JULY · 1949

electronics

A McGRAW-HILL PUBLICATION

SUBMINIATURE
COUNTER

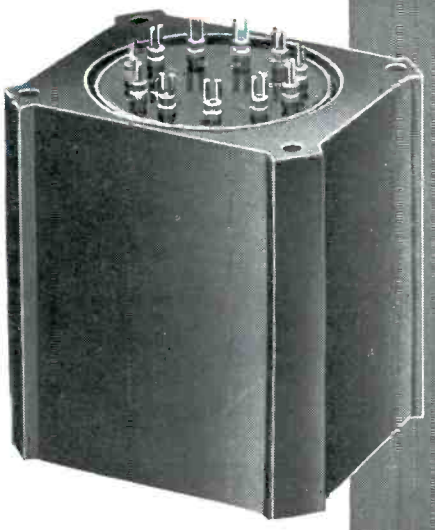
Linear Standard Units...

THE ULTIMATE IN QUALITY...

UTC Linear Standard Audio Transformers represent the closest approach to the ideal component from the standpoint of uniform frequency response, low wave form distortion, high efficiency, thorough shielding and utmost dependability.

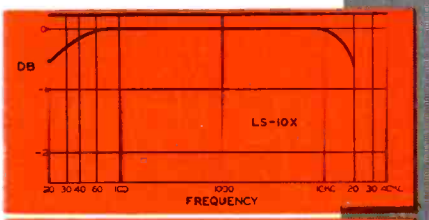
UTC Linear Standard Transformers feature . . .

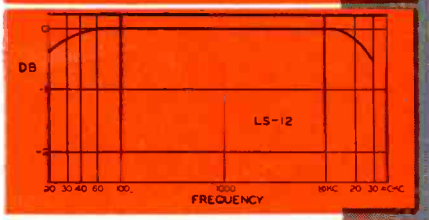
- **True Hum Balancing Coil Structure** . . . maximum neutralization of stray fields.
- **Balanced Variable Impedance Line** . . . permits highest fidelity on every tap of a universal unit . . . no line reflections or transverse coupling.
- **Reversible Mounting** . . . permits above chassis or sub-chassis wiring.
- **Alloy Shields** . . . maximum shielding from inductive pickup.
- **Hiperm-Alloy** . . . a stable, high permeability nickel-iron core material.
- **Semi-Toroidal Multiple Coil Structure** . . . minimum distributed capacity and leakage reactance.
- **Precision Winding** . . . accuracy of winding .1%, perfect balance of inductance and capacity; exact impedance reflection.
- **High Fidelity** . . . UTC Linear Standard Transformers are the *only* audio units with a *guaranteed* uniform response of ± 1 DB from 20-20,000 cycles.

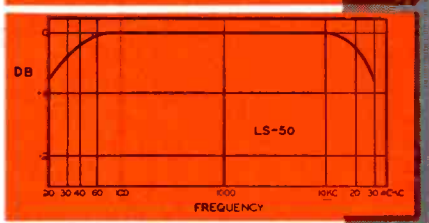


TYPICAL LS LOW LEVEL TRANSFORMERS

Type No.	Application	Primary Impedance	Secondary Impedance	±1 db from	Max. Level	Relative hum-pickup reduction	Max. Unbalanced DC in prim'y	List Price
LS-10	Low impedance mike, pickup, or multiple line to grid	50, 125, 200, 250, 333, 500/600 ohms	60,000 ohms in two sections	20-20,000	+15 DB	—74 DB	5 MA	$25.00
LS-10X	As Above	As above	50,000 ohms	20-20,000	+14 DB	—92 DB	5 MA	32.00
LS-12	Low impedance mike, pickup, or multiple line to push pull grids	50, 125, 200, 250, 333, 500/600 ohms	120,000 ohms overall, in two sections	20-20,000	+15 DB	—74 DB	5 MA	28.00
LS-12X	As above	As above	80,000 ohms overall, in two sections	20-20,000	+14 DB	—92 DB	5 MA	35.00
LS-26	Bridging line to single or push pull grids	5,000 ohms	60,000 ohms in two sections	15-20,000	+20 DB	—74 DB	0 MA	25.00
LS-19	Single plate to push pull grids like 2A3, 6L6, 300A. Split secondary	15,000 ohms	95,000 ohms; 1.25:1 each side	20-20,000	+17 DB	—50 DB	0 MA	24.00
LS-21	Single plate to push pull grids. Split primary and secondary	15,000 ohms	135,000 ohms; turn ratio 3:1 overall	20-20,000	+14 DB	—74 DB	0 MA	24.00
LS-22	Push pull plates to push pull grids. Split primary and secondary	30,000 ohms plate to plate	80,000 ohms; turn ratio 1.6:1 overall	20-20,000	+26 DB	—50 DB	.25 MA	31.00
LS-30	Mixing, low impedance mike, pickup, or multiple line to multiple line	50, 125, 200, 250, 333, 500/600 ohms	50, 125, 200, 250, 333, 500/600 ohms	20-20,000	+17 DB	—74 DB	5 MA	25.00
LS-30X	As above	As above	As above	20-20,000	+15 DB	—92 DB	3 MA	32.00
LS-27	Single plate to multiple line	15,000 ohms	50, 125, 200, 250, 333, 500/600 ohms	30-12,000 cycles	+20 DB	—74 DB	8 MA	24.00
LS-50	Single plate to multiple line	15,000 ohms	50, 125, 200, 250, 333, 500/600 ohms	20-20,000	+17 DB	—74 DB	0 MA	24.00
LS-51	Push pull low level plates to multiple line	30,000 ohms plate to plate	50, 125, 200, 250, 333, 500/600 ohms	20-20,000	+20 DB	—74 DB	1 MA	24.00
LS-141	Three sets of balanced windings for hybrid service, centertapped	500/600 ohms	500/600 ohms	30-12,000	+10 DB	—74 DB	0 MA	28.00







TYPICAL LS OUTPUT TRANSFORMERS

Type No.	Primary will match following typical tubes	Primary Impedance	Secondary Impedance	±1 db from	Max. Level	List Price
LS-52	Push pull 245, 250, 6V6, 42 or 2A5 A prime	8,000 ohms	500, 333, 250, 200, 125, 50, 30, 20, 15, 10, 7.5, 5, 2.5, 1.2	25-20,000	15 watts	$28.00
LS-55	Push pull 2A3's, 6A5G's, 300A's, 275A's, 6A3's, 6L6's	5,000 ohms plate to plate and 3,000 ohms plate to plate	500, 333, 250, 200, 125, 50, 30, 20, 15, 10, 7.5, 5, 2.5, 1.2	25-20,000	20 watts	28.00
LS-57	Same as above	5,000 ohms plate to plate and 3,000 ohms plate to plate	30, 20, 15, 10, 7.5, 5, 2.5, 1.2	25-20,000	20 watts	20.00
LS-58	Pusl, pull parallel 2A3's, 6A5G's, 300A's, 6A3's	2,500 ohms plate to plate and 1,500 ohms plate to plate	500, 333, 250, 200, 125, 50, 30, 20, 15, 10, 7.5, 5, 2.5, 1.2	25-20,000	40 watts	50.00
LS-6L1	Push pull 6L6's self bias	9,000 ohms plate to plate	500, 333, 250, 200, 125, 50, 30, 20, 15, 10, 7.5, 5, 2.5, 1.2	25-20,000	30 watts	42.00

Write for our Catalog PS-409

United Transformer Co.

150 VARICK STREET NEW YORK 13, N. Y.

EXPORT DIVISION: 13 EAST 40th STREET, NEW YORK 16, N. Y., CABLES: "ARLAB"

electronics

A McGRAW-HILL PUBLICATION

JULY • 1949

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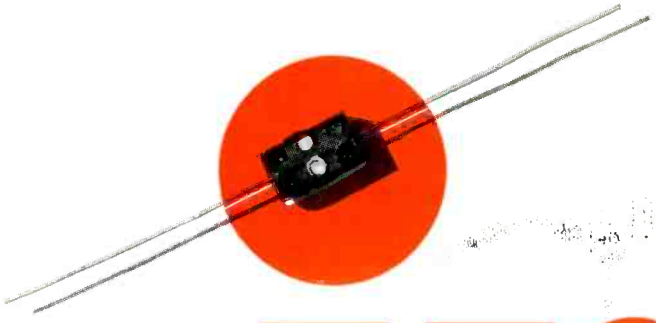

EL-MENCO'S PLACE in YOUR PRODUCT

Wherever fixed mica dielectric capacitors are used, the first choice with men of experience is always El-Menco

Precision-made under rigid conditions, tested seven ways to meet strict Army-Navy standards, thoroughly impregnated and provided in water-sealed low-loss bakelite; these tiny capacitors protect and maintain your reputation for quality equipment. To insure performance-excellence, place *El-Menco* capacitors in *your* product. Results will prove El-Menco to be a wise choice.

THE ELECTRO MOTIVE MFG. CO., Inc.
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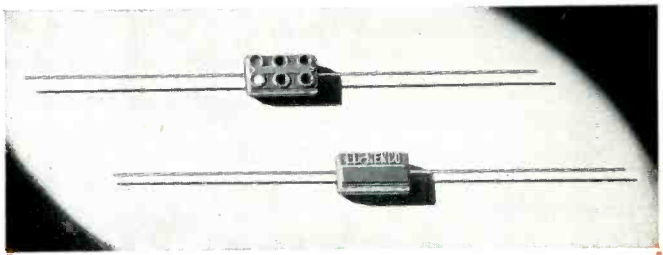

CM 15 MINIATURE CAPACITOR

Actual Size $\frac{9}{32}$" x $\frac{1}{2}$" x $\frac{3}{16}$"
For Radio, Television and Other Electronic Applications
2 to 420 mmf. capacity at 500v DC w
2 to 525 mmf. capacity at 300v DC w
Temp. Co-efficient ±50 parts per million per degree C for most capacity values
6-dot standard color coded

Write on your firm letterhead for Catalog and Samples

MOLDED MICA El-Menco MICA TRIMMER CAPACITORS

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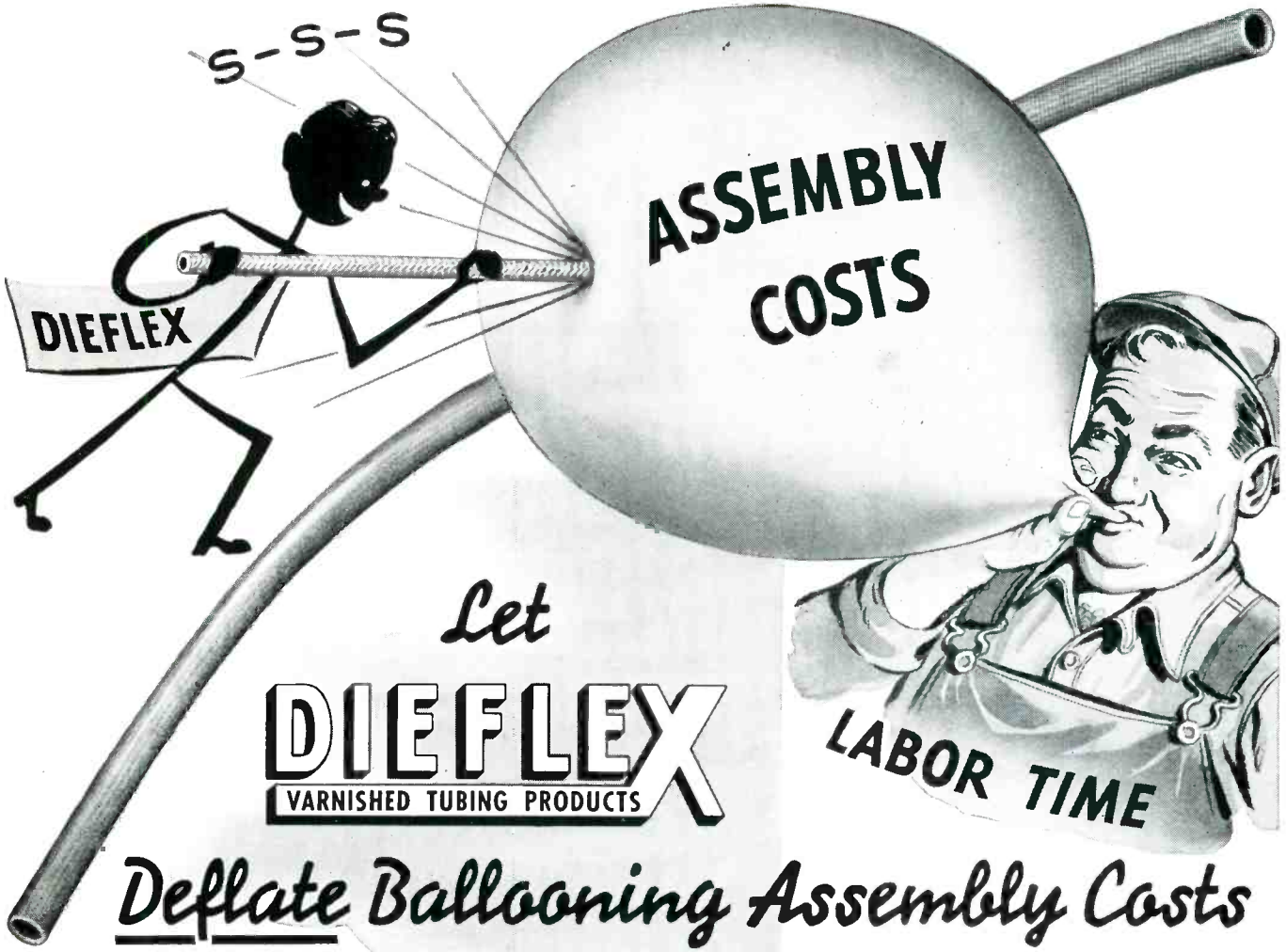

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VARNISHED TUBING PRODUCTS

Deflate Ballooning Assembly Costs

You'll be amazed how labor costs shrink when you use Dieflex Varnished Tubing products to save assembly time. Test the flexibility and stretch of Dieflex . . . see how quickly it slides over rough joints and around sharp bends . . . see how its smooth bore prevents snagging . . . how it cuts cleanly without fraying. All these features add up to easier handling and rock bottom assembly costs.

Now, beyond assembly—you can expect fewer breakdowns, reduced repair costs, minimum lost production, because Dieflex gives top mechanical and dielectric protection. Write or phone the sales office nearest you, and start deflating assembly costs today. A folder giving technical information on Dieflex products will be sent upon request.

Braided glass base varnished tubings and saturated sleevings are as inexpensive as corresponding grades of cotton base varnished tubings and saturated sleevings.

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Grade A-1 Magneto Grade Varnished Tubings
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Grade A-1 Magneto Grade Varnished Glass Tubings
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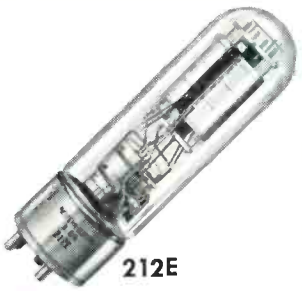
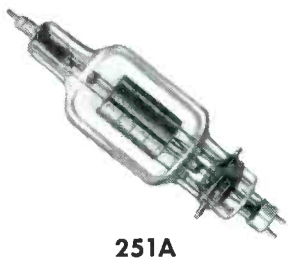


212E

343A

232B

357B



251A

233A

343AA

5541

Stay on the air...

with Western Electric tubes

SINCE the early days of the broadcast industry, Western Electric electron tubes designed by Bell Telephone Laboratories have set the pace for quality performance and long operating life.

Western Electric's line of power tubes and rectifiers for AM and FM includes many codes that have proved their dependability in stations from coast to coast.

For full information on Western Electric power tubes—now being made for Western Electric by Machlett Laboratories—call your local Graybar representative. Or write to Graybar Electric Co., 420 Lexington Ave., New York 17, N.Y.

—QUALITY COUNTS—

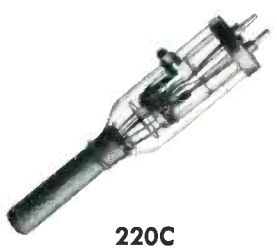
Western Electric

Distributed by Graybar — Offices in 100 principal cities

DISTRIBUTORS: IN THE U. S. A.—Graybar Electric Co. IN CANADA—Northern Electric Co., Ltd.

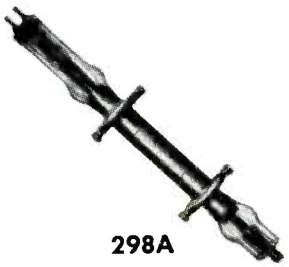
Western Electric's line of high power transmitting tubes includes:

212E	Air cooled triode, 275 watts
220C	Water cooled triode, 10 kilowatts
220CA	Forced-air cooled triode, 5 kilowatts
222A	Water cooled high vacuum rectifier, 25 kv. inverse voltage
228A	Water cooled triode, 5 kilowatts
232B	Water cooled triode, 25 kilowatts
232BA	Forced-air cooled triode
233A	Water cooled high vacuum rectifier, 50 kv. inverse voltage
236A	Water cooled triode, 20 kilowatts
240B	Water cooled triode, 10 kilowatts
241B	Air cooled triode, 275 watts
251A	Air cooled triode, 1000 watts
255B	Mercury vapor rectifier, 20 kv. inverse voltage
270A	Air cooled triode, 350 watts
279A	Air cooled triode, 1200 watts
298A & B	Water cooled triode, 100 kilowatts
308B	Air cooled triode, 250 watts
340A	Water cooled triode, 25 kilowatts
341AA	Forced-air cooled triode, 5 kilowatts
342A	Water cooled triode, 25 kilowatts
343A	Water cooled triode, 10 kilowatts
343AA	Forced-air cooled triode, 5 kilowatts
357B	Air cooled triode, vhf, 400 watts
363A	Air cooled pentode, vhf, 350 watts
379A	Air cooled triode, 1200 watts
5530	Forced-air cooled triode, vhf, 3 kilowatts
5541	Forced-air cooled triode, vhf, 10 kilowatts



220C

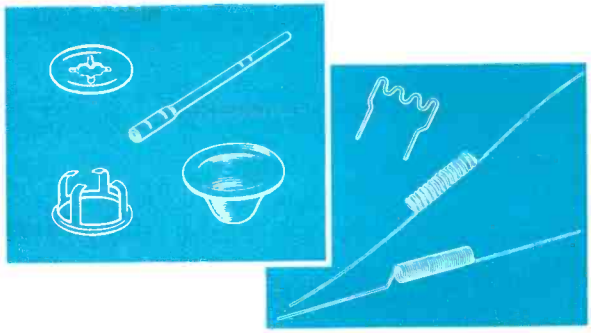
5530



298A

342A

Fansteel will fabricate



Tungsten and Molybdenum

to your specifications or *you* can fabricate in your own plant.

Fabrication processes now available from Fansteel include stamping, forming, machining and assembling.

Thirty-six years of Fansteel's specialized engineering, and every laboratory facility have greatly extended the uses of these high refractory metals for unequaled services with economy, in electrical, electronic and mechanical industries.

Fansteel production assures the utmost in purity. Fansteel metallurgy also integrates the characteristics of tungsten and molybdenum—high melting points, low vapor pressure, resistance to arc erosion and mechanical strength—with the electrical conductivity of silver and copper. Performance and durability for the severest requirements are effected.

Parts, units and complete assemblies can be fabricated by you or will be made complete to your specifications by Fansteel. You are invited to consult us on the possibilities of these metals for your applications. Fansteel Metallurgical Corporation, North Chicago, Illinois.

SOME OF THE USES OF TUNGSTEN AND MOLYBDENUM

ELECTRONIC TUBES
—tungsten for cathodes, lead-in wires and anodes—molybdenum for grids, anodes, supports.

ELECTRICAL CONTACTS
—automotive, ignition, vibrators, telegraph relays, other contacting parts in continuous service.

HEATING ELEMENTS
in electric furnaces of temperatures 1600° to 2000° C, above range of other metals.

HEATING ELEMENTS
in vacuum equipment where metals are deposited by vaporization. Do not contaminate other metals used in process.

TUNGSTEN
is chief ingredient of Fansteel "77" metal for small rotors, flywheels, balance weights, other devices where maximum weight or inertia is required in small space.

TUNGSTEN TARGETS
for all types of X-ray tubes.

INERT GAS WELDING
—tungsten electrodes sustain the arc, giving longer service.

PURE METALS
Tantalum, Tungsten, Molybdenum, and Columbium in sheet, rod, wire, special shapes and parts.

POWDER METALLURGY PRODUCTS
Finished or semi-finished shapes and parts of special analysis to achieve high strength, density, electrical conductivity, resistance to wear, impact, heat erosion, or combinations of these and other properties.

COPPER BASE ALLOYS
Copper alloyed with other elements, to combine high conductivity with strength, elasticity, resistance to heat, impact, or wear. Available in bars, rod, sheet, strip, castings, forgings, finished or semi-finished parts, for current-carrying springs and other parts, soldering tips, resistance welding electrodes, dies and fixtures.

Fansteel

11602

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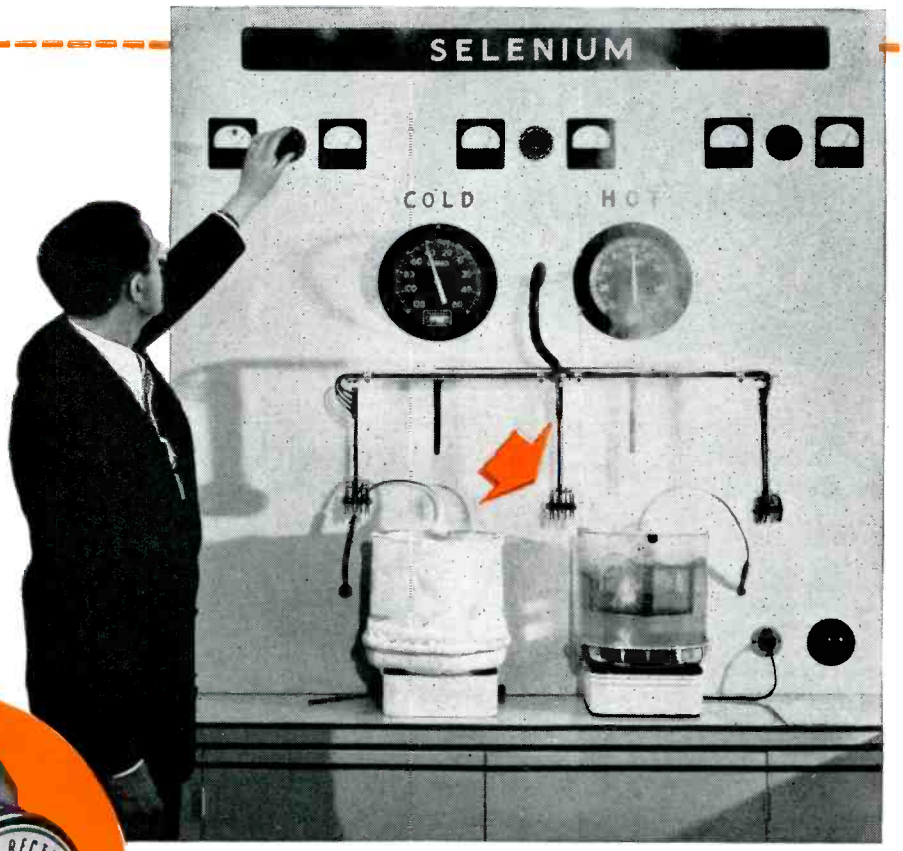
In Controlled Metallurgy

YOU CAN BE **SURE**.. IF IT'S

Westinghouse



New Selenium Licks *HIGH TEMPERATURE* ...HIGH VOLTAGE

Here's good news. Westinghouse offers you these important plus features in selenium rectifiers.

Visitors at the IRE Exposition, held recently in New York City, saw this demonstrated by a unique hot-cold shock cycle test. Every 5 minutes during the 4 days, shock changes in temperature from 40° C below zero to boiling water were applied to a Rectox 24-Volt DC/33 RMS Plate Rectifier. Variation in output was extremely small. Extensive laboratory tests at stack temperatures up to 125° C further prove ability to meet unusual requirements.

Since each plate will stand more voltage, fewer plates are needed . . . smaller stacks may be used.

The exclusive Westinghouse process of manufacture also assures lowest rate of forward aging and constant, uniform cell performance.

TRY A SAMPLE.

Test it under your own conditions. Call your local Westinghouse office for details. Westinghouse Electric Corporation, P. O. Box 868, Pittsburgh 30, Penna. J-21532

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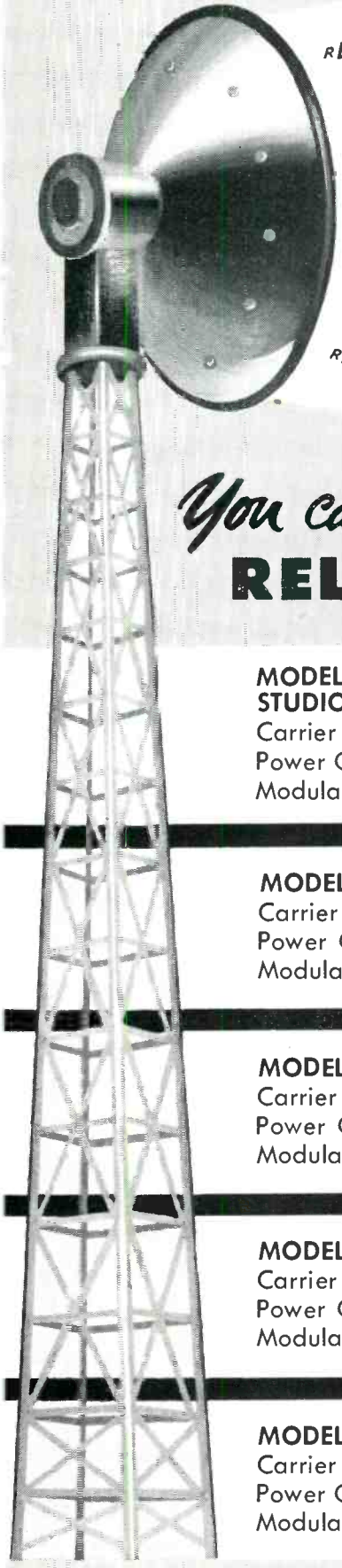
Rectox

SELENIUM RECTIFIERS

MODERN COMMUNICATIONS *Require* ABSOLUTE DEPENDABILITY



REL FM REL FM REL FM REL FM REL FM REL

MODEL 707

MODEL 751

MODEL 752

MODEL 755

MODEL 757

REL FM REL FM REL FM REL FM REL FM REL

You can **RELY** *on*
RELIABLE RELAYS BY REL

MODEL 707 HIGH FIDELITY STUDIO TO TRANSMITTER (STL) LINK:
Carrier Frequency Range...890 to 960 megacycles
Power Output.....5 watts (nominal minimum)
Modulation Range.....50 to 15,000 cycles

MODEL 751 RADIO RELAY SET:
Carrier Frequency Range...450 to 500 megacycles
Power Output.....40 watts
Modulation Range.....250 to 120,000 cycles

MODEL 752 RADIO RELAY SET:
Carrier Frequency Range...450 to 500 megacycles
Power Output.....40 watts
Modulation Range.....50 to 60,000 cycles

MODEL 755 RADIO RELAY SET:
Carrier Frequency Range...146 to 174 megacycles
Power Output.....10 or 100 watts
Modulation Range.....250 to 60,000 cycles

MODEL 757 RADIO RELAY SET:
Carrier Frequency Range...890 to 960 megacycles
Power Output.....5 watts (nominal minimum)
Modulation Range.....250 to 60,000 cycles

VARIATIONS ON THESE STANDARD DESIGNS ARE PRACTICAL AND REL INVITES YOUR INQUIRY IN SUCH SPECIAL CASES

TO THOSE WHO WANT the maximum degree of dependability in point to point equipment, REL offers the five groups listed above. These types cover practically every present day requirement including high-fidelity studio-to-transmitter links, point to point communication and multi-channel telephone and telegraph service. In each instance, the performance characteristics equal or exceed the standard requirements of the service for which the equipment was designed. Throughout all five groups, the electrical, radio and mechanical engineering exceed the exacting standards that have made REL the leader in FM since 1935. All incorporate important exclusive features found only in REL designs:

(a) All direct crystal controlled transmitters and receivers.
(b) Continuous wave for most efficient spectrum use.
(c) All sets are characterized by the low noise and distortion of FM signalling.
(d) All tubes used are conventional triode and pentode tubes and are operated conservatively enough to insure exceptionally long life.
(e) Suitable antennas for each equipment and path are available.

From any standpoint, the complete line of REL FM point to point equipment is the finest, most economical, easiest to operate and most reliable equipment of its kind available today. Write today for details, including specifications and complete descriptions of equipment to meet your needs.

RADIO ENGINEERING LABS · INC.
35-54 36th STREET
LONG ISLAND CITY 1, NEW YORK

Crowded chassis are

on resistors too!

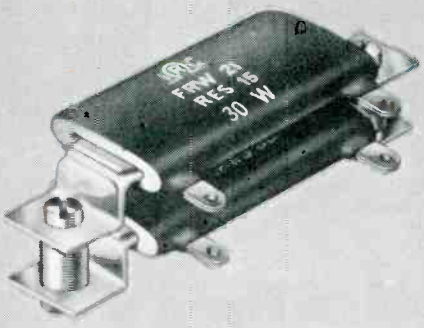
The smaller you make your electrical or electronic instruments and equipment, the bigger your problems grow. But when you specify miniature IRC resistors you conserve space without sacrificing efficiency, and miniaturization creates no bottlenecks.

Because of our years of experience in the manufacture of resistors, IRC long ago foresaw the trend to miniaturization—and prepared for it. With the widest line of resistor types in the industry, we are able now to supply miniature components for most resistor applications.

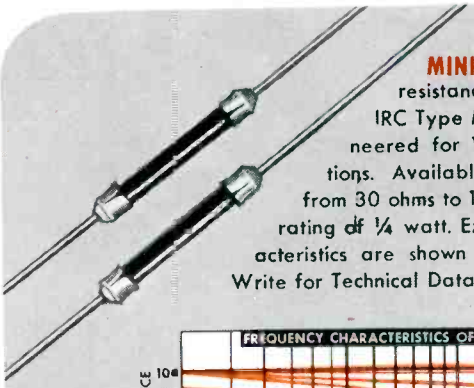
TINY Type BTR were the first miniature insulated resistors. Designed originally for the wartime VT Fuze, they have since been used with success in hearing aids and similar circuits requiring minimum size in a JAN approved resistor. ⅓ watt rating in RMA ranges up to 22 megohms. The convenient coupon brings you full details.

tough

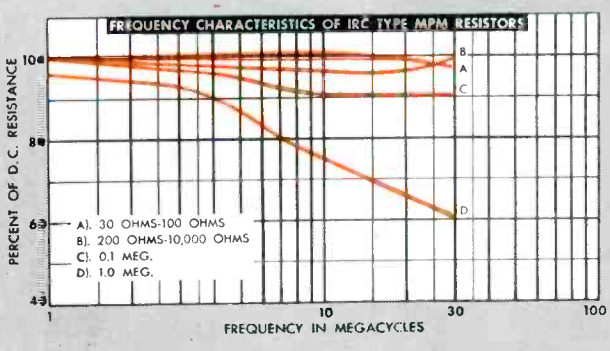
THIN AS A WAFER and no bigger than a nickel, IRC Type HB Fingertip Control features a quiet element, simplified construction and a unique rotating cover and contactor which permit ready resistance adjustment. It entirely eliminates the shaft, bushing and bulky knob of conventional-type controls. Four point switch of similar design is also available. Fully described in IRC Catalog Bulletin A-1.



FLAT POWER WIRE WOUND RESISTORS provide a higher space-power ratio than tubular types. Designed to satisfy requirements of high wattage dissipation in limited space applications, they can be mounted vertically or horizontally, singly or in stacks. The lightweight construction of these flat units includes non-magnetic mounting brackets which permit easy installation and transfer of heat to chassis. Flat FRW's are manufactured in fixed and adjustable types. Bulletin C-1 gives characteristics and specifications.



MINIATURE UNITS with active resistance section only ⅜" long, IRC Type MPM Resistors are engineered for VHF and UHF applications. Available in resistance values from 30 ohms to 1.0 megohm, at a power rating of ¼ watt. Excellent frequency characteristics are shown in the adjacent chart. Write for Technical Data Bulletin F-1.



When you are cramped for standard resistors in a hurry, IRC's Industrial Service Plan gives you the speedy service you need. For small orders of standard resistors for experimental work, pilot runs, maintenance, simply call your local IRC Distributor. We'll gladly send you his name and address.

IRC — *Wherever the Circuit Says*

Power Resistors • Precisions
Insulated Composition Resistors
Low Wattage Wire Wounds
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- ☐ Name and address of local IRC Distributor

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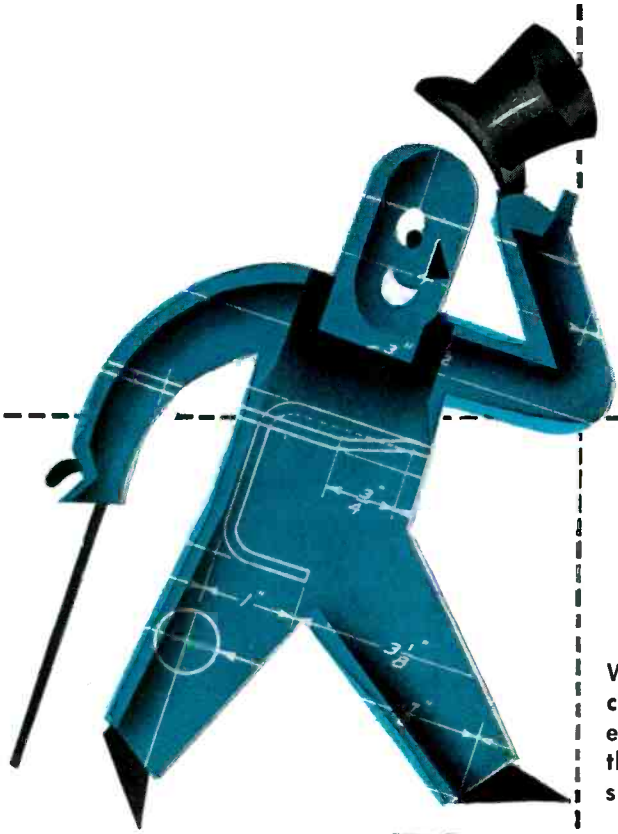

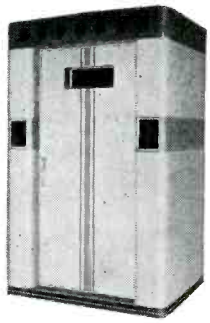

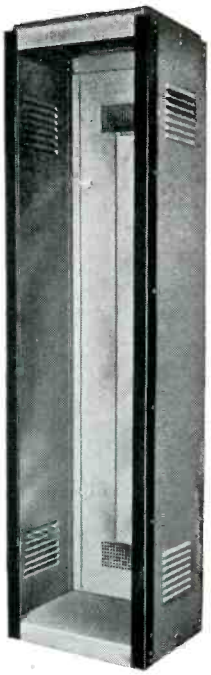

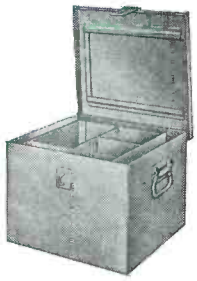

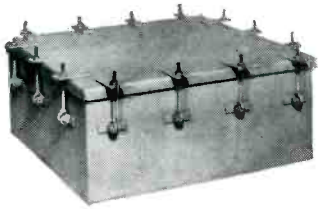

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Whether you come to us for simple stamped-out chassis, ordinary metal boxes or the most intricate electronic apparatus housing, your job will receive the same Karp quality treatment, plus every possible economy.

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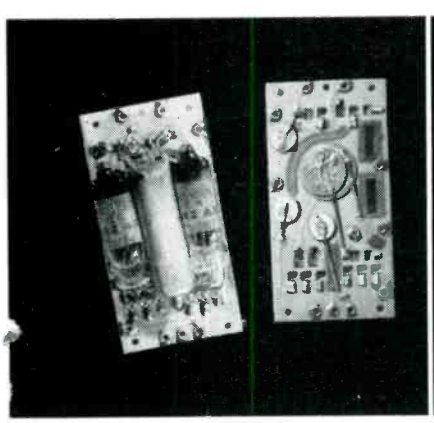
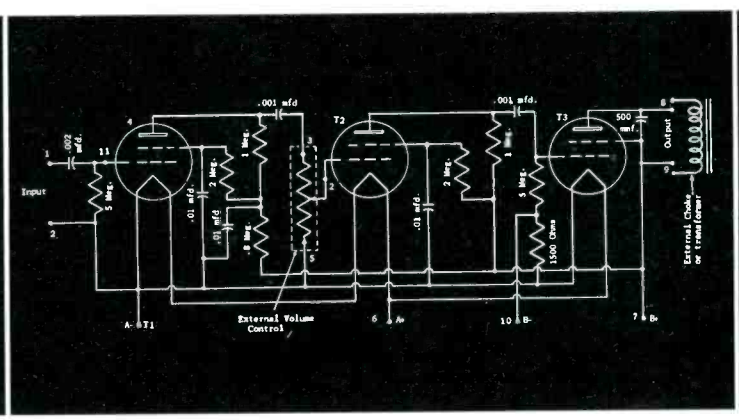
ADVENTURES IN ELECTRONIC DESIGN

HOW FRAZER CUT COSTS 60%!

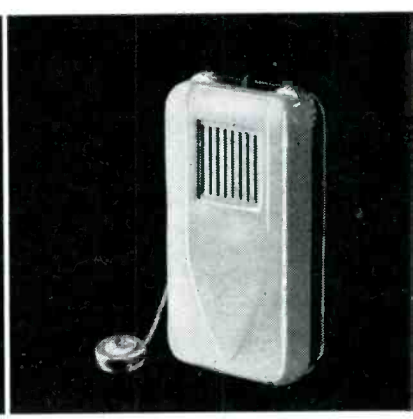
This is the success story of the Frazer Company, Auckland, New Zealand. Recently, started using Centralab's amazing P. E. C.* *Ampec* — a tiny audio-amplifier — in the hearing aids it manufactures. quickly found that with *Ampec's* help, it could produce more and finer hearing aids than ever before. What's more, Frazer found it could cut the costs of its hearing aid production nearly 3/5ths. Now — less than one year since started using Ampec, seven out of every ten deaf patients applying for hearing aids, under New Zealand's Social Security System, ask for . . . and get Frazers. Is there any doubt that is proud of being FIRST in the British Empire to use *Ampec* in hearing aids?



*Each P. E. C. unit—including *Ampec*, above — is an integral assembly of *Hi-Kap* capacitors and resistors, closely bonded to a ceramic plate and connected by "printed" silver paths.



This is a schematic diagram of *Ampec*, Centralab's amazing P. E. C. unit that combines all components of an audio-amplifier — tube sockets, capacitors, resistors and wiring — on one compact, ceramic chassis.



Here's the Frazer Hearing Aid. Because it uses *Ampec*, the Frazer is smaller, lighter. What's more, *Ampec* helps Frazer produce more dependable hearing aids, faster.

Centralab — **DEVELOPMENTS THAT CAN HELP YOU**

Division of GLOBE-UNION INC. • Milwaukee

Centralab reports to

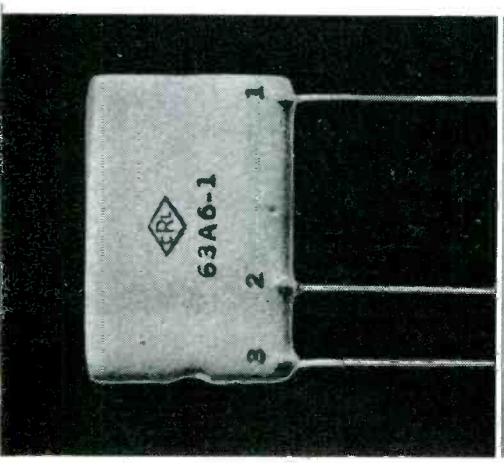
JULY, 1949

How Admiral Uses CRL's Printed Electronic Circuit to build more and finer TV sets!

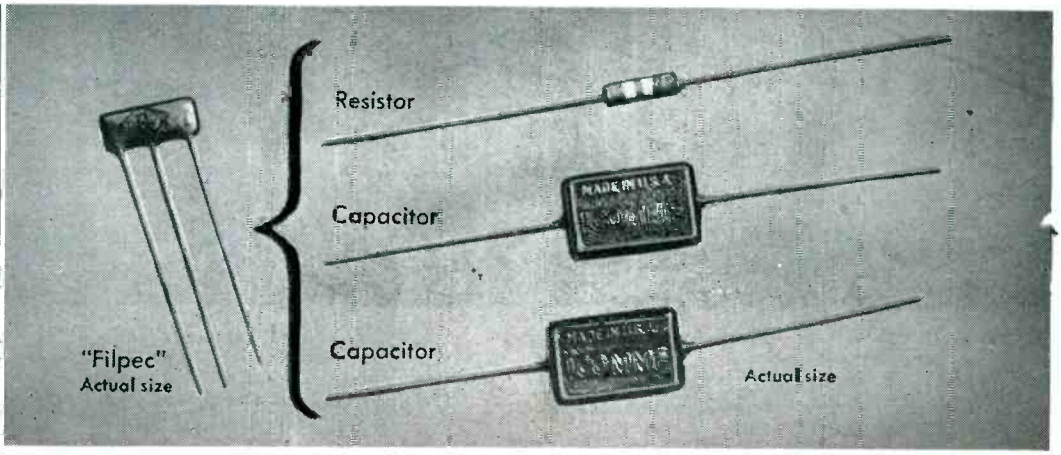
Arrow points to CRL's new *VERTICAL INTEGRATOR NETWORK*—used by Admiral engineers to save space and cut assembling time of their new TV models.

Chassis courtesy of Admiral Corp.

1 Wherever Centralab's revolutionary P. E. C. is used, you are sure to find speeded production . . . quality products. Just look at Admiral Corporation's fine new television receivers. A series of Admiral's video sets makes use of CRL's *Vertical Integrator Network* — a tiny, compact plate containing both capacitors and resistors. It saves production time . . . reduces 16 soldered connections to 3. Simplifies wiring operations for faster assembly. What's more, the *Network* helps produce better TV receivers.

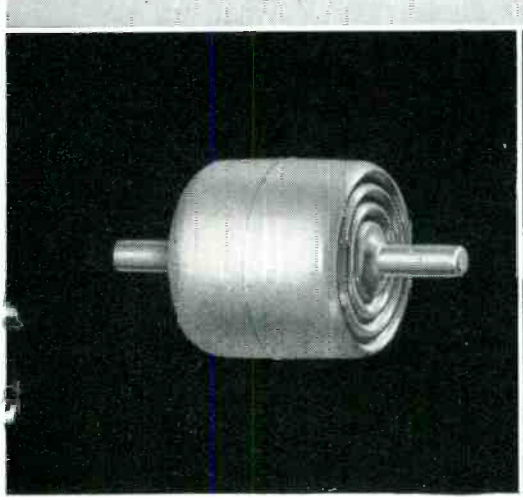


2 This is the new CRL *Vertical Integrator Network* used by Admiral. Variations of this Centralab *Network* are available on special order.

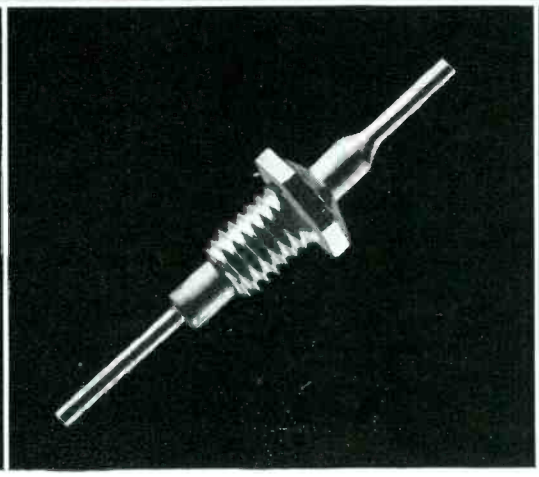


3 Centralab's *Filpec* is designed for use as a balanced diode load filter, combines up to three major components into one tiny unit, lighter and smaller than one ordinary capacitor. Whats more, *Filpec's* Ceramic-X construction assures long life. Capacitor values from 50 to 200 mmf. Resistor values from 5 ohms to 5 megohms.

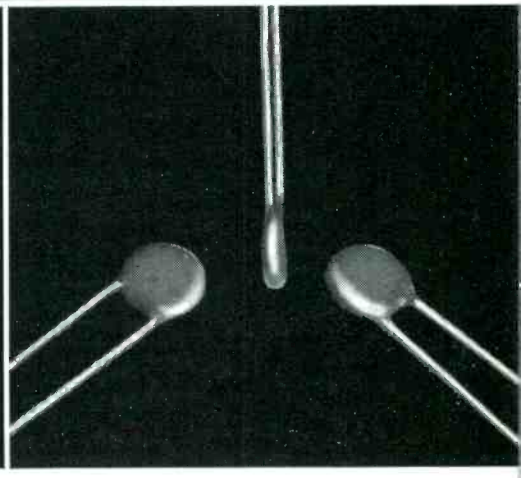
Electronic Industry



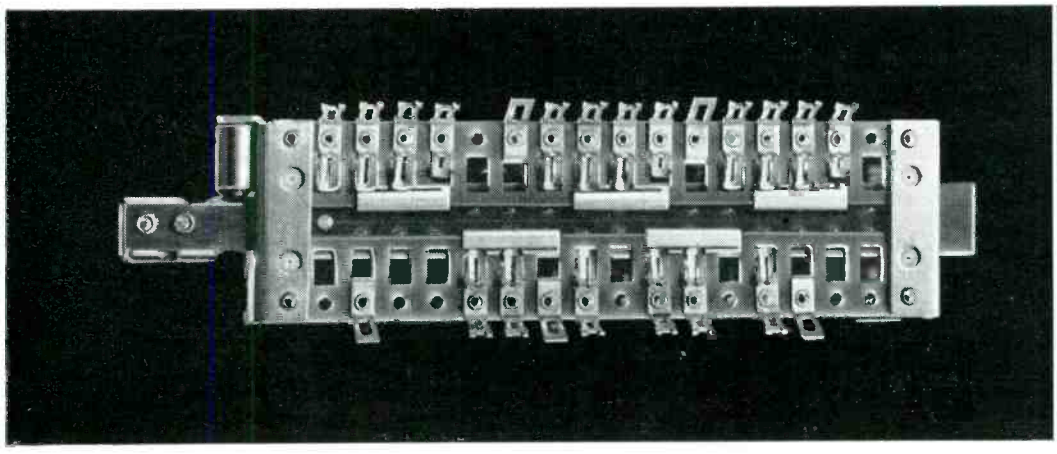
4 *Hi-Vo-Kaps* are filter and by-pass capacitors combining high voltage, small size and a variety of terminal connections to fit most TV needs.



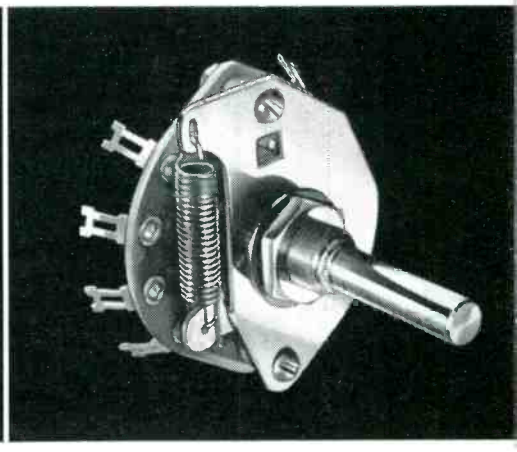
5 FT *Hi-Kaps* Centralab's new feed-thru or bushing mounted capacitors eliminate structural and electrical damage during installation.



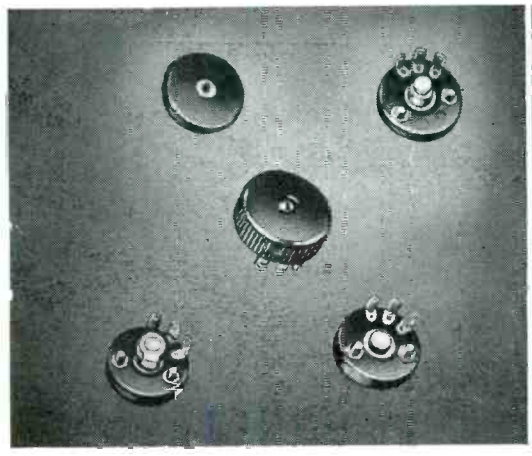
6 For by-pass or coupling applications, check CRL's original line of ceramic disc and tubular *Hi-Kaps*. *Disc Hi-Kaps* are smaller than a dime!



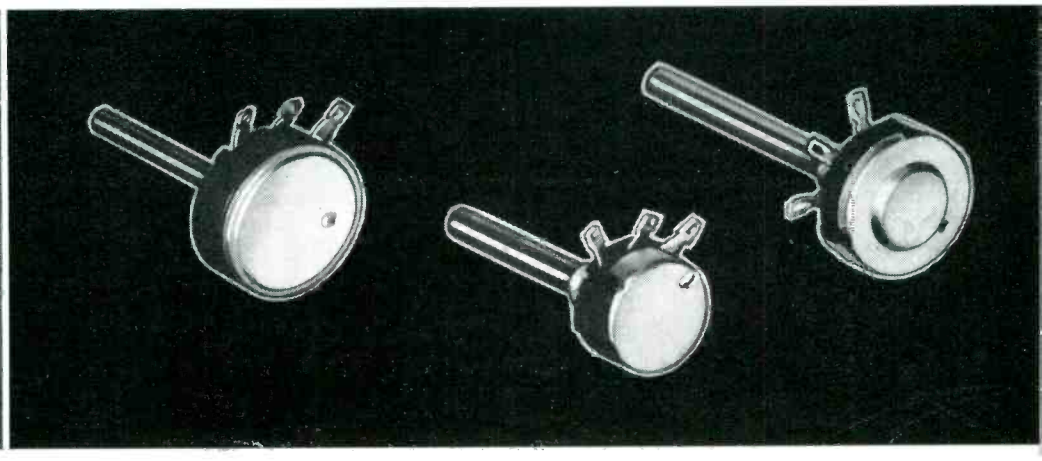
7 Centralab's development of a revolutionary, new *Slide Switch* promises improved AM and FM performance! Flat, horizontal design saves valuable space, allows short leads, convenient location to coils, reduced lead inductances for increased efficiency in low and high frequencies. CRL *Slide Switches* are rugged and efficient, too.



8 Great step forward in switching is CRL's New *Rotary Coil and Cam Index Switch*. Its coil spring gives you smoother action, longer life.



9 Model "1" *Radiohm* control is no larger than a dime. Especially designed for hearing aids, pocket radio receivers, miniature amplifiers.



10 Let Centralab's complete *Radiohm* line take care of your special needs. Wide range of variations: *Model "R"* — wire wound, 3 watts; or composition type, 1 watt. *Model "E"* — composition type, ¼ watt. Direct contact, 6 resistance tapers. *Model "M"* — composition type, ½ watt.

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42-4 — BC DISC HI-KAPS — miniature ceramic BC capacitors.
42-10 — HI-VO-KAPS — high voltage capacitors for TV application.
695 — CERAMIC TRIMMERS — CRL trimmer catalog.
991 — HI-VO-KAPS — capacitors for TV application. For jobbers.
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814 — CAPACITORS — high-voltage capacitors.
975 — FT HI-KAPS — feed-thru capacitors.

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970 — LEVER SWITCH — shows indexing combinations.
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42-7 — MODEL "1" RADIOHM — world's smallest commercially produced control.
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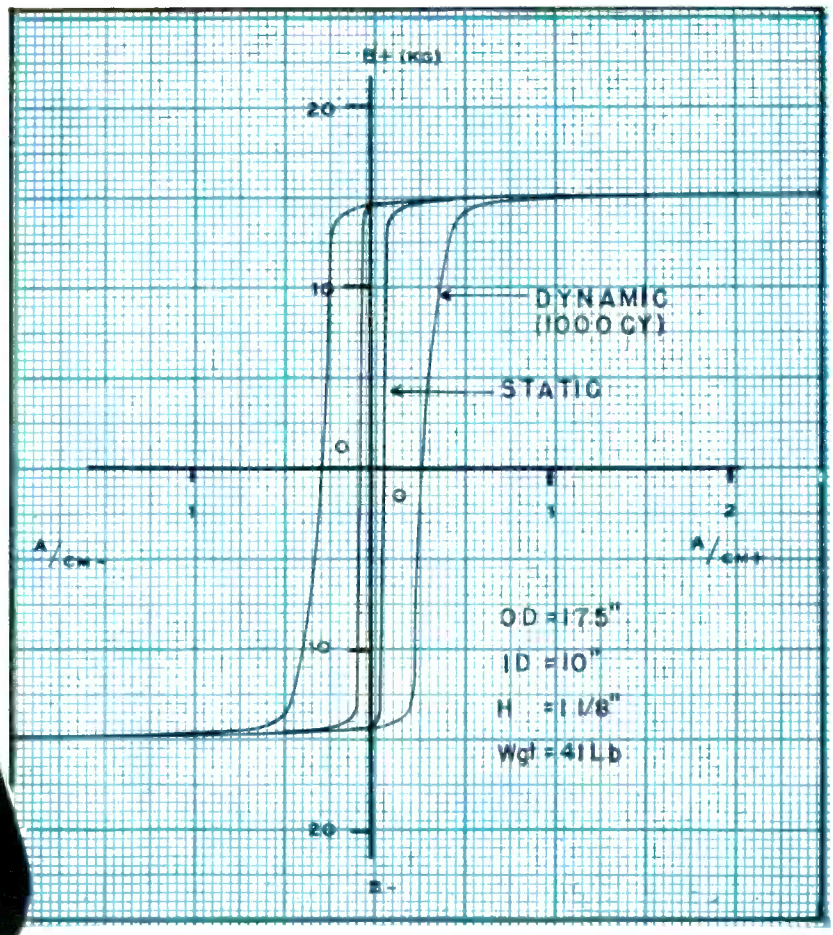


Take another look at Permeron*

. . . I-T-E'S NEW MAGNETIC CORE MATERIAL

Get the full significance of the static and dynamic (1000 cycle) magnetization characteristics of this new alloy. Examine the dynamic curve particularly — as this indicates how the material acts under actual operating conditions.

Note these facts:

1. Magnetic saturation is achieved with only the slightest change in magnetizing current.
2. The extremely low magnetizing current makes it possible to build smaller magnetic amplifiers of extreme reliability.
3. The knees of the saturation curve are sharp, even at higher frequencies.
4. The most important fact: all Permeron cores have identical magnetization characteristics. The dynamic characteristic of each core is checked by a "Vectormeter," specially developed for this purpose. This consistency allows designers to predict amplifier performance accurately and positively.

Permeron Cores are available now

in widths of 20 mm. and 30 mm., in any specified inside and outside diameters. Cores are delivered heat treated and insulated. They are always furnished in housings designed to protect the magnetic material against deformation.

Take Another Look at Permeron — and continue to look to I-T-E to bring you better equipment and better designs . . . *first!*

* Formerly known as "Permanite"

For Additional Information write — I-T-E Rectifier Division or consult your local I-T-E Representative

I-T-E PERMERON

I-T-E CIRCUIT BREAKER COMPANY
19th AND HAMILTON STREETS, PHILADELPHIA 30, PA.

SWITCHGEAR • UNIT SUBSTATIONS • ISOLATED PHASE BUS STRUCTURES • RESISTORS • SPECIAL PRODUCTS • MECHANICAL RECTIFIERS

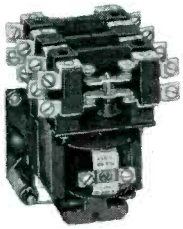
FIXED RESISTORS

In all standard R.M.A. values as follows—½ watt from 10 ohms to 22 megohms; 1 watt from 2.7 ohms to 22 megohms; 2 watt from 10 ohms to 22 megohms. Small in size; tops in quality.

ADJUSTABLE RESISTORS

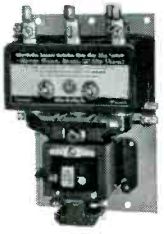
Type J Bradleyometers can produce any resistance-rotation curve. Resistor element is solid-molded as a one-piece ring that is unaffected by age, wear, heat, or moisture. Can be supplied in single-, dual-, or triple-unit construction for rheostat or potentiometer applications. Built-in line switch is optional on single or dual types.

SMALL CONTACTORS



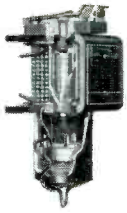
Bulletin 700 Universal Relays are available in 10-amp rating with 2, 4, 6, and 8 poles. Two contact banks permit quick changes from normally open to normally closed contacts. The double-break, silver-alloy contacts require no maintenance. There are no pins, pivots, bearings, or hinges to bind, stick, or corrode.

LARGE CONTACTORS



Bulletin 702 Solenoid Contactors are available for ratings up to 300 amperes. Arranged for 2- or 3-wire control with push buttons or automatic pilot devices. Enclosing cabinets furnished for all service conditions. The double-break, silver-alloy contacts need no maintenance. For complete description and dimensions, please send for Bulletin 702.

TIMING RELAYS



Bulletin 848 Timing Relays are ideal for any service requiring an adjustable, delayed-action relay. They have normally open or normally closed contacts. The magnetic core is restrained from rising by the piston in fluid dashpot. Ideal for transmitter plate voltage control. Time delay period of these relays is adjustable.

LIMIT SWITCHES

Essential for safety interlocks on transmitter cabinets. Also used for sequence switching, restricting machine motions, and starting, stopping, and reversing motors. Let us send you Bulletin 701-2.

RESISTORS • RELAYS • CONTACTORS

for Quality Electronic Equipment

When you design an electronic device that must meet rigid performance specifications... your component parts must be "tops" in quality. For such applications, the leading electronic engineers use Allen-Bradley fixed and adjustable resistors; Allen-Bradley relays and contactors; Allen-Bradley standard and precision limit switches. Let us send you data on all items listed above. In war service and in peacetime applications, Allen-Bradley components are the choice of electronic engineers for television and radar circuits.

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A-B Quality

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RESISTORS RELAYS
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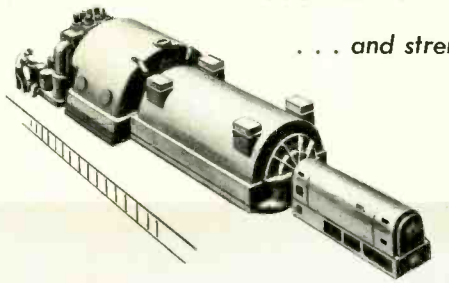
Plastics where plastics belong

for dimensional stability

. . . wear resistance

. . . and strength



Synthane pump bearings used in this Allis-Chalmers vertical mixed flow pump illustrate an interesting application of Synthane requiring stability of dimensions within close tolerances under conditions of severe exposure to wear and water. Other interesting applications for Synthane result from its many additional properties in combination—a few of which are high dielectric strength, good structural strength, light weight, low moisture absorption, and corrosion resistance.

In the Allis-Chalmers pump shown above Synthane was selected as standard bearing material in all units pumping clear water. Tests indicated that Synthane did not swell excessively when constantly immersed in water. In these installations water is the only lubricant.

These few of Synthane's many desirable qualities may suggest its use in your products or process. If so, why not let us help with design, material, or fabricated parts. Write today for the Synthane Plastics Catalog. Synthane Corporation, 6 River Road, Oaks, Pennsylvania.

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DESIGN • MATERIALS • FABRICATION • SHEETS • RODS • TUBES
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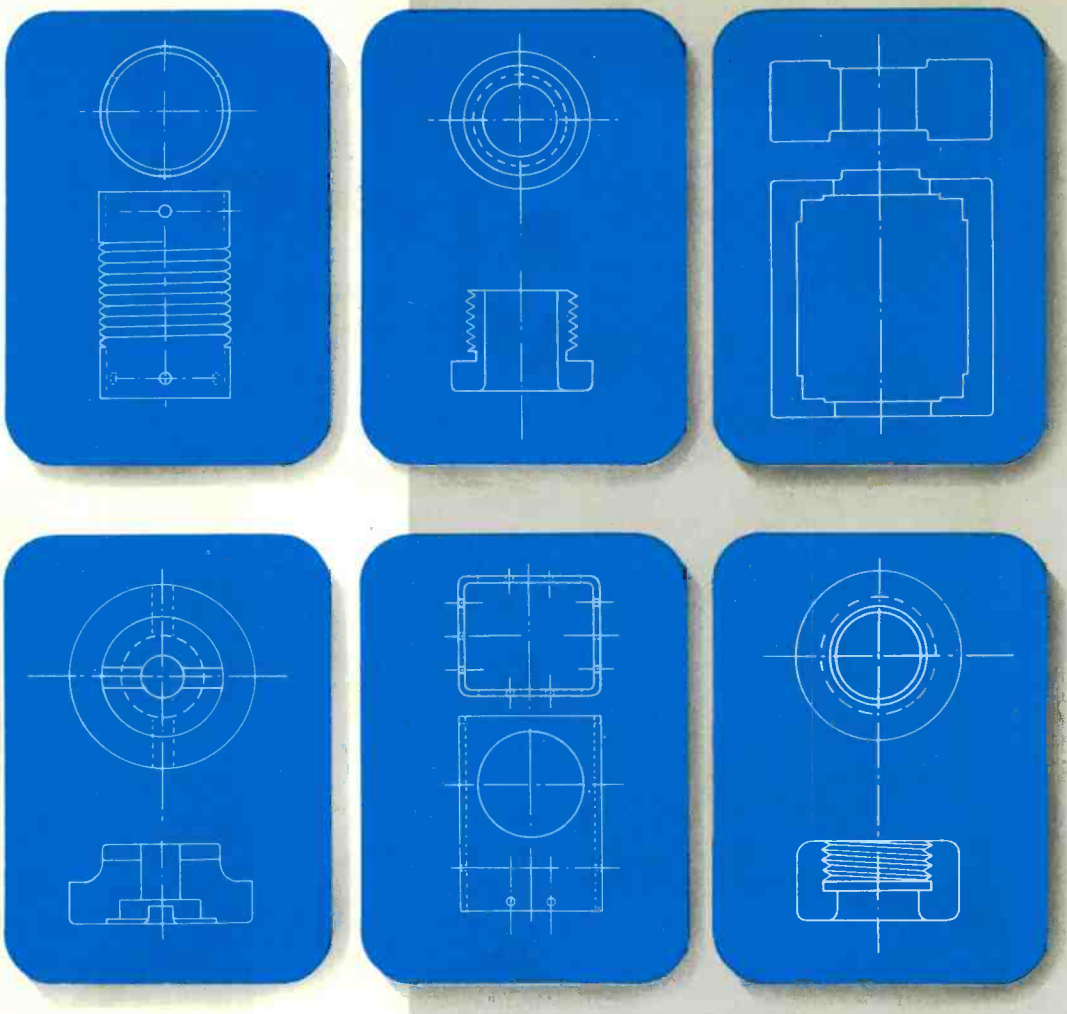
Question:

What 3 points have these 7 JOBS in common?



ANSWER:

1. All of them have an unusual combination of requirements.
2. All of them are made from Synthane laminated plastics.
3. All of them are machined from Synthane tubes or rods.

QUESTION: *What properties in combination?*

ANSWER:

Properties such as structural strength; light weight; toughness; moisture and corrosion resistance; dimensional stability; hardness; abrasion resistance; low coefficient of expansion; and desirable characteristics for electrical applications, as low power factor, high dielectric strength, low dielectric constant.

QUESTION: *Is Synthane easy to machine?*

ANSWER:

Synthane tubes and rods are easily and quickly machined by standard shop equipment, including saws, drills, lathes, millers, punch presses, and automatic screw machines.

QUESTION: *Does Synthane produce finished parts?*

ANSWER:

Synthane produces rods and tubes, helps you design for use of plastics, and delivers top quality finished parts. Send for the Tubing Folder today.

SYNTHANE CORPORATION, 6 RIVER ROAD

Oaks, Pennsylvania

Please send me the Synthane Tubing Folder by return mail

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Company _____

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Address _____

City _____ *Zone* _____ *State* _____

Synthane produces a wide variety of shapes. For example: a—round tubes or rods, b—square or irregular tubes or rods, c—oval tubes or rods, d—angles or channels, e—irregular bore or insert.

Standard round tubing is always a little more economical to use, but if your needs call for an irregular shaped section, it will pay you to inquire about Synthane's diversified line of rods and tubes.

Specifications:

Diameters: Rod—⅛" to 4" O.D.
Tubing—⅛" to 22" I.D., O.D. to specifications.
(Molded tubing to 4" O.D. only.)

Lengths: 18" to 36", longer on order

Colors: Natural (Tan) or black

Finishes: Ground, buffed or varnished

For diameter or wall thickness tolerances, standards of quality for tensile and compressive strength, dielectric strength, density, percent of moisture absorption, power factor, and dielectric constant, write for descriptive Tubing Folder.

SYNTHANE

SYNTHANE CORPORATION OAKS • PENNSYLVANIA

Representatives in ALL Principal Cities

LOW CURRENT PAYS OFF...

with the GENERAL ELECTRIC PM-EM* FOCUS COIL!

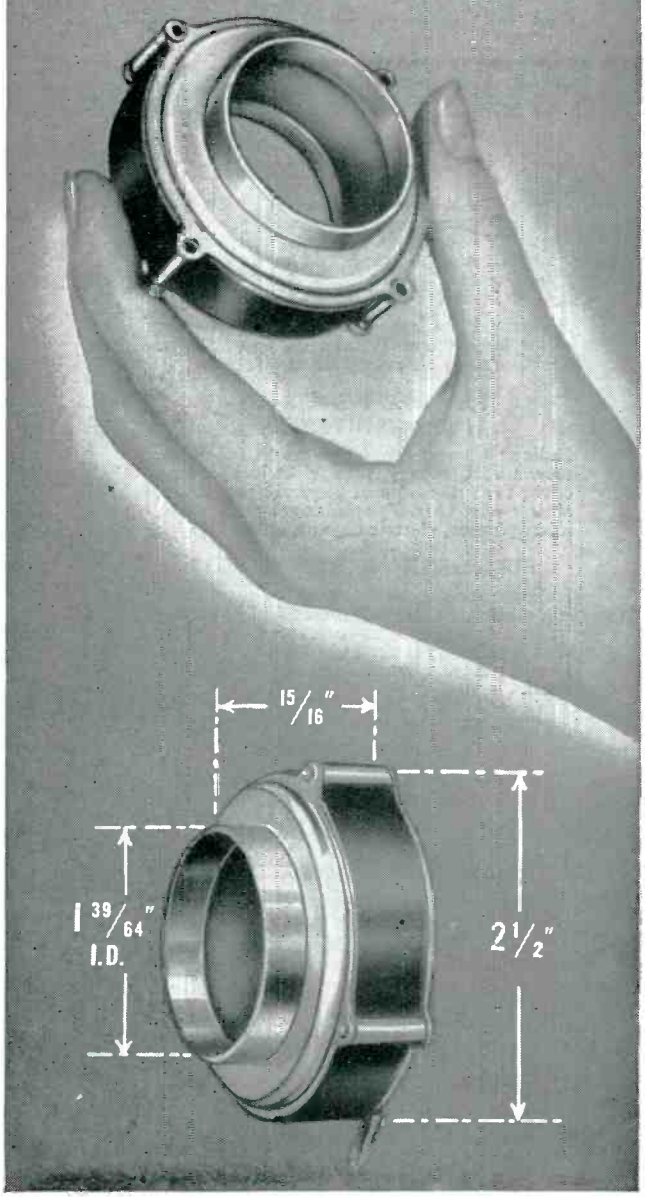
PERFORMANCE-ENGINEERED at Electronics Park, the General Electric Focus Coil is now being used by many leading television manufacturers. The reason for this widespread adoption of the G-E Focus Coil by design engineers is best explained by the following equation:

PEM = I^2R = $.109^2$ x 247 = 2.93 watts
PEM–PM = ^2R = $.029^2$ x 960 = 0.81 watts
Power Saving = 2.12 watts

In addition to its low current requirements (which permit the use of lower-priced power supplies) the G-E focus coil is small, compact and light in weight. These features provide additional space which TV set designers can use to advantage.

For complete information on the G-E Focus Coil and other television components, write: *General Electric Company, Electronics Park, Syracuse, New York.*

**Permanent Magnet—Electro-Magnet.*



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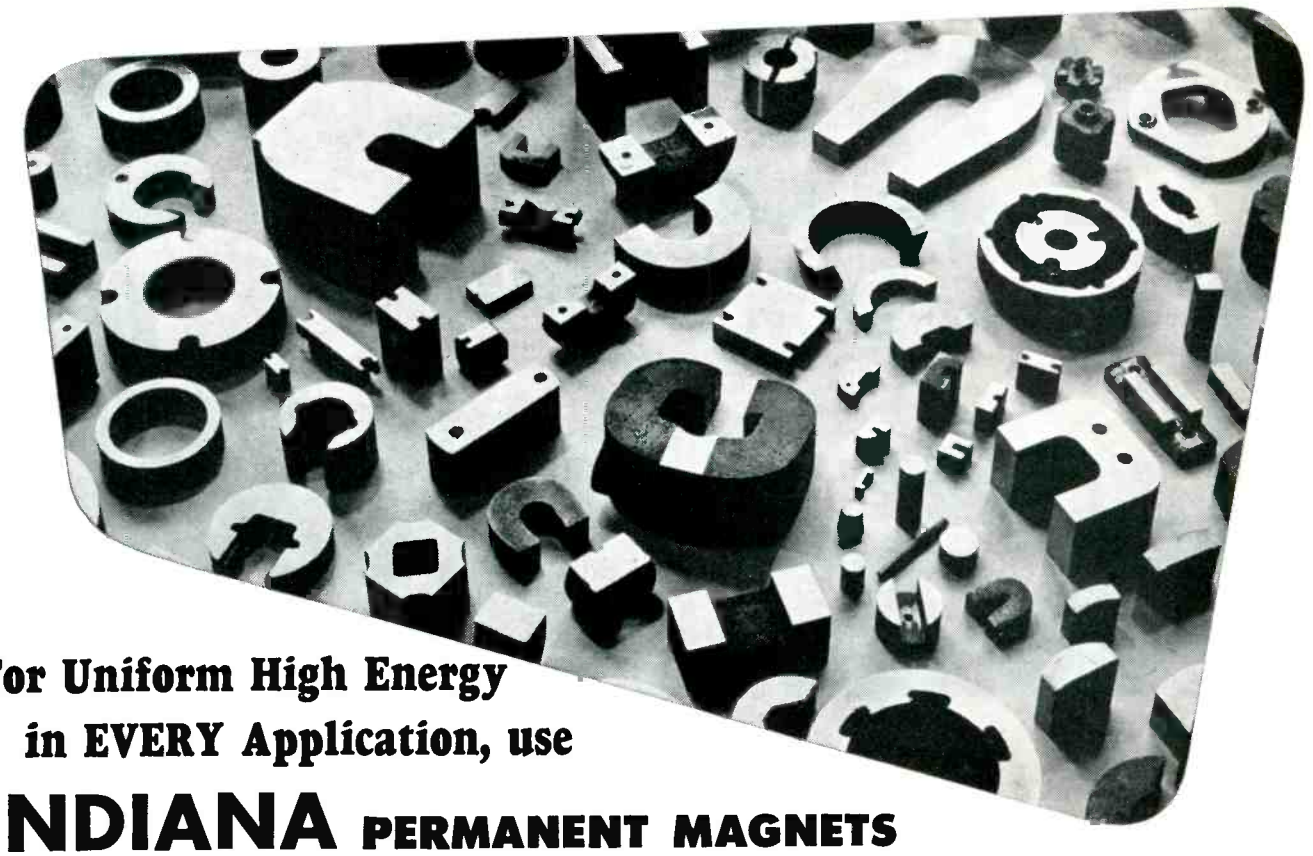
GENERAL ELECTRIC



For Uniform High Energy in EVERY Application, use

INDIANA PERMANENT MAGNETS

THIN-WALL ALNICO RINGS

All sizes of thin-wall, ring-type permanent magnets for television focus coils. Indiana quality assures a strong magnetic field.

"ION-TRAP" PERMANENT MAGNETS

Permanent magnets to deflect electrons out of the ion-electron stream. Made of Alnico and Cunife in all diameters and forms.

PERMANENT MAGNETS FOR PHONOGRAPH PICK-UPS

Indiana permanent magnets for transforming mechanical energy into electrical energy cover the full range of physical properties, sizes, and shapes. For phonograph pick-ups, microphones, electric organs, etc.

PERMANENT MAGNETS FOR SPEAKERS

Indiana permanent magnets for transforming electrical energy into mechanical energy in loud speakers, telephone receivers, polarized vibrators, electric clocks, etc. Indiana has the right permanent magnet for each need.

PERMANENT MAGNETS FOR INSTRUMENTS, RELAYS, AND CONTROLS

A complete variety for ammeters, galvanometers, light meters, voltage regulators, switches, polarized relays, etc. Indiana brings you the latest methods and techniques.

PERMANENT MAGNET SUB-ASSEMBLIES

Assemblies, of which the permanent magnet is a part, designed to meet your specifications. Furnished for all requirements.

● Look to INDIANA for *quality* permanent magnets—for skill in manufacture—for cost-cutting engineering aid. Strict supervision in every step of production is your assurance of exact magnetic and mechanical characteristics.

ALL MATERIALS • ALL SIZES • ALL SHAPES

INDIANA—the world's largest exclusive producer of permanent magnets, and the only manufacturer furnishing *all commercial grades* of permanent magnet alloys—has the know-how and facilities to develop and produce the permanent magnets you require. More than 30,000 different needs have been met successfully by INDIANA "packaged energy." Write today.

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Indalloy
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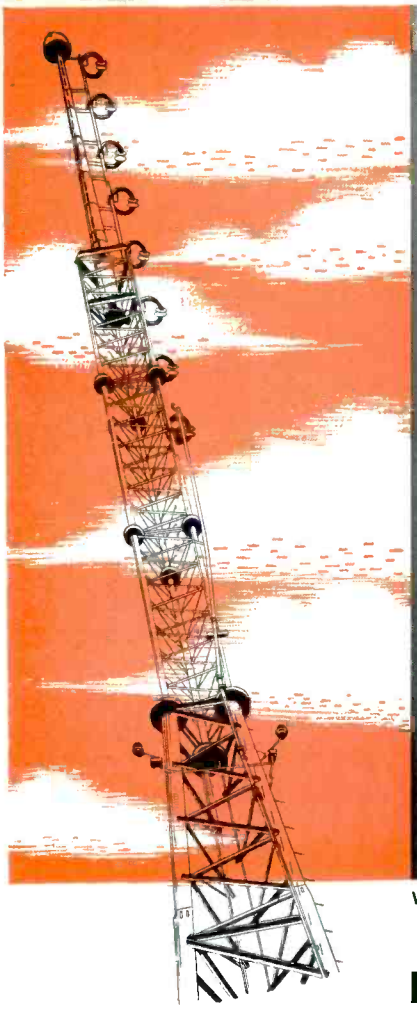
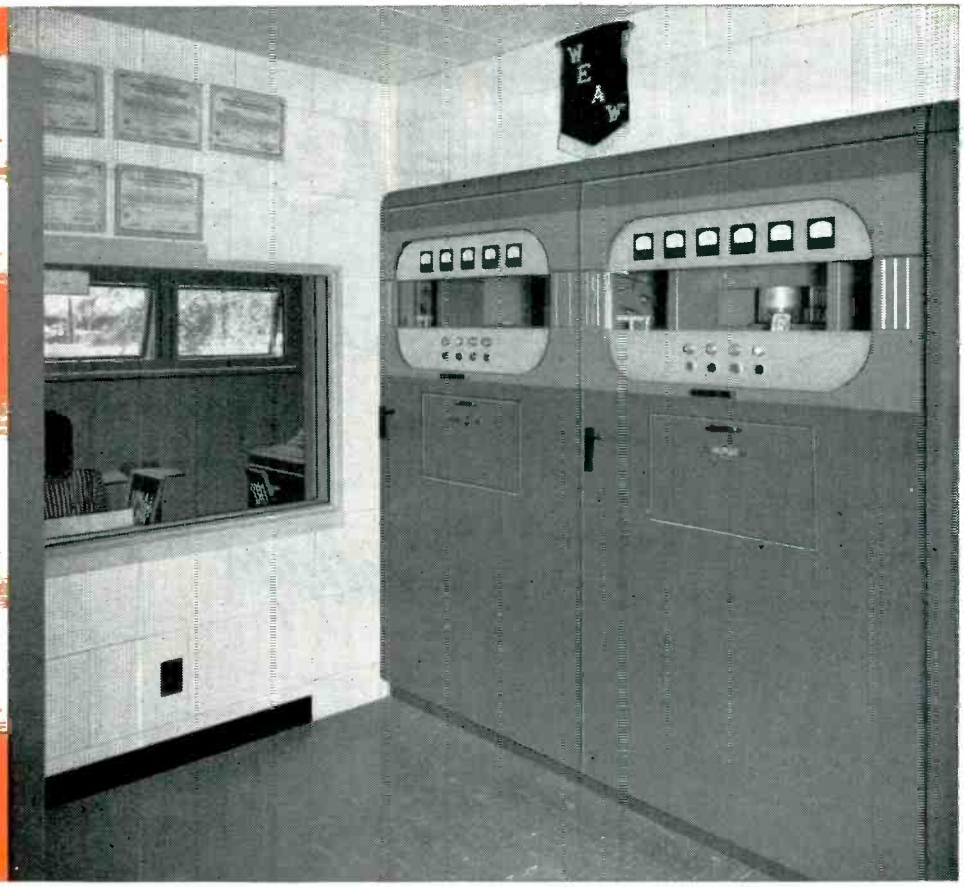
INDIANA PERMANENT MAGNETS

THE INDIANA STEEL PRODUCTS COMPANY

6 NORTH MICHIGAN AVENUE • CHICAGO 2, ILLINOIS

SPECIALISTS IN "PACKAGED ENERGY" SINCE 1908





WEAW-FM's 37M-8 eight-bay antenna

WEAW-FM's 737A "5 kw" transmitter

Nominal power rating: 5 kw FM ... actually a 6½ kw transmitter

WEAW-FM, Evanston, Illinois, has been radiating 36 kilowatts with the Collins 737A "5 kw" transmitter and the Collins 37M-8 eight-bay antenna shown on this page.

Recently the station's management applied to FCC for permission to increase its effective radiated power from 36 to 45 kilowatts.

This increase can be made without buying a more powerful transmitter . . . without even using all the power of which the present transmitter is capable.

Although it is nominally rated in the 5 kw classification, the Collins 737A is actually a 6½ kilowatt FM transmitter.

Operated conservatively, with a 37M-8 Collins antenna having a gain of 8.3, this transmitter presents plenty of power to the transmission line to cover line loss and furnish the 45 kw of radiated power for which WEAW-FM has applied.

The Collins 737A transmitter with a 4-to 8-bay Collins 37M antenna is your best and most economical equipment with which to radiate FM power in the range of 20 to 45 kilowatts. Write us for literature which will give you more complete information.

FOR THE BEST IN FM, IT'S . . . COLLINS

COLLINS RADIO COMPANY, Cedar Rapids, Iowa

11 West 42nd Street, New York 18, N. Y. **458 South Spring Street, Los Angeles 13, California**

ELECTRONICS

Designers

Now..higher voltage

from

GENERAL ELECTRIC

SELENIUM STACKS

using new 18-volt (D-C) cells

New process for depositing selenium gives rectifier stacks greater uniformity, higher efficiency and longer useful life.

Here's real news for rectifier users. G.E.'s new 18-volt selenium cells, made by a special evaporation process which deposits selenium on the aluminum base with greater uniformity than otherwise possible, give you these advantages:

GREATER OUTPUT—With 50% more output than the standard 12-volt cells, the new design can be used for any application except those few which demand 24-hour, year-around service.

HIGHER EFFICIENCY—Not only is the initial efficiency higher, but more uniform coating keeps it high during the life of the stack.

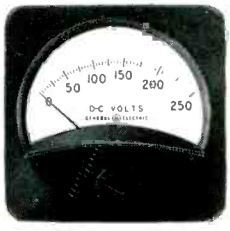
SAVING IN SPACE—About one-quarter less space is required for the same output.

LOWER COST—Depending on the voltage across the stack, the 18-volt cells can save 25% in cost compared to standard 12-volt cells.

Selenium stacks are available in several standard sizes. Output in d-c voltage ranges from 18 to 126; applied a-c voltage, from 26 to 161. Bulletin GEA-5258 will give you detailed information. Send for it today!

STYLED FOR READABILITY BUILT FOR RELIABILITY

This brand-new line of 2½-inch thin panel instruments has streamlined features which will give your panels a "new look." Arc lines have been eliminated,



GENERAL ELECTRIC

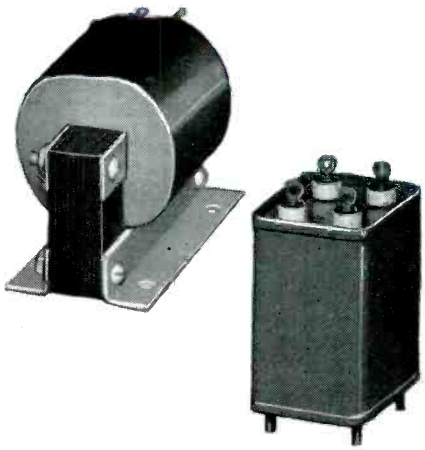
Digest

TIMELY HIGHLIGHTS ON G-E COMPONENTS

leaving only the upright scale divisions. New tapered pointer helps eye focus only on the reading. All but essential markings are masked by attractive case.

Internal mechanism is designed for extra reliability. High coercive Alnico magnet assures proper alignment, even under severe operating conditions. Large air gap reduces danger of stickiness caused by foreign particles. A variety of types and ratings in round or square cases are available for use in radio, television or testing equipment. Get complete details from Bulletin GEC-368.

DESIGNED FOR YOUR REQUIREMENTS



General Electric pulse transformers for radar and associated applications are designed to perform dependably in extremes of operating conditions. Many ratings in current production are of a special nature—designed to keep pace with rapidly changing requirements of the industry. However, for certain applications, they can be built to the specifications of electronic equipment manufacturers. Types available include interstage transformers, blocking oscillator transformers, charging chokes, current transformers, and pulse thyratron grid transformers. For a listing of available designs and ratings, send for bulletin GEC-481.

THEY'RE SMALL BUT THEY CAN TAKE IT

Cast-glass bushings with sealed-in nickel-steel hardware can be readily welded, soldered, or brazed directly to the apparatus, thus eliminating gaskets and providing a better seal. Small, compact structure often makes possible reduction of over-all size and weight of equipment. Practically unaffected by weathering, micro-organisms, and thermal shock, they're particularly well suited for use in electronic equipment and in installations where operating conditions are severe. Available in ratings up to 8.6 kv and for currents to 1200 amperes. Check Bul. GEA-5093.

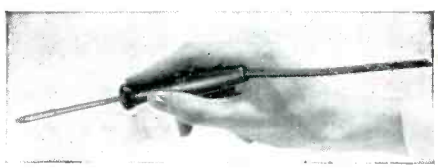
RELY ON THESE FOR STABILITY

Fixed paper-dielectric capacitors are manufactured in accordance with joint Army-Navy specification JAN-C-25. They're constructed with thin Kraft paper, oil or Pyranol* impregnated, for stable characteristics and high dielectric strength. Plates are aluminum foil; special bushing construction provides for short internal leads, prevents possible grounds and short circuits. Cases have permanent hermetic seal.

Case style CP 63 (shown above) is rated 0.1–0.1 muf and 1000 volts. Other ratings range from .01 muf to 15 muf and from 100 to 12,500 volts. Write for detailed description and operating data in bulletin GEA-4357A.
*Reg. U.S. Pat. Off.

DOES A BIG JOB IN CLOSE QUARTERS

G.E.'s midget soldering iron can do a big job with only one-fourth the wattage usually used. This handy 6-volt, 25-watt iron is only 8 inches long with $\frac{1}{8}$" or $\frac{1}{4}$" tips and weighs but $1\frac{3}{4}$ ounces. Designed for close-quarter, pinpoint precision soldering, the "midget" offers you all these advantages: low cost soldering; "finger-tip" operation; quick, continuous heat; easy renewal; long life; low maintenance. A real aid in designing radios, instruments, meters, electric appliances, and many other products requiring precision soldering. Available from stock. Check bulletin GEA-4519.



General Electric Company, Section A667-2
Apparatus Department, Schenectady, N. Y.
Please send me the following bulletins:

- ☐ GEA-4357A D-C Capacitors
- ☐ GEA-4519 Midget Soldering Iron
- ☐ GEA-5093 Glass Bushings
- ☐ GEA-5258 Selenium Stacks
- ☐ GEC-368 Panel Instruments
- ☐ GEC-481 Pulse Transformers

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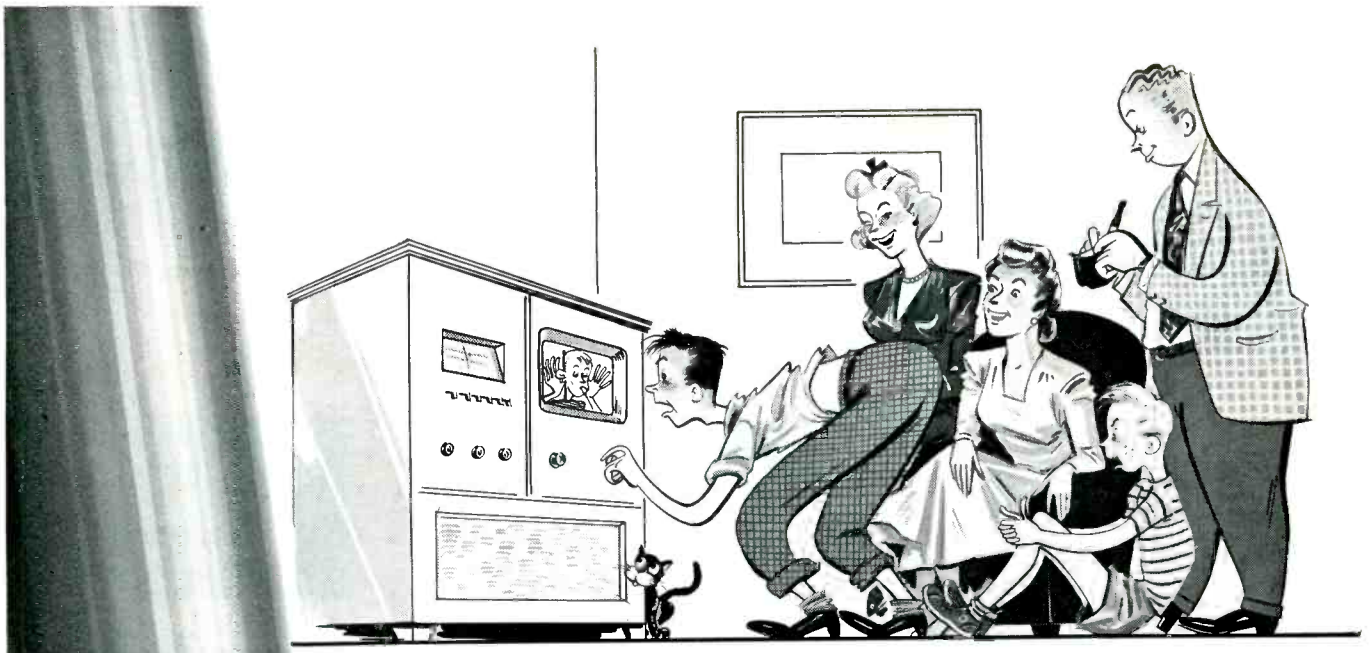


FOR A SHARPER IMAGE OF

TOP PROFITS IN TELEVISION PRODUCTION and SALES

. . . set-builders use

AMERICAN PHILLIPS SCREWS

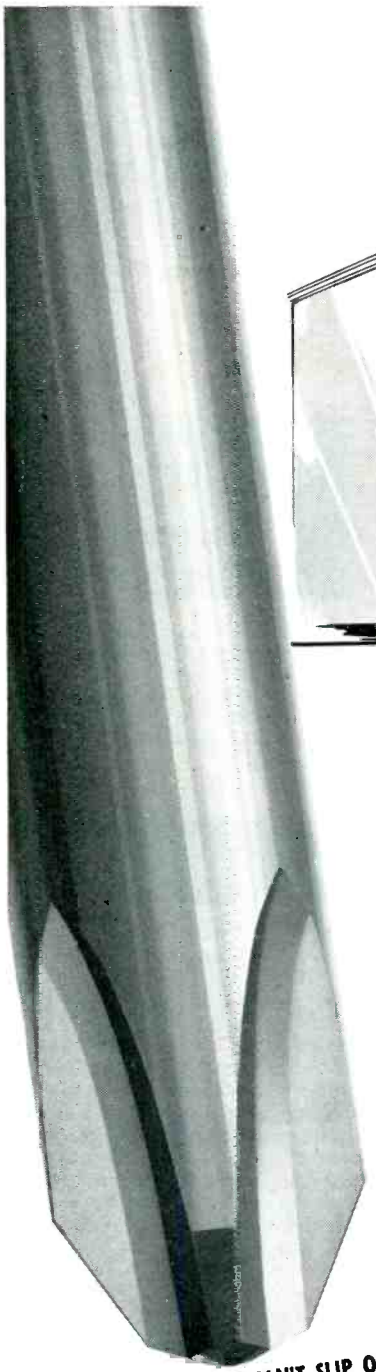
SEE NEW PRODUCTION PROFITS: Assembly of costly television sets puts a prohibition on spoilage. That's why American Phillips Screws are used, to help keep sets rolling out to an eager market, and to keep rejections down. No delays or losses, then, and output hits the main channel with highest return per man-hour, *which means time-savings up to 50%!*

SEE NEW SALES-STIMULATION: Smoothly finished, unmarred cabinet work is the basis of television-set sales. And that's the way sets come from an assembly department using *American Phillips Screws.*

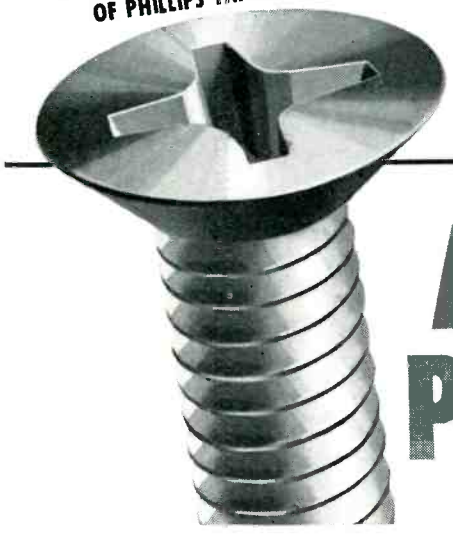
Does YOUR product have this double-feature of production-economy and sales promotion? Then write:

AMERICAN SCREW COMPANY, PROVIDENCE 1, RHODE ISLAND

Chicago 11: **589 E. Illinois St.** *Detroit 2:* **502 Stephenson Building**



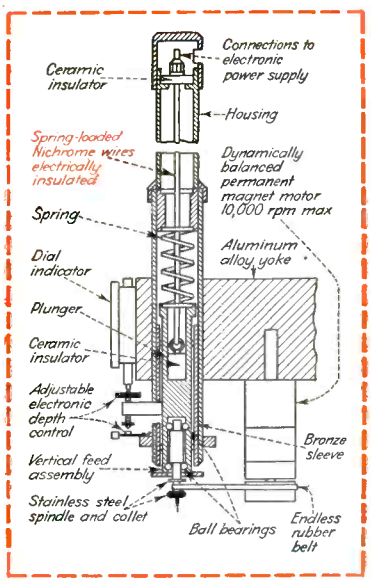
4-WINGED DRIVER CAN'T SLIP OUT OF PHILLIPS TAPERED RECESS



AMERICAN PHILLIPS *Screws*

ALL TYPES
ALL METALS: Steel, Brass, Bronze, Stainless Steel, Aluminum, Monel, Everdur (silicon bronze)

a Revolutionary method of drilling microscopic holes that depends on NICHROME*



High coefficient of linear expansion of Nichrome V permits maximum vertical movement of spindle with shortest possible length of wire.

High tensile strength of Nichrome V permits use of a spring large enough to furnish sufficient force to drive spindle down.

High heat-resistance of Nichrome V permits heating wire to 1700°F. without permanent elongation—affording substantial drill feed range.

High specific resistance of Nichrome V minimizes heating current required.

Until now, precision drilling of extremely small diameter holes (such as .0016″ dia.) has been manually controlled. Even with highly skilled operators, however, drill breakage has been frequent—resulting in waste of time and effort, and damage to work and equipment.

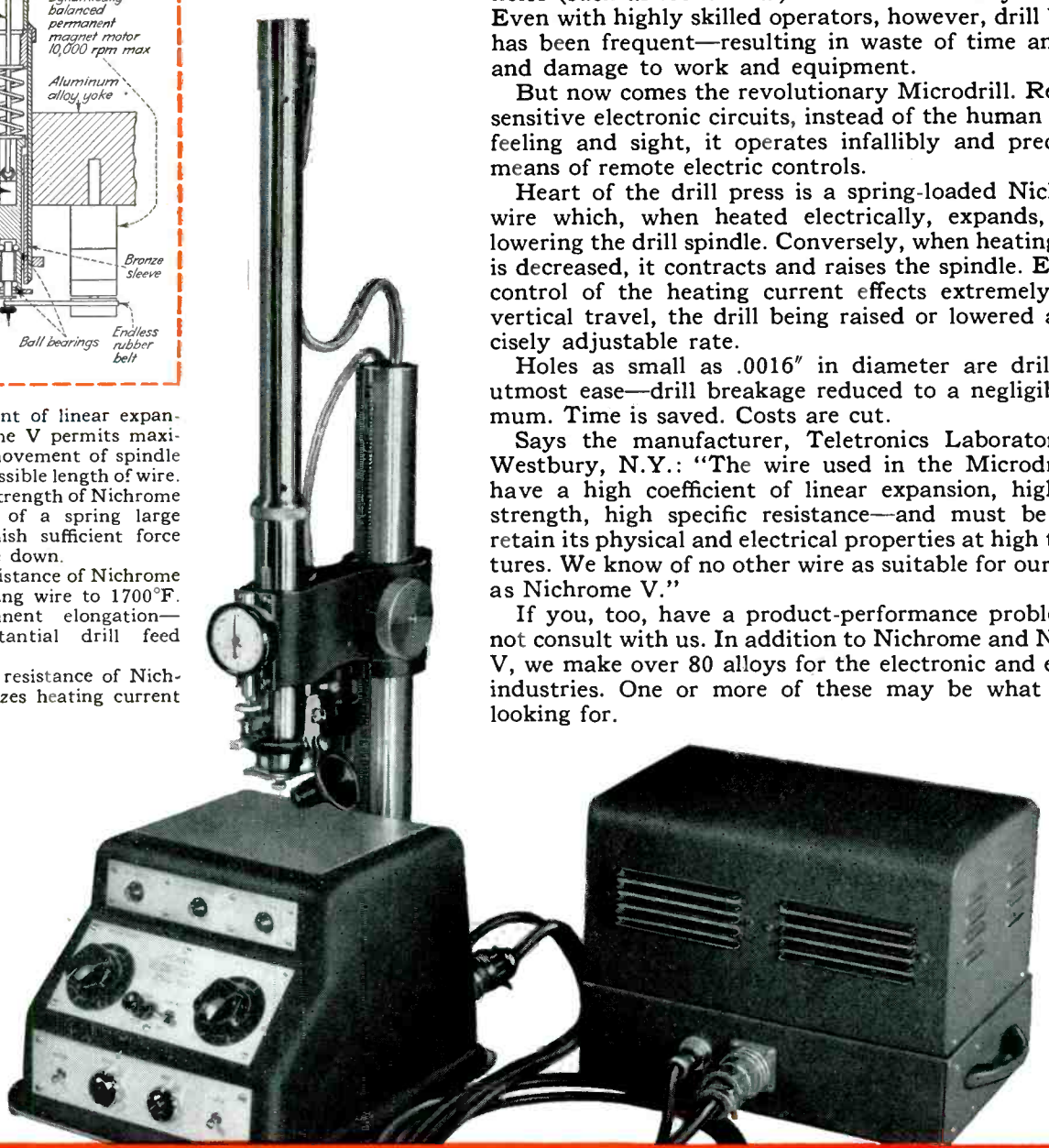
But now comes the revolutionary Microdrill. Relying on sensitive electronic circuits, instead of the human senses of feeling and sight, it operates infallibly and precisely by means of remote electric controls.

Heart of the drill press is a spring-loaded Nichrome V wire which, when heated electrically, expands, thereby lowering the drill spindle. Conversely, when heating current is decreased, it contracts and raises the spindle. Electronic control of the heating current effects extremely smooth vertical travel, the drill being raised or lowered at a precisely adjustable rate.

Holes as small as .0016″ in diameter are drilled with utmost ease—drill breakage reduced to a negligible minimum. Time is saved. Costs are cut.

Says the manufacturer, Teletronics Laboratory, Inc., Westbury, N.Y.: "The wire used in the Microdrill must have a high coefficient of linear expansion, high tensile strength, high specific resistance—and must be able to retain its physical and electrical properties at high temperatures. We know of no other wire as suitable for our purpose as Nichrome V."

If you, too, have a product-performance problem, why not consult with us. In addition to Nichrome and Nichrome V, we make over 80 alloys for the electronic and electrical industries. One or more of these may be what you are looking for.



50TH YEAR — SPECIAL PURPOSE ALLOYS SINCE 1899 — DH — TRADE MARK REG. U. S. PAT. OFF. — 1899 - 1949

*Nichrome is manufactured only by

Driver-Harris Company

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BRANCHES: Chicago, Detroit, Cleveland, Los Angeles, San Francisco, Seattle
Manufactured and sold in Canada by
The B. GREENING WIRE COMPANY, LTD., Hamilton, Ontario, Canada

*T.M. Reg. U. S. Pat. Off.

SIE *Custom-Built*

TRANSFORMERS

At Standard Stock Prices

SIE, one of the leading designers and manufacturers of transformers and reactors for the petroleum geophysical industry, is a recognized specialist in the low frequency field of transformers and sub-sonic hermetically sealed transformers and reactors.

As a result of recently expanded plant capacity and the latest innovations in manufacturing techniques, SIE is now in a position to produce highest quality *custom-built* transformers and reactors to any desired specifications at standard stock prices.

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MEASURE TOTAL DISTORTION
Between 20 cps and 20 kc

330B DISTORTION ANALYZER

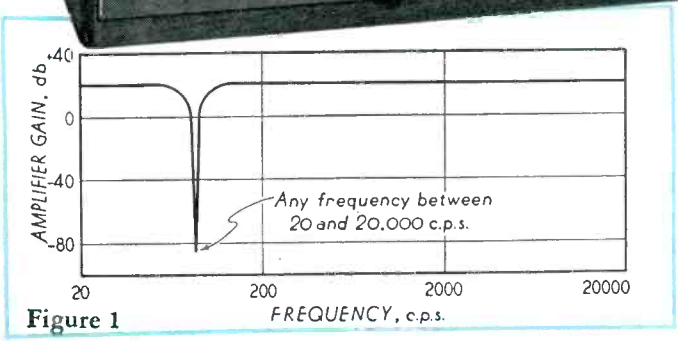

Figure 1

CHECK THESE SEVEN IMPORTANT FUNCTIONS:

1. **Measures total audio distortion.**
2. **Checks distortion of modulated r-f carrier.**
3. **Determines voltage level, power output.**
4. **Measures amplifier gain and response.**
5. **Directly measures audio noise and hum.**
6. **Determines unknown audio frequencies.**
7. **Serves as high-gain, wide-band stabilized amplifier.**

This fast, versatile *-hp-* 330B Analyzer measures distortion at *any* frequency from 20 cps to 20 kc. Measurements are made by eliminating the fundamental and comparing the ratio of the original wave with the total of remaining harmonic components. This comparison is made with a built-in vacuum tube voltmeter.

The unique *-hp-* resistance-tuned circuit used in this instrument is adapted from the famous *-hp-* 200 series oscillators. It provides almost infinite attenuation at one chosen frequency. All other frequencies are passed at the normal 20 db gain of the amplifier. Figure 1 shows how attenuation of approximately 80 db is achieved at any pre-selected point between 20 cps and 20 kc. Rejection is so sharp that second and higher harmonics are attenuated less than 10%.

Full-Fledged Voltmeter

As a high-impedance, wide-range, high-sensitivity vacuum tube voltmeter, this *-hp-* 330B gives precision response flat at any frequency from 10 cps to 100 kc. Nine full-scale ranges are provided: .03, .1, .3, 1.0, 3.0, 10, 30, 100 and 300. Calibration from +2 to −12 db is provided, and ranges are related in 10 db steps.

The amplifier of the instrument can be used in cascade with the vacuum tube voltmeter to increase its sensitivity 100 times for noise and hum measurements.

Accuracy throughout is approximately ±3% and is unaffected by changing of tubes or line voltage variations. Output of the voltmeter has terminals for connection to an oscilloscope, to permit visual presentation of wave under measurement.

Measures Direct From R-F Carrier

The *-hp-* 330B incorporates a linear r-f detector to rectify the transmitted carrier, and input circuits are continuously variable from 500 kc to 60 mc in 6 bands.

Ease of operation, universal applicability, great stability and light weight of this unique *-hp-* 330B Analyzer make it ideal for almost any audio measurement in laboratory, broadcast or production line work. Full details are immediately available. Write or wire for them—today Hewlett-Packard Company, 1437A Page Mill Road, Palo Alto, Calif.

hp laboratory instruments
FOR SPEED AND ACCURACY

Noise and Distortion Analyzers — Wave Analyzers — Frequency Meters
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Amplifiers — Power Supplies — UHF Signal Generators — Attenuators
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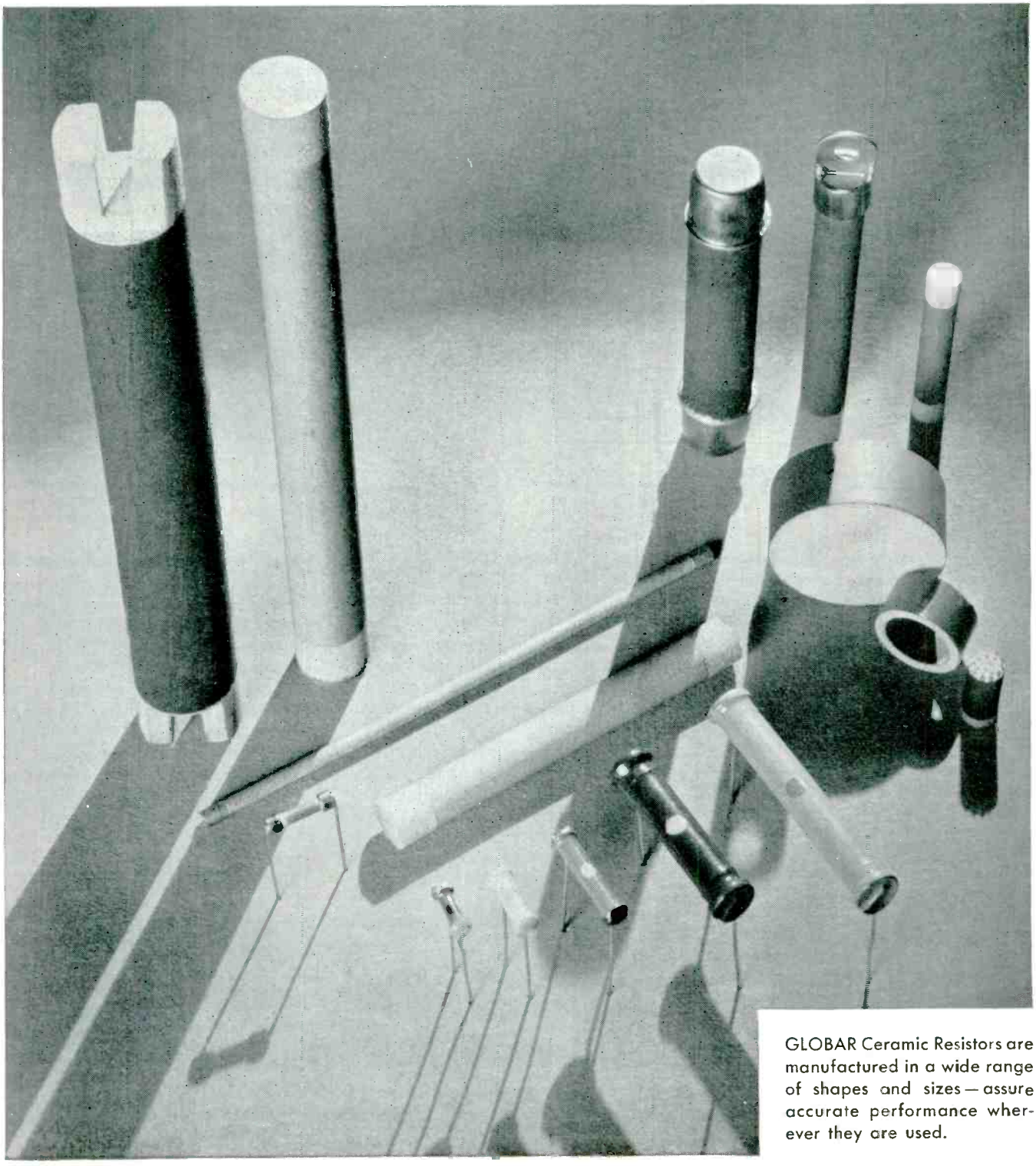
How GLOBAR TRADE MARK



GLOBAR Ceramic Resistors are manufactured in a wide range of shapes and sizes — assure accurate performance wherever they are used.

Resistors Improve Product Performance

THE performance of electronic circuits in radio, television and industrial applications is improved through the use of GLOBAR Brand Ceramic Resistors. That's because GLOBAR resistors are made to meet the exact needs of your circuit. Through careful attention to design and composition, characteristics are imparted which insure accurate operation under the most difficult conditions. In many instances, they provide the most economical way of supplying resistor requirements.

The accompanying table lists a few of the general characteristics and typical applications of GLOBAR resistors. Where required, working samples of each of these types can be supplied for engineering tests. When requesting samples, complete information on your circuit should be furnished.

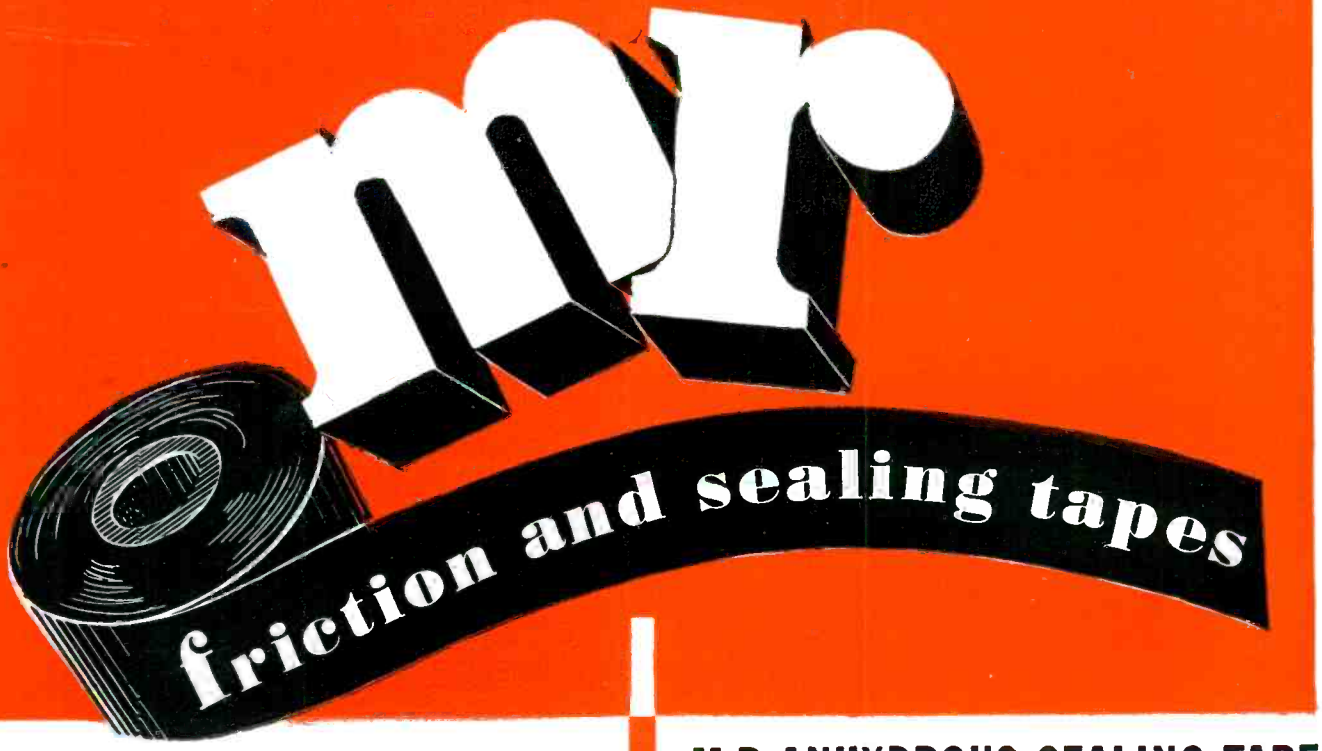
Bulletin R contains useful engineering data on GLOBAR Ceramic Resistors. Copies will be supplied immediately upon request. There is no obligation. Write Dept. V-79, The Carborundum Company, GLOBAR Division, Niagara Falls, N. Y.

TYPE	CHARACTERISTICS	TYPICAL APPLICATIONS
A	Low negative voltage and temperature sensitivity.	General purpose resistor for radio receivers and transmitters.
B	Medium negative voltage and temperature sensitivity.	Instrument compensation. X-Ray Equipment.
BNR	High negative voltage sensitivity.	Magnetic valves. Motor governors.
CX	Low negative voltage and low positive temperature sensitivity.	Radio transmitters for dummy antenna and parasitic suppressors.
F	High negative temperature sensitivity.	AC-DC radio receivers to prevent surge currents when starting tube filaments.

