	Chassis 19F1, 19F1A (Also see PCB	Model T1822 (See Ch. 1981, 1981C) Model T2211 (See Ch. 1981, 1981C)	Model 6C11 (See Ch. 6C1)		Ch. 5D2)
Set 263-1 and Chassis 1981-	•Chassis 19F18, 19F1C (See PCB 112	Model T2211A (See Ch. 19T2A)	Models 6C22, A, 6C23, A (See Ch.	20A1)	(See Ch. 21G1 or 21Q1 and Ch.
Chassis 19G1 (See PCB 78-Set Models 12216A 122174 (See Fh Models 6)21, 6)22 (See Ch. 6)2 Models 24A126 24A126 24A127 (See Ch. 2)G1 or 2)Q1 and Ch.		Model T2212 (See Ch. 19F1A or 19F1B)	OCZ, AI		
219-1 and Ch. 1921—Set 203-21 + 20A2) Addel 6M22 (See Ch. 6M2) + 20A1) 5D2	Chassis 19G1 (See PCB 78-Set	●Models T2216A, T2217A (See €h.	Models 6121, 6122 (See Ch. 612)	Models 24A126, 24A127 (See Ch.	(See Ch. 21G1 or 21Q1 and Ch.
	219-1 and Ch. [9E1-Set 203-2)	20A2)	Model 6M22 (See Ch. 6M2)	20A1)	502]

NOTE: PCB Denote: Production Change Bulletin.

Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver

ADMIRAL-AIRLINE

ADMIRAL-Cont.

Madel: 37F55, 37F56, 37F67 (See Ch. 21G1 or 21Q1 and Ch. 5D2) Madel: 37K15, A, B, 37K16, A, B (See Ch. 21G1 or 21Q1 and Ch. 3C1) Madel: 37K27 A B, 37K24 A

ADMIRAL-Cont.

3C1) •Models 37K27, A, B, 37K28, A, B [See Ch. 21G1 or 21Q1 and Ch. 3C1) •Models 37K35, A, B, 37K36, A, B [See Ch. 21G1 or 21Q1 and Ch. 3C1)

Modeli 37K35, A, B, 37K36, A, B (See Ch, 21G1 or 21G1 and Ch, 3C1)
Modeli 37K55, 37K57, 37K57 (See Ch, 21G1 or 21Q1 and Ch, 3C1)
Modeli 37K55, 37K26, 37K27 (See Ch, 21G1 or 21Q1 and Ch, 3C1)
Modeli 37K15, 37M26, 37M27 (See Ch, 21Z1)
Modeli 39X16, A, 39X17, A (See Ch, 24G1 and Ch, 582)
Modeli 39X165, 39X26 (See Ch, 24G1 and Ch, 582)
Modeli 39X157, 48X178 (See Ch, 24G1 and Ch, 582)
Modeli 39X25A, 39X26A (See Ch, 21J1)
Modeli 39X35, 39X36, 39X37 (See Ch, 21J1) and Ch, 3C1)
Modeli 39X35, 39X36, 39X37 (See Ch, 21J1) and Ch, 3C1)
Modeli 39X35, 39X36, 39X37 (See Ch, 21J1) and Ch, 3C1)
Modeli 47M15, A, 47M16, 47M17 (See Ch, 21W1)
Modeli 57M10, 57M11, 57M12 (See Ch, 21Z1A)
Modeli 12DX12 (See Ch, 19C1)
Modeli 12DX12 (See Ch, 19C1)
Modeli 12DX12A (See Ch, 19C1)

Model 1210X164 (See Ch. 19C1 or 19F1) Model 1210X16L (See Ch. 19K1) Model 1210X17 (See Ch. 19C1) Model 1210X17A (See Ch. 19C1 or

 Model 121DX17A (See Ch. 19C1 or 19F1)

 Model 121DX17A (See Ch. 19K1)

 Model 121DX17A (See Ch. 19K1)

 Models 121K15, 121K16, 121K17 (See Ch. 21M1)

 Models 121K15A, 121K16A, 121K17A (See Ch. 22M1)

 Models 121M11, 121M12A (See Ch. 21M1)

 Models 121M11A, 121M12A (See Ch. 21M1)

 Models 121M11A, 121M12A (See Ch. 22M1)

 Model 221DX151 (See Ch. 22F2)

 Model 221DX154 (See Ch. 19C1) or 19F1)

 Model 221DX154 (See Ch. 19C1) or 19F1)

 Model 221DX154 (See Ch. 19C1) or 19F1)

 Model 221DX154 (See Ch. 19C1) or 19F1)

model 2210X10A [See Ch. 19Cl or 19F1]
 Model 2210X17 (See Ch. 19Cl)
 Model 2210X26 (See Ch. 19Cl)
 Model 2210X26 (See Ch. 19Cl)
 Model 2210X26 (See Ch. 19Cl)
 Model 2210X28 (See Ch. 19Cl)
 Model 2210X38 (See Ch. 19Cl)
 Model 2211X28 (See Ch. 21K1)
 Model 2211X28 (See Ch. 21K1)
 Model 2211X28 (See Ch. 21K1)
 Model 211X28 (See Ch. 21K1)
 Model 211X28 (See Ch. 21K4)
 Model 211X28 (See Ch. 21K4)
 Model 211X28 (See Ch. 21K4)
 Model 211X28 (See Ch. 221K46 (See Ch. 21K1)
 Model 221X55 (See Ch. 19H1)
 Model 2210X15 (See Ch. 22M2)
 Model 2210X15 (See Ch. 22M2)
 Model 2210X15 (See Ch. 22M2)
 Model 2220X17 (See Ch. 1911)
 Models 220X17 (See Ch. 1911)
 Models 220X17 (See Ch. 1911)
 Models 2210X15 (See Ch. 1911)
 Models 2210X15 (See Ch. 1911)
 Models 2210X18 (See Ch. 1911)
 Models 2210X18 (See Ch. 1911)
 Models 2210X18 (See Ch. 1911)
 Models 2110X26 (See Ch. 1911)
 Models 2110X28 (See Ch. 1911)
 Models 2110X28 (See Ch. 1911)<

Ch. 5D2) Model: 321F65, 321F65, 321F67 (See Ch. 21W1 and Ch. 5D2) Model: 321K15, 321K16 [See Ch. 2111 and Ch. 3C1) Model 321K18 [See Ch. 2111 and Ch. 3C1] Model 321K27 [See Ch. 2111 and Ch. 3C1]

ADMIRAL-Cont. •Modei: 32/K35, 32/K36 (See Ch. 2111 and Ch. 3C1) •Modei: 32/K46, 32/K47 (See Ch. 2111 and Ch. 3C1) •Modei: 32/K46 (See Ch. 2111 and Ch. 32/K47 (See Ch. 2111 and Ch. 32/K47 (See Ch. 2111 and 32/K47 (See Ch. 2114) •Modei: 32/M25, 32/M26, 32/M27 (See Ch. 2114) •Modei: 32/M25, 32/M26, 32/M27 (See Ch. 214) •Modei: 32/M25, 32/M26, 32/M27 •Modei: 32/M25, 32/M26, 32/M27 •Modei: 32/M15, 42/M164 (See Ch. 214) •Modei: 42/M15, 42/M164 (See Ch. 214) •Modei: 42/M35, 42/M164 (See •Modei: 42/M35, 42/M36, 42/M37 •Modei: 32/M15, 520M12 (See Ch. 22A2) •Modei: 520M11, 520M12 (See Ch. 22A2) Madeis 520M11, 520M12 (See Ch. 22A2A)
 Madeis 520M15, 520M16, 520M17 (See Ch. 22A2)
 Madeis 521M15, 521M16, 521M17 (See Ch. 21Y1)
 Madeis 521M15A, 521M16A, 521M17A (See Ch. 22Y1) AFRMOTIVE 12-1 191.40 AERO (See Record Changer Listing) AIMCEE (See AMC) AIRADIO
 SU-41D
 11—1

 SU-52A, B, C (Receiver)
 13—2

 TRA-1A, B, C (Transmitter)
 13—1

 3100
 37—1
 AIRCASTLE 136_3 85-1 85-1 48-3 54-3 52-25 50_1 93_1 71_3 87_1 C-300 DM-700 EV-760 G-516, G-518 G-521 G-724 G-725
 X1
 Y3-rit

 P-20
 71-33

 P-22
 87-31

 PAM-4
 101-1

 PC-8, PC-358
 99-1

 PM-78
 100-2

 PM-358
 98-1

 PX
 13-35

 PV248
 127-2

 13-35

 REV248
 127-2

 RZU248
 (See Model REV248-Set 127-2)

 SC-448
 62-2

 TD-6
 103-3

 WEU-262
 91--1

 WRA-1A
 47-1

 WRA-4M
 60-1

 XE750
 XP775

 SC4127-30
 93A--1

 XC50, XP775
 93A--1

 Sc4127-30
 S64-1

 Soft 127-31
 78-35-33

 7B
 52--1

 9
 50-2

 7B
 135--33

 9
 52--1

 9
 50--2

 140-31
 14C-Set

 140-31
 14C-Set

 140-31
 140--3

 15
 67-2

 171, 172
 96.--1

 198
 83.--1

 200
 139.--3

 201
 81.--1

 211
 65.--1

 212
 68.--3

 213
 63.--1

 214
 68.--3

 213
 63.--1

 214
 64.---3

 9312
 (See Model 14C.--Set 140.-3)

 9316
 (See Model 14C.--Set 140.-3)

 936
 136.---Set 140.-3)

 2271, 227w
 84-1

 -312 (See Model 14C-Set 140-3)
 336

 -316 (See Model 14C-Set 140-3)
 350

 -358W
 127-3

 -388W
 127-3

 -316 (See Model 14C-Set 140-3)
 361

 -378W
 127-3

 -412 (See Model 14C-Set 140-3)
 372.1F24, 472.P25 (See Model 472.WP25-Set 168-1)

 -472.W215 (See Model 1472.WP25-Set 168-1)
 472.W25-Set 168-1)

 -472.W215 (See Model 472.WP25-Set 168-1)
 472.W25-Set 168-1)

 -472.W72 (See Model 472.WP25-Set 168-1)
 472.W25-Set 168-1)

 -472.W126 (See Model 472.WP25-Set 168-1)
 472.W25-Set 168-1)

 -472.17XUCM, 472.XUCM.1 (Ch. 3)
 472.17XUC, 472.XUCM.3

 -472.17XUCM, 472.XUCM.2 (TC.XUCM.3)
 472.17XUC, 472.XUCM.3

 -472.17XUC, 472.XUCM.3 (Ch. 278)
 586

 -472.17XUC, 472.17XUT, 472.
 223-2

 -472.17XUT.4, 472.17XUT, 472.
 123-2

 -472.17XUT.4, 472.17XUT, 472.
 223-2

 -472.20XUC (Ch. 2208) (See Model 20XUT-Set 185-3)

 -472.20XUC (Ch. 2208) (See Model 20XUT-Set 185-3)

 -472.20XUC (Ch. 321-8).223-2

 -472.21XUCO (Ch. 321-8).223-2

 -472.21XUCO (Ch. 321-8).223-2</td

AIRCASTLE-Cont. • 472.221XC (Ch. 321-D)	2232
● 472.221XT. 472.221XT.1	(Ch.
472.254	223 -2 215 -2
568.205	14-1
568.205-1 (See Model 2)	00-Set
568.305	141-2 55-1
594-935 (See Model 9	
128-2) 602-182144	114-2
603-PR-8.1	114-2 133-2 230-2
604	53-2
	177 3
607.299 607.314, 607.315 607.316, -1, 607.317, -1. 610.637 610.C351 610.CL152B, M 610.D200	122-2
610.A67	247-2
610.CL152B, M	208-1
610.FE-153	
610.F100 610.F151	138-3
610.H400	172-2 178-2 179-2
610.P-651.1 610.S500	184-2
010, W-100	249-2
621 (Ch. FJ-91) 626 641	18-3
651	17-1
652.A25, 652.A35 652.351 652.5C1M, V	15-1 169-2 231-2 260-3 246-1
652.5C1M, V 652.5T3M, V	260—3 246—1
652.5T5E, V	
652. 8TF1	254-1
652.5C1M, V 652.5T3K, V 652.5T5E, V 652.6TFL, V 652.8TF1 652.24875 652.4875 652.505 659.511, 659.513 659.515 6	211-3
652.505 659.511, 659.513	168—2 167—2
659.520E, I 738.85400, UL	185-4
026	250-2 129-2 128-2
9651, W. 965KI, W (See	Model
•1400C, 1400T	140—3 140—3
• 2000C	140-3
•3170 (For TV Ch. See Set for Radio Ch. See Model	140-3,
Set 126-2)	140-3,
for Radio Ch. See Mode	350-
5000 5001	16-2
5002 5003, 5004, 5005, 5006	19-1 20-1
5008, 5009 5010, 5011, 5012 (Ch. 110) 5015,1	46-1
5015.1	118-3 16-3
5020 5022 5024	123-2 45-1
5025 5027	24-2
3027	49 3
5028	49-3
5028	49-3 44-1 51-1 46-2
5028 5029 5035 5036 5044	49-3 44-1 51-1 46-2 72-2 121-2
5028 5029 5035 5036 5044	49-3 44-1 51-1 46-2 72-2 121-2 48-4
5028 5029 5035 5036 5044 5050 5052 5056-A	49-3 44-1 51-1 46-2 72-2 121-2 48-4 45-2 120-2
5028 5029 5035 5036 5036 5044 5050 5052 5055 5056-A 6042	49-3 44-1 51-1 46-2 72-2 121-2 48-4 45-2 120-2 61-1 74-1
5028 5029 5035 5036 5044 5050 5052 50552 50556-A 6042 6050 6050	49-3 44-1 51-1 46-2 72-2 121-2 48-4 45-2 120-2 61-1 74-1 97-1 18-4
5028 5029 5035 5036 5050 5052 5056-A 6042 6050 6050 6053 6514 6541 6544 6541 5541 5541 5541 5541	49-3 44-1 51-1 51-1 121-2 72-2 121-2 48-4 45-2 120-2 61-1 74-1 97-1 18-4 17-2
5028 5029 5035 5036 5050 5050 5055 5055 5055 6042 6050 6050 6053 6054 6541 6544 6544 6541 6544 541 544 544 544 540 540 540 540 540	49-3 44-1 51-1 46-2 72-2 121-2 48-4 45-2 120-2 61-1 74-1 97-1 18-4 17-2 17-2 17-2 2 6431
5028 5029 5035 5036 5050 5052 5056 A 6042 6050 6051 6054 6554 6541 6541 (See Model 6541—Se 6547 6611, 6612, 6613, 6635	49-3 44-1 51-1 46-22 72-2 121-2 48-4 45-22 120-2 61-1 18-4 17-2 97-1 18-4 17-2 17-2 17-2 6631, 15-2
5028 5029 5035 5036 5050 5052 5055 6053 6050 6053 6514 6544 6541 6544 6541 6544 6541 6544 6541 6543 6612, 6613, 6630 6632, 6634, 6635 7000, 7001	49-3 44-1 51-1 46-22 72-2 121-2 48-4 45-22 120-2 61-1 18-4 17-2 97-1 18-4 17-2 17-2 17-2 6631, 15-2
5028 5029 5035 5036 5050 5052 5055 6053 6050 6053 6514 6544 6541 6544 6541 6544 6541 6544 6541 6543 6612, 6613, 6630 6632, 6634, 6635 7000, 7001	49-3 44-1 51-1 46-22 72-2 121-2 48-4 45-22 120-2 61-1 18-4 17-2 97-1 18-4 17-2 17-2 17-2 6631, 15-2
5028 5029 5035 5036 5050 5050 5052 5056-A 6050 6050 6050 6051 6514 6514 6514 6511 6612, 6613, 6630 7000, 7001 7014, 7015 7015 7015	49-3 44-1 51-1 46-2 72-2 121-2 48-4 45-2 120-2 61-1 74-1 97-1 18-4 17-2 17-2 17-2 14-3 19-2 57-3 99-2 57-3 99-2
5028 5029 5035 5036 5050 5050 5052 5056-A 6050 6050 6050 6051 6514 6514 6514 6511 6612, 6613, 6630 7000, 7001 7014, 7015 7015 7015	49-3 44-1 51-1 51-1 72-2 121-2 48-4 45-2 120-2 61-1 74-1 17-2 174-1 17-2 17-3 14-3 19-2 57-3 14-3 19-2 57-3 19-2 57-3 47-2 45-3 997-2 97-2
5028 5029 5035 5036 5050 5050 5052 5056-A 6050 6050 6050 6051 6514 6514 6514 6511 6612, 6613, 6630 7000, 7001 7014, 7015 7015 7015	49-3 44-1 51-1 51-1 72-2 121-2 48-4 45-2 72-1 21-2 48-4 45-2 74-1 17-2 120-2 631, 15-2 14-3 19-2 57-3 14-3 19-2 57-3 19-2 99-2 997-2 997-2 997-2 954-1
5028 5029 5035 5036 5036 5050 5052 5055 6053 6053 6534 6544 6541 6544 6541 6541 6542 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7015	49-3 44-1 51-1 51-1 72-22 121-2 48-4 45-2 120-2 61-1 74-1 74-1 74-1 17-2 14-3 19-2 14-3 19-2 57-3 19-2 97-2 97-2 97-2 97-2 97-2 97-2 97-2 9
5028 5029 5035 5036 5036 5050 5052 5055 6053 6053 6534 6544 6541 6544 6541 6541 6542 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7015	$\begin{array}{r} 49 \\ -3 \\ 44 \\ -1 \\ 51 \\ -1 \\ 51 \\ -1 \\ -1 \\ -1 \\ -1$
5028 5029 5035 5036 5050 5050 5055 5055 6053 6054 6042 6054 6541 6544 6541 6544 6541 6542 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7004 7015 7015 Forly 7055 7008 9008	$\begin{array}{r} 49 \\ -3 \\ 44 \\ -1 \\ 51 \\ -1 \\ 51 \\ -1 \\ -1 \\ -1 \\ -1$
5028 5029 5035 5036 5050 5052 5055 6052 5055 6052 6054 6054 6054 6314 6417 6417 6417 6417 6417 6417 6417 6437 7004 7004 7004 7004 7004 7015 7015 7015 7015 7015 7015 7015 7014 7015	$\begin{array}{r} 49 \\ -3 \\ 44 \\ -1 \\ 51 \\ -1 \\ 51 \\ -1 \\ -1 \\ -1 \\ -1$
5028 5029 5035 5036 5036 5050 5052 5055 6042 6042 6043 6044 6344 644 644 644 644 644 644	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 121 = 2 \\ 12$
5028 5029 5035 5036 5050 5050 5052 5055 6052 5055 6052 5055 6054 6054 6514 6514 6514 6514 6617 6612, 6613, 6635 7000, 7001 7004, 7015 7015 7015 7015 7015 7014, 7015 7015 7015 7014 7015	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 12 = 2 \\ 72 = 2 \\ 121 = 2 \\ 72 = 2 \\ 121 =$
5028 5029 5035 5036 5050 5050 5052 5055 6052 5055 6052 5055 6054 6054 6514 6514 6514 6514 6617 6612, 6613, 6635 7000, 7001 7004, 7015 7015 7015 7015 7015 7014, 7015 7015 7015 7014 7015	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 121 = 2 \\ 44 = 1 \\ 44 = 1 \\ 44 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 48 = 2 \\ 121 = 2 \\ 48 = 2 \\ 121 = 2 \\ 48 = 2 \\ 121$
5028 5029 5035 5036 5050 5050 5050 5050 5050 5050 5050 5050 5050 5050 5050 5051 5052 5050 6051 6051 6514 6514 6514 6514 6514 6517 6617 6617 6617 6617 6617 6617 6617 6617 6617 6617 6617 6617 6617 7000 7000 7001 7002 7003 7004 7014 7002 70003 70004 70020	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 121 = 2 \\ 46 = 2 \\ 72 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 2 \\ 121 = 2 \\ 121 = 2 \\ 48 = 2 \\ 121 = 2 \\ 12$
5028 5029 5035 5036 5036 5050 5052 5056-A 6042 6050 6053 6514 6541 6544 6541 6544 6541 6542 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7015 Forly 7053 7005 7015 Forly 7053 90081, 9008W 90121, 9012W 10003-1 10003-1 10021-1, 10022-1 10023 10024-1 108014, 108504 121124 127084 138124 138124 138124 139114 (See Model 1391 59-41 147114	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 121 = 2 \\ 46 = 2 \\ 72 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 2 \\ 121 = 2 \\ 121 = 2 \\ 48 = 2 \\ 121 = 2 \\ 12$
5028 5029 5035 5036 5036 5050 5052 5055 6052 5055 6054 6054 6544 6544 6544 6544 6647	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 121 = 2 \\ 46 = 2 \\ 72 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ $
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5028 5029 5035 5036 5036 5050 5052 5055 6053 6053 6514 6544 6544 6544 6544 6544 6544 654 65	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 48 = 4 \\ 45 = 2 \\ 48 = 4 \\ 45 = 2 \\ 48 $
5028 5029 5035 5036 5036 5050 5052 5056-A 6042 6050 6053 6534 6544 6541 6544 6541 6544 6541 6544 6541 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7017 7015 7017	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 151 = 1 \\ 46 = 2 \\ 72 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 2 \\ 48 = 2 \\ 48 = 2 \\ 121 = 2 \\ 1$
5028 5029 5035 5036 5036 5050 5052 5056-A 6042 6050 6053 6534 6544 6541 6544 6541 6544 6541 6544 6541 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7015 7017 7015 7017	$\begin{array}{c} 49 = 3 \\ 44 = 1 \\ 51 = 1 \\ 151 = 1 \\ 46 = 2 \\ 72 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 4 \\ 45 = 2 \\ 121 = 2 \\ 48 = 2 \\ 48 = 2 \\ 48 = 2 \\ 121 = 2 \\ 1$
5028 5029 5035 5036 5036 5050 5052 5055 6050 6053 6053 6053 6053 6053 6054 7055 6054 7055 6056 70555 70555 70555 705555 705555 705555 7055555 705555555555	49-3 44-1 51-1 51-1 21-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-2 45-3 17-2 48-4 17-2 17-2 48-4 17-2 17-2 48-4 17-2 17-2 48-4 45-2 17-2 48-4 17-2 17-2 48-2 45-3 57-1 17-2 45-3 58-2 57-4 40-2 45-3 58-2 57-4 40-2 45-2 57-4 40-2 45-2 57-4 40-2 45-2 57-4 40-2 45-2 57-1 58-2 57-4 40-2 45-2 57-4 58-2 57-4 58-2 57-4 40-2 45-2 57-4 58-2 57-4 58-2 57-4 40-2 57-2 58-2 57-4 40-2 57-2 58-2 57-4 40-2 57-2 58-2 57-4 58-2 57-4 40-2 57-4 58-2 57-4 40-2 57-4 58-2 57-4 40-2 57-4 58-2 57-4 58-2 57-4 40-2 55-2 57-4 40-2 55-2 57-4 40-2 55-2 57-4 40-2 55-2 57-4 58-2 55-2 57-4 40-2 55-2 57-4 58-2 55-2 57-4 58-2 55-2 57-4 55-2 57-4 58-2 55-2 57-4 57-2 57-4 57-2 57-4 57-2 57-4 57-2 57-4 57-2 57-4 57-2 57-2 57-4 57-2 57-2 57-2 57-4 57-2 57-2 57-2 57-4 57-2 57-2 57-2 57-2 57-2 57-2 57-2 57-2
5028 5029 5035 5036 5036 5050 5052 5056 6050 6053 6053 6053 6053 6054 705 6054 7055 6054 7055 6054 70555 7055 7055 7055 7055 70555 7055 7055 7055 7055 7055	49-3 44-1 51-1 51-1 21-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-2 45-3 17-2 48-4 17-2 17-2 48-4 17-2 17-2 48-4 17-2 17-2 48-4 45-2 17-2 48-4 17-2 17-2 48-2 45-3 57-1 17-2 45-3 58-2 57-4 40-2 45-3 58-2 57-4 40-2 45-2 57-4 40-2 45-2 57-4 40-2 45-2 57-4 40-2 45-2 57-1 58-2 57-4 40-2 45-2 57-4 58-2 57-4 58-2 57-4 40-2 45-2 57-4 58-2 57-4 58-2 57-4 40-2 57-2 58-2 57-4 40-2 57-2 58-2 57-4 40-2 57-2 58-2 57-4 58-2 57-4 40-2 57-4 58-2 57-4 40-2 57-4 58-2 57-4 40-2 57-4 58-2 57-4 58-2 57-4 40-2 55-2 57-4 40-2 55-2 57-4 40-2 55-2 57-4 40-2 55-2 57-4 58-2 55-2 57-4 40-2 55-2 57-4 58-2 55-2 57-4 58-2 55-2 57-4 55-2 57-4 58-2 55-2 57-4 57-2 57-4 57-2 57-4 57-2 57-4 57-2 57-4 57-2 57-4 57-2 57-2 57-4 57-2 57-2 57-2 57-4 57-2 57-2 57-2 57-4 57-2 57-2 57-2 57-2 57-2 57-2 57-2 57-2
5028 5029 5035 5036 5036 5050 5052 5056-A 6042 6050 6053 6544 6541 6544 6541 6544 6541 6544 6541 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7004 7004, 7015 7015 6011, 6612, 6613, 6630 7004 7004, 7015 7015 7015 60081, 9008W 90091, 9008W 9008W 9008W 9008W 9008W 9008W 9008W 9008W 9008W	49-3 44-1 51-1 51-1 21-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-2 45-3 17-2 120-2 48-2 120-2 48-2 121-2 48-2 121-2 45-3 17-2 45-3 57-1 17-2 2 45-3 58-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 58-2 55-2 55-2 55-2 55-2 55-2 55-2 55-2
5028 5029 5035 5036 5036 5050 5052 5056 6053 6053 6053 6054 6042 6050 6053 6054 6044 6050 6053 6054 6054 6054 6054 6054 6054 6054 6054 7000 7000 7000 7004 7015	49-3 44-1 51-1 51-1 21-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-2 45-3 17-2 45-3 57-1 17-2 45-3 57-4 17-2 45-3 58-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 58-2 57-4 45-2 57-2 58-2 57-4 58-2 55-2 55-2 55-2 55-2 55-2 55-2 55-2
5028 5029 5033 5044 5050 5052 5055 6050 6053 6053 6054 6042 6050 6053 6054 6044 6541 6541 6544 6541 6611, 6612, 6613, 6630 6632, 6634, 6635 7000, 7001 7014, 7015 7015 7015, 7001 7014, 7015 7005 7007 7015, 7001 7015, 7001 7015, 7001 7015, 7001 7015, 7001 7002, 10022, 10002 10002, 1, 10022, 1 10022, 1 10023, 1 10024, 1 10024, 1 10024, 1 10024, 1 10024, 1 10025, 1 10025, 1 10022, 1 10022, 1 10025, 1 10022, 1 1002, 1 1002, 1 1002, 1 1002, 1 10	49-3 44-1 51-1 51-1 21-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-2 45-3 17-2 45-3 57-1 17-2 45-3 57-4 17-2 45-3 58-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 45-2 57-4 58-2 57-4 45-2 57-2 58-2 57-4 58-2 55-2 55-2 55-2 55-2 55-2 55-2 55-2
5028 5029 5035 5036 5050 5052 5055 6050 6053 6053 6054 6050 6053 6053 6054 6054 6054 6054 6054 6054 6054 6054 6054 6054 6054 6054 6054 6054 6055 6054 72 6055 6056 6054 72 70 70 70 70 70 70 70 70 70 70	49-3 44-1 51-1 51-1 21-2 48-4 45-2 121-2 48-4 45-2 121-2 48-4 45-2 121-2 48-2 45-3 17-2 17-2 48-3 17-2 45-3 19-2 57-3 47-2 45-3 19-2 57-4 47-2 45-3 57-3 99-2 97-2 14-3 99-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 99-2 97-2 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 14-3 97-2 97-2 14-3 97-2 97-2 97-2 97-2 97-2 97-2 97-2 97-2

AIR KING-Cont. A-604	AIR 150
A-625	1. B
A-1000, A-1001 58-3	154
A 100	15V 15V 15V
A2000, A2001 2002 (See Model A2000—Set 75-2) A2010	157
A2012 (See Model A1001A-Set 75-2)	154
1211, 1212 (See Model 16C1-Set 1213)	15V 2
75-2) 1/2CI (See Model 16C1—Set 121-3) 1/2TI, 12T2 (See Model 16C1—Set 121-3) 1/4TI (See Model 16C1—Set 121-3) 1/6CI, 16C2, 16C5	S
•16M1	15V 2 15V 2
16TIB (See Model 16C1 — Set 121-3)	• 15¥
16M1 121-3 16T1 121-3 16T1 121-3 17C2 16C, 700-96) 17C5, 8 (Ch. 700-96) 151-2 17C7, 70, 700-96) 151-2 17C7, 700-96) 151-2 17K1 150-2 17K1 16C, 700-96) 151-2 151-2 17K1 16C, 700-96) 150-2 151-2 17K1 16C, 700-96) 150-2 151-2 17K1 16C, 700-96) 150-2 151-2 17K1 16C, 700-96) 151-2 151-2 17K1 16C, 700-96) 151-2 151-2 17K1 16C, 700-96) 151-2 20K1 171 16C, 700-93) 151-2 20K1 171 151-2 171 151-2 171 151-2 170H 151-2 170H 151-2 170H 151-2	 15v 15v 15v
17K1 (Ch. 700-96)151-2	•15V 25B
150-2 17M1 (Ch. 700-96) 151-2	25B
17T1 (Ch. 700-96)	25B
• 20C1, 20C2 (Ch. 700-93). 151-2 • 20K1 (Ch. 700-95)	•258 •258 •258
• 20M1 (Ch. 700-93)151-2 • 718R	250
• 2017k	250
4603	250 250 250 250 250 250 250 250 250 250
4604 4-25 4704D (See Model 4604—5et 4-25) 4607, 4608 3-1	250
	250
4609, 4610 (Late) 11-2 4625	250
4/04	250 1 250
4705, 4706	• 250
AIR KNIGHT (5KY KNIGHT) CA-500	• 250 • 250
CB-500P 17-31 N5-RD291 17-3	
	250 3
35BR-3158A—Set 221-2) BR-3091A (See Model 35BR-3158A	250 250
AIKLINE BR-3082A, BR-3084A (See Model 35BR-3158A—Set 221-2) BR-3091A (See Model 35BR-3158A —Set 221-2) BR-3182A (See Model 35BR-3158A —Set 221-2) CE50724 CSE 1078A 25D 2	250
-Set 221-2) GSE-1077A, GSE-1078A250-3	25V B 25V
248-1 and Model 35GSE-3076A-	25
 GSE-3178A, B (See PCB 102—Set 248-1 and Model 35GSE-3078A— 	5 25\ 25\
	25V 2 25V
248-1 and Model 350St-3095- Set 238-3) GSE-3197A (See PCB 102-Set 248-1 and Model 350St-3097- Set 238-3) GSL-304C (See Model 35GSL- 3064A-Set 218-3) GSL-304C (See Model 35GSL- 3083A-Set 218-3) WG-157C	25
248-1 and Model 35GSE-3097- Set 238-3)	• 25\
•GSL-3064C (See Model 35GSL- 3064A-Set 218-3)	•25\ •25\
• GSL-3083C (See Model 35GSL- 3083A-Set 218-3)	3 • 25\ • 25\
Juli Jack - Ser 218-3 WG-1572	• 25\ • 25\ • 25\ • 25\ • 25\ • 25\
3075D, E, WG-3077D, E, WG- 3079D, E (See PCB 95-Set 240-1	2
and Model 25WG-3066A—Set 206-2)	•25V
206-2) •WG-3180A (For TV Ch. only See Model 35WG-3171A—Set 222-3) •WG-3190A (For TV Ch. only See Model 35WG-3171A—Set 222-3)	• 25\ • 25\ 2
Model 35WG-3171A-Set 222-3) • 05BR-30218	S
● 058R-3024B 150—3 ● 058R-3027A 150—3	• 25 • 25 • 25
• 05BR-3041A	358
05GAA-992A 125—2 05GCB-1540A, 05GCB-1541A 131—2 •05GCB-3019A 116—2 05GCD-3658A 151—3	• 35E • 35E 3
05GHM-934A 167—3	356
05GHM-1061A	350
•05GSE-3037A	350
• 05GSE-3037A	350 350 350
05WG-1811B (See Model 94WG- 1811A-Set 99-4)	350
05WG-1813A	350
05WG-2748F 139—4 05WG-2749D 129—3 05WG-2752 100—3 05WG-3016A, B (See Set 100-2 and	L
05WG-2752	350 L
000m0-0000m	350
Model 94WG-3006A-Set 72-4) 05WG-3030A 1193 05WG-3030C 148-2 05WG-3031A 1091 05WG-3036A 148-2 05WG-3036A 5 148-2 05WG-3036A 05WG-3036A 1294 05WG-3038A 1294	350
005WG-303YA, 5	• 350
•05WG-3045A	• 350
145-2	• 350 • 350
15BR-1547A	25
158R-27568, 158R-2757A .148-3 • 158R-3035A	• 350 2 5
•15BR-3053A, B	• 350 • 350
15GHM-934A	350
15GHM-936A, 15GHM-937A 134-2	350
15GHM-1070A	• 350

RLINE-Cont.

GSL-1564A, B, 15GSL-1565A, B, 5GSL-1566A, B, 15GSL-1567A, 169—3 351-1504A, E, 1505-3551-1566A, B, 1505-3051-1566A, B, 1506-1546A, B WG-1545A, B, 15WG-1546A, B WG-2749E, F, 151-4 WG-2752D, E, 151-4 144-2 - Set
 SGHM.-938A
 230-4

 SGHM.-938A
 252-4

 SGHM.-9418,
 242-2

 SGHM.-9418,
 242-2

 SGHM.-9418,
 174-3

 SGSE-13556,
 174-3

 SGSE-13556,
 174-3

 SGSE-13568,
 See Model 23GSE

 SGSE-30524,
 25GSE-3063A,

 SGSE-3062A,
 25GSE-3063A,

 SGSE-3063A,
 123-2

 SGSE-3063A,
 123-2

 SGSE-3063A,
 149-2

 SGSE-3063A,
 149-2

 SGSE-3063A,
 149-2

 SGSE-3063A,
 149-2

 SGSE-3063A,
 189-2

 SGSGS-2016A,
 225-2

 SGSE-3063A,
 189-2

 SGSGS-2016A,
 189-1

 SGSGS-2016A,
 189-1

 SGSGS-2016A,
 189-1

 SGSGSC-2
 1359A
 231-2

 1359A
 221-2

 3167A
 336R-3168A

 3167A
 328-2

 3167A
 328-2

 3167A
 221-2

 388-3167A
 328-2

 3167A
 221-2

 388-3168A
 328-2

 3167A
 238-2

 3367A
 221-2

 388-3168A
 338-2

 3367A
 238-2

 3367A
 235-2

 3367A
 235-2

 3367A
 235-2

 367A
 232-4

 367A
 236-4

 367A</ BR-3158A BR-3167A, 35BR-3168A GMD-3309A (Late Version) Tel. UHF Conv. (Similar to Chassis) 194-8
 JGSE-13507A
 (Edit Verticin)
 1611

 JUHF Conv.
 194
 504

 JGSE-1355C
 [See Model 25GSE-1355A-Set 174-3]
 1053A-Set 174-3]

 JGSE-1355C
 [See Model 25GSE-1355A-Set 174-3]
 1053A-Set 174-3]

 JGSE-1356C
 [See Model 25GSE-3053A-Set 175-2]
 238-3

 JGSE-3076A
 238-3
 35GSE-3076A

 JGSE-3076A
 238-3
 35GSE-3063A-Set 195-2]

 JCSE-30076A
 (See PCB 72-Set 212-1 and Model 25GSE-3003A-Set 195-2]
 35GSE-3003A

 JGSE-30076A
 (See PCB 72-Set 212-1 and Model 25GSE-3003A-Set 195-2]
 35GSE-3007A

 JGSE-30076A
 (See PCB 72-Set 212-1 and Model 25GSE-3003A-Set 195-2]
 35GSE-3007A

 JGSE-3007A
 (See Model 25GSE-3003A-Set 195-2]
 35GSE-3007A

 JGSE-3007A
 (See Model 35GSC-2016A-238-3)
 35GSC-2016A

 JGSE-3007A
 (See Model 35GSC-2016B-225-2)
 35GSC-2016B
 225-2)

 JGSE-2016A
 (See Model 35GSC-2016B-225-2)
 35GSC-2016B
 225-2)

 JGSL-3004A, B
 218-3
 35GSL-3064A, B
 218-3

 15GHM-936A,
 15GHM-937A
 35GS-2016
 225-2

 134-2
 35GSC-2016
 249-3

 15GHM-1070A
 184-3
 35GSC-3064A,
 218-3

 15GSE-2764A
 165-4
 •35GSC-3083A,
 8
 218-3

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

A-511, A-512 A-520 A-600

www.americanradiohistory.com

30-2 49-4

AIRLINE-Cont. 35WG-13708, C, 35WG-15718, 35WG-13728 (see Model 25WG-1570A-Set 177-4) 35WG-2741C, D (see Model 15WG-2745C-Set 130-2) 35WG-2745F, G (see Model 15WG-2745C-Set 130-2) 35WG-3070B, (see PCB 92-Set 237-1 and Model 25WG-3070A-Set 212-2) 35WG-3070B, (see PCB 92-Set 237-1 and Model 25WG-3070A-Set 212-2) 35WG-3070B, E, F (See PCB 92-Set 240-1 and Model 25WG-307A-Set 206-2) 35WG-3070D, E, F (See PCB 96-Set 240-1 and Model 25WG-3073A-Set 206-2) 35WG-3073D, E, F (See PCB 96-Set 240-1 and Model 25WG-3073A-Set 206-2) 35WG-3177A, B. 222-3 35WG-3177A, B. 222-3 35WG-3177A, B. 222-3 35WG-3175A, 222-3 35WG-3175A, Set 206-2) 35WG-3175A, Set 206-2) 35WG-3175A, Set 206-2, 35WG-3175A, AIRLINE-Cont. 61-6782 (Similar to Chassis) 61-6782 (Similar to Chassis) 61-6783 (Similar to Chassis) 61-6783 (Similar to Chassis) 146-3 146-3 1-6783 (Similar to Chassi) 10-6784 (Similar to Chassi) 61-6787 174-4 61-6787 256-6 61-6787 236-2 61-6793 237-2 61-6795 237-2 61-6795 232-3 61-6795 242-3 61-12601 241-3 6488-916A 3-34 S1 - 6795 242--3 5(1-1200) 241--3 5(4) S6 - 1200 241--3 5(4) 3--34 468-9(164) 3--34 468-9(164) Set 17-5) Set 0461 748R-9(164) 3--34 468-9(174) 10--1 1 Set 87-9(175) 10--1 1 10-1 1 2-32 468-1051A 2-32 468-1051A 2-32 468-1205A 468-1206A 10--3 468-1205A 16--4 468R-1503B, 648R-1504B (See Model el 548R-1503A-Set 3-4) 648R-1514A, B, 648R-1513A, B, 648R-1513A, B, 648R-1514A, B, 648R-1514A, B, 648R-1514A, B, 648R-1514A, B, 648R-1605A 16--5 2300A-054 4-13 44WG-2700A, B See Model 54WG-2300A-054 4-13 74BR-105B-174BR-1314B 24-4 74BR-1012B-24-20 74BR-1012B-24-20 74BR-2001A (See Model 74BR-2001B-5et 23-2) 74BR-2001A (See Model 74BR-2001B-5et 23-2) 74BR-2702A (See Model 74BR-702B-201A 24-5 74BR-2702A 54 74BS-2702A 54 74BS-2702B 25-3 74BS-2702A 54 74BS-2702A

AIRLINE-Cont. AMBA5SADOR-Cont.

 PARK-1980-20076
 J-WG-20078
 J-WG-20075
 J-WG-20075
 J-WG-20075
 J-WG-20075
 J-WG-20075
 J-WG-20075
 J-WG-20075
 J-WG-20075
 J-WG-20108
 J-WG-201
 ALDENS
 IlidG, 11/G, 12/G (Similar to Chossis)
 Id2-7

 Ito Chossis)
 162-7
 Id2-7

 ALGENE
 22-3
 AR5U
 22-4
 ALLIANCE ALLSTATE ALTEC LANSING ALC-101 • ALC-205, ALC-206 A3238 A323C A-333A A-433A 303A 84-2 105-3 66-2 84-2 165-5 165-5 165-5 AMBA55ADOR • AM17C, CB, CIM, PT, TIM 171-• AM20C, T 171-• A17CS, A17TS (See Model 20PC Set 178-3)

AMBA5SADOR-Cont.	1
 A20CS (See Model 20PC — Set 178-3) 	
•A21QDCS (See Model 20PC—Set 178-3) •A24QDCS (See Model 20PC—Set	
A24QDCS (See Model 20PC-Set	
178-3) A-9121-A -AX (See Model 2102A	1
Set 191.41	
• CD2020	
	1
175-2)	
C2050 (See Model C1/20-Set 175-2) C2052 (See Model T1853-Set 197-3)	
C2150 (See Model C1720-Set	
•C2150 (See Model C1720—Set 175-2) •C2152, A (See Model T1853—Set 197-3)	
●C2155 (See Model T1853—Set 197-3)	
197-3) •C2420	
• PL17CB, CG, PG, TM171-2	
• 11720	
• 14MC, MT	1
■ 14MC, MT	
MXTS	
• 17MC, MT, MXC, MXCS, MXT, MXTS	
•17MC (2nd Prod.), MC5, MT (2nd Prod.), MT5	
A 17PC 17PCS (See Model 20PC-Set	
178-3) •17PT, 17PTS (See Model 20PC—Set	
170-3) • 17PT, 17PTS (See Model 20PC—Set 178-3) • 20C	
• 20C	
178-3) 200C 173-2 200C, MCS, MT, MTS 173-2 200C, 20PCS, 20PCS, 178-3 200C, 20PCS, 20PTS (See Model 20CC-Set 178-3 21CD2A, B (See Model 21C2A-Set 191-4 21C2A, 21C2AL0 191-4 223P 172-2	
20PC-Set 178-3)	
•21CD2A, B (See Model 21C2A—Set 191-4)	
•21C2A, 21C2AL0	
191-41 21C2A, 21C2AL0 171-2 921 (Sae Model 21C2A-Set 191-4) 9120, LO 191-4 9121, M, LO, XB (See Model 21C2A -5et 191-4) 9220, LO 9241, M, LO, XB (See Model 21C2A)	
•9120, LO	
A MAC (A MACEE)	
•1C23 (Similar to Chassis)139-11	
Old Similar to Chassis)126—8 Old Similar to Chassis)126—8	
• 17C, CB (Similar to Chassis) 126-8	
Ame (Almee) 1/23 (Similor to Chassis)139-11 1/272 (Similor to Chassis)1268 1/71 (Similor to Chassis)1268 1/7C, CB (Similor to Chassis)1268 1/7CG, 1/7C3 (Similor to Chassis)	•
 17T (Similar to Chassis)126—8 17TG (Similar to Chassis)149-13 	•
•17720 (Similar to Chassis). 139-11	
• 20CD2A, -1	•
■17CG, 17C3 (Similar to Chossis) 149–13 ■17T (Similar to Chossis), 149–13 ■17TG (Similar to Chossis), 149–13 ■17T20 (Similar to Chossis), 149–13 ■20CD 28 (imilar to Chossis), 149–13 =20CD28 (Early) (See Model 20C2A —Set 188-3) =20CC28 (Early) (See Model 20C2A =20C1 (Similar to Chossis), 149–13 =20CC28 (Early) (See Model 20C2A Set 188-3) =20C28 (Early) (See Model 20C2A Set 188-3)	
•20CD2B (Late)	
• 20C1 [Similar to Chassis]149-13 • 20C2A, -1	
20C2B (Early) (See Model 20C2A— Set 188-3)	
Set 188-3) 20C28 (Late)	1
• 20D, DB (Similar to Chassis), 139-11	
• 20TG (Similar to Chassis)149–13 • 20T24 -1 188–3	
• 20T2B (Early) (See Model 20C2A-	
Set 188-3) 20128 (Lote) 252—2 20121 (Similar to Chossis). 139—11 21CD2A (Early) (See Model 20C2A -Set 188-3) 21C2A (Early) (See Model 20C2A Set 188-3) 21C2A (Lote) -Set 188-3) 21C2A (Lote)	
 20T21 (Similar to Chassis). 139-11 21CD2A (Early) (See Model 20C2A 	
Set 188-3) •21(D24 (late) 252-2	
• 21C2A (Early) (See Model 20C2A-	
Set 188-3) •21C2A (Lote)	
•24T2A, -1	1
111_3	
125P	-
AMERICAN COMMUNICATIONS	
(See Liberty)	
AMPEX (See Recorder Listing)	1
AMPLIFIER CORP.	
OF AMERICA ACA-100DC, ACA-100GE . 63-2	•
ACA-100DC, ACA-100GE . 63-2 AMPLIPHONE	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE 63-2 AMPLIPHONE 10 21-1 20 21-12 AMPRO (See Recorder Listing)	
ACA-100DC, ACA-100GE . 63—2 AMPLIPHONE 10	
ACA-100DC, ACA-100GE . 63—2 AMPLIPHONE 10	
ACA-100DC, ACA-100GE . 63—2 AMPLIPHONE 10	
ACA-100DC, ACA-100GE 63—2 AMPLIPHONE 10 21—1 20 21—1 20 21—1 21—12 AMPRO (See Recorder Listing) ANDREA BT-VK12 76—5 BC-VL17 (Ch. VL17) (See Model C-VL17-Set 152-1) CO-VL15 Set 152-1) CO-VL15 (Ch. VL17) (See Model C-VL17-Set 152-1) CO-VL15 (Ch. VL17) (See Model (Also see PCB 8—Set 112-1) CO-VL16 (Ch. VL16) 125—3 CO-VL19 (Ch. VL16) 125—3 CO-VL19 (Ch. VL17) 126—3 CO-VL19 (Ch. VL17) 126—3 C-VL17 (Ch. VL17) 126—1 C-VM21 (Ch. VM21) 204—3 C-VM21 (Ch.	
ACA-100DC, ACA-100GE 63—2 AMPLIPHONE 10 21—1 20 21—1 20 21—1 21—12 AMPRO (See Recorder Listing) ANDREA BT-VK12 76—5 BC-VL17 (Ch. VL17) (See Model C-VL17-Set 152-1) CO-VL15 Set 152-1) CO-VL15 (Ch. VL17) (See Model C-VL17-Set 152-1) CO-VL15 (Ch. VL17) (See Model (Also see PCB 8—Set 112-1) CO-VL16 (Ch. VL16) 125—3 CO-VL19 (Ch. VL16) 125—3 CO-VL19 (Ch. VL17) 126—3 CO-VL19 (Ch. VL17) 126—3 C-VL17 (Ch. VL17) 126—1 C-VM21 (Ch. VM21) 204—3 C-VM21 (Ch.	
ACA-100DC, ACA-100GE 63—2 AMPLIPHONE 10 21—1 20 21—1 20 21—1 21—12 AMPRO (See Recorder Listing) ANDREA BT-VK12 76—5 BC-VL17 (Ch. VL17) (See Model C-VL17-Set 152-1) CO-VL15 (Ch. VL17) (See Model C-VL17-Set 152-1) CO-VL15 (Ch. VL17) (See Model (Also see PCB 8—Set 112-1) CO-VL15 (Ch. VL16) (25—3 CO-VL19 (Ch. VL16) (25—3 CO-VL19 (Ch. VL17) 152—1 CO-VL19 (Ch. VL17) 152—1 CVL16 (Ch. VL16) 125—3 C-VL17 (Ch. VL17) 152—1 CVL16 (Ch. VL16) 125—3 C-VL17 (Ch. VL17) 152—1 C-VL17 (Ch. VL17) 152—1 C-VM21 (Ch. VM21) 204—3 C-VM21 (C	

ANDREA-Cont. ANSLEY 32 41 (Paneltone) 53 5-27 4-38 24-8 71-6 APEX 485 192A 817, 920, 924 9120, 9121 9820, 98208, 9821 17-6 181-3 181-3 181-3 APPROVED ELECTRONIC INSTRUMENT CORP. FM Tuner A-600AC A710 41-2 175-4 177-5 176-2 175-5 A-800 A-850 ARC 601 25-5 ARCADIA 37D14-600 9-3 ARLINGTON 30114A-056 (Similar to Chassis) 119-33 38112A-058 (Similar to Chassis) 31871 (Similar to Chassis), 85-3 31814 (Similar to Chassis), 85-3 318145 (Similar to Chassis), 85-3 31814-872 (Similar to Chassis) 85-3 31814-872 (Similar to Chassis) 85-3 ARLINGTON Salta-872 (Similar to Chassis) Salta-872 (Similar to Chassis) Salta-350 (Similar to Chassis) Salta-350 (Similar to Chassis) Salta-360 (●518T6A (Similar to Chassis) ●518T9A-918 (Similar to Chas 78 assis) R_4 S181/0A-916 Similar 78-4 \$518110A-916 (Similar to Chassis) 78-4 \$231876A-954 (Similar to Chassis) 85-3 \$231879A-912 (Similar to Chassis) 85-4 \$2321MS39A (Similar to Chassis) 226-11 ARTHUR ANSLEY SP-1 TP-1 60-4 ARTONE ARC21 ARC71 ARD21 205-3 A:: ARD2: AR14L, AR1: AR21 AR21 AR237V-1 MST12, MST14 MST12, MST14 TCD (1st Prod.) TCDR (1st Prod.) TCRR (1st Prod.) TCRR (1st Prod.) TCRR (2nd Prod.) TCRR (2nd Prod.) DCDC (2nd Prod.) 20CD (1st Prod.) 20CD (1st Prod.) 20CD (2nd Prod.) 20CD (2nd Prod.) 20CD (2nd Prod.) 20CB (2nd 170—4 76—7 170—4 172—3 170—4 170—4 1000, 1001 3163CR 8163CR, 8193CM ARVIN 15-550KB-UHF 262 150-TC, 151-TC, (Ch. RE-200 150-TC, 151-TC, (Ch. RE-200 150TC, 151-TC, (Ch. RE-220 150TC, 151TC, (Ch. RE-220 150TC, 151TC, (Ch. RE-231) (Ch. 153T (Ch. RE-232). 33-11 (Ch. RE-232). 49-5 182TFM (Ch. RE-237). 32-32 240-9 (Ch. RE-237). 32-32 240-P (Ch. RE-237). 32-32 240-9 (Ch. RE-237). 32-32 240-P (Ch. RE-237). 32-32 240-9 (Ch. RE-237). 32-32 240-P (Ch. RE-237). 42-32 347 2547, 2547, 255-9 47-33 250-9 (Ch. RE-235), 64-22 280TFM, 263T (Ch. RE-255), 64-22 280TFM, 263T (Ch. RE-255), 64-22 280TFM, 263T (Ch. RE-274), 44-23 241T

AIRLINE-ARVIN

ARVIN-Cont.
 352-FL, 352-FL, 352-FL, 352-FL, 352-FL, 352-FL, 352-FL, 352-FL, 354-FL, 355-FL,
 360TFM,
 361TFM,
 (Ch. 8E-260)

 70-2
 70-2

 440T (Ch. 8E-278)
 96-3

 441T (Ch. 8E-278)
 96-3

 441T (Ch. 8E-278)
 96-3

 441T (Ch. 8E-278)
 96-3

 444 (Ch. 8E-278)
 34-2

 444 (A44A (Ch. 8E-200)
 1-3

 444A, 444A (Ch. 8E-200)
 1-3

 4467 (Ch. 8E-280)
 106-2

 450T, 451T (Ch. 8E-284)
 107-3

 462-CE, 462-CM (Ch. 8E-287-1)
 116-3

 480TFM, 481TFM (Ch. 8E-284)
 107-4

 482CFB, 482CFM (Ch. 8E-288-1)
 107-4

 482CFB, 482CFM (Ch. 8E-288-1)
 117-4

 442 (Ch. 8E-278)
 117-4

 353 (Ch. RE-308)
 159-4

 353 (Ch. RE-308)
 153-3

 358 (Ch. RE-301)
 153-3

 358 (Ch. RE-302)
 153-3

 358 (Ch. RE-201)
 153-3

 358 (Ch. RE-202)
 153-3

 588 (Ch. RE-202)
 153-3

 588 (Ch. RE-202)
 151-3

 591 (TM. (Ch. RE-313)
 152-2

 591 (TM. (Ch. RE-321)
 155-4

 552 (P. Ch. RE292)
 (See Model

 650 (P. Ch. RE292)
 (See Model

 650 (P. Ch. RE292)
 175-6

 651 (Ch. RE-321)
 251-3

 655 SWT (Ch. RE327)
 187-2

 655 (Ch. RE327)
 187-2

 655 (Ch. RE327)
 186-5

 644 (64A (Ch. RE-306)-1)
 29-2

 655 (Ch. RE327)
 18-10

 7401 (Ch. RE323)
 225-4

 7413 (Ch. RE332)
 225-4

 7453 (Ch. RE-342)
 223-3

 7607 (Ch. RE-342)
 223-3

 7607 (Ch. RE-375)
 223-3

 7607 (Ch. RE-375)
 224-3

 8054 (Ch. RE-375)
 226-3

 8054 (Ch. (Also see ros 20 2121TM (Ch. TE280-2, TE-280-3) (Also see PCB 20-26 st 134-1) 2122TM (Ch. TE-280, 211) 2122TM (Ch. TE-280-2, TE280-3) (Also see PCB 20-5et 134-1) ■1231M (Ch. TE-28-2, TE28-3) (Aliso see PCB 20—Set 134.1) 120—3 124CCM (Ch. TE289-2, TE289-3) (Aliso see PCB 20—Set 134.1) 120—3 126CM (Ch. TE289-2, TE-289-3) (Aliso see PCB 20—Set 134.1) 120—3 2140, 2161, 2162, 2164 (Ch. TE-290) 126—3 2100, 2161, 2162, 2164 (Ch. TE-290) 126—3 2100, 2161, 2162, 2164 (Ch. TE-290, 126—2 2100, 2161, 2162, 2164 (Ch. TE-290, 126—2 3100TM, 3100TM, 3120-TM, 3121TM (Ch. TE-272-1, TE- 272-2), TE-280, 20- 3130CM (Ch. TE-276) 93—2 3130CM (Ch. TE-276) 93—2 408DT (Ch. TE282) 104—2 408DT (Ch. TE282) 104—2 408DT (Ch. TE-286)... 130—3 5170CB (Ch. TE-302) (See Model 5170CB) 5170, 576 (Ch. TE-302)... 179—3 \$204CM, 5204CM (Ch. TE-302)... 179—3 \$204CM, 5204CM (Ch. TE-303)... 149—3 \$210, 5211, 5212 (Ch. TE-315, 1, ..., 4, -514, 517
 (Ch. TE-305, -- 149—3 \$210, 5211, 5212 (Ch. TE-315, 1). ..., 4, -514, 517
 (Ch. TE-302)... 179—3 \$204CM, 5204CM (Ch. TE-305, -- ..., 149—3 \$210, 5211, 5212 (Ch. TE-315, -1). ..., 4, -514, 450 see PCB 37—
 \$211, 5212 (Ch. TE-315, -1). 7..., 3, 4, -514, (Sha see PCB 37—
 \$211, 5212 (Ch. TE-315, -1). 7..., 4, -514, 450 see PCB 37—
 \$211, 5212 (Ch. TE-315, -1). 7..., 4, -514, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
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 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$170, 517
 \$175, \$176 (Ch. 1E320)... 179-...
\$204CM, \$206CM (Ch. 1E:300)
\$210, \$211, \$212 (Ch. 1E:315, -1, -2, -3, -4, -5) (Also see PCB 37-...
\$16-1 and PCE 50-...
\$2137M (Ch. 1E331, -1, -2, -3, -4)
\$1737M (Ch. 1E331, -1, -2, -3, -4)
\$1737M (Ch. 1E:331, -1, -2, -3, -4)
\$1757M (Ch. 1E:331, -1, -2, -3, -4)
 chito
 see
 PCB
 66-Set
 203.11

 •62137B
 (Ch. TE.319, 1, -2)
 (Sae
 92

 PCB
 67-Set
 204.1
 ond
 Model

 62137B
 -Ch. TE-319, 1, -2)
 (Sae
 92
 93

 662137B
 -Ch. TE-330, -1, -2, -3, -4, -5, -6)
 (Also Sae
 96
 92
 92
 92

 662137B
 -Ch. TE-330, -1, -2, -3, -5, -6)
 (Also Sae
 92
 92
 92
 92

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. 🔹 Denotes Television Receiver.

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341T (Ch. RE-274) 84-3

ARVIN-BROWNING

ARVIN-Cont.

B211TB-UHF (Ch. TE330-7) (See PCB 88-Set 231-1 and Model 6213TB-UHF-Set 231-1 and Model 6213TB-UHF-Set 208-2)

PCB 88—Set 231-1 and Model 6213Tb.UHF_Sat 208-2) ● 8211TM (Ch. TE319-3) (See PCB 67 —Set 204-1, PCB 89—Set 233-1 and Model 6213TM—Set 195-4) 8211TM-UHF (Ch. TE330-7) (See PCB 88—Set 231-1 and Model 6213TB-UHF-Set 208-2) ● 8213TM (Ch. TE319-2) (See PCB 67 —Set 204-1, PCB 89—Set 233-1 and Model 6213TM—Set 195-4) 8213TM-UHF (Ch. TE330-6) (See PCB 88—Set 231-1 and Model 6213TB-UHF-Set 208-2) ● 8213TM_AUHF (Ch. TE330-6)1 (See PCB 67—Set 204-1, PCB 89—Set 233-1 and Model 6213—Set 195-1) ● 8213TM_AUHF (Ch. TE330-6)1 (See

Or-Set 204-1, PCB 89-Set 233-1 and Model 6213-Set 195-1) B213TMA-UHF (Ch. TE330-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF-Set 208-2) B213CB-UHF (Ch. TE330-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF-Set 208-2) B213CBA-UHF (Ch. TE330-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF-Set 208-2) B213CBA-UHF (Ch. TE330-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF-Set 208-2) B213CBA-UHF (Ch. TE330-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF-Set 208-2) B213CBA-UHF (Ch. TE330-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF (Sh. TE30-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF (Sh. TE30-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF (Sh. TE30-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF (Sh. TE30-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF (Sh. TE30-61) (See PCB 88-Set 231-1 and Model 6213TB-UHF (Sh. TE30-61) (See PCB 88-Set 231-

ARVIN-Cont.

ARVIN-Cont. • 8218CB (Ch. TE310-3) (See PCB 67 --Set 204-1, PCB 89-Set 233-1 and Model 62137M--Set 195-4) • 8218CB-UHF (Ch. TE330-7) (See PCB 80-Set 231-1 and Model 9218CM (Ch. TE310-3) (See PCB 93-Set 204-1, PCB 99-Set 195-4) and Model 62137M--Set 195-4) and Model 62137M--Set 195-4) and Model 62137M--Set 9218CM-UHF (Ch. TE330-7) (See PCB 88-Set 231-1 and Model 62137B-UHF--Set 208-2) • 9210CB (Ch. TE358, -1, -2, -3) • 9210CB (Ch. TE358, -1, -2, -3) • 9210CM-UHF (Ch. TE333, -1, -2, -3) • 9210CM-UHF (Ch. TE333, -1, -2, -3) • 9210CM-UHF (Ch. TE336, -1, -2, -3) • 9212CFP-UHF (Ch. TE336, ARVIN-Cont. 5176) Ch. TE330, -1, -2, -3, -4, -5, -6 (See Model 6213TB-UHF) Ch. TE330-6 (See Model 8213TM-Ch. TE330-6 [See Model 221178-UHF] Ch. TE330-7 (See Model 821178-UHF] Ch. TE330-61 (See Model 8215CBA-Ch. TE330-61 (See Model of JOAN UHF) Ch. TE-331, -1, -2, -3, -4 (See Model 61/75TM) Ch. TE 331-5 (See Model 61/73TM) Ch. TE 331-6 (See Model 81/71TM) Ch. TE332, -1, -2, -3, -4 (See Model 61/73TM-UHF) Ch. TE332-4 (See Model 81/79TM-IHF) Ch. TE332-4 (See Model B171m-UHF) Ch. TE332-5 (See Model S213TM) Ch. TE332-5 (See Model S213TM) Ch. TE-334 (See Model S213TM) Ch. TE-334 (See Model S213TM) Ch. TE-340, -1, -2 (See Model 7276CB-UHF) Ch. TE-354 (See Model 9211TM) Ch. TE-355 (See Model 9211TM) Ch. TE-355, -1, -2, -3 (See Model 9210CB) 9210CB) h. TE 359-1 (See Model 9240CB-
 •212 MEA
 UHF (Ch. TE363, 1, -2, 3)

 •213 TM (Ch. TE363, 1, -2, 238

 •213 TM (Ch. TE355)
 248

 •213 TM (Ch. TE355)
 248

 •213 SM. UHF (Ch. TE365)
 248

 •213 CM. UHF (Ch. TE355)
 248

 •213 SM. UHF (Ch. TE355)
 248

 •213 CM. UHF (Ch. TE356, -1, 2, -3)
 248

 •213 CGB. UHF (Ch. TE365, -1, 2, -3)
 238

 •218 CB. UHF (Ch. TE356, -1, 2, -3)
 238

 •218 CB. UHF (Ch. TE356, -1, 2, -3)
 238

 •218 CB. UHF (Ch. TE356, -1, 2, -3)
 238

 •218 CB. UHF (Ch. TE358, -1, 2, -3)
 238

 •218 CM. UHF (Ch. TE358, -1, 2, -3)
 238

 •218 CM. UHF (Ch. TE358, -1, 2, -3)
 238

 •218 CM. UHF (Ch. TE358, -1, 2, -3)
 238

 •218 CM. UHF (Ch. TE358, -1, 2, -3)
 238

 •218 CM. UHF (Ch. TE358, -1, 2, -3)
 238

 •219 CM. (Ch. TE354, -1, 2, 235
 238
 Ch. TE 337-1 (See Model 9240CB-UHF) Ch. TE 363, -1, -2, -3 (See Model 9210CB-UHF) Ch. TE 364, -1 (See Model 9240CB) Ch. TE 373 (See Model 9240CB) Ch. TE 373 (See Model 9245CM-UHF) ASTATIC CB-1 Tel. UHF Conv.-Booster 224-3 ASTORIA ASTRASONIC (Also see Pentron) ● 2219CM-UHF (Ch. TE363, -1, -2, -3) 238—4 ● 2240CB-UHF (Ch. TE364, -1), 235—2 ● 2240CB-UHF (Ch. TE359, -1) 235—2 ● 2240CM-UHF (Ch. TE373), 247—3 Ch. RE-91 (See Model 444) Ch. RE-200 (See Model 444) Ch. RE-200 (See Model 544) Ch. RE-200 (See Model 544) Ch. RE-200 (See Model 548) Ch. RE-200 (See Model 548) Ch. RE-200 (See Model 140P) Ch. RE-228 (See Model 150TC) Ch. RE-228 (See Model 150TC) Ch. RE-229 (See Model 665) ATLAS AB-45 <u>_5</u> AUDAR AV-71 166--6 MAS-4 "Bingo Amp" 26--6 P-1A 5-10 P-4A 19--3 P-5 5-11 P-7 44--3 P-5 10-1 25-11 13-10 19-4 25-8 62-5 35-2 65-2 PR-6A RE-8A RE-8A Telvar BM-25, BMP-25. Telvar FMC-12 Telvar RER-9 WC-7T 166-6 AUDIO DEVELOPMENT (ADC) Ch. RE-228-1 [See Model 150TC Late) Ch. RE-221 [See Model 665] Ch. RE-231 [See Model 1571] Ch. RE-232 [See Model 1571] Ch. RE-232 [See Model 1571] Ch. RE-232 [See Model 1571] Ch. RE-243 [See Model 1270P] Ch. RE-243 [See Model 240P] Ch. RE-243 [See Model 240P] Ch. RE-243 [See Model 240P] Ch. RE-243 [See Model 240] Ch. RE-243 [See Model 240] Ch. RE-252 [See Model 240] Ch. RE-253 [See Model 240] Ch. RE-253 [See Model 260] Ch. RE-253 [See Model 260] Ch. RE-254 [See Model 360] Ch. RE-254 [See Model 360] Ch. RE-257 [See Model 360] Ch. RE-257 [See Model 3567] Ch. RE-257 [See Model 3567] Ch. RE-277 [See Model 361] Ch. RE-277 [See Model 361] Ch. RE-278 [See Model 467] Ch. RE-278 [See Model 457] Ch. RE-333 [See Model 457] Ch. RE-333 [See Model 557] Ch. RE-347 [See Model 557] C AUTOMATIC
 ADTOMATIC

 Tom Boy
 27-4

 Tom Thumb Buddy
 53-7

 Tom Thumb Buddy
 53-7

 Tom Thumb Buddy
 53-7

 Tom Thumb Buddy
 54-6

 Tom Thumb Jr
 26-7

 Tom Thumb Personal ATTP
 23-4

 8-44
 60-5

 C51
 178-4

 C-54
 186-2

 C60
 5-20

 C+0X
 24-10
 C-60X 24-10 C 65X (See Model C-60X-Set 24-C 35X (See M 10) C-351 CL-152B, M CL-152B, M CL-164B CM-333 148—4 192—3 192—3 230—3 104—3 174—4 D200 D200 D-251 DM-132 F-100 F-151 F-790 M-86 M-90 MM-430 P-651 _4 _3 228-3 103-6 147-2 23-5 34-3 67-4 229-3
 MM-430
 27-3

 P-651
 173-4

 S-551
 146-3

 TR-12
 228-4

 V-707, TV-709, TV-710.
 60-6

 6'V-712 (See Model TV-707-Set

 6'V-712 (See Model TV-707-Set

 103-5)

 TV-5006
 145-4

 TV-5020
 134-4

 TV-5061
 145-4

 TV-5077
 145-4

 TV-5160
 134-4

 TV-5160
 134-4

 TV-5160
 134-4

 TV-707-561
 134-4

 TV-707-66
 134-4
 eTVX404 (See Model TV-707-Set
 TV:X024
 (See Model
 TV-707
 -set

 60-6)
 602
 (Series A)
 13-11

 601, 602
 (Series B)
 22-5

 612X
 1-34
 613X
 1-34

 613X
 1-34
 613X
 1-34

 613X
 163X
 8-2
 2

 614X, 616X
 612X
 1-34

 614X, 616X
 122-3
 640, Series B
 10-4

 640, Series B
 10-4
 660, 662, 666
 22-6

 677
 720
 21-4
 4
 -6 (See Model 22.0) Ch. TE-319, -1, -2 (See Model 6213TM) Ch. TE-319-3 (See Model 8211TB) Ch. TE-319-21 (See Model 8213TMA) Ch. TE-320 (See Models 5175,

AVIOLA (Also see Record Changer Listing) 509 601 608 16-6 15-3 16-6 612 618 BELL-AIR PL17C (Similar to Chassis) 149–13
PL20C (Similar to Chassis) 149–13 BELL SOUND SYSTEMS
 BELL SOUND 513
 75-4

 B-23
 75-4

 PA3710A-P3
 (Above Serial No. 78000)

 225-6
 249-4

 PA3725-8
 244-3

 PA3725-8
 244-5

 250-5
 250-5
 RC-47 (RE-CORD-O-FONE) 30-3 130-4 RT-65, B 171-3 3D 256-7 350 148-5 149-149_4 151_6 150_4 25_9 10_5 77_3 153_1 199_2 37455 161-2 256-8 234-1 228-5 207—1 227—3 78000 3706-M 3710A (Above Serial No. 225 225-6 22-8 249-4 3715 . 3715-B 3717-MB, 3717MB3 3723-MB, -MB3 3725 3725-B 3725-B 3728-M 3728MB 3729MB 3750 238-5 224-4 .224—4 .22—9 .244—3 .24—11 .235—3 .31—5 .250—5 3750 ... 3750-B BELLTONE 5-33 500 BELMONT (Also see Raytheon) 17-7 10-7 10-7 10-7 10-2-27 10-6 113 (Series A). 10-6 22-10 A-6D110 3AW7
 3AW7
 2-27

 4B17
 2-27

 4B17, 4B113 (Series A)
 10-6

 5D110
 22-10

 5D128 (Series A)
 9-4

 5P19 (Series A)
 9-4

 5P19 (Series A)
 9-4

 6D111
 2-33

 6D120
 24-12
 8A59 •21A21 •22A21, 22AX21, 22AX22. 93A-4 55-5
 BENDIX

 CMTB21CS (Ch. T14-7) (See Model FB21CU—Set 213-2)

 CMTB21CU (Ch. T14-4) (See Model FB21CU—Set 213-2)

 CMTM21CS (Ch. T14-4) (See Model FB21CU—Set 213-2)

 CMTM21CS (Ch. T14-7) (See Model FB21CU—Set 213-2)

 CMTM21CU (Ch. T14-4) (See Model FB21CU—Set 213-2)

 CMTM21CU (Ch. T14-4) (See Model FB21CU—Set 213-2)

 FB21CU—Ser 213.2)

 CMX721CU [Ch, 114.4] (See Model FB21CU—Sei 213.2)

 C172
 134—S

 C173
 See Model 2051—Set 111.3)

 C174 (See Model 2051—Set 113.4)
 See Model C172—Set 134.5)

 C172
 See Model C172—Set 134.5)

 C200
 .134—S

 FB21CU [Ch, T14.7]
 (See Model C172—Set 134.5)

 FB21CU [Ch, T14.4]
 .213—2

 FB21CU [Ch, T14.4]
 .213—2

 FB21CU [Ch, T14.4]
 .213—2

 FB21CU [Ch, T14.4]
 .213—2

 HB21CU [Ch, T14.4]
 .213—2

 HB21CU [Ch, T14.4]
 .213—2

 HB21CU [Ch, T14.4]
 .213—2

 HB21CU [Ch, T14.4]
 .213—2

 SB21C [Ch, T14.4]
 .213—2

 SB21C [Ch, T14.4]
 .213—2

 SB21C [Ch, T14.4]
 .213—2

 SB21C [Ch, T14.4]
 .213—2

 SB21C1 [Ch, ● OAK3 (Ch. 114-1) (Also tse PCB 101—5et 247-1) 183-2
 PAR 80 39-3
 PAR 80 39-3
 PAR 80 39-3
 PAR 80 (Ch. 114-6) (For TV Ch. only tse Model F821CU—Set 213-2)
 PB21C (Ch. 114-6) (For TV Ch. only tse Model F821CU—Set 213-2)
 • T821C (Ch. 114-1) (See PCB 101—Set 247-1 and Model OAK3—Set 183-2)
 • T821C (Ch. 114-7) (See Model F821CU—Set 213-2)
 • TM21C (Ch. 114-1) (See PCB 101—Set 247-1 and Model OAK3—Set 183-2)
 • TM21C (Ch. 114-7) (See Model F821CU—Set 213-2)
 • TM21C (Ch. 114-7) (See Model AK3—Set 183-2)
 • TM21C (Ch. 114-7) (See Model F821CU Set 213-2)
 • TM21C (Ch. 114-7) (See Model AK3—Set 183-2)
 • TM21C (Ch. 114-7) (See Model F821CU Set 213-2)
 • TM21C (Ch. 114-7) (See Model AK3—Set 183-2)
 • TM21C (Ch. 114-7) (See Model F821CU Set 213-2)
 • TM21C (Ch. 114-7) (See Model F821CU Set 213-2)

BENDIX-Cont. 63-3 75W5 59-5 66-3 60-7
 300, 73M8, 75P6, 73W3

 59-5

 79M7

 66-3

 9583, 95M3, 95M9.

 60-7

 710, 110W, 111, 111W, 112, 114, 115

 115, 335M1 (Ch. Codes MA, MB, MC, MD)

 69-4

 300, 300W, 301, 302

 69233B1, 75H (Ch. codes MA, MB, MC, MD)

 69-4

 300, 330W, 301, 302

 60233B3 (For TV Ch. only see Model 235M1-58t 69-4)

 416A

 416A

 526MA

 526MA
 410A 526MA, 526MB, 526MC... 43-5 526MA, 526MB, 526MC.... 613 626-A (0626A) 636A, B, C 636D (See Model 636A—Set 40-3 6360 (See Model 636A—Se 646A 656A 676B, 676C, 676D 687A 736P, M, W (Ch. C-19). 847.5 (Facto-Meter' 951 951W 217, 12178, 1217D 1217D (Lote) 1518, 1519, 1524, 1525. 1524 15.4 -31 -23 -3 -8 -8 -8 -8 27-5 36-6 29-4 46-5 37-3 42-4 37-3 136 1521 1524, 1525 1531, 1533 • 2001, 2002 • 2020, 2021 2025
 2025
 2025
 2025
 2025
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 2025
 2025
 2025
 2025
 2025
 111 and Model 2051—Set 111-3) 3001, 3002 84 3030, 3031 84 126-1 84-4 84-4 99<u>5</u> 126-1) 11<u>3</u> • 3033 • 3051 (Also see PCB 16-Set ● 6001 (Also see PCB 16-Set 126-1) ●6002 99—5 ●6003 (Also see PCB 16—Set 126-1
 error (Allo tes PCB 16—Sel 12

 e6920
 111

 e6920
 111

 e7001 (See PCB 16—Sel 126-11

 model 2051—Set 111-31

 ch. 714-1 (See Model 753F)

 ch. 714-4 (See Model 763F)

 ch. 714-4 (See Model 7821C1)

 ch. 714-7 (See Model 7821C1)

 ch. 714-7 (See Model 7821C2)

 ch. 714-7 (See Model 7821C2)
 Model BLONDER-TONGUE BTU-1-(14-83) Tel. UHF Conv .229-4 .254-3 .259-3 BTU-2 Tel. UHF Conv. 99 Tel. UHF Conv. BOGEN (See David Bogen) BREWSTER 9-1084, 9-1085, 9-1086 ... 2-13 BROCINER BROOK ELECTRONICS INC.

BROOKS LABORATORIES, INC.
 ST-14A
 183—3

 ST-10
 195—5

 ST-10A
 237—3

 ST-15A
 234—2
 ST-15A BROWNING

PF-12, RJ12 47-4 RJ-12A 56-6 RJ-12B 146-4 RJ-14A 56-6

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

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CAPEHART-Cont. BROWNING-Cont. 67-5 132-3 67-5 254-4 261-3 46-6 131-3 46-6 RJ-20 RJ-20A RJ-22 . RJ-42 RJ-48 RV-10 RV-10A RV-11 RV31 198-3 BRUNSWICK 28-4 28-4 56-7 29-5 BJ-6836 "Tuscany C-3300 "Darby" D-1000, D-1100 D-6876 "Buckingh C-3300 D-1000, D-1100 D-6876 "Buckingham" T-4000, T-4000½ "Buckingham" 29—5 41—4 400½ "Glas-400½ "Glas-29-5 1-4400, T-44001/2 E-6000, S, SS, SX, T-60001/2 Glas-caw' (See Model T-4000-Set caw" 29-5) 56-7 163-3 163-3 42-5 163-3 163-3 163-3 29-5) T-9000 • 512, 513 • 812, 816 5000 • 5125 • 6165 • 8125, 8165 . BRUSH SOUND MIRROR (See Recorder Listing) BRUSH MAIL-O-VOICE (See Recorder Listing) BUICK 980690, 980733 980744, 980745 18—9 19—5 62—6 59—6 980782 980797, 980798 217—2 224—5 225—7 248—3 257—2 981320 981321 981323 981550 981551 BUTLER BROS. (See Air Knight or Sky Rover) CADILLAC (Auto Radio) Choice Choice 60-8 725807 60-8 7258755 7260205 109-2 7260205 7260405 152-3 7260905 CALLMASTER (See Lyman) CAPEHART F-313 [Ch. CR-85] 215 - 4 RP-135 [Ch. CR-79] 258 - 4 RP-1348 M [Ch. CR-120] CA-133 254 - 5 254 - 5 RP253 [Ch. CR-747] 258 - 4 CA-235 [Ch. CR-747] 254 - 5 RP254 [Ch. CR-747] 132 - 4 IC-20 [Ch. C297] 132 - 4 IC-100 [Ch. C2-277] 203 - 5 T-30 141 - 3 -30 - 1 T-322 [Ch. CR-76] 209 - 1

203.4) (See Ch. C1-72—Sef 203.4) (See Ch. C7-73—Sef 203.4) (See Ch. C7-73—Sef 3C17MX (Ch. CT-27) (Ch. Series CX-33DX) (See Ch. CT-27—Sef 160.2) 3(212A (Ch. CT-77) (Ch. Series CX-33) (See Ch. CT-77—Sef 203.4)

CX-37) [See Ch. CT-77—Set 203-4) 3T55E (Ch. CT-150) ... 261—4 4C20X (Ch. CT-38] (Ch. Series CX-33DX) [See Ch. CT-38—Set 160-2] •C(174 (Ch. CT-99) (Ch. Series CX-37) [See Ch. CT-75—Set 203-4) 4C(174MD (Ch. CT-99) (Ch. Series CX-37) [See Ch. CT-75—Set 203-4) •C(174MS (Ch. CT-79) (Ch. Series CX-37) [See Ch. CT-75—Set 203-4) 4C(174MS (Ch. CT-77) (Ch. Series CX-37) [See Ch. CT-77—Set 203-4) 4H212A (Ch. CT-77) (Ch. Series CX-37) [See Ch. CT-77—Set 203-4) 4H212A (Ch. CT-77) (Ch. Series CX-37) [See Ch. CT-77—Set 203-4) 4H212A (Ch. CT-77) (Ch. Series CX-37) [See Ch. CT-77—Set 203-4) 4H213B, M (Ch. CT-77) (Ch. Series CX-37) [See Ch. CT-77—Set 203-7] [See Ch. CT-77—Set 203-7] [See Ch. CT-77] (Sec Ch. Series 203-7] [See Ch. CT-77] [Sec Ch. CT-77=Set 203-7] [See Ch. CT-77] [Sec Ch. CT-77] (See Ch. CT-77] [Sec Ch. CT-77] [Sec Ch. CT-77] (Sec Ch. CT-77] [Sec Ch. CT-77] [Sec Ch. CT-77] 203-7] [See Ch. CT-77] [Sec Ch. CT-77] 203-7] [Sec Ch. CT-77] [Sec Ch. CT-77] [Sec Ch. CT-77] 203-7] [Sec Ch. CT-77] [Sec Ch. CT-77] [Sec Ch. CT-77] 203-7] [Sec Ch. CT-77] [Sec Chong 203.4) •7H214M (Ch. CT-121) (Ch. Series CX.37) (See Ch. CT-75—Set 203.4) •8F212A (Ch. CT-77) (Ch. Series CX-37) (See Ch. CT-77—Set 203.4) •8F212B (Ch. CT-57) (Ch. Series CX-36) •8F212B (Ch. CT-57) (Ch. Series CX-187-3 -100 (Ch. Series CX-197-3 -100 (Ch. Series

203.4) 23C2148, M (Ch. CT-143) (Ch. Se-rics CK-37) (See Ch. CT-75—Set 203.4) 32P9, 33P9 64---3 34P10 (See Model 32P9--Set 64.3) 35P7 (Ch. P7) 135--4 114N4 65--3 1200-474

115P2 67-6 116N4, 116P4, 118P4.... 65-3

CAPEHART-Cont.
919 (Ch. C-298) [Ch. Series CX-33] (See FCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
919AX (Ch. CT-27) (Ch. Cx-33DX) (See Ch. CT-27—Set 160-2)
920 (Ch. C-289) (Ch. Series CX-331) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
9208X, MX (Ch. CT-27) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
921A (Ch. C-289) (Ch. Series CX-333) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
921A (Ch. C-298) (Ch. Series CX-330) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
921A (Ch. C-298) (Ch. Series CX-330X) (See Ch. CT-27—Set 160-2).
9228, M (Ch. C-281) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
922RAB, RAM (Ch. C-281) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
922RAB, RAM (Ch. C-281) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
922RAB, RAM (Ch. C-281) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
922RAB, RM (Ch. C-281) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
922RAB, RM (Ch. C-281) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1 and Model 323M—Set 112-3).
922AB, M (Ch. C-298) (Ch. Series CX-330X) (See PCB 13—Set 122-1, and PCB 24—Set 142-1) and Model 323M—Set 112-3).
922AB, M (Ch. C-298) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1) and Model 323M—Set 112-3).
922AB, M (Ch. C-298) (Ch. Series CX-330X) (See PCB 13—Set 122-1, and PCB 24—Set 142-1) and Model 323M—Set 112-3).
922AB, M (Ch. C-270) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1) and Model 323M—Set 112-3).
922AB, M (Ch. C-271) (Ch. Series CX-330X) (See PCB 13—Set 122-1, PCB 24—Set 142-1) and Model 323M—Se

CAPEHART-Cont.

CAPEHART-Cont.

 ■300/ (Ch. C-276) (Ch. Series CX. 30)
 ■ 99A-2
 ■ 3008 (Ch. C-297) (Ch. Series CX. 312) (See Ch. CX.23-Set 93A-5)
 ■ 30118, M, 30128, M (Ch. C-281) (Ch. Series CX.331) (See Ch. CX.31-Set 93A-5)
 ■ 4001-M (Ch. C-268) (Ch. Series CX.331) (See Ch. CX.31-Set 93A-5)
 ■ 4002-M (Ch. C-274) (Ch. Series CX.331) (See Ch. CX.31-Set 93A-5)
 ■ 4002-M (Ch. C-274) (Ch. Series CX.331) (See Ch. CX.31-Set 93A-5)
 ■ 4002-M (Ch. C-274) (Ch. Series CX.31) (See Ch. CX.31-Set 93A-5)
 ■ 4002-M (Ch. C-274) (Ch. Series CX.31) (See Model 3007)
 Ch. C-268 (See Model 3007)
 Ch. C-274 (See Model 3008)
 Ch. C-274 (See Model 3008)
 Ch. C-275 (See Model 3007)
 Ch. C-276 (See Model 3023)
 Ch. C-285 (See Model 3213)
 Ch. C-287 (See Model 3213)
 Ch. C-287 (See Model 3213)
 Ch. C-287 (See Model 323)
 Ch. C-297 (See Model 323)
 Ch. C-297 (See Model 323)
 Ch. C-397 (See Model 1006b)
 Ch. C-397 (See Model 1007AM)
 Ch. C-313 (See Model 1007AM)
 Ch. C-313 (See Model 1007AM)
 Ch. C-313 (See Model 17-52)
 Ch. CR-74 (See Model 752)
 Ch. CR-75 (See Model 752)
 Ch. CR-74 (See Model 752)
 Ch. CR-75 (See ch. C1-81 (ch. Series CX.37)
ch. C1-80 (ch. Series CX.37)
ch. C1-70 (ch. Series CX.37) (See Ch. C1-10 (ch. Series CX.37) (See Ch. C1-10 (ch. Series CX.37) (See Ch. C1-75-55 (203.4)
ch. C1-13 (ch. Series CX.37) (See Ch. C1-75-55 (203.4)
ch. C1-75-55 (203.4) Ch. Series CX-30, A (See Model 3001) Ch. Series CX-30-A-2 (See Model 3001) Ch. Series CX-31 (See Model 3004-M) Ch. Series CX-32 (See Model 3005) Ch. Series CX-33 (See Model 323M) Ch. Series CX-331 (See Model 323M) 323M) Ch. Series CX-33L (See Model 326-M) Ch. Series CX-33DX (See Ch. CT-27) C1-27) Ch. Series CX-36 (See Model 11172M) Ch. Series CX-37 (See Ch. CT-75) CAPITOL D-17 T-13 U-24 30—4 28—5 29—6 CARDWELL, ALLEN D. CE-26 14-6 ES-1 (Tel. UHF Conv.) 263-5 CAVENDISH (See Bell Air) CAVALIER 241—4 238—6 242—4 CBS-COLUMBIA (Also see

BROWNING-CENTURY

CB5-COLUMBIA-Cont. • 22M28 (Ch. 821-4) (See Model 18C18—Set 214-2) • 22M38 (Ch. 822-1, -2, -3, -4, -10, • 22M38 (Ch. 822-1, -2, -3, -4, -10, • 255--3 CENTURY (Also see

COOSIEV

CENTURY (20TH)-C	ROSLE
CENTURY (20th) 100X, 101, 104 200 300	12—5 21—5 21—6
20R 60R 200 600 CHANCELLOR (Also see Radionic)	63-4 67-7 68-6 70-3 66-4 65-4 257-3 69-5 62-7 69-5 62-7
CHEVROLET	30-25
986443 1 986515 1 984514	65 19-6 90-2 28-6 75-5 58-7 04-5 89-4 49-5 50-6 19-2 24-6 62-4
	37 <u>4</u> 20 <u>3</u>
11411-N 11801 11802V-M (See Model 1180	6-7 5-8 17-8 8-11 30-5 23-6
121100 12310-W 12708 12801 13101 13201, 13203 14601 14965 16703 1	54—5 31—6 41—5 61—5 46—7 62—8 60—9 66—5 02—2
CLARK PA-10 PA-10A PA-20 PA-20A PA-30	12-6 18-12 13-12 18-13 19-7
CLEARSONIC (See U. S. Television) COLLINS AUDIO PRODUC	
FMA-6	99 <u>_6</u> 72 <u>_6</u>
51.1-3 2	60_6 34_4 71_4
COLUMBIA RECORDS 202	19—3 15—5
	5 Player 17–10 19–9
CONCERTONE (See Recorder Listing)	3
CONCORD	lar to
Chassis) IN437 (Similar to Chassis). 1: IN549 (Similar to Chassis). IN551 (Similar to Chassis). IN554, IN555 (Similar to Chassis).	21-2 38-5 38-6
IN556, IN557 (Similar to C	hassis)
6C51W 6E51B 6E26W	36-10 69-7 19-8 19-8 20-4
7R3APW	21-7 22-11 20-5 21-7 45-6
1-411 1-501 (See Model 6E51B—Set 1-504	485 20-4) 556
1-516, 1-517	51B— 19—7 Model
1-608 (See Model 6F26W	•
1-609 [See Model 6T61W 22-11] 1-611	

IRY (20th)	CONCORD-Cont.	CORONADO-Cont.
101, 104 12—5 21—5	1-1201	● 25TV2-43-9060B (See 205-1 and Model
21—6	53-8)	205-1 and Model 9060A—Set 199-5)
ENGER	2-200, 2-201, 2-218, 2-219, 2-232,	35RA2-43-5101A 35RA4-43-9856A
63—4 67—7	2-235, 2-236, 2-237, 2-238, 2-239, 2-240	35RA33-43-8125 35RA33-43-8145
68—6 70—3	2-106 2-200, 2-201, 2-218, 2-219, 2-232, 2-235, 2-236, 2-237, 2-238, 2-239, 2-240, 62-9 315WL, 315 WM, 53-8 325WL, 325 WN (See Model 2-106 -Set \$4-6)	35RA33-43-8225 35RA37-43-8355
	-Set \$4-6)	358A40-43-8247A
65-4 257-3 69-5	CONRAC	• 35TV2-43-9022C (See 202-1, PCB 72—Set Model 25TV2-43-902
69 -5 62 -7	●10-M-36, 10-W-36 (Ch. 36) (See Ch. 36)	183-4)
69 —5 62 —7	•11-B-36 (Ch. 36) (See Ch. 36) •12-M-36, 12-W-36 (Ch. 36) (See	■ 35TV2-43-9023A
CELLOR		• 35TV2-43-9045D (See 205-1, PCB 71—Set Model 25TV2-43-90
see Radionic)	●13-B-36 (Ch. 36) (See Ch. 36) ●14-M-36, 14-W-36 (Ch. 36) (See	199-5}
		• 35TV2-43-9045E (See TV2-43-9045D)
OLET	 15-P.36 (Ch. 36) (See Ch. 36) 16-B.36 (Ch. 36) (See Ch. 36) 17-P.39 (Ch. 39) (See Ch. 39) 18-M-39, 18-W-39 (Ch. 39) (See 	• 35TV2-43-9050A • 35TV2-43-9060C (See
6 5 19-6	•18-M-39, 18-W-39 (Ch. 39) (See	205-1, PCB 71-Set Model 25TV2-43-900
90—2 28—6	[Cn. 39]	199-51
	 20M.39, 20W.39 (Ch. 39) (See Ch. 39) 21B.39 (Ch. 39) (See Ch. 39) 22P.39 (Ch. 39) (See Ch. 39) 23M.390, 23W.390 (Ch. 39) (See Ch. 39) 24M.36 (Ch. 34) (See Ch. 34) 	• 35TV2-43-9060D (See TV2-43-9060C)
58—7 104—5 189—4	•22-P-39 (Ch. 39) (See Ch. 39)	• 35TV2-43-9061A 43-2027
189-4	Ch. 39)	43—2027 43—5005 43-6301
149—5 150—6 219—2	 24-M-36 (Ch. 36) (See Ch. 36) 25-W-36 (Ch. 36) (See Ch. 36) 26-B-36 (Ch. 36) (See Ch. 36) 27-M-40, 27-W-40 (Ch. 40) (See 	43-6451 43-6485
	●26-B-36 (Ch. 36) (See Ch. 36) ●27-M-40, 27-W-40 (Ch. 40) (See	43-6730 (See Model 4
		11-4) 43-7601 (See Model
LER (See Mopar)	28-B-40 (Ch. 40) (See Ch. 40) 29-P-40 (Ch. 40) (See Ch. 40) 30-M-40, 30-W-40 (Ch. 40) (See	Set 10-11) 43-7601B
		43-76018 43-7602 (See Model Set 10-11)
 20 —3	• 31-P-40 (Ch. 40) (See Ch. 40) • 32-M-44, 32-W-44 (Ch. 44) (See	43-7651
DN 1 6	Ch 441	9-7)
1—5 5—9	• 33-B-44 {Ch. 44} (See Ch. 44) • 34-P-44 {Ch. 44} (See Ch. 44) • 35-M-61, 35-W-61 {Ch. 61} (See	43-7851 43-7852 [See Model Set 47-5] 43-8101 (See Model 8115A—Set 81-5) 43-8130C, 43-8131C
9—6 6—6	 35-M-61, 35-M-61 (Ch. 61) (See Ch. 61) 36-8-61 (Ch. 61) (See Ch. 61) 37-P-61 (Ch. 61) (See Ch. 61) 38-8-61, 38-M-61 (Ch. 61) (See Ch. 61) 	Set 47-5) 43-8101 (See Model
iee Model C-104-Set 1-4)	• 37-P-61 (Ch. 61) (See Ch. 61)	8115A-Set 81-5) 43-8130C 43-8131C
	• 38-8-61, 38-M-61 (Ch. 61) (See Ch. 61)	94RA33-43-8130C-5 43-8160
	 39-M-61 {Ch. 61} [See Ch. 61} 40-M-64, 40-W-64 {Ch. 64} {See Ch. 64} 41-B-64 {Ch. 64} (See Ch. 64) 	43-8177 (See Model 4)
30-5	Ch. 64) •41-8-64 (Ch. 64) (See Ch. 64)	21-8) 43-8178
23-6 M (See Model 11801-Set	•41-8-64 (Ch. 64) (See Ch. 64) •42-P-64 (Ch. 64) (See Ch. 64) •43-8-64, 43-M-64 (Ch. 64) (See	43-8180 43-8190
x	Ch. 64)	43-8201 (See Model 4 21-8)
V 31—6 41—5	Ch. 36	43-8213 43-8240, 43-8241
41-5 61-5 46-7	• Ch. 44 (See PCB 27—Set 148-1 and	43-8305 43-8312A
13203	•Ch. 61, 64 Series	
66—5 102—2	CONTINENTAL ELECTRONICS	43-8353, 43-8354 43-8420
	(See Skyweight)	43-8351, 43-8352 43-8353, 43-8354 43-8420 43-8470 43-8471
	CONVERSA-FONE	43-8576B
126 18-12 13-12	MS-5 (Master Station) SS-5 (Sub- Station)	43-8685 •43-8965
	CO-OP	• 43-8965 • 43-9030 • 43-9031
ONIC	6AWC2, 6AWC3, 6A47WCR, 6A47- WT, 6A47WTR	43-9196
. 5. Television)	CORONADO	43-9201 43-9841A (See Model
15 AUDIO PRODUCTS	•FA43-8965 (See Model 43-8965-	43-9841A (See Model 9841A—Set 79-3) 45RA1-43-7666A
99 <u>6</u> 72 <u>6</u>	Set 86-3) ●K-21 (43-9041}182—3	45RA1-43-7910A, 45R A (See Model 15RA1- Set 134-6)
IS RADIO	K.21 (43.9041) 182—3 K.72 (43.9031) 182—3 K.731 (43.9030) 182—3	Set 134-6) 45RA33-43-8126 (See
260-6	KH37-43-7033	45RA33-43-8126 (See RA33-43-8125-Set 2 45RA33-43-8146 (See
	05841-43-79014 115-2	RA33-43-8145-Set 45RA33-43-8225, 45RA
	05RA2-43-8230A	45RA33-43-8227
219—3 es ''B''	05RA4-43-9876A	8228 (See Model 8225—Set 219-4)
ANDER INDUSTRIES	05RA33-43-8120A	45RA33-43-8355 (See RA37-43-8356A-Set
der 3 Tube Record Player 17-10 19-9	05RA1-43-7755A, 05RA1-43-7755B 101-2 05RA1-43-7901A 115-2 05RA2-43-8230A 125-3 05RA2-43-8215A 10-5 05RA3-43-8120A 05RA3-43-8130C 05RA3-43-8130C 05RA3-43-8130C 05RA3-43-830A 102-3	45RA37-43-8356 (See RA37-43-8355—Set 2 45TV2-43-90238
	05TV1-43-8945A145-5	45TV2-43-9045F (See M)
RTONE acorder Listing)	•05TV1-43-9014A 128-4	43-9045D 45TV2-43-9050B (See M
RD	• 051V1-43-V005A, 051V1-43-V006A, • 051V1-43-V0014A	43-9050A-Set 237- 45TV2-43-9060E (See M
IN435, IN436 (Similar to	• 05TV2-43-90108	43-9045D)
s) 98—5 Similar to Chassis). 121—2 Similar to Chassis). 38—5 Similar to Chassis). 38—6 INS55 (Similar to Chassis).	15RA1-43-7902A	●45TV2-43-9064A
Similar to Chassis). 38-6	15RA4-43-9876C, 15RA4-43-9877	• 45TV11-43-9027A, 9028A (Series XT-100
55-10	Set 103-71	• 45TV11-43-9085A, 9086A, 45TV11-43-9 TV11-43-9089A,
IN557 (Similar to Chassis) 109—7 Similar to Chassis) 90—7	15RA33-43-8245A, 15RA33-43 8246A	TV11-43-9089A, 9090A, 45TV11-43-5 TV11-43-9092A,
Similar to Chassis). 109—7	15RA33-43-8365	TV11-43-9092A, 9093A, 45TV11-43-9 TV11-43-9095A, 45T
IN562 (Similar to Chassis) 97-8	●151V1-43-8957A, B	45TV11-43-9097A.
97-8 Similar ta Chassis). 136-10	• 151V1-43-8957A, B	45TV11-43-9097A, 9098A (Series XT-10 045TV11-43-9130A 451
97-8 Similar ta Chassis). 136-10	• 151V1-43-8957A, B	45TV11-43-9097A, 9098A (Series XT-10 045TV11-43-9130A 451
97-8 Similar ta Chassis). 136-10	• 151V1-43-8937A, B	45TV11-43-9097A, 9098A (Series XT-10 45TV11-43-9130A, 451 31A (Series XT-100). 45TV13-43-9081A 948T41-43-6945A
97-8 Similar ta Chassis). 136-10	• 151V1-43-8925A, B	45TV11-43-9097A, 9098A (Series XT-10 45TV11-43-9130A, 451 31A (Series XT-100). 45TV13-43-9081A 948T41-43-6945A
Similar to Chassi). 136-10 Similar to Chassi). 69-7 19-8 19-8 20-4 19-10 21-7 22-11 20-5 71-7	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	45TV11.43-9097A, 9098A [Series XT-10] 45TV11-43-9130A, 451 31A (Series XT-100). 45TV13-43-9038A 94STV13-43-9081A 94RA1-43-6945A 94RA1-43-7655A, 94RA A
Similar to Chassi). 136-10 Similar to Chassi). 69-7 19-8 19-8 20-4 19-10 21-7 22-11 20-5 71-7	151V2-43-9101A, 151V2-43-9102A 151V2-43-9102A 151V4-43-8948A, 151V4-43-8949A 175 - 7	431V11.43.9097A, 90984 (Series XT-10 9314 (Series XT-10), 451V13.43.9038A 451V13.43.9038A 451V13.43.9081A 94RA1.43.7605A 94RA1.43.7605A 94RA1.43.7751A 94RA1.43.8510A, 94R2
Similar to Chassi), 136–10 Similar to Chassi), 136–10 Similar to Chassi), 19–8 19–8 20–4 19–10 21–7 22–11 20–5 21–7 403 45–6 48–5 set Model 65518—Set 20-4)	151V2-43-9101A, 151V2-43-9102A 151V2-43-9102A 151V4-43-8948A, 151V4-43-8949A 175 - 7	45TV11.43-9097A, 9098A [Series XT-10] 45TV11-43-9130A, 451 31A (Series XT-100). 45TV13-43-9038A 94STV13-43-9081A 94RA1-43-6945A 94RA1-43-7655A, 94RA A
Similar to Chassi). 133-10 Similar to Chassi). 69-7 19-8 19-8 20-4 19-10 21-7 22-11 20-5 21-7 403 45-6 48-5 ee Model 65518-Set 20.4) 55-6 1-510 (56 Model 6C518-	151V2-43-9101A, 151V2-43-9102A 151V2-43-9102A 151V4-43-8948A, 151V4-43-8949A 175 - 7	451V11.43.9097A, 90984 [Series XT-10 3]A (Series XT-10). 451V13.43.9038A 94871.43.9038A 94871.43.7605A 94871.43.7605A 94871.43.751A 94871.43.8510B, 9487 8 94871.43.8510B, 9487 8 94871.43.8510B, 9487 8 94874.43.8230A
Similar ta Chassi). 136–10 Similar ta Chassi). 69–7 19–8 19–8 20–4 19–10 21–7 22–11 20–5 21–7 48–5 48–5 48–5 48–5 48–5 1-310 (Se Model & CS1B–9 8]	15172-43-V101A, 15172-43-9102A 15174-43-8948A, 15174-43-8949A 15742-43-8928A, 15174-43-8949A 175-7 25172-43-9022B (See PCB 65-Set 25172-43-9022B (See PCB 65-Set 35172-43-9022B (See PCB 65-Set 35172-43-902B (See PCB 65-Set 35172-35	451V11.43.9097A, 90984 [Series XT-10] 531A (Series XT-10] 451V13.43.9038A 451V13.43.9038A 94871.43.9081A 94871.43.7605A 94871.43.7605A 94871.43.751A 94871.43.8510A, 9487 A 94871.43.8510B, 9487 94874.43.8510B, 9487 94874.43.8510A 94874.43.8127A 94874.43.8127A 94874.43.8127A
Similar to Chassis). 136-10 Similar to Chassis). 69-7 Similar to Chassis). 19-8 19-8 20-4 19-10 19-10 22-11 20-5 21-7 22-11 20-5 21-7 20-5 21-7 403 45-6 48-5 55-6 9.8 -20-4 -510 (Se Model & CSIB-9-7) -602 1-502 (Se Model - CSIB-9-7) -603 (See Model - CSIB-9-7)	 ISTV2-43-VIOIA, ISTV2-43-9102A ISTV4-43-8948A, ISTV4-43-8949A ISTV4-43-8948A, ISTV4-43-8949A ISTV2-43-9022A IB34 ISTV2-43-9022A (See PCB 65-Set 202-1, pCB 72-Set 212-1 and Model 2STV2-43-9022C (See PCB 65-Set 202-1, PCB 72-Set 212-1 and Model 2STV2-43-9022A 	451V11.43.9097A, 90984 [Series XT-10] 531A (Series XT-10] 451V13.43.9038A 451V13.43.9038A 94871.43.9081A 94871.43.7605A 94871.43.7605A 94871.43.751A 94871.43.8510A, 9487 A 94871.43.8510B, 9487 94874.43.8510B, 9487 94874.43.8510A 94874.43.8127A 94874.43.8127A 94874.43.8127A
Similar to Chassis). 136-10 Similar to Chassis). 69-7 Similar to Chassis). 19-8 19-8 20-4 19-10 19-10 22-11 20-5 21-7 22-11 20-5 21-7 20-5 21-7 403 45-6 48-5 55-6 9.8 -20-4 -510 (Se Model & CSIB-9-7) -602 1-502 (Se Model - CSIB-9-7) -603 (See Model - CSIB-9-7)	 151V2-43-V101A, 151V2-43-9102A 151V4-43-8948A, 151V4-43-8949A 157V4-43-8948A, 151V4-43-8949A 157V2-43-9022A 183-4 16251V2-43-9022B (See PCB 65—Set 202-1 ond Model 251V2-43-9022C (See PCB 65—Set 202-1 20-1 ond Model 251V2-43-9022A — Set 183-40 	451V11.43.9097A, 90984 [Series XT-10 3]A (Series XT-10 451V13.43.9038A 43.9081A 94RA1.43.9081A 94RA1.43.7605A 94RA1.43.7605A 94RA1.43.751A 94RA1.43.8510B, 94R/ B 94RA2.43.8510B, 94R/ B 94RA2.43.8510B, 94R/ B 94RA2.43.8130A 94RA4.43.8130B, 8131A, 94RA4.43.8130B, 8131A, 94RA4.43.8130B, 94RA4.43.8132A 94RA4.43.8132A 94RA4.43.8132A
Similar ta Chassia). 136-10 Similar ta Chassia). 69-7 19-8 19-8 19-8 20-4 19-1 19-8 20-4 19-10 19-7 20-14 19-10 21-7 22-11 20-5 43-6 48-6 5ee Model 6E51B-Set 00-4) 61-510 1-510 (Se Model 6C51B-9-9) 9-8) 1-517 (See Model 6F26W-Set 0) 45-7 (See Model 6F26W-Set 0) 45-7	 151V2-43-V101A, 151V2-43-9102A 151V4-43-8948A, 151V2-43-8949A 151V4-43-8948A, 151V4-43-8949A 151V2-43-9022A 153-4 151V2-43-9022B (See PCB 65—Set 202-1 and Model 251V2-43-9022C (See PCB 65—Set 202-1 and Model 251V2-43-9022A 151V2-43-9022C (See PCB 65—Set 202-1 and Model 251V2-43-9022A 163-41 163-743-9022C (See PCB 65—Set 18-2 and 199—5 163-743-9042C (See PCB 65—Set 199—5 	431V11.43.9007A, 90984 [Series XT-10 431V1.43.9130A, 431 8417V1.43.9130A, 431 9417V1.43.9038A 9417V1.43.9038A 9417V1.43.9038A 9417V1.43.9038A 9417V1.43.951A 9417V1.4
Similar to Chassis). 136-10 Similar to Chassis). 69-7 IP-8 19-8 19-8 20-4 19-10 21-7 22-11 20-5 21-7 21-7 21-7 22-11 20-5 21-7 21-7 22-11 20-5 21-7 21-7 22-11 20-5 21-7 21-7 22-11 20-5 21-7 21-7 22-11 20-5 55-6 9-8 55-6 9-8 1-517 1-502 1-603 (See Model -519 -51	 151V2-43-V101A, 151V2-43-9102A 151V2-43-9102A, 152-4 151V4-43-8948A, 151V4-43-8949A 151V2-43-9022A, 183-4 183-4 182-43-9022B (See PCB 65-Set 202-1 and Model 251V2-43-9022C (See PCB 65-Set 202-1 and Model 251V2-43-9022A - Set 183-4) 251V2-43-9042C (See PCB 66-Set 205-1 and Model 251V2-43-9042C (See PCB 66-Set 205-1 and Model 251V2-43-9045) 183-40 	431V11.43.9007A, 90984 [Series X1-10 431V1.43.9130A, 431 9487.43.9081A 9487.43.9081A 9487.43.9081A 9487.43.7605A 9487.43.7605A 9487.43.751A 9487.43.85106, 9487 9487.43.85106, 94877 9487.457 9487.4577 9487.4577 9487.45777 9487

	ADD Coult
	ADO-Cont.
25TV2-43	3-9060B (See PCB 68—Set and Model 25TV2-43-
9060A-	3-9060B (See PCB 68—Set and Model 25TV2-43- —Set 199 -5}
35RA2-4	3-5101A
35RA4-4	3-9856A
35RA33-4	43-8145
35RA33-4	43-8225
35RA40-4	43-8355
35TV2-43	3-9022C (See PCB 65-Set
202-1, Model	PCB 72—Set 212-1 and 25TV2_43-90224 Set
183-4)	15.11 45 VOILA - Sel
35TV2-43	3-9023A
205-1,	PCB 71-Set 211-1 and
Model	25TV2-43-9045B Set
35TV2-43	-9045E (See Model 35-
TV2-43	-9045D)
35TV2-43	1-9050A
205-1,	PCB 71-Set 211-1 and
Model	25TV2-43-9060A - Set
35TV2-43	9060D (See Model 35-
TV2-43	-9060C)
43-2027	11-3
43-5005	5 28-36
43-6301	
43-6485	46-9
43-6730	(See Model 43-8685-Set
43-7601	3-9000B (See PCB 68—Set and Model 25TV2-43- —Set 199-5) 3-5101A . 214—3 3-8156A . 211—3 3-8156A . 217—5 33-8145 . 217—5 33-8145 . 224—7 3-8255 . 219—4 43-8355 . 225—9 3-9022C (See PCB 65—Set PCB 72—Set 212-1 and 25TV2-43-9022A — Set 9023A . 234—4 9045B (See PCB 66—Set PCB 71—Set 211-1 and 25TV2-43-9045B — Set 9045C (See PCB 66—Set PCB 71—Set 211-1 and 25TV2-43-9045B — Set 9045C (See Model 35- 9045C) (See Model 35- 9046C) (See PCB 66—Set PCB 71—Set 211-1 and 25TV2-43-9060A — Set 9060C) See Model 33- 90600C) See Model 33- 90600C) 1=9061A . 237—5 90600C) . 11—3 5 . 28—306 . 237—5 90600C) . 11—3 5 . 28—306
Set 10	-11)
43-7601B	(See Model 43-76018- -11)
Set 10	-11)
43-7651	(See Model 42 7/5) 5-
9.7)	1000 mouel 43-7031-3ef
43-7851	47-5
43-7852 Set 4	(See Model 43-7851-
43-8101	(See Model 94RA31-43-
8115A-	-Set 81-5) 43-8131C (Sec. Model
94RA3	3-43-8130C-Set 82-3)
43-8160	(See Model 43-76018— -11) 9—7 (See Model 43-7651—Set (See Model 43-7651— (See Model 43-7851— (See Model 94RA31-43— -Set 81-51) (See Model 94RA31-43— -Set 81-51) (See Model 43-8178—Set 12—7 (See Model 43-8178—Set 21—8
21-8)	(Jee model 43-8178-Set
43-8178	
43-8180	10 -12
43-8201	(See Model 43-8178-Set
21-8)	7 (
43-8240,	43-8241 12-8
43-8305	8-3
43-8330	19-12
43-8351,	43-8352 12-9
43-8353,	43-8354
43-8470	
43-8471	
43-8685	11-4
13-8965	
43-8965 43-9030 43-9031	86—3 182—3 182—3
43-8965 43-9030 43-9031 43-9041	86—3 182—3 182—3 182—3 182—3
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201	86-3 182-3 182-3 182-3 182-3 182-3 14-35 24-14
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A	86-3 182-3 182-3 182-3 182-3 14-35 24-14 (See_Model 94RA31-43
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A 9841A-	86-3 182-3 182-3 182-3 182-3 182-3 14-35 24-14 (See Model 94RA31-43- -Set 79-3) -Z46A 232-3
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A 9841A- 45RA1-43 45RA1-43	86-3 182-3 182-3 182-3 14-35 24-14 (See Model 94RA31-43 -Set 79-3) -7666A 232-3 -7910A, 45RA1-43-7911
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A- 9841A- 45RA1-43 45RA1-43 A {5ee Set 13-	86-3 182-3 182-3 182-3 142-3 24-14 (See Model 94RA31-43 -56170-3 -7606A 232-3 -7910A, 4581-43-7901 -7910A, 4581-43-7902A 4.0
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A- 45RA1-43 45RA1-43 A {See Set 134 45RA33-4	86-3 182-3 1
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A- 9841A- 45RA1-43 45RA1-43 45RA1-43 45RA1-43 45RA33-4 RA33-4	86-3 182-3 182-3 182-3 182-3 182-3 182-3 14-35 24-14 (See Model 94RA31-44 -Set 79-3) -7910A, 45RA1-43-7912- -7666A 232-3 -7910A, 45RA1-43-7902A- 4-6) 3-8126 (See Model 35- 3-8126 (See Model 35- 3-8126 (See Model 35- 3-8126 (See Model 35-
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9841A- 45RA1-43 45RA1-43 45RA1-43 A {5ee 5et 134 45RA33-4 RA33-4	86-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 24-14 (See Model 94RA31-43 -56179-3 -7606A
43-8965 43-9030 43-9031 43-904 43-9201 43-9841A 9841A- 45RA1-43 45RA1-43 45RA3-4 45RA33-4 45RA33-4 45RA33-4	86-3 182-3 182-3 182-3 182-3 142-35 24-14 (See Model 94RA31-43 -56179-3) -7606A, 45RA1-43-7912 Model 15RA1-43-7912 Model 15RA1-43-7912 -5125-5et 217-5) 3-8126 (See Model 35- 3-8126 (See Model 35-
43-8965 43-9030 43-9031 43-9031 43-9201 43-9201 43-9201 43-9201 45-92001 45-92001 45-9201 4	86-3 182-3 1
43-8965 43-9030 43-9031 43-9031 43-9201 43-9201 43-9201 43-9841A- 45RA1-43 45RA1-43 45RA1-43 45RA3-4 RA33-4 45RA33-4 8228 825-1000000000000000000000000000000000000	86-3 182-3 182-3 182-3 182-3 182-3 182-3 142-35 24-14 (See Model 94RA31-43- -56179-3) -7606A
43-8965 43-9030 43-9031 43-9041 43-9041 43-9041 43-9041 43-9041 43-9041 43-9041 43-9041A 9841A- 5841A- 458A3-4 458A3-4 458A3-4	86-3 182-3 182-3 182-3 182-3 14-35 24-14 (See Model 94RA31-43 -7666A -7910A, 458A1-43-7911- Model 15RA1-43-7902A -40 3-8125 (See Model 35- 3-8145 (See Model 35- 58+219-4) -3-8355 (See Model 35- 3-8355 (See Model 35- -3-8355 (See Model 35- -3-8356 (See Model 35- -3-8356)
43-8965 43-9030 43-9031 43-9041 43-9041 43-9041 43-9841A- 5841A- 5841A- 5841A- 5841A- 45RA33- 45RA33- 45RA33- 45RA33- 45RA33- 8228 (8225- 45RA33- 47RA33- 47R	(See Model 43.8178—Set 7—5 43.8241 12—8 43.8352 12—9 43.8352 12—9 43.8352 28—7 24-13 8—3 8—3 8—4 9—6 11—4 86—3 182—54 182—3 183—3 183
43-8965 43-9030 43-9031 43-9041 43-9196 43-9201 43-9201 43-9201 43-9201 45-821-43 45-821-43 45-821-43 45-821-43 45-821-43 45-821-43 45-821-43 45-821-43 82-821 45-823-4 45-823-4 RA33-4 R	86-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 182-3 24-14 (See Model 94RA31-43-791- 3626 -7606A 232-3 3-8125 5627-31 3-8125 5627-31 3-8125 5627-31 3-8125 5627-43 3-8145 5627-43 3-8145 5627-43 3-8145 5627-43 3-8145 5627-43 3-8145 5647-33 3-8145 5647-33 3-8145 5647-34 3-8145 5647-34 3-8145 5647-34 3-8145 5647-34 3-8156 5647-34 3-81556 5647-35 3-81556 5647-35 3-8155 5647-35 3-8155 5647-35 3-8156 5647-35
RA37-4	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
RA37-4	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
RA37-4	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
RA37-4	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
RA37-4	3-8335 (See Model 35- 98355—525-9) 90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
15RA 37-4 RA 37-4 15TV 2-43 45TV 2-43 43-904 5TV 2-43 43-9050 15TV 2-43 43-9045 15TV 2-43	3-8356 (See Model 35- 3-8355—Set 225-9) -90238
131K3/-4 151V2-43 151V2-43 151V2-43 43-904 151V2-43 43-904 151V2-43 43-904 151V2-43 15	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
131K3/-4 151V2-43 151V2-43 151V2-43 43-904 151V2-43 43-904 151V2-43 43-904 151V2-43 15	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
131K3/-4 151V2-43 151V2-43 151V2-43 43-904 151V2-43 43-904 151V2-43 43-904 151V2-43 15	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
13 KA 37 - 4 KA 37 - 4 15 TV 2 - 43 15 TV 1 - 44 90 28 A 15 TV 1 - 44 90 90 A, TV 1 1 - 44 45 TV 11 - 44 15 TV 1 3 - 44 15 TV 1	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
13 KA 37 - 4 KA 37 - 4 15 TV 2 - 43 15 TV 1 - 44 90 28 A 15 TV 1 - 44 90 90 A, TV 1 1 - 44 45 TV 11 - 44 15 TV 1 3 - 44 15 TV 1	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
13 KA 37 - 4 KA 37 - 4 15 TV 2 - 43 15 TV 1 - 44 90 28 A 15 TV 1 - 44 90 90 A, TV 1 1 - 44 45 TV 11 - 44 15 TV 1 3 - 44 15 TV 1	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
13 KA 37 - 4 KA 37 - 4 15 TV 2 - 43 15 TV 1 - 44 90 28 A 15 TV 1 - 44 90 90 A, TV 1 1 - 44 45 TV 11 - 44 15 TV 1 3 - 44 15 TV 1	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
13 KA 37 - 4 KA 37 - 4 15 TV 2 - 43 15 TV 1 - 44 90 28 A 15 TV 1 - 44 90 90 A, TV 1 1 - 44 45 TV 11 - 44 15 TV 1 3 - 44 15 TV 1	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
13 KA 37 - 4 KA 37 - 4 15 TV 2 - 43 15 TV 1 - 44 90 28 A 15 TV 1 - 44 90 90 A, TV 1 1 - 44 45 TV 11 - 44 15 TV 1 3 - 44 15 TV 1	3-8336 (See Model 35- 3-8355.—Set 225-9) -90238
35KA37-4 RA37-4 STA72-43 55TV2-43 55TV2-43 55TV2-43 55TV2-43 55TV2-513-9025 51513-9026 55TV2-43 55TV2-43 55TV2-43 55TV2-43 55TV2-43 55TV1-4 9028A 55TV11-4 9098A, 55TV1-4 9098A, 55TV1-4 9098A, 55TV1-4 9098A, 55TV1-4 9098A, 55TV1-3-4 31A (50 55TV3-3-4 31A (50 55TV1-3-4 34RA1-43 A,	3-8335 (See Model 35- 3-8355 – Set 225-9) -90238 – 224-4 -90238 – 224-4 -90368 (See Model 35TV2- -90508 (See Model 36 -81290 (See Model 94- -81290 (See Model 94- -81290 (See Model 94- -81294 (
35KA37-4 RA37-4 STA72-43 55TV2-43 55TV2-43 55TV2-43 55TV2-43 55TV2-513-9025 51513-9026 55TV2-43 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV11-4 9098A 55TV13-4 9078A 55TV13-4 9084A-1-3 9084R-1-43 8 904R-1-43 8	3-8335 (See Model 35- 3-8355 – Set 225-9) -90238 – 224-4 -90238 – 224-4 -90368 (See Model 35TV2- -90508 (See Model 36 -81290 (See Model 94- -81290 (See Model 94- -81290 (See Model 94- -81294 (
35KA37-4 RA37-4 STA72-43 55TV2-43 55TV2-43 55TV2-43 55TV2-43 55TV2-513-9025 51513-9026 55TV2-43 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV11-4 9098A 55TV13-4 9078A 55TV13-4 9084A-1-3 9084R-1-43 8 904R-1-43 8	3-8335 (See Model 35- 3-8355 – Set 225-9) -90238 – 224-4 -90238 – 224-4 -90368 (See Model 35TV2- -90508 (See Model 36 -81290 (See Model 94- -81290 (See Model 94- -81290 (See Model 94- -81294 (
35KA37-4 RA37-4 STA72-43 55TV2-43 55TV2-43 55TV2-43 55TV2-43 55TV2-513-9025 51513-9026 55TV2-43 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV2-13 55TV11-4 9098A 55TV13-4 9078A 55TV13-4 9084A-1-3 9084R-1-43 8 904R-1-43 8	3-8336 (See Model 33- 3-8335)—Set 225-91 -90238234_4 -90358 (See Model 35TV2- DD - 90608 (See Model 35TV2- DD - 90608 (See Model 35TV2- DD - 90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608237_5 -90608451V1-43- 45TV11-43-9088A45 -90697A45TV11-43- 45TV11-43-908A, 45 -90697A45TV11-43- 45TV11-43-9096A, 45 -9050A45TV11-43- 5005A45TV11-43- 5005A45TV11-43- 5005A45TV11-43- 5005A45TV11-43- 5005A45TV11-43- 5006A452-5 -9036A252-5 -6945A695-5 -7655A455-5 -7655A455-5 -7655A453-5 -7556A463-5 -7556A463-5 -7556A463-5 -7556A463-5 -7556A463-5 -7556A463-5 -7556A423-813-1 -85108, 94RA1-43-831- -85108, 94RA1-43-831- -8320A62-10 -8132A (See Model 94- 8127A-5et 62-10 -3815A, 8 94RA3-43-
13 KA 37.4 KA 37.4 15 TV 2-43 15 TV 1-44 15 TV 1-4	3-8335 (See Model 33- 3-8355 – Set 225-9) -90238 – 224-4 -90358 (See Model 35TV2- -90508 (See Model 35TV2- -90508 (See Model 35TV2- -90508 (See Model 35TV2- -90508 (See Model 35TV2- -90608 (See Model 35TV2- -90608 (See Model 33T-5 -90604 – 237-5 -90604 – 237-5 -90504 – 237-5 -90704 – 237-5 -90704 – 237-5 -90704 – 237-5 -90704 – 237-5 -90704 – 237-5 -90704 – 437011-43 (Series XT-100) – 262-5 -90304 – 252-5 -90304 – 252-5 -90304 – 252-5 -90304 – 252-5 -90304 – 252-5 -76560 - 94RA1-43-8511- -75-6 -81290 - 94RA1-43-8511 -75-6 -81290 - 94RA1-43-8511 -75-6 -81290 - 94RA1-43-8511 -75-6 -81290 - 94RA1-43-8511 -75-6 -81290 - 94RA1-43-8511 -75-6 -81290 - 94RA1-43-8511 -81294 – 546 -2-10 -81324 (See Model 94- 81294 – 54 62-10 -81324 (See Model 94- 81294 – 54 62-10 -81354 - 894RA1-43- -81-5 -94814 – 79-3 -98130C 94RA3-43-8
13 KA 37.4 KA 37.4 15 TV 2-43 15 TV 1-44 15 TV 1-4	3-8335 (See Model 35- 3-8355 – Set 225-9) -90236 (See Model 35172- 50256 (See Model 35172- 50257 (See Model 35172- 50257 (See Model 35172- 50737 (See Model 35172- 50136 (See Model 35172- 50257 (See Model 34- 51257 (See Model 34- 51257 (See Model 34- 51257 (See Model 34- 51257 (See Model 94- 51258 (S

CORONADO-Cont. 7651 1652 [See Model 43-7651-Ser 9.7] 7654A (See Model 15RA1-43-7654A -Ser 147.3] 7656A, 7657A (See Model 94RA1-43-7656A-Ser 73.2] 7666A (See Model 94RA1-43-7751A -Ser 232.3] 7756A, 56 Model 94RA1-43-7751A -755A, 56 Model 94RA1-43-7751A -755A, 56 Model 05RA1-43-7751A -36 Model 94RA1-43-7751A -36 Model 94RA1-43-7901A -36 Model 15RA1-43-7901A -36 H 15-2] 7910A, 7911A (See Model 15RA1-43-7902A -36 H 134-6) 8101 (See Model 15RA1-43-7902A -36 H 134-6) 8115A, B, 8115A (See Model Set 2103
 Set 2103
 Set 2004
 Set 2004
 Set 2004
 Set 217-53
 Set 217-53
 Set 217-54
 Set 217-54
 Set 217-55
 Set Model 94RA-43-61476-341 10) 8130C, 8131C (See Model 94RA33-43-8130C-Set 82-31 8145 (See Model 35RA33-43-8145 --Set 224-7) 8160 (See Model 43-8160-Set 12-71 7) 8177, 8178 (See Model 43-8178— Set 21-8) 8180 (See Model 43-8180—Set 10-8190 (See Model 43-8190-Set 19-8201 (See Model 43-8178-Set 21-8201 (See Model 43-8710-541 8) 8213 (See Model 35R43-43-8213-541 7-5) 5255 (See Model 35R43-43-8220-541 219-4) 8230A (See Model 05R42-43-8230-541 21-8) 8240A (See Model 43-8240-541 22-8) 8247A 8246A (See Model 15R43-43-8245A -541 74-5) 8247A (See Model 35R40-8247A -5et 22-6)
 Set 12.8)

 B247A
 B246A
 See Model 3FA33-43.8245A-Set 174-5)

 B247A
 See Model 3FA40-8247A

 -Set 236.3)
 B305 (See Model 43.8305-Set 8.3)

 B312 (See Model 43.8305-Set 8.3)
 B312 (See Model 43.8312A-Set 8.4)

 B330 (See Model 43.8305-Set 8.3)
 B313 (See Model 43.8330-Set 19.1)

 B351, B352 (See Model 43.8351-Set 12.3)
 Set 12.9)

 B353, B354 (See Model 43.8355-Set 8.6)
 Set 22.9)

 B360A (See Model 34RA37.43.8355
 -Set 122.9)

 B360A (See Model 34.837.43.8365
 -Set 169.4)

 B470 (See Model 34.8312A-Set 8.3)
 8420 (See Model 34.8312A-Set 8.3)

 B471 (See Model 34.8312A-Set 8.3)
 8510A. S511A (See Model 34.8312A-Set 8.3)

 B5108, 8511B (See Model 94RA1.43.8310A-Set 71.7)
 8510B, 8511A (See Model 94RA1.43.8310A-Set 71.7)

 B5108, 8511B (See Model 94RA1.43.8515A Set 110.5)
 85768 (See Model 34.8575A)

 B516 (See Model 94RA2.43.8515A Set 110.5)
 Set 8.40

 B5768 (See Model 43.8575A)
 See Model 34.8575A)

 B5768 (See Model 43.8575A)
 See Model 34.8575A)

 B5768 (See Model 43.8555A)
 Set 8.64

 B5768 (See Model 43.8555A)
 Set 110.5)

 B5768 (See Model 43.8556A 9-8) 8685 (See Model 43-8685—Ser 11-4) 8945A (See Model 05TV1-43-8945A—Ser 145-5) 8948A, 8949A (See Model 15TV4-43-8948A—Ser 175-7) •8950A (See Model 05TV2-43-9010-A-Set 146-5) •8953A (See Model 94TV6-43-8953-A-Set 106-3) •8957A (See Model 15TV1-43-8957-A-Set 62-4) B958A, B (See PCB 34—Set 162-1 and Model 15TV1-43-8958A—Set 161-3) •8965 (See Model 43-8965—Set 86-3) 8970A, 8971A, 8972A. 8973A (See Model 94TV2-43-8970A — Set 78-4) •8985A, 8986A, 8987A (See Model 94TV2-43-8970A-Set 78-4)

CORONADO-Cont.

CORONADO-Cont. 8993A. 8994A. 8995A (See Model 941V-43.8970A-Set 78-4) 9005A, 9006A (See Model 05TV1-43.8945A-Set 145-3) 9010A (See Model 05TV2-43-90108 Set 146-5) 9010B (See Model 05TV2-43-90108 -Set 153-2) 9014A (See Model 05TV1-43-9014A -Set 128-4)

WDDA (See Model 05172-43-9010A Set 146-5)
 MOLDA (See Model 05172-43-9010B --Set 123-2)
 MOLDA (See Model 05171-43-9014A 9005A, B, 9016A, B (See Model 15771-43.9957A-Set 162-4)
 MOLDA, B, 9016A, B (See Model 15771-43.9957A-Set 162-4)
 MOLDA, B, 9016A, B (See Model 15771-43.9957A-Set 162-4)
 MOLDA, B, 9016A, B (See Model 25172-34.9927A-Set 162-4)
 MOLDA, See Model 25172-43-9022A --Set 183-4)
 MOLDA (See Model 25172-43-9022A --Set 183-4)
 MOLDA (See Model 25172-43-9022A --Set 183-4)
 MOLDA (See Model 35172-43-9023A --Set 234-4)
 MOLDA (See Model X5172-43-9023A --Set 234-4)
 MOLDA (See Model X572 (43-9031) --Set 182-3)
 MOLDA (See Model X-721 [43-9031] --Set 182-3)
 MOLDA (See Model X-721 [43-9031] --Set 182-3)
 MOLDA (See Model X-721 [43-9031] --Set 182-3)
 MOLDA (See Model X-721 [43-9041] --Set 182-3)
 MOLDA (See Model X5172-43-9025A --Set 23-5)
 MOLDA (See Model X5172-43-9025A)
 MOLDA (See Model X5172-43-905A) --Set 192-3)
 MOLDA (See Model X5172-43-905A) --Set 197-5)
 MOLDA (See Model X5172-43-905A) --Set 199-5)
 MOLDA (See Model X5172-43-905A) --Set 237-5)
 MOLDA (See Model X5172-43-905A) --Set 237-5)

203-1, PCB VI-3ef 211-1 dnd Model 251V2-43.9060A - Set 199-5] 9061A (See Model 35TV2-43.9061A -Set 237-5] 9061A (See Model 45TV2-43.9061A -Set 237-5] 9063A (See Model 45TV2-43.9064A -Set 237-5] 9083A, 9086A, 9087A, 9088A, 9088A, 9083A, 9086A, 9087A, 9088A, 9083A, 9096A, 9087A, 9088A, 9087A, 9085A, 9085A, 9066A, 9087A, 9085A, 9085A, 9066A, 9087A, 9085A, 5065A, 9065A, 9077A, 9085A, 5065A, 9065A, 9077A, 9085A, 512-62-5] 9101A, 9102A (See Model 15TV2-43.9101A-Set 173-5] 9201 (See Model 13A974-3-9230A (See Model 15RA37-43-9230A (See Model 15RA37-43-9841A (See Model 94RA31-43-9841A (See Model 94RA31-43-9855 (See Model 35RA4-43-9855-Set 227-5) 9856A (See Model 35RA4-43-9856A -Set 221-4) 9876A (See Model 05RA4-43-9876A

CORONET

C2 .

CRAFTSMEN (Also see Radio Craftsmen)

CREST 10A, 10B Tel. UHF Conv....239-4

CRESTWOOD

(See Recorder Listing) CROMWELL

(Mercantile Stores)

CROSLEY

NOTE: PCB Denotes Production Change Bulletin. Production Chang

www.americanradiohistory.com

CKOSLET-CONT. DU-31CDM1, CDN, CHM, COB, COL, COLB, COM (Ch. 357-11) 173-13, 11-1) 202-2 EU-17 COM (Ch. 380, 383) 186-3 EU-17 COM (Ch. 380, 383) 186-3 EU-17 COM (Ch. 380, 383) 186-3 EU-17 COL Set 193-3) EU-21 CDBU (Ch. 381, 186-3 EU-21 CDBU (Ch. 381, 186-3) EU-21 CDBU (Ch. 381, 186-3) EU-21 CDBU (Ch. 381, 186-3) EU-21 CDBU (Ch. 381, 384) 186-3 EU-21 CDBU (Ch. 381, 384) 186-3 EU-21 CDBU (Ch. 381, 384) 186-3 EU-21 CDBU (Ch. 383, 186-3) EU-21 CDBU (Ch. 381, 384) 186-3 EU-21 CDBU (Ch. 383, 186-3) EU-21 CDBU (Ch. 381, 384) 186-3 EU-21 COBU (Ch. 383, 384) 186-3 EU-21 COBU (Ch. 381, 384) 186-3 EU-21 COBU (Ch. 387) (Aliso see PGB 73-Set 214-1) Model EU-17COM - Set 186-3) EU-21 COBU (Ch. 387) (Aliso see PGB 73-Set 214-1) EU-21 COBU (Ch. 387) (Aliso see PGB 73-Set 214-1) EU-21 COBU (Ch. 387) (Aliso see PGB 73-Set 214-1) EU-21 COBU (Ch. 387) (Aliso see PGB 73-Set 214-1) EU-21 COBU (Ch. 387) (Aliso see PGB 73-Set 214-1) EU-21 COBU (Ch. 387) (Aliso see PG F-17TOLBH (Ch. 402) F-17TOLBH (Ch. 402-1) F-17TOLBU (Ch. 402-1) F-17TOLH (Ch. 402-1) F-21CDLBH (Ch. 402-1) F-21CDLBH (Ch. 404-1) F-21CDLU (Ch. 404-1) F-21COLBU (Ch. 404-1) F-21COLBU (Ch. 404-1) F-21COLBU (Ch. 404-1) F-21COLBU (Ch. 404-1) F-21COLBH (Ch. 404-1) F-21COLBH (Ch. 403-1) .223—5 .223—5 .223—5 .223—5 .223—5 .223—5 .223—5 .223—5 .223—5 .223—5 • G-21TOBH, G-21TOBU [Ch. 4 263 431 • G-2110MH, G-2110MU (Ch. 431) 263-6 G-2110WH, G-2110W0 (24, 43) G-2110WH (Ch, 43) 263-6 H-21COMH, H-21COBU (Ch, 43)-2 H-21COMH, H-21COBU (Ch, 43)-2 H-21COMH, H-21COMU (Ch, 43)-2 H-21COSH, H-21COWU (Ch, 43)-2 H-21COWH, H-21COWU (Ch, 43)-2 H-21HCWH, H-21HCWU (Ch, 43)-2 H-21HCWH

263--6 eH-21HCWH, H-21HCWU (Ch. 431-21 263--6 eH-21TOBH (Ch. 431, -2) eH-21TOBH (Ch. 431, -2) eH-21TOWH (Ch. 431, -2) 263--6 eH-21TOWH (Ch. 431, -2) 263--6

CROSLEY-Cont.

CROSLEY-Cont. DC3 (Ch. 153-3 58-8 50-4 60-10 59-7 53-9 51-5 50-4 50-5 54-8 9-101 9-102 9-103, 9-104W 9-105, 9-106W 9-113, 9-114W 9-117 9-118W 9-127 9-118W 9-121, 9-120W 9-121, 9-120W 9-201, 9-202M, 9-2038 9-204, 9-205M 52-5 63-5 57-6
 9.204
 9.205M
 \$7-6

 9.207M
 \$3-10

 9.207,9.212M
 \$3-10

 9.213B
 (Sue Model 9.209-Set \$3-10)

 9.214M, 9.214M
 65-6

 9.302
 47-6

 9.403M, 9.403M-2
 79-4

 9.4047, 9.407M-1, 9.407M-2
 66-6

 9.407, 9.407M, 1, 9.407M-2
 66-6

 9.407, 9.413B, 9.413B-2, 9.414B
 79-4

 9.413B, 9.413B-2, 9.419M3-LD, 9.419M2, 94-31
 94-3

 9.419M3, 9.419M3-LD, 94-31
 79-4

 9.420M
 79-4

 9.420M
 81-6
 94–3 79–4 79–4 9423M 91–6 9423M 91–6 9423 924 10-135, 10-136, 10-137, 10-138, 10-307M, 10-308, 10-309, 93–3 10-307M, 10-308, 10-309, 93–3 10-412NU, 10-404M1U, 114–3 10-412NU, 10-404M1U, 114–3 10-414NU, 54, 116–4 10-414MU, 54, 116–4 10-414MU, 54, 116–4 10-414MU, 54, 116–4 10-414MU, 10-416M, 116–4 10-414MU, 10-416M, 116–4 10-414MU, 10-416M, 116–4 10-414MU, 10-414MU, 54 116–4 10-419NU, 114–3 10-420NU, 114–3
 10-418/w
 114-3

 10-419/w
 104-5

 10-419/w
 104-5

 10-420/w
 114-3

 10-427/w
 105-4

 10-427/w
 105-5

 10-427/w
 125-1A

 10-429/w
 129-5

 10-429/w
 16-4

 10-429/w
 16-4

 10-429/w
 16-4

 10-1000, 11-1010, 11-1020, 11-1020, 11-1030, 11-1030, 11-1020, 11-1030, 11-460MU (Ch. 321) ... 126-4
 11-461WU (Ch. 320) ... 147-4
 11-465WU (Ch. 320) ... 147-4
 11-470BU (Ch. 331) ... 126-4
 11-470BU (Ch. 330) ... 147-4
 11-472BU (Ch. 330) ... 147-4
 11-472BU (Ch. 331) ... 126-4
 11-472BU (Ch. 331, ... 1, -21) 126-4
 11-470BU (Ch. 331, ... 1, -21) 126-4
 11-550BU (Ch. 331, ... 1, -21) 126-4
 11-550BU (Ch. 331, ... 1, -2) 156-6
 170C0C1 (1-720C2, 170C0C3, 177
 CDC4 (Ch. 331, ... 1, -2) 156-7
 170C0C1 (1-720C2, 170C0C3, 17-7
 56FA, 56FB, 56FC 31-7
 56FA, 56FB, 5 15-5 31-7 10-9 21-9 4-3 5-14 4-3 5-14 4-9 8-5 33-2 5613 5617 5617 5617 5612 5618, 5615 5610 5710 (See Model 5610—Set
 30:10
 (See Model 56TQ—Set 33.2)

 58TA
 36.4

 58TC
 (See Model 58TW—38.2)

 58TC
 Set (See Model 58TW—38.2)

 58TT
 36.4

 58TC
 Set (See Model 58TW—38.2)

 58TT
 36.4

 58TT
 36.2

 58TT
 36.2

 58TT
 38.2

 58CC
 58.2

 58CC
 58.2

 58CC
 58.2

 58CC
 57.3

 58TA
 58.7

 58TA
 58.7

 58TA
 58.7

 58TA
 58.7

 58TA
 36.5

 88CR (See Model 87CQ—Set 36-5)

 88TA, 88TC
 3B-3

 88TA, 88TC (Revised) (See Set 43-8)

 and Model 88TA—Set 38-3)

 106CP, 106CS
 7-6

 146CS
 25-10

 146CP, 148CQ
 42-6

CROSLEY-Cont. CROYDON CRYSTAL PRODUCTS (See Coronet) DALBAR Barcombo Jr., Barcombo Sr. 10–14 M8 ''Tonomatic'' 8–34 100-1000 Series 10–15 400 9–9 DAVID BOGEN AMB-1 TV Booster 246-3 AM901 195-6 AM901-1 (See Model AM901-Set 195-6) BB-1A TV Booster 228-7 B(B-1 (TV Booster) 228-7 DB-10 2610-228-7 261-6 102-4 253-5 DB10A 102-4 DB10-1 (See Model DB10 - Set 102-4) 102-4) 233-5 DB10-1 (See Model DB10 - Set 102-4) DB20 237-6 DO10 231-5 DP-16 144-8 EQR 227-6 EV23-4 234-4 227-6 234-6 76-9 85-4 83-2 EX326 E66 E75 83 250 198 250 6 30 6 26 9 22-12 25-11 80 4 E75 FC-1 FM801 FR-1 G-50 GO-50 GO-50 CO-125 GX50 23-11 80-6 79-5 78-6 71-8 154-3 80-5 183-5 H15 H30 H30 H50, HL50, H2L50 H623 HE-10 HOH, HOL HO10 HO10 HO125 H220 84-5 HO125 HX30 HX50 HX-632 JOH, JOL JX30 JX50 J50 87—4 82—4 75—7 169—5 253—6 257—4 255—4 J50 LOH, LOL LP16 LSC PH10 PH10-1 .(68-5) PR PS-1 PS-1 PX 258. 80-5 86 227 73 PHIO-Set (See Model 242-5 250-6 183-5 68-5 72-7 242-5 241-5 243-3 183-5 PS-1 PX10 PX10 PX15 RC RP-1, RP-1L RP500 RX

33-3 67-8 175-9 227-6 R602 R604 R701 R701 SA10-40 UCT (Tel. UHF Conv.) UCT-1 UHF Conv. UP16 VP17, VP17X 2AR, 2RS 11D 11U 227---6 252--6 262--6 249--6 86--4 259--4 28--8 77--5 76-10 74--2 77--5 76-10 210 21U 21X 76-10 DEARBORN 100 22-13 DECCA DP11 DP29 PT-10 19-13 25-12 DELCO 42--7 R-705 42--7 R-1227, R-1228, R-1229 15--6 R-1230-A, R-1231-A, R-1232-A 14-33 R-1233 42--8 R-1234, R-1235 7--7 R-1233 R-1234, R-1235 R-1236, R-1237 R-1238 29—7 38—4 R-1236 R-1237 38-4 R-1241 62-11 R-1242 31-8 R-1243 31-8 R-1244 R-1245 R-1243 32-4 R-1244 R-1245 R-1246 R-1246 S2-6 R-1248 R-1248 R-1246 R-1252 21-10 R-1253 R-1255 R-1409 15-7 TV-101 15-7 88-33 TV-102 88-33 TV-102 88-35 TV-201 59-8 DeSOTO (See Mopar) DETROLA DETROLA \$54.1-61A (See Aria Model 554-1-61A-Set 67-2) \$58-1-49A 7--8 \$68-13-221D 9-10 \$718L 10-16 \$718L 10-16 \$718L 9-11 \$72-220-226A 8--6 \$779 7-9 577-1-6A 8-7 579 7-9 7-91 588 582 19-14 610-A 55-8 611-A 50-6 626 Series 11-5 7156 48-6 7270 16-8 19–14 55—8 50—6 11—5 DEWALD DEWALD 4-22 A500 4-22 A5001 (See Model A500—Set 4-22) 4-20 A500W (See Model A500 — Set 4-22) 4-21 A501, A502, A503 4-22 A504, A505 16—9 A-509 31—9 A502, A505 14—27 A-514 Ad02, Ad05 I 6-10 Ad02 (See Model Ad02—Set I6-10) B-400 35—3 8-401 34—6 B-402 45—8 B-402 45—8 B-403 52—7 B-504 43—9 B-506 38—5 B-510 34—7 B-512 35—4 B-513 63—6 B-614 42—9 B-614 56—9 B-614 56—9 B-614 64—4 C-516 64—4 C-516 64—4 C-510 69—7 A605 B-512 B-515 B-612 B-614 • BT-100, BT-101 C-516 C-800 C-316 C-800 C-800 C-7102, CT-103, CT-104 82-5 D-517A D-517A D-517A D-517A D-517A D-518 D-508 C-508 D-518 D-518 D-518 D-518 D-518 D-519 D-518 D-519 D-518 D-519 D-518 D-519 D-519 D-518 D-519 D-518 D-519 D-518 D-519 D-519 D-518 D-505 D-● DT-190 (Also see PCB 58—5et 192-1) 136—7 • DT-1900 (DT-1020A 100—6 • DT-1030, DT-1030A 100—6 • DT-1030, DT-1030A 100—6 • DT-X-160 100—6 • E-520 128—5 • E-140, ET-141 (Also see PCB 58 —5et 192-1) 136—7 • ET-140, ET-141 (Also see PCB 58 —5et 192-1) 136—7 • ET-171 (Also see PCB 58—5et 192-1) 136—7 • ET-1712 (Also see PCB 58—5et 192-1) 136—7 • ET-1712 (Also see PCB 58—5et 192-1) 136—7 • ET-1712 (Also see PCB 58—5et 192-1) 136—7 • ET-1700, R (Also see PCB 58—5et 192-1) 136—7 • ET-1700, R (Also see PCB 58—5et 192-1) 136—7 • ET-1700 (Revised) 136—7 • ET-1700 (Revised) 208—3 • FT-200 (See PCB 58—5et 172-1) and 1974 (DSR 58—5et 136-7) • FT-000 (Revised) 208—3 • FT-200 (See PCB 58—5et 136-7) • F404 58-

DAVID BOGEN-Cont.

.238-7

R300 R501

CROSLEY-DUMONT

DEWALD-Cont.

F-523 G-174 G-201 G-200, G-211 G-200, G-211 H-300 UHF Conv. H-527 H-528 H-533 S11 170-208-208-208-220-250-239-234-71_9 DODGE (See Mopar) DORN'S (See Bell Air) DOUGLAS • 327 (Ch. S-103, T-103) 246-4 DREXEL (Mutual Buying Syndicate) 17CG1, 17TW (Similar to Chassis) 149-13 DUKANE
 JA45-A
 184--5

 IA300, 18300
 187--6

 JU325
 185--6

 4A100
 186--5

 48100 (See Model 4A100-Set

 105-51
 187
 184—5 189—6 4C25 Flexiphone 187-4 DUMONT
 DUMONT

 • RA-103 (Also see PCB 6—Set 108-1)

 • 90-3

 • RA-103D (Also see PCB 9—Set 114-1)

 • 93-4

 • RA-104A (Also see PCB 9—Set 714-1)

 • 93-4

 • 93-4
 • RA-105 (Also see PCB 6-Set 108-1) 72-8
 • RA-112-A1,
 A6 (Also see PCB 38—Set)
 119—5

 • A6 (Also see PCB 38—Set)
 119—5
 119—5

 • RA-113-81, -82, -83, -84, -85, -86, -87, -88 (Also see PCB 38—Set)
 119—5

 • RA-116
 • RA-116
 • RA-116

 • RA-117-A1, -A3, -A5, -A6, -A7
 131—5

 • S6
 • S6, -187, -185, -185, -185, -186 RA-104, A1 (Also see PCB 60—Set 206-1)
 194-1 and PC6 60—Set 206-1)
 RA-165, -81, -82, -83, -86, -87
 RA-165, -81, -82, -83, -86, -87
 RA-165, RA-167, RA-168, RA-169, RA-160, RA-167, RA-177, RA-171, ..., 216-2
 RA-170, RA-177, ..., 216-2
 RA-170, RA-177, ..., 216-2
 RA-166, RA-167, RA-168, RA-169, RA-177, A6 (See Model RA-117A)
 Andover Model RA-147A (See Model RA-147A)
 Andover Model RA-112A)
 Andover Model RA-162-821 through B26 (See Model RA-162)
 Benbury Model RA-162-821 through B26 (See Model RA-162)
 Benbury Model RA-162-821 through B26 (See Model RA-162)
 Berdird Models RA-306, RA-307 (See Model RA-163)
 Brotaford (See Model RA-103, RA-307)
 See Model RA-130, RA-307 (See Model RA-113)
 Brodoff Models RA-306, RA-307 (See Model RA-113)
 Brodoff Models RA-306, RA-307 (See Model RA-113)
 Brodoff Models RA-306, RA-307 (See Model RA-113)
 Brodoff (See Model RA-113-81, -82 (See Model RA-113)
 Brodoff RA-163)
 Brodoff RA-113-81, -82 (See Model RA-113)
 Brodoff RA-113-81, -84 (See Model RA-113)
 Chether Model RA-113-85, -86 (See Model RA-113)
 Chether Model RA-113-85, -86 (See Model RA-13)
 Chether Model RA-164 (See Model RA-163)
 Chether Model RA-164, 168, RA-169
 Chether Model RA-164, 168, RA-169
 Chether Model RA-164, 164, 164 (See Model RA-164)
 Chether Model RA-164, 164, 164, 164
 Club 20 (See Model RA-164, 164, 164, 164, 164
 Club 20 (See Model RA-163)
 Chether Model RA-164, 164, 164
 Chether Model RA-164, 164, 164
 Chether Model RA

www.americanradiohistory.com

DUMONT-EMERSON

DUMONT-Cont. Hanover Model RA-162 (See Model

Hanover Model RA-162 (See Model RA-162)
Hanover II Model RA-170 (See
Model RA-170) Hanover II Model RA-171 (See Model RA-171) Hartford Models RA-306, RA-307 (See Model RA-306)
Hartford Models RA-306, RA-307
(See Model RA-306) Hastings (See Model RA-104A) Lynwood Model RA-167 (See Model
RA-167)
Lynwood Model RA-169 (See Model RA-169)
Monsfield (See Model RA-108A)
Meadowbrook Model RA-103 (See Model RA-103)
Meadowbrook II (See model KA-
Milford Model RA-165-B1 (See
147A) Milford Model RA-165-B1 (See Model RA-165) Mt. Vernon Model RA-112-A3, -A6 (See Model RA-112A)
Newbury [See Model KA-162]
Newbury II Model RA-170 (See Model RA-170)
Newbury II Model RA-171 (See Model RA-171) Newport Models RA-306, RA-307 (See Model RA-306)
Newport Models RA-306, RA-307
Oxford Model KA-16/ (See Model
Park Lane Model RA-117-A7 (See
Parklane (See Model RA-147A)
Putnam Model RA-111-A1, -A4 (See Model RA-111A)
Revere Model RA-113-B3, -B4 (See Model RA-113)
KA-167) Park Lane Model RA-117-A7 (See Model RA-117A) Parklane (See Model RA-147A) Putnam Model RA-111-A1, -A4 (See Model RA-111A) Revere Model RA-113-B3, -B4 (See Model RA-113) Ridgewood Model RA-165-B4 (See Model RA-165)
Model RA-165) Ridgewood ''41'' Model RA-167 (See Model RA-167)
(See Model RA-167) Royal Sovereign (See Model RA- 119A)
Rumson (See Model RA-103D)
Rutland Models RA-306, RA-307 (See Model RA-306)
Savoy (See Model RA-103) Sheffield (See Model RA-103D)
Sheffield Models RA/306, RA-307 (See Model RA-306)
Shelburne Model RA-165-B5 (See
(See Modei RA-306) Shelburne Modei RA-165-85 (See Model RA-165) Sherbroake Models RA-109-A3 -A7 (See Model RA-109A) Sherbroake (See Model RA-109A- FAS) Sherbroake (See Model RA-130A)
Sherbrooke (See Model RA-109A-
Sherbrooke (See Model RA-130A)
Somerset (See Model RA-162) Somerset II Model RA-170 (See
Model RA-170) Somerset II Model RA-171 (See
Model RA-171) Stratford (See Model RA-105A)
Somerset (See Model RA-162) Somerset II Model RA-170 (See Model RA-170) Somerset II Model RA-171 (See Model RA-171) Stratford (See Model RA-105A) Strathmore Model RA-117-A1 (See Model RA-117A) Sumter Model RA-117-A1 (See Model RA-117A) Sussex (See Model RA-105B) Sutton Model (RA-103 (See Model RA-103)
Sumter Model RA-117-A1 (See
Model RA-117A) Sussex (See Model RA-105B)
Sutton Model (RA-103 (See Model RA-103)
Tarrytown Models RA-113-B7, -B8
Tarrytown (See Model RA-120)
(See Model KA-113) Tarrytown (See Model RA-120) Wakefield Model RA-165-B3 (See Model RA-164) Wakefield '41' Madel RA 147 (See
Madel DA 1443
(See Model RA-113) Torrytown (See Model RA-120) Wakefield Model RA-165-B3 (See Model RA-164) Wakefield "41" Model RA-167 (See Model RA-167) Warren Model RA-307) (See Model RA-307)
(See Model RA-113) Tarrytown (See Model RA-120) Wakefield Model RA-165-B3 (See Model RA-164) Wakefield "41" Model RA-167 (See Model RA-307) Warren Models RA-306, RA-307 (See Model RA-306) (See Model RA-306)
[See Model RA-113] Tarrytown (See Model RA-120) Wakefield Model RA-165-B3 (See Model RA-164) Wakefield "41" Model RA-167 (See Model RA-167) Warren Models RA-306, RA-307 (See Model RA-306) Welthongka RA-306, RA-307 Wethongk Model RA-306, RA-307
Model KA-16/) Warren Models RA-306, RA-307 (See Model RA-307) Warwick Models RA-306, RA-307 (See Model RA-306) Wellington (See Model RA104A) Wellington (See Model RA104A) Wellington (See Model RA104A)
Model KA-16/) Warren Models RA-306, RA-307 (See Model RA-307) Warwick Models RA-306, RA-307 (See Model RA-306) Wellington (See Model RA104A) Wellington (See Model RA104A) Wellington (See Model RA104A)
Worten Model: RA-106, RA-307 (See Model: RA-307) Worwick Model: RA-307 Worting Model: RA-306, RA-307 Worting to Radio RA-306, RA-307 Westbrook Model: RA-306, RA-307 (See Model: RA-306) Westbury (See Model RA-105A) Westbury 11 (See Model RA-109A- FAS)
Model KA-10/) Warren Models RA-307 (See Models RA-306, RA-307 (See Model RA-307) Wellington (See Model RA-306, RA-307 (See Model RA-306, RA-307 (See Model RA-306) Westbury (See Model RA-109A- FAS) Westbury 11 (See Model RA-109A- FAS) Westbury 11 (See Model RA-109A- FAS) Westerly Model RA-112A) Westerly Model RA-112A)
Model KA-10/) Warren Models RA-307 (See Models RA-306, RA-307 (See Model RA-307) Wellington (See Model RA-306, RA-307 (See Model RA-306, RA-307 (See Model RA-306) Westbury (See Model RA-109A- FAS) Westbury 11 (See Model RA-109A- FAS) Westbury 11 (See Model RA-109A- FAS) Westerly Model RA-112A) Westerly Model RA-112A)
Model KA-16/) Warren Models RA-306, RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) Westbury (See Model RA-105A) Westbury 11 (See Model RA-105A) Westwiry Model RA-112-A2, -A5 (See Model RA-112A) Westwird (See Model RA-110A) Westwird (See Model RA-110A) Westwird (See Model RA-110A) Whiteholl 11 (See Model RA-130A)
Model RA-10/) Warren Models RA-307 (See Models RA-306, RA-307 (See Model RA-307) Wellington (See Model RA-306, RA-307 (See Model RA-306) Westbury (See Model RA-108, RA-307 (See Model RA-306) Westbury 11 (See Model RA-109A- FAS) Westbury 11 (See Model RA-109A- FAS) Westehall (See Model RA-110A) Westehall (See Model RA-110A) Weitehall (See Model RA-110A) Whitehall 11 (See Model RA-130A) Whitehall 11 (See Model RA-130A) Whitehall 11 (See Model RA-130A) Whitehall 11 (See Model RA-162-B7 (See Model RA-162-B1 (See
Model RA-10/) Warren Models RA-307 (See Models RA-306, RA-307 (See Model RA-307) Wellington (See Model RA-306, RA-307 (See Model RA-306, RA-307 (See Model RA-306) Westbury (See Model RA-108A, FAS) Westbury II (See Model RA-109A- FAS) Westbury II (See Model RA-109A- FAS) Westerly Model RA-112A) Westerly II (See Model RA-110A) Whitehall (See Model RA-110A) Whitehall II (See Model RA-110A) Whitehall II (See Model RA-130A) Whitehall II (See Model RA-130A) Whitehall II (See Model RA-162-B7 (See Model RA-162-B1 (See
Model KA-16/) Warren Models RA-306, RA-307 (See Models RA-307) (See Model RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) Westbury (See Model RA-105A) Westbury II (See Model RA-105A) Westbury II (See Model RA-107A- fAS) Westerly Model RA-112-A2, -A5 (See Model RA-112A) Westword (See Model RA-110A) Whitehall II (See Model RA-110A) Whitehall II (See Model RA-102A) (See Model RA-162-B) (See Model RA-162) Wickford Model RA-162-B) (See Model RA-162) Wimbledon Model RA-162-B) (See Model RA-162)
Model KA-16/) Warren Models RA-306, RA-307 (See Models RA-307) (See Model RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) Westbury (See Model RA-105A) Westbury II (See Model RA-105A) Westbury II (See Model RA-107A- fAS) Westerly Model RA-112-A2, -A5 (See Model RA-112A) Westword (See Model RA-110A) Whitehall II (See Model RA-110A) Whitehall II (See Model RA-102A) (See Model RA-162-B) (See Model RA-162) Wickford Model RA-162-B) (See Model RA-162) Wimbledon Model RA-162-B) (See Model RA-162)
Model KA-16/) Warren Models RA-306, RA-307 (See Models RA-307) (See Model RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) Westbury (See Model RA-105A) Westbury II (See Model RA-105A) Westbury II (See Model RA-107A- fAS) Westerly Model RA-112-A2, -A5 (See Model RA-112A) Westword (See Model RA-110A) Whitehall II (See Model RA-110A) Whitehall II (See Model RA-102A) (See Model RA-162-B) (See Model RA-162) Wickford Model RA-162-B) (See Model RA-162) Wimbledon Model RA-162-B) (See Model RA-162)
Model RA-10/) Warren Models RA-307 (See Models RA-306, RA-307 (See Model RA-307) Wellington (See Model RA-306, RA-307 (See Model RA-306, RA-307 (See Model RA-306) Westbury (See Model RA-108A, FAS) Westbury II (See Model RA-109A- FAS) Westbury II (See Model RA-109A- FAS) Westerly Model RA-112A) Westerly II (See Model RA-110A) Whitehall (See Model RA-110A) Whitehall II (See Model RA-110A) Whitehall II (See Model RA-130A) Whitehall II (See Model RA-130A) Whitehall II (See Model RA-162-B7 (See Model RA-162-B1 (See
Model KA-16/) Warren Models RA-306, RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) (See Model RA-306, RA-307) Westbury (See Model RA-105A) Westbury 11 (See Model RA-107A- fAS) Westbury 11 (See Model RA-107A- fAS) Westward (See Model RA-107A- fAS) Westward (See Model RA-107A- fAS) Westward (See Model RA-107A- fAS) Westward (See Model RA-107A) Whitehall 11 (See Model RA-105A) Whitehall 11 (See Model RA-105A) Whitehall 11 (See Model RA-105A) Whitehall 11 (See Model RA-105A) Whitehall 11 (See Model RA-162-B1 (See Model RA-162-B1 (See Model RA-162-B1 (See Model RA-162-B1 (See Model RA-306, RA-307 (See Model RA-107A-FAS) Winstow Model RA-107A- (See Model RA-107A) Winthrap Model RA-103 (See Model RA-103) DUOSONIC
Model RA-10/) Warren Models RA-300, RA-307 (See Model RA-307) See Model RA-307) (See Model RA-306, RA-307) (See Model RA-306) Wellington (See Model RA-104A) Westbrock Models RA-306, RA-307 (See Model RA-106A) Westbury (See Model RA-105A) Westbury (See Model RA-107A) Fibury II (See Model RA-107A) Westbury II (See Model RA-107A) Westbury (See Model RA-112A) Westbury (See Model RA-112A) Westbury (See Model RA-112A) Whitehall II (See Model RA-112A) Wickford Model RA-162-81 (See Model RA-162) Windlow Model RA-107A, RA-307 (See Model RA-107A) Winslow Kodel RA-107A) See Model RA-107A) Winslow Model RA-107A) See Model RA-107A) See Model RA-107A) Winslow Kodel RA-107A) See Model RA-107A) Winthrop Model RA-103 (See Model RA-103) DUOSONIC
Model RA-16/) Warren Models RA-306, RA-307 (See Models RA-306, RA-307 (See Model RA-307) Warwick Models RA-306, RA-307 (See Model RA-306, RA-307) (See Model RA-107) Westbury (See Model RA-107A- fA3) Westerly Model RA-112-A2, -A5 (See Model RA-112A) Westword (See Model RA-110A) Whiteholl I (See Model RA-1105A) Whiteholl II (See Model RA-105A) Witschord Model RA-162-B1 (See Model RA-162) Witschord Model RA-162-B1 (See Model RA-162) Model RA-162-B1 (See Model RA-162-B6) (See Model RA-162) Winshord Model RA-162-B1 (See Model RA-162-B1 (See Model RA-162) Winshord Model RA-103 (See Model RA-103) W
Warren Maclai, RA-102, J. Warren Madels, RA-306, RA-307 (See Model RA-307) (See Model, RA-306, RA-307) (See Model, RA-104, RA-307) (See Model, RA-104, RA-107) Weitrigton, Model, RA-112, RA-22, -A5 (See Model, RA-112, PA) Weitrigton, Model, RA-112, PA) Weitrigton, Model, RA-112, PA) Weitrigton, Model, RA-112, PA) Weitrigton, See Model, RA-103, PA) Whiteholl, II, Model, RA-162-81 (See Model, RA-162, PK) Wimbledon, Model, RA-102, RA-307 (See Model, RA-102, RA-307, See Model, RA-103, RA-307 (See Model, RA-103, See Model, RA-103, See Model, RA-103, RA-307 (See Model, RA-103, See M
Warren Maclei RA-10/, A.306, RA-307 (See Model RA-307) (See Model RA-307) Warren K Models RA-306, RA-307 Weitbork Machi RA-306, RA-307 Weitbork Machi RA-306, RA-307 Weitbork Machi RA-306, RA-307 Weitbory (See Model RA-105A) Weitbury II (See Model RA-105A) Weitbury (See Model RA-112A) Weitbork Model RA-112A) Weitber (See Model RA-112A) Whiteholl II (See Model RA-105A) Whiteholl II (See Model RA-105A) Whiteholl II (See Model RA-105A) Winklood Model RA-162-80 (See Model RA-162-86 (See Model RA-106A) Winslow Model RA-103(See Model RA-107A) Winslow Model RA-103 (See Model RA-107A) See Model RA-103 (See Model RA-107A) Winslow Model RA-103 (See Model RA-107A) Winslow Model RA-103 (See Model RA-107A) See Model RA-103 (See Model RA-107A) See Model RA-103 (See Model RA-107A) See Model RA-103 (See Model RA-107A) Winslow Geel RA-103 (See Model RA-107A) See Model RA-103 (See Model RA-107A) See Model RA-103 (See Model RA-1
Warren Maclei RA-107 See Model RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-306) RA-307 (See Model RA-306) RA-307 (See Model RA-306) RA-307 (See Model RA-306) RA-307 (See Model RA-108) RA-307 (See Model RA-108) RA-307 (See Model RA-107) I See Model RA-109A- FAS) (See Model RA-112A) - A5 (See Model RA-112A) Weitheholl See Model RA-107A- FAS) Witteholl I See Model RA-107A) Weitheholl I See Model RA-107A) Whiteholl II (See Model RA-107A) See Model RA-162 Wittehold II Model RA-162-80 (See Model RA-162 See Model RA-107A, A-307 (See Model RA-107A) See Model RA-107A, A-307 (See Model RA-103) See Model RA-107A, A-307
Warren Maclei RA-107 See Model RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-306) RA-307 (See Model RA-306) RA-307 (See Model RA-306) RA-307 (See Model RA-306) RA-307 (See Model RA-108A) Weithigton (See Model RA-107A- FAS) Weiterly Model RA-112A) -A5 (See Model RA-112A) Weiterly Model RA-112A) Whiteholl (See Model RA-112A) Weiterly Model RA-112A) Whiteholl (See Model RA-107A) Weiterly Model RA-162-87 (See Model RA-162) Wickford Model RA-162-86 (See Model RA-162) See Model RA-107A, A- A5 Winslew Goel RA-107A, A- A5 See Model RA-107A, A- A5 See Model RA-107A, A- A5 See Model RA-107A, A- A5 Winslew Goel RA-107A, A- A5 See Model RA-107A, A- A5 See Model RA-107A, A- A5 See Model RA- A- A- A5
Warren Maclei RA-16/, p. 306, RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-306) Weltington (See Model RA-306, RA-307) (See Model RA-306) Weltington (See Model RA-103, Model RA-107, Model RA-107, Model RA-107, FAS) Weithy (See Model RA-112A) Weithy Model RA-112A) Weithy Model RA-112A) Whiteholl (See Model RA-107, See Model RA-107, See Model RA-162-86 (See Model RA-162, See Model RA-106, RA-307) Winslow Model RA-103 (See Model RA-107, See Model RA-103, Model RA-103] Winslow Model RA-103 (See Model RA-107, See Model RA-107, See Model RA-103, See Model RA-107, See Model RA-107, See Model RA-107, See Model RA-103, See Model RA-107, See Model RA-103, See Model RA-107, See Model
Worren Model: RA-307 (See Model: RA-306 Weltington See Model: RA-307 (See Model: RA-306 RA-307 (See Model: RA-306 RA-307 Westbury (See Model: RA-107 Westbury (See Model: RA-107 Westbury (See Model: RA-107 Westbury (See Model: RA-107 Westbury (See Model: RA-102 Westbury (See Model: RA-102 Westbury (See Model: RA-102 Wintbode Model: RA-102 See Model RA-103 S
Worren Model: RA-307 (See Model: RA-306 Weltington See Model: RA-307 (See Model: RA-306 RA-307 (See Model: RA-306 RA-307 Westbury (See Model: RA-107 Westbury (See Model: RA-107 Westbury (See Model: RA-107 Westbury (See Model: RA-107 Westbury (See Model: RA-102 Westbury (See Model: RA-102 Westbury (See Model: RA-102 Wintbode Model: RA-102 See Model RA-103 S
Warren Models RA-10, J Warren Models RA-306, RA-307 (See Model RA-307) Warwick Models RA-306, RA-307 Warwick Models RA-306, RA-307 Warwick Models RA-306, RA-307 Warwick Models RA-306, RA-307 Weitbord Medel RA-306, RA-307 Weitbord Medel RA-306, RA-307 Weitbord Medel RA-306, RA-307 Weitbord Medel RA-306, RA-307 Weitbury II (See Model RA-105A) Weitbury II (See Model RA-107A) Yestbury (See Model RA-112A) Weitbed I See Model RA-107A) Weitbed I See Model RA-107A) Whiteholl II (See Model RA-107A) Whiteholl II (See Model RA-107A) Windson Model RA-162-80 (See Model RA-162-80 (See Model RA-162-81 (See Model RA-163) Winslaw Model RA-162-81 (See Model RA-107A) See Model RA-162-81 (See Model RA-163) Winslaw Model RA-162-81 (See Model RA-163 (See Model RA-163) Winslaw Godel RA-162 (See Model RA-163) <td< td=""></td<>
Warren Maclei RA-307 (See Models RA-306, RA-307 (See Models RA-307) Warwick Models RA-306, RA-307 (See Model RA-306, RA-307) Weltington (See Model RA-306, RA-307) Weltington (See Model RA-306, RA-307) Wester (See Model RA-1064) Wester (See Model RA-1074, FAS) Wester (See Model RA-112-A2, -A5) (See Model RA-112-A2, -A5) Wester (See Model RA-112A) Wester (See Model RA-112A) Wester (See Model RA-112A) Wester (See Model RA-112A) Wester (See Model RA-162A) Wester (See Model RA-162A) Witscholl (See Model RA-162A) Witscholl (See Model RA-162-B1 (See Model RA-162) Witscholl RA-162 Witscholl RA-162 Witscholl RA-163 Winscholl RA-103 (See Model RA-103) See Model RA-103 (See Model RA-103) BOYNAVOX AP-514 (Ch. A1) <tr< td=""></tr<>
Model RA-10/1 Warren Models RA-307 (See Models RA-306 Weltington See Model Weltington See Model Weltington See Model Weltington See Model Westbury ISee Model Mithehall ISee Model Mithehall ISee Kale Model RA-102-81 See
Model RA-10/1 Warren Models RA-307 (See Models RA-306 Weltington See Model RA-306 Weltington See Model RA-107 (See Model RA-107 See (See Model RA-107 See Weithigton I (See Model RA-109A-105A) Weithigton I (See Rodel RA-107A) Weithigton I (See Model RA-107A) Weithigton I (See Model RA-107A) Whithehall II (See I (See See Model RA-107A) See Model RA-107A) See Model RA-107A) See See Model RA-107A) See Model RA-107A)
Model RA-10/1 Warren Models RA-307 (See Models RA-306 Weltington See Model RA-306 Weltington See Model RA-107 (See Model RA-107 See (See Model RA-107 See Weithigton I (See Model RA-109A-105A) Weithigton I (See Rodel RA-107A) Weithigton I (See Model RA-107A) Weithigton I (See Model RA-107A) Whithehall II (See I (See See Model RA-107A) See Model RA-107A) See Model RA-107A) See See Model RA-107A) See Model RA-107A)
Warren Maclei RA-107 See Model RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-306) RA-307) (See Model RA-107A) Weitbury (See Model RA-107A) Weitbury (See Model RA-112A) - A5 (See Model RA-112A) Weitbury (See Model RA-112A) Whiteholl (See Model RA-112A) Weitbury (See Model RA-107A) Whiteholl II (See Model RA-162-86) See Model RA-162-87 (See Model RA-162-86) Winblood Model RA-162-86 (See Model RA-162-86) See Model RA-107A) Winslow Model RA-103 (See Model RA-107A) See Model RA-107A) Vinslow Model RA-103 (See Model RA-107A) See Model RA-107A) See Model RA-103 (See Model RA-107A) See Model RA-107A) Minslow Goel RA-107A) See See Model RA-107A) Model RA-107A) See See Model RA-107A) Minslow Goel RA-107A) See Model RA-107A)
Warren Madeis RA-307 (See Models RA-307) Warren Madeis RA-306, RA-307 (See Model RA-307) Warwick Models RA-306, RA-307 (See Model RA-306) Warwick Models RA-306, RA-307 (See Model RA-306) Weithury In See Model RA-105A) Weithury (See Model RA-105A) Weithury (See Model RA-107A) Weithend (See Model RA-107A) Weithend (See Model RA-107A) Whiteholl II (See Model RA-107A) Whiteholl II Model RA-162-87 (See Model RA-162) Winklood Model RA-162-86 (See Model RA-162) Wimbledon Model RA-107A, FAS1 Winslow Model RA-107A, AS See Model RA-107A, AS See Model RA-107A, AS See Model RA-107A, AS Winslow Model RA-107A, AS See Model RA-107A, AS Winslow Model RA-107A, AS See Model RA-107A, AS
Warren Maclei RA-107 See Model RA-307 (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-307) (See Model RA-306) RA-307) (See Model RA-107A) Weitbury (See Model RA-107A) Weitbury (See Model RA-112A) - A5 (See Model RA-112A) Weitbury (See Model RA-112A) Whiteholl (See Model RA-112A) Weitbury (See Model RA-107A) Whiteholl II (See Model RA-162-86) See Model RA-162-87 (See Model RA-162-86) Winblood Model RA-162-86 (See Model RA-162-86) See Model RA-107A) Winslow Model RA-103 (See Model RA-107A) A5 (See Model RA-103) See Model RA-107A) Winslow Model RA-103 (See Model RA-107A) A5 (See Model RA-103) See Model RA-107A) DUOSONIC K1, K2 19-15 K1, K2 19-15 Model RA-103 See

EDWARDS	EMERSON-Cont.
Fidelotuner	5778 (Ch. 1200128) 578 (Ch. 120050) (S —Set 25-13)
(Also see Recorder Listing) 15	579A (Ch. 120034A) 580 (Ch. 120064)
EKOTAPE	581 (Ch. 120014A, 582 (See Model 548
(See Recorder Listing) ELCAR	
602 5–19	586 (Ch. 120023B, 1 587 (Ch. 120033A,
ELECTONE T5TS3 12–34	588 (See Model 54) 590 (Ch. 120101A, 591 (Ch. 120055A
ELECTRO	594, 595 (Ch. 120038
B-20 14—9 ELECTROMATIC	596 597 (Ch. 120073B3
APH301-A, APH301-C 7-11 606A, 607A 5-32	596 597 (Ch. 120073B3 599 (Ch. 120075B) 600 (Ch. 120103-B) 9Set 114-1)
ELECTRO-TONE	601 (Ch. 120075B) 602 (Ch. 120072A,
555 13-17 706, 712 (See Model 555-Set 13-	
16) ELECTRO-VOICE	604A (See Model 5) 605 (Ch. 120076B)
3300 Tel. UHF Conv 222-5	603 (Ch. 120053B) 604A (See Model S) 605 (Ch. 120076B). 606 (Ch. 120066B). 606 (Ch. 120068B 606 (Ch. 120086B 606 (Ch. 120086B) 607 (Ch. 120084B 607 (Ch. 120084B 607 (Ch. 120074A) 608A (Ch. 120084B). 607 (Ch. 120074B) 608 (Ch. 120074B). 608 (Ch. 120086B). 608 (Ch.
ELECTRONIC CORP. OF AMERICA (See ECA)	•606 (Ch. 1200868) 607 (Ch. 120074A
ELECTRONIC SPECIALTY CO. (See Ranger)	609 (Ch. 120089 609 (Ch. 120084-B 610 (Ch. 120100A, 611, 612 (Ch. 120 613A (Ch. 120085A 6614, B, BC, C (Ch.
E/L (ELECTRONIC LABS.)	 611, 612 (Ch. 120 613A (Ch. 120085A
75 (Sub-Station)	•614, B, BC, C (Ch. C)
Z0 20 6 76E, K, M, W (See Model 2701- Set 4-28) Set 4-28 76EU ("Rodio-Utilphone") 20 700 70B, 710M, 710T, 710W, Orthosonic (Ch. 2875) 20 7 710PB, 710PC Orthosonic (Ch. 2875) 20 2887) 2887) 2887) 24 16	C) •614D (Ch. 120095-6 615 (Ch. 120001B). 616 (Ch. 120100A, •619 (Ch. 120092D) •619 (Ch. 120092D)
sonic (Ch. 2875)	020 (Ch. 1200910-
2660 "Master Utiliphone". 8-8	 621 (Ch. 120098B) 622 (Ch. 120098P) 623 (Ch. 120101A)
2701 4-28 3000 Orthosonic 31-10	622 (Ch. 120098) 623 (Ch. 120098P) 623 (Ch. 120101A, 624 (Ch. 12018B) 625 (Ch. 120105B) 626 (Ch. 12010
EMERSON 501, 502 (Ch. 120000, 120029)	
503 (Ch. 120000, 120029) 1-18	 627 (Ch. 1201078). 628 (Ch. 1200988). 629 (Ch. 1201148)
505 (Ch 120002) 89	Set 93A-6) •629B, 629C (Ch. 1)
	 629D (Ch. 1201248) 630 (Ch. 1200998. 631 (Ch. 120109)
507 8–10 508 (Ch. 120008) 7–12 509 8–10	•632 (Ch. 120109). •633 (Ch. 120096B) •633 (Ch. 120114).
510, 510A (Ch. 120000, 120029)	634B (Ch. 120097B 635 (Ch. 120108). 636A (Ch. 120106A
511 8-10 511 (Ch. 120010) (See Model 541	•637, 8, 8C, C (Ch.
511 (Ch. 120010) (See Model 541 Set 16-23) 9-12 512 (Ch. 120006) 9-12 512 (Ch. 120056) 26-11 514 (Ch. 120007) 27-8	●637A (Ch. 120095-1 ●638 (Ch. 1200870
\$12 (Ch. 120056) 26-11 \$14 (Ch. 120007) 27-8 \$15, 516 12-11	●639 (Ch. 120103B)
515, 516	9Set 114-1) 640 (Ch. 120112) 641B (Ch. 120125B 642 (Ch. 120117A 643A (Ch. 120117A 6444, B, BC, C, (Ch.
519 (Ch. 120030) 30-7	642 (Ch. 120117A 643A (Ch. 120111A
520 [Ch. 120000, 120029] 2—1 521 (Ch. 120013, 120031) 7–13 522 8–10	645 (Ch. 120115).
523	646A (Ch. 120121A 646B (Ch. 120121B
525	● 644, B, BC, C, (Ch. C) 645 (Ch. 120115). 646A (Ch. 120121A 646B (Ch. 120121B ● 647, B, BC, C (Ch. C) 648B (Ch. 120134)
529, 529-9 (Ch. 120028) 18-15 530 (Ch. 120006, Ch. 120056) 32-6	PCB 48-Set 18
330 (ch. 12000s, ch. 1200s) 326 326 531, 532, 533. 116 534 (ch. 120007). 278 209 536 (ch. 120036). 21-14 24-17 537 237 537 237 537 237 537 237 537 237 537 237 537 237 537 237	•649A (Ch. 120094A •650 (Ch. 120113C)
5359 536 (Ch. 120036) 21–14 5364 24–17	●650 (Ch. 120118B) ●650B (Ch. 120118
537 23-7 538 (Ch. 120051) (See Model 549 Set 26-12) 539 9-13	650-Set 113-2) •650D (Ch. 120123-E
	48-50F (Ch. 120138-B 650F (Ch. 120138-B 651B (Ch. 120120).
541	 651C (Ch. 120109). 651C (Ch. 120124)
539 -9-13 540A (Ch. 120042) 20-10 541 16-13 542 (See Model 521-Set 7-13) 543 544 (Ch. 120046) 19-30 545 (Ch. 120047) Pl-15 547 (Ch. 120047) Pl-35 546 (Ch. 120047) 21-15 547 (Ch. 120050) 25-13 548 (Ch. 120051) 20-12 550 (Ch. 120050) 26-11 550 (Ch. 120050) 26-11 5514 120006) (See Model 512 -561 9-12 556 557 550 (Ch. 120050) 26-11 5514 120006) (See Model 512 552 20-28 553 553 (Ch. 120058) 31-11 5540 (Ch. 120058) 31-12 560 (Ch. 1200638) 73-4 561 (Ch. 1200638) 73-4 564 (Ch. 1200638) 73-4 564 (Ch. 12000	6618-3et 137.4 6649A (Ch. 120014A 650 (Ch. 120113C) -3et 97.4] 650 (Ch. 120113C) 650 (Ch. 120113C) 650 (Ch. 120113C) 650 (Ch. 120113C) 650 (Ch. 120113C) 650 (Ch. 12012A) 651 (Ch. 12012A) 651 (Ch. 12012A) 653 (Ch. 12012A) 653 (Ch. 12012A) 653 (Ch. 12012A) 653 (Ch. 12013B) 653 (Ch. 12013B) 654 (Ch. 120118B) 654 (Ch. 120118B) 654 (Ch. 120118B) 655 (Ch. 12013A) 655 (Ch. 12013A) 656 (Ch. 12013A) 657 (Ch. 12013A) 656 (Ch. 12013A) 657 (Ch. 12013A) 656 (Ch. 12013A) 657 (Ch. 12013A) 656 (Ch. 12013A) 657 (Ch. 12013A) 657 (Ch. 12013A) 656 (Ch. 12013A) 657 (Ch. 12013A) 657 (Ch. 12013A) 656 (Ch. 12013A) 656 (Ch. 12013A) 657 (Ch.
cer 82 546 (Ch. 120049)	653B (Ch. 120136-B 654 (Ch. 120118B)
548 (Ch. 120051)	•654B {Ch. 120118 654—Set 113-2)
550 (Ch. 120006) (See Model 512 Set 9-12)	48-Set 182-1) . 654F (Ch. 1201238
551A	 655B (Ch. 120123- 655D (Ch. 120123
553A	650D-Set 109-3 655F (Ch. 120138-8 655F (Ch. 120138-8
557B ICh. 1200488)	●658B (Ch. 120124. ●658C (Ch. 120124.
560 (Ch. 120016)	629D—Set 116- 660B (Ch. 120133B
563 (Ch. 120063B)73-4 564 (Ch. 120027) (See Model 540A	e6618 (Ch. 120134) see PCB 48—Set
	18-Set 130-1) . •663B (Ch. 120128-E
Set 26-12) 567 (Ch. 120016) (See Model 560	18-Set 130-1) . • 664B (Ch. 120133-B • 665B (Ch. 1201215
567 [Ch. 120042] (See Model 540A —Set 20-10)	120130-B) •6666B (Ch. 120135
568A (Ch. 120070A) 58-9 549A (Ch. 120062A)	•6668 (Ch. 120135 Radio Ch. 120132 27—Set 148-1) •6678, 6688 (Ch. 1 (Also see PCB
	(Also see PCB
572 (Ch. 120065) (See Model 540A Set 20-10)	• 6698 (Ch. 120129) PCB 24-Set 142
573B (Ch. 120039B)	—Set 181-1) 671B (Ch. 120137- 671D (Ch. 120137 671B—Set 118-6
575 (Ch. 120068A, 120068B) 85-6	6718-Set 118-6

EDWARDS	EMERSON-Cont.
Fidelotuner	577B (Ch. 120012B) 416 •57B (Ch. 120050) (See Model 547A Set 25-13)
(Also see Recorder Listing)	
15 135 6	580 (Ch. 120064) 97-3 581 (Ch. 120014A, B) 68-7
EKOTAPE (See Recorder Listing)	
ELCAR	584 (See Model 558-Set 31-11) ●585 (Ch. 1200258) 61-7
602 5–19	585 (Ch. 1200258) 61-7 586 (Ch. 1200258) 1200838) 72-9 587 (Ch. 120033A, B) 71-10 588 (See Model 547A−Set 25-13) 500 (Ch. 1201014 B) 87-5
ELECTONE T5T53 12–34	588 (See Model 547A—Set 25-13) 590 (Ch. 120101A, B) 87—5
ELECTRO	500 (See Model 34/A-Set 23-13) 590 (Ch. 120101A, B) 87-5 591 (Ch. 120055A) 67-9 593 (Ch. 120063B) 73-4
B-20 14—9	594, 595 (Ch. 120071A) 68-7 596
ELECTROMATIC	597 (Ch. 120073B3 90-5 599 (Ch. 120075B) 69-8
APH301-A, APH301-C 7-11 606A, 607A 5-32	•600 (Ch. 120103-B) (Also see PCB 9Set 114-1)
ELECTRO-TONE	394, 595 (ch. 1200714). 68-7 596 61-6 597 (ch. 12007383. 90-5 599 (ch. 1200758). 69-8 600 (ch. 120103-8) (Also tee PCB 95e T14-1) 87-6 601 (ch. 1200758). 69-8 602 (ch. 120072A, 120022A 55-10
555 13-17 706, 712 (See Model 555-Set 13-	603 (Ch. 1200638)
16)	604A (See Model 576A-Set 40.5) 605 (Ch. 120076B)
ELECTRO-VOICE 3300 Tel. UHF Conv	● 606 (Ch. 120066) 46-25 ● 606 (Ch. 120066B)
ELECTRONIC CORP. OF	●606 (Ch. 120086B-D) 76-11 ●606 (Ch. 120086B)
AMERICA (See ECA)	607 (Ch. 120074A) 90-5 608A (Ch. 1200898)
ELECTRONIC SPECIALTY CO. (See Ranger)	●609 (Ch. 120084-B)
	• 611, 612 (Ch. 1200878-D) 76-11 6134 (Ch. 1200854, 8), 79-7
E/L (ELECTRONIC LABS.) 75 (Sub-Station)	602 (Ch. 120072A, 120082A
76E, K, M, W (See Model 2701	•614D (Ch. 120095-B)
76RU [''Radio-Utilphone''] 20-6 710B, 710M, 710T, 710W, Ortho- sonic (Ch. 2875)	616 (Ch. 120100A, B)71-10 •619 (Ch. 120092D) 76-11
ponta fore ormosome fem	●620 (Ch. 120091D-QD) 76-11 ●621 (Ch. 1200988) 108-5
2000 musier officie . 0-0	•622 (Ch. 120098P)
2701 4–28 3000 Orthosonic 31–10	●624 (Ch. 1200878-D) 76-11 625 (Ch. 1201058) 103-8
EMERSON	••••••••••••••••••••••••••••••••••••
501, 502 (Ch. 120000, 120029) 503 (Ch. 120000, 120029) 504 (Ch. 120000, 120029) 505 (Ch. 120000, 120029) 505 (Ch. 120001) 505 (Ch. 120012) 505 (Ch. 12	84-6 627 (Ch. 1201078). 76-11 628 (Ch. 1200988). 108-5 629 (Ch. 1201148) (See Model 631 -Set 93A-6) 6298 629C (Ch. 120120) 119-6
503 (Ch. 120000, 120029) 1–18 504 (Ch. 120000, 120029) 2–1	●629 [Ch. 120114B] (See Model 631 —Set 93A-6)
505 (Ch. 120002)	●629B, 629C (Ch. 120120).119—6 ●629D (Ch. 120124B)
506	•630 (Ch. 1200998
508 (Ch. 120008)	•632 (Ch. 1200968)93A-7 •633 (Ch. 120114) 93A-6
509 8 -10 510, 510A (Ch. 120000, 120029)	634B (Ch. 120097B). 111-4 635 (Ch. 120108) 92-1
5-36 511	
	C) 97-4 •637A (Ch. 120095-8) 95A-3 •638 (Ch. 120087D) (See Model
512 (Ch. 120006) 9-12 512 (Ch. 120056) 26-11 514 (Ch. 120007) 27-8	●638 (Ch. 120087D) (See Model 571-Set 76-11)
514 [Ch. 120007]	5/1-5ef /0-11] 6d39 (Ch. 120103B) (Also see PCB 9-5et 114-1)
11 12-11 515, 516 12-11 515, 516 (Ch. 120056) 26-11 517 (Ch. 120010) (See Model 541 —Set 16-13)	640 (Ch. 120112)93-5 6418 (Ch. 1201258)120-5
518 8-10	642 (Ch. 120117A) 98—3 643A (Ch. 120111A) 91—4
519 (Ch. 120030)	
522	C) 97-4 645 (Ch. 120115)
524 17-12	6468 (Ch. 1201218)102—6 ●647, B, BC, C (Ch. 120113, B, BC,
525 20—8 528 (Ch. 120038) 21–13 529, 529-9 (Ch. 120028) 18–15 530 (Ch. 120006, Ch. 120056) 120056)	C) 97-4 •648B (Ch. 120134B, G, H) (See PCB 48-Set 182-1 and Model 661B-Set 137-4)
530 (Ch. 120006, Ch. 120056) 32-6	PCB 48—Set 182-1 and Model 6618—Set 137-4)
531, 532, 533 11-6	•649A (Ch. 120094A)106-7 •650 (Ch. 120113C) (See Model 614
535 20-9 536 (Ch. 120036) 21-14	Set 97.4) •650 (Ch. 120118B)113-2
536A	●650 (Ch. 1201188)113—2 ●6508 (Ch. 1201188) (See Model 650—Set 113-2)
534 (Ch. 120007) 27-8 535 20-9 536 536A 24-17 537 23-7 538 (Ch. 120051) 539 9-13	48-Set 182-1) 109-3
540A (Ch. 120042) 20-10	•651B (Ch. 120120)
541	●651C (Ch. 120124)
543, 544 (Ch. 120046) 19-30 545 (Ch. 120047) Photofact Servi-	652 (Ch. 1200328)
5.45 (Lh. 12004) Phototect Servi- cer 82 5.46 (Ch. 120050) 21-15 5.47 A (Ch. 120050) 25-13 5.48 (Ch. 120051) 30-8 5.49 (Ch. 120051) 26-12 5.50 (Ch. 120006) (See Model 512 -55 -55 (51, 20006) (See Model 512 -55	650-5e1 113.2) 6500 [Ch. 120123.8] (Alto see PCB 40-5e1 [82-1] 109-3 6097 [Ch. 12013.8], [133.1A 6518 [Ch. 120120], [119-6 6515 [Ch. 12013.8], [133.1A 6516 [Ch. 120109], [146-5 6515 [Ch. 120124, 8], [145-5 6510 [Ch. 120124, 8], [145-5 652 [Ch. 1200124, 8], [159-5 653 [Ch. 12000808], 98-3 6538 [Ch. 12001388], [159-5 6544 [Ch. 12011388], [159-5 6544 [Ch. 12011388], [65e Model 654-5et [113.2] 6540 [Ch. 1201288], [Also see PCB
547 A (Ch. 120050) 25–13 548 (Ch. 120051) 30–8	654B (Ch. 120118B) (See Model 654—Set 113.2)
549 (Ch. 120051)	•654D (Ch. 120123B) (Also see PCB
330 (Cit. 120030)	634-5et 113-21 6354 (b. 1201238) (Also see PCB 43-5et 182-1) 109-3 6354 (b. 120138) 133-1A 63558 (b. 120138) 109-3 6350 (b. 120123.8) (See Model 6300-5et 109-3) 6357 (b. 120124 (See Model 6358 (b. 120124 (See Model 6290-5et 116-5)
531 A 24-17 551 A 20-8 553 A 20-8 553 A 24-17 554 A 20-8 553 A 24-17 554 Ch. 120018B. 70-4 557 B 1Ch. 120048B. 31-11 559 A (Ch. 120048B. 31-12 560 (Ch. 120018). 31-12 560 (Ch. 120018). 63-27 561 (Ch. 120018). 63-27-14 564 (Ch. 120027) (5ec Model 540A -5et 20-101 565 (Ch. 120018). 565 (Ch. 120028). 70-4	655D (Ch. 120123B) (See Model 650D—Set 109-3)
556, 557 (Ch. 120018B) 70-4	•655F (Ch. 120138-8)
558 (Ch. 120058)	●6588 (Ch. 120124, B) 116-5 ●658C (Ch. 120124) (See Model
560 (Ch. 120016)	●658C (Ch. 120124) (See Model 629D—Set 116-5) ●660B (Ch. 120133B)131—6
563 (Ch. 120063B)	220—Set 116.5) 6008 (ch. 120133B)131—6 6608 (ch. 120134B, c, H) (Also see PCB 48—Set 182.1), 137—4 6628 (ch. 120127.8) (Also see PCB 18—Set 130.1)125—6 6638 (ch. 120128.6) (Also see PCB 18—Set 130.1)125—6 6648 (ch. 120133.8)131—6 6658 (ch. 120133.8)131—6
-Set 20-10)	● 662B (Ch. 120127-B) (Also see PCB 18—Set 130-1) 125—6
	663B (Ch. 120128-B) (Also see PCB 18-Set 130-1) 125-6
567 (Ch. 120016) (See Model 560	●664B (Ch. 120133-B)
567 (Ch. 120042) (See Model 540A	6020 (200.8) 6 do 8 (Ch. 1201358, Ch. 4, and Radio Ch. 1201328 (Aiso ter 26 72—Set 148-1) 6678, 6688 (Ch. 1201348, C, H) (Aiso see PCB 48—Set 182-11 137—4
568A (Ch. 120070A) 58-9	Radio Ch. 120132B) (Also see PCB 27-Set 148-1) 133-5
570 (Ch. 120064)	667B, 668B (Ch. 120134B, G, H) (Also see PCB 48—Set 182-11
Set 25-14) 567 [Ch. 120042] (See Model 540A -584 [Ch. 1200704]. 5889 568A [Ch. 1200704]. 589 576 [Ch. 120064]. 973 5771 [Ch. 120066] 761 572 [Ch. 120065] 761 572 [Ch. 120065] 761 573 [Ch. 120039]. 4211	● 669B (Ch. 120129B. D) (Also see
	137-4 6698 (Ch. 1201296) (Alto see PCB 24-Set 142-1 and PCD 47 Set 181-1], 126-5 6718 (Ch. 120137-81, 118-6 6710 (Ch. 1201370) (See Model 6718-Set 118.6)
574 (Ch. 120064)	6718 (Ch. 120137-8)118-6 6710 (Ch. 120137D) (See Model
85-6 576A (Ch. 120069A)40-5	6718—Set 118-6) 6728 (Ch. 1200978)1317

EMERSON-Cont. 126-5) 6 9780 (Ch. 1201278) [See PCB 18-Set 130-1 and Model 662B—Set 125-6) 6 9790 (Ch. 120140-8)... 165-1A 7 008 (Ch. 120153-8)... 169--6 7 000 (Ch. 120153-8)... 164--9 7 010 (Ch. 120153-8)... 164--9 7 010 (Ch. 120153-8)... 164--9 7 017 (Ch. 120153-8)... 164--9 7 028 (Ch. 120153-8)... 164--9 7 028 (Ch. 120153-8)... 159--5 7 028 (Ch. 120153-8)... 184--6 7 053.8 (Ch. 120153-8). 184--6 7 056.7 078 (Ch. 120153-8). 178--5 7 088 (Ch. 120153-8). 184--6 7 056.7 078 (Ch. 120153-8). 178--5 7 088 (Ch. 120163-8). 178--5 7 088 (Ch. 120163-8). 183--6 7 105 (Ch. 120163-8). 183--6 7 118 (Ch. 120164-8). 183--6 7 127 (Ch. 120164-8). 183--6 7 128 (Ch. 120153-8). 056-4 7 128 (Ch. 120153-8). 056-4 7 128 (Ch. 120153-8). 056-4 7 127 (Ch. 120164-8). 183--6 7 126 (Ch. 120153-8). 056-4 7 127 (Ch. 120163-0)... 190--2 7 167 (Ch. 120163-0)... 190--2 7 167 (Ch. 120163-0)... 190--2 7 177 (Ch. 120163-0)... 190--2 7 179 (Ch. 120163-0)... 190--2 7 170 (Ch. 120163-0)... 190-2

.131-7 •740D (Ch. 120173-D) (See PCB 65

EMERSON-Cont.