GLOBAR Ceramic Resistors
BY CARBORUNDUM
TRADE MARK

"Carborundum" and "Globar" are registered trademarks which indicate manufacture by The Carborundum Company

MITCHELL RAND



M-R FASTHOLD FRICTION TAPE

Double Coated With Rubbery Compounds . . . Tensile Strength more than 44 lbs.—Adhesive Strength more than 50 lbs.

In the manufacture of FASTHOLD FRICTION TAPE the best procurable cotton sheeting (long staple 56/60) is first dried to eliminate moisture . . . then the fabric is thoroughly impregnated with a filler coat of insulating, waterproofing and preserving compound . . . after several days of drying a second coat, exceptionally heavy in rubber content, is forced through the fabric by means of enormous rollers . . . then follows another period of drying out before cutting and wrapping in tin foil for protection. The materials used and the precision and control exercised in the manufacture of FASTHOLD FRICTION TAPE enables it to meet all known electrical tests and requirements . . . and to Guarantee it against Unraveling or Drying Out. FASTHOLD FRICTION TAPE is New York warehouse stocked in widths of ⅜—½—¾—1—1½ and 2 inches.

M-R ANHYDROUS SEALING TAPE

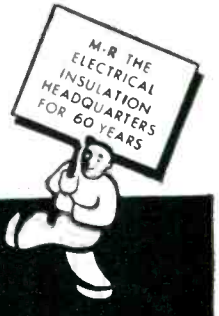
IMPROVES WITH AGE AND SERVICE

25.58% Cotton Sheeting • 74.42% M-R Insulating Compounds
Weatherproof . . . Waterproof . . . Acid, Alkali, Oilproof . . .
Permanently Flexible . . . Will not Vulcanize or Dry Out . . .
Tensile Strength 30 Pounds . . . Dielectric 1,000 volts

ANHYDROUS SEALING TAPE contains nothing which will injure fabrics or metals. It is made of the best procurable cotton sheeting and special M-R Bituminous Compounds. A wrapping of ANHYDROUS TAPE gradually becomes one solid mass (glass hard on the outside and soft inside) that excludes air, moisture, vapors, etc. It can be used to great advantage under conditions which disintegrate ordinary tapes; inside work where acids or alkali fumes or spray prevail; outside for cable joint insulation in conduits transformer connections, extreme high or low temperatures, etc., mines and damp places where atmospheric conditions and constant friction demand maximum wearing qualities. A joint, properly taped with ANHYDROUS, is absolutely waterproof even after complete submergence for many weeks. ANHYDROUS SEALING TAPES are New York warehouse stocked in widths of ¾ and 1½ inches . . . other sizes are available, as ordered.

free
FOR THE ASKING...

Write today for samples of M-R Friction and Sealing Tapes . . . also your Free Card of Varnished Tubing with samples ranging from size 0 to 20 to fit wires from .032 to .325 inches . . . other valuable aids, are the M-R Guide Book of Electrical Insulation . . . the Wall Chart with reference tables, electrical symbols, allowable capacities of conductors, dielectric averages, thicknesses of insulating materials and tap drill sizes . . and the M-R Wax and Compound Guide Book . . . they are full of valuable information . . . write for them on your letterhead.



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"Give us the tools..."

YOUR ONLY CHANCE of Getting Ahead

Where is the "brave new world" so glowingly promised us by the politicians during and after the war? We were told then that postwar America would live 50% better than it had before. Why has that promise faded out? Why are men today discouraged and frustrated?

We have not yet made good 1944's promises because the *American worker turns out no more in an hour now than he did in 1941.* We are getting more total production in our country – but only because we have more people working. Not because each one of us is producing more. American industry's ability to turn out more and more goods – with less of each worker's time and effort – has been stymied for eight long years.

Progress has been blocked because in some cases workers have not been willing to work as hard as they did before the war. In other cases unions restrict the use of labor-saving machines and methods. In some places obsolete building codes and ordinances prevent advances. In still other cases progress has been blocked by collusive practices between unions and manufacturers or operators.

But the biggest block to progress is the fact that our industry in the United States has been unable to provide our workers with all the new tools and equipment that they need.

Increasing productivity – that is, each one of us turning out more in each hour of work – is the key to higher living standards. Productivity depends directly upon the kind of tools workers use. His tools, more than anything else, determine how much a worker can turn out; and what his paycheck will buy depends in large part on what he turns out–not on how long or how hard he works.

Look what happened in our country in the forty years from 1900 to 1940. Productivity of the United States *more than doubled.* It doubled because:

Business investment in capital equipment gave workers new tools – tools that had three and one-half times as much power –

So – Americans' living standard rose almost 50% while the average work week was dropping from 61 to 43 hours.

Industry did continue to raise its output per man hour, even in the depressed 1930's. But it did it because, with unemployment widespread, companies used only their most efficient equipment. *Actually the great depression saw industry fall far behind in the job of providing workers with new tools.*

Then came World War II. Few new tools for peacetime industry were produced. *As a result of depression and war, the U.S. fell behind in needed investment in new industrial facilities by more than $100 billion.*

Since the war business has spent almost $60 billion for new plants and equipment –

But the greater part of that money went to *expand* production to take care of the needs of our bigger population, and to *replace* plants and equipment that were worn out and ready to be junked at the end of the war.

continued on next page

Only a small fraction of the $60 billion went to *modernize equipment* – the equipment that increases efficiency and improves productivity of the individual worker.

Right now industry is desperately trying to do the job of increasing efficiency of machines so that each worker can turn out more.

McGraw-Hill's national survey of Business' Needs for New Plants and Equipment shows that manufacturers plan right now to spend in the 5 years ahead three-quarters of their capital funds to replace and modernize facilities. The biggest part of the more than $55 billion industry plans to spend on its plants and equipment will go directly to improve efficiency of the individual.

If industry can carry through its plans – and expand them as it would like to and as it must do – the U. S. can catch up on its depression-war-time lag in progress within a few short years.

If American industry is allowed to earn the money to buy the equipment, it can raise the American standard of living 50% in our generation – in the next 25 years. No other nation can promise its people that much – and deliver on the promise.

But the promise can only be fulfilled by American industry. Wherever you turn, industry has dramatic new ways of doing things. Using oxygen by the ton, steel makers are increasing production from blast furnaces by 20%. New high-speed machine tools are doing three times the work of 1940 tools. A new coal-mining machine will multiply a miner's daily output 10 times. Diesel locomotives do the work of three steam locomotives on many jobs.

New products – and larger production of standard products – are already making their impact on American life. Two million Americans will get new television sets this year. Automatic washing machines, electric dishwashers, and home freezers are easing the daily tasks of thousands of housewives. Millions of homes that did not have them before the war now have telephones, automatic heat and refrigerators. Frozen foods, nylon clothing – these and many other things coming along now – will shape the *real* new world for Americans.

But industry can provide them only if it can keep on investing at least $15 billion a year now – and more in future years – in new plants and equipment.

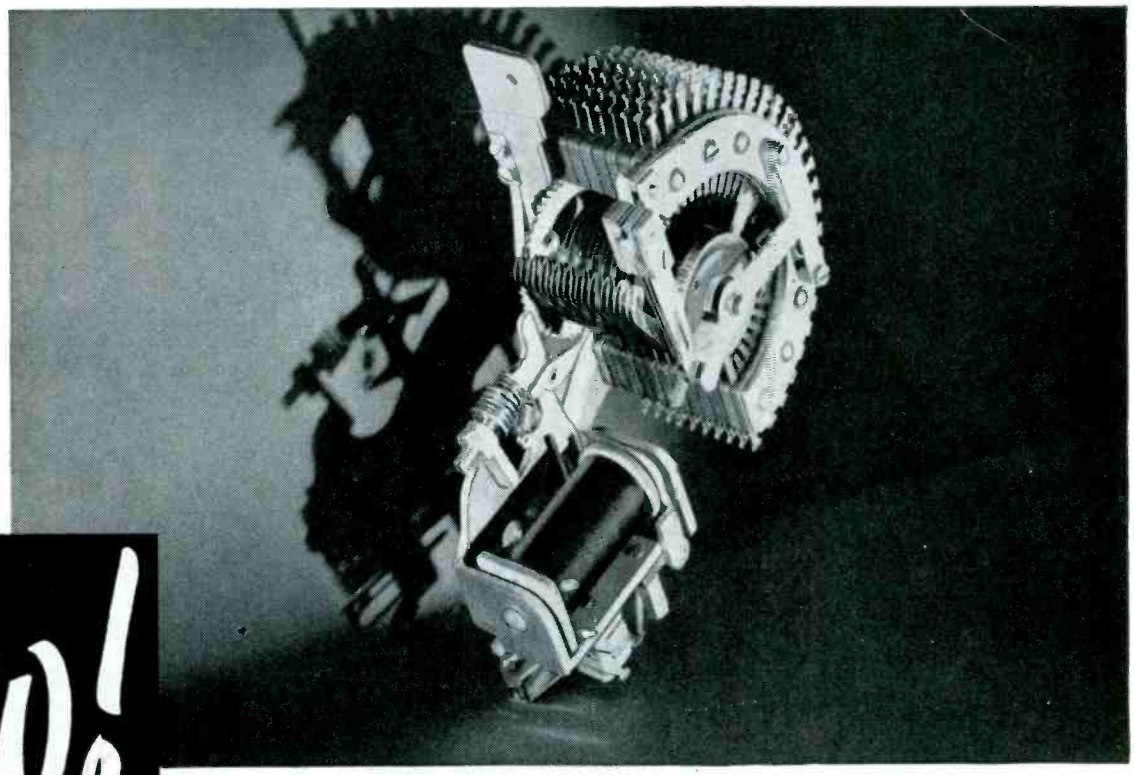
Today Washington is taking a course which, if pursued, will make that investment by industry impossible. Government spending now strains our resources to the limit, and more multi-billion dollar spending proposals are being piled on. *But government spending cannot improve American living standards.* It never has, and it never will. Increasing government spending *now* will only block progress, because the government proposes to pay for its plans by taxing away the profits industry is using, and must continue to use, to improve and expand its plants and equipment – our only hope for greater worker productivity and higher living standards.

Better living can only be paid for with more production. And we can only get more production by increasing productivity – by each one of us producing more for each hour of work.

The first thing is to get the production – in peace and in war – for better living – for security. Industry is planning to provide it – and is using $13 billion of its profits this year to improve and expand its facilities.

The only sensible, the only safe national policy is to make it possible for American industry to do its job – not to terrorize private industry with proposals of ruinous taxation and paralyzing controls and threats of nationalization. For American industry is not a thing apart from the American people any more than is government. American industry is the lifeblood of the American people and whatever makes industry do its work better contributes more to the common welfare than a bureaucratic government can ever hope to do.

President, McGraw-Hill Publishing Company, Inc.



new!

the Type 45 Rotary Switch

70 Steps a Second Speed
Up to 10 (or more) Bank Levels
Only 1 Field Adjustment

For *all* the features you want . . . in *any* remote-control application . . . look to Automatic Electric's Type 45 Rotary Switch!

SPEED . . . it's faster! It carries 10 wipers at 70 steps a second on 46 volts d.c. self-interrupted, or at 35 steps a second, externally interrupted.

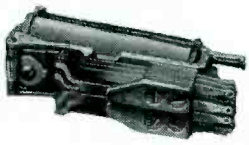
CAPACITY. . . it's greater! Ten or more 25-point bank levels can be accommodated on the same frame, and single ended wipers can be provided for 50-point operation.

ADJUSTMENT . . . it's simpler! A rare readjustment of the interrupter springs is all that's normally required.

OPERATION . . . it's smoother! With an even load on *all* contacts, the Type 45 runs without galloping; there's no chatter or bounce.

ADAPTABILITY. . . it's more useful! With more levels, faster speed and 25- or 50-point operation, it's suitable for a wider variety of control applications.

For complete information on this switch that's new and better, write for our new circular.

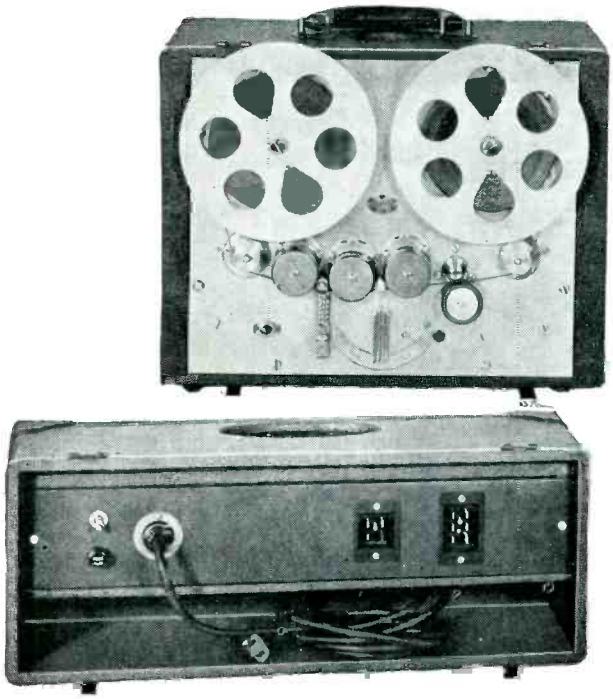


the Class "B" Relay

Here's a new relay, too, that can be used for ordinary relay service—opening, closing or switching circuits—and for extremely high-speed operation. Independently operating twin contacts assure perfect contact operation. Contact points are dome-shaped to maintain uniformly low contact resistance. They may be arranged in one or two pile-ups with a maximum of 16 contacts on 13 springs in each pile.

AUTOMATIC AE ELECTRIC

Distributors in U. S. and Possessions:
Automatic Electric Sales Corporation
1033 West Van Buren Street, Chicago 7, Illinois
In Canada: Automatic Electric (Canada) Limited, Toronto

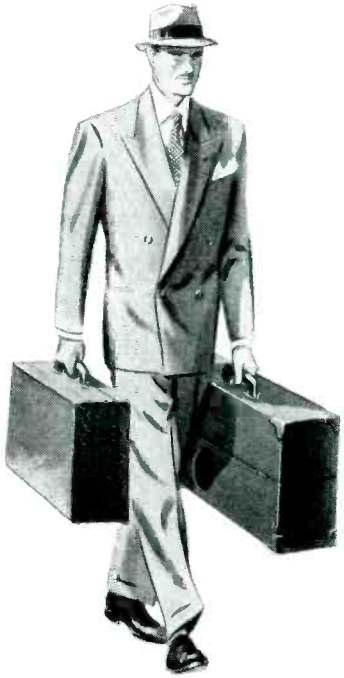


comparisons

indicate this is the world's finest recorder of its type

NEW PRESTO

Portable Tape Recorder 900-P



Complete in two easily portable cases—one containing the recorder, the other the amplifying equipment.

MANY OUTSTANDING FEATURES:

- Three separate heads for superior performance (and for monitoring direct from tape). One head each to erase, record and play back.
- 3 microphone channels with master gain control in recording amplifier.
- Weston type 30 V.U. meter with illuminated dial to indicate recording level, playback output level, bias current and erase current.
- 2-speed, single motor drive system. Toggle switch to change tape speeds from 7½" to 15" per second.

Don't choose your tape recorder until you see the *new* Presto Portable Tape Recorder. Write for complete details today.

Write today to be put on our mailing list for "The Presto Recorder," new house organ of practical ideas for anyone in the recording and broadcasting field.

PRESTO
RECORDING CORPORATION
Paramus, New Jersey

Mailing Address: P. O. Box 500, Hackensack, N. J.
In Canada: WALTER P. DOWNS, Ltd., Dominion Square Building, Montreal

WORLD'S LARGEST MANUFACTURER OF INSTANTANEOUS SOUND RECORDING EQUIPMENT AND DISCS

INSUROK
by RICHARDSON
Dependable names in plastics

UNDIVIDED RESPONSIBILITY

Many users of plastics enjoy Richardson's VARIETY of products and services. They like the convenience of handing all of their plastics problems to one organization. More important, they like for Richardson to assume complete responsibility for their plastics requirements.

Such an arrangement is possible with Richardson because here, from one company, you can get (1) Laminated INSUROK in a wide variety of grades suitable for virtually every plastic laminate requirement (2) complete punching facilities (3) complete fabricating facilities (4) complete molding facilities (5) experienced engineering (6) complete laboratory facilities if your job calls for laboratory research (7) mold and die design and facilities to produce molds and dies and (8) conscientious, personal attention to your particular needs.

Why not see what this variety of products and services can do for you? Send a set of specifications today and learn, without obligation, how Richardson would approach your job . . . find out for yourself how Richardson's "undivided responsibility" can work to your advantage.

INSUROK is a registered trade-mark of The Richardson Company

The RICHARDSON COMPANY

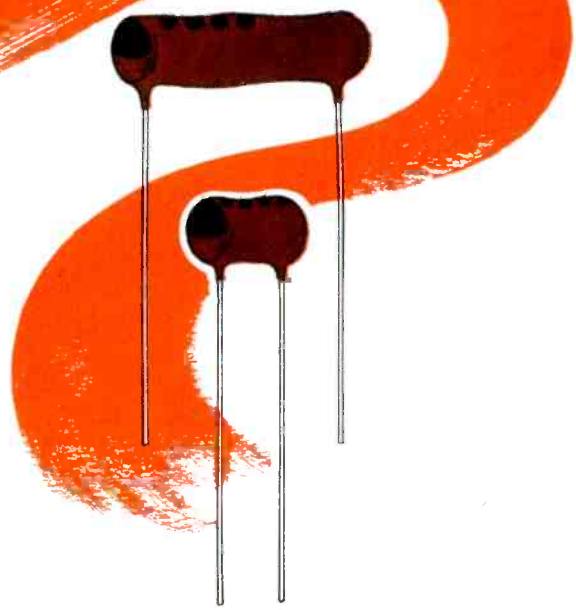
GENERAL OFFICES: LOCKLAND, OHIO FOUNDED IN 1858

Sales Headquarters: MELROSE PARK, ILLINOIS

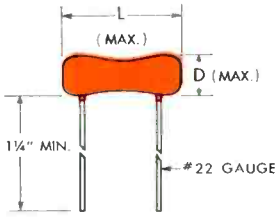
CLEVELAND - DETROIT - INDIANAPOLIS - MILWAUKEE - NEW BRUNSWICK, (N. J.) - NEW YORK - PHILADELPHIA - ROCHESTER - ST. LOUIS

Now...

for positive identification...



ERIE Radial Lead Insulated CERAMICONS® now have distinctive *red bodies*



DIPPED PHENOLIC INSULATED

Style	Dia. "D"	Length "L"	Max. Cap.
331	.240	.460	715 MMF
332	.240	.710	1500 MMF
338	.312	.550	2000 MMF
337	.312	.937	4100 MMF
333	.315	1.250	5100 MMF
344	.415	1.213	8000 MMF
335	.415	1.650	.012 MFD
336	.415	2.025	.016 MFD

ERIE brings order out of confusion . . . by the simple expedient of giving ERIE radial lead, dipped phenolic coated Ceramicons distinctive red bodies.

In the past manufacturers have found it almost impossible to differentiate between the various makes of such condensers. The common brown body color has sometimes caused confusion in incoming inspection departments and in the final assembly lines. In addition, it has been difficult to fix responsibility for any service reports.

Now, ERIE Radial Lead Insulated Ceramicons are positively and unmistakably identified . . . and the red body also makes it easier to read all RMA color code dots. ERIE axial lead ceramicons will continue to have molded low-loss phenolic insulation.

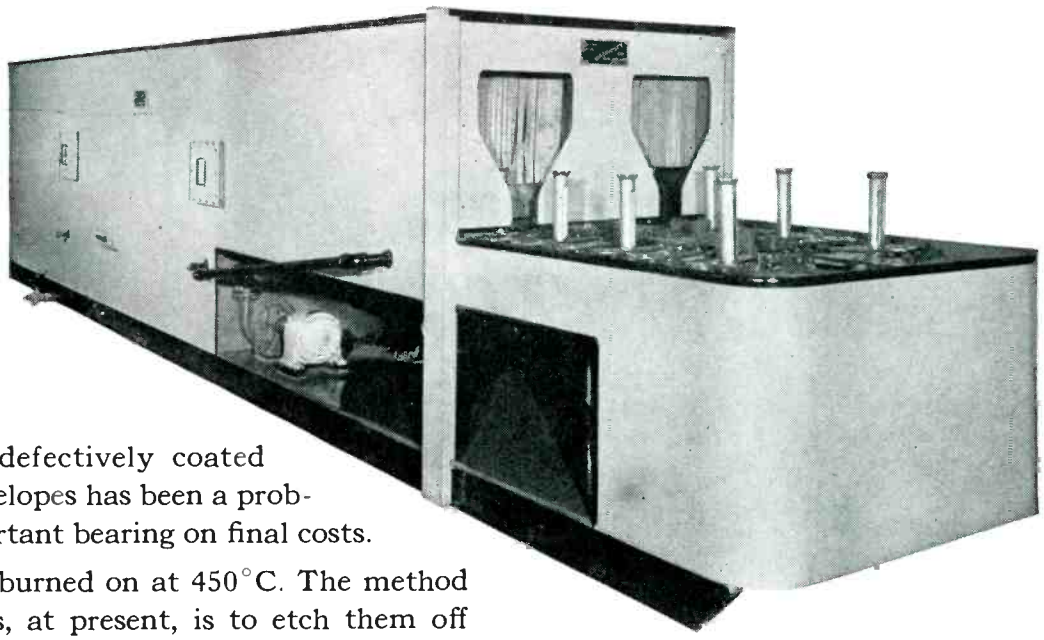
When you see ceramic condensers with the red body color, you can be sure you have high-quality, dependable ERIE radial lead insulated Ceramicons which will "stay put" in your chassis for the life of the set.

Electronics Division

ERIE RESISTOR CORP., ERIE, PA.

LONDON, ENGLAND TORONTO, CANADA.

New washing machine cuts TV tube costs... with the help of Inco Alloys



THE SALVAGING of defectively coated television tube envelopes has been a problem . . . with an important bearing on final costs.

Tube coatings are burned on at 450°C. The method of removing coatings, at present, is to etch them off with ammonium bifluoride or hydrofluoric acid.

Attempts to mechanize the "washing" or etching process ran into this difficulty . . . most metals suitable for machine construction were unable to withstand the corrosive attacks of the etchant solutions.

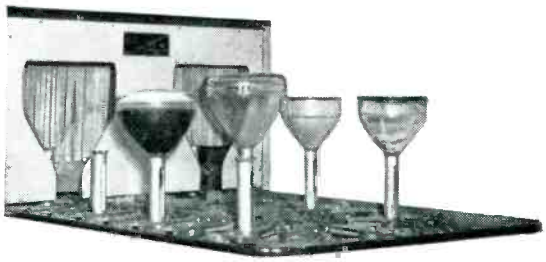
Inco's Corrosion Engineering Section helps

Now the Better Built Machinery Co. of New York City has designed a production machine to clean out new tube envelopes and also salvage defective ones. The problem of a material to resist action of the violently corrosive etching fluids was referred to International Nickel, where corrosion problems have been analyzed for over 40 years. Inco's Corrosion Engineering Section recommended: *Monel** for spray chamber liners and tube holders; Ni-Resist* #2 castings for conveyors.

Result? The new Better Built tube washing machine . . . first of its kind . . . is now at work in the Allan B. Dumont Laboratories. And with tube envelope cleaning and reclaiming on a production basis, tube costs are expected to be significantly lowered.

If you have metal problems, talk them over with Inco. One of the versatile Inco Nickel Alloys may be the solution you are seeking.

THE INTERNATIONAL NICKEL COMPANY, INC.
67 Wall Street, New York 5, N. Y.



How the Better Built Tube Washer Operates

New tube envelopes and those with defective coatings are loaded onto the Monel tube holders. A conveyor, made of Ni-Resist #2 castings, carries the tubes through a Monel-lined spray chamber where etchant solutions "wash" away the unwanted coatings.

Final cleaning of the tubes is accomplishd with a hot caustic wash, followed by several pre-rinses and a final rinse in distilled water.

The washing machine is 30 ft. long, 4½ ft. wide, and 6 ft. high. It follows the general design of standard Better Built machines used for washing glass containers and laboratory ware.

For further information about Better Built machines, write directly to:

BETTER BUILT MACHINE COMPANY
73 East 130th St., New York, N. Y.

EMBLEM OF SERVICE
NICKEL INCO ALLOYS

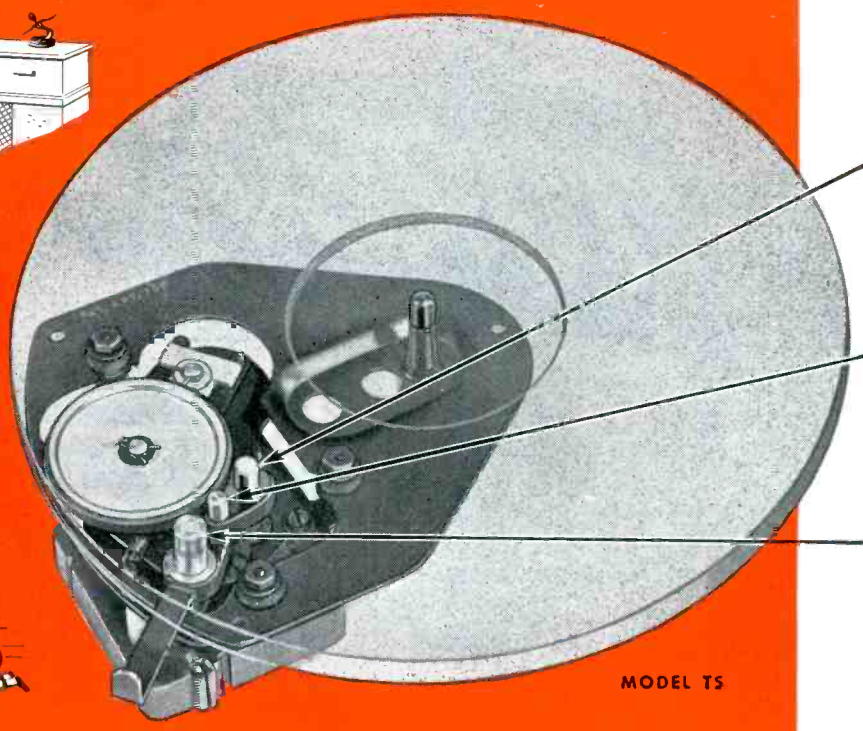
MONEL* • "K"* MONEL • "R"* MONEL • "KR"* MONEL
NICKEL • "D"* NICKEL • "Z"* NICKEL • INCONEL*
*Reg. U. S. Pat. Off.

You're a record year ahead...

LIVING ROOM

RECREATION ROOM

PLAY ROOM



...WITH THIS G 3-Speed PHONOMOTOR

Here's the motor that plays all three types of records without fuss or bother . . . the *one* motor designed, engineered and built to enable radio and phonograph manufacturers to offer their customers dependable, *complete* record entertainment. It's GENERAL INDUSTRIES' new Model TS three-speed phonomotor.

External speed change lever affords positive, accurate shifting to any of the three speeds without removing the turntable. Ingenious, yet simple, shift mechanism is both trouble-free and fool-proof. Compact size of motor makes it ideally suited for portables as well as console models. Cost is surprisingly low.

For complete information—blueprints, performance specifications and quotations—write, wire or phone *today*.

The GENERAL INDUSTRIES Co.

DEPARTMENT B • ELYRIA, OHIO

INSULATION COSTS GO DOWN WITH

TURBO SATURATED SLEEVING*

*EXCLUSIVELY PROCESSED FOR

- HIGHER TENSILE STRENGTH
- GREATER FLEXIBILITY
- ABSOLUTE CONCENTRICITY
- SLOW BURNING COMPOSITION
- LOW MOISTURE ABSORPTION
- FREEDOM FROM PEELING

CHECK THESE *TURBO* PRODUCTS FOR ALL YOUR INSULATION NEEDS

- TURBO VARNISHED TUBING FOR HIGH VOLTAGE
- TURBO EXTRUDED TUBING FOR EXTREME TEMPERATURE
- TURBO GLASS TUBING FOR HIGH HEAT RESISTANCE
- TURBO REL-16-A TUBING FOR SUPER-FLEXIBILITY
- MICA PLATE, BLOCK FILMS AND SEGMENTS
- TURBO WIRE MARKERS FOR LASTING IDENTIFICATION
- VARNISHED CAMBRIC AND PAPER TAPE

Write today for your free sample board of TURBO Tubing—no obligation.

SPECIFICATIONS

SIZES	41 sizes from .022" to 1.5" inside dia.
LENGTHS	Standard bundles of 42" strands. Sizes 13 to 24 inclusive can be supplied in any length on spools.
COLORS	Black, yellow, red, green, brown, blue. Standard up to Size No. 12. Black and yellow on larger sizes. Other colors special.

A low cost insulation tubing impregnated for maximum serviceability and extra long life!

TURBO Saturated Sleeving is made from select cotton braid sleeving, saturated with a special TURBO varnish that seals every pore without impairing flexibility. While relatively low in cost, this tubing offers excellent advantages in general wiring applications—becoming all-purpose when only moderate temperature extremes are encountered, and where electrical stress does not exceed 1200 volts. The impregnation applied to TURBO Saturated Sleeving insures negligible moisture absorption and imparts a high resistance to acid and oil. TURBO Saturated Sleeving is slow burning.

Full particulars on request — please address inquiries on company letterhead

TURBO · IT SAFE-GUARDS · SIT IF

WILLIAM BRAND & COMPANY

276 FOURTH AVE., NEW YORK 10, N. Y. • 325 W. HURON ST., CHICAGO 10, ILL.

To Top Flight Development, Design and Instrumentation Engineers:

This table gives the characteristics of Arma Two-Phase Induction Motors. The information may suggest applications of these components to your designs.

Type	Field Voltages		No Load Speed	Max. Watts Output	Stalled Torque	Rotor Inertia	Weight
	Main	Control	R.P.M. (Min.)	@ R.P.M.	Oz. In. (Min.)	Oz. In.^{2}	(Lbs.)
1A60	40	40	3200	1.5 @ 1500	1.7	0.03	0.8
1B60	115	115	3000	2.4 @ 2000	3.0	0.25	1.4
1D60	115	115	3000	6.4 @ 2150	8.0	0.25	1.4
1E60	115	110	3000	6.0 @ 2000	7.5	0.04	1.5
*1A400	115	115	9800	1.6 @ 5300	0.9	0.03	0.8
5A	75	90	3000	6.3 @ 1800	8.0	0.32	4.0
†5C	90	75	3000	7.5 @ 2000	8.0	5.51	4.3
6	115	90	3000	18.0 @ 2000	17.0	1.38	9.8

Operating Ambient Temperature Range 0°C to 55°C.
Reversible Rotation. 2 Phase. 60 Cycle.
**400 Cycle Unit. †High-Inertia Rotor.*

These Two-Phase Induction Motors Extend the Possibilities of Precision Instrumentation

Arma Corporation designed and built them for use in some of the highest-precision control systems, electromechanical computing systems and servo mechanisms ever devised. Long unpublicized because of security restrictions, many engineers are yet to have their first opportunity to consider new applications of these motors.

Response of Arma Induction Motors is Phenomenally Rapid

Full-Speed reversing in as little as three one-hundredth second characterizes the unusual acceleration and deceleration of Arma Induction Motors. This derives from the high torque-to-inertia ratio reflected in the table of characteristics. Such rapid response might well set new standards of automatic operation for industrial processes too complex to be trusted to manual operation.

Other Advantages of Arma Induction Motors

No Preferred Positions. Symmetrical rotor design eliminates all "clogging" or slot effects.

High Mechanical Accuracy. Extremely close tolerances make possible precise assembly and complete interchangability.

Minimum Inductive Interference. Stray fields are low, larger types are shielded.

Arma Induction Motors are designed to minimize the possibility of damage by shock or corrosion. They are nearly noiseless in operation. All types have double shaft extensions.

Use These Other Arma Components, Too

Investigate possible applications of these other Arma components released for private industry: Tachometer-type Induction Generators for high-performance servo systems; Electrical Resolvers* for solving problems involving triangles, coordinates and vectors; Synchro Units for remote control and indicating purposes; high-precision Mechanical Differentials for computing applications.

How Ideas Become Realities

For over 30 years Arma Corporation has been quietly taking on (under wraps) one complex development and design problem after another for the U. S. military establishments—problems concerned with instrumentation. In the initial stage these problems may be little more than a gleam in someone's eye, a vague hope, a "dream"! That's where Arma *starts*. When Arma *finishes*, the problem is not only solved but the actual equipment to do the job, *built*—whether it be a complicated gun director, a gyro compass or a complex remote control system. Arma follows through to practical realities.

You are invited to request whatever information you may need to explore the possibilities of making use of any Arma product which has been released from security restrictions.

ARMA CORPORATION

254 36th STREET, BROOKLYN 32, N. Y.

SUBSIDIARY OF AMERICAN BOSCH CORPORATION

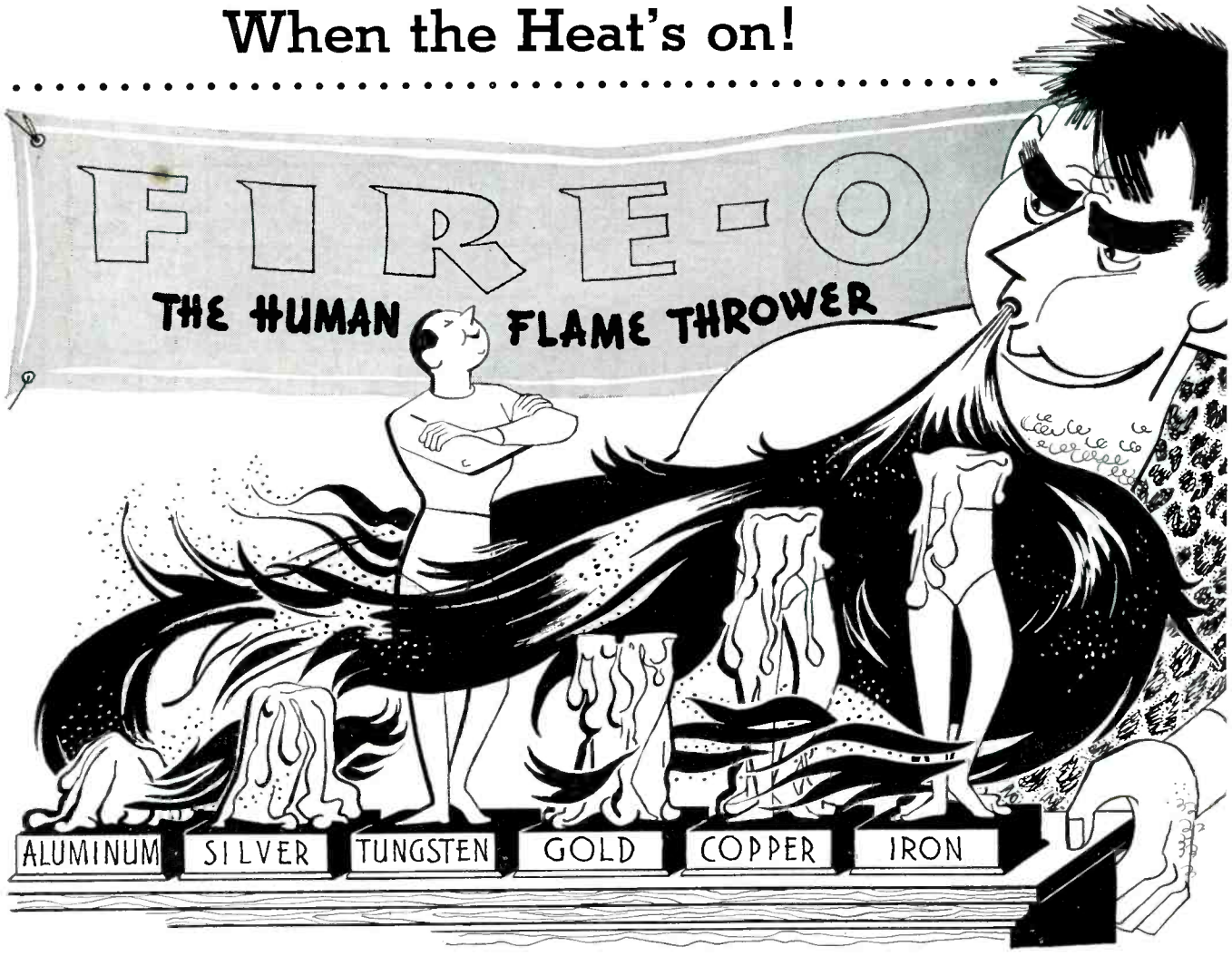
ARMA PRODUCTS RELEASED FOR PRIVATE INDUSTRY

ARMA ELECTRICAL RESOLVERS* · ARMA SYNCHROS · ARMA INDUCTION MOTORS · ARMA INDUCTION GENERATORS · ARMA MECHANICAL DIFFERENTIALS · ARMA ALTERNATING VOLTAGE COMPARATOR · COMPUTING MECHANISMS · INDUSTRIAL CONTROLS · STABILIZATION DEVICES · NAVIGATIONAL EQUIPMENT · LIMITRON AUTOMATIC INSPECTION SYSTEM

* Licensed for use under Arma patents Nos. 2,465,624 and 2,467,646. License information available.

QUALITY ARMA INSTRUMENT PRECISION

When the Heat's on!



BECAUSE the *melting point* of tungsten is higher than the *boiling point* of iron, copper, aluminum, silver, gold, and nickel, it is the perfect material for the application of heat in processes which involve a physical change in these metals. More and more, manufacturers are adapting improved techniques made possible by tungsten's exceptional qualities as a substitute for conventional methods.

ELMET Tungsten offers unique possibilities to manufacturers with production problems calling for a metal which combines the features of strength, hardness, ductility, and resistance to unusually high temperatures. North American Philips can supply tungsten in powder, rod, or wire form to your precise specifications. We will be glad to show you how ELMET Tungsten can fit your particular requirements.

★ ★ ★

North American Philips also specializes in drawing, enameling, and plating extremely fine wires in practically all metals and alloys.

So when you have a problem on Fine Wire, Tungsten, or Molybdenum, why not call on Fine Wire Headquarters—phone, wire, or write to North American Philips, makers of NORELCO Fine Wires and ELMET Tungsten and Molybdenum products.

NORTH AMERICAN PHILIPS COMPANY, INC.

Dept. FA-7, 100 East 42nd Street, New York 17, N. Y.

THESE NEW LONG-LIVED THYRATRONS LEAD FOR MOTOR-CONTROL APPLICATIONS

With oversize gas charge to offset absorption from inductive loads
—high anode voltage
—high peak-to-average current ratio
—stable control characteristics
—short heating time
—"climate-proof" ambient temperature range

SPECIFY General Electric's 3.2-amp GL-5544 or 6.4-amp GL-5545 for the motor-control unit now on your drawing-boards. Your equipment will benefit (no snubber circuit is needed with these tubes), while users will have the advantage and economy of full-measure tube life.

Both thyratrons have a charge of inert gas twice that of former types—sufficient to offset anode gas absorption caused by the inductive load in field and armature-control circuits.

Though of paramount value, this is but one of many improvements that put the GL-5544 and GL-5545 far ahead of other gas-filled thyratrons. Study the list of features above. Then add *strength of construction*. Key tube parts are internally braced; the grid-anode structure is solidly supported both at top and bottom. Add *electrical stability* . . . a special shielded-grid design cushions any grid effect from voltage surges. Here are dependable tubes you can count on to do a job where men are pushing machines hard for high production!

Help in applying the GL-5544 or GL-5545 to new motor-control circuits gladly will be given you by experienced G-E tube engineers. Phone your nearby G-E electronics office. Or wire or write *General Electric Company, Electronics Department, Schenectady 5, New York.*

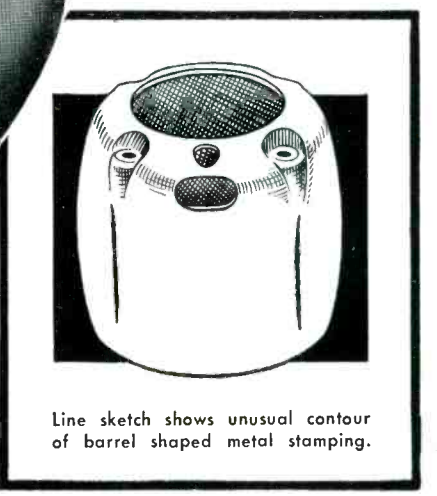
"THEY OUTLAST AND OUT-PERFORM GAS-FILLED TUBES OF EARLIER DESIGN"

	GL-5544	GL-5545
Filament voltage	2.5 v	2.5 v
Filament current	12 amp	21 amp
Peak anode voltage, forward and inverse	1,500 v	1,500 v
Peak cathode current	40 amp	80 amp
Avg cathode current	3.2 amp	6.4 amp
Current averaging time	15 sec	15 sec
Ambient temp range	−55 to +70 c	−55 to +70 c

GENERAL ELECTRIC

180-H28

FIRST AND GREATEST NAME IN ELECTRONICS



Line sketch shows unusual contour of barrel shaped metal stamping.

AN ACCOMPLISHMENT IN METAL FORMING . . .

An ordinary cylindrical shape presents no particular metal stamping problem. However, to maintain the precise specifications of this barrel shaped body in perfect concentricity presented an unusual and difficult manufacturing problem.

Ribs were provided in the body for strength and to overcome the need for appurtenant reinforcements. Another feature . . . to aid economy in assembling, the bolt head seats were struck flat, eliminating the need for costly machining.

Again Presteel engineering, toolmaking and metal forming techniques made a routine job out of the unusual.

ALLOY STEELS AND OTHER METALS COLD FASHIONED SINCE 1883

Representatives in ALEXANDRIA, VA. • BUFFALO • CANTON, OHIO • CHICAGO
DENVER • DETROIT • FORT WORTH • INDIANAPOLIS • LOS ANGELES • NEW YORK
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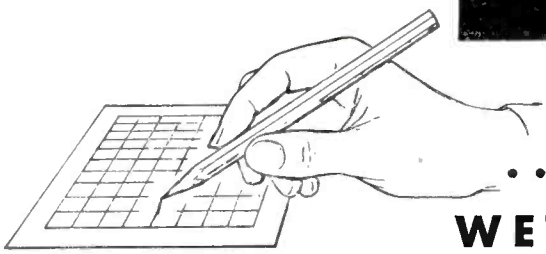
WORCESTER PRESSED STEEL CO.

307 BARBER AVENUE
WORCESTER 6, MASS.

FONO-FITTED TORQUE & DRIVE **CARTRIDGES**



...you draw the curve

WE'LL BUILD THE CARTRIDGE

*Your specifications . . . your special requirements in phono pickup cartridges . . . are ideally "custom-solved" through E-V creative engineering . . . unusual manufacturing facilities . . . and inherent advantages of exclusive TORQUE DRIVE.**

CUSTOM RESPONSE

Smooth upper response with roll off frequency to your specifications or wide range, peak-free response to 10 kc. You draw the curve, we'll build the cartridge.

VOLTAGE

E-V TORQUE DRIVE cartridges provide the highest compliance per volt output. For example, the E-V 14 cartridge tracks at 5 grams with excellent wave form down through 50 c.p.s. on the RCA 12-5-31V record at 1 volt at 1,000 c.p.s.

TRACKING FORCE

With the high compliance and low mass of the driving system, needle forces at 5 grams for both one and three mil records are used in everyday production by leading manufacturers. Cartridges with even lower needle force with slight reduction in voltage are thoroughly practical. 3 gram tracking pressures are definitely in sight.

COMBINATION
One and Three Mil

E-V TORQUE DRIVE again leads in twin needle cartridge design. Tracking force of 5 grams on both one and three mil records precludes weight changing. Straight line needle position assures accurate set down when used with changers. Approximately the same output is obtained on both stylii. The E-V Twin-Tilt cartridge mounts in any arm with ½" mounting holes with no modification except adjustment for correct needle force.

MOISTURE PROOFING

The cartridge is *entirely filled* with DC4 Silicone jelly—the material that is used for inhibiting moisture on aircraft wiring. Tests indicate that it increases the life of an ordinary crystal *some 20 times.* This is a *plus* feature, found in all E-V crystal cartridges.

Our engineering staff and full facilities are at your service. Contact us today.

Modern One-Acre Plant with Complete Internal Facilities for Quality-Controlled Volume Production

From original conception to final product, you get full benefit of the unusual E-V processes. Here are E-V laboratories, where constant research keeps making new contributions to the Art. Here we make tools and dies . . . die cast, plate, screw machine, stamp, mold plastics, and assemble. Here we use specially designed test equipment for quality control. With all these facilities, we produce high standard acoustical products in quantity, with utmost economy. Come—see this plant in action.

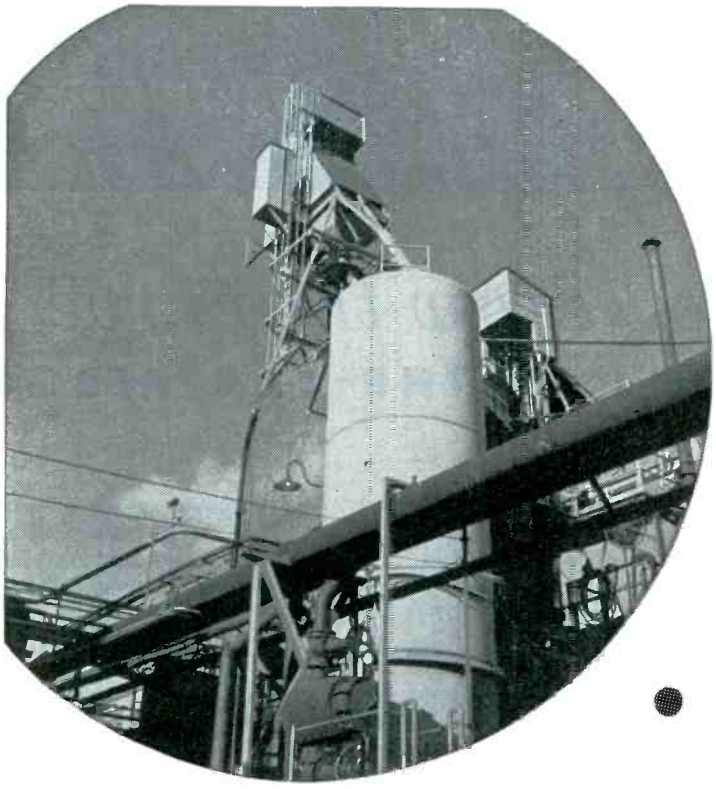
NO FINER CHOICE THAN

Electro-Voice

*E-V Pat. Pending
Licensed under Brush patents

*Export: 13 East 40th St., New York 16, U.S.A.
Cables: Arlab*

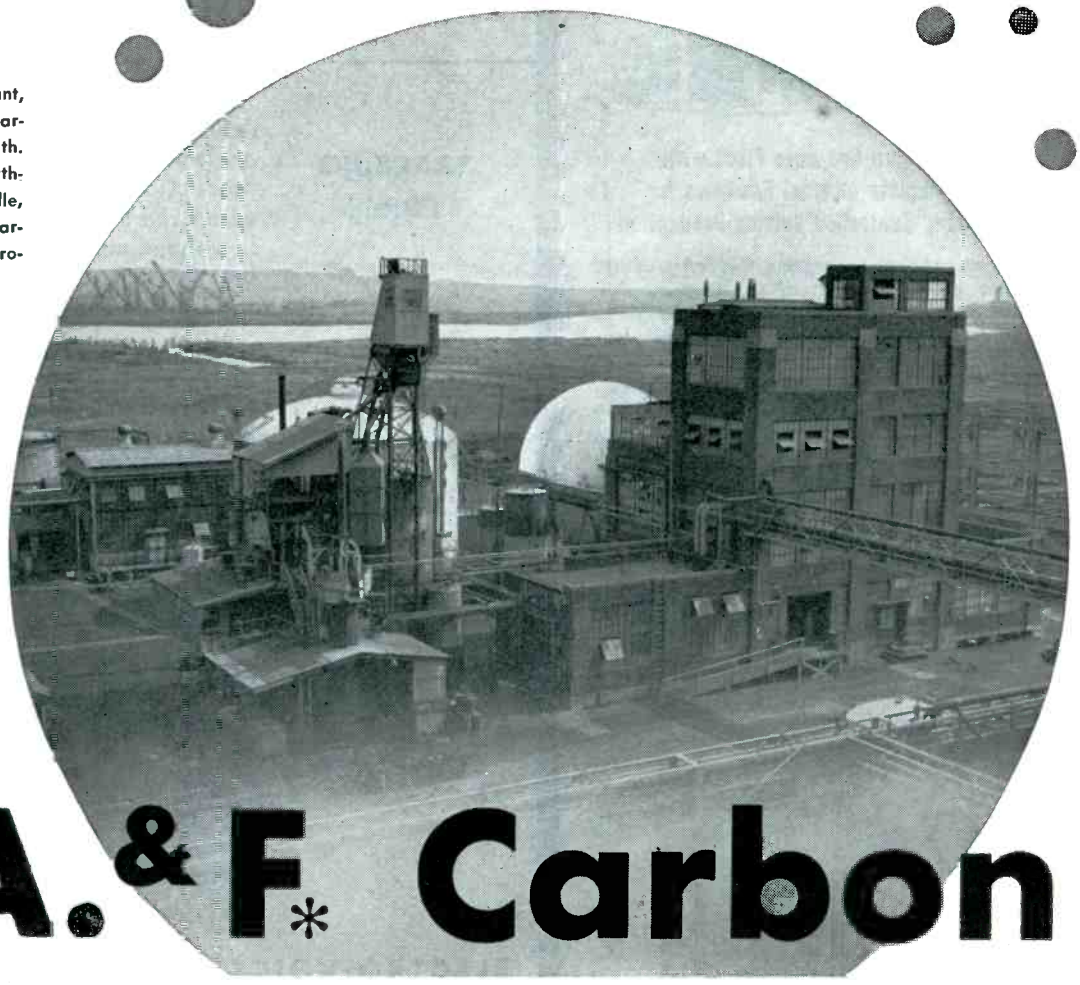
ELECTRO-VOICE, INC. • BUCHANAN, MICHIGAN



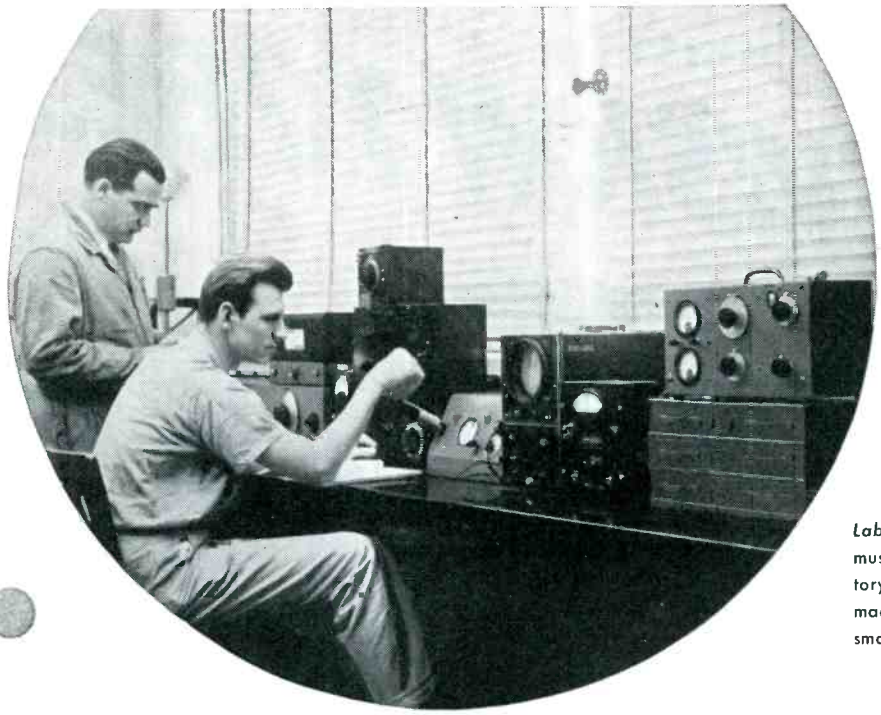
Chemically Processed—Highly specialized chemical equipment, such as illustrated here, reacts carbon monoxide with iron-containing ores to form liquid iron pentacarbonyl. Further processing decomposes the liquid into the spheres which are Carbonyl Iron Powder. The closest attention to detail assures products of constantly uniform properties.

carbonyl iron

Plant Facilities—The Grasselli N. J. plant, right, was the sole producer of Carbonyl Iron Powders until this month. Now, increased production will be forthcoming from the new plant at Huntsville, Ala. The demand for all grades of Carbonyl Iron Powder has made this production increase necessary.



G. A. & F.* Carbon



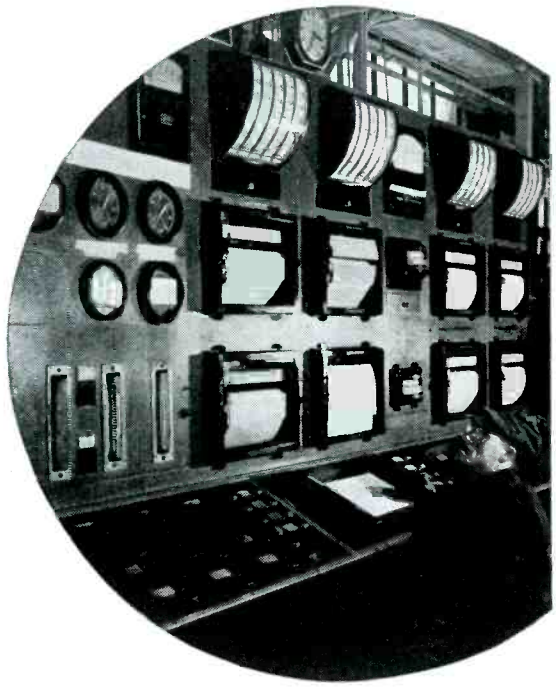
Laboratory Controlled—Every batch of CIP must be put through very extensive laboratory tests to keep quality high. Test cores are made from every batch at the lab. Above, a small section of the test equipment.

powders are superior

Carbonyl Iron Powders are high quality products with low loss characteristics—superior in every way because this quality is achieved by strict control in processing. These high "Q" materials work best because they are manufactured and tested for quality under the most careful conditions.

Chemically, Carbonyl Iron Powders are high in iron with an absence of non-ferrous materials. Structurally, the particles are spherical, built up of concentric cells. Particle distributions range from 0.5 to 15 microns diameter. Some grades are mechanically hard and quite incompressible. Hysteresis loss is low, insulation is easy thus keeping eddy currents low. Particle size distribution is controlled.

The illustrations on these pages show to some extent the manufacture, the tests for quality, and the checks on control made by GA&F. For more detailed information on any problem involving Carbonyl Iron Powders write . . .



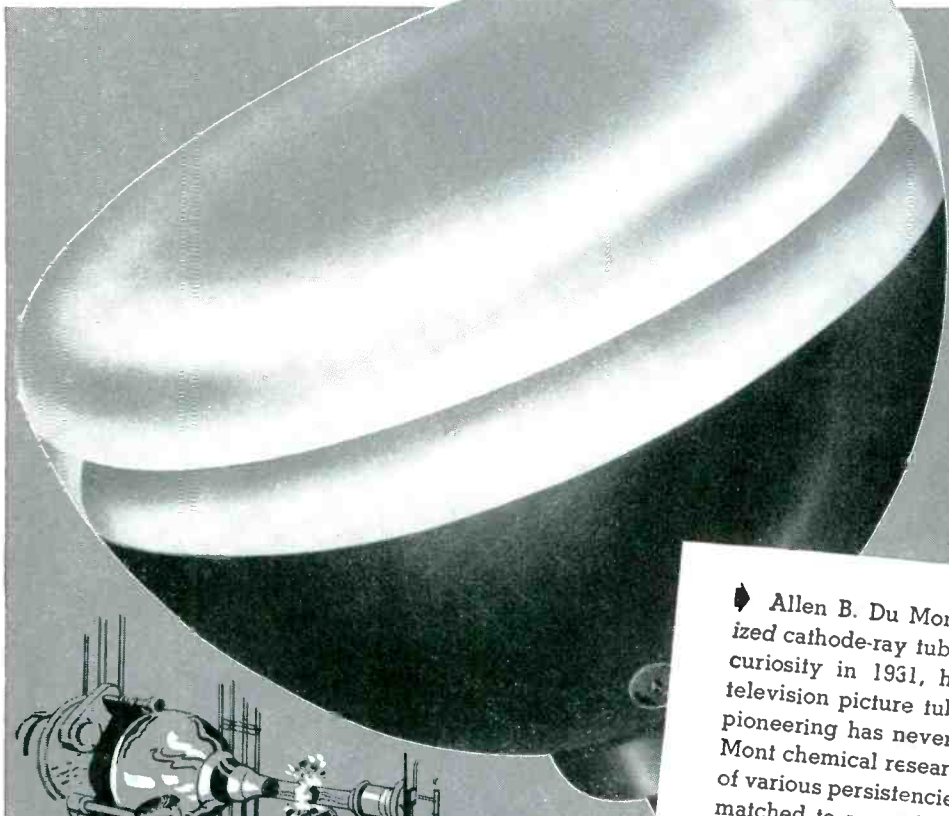
Production Controlled—Instruments, such as these, control the processes which make Carbonyl Iron Powders. Such control makes possible the constant uniformity of CIP. The panel above is one of many instrument boards used for controlling the processing of GA&F Carbonyl Iron Powders.

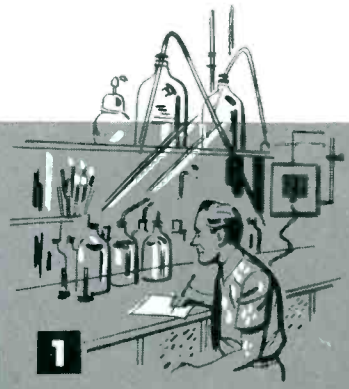
MEMBER mpa METAL POWDER ASSOCIATION

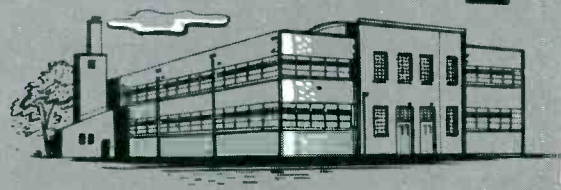
ANTARA* PRODUCTS
GENERAL ANILINE & FILM CORPORATION
444 Madison Ave.
New York 22, N. Y.
*®

yl Iron Powders

First with the Finest in TELEVISION TUBES!







Allen B. Du Mont gave us the commercialized cathode-ray tube. Starting with a scientific curiosity in 1931, he pioneered the practical television picture tube of today. And Du Mont pioneering has never ceased. Examples? **1** Du Mont chemical research has led to tube screens of various persistencies and intensities precisely matched to any television requirements. **2** Du Mont research and development engineers have always led in large television tubes—those 12½", 15" and 20" Teletrons*—because Dr. Du Mont has insisted on "comfortable" televiewing. **3** Du Mont craftsmen, provided with the finest glass-working equipment known, can translate advanced tube designs into greater tube values at lesser prices. **4** And to keep pace with the huge and still growing demands, Du Mont quantity-*quality* production has steadily stepped up, climaxed by the new Allwood plant. Yes, it's Du Mont Teletrons for the "First with the Finest in Television Tubes."

*Trade-mark

FIRST WITH THE FINEST IN TELEVISION TUBES

DU MONT Teletrons

ALLEN B. DU MONT LABORATORIES, INC., TUBE DIVISION, PASSAIC, N. J.

SPRAGUE KOOLOHM RESISTORS

T.M. Reg. U.S. Pat. Off.

Tops for TV and other difficult applications!

Available in 5, 10, 25, 50 and 120 watt ratings.

WIRE-WOUND RESISTORS WITH LOW S.Q.!

S.Q.?? That means "Service Quotient." With dependable, tropicalized Koolohm resistors, it's practically nil!

That's why major television manufacturers specify Sprague Koolohms and avoid unnecessary and expensive service calls due to resistor failures.

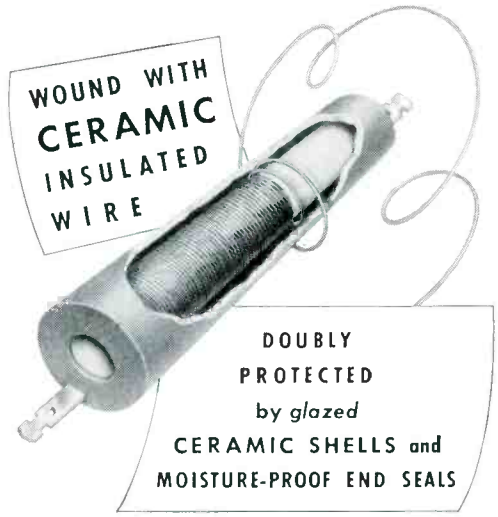
Koolohms far outperform and outlast ordinary wire-wound resistors, yet are smaller in size than ordinary units of the same wattage rating. Koolohms are wound with larger diameter wire for the same rating yet are available in far higher resistance values (for example, 70,000 vs 25,000 ohms at a full 10 watts). Koolohms are available in *truly non-inductive* windings when needed. Koolohms have exceptional resistance stability.

Koolohms have all these advantages because they are the *only* resistors wound with ceramic-insulated wire (an exclusive Sprague development) and are enclosed in glazed moisture-resistant ceramic outer shells. Mounted on a metal chassis, Koolohms will withstand a 10,000 volt breakdown test from winding to ground.

Koolohm resistors are ideal for television sets and other tough applications—and are equally good for all ordinary electronic and industrial control uses.

Best of all, premium-quality Koolohm resistors are *competitively priced.*

Sprague Catalog 100E tells The Complete Koolohm Story. Write for your copy today.



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PERMANENT MAGNET MATERIALS

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- Deltamax Toroidal Cores • Supermalloy* Toroidal Cores
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*Manufactured under licensing arrangements with WESTERN ELECTRIC COMPANY

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THE ARNOLD ENGINEERING COMPANY

SUBSIDIARY OF ALLEGHENY LUDLUM STEEL CORPORATION

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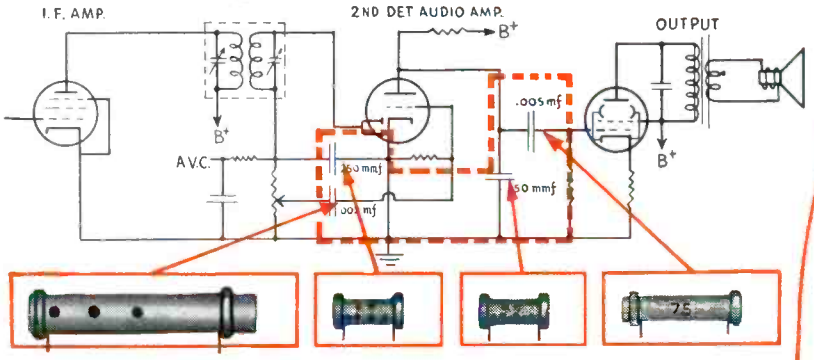
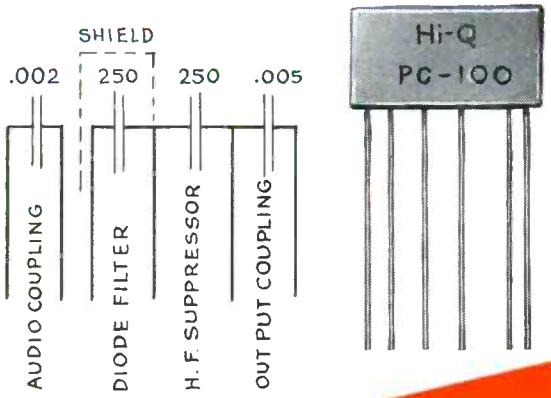
Specify Hi-Q COMPONENTS for PRINTED CIRCUITS



. . . THE PROBLEM

Hi-Q engineers were recently asked to design a component which would replace the 4 standard components called for in the schematic drawing illustrated at left. The problem was one of space saving without affecting the operation of the circuit.

HERE IS HOW Hi-Q SOLVED THE PROBLEM OF SPACE SAVING AND REDUCED COST



THE SOLUTION

Hi-Q engineers designed a printed circuit known as the **Hi-Q** P. C. 100. This component replaced all 4 of the standard sized units formerly used, thus reducing the physical proportions of the space formerly required. In addition, this new component eliminated 25% of soldering time as well as eliminating 75% of the unit handling cost. The result of this customer's foresight in placing his problem before **Hi-Q** engineers is that a new component was designed which saved our customer space, labor and time.

WHAT'S YOUR PROBLEM?

Our engineering department will gladly work with you on any problems you might have. Consult with us and ask for our suggestions regarding your specifications before your design has gone too far. Perhaps we can work out savings in space, time and labor for you.

Hi-Q COMPONENTS BETTER 4 WAYS

PRECISION Tested step by step from raw material to finished product. Accuracy guaranteed to your specified tolerance.

UNIFORMITY Constancy of quality is maintained over entire production through continuous manufacturing controls.

DEPENDABILITY Interpret this factor in terms of your customers' satisfaction . . . Year after year of trouble-free performance. Our Hi-Q makes your product better.

MINIATURIZATION The smallest BIG VALUE components in the business make possible space saving factors which reduce your production costs . . . increase your profits.

WRITE FOR FREE CATALOG

Hi-Q *Electrical Reactance Corp.*
FRANKLINVILLE, N. Y.

Plants: FRANKLINVILLE, N. Y.—JESSUP, PA.
Sales Offices: NEW YORK, PHILADELPHIA, DETROIT, CHICAGO, LOS ANGELES

Watch Master

Frequency Standards

GUARANTEED ACCURACY
1 part in 100,000
(.001%)

Type 212

TERMINATION
Front and Rear
CONSTRUCTION
Standard 8¾" x 19" Panel
HOUSING
8¾" x 19" x 8" Metal Cabinet
WEIGHT
25 pounds

Uses

Time bases, rate indicators, clock systems, chronographs, geo-physical prospecting, control devices and for running small synchronous motors.

Features

1. **Bimetallic, temperature-compensated fork, no heating or heat-up time is required.**
2. **Fork is hermetically sealed, no barometric effects on frequency.**
3. **Precision type, non-ageing, low coefficient resistors used where advantageous.**
4. **Non-linear negative feedback for constant amplitude control.**
5. **No multi-vibrators used.**
6. **Synchronous clock simplifies checking with time signal.**

Specifications

Accuracy—1 part in 100,000 (.001%).
Temperature coefficient—1 part in 1,000,000 per degree centigrade (or better).
Outputs—

1. **60 cycles, sine wave, 0-110 volts at 0 to 10 watts (adjustable).**
2. **120 cycle pulses, 30 volts negative.**
3. **240 cycle pulses, 30 volts positive and negative. Pulse duration, 100 micro-seconds.**

product of

AMERICAN TIME PRODUCTS INC.

580 Fifth Avenue **New York 19, N. Y.**

Operating under patents of the Western Electric Company

American Time Products, Inc.,
580 Fifth Ave., New York 19, N. Y.
Gentlemen:
Please send descriptive folder, No. 212

Name.....

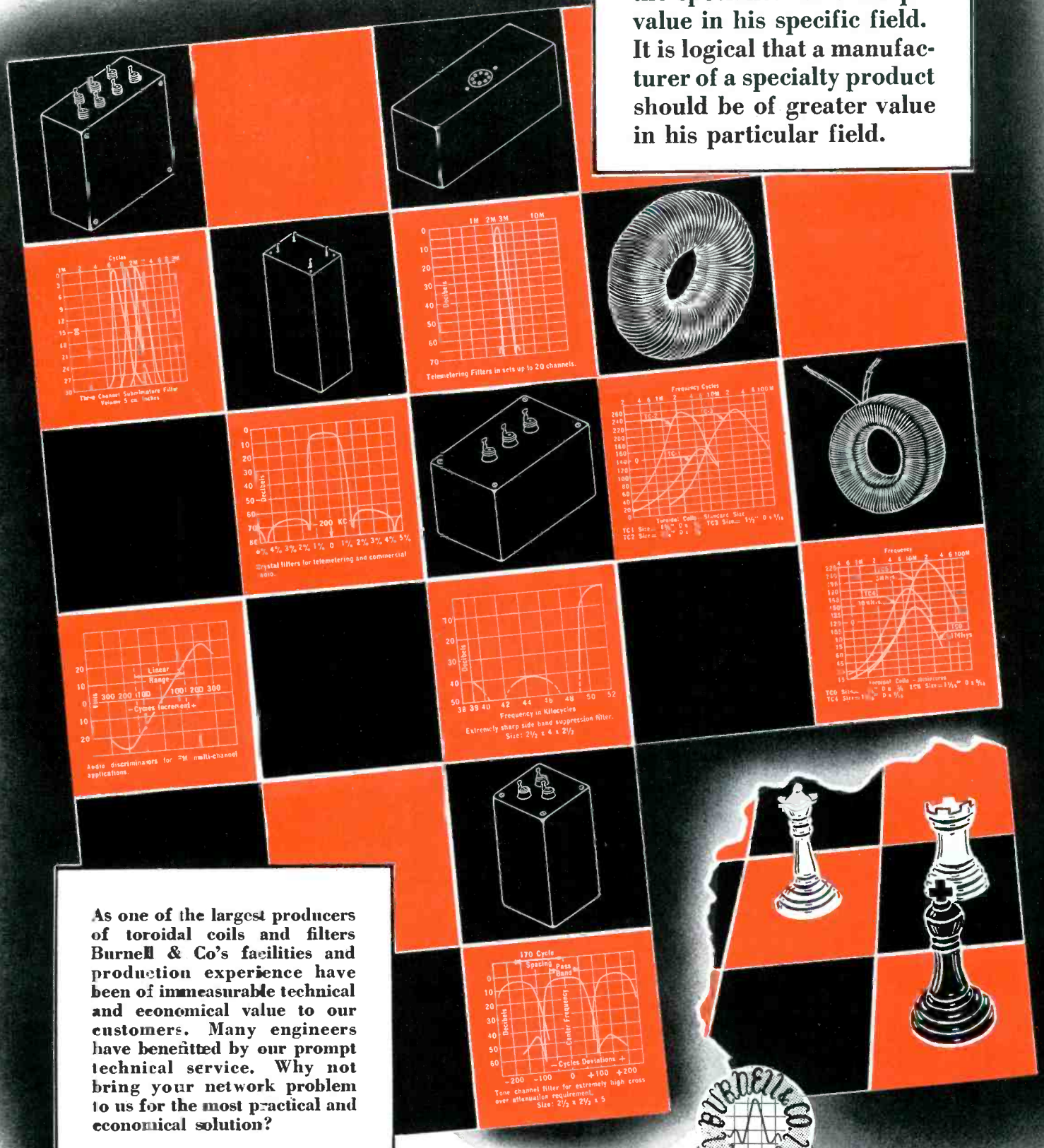
Company.....

Address.....

City..... State.....

Check YOUR NETWORK PROBLEM WITH LOGIC

In any technical business the specialist has a unique value in his specific field. It is logical that a manufacturer of a specialty product should be of greater value in his particular field.



As one of the largest producers of toroidal coils and filters Burnell & Co's facilities and production experience have been of immeasurable technical and economical value to our customers. Many engineers have benefitted by our prompt technical service. Why not bring your network problem to us for the most practical and economical solution?

EXCLUSIVE MANUFACTURERS OF COMMUNICATIONS NETWORK COMPONENTS

WRITE FOR TECHNICAL INFORMATION
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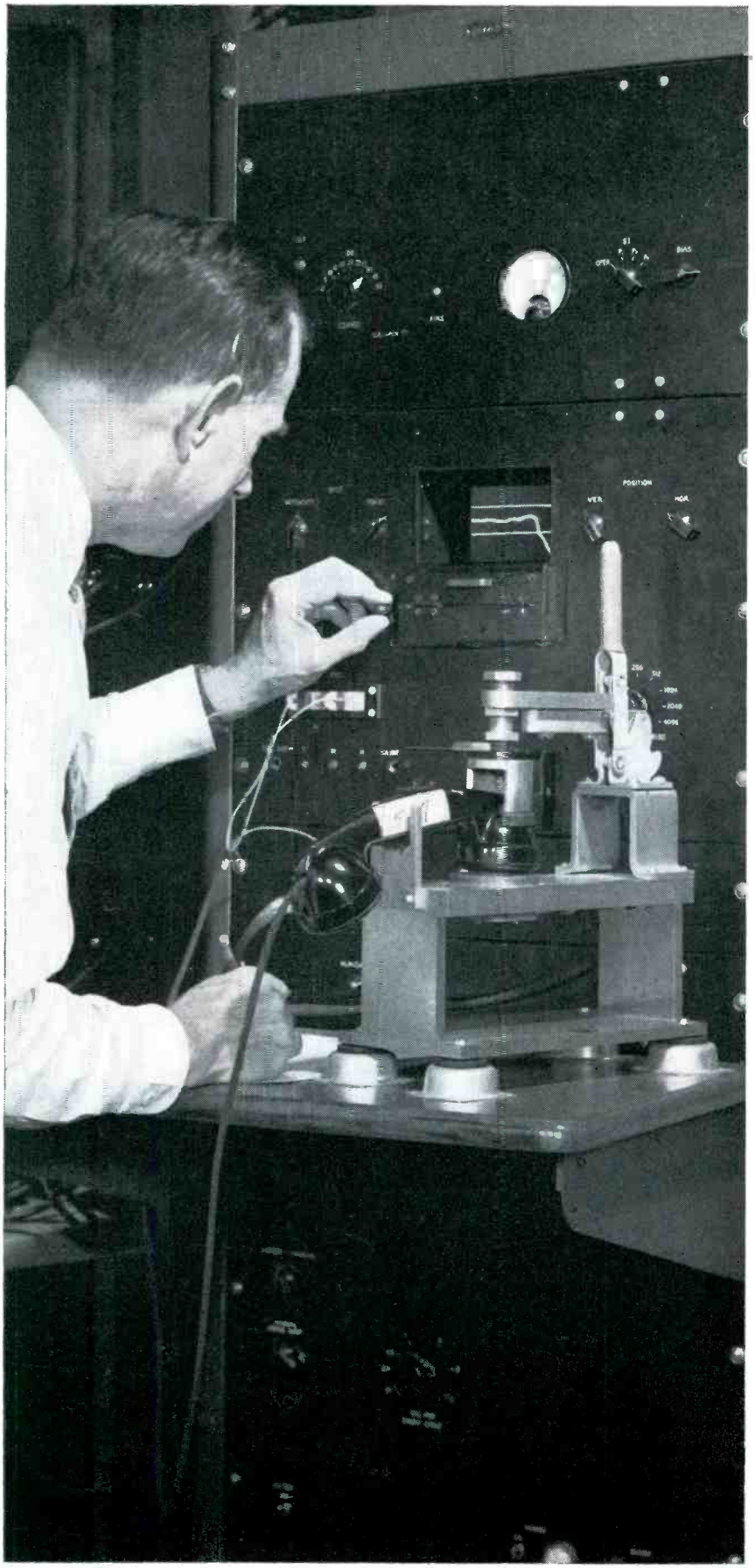


YOUR telephone receiver should treat each tone in the voice alike; that is important to you, because proper balance makes pleasant listening and easy understanding. Naturalness in receiver performance is pictured in a matter of seconds by the apparatus shown at left.

The receiver is clamped in place and an oscillator feeds into it frequencies representing all talking tones. Then a bright spot darts across an oscilloscope screen leaving behind it a luminous line which shows instantly the receiver's response at each frequency. It is precise; and it is many times faster than the old method of measuring receiver performance point-by-point and then plotting a curve.

It listens so YOU can hear better

At Bell Laboratories, development of techniques to save *time* parallels the search for better *methods*. For each time an operation is made faster, men are freed to turn to other phases of the Laboratories' continuing job—making your telephone system better and easier for you to use each year.

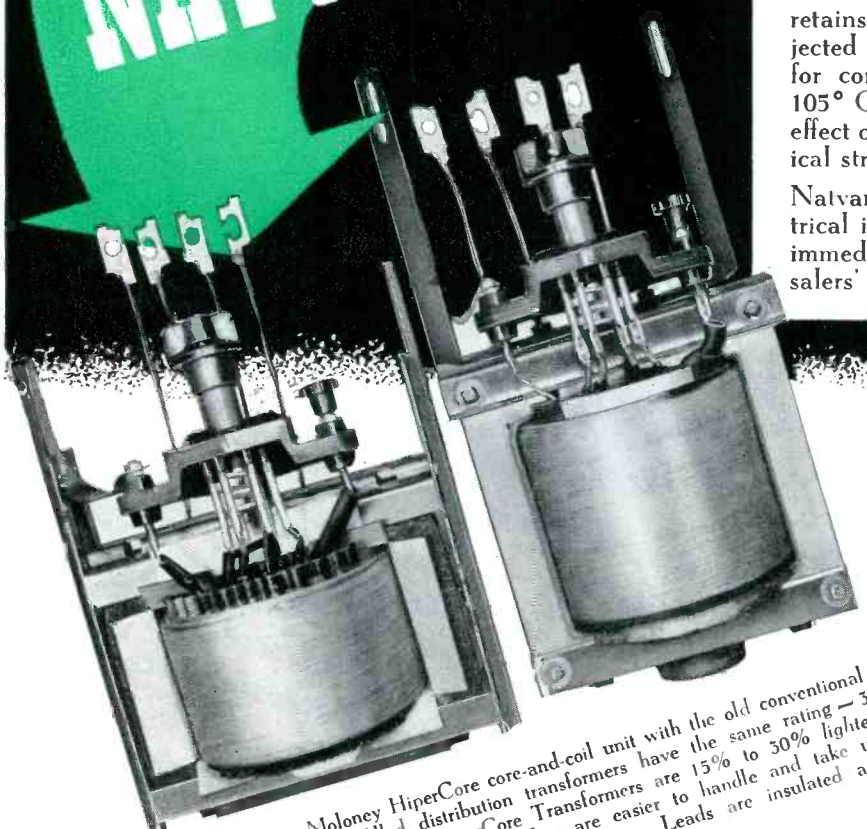
MOLONEY ELECTRIC'S NEW *HiperCore* TRANSFORMER HAS LEADS INSULATED AND PROTECTED *with* NATVAR 400

THE new HiperCore Transformers manufactured by Moloney Electric Company, St. Louis, are lighter and smaller than their predecessors, and yet have improved performance characteristics. They provide better voltage regulation and permit greater short-time overloads.

Cores are wound of high permeability, oriented silicon steel having 30% to 50% greater flux carrying capacity than hot rolled core steel, making it possible to decrease the amount of steel, copper and other materials, and at the same time improve operating characteristics.

Natvar 400 Extruded Vinyl Tubing is used to insulate and protect leads because it retains its original properties when subjected to *both heat and oil*. It is approved for continuous operating temperatures of 105° C, and immersion in oil has no adverse effect on its flexibility, dielectric, or mechanical strength.

Natvar 400 and other Natvar flexible electrical insulating materials are available for immediate delivery, either from your wholesalers' stocks, or direct from our own.



Compare the new Moloney HiperCore core-and-coil unit with the old conventional type. Both of these oil-filled distribution transformers have the same rating — 3 Kva, 7200-120/240 volts. Yet HiperCore Transformers are 15% to 30% lighter and up to 30% *smaller*, which means they are easier to handle and take up less space on the line truck and in the storeroom. Leads are insulated and protected with Natvar 400.

Natvar Products

- Varnished cambric—straight cut and bias
- Varnished cable tape
- Varnished canvas
- Varnished duck
- Varnished silk
- Varnished special rayon
- Varnished Fiberglas cloth
- Silicone coated Fiberglas
- Varnished papers
- Slot insulation
- Varnished tubings and sleevings
- Varnished identification markers
- Lacquered tubings and sleevings
- Extruded vinyl tubing and tape
- Extruded vinyl identification markers

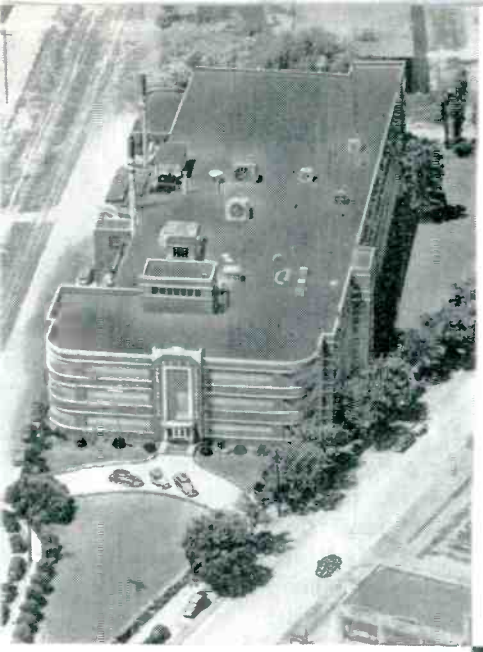
Ask for Catalog No. 21

THE NATIONAL VARNISHED PRODUCTS *Corporation*

TELEPHONE
RAHWAY 7-2171

CABLE ADDRESS,
NATVAR: RAHWAY, N. J.

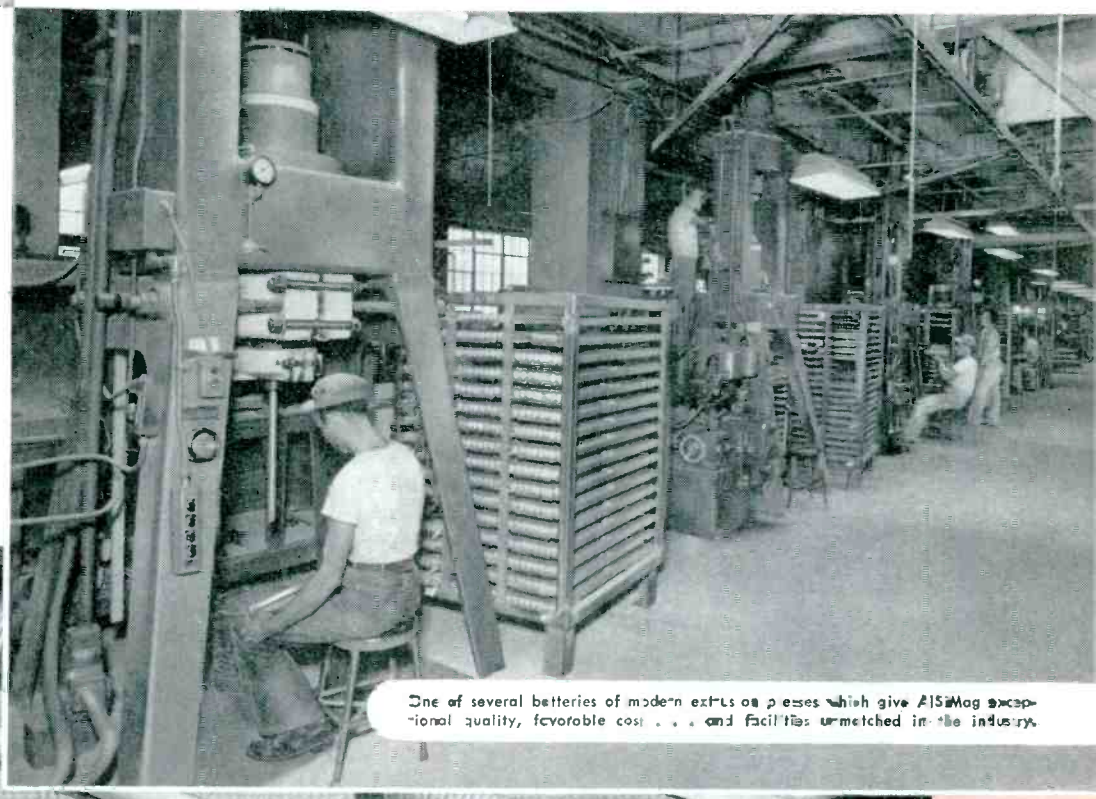
201 RANDOLPH AVENUE ★ WOODBRIDGE, NEW JERSEY



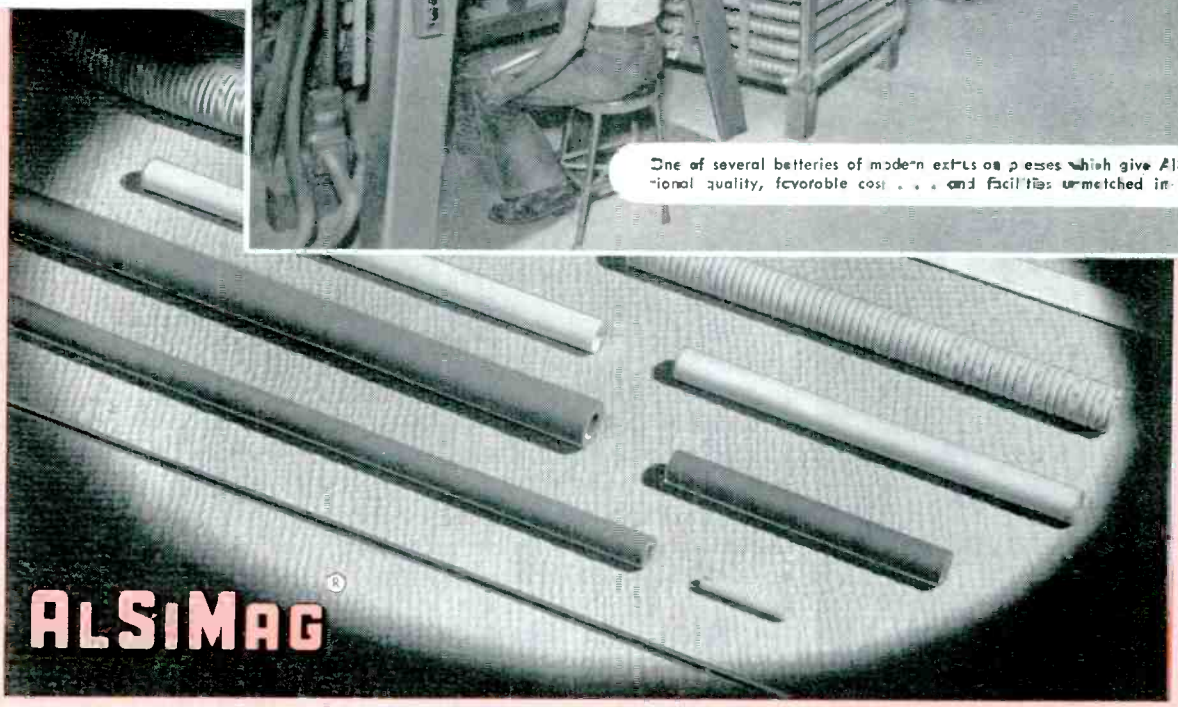
extrusion

Carefully controlled compositions extruded through precision made dies . . . a fast, economical production method for many shapes in Custom Made Technical Ceramics

Basic shapes which have been extruded can be cut, machined, threaded, drilled in the unfired state. This combination of processes . . . all available under one roof . . . can produce seemingly complex parts at prices favorable to your production budget. Send us your blueprint for recommendations.



One of several batteries of modern extrusion presses which give AlSiMag exceptional quality, favorable cost . . . and facilities unmatched in the industry.



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48TH YEAR OF CERAMIC LEADERSHIP

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NEW ENGLAND, 38-B Brattle St., Cambridge, Mass., Kirkland 4498 • ST. LOUIS, 1123 Washington Ave., Garfield 4959

BUSINESS BRIEFS

By W. W. MacDONALD

Prices Are Dropping. This will be news to nobody. But you may not sit at a vantage point like ours, so you may not realize that while prices are dropping they have not yet dropped much.

Will prices drop farther? We think so, but we do not think they are going into the cellar. Just as soon as they are low enough to bring people who have money to spend but do not think it buys enough at present back into the market the drops will stop.

This may be in late 1949. Or it may be later.

Comparison Shopping is just around the corner in the television receiver market, unless we miss our guess. Already there are signs that initial enthusiasm has worn off to the point where buyers are becoming interested in more than just the size of the picture. They are beginning to check up on brightness, sharpness and steadiness. And the eye is more critical than the ear, so this tendency may play a much more important part in the television business than it ever did in radio.

Little differences in television receiver design may in the near future make a sale or lose it to a competitive make. Several manufacturers are aware of this and are improving picture quality rather than just shooting at price. One, for example, is building voltage-regulating transformers into his sets, with another on the verge of following suit. The trick transformer is considerably more expensive than a conventional type but we understand that the differential was held to a mere 68 cents by taking advantage of better regulation to effect economies in other parts.

Nearly All established tube manufacturers are now turning out cathode-ray tubes for television, so the bottleneck is pretty well broken. There are, as a matter of fact, a lot of new companies in the field so the competition for business is apt to be keen in the months immediately ahead. Already, we hear, set manufacturers have been offered price concessions in return for long-term contracts.

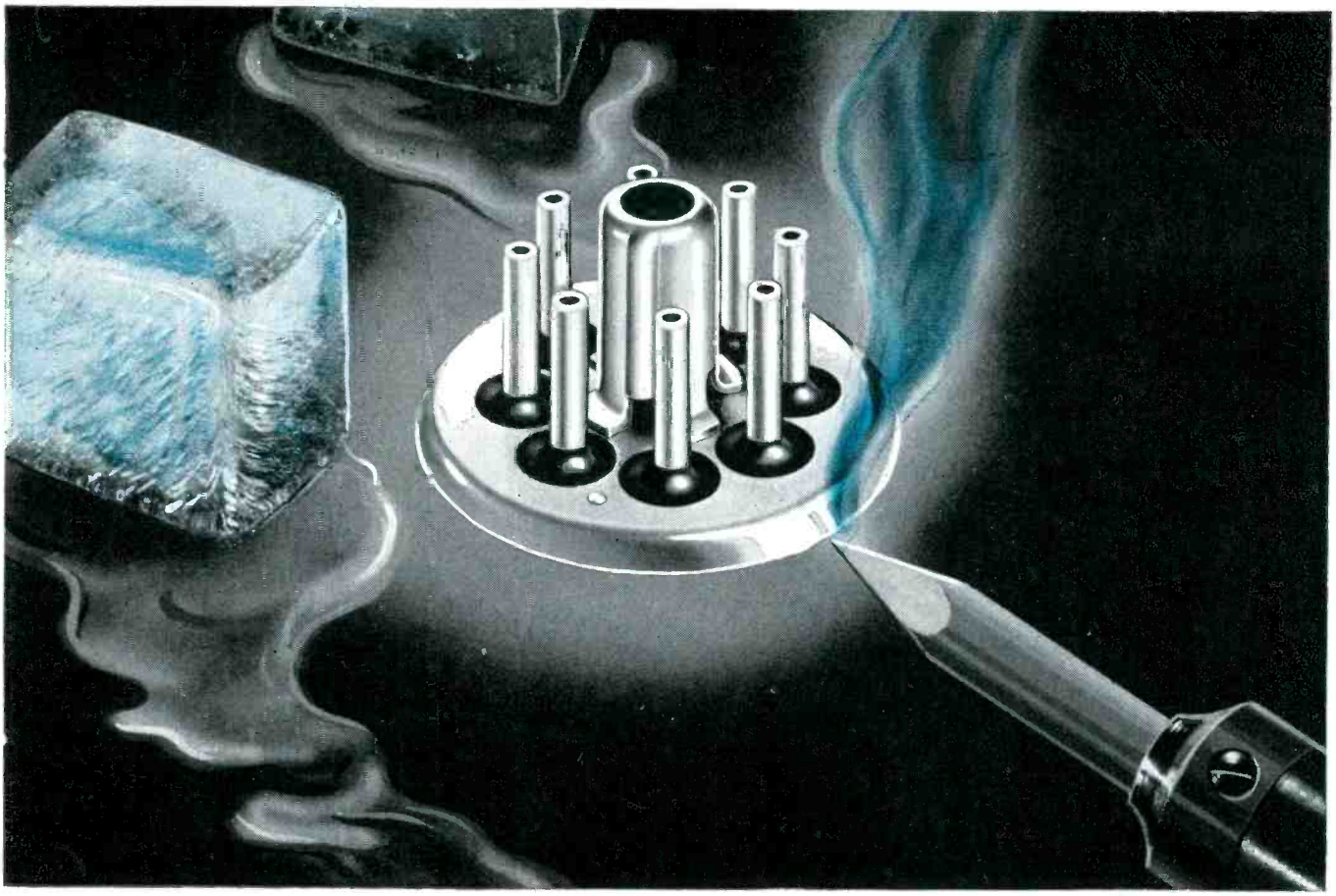
Beating Popular Magazines and newspapers to a possible low punch, we have it on good technical authority that picture tubes in television receivers radiate no measurable quantity of x-rays when operated below 10,000 volts (where most of the sets at present on the market *do* operate) and not enough even at double this voltage to be injurious unless one does a Rip Van Winkle in their presence.

We understand, furthermore, that where large-screen direct-view or projection models use very high voltages manufacturers have already quietly taken design steps to eliminate any radiation that might occur, playing it safe for their own workers as well as the ultimate consumer.

An NAB Study indicates that with only 57 stations on the air television already employs about 10 percent as many full-time workers as the entire a-m/f-m broadcasting industry. The average station at present employs 46 full-time workers. About 50 percent of these people are technicians, 22 percent program personnel, 16 percent general administration, 8 percent film department and 4 percent sales.

Record-Player Makers have pulled out all the stops in their effort to give the consumer machines that handle 33⅓, 45 and 78-rpm platters. Out at the Parts Show in Chicago we saw a new one that not only plays all three but plays them automatically on both sides. About the only thing it will not play is a manhole cover.

Speaking Of Chicago, trouble seems to be brewing for the Parts Show policy makers. Many exhibiting manufacturers were unhappy about the comparatively light distributor attendance, didn't know



Let's Put the Chill on a Hot Subject . . .

As you read this message engineers the country over are hard at work planning, experimenting on fused hermetic sealing for their company's electrical product.

When the subject of a so-called glass terminal comes up (and it's bound to) they're apt to talk in terms of thermal shock. That's where Fusite Hermetic Terminals come in.

Take the interfusion of steel and inorganic glass that is a Fusite terminal. Apply the sizzling heat of a soldering or welding operation. And if you want to be ornery, shove it right out on the shipping dock on a zero day.

What happens?

Absolutely nothing. Your seal remains as tight as your production skill made it. All Terminals remain as smooth, as rugged, and uniform as only Fusite makes them.

Would you like to know more, or see samples? Write to Dept. E.

TERMINAL ILLUSTRATED 908HTO—For plug-in to standard "Octal" sockets. Available with two to eight hollow tube electrodes.

INSULATE ELECTRICALLY
GLASS TO METAL
FUSITE
TERMINALS
PROTECT PRODUCT PERFORMANCE
SEAL HERMETICALLY

THE FUSITE CORPORATION

CARTHAGE AT HANNAFORD, NORWOOD, CINCINNATI 12, OHIO

how much to attribute to a general slackening of business and how much to the fact that admission was limited to members of NEDA during certain hours.

Military Business for the electronics industry has so far this year been disappointingly less than expected, according to RMA's Max Balcom. He expects it to pick up, however, in the near future.

Potted Circuits have moved out of the experimental into the early commercial stage. Subassemblies cast in plastic are now in use in a number of military items and we know of several examples of use in connection with apparatus offered for general sale.

Suppliers of plastics privately admit that they still have much to learn and point out that a potting material suitable for one application may not be suitable for another. They are making progress, however, and one of the things they have learned is that in addition to protecting parts against shock, vibration, humidity, temperature and tampering some assemblies can actually be made cheaper because no chassis and no anchoring accessories are needed.

The technique may not grow fast, but it is certain to grow.

Back In March (p 66) we pointed out that static electricity could be used to attract liquids or powders to paper or cloth.

Huebner Laboratories of New York has developed a method of printing without pressure, based on this principle. In connection with his process W. C. Huebner uses the words *electro-migratetics* (for liquids, wet particles, solvents, vapors, dyes and lacquers), *electronographics* (for inks, semi-wet particles, pigments and pastes), *depositronics* (for powders, semi-dry particles, defloculated materials), *magnetetics* (for metallic dry particles) and *combustion-precipitronics* (for smoke particles, chemical colors and gases).

A Friend Of Ours out in Detroit has an idea that should interest people who use tubes in equipment requiring extremely uniform char-

acteristics and long life. He is set up to study the operation of various tubes in newly designed apparatus, duplicate required operating conditions in a test setup, and then to build or supply instructions for building test racks in which a supply of tubes can be aged and checked.

Sounds to us like a natural for certain measurement, control and computer applications.

Test Equipment is big business. A whale of a lot of instruments go into manufacturing plants of all kinds. Take the Electronics Section of The Glenn L. Martin Company, down in Baltimore, for example. It owns:

47 a-f signal generators
41 ammeters
16 amplifiers
4 analyzers
10 bridges
51 capacitor decades
8 field-strength meters
12 frequency meters
37 miscellaneous items
64 oscilloscopes
3 potentiometers
95 power supplies
31 pulse generators
20 Q-meters
5 receivers
5 recording meters
65 resistor decades
14 r-f meters
43 r-f signal generators
9 special-purpose testers
20 special r-f items
8 square-wave generators
23 synchroscopes
2 tube testers
80 vacuum-tube voltmeters
51 variable-power controls
30 voltage regulators
56 voltmeters
105 volt-ohm-milliammeters
4 wattmeters
8 wavemeters

One will get you three that the average reader of ELECTRONICS doesn't even know that Martin, well known for its airplanes, is even casually active in our field.

On The Odd Chance that you are as interested in our problems as we are in yours, one of the crosses an editor has to bear is the fact that he continually runs across engineers who have a good technical story in their system but "no time to write." This phrase is indelibly engraved upon the mind of every staff man.

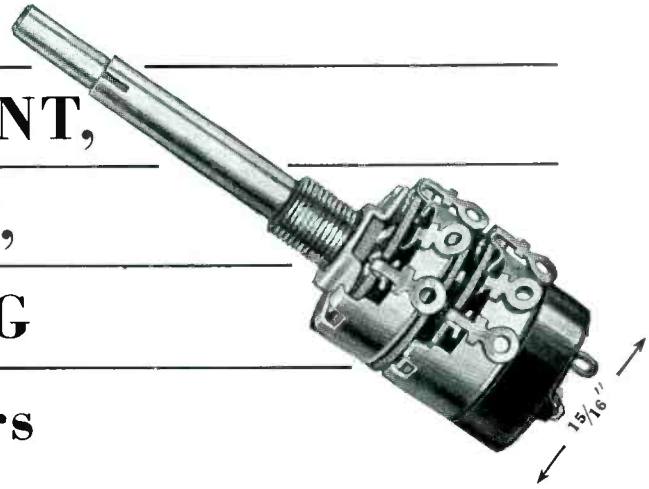
Usually, there is some mutually advantageous solution. We have developed a number of effective shortcuts. Try us and see.

He studied electrons with vigor;
An oscilloscope's use was de rigeur.
But his poor mind was maimed;
Saw a girl and exclaimed,
"What a beautiful Lissajous figure."

—Sam H. Seeleman
McLaughlin Research Corp.
New York

NOW! The MALLORY MIDGETROL DUAL

. . . to help you make MORE CONVENIENT, MORE EFFICIENT, BETTER LOOKING Television Receivers



Highlights of the MALLORY MIDGETROL DUAL

1. Combines two quiet, compact controls on concentric shafts.
2. Insulated for the higher voltages encountered in television.
3. Special low-drift resistance element meets temperature-humidity drift problem.
4. Only dual control with two-point shaft suspension, which means—shorter bushing may be used, more stable resistance values are obtained, less danger of damage in assembly, longer life, longer shafts may be safely specified.
5. Available now for prompt delivery and competitively priced!

Now Mallory has produced a *Dual* Mallory Midgetrol with concentric shafts.

Mallory precision manufacturing PLUS small size (15/16" diameter) provide a method to move several key television adjustments from the rear of the chassis to the front. Eight single controls now required to make adjustments can be changed to only four Dual Mallory Midgetrols, permitting ready adjustment at the front of the chassis.

You get a cleaner-looking set, an easier set to produce —and the Mallory Midgetrol provides the ruggedness and dependability television parts must have.

Read the highlights of the Mallory Midgetrol *Dual* . . . and see why those who have seen what it can do to improve quality and cut costs are so enthusiastic about its future.

P. S. The unique qualities of the Mallory Midgetrol *Dual* make it perfect for many applications in other fields as well. Mallory engineers will be glad to tell you more about it. Write Mallory today.

Precision Electronic Parts—Switches, Controls, Resistors

P. R. MALLORY & CO. Inc.

MALLORY

P. R. MALLORY & CO., Inc., INDIANAPOLIS 6, INDIANA

SERVING INDUSTRY WITH

Capacitors — Rectifiers
Contacts — Switches
Controls — Vibrators
Power Supplies
Resistance Welding Materials

CROSS TALK

► **INVENTION** . . . It is fashionable in our industry to say that patents have become unimportant, that they represent only a license to sue. But the electronics business operates on the basis of patent pools operated, and for the most part wisely administered, by a few large corporations. The question of what constitutes an invention is, therefore, of prime importance to the electronic engineer, whether he be inventor or licensee.

The basic argument seems to be between the Patent Office and the Courts, notably the Supreme Court. Unless the patent discloses a transport of pure inventive genius, the chances are it will be ruled invalid by the high courts. The process of assembling prior art into a system or process which fills a long-felt need is considered by the Bench to be praiseworthy but not patentable.

We think a recent dissenting opinion of Mr. Justice Jackson reveals the fallacy of this argument with telling effect. The case involved the "lost-wax" process of casting intricate metal shapes, and it was shown that Benvenuto Cellini had used a similar process centuries ago. But it was also shown that the casting industry had not known how to apply the Cellini technique and hence needed, and had been eager to obtain licenses under, the patent in question. Said Mr. Justice Jackson: "And if Benvenuto Cellini's age-old writings are so revealing to us laymen of the Appellate Bench, it is hard to see why this practical-minded industry, which the Court says was following Cellini, failed through all the years to get his message." We hope the other members of the Bench get Mr. Jackson's message. Otherwise inventive progress may slow to a walk.

► **OBIT** . . . We regret to record the passing of Edwin H. Colpitts, whose name is known to tens of thousands of radio amateurs and engineers for his development of the Colpitts oscillator. Like his colleagues Hartley and Heising at the Bell Laboratories, Colpitts entered the ken of many a young man when the momentous decision of what kind of an oscillator to build, and how to modulate it, was made. Like these men, also, he is best known for a minute part of the work of a busy lifetime. Dr. Colpitts worked with the great G. A. Campbell on telephone line loading, he designed toroidal repeating and retarding coils, cross talk and transposition systems, and as early as 1911 was in charge of the staff working on application of electron tubes to long-distance telephony by wire and radio. In 1937, then vice-president of the Laboratories, he retired, but remained active in engineering affairs until his death at the age of 77. His was a vigorous life, well spent in a demanding profession, a challenging example for those that follow.

►**MISCELLANY** . . . Viennese violinists can dial a number and get standard musical pitch from the Vienna Bureau of Weights. Bell System please copy. . . . The CIO's Political Action Committee has tipped off local leaders that they can get a citizens radio permit by return mail from the FCC, suggest using handie-talkies to operate picket lines and to get out the vote. Being neutral in politics but partisan for citizens radio, we urge the NAM and the U. S. Chamber of Commerce to rally around with some uses of their own, including getting out the vote. . . . A cyclotron in Chicago has been caught interfering with flight communications at LaGuardia Field in New York. The professors have been busy plugging up the chinks in the shielding and at last report they had left the field to old man static, who remains supreme. . . . By a very roundabout method, National Bureau of Standards men have come up with two new digits in the charge-to-mass ratio of the electron. Paste it in your hats, boys, it's 1.7588×10^7 emu per gram.

NEEDED: Better Parts for Industrial Controls

An equipment designer serving the industrial field tells what new components are needed and makes suggestions for improvement of existing lines. Demand for industrial rather than radio-type parts is still great

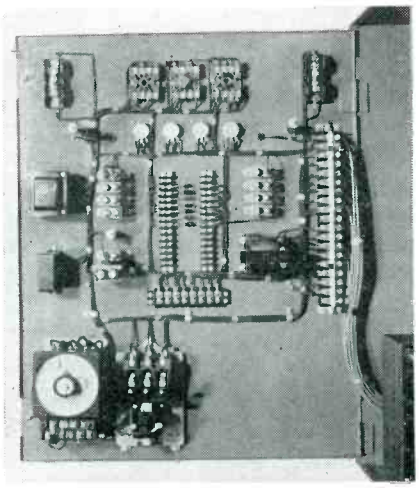
SINCE the end of the war the designer of industrial electronic devices has seen the development of a variety of components more suitable for his specialized requirements than radio-type parts.

Many rugged and conservatively rated components designed to meet the needs of industry have appeared on the market. However, the need for other parts, and improvement of existing types, is still great.

Connectors and Terminal Boards

Servicing of industrial devices is simplified by a minimum number of soldered connections. Screw connections are preferred in many cases since a screwdriver is the most common tool around any plant. Furthermore, use of this technique often decreases production costs. Design has advanced to the point where solderless connectors, properly applied, result in connections as good as any well-soldered joint.

Terminal boards and strips are available in a large variety of designs. A compact feedthrough-type board with screw terminals on both sides would, however, be a welcome addition. It is further suggested that there be included in such a line resistor and capacitor mounting boards with screw terminals. The design should be such as to permit making connections to the mounting board without disturbing resistor or capacitor leads. More generous electrical barriers should be placed between adjacent terminals. Tie points should be stronger and have better electrical clearances to ground than they do at present.



Electronic regulator using a hinged panel, generous spacing of parts and screw-type terminal strips to simplify maintenance

Tubes and Sockets

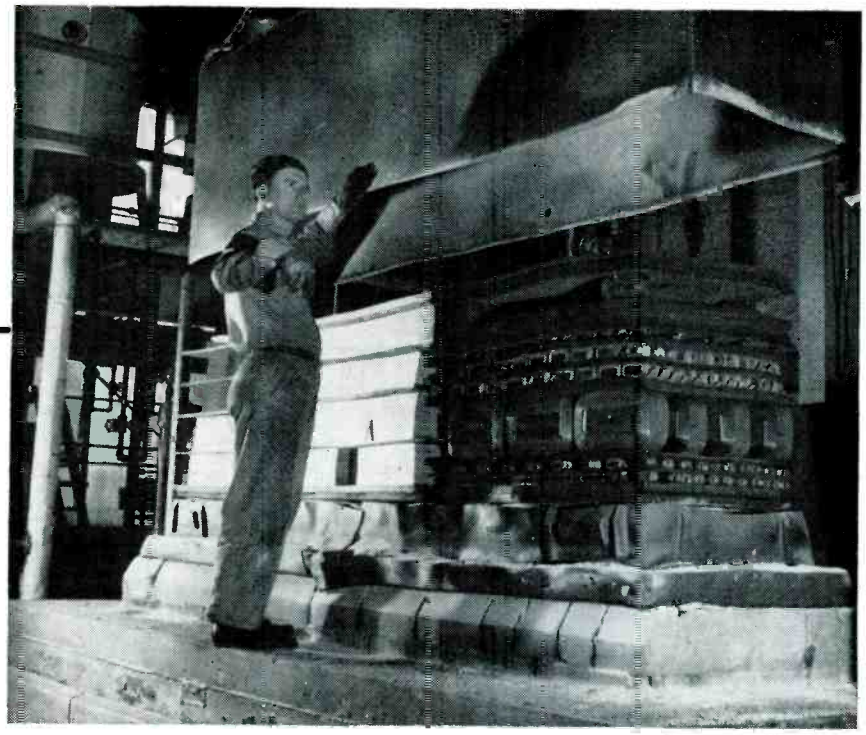
A few phototubes, regulator tubes, amplifier tubes and high-vacuum rectifier tubes are already available in industrial versions. Conventional radio amplifier tubes such as the 6SN7, 6SJ7 and 6SL7 are also available in ruggedized design, providing excellent uniformity, stability and long life. In line with this trend, there should also be a more extensive line of high-vacuum rectifiers, regulator tubes, and phototubes designed specifically for industrial use.

Some noteworthy strides have been made in tube sockets. Screw terminals have been provided. Good insulating materials give high dielectric strength, satisfactory shock factors and low moisture absorption. Barriers providing electrical clearances are more than adequate. Metal parts are well protected against corrosive atmospheres and tube pin contacts are designed to maintain good spring tension under conditions of high temperature. Contact resistance has been reduced to a minimum through increased pin contact area.

While the socket line is fairly complete in its coverage, some weaknesses have shown up which may be worthy of consideration by manufacturers. In some industrial octal sockets the center hole has been found to be slightly undersize, making it difficult to insert or remove tubes. The metal screw terminals permit utilization of only a very short threaded section, restricting the number of connections that can be made to any one terminal. It might be desirable to use a speednut style which would accommodate a standard machine-screw size, thereby making effective use of the full threaded length of

TIPOFF

Parts manufacturers may find here just the idea they need to open up new accounts or increase sales to those already served



Heavy industry needs controls that are rugged and stand up under the extreme conditions encountered in a variety of plants

By ROLAND RUSSO
The Clark Controller Company
Cleveland, Ohio

the terminal screw. Binding-head terminal screws might be indicated.

On most angle-type sockets for medium-base four-pin tubes, the terminal screws are definitely too small; wires that have to carry heavy filament current cannot be readily accommodated. The insulating barriers which separate the terminals of such sockets are often located so that wiring of the socket is quite difficult. The terminal design of the super-jumbo angle socket is good and the same scheme should be worked out for the medium-base socket.

Resistors and Capacitors

Little need be said about the composition resistor situation inasmuch as fixed resistors of this type to satisfy almost any requirement are available.

In the wire-wound styles the selection is also satisfactory. The situation, however, in the variable-resistor types is not as good, especially in the lower ratings from less than one watt up to about 25 watts. Such types do not always have adequate clearances between terminals or from terminals to case. Screw-type terminals and heavier construction in mechanical details would be desirable, with insulation designed to withstand at least 2,500 volts to ground.