- Set 202-1, PCB 77—Set 218-1 and Model 7100—Set 197-5)
 Y41D (Ch. 12018-0) (See PCB 61 Set 195-1, PCB 71—Set 211-1 and Model 7100—Set 190-2)
 Y41F (Ch. 120182-0) (Also See PCB 103—Set 249-11 235—S 7428 (Ch. 120171-8) (See Model 7368)
 Y428 (Ch. 120171-8) (See PCB 65 —Set 202-1, PCB 77—Set 218-1 and Model 710D—Set 197-3)
 Y448 (Ch. 120173-8) (Z2B—9 747 (Ch. 120175-8) 221—6 7468 (Ch. 120175-8) 221—6 7468 (Ch. 120175-8) 221—6 7468 (Ch. 120175-8) 223—6 7468 (Ch. 120176-8) 223—6 7468 (Ch. 120176-8) 223—6 7550 (Ch. 120166-D) (See PCB 65 —Set 202-1, PCB 77—Set 218-1 and Model 71D—Set 197-5) 9750 (Ch. 120166-D) (See PCB 65 —Set 195-1, PCB 77—Set 218-1 and Model 7105—Set 197-5) 9750 (Ch. 120166-D) (See PCB 65 —Set 195-1, PCB 77—Set 218-1 and Model 7105—Set 197-5) 9750 (Ch. 120168-D) (See Model 754, 8 (Ch. 120174-8), 243—4 7345 (Ch. 120174-8), 243—4 7346 (Ch. 120194-D) (See PCB 103 —Set 195-1, PCB 71—Set 211-1, PCB 86—Set 227-1 and Model 7160—Set 190-2) 7577 (Ch. 120182-D) (See PCB 103 —Set 249-1 and Model 785K— Set 235-5) 7577 (Ch. 120194-D) (See PCB 103 —Set 249-1 and Model 785K— Set 235-5) 7500 (Ch. 120194-D) (See PCB 103 —Set 249-1 and Model 785K— Set 235-5) 7500 (Ch. 120194-D) (See PCB 103 —Set 249-1 and Model 785K— Set 235-5) 7500 (Ch. 120173-D) (See Model 7160—Set 190-2) 7534 (Ch. 120173-D) (See Model 7160—Set 190-2) 7536 (Ch. 120173-D) (See PCB 103 —Set 249-1 and Model 785K— Set 235-5) 7500 (Ch. 120173-D) (See Model 7160—Set 190-2) 7500 (Ch. 120173-D) (See Model 7160—Set 190-2) 7500 (Ch. 120173-D) (See Model 7160—Set 190-2) 7764 (Ch. 120173-D) (See Model 7160—Set 190-2) 7764 (Ch. 120173-D) (See Model 7764 (Ch. 1201

●795C (Ch.	120192-B)	243-4
@796C (Ch.	120203-B)	. 263-7
@7978 (Ch.	120204-B)	.263-7
0797C [Ch.	120205-BL	263_7
•798B (Ch.	120205-B)	. 263-7

NOTE: PCB Denotes Production Change Bulletin, Production Change Bulletin, Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

EMERSON-Cont. @799E (Ch. 120209-F)....243—4 801 (Ch. 120154-B) (See Model 704 —Set 184-6) 8058 (Ch. 1202020)....260—7 @1000C (Ch. 120206-0) (See PCB 103—Set 249-1 and Model 741F —235-5) @1001G (Ch. 120208-0) (See PCB 103—Set 249-1 and Model 741F —Set 235-5) @1001G (Ch. 120208-0) (See PCB 1032-51 249-1 and Model 741F —Set 235-5) @1001G (Ch. 120206-0) (See PCB 1032-51 249-1 and Model 741F Set 235-5) @1002C (Ch. 120206-0) (See Model 1032-51 249-1 and Model 741F Set 235-5) @1002C (Ch. 120206-0) (See Model 1032-51 249-1 and Model 741F Set 235-5) @1002C (Ch. 120206-0) (See Model 1032-51 249-1 and Model 741F Set 235-5) @1002C (Ch. 120206-0) (See Model 1033-51 249-1 and Model 741F Set 235-5) @1002C (Ch. 120206-0) (See Model 1033-51 249-1 and Model 741F Set 235-5) @1002C (Ch. 120206-0) (See Model 915) @1002C (EMERSON_Cont. EMERSON-Cont. Set 235-3) 1002D (Ch. 120206-D) (See Model 781E) 1003 (See Model 1002—Set 16-14 1003E (Ch. 120208-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5) 1003G (Ch. 120208-D) (See Model 1001E) 103—Set 249-1 and Model 741F —Set 235-5) 1004C (Ch. 120208-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5) 1003=Et 249-1 and Model 741F —Set 235-5) 1003=Et 249-1 and Model 741F —Set 235-5) 1003=Ch. 120208-D) (See Model 103=Set 249-1 and Model 741F —Set 235-5) 1003F (Ch. 120208-D) (See Model 1003F (Ch. 120208-D) (See Model 1005F (Ch. 120208-1001E) 1005E (Ch. 120211-F) (See Model 703E) 1003—Set 249-1 and Model 741F —Set 235-5] 1007E (Ch. 120206-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5] 1007G (Ch. 120211-F) (See Model 703E) 1008E (Ch. 120206-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5] 1009E (Ch. 120211-F) (See Model 703E) 1009E (Ch. 120211-F) (See Model 703E) 1009C (Ch. 120211-F) (See Model 703E) 1000C (Ch. 120211-F) (See Model 703E) 1010C (Ch. 120206-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5] 1011C (Ch. 120206-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5] 1011C (Ch. 120206-D) (See PCB 103—Set 249-1 and Model 741F —Set 235-5] 1011C (Ch. 120211-F) (See Model 703E) 1035 (Ch. 120211-D) (see Model 784M) 1024C (Ch. 120206-D) (see Model 7816) 1025E (Ch. 120211-D) (see Model 784M) 784M] 1026C (Ch. 120206-D) (See Model 781E) 1027E (Ch. 120211-D) (See Model 104471 1027E (Ch. 120206-D) (See Model 7848) 1027E (Ch. 120211-D) (See Model 7848) 1028C (Ch. 120206-D) (See Model 7848) 1029E (Ch. 120206-D) (See Model 7848) 1040F (Ch. 120206-D) (See Model 545) Ch. 1200258 (See Model 545) Ch. 120047 (See Model 545) Ch. 120046 (See Model 5471) Ch. 120066 (See Model 5711) Ch. 120088 (See Model 5711) Ch. 1200878-D (See Model 6411) Ch. 1200974. (See Model 6420) Ch. 1200924 (See Model 6420) Ch. 1200928 (See Model 6420) Ch. 1201048 (See Model 6420) Ch. 1201048 (See Model 6421) Ch. 1201048 (See Model 6423) Ch. 1201048 (See Model 6428) Ch. 1201078 (See Model 6483) Ch. 120110, B, BC, C (See Model 648) Ch. 120113, B, BC, C (See Model 648) Ch. 120113, B, SC, C (See Model 648) Ch. 120124 (See Model 6433) Ch. 120124 (See Model 648) Ch. 12

Ch. 120135B, G, H (See Model 666B)

Ch.	120136-B (See Model 653B) 120138-B (See Model 653B) 120138-B (See Model 650F)	
Ch. Ch. Ch. Ch. Ch.	1201408 (See Model 6766)	
Ch. Ch. Ch.	6D) 120147-B (Se Model 790B) 120147-B (See Model 725A)	
Ch	120150-B (See Model 718B)	
Ch.	20152-8 (See Model 7310)	
Ch. Ch.	120152-F (See Model 733F) 120153-B (See Model 700B) 120154-B (See Model 704) 120155A, B (See Model 705A,	
81		
Ch.		
Ch. Ch. Ch.	120164-B (See Model 711E) 120166-D (See Model 721D)	
Cn.		
Ch. Ch. Ch. Ch. Ch.	120169-D (See Model 720F) 120169F (See Model 733F) 120170-B (See Model 729B) 120171-B (See Model 736B) 120172A, B (See Model 737A,	
	120173-D (See Model 740D)	
Ch. Ch. Ch. Ch. Ch.	120173-D (See Model 740D) 120174-B (See Model 752A) 120175-B (See Model 744B) 120176-B (See Model 745B) 120177-B (See Model 746B)	
Ch. Ch.	120177-B (See Model 7466)	
Ch.	20180-D (See Model 753D)	
Ch. Ch. Ch.	120182-D (See Model 741F) 120184-B (See Model 775A) 120185-B (See Model 732G) 120190-D (See Model 760H)	
Ch. Ch.	120191-D (See Model 760D)	
Ch. Ch. Ch.	120192-B (See Model 767A) 120192-D (See Model 771D) 120192-F (See Model 775A)	ľ
C C C C C C C C C C C C C C C C C C C	120192-D (See Model 771D) 120192-F (See Model 775A) 120193-B (See Model 768A) 120193-F (See Model 768A) 120193-F (See Model 766A)	
Ch. Ch.	120195-D (See Model 785K)	
Ch. Ch.	120197-D (See Model 784C)	
Ch. Ch.		
Ch. Ch.	120200-B (See Model 7838) 120201-B (See Model 7888) 120202-D (See Model 8058)	
0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	120202-D (See Model 805B) 120203-B (See Model 748C) 120204-B (See Model 777B) 120205-B (See Model 797C)	
	120200-D (See Model 781E)	
Ch.	120208-D (See Model 1001E)	
Ch. Ch.	120209-F [See Model 799E] 120210-D (See Model 766D)	1
Ch.	120211-D (See Model 784M)	
	120211-D (See Model 784M) 120211-F (See Model 793E)	
EMP	120211-D (See Model 784M) 120211-F (See Model 793E) RESS 56	
EMP 55, ESPI	RESS 56	
EMP 55, ESPI RR13 7B . 7C .	RESS 56 7–14 EY (Also see Philharmonic) 1, RR131 13–17 47–8 153–4	
EMP 55, ESPI RR13 78 - 7C - 188 31 -	RE55 56	
EMP 55, ESPI RR13 78 - 7C - 188 31 - 100 101	RESS 7-14 (Y (Also see Philharmonic) 1, RR131 13-17 47-8 153-4 103-9 236-4	
EMP 55, ESPI RR13 78 . 7C . 188 31 . 100 101 200 300 400	RE55 56	
EMP 55, ESPI RR13 76. 77. 188 31. 100 101 200 300 101 200 300 5112 5128	RE55 56	
EMP 55, ESPI RR13 76 - 77 - 188 31 - 100 101 200 300 101 200 300 5112 5128 5138	RE55 56 7-14 EY (Also see Philharmonic) , RR131 13-17 47-8 153-4 90-7 103-9 236-4 241-7 247-4 500 245-3 174-6 68-8 182-4 514 63-8	
EMPP 55, ESPI RR13 76. 188 31. 100 101 200 300 400, 5112 5128 512 5128 513, 524 581	RESS 56	
EMP 55, ESPI RR13 76 . 77C . 188 31 . 100 100 100 100 200 400, 5112 513, 512 513, 524 581 621 641, 651, 652, 9.	RESS 56	
EMP 55, ESPI RR13 76 . 77C . 188 31 . 100 100 100 100 200 400, 5112 513, 512 513, 524 581 621 641, 651, 652, 9.	RESS 56	
EMP 55, ESPI RR13 76 . 77C . 188 31 . 100 100 100 100 200 400, 5112 513, 512 513, 524 581 621 641, 651, 652, 9.	RESS 56	
EMP 55, ESPI RR13 76 . 77C . 188 31 . 100 100 100 100 200 400, 5112 513, 512 513, 524 581 621 641, 651, 652, 9.	RESS 56	
EMPP 55, ESPI Rel 3 76.3 76.3 188 31.3 100 100 100 100 100 100 100 10	RESS 56 7-14 56 7-14 13-17 47-8 13-4 13-4 13-4 13-4 13-4 13-4 13-7 13-4 13-4 13-7 13-7 13-4 13-4 13-7 24-8 500 245-3 247-4 247-4 500 245-3 182-4 514 514 50-7 182-4 514 533 (See Model 651-5e 9-14 563 653 (See Model 651-5e 22, -5, 6514, 6516, 6517. 23, -5, 6514, 6516, 6517. 20, -2, 6521, 6533 (Ch. FJ971) 6541 8-12 9-14 651- 651-5e 51-16 (Ch. FJ97) (See Model 651- 9-14 51-16 (Ch. FJ97) (See Model 651- 9-14 5-16 (Ch. FJ97) (See Model 651- 9-14 5-16 (Ch. FJ97) (See Model 651-	
EMP 55, FSP13 76 76 76 81 81 81 81 81 90 90 90 90 90 90 90 90 90 90 90 90 90	RESS 56 7-14 56 7-14 13-17 14 13-17 47-8 153-4 153-4 103-9 236-4 236-4 247-4 247-4 242-6 500 245-3 500 245-3 1174-6 68-8 514 63-8 514 63-8 514 63-8 182-4 514 514 63-8 182-4 514 500 245-3 642 8-11 653 (See Model 651-Set 14) 653 (See Model 551-Set 14) 7 -2, -5, 6514, 6516, 6517, 58-14) 653 (See Model 651-Set 914) 7 -41 8-12 (Ch. FJ97) (See Model 651-97) 9<-14)	
EMP 55, ESPI 76, 77, 18, 31, 31, 31, 31, 31, 31, 31, 31, 31, 31	RESS 56 7–14 FY (Also see Philharmonic) 1, RR131 13–17 47–8 133–4 900-7 133–9 234–4 244–4 500 244–6 244–4 500 244–6 174–6 69–8 174–6 69–8 514 66–8 90–7 14–10 163–1 642 8–11 9–14–10 163–1 642 8–11 9–14–10 163–15 183–14 053 (See Model 651–Set 91–4 9–14 90–7 14–10 163–15 183–14 053 (See Model 651–Set 9–14 9–14 10–17 10–17 5–16 (Ch. FJ97) (See Model 651– 9–12 (Ch. FJ97) (See Model 651–	
EMP 55, ESPI3 76, 776, 776, 776, 776, 776, 776, 776,	RESS 56 7-14 56 13-17 43-8 13-17 45-8 13-4 13-4 13-4 13-4 13-4 13-7 43-8 13-4 13-4 13-7 13-7 13-4 13-4 13-7 247-8 247-4 247-4 500 245-3 500 245-3 182-4 63-8 514 60-7 10-17 642 643 8-11 653 (See Model 651-Set 14) 90-7 -2, -5, 6514, 6516, 6517 50, -2, 6521, 6533 (Ch. FJ97) 653 (See Model 651-Set 14) 90-7 -2, -5, 6514, 6516, 6517 (Ch. FJ97) Se-16 (Ch. FJ97)	
EMP 55, ESPI3 76 77 76 77 75 18 18 18 18 18 10 10 10 10 10 10 10 10 10 10 10 10 10	RESS 56 7-14 56 7-14 1410 13-17 47-8 13-7 47-8 13-7 13-9 7 13-7 10-7 13-7 10-7 103-7 10-7 236-1 241-7 247-4 242-6 500 245-3 500 245-3 182-4 514 514 50-7 182-4 514 514 518-1 633 (551-5et 141 90-7 -2, -5, 6514, 6516, 65175et 141 8-12 (Ch. F197) 5-16 (Ch. F197) 5-16 <td></td>	
EMP 55, FSPI 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C,	RESS 56 7-14 56 7-14 LY (Also see Philharmonic) 13-17 1, RR131 13-17 153-4 153-4 153-4 153-4 153-4 153-4 163-4 153-4 200-7 103-9 236-4 2417 247-4 242-6 500 245-3 500 245-3 514 63-8 182-4 514 514 63-8 182-4 514 514 63-8 642 8-11 90-7 14-10 653 (See Model 651-Set 914) 90-7 161 651-2 914 651 95-14 8-12 (Ch. FJ97) (See Model 651-3 914 8-12 (Ch. FJ97) (See Model 651-3 914 8-12 (Ch. FJ97) (See Model 651-9 914 8-12 (Ch. FJ97) (See Model 651-9	
EMP 55, FSPI 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C,	RESS 56 7-14 56 7-14 Y (Also see Philharmonic) 13-17 47-8 103-9 103-9 20-7 236-4 241-7 247-4 247-4 242-6 500 500 245-3 500 245-3 514 63-8 514 63-8 514 63-8 514 63-8 514 63-8 642 8-11 90-7 14-10 653 (See Model 651-Set 90-17 -2 7-2, -5, 6514, 6516, 6517Set 90-17 14) 90-7 90-17 5-16 (Ch. FJ97) (See Model 651 9-14) 8-12 6512 6613, 6614, 6615 9-14 8-12 (Ch. FJ97) (See Model 651 9-14) 90-7 914) 90-7 914) 90-7 914 90-7 <tr< td=""><td></td></tr<>	
EMP 55, FSPI 76 - 77 - 76 - 77 - 76 - 77 - 77 - 70 - 70 - 70 - 70 - 70 - 70	RESS 56 7-14 56 7-14 Y (Also see Philharmonic) 1, RR131 13-17 478 153-4 90-7 103-9 236-4 247 247-4 242-6 500 245-3 500 245-3 500 245-3 514 63-8 514 63-8 514 63-8 514 63-8 514 63-8 642 8-11 643 64-7 90-7 -7 -2, -5, 6514, 6516, 6517, -9 90-7 -14-10 653<(See Model 651-Set 9-14)	
EMP 55, FSPI 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C,	RESS 56 7-14 Standard 13-17 $47-8$ 13-7 $47-8$ 13-6 $13-9$ 7-8 $13-9$ 7-9 $13-7$ 13-7 $13-7$ 13-7 $13-7$ 13-7 $13-9$ 90-7 $236-4$ 247-4 $247-4$ 247-4 $247-4$ 247-4 500 245-3 500 245-3 $612-667-866-866$ 182-4 514 63-8 $62-45-866-866-867-970-7$ 14-10 653 (56-567-564) 642 8-11 653 (56-567-564) $651-970$ 5-16 (Ch. FJ97) (5ce Model 651-9-9-14) 6512 (561-9-14) $9-14$ 8-12 (Ch. FJ97) (5ce Model 651-9-9-14) $9-14$ 8-12 $(Ch. FJ97)$ (5ce Model 651-9-9-14) $9-14$ 90-7 UIRE 90-7 18-16	
EMP 55, 75, 76, 76, 76, 76, 76, 76, 76, 76, 76, 76	RESS 56 7-14 56 7-14 Y (Also see Philharmonic) , R131 13-17 478 153-4 90-7 103-9 236-4 247-4 247-4 242-6 500 245-3 500 245-3 500 245-3 514 63-8 642 8-11 633 (See Model 651-6517, 0517, 0533 (Ch. F)97) 50. -2.3, 6514, 6516, 6517, 0514, 6516, 6517- 702, 6513, 651-6517, 6531- 9-14 6541 8-12 (Ch. F)97) 5-16 (Ch. F)97) 5-16 (Ch. F)97) 5-16 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7 9.14] 90-7	
EMP 55, FSP 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C,	RESS 56 7-14 56 7-14 Y (Also see Philharmonic) 1, R131 13-17 478 153-4 90-7 103-9 236-4 241-7 247-4 244-6 500 245-3 500 245-3 500 245-3 500 245-3 514 63-8 514 63-8 514 63-8 514 63-8 642 8-11 643 8-12 644 8-11 653 (See Model 651-Set 914) 653 (See Model 651-Set 914) 6512 6613 6615 9141 8-12 (Ch. FJ97) (See Model 651- 9141 8-12 (S12, 6613, 6614, 6615, 6635 97-14 8-12 (See Model 651- 90-7 9141 90-7 9142 8-12 (S12, 6613, 6614, 6615, 6635 97-3 18-16 <trr></trr>	
EMP 55, FSP 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C, 7C,	RESS 56 7-14 56 7-14 Y (Also see Philharmonic) 1, R131 13-17 478 153-4 90-7 103-9 236-4 241-7 247-4 244-6 500 245-3 500 245-3 500 245-3 500 245-3 514 63-8 514 63-8 514 63-8 514 63-8 642 8-11 643 8-12 644 8-11 653 (See Model 651-Set 914) 653 (See Model 651-Set 914) 6512 6613 6615 9141 8-12 (Ch. FJ97) (See Model 651- 9141 8-12 (S12, 6613, 6614, 6615, 6635 97-14 8-12 (See Model 651- 90-7 9141 90-7 9142 8-12 (S12, 6613, 6614, 6615, 6635 97-3 18-16 <trr></trr>	
EMP 55, 75, 76, 76, 76, 76, 76, 76, 76, 76, 76, 76	RESS 56 7-14 S6 7-14 Y (Also see Philharmonic) $R131$ 13-17 $47-8$ 153-4 $90-7$ 103-9 $236-4$ 90-7 $236-4$ 90-7 $247-4$ 247-4 500 245-3 500 245-3 500 245-3 514 $63-8$ 642 $8-12$ 653 (See Model 651-Ser 9-14) 653 (See Model 651-Ser 9-14) 6541 $8-12$ (Ch. FJ97) S-16 (See Model 651-Ser 9-14) $8-12$ (Ch. FJ97) S-16 (See Model 651-9-Ser 9-14) $90-7$ 9-14) $90-7$ 9-14) $90-7$ 9-14) $90-7$ <td></td>	
EMP 55, ESPI 76, 77, 77, 70, 70, 70, 70, 10, 10, 10, 10, 10, 10, 10, 10, 10, 1	RESS 56 7-14 56 13-17 1, RR131 13-17 103-0 90-7 236-4 2417 247-4 242-6 500 245-3 500 245-3 514 63-8 182-4 514 514 63-8 182-4 90-7 14-10 90-7 140 90-7 141 90-7 141 90-7 9-14 8-12 (Ch. FJ97) [See Model 651Set 14] 9-14 8-12 (Ch. FJ97) [See Model 6519 9-14 8-12 9-14 8-12 (Ch. FJ97) [See Model 6519 9-14 90-7 UIRE 0, 653.1, 663.2, 663.4, 663.5 0, 65	

•H421T (See Model UH21T — Set 228-10)	
H4211 (See Model UH211 Set 228-10) H442C	
P80 27—9 P82 21–16 P100 27–10	
P82 21-16 P100 27-10 P111 178-6 P130 135-7 87C15 87C25 871025 114-4 81050 114-4 854C20 142-8 854T15 142-8 854T15 142-8 854C20 142-8 854T30 142-8 854C55 134-7 956C50 134-7 957C20 \$7C30 957C70 134-7 957C50 134-7 957C50 134-7	
R7C15, R7C25 158—3 R-1025 114—4	
•R-1050 114-4 •S4C20 142-8	
• S4C40	
• S4T30 • S6C55 134-7	
• S6C70	
• S7C20, S7C30 (See Model S6C55- Set 134-7)	
Set 1347 S7C70 1347 S7C65 1347 S9C10 1347 S1015 1094 S1020 1094 S1030 1094 S1030 1094 S1030 1094 S10455, S1055X 1347 S1060 1347	
• \$9C10	
134.7) • \$1015 109-4	
• \$1020	
•\$1055, \$1055X	
• S1065	
•UDL2100T	
• U1700CD	
•2100C 228-10 •U2150C 228-10	
• V21T (See Model 215C—Set 200-5) • V21T6 (See Model 215C — Set	
200-5) •V211CD	
• \$1013 109-4 • \$1020 109-4 • \$1030 109-4 • \$1035, \$1035X 134-7 • \$1060 134-7 • \$1065 134-7 • \$1065 134-7 • \$1065 134-7 • \$1065 134-7 • \$1050 134-7 • \$1050 134-7 • \$1065 134-7 • \$1065 134-7 • \$1007 228-10 • \$1070CD 244-4 \$1070CD 244-4 \$2100C 228-10 \$2116 \$see Model \$215C-\$set \$200-5\$ \$20116 \$see Model \$215C \$-\$set \$200-5\$ \$213CD \$257-5\$ \$2100-5\$ <td></td>	
• V213CD	
200-51	
• V271T, V273T 259–5 • 7C42 179–5 • 7C52 179–5	
•7132	
•17T9 204-4 •20C22 1803	
• 20T12 180-3 • 21C2 200-5	
•21T	
•2173 (See Model DL217 — Set 200-5) •2174 (See Model 215C—Set 200-5) •2474 (See Model 215C—Set 200-5) •2471 (See Model 215C—Set 200-5) •2471 (See Model 215C—Set 200-5) •2471 (See Model 215C—Set 200-5) •215C 200-5 •215C 200-5 •02 200-5 •03 100-3	
• 24C4, 24C5	
• 24T10 180-3 • 1731 175C 177CD 192-5	
• 215C	
602 14-12 605, 606 Series 1-13 609, 610 Series 1-15 633 17-13 637 17-14	
633	
637 17-14	
652 Series 1-23	
637 17-14 652 Series 1-23 700 32-7 711 28-10 70 28-10 • 721 17-7 71	
711	
711	
700 326-7 711 28-10 720 772 728-10 7740 28-10 7751 (See Model 7132-Set 1777) 780 64-6 795 36-7 795 74-3	
700 326-7 711 28-10 720 772 728-10 7740 28-10 7751 (See Model 7132-Set 1777) 780 64-6 795 36-7 795 74-3	
700 32 711 28-10 720 177-7 740 28-10 772 177-7 740 31(5ce Model 7132-Set 177-7) 795 34-5 795 34-5 830 97-5 845 97-6 855 92-2 880 95A-5 899 74-3	
700 32 711 28-10 7721 177-7 740 28-10 97751 (See Model 7132-Set 177.7) 790 36-7 795 36-7 830 97-5 845 97-6 855 92-2 880 95A-5 899 74-3 923 89-6 930, 940 74-3	
700 32 711 28-10 721 177-7 740 28-10 7731 (See Model 7132-Set 177-7) 36-7 790 64-6 795 36-7 830 97-6 845 97-6 855 92-2 880 95A-5 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 925 89-6 926 89-6 926 89-6 920 74-3	
700 32 711 28 177 740 177 177 740 177 177 740 28 107 740 31 (See Model 7132—Set 177 178 795 34 3 830 97 5 845 97 6 855 92 2 880 95 5 899 74 3 925 89 6 930, 940 74 3 955 1-17 1001 17 1001 17	
700 32 711 28-10 721 177-7 740 28-10 9740 28-10 9740 28-10 9751 58e Model 7132-Set 177-7 970 64-6 775 36-7 830 97-6 845 97-6 880 755-5 890 74-3 925 89-6 930, 940 74-3 965 89-6 1000 Series 1-7 1001 17-15 FAIRMONT 74	
700 32–7 711 28–10 721 177–7 740 177–7 740 58–10 7731 (See Model 7132–Set 1777-7) 795 54–5 795 34–5 830 97–5 845 97–6 855 92–2 880 955–5 899 74–3 925 89–6 1000 Series 1–17 1001 17–15 FAIRMONT 307142-056 338102-056 5imilor to Chossitil 338102-056 5imilor to Chossitil	
700 32 711 28-10 721 177-7 740 28-10 7721 177-7 780 28-10 795 36-7 795 36-7 830 97-6 845 97-6 885 92-2 880 955-5 999 74-3 925 89-6 930, 940 74-3 965 89-6 1000 Series 1-17-15 FAIRMONT 30714A-056 (Similar to Chossil) 938712A-058 (Similar to Chossil) 219-3	
700 32 711 28-10 721 177-7 740 28-10 7721 177-7 780 28-10 795 36-7 795 36-7 830 97-6 845 97-6 885 92-2 880 955-5 999 74-3 925 89-6 930, 940 74-3 965 89-6 1000 Series 1-17-15 FAIRMONT 30714A-056 (Similar to Chossil) 938712A-058 (Similar to Chossil) 219-3	
700 32–7 711 28–10 721 177–7 740 28–10 7731 58–10 780 58–1777 780 36–7 783 36–7 855 97–5 855 92–5 930, 940 74–3 925 95–5 930, 940 74–3 900 Seriet 1–17 1001 17–15 FAIRMONT 30714A-056 93713 (Similar to Chassis) 109–1 93713 (Similar to Chassis) 109–1 931874 Similar to Chassis) 85–3	
700 24-7 711 28-10 721 177-7 740 177-7 740 28-10 7731 (See Model 7132-Set 177-7) 795 54-5 795 34-5 830 97-5 845 97-6 855 92-2 880 956-5 990 74-3 905 89-6 1000 56-7 9307 17-7 945 89-6 1000 17-15 FAIRMONT 308142-056 318124-056 (Similar to Chassis) 131713 (Similar to Chassis) 31814 (Similar to Chassis) 85-3 31814-872 Similar to Chassis) 85-3 318164-872 Similar to Chassis) 85-3 31816	
700 24-7 711 28-10 721 177-7 740 28-10 7731 58-10 7753 58-10 7753 58-10 7753 58-10 7753 54-5 7753 54-5 7753 54-5 7753 54-5 830 97-5 845 97-6 855 92-2 880 956-5 929 74-3 925 89-6 930, 940 74-3 945 89-6 1000 17-15 FAIRMONT 30714A-056 30814 51milar to Chassisi) 31814 51milar to Chassisi) 85-3 31814 74-90	
700 24-7 711 28-10 721 177-5 740 28-10 7731 58-10 7753 58-10 783 54-5 783 54-5 783 54-5 783 54-5 783 54-5 830 77-5 830 77-5 845 97-5 899 74-3 925 89-6 930, 940 74-3 945 89-6 1000 1-17 1001 17-15 FAIRMONT 30714A-056 30812A-058 19-3 31814 15 31814 15 31814 15 31814 16 85-3 31814 31816 100 85-3 31816 31816 100 85-3 31816 31814 100 <	
700 24-7 711 28-10 721 177-7 740 28-10 7731 58-10 7740 28-10 7750 58-10 7830 64-5 7830 64-5 7830 74-3 830 97-5 830 97-5 845 97-6 9725 89-6 9205 89-6 9206 74-3 965 89-6 1000 17-15 FAIRMONT 109-1 30714A-056 (Similar to Chossis) 30714A-058 (Similar to Chossis) 307142 (Similar to Chossis) 307142 (Similar to Chossis) 307142 (Similar to Chossis) 307142 (Similar to Chossis) 31874 (Similar to Chossis) 31876A-900 (Similar to Chossis) 31876A-900 (Similar to Chossis) 31876A-900 Similar to Chossis)	
700 24-7 711 28-10 721 177-7 740 28-10 7731 (See Model 7132-Set 177-7) 760 64-6 7790 54-6 7830 64-6 7830 64-6 7830 64-6 7830 64-6 7830 94-7 830 97-5 830 97-5 845 97-6 855 92-2 880 95-6 920 74-3 925 89-6 920 74-3 925 89-6 920 74-3 925 89-6 920 74-3 925 89-6 920 74-3 921 89-6 922 89-6 920 74-3 921 1713 921 1714 930114-0556 930114-0556	
700 24-7 711 28-10 721 177-7 740 28-10 7721 177-7 740 28-10 7731 (See Model 7132-Set 177-7) 780 36-7 783 36-7 835 97-6 835 97-7 980 95-2 880 97-3 930 95-2 980 95-2 980 95-2 980 95-4 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5 9740 74-5	
700 24-7 711 28-10 721 177-7 740 28-10 7721 177-7 740 28-10 7721 58-10 780 36-7 780 36-7 833 97-6 845 97-6 883 97-6 883 97-6 883 97-6 883 97-6 8845 97-6 883 97-6 8845 92-2 880 74-3 980 74-3 980 74-3 980 74-3 9765 85-6 900 74-3 9765 85-6 1000 17-15 FAIRMONT 199-1 930714A-058 (Similar to Chossis) 931874A508 (Similar to Chossis) 931874A72 (Similar to Chossis) 931874A7900 (Similar to Chossis)	
700 24-7 721 28-10 722 177-7 740 28-10 7721 178-7 740 28-10 7731 58-10 7837 58-10 7837 58-10 7837 58-10 7830 54-5 830 97-5 830 97-5 845 97-6 855 92-2 880 956-5 990 74-3 925 89-6 9307 14-7 1001 17-15 FAIRMONT 30714A-056 308112A-058 19-7 31814 19-3 31814 19-1 31814 19-3 31814 19-3 31814 19-3 31814 19-3 31814 19-3 31814 19-3 31814 19-3 31814 19-3	
700 24-7 721 28-10 722 177-7 740 28-10 7721 178-7 740 28-10 7731 (See Model 7132-Set 177-7) 780 64-6 7830 64-6 7830 94-6 830 97-5 830 97-5 830 97-5 830 97-5 845 97-7 925 89-6 930, 940 74-3 945 89-6 1001 17-15 FAIRMONT 109-1 931714-056 (Similar to Chossis) 9318712A-058 (Similar to Chossis) 931874-872 (Similar to Chossis) 931874-872 (Similar to Chossis) 931874-872 (Similar to Chossis) 931874-970 (Similar to Chossis) 931874-970 (Similar to Chossis) 931874-970 (Similar to Chossis) 9318764-970 (Similar to Chossis)	
700 24-7 711 28-10 721 177-7 740 28-10 7721 178-10 740 28-10 7731 58-10 783 58-10 783 54-50 783 54-50 783 54-50 830 97-5 845 97-5 855 92-2 880 956-5 990 74-3 925 89-6 930, 940 74-3 995 89-6 1000 17-15 FAIRMONT 30714A-056 30814 Similar to Chassil, 17-7 1001 17-15 31814 Similar to Chassil, 185-3 31816 Similar to Chassil, 185-3 31817A-9200 Similar to Chassil, 185-3 31817A-9216	
700 24-7 711 28-10 721 177-7 740 28-10 7721 178-0 740 28-10 7731 58-10 780 36-7 783 36-7 783 36-7 783 36-7 845 97-3 855 92-6 930 74-3 925 92-6 930, 940 74-3 925 174-3 93014A-056 15-7 1001 17-15 FAIRMONT 30714A-056 930714A-058 Similar to Chassis 931874A-058 Similar to Chassis 931874A-058 Similar to Chassis 931874A-970 Similar to Chassis 931874A-9708 Similar to Chassis	
700 24-7 711 28-10 721 177-7 740 28-10 7721 178-0 740 28-10 7731 58-10 780 36-7 783 36-7 783 36-7 783 36-7 845 97-3 855 92-6 930 74-3 925 92-6 930, 940 74-3 925 174-3 93014A-056 15-7 1001 17-15 FAIRMONT 30714A-056 930714A-058 Similar to Chassis 931874A-058 Similar to Chassis 931874A-058 Similar to Chassis 931874A-970 Similar to Chassis 931874A-9708 Similar to Chassis	
700 24-7 711 28-10 721 177-7 740 28-10 7747 28-10 7740 28-10 7740 28-10 7750 28-10 780 28-10 780 28-10 780 28-10 780 28-10 830 97-5 830 97-5 830 97-5 845 97-6 920 74-3 921 89-6 923 89-6 924 89-6 925 89-6 926 89-6 927 197-1 1001 17-15 FAIRMONT 109-1 30714A-058 198-3 931874 199-3 31874 199-3 31874 199-3 31876A-900 198-4 18170A-916 198-3 31876A-900 198-4	
700 24-7 711 28-10 721 177-7 740 28-10 7747 156-10 740 28-10 7731 156-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 74-3 750 74-3 750 74-3 750 74-3 750 74-3 750 74-3 750 74-3 925 89-6 920 74-3 921 744 925 89-7 925 89-6 926 19-1 930714A-058 191-1 930714A-058 191-1 93	
700 24-7 711 28-10 721 177-7 740 28-10 7721 177-7 740 28-10 7731 58-10 780 34-7 780 34-7 783 34-7 783 34-7 783 34-7 845 97-3 845 97-3 920 74-3 925 92-6 930, 940 74-3 925 92-7 930 94-7 9307 74-3 9307 74-3 940 74-3 941 119-3 9307 74-3 940 74-3 9307 74-3 9307 74-3 9307 74-3 9307 74-3 9307 74-3 9307 74-3 9307 74-3 9307	
700 24-7 711 28-10 721 757 740 28-10 7731 528-10 740 28-10 7731 528-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 34-5 750 34-5 830 97-5 830 97-5 845 97-7 845 97-7 845 97-7 845 97-7 845 97-7 845 97-7 845 97-7 845 97-7 845 97-7 845 97-7 925 89-6 930714A-056 Similar to Chassil 301714-058 Similar to Chassil 301714-6750 Similar to Cha	
700 24-7 711 28-10 720 177-7 740 28-10 7721 177-7 740 28-10 7721 177-7 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 28-10 740 74-3 750 74-3 750 74-3 750 74-3 750 74-3 750 74-3 750 74-3 750 74-3 750 74-3 740 74-3 750 74-3 740 74-3 740 74-3 740 74-3 740 74-3 7480	

FARNSWORTH-Cont. FARNSWORTH-LGAT. Ch. 150 (See Model ET-060) Ch. 152, 153 (See Model ET-060) Ch. 156, 157 (See Model EK-081) Ch. 158, 159 (See Model EC-260) Ch. 162 (See Model EC-260) Ch. 170 (See Model GK-100) Ch. 194, 201, 216 (See Model GK-100) 100) FEDERAL MFG. CO. 104 (Select-A-Call) 18–17 135 (Select-A-Call) 11—7 FEDERAL TEL. & RADIO CORP. 1040B (See Model 1040T—Set 23-9) 1540T FEDWAY • 321MS39A (Similar to Chassis) • 2321MS39A (Similar to Chassis) • 2321MS39A (Similar to Chassis) • 226–11 FERRAR C-81-B T-61B WR-11 17-16 39-4 15-10 FIRESTONE (AIR CHIEF) 4-A-2 (Code No. 297-6-LMMU-143) 14-4 4-A-3 (Code No. 297-6-LMFU-134) 31-13 4-A-10 (Code No. 297-7-RN228) 4-A-10 [Code No. 297-7-RN228] 4-A-11 (Code No. 188-8-4A11) 4-A-12 (Code No. 213-8-8370) 4-A-12 (Code No. 213-8-8370) 49-8 4-A-15 (Code 17.7.4A15), 36-7 4-A-17 (Code No. 213.7.7170) 4-A-21 (Code S-5.9000-A), 15-11 4-A-21 (Code No. 5.5.9001A) 4-A-22 (Code No. 5.5.9001A) 4-A-23 (5.5.9003-A) 4-A-23 (Code 291-6.556), 13-5 4-A-25 (Code 291-6.572), 13-6 4-A-25 (Code 291-6.572), 13-6 4-A-25 (Code 291-6.572), 13-6 4-A-26 (Code 391-6.972), 13-6 4-A-27 (Code 391-6.972), 13-6 4-A-28 (Code 391-6.972), 13-6 4-A-27 (28-12 4-A-37 (Code 177-5-4A31), 13-7 4-A-41 (Code 291-75-6), 52-8 4-A-42 (Code 291-75-6), 52-8 4-A-42 (Code No. 177-74-442) 30-9 4-A-60 (Code No. 307-8-9047A), 36-9 38 4-A-61 (Code No. 332-8-137J2T) 4.A.61 (Code No. 332-8-137/271, 48-77 4.B.77 4.A.63 4.A.64 68-70-10 4.A.64 A.65 68-77 68-70 4.A.64 68-70 4.A.64 Code No. 137:8-4A66) 74-4 A.66 4.A.64 Code No. 132:8-143653) 53-11 4.A.69 4.A.70 155-8-85) 4.A.71 (Code No. 155-8-85) 4.A.72 136-8 4.A.73 118-7 4.A.85 18-7 4.A.85 132-6 4.A.85 144-4 A.95 144-4 A.96 (See Model 4.A.87-Set A.97 (A.97 A.97 (A.98 A.97 (A.98 A.97 (See Model 4.A.87-Set A.97 (A.98 A.97 (See Model 4.A.87-Set A.97 (See Model 4.A.92 A.108 (Code 297-2.361) A.110 (See Model 4.A.92-Set A.113 (A.114 224-8 A.113 (A.114 224-9 -A-95 144 4A-113, 4A-114 219-5 4-A-118 219-5 4-A-118 See Model 4-A-92-Set 154-4 4-A-122 4-A-127, 4-A-128 259-7 4-B-1 (Code 7-6-PM13) 7-1 4-B-2 (Code 7-6-PM14) 8-18 4-B-6 (Code 7-6-PM14) 8-18 4-B-6 (Code 7-6-PM14) 8-18 5) 4) 18 177.7-PMI8 29-8 133-6 133-6 135-5 155-6 3-4 -6 4-B-56 133-4-B-57 124-4-B-58 135-4-B-60 53-4-B-60 55-4-B-60 55-4-B-62 55-4-B-63 (Similar to Chossis) 173-4-B-67 (Code 120-2-F152) 187-4-B-69 235-235-222-4.B-67 (Code 120-2-F152) 187-6 4-B-69 235-6 4-B-71 222-6 4-B-72 222-6 4-B-72 223-7 4-C-3 (Code 291-7.574) 33-6 4-C-6 19-17 4-C-13 (Code 332-B-140623 66-9 4-C-18 10-8 4-C-19 10-8 4-C-19 10-8 -6 4-C-13 (Code 332-8-140623 66--9 4-C-16 4-C-17 ... 120--6 4-C-18 10--8 4-C-19 4-C-20 ... 170--7 4-C-21 (Code 120-2-C51-U) 185--7 4-C-22 4-C-22 240--2 4-C-24 257--6 3-G-3 (Code 347-9-2498) 73--5 3-G-5 (Code 291-9-2498) 73--5 13-G-48 -10-52 (Code 307-1-9/0224, AA, B, BA) 193--4 3-G-57 158--4 3-G-57 158--4 3-G-107 13-G-108 (Code 105-2-700140) 197--6 120-6 110-8 170-7

EMERSON-FORD

FIRESTONE-Cont.	
13-G-109, A (Code 105-2-700100, 105-2-700104)	
13-G-110A (Code 334-2-M529A) 13-G-110A (Code 334-2-M531CA)	
(Also see PC8 60—Set 194-1 and PCB 76—Set 217-1) 182—5 13-G-114, A (Code 105-2-8170)	
(Ch. 817)	
13-G-110 (Code 334-2-MS2PA) 180-4 13-G-110A (Code 334-2-MS31CA) (Aitos eer PC8 40-Set 194-1 and PC8 76-Set 217-1) 182-5 182-5 13-G-114, A (Code 105-28170) 18-5 13-G-114, A (Code 105-28170) 16-6 13-G-114, A (Code 105-28170) 16-6 13-G-115, I3-G-116 (Code 334-2-MS31CA 18-5 194-1 and PC8 76-Set 217-1] 182-5 182-5 194-1 and PC8 76-Set 217-1] 182-5 182-5 13-G-117 (Code 105-2.8170) 171	
194-1 and PCB 76—Set 217-1) 182—5 13-G-117 (Code 105-2-8170) (Ch. 817) 198—6 13-G-119, 13-G-120 (Code 334-2- 4521CA) (Also PCB 40 Sat	
194-1 and PCB 76—Set 217-1) 182—5 13-G-122 (Code 105-2-700140) 197—6	
Model 13-G-107—Set 197-6) 13-G-125 (Code 105-2-81700) (See	
13-G-122 (Code 105-2-200140) 197 — 6	
12 C 128 12 C 120 12 C 120	
13-G-132	
13-G-145, 13-G-146 230−6 13-G-150 256−9	
 13-G-153 (See Model 13-G-155— Set 241-8) 	
• 13-G-155	
50-A	
209-3 30-F 262-9 50-F 262-9 30-7 30-7 50R, 50RT 231-7 70-A 263-8 70RT 263-9 30-7 30-7	
50R, 50RT 231-7 70-A 263-8 70RT 258-7	
FLEETWOOD	
600 209-4 610 248-7 700 243-5	
•710	
5P	
FORD FAC-18805-A	
FAC-18805-A	
11 4 1 20151	
Model 3mr) FAD-18805-D 208—6 FAE-18805-A 215—7 FDA-18805-A 255—6 FDA-18805-B1 236—5 FDA-18805-B2 250—10 CERPER CONTRACT	
FDA-18805-8-2	
GF890, E (DA.18805-81),109	
M-2 (1A-18805-A1)	
M4—Set 184-7) M-4B (FDA-18805-B1)236—5 OA-18805-A1 (See Model M-1A or	
OBF (OA-18805-A1 (Serial No. 150,000 and below) (See Model A1 Set 46 A)	
Model M-1A-1) 135	
OCF751-1 (1A-18805-D)157-4 OMF (OA-18805-A2)135-9	
GF890—Set 109-5) 1A-18805-A1	
1A-18805-A2	
Set 158-5) 1A-18805-D	
Set 158-5) 1A-18805-D 157-4 1A-18805-D 157-4 1BF (1A-18805-AT) [See Model M-2 Set 132-7) 1CF743 (1A-18805-B) 133-7 1CF743 (1A-18805-B) 133-7 1CF743 (1A-18805-B) 133-8 1CF743 (1A-18805-B) 133-8 1SFT751-2 (1A-18805-G) 158-5 1SFT751-2 (1A-18805-G) See Model 1CFT751-2-Set 157-4) 2BF [FAC-18805-B) (See Model M-2) 2CF754 (FAC-18805-B) 167-7 2CF754 (FAC-18805-B) 167-7	
1CF743-1 (1A-18805-8) 158-5 1CF7751-2 (1A-18805-G) 157-4 1MF (1A-18805-A2) 131-8	
1SFT751-2 (1A-18805-G) (See Model 1CFT751-2-Set 157-4) 285 (EAC 18905 All) (See Model	
M4-Set 184-7) 2CF754 (FAC-18805-8) 167-7 2WE (FAC-18805-8) 167-7	
model (LF/13/123ef 13/-1) 2BF (FAC-18805.A1) 2CF734 (FAC-18805.A) 2CF734 (FAC-18805.A) 2BF (FAC-18805.C) 2BF (FAC-18805.C) 2BF (FAC-18805.C) 2BF (FAC-18805.C) 2BF (FAC-18805.C) 2BF (FAC-18805.C) 206-5 3MF (FAD-18805.C) 206-5 3MF (FAD-18805.A) 215-7 35F735 (FAD-18805.A) 255-6 MHF (FDA-18805.A) 255-6 MF080 (51A-18805.A) 40-18 6MF780 (51A-18805.A) 62-12	
3MFT (FAE-18805-C) 206-5 3MFT (FAE-18805-A) 215-7 3SF755 (FAD-18805-D) 208-6	
45F (See Model M48—Set 236-5) 4MF (FDA-18805-8-2)	
6MF080 (51A-18805-A1) (Ch. 6CA1) 10-18 6MF780 (51A-18805-A1) . 62-12	
8A-18805-A 44-4 8A-18805-A1 46-4 8A-18805-A3 (See Model 9MF)	
OMF/10/2 [J] AF-1 (BdUJ) (See Mode) 6MF780-Set 62-12) 83-4 8A-18805-A 44-4 8A-18805-A3 (See Mode) 9MF) 45-4 8A-18805-A3 (See Mode) 9MF) Set 42-12 or Model 8MF880- Set 42-12 or Model 8MF980- Set 42-12 or Model 8MF980- Set 42-12 or Model 8MF980- Set 43-19 or Model 8MF980-	
Set 61.9) 83-4 8A-18805-81 83-4 8C-18805-8 47-9 8MF880 (8A-188058) 42-12 8MF881 (8C-188058) 47-9	
8MF881 (8C-18805B) 42-12 8MF881 (8C-18805B) 47-9	

NOTE: PCB Denotes Product Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

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FORD-HALLICRAFTERS

GENERAL ELECTRIC-Cont. FORD-Cont. FREED EISEMAN 46 11-8 • 54, 55, 56, 68 (Ch. 1620C) 113-1A GALVIN (See Motorola) GAMBLE-SKOGMO (See Coronado)
 AA1, 4A-2
 29-9

 48-1
 51-6

 5A-1
 22-15

 5A-2
 5-28

 5A-3
 44-5

 5A-4
 44-5
 GAROD (Also see Majestic)
 DA-1
 22-13

 SA-2
 3-28

 SA-3
 46-5

 SA-4
 46-5

 SA-1
 15-12

 SA-3
 46-5

 SA-4
 46-5

 SA-5
 15-12

 SD, 5D-2
 12-12

 SD-3, 5D-3A
 22-16

 SC-1
 36-7

 SRC-1
 36-8

 6A-2
 5-3

 6A-1
 25-9

 6BU-1A-The Senotor
 13-18

 6D25, 60P5-A
 10723, 10723, 10724, 10724, 10724, 10723, 10724, 10725, 107220, 107221, 10722, 10723, 10724, 10725, 107220, 107221, 10722, 10722, 10722, 10722, 10722, 12726, 12726, 12727, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 12722, 15727, 60-12

 15726, 15727, 60-12
 15726, 15727, 60-12

 15726, 15727, 15727, 60-12
 15726, 15727, 60-12

 15726, 15727, 60-12
 95A-4

 15726, 15727, 15725, 15726, 15726, 15727, 55A-4

 16724, 16725 (58e Meijestic Model

 16724, 16725 (58e Meijestic Model

 16724, 16725 (58e Meijestic Model
 • 2549T • 3912 TVFMP, 3915 TVFMP 95A-6 GARRARD (See Record Changer Listing) GENERAL (Mutual Buying Syndicate) •17CG1, 17TW (Similar to Chassis) 149–13
 GENERAL ELECTRIC (Also see Record Chonger Listing)

 A1-200
 243--6

 A1-300
 238--8

 UHF-103 Tel. UHF Conv.. 209--5
 YR8-60-2, YR8-60-2, YR8-60-7, YR8-60-2, YR8-60-1, 10760-96-4

 • 10C101, 10C102
 96-4

 • 10T1
 96-4

 • 10T6
 96-4
 1001, 1001, 1001, 1001, 1001, 1001, 1001, 1001, 1001, 1001, 1001, 1000, 1001, 12K1 95A-6 12K1 95A-6 12T1 95A-6 12T3, 12T3B, 12T4, 12T4B 125-7 12T7 99A-5 , 1214, 1214B 125—7 99A—5 35—8 103 123—4 123—4 123—4 111 123—4 14 14C102, 14C103 14T2, 14T3 16C103 16C110, 16C111 16C113

17C117 (See Model 17C113—Set 166-10) 17(117 [See Model 17(113—Set 176(1-0) 177(125 (See PCB 64—Set 201-1 and Model 21(201—Set 194-2) 177(125-UHF [for TV Ch. tee PCB 64 —Set 201-1 and Model 21(201— Set 194-2, for UHF Conv. See Model UHF-103—Set 209-5) 017(1) 7172, 1773 (Alios ce PCB 32— Set 158-1) 141—6 1771 (See Model 17C113—Set 141-6) Set 158-1 and Model 17C103— Set 141-6) 1771 (See Model 17C113—Set 166-10) 1771 (See Model 17C113—Set 166-10)
 • 110
 • 100
 • 100
 • 129
 129
 -7

 • 2120, 2172
 237-7
 237-7
 -7
 -5
 -7
 -6
 -6
 -6
 -6
 -6
 -6
 -6
 -6
 -6
 -6
 -7
 -6
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 -7
 -7
 -6
 -7
 -7
 -7
 -7
 -7
 -7
 -7
 -7
 -7
 -7

64, 6 66, 100,	
102	102W 41_8
103,	105
113	107W 41-8 51-7 114W, 115, 115W 41-8
114,	114W, 115, 115W 41-6 119M, 119W 39-5
123,	See Model 118-Set 39-5)
135,	136 81—8 30–10 75—9
145	
150	
165 180	89—7 20-11
186-	201. 202. 203. 205. 2054
210,	211. 212
218, 219, 226	
230	(See Kaiser-Frazier Mode
20	0001—Set 35-13) 4-13
254	
280	
304	32–10 3–26
324	
326, 328 329, 64	220 (5 Madel 224 5-
64	-7) 355
354, 356, 376,	357, 358 37-6
400,	401 118 405 121 405 120 120 120 120 120 120 120 120 120 120
408	405 121-0
410	
411 412 412F 414	190 0
414F 415 415F 416	
416	211- 175-11 211-
417	
122	423 154 425 233
430	423
431,	432
450,	451, 452 (See Model 424—Se 3-2)
500, 502	35-9
505,	511
510F	, 511F, 512F, 513F143
515F 521, 521F	, 516F, 517F, 518F. 143- 522
626	151
542,	543
551, 555, 557,	547, 548, 549 552 555G, 556 250-1
557,	558, 559 (See Model 560-Se
24 560, 564,	561
600 601	561 249 565, 566 251 109 109 603, 604 115 606 145
605,	603, 604 109- 606 115- 606 605-Se 608 606-Se 611 147- 613 231- 615 199- 626 (See Model 612-Se 626 (See Model 612-Se 626 (See Model 612-Se 626 (See Model 612-Se 631 632 261-
14	608 (See Model 605Se 5-6) 611
612,	611
620,	613 231 615 199 621, 622 262 626 (See Model 612—Se
23	1-9)
640,	641 (See Model 614-Se
650	101— 157—
752,	753 157 167
755	9-6) 101
757	167
Se	178-7)
• 802 • 803	91A
	806, 807, 809 Series 78- 53-1 63-
•811 •814	
 814 815 817 919 	69— 97A— 78— 95A
	95A
835	Early
• 901	·····
•910	
	IERAL IMPLEMENT
9A5	
	IERAL INDUSTRIES (See nger and Recorder
	ings)
GEN	IERAL INSTRUMENT
	o see Record Changer

GENERAL TELEVISION 1A5, 2A5, 3A5, 5A5 (Ch. 1-1) 485 2 9A5, 585Y 2 15A3 (Ch. 1-1) 1 17A3 (Ch. 1-1) 1 22A5C 1 23A6 3 2585 2 2685 2 27C5 3 564C1, 568CR (See Model 5 564C1, 568CR (See Model 5 564C1, 568CR (See Model 5 564C1, 568CA (See Model 5 564C, 560 568C1, 568CA (See Model 5 564C, 560 568C2, 560 564C3 568C4 578 589, 580 568C3 564C4 <tr< th=""><th>ST-83 SX-42 SX-42 SX-42 SX-62 SX-62 T-11 SX-71 7-12 T-54 [E 7-12 T-54 [E 7-13 ST-60 6-10 St-74 3-21 St-74 5-22 TW-500 2-14 TW-500 3-19 TW-100 6-11 \$R10. 5 \$R10. 9-11 (Run 6-11 \$R11.5 5 \$R20.7 6A \$R30.7 A, 55 \$R50.5</th></tr<>	ST-83 SX-42 SX-42 SX-42 SX-62 SX-62 T-11 SX-71 7-12 T-54 [E 7-12 T-54 [E 7-13 ST-60 6-10 St-74 3-21 St-74 5-22 TW-500 2-14 TW-500 3-19 TW-100 6-11 \$R10. 5 \$R10. 9-11 (Run 6-11 \$R11.5 5 \$R20.7 6A \$R30.7 A, 55 \$R50.5
1 A5, 2A5, 3A5, 5A5 (Ch. 1-1) 485 2 985 3 986 3 14A4 3 15A5 (Ch. 1-1) 17A5 17A5 19A3 (Ch. 1-1) 17A5 2 18A4 1 12A5 2 19A5 (Ch. 1-1) 1 17A5 1 18A5 2 2000 1 2010 2 2011 2 2012 2 2013 2 2014 2 2015 2 2015 2 2015 2 2016 2 2017 2 2018 2 2019 2 2010 2 2011 2 2012 2 2015	1-21 SX-71 7-11 0-54 [E 7-12 0-54 [C 7-12 0-54 [C 7-12 0-54 [C 7-12 0-54 [C 7-12 0-54 [C 7-12 0-54 [C 7-15 0-54 [C 7-15 0-54 [C 7-10
9A5 3 9B6P 3 15A5 (Ch. 1-1) 17A5 17A5 19A3 (Ch. 1-1) 17A5 19A3 (Ch. 1-1) 12A5 12A5C 12A5C 12A5C 2486 33 2585 22 2685 22 27C5 3 GILFILLAN 56A, 56B 56E (See Model 56A—Set 1-2 56E (See Model 56A—Set 1-2 56E (See Model 56A—Set 1-2 56B 'The Overland'' 66D, 66DM 66D, 66PM ''The El Dorada''	9-6 •1-60. 6-10 •1-61, T. 3-21 •1-61, T. 5-1 •1-63. 5-22 TW-25 1-21 TW-500 2-14 TW-500 3-19 TW-100 3-19 TW-100 3-10 TW-100 3-
14.44	6-10 8-1-61, T- 3-21 Set 1 1-21 0-68, - 5-22 TW-250 2-14 TW-500 2-14 TW-500 3-19 TW-100 4-14 SR10A 6-15 SR10A 6-11 SR11, 5 SR18, 5 SR18, 5
3A3 [Ch. 1-1] 7A3 [Ch. 1-1] 19A3 [Ch. 1-1] 21A4 1 22A5 1 23A5 2 2585 2 2685 2 27C5 3 GILFILLAN 56A, 56B 56C 50C-1 50C	S-22 IW-25 1-21 IW-500 2-14 IW-600 3-19 TW-100 4-14 SR10A 6-15 SR10A 6-11 SR11, 5 6-11 SR11, 5 SR18, 5 SR18, 5
19A3 (Ch. 1-1) 21A4 12A4 12A5C 23A6 24B6 25B5 26B5 27C5 36B5 27C5 36C1 56BC1 56BC6 56BC7 56C 56C 56C 56C 56C 56C 56E 56E 56B 56E 56E 56E 56E 56E 56C 56E 56E 56E 56E 56E 56E 56E 56E 56E 56B	1-21 TW-500 2-14 TW-600 3-19 TW-100 4-14 SR10. 7-8 SR10A 6-15 SR10A 9-11 (Run 6-11 SR11, 5 SR18, 5 Mode
23A6 2486 2585 2685 27C5 3 GILFILLAN 56A, 568 568C1, 568CR 568C1, 568CR 568C1, 568CR 564, 560 564, 560 566, 560	4-14 SR10. 7-8 SR10A 6-15 SR10A 9-11 (Run 6-11 SR11, 5 SR18, 5 Mode
2685 2 27C5 3 GilFilLAN 564, 568 566C1, 568CR (See Model 5 Set 1-27) 56C, 560 56E (See Model 56A—Set 1-2 58m, 58W 66B, 50M 66B, 66AM 66D, 66DM 66D, 66DM 66P, 66PM<''The El Dorada'' 48B-D	6-15 SRIUA 9-11 (Run 6-11 SR11, 5 5R18, 5 Mode
27C5 3 GILFILLAN 56A, 56B 56BC1, 56BCR (See Model 5 56C, 56D 56C (See Model 56A—Set 1-2 58M, 58W 66A, 66A Model 56A 66B, 66B Model 56A 68B, 0 68B,	6-11 5R11, 5 5R18, 5 Mode
56A, 56B 56BC1, 56BCR (See Model 5 Set 1-27) 56C, 56D 56E (See Model 56A—Set 1-2 58M, 58W 66A, 66AM 66B, 66DM 66D, 66DM 66P, 66PM "The El Dorada" 48B,D	Mode
SoBLI, SoBLK (See Model S Set 1.27) S6C, S6D S6E (See Model S6A—Set 1.2 S8M, S8W 66A, 66AM 66B, 'The Overland' 66D, 66DM 66D, 66DM 66P, 66PM ''The El Dorada''	6A- 5R30, A
56E (See Model 56A—Set 1-2 58M, 58W 66A, 66AM 66B 'The Overland'' 66D, 66DM 66P, 66PM 'The El Dorada'' 68B.D	5050 F
58M, 58W 66A, 66AM 66B 'The Overland' 66D, 66DM 66P, 66PM 'The El Dorada' 68B.D	71 5R100A
66P, 66PM "The El Dorada" 68B-D	8-16 5R230,
688.D d	8-17 8-16 9-15 8R40, 8 017T310
68B-D 4	6-10
68-48 86C, 86P, 86U (86 Series) 2	400, 4 1-10 6-16 9-10 505 (Ed 505 (Ed 505 (Ed
108-48	9-10 505 (Lo -Set 506 (Ec
GLOBE 58P1 1	8-20 • 506 (La
6AP1	0-13 158-1
AU1 7	0-13
51 62C	9-18 0514
85	9-19 9-9 9-9 518, 51 520E 520E 521 521 9-7 521E 9-7 524 -1-9 524 -1-9
456 457	0-7 9-7 •521E
500 517	0000, ot
551 552 553	080, 0
559 2	0-8 0715, A
GODFREY 6AD	28-17 28-17 28-17 28-17 28-17 28-17 2740, 74 Set 1 2745
	28-17 •740, 74 Set 1
GONSET 3-30 Meter Converter	1-11 0750, 75
ATB-3 7	7-9 •760,76 0-5 •805,8 3-6 •810
NSA-20	•810A •810C (
(Also see Mantola)	•811 •815
92-527, 92-528	•822
GOTHAM • 319 • 323	9-6 832, 83 860, 86
• 323 25 GRANCO	•8/0, 8 124-
	7-6 880 (S
W. T. GRANT (See Grant	1001
GRANTLINE 300 (Series B)	
300 (Series B) 500, 501 (Series A) 501-7 504-7	
504-7 508-7	4-8 W120
510-A 605, 616 641	24-19 01012P 2-17 W120
	1-9 1013C 1-9 1015, 1 35-11 A110
6547	1-10 • 1019 (C • 1021P
GROMMES LJ-2	
LJ-2 20 50PG, 51PG 10 50PG2 20	
	89-10 X120 0-3 •1027C 1-10 •1050,
117PS	10 PCB
215BA	78-8 PCB
HALLICRAFTER5 (Also see Echophone)	• 1053P, PCB
A-84 (Run 1)	09-7 1010 1055C, 1055C, PCB
ATCL-9, -10, -11 (Run 1)2 CA-2, CA-2A CA-4	30-12 1010 36-13 1060C,
S-388	
S-38C (Run 2) 15 S-40 S-40A S-40B S-41G, S-41W S-41G, S-41W	2-19 1062C, 33-10 PCB
S-40B S-41G, S-41W	22_4 1010 10-19 01072 (1
S-51	0-8 1074 (0
S-52 S-53	
5-52 5-53 553A, AU 5-55, S-56 5-58 5-59	1-5 5-9 7-8 •1075 (0
5.59	8-10 01075A
\$-58 \$-59 \$-72	32-6 -107547
S-58 S-59 S-72 S-72L S-76U 12	58-10 •1075A 32-6 •1075A 73-6 • 1075A PCB 1 13-9 • 1077 (0
S-72 S-72L S-76, S-76U S-77 S-77 S-78	13_6 13_9 107541 PCB 1 PCB 1 13_9 1077 {r 1078 {c 107541 PCB 1 107541 PCB 1 1077541 PCB 1077541 PCB 1
S-72 S-72L S-76, S-76U S-77 S-78A S-78A (Run 1)	12 0 1075A1 73 6 PCB I 13 9 1077 (r) 16 7 1078 (c) 24 5 1078A 30 6 1078A 12 4 1078A
S-72 S-72L S-76, S-76U S-77 S-78A S-78A (Run 1)	12 0 1075A1 73 6 PCB 1 13 9 1077 (r) 16 7 1078 (c) 24 5 1078A

RAFTERS-Cont. 44--6 45-13 61-12 111--6 **111**—6 **48**—10 **91**—6 **63**—10 irly) 64, T-67 (Also see PCB 32-58-1) 65-3, M, W 06, 409, 410, 411, 412 52-9 48-10 B-10] (Also see PCB 32—Set 65—7 96—5 80—7 13 9. 520 92-3 80-7 92-3 80-7 80-7 92-3 07-5 602, 603, 604. 92 250-12 113-3 113-3 113-3 113-3 6 Model 680-Set 113-3) 31 (Run 1) (See Model 680-13-3) 11 (Run 1) (See Model 680-13-3) 105-4 105-4 105-4 105-4 136-9 136-9 ee Model 805-Set Model 810A-Set 124-6 124-6 121-1A 124 71 (See Model 810A-Set
 371
 (See Model 810A-Set 124-6)

 -60
 -60

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 1016, 1017, 1018, 1019 (Ch.

 0D
 177 --8

 Ch. 21000D)
 180 --7

 ICh. D1200D, L1200D,
 1200D,

 0D
 188 --6

 ICh. D1200D)
 188 --6

 ICh. D1200D,
 172 --4

 ICh. D1200D,
 188 --6

 ICh. D1200D,
 11200D,

 0D
 188 --6

 ICh. D1200D,
 188 --6

 ICh. D1200D,
 188 --6

 ICh. J1200D,
 188 --6

 ICh. J1200D,
 188 --6

 ICh. J1200D,
 188 --6
 ---Set 188-6) 1063C (Ch. J1200D) (See 75--Set 216-1 and Model --Set 188-6)
 Project
 Set 188-6)

 (Ch. AG1200D)
 211-7

 (Ch. AR1200D)
 211-7
 211-7 Ch. AR1200D)

(Ch

NOTE: PCB Denotes Production Change Bulletin, Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

HALLICRAFTERS-KAYE-HALBERT

JACKSON-Cont. JP-200 ... JP-300 ... JP-400 ... 10C, 10T 12C, 12T 14C, 14T 16C, 16T 171-6 174-7 171-6 132-8 132-8 B 254 255 312 316 350 412 132 _8 __8 131—9 132—8
 11
 132-s

 14
 132-s

 14001 (Sse Madel 10C-Set 132.s)
 Standard 10C-Set

 132.s)
 T (Sse Madel 10C-Set 132.s)

 5000, 5050
 88-5

 52000, 5550
 88-5

 5500, 5550
 88-5

 5400, 5550
 88-5

 5400, 5550
 88-5

 5400, 5550
 88-5

 5400, 5550
 88-5

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 88-5

 5400, 5550
 88-5

 • 416 JEFFERSON-TRAVIS JEWEL •17C9, 17T9, 17TW7 •21C9, 21T9 300 304 187-7 23-11 35-12 98.5 9600, 961 (See Model 960-Set 97.8) 985 99-8 5007 99-8 5010 182 5020
 5020
 11-7

 5020U (See Model 5020—Set 136-10

 100

 5040

 5050

 5050

 5057U

 5100

 5100
 160-5 128-7 109-7 159-7 217-7 194-6 196-4 206-7 5057U 5100, E, U 5125U 5200 5205 5250 225-12 5310 KAISER-FRAZER
 Halbertonic
 128—8

 100170
 128—8

 100205
 139—6

 100330 (See Model 100170—Set

 128.8)
 200001

 200001
 35–13

 200002
 56–13
 KAPPLER 102T 54-10 KARADIO
 M80B
 233-3

 80C
 66-10

 1275, 1275A
 85-7

 1276
 115-4
 KAYE-HALBERT C-024 (Ch. 253) (For TV Ch. only See PCB 63-Set 197-1 and Model 014 (Set 146-8) 169-9 014 (Ch. 253) (Also see PCB 63-Set 197-1) 146-8 024 (Ch. 253) (Also see PCB 63-Set 197-1) 146-8 033, 034, 035, 036, 037 (Ch. 242) 139-7 KAYE-HALBERT •033, 034, 035, 036, 037, 014, 2421 •044, 045, 046 (Ch. 253) (Alto see PCB 63-Set 197-1) • 146_B •074, 076, 077 (Ch. 253) (Alto see PCB 63-Set 197-1) • 146_B •104, 114 (Ch. F-243) (See PCB 96-Set 241-1 ond Model 012-Set 169-9) 104, 114 [Ch. F-243] (see FCL 90-Ser 241-1 and Model D12-Set 169-9)
104 [Ch. 243] (See Model 012-Set 169-9)
114 [Ch. 243] (See Model 012-Set 169-9)
114 [Ch. 243] (See Model 012-Set 169-9)
114 [Ch. F-243] (See FCB 90-Set 249-9) and Model 012 - Set 169-9)
124 [Ch. F-243] (See FCB 90-Set 241-1 and Model 012 - Set 169-9)
124 [Ch. F-243] (See FCB 90-Set 241-1 and Model 012 - Set 169-9)
124 [Ch. F-243] (See FCB 90-Set 241-1 and Model 012 - Set 169-9)
138 [Ch. F-243] (See Model 012-Set 169-9)
138 [Ch. F-243] (See Model 012-Set 169-9)
138 [Ch. F-243] (See Model 012-Set 169-9)
144, 145, 146 [Ch. F-243] [See PCB 96-Set 241-1 and Model 012-Set 169-9)
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]
144, 145, 146 [Ch. F-243] [See Model 012-Set 169-9]

 HALLICRAFTERS-Cont.

 ■1081B (Ch. AZ1200D (See PC8 81— Sit 222-1 and Model 1050—Set 2177)

 ■1081C (Ch. B&1200D) (See PC8 81 -Set 2177)

 ■1081C (Ch. B&1200D) (See PC8 81)

 Set 2177)

 ■1081C (Ch. B&1200D) (See PC8 81)

 Set 2177)

 ■1081E (Ch. AZ1200D) (See PC8 81)

 Set 2177)

 ■1081E (Ch. B&1200D) (See PC8 81)

 Set 21171

 ■10858 (Ch. AZ1200D) (See PC8 81)

 Set 21171

 ■10858 (Ch. AZ1200D) (See PC8 81)

 Set 221.171

 ■10858 (Ch. AZ1200D) (See PC8 81)

 Set 222.1 and Model 1050—

 Set 221.71

 ■10888 (Ch. AZ1200D) (See PC8 81)

 Set 222.1 and Model 1050—

 Set 211.71

 ■10888 (Ch. AZ1200D) (See PC8 81)

 Set 222.1 and Model 1050—

 Set 222.1 and Model 1050—

 Se HALLICRAFTERS-Cont. HOFFMAN-Cont. C-506, C-507 C-511 C-512 C-513 C-514 49-10 48-11 51-9 50-9 47-10 61-13 C-512 C-513 C-514 C-514 C-516 C-1006, C1007 C-1006, C1-801, C1-900, C1-901 C-78006, C1-801, C1-900, C1-901 C-78104 (Ch. 190, B) 205-5 205-5 205-5 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 205-5 204-4 205-5 204-4 205-5 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-4 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 204-20 205-5 204-20 204-20 205-5 204-20 205-5 204-20 205-5 204-20 204-20 205-5 204-20 205-5 204-20 204-20 205-5 204-20 205-5 204-20 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5 204-20 205-5
 63-11

 78103 (Ch. 120, M)
 205-5

 78113 (Ch. 201, 205-5

 78113 (Ch. 212, M)
 194-4

 78123 (Ch. 212, Ke Model 781138

 -Set 194.41
 236-6

 78137 (U (Ch. 300.17) (Aiso see PCB 108-5er 256-1)
 236-6

 78137 (U (Ch. 300.17) (Aiso see PCB 108-5er 256-1)
 236-6

 78137 (U (Ch. 300.17) (Aiso see PCB 108-5er 256-1)
 236-6

 774103 (Ch. 120, B)
 201-5

 774112 (Ch. 202)
 205-5

 774113 (Ch. 212, M)
 194-4

 774113 (Ch. 212, M)
 256-6

 774113 (Ch. 212, M)
 256-5

 774113 (Ch. 212, M)
 256-5

 774114 (Ch. 212, M)
 256-5

 774115 (Ch. 100, B)
 201-5

 774114 (Ch. 212, M)
 201-5

 774113 (Ch. 1371)
 168-8

 2081027 (Ch. 1831)
 168-8

 2081027 (Ch. 1831)
 168-8

 2081027 (Ch. 1831)
 168-8

 2081037 (Ch. 1831)
 168-8

 2081037 (Ch. 1831)
 168-8

 2081037 (Ch. 1831)
 168-8

 2081037 (Ch. 191, 8)
 201-5</ • 17810M • 17813.+ • 17812, 17813, 17814, 17815.+ • 17812, 17813, 17814, 17815.+ • 17816, 17817 • 156-6 • 17816, 17817 • 156-6 • 155-8 • 155-8
 17824.
 135-6

 17825.
 165-6

 17825.
 17804C-Set

 155.8
 11000.

 1025.5et
 1697.1

 17838.
 155-8

 17844.
 155-8
 152-9 17908 (See Model 17824-A—Set 165-6) 17928 (See Model 17824-A—Set 165-6) 17922 (See Model 17824-A—Set 165-6) 17934 (5-0) 17934 (5-0) 165-6 165-6 165-6 165-6 165-6 165-6 165-6 165-6 17924 165-6 165-6 17924 165-6 17924 165-6 17924 165-6 17924 17924 165-6 17924 17924 17924 165-6 17924 17927 17 17933, 165—6 167–10 165—6 155—8 154—6 165—6 165—6 165—6 165—6 • 20823 (Ch. M900D) • 20823B (Ch. L900D) • 20823C 20823C 20990, 209905, 20994 21923 21928 21928 21980 21940 21940 Charles and the second HAMILTON ELECTRONICS H-15-S 16-17 H-20-25 16-18 HAMILTON RADIO CORP. (See Olympic) HAMMARLUND HARVEY-WELLS AT-38-6, AT-38-12 ATR-3-6, ATR-2-12 32-11 36-14 HBR-5 HOFFMAN A-200 (Ch. 103) A-202 (Ch. 119) A-300 (Ch. 119) A-309 (Ch. 119) A-401 (Ch. 102) A-500 (Ch. 107) A-501 (Ch. 1085T) A-500 (Ch. 1105) B-400 4-23 11-11 4-41 11-11 11-12 4-34 3-35 12-16 17-17 20-14 48-11 51-9 50-9

• 17824

HEATH

A-501 A-700 B-400 B-1000 C-501

C-503 C-504 (Ch. 123)

638) Ch. 186 (See Model 963) Ch. 187, B, C (See Model 248707) Ch. 190, B (See Model 781041 Ch. 191, B (See Model 218107) Ch. 192 (See Model 218901)

HOFFMAN-Cont.

HOFFMAN-Cont. Ch. 194 (See Model 208102F) Ch. 196, M (See Model 218116) Ch. 196 (See Model 218176) Ch. 197 (See Model 21870) Ch. 197 (See Model 218007) Ch. 199 (See Model 218007) Ch. 200 (See Model 218007) Ch. 201 (See Model 218102) Ch. 201 (See Model 218102) Ch. 201 (See Model 21813) Ch. 211, M (See Model 21813) Ch. 300-21 (See Model 21814, U) Ch. 300-17 (See Model 21814, U) Ch. 300-17 (See Model 21814, U) Ch. 301-21 (See Model 218167) Ch. 301-21 (See Model 218167) Ch. 302 (See Model 218167) Ch. 302 (See Model 218167) Ch. 400-21 (See Model 21817) Ch. 403-24 (See Model 21817) Ch. 403-24 (See Model 21817) Ch. 403-21 (See Model 21817) Ch. 403-21 (See Model 21817) Ch. 403-21 (See Model 21831) Ch. 403-21 (See Model 218331) Ch. 405-21 (See Model 218331) HOWARD HOWARD 472AC, 472AF, 472C, 472F 31-14 478AC, 472AF, 472C, 472F 32-12 4751V, Photofoct, Sarvice 84 4816, 481C, 481M, 48-12 901A, 48-14 901A, Fe, H, H, M, W (See Model 901A, Series 1-8) 1-8 901A, Series 1 10-8 906, 906C 17-18 906W, 905A 25-15 907 5-7 HUDSON (Auto Radia) HUDSON (Auto Radio) D847 (Fact. No. 64H189), 25–16 D848 (Fact. No. 64H189), 25–16 D8548 (Fact. No. 64H189), 25–16 225908 (Fact), ..., 149–6 225908 (Late) (Ch. 749-1), 167–11 226403 (Ch. 749-2), ..., 167–11 236476 (Sh759), ..., 215–8 236040 (Sh758), ..., 214–4 23600 (Sh758), ..., 214–4 HUDSON (Dept. Stores) HUDSON (Dept. Stores) 30T14A-056 (Similar to Chasis) 119-3 38T12A-058 (Similar to Chasis) 199-1 317T3 (Similar to Chasis) 318T4 (Similar to Chasis) 318T4 (Similar to Chasis) 318T4 (Similar to Chasis) 318T4 (Similar to Chasis) 318T45 (Similar to Chasis) 318T64 (Similar to Chasis) 318T64-950 (Similar to Chasis) 31816A (Similar to Chossis) 85–3 31816A (Similar to Chossis) 31816A (Solo (Similar to Chossis) 31817A-900 (Similar to Chossis) 321MS31CA (Similar to Chossis) 321MS30A (Similar to Chossis) 321MS31C-A (Similar to Chossis) 321MS39A (Similar to Chossis) 226-11 321MS39A (Similar to Chossis) • 34 1m3370 220-• 518T6A (Similar to Chassis) 85-• 518T9A-919 (Similar to Chass 78- Sist9A-919 (Similar to Chosis) Sist10A-916 (Similar to Chosis) 2318t0A-954 (Similar to Chosis) 2318t0A-954 (Similar to Chosis) 2318t0A-912 (Similar to Chosis) 78 2321M539A (Similar to Chosis) 226-11 HUDSON ELECTRONICS 186-6 191-11 194-5 186-7 190-5 194-5 194-5 198-9 123-6 121-8 126-6 188-7 191-12 188-7 191-12 HYDE PARK HYDE PARK AR14L AR17L MST12, MST14 I47R, I67R 17CD (1st Prod.) 17CC (1st Prod.) 17CCR (1st Prod.) 17CRG (1st Prod.) 17ROG (1st Prod.) 20CD (1st Prod.) 20CD (2nd Prod.) 20CD (2nd Prod.) 20CD (2nd Prod.) 312 203D (1st Prod.) 313 203D (1st Prod.) 314 312 819 819 8193CM 8193CM 169-8 168-9 168-9 168-9 169-8 169-8 169-8 169-8 169-8 169-8 168-9 169-8 168-9 168-9 168-9 168-9 168-9 168-9 168-9 168-9 169—8 168—9 168—9 168—9 INDUSTRIAL ELECTRONIC CORP. (See Simplon) INDUSTRIAL TELEVISION INDUSTRIAL TELEVISION (Also see Century) 01T-407, [T-427, (Ch. 1T-267, 1T-357, 1T-397, 1T-427, (Ch. 1T-217, 17-377, 12-372, 12-INTERNATIONAL ELECTRONICS (See Recorder Listing) JACK5ON DP-51 JP-20 JP-30 JP-50

HOFFMAN-Cont.

NOTE: PC	B Denster	Benduction.	C	B 11 41

50-9

www.americanradiohistory.com

156—7 173—7 153—7 155—9 Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

KAYE-HALBERT_Cont.

KAYE-HALBERT-MAJESTIC 146 (Ch. 253) (See Model 014—Set 146-8)
146 (Ch. 253DX) (See PCB 45—Set 179-1 and Model 114DX—Set 170.9 154, 164 (Ch. F-243) (See PCB 96---Set 241-1 and Madel 012---Set 169.9) 154 (Ch. 243) (See Madel 012---Set 169-9) 164 (Ch. 243) (See Madel 012---Set 169.9) 174 (Ch. 243) (See Madel 012---Set 169.9) 170-9) 74 (Ch. 169.9) 169. 233, 233, 234, 235, 236, 237, 238, 239, 240, 241 (Ch. 231, 242)
234 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012 - Set 169-9)
314 (Ch. 253DX) (See PCB 45-Set 170-1 and Model 114DX-Set 170-9)
314 (Ch. F-243) (See PCB 45-Set 241-1 and Model 114DX-Set 170-9) 322 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012-Set 169-9)
322 (Ch. 253DX) (See PCB 43-Set 170-9)
324 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012 - Set 169-9)
324 (Ch. 253DX) (See PCB 96-Set 241-1 and Model 114DX-Set 170-9)
338 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012 - Set 169-9)
338 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012 - Set 169-9)
338 (Ch. 253DX) (See PCB 45-Set 169-9)
338 (Ch. 253DX) (See PCB 45-Set 169-9) 241-1 and Model U12 — Set 169-9) •338 (Ch. 253DX) (See PCB 45—Set 170-1 and Model 114DX — Set 170-9) •344 (Ch. F-243) (See PCB 96—Set 241-1 and Model 012 — Set 169-9) •354 (Ch. F-243) (See PCB 45—Set 170-1 and Model 012 — Set 241-1 and Model 012 — Set 170-9) •354 (Ch. 253DX) (See PCB 45—Set 170-1 and Model 114DX—Set 170-9) •354 (See PCB 45—Set 170-9) •354 179-1 and Madel 1140X—Set 170-9
 1140X—Set 1 179-1 and Model 114DX-Set 170-9 385 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012 - Set 169-9) 385 (Ch. 253DX) (See PCB 45-Set 170-1 and Model 114DX-Set 170-9 394, 395, 396 (Ch. 263) (See Ch. 263-Set 217-8) 424, 425, 426 (Ch. 253DX) (See PCB 45 -Set 179-1 and Model 114DX-Set 170-9) 426 (Ch. F-243) (See PCB 96-Set 241-1 and Model 012 - Set 169-9) 426 (Ch. 243) (See Model 012-

 ●734, 735, 736, 737 (Ch. 242)

 ■139—7

 ●744, 745 (Ch. 253) (Also see PCB 63

 ●33—Set 197-1)

 ■146—8

 ●777 (Ch. 253) (Also see PCB 63

 ●577 (Ch. 253) (Also see PCB 63

 ●58 (197-1)

 ■646—8

 ●741 (Ch. 253) (Also see PCB 63

 ●541 (Ch. 253) (Also see PCB 63

 ●541 (Ch. 253) (See PCB 63—Set 197-1)

 ■646—8

 ●244 (Ch. 253) (See PCB 63—Set 197-1)

 ■645

 ●171 (Also see PCB 63—Set 197-1)

 ■646—8

 ●244 (Ch. 253) (See Model 014—Set 146-8

 ■646.8 (See Model 231)

 Ch. 7243 (See Model 033)

 Ch. 7243 (See Model 012)

 Ch. 253 (See Model 012)

 Ch. 253 (See Model 114DX)

 ●Ch. 263
 … 217—8

 KAY MUSICAL INSTRUMENT CO. 42-13 KITCHENAIRE 5 Tube Radio KNIGHT (Also see Recorder Listing) 240-4) 246---7 252---7 248--8 40--7 4152, 5A154...12-17 12-15 18 176 20-15 20-15 20-15 20-16 20-17 30-13 SX11L719 SX14L721 SX19L720 4D-450 4G-420 4D-450 4G-420 5A150, 5A152, 5A154.... 5A-190 58-160 58-175, 58-176 5B-185 5C-290 5D-250, 5D-251 5D-455 30-13 50-250, 50-251, 34-9 51-250, 51-251 (Similar to Chassis) 36-25 51-25, 51-520, 53-23 51-525, 51-520, 53-13 51-555, 5520, 53-12 51-550, 5531, 55-12 51-550, 5531, 55-12 51-550, 5531, 55-12 51-550, 5531, 5

77

102

5H-605	17	
	HT—Cont. , 5H-608 (Similar to Chas- 97-15	
	, 5H-608 (Similar to Chas- 97-15 5H-679 (Similar to Chas-	
5H-678 sis) 5H-700	109-7	
6A-122	9–18	
6A-12/ 6A-195	9–19 16–19	
5)-705 5K715 6A-122 6A-127 6A-195 6B-122 9-18 6B-127 9-10	(See Model 6A-122-Set	
68-127 9-19	(See Model 6A-127—Set	
9-19 6C-225 6D-225	30-14 , 6D-226 (See Model 6C-225	
6D-235	54-11	
6D-360 6G-400) (See Model 449-Set 83-5)	
6H-580 6K718	217_9	
78-220 7D-405	39-11	
88-210 8D-340	46-13	
999101		
108-24 11C-30	9	
108-24 11C-30 11D-30 12H-61 14F-49- 15H-60	0 29–12 57–9 0 176–5	
14F-49 15H-60	0, 14F-495, 14F496, 63-12 09 (See Model 511B-Set	
125- 19F492	9) 2, 19F497, 19F498 58-11	
125- 19F492 20H611 93SX32 93-017 93-024 93-103 93-146 93-155	1	
93-017 93-024	31–15 32–13 31–16	
93-103 93-146	31–16 36– 15	
93-146 93-155 93-191 93-320 93-330 93-350 93-360 93-370 93-370 93-380 93-431 96-279 96-326	37–10 38––8	
93-320 93-330	74_5 99_9	
93-350 93-360	76–13 79– 9	
93-370 93-380	75 -10 90 -8	
93-431 96-279	90—8 167–12 160—6	•
96-326 96-354 97-870	160-6 137-5 (Similar to Chossis) 139-15 78-9	1
97-870 449 511B	78—9 83—5 125—9	
LAFA1	FA15Y 15 15	
J62, J6 MC10B MC11 MC12	V, FA15Y	
MC11 MC12	28–18 27–15 15–16	
MC12 MC13 MC16		•
P564 {	Similar to Chassis). 38-5 IN435, IN436 (Similar to	
Chas	(a) 00 K	
IN 549 IN 551	(Similar to Chassis), 121-2 (Similar to Chassis), 38-5 (Similar to Chassis), 38-6	
110354	, INSSS (Similar to Chassis) 55-10	
IN556	, IN557 (Similar to Chassis)	
IN559 IN560	(Similar to Chassis), 109-7	•
IN819 19184	(Cintles to Chantel 60 7	
	(Similar to Chassis). 149-13	
• 1P185	97—8 (Similar to Chassis). 69—7 (Similar to Chassis). 149–13 , 1P186 (Similar to Chassis) 149–13	
178M1 20CP	(Similar to Chassis). 149 -13 , 1P186 (Similar to Chassis) 149 -13 (Similar to Chassis). 149 -13 (Similar to Chassis). 149 -13	
17BM1 20CP 27BM1	149–13 (Similar to Chassis), 149–13 (Similar to Chassis), 149–13 (Similar to Chassis), 149–13	
178M1 20CP 278M1 LAMC	(Similar to Chassis). 149–13 (Similar to Chassis). 149–13 (Similar to Chassis). 149–13 (Similar to Chassis). 149–13	
178M1 20CP 278M1 LAMC	(Similar to Chassis). 149–13 (Similar to Chassis). 149–13 (Similar to Chassis). 149–13 (Similar to Chassis). 149–13	
178M1 20CP 278M1 LAMC 1000 LEAK	149-13 149-13 (Similar to Chassis), 149-13 13 (Similar to Chassis), 149-13 13 (Somilar to Chassis), 149-13 16-20	
178M1 20CP 278M1 LAMC 1000 LEAK	(Similar to Chassis). 149–13 (Similar to Chassis). 149–13 (Similar to Chassis). 149–13 (Similar to Chassis). 149–13	
178M1 20CP 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See	149-13 (Similar to Chassie). 149-13 (Similar to Chassis). 149-13 </td <td></td>	
178M1 20CP 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See	[Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 ::0 162-0	
178M1 20CP 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See	[Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 ::0 162-0	
178M1 20CP 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See	[Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 ::0 162-0	
178M1 20CP 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See	[Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 [Similar to Chassis]. 149-13 ::0 162-0	
178M1 20CP 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See	149-13 (Similar to Chassis). 149-13 (Similar to Chassis). 149-13 (Similar to Chassis). 149-13 :O 16-20	
• 178M1 • 20CP • 278M1 LAMC 1000 LEAK TL/12 RC/PA LEAR (See LEAR/ RM-40 561, 5 563, 5 1281-1 6610P 6614, 6617P Chassi LEE (S	149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Somilar to Chassis), 166-12 (Somilar to Chassis), 6612, 6619 (Somilar to Chassis), 6614, 6619 (Somilar to Chassis), 51-11 See Royal)	
17841 20CP 27841 LAMC 1000 LEAK C/PA LEAR (See LEAR, RM-40 563, 5 1281-1 6610P 6614, 6617P Chassi LEE (Sec LEE T	149-13 (Similar to Chassis). 149-13 (Similar to Chassis). 149-13 (Similar to Chassis). 149-13 :O 16-20	
17841 20CP 27841 LAMC 1000 LEAK C/PA LEAR (See LEAR, RM-40 563, 5 1281-1 6610P 6614, 6617P Chassi LEE (Sec LEE T	149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 :O 16-20	
17841 2000 27841 LAMC 1000 LEAK TL/12 RC/PA LEAR (See LEAR) 8617 8617 6617 Chassi LEE (LEE T AP-10 LEWA	149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 :O 16-20	
• 178M1 • 202P • 278M1 1000 LEAK TL/12 RC/PA LEAR RM-40 6612 Chassi LEE (1 LEE T AP-100 6613A 711.	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :So 16-20	
178M1 20CP 27BM1 1000 LEAK KC/PA LEAR (See LEAR R-40 563, : 563, : 563, : 563, : 563, : 563, : 1281-1 281-1 281-1 (See LEAR Chassi LEE () LEE T AP-100 LEWY 615A Chassi LEE () LEE T AP-100 LEWY 615A Chassi LEE () LEE T AP-100 LEWY 615A Chassi LEE () LEE T AP-100 LEWY 615A Chassi LEE () LEE T AP-100 LEWY 615A Chassi LEE () LEE T AP-100 LEY Chassi Chasi	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :O 16-20	
• 178M1 • 202P • 278M1 EAMC 1000 LEAK RC/PA LEAR RC/PA LEAR RM-40 561, 2 6612 6614 6617 Chassi LEE (LEE T AP-100 615A 711 - 1 LEXIN 6635 LIBER	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :O 16-20	
• 178M1 • 202P • 278M1 EAMC 1000 LEAK RC/PA LEAR RC/PA LEAR RM-40 561, 2 6612 6614 6617 Chassi LEE (LEE T AP-100 615A 711 - 1 LEXIN 6635 LIBER	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :O 16-20	
278M1 20CP 278M1 1000 LEAK C/PA LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR (See (Sea (Sea (Sea (Sea (Sea (Sea (Sea	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :O 16-20	
278M1 20CP 278M1 1000 LEAK C/PA LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR (See (Sea (Sea (Sea (Sea (Sea (Sea (Sea	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :O 16-20	
278M1 20CP 278M1 1000 LEAK C/PA LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR RM-40 (See LEAR (See (Sea (Sea (Sea (Sea (Sea (Sea (Sea	149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 (Similar to Chassia). 149-13 :O 16-20	
278M1 20CP 278M1 1000 LEAK (See LEARC RR-40 (See LEARR RR-40 (See LEARR RR-40 (See LEARR RR-40 (See LEARC RR-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LECC RC-40 (See LECC RC-40 (See SO) (Sea (Sea SO) (Sea (Sea SO) (Sea (Sea (Sea (Sea (Sea (Sea (Sea (Sea	149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 :O 16-20	
278M1 20CP 278M1 1000 LEAK (See LEARC RR-40 (See LEARR RR-40 (See LEARR RR-40 (See LEARR RR-40 (See LEARC RR-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LEACC RC-40 (See LECC RC-40 (See LECC RC-40 (See SO) (Sea (Sea SO) (Sea (Sea SO) (Sea (Sea (Sea (Sea (Sea (Sea (Sea (Sea	149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 (Similar to Chassis), 149-13 :O 16-20	
275841 2005 275841 275841 275841 275841 275841 27584 275841 27584 275854 275854 275854 275855 275855 275855 275855 275	149-13 (Similar to Chassia). 149-13 (Chassia). 166-12 Record Changer Listing) ADIO (2C (Leoravian). 42-15 56581. 566. 567. 568. 9-20 (C (Ch. 78). 564. 49-11 C, 6611PC. 6612PC. 9-21 56581. 566. 567. 568. 9-20 (C (Ch. 78). 51-11 See Royal) TONE 0 16-23 (T 11-13 42-16 NGTON 13-20 RIY A6P. 6K 20-18 210-18805.8 210-18805.8 210-18805.8 210-18805.8 211-25 1805	
275841 2005 275841 275841 275841 275841 275841 27584 275841 27584 275854 275854 275854 275855 275855 275855 275855 275	149-13 (Similar to Chassie). 149-13 (Similar to Chassie). 149-13 (Similar to Chassie). 149-13 16 (Similar to Chassie). 149-13 16 (Similar to Chassie). 149-13 16 16 16 16 16 16 16 16 17 16 18 19 10 10 10 12 14 13 14 14 15 14 15 16 16 16 16 16 17 11 18 18 18 18 18 19 10 11 12 14 15	

INCOLN-Cont. CH753 (FAA-18805-A) 167-7	
C(H753) (FAA-18805-A) 167-7 SH756 (FAG-18805-A) 214-5 SH764 (FDD-18805-A) 347-64 (FDD-18805-B) 246-8 SH1-18805-B 66-11 SH0805-B) 66-11 SH10805-B) 66-11 SH10805-B) 66-11 SH018805-B) 66-11 SH018805-B) 66-11 SH018805-B) 66-11	
SH764 (FDD-18805-A), 4SH766 (FDD-18805-B)	
SEH-18805-B 66-11 'ML080 (SEH-18805-A), 7ML081 (SEH18805-B) 66-11 U 18805-B 66-11	
(5EH18805-B) 66-11 8H-18805 83-4	
SH-18805-A (See Model 8ML882Z— Set 44-7 or 8ML985Z—Set 83-4)	
(5EH18805-B) 66-11 H-18805 83-4 H-18805-A (See Model 8M1882Z- Set 44-7 or 8M1985Z-Set 83-4) L-18805-A (See Model 8ML882- Set 44-7 or 8M1985-Set 83-4) L-18805-B 83-4 H-18805-A) (Cb. 88821 44-7 ISH-18805-A) (Cb. 8821 44-7	
3L-18805-8 83-4 ML882 (8L-18805-A), BML882Z (8H-18805-A) (Ch. 8E82) 44-7 ML985 (8L-18805-A), BML985Z (8L-18805-B), BML985Z (8H- 18805-A), BML985ZE (8H-18805) 83-4	
(8H-18805-A) (Ch. 8E82) 44-7 3ML985 (8L-18805-A), 8ML985E	•
18805-A), 8ML985ZE (8H-18805)	•
S13L-В 2 —10	•
LINCOLN (Allied Radio Corp.)	
5A-110	
LIPAN (See Supreme)	
LULLABY (See Mitchell)	
LYMAN	•
CM10, CM20 44—8 LYRIC (Also see Ravland)	
546T, 546TY, 546TW 7-17	
	•
500, 501 5-40 504 (Bottle Receiver) 22-18 508 (Keg Radio) 38-9	
500, 501 5-40 504 (Bottle Receiver) 22-18 508 (Keg Radio) 38-9 510 52-10 900 38-9	•
MAGNAVOX	•
CP251M (Chassis AMP-128A, B, AMP-129)	•
252M (Chassis CR700 and AMP132) 260-9	1
104 Series (Ch. CT301 thru CT314) 161-4	
108, 108A Series	
2124 Centers Choose 260-9 104 Series C1301 thruc C13141 108, 108A Series 219-6 1088 Series 239-6 1088 Series 240-5 300 Series 263-9 Chasis AMP-101A, AMP-101B 43-12	
Chassis AMP-108A, AMP-108B	•
Chassis AMP-108A, AMP-108B Chassis AMP-111A, B, C. 68-10 Chassis AMP-128A, B .254-7 Chassis AMP-129, .254-7 Chassis AMP-131A, B .249-9 Chassis AMP-131A, B .240-9 Chassis CMUA4038B, CMUA4028B, CMUA4038B, CMUA4028B, CMUA4028B,	
Chassis AMP-129	•
Chassis AMP132	•
CMUA403BB, CMUA404BB, CMUA405BB, CMUA406BB, CMUA405BB, CMUA406BB, CMUA407BB (108B Series)	•
Chossis AMP-131A, B	
Chassis CMUA41388 [1088 Series]	
240-5 Chossis CMUA41888, CMUA41988, CMUA42088 (1088 Series) 240-5	
Chassis CMU422BC (1008 Series) 240-5 Chassis CMU422BC (300 Series) 263-9 Chassis CMU401AA, CMU402AA,	
Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU404AA, CMU405AA, CMU406AA, CMU407AA (108, 108A Series) 239-0	
CMU405AA, CMU406AA, CMU407AA (108, 108A Series) 239-6	
Chassis CMU410AA (108, 108A	1
Series) 239—6 Chassis CMU413AA (108, 108A Series) 239—6 Chassis CMU413AA, CMU419AA,	
Series) 239-6 Chassis CMU418AA, CMU419AA, CMU420AA (108, 108A Series) 239-6 Chassis CP. 188 (1558 Penemer Svm-	
239-6	
239-6 Chassis CR-188 (1558 Regency Symphony) 18-22 Chassis CR 190A, CR 190B, 46-14 Chassis CR-192A, CR-193B 41-11 Chassis CR-192A, CR-193B 41-11 Chassis CR-192A, B, C (Hepple- white, Madern Symphony) 17-20 Chassis CR-199. 63-13	
Chassis CR190A, CR190B. 46-14 Chassis CR-192A, CR-193B 41-11 Chassis CR-197C	
Chassis CR-198A, B, C (Hepple- white, Modern Symphony) 17-20	
CLASSIC CR 2004 R C D E E	
Chasii Ck-200A, B, C, D, 41-12 Chasii Ck-207A, B, C, D, 41-12 Chasii Ck-208A, CR-208B, 43-13 Chasii Ck-208A, CR-208B, 43-13 Chasii Ck-210A, CR-210B, 52-11 Chasii Ck-210A, CR-210B, 53-11 Chasii Ck-210A, CR-210B, CR-200B, CR-200B, CR-200B, CR-200B, CR-200B, CR-200B, CR-200B, CR-200B, CR-200B, Se- CTA403BB, CTA407BB, CR-4007BB, CR-4007	
Chassis CR-208A, CR-208B 43-13 Chassis CR-210A, CR-210B. 52-11 Chassis CR-211A, B	
Chossis CR700	
CTA403BB, CTA404BB, CTA405BB, CTA406BB, CTA407BB (108B Se-	
Chassis CTA410BB (108B Series)	
Chassis CTA413BB (108B Series)	
Chassis CTA418BB, CTA419BB,	
240-5 Chassis CTA41388 (1088 Series) 240-5 Chassis CTA41885, CTA41988, CTA42086 (1088 Series) 240-5 Chassis CT84228C (300 Series) 263-9 Chassis CT-214, CT-218	
Chassis CT-214, CT-218 62-13 Chassis CT-219 CT-220 82-7	
Chassis CT-221 62–13 Chassis CT-222 82–7	
Chassis CT-224	
Chassis CT-235 97A-8 Chassis CT-236 93A-9	
Chassis CT-237, CT-238 (See Set 95A-9 and Ch. CT219—Set 82-7)	
Chassis CT44228C [302 263-07] Series] Chassis CT44228C [302 263-07] Chassis CT-214, CT-218 22-13 Chassis CT-219, CT-220 82-77 Chassis CT-221, CT-220 82-77 Chassis CT-222 92-77 Chassis CT-223 97A-6 Chassis CT-225 97A-6 Chassis CT-235, CT-238 [See Set 95A-9 and Ch-219, CT246 See Set 95A-9	
Chassis CT250, CT251 135-1A Chassis CT252, CT253 95A-9	
Chassis CT257, CT258, CT259, CT260	
Chossis CT244, CT245, CT246, 93A − 9 Chossis CT250, CT231, 135-1A Chossis CT257, CT258, CT259, CT250, CT257, CT258, CT259, CT254, CT254, CT254, CT254, CT255, CT254, CT254, CT254, CT255, CT265, CT265, CT265, CT265, Chossis CT266, CT266, CT267, CT269	
LINUSSIS LIZOD, LIZO/, LIZO/	1