Capacitors generally present little or no problem in procurement. Some of the needs in the industrial field are being presently fulfilled, with one of the more recent innovations being a line of molded tubular paper capacitors, small in size and able to operate in high temperatures and withstand high humidity.

Metal-can capacitors with good electrical properties are widely available but a lack of screw-type terminals prevails. The most common terminals seem to be the threaded-stud type on the larger capacitors and the solder terminal on the smaller types. Capacitors with screw-type terminals, insulating barriers between terminals and means of restricting solderless connections from turning and touching together are needed.

Transformers used in industrial electronic circuits are varied in design and type. The majority are necessarily pretty specialized. However, a standard line of filament transformers could be offered industrial equipment designers for use with the more commonly used rectifier tubes. Since tube filament voltage must be maintained within close limits for proper tube operation, provision should be made for easy correction of secondary voltage.

A standard line of universal power transformers for supplying control-amplifier d-c voltages would also be desirable. At the present time the radio-type universal replacement power transformer is generally used. This type of transformer is not ideally suitable for industrial work since the rating is generally too liberal and construction is not rugged enough.

Other Needs

There is a need for rugged and inexpensive time-delay relays for filament pre-heating, preferably of the adjustable type. Those presently available in the low-priced field are often susceptible to faulty operation under shock and vibration conditions. Most types instantly release when there are momentary power failures, resulting in unnecessary delay while the relay recloses.

While fuses generally are used in the anode circuit of the power rectifier for tube protection, it is extremely desirable to use circuit breakers so that controlled protection is available and immediate resetting may be provided. However, no circuit breaker with tripping characteristics that match tube current ratings is at present known to the writer.

A new connector for the medium C1-5 tube cap is also needed, one which has no exposed metal, is molded of high-temperature insulating material and to which leads may be attached with a screwdriver. Riveted or soldered connectors are undesirable from the standpoint of the heat encountered at tube caps as well as the amount of time expended in wiring the leads to the cap connectors.

CONTINUOUSLY

Designed to cover the band from 475 to 890 mc, this unit will feed the antenna input or i-f amplifier of an existing receiver to extend range to proposed uhf channels. Modification of Karplus coaxial tuner used in antenna and oscillator circuits

By ROBERT P. WAKEMAN *Research Division, Allen B. DuMont Laboratories, Inc. Passaic, N. J.*

THE growth of television during the past year, its remarkable acceptance by the public, and the increasing interference as new stations come on the air have combined to prove the inadequacy of the twelve channels now assigned to commercial broadcasting. It appears quite probable, therefore, that ultrahigh frequency allocations will be made by the FCC in the near future. When uhf service starts, the receiver manufacturers will have uhf receivers available. But, there are approximately one and a half million television receivers in use today and there will probably be another million in use before uhf television becomes a reality. It is certainly in the manufacturer's interest as well as his responsibility to protect the investment of the pioneer viewers. The protection may take the form of a converter located near the receiver. In some cases it may be possible to place a small unit inside the television cabinet and bring out additional controls on the front panel.

FIG. 1—External view of converter. Dial scale shows compression of tuning at high-frequency end of band

The receivers to be sold during the next few months present more of a problem. Protection can work two ways. The customer must be protected against obsolescence, but he must also be protected against being forced to buy a gadget which he can never use. Since many homes may never be within range of a uhf station, it is equally wrong to build in a uhf tuner as an integral part of every television receiver or to ignore the problem entirely. Probably the best solution is to design future receivers so that a uhf converter section can be readily installed and made an integral part of the set, when and if a uhf station becomes available to the purchaser.

The portion of the uhf band to be made available for commercial television, the number of channels and their spacing have not yet been decided. Consequently, the tuner, either in the converter form or as an additional unit to be installed in the receiver, must be capable of covering the entire uhf television band. In the interest of minimizing expense to the set owner when he moves from one area to another, a continuous tuner is desirable. Such a tuner has certain other advantages. The initial allocations may be on a temporary basis subject to change. The continuous tuner ob-

UHF TELEVISION NOW IN THE WORKS

On May 26, 1949, the FCC announced a plan for allocating approximately 35 channels for 6-mc black-and-white television, in the lower half of the uhf band from 475-890 mc. While this plan must go through the formal rule-making procedure, including a hearing to be held this fall, it is expected that the final allocation will follow closely the present proposal, and that applications for uhf television broadcasting may be acted upon early in 1950. The equipment described in Mr. Wakeman's paper is, therefore, of particular significance.

The Editors

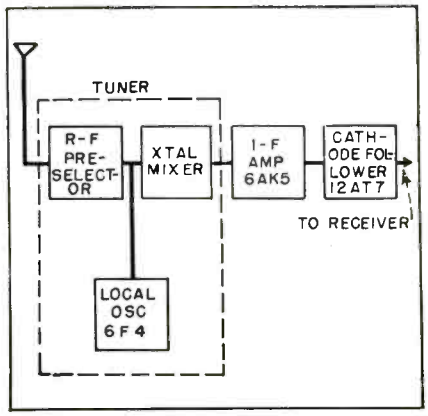


FIG. 2—Block diagram. Adjustment of oscillator permits choice of output frequency on vhf channel or i-f of receiver

TUNED CONVERTER for UHF Television

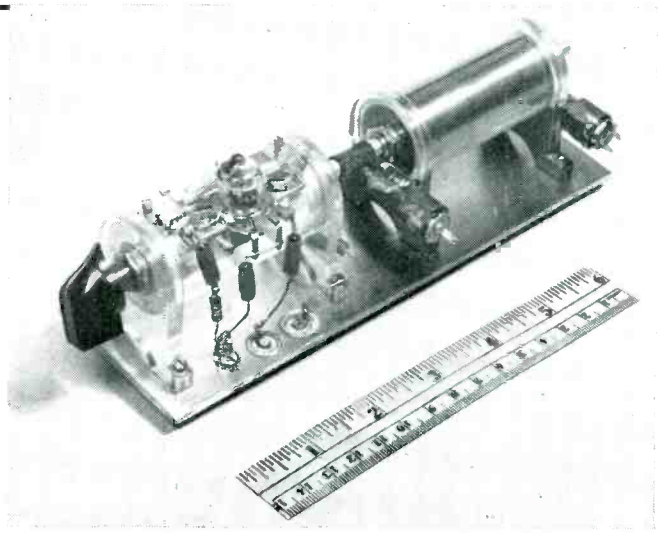


FIG. 3—Tuning assembly. Oscillator at left uses 6F4 acorn tube. Compression screws at ends of assembly adjust tracking

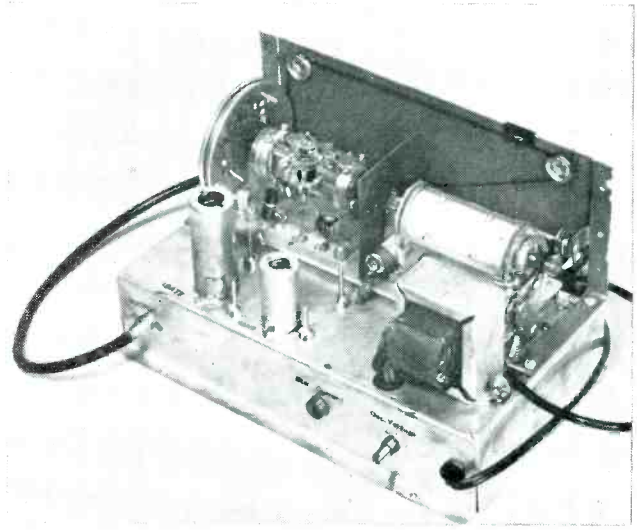


FIG. 5—Rear view of converter assembly. Dial cord at right permits vernier adjustment of tuning

viates the necessity of readjusting a large number of receivers in the field. Furthermore, initial installations will be simplified since the receiver will not have to be set up on specific channels.

Converter Design

These considerations have been taken into account in the converter illustrated in Fig. 1, designed to be used with present day receivers. In a slightly different form it may fit into a specially prepared niche in future receivers.

Figure 2 is a block diagram of the converter. The preselector and local oscillator are ganged and tune from 475 mc to 900 mc. The uhf signal is mixed with the local oscillator signal in a crystal mixer, the difference frequency is selected and amplified in a broad-band i-f stage, and a cathode follower transforms the output to a low impedance. The local oscillator is tuned below the carrier so that the normal position of sound carrier, higher in frequency than picture carrier, is maintained. This is

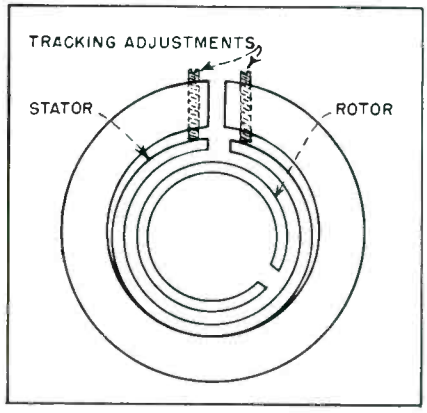


FIG. 4—Cross-section view of coaxial tuner elements

necessary since the signal is being fed to the antenna input of the receiver. The i-f amplifier can be tuned to Channels 1, 2 or 3, depending upon which of these is unoccupied in the area where the converter is to be used.

Both uhf and vhf antennas are brought into the converter. A switch permits connecting either the vhf antenna or the converter output to the receiver antenna terminals. This switch disables the uhf local oscillator, by removing its plate voltage, when vhf is being used. This precaution helps to reduce spurious "birdies".

When the converter is used as an integral part of a receiver, the output frequency is made equal to the receiver intermediate frequency and the switch connects either the vhf or uhf tuner to the i-f amplifier. In this case the switch also serves to disable whichever local oscillator is unused. This system has been found to operate satisfactorily with present receivers and it will probably work even better with the higher intermediate frequency now being considered as an industry standard.

Tuner Construction

The heart of the converter, the tuner, is shown in Fig. 3. The oscillator tuner and tube are at the left and the preselector is at the right. The antenna input is at the far right and the crystal mixer is in the center.

Figure 4 shows a cross section of one of the tuning elements. This

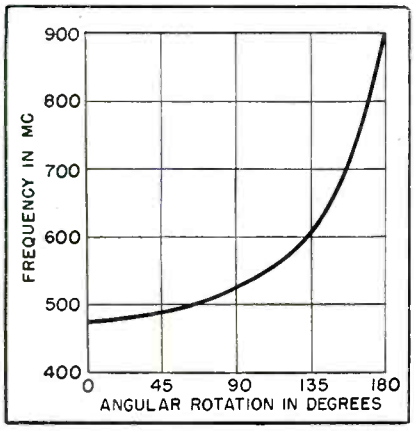


FIG. 6—Tuning characteristic. Compression of frequency scale at high end can be corrected by shaping tuner cylinders

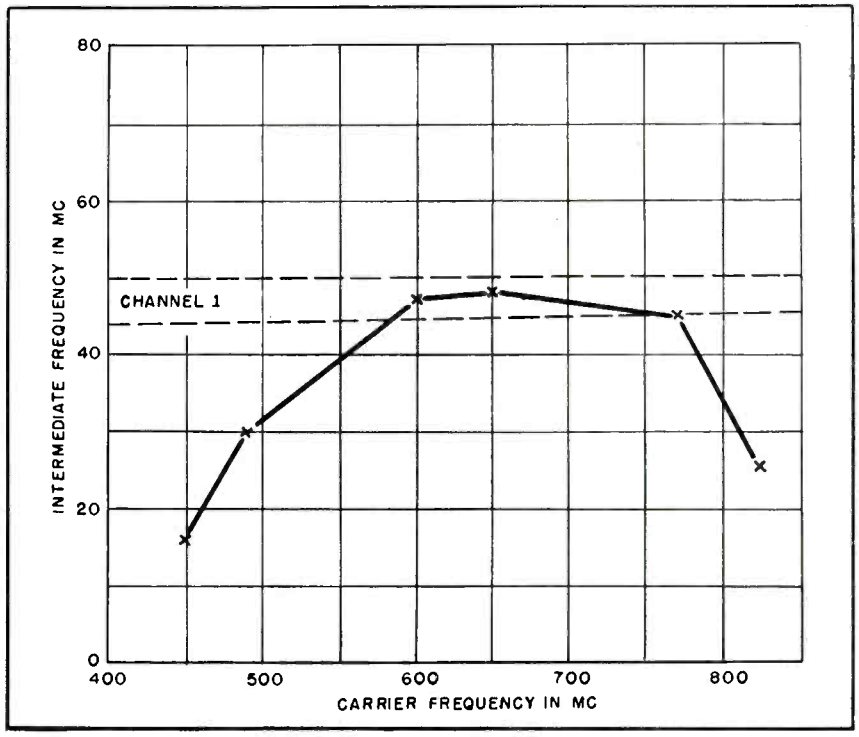


FIG. 7—Tracking characteristic, for feeding on channel 1 to existing receiver. Range from 580 to 780 mc is covered adequately, but end regions require correction

tuner was first described by Edward Karplus and a complete discussion of the theory and construction may be found in his paper[1]. It consists of two slotted coaxial cylinders, the inner one free to rotate, a housing and means of adjustment.

In the oscillator tuner, the plate and grid of the 6F4 tube are connected across the center of the slot in the outer cylinder with appropriate bypass condensers, and the cathode is returned to an intermediate point on this cylinder. When the two slots are aligned the *L* and *C* are minimum and the highest frequency is obtained. This frequency is determined primarily by the dimensions of the outer cylinder and the tube capacity. When the inner cylinder is rotated 180 deg. minimum frequency is obtained. This frequency, and consequently the range of the tuner, is largely determined by the spacing of the two cylinders. A greater frequency range requires closer spacing with the attendant problems in mechanical precision. Several adjusting screws are provided which permit slight deformation of the external cylinder to obtain the desired minimum frequency.

The preselector tuner is similar to the oscillator tuner except that there is no cutout for the tube. Similar adjusting screws are provided to permit tracking of this unit with the oscillator.

A primary advantage of this type of tuner is the complete absence of any sliding metallic contacts, thus eliminating this source of noise, attenuation and service problems.

The complete converter assembly is shown in Fig. 5. The two tuning elements are ganged with a flexible coupling and driven by the pulley arrangement shown. In addition, the preselector tuner contains a second inner cylinder about one-fourth inch long which is driven from the right hand end. This permits a front panel tracking adjustment. The chassis also contains a selenium rectifier power supply and the i-f tubes. A jack in the rear permits measurement or monitoring of the crystal current.

Tuner Characteristics

Significant characteristics of the tuner are shown in Fig. 6 through 10. Like every engineering problem, this one is never completed and these curves represent more or less transitory samples of the converter characteristics. Figure 6 shows the curve of frequency versus angular

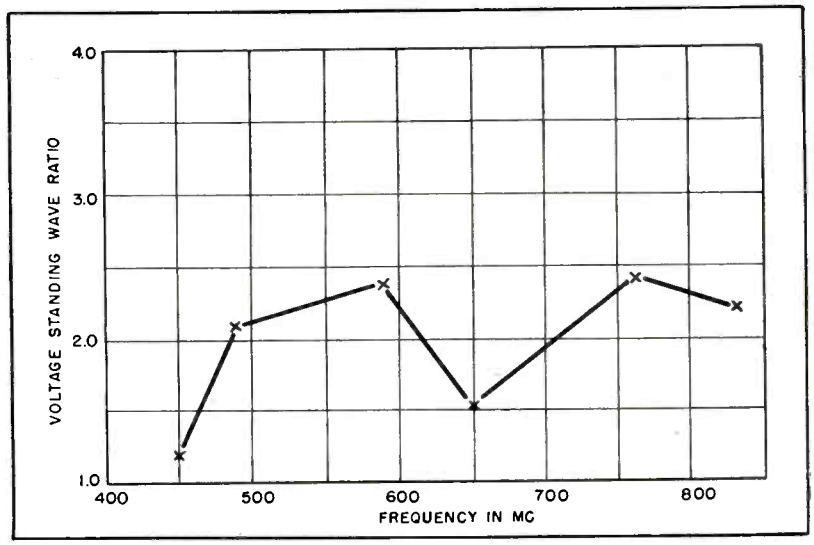


FIG. 8—The match to the 50-ohm input transmission line is excellent over the entire band

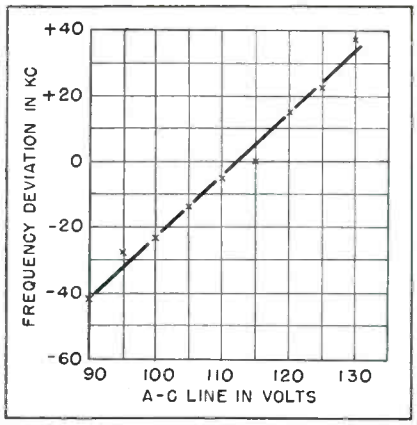


FIG. 9—Stability of oscillator frequency against line voltage changes. Deviation is less than 10 kc over 110-120 volt range

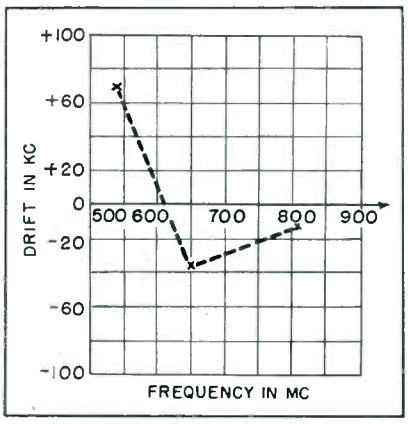


FIG. 10—Drift characteristic during warm-up period at various frequencies. Continuous tuning makes drift permissible

rotation of the rotor. As can be seen, the entire band is covered, but the compression at the high-frequency end is rather severe. Shaping of the rotors can alleviate this condition and work is now going forward toward producing a more nearly linear characteristic throughout the tuning range.

In Fig. 7, tracking is illustrated by plotting the beat frequency versus the incoming signal frequency. This characteristic was taken on a pre-production unit and shows good tracking between the limits of 580 mc and 780 mc. Again the low-frequency tracking can be improved by shaping the preselector rotor.

The standing wave ratio versus frequency at the converter input measured with fifty-ohm coaxial line for one particular unit is shown on Fig. 8. The mismatch ratio does not exceed 2.5 at any point within the band.

Figure 9 shows the oscillator frequency variation as a function of line voltage. Over the range from 100 to 130 volts, the oscillator variation is only ±40 kc. Abrupt changes of this magnitude are rare, so this variation is not considered serious.

Drift Characteristic

The oscillator drift problem is one of the most serious. Figure 10 shows the drift after a warmup period, as a function of frequency. A large amount of work has been done on this problem and a measure of success has been achieved. A positive coefficient applies over part of the band and a negative coefficient over another part. This particular characteristic was taken using silvered brass cylinders, but no frequency compensating device was employed. Experiments are continuing with other materials in the interest of minimizing this drift.

Finally, Fig. 11 illustrates comparative reception on vhf and uhf. The two test patterns shown here were taken at the same time at a location, within line-of-sight, about 14 airline miles from New York. The two transmitters were located at the same point atop the 515 Madison Avenue building. The picture at the right was received from WABD operating on channel 5 with an effective radiated power of 14,000 watts while that on the left was received from the uhf transmitter operating at 612 mc with an effective radiated power of about 40 watts. The vhf signal measured at the receiver terminals was 47,000 μv and the uhf signal was 450 μv. These pictures are not exceptional but were selected because neither showed an appreciable ghost. At approximately fifty random spot checks, the ghost problem was found to be less severe on the uhf band than on the vhf band.

Reference

(1) Edward Karplus, Wide-Range Tuned Circuits and Oscillators for High Frequencies, *Proc. IRE* 33, p 426, July 1945.

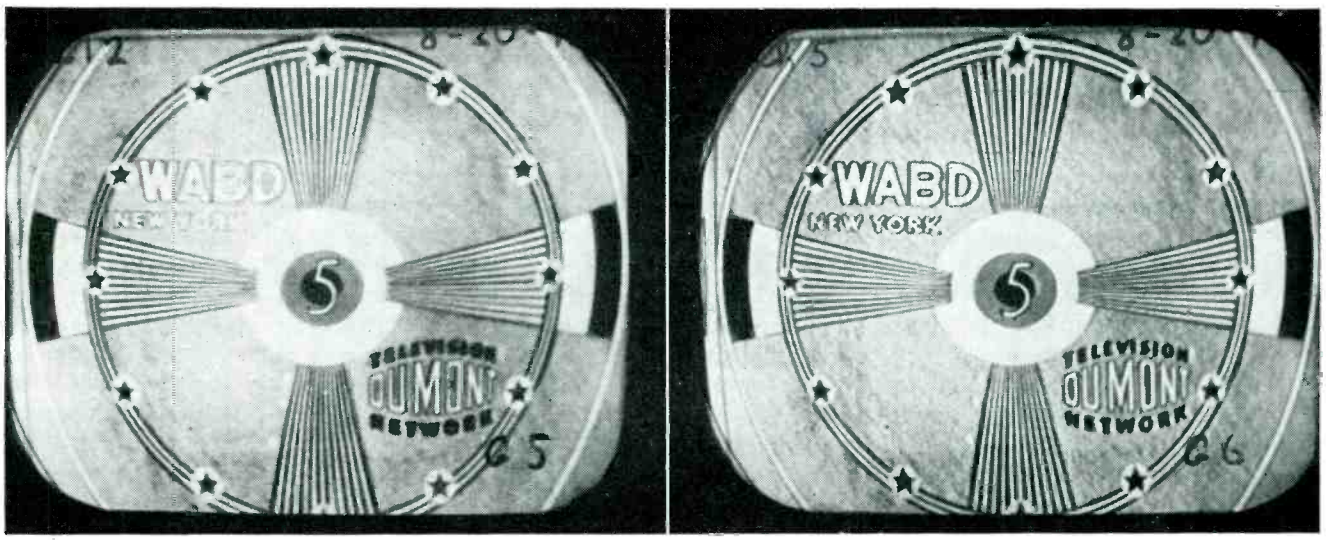
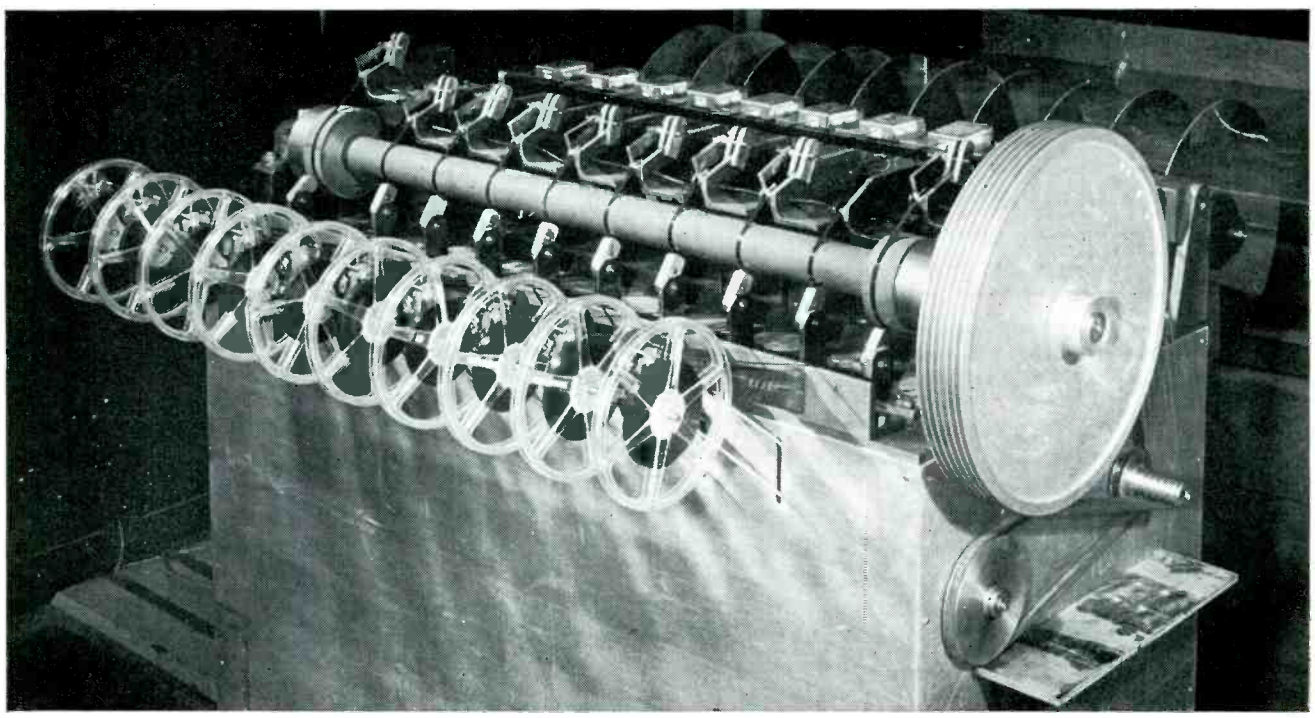


FIG. 11—Images photographed at 14 miles airline from DuMont transmitters. At left, 612 mc, 40 watts radiated power. At right, 77.25 mc at 14 kw radiated power

DUPLICATING



General view of multiple magnetic tape duplicating machine, with takeup reels for recorded tapes in foreground. Recording heads are on highest bar. Large pulley at right is on common capstan shaft

By REYNOLDS MARCHANT

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SINCE practically all magnetic tape recorders are also playback machines, the question has very naturally arisen about the possibility of supplying pre-recorded program material on tape. While the practicability of duplicating magnetic tape records in quantity was generally accepted, little was known about the economics involved. It was felt that a proper analysis could be made only through the construction and operation of a multiple duplicating machine which would be a production prototype and would permit a detailed study of the operations involved.

The main problem was found to be that of mass handling of tape, which has to be unwound from a stock roll, passed through the recorder and rewound onto a hub or reel for subsequent distribution. Direct labor accounts for most of the recording cost, even though little labor is required for the actual recording operation. Most of the operator's time is consumed in changing reels and threading the machines.

It was decided to drive a number of tapes side by side on a common capstan. Recording on these tapes is by individual recording heads, the recorded signal being supplied from a master tape driven by the same capstan. Elements of the machine are arranged to permit easy threading of the tape and quick exchange of reels on the windup spindles.

Over-All Design Details

The recording section of the capstan has basic operating speeds of 7½, 15 and 30 inches per second. The playback section of the capstan, which accommodates master tapes, is run at twice the speed of the recording section, because better dubbings are obtained from masters run at higher speeds than copies.

The tentative RMA standard for two-track recording provides that the two tracks shall be played in opposite directions. This is to permit playing a tape completely to one end on one track and playing back on the second track to the starting point, to avoid the necessity of rewinding and to permit essentially uninterrupted playing of the entire tape. Each tape recording channel of the duplicator is therefore provided with two heads which simultaneously record the two tracks, one being put on in reverse. Program material is provided from a special two-track master tape which is passed over playback heads displaced to either side of the tape center line.

The duplicator is designed so that satisfactory dubbings can be made from a master tape played either in the forward or reverse direction. Recording of the tape copies from reversed masters eliminates the necessity for rewinding, the copy tapes being ready for playing as they are removed from the machine. In simultaneous two-track dubbing, recording is started from the reverse end of the tape, so that the number-one recording track is made in the reverse direction and the tape is ready for immediate playback when removed from the machine.

TAPE RECORDINGS

Pilot-model duplicator places program material on eight reels of two-track tape simultaneously as prelude to mass duplication of tape records for home entertainment. Doubling supersonic-bias frequency permits recording at twice playback speed, lowering cost

The recording and playback amplifiers were designed to have a total harmonic distortion no greater than 1 percent at their maximum operating loads. The basic frequency response of these amplifiers was to be such as to provide essentially flat output from 30 to 15,000 cycles.

A common bias supply is used for all recording channels. Bias frequency is adjustable from 20,000 to 100,000 cycles and the output of the bias system is terminated in an adjustable-impedance network to match the characteristics of different recording heads.

The pilot machine has 8 duplicating channels and 2 playback channels for master tapes. This arrangement provides adequate accessibility to all parts of the machine and space for experimental machine modifications. The use of two master channels permits alternate use of separate master tapes so that either master can be rewound while the other is used for recording.

Capstan Design Details

The capstan is essentially a slow-speed element having an outside diameter of approximately 2 inches. The capstan surface is covered with a $\frac{1}{8}$-inch thick layer of rubber which is vulcanized in place. This rubber surface is ground to a concentricity of better than 0.0002 inch with the capstan bearings. Bearing surfaces are one-inch diameter sections turned on the ends of the capstan shaft. The bearing blocks are made of bronze and are relieved over most of their circumference so that bearing pressure is applied to the shaft at three narrow points spaced equally around the shaft. This prevents the capstan shaft from wandering, and spring loading of the bearing caps eliminates the possibility of binding of the shaft.

The playback capstans are rubber-coated sections fastened to each end of the recording capstan. Their surfaces are ground to concentricity with the recording capstan. A flywheel is mounted on one end of the capstan shaft to provide mechanical filtering. The fly wheel is rim-driven from the motor pulley by six round plastic belts which are made of special material having high elasticity and high internal friction. The belts are essentially endless and the belt diameter and number of belts was selected so that the internal belt friction provided approximately critical damping for the system.

The motor pulley size is selected to give a proper speed reduction to the capstan. From a basic motor speed of 900 rpm, the capstan speed must be reduced to approximately 75 rpm to provide a $7\frac{1}{2}$-inch-per-second basic recording capstan speed. The size of the motor pulley is changed to provide other basic capstan speeds.

Tape Traction and Tension

Positive tape traction at the capstan surface is obtained by use of individual pressure rollers which increase the friction pressure of the tape against the capstan. These rollers are mounted on a common lever which can be moved to disengage them from the capstan.

Uniform and adequate contact of the tape surface with the recording head must be maintained in order to produce uniform results. Since most record heads are cylindrical in shape, radial pressure of the tape against the head can usually be produced by maintaining the tape under tension. This tension must be maintained at a relatively uniform value and instantaneous variations should be particularly avoided to prevent frequency modulation of the recorded signal.

Proper tape tension is provided, in this case, by stationary pressure pads through which the tape moves. These pads are provided with felt faces to equalize the friction pressure and to provide a uniform friction surface. Weights are provided for use with these pads to change the tape tension.

A small amount of tape tension is supplied by a friction brake ap-

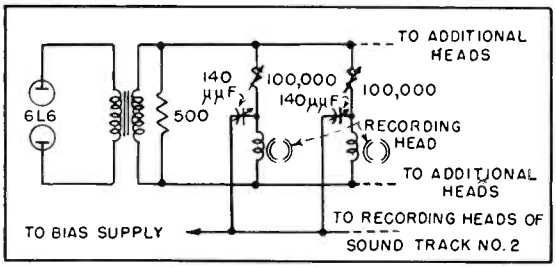


FIG. 1—Method of feeding signal and bias currents to each recording head

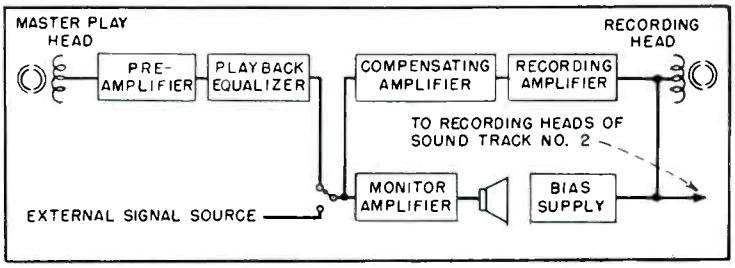
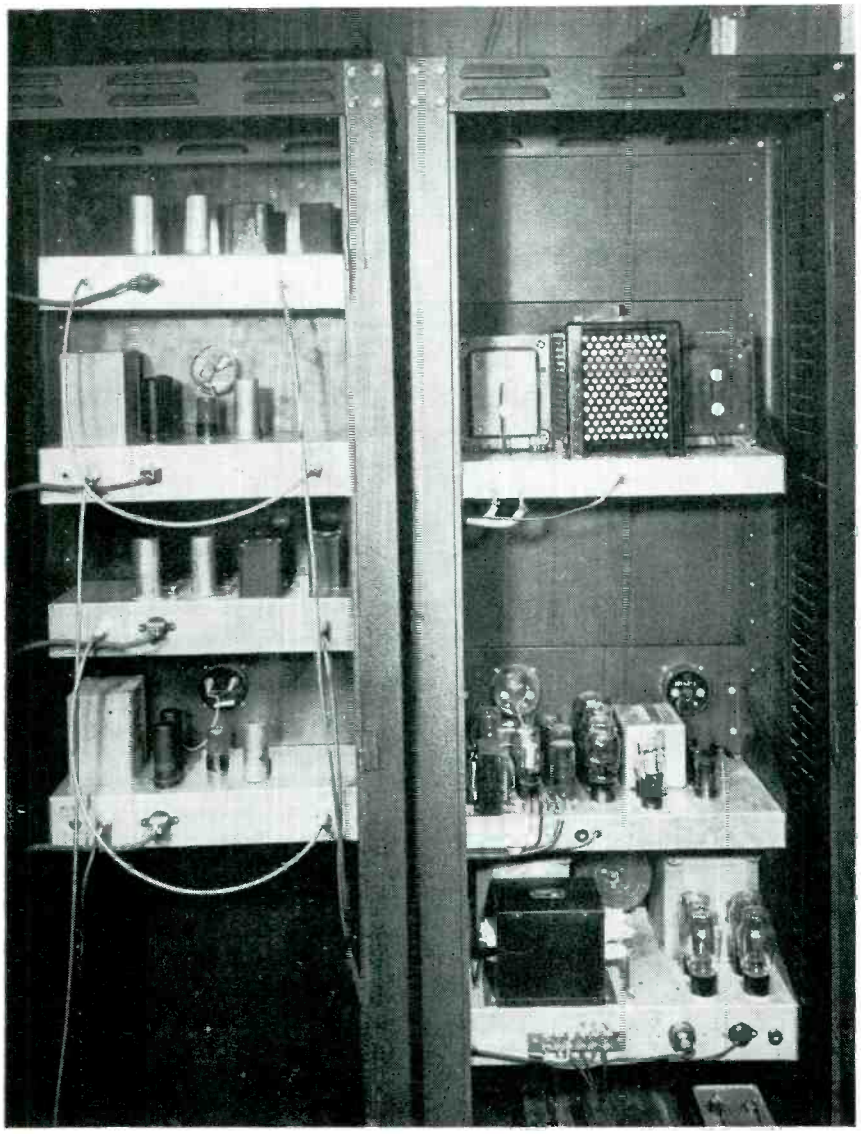
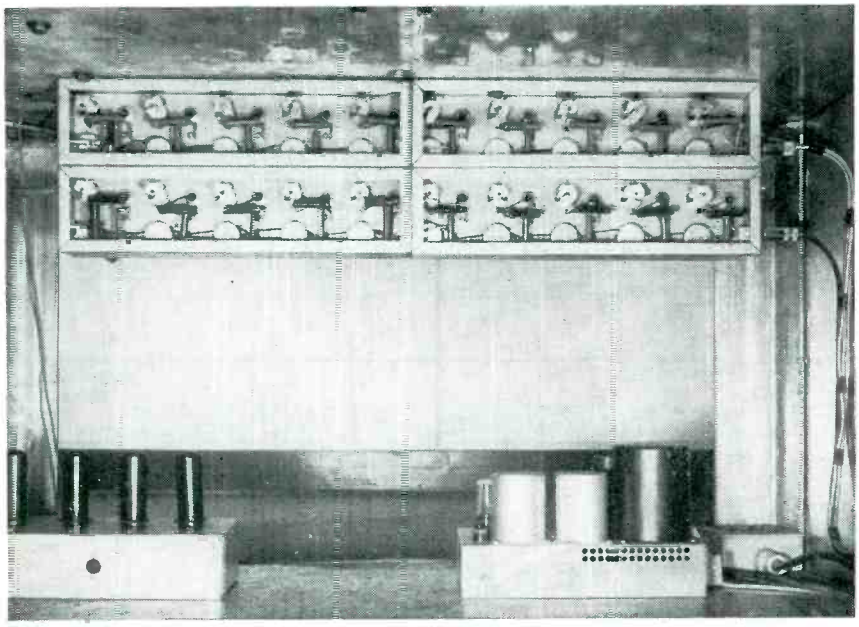


FIG. 2—Block diagram of playback and recording amplifiers, showing equalizer and compensating amplifier locations in system



Recording amplifiers and equalizers for tape duplicator are in left-hand rack, and regulated power supply is in rack at right



Interior of base of multiple recorder, showing high-frequency bias supply and individual networks for supplying bias and signal to recording heads

plied to the tape stock reel shaft. Since this friction is constant, the tape tension varies from the outside to the inside of a stock reel, but because this tension is a small portion of the total tape tension, its effect is negligible.

The stock roll shafts are designed to accommodate reels of tape up to 20 inches in diameter. Such reels would hold enough tape for a large number of recorded programs, thus eliminating the necessity for frequent threading of tape through the machine.

The windup spindles are designed to accommodate reels up to 15 inches in diameter. They are provided with automatic friction drives which can be preset to wind the tape at either constant torque or constant tension, or a compromise between the two. Constant torque winding is usually considered most desirable where the ratio of reel diameter to hub diameter is not excessive.

Recording Head Mounting

The recording heads are mounted on plates which are pivoted on the head assembly bracket. Adjusting screws permit the head gap position to be set so that the recorded signal on the tape is oriented exactly at right angles to the direction of tape travel. Proper orientation of the recorded signal on the tape is very necessary to the achievement of uniform playback characteristics on other magnetic recording equipment. Exact orientation of the record head is determined by comparison of a tape made on this head with a specially prepared head alignment tape when both are played on the same reproducing system.

Bias and Audio Feed

Previous experience with several individual recording machines operating in close proximity to each other indicated that troubles were often encountered from beat notes in the audio-frequency range. These beat notes resulted from small differences in frequency of the high-frequency oscillators. To avoid this problem, a common source of high-frequency bias was used for all recording channels on the duplicating machine.

The waveform of the bias current should be sinusoidal and should be relatively free from harmonics. The presence of even-order harmonics is particularly objectionable. This type of wave distortion tends to greatly increase the background noise of the tape and thus reduce the useful dynamic recording range. Adjustment of the bias frequency can be made over a frequency range of from 20,000 to 100,000 cycles and impedance-matching networks are provided to permit use of record heads having a wide range of impedances. Proper bias current is supplied to each recording head individually through an adjustable coupling capacitor. This permits adjustment of the bias to suit individual head characteristics.

Two amplifiers are provided for simultaneous two-track recording. Each amplifier feeds a group of recording heads to supply the proper signal to the separate tape tracks. Individual heads are connected to the source of audio signal through a constant-current network so that the current in the recording head is independent of frequency.

Figure 1 shows the network used to feed the bias current and the audio signal to a recording head, and Fig. 2 shows the amplifier and equalizer system. For simultaneous two-track recording, an identical amplifier and equalizer system is used to supply the audio signal to all of the heads in the No. 2 track position. A common bias oscillator provides the bias current for all record heads.

Preamplifier and Equalizer

The signal from a playback head on the master tape is fed to a special pre-amplifier having flat frequency response. The cathode heating current for the tubes in this amplifier is supplied from a d-c source. The plates are fed from an electronically regulated and filtered power supply having a ripple component less than 0.00001 percent. Tubes are selected for low microphonic and emission noise. The entire amplifier is mounted inside a heavy malleable-iron box which provides shielding.

When the value of audio signal current supplied to a recording head is kept constant regardless of the signal frequency, the recorded signal on the tape does not produce a uniform output when the tape is played on a standard playback head. Part of the reason for this is that the voltage developed by the playback head is proportional to the rate of change of the magnetic flux supplied by the tape. For a given remanent tape flux the output voltage from the head is, therefore, directly proportional to the frequency of the recorded signal. This relation would hold true throughout the entire audio-frequency range, were it not for the effect of other factors relating to the head gap length and to the wavelength of the recorded signal. These factors tend to reduce the output at higher frequencies. It is therefore necessary to equalize the signal from a recorded tape in order to produce a flat frequency output. To accomplish this, the signal from the tape is passed from the preamplifier through a special playback equalizer in which amplification is incorporated to compensate for the equalizer loss. A switch is provided to permit the characteristics of the equalizer to be changed as required by differing tape speeds.

Figure 3A shows the relative voltage output from a playback head at different tape speeds, when the signal on the tape has been recorded at these same speeds with constant current. Figure 3B shows the characteristics of the equalizer settings which are required to produce the uniform signal output of Fig. 3C at the different tape speeds.

Response Curves

The equalizer output signal should be a faithful replica of the signal originally impressed on the tape, and would normally pass directly to the recording amplifier for re-recording. It is often desirable, however, to alter the character of the original signal in order to compensate for some deficiencies in the original recording. It may also be desirable to pre-emphasize either the high or low frequencies as recorded on the tape in order to improve the signal-to-noise ratio or to match the playback characteristics of some special commercial recording equipment. For this reason, the signal from the playback equalizer is passed through a compensating equalizer before it enters the recording amplifier. This compensating equalizer is provided with controls which may be set to pass the signal without alteration, or which may permit boost or attenuation of the signal at either low or high frequencies. The frequency transmission characteristics of this equalizer are shown in Fig. 3D.

The recording amplifier is de-

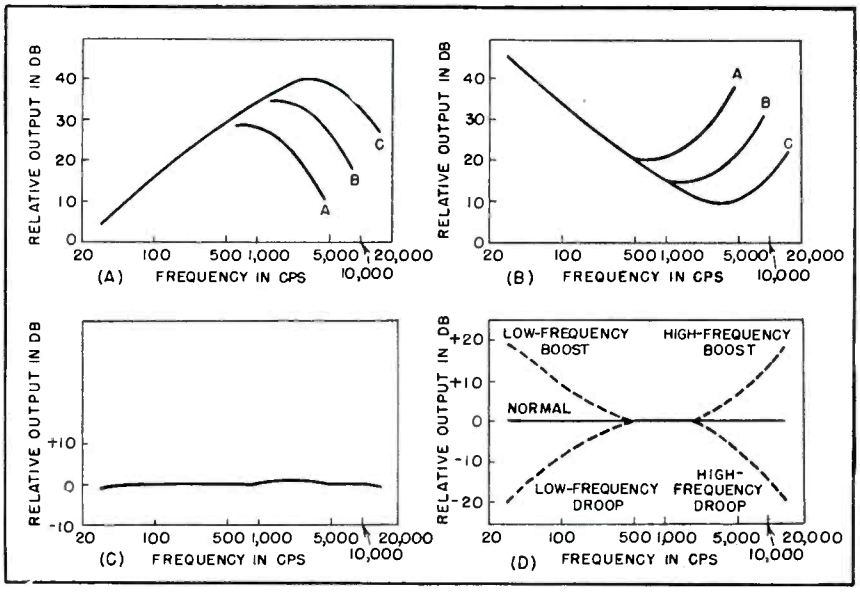


FIG. 3—Response curves of duplicator. (A) Playback characteristic with constant recording current and various tape speeds; (B) Equalizer amplifier frequency characteristics required for various tape speeds; (C) Equalized playback output for 15 feet per second; (D) Frequency characteristics of compensating amplifier

signed to supply adequate signal to eight heads in parallel. The current fed to each head is individually adjustable to accommodate individual variations in impedance and efficiency. Sufficient latitude is provided in this adjustment to permit use of heads having considerable differences in impedance.

The recorder section may also be fed from an external signal source so that master tapes, to supply a number of duplicating machines, can be made simultaneously on one machine. For two-track recording an identical system is used to supply the recording heads for the number-two tracks.

A monitor amplifier and loudspeaker are provided for listening as required. Since the installation of monitor heads in the recording channels would complicate the machine design considerably, it was felt that all monitoring of the dubbed copies should be done on separate playback equipment. A quality-control procedure based on selective sampling of the tapes from different recording channels would permit adequate inspection of the finished product.

The high-voltage supply for the amplifier tubes is obtained from a rectifier whose output is controlled by a combination of voltage and current-regulator tubes which limit the output voltage fluctuations from any source to less than 0.0001 percent. Regulation of the power supply to this unusual extent permitted an appreciable gain in signal-to-noise on the recorded tapes by eliminating random background noise resulting from rapid line-voltage fluctuations.

The high-voltage power supply, the equalizing networks and the recording amplifier are mounted in standard relay racks. The bias supply and the playback preamplifiers are mounted in the base of the recorder in order to keep the connections to the heads as short as possible. The lead wires to the heads are made of low-capacitance shielded cable to minimize attenuation of the high-frequency bias to the recording heads and to reduce the possibility of changing the resonant frequency of the playback heads.

A further gain in production efficiency can be achieved by operating the tapes at higher than normal playback speed during the recording process. This time multiplication can be successfully employed within a restricted range of speeds. For example, tapes to be played at a standard operating speed of 7.5 inches per second can be recorded without difficulty at 15 inches per second. In order to do this the master tape and the copy tapes must all be run at twice their normal speeds.

When the signal frequencies from the master tape are doubled by speed-up, the frequency of the supersonic bias current must also be doubled in order to maintain satisfactory frequency relationships. In the case of tapes normally played at 7.5 inches per second, a bias frequency of 35 kc may normally be used for a top audio-frequency range of 7,500 cycles. When the recording process is accelerated to twice normal speed, the top limit of audio frequency becomes 15,000 cycles and this requires a 70-kc bias frequency.

Individual mounting bracket for pair of recording heads that act simultaneously on two sides of a single tape to produce two tracks

Recording Speed Limitations

If the recording speed is increased by a factor of 3, the maximum audio frequency becomes 21.5 kc and the bias frequency must be 105 kc. Since most recording heads in use today lose efficiency at a rapid rate with bias frequencies greater than 70 kc, the practical limitation to increasing the recording speed is one of recording-head design.

If suitable heads can be made, it appears perfectly practical to speed up the recording process by a factor of four or five from a basic playing speed of 7.5 inches per second. Since the maximum recording speed is limited by a fixed maximum frequency response, the amount of speed increase is a function of the maximum audio frequency resulting from such increase. For example, tape masters made at 15 inches per second and having a maximum frequency response of 15,000 cycles would require a bias frequency of 60 to 70 kc. Copies of this tape for playing at 15 inches per second would be made at normal playing speed.

As contrasted with this, tapes made for a playing speed of 3.75 inches per second would have a maximum frequency response in the neighborhood of 4,500 cycles. Increasing the recording speed by a factor of 3 or 4 would result in a maximum audio frequency of 15 to 20 kc, and a bias frequency of 70 to 80 kc would permit satisfactory recording. From an economic standpoint, time multiplication is more advantageous for the lower tape speeds because the reduction in cost provided by the increased speed would parallel the cost reduction achieved by lowered tape cost.

Economic Aspects

There is a very practical economic limit to the speedup process in recording. Since the speedup process has very little effect on the cost of direct labor required by the recording process, the net effect of the speedup is to permit greater production from the machine, but not from the operator. Much greater gains can be made by reducing the direct labor involved in the recording operation. Such reduction can be accomplished through the use of automatic threading and reel changing devices which will minimize the machine shutdown time. The design of such a mechanism has been completed.

Production experience has indicated that the cost of recording can be held to a small proportion of the total tape record cost so that mass production of tape recordings is commercially practical.

Tunable A-F Amplifier

Variable-frequency circuit used as an oscillator from 200 to 10,000 cycles also serves as a selective amplifier in the same range. For code reception through interference, the device is switched to provide better rejection than a crystal filter

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RECENT DISCLOSURE of a simple phase-inverter connection for driving a half-lattice R-C filter of the all-pass type[1] greatly simplifies a variable-frequency circuit useful both as an audio oscillator and as a selective amplifier for rejecting or emphasizing a particular frequency.

This circuit has certain interesting advantages in comparison with the conventional bridged-T, parallel-T, and Wien-bridge methods of accomplishing an equivalent result. It makes practical, for example, an easily-constructed wide-range oscillator in which the magnitude of the feedback voltage is substantially independent of the operating frequency. Thus, it is possible to dispense with special limiting or variable-impedance devices for automatic amplitude control.

When the circuit is used as a rejection network, only one knob need be turned in order to find the null. Inexpensive ganged resistances may be used to change frequency, and frequency ratios of the order of 100 to 1 may readily be obtained without range switching. Finally, the circuit as an oscillator inherently provides a source of quadrature voltage suitable for obtaining a circular sweep on a cathode-ray tube.

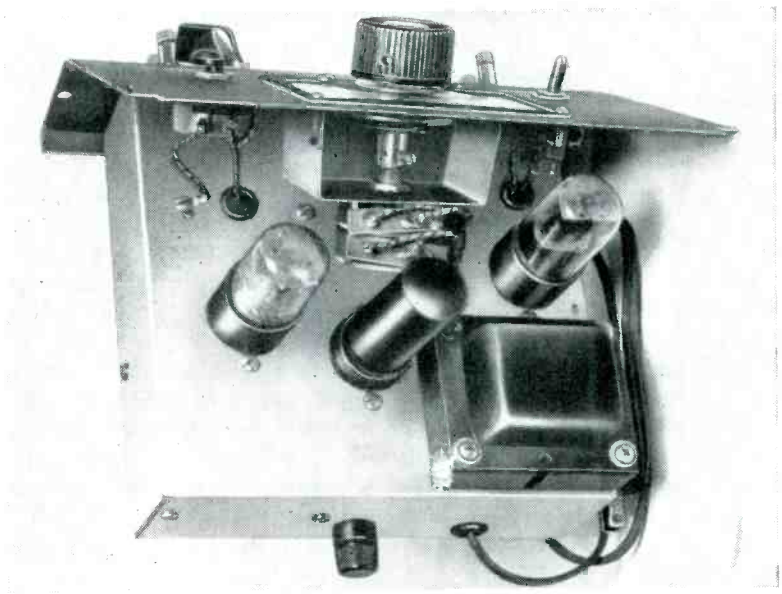
Method of Operation

A block diagram of one useful form of this circuit is shown in Fig. 1.

The all-pass-type filter delivers an output voltage whose magnitude is independent of frequency, but whose phase is determined by frequency. The variation of this phase with frequency (that is, the time constant of the network) is adjustable, and this adjustment also has no effect on the magnitude of the output voltage. In Fig. 1A a null will occur when the transmission through each of the parallel circuit branches is equal, and the phase shift through the network is 180 degrees. In Fig. 1B, oscillation occurs when the phase shift of the voltage fed back around the single-stage amplifier is 180 degrees. Consequently oscillations and the null will occur at the same frequency for a given setting of the network time constant.

It is convenient to do the phase shifting in this network in two sections. In Fig. 2 will be found the essential details of one section. Each may be viewed either as an R-C phase shifter of the familiar variety shown in many textbooks, (see Fig. 2A), or as one half of an R-C lattice filter of the all-pass phase-correcting type, as in Fig. 2B. The vector diagram of one section, which shows why the output voltage remains constant as either R, C, or frequency f is varied, is given in Fig. 2C. The phase shift of the output with respect to the input is 2 arctan $2fCR$. The network may be driven equally well by a vacuum-tube phase inverter, or by a transformer.

The special advantage of this particular half-lattice, when used as part of a null bridge or oscillator, is the fact that changing the phase shift by varying R cannot alter the phase-shifter output voltage and consequently affect the completeness of bridge balance or the magnitude of the oscillator feedback. If the corresponding full lattice were used (see the dashed lines in Figure 2B), both resistances would have to be varied in exact synchronism if changes in the magnitude of



Top chassis view showing parts layout. Ganged variable-resistor frequency control at center

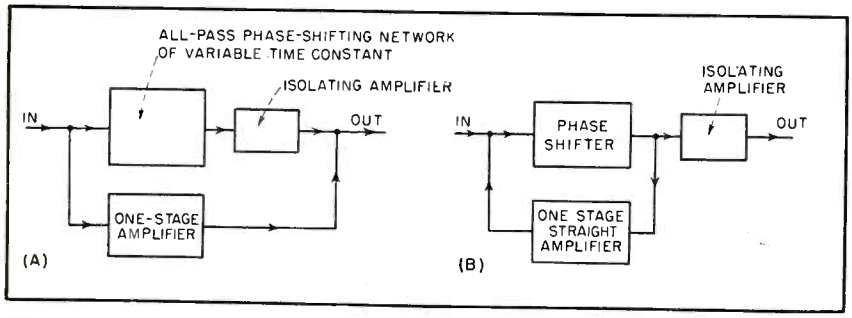


FIG. 1—Block diagram of basic rejection circuit (A) and basic oscillator circuit (B)

the output voltage were to be avoided.

Lattice-Filter Method

Another method of obtaining feedback voltage whose magnitude is independent of frequency or frequency-control setting, and also using an all-pass lattice filter, has been disclosed[2] but is considerably more complicated than the present arrangement because no loss in the all-pass network was permitted. In the present case, greater constructional simplicity is obtained at the expense of a certain amount of amplification.

With the conventional Wien-bridge circuit, two accurately-ganged capacitors or resistors must be varied to change frequency. If these elements are not in perfect track, the depth of the null will be proportionately reduced, and the feedback voltage will not be constant when the circuit is used as part of an oscillator. Similarly, parallel-T networks which must be varied over a wide frequency range require the accurate ganging of three circuit elements. It is usually necessary, with these circuits, to provide a fine balance control in addition to the coarse frequency control.

Constructional Details

A complete schematic of a typical oscillator-rejection filter device is found in Fig. 3, together with a vector diagram illustrating its operation in rejecting a particular signal. With two phase-shifter stages (V_1 and V_2) it is seen that the null is found when the phase shift through each stage is 90 degrees—that is, when the frequency is such that X_c equals R in Fig. 2C. It follows that the null frequency is inversely proportional to resistance. The same is true of the oscillation frequency.

The gain control P in the grid of V_1 allows adjustment of the depth of the null when the switch S is at the 2, or null, position. Once set for best rejection at one frequency, it is ordinarily not necessary to readjust this control when frequency is changed. When S is set in the 1, or oscillator position, this same gain control P adjusts the amount of feedback. When the feedback is set somewhat below the position at which oscillation occurs, the unit becomes a variable-frequency selective amplifier.

The sharpness of the passband may be controlled by adjusting the amount of feedback. When oscillations are desired, the gain control is set slightly above the threshold of oscillation. Under these conditions waveform will be good and output will not vary appreciably as frequency is changed. Too much feedback causes distortion; too little will make the oscillations unstable and likely to drop out with small residual changes in feedback as frequency is varied.

The only critical circuit components in Fig. 3 are the plate and cathode resistors of the phase inverters. These must be matched very accurately in pairs. The absolute magnitude, of course, is not important. Similarly, the two-to-one ratio between the corresponding resistors of the two tubes need only be approximate. Thus the matching may readily be done on an ohmmeter. For best long-time stability, precision resistors should be used.

It is desirable that the power supply be well-filtered and have a very low output impedance, in order to avoid coupling between the phase inverter stages. Where stability of operation must be maintained in spite of large line-voltage fluctuations, voltage regulation is desirable.

Dial Calibration

In a great many so-called resistance-tuned oscillators, capacitance is varied in order to change frequency. Owing to the effect of the minimum capacitance inherent in variable capacitors, the tuning

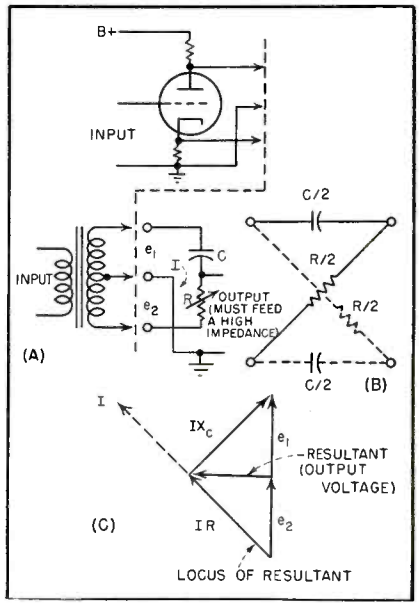


FIG. 2—Phase-shift circuit (A) that can be driven by transformer or vacuum tube; (B) all-pass lattice from which the simple phase-shifter is derived; (C) vector diagram

range obtainable is generally of the order of 10 to 1. By varying resistance in the present circuit, a wide tuning range may be covered in one rotation of the dial. If a straight line frequency-versus-resistance characteristic is desired, the phase-shifting capacitor in Fig. 2A can be replaced by an inductance. However an inverse frequency-versus-resistance calibration is quite practical in many applications. The dual-ganged resistance used in the unit of Fig. 3 is a readily-available Centralab type C-104 which has what is termed a standard audio taper. By taking advantage of this taper, the range from 200 to 10,000 cycles can be spread out reasonably well on a standard 180-degree vernier dial.

The chief limitation on the upper frequency limit which may be achieved by progressively reducing resistance, in addition to amplifier frequency response, is the loading effect of each R-C phase-shifting network on its associated phase inverter. This upsets the equality of the plate-to-ground and cathode-to-ground a-c voltages, and causes their relative phase to depart from exact phase opposition.

Sharpness of Rejection Band

It is desirable that a frequency-rejection device have as sharp a rejection notch as possible. The circuit described has a performance in this respect which is slightly superior to that of both a Wien and a parallel-T R-C bridge.

A curve of percent response versus frequency is shown in Fig. 4. The parallel-T response curve shown is that of a commonly used and relatively simple type[2] in which two of the resistors and two of the capacitors are identical and the other two elements are half or twice as large. A sharper rejection curve can be obtained by using a more complex relationship between these elements, but even when this is done the best of several typical cases[3] does not equal the performance of the phase shift bridge.

Discrimination of the phase-shift bridge may be improved by adding additional phase-shifting sections. With three instead of two, a second null, rather than a maximum of transmission, will occur as frequency approaches either zero or infinity, depending on circuit polarity. With the oscillator connection, there would accordingly be a tendency for simultaneous oscillation at two frequencies. However it is possible that the second oscillation might not prove too troublesome in view of the falling-off in amplifier response at the frequency involved.

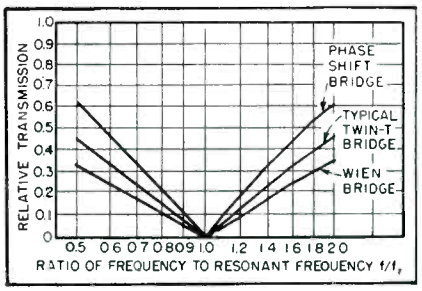


FIG. 4—Relative transmission as a function of frequency rejection

Applications

The ease with which this device may be constructed, recommends it for application wherever a simple general-purpose audio signal source, variable-frequency selective amplifier, and frequency-rejection filter would be useful.

By providing an output connection shown in Fig. 3 which samples a portion of the voltage at the junction between the two phase shifters, a quadrature voltage is available by means of which a variable-frequency circular sweep on an oscilloscope may be obtained. In this case, the accuracy of the 90-degree phase shift is a function of the accuracy with which the two variable resistors remain in step as the common shaft is rotated, and accordingly will not be very good unless precision resistors are used.

This unit is particularly suitable as an accessory for a communications receiver. In phone reception, the frequency-rejection feature may be used to eliminate interfering heterodyne whistles. The sharpness of the rejection slot is, if anything, superior to that of a good crystal filter. For code work, the operator has a choice: he may use the device to reject an interfering code station, leaving the desired signal little affected, or by throwing a switch he may use it as a variable-frequency selective amplifier to amplify one signal more than the others. The selectivity is continuously variable and may be adjusted to suit.

It is interesting, as this control is advanced, to hear a signal of one particular pitch rise up out of the others simultaneously present. Since the null frequency and frequency of regeneration are the same, it is possible to select and amplify a particular signal, and then by throwing the switch to make it disappear leaving all the others behind.

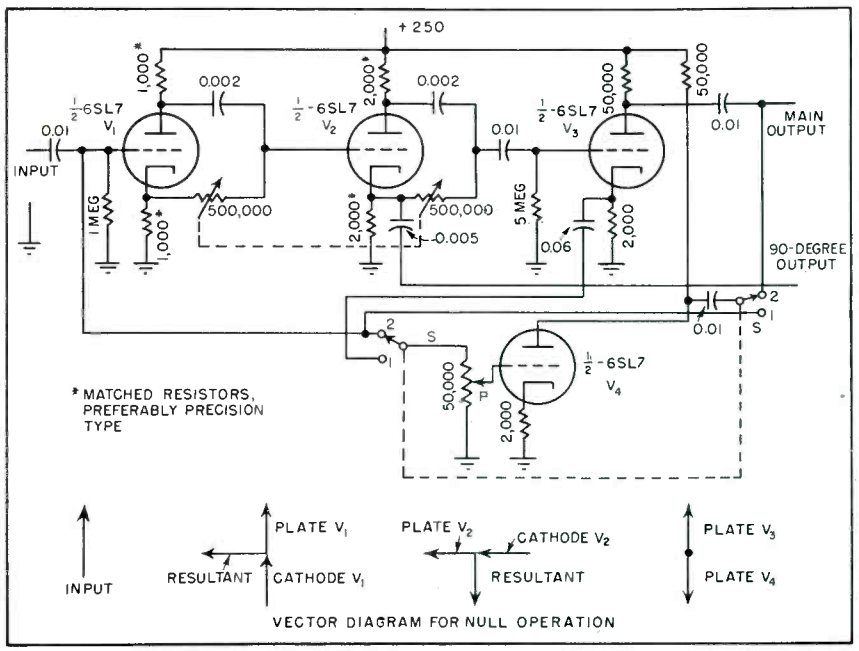


FIG. 3—Schematic circuit diagram and vector diagram for null operation

Acknowledgment

The author is indebted to his colleague, F. W. Clelland, for the suggestion that this oscillator may be used as a source of quadrature voltages. This work is an outgrowth of research for the Watson Laboratories, Air Materiel Command, under Contract W28-099-Ac-131.

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METAL DETECTOR

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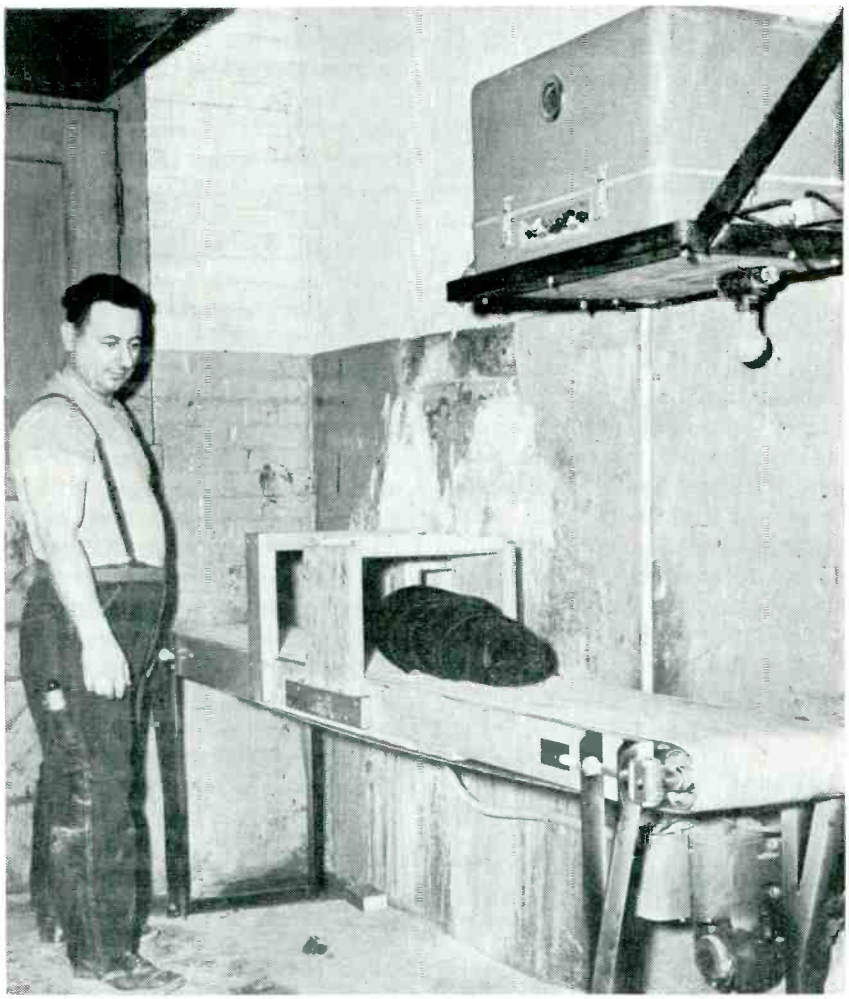
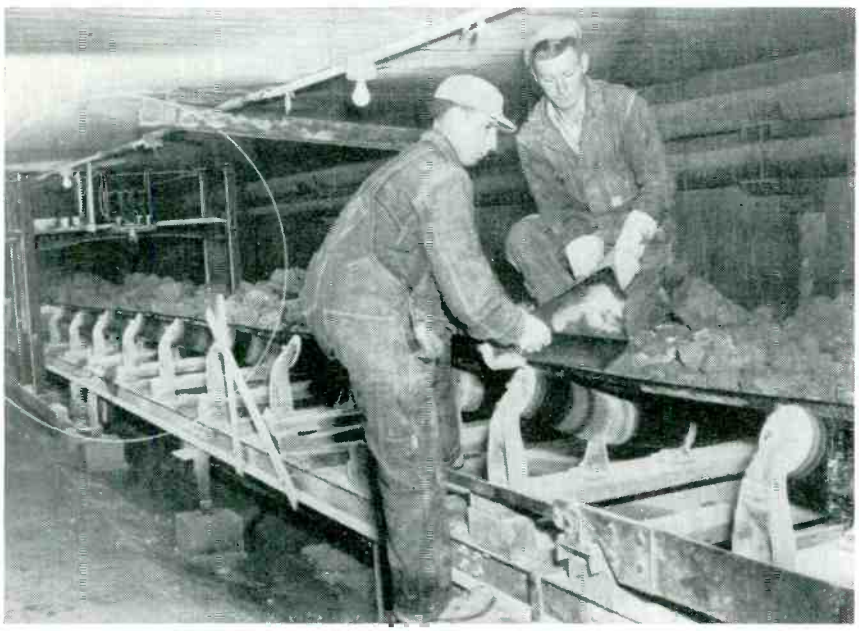


Operator runs bolt of rubber through metal detector coil, shown over conveyor belt housed in wood baffle for protection. Metal detector unit may be seen on shelf at upper right corner of picture



Workmen remove a manganese steel (nonmagnetic) shovel tooth from a conveyor belt loaded with limestone. Inspection coil and marker device are encircled in background. Marker dumps cup of white chalk on conveyor when metal is detected

INDUSTRY is continually confronted with the problem of finding metal (nonmagnetic as well as ferromagnetic) in process media before serious damage is done to machinery, plant, product, or—in the case of foods and drugs—before it reaches the consumer. The metal detector described in this paper should find extensive application in the textile, rubber, plastics, lumbering, paper, mining, milling, sugar, grain and drug industries.

Metal detectors generally work on the distortion of a radio- frequency or audio-frequency field. The Army Engineers have mine detectors utilizing these principles that do the job for which they were designed very well, but in general they are not sufficiently sensitive, stable or versatile to find many industrial applications. The metal detector described is the result of an independent development specifically for industrial application to a wide variety of problems.

Principles of Operation

The operation of the instrument is based on the momentary distortion of the r-f field when a metallic particle passes through or near the tank coil of a stable oscillator. This distortion may result in an increase or a decrease in the efficiency or Q of the tank and will, therefore, be reflected back into the plate circuit as a change in the resistive component, giving rise to a change in voltage magnitude. If this change is in the negative direction, and of sufficient steepness and amplitude, an alarm signal results.

Most common materials cause a decrease in the Q due to the increased losses. These losses are apparently of three characters: eddy

for CONVEYORS

Metallic particles passing through or near the tank coil of a stable oscillator cause a change in the output of the oscillator due to eddy current, hysteresis and dielectric-loss changes. Change in output is detected, amplified and used to actuate alarm and marker circuits

current, hysteresis and dielectric. The magnitudes of the losses depend, in general, on the surface, shape, mass, resistivity, and permeability of the material and the frequency and concentration of the electromagnetic field. Since two classes of material, the product to be inspected and the tramp metal to be detected, are involved in the metal detector problem and since the designer has no control over the physical characteristics of either, his aim is to choose an operating frequency and coil design that will emphasize the losses due to the tramp metal and minimize those due to the product.

The depth of the penetration δ of an electromagnetic field in a conductor, limited by skin effect, is given by:

$$\delta\ (\text{cm}) = \sqrt{\frac{\rho \times 10^2}{\mu\mu_0\pi f}} \quad \text{or}$$

$$\delta'\ (\text{mils}) = 1.99\sqrt{\frac{\rho}{\mu f}} \qquad (1)$$

where δ is the depth at which the current is reduced to 37 percent of the surface value, ρ is the resistivity in ohms per cm cube, $\mu_0 = 4\pi \times 10^{-7}$, μ is the permeability, and f the frequency in cycles. For copper δ' is 6, 12 and 26 mils at frequencies of 200, 50, and 10 kc respectively. For iron of assumed permeability 200, δ' at 50 kc is only 2 mils. Thus it is the surface area of a conducting sheet or particle that usually influences or is influenced by the r-f field.

Eddy-current losses in an object of volume V cubic meters are, neglecting skin effect[1]:

$$W_e' = \frac{\pi^2 f^2 t^2 B_{\max}^2 V}{6\rho} \qquad (2)$$

where $W\acute{e}$ is in watts, t is the thickness of the object in meters, B is in webers per square meter, and ρ is in ohms per cm cube. Since B may be written as $\mu\mu_0 H$, it is seen that the eddy-current losses are proportional to the square of the frequency and permeability, and inversely proportional to the resistivity. If we take into account the redistribution of induced current due to skin effect, the equation for the eddy-current loss becomes:

$$W_e = \frac{fB_{\max}^2 V}{12\mu}\left(\frac{t}{2\times 10^{-2}\delta}\right)^2 \left[1 - \frac{6}{945}\left(\frac{t}{2\times 10^{-2}\delta}\right)^4 \cdots\cdots\right] \qquad (3)$$

or

$$W_e = W'_e \left[1 - \frac{6}{945}\left(\frac{t}{2\times 10^{-2}\delta}\right)^4 \cdots\cdots\right] \qquad (4)$$

If we assume a sheet of copper 1 millimeter thick and a frequency of 50 kc, the term in the brackets amounts to 5 percent. Considering the material characteristics and field as fixed, we may write Eq. 3 in terms of frequency.

$$W_e = K_1 f^2 (1 - K_2 f^2) \qquad (5)$$

and

$$f_c = \frac{1}{\sqrt{2K_2}} \qquad (6)$$

Equation 5 shows that at or beyond a critical frequency f_c there will be no appreciable eddy-current losses. Since K_2 is a function of the material, calculations based on the above formulas are useful in selecting a frequency that will give maximum discrimination between two media.

Hysteresis losses, appreciable only for ferromagnetic materials, are due to a tendency to oppose a change in magnetic state. These losses may be expressed in the form:

$$W_h' = \alpha f B_{\max}^n V \qquad (7)$$

where the values of α and n depend on the material. Note the hysteresis losses vary linearly with frequency if we neglect the skin effect. Actually with magnetic materials the skin effect is far from negligible. Qualitatively, the depth of penetration may be considered as limiting the value of $B_{\max}^n$ over a portion of the volume, and thus reducing the loss W_h' to some value W_h. The quantitative expression is somewhat difficult to handle and experimental comparison of the amount of signal (loss) produced by steel and copper spheres of equal diameters at various frequencies seem to substantiate the equations,

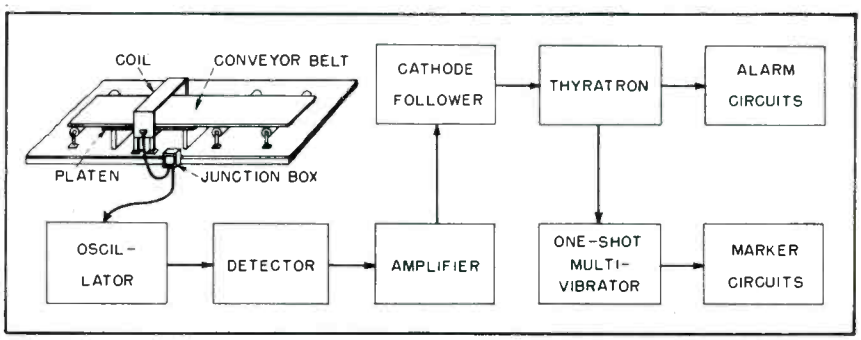


FIG. 1—Block diagram of metal detector. Lines up to 40 feet long have been used successfully between inspection coil and oscillator

and are a great deal simpler to handle.

The third type of loss mentioned is that found in dielectric materials as contrasted to conductors. The loss in a dielectric is generally expressed in terms of frequency, capacitance and power factor of an ideal capacitor whose only losses are in the dielectric. This type of loss is noticed in metal detector applications where the product being inspected momentarily occupies a large portion of the volume of the coil, and the resistivity is high. The losses are directly proportional to frequency, since there is no radical change in power factor over the range of frequencies utilized. This must also be considered in selecting the inspection frequency.

Circuits

Figure 1 is a block diagram of the Eriez metal detector, the circuitry of which is shown in Fig. 2. The material to be inspected is passed through or near the coil which, together with a fixed capacitor, forms the tank circuit of the 6J5 oscillator. The operating frequency, between 10 and 200 kc, is selected as previously outlined, and the tank circuit is designed to match the plate impedance of the tube at this frequency. A decrease in tank efficiency or Q, such as might be caused by a piece of tramp metal, causes a momentary decrease in the magnitude of the generated voltage.

Half of V_2 is used as a rectifier, conducting on the negative portion of the oscillator cycle and charging C_1 and C_2 negatively to approximately the peak oscillator voltage. Under steady-state conditions no signal will be applied to the first amplifier grid unless the magnitude of the generated voltage is suddenly changed. A decrease in oscillator voltage will allow C_2 to discharge to a new and less negative value, thus applying a positive signal to the amplifier grid.

The two-stage amplifier is capacitance coupled, having an overall voltage gain of approximately 60 db, with the half-power points at ¼ cycle and 40 cycles. The upper frequency could easily be raised, but is kept low to reduce the noise level. The low-frequency response is more difficult to improve, and imposes some limitations on the application of the device. Inspection must be accomplished at sufficiently high speed so that the fundamental frequency of a pulse generated by a small metal object will be amplified at near maximum gain to secure the utmost in sensitivity. The long time constants necessary to attain the low-frequency response also result in a long recovery time after a large signal. With the present circuit values a large signal may upset the circuit for as long as 8 seconds, during which time a small signal might be lost. This time must be considered in certain types of installations.

The output of the amplifier, in the form of a positive pulse, is capacitively coupled to the grid of a biased cathode follower. The bias voltage is obtained by a voltage-doubler circuit across the filament supply. The output of the cathode follower is directly coupled to the control grid of a type 2050 thyratron, and the grid level established by adjusting the cathode-follower bias. A positive pulse applied to the cathode follower will lower the thyratron grid and allow it to fire. When the thyratron fires, relay RE_1 is energized. Holding contacts keep RE_1 energized until the circuit is broken by pressing a reset button, while V_5 is extinguished very quickly when its plate voltage drops almost to zero as current is supplied through the one-megohm resistor, R_1. The alarm relay, RE_1, may be used to actuate controls for shutting down a conveyor, blowing a horn, or turning on any type of alarm.

When the thyratron fires, a negative pulse is applied to the grid of the conducting side of a one-shot multivibrator. This flips the circuit, de-energizing the marker relay, RE_2, for the duration of a delay time determined by R_2 and C_3. This delay time, variable from about 0.1 to 2 seconds is intended to facilitate adjustment of control and marking devices. When the marker circuits are used for controlling automatic reject mechanisms, an external time-delay relay may often be necessary. Since both the thyratron and the multivibrator are quickly restored to normal after an alarm signal, a subsequent signal or signals will actuate the marker relay even though the alarm relay has not

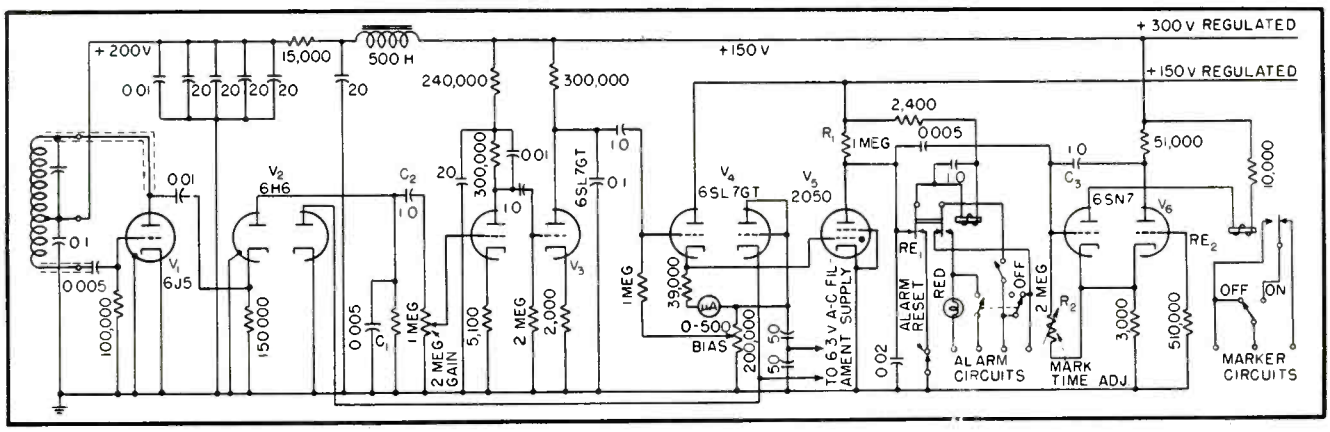


FIG. 2—Schematic diagram of metal detector minus power supply. Extremely well-regulated d-c voltages are necessary because of the high degree of circuit stability required

been reset. The installation shown in one of the photographs makes use of this feature. The first signal shuts down the conveyor and trips the first marker (the device above the coil). Should a second or third or fourth alarm signal be received while the belt is coasting to a stop the respective markers would be operated indicating the locations on the belt of the additional contamination.

The power-supply circuits are fairly conventional. Input power is applied through a constant-voltage transformer of ½-percent regulation and about 0.1-second response time. The output of the full-wave rectifier is applied through a capacitor-input filter to a degenerative voltage regulator. Two sets of VR tubes act as voltage dividers (and decoupling networks) to split the regulated voltage into four channels. The response of the overall regulated power supply is sufficient to nullify the effect of normal line variations, but is still not capable of entirely eliminating the transients caused by such inductive loads as small motors, relays and fluorescent lights. A power source (125 watts) free from these transients is therefore required if the unit is to be operated at maximum sensitivity and without false alarms.

Installation and Maintenance

Coils are designed for each specific application, and may range in size from 1 in. by 1 in. to 4 ft by 6 ft, with maximum sensitivities of $\frac{3}{32}$ to 2-inch diameter steel balls, respectively. An intermediate coil, such as pictured in the rubber bolt inspector, has an optimum sensitivity of 0.187 inch, while the large coil over the limestone conveyor has a maximum sensitivity of 1 inch. Because of an orientation effect (the most unfavorable condition for a long thin object is perpendicular to the axis of the coil) sensitivities are conservatively referred to in terms of diameters of steel, brass or aluminum spheres. How near to the maximum sensitivity a given installation may be operated is usually governed by the mechanical details of the installation and the product to be inspected.

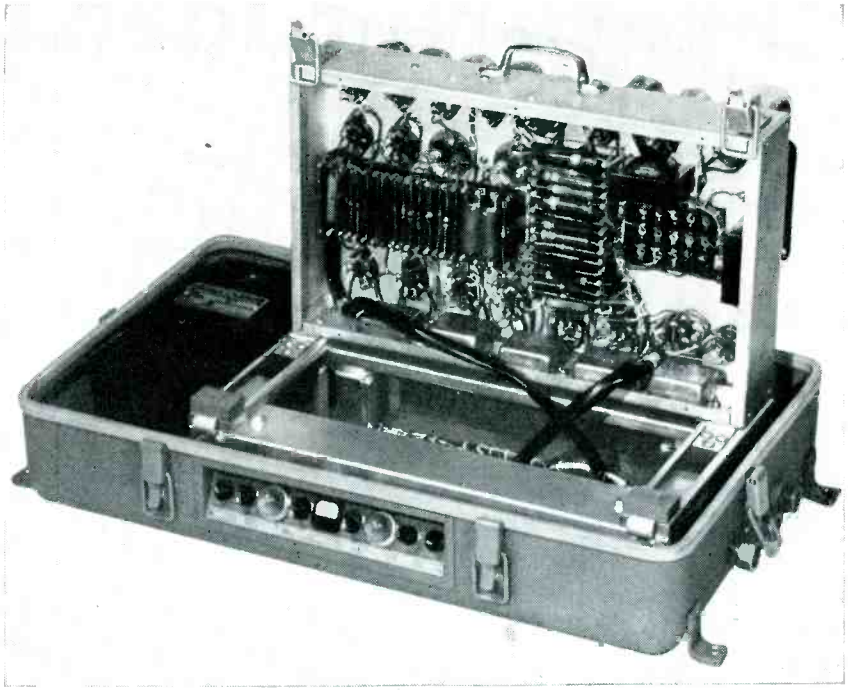


FIG. 3—Metal detector chassis shown in position for servicing

The frequency response characteristic of the amplifier requires an alarm pulse having a fundamental frequency greater than ¼ cycle for maximum sensitivity. To obtain such a pulse from a small object requires a minimum inspection speed of approximately 20 feet per minute for a 2-inch aperture and 120 feet per minute for a 12-inch aperture. For most applications this is no problem, as it is within the normal operating range of conveyors and chutes.

Stationary metal objects near the coil reduce the overall efficiency but do not cause an alarm. Moving metal must be shielded or kept two to six times the coil dimensions away from the coil, depending on the size and symmetry of the object. A moving loop circuit or an intermittent shorted turn if oriented so as to loop a portion of the electromagnetic field is capable of causing false alarms. These factors must be considered in selecting an installation area and in designing or altering materials-handling equipment for use in conjunction with the Eriez metal detector.

The metal detector chassis is shock-mounted in a gasket-sealed aluminum case, permitting installation in exposed locations. The inspection coil is connected to the detector by up to forty feet of conduit, coaxial cable being used for the plate and grid circuits. This makes the installation very flexible in that a minimum of space is required in the inspection zone, and the control equipment can be located in any convenient place.

The tilting-chassis type construction makes the components and tube sockets readily accessible for voltage checking and servicing. Actual installations are made simply by connections to terminal blocks.

The only maintenance required is an occasional sensitivity check with a standard test specimen, and the normal periodic check of the tubes.

Acknowledgment

The author wishes to acknowledge with thanks the assistance and contributions of E. A. Gilbert and B. F. Snively, both of the Radio Frequency Laboratories, Inc., to the success of this development. The cooperation of the Eriez Manufacturing Company, which markets the Metal Detector, in supplying photographs is greatly appreciated.

Reference

(1) E. E. Staff, MIT, "Magnetic Circuits and Transformers," John Wiley and Sons, Inc., Ch. V, 1943.

Picture Storage Tube

Combination kinescope and iconoscope in one glass envelope consists of two cathode-ray guns bombarding a special target plate. One gun writes the pattern on the target and the other scans it to generate signals and erase the picture

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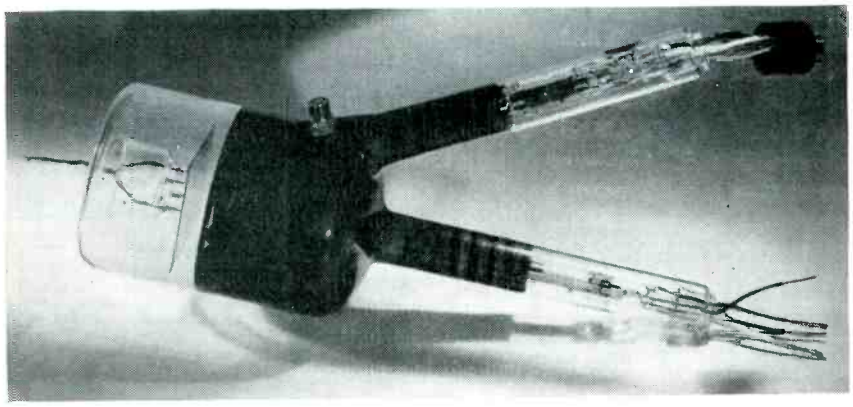


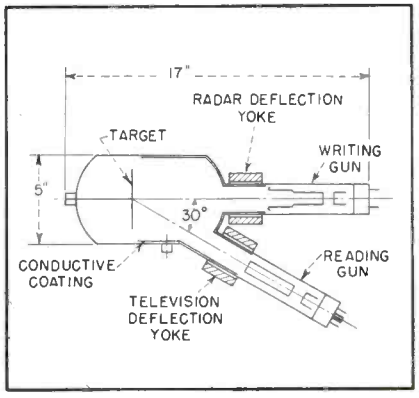
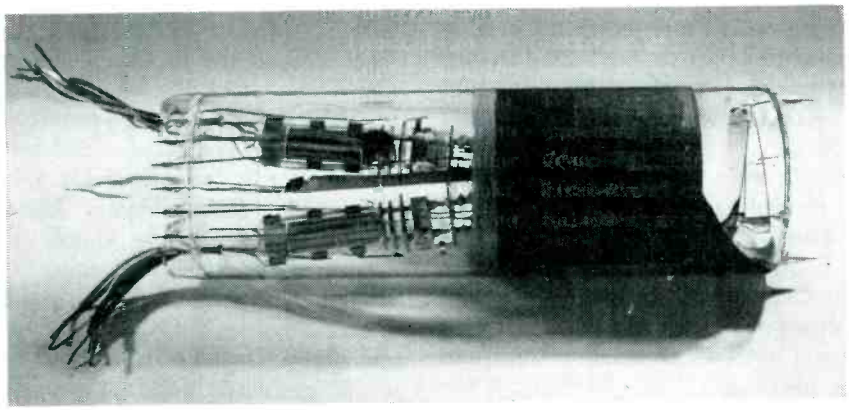


FIG. 1—Magnetic-deflection type of graphechon



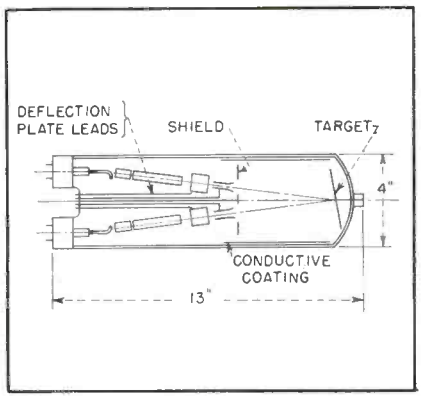
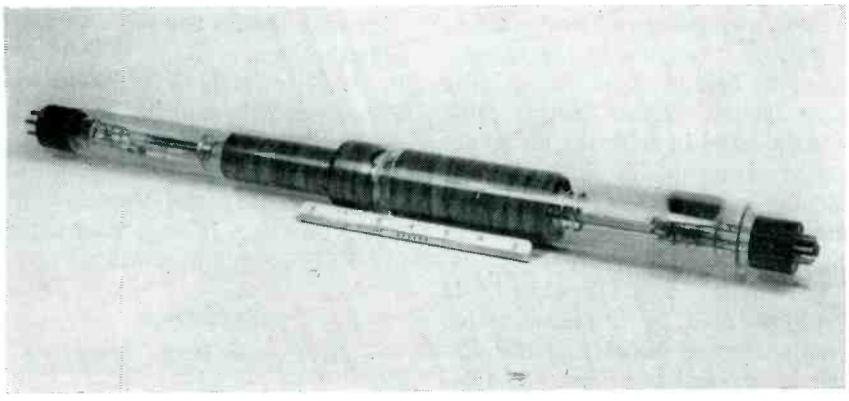


FIG. 2—Electrostatic type of graphechon



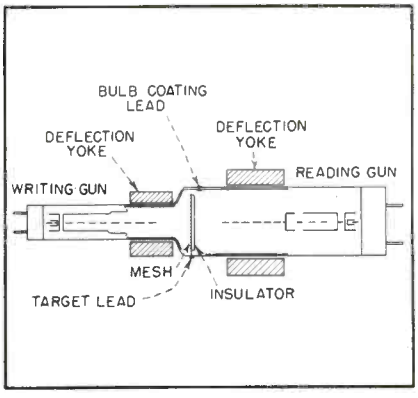


FIG. 3—Double-ended type of construction

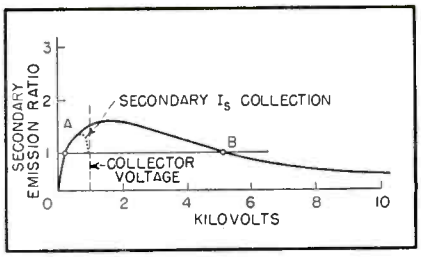


FIG. 4—Typical curve for secondary emission from silica

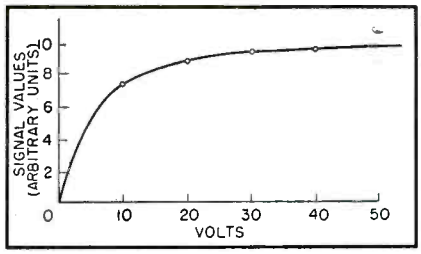


FIG. 5—Surface potential in volts below collector potential

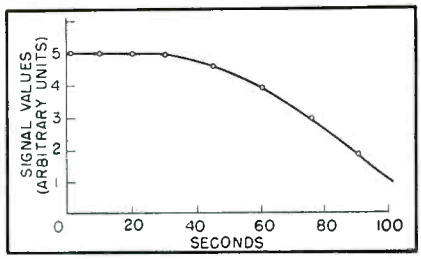


FIG. 6—Typical signal output against viewing time

THE PROBLEM of providing a means for electrically storing complete radar ppi-type patterns and generating from them signals which could provide television pictures of the radar patterns arose in the Teleran system[1] for airborne navigation.

It was highly desirable to be able to broadcast a composite television picture of a radar pattern, its associated ground map and other information. The tube that was developed to meet this need proved to have several other interesting applications.

A means of converting radar signals to television signals without loss of the pattern geometry was needed. This implies storage of the radar signals for at least several seconds because it can take this long to complete one ppi pattern. Also, because television pictures are generated at the rate of thirty per second, it may be necessary to generate several hundred television copies of a radar pattern before it fades out. Such conversion of signals has been obtained with a special high-capacity orthicon[2] picking up the initial flash of a cathode-ray tube without any afterglow, the picture being retained in the capacity of the orthicon photocathode.

To obtain an all-electronic converting scheme, a new type of tube called a graphechon was built. This name is derived from the Greek words graphe (to write) and echo (to keep or to hold). The tube can be regarded as a kinescope and iconoscope in one bulb with the mosaic and kinescope screen replaced by a charge-sensitive high-capacity storage target. The kinescope gun will be referred to as the writing gun which takes the radar signal and writes it on the target. The other gun will be called a reading gun. Its function is to generate the television signal and gradually remove the stored signals.

Construction of Tube

The design of the bulb is determined by the requirements of the cathode-ray guns. Figure 1 shows a sketch and photograph of one type of tube using magnetic deflection. To simplify the circuit requirements, the writing gun is mounted perpendicular to the target, which avoids keystone correction for a radial deflection pattern. This correction has been solved very simply for the iconoscope, and so the reading gun is mounted off the axis at the same angle as is used for the standard iconoscope.

When preferable, a tube can be built with all-electrostatic focus and deflection. It is more suitable for oscilloscope operation or, where weight and size are critical, it permits eliminating the deflection yokes. Figure 2 shows such a tube which can be made smaller and more compact than the magnetic deflection type, but is necessarily subject to the lower resolution limits imposed by the electrostatic deflection system.

Figure 3 illustrates the most recent form of the tube. This modification was built to make possible mounting the guns on a common axis and thereby avoid the need for keystone correction. The target construction was modified to permit the writing beam to penetrate through the target.

For the magnetic deflection writing gun it is possible to use a standard kinescope gun with either magnetic focus (type 12DP7) or electrostatic focus (type 12AP4). Both types have been used for radar purposes and have adequate resolution at the rated voltages of 6,000 to 10,000 volts, which is also the range of voltage used in the graphechon. The reading gun can be a standard iconoscope gun and runs at standard iconoscope voltages, 800 to 1,000 volts.

The target consists of a plate of metal upon which is deposited a film of insulating material of the order of 6,000 Angstroms thick (approximately half a micron). Where the two guns are on the same side, any of a number of metals thick enough to be self supporting can be used for the target. The insulator film can be any good insulator like silica or magnesium fluoride, applied by any suitable means, such as evaporation.

In tubes where the guns are on opposite sides of the target, it is necessary to make the metal backing transparent to electrons and yet strong enough to support the insulating layer. This can be done by using very fine mesh with a high transmission factor to provide the mechanical support. Then an organic film is spread over the mesh to act as a base upon which to evaporate a thin layer of aluminum. The insulating layer is evaporated onto the aluminum to complete the target. The high-voltage writing gun is located on the mesh side of the target. The mesh is made fine enough so that it does not limit the resolving power of the tube. Sample targets have employed approximately 500-per-inch mesh.

The reading beam, operating at

1,000 volts, has a secondary emission ratio greater than unity. It scans uniformly over the insulator surface and therefore brings it approximately to the potential of the collector, which is the conductive wall coating. This is true regardless of the potential of the underlying metal. It is therefore possible to adjust the potential drop across the thickness of the insulating film to approximately the difference in potential between the target metal and the wall coating.

It is possible to regard the insulator as the dielectric in a capacitor, one of whose plates is the target metal and the other is the surface scanned by the electron beam. As a starting equilibrium condition, the capacitor is charged uniformly over its area. Because the one plate is the insulating surface of the dielectric and does not conduct transversely, it is possible to discharge any part of the capacitor without affecting the rest of it. Such discharging can occur in any arbitrary pattern.

The mechanism for discharging the dielectric is a newly discovered phenomenon[3] which can be observed in films thin enough to be completely penetrated by an electron beam. It can be shown that currents can flow through the film which are many times larger than the bombarding beam, that the currents flow in the direction of the gradient, and that the insulation recovers on removal of the beam.

Since the penetration of an electron beam increases with the square of the voltage, a film may be chosen of such thickness that, though fully penetrated by a 10,000-volt beam, it is scarcely penetrated at all by a 1,000-volt beam. If the latter low-velocity beam is employed to charge up the dielectric, the 10,000-volt beam may be used to discharge it.

The mechanism for signal generation is a simple form of that in the iconoscope[4]. The target surface is brought to equilibrium potential with the target metal at approximately 50 volts negative. Where the writing beam has struck and driven the surface negative, the secondary emission collection is greater than unity and some charge is removed every time the reading beam scans those areas. This removal of charge produces the signal which is amplified to operate the viewing kinescope. As is true for all capacitors, removal of charge from one electrode causes an equal charge to flow onto the other, which, in this case is the signal plate. This current produces an IR drop across the load resistor R (see Fig. 7) and thereby produces the signal.

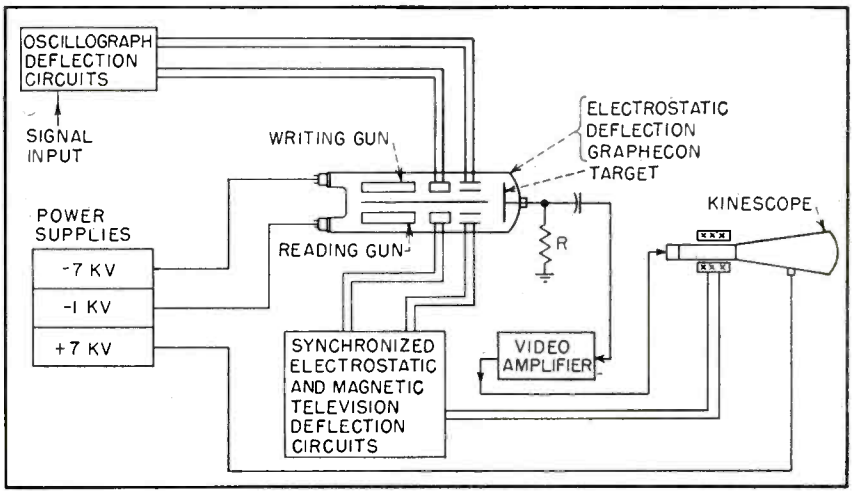


FIG. 7—Block diagram of circuits for using the graphechon as an oscilloscope

Figure 4 shows the relationship between the secondary emission ratio and the secondary emission collection (dotted line). When the surface is at collector potential, the secondary emission collection is equal to the beam current and the ratio is unity. However, if the surface goes below equilibrium the collection tends quickly to go to the true secondary emission ratio which is characteristic of the particular material. Because the collection is the charge removed, the signal output increases with decreasing surface potential to the limit of saturated secondary emission.

Output Signal

The actual variation of the output signal is shown in Fig. 5. The curve levels off at the higher voltages because the secondary emission collection tends to saturate at relatively weak fields, and the signal current therefore remains almost constant at the higher fields.

The saturation of secondary emission provides a means of obtaining many television pictures of the writing pattern. The saturated secondary emission is proportional to the beam current so that it is only necessary to reduce the beam current to reduce the amount of charge removed on each scan. However, this also reduces the signal output and the lower limit in this direction is the noise inherent in the video amplifier.

Approximate calculations were made on the time for which a signal would be seen, assuming a television type scan for the reading beam and that one spot of the target was discharged completely by the writing beam. The amount of charge removed on each scan is assumed to be a constant. The formula is

$$T = 0.0885 \times 10^{-12} \frac{kAV}{d} (r - 1) I \text{ seconds}$$

where T = viewing time, d = film thickness, A = target area, V = target voltage, r = secondary I_s ratio and I = beam current.

An experimental value for T of 5 minutes was obtained with V = 100 volts, $d = 5 \times 10^{-5}$ cm and r = 1.3. One to two minutes of continuous viewing is more usual. Several thousand scans at television standards are therefore quite feasible. Value T can be called the viewing or charging time, or the period during which the element will produce a detectable signal in the reading amplifier. The storage time when the reading beam is turned off is much greater and is determined only by the leakage resistance of the insulator. A value of ten days was obtained in one test.

It should be noted that the equation for T does not involve the number of elements in the picture, nor does it require scanning, but is exactly that which would be obtained

by calculating the charging time, if it is assumed that current I is spread out uniformly over the whole area of the target.

Because the charging time is proportional to the total area of the target, a reduction in tube size will result in a proportional reduction in the maximum viewing time. However, in applications where it is not necessary to keep the reading beam scanning constantly, the combination of storage time and viewing time can make the picture available for periods of time greater than T as given by the equations.

Target Factors

The factor of insulator thickness, however, does not necessarily vary the maximum charging time even though it varies target capacitance. If it is assumed that the dielectric strength of the insulator is constant, then varying the thickness also permits varying the voltage across it in proportion. As the capacitance per element goes down, the voltage can go up, and the charge per element remains constant. Therefore, the charging time remains constant and the maximum viewing time is independent of the insulator thickness.

The film thickness is subject to a basic limitation arising from the requirements of the conduction effect which depends on the penetration of the film by the writing beam. The efficiency of the effect, that is, the number of conduction electrons per primary, depends on the absorption of the energy of the beam. There is, therefore, an optimum writing beam voltage for each film thickness such that the maximum amount of beam energy is absorbed in the insulator. This voltage is somewhat greater than that required for complete penetration alone. Fortunately, this value is not very critical. Another factor affecting the efficiency is the gradient through the film, which should be as high as possible if it is desired to obtain the greatest sensitivity to the writing beam.

Varying the film thickness also varies the degree of half-tone reproduction. Half-tones are obtained in the voltage range where the output signal varies with the surface potential (the sloping part of the curve in Fig. 5). Beyond this slope, the signal is independent of surface potential and produces a black and white picture, so the signal is either at its maximum value or is not present. If the film is thin or the total film voltage is less than ten volts for any other reason, the reproduction will be all half-tone and the viewed picture will decay continuously.

On the other hand, a thick layer can take a large voltage and the signal will be black and white for most of the charging time. The picture will stay at constant level for a while and then decay. The choice of film thickness will, therefore, be determined by the desired ratio of half-tone to black and white viewing times and by the penetration limitations.

A typical curve of signal output versus time is shown in Fig. 6. The actual duration of the signal can be made to vary by varying the reading beam, but the ratio of the times in the two modes of operation stays constant for any given voltage change on the film. Reducing this voltage from the maximum possible reduces the viewing time as well as the ratio of black and white to half-tone time.

One of the applications of the tube is as a d-c or single-trace oscilloscope which can provide a bright picture of the complete trace for adjustable periods of time. The circuits for such a function are relatively complex compared to an oscilloscope with an afterglow type phosphor, but there are several advantages that may justify the extra equipment.

The problem of large-screen oscillography for viewing by large numbers of people can be met by using a commercial television projection set and operating the graphechon as an oscilloscope-iconoscope combination. The problem of photography of very short duration transients can be met by recording the trace in the graphechon and photographing the picture on a standard kinescope. If the interval between transients is long, the reading beam and kinescope need only be turned on when desired for photographing. In either case, the tube can be made sensitive to the writing beam and thereby reduce the need for a high-voltage type of oscilloscope which ordinarily might be required for high writing speeds.

Oscillograph

For such applications, where the writing beam is not modulated in intensity, the circuit requirements are shown in block form in Fig. 7. The components are all of a type that can be found described in television and oscillography literature.

The requirement that the writing beam be not modulated in intensity arises from the fact that it will produce a video signal in the target of the same form as the modulation and of an intensity that could be many times that of the signal produced by the reading beam. This occurs because, as was shown above, any removal or addition of charge to the target produces a signal and the writing beam, being above the second crossover point, tends to put down charge which will vary in amount with the intensity of the beam. As long as the writing beam intensity is constant, it produces only a d-c type of signal which is blocked by the input capacitor of the video amplifier.

For many applications, such as for radar conversion, it becomes necessary to modulate the writing beam at frequencies in the same range as that of the video output signal and it is therefore not possible to separate the two signals on the basis of signal frequency. However it is possible to create a frequency difference between the reading and writing signals by modulating the reading beam at some frequency well above the maximum contained in the writing signal. The output signal will now be an amplitude-modulated high-frequency carrier, which can be amplified by conventional means and rectified to provide the desired video signal free of the writing modulation.

A typical circuit is shown in block diagram form in Fig. 8, giving the components required to operate the tube as a radar converter. The operation of the tube in this manner is quite satisfactory provided suitable precautions are maintained.

The original objective and main application of this tube is to provide means of viewing radar ppi patterns. A number of advantages can be attained over conventional

practice with systems using tubes made with the P7 type phosphor. A few of these will be mentioned without description:

The decay curve of the brightness of a signal is very much improved over the exponential decay of phosphors (see Fig. 6).

The brightness level is limited only by what the best cathode-ray tubes can do, so that ambient light level is not important.

The size of the picture can be made as large as desired by television projection techniques.

The viewing time is continuously adjustable over the range of a few seconds to several minutes.

A means is provided for obtaining television type signals and this means can be used to reduce the bandwidth requirements for relaying purposes.

Improvements in signal-to-noise ratio are possible by the integration effects of superposing successive radar patterns.

A block diagram of a system is shown in Fig. 8. In the tests performed, the radar system was adjusted to a rotation period of approximately 6 seconds and the sweep times were operated at both 800 microseconds (80-mile range) and 100 microseconds (10-mile range) with adequate performance at both ranges. This showed that the writing speed was adequate to record the short-range radar which required much higher sweep speeds and peak currents in the writing beam than the long-range radar equipment.

Single-Frame Television

The high writing speed makes possible operation of the writing gun with television-type scan in which the modulating signal is applied for a thirtieth of a second (one frame time) during which time the whole target can be covered. The writing beam can then be turned off for one or more seconds before another picture is flashed on, but the reading beam, operating continuously, produces a signal for a steady picture on the kinescope. This type of operation provides a means of viewing continuously a television type picture that is generated at a rate too slow for normal viewing due to excessive flicker. Such operation has been tested and found satisfactory both in terms of storage time and resolution.

The resolution of the stored picture is best discussed in terms of television practice. Because the picture is formed by the action of a moving cathode-ray beam, the smallest picture element possible is the size of the focused spot. Therefore, the maximum picture content possible is the number of elements or adjacent spot areas that can cover the total area of the target.

A television-type scan is the most efficient because it arranges the elements as close together as possible

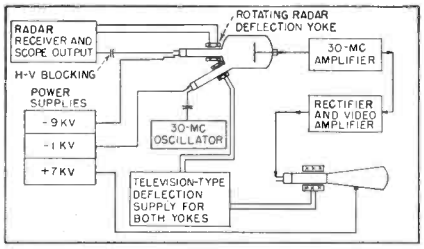


FIG. 8—Circuits required for using the graphechon to view ppi-type radar

without producing any overlapping. The ppi-type scan has considerable overlapping near the center of the picture, but this does not appreciably affect the resolution. Its only effect is to increase the bandwidth of the signal required to send its pictures over that required for the same picture rate with television type scan.

It can be shown, too, that the number of picture elements possible does not vary with the target size. A larger target must be moved further away from the electron lens of the gun if it is to be covered by the same deflecting angle of the beam. The increased gun-to-target distance causes the spot area to increase in direct proportion to the increase in target area, and so the number of elements stays constant. This property, inherent in the electron optics of cathode-ray tubes, applies when all other factors stay constant.

In view of the above, it is customary to refer to the number of elements contained in a picture by the number of parallel lines in which they can be arranged, which is the number of scanning lines used to build up the picture. A standard television picture has approximately 500 lines and an aspect ratio of 4:3 or its height is three-fourths of its width, and it therefore contains over 300,000 elements. This is the order of magnitude of the picture content available in the graphechon with present standard guns and techniques.

Writing speed is customarily measured in oscillographic practice in feet or meters per second. So measured, the writing speed of the graphechon is considerably better than 4,000 feet per second. Expressed in more meaningful terms, this is equivalent to better than nine million elements per second. This speed has been demonstrated by the test of television operation in which a picture containing 300,000 elements was written onto the target in one thirtieth of a second. Still higher writing speeds can be obtained, though only at the expense of resolution, because they require higher beam currents and this causes the spot size to increase, when all else is constant.

General Comments

It should be noted that the effect of the writing beam is not necessarily the complete discharge of the target potential but, for small beams, the target is only partially discharged. Therefore, small writing signals will disappear faster than large ones. This effect can be useful in looking at noisy radar ppi pictures. The noise disappears quickly, leaving only the stronger radar pips. Also, when the tube is adjusted to store for several radar frames, which are superimposed, the signal input to any point is additive. Therefore a repeated signal will give a strong output signal, whereas random noise of the same level will not repeat to the same point to the same extent, and so produce a weaker output signal.

The author wishes to acknowledge the invaluable advice and assistance of L. E. Flory, A. Rose, H. B. Law, and many others at the RCA Laboratories.

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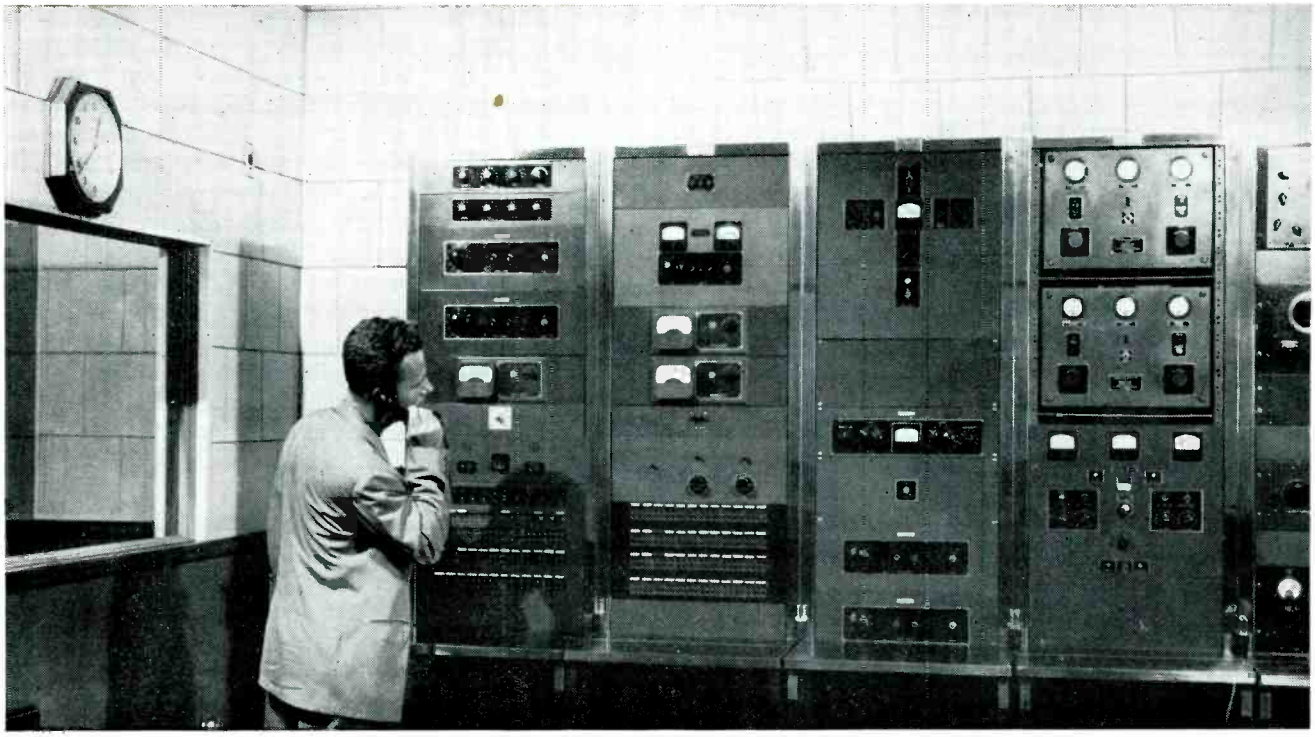

Audio facilities (left) transmitter monitoring equipment (right) at modern a-m station includes phase monitor for directional antenna array

A-M and F-M Broadcast Station Measurements

Routine operating checks required by law and proof-of-performance measurements necessary before a station can be authorized for regular operation. New audio-frequency and noise measurements mandatory for a-m transmitters after August 1949 are summarized

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BEFORE granting a broadcast station license the Federal Communications Commission requires that certain measurements be made (during the equipment test). After the station goes into regular service other continuous measurements are mandatory. In addition, there are periodic measurements necessary in order to conform to legal requirements.