LINCOLN-Cont.	MAGNAVOX-Cont.
2CH753 (FAA-18805-A)167-7 3SH756 (FAG-18805-A)214-5 (SH744 (FDD 18805-A)214-5	
35H756 (FAG-18805-A)214-5 45H764 (FDD-18805-A), 45H766	 Chassis CT-270, CT-271, CT-272, CT-273, CT-274, CT-275, CT-276, CT-277, CT-278, CT-279, CT-280, CT-277, CT-278, CT-279, CT-280,
(FDD-18805-B)	Charle CT292 155 10
5EH-18805-B	
7ML080 (5EH-18805-A), 7ML081 (5EH18805-B)	Chasis C1286 155-10 Chasis C1287 (1288 131-1A Chasis C1287 (1288 131-1A Chasis C1289 155-10 Chasis C1299 155-10 Chasis C1291 (1293 155-10 Chasis C1291 (1293 155-10 Chasis C1297 155-10 Chasis
8H-18805	Chassis CT289
Set 44-7 or 8ML985Z—Set 83-4)	• Chassis CT291, CT293 155-10
Set 44-7 or 8M1985Z—Set 83-4) 8L-18805-A (See Model 8ML882— Set 44-7 or 8M1985—Set 83-4)	• Chassis C1294
8L-18805-8 83-4 8ML882 (8L-18805-A), 8ML882Z (8H-18805-A) (Ch. 8E82) 44-7 8ML985 (8L-18805-A), 8ML985E	 Chassis CT301 thru CT314 . 161—4 Chassis CT331 thru CT349 (105)
(8H-18805-A) (Ch. 8E82) 44-7	
	Series)
18805-A), 8ML985ZE (8H-18805) 83-4	Chassis CT358 (107 Series) 226-4 Chassis CT358AA AB, BA, BB, CB,
LINCOLN	DC (107 Series) (See Ch. CT358
S13L-B 2-10	—Set 226-4) •Chassis CT359AA, AB, BA, BB, CB (107 Series) (See Ch. CT358—Set
LINCOLN (Allied Radio Corp.)	(107 Series) (See Ch. CT358—Set 226-4)
5A-110	 Chassis CT362, CT363 (105L, M
LINDEX CORP. (See Swank)	Chassis CT372, CT373 (105L, M, N
LIPAN (See Supreme)	Series)
LULLABY (See Mitchell)	205-6 • Chassis CT385CB, DC (107 Series)
	(See Ch. CT358-Set 226-4)
LYMAN CM10, CM20 44—8	 (See Ch. CT358—Set 226-4) Chassis CT385AA, AB, BA, BB, CB (107 Series) (See Ch. CT358—
LYRIC (Also see Rauland)	
546T, 546TY, 546TW 7-17	 Chassis C1386AA, AB, BA, BB, CB (107 Series) (See Ch. CT358— Set 226-4)
	Set 226-4) Chassis CUA401BB, CUA402BB,
500, 501 5 -40	• Chassis CUA401BB, CUA402BB, CUA403BB, CUA404BB, CUA405BB, CUA404BB, CUA405BB, CUA406BB,
508 (Keg Kadio) 38-9	CUA40/BB (1088 Series) 240-3
510 52-10	Chassis CUA410BB (108B Series) 240—5
,	Chassis CUA413BB (1088 Series)
MAGNAVOX CP251M (Chassis AMP-128A, B,	Chassis CUA41888 CUA41988.
AMP-129)	CUA420BB (108B Series) 240-5 Chassis CT401AA, CT402AA,
	CT403AA, CT407AA, CT403AA,
• 104 Series (Ch. CT301 thru CT314) 161-4 • 108, 108A Series 239-6	Series)
	Series)
• 300 Series	Chassis CT418AA, CT419AA, CT420AA (108, 108A Series)
Chassis AMP-101A, AMP-101B 43-12	•Chassis CU401AA, CU402AA,
Chassis AMP-108A, AMP-108B 41-10	
Chassis AMP-111A, B, C. 68-10	CU403AA, CU404AA, CU405AA, CU407AA, (108, 108A Series)
Chassis AMP-129	
Chassis AMP-131A, B	Chossis CU413AA (108, 108A
Chassis AMP-131A, 8	•Chassis CU418AA, CU419AA,
CMUA405BB, CMUA406BB,	CU420AA (108, 108A Series)
CHULL 10700 11000 C	239-6
240-5	• Chassis MCT228
	Chassis MCT228
240-5 • Chassis CMUA410BB (108B Series) 240-5 • Chassis CMUA413BB (108B Series)	• Chassis MCT22895A—9
240-5 • Chassis CMUA4108B (108B Series) 240-5 • Chassis CMUA4138B (108B Series) 240-5 • Chassis CMUA4138B, CMUA4138B	• Chassis MCT228
240—5 • Chassis CMUA410BB (108B Series) 240—5 • Chassis CMUA413BB (108B Series) 240—5 • Chassis CMUA413BB, CMUA419BB • Chassis CMUA418BB, CMUA419BB	Chassis MCT228
240-5 • Chassis CMUA4108B (1088 Series) 240-5 • Chassis CMUA4138B (1088 Series) • Chassis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 • Chassis CMU4228C (300 Series)	Chassis MCT228
240-5 • Chassis CMUA4108B (1088 Series) 240-5 • Chassis CMUA4138B (108 Series) 240-5 • Chassis CMUA4188B, CMUA4198B, CMUA4208B (108 Series) 240-5 • Chassis CMU4228C (200 Series) 263-9 • Chassis CMU428C (200 Series) 263-9 • CMU4028C (200 Series) (200 Series)	Chassis MCT228
240-5 • Chossis CMUA410BB (1088 Series) 240-5 • Chossis CMUA413BB (1088 Series) CMUA420BB (108B Series) 240-5 CMU4420BB (108B Series) 240-5 • Chossis CMU422BC (300 Series) • Chossis CMU422BC (300 Series) • Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU404AA, CMU403AA, CMU404AA, CMU403AA, CMU403AA, CMU404AA, CMU403AA, CM	• Chassis MCT228
240-5 Chossis CMUA4108 (1088 Series) 240-5 Chossis CMUA41388 (1088 Series) 240-5 Chossis CMUA41888 CMUA1988, CMUA42088 (1088 Series) 240-5 Chossis CMU4228C (300 Series) 240-5 Chossis CMU4228C (300 Series) 263-9 Chossis CMU403AA, CMU403AA, CMU403AA, CMU403AA, CMU403AA, CMU403AA,	Chassis MCT228
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240-5 Chassis CMUA4108B (1088 Series) 240-5 Chossis CMUA41388 (1088 Series) 240-5 Chossis CMUA41888, CMUA41988, CMUA4208B (1088 Series) 240-5 Chossis CMUA228C (300 Series) 240-5 Chossis CMUA228C (300 Series) 240-5 Chossis CMUA228C (300 Series) 240-5 Chossis CMUA228C (300 Series) CMUA03AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU404AA, CMU403AA, CMU404AA, CMU403AA, CMU404AA, CMU403AA, CMU404AA, CMU403AA, CMU406AA, CMU407AA (108, 108A Series) Chossis CMU410AA (108, 108A Series) Chossis CMU410AA (108, 108A Series) Chossis CR190A, CR190B, 46-14 Chossis CR190A, CR20B, 46-14 Chossis CR200A, B, C, C, E, F Chossis CR200A, B, C, C, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B	Chassis MCT228
240-5 Chassis CMUA4108B (1088 Series) 240-5 Chassis CMUA4138B (1088 Series) 240-5 Chassis CMUA4138B (1088 Series) 240-5 Chassis CMUA428B (1088 Series) 240-5 Chassis CMUA428C (300 Series) 263-9 Chassis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU406AA, CMU403AA, CMU4106A, Series) 239-6 Chassis CMU413AA, CMU419AA, CMU420AA (108, 108A Series) 239-6 Chassis CR192A, CR193B 41-11 Chassis CR197C, 37-11 Chassis CR197C, 37-11 Chassis CR197C, 37-11 Chassis CR197C, 37-11 Chassis CR207A, B, C Heeple- white, Modern Symphony) 17-20 Chassis CR207A, B, C, D, E, F Chassis CR207A, CR208B, CTA4038B, CTA4032B, CTA403	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 240-5 Chossis CMU428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU4106A, Series) 239-6 Chossis CA10418A, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR192A, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR207A, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA405B, CTA4058B, CTA4058B, CTA4038B, CTA405BB, CTA4058B, CTA4058B, CTA4038B, CTA405BB, CTA4058B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4058B, CTA4038B, CTA4058B, CTA4058B	Chassis MCT228
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240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
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240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chossis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chossis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B, CMUA4198B, CMUA4208B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU419AA, CMU400AA (108, 108A Series) 239-6 Chossis CR102A, CR190B, 46-14 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR197C, CR193B 41-11 Chossis CR20AA, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR200A, B, C, D, E, F Chossis CR200A, B, C, D, E, F Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 43-13 Chossis CR200A, CR208B 52-11 Chossis CR200A, CR208B 52-11 Chossis CR201A, B, CB-10 Chossis CR201A, B, CH20B 52-11 Chossis CR201A, CR208B, CTA4058B, CTA4038B, CTA4058B, CTA4058B, CTA4038B, CTA4058B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B (108B Series) 240-5 Chossis CTA4138B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, CTA4198B, Chassis CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA4198B, CTA4138B, CTA4198B, CTA4138B, CTA4198B, Chassis CTA4138B, CTA	Chassis MCT228
240-5 Chossis CMUA4108B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA4138B (1088 Series) 240-5 Chossis CMUA428C (300 Series) 263-9 Chossis CMU401AA, CMU402AA, CMU403AA, CMU402AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU400AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU403AA, CMU406AA, CMU407AA (108, 108A Series) 239-6 Chossis CMU413AA, CMU419AA, CMU420AA (108, 108A Series) 239-6 Chossis CR102A, CR193B 41-11 Chossis CR192A, CR193B 41-11 Chossis CR192A, CR193B 41-11 Chossis CR20AA, CR208B 43-13 Chossis CR20A, B, C (Hepple- white, Modern Symphony) 17-20 Chossis CR20A, B, C, D, E, F Chossis CR20A, CR208B 43-13 Chossis CR20A, B, C, D, E, F Chossis CR404BB, CTA4058B, CTA403BB, CTA405BB, CTA4058B, CF Chossis CTA413BB (108B Series) 240-5 Chossis CTA413BB (108B Series) 240-5 Chossis CTA413BB (108B Series)	Chossis MCT228

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20783 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 20785 (20785, 20787, 20785, 20786, 20787, 153-8 and PCB 43—Set 177-1)
 20781 (Series 108) (See Model 70 —Set 153-8 and PCB 43—Set 177-1)
 20782 (Series 108) (See Model 70 —Set 153-8 and PCB 43—Set 177-1)
 20782 (20783, 20784 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 2050, 21031 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 2050, 21031 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 2050, 21031 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 2050, 21031 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 20782, 21787 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 20782, 21787 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 20782, 21783 (Series 108-1) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 21760, 21721 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 21720, 21721 (Series 108) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 221 Thru 35 (Series 106-5) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 21720, 21721 (Series 106) (Alto see PCB 43—Set 177-1)
 221 Thru 35 (Series 106-5) (See Model 70—Set 153-8 and PCB 43—Set 177-1)
 21720, 121, 1218 (Ch. 99) (Alto see PCB 43—Set 177-1)
 2124, 73 (See CB 37—Set 166-2 and Model 170A—Set 127-7)
 143 (See PCB 33—Set 177-7)
 144, 1418 (Ch. 100), 1417 (Ch. 101), 142, 1428 (Ch. 100), 1410 (See Model 1724—Set 108-7)
 1450, 600, 122, 203, 804 (Series 106), 160, 160, 162, 162, 163, 177-7)
 143 (See Model 1224—Set 177-7)
 144, 1414 (See Model 1224—Set 177-7)
 1450, 600, 122, 203, 804 (Series 177-7)
 1460, 1605, 162, 163-87-71
 147, 143 (See Model 1224—Set 177-7)
 1480, 600, 122, 203,

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MAJESTIC-MOTOROLA

	MAJESTIC-MOTOROLA
	MOPAR-Cont. 820 (D-5207)
	820 (D-5207)
	202.31
	829
	MOTOROLA (Also see
	Record Changer Listing) AR-96-23 (M-5) 11-16 BKO-A (See Ch. 10A—Set 106-10) BK2A (Ch. 2A and P6-2 or P8-2)
	BKO-A (See Ch. 10A—Set 106-10) BK2A (Ch. 2A and P6-2 or P8-2)
	BK2M (Ch. 2M ond P6-2 or P8-2) 197-7
	BK3A6 (Ch. R-15A6 and P6-2 or
	BK-6 10-23 BK8, X (See Ch. 8A-Set 46-16)
	BK53A6 (Lh. R1/A6 and P6-2 or P8-2)
	CR-76
1	P8-2) 256-10 BK-6 10-23 BK8, X (See Ch. 8A-Set 46-16) BK53A6 (Ch. R17A6 and P6-2 or P8-2) CR-6 263-13 CR-6 25-21 CTA3 230-72 CTM3 230-72 CTM3 235-9 CTI (See Model CT-9-Set 82-8) CTI (See Ch. 1A-Set 134-8) CTIM 143-11 CTA6 (Ch. R-15A6 and P6-2 or P8-2) CT2A6 (Ch. R-15A6 and P6-2 or P6-2)
	CT1M
	C12A6 (Ch. 2A Gud Pol - 197-7 C12A6 (Ch. R-15A6 and P6-2 or P8-2) C12M (Ch. 2M and P6-2 or P8-2)
	P8-2)
	P8-2)
	CT8-A (See Ch. 10A—Set 106-10)
	FD-6 7-20 FD7 (See Model FD-6-Set 7-20)
	CT9 82-6 FD-6 7-20 FD7 (See Model FD-6-Set 7-20) FD8 (See Ch. 8A-Set 46-16) GMOT (See Ch. 10A-Set 106-10) GMT2A (Ch. 2A and P6-2 or P8-2) 197-7
	GMT2A (Lh. 2A dna Po-2 of Po-2) 97-7 GMT2M (Ch. 2M and P6-2 or P8-2) 197-7 GMT3A6 (Ch. R-15A6 and P6-2 or P8-2) GMT3A6 (Ch. R17A6 and P6-2 or
	GMT3A6 (Ch. R-15A6 and P6-2 or
	CHOT & IS-+ Ch 104 Set 160.
	10) HJ2A (Ch. 2A and P6-2 or P8-2) HJ2M (Ch. 2M and P6-2 or P8-2) HJ2M (Ch. 2M and P6-2 or P8-2) 197-7
	HJ2M (Ch. 2M and P6-2 or P8-2)
	HJ2M (Ch. 2M and P6-2 or P8-2) 197
	HNZAG (Ch. K-ISAG and PO-2 of
1	P8-2)
	HNIZAA (Ch. P.15A6 and PA.2 or
	P8-2)
	HN8, HN9 (See Ch. 8A—Set 40-16) HT3A6 (Ch. R-15A6 and P6-2 or PR-2) 256-10
	HN8, HN9 (See Ch. 8.4—Set 46-16) HT3A6 (Ch. R-15A6 and P6-2 or P8-2)
	IL2T2 (See Ch. 1A—Set 134-8) KR1 (See Ch. 1A—Set 134-8)
	KR1 (See Ch. 1A—Set 134-8) KR2A (Ch. 2A and P6-2 or P8-2) 197-7 KR2M (Ch. 2M and P6-2 or P8-2) 197-7
1	KKJAG (U.N. K-IDAG and ro-2 or
	P8-2)
	NHIC NH2AC (See Nash Model AC-152-
	216-6) 9-24 NH6 9-24 NH8 (See Ch. 8A-Set 46-16) OEO (See Ch. 10A-Set 106-10) OE2 (See Ch. 8A-Set 46-16) OE24 (Ch. 2A and P6-2 or P8-2) 07-7
	OEO (See Ch. 10A-Set 106-10) OE2 (See Ch. 8A-Set 46-16)
	OE2A (Ch. 2A and P6-2 or P8-2) 197-7
	OE2A (Ch. 2A ond P6-2 or P8-2) 197-7 OE2A6 (Ch. R-15A6 and P6-2 or P8-2) OE2M (Ch. 2M and P6-2 or P8-2) 0E2M (Ch. 2M and P6-2 or P8-2) 197-7 OFA 8-21
	OE6
	197_7 OE6 8-21 OE8, OE9 (See Ch. 8A—Set 46-16) PCO (See Ch. 10A—Set 106-16) PC2 (See Ch. 10A—Set 106-16) PC2A (Ch. 2A and P6-2 or P8-2) 197_7 PC2A6 (Ch. R-15A6 and P6-2 or P8-2) 256-10
	PC2A (Ch. 2A and P6-2 or P8-2) 197-7
	PC2A6 (Ch. R-15A6 and P6-2 or P8-2)
	PC2M (Ch. 2M and P6-2 or P8-2) 197-7 PC6 8-21
	PC6 8-21 PC8, PC9 (See Ch. 8A—Set 46-16) PC9-A (See Ch. 10A—Set 106-10)
	PD2A (Ch. 2A and Po-2 or P8-2)
	197-7 PC6 8-21 PC8, PC9 (See Ch. 8A-Set 46-16) PC9-A (See Ch. 10A-Set 106-10) PD2A (Ch. 2A and P6-2 or P8-2) 197-7 PD3A6 (Ch. R-15A6 and P6-2 or P8-2) PD2M (Ch. 2M and P6-2 or P8-2) PD2M (Ch. 2M and P6-2 or P8-2) 197-7 SROB (Ch. OB) 105-7
	1977 SROB (Ch. OB) 1057 SR1B (See Ch. 18Set 136-11) 5824 (Ch. 2A and P6-2 or P8-2) SR2A (Ch. 2A and P6-2 or P8-2) 1077
1	SR1B (See Ch. 18—Set 130-11) SR2A (Ch. 2A and P6-2 or P8-2)
	SR2A6 (Ch. R-15A6 and P6-2 or
	SR2M (Ch. 2M and P6-2 or P8-2)
1	SR3A6 (Ch. R-15A6 and P6-2 or P8-2) 256-10 SR6, SR8, SR9 (See Ch. 8A—Set 46-16) 364
	SR9A (See Ch 10A-Set 106-10)
	SR52A6 (Ch. R17A6 and P6-2 or P8-2)
	SR52A6 (Ch. R17A6 and P6-2 or P8-2)
	ter Televisien Persiver

	1 MARCO Com
MAJESTIC-Cont. Ch. 12B26E (See Model 12FM475) Ch. 12C22E (See Model 12FM895)	MASCO-Cont. ME-27 155-11 ME-36, ME-36R 1547 ME-32 1497 MHP-110 1137 MHP-110X 1137 Midgetalk 1157 MM-27P 16-23 MSD-16 1505 MU-5 1176 MU-17 1856 PR-1 2186 PK-5 (Early) 33-11 RK-5, RK-5L, RK-5M,
Ch. 18C90, 18C91 [See Model	ME-36, ME-36R
7TV850) Ch. 4501 (See Model 5A410) Ch. 4504 (See Model 5A430) Ch. 4702 (See Model 5A445) Ch. 4702, 4703 (See Model 75433) Ch. 4705 (See Model 774420) Ch. 4706 (See Model 77442) Ch. 4707 (See Model 77478) Ch. 4708 (See Model 7778) Ch. 4810 (See Model 71/K7778) Ch. 4810 (See Model 81/855)	MHP-110
Ch. 4506 (See Model 5A450) Ch. 4506 (See Model 5A445) Ch. 4702 4703 (See Model 75433)	MM-27P 153-9 MPA-3 MPT-4 16-25
Ch. 4705 (See Model 7P420) Ch. 4706 (See Model 7C432)	MSD-16 150-9 MU-5 117-6
Ch. 4707 (See Model 7C447) Ch. 4708R (See Model 7JK777R)	MU-17
Ch. 4810 (See Model 85452) Ch. 4810B (See Model 8JL885)	PK-5 (Early)
Ch. 4810B (See Model 8J1885) Ch. 41201 (See Model 12FM475) Series 106 (See Model 70—Set	PK-5 [Early] 33-11 RK-5, RK-5L, RK.5M, RK-5M, RK.5SL 168-11 RK-5SLR 1779 RK6, RK6R 244-7 T-16 1238 T0-16 1208 TP-16A 30-17 TWB (TV Booter) 2548 WF-1A 2098 76, 711 20-20 86, 811 20-21
153-8) Series 106-5 (See PCB 43—Set 177-1 and Model 70—Set 153-8)	RK6, RK6R
Series 109 109 5 /See BCB 43-Set	TD-16
177-1 and Model 70-Set 153-8) CUA420BB (108B Series) 240-5 Series 109 (See Model 20FP88- Set 170-10)	WF-1A
Set 170-10) • Series 110, 111 (See Model 21P62	86, 811 20-21
—Set 221-7) •Series 112, 112-2, 113233—4	MASON
MALLORY	45-1A
TV-101 (Below Serial No. 200,000) Tel. UHF Conv	MATTISON
Tel, UHF Conv	 630DXM (Series 26000)243—7 630DXM (Series 27000) (See PCB 105 — Set 252-1 and Model 630DXM—Set 243-7)
MANTOLA (B. F. Goodrich Co.)	105 - Set 252-1 and Model 630DXM-Set 243-7)
R630-RP	630MDXL (Series 26000)243—7 630MDXL (Series 27000) (See P⊡B 105 — Set 252-1 and Model 630MDXL 243-7
4-29) R643W	
R652, R652N 9-22 R654 PM, R654-PV 3-5 R655W (Ch. No. 501 APH) 8 20	•630-6A 218-7 •630-6AB 218-7
4.29 8643W 4-29 8652, R652N 9-22 8654 PM, R654-PV 3-3 R654, R662N 8-20 R662, R664PV, R664-W 23-13 R743.W (See Model 3643W—Set 4.29	MAYFAIR 510, 510W, 520, 520W, 530,
R-743-W (See Model 3643W—Set 4-29)	510, 510W, 520, 520W, 530, 530W 25-20 550, 550W 24-22
R-7543 18-23 R-75143 39-12 R-75152 38-10 R-75343 39-12	McGOHAN (Don)
R-75152	MG-7 195—7 MG-10B 190—8 MG-18B 191—6 MG-20-B 189—5 MG-30-B 188—9 MG60 260–10 WA-312 227—9
K-76143 (See Model 2480-Set 25- 17)	MG-188
R-76162 40-10 R76262 (Fact. No. 7160-17) 51-12 R-78162 43-11 2486 25-17	MG-30-B
2486	McGRADE
4-29) 92-503, 92-504 (See Model R654PM	M-100 16-27
	McINTOSH 257-8
k-78162 43-11 2486 25-17 92:502 (See Model R643W-Set 4.29) 92:503, 92:504 (See Model R654PM -Set 3.5) 92:505, 92:506 (See Model 664PM -Set 23-13) 92:520, 92:521, 92:522 68-11 92:529 150-8	A-116
92-529	MECK (Trail Blazer-Plymouth)
MARKEL (See Record Changer Listing)	CD-500 (PX-5CS-EW-19) 33-12 CE-500 (5CS-P12) 34-10
MARK SIMPSON (See Masco)	CM-500 (5D7-W18) 34-11 CR-500 38-11
MASCO (Also see Recorder Listing)	CW-500
	EC720
ACS, ACS-6	EV-760
CM-20 218-6 EMM-6 216-3	JM717C (Ch. 9032) 186-9 JM717C (Ch. 9040)
AC-12, AC-24 222-7 ACL 222-7 ACS, ACS-6 222-7 CM-10 255-8 CM-20 218-6 BMM-6 216-3 JMA-5 41-13 JMA-5 31-17 JM-5 (Master Station), JR (Sub-Station) 42-18	• JM717CU (Ch. 9021) 148-E1 • JM717T (Ch. 9021) 148-T1
JMR 31-17 JM-5 (Master Station), JR (Sub-	• JM717T (Ch. 9032)
JM-10	• JM/1/10 (Ch. 9021)148-11
IMP-0	• JM/20C, CU (Ch. 9021) 148-11
MA-8N 119_8	■JM720C, CU (Ch. 9021)148-11 ■JM720C (Ch. 9032)186-9 ■JM720T (Ch. 9021)148-17 ■IM720T (Ch. 9032) 186-9
MA-8N 119—8 MA-10HF 112—4 MA-10EX 113—4	■JM/20C, CU (Ch. 9021)148-11 ■JM/20C (Ch. 9032)186-9 ■JM/20T (Ch. 9032)148-11 ■JM/20T (Ch. 9032)148-11 ■JM/20TU (Ch. 9032)148-11 ■M/20TU (Ch. 9032)186-9
MA-BN 119—8 MA-10HF 112—4 MA-10EX 113—4 MA-12HF 51-13 MA-17 14-32	MM 20C, CU (Ch. 9021). 186-1 IM 220C (Ch. 9022). 186-9 IM 20T (Ch. 9021). 148-1 IM 20T (Ch. 9021). 148-1 IM 20T (Ch. 9022). 186-9 IM 20TU (Ch. 9022). 186-9 IM 721C, CD (Ch. 9022). 186-9 IM 721C, D (Ch. 9040). 220-4 Mm 510T, MM 512C, MM 516C, MM
MA-BN 119-8 MA-10HF 112-4 MA-10EX 113-4 MA-12HF 51-13 MA-17 MA-17 14-32 MA-17N 50-11 MA-17P 14-32	■ Mx 20C, CU (Ch. 9021). 188-1 ■ Mx 20C (Ch. 9021). 188-9 ■ Mx 20T (Ch. 9021). 188-9 ■ Mx 20T (Ch. 9021). 188-9 ■ Mx 20TU (Ch. 9022). 186-9 ■ Mx 20TU (Ch. 9022). 186-9 ■ Mx 20C, CD (Ch. 9040). 220-4 ■ Mm 516T, MM 512C, MM 516C, MM 516T ■ 110-9 ■ Mm 614C, T (Ch. 9018) (Aiv. 189
MA.9N 119-9 MA.10HF 112-4 MA.10EK 113-4 MA.10EK 51-13 MA.17 51-13 MA.17 50-11 MA.17P 50-11 MA.17P 50-11 MA.17P 50-21 MA.77PN 50-21 MA.20HF 28-21	MECK (Trail Blazer-Plymouth) CD-500 (PX-5CS-EW-19) 33-12 CE-500 (SCS-Pl2) 34-10 CM-500 (SCS-Pl2) 34-11 CR-500 (SD-7V18) 34-11 CW-500 (SD-7V18) 34-11 CW-500 (SD-7V18) 34-11 CW-500 (SD-7V18) 81-11 CW-500 (SD-7V18) 81-13 DA601, D86021 (S1-16, 10003) 87-8 EV-760 (CA-9021) (SD-902) 148-11 JM717C (Ch, 9021) (AS-18 148-11 JM717T (Ch, 9021) (AS-18 148-11 JM717T (Ch, 9021) (AS-18 148-11 JM720T (Ch, 9021)
MA-9N 119-5 MA-10HF 112-4 MA-10EK 113-4 MA-10EK 51-13 MA-17N 50-11 MA-17N 50-11 MA-17PN 50-11 MA-20HF 28-21 MA-17PN 50-11 MA-20HF 28-21 MA-25EK 60-15 MA-25EH 54-13	 IM 20C, CU (Ch. 9021). 188-1 IM 220C (Ch. 9022). 186-9 IM 220T (Ch. 9021). 148-1 IM 220T (Ch. 9021). 148-1 IM 221C, CD (Ch. 9022). 186-9 IM 221C, CD (Ch. 9022). 186-9 IM 21C, CD (Ch. 9022). 186-9 IM 21C, CD (Ch. 9021). 117-88 IM 21C, CL (Ch. 9018). (Also 386)
MA.3N. 119-5 MA.10HF 112-4 MA.10EK 113-4 MA.10EK 51-13 MA.10EK 51-13 MA.17N 50-11 MA.17P 14-32 MA.17P 50-11 MA.20HF 28-21 MA.25EK 60-13 MA.25EK 60-14 MA.25HF 54-13 MA.25HF 54-13 MA.25NR 49-14	 IM /20C, CU (Ch. 9021). 188-1 IM /20C (Ch. 9022). 186-9 IM /20T (Ch. 9021). 188-1 IM /20T (Ch. 9021). 188-9 IM /20T (Ch. 9021). 188-1 IM /20T (Ch. 9021). 188-1 IM /20T (Ch. 9021). 220-4 IM /21C, CO (Ch. 9030). 220-4 IM /21C, T (Ch. 9018). (Also see PCB 12-Set 120-1)117-8 IM /21C, T (Ch. 9018). (Also see PCB 12-Set 120-1)117-8 IM /21C, T (Ch. 9032). (See Modul. IM /21C-Set 186-9). IM /21C, Ch. 9040). 220-4 IM /21C (Ch. 9048). (Also see PCB
MA 3N 119-5 MA 10HF 112-4 MA 10HF 112-4 MA 10HF 112-4 MA 10EK 113-4 MA 12HF 51-13 MA 17N 50-11 MA 17P 14-32 MA 17PN 50-11 MA 20HF 28-21 MA 25EK 60-15 MA 25HF 54-13 MA 25NR 43-14 MA 25NR 43-12 MA 25NR 49-12 MA 25PN (See Model MA 25-Set	 IM /20C, CU (Ch. 9021). 186-9 IM /20C (Ch. 9022). 186-9 IM /20T (Ch. 9021). 186-9 IM /20T (Ch. 9021). 186-9 IM /20T (Ch. 9022). 186-9 IM /21C, CD (Ch. 9022). 186-9 IM /21C, CD (Ch. 9021). 186-9 IM /21C, CD (Ch. 9021). 186-9 IM /21C, CD (Ch. 9012). 117-8 IM /21C, CD (Ch. 9018) (Also see PCB 12-Set 120-1). 117-8 IM /21C, T (Ch. 9018) (Also see PCB 12-Set 120-1. 117-8 IM /21C, CI (Ch. 9018) (Also see PCB 12-Set 120-1. 117-8 IM /21C, CL (Ch. 9022) (See Model JM /17C-Set 186-9 IM /21C (Ch. 9018) (Also see PCB 12-Set 120-1. 117-8 IM /21C (Ch. 9018) (Also see PCB 12-Set 120-1. 117-8
JMR 31-17 JM-5 (Matter Station), JR (Sub- Station) 42-18 JM-10 187-8 JM-10 147-7 JMP-6 147-7 147-7 JM-10 JMP-12 147-7 MA-10H 112-4 MA-10HF 112-4 MA-10HF 112-4 MA-10HF 112-4 MA-10HF 112-4 MA-10HF 12-43 MA-10HF 12-43 MA-17PN 50-11 MA-20HF 28-21 MA-25H 50-11 MA-25H 50-11 MA-25HF 54-13 MA-25H 16-24 MA-25NR 43-14 34-12 14-32 MA-25NR 43-14 34-12 34-12 MA-35NR 16-24 MA-25NR 43-14 MA-35NR 16-25 54 34-12 MA-35NR 16-25 54 34-14 MA-35 21-20 35 34-20	 MM616C, T (Ch. 9018) (Also see PCB 12–Set 120-1117–8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM617T (Ch. 9040)220–4 MM617T (Ch. 9043) (Also see PCB 12–Set 120-1)117–8 MM-617C (Ch. 9032) (See Model JM-717C—Set 186-9) MM-617C (Ch. 9032) (See Model JM-717C—Set 186-9)
MA.BN 119-8 MA.BN 119-8 MA.IOHF 113-4 MA.IOHF 13-4 MA.12HF 51-13 MA.77 14-32 MA.77 50-11 MA.77 50-11 MA.77 50-11 MA.77 50-11 MA.77 50-11 MA.25 16-24 MA.25N 43-14 MA.25N 43-14 MA.25N 43-14 MA.25N 43-14 MA.25N 43-14 MA.25N 16-24 MA.25N 16-24 MA.35N 21-20 MA.35N 44-11 MA.35N 44-11 MA.35N 21-20 MA.35N 30-16	MM616C, T (Ch. 9018) (Also see PCB 12–Set 120-1117–8 MM617C, T (Ch. 9032) (See Model JM717C–Set 186-9) MM617T (Ch. 9040)220–4 MM619C (Ch. 9018) (Also see PCB 12–Set 120-1)117–8 MM-620C, T (Ch. 9032) (See Model JM-717C–Set 186-9) MM621C (Ch. 9040)220–4 MM621PT, RPTB (Ch. 9040)
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	 MM616C, T (Ch. 9018) (Also see PCB 12—Set 120-1117—8 MM617C, T (Ch. 9032) (See Model JM717C—Set 186-9) MM619C (Ch. 9018) (Also see PCB 12—Set 120-1)117—8 MM-620C, T (Ch. 9032) (See Model JM-717C—Set 186-9) MM621C (Ch. 9040)220—4 MM621C (Ch. 9043) (See Model JM-617C, T (Ch. 9023) (See Model MM621C (Ch. 9043) (See Model MM621C (Ch. 9043) (See Model MM62C, T (Ch. 9023) (See Model M616C, T (Ch. 9023) (See Model
MA-35N	MM616C, T (Ch. 9018) (Also see PCB 12–Set 120-1117–8 MM617C, T (Ch. 9032) (See Model JM717C–Set 186-9) MM617T (Ch. 9040)220–4 MM619C (Ch. 9018) (Also see PCB 12–Set 120-1)117–8 MM-620C, T (Ch. 9032) (See Model JM-717C–Set 186-9) MM621C (Ch. 9040)220–4 MM621PT, RPTB (Ch. 9040)

	MECK-Cont.
155-11	
154-7	• XT-785 • XX900 • XX900 • XX910 • XX900
	4C7 35-14 5A7-P11, 5A7-PB11 31-18
	• XX900 110-9 4C7 35-14 5A7-P11, 5A7-P811 31-18 5D7/WL18 21-22 6A6-W4 16-26 • 514C I (Cb. 9018) (Spe. Model
116-7	507/W118 21-22 6AC-W4 16-26 514C, T (Ch. 9018) (See Madel MM614C-Set 117-8 and PCB 12Set 120-1) 614C, 614T1 (Ch. 9022) (See Madel JM717C-Set 148-11) 616C, 617T1 (Ch. 9018) (See Madel JM717C-Set 148-11) 6167C, 617T1 (Ch. 9022) (See Madel JM717C-Set 148-11) 6197C, 7 (Ch. 9018) (See Madel JM717C-Set 120-11 9030 9030 228-11
16-25	MM614C-Set 117-8 and PCB
150-9	12-Set 120-1)
	•614C, 614TL (Ch. 9022) (See Model
	•616C. T (Ch. 9018) (See Model
	MM614C-Set 117-8 and PCB
K-SML, RK-	12-Set 120-1)
K-5ML, RK- 168-11 177-9	JM717C-Set 148-111
	•619C, T (Ch. 9018) (See Model
	MM614C-Set 117-8 and PCB 12
30-17	9030
	Ch. 9018 (See Model MM614C)
209-8	Ch. 9021 (See Model JM717C)
20-21	Ch. 9023 (See Model MoloT)
	Ch. 9032 (See Model JM717C)
	9030 228-11 Ch. 9018 [See Model MM614C] Ch. 9018 [See Model JM717C] Ch. 9022 [See Model 614C] Ch. 9023 [See Model M6167] Ch. 9032 [See Model JM717C] Ch. 9040 [See Model JM717C]
5.4 45.5	MEDCO (See Telesonic)
14-18 5-4, 45-5 t 14-18)	MEISSNER
	•TV-1 (Ch. 24TV)
	4E
(See PCB	5A (See Maguire Model 571—Set 44-10)
nd Model	6H (See Maguire Model 661-Set
243_7	12-18)
)243—7) (See PCB	8BT
nd Model	9AJ
218.7	9-1065
	9-1091A, 9-1091B
	9-1093 55-13 9-1160 257-9
0W 520	
0W, 530, 25-20 24-22	16A
25 -20 24 -22	574 (See Maguire Model 571—Set 44.10)
	44-10)
195-7	661 (See Maguire Model 661—Set 12-18) 2961 Series
190-8	2961 Series 27-19
191-6	ME2CURY (Automobile)
189-5	FA8-18805-A
195-7 190-8 191-6 189-5 188-9 260-10 227-9	FAF-18805-A
	FDC-18805-A
	GM891 (OM-18805-A) [See PCB 105—Set 252-1 and Ford Model
16-27	GF890 (OA-18805-B) - Set
	109-5]
	1CM747-1 (1M-18805) (See Ford
231-10	Model 1CF743-Set 133-7}
257—8 231-10 252-10	107-3) OM-18805-A (See Model GM891) 1CM747-1 (1M-18805) (See Ford Model 1CF743-Set 133-7) 1CM747-1 (1M-18805)158-5 1M-18805 (See Model 1CM747 or 1CM747 1
	1CM747-1)
lymouth)	IM-18805 (See Model ICM/47 or ICM/47.1) 2CM752 (FAF.18805-A) 167—7 3SM757 (FAF.18805-A) 214—5 4SM767 (FDC-18805-A) 246—8 6MM790 (59A-18805) .62—12 8MM890 (Ch. 8E90) (84–18805) 9 13 40
33-12 34-10	35M757 (FAF-18805-A)214-5
34-10 34-11 38-11	45M/0/ (FUC-18805-A) 246-8 6MM790 (594-18805-A1) 62-12
38-11	6MM790-E (59AF-18805) 62-12
48-13	8MM890 (Ch. 8E90) (8M-18805-B)
48-13 81-10	49-13 8MM990 (8M-18805-8) 69-10 8MM991 (8M-18805-8), 8MM991-E, (8M-188051) 83-4
85-8	8MM991 (8M-18805-B) 09-10 8MM991 (8M-18805-B) 8MM991-F
148-11	8M-18805-B (See Model 8MM890 or 8MM890 or 8MM991)
	8MM990 ar 8MM991) 59AF-18805
	59AF-18805 62–12 59A-18805-A1 62–12
	MEDCUDY (Desifie Moneyers)
	@2013 (Ch. 150-2) (Also see PCB
	57-Set 191-1)
148-11 186-9	2013 (Ch. 150-2) (Also see PCB 57—Set 191-1)
	172-6)
186-9	•2081 (Ch. 150-4 and Radio Ch.
186 —9 148 –11	•2113, 2115 (Ch. 150-11 -81) (Also
	see PCB 57-Set 191-1) .172-6
516C, MM	• 2116, 2117 (Ch. 150-8) (See PCB
516C, MM	-Set 172-6)
(Also see 117-8	@2181 {Ch. 150-31, -61 and Radio
	Ch. 155)
(Also see 	•2224 (Ch. 200-11) 216-8
See Model	•2284 (Ch. 200-11)
	PCB 57-Set 191-11 172-4
220-4 so see PCB	•2424 (Ch. 201-34)
See Model	@ 2701 (Ch. 201-553, Audio Amp. Ch. 159-1 and Padia Ch. 160-11
	254-9
	•4120 (Ch. 150-2) (Also see PCB
220-4	•4220 (Ch. 150) (Also see PCB 57
See Model	-Set 191-1) 172-6
See Model	•4317 (Ch. 150-9)
	Set 191-1 and Model 2013—Set 172-0 2081 (Ch. 150-4 and Radia Ch. 199-11 2113, 2115 (Ch. 150-11, 1172-6 ree PCB 57—Set 191-1) 172-6 27—Set 191-1 and Model 2013 —Set 172-6) 2116, 2117 (Ch. 150-6) (See CCB 57—Set 191-1 and Model 2013 —Set 172-6) 2181 (Ch. 150-3), -61 and Radia (Ch. 155)
21-19	•4421 (Ch. 150-81) (See Model 2013
21-19	 T2-6 and PCB 57—Set 10:5: 172-6 and PCB 57—Set 19:5: 172-6 and PCB 57—Set 10:5: 150-2 (see Model 2081) Ch. 150-4 (see Model 2081) Ch. 150-9 (see Model 4317) Ch. 150-9 (see Model 4317) Ch. 150-11 (see Model 4317) Ch. 150-12 (see Model 4317) Ch. 150-12 (see Model 4317) Ch. 150-13 (see Model 2181) Ch. 150-31 (see Model 2181) Ch. 150-31 (see Model 2181) Ch. 150-61 (see Model 2181) Ch. 150-61 (see Model 2181) Ch. 150-11 (see Model 2181) Ch. 150-11 (see Model 2181) Ch. 150-11 (see Model 2171) Ch. 200-11 (see Model 2701) Ch. 201-134 (see Model 2424) Ch. 201-533 (see Model 2701)
31–18 101–4 61–16	Ch. 150-2 (See Model 2013)
61-15	Ch. 150-4 (See Model 2081)
701 — Set	Ch. 150-9 (See Model 4317)
101 5	Ch. 150-11 (Se Model 2113)
1015 7614 1015	Ch. 150-12 (See Model 4317) Ch. 150-15 (See Model 4320)
101-5	Ch. 150-31 (See Model 2181)
101-5	Ch. 150-51 (See Model 2401)
101-5 110-9 101-5 110-9	Ch. 150-61 (See Model 2181) Ch. 150-81 (See Model 2113)
101-5	Ch. 155 (See Model 2081)
101-5 110-9 101-5 101-5 101-5 101-5 101-5 110-9 101-5 110-9	Ch. 159-1 (Se Model 2701)
	Ch. 200-11 (See Model 2217)
110-5	Ch. 201-34 (See Model 2424)
PCB 12	Ch. 201-553 (See Model 2701)
and PCB	м6в 2–30
	MIDWEST
	P6, PB-6
110—9 101—3 110—9	R-12, RG-12, RT-12 [Ch. RGL-12]
	hange Bulletin Nos. 1 Through 63 Are Al
Production C	

ont:	
	MIDWEST-Cont.
101—5 110—9 35 14	R-12, RG-12, RT-12 (Ch. RGT-12)
35–14 5A7-PB11 31–18	44-13 R-16, RG-16, RT-16 (Ch. RGT-16) 45-16
	st.16 kG-16 kG-16 st.16 kG-16 st.16 st.17 st.16 st.16 st.17 st.16 st.16 st.17 st.16 st.16 st.12 st.16 st.16 st.12 st.17 st.17 st.12 st.17 st.17 st.12 st.17 st.17
21-22 16-26 (Ch. 9018) (See Model -Set 117-8 and PCB 120-1) 11 (Ch. 9022) (See Model -Set 148-11) (Ch. 9018) (See Model 120-1) 120-1) 120-1) 120-1) 120-1) 120-1) (Ch. 9018) (See Model -Set 148-11) (Ch. 9018) (See Model -Set 117-8 and PCB 120-1) 228-11	\$-12, SG-12, ST-12 (Ch. SGT-12)
(Ch. 9018) (See Model	21-13 5-16, SG-16, ST-16 (Ch. SGT-16)
120-1)	5.16, SG.16, S1.16 (Ch. SG1-10) 21-24 TM-8 (Ch. STM-8) 716, A (See Model S-16—Set 21- 24) Ch. KD 14
TL (Ch. 9022) (See Model	TM-8 (Ch. STM-8) 15-19
(Ch. 9018) (See Model	24)
-Set 117-8 and PCB	Ch. KD-16
TL (Ch. 9022) (See Model	
-Set 148-11)	MILWAUKEE ERWOOD (See Record Changer Listing)
-Set 117-8 and PCB 12	
20-1)	MINERVA
	L-702
(See Model JM717C) (See Model 614C) (See Model M616T) (See Model JM717C) (See Model JM717C)	W-117, Tropic Master 6-17
(See Model MoloT)	W-117-3 11-14 W-702B 12-20
(See Model JM717C)	W710, W710A (W119) 5-25 W-728 11-15
	410, 411 41–13
See Telesonic)	L-728 11-15 W-117, Topic Master 6-17 W-117, 1 Topic Master 11-14 W-702 W-710A (W119) 5-25 W-703 W-710A (W119) 11-15 410, 411 41-14 729 (Portapol) 23-14
R	
24TV)	MIRRORTONE (Also see Meck) A.17C, T (Ch. 9040)
Maguire Model 571—Set	A-17C, 1 (Ch. 9040)
Aaguire Model 661—Set	216-4
	•14MTS
161—5 37-12 123—9 3-15	• 14MTS 163-7 • 16MC, MT, 17MC, MT, MZ-C, MZ-T 163-7
123-9	• DMC, M1, 17MC, M1, M2-C, M2-1 • TPC (Ch. 9025) (Series 'P') (See Model 20PC-Set 175-12) • TPCSB, 17PCW Model 20PC-Set 175-12) • TPTF [Ch. 9025) (Series 'P') (See Model 20PC-Set 175-12) • TPTF • 202-5
	Model 20PC-Set 175-12) • 17PCSB, 17PCW 204 5
	•17PT (Ch. 9025) (Series ''P'') (See
	Model 20PC—Set 175-12) • 17PTE
1168 55-13 2579 1056 Model TV1Set 56-15	20MC, MT, MZ-C, MZ-T 163-7
Maguire Model 571—Set	• 20PC 175-12 • 20PCSB, 20PCW 204-5
Maguire Model 661—Şet	Model 20PC
27-19	• 20PTE, 20PTS, 20PTSB, 20PTW
f (Automobile)	© 20PRSB 204-5
-A	20PTE 20PTS 20PTW 204 -5 -5 20PRSB 204 -5 21PCS 204 -5 21QCS 204 -5 21QCS 204 -5 24QDCS 204 -5 24QDCS 204 -5 Ch. 9040 (See Model A-17C) -11 -11 Ch. 9048 250 -14 Ch. 9048 250 -14 Ch. 9050 250 -14 Ch. 9050 250 -14 Ch. 9053 9054 250 Ch. 9055 251 -11
-A	• 24QDCS
DM-18805-A) [See PCB	Ch. 9040 (See Model A-17C)
A	• Ch. 9048
A (See Model GM891)	• Ch. 9050
(1M-18805) (See Ford	• Ch. 9051
CF743—Set 133-7} (1M-18805)158—5	•Ch. 9055
(See Model 1CM747 or	MITCHELL
A (See Model GM891) (14.18805) (See Ford CF43-Set 133-7) (14.18805)158-5 (See Model 1CM747 or 16.18805-A)167-7 AF-18805-A)214-5 DC-18805-A)214-5 DC-18805-A]246-8 SA-18805-A]62-12 (S9AF-18805)62-12 (S9AF-18805)62-12	•T16-B, -M, T16-2KB, T16-2KM, T17-
AF-18805-A)214—5 DC-18805-A)246—8	•T172B, T-172M
59A-18805-A1). 62-12	• T212-B, -M
Ch. 8E90) (8M-18805-B)	1250, 1251
RM-18805 B) 69-10	1252, 1253
BM-18805-B), 8MM991-E,	1256
49-13 8M-18805-8) 69-10 8M-18805-8), 8MM991-E, 05) 83-4 8 (See Model 8MM890 or	1256 156—8 1261, 1262 259—8 1263, A, 1264, A 259—9
or 8MM991)	1256 156—8 1261, 1262 259—8 1263, A, 1264, A. 259—9 1267 158—7 12688 127—9
ar 8MM991) 5	1256 156
ar 8MM991) 5	1256 156
ar 8MM991) 5	MITCHELL • 116-BM. T16-2KB, T16-2KM, T17- BM
B (See Model 8MM890 or or 8MM991) 15 62-12 1-A1 62-12 (Pacific-Mercury) 150-2) (Also see PCB 191-1) 172-6 150-2) (See PCB 57- 1 and Model 2013-Set	MOLDED INSULATION CO.
B (See Model 8MM890 or or 8MM991) 15 62-12 1-A1 62-12 (Pacific-Mercury) 150-2) (Also see PCB 191-1) 172-6 150-2) (See PCB 57- 1 and Model 2013-Set	1256 156-8 1261, 1262 259-8 1263, A, 1264, A 259-8 1267 158-7 1268 127-2 1271, 1272, 1273 260-11 1274, 1275 257-10 1276, 1277 250-15 1283, 1284 263-11 MOLDED INSULATION CO. (Also see Viz) MR-6 (Wiretone) MR-6 (Wiretone) 41-15
B (See Model 8MM890 or or 8MM991) 15 62-12 1-A1 62-12 (Pacific-Mercury) 150-2) (Also see PCB 191-1) 172-6 150-2) (See PCB 57- 1 and Model 2013-Set	(Also see Viz) MR-6 (Wiretone)
B (See Model 8MM890 or or 8MM991) 15 62-12 1-A1 62-12 (Pacific-Mercury) 150-2) (Also see PCB 191-1) 172-6 150-2) (See PCB 57- 1 and Model 2013-Set	(Also see Viz) MR-6 (Wiretone)
B (See Model 8MM890 or or 8MM991) 15 62-12 1-A1 62-12 (Pacific-Mercury) 150-2) (Also see PCB 191-1) 172-6 150-2) (See PCB 57- 1 and Model 2013-Set	Molec March 41-15 MR-6 (Wiretone) 41-15 MONITOR 41-15 41-15 M-03 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-510 (Fact. No. 472) 28-23
B (See Adde is AMA90 or or BMA99) 5	Molec March 41-15 MR-6 (Wiretone) 41-15 MONITOR 41-15 41-15 M-03 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-510 (Fact. No. 472) 28-23
B (See Adde is AMA90 or or BMA99) 5	(Also see Viz) MR-6 (Wiretone)
B (See Adde is AMA90 or or BMA99) 5	Motion Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 M-403 (Fact. No. 470-2) 22–20 M-500 (Fact. No. 475) 28–23 M-510 (Fact. No. 472) 23–15 M-3070 29–15 RA-50 24–23 TA56M, TW56M 6–18 MONITORADIO 20
B (See Adde is AMA90 or or BMA99) 5	Mobile Mobile Allos Allos (Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 41–15 M-03 (Foct. No. 470-2) 22–20 32 M-500 (Foct. No. 475) 23–23 34–30 M-500 (Foct. No. 475) 23–15 29–15 R-50 24–23 24–23 TASGM, TW56M 6–18 MONITORADIO (Dotto Accounture) (Dotto Accounture) 24–23
B (See Adde is AMA90 or or BMA99) 5	Mobile Mobile Allos Allos (Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 41–15 M-03 (Foct. No. 470-2) 22–20 32 M-500 (Foct. No. 475) 23–23 34–30 M-500 (Foct. No. 475) 23–15 29–15 R-50 24–23 24–23 TASGM, TW56M 6–18 MONITORADIO (Dotto Accounture) (Dotto Accounture) 24–23
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Mobile Mobile Allos Allos (Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 41–15 M-03 (Foct. No. 470-2) 22–20 32 M-500 (Foct. No. 475) 23–23 34–30 M-500 (Foct. No. 475) 23–15 29–15 R-50 24–23 24–23 TASGM, TW56M 6–18 MONITORADIO (Dotto Accounture) (Dotto Accounture) 24–23
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Mobile Mobile Allos Allos (Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 41–15 M-03 (Foct. No. 470-2) 22–20 32 M-500 (Foct. No. 475) 23–23 34–30 M-500 (Foct. No. 475) 23–15 29–15 R-50 24–23 24–23 TASGM, TW56M 6–18 MONITORADIO (Dotto Accounture) (Dotto Accounture) 24–23
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Mobile Mobile Allos Allos (Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 41–15 M-03 (Foct. No. 470-2) 22–20 32 M-500 (Foct. No. 475) 23–23 34–30 M-500 (Foct. No. 475) 23–15 29–15 R-50 24–23 34 TASGM, TW56M 6–18 MONITORADIO (Dotto Accounture) (Dotto Accounture) 24–23
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Motion Also see Viz) MR-6 (Wiretone) 41–15 MONITOR 41–15 M-403 (Fact. No. 470-2) 22–20 M-500 (Fact. No. 475) 28–23 M-510 (Fact. No. 472) 23–15 M-3070 29–15 RA-50 24–23 TA56M, TW56M 6–18 MONITORADIO 4
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Moleci Instantion CC. (Also see Viz) MR-6 (Wiretone) 41-15 MONITOR M-403 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 DR-200 261-8 DR-300 261-8 MR-32 233-5 M-31 162-8 M-101 159-9
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-03 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 29-15 M-3070 29-15 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 DR-12 233-5 M-101 162-8 M-101 155-9 MONTGOMERY WARD (See Airline) MORAP MORAP
B (See Made BMB90 or or BMB91) 5 62-12 A1 62-12 f (Pacific-Mercury) 150-2) (Also see PCB 150-2) (Also see PCB 150-2) (See PCB 57- 1 and Madel 2013-Set 150-4 and Radio Ch. 198-11 5(Ch. 150-11, 81) (Also 57-Set 191-1) .172-6 150-31, -61 and Radio 150-31, -61 and Radio)	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-03 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 29-15 M-3070 29-15 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 DR-12 233-5 M-101 162-8 M-101 155-9 MONTGOMERY WARD (See Airline) MORAP MORAP
B (See Made BMB90 or or BMB91) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-03 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 29-15 M-3070 29-15 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 DR-12 233-5 M-101 162-8 M-101 155-9 MONTGOMERY WARD (See Airline) MORAP MORAP
B (See Made BMB90 or or BMB91) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-03 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 29-15 M-3070 29-15 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 DR-12 233-5 M-101 162-8 M-101 155-9 MONTGOMERY WARD (See Airline) MORAP MORAP
B (See Made BMB90 or or BMB91) 5	Moleci Nostanion CC. (Also see Viz) MR-6 (Wiretone) 41-15 MONITOR 22-20 M-500 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 477) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-512 233-5 M-514 162-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 19-20 603 65-9 604 106-9 604 106-9 607 170-11 607 173-9 607 170-11
B (See Made BMB90 or or BMB91) 5	Moleci Nostanion CC. (Also see Viz) MR-6 (Wiretone) 41-15 MONITOR 22-20 M-500 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 477) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-512 233-5 M-514 162-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 19-20 603 65-9 604 106-9 604 106-9 607 170-11 607 173-9 607 170-11
B (See Made BMB90 or or BMB91) 5	Moleci Nostanion CC. (Also see Viz) MR-6 (Wiretone) 41-15 MONITOR 22-20 M-500 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 477) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-512 233-5 M-514 162-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 19-20 603 65-9 604 106-9 604 106-9 607 170-11 607 173-9 607 170-11
B (See Made BMB90 or or BMB91) 5	Moleci Nostanion CC. (Also see Viz) MR-6 (Wiretone) 41-15 MONITOR 22-20 M-500 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 477) 23-15 M-3070 29-15 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR5-10 261-8 M-514 162-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 19-20 603 65-9 604 106-9 604 106-9 103-9 607 170-11 65-9
B (See Made BMB90 or or BMB91) 5	Moleci Nostanion CC. (Also see Viz) MR-6 (Wiretone) 41-15 MONITOR 22-20 M-500 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 477) 23-15 M-3070 29-15 TA56M, TW56M 6-18 MONITORADIO (Radio Apparatus) AR-1 164-5 AR-3 175-13 DR5-10 261-8 M-514 162-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 19-20 603 65-9 604 106-9 604 106-9 103-9 607 170-11 65-9
B (See Made BMB90 or or BMB91) 5	Molece Vizy MR-6 (Wiretone) 41-15 MONITOR 41-15 M-030 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-500 (Radio Apportus) 6-18 MONITORADIO (Radio Apportus) AR-1 164-5 AR-3 175-13 DR5-10 261-8 M-511 (Sacton
B (See Model B/MB90 or or B/MB91) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-030 (Fact. No. 470-2) 22-20 M.500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apporatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 602 133-9 607 170-11 168 207-4 609 201-6 6010T 220-5 6117 (See Model 610T-Set 220-5) 612 (See Model 610T-Set 220-5) 6117 (See Model 610T-Set 220-5) 612 (See Model 60T-Set 220-5) 612 (See Model 60T-Set 220-5) <
B (See Model B/MB90 or or B/MB91) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-030 (Fact. No. 470-2) 22-20 M.500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apporatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 602 133-9 607 170-11 168 207-4 609 201-6 6010T 220-5 6117 (See Model 610T-Set 220-5) 612 (See Model 610T-Set 220-5) 6117 (See Model 610T-Set 220-5) 612 (See Model 60T-Set 220-5) 612 (See Model 60T-Set 220-5) <
B (See Model B/MB90 or or B/MB91) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-030 (Fact. No. 470-2) 22-20 M.500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apporatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 602 133-9 607 170-11 168 207-4 609 201-6 6010T 220-5 6117 (See Model 610T-Set 220-5) 612 (See Model 610T-Set 220-5) 6117 (See Model 610T-Set 220-5) 612 (See Model 60T-Set 220-5) 612 (See Model 60T-Set 220-5) <
B (See Made Jamber) or or BMA99) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-033 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-31 M-500 (Fact. No. 472) 23-13 M-500 (Fact. No. 472) 23-13 M-3070 29-15 RA-500 24-23 TASOM, TWS6M 6-18 MONITORADIO (Radio Apportatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 M-51A 162-3 MONTGOMERY WARD 65-9 602 (671A) 19-20 603 106-9 604 103-9 MOPAR 200-4 609 201-6 6101 5e-2 602 (C-4008) (Revised) 42-19 803 (PD-4908) 66-12 804 (C-40908) 66-12
B (See Made (MM890 or or BMM891) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-033 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-31 M-500 (Fact. No. 472) 23-13 M-500 (Fact. No. 472) 23-13 M-3070 29-15 RA-500 24-23 TASOM, TWS6M 6-18 MONITORADIO (Radio Apportatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 M-51A 162-3 MONTGOMERY WARD 65-9 602 (671A) 19-20 603 106-9 604 103-9 MOPAR 200-4 609 201-6 6101 5e-2 602 (C-4008) (Revised) 42-19 803 (PD-4908) 66-12 804 (C-40908) 66-12
B (See Model B/MB90 or or B/MB91) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-033 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-31 M-500 (Fact. No. 472) 23-13 M-500 (Fact. No. 472) 23-13 M-3070 29-15 RA-500 24-23 TASOM, TWS6M 6-18 MONITORADIO (Radio Apportatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 M-51A 162-3 MONTGOMERY WARD 65-9 602 (671A) 19-20 603 106-9 604 103-9 MOPAR 200-4 609 201-6 6101 5e-2 602 (C-4008) (Revised) 42-19 803 (PD-4908) 66-12 804 (C-40908) 66-12
B (See Model 2013) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-033 (Fact. No. 470-2) 22-20 M-500 (Fact. No. 475) 28-31 M-500 (Fact. No. 472) 23-13 M-500 (Fact. No. 472) 23-13 M-3070 29-15 RA-500 24-23 TASOM, TWS6M 6-18 MONITORADIO (Radio Apportatus) AR-1 164-5 AR-3 175-13 DR5-1 261-8 M-51A 162-3 MONTGOMERY WARD 65-9 602 (671A) 19-20 603 106-9 604 103-9 MOPAR 200-4 609 201-6 6101 5e-2 602 (C-4008) (Revised) 42-19 803 (PD-4908) 66-12 804 (C-40908) 66-12
B (See Model 2013) 5	Molece Viz) MR-6 (Wiretone) 41-15 MONITOR 41-15 M-030 (Fact. No. 470-2) 22-20 M.500 (Fact. No. 475) 28-23 M-500 (Fact. No. 475) 28-23 M-500 (Fact. No. 472) 23-15 M-3070 29-15 RA-50 24-23 TA56M, TW56M 6-18 MONITORADIO (Radio Apporatus) AR-1 164-5 AR-3 175-13 DR-200 261-8 M-101 159-9 MONTGOMERY WARD (See Airline) MOPAR 602 602 133-9 607 170-11 168 207-4 609 201-6 6010T 220-5 6117 520-51 612 (See Model 610T-Set 220-51 6117 (See Model 610T-Set 220-51 612 (See Model 610T-Set 220-51 612 (See Model 600-Set 220-51 802 (C-4608) (Revised) 42-19 803 (FD-4908) 66-12 804 (C-408) (See Model 803-Set 66

MINERVA	
L-702 L-728	12-20 11-15 6-17
W-117, Tropic Master W-117-3	11-14
VY-/ UZB	12_20
W710, W710A (W119) W-728 410, 411 702H 702H-1	5-25 11-15 41-14
410, 411 702H,702H-1 729 (Portapol)	
	Meck)
A-17C, T (Ch. 9040)	.216-4 h. 9040)
A24C (Ch. 9049, 9051) .	216-4
• 14M15	.163-7
 14M13 16MC, MT, 17MC, MT, MZ 17PC (Ch. 9025) (Series '' Model 20PC—Set 175-1 17PCSB, 17PCW 17PT (Ch. 9025) (Series '' Model 20PC—Set 175-1 17PTE 20MC, MT, MZ-C, MZ-T 20PCSB, 20PCW 20PC, ISse Model 20PC—Set 20PC	163-7
Model 20PC-Set 175-1	2)
• 17PT (Ch. 9025) (Series '	P'') (See
•17PTE	204-5
• 20PC	175-12
17PTE 20MC, MT, MZ-C, MZ-T 20PC 20PCSB, 20PCW 20PT [See Model 20PC	Set 175-
• 20PTE, 20PTS, 20PTSB, 20	0PTW . 204-5
• 20PRSB	.204-5
	204—5 204—5 204—5
• 24QDCS Ch. 9040 (See Model A-17	C)
Ch. 9040 (See Model A-17 Ch. 9047 Ch. 9047 Ch. 9048 Ch. 9049 Ch. 9050 Ch. 9051 Ch. 9053, 9054	.204—5 .204—5 C) .251–11 .250–14 .247—6 .250–14 .247—6 .250–14 .251–11
• Ch. 9049 • Ch. 9050	247-6
• Ch. 9051 • Ch. 9053, 9054	247-6
•Ch. 9055	. 251-11
	KM, T17-
В, М	154—8 189—11
•T212-B, -M	190-9
1250, 1251	55-14
1254, 1255	159—8 156—8
1256 1261, 1262 1263, A , 1264, A	259-8
	259-9 158-7 127-9
1268R 1271, 1272, 1273	260-11
	957 10
1274, 1275	260-11 257-10 250-15
1276, 1277 1283, 1284	. 263-11
1274, 1277 1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz)	. 263–11 CO.
1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	. 263–11 CO.
1274, 1277 1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MONITOR M 403 (Earth No. 470;2)	. 263–11 CO. . 41–15
1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	. 263–11 CO. . 41–15
1276, 1277 1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	. 263–11 CO. . 41–15 . 22–20 . 28–23 . 23–15 . 29–15 . 24–23
1274, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MONITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 475) M-500 (Fact. No. 472) M-3070 RA-50 TA56M, TW56M	. 263–11 CO. . 41–15 . 22–20 . 28–23 . 23–15 . 29–15
1276, 1277 1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18
1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18
1276, 1277 1276, 1277 1283, 1284 MOLED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18
1276, 1277 1276, 1277 1283, 1284 MOLED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18
1274, 1277 1276, 1277 1283, 1284 MOLED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 22-20 28-23 23-15 29-15 24-23 6-18 164-5 175-13 261-8 261-8 261-8 233-5
1274, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18
1274, 1277 1276, 1277 1283, 1284 MOLED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18
1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 22-20 28-23 23-15 29-15 24-23 6-18 164-55 175-13 261-8 261-8 261-8 261-8 159-9 19-20
1274, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MA-03 (Fact. No. 470-2) M-500 (Fact. No. 472) MA-510 (Radio Apparatus) AR-1 AR-3 DR5-1 DR-200 MR-32 M-51A M-51A MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 603 604	263-11 CO. 22-20 28-23 23-15 29-15 24-23 6-18 164-5 175-13 24-23 6-18 164-5 175-13 24-23 6-18 155-19 175-19
1276, 1277 1276, 1277 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone)	263-11 CO. 22-20 28-23 23-15 29-15 24-23 6-18 164-5 175-13 24-23 6-18 164-5 175-13 24-23 6-18 155-19 175-19
1274, 1277 1283, 1284 1283, 1284 1283, 1284 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MMNTOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 475) M-510 (Fact. No. 472, 1, M-3070 RA-50 TA56M, TW56M MONITORADIO (Radio Apparatus) AR-1 AR-3 DR-200 M-511 DR-200 MCNTGOMERY WARD (See Airline) MOPAR 602 (671A) 608 609	263-11 CO. 22-20 28-23 23-15 29-15 24-23 6-18 164-5 175-13 24-23 6-18 164-5 175-13 24-23 6-18 155-19 175-19
1274, 1277 1283, 1284 1283, 1284 1283, 1284 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MMNTOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 475) M-510 (Fact. No. 472, 1, M-3070 RA-50 TA56M, TW56M MONITORADIO (Radio Apparatus) AR-1 AR-3 DR-200 M-511 DR-200 MCNTGOMERY WARD (See Airline) MOPAR 602 (671A) 608 609	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18 164-5 175-13 261-8 261-8 261-8 263-9 162-8 159-9 162-9 133-9 170-14 2001-6 220-5 270-7 270-7 2
1274, 1277 1283, 1284 1283, 1284 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MOITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 475) M-500 (Fact. No. 472) M-3070 RA-50 TA56M, TW56M MONITORADIO (Radio Apparatus) AR-1 AR-3 DB-10 MONTGOMERY WARD (See Airline) MOPAR 602 604 605 606 607 6111 (See Model 610T-Set 612 (See Model 607-Set	263-11 CO. 41-15 22-20 28-23 23-15 24-23 6-18 164-5 175-13 261-8 261-8 261-8 261-8 261-8 261-8 159-9 133-9 170-11 207-4 201-6 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 201-6 182-5 201-6 182-5 201-6 201-5 201-6 20
1274. 1277. 1283. 1284. 1283. 1284. 1283. 1284. 1283. 1284. 1283. 1284. MOLDED INSULATION (Also see Viz) MR.6. MONITOR M.403 (Fact. No. 470.2). M.500 (Fact. No. 470.2). M.500 (Fact. No. 472.1). M.500 (Fact. No. 472.1). M.500 (Fact. No. 472.1). M.500 (Fact. No. 472.1). M.5070 RA-50. MASM.TWS6M. MONITORADIO (Redia Apparatus) AR-1 AR-3 AR-30. MSS.1 DR-300. M.510 MONTGOMERY WARD (See Airline) MOPAR 602 (671A). 604 606. 607 608 608 609 6101 (See Model 6107—Se 6121 (See Model 6107—Se 612 (See Model 609—Set 603 (PD-4908) 803 (PD-4908)	263-11 CO. 41-15 22-20 28-23 23-15 24-23 6-18 164-5 175-13 261-8 261-8 261-8 261-8 261-8 261-8 159-9 133-9 170-11 207-4 201-6 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 220-5 201-6 182-5 201-6 182-5 201-6 201-5 201-6 20
1274. 1277. 1283. 1284. 1283. 1284. 1283. 1284. 1283. 1284. 1283. 1284. MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MR-6. MONITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 470.2) M-500 (Fact. No. 472.1) M-500 TA56M, TW56M MONITORADIO (Redio Apparatus) AR-1 AR-3 DR-100 (Redio Apparatus) AR-1 MAS-1 DR-200 MR-32 M-530 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 604 607 6107 6117 (See Model 6107—See 612 (See Model 609—Set 612 (See Model 609—Set 612 (See Model 609—Set 612 (See Model 609—Set 613 (PD-4908) 803 (PD-4908) 804 404.4088 (C-4008) (C-4008) (See Cappa and apparatus) 	263-11 CO. 41-15 22-20 28-23 23-15 29-15 20-18 20-19 20-16 20-16 20-16 20-18 20-16 20-
1274, 1277 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MA01TOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 472-1) MA-500 (Fact. No. 472-1) MA-510 (Fact. No. 472-1) M-511 (Fact. No. 472-1) M-512 (See Airline) MOPAR 602 (671-1) 603 604 605 607 608 609 6101 (See Model 6107Se 802 (C-4	263-11 CO. 21-15 22-20 28-23 23-15 29-15 24-23 6-18 164-5 24-23 6-18 155-13 261-8 233-5 162-8 159-9 170-11 207-4 213-9 175-13 201-6 182-20 192-20 192-
1274, 1277 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MA01TOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 472-1) MA-500 (Fact. No. 472-1) MA-510 (Fact. No. 472-1) M-511 (Fact. No. 472-1) M-512 (See Airline) MOPAR 602 (671-1) 603 604 605 607 608 609 6101 (See Model 6107Se 802 (C-4	263-11 CO. 21-15 22-20 28-23 23-15 29-15 24-23 6-18 164-5 24-23 6-18 155-13 261-8 233-5 162-8 159-9 170-11 207-4 213-9 175-13 201-6 182-20 192-20 192-
1272, 1277 1283, 1284 1283, 1284 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MONITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 472) M-500 (Fact. No. 472) MA: 3070 RA-30 AR-31 MONITORADIO (Redia Apparatus) AR-3 AR-3 AR-3 MB-200 MR-302 MR-302 MA-51A M-101 MONTGOMERY WARD (See Airline) MOPAR 602 (C-1408) 603 (F1 (See Model 6107-See 6104 (See Model 6107-See 6105 (C-4008) 805 (C-4008)	263-11 CO. 21-15 22-20 28-23 23-15 29-15 24-23 6-18 164-5 24-23 6-18 155-13 261-8 233-5 162-8 159-9 170-11 207-4 213-9 175-13 201-6 182-20 192-20 192-
1272, 1277 1283, 1284 1283, 1284 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MONITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 472) M-500 (Fact. No. 472) MA: 3070 RA-30 AR-31 MONITORADIO (Redia Apparatus) AR-3 AR-3 AR-3 MB-200 MR-302 MR-302 MA-51A M-101 MONTGOMERY WARD (See Airline) MOPAR 602 (C-1408) 603 (F1 (See Model 6107-See 6104 (See Model 6107-See 6105 (C-4008) 805 (C-4008)	263-11 CO. 21-15 22-20 28-23 23-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 20-18 175-13 261-8 233-5 162-8 159-9 170-11 207-4 201-6 133-9 170-11 207-14 201-6 18-24 42-19 66-12 67-12 71-11 58-16 107-6 105-58-1 107-6
1276, 127 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MADITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 472] M-3070 RA-50 TA56M, TW56M MONITORADIO (Radio Apparetus) AR-1 AR-3 DR-200 MK-31 M-101 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 603 604 605 6101 (See Model 6107—Set 802 (C-4008) 803 (FD-4908) 804 805 (Sor (See Model 803—12) 808 909 (C-5009) (See Model 803—12) 808 809 (C-5009) (See Model 803—12) 813 (DS107)	263-11 CO. 21-15 22-20 28-23 23-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 20-18 175-13 261-8 233-5 162-8 159-9 170-11 207-4 201-6 133-9 170-11 207-14 201-6 18-24 42-19 66-12 67-12 71-11 58-16 107-6 105-58-1 107-6
1272, 1277 1283, 1284 1283, 1284 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MR-6 (Wiretone) MR-6 (Wiretone) MR-6 (Wiretone) MR-101 MR-101 (Redia Apparatus) AR-3 DR-100 (Redia Apparatus) AR-3 DR-100 MR0NTGRADIO (Redia Apparatus) AR-1 DR-200 MR-302 MR-51A M-51A MONTGOMERY WARD (See Airline) MOPAR 602 (G71A) 603 C-4008) (Revised) 803 (PD-4908) 804 (-4098) 805 (C-4008) 804 (-2408) 805 (C-5009) (See Model 803-12) 807 (11) 813 (D5107) 814 415 (C-5109) 815 (C-5109) 	263-11 CO. 21-15 22-20 28-23 23-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 29-15 20-18 175-13 261-8 233-5 162-8 159-9 170-11 207-4 201-6 133-9 170-11 207-14 201-6 18-24 42-19 66-12 67-12 71-11 58-16 107-6 105-58-1 107-6
1276, 127 1283, 1284 1283, 1284 MOLDED INSULATION (Also see Viz) MR-6 (Wiretone) MADITOR M-403 (Fact. No. 470-2) M-500 (Fact. No. 470-2) M-500 (Fact. No. 472) M-500 (Fact. No. 472) M-3070 RA-50 TA56M, TW56M MONITORADIO (Radio Apparentus) AR-1 AR-3 DR-100 (Radio Apparentus) AR-1 M-101 MONTGOMERY WARD (See Airline) MOPAR 602 (671A) 603 604 605 6101 6111 (See Model 6107—Se 802 (C-4008) (Revised) 803 (FD-4908) 804 805 (Ser Vise Model 803—12) 121 806 807 (See Model 803—12) 121 806 807 (See Model 803—12) 121 808 809 (C-5009) (See Model 803—12)	263-11 CO. 41-15 22-20 28-23 23-15 29-15 24-23 6-18 164-55 175-13 24-23 6-18 164-51 175-13 24-23 175-13 24-23 164-55 175-13 24-23 175-13 24-23 175-13 24-23 159-9 103-9 139-8 139

NOTE: PCB Denotes Production Change Bulletin, Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200.

Denotes Television Receiver.

MOTOROLA

MOTOROLA-Cont.

icer 82 • VK106, B, M (Ch. TS-9, A, B, C) • VK106, VK107 (Ch. TS-9E, TS-9E1) 77-05

• VT-73, VT-73A (Chassis TS-4J Late) 71-12

•VT101 (Ch. TS-3) •VT105 (Ch. TS-9D) Photofact

 Icer
 82

 •VT105, VT105M (Ch. TS-9, TS-9A, TS-9B, TS-9C)
 67–13

 •VT107 (Ch. TS-9D) Photofact Serv

•VT107 (Ch. TS-9D) Photofact Serv-icer 82 •VT107, B, M (Ch. TS-9, A, B, C) 67-13 •VT121 (Ch. TS-15) 91A-9

(Also see PCB 106—Sef 253-1) 9'21K15A (Ch. RT5 502') (See PCB 106 — Sef 233: 1 and Model Y17K17—Sef 237-3) (Also see PCB 106—Sef 233:1) (Also see PCB 106—Sef 233:1) 21K16A (M) (Ch. RT5 502') (See PCB 106—Sef 235-1) and Model Y17K17—Sef 237-8) 9'21K16W (Ch. RT5 502', QT5-502') (Also see PCB 106—Sef 233-1) (Also sef 233-1) (Also sef 233-1) (Also sef 233-1) (Also sef 233-1) (Also s

Y21K16W [Ch. T5-5027, OT5-5027]
 Y21K17 [Ch. T5-5027] (Also see PCB 106—Set 253-1]
 Y21K17 [Ch. T5-5027] (Also see PCB 106—Set 253-1]
 Y21K17 [Ch. Y5-5027] (See PCB 106—Set 253-1] and Model Y17K17—Set 237-8]
 Y21K18, 8 [Ch. PT5-5027] [See PCB 106—Set 233-1] and Model Y17K17—Set 237-8]
 Y21K18, AE (Ch. YT5-5027] [Also see PCB 106—Set 233-1] and Model Y17K17—Set 237-8]
 Y21T3, AE (Ch. T5-5027] [Also see PCB 106—Set 233-1] and Model Y17K17—Set 237-8]
 Y21T11, 8, W [Ch. YT5-5027] [Also see PCB 106—Set 233-1] and Model Y17K17—Set 237-8]
 Y21T13, 8 (Ch. T5-5247] [See PCB 106—Set 233-1] and Model Y17K17—Set 237-8]
 Y21T14 [Ch. T5-5027] [See PCB 106—Set 233-3] and Model Y17K17—Set 237-8]
 Y21T4 [Ch. T5-5027] [See PCB 106—Set 233-8]
 Y21T4 [Ch. T5-5027] [See PCB 106—Set 233-8]

3MF (See Ford Model 3MF—Set 206-5)

17F3BA [CII: HS-253]
 17F4 (Ch. TS-118 and Radio Ch. HS-253) (See Model 14K1BH)
 121-10

 121-10

 17F4A (Ch. TS-89 and Radio Ch. HS-253)

 121-10

 17F5 (Ch. TS-118 and Radio Ch. HS-261)

 121-10

3MFT (See Ford Model 3MFT-Set 215-7)

104

MOTOROLA-Cont.
 MOTOROLA-Cont.

 SA7 (Ch. HS-62), SA7A (Ch. HS-62A)
 29-16

 SC1 (Ch. HS-228)
 116-9

 SC2 (Ch. HS-258)
 116-9

 SC3 (Ch. HS-262)
 116-9

 SC4 (Ch. HS-270)
 116-9

 SC4 (Ch. HS-271)
 116-9

 SC4 (Ch. HS-271)
 ISEe Model SC1

 -Set 116-91
 SC6 (Ch. HS-272)

 SC6 (Ch. HS-272)
 See Model SC1

 -Set 116-91
 SC6 (Ch. HS-272)

 SU1 (Ch. HS-250), SH3U (Ch. HS-224)
 117-9

 SU1 (Ch. HS-250), SJ1U (Ch. HS-224
 100-7

 SU2 (Ch. HS-250) (See Model SJ1
 10-7

MOTOROLA-Cont.

SJI (ch. HS-250), SJIU (ch. HS-224)
 224
 100-7
 SIZ (ch. HS-220) (See Model SJI-set 100-7)
 Stet 100-7)
 Stet 100-7)
 Stet 100-7)
 SIZ (ch. HS-250), SLIU (ch. HS-224) (See Model SJI-set 100-7)
 Sti 2 (ch. HS-250) (See Model SJI-set 100-7)
 Stet 100-7)
 Stet 100-7)
 Stet 100-7)
 Sti 2 (ch. HS-224) (See Model SJI-set 100-7)
 Sti 100-7)
 Stet 100-7)
 Sti 10, Shi 24, SRI 34, SR

243) - 114-7 52210, 5220, 5230 (Ch. H5. 259) - 120-7 611, 612 (Ch. H5.264). 102-7 63110, 6312 (Ch. H5.264). 112-5 7F11, 7F118 (Ch. H5.264). 113-5 7F11, 7F118 (Ch. H5.264). 113-5 87F0 (See Ch. 8A-Set 46.16) 87F01, 9FA218 (Ch. H5.244) 9FA21, 0FA518, Al (See Model 7771, 0K 51(6h, 15, 4A, 8], 92-4 10V16 (Ch. T5.44, A, 8], 92-4 10V12 (Ch. T5.14, A, 8], 92-4 10V12 (Ch. T5.14, A, 8], 92-4 10V12 (Ch. T5.14, A, 8], 92-4 10V12 (Ch. T5.44, A, 8], 92-4 10V12 (Ch. T5.45, 75.9E1) 77-6 10V110 (Ch. T5.45, 75.9E1) 77-6 10V122 (Ch. T5.4, A, 8], 92-4 12X2, 8 (Ch. T5.238) (See Model 12X2, 9 (Ch. T5.33) (See Model 12X2, 9 (Ch. T5.33) (See Model 12X2, 8 (Ch. T5.33) (See Model 12X2, 8 (Ch. T5.33) (See Model 12X3, 8 (Ch. T5.33) (See Model 12X3, 8 (Ch. T5.33) (See Model 12X4, 8 (Ch. T5.33) (See Model 12X3, 8 (Ch. T5.33) (See Model 12X4, 8 (Ch. T5.33) (See Model 12X3, 8 (Ch. T5.33) (See Model 12X3, 8 (Ch. T5.30), 115-7 12V148, 8, R.C (Ch. T5.33) (See Model 12713-5ar 92-4) 12V1713 (Ch. T5.30, A) (Altor PCB 3 -Set 106-1] 77-6 12V113 (Ch. T5.48) 112-5 144, 8 (Ch. T5.48) 112-5 144, 8 (Ch. T5.48) 112-5 144, 8 (Ch. T5.48) 112-5 1474, 9 (Ch. T5.48) 112-5 1474, 9 (Ch. T5.48) 112-10 1474, 9 (Ch. T5.48) 010 1474, 9 (Ch. T5.48) 012-8 16618 (Ch. T5.49 010 16474 (Ch. T5.49 010 16474 (Ch. T5.49 010 16474 (Ch. T5.48 01 Redic Ch. H5-233 -5et 106-1] 177-63

IPF 36, C. (Ch. 15-174 and Radio Ch. HS-233) [See Madel 14K1BH-Set 121-10]
 IPF 36, C. (Ch. 15-174 and Radio Ch. HS-233) [See Madel 14K1BH-Set 121-10]
 IPF 378 (Ch. 15-174 and Radio Ch. HS-233) [See Madel 14K1BH-Set 121-10]
 IPF 38 (Ch. 15-174 and Radio Ch. HS-231) [See Madel 14K1BH-Set 121-10]
 IPF 30 (Ch. 15-174) [See Madel 14K1BH-Set 121-10]
 IPF 30 (Ch. 15-228 and Radio Ch. HS-330; A. and Radio Ch. HS-330] [For TV Ch. See Madel 17F12-Set 171-8]
 IPF 12, A, and Radio Ch. HS-319, So (Ch. 15-305, A) and Ch. See Set 183-1 and Madel 21F1-Set 171-8]
 IPF 13, G (Ch. 15-400A and Radio Ch. see Madel 17F12-Set 171-8]
 IPF 13, G (Ch. 15-400A and Radio Ch. HS-319) [For TV Ch. see Madel 17F12-Set 171-8]
 IPF 13, G (Ch. 15-403A and Radio Ch. see Madel 17F12-Set 171-8]
 IPF 13, C (Ch. 15-403A and Radio Ch. HS-319) [For TV Ch. see Madel 17F12-Set 171-8]
 IPK 13, C (Ch. 15-403A and Radio Ch. HS-319) [For TV Ch. see Madel 17F12-Set 171-8]
 IPK 14, IPK 14A (Ch. 15-95) 121-10
 IPK 14, IPK 14A (Ch. 15-95) 121-10
 IPK 14A (Ch. 15-4051 (21-10)
 IPK 14A (Ch. 15-4051 (21-10)
 IPK 14A (Ch. 15-4051 (21-10)
 IPK 14A (Ch. 15-172) [See Madel 14K1BH-Set 121-10]
 IPK 14A (Ch. 15-172) [See Madel 14K1BH-Set 121-10]
 IPK 14A (Ch. 15-174) [See Ma

326) 171-8 1779 (Ch. 15-325A, B) (See Model 1779 (Ch. 15-325A, B) (See Model 1779 (Ch. 15-325A, B) (See Model 17712-Set 171-8) 17719E (Ch. 15-325A, B) (See Model 17712-Set 171-8)

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NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200.

MOTOROLA-Cont. •1719EF (Ch. TS-401) (See PCB 49 —Set 183.1 and Model 21F1--Set 173-9) •17110 (Ch. TS-3258) (See Model 17F12-Set 171-8) •17101 (Ch. TS-326A, 8) (See Model 17F102 (Ch. TS-404, 8) (See Model 17102 (Ch. TS-401) (See PCB 49-Set 183-1 and Model 21F1-Set 173-9) •17111 (Ch. TS-395, -02) ...192--•17111 (Ch. TS-408A) (See Model 21C1-Set 191-13) •17111E (Ch. TS-408A) (See Model 21C1-Set 191-13) •17112 (Ch. TS-408A) (See Model

MOTOROLA-Cont.

MONORIA - Cont.
 21K4, A. (Ch. 15:292A, B. C) (Also see PCB 63—Set 197-1 and PCB 73—Set 214-1)
 191-13
 21K4AY (Ch. 15:292A, B. C) (Also see PCB 63—Set 197-1, PCB 73—Set 214-1)
 21K4B (Ch. 15:292A, B. C) (Also see PCB 63—Set 197-1)
 21K4B, BY (Ch. WIS-292A, AY, B. KY, CY) (See PCB 63—Set 197-1)
 21K4B, BY (Ch. WIS-292A, AY, B. KY, CY) (See PCB 63—Set 197-1)
 21K4B, Ch. 15:292A, B, C) (Also see PCB 63—Set 197-1)
 21K4B, Ch. TS:292AY, BY, CY) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292AY, BY, CY) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292AY, BY, CY) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, AY, B. SY, C, CY) (See PCB 63—Set 197-1)
 21K4W (Ch. TS:292A, AY, B. SY, C, CY) (See PCB 63—Set 197-1)
 21K4W, WDY (Ch. WIS-292A, AY, B. SY, C, CY) (See PCB 63—Set 197-1)
 21K4W, WDY (Ch. WIS-292A, AY, B. SY, C, CY) (See PCB 63—Set 197-1)
 21K4W, WDY (Ch. WIS-292A, AY, B. SY, C, CY) (See PCB 63—Set 197-1)
 21K4W, Ch. TS:292A, B, C) (Also see PCB 63—Set 197-1)
 21K4W, 21K4Y (Ch. TS:292AY, B, C) (Also see PCB 63—Set 197-1)
 21K4W, Ch. TS:292A, B, C) (Also see PCB 63—Set 197-1)
 21K4B, BY, C, CY) (See PCB 63—Set 197-1)
 21K4B, BY, C, CY (See PCB 63—Set 197-1)
 21K4B, C, C, TS:292A, B, C) (Also see PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, BY, C) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, BY, C) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, B, C) (Also see PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, B, C) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, B, C) (Also see PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, B, C) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, C) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, C) (See PCB 63—Set 197-1)
 21K4B, Ch. TS:292A, Y, C) (See PC

Denotes Television Receiver.

MOTOROLA-Cont.

●1/112, ●1/712C (Ch. TS-408A) (See Model 21C1—Set 191-13) ●1/712W (Ch. TS-395A, -02) 192—6

MOTOROLA-Cont.

MOTOROLA-Cont.

 MOTOROLA-Cont.

 •2114AC, ACE (Ch. 15.2928, C) (See PCB 63-Set 197.1, PCB 73-Set 214.1 and Model 21C1-Set 191.13)

 •2114ACY (Ch. T5.292AY, BY, CY) (See PCB 63 - Set 197.1, PCB 73-Set 214.1 and Model 21C1 -Set 191.13)

 •2114ACY (Ch. T5.292AY, BY, CY) (See PCB 63-Set 197.1), ..., 191.13

 •2114E (Ch. T5.324A, B) (Alico isee PCB 63-Set 197.1), ..., 191.13

 •21175, B, BY, Y (Ch. VT5.292A, AY, B, BY, C, CY) (See PCB 43-Set 24.3-ign), TPCB 73-Set 24.1-grad, AC (Ch. T5.502) (Alico See PCB 106 (Set 233.1), ..., 237-88

 •21174, B, AT (Ch. YT5.502) (Alico See PCB 106 (Set 233.1), ..., 237-88

 •21171, B, W (Ch. VT5.502) (Alico See PCB 106 (Set 233.1), ..., 237-88

 •21171, B, W (Ch. VT5.502) (Alico See PCB 106 (Set 233.1), ..., 237-88

 •21171, B, W (Ch. VT5.502) (Alico See PCB 106 (Set 233.1), ..., 237-88

 •21171, B, W (Ch. VT5.502) (Alico See PCB 106 (Set 233.1), ..., 237-88

 •21171, B, St, T5.507 (See PCB 106 Set 237-8)

 •21171, B, Ch. T5.507 (See PCB 106 Set 237-8)

 •21171, B, Ch. T5.507 (See PCB 106 Set 237-8)

 •21171, B, Z4K2, B, 24K3, W (Ch. T5.602)

 •21742, (Ch. H5.60)
 Set 237-61

 •21742, (Ch. H5.60)
 9-33

 •21744, (Ch. H5.60)
 9-33

 •21744, (Ch. H5.60)
 9-33

 •21742, (Ch. H5.60)
 9-33

 •2742, 6, CHX5ChO, T5-002) 233-6
 77-7 51C1, 51C2, 51C3, 51C4 (Ch. H5. 288) (See Model SC1—Set 116-9) 51L1U, 51L2U (Ch. H5.224) (See Model 51)-Set 100-7] 51M1U, 51M2U (Ch. HS.283)

 14A, 52813A, 248104
 78—7

 317)
 77
 78

 52811U, 52812U, 52813U, 528-14U, 52815U, 52816U (Ch. H5-315)
 77-11

 315)
 77-11

 33C1, 53C2, 53C3, 53C4 (Ch. H5-360)
 236—7

 33C6, 53C7, 53C8, 53C9 (Ch. H5-360)
 235—7

 33D1 (Ch. H5-360)
 235—9

 53E2 (Ch. H5-360)
 234—9

 Syntham
 <t

 22(1-5s; 199-17)
 (See model)

 622(2)
 (Ch. H5.299)
 189-12

 62(2A)
 (Ch. H5.299)
 (See Model)

 62(23)
 (Ch. H5.299)
 (See Model)

 62(23)
 (Ch. H5.299)
 (See Model)

 62(23)
 (Ch. H5.299)
 (See Model)

 62(3-(Ch. H5.299))
 (See Model)
 (See Model)</td 62X11U, 62X12U, 62X13U (Ch. HS 175-1 62X11U, 62X12U, 62X13U (CH. 1-4 314) 175-14 62X21 (Ch. HS-326) 228-12 63L5S (Ch. HS-415) 251-13 63L1, 63L2, 63L3 (Ch. HS-361) 222-45

 30-20

 67XM21 (Ch. HS-64)
 32-14

 68F12, 68F14, 68F14, 68F14, 68F14, 68F14, 68F14, 68F14, 68F14, 64F14, 68F14, 67F14, 33-14 309 63-14 400 99-10 401 131-12 401A 779-8 403 403 216-5 405 (Ch, AS-13) 3-8 405M (See Set 21-25 ond Model 405-Set 3-8) 38-12 408 38-12 201-6) 700 100-8 701 37-8 702 (Ch. 81-2 and 6-2) 197-7 705 (Ch. 45-16) 7-19 708 40-12 709 (See Model 708-Set 40-12] 800 103-10 801 197-10 103-10 10

MDTDMCLA_cont. Ch. H5-60 (See Model 57X1)) Ch. H5-62 (See Model 57X1) Ch. H5-62 (See Model 57X1)) Ch. H5-64 (See Model 67KR21)) Ch. H5-87 (See Model 67KR21)) Ch. H5-87 (See Model 77F31) Ch. H5-87 (See Model 77F31) Ch. H5-97 (See Model 77F31) Ch. H5-97 (See Model 77F31) Ch. H5-97 (See Model 77F32)) Ch. H5-98 (See Model 77F32)) Ch. H5-98 (See Model 77F32)) Ch. H5-98 (See Model 77F32)) Ch. H5-102 (See Model 77F32)) Ch. H5-103 (See Model 77F32)) Ch. H5-103 (See Model 77F32)) Ch. H5-103 (See Model 78F11)) Ch. H5-119 (See Model 68K11)) Ch. H5-119 (See Model 68K11)) Ch. H5-119 (See Model 68K11)) Ch. H5-127 (See Model 68K11)) Ch. H5-137 (See Model 68K11)] Ch. H5-137 (See Model 68K11)] Ch. H5-136 (See Model 78F72A) Ch. H5-136 (See Model 58G11) Ch. H5-138 (See Model 58G11) Ch. H5-138 (See Model 58G11) Ch. H5-128 (See Model 58G11) Ch. H5-128 (See Model 58G11) Ch. H5-124 (See Model 58G11) Ch. H5-124 (See Model 58G11) Ch. H5-124 (See Model 59K11) Ch. H5-224 (See Model 59K11) Ch. H5-234 (See Model 50K1) Ch. H5-237 (See Model 50K1) Ch. H5-237 (See Model 52K1) Ch. H5-337 (See Model 52K1) Ch. H5-337 (See Model 52K1) Ch. H5-337 (See Model 52K1) Ch. H5 Ch. TS-15 (See Model VT-121) Ch. TS-15C, TS-15C1 (See Model 12VK188) (See Model 16VF88) 12VK188) Ch. TS-16, A (See Model 16VF88) Ch. TS-18, A (See Model 7VT)) Ch. TS-23, A, B (See Model 12-VKI Ch. TS-30, A (See Model 12VK15)

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MOTOROLA-Cont.

MOTOROLA-Cont. Ch. 75-52 (See Made) 16K2() Ch. 75-52 (See Made) 12K2) Ch. 75-60 (See Made) 12K2) Ch. 75-60 (See Made) 19F1) Ch. 75-74 (See Made) 19F1) Ch. 75-74 (See Made) 19F1) Ch. 75-78 (See Made) 14K1 Ch. 75-79 (See Made) 14K18H Ch. 75-79 (See Made) 14K18H Ch. 75-710 (See Made) 14K18H Ch. 75-719 (See Made) 14K18H Ch. 75-719 (See Made) 17K18L) Ch. 75-719 (See Made) 17F18 Ch. 75-719 (See Made) 17F18 Ch. 75-719 (See Made) 17F18 Ch. 75-719 (See Made) 17F38C Ch. 75-723 (See Made) 17K38C Ch. 75-723 (See Made) 17K38C Ch. 75-727 (See Made) 17K38C Ch. 75-7 MOTOROLA-Cont. 21(1) (Ch. 15-292AY, BY, CY (See Model 21(1Y) (Ch. 15-307 (See Model 20K6) (Ch. 15-307 (See Model 20K6) (Ch. 15-314A, B, 15-315A, B (See Model 17K10E) (Ch. 15-324, A, B (See Model 2114) (Ch. 15-324, A, B (See Model 2114) (Ch. 15-325, A, 15-326, A (See Model 17F12) (Ch. 15-327, A, 15-326, A (See Model 17F12) (Ch. 15-327, A) (See Model 17F13) (Ch. 15-327, A) (See Model 17F13) (Ch. 15-307, C) (See Model 17F13) (Ch. 15-400A) (See Model 17F13) (Ch. 15-501A) (See Model 17F13) (Ch. 15-502) (See Model 17T13) (Ch. 15-502) (See Model 21713) (Ch. 15-502) (See Model 17113) (Ch. 15-502) (See Model 17114) (Ch. 15-502

MUNTZ 2053) 49 (Ch. TV17A7) (See Model 2053) B M49

MOTOROLA-NOBLITT SPARKS

MUNTZ-Cont.

- MUNTZ-Cont. 2054-A (Ch. 1781, 1782) (For TV Ch. only see Ch. 1781.-Set 163-60. only see Ch. 1781-Set 163-2055 (Ch. 17A7) (See PCB 33-Set 159-3 and Model M31-Set 116-10. 305900 or Ch. 1786, Above Serial No. 3619500)... 207-55 2055-A (Ch. 1781, 1782) (See Ch. 1781-Set 163-8) 2055-A (Ch. 1782, Above Serial No. 369500 or Ch. 1786, Above Serial No. 3619500]... 207-55 2055-8 (Ch. 1782) (See Ch. 1782-Set 163-8) 20556 (Ch. 1782, Above Serial No. 369500 or Ch. 1786, Above Serial No. 3619500]... 207-55 20558 (Ch. 1782) (See Ch. 1782-Set 163-8) 20556 (Ch. 1787) (See PCB 33-Set 159-3 and Model M31-Set 116-10 2056-A (Ch. 1781, 1782) (See Ch. 1781-Set 163-8) 2060

- (a) Summer (C) (See Ch. 1781, 1782) (See Ch. 1781–Sei 163-8)
 (a) Cob (Ch. 1782, Above Serial No. 369500 or Ch. 1786, Above Serial No. 369500 or Ch. 1786, Above Serial No. 369500, ... 207–5
 (a) See Ch. 1782, Above Serial No. 369500 or Ch. 1786, Above Serial No. 369500 or Ch. 1786, Above Serial No. 369500 or Ch. 1785, Ch. 1783, Ch. 1781, Ch. 1781, Ch. 1783, Ch. 1784, Ch. 1785, Ch. 1785,

MURPHY

MUSITRON

PT-10	15-20
PX	16-28
SRC-3	13-21
101 "Piccolo"	
103 "Piccolo"	
105	
202	21-27

MUTUAL BUYING SYNDICATE (See Drexel or General)

NASH

AC-152	NH2A	c)	184-9	,
NH3C .				\$
6MN082			9-25	5

NATIONAL CO.