These requirements and the equipment necessary for satisfying them are described below. Functional descriptions of the manner in which the measurements are made are not included, because most engineers have their own particular methods which depend upon the exact equipment used.

When the station has been completed in accordance with the terms of the construction permit, equipment tests are conducted. During this time the proof-of-performance of the station and antenna resistance measurements are made. Until the latter measurement has been made and approved by the Commission the station must measure its power by the indirect method. This entails finding the product of the three parameters, the plate voltage, plate current and an efficiency factor laid down by the Commission for the class of station. The resultant figure is then used as the output power until the antenna measurements have been approved and authority given to operate, measuring power by the direct method. As its name implies, the direct method involves the actual antenna current and the antenna resistance only. The product of $(I_{ant})^2 \times R_{ant}$ gives the actual power in the antenna.

Although it may not be recognized as a separate indicating or measuring instrument, the antenna meter is one of the most essential pieces of equipment the broadcast operator uses. Whenever any measurements involving this instrument

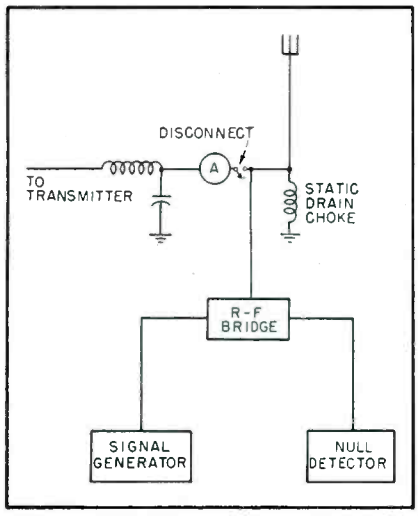


FIG. 1—Apparatus setup for antenna resistance measurements

are filed they must be accompanied by a statement giving the maker's name, name of instrument, manufacturer's rated accuracy, and the date, the determined accuracy and name of person by whom it was last calibrated. During the time that the station is on equipment test the antenna resistance measurements will be made. After these have been approved and authority given to measure output power using the direct method the antenna ammeter comes into its own, and is the indicator of power output.

In addition to determining antenna resistance when a new station is put on the air, this parameter must also be measured at other times. For example: if any characteristics of the antenna are changed, or the directional pattern is changed or any damage to the antenna itself occurs, the resistance must be remeasured and authority to indicate output power by the direct method requested.

To measure antenna resistance, the following equipment is required: A signal generator that will cover at least 60 kc each side of the assigned frequency, an r-f bridge and some form of balance detector, such as a sensitive receiver.

The equipment is connected as shown in the block diagram in Fig. 1, and a series of resistance measurements is made on the antenna at frequency intervals of 10 kc. A curve is drawn through these points and the resistance at the operating frequency taken from this graph. The antenna is disconnected from the transmitter during the measurements. For a directional array, the resistance at the common junction point is measured, not at the individual towers. Figure 2 illustrates this method of measurement.

Field Intensity

For the proof-of-performance measurements, a field intensity measuring set like that illustrated is used. For ease of operation the set is frequently built into a semi-permanent installation in a car or station-wagon as shown. In the latter case the whole unit, including the car, has to be calibrated by a responsible organization (such as the National Bureau of Standards) to satisfy the FCC that the measuring equipment is accurate and reliable. This check on reliability also applies to the engineer. When presenting his data he must include proof of his qualifications as an engineer to show that he is able to do an accurate job. Of course, if his qualifications are already on file with the Commission, a statement to that effect is sufficient. Measurements are made along a number of

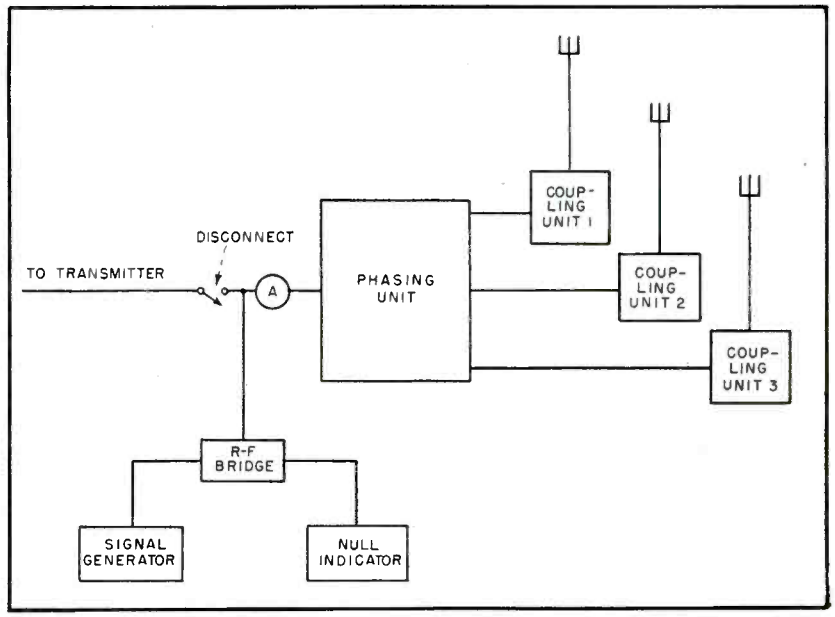


FIG. 2—Resistance measurements on a three-tower array are made at the phasing unit using the same type of testing equipment as for the simple antenna

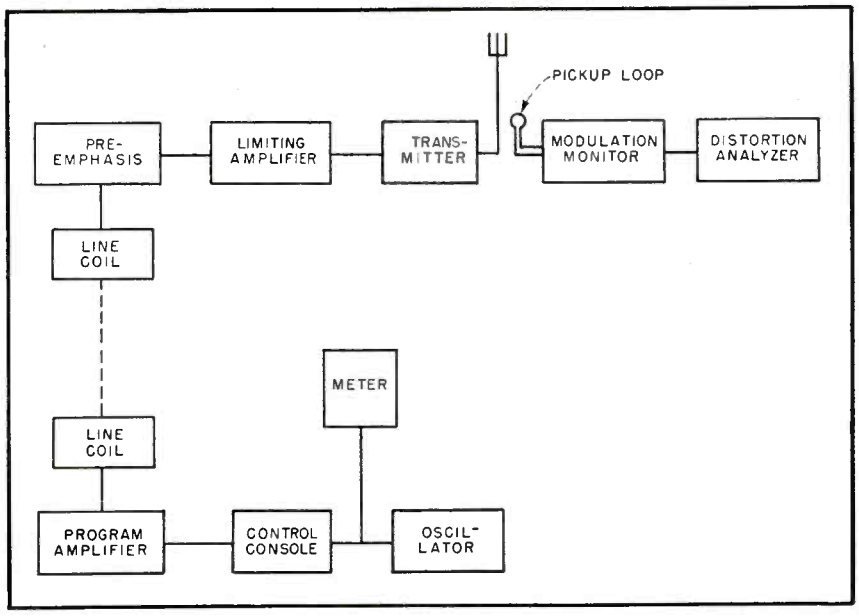


FIG. 3—Arrangement of apparatus for audio measurements on f-m transmitter

radials running out from the transmitter site. A minimum of eight radials is usual. The field strengths are plotted against distance and from these curves the distance to the various contours can be found and the contours themselves outlined on a chart.

In the case of a directional antenna the proof is more involved in that it is necessary to determine the pattern of the antenna system,[1] and prove that it is operating the way the application said it would. It often takes days and sometimes weeks to get the radiation in the critical directions down to the values specified in the construction permit.

In the adjustment of the directional antenna, as well as in the normal operation of the transmitter, a very important part is played by the phase monitor. This may be a commercial model or composite (homemade) type.[2] Because the commercially manufactured equipment has already been type-approved by the FCC, and since full details must be submitted by applicants using unapproved equipment, and requirements are rigid, it is usual to employ the commercial apparatus.

Table I—Measurements and Equipment for Broadcast Stations

Measurements	Mod.	Equip. Required	Location Portable	Location Fixed	Conditions Essential	Conditions Optional
Antenna resistance and reactance	a-m	Signal generator, r-f bridge null detector, receiver	Base of antenna, or common point for directional antenna		For license (and after change in any antenna parameters)	
Antenna power	a-m	Remote reading r-f ammeter		Transmitter	Regular use	
Antenna power	f-m	Power output meter (calibrated with dummy antenna when transmitter installed)		Transmitter	Regular use	
Antenna phase	a-m	Phase monitor for checking currents in each tower of directional antenna		Transmitter	Regular use	
Field intensity	f-m	Field intensity measuring set, auto recording milliammeter	Field, service area		For license	When desired
Field intensity	a-m	Same as above	Field service area		For license (after change in directional antenna)	When desired
Audio response	f-m	Audio-freq. oscillator, distortion analyzer, vtvm	Studios and transmitter		For license	When desired
Audio response	a-m	Same as above plus frequency-shift indicator (freq. monitor)	Studios and transmitter		For license renewal	When desired
Transmitter efficiency	a-m f-m	Plate current and voltage meters, antenna current meter		Transmitter	License and renewal	When desired
Frequency and modulation	f-m	Freq. and modulation monitors		Transmitter	Regular use	
Frequency and modulation	a-m	Freq. and modulation monitors		Transmitter	Regular use	

Frequency and Modulation Monitors

Frequency and modulation monitors are often grouped together, because their functions are sometimes combined in a single unit of equipment. Even when the modulation monitor is not so combined, this ancillary equipment is customarily designed for rack mounting, and quite often placed next to the frequency monitor for convenience. In operation, the modulation monitor can be set to indicate peaks of modulation of any value up to 100 percent. Some models will show as high as a calibrated 120 percent.

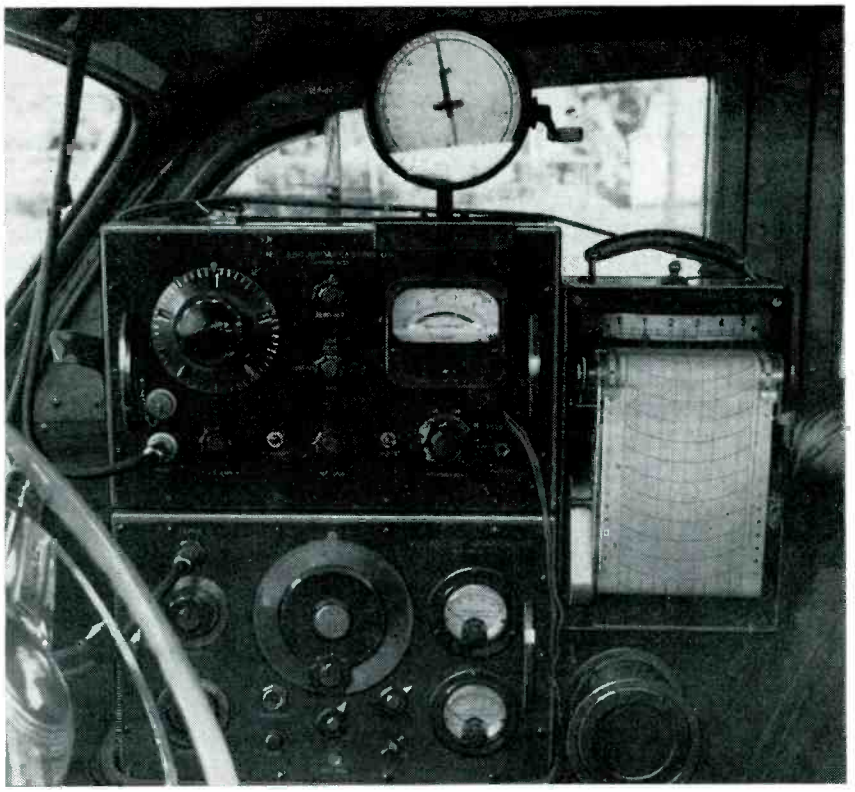
The frequency monitors used for a-m are a little different from those for f-m in their operating characteristics, as well as their method of operation. The frequency tolerance for a-m on the standard broadcast band is plus or minus 20 cycles, so that the range of the meter is not required to be very great, whereas in f-m (because of the nature of the modulation) the allowable deviation is plus or minus 2,000 cycles, and a different type of meter is used to accommodate greater range.

External Frequency Checks

The accuracy of the frequency monitor is a matter of great importance. Although the FCC does not require that it be checked regularly, most radio stations obtain a monthly frequency check of the transmitter from one of the commercial frequency checking services. The frequency monitor is thereby checked at the same time (since its indicated frequency can be compared with the external reading). By this means, any tendency of the monitor to drift off frequency and give inaccurate readings will be stopped before interference is caused.

Less attention is required by the modulation monitor. The level of the r-f signal fed into it must be adjusted to ensure accurate readings, and routine checks of the various voltages made. There are no oscillatory circuits to get out of tune.

A heterodyne-type frequency monitor is used in most cases. The signal from a local, very stable os-



Field strength measuring equipment mounted in station wagon. Loop is oriented by turning crank and direction is indicated on dial

cillator, crystal-controlled with temperature correction, is mixed with the sample signal from the transmitter. The resulting beat at some low audio frequency is amplified and used to drive a zero-center type of meter. When the transmitter is on frequency and the monitor is operating correctly zero deviation will be indicated. As the frequency varies one way or the other the resulting positive or negative difference will be read on the meter directly in cycles.

New Audio and Noise Measurements

The modulation monitors of various manufacture also work on a more or less common principle although no two designs are alike. Generally speaking, the signal to be measured is applied to a diode circuit and rectified; this provides a means of calibrating the equipment. The audio component of the rectified r-f is then rectified and applied to a vacuum-tube voltmeter circuit with suitable circuit constants so that the a-f peaks are indicated. The visual flasher for indicating overmodulation is operated from a relay which is driven by the a-f signal and adjusted to close on varying modulation peaks according to the setting of the sensitivity control.

Until quite recently, audio measurements for a-m stations were not required by the FCC. Although they do not now have to be supplied with the license application they are required to be made annually, and must be made within the four months preceding the license renewal application.[3] Since these measurements are very similar in nature to those required for an f-m license application the description of the equipment involved will be combined with that for f-m below. The equipment is only employed once a year and therefore can be borrowed or hired for the occasion.

The audio measurement requirements of the FCC for a-m stations are detailed in paragraphs 3.45 and 3.46 of the Rules and Regulations, and are abstracted in the accompanying box.

Frequency-Modulation Requirements

The license application for an f-m station calls for a field intensity survey to be made of the area purported to be served by the station, and the submission of maps showing the area, routes followed (radials) and the 1 millivolt-per-meter and 50 microvolt-per-meter contours (class B station).

The field intensity measurements are made in a similar manner to those for a-m except for the fact that continuous recordings are required along the radials from the transmitter.[4] Equipment for this service is generally self-powered from a six-volt storage battery and vibrator power supply in a separate case. The antenna supplied with it is a dipole adjustable to length for any of the f-m frequencies and mounted on a collapsible tripod. For full field survey work the set is often mounted in a station wagon with a circular loop antenna above the roof and a calibration curve made for the whole unit.

The requirement of continuous recordings makes a nondirectional loop almost mandatory, but at the same time cuts down the sensitivity of the equipment. An Esterline-Angus recording milliammeter is driven from the output of the field set. The paper feed is turned by a flexible drive from the speedometer shaft drive. In this way the distance and field intensity can be correlated, provided the car follows a reasonably straight route. As an aid to this, prominent landmarks and position fixes are marked on the chart to help in identifying locations.

Audio Standards for F-M

The Commission requires that the audio measurements be made in accordance with the following, abstracted from Sections 8 and 13 of the Standards of Good Engineering Practice. All measurements shall be made with the equipment adjusted for normal program operation and include all circuits between the main studio microphone terminals and the antenna output, including telephone lines, pre-emphasis circuits and any equalizers employed (except for microphones) and without compression if a compression amplifier is installed.

The usual setup for making these measurements is shown in block diagram form in Fig. 3. The general arrangement is the same whether the main studio or local input to the transmitter is being used. A good audio oscillator is essential, and a distortion analyzer is needed.

The same equipment is also required for making the a-m audio measurements referred to above. For measuring the a-m carrier noise on f-m transmitters a separate diode circuit is needed for a-m rectification. A number of the distortion analyzers on the market make provision for this by including a diode in the circuit.

Measurements of audio-frequency response are made with 25, 50 and 100 percent modulation on the following minimum number of frequencies: 50, 100, 500, 1,000, 5,000, 10,000 and 15,000 cycles. These measurements are normally made without using de-emphasis, but if the accuracy of the de-emphasis circuits is good enough to ensure that the measured response is within the required limits, it can be used.

Harmonic distortion for the same modulation percentages is also required to be measured at the following frequencies: 50, 100, 400, 1,000 and 5,000 cycles; also harmonics for 100-percent modulation with fundamental frequencies of 10,000 and 15,000 cycles. Harmonics to 30,000 cycles shall normally be included. The standard (75 microsecond) de-emphasis is used in the system or measuring equipment.

Measurement is also required of the output noise level (f-m) between 50 and 15,000 cycles in decibels below the audio-frequency level representing a frequency swing of 75 kc. The 75-microsecond de-emphasis shall also be used here. The a-m noise level in the same frequency band below the level representing 100-percent modulation is also required. In this case, too, standard de-emphasis is used.

Frequency and modulation monitors are just as essential in f-m stations as in a-m. The two functions of monitoring are combined in these instruments, making for more compact station layouts. These instruments come under the classification of essential instruments, and waiver of the appropriate sections of the Rules and Regulations must be requested to cover operation without them. When the application for license is submitted, full data on the frequency calibration checks of both the transmitter and frequency monitor must be supplied to show the comparative readings of the two instruments.

Although the instruments themselves are part of the transmitter proper, and thus could be excluded on the grounds that they are not separate instruments in the general sense of the word, the indications of the plate current and voltage meters in the final stage (both a-m and f-m) are extremely important. No specific external readings are made on them, but the regular current and voltage readings entered in the operating log are measurements which are essential to the broadcaster in maintaining legal power output.

Table I is appended showing the various types of equipment, operation, and location for various measurements required by the FCC either for initial installation, regular operation or in special contingencies.

Broadcast Audio Tests Required After Aug. 1, 1949

The licensee of each standard broadcast station shall make the following equipment performance measurements at yearly intervals. One such set shall be made during the four-month period preceding the date of filing application for renewal of station license. Since renewals are to be filed two months before expiration date, that means any station which files on or after February 1, 1950 for renewal will be required to state on the application that measurements have been made.

Data and curves showing overall audio-frequency response from 30 to 7500 cycles for approximately 25, 50, 85 and 100 (if obtainable) percent modulation. Family of curves should be plotted (one for each percentage above) with db above and below a reference frequency of 1,000 cycles as ordinate, and audio frequency as abscissa.

Data and curves showing audio-frequency harmonic content for 25, 50, 85 and 100-percent modulation for fundamental frequencies of 50, 100, 400, 1000, 5000 and 7500 cycles (either arithmetical or root sum square values up to the tenth harmonic or 16,000 cycles). Plot family of curves (one for each percentage above) with percent distortion as ordinate and audio frequency as abscissa.

Data showing percentage carrier shift for 25, 50, 85 and 100-percent modulation with 400-cycle tone.

Carrier hum and extraneous noise generated within the equipment and measured as the level below 100-percent modulation throughout the audio spectrum or by bands.

Measurements or evidence showing that spurious radiations including radio-frequency harmonics are suppressed or are not present to a degree capable of causing objectionable interference to other radio services. Field intensity measurements are preferred but observations made with a communications type receiver may be accepted. However, in particular cases involving interference or controversy, the Commission may require actual measurements.

Measurements shall be made with the equipment adjusted for normal program operation and shall include all circuits between main studio amplifier input and antenna output, including equalizer or correction circuits normally employed, but without compression if such amplifier is employed.

The above data together with a description of instruments and procedure signed by the engineer making the measurements, shall be kept on file at the transmitter and shall be made available upon request to any duly authorized representative of the FCC

Typical field-measurement car showing loop antenna on roof

References

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Incremental

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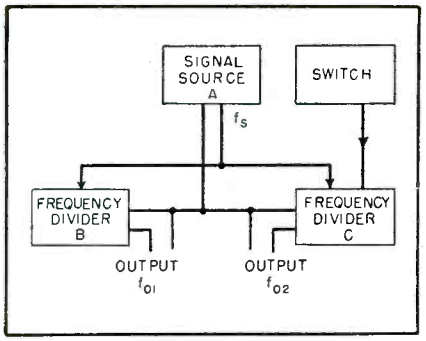


FIG. 1—Block diagram of a basic phase splitter

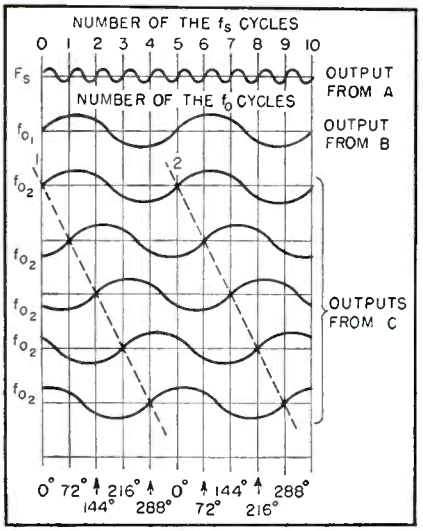
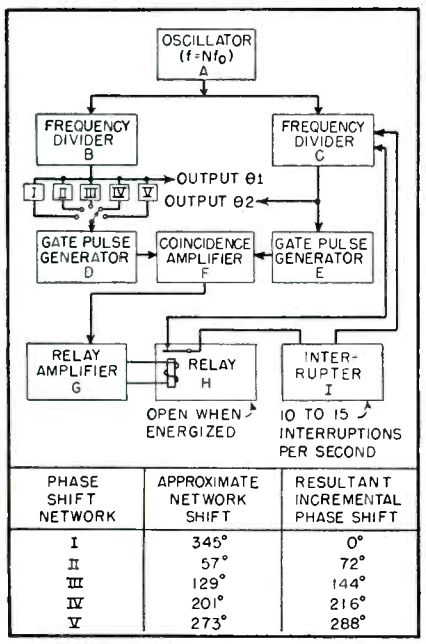


FIG. 2—Phase relations in the incremental phase splitter



PHASE SHIFT NETWORK	APPROXIMATE NETWORK SHIFT	RESULTANT INCREMENTAL PHASE SHIFT
I	345°	0°
II	57°	72°
III	129°	144°
IV	201°	216°
V	273°	288°

FIG. 3—Phase splitter allowing predetermined selection

THE incremental phase splitter and range simulator to be described is a circuit productive of two signals of the same frequency and differing in phase by a series of discrete increments of equality.

The incremental phase splitter is ideally suited to applications requiring precise time or phase relationships between two signals of the same or harmonically related frequencies. A few of its possible applications are the simulation of radar and loran data, generation of accurate synchronizing signals for the production of delay gates and timing pulses, and use as a laboratory phase standard.

Range Simulator

The circuit was developed as a target range simulator to facilitate the development of radio ranging equipment.

An 81.94-kc sine wave, corresponding to 2,000 radar yards per cycle, is employed as the ranging system's time base. The phase displacement between the transmitted and received timing signals is determined by their transmission time through space and is directly proportional to target range. In order to function as a calibrating range simulator, the circuit must provide two 81.94-kc sinusoidal signals, one fixed in time and the other variable through a series of angular displacements corresponding accurately to the required range test points. The ranging system's test points are: 0, 400, 800, 1,200, and 1,600 yards. The corresponding phase displacements between the transmitted and received signals are: 0, 72, 144, 216, and 288 degrees.

The basic circuit of the incremental phase splitter is shown in block form in Fig. 1 wherein f_s is the source frequency, f_o is the output frequency, N is required number of phase increments, and $f_s = Nf_o$. The circuit consists of signal source, A, of frequency f_s; a constantly operating frequency divider, B, synchronized by A and dividing its output frequency by N; and another frequency divider, C, identical to B but provided with means whereby its operation may be momentarily interrupted. The circuit operates as follows. Divider B provides the fixed, or reference phase. Divider C provides the incrementally variable phase. A momentary contact switch is wired into C in such a manner as to render it inoperative when the switch is closed. Upon releasing the switch, divider C again becomes operative, synchronizing with A in one of N phase relationships. This is graphically illustrated by Fig. 2 in which $N = 5$.

The generalized values of the N phase relationships the $\theta + 0$, $\theta + [360/N]$, $\theta + [2(360)/N]$, . . . $\theta + [(N-1)\ 360/N]$ degrees, where θ represents the residual phase displacements between the outputs of B and C when the incremental displacement equals zero. The value of θ reduces to zero when B and C are synchronized at identical points in time on the signal from A. The phase selection sequence cannot be predetermined in this basic circuit because of the random nature of the synchronization of C to any one of five cycles of A.

Figure 3 illustrates a method whereby any one of a predetermined series of angular increments can be selected at will. Blocks A, B and C comprise the oscillator-divider combination previously described. Here, again, $N = 5$. Divider B feeds five networks that shift the phase of its output to a few degrees less than the required in-

Phase Splitter

Range simulator circuit produces two signals at the same frequency but differing in phase by fixed and equal amounts. Developed for testing radar equipment, the device serves as a laboratory phase standard

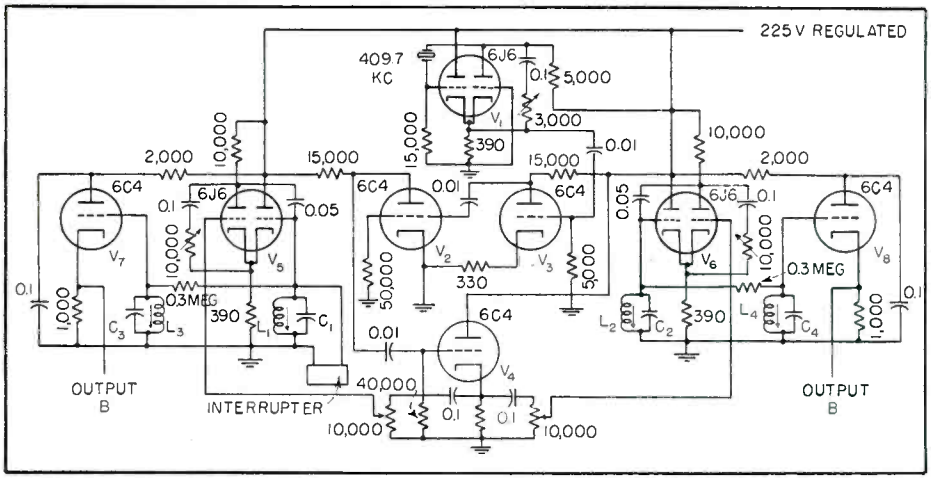


FIG. 4—Schematic of the incremental phase splitter with frequencies chosen for radar range simulation

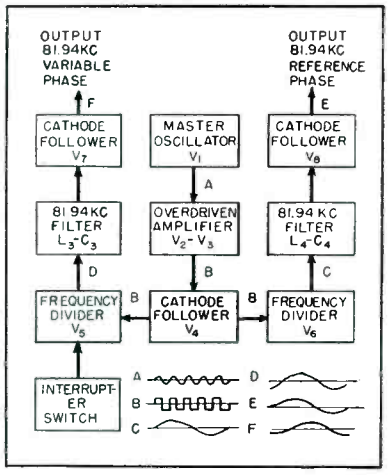


FIG. 5—Block diagram and waveforms for the circuit of Fig. 4

cremental displacements. The output of the selected network is fed to a gate pulse generator, D, via the selector switch. Divider C also feeds a similar pulse generator, E. The two pulse generators feed a coincidence amplifier, F, which produces one pulse per cycle only when the two gate pulses overlap in time. A continuously acting interrupter, I, throws C in and out of operation, thus permitting C to synchronize repeatedly to any one of the five cycles of A at random. When the output of C is such that it is approximately in phase with the selected signal from the phase-shift networks, the resultant output pulses from the coincidence amplifier, F, energize relay H via its control amplifier, G. This action immediately disconnects the interrupter and stabilizes the circuit at the required incremental phase shift.

Figure 4 illustrates a practical version of the circuit shown in Fig. 1. Tube V_1 is a 409.7-kc crystal master oscillator; V_2 and V_3 are overdriven amplifiers which decrease the rise time of the synchronizing signal and thus minimize phase jitter between outputs. The cathode follower, V_4, couples the synchronizing signal from V_2—V_3 to the two frequency dividers, V_5 and V_6. The low source impedance of V_4 prevents interaction between V_5 and V_6. The Crosby[1] two-terminal, resistance-stabilized oscillators[2] are excellent frequency dividers, readily synchronized and of good sinusoidal waveform. Filters L_3—C_3 and L_4—C_4 feed reasonably pure sine waves to the output cathode followers, V_7 and V_8.

In use, the simulator signals are fed to the range-determining circuits in place of the transmitted and received signals. After zero-setting the range indicator, the interrupter switch connected to V_5 is repeatedly actuated and the new indicated ranges are recorded.

This process is repeated until all five check points have been recorded. If desired, one of the simulator signals can be inverted in phase to provide five more check points; 200, 600, 1,000, 1,400, and 1,800 yards. Error curves relating actual and indicated range can be readily plotted from the recorded data.

Accuracy after a brief warm-up is such that no short-time change in the incremental phase shift is detectable by conventional methods. Because of the phase-sensitive nature of the resonant filters, the circuit exhibits a gradual drift of θ, the residual constant. Since drift compensating arrangements are many, and fairly well known, they are not considered here.

Many incremental phase-splitter applications require the generation of a pair of pulses occurring at a known repetition rate and displaced from one another by one of a series of discrete time increments. This requirement can be met by replacing the sinusoidal frequency dividers with multivibrators and differentiating their outputs.

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Improved Ultrasonic Delay Lines

Forged magnesium-alloy delay lines developed as memory devices have bandwidths as great as 4 mc at a carrier frequency of 10 mc. The attenuation is the least so far available in practical lines. Special clamping of S-cut ADP crystal transducers is described

THE ULTRASONIC DELAY LINE is a device developed during World War II to store intelligence for periods of several milliseconds and is now used in high-speed digital computers and other devices.

The construction and operation of a typical delay line is shown in Fig. 1. The crystals have a resonant frequency in the range of 10 to 30 mc. The intelligence to be stored modulates the carrier frequency. The first delay lines used employed liquids as transmitting media, but the many disadvantages of liquids caused a search to be made for a suitable solid.

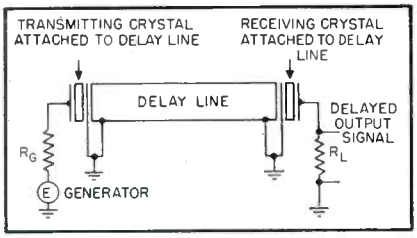


FIG. 1—Elementary delay line, showing how signal is transmitted by input transducer and delayed output having same waveform is received

During the war much effort was spent in finding solids with low ultrasonic absorption for use in constructing ultrasonic delay lines. An account of this work, and the solid delay lines constructed, are to be found in the report of D. L. Arenberg[1]. A complete bibliography of previous work is also given in his report.

At the end of the war, Arenberg's conclusions were that fused quartz offered the best transmission qualities of any known substance, but that the length of delay was limited by the size of the blanks available. It was also difficult to machine properly, and great angular accuracy of the reflecting faces was necessary to prevent the generation of spurious signals resulting from inaccuracies.

Single crystals showed good ultrasonic transmission, but when polycrystalline media such as steel, tungsten, fine-grained aluminum and magnesium were tried, their absorption was too high for delay-line purposes. Magnesium alloys were not considered at that time.

The Delay Medium

The objective of our investigations was to find a medium from which lines having 3 milliseconds or more delay could be constructed, operating at a carrier frequency of 10 mc or higher, and having a bandwidth greater than 2 mc. At the time these studies were initiated, there was no solid that would give this performance. Fused quartz was acceptable, except that 2,000 μsec was the longest delay obtainable without strong spurious signals.

Many materials were tested to de-

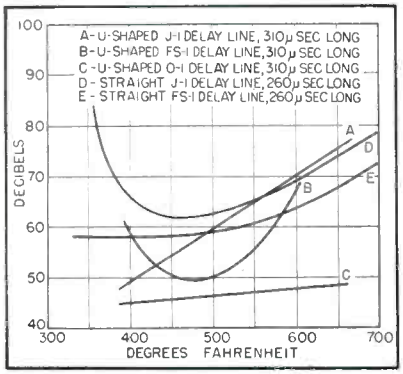


FIG. 2—Successive annealings at increasing temperatures change the attenuation

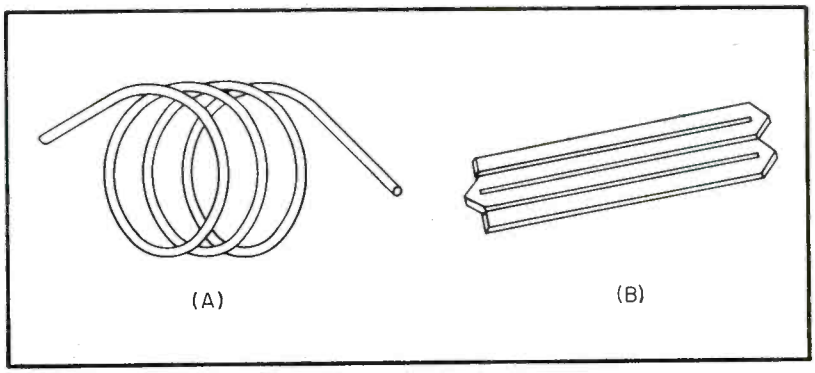
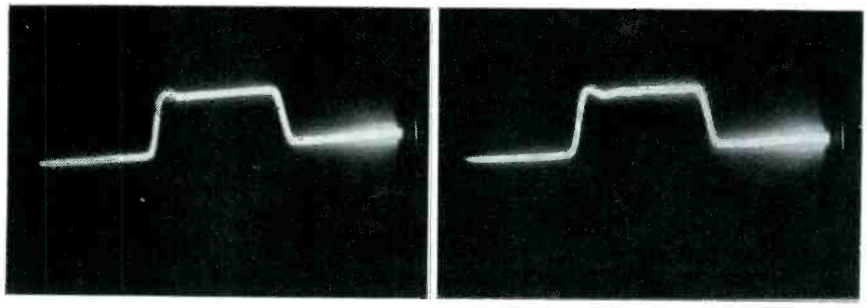


FIG. 3—Two of the experimental folded forms of delay lines used. Various conformations were tried in developing compact units



A 2.4-microsecond pulse (left) is received (right) with little distortion

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termine their suitability. Some results are shown in Table I. The velocity measurements were taken with a Sperry Reflectoscope at a frequency of 10 mc.

To determine whether the attenuation was low enough in the metal, test lines having about 500-μsec delay were constructed and the losses in the crystals and medium measured. In all measurements taken, mismatch and cement losses were of the order of 30 db.

This attenuation was sufficient to reject all materials listed in Table I except fused quartz and the magnesium alloys O-1, J-1 and FS-1. These materials were far superior to any of the others, the transmission being best in the order named. For example, a J-1 delay line, delay 397 μsec, at carrier of 10 mc had an attenuation of 40 db; and an FS-1 delay line, 970 μsec, at 10 mc, had an attenuation of 50 db. These measurements were made with 1,500-ohm resistors and a resonant coil shunting the crystals. The shear mode was used in both cases, with the crystals cemented to the magnesium alloy. No end cells were used. Other examples include a straight rod of O-1 alloy, delay 329 μsec, with attenuation of 35 db when untreated. After heat treatment at 450 F, the attenuation was 30 db, and the pulse shape improved. A straight rod of FS-1 alloy, with a delay of 330 μsec, had an attenuation untreated of 38 db; upon treatment at 450 F attenuation dropped to 32 db, with improved pulse shape.

The next series of tests was made using rods bent into the shape of a U. Three rods of J-1, FS-1, and O-1 were heated to 400 F and bent. Before heat treatment the attenuations at 10 mc were FS-1, 67 db; O-1, 47 db; and J-1, 75 db.

The rods were then heat treated and tested after the temperature was raised in steps. The results are shown in Fig. 2. If plots had been made at lower temperatures minima could have been found for O-1 (C) and J-1 (A) also.

To determine these minima, readings were taken on two other samples of J-1 (D) and FS-1 (E). These curves are also plotted in Fig. 2. There is little agreement in these curves. It seems that 500 F is a good annealing temperature, but the results vary too much in the two samples to arrive at any general conclusion. The composition of commercial alloys is not constant enough to determine the best heat treatment. Laboratory samples of these alloys will probably give consistent results.

As an illustration of the great variation in transmission properties, one long rod tested showed a signal internally reflected several times that was delayed 4,950 μsec, with an attenuation 47 db below the input pulse. But in the compact, folded configurations used in these

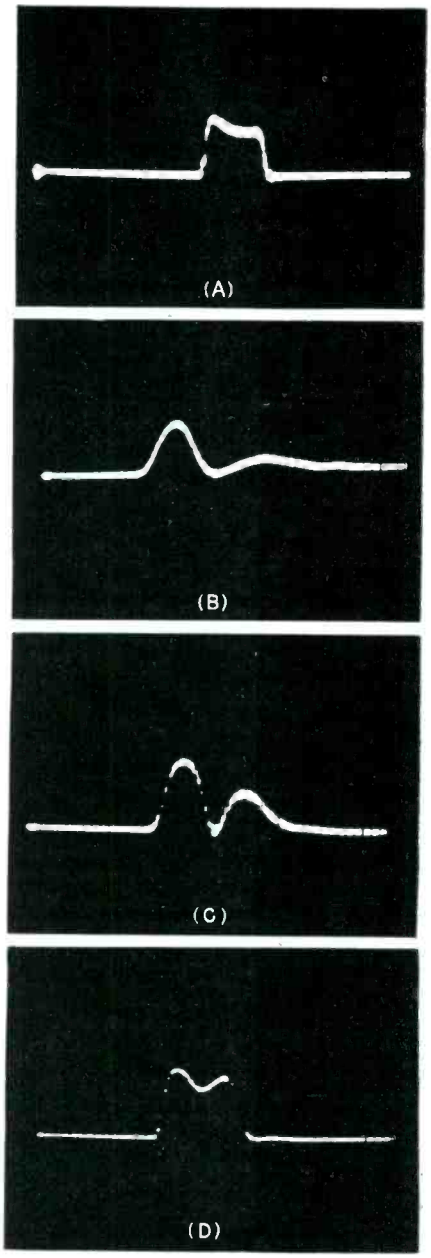

FIG. 4—Change in transmission characteristics after successive forgings. The transmitted pulse is shown at (A). See text for explanation of (B), (C) and (D)

experiments, 1,600 μsec is the upper limit that can be relied upon using commercial alloys. Two of the configurations used are shown in Fig. 3.

Another type of treatment to improve transmission in magnesium and the alloys mentioned above was hot forging with a drop hammer forge. The pressure used was approximately 5 tons per square inch.

The first sample treated by forging was a billet of pure magnesium 10 centimeters long. The results

obtained are illustrated in Fig. 4, the transmitted pulse being shown at 4A. Before forging, the signal could not be seen, placing the attenuation above 90 db. After the first forging at 550 F, and heat treatment, the attenuation was 61 db, with a change in wave shape as shown at 4B. After the second forging the received pulse was down 68 db as at 4C. The third forging, not illustrated, showed an increase in attenuation but a somewhat better pulse response. The fourth forging, at 500 F, showed marked improvement in pulse response with attenuation at 61 db, as indicated in 4D.

Before treatment the grain size of the magnesium was small and very jumbled. After the final forging, the grain size was larger, and more orderly in arrangement. The amount of inclusion was not changed.

A sample of J-1 alloy was also forged that had good transmission, but poor pulse reproduction. After passing through the same treatment as the pure magnesium, the pulse reproduction was much improved.

Upon microscopic examination, the grain size proved to be unchanged after forging, being smaller than the pure forged magnesium. The compound was more evenly distributed between grains after forging. The sample had an attenuation of 38 db, and was 10 centimeters long.

In addition to the transmission

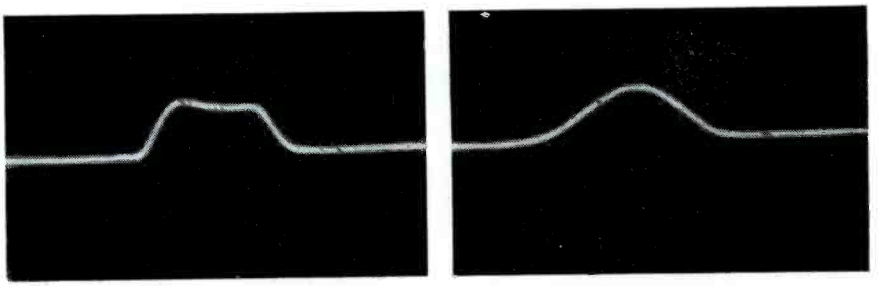

FIG. 5—A 1-microsecond 10-mc pulse, at left, and the corresponding received pulse through a magnesium delay line using cemented-quartz AC-cut transducers

and pulse fidelity of the medium, the change of delay time of the signal with temperature is of importance in using these devices. This condition was measured by mounting a delay line made of FS-1 alloy 10 inches long inside an oven and the change in delay time measured. The change in delay time with temperature proved to be linear, and the total delay time for a sample of length L is given by

$$D_{Mg} = L\ (8.34 + 0.0021T)$$

T being the temperature in degrees centigrade, and 8.34 being the delay per inch at 0 C.

In Report 745, Radiation Lab., MIT, Jacobson obtained for a mercury delay line.

$$D_{Hg} = L\ (17.42 + 0.0052T)$$

where the symbols have the same meaning as before. From these relations the temperature coefficient of delay of mercury is 2.99×10^{-4} sec per sec per deg C while for FS-1 alloy it is 2.52×10^{-4} sec per sec per deg C. The coefficient for mercury is 18.7 percent greater than that of FS-1 alloy.

The shear mode of vibration was found to be the best type for solid delay-line application. Since the bars used were many wavelengths wide, there was no velocity dispersion present in the bar. The use of the shear mode has the advantages of less spreading of the sound beam in the medium, decreased velocity of propagation, and a noticeable improvement in signal-to-noise ratio of the delay line.

Shear Crystals

Since the shear mode gives a polarized wave, only a portion of the noise originating in the medium affects the receiving crystal. The computed gain in signal-to-noise ratio over the compressional mode is 4.97 db.

These advantages have been realized in practice, and use of the longitudinal mode has been discontinued in solid delay lines.

The first delay lines constructed using magnesium alloys used AC-

Table I—Characteristics of Delay-Line Materials

Material	ρ (grams per cu cm)	V_L (cm per sec $\times 10^5$)	V_T (cm per sec $\times 10^5$)	V_R (cm per sec $\times 10^5$)	σ	E (dynes per sq cm $\times 10^{11}$)
FS-1 Extruded Magnesium	1.690±0.020	5.473±0.012	3.030±0.013	2.800	0.279±0.004	3.07±0.19
J-1 Extruded Magnesium	1.700±0.030	5.673±0.013	3.010±0.013	2.793	0.304±0.004	4.02±0.19
AM3S Magnesium	1.735±0.002	5.787±0.029	3.095±0.015	2.870	0.300±0.006	4.32±0.07
M-Extruded Magnesium	1.750±0.010	5.758±0.011	3.092±0.010	2.866	0.297±0.002	4.34±0.05
0-1 Extruded Magnesium	1.817±0.002	5.800±0.029	3.041±0.015	2.825	0.310±0.005	4.40±0.06
Fused Quartz	2.198±0.004	5.926±0.030	3.751±0.019	3.395	0.166±0.006	7.30±0.12
Pyrex	2.226±0.001	5.574±0.028	3.436±0.017	3.127	0.194±0.010	6.27±0.12
Plate Glass	2.510±0.010	5.769±0.029	3.426±0.017	3.137	0.227±0.008	7.32±0.14
2SO Aluminum	2.713±0.005	6.349±0.032	3.105±0.016	2.900	0.343±0.001	7.02±0.10
Molybdenum	10.09±0.03	6.286±0.031	3.348±0.016	3.106	0.302±0.004	29.4±0.5
Tungsten	19.25±0.01	5.183±0.026	2.873±0.014	2.654	0.278±0.006	40.6±0.6

ρ = density
V_L = longitudinal velocity
V_T = transverse velocity
V_R = Rayleigh wave velocity (computed from V_L and V_T in this table)
σ = Poisson's ratio
E = Young's modulus
V_L and V_T correspond to those computed using the bulk modulus of elasticity

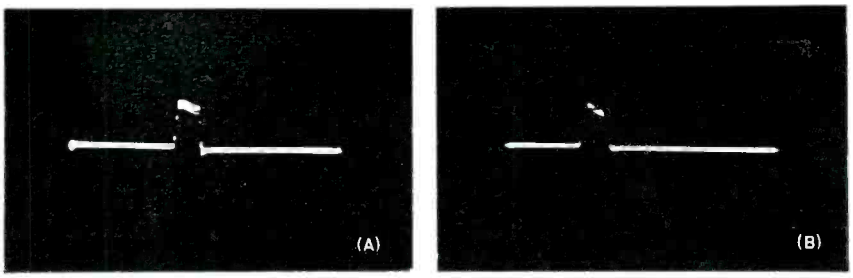

FIG. 6—A 1.5-microsecond 10-mc pulse, at left, and the pulse received after a delay of 225 microseconds, using S-cut ADP crystal transducers

cut quartz crystals as transducers. The crystal capacitance was tuned out with an inductance, and the resulting resonant circuit loaded with a 1,500-ohm resistor to improve the response. The crystals were cemented to the magnesium alloy with a thin film of phenyl benzoate, which is applied melted and cools to form an adherent layer.

Bandwidth of Lines

Although the attenuation in these delay lines was low, a measurement of the response showed the bandwidth to be 0.8 mc at a carrier frequency of 10 mc. This is entirely inadequate for many applications of the device.

Since the typical pulse response of the delay line, shown in Fig. 5, was not satisfactory, it appeared that this might be improved by a different choice of crystal. According to the current theory used in delay line design,[2,3,4] for optimum bandwidth the ratio of the acoustic impedances of the magnesium to the crystal should be equal to the square root of 2. The crystal should have a high dielectric constant and a high piezoelectric constant for good coupling of energy into the medium.

The crystal chosen was S-Cut ADP (Ammonium Dihydrogen Phosphate, $NH_4H_2PO_4$) which is nearly ideal from these considerations. Its constants are: piezoelectric constant, 24×10^{-10} cm per volt; sound velocity in crystal, 2.02×10^5 cm per sec; acoustic impedance, 3.6×10^5 acoustic ohms; dielectric constant, $K_s = 55$; $K_s = 14.5$.

This cut is derived from Z-cut by rotation about the X axis, 45 deg off the Y axis, and vibrates in thickness shear.

The thickness constant for this crystal is fairly small, and blanks were available at a resonant frequency of 1 mc. To operate at 10 mc, the 1-mc blank was cemented to the magnesium, as in the case of the quartz crystal, and then lapped down in a special jig to the required frequency. There was considerable improvement over quartz, but the results were still inadequate.

The results are shown in Fig. 6. From the rise time of the delayed pulse, the estimated response is seen to be somewhat greater than 1.2 mc. This is not considered adequate except for fairly wide pulses.

It was apparent that the bandwidth obtained was much less than that predictable using existing theories—both in the case of quartz and ADP crystals. While there is good reason to question the adequacy of the existing theories describing the bandwidth of loaded piezoelectric crystals when the loading is as heavy as occurs in delay lines,* it was also felt that the effectiveness of the cement bond might be a limiting factor in the obtainable bandwidth.

Mason and McSkimin[6] show that slippage due to poor bonding between the crystal and delay line can be considered as a shunt capacitance across the delay line. In the equivalent circuit they use for illustration it is obvious how improper bonding limits the bandwidth of a delay line. Since a wide bandwidth is required in the storage of narrow pulses it became evident that radical changes would have to be made in order to remove the limitations of solid delay lines using cemented crystals. Efforts made in this direction resulted in the development of a pressure mounted crystal with which control of the bonding between the crystal and the delay line is secured by varying the pressure applied to the crystal through a pressure block. This pressure block has the additional function of absorbing spurious reflections. A further result of the development of pressure-mounted crystals was extreme ruggedness and resistance to changes due to elevated temperatures.

Figure 7 shows the possible design of a pressure-mounted crystal which, while mechanically simpler than designs actually used, indi-

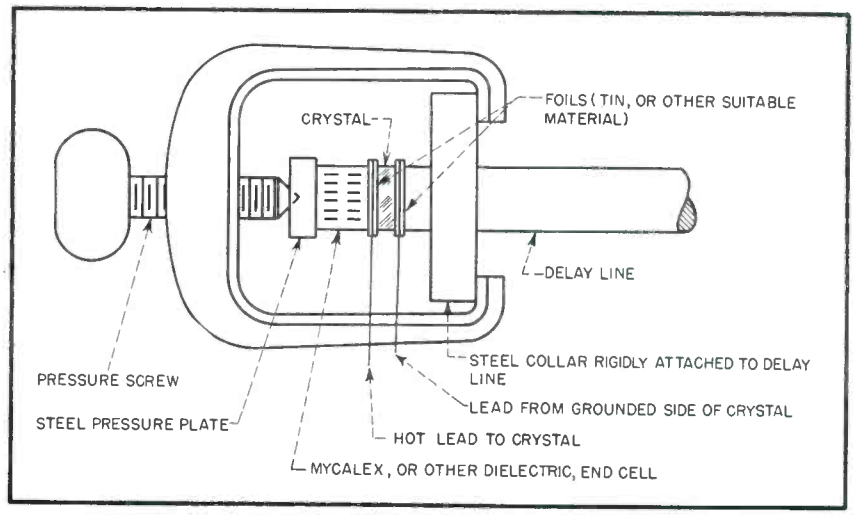

FIG. 7—Improved method of pressure-mounting a quartz crystal to a solid delay line

* Swann[5] shows that the acoustic output is theoretically a nonlinear function of applied emf, and that the relative prominence of harmonics increases with acoustic loading.

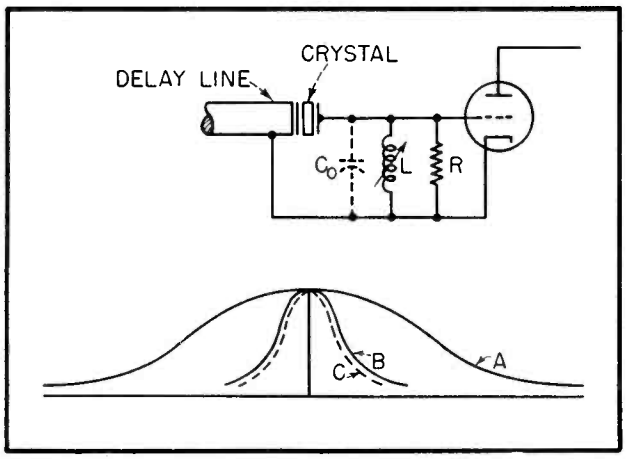

FIG. 8—Output circuit and characteristic curves for a delay line using conventional electrodes

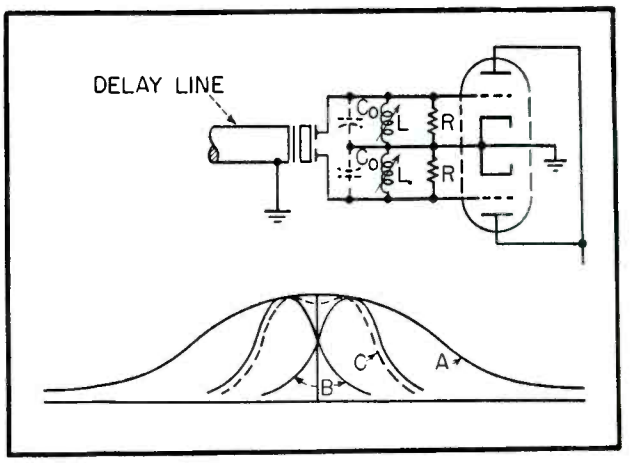

FIG. 9 — Divided-electrode output circuit and delay-line characteristics

cates clearly the function of the various parts. Using pressure-mounting methods similar to that illustrated, it was found that the acoustic response of the delay line was as great as 62.5 percent. This measurement was made using r-f modulated by 400 cycles and tuning out the shunt crystal capacitance as the r-f frequency was varied. This bandwidth was considerably greater than could be obtained in practice due to limitations imposed by the purely electrical characteristics of the delay line.

The receiving end of a delay line with the necessary attached circuit elements is shown in Fig. 8. Shunt capacitance of the crystal and any necessary stray capacitance is denoted by C_0. A tuning coil L is used to tune out C_0 at the carrier frequency used. The resistance R is used to broaden the frequency response of L and C_0 in parallel. In practice, R cannot usually be made much smaller than 500 ohms.

In Fig. 8, curve A typifies the acoustic response of the delay line-crystal combination, B the frequency response of the parallel C_0, L, and R combination and curve C typifies the overall frequency response of the delay line in conjunction with the necessary electrical circuit elements. Although these curves are not drawn to scale, they show that with clamped crystals the overall bandwidth is now limited by the electrical circuits that must be used at the terminations of the line.

An arrangement used to broaden the overall frequency response of a delay line is indicated in Fig. 9. It will be noted that the hot electrode of the crystal is now divided and that each division is separately tuned and damped. In the illustration the signals applied to the two grids of the tube are mixed electronically and the amplified resultant appears at the plates of the tube. This output is depicted by curve C in Fig. 9. Curve A is the same as that in Fig. 8 and the two curves B are the responses appearing at the two grids of the mixer. In practice, as many as four subdivisions of the hot electrode of the crystal have been used. Overall responses curresponding to curve C of Fig. 9 and as wide as 4 mc have been attained working at a carrier frequency of 10 mc, using two subdivisions of the hot electrode. Circuit arrangements similar to those in Fig. 8 and 9 are used at the input of delay lines. By careful use of this method the overall bandwidth of the delay line may be made to approach its acoustical response.

Acknowledgement

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Modern Breadboard Chassis

Components and tubes for experimental circuits are mounted and wired in less than half the usual time by employing a novel arrangement of socket holes, bus bars, special spring contacts and flexible leads

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TESTED in more than a dozen laboratories, the chassis system to be described has proved highly successful. Its convenience and versatility will appeal to the electronic engineer as well as the technician, teacher, or researcher whose work involves the temporary or experimental assembly of electrical circuits.

The design of the chassis combines the best features of older breadboard designs with several important innovations that contribute materially to the convenience and ease of assembly of experimental circuits. Tube sockets are mounted so that the terminals are accessible for easy wiring. Bus bars, tie-points, the shelf-like base of the chassis, and a vertical panel with holes of several sizes provide means for mounting various types of electronic components, while the general shape of the chassis permits simple, compact wiring.

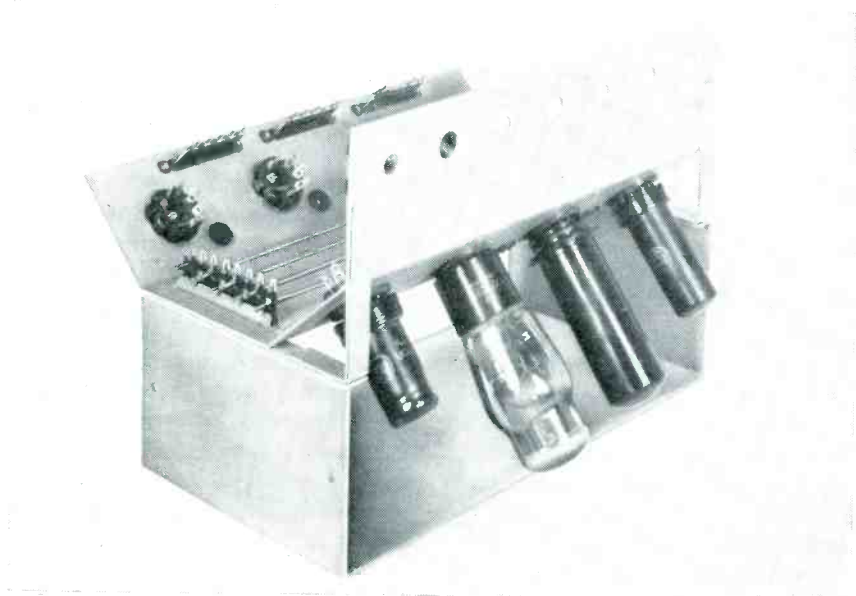
Pins on the ends of the bus bars and on some of the tie points fit the sockets on flexible leads so that the leads can be used for connecting circuits on the chassis to external equipment. Although the chassis and leads have been designed to be used together, they may also be used independently. The leads are particularly useful for making the temporary hookups frequently required around the laboratory.

The leads are flexible, insulated conductors of assorted lengths, with socket-like terminals at both ends which can engage pins $\frac{3}{32}$ inch in diameter—similar to those used on some types of vacuum-tube bases. Such pins form an integral part of various kinds of terminal fittings such as lugs, clips, and probes, which can be plugged into the ends of the leads. This system eliminates both the waste of material associated with the use of new wire for every temporary hookup, and the waste of time entailed in trying to re-use old hookup wire from the tangled pile in which it invariably collects.

A typical lead is shown in Fig. 1. The sockets at the ends of the leads are covered with insulating plastic sleeves to reduce the possibility of accidental contact with metallic parts of the sockets and lead. A lead socket with its insulating sleeve is only slightly larger in diameter than the rubber covered wire used for the leads; yet, despite its small size, it gives a firm electrical connection between the lead and an inserted pin. The connections will carry more than two amperes without overheating.

Special Connectors

Some frequently used types of terminal fittings and connectors are shown in Fig. 2. The fittings include banana plugs, pin plugs, alligator clips, battery clips, test probes, spade lugs, grid cap clips, Fahnestock clips and snap connectors. Short lengths of $\frac{3}{32}$-inch-diameter brass rod with slightly rounded ends make very versatile connectors. A $\frac{3}{8}$-inch length of such rod is useful for joining the end of one



Chassis for assembly of experimental and temporary electronic circuits

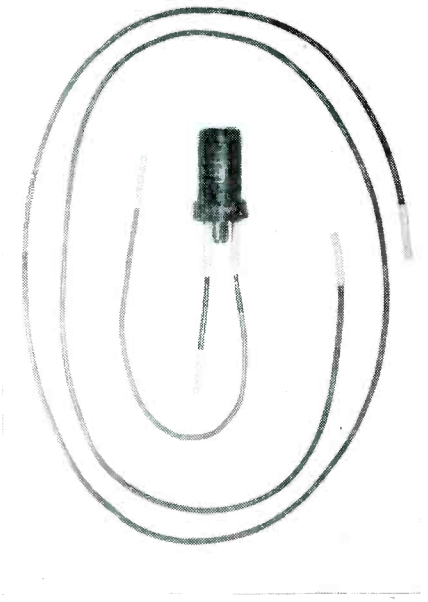


FIG. 1—Wire leads are terminated in spring sockets which grip tube pins

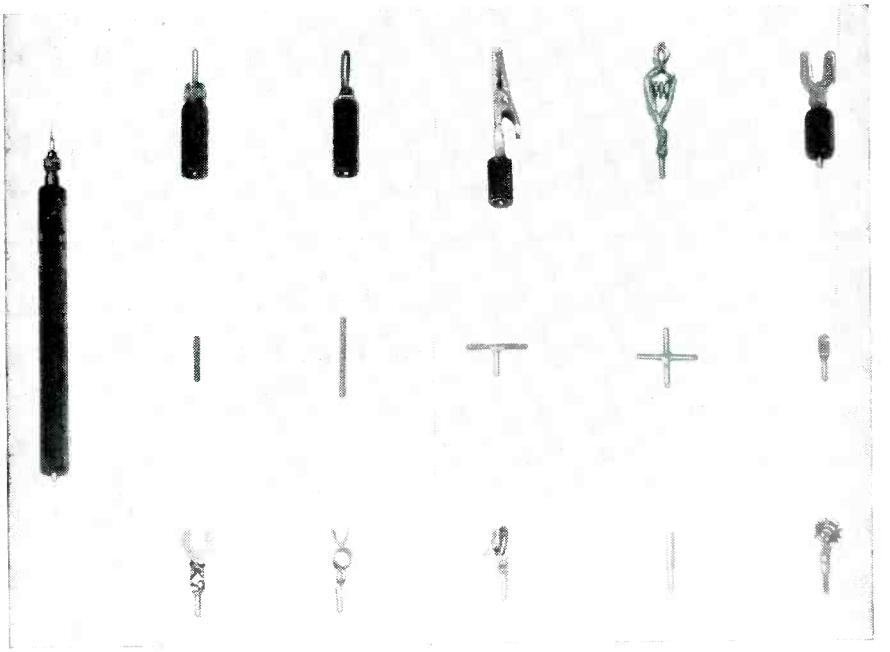


FIG. 2—All fittings and connectors have pins that fit the sockets on wire leads. The lug at right of the cross connector is slotted to fit a wire

lead to another. A similar rod slightly more than an inch long may be used either straight or appropriately bent to make connections to many types of terminal strips or binding screw terminals. Such a rod, in conjunction with one type of commonly used binding post having a hole in the stud, permits the connection of leads on both sides.

Three or more leads can be connected together by use of tees or crosses, both of which are shown in Fig. 2. One very useful stub connector shown has a pin at one end and is flattened and tinned at its other end so that it may be soldered to any point of a circuit where it is desired to connect a lead. A slot in the flattened part facilitates soldering of the stub to wires and to irregular surfaces. These stubs are particularly useful where other types of terminal fittings are either too bulky or too insecure.

Chassis Details

The breadboard chassis is shown in Fig. 3. Space is provided for eight tube sockets. Although it is not usually convenient to mount as many as eight vacuum tubes within the space of a single chassis, it is desirable to have extra sockets available for mounting components of the plug-in type. The growing list of components which mount in the ordinary octal sockets includes capacitors, crystals, transformers, relays and vibrators.

The breadboard design anticipates that most circuits assembled on it will have soldered connections. However, connections between the breadboard and external equipment, such as batteries and meters, are most conveniently made by means of the flexible leads which can be plugged onto the pins provided on the chassis for this purpose.

When a breadboard is not in use the leads are easily pulled off so that there are no dangling wires. This feature is especially appreciated when the chassis is used for circuits of a semipermanent nature, and has to be kept on a shelf for extended periods.

The vertical panel of the chassis has $\frac{3}{8}$-inch and $\frac{1}{2}$-inch holes for mounting components such as switches, rheostats, potentiometers, jacks and variable capacitors. The knobs and dials associated with these components appear near the top of the chassis where they are easy to adjust and read.

Mounting the vacuum tubes at an angle, instead of vertically, has important advantages. The chassis height required to accommodate tubes of a given size is reduced, and almost the whole base of the chassis is made available as a shelf for mounting heavy or bulky components such as batteries or transformers. Furthermore, the angular arrangement of the panels makes wiring more compact and easier to install. Connections to components placed on the base of the chassis or connections to grid cap terminals on the tubes may be carried through rubber-grommetted holes.

Small components usually need no support on a breadboard other than that provided by their leads, and they can generally be bridged directly between terminals of the larger components, or bridged between terminals and bus bars. When this is impractical, the six terminal strips along each side of the chassis may be used to support these small components. There are twenty-four additional tie-points on the strips supporting the bus bars; eight of these have pins for connection with the leads and twelve connect to the bus bars.

Grooved Bus Bars

The bus bars are generally used for those parts of a circuit which represent the juncture of many elements, like ground or B leads. By insuring that the wires connected to them will all be at nearly the same potential, bus bars reduce unwanted interactions between different parts of a circuit. Poor grounds, a constant source of trouble for the experimenter, are almost completely eliminated.

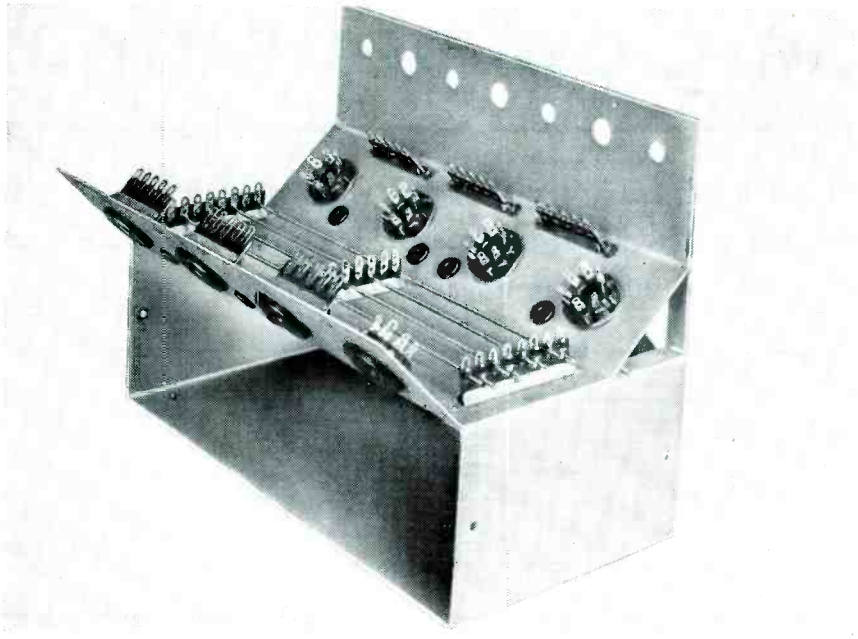


FIG. 3—This layout of wiring points, tube sockets and slotted bus bars permits ready access when circuit changes are contemplated

The bus bars have pins at their ends to which the leads may be plugged. Another important innovation is a shallow groove along the top of each bar. The grooves run nearly the full length of the bars, stopping just short of the pins formed by the ends. The bars are tinned and the grooves are partly filled with solder so that wires to be attached to the bars need only be tinned, laid in the groove, and touched with a soldering iron. Removal of wires from the bars is just as easy as their attachment.

The four bus bars on the chassis are supported about one-quarter inch above it by three insulating strips. Two of these strips, one at each end of the chassis, also support four short pins which can be used with the leads for making external connections to circuits on the chassis. Connections between the pins and equipment on the chassis are made by means of metal lugs which also serve to secure the pins to the insulating strips. These pins, together with the pins on the ends of the bus bars, provide for connection of twelve different external leads. Additional pins for plugging on external leads may be provided, if necessary, by inserting stub connectors at appropriate points on the chassis.

Two or more chassis may be bolted end to end when required for circuits that have more tubes or components than can be mounted on a single chassis. This gives a rigid combination which is effectively the same as a single large chassis. Short jumpers may be used to join the bus bars into conductors running the whole length of the combination.

In building up models of complex circuits, it is frequently advantageous to use a separate chassis for each block or major subdivision of the system. When the chassis are used in this way it is desirable to use the flexible leads for interconnecting them, since the different parts of the circuit can then be easily disconnected and isolated for individual testing.

The chassis has electrical characteristics superior to most breadboards. It provides electrical shielding which is usually sufficient to permit operation of circuits at moderately low levels without appreciable pickup from external fields. With suitable precautions as to arrangement of wiring, the chassis can usually be used at any frequency handled by ordinary receiving tubes.

The chassis is well adapted to instructional uses. Some types of shallow wafer sockets permit the pins of octal tubes to protrude far enough so that the flexible leads can be plugged directly to them. Using sockets of this type, and stub connectors soldered to the terminals of other components mounted on the chassis, it is possible to hook up even complex circuits entirely by means of the flexible leads, without the use of a soldering iron.

In most laboratories, it is frequently necessary to build up amplifiers, oscillators, or test equipment of various types for extended but not permanent use. The chassis described is ideally suited to this type of service. The compact arrangement of the chassis permits it to be handled and stored conveniently, and the plugin system of leads permits the chassis to be easily connected to, or disconnected from, associated apparatus.

The flexible leads should be used for all external connections to the chassis; that is, the leads should be used for all connections between the chassis and equipment which can not be mounted directly on it. It is also advantageous to use the leads for making minor temporary or experimental changes in a circuit already on the breadboard. Between twenty and fifty leads in an assortment of lengths ranging from three inches to three feet will be adequate for the needs of the average worker.

Experience has indicated that a circuit can be assembled on the chassis in from one-quarter to one-half of the time required to assemble the same circuit without the use of the chassis.

Breadboard chassis of this type have been in use at the Laboratory for nearly two years. They have proved themselves in many types of applications ranging from relatively simple circuits having one or two tubes, to fairly complex circuits involving more than fifty tubes. Those accustomed to using the chassis regard them as indispensable.

The chassis includes the ideas of many members of the Naval Ordnance Laboratory staff. Particularly significant contributions were made by C. E. Kelly, L. M. Robertson, G. White, R. J. Wylde and T. F. Johnston. Many valuable suggestions regarding applications and methods of using the equipment have been made by Stanley F. Reed of Uni-Products, Inc., who also aided in preparation of this article.

Cathode-Compensated

In this concluding installment, the input admittance of the compensated amplifier is derived theoretically and the experimental verification described. The performance characteristics of this and other video amplifiers are compared

Part II

By

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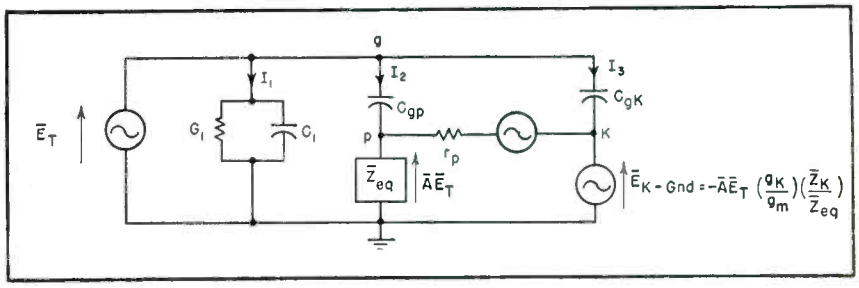

FIG. 11—Equivalent amplifier input circuit for admittance calculations

AN investigation of the factors affecting the input admittance in amplifiers is very important since the input admittance determines to a large extent the loading on the preceding stage. In order to make this investigation, a fictitious test voltage $\bar{E}_T$ is applied in the input circuit of an amplifier such as shown in Fig. 1B (Part I). The resulting flow of current from $\bar{E}_T$ determines the input admittance of the amplifier. As shown in Fig. 11 this current flows through three distinct paths, indicated at I_1, I_2 and I_3.

The current I_1 includes all of the currents except those specifically flowing through C_{gp} and C_{gk}. The conductance G_i, the intrinsic input conductance, would effectively be that which would be obtained with a cold tube in the socket. The capacitance C_i, which will be called the intrinsic input capacitance, is not as easily defined or measured but includes the input lead to ground capacitance, the grid to screen capacitance, and the grid to suppressor capacitance. Of course, the intrinsic input conductance and capacitance are modified by the fact that they include distributed as well as lumped effects. The distributed parameters must be taken into account in the analysis.

The magnitude and phase of the current $\bar{I}_2$ will depend on the amplification and phase shift of the amplifier and the magnitude of C_{gp}. This is the ordinary Miller effect which is described in most texts on communications under the heading of input admittance. The input conductance and input capacitance due to the grid-plate capacitance are

$$G_{i_{gp}} = \omega C_{gp} A \sin \theta \qquad (32)$$

and

$$C_{i_{gp}} = C_{gp}(1 - A \cos \theta) \qquad (33)$$

In this case A represents the magnitude of the voltage amplification and θ the phase shift of the plate to ground voltage with respect to the grid to ground voltage. For an uncompensated amplifier with infinite cathode bypass, θ will range from 90 to 180 degrees for capacitive loads and from 180 to 270 degrees for inductive loads. Thus it is seen that capacitive loads tend to produce positive input conductances while inductive loads tend to produce negative input conductances. In the case of the amplifier using cathode compensation, the angle θ can fall outside the limits specified above, but otherwise the two equations apply.

The magnitude and phase of the current $\bar{I}_3$ will depend on the magnitude of C_{gK} and on the vector cathode to ground voltage $\bar{E}_{K-Gnd}$. If the values of $\bar{A}_2$, $\bar{Z}_K$, and $\bar{Z}_{eq}$ from Eq. 25, 16 and 24 respectively are substituted in the expression for $\bar{E}_{K-Gnd}$, the following expression results:

$$\bar{E}_{K-Gnd} = -A\left(\frac{g_K}{g_m}\right)\left(\frac{\bar{Z}_K}{\bar{Z}_{eq}}\right)\bar{E}_T$$

$$= -\left[\frac{-gm(1+g_KR_K)R_{eq1}}{(1+g_KR_K)+ja\frac{\omega}{\omega_0}}\right] \times \left[\frac{1+ja\frac{\omega}{\omega_0}}{1+j(1+g_KR_K)\frac{\omega}{\omega_0}}\right]\frac{g_K}{g_m} \times \frac{\left[\frac{R_K}{1+ja\frac{\omega}{\omega_0}}\right]\bar{E}_T}{\left[\frac{(1+g_KR_K)R_{eq1}}{1+j(1+g_KR_K)\frac{\omega}{\omega_0}}\right]}$$

$$= \frac{+g_KR_K\bar{E}_T}{(1+g_KR_K)+ja\frac{\omega}{\omega_0}} \qquad (34)$$

If the cathode compensation circuit of Fig. 1C is used then the same equation holds with the exception that a_{eq} from Eq. 31 (Part I) should be used in place of a. Then

$$\bar{E}_{K-Gnd} = \frac{g_KR_K\bar{E}_T}{(1+g_KR_K)+j\,a_{eq}\frac{\omega}{\omega_0}} \qquad (35)$$

A loop equation can now be written for the outside loop so that

$$\bar{E}_T - \frac{g_KR_K\bar{E}_T}{(1+g_KR_K)+ja_{eq}\frac{\omega}{\omega_0}} = \bar{I}_3\left(-j\frac{1}{\omega C_{gK}}\right) \qquad (36)$$

and

$$\bar{Y}_{i_{gK}} = \frac{\bar{I}_3}{\bar{E}_T} = \frac{\omega C_{gK}(1+ja_{eq}\frac{\omega}{\omega_0})}{a_{eq}\frac{\omega}{\omega_0} - j(1+g_KR_K)} \qquad (37)$$

Video Amplification

Rationalizing,

$$\overline{Y}_{i_{gK}} = \frac{-\omega C_{gK}\, a_{eq}\frac{\omega}{\omega_0}\, g_K R_K + j\omega C_{gK}\left[\left(a_{eq}\frac{\omega}{\omega_0}\right)^2 + (1+g_K R_K)\right]}{\left(a_{eq}\frac{\omega}{\omega_0}\right)^2 + (1+g_K R_K)^2} \quad (38)$$

Therefore

$$G_{i_{gK}} = \frac{-\omega C_{gK}\left(a_{eq}\frac{\omega}{\omega_0}\right) g_K R_K}{\left(a_{eq}\frac{\omega}{\omega_0}\right)^2 + (1+g_K R_K)^2} \quad (39)$$

and

$$C_{i_{gK}} = \frac{C_{gK}\left[a_{eq}\left(\frac{\omega}{\omega_0}\right)^2 + (1+g_K R_K)\right]}{\left(a_{eq}\frac{\omega}{\omega_0}\right)^2 + (1+g_K R_K)^2} \quad (40)$$

As long as $\overline{Z}_K$ is capacitive in nature a_{eq} will be positive and the input conductance due to the grid-cathode capacitance will be negative. For values of frequency at which $\overline{Z}_K$ is inductive in nature a_{eq} becomes negative and therefore this particular input conductance will be positive.

All terms in the expression for the input capacitance due to the grid-cathode capacitance are essentially positive so that this input capacitance will always be positive but will be variable in magnitude.

The total input conductance will be the sum of the input conductances seen by the three currents and may be either positive, zero or negative depending upon the relative values involved. In order to avoid the possibility of high negative values of input conductance, which might result in oscillations, it is desirable to keep the grid-cathode capacitance as low as possible.

In a like manner the total input capacitance will be the sum of the input capacitances seen by the three currents. The input capacitance due to C_{gp} will tend to decrease with increasing frequencies. The input capacitance due to C_{gK} will be $C_{gK}/(1 + g_K R_K)$ at low frequencies, attaining a maximum of C_{gK} at f_R (when $a_{eq} = \infty$) and again decreasing to $C_{gK}/(1 + g_K R_K)$ at very high frequencies. There is a net tendency towards cancellation of the changes in these two capacitances at frequencies below f_R, although the change will be in the same direction at frequencies above f_R.

Experimental Verification

Proper experimental verification of the input admittance relations would require that the effects due to the various paths be measured individually and then combined to produce the proper total value. The only quantity that can be determined directly with any degree of accuracy is the intrinsic input conductance of the circuit. This is measured with a cold tube in the socket since in this case the C_{gp} and C_{gK} paths introduce practically pure capacitance as far as the input admittance is concerned.

A separation of C_{gp} and C_{gK} from all the other capacitances in the circuit by direct measurement would be quite difficult due to the possibility of multiple paths between the various points. It will be noticed, however, that at the frequency f_R the input conductance due to C_{gK} is equal to zero because at this frequency $a_{eq} = \infty$. The remaining input conductance must therefore be the sum of the intrinsic conductance and the conductance due to C_{gp}. Since the intrinsic conductance can be measured directly, the difference between the total input conductance and the intrinsic conductance, at this frequency, will be due solely to the C_{gp} path and therefore we can solve for C_{gp} in Eq. 32. Of course, values of A and θ in this equation must be determined in the manner shown in Table I, part I.

The input conductance due to C_{gp} can now be computed for any other suitable frequency, such as $f_R/2$, at which the input conductance due to C_{gK} is relatively prominent. If the total input conductance for this frequency is measured and the measured intrinsic and computed grid-plate input conductances are subtracted from it, the difference must be the input conductance due to C_{gK}. Using this difference and Eq. 39 the capacitance C_{gK} can be determined.

Experimental data for only two frequencies were required to determine C_{gp} and C_{gK}, but with these values and the experimental intrinsic input conductance the total input conductance can be computed

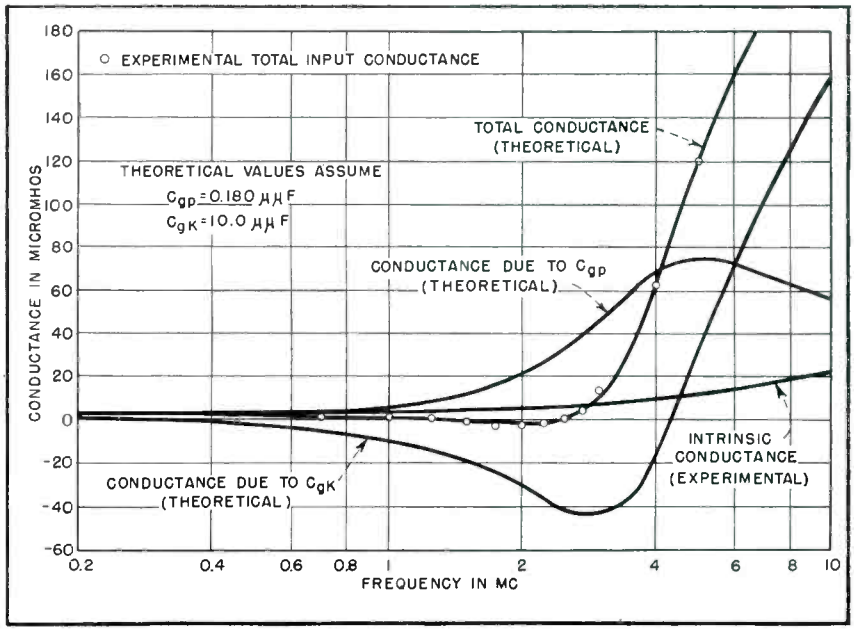

FIG. 12—Input circuit conductance for cathode-compensated amplifier

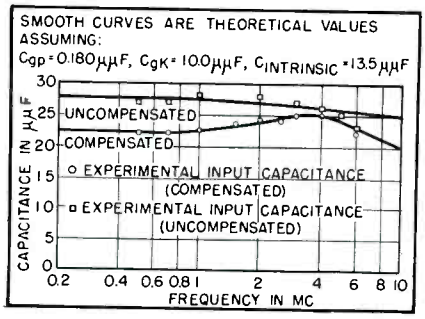

FIG. 13—Theoretical and experimental values of input capacitance

for any frequency. A measure of the accuracy of the method will be the correlation between measured and computed input conductance at frequencies other than the two used to determine C_{gp} and C_{gK}.

The curve for the intrinsic input conductance, shown in Fig. 12, was obtained experimentally. It was found to be the same for both the compensated and uncompensated amplifiers. At low values of frequency it approaches 2 micromhos which is the value of the 0.5-megohm grid leak resistor used. This conductance increases gradually with frequency, reaching approximately 24 micromhos at 10 megacycles.

By the methods described previously for the compensated amplifier, C_{gp} was found to be 0.180 $\mu\mu$f and C_{gK} was found to be 10.0 $\mu\mu$f. The two smooth curves for input conductances due to C_{gp} and C_{gK} were computed using Eq. 32 and 39 respectively, and were then combined to obtain the theoretical total input conductance curve. Experimental values of total input conductance were also determined and they are shown by the circled points on this diagram. The correlation obtained is very satisfactory and it is believed that the values determined for C_{gp} and C_{gK} are quite accurate.

The intrinsic input capacitance can be determined by measuring the total input capacitance, at any convenient frequency, and subtracting from it the sum of the input capacitances due to C_{gp} and C_{gK}. The total input capacitance can then be determined for any frequency by adding to the intrinsic input capacitance the effective input capacitances due to C_{gp} and C_{gK} at that frequency.

The smooth curves in Fig. 13 are the theoretical input capacitances expected for the amplifier, both compensated and uncompensated, and the circled and squared points are the corresponding experimental values obtained. The correlation appears to be quite satisfactory.

The value determined for the intrinsic input capacitance of the compensated amplifier was 13.5 $\mu\mu$f. The various values of capacitance determined are not believed to be typical of normal practice since the amplifier used was set up on a standard breadboard used for classroom demonstration. Resistors and capacitors were connected to Fahnestock clips and while reasonable care had been exercised in separating the grid and plate leads no attempt had been made to isolate the grid, cathode, and ground return leads. In normal practice it is doubtful that C_{gp} could be reduced appreciably but it would probably be reasonable to expect a reduction of 2 to 3 $\mu\mu$f in C_{gK} and about 4 to 5 $\mu\mu$f in the intrinsic input capacitance. The total input capacitance and conductance would also be modified correspondingly.

In Fig. 14, the theoretical input conductance computed for the uncompensated amplifier using C_{gp} = 0.180 $\mu\mu$f is slightly lower than the experimental values shown by the circled points. This discrepancy would have been eliminated if 0.10 $\mu\mu$f had been added to C_{gp} in computing the theoretical input conductance. It is entirely possible that a minor circuit rearrangement could have actually caused this change in capacitance.

The input capacitance and input conductance of the compensated amplifier do not become undesirably excessive in any region of the frequency range considered. Sample computations for some of the points in Fig. 12 and 13 are carried out in Table II.

Comparison With Other Circuits

A basis of comparison among different types of video amplifier circuits can be established on many points, the most important of which

Table II—Sample Calculations for Input Admittance of Compensated Amplifier (Data Plotted in Fig. 12 and Fig. 13)

Working Equations:

$$C_{i_{gp}} = C_{gp}(1 - A\cos\theta) \qquad G_{i_{gp}} = \omega C_{gp} A \sin\theta$$

$$C_{i_{gK}} = \frac{C_{gK}[(a_{eq}\,\omega/\omega_o)^2 + (1 + g_K R_K)^2]}{(a_{eq}\,\omega/\omega_o)^2 + (1 + g_K R_K)^2} \qquad G_{igK} = \frac{-\omega C_{gK}(a_{eq}\,\omega/\omega_o)\, g_K R_K}{(a_{eq}\,\omega/\omega_o)^2 + (1 + g_K R_K)^2}$$

$$C_i = C_{Intrinsic} + C_{i_{gp}} + C_{i_{gK}}$$

$$G_i = G_{Intrinsic} + G_{i_{gp}} + G_{i_{gK}}$$

Circuit Constants in Addition to Those in Table I:

C_{gp} = 0.180 $\mu\mu$f, C_{gK} = 10.0 $\mu\mu$f, $C_{Intrinsic}$ = 13.5 $\mu\mu$f

$A_m = 20.8/180°$

Quantity					
ω/ω_o	0.03	0.1	0.3	1.0	3.0
f (mc)	0.106	0.354	1.06	3.54	10.6
$G_{Intrinsic}$ (micromhos)	2.00	3.00	5.10	9.70	27.0
A	20.8	20.8	20.55	18.2	4.41
θ	178.41°	174.71°	164.46°	124.46°	77.80°
$A\cos\theta$	−20.8	−20.6	−19.8	−10.3	+.93
$C_{i_{gp}}$ ($\mu\mu$f)	3.92	3.89	3.74	2.04	.013
$(a_{eq}\,\omega/\omega_o)$	0.0681	0.2280	0.7230	6.600	−1.384
$(a_{eq}\,\omega/\omega_o)^2$	0.0046	0.052	0.524	43.6	1.92
$(a_{eq}\omega/\omega_o)^2+(1+g_K R_K)$	2.135	2.182	2.654	45.73	4.05
$(a_{eq}\omega/\omega_o)^2+(1+g_K R_K)^2$	4.545	4.592	5.064	48.14	6.46
$C_{i_{gK}}$ ($\mu\mu$f)	4.70	4.75	5.25	9.50	6.27
C_i ($\mu\mu$f)	22.12	22.14	22.49	25.04	19.78
$A\sin\theta$	0.576	1.92	5.51	15.00	4.31
$G_{i_{gp}}$ (micromhos)	0.069	0.769	6.59	60.1	51.7
$G_{i_{gK}}$ (micromhos)	−0.112	−1.245	−10.70	−34.4	+161.2
G_i (micromhos)	1.957	2.524	0.99	35.4	239.9

are probably: (a) cost, (b) simplicity, (c) disturbance of normal circuit relations, (d) gain, (e) frequency response, (f) time delay, (g) linearity of the output voltage-vs-input voltage characteristic and (h) input admittance relations. Cathode compensation as developed in this paper is superior to other circuits in most of these aspects and is comparable in the rest.

On a cost basis, the circuit with cathode compensation is not only less expensive than any other compensated circuit but is even less expensive than the ordinary uncompensated video amplifier. In an ordinary video amplifier a large electrolytic capacitor is used in parallel with the cathode resistor. Very often this is bypassed by a small paper or mica capacitor which takes over at the higher frequencies at which the electrolytic capacitor becomes very poor. With cathode compensation the large electrolytic capacitor is discarded, the small capacitor is made the proper size, and an inductor consisting of about ten turns of enameled wire on a quarter-inch Bakelite spool is inserted in series with the small capacitor. A counterbalancing effect might be the necessity of increasing the wattage rating of the load resistor but even this will not overcome the cost advantage of eliminating the electrolytic capacitor.

As far as simplicity is concerned, the ordinary shunt-peaking type of circuit is the only one that compares with cathode compensation. All other circuits require additional elements. In the series peaking circuits a certain division of the stray capacitance is required. If this is not available, then the theoretical curves are not reproduced. Sometimes it is necessary to insert additional capacitance in the circuit in order to obtain this proper distribution. This of course will tend to impair the available frequency response. Adding elements in the plate circuit will also tend to increase the stray capacitance present. This effect was noticed to a slight extent in the experimental case discussed but need not have been present at all if the proper value of resistance had been available.

In all other compensating circuits the impedance of the compensating elements is of the same order of magnitude as the load impedance. In the case of the inductances this results in difficulties due to self-resonance effects which are normally not taken into account. One instance in which this effect is taken into account is in the improved shunt-peaking[1] circuit. In the case of cathode compensation there is never any reason for concern over the stray capacitance of the inductors or the series inductance of the capacitors.

On the basis of gain from a certain tube for a given frequency response, cathode compensation is as good as ordinary shunt peaking

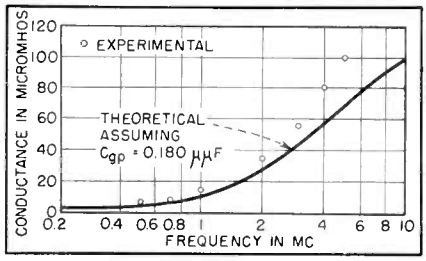

FIG. 14—Input conductance versus frequency of uncompensated amplifier

and improved shunt peaking but not quite as good as the series peaking circuits which make use of filter circuit characteristics. This however is further modified by considerations as to whether frequency response is limited by amplitude or time delay considerations. On an amplitude consideration basis the series peaking circuits probably have a slight advantage over cathode compensation but this advantage disappears if time delay is used as the criterion of frequency response.

As a matter of fact, video amplifiers intended for television applications continue to have useful output as long as the time delay variations do not become excessive. In the amplifier of Fig. 8 (part I) the variation in time delay between the valley and the peak of the curve is of the order of magnitude of 0.004 microsecond. This represents a horizontal distance which corresponds to approximately one-twentieth of the distance between line centers in a television picture. This is certainly a negligible variation in time delay. The only other circuit that even approaches this constant a time delay over such a large frequency range is the shunt peaking compensation in which the inductive reactance at f_o is equal to 35 percent of the load resistance.

On the basis of linearity of output voltage for a given frequency response, cathode compensation is superior to all other circuits in the middle-frequency region and probably as good as any of them at the high-frequency end of the characteristic.

A thorough comparison of the input admittances of the various circuits is not possible because of the lack of data on the other circuits. With cathode compensation the input capacitance is slightly lower than in the corresponding uncompensated amplifier. The input conductance has some elements that tend to make it negative and others that tend to make it positive. A judicious combination of these elements will produce practically zero input conductance over most of the operating range.

All other video amplifiers are limited in their low-frequency response to some extent by the cathode bypass capacitance used. In the case of cathode compensation, the circuit behaves as though the original uncompensated amplifier had infinite cathode bypass capacitance. Of course the screen bypass and coupling capacitors still have the same effect as they have in any circuit.

There is a possibility that the introduction of additional elements in the plate circuit might make the linearity in the high-frequency region comparable to that obtained at middle frequencies. This possibility has not been investigated up to the present time.

The author wishes to acknowledge the opportunity that he has had for discussing the problems involved in this development with his colleagues and especially with Professor W. C. Osterbrock. He would also like to thank the electrical engineering class of '48 of the University of Cincinnati, for the time they devoted to calculations in his behalf in the early stages of the project.

REFERENCE

(1) A. B. Bereskin, Improved High Frequency Compensation for Wide Band Amplifiers, *Proc. IRE*, p 608, Oct. 1944.

Portable High-Voltage POWER SUPPLY

Weighing less than 35 pounds, this rectified-60-cycle unit provides continuously adjustable voltage from 0 to 30 kv at currents as high as 500 μa, with reversible polarity and approximately 5-percent ripple at full load. Protective circuits insure long life of components and operating personnel

By VICTOR WOUK

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A GROWING NEED has been felt in many fields of research and engineering for a compact, portable, low-current high-voltage d-c power supply, continuously adjustable from 0 to 30,000 volts.

In home television receivers, voltages up to 30 kv are required for the accelerating potential of the cathode-ray tube. In nuclear physics, dust precipitation, some fields of medical testing, the new field of xerography[1], experimentation on electrostatic-charge dissipation and electrostatic painting high voltages at low currents are needed. In most of these applications, the maximum current drain required from the power supply is 1 ma. Usual maximum current requirements are of the order of 500 microamperes. Where it is desired to test puncture strength on flashover ratings of insulating materials or circuit components, considerably smaller currents are normally satisfactory.

A portable, reversible-polarity power supply capable of providing these voltages and currents, employing rectified 60-cycle power, has been made feasible by the development of new insulating materials, new rectifiers for television applications and new compact circuit components with high-voltage ratings. This article describes the design and construction of such a power supply.

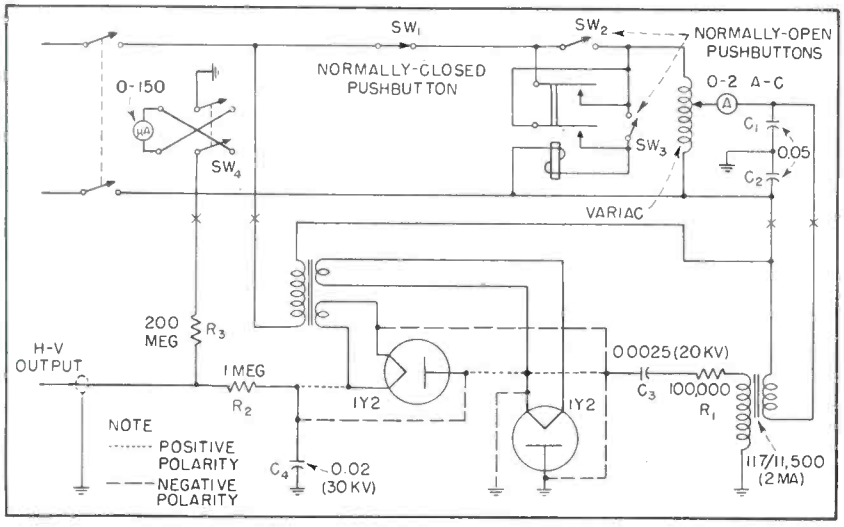


FIG. 1—Circuit diagram of portable high-voltage power supply. Switches 1, 2 and 3 are momentary switches. Control panel may be removed from power supply and cabled at points marked with x's

Desirable Properties

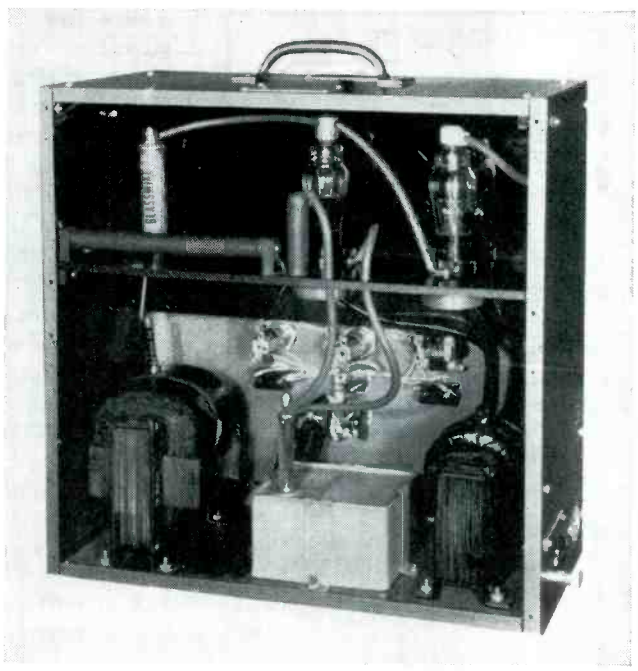
Desirable features in a general-purpose high-voltage power supply include the following: (1) Continuous adjustability, (2) compactness and light weight, (3) reversible high-voltage polarity (In television work, positive high voltage with respect to ground is required, while in dust precipitation work the opposite is often the case. In many nuclear physics studies, both polarities are often required during the course of a series of tests), (4) moderately accurate output-voltage indication, (5) safety to operating personnel whether skilled or unskilled, (6) reliability (wide margins against component failure), (7) minimum corona compatible with general low cost and compactness and (8) low ripple (less than 5 percent being desirable for television and nuclear physics work).

Available Circuits

In general, high-voltage power supplies fall into four common categories: r-f[2], fly-back, pulsed[3], and rectified 60-cycle. The fly-back type, when considered as an independent supply, becomes a pulsed power supply.

In planning the design of a supply incorporating the features listed above, r-f and pulsed types were discarded for several reasons. If the supply is to be continuously adjustable, the filaments of the rectifiers cannot be energized from the

Front view of 30-kv portable power supply. Control panel may be removed and cabled to power supply for remote operation



Cover-removed rear view of power supply, showing physical placement of components

same source that supplies the high-voltage power, as in usual r-f and pulsed types. When filaments are so energized, the filament voltage decreases with lowered output voltage, reducing the cathode's emissivity; when the cathodes are cold the output voltage varies greatly with small changes in heater voltage.

Further disadvantages of this type of operation are the long time lags between successive equilibrium states when the output voltage is changed slightly at low output voltage and shortened rectifier life due to high forward tube drops when filament voltage is low and normally-rated currents are being drawn. Separate filament-energizing transformers must be of the low-capacitance type in these types of supplies, otherwise excessive capacitance loading of the high-voltage generator will occur. A low-capacitance transformer of suitable voltage rating is bulky, and if two filaments are at high r-f voltage the capacitance between filament windings must be low as well as the capacitance to ground. Such a transformer would be bulky and expensive.

A straightforward 60-cps rectifier is less complicated, and hence more reliable, since it eliminates the two stages of low-voltage rectification and high-frequency generation found in r-f and pulsed types of supplies. It was also in the interest of reliability through less complication that separate r-f or pulsed-filament energizing was not considered for use with an r-f or pulsed power supply.

Finally, and oddly enough, a 0 to 30-kv rectified 60-cps supply is lighter and less bulky than an r-f or pulsed type of similar rating. This is so because of the weight of filter chokes and plate and filament transformers. True, the high-voltage r-f coil or pulsing coil is considerably lighter than the high-voltage 60-cps transformer, and the high-voltage filter capacitors are of much lower capacitance, and hence less weight, in the r-f or pulsed units. However, these weight savings are considerably overbalanced by the plate B+ supply requirements.

It must be remembered that the r-f and pulsed power supplies are inherently low-efficiency devices; a 30-percent efficiency in conversion of B+ to high voltage is excellent. Thus, for 30 kv at 500 μa, an r-f or pulsed supply operating at 350 volts B+ will require at least 150 ma, well filtered. Such a B+ supply, with associated filament transformers, is heavier than the combined weights of a 60-cps 12-kv transformer, and a 0.02 μf, 30-kv polyethylene-dielectric capacitor.

As to bulk, an r-f or pulsed power supply for 30 kv requires more stages of voltage multiplication than a rectified 60-cps system. An 11-kv rms transformer yields a peak voltage greater than 15 kv, producing 30 kv after doubling. However, r-f and pulsed supplies using ordinarily available tubes and circuit components can produce not much more than 10 kv peak at the high-voltage generator, requiring three stages of multiplication.

The 10-kv value is the limiting factor on r-f power supplies because of corona on the high-voltage coil. Since a high-Q r-f coil is required in an r-f power supply, thin wire is used in winding the high-voltage pies. The thin wires are sources of heavy corona above 10 kv.

In pulsed supplies, the 10-kv figure is determined by the peak plate voltage rating of the driver tube[3]. A 6BG6G can handle no more than 6 kv reliably. By means of autotransformer action of the peaking coil, this can be stepped up, but analysis[3] shows that a step-up much more than 50 percent is inefficient.

Because of the above-mentioned factors, 60-cycle power was chosen

the output is set for high voltage, and there is a short circuit or flashover in the external load.

Resistor R_3 is rated at 40 kv by the manufacturer. It has been found that these are linear up to about 30 kv, permitting an initial full-scale meter indication accuracy of about 3 percent. The resistor warms up perceptibly, introducing an error as large as 2 percent above 30 kv. This is compensated for by calibrating each meter to read slightly low when cold. The reading is then slightly high when warm. (The resistors have negative temperature and voltage coefficients.)

Resistor R_1 is included to lengthen tube life by limiting capacitor-charging current surges when the output control is set for high voltage, and power is suddenly turned on.

Corona

To minimize corona, sharp points at high voltage are avoided. Where sharp points are unavoidable, these regions are surrounded by anti-corona shields. This is particularly the case around the rectifiers' cathodes.

Where other connections are made at high voltage, rounded brass caps are used. These are employed on the two capacitors, and can be seen in Fig. 3G. All 30-kv points are kept at least one inch from the nearest ground through air, or two inches if flashover can occur across a surface.

Resistors R_2 and R_3 are wax-dipped to minimize corona from the sharp edges of the conducting material. This wax coating also prevents minor knocks from chipping the thin conducting deposit on the ceramic form and developing an open circuit in the resistor.

Regulation

Although good regulation is usually desirable in any power supply, it is not attained readily in this type of high-voltage-generating circuit without increasing the weight, size and circuit complexity considerably. Since in many general laboratory and test applications of the power supply, such as voltage-breakdown testing, cathode-ray-tube life testing, and dust precipitation, good regulation is not necessary, no automatic regulation was incorporated into the unit.

The regulation of the power supply is indicated in Fig. 4. The load lines for various fixed Variac positions are shown. It can be seen from line A, the curve for maximum Variac setting with a 1 to 1 Variac ratio, that at no load slightly over 30 kv are available. If the Variac is set to give 135 volts output, then the load line is B, and over 500 μa are available at 30 kv, or 1 ma at about 27 kv. Due to the fact that the output capacitor C_2 is rated closely at 30 kv, the curve B is not extended above the 30-kv line; curve B indicates use of the power supply to yield relatively heavy currents in the 20 to 30-kv range, and not use to provide more than 30 kv.

From Fig. 4 it is further seen that the output voltage drops off linearly with load current for fixed Variac settings. The rate of terminal-voltage drop-off is, as theoretical considerations indicate, independent of the input voltage—that is, the load lines are all parallel, meaning that the internal resistance of the power supply is independent of the input voltage and load resistance. From the slope of the lines, it can readily be calculated that the internal resistance is approximately 8 megohms.

Extrapolation of the load line A indicates that the steady-state short-circuit current should be 4 ma. Measurements reveal this to be the case. As previously discussed, this value is well below the let-go value of current.

Actual ripple measurements, made under typical operating conditions, show close adherence to the ripple values as calculated by standard methods for the type of filter used.

The minimum ripple percentage is about 0.4 percent, due to the constant presence of the voltmeter load represented by R_3 in Fig. 1.

As typical values, the ripple present when the power supply is used on a projection television tube requiring 300 μa at 25 kv, or a load of 83 megohms, is 1.2 percent. This is satisfactory for all normal projection television applications. For a direct-viewing tube of 7 kv and 400 μa, or a load of 17.5 megohms, the ripple is approximately 5 percent; this is just about the limit of acceptability for high-quality picture appearance. It is very good for routine test purposes.

Additional Features

In order to make the power supply quite flexible and useful for many applications, several features are included in the control circuits that are not ordinarily associated with a high-voltage power supply.

In many applications, it is desired to control the high voltage remotely. Therefore, the control panel has been made removable by means of a cable connector set. The points in the wires where the various breaks occur are indicated by X's in the diagram. The fuse, switches, pilot lights, pushbuttons, relay, Variac and meters are located on the control panel. All other components are located either in or on the cabinet that houses the high-voltage components.

Since some corona is present in the secondary side of the high-voltage transformer, a small amount of r-f noise is fed back into the mains. To minimize the r-f effects, two capacitors, C_1 and C_2 (Fig. 1) are employed as a high-frequency filter. At maximum output voltage, the r-f radiated away and fed back into the mains does not affect reception on a radio plugged into a utility socket on the control panel.

The entire unit is 16 inches wide x 16 inches high x 8 inches deep and is provided with a suitable carrying handle. Total weight is 35 pounds.

Because of the wide variation of types of connector used for different applications at high voltage, no special attempt has been made to provide a high-voltage connector of particular design. Instead, a large-size battery clip with rubber shield is provided. This proves satisfactory for all applications except those in which corona must be reduced to a minimum.

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(1) Xerography, a Dry Printing Process, *Electrical Engineering*, 68, p 46, Jan. 1949.

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(3) G. J. Siezen and F. Kerkhof, Pulse-Type High-Voltage Supply, *PROC. IRE*. 36, p 401, Mar. 1948.

(4) D. L. Waidelich and C. H. Gleason, The Half-Wave Voltage-Doubling Circuit, *PROC. IRE*. 30, p 535, Dec. 1942.

(5) C. F. Dalziel, Effects of Electric Currents in Man, *Electrical Engineering*, 60, p 63, Feb. 1941.

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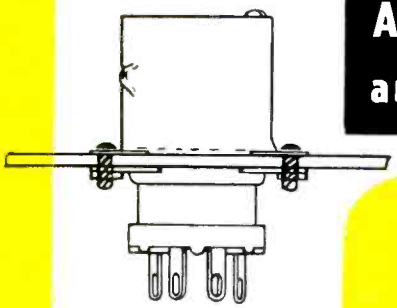

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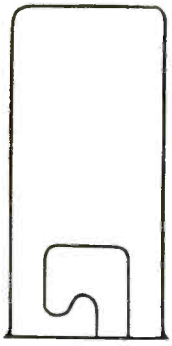

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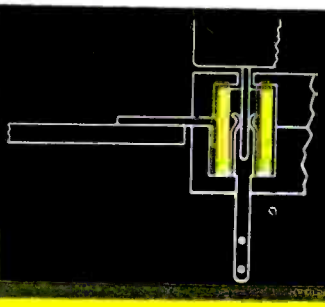

This schematic diagram shows the basic design principle. The silvered ceramic condensers are shown in yellow. Note that the condenser completely surrounds the tube pin, and that specially designed tube prong terminals are used.

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ATTENUATION
Between Paraboloid Antennas

Antenna diameters, distance and wavelength figures are simply converted to gain and loss in db with the table. Algebraic addition shows attenuation

By E. DYKE
Communication and Electronics Div.
Motorola Inc.
Chicago, Ill.

THE TABLE provides a convenient means of calculating line-of-sight space attenuation between two paraboloid antennas, but can be used for other shapes and designs if the effective diameter is utilized.

The left-hand column represents the physical quantities shown in the figure and listed below. The corresponding right-hand numerals are equivalent decibel values. The table can be extended since the right column is 20 $\log_{10}$ of the left column. Equation 1 shows the algebraic signs to be applied to the db values. The 93-db constant is a value representative of good design practice.

Space attenuation, $P_r/P_t = -93 - S - \lambda + D_r + D_t$ decibels (1)

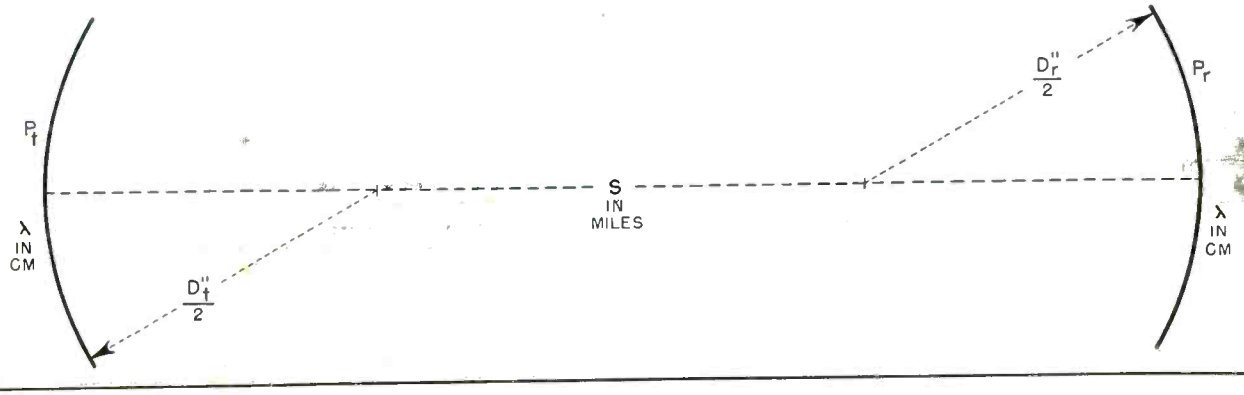
When D is antenna diameter in inches
S is separation between antennas in miles
λ is wavelength in centimeters
P_r is power received
P_t is power transmitted

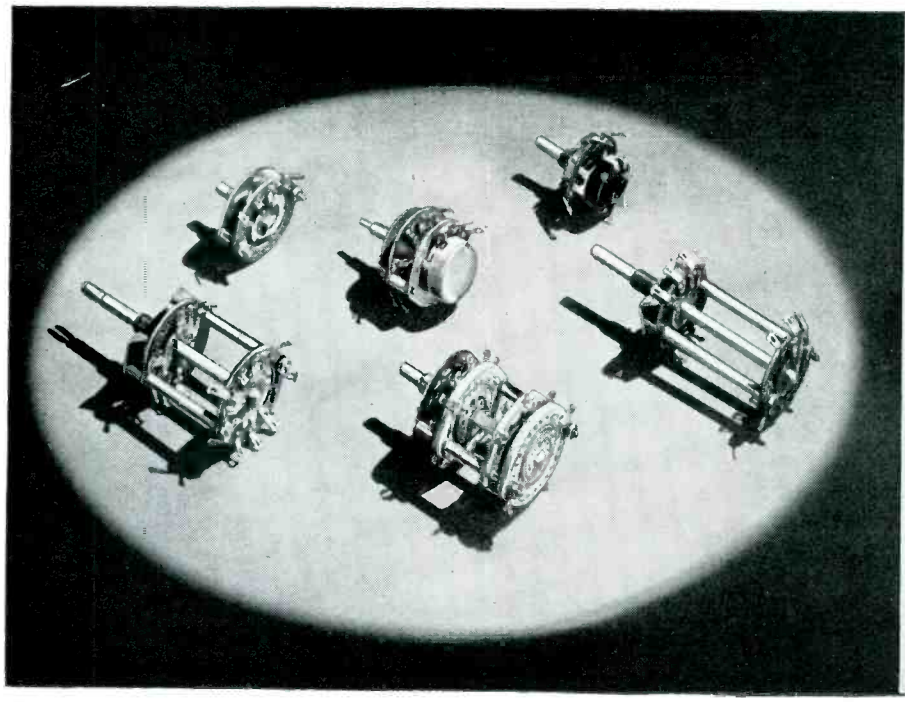
Physical Quantities	Gain or Loss in Db
0.1	−20.0
0.5	− 6.0
1.0	0.0
2	+ 6.0
3	+ 9.5
4	12.0
5	14.0
6	15.6
7	16.9
8	18.0
9	19.1
10	20.0
12	21.6
14	22.9
16	24.0
18	25.1
20	26.0
22	26.8
24	27.6
26	28.3
30	29.5
35	30.9
40	32.0
45	33.1
48	33.6
50	34
60	35.6
70	36.9
72	37.2
80	38.1
90	39.1
100	40
120	41.6
140	42.9
160	44.1
180	45.1
200	46.0
250	48.0
300	49.5
400	52.0
500	54.0

Example:

Factor	Dimension	Db
Constant	....	−93
Distance (S)	50 miles	−34
Wavelength (λ)	4.5 cm	+13
Rec ant. (D_r)	40 in.	+32
Trans ant. (D_t)	40 in.	+32
Attenuation		−76

Received power P_r can be obtained in dbm by adding the value of transmitted power P_t in dbm to the db value of the attenuation.