HFS 62-14 HRO-7R, HRO-7T 50-12 HRO-500 112--7 HRO-50R1, HRO-50T1 169-11 HRO-60 202-4 •NC-TV7, NC-TV7M, NC-TV7W 1732 145-7 • T-2029, TV-2030 145-7 NATIONAL UNION G-613 ''Commuter'' G-619 571, 571A, 571B 19-23 11-35 17-22 NEWCOMB A-104R 1 H-10 H-14 Kx-30 196—8 14-20 15-22 15-23 NOBLITT SPARKS (See Arvin)

NORELCO-PHILCO

N	OI	RE	LC	0	

NORELCO	OPER
• PT200, PT300	1A30 1A35
• PT200, PT300	1843
164-7)	1A65 1A70-
OAK	1A14
(See Record Changer Listing)	4A25
	4A30 4A35
OLDSMOBILE	4A50 4A55
982375 20-25 982399 59-14	4455
	4M25 11A5
982421 87-7 982454 60-16	530,
982454	
982543	ORTI
982697, 982698 (See Model 982544 Set 96-7)	(See
-Set 96-7)	PAC
982990	(See
982699,982700 150-10 982990 225-13 983004 235-8 983091 261-10	
983091 261-10	PAC
OLYMPIC	PA-38 PA-39 41638
•DX-214, DX-215, DX-216 .106-11	41638
•DX-619, DX-700 DX-621, DX-622 106-11	41639
• DX-931, DX-932	4392) and
•DX-950	4393
RTU-3H (Duplicator) 62-15	4393
• TV-104, TV-105 67-15	4396
TV-106, 1V-107, 1V-108 [See Model TV-104—Set 67-15]	4396
OLYMPIC DX-214, DX-215, DX-216.106-11 DX-619, DX.107 DX-621, DX-622 DX-619, DX.107 DX-621, DX-621 DX-931, DX-932 106-11 DX-930 106-11 HF500 256-11 RTU-3H (Duplicator) 62-15 TV-104, TV-105 67-15 TV-104, TV-108 (See Model TV-922 58-14 TV-922 58-14 TV-928 (See Model TV-922-Set S8-14 TV-944, TV-945 67-15	and
TV-928 (See Model TV-922-Set	43960 and
58-14)	4396
TV-946 (See Model TV-104-Set	enc
J00-147 TV-945 67-15 ●TV-946 (See Model TV-104—Set 67-15) 67-15 ●TV-946 (See Model TV-104—Set 67-15) 85-10 ●TV-948 (See Model TV-104—Set 67-15) 85-10	PAC
eTV-947	
67-15) 85-10 TV-947 85-10 TV-948 [See Model IV-104—Set 67-15) 85-10 TV-949, TV-950 85-10 TV-949, TV-950 85-10 St-10, L-11 109-8 St-10, 6-502, 6-503, 4-10 6-501, 6-502, 6-503, 4-10 6-501, V-U (See Model 6-501W-U- 3-20 6-504, 6-504, 0-502-U 3-20 6-504, 6-504, 0-602 8-24 6-604, V-10, 6-604, 200, 6-604, 8-10 3-25 6-604, V-10, 6-604, 200, 6-604, 8-11 3-25 6-604, V-10, 6-604, 200, 6-604, 8-11 3-25 6-604, N-10, 6-604, 200, 6-604, 8-11 3-25 6-604, Series -504 6-604, N-10, 6-604, 200, 6-604, 8-11 -604, 8-11 6-604, N-10, 6-604, 504, 8-11 -501	C136 C146
•TV-949, TV-950	5DA
•XL-612, XL-613 109-8	5FP 100
6-501, 6-502, 6-502-P, 6-503 4-10	100
Set 3-20)	261 471 531 532
6-501W-U, 6-502-U 3-20	531
6-601W, 6-601V, 6-602 8-24	551
6-604 Series 22-21	551-1
110, 6-604W-150, 6-604-220	561 563 576
110, 6-604W-150, 6-604-220 (See Model 6-604 Series-Set	576
22-21) 6-606 4-36	568 571
6-606-4 11-17	571 572
6-606-U 6-617 11-18 4-7	581
6-617U (See Model 6-617-Set 4-7)	621 631
7-421V, 7-421W, 7-421X, 57-13 7-435V, 7-435W, 34-13	651 661
7-526	662 673A
7-532W, 7-532V	673A
4−7 4−7 4−7 4−7 4−17 421V, 7-421W, 7-421X, 57-13 457V, 7-435W, 7-421X, 57-13 7-352V, 30-21 7-532V, 30-21 7-532V, 32-15 7-532, 34-14 7-23 7-53 4−14 7-23 7-53 7-53 7-53	682 771
	861
7-724	872
7.728 (See Model 7.724-Set 29-	872 880,
7.728 (See Model 7.724-Set 29-	880, 881-
7.728 (See Model 7.724-Set 29-	880, 881- 884, 1052
7.728 (See Model 7.724-Set 29-	880, 881- 884, 1052 1054
7.728 (See Model 7.724-Set 29-	880, 881- 884, 1052 1054
7.728 (See Model 7.724-Set 29-	880, 881- 884, 1052 1054 1063 1181 1273 1472
7.728 (See Model 7.724-Set 29-	880, 881- 884, 1052 1054 1063 1181 1273 1472
7.728 (See Model 7.724-Set 29-	880, 881- 884, 1052 1054 1063 1181 1273 1472
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 8.451 48-15 8.533V, 8.533W 57-14 8-618 8-618 925, 8.934, 8.936 9451 9-435V, 9.435W 17224 1725 1725 17264 1725 1726 1727 1728 1729 1720 182 182 182 182 182	880, 881- 884, 1052 1054 1063 1181 1273 1472
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 31-22 8.451 48-15 8.533V, 8.533W 57-14 8-618 8-618 35-16 8-925, 8.934, 8.936 9-435V, 9-435W 17C24 17C24 17C24 17C24 17C3 17C5 (See Model 752-Set 126-8) 17C57 17C54 17K31 17K32 182-6 17K31 1764 1757 1764 1764 17832 182-6 17637 182-6 17637 182-6 17647 17647 182-6 17637 182-6 17647 182-6 17647 182-6 17647 182-6 182-6 <t< td=""><td>880, 881- 884, 1052 1054 1063 1181 1273 1472 1841 1941 2001 2041</td></t<>	880, 881- 884, 1052 1054 1063 1181 1273 1472 1841 1941 2001 2041
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 8.451 48-518 8.533V, 8.533W 57-14 8-618 8-618 925, 8.934, 8.936 9451 9-435V, 9-435W 17C24 17C24 17C24 17C24 17C24 17C30 17C57 (Ch. TM-17) 17C57 (Ch. TM-17) 17C53 17K32 17K31 17K41, 17K42 (Ch. TK17) 196-9 17K50, (Ch. TK17) 1764 17K31 17K32 1784	880, 881- 884, 1052 1054 1063 1181 1273 1472 1841 1941 2001 2041
7.728 (See Model 7.724—Set 29- 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.533V, 8.533W, 57-14 8.618 8.618 8.925, 8.934, 8.936, 45-19 9.435V, 9.435W, 152-11 9.727 (See Model 752-Set 126.8) 1724 9.7257 (Ch. TK.17), 216-7 9.7265 (Ch. TK.17), 196-9 9.7K53 (Ch. TK.17), 196-9 9.7K55 (Ch. TK.17), 196-9 9.7K55 (Ch. TK.17), 216-7 9.726-7 1720, 182-6 1720, 182-6	880, 881- 884, 1052 1054 1063 1181 1273 1472 1841 1941 2001 2041
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 8.451 48-518 8-513V, 8-533W 57-14 8-618 8-618 35-16 8-934, 8-533W 57-14 8-618 35-16 8-925, 8-934, 8-936 9-435V, 9-435W 17224 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1724 1725 1726 1726 1727 182-6 1733 182-6 1740 (Ch, TK17) 182-6 1740 (Ch, TK17) 182-6 1740 (880, 881- 884, 1052 1054 1063 1181 1273 1472 1841 1941 2001 2041
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 31-22 8.451 48-15 8.533V, 8.533W 57-14 8.618 35-16 8.924, 8.936 9.435W 9.435W 9.435W 9.435W 9.435W 9.435W 9.435W 9.725 9.724 17C24 170 (See Model 752—Set 126.8) 17C57 (Ch. TM-17) 176 (See Model 752—Set 126.8) 17631, 17632 1764 (Ch. TK-17) 182—6 1764 (Ch. TK-17) 1720 1720 1748 (Ch. TK-17) 182—6 17133 1720 1720 1720 1733 182—6 17134 (Ch. TK-17) 196—9 1748 (Ch. TK-17) 182—6 17134 (Ch. TK-17)	880, 881- 884, 1052 1053 1053 1053 1053 1053 181 1941 2001 2041 2105 2041 2105 2115 2115 2115 2115
7.728 (See Model 7.724—Set 29- 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451,	880, 881- 884, 1052 1053 1053 1053 1053 1053 181 1941 2001 2041 2105 2041 2105 2115 2115 2115 2115
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7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 8.451 48-518 8.533V, 8.533W 57-14 8-618 8-618 35-16 8-934, 8.936 8-512 9-435V, 9-435W 17C24 17C24 17C24 17C24 17C24 17C30 17C57 (Ch. TK-17) 17C57 (Ch. TK-17) 17C44 17K32 1713 17148 17148 17148 17148 17148 17141 17142 17143 17144 17147 17148 17147 17148	880, 881, 881, 1052 1053 1053 1053 1053 1053 1053 1053 1273 1472 1841 2004 2105 2117 2118 2147 2117 2118 2147 2117 2118 2202 2299 22 2292
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 8.451 48-518 8.533V, 8.533W 57-14 8-618 8-618 35-16 8-934, 8.936 8-512 9-435V, 9-435W 17C24 17C24 17C24 17C24 17C24 17C30 17C57 (Ch. TK-17) 17C57 (Ch. TK-17) 17C44 17K32 1713 17148 17148 17148 17148 17148 17141 17142 17143 17144 17147 17148 17147 17148	880, 881, 884, 1052 1053 1055
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.934 8.935 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.7257 9.7267 9.727 9.727 9.727 9.727 9.727 9.7204 9.727	880, 881, 884, 1052 1053 1055
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.934 8.935 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.7257 9.7267 9.727 9.727 9.727 9.727 9.727 9.7204 9.727	880, 881, 884, 1052, 1054, 10554, 105554, 10554, 105554, 105554, 105554, 105554, 105554, 105554, 1
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.934 8.935 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.7257 9.7267 9.727 9.727 9.727 9.727 9.727 9.7204 9.727	880, 881, 884, 1052, 1054, 10554,
7.728 (See Model 7.724—Set 29- 19) 19 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.934 8.935 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.7257 9.7267 9.727 9.727 9.727 9.727 9.727 9.7204 9.727	880, 881, 884, 1052, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105554, 105554, 105554,
$\begin{array}{c} 7.728 \ (\text{See Model } 7.724 {$	880, 881, 884, 1052, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105554, 105554, 105554,
7.728 (See Model 7.724—Set 29- 19) 19) 7.925, 7.934, 7.936, 7.939 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.934 8.935 8.934 8.935 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.756 9.756	880, 881, 884, 1052, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105554, 105554, 105554,
7.728 (See Model 7.724—Set 29- 19) 19) 7.925, 7.934, 7.936, 7.939 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.934 8.935 8.934 8.935 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.756 9.756	880, 881, 884, 1052, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105554, 105554, 105554,
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W, 57-14 \\ 8.618, 35-16 \\ 8.925, 8.934, 8.936, 8.936, 45-19 \\ 9.435V, 9.435W, 152-11 \\ 9.7C24, 9.435W, 152-11 \\ 9.7C24, 9.435W, 152-11 \\ 9.7C24, 100, 172, 196-9 \\ 9.7C25, 100, 172, 110, 172, 172, 1720, 182-6 \\ 9.7740 \ (Ch, TK17), 196-9 \\ 9.7745 \ (Ch, TK17), 196-9 \\ 9.7746 \ (Ch, TK17), 196-9 \\ 9.0053, 2.0C53 \ (Ch, TL20), 196-9 \\ 9.0053, 2.0C53 \ (Ch, TL20), 196-9 \\ 9.0053, 2.0C47 \ (Ch, TL20), 196-9 \\ 9.0053, 2.00$	880, 881, 884, 1052, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105554, 105554, 105554,
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$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451 & 48-18 \\ 8.4518 & 35-14 \\ 8.618 & 35-16 \\ 8.925, 8.934, 8.936 & 45-19 \\ 9.435V, 9.435W & 152-11 \\ 9.725V & 152-11 \\ 9.725V & 152-11 \\ 9.725V & 152-11 \\ 9.725V & 172-21 \\ 1724 \ (Ch. TK.17) & 216-7 \\ 9.725V & 172-21 \\ 1724 \ (Ch. TK.17) & 216-7 \\ 9.725V \ (Ch. TK.17) & 196-9 \\ 9.755V \ (Ch. TK.17) & 196-9 \\ 9.755V \ (Ch. TK.17) & 196-9 \\ 1755 \ (Ch. TK.17) & 196-9 \\ 1755 \ (Ch. TK.17) & 196-9 \\ 17748 \ (Ch. TK.17) & 196-9 \\ 17740 \ (Ch. TK.17) & 196-9 \\ 17750 \ (Ch. TK.21) \ 124-7 \\ 1770 \ (Ch. TK.21) \ 124-7 \\ 1770 \ (Ch. TK.21) \ 214-7 \\ 21770 \ (Ch. TK.21) \ 214-7 \\ 2177$	880, 881, 882, 1052, 1053, 1053, 1053, 1054, 1053, 1054, 10554,
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W, 57-14 \\ 8.618,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.942, 1762,, 182-6 \\ 1764, 1.754, 2.164, 177,, 196-9 \\ 1765, 1764, 1.754, 2.164,, 1774, 1774, $	880, 881, 884, 1052, 1054, 10554,
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W, 57-14 \\ 8.618,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.942, 1762,, 182-6 \\ 1764, 1.754, 2.164, 177,, 196-9 \\ 1765, 1764, 1.754, 2.164,, 1774, 1774, $	880, 880, 881, 884, 1052, 1053, 1053, 1181, 1273, 1472, 181, 1273, 181, 1273, 181, 1273, 181, 1273, 181, 1201, 2101, 2041, 211, 211, 211, 211, 211, 211, 220, 229, 229, 229, 220, 22, 220, 22, 220, 22, 220, 2301, 2301, 242, 2600, 2602, 2602, 2602, 2602, 2602, 272, 272, 272, 272, 272, 272, 280, 281, 284, 284,
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W, 57-14 \\ 8.618,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.942, 1762,, 182-6 \\ 1764, 1.754, 2.164, 177,, 196-9 \\ 1765, 1764, 1.754, 2.164,, 1774, 1774, $	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1181, 1273, 1472, 1814, 2010, 2100, 2100, 2100, 2100, 2117, 2117, 2114, 2100, 2117, 217,
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W, 57-14 \\ 8.618,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.925, 8.934, 8.936,, 35-16 \\ 8.942, 1762,, 182-6 \\ 1764, 1.754, 2.164, 177,, 196-9 \\ 1765, 1764, 1.754, 2.164,, 1774, 1774, $	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1181, 1273, 1472, 1814, 2010, 2100, 2100, 2100, 2100, 2117, 2117, 2114, 2100, 2117, 217,
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W,, 48-15 \\ 8.533V, 8.533W,, 48-15 \\ 8.533V, 8.533W,, 48-15 \\ 8.525, 8.934, 8.936,, 8936,, 45-19 \\ 9.435V, 9.435W,, 126-17 \\ 9.7224,, 182-7 \\ 9.7244 \ (Ch, TK17),, 196-9 \\ 9.7257, TC44 \ (Ch, TK17),, 196-9 \\ 17C57, TC44 \ (Ch, TK17),, 196-9 \\ 17C56 \ (Ch, TK20),, 196-9 \\ 17C56 \ (Ch, TL20),, 196-9 \\ 17C57, 12C72,, 12C4 121 \$	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105
$\begin{array}{c} 7.728 \ (See Model 7.724—Set 29-19) \\ 7.925, 7.934, 7.936, 7.939 31-22 \\ 8.451,, 48-15 \\ 8.533V, 8.533W,, 48-15 \\ 8.533V, 8.533W,, 48-15 \\ 8.533V, 8.533W,, 48-15 \\ 8.525, 8.934, 8.936,, 8936,, 45-19 \\ 9.435V, 9.435W,, 126-17 \\ 9.7224,, 182-7 \\ 9.7244 \ (Ch, TK17),, 196-9 \\ 9.7257, TC44 \ (Ch, TK17),, 196-9 \\ 17C57, TC44 \ (Ch, TK17),, 196-9 \\ 17C56 \ (Ch, TK20),, 196-9 \\ 17C56 \ (Ch, TL20),, 196-9 \\ 17C57, 12C72,, 12C4 121 \$	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105
$\begin{array}{c} \textbf{7.728} \ (\text{See Model } \textbf{7.724} - \text{Set } \textbf{29}.\\ \textbf{19} \\ \textbf{7.925}, \textbf{7.934}, \textbf{7.936}, \textbf{7.939} \textbf{31} - \textbf{22} \\ \textbf{8.451} & \textbf{48} - \textbf{15} \\ \textbf{8.925}, \textbf{8.934}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.018} & \textbf{35} - \textbf{16} \\ \textbf{8.925}, \textbf{8.934}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.925}, \textbf{8.934}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.925}, \textbf{8.944}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.925}, \textbf{8.944}, \textbf{8.936} & \textbf{152} - \textbf{11} \\ \textbf{17C24} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17C24} & \textbf{(Ch. TK17)} & \textbf{216} - \textbf{7} \\ \textbf{17C34} & \textbf{(Ch. TK17)} & \textbf{216} - \textbf{7} \\ \textbf{17C34} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K31}, \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31}, \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31}, \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31} & \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K35} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K35} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K36} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17T36} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17T40} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17T40} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C53} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C53} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C53} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{21C68} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{21C66} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C52} & \textbf{21C62} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{3152} & \textbf{11} & \textbf{6} \\ \textbf{355} & \textbf{350} & \textbf{355} - \textbf{350} \\ \textbf{355} & \textbf{350} & \textbf{355} - \textbf{350} \\ \textbf{355} & \textbf{350} & \textbf{350} & \textbf{350} \\ \textbf{355}$	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105
$\begin{array}{c} \textbf{7.728} \ (\text{See Model } \textbf{7.724} - \text{Set } \textbf{29}.\\ \textbf{19} \\ \textbf{7.925}, \textbf{7.934}, \textbf{7.936}, \textbf{7.939} \textbf{31} - \textbf{22} \\ \textbf{8.451} & \textbf{48} - \textbf{15} \\ \textbf{8.925}, \textbf{8.934}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.018} & \textbf{35} - \textbf{16} \\ \textbf{8.925}, \textbf{8.934}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.925}, \textbf{8.934}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.925}, \textbf{8.944}, \textbf{8.936} & \textbf{45} - \textbf{19} \\ \textbf{8.925}, \textbf{8.944}, \textbf{8.936} & \textbf{152} - \textbf{11} \\ \textbf{17C24} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17C24} & \textbf{(Ch. TK17)} & \textbf{216} - \textbf{7} \\ \textbf{17C34} & \textbf{(Ch. TK17)} & \textbf{216} - \textbf{7} \\ \textbf{17C34} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K31}, \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31}, \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31}, \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31} & \textbf{17K32} & \textbf{182} - \textbf{6} \\ \textbf{17K31} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K35} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K35} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17K36} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17T36} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17T40} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{17T40} & \textbf{(Ch. TK17)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C53} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C53} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C53} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TL20)} & \textbf{196} - \textbf{9} \\ \textbf{20C53} & \textbf{20C54} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{21C68} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{21C66} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C52} & \textbf{21C62} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{21C55} & \textbf{(Ch. TN-21)} & \textbf{214} - \textbf{7} \\ \textbf{3152} & \textbf{11} & \textbf{6} \\ \textbf{355} & \textbf{350} & \textbf{355} - \textbf{350} \\ \textbf{355} & \textbf{350} & \textbf{355} - \textbf{350} \\ \textbf{355} & \textbf{350} & \textbf{350} & \textbf{350} \\ \textbf{355}$	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105
7.728 (See Model 7.724—Set 29- 19) 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 9.4359 17C24 17C44 17K30 17K31 17K32 17K31 17K32 17K32 17K31 17K32 17K31 17K31 17K32 17K31 17K31 17K31 17K31 17K31 17K32	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105
7.728 (See Model 7.724—Set 29- 19) 7.928 (See Model 7.724—Set 29- 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.453 9.4354 9.4554 9.4554 9.454 9.454 9.454	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 105554, 105554, 105554, 105554, 105554, 105
7.728 (See Model 7.724—Set 29- 19) 7.928 (See Model 7.724—Set 29- 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.453 9.4354 9.4554 9.4554 9.454 9.454 9.454	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 10554, 10554, 10554, 10554, 10554, 10554, 10554
7.728 (See Model 7.724—Set 29- 19) 7.928 (See Model 7.724—Set 29- 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.453 9.4354 9.4554 9.4554 9.454 9.454 9.454	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 10554, 10554, 10554, 10554, 10554, 10554, 10554
7.728 (See Model 7.724—Set 29- 19) 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 9.4354 9.4554 9.4554 9.4554 9.4554 9.4564	880, 881, 884, 1052, 1054, 1053, 1054, 1053, 1054, 1055,
7.728 (See Model 7.724—Set 29- 19) 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 9.4354 9.4554 9.4554 9.4554 9.4554 9.4564	880, 881, 884, 1052, 1054, 1053, 1054, 1053, 1054, 1055,
7.728 (See Model 7.724—Set 29- 19) 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 9.4359 9.459 9.459 9.459	880, 881, 884, 1052, 1054, 1053, 1053, 1054, 1053, 1054, 10554, 10554, 10554, 10554, 10554, 10554, 10554, 10554
7.728 (See Model 7.724—Set 29- 19) 7.928 (See Model 7.724—Set 29- 19) 7.925, 7.934, 7.936, 7.939 31-22 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.451 8.4533W, 8-533W 9.435W, 9.435W 9.435V, 9.435W 17C24 17C44 (Ch. TK17) 17C57 (Ch. TK17) 17C57 (Ch. TK17) 17C57 (Ch. TK17) 17K31 (TK32 17K32 17K35 (Ch. TK17) 1762 (Ch. TK17) 1710 (Ch. TK17) 1720 (Ch. TK17) 1740 (Ch. TK17) 1740 (Ch. TK17) 1755 (Ch. TM-17) 1755 (Ch. TM-17) 1765 (Ch. TK17) 1765 (Ch. TK17) 1765 (Ch. TK17) 1765 (Ch. TK17) 1766 (Ch. TK17) 1767 (Ch. TK17) 1768 (Ch. TK17) 1769 1756 (Ch. TK17)	880, 881, 884, 1052, 1054, 1053, 1054, 1053, 1054, 1055,

RADIO	PARKVIEW
34-15	•17X
33 -15 48-16	PATHE
33–15 48–16 5–––––––––––––––––––––––––––––––––––	•17-N25, 17-RPC, 17-RPT (Ch. TAP) (Similar to Chassis) 127-12
0.4 47-16 0.0 46-17 5.E 101-8 9.A 102-9 5. 100-9 9.4 451-A 9.5 100-9 5. 100-9 5. 100-9 5. 100-9 5. 103-6 531 1335 37-14 37-14	PENTRON
5-E 101—8 102—9	(Also see Recorder Listing)
100-9	AM-T
100-9	HFP-1 253-10
5C 99–11 55 113—6	
531, 1335 "Soundcaster"	PHILCO (Also see Record Changer Listing)
	A-T1814 (Code 123) (Ch. 81, H-1,
HOSONIC	 A-T1814 (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set 224-1 and Model 53-T1824—Set 201-7) A-T1816, L (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set 221-7) and Model 53-T1824—Set 201-7) A-T1816 (Code 122) (Ch. 81A,
Electronic Labs,)	A-T1816, L (Code 123) (Ch. 81, H-1,
IFIC MERCURY	H-1A) [See PCB 83—Set 224-1 and Model 53-T1824—Set 201-7]
Mercury)	 and Model 53-11824—Set 201-7) anti Model 53-11824—Set 201-7) anti 816 (Cade 129) (Ch. 81A, D-81) anti 227-10 anti 817, HM (Cade 123) (Ch. 81, H-1, H-1A) Tel. Rec. (See PCB 83 —Set 224-1 and Model 53-11824 —Set 221-7) Anti 818 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82 —Set 223-1 and Model 53-11853 —Set 185-10) Anti 855, HM, L, W (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83 —Set 201-7) Anti 855W (Cade 129) Ch. 81A,
KARD	A-T1817, HM (Code 123) (Ch. 81,
KARD BZ042 20-26 93607 57-15 93607 187 160-7 145-8 179 See PCB 104-Set 250.1 04 Model 416387-Set 160-71 100 (See PCB 104-Set 250.1 04 Model 416387-Set 160-71 03137-Set 160-71 138, 439339 .229-8 051 (See PCB 104-Set 250.1 04 Model 416387-Set 160-71 053 (See PCE 104-Set 250.1 04 Model 416387-Set 160-71 053 (See PCB 104-Set 220.1 04 Model 439338-Set 227.81 053 (See PCB 104-Set 250.1 054 (See 1250.1 124 -220-81 055 (See PCB 104-Set 250.1	-Set 224-1 and Model 53-T1824
160-7	
79 (See PCB 104-Set 250-1	(See PCB 66-Set 203-1, PCB 82
d Model 416387—Set 160-7) 310 (See PCB 104—Set 250-1	-Set 185-10)
d Model 416387-Set 160-7)	A-T1856, HM, L, W (Lode 123) (Ch. 81, H-1, H-1A) (See PCB 83
61 (See PCB 104-Set 250-1	-Set 224-1 and Model 53-T1824
63 (See PCB 101-Set 247-1	
d Model 439338—Set 229-8)	A-T1858 (Code 128) (Ch. 91A, J-2)
d Model 416387-Set 160-7)	(See PCB 66—Set 203-1, PCB 82 —Set 223-1 and Model 53-T1853
65 (See PCB 104—Set 250-1 d Model 416387—Set 160-7) 566 (See PCB 101—Set 247-1 d Model 439338—Set 229-8)	
KARD-BELL	A-12230, L (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set 224-1 and Model 53-T1824—Set
52 12-21	201.7)
51 12–22 16–29	A-T2230 (Code 129) (Ch. 81A, D-811 227-10
44–15	H.1, H-1A) [See PCB 83—Set 224-1 and Model 53-T1824—Set 201-7) A.T2230 [Code 129] (Ch. 81A, D.81)
1-29 53-16	and Model 53-T1824-Set 201-7)
21-28 30-22 231-11	A-T2233 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82
	-Set 223-1 ond Model 53-T1853
	A-T2234 (Code 128) (Ch. 91, J-2)
D (See Model 551—Set 2-7) 2—35	(See PCB 66—Set 203-1, PCB 82 —Set 223-1 and Model 53-T1853
[See Model 561-Set 2-35] (See Model 551-Set 2-35) (See Model 551-Set 2-7) 19-24	-Set 185-10) A-T2262HM (Code 123) (Ch. 81.
(See Model 572-5et 22-22)	 A-T2262HM [Code 123] (Ch. 81, H-1, H-1A] (See PCB 83—Set 224-1 and Model 53-T1824—Set
(See Model 5/2-Jet 22-22) 22-22	
22-22 (See Model 5DB-Set 44-15) 181-8 	A-T2266, L [Code 128] (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-
	82-Set 223-1 and Model 53- T1853-Set 185-10)
8-25 13-22	A-T2271HM (Code 128) (Ch. 91A,
A 6738	62—3ei 223-1 dim Model 53- T1853—Set 185-10) ●A-T2271HM (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53- T1853—Set 18S-10)
44_16	T1853—Set 185-10) • A-T2272, L (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set 224-1 and Model 53-T1824—Set 201 7)
17-23	H-1, H-1A) (See PCB 83—Set 224-1 and Model 53-T1824—Set
31-23 , 880A 46-16 -A, 881-8 47-17	201.7) 1201.7)
-A, 881-B	2017) A.12272 [Code 129] (Ch. 81A, D-81]
2, 1052A	• A-2274, W (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set
3 18–25 1, 1181A 75–12 3 46–19	
	A-T22745 (Code 128) (Ch. 91A J-2) (See PCB 66—Set 203-1, PCE 82—Set 223-1 and Model 53- T1853—Set 185-10)
3 48-17 1, 1842 (Ch. 1840) 260-12 1, 1942 (Ch. 1840) 260-12 1, 1942 (Ch. 1840) 260-12 17, 20021 V. 260-12 1, 2002 2043, 2044 (Ch. 2040) 1, 2002 2043, 2044 (Ch. 2040) 5, 2105A 123-10 5, 2105A 123-10 5, 2105 (Ch. 2115-2) 195-9 8 204-7 7 (Ch. 2113, 2144 (Ch. 2040)	82-Set 223-1 and Model 53-
1, 1942 (Ch. 1840) 260-12 1TV. 2002TV	• A-T22755 (Code 129) (Ch. 81A,
1, 2042, 2043, 2044 (Ch. 2040)	H833367 103-101 0.4.712275 (Code 129) (Ch. 81A, D-81)
1, 2102 123-10	H-1, H-1A) (See PCB 83-Se
5, 2116 (Ch. 2115-2) .195-9	201-7)
7 (Ch. 2117)	A-T2277S (Code 128) (Ch. 91A, J-2 (See PCB 66—Set 203-1, PCB 82
1, 2142, 2133, 2144 (Ch. 2040) 233-8	Set 223-1 and Model 53-T1853 Set 185-10)
12, 2204	• A-T2279 (Code 123) (Ch. 81, H-1 H.14) (See PCB 83-Set 224.1
295TV, 2296TV 82-10	and Model 53-T1824-Set 201-7
rd	(See PCB 66-Set 203-1, PCB 82
8-TV	
1, 2142, 2133, 2144 [Ch. 2040] 2, 2204 233	201.71 ● A.T22775 [Code 128] (Ch. 91A, J-2 (See PCB 66—Set 203.1, PCB 82; — Set 223.1 and Model 53.T1853; — Set 185.10] ● A.T2279 [Code p23] (Ch. 81, H-1 H-1A] [See PCB 83—Set 224.1 and Model 33.T1824—Set 201.7; A.T2280 [Code 128] (Ch. 91A, J-2 (See PCB 66—Set 203.1, PCB 82; — Set 185.10] ● A.T2281 [Code 128] (Ch. 91A J-2] [See PCB 66—Set 203.1; PCB 82—Set 23.1 and Model 53.T1853—Set 185.10] ● A.T2288, HM [Code 123] [Ch. 81
1, 2422, 2423	PCB 82-Set 233-1 and Mode
122-0 123-10	A-T2288, HM (Code 123) (Ch. 81
Berty B2-10 1.TV B2-10 1.TV 1269 12 (See Model 230)-Set 1269 1.1.TV 1269 1.1.TV 1269 1.1.TV 1226 1.2.22 127	A-T2288, HM (Code 123) (Ch. 81 H-T, H-1A) (See PCB 83-Se 224-1 and Model 53-T1824-Se
21, 2722 (Ch. 2720) 207-6	201-7) A-T2288HMS, 5 (Code 128) (Ch
2, 2743 (Ch. 2740) 238-10	201-7] A.T2288HMS, S (Code 128) (Ch 91A, J-2] (See PCB 66-Se 203-1, PCB 82-Set 223-1 an Model 53-T1853-Set 185-10) A.T2289 (Code 128) (Ch. 91A, J-2 (See PCB 66-Set 203-1, PCB 8; Set 185-10) A.T2292 1 (Code 128) (Ch. 94 A
120-9 131V 129-8	Model 53-T1853-Set 185-10}
1A	(See PCB 66—Set 203-1, PCB 8
12, 2843, 2844 (Ch. 2740) 238-10	
16, 2847 (Ch. 2840) (See Model	A-T2292, L (Code 128) (Ch. 94, A
21, 2922	Ch. Only See PCB 85-Set 266-
12 (Ch. 2940-1)	A-T2294 (Code 128) (Ch. 94, J-
1, 292 213-4 1, (Ch. 2940-1) 238-10 12 (Ch. 2840) 242-7 14, (Ch. 2840) (See Model)	and Radio Ch. RT-11) (For TV Ch Only See PCB 85-Set 226-1 an
94_6	
42 (Ch. 3040-1)	H-1, H-1A) (For TV Ch. see PC
1840 (See Model 1841)	T1824-Set 201-7, for UHF Tune
2040 (See Model 2041) 2115-2 (See Model 2115)	see Model UT218-Set 223-9) A-UT1817 (Code 1231 (Ch 81 H-1)
2117 (See Model 2117)	A-UTIBI7 (Code 123) (Ch. 81, H-1 H-1817 (Code 123) (Ch. 81, H-1 H-1A1 (For TV Ch. see PCB 83– Set 224-1 and Model 53-T1824– Set 201-7, for UHF Tuner se Model UT218–Set 223-9)
2710 (See Model 2723)	Set 201-7, for UHF Tuner se
. 2720 (See Model 2721) . 2740 (See Model 2742)	Model UT218—Set 223-9) •A-UT1818 (Code 128) (Ch. 91A
2840 (See Model 2841) 2940-1 (See Model 2941)	A-UT1818 (Code 128) (Ch. 91A J-2) (See PCB 66Set 203-1, PC 82Set 223-1 and Model 53 T-1853Set 185-10)
1841Set 2427) 91V 946 41 (ch. 2940-1) 238-10 42 (ch. 3040-1) 2427 42 (ch. 3040-1) 2427 1840 (See Model 2041) 7 2115-2 (See Model 2011) 202-2 22115-2 (See Model 22115) 2117 (See Model 22115) 2710 (See Model 2723) 2720 (See Model 2723) 2740 (See Model 2721) 2740 (See Model 2742) 2740 (See Model 2841) 2940-1 (See Model 2841) 3040-1 (See Model 3042) 3040-1 (See Model 3042)	T-1853-Set 185-10)

17-N25, 17-RPC, 17-RPT (Ch. TAP)	53-T1824-Set 201-7, for UHF
(Similar to Chassis) 127-12	Tuner see Model UT21B—Set 223-9)
PENTRON (Also see Recorder Listing)	• A-UT1858 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB
AM-T	82—Set 223-1 and Model 53- T1853—Set 185-10)
AM.T	• A-UT2230 (Code 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83-
MM4	H-1A) (For TV Ch. see PCB 83— Set 224-1 and Model 53-T1824—
PHILCO (Also see	Set 224-1 and Model 53-T1824- Set 201-7, for UHF Tuner see Model UT218-Set 223-9)
Record Changer Listing) A-T1814 (Code 123) (Ch. 81, H-1,	Model UT218—Set 223-Y) • A-UT2232 (Code 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83— Set 224-1 and Model 53-T1824— Set 201.7 (r. UHE Tuper see
A-T1814 (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83-Set 224-1 and Model 53-T1824-Set 201-7)	H-1A) (For IV Ch. see PCB 83- Set 224-1 and Model 53-T1824-
A-T1816, L (Code 123) (Ch. 81, H-1,	Set 224-1 and Model 33-11824- Set 2201-7, for UHF Tuner see Model UT218) 6-AUT2233 (Code 128) (Ch. 91A, J-2) (See PCB 66-Set 203-1, PCB 82-Set 223-1 and Model 53- T1853-Set 185-10 AUT2324 (Code 128) (Ch. 91A)
and Madel 33-11824—Set 201-7) A-11816, (Code 123) (Co, 81, H-1, H-1A) (See PCB 83—Set 224-1 and Madel 53-11824—Set 201-7) A-11816 (Code 129) (Ch. 81A, D-81)	A-UT2233 (Code 128) (Ch. 91A,
A-T1816 (Code 129) (Ch. 81A,	J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-
A-T1817, HM (Code 123) (Ch. 81,	T1853—Set 185-10) • A-UT2234 (Code 128) (Ch. 91A,
H-1, H-1A) Tel. Rec. (See PCB 83	11633—3ef 103-101 A-UT2234 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53- T1853—Set 185-10 A-UT2266, L (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-T1853—Set 185-101 A-UT227 (Code 123) (Ch. 81.
-Set 201-7)	82—Set 223-1 and Model 53- T1853—Set 185-10)
A-T1818 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82 —Set 223-1 and Model 53-T1853 —Set 185-10)	A-UT2266, L (Code 128) (Ch. 91A,
	PCB 82-Set 223-1 and Model
	53-T1853—Set 185-10) • A-UT2272 (Code 123) (Ch. 81,
-Set 224-1 and Model 53-T1824	■ A-UT2272 (Code 123) [Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner see Model UT21B—Set 223-9)
-Set 201-7)	T1824-Set 201-7, for UHF Tuner
D-81)	see Model UT218-Set 223-9] • A-UT2272 (Code 129) (Ch. 81A,
(See PCB 66—Set 203-1, PCB 82	
	D.81)
A-T2230, L (Code 123) (Ch. 81,	83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner
A-T2230, L (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set 224-1 and Model 53-T1824—Set	see Model UT218-Set 223-9)
201-7) A-T2230 (Code 129) (Ch. 81A, D-81)	H-1, H-1A) (For TV Ch. see PCB
D-81)	83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner
D-81)	see Model UT218-Set 223-9)
and Model 53-T1824-Set 201-7)	H-1, H-1A) (For TV Ch. see PCB
(See PCB 66-Set 203-1, PCB 82	83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner
and Madel 33-T1824—Set 201-71 A-7233 (Cade 128) (Ch. 91 A. J-21 (See PCB 66—Set 203-1, PCB 82 —Set 223-1 and Madel 53-T1853 —Set 185-10] A-72234 (Cade 128) (Ch. 91, J-21 (See PCB 66—Set 203-1, PCB 82 —Set 223-1 and Madel 53-T1833 —Set 185-10] A-72262HM (Cade 123) (Ch. 81, H-1, H-1A) (See PCB 83—Set 224-1 and Madel 53-T1824—Set 2201-7)	83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner see Model UT21B—Set 223-9) A-UT2277 (Code 123) [Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner see Model UT21B—Set 223-9) A-UT2279 (Code 123) [Ch. 81, H-1, H-1A) [For TV Ch. see PCB 83—Set 224-1 and Model 53- T1824—Set 201-7, for UHF Tuner see Model UT21B—Set 223-9) A-UT2280 (Code 128) (Ch. 91A, J-2) [See PCB 66—Set 203-1, pCB 82—Set 223-1, and Model 53-T1833—Set 185-10) A-UT2281 (Code 128) (Ch. 91A, J-2] (See PCB 66—Set 203-1, pCB 82—Set 223-1, and Model 53-T1833—Set 185-10] PCB 82—Set 223-1, and Model 53-T1833—Set 185-10] A-UT228 (Code 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83— Set 224-1 and Model 53-T1824—
(See PCB 66—Set 203-1, PCB 82	J-2) (See PCB 66-Set 203-1,
-Set 223-1 and Model 53-T1853	53-T1853-Set 185-10)
A-T2262HM (Code 123) (Ch. 81,	A-UT2281 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1,
224-1 and Model 53-T1824-Set	PCB 82—Set 223-1, and Model 53-T1853—Set 185-101
201-7) A-T2266, L (Code 128) (Ch. 91A,	A-UT2288 (Code 123) (Ch. 81, H-1,
A-T2266, L (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Mode! 53-	Set 224-1 and Model 53-T1824-
T1853-Set 185-10)	Set 224-1 and Model 53-T1824- Set 201-7, for UHF Tuner see Model UT218-Set 223-9)
J-2) [See PCB 66-Set 203-1, PCB	●A-UT2289 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1,
82-Set 223-1 and Model 53- T1853-Set 185-10)	Model UT218—Set 223-9] A. UT2289 (Code 128) (Ch. 91A, 1-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1, and Model 53-T1853—Set 185-10] A. UT2292U (Code 128) (Ch. 94A, 1-5 and Radio Ch. RT-10] (For TV Ch. Only See PCB 85—Set 226-1 and Model 53-T2285—Set 213-5 B569 (Code 121) 226—13 B570 (Code 121) (See Model B570 —Set 226–13)
J-21 (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53- T1853—Set 185-10) A-T2271Hw (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53- T1853—Set 185-10) T1853—Set 185-10 H (Code 122) (Ch. 81, H (24) H (A) (See PCB 83—Set 201.77 m/ Model 53-11824—Set 201.77	A-UT2292L (Code 128) (Ch. 94A,
224-1 and Model 53-T1824—Set 201-7)	Ch. Only See PCB 85-Set 226-1
A-T2272 (Code 129) (Ch. 81A,	and Model 53-T2285—Set 213-5) B569 (Code 121)
A-12272 [Code 129] (Ch. 81A, D-81]	B570 (Code 121)
224-1 and Model 53-T1824-Set	B572 (Code 121) (See Model 8570
201-7) A-T2274S (Code 128) (Ch. 91A,	
J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-	B549 (See Model B650-Set 226-5)
T1853-Set 185-10)	B650
201-7] &-122745 (Code 128) (Ch. 91A, J-2] (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53- T1853—Set 185-10] A-122755 (Code 129) (Ch. 81A, 227-10 47077 (Code 129) (Ch. 81A, 227-10	12) B-652
D-81)	8-652
201.7)	B710
A-T2277S (Code 128) (Ch. 91A, J-2)	B710
Set 223-1 and Model 53-T1853	701-Set 193-6)
A-T2279 (Code 123) (Ch. 81, H-1,	B714 (Codes 121, 123) 229-10 B714X (Code 121)
(See PCb co-Set 203-1; PCb 22 Set 223-1; and Model 53-T1853 Set 185-10] A-T2279 (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83Set 224-1 ond Model 53-T1824Set 201-7) T2020 (C. 4: 198) (Ch. 01, 4: 12)	B804 (See Model 53-804-Set 210-4)
(See PCB 66-Set 203-1, PCB 82	B.956 218-8
	B1350 (See Mode) 53-1350-Set
	203-7)
52 T1952 Set 185.101	B-1352
A-T2288, HM (Code 123) (Ch. 81,	B1752
A-T2288, HM (Code 123) (Ch. 81, H-1, H-1A) (See PCB 83-Set 224-1 and Model 53-T1824-Set 201-7)	B1753
201-7) A-12288HMS, 5 (Code 128) (Ch.	B1756
91A, J-2) (See PCB 66-Set 203-1 PCB 82-Set 223-1 and	214-8) 81756
Model 53-T1853-Set 185-10)	Model 802-Set 18-24) C-4608 (Code 122) (See Mopor
(See PCB 66-Set 203-1, PCB 82	Model 802 Revised—Set 42-19) C-4908 (See Mopar Model 805—Set
201-7) A-122881MAS, S (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-T1853—Set 185-10) A-12289 (Code 128) (Ch. 91A, J-2) (See PCB 66—Set 203-1, PCB 82 —Set 185-10) A-12292 (Code 128) (Ch. 94 A A-12292 (Code 128) (Ch. 94 A	71-11)
 A-T2292, L (Code 128) (Ch. 94, A, J-5 and Radio Ch. RT-10) (For TV 	C-5009 (See Mopar Model 809—Set 71-11)
5et 185-10) A-12292, L (Code 128) (Ch. 94, A, J-5 and Radio Ch. RT-10) [For TV Ch. Only See PCB 85-Set 266-1 and Model 53-12285-Set 213-5) A-12294 (Code 128) (Ch. 94, J-5 and Radio Ch. RT-11) (For TV Ch. Only See PCB 85-Set 226-1 ond Model 53-12285-Set 213-5) A-UTIBIA L (Code 123) (Ch. 81, L (Code 123) (Ch.	C-5010 (See Mopar Model 805-
A-T2294 (Code 128) (Ch. 94, J-5	C-5109 (See Mopar Model 815—Set 139-8)
Only See PCB 85-Set 226-1 and	C-5110 (See Mopar Model 816—Set 139-8)
Model 53-T2285-Set 213-5) • A-UT1816, L (Code 123) (Ch. 81.	C-5111 (See Mopar Model 817—Set
H-1, H-1A) (For TV Ch. see PCB	139-8) C-5209 (See Mopar Model 824—Set 202-3)
Model 33-12283-Set 213-3) A-UT1816, L [Code 123] (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83-Set 224-1 and Model 53- T1824-Set 201-7, for UHF Tuner see Model UT218-Set 223-9)	C-5409 (See Mopar Model 830—Set
A-UT1817 (Code 123) (Ch. 81, H-1,	249-10) CR-2 35-17
H-1A1 (For TV Ch. see PCB 83- Set 224-1 and Model 53-T1824-	CR-4, CR-6 33-17
● A-UT1817 (Code 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83— Set 224-1 and Model 53-T1824— Set 201-7, for UHF Tuner see Model UT218—Set 223-9)	CR-8 38-13 CR-9 44-17

	Ρ	н	ILC	co	0	ont	•
•	A	٠U	IT1	85	6,	HM,	1

- (-U11856, HM, L, W (Code 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83-Set 224-1 and Model 53-T1824-Set 201-7, for UHF Tuner see Model UT21B-Set 23.0

- - 226-5 ee Model 52-640-Set 153-
 - 234-10 ee Model 53-656-Set 187-

 - 223---8 Code 121) (See Model 8710 + 223-8) (Code 121) (See Model 53--Set 193-6) Codes 121, 123) ...229-10 (Code 121) ...229-10 (See Model 53-804--Set 4)
 - 218—8 259–11 (See Model 53-1350—Set 7)

 - (See Model 53-1750-Set 7)
 - (See Model 53-1754—Set B) 241-10 259-11
 - 259-11 {Code 121} (See Mopor 1 802--Set 18-24) (Code 122) (See Mopor 1 802 Revised--Set 42-19) (See Mopor Model 805--Set

 - [See Mopar Model 809-Set
 - (See Mopar Model 805-1-11)
 - (See Mopar Model 815—Set 8) (See Mopar Model 816—Set 8) (See Mopar Model 817—Set 9)
 - See Mopar Model 824-Set
 - 3) (See Mopar Model 830—Set 10) 35-17 33-17 38-13 44-17 R-6
- Set 201-7, for UHF Tuner see Model UT218—Set 223-9) (-UT1818 (Code 128) (Ch. 91A, J-2] (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-T-1853—Set 185-10)
 CR-9
 44-17

 CR-9R (See Model CR-9—Set 44-17)
 CR-12

 CR-12
 39-16

 CR-501
 142—9

 CR-503
 128-10

PHILCO-Cont.

- PHILCO-Cont.

 CR-505
 130-10

 D-5107 (See Mopar Model 813-Set

 139-8)
 D-5207 (See Mopar Model 820-Set 202-3)

 D-5407 (See Mopar Model 820-Set 202-3)

 D-5407 (See Mopar Model 820-Set 20-26)

 Set 202-3)

 P-4635 (See Packard Model PA-393007-Set 57-15)

 P-5106 (See Mopar Model 812-Set 139-8)

 P-5206 (See Mopar Model 812-Set 139-8)

 Set 20-23)

 P-5206 (See Mopar Model 819-Set 20-23)

 P-5206 (See Mopar Model 819-Set 20-23)

 Set 262-3;

 P-4908 (See Mopar Model 803-Set 4624-Set 21-32)

 Set 66-12

 S-6427 (See Studeboker Model A22-Set 12-32)

 S-132 (See Studeboker Model A22-Set 12-32)

 S-332 (See Studeboker Model A22-Set 12-32)

 S-332 (See Studeboker Model A22-Set 12-32)

 S-332 (See Studeboker Model A22-Set 123-8)

 S-332 (See Studeboker Model A22-Set 123-8)

 S-332 (See Studeboker Model A22-Set 123-8)

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- 2300—Sef 229-14) UN6-100 ... 19–26 UN6-400 ... 30–23 UN6-450 ... 18–26 UN6-500 ... 17–24 UT20A, B Tel, UHF Tuner (See PCB B2—Sef 223-1) UT20D Tel, UHF Tuner (See PCB 111 —Sef 260-1] UT-21A, B Tel, UHF Tuner (See PCB 111 —Sef 260-1] UT-21A, B Tel, UHF Tuner (See PCB 111 —Sef 260-1] UT-21A, B Tel, UHF Tuner (See Model A-UT2272—Set 227-10] UT21D Tel, UHF Tuner (See Model 188U3000—Sef 227-10] B83000 (Code 140) (Ch, R-191, D-188J000 (Code 130) (Ch, R-181, D-181) (See Model 188J300—Sef 260-1] (Alto see PCB 111—Sef 260-1] (Alto see PCB 111—Sef 260-1] (See Model 188J300—Sef 277-10] B83100, UK, i (Code 130) (Ch, R-191, D-191) (Alto see PCB 111—Sef 260-1] (See Model 183000—Sef 277-10] B83100, UC (Code 140) (Ch, R-191, D-191) (Alto see PCB 111—Sef 260-1] (See PCB 111—Sef 260-1] (Code 130) (Ch, R-191, D-191) (Alto see PCB 111—Sef 260-1] (See PCB 111—Sef 271-10] (See PCB 111—Sef 271-10] (See Model 183000—Sef 231-12] B803100 (Code 130) (Ch, R-181, D-181] (See Model 183000—Sef 231-12] B284000 (Code 130) (Ch, R-181, D-181] (See Model 183000—Sef 231-12] D-181] (Se

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A 200. • Denotes Television Receiver.

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 \$52-11850-W (Code 124) (Ch. 71, G1) (Also see PCB 57—Set 191-52-71882 (Code 121) (Ch. 44, D4, D4A) (Also see PCB 57—Set 191-1)

 for Radio Ch. see Set 139-2A)

 52-540, 52-540, 52-541, 52-541, 52-541, 52-541, 52-541, 52-541, 52-541, 52-541, 52-542, 52-541, 52-542, 52-552, 52-542, 52-552, 52-542, 52-552, 52-552, 52-5

10) • 53-T1827, -F, -HM (Code 128) (Ch. 91, J-2) (See PCB 66—Set 203-1, PCB 82—Set 223-1 and Model 53-T1853—Set 185-10)

107

Denotes Television Receiver.

PHILCO--Cont. •51-11872 (Code 122) (Ch. 35, CP1 and Rodio Ch. RT-4)...135-10 •51-11874 (Code 121) (Ch. 391, CP1 and Rodio Ch. RT-4)...135-10 •51-11875 (Code 121) (Ch. 391, CP1 and Rodio Ch. RT-2) (For TV Ch. see Set 135-10, for Rodio Ch. see Model 51-12102--Set 1322-10] •51-171876 (Code 121) (Ch. 391, CP1 and Rodio Ch. RT-4)...135-10 •51-72102 (Code 122) (Ch. 35, F21 •51-72130 (Code 121) (Ch. 35, F21 •51-72132 (Code 121) (Ch. 35, F21 •51-72132 (Code 121) (Ch. 382; •51-12133 (Code 121) (Ch. 3R2, 132-10 FR2) 51-T2134 (Code 124) (Ch. 35, F2) 132-10 51-530 51-532 51-534 51-537, 51-5371 51-629 51-631 51-632 51-632 51-930, 51-931, 51-932. 51-934 122---/ 126-10 136-13 106-12 136-13 153-11 102-10 130-11 51-1730, 51-1730 (L)... 51-1730, 51-1730 (L)... 51-1731, 51-1732 51-1733, 51-1733 (L), 140—8 124—7 51-1734 137-9 51-1733, 51-1733, 1(1), 51-1733
 52-11610 (Code 122) (Ch. 32, C1) (See Model 51-11601, Code 122 -Set 138-7)
 52-11612 (Code 122) (Ch. 32, C1) (See Model 51-11601, Code 122 -Set 138-7)
 52-11802 (Code 123) (Ch. 37, C2) (See Model 51-11800—Set 148-13) • 52-11810(c, n, 148-13 C2) • 52-11812 (Code 122) (Ch. 33, C2) • 148-13 • 52-11812 (Code 123) (Ch. 37, C2) • 52-11812 (Code 123) (Ch. 37, C2) 148-13 Stab Model 31-11600—Set 148

 (3)
 (3)
 (3)
 (5)
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 (6)
 (10)
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 (5)
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PHILCO-Cont.

• 52-T1842 {Code 123} {Ch. 37, C21 148-13

48-13 • 52-T1842L (Code 124) (Ch. 33, C2) (See Model 52-T1842—Set 148-13)

(See model, Sec. 12) 13) 52-11844 (Code 121) (Ch. 41-D1, DA1) (See PCB 56—Set 190-1 and Model 52-71206—Set 171-9) 52-71844 (Code 122) (Ch. 33, C2) 148-13 148-13

• 52-T1844 (Code 123) {Ch. 37. C21 148-13 • 52-T1844 (Code 124) (Ch. 33, C2) 148-13

• 52-11845 (Ch. 3R2, CR2) (Code 124) (See Model 51-11833—Set 135-10)

135-10) • 52-T1850 (Code 121) (Ch. 4), D1, D1A) (See PCB 56—Set 190-1 and Model 52-T2106—Set 171-9)

PHILCO-Cont.

50-T1630, Code 14 -10) 50-T1630 •50-T1632, 50-T1633 •50-T1632, 50-T1632 •50-T1632, 50-T1

50-520, 50-520-1 50-522, 50-522-1, 50-524. 50-526 50-527, 50-527-1 50-620 50-621 96 80-11

10) •51-T1606 (Code 132) (For Defl. Ch. see Model 50-T1600 (Code 121)— Set 91A-10, for RF Ch. see Model 50-T1600 (Code 122)—Set 110-

10) •51-T1607 (Code 121) (Ch. 33, C1) 138—7 •51-T1607 (Code 122) (Ch. 32, C1) 138—7 138—7 •51-T1607 (Code 122) (Ch. 32, C1) 138—7 •51-T1607 (Code 122) (Ch. 32, C1)

●51-1160/ [Loae 122] (Ch. C, L] {See PCB 20 - Set 134-1 and Model 50-11600-Set 110-10] (See PCB 20 - Set 134-1 and Model 50-11600-Set 110-10] ●51-11634 (Code 122) (Ch. B, J] (See PCB 20 - Set 134-1 and Model 50-11600-Set 110-10] ●51-11634 (Code 123) (Ch. 33, C1) -51-11634 (Code 124) (Ch. 32, C1) -51-11634 (Code 124) (Ch. 32, C1) -52-01 ●51-T1800 (Code 121) (Ch. 33. (148-•51-T1800 (Code 122) (Ch. 32, C2) •51-T1800 (Code 122) (Ch. 32, C2) 148-13

•51-T1830 (Code 121) (Ch. 33, C2) •51-T1830 (Code 121) (Ch. 33, C2)
 148-13

 •51-T1833
 {Code 121}

 (Ch. 3P1, CP1)
 135-10

 •51-T1834
 (Code 121)

 (Ch. 33, C2)

 148-13
 ●51-T1834 (Code 121) (Ch. 33. C21) (R8-13 (CR3) ●51-T1835 (Code 121) (Ch. 372. CR3) ●51-T1836 (Code 122) (Ch. 34. C31) ●51-T1836 (Code 123) (Ch. 34. C31) ●51-T1838 (Code 124) (Ch. 37. CR3) ●51-T1870 (Code 121) (Ch. 37. CP1) ●51-T1871 (Code 121) (Ch. 37. CP1) ●51-T1877 (Code 121) (Ch. 37. CP1) ●51-T1877 (Code 121) (Ch. 37. C91) ●51-T1877 (Ch. 37. C91) ●51-T1877 (Ch. 37. C91) ●51-T1877 (Ch. 37.

• 51-T1872 (Code 121) (Ch. 3P1, CP1 and Radio Ch. RT-4)...135-10

www.americanradiohistory.com

1221, 47-1401 49-1401 (See Model 49-1405—Set 54-24) 54-24 NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200.

 PHILCO-Cont.

 •228U4307HM
 (Code 140)
 (Ch.

 R-191U, D-191)
 (Also see PCB
 111--Set 260-1)
 .231-12

 •228U4307HM
 (Code 141)
 (Ch.
 R-192U, D-191)
 (See PCB
 111--Set 260-1)
 .231-12

 •228U4307HM
 (Code 141)
 (Ch.
 R-192U, D-191)
 (See PCB
 111--Set 260-1)
 .241-11

 •228U4308 (Code 150)
 (Ch. R-207, D-208)
 .236-10
 .236-10

 •2488U606, L
 (Ch. R-207, D-208)
 .236-10
 .248U6300
 (Ch. R-207, D-208)
 .246-10

 •2488U6300
 (Ch. R-207, D-208)
 .236-10
 .248U6300
 .236-10
 .248U6300
 .236-10

 •2488U6300
 (Ch. R-207, D-208)
 .236-10
 .248U6300
 .236-10
 .248U6300
 .236-10

 •2488U6300
 (Ch. R-207, D-208)
 .236-10
 .236-10
 .236-10
 .236-10

 •248U6300
 (Ch. R-207, D-208)
 .236-10
 .236-10
 .236-10
 .236-10

PHILCO-Cont.

D-181) (See Model 1883000—Set 227-10) 46-131 ...5-13 46-132 ...4-20 46-132 ...4-20 46-132 ...4-20 46-200 Series ...1-24 46-200 Series ...1-24 46-200 Series ...1-24 46-200 Series ...1-24 46-250 ...46-201 ...46-202 46-250 ...46-201 ...46-202 46-420 ...46-201 ...46-202 46-427 ...421-1 ...46-22 46-427 ...421-1 ...5-12 46-427 ...421-1 ...5-12 46-427 ...421-1 ...5-12

(Revised)

46-480

46-120

46-1201

46-1201 (Revised) 46-1203 46-1209 46-1213 46-1226 47-1226 47-1226 47-1227 47-1230 48-141, 48-145 48-150 48-200 48-

48-150 48-200, 48-200-1 48-206 48-214 48-225, 48-230 48-250, 48-250-1 48-300 48-360 48-360 48-360, 48-460-1 48-461

48-401 48-464 48-472, 48-472-1 48-472 (Revised)

•48-700 •48-1000, 48-1000-5 (Code 122) •48-1001, 48-1001-5 (Code 121) •48-1001, 48-1001-5 (Code 121 and 122) •53-17 ● 48-1001, 48-1050-5 (Code 1 ● 48-1050, 48-1050-5 (Code 1 53

48-1274, 40-1274, 40-127 48-1282 5-18 48-1283 (See Model 48-1282—Set 35-18) 48-1284 45-20 48-1286 51-15 48-1290 47-18

48-475 48-482 48-485

48-1200

48-1200 48-1201 48-1253 48-1256 48-1260 48-1262 48-1263 48-1264

·48-2500

122) 49-101

49-602

49-603 49-605

49-900-49-901 49-902 49-904 49-905 49-906 49-909

48-1264 48-1266 48-1270 48-1274, 48-1276

49-101 49-500, 49-500-1 49-501, 49-501-1 49-503 49-505 49-505 49-506 49-601

49-607 49-900-E, 49-900-I

49-1002 (Code 121)... 49-1040 (Code 121)... 49-1040 (Code 121)... 49-1040 (Code 123)... 49-1075 (Code 121)

 49:1076 (Code 121 and 122)

 93.11

 94:1076 (Code 122)

 93.11

 94:1076 (Code 123)

 93.11

 122)

 93.11

 92.5

 49:1076 (Code 123)

 92.100

 49:107

 49:107

 49:106

49-1100 49-1101 49-1101 49-1101 (Codes 121 ord 123) 70-6 49-1175 (Codes 122, 124), 92-5 49-1175 (Codes 122, 124), 92-5 49-1175 (Codes 121, 123), 93A-11 49-1240 (Codes 121, 123), 93A-11 49-1278 (Code 124) 92-5 49-1278 (Code 122) 93A-11 49-1278 (Code 122) 93A-11 49-1278 (Code 122) 93A-11 49-1278 (Code 122) 92-5 49-1401 45-21 45-2140 (See Model 49-1405-54

2-12 10-24 6-22 5-12 2-25 19-25

4-35 29-21 6-23 13-24 33-18 25-23 34-16 33-19 37-15 33-19 37-15 33-19 37-17 38-14 34-17 38-15 26-20 43-15

48-18 40-14

30-24

29-20 31-25 36-17

34-18

31-25 35-19 32-18 36-18 39-15 42-20 41-17

21 and 89–10 87—8 48–19

56-18 52-15 54-17 53-18 48-19 42-21 41-18 59-15 58-15 58-15 58-15 56-19 51-16 58-16 52-16 57-16

914 -10 91A-10 92-5

• 2284107, L [Code 140) (Ch. R-191, D-191) (See Model 1883002—Set 231-12)

PHILCO-Cont.

231-121 2284108 [Code 150] (Ch. 8-201, 2284108 [Code 150] (Ch. 8-201, 2284109M [Code 140] (Ch. 8-191, 2284109M [Code 140] (Ch. 8-191, 2-201) [Ch. 8-191, 2-201] [Ch. 8-191, 2-201,

D-191) [See Model 1883002-Set 231-12] • 2284150 [Code 140] (Ch. R.191, D-191] [Aito see PCB 111-Set 260-1] • 2284150[Code 140] (Ch. R.191, D-191] [See PCB 111-Set 260-1] • 2284301 [Code 140] (Ch. R.191, D-191] (Aito see PCB 112-Set 260-1] • 2284302 [Code 140] (Ch. R.191, D-191] [Aito see PCB 123-12] • 2284303 [Code 130] [Ch. R.191, D-191] [Aito see PCB 123-12] • 2284303 [Code 130] [Ch. R.191, D-191] [Aito see PCB 13-5et 201] [Aito see PCB 13-5et 260-1] [Aito see PCB 13-5et 270-5et 2

22804000 (Code 130) (Ch. R.181U, D-181).
 22710
 22804000X, XD (Code 130) (Ch. R.181, D-181) (See Model 18803000-Set 227-10)
 22804001, E, L (Code 130) (Ch. R.181, D-181) (See Model 18803000_Stet 227-10)
 22804002, L (Code 140) (Ch. R.191U, D-191) (Also see PCB 11)
 Set 240-1).
 231-12
 22804002, L (Code 140) (Ch. R.191U, D-191) (Also FCB 11)
 Set 240-1).
 231-22
 22804002, L (Code 140) (Ch. R.191U, D-191) (Also FCB 11)
 Set 240-1).
 231-12
 22804002, L (Code 141) (Ch. R.192U, D-191) (See FCB 111-Set 260-1)
 231-12
 22804003 (Code 130) (Ch. P.101)

231-12) • 28844003 (Code 130) (Ch. R-181, D-181) (See Model 1883000— set 227-10) • 22844004 (Code 140) (Ch. R-191U, D-191) (Alio see PCB 111—Set 200-1 and Model 22844004 -Set 231-12 • 22844004 (Code 141) (Ch. R-192U, D-191) (See PCB 111—Set 200-1 and Model 22844004—Set 231-• 22844008 - 23844004 -Set 231-

and Model /2804004--3et /231-12) 22804008, 22804009 [Code 150] (Ch. R-201, D-201].....241-11 *22804100 [Code 130] (Ch. R-181U, D-181].....227-10 *228041004 [Code 130] (Ch. R-181U, D-181].....227-10] *228041001 [Code 130] (Ch. R-181U, D-181].....227-10 *228041002 [Code 130] (Ch. R-181U, D-181] See Model 22804000--5et 227-10] *22804000--5et 227-10] *22804000--5et 227-10]

Set 231-12) •228U4302 (Code 140) (Ch. R-191U, D-191) (Also see PCB 111-Set 260-1) •228U4302 (Code 141) (Ch. R-192U, D-191) (See PCB 111-Set 260-1 and Madel 228U4302-Set 231-12)

D-191) (See PCB 111 -Set 260-1 and Model 22BU4304 -Set 231-12)

12) • 228U4306, L (Code 140) (Ch. R-191U, D-191) (Also see PCB 111-Set 260-1) • 228U4306, L (Code 141) (Ch. R-192U, D-191) (See PCB 111-Set 260-1 and Model 228U4306-Set 231-12)

•22BU4108 (Code 150) (Ch. R-201

PHILCO-RCA VICTOR

PHILCO-Cont.

- Hinked-Conf., 633-11852 (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1).
 Sor T1852 (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 191-1 and Model 52-T1802—Set 191-1 and Model 52-T1802—Set 191-1 and Model 52-T1802—Set 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 201-7)
 Sor T1852H (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 201-7)
 Sor T1852L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 201-7)
 Sor T1852L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 1979 ond Model 53-T1825A (Code 124) (Ch. 71, G-1) (See PCB 86—Set 203-1)
 Jor PCB 853, L (Code 126) (Ch. 91, J-2) (See PCB 66—Set 203-1)
 Sor T1853, L (Code 126) (Ch. 91, J-2) (See PCB 66—Set 203-1)
 Sor T1853, L (Code 123) (Ch. 81, H-1, H-1, H-1A) (Also see PCB 83—Set 185-10)
 Sor T1853, L (Code 123) (Ch. 81, H-1, H-1, H-1A) (Also see PCB 66—Set 203-1)
 Sor T1853, L (Code 123) (Ch. 81, H-1, H-1, H-1A) (Also see PCB 83—Set 223-1) and Model 53-T1883 (Code 123) (Ch. 81, H-1, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T1884 (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T1884 (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T1884 (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T2122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T2122, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 224-1)
 Sor T2225, L (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83—Set 2

- 201-7 53-T2260 (Code 123) (Ch. 81, H-1, H-1A) (Also see PCB 83 Set 224-1) 201-7 \$53-T2260 (Code 125) (Ch. 42, G21 186-10
- S3-12260 [Code 123] [Ch. 12, 34]
 S3-12260 [Code 123] [Ch. 12, 34]
 HalAi [Alio see PCB 31-52 224-1]
 224-1]
 23-12262 [Code 125] [Ch. 42, C2]
 S3-12264 [Code 123] [Ch. 31, H-1,
 H-1Ai [Chie 123] [C

- 1.4)
 1410
 188--361

 224-1)
 201--7

 53-12264, [Code 125]
 1Ch, 42, G2)

 1.1)
 168-10

 53-12266, [Code 126]
 128-10

 53-12268, [Code 126]
 128-10

 53-12268, [Code 126]
 128-10

 53-12268, [Code 126]
 128-10

 53-12269, [Code 126]
 128-10

 53-12269, [Code 126]
 128-10

 53-12269, [Code 126]
 128-10

 53-12270, [Code 128]
 128-10

 53-12270, [Code 126]
 128-10

 53-12271, [Code 126]
 128-10

 53-12271, [Code 126]
 128-10

 53-12271, [Code 126]
 128-10

 53-72271, [Code 126]
 128-10

 53-72271, [Code 126]
 128-10

108

 PHONCLA

 K-92, K-104

 K-105

 K-202, K-263

 TK-134

 TK-146B

 TK-234

 TK-234

 TK-234

 TK-234

 TK-234

 TK-236

 TK2146, -2

 TK2149

 PiLoT

 AA.901

 AA.902

 AF-605

 AF-723, U

 AF-723, U

 AF-821A, U

 T-41-1

 T-741

 TV-37

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver

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FILOT

PHILCO-Cont.

- Hinke D-LBH,
 13.72285, L (Code 128) (Ch. 94, J-5 and Radio Ch. RT-8) (See PCB 85.5528 (Code 123) (Ch. 94, J-5 and Radio Ch. RT-8) (See PCB 85.5528) (Code 126) (Ch. 94, J-5 and Radio Ch. RT-8) (See PCB 85.5528) (Code 126) (Ch. 94, J-5 and Radio Ch. RT-11) (Te Ch. only).
 13.72285 (Code 126) (Ch. 94, J-5 and Radio Ch. RT-11) (Te Ch. only).
 13.72285 (Code 126) (Ch. 94, J-5 and Radio Ch. RT-11) (Te Ch. only).
 13.72287 (Code 126) (Ch. 94, J-5 and Radio Ch. RT-11) (Te Ch. only).
 14. and Radio Ch. RT-11) (Te Ch. only).
 15.3.72287 (Code 126) (Ch. 94, J-5 and Radio Ch. RT-11) (Te Ch. only).
 15.3.72287 (Code 128) (Ch. 94, J-5 and Radio Ch. RT-11) (Te Ch. only).
 11.1 (See PCB 66.5er 203-1, FCB 82.5er 223-1 and Madel 53-17285.7er 123-3)
 15.3.12287 (Code 123) (Ch. 91, J-2) (See PCB 66.5er 203-1, FCB 82.5er 223-1 and Madel 53-17853.7er 185-10)
 15.3.12327 (Code 123) (Ch. 81, H-1, H-1-14 (For TV Ch. see PCB 83.5er 123-10)
 13.1 (See PCB 66.5er 203-1, PCB 83.5er 23-1 and Madel 53-17833.7es 185-10)
 13.1 (See PCB 66.5er 203-1, PCB 83.5er 23-1 and Madel 53-17833.7es 185-10)
 13.1 (See PCB 66.5er 203-1, PCB 83.2er 23-1 and Madel 53-17824.5er 123-1 and Madel 53-17824.5er 123-1 and Madel 53-17824.5er 123-1 (Ch. 91, J-1) (See PCB 66.2er 233) (Ch. 91, H-1, H-1A (For TV Ch. see PCB 83.2er 23-1 and Madel 53-17824.5er 123-1 (Ch. 91, J-1) (See PCB 66.2er 233) (Ch. 91, H-1, H-1A (For TV Ch. see PCB 83.2er 23-1 and Madel 53-17824.5er 123-1 (Ch. 91, J-1) (See PCB 66.2er 233) (Ch. 91, H-1, H-1A (For TV Ch. see PCB 83.2er 23-1 and Madel 53-17824.5er 221-7, for UHF Turer see Madel UT21A.Ser 223-9)
 53.U2226 (Cade 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83.2er 224-1 and Madel 53-17824.5er 220-7, for UHF Turer see Madel UT21A.Ser 223-9)
 53.U2226 (Cade 123) (Ch. 81, H-1, H-1A) (For TV Ch. see PCB 83.2er 224-1 and Madel 53-17824.5er 223-9)

- 153-12) 53-656, 53-658 53-700, 53-700-1, 53-701, 53-701-1 701-1 193-6 202-5 202-5 . 187-10

 12-24

 T-601
 ''Piloturer'
 28-26

 T-741
 37-18

 V-737
 62-16

 TV-273.U
 133-13

 TV-275.US See Model TV-270
 53

 TV-275.US See Model TV-270
 53

 TV-275.See Model TV-270
 53

 TV-275.See Model TV-270
 53

 TV-275.See Model TV-270
 53

 TV-275.See Model TV-270
 54

 T PLYMOUTH (See Mopar)

PHILCO-Cont.	PLYMOUTH (Interstate Stores)
Ch. R-191, R-191U, D-191 (Also see PCB 111-Set 260-1)231-12	1010
PCB 111—Set 260-1)231-12	1020 89—5
Set 260-1 and Set 231-12)	POLICALARM
PhileCo-Lohn. Ch. R. 191, R. 191U, D. 191 (Also see PCB 111—Set 260-1) 231-12 Ch. R. 192U, D-191 (See PCB 111— Set 260-1 and Set 231-12) Ch. R. 207, D-208 236-10 Ch. 3P1, CP1 135-10 Ch. 3P1, CP1 135-10 Ch. 3P2, CR2 135-10 Ch. 32, C1 138—7 Ch. 32, C2 148-13 Ch. 32, C2 148-13 Ch. 32, C2 148-13 Ch. 35, F2 132-10 Ch. 37, C2 148-13 Ch. 37, C2 148-13 Ch. 37, C2 148-13 Ch. 37, C2 148-13 Ch. 41, D-1, A (Aito tee PCB 56- Set 190-1) 171—9 Ch. 42, G-2	PR-8
Ch. R-207, D-208	PR-31
Ch. 3P1, CP1135-10	PONTIAC
Ch. 3R2, CR2	984170 20-27
Ch. 3R2, CR3	984170 20-27 984171 14-22 9842966, 984570 95-4 984592 165-8
Ch. 31, A1,	984296, 984570 95-4
Ch. 32, C1	984592 984688 (See Model 984592 - Set
Ch. 32, C2	165.8)
Ch 33, Cl	984817
Ch. 34, C3	PORTO BARADIO (Also see
Ch. 35, CP1	Porto Products)
Ch. 35, F2	PA-510 (9008-A), PB-520 (9008-B)
Ch. 41, D-1 A (Aiso see PCB 56-	33-16
Set 190-1)	PA-510, PB-520 (Revised). 48-21
Ch. 42, G-2	PORTO PRODUCTS
Cn. 44, D-4, 9 (Also see PCB 5/ Set 191.1) 181_0	SP 400 /Ch. 90404 "Smekerette"
Ch. 44, G-4 196-11	(See Porto Baradio Model PA-510
Ch. 71, G-1 (Also see PCB 57-Set	SR-600 (Ch. 9040A ''Smokerette'') (See Porto Baradio Model PA-510 —Set 33-16)
[9]-1)	PREMIER
Ch. 81A, D-81,	15LW 6-24
Ch. 91, J-1 (Also see PCB 66-Set	
203)	PURE OIL (See Puritan)
203-1, PCB 82-Set 223-1 and	PURITAN
Set 190.11 110.6 te C 1930-9 Ch. 42, G2, 42, G2, A4, D4, 9 (Also see PCB 57-5et 191-1) 181-9 Ch. 44, G.4, 9 (Also see PCB 57-5et 191-1) 181-9 Ch. 44, G.4, 9 (Also see PCB 57-5et 191-1) 181-9 Ch. 44, G.4, 9 (Also see PCB 57-5et 191-1) 181-9 Ch. 44, G.4, 9 (Also see PCB 57-5et 191-1) 181-9 Ch. 71, G-1 (Also see PCB 56-5et 2031-00 201-7 Ch. 91, A, J-2 (See PCB 66-5et 2031-00 185-10 Ch. 94, A, J-5 (See PCB 85-5et 2231-00 213-5 Ch. 94, A, J-5 (See PCB 85-5et 223-100 226-100 Set 185-10 20.5 224-100 Ch. 94, A, J-5 (See PCB 85-5et 223-100 226-100 Set 185-10 20.5 224-100 Ch. 94, A, J-5 (See PCB 85-5et 223-100 23-5 PHILHARMONIC 213-5	501 (Ch. 5D15WG), 502 (Ch. 5D-25WG) 4—5 501x (Ch. 5D15WG), 502x (Ch. 5D25WG) 4—26 503 10-25
Ch. 94, J-4	25WG) 4—5
226-1 and Set 213-5)	501X (Ch. 5D15WG), 502X (Ch.
	503 10-25
	503W (See Model 503-Set 10-25)
• 20CD28 (See Model 520Set 173-	504 (Ch. 6A35WG) 5-39
10) • 20C2B (See Model 520—Set 173-	503 10-25 503W (See Model 503—Set 10-25) 504 (Ch. 6A33WG). 5-39 504W (See Model 504—Set 5-39) 506 (6D155W), 501 (6D255W) 3-10
10)	3-10
• 20T2B (See Model 520-Set 173-	3-10 506X, 507X (See Model 506—Set 3-10}
•21CD2A [See Model 520-Set 173-	508 (Code 7A35SW)
101	509
@21C2A (See Model 520-Set 173-	515 26 -24
•21C2A (See Model 520—Set 173- 10)	515
•21C2A (See Model 520—Set 173- 10)	515 26-24 RADIO APPARATUS CORP.
•21C2A (See Model 520—Set 173- 10)	515 26-24 RADIO APPARATUS CORP. (See Policalarm & Monitoradio)
●21C2A (See Model 520—Set 173- 10) 38-16 100C 38-16 100T 33-20 ●111, 112 (See Modei 520—Set 173- 10) 10C 520. C 55-19	S15
●21C2A (See Model 520—Set 173- 10) 38-16 100C 38-16 100T 33-20 ●111, 112 (See Modei 520—Set 173- 10) 10C 520. C 55-19	S15
●21C2A (See Model 520—Set 173- 10) 38-16 100C 38-16 100T 33-20 ●111, 112 (See Model 520—Set 173- 10) 149C, 249-C 55-19 349-C 58-17 59-40, 770, 790, 921	S15
●21C2A (See Model 520—Set 173- 10) 38-16 100C 38-16 100T 33-20 ●111, 112 (See Model 520—Set 173- 10) 149C, 249-C 55-19 349-C 58-17 59-40, 770, 720, 920, 921	S15
●21C2A (See Model 520—Set 173- 10) 38-16 100C 38-16 100T 33-20 ●111, 112 (See Model 520—Set 173- 10) 149C, 249-C 55-19 349-C 58-17 59-40, 770, 720, 920, 921	S15
	S15
e21C2A (See Model 520—Set 173- 10) 100C 38-16 100T 33-20 111, 112 (See Model 520—Set 173- 10) 149C, 249-C 55-19 349-C 58-17 520, 620, 720, 724, 820, 824 173-10 e920, 924 (Lote) 245-4 e5000 5201 160-9	S15
	S15
●21CŽA (See Model 520—Set 173-10) 100 38-16 1007 33-30 101 33-30 101 33-30 101 33-30 101 33-30 101 349-C 349-C 58-17 520, 620, 720, 724, 820, 824 173-10 •920, 924 (Eorly) (See Model 520 -	515
	515
	515
	515
	515
	515
	515
	515
	515
	515 26-24 RADIO APPARATUS CORP. (See Policelarm & Monitoradio) RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (Ch. RC-1087) 109-10 A-82 (Ch. RC-1087) 109-10 A-83 (Ch. RC-1094) 137-10 A-101 (Ch. RC1096) 137-10 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) 97-12 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-2-C, B2-F, B2-H (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-411 (Ch. RC1098) 132-12 BX6 (Ch. RC1088) 132-12 BX65 (Ch. RC1088) 102-11 CT-100 (Ch. CTC2) 252-11 M-12224 M-12224 103-13 BX55 (Ch. RC1088) BX57 (Ch. RC1027) M-12224 M-1223 4 M-12224 M-1223 4 M-12236 A - 8, -C, M1-1223 -A M-12236 -A, -8, -C,
●21CŽA (See Model 520—Set 173-10) 100 38-16 1007 38-26 1007 33-20 11, 112 (See Model 520—Set 173-10) 149C, 249-C 58-17 349-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 •200, 924 (Eorly) (See Model 520 •200, 924 (Lote) 245-4 •200, 924 (Lote) 245-4 •5000 160-9 •5201 (See Model 520—Set 173-10) •5250 500 •5400, 5401 160-9 •5500, 5501 160-9 •5500, 5500 160-9 •5500, 5500 160-9 •5500, 570 RT, 5701 160-9 •5500, 570 RT, 160-9 •5800 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •712	515 26-24 RADIO APPARATUS CORP. (See Policelarm & Monitoradio) RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (Ch. RC-1087) 109-10 A-82 (Ch. RC-1087) 109-10 A-83 (Ch. RC-1094) 137-10 A-101 (Ch. RC1096) 137-10 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) 97-12 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-2-C, B2-F, B2-H (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-411 (Ch. RC1098) 132-12 BX6 (Ch. RC1088) 132-12 BX65 (Ch. RC1088) 102-11 CT-100 (Ch. CTC2) 252-11 M-12224 M-12224 103-13 BX55 (Ch. RC1088) BX57 (Ch. RC1027) M-12224 M-1223 4 M-12224 M-1223 4 M-12236 A - 8, -C, M1-1223 -A M-12236 -A, -8, -C,
●21CŽA (See Model 520—Set 173-10) 100 38-16 1007 38-26 1007 33-20 11, 112 (See Model 520—Set 173-10) 149C, 249-C 58-17 349-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 •200, 924 (Eorly) (See Model 520 •200, 924 (Lote) 245-4 •200, 924 (Lote) 245-4 •5000 160-9 •5201 (See Model 520—Set 173-10) •5250 500 •5400, 5401 160-9 •5500, 5501 160-9 •5500, 5500 160-9 •5500, 5500 160-9 •5500, 570 RT, 5701 160-9 •5500, 570 RT, 160-9 •5800 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •712	515 26-24 RADIO APPARATUS CORP. (See Policelarm & Monitoradio) RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (Ch. RC-1087) 109-10 A-82 (Ch. RC-1087) 109-10 A-83 (Ch. RC-1094) 137-10 A-101 (Ch. RC1096) 137-10 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) 97-12 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-2-C, B2-F, B2-H (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-411 (Ch. RC1098) 132-12 BX6 (Ch. RC1088) 132-12 BX65 (Ch. RC1088) 102-11 CT-100 (Ch. CTC2) 252-11 M-12224 M-12224 103-13 BX55 (Ch. RC1088) BX57 (Ch. RC1027) M-12224 M-1223 4 M-12224 M-1223 4 M-12236 A - 8, -C, M1-1223 -A M-12236 -A, -8, -C,
●21CŽA (See Model 520—Set 173-10) 100 38-16 1007 38-26 1007 33-20 11, 112 (See Model 520—Set 173-10) 149C, 249-C 58-17 349-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 •200, 924 (Eorly) (See Model 520 •200, 924 (Lote) 245-4 •200, 924 (Lote) 245-4 •5000 160-9 •5201 (See Model 520—Set 173-10) •5250 500 •5400, 5401 160-9 •5500, 5501 160-9 •5500, 5500 160-9 •5500, 5500 160-9 •5500, 570 RT, 5701 160-9 •5500, 570 RT, 160-9 •5800 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •712	515 26-24 RADIO APPARATUS CORP. (See Policelarm & Monitoradio) RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (Ch. RC-1087) 109-10 A-82 (Ch. RC-1087) 109-10 A-83 (Ch. RC-1094) 137-10 A-101 (Ch. RC1096) 137-10 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) 97-12 A-106 (Ch. RC1096) 141-10 B-A, B1-8, B1-C (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-2-C, B2-F, B2-H (Ch. KC524-1) For YV (Ch. only see Model 8FC541- Set 90-91 B-411 (Ch. RC1098) 132-12 BX6 (Ch. RC1088) 132-12 BX65 (Ch. RC1088) 102-11 CT-100 (Ch. CTC2) 252-11 M-12224 M-12224 103-13 BX55 (Ch. RC1088) BX57 (Ch. RC1027) M-12224 M-1223 4 M-12224 M-1223 4 M-12236 A - 8, -C, M1-1223 -A M-12236 -A, -8, -C,
●21CŽA (See Model 520—Set 173-10) 100 38-16 1007 38-26 1007 33-20 11, 112 (See Model 520—Set 173-10) 149C, 249-C 58-17 349-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 •200, 924 (Eorly) (See Model 520 •200, 924 (Lote) 245-4 •200, 924 (Lote) 245-4 •5000 160-9 •5201 (See Model 520—Set 173-10) •5250 500 •5400, 5401 160-9 •5500, 5501 160-9 •5500, 5500 160-9 •5500, 5500 160-9 •5500, 570 RT, 5701 160-9 •5500, 570 RT, 160-9 •5800 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •712	515
●21cZa (See Model 520—Set 173- 10) 100C 38-16 100T 33-20 101 102C 102 33-20 111, 112 (See Model 520—Set 173- 10) 149-C 149-C, 249-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 173-10 •200, 924 (Eorly) (See Model 520 160-9 •200, 5201 160-9 •2200, 5201 160-9 •5200, 5201 160-9 •5400, 5401 160-9 •5500, 5001 160-9 •5500, 5001 160-9 •5500, 5001 160-9 •5500, 5700 RT, 5701 160-9 •5500, 5700 RT, 5701 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •7120, 7820 173-10 •810 (Ch, RR14) 18-27 •7120, 8702, 8703, 8710, 8711, 8712 (Or 173-10 •7120, 921 (Eorly) (See Model 520 •728+173-10 192-9 •720, 921 (Eorly) (See Model 520 •7	515
●21cZa (See Model 520—Set 173- 10) 100C 38-16 100T 33-20 101 102C 102 33-20 111, 112 (See Model 520—Set 173- 10) 149-C 149-C, 249-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 173-10 •200, 924 (Eorly) (See Model 520 160-9 •200, 5201 160-9 •2200, 5201 160-9 •5200, 5201 160-9 •5400, 5401 160-9 •5500, 5001 160-9 •5500, 5001 160-9 •5500, 5001 160-9 •5500, 5700 RT, 5701 160-9 •5500, 5700 RT, 5701 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •7120, 7820 173-10 •810 (Ch, RR14) 18-27 •7120, 8702, 8703, 8710, 8711, 8712 (Or 173-10 •7120, 921 (Eorly) (See Model 520 •728+173-10 192-9 •720, 921 (Eorly) (See Model 520 •7	515
●21cZa (See Model 520—Set 173- 10) 100C 38-16 100T 33-20 101 102C 102 33-20 111, 112 (See Model 520—Set 173- 10) 149-C 149-C, 249-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Eorly) (See Model 520 173-10 •200, 924 (Eorly) (See Model 520 160-9 •200, 5201 160-9 •2200, 5201 160-9 •5200, 5201 160-9 •5400, 5401 160-9 •5500, 5001 160-9 •5500, 5001 160-9 •5500, 5001 160-9 •5500, 5700 RT, 5701 160-9 •5500, 5700 RT, 5701 160-9 •5800 173-10 •610 (Ch, RR14) 18-27 •7120, 7820 173-10 •810 (Ch, RR14) 18-27 •7120, 8702, 8703, 8710, 8711, 8712 (Or 173-10 •7120, 921 (Eorly) (See Model 520 •728+173-10 192-9 •720, 921 (Eorly) (See Model 520 •7	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CŽA (See Model 520—Set 173.10) 100 38-16 100 33-20 101 100C 38-16 100 33-20 101 149C, 249-C 58-17 101 149C, 249-C 58-17 103 520, 620, 720, 724, 820, 824 173-10 949-C 58-17 520, 620, 720, 724, 820, 824 173-10 • 200, 924 (Early) (See Model 520 - - 500 160-9 • 5200, 5201 160-9 • 5200, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5500 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5800 173-10 • 610 (Ch, RR14) 18-27 • 7120, 7120, 712-10 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CŽA (See Model 520—Set 173.10) 100 38-16 100 33-20 101 100C 38-16 100 33-20 101 149C, 249-C 58-17 101 149C, 249-C 58-17 103 520, 620, 720, 724, 820, 824 173-10 949-C 58-17 520, 620, 720, 724, 820, 824 173-10 • 200, 924 (Early) (See Model 520 - - 500 160-9 • 5200, 5201 160-9 • 5200, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5500 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5800 173-10 • 610 (Ch, RR14) 18-27 • 7120, 7120, 712-10 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CŽA (See Model 520—Set 173.10) 100 38-16 100 33-20 101 100C 38-16 100 33-20 101 149C, 249-C 58-17 101 149C, 249-C 58-17 103 520, 620, 720, 724, 820, 824 173-10 949-C 58-17 520, 620, 720, 724, 820, 824 173-10 • 200, 924 (Early) (See Model 520 - - 500 160-9 • 5200, 5201 160-9 • 5200, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5500 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5800 173-10 • 610 (Ch, RR14) 18-27 • 7120, 7120, 712-10 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CŽA (See Model 520—Set 173.10) 100 38-16 100 33-20 101 100C 38-16 100 33-20 101 149C, 249-C 58-17 101 149C, 249-C 58-17 103 520, 620, 720, 724, 820, 824 173-10 949-C 58-17 520, 620, 720, 724, 820, 824 173-10 • 200, 924 (Early) (See Model 520 - - 500 160-9 • 5200, 5201 160-9 • 5200, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5401 160-9 • 5500, 5500 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5500, 5700 RT, 5701 160-9 • 5800 173-10 • 610 (Ch, RR14) 18-27 • 7120, 7120, 712-10 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10 • 8120 173-10	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CZA (See Model 520—Set 173-10) 100 38-16 1001 38-16 1007 38-36 1001 33-20 101 149C, 249-C 103 58-17 104 520, 620, 720, 724, 820, 824 173-10 173-10 1949-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Early) (See Model 520 -58-17 •5000 160-9 •5200, 5201 160-9 •5200, 5201 160-9 •5200, 5401 160-9 •5500, 5401 160-9 •5500, 5501 160-9 •5500, 5700 RT, 5701 160-9 •5800 173-10 •8120 173-10 •8120 173-10 •8120 173-10	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CŽA (See Model 520—Set 173-10) 100 100 100 100 100 100 100 100 112 100 100 100 149-C 100 149-C 100 149-C 100 149-C 100 149-C 173-10 920, 924 (Early) (See Model 520 920, 924 (Late) 1400-9 9200, 920 160-9 9200, 5201 160-9 9221 (See Model 520—Set 173-10) 9220, 530 9260, 5401 160-9 9300, 500 930, 5700 RT, 5701 160-9 9500, 5500 T 160-9 9500, 5500 T 160-9 9500, 5700 RT, 5701 160-9 9500, 5700 RT, 5701 160-9	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CZA (See Model 520—Set 173-10) 100 38-16 1001 38-16 1007 38-36 1001 33-20 101 149C, 249-C 103 58-17 104 520, 620, 720, 724, 820, 824 173-10 173-10 1949-C 58-17 520, 620, 720, 724, 820, 824 173-10 •200, 924 (Early) (See Model 520 -58-17 •5000 160-9 •5200, 5201 160-9 •5200, 5201 160-9 •5200, 5401 160-9 •5500, 5401 160-9 •5500, 5501 160-9 •5500, 5700 RT, 5701 160-9 •5800 173-10 •8120 173-10 •8120 173-10 •8120 173-10	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA 'ViCTOR (Also see Changer and Recorder Listing) A-55 (ch. RC-1087)
●21CŽA (See Model 520—Set 173-10) 100 100 100 100 100 100 100 100 112 100 100 100 149-C 100 149-C 100 149-C 100 149-C 100 149-C 173-10 920, 924 (Early) (See Model 520 920, 924 (Late) 1400-9 9200, 920 160-9 9200, 5201 160-9 9221 (See Model 520—Set 173-10) 9220, 530 9260, 5401 160-9 9300, 500 930, 5700 RT, 5701 160-9 9500, 5500 T 160-9 9500, 5500 T 160-9 9500, 5700 RT, 5701 160-9 9500, 5700 RT, 5701 160-9	515 26-24 RADIO APPARATUS CORP. [See Policolarm & Monitoradio] RCA YiCTOR (Also see Changer and Recorder Listing) A.55 (Ch. RC-1087)

36-19)...168-12 21C, RS.123D) ...61-17 250-17 253-11 255-10 ...255-11 ...255-13 31-1, RC617B) 91A-11 93-9 51-17 79-11 55-20 83-8 158-9 108-9 159-11 259-12

258-9

199---8

222-9 172-7 222-10 194-10 220-6 199-8 223-10 15-25 12-23 5-24 19-27 12-24

- TIOD (Ch. KCS.38)
 19³-9
 TI20, TI21 (KCS34C)
 93-9
 TI42(T121 (KCS34C)
 93-9
 TI42(T121 (KCS34C)
 199-11
 TA.128 (Ch. KCS42A and Radio Ch. KCS42A and Radio Ch. KCS42A and Radio Ch. See Model
 TA-129, Ch. SCS41A-1 and Radio
 Ch. RK135D) (For TV Ch. see Set
 TI0-11, for Radio Ch. see Model
 TA-129, Ch. KCS41A-1 and Radio
 Ch. RK135D) (For TV Ch. see Model
 TA-129, Ch. KCS41A-1 and Radio
 Ch. RK135D) (For TV Ch. see Model
 TA-129, Ch. KCS43A and Radio Ch. RK135D)
 TI0-11, for Radio Ch. See Model
 TA-129, CT 124, TC 125, TC 127, TC 128, TC 127, TC 1
- •TC165, TC166, TC167, TC168 (Ch. KC5400, 109-10) UIA (Ch. KRK-19) Tel. UHF Conv. 190-12 UIB (Ch. KRK-19A) Tel. UHF Conv. 190-12 U2 (Ch. KC570) Tel. UHF Conv. 191-15 U70 (Ch. KC570) Tel. UHF Conv. 192-27

RCA VICTOR-Cont. 2CS21, 2CS22, 2CS27 (Ch. RC-1120A) 2CS21, 2CS22, 2CS27 (Ch. RC-1120A) 2ES31 (Ch. RS-142) 205—7 2ES31 (Ch. RS-142) 205—7 2ES31 (Ch. RS-142) (See Model 2ES3BA (Ch. RS-142) (See Model 2ES3BA (Ch. RS-142) 2ES33 (Ch. RS-142) 205—7 2ES33 (Ch. RS-142) (See Model 2ES3BA (Ch. RS-142) 2ES38 (Ch. RS-142) 205—7 2ES38 (Ch. RS-142) (See Model 2ES3BA (Ch. RC117D) 222-11 2S7 (Ch. RC1117D) 222-11 2S7 (Ch. RC1117D) 222-11 2S7 (Ch. RC1117D) 222-11 2S7 (Ch. RC1117D) 222-11 2S10 (Ch. RC145) Allos cee PCB 11 -5et 118-1) -111-11 -Set 118-1) -111-11 -5et 118-1) -111-11 2V50 (Ch. KC454) (Also see PCB 11 -5et 118-1) -111-11 2V57 (A (Ch. RC1080C) -177—8 2X42 (Ch. RC-1080C) 2V57 (Ch. RC-1080C) 197—8 2X42 (Ch. RC-1080C) 2V57 (Ch. RC-1123) 224—13 205—9 2X51 (Ch. RC-1123) 224—14 205—9 2X521 (Ch. RC-1125) 224—14 3HES5 - (Ch. RS-145X) 22

6174, 6175, 6176 (Ch. KCS47A, AT] (Alio see PCB 12—Set 120-1)
61784 (Ch. KCS 48, T and Radio Ch. RC-1090) (For TV Ch. see PCB 12 - Set 120-1) and Model 6154—Set 113-7, for Radio Ch. Rc-1092) (For TV Ch. see PCB 12—Set 120-1) and Model 6154—Set 113-7, for Radio Ch. RC-1092) (For TV Ch. see PCB 12—Set 120-1) and Model 6154—Set 113-7, for Radio Ch. Rc-1092) (For TV Ch. see PCB 12—Set 120-1) and Model 6154—Set 113-7, for Radio Ch. RC-1092) (For TV Ch. see PCB 12—Set 120-1) and Model 71103—Set 134-9
671103, 71104 (Ch. KCS 47F) (See PCB 26—Set 146-1) and Model 711118—Set 156-11)
671104, Ch. KCS 47GF-2). 134-9
671103, 71104 (Ch. KCS 47GF-2). 134-9
671103, 71104 (Ch. KCS 47GF-2). 134-9
771123, Ch. KCS 47GF-2). (See Model 711118—Set 156-11)
771122, 771123 (Ch. KCS 47GF)
771226, 771123B (Ch. KCS 47GF)
771226, 771123B (Ch. KCS 47GF)
77124, 77125 (Ch. KCS 47GF)
77124, 77125 (Ch. KCS 47GF)
771245 (Ch. KCS 47GF)
771245 (Ch. KCS 47GF)
771245 (Ch. KCS 47GF)

BBX65 (See Model 8BX6-Set 44-

1060A) 53-20 8R74, 8R75, 8R76 (Ch. RC-1060, A) 53-20

A) •87241, 87243, 87244 (Ch. KC528) 74-8

RCA VICTOR-Cont. RCA VICTOR-Cont.
 RCA
 VICTOR-Cont.