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- Six rotor supports on the stator—insure accurate alignment.
- Brass rotor shoes, heavily silver-plated—insure low contact resistance.
- All shoes held flat and securely to phenolic rotor by rivets—prevents stubbing—insures smooth rotation—*minimum of noise in critical circuits.*

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Send for the Mallory Engineering Data Sheets on the RS series. They contain complete specifications for available circuit combinations with respective terminal locations, dimensional drawings — everything the engineer needs.

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Edited by VIN ZELUFF

Electronic Instruments In Large Aircraft

BY JOSEPH ALBIN
New York, N. Y.

IN THE DAYS when the still-popular DC-3 was the ruler of the commercial airways, and later, when its big brother, the DC-4 took over on some of the longer runs, the instrument maintenance problem was one chiefly of mechanics, pneumatics and hydraulics. Lately, however, the popularity of the DC-6 with its preponderance of electronic instruments has caused a noticeable change in the maintenance scene.

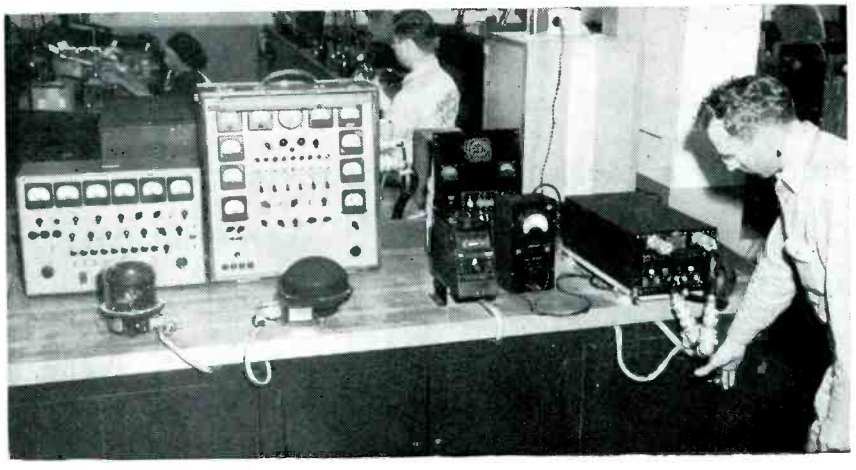
The American Airlines maintenance depot at Tulsa, Oklahoma, which had been fully equipped, both in equipment and personnel, for servicing DC-3's and DC-4's, found itself lacking in the ability to repair and maintain the numerous electronic instruments in the DC-6's. A completely new air-conditioned electronic laboratory has been installed and manned, chiefly by former radio personnel.

The accompanying photographs show several examples of the resulting gear for testing the highly complex DC-6 instruments. The large photograph shows a test bench setup which allows rapid and dependable checking of the A-12 automatic pilot. It includes a complete operating system of all the units of the A-12 comparable to the system which is installed in the DC-6's. Through the use of this test analyzer and the substitution of questionable components in the mockup, defective units may be detected and isolated. Ship wiring systems are duplicated in the cabinet beneath the shelf.

The horizon test stand is used principally for aligning the horizon-rotor axis to the true vertical position. The microscope is so designed that a deviation of 15 minutes is easily discernible and a difference of as little as 1 degree exceeds the field of view of the microscope; that is, no image of the roto shaft is seen in the microscope when the deviation exceeds 1 degree.

Strobotac and microscope allow visual alignment of horizon rotor for angular accuracies of 15 minutes

The third photograph shows the cabin pressurization instrument test panel which is complete with pressure lines, vibrators and electrical connectors so that any malfunctioning unit can be detected immediately upon test. Through the manipulation of the various



Test setup for checking the A-12 automatic pilot. Questionable components are plugged into this complete test-bench version, and malfunctioning units can be isolated

Test setup for checking operation of cabin pressurization instruments and gages

SOLDERING TIPS

Previous to the late war, many of the largest users of solder maintained schools to teach their employees the art of soldering. Due to the great need of materials during the war and the great rush to be first on the market in the post-war years, much of this educational work has been pushed into the background. As a result, on many production soldering lines, many different techniques have been developed. The lack of a thorough understanding of making an efficient soldered joint has resulted in the waste of high-priced time and valuable materials. Most solder users understand the correct method of making a solder joint, but perhaps a brief resume of the essential points may bring to mind some forgotten technique and further the cause of a well-made, efficient soldering operation.

1. A SOLDERING IRON OF SUFFICIENT HEAT CAPACITY to rapidly heat the metal being soldered to a temperature sufficient to melt the solder.
2. A CLEAN IRON TIP, WELL TINNED. Keep a rag handy to the soldering operation so that the iron may frequently be wiped clean of the burnt particles of the soldering flux.
3. USE THE FULL FACE OF THE IRON TIP, not just the point. This will assist in transmitting the heat more rapidly.
4. ROTATE THE IRON TIP. Soldering irons have many sides. Use them. This will increase the life of your tip between dressings.
5. USE THE PROPER AMOUNT OF FLUX FOR YOUR OPERATION. Too much flux results in spreading solder and flux over the adjacent area and makes a bad-looking joint. Too little flux will result in an inefficient, poorly-soldered joint.
6. FLUX-CORE SOLDER should always be applied to the exact junction of the metal and the soldering iron. Flux-core solder applied high up on the iron will result in the dissipation of all or part of the flux before it reaches the metal to be soldered.

Finally, an efficient solder operation requires CLEANLINESS—HEAT—THE PROPER SOLDER—THE PROPER FLUX.

QUESTION: What is the smallest diameter flux-core solder made?

ANSWER: Kester Solder Company makes a flux-core solder that is .0085" (eight and one-half thousandths) in diameter. However, generally speaking, the smallest made for practical use is .011" (eleven thousandths), produced by Kester Solder Company as a regular item.

"Soldering Tips" will be pleased to answer all inquiries pertaining to solder, soldering fluxes, and soldering technique. Merely address "Soldering Tips", Kester Solder Co., 4204 Wrightwood Ave., Chicago 39, Ill.

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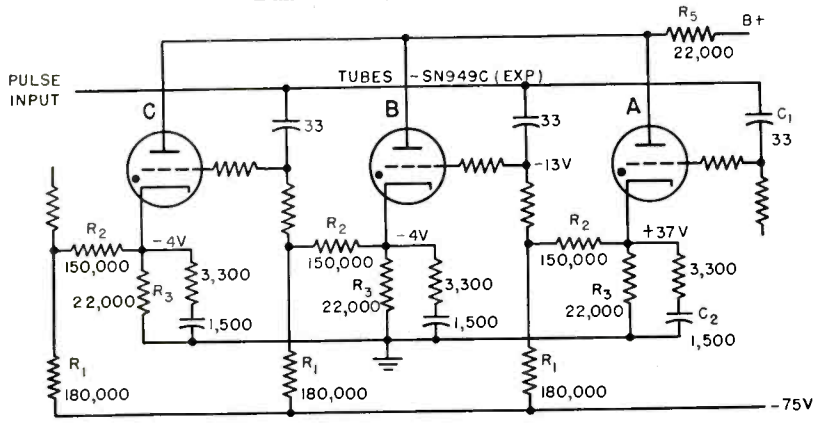


CONTAINING 11 tubes, 80 resistors and 23 capacitors, the decade ring counter counts pulses at a random rate or in a continuous train of rates from 0 to 5,000 per second and holds the count indefinitely or until the power is turned off or a tube fails.

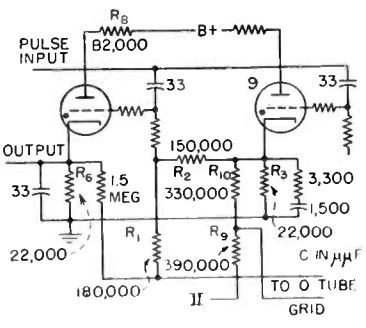
The basic operation of three typical counting tubes is illustrated in the accompanying diagram. The resistor network composed of R_1, R_2 and R_3 is a voltage divider which places the cathode voltage to tubes *B* and *C* at about −4 volts and puts the grid voltage of tube *C* at about −38 volts. Assume that tube *A* is conducting and the current through the tube and the resistor R_3 are such that the cathode of tube *A* is at about positive 37 volts. Voltage divider R_1R_2 in the circuit of tube *A* then places the grid of tube *B* at −13 volts. The bias becomes −34 volts for tube *C*, but is only −9 volts for tube *B*. Since the pulse input line is connected to all the grids, each tube grid will receive the same pulse, but tube *B* will be fired by a much lower pulse than tube *C*, say a pulse of 15 volts positive. This still leaves a considerable margin of safety so that tube *C* is still biased to about −34 + 15 = −19 volts.

After tube *A* has been conducting for a few microseconds, capacitor C_2 is charged to the cathode potential or −37 volts. When tube *B* fires, an additional current flows through the common plate resistor R_5 and this causes a sudden drop in anode voltage, but the capacitor tends to hold the cathode at −37 volts. This allows the anode voltage to drop below the critical value long enough so that conduction stops, thus permitting the grid to regain control. The count has now advanced from tube *A* to tube *B* and continues through the tubes until tube 9 is conducting. The circuit for this tube is shown in the small diagram.

When tube 9 is conducting, it sets up the bias or primes both the 0 tube and the transfer tube in exactly the same fashion as before. When the next or 10th pulse comes along the 0 tube and the transfer tube will both conduct for a few microseconds and then go out because $R_6 + R_8$ is quite high. A pulse is thus sent through the output to the next decade.

When the equipment is turned on and before any pulses are applied the voltage is removed momentarily from the line marked II. This removes the bias from the 0 tube and puts zero bias on the tube, and thus the tube fires.

The pulse height may be between 15 and 25 volts. The rise time of the pulse can be rather slow compared to many other modern counters.



controls, actual atmospheric conditions at various altitudes can be applied to the pressure instruments for checking.

Other electronic test gear includes a unit which introduces an artificial signal into the C-2 gyrosyn compass system amplifier for the purpose of checking the resulting output. Another setup is provided for checking the operation of fuel quantity gages used on DC-6's and Convairs.

Reduced Ignition Interference

RELIEF for communications services that suffer from ignition interference is promised by the future use of resistor-type spark plugs on automobiles.

Until recently, the opinion has prevailed that resistor-type plugs required increased voltage over that used by non-resistor plugs of identical design when set at the same gap settings, and the opinion has been expressed that resistor plugs would adversely affect starting and road load fuel economy. Investigations have shown that resistor plugs with values up to 20,000 ohms have no practical effect upon starting and require no increase in secondary voltage over those of non-resistor plugs of identical design when used with the same gap setting.

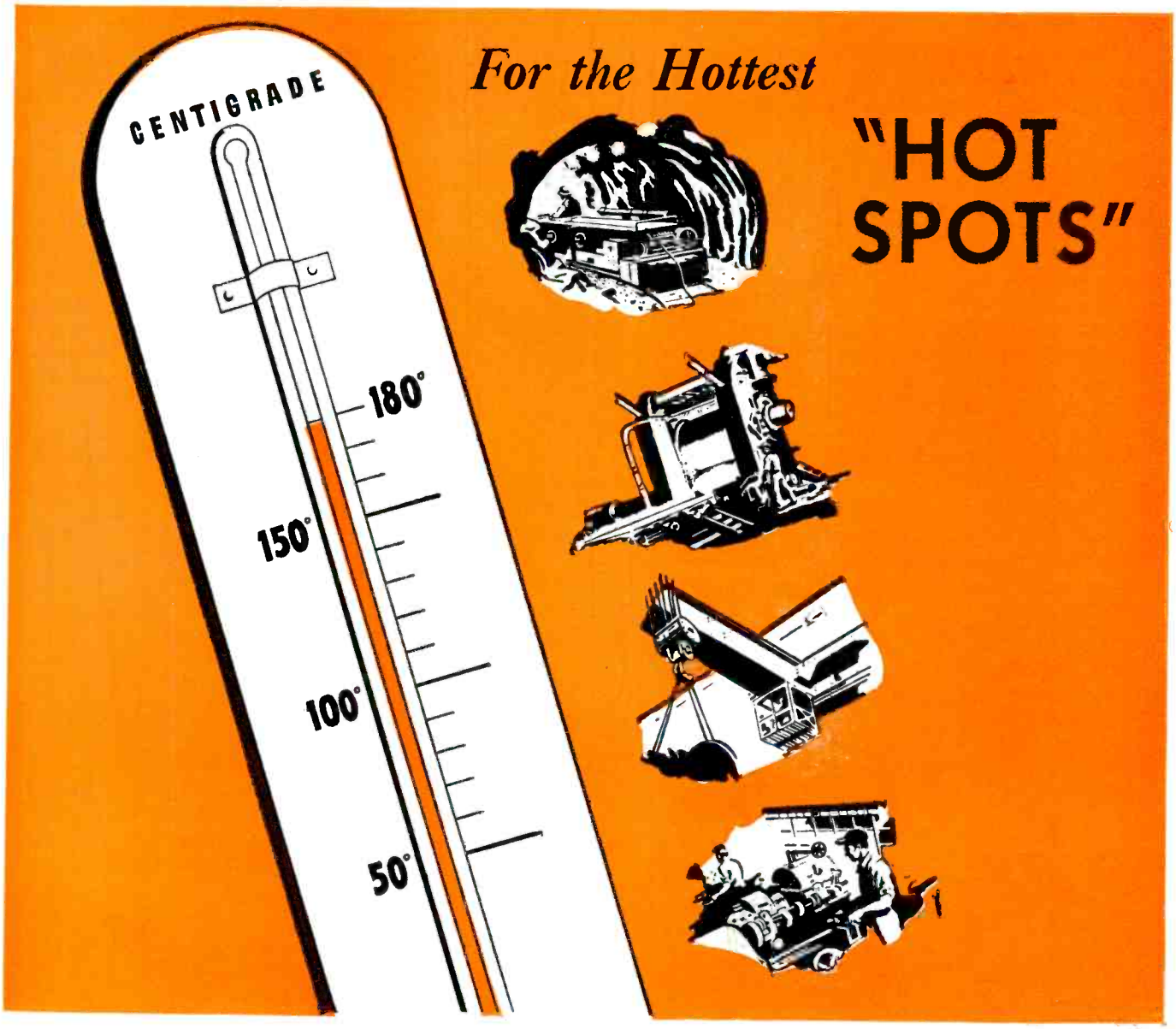
An investigation was undertaken by engineers of the Electric Auto-Lite Co. to analyze the possibilities of wider initial gap settings.

It has been found that wider gap settings, when used in conjunction with resistors and an ignition coil having improved wave front characteristics can bring about increased effectiveness of the spark discharge and initiate combustion through a wider band of complex and variable factors.

A spark or a spark followed by an arc is the process whereby an electrical circuit in a highly unstable condition returns to a more stable state by passing a current through the intervening gas between two electrodes. This return to stability or lower electrical stress occurs in a very short period of time and an

(continued on p 132)

A MAGNET WIRE



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THE ELECTRON ART

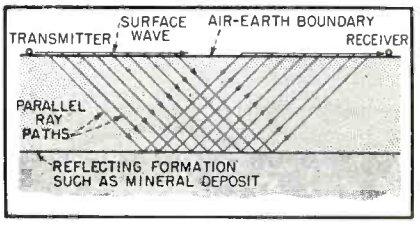
Edited by JOHN MARKUS

Underground Prospecting Tests with Radio Waves

GEOLOGISTS, geophysicists and radio engineers in an abandoned tunnel of a deep salt mine at Grand Saline, Texas, recently witnessed a demonstration of radio reception from a transmitter located some 1,200 feet away on the surface. The test, made by engineers of William M. Barret, Inc., consulting geophysicists in Shreveport, La., was conceived to provide proof that the specially transmitted waves actually traveled through the earth. In actual prospecting both receiver and transmitter would be on the surface, and waves would be reflected from the subsurface deposit being explored.

Mineral Radiolocation Problems

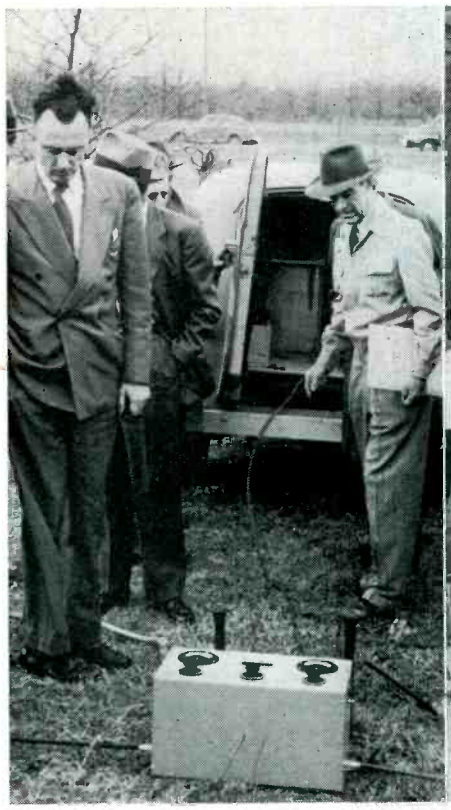
To indicate clearly the existence and size of a mineral deposit deep underground, it is essential that the radio waves be directed along selected paths. However, if the frequency is made high enough to permit use of convenient sizes of antenna arrays, then the waves are absorbed after traveling only a relatively short distance into the earth. Furthermore, only a small percentage of the energy actually enters the earth, most being reflected at the surface. Conversely, if the frequency is made low enough to prevent excessive absorption, surface reflection increases still more and the antenna system required approaches an office building in size.



Special antennas on surface produce parallel underground ray paths that reinforce each other at receiver after refractions

Studies indicate that geologic strata selectively absorb and transmit electromagnetic waves, with certain frequencies undergoing far less absorption than others. These critical frequencies are not necessarily adapted to transmission through the air-earth boundary by conventional means, however. This problem is believed to have been solved by use of a unique type of radiating device, technical details of which have not yet been revealed. As indicated in the diagram, this antenna system directs a surface wave along the air-earth boundary. Rays progressively peel off the wave by refraction and enter the earth along a multitude of parallel-ray paths. When these parallel rays encounter a reflecting formation or mineral deposit, they are partially refracted downward and partially reflected back to the earth's surface for final refraction to the receiving antenna. All of the reflected rays reach the receiver in space phase and time phase and therefore reinforce each other to give the required signal input strength.

Through differences between reflecting properties of mineral deposits and sedimentary media, the character of the received waves may disclose the presence of underground deposits. The surface wave picked up directly by the receiver acts as a reference wave for inter-



W. M. Barret (right) explains operation of his radio system for geophysical prospecting during demonstration at Grand Saline, Texas. Note insulated antenna wires running along ground in opposite directions from transmitter

Listening to code messages picked up by receiver deep underground in salt mine. Receiver is perched on dynamite box, with antenna wires running in opposite directions from it along floor of tunnel 1,800 feet from shaft of mine

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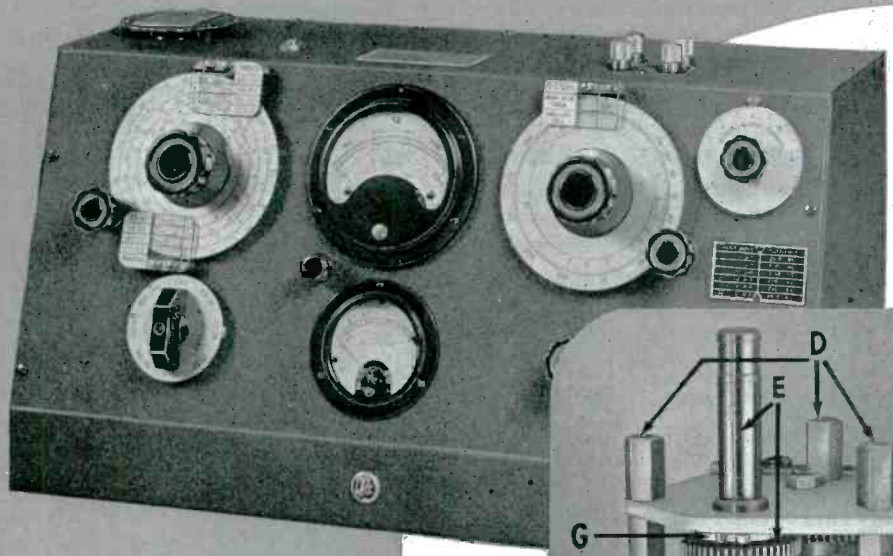

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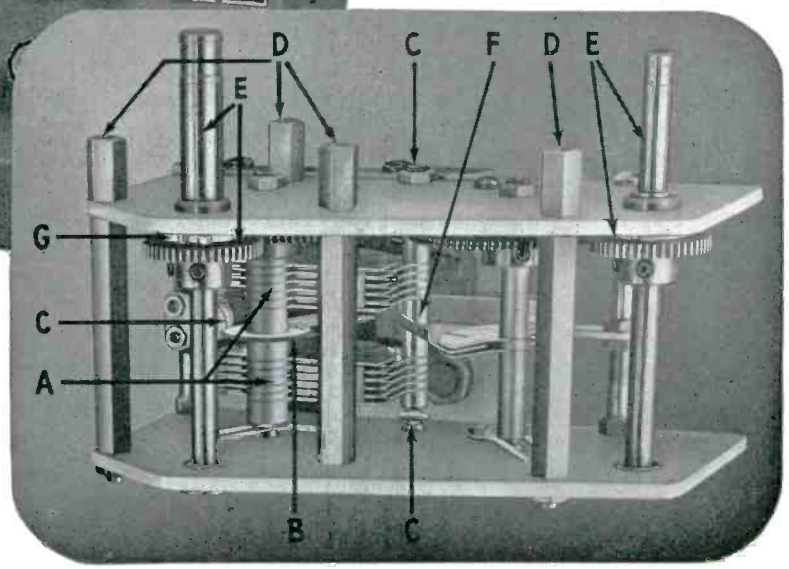
160-A Q-METER
50 KC. to 75 MC.



Radio frequency circuit design often requires the accurate measurement of Q, inductance, and capacitance values. For this application, the 160-A Q-Meter has become the universal choice of radio and electronic engineers throughout the country.

Each component part and assembly used in the manufacture of this instrument is designed with the utmost care and exactness. Circuit tolerances are held to values attainable only in custom built instruments.

Consider, for example, the Q tuning capacitor assembly of the 160-A Q-Meter, specially manufactured for maximum range, low loss, and minimum residual inductance. The ultimate design of this unit was reached only after months of intensive engineering research to produce the finest in performance, quality, and workmanship.

This is but one of the many desirable features of the 160-A Q-Meter which contribute to its outstanding accuracy and dependability.

Be sure to include the 160-A Q-Meter in your new equipment plans.

Write for Catalog "F"

Shown above is the Q tuning capacitator assembly of the 160-A Q-Meter. Note the following design features of this unit — features which insure reliable, trouble-free operation.

A. Parallel connection of dual rotor and stator assemblies minimizes internal inductance and resistance.
B. Spring silver fingers contact both sides of silver disc to provide low series resistance.
C. Three point pyrex ball stator suspension reduces losses and permits accurate stator alignment.
D. Four point panel mounting designed to produce maximum structural rigidity and capacitance stability.
E. Precision-cut brass spur gears and stainless steel shafts, mounted in oversize bearings, assure long, trouble-free service.
F. Common stator mounting for main and vernier stator plates reduces loss and internal series resistance of vernier capacitor section.
G. Positive shaft stop protects main rotor assembly and gears against mechanical overload.

SPECIFICATIONS

Oscillator Frequency Range: 50 kc. to 75 mc. in 8 ranges.
Oscillator Frequency Accuracy: ±1%, 50 kc.—50 mc.
±3%, 50 mc.—75 mc.
Q Measurement Range: Directly calibrated in Q, 20-250. "Multiply—Q—By" Meter calibrated at intervals from x1 to x2, and also at x2.5, extending Q range to 625.
Q Measurement Accuracy: Approximately 5% for direct reading measurement, for frequencies up to 30 mc. Accuracy less at higher frequencies.
Capacitance Calibration Range: Main capacitor section 30-450 mmf, accuracy 1% or 1 mmf whichever is greater. Vernier capacitor section +3 mmf, zero,—3 mmf, calibrated in 0.1 mmf steps. Accuracy ±0.1 mmf.

BOONTON RADIO Corporation
BOONTON·N·J·U·S·A·

DESIGNERS AND MANUFACTURERS OF THE Q METER · QX CHECKER FREQUENCY MODULATED SIGNAL GENERATOR · BEAT FREQUENCY GENERATOR AND OTHER DIRECT READING INSTRUMENTS

preting reflected waves returning from underground geologic strata.

In practice, the subsurface may be explored by simultaneously moving transmitter and receiver or by varying the separation between them. The depth to a reflecting formation may be measured by determining the separation when the first reflected energy is received, by determining the transit time of the underground rays or by varying the frequency and analyzing the resulting interference patterns between surface and reflected rays.

Details of Test

The radio transmission demonstration at Grand Saline was conceived to provide proof that the transmitted waves actually traveled through the earth. The receiver was set up in an abandoned part of the mine that was free of metal and separated from the shaft by 1,800 feet of circuitous tunnels, with the two long wires of its special antenna extending in opposite directions along the mine tunnel much like a conventional dipole for the 1,602-kc carrier frequency employed.

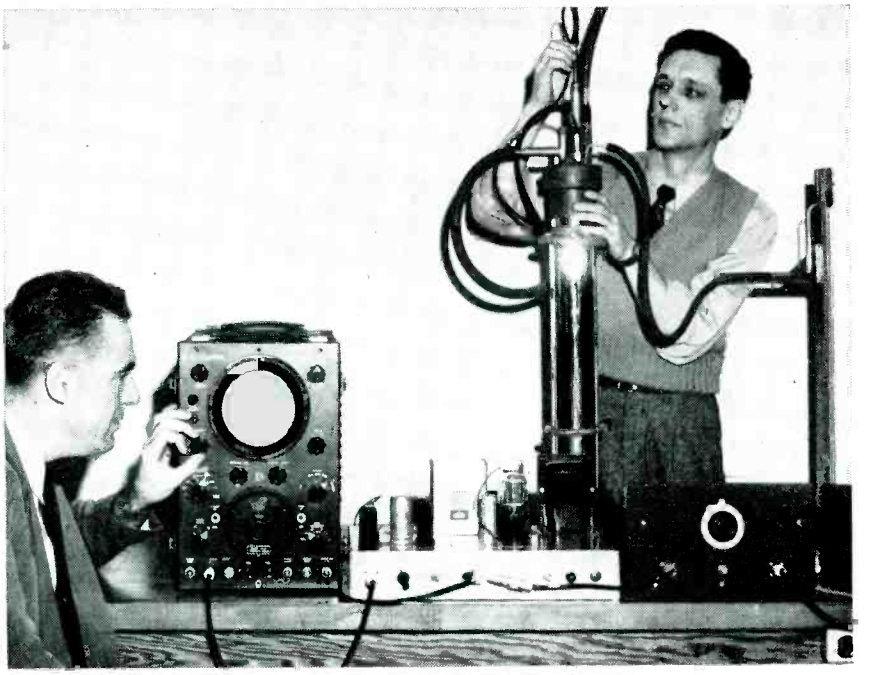
Elaborate precautions were taken to prevent signals from reaching the receiver through air or metal in the shaft. Electric and phone lines were cut and grounded at both top and bottom. The water line and pneumatic-signaling tube were likewise grounded. The hoist cable was grounded at the hoist, at the sheaves and at the bottom of the mine. Vertical and interconnected reinforcing rods within the concrete shaft were naturally grounded by a heavy seepage of salt brine at the 200-foot level. The diameter of the shaft was 14.5 feet, considered far too small to act as a waveguide for the 614-foot wavelength used.

Superconductivity Research Program

As a part of a comprehensive research program on superconductivity at the National Bureau of Standards, an experimental investigation was recently made of the restoration of the resistance of superconducting wires with increase in current. Straight lengths of pure indium wires of three different diameters were immersed in a bath of liquid helium and cooled until they became superconducting.

It was found that there was a sudden rise of resistance when the current reached a critical value, followed by a slower rise of resistance as the current was further increased. Moreover, the amount of resistance that appeared suddenly was independent of the temperature of the specimen, even though the current required to restore this resistance was temperature-dependent. To this extent the results described are in agreement with the theory. However, the magnitude of the sudden rise of resistance was 77 to 85 percent of the normal resistance, instead of one-half as predicted. Also, the larger the diameter of the wire, the smaller was the fraction of the normal resistance that reappeared when the current reached the critical value, although the theory shows no dependence on specimen diameter.

This disagreement with theory adds interest to the experimental results. Recent theoretical investigations on the nature of the intermediate state of superconductors have pointed out in a qualitative way some of the shortcomings of the earlier theory, but as yet no quantitative theoretical treatment has explained the results obtained experimentally.



Apparatus being used at the National Bureau of Standards for the study of the velocity and attenuation of second sound in helium II near absolute zero. Oscilloscope at left triggers multivibrator (center) and at same instant begins its horizontal time sweep. Electrical pulses from the multivibrator then travel through coaxial lines to a Dewar flask of liquid helium II which is mounted in the Dewar of liquid air in the background. The heat pulses thus generated travel through the helium II as second sound and are detected by a temperature-sensitive element. The resultant faint voltage signals are amplified by an audio amplifier (right) and impressed upon the vertical plates of the oscilloscope to give an easily detected visual signal

Microwaves and Superconductivity

Another phase of superconductivity research at the Bureau concerns the behavior of superconductors at microwave frequencies. In experiments using low-frequency or direct currents, superconductors show a complete loss of resistance below the transition temperature, whereas at optical and infrared frequencies the superconducting state does not occur. The microwave region remains as a kind of twilight zone; here the metals exhibit an intermediate type of behavior, losing only a portion of their resistance at low temperatures.

Second Sound

At 2.19K, ordinary liquid helium (HeI) undergoes a transition to HeII with a radical alteration of

(continued on p 156)

This New VARGLAS Tubing is better 5 ways!

Impregnated with General Electric's PERMAFIL for superior insulation...

Varglas Permafil Tubing excels oleoresinous and other synthetic coated tubing in several important performance characteristics. Outstanding among these are:

1 TOUGHNESS

Remains pliable even after severe flexing. This new tubing can be twisted, bent or tied in knots with no loss in its dielectric value (7,000 volts).

2 SOLVENT RESISTANCE

Is relatively immune to alcohol. Petroleum and aromatic hydrocarbons have only slight effect after long exposure.

3 HEAT AGING

Withstands more than 2,000 hours at 105° to 110° C., 1,000 hours at 125° C. and extensive periods at 150° C.

4 BAKING

Can be after-treated in baking and varnishing operations—reacts better than most oleoresinous materials.

5 AVAILABLE IN COILS

—In standard colors and wide range of sizes. Meets or exceeds all requirements of A.S.T.M. specifications.

Varflex CORPORATION

Makers of Electrical Insulating Tubing and Sleeving

Send for FREE SAMPLE and complete data.

VARFLEX Corporation, 308 Jay St., Rome, N. Y.

Please send me full information as well as a free sample of your new Varglas Tubing impregnated with G.E. Permafil. I am particularly interested in samples suitable for.....

Name.....

Company.....

Street.....

City.....Zone.....State.....

NEW PRODUCTS

Edited by A. A. McKENZIE

Tele Remote Control

TRANSVISION, INC., New Rochelle, N. Y., announces a new remote control unit designed to operate and control any television set from a distance up to 50 feet. It features

continuous tuning on all channels. The tuner unit has a high-gain with about 50-μv sensitivity, factory-wired and tuned.

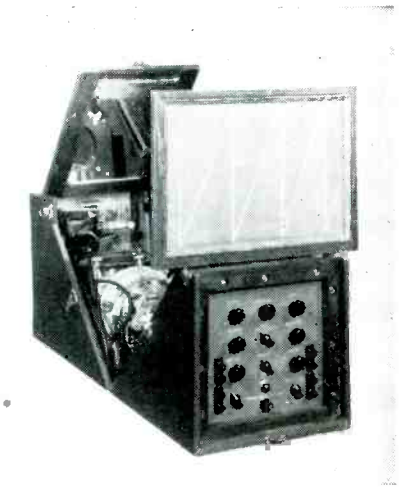
Tiny Ballast Tube

AMPERITE CO., INC., 561 Broadway, New York 12, N. Y. The new subminiature ballast tube requires no base; leads can be soldered directly to the leads coming from the tube. It can be supplied to dissipate any wattage up to 3 watts. Maximum

current is 0.9 ampere. A 100-percent increase in voltage across the the tube will produce a current change of less than 5 percent. An ambient change of −50 to +70 C will produce a current change through the ballast of less than 2 percent.

Projection Oscilloscope

BETA ELECTRIC CORP., 1762 Third Ave., New York 29, N. Y. Model 701 portable projection oscilloscope



designed for use in educational institutions gives an oscillogram approximately 16 inches wide by 12 inches high. Vertical deflection sensitivity is approximately 60 millivolts rms per inch, or 0.6 volt for full-scale deflection. Horizontal deflection sensitivity is approximately 0.65 volt rms per inch or 1.0 volt full scale. Vertical amplifier response is good to 50 kc and usable to 100 kc. Horizontal sawtooth sweeps are good to 2 kc and usable to 5 kc.

Resistor Spark Plug

THE ELECTRIC AUTO-LITE CO., Toledo 1, Ohio, has developed a new resistor spark plug designed to prevent interference with television reception caused by the ignition system of automobiles. The heart of the unit is a 10,000 ohm built-in and concealed resistor which dampens the high-voltage peaks in the capacitance phase of the spark so its effect on the radio signal is kept below an acceptable minimum (within 35 μv per meter from 540 kc to 150 mc at 50 ft).

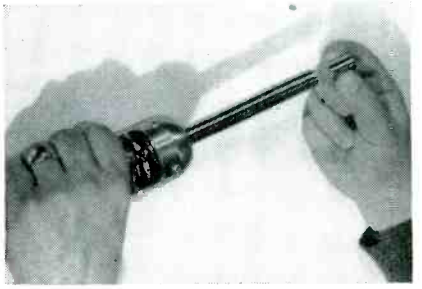
Instrument Kit

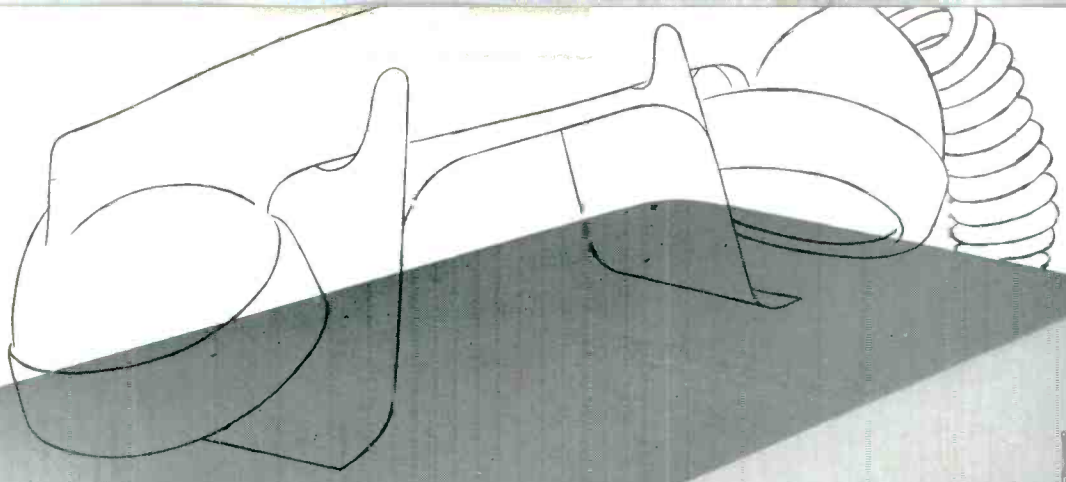
ELECTRONIC INSTRUMENT CO., INC., 276 Newport St., Brooklyn 12, N. Y., is now supplying most of its test instruments in a kit form de-

signed for quick and economical assembly. Model 221K vacuum-tube voltmeter illustrated is a sample of the line of equipment being put together by students, experimenters and servicemen.

Sound Measuring Device

MASSA LABORATORIES, INC., 3868 Carnegie Ave., Cleveland 15, Ohio. Model GA-1002A sound pressure measurement equipment has a specially isolated socket tip which effectively separates the microphone clamping structure from the pre-

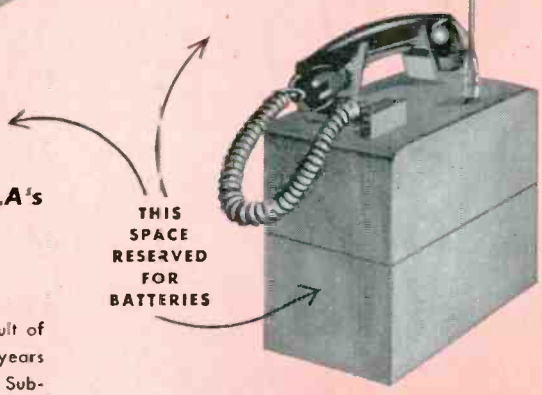




THIS SPACE RESERVED FOR 18 RAYTHEON SUBMINIATURE TUBES

Here is the actual size of a portable FM Radiotelephone Transmitter and Receiver that provides up to five mile, 2-way communication on the 25-50 mc. band or, with a different electrical design, on the 152-162 mc. band.

It employs 17 or 18 Raytheon Flat Subminiatures with plenty of room left over for dozens of other components. The uses for these small, light (not over 9 lbs.) "Handie-Talkie" units are growing by leaps and bounds. Contractors, Farmers, Fire Fighters, Foresters, Game Wardens, Geophysicists, Lumbermen, Miners, Movie Directors, Oilmen, Police, Ranchers, Railroad Men, Reporters and Surveyors find them invaluable — and thoroughly *dependable*, thanks in large measure to the reliability as well as the compactness of Raytheon Subminiatures.



Why leading makers of electronic equipment such as MOTOROLA's "Handie-Talkie" and DOOLITTLE's "littlephone" use RAYTHEON Subminiature Tubes:

1. **Increased Product Salability** — Raytheon Filamentary Subminiatures are *flat*. Filament drain is extremely low. Product size is reduced, convenience increased.
2. **Plug Into Standard Sockets.** All Raytheon Subminiatures can be soldered in, or plugged into readily available sockets.
3. **Raytheon Reliability** — the result of unique precision methods and ten years continuous production of long-life Subminiature Tubes.
4. **Readily Available From Stock** — over half a million on top at all times. Over 40 types. Standard throughout the world. Over 300 Raytheon Special Purpose Tube Distributors are ready to serve you.

Write for Data Sheets

SUBMINIATURE TUBES • SPECIAL PURPOSE TUBES • MICROWAVE TUBES
CATHODE RAY TUBES • RECEIVING TUBES

RAYTHEON

Excellence in Electronics

RAYTHEON MANUFACTURING COMPANY

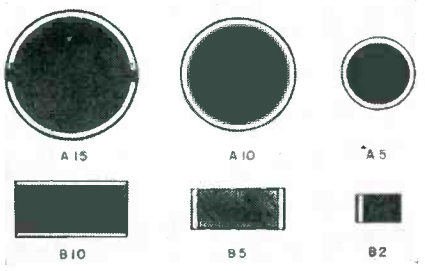
SPECIAL TUBE SECTION

Newton 53, Massachusetts

amplifier extension tube. Dynamic range is such that sound pressures from less than 1 and up to 20,000 dynes per sq cm (160 db level) may be directly measured. A multiplier is available for extending the range up to 200,000 dynes per sq cm (180 db). A built-in calibrating circuit is provided.

Photoelectric Cells

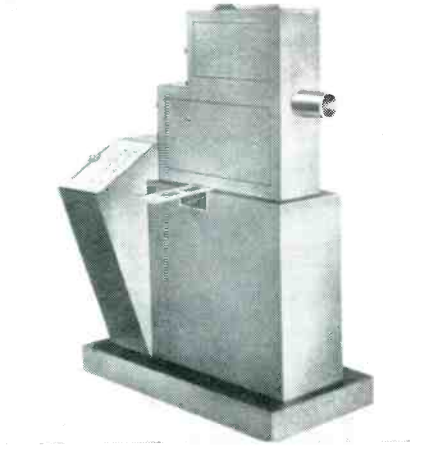
INTERNATIONAL RECTIFIER CORP., 6809S. Victoria Ave., Los Angeles 43, Calif. The new line of unmounted selenium self-generating photoelectric cells find use in such



applications as photographic exposure meters and illumination meters. Sizes vary from the rectangular 23/32 in. by $\frac{7}{16}$ in. to the round type $1\frac{3}{4}$ in. in diameter. Sensitivity is of the order of 600 μa per lumen.

Tele Slide Projector

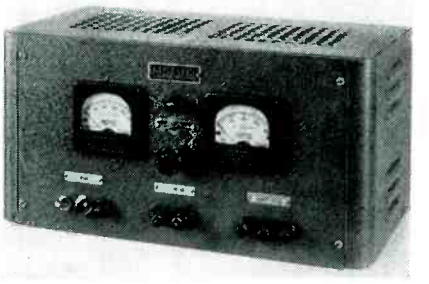
GRAY RESEARCH & DEVELOPMENT CO., INC., 16 Arbor St., Hartford 1, Conn. Type T-101 Telop is a television optical projector for use with television film cameras. Cards and slides measuring $3\frac{1}{4} \times 4$ in. as well as small physical objects may be dually projected, with one image fading to another instantly or by superimposing, with exact density



control of each object. The unit has four slide openings with individual brightness controls for each. Light intensity through the lens is 12 to 15 foot candles.

Regulated Power Supply

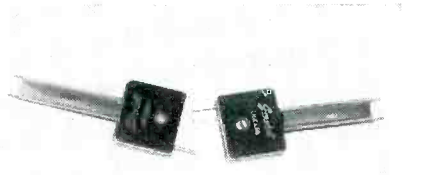
KEPCO LABORATORIES INC., 149-14 41st Ave., Flushing, N. Y. Model 245 power supply has a d-c output of 200 to 450 volts at currents from 0 to 200 ma, regulated; and an a-c output of 6.3 volts at 6 amperes,



unregulated. Regulation is 0.5 percent for both load and input variations. Power required is 300 watts, and output impedance is less than 2 ohms.

Twin Line Connector

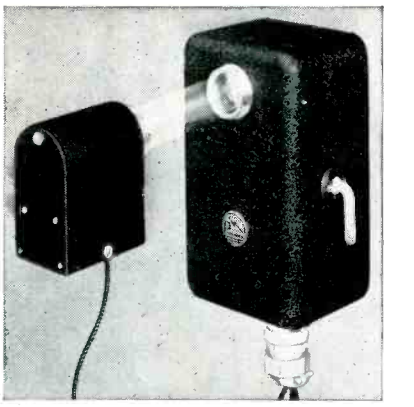
GRAYHILL, 1 North Pulaski Road, Chicago 24, Ill., has announced a twin line connector for television receivers and accessories. Such ac-



cessories as inside and outside antennas, boosters, matching stubs and matching devices can be connected. Added lengths of line can be inserted for standing wave correction. Impedance within the connector is matched to that of the 300-ohm twin line wire.

Photoelectric Control

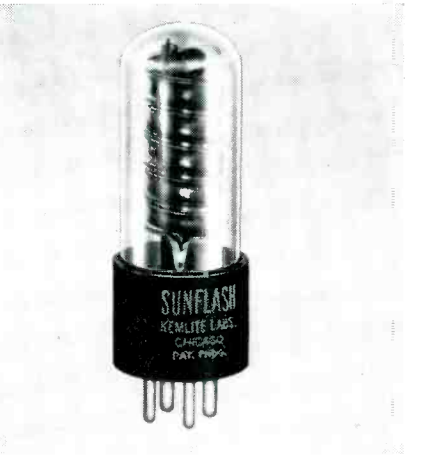
PHOTOSWITCH INC., 77 Broadway, Cambridge 42, Mass. Type 20DA4 delayed action photoelectric control is designed to indicate the



presence of a jam and to introduce stop motion or other correction on a conveyor line. The dpdt relay is operated in 0.05 second. Delayed action is adjustable from 0.05 to 5 seconds. The control operates on 115 and 230 volts, 50-60 cycles a-c. Bulletin PA494 is descriptive of the unit.

Photo-Flash Lamp

KEMLITE LABORATORIES, 1819 W. Grand Ave., Chicago 22, Ill. The Sunflash is an electronic photoflash lamp for use in photography or any application requiring intense, instantaneous light values. In use as a photographic illuminator, 100,000 brilliant white flashes of metered

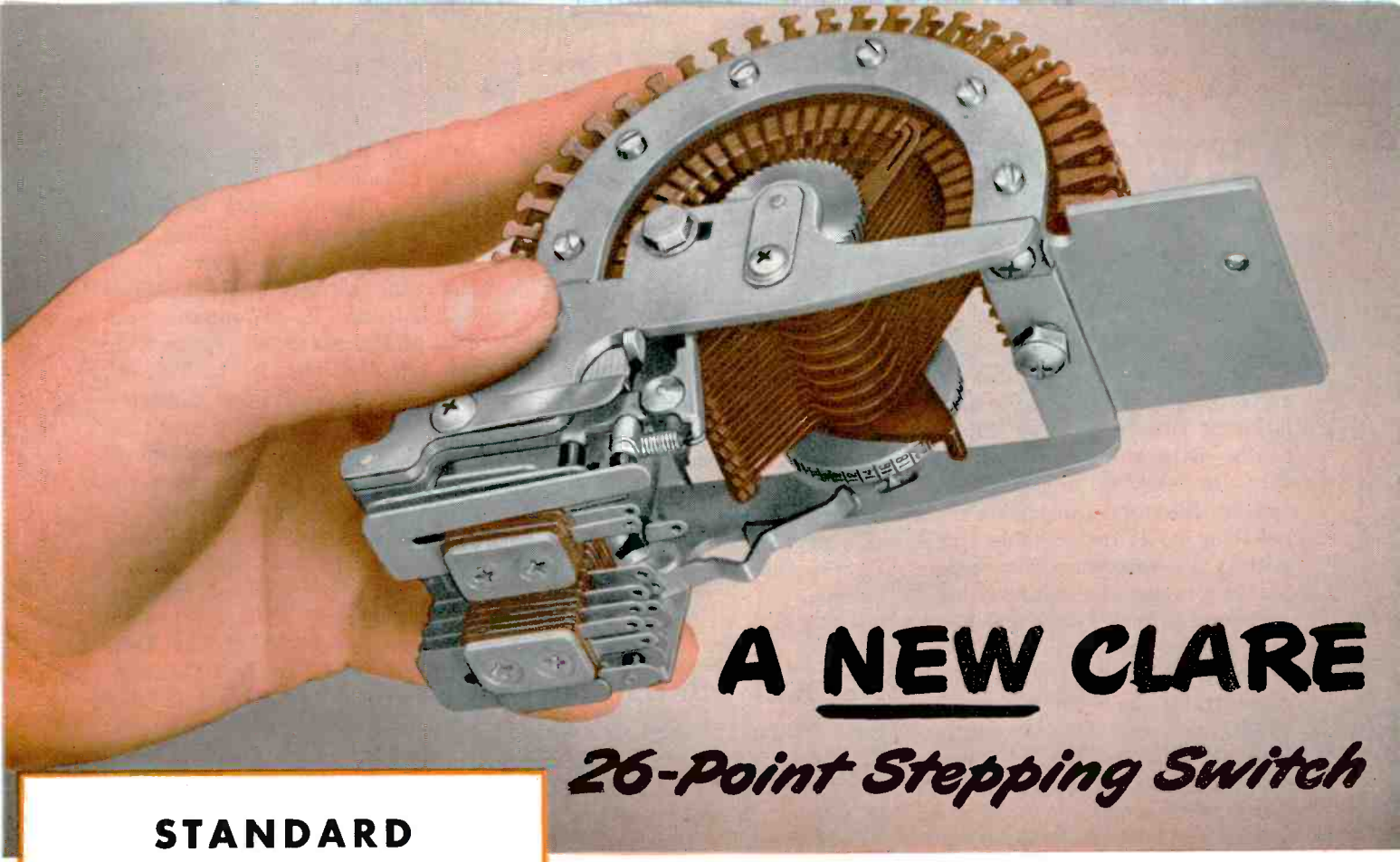


consistency are commonly realized. It is self-ionizing and requires no auxiliary triggering circuit for its operation.

Wideband Oscilloscope

FEDERAL TELECOMMUNICATION LABORATORIES INC., 500 Washington Ave., Nutley 10, N. J. Model FTL-

(continued on p 170)



A NEW CLARE

26-Point Stepping Switch

For Selection - Sequence Control - Counting - Totalizing

Selection of any channel or circuit path from a total of 26 or 52 circuits is provided by this new CLARE Stepping Switch.

This selection may be at the rate of 30 steps per second on remote control—up to 60 steps per second on self-cycling operations. Operating at these speeds, the switch gives a minimum life of 5 million half-revolutions or 130 million stepping operations.

Each of the ten levels possible for the Type 26 Switch, or the five levels of the Type 52 Switch, is unit-molded in Bakelite. Hand positioning of individual contacts is thus eliminated, and each bank level is easily replaced if a contact becomes damaged in service.

In operation, a pair of double-ended wiper springs is stepped over each bank level of 180 degrees. One end of the wipers is engaged with the bank contact at all times, one end is always free of the bank. The stepping magnet may be remotely controlled or wipers may be stepped automatically by interrupting the magnet circuit through a pair of interrupter springs. As many as eight auxiliary interrupter springs may be provided for other control or signal functions.

Like many other CLARE developments, this new stepping switch was designed to meet a specific requirement . . . has provided an answer to others. Whatever your relay problem, it will pay you to submit it to CLARE. Sales engineers are located in principal cities for your convenience. Look in your classified telephone directory . . . or write to C. P. Clare & Co., 4719 West Sunnyside Ave., Chicago 30, Illinois. In Canada: Canadian Line Materials Ltd., Toronto 13. Cable address: CLARELAY.

STANDARD SPECIFICATIONS

OPERATION:
Automatic (self-interrupting) or remote controlled.

WIPERS:
One to ten, traversing individual contact levels.

INTERRUPTER SPRINGS:
Form 1B (to open the operating circuit at the end of each step). Contacts are single platinum-iridium.

OPERATE SPEED:
Remote controlled operation: maximum 30 steps per second. Self cycling operation: average 60 steps per second, with 48-volt power supply.

FINISH:
Framework and armature: cadmium; Bank contacts and wipers: phosphor bronze.

MOUNTING:
Frame drilled and tapped at each end to accomodate No. 8-32 mounting screw.

DIMENSIONS:
Overall lenght: 6-9/16 in.; width: 2-3/8 In.; height: 4-5/8 in.

NET WEIGHT:
27 oz., approximately.

SHIPPING WEIGHT:
4 lbs., approximately.

Write for Clare Bulletin 101 on complete details.

CLARE RELAYS

First in the Industrial Field

NEWS OF THE INDUSTRY

Edited by WILLIAM P. O'BRIEN

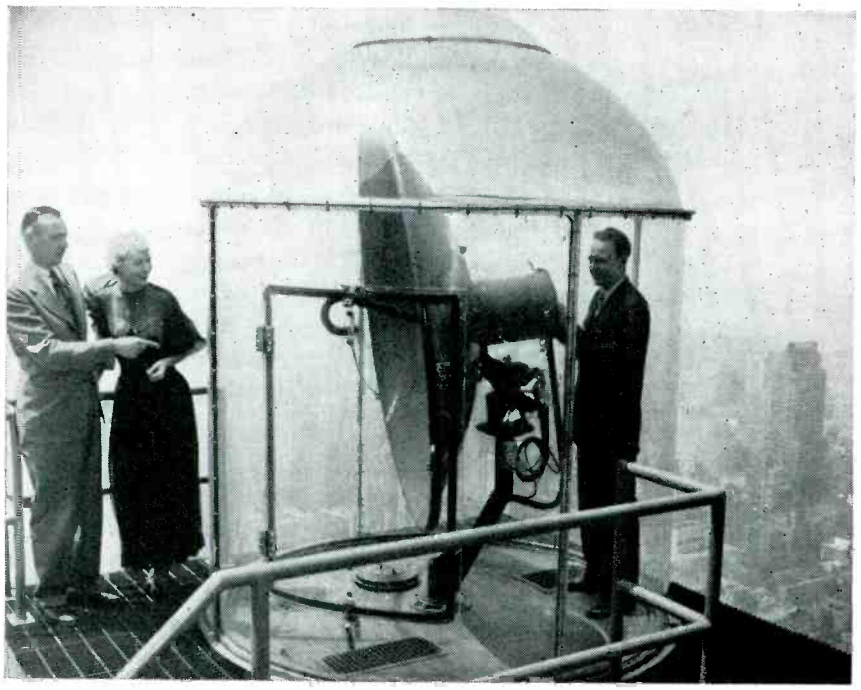
Radomes Aid All-Weather Microwave Television Reception

THE NATIONAL BROADCASTING COMPANY recently completed the installation of two radomes on the roof of the RCA Building, New York City, to provide a reliable all-weather microwave television relay receiving point for portable transmitters at remote pickup points within a radius of about 30 miles.

Housed in each Lucite and Plexiglas radome is the receiving antenna, a six-foot parabola which concentrates the short radio waves (7,000 mc, approximately equivalent to 1 1/8 inches) toward a waveguide element at the parabola's focus. The parabola is mounted on a fixture which permits directing it both horizontally and vertically toward the transmitting point.

The output of the primary receiving element in the parabola is connected with coax cable to the main receiving equipment on the 67th floor of the RCA Building and thence to the tv master control board.

The radomes are heated and ventilated for both winter and summer and may be operated under all weather conditions without interfering with broadcast reception. They have been installed on each side of the building and between them cover the entire 360-degree horizon.



Radome housing 7,000-mc receiving parabola for remote television pickups, recently installed atop RCA Building, Radio City, New York. Left to right: Chester Rackey, NBC engineer; Kyle MacDonnell, television actress; Robert Barnaby, NBC engineer

New RMA Officers

AT A MEETING of the board during the Radio Manufacturers Association Silver Anniversary Convention at Chicago, May 16 to 20, officers were elected for the coming year. The 1949-50 RMA officers are as follows:

President, Raymond C. Cosgrove, executive vice-president of Avco Mfg. Co.; treasurer, Leslie F. Muter, president of The Muter Co., Chicago; executive vice-president and secretary, Bond Geddes of Washington, D. C. John W. Van Allen of Buffalo was reappointed general counsel.

Nine directors were re-elected. Five new ones are J. B. Elliott, vice-president of RCA Victor; W. J. Halligan, president of Hallicrafters Co.; Richard A. O'Connor, president of Magnavox, all representing the set division; R. L. Triplett, president of the Triplett Electrical Instrument Co., in the parts division; A. Liberman, president of Talk-A-Phone, in the amplifier and sound equipment division.

New vice-presidents, in addition to two holdover ones, include R. E. Carlson, vice-president of Tung-Sol Lamp Works; W. J. Barkley, executive vice-president of Collins Radio Co.; and A. Liberman of Talk-A-Phone. Max Balcom, former RMA president, was chosen chairman of the tube division. Other division chairmen are: Transmitter, T. A. Smith of RCA Victor; amplifier and sound equipment, A. G. Schifino of Stromberg-Carlson.

ASTM Annual Meeting

THE 52nd annual meeting of the American Society for Testing Materials will be held at the Chalfonte-Haddon Hall, Atlantic City, N. J., during the week of June 27. In the diversified technical program scheduled, the sessions of particular interest to electronic engineers will be those on radiography and ultrasonic testing.

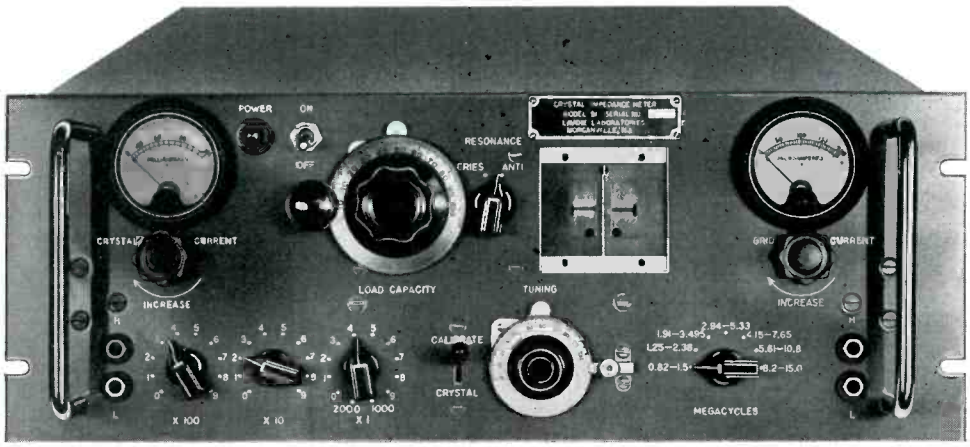
Two series of papers on these topics have been arranged by Committee E-7 on Nondestructive Testing. Six papers on radiography will cover such subjects as x-ray moving pictures and the radium exposure calculator. Five others will deal with the basic principles of practical ultrasonic testing, its uses in the forging industry, railroad field, nonferrous metals field and the consumer's plant.

Analog Computation Course

DESIGNED particularly to meet the needs of users of industrial types of computing machines, a special course in analog computation is being given at the Massachusetts Institute of Technology for the

PREDICT Crystal Oscillator Operation with the

LAVOIE CRYSTAL IMPEDANCE METER



Model 50 . . . ***Frequency range, 76 kc to 1100 kc with provision for plug in coils. Maximum resistance, 29,900 ohms (3 place setting).***

Model 51 . . . ***Frequency range, 820 kc to 15 mc. Maximum resistance, 2,990 ohms (3 place setting).***

POWER . . . 115 V 60 CPS SIZE . . . 7"x19"x7⅞" WEIGHT . . . 21 LBS., 12 OZS.

CONTROLS AND INDICATIONS

CRYSTAL ACTIVITY RESISTANCE ADJUSTMENT
CRYSTAL VOLTAGE MEASURING POINTS
SERIES RESONANCE — PARALLEL RESONANCE
CRYSTAL CURRENT (MODEL 51 ONLY)
FREQUENCY ADJUSTMENT (COARSE AND FINE)
LOAD CAPACITANCE
GRID CURRENT
CRYSTAL-RESISTOR SELECTION SWITCH

Measures parameters of piezoelectric crystals sufficient to predict quality and operation properties of oscillators in which they will be used.

Measurements of a crystal resistance can be made at either the series or anti resonant frequency of the crystal. An indication of the equivalent resistance of a crystal is an indication of the quality of the crystal. The CI meter yields a measurement of crystal activity in terms of ohmic resistance. This is in contrast to previous measurements of crystal quality in terms of arbitrary activity in a standard oscillator. At present, **Government** specifications on crystal units specify a maximum allowable series resonant resistance.

The Crystal Impedance Meter consists of a tuned oscillator with the crystal unit connected in the feedback path. A switching arrangement is provided whereby a condenser may or may not be used in series with the crystal. This condenser is calibrated and is used to simulate load capacity when the crystal resistance is to be measured at the anti resonant frequency of the crystal. The condenser is shorted when the series resonant resistance of the crystal is measured. In addition, a switching arrangement is provided to substitute three banks of calibrated decade resistors into the feedback path replacing the crystal. A grid current meter is provided as an indication of oscillator activity with either crystal or resistance in the feedback path of the oscillator.

In addition to the crystal switching circuit, the calibrated decade switches, frequency controls, the variable capacitor in the crystal circuit, and the oscillator grid current meter, a control which varies oscillator activity, and thereby crystal current, is provided in both models 50 and 51. A crystal current meter is provided in model 51 only.

The series and anti resonant frequencies of crystals can be measured with conventional frequency measuring equipment. With frequency measuring equipment and a VTVM, simple measurements and calculations can be made to yield crystal voltage at either series or anti resonant operation, the series inductance of the crystal, the series capacitance of the crystal, and the Performance Index of the crystal.

U H F

Lavoie Laboratories

RADIO ENGINEERS AND MANUFACTURERS
MORGANVILLE, N. J.

Specialists in the Development and Manufacture of UHF Equipment

three weeks beginning June 20, 1949. Chief subject will be the treatment of engineering problems by machines designed for the solution of differential equations.

The course meets for one and one-half hours of lectures and demonstrations each week-day from June 20 through July 9. It is under the direction of S. H. Caldwell, professor of electrical engineering and director of the Institute's Center of Analysis.

Demonstrations have been planned which will make use of the MIT differential analyzer as well as various types of electronic analyzers available or under development at the Institute.

Proposed Low-Power Rules

TO PROVIDE for operation of low-power radio devices without interference to established radio services, and to learn more of the nature of the devices now operating, the FCC has proposed amendments to its present rules.

The Commission contemplates recognizing two categories of radiation devices: incidental and restricted. Incidental devices would include laboratory signal generators, beat-frequency audio oscillators and radio receiver oscillators. The restricted group would cover wireless record players, carrier current communication systems and remote-control devices using radio.

It also proposed that no low-power broadcasting be permitted on any frequency other than in the 535 to 1,605-kc band, and then only in accordance with FCC broadcast service rules, as appropriately amended. Use of the radio spectrum by restricted radiation devices will be subject to certain provisions.

Comment by interested parties received up to and including June 1 is being considered before final action is taken.

NEW FCC EMISSION AND MODULATION SYMBOLS

Type of modulation or emission	Type of transmission	Symbol
1. Amplitude	Absence of any modulation	A0
	Telegraphy without the use of modulating audio frequency (on-off keying).	A1
	Telegraphy by the keying of a modulating audio frequency or audio frequencies or by the keying of the modulated emission (special case: an unkeyed modulated emission).	A2
	Telephony	
	Double sideband, full carrier	A3
	Single sideband, reduced carrier	A3a
	Two independent sidebands, reduced carriers.	A3b
	Facsimile	A4
	Television	A5
	Composite transmissions and cases not covered by the above.	A9
	Composite transmissions, reduced carrier	A9c
2. Frequency (or phase) modulated	Absence of any modulation	F0
	Telegraphy without the use of modulating audio frequency (frequency shift keying).	F1
	Telegraphy by the keying of a modulating audio frequency or audio frequencies or by the keying of the modulated emission (special case: an unkeyed emission modulated by audio frequency).	F2
	Telephony	F3
	Facsimile	F4
	Television	F5
	Composite transmissions and cases not covered by the above.	F9
3. Pulsed emissions	Absence of any modulation intended to carry information.	P0
	Telegraphy without the use of modulating audio frequency.	P1
	Telegraphy by the keying of a modulating audio frequency or audio frequencies, or by the keying of the modulated pulse (special case: an unkeyed modulated pulse).	
	Audio frequency or audio frequencies modulating their pulse in amplitude.	P2d
	Audio frequency or audio frequencies modulating the width of the pulse.	P2e
	Audio frequency or audio frequencies modulating the phase(or position)of the pulse.	P2f
	Telephony	
	Amplitude-modulated pulse	P3d
	Width-modulated pulse	P3e
	Phase-(or position)- modulated pulse	P3f
	Composite transmissions and cases not covered by the above.	P9

MEETINGS

JUNE 27–29: Conference on Ionospheric Research, The Pennsylvania State College, State College, Pa.

JUNE 27-JULY 1: 1949 Annual Meeting of the American Society for Testing Materials, Chalfonte-Haddon Hall, Atlantic City, N. J.

AUG. 29-SEPT. 1: National Conference of Associated Police Communications Officers, Hotel New Yorker, New York City.

AUG. 30-SEPT. 1: Fifth Annual Pacific Electronic Exhibit sponsored by the WCEMA and the 1949 IRE western regional convention, Civic Center, San Francisco, Calif.

SEPT. 12–16: Instrument Society of America National Conference and Exhibit, Municipal Auditorium, St. Louis, Mo.

SEPT. 26–28: National Electronics Conference, Edgewater Beach Hotel, Chicago, Ill.

OCT. 10–14: ASTM 1949 West Coast Meeting, Fairmont Hotel, San Francisco, Calif.

NOV. 14–18: 23rd NEMA Annual Meeting, Haddon Hall Hotel, Atlantic City, N. J.

OTS Lists Infrared Reports

THE Office of Technical Services has compiled a bibliography of 165 reports on infrared, designated as SB-6. Listed therein are PB num-

(Continued on page 202)

Finger tip facts on Germanium Diodes

Here, combined in a single booklet, are all the essential facts you want on the entire line of 12 Sylvania Germanium Crystal Components—*the most extensive line of Germanium Diodes, Duo-Diodes and Varistors on the market.*

This new booklet contains complete electrical and mechanical specifications and includes typical static characteristic curves on all diode types.

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SYLVANIA ELECTRIC

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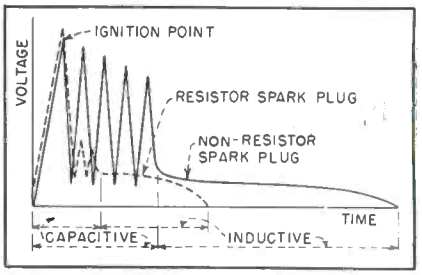
ELECTRONIC DEVICES; RADIO TUBES; CATHODE RAY TUBES; PHOTOLAMPS; FLUORESCENT LAMPS, FIXTURES, WIRING DEVICES, SIGN TUBING; LIGHT BULBS

enormous amount of power is precipitated into the space between two electrodes. In an automotive ignition system with secondary capacitance of 50 $\mu\mu$f discharging at 10 kv, peak amperages of the order of 30 amperes for 2.5×10^{-8} second have been measured. This amounts to a power output of 300,000 watts or 400 hp for 2.5×10^{-8} second. No comparable mechanism with which we are acquainted can precipitate such great amounts of energy as can the spark discharge.

Increased spark plug gap settings are conducive toward ignition of lean mixtures, as are electrodes of small mass and high temperature, located as remotely as possible from any surfaces which might detract



Discharge chart for both types of spark plugs shows that ignition point is practically the same

from the heat content of the initiating sphere of burned mixture.

By incorporating a 10,000-ohm resistor in the spark plug, as is done in the Autolite resistor plug, a very substantial reduction in electrode erosion can be obtained. With resistor plugs set initially at 0.035 inch as against non-resistor plugs set initially at 0.025, after 10,000 miles both types of plugs will have eroded to 0.040.

Resistor plugs do not have a practical detrimental effect upon starting because of the reduced gap erosion and the fact that after use, their required voltage is usually less than that of non-resistor plugs.

By improvements in the magnetic circuit of the average automotive coil, increased voltage can be obtained without increasing primary current. Also, some very high frequency secondary oscillations can be obtained in the portion of the spark discharge immediately following ignition. It is believed that these oscillations, well up in the megacycle range, can and do contribute

Type 1301-A Low-Distortion Oscillator

Here's Your "PROOF-OF-PERFORMANCE"

AS ANNOUNCED by the Federal Communications Commission,* effective August 1, 1949 all a-m and f-m broadcast stations will be required to make proof-of-performance checks of over-all noise and distortion of the complete station at least once a year.

Many stations already make these measurements at frequent intervals as routine operating maintenance to insure the continuous high-quality service the modern transmitter system is capable of supplying.

General Radio instruments for these measurements have been available for some time, and are in regular use by the leading stations where this equipment has given accurate, convenient-to-use and trouble-free service.

The G-R Type 1932-A Distortion and Noise Meter meets all of the F.C.C.'s requirements for measurements of this type for both a-m and f-m services; the Type 1301-A Low-Distortion Oscillator is the ideal companion unit for use with the Type 1932-A. Both of these instruments are relay-rack mounted and can be supplied in panel finishes to match most existing installations.

TYPE 1932-A DISTORTION & NOISE METER

For measurements of sine-wave voltages, distortion and noise throughout the audio range. Over-all pass-band of the voltmeter circuit extends to 45,000 cycles, thus including all noise and distortion products contained in this range; particularly the 3rd harmonic of a 15,000-cycle test is included.

This instrument is continuously adjustable and can be set to any frequency quickly since it has only one main tuning control plus a small trimmer. With it measurements can be made on a-f distortion in radio transmitters, line amplifiers, speech amplifiers, speech input equipment to lines; noise and hum levels of a-f amplifiers, wire lines to the transmitter, remote pick-up lines and other station equipment.

Full-scale deflections on the large meter read distortions of 0.3, 1, 3, 10 or 30 per cent; range for carrier noise measurements extends to 80 db below 100% modulation, or 80 db below an a-f signal of zero dbm level. The a-f range is 50 to 15,000 cycles, fundamental, for distortion measurements and 30 to 45,000 cycles for noise and hum.

Type 1932-A Distortion and Noise Meter: **$575.00**

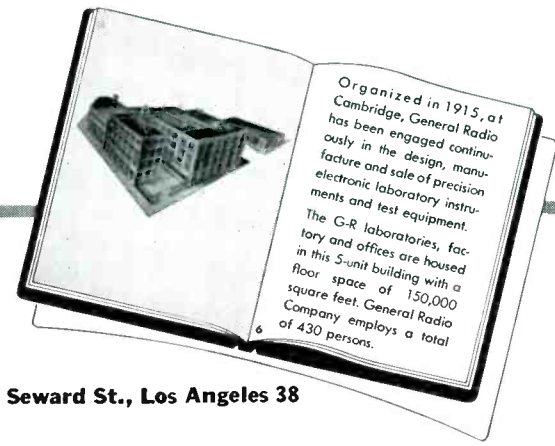
TYPE 1301-A LOW-DISTORTION OSCILLATOR

Especially designed for rapid measurements, this highly-stable oscillator has exceptionally low distortion. By means of push buttons, 27 fixed frequencies between 20 and 15,000 cycles may be selected in logarithmic steps. Any frequency between steps can be obtained by plugging in external resistors. The distortion over the entire range will not exceed the following percentages: with 5,000-ohm output, 0.1% from 40 to 7,500 cycles; 0.15% at other frequencies. With 600-ohm output 0.1% from 40 to 7,500 cycles; 0.25% from 20 to 40 cycles and 0.15% above 7,500 cycles.

The oscillator is calibrated to within $\pm(1\frac{1}{2}\% + 0.1$ cycle); the calibration is not affected by changes in load or plate supply voltage; drift is less than 0.02% per hour after a few minutes operation. The operation of the oscillator is unaffected by ordinary climatic changes.

Type 1301-A Low Distortion Oscillator: **$395.00**

*F.C.C. Rules and Regulations, Sections 3.254 and 3.46, as amended



GENERAL RADIO COMPANY

Cambridge 39, Massachusetts

90 West St., New York 6 920 S. Michigan Ave., Chicago 5 1000 N. Seward St., Los Angeles 38

to the flame propagation process under part-throttle conditions either through the creation of nascent oxygen or mechanically by accelerating the expansion of the initiating sphere of burning gases.

Making Oil from Coal

MEASUREMENT and control of all the major process variables in the high-pressure coal hydrogenation process demonstrated recently at Louisiana, Missouri, presented many new problems to the instrumentation engineers of Bechtel Corporation and the Bureau of Mines.

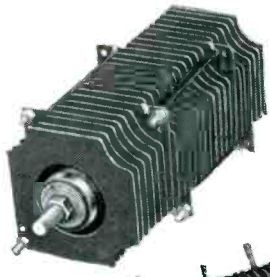
All temperatures in the high-pressure area are measured by means of thermocouples connected to panel-mounted ElectroniK potentiometers which are either indicators, recorders, or recorder-controllers. For control of temperatures, separate Brown ElectroniK circular chart potentiometers equipped with Air O-Line pneumatic control are used. This type of control provides a throttling action of the pneumatic-operated control valves, such that the temperature is maintained close to the desired value in spite of varying requirements for heat in the process.

All pressure recorders, controls, and recorder-controllers in the high-pressure area utilize Bourdon tube elements for measurements. Fisher nonindicating pressure controls are locally mounted on the process equipment, but the Brown recorders and recorder-controllers are located in the control house and connected to locally mounted indicating pneumatic transmitters containing the Bourdon tube elements.

The large majority of gas, liquid, and vapor flows in the hydrogenation process are measured on the differential pressure principle whereby an orifice placed in the flow line creates a pressure drop which is a measure of the rate of fluid flow.

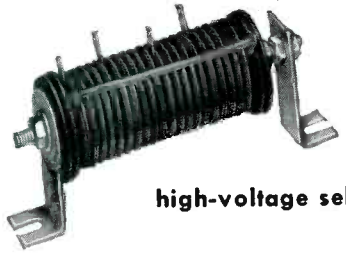
For the measurement of high-pressure flows two different types of nonindicating differential pressure transmitters are utilized, namely: Statham elements for flows to be recorded only, and special Brown electric meter bodies of the mercury manometer type for flows

And which Metallic Rectifier Is Best?



copper-oxide

low-voltage selenium



high-voltage selenium

No one type is "best." Each type of rectifier has characteristics which made it a "natural" for a particular application. For every application there is usually one best type. The correct choice depends upon the application. Here are general recommendations!

GENERAL RECOMMENDATIONS

Where you want	Use	Because
Small size	High-Voltage Selenium	Except for 12 volts and below, fewer high-voltage selenium cells are needed.
Light Weight	High-Voltage Selenium	Selenium-on-aluminum cells are much lighter than copper-oxide.
High Power for a few seconds	Copper-Oxide	Both types will withstand high short-time *current* overloads but only copper-oxide will withstand the higher a-c voltage necessary to deliver short-time high power output.
High current with Low Voltage	Fan Cooled Copper-Oxide	While with fan cooling, selenium can operate at higher current densities than copper-oxide, efficiency will be lower. Copper-oxide aging remains stable.
High Voltage	High-Voltage Selenium	Fewer selenium cells are required.
Low Current at 6 volts or less	Copper-Oxide	Cell for cell, copper-oxide costs less than selenium. Where the minimum number of cells of either type is required, copper-oxide will be *cheaper*.
Long life with unchanged output	Copper-Oxide	While both types appear to have unlimited life. Characteristics of copper-oxide do not change after the first 6 to 12 months of continuous operation. Selenium continues to age—to build up internal resistance with time and particularly with high current densities.
Blocking in D-C Circuits	Copper-Oxide	Selenium tends to "unform" when used as a check valve in d-c circuits or when idle for a period of time (though it reforms quickly when reverse voltage is impressed).
Resistance to Corrosive Atmosphere	Oil-Filled Selenium	Stacks are hermetically sealed in oil, protected against fumes, dirt and dust.

Low-voltage selenium is generally recommended as a compromise between copper-oxide and high-voltage selenium. Where some of the features of both high-voltage selenium and long life copper-oxide are desired, low-voltage selenium would be a logical choice.

To fully meet your needs General Electric makes all three types. If you have a rectifier problem, bring it to us. As we make all three types, we play no "favorites." You can expect an impartial recommendation. Contact your G-E Apparatus Agent or write *Apparatus Dept., General Electric Company, Schenectady 5, New York.*

GENERAL ELECTRIC

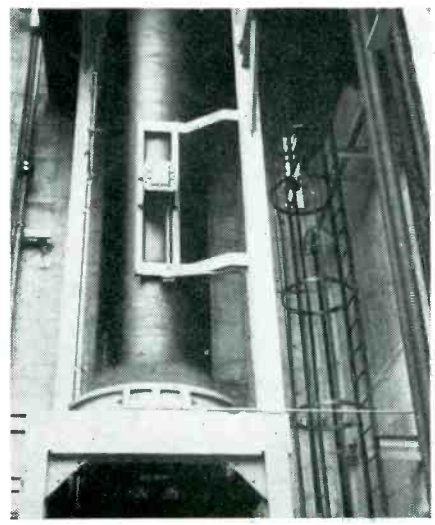
456-14

to be recorded and controlled. Both types employ separate panel-mounted Electronik circular chart potentiometers for recording or control.

The Statham element operates on the principle that stretching or compressing wire causes changes in electrical resistance and that such a change can be a measure of the force acting on the wire. For flow measurement the differential pressure across the orifice plate is connected to the element in such a way that a force in one direction is created on four wires in the element. The wires are arranged so that two tend to be stretched by the force while the other two are compressed. Thus an appreciable resistance change, measured by the potentiometer, is created as an indication of the flow.

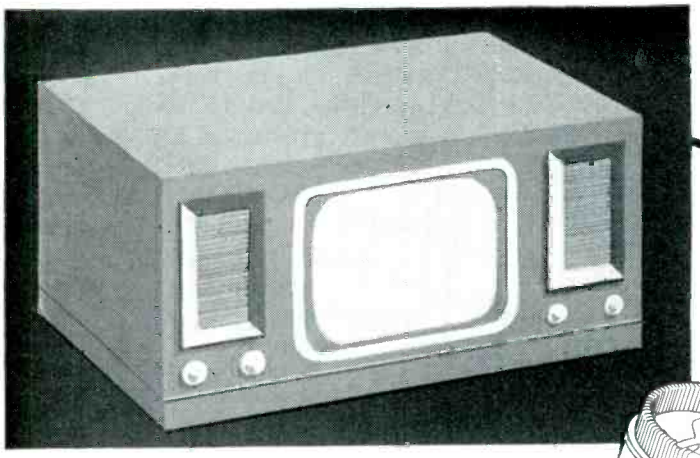
In the low-pressure vessels several designs of nonindicating level controls or alarms as well as level indicators are employed. These are: Fisher displacement type with pneumatic control, Varec float type remote indicator, Bin-Dicator diaphragm type electric alarm, and Taylor diaphragm type with pneumatic transmission of level readings.

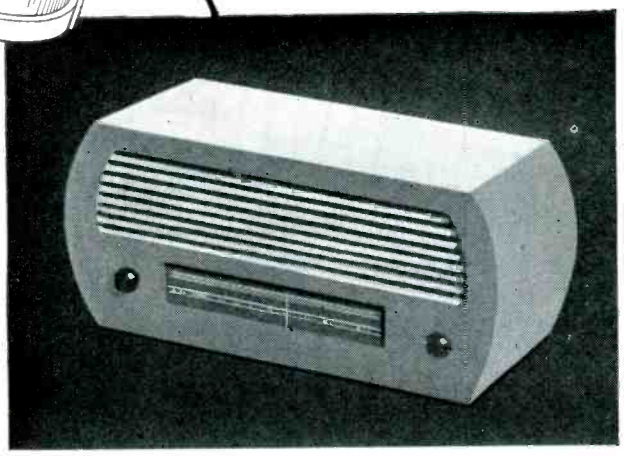
As a check on the composition of the gas streams in both the liquid and vapor phases, several Bailey hydrogen analyzers and recorders, together with Ranarex specific gravity recorders, are used. The gas samples are let down from 700 atmospheres to 10 inches of water



Sensing element of gamma-ray level indicator is square box mounted on side of this hot catchpot

Hook-up wire jacketed with HEAT-RESISTANT DU PONT NYLON PLASTIC approved for temperatures to 90°C.





NEW NYLON-JACKETED WIRE

for Radio, Electrical and Electronic Devices

HEAT-RESISTANT nylon-jacketed wire, made by Gavitt Manufacturing Co., Brookfield, Mass., in two types: 1/64" wall thickness with 300-volt rating, and 1/32" wall thickness with 600-volt rating—both with 5-mil extruded nylon jackets.

Small diameter, light weight, and flexibility among the many *extra* advantages of nylon heat-resistant jackets

The first thermoplastic-insulated wire to receive Underwriters' approval for use in electrical appliances at temperatures to 90°C. is now being made by covering the wire with a jacket of Du Pont nylon plastic.

Only a thin coating of lightweight nylon is needed to provide this added heat-resistance, instead of the heavy asbestos jacket formerly used. Thus this wire has the advantages of *light weight*, *small diameter*, and *flexibility*.

And in addition to raising the heat-resistance of the primary insulation, nylon provides improved resistance to oils, chemicals, and abrasion . . . plus *extra smoothness* for easier pulling.

To help you make better products

Today, manufacturers of electrical wire are finding that a jacket of nylon reduces deformation under load at elevated temperatures, and they are using this property to help meet the increasing demand for heat-resistant wiring. Nylon can help you make many electrical products better. This Du Pont plastic can be extruded over bare wire or over primary insulation. It can be molded into thin sections and intricate shapes, and around metal inserts.

How can you take advantage of its unusual properties? To see how other manufacturers are using nylon profitably, and for valuable information on molding and extrusion of nylon, write for free booklets.

E. I. du Pont de Nemours & Co. (Inc.), Plastics Department.

MAIN SALES OFFICES: 350 Fifth Avenue, New York 1, N. Y.; 7 So. Dearborn Street, Chicago 3, Illinois; 845 E. 60th Street, Los Angeles 1, California.

DU PONT
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Plastics
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. . . THROUGH CHEMISTRY

through capillary tubing, which also tends to reduce the time lag of measurement. The hydrogen analyzer operates on the thermal conductivity principle, measuring the hydrogen content of the sample by its cooling effect on an electrically heated wire as compared to that of a standard.

The specific gravity recorder operates on the principle that the turning force imparted by the gas sample on an impeller-type fan wheel is directly related to the specific gravity of the gas. The turning force of air on a similar fan wheel is opposed to the sample wheel as a basis for comparison, and the difference in the two forces is mechanically connected to the instrument indicating pointer and the recording pen.

Combustion Check

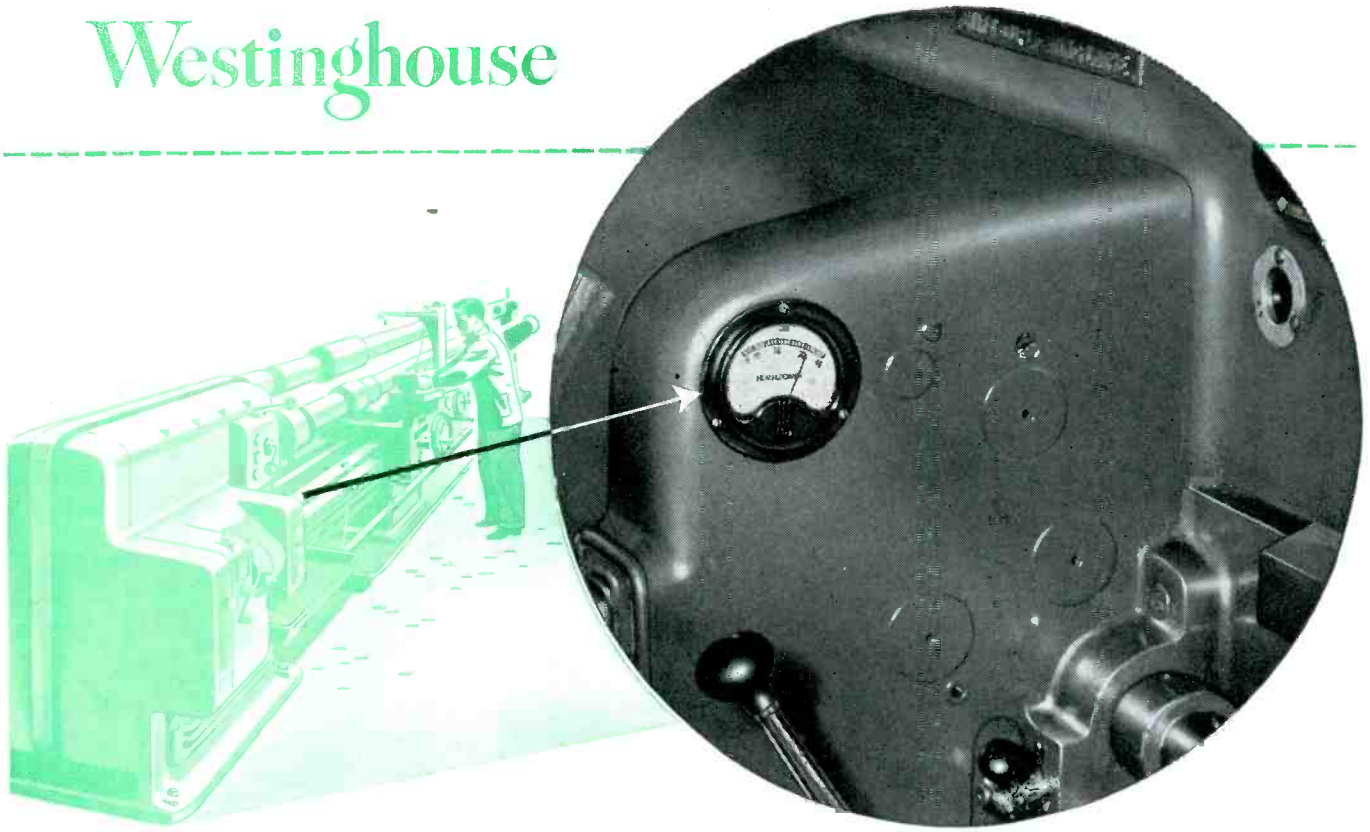
To insure safe combustion of the fuel gas in the paste and vapor phase preheaters and in several other portions of the process, Protectoglo combustion safeguard controls detect the presence or absence of a flame by electrodes inserted at the burners. In the event of flame failure, they function to shut off the fuel supply as well as to energize alarm signal lights and horns in the control room.

The major phase of the coal hydrogenation process from the instrument viewpoint is the high-pressure area. Industrial instruments used for automatic control of coal preparation in this operation are panel-mounted on the ground floor of the coal preparation building and include (1) a Foxboro temperature controller on the furnace which supplies hot gases used to dry the pulverized coal in the ball mill; (2) a Wheelco combustion safeguard system on the fuel supply of the gas furnace; and (3) a Bailey oxygen analyzer and recorder for the gases out of the furnace.

Of particular interest is the special Kennedy Van Saun device for controlling the level of pulverized coal in the ball mill by operation of a Bailey disc feeder on the crushed coal inlet line. The control comprises a panel-mounted unit which contains a small glass U-

YOU CAN BE **SURE**.. IF IT'S

Westinghouse



This Westinghouse Instrument helps set *New Production Records*

Savings in machine time up to 75% are common among the users of the American Tool Works Company's new hydraulic duplicating lathes!

A standard feature of these lathes is the Westinghouse horsepower instrument. It shows, at a glance, the horsepower being consumed by the cut. This enables the operator to take full advantage of the capabilities of the machine and to make maximum cuts without overloading. Machines can be easily operated at peak loads, without the dangers of overtaxed motors and damaged cutting tools.

This is another example of the application of Westinghouse instruments to *specific* problems. Westinghouse instruments are *engineered* and built to give you reliable performance in *every* application. The completeness of the line means electrical measuring instruments to fill *your* needs exactly in every field of industry.

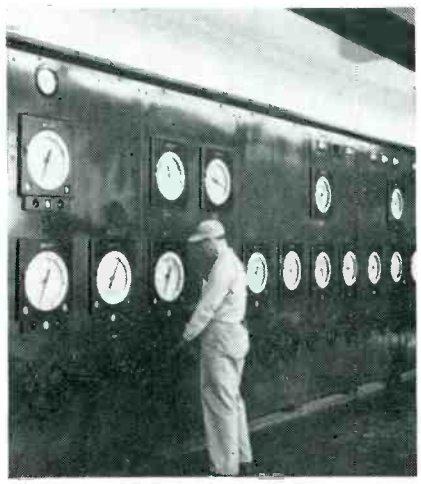
Westinghouse instrument specialists are available in the field for consultation. Call your nearest Westinghouse office or write Westinghouse Electric Corporation, P. O. Box 868, Pittsburgh 30, Pennsylvania. J-40373

Westinghouse

ELECTRICAL MEASURING INSTRUMENTS FOR *ANY* JOB

tube, one side of which is connected to a vertical tube installed in the ball mill to the level control point. This tube is normally subjected to the draft pressure in the mill when the level is below its bottom end and results in a certain level of liquid in the U-tube. When the level reaches the bottom of this tube, the change in pressure causes the U-tube liquid level to change and intercept a photoelectric cell which electrically actuates the coal feeder.

Primary instruments used in paste preparation include: (1) three Taylor indicating level gages connected to diaphragm-type transmitters installed on the bottom of

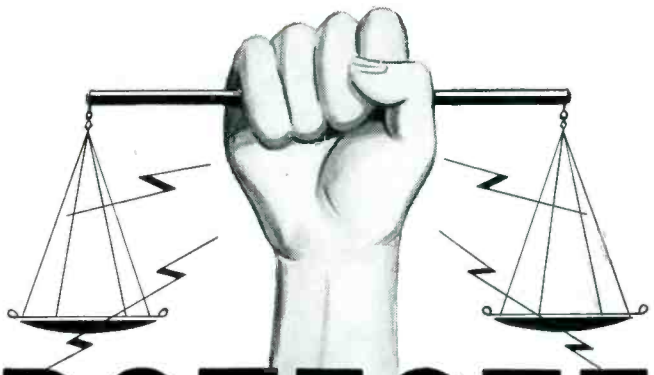


Some electronic gear of the recorder-controllers for liquid level, flow and temperature used in coal to oil conversion

the paste feed and other storage tanks, (2) three Jeffrey Waytrol control units for the automatic weighing scales which proportion the amounts of pulverized coal and dry catalysts to the paste mixer, and (3) a Brown recording paste oil flow controller which regulates the amount of oil to solids in the paste mixer.

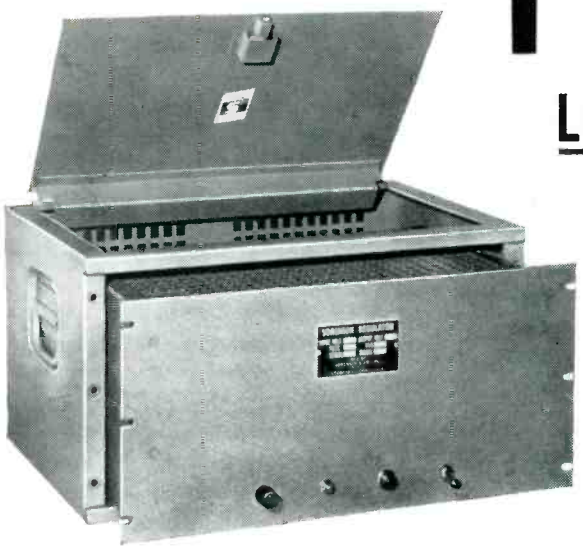
In this stage of the process a number of auxiliary control devices are used for high limit and supplementary control functions. For example, high and low level Bin-Dicator alarms are installed on the pulverized coal storage bin. Also, Taylor self-operated thermometer-actuated control valves are used on such service as regulating glow-pressure steam to the jacket of the coal paste mixer and to the paste feed storage tank, as a means of temperature control. Fisher displacement type level controls are

operate in safety



WITH FULLY PROTECTED

LINE AND LOAD STABILIZATION



Sorensen Electronic Voltage Regulators *alone* give you all these extra safety features:—

- Full protection against both line and load changes from *one* instrument.
- Overvoltage protection using the special Safety Diode, developed by Sorensen for hair line precision.
- Additional protection against overvoltage by use of a Heinemann Circuit Breaker.
- Protection against overload through a Klixon Overload Protector.

The Sorensen Voltage Regulator is simple and compact, easy to install. It has *only four tubes* — all standard except the special Sorensen Diode*. It is designed to fit in a small space — ideal for either relay rack mounting or cabinet mounting.

Don't take chances! There is one sure, safe protection for delicate instruments and complex equipment — *Sorensen Voltage Regulators.*

SPECIFICATIONS
for the 1000S Model

Input Voltage Range	95—125 V.
Output Voltage Range	adjustable between 110—120 V.
Output Load Range	0—1 KVA
Regulation Accuracy	± 0.1% against line ± 0.2% against load
Harmonic Distortion	less than 2%
Power Factor Range	down to 0.7 P. F.
Recovery Time	3 to 6 cycles
Line Frequency Range	50 to 60 cycles

Other Models from 150 VA to 15 KVA single phase and 45 KVA three phase.

NOBATRON and B-NOBATRON

Send for information on these highly stabilized D. C. Regulators.

Literature Available! Send for your Saturable Core Reactor Data Booklet — It's FREE.

NEW 400 CYCLE REGULATORS

Two 400 cycle regulators of higher capacity than previously advertised are now available in the Sorensen 400 cycle line.

These units, primarily designed for aircraft, are compact and lightweight. Working from a 115 VAC, 400 cycle source, the regulators will hold the output at 115 VAC at an accuracy of 0.5% over a wide input frequency and voltage range. The capacities of the regulators are 1200 and 2000 VA.

TECHNICAL SPECIFICATIONS

Input Voltage Range	**95 to 125 volts**
Output Voltage Range	**110 to 120 volts**
Regulation Accuracy	**0.5%**
Inductive Power Factor Range	**Down to 0.7 P. F.**
Ambient Temperature Range	**—55°C to +70°C**
Input Frequency Range	**400 to 2400 cycles**

Sorensen and Company, Inc.

375 Fairfield Ave., Stamford, Connecticut

also used on vessels in this portion of the process.

One unusual instrument application is the Brown area meter which measures the flow of viscous paste from storage to the preheaters. This unit operates on the inductance bridge principle and utilizes changes in area through a variable orifice with a fixed differential pressure as the basis for flow measurement.

Two Level Indicators

Measurement and control of the heavy oil level was probably the most difficult instrumentation problem to solve in connection with the hot catchpot. Should the level in this vessel go too low, all pressure in the system would be lost; should the level rise too high, failure to make separation of the lighter hydro-carbons and hydrogen from the heavy oil could occur. Two methods of measurement are employed and arranged so that either can be used to control the level.

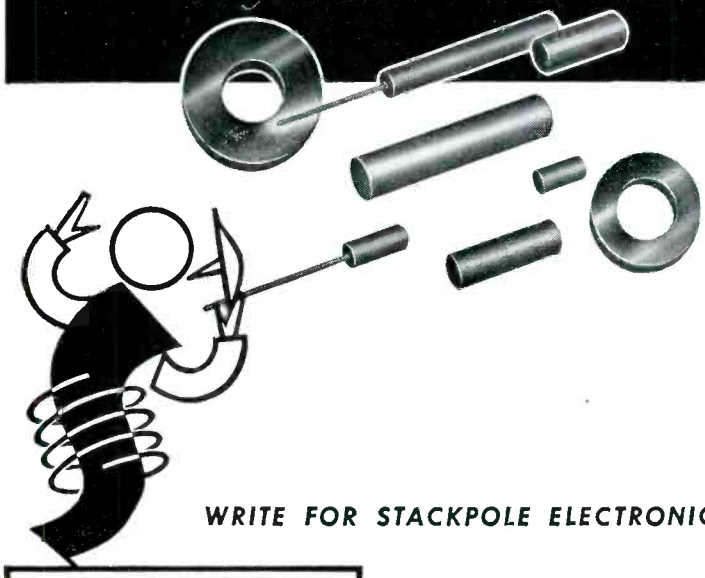
In one arrangement, a Brown high-pressure mercury manometer measures the differential pressure between two hydrogen purge lines. One line is connected to the upper vapor space of the catchpot; while the outlet of the other line, which passes vertically down through the liquid, is located slightly less than two feet above the bottom of the vessel. It is desired to maintain the level about five feet above the bottom of the vessel.

Equal flows are maintained in both purge lines so that the pressure difference is due only to the liquid head in the hot catchpot. Hydrogen flows through these tubes must also be sufficient to prevent asphalt from creeping back onto the lines.

Level readings are transmitted electrically to an electronic recorder and pneumatic controller on the main instrument control panel. This latter instrument automatically controls the heavy oil level by throttling the flow of heavy oil through a diaphragm motor valve located on the heavy oil outlet line.

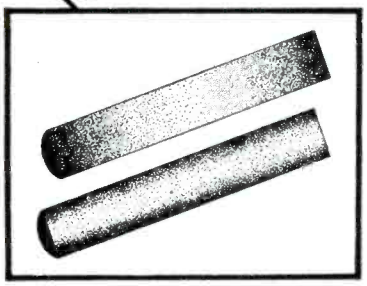
The second method of checking and alternately controlling the above level is accomplished by a Geiger-Muller detector, known as the Gagetron, which is installed on

IT'S STACKPOLE FOR IRON CORES!



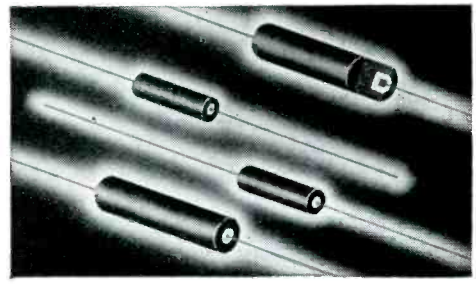
The rapid increase in the use of molded iron cores throughout electronic engineering has resulted in large part from Stackpole engineering that has made new and improved types available at attractive prices. In addition to dozens of standard broadcast, permeability tuning and high frequency types, Stackpole offers numerous others, a few of which are illustrated below.

WRITE FOR STACKPOLE ELECTRONIC COMPONENTS CATALOG RC-7



◀ SIDE MOLDED

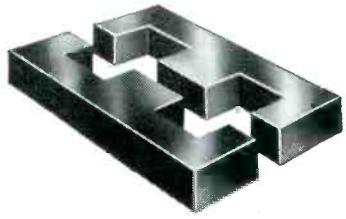
Extra density of pressure extends evenly the entire length of the core. Resulting uniform permeability makes Stackpole Side-Molded Cores outstandingly superior for tuning applications. Broadcast band and short-wave types available.



TRANSFORMER CORES ▶

for filter coils in carrier frequency equipment.

Assure constant inductance over a given frequency range. Widely used where constant inductance, limited only by predetermined saturation point of core, is needed for various currents.

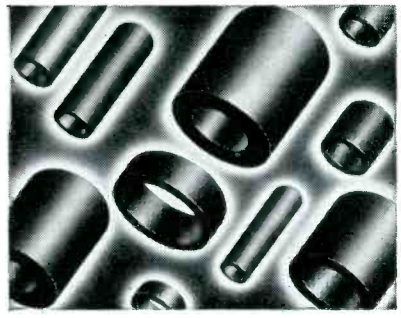


CHOKE COIL CORES ▲

Ideal for audio, "hash," r-f chokes and others. Reduce coil dimensions and increase "Q." Insulated leads connect to coil and permit point-to-point wiring. Frequency ranges from 100 cycles to 175 megacycles.

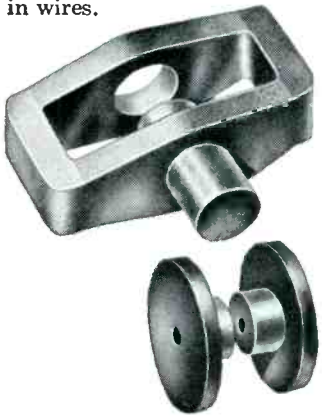
HIGH-RESISTIVITY CORES

Made of a special material showing resistance of practically infinity. Reduce leakage currents and noise troubles, minimize voltage breakdown possibilities between coils and core; and, where cup cores are used, eliminate heavily insulated lead-in wires.



◀ SLEEVE CORES

By permitting use of smaller cans of less critical and less costly materials, these cores assure a high order of tuning efficiency in greatly reduced size. In some instances, it may not even be necessary to use cans.

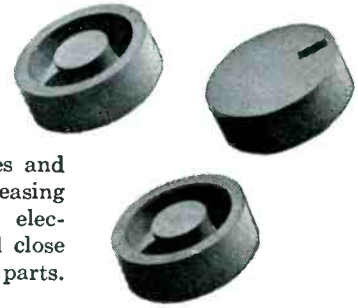


◀ TELEVISION CORES

From horizontal deflection and flyback transformer cores to I.F. and other types, Stackpole offers a complete line. The types illustrated here assure remarkably uniform results, save on assembly costs.

CUP CORES ▶

These unique, self-shielding units are available in a wide range of shapes and sizes and are finding steadily increasing use throughout modern electronics. Can be mounted close to chassis or other metal parts.



ELECTRONIC COMPONENTS DIVISION

STACKPOLE CARBON COMPANY, St. Marys, Pa.

the outside of the vessel. This unit detects gamma rays which are emitted by a radium salt contained in an iridium-platinum needle mounted on the pyrometer tube located inside the vessel. The gamma-ray absorption properties of the heavy oil differ sufficiently from the vapors and gases in the vessel so that this device serves well to detect the heavy oil level. This type of measurement is not influenced by changes in temperature, pressure, or chemical composition of the fluids in the vessel.

Impulses received by the Gagetron are amplified and transmitted to a Brown electronic recording controller located on the main instrument control panel. Hand valves in the control air lines from the two level controllers are provided so that either can be used to operate the control valve.

Compact Microwave Signal Generator

By William Eisner
Leru Laboratories
New York, N. Y.

The klystron signal generator to be described provides a handy source of microwave energy for use in studying uhf phenomena, as a demonstration unit to illustrate microwave beacon systems, or as a piece of test equipment for making sensitivity and signal-to-noise measurements on microwave receivers. The unit employs a 2K25 klystron operating at approximately 10,000 mc, and either modulated or continuous-wave output is available.

The unit consists of three main sections: the rather unique circuits used for modulating the klystron output, the scope and its associated circuits to give a visual indication of the modulating pulses, and the power supply section.

The klystron signal generator utilizes a system of modulation which was developed by Robert Rudin, formerly associated with the Leru Laboratories. The system is based on the intermittent generation of a carrier of constant amplitude with the ratio of on to off periods being varied.

To illustrate this principle, let us

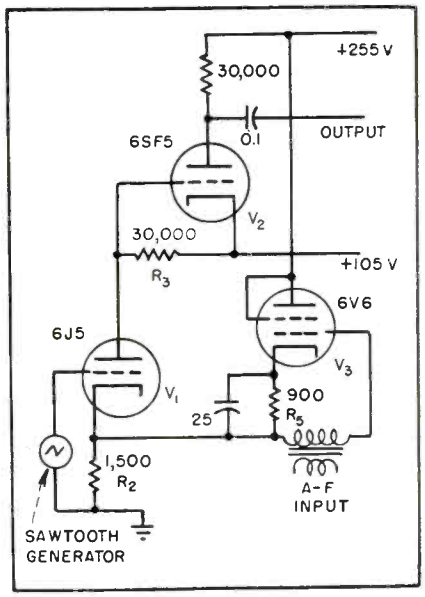


FIG. 1—Circuit diagram of unique modulator used in microwave signal generator

suppose that the emission of an r-f wave is being interrupted at a certain rate and that the on periods are as long as the off periods; the envelope will then be a square wave. If this signal is then detected at the receiver by a diode rectifier, the diode current will follow the envelope and the resulting square wave, if averaged over a period of time, will assume a steady value. If now the ratio of on to off periods is changed so that the emission is on longer than off, the average diode current at the receiver will increase. Lengthening the off periods and shortening the on periods will result in a reduction of diode current.

It is convenient to keep the repetition rate (25,000 pps) of the pulses constant and vary the length of the on periods. Also instead of completely cutting off the emission of the carrier wave during the off periods, its amplitude can be reduced to a constant predetermined fraction of the amplitude during the on periods. It is seen that the relative variations of diode current depend only on the ratio of on to off periods and are independent of the actual amplitude. It is therefore possible to pass the received signals thru amplitude-limiting devices before detecting them and in this way practically eliminate the influences of variations in transmission.

To accomplish the cutting on and

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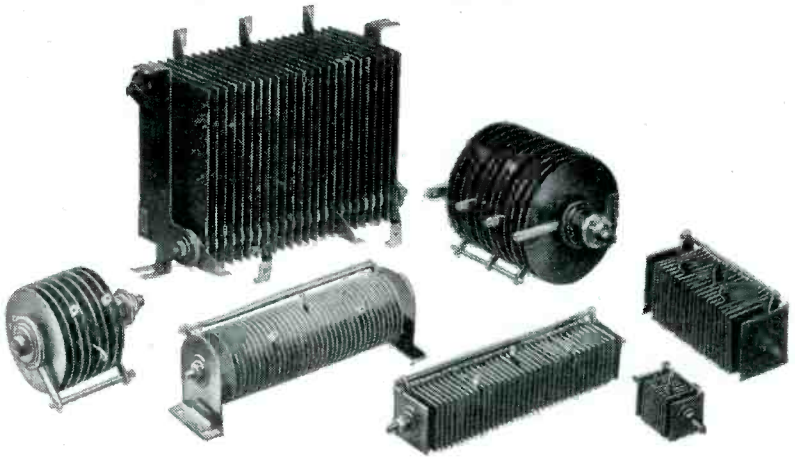

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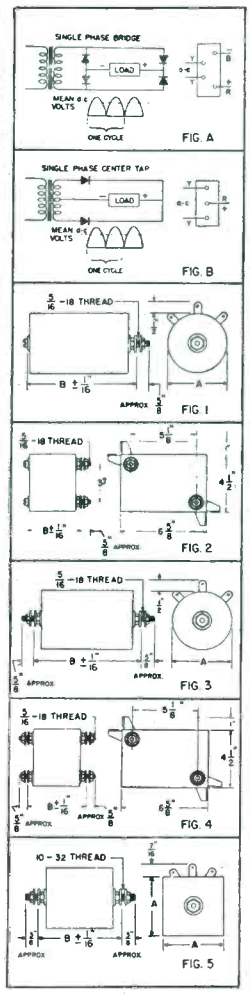

D.C. OUTPUT VOLTS	D.C. OUTPUT AMPS	RECTIFIER STACK CODE NUMBER	APPROX. A.C. INPUT VOLTS NEW	APPROX. A.C. INPUT VOLTS MAX.	CIRCUIT AND STACK CONN. DIAGRAM	RECTIFIER STACK DIMENSIONS A	RECTIFIER STACK DIMENSIONS B ± 1/16"	RECTIFIER STACK DIMENSIONS FIG.	CATALOG NUMBER
	2	6C1ABLX1	8	9		3⅜"	1 9/16"	1	2001
	4	7C1ABLX1	8.2	9		4⅜"	1 9/16"	1	2002
6	6	233C1ABLX1	8.5	11	'B'	4⅜"	1¾"	1	2003
	8	28C1ALX1	8.2	9		6⅝"x4½"	1½"	2	2004
	12	234C1ALX1	8.5	11		6⅝"x4½"	1 15/16"	2	2005
	2	6B1ABLX1	9	18		3⅜"	2 1/16"	1	2006
	4	7B1ABLX1	9.4	18		4⅜"	2 1/16"	1	2007
6	6	338B1ABLX1	10	18	'A'	4⅜"	2 11/16"	1	2008
	8	28B1ALX1	9.4	18		6⅝"x4½"	2 1/16"	2	2009
	12	34B1ALX1	10	18		6⅝"x4½"	2 11/16"	2	2010
	2	6B1ABLX1	16	18		3⅜"	2 1/16"	1	2011
	4	7B1ABLX1	16.3	18		4⅜"	2 1/16"	1	2012
12	6	233B1ABLX1	16.8	22	'A'	4⅜"	2 11/16"	1	2013
	8	28B1ALX1	16.3	18		6⅝"x4½"	2 1/16"	2	2014
	12	234B1ALX1	16.8	22		6⅝"x4½"	2 11/16"	2	2015
	2	6B2ALX1	32	36		3⅜"	3 9/16"	3	2016
	4	7B2ALX1	32.6	36		4⅜"	3 9/16"	3	2017
24	6	233B2ALX1	33.6	44	'A'	4⅜"	5"	3	2018
	8	28B2ALX1	32.6	36		6⅝"x4½"	3⅝"	4	2019
	12	234B2ALX1	33.6	44		6⅝"x4½"	5"	4	2020
	2	206B2ALX1	41	44		3⅜"	3 9/16"	3	2021
	4	207B2ALX1	41.5	44		4⅜"	3 9/16"	3	2022
32	6	133B2ALX1	42.5	52	'A'	4⅜"	5"	3	2023
	8	228B2ALX1	41.5	44		6⅝"x4½"	3⅝"	4	2024
	12	134B2ALX1	42.5	52		6⅝"x4½"	5"	4	2025
	2	106B2ALX1	45	52		3⅜"	3 9/16"	3	2026
	4	107B2ALX1	45.5	52		4⅜"	3 9/16"	3	2027
36	6	133B2ALX1	46.7	52	'A'	4⅜"	5"	3	2028
	8	128B2ALX1	45.5	52		6⅝"x4½"	3⅝"	4	2029
	12	134B2ALX1	46.7	52		6⅝"x4½"	5"	4	2030
	2	206B3ALX1	61.5	66		3⅜"	4½"	3	2031
	4	207B3ALX1	62	66		4⅜"	4½"	3	2032
48	6	133B3ALX1	63.5	78	'A'	4⅜"	6¾"	3	2033
	8	228B3ALX1	62	66		6⅝"x4½"	4 13/16"	4	2034
	12	134B3ALX1	63.5	78		6⅝"x4½"	7 1/16"	4	2035
	.5	104B6SALX1	148	156		1 17/32" sq.	4⅞"	5	2036
	1.	105B6ALX1	148	156		2⅝"	7⅝"	3	2037
120	2.	106B6ALX1	149	156	'A'	3⅜"	7⅝"	3	2038
	4	107B6ALX1	151	156		4⅜"	7⅝"	3	2039
	6	133B7ALX1	157	182		4⅜"	14⅛"	3	2040

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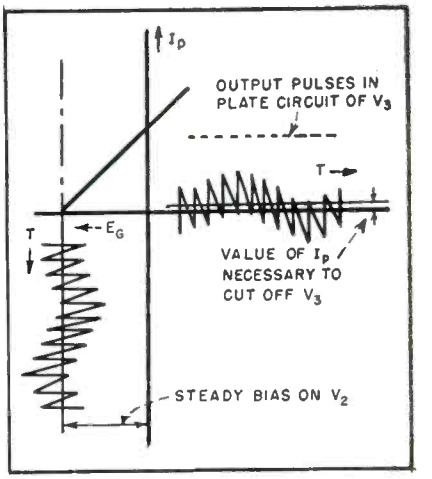
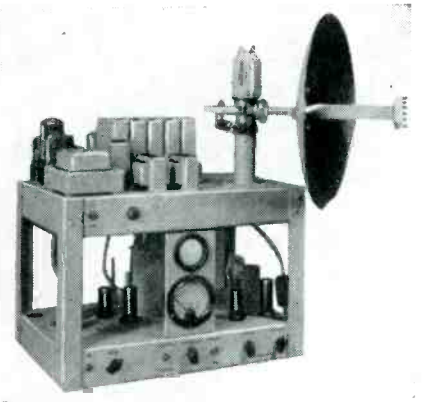


FIG. 2—Curve of E_G vs I_P showing how length of output pulses is changed by modulator shown in Fig. 1

off of the 2K25 klystron output in a practical way, the circuit of Fig. 1 is used. A sawtooth voltage is applied to V_1. The cathode of V_1 is biased by the voltage output of the cathode-follower triode V_3 which in turn is modulated by the a-f input. The steady cathode bias of V_1 is determined by R_5 which also determines the grid bias of V_3. The drop in the cathode resistor R_2 determines the bias of V_1 and determines the ratio of on to off of V_1. The plate current of V_1 is carried thru R_3 and the voltage drop of the plate current thru R_3 is applied to the control grid of V_2. The length of the plate current pulses in V_2 are the on and off periods desired (see Fig. 2). These pulses are amplified and used to turn the Klystron plate voltage on and off.