 08TV321, 8, 8TV333, 8 (Ch. KC5-30-1 and Rodio Ch. RC-6168, C. J, K)
 74-8

 8V7 (Ch. RC-616), ISee Model 77V1
 74-8

 -Set 38-18]
 8V90 (Ch. RC-618, RC-6164), 58-00

 8V90 (Ch. RC-618, RC-6164), 58-00
 8V111, 8V112 (Ch. RC-6164), 58-00

 8V131
 Ch. RC-616A, RC-6164), 59-00

 8V133
 Ch. RC-616A, RC-6164), 59-00

 8V131
 61-17

 8V32 (R272 (RC-1070), 43-15

 8X541—Set 59-16
 59-16

 8X547
 59-16

 8X681, 8X682 (Ch. RC-1061) 65-10
 59-16

 98X5 (Ch. RC-10598, C) (See Model
 88X5-5et 46-20

 98X56 (Ch. RC-1068)
 79-13

 9EY3 (Ch. RS-132)
 158-10

 9FY41, RS-123
 158-10

 9FY21A, B, C (Ch. KC524C-1, D, KRX-4, KS208-1, KRS21A-1, RS-123A)
 90-9

 9F737 (Ch. KC549, 71)
 122-8

 9779 (Ch. KC549, A, AT, T)
 122-8

 9778 (Ch. KC549, A, AT, T)
 122-8

 9779 (Ch. KC549, A, AT, T)
 122-8
 and Radio Ch. 122—8 134—9
 ●9789 (Ch. KC530, T and Redio Ch. RC1092)
 122--B

 ●97105 (Ch. KC5490)
 134--9

 ●971128 (Ch. KC5490)
 134--9

 ●971128 (Ch. KC5490)
 134--9

 ●971128 (Ch. KC5490)
 134--9

 ●971128 (Ch. KC5490)
 134--9

 ●97124 (Ch. KC540A and Redio Ch. RC1092) (For TV Ch. see Set 134-9, For Redio Ch. see Model 97240 (Ch. KC528)
 74--B

 ●97243 (Ch. KC538)
 74--B

 ●97244 (Ch. KC538)
 93--9

 ●97256 (Ch. KC538)
 93--9

 ●97263 (Ch. KC538)
 74--B

 ●97264 (Ch. KC538)
 93--9

 ●97272 (Ch. KC538)
 74--B

 ●97257 (Ch. KC538)
 93--9

 ●97257 (Ch. KC538)
 74--B

 ●97257 (Ch. KC538)
 93--9

 ●97257 (Ch. KC538)
 74--B

 ●97257 (Ch. KC538)
 74--B

 ●97257 (Ch. KC538)
 93--9

 ●97257 (Ch. KC538)
 74--B

 ●97257 (Ch. KC538)
 93--9

 ●97257 (Ch. KC538)
 93--9

 ●97257 (Ch. KC537)
 93--9

 ●97257 (Ch. KC538)
 93--9

 ●97257 (Ch. KC538)</t •91C247, 91C275 (Ch. KCS29C) •91C272, 91C275 (Ch. KCS29C) 85-13 9 W101, 9 W102, 9 W103 (Ch. RC-6188), 9 W105 (Ch. RC-618C) 9 W106 (Ch. RC-622) 97-12 9 X561 (Ch. RC-1079B) 9 X562 (Ch. RC-1079C) 101-9 9 X571 (Ch. RC-1079), 9 X572 (Ch. RC-1079A) 107-7 9 X641 (Ch. RC-1080), 9 X642 (Ch. RC-1085A) 104-9 9 Y516 (Ch. RC-1085), 9 X552 (Ch. RC-1085A) 104-9 9 Y7 (Ch. 1057B) 75-13 9 Y510 (Ch. RC-1077) 98-11 9 Y510 (Ch. RC-1077) 131-13 16 T152 (Ch. RC-1077) 131-13 16 T152 (Ch. RC-1077) 28-15 175349 (Ch. RC-1077) 228-15 175349 (Ch. RC-1078) 228-15 1753350 (Ch. RC-1078) 228-15 175350 (Ch. RC-1078) 228-15 17550 (

RCA VICTOR-Cont. 215348 (Ch. KCS83P) ... 242---8 215348C (Ch. KCS83P) ... 242--8 215348C (Ch. KCS83P) ... 242--8 215348K (Ch. KCS83P) ... 258-10 215348K (Ch. KCS83C) ... 242--8 215353 (Ch. KCS83C) ... 242--8 215353G (Ch. KCS83C) ... 242--8 215353G (Ch. KCS83C) ... 242--8 215354G (Ch. KCS 213332 (Ch. KCS83C, PC. G. G. PK)
 213335 (Ch. KCS83C, PC. G. G. PK)
 213355 (Ch. KCS83C, PC. G. G. PK)
 213355 (Ch. KCS88)
 213355 (Ch. KCS88)
 213355 (Ch. KCS88)
 213357 (Ch. KCS88)
 215357 (Ch. KCS88)
 215357 (Ch. KCS83)
 215362 (Ch. KCS83)
 22562 (Ch. KCS83)
 23667 (Ch. KCS83)
 2367 (Ch. KCS83)

 PK)
 242-5

 • 21S369KU (Ch. KCS83D, PD.

 • 21S369KU (Ch. KCS88F)
 258-10

 • 21S369KU (Ch. KCS88F)
 258-10

 • 21S369KU (Ch. KCS88F)
 258-10

 • 21T159DE (Ch. KCS68F)
 258-10

 • 21T159DE (Ch. KCS68F)
 197-9

 • 21T164DE (Ch. KCS68F)
 197-9

 • 21T165DE (Ch. KCS68F)
 197-9

 • 21T177DE (Ch. KCS68F) (See Model 21T159DE-Ser 197-9)
 11T7ADE (Ch. KCS68F) (See Model 21T159DE-Ser 197-9)

 • 21T177DE (Ch. KCS68F) (See Model 21T159DE (Ch. KCS68F) (See Model 21T159DE (Ch. KCS68F) (See Model 21T179DE (Ch. KCS68C) (Alto we PCB 56-Ser 190-1)

 • 21T177DE (Ch. KCS68C) (Alto we PCB 56-Ser 190-1)
 157-8

 • 21T177DE (Ch. KCS68C) (Alto we PCB 56-Ser 190-1)
 157-8

 • 21T177DE (Ch. KCS68A, Rodie Ch. RC11111A and Audie Ch. R5141A1
 209-10

 • 21T197DE (Ch. KCS72A) (See PCB 59-Ser 193-1)
 184-12

 • 21T1272 (Ch. KCS72D-1 (See PCB 59-Ser 193-1)
 184-12

 • 21T1272 (Ch. KCS72D-2, Rodie Ch. RC111172
 184-12

 • 21T224 (Ch. KCS72D-2, Rodie Ch. RC111172
 21T242 (Ch. KCS72D-2, Rodie Ch. RC111172

 • 21T342 (Ch. KCS72D-2, Rodie Ch. RC111172
 202-6

 • 21T342 (Ch. KCS72D-2, Rodie Ch. RC111172
 232-5) 211364U (Ch. KC583B) ...232-5 211365, U (Ch. KC583, B) 232-5 211372, U, 211373, U, 211374, U (Ch. KC583, B)232-5

 RCA
 VICTOR-Cont.

 ≥211375G, GU (Ch. KC583G, E) (See model 211375, U—Set 232-5)

 ≥11375U (Ch. KC583B)... 232-5

 ≥113792, U (Ch. KC583B)... 232-5

 ≥113792, U (Ch. KC583B, H. 8. Rodio Ch. RC 11178) (For TV Ch. See Model 215348—Set 242-8, For Rodio Ch. See Model 211242--Set 202-6)

 ≥11392, U (Ch. KC583F, H. Rodio Ch. RC-1111C and Audie Amp R5 1410) (For TV Ch. See Model 215348—Set 242-8, For Rodio Ch. See Model 21D346—Set 219-7)

 ≥21423, U (Ch. KC584C, E) 245--5

 ≥41430, U (Ch. KC584C, E) 245--5

 ≥770382 (Ch. KC577F)... 235-10

 ≥770382 (Ch. RC577F)... 235-10

 ≥770382 (Ch. RC577F)... 235-10

 ≥770382 (Ch. RC577F)... 235-10

 ≥770383 (Ch. RC577F)... 235-10

 ≥770382 (Ch. RC537F)... 235-10

 ≥770383 (Ch. RC577F)... 235-10

 ≥770383 (Ch. RC577F)... 235-10

 ≥770383 (Ch. RC577F)... 235-10

 ≥770382 (Ch. RC537F)... 235-10

 ≥770382 (Ch. RC537F).... 235-10

 ≥770383 (Ch. RC1077
 56X, 56X2, 56X3
 (Ch. RC-1011)

 1-16
 56X5
 (See Model 56X10—Set 1-12)

 56K10
 (Ch. RC-1023B)
 1-12

 58K7
 (See K-605)
 1-12

 58K7
 (Set R-1023B)
 1-12

 58K7
 (Set R-1023B)
 1-12

 58K7
 (Set R-10237A)
 1-32

 54F7
 64F7
 64F7

 64F7
 64F7
 64F7

 64F7
 64F7
 64F7

 65K9
 (Ch. RC-1037A)
 4-16

 65F8
 (Ch. RC-107A)
 4-23

 65L4
 , 65U
 (Ch. RC-107A)
 4-23

 65L4
 , 65U
 (Ch. RC-107A)
 4-23

 65L4
 , 65U
 (Ch. RC-1034)
 4-30

 65K1
 , 65K2
 (Ch. RC-1034)
 3-12

 65K3
 , 65K9
 (See Model 65K1)
 3-26

 65K4
 , 65K2
 (Ch. RC-1034)
 3-30

 65K1
 , 65K2
 (Ch. RC-1044)
 31-26

 65K3
 , 65K2
 (See Model 65K1)
 -56

 05.84, 05.84 (3ee Model 05.41—581

 4.30)

 668X (Ch. RC-1040, RC-1040.4)

 14-24

 666 (Ch. RS-126)

 14-24

 666 (Ch. RS-126)

 17-23

 6647, 6648 (See Model 6641—5et

 7.23

 6647, 6648 (See Model 6641—5et

 7.24

 668, 6641, 66413 (Ch. RC-606)

 7.27

 6887, 6682, 6683, 6684 (Ch. RC-606)

 698

 698

 6881, 6682, 6683, 6884 (Ch. RC-606)

 698

 698

 698

 698

 7541, 75418, 75418, 75419 (Ch. RC-6050)

 794

 794

 6647

 794

 6797

 794

 794

 794

 794

 794

 4-30) 668X (Ch. RC-1040, RC-1040A) 1238) 90-710V2 (Ch. RC-613A) 40-1 711V1 (See Model 711V2-Set 22 241 40-15
 24)

 711V2, 711V3 (Ch. RK-117 ond RS-123)

 22-24

 711V3 [See Model 711V2---Set 22: 24]
 71113 [See Model / 11/2---3et 4.2-24] •7211C5 (Ch. KCS26A-1, -2] (See Similor Model 7307VI-Set 70.7) •72115 (Ch. KCS26-1, -2] (See Sim-ilar Model 7307VI -Set 70.7) •7301V1 (Ch. KCS27-1, -2 and Ra-dio Ch. RC6108] •70-7 •7419C5 (Ch. KCS248-1, KR1A-1, KR520A-1, KR521A-1, RS-123C) •Ch. C1C2 (See Model CI-100) •741PCS (Ch. KCS24B-1, KR1A-1, KR520A-1, KR521-A-1, KS-123C) ← CTC2 (See Model CT-100) Ch. KCS20A [See Model 630TC5] Ch. KCS20B-1 [See Model 630TC5] Ch. KCS20A-1 [See Model 6480TK] Ch. KCS24A-1 [See Model 648PC3] Ch. KCS24A-1 [See Model 8PC341] Ch. KCS24A-1 [See Model 8PC341] Ch. KCS24C-1 [See Model 8PC341] Ch. KCS252C-1 [See Model 8PC341] Ch. KCS252-1 [See Model 8PC341] Ch. KCS25C-1 [See Model 8PC341] Ch. KCS32C-1 [See Model 8PC341] Ch. KCS32A-1 [See Model 8PC32] Ch. KCS33A-1 [See Model 8PC32] Ch. KCS33A-1 [See Model 8PC32] Ch. KCS34A-1 [See Model 7A-129] Mage Bulletin Not, 1 Through 63 Are J NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos, 1 Through 63 Are All Contained in Set No. A-200.

Denotes Television Receiver.

RCA VICTOR-Cont.

RCA VICTOR-Cont. Ch. KCS42A (See Model TA-128) Ch. KCS43, A (See Model Z151) Ch. KCS43, A (See Model Z151) Ch. KCS478, C (See Model Z151) Ch. KCS478, C (See Model Z151) Ch. KCS478, C (See Model Z1132) Ch. KCS478, C (See Model Z1132) Ch. KCS478 (See Model Z1132) Ch. KCS478, C (See Model Z1132) Ch. KCS478, C (See Model Z1132) Ch. KCS478, C (See Model Z1143) Ch. KCS488, C (See Model Z1165) Ch. KCS488, C (See Model Z1165) Ch. KCS478, C (See Model Z1165) Ch. KCS488, C (See Model Z1165) Ch. KCS648, C (See Model Z1175) Ch. KCS648, C (See Model Z11750) Ch. KCS648, C (See Model Z11750) Ch. KCS648, C (See Model Z11750) Ch. KCS648, C (See Model Z11759) Ch. KCS648, C (See Model Z11759) Ch. KCS648, C (See Model Z11750) Ch. KCS74, See Model Z11750) Ch. KCS74, See Model Z11750) Ch. KCS74, See Model Z11750) Ch. KCS774, See Model Z117424) Ch. KCS774, See Model Z11582 Ch. KCS774, See Model Z11582 Ch. KCS774, See Model Z1159 Ch. KCS777 (See Model Z70383) Ch. KCS774, See Model Z70382) Cli, CCS78F, H (See Model 175349, U) Ch, CCS78F, H (See Model 1753520) Ch, CCS78I (See Model 1753520) Ch, CCS78I (See Model 175349CU) Ch, CCS78 (See Model 175349CU) Ch, CCS78 (See Model 175349CU) Ch, CCS81D, E (See Model 21D353, U) Ch 36, U) Ch 46, CS15 (See Model 21D354) Ch 46, CS15 (See Model 21D354) Ch 36, U) KCS81F, J (See Model 21D358) KCS82, A, B (See Model Ch. Ch. KCS82, A, B (See Model 217303, U) Ch. KCS820, E (See Model 217342) Ch. KCS83 (See Model 215362M or 217363) Ch. KCS83A (See Model 215362MU) Ch. KCS83A (See Model 215353 or 217363) Ch. KCS83C (See Model 215353 or 217363) Lin, Lissia, Isee Model 213348 Ch. KCS835 (See Model 213353) Ch. KCS835 (See Model 213353) Ch. KCS835 (See Model 213353) Ch. KCS837 (See Model 213353) Ch. KCS837 (See Model 213320) Ch. KCS837 P(See Model 213320) Ch. KCS837 P(See Model 213326) Ch. KCS837 P(See Model 213348) Ch. KCS837 (See Model 2133348) Ch. KCS837 (See Model 2133348) Ch. KCS887 (See Model 2133348) Ch. KCS887 (See Model 2133348) Ch. KCS887 (See Model 2133348) Ch. KCS888 (See Model 213348) Ch. KCS888 (See Model 213348) Ch. KCS888 (See Model 213348) Ch. KCS887 (See Model 213348) Ch. KC5987 (See Model 213348) Ch. RC597 (See Model 21348) Ch. RC597 (See Model 26771) Ch. RC597 (See Model 2771) Ch. RC597 (See Model 2771) Ch. RC597 (See Model 2771) Ch. RC597 (See Model 8V90) h. RC-618, B, C (See Model Ch. K. 9W1011 PC-6 9W1011 Ch. RC-622 (See Model A106) Ch. RC-1004E (See Model 55F) Ch. RC-1011 (See Model 55K) Ch. RC-1017 (See Model 55K1) Ch. RC-10278 (See Model 65AU) Ch. RC-1034 (See Model 65AU) Ch. RC-1037, RC-1037A (See Model A(E)) Ch. RC-1037, NS-1038 64F1) Ch. RC-1037B (See Model 8F43) Ch. RC-1038, RC-1038A (See Model 66K1) Ch. RC-1040A (See Model 8BX6) Ch. RC-1040C (See Model 8BX6) D-1045 (See Model 8BX6) Ch. RC-1045 (See Model 65BR9) Ch. RC-1046, A, B (See Model 66X11) Ch. RC-1047 (See Model 54B5) Ch. RC-1050, RC-1050B (See Model 75X11) Ch. RC-1037A [See Model 77U] Ch. RC-1037A [See Model 77U] Ch. RC-1057B [See Model 977] Ch. RC-1057B [See Model 8BX5] Ch. RC-1059B, RC-1059C [See Model 9BX5]

RCA VICTOR-Cont.

RCA VICTOR

RCA VICTOR-Cont. Ch. RC-1060 (See Model 8871) Ch. RC-1060 (See Model 8872) Ch. RC-1061 (See Model 8873) Ch. RC-1064 (See Model 8533) Ch. RC-1065 (See Model 6533) Ch. RC-10664 (See Model 85321) Ch. RC-10664 (See Model 85221) Ch. RC-10664 (See Model 85231) Ch. RC-10664 (See Model 85231) Ch. RC-10664 (See Model 85231) Ch. RC-10704 (See Model 8751) Ch. RC-10704 (See Model 8711) Ch. RC-1077 (See Model 8711) Ch. RC-1077, (See Model 8711) Ch. RC-1077, (See Model 8711) Ch. RC-1077, (See Model 8751) Ch. RC-1079, RC-1079C (See Model 9510) Ch. RC-1070C (See Model 9510) Ch. RC-1070C (See Model 9510) Ch. RC-1070C (See M RCA VICTOR-Cont. Ch. RC-1079E, RC-1079C (See Mode) el 9X531) Ch. RC-1079K, L (See Mode) 1X591) Ch. RC-1080C (See Mode) 2X631) Ch. RC-108D (See Mode) 2X631) Ch. RC-1085, RC-1085A (See Mode) 9X631) Ch. RC-1085, RC-1085A (See Mode) 2X531) Ch. RC-1085, RC-1086A (See Mode) 2X531) Ch. RC-1089, C (See Mode) 4X511) Ch. RC-1090 (See Mode) 47511) Ch. RC-1090 (See Mode) 47511) Ch. RC-1096 (See Mode) 47511) Ch. RC-1096 (See Mode) 4.1081) Ch. RC-1096 (See Mode) 4.1081) Ch. RC-1096A (See Mode) 4.1081) Ch. RC-1010 (See Mode) 4.1081) Ch. RC-1101 (See Mode) 4.1081) Ch. RC-1101 (See Mode) 4.1081) Ch. RC-1111 (See Mode) 210346, U or Model 2117970E) Ch. RC-1111 (See Model 210346, U or Model 2117970E) Ch. RC-1117A (See Model 217393) Ch. RC-1117A (See Model 217393) Ch. RC-1117A (See Model 217393) Ch. RC-1117A (See Model 21757) Ch. RC-1117A (See Model 21757) Ch. RC-1117A (See Model 2257) Ch. RC-1117A (See Model 2257)] Ch. RC-1117A (See Model 2257)] Ch. RC-1112 (See Model 2257)] Ch. RC-1124 (See Model 2257)] Ch. RC-1125 (See Model 2257)] Ch. RC-1124 (See Model 2557)] Ch. RC-1124 (See Model 2757)] Ch. RC-1125 (See Model 2757)] Ch. RC-1124 (See Model 2757)] Ch. RC-1125 (See Model 2757)] Ch. RC-1125 (See Model 2757)] Ch. RC-1124 (See Model 2757)] Ch. RC-1125 (See Model 2757)] Ch. RC-1125 (See Model 2757)] Ch. RC-1124 (See Model 2757)] Ch. RC-1125 (See Model 2757)] Ch. RC-1126 (See Model 2757 Calhoun (See Model 171173, 171-1738) Cameron (See Models 215355, G, GU, U) Clarendon (See Model 215179, DE) Clarendisee Model 211179, DE) Cobeland (See Model 171150) Coveland (See Model 171163) Crandell (See Model 21107, G) Crandell (See Model 21166) Deavville (See Model 21165, U) Deborn (See Model 21177, U) Dobnon (See Model 21177, U) Dobnon (See Model 21177, V) Poinfeld (See Model 2117, V) Poinfeld (See Model 211166DE) Farriell (See Model 21166DE) Farriell (See Model 21369, GU)

RCA VICTOR-SENTINEL

RCA VICTOR-Cont.

 RCA
 VICTOR-Cont.

 Ft. Knox (See Models 215367, G, GU, U)
 Olendale (See Model 171302)

 Glenaide (See Model 171302)
 Olenaide (See Model 171301)

 Hampton (See Model 17116)
 Hampton (See Model 171301)

 Hartford (See Model 171301)
 Hartford (See Model 171301)

 Hartford (See Model 171301)
 Hartford (See Model 171301)

 Hartford (See Model 171301)
 Hartford (See Model 171301)

 Highland (See Model 211316, U)
 Jeffrey (See Model 211312, U)

 Hillsdale (See Model 211313, U)
 Kendale (See Model 211328, U)

 Kendall (See Model 171374, 17174,

Kendali (See Madel 171174, 171-174K) Kent (See Madel 6154, 71104, 711048) Kentwoad (See Madel 171202) Kingbury (See Madel 171202) Kingbury (See Madel 2103, U) Lambert (See Madel 2117208) Langchamps (See Madel 211727) Langchamps (See Madel 270384, U) Master 21 (See Madels 215348, G, U) Master 21 (See Models 215348, G,

Longchamps [See Model 27D384, U] Master 21 (See Models 21S348, G, GU, U) Meredith (See Model 21I354) Meredith (See Model 21I354) Modernette (See Model 21I357, U] Modern (See Model 21735, 71104) Modernette (See Model 21S357G, GU) Northampton (See Model 21735, 71103) Northampton (See Model 21737, U) Penfield (See Model 217244) Prentis (See Model 21714, U) Preston (See Model 21714, U) Preston (See Model 21714, U) Preston (See Model 21734, U) Proston (See Model 21734, U) Proston (See Model 21734, U) Proston (See Model 210346) Rutherford (See Model 210346) Rutherford (See Model 210346) Rutherford (See Model 211374, U) Selfridge (See Model 21789, 211780E) Sewell (See Model 21780, 211780, 211780E) Sewell (See Model 211324, U) Statunton (See Model 211324, U) Statunton (See Model 211324, U) Statunton (See Model 211324, U) Statuton (See Model 211324, U) Statuton (See Model 21731, 211327, U) Sudiok (See Model 211324, U) Statuton (See Model 21732, U) Statuston (See Model 21732, U) Notifick (See Model 21732, U) Statuston (See Model 21732, U) Status RME DB-22A 50-14

HF10-20		49-17
VHF 2-11	 	 79-14
VHF-152A	 	 51-18
45		13-25
84		14-13
200 Tel.		

RADIOLA

61-1, 61-2, 61-3 (Ch. RC-1011) 61-1, 61-2, 61-3 (Ch. RC-1011) 14-25 61-5 (Ch. RC-1023) 12-25 61-8, 61-9 (Ch. RC-10238) 12-21 61-0 (Ch. RC-10238) 12-23 522 (See RCA Model 65U-1) Set 14-25 752U (Ch. RC-1063A) 36-19 752U (Ch. RC-1063A) 36-10 762X11, 762X12 (Ch. RC-1058, RC-1058A) 36-20 Ch. RC-101 (See Model 61-1) Ch. RC-1023, RC-1023B (See Model 61-5) 61-5) Ch. RC-1023B (See Model 61-10) Ch. RC-1034 (See Model 61-8) Ch. RC-1058, RC-1058A (See Model Ch. RC-1063A (See Model 75ZU) RADIO CRAFTSMEN

lso see Craftsmen)

	(Mise see craitsment)
	C400
	RC-1 (Tuner), RC-2 (Audio Amp.)
	39-19
	"Kitchenaire" 6-14
	RC-8 66-13
	RC-10
•	RC100
	RC-100A (Also see PCB 39-Set
	170-2)
•	RC101
•	RC200 (Also see PCB 40 - Set
	172-1)
	RC201
	2
	10
•	202
	500
	800
	RADIO DEVELOPMENT &
	RESEARCH CO.
	(See Magic-Tone)
	(
	RADIOETTE
	PR-2 50-15

RADIONIC

(Also see Chancellor) Y62W, Y728 . 26-22

RADIO MFG. ENGINEERS (See RME)

RADIO RECEPTOR

C-1709-P Tel. UHF Conv... 222-12 RADIO WIRE TELEVISION (See Lafayette)

RANGER 118

28-27 RAULAND BAU21 BA21 W-819-A 87-10 43-16 251-15 1801A . 1805A . 251-15 179-10 99-13 100-10 59-17 97-14 251-15 60-17 58-19 140-10 229-12 148-14 208-9 212-4 1810 1814 820 1820 1821, 1822 1825 1826 (1801A, 1805) 1835 1841 190 1916 1960
 1961
 212_4

 2100
 (Sub-storion)
 39-20

 2101 A. (Master Storion)
 36-21

 2105 (Master Storion)
 36-21

 2105 (Master Storion)
 36-21

 2104 F. (2104)
 236-11

 2112 F. (2112)
 236-11

 2120 S. (2204)
 2212, 22124)

 2306, 2312, 2324
 87-10

 2400 Series
 33-12

 2400 Series
 33-12

 3412, H
 210-6

 3424, H
 210-6
 1961 RAY ENERGY

AD 7-24 AD4 7-25 SRB-1X 13-26 RAYTHEON (Also see Belmont)

A-7DX22P [See Model 7DX21-Set

- C-2103A, C-2105A (Ch. 21AY21)
 T73-1A
 C-2108A (Ch. 21T1) (Also See PCB 87-Set 230-1)
 T89-14
 C-2109A (Ch. 21T2) (For TV Ch. See PCB 97-Set 230-1 and Model C-1735A-Set 189-14. For UHF Tuner See Model UHF-100-Set 207-8)
 C-2110A, C-2111A (Ch. 21T1) (Also See PCB 87-Set 230-1). 189-14
 C-2115A, C-2116A, C-2118A (Ch. 21T3) (Also see PCB 89-Set 233-1)
 C-2129A, C-2129A (Ch. 21T5) (See

C-1735A-Set 189-14) C-2137A, C-2138A (Ch. 21711) 244-B C-2401A, C-2402A (Ch. 2473) 749 FR81A, FR82A (Ch. 9AF25A) 232-6 M701 (Ch. 10AY22) (Although CPC)

-Set 105-1) •M1101, M1103, M1105 (Ch. 12AX-22] (Also see PCB 3-Set 105-1) 94-8

94—8 • M1105B, M-1106, M-1107 (Ch. 12AX26, 12AX27) ...141-11 • M-1402, M-1403, M-1404 (Ch. 14AX21) ...123-12

14AX21) 123-12 •M-1601 (Ch. 16AX23, 25, 26) 99-14
 •M-1601
 •O
 99-14

 •M-1611A
 (Ch. 16AY211), M-16116
 M-16116

 (Ch. 16AY28)
 (Aliso see PCB 19-

 •Set 132-1)
 124--8

 •M-1612A
 (Ch. 16AY211), M-1612B

 (Ch. 16AY28)
 (Aliso see PCB 19-

 Ch. 132-1)
 124--8

RAYTHEON-Cont.

RAYTHEON-Cont.

RECORDIO (Wilcox-Gay)

RECONDIG (WHEOX-Ge 1810 1C-10 1J10 (Ch. 1J1) 2A10 6A10, 6A20 (Ch. 6A) 6B10, 6B20, 6B30, 6B32 7D42, 7D44 (Ch. 7D1) 7E40, 7E44 (Ch. 7D1) 7E40, 7E44 8J10, 8J50 9G10 9G40M 9G42

9G10 9G40M, 9G42 9H408 Ch. 1J1 (See Model 1J10) Ch. 6A (See Model 6A10) Ch. 7D1 (See Model 7D42)

REELEST (See Recorder Listing) REGAL (TOK-FONE)

 Tok-Fone
 (20-wait
 Amp.)
 13-27

 AP40,
 ARP400,
 ARP450.
 15-26

 BP48
 49-18
 49-18

 C473
 217-12
 197

CD31 (See Model 16T31-Set 80-

W700 (See Model W800-

26) W800, W801 W900, W901 •16T31 •17HD31 17HD36

205 208 (See Model W800-271 472

575 747

777 • 1007 • 1030, 1031 1049 1107

●1207, 1208 ●1230 1500

REGENCY

REMLER

RENARD

REMBRANDT

• 1607 • 1708, 1708DX • 1749 • 1877

•2217, 2217DX, 2219, 2219D

16131
17HD31, 17HD36
17T22, 17T22DX
19C31, 19C36
19D31, 19D36

14) CR761 CR762 CR871 FM78 L-7*

-175

y) .149-10 .146-9 .128-12 .163-10 .10-27 .8-27 .52-18 .47-20 .62-17 .91-10

91-10 86-9 89-13

50-16 195-11 238-11 68-14

5-18

-Set 14

14-26 13-28 80-14 147-10 143-13 147-10

147-10

26-23 -Set 14-26 210-7

217-12 210-8 27-22 53-21 83-9 80-14 17-28 41-19 83-9 80-14

41-19 83-9 80-14 38-19 83-9 .143-13 28-29 .182-10

143-13 70-8 69-12

66-14 40-16

KA THEOR-Cont.
 M-1613A (Ch. 164Y211), M-1613B (Ch. 164Y21), M-1613B (Ch. 164Y21), M-1613B (Ch. 164Y21), M-1613B (Ch. 174Y21), (Alto see PCB 19-164), M-1712A (Ch. 174Y21), M-1712B (Ch. 174Y21), (Alto see PCB 19-164), M-1712B (Ch. 174Y21), (Alto see PCB 19-164), M-1713B (Ch. 174Y21), (Alto see PCB 19-164), M-173B, Ch. 174Y21), (See PCB 19-164), M-173B, Ch. 1771), (Alto 199-14), M-173B, Ch. 1771), Ch. 17610, M-1736A, Ch. 1771), Ch. 17610, M-1736A, Ch. 17712), (For TV Ch. See PCB 87-Sei 120-11 and Model C-1735A-Sei 189-14)
 M-173BA, Ch. 17712), (For TV Ch. See PCB 87-Sei 230-1 and Model C-1735A-Sei 189-14)
 M-173DA, C, G, K, M-1731D, F, M-1750D, F, M-1752E, L (Ch. 17718), 261-13
 M-2007A, M-2008A (Ch. 2735D, F, M-1753D, F,

12)
RC-1618A (Ch. 16AY211), RC-1618B (Ch. 16AY28) (Also see PCB 19—Set 132-1). ...124—8
RC-1619B (Ch. 16AY28) (Also see PCB 19—Set 132-1). ...124—8
RC-1718A (Ch. 17AY24) (See PCB 19—Set 132-1). ...124—8
RC-1718B (Ch. 17AY24) (See PCB 19—Set 132-1). ...124—8
RC-1718B (Ch. 17AY24) (See PCB 19—Set 132-1). ...124—8
RC-1719B (Ch. 17AY24) (Also see PCB 19—Set 132-1). ...124—8
RC-1719B (Ch. 17AY24) (See PCB 19—Set 132-1). ...124—8
RC-1719B (Ch. 17AY21) (Also see PCB 19—Set 132-1). ...124—8
RC-1719B (Ch. 17AY21) (Also see PCB 19—Set 132-1). ...124—8
RC-1719B (Ch. 17AY21) (Also see PCB 19—Set 132-1). ...124—8
RC-1719B (Ch. 17AY21) (Also see PCB 19—Set 132-1). ...124—8
RC-1720A (Ch. 17AY21) (Also see PCB 19—Set 132-1). ...124—8
RC-1720A (Ch. 17AY21) (Also see PCB 43—Set 177-1 ond Model C-2001A—Set 149-9)
RC-2117A (Ch. 2173) (See PCB 89—Set 233-1) and Model C-2112A—Set 233-1] and Model C-1735A. UC-1736A, UC-1736A (Ch. 1775) (For TV Ch. See PCB 87—Set 230-1 and Model C1735A—Set 189-14, For UHF Tuner See Model UHF-100—Set 207-8)
UC-1740A, UC-7424 (Ch. 1775) (For TV Ch. See PCB 87—Set 230-1 and Model C1735A—Set 189-14, For UHF Tuner See Model UHF-100—Set 207-8)
UC-2128A, UC-2143A (Ch. 2175) (For TV Ch. See PCB 87—Set 230-1 and Model C1735A—Set 189-14, For UHF Tuner See Model UHF-100—Set 207-8)
UC-2128A, UC-2141A, UC-2142A, UC-2142A, UC-2142A, UC-2143A, UC

REVERE (See Recorder Listing)

 RAYTHEON--Cont.

 10DX21, 10DX22 (Aiso see PCB 3--Set 105-1)

 5et 105-1)

 10DX24 (See Model A.10DX24-Set 75-14)

 18DX21A

 198

 100 Kat X23

 198

 198

 198

 198

 198

 198

 198

 1010

 1011

 1020

 1031

 1031

 1031

 1031

 1031

 1031

 1031

 1031

 ROLAND 215-11 225-14 231-13 231-13 233-9 205-8 208-10 204-9 231-14 238-12 STIE STIV 5T2M 5T3 5T4 236-12 234-11 217-13 247-9 236-12 216-9 214-9 211-11 5X1, 5X2 5X3, 5X4 6P2 6T1M 8FT1M 8XF1, 8XF2 8XF3-M, 8XF4-M 10TF1 249-13 249-14 ROYAL (Lee) AN150, AN160 • 20CP, 20TW (Similar to Chossis) 149–13
 149-13

 SCOTT (E. H.)

 Music Control, Dynamic Noise Suppressor

 46-21

 Wisic Control, Dynamic Noise Suppressor

 46-21

 "Revenswood"

 105-21

 52-19

 16A

 105-21

 52-19

 16A

 100

 100

 100

 100

 100

 100

 100

 100

 100

 100

 1010

 10111A (Alto see PCB 4--Set 105-2 and Model 6T11-Set 52-19)

 1010
 100-14

 510
 100-14

 5115
 165-11

 100-12 and Model 6T11-Set 52-19

 105-2 and Model 6T11-Set 52-19

 8172 (Ch. 9024, 9031) (See Model 820C-Set 178-9)

 8172 (Ch. 9024, 9031) (See Model 820C-Set 178-9)

 8171 (Ch. 9029, 9031) (See Model 820C-Set 178-9)

 8171 (Ch. 9024, 9037, 9038, 9039)

 8171 (Ch. 9034, 9037, 9038, 9039)

 8171 (Ch. 9034, 9037, 9038, 9039)

 8171 (Ch. 9034, 9037, 9038, 9039)

 SCOTT (E. H.)
 217-1
 217-1

 821CE (Ch. 9043)
 234-12

 821CB (Ch. 9036, 9037, 9038, 9039)
 17-14

 821CB (CH. 9043)
 234-12

 821CB (CH. 9036, 9037, 9038, 9039)
 17-14

 821CB (CH. 9043)
 217-14
 •821D, DB, DBH, DM, DMH [Ch. 9043] 234-12 234-12 217-14 234-12 0MH (Ch. 242-9 150-11 176-11 242-9 180-8 • 924W • 924XW (Ch. 9045) 1000 181
 1310
 229-13

 2000
 229-13

 2510
 233-10

 Ch. 9029, 9031 (See Model 817C)

 Ch. 9036, 9037, 9038, 9039 (See Model 817C)

 Ch. 9045 (See Model 817C)

 Ch. 9045 (See Model 817C)
 SCOTT (H. H.) SCOTT (H. H.) 99.A 111-B 112-B 120.A 210.A 210.A 211-A 211-A 214.A (120.A, 220.A). 220-A .257-14 .143-14 .144---8 .183-13 .79-15 .145--9 .81-14 183-13 SEARS-ROEBUCK (See Allstate or Silvertone) SEEBURG (See Record Changer Listing) SENTINEL 1U-284GA 22-25 1U-284I, 1U-284NA, 1U-284NI, 1U-284W 1-2 10.2841, 10.284NA, 10.284NI, 10.284NI, 10.284NI, 10.284NI, 10.284NI, 10.284NI, 10.285P, 6-27 10.2937, 10.2937, 10.2937, 10.293W, 10.14 10.2941, 10.2947, 10.294W, 10.294T, 1-11 10.312PG, 10.312PW, 103.214 10.312, 10.312W, 39-21 10.314, 10.314W, 39-21 1U-3131, 1U-313W 1U-314E, 1U-314I, IU-314W 122-9 111-12 129-10 155-14 212-6 211-12

RC-600 Tel. UHF Conv..... 200---8 •721, 1606, 1606-15, 1950. 65-11 MP5-5-3 5300B, 5300B1, 53001.... 23-18 40-17 44-19
 53006, 53001, 23–18

 5310
 40–17

 5400, 5410
 44–19

 5500
 "Scottie Pup"
 27–23

 5505
 "Scottie Pup"
 27–23

 5515
 "Scottie Pup"
 27–23

 5515
 "Scottie Pup"
 27–23

 5500
 "Scottie Pup"
 27–23

 5515
 "Scottie Pup"
 254

 5500
 "Scottie Pup"
 27–23

 5520
 SScottie Pup"
 10

 5200
 "Scottie Pup"
 27–23

 5200
 Scottie Pup"
 10

 5200
 Scottie Pup"
 10

 5200
 Scottie Pup"
 17–23

 5200
 Scottie Pup"
 17–9
 1U339-K 1U340-C 1U342K 1U-343 1U-344 1U345P 10346

183-14

12

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. 🔸 Denotes Television Receiver.

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SENTINEL-SILVERTONE

SILVERTONE-Cont.

SENTINEL-Cont.
• 10420B
10421, 10422 (Series ''YA'') (See
PCB 16-Set 126-1 and Model
•1U4208
412-3er 100-11)
• 10423 (Also see PCB 19-Set
132-1)
@1114238 111423.17 (See PCR 10_
6-1 120 1
132-1)
[24-9]
•1U424 (Also see PCB 19-Set 132-
11 124 0
1)
-10424-17 [See PCB 19-Set 132-1
and Model 10424-Set 124-9)
• 1U-425
and Model 1U424Set 124-9) 1U-425
•1U428
•10429, 10430, 10431 (See PCB 25
-Set 144-1 and Model 1U420B-
Set 124-9)
•1U-432 [Also see PCB 21-Set 136-
10-452 (AISO SEE FCB 21-3ET 130-
1) 127-10 10435 (See PCB 21-Set 136-1 and 10435 (See PCB 21-Set 136-1 and
 1U435 (See PCB 21—Set 136-1 and
Model 1U425-Set 127-10)
Model 10425Set 127-10) •10438, 10439, 10440, 10441, 10- 443, 10444 (Series ''XD, XXD, 2XD'') 1579
443, 10444 (Series XD, XXD,
2XD'') 157-9 •1U446, 1U447 (Series 'XD, XXD, 2XD'') (See Model 1U438-Set
●1U446, 1U447 (Series ''XD, XXD,
2YD''I (See Model 111428 Set
2X0) (See model 10430-Set
157-9)
10447-A, 10448-A, 10449-A, 10-
450-A 1U451-A
10447-A, 10448-A, 10449-A, 10- 450-A, 10451-A,
10440, 10-447, 10-450 (Series
AD, AAD, ZAD) (See Model
1U-438—Set 157-9)
10-454, 10-455, 10-456, 10-457
(Also see PCB 63_Set 107.1
U-438—Set 157-9) ●1U-454, 1U-455, 1U-456, 1U-457 (Also see PCB 63—Set 197-1 191-17
(Also see PCB 63—Set 197-1 191-17 •1U-458, 1U-459, 1U-460, 1U-461 199-10
01U462, 1U463 (Ch. 2WA) 205-9
• 111500
•10300
199-10 1U462, 1U463 (Ch. 2WA). 205-9 1U500
•1U515
• 111.520 226 S
- 14 500D /C DCD 07 C + 040 1
-10-320B (See PCB 97-Set 242-1
and Model 1U-520-Set 226-8)
•1U-521
@111.5218 (See PCB 97_ Set 242 1
and Model 10-521-Set 226-8)
1U-521
●1U-522B (See PC8 97-Set 242-1
- 111 500
•10-523
•10525
•10-532, A
01U-542 A 230_8
• 111 552 111 654
•10-552, 10-554
and Model 10-522Set 2268 1U-523 2268 1U5525 2268 1U-524, A 2398 1U-542, A 2398 1U-552, U-554 2398 1U-562, 1U-554 2398 1U-562, U-564 2398

• 1U-701 • 1U-711 • 1U-714

1U-72 U-724 U-752 U-755 U-758 11-762 U-765

L-2841, L-284NA, L-284NI, NR, L-284W 284GA

2841 284NA, 284NI 285P

285P 286P, 286PR 289T

293 Series 293-CT

292K

342k 343 344 345P 346 • 400TV • 401, 4

405TVM
405 Series
406 Series
407 Series
409 Series

SETCHELL-CARLSON 20-LR 155-15 2-14 21-29 39-22 40-20 106-13 99-15 209-12 97-15 144-9 437 447 458-RD 469 • 531 (Ch. 152) 570 • 2500, 2500LP • 5301, 5302 (Ch. 152) Ch. 152 (See Model 53) Ch. 153 (See Model A53) 209-12 SHAW • Ch. 224 (Runs 301, 302, 303, 304, 304-1, -2, 305, 305-2) ... 202-8 SHERATON (Also See Video Products) C308, M. 176–13 C30824, C30024. 176–13 C-2125 (Ch. 250XL Series) 218–10 T76–13 T-1755 (Ch. 250XL Series) 218–10 T-7755 (Ch. 250XL Series) 218–10 T-7755 (Ch. 250XL Series) 218–10 T-7755 (Ch. 250XL Series) 218–10 T-77720 (Ch. 530DX-A) (See PC8 89 -Set 233-1 and Model 17MT20— Set 210-9) 218C10 (Ch. 530DX Series) 210–9 218D10 (Ch. 530DX Series) 210–9 218000 (Ch. 530DX Series) 210–9 218000 (Ch. 530DX Series) 210– SHERATON (Also See Video Products) 10-562, 10-564, 239-8
 10-581, 10-582, 240-7
 10-584, 10-582, 240-7
 10-584, 10-585, 240-7
 10-600, 10-500-584, 226-8|
 10-610, 10-612 (See PCB 97-Set 242-1)
 and Model 10-510-Set 226-8|
 10-620, 10-622 (See PCB 97-Set 242-1)
 and Model 10-520-Set 226-8|
 10-620, 10-622 (See PCB 97-Set 242-1)
 and Model 10-520-Set 226-8|
 10-620, 10-622 (See PCB 97-Set 242-1)
 and Model 10-520-Set 226-8|
 10-620, 10-622 (See PCB 97-Set 242-1)
 and Model 10-520-Set 226-8|
 10-620, 10-622 (See PCB 97-Set 242-1)
 and Model 10-520-Set 226-8|
 10-620, 10-622 (See PCB 97-Set 242-1)
 and Model 10-520-Set 242-10
 and 30-520-Set 2 2 model 10-320-347 242-11 24 L-284 23-19 22-29 1-20 1-20 1-20 6-27 -19 23-20 6-28 16-30 1-14 29-22
 292K
 16-30

 2923
 series
 1-14

 293-CT
 29-22

 2931
 2931

 2941
 2944

 2945
 Series

 2941
 2944

 2945
 Series

 2941
 2944

 2945
 Series

 2946
 2964

 2965
 2964

 2965
 2964

 2965
 2964

 305-1
 305-1-3

 305-1
 305-1-3

 305-1
 305-1-3

 305-1
 305-1-3

 305-1
 305-1-3

 3126
 302-13

 314-1
 314-14

 313
 See Model 313-1-Ser

 314-1
 314-14

 313
 See Model 313-Ser

 313
 See Model 313-Ser

 313
 See Model 313-Ser

 314-1
 314-4

 314-1
 314-4

 314-1
 314-4

 315-14
 344

 344
 SHERIDAN ELECTRONICS (See Vogue) SIGNAL
 37-19

 141
 44-21

 241
 33-25

 341-A
 39-23

 341-T
 25-25
 SILVERLINE (See General Instrument)
 1/0 ki (Jiso See Chonger and Recorder Listing)

 1 (Ch. 132, 878)

 1 (Ch. 132, 877)

 1 (Ch. 133, 247)

 2 (Ch. 132, 888)

 409 Series

 411 Series (See Model 401 Series— Set 70-9)

 412, 413, 414, 415 (Series YA, YB, YC, YO, YE, YF) (Alto see PCB 4 (Set 105-2)

 416

 417-12

 419, 420

 415-9

SENTINEL-Cont.

 419, 420
 124--9
 4208
 124--9
 421, 422 (See PCB 16-Set 126-1
 and Model 412--Set 100-11)
 423, 424 (Also see PCB 19-Set
 132-1)
 124-9
 4238. 423-17 (See PCB 19-Set
 132-1 and Model 423B-Set
 124-9
 δ7 (Ch. 101.859-1, 2) (See Model 64 — Set 113-8)

 δ7B (Ch. 101.859-2) (See Model 64 — Set 113-8)

 69 (Ch. 100.201)
 162-10

 72 (Ch. 134.11)
 142-11

 ● 101 (Ch. 549.100)
 102-12

 ● 1024 (Ch. 549.100-1)
 102-12

 ● 1024 (Ch. 549.100-1)
 102-12
 NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

www.americanradiohistory.com

-1, -2) .215–12 .221—9

111

 SILVERTONE-Cont.

 1188-20 (Ch. 110.700-1401 201-88

 1239 (Ch. 488.237) (See Model 237

 -Set 145-10)

 1260 (Ch. 456.150.-2)

 1261 (Ch. 456.150.-2)

 1262 (Ch. 456.150.-2)

 1263 (Ch. 456.150.-2)

 1264 (Ch. 456.150.-1)

 1270.21 (Ch. 456.150.1)

 1270.21 (Ch. 456.150.1)

 1270.21 (Ch. 456.150.1)

 1272.21 (Ch. 456.150.1)

 1272.21 (Ch. 456.150.1)

 1272.21 (Ch. 456.150.1)

 1273.21 (Ch. 456.150.1)

 1274.21 (Ch. 456.150.1)

 1275.21 (Ch. 456.150.1)

 1300 (Ch. 319.200, 1300-1 (Ch. 319.200, 10-10)

 2001, 2002 (Ch. 132.878) (See Model 1-Set 101-10)

 2003, 2004, 2005, 2006 (Ch. 7.57.-110)

 2007 (Ch. 737.100)

 1200, 2003, 2004, 2005, 2006 (Ch. 7.57.-110)
 SILVERTONE-Cont SILVERTONE-Cont.
 SILVERTONE-Cont.

 0106, 107 (Ch. 132.889-2).149-12

 0108 (Ch. 549.100)....102-12

 010, A (Ch. 478.303, A) (See Model 125-5et 104-10)

 0112 (Ch. 478.302) (See Model 125 -5et 104-10)

 0112 (Ch. 478.303) (See Model 125 -5et 104-10)

 0115 (Ch. 110.499-7A, B, BA, B)
 •116, 116A (Ch. 110.700-1, -10) 139–13 •120 (Ch. 478.311) •125 (Ch. 478.257) 104–10 116, 116A [LR. 110.7001, 139-13
 120 (Ch. 478.311) 115-11
 125 (Ch. 478.237) 104-10
 131, 131A (Ch. 110.700-1, -10)
 132 (Ch. 110.499-1) (See Model 9123—Set 79-16)
 133 (Ch. 100.107 and Radio Ch. 100.043) 156-12
 133 (Ch. 110.499-7A, B, 8A § B) 2003, 2004, 2005, 2006 (Ch. 757.-110) 211-13 2007 (Ch. 757.100) 211-13 2009, 2010, 2011, 2012, 2013 (Ch. 132,022) 196-14 2014, 2015, 2016 (Ch. 132.021) 2022 (Ch. 132.027) 197-11 2033, 2024, 2025, 2026, 2027 (Ch. 132,896-1) (See Model 10-Set 144.11) 2028 (Ch. 528.230) 203-8 20354 (Ch. 528.230) 203-8 20354 (Ch. 528.195, -1, -2) 204 (Ch. 528.195, -1, -2) 2054 (Ch. 528.195, -1, -2 ■ 135 (Ch. 110.499-7A, B, BA, B)
 ■ 137 (Ch. 549.100-1 and Radio Ch. 101.831-1) (For TV Ch. See Madel 101—5er 102-12, for Radio Ch. see Model 8127—5er 41-20]
 ■ 138 (Ch. 549.100-3 and Radio Ch. 101.831-1) (For TV Ch. see Model 8127—5er 41-20]
 ■ 138 (Ch. 549.100-3 and Radio Ch. 101.831-1) (For TV Ch. see Model 8127—5er 41-20]
 ■ 143 (Ch. 132.889-2). 149-12
 ■ 143 (Ch. 100.11) . 121-12
 ■ 143 (Ch. 100.11) . 121-12
 ■ 144 (Ch. 478.312 and Radio Ch. 478.230). 160-11
 ■ 149 (Ch. 100.107-1) (See Model 133—5er 156-12)
 ■ 50-14 (Ch. 478.338). . 142-12
 ■ 150-14 (Ch. 478.338). . 142-12
 ■ 151-17 (Ch. 528.630-1) 2028 (Ch. 528.230) ... 203-2035A (Ch. 528.235) ... 208-11 2041 (Ch. 528.235) ... 208-11 2041 (Ch. 528.235) ... 208-11 2041 (Ch. 528.235) ... 207-2053, 2064 (Ch. 101.861, -1) 2053, 2064 (Ch. 102.2021 (See Model 1066-Set 162-10) 20100 (Ch. 110.700-100, -104) 21004 (Ch. 110.817-1) ... 217-15 2105 (Ch. 132.024, -1, -2) 198-13 21054 (Ch. 120.204, -1, -3, -5) 21105 (Ch. 132.024, -1, -3, -5) 21205 (Ch. 132.024, -1, -2, -5, -5) 21205 (Ch. 132.024, -1, -2, -5, -5) 21205 (Ch. 132.024, -1, -2, -5, -5) 21205 (Ch. 100.210, -1, -3) 207-10 2140 (Ch. 110.817-1) ... 217-15 21458 (Ch. 132.024, -1, -2) 198-13 21459 (Ch. 132.024, -1, -2) 198-13 21450 (Ch. 110.700-100, 201-8 21500 (Ch. 110.700-100, 201-8 21500 (Ch. 110.200-1, -2) 107-8 21500 (Ch. 110.200-1, -2) 120-7 21500 (Ch. 110.200-1, -2) 120-7 21500 (Ch. 110.200-1) ... 217-15 21508 (Ch. 132.024, -1, -2) 798-13 21500 (Ch. 110.200-1) ... 217-15 21508 (Ch. 132.024, -1, -2) 798-13 2150 (Ch. 100.200-1) ... 217-15 21508 (Ch. 132.024, -1, -2) 79-10 21509 (Ch. 132.024, -1, -2) 79-10 2174 (Ch. 132.0251) ... 16528.23 ... 217-7 2160, 2162 (Ch. 528.631, -1, Ch. 528. 632A, -1, -2, -3, -5) ... 212-7 2170-0, -E (Ch. 100.200, -1, -3] 207-10 2172 (Ch. 100.201, 01.2054) 239-9 2225 (Ch. 528.233) ... 208-10 2210 (Ch. 132.930) (See Model 1066-5et 109-12) 2215, 2217, 2218 (Ch. 528.230) ... 219-9 2225 (Ch. 528.233) ... 208-10 2200-222 (200, 200) (See Model 1066-5et 109-12) 215, 2217, 2218 (Ch. 528.230) ... 208-10 2200 (Ch. 132.940) (See Model 1066-5et 109-12) 2215, 2217, 2218 (Ch. 528.230) ... 208-10 2200 (•168-16 (Ch. 549.100-3) ... 161-9 •169-16 (Ch. 549.102, 549.102-2) •170-16 {Ch. 549.102, 549.102A} 170-16 (Ch. 549, 102, 347, 102A)
173-16 (Ch. 110, 700-10). 139-13
175-16 A (Ch. 547, 100-5, 8. 9)
176-19 (Ch. 549, 100-6), 8. 9)
176-19 (Ch. 10, 700-40). 139-13
179-16 (Ch. 100, 700-40). 130-12
185-16 (Ch. 549, 101-2).
185-16 (Ch. 549, 101-2).
185-16 (Ch. 549, 101-3).
187-16, 188-16 (Ch. 110, 700-10)
(See Model 116—5e1 139, 13)
189-16 (Ch. 110, 700-1, -10)
189-16 (Ch. 132, 890) • 189-16 (Ch. 110.700-1, -10) 139-13 (14.10, 195-16 (Ch. 132.890) 130-12 (15.10, 132.880) (199-12 (15.10, 132.890) 215 (Ch. 528.174) (177-13 (177-13) (1 239 (Ch. 548.360-1, 115-12 245 (Ch. 548.358-1) 107-9 246 (Ch. 137.906) 111-14 249 (Ch. 548.360-1, 548.361) 115-12 249 (Ch. 548.360-1, 548.361) 115-12 246 (Ch. 137,906) 111-114 247 (Ch. 137,906) 111-114 249 (Ch. 137,906) 112-11 1037, 1018 (Ch. 528,210, 1-21 1033, Ch. 528,196, 1-32 1035, A (Ch. 528,196, 1-32 1036, Ch. 528,196, 1-32 1036 (Ch. 528,194,196, 1-32 1040, 1045 (Ch. 528,194,1181-12 1040, 1045 (Ch. 528,194,1181-12 1040, 1045 (Ch. 528,194,1181-12 1040, 1045 (Ch. 528,194,11) (See Model 1040-Set 181-12) 1040 (Ch. 528,194,11) (See Model 1040-Set 181-12) 1045 (Ch. 132,011, 174-10 1053 (Ch. 132,011, 174-10 1053 (Ch. 132,011, 173-12 10554 (Ch. 132,012, 173-12 10554 (Ch. 132,012, 173-12 10554 (Ch. 132,012, 173-12 10554 (Ch. 132,012, 173-12 10555 (Ch. 101,800,162-11 1065 (Ch. 102,002, 162-10 1055 (Ch. 101,800,162-11 1066 (Ch. 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 1064, 100,202, 162-10 201-80 100,17, 11300-17 (Ch. 110,700-100, 104) 3032 (Ch. 528.527) 3035A (Ch. 528.253) 215-12 3040 (Ch. 528.253) 21-9 3041 (Ch. 528.253) 221-9 3041 (Ch. 528.254) (See Model 2041-Set 208-11) 3045, 3046 (Ch. 528.254) 216-10 3052, 3053 (Ch. 132.053) 225-15 3054, 3055 (Ch. 132.053) 225-15 3054, 3055 (Ch. 132.054) 225-15 3054, 3055 (Ch. 132.054) 225-15 3054, 3052 (Ch. 101.840-31 240-8 3064 (Ch. 101.861-1) (See Model 2060-Set 203-9) 3063, 3064 (Ch. 101.860-3) 240-8 3067 (Ch. 101.861-3) (See Model 2100A-Set 217-15) 3100 (Ch. 110.817-1, -3) (See Model 2100A-Set 217-15) 3101 (Ch. 110.817-1, -3) (See Model 2100A-Set 217-15) 3101 (Ch. 10.817-3) (See Model 2100A-Set 217-15) 3101 (Ch. 10.817-3) (See Model 2100A-Set 217-15) 3102X (Ch. 528.271, -1, -2, -3, -4, -5) (See Model Model-Set 217-15) 3104 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 215-1) 3105 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3106 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3109 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see PCB 90-Set 235-1) 3100 (Ch. 132.045, -1, -2, -3, -4, -5) (Also see P •1172-17 {Ch. 110.700-100. -104} 201-3 1173-20 (Ch. 110.700-140) 201-8 1176-21 (Ch. 101.208) ...165-12 1181-20 (Ch. 110.700-120) 201-8 1183-21 (Ch. 110.700-150) 201-8 1184-20 (Ch. 528.631, -1) 181-13 1186-21 (Ch. 100.208) ...165-12

SILVERTONE-SONORA

SILVERTONE-SONORA
SILVERTONE—Cont. •127W (Ch. 456.200-11, -12, -13, -21, -22, -23) (See PCB 109—Set 257.1 and Model 3376—Set 225-
257-1 and Model 3376—Set 225- 16)
16) 227-12 •128 (Ch. 528.264-2) .227-12 •128 (Ch. 528.262,27) .253-12 •129 (Ch. 528.263-2) .237-12 •129 (Ch. 528.263-2) .227-12 •1294 (Ch. 528.263-2) .227-12 •1295 (Ch. 528.362,1) .245-6 •1296 (Ch. 528.362,0) .235-12 •1292 (Ch. 528.264,2) .245-6 •1292 (Ch. 528.362,00,11, .12, -13,,,,,,,, .
•4129 (Ch. 528.263-2)
•4129B (Ch. 528.303, -1)245—6 •4129W (Ch. 456.200-11, -12, -13, -21 -22, -23) (See PCB 109—
Set 257-1 and Model 3376-Set 225-16)
•4131 (Ch. 528.263-1)227-12 •4132 (Ch. 528.291-2)253-12 •41328 (Ch. 528.291-3) (See Model
4111A-Set 253-12) • 4133 (Ch. 528.292-2, -3) 245-6
(See Model 41188—Set 245-6) •4135 (Ch. 528.292, -1, -3) 2456
•41358 (Ch. 528,292, -1, -2, -3, -4) (See Model 4113ASet 245-6)
•4139 (Ch. 528.270)
•4140 (Ch. 528.247, -1) 217-16 •4140D (Ch. 528.266-1) 227-12
4140 (Ch. 528.299-2, -3) .253-12
•4143 [Ch. 528.247, -1]217-16 •4143D [Ch. 528.266-1]227-12
•4145 (Ch. 528.247, -1)217-16 •4145 (Ch. 528.266-1)227-12
•4149 (Ch. 528.270)
•4150 (Ch. 528.247, -1)
•4153 (Ch. 528.247, -1) 217-16 •4153D (Ch. 528.286) 227-12
225 -16) 4 (13) (Ch. 528,263-1) 227-12 4 (132) (Ch. 528,291-2) 253-12 4 (132) (Ch. 528,291-2) 253-12 4 (132) (Ch. 528,292,-1) .25,-3,-4) (5e Model 41188-5et 245-6) 4 (133) (Ch. 528,292, -1, -3) .2456 4 (135) (Ch. 528,292, -1, -3) .2456 4 (135) (Ch. 528,292, -1, -3) .2456 4 (135) (Ch. 528,292, -1, -3) .2456 4 (139 (Ch. 528,299, -1, -2) 4 (140) (Ch. 528,247, -1) 217-16 4 (140) (Ch. 528,247, -1) 217-16 4 (140) (Ch. 528,240, -1) 227-12 4 (143) (Ch. 528,240, -1) 227-12 4 (143) (Ch. 528,240, -1) 227-12 4 (143) (Ch. 528,240, -1) 227-12 4 (145) (Ch. 528,240, -1) 227-12 4 (146) (Ch. 528,240, -1) 227-12 4 (147) (Ch. 528,247, -1) 217-16 4 (1350) (Ch. 528,240, 227-12 4 (136) (Ch. 528,240, 227-12 4 (1350) (Ch. 528,240, 227-12 4 (136) (Ch. 528,240, 227-12 4 (136) (Ch. 528,240, 227-12 4 (136) (Ch. 132,0607) 255-13 4204 (Ch. 132,067) 255-13 4204 (Ch. 132,081) 15-29 6052 (Ch. 104,521) 15-29 6052 (Ch. 104,521) 15-29 6052 (Ch. 104,521) 15-29 6052 (Ch. 104,521) 15-29 6052 (Ch. 104,522)
•4155D (Ch. 528.286) 227-12 •4155E (Ch. 528.300-2, -3) 2456
4200 (Ch. 757.140)
4242 (Ch. 548.401-1)258-11 • 5111 (Ch. 528.302, -1)253-12
• 5113 (Ch. 528.303-1) (See Model 4118C—Set 245-6) 6002 (Ch. 132 818) 5-35
6011 (Ch. 132.816), 6012 (Ch. 132.816A) 15–27
6016 (Ch. 132.820) 27-24 6050 (Ch. 132.825-4) 15-28 6051 (Ch. 110.451) 6052 (Ch.
110.452} 13-29 6052A (Ch. 110.452, -1) [See Mod-
el 6051—Set 13-29) 6071 (Ch. 132.826-1) 15-29 6072 (Ch. 110.464) 13-20
6092 (Ch. 101.672-18), 6093 (Ch. 101.672.1A) 10-28
6100 (Ch. 101.660-1A) 6-29 6104 (Ch. 101.662-2D) (See Model
6105 (Ch. 101.622-2B) 7-26 6106A (Ch. 101.662-4E). 29-23
6111 (Ch. 101.662-3C) 7-26 6111A (Ch. 101.662-5F) 29-23 6200A (Ch. 101.800.21) 45 12
6200A [Ch. 101.800-1] 9-29 6203 [Ch. 101.800A] (See Model
6200A-Set 9-29) 6220, 6220A (Ch. 101.801, 101
6230 (Ch. 101.802) 11-21 6230A (Ch. 101.802-1) 11-21
6285A (Ch. 101.666-18) 20-28 6286 (Ch. 528.6286, -1, -3) 185-12 6287 (Ch. 528.6287, -1, -3) 185-12
2434 (Ln. 201390-187. 25-29 2526 (Ch. 528.528, -1, 31185-12 2626 (Ch. 528.528, -1, 31185-12 2629 (Ch. 528.428, -1, 31185-12 2629 (Ch. 528.428, -1, 3120-20 2629 (Ch. 528.4295) 98-12 26455 (Ch. 139.150, Ch. 139.150-11 26455 (Ch. 139.150, Ch. 139.150-11 2650 (Ch. 725.10, 11) Tel. JUHE
6295 (Ch. 528.6295) 98-12 6685 (Ch. 139.150, Ch. 139.150-1). Power Shifter 15-30
7021 (Ch. 101.807, 101.807A)
16-31 7025 {Ch. 132.807-2} 29-24 7054 {Ch. 101.808} 15-31 7070 {Ch. 101.817} 30-26 7080 {Ch. 101.809} 16-32 7080 {Ch. 101.809} 16-32
7070 (Ch. 101,817) 30-26 7080 (Ch. 101,809) 16-32 7080, 7080A (Ch. 101,809-2)
root, rooter (ch. toriotrici,
7115 C.4 14 221
7100 (Ch. 101.811) 17–29 7100 (Ch. 101.814) 30–27 7103 (Ch. 110.466-1) 27–25 7113 (Ch. 110.466-1) 37–25 7111 (Ch. 434.140) 30–28 7115 (Ch. 101.825), 7116 (Ch. 101.825-1A), 7117 (Ch. 101–
7111 (Ch. 434,140)
7119 (Ch. 101.825-2C) 62-18 7145 (Ch. 436 200) 23-21
7153 (Ch 109 627) 26-30
7165 (Ch. 101.823.A, 1A). 10 -29 7166 (Ch. 101.823, 101.823-1) 10-29
7210 (Ch. 101.820) 32-20 7220 (Ch. 101.801-2C) (See Model
7226 (Ch. 101.819A) 31-28 7230 (Ch. 101.802-2A) (See Model
6230—Set 11-21) 7300 (Ch. 435.240)
7262 /6 // / 7260 6 . 28 201
8005 (Ch. 132.839) 33-26 8010 (Ch. 132.840) 40-21 8011 (See Model 8010,—Set 40-21)

SILVERTONE-Cont. 8020 (Ch. 132.841) 43-17 8021 (Ch. 132.848) 70-10 8024 (Ch. 132.868) 70-10 8024 (Ch. 132.868) 70-10 8024 (Ch. 132.868) 70-10 8054 (Ch. 101.813) 33-27 8051 (Ch. 101.839) 49-19 8052 (Ch. 101.808-10) (See Model 8052-Cei 68-15) 8070 (Ch. 101.817-1A) (See Model 7070-Sei 68-15) 8072 (Ch. 101.8341) 34-19 8073 (Ch. 101.8242) 52-20 8080 (Ch. 101.852) 52-20 8083, 8083A (Ch. 101.807-14) 58-20
8021 (Ch. 132.868) 70-10 8024 8025 (Ch. 478.206-1) 80-15
8050 (Ch. 101.813) 33-27 8051 (Ch. 101.839) 49-19
8052 (Ch. 101.808-1C) 68-15 8053 (Ch. 101.808-1D) (See Model
8052-Set 68-15) 8070 (Ch. 101.817-1A) (See Model
7070—Set 30-26) 8072 (Ch. 101.834) 34-19
8073 (Ch. 135.243) 84—9 8080 (Ch. 101.852) 52–20
8083, 8083A (Ch. 101.809-1A) 58-20
8084, 8084A [Ch. 101.809-18] 58-20
8086 (Ch. 101.814-5C) 61-18 8086A, 8086B (Ch. 101.814-6C)
8090 (Ch. 101.821) 61-18 49-20
8097 (Ch. 101.825-3G) (See Model 8115-Set 62-18)
8097A (Ch. 101.825.4) 62–18 8100 (Ch. 101.829) 51–19
8101, 8101A, 8101B, 8101C (Ch. 101.809-3C) 58-20
8102 (Ch. 101.814-28)
8102B (Ch. 101.814-2B) 61-18 8103 (Ch. 110.473) 56-21
8104 (See Model 8080-Set 61-16) 8105, 8105A (Ch. 101.833) 35-20
Model 8105-Set 35-20)
8109 (Ch. 101.851-1) 64-10 8112 8113 (Ch. 101.851) (See
B084, 8084A (Ch. 101.80-16) B084, 8084A (Ch. 101.81-30-16) B086 (Ch. 101.814-3C) B086 (Ch. 101.814-3C) B086 (Ch. 101.814-3C) B086 (Ch. 101.821) 40-20 B097 (Ch. 101.821) 40-20 B097 (Ch. 101.825.41) 61-18 8100 (Ch. 101.825.41) 61-18 8100 (Ch. 101.825.41) 610-18 8100 (Ch. 101.825.41) 610-18 8100 (Ch. 101.825.41) 610-2 8107.8 (Ch. 101.814.381) 81028 (Ch. 101.814.28) 81028 (Ch. 101.814.28) 81028 (Ch. 101.814.28) 81028 (Ch. 101.814.28) 81028 (Ch. 101.813.31.4) 81028 (Ch. 101.831.31.4) 8103 (Ch. 101.831.31.4) 8104 (See Model 8060–Set 61-18) 8105, A106, 81038 (Ch. 101.831.31.4) 8107, 8106, 81038 (Ch. 101.831.31.4) 8107, 8106, 81038 (Ch. 101.831.31.4) 8107, 8106, 81038 (Ch. 101.831.4) 8107, 8106, 81038 (Ch. 101.831.4) 8107, 8106, 81038 (Ch. 101.831.4) 8107, 8106, 81038 (Ch. 101.831.4) </td
8115, A, B, C (Ch. 101.825-4) 62-18
6115, A, B, C (Cl. 101.825-4) 62-18 8115D (Ch. 101.825-4) (See Model 8115 A (Ch. 101.825-31) 8117 (Ch. 101.825-35) 62-18 8118 (Ch. 101.825-35) 62-18 8118 (A, B, C (Ch. 101.825-3) 62-18 8118 (A, Ch. 101.825-31) 62-18
8117 (Ch. 101.825-3E) 62-18 8118 (Ch. 101.825-3F) 62-18
8118 A, B, C (Ch. 101.825-4) 62-18
8118D (Ch. 101.825-4) (See Model 8118A-Set 62-18)
8118 (Ch. 101.825-37) ∞2-18 8118 A, B, C (Ch. 101.825-4) 562-18 8118D (Ch. 101.825-4) (See Model 8118A—Set 62-18) 8127.9 8124, 8125, 8126 (Ch. 101.831A, 101.831-1) (See Model 8127— Set 41-20) 8127. A, B, C (Ch. 101.831A), 18128, A, B, C (Ch. 101.831A), 8127, A, B, C (Ch. 101.831A), 8128, A, B, C (Ch. 101.831A), wire Recorder Amp. (Ch. 101.831A), 9129, A, B, C (Ch. 101.831A) 8120 8127—Set 41-20) 8130 (Ch. 101.834) 66-15 8133 (Ch. 101.834) 66-15 8133 (Ch. 101.834) 66-15 8144 (Ch. 431.199) 32-21 8145 (Ch. 109.431) 45-23 8146 (Ch. 109.433) 48-23 8147 (Ch. 109.433) 48-23 8150 (Ch. 109.433) 48-23
8127, A, B, C (Ch. 101.831A), 8128 A B C (Ch. 101.831A)
Wire Recorder Amp. (Ch. 101 773) 41-20
8127CX (Ch. 101.831A and Wire Recorder Amp, 101.773) (See
Model 8127-Set 41-20) • 8130
8132 (Ch. 101.854)
66-15 8144 (Ch. 431.199) 32-21
8145 (Ch. 109.631) 45-23 8148 (Ch. 109.632) 44-22
8149 (Ch. 109.633) 48-23 8150 (Ch. 109.634) 32-22
8152 (Ch. 109.035) [See Model 8153—Set 42-22]
109.635-1)
8160 (Ch. 109.636A) 50-17 8168 (Ch. 109.638) 46-23
8169 (Ch. 109.638) (See Model 8168-Set 46-23)
■8133 (Ch. 101.829-1, (Ch. 101.846) ■8133 (Ch. 101.829-1, (Ch. 101.846) ■144 (Ch. 431.199) 32-21 8145 (Ch. 109.631) 45-23 8148 (Ch. 109.632) 44-22 8148 (Ch. 109.633) 48-23 8150 (Ch. 109.634) 32-22 8152 (Ch. 109.634) 32-22 8153 (Ch. 109.635) [See Model 8153 = 42-27] 8153 (Ch. 109.635) 57-17 8160 (Ch. 109.635) 57-17 8160 (Ch. 109.635) 57-17 8160 (Ch. 109.635) 42-22 8155 (Ch. 463.155) 57-17 8160 (Ch. 109.635) (See Model 8168 = Set 42-23) 8169 (Ch. 109.638) (See Model 8168 = Set 46-23) 8200 (Ch. 101.800.28) (See Model 8200 (Ch. 100.800.28) (See Model 8200 (Ch.
12)
8220, 8221 (Ch. 101.801-3D) (See
8222 (See Model 6220—Set 9-30) 8230 (Ch 101 835) 59-18
8231 (See Model 8230-Set 59-18) 8260 (Ch. 101.823-28) (See Model
B201 [See Model 6200A—Set 65.] 12) [See Model 6200A—Set 65.] 12) [See Model 6200A—Set 65.] 1210 [Ch. 101.80.130] [Ch. 101.80.130] 120 [Ch. 101.80.130] [See Model 6220—Set 9.30] 8220 [Ch. 101.835] \$9-18 8230 [Ch. 101.820.32] \$57-18 8240 [Ch. 101.822.32] [See Model 716] 8260 [Ch. 101.822.2] [See Model 716] 8270 [Ch. 101.822.2] 8270A 101.822.A)
7165—Set 10.29 8270 (Ch. 101.822), 8270A (Ch. 101.822A) 57-18 9000 (Ch. 132.857) 65-13 9005, 9006 (Ch. 132.858), 72-11 9022 (Ch. 132.871) 76-17 9034 (Ch. 132.871) 76-17 9034 (Ch. 132.849) 76-17 9073, 9073A (Ch. 135.244), 90738
9005, 9006 (Ch. 132.858), 72-11 9022 (Ch. 132.871)
9073, 9073A (Ch. 135.244), 9073B
9073C (Ch. 135.243-1) (See Model 9073-Set 83-10)
0092 (CL 126 246) 101 11
9084 (Ch. 135.245) (See Model 41
9084 (Ch. 135.245) [See Model 41 —Set 101.11] 9101 (Ch. 101.809-3C) [See Model
9084 (Ch. 135,243) [See Model 41 —Set 101-11] 9101 (Ch. 101,809-3C) [See Model 7080—Set 58-20] 9102 [See Model 7080—Set 58-20]
V084 [Ch. 135,243] (See Model 4 —Set 101-11) 7080 [Ch. 101.809-3C] (See Model 7080—Set 58-20) 7082 [See Model 7080—Set 58-20] 9102 [See Model 7080—Set 58-20] 9105 [Ch. 102,857-1] (See Model
1034 (bt. 135,245) (bc. 135,245) 1038 (bt. 135,245) (bc. Model 141) 3et 101.11) (bc. 32,245) (bc. 32,245) 101 (bt. 101,800-3C) (bc. 32,245) (bc. 32,245) 102 (bc. Model 7306) (bc. 32,35) (bc. 32,35) (bc. 32,35) 103 (bc. 101,8075) (bc. 32,35) (bc. 32,35) (bc. 32,35) (bc. 32,35) 103 (bc. 101,805,15) (bc. 32,35) (bc. 32,35) (bc. 32,35) (bc. 32,35) 104 (bc. 31,35,35) (bc. 32,35) (bc. 32,35) (bc. 32,35) (bc. 32,35) 105 (bc. 31,35,35) (bc. 32,35) (bc. 33,35) (bc. 33,3
 1032 (Ct. 135.245) (See Model 41 1032 (Ct. 135.245) (See Model 41 1034 (Ct. 135.245) (See Model 41 1045 (Ct. 101.805.1) (See Model 41 105 (Ct. 102.875) (See Model 44 107 (Ct. 101.855.1) (See Model 44 107 (Ct. 101.851.1) (See Model 8107A (Ct. 101.851.1) (See Model 8107A (Ct. 101.851.2) (See Model 8107A (Ct. 101.857.2) (See Model 64-Set 113.8) 10705 (Ct. 101.857.2) (See Model 64-Set 113.8)
9022 (Ch. 132, 871) 76-17 9034 (Ch. 101, 849) 63-16 9073 (Ch. 135, 243-1) 83-10 9073 (Ch. 135, 243-1) 83-10 9073 (Ch. 135, 243-1) 83-10 9073 (Ch. 135, 243-1) 88-10 9073 (Ch. 135, 243-1) 86-10 9073 (Ch. 135, 243) 86-10 9082 (Ch. 135, 243) 16e Model 41 Sat 101-11 9101 (Ch. 101.809-3C) (See Model 41 -Sat 101-11 9103 (Ch. 103, 287) 9103 (Ch. 103, 287) 89-14 9107 (Ch. 101, 854-1) 89-00 9105 (Ch. 132, 87) 89-14 9107 (Ch. 101, 854-1) (See Model 13, 28, 75) 9107 (Ch. 101, 854-1) (See Model 13, 28, 75) 9107 (Ch. 101, 854-1) (See Model 13, 28, 75) 9107 (Ch. 101, 854, 11, 49) 9107 (Ch. 101, 854, 21) 9107 (Ch. 101, 854, 21) (See Model 13, 28, 75) 9107 (Ch. 101, 854, 21) (See Model 44, 21) 64-5et 13, 84) 9107 9107 (B (Ch. 101, 854, 21) (See Model 44, 24) 64-5et 13, 84) 9107 9108 (Ch. 101, 854, 91)
1034 104, 135, 233, 124, 107-11 1038 1031, 130 1056 Model 41 9101 (Ch. 101, 1809-3C) (See Model 47 Model 47 1080 Set 58, 20) 9102 (See Model 47 Model 47 1090 (Ch. 101, 132, 875) 89-14 89-14 9107 (Ch. 101, 132, 875) 89-14 9105 (Ch. 101, 132, 875) 89-14 8907 89-14 9107 (Ch. 101, 1859-1) (See Model 1807-85) 89-14 9107 (Ch. 101, 1859-1) (See Model 44-56) 131, 36) 91074 (Ch. 101, 1859-1) (See Model 44-56) 134, 36) 131, 36) 9108 (Ch. 101, 1359-1) (See Model 44-56) 134, 46, 56) 134, 46, 56, 113, 36) 9101 (Ch. 110, 499) (See Model 44-56) 134, 46, 56, 113, 36) 9111 (Ch. 110, 499) (See Model 44-56) 9123, 56, 77, 96, 136) 9124 924, 75, 76, 76, 76, 76, 76, 76, 76, 76, 76, 76
 Yosa (Ch. 135.245) field (Ch. 135.24
 9111 (Ch. 110,499) (See Model 9123—Set 79-16) 9112 (Ch. 110,499-1) (See Model 9124—Set 79-16) 9113 (Ch. 110,499) (See Model
 9111 (Ch. 110,499) (See Model 9123—Set 79-16) 9112 (Ch. 110,499-1) (See Model 9124—Set 79-16) 9113 (Ch. 110,499) (See Model
 9111 (Ch. 110,499) (See Model 9123—Set 79-16) 9112 (Ch. 110,499-1) (See Model 9124—Set 79-16) 9113 (Ch. 110,499) (See Model
 9111 (Ch. 110,499) (See Model 9123—Set 79-16) 9112 (Ch. 110,499-1) (See Model 9124—Set 79-16) 9113 (Ch. 110,499) (See Model
 9111 (Ch. 110,499) (See Model 9123—Set 79-16) 9112 (Ch. 110,499-1) (See Model 9124—Set 79-16) 9113 (Ch. 110,499) (See Model
 9111 (Ch. 110,299) (See Model 9123-Sei 79-16) 9112 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9113 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9114 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9115 (Ch. 478,221, 9116 (Ch. 478,221, 97-16 9116 (Ch. 101,862, 1), * 9120 (Ch. 101,862, 1), * 9121 (Ch. 101,862, 1), * 9122 (Ch. 101,862, 1), *
 9111 (Ch. 110,299) (See Model 9123-Sei 79-16) 9112 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9113 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9114 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9115 (Ch. 478,221, 9116 (Ch. 478,221, 97-16 9116 (Ch. 101,862, 1), * 9120 (Ch. 101,862, 1), * 9121 (Ch. 101,862, 1), * 9122 (Ch. 101,862, 1), *
 9111 (Ch. 110,299) (See Model 9123-Sei 79-16) 9112 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9113 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9114 (Ch. 110,499.1) (See Model 9124-Sei 79-16) 9115 (Ch. 478,221, 9116 (Ch. 478,221, 97-16 9116 (Ch. 101,862, 1), * 9120 (Ch. 101,862, 1), * 9121 (Ch. 101,862, 1), * 9122 (Ch. 101,862, 1), *
 9111 (Ch. 110,499) (See Model 9123—Set 79-16) 9112 (Ch. 110,499-1) (See Model 9124—Set 79-16) 9113 (Ch. 110,499) (See Model

SILVERTONE-Cont.
9126—Set 79-16) 9128A (Ch. 101.868)*
9129 (Ch. 110.499) (See Model 9123—Set 79-16) 9130 (Ch. 110.499-1) (See Model
9124-Set 79-16) 9131 (Ch. 478.210) 84-10 9132 (Ch. 10, 499 1) (See Medel
9124-Set 79-16) 9133, 9134 (Ch. 101.866 and Radio
Ch. 101.859)
9153 (Ch. 435.417) 67-16 9161 (Ch. 548.358) 88-10
9280 (Ch. 101.850) 51–20 9270 (Ch. 547.245) 82–11 9280 (Ch. 528.168) 94–9
Ch. 100.043 (See Model 133) Ch. 100.107 (See Model 133) Ch. 100.107-1 (See Model 149)
Ch. 100.111 (See Model 143A) Ch. 100.112 (See Model 161-16)
Ch. 100.120 [See Model 165-16] Ch. 100.201 [See Model 69] Ch. 100.202 [See Model 1066]
Ch. 100.202-1 [See Model 2195-21 or 3195] Ch. 100.208 (See Model 1176-21)
Ch. 100.208-1 (See Model 2195-21) Ch. 100.209 (See Model 2170-C)
Ch. 100.210, -1 [See Model 2130] Ch. 100.210-2 [See Model 3195] Ch. 100.210-3 [See Model 3130]
Ch. 100.400 (See Model 3177A) Ch. 101.660-1A (See Model 6100) Ch. 101.662-28 (See Model 6105)
Ch. 101.662-2D (See Model 6105) Ch. 101.662-3C (See Model 6111)
Ch. 101.662-3F [See Model 6106A] Ch. 101.662-3F [See Model 6111A] Ch. 101.666-1B [See Model 6283A]
Ch. 101.672-1A (See Model 6093) Ch. 101.672-1B (See Model 6092) Ch. 101.677B (See Model 6092)
Ch. 101.733 (See Model 8127) Ch. 101.800-1, -1A (See Model
SILVERTONE-Conf. 9127 (Ch. 100.499-2) [See Model 9128 (Ch. 101.866] * 9129 (Ch. 101.866] * 9129 (Ch. 101.869] (See Model 9123-Set 79-16) 9131 (Ch. 479.21) (See Model 9132 (Ch. 110.499-1) (See Model 9132 (Ch. 110.499-1) (See Model 9132 (Ch. 110.499-1) (See Model 9132 (Ch. 101.865 ond Ratio Ch. 101.859] 95-5 9139, 9140 (Ch. 110.499-1) (See Model 9124-Set 79-16) 9131 (Ch. 435.417) 67-16 9161 (Ch. 548.358] 88-10 9200 (Ch. 101.850] 97-5 9200 (Ch. 547.245) 82-11 9200 (Ch. 528.168] 94-9 Ch. 100.043 [See Model 133] Ch. 100.107-1 [See Model 133] Ch. 100.107-1 [See Model 143A] Ch. 100.107-1 [See Model 143A] Ch. 100.107-1 [See Model 145-16] Ch. 100.201 [See Model 145-16] Ch. 100.202 [See Model 1455-16] Ch. 100.202 [See Model 1455-16] Ch. 100.202 [See Model 1455-16] Ch. 100.203 [See Model 1475-21] Ch. 100.204 [See Model 1475-21] Ch. 100.204 [See Model 1475-21] Ch. 100.205 [See Model 1475-21] Ch. 100.206 [See Model 1475-21] Ch. 100.206 [See Model 1475-21] Ch. 100.207 [See Model 1475-21] Ch. 100.208 [See Model 1377A] Ch. 100.208 [See Model 1377A] Ch. 101.662-26 [See Model 3177A] Ch. 101.662-26 [See Model 3177A] Ch. 101.662-26 [See Model 3177A] Ch. 101.662-26 [See Model 3177A] Ch. 101.662-26 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-26 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-28 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-28 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-28 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-26 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-28 [See Model 6105] Ch. 101.662-28 [See Model 6105] Ch. 101.662-26 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-27 [See Model 6105] Ch. 101.662-27 [See Model 6200] Ch. 101.860-3 [See Model 7070] Ch. 101.860-3 [See Model 7070] Ch
Ch. 101.801, -1A (See Model 6230) Ch. 101.802, -1 (See Model 6230) 101.807, A (See Model 7021)
Ch. 101.808 (See Model 7054) Ch. 101.808-1C (See Model 8052) Ch. 101.808-1C (See Model 8052)
Ch. 101.809 (See Model 7080, Ch. 101.809)
Ch. 101.809-1A (See Model 8083) Ch. 101.809-1B (See Model 8084) Ch. 101.809-2 (See Model 7080,
Ch. 101.809-2) Ch. 101.809-3C (See Model 8101) Ch. 101.819 (See Model 7090)
Ch. 101.811 (See Model 7100) Ch. 101.813 (See Model 8050)
Ch. 101.814 (See Model 7085) Ch. 101.814-1A (See Model 7102) Ch. 101.814-2B (See Model 8102)
Ch. 101.814-38 (See Model 8102A) Ch. 101-814-5C (See Model 8086) Ch. 101-814-5C (See Model 8086)
Ch. 101.817 (See Model 7070) Ch. 101.819A (See Model 7226)
Ch. 101.820 (See Model 7210) Ch. 101.821 (See Model 8090) Ch. 101.822 (See Model 8270)
Ch. 101.822A (See Model 8270A) Ch. 101.823, -1 (See Model 7166) Ch. 101.823.4 .1A (See Model
7165) Ch. 101.825 (See Model 7115)
Ch. 101.825 (See Model 7115) Ch. 101.825-1A (See Model 7116) Ch. 101.825-1A (See Model 7116) Ch. 101.825-1B (See Model 7117) Ch. 101.825-2C (See Model 7119)
Ch. 101.825-3D [See Model 8115]
Ch. 101.825-3G [See Model 8097] Ch. 101.825-4 (See Model 8097A) Ch. 101.825 (See Model 8097A)
Ch. 101.829-1 (See Model 8133) Ch. 101.831 (See Model 8128)
Ch. 101.831A (See Model 8127) Ch. 101.831-1 (See Model 8124) Ch. 101.833 (See Model 8105)
Ch. 101.834 (See Model 8072) Ch. 101.835 (See Model 8230) Ch. 101.839 (See Model 8051)
Ch. 101.846 (See Model 8133) Ch. 101.849 (See Model 9054)
Ch. 101.851 (See Model 9260) Ch. 101.851 (See Model 8107A) Ch. 101.851-1 (See Model 8109)
Ch. 101.852 (See Model 8080) Ch. 101.854 (See Model 8132) Ch. 101.859 (See Model 9133)
Ch. 101.859-1 (See Model 67) Ch. 101.859-2 (See Model 64) Ch. 101.869-2 (See Model 64)
Ch. 101.860-3 (See Model 3058) Ch. 101.861, -1 (See Model 2060)
Ch. 101.825-26 [See Model 8115] Ch. 101.825-36 [See Model 8115] Ch. 101.825-36 [See Model 8115] Ch. 101.825-36 [See Model 8097] Ch. 101.825-36 [See Model 8097] Ch. 101.825-36 [See Model 8097] Ch. 101.827 [See Model 8103] Ch. 101.827 [See Model 8103] Ch. 101.831 [See Model 8103] Ch. 101.831 [See Model 8123] Ch. 101.833 [See Model 8123] Ch. 101.833 [See Model 8123] Ch. 101.833 [See Model 8123] Ch. 101.833 [See Model 8123] Ch. 101.834 [See Model 8133] Ch. 101.835 [See Model 8133] Ch. 101.835 [See Model 8133] Ch. 101.835 [See Model 8133] Ch. 101.845 [See Model 8133] Ch. 101.845 [See Model 8133] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 8132] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 8132] Ch. 101.857 [See Model 8132] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 8133] Ch. 101.857 [See Model 913] Ch. 101.865 [See Model 913] Ch. 101.865 [See Model 913] Ch. 101.865 [See Model 913] Ch. 101.865 [See Model 9124] Ch. 101.865 [See Model 913] Ch. 102.635 [See Model 913] Ch. 103.635 [See Model 913] Ch. 104.635 [See Model 913] Ch. 104.635 [See Model 913] Ch. 105.635 [See Model 913] Ch. 105.635 [See Model 913] Ch. 106.635 [See Model 913] Ch. 106.645 [See M
Ch. 101.866 (See Model 9133) Ch. 101.867 (See Model 9121) Ch. 101.868 (See Model 91224)
Ch. 109.626 (See Model 7152) Ch. 109.627 (See Model 7153) Ch. 109.627 (See Model 7153)
Ch. 109.632 (See Model 8148) Ch. 109.633 (See Model 8149)
Ch. 109.634 (See Model 8150) Ch. 109.635 (See Model 8153) Ch. 109.635-1 (See Model 81534)
Ch. 109.636 (See Model 8160) Ch. 109.636A (See Model 8160A) Ch. 109.636A (See Model 8160A)
Ch. 110.451 (See Model 6051) Ch. 110.452 (See Model 6052)
Ch. 110.452 [See Model 6052] Ch. 110.454 [See Model 6072] Ch. 110.466 [See Model 7038] Ch. 110.466 [See Model 7038] Ch. 110.473 [See Model 7103] Ch. 110.479 [See Model 9123] Ch. 110.499 [See Model 9124] Ch. 110.499-1 [See Model 9126]
Ch. 110.473 [See Model 8103] Ch. 110.499 [See Model 9123] Ch. 110.499-1 [See Model 9124]
Ch. 110.499-1 (See Model 9124) Ch. 110.499-2 (See Model 9126)

• 91 • 91 • 91

.91

• 91 91 • 91

SILVERTONE-Cont. Ch. 110.700-1 (See Model 116) Ch. 110.700-10 (See Model 116) Ch. 110.700-40 (See Model 177-19 Ch. 110.700-100 (See Model 1177-19 191 17) . 110.700-120 (See Model 1181-Ch. 110.700-120 [See Model 1145-20] Ch. 110.700-140 (See Model 1145-20) Ch. 110.700-140 (See Model 1145-20) Ch. 110.700-150 (See Model 1183-21) Ch. 110.702-10, -50 (See Model 1171-17) 171-171 171-171 180-17-1 [See Model 2100A] Ch. 110.817-3 [See Model 2150A] Ch. 110.820-3 [See Model 2150A] Ch. 132.011-1 [See Model 1053] Ch. 132.011-1 [See Model 1054] Ch. 132.011-1 [See Model 2014] Ch. 132.012-1 [See Model 2014] Ch. 132.021-3 [See Model 2014] Ch. 132.021-3 [See Model 2014] Ch. 132.024-3 [See Model 2015A] Ch. 132.024-3 [See Model 2105A] Ch. 132.024-3 [See Model 2022] Ch. 132.024-3 [See Model 2022] Ch. 132.024-3 [See Model 2022] Ch. 132.035 [See Model 3175] Ch. 132.035 [See Model 3175] Ch. 132.035 [See Model 3052] Ch. 132.053 [See Model 3025] Ch. 132.053 [See Model 3025] Ch. 132.054 [See Model 3025] Ch. 132.054 [See Model 3025] Ch. 132.055 [See Model 3025] Ch. 132.057 [See Model 6003] Ch. 132.057 [See Model 6003] Ch. 132.057 [See Model 6005] Ch. 132.047 [See Model 6005] Ch. 132.047 [See Model 6005] Ch. 132.047 [See Model 6005] Ch. 132.048 [See Model 6005] Ch. 132.048 [See Model 6005] Ch. 132.047 [See Model 8070] Ch. 132.047 [See Model 8070] Ch. 132.047 [See Model 8070] Ch. 132.047 [See

SILVERTONE-Cont. SILVERI GRE-LONT. Ch. 528.196 (See Model 1032) Ch. 528.196 (See Model 1032) Ch. 528.196 (See Model 1032) Ch. 528.210, -1 (See Model 1038) Ch. 528.210, -1 (See Model 1038) Ch. 528.203 (See Model 2028) Ch. 528.203 (See Model 2028) Ch. 528.233 (See Model 2028) Ch. 528.235 (See Model 2028) Ch. 528.239 (See Model 2024) Ch. 528.239 (See Model 2014) Ch. 528.249, -1, -2 (See Model 3170) Ch. 528.249, -1, (See Model 3170) Ch. 528.249 (See Model 304) Ch. 528.249 (See Model 304) Ch. 528.249 (See Model 304) Ch. 528.249 (See Model 3170) Ch. 528.249 (See Model 3170) Ch. 528.245 (See Model 3170) Ch. 528.245 (See Model 3170) Ch. 528.246 (See Model 4115) Ch. 528.246 (See Model 4115) Ch. 528.249, -1, -2 (See Model 3109) Ch. 528.240 (See Model 4115) Ch. 528.290, -1 (See Model 4115) Ch. 528.290, -1 (See Model 4107) Ch. 528.201, -1 (See Model 151-16) Ch. 528.602, -1, -2, -3 (See Model 4107) Ch. 528.602, -1, -2, -3 (See Model 4106) Ch. 528.602, -1, -2, -3 (See Model 4107) Ch. 528 Model 175-10) Ch. 549.102, -2 (See Model 169 16) Ch. 725.101-1 (See Model 2007) Ch. 737.100 (See Model 2003) Ch. 737.120 (See Model 3007) Ch. 737.120 (See Model 3004) Ch. 737.140 (See Model 4200) SIMPLON 5KY KNIGHT (See Air Knight) SKYRIDER (See Hallicrafters) SKYROVER NS-RD-250 (9022-N), NS-RD-251 (9022-H) 6-31 NS-RD295 (Ch. 5A7) 21-30 SKY WEIGHT 81B 20–30 82 13–13 50NOGRAPH 50NORA SONORA RBU-176 5-31 RB-207 (See Model RBU-176—Set) 5-30 RDU-1206 3-29 RET-210, RGMF-230 24-24 RGM-212, RGMF-230 27-26 RKRU-215 (Ch, RKRU) 9-31 RMR-220, RMR-245 (See Model RMR-219 8-23 RWR-220, RMR-245 19-28 RWR-220, RMR-245 3-24 RX-233 19-29 WAU-238 23-24 RX-223 19-27 WAU-239 32-23 WCU-244 36-22 WDU-233 25-27 WDU-249 37-20 WEU-262 33-28 8-23 23-24 19-29 27-27 32-23 36-22 25-27 37-20 33-28 24-25 36-23 34-20 37-21 WBU:255 37-20 WEU:262 33-28 WGFU:341, WGFU:242 24-25 WU:353 36-23 WI:RU:256A 37-21 WI:RU:256A 37-21 WI:RU:256A 37-21 WI:RU:256A 37-21 WI:RU:256A 37-21 WI:RU:256A 37-21 WI:RU:256A 566 WI:RU:256A 37-21 WI:RU:256A 566 WI:RU:256A 37-21 WI:RU:256A 566 WI:RU:256A 37-21 YI:RU:256A 566 WI:RU:256A 567 WI:RU:256A 566 WI:RU:256A 566 WI:RU:256A 566 WI:RU:256A 567 WI:RU:256A 568 WI:RU:256A <td

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79-16

SONORA-STROMBERG-CARLSON

SONORA	-STROMBERG-CARLSON
SPARTON-Cont.	STEWART-WARNER-Cont.
Ch. 2655172, A, B (See Model	
52071	•21T-9340A, B, D, R, RB, S, T 258-12 •24C-9360A, AB (Series A, AB)
Ch. 27D173 (See Model 5325A) Ch. 27D213 (See Model 5342A) Ch. 27D213-A (See Model 5382B)	• 24C-9360A, AB (Series A, AB) 254-11 • 24C-9370A, AB (Series A, AB) 254-11
Ch. 27D213-A (See Model 5382B) Ch. 27D273 (See Model 26542)	WZ4C-YJ/UA, AD (Jerres A, AD)
Ch. 27D273 (See Model 26542) Ch. 29U213 (Se Model 26542) Ch. 29U213 (See Model 24542) Ch. 29U273 (See Model 24542)	• 27C-9212A (Series A, B, C) 211-15
Ch. 417 (See Model 4AW17)	
Ch. 417 [See Model 4AW17] Ch. 417A [See Model 5AW17A] Ch. 666A [See Model 5-65A]	• 27C-9350A, AB (Series A, AB) 254-11
SPIEGEL (See Aircastle)	ELTAL LC-J. DODARY ELTEL LCode
	9024-C)
STARK 410 40-22	(Code 9018-F), 51T146 (Code 9018-B)
410	9018.HJ, 511176 (Code 9012.A), 61726 (Code 9022.A), 11-56 9012.2.B) 1 6 62716 (Code 9023.C), 62716 600-08 11-22 9001.C, 221 9001.C, 10-20 9002.R, 9
1020 89—5	61116 (Code 9022-A), 61126 (Code 9022-8)
STARRETT	62T16 (Code 9023-C), 62T16 (Code
Gotham	62TC36 (Code 9023-F). 2-21
John Hancock	72CR16, 72CR26 18–28 9000-8 11–22
Robert E. Lee	9001-C, D, E, F
Actional rule 92-7 Robert E. (Cr., 1/S) 92-7 Al72C-1(Cr., 1/S) (See Ch., 1/S)	9002-A, 9002-B, 9002-P, 9002-R 38-24
A17TG-1 (Ch. 17S1) (See Ch. 17S1	9005-A, B 13-31 9007-A F G 10-30
•A20C-2 (Ch. 1851) (See Ch. 1851	•9100A, 9100B, 9100C, 9100D,
Set 165-2A)	9100E, 9100F, 9100G, 9100H 75–15
Set 165-2A) • A20CD-1 (Ch. 1851) (See Ch. 1851 Set 165-2A) • A20TG (Ch. 1851) (See Ch. 1851 Set 165-2A) Set 165-2A)	75-15 •9103-B, -C, 9104-A, -B, -C. 105-10 •9106A, B. 118-10 •9108A, B, 9109A, B. 118-10 •9108A, B, 9109A, B. 118-10
 A20TG (Ch. 1851) (See Ch. 1851 —Set 165-2A) 	•9108A, B, 9109A, B 118-10
• 17BM1 (Ch. 12S1)	9113A. 118-10 9113A. 118-10 9120-A, -B, -C, -D, -E, -F, 137-11 9121-A, -18, 52, -7, 138-9 9126-A, -B (see PCB 51-Set 185-1 9126-A, -B (see PCB 51-Set 185-1
• 27BM1 (Ch. 1251)	•9121-A, 9121-B, 9122-A. 138-9
• 29AM1 (Ch. 14S1)	and Model 9120-A-Set 137-11)
• 37BB1 (Ch. 12S1)	• 9127-A
	9150-B, 9150-D, 9150-DZ. 140-12
Ch. 14S1 (See Model 29AM1) Ch. 15S1 (See Model 20BM1)	9152-A, -B, -C
Ch. 1751	9153-A 108-12
ch. 1851	9160 AU, BU, CU, DU, EU. 171-10
STEELMAN	9161A, B, C
AF1100	•9126-A, B (See PCB 51—Set 185-1 nof Model 9120-A—Set 187-11) •9127-A
152 257 -15	9165A, -B
3AR3	9170-B, -C, -D
3A2	9180B, H
3A5	9182-C, -H, -J
3D2	9187-B, -E, -J
3D5, 3D6	168-13) 9165A, -8, 19175-8, -C, -0 230-11 1975-8, BU, G, CU, H, HU. 249-18 91808, H 19181A, C, D, F, F 243-11 19181A, C, D, F, F 243-11 19181-8, C, D, F, F 255-15 187.6, E, -J 257-16 9200-A, -C, -D, -FA, -G. 132-13 9200-A, -G. 18 (Hru Saries 'B'') [See Model 9202-C (Series 'B'')—Set 158-12]
3RP1	158-12]
BE-20, BE-21, BE-22, 247-11 152, 257-15 3A2 3A32 243-10 3A2 3A32 244-11 3D2 3A4 250-20 3A5 211-14 3D37 (See Model 3D5-Ser 245-8) 3D4 211-14 2037 352 245-8 352 245-11 102 164-14 107 178-12 151M 223-11 2303 3127 182-13 323 323 331 2351 <	158-12] •9202-A, -B (Thru Series ''H'') •772-9 •0202-A, B (Series ''H'') [Series PCB
102	• 9202-A, -B (Thru Series 'H') 172-9 • 9202-A, -B (Series 'H') [See PCB 60—Set 194-1 and Model 9202- A (Series 'H')—Set 172-9] • 9202-C, -DA, -DB, -DD, -E, -F (Thru Series 'H')—Set 172-9] • 9202-C, -DA, -DB, -DD, -DDA, -E, -F (Thru Series 'H')—
151M	A (Series "H")-Set 172-9]
200 23–25 215	•9202-C, -DA, -DB, -DD, -E, -F (Thru Series "B" 158-12
303 19 -31	•9202-C, -DA, -DB, -DD, -DDA, -E,
330	•9202-C, -DA, -DB, -DD, -DDA, -E,
350, 351	-F (Series "M") [See PCB 60-
357	Set 194-1 and Model 9202-A (Series ''H'')—Set 172-9] 9202-FA (Thru Series ''B'') [See Model 9202-C (Series ''B'')—Set
487	Model 9202-C (Series "B") See
517	158-121 • 9202-FA (Thru Series ''H'') 1729
597	• 9202-FA (Series 'M'') [See PCB 60
602	138-121 9202-FA (Thru Series "H") 1729 9202-FA (Series "M") [See PCB 60 Set 194-1 and Model 9202-A (Series "H")Set 172-9 9203-A
5000	● 9203-A
5101	• 9209-A, AW, B, C, D (Series A, B,
	•9204.A
STEWART-WARNER AVC1 (Code 9054B), AVC2 (Code	
 AVC1 (Code 9054B), AVC2 (Code 9054C), AVT1 (Code 9054-A) 64-12 64-13 	ST, GEORGE (See Recorder Listing)
	STRATFORD
ASITI (Code 9020-A), A-51T2 [Code 9020-B], ASIT3 (Code 9020-C), ASIT4 (Code 9020-D) 17-32	•916, 917, 920, 921, 1016, 1017, 1020, 1021 (Ch. 6353, C). 219 –11
AA:CR1 (Code 2024 C) AA1CR2	
17-32 A6iCR1 (Code 9034-C), A61CR2 (Code 9034-D), A61CR3 (Code 9034-E), A61CR4 (Code 9034-F)	STRATOVOX 579-58A
A61P1 (Code 9036-A), A61P2 (Code 9036-B), A61P3 (Code 9036-C)	STROMBERG-CARLSON
	AM-48, AM-49
A/211 (Lode 9026-A), A7212 (Code 9026-B), A7213 (Code 9026-C),	AP-50
A72T1 (Code 9026-A), A72T2 (Code 9026-B), A72T3 (Code 9026-C), A72T4 (Code 9026D), 32-24 A92CR3, A92CR3S (Code 9028-C),	AR-37A
AYZCRO, AYZCROS (Code YUZO-F)	AR-425
29-26 B51T1, B51T2, B51T3 (Code 9044A, B, C) 58-22	AU-29
B, C) 58-22 B61T1, B61T2 (Code 9046A, B)	AU-33
B72CR1 (Code 9038A) 47-22	AU-35
59-19 B72CR1 (Code 9038A). 47-22 B92CR1 B92CR2, B92CR3, B92CR4, B92CR8, B92CR9, B92CR0 (Codes 9043A, B, C D, K, L, M) 65-14 C51T1 (Code 9054-A), C51T2 (Code 9054B) 9054-A), C51T2 (Code 9054B) 9054-A), C51T2 (Code	AU-42 137-12
892CR8, 892CR9, 892CR10 (Codes 9043A, B. C. D. K. L. M) 63-14	AV-38, AV-39
C51T1 (Code 9054-A), C51T2 (Code	C-1
9054-B)	SR-401
•1-711M (Code 9031-AM)95A-12 •1-712 (Code 9031-B)95A-12	●TC-10 (Also see PCB 1—Set 103-
	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
@21C-9210C (Series "A, B, C, D,	•TC-125
A 21C 0211D E E C (Serier A B	TV-12 (See Model TV-125 Set
C)	68-16) TV-12 PGM (For TV Ch. only see
C) 200-9 • 21C-9300E, F, G, K, KB, L, LB, M, MB, P (Series A thru T). 223-12 • 21C-9326F, G • 258-12 • 21C-9326F, K, KB, L, LB, M, MB	Model TV-125-Set 68-16)
MB, P (Series A thru T). 223-12 •21C-9325F, G	00-107 FORM (For TV Ch. only see Model TV-125—Set 68-16) FV-12M5M (For TV Ch. only see Model TV-125—Set 68-16) FV-12LM (See Model TV-125—Set
E'') 192-8 •211-92118 (Series A, 8). 200-9 •211-9211C (Series A, 8, C). 200-9 •211-9200A, AA, 8, D, H, HA, R, RB, S, T (Series A thru T) 223-12	• TV-123 (Ch. 12) • 68-16 • 16 Series 135-12 • 17 Series 135-12 • 21TM, TQ 258-13 • 22TM, TQ 258-13
•211-9300A, AA, B, D, H, HA, R, RB, S, T (Series A thru T) 223-12	e22TM, TQ

5ONORA-Cont.
101
102 53-23
171
172 (See Model 171-Set 109-13)
172 (See Model 171-Set 109-13) 302, 303 97A-13
305 174–11
306
314, 315 253-13
323, 324, 325174-11
327A, 328A
332 174 –11 335, 336 250 –19
335, 336
348A
349
350, 351
352
356
366A
379
389. 390
401 47-21
401
19-28)
402F (See Model WLRU-219A-Set
37-21)
413, 414, 415, 416 (For TV Ch. Only See Model 421-Set 221-
10) Unly See Model 421-Set 221-
421, 422, 423, 424, 425, 426, 428,
429
441, 442
458, 459
464, 465, 466
467
470A
477, 478
SOUND, INC.
"Intersound"
MB6P3, MB6P6, MB6P30, MB6R4
35-21
MB7E3
MB7E8
5R2

SPARKS-WITHING (See Sparton) 12A203 [Ch. 3J0214] 233-14 12A210 [Ch. 3J0214] 255-14 100, 101 [Ch. 5A7] 38-23 102, 103, 104 [See Model 100 55-17 5et [Ch. 2] 57-19 130, 132, 135, 139 [Ch. 5A10] 57-19 130, 132, 135, 139 [Ch. 5A10] 130, 132, 135, 139 [Ch. 5A10] 141 [See Model 121-Set 57-19] 141 [See Model 121-Set 57-19] 141 [See Model 121-Set 57-19] 150, 151, 152, 155 [Ch. 4E10] 150, 151, 152, 155 [Ch. 4E10] 91-12 230 (Ch. 5A10, A) 210-10 324 (Ch. 5A30, A) 210-10 325 (Ch. 5A10, A) 210-10 326 (Ch. 5A30, A) 210-10 327 (Ch. 5830, C) < 1030, 1030k (Ch. 846). 37-22 1031, A (See Model 1030-Set 37. 22) 1035, 1035, 1036, 1036A, 1037, 1037, 1037, 1039, 1040, 1041 (Ch. 918). 52-19 1040, AXX, 1041, XX (Ch. 9W10) 52-19 1040, XX, 1041, XX (Ch. 9W10) 1031, 1032 (Ch. 68). 1032 (Ch. 68). 1033 (Ch. 613). 1031, 1032 (Ch. 68). 1031, 1032 (Ch. 68). 1031, 1032 (Ch. 68). 1031, 1032 (Ch. 613). 1031, 1032 (Ch. 613). 1031, 104, 104 (Ch. 613). 1031, 104 (Ch. 613). 1031, 104 (Ch. 613). 1051, 1052 (Ch. 613). 1051, 105 141XX_Set 126-121 1300, 1301 (Ch. 613)...197-12 649017 (Ch. 24179C, 3179C, 918A) 64916, 4917, 4918 (Ch. 241110, 31110, 6510)....164-9 64920, 4921, 4922 (Ch. 247M10) 64920, 4921, 4922 (Ch. 247M10) 164-9

NO

 solas, solas (Ch. 28D190, 25RD190) solas, solas (Ch. 2RD190, 25RD190) solas, solas (Ch. 2RD190, 25RD190) (38D170 and Radio Ch. 28D180, 26D170 and Radio Ch. 28D180, (600 Ch. 28E 128-13], for Radio Ch. 28E 128-13], for Radio Ch. 28E 128-13], for Radio Ch. 28E 128-13], (510, 5102, 5103 (Ch. 26S5170, P) (See PCB 22—Set 138-1 and Model 5025—Set 128-13] (512, 5153, 5154 (Ch. 26S5170, P) (See PCB 22—Set 138-1 and Model 5025—Set 128-13] (5155, 5153, 5154 (Ch. 26S5170, P) (See PCB 22—Set 138-1 and Model 5025—Set 128-13] (5155, 5155, 5157 (Ch. 26SD170X, XP) (See PCB 22—Set 138-1 and Model 5025—Set 128-13] (5155, 5155, 5164 (Ch. 26SD170X, XP) (See PCB 22—Set 138-1 and Model 5025—Set 128-13] (5155, 5166X (Ch. 26SD170), S104, 5166X (Ch. 26SD171) (5171 (Ch. 25SD20), 25D- (5171) (Ch. 25SD20), 25D- (5171) (Sh. 25SD20), • 52964. 52974 (Ch. 2cC020] • 52964. 52974 (Ch. 2cC020] • 176-11 • 5298 (Ch. 2sC0202) 178-11 • 5299 (Ch. 2sC0202) [See Model • 5298 (Ch. 2sC0202) [See Model • 5298 (Ch. 2sC0202) [See Model • 5304 (Ch. 25173-0] ... 201-10 • 5324 (Ch. 25173-0] ... 222-14 • 53264 (Ch. 2501731, 222-14 • 53264 (Ch. 2501731, 222-14 • 53264 (Ch. 2501731, 222-14 • 53243 (Ch. 2501731, 222-14 • 53244 (Ch. 2501731, 210-11 • 5342 (Ch. 270173], 210-11 • 5342 (Ch. 270173], 222-14 • 5363 (Ch. 270173], 222-14

SPARTON-Cont.
S380, 5381 (Ch. 215213), 201-10
S382A (Ch. 250213) (See PCB 104 —Set 210-11)
S383A (Ch. 270213)......210-11
S383B (Ch. 270213).....210-11
S384 (Ch. 250213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S384 (Ch. 250213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S384 (Ch. 250213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S386 (Ch. 270213).....210-11
S386 (Ch. 270213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S386 (Ch. 270213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S387 (Ch. 220213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S387 (Ch. 220213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S387 (Ch. 220213) (See PCB 104—Set 250-1 and Model 5342A—Set 210-11)
S387 (Ch. 270213A and Radio Ch. 387(Ch. 220213) (See Model 141:X—Set 126-12)
N352A (Ch. 270213A and Radio Ch. 387(Ch. 270213A and Radi

Ch. 26SD171 (See Model 5165X)

Ch. 265D1/1 [See Model 5165X] Ch. 265D172C (See Model 5267) Ch. 265D172C (See Model 5220) Ch. 265S160, 8 (See Model 5276) Ch. 265S160L (See Model 5076) Ch. 265S170D, P (See Model 5101) Ch. 265S170D, P (See Model 5140)

 •21:0-20:0
 No. 5: 45: 75 min
 mb/21
 mb/21

 •21:0-21:0
 Scriet
 A. 8: 72
 68:10
 68:10

 •21:1-92:16
 Scriet
 A. 8: 72
 74:10
 174:12

 •21:1-92:116
 Scriet
 A. 8: 72
 174:12
 174:12

 •21:1-92:116
 Scriet
 A. 8: 72
 175:12
 175:12

 •21:1-92:116
 Scriet
 A. 8: 72
 175:12
 175:12

 •21:1-92:10:0A: A. 4: 8: 9: 0H: HA, R.
 •21:17:14
 175:12
 •21:14:10

 •21:1-92:10:0A: A. 4: 9: 0H: HA, R.
 •21:14:10
 •21:14:10
 •21:14:10

TE: PCB Denotes Production Change Bulletin.	Production Change Bulletin Nos. 1	Through 63 Are All Contained in Set No	. A-200. • De
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STROMBERG-CARLSON-	TELE-KING
STROMBERG-CARLSON-Cont.	SYLVANIA-Cont.
24 Series 138-11 32 11-23 11-23 9116 Series 135-12 9117 Series (See Model 119CDM Series (See Model 119CDM	• 22M (Ch. 1-387) (See Model 2221M —Set 137-13) 22M-1, -2 (Ch. 1-387-1) (Also see PCB 41—Set 174-1),154-12 22M-11 (Ch. 1-507-1),174-13 • 23B, B-1, M, M-1 (Ch. 1-387-1) • 24 (Ch. 1-507-1),174-13
•117 Series (See Model 119CDM- Set 130-14)	PCB 41-Set 174-1] 154-12 • 22M-11 (Ch. 1-507-1] 174-13
Set 130-14) 119C (See PCB 43—Set 177-1 and Model 119CDM—Set 130-14)	(AISO SEE PLD 41-Jer 174-1)
 1)9C (See PCB 43—Set 177-1 and Model 1)9CDM,—Set 130-14 1)9CDM, 1)9CM = 130-14 1)99KA, D, G, I, M, R. 130-14 1)99KA, D, G, I, M, R. 130-14 30/17PM, 31/7TM = 146-10 321CD2M, 321CD20, 321CF, 321- C2M = 105-14 524CDM, 324CSM (Series 324) 172-10 417C5-M, 417C5-0, 417C5-Dec. 	23B-11 (Ch. 1-507-1) 154-12 23M-11 (Ch. 1-507-1) 174-13 23M-11 (Ch. 1-507-1) 174-13 24M (Ch. 1-462-1) 154-12
•317 RPM, 317TM	●24M (Ch. 1-462-1)
C2M 165-14 • 324CDM, 324C5M (Series 324)	24M (Ch. 1-402-1)
•417C5-M, 417C5-O, 417C5-Dec., 417TX (Series 417)178-15	Set 174-1 and Model 24M-1-Set 154-12) • 25M 25M-1 (Ch. 1-387-1 and Pa-
• #21CDM, CM, TX (Also see PCB 47 -Set 181-1)	dio Ch. 1-603-1) (For TV Ch. see PCB 41—Set 174-1 and Model
•421 Series (Revised)198-14 •521CDM, CM, CO, C5D224-14	134-12) •25M, 25M-1 (Ch. 1-387-1 and Ra- dio Ch. 1-603-1) (For TV Ch. see PCB 41-Set 174-1 and Model 22M-1-Set 154-12, for Radio Ch. see Model 178B-Set 192-9) •71M (Ch. 1-441) (See Model 7110/81)
417TX (Series 417)178–15 421CDM, CM, TX (Alio see PCB 47 —Set 181.1)170–13 421 Series (Revised)198–14 521CDM, CM, CO, C5D224–14 521CSG, 521CS1, 521CSM, 521CSD, 521CSR (See Model 521CDM— Set 224–14) 521TM, TO	•71M (Ch. 1-441) (See Model 7110XB) •71M-1 (Ch. 1-502-1) (Also see PCB
Sei 224-14) 5211M, TO 224-14 631ACDM, ACDO, ACM, ACO, ACSF, ACSI, ACGM, ACSO, ACSF, ATM, ATO 2245-13 6321CDM, CDO, CM, CO, CSF, CSI, CSM, CSO, CSR, TM, TO 235-12 6322CDM, CDO, CM, ROM, RPO 6322CDM, CDO, CM, RPM, RPO 6422CDM, CDO, CM, RPM, RPM, RPO 6422CDM, CDO, CM, RPM, RPM, RPM, RPO 6422CDM, CDO, CM, RPM, RPM, RPM, RPM, RPM, RPM, RPM, RP	•71M-1 (Ch. 1-502-1) (Also see PCB 42-Set 176-1) ••••••••••••••••••••••••••••••••••••
AC5E, AC51, AC5M, AC5O, AC5R, ATM, ATO	
622(CDM, CDO, CM, CO, CSE, CSI, C5M, C5O, C5R, TM, TO.235-12 6422(CDM, CDO, CM, CO, CSE, CSI	 728-1 (Ch. 1-502-1) (Also see PCB 42—Set 176-1)
C5M, C5O, C5R, TM, TO. 236-13 •624CDM, CDO, CM, RPM, RPO	
•623CDM, CDO, CM, RPM, RPO, 240-9	•72M (Ch. 1-366) (See PCB 55-Set 189-1 and Model 7110X-Set
1020 [See Model 1220 Series-Ser	124-10) •72M-1 (Ch. 1-502-1) (Also see PCB 42Set 176-1)
1100-H, 1100-HI 20-31 1101-HB, 1101-HI (Ch. 112002),	/38-5)
1101-HM, 1101-HW, 1101-HY Ch. 112001]	•72M-11 (Ch. 1-502-3) (See PCB 42 —Set 176-1 and Model 71M-1— Set 163-12)
1101-HM, -HW, -HY (Ch. 112001) 2—9 1101-HPW 41-23	 73B (Ch. 1-366) (See PCB 55—Set 189-1 and Model 7110X—Set
1101-HPW 41-23 1105 (Series 10-11) 18-29 1110-HW, 1110-PTW (Series 10) 18-30 18-30	124-101
1120 (See Model 1220 Series-Set	•73B-5 (Ch. 1-437-3) (See PCB 41
1121-HW, LW, M1-0, M2-W, M2-Y, PFM, PFW, PGM, PGW, PLM, PLW, PSM (Series 10-11-12)	•73B-11 (Ch. 1-502-3) (See PCB 42 Set 176-1 and Model 71M-1- Set 163-12)
PLW, PSM (Series 10-11-12) 10-31	•73M (Ch. 1-366) (See PCB 55-Set 189-1 and Model 7110X-Set 124-10)
10-31 1135.PFM, 1135.PLM, 1135.PLM, (Series 10-11) 23-26 1200 57-20 1202 (Series 10) 55-21 1204 (Cb. 112021) 34-22	•73M-1, 73M-2 (Ch. 1-502-2) (Also see PCB 42—Set 176-1) .163-12
1202 (Series 10) 55-21 1204 (Ch. 112021) 34-22	124-10) 73M-1, 73M-2 (Ch. 1-502-2) (Also see PCB 42—Set 176-1), 163-12 73M-3, -5, -6 (Ch. 1-437-3) (See PCB 41—Set 174-1 and Model 7140MA—Set 131-15) 73M-11 (Ch. 1.502, 2) (See PCB 42)
1200 57-20 1202 (Series 10) 55-21 1204 (Ch. 112021) 34-22 1210M2-M, 1210M2-W, 1210M2-Y, 1210PGM, 1210PLM, 1210PGW (Series 10,11) 37-23	7140MA—Set 131-15) •73M-11 (Ch. 1-502-3) (See PCB 42 —Set 176-1 and Model 71M-1- Set 163-12)
1220 Series 50–19 1235 Series 49–23	Set 163-12) •748 (Ch. 1-356) (See PCB 55—Set 189-1 and Model 6140M—Set
	120-10)
1407PFM, 1407 PLM 58-23 1409M2-M, 1409M2-Y, 1409M2-W, 1409M3-A, 1409M3-M, 1409PG- M, 1409PG-W 62-10 1500 132-15	•748-1 (Ch. 1-437-1) (See PCB 41- Set 174-1 and Model 7140MA- Set 131-15)
1500 132–15 1507 133–13 1608 150–12	Set 174-1 and Model /140MA- Set 131-15} •74B-2 (Ch. 1-437-2) (See PCB 41- Set 174-1 and Model 7140MA- Set 131-15)
STUDFBAKER	 Set 131-15) 74M (Ch. 1-356) (See PCB 55—Set 189-1 and Model 6140 M—Set
AC2111 (\$5127)	
AC2111 (55127) 166–15 AC2113 (55123) 172–11 AC-2300 (5-5327) 229–14 AC-2301 (5-5323) 213–8 S-4624, S-4625 21–32 S-4226 S-423 19–32	• 74M-1 (Ch. 1-437-1) (See PCB 41— Set 174-1 ond Model 7140MA— Set 131-15) 74M-2 (Ch. 1-437-2) (See PCB 41—
S-4624, S-4625 21-32 S-4626, S-4627 19-32	• 74M-2 (Ch. 1-437-2) (See PCB 41
SUPREME (Lipan) 711 68–17 7125 63–17	
733 60-19	 75B, M, M-1 (Ch. 1-437-1 and Ra- dio Ch. 1-603-1) (For TV Ch. see Model 5150M—Set 131, for Ra-
738LP 64–13 750 55–22	dio Ch. see Model 1788-Set
SUTCO (Sutton) 21-A Tel, UHF Conv	192-7) 1058U (Ch. 1-504-1)
21-A Tel, UHF Conv	●105MU (Ch. 1-504-2, -4) .212-8 ●105-14 Series (Ch. 1-514-1, -3)
SWANK 5 Tube Radio-phono (DU101) 5-21 ER61	234–13
ER61 17-33 SYLVANIA	(Also See PCE 100–Set 245-1) (Also See PCE 100–Set 245-1) .234–13 1208 (Ch. 1-510-1) 212–8 1208U (Ch. 1-510-2, -4) 212–8 1208U (Ch. 1-510-2, -4) 212–8
C33M Tel. UHF Conv 199–13 SH758 (See Hudson Model 236486 —Set 214-4)	120B (Ch. 1-510-1)
SUZED (See Undeen Medel 226476	•120MU (Ch. 1-310-2, -4) .212-0
	• 120-20 Series (Ch. 1-520-1, -3) (Also See PCB 100—Set 245-1)
-Set 103-20 and PCB 49-Set	(Also See PCB 100-Set 245-1) 234-13
103-1)	(Also See PCB 100—Ser 245-1) .234-13 .246 (Ch. 1-510-1) .212—8 .1268 (Ch. 1-510-2, .4) .212—8 .1268 (Ch. 1-510-2, .4) .212—8 .1264 (Ch. 1-510-1) .212—8 .1264 (Ch. 1-510-1) .212—8 .1264 (Ch. 1-510-1) .212—8 .1264 (Ch. 1-510-2, .4) .212 (Ch. 1-
1-090 (Ch. 1-168) (Also see PCB 49 −Set 183-1)	•126L (Ch. 1-510-1)
Set 182-1)	•126MU (Ch. 1-510-2, -4) .212-8 •150A, L (Ch. 1-437-3) (Codes CO6
-1-120 (CII. 1-100) (AISO SEE FC0 2	 120m0 (ch. 1-310-2, -4) .212-6 150A, L (ch. 1-437-3) (codes CO6 and up)
Set 103-20 and PCB 49Set 183-1)	• 172K (Ch. 1-508-1, -3) {Also see PCB 70-Set 210-1)
	1/22k (Ch. 1.508-1, -3) (Also see PCB 70Set 210-1) 1929 1/22k (Ch. 1.508-2) (Also see PCB 70Set 210-1) 1929 1/22M (Ch. 1.508-1, -3) (Also see PCB 70Set 210-1) 1929
92-81	172MU [Ch. 1-508-2] [Also see PCB]
•1-197-1 (Ch. 1-186) (Also see PCB 49—Set 183-1) 113—9 1-210 (Ch. 1-139) (See PCB 48— Set 182-1 and Model 1-075—Set	70—Set 210-1) 192 —9 •175B (Ch. 1-508-1, -3) (Also see PCB 70—Set 210-1) 192 —9
	PCB 70—Set 210-1) 192—9 •175BU (Ch. 1-508-2) (Also see PCB 70—Set 210-1) 192
 I-245, 1-246 (Ch. 1-139) [See PCB 48—Set 182-1 and Model 1-075 —Set 92-8] 	• 1758U (Ch. 1.508-2) (Also see PCB 70—Set 210-1)
see PCB 49-Set 183-11 113-9	175MU (Ch. 1-508-2) (Also see PCB 70—Set 210-1)
	(Also See PCB 107-Set 255-1) 229-15
	29-15 •175-18 'U' Series (Ch. 1-518-2) (Also See PCB 107—Set 255-1)
	duction Change Bulletin Production C

SYLVANIA

- 1.113 1.114 (Also use PCB 48-92-8 48-5et 182-11 (Also use PCB 48-92-8 48-92

114

SYLVANIA-Cont.

- SYLVANIA-Cont.

 •22M (Ch. 1-387) [See Model 2221M

 --Set 137-13]

 •22M-1, -2 (Ch. 1-387-1) (Also see

 PCB 41--Set 174-1)

 •22M-1 (Ch. 1-367-1)

 •22M-1 (Ch. 1-507-1)

 •23B, B-1, M, M-1 (Ch. 1-387-1)

 (Also see PCB 41-Set 174-1)

 •23B-11 (Ch. 1-507-1)

 •23B-11 (Ch. 1-507-1)

 •23B-11 (Ch. 1-507-1)

 •23M-11 (Ch. 1-507-1)

 •24M-1 (Ch. 1-387-1)

 •24M-1 (Ch. 1-387-1)

 •24M-1 (Ch. 1-387-1)

 •24M-1 (Ch. 1-387-1)

 •154-12

 •24M-1 (Ch. 1-387-1)

 •154-12

 •24M-1 (Ch. 1-387-1)

 •24M-1 (Ch. 1-387-1)

 •24M-1 (Ch. 1-387-1)

 •24M-1 (Ch. 1-387-1)

 •24M-3 (Ch. 1-387-1)

 •24M-3 (Ch. 1-387-1)

 •25M-11 (Ch. 1-387-1)

 •26B 41-Set 174-1

 •27B 1-1-Set 154-12, for radio

 •156 12, for radio

 •156 12, for radio

 •158 -12, for radio

 •171 M; (Ch. 1-48B-Set 192-9)

 •21M, (Ch. 1-441) (See Model
- SYLVANIA-Cont.

 229-15

 * 1768 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 1768 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 1764 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 1778 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 1778 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 1778 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-1, -3) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 778 (Ch. 1-508-2) (Also see PCB 700-Set 210-1)

 * 700-Set 210-1)

 * 7178 (Ch. 1-508-2, and Radio Ch. 1-603-1) (Also see PCB 700-Set 210-1)

 * 7178 (Ch. 1-508-2, and Radio Ch. 1-603-1) (Also see PCB 700-Set 210-1)

 * 7178 (Ch. 1-508-2, and Radio Ch. 1-603-1) (Also see PCB 700-Set 210-1)

 * 710 (Ch. 1-508-2, and Radio Ch. 1-603-1) (Also see PCB 700-Set 210-1)

 * 7178 (Ch. 1-504-1, 2, 2, 4)

 * 7178 (Ch. 1-504-1, 2, 2, 4)

 * 7180 (Ch. 1-504-2, 4)

 * 710 Series (Ch. 1-510-1
- PCB 41-Set 174-1 and Model 22M-1-Set 174-12, for Radio Ch. see Model 178B-Set 192-9) 71M (Ch. 1-441) (See Model 7110XB) 71M (Ch. 1-502-1) (Also see PCB 42-Set 176-1)163-12 72B (Ch. 1-366) (See PCB 55-Set 184-10) 72B-1 (Ch. 1-502-1) (Also see PCB 42-Set 176-1 and Model 7110X-Set 124-10) 72B-1 (Ch. 1-502-3) (See PCB 42 -Set 176-1 and Model 7110X-Set 184-10 (See 726 55-Set 184-10 (See PCB 55-Set 184-10, 1-366) (See PCB 42 -Set 176-1) (Also see PCB 42-Set 176-1) (Also see PCB 42-Set 176-1) (Also see PCB 184-10, 1-366) (See PCB 42 -Set 176-1) (See PCB 42 -Set 176-1) and Model 711M-1-Set 163-12) 72M (Ch. 1-366) (See PCB 42 -Set 176-1) and Model 711M-1-Set 163-12)

 - 212-8
 270 Series (Ch. 1-510-1, 2, 4)
 (See Model 1208—Set 212-8)
 271 Series (Ch. 1-510-1, 2, 4)
 275 Series (Ch. 1-510-1, 2, 4)
 275 Series (Ch. 1-510-1, 2, 4)
 275 Series (Ch. 1-510-1, 2, 4)
 210 Series (Ch. 1-510-1, 2, 4)
 211 Series (Ch. 1-510-1, 2, 4)
 230 Series (Ch. 1-514-4) (Also See PCB 100—Set 245-1)
 230 Series (Ch. 1-514-4) (Also See PCB 100—Set 245-1)
 230 Series (Ch. 1-514-4) (Also See PCB 100—Set 245-1)
 230 Series (Ch. 1-514-4) (Also See PCB 100—Set 245-1)
 230 Series (Ch. 1-520-4) (Also See PCB 100—Set 245-1)
 230 Series (Ch. 1-520-4) (Also See PCB 100—Set 245-1)
 231 Series (Ch. 1-520-5) (See PCB 100—Set 245-1)
 231 Series (Ch. 1-520-6) (See PCB 100—Set 245-1 and Model 120-20 Series—Set 234-13)
 231 Series (Ch. 1-520-1, 3) (Also See PCB 100—Set 245-1 and Model 120-20 U' Series—Set 234-13)
 231 Series (Ch. 1-520-3) (Also See PCB 100—Set 245-1 and Model 120-50 U' Series (Ch. 1-520-3) (Also See PCB 100—Set 245-1 and Model 326 Series (Ch. 1-520-3) (Also See PCB 100—Set 245-1 and Model 326 Series (Ch. 1-520-3) (Also See PCB 100—Set 245-1 and Model 326 Series (Ch. 1-520-3) (Also See PCB 100—Set 245-1) 234-133
 331 Series (Ch. 1-512-2, 4)
 333 Series (Ch. 1-513-2, 4)
 334 Series (Ch. 1-513-2, 4)
 335 Series (Ch. 1-513-2, 4)
 336 Series (Ch. 1-513-2, 4)
 337 Series (Ch. 1-518-1, 3)
 338 Series (Ch. 1-518-1, 3)
 339 Series (Ch. 1-518-2, 4)
 330 Series (Ch. 1-518-1, 3)
 331 Series (Ch. 1-518-1, 3)
 332 Series (Ch. 1-518-1, 3)
 334 Series (Ch. 1-518-1, 3)
 335 Series (Ch. 1-518-1, 3)
 <li

 - •386B (Ch. 1-512-1) •386BU (Ch. 1-512-2) •386M (Ch. 1-512-1) 220-10 220-10 220-10
 - 386MU (Ch. 1-512-2) 220-10

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NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Televisian Receiver.

SYLVANIA-Cont.

- SYLVANIA-Cont.

 •20 "U" Series (Ch. 1-520-4) (See PCB 100—Set 245-1 and Model 320 "U" Series.-Set 234-13)

 •21 "U" Series.-Set 234-13)

 •21 "U" Series.-Set 234-13)

 •21 "U" Series.-Set 234-13)

 •21 Series.-Set 234-13)

 •21 Series.-Set 234-13)

 •21 Series.-Set 234-13)

 •21 Series.-Set 234-13)

 •22 Series.-Set 234-13)

 •25 Series (Ch. 1-520-5) (See PCB 100—Set 245-1 and Model 120-20 Series.-Set 234-13)

 •25 Series.-Set 234-13)

 •25 Suries.-Set 234-13)

 •25 Series.-Set 234-13)

 •25 Series.-Set 234-13)

 •25 Series.-Set 234-13)

 •25 Series.-Set 234-13)

 •26 Series.-Set 234-13)

 •27 Series.-Set 234-13)

 •28 Series.-Set 234-13)

 •29 Series.-Set 234-13)

 •20 Series.-Set 234-13

 •20 Series.-Set 235-1 and Model

 ±00-Set 245-1 and Model

 ±00-Set 245-1 and Model

 ±00-Set 245-1 and
 </t

SYLVANIA-Cont. Ch. 1-387-1 (See Model 72M-1) Ch. 1-437 (See Model 74B-2) Ch. 1-437 (See Model 74B-2) Ch. 1-437-2 (See Model 74B-2) Ch. 1-437-3 (See Model 74B-2) Ch. 1-437-3 (Code SCOG end up) (See Model 150A) Ch. 1-441 (See Model 7110XB) Ch. 1-442 (See Model 7110XFA) Ch. 1-461 (See Model 7110XFA) Ch. 1-461 (See Model 7110XFA) Ch. 1-632-1 (See Model 73M-1) Ch. 1-502-2 (See Model 105B) Ch. 1-502-2 (See Model 105B) Ch. 1-502-1 (See Model 105B) Ch. 1-503-1 (See Model 105B) Ch. 1-504-2 (See Model 105B) Ch. 1-508-1 (See Model 105B) Ch. 1-508-1 (See Model 105B) Ch. 1-508-1 (See Model 105B) Ch. 1-510-2 (See Model 102B) Ch. 1-512-2 (See Model 127K) Ch. 1-513-1 (See Model 313 Series) Ch. 1-513-2 (See Model 331 Series) Ch. 1-513-3 (See Model 331 Series) Ch. 1-514-1, -3 (See Model 331-514)

Series) Ch. 1-514-1, -3 (See Model 105-14 Series) Ch. 1-514-4 (See Model 105-14

Ch. 1-514-4 (See Model 105-14 "U" Series) Ch. 1-514-5 (See Model 301 Series) Ch. 1-514-6 (See Model 301 "U" Series) Ch. 1-518-1 (See Model 175-18 Series) Ch. 1-518-2 (See Model 175-18 "U" Series) Ch. 1-518-3 (See Model 175-18 Series)

"U" Series) Series) Ch. 1-518-3 (See Model 175-18 Series) Ch. 1-518-5 (See Model 372 Series) Ch. 1-518-6 (See Model 372 ''U'' Series) Ch. 1-520-0 (See Model 326 Series) Ch. 1-520-4 (See Model 120-20 Ch. 1-520-4 (See Model 120-20) Ch. 1-520-6 (See Model 32 Series)

Ch. 1-520-4 (See Model 321 Series) Ch. 1-520-5 (See Model 321 Series) Ch. 1-520-6 (See Model 321 "U" Series) Ch. 1-520-7 (See Model 326 Series) Ch. 1-520-8 (See Model 326 "U" Series)

Ch. 1-520-8 (See Model 326 "U" Sories) Ch. 1-530-1 (See Model 410 Series) Ch. 1-530-2 (See Model 5118) Ch. 1-601-2 (See Model 5118) Ch. 1-601-2 (See Model 5138) Ch. 1-601-2 (See Model 5418) Ch. 1-602-2 (See Model 543) Ch. 1-602-3 (See Model 543) Ch. 1-603-1 (See Model 4338) Ch. 1-606-1 (See Model 4338) Ch. 1-606-1 (See Model 4338)

(Also see Recorder Listings)

8H67 "Musalarm" 44-23

• 38T12A-058 (Similar to

• 317T3 (Similar to Chassis) . 72 • 318T4 (Similar to Chassis) . 85 • 318T4-872 (Similar to Chass . 85

•318T6A (Similar to Chassis) 85—3 •318T6A-950 (Similar to Chassis)

 31876A-950 (Similar to Chossis)
 31879A-900 (Similar to Chossis)
 321MS39A (Similar to Chossis)
 226-11
 226-11 •518T6A (Similar to Chassis) 85-•518T9A-918 (Similar to Chass 78-78-

•518T10A-916 (Similar to Chas 78-

•2318T6A-954 (Similar to Chassi) •2318T9A-912 (Similar to Chassi) •2318T9A-912 (Similar to Chassi) 78-4

•2321MS39A (Similar to Chassis) 226-11

 TELE-KING

 •K21 (Ch. TVJ)
 177-13

 •K72 (Ch. TVJ)
 177-13

 •K731 (Ch. TVJ)
 177-13

 •K732 (Ch. TVJ)
 177-13

 •K732 (Ch. TVJ)
 177-13

 •K72 (Ch. TVJ)
 177-13

 •K72 (Ch. TVJ)
 177-13

 •K0270 (Ch. TVJ)
 177-13

 •K0276 (Ch. TVJ)
 177-13

 •K0276 (Ch. TVJ)
 177-13

 •K0276 (Ch. TVJ)
 177-13

 •K0276 (Ch. TVJ)
 177-13

 •K0278 (Ch. TVJ)
 177-13

 •K0278 (Ch. TVJ)
 177-13

 •K0278 (Ch. TVJ)
 177-13

 •K0278 (Ch. TVJ)
 177-13

 •K1 (Ch. RD-1)
 203-12

 •K41 (Ch. RD-1)
 203-12

 •K41 (Ch. RD-1)
 203-12

 •K13
 (Ch. TVL)

 •K14 (Ch. RD-1)

 •K14 (Ch. RD-1)

 •K14 (Ch. RD-1)

13) • 16CD3CR (For TV Ch. only see Model 162—Set 129-12) .141-13
 Model
 162—Set
 129-12)

 114
 141-13

 116, 116C
 141-13

 117, 117C, 117C0
 141-13

 117CA, CAF (For TV Ch, only see Model
 117-Set
 141-13

 1162
 129-12

TELE-KING

25-28

263-15

Chassis) 109-1

ssis

ssis

SYMPHONETTE 45-KA-37

TAPEMASTER

TECH-MASTER

PA-1

TELECHRON

TELECOIN

M5TS4 . TELECRAFT

Ch.

SYLVANIA-Cont.

- UM, MA
- 119-11
 5418, H., M. 5428R, C.H. GR. PE, YE (Ch. 1-602-1) 159-13
 543 (Ch. 1-602-3) 225-18
 5638 (Ch. 1-601-3) 221-11
 593 (Ch. 1-602-3) 225-18
 1110X (Ch. 1-327) [See PCB 47-128-16]
 1210X (Ch. 1-321) (Also toe PCB 44-55-58-1189-1 and Model 51308
 -Set 120-10]
 21408, M. (Ch. 1-462) (See PCB 55-Set 189-1 and Model 51408
 -Set 120-10]
 22104 (Ch. 1-387) 137-13
 4120M (Ch. 1-367) 137-13
 4120M (Ch. 1-367) 137-13
 4120M (Ch. 1-367) 137-13
 4120M (Ch. 1-367) 1124-10
 5130B, M. W (Ch. 1-200) (Also tee PCB 55-Set 189-1 and Model 51408
 -Set 120-10]
 221M (Ch. 1-367) 137-13
 4120M (Ch. 1-320) (Also tee PCB 55-Set 189-1) 124-10
 5130B, M. W (Ch. 1-270) (Also tee PCB 55-Set 189-1) 124-10
 5130B, M. W (Ch. 1-270) (Also tee PCB 55-Set 189-1) 124-10
 5130B, M. W (Ch. 1-270) (Also tee PCB 55-Set 189-1) 124-10
 5130B, M. W (Ch. 1-271), 120-10
 5130B, M. W (Ch. 1-271), 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (See PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (See PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7110X (Ch. 1-366) (Also tee PCB 55-Set 189-1) 124-10
 7120 (Ch. 1-3

TELE-KING-VIDEO PRODUCTS TRUETONE-Cont.

TELE-KING-Cont.	TELE-TONE-Cont.
+172 (Ch. TVG) (See Medal 201 Set	156 (Ch. Series U)
131-16) •174 (Ch. TVG) (See Model 201- Set 131-16)	135-Set 14-29)
•174 (Ch. TVG) (See Model 201- Set 131-16) 201, 202	157 (Ch. Series AE) 49-24 158 (Ch. Series AT) 59-20
	133—54 14-29) 157 (Ch. Series AE] 49–24 158 (Ch. Series AT] 59–20 159 (Ch. Series AT] 38–22 160 (Ch. Series T) 36–24 161, 162 (Ch. Series T) 36–24 163, 164 (Ch. Series T) 38–25 163, 164 (Ch. Series T) 59–20 Model 135—54t 14-29) 165 (Ch. Series AG) 50–20
•410	161, 162 (Ch. Series T) 38-25 163, 164 (Ch. Series "H") (See
• 510 (See Model 410—Set 88-12) • 512 88-12	Model 135-Set 14-29) 165 (Ch. Series AG) 50-20
510 (See Model #10—Set 86-12) 512	166 (Ch. AE)
•710 88-12 •712 (See Model 410-Set 88-12)	Model 133—3et 14-29) 165 (Ch. Series AG) 50–22 166 (Ch. AE) 49–24 167, 168, 171 (Ch. Series 1) 38–22 172 (Ch. Series U) 35–22 174 (Ch. Series U) 35–22 185 (Ch. Series U) 35–22 183 (Ch. Series 4) 185 (Ch. Series 4) 53–24
• 12 Oter Model 110 129-12 • 816.3CR (For TV Ch. only see Model 162—Set 129-12) • 916C • 916C • 129-12 • 129-12	176 (Ch. Series U) 35-23
Model 162-Set 129-12)	183
Model 102-3et 129-12 916C	190 (Ch. Series AZ) 61-19
•919C	183 53–24 185 (Ch. Series AH) 52–21 190 (Ch. Series AZ) 61–19 195 (Ch. Series BH) 71–15 198 59–20
•919CAF (For TV Ch. only see Model 114—Set 141-13) •920 (Ch. TVG) (See Model 201—	200 (Ch. Series "A2") [See Mode
 920 (Ch. TVG) (See Model 201— Set 131-16) 	201 (Ch. Series AX) 74-5 205 (Ch. Series BD) 73-12
114-3ef 141-13 920 (Ch. TVG) (See Model 201- Set 131-16) 1014 (Ch. TVG) (See Model 201- Set 131-16) 1016 (Ch. TVG) (See Model 201- Set 131-16) Ch. PD-1 (See Model 201- Ch. PD-1 (See Model 201- Set 131-16) (See Model 201- (See Mod	201 (Ch. Series AX) 74–5 205 (Ch. Series BD) 73–12 206 127–11 214 (Ch. Series ''AZ'') (See Model 190–Set 61.19)
 1016 (Ch. TVG) (See Model 201- Set 131-16) 	190—Set 61-19) 215 (Ch. Series BD)
Ch. RD-1 (See Model RK41) Ch. TVG (See Model 201) Ch. TVJ (See Model K21) Ch. TVJ (Revised) (See Model K-74)	215 (Ch, Series BD)
Ch. TVJ (See Model K21)	205 (Ch. Set 73-12)
TELEQUIP	Ch. Series A (See Model 100)
5135, 5136, 5140A 11-24	Ch. Series AE (See Model 157) Ch. Series AE (See Model 157)
TELESONIC (Medco)	Ch. Series AG (See Model 165) Ch. Series AH (See Model 185)
1635 20-22 1636 21-33 1642 20-23 1643 21-34	Ch. Series AT (See Model 158) Ch. Series AX (See Model 201)
1642	Ch. Series AZ (See Model 190) Ch. Series BD (See Model 205)
TELETONE	Ch. Series BH (See Model 195) Ch. BL (See Model 228)
• TV149	Ch. BQ (See Model 235) Ch. Series C (See Model 134)
IVI 49 56-22 IV. 170 83-12 IV. 208 90-11 IV 2081R 95-6 IV. 209 [See PCB 21-Set 136-1 and Model IV-249-Set 57-21] IV.210 [See PCB 21-Set 136-1 and Model IV-249-Set 57-21] IV.209 [See PCB 20-Set 357-21]	Ch. Series CA (See Model 133) Ch. Series D (See Model 117A)
• TV-208 TR 95-6 • TV-209 (See PCB 21-Set 136-1 and	Ch. Series H (See Model 135) Ch. Series I (See Model 109)
Model TV-249—Set 57-21) • TV-210 (See PCB 21—Set 136-1	Ch. Series N (See Model 138) Ch. Series R (See Model 138)
and Model TV-249—Set 57-21) • TV-220	Ch. Series S (See Model 143) Ch. Series S (See Model 148)
•TV-249 (Also see PCB 21—Set 136-1)	Ch. TAA, TAB (See Model TV-315)
•TV-250 91-13 •TV-254 91-13	Ch. TAC (See Model TV-308) Ch. TAH (See Model TV-316)
•TV-255, TV-256 (Ch. TS) 101-13 •TV-259 (See Model TV-249-Set	Ch. TAJ (See Model TV-314) Ch. TAM (See Model TV-318)
and Model IV-249—Set 37/21) IV-220	Ch. TAO (See Model TV-330) Ch. TAP, TAP-1, TAP-2 (See Mode
TV-283 (See Model TV-285-Set	232 (Ch. Series "B"') (See Mode 205—Set 73-12) 141-14 Ch. Series A (See Model 100) Ch. Series A (See Model 100) Ch. Series AE (See Model 157) Ch. Series AE (See Model 157) Ch. Series AE (See Model 158) Ch. Series AE (See Model 205) Ch. Series BD (See Model 205) Ch. Series C (See Model 134) Ch. Series C (See Model 133) Ch. Series I (See Model 138) Ch. Series I (See Model 148) Ch. Series I (See Model 143) Ch. Series I (See Model 143) Ch. Series I (See Model 143) Ch. TAA, TAB (See Model 17-316) Ch. TAA, TAB (See Model TV-306) Ch. TAA, TAP (See Model TV-306) Ch. TAA, TAP (See Model TV-306) Ch. TAA, TAP (See Model TV-306) Ch. TAA, TAB (See Model TV-306) Ch. TAA, See S (See Model TV-306) Ch. TAA, See S (See Model TV-306) Ch. TAA, See S (See Model TV-306) Ch. TY, TZ (See Model TV-306) Ch. Series I (See Model TV-306) Ch. Series
87.13) 1V-284	Ch. TW, TX (See Model TV-300) Ch. TY, TZ (See Model TV-306)
• TV-285, 287, 288	Ch. Series U (See Model 156) Ch. Series Y (See Model 160)
• TV-300, TV-301 (Ch. TAA, TAB) 99A-12	Ch. 8001, 8002, 8003 (See Mode TV-355)
•TV-300, TV-301 (Ch. TW) 107-10 •TV-304, TV-305 (Ch. TAA, TAB)	TELE-VOGUE (See Muntz)
•TV-304, TV-305 (Ch. TX). 107-10	TELEVOX
•TV-306, TV-307 (Ch. TV, TZ)	
	RP 22-29
•TV-308 (Ch. TAC)	27 IB-2W 20-33
104-12 TV-308 (Ch. TAC)109-14 TV-314 (Ch. TAJ)125-12 TV-315 (Ch. TAA, TAB)135-13 TV-316 (Ch. TAH)135-13	27-P-1 22-28
104-12 TV-308 (Ch. TAC) 109-14 TV-314 (Ch. TAJ) 125-12 TV-315 (Ch. TAA, TAB) 115-13 TV-316 (Ch. TAH) 135-13 TV-318 (Ch. TAM) 124-11 TV-322 (Ch. TAM) 124-11	TELE-VAR (See Audar)
104-12 TV-308 (Ch, TAC) 109-14 TV-314 (Ch, TAJ) 125-12 TV-315 (Ch, TAA, TAB) 115-13 TV-316 (Ch, TAA) 135-13 TV-318 (Ch, TAA) 124-11 TV-323 (Ch, TAA) 124-11 TV-323 (Ch, TAA) 124-11 TV-323 (Ch, TAA) 124-11 TV-324 (Ch, TAA) 124-11	27-P-1 22-20 TELE-VAR (See Audar) 1 TEMPLE 21-32
104-12 TV-308 (Ch. TAC) 109-14 TV-314 (Ch. TAJ) 125-12 TV-315 (Ch. TAA, TAB) 115-13 TV-316 (Ch. TAH) 135-13 TV-318 (Ch. TAH) 135-13 TV-323 (Ch. TAH) 124-11 TV-323, TV-323 (Ch. TAH) 124-11 TV-324, TV-323, TV-326 (Ch. TAP) 127-12 TAP-1, TAP-2) 127-12 TAP-2, TAP-2) 127-12	Z/-P-1 ZZ-28 TELE-VAR (See Audar) TEMPLE E-301 ZZ-38 E-510 ZZ-32 E-510 ZZ-32
• IV. 286, 287, 288 • 93-10 • IV. 300, TV. 301 (Ch. TAA, TAB) • 99A-12 • IV. 300, TV. 301 (Ch. TW) 107-10 • 99A-12 • IV. 304, TV. 305 (Ch. TAA, TAB) • 99A-12 • IV. 304, TV. 305 (Ch. TX). 107-10 • 99A-12 • IV. 304, TV. 305 (Ch. TX). 107-10 • 99A-12 • IV. 304, TV. 305 (Ch. TX). 107-10 • 99A-12 • IV. 304, TV. 305 (Ch. TX). 107-10 • 99A-12 • IV. 304, TV. 305 (Ch. TA). 107-10 • 104-12 • IV. 314 (Ch. TAA). 109-14 • 135-13 • V. 316 (Ch. TAA). 109-14 • 135-13 • V. 316 (Ch. TAA). 108-11 • 132-12 • V. 324, TV. 325, TV. 326 (Ch. TAP, 142-11 • V. 322, TV. 329 (Ch. TAP, 142-11 • V. 328, TV. 329 (Ch. TAP, 142-11 • V. 329, TV. 329 (Ch. TAP, 142-11 • V. 320, TV. 331, TV. 322, TV. 333 • (TAC). 142-12 • (TAC). 142-12 <	Z/-P-1 ZZ-28 TELE-VAR (See Audar) TEMPLE E-301 ZZ-38 E-510 ZZ-32 E-510 ZZ-32
(CR. TAO)	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
TV-335, TV-336 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-340 (Ch. TAP, TAP-1, 127-12	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. TAC) 143-11 • TV-335, TV-336 (Ch. TAP, TAP-1, TAP-2) • TV-340 (Ch. TAP, TAP-1, TAP-2) • TV-345 (Ch. TAP, TAP-1, TAP-2)	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. TAC) 143-11 • TV-335, TV-336 (Ch. TAP, TAP-1, TAP-2) • TV-340 (Ch. TAP, TAP-1, TAP-2) • TV-345 (Ch. TAP, TAP-1, TAP-2)	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. 1AC) 1V-335, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-2, 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2, 127-12 TV-345, TV-349 (Ch. TAP-2, ISE Model TV-324—Set 127-12) TV-345, See Model TV-324—Set	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. 1AC) 1V-335, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-2, 127-12) TV-345 (Ch. TAP, TAP-1, TAP-2, 127-12) TV-345 (Ch. TAP, TAP-1, TAP-2, 127-12) TV-345 (See Model TV-324—Set 127-12) TV-352 (See Model TV-324—Set 127-12) TV-352 (Ch. B001, 8002, 8003)	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. 140) 1V-333, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-1, 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-348, TV-349 (Ch. TAP-2) (See Model TV-324—Set 127-12) TV-352 (See Model TV-324—Set 127-12) TV-357 (Ch. 8001, 8002, 8003) T45-11 TV-357 (Ch. 8001, 8002, 8003)	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. 140) 1V-333, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-1, 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-348, TV-349 (Ch. TAP-2) (See Model TV-324—Set 127-12) TV-352 (See Model TV-324—Set 127-12) TV-357 (Ch. 8001, 8002, 8003) T45-11 TV-357 (Ch. 8001, 8002, 8003)	Z/-P-1 ZZ-20 TELE-VAR (See Audar) TEMPLE E-301 21-32 E-510 22 E-511 11-22 E-512, E-514 (See Model E-510- Set 2-3) Set 2-31 E-319 22 F-301 12-22
(Ch. 140) 1V-333, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-1, 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-348, TV-349 (Ch. TAP-2) (See Model TV-324—Set 127-12) TV-352 (See Model TV-324—Set 127-12) TV-357 (Ch. 8001, 8002, 8003) T45-11 TV-357 (Ch. 8001, 8002, 8003)	$\begin{array}{c} \textbf{Z}_{1}(\textbf{P},\textbf{I}) & \textbf{Z}_{2}(\textbf{Z},\textbf{Z}) \\ \textbf{TELE-VAR} (See Audor) \\ \textbf{TEMPLE} \\ \textbf{E}_{301} & \textbf{21}_{-32} \\ \textbf{E}_{310} & \textbf{21}_{-32} \\ \textbf{E}_{310} & \textbf{21}_{-32} \\ \textbf{E}_{311} & \textbf{E}_{11} \\ \textbf{E}_{312} \textbf{E}_{514} (See Model \textbf{E}_{510} \\ \textbf{E}_{312} \textbf{E}_{-31} \\ \textbf{E}_{319} & \textbf{2}_{-22} \\ \textbf{E}_{310} & \textbf{1}_{-22} \\ \textbf{E}_{310} & \textbf{1}_{-23} \\ \textbf{E}_{310} & $
(Ch. 140) 1V-333, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-1, 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-348, TV-349 (Ch. TAP-2) (See Model TV-324—Set 127-12) TV-352 (See Model TV-324—Set 127-12) TV-357 (Ch. 8001, 8002, 8003) T45-11 TV-357 (Ch. 8001, 8002, 8003)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 140) 1V-335, TV-336 (Ch. TAP, TAP-1, TAP-2) TV-340 (Ch. TAP, TAP-1, TAP-1, 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) 127-12 TV-345 (Ch. TAP, TAP-1, TAP-2) TV-345 (Ch. TAP, TAP-1, TAP-2) TV-352 (See Model TV-324—Set 127-12) TV-355 (Ch. 8001, 8002, 8003) TV-355 (Ch. 8001, 8002, 8003) TV-355 (Ch. 8001, 8002, 8003) TV-355 (Ch. 8001, 8002, 8003) TV-355 (Ch. 8001, 8002, 8003) TV-356 (Ch. 8001, 8002, 8003) TV-356 (Ch. 8001, 8002, 8003) TV-356 (Ch. 8001, 8002, 8003) TV-357 (Ch. 8001, 8002, 8003) TV-356 (Ch. 8001, 8002, 8003) TV-356 (Ch. 8001, 8002, 8003) TV-357 (Ch. 8001, 8002, 8003) TV-356 (Ch. 8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 1AC) 143-11 TV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 1AC) 143-11 TV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 1AC) 143-11 TV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 140) (Ch. 140) (Ch. 147) (Ch. 147) (Ch. 147, 147, 147, 147, 147, 147, 147, 147,	$\begin{array}{c} Z_{1} P_{1} & Z_{2} P_{1} \\ \hline TELE-VAR (See Audor) \\ \hline TEMPLE \\ \hline F:301 & 21-32 \\ \hline F:510 & 21-32 \\ \hline F:611 & 9-33 \\ \hline F:617 & 21-22 \\ \hline F:611 & 9-33 \\ \hline F:617 & 21-22 \\ \hline F:611 & 9-33 \\ \hline F:617 & 21-22 \\ \hline F:616 & 5-33 \\ \hline F:617 & 21-22 \\ \hline F:616 & 5-33 \\ \hline F:617 & 21-22 \\ \hline F:616 & 5-33 \\ \hline F:617 & 21-22 \\ \hline G:415 & 23-32 \\ \hline F:617 & 21-22 \\ \hline G:415 & 23-32 \\ \hline G:415 & 21-32 \\ \hline$
(Ch. 140) (Ch. 140) (Ch. 147) (Ch. 147) (Ch. 147, 147, 147, 147, 147, 147, 147, 147,	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 140) 143-1 17-313, TV-336 (Ch. TAP, 1AP, 127-2) 17-345 (Ch. 1AP, 1AP-1, 127-2) 17-352 (See Model TV-324—Set 127-12) 17-352 (See Model TV-324—Set 127-12) 17-355 (Ch. 8001, 8002, 8003) 145-11 17-355 (Ch. 8001, 8002, 8003) 145-11 17-356 (Ch. 8001, 8002, 8003) 145-11 17-356 (Ch. 8001, 8002, 8003) 145-11 100, 100-A, 101, 109 (Ch. Series A) 105 (See Model 117-A—Set 1-35) 105 (See Model 117-A—Set 1-35) 127 (Ch. 8011, 127-4) 128 (See Model 117-A—Set 1-35) 129 -26 124 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 127 (See Model 117-A—Set 1-35) 128 (See Model 117-A—Set 1-35) 129 -26 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 127 (See Model 117-A—Set 1-35) 128 (See Model 117-A—Set 1-35) 129 -26 (See Model 117-A—Set 1-35) 120 (See Model 117-A—Set 1-35) 121 (See Model 117-A—Set 1-35) 122 (See Model 117-A—Set 1-35) 123 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 127 (See Model 117-A—Set 1-35) 128 (See Model 117-A—Set 1-35) 129 -26 (See Model 117-A—Set 1-35) 120 (See Model 117-A—Set 1-35) 121 (See Model 117-A—Set 1-35) 122 (See Model 117-A—Set 1-35) 123 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A=Set 1-35) 125 (See Model 117-A=Set 1-35) 126 (See Model 117-A=Set 1-35) 127 (See Model 117-A=Set 1-35) 128 (See Mode	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(Ch. 140) 143-1 17-313, TV-336 (Ch. TAP, 1AP, 127-2) 17-345 (Ch. 1AP, 1AP-1, 127-2) 17-352 (See Model TV-324—Set 127-12) 17-352 (See Model TV-324—Set 127-12) 17-355 (Ch. 8001, 8002, 8003) 145-11 17-355 (Ch. 8001, 8002, 8003) 145-11 17-356 (Ch. 8001, 8002, 8003) 145-11 17-356 (Ch. 8001, 8002, 8003) 145-11 100, 100-A, 101, 109 (Ch. Series A) 105 (See Model 117-A—Set 1-35) 105 (See Model 117-A—Set 1-35) 127 (Ch. 8011, 127-4) 128 (See Model 117-A—Set 1-35) 129 -26 124 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 127 (See Model 117-A—Set 1-35) 128 (See Model 117-A—Set 1-35) 129 -26 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 127 (See Model 117-A—Set 1-35) 128 (See Model 117-A—Set 1-35) 129 -26 (See Model 117-A—Set 1-35) 120 (See Model 117-A—Set 1-35) 121 (See Model 117-A—Set 1-35) 122 (See Model 117-A—Set 1-35) 123 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 126 (See Model 117-A—Set 1-35) 127 (See Model 117-A—Set 1-35) 128 (See Model 117-A—Set 1-35) 129 -26 (See Model 117-A—Set 1-35) 120 (See Model 117-A—Set 1-35) 121 (See Model 117-A—Set 1-35) 122 (See Model 117-A—Set 1-35) 123 (See Model 117-A—Set 1-35) 124 (See Model 117-A—Set 1-35) 125 (See Model 117-A=Set 1-35) 125 (See Model 117-A=Set 1-35) 126 (See Model 117-A=Set 1-35) 127 (See Model 117-A=Set 1-35) 128 (See Mode	Z/-P-1 Z-2-20 TELE-VAR (See Audor) TEMPLE E-301 21-32 E-310 21-32 E-311 11-22 E-312 E-514 (See Model E-510 E-317 22-26 E-319 22-27 E-319 22-27 F-311 11-22 F-317 22-27 F-319 22-27 F-319 22-27 F-319 22-27 F-319 22-27 F-319 22-27 F-411 72-27 G-415 G-419 G-513 17-37 G-514 28-37 G-515 28-37 G-516 28-37 G-520 22-32 G-721 24-32 G-721 24-32 G-723 Gee Model G-722-Set 24 G-724 38-32 G-725 34-32 G-6251 G-722-Set 24 G-724 38-32 G-408<(See
(Ch. 1AC) 143-11 TV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2)	Z/-P-1 Z-2-20 TELE-VAR (See Audor) TEMPLE E-301 21-32 E-310 21-32 E-311 11-22 E-312 E-514 (See Model E-510 Ser 2-31 22 F-301 12-22 F-616 5-33 G-513 27-3 G-514 G-313 G-515 28-32 G-516 28-32 G-517 28-22 G-518 28-32 G-519 28-32 G-721 24-32 G-721 24-32 G-723 See Model G-722-Set 24 G-724 38-22 G-130 G-38-23 G-725 34-32 G-620 4-34 G-725 34-
(Ch. 140) 11. 14. 14. 14. 14. 14. 14. 14. 14. 14.	Z/P^1 $ZZ-Z$ TELE-VAR (See Audor) TEMPLE F:301 $Z1-33$ E:510 $ZZ-Z$ E:510 $ZZ-Z$ E:510 $ZZ-Z$ E:510 $ZZ-Z$ E:510 $ZZ-Z$ E:511 $Z=24$ F:312 $Z=24$ F:313 $Z=27$ F:411 $9-33$ F:616 $S=33$ F:617 $ZZ-22$ G:418 G:419 G:513 $ZZ-22$ G:514 $ZZ=12$ G:515 $TZ-32$ G:516 $ZZ=32$ G:517 $ZZ=22$ G:518 $ZZ=22$ G:721 $ZZ=427$ G:721 $ZZ=427$ G:721 $ZZ=427$ G:724 $ZZ=27$ G:725 $ZZ=427$ G:724 $ZZ=27$ G:725 $ZZ=427$ G:7205 $ZZ=Model G:722-Set 24$ G:7205 $ZZ=Model G$
(Ch. 140) 11. 14. 14. 14. 14. 14. 14. 14. 14. 14.	Z - P - 1 $Z - 2k$ TELE-VAR (See Audor) TEMPLE F.301 $21 - 3i$ E.510 $21 - 3i$ E.511 $11 - 2i$ E.512 E.510 E.513 $21 - 2i$ F.311 $9 - 3i$ F.611 $9 - 3i$ F.616 $5 - 3i$ F.617 $12 - 2i$ G-418 G - 19 G-518 $29 - 2i$ G-518 $29 - 2i$ G-518 $29 - 2i$ G-519 $22 - 3i$ G-721 See Model G-722 - Set 24 G-723 See Model G-722 - Set 24 G-723 See Model G-722 - Set 24 G-724 Ge 24 - 27i G-725 See Model G-722 - Set 24 G-720 Ge 24 - 27i G-720.5 (See Model G-722 - Set 24 G-720.5 (See Model G-521 - Set 28 G-720.5 (See Model G-521 - Set 28 G-72
(Ch. 140) 143-11 1V-335, TV-336 (Ch. TAP, TAP-1, 127-12 1V-345 (Ch. 1AP, TAP-1, 127-12 1V-352 (See Model TV-324—Set 127-12) 1V-352 (See Model TV-324—Set 127-12) 1V-357 (Ch. 8001, 8002, 8003) 145-11 100, 100-A, 101, 109 (Ch. Series A) 100, 100-A, 101, 109 (Ch. Series A) 110 (See Model 117-A-Set 1-35) 112 (See Model 117-A-Set 1-35) 123 (See Model 117-A-Set 1-35) 124 (See Model 117-A-Set 1-35) 125 (See Model 117-A-Set 1-35) 126 (See Model 117-A-Set 1-35) 127 (See Model 117-A-Set 1-35) 133 (Ch. Serier N) 23-26 124 (See Model 117-	$Z - P_{1}$ $Z - 2i$ TELE-VAR (See Audor) TEMPLE E 301 $21-3i$ E \$10 $21-3i$ E \$11 $11-2i$ E \$12, E-514 (See Model E-510- E \$12, E-514 (See Model E-510- E \$12, E-514 (See Model E-510- F-301 $12-2i$ F-616 $5-33$ F-617 $12-2i$ G-418, G-419 $26-2i$ G-518 $29-2i$ G-518 $29-2i$ G-518 $29-2i$ G-518 $29-2i$ G-721 (See Model G-722-Set 24 271 $24-2i$ G-723 See Model G-722-Set 24 272 $2-2i$ G-721 (See Model G-722-Set 24 272 $34-2i$ G-723 (See Model G-722-Set 24 271 $47-2i$ G-7205 (See Model G-722-Set 28 24-27 $42-2i$ G-7205 (See Model G-722-Set 28 24-27
(Ch. 140) 143-11 1V-335, TV-336 (Ch. TAP, TAP-1, 127-12 1V-345 (Ch. 1AP, TAP-1, 127-12 1V-352 (See Model TV-324—Set 127-12) 1V-352 (See Model TV-324—Set 127-12) 1V-357 (Ch. 8001, 8002, 8003) 145-11 100, 100-A, 101, 109 (Ch. Series A) 100, 100-A, 101, 109 (Ch. Series A) 110 (See Model 117-A-Set 1-35) 112 (See Model 117-A-Set 1-35) 123 (See Model 117-A-Set 1-35) 124 (See Model 117-A-Set 1-35) 125 (See Model 117-A-Set 1-35) 126 (See Model 117-A-Set 1-35) 127 (See Model 117-A-Set 1-35) 133 (Ch. Serier N) 23-26 124 (See Model 117-	Z/-P-1 ZZ-24 TELE-VAR (See Audor) TEMPLE F-301 21-32 E-510 22-32 E-510 21-32 E-510 22-32 E-510 22-32 E-510 22-32 E-511 10 E-512 See Audor) F-611 9-33 F-616 5-33 F-617 12-22 G-418 G-419 G-515 17-33 G-516 18-33 G-518 29-27 G-518 29-27 G-518 29-27 G-518 29-27 G-518 29-27 G-721 See Model G-722-Set 24 G-721 See Model G-722-Set 24 G-725 See Model G-722-Set 24 G-725 See Model G-722-Set 24 G-7205 See Model G-722-Set 24
(Ch. 140) 143-1 IV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2) 127-12 TV-340 (Ch. TAP, TAP-1, TAP-1, TAP-2) 127-12 IV-345 (Ch. TAP, TAP-1, TAP-2) IV-345 (Ch. TAP, TAP-1, TAP-2) IV-345 (Ch. 140, TAP-2, TAP-2) IV-345 (Ch. 140, TAP-2, TAP-2) IV-357 (Ch. 140, 140, 145-2) IV-357 (Ch. 140, 145-1) IV-357 (Ch. 145-1)	Z/-P-1 ZZ-24 TELE-VAR (See Audor) TEMPLE E-301 21-32 E-510 22-24 E-511 11-22 E-512 E-510 E-731 12-22 F-611 9-33 F-616 5-33 F-617 12-22 G-410 27-26 G-415 43-11 G-416 5-33 F-616 5-33 F-616 5-33 G-418 G-419 G-518 29-27 G-518 29-27 G-518 29-27 G-721 Se-22 G-642 24-27 G-721 Se-28 G-721 Se-29 G-721 See Model G-722-Set 24 272 24-27 G-724 38-27 G-725 34-22 G-7205 (See Model G-722-Set 24 272 24-27 G-723 (See Model G-722-Set 24 2725 34-22 G-7205 (See Model G-722-Set 2
(Ch. 140) 143-1 IV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2) 127-12 TV-340 (Ch. TAP, TAP-1, TAP-1, TAP-2) 127-12 IV-345 (Ch. TAP, TAP-1, TAP-2) IV-345 (Ch. TAP, TAP-1, TAP-2) IV-345 (Ch. 140, TAP-2, TAP-2) IV-345 (Ch. 140, TAP-2, TAP-2) IV-357 (Ch. 140, 140, 145-2) IV-357 (Ch. 140, 145-1) IV-357 (Ch. 145-1)	Z/-P-1 ZZ-24 TELE-VAR (See Audor) TEMPLE E-301 21-3: E-310 21-3: E-311 11-2: E-312 E-514 (See Model E-510 E-319 22: E-310 22-2: E-311 12-2: E-312 E-514 (See Model E-510 E-319 22: F-311 9-2: F-611 9-3: F-616 5-3: F-617 12-2: G-418 G-419 G-418 G-419 G-513 17-3: G-514 29-2: G-515 17-3: G-518 29-2: G-522 26-2: G-649 22-3: G-721 28-3: G-722 24-2: G-724 38-2: G-724 38-2: G-725 34-2: G-724 38-2: G-725 34-2: G-725 34-2: G-725 4-2:
$ \begin{array}{c} (ch, 140) \\ (ch, 140) \\ (ch, 140) \\ (ch, 140, 140) \\ (ch, 140$	Z/-P-1 ZZ-24 TELE-VAR (See Audor) TEMPLE E-301 21-32 E-510 22-24 E-511 11-22 E-512 E-510 E-731 12-22 F-611 9-33 F-616 5-33 F-617 12-22 G-410 27-26 G-415 43-11 G-416 5-33 F-616 5-33 F-616 5-33 G-418 G-419 G-518 29-27 G-518 29-27 G-518 29-27 G-518 29-27 G-519 22-32 G-642 24-24 G-721 See Model G-722-Set 24 Z71 See Model G-722-Set 24 Z72 G-723 See 24-22 G-724 38-27 G-725 34-22 G-726 See Model G-722-Set 24 Z71 See Model G-722-Set 28 G-7205 See Model G-722-Set 28 Stose Model G-725-Set 44 27
(Ch. 140) 143-1 IV-335, TV-336 (Ch. TAP, TAP-1, TAP-1, TAP-2) 127-12 TV-340 (Ch. TAP, TAP-1, TAP-1, TAP-2) 127-12 IV-345 (Ch. TAP, TAP-1, TAP-2) IV-345 (Ch. TAP, TAP-1, TAP-2) IV-345 (Ch. 140, TAP-2, TAP-2) IV-345 (Ch. 140, TAP-2, TAP-2) IV-357 (Ch. 140, 140, 145-2) IV-357 (Ch. 140, 145-1) IV-357 (Ch. 145-1)	Z/-P-1 ZZ-24 TELE-VAR (See Audor) TEMPLE E-301 21-3: E-310 21-3: E-311 11-2: E-312 E-514 (See Model E-510 E-319 22: E-310 22-2: E-311 12-2: E-312 E-514 (See Model E-510 E-319 22: F-311 9-2: F-611 9-3: F-616 5-3: F-617 12-2: G-418 G-419 G-418 G-419 G-513 17-3: G-514 29-2: G-515 17-3: G-518 29-2: G-522 26-2: G-649 22-3: G-721 28-3: G-722 24-2: G-724 38-2: G-724 38-2: G-725 34-2: G-724 38-2: G-725 34-2: G-725 34-2: G-725 4-2:

	TONE PAK	
35-23) (See Model	AC8HF	
	TRAD • C-2020, C-2420, CD2020 . 173–14 • T-20, A	
49-24 59-20 38-26 36-24	T.20, A 133-14 T.20, E 165-17A T.1220 173-14 T.1220 173-14 T.1853, A 200-10	
	•T-1720 •T-1853, A	
29) 50 –20	TRANSVISION	-
50-20 49-24 ries T) 38-25 35-23 38-25 35-23 51-22	• Ch. Model A 107-11 • Ch. A-3 130-15 • Ch. A-41 192-10 • WRS-3 112-10	
35-23	• Ch. A-41	
38-25 35-23 51-22	TRANSVUE	
53–24 52–21	17XC, 17XT (Similar to Chassis) 132—8 20XC, 20XT (Similar to Chassis)	
71 -15	●20XC, 20XT (Similar to Chassis) 132—8 ●601 (Ch. 16AX23, 25, 26) (Similar to Chassis) 99-14	
59-20 } (See Mocel		
	to Chassis)	
74-9 73-12 127-11) (See Model	• of 0 (ch. 16AX23, 25, 26) (similar to Chossis)	
	TRAV-LER (Also see	
73-12 144-13) {See Model	Record Changer Listing) • 10T	
	Record Changer Listing) 101 86–11 12150, A 108–13 108–13 127 86–11 1450, A, 14C50, A 108–13 14850, A, 14C50, A 108–13 16850A 108–13 16850A, 16750A 108–13 168-50A 165–13 141 (Also see PCB 31–Set 156-3) 86–11 166–13	
lel 100) del 159) del 157)	14850, A, 14C50, A 108–13 •16G50A	
del 157) del 165)	●16K50A, 16150A ●16T (Also see PCB 31—Set 156-3)	
del 185) del 158)	• 20A50 146-11	
del 15/} odel 165) odel 185) odel 201) odel 201) odel 205) odel 195] 8)	● 16T (Also see PCB 31—3ct 150-3) 86-11 820A50 186-11 827850, 637850 150-13 847850, 647850-1, 647850-2 146-11 856550, -1, -2 (See Model 20450- 5ct 146-11) 754500, 75450-1, 75450-2 146-11	
del 205) del 195) 8)	Set 146-11) •75A50, 75A50-1, 75A50-2, 146-11	
35) lel 134)	•114-1A, -2 (Ch. 32A1) 150-13 •117-3, -4, -6 (Ch. 32A1) 150-13	
el 133) el 117A) lel 135)	●119-5 (Ch. 32A1)	
el 1091	•217-15, 217-16 (Ch. 34A2) 170-14	
del 138) del 145) lel 143) del 150)	Set 146-11) 75A50, 75A50-1, 75A50-2, 146-11 114-1A, -2 (Ch. 32A1)150-13 117-3, -4, -5 (Ch. 32A1)150-13 119-5 (Ch. 32A1)150-13 217, -10, -11, -12, -14 (Ch. 32A2) 171-11 217-15, 217-16 (Ch. 34A2) 170-14 217-25 (Ch. 33A2) (See Model 217- 217-5, (Ch. 33A2) (See Model 217-	
del 143) del 150)		
odel TV-315) TV-308)	15—5et 170-14) 219-8A, 219-8B (Ch. 11A2) 162-14 220-9, -9A, -9B (Ch. 33A2) 171-1 120-22, -23, -24, -27 (Ch. 3AA2) (See Model 217-15—Set 170-14) -317-44, A (Ch. 4653) 240-10 -317-47 (Ch. 46A3) 240-10 -321-46, -321-48 (Ch. 46A3) 240-10 -5000 (See Model 50001—Set 11- -27)	
TV-316) TV-314) TV-318)	(See Model 217-15—Set 170-14) 317-44 A (Ch 4683) 240-10	
TV-318) TV-330) 2 (See Model	• 317-47 (Ch. 46A3)	
	5000 (See Model 50001-Set 11- 27)	
-255) del TV-300) lel TV-306)	50001 11-27 5002 Series (Ch. 109) 12-28	
del 1561 del 160)	271 11-27 50001 12-28 5007, 5008, 5009 (Ch. 104) 1-36 5010, 5011, 5012 (Ch. 105) 2-5 5015 36-25	
3 (See Model	5015 36-25 5019 23-30 5020 (Ch. 800) 11-28	
Nuntz)	5019 23-30 5020 (Ch. 800) 11-28 5021 43-20 5022 101-14 5027 31-30	
22 –29	5027 31-30 5028 34-24 5029 31-30	
20-32 20-33	5029 33 -29 5030, 5031 32 -25	
	5036	
lar)	3049 32-26 5051 32-26 5054 36-26 5056-A 90-12 5060, 5061 116-11 5066 42-24 5091 252-12 5170 163-13	
21–35 2—3 11–26	5060, 5061	
11-26 odet E-510-		
2—3	5180B, M	
1226 9-32 5-38	5182-8,-M 264-16 5300 224-13 5301 224-15 5305 260-15 5310 243-12 5327 240-10 6040 42-23 6050 5-231	
5-38 12-27	5305	
12-27 27-28 43-18 26-25 23-29	6040	
	6053 (See Model 6050—Set 56-23) 7000, 7001 59-23	
17–34 18–31 29–27 28–33	6050 56-23 6053 (See Model 6050—Set 56-23) 7000, 7001 59-21 7003 (Ch. 501) 12-29 7014 59-21 7014 59-21	
20-26	7023	
22-30 44-24	7036 112–11 7053 262–14	
34 07	Ch. 11A2 (See Model 219-8A) Ch. 32A1 (See Model 62R50)	
24-27 722-Set 24-	Ch. 33A2 (See Model 217-15) Ch. 34A2 (See Model 217-15) Ch. 35B2 (See Model 217-27)	
38-27 34-23 43-19	Ch. 46A3 (See Model 317-47) Ch. 46B3 (See Model 317-44)	
38-27 34-23 43-19 G-418Set	7036 112-11 7053 262-14 Ch. 31A1 (See Model 219-8A) Ch. 32A1 (See Model 217-15) Ch. 33A2 (See Model 217-15) Ch. 33B2 (See Model 217-17) Ch. 463A (See Model 317-47) Ch. 104 (See Model 317-47) Ch. 105 (See Model 3007) Ch. 107 (See Model 5007) Ch. 308 (See Model 3000) Ch. 309 (See Model 5002) Ch. 309 (See Model 5002) Ch. 309 (See Model 5002) Ch. 309 (See Model 5002)	
G-722—Set	Ch. 109 (See Model 5002) Ch. 501 (See Model 7003)	
47-23	Ch. 800 (See Model 5021) TRELA	
44-24	HW301 14-28	
725Set 34-	TRUETONE	
V-1778, TV- 66-16	D1034A, B. C (See Model D1046A Set 102-15) D1046A 102-15	
	— 3et 102-13) D1046A	
28	D1092 (Similar to Chassis) 108-7 D-1234A, B 189-15	
Temple)	D1240A	1
8 -31 30 -30	D1046B, C, D (see Model D1046 	
8-31 30-30 57-22 9-33 20-34 76-18	D1645 (Foctory 26A76-650) 6-33 D1747, D1748 32-27 D1752 (Foctory 7901-14) 34-25 D1835 (Foctory Model 25A86-856)	
20-34 76-18	D1835 (Factory Model 25A86-856) 44-25	
	D1836, D1836A (Factory 26885- 856) 45-25 D1840 (Fact. No. 138PCXM) 46-24	
ger Listing)	D1840 (Fact. No. 138PCXM) 46-24	

TELE-TONE-Cont.	TONE PAK	TRUETONE-Cant.
156 (Ch. Series U)	AC8HF 24-28	D1845 31-31 D1845 40-23 D1850 (Series A) 51-23 D1949 60-20 D1950 (D1951 (See Model D1850 -Set 51-23) D1952 (See Model D1940—Set 60-
135-Set 14-29)	TRAD	D1850 (Series A) 51-23
157 (Ch. Series AE) 49-24 158 (Ch. Series AT) 59-20	•C-2020, C-2420, CD2020 173-14 •T-20, A 133-14	D1950, D1951 (See Model D1850
159 (Ch. Series AA) 38-26 160 (Ch. Series Y) 36-24	• C-2020, C-2420, CD2020 • T-20, A • T-20-E • T-72-E • T-1720 • T-1720	—Set 51-23) D1952 (See Model D1949—Set 60-
161, 162 (Ch. Series T)	•T-1853, A	20) = D1990 (Eastory No. 74522) 69-3
133-561 14-29 137 (Ch. Series AE) 49-24 138 (Ch. Series AT) 59-20 139 (Ch. Series AT) 38-26 160 (Ch. Series T) 36-24 161 162 (Ch. Series T) 36-24 163 (Science T4) 36-24 36-26 164 (Science T4, 29) 56-21 36-26 165 (Science T4, 29) 56-20 56-20	TRANSVISION	D1991, B. 77–11 D1992 (Factory No. 7AF22) 69–13 D1993, B. 77–11 D1994 . 77–11
moder (J)=-3er(4-27) 50-20 165 (Ch. AE)	• Ch. Model A 107-11 • Ch. A-3 130-15 • Ch. A-4. 192-10 • WRS-3 112-10	•D1992 (Factory No. 7AF22) 69-13 •D1993, B
167, 168, 171 (Ch. Series T) 38-25 172 (Ch. Series U) 35-23	• Ch. A-41	•D1994
174 (Ch. Series T) 38-25		18)
182	TRANSVUE • 17XC, 17XT (Similar to Chassis)	D2017, D2018
183	●20XC, 20XT (Similar to Chassis)	D2020 106-15 D2025A (Fact. Mod. 26A95-906) 83-14 D2027A 97-18
190 (Ch. Series AZ) 61-19 195 (Ch. Series BH) 71-15		D2027A
176 (ch. series U) 35-23 182 51-22 183 (ch. series AH) 52-21 185 (ch. series AH) 52-21 190 (ch. series AZ) 61-19 195 (ch. Series MAZ') (See Model 190-Set 61-19) 201 (ch. Series XA) 74-9	 601 (Ch. 16AX23, 25, 26) (Similar to Chassis)	D2103A, B
190-Set 61-19)	to Chassis) 99-14 610 (Ch. 16AX23, 25, 26) (Similar to Chassis) 99-14 14001 (Similar to Chassis) 132-8 1700C, (Similar to Chassis) 132-8	D2145
190-set 61-19) 201 (Ch. Series AX)	●1400T (Similar to Chassis) 132—8 ●1700C (Similar to Chassis) 132—8	D2214A
206	• 2000C (Similar to Chassis) 132-8	D2226
190—Set 61-19) 215 (Ch. Series BD) 73-12	TRAV-LER (Also see	D2255
215 (Ch, Series BD)	Record Changer Listing) •10T	B3-14 B3-14 D2027A 97-18 D2103A, B 200-11 D2103A, B 200-11 D2103A, B 200-11 D2103A, D2109A 199-14 D2145 197-13 D22205 201-12 D2214A 204-10 D2227A 182-15 D2237A 182-15 D2235 197-14 D2243 190-14 D2235-A 205-11 D2335-A 205-11 D2338, D2387, D2388 230-13
205-Set 73-12)	•12L50, A	D2383
205—Set 73-12) 235 (Ch. BQ)	101 80-11 12150, A 108-13 121 86-11 14850, A, 14C50, A 108-13 16650A, 16750A 108-13 16760A, 16750A 108-13 161 (Also see PCB 31-Set 156-3) 86-11	D2389
	●16G50A 108-13 ●16R50A, 16T50A 108-13	D2410A D2411A D2412A D2413A
Ch. Series AE (See Model 157) Ch. Series AE (See Model 157) Ch. Series AG (See Model 165) Ch. Series AH (See Model 185)	●16T (Also see PCB 31—Set 156-3) 86-11	225–19 D2418A, D2419A, D2420A 257–18 D2483 261–14
	• 20A50	D2603 (Factory No. 461) 13-33
Ch. Series AX (See Model 201) Ch. Series AZ (See Model 190)	• 20A50 146-11 • 62R50, 63R50 150-13 • 64R50, 64R50-1, 64R50-2 146-11 • 65G50, -1, -2 (See Model 20A50	DOLOG (E. A. H. L. DAMON D. 24
Ch. Series BD (See Model 205) Ch. Series BH (See Model 195) Ch. BL (See Model 228)		D2606
Ch. BL (See Model 228) Ch. BD (See Model 228)	•75A50, 75A50-1, 75A50-2 146-11	D2613 13-37
Ch. BQ (See Model 235) Ch. Series C (See Model 134) Ch. Series CA (See Model 133)	54.500 75450-1, 75450-2 146-11 114-1A, -2 (Ch. 32A1) 150-13 117-3, -4, -6 (Ch. 32A1) 150-13 119-5 (Ch. 32A1) 150-13 217, -10, -11, -12, -14 (Ch. 32A2)	D2616 (Factory Model 6D110) 2-18
Ch. Series D (See Model 117A)	●119-5 (Ch. 32A1)	D2616-B
Ch. Series H (See Model 135) Ch. Series J (See Model 109)	•217-15, 217-16 (Ch. 34A2) 170-14	D2619 (Factory No. 2701). 27-29 D2620
Ch. Series N (See Model 138) Ch. Series R (See Model 145)	217-15, 217-16 (Ch. 34A2) 170-14 217-25 (Ch. 34A2) (See Model 217-15-Set 170-14) 217-27 (Cl. 2502) (See Model 217	02612 (Code 3W-9022-0) - 33 02613 (Factory Model 6D110) 218 02616 (Factory Model 6D117) 10-32 02616-8 - 3132 02619 (Factory No. 2701) 27-29 02620 - 128 02622 - 14-30 02623 - 14-30 02623 - 11-29 02624 (Factory 27014-600) 26
Ch. Series S (See Model 148) Ch. Series T (See Model 150)	•21/-2/ (Ch. 3362) (See Model 21/-	D2623 11-29
Ch. TAA, TAB (See Model 150) Ch. TAA, TAB (See Model TV-315)	• 219-8A, 219-8B (Ch. 11A2) 162-14	D2624 (Factory 27D14-600) 2-6 D2626 (Fact. No. 457-2). 52-22 D2630 (Factory 27D14-602 Issue A)
Ch. TAA, TAB (See Model TV-315) Ch. TAC (See Model TV-308) Ch. TAH (See Model TV-316)	• 220-9, -9A, -9B (Ch. 33A2) 171-11 • 220-22, -23, -24, -27 (Ch. 34A2)	······························
Ch. TAJ (See Model TV-314)	(See Model 217-15-Set 170-14)	
Ch. TAM (See Model TV-318) Ch. TAO (See Model TV-330)	15—5et 170-141 210-8A, 219-88 (Ch. 11A2) 162–14 220-9, -9A, -98 (Ch. 33A2) 171–11 220-22, -23, -24, -27 (Ch. 33A2) (See Model 217-15—Set 170-14) 317-44, A (Ch. 4683)	D2640 (Factory No. 459). 43-21 D2642
Ch. TAP, TAP-1, TAP-2 (See Model TV-324)		D2644 (Factory No. 101C). 11-30 D2645 4-39
Ch. TS (See Model TV-255) Ch. TW, TX (See Model TV-300)	27) 50001	D2044 (Factory No. 101C), 11–30 D2061 (Factory 4819) 2–23 D2063 (Ch. 4C1) 11–31 D2065 (Factory 48114 Series A)
Ch. TW, TX (See Model TV-300) Ch. TY, TZ (See Model TV-306) Ch. Series II (See Model TV-306)	5002 Series (Ch. 109) 12-28 5007 5008 5009 (Ch. 104) 1-36	D2665 (Factory 48114 Series A)
Ch. Series U (See Model 156) Ch. Series Y (See Model 160)	5010, 5011, 5012 (Ch. 105) 2-5	D2692
Ch. 8001, 8002, 8003 (See Model TV-355)	5015 5019 23 –30	D2692
TELE-VOGUE (See Muntz)	5020 (Ch. 800) 11–28 5021 43–20	23-31 D2718 (Factory No. 227D14-638IU)
TELEVOX	5022 101–14 5027 31–30	D2718 (Factory-No. 227D14-638IU) 23-32 D2743 25-29 D2745 (See Model D1645-Set 6-33)
RP 22–29 27.18-2W 20–32	5028	D2745 (See Model D1645-Set 6-33)
RP 22-29 27.'B-2W 20-32 27K-W 20-33 27-P-T 22-28	5030, 5031 32–25 5036 54–19	D2748 (Ch. 7156)
TELE-VAR (See Audar)	5049	
TEMPLE	5054	D2810 (Factory No. 24D24-730BB) 36-27 D2815 48-25 D2819 (Factory No. 26A82-738) 35-24 29 29
E-301	5060, 5061	D2819 (Factory No. 26A82-738)
E-511 11-26	5091	D2851
E-512, E-514 (See Model E-510- Set 2-3)	5170 163-13 5180B, M	D2906 (Factory No. 189). 69–14 D2907
E-519 2—3 F-301 12-26	5182-B, -M	D2910
F-611 9-32 F-616 5-38	5301	D2963
F-617 12-27	5310	D2985
G-415	6040	D3120A 203-12
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	5000 (See Model 5000)—Set 11. 77) 5001	33-24 D2851 38-28 D2906 [Fectory No. 189]. 69-14 D2907 69-14 D2910 65-16 D2919 [Fect No. 60F21). 59-22 D2963 68-18 D2985 70-11 D2987 69-13 D3120A 203-12 D3130A, B 203-12 D3120A 190-15 D2265A 189-16 D3000 225-20
G-515	6033 (36e model 6050-set 367.3) 7000, 7001 59-21 7003 (Ch. 501) 12-29 7014 59-21 7015, 7017 84-11 7023 83-13 7036 112-11 7035 262-14	D3265A
G-518	7014	D3351, D3352, D3353 224-16 D3615 (Factory 258D2-606) 18-32
G-522 26-26 G-619 20 26-26	7023 83-13 7036	D3619 (Foctory 5P110) 10-33
G-622 44-24 G-721 (See Model G-722-Set 24-	7053	D3720 24-29
271	Ch. 32A1 (See Model 62R50)	D2265A 189-16 D3300 225-20 D3351, D3352, D3353, 224-16 236 D3615 [Foctory 25B02-606] 18-32 D3619 [Foctory 5P110] 10-33 D36300, 105-30 10-33 D3720 105400 D3720 [Factory 1008x] 32-28 D3721 [Factory 1008x] 32-28 D3726 [Factory 1008x] 32-29 D3706 [Factory No. 178] 43-22 D3708 [Factory No. 178] 43-27
G-723 (See Model G-722-Set 24-	Ch. 33A2 (See Model 217-15) Ch. 34A2 (See Model 217-15)	D3809 (Factory No. 178) 43-22 D3810
271		D2011 (East No. 1148YH) 47 24
	Ch. 35B2 (See Model 217-27) Ch. 46A3 (See Model 317-47)	D3840 49-24
G-725 34-23	Ch. 35B2 (See Model 217-27) Ch. 46A3 (See Model 317-47) Ch. 46B3 (See Model 317-44) Ch. 104 (See Model 5072)	D3910 (Fact. Model 140611) 74-10
G-724 38-27 G-725 34-23 G-1430 43-19 G-4108 (See Model G-418-Set	Ch. 35B2 (See Model 217-27) Ch. 46A3 (See Model 317-47) Ch. 46B3 (See Model 317-44) Ch. 104 (See Model 5007) Ch. 105 (See Model 5001)	D3910 (Fact. Model 140611) 74-10
26.251	Ch. 3582 (See Model 217-27) Ch. 46A3 (See Model 317-47) Ch. 4683 (See Model 317-44) Ch. 104 (See Model 5007) Ch. 105 (See Model 5010) Ch. 107 (See Model 5002) Ch. 301 (See Model 5002)	D3910 (Fact. Model 140611) 74-10
26-25) G-7205 (See Model G-722—Set 24-27) H-411 47-23	7036 112-11 7053 262-14 Ch. 11A2 (See Model 217-8A) Ch. 32A1 (See Model 247-85) Ch. 33A2 (See Model 217-15) Ch. 33A2 (See Model 217-15) Ch. 33A2 (See Model 217-47) Ch. 46A3 (See Model 317-44) Ch. 104 (See Model 317-44) Ch. 104 (See Model 3007) Ch. 107 (See Model 5002) Ch. 309 (See Model 5010) Ch. 309 (See Model 5002) Ch. 309 (See Model 5002)	D3910 (Fact. Model 140611) 74-10
C4.106 (See Model G-416-Set Set 26.25) (See Model G-722-Set 24.27) H-411 47-23 H-521 (See Model G-521-Set 28-33)	TRELA	D3910 (Fact. Model 140611) 74-10
C4.106 (See Model G-416-Set Set 26.25) G-720.5 (See Model G-722-Set 24.27) H-411 47-23 H-521 (See Model G-521-Set 28-33)	HW301 14-28	D3910 (Fact. Model 140611) 74-10
G. 4100 (See Model G-712—Set 26.25) G-7205 (See Model G-722—Set 14.11	TRELA HW301 14–28 TRUETONE	D3910 (Fact. Model 140611) 74-10
G.4100 (See Model G-416Set 26-25) G-702-Set 24-27) H-411 47-23 H-521 (See Model G-521Set 28- 33) H-622 H-727 (See Model G-725Set 34- 4-727 14-24	TRELA HW301 14-28 TRUETONE D1034A, B. C (See Model D1046A Set 102-151	D3910 (Fact. Model 140611) 74-10
G. 4106 (See Model G-416—Set) 26-25) G-7205 G. 7205 (See Model G-722—Set) H-411	TRELA HW301 14-28 TRUETONE D1034A, B. C (See Model D1046A Set 102-151	D3840 (Foct. Model 140611) 74-10 D3910 (Foct. Model 140611) 74-10 D4142A . 200-12 D4142A . 142-14 D4320 . 227-13 D43208 . 247-13 D43208 . 247-13 D4320 (Foctory No. 5C12) 26-28 D4730 (Foctory 26C19-61) 7-28 D4813 (Foct. No. 25C22-82) 47-23 D4832 (Foct. No. 25C22-82) 47-23 D4823 (Foct. No. 25C22-82) 47-23 D4843 (Foct. No. 25C22-82) 47-23 D4844 (Foct. No. 25C22-82
G-100 (See Model G-136-Set 24-27) 26-25) G-7205 H-411 47-23 H-521 (See Model G-521-Set 28-33) H-622 44-24 H-727 (See Model G-725-Set 34-23) •TV-1776, TV-1777, TV-1778, TV-1778, TV-1776, TV-1776	TRELA HW301 14-28 TRUETONE D1034A, B, C (See Model D1046A	D38401 - 49-26 D39101 (Foct. Model 140611) D412A - 420-12 D412A - 421-14 D4320 - 4227-13 D4300 - 227-13 D4300 - 227-13 D4300 - 227-13 D4300 - 227-13 D4301 Foctory No. 5C12 D4301 Foctory No. 5C12 D4318 (Foctory No. 5C12, 26-28 D4318 (Foctory No. 5C22, 42, 47-25 D4823 (Foctory No. 26C21-81) D210088A - 105-11 2D10088A - 105-11 2D10089A - 113-10 2D10089A - 113-10 2D10089A - 136-14 2D10093A, 201094A - 113-10 2D10095 - 34-11
G-100 (See Model G-136-Set 24-27) 26-25) G-7205 H-411	TRELA HW301 14-28 TRUETONE D1034A, B. C (See Model D1046A -Set 102-15) D1046B, C, D (See Model D1046A -Set 102-15) D1046B, C, D (See Model D1046A -Set 102-15) D1044B, C, D (See Model D1046A -Set 102-15) D102(Similor to Chossis) D1092 (Similor to Chossis) 108-7 D1240A 187-12 D1433A D1436A 239-12	D3840 49-26 D3910 (Foct. Model 140611) D412A 142-14 D4132A 142-14 D4320 227-13 D4321A 142-14 D4320 227-13 D4321A 227-13 D4320B 247-13 D4321A 224-16 D4301G (Factory, No. 5C12 D4301G (Factory, 26C21-81) D4301G (Factory, 26C21-81) D210888 105-11 2D10888 145-14 2D1089A 13-10 2D1089A 136-14 2D1099A 136-14 2D1095 136-11 2D1095 136-11 2D1095 136-11 2D1095 136-11
G-106 (See Model G-116Set 26-25) G-7205 (See Model G-722Set 24) H-11 (A-72) H-21 (See Model G-521-Set 28) -33 (See Model G-521-Set 28) -33 (See Model G-725-Set 34) H-727 (See Model G-725-Set 34) -779 (See 16) TEMPOTONE 500 E Series 500 E Series 2-8 TEMPLETONE (See Temple) THORDARSON THORDARSON	TRELA HW301 14-28 TRUETONE D1034A, B, C (See Model D1046A -Set 102-15) D1046A D1046B, C, D (See Model D1046A -Set 102-15) D1046B, C, D (See Model D1046A -Set 102-15) D1092 (Similar to Chassis) D1234A, B 189-15 D1240A, B 187-12 D1435A, D1436A 239-10 D1412 28-30	D3840 49-26 D3910 (Foct. Model 140611) D412A 142-14 D4132A 142-14 D4320 227-13 D4321A 142-14 D4320 227-13 D4321A 227-13 D4320B 247-13 D4321A 224-16 D4301G (Factory, No. 5C12 D4301G (Factory, 26C21-81) D4301G (Factory, 26C21-81) D210888 105-11 2D10888 145-14 2D1089A 13-10 2D1089A 136-14 2D1099A 136-14 2D1095 136-11 2D1095 136-11 2D1095 136-11 2D1095 136-11
G-106 (See Model G-116Set 26-25) G-7205 (See Model G-722Set 24) H-11 (A-72) H-21 (See Model G-521-Set 28) -33 (See Model G-521-Set 28) -33 (See Model G-725-Set 34) H-727 (See Model G-725-Set 34) -779 (See 16) TEMPOTONE 500 E Series 500 E Series 2-8 TEMPLETONE (See Temple) THORDARSON THORDARSON	TRELA HW301 14-28 TRUETONE D1034A, B, C (See Model D1046A -Set 102-15) D1046A D1046B, C, D (See Model D1046A -Set 102-15) D1046B, C, D (See Model D1046A -Set 102-15) D1092 (Similar to Chassis) D1234A, B 189-15 D1240A, B 187-12 D1435A, D1436A 239-10 D1412 28-30	D3840 49-26 D3910 (Foct. Model 140611) D412A 200-12 D4142A 142-14 D4320 227-13 D4320 247-13 D4320 247-13 D4320 247-13 D4320 6 D4730 (Factory No. 5C12) D4812 (Factory 26C19-61) D4812 (Fact. No. 25C22-82) D4832 (Fact. No. 25C22-82) D1088A 105-11 D1088B 145-14 D101089A 136-14 D10093A 20104A 19-12 D1095 136-14 D201095 136-14 D201095 136-14 D201095 136-14 D2011856 54-13
G-100 (See Model G-136-Set 26-25) 26-25) G-720-Set 24-27) H-411	TRELA HW301 14–28 TRUETONE D1034A, B, C (See Model D1046A —Set 102-15) D1046A D1046B, C, D (See Model D1046A —Set 102-15) D1046B, C, D (See Model D1046A —Set 102-15) D10405 (Similar to Chassis) D10340, B, D1336A D10435A, D1336A D1044 D102 D1045A D12405 D12405 D12405 D12405 D12406 B7-12 D135 D1641 12-30 D1644 12-30 D1645 (Factory 766-50) D1642 (Factory 701-14) 32-72 D152 (Factory 701-14) 32-72	D3840 49-26 D3910 (Foct. Model 140611) D4142A 142-14 D4320 227-15 D4320 226-28 D4730 (Factory xo. 5C12) D4818 (Factory xo. 5C2) D4818 Foct. No. 25C22-82 D4832 (Fact. No. 25C2)-81 D4888 105-11 D10888 105-11 D2010898 105-11 D2010898 136-14 D201099 136-14 D201098 136-14 D201098 136-14 D201098 136-14 D201095 134-11 D201856 154-13 D2011858 154-13 D2011858 <td< td=""></td<>
G-100 (See Model G-136-Set 26-25) 26-25) G-720-Set 24-27) H-411	TRELA HW301 14–28 TRUETONE D1034A, B, C (See Model D1046A —Set 102-15) D1046A D10404, C, D (See Model D1046A —Set 102-15) D1046B, C, D (See Model D1046A —Set 102-15) D10405, C, D (See Model D1046A —Set 102-15) D10404 D1070 (Similar to Chassis) 108–7 D1020 (Similar to Chassis) 108–7 D1240A 12435A, D1436A 239–10 D1641 28–34 D1644 12-30 D1645 (Factory 76476-650) G-33 D1445 (Factory 7001-14) 34–25 D1835 (Factory Model 25A86-854) 44–25	D3840 49-26 D3910 (Foct. Model 140611) D412A 200-12 D4142A 142-14 D4320 227-13 D4320 227-13 D4320 227-13 D4320 227-13 D4320 227-13 D4320 627-13 D4320 727-13 D4320 727-13 D4320 727-13 D4320 727-13 D4320 726-28 D4730 (Factory 26C19-61) D4818 17-13 D4832 (Fact. No. 25C22-82) D4832 (Fact. No. 26C2-82) D20108
G-106 (See Model G-116Set 26-25) G-7205 (See Model G-722Set 24) H-11 (A-72) H-21 (See Model G-521-Set 28) -33 (See Model G-521-Set 28) -33 (See Model G-725-Set 34) H-727 (See Model G-725-Set 34) -779 (See 16) TEMPOTONE 500 E Series 500 E Series 2-8 TEMPLETONE (See Temple) THORDARSON THORDARSON	Image Image TRUETONE D1034A, B. C (See Model D1046A —Sei 102-15) D1046B, C, O (See Model D1046A —Sei 102-15) D1046B, C, O (See Model D1046A —Sei 102-15) 01046B, C, O (See Model D1046A —Sei 102-15) D1046B, C, O (See Model D1046A —Sei 102-15) 01046B, C, O (See Model D1046A —Sei 102-15) D182-15 D1240A 01092 (Similor to Chossis) 108—7 D1234A, B 187-12 D1435A, D1436A 01641 28-30 D1645 (Factory 26A76-650) 01747 D1748 32-27 D1732 (Factory 7901-14) 01835 D1836 (Factory 26A76-650)	D3840 49-26 D3910 (Foct. Model 140611) D412A 200-12 D412A 142-14 D4320 227-13 D4320 227-22 D4300 (Factory, No. 5C12 D4318 (Factory, No. 5C12 D4318 (Factory, No. 5C22-82) D4318 (Factor, No. 26C21-81) D4318 (Factor, No. 26C21-81) D210888 105-11 2D10888 105-11 2D10888 136-14 2D10980 136-14 2D10980 136-14 2D1095 134-11 2D10885 136-14 2D1095 134-11 2D1085 134-11 2D1085 134-11 2D1085 134-13 2D1185C 0 (Sec 84 3-Set 177-1