The front panel controls provide a means for varying the klystron repeller voltage and thereby vary the r-f frequency within narrow



Compact microwave signal generator capable of producing modulated or unmodulated r-f at approximately 10,000 mc. Scope monitors modulating pulses, and meter reads average klystron cathode current

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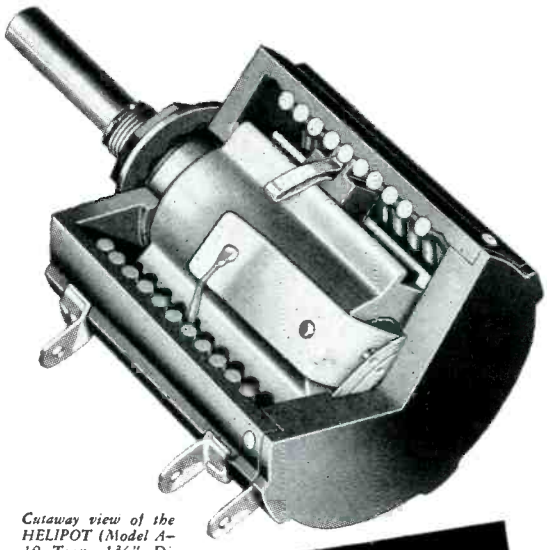

Cutaway view of the HELIPOT (Model A–10 Turn–1¾" Diameter)

THE BECKMAN Helipot

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Provides *many times* greater resistance control in *same* panel space as conventional potentiometers!

IF YOU are designing or manufacturing *any type* of precision electronic equipment be sure to investigate the greater convenience, utility, range and compactness that can be incorporated into your equipment by using the revolutionary HELIPOT for rheostat-potentiometer control applications...and by using the new DUODIAL turns-indicating knob described at right.

Briefly, here is the HELIPOT principle...whereas a conventional potentiometer consists of a *single* coil of resistance winding, the HELIPOT has a resistance element *many times* longer coiled *helically* into a case which requires no more panel space than the conventional unit. A simple, foolproof guide controls the slider contact so that it follows the helical path of the resistance winding from end to end as a single knob is rotated. Result...*with no increase in panel space requirements*, the HELIPOT gives you as much as 12 times* the control surface. You get far greater accuracy, finer settings, increased range–with maximum compactness and operating simplicity!

COMPLETE RANGE OF TYPES AND SIZES

The HELIPOT is available in a complete range of types and sizes to meet a wide variety of control applications...

MODEL A: *5 watts, 10 turns, 46" slide wire length, 1¾" case dia., resistances 10 to 50,000 ohms, 3600° rotation.*

MODEL B: *10 watts, 15 turns, 140" slide wire length, 3¼" case dia., resistances 50 to 200,000 ohms, 5400° rotation.*

MODEL C: *3 watts, 3 turns, 13½" slide wire length, 1¾" case dia., resistances 5 to 15,000 ohms, 1080° rotation.*

MODEL D: *15 watts, 25 turns, 234" slide wire length, 3¼ case dia., resistances 100 to 300,000 ohms, 9000° rotation.*

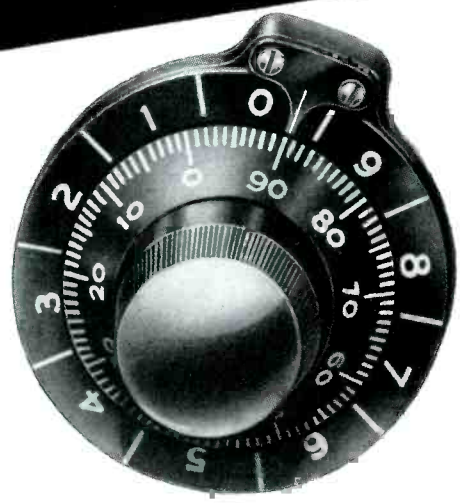
MODEL E: *20 watts, 40 turns, 373" slide wire length, 3¼" case dia., resistances 150 to 500,000 ohms, 14,400° rotation.*

Also, the HELIPOT is available in various special designs...with double shaft extensions, in multiple assemblies, integral dual units, etc.

Let us study *your* potentiometer problems and suggest how the HELIPOT can be used–possibly is already being used by others in your industry–to increase the accuracy, convenience and simplicity of modern electronic equipment. No obligation, of course. Write today outlining your problem.

**Data for Model A, 1¾" dia. Helipot. Other models give even greater control range in 3" case diameters.*

THE BECKMAN Duodial



The inner, or Primary dial of the DUODIAL *shows exact angular position of shaft during each revolution. The outer, or Secondary dial shows number of complete revolutions made by the Primary dial.*

A multi-turn rotational-indicating knob dial for use with the HELIPOT and other multiple turn devices.

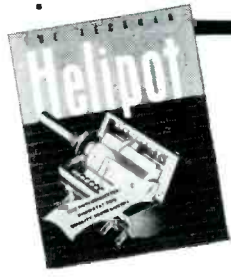
THE DUODIAL is a unique advancement in knob dial design. It consists essentially of a primary knob dial geared to a concentric turns-indicating secondary dial–and the entire unit is so compact it requires only a 2" diameter panel space!

The DUODIAL is so designed that–as the primary dial rotates through each complete revolution–the secondary dial moves one division on its scale. Thus, the secondary dial counts the number of complete revolutions made by the primary dial. When used with the HELIPOT, the DUODIAL registers *both* the angular position of the slider contact on any given helix as well as the particular helix on which the slider is positioned.

Besides its use on the HELIPOT, the DUODIAL is readily adaptable to other helically wound devices as well as to many conventional gear-driven controls where extra dial length is desired without wasting panel space. It is compact, simple and rugged. It contains only two moving parts, both made entirely of metal. It cannot be damaged through jamming of the driven unit, or by forcing beyond any mechanical stop. It is not subject to error from backlash of internal gears.

TWO SIZES—MANY RATIOS

The DUODIAL is now available in two types–the Model "R" (illustrated above) which is 2" in diameter, and the new Model "W" which is 4¾" in diameter and is ideal for main control applications. Standard turns-ratios include 10:1, 15:1, 25:1 and 40:1 (ratio between primary and secondary dials). Other ratios can be provided on special order. The 10:1 ratio DUODIAL can be readily employed with devices operating *fewer* than 10 revolutions and is recommended for the 3-turn HELIPOT. In all types, the primary dial and shaft operate with a 1:1 ratio, and all types mount directly on a ¼" round shaft.



Send for this HELIPOT AND DUODIAL CATALOG!

Contains complete data, construction details, etc., on the many sizes and types of HELIPOTS...and on the many unique features of the DUODIAL. Send for your free copy today!

THE Helipot CORPORATION, SOUTH PASADENA 2, CALIFORNIA

limits. The klystron can also be operated continuous wave. If the klystron is to be evenly pulsed (no modulation), the centering control is used to vary the length of the pulse, and this modulating pulse can be seen on the scope. The meter on the front panel gives the average klystron cathode current.

The output of the microwave generator may be radiated by the antenna system, shown in the photograph, which is mounted on a swivel arrangement so that the r-f can be radiated in any desired direction. Or the parabolic reflector and end piece may be removed and a 3-cm waveguide clamped in place and used to pipe the microwave signal to the desired location.

Generator Regulation by Saturable Reactors

By T. A. Benham
Assistant Professor in Physics
Haverford College
Haverford, Pennsylvania

An existing 24-volt d-c generator had a rather poor regulation characteristic. It was desired to design a simple compensating system without the use of vacuum tubes as that method would entail relatively expensive tubes, and the control would be as costly as the generator itself. Since the author had had some experience with the use of saturable reactors for both controls and amplifiers, efforts were directed along

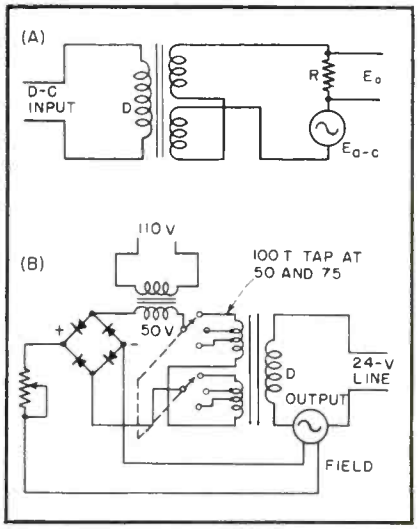


FIG. 1—Schematic diagrams of (*A*) basic saturable reactor circuit, and (*B*) the actual circuit for using a saturable reactor to control the voltage output of a generator

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these lines experimentally.

The theory and function of such reactors are fairly common knowledge, therefore only a brief explanation will be given here. If a three-leg laminated core of the E-I type is arranged with windings on each leg and with the outside pair connected in series-aiding, then there will be no transformer action between this pair of windings and the center coil.[1,2,3] This is because the flux from one outside coil goes directly from one outside leg to the other without going through the center leg. However, flux due to a current in the center leg passes through the outside legs. The inductance, and hence the reactance, of the outside coils is a function of the permeability of the core material. If direct current is passed through the center coil, the resulting steady flux causes the permeability of the outside legs to become smaller thus reducing the reactance of these coils. Figure 1A shows how this principle may be used to vary the voltage appearing across R as the direct current through D is changed.

Now suppose R is replaced by a dry-disc rectifier while the d-c output of the rectifier is connected to the field winding of the generator to be regulated. Further, suppose the output current of the generator is caused to flow through the center winding D in Fig. 1B. With no load current being drawn from the generator, the field rheostat is varied to obtain the proper generator output voltage.

Of course, the rectifier must be capable of delivering the rated field current, and the a-c source must supply a voltage which is larger than the desired field voltage by an amount equal to the drop across the outside coils of the reactor plus the losses in the rectifier.

When the initial adjustments have been made, a load may be connected to the generator. The current flows through coil D thus reducing the reactance of the coils in series with the field supply. This results in an increase in field excitation and an increase in the generated voltage.

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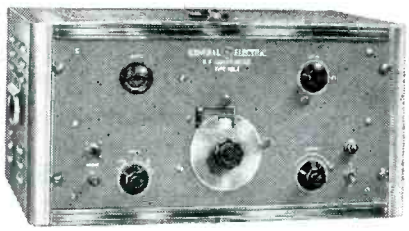

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- Output voltage 0-75 volts.
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- Rise time .3 microsecond.

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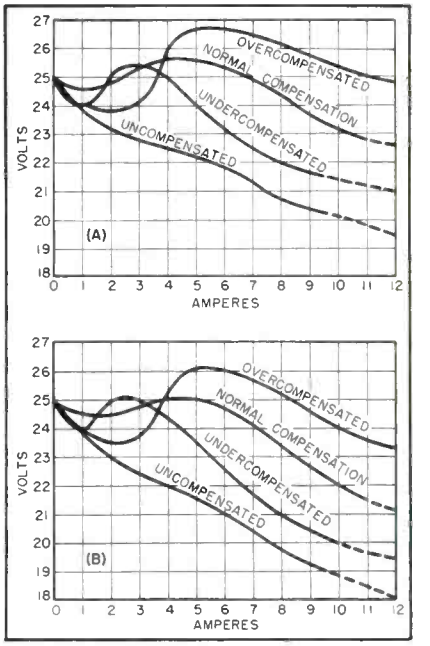


FIG. 2—Response curves for saturable reactor-controlled generator. Curves in (*A*) are taken at generator output terminals, while those in (*B*) are from the end of a 0.12-ohm line

will run away, and the generator might be permanently damaged. Proper fusing, therefore, is indicated. However, in the model under discussion, the amount of compensation could be adjusted by selecting the proper taps on the series coils as shown in Fig. 1B. It was found that 75 turns on each coil gave satisfactory compensation while 100 turns on each resulted in slight over-compensation (Fig. 2A). Still more turns would overcompensate sufficiently to permit the use of a long line.

For the purpose at hand, the system is entirely satisfactory. However, there is one serious disadvantage for certain applications where rapid response is required. Because of the lag in the magnetic effects in the core, the voltage regulation is poor for sudden changes in load. For example, when full load is removed suddenly, the voltage momentarily jumps up by an amount of approximately 10 percent and then settles back to the original value.

References

(1) Alan S. FitzGerald, Magnetic Amplifier Characteristics — Neutral Type, *J. Frank. Inst.*, p 249, Oct. 1947; and p 415, Dec. 1947.

(2) Alan S. FitzGerald, Some Notes on the Design of Magnetic Amplifiers, *J. Frank. Inst.*, p 323, Nov. 1947.

(3) Frank G. Logan, Saturable Reactors and Magnetic Amplifiers, ELECTRONICS, p 104, Oct. 1948.

(continued from p 122)

many of its properties. In some ways HeII acts as though it has no viscosity, flowing through virtually vacuum-tight openings and up the side of a containing vessel in apparent defiance of gravity. At the transition temperature the thermal conductivity of HeI increases very abruptly to an apparent value for HeII much greater than that of any other substance. This is because heat is propagated in HeII as a kind of wave motion analogous to sound and known as "second sound," whereas in other materials heat flow is purely a diffusion phenomenon. All of these effects may be explained by the presence in HeII of a superfluid. The atoms of the superfluid have had their energies reduced by cooling to the point where thermal motion has almost ceased, yet the intermolecular forces are not great enough to produce a rigid solid. As a result, viscosity practically disappears, and other remarkable properties are observed.

Second sound has recently been obtained at the National Bureau of Standards through use of liquid helium produced in a new Simon-type liquefier. Unlike ordinary sound, second sound is generated thermally and can be detected only by temperature-sensitive devices, rather than by microphones. The present investigation employs a recently developed pulse method so that signals that would otherwise be quite difficult to detect are presented on an oscilloscope screen for visual observation. Pulses of heat generated electrically within liquid HeII travel through the helium and are detected upon arrival at a temperature-sensitive element; meanwhile, their transit time is measured accurately by electronic timing circuits.

Bombardment of Semi-Conductors with Neutrons

BY ADDING carefully controlled amounts of impurity atoms to pure silicon and germanium, it is possible to produce at will semi-conductors which owe their conductivity at room temperature primarily to carriers released by ionization of the impurity centers. Any of the ele-

MARGIN CONTROL RECORDING BOOSTS MICROGROOVE RANGE

By A. C. Travis, Jr.*

For some time now Mercury Records have carried a little notation on their record envelopes explaining that the recording was done by a special process called, "Margin Control". That many recordists are not familiar with the meaning of these words is evidenced by the fact that we have so many times been asked for an explanation. Credit for the technique goes, according to all indications, to Bob Fine of Reeves Sound Studios. An interpretation of "Margin Control" follows in the form of a quotation from the external house organ of a famous manufacturer of blank records for both master and instantaneous recording.

"It seems that one of the major tactical problems in the ten inch versus seven inch microgroove war is the problem of the crescendo (evidently an old Mexican word meaning a noise that grows so loud it wakes up the customers). Now, when one of these crescendo passages comes along in microgroove recording, naturally the cutting stylus starts beating from side to side with such ferocity, that, while it cuts, it also displaces land material sufficiently to distort the adjoining groove. The resulting echo, even with the best discs, has relegated many master recordings to the reject pile. The obvious remedy of reducing volume cuts dynamic range, but, of course, when an irresistible force meets an immovable object, something has to give. Bob Fine gave—with an idea. He runs through the original recording or live number and "scores" it by plotting VU meter readings against time. Then, using new Fairchild equipment wherein lines-per-inch are infinitely variable from approximately ninety to five hundred, he makes the master fine-line recording by monitoring the lines-per-inch so that spacing is finest on lowest passages, coarsest on loudest ones. Appearancewise this procedure makes, from a light pattern standpoint, a funny looking record. For our money a disc recording, however, was always something to be more listened to than looked at. So, Mercury Records seem downright pleased with the resulting 62 db dynamic range."

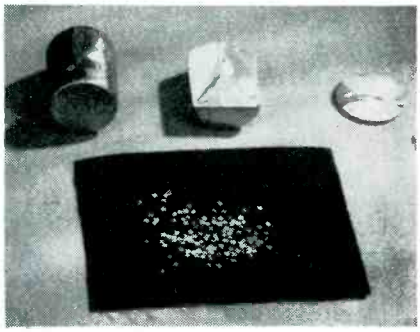
"Margin Control", according to Mr. Fine, because of the inherent low noise level of the material is particularly effective with Soundcraft 'Maestro' discs. Soundcraft's triple-filtering to remove foreign matter, and Soundcraft's uniform consistency establish wide-dynamic-range microgroove recording on a predictable basis. Incidentally, Soundcraft ads, like Soundcraft discs are equally effective either way up.

Advertisement

*Vice Pres., Reeves Soundcraft Corp.

ments from the fifth column in the periodic table will produce n-type material conducting by electrons. Any of the elements added from the third periodic group will produce p-type conducting by defect electrons or holes that react as solid charges. Each of the impurity atoms is supposed to release one carrier only.

With the number of electrons or positive holes and their temperature dependency as determined from Hall effect, it is possible to develop a general theory of resistivity and thermoelectric power which accounts completely for the



Bell Labs photo showing purified germanium ingot, first saw cut, slab and finished pellets ready for use in semi-conductors

electrical behavior of these semi-conductors from very low temperatures up to the melting point.

By adding a large enough number of impurity centers it is possible to produce a semi-conductor which follows quantum statistics. By measuring the conductivity to low temperatures it is possible to go continuously from classical to quantum statistics, for the first time producing an experimental proof for this behavior of the electron gas.

Recently it has been possible to develop a new type of semi-conductor by displacing the atom in the semi-conductor due to nuclear bombardment by either neutrons or alpha particles or deuterons from the cyclotron. Polonium alpha particles have also been used with success. In this way it is possible to change an N-type semi-conductor into a P-type semi-conductor and study in detail the changes in rectifying action by bombarding, for instance, germanium-point contact rectifiers with nuclear particles.

If silicon containing both p and

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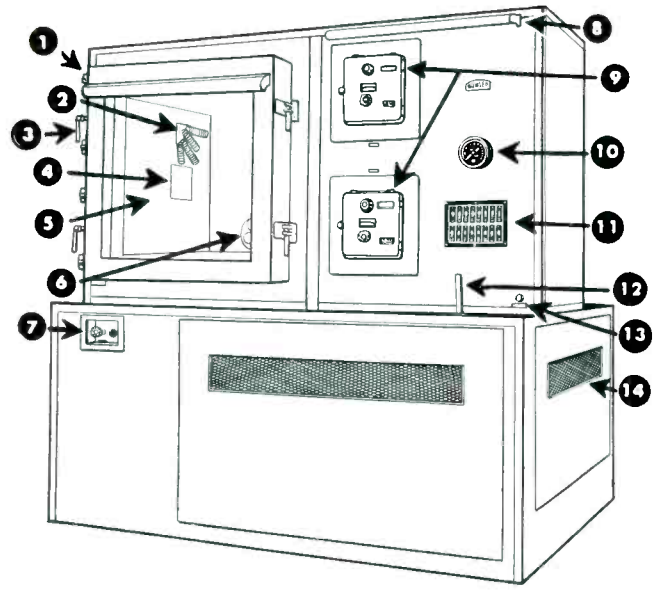
Designed by Bowser, Inc., to meet the most rigid requirements for testing electronic components or equipment in relation to temperature, humidity or altitude. Used widely by government and industry in laboratories for research and development work and on the production line.



1. Door Light
2. Internal Terminal Pad
3. Cam Latch
4. Access Port
5. Inspection Window
6. Air Mover
7. Hand Regulating Water Valves
8. Instrument Panel Light
9. Indicating Potentiometer, Controller (Wet and Dry Bulb)
10. Altitude Gauge
11. Control Panel
12. Climb-Dive Valve
13. Manometer Connection
14. Condensing Unit Compartment

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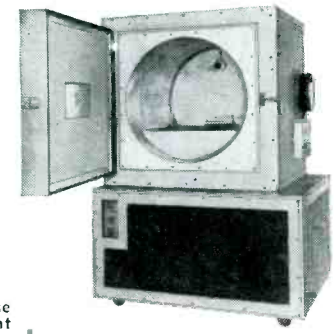
MODEL NO.	SIZE H	W	D	LOW TEMP. POINT F.	PULL DOWN FROM AMB. MIN.	DISSIPATION AT LOW OPERATING POINT AT SEA LEVEL	MASS LOAD OF STEEL	8 POST, 4 THERMOCOUPLE TERMINAL PAD	CUT OUT AND REMOVABLE INSULATION BATT
L1-50 VH L1-76 VH L1-100 VH	12″	12″	12″ (1 cu. ft.)	—50°F. —76°F. —100°F.	70 105 170	100 watts 100 watts 50 watts	25# 25# 25#	Available in all 3 L1 Units installed on left side wall, only if " cut out " not required	Available in all 3 L1 Units, installed on left side wall, only if Terminal Pad is not required
L5-50 VH L5-76 VH L5-100 VH	18″	30″	15½″ (5 cu. ft.)	—50°F. —76°F. —100°F.	70 110 200	200 watts 200 watts 100 watts	50# 50# 50#	Installed in left side wall	Installed in left side wall
L8-50 VH L8-76 VH L8-100 VH	24″	24″	24″ (8 cu. ft.)	—50°F. —76°F. —100°F.	70 110 200	200 watts 200 watts 100 watts	50# 50# 50#	Installed in left side wall	Installed in left side wall
L18-50 VH L18-76 VH L18-100 VH	30″	30″	36″ (18 cu. ft.)	—50°F. —76°F. —100°F.	70 110 210	200 watts 200 watts 100 watts	25# 25# 25#	Installed in left side wall	Installed in left side wall
L27-50 VH L27-76 VH L27-100 VH	36″	36″	36″ (27 cu. ft.)	—50°F. —76°F. —100°F.	75 110 210	200 watts 200 watts 100 watts	100# 100# 100#	Installed in left side wall	Installed in left side wall

THE FOLLOWING SPECIFICATIONS ARE STANDARD FOR ALL MODELS:

1. Reheat time from ambient to +180°F. is 70 minutes.
2. Thermocouple Type Indicating Controller; installed in instrument panel to right of free-working space. Range: —150° F. to +200°F.
3. Altitude Simulation Equipment: Laboratory Type, Oil Sealed Vacuum Pump and Hand Operated Climb - Neutral - Dive Valve.
4. Current (for control): 110 volt, 60 cycle, single phase. (for power): 220 volt, 60 cycle, three phase.
5. Average Climb Rate: 3,000 feet per minute to 50,000 feet.
6. Maximum Vacuum: 1" mercury obsolute.
7. Vacuum Gauge: 4½" Dial Type, 0' to 80,000'.
8. ⅜" I.D. low Pressure Pipe: 50 psi. installed in left side wall.
9. Special instrumentation can be supplied at customer's request.

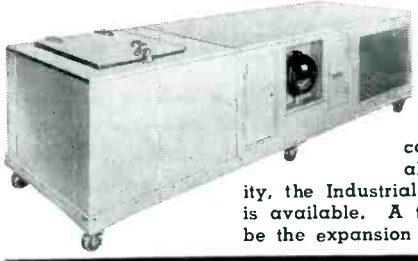
CONSTRUCTION

Cabinet mounted on rigid steel base of welded channel irons to prevent warpage or distortion. Refrigeration equipment and vacuum pump, etc., mounted on separate inner frame to minimize vibration. Work being tested checked during processing through inspection window mounted in door of chamber. Interior illuminated by means of a light mounted on door outside the chamber. Instrument panel is also supplied with a light mounted over it.



UTILITY UNITS

Designed for rapid, dependable production testing and processing. It is also capable of being used for limited amounts of research and development work. Adaptable to a wide range of applications from production processing of radio crystals to testing of cameras and camera lenses. Provided with temperature control from +158°F. to —80°F., with a tolerance of control of ±3°F. over the range.



INDUSTRIAL

For the user whose requirements do not call for conditions of high altitude or relative humidity, the Industrial "low temperature" Unit is available. A typical application might be the expansion fitting of bushings.

OTHER BOWSER UNITS

Some of the many Bowser units are shown and briefly described on this page. They have a wide scope of application throughout industry. Complete details regarding any of them are available upon request.

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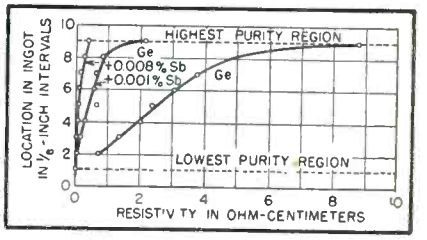
IN CANADA, S. F. BOWSER CO., LTD., 344 SHERMAN AVE., HAMILTON, ONTARIO



Effect of antimony additions on resistivity of germanium

n-type impurities is caused to solidify slowly the first frozen region is p type and the last frozen region n type. The boundary between the two regions is the seat of an interesting rectification and photovoltaic effect. This boundary may be resolved microscopically. Also the segregation and compensation effects may be employed to reduce the variation in resistivity in an ingot.

The germanium used for high-back-voltage rectifiers or for transistors may be converted reversibly from n to p type by heat treatment. This is interpreted as being due to the simultaneous presence of both p and n type impurities. Normally the n-type impurities are in excess.

The study of alloys of germanium with radioactive antimony has permitted the accurate determination of the distribution of antimony in an ingot even for concentrations as low as 4×10^{-6} percent. The concentrations determined by analysis agree with those computed from measurements of electrical properties. By this means it has been shown experimentally that each antimony atom present contributes one conduction electron to the germanium.

These applications of nucleonics to semi-conductors were reported in separate papers by J. H. Scaff of Bell Laboratories and K. Lark-Horovitz of Purdue University at the 1949 IRE National Convention.

Study of Vanishing Gases

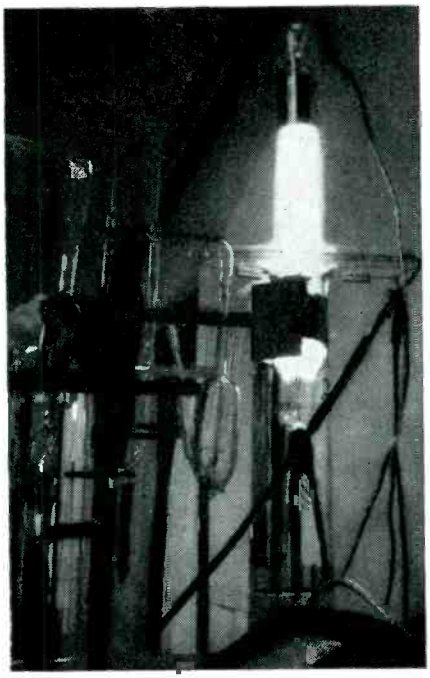
THE LIFE of gas-filled tubes is limited by a gradual reduction in gas pressure with use. This tendency of filler gases to disappear from the tube volume is known as clean-up and is generally thought to result from the bombardment of negatively charged electrodes by high-velocity positive gas ions that penetrate the metal surfaces and

become permanently trapped.

A study of clean-up phenomena is now underway at the Electron Tube Laboratory of the National Bureau of Standards. A specially-designed discharge tube with a replaceable tantalum probe wire to collect the positive ions is being used. During operation, the rate of gas clean-up is measured for various negative d-c potentials on the probe in the presence of an arc discharge.

Since self clean-up cannot be avoided completely, its value is determined experimentally by operating the discharge tube with a positive probe voltage so that electrons rather than positive ions are drawn to the probe. Each test run is preceded by a self clean-up run, yielding a correction factor for the net clean-up into the probe. To avoid overheating the probe wire, negative voltage is applied in pulses of several milliseconds duration repeated several times a second.

Further problems under study include the complete recovery of trapped gas, a determination of the amount of gas which can be absorbed by the probe before satur-



Special helium-filled arc discharge tube in operation in the Electron Tube Laboratory of the National Bureau of Standards. The ionized helium in the discharge column gives off enough rose-colored light to illuminate the other apparatus clearly. The tube contains a nickel anode at the top, a tantalum probe wire at the center, and an oxide-coated cathode at the bottom

ation occurs, and a correction of the probe current for electron emission. Now that satisfactory techniques have been developed for a particular probe material and filler gas, these methods can be extended to other solids and noble gases of interest to tube designers.

Double-Ended D-C Restorer

By D. A. Bell
Taplow, Maidenhead England

Direct-Coupled amplifiers are apt to be inconvenient for a number of reasons. Not the least of these is the risk of drift in the first stage causing serious unbalance or even overloading when amplified and applied to the last stage. There is therefore a motive for using an a-c coupling whenever possible.

When the signal has periodic excursions to a fixed limit but contains a d-c component because of varying amounts of signal on either side of the center line, a-c coupling can be used with a d-c restorer or clamping diode which fixes the mean position of the wave by reference to the excursions to the fixed limit. The name clamping diode does not seem to have come into general use, but

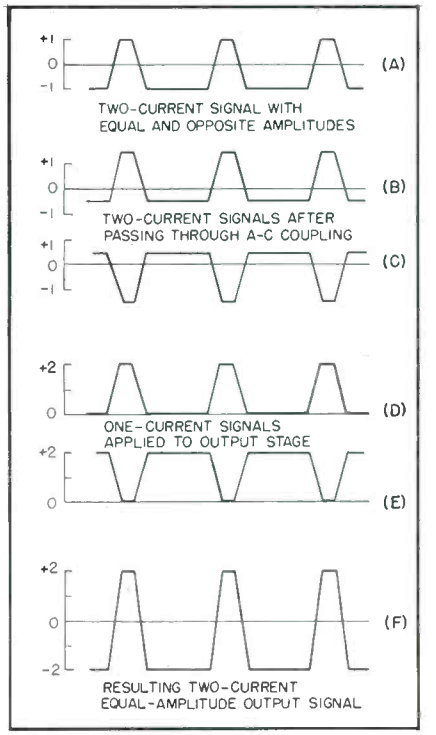


FIG. 1—Waveforms of 3-to-1-ratio of off-to-on telegraph signal, and effects of a-c coupling networks and d-c restoration circuits

is very expressive of the function of the diode in clamping one limit of the waveform to a fixed voltage level.

Probably the most familiar example of the d-c-restoring technique is to television video amplifiers, where the line sync pulses provide a repeated excursion to a fixed limit. There are cases, however, where the requirement is rather to keep the signal symmetrically balanced (in amplitude) on either side of the datum line, in spite of differences in proportion of time spent with either polarity.

The best example of this is a telegraph signal working on a mark and space basis represented by signals of opposite polarity. Figure 1A represents a hypothetical signal having the times spent on space and mark in the ratio 3 to 1 but with equal and opposite amplitudes of $+1$ and -1. Figure 1B shows the result of passing a repeated signal of this form through an a-c coupling (capacitor and leak). The datum line has shifted so as to produce equal areas on either side of zero, instead of equal amplitudes.

Now the problem is to get the datum line back into the center of the waveform, so that a relay or other device will operate exactly in the center of the transition from mark to space. This would not be important if the waveform were square, but in practice the reversals take a finite time and any departure from a symmetrical datum line will change the ratio of mark-to-space times. A distortion of mark-to-space time ratio of this kind is called bias distortion by telegraph engineers.

The desired result can be achieved by the circuit shown in Fig. 2, which includes a double-ended d-c restorer and operates as follows. The first tube is simply a phase-splitter, so that in addition to the waveform shown in Fig. 1B we have the inverted waveform of Fig. 1C. Each of the waveforms is applied to a d-c restorer consisting of the coupling capacitor between the phase-splitter output and the grid of one of the push-pull tubes in conjunction with a diode (half a 6H6 for each side). The diode is inverted, with anode grounded, so that signals on the

grids of the pushpull tubes are positive-going only. (This polarity was chosen so that the output stage could be fairly heavily biased and run cool in the absence of a signal.)

Since the signals shown in Fig. 1D and Fig. 1E are applied to the output stage in pushpull, their combined effect in the common anode circuit is proportional to their difference as shown in Fig. 1F, which is a true copy of Fig. 1A. This waveform may be viewed by connecting the points Y_1 and Y_2 directly to the plates of a cathode-ray tube. It will not be seen if the points are connected to the input terminals of an oscilloscope having capacitor-coupled input, since the introduction of this a-c coupling destroys

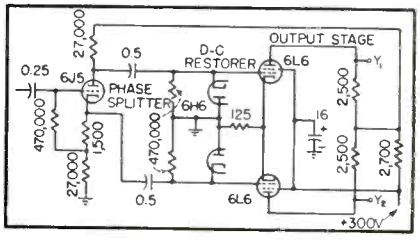


FIG. 2—Circuit diagram of double-ended d-c restoration amplifier

the d-c-restored condition which has been achieved in the amplifier. A striking demonstration of the efficacy of the system is given by having a changeover switch to give either direct or capacitive coupling from the points Y_1 and Y_2 to the plates of the cathode-ray tube.

For more practical use the loads in the anode circuit of the output stage may consist of the two halves of the windings of a telegraph relay or recorder.

Besides allowing a telegraph signal to be amplified in a-c-coupled stages and d-c-restored in the final stage, this circuit might be used for converting single-current (Fig. 1D) to double-current (Fig. 1F) signals. As mentioned above, a telegraph relay must change over at a signal amplitude exactly half way between the mark and space levels in order to avoid bias distortion of the signals, and with double-current working the changeover should occur at the neutral point of zero current. But in single-current working, where space is indicated by zero current, the changeover must occur at half the

mark amplitude to avoid distortion.

This is normally achieved by biasing the operating point of the relay to half the signal amplitude, and therefore requires adjustment for any change of signal amplitude. By using the phase-splitter and double-ended d-c restorer, either with or without preceding a-c amplification, a symmetrical two-current output is obtained. This has the advantage of operating a relay at neutral bias, so that it changes over at zero current and its operation does not require adjustment for signal amplitude.

A New Moisture-Sealing Compound

By W. B. Ritchie Agnew
Consulting Engineer
Bellflower, California

Moisture will leak into holders for quartz crystals and other components through gasket or pin leaks and may also transfer through phenolic housing material by moisture vapor transmission. To combat this action in small phenolic holders for crystals intended for tropical use, a special moisture sealing compound was developed in the Aircraft Radio Laboratory at Wright Field.

Several types of holders were involved in the initial research problem. The top loader type is sealed with a phenolic or metal cover and a neoprene gasket. One type of side loader has a round screw in cover and gasket. The inverted type seals with a gasket near the pin end. Such holders have two pins molded into the plastics container, one-half inch apart for contact through a suitable socket to the radio circuit.

The day to night cycling of temperature or the change in pressure from ground to high elevation brought on by airplane flight or a sunshine to shade cycling of temperature will cause breathing. This breathing sucks in moist air. When this air is exhaled at the other end of the cycle moisture will remain within the holder. It has been reported that some holders which were subjected to high humidity for long periods of time were actually

partially filled with water when opened for inspection.

Development Procedure

Over one hundred different materials were tested, including plastics, resins, waxes, paints and varnishes. A commercial asphaltum paint showed virtues of having the best sealing properties. This material had several disadvantages, such as being too brittle at −55 C and too soft at +90 C. These two temperatures are the extremes that a crystal unit must withstand in the using organizations of the Services.

Upon investigation, it was found that the asphaltum paint contained some rosin, which was eliminated so that the material would not be brittle at −55 C. This new material was still too soft at +90 C. Gilsonite was added to Hydrolene in various quantities until a formula was found that had enough plasticity at −55 C and still remained in a suitable state at +90 C. The percentages finally used were 60 percent Gilsonite and 40 percent Hydrolene.

Gilsonite is a natural asphaltum and is mined in Utah, while Hydrolene is a trade name of a material procured from Standard Oil Company and is a brand of petroleum asphaltum.

Several mixes of the above-mentioned proportions of asphaltum were tried in different mineral spirits and aromatic thinners. Xylene was decided upon as the vehicle due to its ease of coating and its drying behavior.

Another series of mixtures was tested, one containing 40 percent nonvolatile matter, another 50 percent and still another 60 percent. The 60 percent mixture, when heated in a water bath to 100 F. gave a coating material of the right viscosity for a dip-coating thickness of approximately 0.004 inch. Tests had shown this thickness was necessary to exclude a reasonable amount of moisture in a one-coat dip. The dip-coating compound was composed of 6 parts Gilsonite and 4 parts Hydrolene to make up 60 percent of the mixture, and Xylene to make up the remaining 40 percent.

A small amount of commercial grade aluminum paste as a filler

aided moisture imperviousness, and 12 ounces per gallon were added to the above formula. Materials were mixed in the above order.

Results of Tests

All moisture imperviousness and moisture vapor transmission tests were accomplished by coating a given holder which had previously had a chemically-treated blank installed in place of the crystal blank. The moisture transferred to within the holder was then detected by an electrolytic reaction and indicated with the aid of a specially-constructed moisture indicating meter.

All tests were run in humidity cabinets at one of the following temperatures with a 95-percent relative humidity: cycling 25 to 50 deg C, cycling 25 to 65 deg C, and static at 50 deg C.

It was also noted that resistance between pins remained nearer to the original resistance of 50,000 megohms or better after being coated. Some uncoated holders dropped to less than 100 megohms in a few days. This was due to water absorption of the phenolic material. The moisture sealing compound was found to have high dielectric characteristics and would resist fungus growth more readily than some of the phenolics of the uncoated holders.

Dipping Technique

Dipping is best done automatically at a slow speed, probably not more than 1½ inches a minute withdrawal speed. This is intended to eliminate any drip or bead on the edge of the holder.

After some production by a West Coast contractor, it was found that spraying under pressure with special spraying equipment designed by Alemite Corporation was superior to the dipping process. Tears and heavy drainage areas were entirely eliminated.

After the crystal units were coated with the moisture sealing compound and allowed to dry for approximately 18 hours, a second coat was applied, this time using a special aluminum paint which would not wrinkle in humid atmospheres. This special aluminum paint differed from the commercial alumi-

num paint inasmuch as it contained a resin vehicle designated BR254 resin. The application of this aluminum paint overcame all stickiness at elevated temperatures.

Some of the specifications of the moisture sealing compound are as follows: Solids content, 60 percent by weight; specific gravity at 25 deg C, 0.984; weight per gallon, 8.2 pounds; viscosity at 25 deg C, 115 to 120 Kreb units; drying time at 25 deg C, 16 to 18 hours; flash point, 93.

The material should be heated in a water bath at 100 deg F. This gives a consistent coating of approximately 0.004 inch in both winter and summer months.

Determining Form Factors of I-F Transformers

By WILLIAM C. VERGARA

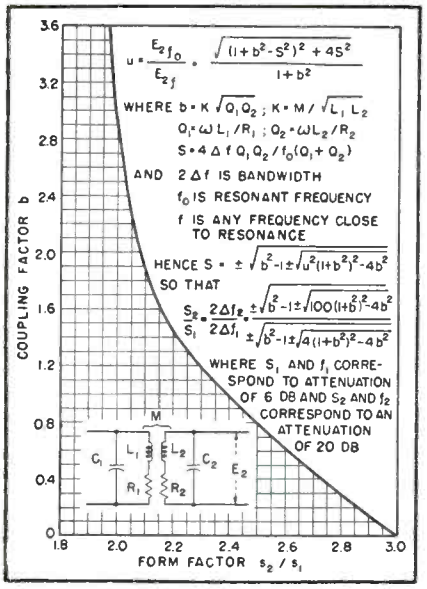
Communication and Navigation Section
Bendix Radio Div., Bendix Aviation Corp.
Baltimore, Md.

THE DEGREE OF COUPLING of a conventional i-f transformer can be determined readily by measuring the bandwidths at two levels of attenuation and computing the ratio of these bandwidths. This ratio is directly related to the coupling factor of the transformer and is plotted in the accompanying graph to facilitate the determination.

Development of Method

The selectivity characteristic of the circuit shown on the graph is given by the well known (see for example J. E. Maynard's treatment in ELECTRONICS, p 15, Feb. 1937) relation given at the top of the graph with the terms as defined. The assumptions on which this relation was derived limit its validity to the practical case where only frequencies close to resonance are of interest; that is (1) the Q's are constant for all frequencies close to resonance, (2) the Q's are sufficiently high so that the inductive and capacitive reactances are equal and parallel and series resonances occur at substantially the same frequency, (3) there is no feedback in the associated vacuum tube circuit and (4) the tuned circuits are coupled by pure reactance.

This relation (at the top of the



Transformer coupling can be determined simply from this chart and measurements at bandwidth at two levels of attenuation from the response at resonance

graph) can be solved for s giving the result shown on the graph. This expression relates the departure from resonance s to the coupling factor b and the attenuation factor u.

The factor s and therefore the bandwidth can be computed for any level of attenuation by substituting the appropriate value of u. Let s_1 be defined as the bandwidth factor corresponding to an attenuation of 6 db below the response at the resonant frequency; u is then equal to 2. Similarly, s_2 corresponds to an attenuation of 20 db for which u is 10.

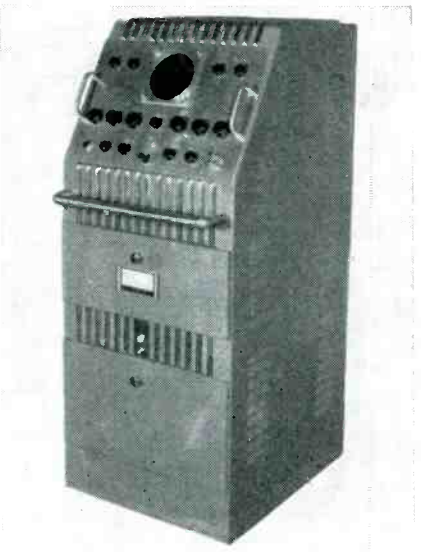
Substituting these values of u and writing the ratio s_2/s_1 gives the final equation presented on the graph. This equation is plotted as the curve of the graph and is used in determining the coupling factor of a transformer.

Using the Graph

The ratio s_2/s_1 equals the ratio of the bandwidths at 20 and at 6-db attenuation. The coupling factor b can be determined for a particular transformer by measuring s_2/s_1 and then reading the corresponding value of b from the graph.

The choice of 6 and 20-db levels for the bandwidth measurements was made arbitrarily for ease and accuracy of performing the measurements.

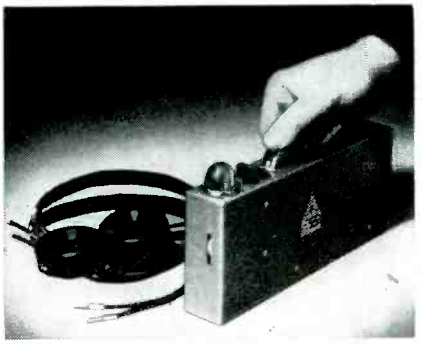
(continued from p 126)



32A video oscilloscope enables the observation of waveforms having frequency components as high as 50 mc and as low as 10 cps. This wideband frequency response is obtained with sufficient amplification to provide deflection sensitivity of 0.1 peak-to-peak volt per inch. The horizontal amplifier has a bandwidth of 10 cps to 10 mc.

Survey Meter

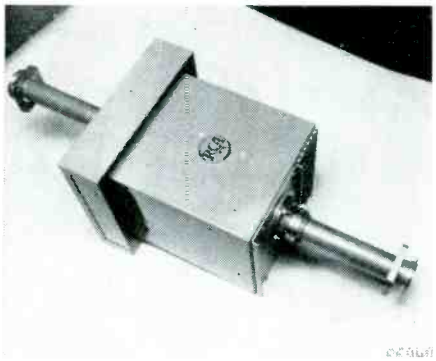
RADIATION COUNTER LABORATORIES, INC., 1844 W. 21st St., Chicago 8, Ill. The Atomic Blinker is a portable survey meter containing a low-voltage thin-wall Geiger counter for radiation detection. Amount of radia-



tion is indicated instantaneously by the rate of flashing of a lamp. Earphone tip-jacks are also provided. Battery life is from three to six months with normal usage.

F-M/A-M Isolation Unit

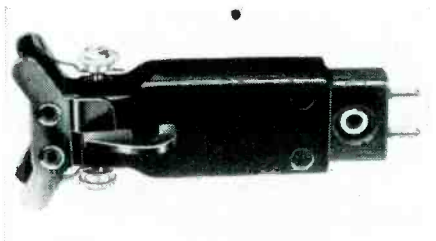
RADIO CORP. OF AMERICA, Camden, N. J. Type BAF-14A f-m/a-m isolation unit weighing less than 30



pounds was recently announced. The device is used to transfer f-m power across the insulating zone of an a-m antenna tower to feed an f-m antenna mounted atop the tower. It provides isolation of f-m and a-m signals and efficient operation over the entire f-m frequency range. The unit features swivel flanges at input and output which connect to standard 1⅝-in. 51.5-ohm flanged line.

Crystal Phono Cartridges

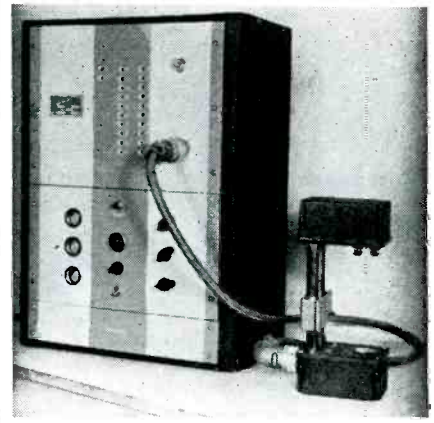
SHURE BROTHERS, INC., Chicago, Ill., has announced the Vertical Drive series of crystal phonograph cartridges. Tracking force is 5 grams on fine-groove records, 7 grams on 78-rpm recordings. The cartridge uses Muted Stylus needles which



rotate on a vertical axis. It is available in three models: one for standard records, another for fine-groove, and a third, which is an all-purpose turnover model with replaceable needles for playing both standard and fine-groove records with the same pickup head.

Industrial Counters

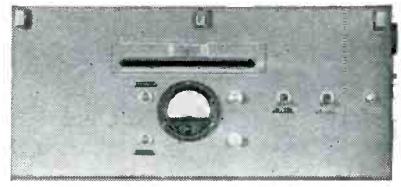
AIRLECTRON INC., P. O. Box 151, Caldwell, N. J., has announced a new series of presettable high-speed electronic counters for industrial applications. Having a counting speed of 10,000 per minute, the devices operate from photoelectric or magnetic pickup sources. Output circuits may be connected so as to



start and stop machine operation or perform any function associated with counting. Further information is contained in bulletin C-140.1.

Portable Recording Oscillograph

CENTURY GEOPHYSICAL CORP., 1333 North Utica, Tulsa, Oklahoma. The portable recording oscillograph is applicable for laboratory or field work. It is equipped with mirror-



type galvanometers, fork-controlled synchronous timing system and variable paper widths up to 6 inches maximum. The unit may be battery or a-c operated and is available for multiple channel recording up to 25 traces.

Insulated Leads

AIRCRAFT-MARINE PRODUCTS INC., 1611 N. Fourth St., Harrisburg, Pa., has added to its line of solderless wiring devices new plug-in leads with a special flexible plastic insulation. They feature precision positioning of the jack-pin and will withstand temperatures up to 170 F.

Hermetic Relays

STRUTHERS-DUNN, INC., 150 N. 13th St., Philadelphia, Pa. Type CX3554 is a hermetically-sealed d-c miniature relay of special aviation design. It has shock resistance up to 50 g; vibration resistance better

than 10 g; high-speed opening and closing without contact bounce; and reliable operation over an ambient temperature range from minus 75 to plus 200 C. The hermetic sealing makes the unit insensitive to humidity changes and capable of rated operation at altitudes as high as 70,000 feet.

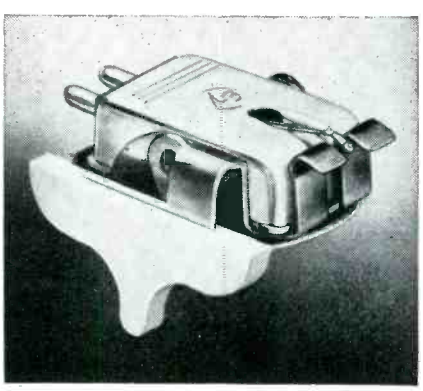
Communications Measurement

WESTON ELECTRICAL INSTRUMENT CORP., 617 Frelinghuysen Ave., Newark 5, N. J. Model 779, type 5, analyzer, was designed for communication system maintenance. It measures low-level speech circuits

with a minimum of circuit disturbance. The a-c response is essentially flat to 50 kc within 1 db over the range −20 to +22 dbm, and is usable for comparative db readings on all common carrier current frequencies above 50 kc.

Pickup Cartridge

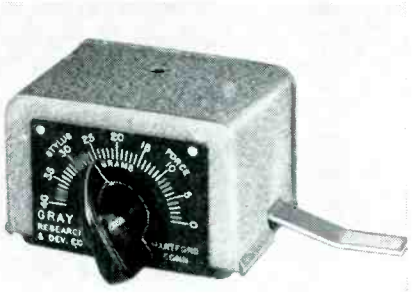
ELECTRO-VOICE, INC., Buchanan, Mich., has announced the Twilt, a new torque-drive twin-tilt phono pickup cartridge. The cartridge with a single twin-tip replaceable needle plays 78, 45 and 33⅓-rpm



records without weight change and with a tracking pressure of only 6 grams on either needle tip. Tilting the Twilt selects the one-mil or three-mil needle tip as desired.

Stylus Force Gage

GRAY RESEARCH & DEVELOPMENT CO., INC., 16 Arbor St., Hartford 1, Conn. The instrument illustrated, which is accurate to grams, is designed to check stylus force to obtain maximum quality reproduction



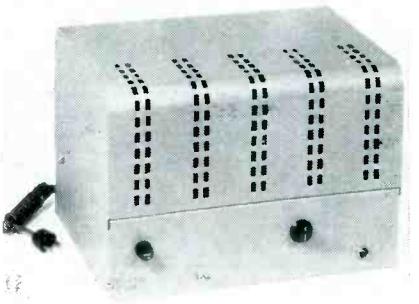
from records. Correct stylus pressure preserves high quality, prolongs record use and reduces replacement costs.

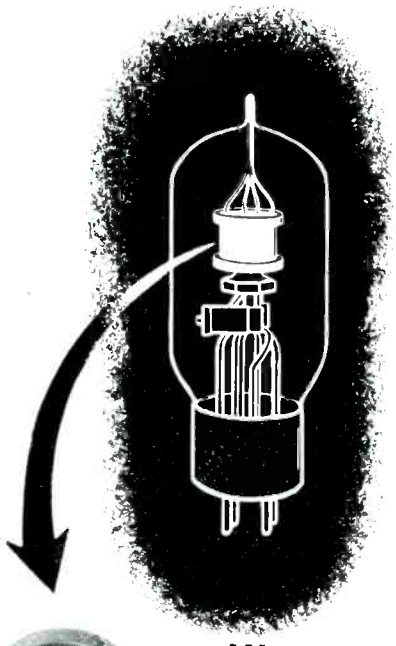
VHF Airborne Receiver

FEDERAL TELEPHONE AND RADIO CORP., Clifton, N. J. Type 139-BY vhf radio receiver for single-channel aircraft reception is the successor to the 139-B. Discrimination against undesired pulsed carriers and against spurious responses is good. Technical details of the equipment performance can be obtained from the manufacturer.

R-F Power Supply

EMBASSY ENGINEERING CO., 224 E. 204th St., New York 58, N. Y., has developed a new high-voltage r-f power supply for a wide variety of uses including television, c-r oscillography and general experimental





IN RUGGED SERVICE SPEER GRAPHITE ANODES *WORK BEST*

You don't have to run the risk of tube failure in applications where operating conditions may be tough. Graphite — and *only* graphite — anodes work best when the going's roughest.

Here's why:

- Graphite anodes are capable of 200-300 % higher power rating over most metallic anodes.
- They provide stability — keep their original characteristics — won't warp even over the 200 megacycle range.
- Graphite *lasts* because it operates at lower temperatures, even when usage is severe and continual.

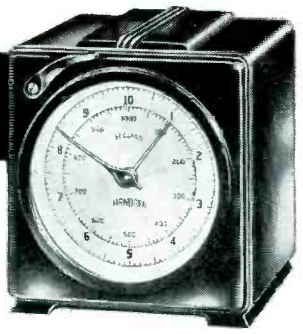
More and more, equipment manufacturers are *demanding* graphite anodes tubes for such applications as diathermy, vhf, short wave and FM transmitters, motor control, electrostatic precipitation, resistance welding, electronic heating, counting and sorting. Follow their lead, and you'll get better tube performance!

5464

Speer

CARBON COMPANY
ST. MARYS, PENNA.

Standard TIMERS



WORLD'S MOST ACCURATE AND RUGGED TIME MEASURING INSTRUMENT. CAN BE MANUALLY OR ELECTRICALLY OPERATED. FURNISHED IN PORTABLE CASES OR FOR PANEL MOUNTING

T-1E

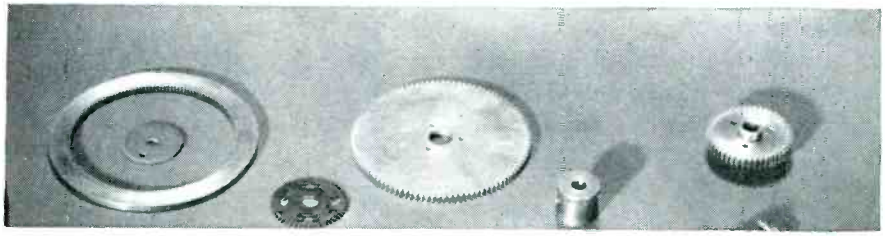
Model	Reads	Totalizes	Accuracy
S-100	1/5 sec.	6000 sec.	±.1 sec.
S-60	1/5 sec.	60 min.	±.1 sec.
SM-60	1/100 min.	60 min.	±.002 min.
S-10	1/10 sec..	1000 sec.	±.02 sec.
S-6	1/1000 min.	10 min.	±.0002 min.
S-1	1/100 sec.	60 sec.	±.01 sec.
MST	1/1000 sec.	.360 sec.	±.001 sec.
MST-500	1/1000 sec.	30 sec.	±.002 sec.

WRITE FOR BULLETIN 153

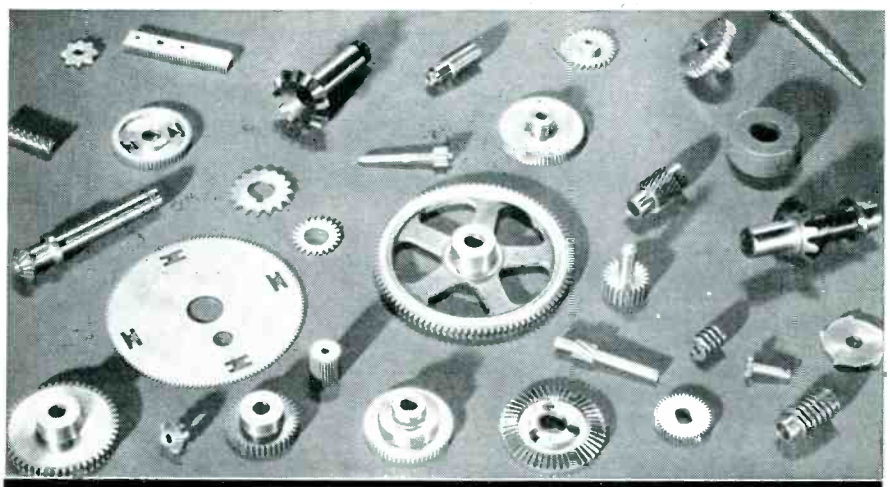
also Standard Chrono-Tachometers • Standard Custom-built Laboratory Test and Distribution panels

THE *Standard Electric Time Co.*

97 Logan Street — STANDARD FOUNDED 1884 — Springfield, Mass.



SPECIALISTS IN ELECTRONIC GEARS



QUAKER CITY GEAR WORKS 1908-32 N. FRONT ST. PHILADELPHIA 22, PA.

work. Input voltage is 110 v, 60 cycle a-c, with output voltage factory preset at 30 kv. Output current is 200 μa normal at 30 kv; regulation is 3.3 percent at 30 kv with a load of 50 to 200 μa. Power consumption is 75 watts.

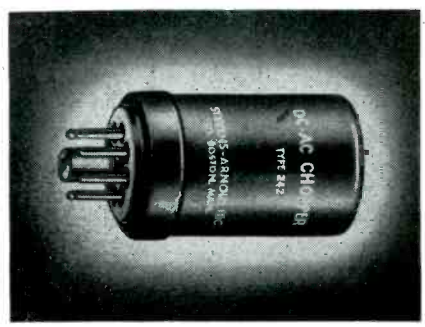
Automatic Locking Plugs

RUSSELL & STOLL CO., INC., 125 Barclay St., New York 7, N. Y., announces a new line of midget Ever-Lok automatic locking plugs, receptacles and cord connectors, adaptable as components for all

types of portable electrical equipment. A 12-page catalog EL49-64 describes and illustrates the unit's many features.

D-C/A-C Chopper

STEVENS-ARNOLD INC., 22 Elkins St., South Boston 27, Mass. Type 242 chopper is a single-pole, double-throw electromechanical chopper, rectifier, demodulator or square-wave generator which will operate



at any frequency over the 45 to 65-cps range. The unit features liquid filling, special shielding and make-before-break contacts. Complete details are given in catalog 246.

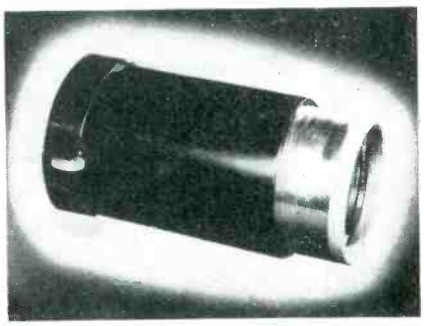
Electrical Tape

BAUER & BLACK, Dept. F., 222 West Adams St., Chicago, Ill. Polyken 822 is a plastic-backed electrical adhesive tape with a dielectric strength of over 10,000 volts. It has the insulation and electrical

characteristics of polyethylene. Thickness is 0.009 inch and tensile strength is 22 pounds per inch of width.

Projection Lens

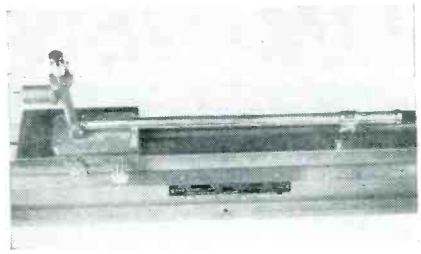
ALLEN B. DUMONT LABORATORIES, INC., 1000 Main Ave., Clifton, N. J. Type 2542 projection lens is a two-element, symmetrical objective lens having a relative aperture of f 3.3 and a focal length of 7.7 inches. It projects an oscillographic pattern



of an area up to 3 inches square to distances from 8 to 30 ft from the screen of the c-r tube, resulting in a picture size that may be as large as 12 sq ft. Axial light transmission of the lens system is approximately 85 percent.

Slotted Line

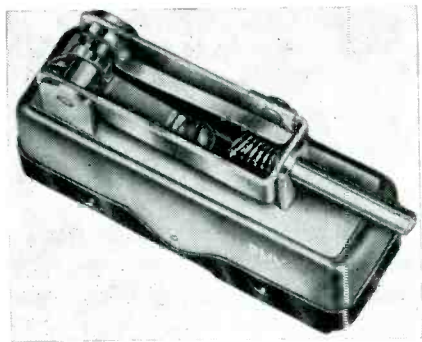
FEDERAL TELECOMMUNICATION LABORATORIES, INC., 500 Washington Ave., Nutley 10, N. J., have developed the FTL-30A slotted line, a precision device for measuring impedance and wavelength in the 60 to 1,000-mc range. Measurements can also be made with slightly less



accuracy in the 1,000 to 2,000-mc range. The unit is a coaxial line 250 cm long having a surge impedance of 51.0 ohms ± 0.5 ohm.

Switch Adaptor

UNIMAX SWITCH DIVISION OF THE W. L. MAXSON CORP., 460 W. 34th St., New York 1, N. Y. Style "P" Adaptaplate provides single-button, maintained-contact control with a-c, a-c/d-c, or metal-cased snap acting



switches. It comprises a ratchet-driven rotary detent cam which alternately presses and releases the operating button of the switch when the drive plunger is pushed.

Vibration Measurement

HERMON HOSMER SCOTT, INC., 385 Putnam Ave., Cambridge 39, Mass. Type 410-X5 vibration integrator and type 410-X6 calibrated vibration pickup enable measurement of vibration displacement, velocity and acceleration in the audio-frequency

range. Displacement can be measured from 0.14 microinch to 0.028 in.; velocity, from 51.3 microinches per second to 10.3 inches per second; and acceleration, from 0.15 in. per second per second to 3,900 in. per second per second over a 25 to 3,000-cycle range. Response is flat from 60 to 1,000 cycles.

High-Fidelity Transformer

ACRO PRODUCTS Co., 5328 Baltimore Ave., Philadelphia 43, Pa. The TI-100 is a transformer unit for preamplifying and equalizing the output of reluctance-type pickup cartridges. It provides full undistorted high-frequency response, plus a rising bass characteristic for low-frequency equalization necessary for quality reproduction. The unit's output provides sufficient voltage to energize the tuner, phonograph, or other medium-level high-impedance input channels.

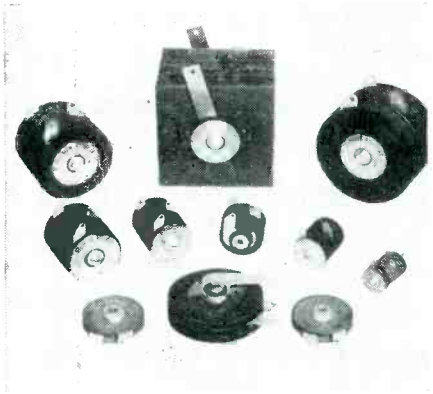
Deflection Amplifiers

HYTRON RADIO & ELECTRONICS CORP., Salem, Mass. Types 6BQ6GT (illustrated) and 25BQ6GT beam pentodes were designed specifically for use as horizontal deflection amplifiers in television receivers using magnetic deflection tubes. The 6BQ6GT with its 6.3-volt heater

is for use in transformer-operated sets, while the 25BQ6GT with its 25-volt heater is used in sets with series heater connections. Complete mechanical and electrical data are found in bulletin 140.

H-V Selenium Rectifiers

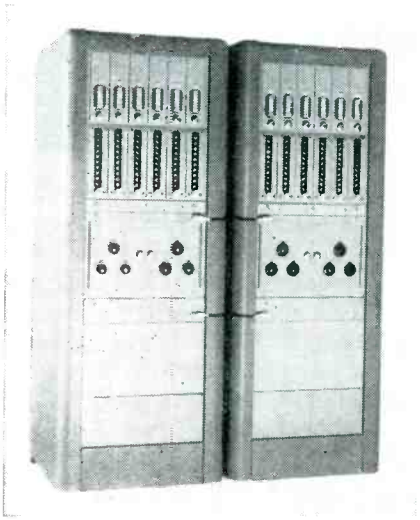
WESTINGHOUSE ELECTRIC CORP., P. O. Box 868, Pittsburgh 30, Pa., has announced new high-voltage selenium rectifier cells designed for 24 volts per cell d-c, with an rms a-c voltage of 33 volts per cell for single-phase bridge circuits. They are available in six round sizes



from 1 to 4⅜ in. in diameter, and in five-inch-square and 4¼ × 6-in. sizes.

Pulse Amplitude Analyzers

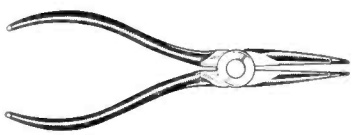
CANADIAN MARCONI CO., P. O. Box 1690, Montreal, P. Q., Canada. Illustrated are two 6-channel pulse amplitude analyzers for research into the energy spectrum of a radioactive sample. Analysis is possible up



to 48 energy ranges. Six channel assemblies use the standard decade, numerator, discriminator and power supply units with the addition of driving amplifier, reset unit, discriminator bias controls and associated power supply units.

Precision Pliers

TRANSVISION, INC., New Rochelle, N. Y. Model P-1 Hook-Cut pliers has both a sharp, tempered cutting edge and a long nose for probing



into small places such as miniature sockets. Overall length is 6½ inches; width tapers from 2 inches on the handle to ⅛ inch on the extreme tip.

Smaller Tubular

AEROVOX CORP., New Bedford, Mass. Stud terminals in place of conventional rivet-type terminals make possible a reduction in the bulk of new PRS midget-can dual-section capacitors with dual leads.

Microwave Meter

KAY ELECTRIC CO., Pine Brook, N. J. The Microwave Mega-Match operates between 8,500 and 9,700 mc. It includes a delay waveguide approximately 75 feet long formed

into a space of 8 ft by 1 ft, a calibrated X-band wave meter, and a box housing power supply and control devices. Reflection coefficient changes down to 0.02 are indicated. Frequency sweep on the display up to 30 mc anywhere in the X-band is available.

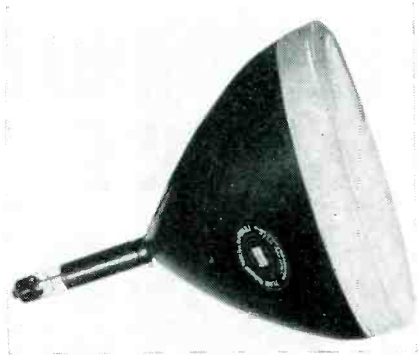
Thermal Switch

MANNING, MAXWELL & MOORE, INC., Bridgeport 2, Conn. The Microsen thermal switch operates from a

thermocouple input to signal temperature variations in heating processes. Signal output is given by electrical relay action. On and off switching of 10 amperes at 115 volts a-c or 32 volts d-c directly is possible for any temperature setting from 100 to 2,000 F. A single 6SN7 vacuum tube operates in conjunction with the Microsen balance and a precision relay.

Glass Picture Tube

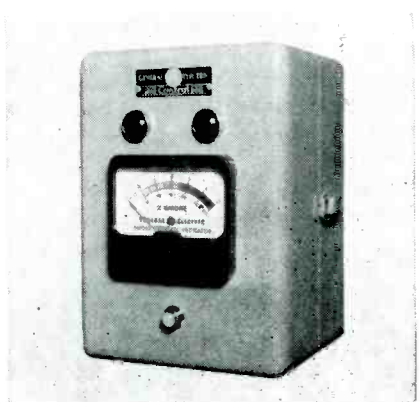
ZETKA TELEVISION TUBES, INC., 131-137 Getty Ave., Clifton, N. J., is now producing a 16-in. glass television tube which features a flat face for greater picture area. The tube also has an ion trap which



eliminates the brown stain sometimes found in the center of the picture. It is one inch shorter than the 15-in. glass tube and two inches shorter than the 16-in. glass-to-metal tube.

Smoke Control

GENERAL ELECTRIC CO., Schenectady 5, N. Y. A new smoke density indicator and control comprises a light source, phototube holder and an enclosure containing the required control and indicating meter calibrated in Ringlemann units. In



operation, a relay is set to operate when smoke density reaches some predetermined level such as 35 percent at which time a blower forces air to the firebox until smoke density drops to approximately 15 percent.

Continuous Loop Recorder

AMPLIFIER CORP. OF AMERICA, 398–7 Broadway, New York 13, N. Y. Models CL-3 and CL-10 continuous loop drive mechanisms make possible continual repetition of any recorded message from 4 seconds to 3 minutes and 4 seconds to 10 minutes in duration respectively.

Both systems are designed in detachable form for easy installation on Twin-Trax tape recorders, and either can be adapted for automatic recycling if desired.

Marine Radar

WESTINGHOUSE ELECTRIC CORP., Box 868, Pittsburgh 30, Pa. Type MU-1 marine radar detects targets at ranges between 80 yards and 40 miles. A newly developed 12½-inch flat-face scope provides a usable

area of 95 sq in. for the ppi display. The unit's design includes a new sea suppressor control which gives constant target intensity above sea return.

VTVM

SYLVANIA ELECTRIC PRODUCTS INC., 500 Fifth Ave., New York 18, N. Y. Type 221 Polymeter is a vacuum tube voltmeter providing an essentially flat response from 20 cycles to 300 mc; and useful measurement between 300 and 500 mc. The r-f probe contains a special subminia-

ture tube which provides a combination of high input impedance and very low input capacitance. By means of switching design, four leads permit rapid measurement on all ranges of a-c, d-c, r-f, milliamperes and resistance without interchanging the panel connectors.

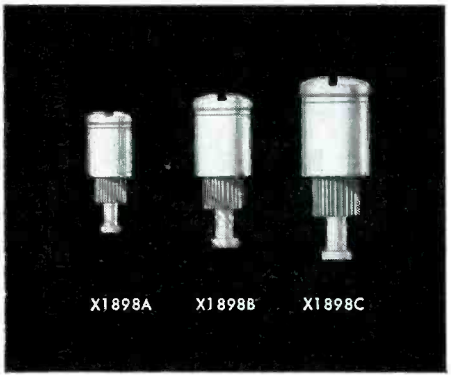
Heat Radiating Connectors

BUD RADIO, INC., 2118 E. 55th St., Cleveland 3, Ohio. Nine sizes of heat radiating connectors are available to fit all grid and plate leads for tubes operating in the range from 50 to 2,000 watts. Machined from special aluminum rod stock, the edges of these connectors are rounded to prevent corona loss.

Cycle Timers

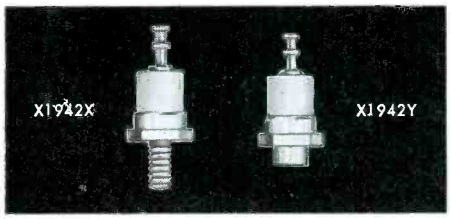
THE R. W. CRAMER CO., INC., Centerbrook, Conn. The type CF3 single or multi-contact cycle timers control automatically a one, two, three or four-circuit operation in a predetermined timing sequence. The unit is designed for built-in applications

TWO NEW CTC TERMINALS PROMISE IMPROVED WIRING



1. ***New Combination Terminal In 3 Sizes Has Variety of Uses***

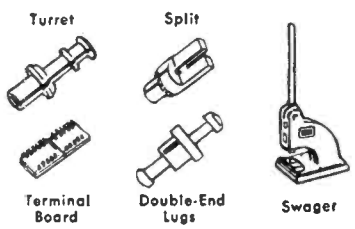
With a screw on top and a terminal lug on the bottom, this combination simplifies top and bottom wiring. Remove the screw and you can mount components directly to the screw end. Or, you can adapt this terminal to provide removable link connections at the screw end. Terminal is plated with bright alloy for corrosion resistance and ease of soldering. Mounting shank is heavily knurled for secure mounting into terminal boards.



2. ***New Ceramic Stand-Off***

The body of this stand-off is made of JAN-1-10-grade L-5 ceramic, silicone impregnated. This gives you a component with highly improved resistance to moisture and fungi, as well as higher dielectric properties. X Type has a 6-32 thread screw stud; Y Type has a rivet stud.

These and other *Guaranteed Components* are described at length in the new CTC #300 Catalog. Write for it today.



Custom or Standard
The Guaranteed Components

CAMBRIDGE THERMIONIC CORP.
437 Concord Ave., Cambridge 38, Mass.

TWO NEW *TWIN* POWER SUPPLIES

MODEL 610-F

- Precise Electronic Regulation.
- 2 Independent Sources of Power.
- 0-335 V.D.C. at 0-60 Milliamperes. Continuously Adjustable.
- 0-325 V.D.C. at 0-120 Mils if the 2 Sources are Combined.
- Both D.C. Outputs Metered for Voltage or Current.
- 6.3 and 12.6 V.A.C. Outputs Provided.
- A.C. Ripple Less than 10 Millivolts.

MODEL 1210

- Precise Electronic Regulation.
- 2 Independent Sources of Power.
- 0-500 V.D.C. at 0-150 Milliamperes. Continuously Adjustable.
- 0-500 V.D.C. at 0-300 Mils if the 2 Sources are Combined.
- Both D.C. Outputs Metered for Voltage or Current.
- 6.3 or 12.6 V.A.C. Outputs Provided
- A.C. Ripple Less Than 10 Millivolts.

Furst *Twin* Power Supplies double the usefulness of a single unit at considerable saving in space and cost. Write for complete specifications on these and other Furst *Twin* Power Supply Models.

FURST ELECTRONICS
10 S. Jefferson St., Chicago 6, Ill.

Large or Small
SQUARE, ROUND OR RECTANGULAR PAPER TUBES
FOR COIL WINDING

Inside Perimeters from .592" to 19"

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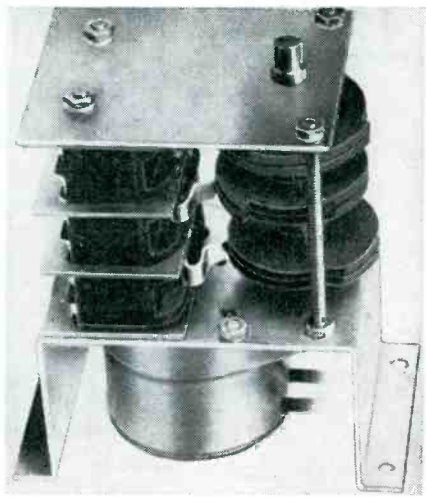
Paramount PAPER TUBE CORP.
616 LAFAYETTE ST., FORT WAYNE 2, IND.
Manufacturers of Paper Tubing for the Electrical Industry



to control a series of machine operations, to reverse motors, or to operate motors, valves, signals or combinations of these in sequence. Twenty-seven different time ranges are available from one revolution in 10 seconds to one revolution in 24 hours. For detailed information request bulletin 1520.

Mike Desk Stand

ELECTRO-VOICE, INC., Buchanan, Mich. The Break-In touch-to-talk stand has a specially-designed lever-type switch for relay operation or microphone ON-OFF. The switch closes on pressing the lever and opens when pressure is released. The unit may be kept in the TALK position by pressing a locking button. Four models, either with or without a dpdt switch, are available.

Vertical Power Resistor

CLAROSTAT MFG. CO., INC., Dover, N. H. The Standee vertical power resistor for above-chassis mounting

comprises a wire-winding on fiberglass core, bent in hairpin form with mica separator between the legs, placed in a ceramic tube filled with cold-setting inorganic cement and provided with bottom terminals and mounting bracket. Available in heights of 1½, 2, 2½ and 3 inches, the resistors have respective power ratings of 10, 15, 20 and 25 watts. Maximum resistance values are 6,000, 9,000, 12,000 and 15,000 ohms, respectively.

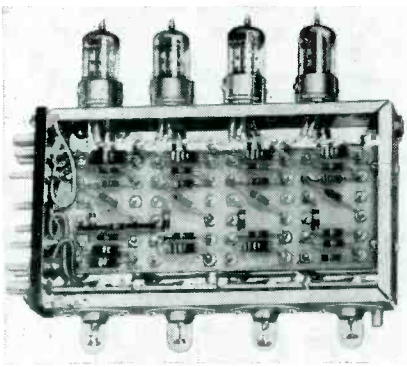
Miniature Tube

GENERAL ELECTRIC CO., Schenectady, N. Y. Type GL-5670 miniature tube is a high-frequency twin triode designed for such applications as mobile communication and aircraft radio equipment. Heater voltage is 6.3 volts, a-c or d-c, with a heater current of 0.350 ampere.

Plate voltage is 300 volts, maximum. The tube has a maximum height of 1½ in. and a maximum diameter of ⅞ in.

Counter Decades

POTTER INSTRUMENT CO., INC., 136-56 Roosevelt Ave., Flushing, N. Y. The plug-in decade illustrated uses



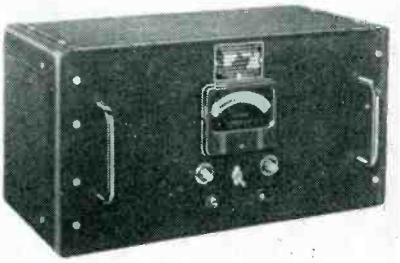
four type 12AU7 tubes and can be used at counting rates up to 130,000 per second accurately. The unit features a wide bias range. Direct decimal readout (0 to 9) on four neon-glow lamps provides a simple means of locating a defective tube since the lamps directly indicate the on-off condition of each tube.

Lab Amplifier

GAWLER-KNOOP, INC., 1060 Broad St., Newark 2, N. J. Type 106 d-c amplifier for general laboratory use is particularly suitable for increasing the sensitivity of d-c oscillographs. Maximum voltage gain is 150 times. Response is flat within 0.5 percent from 0 to 20 kc, and is down less than 25 percent at 100 kc. Standard input impedance is 20,000 ohms resistance. At reduced gain settings it can handle signals as large as 100 volts and transient peaks as high as 600 volts.

Voltage Regulator

THE SUPERIOR ELECTRIC CO., 77 Hannon Ave., Bristol, Conn. Stabiline type EM4102 automatic voltage regulator consists of a variable transformer controlled by a specially-designed electronic detector.

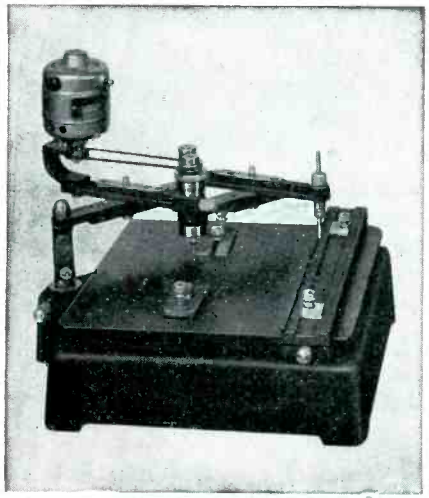


Ratings are as follows: input range, 95 to 135 volts; output, adjustable between 110 and 120 volts; output current, 20 amp; output kva, 0 to 2; input frequency range, 50 to 60 cycles; waveform distortion, zero; recovery time, 0.075 second per volt.

Grid Bias Cell

P. R. MALLORY & CO., INC., Indianapolis 6, Ind. The new miniature-type grid bias cell provides a constant potential for bias of electronic tubes and circuits where no current is required of the cell. It is avail-

—MICO— ENGRAVER



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5. Copy and work right-side up and in view of operator.

Catalog on Request

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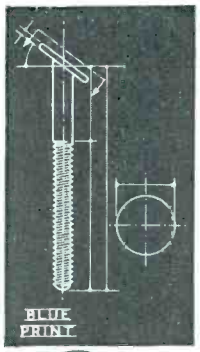
76E Trowbridge St. Cambridge 38, Mass.



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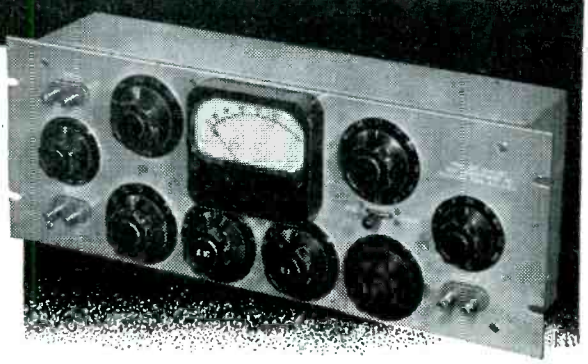
NEW... Improved Wiring Eliminates Leakage

TYPE 12AT & TYPE 12ATK (KIT)

TRANSMISSION MEASURING SET



Range: 111 db. in 0.2 steps.
Frequency resp.: 0.1 db. from 0 to 20 kc.
Accuracy: 0.1 db.
Impedance, load section: 4, 8, 16, 50, 150 200, 500, & 600 ohms.
Impedance, transm. set.: 50, 150, 200, 500 & 600 ohms.
Reference level: 1mw. into 600 ohms.
Circuit: "T", unbalanced.
Attenuators: 10x10, 10x1 & 5x0.2 db.
Load carr. cap.: Transm. sect. 1 w. Load section 10 w.

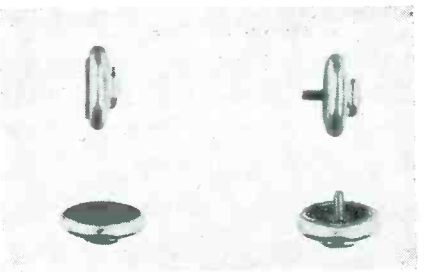
A precision Gain Set with specially developed wiring that permits no troublesome leakage and provides improved frequency characteristics. Available completely assembled, or in kit form—which permits the sale of a high accuracy instrument at a low price.

WRITE FOR DESCRIPTIVE BULLETIN

TECH LABORATORIES, INC.

Manufacturers of Precision Electrical Resistance Instruments

PALISADES PARK, NEW JERSEY



able in 1.5 and 1.75 volts. At audio frequencies the cells have a nonreactive impedance between 250 and 1,500 ohms. Satisfactory operation can be had from −60 to +60 C.

Literature

G-M Counter Instructions. Tracerlab Inc., 55 Oliver St., Boston, Mass. A recent six-page folder gives operating instructions for types TGC-1/1B83 and TGC-2/1B-84 Geiger-Muller counters. The tubes described are self-quenching counters suitable for the measurement of gamma and x-ray photons and most beta particles.

Electronic Control. Sargrove Electronics Ltd., Effingham, Surrey, England. A recent folder contains seven leaflets on photoelectric cell or electronic eye applications for counting, protection, inspection and control. Technical information and illustrations of several units are included.

Tele and Radio Noise Filters. Cornell-Dubilier Electric Corp., South Plainfield, N. J. Bulletin NB-132 describes four new television and radio noise filters developed for use on motors, generators and r-f heating equipment. Ratings, dimensions, attenuation and outstanding features are listed.

Narrow Beam Antenna. Andrew Corp., 363 E. 75th St., Chicago 19, Ill. Type 3605 Corner Reflector antenna for use in the 152 to 162-mc band is described and illustrated in bulletin 84. Included on a single sheet are electrical and mechanical features, specifications and accessories.

Parts Catalog. Standard Transformer Corp., 3580 Elston Ave., Chicago 18, Ill., has announced

publication of the 1949 edition of its catalog giving detailed electrical and physical specifications, including list prices, of more than 400 items. Audio and power transformers, chokes and related components for radio, television and other electronic applications are included.

Relay Guide. Struthers-Dunn Inc., 150 N. 13th St., Philadelphia, Pa., has available a booklet comprising a list of relays classified according to function. Types listed include power relays, small relays, sensitive relays, latch relays with electric reset, special-purpose relays and timers. Comprehensive data and adaptations are given.

Resistor Bulletin. International Resistance Co., 401 N. Broad St., Philadelphia 8, Pa. Bulletin B-5 is a catalog sheet giving technical data on the type BW ½, 1 and 2-watt insulated wire-wound resistors. The units covered feature small size, light weight, full insulation and stability.

Recording Counter. Streeter-Amet Co., 4101 N. Ravenswood Ave., Chicago 13, Ill. A four-page illustrated circular deals with the scientific and industrial counter which can be used in conjunction with an arc welder, drill press or other power device, as well as Geiger counters and scaling circuits. Well-labeled drawings and samples of printed tape are included.

Tube Application Notes. Radio Corp. of America, Harrison, N. J., recently issued two new sets of electron tube application notes, AN-138 and AN-139. The former describes the application of the 6J6 or the 19J6 in an a-m/f-m circuit in which one section of the tube is used as a mixer and the other section as a local oscillator; the latter covers characteristics of pentodes and triodes in mixer service.

Motor-Control Unit. Servo-Tek Products Co., 4 Godwin Ave., Paterson 1, N. J. A 4-page brochure describes the new stepless variable-speed motor control unit. The catalog complete with illustrations of the unit and details of

NEW PRODUCTS (continued)

the operation and uses will be mailed on request.

Catalog Inserts. Eitel McCullough, Inc., San Bruno, Calif. Three recent 4-page pamphlets for insertion in a loose-leaf catalog cover types VVC60-20, VVC2-60-20 and VVC4-60-20 variable vacuum capacitors; the 100TH high-mu triode; and the 100TL low-mu triode. Characteristics and dimensional drawings of each are given.

Remote Antenna Control. Eclipse-Pioneer Division, Bendix Aviation Corp., Teterboro, N. J. A remote microwave antenna position control device featuring pushbutton selection is illustrated and described in a recent 8-page folder. Dimensional drawings are included.

Twin Power Supply. Furst Electronics, 12 S. Jefferson St., Chicago 6, Ill. Model 610-F electronically regulated twin power supply is described on two sides of a recently issued catalog sheet. Complete technical data are given.

Sealed Relays. Automatic Electric Sales Corp., 1033 W. Van Beuren St., Chicago 7, Ill. The illustrated circular 1700 describes a line of relays hermetically sealed in a metal container enclosing an atmosphere of dry, inert gas; sealing offers complete protection from the harmful effects of moisture, ice, fungi, acid, salt and varying air pressure. Outlined in the circular are the advantages of such sealing, a description of the process, and a list of some of the applications.

Electronic Alloys. The International Nickel Co., Inc., 67 Wall St., New York 5, N. Y. A 26-page booklet describes the electrical and electronic properties of 18 high-nickel alloys. Designed primarily for electrical engineers, it cites typical uses, mechanical and other properties, and the various forms in which the materials are available.

General Price List. Andrew Corp., 363 E. 75th St., Chicago 19, Ill. Bulletin 10B is a 28-page general price list of a wide line of coaxial

cables and fittings, miscellaneous line accessories, tower lighting equipment, antennas, antenna equipment and components.

Phase Meter. Technology Instrument Corp., 1058 Main St., Waltham 54, Mass. A cardboard-covered bulletin gives an illustrated description of the type 320-A phase meter. The instrument described makes possible the measurement of phase difference between two voltages at audio and ultrasonic frequencies essentially independent of voltage amplitude, frequency and wave shape.

Timing Motors and Devices. Haydon Mfg. Co., Inc., Torrington, Conn. Catalog 321 gives a twenty-page detailed treatment of a line of synchronous timing motors, chart drives, timing devices and clock movements. A separate page is devoted to each item for ease of reference.

Recording Equalizers. Fairchild Recording Equipment Corp., 154th St. & 7th Ave., Whitestone, N. Y. The 626-A1 and B1 NAB equalizers for modifying frequency characteristics of a recording system are described and illustrated in a new bulletin. Specifications and catalog listings are included on the single sheet.

Capacitance Checking. Aerovox Corp., New Bedford, Mass., has issued an illustrated folder on the capacitance and resistance bridge for quick checking of capacitance, resistance, power factor, shorts, and opens, and leakage.

X-Ray Protection. National Bureau of Standards, U. S. Dept. of Commerce, Washington 25, D.C., has published a handbook, Medical X-Ray Protection up to Two Million Volts, giving recommended standards of safety for the installation and use of high-voltage x-ray equipment. The 49-page handbook No. 41 is obtainable for 15 cents from the Superintendent of Documents, U. S. Govt. Printing Office, Washington 25, D. C.

European Technology. Office of Technical Services, Dept. of Commerce, Washington 25, D. C. A new 270-page subject index and abstract collection of more than

1,000 unclassified scientific and technical reports on European technology has been prepared by the Combined Intelligence Objectives Subcommittee. Designated as PB96941, the volume sells for $3.00 per copy.

Selenium Rectifiers. Vickers Electric Division, Vickers Inc., 1815 Locust St., St. Louis 3, Mo. A 24-page catalog illustrating selenium rectifier characteristics, applications, design factors and listing prices is now available on request. Ask for catalog VC-3000.

Capacitor Assembly. The Compton Co., Bethesda, Md. A short bulletin on one side of a sheet covers the type 6MA Capaci-Ring, a capacitor assembly designed to simplify the problem of socket terminal r-f by-passing. The unit described is designed for application to the standard 7-pin miniature tube socket.

D-C Motor Control. Westinghouse Electric Corp., P. O. Box 868, Pittsburgh, Pa. Booklet B-4112 is a 23-page treatment of Mot-O-Trol, a packaged electronic, adjustable speed drive for precise control of d-c motors operated from a-c sources. Technical and application data are included.

House Organ. International Rectifier Corp., 6809 So. Victoria Ave., Los Angeles 43, Calif., has announced publication of the first issue of Rectifier News. The four-page periodical will feature technical articles on new developments in the field of dry-plate rectifiers for converting a-c to d-c. Regular subscription is available to all qualified engineers without charge if requested on company stationery.

Photoelectric Cells. Vickers Electric Division, Vickers Inc., 1815 Locust St., St. Louis 3, Mo., has made available catalog VC-4000, describing and illustrating a line of self-generating photoelectric cells. Applications and design specifications are given.

Tele Camera Chain. Television Equipment Corp., 238 William St., New York 7, N. Y. Model 1200A portable television camera chain, designed for image orthicon pick-

up tubes, is discussed in a four-page brochure. Description, features and summary specifications are included.

Technical Data Sheets. Radio Corp. of America, Harrison, N. J. Four recent data sheets give technical information on the 3RP1, a 3-in. oscillograph tube; the 12S8-GT, a triple diode, high-mu triode; the 5794, a fixed-tuned oscillator triode for radiosonde service at 1680 mc; and the 408S3, an 8-in. permanent magnet speaker.

Multipurpose Carrier. Lenkurt Electric Co., Inc., 1113 County Road, San Carlos, Calif. Radio and wire-line applications are both covered by the Type 44 carrier equipment described in a new folder, Form 44P4. The pamphlet shows how the units can be used for voice, telegraph, telemetering and control installations as well as a wide variety of combinations of the four uses.

Signal Generator. J. & A. Television & Manufacturing Co., 5066 Broadway, Chicago 40, Ill. A four-page bulletin describes and illustrates model 30G1 composite video generator designed for use on the television receiver production line, in the laboratory, television transmitter or by the serviceman. The unit described supplies video synchronizing and blanking pulses plus a video dot pattern for alignment purposes.

Tube Data. Radio Corp. of America, Harrison, N. J. Bulletins are now available giving technical data on the following new tubes: the 4-65A a vhf power tetrode; the 16AP4, a 16-inch metal picture tube; the 5763, a vhf beam power amplifier (9-pin miniature type); the 715-C, a pulse amplifier tetrode; and the 5825, a half-wave rectifier tube for r-f operated, high-voltage, low-current power supplies.

Mobile-Service Antenna. Andrew Corp., 363 E. 75th St., Chicago 19, Ill. Tentative Bulletin 102 is a one-page description of the Cardioid antenna, a vertically polarized, directional, ground plane antenna for transmitting and receiving in the 152 to 162-mc band. Accessories are also listed.

(continued from p 130)

ber, author, title, date, paging and prices. Volume and page numbers given in parentheses at the end of citations refer to the Bibliography of Scientific and Industrial Reports where abstracts may be found.

The 16-page infrared bibliography is available from the Office of Technical Services, U. S. Department of Commerce, Washington 25, D. C.

Television Information Committee

TO PRESENT full, factual information on television to the public, the government and other interests, an industry committee was recently appointed by Max F. Balcom of the RMA. Outstanding engineers and technical television experts of the industry will assist in the public relations project which will include information on present tv service and receivers in the vhf channels, and also in prospective future uhf channels.

The committee is headed as chairman by Paul V. Galvin of Motorola Inc., Chicago. Other members are as follows: Benjamin Abrams of Emerson Radio & Phonograph Corp.; W. R. G. Baker of GE; H. C. Bonfig of Zenith Radio Corp., James H. Carmine of Philco Corp.; James W. Craig of Crosley Division, Avco Mfg. Corp.; Allen B. DuMont of Allen B. DuMont Laboratories, Inc.; Joseph B. Elliott of RCA Victor; and William J. Halligan of the Hallicrafters Co.

BUSINESS NEWS

MICROTONE Co., Minneapolis, Minn., hearing-aid manufacturer, has purchased the Audiometer Division of the Audio Development Co., Minneapolis, to consolidate production of medical and portable speech-testing audiometers.

WALTER E. PEEK, INC., Indianapolis, Ind., is a newly formed company engaged in the manufacture of television antennas.

AIRBORNE INSTRUMENTS LABORATORY, Mineola, N. Y., recently organized a new research group designated as the Applied Physics Section. The new unit is presently

engaged in the development of a neutron velocity selector for Brookhaven National Laboratories.

COLUMBIA WIRE & SUPPLY CO., assemblers of cord sets, wire and wire products, recently moved into a new

Columbia Wire's new building

and larger building at 2850 Irving Park Road, Chicago 18, Ill.

GENERAL ELECTRIC CO., Syracuse, N. Y., will spend over a million dollars to provide for picture tube manufacturing and engineering facilities at Electronics Park. Production is expected to start in August. The first size to go into mass production will be the new 8½-inch metal-cone tube.

STATION WOR-TV has purchased the entire square block bounded by 67th and 68th Streets, Broadway and Columbus Ave., New York City, as a site for the future construction of buildings for offices and studios.

PERSONNEL

ARTHUR V. LOUGHREN, formerly director of engineering, has been elected vice-president in charge of research at Hazeltine Electronics Corp.

ORVILLE M. DUNNING, for the past several years engaged in administrative and technical supervision of engineering work under military contracts for Hazeltine Electronics Corp., was recently elected its vice-president in charge of engineering.

WAYNE S. WAMSLEY, formerly electronics project engineer in the Research and Development Laboratories at Ft. Belvoir, Va., has joined the staff of the National Bureau of Standards where he will conduct radar, radio and electronics research in the Ordnance Engineering Laboratory of the Electronics Division.

HARRY JACOBS, with the KGO engineering staff since 1937, was re-

cently appointed station engineer in charge of the KGO-TV and KGO-FM transmitters in San Francisco, Calif.

HARVEY J. FINISON, former application engineer for the General Electric Co., has been named assistant chairman of the electrical engineering department of Armour Research Foundation, Illinois Institute of Technology.

ROGER E. ROBERTSON, previously associated with Bell Aircraft Corp. as an electronics engineer, has been appointed to the staff of the National Bureau of Standards to conduct engineering research for the guided missile projects of the Electronics Division.

JOHN F. DREYER, JR., formerly consulting engineer for Dreyer Surveys, Inc., has joined the staff of Crosby Laboratories, Mineola, N. Y.

RAYMOND F. GUY, manager of radio and allocations engineering for the NBC, was recently appointed chairman of the engineering committee of the Television Broadcasters Association Inc.

FRANK R. NORTON has been promoted from principal research engineer to chief engineer of the radio-television and broadcast division of Bendix Aviation Corp., Baltimore, Md.

F. R. Norton

R. J. Slutz

RALPH J. SLUTZ, formerly with the Institute for Advanced Study, has joined the electronics division of the National Bureau of Standards to work on basic research, design and development of electronic computers.

LESLIE J. WOODS, with Philco since 1925 in various engineering and management capacities, has been

appointed vice-president and director of research and engineering at Philco Corp., Philadelphia, Pa.

PAUL F. WALKER, formerly with the Andrew Corp., Chicago, has joined the engineering staff of Cleveland Container Co., manufacturers of tubes for television deflection yokes.

DAVID R. HULL, formerly assistant chief of the Bureau of Ships for electronics in the Navy and more recently assistant technical director of the International Telephone and Telegraph Corp., has been named executive vice-president of Capehart-Farnsworth Corp., subsidiary of IT&T.

CLEDO BRUNETTI, associate director of Stanford Research Institute, has been appointed to the Research and Development Board of the National Military Establishment, to head the board's subpanel on miniature components and packaged subassemblies.

ROGER M. WISE, presently engaged in tube research and development for Philco Corp., has been awarded the Certificate of Merit by President Truman for his war work on subminiature tubes for proximity fuzes.

COAX CABLE INVENTORS

Twentieth anniversary of the invention of the coaxial cable system (May 23, 1949) found the two Bell Telephone Laboratories engineers who invented it comparing their first experimental model with the newest type of cable. Lloyd Espenschied, left, holds a section of the early, experimental cable which was installed at Phoenixville, Pa., late in 1929. His colleague, Herman A. Affel, holds a section of the modern, eight-tube cable now being installed in the Bell System's expanding coaxial cable network. Today's cable can carry 600 simultaneous telephone conversations or two television programs on each pair of the eight tubes

NEW BOOKS

Radio Wave Propagation

Report of the N. D. R. C. Committee on Propagation, C. R. BURROWS, *Chairman,* STEPHEN S. ATTWOOD, *Editor. Academic Press Inc., New York, 1949, 548 pages, $8.80.*

THIS book has been long awaited by the many workers who are familiar with the program of study of wave propagation conducted during the war by the NDRC Committee on Propagation as an aid to siting and predicting the performance of radar equipment. The only other book to cover this ground is Volume 13 of the Radiation Laboratory Series, which recounts the work of the MIT group on microwave frequencies. The present volume generally covers the frequency from 100 to 100,000 megacycles.

The book is divided into three sections. The first is a technical survey, including theoretical and practical studies of standard and nonstandard propagation. The second records a number of propagation experiments made under military and NDRC auspices, while the third treats transmission problems in the standard atmosphere in detail.

The book is as authoritative and exhaustive in its treatment of the vhf and uhf propagation problems as one could wish. The treatment is mathematical, but a number of useful nomograms are included for those not inclined to lengthy computations. The book should prove most useful in bringing a wider circle of readers into the mysteries of propagation above 100 mc, on which the future development of radar, television and microwave communications so largely depends.—D. G. F.

Nuclear Radiation Physics

BY R. E. LAPP AND H. L. ANDREWS. *Prentice-Hall, New York, N. Y., 1948, 487 pages, $6.00.*

WRITTEN as an introductory textbook to the suddenly important field of nuclear physics, this book presents well-rounded descriptions of various radiation phenomena in nuclear physics. The sequence of subject matter of the chapters and the developments within chapters are from simpler concepts and phenom-

ena to the more complex, following the historical growth where it fits this pattern. The treatment is predominantly descriptive, interspersed with illustrative calculations and problems.

Whereas most of the recent books on this subject follow a pattern of more or less rigorous mathematical development of theory, this text describes the phenomena and the theory of its mechanism with a minimum of mathematical derivation. It might well be termed an engineering treatment as distinguished from a scientific treatment. Thus, although the academician may criticize the book for lack of rigor at some points, the practicing engineer will find it an illuminating introduction to nuclear phenomena and means for dealing with it, as well as a compact, readable presentation. For those wishing to pursue certain topics further, well-chosen references at the end of each chapter provide a key to the literature. —FRANK H. ROCKETT, *Airborne Instruments Laboratory, Mineola, N. Y.*

Theory of Oscillations

BY A. A. ANDRONOW & C. E. CHAIKIN. *Edited under the direction of Solomon Lefschetz. Princeton University Press,* 1949, 358 *pages,* $6.00.

IT IS not easy to find books written on theoretical subjects of interest to electrical engineers where the difficult problem of combining advanced mathematics and circuit practice is solved as satisfactorily as in this work on theory of oscillations.

The authors of this book are Russian and from reading the text one can presume that they are a mathematician and engineer respectively. The book however has been translated, condensed and edited by a group of Princeton University personnel under the direction of Professor Lefschetz; it is not easy therefore to share the credit properly between the Russian authors and the American editors and translators.

The field of the theory of oscillations has been studied for more than a century and the mass of theoretical material available on the

subject is unquestionably staggering. Some of the abstractions and generalizations which were formerly of no practical interest have been realized by means of vacuum tubes. Thus the theoretical mathematician finds his love for abstractions once more vindicated when the engineer has to use basic theories written many decades ago to fully explain the characteristics of flip-flop circuits or discontinuous oscillators. On the other hand the authors were faced with the difficult task of choosing the important contributions in a century of scientific work, coordinating the different sections and illustrating each step with practical considerations. In this task the authors succeeded beyond expectations. The book is such that engineers, who remember their college mathematics and are not afraid of the apparent complication of some of the terminology, can read without difficulty. The reader will be amply rewarded by a clearer understanding of devices he uses every day, an understanding that will help him in many development problems.

The book begins with an explanation of the familiar L, C, R tuned circuits from a point of view that will be new to many engineers. Full use is made of the representation in the phase space where the coordinates are displacement and velocity, or charge and current or voltage and current. Such concepts as singular points and phase portraits are thus introduced with reference to extremely well-known physical examples. Naturally the importance of these concepts in nonlinear oscillators derives from the fact that it is often much easier to determine the trajectories of the point representing an oscillator in the voltage-current coordinate plane than to determine the functional relation between these magnitudes and time.

Nonlinear systems are then considered and the concepts introduced in the first chapter are expanded to cover first nonlinear systems without friction or externally supplied energy, and then nonlinear systems where energy is either expended or supplied (non-conservative); systems which produce periodic motions whose amplitudes do not vary much when the systems are changed

a great deal are considered in particular detail. In this chapter the clock and feedback (tuned grid) oscillator are considered together.

The general family of systems of which the gas tube sweep generator is a typical member is then discussed, followed by a theoretical chapter on the large family of systems that need for their definition two first-order differential equations. The flip-flop circuit is a typical representative of this family and this reviewer found here one of the most satisfactory explanations of this familiar device. Discontinuous oscillators, of which the capacitance-coupled multivibrator is a typical example, are then fully discussed.

After a short chapter on cylindrical phase fronts of very little interest for electronics engineers, the book ends with a chapter on the Van der Pol and the Poincare's method for the quantitative study of wave shapes in nonlinear systems that do not differ too much from linearity. Here the difference between self-starting (soft) and non-self-starting (hard) oscillations is discussed. Mixed cases are also considered. This chapter is the only one where detailed analysis of wave shapes is actually made. A tribute to the power of the mathematical methods employed in the previous chapters is represented by the fact that almost all information necessary for the development of nonlinear oscillators had been given before employing only the representation in the phase space.—E. G. FUBINI, *Supervising Engineer, Airborne Instruments Laboratory, Mineola, L. I., N. Y.*

• • •

Books Received for Review

DICTIONARY OF GUIDED MISSILE TERMS. By Committee on Guided Missiles, RDB. Public Affairs Press, Washington, D. C., 57 pages, $1 paperbound, $2 clothbound. Outgrowth of smaller classified monograph compiled in 1947 by Lt. Col. J. A. White, defining new words coined for guided missile art, conventional words that have been given different meanings, and certain general technical terms.

PERSONNEL MANAGEMENT. By W. D. Scott, R. C. Clothier and W. R. Spriegel. McGraw-Hill Book Co., Fourth Edition, 1949, 648 pages, $4.50. Principles, practices and point of view. Completely revised to emphasize wartime and reconversion changes in union-management relations and the increasing importance of psychology in initial selection, transfer, promotion, training, morale measurement and boosting productive efficiency.

Backtalk

This department is operated as an open forum in which our readers may discuss problems of the electronics industry or comment upon articles that ELECTRONICS has published.

Shocking Business

DEAR SIRS:

ON SEEING MY LETTER to Steven Pantages in print (April *Backtalk*), it looked rather sarcastic, so I'd like to do a little apologizing.

His suggestion brings up some interesting points on the electric shock hazard. The idea of wearing a short circuit between hands would look a little less risky in high-power circuit applications if *insulated* jumpers and contacts were applied. However, one would still get his fingers or hands burned off.

Still another angle lies in the matter of migration currents. Since body skin resistance is relatively high, the presence of a metallic jumper making contact with the fingers, hands or arms, might not shunt enough current to prevent electrocution. Only about 0.1 ampere will kill, regardless of the voltage applied.

Another problem is that an electrical shock presents other hazards besides strangulation, heart stoppage, tissue burns and so on. One might fall off a high tower, drive a screw-driver through an eye, smash one's skull on a steel beam, burn one's eyes out with a blast of molten metal, damage the retinas with an intense short-circuit arc flash, cause one to shove his arm into moving machinery, and so forth.

However, the jumper idea has some interesting possibilities. A large insulated conduction band around both arms might shunt enough current around the vital heart, lung and brain areas to prevent death, even though hands might be charred or severed by high-power circuits.

While working on power transmission systems, some electricians and technicians safeguard themselves by pulling all fuses and switches, tying switches and break-

ers in the open position, and by coupling massive jumpers across the feeders at the point where the work is being done so that breakers or fuses will blow if some irresponsible worker throws them without checking up first.

Another difficulty with applying safety devices lies in attempting to get personnel to wear them, particularly in hot weather. The resistance to regulations, to something new, and the addiction to the gambling urge, seem to be all too universal human traits.

TED POWELL
Maspeth, N. Y.

Valves

DEAR SIRS:

IN THE ARTICLE entitled, "European Receiving Tubes" by H. A. S. Gibas in February, 1949 ELECTRONICS, the names of the principal British valve manufacturers are given, and the statement made that, "All these make similar tubes as the Continental standard types, some with different designations."

We wish to put on record the fact that Standard Telephones and Cables Limited do not make equivalents of the so-called Continental types, and do not contemplate doing so.

Our policy has been consistently directed to cover all overseas markets, and with that point in view a comprehensive range of the more popular American types are manufactured and listed by this Company under the "Brimar" trade mark.

B. J. AXTEN
Publicity Manager
Standard Telephones and Cables Ltd.
London, England

How About Gates?

DEAR SIRS:

ALL THIS TALK, talk, and more talk about where are the frequencies to come from for the utility companies, the taxicab companies, the nurses' call, doctors' exchange, and miscellaneous other utilities (including police and fire) seems to me a bit superfluous.

While it may be true that in New

York, Chicago, Los Angeles, and other cities whose population exceeds 1 million, a problem may arise, the solution for the major part of the USA seems simple.

Under the present setup, only one taxicab can logically have a station on the share-the-same-frequency setup. No other taxicab company will get radio for their competitor to "listen in" on a share-time basis. This has been the main objection of the second and third "sharers" to get radio, after one company already has it.

Apparently a very important development of the war has been forgotten in planning utility radio. That is the idea of pulse time modulation.

It seems to me that a band of frequencies similar to the television channels could be set up for pulse time stations in the public interest. Owned and operated by a separate company or a corporation whose stock is controlled by the individual subscriber companies, the pulse time station would operate at all times, transmitting those messages it receives from the individual dispatchers in the member company offices.

The cabs of company A would receive only the signals meant for them, as their receivers would be gated that way (to borrow the term from radar). Likewise, company B's mobile units would not receive any of company A's or anyone else's messages except his own.

A system for New Orleans, as an example, would not need more than ten or twelve gates. This would take care of the police department (1), fire department (2), utility companies (3 and 4), three taxicab companies (5, 6 and 7), doctors, nurses and emergencies (8), city emergency services (9), and for twelve channels, the remaining channels would be available for other services.

The system is one in which the transmission (c-w) is cut up into twelve equal pulses, or gates, and a thirteenth trigger pulse. In each section of time, the voice frequencies are modulated on the carrier only during the gate applying to one particular subscriber's time. In other words, gate number one might carry only the information

of dispatcher A, and so on.

Each receiver would have an oscillator which is synchronized by the trigger pulse, then phased to the proper gate time, and applied to the i-f's to turn them on only during the proper gate.

I believe the whole system could be placed in one channel about the size of one present television channel. Answer back would require a separate frequency for each subscriber, but if the answer back is allocated in the vhf band (about 200 or 300 mc) and suitable receivers placed at selected spots in the city, sufficient room could be found. Several noncompetitive subscribers could even use the same answer back frequency, as most answers are short messages.

In cities other than the crowded few, it would be highly possible to utilize one or more of the unused television channels for this purpose. Look at all the unused frequencies all over the country being held open for no justifiable reason except that they are being used in New York, and will maybe be used 1 or 2 hundred years from now in another city.

Another item that needs rectification is the present ship-to-ship and ship-to-shore frequency setup. There is no earthly reason, from the low frequencies and short distances involved, to continue to use the crowded short wave (2 to 5-mc) range. In New Orleans, some fisherman cannot tell his wife that he will be late for dinner because a 100-watt tug is carrying on a long-winded orders conversation with his office. Again on 2,670 or 2,638 it is next to impossible to find time to talk. It seems that everyone is there. Why not give the geophysics floating laboratories their own frequency and forbid them the use of the fisherman's channel; give the tugs their own frequency to use and forbid them to use the geophysicist channel and so on.

The only ones that seem to have logical reasoning in assignment are the present vhf aircraft channels.

Yours for better utility of the radio spectrum,

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4J47	45.00	10	.67	811	2.20	5HP1	4.95
4T4/2	9.95	10Y	.60	812	2.85	7AP7	6.49
5C30/C5B	9.95	12A6	.23	813	8.90	7BP7	4.75
5D21	24.95	12AH7GT	.87	814	2.61	7HP7	5.95
5J29	17.98	12AT6	.45	815	2.45	9GP7	13.98
5R4GY	1.05	12AU7	.69	816	1.10	9JP1	3.95
5T4	.96	12AX7	.89	826	.69	9LP7	2.69
5U4G	.46	12BA7	.89	828	6.49	12DP7	14.95
5V4	.95	12BE6	.45	829B	5.95	12GP7	12.80
5W4	.87	12C8	.65	832	2.45	12LP4	38.49
5X4G	.71	12H6	.36	836	1.12	912	79.95
5Y3GT	.38	12J5GT	.45	837	2.35	**Tungar*Bulbs**	
5Z3	.81	12K8	.85	838	3.98	20X672*	$2.95
6A3	.98	12K8Y	.98	842	2.75	189048*GE	3.49
6A4	1.29	12Q7GT	.69	845	4.75	199698*	2.95
6A6	1.02	12S8GT	.79	851	16.95	289881*	2.50
6AB7/1853	.84	12SA7	.59	860	1.97	**Aviation Lites**	
6AC7	.85	12SA7GT	.50	861	11.90	C1249	
6AF6G	.87	12SG7	.69	865	1.00	12VGR	
6AG5	.81	12SJ7	.64	866A	.99	12 for	$1.00
6AG7	1.27	12SK7	.63	866Jr.	1.00	**Sealed Beam**	
6AH6	.98	12SK7GT	.58	868/PJ23	1.90	4522/250W	1.49
6AJ5	.85	12SL7GT	.85	872A	2.45	4560/600W	3.50
6AK5	.85	12SN7GT	.54	874	1.49		

Tubes Gtd Exc Open File Breakage. C'R Tubes Gtd Only Via R'Exp

LAMPS, PILOT LIGHTS

Mazda PL**		Neon Bulbs	
47**Box 10	.50	NE2Qty100	3.98
44**Box 10	.50	NE16/991	.25
49**Box 10	.50	NE45/½W	.24
55**Box 10	.50	NE51 NE20	.07
64**Each	.07	100 for	5.00
S6 T4**Ea	.15	**Bull's Eye PL****	
10 for	1.39	DIALCO w/S6	
100W/20V**	.25	115Vbulb 2/98¢	
313 28V**	.10	Wstghs C7**	
323/3V**	.10	7W/120V	.09
Sylvania S6**		**TelSlide Lamps**	
6W/120V	.15	6, 12, 24, 48,	
Qty 10	1.25	55V Each	18¢

BASIC PHOTOFLASH KIT

Complete Pwr Supply Parts, Data, Lamp&Refl. For115vac ONLY $29.95

FLASH CONDENSERS—FILM

5(109.5W-Secs) for $12.50

16mfd/600vac/2800vdcINT 6.49

TAB "Sunflash" Special

NON-DARKENING, UNIFORM LITE OUTPUT, 100 to 300 Watt-Sec Input, SHOCK MTD, 100,000 or MORE FLASHES, 4-PRONG BASE interchangeable 5804X w/DATA& CKT SPECIAL $10.98

X400 Air Corps Lamp $11.98

Write for your FREE Tabogram

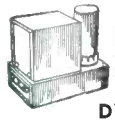
2J1G1 Selsyns Buy!

with DATA 24V or110V 60 cyc AC Used Tested, TWO for **$1.49**

HEAVY DUTY MICA

Cndsr CornDub BT14 .012mf/25000 ..... $4.98

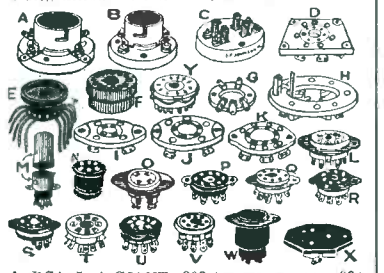
VIBRAPACKS



6VDCin, 425V/110ma $10.95
PE157SpkrBat&Chgr p/o SCR-593 & Spkr 8.95
12VDCin, 190V/85ma Out 3.49
PP18AR 12-13 Vin24VDC $6.95

DYNAMOTORS

6vIn/240vOut/100ma (125maInt) or 12&24vIn/500v Out 50maNEW HiEff P'Mag Gtd..$3.49
28vIn Output375v/160ma Cont (540/250maInt) p/o SCR274 Good Used $1.49
12or24vin/275v@110ma &12v@3a. PM $1.95
PE-94A BENDIX MG-1A NEW Complete V'Reg in&out fitrs & RelaysForSCR522..$9.95



A. RCA 5-pinGIANT, 803etc ..... 90¢
B. Johnson 4-pinBayon, 866etc ..... 49¢
C. Johnson 124-213, 304TLetc 1.15
D. Johnson 7-pinSteatite, 829B, 25¢ ..... 5/$1
E. SmallShell DUODECAL, 2BPletc ..... 59¢
F. MedShell DIHEPTAL CinchM1CAbklt ..... 69¢
G. 5-pinACORN 1 9/16"diaHAMLET 25¢; 5/$1
H. Johnson122-234, w/tubeLock, 5D21etc. 69¢
I. 4-prongSTEATITE Johnson, 866 ..24¢; 5/$1
J. 5-prongSTEATITE Johnson, 807 ..27¢; 4/$1
K. 7-pr STEAT Johnson, 1625 ..... 29¢; 2/49¢
L. 7-pinNATIONAL 4-TRTL Steatite.24¢; 5/$1
M. MIN 7-pin Mica147-913&Shield ..... 30¢
M. MIN 7 pin Amph 78-7PT ..... 11¢; 10/98¢
N. AMPH fem78PTin4,5,6,7,8 ea ..... 16¢; 6/89¢
O. 4-pinAMPH49RS84&mtgCeramic..24¢; 5/$1
P. OCTAL 8-pin&plateSteatite Cinch..9¢; 12/$1
Q. OCTAL 8-pin&plateSteatite Cinch..18¢; 7/$1
R. LOKTAL 8-pin&lock plate Cinch..11¢; 10/$1
S. KLYSTRONSocket Cinch, ea ..... 35¢; 10/$3
T. LOKTAL Amph 49S8L Steatite..24¢; 5/$1
U. OCTAL Amph 78S8micaBklte..8¢; 25/$1.49
V. U. 11-pin78S11/931Amph ..... 15¢; 7/$1
V. OCTAL Amph49S8Steatite..15¢; 12/$1.49
W. HiV Safety4-pinAmph77A4 ..... 30¢; 4/$1.15
Y. MAGNAL 49S11L ceramic ..... 54¢; 2/98¢
BANTAM Jr. 78-5H Amphenol ..... 7¢
SOCKET FOR 872-211 ..... 49¢
SOCKET Ceramic 4-prongSilvPl simJOHNSON 122-244 for 8008, C6J, 5C22, 575 ..... 98¢
MAGIC EYE ASSY Amphenol ..... 59¢

TRANSFORMERS—115V 60 cyc Input

1000VCT/200ma, 6V/5A, 5V/6A, Fully Encl w/90V biasTap&18V/.55Awdg $6.95
880VCT/125ma, 6.3VCT/3A, 5VCT/3A, 6.3VCT /2A H'Sld HVins Dlvrs250maUSN $3.98
700VCT/120ma, 115V/100ma, 2x6.3V/1A, 5V/ 2A Csd HVins $2.98
650VCT/175ma, 5V/3A, 6.3V/2.1A $3.29
500VCT/60ma, 6.3V/4A USN H'Sld $1.29
420VCT/85ma, 6.3/1.9A&Pri's 6-12-24-115VDC &230VAC UnivVibXfmrCsd $2.39
2x330VCT 10ma(or660VCT/10ma) Csd $1.49
1200VCT 300ma&18V/1AwndgCsdHVins $6.95
1800V/4ma USN Csd Altec/GE HVins $3.29
2100V/10ma STANCOR Csd HVins 3.98
3000V/10ma WE/ChiTrans Csd HVins 4.50
5000V/10ma(or2X2)Csd 7.95
7500or15000V Dblr,35ma 17.95
10800VCTor2100V Dbh@95maCsd $19.95
2.5V 1.75A, 4V/16A 20KVins Csd 4.95
2.5V 2A(or2X2)HVins 69¢; 10 for 5.98
5VCT/60A KENYON HVins 6.95
5V/115A KENYON HVins 12.95
6.3VCT/.7A USN Csd HVins 1.39
6.3VCT/4A(gud6.5A)Csd HV USN 1.69
12.6VCT/2A H'Sld HVins $1.49; 2 for 2.79

FILTER CHOKES

13.5Hy/1Amp/42ohm/17KVins $54.00
15-29Hy/150ma Swinging Cased 2.95
12Hy/300ma ....$3.95; 3Hy/40ma..3 for.. 1.00
15Hy/400ma or 20Hy/300ma/12KVins..... 7.95
8Hy/150ma NewI"Ts CrekedBkltT'bd 2/ 2.25
50Hy/125ma Csd..$1.95; 8Hy/100ma..... 1.10
12Hy/275ma....$3.29; 15Hy/80maGE..... .79
3Hy/275ma &2x17Hy/125ma H'Sld..... 3.49

BATTERIES—Storage & Dry

A. BB206U 2V/11AH $1.89
A. NT6/BB214U 6V/6AH Willard S'Bat $1.75
B. BB54 2V/27AH ..$1.89
C. Willard 4v/40AH..$5.95
D. Willard ER25 6V/25AH S'B.....$3.98
D. Willard ER40 6V/40AH S'B..... 6.98
E. BR18/BR52 36VminS'B....98c; 12/$10
F. BurgessXF2BP '47date.....8 for $1
G. Eveready HvyDty Minimax BA43, 90, 45, 1½V w/octal skt 2⅝x4¾x6¾"/Grd. '47date ..... 98c; 2/$1.89

USN Hydrometer Kit & Box..... 1.98
BatAcid (R'Exp) pt. .....59c; 2 pts....98c
WESTON Std Cell unmtd 1.019‡Avg..$5.98

BARGAINS—New Dry Batt's

SigCorps SPECIFICATIONS

OutDated Tested—Gtd Plenty Life!

SigC	Volts	simBurgess	Each
BA34	−7½,−6,−4½	5540p 0772	39¢
	−3,−1½	WestonMtr	
BA35	1½	4FH	39¢
BA36	45, 22½	5308	1.25
BA37	1½	HvyDty Walky Talky	29¢
BA38	103½	Walky Talky	$1.49
BA40	90, 1½	4GB60	$1.19
BA40	90, 1½	4GB60	$1.69
BA41	60,25½,4½	3½x2½x2"	89¢
BA51	67½	MiniMax	89¢
BA70	90,60,4½	6½x10½x4½	$2.50

XTAL DIODES

No.	Each	2 for	10 for
1N21	$1.00	$1.79	$8.30
1N21A	1.00	1.79	8.30
1N21B	1.75	3.35	15.00
1N22	1.50	2.79	14.00
1N23	1.50	2.79	14.00
1N23A	1.50	2.79	14.00
1N23B	3.00	5.90	27.50
1N26	3.00	5.90	27.50
1N27	1.75	3.15	14.98
1N35	2.79	5.30	25.98
1N34	1.15	2.25	10.49
1N48	1.28	2.49	11.50
1N51	1.28	2.49	11.50

XTAL OVEN for ANY FT-243mtd XTAL oper 4–28VACDC ..... 98¢

THERMISTORS, VARISTORS

D167019 Vol Limitr..... Ea. $2.95
D168391 ThermComp ..... Ea. $2; 3/$5
D168392 ThermComp ..... Ea. $1; 6/$5
D170396 HF PwrMeas..... 90¢; 3/$2.50
1C Bulb TimeDelay..... 90¢; 3/$2.50
USN CW20259 Varistor38C..... $2.95

PRECISION RESISTORS

.116to95,000 ohms ..... 30¢; 10/$2.50
100Kto950K ohms ..... 40¢; 10/$3.50
1 to 20 Megohms..... 75¢; 10/$6.50
Vac Precision HiVolt Resistors .12, .25, .6, .75, .83, .99, 1, 1.5, 2, 3, 3. 75megohms ½% accy ..... $1; 10/$7.50
1Meg/MFC105/.5%accy JAN..$1.98; 6/$10
30Meg/MVZ8/20W/25KV ....$1.98; 6/$10
50Meg/MVE8/25W/40KV ....$1.98; 6/$10
20Meg/20KV/½% SPRAGUE $10.98
w/O-1ma Meter $14.98

NEW RCA TV Components

Part No.	Your Cost
Sim RCA 201D1 Yoke	$4.23
RCA 201D2 Yoke	7.26
RCA 202D2 Foc Coil	6.13
RCA 203D1 Ion Trap	2.79
sim RCA 204T2 V'Xfmr	2.98
Sim RCA 211T1 H'Out&HV	4.98
RCA 211T5 H'Out&HV	7.15

Also RCA Parts—201R1, 55¢; 201R5, 66¢; 201T6, $14.52; 202D1, $4.23; 204T1, $11.17; 204T3, $6.71; 204T9, $2.52; 208T1, $2.18; 208T2, $1.72; 208T3, $1.53; 211T2, $10.61.

Kit—**CONVERSION** to 16" PipRCA parts 201R4, 201R5, 202D2, 211T5 ..... $15.98

XTRA SPECIAL—New TV Parts

UTAH 9318 H'Blkg Osc Xfmr H'sld..98c
UTC S8662 V'Blkg Osc Xfmr Herm Sld 98c
Focus Coil Magn Focus Kinescopes..$3.79
ERIE HiV Cndsr 500mmf/10KV 40c
JEFFERS Cndsr 500mmf/20KV 75c
TWINEX 300 ohm TV cable 100 ft..$1.98
1000 ft. $16.98; 5000 ft..... $59.95
HELLER SPEED Twinex Tacker..... $3.98
5000 Hvy Dty Staples, Boxed..... 2.98

BLOWERS—Cool That Tube

40CFM 28vacde $3.49
100CFM 12vacde 5.95
100CFM 28 vacde $4.95
Xfmr 12or28v to 115vac 1.98
250CFM&28/115vac Xfmr 10.95
70CFM 115v/400cy USN..... 4.49
100CFM 115vacde HvyDty..... 7.98
180CFM 115vacde HvyDty..... 10.98

4 Year FLASHER—Indispensable for Car or Boat, Neon Bulb Flashes Brilliantly, 4 yrs Shelf Life Less Batt....$1.19; 5/$4.98 with Batt's $1.98

ANTENNA UHF 12"/30 cm ATI/APN2, ATS/ARR1 usable citizen & Ham Band Thd'd Coax Term Instrd SilvPl Cont w/wpf kask flange & hardware for MOBILE mtg NEW 49c; 3/$1.00; PLS9 for above. 29¢

ANT AN130B Spring Swiv'ld Whip 33" lg SPECIAL..... 98c

ANT AN30 Telescopic Whip 12"to9ft

NEW O'Seas pkg ea$1.49; 2/$2.49

ANT MS49to52, 12½ ft..... $1.69

ANT MS49to53, 16ft..... 2.49

ANT MS49to54, 18ft..... 3.69

ANT MS49to56, 25½ft..... 5.98

AN131A11ftComprSpring&Sect $1.89

TAB MONEY BACK GUARANTEE 53 MIN. ORDER F.O.B. N.Y.C. ADD SHIPPING CHARGES AND 25% DEPOSIT. PHONE WO. 2-7230

THAT'S A BUY "TAB" THAT'S A BUY

DEPT. TE SIX CHURCH ST. NEW YORK 6, N.Y., U.S.A. - CORNER CHURCH & LIBERTY STS. ROOM 200

TAB MONEY BACK GUARANTEE 53 MIN. ORDER F.O.B. N.Y.C. ADD SHIPPING CHARGES AND 25% DEPOSIT. PHONE WO. 2-7230

PULSE EQUIPMENT

PULSE TRANSFORMERS

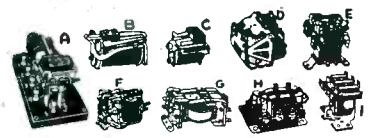
G.E.K.-2745 ..... $39.50
G.E.K.-2744-A. 11.5 KV High Voltage, 3.2 KV Low Voltage @ 200 KW oper. (270 KW max.) 1 microsec. or ¼ microsec. @ 600 PPS $39.50
W.E. #D166173 Hi-Volt input transformer, W.E. Impedance ratio 50 ohms to 900 ohms. Freq. range: 10 kc to 2 mc. 2 sections parallel connected, potted in oil $36.00
W.E. KS 9800 Input transformer. Winding ratio between terminals 3-5 and 1-2 is 1.1:1, and between terminals 6-7 and 1-2 is 2:1. Frequency range: 380-520 c.p.s. Permalloy core $6.00
G.E. #K2731 Repetition Rate: 635 PPS, Pri. Imp: 50 Ohms, Sec. Imp: 450 Ohms, Pulse Width: 1 Microsec. Pri. Input: 9.5 KV PK, Sec. Output: 28 KV PK. Peak Output: 800 KW. Riflar 2.75 Amp. $64.50
W.E. #D169271 Hi Volt input pulse Transformer. $27.50
G.E. K2450A. Will receive 13KV, 4 micro-second pulse on pri., secondary delivers 14KV. Peak power out 160KW. G.E. $4.50
G.E. #K2748A. Pulse Input, line to magnetron. $36.00
#9280 Utah Pulse or Blocking Oscillator XFMR Freq. limits 790-810 cy-3 windings turns ratio 1:1:1 Dimensions 1 13/16 x 1⅝" 19/32 ..... $1.50
G.E. 9318 Pulse Trans. 1:1:1 ..... $1.50
Raytheon UX 8693 3 x 32 Turns T.V. 1000 RMS. $4.95
UX-7350 ..... $5.95

PULSE NETWORKS

15A—1-400-50: 15 KV, "A" CKT. 1 microsec., 400 PPS, 50 ohms imp $42.50
G.E. #6E3-5-2000-50P2T, 6KV, "E" circuit, 3 sections, .5 microsecond, 2000 PPS, 50 ohms impedance. $6.50
G.E. #3E (3-84-810; 8-2.24-405) 50P4T: 3KV, "E" CKT Dual Unit: Unit 1, 3 Sections, .84 Microsec. 810 PPS, 50 ohms imp.: Unit 2, 8 Sections, 2.24 microsec. 405 PPS, 50 ohms imp $6.50
7.5E3-1-200-67P, 7.5 KV, "E" Circuit, 1 microsec. 200 PPS, 67 ohms impedance, 3 sections $7.50
7.5E4-16-60-67P, 7.5 KV, "E" circuit, 4 sections, 16 microsec. 60 PPS, 67 ohms impedance $15.00
7.5E3-3-200-6PT 7.5 KV, "E" Circuit, 3 microsec. 200 PPS, 67 ohms imp., 3 sections $12.50

DELAY LINES

D-168184: .5 microsec. up to 2000 PPS, 1800 ohm term $4.00
D-170499: .25/.50/.75 microsec. 8 KV, 50 ohms imp $16.50
D-165997: 1¼ microsec. $7.50



RELAYS

Type	Con-tacts	Rating	Res. Coil	Mfg	Price
H	DPDT (8A)	24–28V vde	170 ohms	GECR2791B 100F3	$1.75
H	3PDT	28 vdc	175 ohms	GECR2791B	1.25
H	3PDT	24–28 vdc	175 ohms	GECR2791B	1.75
H	4PST	24 vdc	180 ohms	GECR2791G	1.75
G	DPDT SPST	12 vdc	44 ohms	Leach 1067–490	1.45
G	DPDT	22–28 vdc	160 ohms	Leach	1.25
D	SPST	28 vdc	250 ohms	Allied BO48	1.39
I	DPST	14 vdc	85 ohms	Price X20-A	1.50
D	3PDT	24–28 vdc	280 ohms	Allied DOX-3	2.50
H	SPST	24–28 vdc	2490	GM 12917–1	2.00
D	DPDT	24 vdc	280	Allied BO635	2.00
D	3PDT	26 vdc	280	Allied KS	1.10
D	DPDT	28 vdc	280	Allied BO	2.10
D	SPST (NC)	75MA	60	Allied KS 5862	1.10
H	DPDT	20–30 vdc		Ounce 50XB	2.00
H	DPDT	10–14 vdc		Ounce 100AB	2.00
H	DPDT	24–28 vdc		PB21C057-A	1.75
H	3PDT	24–28 vdc		GECR2791	2.60
H	SPDT	24–28 vdc		GECR2791	1.75
A	DPDT (6A)	12 vdc		Ounce CX3190	2.40
A	SPDT	10–12v 60 cy	125	Ounce CX2120	2.40
H	DPDT	27.5 vdc	400	Allied	1.10
D	DPDT	9–14 vdc		Allied	1.10
H	DPDT	24v60cy	50	Allied	1.40

RADAR SONAR

- SE 10CM Shipboard Radar (Magnetron)
- SF 10CM Shipboard Radar
- SG 10CM Shipboard Radar
- SN 10CM Shipboard Radar (Lighthouse)
- SO1 10CM Shipboard Radar (Magnetron)
- SO13 10CM Shipboard Radar (Magnetron)
- SQ 10CM Shipboard Radar (Lighthouse)
- CPN6 3CM Beacon Gnd Installation
- APS3 3CM Airborne Radar
- APS4 3CM Airborne Radar
- APS15 3CM Airborne Radar
- QSG Underwater Sound Unit (Sonar)
- TBM Navy Transmitters
- TDE Navy Transmitters
- TBK Navy Transmitters
- RAK7 Navy Receivers
- DAB HF-Direction Finder
- DP12 LF-Direction Finder
- RC145 200 Mc. IFF
- RC148 200 MC. IFF
- SCR518 Pulse Altimeter
- APS2 10CM Airborne Radar

WRITE FOR INFORMATION AND PRICE

COMMUNICATIONS EQUIPMENT COMPANY *for your needs*

J.A.N. APPROVED
UG TYPE CONNECTORS

Deduct 10% from prices shown on orders of 100 or more per type

AN #	Price ea.	AN #.	Price ea
UG- 9/U	$1.18	UG-114/U	1.88
UG-10/U	1.95	UG-115/U	1.69
UG-11/U	1.82	CW-123/U	.56
UG-12/U	1.18	UG-131/U	7.50
UG-13/U	1.95	UG-146/U	2.81
UG-14/U	1.82	UG-154/U	6.69
UG-15/U	1.18	CW-155/U	.50
UG-16/U	1.95	UG-155/U	6.69
UG-17/U	1.82	UG-156/U	5.31
UG-18/U	1.25	UG-157/U	5.31
UG-18A/U	1.31	UG-160/U	2.38
UG-18B/U	1.95	UG-160A/U	1.94
UG-19/U	1.57	UG-167/U	3.75
UG-19A/U	1.72	UG-167A/U	5.31
UG-19B/U	1.82	UG-173/U	.38
UG-20/U	1.46	UG-174/U	20.00
UG-20A/U	1.57	UG-175/U	.19
UG-20B/U	1.76	UG-176/U	.19
UG-21/U	1.25	UG-188/U	1.18
UG-21A/U	1.31	MX-195/U	.94
UG-21/BU	1.36	UG-197/U	6.25
UG-22/U	1.35	UG-201/U	2.89
UG-22A/U	1.72	UG-202/U	3.44
UG-22B/U	1.68	UG-203/U	.76
UG-23/U	1.25	UG-204/U	2.81
UG-23A/U	1.57	UG-204A/U	2.81
UG-23B/U	1.62	UG-206/U	1.28
UG-27A/U	3.44	UG-207/U	22.50
UG-28/U	2.93	UG-208/U	22.50
UG-29/U	1.53	UG-212/U	5.63
UG-29A/U	1.95	UG-213/U	5.63
UG-30/U	2.19	UG-215/U	4.19
UG-32/U	25.00	UG-216/U	10.87
UG-33/U	25.00	UG-217/U	3.88
UG-34/U	21.88	UG-218/U	8.13
UG-35A/U	20.00	UG-222/U	43.75
UG-36/U	20.00	UG-231/U	2.50
UG-37/U	20.00	UG-235/U	35.63
UG-37A/U	20.00	UG-236/U	14.69
UG-57/U	2.81	UG-239/U	.64
UG-58/U	.81	UG-241/U	2.75
UG-59/U	3.44	UG-242/U	3.13
UG-59A/U	2.12	UG-243/U	3.44
UG-60/U	2.38	UG-244/U	3.13
UG-60A/U	1.63	UG-245/U	1.56
UG-61/U	2.56	UG-246/U	1.85
UG-61A/U	2.25	UG-252/U	5.63
UG-62/U	35.00	UG-254/U	2.28
UG-83/U	1.88	UG-254A/U	2.81
UG-85/U	2.06	UG-255/U	2.31
UG-86/U	2.16	UG-256/U	13.75
UG-87/US	1.75	UG-257/U	13.75
UG-88/U	1.46	PL-258	1.22
UG-89/U	1.19	PL-259	.70
UG-90/U	1.31	PL-259A	.76
UG-91/U	1.56	UG-259/U	5.13
UG-91A/U	1.31	UG-260/U	1.24
UG-92/U	1.38	UG-261/U	1.19
UG-92A/U	1.59	UG-262/U	1.31
UG-93/U	1.56	UG-269/U	3.25
UG-93A/U	1.81	UG-270/U	8.13
UG-94/U	1.56	UG-271/U	8.13
UG-94A/U	1.31	UG-273/U	1.88
UG-95/U	1.38	UG-274/U	2.48
UG-95A/U	1.69	PL-274	1.40
UG-96/U	1.55	UG-275/U	5.63
UG-96A/U	1.81	UG-276/U	5.63
UG-97/U	4.38	UG-279/U	3.00
UG-98/U	1.94	UG-287/U	6.56
UG-100/U	2.93	UG-290/U	1.06
UG-101/U	3.69	UG-291/U	1.31
UG-102/U	.90	UG-306/U	2.54
UG-106/U	.56	UG-333/U	5.88
UG-107/U	2.56	UG-334/U	7.19
UG-107A/U	2.88	UG-335/U	13.75
UG-108/U	2.19	UG-352/U	7.50
UG-109/U	2.19	M-358	1.32
		M359	1.32

If you don't see it write for it

CERAMICON CONDENSERS
$7.50 per 100

3 mmf	±5%	60 mmf	±3%
5 mmf	±5%	67 mmf	±20%
4 mmf	±5 mmf	115 mmf	±2%
8.5 mmf	±5 mmf	120 mmf	±5%
11 mmf	±5%	240 mmf	±3%
15 mmf	±2.5 mmf	250 mmf	
50 mmf	±20%	1000 mmf	±5%

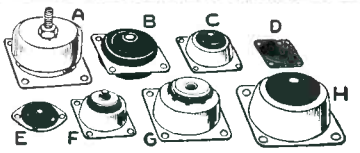
THERMISTORS

D-167332 (tube) ..... $.95
D-170396 (bead) ..... $.95
D-167613 (button) ..... $.95
D-166228 (button) ..... $.95
D-164699 for MTG. in "X" band Guide $2.50
D-167018 (tube) ..... $.95

WRITE FOR C.E.C. CATALOG NOW AVAILABLE **FREE**

VARISTORS

D-170225 ..... $1.25
D-167176 ..... $.95
D-168687 ..... $.95
D-171812 ..... $.95
D-171528 ..... $.95
D-168519 ..... $.95
D-162482 ..... $3.00
D-163298 ..... $1.25
D-99428 ..... $2.00
D-161871A $2.85
D-171121 ..... $.95
3A(12-43) $1.50
D-167020 ..... $3.00



SHOCK MOUNTS

D	Lord	#1	1 1/4x1 1/4x3/8H	10¢
D	Lord	#6	1 1/4x1 1/4x3/8H	10¢
D	Lord	#5	1 1/4x1 1/4x3/8H	10¢
B	Lord	#15	1 3/4x1 3/4x5/8H	15¢
B	Lord	#12	1 3/4x1 3/4x9/16H	15¢
B	Lord	#35	2 1/4x2 1/4x1"H	18¢
G	U. S.	#5150-C	2 3/8x2 3/8x1 1/8H	55¢
F	Lord	#4	1 23/32x1 23/32x1"H	35¢
C	Lord	#1	1 11/16x1 11/16x3/4"H	14¢
C	Lord	#10	2 3/8x2 3/8x1 1/16H	25¢
C	Lord	#8	2 3/8x2 3/8x1 1/16H	20¢
H	Lord	#35	3x3x1 1/2H	45¢
H	Lord	#20	3x3x1 5/8H	39¢
H	Lord	#25	3x3x1 5/8H	45¢
H	Henrite	#55	3x3x1 5/8H	49¢
H	Lord	#15	3x3x1 1/2H	35¢
H	Lord	#45	3x3x1 1/2H	49¢
A	Barry	#C2070	3x3x1 1/2H	55¢
A	Barry	#C2069	3x3x1 1/2H	55¢
A	Barry	#C2090H	3"x3"x1 1/2H	55¢

Shaft 6 1/8"Lx3/8" Dia Thread both sides with nuts, washer, and two woven leads ..... ea. 35¢

WRITE FOR TYPES NEEDED

30' U. S. ARMY SIGNAL CORPS RADIO MASTS

Complete set for the erection of a full flat top antenna. Of rugged plymold construction telescoping into 3 ten-foot sections for easy stowage and transportation. Supplied complete: 2 complete masts, hardware, shipping crate. Shipping wt. approx. 300 lbs. Sig Corps #2A289-223-A. New ..... $35.00 per set of 2

400 CYCLE TRANSFORMERS

352-7273: Pri: 115 v, 400 cy. Sec: 6.3 v, 2.5 amp; 6.3 v, .06 amp; 6.3 v, .9 amp; 5 v, 6 amp; 700 vct ... 2-5U4's. For APS-15, T201 ..... $4.75
352-7176: Pri: 115v, 400 cy. Sec: 6.3 v, 20 amp; 6.3 v, .5 amp; 6.3 v, .5 amp; 320 v (2-6X5's). For APS-15, T202 ..... $5.25
352-7278: Pri: 115 v, 400 cy. Sec: 2.5 v, 1.75 amp, 3500 v (2X2). For APS-15. T203, (Anode #2 5FP7) $5.85
352-7070: Pri: 118 v, 440 cy. Sec: 2.5 v, 2.5 amp; 2.5 v, 2.5 amp; (2000 v ins.): 6.3 v, 2.25 amp; 1200 v, tapped at 1000 and 750 v, p/o AN/APS 15 ..... $4.95
#7469105: Pri: 115 v, 400 cy. Sec: Tapped to give 742.5 v, 50 ma; 709 v, .0477 amp; 671 v, .045 amp $2.95
M-7474319: Pri: 115 v, 400 cy, Sec: 6.3 v, 2.7 amp; 6.3 v, 66 amp; 6.3 v, 21 amp $2.95
32332: Pri: 115 v, 400-2400 cy. Sec: 400 vct, 35 ma; 6.4 v, 2.5 amp; 6.4 v, .15 amp $2.25
332-7138M: Pri: 115 v, 400-2400 cy. Sec: 640 v, .5 ma; 2.5 v, 1.75 amp $3.85
352-7179: Pri: 115 v, 400-2400 cy. Sec: 6.5 v, 12 amp ct, 250 v, 100 ma; 5 v, 2 amp $3.50
#9069: Pri: 115/80 v, 400-2600 cy. Sec: 650 vct, 50 ma; 6.3 vct, 2 amp; 5 vct, 2 amp $2.15
352-7096: Pri: 115/80 v, 400-2400 cy. Sec: 2.5 v, 1.75 amp, 3 KV ins; 5 v, 3 amp; 6.5 v, 6.5 amp; 6.5 v, 1.2 amp $3.95
KS 9607: Pri: 115 v, 400-2400 cy. Sec: 734 vct, 177 ma, 1710 vct, 177 ma $5.95
D-166333: Pri: 115 v, 400-2400 cy. Sec: 6.3 v, 0.9 amp; 7.7 v, 0.365 amp $2.79
GE #7471957: Pri: 100/110/120/130 v, 400-2400 cy. Sec: 2.5 v, 20 amp, HV ins $4.85
D-163254: Pri: 115 v, 400 cy. Sec: 6.3 v, 12 amp; 6.3 v, 2 amp; 6.3 v, 1 amp. P/O AN/APQ-5 ..... $5.85
KS-9685: Pri: 115 v, 400-2400 cy. Sec: 6.4 vct, 7.5 amp; 6.4 v, 3.8 amp; 6.4 v, 2.5 amp $4.35
PLATE XFMR: Pri: 115 v, 400 cy. Sec: 9800 v, or 8600 v, @ 32 ma dc $12.50
#12033: Plate Xfmr. Pri: 115 v, 800 cy. Sec: 4550 vct, 250 ma $7.95

WRITE TO C.E.C. FOR YOUR 400 CYCLE NEEDS

TELEPHONE EQUIPMENT

Pike Pole. Telephone, MC123, for Wire Laying 2 sections, 4½ ft. ea. section w/M100 Lock. New Unused $5.95
Telephone Handset Shell. For TS10 Sound Power W.E. Light weight ..... 69¢
Tape Bridge TG8I5: McElroy used for standard ¾" White Paper, for Sight Reading and Typewriter transcription. SPECIAL PRICE $5.50

W.E. Teletype Switchboard #5. Complete Installation, 6-20 ft. bays. NEW EXPORT PACKED. AVAILABLE FOR INSPECTION.

BC 686 LINE AMPLIFIER

With magnet ringer, 3-tube 25L6 amplifier. For local point-to-point telephone operation, remote operation of Phone Xmtr, remote reception of receiver output, monitoring facility. Requires only 24 vdc for tube "B" plus supply for full operation.
New, less tubes, in wooden chest $18.50
Per pair for 2 way pt-to-pt operation $35.00

Silver-Mica Button Capacitors
(Standard Brand) $9.50 per 100

185 mmf ..... ±2.5 mmf
175 mmf ..... ±2.5 mmf
500 mmf ..... ±10%

COMMUNICATIONS EQUIPMENT COMPANY
CABLE ADDRESS: COMSUPO
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NEW YORK 7, N.Y.
C.E.C. MONEY BACK GUARANTEE, $3 MIN. ORDER.
F.O.B. N.Y.C. SEND MONEY ORDER OR CHECK, ONLY SHIPPING CHARGES SENT C.O.D.
RADAR TELEVISION ELECTRONICS
FM MICROWAVE RADIO SONAR

YOU'LL SAVE MANY DOLLARS WITH THIS FREE CATALOG

FREE WRITE FOR OUR CATALOG TODAY AND SAVE **FREE**

FILTER CHOKES

15-39NY/150MA	$3.25	8.5HY/125MA	$1.50
25HY/65MA	1.00	6HY/150MA	1.50
Dual 7HY, 75MA, 11HY/65MA			1.65
7HY 140MA	1.60	Dual 2HY/100MA	.75
Dual 2.5HY/130MA	1.25	.116HY/150MA	4.25
.01HY, 2.5A	1.45	.35HY 350MA	7.25
Dual .5HY, 380MA	1.00	5HY/40MA	.55
2HY 200MA	.75	Dual 120HY/17MA	2.45
30HY 20MA	.85	5HY 200MA	1.45
2.1HY 200MA	1.20	2 x 2.2HY .55A	9.95
25HY, 75MA	1.10	20HY/300MA	12.95
Dual .22HY/600MA	.44HY/400MA		1.95
Swing 1-3HY/225	.02A, 1.75HY/225MA		2.25
Tapped Choke 2 x 1.52HY/167MA			2.25
.033HY, 7A	9.50	Dual 10HY/150MA	3.50
Dual 1.52HY/167MA	2.49	Dual 2.2HY/550MA	5.95
5HY 200MA	1.49	1.35HY/1.1A	4.95
12HY 100MA	1.75	11HY/100MA	.60
2x2.5HY 700MA	6.95	Send For	
3.5HY/400MA	5.95	Lists of Others	

POWER EQUIPMENT

- Fil. Trans. 110v 60 cy in., 5vct/30A out.... $9.95
- In 110v 60 cy out 6.3vct/20A, 6.3v/1.8A, 6.3v/600 MA.... $4.95
- In 110v 60 cy out 2x5vct/6.75A, 5vct/13.5A, 3500 Test.... $6.95
- In 110v 60 cy out 10vct/13A, 10vct/6.5A, 6.3vct/2A.... $7.95
- In 115v 60 cy out 760vct/500MA, 800vct/40MA.... $10.95
- In 110v 60 cy out 690vct/400MA.... $6.95
- Tapped in. 107 to 127v out 160v to 200v/700MA 12 Taps.... $12.95
- In 110v 60 cy out 4v/16A, 2.5v/1.75A.... $4.75
- In 110v 60 cy out 17000v/144MA, w/choke 26" x 29"x13" oil immersed.... $65.00
- In 115v 60 cy out 2x5v/5.5A 29kv ins.... $24.50
- In 115v 60 cy out Tapped to give 2750/2470/2240/@ 750 MA 7000v ins.... $34.50

SPECIAL TRANSFORMERS

- In 440/220/110v 60 cy 3kva out 115v 25kv ins. 12"x12"x7".... $40.00
- In 220v 60 cy .05kva out 5vct 34kv Test.... $24.50
- In 115v/230v 50-60 cy out 21000v 100MA.... $120.00
- In 220v 60 cy out 220v/360MA, 3x2.5v/5A, 2.5v/15A.... $6.75
- In 220v 60 cy out 10vct/13A, 7.5vct/2.5A.... $5.25
- In 220v/440v 60 cy out 123vct/2.85A.... $7.50
- In 240v 60 cy 7000vct/900MA, 4700vct/750 MA.... $135.00
- In 210/15/20/25/30/35/240v 60 cy out 11vct/35A, 10vct/35A, 7.5vct/35A, 5vct/35A.... $37.50
- In 220/440 60 cy 1 ph out 123vct 2.85 amp Test 1780.... $6.95
- In 230/460 out 7320vct/6.55A, 660vct/2A.... ——

TRANSTAT AMERTRAN

Input: 0.115 v. 50-60 cycle. Max. **output:** 115 v. 100 amp.

All units are new, guaranteed $95

2 KVA: 90-130v input 50-60 cycles, output 115v 2kva type RH Amertran $29.95 each

KITS POWER SUPPLY

Basic TV 5" & 7" Pwr Supply

Consists of xfrmr 2300v/4MA, 2.5v /2A, 1 condenser .1.1 mfd 7500v Pvr., 2x2 tube, socket 100K ohm resistor price $9.95

5BP1..$1.95 **5BP4**..$4.95 **5CP1**..$3.75

Basic TV 3" & 5" Pwr Supply

Consists of xfrmr 1080v/55MA, 2x6.3v/1.2A, 1 Cond. .1.1 mfd 7500v Pvr., 2x2 tube, socket 100 K ohm resistor. Price $7.95

3BP1..$2.25 **3DP1**..$2.25 **3EP1**..$2.95

3" Oscilloscope Kit

BC929 uses 9 tubes 3BP1, 6SN7, 6H6, 6B6G, 6X5 2X2 (now 400 cy) easily converted to 115v 60 cy New Complete w tubes & conver. inst $22.50

5" Oscilloscope Kit

BC 704 Less Pwr Supply Kit includes 8 tubes, 5BP1, 6AC7, 6116 w/wooden Case & Diag....$29.50

COMMUNICATIONS EQUIPMENT COMPANY *for your needs*

932 PHOTOTUBE

This tube is a gas phototube having 5-1 response, particularly sensitive to red and near infrared radiation. Can be used with incandescent light source. Send for data.

PRICE.... $1.00

GREAT TUBE VALUES

01-A	$ .45	12SR7	$ .72	804	$9.95
1B26	4.85	15P	1.40	815	2.50
2C21	.69	28D7	.75	836	1.15
2C22	.69	30 (Spec.)	.70	837	1.95
2J21-A	25.00	45 (Spec.)	.59	843	.59
2J22	25.00	39/44	.49	860	15.00
2J26	25.00	35/51	.72	861	40.00
2J27	25.00	227A	3.85	874	1.95
2J31	25.00	225	8.80	876	4.95
2J32	25.00	268-A	20.00	1005	.35
2J38	35.00	355-A	19.50	1619	.21
2J39	35.00	417A	25.00	1624	.85
2J34	55.00	530	90.00	1629	.35
2J40	65.00	531	45.00	1961	5.00
2J49	85.00	532	3.95	9002	.65
3J31	55.00	559	4.00	9004	.47
2K41	65.00	562	90.00	CEQ 72	1.95
2X2/879	.69	615	.89	EF 50	.79
3BP1	2.25	700A,B,C,D	50.00	F-127	20.00
2CP24	.60	703-A	7.00	FC 258A	165.00
3C30	.70	704-A	.75	GL 532	7.50
3D6	.79	705-A	2.85	FC 271	40.00
3CP1	3.50	706AY,BY, DY	50.00	GL 562	75.00
3D21-A	1.50	706EY,FY, GY	50.00	GL 623	75.00
3DP1	2.25			GL 697	75.00
3EP1	2.95			ML 100	60.00
3FP7	1.20	707-B	20.00	QK 59	65.00
3Q5	.79	714AY	25.00	QK 60	65.00
5BP1	1.95	715-B	12.00	QK 61	65.00
5BP4	4.95	720BY	50.00	QK 62	65.00
5CP1	3.75	720CY	50.00	VR 91	1.00
5FP7	3.50	721-A	3.60	VR 130	1.25
5J30	39.50	723-A/B	12.50	VR 135	1.25
6G	2.00	724B	1.75	VR 137	1.25
6SC7	.70	725-A	25.00	VU 120	1.00
7C4	1.00	726-A	15.00	VU 134	1.00
7E5	1.00	728AY,BY, CY,DY,EY, FY,GY	50.00	WL 532	4.75
7E6	.72			WN 150	3.00
10Y	.60			WT 260	5.00
12A6	.35	730A	25.00		
12K8Y	.65	800	2.25	†With cavity.	
12SF7	.49	801-A	1.10	Cavity only 5.00	

Socket 715B, 705A.... $1.00

Socket Klystron 723A/B.... 2 for $1.00

Time Delay Relay Vacuum, Time Delay 30 sec. 117v 60 cy Metal Tube, 4 Prong, Edison.... $2.25

Grid Cap H.V. Bakelite ¾" w/wire lead 10 for $1.00

Tube Clamps. Bircher 926-A-B-B5-C-A2-B1 etc. 10 for $1.10

Thermostatic Switch N.C. 3 amp contacts opens 75° 7 For $1.00

Fuses 250v indicators amps 1, 2, 3, 4, 5, 6 @ 22¢ 5 for $1.00

Fuses 1000v amps ¼, ⅜, 1, 1½, @ 18¢....5 for 75c

Fuses 2500-3000v amps ¼, ¾, 1, 1½, 20¢....5 for 90c

RF Indicator contains neon bulb, 20¢.....5 for 90¢

TRANSFORMERS

115V 60cy. INPUT

Equip. Conservatively Rated

FILAMENT TRANSFORMERS

5 Volts/6 Amp	$2.25
F083; 6.3VCT/6A, 5V/2A	1.85
F- 2.5VCT/6.5A	3.25
F- 6.3VCT/2A, 6.3VCT/2A	2.45
F087; 6.3VCT/1A, 6.3VCT/7A	2.75
F103; 6.3V/1A, 6.3V/1A	1.95
F123; 6.3VCT/5A, 6.3V/1A	2.25
F127; 6.3VCT/3.2A, 6.3VCT/1A	2.25
F674; 8V/1.5A	2.75
F- 2.5/1.75A, 6.5/8A, 5V/3A, 6.5/.6A	3.95
F414; 2 x 2.5VCT/6.5A	3.25
F161; 6.3VCT/7A, 6.3VCT/5A, 5VCT/6A 2 x 6.3V/.6A, 6.3V/.3A	3.95
F829; 6V/2.5A	1.75
F38A; 6.3V/2.5A, 2 x 2.5V/7A	3.25
F112; 2 x 2.5VCT/6.5A, 2.5V/6.5A	4.25
F14A 6.3/6A	1.95

PLATE TRANSFORMERS

P410; 800VCT/40MA, 760VCT/500MA	6.50
P415; 690V/450MA	4.95
P699; 2 x 300VCT/150MA	2.25
P403; 70V/1A	2.25
P413; 510VCT/150MA, 650VCT/15MA	4.95
P842; 600VCT/.0166A, 250VCT/.077A	2.95
P885; 1620VCT/400MA HV INS	11.95
P894; 2 x 200V/350MA, 2 x 20V/.01A	1.95
P450; 2 x 150V/940MA	4.50
P371; 246VCT/830MA	3.95
P345; 1470VCT/1.2A, 3500T	24.00

COMBINATION TRANSFORMERS

C965; 78V/600MA, 6.3V/2A	$3.95
C111; 2 x 300V/42MA, 55V/125MA 45V/3.5 Amp	3.95
C608; 880VCT/150MA, 5V/3A, 6.3V/6.25A	5.00
C931; 585VCT/86MA, 5V/3A, 6.3V/6A	3.95
C055; 525VCT/75MA, 5V/2A, 6.3V/1.8A 10V/2A	4.45
T102; 1080VCT/55MA, 2 x 6.3V/2A	5.95
C848; 600VCT/155MA, 6.3VCT/5A 5VCT/3A HV Ins	3.95
C899; 2 x 110VCT/.01A, 6.3V/1A 2.5VCT/7A	4.50
C760; 6.3VCT/10A, 65V/1A, 100VCT/.1A 40V/.1A, 18VCT/.1A, 18V-6V/.1A, 6.3V/.1A	5.50
C354; 825VCT/190MA, 5VCT/3A	3.95
C367; 5VCT/3A, 580VCT/.040A	2.95
T160; 1120VCT/770MA, 590VCT/.082A HV Ins	12.75
C579; 24V/900MA, 770V/.0025, 2.5V/3A HV Ins	4.25
T378; 2300V/.004A, 2.5V/2A HV Ins	8.95
C375; 1120VCT/600MA, 2 x 5VCT/6-2A 6.3VCT/3A, 6.3V/300MA	14.95
C364; 6.3VCT/3A, 5VCT/6A, 610VCT/ 330MA	4.75
C434; 40V/.01A, 6.3V/1.25A	1.95
C383; 215VCT/300MA, 5VCT/6A	2.29
C360; 640VCT/.080A, 5VCT/3A, 6.3VCT/ 3.2A	3.95
C821; 1500V/.4A, 6.3V/.6A, 2.5V/1.75A, 3500T	8.95

CONDENSERS

MICA

Mfd	Voltage		Price
.01	1200WVDC	2 for	95¢
.00025	2500TVDC	2 for	55¢
.00004	2500WVDC	2 for	75¢
.000047	2500WVDC	2 for	75¢
.01	500WVDC	4 for	95¢
.002	3000WVDC	2 for	$2.00
.01	2000WVDC	2 for	2.90
.00003	2000WVDC	2 for	95¢
.00009	3000WVDC	2 for	1.45
.00082	3000WVDC	2 for	1.95
.002	3000WVDC	2 for	1.95
.005	5000WVDC	2 for	3.25
.0004	6000WVDC	2 for	2.95
.0006	3000WVDC	2 for	1.95
.0008	3000WVDC	2 for	1.85
.0016	3000WVDC	2 for	1.25
.000090	3000WVDC	2 for	75¢
.05	1500WVDC	2 for	19.50
.03	2000WVDC	2 for	23.50
.045	2000WVDC	2 for	23.50
.00015	20KVDC	2 for	47.50
.0001	20KVDC	2 for	47.50
.002	15KVDC	2 for	37.50
.006	2500WVDC	2 for	2.85
.00027	2500WVDC	2 for	65¢

Send for Lists of Others

UPRIGHT OILS

Mfd	Voltage	Terminals		Price
.1	600VDC	2	3 for	$1.00
.25	400VDC	2	3 for	1.10
.5	600VDC	2	3 for	1.00
.1	600VDC	2	3 for	1.10
2 x .5	600VDC	3	3 for	1.45
3 x .1	600VDC	3	2 for	1.05
.25	400VDC	2	3 for	1.10
.5	600VDC	2	3 for	1.00
.5	600VDC	2	3 for	1.00
.1	400VDC	2	3 for	1.00
.1	400VDC	2	2 for	75¢
.4	600VDC	2	3 for	1.10
.1	600VDC	2	2 for	83¢
2 x .1	600VDC	2	2 for	95¢
1.75	400VDC	2	3 for	1.00
3 x .1	600VDC	3	2 for	1.05
2 x .5	600VDC	3	2 for	95¢
.1	600VDC	2	2 for	85¢
.1	600VDC	2	2 for	85¢
.1	500VDC	2	2 for	85¢
.1	500VDC	2	2 for	85¢
.1	600VDC	2	2 for	85¢

OIL CONDENSERS

.0016 MFD	15000 VDC	$8.00
.015 MFD	16000 VDC	7.00
.01-.005-.005 MFD	10000 VDC	4.75
.1 MFD	2500 VDC	1.25
.1-.1 MFD	7000 VDC	3.49
.1 MFD	6000 VDC	2.97
.1 MFD	7500 VDC	3.00
2 x .1 MFD	4800 VDC	3.00
.15 MFD	4000 VDC	3.00
.15-.15 MFD	6000 VDC	4.00
2 x .15 MFD	8000 VDC	5.00
.25 MFD	1500 VDC	1.05
.4 MFD	5000 VDC	3.00
.5 MFD	1000 VDC	.70
.5 MFD	750 VAC	1.75
1 MFD	600 VDC	.49
1 MFD	2000 VDC	1.00
1 MFD	1500 VDC	.89
1.5 MFD	1500 VDC	.95
2 MFD	1500 VDC	1.05
4 MFD	1000 VDC	.98
6 MFD	600 VDC	1.05
6 MFD	1500 VDC	2.25
7 MFD	600 VDC	1.05
7 MFD	800 VDC	1.25
10 MFD	1000 VDC	1.95
15 MFD	220 VAC	2.29
15 MFD	1000 VDC	2.25

H. V. OIL CONDENSERS

1.5 MFD	6000 VDC	10.00
1 MFD	15000 VDC	32.50
.5 MFD	25000 VDC	37.50
.1 MFD	25000 VDC	85.00
.1 MFD	10000 VDC	15.00
.06 MFD	15000 VDC	8.00
.25 MFD	20000 VDC	17.50

★ ★ ★ SPECIALS ★ ★ ★

2500 MFD	3VDC	2 For 70¢
2000 MFD	25VDC	$1.15
100 MFD	50VDC	4 For 1.00
400 MFD	6 VDC	5 For 1.00
50 MFD	12VDC	5 For 1.00
10 MFD	25VDC	10 For 1.00
3 x 20 MFD	25WV	4 For 1.00
25 MFD	25VDC	10 For 1.45
30MFD	50VDC	5 For 1.10

Write For Lists of Many Others in Stock

T 311 3000v/5MA, 720vct/200MA 6.4v/8.7A, 6.4v/.6A, 5v/3A, 1.25v/.3A Scoop $6.95

T-482 10000v 5MA for 10" x 15".... $10.95

PRECISION RESISTORS

1.01	125	1450	20000
3	128	1900	25000
5	150	2230	30000
5.05	200	4300	33000
10	250	5000	35000
10.1	300	7000	40000
18	430	7500	50000
43.5	468	8500	55000
50	800	10000	57000
75	920	12000	75000
82	1000	17000	Ship type
120	1100	17300	In stock

Above Ea...30¢ Ten For..$2.50

100000	150000	200000	250000
120000	170000	220000	500000

Above Ea...40¢ Ten For..$3.50

1,000,000 ohms.....Each 75¢

MISCELLANEOUS

15 Watt Power Supply

Consists of xfrmr 600vct/155MA, 6.3v/5A, 5v/3A. 2-7mfd 600v, dual 10 hy 200MA choke, 1-ST4, 1-socket. Price.... $8.95

50 Watt Power Supply

Consists of xfrmr 880vct/150MA, 5v/3A, 6.3v/6.25A, 2-7 mfd 800v, 1-5T4. socket. Price.....$10.95

Filter Line GE 100amp w/2x5 mfd 50v 0.1 Cond. operates on 110vdc $1.98

Filter Line 1kw. Clean up your BCI & TVI. Easy to mount, uses 4-.002 Cond. Complete.....$4.25

Deflection Yoke for 5" to 12" tube RAY20A.... $4.49

COMMUNICATIONS EQUIPMENT COMPANY

CABLE ADDRESS: COMSUPO
PHONE DIGBY 9-4124
131 LIBERTY ST. DEP'T. E
NEW YORK 7, N.Y.

RADAR TELEVISION ELECTRONICS FM MICROWAVE RADIO SONAR

C.E.C. MONEY BACK GUARANTEE, $3 MIN. ORDER.
F.O.B. N.Y.C. SEND MONEY ORDER OR CHECK, ONLY SHIPPING CHARGES SENT C.O.D.

SPECIAL SURPLUS BROADCAST OF OUR SUPER SPECIALS!!!

I. F. F. TRANSMITTER ASB-7A

Uses 2 transmitting UHF tubes, 15E and contains 400 cycle blower unit, etc. Freq. range 500 MCS. 18x8x7½ New $12.95

SPERRY A-5 VERTICAL GYRO UNIT

#644841. 115 V. 400 CY 3 phase. Contains gyro assembly, erection motor, erection relay assembly, pick-off assembly, elevator and aileron limit switches, and roll axes. 15 x 12 x 9. New. $27.50

G.E. MOTOR CONTROLLED VOLTAGE REGULATOR

Cat. #837625, Type 'Airs', Form M, .568 KVA, cont. duty, 60 cy., primary volts 115, Load Amps 16.2. Indoor service. Voltage controlled by mtr. 120/1/60.1/40 HP..$39.50

Outdoor Distribution Transformers OIL FILLED—BRAND NEW

General Electric 3 KVA; Type HS; 3000/5200Y - 115/230 volts. Style 3266596-GI.
In original Factory Cases **$36**

Westinghouse Type S. 2400/4160 Y—120/240 volts. 3 KVA **$50.00**

1½ KVA **$37.50**

G. E. Motor Starting Reactors

Type 11K2840G2

Rated at 440 Volts, 3 Ph., 60 Cy., 16.8 Amp. 15-20 HP. Waterproof steel case. 17" x 15" x 10". New in orig. cases.

Special of the month

$7.75

DICTOGRAPH INTER-COMMUNICATION SETS

Designed to bring to homes and offices the conv. of two-way convers. w/o the use of telephone, household elec. current, or radio. Efficient to 800 ft. off flashlight batteries. New Pair.....$9.95

SPERRY A-5 AMPLIFIER RACK

#644890, contains Weston Model 833 Voltmeter 0-130 and Weston Model 637 Frequency Meter 350-450 cycles. Several 24 VDC relays, transformers and condensers. New $12.95

Blower Assembly MX-215/APG

John Oster C-2P-1L 28 v. DC 7000 RPM 1/100 hp. #2. L-R Blower. 25 C.F.M.....Price $2.75

John Oster, 6 Volt, DC Motor

1.8 Amps—5000 R.P.M. #1½ L-R Blower 5.0 C.F.M. .....Price $4.50

Westinghouse Type FL Blower

115 V. 400 Cy. 6700 RPM. 2" Sirrocco Impeller 17 C.F.M. .....Price $4.50

F. A. Smith AC Blower

115 V. 60 Cy. 0.38 A 3250 RPM. Outlet 1¼" Diameter Motor fan cooled. 25 C.F.M.....Price $7.95

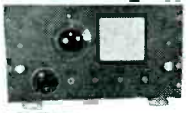
D. C. 604 F. M. TRANSMITTER

Wide or narrow band FM. 30 watt power output. Excellent possibility for ten or eleven meter exciter. Freq. 20-27.9 MC. Working space permits modification. W/ tubes but less power supply and xtls. LN $11.50. Complete with Crystals $27.50

New Submarine Signal QBE-1 Underwater Sound Equipment

CBM 52265 Driver Rectifier

Emission A1. Freq. 18-25 KC, 30W output. 110V. 60 Cy. 1 ph supply 19x13x 10 .....Price $32.50



Type CBM 46169. Receiver amplifier. Freq. 18-25KC., input 115/1/60. 75 lbs. 19 x 13 x 10½....$26.50

Type CBM 55081 Indicator Unit — Ranges 0-1000 yds. and 0-5000 yds., Visual & Audio Indication Synchronous motor driven, input 115/1/60. 20 x 16 x 8½.....$25.00

DELCO CONSTANT SPEED MOTOR

Type A-7155, 27 VDC, 2.4 A 1/30 HP, 3600 RPM. 2½" Diam. x 5½ L. ⅞" Sh. Ext. Cont. Duty. Base mounted...$4.25 ea.

SELECTOR SWITCHES

Heavy duty, U. S. N. Control any type of multi-circuit devices. Removable contacts enabling any comb. of closed and open circuit. The following available: 5 section-10 pole or 10 section-20 pole, $1.50 ea. Case lots of (8) $8.00 or (5) cases, special....$32.50

INDUCTION VOLTAGE REGULATOR

Type IRT, form M, 1.64 KVA, 3 phase, 60 cycles, cont. duty. Outdoor service. Primary: 208 V., 10.5 load amps. Oil-filled. Wgt. 365 lbs. 33 x 17" x 14".....$53.50

FITCH CRYSTAL DUPLICATOR

Calibrates crystal plate of unknown freq. against standard plate of desired freq. Consists of standard and test oscillators whose outputs are mixed to produce an amplified beat note; the freq. is shown on 500, 5000, 50,000 cycle meter. Metal cabinet w/hinged cover. 9" H. x 13" W. x 19" L. Comp. w/4" sq. activity and freq. meter.....$22.50

DYNAMOTOR GENERATOR

Model 3975-1. Electric Sprayit Co., p/of "Gibson Girl". Input 28 VDC @ .175 amps. Output 300 VDC @ .040 amps. 5" L. 3¼" D. .....$1.00 ea.

RCA TRACK LIGHTING & CONTROL PANEL

Model 713-AS, comp. wire ready for immed. oper. Controls the filament volt. on vacuum tubes in the process of being exhausted on rotary turn table equip. 7" H, 15" D, 32" W. Units complete with meters, variac dist. transformers, switches, rheostats, etc. $275.00

RETARD CHOKE COILS

Amertran, Disc Type. Line voltage 15,000; ripple freq. 120. Oil-filled; .020A DC @ 900H @ 48% ripple. 52A DC @ 25H @ 48% ripple. 17"x17"x22" w/term. 10" above case. 40°C temp. rise.....$34.00

MILLIAMMETERS

150-0-150 MA DC. Accuracy ½ of 1%. Scale length 4⅛", Wt. 3½ lbs. 6" x 2½" x 4⅛". L. N. $2.50

MINE DETECTOR SCR 625

Detects metallic objects (ferrous or non-ferrous) to a depth of approx. 6 ft. Find outboard motors on the bottom of lakes, locate underground piping, treasure, metallic fragments in lumber, etc. New, complete with inst. book, $65.00. Used but like new.....$45.00

SPECIAL of MONTH

W.E. Motor KS-5603-L02, 28 v. DC. 0.6 amps. 1/100 hp. 4 lead shunt.

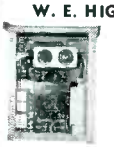
Price $1.50 ea.

TRANSTAT VOLTAGE REGULATOR

Amertran type RH. Input: 115 V. 400 cy. 0.5 KVA, 5.5 max. amps. Output: 92-115 V. 5½x4½x3¼. $1.95

.25 KVA Fixed winding 115/1/60. Commutator range 103-126 V. 2.17 Max Amps.....$9.45

W. E. HIGH VOLTAGE POWER SUPPLY



RA50-A, used with SCR 296A. Secondary of hi voltage trans. supplies 20,000 volts @ 45 MILS to two 705A'S; the filaments are heated from 5 V. 10 A. trans. Also 0.05 mfd 12,500 V. cond. 21½ x 17 x 11½.....$49.95

AMERTRAN HEAVY DUTY TRANSFORMERS

Pri.: 115/230 VAC 60 cy. Sec.: 4730/2365 V. 1.66KVA. RMS. 12 KV. Wgt. 150#. 11"x11"x9", 700 Ma. New $27.50

Standard Brand RHEOSTATS

High shock rheostats, four 13" plates, 100 ohms 8-2A, 175-345 V connected in series. Assembled for back of board mtg. or by reversing the supporting brackets for floor or table oper. New $19.75

DECK ENTRANCE INSULATORS (Bowl and Flange Type)

Mfd. by Ohio Brass Co. heavy galv. metal flange 10½" D., porc. bowl set in rubber gaskets. Top bell 7¾" D. brass feed thru rod 10½" L. Insul. dist. between top bell and flange 6½". $2.50

DAVEN SOUND ATTENUATORS

Type 350-A, Network, ladder, linear, imped. 30/30 ohms. 2DB attenuation. 10 W dissipation. Brand new.....$3.95

DC SERVO MOTORS

White Rodgers Elec. Co. (6905X-46). 24 VDC @ .65 Amps. Torque 50 in/lbs. ½ RPM reversible, comp. w/limit switch, relays and selenium rectifiers on top of motor, to keep AC out of motor. 5x5x4. $7.95

6904X-27, 24 VDC @ 1 Amp., 150 in/lbs. torque. 2½" RPM reversible. Complete w/limit switch, relays and selenium rectifiers same as above.....$7.95

TUBE SPECIALS THIS MONTH ONLY

C1B/3C31	$2.00	12SK7GT	$ .58
1R4/1294	.80	12SR7	.45
2A3	.92	28D7	.30
2C22	.20	39/44	.20
2E22	1.10	53	1.00
2X2/879	.60	OB3/VR90	.65
3B24	1.75	OD3/VR150	.65
4B24	3.75	250R	5.00
4B26	4.50	274B	1.20
5AP1	3.95	304TH	5.75
5BP1	2.50	304TL	1.50
5CP1	3.50	371A	1.25
5FP7	1.00	WL417A	9.00
6AG5	.90	WL481	2.00
6AK5	1.00	WL531	1.75
6AK6	.90	705A	1.85
6H4G	1.20	708A	2.00
6H6G	.85	714AY	5.00
6H16	.50	721A	2.00
6J5GT	.50	723A/B	9.50
6L6	1.10	724A	4.00
6L7S	1.00	801A	.49
6SA7GT	.50	874	1.50
6SC7/1655	.70	1616	1.20
6SG7	.75	1622	1.70
6SH7	.40	1625	.39
6SJ7Y	.62	1626	.45
6SN7GT	.65	1629	.20
10Y	.50	2050	.95
12SC7	.65	GL8020	3.50
12SH7	.39		

ESD ELECTRO Sales Co.

110 PEARL ST., Dept. E6, Boston 10, Mass. . . . Liberty 2-5589 . . . HAncock 6-5069

Finest of Surplus PEAK ELECTRONICS CO. Fraction of Cost

H.V.-H. CURRENT PLATE TRANS.

1500-0-1500 volts at 1.5 amps. Tapped at 1350 and 1250, Pri. 110/220 volts 50/60 cycles in 2 Separate windings. Built to rigid Navy specs by Amertran. Suitable for broadcast transmitters, induction heating, etc. Continuous duty. 10 x 10 x 7. swt 125 lbs.

New only 39.50

BARGAIN OF THE MONTH

As illustrated above. 1500-8-1500 volts at 600 ma. Pri. 110/220 v. 50/60 cycles. 8 x 8½ x 7 s.w.t. 78 lbs. Made by Amertran. Only.....19.95

HIGH CURRENT TRANSF. 820 Volts CT at 775 Ma. Pri. 110/220 Volts 60 cycles. Fully Cased 6.95

MALLORY VIBROPACK

6.3 Volt input—output 300 Volt @ 100 ma. Complete only .....each $8.95

MALLORY TRANSFORMER & 534C Vibrator as used in above. Both for.....$5.95

UTC type PA 5000 ohm plate to 500 ohm line and 6 ohm voice coil. 10 watts. 60 to 10,000 cps +1 DB. GREAT VALUE.....ea. $2.75

THORDARSON PLATE TRANSF. 2370 volts CT at 250 MA tapped at 300-0-300 volts, plus 215 volts 55 MA bias winding. 110 volt 60 cy. pri. Fully shielded .....ea. $11.95

GENERAL PURPOSE TRANSFORMERS

Ideal for Bias, Filament, Isolation, Stepdown, etc. 2 isolated 110v pr. sec. 110v at 900 ma plus 6.3 @ 2 amps. Fully cased.....Now $1.49 ea.

SCOPE TRANSFORMERS

Pri 110V 60Cy — Hermetically Sealed

2500V @ 12Ma.....$3.95
2300 @ 4Ma, 2.5 Volts @ 2 Amp.....4.95
1050V @ 20Ma, 20V 4.5A, 2.5V 5A.....4.75
4500V @ 4 Ma.....8.50

SOLA CONSTANT VOLTAGE TRANS.

Pri. 95-125 Volts 60 Cy See 115V, 120VA.....17.95

PLATE AND FIL. TRANSF. PRI 110v 60 cy. sec. 1120 volts CT @ 600 ma. 6.3v CT # 3A, 2x5VCT @ 6A Hermetically sealed.....$9.95 ea.

1500, 5000 Ohm 100 Watt Ferrule Resistors. 20,000 Ohm 50 Watt Ferrule Resistors. Any Types only .10 ea. Min. order 50.

HS 30 HEADPHONES

250 ohms imp. Can be used for sound power Telephones.

Brand new ..... .69 ea.

LARGE QUANTITY AVAILABLE

STEPDOWN TRANSFORMER

220/110 volts, 100 watts. Fully encased, 5⅛ x 4¼ x 5⅛. 110V 60 cycle.....$2.49 each

PHASE SHIFT CAPACITOR

4 Stator Single Rotor. 0-360 Degrees Rotation .....Only $2.95 each

ODDS AND ENDS BARGAINS

.004 4000 VDC Micas .....9 for .99
.01 600 VDC Mica Cond.....9 for .99
GE 24V DC Relays .....5 for .99
.02 400 V DC Tubulars.....15 for .99
1000 MFD 25 Volt Electrolytic.....2 for .99
25 MFD 25 Volt Elect. Tubular.....6 for .99
JAN 6CX Tubes, New, Boxed.....4 for .99
3:1 PP Input, Hermetic Seal.....2 for .99
.05 600 VDC Oil Tubular.....10 for .99
10 MMF Midget Variable Cond.....4 for .99
Heineman 5 Amp 110 VAC CKT Breaker..... .99
Heineman 25 Amp 110 VAC CKT Breaker..... 1.49
2 MFD 250 VAC Oil Cond.....5 for .99
Solar .02 600 VDC Dominoes.....9 for .99
Erie .0005 N750D Ceramicons.....15 for .99
.1x.1 2 KV DC Oil-Condenser..... .79
H&H SPST P.B. Switch N.O.....5 for .99
Weston 507 RF Meters, Less Thermo..... .99
1/48 Amp (25 Ma) Littlefuses.....15 for .99
.25 MFD 600 V. Tubulars.....6 for .99
C-D 1 MFD 400 V Oil Tubulars.....9 for .99
Butterfly Cond 2-11 MMF Ball Bearings...2 for .99
50 MFD 50 Volt Elect. Tubulars .....5 for .99
.0015 5% Silver Micas.....9 for .99
Midget Closed CKT Jacks.....7 for .99
CD Type 4 .001 600 VDC Micas.....50 for 4.99

SELSYN MOTORS

115 volts 60 cycles. Large size, high torque. Made by Diehl and Bendix. Ideal for rotating TV beam, etc. Great value at $6.75 per pair.

PANEL METERS—BRAND NEW

2" WESTON .0-1 Ma Dc 26 ohms res.....$3.50
2" GE 0-1 Ma DC (volt scale)..... 2.95
2" GE 0-5 Ma DC (amp scale)..... 1.95
2" WESTINGHOUSE 0-10 Ma DC..... 2.45
2" GE 0-500 Ma DC..... 1.95
2" GE 0-10 Volts AC..... 2.50
2" GE 0-30 Volts DC 1000Ω/v..... 2.50
2" WESTON 0-250 Volts DC..... 2.50
2" WESTON 150-0-150 Microamps DC..... 3.49
2" GE 0-30 Amps DC..... 2.45
2" GE 0-1 Amp RF (Internal Thermo)..... 2.45
2" WESTON 0-1 Amps RF (Internal Thermo).. 2.50
3" McCLINTOCK 0-1 Ma DC. (MA Scale)..... 3.95
3" WESTINGHOUSE 0-2 Ma DC..... 3.95
3" GE 0-15 Ma DC (Square Case)..... 3.95
3" WESTERN ELECTRIC 0-80 Ma DC..... 2.95
3" DEJUR 0-100 Ma DC..... 2.95
3" GE 0-200 Ma DC..... 3.95
3" WESTINGHOUSE 0-50 Amps AC..... 3.95
3" WESTON 0-50 Amps AC..... 4.95
3" TRIPLETT 0.75 Amps AC..... 2.95
3" WESTINGHOUSE 0-20 Ma DC..... 3.95
3" WESTINGHOUSE 0-150 Volts AC..... 3.95

2" GE 0-200 MICROAMPS

Model DW51 .....$4.50 ea.

FILAMENT TRANSFORMERS

110V 60Cy Pri. Fully Cased.
5 Volt 15 Amp.....$2.75
2.5 Volt 10 Amp..... 3.49
2.5 Volt CT 21 Amp..... 4.75
6.3 Volt 10 Amp..... 1.89

MULTIPLE SECONDARIES

5¼V CT 21A, 7.5V 6A, 7.5V 6A.....$4.95
6.3V 21 Amp, 6.3V 2A, 2.5V 2A..... 3.95
5 Volt 4A, 6.3V, 3A..... 2.45
2.5V CT 20A, 2.5V CT 20A..... 6.95
2.5V CT 10A, 10V 3A, 5V 3A, 5V 3A..... 3.95

CHOKE BARGAINS

6 Henry 50 ma 300 ohms .....3 for $0.99
6 Henry 80 ma 220 ohms .....2 for .99
8 Henry 160 ma 140 ohms..... .99
1.5 Henry 250 ma 72 ohms..... .59
6 Henry 300 ma 65 ohms..... 3.75
4.3 Henry 620 ma 42 ohms..... 6.95
Swing. Choke 1.6/12 Henry 1 Amp/100 ma 15 ohm 19.95

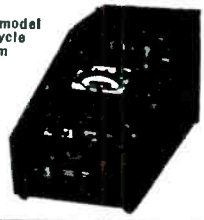
U. H. F. COAX. CONNECTORS

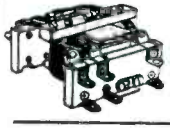
83IAP-UG12U—UG21U-UG-14U-83I R-83ISP .39 ea.

FEDERAL ANTI-CAPACITY SWITCH. Double Pole. Double Throw.....85¢ each; 10 for $7.50

MEGOHM METER

Industrial Instruments model L2AU 110/220 volts 60 cycle input. Direct reading from 0-100000 megohms on 4" meter can be extended to 500000 megohms with external supply. Sloping hardwood Cabinet 15"x8"x10". Brand new with tubes plus running spare parts including extra tubes. Great value Only $69.50.





ADVANCE D.P.D.T. ANTENNA RELAY

110 V. 60 cycle coil Steatite Insulation. Only $1.95 each.

DUNCO RELAY 6 volt 60 cycle coil DPST....$1.39

WIRE WOUND RESISTORS

5 Watt type AA, 20-25-50-200-470-2500-4000 ohms ..... .09 ea.
10 watt type AB, 25-40-84-400-470-1325-1900-2000-4000 ohms ..... .15 ea.
20 watt type DG, 50-70-100-150-300-750 1000-1500-2500-2700-5000-7500 10000-16000-20000-30000 ohms ..... .20 ea.

30 WATT WIRE WOUND RESISTORS

Ohms: 100-150-1500-2500-3k-4k-4500-5k-5300-10k-15k-18k-40k ..... .15 ea. 8 for .99

ADJUSTABLE RESISTORS

20 Watt: 1, 5, 50 Ohms..... .25
50 Watt: 80, 100, 500 Ohms..... .35
75 Watt: 40, 80, 100, 150, 200 Ohms..... .39
100 Watt: 20, 50, 75, 120, 180 Ohms..... .49
150 Watt: 50, 100 Ohms..... .59

1% PRECISION RESISTORS

2000-2500-5000-8500-10,000 ohms .....ea. .25
50000-95000 ohms .....ea. .29
10000-750000-1 meg .....ea. .69

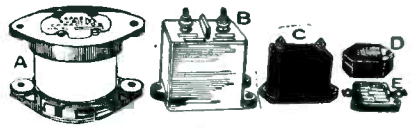
Precision 15 Meg. 1% Accuracy Resistor. Non-inductive, 1 watt, hermetically sealed in glass. .29 ea. 10 for.....$2.50

50 megohm 35 watt Resistor with mount...$1.95 each; 10 for $15.00

W. W. POWER RHEOSTATS

25 Ohms 25 Watt ..... .49
150 Ohms 50 Watt ..... .59
250 Ohms 50 Watt ..... .59
300 Ohms 50 Watt ..... .59
Dual 200 Ohms 50 Watt..... .79
8 Ohms 150 Watts..... 1.79

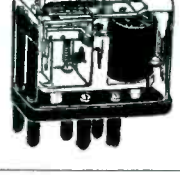
HIGH VOLTAGE—CURRENT MICAS



	MMF	VDC	Price		MMF	VDC	Price
D	.001	600	$.18	C	.0005	5 KV	$ .85
E	.01	600	.24	C	.0015	5 KV	1.60
E	.02	600	.26	C	.003	5 KV	1.90
E	.027	600	.26	C	.005	5 KV	2.50
D	.039	600	.30	B	.007	5 KV	2.75
C	.01	1 KV	.45	B	.002	6 KV	3.50
C	.056	1 KV	.50	B	.003	6 KV	3.75
C	.07	1 KV	.55	A	.004	6 KV	4.95
D	.02	1200	.35	B	.006	6 KV	4.25
C	.024	1500	.65	B	.0085	8 KV	2.90
C	.033	1500	.75	B	.001	8 KV	3.25
C	.015	2 KV	.80	B	.002	8 KV	4.00
C	.02	2 KV	.90	B	.003	8 KV	4.75
D	.002	2500	.45	B	.004	8 KV	5.50
E	.005	2500	.55	B	.005	8 KV	5.75
C	.025	2500	1.25	A	.006	15 KV	26.50
C	.001	3 KV	.90	A	.0098	15 KV	32.50
C	.002	3 KV	.95	A	.0059	18 KV	28.50
D	.005	3 KV	.70	A	.0013	30 KV	36.50
C	.005	3 KV	1.24	A	.00025	35 KV	26.50
C	.006	3 KV	1.50	A	.0001	10 KV	4.95
D	.002	3 KV	.70				
C	.0001	5 KV	.76				

OIL CONDENSERS

20	mfd	330	vac—1.85	6	mfd	2000	vdc—3.95
5	mfd	150	vac— .49	2	mfd	4000	vdc—4.95
1	mfd	600	vdc— .29	1	mfd	5000	vdc—4.50
2	mfd	600	vdc— .39	.1/.1	mfd	7000	vdc—2.25
4	mfd	600	vdc— .59	.1	mfd	7500	vdc—1.95
6	mfd	600	vdc— .79	1	mfd	7500	vdc—9.25
3/3	mfd	600	vdc— .79	.01/.01	mfd	12	kv
10	mfd	600	vdc— .89				dc—5.75
2	mfd	1000	vdc— .79	.005/.01	mfd	12	kv
4	mfd	1000	vdc— .95				dc—5.50
15	mfd	1000	vdc—2.95	.015	mfd	16	kv dc—5.75
2	mfd	1500	vdc—1.25	.05	mfd	12,500	
6	mfd	1500	vdc—2.95				vdc—12.95
1	mfd	2000	vdc—1.45	.75/35	mfd	8/16	kv—7.95
2	mfd	2000	vdc—2.25	2	mfd	18	kv dc—59.50



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Type MN Overcurrent Relay, Adjustable from 250 ma. to 1 amp. External Push Button Reset. Enclosed in glass case. Hand calibrated adjustments, only $6.75

Tremendous stocks on hand. Please send requests for quotas. Special quantity discounts. Price f.o.b. N. Y. 20% with order unless rated, balance C. O. D. Minimum order $5.00.

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DEPARTMENT EA
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SPECIAL METERS

WATTMETER, 0-10 Watts Full Scale, Weston 498, 5½" Square surface mtd case, Single phase A.C. or D.C. 115 Volt Normal, 140 volt Maximum. 80 M.A. Normal, 160 M.A. Maximum. Current coil 35 ohms. (These units have been used but have been completed, checked and tested and are fully guaranteed) $27.50

FREQUENCY METER, 58 to 62 cycles, Westinghouse type HA, complete with external reactor, 5½" Square flush or surface mtd. (State which you require) $35.00

FREQUENCY METER, 55 to 65 cycles, James Biddle Co. type MF-11, Frahm vibrating reed type, 11 reeds, 100 to 150 volt operation, 3½" round flush bakelite case $7.50

FREQUENCY METER, Dual range, 48 to 52 & 58 to 62 cycles, J.B.T. type 30-F, dual element, vibrating reed, 115 volt, 3½" rd fl metal case $5.95

FREQUENCY METER, 350-450 cycles, Weston 637, 3½" Aircraft type, black scale, iron core dynamometer type, 5 cycles per sc division $4.95

D.C. MILLIAMMETER, Weston 271, Fan type, 1-0-1 MA (60-0-60 M.V.) movement, Sc. cal. 600-0-600 R.P.M. $12.50

RECTIFIER TYPE MILLIAMMETER, Weston 545 type 81, Aircraft type, full scale equals 1.1 MA AC, 940 UA DC mvt, 70 ohms resistance, black scale cal 0-270° $6.50

DECIBEL METER, Weston 301 type 61, minus 10 to plus 6 DB, 3½" rd fl bake case, 6 MW 600 ohms. High speed type, with 3 external wire wound multipliers to extend range. List Price $37.50 ..... $11.50

D.C. MILLIAMMETER, —1-0-1.25 miniature MA, black sc, Aircraft style G-1, 1 ¾" sq bake case, Bulova Watch Co. $3.95

D.C. MILLIAMMETER, 0-2 miniature meter, Roller Smith 0-2 MA 0-20 MV movement, 1 ¾" square $2.50

D.C. MILLIAMMETER, 0-12.5 miniature meter, Roller Smith 12.5 MA 0-50 MV movement 1 ¾" square $4.50

PORTABLE TACHOMETERS

0-20,000 RPM Range, Jaeger #43 A-6 Chronometric type $24.50

300-1200, 1000-4000, 3000-12000 RPM, **Jones Motorola Co.**, Multiple Range, Continuous Indicating $24.50

300-1500, 1000-5000, 3000-15000 RPM, **Jones Motorola Co.**, Multiple Range, Continuous Indicating $25.50

TACHOMETER GENERATOR, Weston 752 type J4, 2 terminals $22.50

SALINITY INDICATOR, McNab Model M. $95.00

CELLS for above panel $60.00

BC 1161-A RADIO RECEIVER 150-210 Megacycles, operates off 115 volt 60 cycle, with 14 tubes $34.50

BC 1160-A TRANSMITTER, 157 to 187 Megacycles, operates off 117 volt 60 cycle, with blower, variac, 10 tubes, 3" 0-1 MA meter, etc. $29.50

GASOLINE HEATER, Motorola GN-3-24, 15,000 B.T.U., 1 gal. gasoline lasts 6 hours, 24-28 volt D.C. supply, can be adapted to 115 volt 60 cycle by use of transformer & rectifier $22.50

BOWL INSULATOR, Clear Glass, all brass fittings, S. C. Stock #3G-1830-67076.1 Corning Glass Works #67076 type C, comprises flanged bowl 4 ⅝" x 6 15/16" O. D. at base. Center lead-in pin ⅝" Dia x 11½" long, mounts by means of 6 studs through mtg. flange. Overall dia 8 ¾" $6.00

COMBINATION OFFERS

30 AMP A.C. METER
150 VOLT A.C. METER

Triplett 331-JP 3" round flush bakelite case

Both Meters for $7.95

Both above meters plus an external resistor to extend the range of the Voltmeter to 300 volts

Complete for $8.95

30 AMP A.C. METER
150 VOLT A.C. METER

Triplett 332-JP 3" round flush metal case

Both Meters for $6.95

PORTABLE METERS

A.C. AMMETER, 0-3 & 0-15, Weston 528 with case & leads $12.50

D.C. VOLTMETER, 3-0-3, W.H. PX-4, 100 ohms per volt $9.50

D.C. VOLTMETER, 0-3 & 0-150, W.H. PX-4, 200 ohms per volt $17.50

D.C. VOLTMETER, 0-15 & 0-150, Roller Smith "Steel Six", 100 ohms per volt $21.00

CURRENT TRANSFORMER, Weston 461 type 4, 5 Amp Secondary, 50, 100, 250, 500 & 1000 Amp Primary, 15 V.A. capacity, ¼% acc. $35.00

POTENTIAL TRANSFORMER, Weston 311, for use with 150 volt instruments, Max potential ratio of 1500 & 750 volts to 150 volts, 15 V.A., 1/5% acc. $90.00

INSULATION TESTER, Vibrotest Model 201, Range 0-200 Megohms & 0-2000 ohms & 0-150/300/600 Volts A.C. & D.C. (Slightly used—excellent condition—guaranteed) $38.00

INDUSTRIAL ANALYZER, Weston 639 type 2, measures Volts, Amps, Power Factor & Kilowatts, single & polyphase. (Used—excellent condition—guaranteed) $245.00

DUAL RANGE MILLIAMMETER, Weston 264, 0-25 & 250 milliammeter, mtd on vertical stand with test cord $9.00

AC VOLTMETERS

0-15 **G.E.**, AW-41, 2" R-B bl sc, 800 cyc $2.50

0-15, **G.E.**, AW-41, 2" R-B bl sc, Signal Corps IS-122 ..... $2.50

0-15 **G.E.**, AO-22, 3" R-B bl sc $3.00

0-15 **Weston**, 476, 3" R-B $4.50

0-15 **W.H.**, NA-35, 3" R-B $3.95

0-40 **Weston**, 517, 2" R-M 400 cyc $3.50

0-40 **W.H.**, NA-33, 2" R-B 400 cyc $3.50

0-75 **Weston**, 517, 2" R-M ring mtd $2.95

0-150 **G.E.**, AO-22, 3" R-B 400 cyc $4.00

0-150 **Triplett**, 332-JP, 3" R-M $4.00

0-150 **Triplett**, 331-JP, 3" R-B $4.50

0-150 **Triplett**, 331-JP, 3" R-B W/Resistor for 300 volts $5.50

0-500 **G.E.**, AO-22, 3" R-B $12.00

AC AMMETERS

0-30 **Triplett**, 331-JP, 3" R-B $4.00

0-30 **Triplett**, 332-JP, 3" R-M $3.50

0-50 **G.E.**, AO-22, 3" R-B $4.50

0-50 **W.H.**, NA-35, 3" R-B $4.50

0-60/120 **Burl**, 32XC, 3" R-B w/Ext Transformer $7.50

0-60/120 **Burl**, 32XC, 3" R-B without Ext Trans $4.50

0-150 **G.E.**, AO-22, 3" R-B 5 Amp mvt, with ext. Trans. $7.50

RF AMMETERS

0-120 MA **Simpson**, 25, 3" R-B $7.50

0-1 **G.E.**, DW-44, 2" R-B bl sc $2.95

0-1 **G.E.**, DW-44, 2" R-B $3.50

0-1 **G.E.**, DW-52, 2" R-M $3.00

0-1.5 **G.E.**, DW-52, 2" R-M bl sc $2.95

0-1.5 **Weston**, 507, 2" R-M bl sc $2.50

0-1.5 **Weston**, 425, 3" R-B $8.25

0-2 **Simpson**, 135, 2" R-B $3.50

0-2 **Weston**, 425, 3" R-B $8.50

0-2.5 **Weston**, 507, 2 R-B $3.95

0-2.5 **McClintock**, 3" R-B S.C. #IS-111 ..... $4.50

0-2.5 **Simpson**, 35, 3" R-B $4.95

0-2.5 **Weston**, 425, 3" R-B $8.50

0-2.5 **W.H.**, NT-35, 3" R-B $5.50

0-3 **W.H.**, NT-35, 3" R-B $5.50

0-3 **Weston**, 425, 3" R-B $8.50

0-3 **Weston**, 425 3" R-B W/Ext couple $9.50

0-4 **G.E.**, DW-44, 2" R-B bl sc $2.95

0-5 **Weston**, 425, 3" R-B $8.50

0-6 **G.E.**, DW-44, 2" R-B bl sc $2.50

0-20 **Weston**, 507, 2" R-B $3.50

0-20 **G.E.**, DO-44, 3" R-B $4.95

0-30 **Triplett**, 0347-A, 3" S-B W/Ext leads & couple $8.00

DC MICROAMMETERS

0-200 **Superior**, 4"x4 ⅝" F-B $7.50

0-200 **W.H.**, NX-35, 3" R-B MR 35 W 200 DC UA $8.50

0-400 **Triumph**, 4"x4 ⅝" F-B $5.50

0-500 **De Jur Amsco**, 2" R-B $3.00

0-500 **Gruen**, 221-T, 2" R-B $3.95

0-500 **Simpson**, 6103, 2" R-B $3.50

0-500 **Triplett**, 0221-T, 2" R-B $3.50

DC MILLIAMMETERS

0-1 **G.E.**, DW-41, 2" R-B Spec Scale $3.00

0-1 **G.E.**, DW-51, 2" R-B Spec Scale $3.50

0-1 **W.H.**, NX-33, 2" R-B Black Spec Scale .. $3.00

0-1 **G.E.**, DO-41, 3" R-B $5.50

0-1 **G.E.**, DO-41, 3" R-B Spec Scale $4.50

0-1 **McClintock** S-1811, 3" S-B Spec Scale $3.50

0-1 **McClintock**, 3" R-B Spec Scale $3.50

0-1 **W.H.**, NX-35, 3" R-B MR 35 W 00 1 DC MA $7.50

0-1.5 **Hickok**, 56-R, 2" R-M $2.00

0-3 **Gruen**, GW-580, 2" R-B $3.50

5-0-5 **W.E.**, 3" R-B Concentric style $3.00

0-15 **Simpson**, 26, 3" R-B $4.50

0-20 **G.E.**, DW-55, 2" R-B Black Scale $3.00

0-20 **G.E.**, DO-53, 3" S-B $3.75

0-30 **G.E.**, DO-41, 3" R-B $3.50

0-80 **G.E.**, DO-41, 3" R-B $3.75

0-150 **Gruen**, 508, 2" R-B $3.00

0-200 **Gruen**, 511, 2" R-B $3.00

0-200 **Marion**, 3" R-B $4.00

0-200 **Simpson**, 25, 3" R-B $4.50

0-200 **G.E.**, DO-41, 3" R-B $4.50

0-200 **W.H.**, NX-35, 3" R-B $4.50

0-500 **W.H.**, NX-33, 2" R-B $3.95

DC AMMETERS

0-2 **Simpson**, 25, 3" R-B $4.00

0-5 **Gruen**, 531, 2" R-B $3.50

0-15, **Sun**, AP-381, 3" R-B $3.50

0-15 **Triplett**, 0321-T, 3" R-B $4.00

0-30 **Hoyt**, 123, 2" R-M $2.50

30-0-30 **Beede**, 2" R-M $2.95

30-0-30 **G.E.**, DW-51, 2" R-M $3.50

30-0-30 **U. S. Gauge**, 2" R-M $1.50

0-150 **Simpson**, 125, 2" R-M with shunt $5.50

0-200 **Weston**, 506, 2" R-B with shunt $7.50

0-200 **G.E.**, DO-41, 3" R-B with shunt $9.50

0-300 **G.E.**, DW-51, 2" R-B with shunt $7.50

0-500 **G.E.**, DW-51, 2" R-B less shunt $3.50

DC VOLTMETERS

0-3 **Simpson**, 125, 2" R-M ring mtd $2.00

0-5 **W.H.**, NX-33, 2" R-B 200 r/v $3.50

0-10 **Sun**, 2AP458, 2" R-B 100 r/v $2.50

0-15 **Gruen**, GW 505, 2" R-B $3.50

0-15 **McClintock**, D-100-R-1, 2" R-B Black scale, 1000 r/v $3.00

0-30 **DeJur Amsco**, 210, 2" R-B $2.50

0-30 **G.E.**, DW-41, 2" R-B 250 r/v $2.95

0-50 **Weston**, 301, 3" R-B 200 r/v $5.50

0-50 **Readrite**, 2" R-M $1.00

0-150 **Weston**, 301, 3" R-B Surf mtd 200 r/v .. $4.50

0-150 **G.E.**, DW-51, 2" R-B Special scale $3.95

0-500 **Sun**, 3" R-B MR35W500DCVV $7.00

0-5 KV **W.H.**, NX-35, 3" R-B 1 MA mvt, less resistor $4.95

0-1.5 KV **W.H.**, NX-35, 3" R-B 1 MA mvt, with resistor $7.50

0-15 KV **G.E.**, DO- 53, 3" S-B 500 ua mvt, less resistor $4.95

0-15 KV **W.H.**, NX-35, 3" R-B 1 MA mvt, less resistor $4.50

0-20 KV **G.E.**, DO-41, 3" R-B 500 UA mvt, less resistor $4.95

0-20 KV **G.E.**, OX-33, 2" R-B Black sc 1 MA mvt, less resistor $3.50

0-20 KV **G.E.**, DO-41, 3" R-B 1 MA mvt, less resistor $4.50

0-35 KV **W.H.**, NX-35, 3" R-B FS 1 Ma mvt, less resistor $4.95

All meters are in round flush bakelite case with white scale and are standard in every respect unless otherwise specified. All items are Surplus — New — Guaranteed unless specified otherwise.

MARITIME SWITCHBOARD
338 CANAL STREET
NEW YORK 13, N. Y.
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1B27	4.95
1B29	.89
1B32	4.95
1B36	4.95
1B38	49.50
1B40	4.95
1B60	4.95
1P23	1.95
1S21	1.96
2B4	.98
2AP1	3.95
2C4	1.18
2C21	.98
2C22	.39
2C26A	.28
2C34	.59
2C40	1.98
2C43	7.50
2C44	1.75
2C46	7.50
2D21	1.18
2E22	1.50
2E24	4.95
2E25	4.25
2E26	3.95
2E30	2.39
2J21A	12.95
2J26	8.95
2J31	10.95
2J32	13.95
2J33	24.95
2J34	24.95
2J37	17.95
2J38	13.95
2J49	24.95
2JB51	4.95
2J54B	17.95
2K23	24.95
2K25	24.95
2K28	24.95
2K41	24.95
3AP1	4.95
3B22	4.95
3B23	4.95
3B24	1.98
3B26	1.89
3B27	3.95
3B28	5.95
3BP1	3.95
3C22	18.95
3C23	4.95
3C24	.69
3C30	1.50
3CP1	3.00
3D21A	1.50
3DP1	3.95
3EP1	3.95
3E29	4.95
3FP7	3.95
3J31	49.50
4-65A	14.50
4-125A	27.50
4-250A	37.50
4A1	1.98
4AP10	6.95
4B24	4.95
4C35	19.95
4E27	12.95
4J26	110.00
5AP1	4.95
5AP4	5.95
5BP1	2.95
5BP4	4.95
5CP1	3.95
5CP7	13.95
5D21	29.95
5FP7	3.95
5GP1	9.95
5HP4	9.95
5JP2	11.95
5LP1	11.95
5LP5	14.95
5NP1	2.95
6AF6G	.88
6C21	24.95
6D4	2.75
6F4	5.95
6J4	6.50
7BP7	4.95
7C23	75.00
7C24	80.00
7C25	90.00
9C23	250.00
9GP7	15.00
9JP1	7.95
9LP7	15.00
9NP1	7.95
10Y	.69
10SPEC	.69
10BP4	34.95
10CP4	39.50
12DP7	14.95
12DP8	14.95
12FP7	14.95
12GP7	14.95
12HP7	14.95

Type	Price
12LP4	$55.00
15E	1.50
15R	1.50
23D4	.49
24G	.98
35T	4.95
45SPEC	.49
75TL	3.95
100TH	12.95
100TS	3.00
114A	.69
114B	1.25
120	5.95
121A	2.65
203A	16.95
205B	4.50
211	.98
215A	3.00
217C	7.30
218	49.50
221A	2.95
231D	1.49
242C	6.95
249C	3.49
250R	7.95
250TH	19.50
250TL	19.50
252A	4.95
254	19.95
259A	4.95
262A/B	3.50
274A/B	1.25
282A/B	9.95
290A	4.95
291A	4.95
294A	4.95
304B	5.95
304TH	6.95
304TL	1.49
307A	4.95
316A	.69
327A	4.95
338A	4.93
339A	24.95
350A/B	2.95
354C/D	19.95
368AS	4.93
371A/B	.89
393A	7.95
394A	7.50
399A	2.50
400A	3.25
401A	1.95
403A/B	1.75
408A	1.75
417A	24.95
434A	7.95
446A/B	1.95
450TH	24.95
527	12.95
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575A	14.95
701A	4.95
703A	4.95
705A	2.95
706CY	18.95
707A/B	24.95
708A	7.95
710A	2.95
713A	1.65
714AY	6.95
715A/B	9.95
715C	24.95
717A	.99
720DY	34.95
721A/B	4.35
723AB	7.95
724A/B	4.95
725A	9.95
726A	23.50
750TL	49.50
800	2.25
801A	.98
802	3.75
803	8.95
804	12.95
805	5.95
807	1.25
808	1.89
809	2.93
810	7.95
811	2.45
812	2.95
812H	6.90
813	8.95
814	3.95
815	2.95
816	1.19
826	.69
828	6.95
829A/B	7.95
829B/3E29	4.95
830	2.95
830B	5.25
832/A	4.95
833A	34.50
834	5.95
836	1.15
837	2.50

Type	Price
838	$3.95
841	.69
843	.69
845/W	4.95
851	75.00
860	3.00
861	49.95
864	.69
865	2.98
866/A	.99
866JR	1.19
869B	75.00
872A	2.95
874	2.49
878	2.49
884	1.49
885	.98
891	110.00
892	175.00
902P1	7.95
904	9.95
905	11.95
923	.98
925	1.40
931A	4.95
950	.98
954	.75
955	.75
956	.75
957	.75
958A	.75
959	2.95
991	.75
1608	4.95
1611	.98
1613	.75
1614	1.75
1616	1.39
1619	.75
1620	4.95
1622	1.75
1624	1.75
1625	.49
1626	.49
1628	4.95
1629	.69
1631	1.50
1634	.79
1635	1.10
1636	5.95
1638	.98
1641	.79
1642	.98
1644	1.49
1851	1.25
1852	1.06
1853	1.06
1960	.95
2050	1.19
2051	.98
5514	4.95
5516	5.95
5562	10.00
7193	.39
8003	5.95
8005	4.95
8011	2.95
8012A	4.95
8013A	2.95
8014A	24.95
8016	1.49
8020	3.95
8025	7.95
C5B	12.95
C6J	12.95
CEO72	1.95
CK1005	.35
CK1006	.69
CK1090	4.95
EF50	.79
EL1C	4.95
EL3C	4.95
F123A	12.95
F660	150.00
FG17	3.25
FG27A	9.95
FG33	8.95
FG67	12.95
FG81A	6.95
FG105	19.95
FG172A	32.50
FG235	59.50
FG238B	160.00
GL146	11.00
GL502A	1.98
GL530	49.50
GL559	5.35
GL697	150.00
HF100	3.95
HF200	12.95
HF210	17.95
HY65	2.49
HY69	2.49
HY75	1.25
HY615	1.25
HYE1148	.48
KU610	9.95

Type	Price
ML101	$150.00
REL36	.98
RK22	4.95
RK23	4.95
RK25	2.95
RK33	.98
RK34	.59
RK39	1.75
RK59	5.95
RK60	.79
RK65	24.95
RK72	1.95
RK73	3.95
RX120	10.00
SD809	4.95
T20	1.50
T55	3.95
T200	10.95
TZ20	1.50
TZ40	2.95
UH50	5.95
V70D	6.95
VR75	.98
VR78	.75
VR90	.75
VR91	1.49
VR105	.98
VR150	.75
VT127A	3.00
VU111	1.19
WL460	14.95
WL468	14.95
WL532A	4.95
WL562	150.00
WL616	105.00
Z225	1.95
ZB120	6.95
ZP477/12DP8	14.95
0A2	1.69
0A3/VR75	.98
0A4G	1.06
0B2	2.05
0B3/VR90	.75
0C3/VR105	.98
0D3/VR150	.75
OY4	.88
0Z4	.88
PZ4G	.88
O1A	.50
1A3	.72
1A4	1.28
1A4P	1.56
1A5GT	.72
1A6	1.28
1A7GT	.80
1B3GT	1.49
1B4	1.56
1B5/258	1.28
1B7GT	1.06
1C5GT	.88
1C6	1.28
1C7G	1.28
1D5GP	1.55
1D7G	1.28
1D8GT	1.56
1E5GT	1.38
1E7G	1.56
1F4	1.06
1F5G	1.06
1F6	1.56
1F7G	1.56
1G4GT	1.06
1G6GT	1.06
1H4G	.88
1H5GT	.66
1H6G	1.28
1H6GT	1.28
1J6GT	1.28
1L4	.80
1LA4	1.06
1LA6	1.06
1LB4	1.06
1LC5	1.06
1LC6	1.06
1LD5	1.06
1LE3	1.06
1LG5	1.06
1LH4	1.06
1LN5	1.06
1N5GT	.80
1P5GT	1.06
1Q5GT	1.06
1R4	1.06
1R5	.80
1S4	.96
1S5	.72
1T4	.80
1T5GT	1.06
1U4	.80
1U5	.72
1V	.88
2A3	1.28
2A4G	1.28
2A5	.88
2A6	1.06
2A7	1.06
2B7	.88
2V3G	1.98
2X2A	1.25
3A4	.39

Type	Price
3A5	$ 1.49
3A8GT	1.98
3B7	.36
3D6	.36
3LF4	1.28
3Q4	.88
3Q5GT	.96
3S4	.80
3V4	.80
5AZ4	.50
5R4GY	1.15
5T4	1.28
5U4G	.60
5V4G	.96
5W4	1.06
5W4GT	.66
5X4G	.72
5Y3GT	.42
5Y4G	.60
5Z3	.72
5Z4	1.06
6A3	1.28
6A6	1.06
6A7	.80
6A8	.80
6A8GT	.80
6AB5/6N5	.88
6AB7/1853	1.06
6AC5GT	1.16
6AC7/1852	1.16
6AD6	.88
6AD7G	1.28
6AF6	1.25
6AG5	1.06
6AG7	1.28
6AH6	1.56
6AJ5	.99
6AK5	1.56
6AK6	.96
6AL5	.80
6AL7GT	1.06
6AQ5	.80
6AQ6	.72
6AQ7GT	.88
6AR5	.66
6AS7G	4.95
6AT6	.60
6AU6	.80
6AV6	.60
6B4G	1.28
6B5	1.56
6B7G	.88
6B7	1.28
6B8	1.28
6B8G	1.28
6BA6	.80
6BE6	.72
6BG6G	1.92
6BH6	.80
6BJ6	.80
6C4	.39
6C5	.66
6C5GT	.66
6C6	.80
6C7	1.28
6C8G	1.28
6D6	.66
6D8G	1.28
6E5	.85
6E6	1.06
6F5	.66
6F5GT	.66
6F6	.80
6F6GT	.66
6F7	1.06
6F8G	1.28
6G6G	1.06
6H6	.60
6H6GT	.60
6J5	.54
6J5GT	.54
6J6	1.16
6J7	.80
6J7GT	.80
6J8G	1.28
6K5GT	.96
6K6GT	.60
6K7	.66
6K7GT	.66
6K8	.96
6K8GT	.96
6L5G	1.06
6L6	1.42
6L6G	1.16
6L6GA	1.16
6L7	.96
6L7G	1.16
6N6G	1.56
6N7	.96
6N7GT	.96
6P5GT	.96
6Q6G	1.36
6Q7	.80
6Q7GT	.72
6R7	1.06
6R7GT	1.06
6S7	1.28
6S7G	1.28
6S8GT	1.06
6SA7	.66

Type	Price
6SA7GT	$ .66
6SB7Y	.88
6SC7	.72
6SD7GT	.49
6SF5	.66
6SF5GT	.72
6SF7	.80
6SG7	.80
6SH7	.39
6SJ7	.66
6SJ7GT	.66
6SK7	.66
6SK7GT	.66
6SL7GT	.96
6SN7GT	.88
6SQ7	.60
6SQ7GT	.60
6SR7	.72
6SR7GT	.72
6SS7	.66
6ST7	.88
6SV7	.88
6T7G	1.24
6U5G5	.72
6U6GT	.72
6U7G	.72
6V6	1.28
6V6GT	.80
6W7G	.88
6X4	.60
6X5GT	.60
6Y6G	.96
6Y7G	.88
6Z7G	1.28
6ZY5G	.88
7A4/XXL	.72
7A5	.72
7A6	.72
7A7	.72
7A8	.72
7AD7	1.06
7AF7	.72
7AG7	.88
7AH7	.88
7B4	.72
7B5	.72
7B6	.72
7B7	.72
7B8	.72
7C4/12303A	.39
7C5	.72
7C6	.72
7C7	.72
7E5/1201	1.66
7E6	.72
7E7	.88
7F7	.88
7F8	1.06
7G7/1232	1.06
7H7	.80
7J7	1.06
7K7	1.06
7L7	.88
7N7	.88
7Q7	.72
7R7	.88
7S7	1.06
7V7	1.06
7W7	1.06
7X7/XXFM	1.06
7Y4	.72
7Z4	.72
10	.69
12A	.60
12A6	.39
12A6GT	.29
12A7	1.28
12A8GT	.80
12AH7GT	.88
12AL5	.80
12AT6	.60
12AT7	1.16
12AU6	.80
12AU7	.96
12BA6	.72
12BE6	.72
12C8	.69
12F5GT	.72
12H6	.39
12J5GT	.39
12J7G	.80
12J7GT	.80
12K7GT	.66
12K8	.88
12K8GT	.96
12Q7GT	.72
12SA7	.66
12SA7GT	.66
12SC7	.72
12SF5	.80
12SF5GT	.80
12SF7	.83
12SF7GT	.80
12SG7	.72
12SH7	.39
12SJ7	.66
12SJ7GT	.66
12SK7	.66
12SK7GT	.66
12SL7GT	.88

Type	Price
12SN7GT	$ .80
12SQ7	.60
12SQ7GT	.60
12SR7	.39
12SR7GT	.39
12X3	.98
12Z3	.88
14A7/12B7	.88
14AF7/XXD	.88
14B6	.88
14B8	.88
14C5	.88
14C7	.88
14E6	.72
14E7	.88
14F7	.88
14F8	1.06
14H7	.88
14J7	1.06
14N7	1.06
14Q7	.88
14R7	.88
14S7	1.06
14W7	1.06
14X7	1.06
14X4	.88
19	1.28
19T8	1.56
22	1.28
24A	.88
25A6	1.06
25A6G	1.06
25AC5GT	1.16
25L6GT	.66
25Y5	1.16
25Z5	.60
25Z6GT	.60
26	.72
27	.60
28D7	.39
30	.39
31	.39
32	1.28
32L7GT	1.28
33	.39
34	.38
35/51	.80
35A5	.72
35B5	.80
35L6GT	.66
35W4	.46
35Y4	.72
35Z3	.72
35Z4GT	.60
35Z5GT	.59
36	.39
37	.39
38	.39
39/44	.39
41	.66
42	.66
43	.66
45	.66
45Z3	.60
45Z5GT	.72
46	1.06
47	.96
49	.88
50	1.56
50A5	.88
50B5	.66
50L6GT	.66
50Y6GT	.72
53	1.06
56	.72
57	.80
58	.80
59	1.06
70L7GT	1.56
71A	.80
75	.66
76	.66
77	.66
78	.66
79	.88
80	.46
81	1.56
82	1.06
83	1.06
83V	1.28
84/6Z4	.72
85	.88
89	.72
89Y	.39
117L7GT	1.56
117M7GT	1.56
117N7GT	1.56
117P7GT	1.56
117Z3	.60
117Z4GT	1.16
117Z6GT	.96
FM-1000	1.28
UX120	1.38
UX200	1.28
9001	.89
9002	.39
9003	.69
9004	.49
9005	.98
9006	.49

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Blower Assembly MX-215/APG

John Oster C-2P-1L 28 v. DC 7000 RPM 1/100 hp. #2 L-R Blower.
Stock #SA-202.
Price $2.95 each

Universal Electric DC
W.E. KS-5603-L02, 28 v. DC 0.6 amps. 1/100 hp. 4 lead shunt. Stock #SA-233.
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Fractional Motors M-100. 3/16 HP.
Compound wound. Cont. duty. 115 v. DC. 5" diam. 8" lg. 1¾" shaft ext. x ½" diam. Stock #SA-171. **Price $6.75 each.**
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DC SERVO MOTORS

C-1 Autopilot Servo Unit—28 v. DC Shunt motor. 2250 rpm. 2 magnetic clutches, reduction gear, differential and 2 magnetic brakes. Output shaft 15 rpm. Torque 225 in/lbs.
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Stock #SA-211 **Price $12.50 each**

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Pioneer CL-3
Use as transmitter or indicator on 26 v. 400 cy. or 52 v. 800 cy. May be used as indicator with 360° potentiometer on DC.
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D-101 27 v. DC in @ 1.5 amps. DC out. 285 v. @ 0.60 amps. Stock #SA-187.
Price $1.50 each

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Pioneer 5 tube amplifier converted for Autosyn input. 115 volts, 400 cycles. Stock #SA-45A. **Price $29.50 each net with tubes.**

ALSO
COMPLETE 400 CYCLE SERVO SYSTEMS
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400 CYCLE BLOWERS
PRECISION AUTOSYNS
MAGNETIC AMPLIFIER ASSEMBLIES
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AC-SERVO MOTORS

Pioneer—CK-2 and 10047-2A for 400 cy.
Kollsman—776-01 for 400 cycles.
Diehl—FP-25-3. **FPE-25-11** (CDA-211052) and ZP-105-14 for 60 cycles.
Prices on Request

Remote Position Indicating System
6-12 v, 60 cycles 5 inch indicator with 0 to 360° dial. Heavy duty transmitter. Stock #SA-115. **Price $9.95 per system**

LP-21-LM Compass Loops

New

QUANTITY PRICES ON REQUEST

MERCURY CONTACT RELAY

W.E. D-168479
Millisecond switching at up to 60 c.p.s. Technical data on request. Stock #SA-259. **Price $4.75 ea. Special qty. prices.**

INVERTERS

400 Cycles
Three Phase

Holtzer Cabot MG-153—Input 28 volts DC at 52 amps. Output three phase 115 volts 400 cycles at 750 va. 0.90 P.F. Also second output of 26 volts 400 cycles at 250 V.A. Voltage and frequency regulated.
New—Perfect ..... **$99.50 ea.**
New—Surface Damages ..... **59.50 ea.**

Leland SD-93—(10285)—Input 28 volts DC at 60 amps. Output 115 volts three phase 400 cycles at 750 va. 0.90 P.F. Second output voltage of 26 volts 400 cycles at 50 V.A. Voltage and frequency regulated. Designed for use with various autopilots. Stock #SA-209. **Price $79.50 each**

Holtzer Cabot MG-149H—Similar to MG-149F but draws 44 amps DC at 28 v. Output ratings are at 0.90 P.F. Equipped with high altitude brushes. Stock #SA-4.
Price $34.50 each

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Sperry A5 Vertical Gyro. Part No. 644841, 115 volts 400 cycle 3 phase, **$19.50 ea.**
Sperry A5 Directional Gyro. Part No. 656029, 115 volts 400 cycle, 3 phase.
Schwein Free & Rate Gyro, Type 46800.

Schwein Free & Rate Gyro—45600—Stock #SA-148. **Special Price $8.75 each.**

Bodine NYC-13 AC Motor
115 v. 60 cycles, 1/40 hp. 1800 rpm. Cont. duty, .55 amps. Stock #SA-245.
Price $9.50 each.

SYNCHROS

Navy Types
1G, 1F, 1CT, 5C, 5F, 5CT, 5DG, 5HCT, 5SF, 5HSF, 5SDG, 6DG, 6G, 6DG, 7G, etc.
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THERMOSTATIC TIME DELAY RELAYS

Amperite type 115 No-45.

Heater voltage 115V. Normally open SPST contacts. 45 sec. delay. Contact rating 115V-3A., A.C. (or 440V., A.C. 2A.) max. voltage on contacts—1000. max voltage bet. contacts and heater—1500. Size 3 9/32 x 1 ¼" overall. Made for U. S. Navy.

New surplus $1.10

MOTOR GENERATORS

Allis Chalmers 115V. D.C. to 120V. 60 cy. 1 Ph. 1.25 K.V.A., P.F. .80 Centrifugal starter. Fully enclosed.

New $97.50

Same as above but for 230V. D.C. input **$125.00**

Diehl 120V. D.C. to 120V. A.C., 60 cy., 1 Ph., 2.5 K.V.A., P.F. 4. Complete with magnetic controller, 2 field rheostats and full set of spare parts including spare armatures for generator and motor.

New $185.00

O'Keefe and Merritt, 115V. D.C. to 120V. A.C. 50 cycles, 2 K.V.A., Pf .9 Idles as a 3 phase synchronous motor on 208V. 50 cy.

New $165.00

Electrolux Dynamotor 105/130V. D.C. at 6 amps. to 26 or 13V. D.C. at 20 amps. or 40 amps. respectively. Fully filtered for radio use and complete with Square "D" lineswitch. Navy type CAJO 211444.

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PEAK-TO-PEAK V.T.V.M.

A small, lightweight, portable instrument designed to measure peak-to-peak voltages of recurrent waves, particularly of the type normally found in radar video circuits. It is especially intended for use in setting the levels of video and synchronizing voltages in radar equipment where the relationships between these voltages are important to the operation of associated equipment.

Designed by Radiation Labs. M.I.T. for the U. S. Navy.

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90 degree elbow — Bronze—Brand New

Price $9.75

LINEAR SAWTOOTH POTENTIOMETER

W.E. No. KS 15138

Input 24 volts D.C. Output varies in accordance with linear sawtooth wave.

Brand New $5.75

STEPDOWN TRANSFORMERS

Input: 115V. 60 cycles. Output: 20 V., at 10 amps. Also tapped at 6V., for pilot light. Ideal for Selenium Rectifier Applications, etc.

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CRP-23AGC Load Dividers for use with S.G. Modernization Kits. New.

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Provides 4 Types of Presentation:
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Designed for use with receiving equipment AN/ARR-7, AN/ARR-5, AN/APR-4, SCR-587 or any receiver with I.F. of 455kc, 5.2mc, or 30mc. With 21 tubes including 3" scope tube. Converted for operation on 115 V. 60 cycle source.

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Primary: 115 V., 60 cycles.
Secondary: 8000 V., C.T., 800 V.A.

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Lord #20, 3" x 3" x 1¾"	.40
U. S. Ruther #5150 C, 2⅜" x 2⅜" x 1⅛"	.30
Lord 15, 2⅜" x 2⅜" x 1⅛"	.25
Lord #10, 1¼" x 1¼" x ⅝"	.10
Lord #3, 1¼" x 1¼" x ⅜"	.10

PARABOLOIDS

17½" diameter, spun magnesium dishes, 4 inches deep. Reinforced perimeter. Two sets of mounting brackets on rear. Opening at apex for waveguide dipole assembly 1½" x 1⅝".

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Clare octal base Relay No. 30FMX 115V. 60 cy. 0.140 amp. Res. 75 ohms. Makes two breaks one.