TRUETONE-Cont.	
• 2D1230C, D, E (See PCB 243-1 and Model 2D12	98—Set
243-1 and Model 2D12 185-14)	305361
185-14) • 2D1230B (Also see PCB 193-1) • 2D1235A (Ch. 17MS34S) . • 2D1235B, C, D, E (See PCE 215-1 and Model 2D12 188-13)	59Set . 185-14
•201235A (Ch. 17MS34S) .	188-13
215-1 and Model 2D12	35A—Set
188-13) •2D1303A	207-11
188-13) 2D1303A 2D1315A 2D1315A 2D1325A 2D1326A 2D1230B 2D1	204-11
©2D1316A ©2D1325A	.224-17
• 2D1326A	.224-17
and Model 2D1230B-	Set 185-
14) •201331A B	233-11
•2D1331A, B •2D1331C, D (See Model 2C Set 233-11)	1331A-
• 2D1336A	.238-14
Ser 233-11) • 2D1336A • 2D1336A • 2D1354A • 2D1352A • 2D1352A • 2D1353A (Series A Thru M • 2D1358A • 2D1358A • 2D1359A (Series A, C	210-13
•2D1353A (Series A Thru M	244-12
•2D1354A (Ch. 9210P) •2D1358A	242-10
•2D1359A (Series A, C	D, E)
 2D1358A 2D1359A (Series A, C 2D1415A (Ch. 21T16) 2D1416A (Ch. 21T16A) 2D1426A (Ch. 21T16A) 2D1420A (See PCE 98–5 ond Model 2D12308–14) 	249-19
 2D1416A (Ch. 21T16A) 2D1426A (Ch. 21T16A) 	.249-19 249-19
• 2D1430A (See PCB 98	Set 243-1
and Model 2012308-	Set 183-
• 2D1430B [See Model 2D14	(30A)
• 2D1430B [See Model 2D14 • 2D1430C • 2D1431A • 2D1431A	.261-15 .161-10
• 2D2043A • 2D2047B	161-10 161-10
• 202052	.134-11
•202149A (Ch. 17AY212)	177-14
•2D2152A (Ch. 17AY26) .	·· •
• 2D2219A	.179-13
 2D2223A (Ch. 21AY21A) 2D2301A, 2D2302A 	229-17
• 2D2312A	204-11
•2D2313C (Ch. 17T5)	249-19
• 2D2314A	204-11
• 2D2321A	204-11
• 2D2322A, B • 2D2333A, B	203-14
2D1431C 2D1431A 2D2043A 2D2043A 2D2047B 2D2052 2D2052 2D2149A (Ch. 17AY22) 2D2149A (Ch. 17AY22) 2D215A (Ch. 17AY22) 2D215A (Ch. 21AY21A) 2D2215A (Ch. 21AY21A) 2D2201A (Ch. 21AY21A) 2D2201A (Ch. 17T5) 2D2214A 2D2214A 2D2214A 2D2214A 2D2214A 2D2214A 2D2231A 2D2234A 2D234A 2D2234A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D244A 2D24A	.233-11
• 2D2414A (Ch. 21114)	
• 2D2422A (Ch. 17T8)	249-19
• 2D24228 (Ch. 17T4) • 2D2433A (See PCB 98- and Model 2D12308-	Set 243-1
and Model 2D1230B- 14)	Set 185-
3D6000 Tel. UHF Conv	.221-12
TURNER	
TV-3 Tel. UHF Conv	.231-17
ULTRADYNE	
L-46	4-21
ULTRATONE	
	253-14
400	
400 UNITED MOTORS SERV Delco or Suick, Cadillo	ICE (See
400 UNITED MOTORS SERV Delco or Buick, Cadillo rolet, Oldşmobile and	ICE (See
400 UNITED MOTORS SERV Delco or Suick, Cadillo rolet, Oldşmobile and U. S. TELEVISION	ICE (See ic, Chev- Pontiac)
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400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 110030 110030 State, SB16, SC16 (Sec SC66—Set 17-9) SA66, SB66, SC66, SC66 Early 8-16M (Dumbarton) UNITONE 88	File See ac, Chev- Pontiac) .99A-12 .99A-12 .89-15 .99A-12 .99A-12 .99A-12 .99A-12 .90A-12 .90A-12 .9
400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early 8-164 (Jumbarton) UNITONE	File See ac, Chev- Pontiac) 99A-12 .99A-12 .89-15 .99A-12 .99A-12 <t< td=""></t<>
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400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10923 116030 SA16, SB16, SC16 SC66-Set 17-9 SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Record Changer V-M (Also see	IICE (See
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 199A-1
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (SC SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10923 T10931 SA16, SB16, SC16 (St SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer Listin 10 555-M, -O 972 975 980 985 986	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 110031 SA16, SB16, SC16 (S SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-10M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin	(ICE (See ac, Chev- 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 89-15 99A-12 199A-12
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10923 T10923 T10923 T10923 SA16, SB16, SC16 (St SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer 121 130 131 130 131 131 130 131 130 131 130 131 130 131 130 131 131	ICE (See ic, Chev- Pontaio 99A-12 99A-12 89-15 99A-12 89A-12 99A-12 e Model 5066MPA 24-30 . 17-9 . 26-29 . 5-26 Listing) 99 .191-19 .242-11 .139-15 .213-9 .231-20 .139-15 .213-9 .231-20 .139-15 .213-9 .231-20 .139-15 .213-9 .231-20 .139-15 .231-20 .139-15 .235-16 .138-12
400 UNITED MOTORS SERV Delco or Buick, Catille rolet, Oldşmobile and U. S. TELEVISION C16030 T10923 T10923 T10923 SA16, SB16, SC16 (S SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH 100 121 150 151 160 555-M, -0 972 975 980 985 986 990 101-A VAN-CAMP S76-1-6A	rICE (See ray CE (See 99A-12 99A-12 99A-12 89A-12 89A-12 89A-12 89A-12 99A-12 101-19 242-11 103-15 138-12 136-16 136-16 136-16 136-16 140-34 10-34
400 UNITED MOTORS SERV Delco or Buick, Catille rolet, Oldşmobile and U. S. TELEVISION C (16030 T 10931 T 10931 State, SB16, SC16 (Sc SC66—Set 17-9) SA66, SB66, SC66, SC66 Early B 16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Record Changer Listin 10 10 110 110 10 10 10 10 10	rICE (See ray CE (See ray Chev-Pontiac) 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 e Model 17-9 24-30 24-20 Listing) g) .191-19 .242-11 .39-15 .213-9 .231-9 .313-9 .159-15 .203-15 .165-16 .165-16 .165-16 .247-14 .248-11 .10-34
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 SA16, SB16, SC16 (St SC66-Serl 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer Listin 10 10 10 15 150 150 150 150 15	rICE (See ray CE (See ray Chev-Pontiac) 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 e Model 17-9 24-30 24-20 Listing) g) .191-19 .242-11 .39-15 .213-9 .231-9 .313-9 .159-15 .203-15 .165-16 .165-16 .165-16 .247-14 .248-11 .10-34
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10923 T10923 T10923 SA16, SB16, SC16 (S SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin 10 121 150 151 160 S55-M, -O 972 973 985 976 985 976 976-16A VIDEO CORP. OF AME (See Videola) VIDEO DYNE	'ICE (See ic, Chev- 99A-12 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 e Model 17-9 24-20 5-26 Listing) g)
400 UNITED MOTORS SERV Delco or Buick, Call rolet, Oldşmobile and U. S. TELEVISION C16030 110023 114030 SA16, SB16, SC16 (S SC66-Set 17-9) SA66, SB66, SC66, SC66 Early 816M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin 110 121 150 151 160 S55-M, -O 972 973 983 983 986 990 101-A VAN-CAMP S76-1-6A VIDEO CORP. OF AME (See Videola) VIDEO LIST, IZIV	'ICE (See ic, Chev- 99A-12 99A-12 99A-12 99A-12 99A-12 89-15 99A-12 e Model 17-9 24-20 5-26 Listing) g)
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10923 T10931 SA16, SB16, SC16 (St SC66-Set 17-9) SA66, SB66, SC66, SC66 Early S16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH (See Record Changer S55.M, -O S55.M, -O S55.M, -O S55.M, -O S75 980 985 990 1001-A VAN-CAMP 576-1-6A VIDEO CORP., OF AME (See Videola) VIDEODYNE *1074, 12174, 12174	'ICE (See ic, Chev- 99A-12 179 24-20 5-26 Listing) g) 191-19 242-11 242-21 213-20 213-20 213-20 135-16 138-12 136-16 247-14 248-11 10-34 7-29 'RICA
400 UNITED MOTORS SERV. Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10923 T10931 SA16, SB16, SC16 (St SC66-Set 17-9) SA66, SB66, SC66, SC66 Early S16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH (See Record Changer UTAH (See Record Changer S55.M, -O S55.M, -O S55.M, -O S55.M, -O S75 980 985 990 1001-A VAN-CAMP 576-1-6A VIDEO CORP., OF AME (See Videola) VIDEODYNE *1074, 12174, 12174	'ICE (See ic, Chev- 99A-12 179 24-20 5-26 Listing) g) 191-19 242-11 242-21 213-20 213-20 213-20 135-16 138-12 136-16 247-14 248-11 10-34 7-29 'RICA
400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 116030 SA16, SB16, SC16 (S SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer Listin 10 10 10 10 10 10 10 10 10 10	'ICE (See ic, Chev- 99A-12 179 24-20 5-26 Listing) g) 191-19 242-11 242-21 213-20 213-20 213-20 135-16 138-12 136-16 247-14 248-11 10-34 7-29 'RICA
400 UNITED MOTORS SERV Delco or Buick, Catille rolet, Oldşmobile and U. S. TELEVISION C16030 T10023 T10023 T10023 SA16, SB16, SC16 (S. SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin 10 121 150 S50 S75 985 985 986 986 986 986 986 986 986 986	'ICE (See ic, Chev- 99A-12 179 24-20 5-26 Listing) g) 191-19 242-11 242-21 213-20 213-20 213-20 135-16 138-12 136-16 247-14 248-11 10-34 7-29 'RICA
400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10933 T16030 SA16, SB16, SC16 (Sc SC66-Serl 7-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer Listin 10 10 10 10 10 10 10 10 10 10	(ICE (See (a; Chev-Pontiac) 99A-12 99A-12 99A-12 89-15 99A-12 91 17-9 Listing) 91 191-19 -242-11 -31-20 -31-20 -31-3 -35-13 -35-13 -35-14 -248-11 -34-14 -248-11 -34 -7-29 (RICA -92-9 'Y 'Y 'Y<
400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10933 T16030 SA16, SB16, SC16 (Sc SC66-Serl 7-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer Listin 10 10 10 10 10 10 10 10 10 10	(ICE (See (a; Chev-Pontiac) 99A-12 99A-12 99A-12 89-15 99A-12 91 17-9 Listing) 91 191-19 -242-11 -31-20 -31-20 -31-3 -35-13 -35-13 -35-14 -248-11 -34-14 -248-11 -34 -7-29 (RICA -92-9 'Y 'Y 'Y<
400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10933 T16030 SA16, SB16, SC16 (Sc SC66-Serl 7-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer Listin 10 10 10 10 10 10 10 10 10 10	(ICE (See (a; Chev-Pontiac) 99A-12 99A-12 99A-12 89-15 99A-12 91 17-9 139-13 139-15 131-20 131-20 131-20 138-12 145-16 145-16 145-16 145-16 145-16 145-16 145-16 146-16 146-16 146-16 146-16 146-16 14
400 UNITED MOTORS SERV Delco or Buick, Call rolet, Oldşmobile and U. S. TELEVISION C16030 T10023 T10023 T10031 SA16, SB16, SC16 (S. SC66-Set 17-9) SA66, SB66, SC66, SC66 Early B16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Record Changer UTAH (See Record Changer Listin 10 121 150 151 160 S55-M, -O 972 973 985 986 976 100-A VIDEO CORP. OF AME (See Videola) VIDEOLA SV5-165, VS-167 VIDEO PRODUCTS	(ICE (See (a; Chev-Pontiac) 99A-12 99A-12 99A-12 89-15 99A-12 91 17-9 139-13 139-15 131-20 131-20 131-20 138-12 145-16 145-16 145-16 145-16 145-16 145-16 145-16 146-16 146-16 146-16 146-16 146-16 14
400 UNITED MOTORS SERV Delco or Buick, Cadille rolet, Oldşmobile and U. S. TELEVISION C16030 T10931 T10931 T1093 T1093 SA16, SB16, SC16 (Sc SC66-Serl 7-9) SA66, SB66, SC66, SC66 Early B-16M (Dumbarton) UNITONE 88 UNIVERSAL CAMERA (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer UTAH (See Recard Changer UTAH S55-M, -O 972 975 980 985 986 990 1001-A VAN-CAMP S75-1-6A VIDEO PRODUCTS (Also SEA PRODUCTS (Also SEA STACA See Recard Changer Second Changer STA S55-1-6A VIDEO CORP, OF AME (See Videola) VIDEOPROBUCTS (Also SEA STACA STACA STACA SEA STACA SEA STACA SEA STACA SEA STACA SEA SEA SEA SEA SEA SEA SEA SE	(ICE (See (a; Chev-Pontiac) 99A-12 99A-12 99A-12 89-15 99A-12 91 17-9 139-13 139-15 131-20 131-20 131-20 138-12 145-16 145-16 145-16 145-16 145-16 145-16 145-16 146-16 146-16 146-16 146-16 146-16 14

NOTE: PCB Denotes Production Change Bulletin. Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. • Denotes Television Receiver.

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VIEWTONE-WESTINGHOUSE

VIEWTONE—WESTINGHO	USE
VIEWTONE	v
RC-201A, RRC-201 11-32 VISION MASTER	н
•14MC, MT (Similar to Chassis) 117-8 •16MC, 16MT, 16MXC, 16MXCS,	Ĥ
	H
 isis)	н
17MXT, 17MXTS (Similar to Chas- sis)	Н
VIZ	Н
RS-1 14-31 VOCATRON	H
CC-20 (D)	н
VOGUE	н
532 A-P 11-33 Ch. Models 533R, 554R 8-32	н
WALSCO 2000 (Tel. UHF Conv.) 261-16	н
WARWICK (See Clarion)	н
WATTERSON	н
ARC-4591A	Н
4581	Ĥ
4782	H e H
4800 43-23 WAVEFORMS	eH eH
A-20 C-5 191–20 191–20	н
WEBCOR	H
(See Webster-Chicago) WEBSTER-CHICAGO (Also see	H
Changer and Recorder Listings)	•H
B-123-1 204-12	
	●H
B-136-1 D-300-1	н
F-123-1	H
F-123.1 204-12 F-134-1 205-12 F-136-1 207-12 F-136-1 207-12 66-1A 34-26	۰H
100-608	• H
130	•H
166	H H
288 117-14 333-1, 333-2 250-22 362 105-12	• H
333-1, 333-2 362 760 112-12 762 105-12 105-12	• H
1024 (See Model B-124-1-Set 203-16)	• H
1034 (See Model B-134-1-Set 205-12) 1035 (See Model B-135-1-Set	
1035 (See Model B-135-1—Set 210-14) 1036 (See Model B-136-1—Set 207-12)	e H
	н
WEBSTER ELECTRIC (Also see Recorder Listing)	н
RFM-1, -2, -3 263-17 81-15, 81-15A 142-15 82-25, 82-25A, 83-25 143-15 84-25 145-12 85 25 145-12	н н
	н
605M, S, 606M, S	н
1105M	н
WEBSTER (Telehome) W606M	"
W606M 56-24 604M 57-23 WELLS-GARDNER	н
WG-30A8-A-496 246-12	H
• 317GS34C-218 (Also See PCB 84- Set 225-1)	н
317GS34C-220 (Alto See PC8 84 -	н
■ 317GS34C-220 (Also See PCB 84	н
■ 317GS34C-220 (Also See PCB 84	
■ 317GS34C-220 (Also See PCB 84	н
■ 317GS34C-220 (Also See PCB 84	н
■ 317GS34C-220 (Also See PCB 84	
■17/65346.220 (Alio See PC6 84 Set 225.1] Alio See PC6 84 Set 225.1] Alio See PC8 84 Set 225.1] 2017 (S546.278 (Alio See PC8 84 Set 235.1] 2017 (S76 194 3214/531C.222, 2274, 2776 194 3214/531C.280, 282, 284 194 3214/531C.280, 282, 284 194 3214/531C.280, 282, 284 194 3214/530.376 1 226 3214/530.376 1 226 3214/530.376 226 3214/530.376 226 3214/530.376 226 3214/530.376 226 3214/530.376 226 3214/530.376 226 32214/530.376 226 32214/530.376 226 3214/530.376 226 3214/530 3214/5	H H
■17/65346.220 (Alto See PC8 84- Set 2251)	H H H
■17/65346.220 (Alio See PC6 84 Set 225.1) (Alio See PC6 84 Set 225.1) (Alio See PC6 84 Set 225.1) (See PC6 84 Set 235.1) (See PC6 84 Set 235.1) (See PC6 84 Set 235.1) (See PC6 84 Set 235.1) (See PC6 84 See PC6 84	H H H H H
■17/65346.220 (Alio See PC6 84- Set 2251)	H H H H H H
■17/65346.220 (Alio See PC6 84 Set 225.1) Alio See PC6 84 195-12 (S5346.278) (Alio See PC6 194 195-12 (S5346.278) (Alio See PC6 194 1321 (S536.278) (Alio See PC6 194 WESTERN AUTO (See Truetone) WESTINGHOUSE (Alio See Record Changer Listing) H-104, H-105	H H H H H H H
■17/65346.220 (Alio See PC6 84 Set 225.1) Alio See PC6 84 195-12 (S5346.278) (Alio See PC6 194 195-12 (S5346.278) (Alio See PC6 194 1321 (S536.278) (Alio See PC6 194 WESTERN AUTO (See Truetone) WESTINGHOUSE (Alio See Record Changer Listing) H-104, H-105	
■17/65346.220 (Alio See PC6 84 Set 225.1]	
■17/65346.220 (Alio See PC6 84- Set 22:51)	
■17/G534C-220 (Alio See PC6 84 Set 22-1)	H H H H H
■17/G534C-220 (Alio See PC6 8A Set 225-1)	H H H H H H H H H H H H H H H H H H H

2	WESTINGHOUSE-Cont.	WESTINGHOUSE-Cont.
1	H-148A (See Model H-148—Set 15- 37) H-153, H-153A (Ch. V-2103) 35-25	H-355T5, H-356T5 (Ch. V-2157-5) 161-11 H-357C10 (Ch. V-2180-5), 161-12 H-3575 H-340T6 (Ch. V-2180-5), 161-12
s) 8	H-153, H-153A (Ch. V-2103) 35 –25 H-154 (See Set 21-36 and Model H-104—Set 4 -11)	
-	H-155	191–21 H-361T6 (Ch. V-2181-1). 186–15 H-365T5, H-366T5 (Ch. V-2157-7)
8	25) H-157 (Ch. V-2122) 33-31 H-161 (Ch. V-2118) 34-27 H-162 (See Model H-117—Set 11-	185-15 H-367T5 (Ch. V-2157-8). 189-17 H-368P5, H-369P5 (Ch. V-2156-1U)
8	34)	(See Model H-342P30—Ser 138- 13)
1	H-164 (Ch. V-2119-1) 36-28 H-165	H-37017, H-37117 (Ch. V-2180-8) 186-16 H-372P4, H-373P4, Ch. V-2182-1 H-372P4, H-373P4, Ch. V-2182-1
	H-166, H-167 36-28 H-168, H-168A, H-168B (Ch. V- 2118) 34-27 H-168B (Ch. V-2118) (See Model H-168-Ser 34-27) H-169 (Ch. V-2124-1) 37-24	and H-377 Oprional Pwil. Supply
1	H-1688 (Ch. V-2118) (See Model H-168-Set 34-27)	H-374T5, H-375T5 (Ch. V-2157-9)
3	H-169 (Ch. V-2124-1) 37–24 H-171 (Ch. V-2103) 35–25 H-171A, C (Ch. V-2103) (See Model	H-376P4 (Ch. V-2182-1 and H-377 Optianal Power Supply). 188-:4
2	H-153-Set 33-25}	H-377 (Power Supply) (See Set 188-14 or Set 233-12) H-37815, H-37915, H-38015, H- 38115 (Ch. V-2184-1), 211-17
6	H-182 {Ch. V-2128, V-2128-11	H-38215, H-38315 (Ch. V-2157-10)
	53-25 H-183, H-183A 48-26 H-184 (See Model H-153-Set 35- 25)	215-14 H-384T5 (Ch. V-2157-10) (See Model H-382T5-Set 215-14) H-385T5, H-386T5 (Ch. V-2157-11)
6	H-185 (Ch. V-2131, V-2131-1) 54-20	H-385T5, H-386T5 (Ch. V-2157-11)
2 5 2	H-186M, H-187 (Ch. V-2132) 60-21 H-188 (Ch. V-2133) 51-25 H-190, H-191, H-191A (Ch. V-2134) 69-23	204-13 H-387T5 (Ch. V-2157-11) [See Model H-385T5-Set 204-13] H-388T5 (Ch. V-2157-12).215-15 H-391T5, H-392T5 (Ch. V-2157-14)
4	H-190, H-191, H-191A (Ch. V-2134)	
4	 H-196 K-17 H-196A (Ch. V-2130-1) (See Model H-196—Set 65-17) H-196A (DX) (Ch. V. 2130, 110X, 	231-19 H-393T6 (Ch. V-2181-2). 210-15 H-397T5, H-398T5 (Ch. V-2184-2)
	UN-170A (DA) (Ch. V-2130-11DA OF	232-10
0	V-2130-12DX) 84-13 H-198 (Ch. V-2137-2) 73-15 H-199 (Ch. V-2137-1) 69-16 H-202 (Ch. V-2182-2) 50-22	H-400P4, H-401P4, H-402P4, H- 403P4 (Ch. V-2164-2). 205-13 H-405T5 (Ch. V-2157-14) (See Model H-391T5-Set 231-19)
	H-203 [CH. V-2137] 02-21	H-409P4, H-410P4, H-411P4 (Ch. V-2185-1 and H-377 Optional
e	H-204 50-22 H-207A (Ch. V-2130-1, V-2137)	Power Supply]
2	 H-207A (DX) (Ch. V-2130-11DX or V-2130-12DX and Radio Ch. 	257-19 H-417T5, H-418T5 (Ch. V2186-1) 239-11
6	V-2137)	H.422PA H.423PA H.424PA
4	V-2137)	H-425P4 (Ch. V-2188-1) 245-11 H-451T5 H-452T5, H-453T5, H-454T5 (Ch. V-2184-1) (See Model H-378T5-Set 211-17) H 461P4 H-462P4 H-463P4
6 2 2	H-212 (Ch. V-2137) 61-20	H-461P4, H-462P4, H-463P4, H-464P4 (Ch. V-2182-2). 257–19 H-479P4 (Ch. V-2182-2)257–19
2	H-214, H-214A (Ch. V-2103-3)	H-479P4 (Ch. V-2182-2)257-19 •H-600T16 (Ch. V-2150-61, A, B) 98-14
6 4	75-16 H-216, H-216A (Ch. V-2146-05, V-2146-45, V-2149-1)97A-14 H-217, A (Ch. V-2140-110X, V- 2137, V-2149) (See Set 99A-14 and Model H-217B-Set 91-14) H-2178 (Ch. V-2142 220X V-2127	●H-601K12, H-602K12 [Ch. V-2150-
3	2137, V-2149) (See Set 99A-14 and Model H-217B—Set 91-14) •H-217B (Ch. V-2146-35DX, V-2137,	•H-603C12 (Ch. V-2152-01 and V- 2149-3) 100-14
3	V-2149} 91-14	 H-604T10, A (Ch. V-2150-91A, -94, -94A) (See Set 99A-14 and Model H-609T10—Set 95-7)
342	H-220 H-223 (Ch. V-2150-01, V-2150-02) 	●H-605T12 (Ch. V-2150-101) 97-19 ●H-606K12 (Ch. V-2150-111, A)
2	•H-225 (DX) (Ch. V-2130-31DX or V-2130-32DX) 84-17 •H-226 (Ch. V-2146-21DX, -25DX,	•H-607K12 (Ch. V-2150-111, A) 120-12
2	V-2149) (See Model H-217B-Set 91-14)	 H-608C12 (Ch. V-2152-01, V-2149- 3) (See Model H-603C-12—Set
1	 H-231 (Ch. V-2150-51 and V-2137- 3 or V-2137-35, V-2149-2) 994-14 	100-14) •H-609T10 (Ch. V-2150-94C) 957 •H-610T12 (Ch. V-2150-136) 105-13
1	97A-14 H-242 (Ch. V-2150-31) 97A-14 H-251 (Ch. V-2150-81, -82, -84) (See 99A-14 and Model H-609T10 - Set 95 71	100-14) H-60710 (Ch. V-2150-94C) 95-7 H-610710 (Ch. V-2150-136) 105-13 H-611C12 (Ch. V-2150-136) 105-13 H-611C12 (Ch. V-2152-16) 112-14 H-613K16 (Ch. V-2150-146) 107-12 H-614712 (Ch. V-2150-136) 105-13 H-615C12 (Ch. V-2152-16) 112-14 H-617112 (Ch. V-2150-176, U, -177U) (Also see PCB 10-5et 116-11 2013 (Ch. V-2150-176, U, -1700 (Ch. V-2150) (Ch. V-2150-176, U, -1700 (Ch. V-2150-176, U, -170
		H-614T12 (Ch. V-2150-136) 105-13 H-615C12 (Ch. V-2152-16) 112-14 H-617T12 (Ch. V-2150-176 II
	H-302P5 (Ch. V-2151-1) 91-15	-177U) (Also see PCB 10-Set 116-1) 103-17
5	H-303P4, H-304P4 (Ch. V2153) 89-16 H-307T7, H-308T7 (Ch. V-21361	H-618T16 (Ch. V-2150-186, A, C, CA} (Also see PCB 10-Set 116-1) 103-17
2	H-309P5, H-309P5U (Ch. V-2156)	 H-619T12, U (Ch. V-2150-176, U, -177U) (Also see PCB 10—Set
778	101-16 H-310T5, H-310T5U, H-311T5, H- 311T5U (Ch. V-2161, V-2161U)	116-1) 103-17 •H-620K16 (Ch. V-2150-186, A, C, CA) (Also see PCB 10-Set 116-1)
ŏ	H-312P4, H-312P4U, H-313P4, H-	103-17
4	313P4U, H-314P4, H-314P4U, H-315P4, H-315P4U (Ch. V- 2153 I)	CA) (See PCB 10—Set 116-1 and Model H-617112—Set 103-17)
	H-316C7 [Ch. V-2136-1]. 112-13 H-317C7 (Ch. V-2136-1] [See Model H-316C7-Set 112-13]	●H-625T12 (Ch. V-2150-197) 114-11 ●H-626T16 (Ch. V-2172)116-13 ●H-627K16 (Ch. V-2171)116-13
2	H-316C7—Set 112-13) H-318T5, U (Ch. V-2157, U) 117–15	H-628K16, H-629K16 (Ch. V-2171) 116-13
2	H-32015, U (Ch. V-2157, U)	H-628K16, H-629K16 [Ch. V.2171] 116–13 H-630T14 (Ch. V.2176), 116–13 H-633C17, H-634C17 [Ch. V.2173] 122–11 124
2	H-32175, U, H-32275, U (Ch. V-2157-1, U)	H-637114 (Ch. V-2175) 116-13 H-637114 (Ch. V-2177) 116-13
4		
	2)	640T17A (Ch. V-2192, -1, -2, -3, -4, -5, -6) (Also see PCB 28-Set
4	112-13) H-32776U (Ch. V-2157-3U) 126-14 H-328C7 U (Ch. V-2136-4) 137-15	150-1) 133 -15 H -641K17 (Ch. V-2175-1, -5), H- 641K17A (Ch. V-2192, -1, -2, -3, -4, -5, -6) (Also see PCB 28-
	H-328C7, U (Ch. V-2136-4) 137-15 H-331P4, U (Ch. V-2164, U1 (Also see PCB 52-Set 186-11, 171-12	641K1/A (Ch. V-2192, -1, -2, -3, -4, -5, -6) (Also see PCB 28
)	H-332P4 (See Model H-331P4U- Set 171-12)	•H-642K20 [Ch. V-2178-13]
	H-333P4, U {Ch. V-2164, U} /Also see PCB 52—Set 187-1}.171-12 H-334TZU, H-335TZU {Ch. V-2136-	H-642K20A (Ch. V-2194, V-2194A, V-2194-1) 137-16 H-643K16 (Ch. V-2179, V-2179-11 127-13
	5U)	127-13 H-646K17 (Ch. V-2192) 133-15 H-647K17 (Ch. V-2175-3) 133-15 H-647K17 (Ch. V-2175-3) 133-15
,	2157U)	 H-647K17 {Ch. V-2175-3]. 133-15 H-648T20 (Ch. V-2201-1) (Atso see PCB 42—Set 176-1)154-15
•	H-338T5U (Ch. V-2157-4U) 140-13 H-341T5U (Ch. V-2157-4U) 140-13 H-342P5U, H-343P5U (Ch. V-2156-	PCB 42—Set 176-1) 154-15 H-649T17 (Ch. V-2200-1) (Alro see PCB 42—Set 176-1) 154-15
4	10)	et H-639T17 (Ch. V-2192-4) (See Mod- et H-639T17-Set 133-15)
† >	13) H-348P5, H-349P5 (Ch. V-2156-1U)	eH-650K21 (Ch. V-2192-4) (See Mod- el H-639T17-Set 133-15)
5	(See Model H-342P5U-Set 138-	H-650T17 (Ch. V-2200-1) (Also see PCB 42—Set 176-1)154-15 H-651K17 (Ch. V-2192) (See Model
5	13) H-35017, H-351177 (Ch. V-2180-1) (Also see PCB 52—Set 186-1) 154-14	H-639T17—Set 133-15)
	H-354C7 (Ch. V-2180-2)158-13	H-651K17 {Ch. V-2200-1} {A'so see PCB 42Set 176-1}154-15

+ 15-	WE5TINGHOUSE-Cont. H-355T5, H-356T5 (Ch. V-2157-5)	- N
5-25	H-357C10 (Ch. V-2180-5), 161-12	
Nodel	H-35975, H-36075 {Ch. V-2157-6} 191-21 H-36176 (Ch. V-2181-1), 186-15	•
5-25 3 5 -	H-365T5, H-366T5 (Ch. V-2157-7) 185-15	
3-31 4-27	191-21 H-361T6 (Ch. V-2181-1), 186-15 H-365T5, H-366T5 (Ch. V-2157-7), 183-15 H-367T5 (Ch. V-2157-8), 189-17 H-368P5, H-369P5 (Ch. V-2156-10) (See Model H-342P5U—Set 138-	• •
	13) H-370T7, H-371T7 (Ch. V-2180-8)	• F
6-28 2-29 6-28		• eF
4-27 Aodei	and H-377 Optional Pwr. Supply 188–14	•H
7-24 5-25	H-374T5, H-375T5 (Ch. V-2157-9) 189-17 H-376P4 (Ch. V-2182-1 and H-377 Optianal Power Supply), 188-14 H-377 (Power Supply), 188-14	eH
5-25 Nodel	n-37674 [CR, V-2182-1 onto H-377 Optional Power Supply] 188-14 H-377 (Power Supply] 188-14 H-37815, H-37915, H-38015, H- 38115 (Ch, V-2184-11, 211-17 H-38215, H-38315 (Ch, V-2157-10) 215-14 H-38415 (Ch, V-2157-10) [See	•
5-26	188-14 or Set 233-12) H-378T5, H-379T5, H-380T5, H- 381T5 (Ch. V.2184.11, 211-17	•
3-25 8-26	H-382T5, H-383T5 (Ch. V-2157-10) 215-14	•
35- 31-1)		
4~20 0~21	Model H-38275—Set 215-14) H-38575, H-38675 (Ch. V-2157-11) 204-13 H-38775 (Ch. V-2157-11) (See Model H-38375—Set 204-13) H-38875 (Ch. V-2157-12, 215-15 H-39175, Ch. V-2157-12, 215-15 H-39775 (Ch. V-2161-2), 210-15 H-39775 (Ch. V-2161-2), 210-15	eH
1–25 (Ch. 9–23	Model H-385T5-Set 204-13) H-388T5 (Ch. V-2157-12).215-15	• H
9-23 4-20 5-17	H-391T5, H-392T5 (Ch. V-2157-14) H-393T6 (Ch. V-2181-2)210-15 H-397T5, H-398T5 (Ch. V-2184-2) 222-10 H-400P4, H-401P4, H-402P4, H-	-
lodel	H-393T6 (Ch. V-2181-2). 210-15 H-397T5, H-398T5 (Ch. V-2184-2) 232-10	•
X or 4-13	232-10 H-400P4, H-401P4, H-402P4, H- 403P4 (Ch. V-2164-2), 205-13 H-405T5 (Ch. V-2157-14) (See Model H-39175-Set 231-19) H-400P4, H-410P4, H-411P4 (Ch. V-2185-1) and H-377 Optional Reverse Sumptive 233-12	θH
3-15 9-16 0-22	H-405T5 (Ch. V-2157-14) (See Model H-391T5-Set 231-19)	•H
0-22 2-21 0-22	V-2185-1 and H-377 Optional Power Supply)	•
1 37) 5 17	Power Supply)	• H
Ch.	H-41974, H-41374 (ch. V-2102-2) H-41775, H-41875 (ch. V2186-1) H-422P4, H-423P4, H-424P4,	
X or Ch.		• H
4-13 V- 1-20	H-454T5 (Ch. V-2184-1) (See	• H
2 21	Model H-37875—Set 211-17) H-461P4, H-462P4, H-463P4, H-464P4 (Ch. V-2182-2), 257-19 H-479P4 (Ch. V-2182-2), 257-19 H-600T16 (Ch. V-2182-2), 257-19 H-600T16 (Ch. V-2150-61, A, B) 98-14	
03-3) 5-16 5-05,	•H-600716 (Ch. V-2150-61, A, B) 98-14	
-14	41) 98-14	• H
, V- A-14 14) 137, 1–14	•H-603C12 (CR. V-2132-01 and V- 2149-3)	• H
9-23	H-603C12 (Ch. V-2152-01 and V- 2149-3)	
0-02) 8–14 Xor		• H
4–17 5DX,	H-607K12 (Ch. V-2150-11, A) 120-12 H-607K12 (Ch. V-2150-11, A) 120-12	07
-Set	3) (See Model H-603C-12—Set	• H
(9-2)	100-14) H-609T10 (Ch. V-2150-94C) 95-7 H-610T12 (Ch. V-2150-136) 105-13 H-611C12 (Ch. V-2150-16) 112-14 H-613K16 (Ch. V-2150-16) 107-12 H-614T12 (Ch. V-2150-16) 107-13 H-615C12 (Ch. V-2150-176, U, 116-112 (Ch. V-2150-176, U, 117U) (Also see PCB 10-5ct 116-11 103-17	
-14 -84) 9110	H-611C12 (Ch. V-2152-16) 112-14 H-613K16 (Ch. V-2150-146) 107-12	• H
148)	H-614112 (Ch. V-2150-136) 105-13 H-615C12 (Ch. V-2152-16) 112-14 H-617T12 (Ch. V-2150-176 II	• H
8-14 1-15	-177U) (Also see PCB 10-Set 116-1) 103-17	
153) 9–16 1361	 H-618T16 (Ch. V-2150-186, A, C, CA) (Also see PCB 10—Set 116-1) 	• H
0-13	103-17 •H-619T12, U (Ch. V-2150-176, U, -177U) (Also see PCB 10-Set 116-1] •U (2001) (Ch. V2010 2010 - 103-17	
156) 1-16 , H- 61U)	-177U) (Also see PCB 10—Set 116-1) H-620K16 (Ch. V-2150-186, A, C, CA) (Also see PCB 10—Set 116-1)	• H
6101 9–18 H-		•H
P4U, V-	•H-622K16 (Ch. V-2150-186, A, C, CA) (See PCB 10—Set 116-1 and Model H-617T12—Set 103-17)	
8-13 2-13 lodel	Model H-61/112	•H
UI	H-628K16, H-629K16 (Ch. V-2171) 116-13 116-13	• H
7-15 U) 7-15	H-6228K16, H-629K16 (Ch. V-2171) H-628K16, H-629K16 (Ch. V-2171) 116-13 H-630T14 (Ch. V-2176) 116-13 H-633C17, H-634C17 (Ch. V-2173) 122-11 122-11	
(Ch. 7-15	H-636T17 (Ch. V-2175) 116-13	●H
U1 7-15	H-638K20 (Ch. V-2178) 129-13 H-639T17 (Ch. V-2192, -1) 133-15	●H
136- 3-13 Set	H-640T17 (Ch. V-2175-3, -41, H- 640T17A (Ch. V-2192, -1, -2, -3,	
5-14	H-633C17, H-634C17 (Ch. V-2173) H-633C17, H-634C17 (Ch. V-2173) 122-11 H-636117 (Ch. V-2175). 116-13 H-638714 (Ch. V-2177). 116-13 H-638710 (Ch. V-2178). 129-13 H-6397117 (Ch. V-2178). 129-13 H-640717 (Ch. V-2178). 133-15 H-640717 (Ch. V-2192, -1, -2, -3, -4, -5, -6) (Also tee PCB 28—Set 150-1). 133-15 H-641K17 (Ch. V-2192, -1, -2, -3, -3, -4, -5, -6) (Also tee PCB 28- Set 150-1). 133-15 H-641K17 (Ch. V-2192, -1, -2, -3, -3, -5, -6) (Also tee PCB 28- Set 150-1). 133-15 H-642820 (Ch. V-2178)3 H-642820 (Ch. V-2178)3 H-742820 (Ch. V-2178)3 H-7428200 (Ch.	•н •н
Also	641K17A (Ch. V-2192, -1, -2, -3, -4, -5, -6) (Also see PCB 28- Set 150-1)	
1-12 IU-	en outre ten ten of	●H
Also I-12	V.2194.11 137-16	
136-		•H
V.		●H
0-13 0-13	eH-648T20 (Ch. V-2201-1) (Atso see PCB 42—Set 176-1) 154-15 PH-649T17 (Ch. V-2200-1) (Atso see	• H
156- 8-13 -4U)	H-649717 (Ch. V-2200-1) (Also see PCB 42—Set 176-1) 154–15 H-649717 (Ch. V-2192-4) (See Mod-	● H
40-	 H-649T17 (Ch. V-2192-4) (See Model H-639T17—Set 133-15) H-650K21 (Ch. V-2192-4) (See Model H-639T17—Set 133-15) 	♦H
.1U) 138-	el H-639117—Set 133-15) eH-650117 (Ch. V-2200-1) (Also see PCB 42—Set 174 11	•H
0-1) 6-1)	 H-650117 (Ch. V-2200-1) (Also see PCB 42—Set 176-1) 154–15 H-651K17 (Ch. V-2192) (See Model H-639117—Set 133-15) H-51K17 (Ch. V-2200-11) (Also see 	♦H
14	H-651K17 {Ch. V-2200-1} {Also see	

w	ES	TIN	IGH	ou	51	E—(Co	nt
- 11	100	222	~ 10			· · · ·	~ .	

 $\begin{array}{c} \textbf{WESTINGHOUSE-Cont.} \\ \textbf{WESTINGHOUSE-Cont.} \\ \textbf{H-652K20 (Ch. V-2194-2, -3) (See} \\ \textbf{FCB 31-Set 157-3 ond Model } \\ \textbf{H-642K20A-Set 157-16} \\ \textbf{H-652K20 (Ch. V-220-1) (Alio see \\ \textbf{PCB 42-Set 176-1} \\ \textbf{H-653K24 (Ch. V-2202, V-210-1) \\ \textbf{I} (Alio see PCB 35-Set 160-1) \\ \textbf{H-653K17 (Ch. V-2192, V-210-1) \\ \textbf{H-655K17 (Ch. V-2192, -1, -133-15) \\ \textbf{H-655K17 (Ch. V-2192, -4, -5, -6) \\ \textbf{(See PCB 28-Set 150-1) \\ \textbf{H-655K17 (Ch. V-2192, -4, -5, -6) \\ \textbf{(See PCB 28-Set 150-1) \\ \textbf{H-655K17 (Ch. V-2192, -4, -5, -6) \\ \textbf{(See PCB 28-Set 150-1) \\ \textbf{H-655K17 (Ch. V-2192, -4, -5, -6) \\ \textbf{(See PCB 28-Set 150-1) \\ \textbf{H-655K17 (Ch. V-2192, -4, -5, -6) \\ \textbf{(See PCB 28-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2192, -1) (See PCB 42-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2204, -1) (See PCB 28-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2204, -1) (See PCB 28-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2204, -1) (See PCB 42-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2204, -1) (See PCB 42-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2204, -1) (See PCB 42-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2204, -1) (Alio see PCB 42-Set 130-1) \\ \textbf{H-655K17 (Ch. V-2202, -1) (See PCB 42-Set 170-1) \\ \textbf{H-655K17 (Ch. V-2202, -1) (Alio see PCB 42-Set 170-1) \\ \textbf{H-655K17 (Ch. V-2202, -1) (Alio see PCB 42-Set 170-1) \\ \textbf{H-655K17 (Ch. V-2202, -1) (Alio see PCB 42-Set 170-1) \\ \textbf{H-655K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 40-Set 172-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 40-Set 172-1) \\ \textbf{H-657K17 (Ch. V-2204) (Alio see PCB 40-Set 172-1) \\ \textbf{H-657K17 (Ch. V-2204) (Ch. V-2216) \\ (Alio see PCB 40-Set 172-1) \\ \textbf{H-657K17 (Ch. V-2207, 1) (See PCB 42-Set 170-1) \\ \textbf{H-657K17 (Ch. V-2207, 1) (See PCB 40-Set 172-1) \\ \textbf{H-657K17 (Ch. V-2217, 1) (See PCB 40-Set 172-1)$ L and Model H.667117—Set 167. H-638k24 [Ch. V-2219-1] [Alto see PCB 52—Set 186-1]...174–14 H-638k24 [Ch. V-2219-1] [Alto see PCB 52—Set 186-1]...174–14 H-638k14 [Ch. V-2219-1] [See PCB 40—Set 172-1, PCB 58—Set 167.15] H-670k21, H-691k21 [Ch. V-2217. 1] [See Model H-667117—Set 167.15] H-670k21 [Ch. V-2217-2, 3] [See PCB 46—Set 177.1, PCB 52— Set 1867.16] H-670k21 [Ch. V-2217-2, 3] (See H-670k21] [Ch. V-2217-2, 3] (See Model H-667117—Set 168.43—Set 177.1, PCB 45—Set 168.43—Set 177.1, PCB 45—Set 168.43—Set 177.1, PCB 45—Set 1696 [Ch. V-2216-2, 3] H-690k13] (Ch. V-2217-2, 3] H-690k13] (Ch. V-2216-2, 3] H-700117 (Ch. V-2216-2, 3] H-700117 (P1-1, PCB 55—Set 186-1 and Model H-667117—Set 167-1 15] H-701421 (Ch. V-2217-2) [See PCB 43—Set 177.1] (Ch. V-2217-2) [See PCB 43—Set 177.1] (Ch. V-2217-2) [See PCB 43—Set 177.1] [Set 167.1] H-701421 (Ch. V-2217-2) [See PCB 15] 42—541 [77-1 and Model H-667T17—541 [67-15] +702X17, H-703X17 [Ch. V-2216-2, -3] (See PCB 40—Set 172-1, PCB 45—Set 177-1, PCB S2—Set 186-1 and Model H-767T17—Set 167-15)
 15)

 14.704171 (Ch. V-2216-2) (See PCB

 40—Set 172-1, PCB 45—Set 187, I, PCB 52—Set 186-1 and Model H-667172—Set 187-15)

 151 (See Set 181, PCB 52—Set 186-1 and Model H-667717—Set 187-15)

 H-704171 (Ch. V-2216-4, -5)

 H-704171 (Ch. V-2216-4, -5)

 H-704171 (Ch. V-2216-4, -5)

 H-704171 (Ch. V-2216-4, -5)

 H-704171 (Ch. V-220-2, -3)

 H-705170 (Ch. V-220-1, -193-12)

 H-705170 (Ch. V-220-1, -193-12)

 H-705171 (Ch. V-220-1, -193-12)

 H-705171 (Ch. V-220-1, -3, -1193-12)

 H-705171 (Ch. V-220-1, -3, -1193-12)

 H-705171 (Ch. V-220-1, -3, -1193-12)

 H-705171 (Ch. V-2217-2, -3)

 See PCB 40—Set 172-1, PCB 43—Set 177-1, PCB 43

 S2-Set 166-1 Set 167-15)

 H-710721 (Ch. V-2217-2, -3)

 H-710721 (Ch. V-2217-2, -3)

 H-710721 (Ch. V-2217-2, -3)

 H-710721 (Ch. V-2217-2, -3)

 H-711721 (Ch. V-2217-2, -3)

 H-711721 (Ch. V-2217-2, -3)

 H-711721 (Ch. V-2217-2, -3)

 H-71172 (Ch. V-2217-2, -3)

 H-71172 (Ch. V-2217-2, -3)

 H-71172 (Ch. V-2217-2, -3)

 H-71174 (Ch. V-2217-2, -3)

 H-71174 (Ch. V-2217-2, -3)

 H-835K21 (Ch. V-2263-22) 253-17

 WESTINGHOUSE-Cont.
 H-721K21 (Ch. V-2217-4, -5)
 H-722K21 (Ch. V-2217-2, -3) (See PG8 40-Set 172-1, PC8 43—Set 177-1, PC8 52—Set 186-1 and Model H-65717-Set 167-15)
 H-722K21 (Ch. V-2217-5), 202-10
 H-723K21 (Ch. V-2217-5), 202-10
 H-723K21 (Ch. V-2217-5), 202-10
 H-7242(2) (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1 and PC8 68—Set 205-11
 H-730C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1 and PC8 68—Set 205-11
 H-730C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1 and PC8 68—Set 205-11
 H-730C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1)
 H-732C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1)
 H-732C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1)
 H-732C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1)
 H-732C21 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1)
 H-732C11 (Ch. V-2218-1) and Radio Ch. V-2180-9, -10) (Alio see PC8 59—Set 193-1)
 H-733717 (Ch. V-2227-1) (Alio see PC8 59—Set 193-1)
 H-737171 (Ch. V-2227-1) (Alio see PC8 59—Set 193-1)
 H-737171 (Ch. V-2223-2) (212—9
 H-738717 (Ch. V-2233-1) (214-10
 H-737171 (Ch. V-2233-1) (214-10
 H-737171 (Ch. V-2233-1) (214-10
 H-737171 (Ch. V-2233-1) (212—9
 H-736121 (Ch. V-2213-2) (212—9
 H-736421 (Ch. V-2213-2) (212—9
 H-735421 (Ch. V-2213-2) (212—9
 H-735421 (Ch. V-2213-2) (212—9
 H-735421 (Ch. V-2233-2) (212—9 H-769TU21 [Ch. V.2273-122]
 H-770T21A (Ch. V.2263-12] 23-17
 H-770T21A (Ch. V.2263-12] 23-17
 H-770TU21A (Ch. V.2263-12] 23-17
 H-771TU21A (Ch. V.2263-12] 23-17
 H-771TU21A (Ch. V.2263-12] 23-17
 H-786K21 (Ch. V.2263-12) 23-17
 H-786K21 (Ch. V.2263-12) 23-17
 H-787KU21 (Ch. V.2263-12) 23-17
 H-787KU21 (Ch. V.2273-122) 23-17
 H-787KU21 (Ch. V.2273-122) 23-17
 H-795727, H-795TU27 (Ch. V.2270-12) 11 (Allo see 7CE 105-5et 23-17) 241-12
 H-798TU7 (Ch. V.2260-12, 241-12 •H-798T17 {Ch. V-2260-12 2. -14) ●H-799TU17 (Ch. V-2270-122, -124)
 ●H-799TU17 (Ch. V-2260-12, -14)
 ●H-799T17 (Ch. V-2260-12, -14)
 255-17
 255-17 H-799117 (Ch. V-2260-12, -14]
 H-7991107 (Ch. V-2270-122, -124]
 H-802 (Ch. V-11900-1, -2, -3, -4, -5, V-11213) Tel. UHF Conv.
 H-815724, H-8157U24 (Ch. V-2250-1, -4) (Also see PCB 105-Set 252-1), -241-12
 H-817K24, H-817KU24 (Ch. V-2250-1, -4) (Also see PCB 105-Set 252-1), -241-12
 H-827K21 (Ch. V-2263-12) 253-17
 H-827KU21 (Ch. V-2263-12) 253-17 eH-828T21 (Ch. V-2263-12, 13, -14, -15) 253-17 eH-828TU21 (Ch. V-2273-122, 134) 253-17

NOTE: PCB Denotes Production Change Bulletin.

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ZENITH-Cont.

13)

•H2241R (Ch. 22H21) •H2242E, R (Ch. 22H22) •H2250R (Ch. 22H22) •H2252R, H2253E (Ch.

ZENITH-Cont. ZENITH-Cont. G3158R21 (Ch. 23G2421 and Radio Ch. 8G22) (See Ch. 23G24 and Ch. 8G20; (See Ch. 23G24 and G3173R2, C. G3174R2 (Ch. 23G24 and Radio Ch. 8G20/22) (See Ch. 23G24 and Ch. 8G20/22) (See Ch. G3259R2 (Ch. 24G26 and Radio Ch. 8G20/22) (For TV Ch. see Ch. 24G26-Set 91A-12, For Radio Ch. see Ch. 8G20/22-Set 91A-13) G3259R21 (Ch. 24G2621 and Radio 91A-13) • G3259721 (Ch. 24G2621 and Radio Ch. 8G22) (For TV Ch. see Ch. 24G26-Set 91A-12, for Radio Ch. see Ch. 8G20/22-Set 91A-13) • G32622 (Ch. 24G26 and Radio Ch. 8G20/22) (For TV Ch. see Ch. 24G26-Set 91A-12, for Radio Ch. see Ch. 8G20/22-Set 91A-13) • G32621 (Ch. 13)
 G3262Z1 (Ch. 24G26Z1 and Radio Ch. 8G22) (For TV Ch. see Ch. 24G26—Set 91A-12, for Radio Ch. see Ch. 8G20/22—Set 91A-Ch. see Ch. 8620/22-Set 91A-13) G3275RZ (Ch. 24G26 and Radio Ch. 8620/22) (For TV Ch. see Ch. 24G26-Set 91A-12, for Ra-dio Ch. see Ch. 8620/22-Set 91A-13) G32762 (Ch. 24G26 and Radio Ch. 8G20/22) (For TV Ch. see Ch. 24G26-Set 91A-12, for Radio Ch. see Ch. 8G20/22-Set 91A-13) 127-14 H880RZ (Ch. 8H20) 114-12 H1083E (Ch. 10H20) (See Model H3467R-Set 120-13) H1086R, H-1087R (Ch. 10H20) (See Model H3467R-Set 120-13) H2029R, H2030B (Ch. 20H20) 144-15 eH2047R (C K515 (Ch. 5K03) (See Model Set 176-14) J514 Set 176-14) K518 (Ch. 5/03) (See Model J514 —Set 176-14) K526, W, Y (Ch. 5K04)... 215-18 K622, F, G, W (Ch. 6K03) 203-17 K666R (Ch. 6K02)... 203-18 K7252, F, G (Ch. 7K01)... 212-10 K777E, R (Ch. 7K02)... 184-15 K18127 (Ch. 19K20)... 184-15 K18127 (Ch. 19K20)... 184-15 K18127 (Ch. 19K20)... 184-15 K1820E-3 (Ch. 19K20)... 184-15 K1840E (Ch. 19K20)... 184-15 K2229F (Ch. 19K23)... 184-15 K2229F (Ch. 19K23)... 184-15 K2229F (Ch. 19K23) (See Model K1812E-Set 184-15) K2223F (Ch. 19K23) (See Model K1812E-Set 184-15) K2225F 3 (Ch. 19K23) (See Model K
 H-2052R, H2053E
 (Ch. 20H20)

 144-15
 144-15

 221201
 114-13

 H2229R, H2230E, R
 114-13

 H2229R, H2230E, R
 (Ch. 22H21)

 151-13
 H2241R (Ch. 22H22)

 H2250R (Ch. 22H22)
 151-13

 H2242F, R
 (Ch. 22H22)
 151-13

 H2250R (Ch. 22H22)
 151-13
 22H21) 151-13 151-13 H2252R, H2253E (Ch. 22H21)
 STI-13
 H2254R (Ch. 22H21)
 STI-13
 H2254E (Ch. 22H22)
 STI-13
 H2235E (Ch. 22H20)
 H24-13
 H233EE, EZ, R, RZ (Ch. 23H22, Z)
 H233EE, EZ, R, RZ (Ch. 23H22, Z)
 H233EE, R (Ch. 23H22, Z)
 H233EE, STI-113
 H233EE, STI-113-113
 H2352R, RZ, H2352E, STI-18-11
 H2352R, RZ, H2352E, SET (BE-11)
 H2436Q (Ch. 24H21) (See Model H3477R-Set 120-13)
 H2447R (Ch. 24H20) (See Model H2439R (Ch. 24H20) (20-13)
 H2447R (Ch. 24H21) (20-13) H2447R (Ch. 24H21)
 120-13
 H-2447F (Ch. 24H21)
 120-13
 H-2447F (Ch. 24H21)
 120-13
 H-268 (Ch. 20H20 and Radio Ch. 8H202) (For TV Ch. see Model H. 2027F—Set 144-15, for Radio Ch. see Model J880—Set 168-14)
 H3068F (Ch. 22H21 and Radio Ch. 8H202) (For TV Ch. see Model H2229F—Set 151-13. for Radio Ch. see Model J880—Set 168-14)
 H-3074 (Ch. 20H20 and Radio Ch. 10H202) (For TV Ch. see Model H2029F—Set 151-13.
 H3068F (Ch. 23H22 and Radio Ch. 13) •H3168R (Ch. 23H22 and Radio Ch. 8H20) (For TV Ch. see Model H2328E—Set 118-11, for Radio Ch. see Model H880RZ—Set 114-12) Ch. see Model H880RZ—Set 114-12) H3267, R (Ch. 24H20 and Radio Ch. 8H20) [For IV Ch. see Set 120-13, for Radio Ch. see Model H800RZ—Set 114-12) H3273E, H3274R (Ch. 22H21 and Radio Ch. 10H202) ... 151-13 H3248R (Ch. 22H22 and Radio Ch. 10H202) ... 151-13 H3248F (Ch. 22H22 and Radio Ch. 10H202) ... 120-13 H3245F (Ch. 24H20 and Radio Ch. 10H20) [See Model H3467R—Set 120-13] H32477R (Ch. 24H21 and Radio Ch. 10H20) ... 120-13 H32477R (Ch. 24H21 and Radio Ch. 10H20) ... 120-13

H3478E (Ch. 24H21 and Radio Ch. 10H20) 120-13

WESTINGHOUSE-Cont, WESTINGHOUSE-Cont. ●H-835KU21 (Ch. V-2273-222) 253-17 ●H-836T21 (Ch. V-2263-35) 253-17 ●H-836TU21 (Ch. V-2263-35) 253-17 Ch. V-2157-2, -2U (See Model H-323T5) Ch. V-2157-3U (See Model H-Ch. V-21. 32716U) H-8361U21 (Ch. V-22/3-322)
 S3-17
 H-838K21 (Ch. V-2263-15) 253-17
 H-838K21A (Ch. V-2263-15) (See Model H-769721—Set 253-17)
 H-838KU21 (Ch. V-2273-122) V-2157-4U (See Model H338-Ch. V.2157-4U (See Model H338-TSU) Ch. V.2157-6 (See Model H.35515) Ch. V.2157-6 (See Model H.35915) Ch. V.2157-8 (See Model H.35915) Ch. V.2157-8 (See Model H.35915) Ch. V.2157-10 (See Model H.37415) Ch. V.2157-11 (See Model H.37415) Ch. V.2157-11 (See Model H.38815) Ch. V.2157-14 (See Model H.38815) Ch. V.2167-14 (See Model H.38174) Ch. V.2167-14 (See Model H.30717) Ch. V.2167-14 (See Model H.40716) Ch. V.2175-15 (See Model H.4026116) Ch. V.2175-15 (See Model H.4026116) Ch. V.2175-3, -4 (See Model H.4017) Ch. V.2175-5, (See Model H.4031714) Ch. V.2175-5 (See Model H.4031714) Ch. V.2175-5 (See Model H.4031714) Ch. V.2175-5 (See Model H.4031714) Ch. V.2177 (See Model H.4031714) Ch. V.2177, (See Model H.4031714) Ch. V.2173, -1, -3 (See Model H.4031714) Ch. V.2170, (See Model H.4031717) T5U) H-B38K21A [Ch. V-2263-15] (See Model H-759721-821 53-17)
 H-B38KU21 (Ch. V-2273-122)
 H-B38KU21 (Ch. V-2273-124) (See Model H-759721-261 53-17)
 H-B39K21 (Ch. V-2263-15) 253-17)
 H-B39K21 (Ch. V-2263-15) 253-17)
 H-B39K21 (Ch. V-2263-15) 253-17)
 H-B40K15 (Ch. V-2273-324) (See Model H-759721-Set 253-17)
 H-B40K121A (Ch. V-2273-324) (See Model H-769721-Set 253-17)
 H-B45121A (Ch. V-2273-324) (See Model H-769721-Set 253-17)
 H-B455121A (Ch. V-2273-324) (See Model H-769721-Set 253-17)
 H-B455121A (Ch. V-2273-324) (See Model H-769721-Set 253-17)
 H-B65121A (Ch. V-2273-324) (See Model H-1679721-Set 253-17)
 H-B65121A (Ch. V-2273-324) (See Model H-1679721-Set 253-17)
 H-B65121A (Ch. V-2273-324) (See Model H-1679721-Set 253-17)
 H-B65121A (Ch. V-2273-324) (See Model H-161)
 Ch. V-2103 (See Model H-161)
 Ch. V-2103 (See Model H-161)
 Ch. V-2103 (See Model H-161)
 Ch. V-2123 (See Model H-163)
 Ch. V-2123 (See Model H-164)
 Ch. V-2128 (See Model H-164)
 Ch. Ch Ch. V.2137-3, V.2137-35 (See Model H-231) Ch. V.2144, V.2144-1 (See Model H-210) Ch. V.2146-05 (See Model H-216) Ch. V.2146-11DX (See Model H-217) Model Press Ch. 9/2146-35DX [See Model H-216] Ch. 9/2146-45 [See Model H-3015] Ch. 9/2149 [See Model H-2178] Ch. 9/2149-1 [See Model H-213] Ch. 9/2149-1 [See Model H-233] Ch. 9/2149-2 [See Model H-233] Ch. 9/2149-3 [See Model H-203] Ch. 9/2149-3 [See Model H-203] 9/2150-02 [See n-ouutió) h. V-2150-81, -82, -84 (See Mod-el H-251) Ch. V-2150-91A [See model H-604-Ch. V-2150-94 [See And TIO, A] Ch. V-2150-94C [See Model H-609710) h. V-2150-101 (See Model H-Ch. V-2150-101 (See Mode' 605112) Ch. V-2150-111, A (See Mode' H-606K12) Ch. V-2150-136 (See Model H-610112) Ch. V-2150-146 (See Model H

Ch. V.217/ [See Model H-057114] Ch. V.217/ [See Model H-050717] Ch. V.2180-1 [See Model H35077] Ch. V.2180-2 [See Model H-050C77] Ch. V.2180-3 [See Model H-050C77] Ch. V.2180-5 [See Model H-050C77] Ch. V.2180-8 [See Model H-050C77] Ch. V.2180-8 [See Model H-050C77] Ch. V.2180-8 [See Model H-05077] Ch. V.2181-1 [See Model H-05077] Ch. V.2181-1 [See Model H-05077] Ch. V.2182-2 [See Model H-05077] Ch. V.2182-2 [See Model H-05775] Ch. V.2182-1 [See Model H-1775] Ch. V.2182-1 [See Model H-1775] Ch. V.2182-1 [See Model H-05775] Ch. V.2182-1 [See Model H-05775] Ch. V.2182-1 [See Model H-0775] Ch. V.2182-1 [See Model H-0775] Ch. V.2192, -1 [See Model H-639717] Ch. V.2192, -1 [See Model H-42244] Ch. V-2192, -1 (See mous-639117) Ch. V-2192, -3, -4, -5, -6 (See Model H-640117A) Ch. V-2194, V-2194A, V-2194-1 (See Model H-642K20A) Ch. V-2194-2, -3 (See Model H-452K20) - Kon Model H-651-Ch. V-2200-1 (See Model H-651-K17) Ch. V-2201-1 (See Model H-K20) Ch. V-2202-2 (See Model H-
 K2U
 Construction
 <thConstruction</th>
 Construction
 653K24) h. V-2214-1 (See Model H-
 O33K41
 Constraint
 Constraint< 0/3821) Ch. V-2217-2, -3 (See Model H-692T21) Ch. V-2217-4, -5 (See Model H-710T21) Ch. V-2218-1, -2, 11 (See Model H-730C21) Ch. V-2218-1 (See Model H-688K24) Ch. V-2220-1 (See Model H-708T20) Ch. V-2220-2 [See Model H-718K20]
 TIBK20
 Gee
 Model
 H

 718K20
 -11
 (See
 Model
 H

 708T20
 -11
 (See
 Model
 H

 708T20
 -11
 (See
 Model
 H

 736T17
 (See
 Model
 H 739T17

 Ch.
 V-2232-2
 (See
 Model
 H

 737T77
 Ch.
 V-2233-2
 (See
 Model
 H

 7047213
 Ch.
 V-2232-2
 (See
 Model
 H 7047213
 Ch. V-2233-2 (See Model H-751T21) Ch. V-2233-3 (See Model H-750721) Ch. V-2233-4 (See Model H-746K21) Ch. V-2250-1 (See Model H-795T27) Ch. V-2230-1 (See Model H-795127) Ch. V-2250-4 (See Model H-815123) Ch. V-2263-11, -12, -13, -14 (See Model H-830K21) Ch. V-2263-15 (See Model H-827121) Ch. V-2263-25 (See Model H-834K21) Ch. V-2273-111, -122, -124, -132, -134 (See Model H-830KU21) Ch. V-2273-322 (See Model H-834KU21) Ch. V-2273-322 (See Model H-834KU21) H-834K021) H-834T021) Ch. V-2273-322 (See Mode' H-834T021) Ch. V-2273-324 (See Mode' H-833T021A) Ch. V-2284-15 (See Model H-840CK15) Ch. V-11213 (See Model H-802) Ch. V-11900-1, -2, -3, -4, -5 (See Model H-802) NOTE: PCB Denotes Production Change Bulletin, Production Change Bulletin Nos. 1 Through 63 Are All Contained in Set No. A-200. Denotes Television Receiver.

(Also see Majestic) (Also see Recordio) WILLYS-OVERLAND 8030 (670777) 50-23 670777 (See Model 8030-Set 50 WILMAK W-446 "DENchum" 21-11 WIRE RECORDING CORP. (See Recorder Listing) WOOLAROC
 3:1A
 (Ch. 6-9022-J), 3-2A
 (Ch. 6-9022-J), 3-2A

 6:9022-K)
 6-37
 3:3A
 (Cade 7-9003-D)

 5:5A
 22-32
 3:6A/5
 24-32

 3:6A/5
 24-32
 3:9A, 3:10A
 7-33

 3:1A (Ch. 56A76)
 8-33
 3:12/3
 23-32
 6-37 6-38 22-32 24-32 7-30 12/3 13A, 3-14A, 3-15A, 3-16A 34-28 17A, 3-18A 34-29 34-29 3-1/A, 3-18A 3-20A 3-20A 3-24-33 3-29A 7-31 3-61A (See Model 3-71A—Set 36 ZENITH (Also see Record Changer Listing) 12) G2442E, R (Ch. 24G22/24) 98-17 G2442RZ (Ch. 24G22/24) 98-17 G2442RZ (Ch. 24G26) (See Ch. 24G26-Set 91A-12) G2442EZI, G2442RZI (Ch. 24G-24Z1) (See Ch. 24G26-Set 91A-12) 12) • 62448R (Ch. 24622/24) ... 98–17 • 2448R2 (Ch. 246226) (See Ch. 24626 (Ch. 24626) (See Ch. 24626—Set 91A-12) • 62448R21 (Ch. 24621) (See Ch. 24626—Set 91A-12) • 62454R(Ch. 24621) ... 93–11 • 6-2454-ROX (Ch. 24621-0X) • 33–11 93-11 93 G2957, R (Ch. 23G23 and Radio Ch. 6G20) 98–17 • G2958R (Ch. 23G23 and Radio Ch. 6G20) 98-17 91A-13) 9G3158RZ (Ch. 23G24 and Radie Ch. 8G20/22) (See Ch. 23G24 and Ch. 8G20/22—Set 91A-13)

WILCOX-GAY

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117

V-2146-21DX, -25DX (See Ch

Model H-226} h. V-2146-35DX {See Model

Ch. V-2149-3 (See Model 1. 2017) 12) Ch. V-2150-01, V-2150-02 (See Model H-223) Ch. V-2150-31 (See Model H-401K-1242) Ch. V-2150-31 (See Model H-401K-1231) Ch. V-2150-51 (See Model H-231) Ch. V-2150-61, A, B (See Model H-H-A00116)

613K16) Ch. V-2150-176, U (See Mode H-617T12) Ch. V-2150-177U (See Model H-

H-617.1.2. Ch. V-2150-177U [See Ho-617712] Ch. V-2150-186, A, C, CA [Ser Model H-618716] Ch. V-2150-197 [See Model H Ch. V-2150-197 [See Model H-302P5]

Ch. V-2152-01 (See Model H-603 C12) Ch. V-2152-16 (See Model H 611C12)

Ch. V-2153 (See Model H303P4) Ch. V-2153-1 (See Model H-312P4 Ch. V-2156 (See Model H-309P? Ch. V-2156-1U (See Model H-342

Ch. V-2157, U (See Model H-31875

Ch. V-2157-1, -1U (See Model H-32175)

P5U)

Ch

Ch

ZENITH

ZENITH-Cont.

 ZENITH--Cont.

 ●K2291E-3 (Ch. 21K20 and Radis Ch. 10H202) [Far TV Ch. see Sei H3273E-Sei To Ch. see Madel H3273E-Sei To Ch. see Madel H3273E-Sei To Ch. see Madel H3273E. See To Ch. See Madel H3273E. See To Ch. See Madel H328 Ch. See Madel H12E-See T23-To Ch. See Madel H12E-See T23.
 ZENITH-Cont. 234-14
 236-16
 236-17
 237-13
 23800
 233-13
 23800
 233-13
 23800
 233-13
 23800
 23710
 23812
 23800
 23812
 23800
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ENITH-Cont. ● M2200R (Ch. 20M20) 261-17 ● M2200RU (Ch. 20M20U) 261-17 ● M2200RU (Ch. 20M20U) 261-17 ● M2200RU (Ch. 20M20U) 261-17 ● M2201U (Ch. 20M20U) 259-16 ● RIB00EUZ (Ch. 19M20U) 259-16 ● RIB00EUZ (Ch. 19M20U) 259-16 ● RIB12EUZ (Ch. 19M21U) 259-16
•M2260R (Ch. 20M20)
M2260RUZ (Ch. 20M20UZ) 261-17 M2260RZ (Ch. 20M20Z) 261-17
M2261E (Ch. 20M20)
• M2261EZ (Ch. 20M20Z) 261-17
•M2267YU (Ch. 20M20)
M2267YZ (Ch. 20M20Z) 261–17 R1800EUZ (Ch. 19M20U) 259–16
• R1800EZ (Ch. 19M20) 259-16
• R1800RZ (Ch. 19M20)
•R1812EU2 (Ch. 19M20U)259–16 •R1812EZ (Ch. 19M20)259–16
R1812RUZ (Ch. 19M20U)259-16 R1812RZ (Ch. 19M20)259-16
R2229EUZ (Ch. 19M21U)259-16
•R2229RUZ (Ch. 19M21U) .259-16
• R2229RZ (Ch. 19M21) 259-16 • R2230EUZ (Ch. 19M21U) 259-16
R2230EZ (Ch. 19M21)
R2230RZ (Ch. 19M21) 259-16
• R2249EZ (Ch. 19M210)
•R2249RUZ (Ch. 19M21U)259-16 •R2249RZ (Ch. 19M21)259-16
R2250EUZ (Ch. 19M21U)259-16 R2250EZ (Ch. 19M21)
R2250RUZ (Ch. 19M21U)259-16
• R2257EUZ (Ch. 19M21)
• R2257EZ (Ch. 19M21) 259–16 • R2257RUZ (Ch. 19M21U)
• R2257RZ (Ch. 19M21) 259-16 • R2258EUZ (Ch. 19M21U) 259-16
• R2258EZ (Ch. 19M21) 259-16
•R2258R02 (Ch. 19M210)259-16 •R2258RZ (Ch. 19M21)259-16
S-9010 (Ch. 4L02)
5-9013 (Ch. 3M01)
4G800 (Ch. 4E41) 35-27 4G800WZ, 4G800YZ, 4G800Z (Ch. 4E41Z) 52-23
4E412) 52-23 4G903, 4G903Y (Ch. 4F40) 76-20 4K016 (Ch. 4C52) 6-39 4K035 (Ch. 4C53) 6-40 5D011, 5D027 (Ch. 5C01, 5C012)
4K016 (Ch. 4C52) 6-39 4K035 (Ch. 4C53) 6-40
5D011, 5D027 (Ch. 5C01, 5C01Z) 3-17
50810 (Ch. 5E02) 54-21
5G003Z (Ch. 5C40Z, 25G003ZZ
(Ch. 5C40ZZ) 30-31 5G036 (Ch. 5C51) 30-32 5R080-5R086 (Ch. 5C02, 5C04)
51000-51000 (Ch. 5002, 5004)
6D014, 6D014W, 6D029, 6D029G (Ch. 6C01) 9-35
6D015, 6D015Y 6D030 (Ch AC05
6D815, 6D815W 6D815Y 1Ch
3-14
6G001YZ1 (See Model 6G001—Set 3-14)
3-14) Geodari (Ch. 6C41) 20-35 36038 (Ch. 6C50) 32-30 36038 (Ch. 6C50) 32-30 36038 (Ch. 6C41) 20-35 36038 (Ch. 6C50) 32-30 36038 (Ch. 6C21) 32-30 36038 (Ch. 6C21) 20-35 37886 (Ch. 6C22) 7-32 78820 (Ch. 7E02) 34-30 7H8202 (Ch. 7E02) 7H52 7H932 (Ch. 7E02) 7H52 7H920 7H9200 (Ch. 7F01) 7H921 (Ch. 7F02) 75-18 7H922 (Ch. 7F02) 73-16 7H922 (Ch. 7F02) 73-16 7H921 (Ch. 6C06) 37-25 78887 (Ch. 6C06) 7-33 8G005YT (21) (Ch. 8C401) 7-33 8G005YT (21) (Ch. 8C401) (21) 8G005YT (22) (Ch. 8C401) (22)
6G801 (Ch. 6E40)
6R087 (Ch. 6C22)
7R886 (Ch. 6E02)
7H822 (Ch. 7E02), 7H822WZ, 7H822Z (Ch. 7E02Z) 55-25
7H918 (Ch. 7F03)
7H921 (Ch. 7F04) 73-16
7R070 (Ch. 6C06) 37-25
7R887 (Ch. 7E22) 54–22 8G005Y (Ch. 8C40) 7–33
8G005YT (Z1) (Ch. 8C40T) (Z1), 8G005YT (Z2) (Ch. 8C40T) (Z2)
8H023 (Ch. 8C01) 53-27 4-40
8H032, 8H033 (Ch. 8C20). 1-33
8H034 4-40 8H050, 8H051, 8H052, 8H061 1-33
8H050, 8H051, 8H052, 8H061 1-33 8H832, 8H861 (Ch. 8E20). 52-24 9H079, 9H079E, 9H079R, 9H081,
9H082R, 9H085R, 9H088R (Ch
9H881, 9H882R, 9H885, 9H888R (Ch. 9F21) 43-25
9H984, 9H984LP (Ch. 9F22) 64-14
12H090, 12H091, 12H092, 12H093,
12H094 (Ch. 11C21) 2-20 14H789 (Ch. 13D22) 41-24
• 27T965R (Ch. 27F20) 95-8 • 28T925, E, R (Ch. 28F22)
• 287926E, R (Ch. 28F25) (See Model
• 287960E (Ch. 28F20) (See Model
8C21) 7-34 9H881, 9H882R, 9H885, 9H888 43-25 (Ch. 9E21) 43-25 9H984, 9H984P (Ch. 9F22) 64-14 9H995 (Ch. 9F212), 74-12 9H994, 9H984P (Ch. 9F22) 64-14 9H995 (Ch. 9F212), 74-12 12H090, 12H091, 12H092, 12H093, 12H093, 12H093, 12H093, 12H091, 12H092, 12H093, 12H094,
201700301 04-13)

ZENITH-Cont. •281960-GO, 281960K (Ch. 28720) (See Model 281960-Sei 64-13) •281961E, 281961-GO (Ch. 28721) (See Model 28196)-[See Model 281962-Sei 64-13] •281962R-Sei 64-13] •281963 (Ch. 28721) ... 74-13 •271998RIP (Ch. 28723 and Radio Ch. 96212) (For TV Ch. see Model 421999RIP-Sei 74-13, for Radio Ch. 96212) (For TV Ch. see Model 42199PRIP (Ch. 28720 and Radio Ch. 96212) (For TV Ch. see Model 281960-Sei 64-15, for Radio Ch. 96212) (See Model 281964R) Ch. 3100 (See Model 5.9011) Ch. 3100 (See Model 45.9011) Ch. 4213 (See Model 46300) Ch. 4E412 (See Model 46300) Ch. 4E412 (See Model 46300) Ch. 4E412 (See Model 46300) Ch. 4E40 (See Model 46300) Ch. 4E41 (See
 58080)

 Ch. 5C04 (See Model 58080)

 Ch. 5C04 (See Model 560031)

 Ch. 5C04 (See Model 560032)

 Ch. 5C07 (See Model 560032)

 Ch. 5C07 (See Model 560032)

 Ch. 5C07 (See Model 560030)

 Ch. 5C07 (See Model 5010)

 Ch. 5C07 (See Model 6511)

 Ch. 5C07 (See Model 6503)

 Ch. 5C07 (See Model 1503)

 Ch. 5H01 (See Model H500)

 Ch. 5H01 (See Model H503)

 Ch. 5H03 (See Model H503)

 Ch. 5H04 (See Model H503)

 Ch. 5H04 (See Model H503)

 Ch. 5H04 (See Model L5164)

 Ch. 5H04 (See Model L518)

 Ch. 5H04 (See Model L518)

 Ch. 5H04 (See Model L507)

 Ch. 5H04 (See Model G0014)

 Ch. 6C02 (See Model R0014)

 Ch. 6C02 (See Model R0015)

 Ch. 5H04 (See Model G0015)

 Ch. 6C02 (See Model G0015)

 Ch. 6C02 (See Model G0015)

 Ch. 6C02 (See Model G0015)
 </tr Ch. 7G01 (See Model G725) Ch. 7G01 (See Model H725) Ch. 7G02 (See Model G724) Ch. 7G02 (See Model G723) Ch. 7H02 (See Model H724) Ch. 7H022 (See Model H7242) Ch. 7H0222 (See Model H72421) Ch. 7H0222 (See Model H72422)

ZENITH-Cont.

 ZENITH—Cont.

 Ch. 7H04 (See Model H723)

 Ch. 7H042 (See Model H7232)

 Ch. 7M042 (See Model H7233)

 Ch. 7M042 (See Model H7232)

 Ch. 7M04 (See Model H7233)

 Ch. 7K0 (See Model H7232)

 Ch. 7K0 (See Model H7232)

 Ch. 7K0 (See Model H023)

 Ch. 8C0 (See Model H023)

 Ch. 8C0 (See Model H023)

 Ch. 8C0 (See Model 8G005)

 YT (21)

 Ch. 8C00 (See Model 8G005)

 YT (21)

 Ch. 8C00 (See Model 8B807)

 Ch. 8C00 (See Model 8B807)

 Ch. 8C00 (See Model 8B807)

 Ch. 8C00 (See Model 18807)

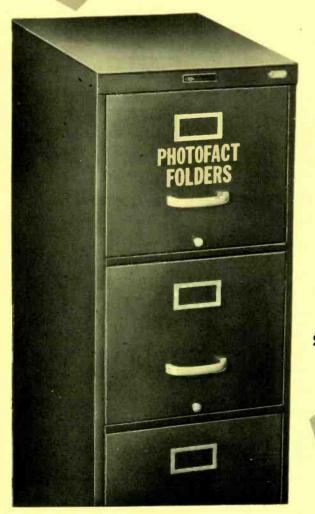
 Ch. 8L20 (See Model 18807)

 EU) h. 19126, U (See Model L1812E, Ch. 19L26, U (See model L2236E, EU) Ch. 19L27, U (See Model L2236E, Ch. 19127, U (See Model L2229E, EU) Ch. 19128, U (See Model L2229E, EU Ch. 19128, U (See Model 12250EU) Ch. 19130, U (See Model 12250EU) Ch. 19133, U (See Model 12228k, RU) Ch. 19134, U (See Model 11800R, Ch. 19134, U (See Model 11800R, h. 19134, U (see model M1800E) RU) h. 19M20 (See Model M1800E) h. 19M20U (See Model M1800E2) h. 19M20Z (See Model M1802238R) h. 19M21U (See Model M2228R) h. 19M21U (See Model M2228R) h. 19M21UZ (See Model M2230 m210 (See Model M2230 h. 19M21UZ (See Model M2230 RUZ) Ch. 19434, U (See Model L1800R, RU) Ch. 19M20 (See Model M1800E) Ch. 19M20U (See Model M1800E) Ch. 19M20U (See Model M1800EU) Ch. 19M21U (See Model M2228R) Ch. 19M21U (See Model M2228R2) Ch. 19M21U (See Model M2228R2) Ch. 20M20 (See Model M2237E) Ch. 20M20 (See Model M2237E) Ch. 20M20U (See Model M2237E) Ch. 21M20 (See Model M2237E) Ch. 21M20 (See Model M2237E) Ch. 21M20 (See Model K2260C3) Ch. 21K20-3 (See Model K2260C3) Ch. 21K20-3 (See Model K2260C3) Ch. 21K20-3 (See Model K2260C3) Ch. 21L21, U (See Model L2257E) Ch. 21L21, U (See Model L2257E) Ch. 21/21, U (See Model 122595, EU) Ch. 22H20 (See Model H2228R) Ch. 22H21 (See Model H2228R) Ch. 22H21 (See Model H2229R) Ch. 22H22 (See Model H2242E) Ch. 23G22 (See Model C2322) Ch. 23G22 (See Model G2957) Ch. 23G24 (See Model G2957) Ch. 24G20 (See Model G2420E) H-2328E) Ch. 24G20 (See Model G2420E) Ch. 24G20-OX (See Model G2420-EOX) EOX) Ch. 24G21 (See Model G2454R) Ch. 24G21-OX (See Model G2454. ROX) Ch. 24G21-OX [See Model G2454-ROX] Ch. 24G22/24 [See Model G2441R] Ch. 24G23/25 [See Model G2441] Ch. 24G24 [See Model G2441] Ch. 24G26 [See Model G2441] Ch. 24G2621 [See Model G2441] Ch. 24G2621 [See Model G2441] Ch. 24H20 [See Model G24172] Ch. 24H20 [See Model 271965R] Ch. 28F20 [See Model 281906] Ch. 28F21 [See Model 281926] Ch. 28F23 [See Model 281926] Ch. 29G20 [See Model G2951]

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ADMIRAL	ADMIRAL-Cont.	COLLARO	GARRARD	MAGUIRE
RC-150,	RC500	RC.521, RC.522 (CM-5) 205-4	RC-60 (CM-2) 81-7	ARC-1
(See Model RC200-Set 9 and	RC-550 [See Model RC-500—Set 132-2 (CM-4) and Model RC-550	3RC.521, 3RC.522.(CM-5) 205-4 3RC-531, 3RC-532	RC-80 (CM-4) 157-5 RC90	MARKEL
Model RC-160—Set 21-37) RC-170, RC-170A(CM-1) 31—2	Set 185-2 (CM-5]] RC600	COLUMBIA	GENERAL ELECTRIC	70, 71 (CM-2) 84-
RC-180, RC181 (CM-2) 76-1		104124—2	P6	74, 75 [See Set 91-7 (CM-3) an Supplement—Set 131-11]
RC-182 (See Model RC-181-Set 76-1 and Supplement-Set 76-2)	AERO	CRESCENT	GENERAL INDUSTRIES	MILWAUKEE ERWOOD
(CM-2)	46A	C-200	RC130L	10700 (CM-1) 16-3
RC-200		250 Series	GENERAL INSTRUMENT	11200 (CM-2) 86-
	AVIOLA	350 Series	204 (CM-1) 23-34	11600
RC-220, RC-221, RC-222, RC-320, RC-321, RC-322 [See Set 79-1	100	FARNSWORTH	205	MOTOROLA
and Changes in Set 108-2 (CM-3)]	BELMONT	P-51, P56 (CM-1) 13-36	LEAR	B24RC, B25RC, B27RC, B28R
RC400 (CM-4) 104-1	C-9 (CM-2) 34-21	P-72, P73 (CM-2) 75-8	PC-206A (CM-1) 18-33	(CM-1) 12-3
MOTOROLA-Cont.	RCA-Cont.	TRAV-LER	V-M-Cont.	ZENITH
RC30	RP-178	A	950 [See Set 107-13 (CM-3) and	S11478 (CM-1) 23-3
RC36C (See Model RC36—Set	RP-190 Series (CM-4) 144-7	UNIVERSAL CAMERA	Supplement-Set 131.17] 950, 951 (Late) (CM-5) 216-11	Series 700R (CM-2) 91-1
147-8) RC37	SEEBURG	100 (CM-1) 36-30	WEBSTER-CHICAGO	S11680
RC40 [See Model RC37—Set 141-8	K	UTAH	50	\$13675, S-14002, S14006, S14008
(CM-4)]	M	550 (CM-1) 8	56	S14004, S14007 (CM-2) 85-1
OAK	S, SQ	650	70	S14012, S14014 (CM-3) 110-14
6666	SILVERTONE	7001	100 (CM-4) 135-14	S14022
	101.761-2, 101.762-2 (CM-2) 77-10	V-M	106(CM-4) 146-12 121, 122, 123, 124, 125	S14024, S14025 (CM-3) 112-1
PHILCO D10, D10A(CM-1) 14-21	101.761-3, 101.762-3	200-B (CM-1) 15-36	(CM-5) 206-12	S14026
M-4 (CM-1) 25-30	101.762, 101.763 (CM-2) 83-11	400	126, 127, 129 (CM-5) 208–13 133	S14027
M-7 (CM-1) 28-35 M-8	(CM-2) 88-11	402, 400C (CM-2) 82-12	148	14031 (CM-4) 145-1:
M-9C	488.218	402D, 400D (CM-2) 87-14 404 [See Model 405-Set 73-14	246	S-14036 (CM-4) 145-13 S-14053, S-14054, S-14056
M-12C (CM-3) 109—9 M-20 (CM-3) 103–11		(CM-3)]	346	S-14057
M-22	SPARTON	405		MISCELLANEOUS
RCA	C48	800 (CM-1) 21-38 800-D (CM-2) 84-12	WESTINGHOUSE	Series 700F (CM-2) 89-
RP168	THORENS	802 (CM-3) 77-12	V4914	Series 700F 33/45.(CM-3) 75-11
	CD-40	910 (CM-3) 115-14	V6235	Series 700FLP (CM-2) 101-0
RP-176 (CM-1) 25-31 RP-177	CD43	935, 936	V6676 136-15	Series 700F5 (CM-2) 104-8

AMPEX 400A, 401A (CM-5) 213-1 AMPRO

AMPRO	M-3000
730 (CM-4) 133-4	M-3001
731 (For electrical unit see Folder	M-3500
	900 Serie
166-5; for mechanical unit see	1000 Ser
Folder 133-4)	1000 Seri
731-R (See Model 731)	
755, 756 262-1	CRESTW
BRUSH SOUND MIRROR	CP-201 .
BK-401	400 Serie
8K-403 (CM-2) 78-3	
9K 414	DUKAN
BK-416	
BK-437, BK-4375, BK-441, BK-442,	11A55FF,
BK-443P (CM-5) 164-3	11A75
BK-455P	
	EICOR
BRUSH MAIL-A-VOICE	230
BK-501, BK-502, BK-503(CM-1)	400
BR-307, BR-302, BR-303(CM-1)	1000
CONCERTONE	1000
	TUOTAD
1401 (401) (CM-4) 155-4	EKOTAP
	101-4, 5
CRESCENT	104-4,
11.1.4	101-8,
H-1A	
H-2A1 Series (CM-3) 119-4	109, 110,
H-19 Series "Steno"	114, 115,
(CM-4) 122—3	205, 206
H-20A1 (See Model H22A1-Set	200, 200
125-4)	FEDERAL
H-22A1 125—4	
H2000 Series (CM-4) 120-4	37-8

1-RETMA Production Saurce Code (Jan. 1, 1954).....

2-RETMA Production Source Code

3-TRADE DIRECTORY-

Parts Manufacturers 12 4-National Electrical Code on Antennos... 88

CRESCENT-Cont.	GENERAL INDUSTRIES
M-2001 Series (CM-4) 120-4	R70, R90
M-2500 Series (CM-4) 120-4	R90L [See Model R90-Se
M-3000 Series (CM-4) 120-4	(CM-1)]
M-3001 Series (CM-4) 120-4	250 (CM-4)
M-3500 Series (CM-4) 120-4 900 Series	
1000 Series (CM-2)	INTERNATIONAL ELECT
1000 Series Revised (CM-3) 77-4	PT3 (CM-2)
CRESTWOOD	KNIGHT
CP-201 (CM-3) 118-4	96-144 (CM-4)
400 Series (401, 402) 251-5	96-485 (CM-5)
	96-499 (CM-4)
DUKANE	96-590
11A55FF, 11B55 (CM-5) 187-5	
11A75	LEAR DYNAPORT
	WC-311-D (CM-2)
EICOR	
230 2236	MAGNECORD AUDIAD
400	AD-1R
1000	PT6, A, AH, AHX, AX
EKOTAPE (WEBSTER-ELECTRIC)	(CM-5)
	PT63-A, AH, AHX, AX
101-4, 5, 102-4, 5, 103-4, 5, 104-4, 5 (CM-3) 116 -12	(CM-5)
101-8, 101-9, 102-9, 103-8	MASCO
(CM-5) 170-6	
109, 110, 111, 112 (CM-4) 152-5	DC37R(CM-4)
114, 115, 116, 117 (CM-5) 189-8	D37
205, 206 228-8	LD37, LD37R (CM-4)
	52, 52C, 52CR, 52L, 52
FEDERAL	1CH 51

OLIVERAL INDOSTRIES
R70, R90 (CM-1) 35-28
R90L [See Model R90-Set 35-28
(CM-1)1
250 (CM-4) 143-8
INTERNATIONAL ELECTRONICS
PT3 (CM-2) 88-4
(10
KNIGHT
96-144 (CM-4) 158-6
96-485 (CM-5) 183-8
96-499 (CM-4) 158-6
96-590
LEAR DYNAPORT
WC-311-D(CM-2) 80-8
MAGNECORD AUDIAD
AD-1R
PT6, A, AH, AHX, AX
[CM-5] 190-6
PT63-A, AH, AHX, AX
с. (См-5) 190—8
MASCO
DC37R
D37 (CM-4) 148-9
D37R (CM-4) 148-9
1D37 1D378 (CM-4) 148-9

LD37,	LD37R	.(CM-4)	148-9
52, 52	C, 52CR,	52L, 521	R, 52R
		.(CM-5)	214-6
375		. (CM-3)	1177

MITCHELL	
1290	
PENTRON	
PB-A2, PB-1	CM-5) 184-11
97-3	
9T-3C	CM-4) 162-9
RCA	
MI-12875	CM-2) 85-12
SRT-301 (M1-15910)	224-11
RECORDIO (See V	Vilcox Gay)
	(under lody)
REELEST	
C1A	CM-4) 123-13
REVERE	
T-100(CM-4) 149-11
T-500 [See Model T-1	00-Set 149-
11 (CM-4)]	
TR-200, TR-600 (For see Folder 165-10;	
cal unit see Folder	
T-70153, T-70157,	T-70163, T-
70167, T-70253,	T-70257, T-
70263, T-70267,	T-77153, T-
77157, T-77163, 77253, T-77257,	T-77167, T- T-77263, T-
77267	CM-51 193-9
SILVERTONE	
70 (Ch. 567.230, 57)	CH 4) 121 11
771	CM-1) 26-32
101.774-2, 101.774-	4

s 700F5	(CM-2
GEORGE	
c :	1011 1

.... (CM-1) 40-24 1100 Series . TAPE MASTER

TELECTRO-TAPE

ST.

TDC WEBSTER-CHICAGO WEBSTER-CHICAGD 79-80 (CM-1) 37-26 178 (CM-3) 113-12 210 (CM-4) 159-17 228 (CM-4) 156-13 2010 (See Model 210-Set 159-17 (CM-4)

WEBSTER ELECTRIC (See Ekotape)

WILCOX GAY

WILCOX GAT	
2A10, 2A108, 2A11, 2A118 180-1	0
3A10, 3A11 (CM-5) 200-1	
3C10 (CM-5) 215-1	7
3F10 (CM-5) 220-1	1
4A10	8
WIRE RECORDING CORP.	
WP	9

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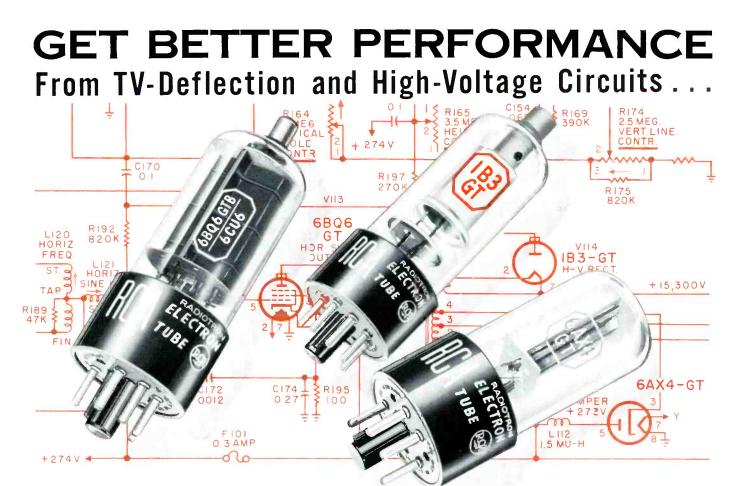
246

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8—"Let's Look at the Sync Pulses"	64	1
9-Replacement of Disc & Plate Type		1
Ceramic Capacitors	68	1
10—Certificate entitling subscriber to PHOTO-		
FACT Volume Lobels for Vols. 1-10	62	1
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FACT Volume Labels for Vols. 11-20		
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13-Alliance Model DIR Rotator	240	2
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15-Alliance	Model	HIR	Rotatar

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17-Alliance Model U-83 Rotator
18—Photofact Television Course
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