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SELENIUM RECTIFIER

Bridge Type

Input: 36 V. AC.
Output: 28 V. DC., 1.1 Amps.

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WESTERN ELECTRIC MERCURY CONTACT RELAYS

TYPE D-168479

These relays are glass sealed, mercury-wetted contact switches surrounded by operating coils and encased in metal housings, mounted on an octal tube base.

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- High speed keying
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- Relay Amplifiers
- Vibrator Power Supplies
- Servo-mechanisms

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- High speed of operation
- Constant operating characteristics
- Freedom from chatter
- High current capacity
- Long, trouble-free service

Single Pole, Double Throw Contacts. Two coils of 700 ohms and 3300 ohms. Operating current with coils connected in series 6.6 ma. Release current 5.2 ma.

When operated under specified conditions this relay has a life expectancy of 1000 hours at 60 operations per second.

Overall length—3-3/8". Overall dia.—1-5/16"

Brand new Priced at a fraction of Government cost **$4.75**

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Type TP3

For two-way signalling for voice communication. No batteries needed. May be used on metallic or grounded circuits, open-wire lines, cables or circuits using local-battery telephones, switchboards; two-way-ring-down trunk circuits of common battery switchboards, etc. Contained in treated waterproof fabric cases with adjustable carrying straps.

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25,000 VOLT CAPACITORS STANDARD BRANDS

Inerteen Type FP 25,000 volts .5 MFD. Size 13½"x 16½"x4½" with mounting brackets.

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15,000 Volts 1MFD. Cat. No. 1463. Size 12"x16½" x4". With mounting flange.

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RG 8/U 52 OHM—Per 1,000 ft. $50

RG 22/U 95 OHM (2 cond.) per 1000 ft...$120.00
RG 62/U 93 OHM per 1000 ft....$ 50.00

COAXIAL FITTINGS

Angle Adapter	Plug	Socket	Hood
22c	28c	28c	9c
M-359	PL-259	SO-239	83-1H
83-1AP	83-1SP	83-1R	

PL-259-A, 83SPN 28c; 83-1F 75c; 83-1J 65¢ 83-2R; 83-2AP. UG 13/U; UG 21/U; UG 22/U; UG 24/U; UG 27/U, UG 59/U; UG 87/U; UG 281/U with short length of coax attached. Each ONLY.....50¢

COAXIAL RELAY. Struthers Dunn—coil 12 V.D.C., 90Ω Equipped with three UG 87/U BN receptacles for small size RF cable.....$8.95

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Water-tight, 14 ga. steel. 17"x25"x6½". Screw type brass hinge on lid. 50 lb. Reduced to $2.95.

ALLEN SET SCREWS

4-40 x 1/8	6-32 x 1/8	8-32 x 3/16
4-40 x 3/16	8-32 x 1/8	8-32 x 5/16

ALL SIZES.....$1.50 per 100

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Mfg.	ID	OD	Width	Price
Fafnir 33K5	3/16"	1/2"	5/32"	$.25
N.D. 38	5/16"	7/8"	9/32"	.45
Fafnir K8A	1/2"	1 1/8"	5/16"	.60
N.D. 3201	15/32"	1 1/4"	3/8"	.60
N.D. 5202C13M	1/2"	1 3/8"	1 3/8"	1.00
Fafnir 7308W	1 37/64"	3 9/16"	15/16"	2.00
SKF 466430	6"	8"	1"	5.00
SKF 170645	3 11/32"	4 1/8"	7/16"	1.50
Fafnir K37B	2 5/16"	3 1/16"	11/32"	1.00
Fafnir 545	2 1/16"	2 5/8"	15/32"	1.00

NEEDLE BEARINGS

B88 1/2" wide	1/2"	11/16"	25¢
B108 1/2" wide	5/8"	13/16"	30¢
GB34X 1/4" wide	3/16"	11/32"	25¢

POWER RHEOSTATS

25 WATT

Resist.	Mfg.	Shaft	Pr.
10Ω	Clarostat	1/16"	.79
15	Ohmite	7/16"	.95
25	IRC	S.D.	.79
35	Ohmite	1 1/4"*	.95
50	Clarostat	1/2*	.79
145	Grimes Mfg.	1/2" with switch	.95
200	IRC	7/16"	.79
250	Ohmite	7/16"	.95
350	Ohmite	7/16"	.95
370	IRC	1/2"	.79
1,500	Clarostat	7/16"	.79
2,000	Ohmite	7/16"	.95
2,500	Ohmite	S.D.*	.95
3,500	Ohmite	7/16"	.95
5,000	Ohmite	S.D.*	.95

50 WATT

2Ω	Ohmite	1/4"	1.11
6	Ohmite	1/4"	1.11
8	Ohmite	S.D.*	1.11
10	Ohmite	1/4"	1.11
12	Ohmite	1/4"	1.11
20	Ohmite	1/4"	1.11
50	Ohmite	1/4"	1.11

50 WATT

90Ω	Clarostat	1/2"	.99
123	IRC	1/2"	.99
500	Ohmite	1/4"	1.11
1,000	Ohmite	1/4"	1.11
1,250	Ohmite	1/2"	1.11
2,000	Ward Leonard	1/2"	.99
3,500	Ohmite	1/8"	1.11

100 WATT

2Ω	Ohmite	1/2"	1.99
25	Ohmite	1/4"	1.99
1,000	Ohmite	1/4"	1.99
2,000	Hardwich Hindle	1/8"	1.79
10,000	Ohmite	S.D.*	1.99

150 WATT

8Ω	Ohmite	1/2"	2.75
75	Ohmite	1/4"	2.75
100	Ohmite	1/4"	2.75
150	Ohmite	1/4"	2.75

300 WATT

100Ω	Ohmite	2"	4.75
150	Ohmite	2"	4.75

400 WATT

500Ω	Ohmite	2"	6.75

* S.D. = Screwdriver

PRECISION POTENTIOMETERS

6 WATT

20,000Ω	Muter	314A	$1.70
20,000	GR	314A	2.50
6,000	GR	314A	2.50
6,000	De jur	260	1.70
6,000	Muter	314A	1.70
5,000	Muter	314A	2.50
5,000	GR	314A	2.50
5,000	GR	214A	1.40
2,000	De jur	260	1.70
600	GR	314A	2.25
200	GR	214A	1.40
40	GR	214A	1.40

4 WATT

500Ω	Centralab	48-501	$.90
50	De jur	292	.75
50	GR	301	1.10
25	GR	301	1.10
20	De jur	292	.75
20	GR	301	1.10
12	GR	301	1.10

12 WATT

10,000Ω	GR	471-AS15	3.50
10,000	GR	371T	2.50
10,000	Muter	371T	2.50
10,000	De jur	271T	2.00
5,000	De jur	271T	2.00

PHASE SHIFT CAPACITOR

4 Stators — single rotor — 90° quadrants—
4 taps—360° rotation.
ONLY $2.79—Lots of 10.....$25.00

CAPACITORS

POSTAGE STAMP MICAS

8.2mmf	56mmf	200mmf	560mmf	.0015mfd
10	60	220	600	.002
18	70	250	650	.0026
20	90	270	680	.0027
22	100	350	800	.003
25	140	370	.001mfd	.0039
40	150	400	.0012	.007
47	160	470	.0013	.008
50	180	500	.00135	.01

Price Schedule

8.2mmf to .001mfd 5¢ .003mfd to .008mfd 12¢
.0012mfd to .002mfd 7¢ .01mfd 18¢

SILVER MICAS

10mmf	125mmf	390mmf	680mmf	.0025mfd
22	150	400	700	.0027
39	180	430	750	.003
50	200	466	820	.0033
62	240	470	.001mfd	.0039
66	250	488	.0012	.004
68	300	510	.0013	.005
100	330	525	.0015	.0051
110	360	560	.002	.0068
120	370	665	.0024	.01

Price Schedule

10mmf to .001mfd 10c .003mfd to .0068mfd 50¢
.0012mfd to .0027mfd 20c .01mfd 65¢

CERAMICS

3mmf	12mmf	22mmf	56mmf	110mmf	220mmf
3.44	13	27	62	115	1000
1.7	15	33	68	140	1090
6.8	16	40	75	150	
8	18	47	82	180	
10	20	50	91	200	

$6 per 100

OIL FILLED

MFD	V.D.C.	Price	MFD	V.D.C.	Price
.1	25,000	$14.95	.1–.1	7,000	$1.75
.012	25,000	6.20	.1	7,000	1.95
.03	16,000	4.50	.02–.02	7,000	1.65
.375@	16,000 and		1	6,000	8.50
.75@	8,000(dual)	8.95	.1	6,000	1.75
.15–.15	8,000	2.85	.03–.03	6,000	1.65
5	7,500	23.95	2	4,000	4.50
.1	7,500	1.85	.25	3,000	1.75
			.2	750 V.A.C.	
			(2,200	V.D.C.)	.39
			1	2,000	.95
			4	1,000	.90
			3	1,000	.80
			2	1,000	.65
			1	800	.40
			10	600	1.00
			4	600	.69
			2	600	.39

2 mfd. 4,000 V. D. C. #23F47 SPECIAL! $4.50

BATH TUBS

4 mfd	50 VDC	.21¢	.25	600 VDC	.23¢
2 mfd	200 VDC	.14¢	.5	600 VDC	.25¢
.2 mfd	400 VDC	.15¢	1	600 VDC	.30¢
.25 mfd	400 VDC	.15¢	2 x 1	600 VDC	.36¢
.05 mfd	600 VDC	.15¢	2	600 VDC	.36¢
.1 mfd	600 VDC	.20¢	.06	1000 VDC	.17¢
2 x .1 mfd	600 VDC	.27¢	.1	1000 VDC	.25¢
3 x .1	600 VDC	.30¢	1	1000 VDC	.36¢
.176	600 VDC	.21¢			

SPAGHETTI SLEEVING—Asst. sizes and colors, 3 ft. lengths.....99 feet—**Only $1.00**

Gear Asst.—Mostly stainless steel and brass. Over 100 pcs.—Experimenter's Dream—Only $6.50.

WW PRECISION RESISTORS 1%

¼ WATT—25c

6.68Ω	12.32Ω	16.37Ω	123.8Ω	414.3Ω
10.48	13.02	20	147.5	705
10.84	13.52	62.54	220.4	2193
11.25	13.89	79.81	301.8	10,000
11.74	14.98	105.8	366.6	59,148

½ WATT—25c

.250Ω	11.1Ω	235Ω	4,451Ω	15,000Ω
.334	13.15	260	5,000	15,750
.502	46	270	5,900	17,000
.557	52	298.3	6,500	20,000
.627	55	400	7,000	30,000
.76	75	723.1	7,500	100,000
1.01	97.8	2,500	8,000	150,000
1.53	125	2,850	8,500	
2.04	180	3,427	10,000	
	210	4,000	14,825	

1 WATT—30c

1.01Ω	5.21Ω	1,250Ω	9,000Ω	55,000Ω
2.58	10.1	3,300	18,000	65,000
3.39	10.9	7,000	50,000	70,000
5.05	270			75,000

1 WATT—40c

100.000Ω	128.000Ω	180.000Ω	522.000Ω	700.000Ω
120.000	130.000	320.000	525.000	
125.000	160.000	470.000	600.000	

1 Megohm, 1 Watt, 1%—65c.; 5%—40c
Orders for 100 pieces—10% off;
Orders for 1,000 pieces—20% off.

UNIVERSAL JOINT

ALUMINUM

1⅛" long x ½" O. D. ¼" ID

ONLY 40c

JONES BARRIER STRIPS

Type	Price	Type	Price	Type	Price
2-140Y	$.05	5-141Y	.25	5-142	.21
3-140 3/4W	.12	7-141	.26	6-142	.25
3-140	.10	8-141	.27	8-142	.38
4-140	.13	8-141 3/4W	.38	8-142Y	.52
5-140Y	.19	9-141Y	.42	10-142 3/4W	.58
8-140	.23	10-141 3/4W	.47	11-142	.48
10-140 3/4W	.41	12-141	.43	12-142Y	.68
13-140	.36	14-141	.51	17-142Y	.97
15-140	.42	17-141	.60	18-240	.35
2-141	.09	17-141Y	.78	22-240	.45

Any order for 100 pieces—10% off;

PULSE TRANSFORMERS

X 124 T2, UTAH, marked 9262 or 9280, small gray case 1⅞" high x 1⅛" x ⅝" with two 6-32 mtg. studs. Ratio 1:1:1, hypersil core....$1.50
352-7178—Spec. 10, 111 Chicago Trans., equivalent to 9262 (above).....$1.50
D161310, 50 Kc to 4 Mc. 1¾" dia. x 1⅞" high, 120 to 2350 ohms.....$2.00
TR 1048, Dinion Coil Co.....$1.25
TR 1049, Dinion Coil Co.....$1.25
352-7250-2A, cased 15/16" dia. x 1⅝" high. DC 10 ohm, 3½ ohm, 140 cy. to 175 KC.....$1.25
352-7251-2A, similar—shorter pulses ..$1.25
300 KVA GE 7557296, 50 ohm pulse cable connection; 3,850 V. in., 17,300 V. out. (250 KVA @ ⅛ microsecond).....$15.00
800 KVA G.E. K2731, 28,000 Volt pk. output. Bifilar, pulse width; one-microsecond..$19.50
D166173, W. E. Freq. response 10KC to 2 MC.....$12.00
KS9800, Ratio, 1.1:1, 2:1, Freq. range 380 to 520 C.P.S.....$4.00

TIME DELAY RELAY

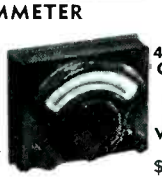
Raytheon CPX 24166
KS 10193-60 Sec.

- **115 V., 60 Cycle**
- **Adj. 50-70 Seconds**
- **2½ seconds recycling time, spring return**
- **Micro Switch Contact, 10A**
- **Holds On as long as power is applied**
- **Fully Cased.**

ONLY.....$6.50

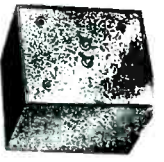
DC AMMETER

0-15A BASIC MOVE. 12 Ma 5" x 4" METAL CASE MIRROR SCALE Lots of 10—$35



$3.85 ea.

400 MA CHOKE 12 H. 90 Ω 6.000 V. D. C. TEST $3.85



DYNAMOTOR RIOT!

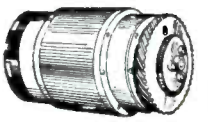
NEW and GUARANTEED

Black & Decker		GE	
In	Out	In	Out
27V.	255V.	27V.	285V.
1.4A.	.06A.	1.75A.	.075A.

Your Choice.....95¢
Lots of 10.....$8.50

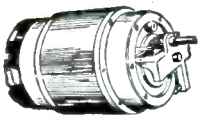
SELSYNS

115 V., 60 Cyc.
3¼" dia. x 4½" body
#C78248
$7.25 pair



DIFFERENTIAL

115 V., 60 Cyc.
#C78249
$2.25 ea.



Used between two #C78248's as dampener. Can be converted to a 3600 RPM Motor in 10 Minutes. Conversion sheet supplied.
Mounting Brackets—(Bakelite) for selsyns and differentials shown above.....25¢ pair

MINIMUM ORDERS $3 All orders f.o.b. PHILA. PA.

RELIANCE MERCHANDIZING CO.

12th St. Cor. Buttonwood, Phila. 23, Pa. *Telephone MArket 7-2401*

RELAYS

FOR EVERY PURPOSE

Over a Million in Stock!

Whether you require large quantities of relays for production runs or single units for laboratory or amateur work, Wells can make immediate delivery and save you a substantial part of the cost.

Our capable engineering staff is prepared to offer assistance in the selection of correct types to suit your exact requirements.

Each relay is brand new, standard make, inspected, individually boxed and fully guaranteed.

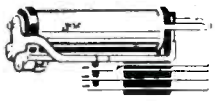
The following list represents only a tiny portion of our relay stock. Write or wire us for information on types not shown.

STANDARD DC TELEPHONE RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-101	24V	1500.	DPST (NO)	Auto. Elec.	$1.35
R-102	24V	400.	SPDT	Auto. Elec.	1.10
R-103	24V	DUAL-1000	3PST (NO)	Auto. Elec.	1.35
R-105	24V	600.	3PST (NO)	Clare	1.20
R-106	24V	1300.	3PST (NC)	Clare	1.25
R-152	12V	50.	DPDT-SPST (NO)	Guardian	1.10
R-153	12V	200.	SPDT-SPST (NO)	Stromberg	1.25
R-154	12V	200.	SPST (NO)	Clare	1.20
R-155	12V	100.	SPST (4NO4NC)	Auto. Elec.	1.15
R-158	6V	50	4PST (NO)	Stromberg	1.10
R-159	6V	50	DPST (NO)	Stromberg	1.10
R-160	6V	12	3PDT-3PST (NO)	Auto. Elec.	1.05
R-161	6V	10	3PST (2NC-1NO)	Auto. Elec.	.90
R-121	150V	5000.	2PST (NO) SPDT	Clare	1.65
R-123	150V	6300	SPST (NO)	Clare	1.75
R-602	150V	6500	3PST (NO)	Clare	1.75
R-515	24V	750	SPST (NO)	Clare	1.25
R-517	12V	250	DPST (NO)	Clare	1.20
R-519	250V	14000.	SPDT	Auto. Elec.	1.95
R-520	250V	14000	DPDT	R.B.M.	2.10
R-521	32V	1000.	DPDT	Kellogg	1.20
R-166	24V	DUAL-200.	DPDT-SPST (NO)	Stromberg	1.59
R-168	24V	DUAL-200.	4PST (NO)	Auto. Elec.	1.20
H-240	250-350V	40000	DPST (NO)	Auto. Elec.	2.95
H-241	48V	660	SPDT-SPST (NO)	Clare	1.25

TYPE 18 DC TELEPHONE RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-109	24-48V	4000.	SPDT	Auto. Elec.	$1.50
R-110	24-32V	3500	SPDT	Auto. Elec.	1.50
R-112	90-120V	6500	SPST (NC)	Auto. Elec.	1.75
R-114	24V	500	4PST (NO)	Auto. Elec.	1.30
R-603	24V	400	DPST (NO)	Auto. Elec.	1.25
H-238	24V	150	DPDT-SPST (NC)	R.B.M.	1.25
H-239	24V	180	DPST (NO)	Auto. Elec.	1.25



SEALED DC TELEPHONE RELAYS

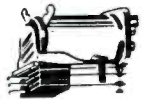
Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-125	24V	300.	DPDT	Clare	$2.75
R-126	90-120V	2000	DPDT	Clare	3.00
R-504	24-70V	2800	SPDT	GE-C103C25	3.00

V TYPE DC TELEPHONE RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-164	24-32V	1000.	SPST (NO)	W.E.	$1.20
R-512	24-48V	3500	DPDT	W.E.	1.30
R-513	12-24V	300	DPDT-DPST (NC)	W.E.	1.20
R-514	4-6V	60	SPDT	W.E.	1.05
R-526	6V	35	DPDT-SPST (1NC-1NO)	W.E.	1.05

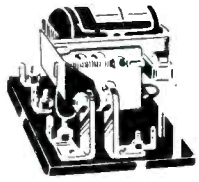
AC-STANDARD TELEPHONE RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-212	90-135V	—	NONE	Clare	$0.95
R-213	5-8V	—	DPST (NO)	Clare	1.50
R-605	24V	—	3PST (NO)	Auto. Elec.	.95
R-606	24V	—	DPST (1NO-1NC)	Auto. Elec.	.95
R-607	24V	—	SPST (NO)	Auto. Elec.	.95



DIRECT CURRENT MIDGET RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-132	24V	300	DPDT	Clare	$1.20
R-133	24V	300	NONE	Clare	.60
R-134	24V	250	4PDT	Clare	1.20
R-135	24V	300	SPST (NC)	Clare	1.15
R-137	24V	300	SPDT	Clare	1.15
R-138	24V	300	4PST (NO)	Clare	1.15
R-139	24V	200	4PDT	Clare	1.15
R-140	24V	280	SPDT	R.B.M.	1.15
R-141	24V	280	3PST (NO)	R.B.M.	1.15
R-142	24V	400	DPDT	Allied Cont.	1.20
R-143	24V	280	SPST (NO)	R.B.M.	1.15
R-144	24V	250	SPST (NO)	Allied Cont.	1.15
R-145	24V	300	DPST (NO)	Allied Cont.	1.15
R-146	12V	126	DPST (1NO) (1NC)	Clare	1.10
R-147	9-14V	75	SPDT	Guardian	1.05
R-148	12V	100	DPDT-SPST (NC)	Price Bros.	1.10
R-149	6-8V	45	SPST (NC)	Clare	1.00
R-150	6V	30	SPST (NO)	E-Z Elec.	.95
R-522	2-6V	2.	SPST (NO)	R.B.M.	.65
R-523	90-125V	6500	DPDT	Clare	1.90
R-222	12V	100	DPST (NO)	P & B	.95
H-242	24-32V	300	DPDT	R.B.M.	1.20
H-243	24-32V	300	4PDT	R.B.M.	1.20



SENSITIVE DC RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-218	4-6V	1800.	SPDT	Kurman 220C	$1.95
R-220	75V	5000	SPDT	Allied Cont.	1.20
R-221	18-24V	5000	SPST (NO)	Allied Cont.	1.15
R-174	250V	5000	DPST (NO)	G.M.	1.85
R-175	350V	11000	DPDT-DPST (NO)	G.M.	2.95
R-176	24V	250	DPST (NO)	G.M.	1.50
R-177	24V	300	4PDT	G.M.	1.65
R-600	8-12V	5000	SPDT	S-Dunn-KS	2.10
R-507	24-48V	1000	SPDT-DPST (NC)	Guardian	1.15

TYPE BO DC RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-169	24V	250	SPST (NO)	Allied Cont	$1.95
R-171	24V	230	DPDT	Allied Cont.	2.15
R-172	5-8V	30	DPDT-SPST (NO)	Allied Cont.	1.70
R-173	2-6V	5	SPST (NO)	Allied Cont.	1.25
R-529	24-48V	1000	DPDT	Allied Cont.	2.50

TYPE BJ DC RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-204	12V	65	DPST (NO)	Allied Cont.	$1.15
R-205	24V	260	DPDT	Allied Cont.	1.25
R-224	12V	75	SPST (NO)	Allied Cont.	1.15
H-237	27V	230	DPDT	Allied Cont.	1.25

HEAVY DUTY KEYING RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-248	28V DC	150	SPST (NO) 10A.	Guard. 36471	$1.05
R-244	25V AC	265	SPST (NO) 20A.	Leach 1327	1.75
R 206	24V DC	150	5POT-3 AMP.	P&B-KL	1.20
R-207	24V DC	210	4POT-3 AMP.	P&B-KL	1.10
R-219	50V DC	1500	DPST (NO) 15A.	P&B-SP	1.25
R-217	115 AC	600	SPOT-10 AMP.	St. Dunn 1XAX	2.25
R-525	24V DC	200	DPDT-10 AMP.	Guard. 34464	1.25
R-508	110 AC	600	SPDT-6 AMP.	Guard. 37189	1.95
R-506	24 V DC	300	DPST (NO) 6A.	—	.95
R-510	24 V DC	200	3PDT-10 AMP.	Guard 516983	1.05
R-604	24 V DC	200	SPST (NO) 30A.	St. Dunn-B2A	1.25
H-608	115 AC	—	SPST (NO) 20A.	St. Dunn-1HXX	2.25
R-620	12V DC	35	3PST (NO) 10A.	Guard-BK2	1.05
R-223	28V DC	150	SPST (NO) 40A	Price Bros.	1.35
H-230	12-24V DC	80.	DPST (NO) 10A.	—	1.20
H-231	24V	230.	DPST (NO) 5A.	R.B.M.	1.15

DC-TYPE 76 ROTARY RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-197	9-16V	70	DPDT	Price Bros.	$1.65
R-198	9-16V	125	6PST (3NO) (3NC) SPDT	Price Bros.	1.65
R-199	24-32V	250	SPDT-DPST (NC)	Price Bros.	1.65
R-200	24-32V	275	3PDT-SPST (NC)	Price Bros.	1.65
R-201	24-32V	250	DPST (NO) SPDT (NC) DPDT	Price Bros.	1.65
R-601	9-14V	60.	3PST (NO)	Price Bros.	1.65

DIRECT CURRENT KEYING RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-190	12V	65	DPDT 10 AMP	Advance Elec. Type 2000-A	$1.15
R-191	28V	125	DPDT 10 AMP	Guardian	1.20
R-192	12V	44	3PDT 10 AMP	Allied Cont. Type NB5	1.35
R-193	5-8V	11	DPDT 10 AMP SPST (NO)	Leach Type 1027	1.05
R-194	24V	265	DPST (NO) 10 AMP	Leach Type 1054SNW	1.25
R-195	6V	32	DPDT 3 AMP	G.E.Co.	1.15
R-196	12V	50	DPDT 10 AMP SPST (NC)	Guardian	1.15
R-242	24V	170	SPDT 2 AMP	Leach Type 1253DEW	1.25
H-236	5-8V	18.5	SPDT 10 AMP	Leach-BFM	1.05

CUTLER HAMMER HEAVY DUTY CONTACTORS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-178	24V DC	100	SPST (NO) 100A.	6141H34A	$3.85
R-179	6V DC	6.5	SPST (NO) 50A.	6041H83A	3.00
R-180	12V DC	25.	SPST (NO) 50A.	604H308	3.25
R-181	24V DC	65	SPST (NO) 100A.	6041H8B	3.85
H-232	24V	55.	SPST (NO) 50A.	Metal Cased	3.25
H-233	6V	15	SPST (NO) 50A.	Metal Cased	3.15
H-235	24V	70.	SPST (NO) 100A.	Type B6	3.85

DIRECT CURRENT AIRCRAFT CONTACTORS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-182	28V	80	SPST (NO) 25 A.	Guardian	$1.85
R-183	24V	60	SPST (NO) 50 A.	Allen Bradley Type B6A	2.75
R-184	28V	50	SPST (NO) 100A.	General Elec.	2.95
R-185	24V	100	SPST (NO) 50 A.	Leach 5055ECR	2.75
R-186	24V	132	SPST (NO) 50 A.	Leach 7220-3-243	3.50
R-187	24V	100	SPST (NO) 50 A.	Allen Bradley	2.95
R-188	24V	200	SPST (NO) 75 A.	Allied Cont.	2.95
H-234	14V	45	SPST (NO) 30 A.	—	1.65

ANTENNA CHANGEOVER RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-192	6-12V DC	44	2POT 10 AMP	Allied-NB5	$1.35
R-231	12VDC	100.	DPDT 6 AMP	G. E.	1.95
R-256	24-32V DC	—	SPDT-DPST (NC) 1KW	Guardian	1.45
R-501	110 AC	4.	DPDT (1KW)	G. E.	2.45
R-503	12-32V DC	100	SPDT-5PST	G. E.-500 W.	1.95

COMBINATION PUSH BUTTON AND REMOTE RELAY

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
H-244	12-24 V DC	Dual-60	SPDT	CR2791-R106C8	$1.65

ADJUSTABLE TIME DELAY RELAY

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-246	115 AC	—	SPST (NO) or (NC) 10 AMPS	R. W. Cramer 1-120 Sec.	$8.95

DC MECHANICAL ACTION RELAYS

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-245	12V	25.	4" Lever	G.M.	$0.95
R-527	6-12V	200.	2" Lever	—	.95

TYPE C.M.S. RELAY

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-511	24V DC	200	MICRO-SW. SPST (NO)	Clare	$2.45

DC CURRENT REGULATOR

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-509	6-12V DC	40	SPST (NC)	G. E.	$0.85

LATCH AND RESET RELAY

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-500	12V DC	10.	DPDT-10 AMP	SI. Dunn-CX-3190B	$2.85

DC-ROTARY STEP RELAY

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-621	6-12V	30.	3 POLE 23 POSITION	W. E.	$10.95

DC-RACHET RELAY

Stock No.	Operating Voltage	Coil Resistance	Contacts	Manufacturer	Net Each
R-230	5-8V	2.	SPDT-DPST (NO)	Guardian	$2.15

Special Sample Engineering Offer

Any ten relays listed (one of each type) with the exception of Stock Nos. R-621 and R-246—only $10.00.

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3" Shield $1.47
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1000 KC Crystal $2.97
Socket ..... .07

SELENIUM RECTIFIERS

Full Wave Bridge Type

INPUT		OUTPUT		
up to 18v AC	up to	12v DC	½ Amp.	$1.47
up to 18v AC	up to	12v DC	1 Amp.	1.97
up to 18v AC	up to	12v DC	5 Amp.	5.27
up to 18v AC	up to	12v DC	10 Amp.	8.97
up to 18v AC	up to	12v DC	15 Amp.	11.57
up to 18v AC	up to	12v DC	30 Amp.	22.57
up to 36v AC	up to	28v DC	1 Amp.	3.47
up to 36v AC	up to	28v DC	5 Amp.	8.57
up to 36v AC	up to	28v DC	10 Amp.	14.57
up to 36v AC	up to	28v DC	15 Amp.	22.27
up to 115v AC	up to	100v DC	.25 Amp.	2.57
up to 115v AC	up to	100v DC	.6 Amp.	5.27
up to 115v AC	up to	100v DC	5 Amp.	22.57
up to 115v AC	up to	100v DC	3 Amp.	17.97

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NATIONALLY ADVERTISED BRANDS
All Ratings D. C.

2x.1mfd.	600v	$0.37	1mfd.	2000v	$0.97
.25mfd.	600v	.37	2mfd.	2000v	1.77
.5mfd.	600v	.37	4mfd.	2000v	3.77
1mfd.	600v	.37	15mfd.	2000v	4.97
2mfd.	600v	.37	4mfd.	2500v	3.97
4mfd.	600v	.57	2mfd.	2500v	2.47
8mfd.	600v	1.07	.1mfd.	2500v	1.27
10mfd.	600v	1.17	25mfd.	2500v	1.47
3x.1mfd.	1000v	.47	.5mfd.	2500v	1.77
.25mfd.	1000v	.47	.05mfd.	3000v	1.97
1mfd.	1000v	.57	.1mfd.	3000v	2.27
2mfd.	1000v	.67	.25mfd.	3000v	2.67
4mfd.	1000v	.87	1mfd.	3000v	3.47
8mfd.	1000v	1.97	12mfd.	3000v	6.97
10mfd.	1000v	2.07	2mfd.	4000v	5.97
15mfd.	1000v	2.27	1mfd.	5000v	4.97
20mfd.	1000v	2.97	.1mfd.	7000v	2.97
24mfd.	1500v	6.97	3mfd.	4000v	6.97
.1mfd.	1750v	.87	2mfd.	3000v	3.47
.1mfd.	2000v	.97	2x.1mfd.	7000v	3.27
.25mfd.	2000v	1.07	.02mfd.	12000v	9.97
.5mfd.	2000v	1.17	.02mfd.	20000v	11.97

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10,000 mfd.—25 WVDC	$6.97
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1000 mfd.—15 WVDC	.97
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4000 mfd.—18 WVDC	1.97
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TWO-SPEED PLANETARY DRIVE

Auxiliary Speed Reducer fits on Condenser Shaft back of panel or on dial knob shafts. Ratios 5 to 1 and 1 to 1. Fits any ¼ inch round shaft.

57c Each—Two for 97c

BC—223 TRANSMITTER TUNING UNITS

TU-17 Frequency 2000 KC to 3000 KC
TU-18 Frequency 3000 KC to 4500 KC
TU-25 Frequency 3500 KC to 5250 KC
Price—NEW **$3.97**

TEST PROBE

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For high-frequency work and to eliminate stray pickup for use with Oscilloscope. AMPHENOL # 93M COAX. Connector on one end. Part of Dumont 224A Oscillograph.
Special **$2.47**

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NEW! STANDARD BRANDS!

1 24	$4.87	802	$2.97	OZ4	$ .67
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1N21	.67	807	1.07	1L4	.67
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2C21	.27	812	2.47	1LN5	.67
2C22	.17	813	6.47	1N5GT	.57
2C26A	.27	814	2.67	1R5	.67
2C34	.27	815	1.87	1S4	.67
2C40	6.57	816	1.07	1S5	.57
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2J48	19.97	837	1.27	5T4	.97
2J54B	39.97	838	2.87	5U4G	.47
2K25	32.97	841	.37	5V4	.87
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2V3G	.97	845	4.17	5X4	.57
2X2	.37	851	24.97	5Y3	.37
3AP1	3.97	860	1.87	5Y4	.47
3B22	2.97	861	10.47	5Z3	.47
3B24	1.87	862A	497.47	5Z4	.77
3B26	1.47	864	.47	6A7	.67
3BP1	1.37	865	.97	6A8GT	.67
3CP1	2.67	866A	1.17	6AB7	.77
3C21	3.97	866JR	1.17	6AC7	.77
3C23	2.47	869B	27.57	6AG5	.87
3C24/24G	.57	872A	1.47	6AG7	1.17
3C30	.37	874	.57	6AJ5	.87
3C31	1.47	876	.67	6AK5	.87
3D21A	1.47	878	1.27	6AK6	.87
3DP1	1.97	884	1.27	6AL5	.67
3E29	8.97	885	1.27	6AQ5	.67
3GP1	4.97	902P1	4.97	6AQ6	.67
4API0	2.97	905	1.87	6AT6	.47
4B24	2.27	923	.87	6AU6	.77
4E27	12.97	954	.27	6B4G	.97
5AP4	3.97	955	.37	6BG6G	1.97
5BP1	1.87	956	.37	6BE6	.67
5BP4	2.97	957	.27	6B8	.87
5CP1	1.97	958A	.27	6C4	.27
5CP1A	8.97	1613	.57	6C5	.47
5D21	34.97	1616	.87	6C8	.57
5FP7	1.37	1619	.27	6D6	.47
5JP2	39.97	1624	.77	6F6	.57
5LP1	13.97	1625	.37	6F7	.97
5NP1	8.97	1626	.37	6G6	.77
5R4GY	1.17	1629	.27	6H6	.47
6C21	24.97	1630	1.87	6J5	.47
6J4	5.87	1636	3.97	6J6	.87
9GP7	9.97	1638	1.47	6J7	.67
9JP1	3.57	1641	.57	6K6	.47
9LP7	3.57	1654	1.97	6K7	.57
10Y	.37	1851	.97	6L6	1.17
12DP7	12.97	1960	2.97	6L6G	.97
12GP7	12.97	2050	.67	6L7	.87
15E	1.97	2051	.47	6N7	.77
15R	.77	8011	1.27	6Q7	.67
28D7	.37	8012A	1.47	6SA7	.47
30 Spec.	.27	8013A	1.27	6SC7	.67
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75TL	2.87	8020	1.47	6SG7	.67
100R	1.47	8025	3.57	6SH7	.47
100TH	9.97	9001	.37	6SJ7	.47
211	.47	9002	.37	6SK7	.47
227A	2.97	9003	.37	6SL7	.57
249C	2.57	9004	.37	6SN7	.57
250R	9.97	9006	.27	6SQ7	.47
250TH	19.47	C6J	3.97	6V6GT	.67
250TL	19.47	CK507AX	1.47	6X5GT	.57
294A	4.97	CK1005	.27	6ZY5G	.87
304TH	3.47	CK1090	1.27	12A6	.17
304TL	1.47	E1148	.67	12AT6	.57
305A	12.47	EF50	.47	12AU6GT	.57
307A	3.97	F123A	14.97	12C8	.37
316A	.67	F127A	17.97	12J5GT	.37
327A	2.97	F128A	39.47	12SA7GT	.57
350B	1.47	F660	39.47	12SK7GT	.57
368AS	3.27	F862A	497.47	12SQ7GT	.57
371B	.97	FG17	2.87	12SH7GT	.57
378A	1.97	FG81A	3.97	12SL7GT	.67
434A	3.27	FG95	8.97	12SQ7GT	.57
446A	.67	FG105	9.97	12SR7GT	.57
450TH	18.47	GL697	29.47	14A7	.87
451	1.47	HY69	3.97	14Q7	.57
530	22.57	HY615	.37	24A	.67
531	4.97	ML100	19.97	25L6GT	.57
532	2.87	ML101	49.47	25Z5	.47
559	.87	ML502	69.47	27	.47
575A	12.97	RK59	1.97	35/51	.57
703A	3.27	RK60	.57	35L6GT	.57
705A	1.97	RK72	.67	35Z3	.57
706CY	18.97	RK73	.97	35Z5	.47
707B	8.47	RK75	3.97	45	.57
708A	1.97	RK705	1.97	50B5	.67
713A	1.27	RX21	3.27	50L6GT	.57
715B	7.57	RX120	9.97	56	.47
715C	34.97	S836	2.97	76	.47
717A	.67	VR75	.97	77	.47
721A	2.97	VR78	.37	78	.47
723AB	12.97	VR90	.67	80	.47
725A	12.87	VR105	.67	83	.77
726A	7.57	VR150	.57	84/6Z4	.67
750TL	44.97	VT127A	2.37	117Z3	.57
800	1.87	VU111	.37	117Z6GT	.87
801A	.27				

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TRANSFORMER—115 V. 60 Cy.
HI-VOLTAGE INSULATION

2500v @ 15 ma	$4.97
2150v @ 15 ma	3.97
2100v @ 10 ma	4.87
1800v @ 10 ma; 6.3v @ 2A; 2.5v @ 2A	4.97
1750v @ 4 ma; 6.3v @ 3A	4.27
1600v @ 4 Ma.; 700v CT @ 150 ma; 6.3v @ 9A	6.47
525-0-525v @ 60 ma.; 925v @ 10 ma.; 2x5v @ 3A; 6.3v @ 3.6A; 6.3v @ 2A; 6.3v @ 1A	6.97
500-0-500v @ 25 ma.; 262-0-262v @ 55 ma.; 6.3v @ 1A; 2x5v @ 2A	4.47
335-0-335v @ 70 ma.; 2.5v @ 10A; 5v @ 6A; 5v @ 3A	4.97
450-0-450v @ 300 ma.; 140-0-140v @ 100 ma.; 36v @ 1A, 6.3v @ 5A, 5v @ 3A, 110/220 Dua. Pri	7.97
400-315-0-100-315v @ 200 ma.; 2.5v @ 2A; 5v @ 3A; 6.3v @ 9A; 6.3v; 9A.	5.97
385-0-385-550v @ 200 ma.; 2½v @ 2A; 5v @ 3A; 3x6.3v @ 6A—PRI. 110/220	6.27
340-0-340v @ 300 ma.; 1540v @ 5 ma.	4.97
300-0-300v @ 65 ma.; 2x5v @ 2A; 6.3v @ 2½A; 6.3v @ 1A	3.47
150-0-150v @ 80 ma.; 150v @ 40 ma.; 6.3v @ 3.6A; 6.3v @ 1A	1.97
120-0-120v @ 50 ma	.97
80-0-80v @ 225 ma.; 5v @ 2A; 5v @ 4A	3.97
24v @ 6A	3.47
18v @ 15A	9.97
13.5v CT @ 3.25A	2.97
3x10.3v @ 7A; CT	7.97
6.3v @ 12A; 6.3v @ 2A; 115v @ 1A	3.47
6.3v @ 10A; 6.3v @ .6	2.97
6.3v CT @ 3.5A; 2.5v CT @ 3A; 2.5v CT @ 3A	2.97
6.3v @ 1A; 2½v @ 2A	2.47
6.3v @ 21½A; 6.3v @ 2A; 2½v @ 2A	4.97
6.3v @ 1A....$0.97 8v CT 1A	.97
2.5v @ 20A	3.47
5v @ 3A; 2.5v @ 2A	2.97
5v @ 20A, Dual 110v Pri	3.47

FILTER CHOKES
HI-VOLTAGE INSULATION

8 hy @ 300 ma	$3.97	1 hy @ 800 ma	$14.97
25 hy @ 160 ma	3.47	10 hy @ 250 ma	2.47
12 hy @ 150 ma	3.27	10 hy @ 200 ma	1.97
25 hy @ 65 ma	1.37	10/20 @ 85 ma	1.57
.05 hy @ 15 amps.	7.97	15 hy @ 125 ma	1.47
1 hy @ 5 amps	6.97	15 hy @ 100 ma	1.37
4 hy @ 600 ma	5.97	3 hy @ 50 ma	.27
200 hy @ 10 ma	3.47	30 hy Dual @ 20 ma.	1.47
600 hy @ 3 ma	3.47	8/30 hy @ 250 ma.	3.47
325 hy @ 3 ma	3.47		

UHF 83 SERIES CONNECTORS
UHF—Small—Coaxial

Amphenol No.	Army or AN No.	Description	
83-1SP	PL-259	Plug	37¢
83-168	UG-176/U	Reducing Adapter. Use with 83-1SP or 83-1SPN	17¢
83-1R	SO-239	Receptacle	37¢
83-1T	M-358	T Connector	117¢
83-1AP	M-359	Angle Plug Adapter	27¢
83-1J	PL-258	Junction	77¢
83-1F	PL-274	Feed-thru Pressurized	87¢

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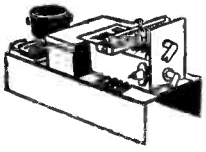
GUARANTEED GOVT SURPLUS

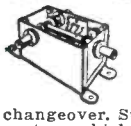


420—750 MC OSCILLATOR.

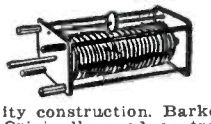
Compact, beautifully built line oscillator employing two W.E. 368AS (703A) "doorknob" tubes in push-pull. Exceptionally stable. 5W output at 420mc, 2W at 700mc. Independent grid and plate tuning. Adjustable output coupling and tuning assembly. Coaxial output connection. Built-in blower may be operated from 110VAC. Power requirements: 300VDC/150ma, 1.2V/4A, 1.2V/4A. 5¼"x6½"x11½". 7 lb. Supplied complete with tubes. Ideal for 420mc amateur operation or for use in the 460-470mc citizens radio band. **Stock No. APO-66...$6.95**
Spare 368AS/703A tubes.....**$1.69 ea.**

UHF 50 OHM COAXIAL POWER MEASURING ASSEMBLY. Panel mounting, silver-plated assembly with integrally coupled crystal mount. Type "N" UG-58U female receptacle (easily replaced by SO-239). Originally designed for power measurement at frequencies up to 700mc. **Stock No. APM-89**.....**$3.95**
MATING TYPE "N" MALE PLUG. For use with above. **Stock No. PCM-17**.....**$0.49**

SPERRY MODEL 12 KLYSTRON TUNER for use with 2K39, 2K42, 2K43, 2K44, 417A. **Stock No. VKT-27**.....**$1.95**
MAGNETRON MAGNET 1900 GAUSS. Pole dia. 1-⅝. Gap 1½". **Stock No. UMM-21**.....**$5.75**
MAGNETRON MAGNET 4800 GAUSS. Pole tip dia. ¾". Gap 0.635". **Stock No. UMM-48**.....**$7.00**



50 OHM COAXIAL RELAY. Double coil actuating relay operates from either 12VDC/120ma or 24VDC/60ma. May be operated in plate return circuits to provide automatic transmitter-receiver antenna changeover. Supplied with British type connectors which are easily replaced by standard SO-239 (83-1R) receptacles or soldered to directly. Completely enclosed in compact housing. 2-¾" x 3" x 4-¾". An outstanding buy at **$2.49. Stock No. KDC-723.**



VARIABLE INDUCTOR. 67 microhenries max. Minimum near zero. Wheel type sliding short. Ceramic insulation. Quality construction. Barker-Williamson #1565. Originally used as transmitter plate tank coil to tune from 1½ to 20mc. Ideal for pi-networks, antenna tuners and plate tanks. **Stock No. LRF-32**.....**$1.95**

APC AIR TRIMMER. 35 mmf max. Screw slot adjustment. **STOCK NO. CAV-105. 10 for $1.00**

APC AIR TRIMMER. Two separate trimmers on ceramic base. Shield between sections. Each section 25 mmf max. **Stock No. CAV-104**.....**10 for $1.00**
AIR CAPACITOR 100 MMF MAX. ¼" dia. shaft. Receiving type. Ceramic insulation. Standard Brand. Similar to MC-100-M. Straight-line capacity. **Stock No. CAV-15 $0.72**

SUPER-FLEXIBLE PIGTAIL WIRE. Sperry Special. Part No. P55357. Consists of 350 strands of 0.002" diameter soft copper wire. Total diameter: 1/32". Useful in applications where electrical connection is to be made to moving parts, e.g., variometers, variable capacitors, motor-brushes, etc. **Stock No. WFP-350. 10 foot rolls. $0.69 per roll.**

750 CPS BANDPASS TRANSFORMER. Center frequency adjustable over a small range. Input 23,000 ohms. Output 225,000 ohms. Triple alloy shielded. 1½" x1½"x2". **Stock No. ZBP-750 $2.49**

BLOCKING OSCILLATOR TRANSFORMER. Two winding 1.35:1. Ideal for television sweep oscillators. Compact. **Stock No. TFF-64**.....**$0.95**

NON-INDUCTIVE CERAMIC RESISTOR. 350 ohms/24 watt. Standard Brand. **Stock No. RCF-52**.....**8 for $1.00**

Tube Specials

1A7GT	$0.72	6Q7	.72	215A	.95
1G6GT	.49	6SA7GT	.60	304TH	7.75
1V	.49	6SC7	.69	304TL	1.95
2A3	.98	6SF7	.72	316A	.89
2C4	.95	6SH7GT	.39	350A	2.95
2C21/1642	.29	6SJ7	.59	417A	14.95
2C34/RK34	.29	6SJ7GT	.49	559	1.19
2C40	1.98	6SK7	.72	705A	2.95
2C44	.75	6SL7GT	.69	723A/B	9.95
2D21	1.49	6SN7GT	.79	725A	14.95
2J26	14.95	6SR7	.67	730A	12.50
2J38	14.95	6SU7GT/Y	1.29	801	.79
2J48	15.95	6V6GT	.79	803	8.95
2J55	39.75	6V6	1.09	805	3.95
2K28	12.95	6X4	.69	807	1.19
2X2	.69	6X5GT	.63	811	1.95
3B7/1291	.39	6Y6G	.88	813	7.95
3C23	2.95	6ZY5G	.81	814	3.95
3D21A	1.95	7C7	.81	815	1.95
3E29	3.49	7E6	.72	836	.89
3FP7	1.95	7G7	1.06	837	1.49
3Q4	.69	7H7	.72	861	15.00
4A1	.49	7Q7	.72	866A	.95
5BP1	1.95	7V7	.72	872A	1.69
5CP1	1.95	7Y4	.72	874	.59
5R4GY	1.09	7Z4	.72	902A	3.95
5U4G	.65	12SF7	.59	931A	3.95
5V4G	1.09	12SG7	.59	954	.39
5Y3GT/G	.49	12SH7	.59	955	.39
6AC7	.79	12SJ7	.59	956	.49
6AE5GT	.79	12SL7GT	.79	957	.39
6AG7	1.29	12SQ7	.65	958A	.39
6AK5	1.29	12SR7	.72	959	.39
6AU6	.95	14F7	.72	991/NE-16	.29
6C4	.49	14H7	.79	1625	.49
6C8G	.72	14N7	.72	1626	.39
6F6	.89	RK21	.95	1629	.29
6F8G	.89	25Z5	.59	1641/RK60	.95
6G6G	.49	25Z6GT	.59	2050	.79
6H6	.49	35W4	.49	8013	1.49
6H6GT/G	.29	46	.72	9001	.39
6J5	.57	EF50	.49	9002	.39
6J6	1.15	RK69	1.49	9003	.39
6J7	.69	RKR72	1.49	9004	.39
6K6GT/G	.65	RKR73	.39	9005	.79
6K8	.88	80	.45	9006	.39
6L6	1.28	85	.72	VR90	.69
6L6GA	.89	89Y	.54	VR105	.69
6L7	.98	117Z6GT/G	.88	VR150	.59
6N7	.95	FG178	1.95		
6N7GT	.79	211	.69		

OIL—FILLED CAPACITORS

Mfd	Rating	Price	Mfd	Rating	Price
2-2	600 VDC	$0.75	0.1	5000 VDC	$1.95
4	600 VDC	.84	2	5000 VDC	7.30
7	600 VDC	1.15	1	6000 VDC	6.95
10	600 VDC	1.37	.1-.1	7000 VDC	1.95
50	330 VAC	4.95	.05	7500 VDC	1.75
2	1000 VDC	.95	2½	7500 VDC	11.95
4	1000 VDC	1.19	.02	10 KV DC	2.95
8	1000 VDC	1.71	1	15 KV DC	19.95
0.25	2500 VDC	1.06	0.25	20 KV DC	15.95
2	4000 VDC	4.95	15	440 VAC	
3	4000 VDC	5.95		1500 VDC	2.95

Note: 10 or more capacitors of a type 10% dis.

RF and DC PANEL METERS

Stock	Description	Price
MAD-251	0-2 ma DC Westinghouse 3½" round	$3.95
MAD-262	0-20 ma DC Westinghouse 3½" round	3.95
MAD-265	0-80 ma DC W.E. 3½" round	3.49
MAD-503	0-1000 ma DC DeJur 3½" round	3.95
MAD-276	0-30 ADC GE 2½" round	2.95
MRT-355	0-100 ma RF Weston 425 3½" round	11.95
MRT-372	0-120 ma RF Weston 507 2½" round	8.95
MRT-367	0-1A RF GE 2½" round	2.95
MRT-394	0-20A RF GE 3½" round	6.95

INVERTER PE 218D. Output 115V/400 cps/1500VA/1ph. Input 24-28 VDC. Made by Wincharger. Complete with starting relays, hash filters, voltage and speed regulators. 5½"x11"x15". Brand new in original packing. **Stock No. GAC-10..$27.50**

Delivery: Immed. from stock (subj. to prior sale).
Minimum Order: $5.00.
Terms: Rated organizations (U. S. and Canada). Open account.
Others: Cash with order, or 20% with order, balance C. O. D.
Foreign: Payment in U. S. funds with order or irrevocable letter of credit payable against documents in U. S. funds at New York.
Condition of material: The major portion of the material listed above is brand new. Some of the items have been removed from new equipments. We guarantee material to be clean and in perfect operating condition.
All prices above are quoted domestic packed f.o.b. our warehouse, Corona, New York.

Wide Range Butterfly Wavemeter & Oscillator Elements

Precision wide range butterfly circuit elements. Sturdily constructed. Mounted in ball bearings. Suitable for motor drive. Ideal for use as wavemeters and oscillators (see description below).

Stock No.	Freq. (mc.)	Notes*	Unit Price
TN-20	105-330	1, 3	$2.95
TN2A	75-300	1, 4	2.95
TN-30	135-485	2, 3	3.95
TN3A	300-1000	2, 5	4.95

Brand new, in original packing.

*NOTES: 1) Aluminum construction
2) Silver-plated brass
3) Designed as oscillator element (955 acorn triode)
4) Has diode socket mounted on unit (955 as diode)
5) Has crystal diode mount for 1N21 crystal

BLILEY SMC-100 100 AND 1000KC CRYSTAL. Regularly sells for $8.75. **Stock No. QCM-19**.....**$5.95**

HAMMARLUND CERAMIC ACORN SOCKETS. 5 contact. Silver-Plated. **Stock No. XRT-25**.....**20 for $1.00**

CINCH MICA FILLED OCTAL SOCKETS. 1" dia. 1-5/16" mtg ctrs. **Stock No. XRT-20. 20 for $1.00**
1-⅛ dia. 1½ mtg. ctrs. **Stock No. XRT-40. 20 for $1.00**

DELAY LINE. 2 microsecond (one direction). 1500 ohms. Bandwidth 1mc. 8 section tapped. **Stock No. ZAL-22**.....**$1.69**
DELAY LINE. 1¼ microsecond (one direction). 1500 ohms. Bandwidth 1mc. 6 section tapped. **Stock No. ZAL-13 $1.49**
DELAY LINE. 5 microsecond (one direction). 1500 ohms. Bandwidth ½mc. **Stock No. ZAL-14**.....**$0.89**

4200 VOLT TELEVISION OR SCOPE TRANSFORMER. Primary: 115V/60c. Secondary: 3000VRMS (4200 Volts Peak) 10ma. Hermetically sealed. 4½"x4-¾"x5½". **Stock No. TFF-83**.....**$5.95**

HV TFMR. 10,000-0-10,000 VOLTS @42 MA. Oil-filled, hermetically sealed. 11"x13" x6". Pri. 115V/50-60cy. **Stock No. TFF-451 $29.95**

FILTER CHOKES

Stock No.	Description	Price
LFF-45	10H/120ma/600 ohms	$0.95
LFF-21	20H/300ma/125 ohms/5000V	9.95
LFF-144	2½H/700ma/16 ohms/1500V	4.95

MULTIPLIER PHOTOTUBE HOUSING. Cast aluminum cylindrical housing containing a submagnal 11 pin socket (for 931A, 1P21, 1P22) and a dynode voltage divider network. Moisture proof construction. An integral 6 volt pilot lamp provides light source when used as a noise generator. A window may be drilled in the housing for use with an external light source. Operates with approximately 700 volts at 3-4ma. 2" dia. x 4" long. Supplied less phototube. **Stock No. AMP-65**.....**$3.95**

PRECISION HIGH TORQUE TYPE 5 SELSYNS. Bronze housing 4½" dia. x 5" long. 115V/60c operation. Brand new in original packing. **Stock No. SEL-44**.....**$4.95 each**

110/60CPS/0.38A BLOWER. Exceptionally quiet. 50 cu. ft. min. **Stock No. BLR-344..$8.95**

3" SCOPE INDICATOR. 3BP1 cathode ray tube mounted in a mu-metal housing with an adjustable light shield. May be mounted on a panel, tabletop or clamped to a bar. When mounted on a table top or wall, the scope housing may be tilted at any angle up to 45° from the mount for comfortable viewing. Ideal for remote scope indicators. An outstanding buy at **$5.95.** Stock No. **ASI-35.**

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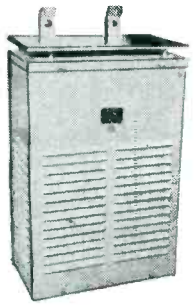

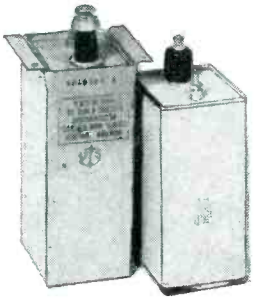

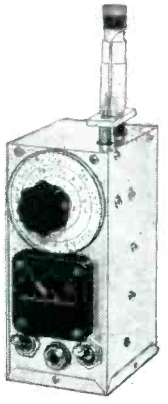

VOLTAGE REGULATOR

Raytheon CRP-301407. Prim. 92-138v, 57/63 cps. Sec. 115v .82 kva 1% reg., .96 PF. Regulating trans., chokes, capacitors, power correct. In navy gray cabinet, 36" x 20" x 12", net wt. 250 lbs.

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Complete at $29.50

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2 mf 6000 vdc	6.50
1 mf 7500 vdc	5.50
1 mf 5000 vdc 5009	3.95

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An all-around laboratory instrument for measurement of resonant circuits, Q, rf voltages, antennas and many other purposes—3 mc to 250 mc or other extended ranges. Compact and complete in kit form at $21.50 with instruction and application booklet.

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3700–0–3700v @ 500 ma	$59.00
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1800–0–1800v @ 350 ma	17.50
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230/460 to 115v @ 2 kva	28.00
440v to 115v @ 50 kva	150.00
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11.5v @ 11.5–20 amp	3.50
10v @ 6 amp	2.75
2.5v @ 10A, 10 kv	3.75
4500v @ 4.5 ma; 5v @ 3A	6.75
3750v @ 2 ma	4.50
1200v @ 2 ma, 6.3v @ 4A, 5v @ 3A	3.95
1300vct @ 160–200 ma, 5v @ 2–3A, 2–2.5v @ 2A	5.50
1100vct @ 200 ma, 6.3 @ 4A, 6.3 @ 4A, 5 @ 3A	7.50
830vct @ 125 ma, 6.3 @ 6A, 5 @ 3A	3.95
850vct @ 150 ma	2.50
750vct @ 300 ma	3.50
78v @ 1.34 amp	2.50

230V 50/60 CPS

3000v @ 800 ma 3 ph	32.50
700–0–700 @ 350 ma	5.70
5.0v @ 30 amp	6.50
6.3v @ 2.7 amp	1.50

OIL CAPACITORS

2 mf 600 vdc	$0.35
4 mf 600 vdc 609 etc	0.60
6 mf 600 vdc	0.75
7 mf 600 vdc, rect	0.75
10 mf 600 vdc A1000	1.15
2 mf 1000 vdc 1009	.70
4 mf 1000 vdc 23F252	.95
10 mf 1000 vdc 22F47	1.95
4 mf 1500 vdc TJU	1.85
2 mf 2000 vdc 23F161	1.95
1 mf 3600 vdc 8412	3.10
0.15 mf 4000 vdc 26F386	2.10
.25 mf 4000 vdc 26F767	2.85
.1 mf 7000 vdc B8B1170	1.95
.005–.01 mf 12 kv 25F646	4.75
.02 mf 20 kv BT-15G	5.95

VARIABLE CAPACITORS

10 mmf midget Card. ZR10AS	$.50
15 mmf midget BUD MC-1850	.45
15 mmf midget Card. ZR15AS	.50
25 mmf midget double sp	.55
3–18 mmf micro-dual, dbl sp	1.15
2–2.8 mmf dual neut. Card	.40
250 mmf Trans. Jr Bud JC1528	.85
240 mmf dual .1 gap Card. XE240XD	4.35
190 mmf dual .05 gap Card. MO180BD	1.95
260 mmf dual .03 gap Card. MR260BD	1.35

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Capacity	Wkg Volts	Price
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560	5,000	.75
375	5,000	.75
.001	4,500	1.10
.002	3,500	.95
.003	3,000	.95
700	3,000	.60
500	3,000	.70
400	3,000	.55
200	3,000	.70
100	3,000	.55
90	3,000	.50
50	3,000	.50
.025	2,500	1.10
.006	2,500	.70
30	2,000	.45
.015	1,500	.75
.12	500	1.15

Type H, A2, #4, 9

.002	3500 #9	$.60
.005	2500 #4	.45
400	2500 #9	.30
350	2500 #9	.35
.002	1000 #4	.25

Ceramicons

50 mmf Feedthru	$.06
50 mmf 7,500 vdc	.30

WIRE

#20 HV str. white plastic	$4.95/M
#20 str. white lacquer	3.50/M
#20 str. red lacquer	3.50/M
#20 str. green lacquer	3.50/M
3/16" magnet, DCC, rect	.35/lb
#30 SSE magnet	.60/lb
1/4" tin shield braid	.30/lb

METERS

DC Milliammeters

0–30 ma Gruen 2½" rd	$2.00
0–15 ma G.E. 3½" rd	3.50
0–500 ma Elec. rd	3.50
0–800 ma G.E. 3½" rd	4.50
AC Voltmeter	
0–150v Simp. 4½" sq. flush	$5.50
RF Ammeter	
0–2.5A, McClin. 3½" rd	$3.95

WIRE WOUND RESISTORS

5 Watt—200–600–10,000 ohms	$.07
10 Watt—1–42–50–80–150–350–750–1000–4500–5000–9000–10,000–25,000–39,000–75,000 ohms	.12
25 Watt—2.5–12.6–50–100–500–650–1250–2000–3000–7500–10,000 ohms	.20
16 Watt—63,000 ohm	.18
50 Watt—150–1500–20,000 ohm	.45

FILTER CHOKES

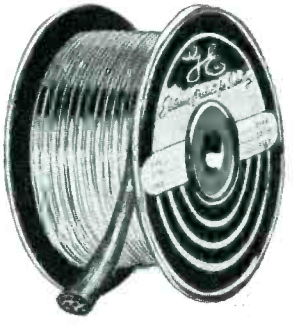
10H/75ma/260 ohm, herm	$.70
4–20H/100ma/120 ohm, herm	.95
10H/100ma/260 ohm, herm	.90
5H/130ma/100 ohm, herm	1.20
10–14H/145–200ma/100 ohm	1.95
5H/200ma/70 ohm	1.95
3–3H/200ma/60 ohm, herm	2.50
6H/350ma/82 ohm	4.50
16H/450ma/112 ohm, herm	9.50
8H/500ma/80 ohm	8.50
5–20H/500ma/80 ohm	8.25
8H/700ma/60 ohm	12.75
5–20H/700ma/60 ohm	12.50
3H/275ma, 17H/175ma, 17H/125ma	3.75
4H/85ma, 6H/90ma, 12H/65ma	2.10

RELAYS — CONTACTORS

Type	Coil	Contacts	Price
CH Contactor	115vac	4PST, 30A	$7.95
West.MC gl.encl.	115vac	4PST, 20A	7.50
Allied BO	6vdc	DPDT, 10A	.75
Advance min.	450 ohm 12vdc	SPST, 5A	.60
G.E. PJC adj. overload, 4–12A ac/dc			12.50
G.E. PJC adj. overload, 2–8A ac/dc			12.50
G.E. PJC adj. overload, 0.5–1.5A ac/dc			7.95

CABLE

9 cond. #20 str. plas. 2 vinyl jack, shield, ½", G.E.	$.08/ft
10 cond. #20 sol. plas., vinyl jack, ½" dia.	.07/ft
28 cond. #20 str. plas., vinyl jack, ¾" dia.	.20/ft
4 cond. ¼" str. plas., vinyl jack, 1" dia.	.26/ft
3 cond. #18 str., shield, jack	.04/ft
2 cond. #20 str., shield, jack	.03/ft
RG8/U Amphenol, Federal	.07/ft
RG77/U Federal	.06/ft



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3B7–4	4 AMP.	$32.95
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3B13–4	4 AMP.	$56.00
3B13–6	6 AMP.	81.50
3B13–15	15 AMP.	120.00

CENTER TAPPED RECTIFIERS

Input 12–0–12VAC Type #	Current	Output 0–8*VDC Price
C1–10	10 AMP.	$6.95
C1–20	20 AMP.	10.95
C1–30	30 AMP.	14.95
C1–40	40 AMP.	17.95
C1–50	50 AMP.	20.95
C1–80	80 AMP.	26.95
C1–120	120 AMP.	34.95

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FULL WAVE BRIDGE RECTIFIERS

Input 0–18VAC Type #	Current	Output 0–13*VDC Price
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B1–500	500 MA.	1.95
B1–1	1 AMP.	2.49
B1–1X5	1.5 AMP.	2.95
B1–3X5	3.5 AMP.	3.95
B1–5	5 AMP.	5.95
B1–10	10 AMP.	9.95
B1–15	15 AMP.	13.95
B1–20	20 AMP.	15.95
B1–30	30 AMP.	24.95
B1–40	40 AMP.	27.95
B1–50	50 AMP.	32.95
B1–60	60 AMP.	36.95
B1–80	80 AMP.	44.95
Input 0–36VAC Type #	**Current**	**Output 0–26*VDC Price**
B2–150	150 MA.	$.98
B2–250	250 MA.	1.25
B2–300	300 MA.	1.50
B2–450	450 MA.	1.95
B2–1	1 AMP.	3.95
B2–2	2 AMP.	4.95
B2–3x5	3.5 AMP.	6.95
B2–5	5 AMP.	9.95
B2–10	10 AMP.	15.95
B2–15	15 AMP.	24.95
B2–20	20 AMP.	27.95
B2–30	30 AMP.	36.95
B2–40	40 AMP.	44.95
Input 0–54VAC Type #	**Current**	**Output 0–40*VDC Price**
B3–150	150 MA.	$1.25
B3–250	250 MA.	1.95
B3–600	600 MA.	3.25
B3–5	5 AMP.	13.95
B3–10	10 AMP.	24.95
Input 0–72VAC Type #	**Current**	**Output 0–54*VDC Price**
B4–600	600 MA.	$3.95
B4–3	3 AMP.	14.95
B4–5	5 AMP.	17.95
B4–10	10 AMP.	32.95
Input 0–115VAC Type #	**Current**	**Output 0–110*VDC Price**
B6–150	150 MA.	$1.95
B6–250	250 MA.	2.95
B6–1	1 AMP.	7.95
B6–3X5	3.5 AMP.	18.95
B6–5	5 AMP.	24.95
B6–10	10 AMP.	36.95
Input 0–234VAC Type #	**Current**	**Output 0–180*VDC Price**
B13–600	600 MA.	$12.95
B13–1	1 AMP.	16.95
B13–3	3 AMP.	35.95
B13–5	5 AMP.	54.95
B13–10	10 AMP.	69.95

** Select Proper Capacitor to Obtain Higher VDC Than Indicated.*

RECTIFIER CAPACITORS

CF-13	6000 MFD	10VDC	$2.49
CF-14	3000 MFD	12VDC	1.69
CF-15	6000 MFD	12VDC	2.95
CF-1	1000 MFD	15VDC	.98
CF-2	2000 MFD	15VDC	1.69
CF-20	2500 MFD	15VDC	1.95
CF-3	1000 MFD	25VDC	1.25
CF-4	2X3500 MFD	25VDC	3.45
CF-5	1500 MFD	30VDC	2.49
CF-6	4000 MFD	30VDC	3.25
CF-7	3000 MFD	35VDC	3.25
CF-8	100 MFD	50VDC	.98
CF-19	500 MFD	50VDC	1.95
CF-16	2000 MFD	50VDC	3.25
CF-9	200 MFD	150VDC	1.69
CF-10	500 MFD	200VDC	3.25
CF-12	125 MFD	350VDC	2.49

RECTIFIER TRANSFORMERS

All Primaries 115VAC 50/60 Cycles

Type #	Volts	Amps.	Price
XF15–12	15	12	$3.95
TXF36–2	36	2	3.95
TXF36–5	36	5	4.95
TXF36–10	36	10	7.95
TXF36–15	36	15	11.95
TXF36–20	36	20	17.95
XFC1710	17	10	4.95

All TXF Types are Tapped to Deliver 32, 34, 36 Volts. XFC type is tapped to deliver 15, 16, 17 Volts Center-Tapped.

RECTIFIER CHOKES

Type #		Amps.	Price
HY6	.02 Hy	5	$3.25
Dimensions	3¾"H x 3"D x 3½"W		
Wt. 5 Lbs.	Hermetically Sealed		
HY8X5	.02 Hy	8.5	7.95
HY10	.02 Hy	10	9.95
HY12	.02 Hy	12	12.95
HY15	.015 Hy	15	13.95

RECTIFIER MOUNTING BRACKETS

For Types B1 through B6, and Type C1 ..... $ .35 per set
For Types B13 ..... .70 per set
For Types 3B ..... 1.05 per set

RECTIFIER KIT

6 and 12 VDC at 10 Amps.

This unit will deliver unfiltered direct current for operation of motors, dynamotors, solenoids, electroplating, battery charging and similar equipment.
The following components are supplied:

1 ea. Full Wave Bridge Rectifier
1 pr. Rectifier Mounting Brackets
1 ea. Transformer 115 VAC 50/60 CPS.
3 ea. Silver-Plated Binding Posts
1 ea. 4-Position Tap-Switch
1 ea. Fuse and Fuse Holder
1 ea. Line Cord and Plug

The primary of the transformer is multi-tapped permitting adjustment of the DC output voltages.

Complete with schematic diagram **$15.95**
Filter Kit for above **$3.50**

SYNCHRO MOTORS

Type 1F Special—KS-5949, L1 Western Electric 115/90 VAC—400 Cycles
Price Each **$8.00**

WRITE FOR CATALOG #619 ON COMPANY LETTERHEAD

VACUUM CAPACITORS

Standard Brands

12 Mmfd	20 Kv.	$4.95
50 Mmfd	20 Kv.	4.95
50 Mmfd	32 Kv.	5.95

SILVER CERAMIC TRIMMERS

Type		
820-Z	5–20 Mmfd Zero Temp	24¢
822-N	5–20 Mmfd Neg. 300	24¢
822-AZ	4.5–25 Mmfd Zero Temp	24¢
823-AN	20–125 Mmfd Neg. 650	33¢

VARIABLE AIR TRIMMERS

Standard Brands—Screw Driver Adj.

	Lots of 10	Lots of 100
7.5 MMF	$2.90	$27.00
25 MMF	3.10	29.00
50 MMF	3.30	31.00
100 MMF	4.10	39.00
140 MMF	4.90	47.00

ATTENTION!!!
INDUSTRIALS, EXPORTERS, SCHOOLS, GOV'T AGENCIES, LABORATORIES

Our engineering staff is at your service to facilitate the application of rectifiers to your specific requirements.

Write for quantity discount on company letterhead.

OIL CONDENSERS

2 Mfd 200VDC Bathtub	$ .20
.5 Mfd 400VDC	.20
2 Mfd 400VDC Bathtub	.30
2X.1 Mfd 600VDC	.39
6 Mfd 600VDC w/mtg. Clamp	.79
10 Mfd 440VAC/1500VDC	1.55
8 Mfd 660VAC/2000VDC	3.50
15-.15 Mfd 8000VDC Voltage Doubler Type	3.95

ELECTROLYTIC CONDENSERS

Cap	WV DC	Each	Lots of 10	Lots of 100
100 Mfd	50	$0.27	$2.20	$19.00
40 Mfd	150	.23	1.80	17.50
8–8–20 Mfd	350/150	.40	3.50	30.00
20–20 Mfd	400/250	.35	3.00	25.00
10 Mfd	450	.30	2.50	20.00
15 Mfd	450	.30	2.50	20.00
40 Mfd	450	.50	4.20	36.00

Minimum order $3.00. No C.O.D.'s under $25.00. 25% deposit on C.O.D. Add 10% for Prepaid Parcel Post and Handling. Terms: Net 10 days in the presence of approved credit.

All prices subject to change w thout notice.

Orders Promptly Filled from Our Stocks
All Prices F.O.B. our NYC Warehouse

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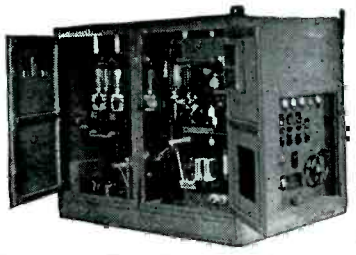
Phone: BEekman 3-7385-6

INDUSTRIAL POWER SUPPLY EQUIPMENT

for worthwhile savings to you

7.5 KW 0-15 KV OUTPUT RECTIFIER POWER SUPPLY

NEW RA-38 HIGH VOLTAGE POWER SUPPLIES: 0-15,000 volts d-c @ 500 ma. Ripple ½% @ 100 ma; 3% @ 500 ma. Regulation 15,800 volts @ 100 ma, 15,000 volts @ 500 ma; 6,800 volts @ 100 ma, 5,000 volts @ 500 ma. Input 115 volts 60 cycle single phase. Full wave bridge rectifier using 4 371B tubes is utilized. Units are designed for continuous duty operation. Units have a full complement of controls, meters and safety devices. A remote control and spare set of tubes are included with each unit. Units are assembled in steel cabinets 62-½" long by 53-¾" wide by 56-¾" high. The cabinets are rubber shock mounted on skids. Weight 2040 lbs. Priced at less than 25% Government acquisition cost. Complete detailed information on request.



ASD RADAR TRANSMITTER

3 centimeter, complete w/725A magnetron, cavity, two 723A/B klystrons, RKR 73, four 72's, 715B, 829B, two 724B's, two 6AC7's, IN23 crystal diode, high voltage supply, cooling blowers, etc. Input: 115 v 400 c. N-2 condition $110.00

PARTS FROM ABOVE EQUIPMENT

Pre. Amp. Assembly: includes plumbing, two 723A/B Klystrons, two 6AC7's, two 724B's, IN23 crystal diode etc...$37.50
Power transformer: D9178, two 2.5 volt windings, 6.3 volt winding and high voltage winding, 115 v, 400 cy. Prl. $11.50
725A Magnetron 12.50
Magnet for 725A. Pole dia. ¾", spacing ⅝" 4850 Gauss.... 7.50
Tubes, filaments guaranteed: CRP 72..$1.10; RKR73..$1.30; 715B ..$5.25; 829B..$2.50.
Capacitor: Vitamin Q, .30 mfd @ 2,000 v d-c ..... .85
Capacitor: Vitamin Q, 2 x .15 mfd @ 8,000 v or .075 mfd. @ 16,000 volts 2.90
Telephone Type Relays: #1 DPST normally open; #2 same as #1 plus a SPDT contact; 1,000 ohm coils both mounted in metal case 3¼ x 3¾ x 4½..... 2.50
Motor blowers: 28 v a-c/d-c.. 2.95

NEW CAPACITORS

STANDARD BRANDS

OIL

2 mfd 600 v d-c tubular: $.30 each
10 for $2.50
3.5/.5 mfd 1000 v d-c.....90 each
4 for 3.00
3 x 1.0 mfd 3 kv d-c test, 1.2 kv d-c wk. Isolated sections. 1.20
1.25/1.25 mfd 7.5 kv d-c or .625 mfd 15 kv d-c Pyranol....12.50
.25/.25 mfd 6 kv d-c or .125 mfd 12 kv d-c..... 3.75
1.0 mfd 25 kv d-c; 65 lbs net; Pyranol 36.00

ELECTROLYTIC

500 mfd 200 wv d-c, insulated terminals ..... .95

MICA

.001 mfd 25 kv d-c; 25 a @ 3,000 kc, 18 a @ 1,000 kc, 11 a @ 300 kv 25.00

VACUUM

50 mmfd 32 kv d-c; tubular 4.95

SPECIALS

WESTINGHOUSE METER MULTIPLIER: 1 meg; ½% accuracy; wire wound; noninductive $1.25
RUNNING TIME METER: R. W. Cramer Type RT3H; 220 v 60 c; 3" square face; 5 figure indicator. (new) 6.95
FILAMENT TRANSFORMER: Constant current type, prl. 110/220 v 50/60 c, sec. 21.5 v 40.5 amps....17.50
TUBE WL 386/ML-3W; 125 kv X-ray rectifier; oil immersion type; filament; 10 v # 11.6 amps 32.00
CRAMER TIME DELAY RELAY type TD2 120S: 0-120 seconds 115 v 60 c; synchronous motor driven; contact rating 10 amps 115 v; single pole normally open 4.95

VOLTAGE REGULATORS

TRANSTAT: 115 v 50/60 cycle input; 0-115 v 100 amps 11.5 KVA output $95.00
TRANSTAT: 115/230 v 50/60 c input; 0-260 v output @ 2.5 amps...$21.50
TRANSTAT: 115 v 50/60 c input; 0 to 130 v output @ 10 amps..$24.50

METERS

Weston or Westinghouse

3" 0-120 a-c amps, w/current transf $ 8.50
3" 0-20 kv d-c w/precision multiplier 18.00
3" 0-4 kv d-c w/precision multiplier 9.50
3" —10 to +6db, 6 mw 600 ohms 6.50

CONSTANT VOLTAGE TRANSFORMERS

SOLA

95 to 125 volt 50 cycle single phase input; 115 volt output:
60 va ...$ 8.40 380 va ...$27.00
120 va ....13.20 500 va 34.00
190 to 250 volt input; 220 volt output:
60 va .... 8.40 250 va 18.00

RAYTHEON

198 to 242 volts 50/60 cycle single phase input; 220 volt 500 watt output $38.00

POWER FACTOR Correction

9.12 mfd 1265 v a-c, 60 c, 1 ph, 5 kilovolt amps reactance. New G. E. Pyranol $17.50

TUBES

All Tubes are New, of Standard Mfg., in original boxes

Type	Price
1B22	$5.75
1B23	9.75
1B24	4.75
2D21	1.25
2J62	47.50
3B22	2.75
3B24	1.75
3C23	3.75
4B28	2.75
15E	1.25
250R	7.50
250TH	19.50
250TL	19.50
*304TL	7.50
307A/RK75	4.50
316A	.75
371B	2.75
388A	2.75
450TH	22.50
700A	37.50
701A	4.75
702A	3.75
703A	4.75
704A	2.25
705A	2.25
706BY	17.50
706EY	19.50
707A	14.75
707B	16.50
708A	4.75
713A	1.25
714AY	5.75
715A	9.50
717A	.75
719A	11.75
721A	2.75
722A	13.75
725A	17.50
730A	19.50
750TL	47.50
811	1.75
830B	4.75
872A	2.25
921	1.25
931A	2.75
C5B	8.50
C6A	8.50
C6J	9.50
FG81A	4.75
WE-203A	4.75
WL-531	17.50
WL-533	17.50

*Includes 115 v 60 c H.V. fil. trans & socket.

T-102—Filament Transformer, American Transformer Co. Spec. 29106, Type WS .050 KVA, 50/60 cyc. Single phase, 35 KVA test, 12 KV D.C. operating. Primary 115 V., secondary 5 V., 10 amps with integral standoff insulator and socket for 250 T, 371, 872 and 5563, etc. rectifier tubes $12.50 Net Wt. 15¾ lbs. Dim 6½" W x 6" D x 12" H.O.A

WIRE

600 volt Simplex Type S (19) conductor #18 AWG ..... $170.00 per M*
3000 volt Simplex underground single conductor #8 AWG..... $140.90 per M*
No. 18 AWG single conductor, solid, annunciator wire 7-lb spool...$2.90 10 spools...$27.00

*Above cable in full spools only, i.e. 1000 to 1200 feet.

All merchandise in "as new" condition. Add approx. 20% to net weights for estimated shipping weights. Terms are 30% with order, balance C. O. D. All prices f.o.b. Los Angeles Warehouse. Write for additional detail information on any of the above items and for special quantity discounts. **Telephone MAdison 6-5381**

1527 E. SEVENTH ST. **EPCO** LOS ANGELES 21, CALIF.

UNITED'S SUMMER VALUES

TOP QUALITY COMPONENTS

PRECISION MICA CONDENSERS (Silver-Cap. 1%)

Size ½" x 1"
400 Mmfd., 1000 Mmfd., 1500 Mmfd., 2000 Mmfd.
19¢, each
100 assorted for $15.00

PRECISION RESISTORS

WW-3 150,000 Ohms ¾" x 1¼" .25¢, 100 for $21.00
W-1 10,000 Ohms 1% 9/16" x 9/16" .25¢, 100 for $21.00

GLASS, VACUUM SEALED

Within ½ of 1% minus tolerance. Each unit marked with exact value to the 6th place. With pigtail leads. 4.0 Megohms at 85¢, each. 10 for $7.50

FERRULE TYPE RESISTORS

Supplied with clips for mounting. Well-known makes.

GLASS TYPES

15 Watts, 19¢, ea. 30 Watts 35¢ ea. 90 Watts, 59¢
1800 Ohms 400 Ohms 4 Ohms
2000 Ohms 630 Ohms 4000 Ohms
3000 Ohms 5000 Ohms 7500 Ohms
3150 Ohms 10,000 Ohms 15,000 Ohms
120 Watts.....79¢ ea.
63 Ohms
750 Ohms
INSTRUMENT MULTIPLIER, 3 Megohms 3 Watts 3000 V. 1.0 Ma Ea..... 98¢

VITREOUS TYPES

25 W. 8 Ohms.....15¢ 100 W. 800 Ohms..65¢
25 W. 20 Ohms....15¢ 100 W. 3000 Ohms.65¢
30 W. 2800 Ohms..29¢ 100 W. 6500 Ohms.65¢
90 W. 800 Ohms...59¢ 200 W. 10,000 Ohms 85¢

OIL FILLED TUBULAR CONDENSERS

Phenolic shell over metal case. Size ¾" x 3⅛". 8-32 screw terminals. .1 Mfd. 1250 V.D.C. Each 23¢. 10 for $2.00

ROUND METAL CAN UPRIGHT FILTER CONDENSERS

40 + 40 Mfd. 250 V.D.C. 1⅜" D. x 4" L. 55¢ Ea. 10 for $5.00; 500 Mfd. 200 V.D.C.W. 2" D. x 4½" L. With mtg. bracket. Ea..$1.19. 10 for $11.00

AMMETER SHUNT

Leece-Neville #S-24602. .005 Ohms mounted on asbestos base with aluminum mounting plate. Perforated metal shield for personnel protection and air cooling. Capable of handling at least 200 Amps. New—$1.39.

CURRENT TRANSFORMER

Model 880—Ratio 75:1. Freq: 50 to 133 Cycles. With mounting bracket. Shpg. Wt. Approx. 1 Lb. New—$2.75.

D. C. AMMETER RELAY

Well known brand. 6½" Diameter 3¾" Deep. Industrial. Stand-off type. 0-50 Amps. for 250 Mv. drop. Relay adjustable over full scale. Relay operates when current drops to preset minimum. *Approx. Shpg. Wt. 10 Lbs. New—$10.50.

COAXIAL CABLE

RG-21/u 53 Ohms. New—$3.49 per 100 Ft. *Approx. Shpg. Wt.—12½ Lbs.

COAXIAL FITTINGS

Female SO-239. 3 for 55¢. Right Angle—Male and Female M-359-A. 3 for 55¢.

NAVY TYPE DYNAMOTORS

High efficiency PM. field units. May be used on 6 V.D.C. with ½ output voltage ratings. MODEL #516 REC.—Output: 275 V. @ 110 Ma. Input: 12 to 24 V.D.C. Approx. Shpg. Wt.—10½ Lbs. $2.50. MODEL #515 TRANS.—Output: 500 V. @ 50 Ma. Approx. Shpg. Wt. 10½ Lbs. $3.50. New in cartons.

OUNCER TRANSFORMER W-226262-4

AF OUTPUT. Pri. Impedance: 10,000 Ohms. Sec. Impedance: 4000 Ohms, tapped at 250 Ohms. Metal can; 1⅞" Lg. x 1" O. D. Overall. 10% at 75 Mw. @ 400 Cyc. 20% at 75 Mw. @ 250 Cyc. Response: 250 to 2500 Cyc. ± 3 DB. Glass sealed. New—95¢ each.

OUNCER TRANSFORMER #7254502

Pri. Impedance: 5000 Ohms. Sec. Impedance: 250 Ohms. Size: 1⅜" Lg. x 1" Overall. Diagram on case. Hermetically sealed. New—89¢ each.

STEPPER RELAY

Type H-706. 4 circuits 25 positions, continuous. Position indicator on drum. D.C. Coil resistance 12 Ohms. Like New condition—$4.75.

WAVE GUIDES

5' long with flange at both ends. Approx. 3 CM. Completely silver plated. Outside finished in Battleship Gray. Flange ends are sealed. New with Flange Hdwe.—$3.39. *Approx. Shpg. Wt.—4 Lbs. *Shipped Railway Express only

WRITE FOR QUANTITY PRICES

Stocks are limited! Order now! C.O.D. orders require 25% deposit. All prices F.O.B. Chicago. Minimum order—$2.00.

UNITED SURPLUS MATERIALS

312 South Halsted St.,
Chicago 6, Illinois
Telephone
CEntral 6-4899

Yes Sir! the **HOTTEST LIST** in the LAND. brim full of electronics, hydraulics, aircraft parts, gadgets Rush me your name TODAY

AC/DC SELSYN SYSTEM

Here's the perfect remote position indicating system—very accurate—operates from 6-12 volts d.c. or 110 a.c. with 75 ma. half wave rectifier and resistor. Diag. furnished.

Per set **$4.95**

MIDGET SELSYNS

AY type operates from 6-12 V. 60 cycle. (26 V 400 cycle) use for either transmitter or receiver ..... **ea. 98c**

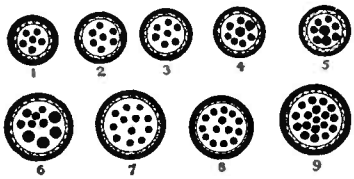
500 CYCLE GENERATOR

4 KVA 110 Volt single phase p/f 1 3400 RPM. Just the thing to hook up to a 60 cycle motor as a power source to operate surplus 400-500 cycle equipment. Has 1 ⅛" keyed drive shaft. Built in exciter and separate DC output of 14 volts @ 40 amps. OD 25 ½ x 12" dia. Wt. approx. 200 lbs. Brand New. FOB EVERETT OR MID WEST. **ea. $79.95**

AMPLIDYNE

GE #5AM31NJ9A 28 VDC input 60-0 60 VDC output at 8.8 Amps. 1 watt field power controls 530 watts output power. The ideal DC motor speed control & AC generator voltage control. Brand New ..... **ea. $2.95**

CONTROL CABLE



1. 6 cond. #18 stranded, shielded, rubber covered .440 OD ft. ..... 8¢
2. 7 cond. #20 stranded, shielded, rubber covered. .440 OD ft. ..... 8¢
3. 7 cond. #16 stranded, plastic covered ft.... 9½¢
4. 8 cond. (2 #14, 6#20) stranded, shielded, plastic covered ft. ..... 9½¢
5. 8 cond. (2#16, 6#20) stranded, shielded, plastic covered, ft. ..... 10½¢
6. 10 cond. (4#12, 2#16, 4#18) stranded, shielded, plastic covered. .730 OD., ft. ..... 14¢
7. 12 cond. #18 stranded, shielded, plastic covered, ft. ..... 15¢
8. 16 cond. #18 stranded, shielded, plastic covered, ft. ..... 16¢
9. 18 cond. (2#16, 16#20) stranded, shielded, plastic covered, ft. ..... 16¢

All conductors color coded. Write for other sizes and types of control cable.

Include return address. Satisfaction Guaranteed or your money back. Hundreds of bargains in our free illustrated list.

DICK ROSE ERECO
2912 Hewitt Ave. Everett 20, Wash.

TS-155B/UP SIGNAL GENERATOR, pulsed, calibrated output, 110 v. 60 cy. NEW.

TS-34/AP SYNCHROSCOPE.

S BAND STANDARD REFERENCE CAVITY, Type N input connector, crystal holder **$15.00**

ECHO BOX CUO—14AAY FOR OBU-2 RADAR.

APR-1 RADAR SEARCH RECEIVER, complete with tuning units for range of 38-4000 mc, 30 mc I.F., 2 mc wide.

TUNING UNITS for APR-1 or APR-4 RECEIVERS (can be used with any 30 mc amplifier):

TN-16, range 30-90 mc
TN-17, range 80-300 mc
TN-19, range 1000-2000 mc
TN-54, range 2000-4000 mc

A LOW COST SUBSTITUTE FOR APR-4 RECEIVER, consisting of an APR-4 power supply and 30 mc I.F. with video amplifier chassis of BC8000AH, complete with tubes and necesary schematic. Equipment is new, but requires minor changes in wiring..complete..... **$60.00**

ANOTHER POSSIBLE SUBSTITUTE consists of 30 mc I.F. and video amplifier chassis, plus power supply, 115 V, 60-800 cps, of APR-5 Radar Receiver. Bandwidth is 10 mc. Complete with tubes, NEW..... **$90.00**

X BAND VSWR TEST SET TS-12/AP, complete with linear amplifier, direct reading VSWR meter, slotted wave guide with gear driven traveling probe, matched termination and various adapters, with carrying case, new.

X BAND POWER METER TS-36/AP, 8700-9500 mc, .1 to 1000 milliwatts.

X BAND PICK-UP HORN AT-48/UP, with coaxial fittings..... **$5.00**

S BAND SIGNAL GENERATOR CAVITY with cut-off attenuator, 2700-2950 mc, 2C40 tube, with modulator chassis **$30.00**

TEST SET TS-278/AP, for AN/APS-13, synchronized, delayed pulse signal generator, 400-430 mc, calibrated waveguide below cut-off attenuator, synchronized marker generator, 115 V 60 cps, new, complete.

HIGH PASS FILTER, cut-off at 1000 mc, coaxial, 50 ohms..... **$12.00**

BROAD BAND TEST LOAD, 50 ohms, 1 watt, V.S.W.R. less than 1.1 to 2500 mc **$7.50**

S BAND TEST LOAD, TPS-55PB/T, 50 ohms **$8.00**

X BAND TEST LOAD, TS-108/AP, 150 watts, accessories **$35.00**

COAXIAL WAVEMETER, Mico Instrument, from 1250 Mc to 4000 Mc... **$60.00**

NOISE FIGURE METER 10-400 mc., measures N. to 30, for 50 ohm impedance. 75 and 270 impedance also supplied.

MUTUAL INDUCTANCE ATTENUATOR, Calibrated; frequency range .1 to 1000 mc by means of plug-in coils, attenuation range 120 db..... **$100.00**

MUTUAL INDUCTANCE OR PISTON TYPE ATTENUATOR, type N connectors, rack and pinion drive, attenuation variable 120 decibels, calibrated 20-120 db, frequency range 300-2000 mc. **$32.00**

LOSSY LINE ATTENUATOR, consisting of RG-21/U cable rolled in metal box with UG-10/U connectors, furnished in any attenuation up to 20 db at 3000 mc **$15.00**

S BAND MIXER, type N signal input, oscillator input, and I.F. output connectors, variable oscillator injection.. **$17.50**

SHIPBOARD RADAR—SQ, SN, SD-3 and SA-1

GENERAL RADIO PRECISION WAVEMETER, type 724A, range 16 kc to 50 mc, 0.25% accuracy, V.T.V.M. resonance indicator, complete with accessories and carrying case, new..... **$175.00**

RDF EQUIPMENT DP-15, 100-1500 kc, for ship use, complete with pedestals, azimuth scale, loop assembly, used 110 V 60 cps **$250.00**

TUBES: W.E. 703, 704A Miniature Diode, and 705A H.V. Rectifier..... **$2.00** each

DM-43 DYNAMOTOR, G.E., 24 V. 515/1030/2/8 volts at 250/280 ma, new, export packed **$5.00**

LOOP MN-20 E for MN-26, D.F., new **$7.00**

TRANSFORMERS, 115 volts, 60 cps primaries:

1. 6250, 3250 and 2000 volts, tapped primary, voltage doubler, 12.5 kv ins **$14.00**
2. 6250 volts 80 ma, ungrounded, G.E. voltage doubler, 12.5 kv ins.... **$12.00**
3. 2 secondaries at 500 volts 5 amps each, wt 210 pounds..... **$50.00**

PULSE INPUT TRANSFORMER, permalloy core, 50 to 4000 kc impedance ratio 120 to 2350 ohms..... **$3.00**

PULSE TRANSFORMER, UTAH 9280 **$1.50**

PULSE TRANSFORMER 132-AWP.. **$6.00**

PULSE TRANSFORMER, GE 68G, 828G-1 **$5.00**

PULSE TRANSFORMER, Westinghouse 145-EWP **$10.00**

W.E. EQUALIZER D162118..... **$5.00**

HYPERSIL CORE CHOKE, 1 Henry, Westinghouse L-422031 or L-422032 **$3.00**

PULSE FORMING NETWORK, 20 kv, .92 microsecond, 50 ohms, 800 p.p.s.. **$40.00**

Clough Brengle Resistance Capacity Bridge, model 230A, new..... **$50.00**

Audio Signal Generator, Hickok 198, RC tuned 20-20,000 cps..... **$45.00**

CONNECTORS:

UG-10/U	.80	UG-190/U	1.00
UG-12/U	.80	UG-201/U	2.00
UG-21/U	.80	UG-245/U	.60
UG-22/U	.80	SO-239	.28
UG-24/U	.80	PL-259	.28
UG-25/U	.80	(for small cable)	
UG-27/U	.50	M-359	.28
UG-29/U	1.00	UG-266	1.00
UG-30/U	1.00		
UG-30/U special	1.00		
UG-58/U	.60	PL 54	.10
UG-59/U	1.00	PL 81	.50
UG-83/U	1.00	AN-3102-14S-5P	.25
UG-86/U	1.00	AN-3102-14S-2P	.25
UG-167/U	2.00	RC-10066-20-IP	.50

METERS:

0-350 VOLTS, WESTINGHOUSE NX-35 METER, 1000 ohms per volt, 3½" **$4.50**

0-8 AMPS R.F. SIMPSON IS-89, 2½" to 10 mc **$4.50**

0-10 AMPERES, TRIPLETT 327-A, 3" square **$4.00**

CAPACITORS:

Feed thru, ceramic, 55 mmfd, 1000 VDC, threaded ..... **.10 each**

Feed thru, silver mica, disc type, 300 mmfd, 500 v..... **.20 each**

Ceramic double cap. 55 mmfd, 10,000 v **.50 each**

Mica .005, 2500 W.V. DC..... **10 for 5.00**

TRANSMITTING OIL-FILLED CAPACITORS:

2 MFD 600 WVDC ROUND CAN 10 for $2. 100 for **$10.00**

2 Mfd	1000 WV	1.00
1 mfd	2500 WV	1.50
.15 mfd	4000 WV	1.00
2 mfd	4000 WV	5.00
.1 — .1 mfd	7000 WV	2.00
.075 — .075 mfd	8000 WV	2.00
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AB26CR MAST EQUIPMENT COMPONENTS such as Anchor screws, coupling units, base plates and guy cables, designed for 72 ft transportable mast. New Equipment.

INVERTER PE 206, INPUT: 28 VDC, 38 Amps. OUTPUT: 80 V, 800 Cy., 500 VOLT-AMPS **$12.50**

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L & N MICROMAX
—D. C. POTENTIOMETER
Model S INDICATING & RECORDING CONTROLLER

Rebuilt, Reconditioned, Adjusted Electrically and Mechanically.
Single Point, Curve-Drawing, Continuous Line, Set H-C-L Contacts. 115 V 60 cy. Motor.

Ranges:
0—1200°F C/A
0—1500°F C/A
0—1800°F C/A
200—2000°F C/A
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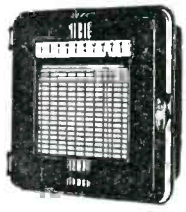
1000—3000°F Plat. 10%R



$210.00

STEP DOWN TRANSFORMERS SPECIAL
Made by GE, heavy duty, considerable over-design, open frame, ideal for rectifier application, size: 3½" x 3½" x 4".
PRI—115 Volts 60 Cycles
SEC—15 V at 12 Amps **$3.75**

HIGH VOLTAGE CAPACITORS

1 MFD 20 KV DC	18"x13½"x5"		$25.00
.1 MFD 25 KV DC	13"x7"x4"		9.85
.001 MFD 50 KV DC	5½"x7¾"x4"	insulators 4" dia. x 7" high	12.50

Cap Mfd.	Volts D.C.	Height	Width	Length	Price
10	1000	5-7/8 x	1-3/4 x	3-7/8"	$1.85
4	1000	5-7/8 x	2-3/4 x	1-1/4"	.85
1	1000	3-5/7 x	2 x	1-1/16"	.50
1	500	2" x	1-1/4" x	1-1/16"	.25
.25	1000	1-1/2 x	1" x	3/4"	.25

RACK PANEL CABINET
42" H x 22" W x 16½" D
Heavy Gauge Metal, Black Wrinkle Finish, shipped knocked down, ready to assemble with rear door and hardware. Front Panel not included. Panel size 19⅛" x 36¾". Shipping weight 99 lbs.
NEW! A REAL BUY $17.50

PANEL METERS
Code—R-Round, S-Square, B-Bakelite, M-Metal, F-Flush, SF-Surface, FS-Full Scale

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Weston	517	0-10	2" R-M	2.95
Weston	517	0-15	2" R-B	2.95
Weston	517	0-150	2" R-B	3.50
Whse	RA35	0-7.5	3" R-B	3.95
Weston	476	0-8	3" R-B	3.95
Trpltt	331JP	0-150	3" R-B	4.50
Whse	RA37	0-300/600	4" S-B w/2 to 1 Potential Transformers	9.75

AC AMPS

Trpltt	332JP	0-30	3" R-M	4.95
Weston	642	0-75	4" R-M SF or F	7.50
Whse	RA37	0-75/150	4" S-B w/external Current Transformers	9.75

DC MICROAMPS

Weston	301	0-100	3" R-B	12.50

DC MILLIAMPS

McClntk	2001	0-1	2" R-B	3.95
GE	DW41	0-25	2" R-B Wide Flange	3.50
Simpson	25	0-1	3" R-B Spec Scale	4.50
GE	DO41	0-1	3" R-B Black Spec Scale	4.50
Weston	301	0-1	3" R-B Spec Scale	7.50
Weston	301	0-25	3" R-M	5.95
Weston	301	0-200	3" R-B	6.50
Weston	301	0-300	3" R-B	6.50
Weston	301	0-500	3" R-B	6.50

DC AMPS

Weston 506	50-0-50MV		2" S-B Spec Scale	3.95
GE	DO50	50MV	3" S-B Spec Scale	2.95
Weston 301	0-1		3" R-M	6.50

DC VOLTS

Sun	378	0-3	2" R-B	2.50
Simpson	125	0-35	2" R-M	2.50
Weston	301	0-150	3" R-M Blk Scale	5.95

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INCLUDE SUFFICIENT FOR POSTAGE

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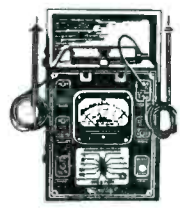

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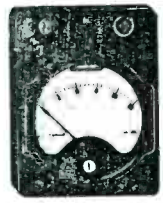
WESTON Model 772, Type 6 with televerter to extend DC range to 5000 V.
SENSITIVITY—
20,000Ω/V-DC
1,000Ω/V-AC
RANGES: (All self contained) AC & DC Volts—5/10/50/250/1000
DC Amps—1/10 A
DC MA — 1/10/50/250 MA MICRO A — 100 MICS
RESISTANCE—3000/30 K/3 Meg/30 Meg Db—6 Ranges from —14 to +54
In handsome wood case



WHSE PORTABLE GALVANOMETER
Type PX-12, Movement 7 MA, special scale, solid connecting terminals, contains a 1 Volt internal cell which can be easily removed for conversion to DC AMMETERS & VOLTMETERS, with leather case and canvas carrying strap.
A BUY at $4.95

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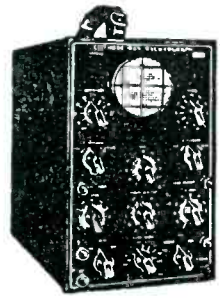
Used! Guaranteed



3" CRT operates at accelerating potential of 1100 V—brilliant well - defined trace Vert amp voltage gain approx 43, horiz amp voltage gain approx 55, Freq. range vert. & hor. amp both uniform ±3 DB from 5-100,000 CPS Input impedance 1 megohm vert, .8 megohm hor. Operates 115 V, 40-60 cycle.
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Your Cost $77.50

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Laboratory Equipment

GENERAL RADIO
107-M Variable Inductors.....$35.00
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33A Crystal Calibrator
34-A U.H.F. Crystal Calibrator....$175.00
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796 Megohmeter (0-200 Megohms)..$50.00

MULTIFLEX
MG3 Spotlight Galvanometer.....$125.00
.00254 μamp per MM

BOONTON
140-A Beat Frequency Generator..$550.00 (20 Cps to 5 Mc ± 2%)
110-A QX CHECKERS
120-A V.H.F. Circuit Checkers.....$95.00 (3 Ranges—27-210 Mc.) For TV & FM
DUMONT 208B, 224A Scopes; 185A S.W. Gen **RCA** Audio Freq. Meter **MEAS. CORP.** 78B.
SHALLCROSS 630 Wheatstone Bridge $60.00
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5	150	2.74	400	25	.98
6	25	.98	500	25	.98
6	50	1.24	500	75	1.97
7	25	.98	585	150	2.74
7.5	100	2.25	750	25	.98
8	50	1.24	750	150	2.74
10	25	.98	1000	25	.98
12	25	.98	1200	225	3.25
15	25	.98	1250	50	1.24
16	50	1.24	1250	150	2.74
22	50	1.24	1500	50	1.24
25	25	.98	2000	25	.98
50	25	.98	2000	50	1.24
50	50	1.24	2500	100	2.25
60	25	.98	3000	25	.98
75	150	2.74	3000	100	2.25
80	50	1.24	3500	50	1.24
80	500	4.95	5000	25	.98
100	50	1.24	5000	50	1.24
125	25	.98	7500	50	1.24
150	50	1.24	7500	100	2.25
200	25	.98	10000	50	1.24
250	25	.98	10000	100	2.25
350	25	.98	20000	150	2.74

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ALLEN-BRADLEY
potentiometers

Type "J"

60	1200	10000	75000
100	1500	12000	80000
150	2000	15000	100000
200	2100	16000	200000
400	2200	20000	250000
500	4000	25000	300000
600	4700	30000	1.0 meg
1000	5000	50000	5.0 meg

Type "JJ" and Type "JJJ"

2 x 500	2 x 150K	3 x 750K
2 x 600	2 x 200K	3 x 800K
2 x 2K	2 x 250K	3 x 1.0 meg
2 x 10K	2 x 1.0 meg	2 x 5.0 meg

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FAMOUS MAKES
most with ceramic pillar insulators.

.1 Mfd	3000 vdcw	$9.75
.25 Mfd	3500 vdcw	1.15
1.0 Mfd	500 vdcw	.28
1.0 Mfd	600 vdcw	.35
2.0 Mfd	400 vdcw	.35
2.0 Mfd	600 vdcw	.39
4.0 Mfd	500 vdcw	.59
4.0 Mfd	600 vdcw	.69
6.0 Mfd	400 vdcw	.75
6.0 Mfd	600 vdcw	.79
10.0 Mfd	600 vdcw	.98
14.0 Mfd	600 vdcw	1.75
15.0 Mfd	600 vdcw	1.98
15.0 Mfd	1000 vdcw	2.25

4-4-4 Mfd 400 vdcw 3 sec. 4 prong plugs in can 4¼" high x 3" Dia. **$1.49**

BATHTUB CAPACITORS
FAMOUS MAKES

.033/400V	.17¢	1.0/200V	.29¢
.05/200V	.13¢	1.0/600V	.35¢
.05/400V	.19¢	2.0/600V	.45¢
.05/600V	.21¢	2x.05/1500V	.33¢
.1/200V	.17¢	2x.1/600V	.29¢
.1/400V	.20¢	2x.1/1000V	.31¢
.1/600V	.22¢	2x.16/600V	.28¢
.15/600V	.23¢	2x.25/600V	.29¢
.25/200V	.19¢	2x.5/600V	.34¢
.25/400V	.21¢	3x.05/600V	.30¢
.25/600V	.23¢	3x.1/600V	.33¢
.5/200V	.20¢	3x.25/600V	.30¢
.5/400V	.23¢	3x1.0/100V	.35¢
.5/600V	.25¢		
4.0/50V	.35¢	200/12V	.25¢
25/25V	.27¢	300/6V	.35¢
25/50V	.28¢	2x10/25V	.25¢
25/75V	.30¢	2x200/9V	.49¢
50/25V	.28¢		

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Standard Brand

6	248	1155	5294	29500
24	280	1250	5470	29870
28	286	1260	5500	30000
34.6	300	1280	5910	32000
35.7	370	1400	6000	33800
38.6	400	1477	6207	37500
40	450	1485	6550	38140
47.7	500	1637	6800	39000
75	636	2000	7000	40500
78.8	650	2142	7500	47710
80	680	2500	15000	60000
88	700	3460	17000	61000
100	733	3500	18380	61430
107.85	743	3760	19500	70000
110	750	3900	20000	72000
125	900	4000	20500	75000
200	946	4280	21000	76100
215	100	4500	22000	83700
225		5000		90000

Any Above Each 30¢; 10 for $2.50

1000000	125000	145000	347000
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brand new in sealed cartons
Type B-19 Pack, Mark II
Mfd. by Delco, Pioneer, Winco.
Input: 12 volts @ 9.4 amps
Output: 275 volts @ .110 amps
500 volts @ .050 amps
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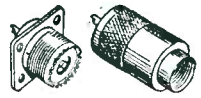

SO 239 sockets 35¢ — PL 259 plugs 35¢

Hoods 10¢ ..... M359 angles 20¢
UG 87U, UG 21U ..... 40¢
UG 167U $1.50

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PRICE fast acting solenoid type 110, has 115 vac coil marked Z30 (70 ohm dc). The long fast travel (5/16") and the use of two contacts in series on each circuit insures reliable service while breaking DC. Cont. duty.

#110—3P N.O., ½ inch dia. cont. on two, ⅜" on other contact ..... **ONLY $3.25 ea.**

Allied DOX, 115 v.a.c. coil, 3 P.D.T., 6 ampere contacts $2.50

Either type ..... **ONLY $3.25 ea.**

Plate Circuit, Leach 1024, 10,000 ohm, 12.5ma coil, DPST NO 3/16" contacts $1.10

SIGMA tiny 1200 ohm 10ma coil, SPDT, ⅞"x⅞"x 1-7/16" ..... 55¢

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50 foot two conductor #18 rubber covered cord on a spring return reel. Features dual silver plated contacts and slip rings. Pays for itself in the time saved from untangling ordinary drop cords. Install one in your closet at home for the vacuum cleaner. Regular price $26.50
Sale Price $9.95

26 CONDUCTOR CABLE made up by Western Electric in 50 foot lengths with S324CT connectors on each end. Each conductor is #22 stranded and rubber covered. Although the O.D. is only 9/16 inches there is a heavy live rubber jacket. Complete with two mating P324AB connectors **ONLY $7.50**

1N21 crystal diode up to 3000 Mc., 8.5db conversion loss, 4.0 output noise ratio, burn out test 0.3erg
SPECIAL ..... 49¢

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3/16" CONTACTS

Mossman 8PDT center open $1.45
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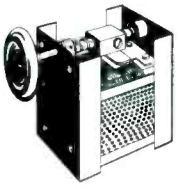

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CONNECTORS - CABLE

Cannon DP and AN Types: large quantities of several types available. Also large stock of multi-conductor cable, transformers, capacitors, panel meters and other electronic components. Write for list or send us your requirements.

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5AP1	3DP1	371B .... .70
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$1.95	95¢	800 .... .65
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Brand new, reads continuously from .005 through 1200. Net price $17.50 f.o.b. Boston.

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Teletypewriters complete, components or parts. Any quantity and condition.

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EXHAUST MACHINE

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WESTERN ELECTRIC VACUUM TUBES

Types 101F, 102F, 272A, 274A or B, 310A or B, 311A, 313C, 323A, 328A, 329A, 348A, 349A, 352A, 373A, 374A, 393A, 394A, 121A Ballast Lamps.

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1000 MMFD ... 10,000 volts
120 MMFD ... 10,000 volts
100 MMFD ... 10,000 volts
20 MMFD ... 10,000 volts
3000 MMFD ... 7,000 volts
YOUR CHOICE $3.00 ea.

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WILL BUY ALL
BC348's with Dynamotor

All letters except "C" $60.00 ea., modified types $50.00 ea. Also ART-13 Transmitters type 47—$80. ea. Type 47A—$95.00 ea.
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Fits most types on market. Made of heavy duty aluminum casting. Excellent for desk, mobile or marine use. BRAND NEW.

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WANTED—NEW TEN SCR 694 Radio Receiver-Transmitters

Govt Surplus

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TBS XMITTER-RCVR
Will xmit or rcve messages by means of voice or telegraphically key tone—mod signals in freq range 60-80 Mc. Rcvr: Xtal cont, output 2W, RF imp 70 ohm, sensitivity 5 microvolt, input 110vac 60 cy. Xmitter: Freq stability +— .025%, output 50W, mod capability 100%, external pwr required. All accessories available. Less tubes & xtals w/inst book, brand new $175.00

TBY-8 TRANSCEIVER
28-80 Mc in 4 bands voice or MCW. Xtal calibrated in 130 channels. Comes in original trunk complete w/vibropack, headset, mic, ant, spare tubes & inst book. Like new $39.50

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R-28 RCVR: Superhet operating on 4 xtal channels, 100-156 Mc, remote control to actuate turret-tuning mechanism, 12 tubes—4-717A, 1-12A6, 3-12SH7 & 2-12SL7GT, w/dyn.
T-23 Xmitter: MCW & phone on 4 channels, 100-156 MC, automatic turret tuning, tank circuits remote controlled, 4 tubes—2-1625, 2-832A.
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BC-1161 RCVR
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157-187 MC. Input 117VAC 60 cy. Has parallel rod OSC using 2-826 PP, contains pwr supply, general radio variac 1.5A, 3½" 0-5 kilovoltmeter, 10 tubes and loads of other parts too numerous to mention. W/circuit. Diagram & tubes, used..... $22.00

ARR-5 RCVR
27.8-143 MC in 3 bands FM or AM. New...$125.00

APR-1 RCVR
Comes w/tunning units TN-1B 38-95 MC & TN-3B 300-1000 MC. W/manuel. New..... $275.00

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90-1000 MC. Has automatic scanning & recording device. Includes ANT filter F-3/APR-2, mounting rack & inst book brand new..... $175.00

APR-5 RCVR
1000-3000 MC & 3000-6000 MC continuously by use of interchangeable tuners. IF freq. 30 Mc.
NEW ..... $195.00 USED $125.00

APS-13 TAIL WARNING RADAR
Contains 9-6AG5, 5-6J6, 2-2D21 & 1-VR-150/30. 420-460 MC. Brand new..... $14.50
W/ANT, warning bell, plug & handbook. New..$18.50

BC-800 RADAR XMITTER RCVR
5 stages RF at 30 MC, 2 stages RF 160-186 MC, uses 2-2C26, 19 tubes total, has blower.
BRAND NEW ....$29.50 USED..... $12.95

PP-104/APT-5
Power supply for APT-5 jammer brand. New..$14.95

T9/APQ-2 JAMMER
210-500 MC, 8 tubes: 2-388, 1-931, 2-6AC7, 1-6AG7, 2-807, 11 watt. Brand new..... $14.00

T-28/APT-1 JAMMER
93-212 MC, 14 tubes: 1-931A, 3-6AC7, 1-6V6, 1-6x5, 2-5R4GY, 2-6C4, 2-832. Has 2 blowers. Used..$22.50

RECORDER RD-7/APA-23
Drive motor 28V DC. Pwr supply 110VAC 60 cy for tubes. 2-2050, 1-6SN7, 1-5Y3 & 1-6AC7. Used. $45.00

T-43/ART-3 JAMMER
Covers 27-34 & 34-45 MC. Uses PP 304TL. Complete with 400cy pwr supply & 2 tunning units. Brand new $75.00

T-36/ART-9 JAMMER
37-44 MC. Uses PP 35TG. Complete w/shock mount & book. Brand new..... $25.00

BC-1334 IF AMP.
36 MC, band width 1.4 MC, built in AVC, 7 tubes. New $25.00

RADAR XMITTER RCVR
CW-43AAF-1. Used W/SJ, SE, SH & Mark 16 Radar. Uses 706 Magnetron and 707A Clystron. Complete with tubes & wave guide fitting. Used excellent....$72.00

MARK 16 RADAR TEST SCOPE
CW-60ABP-1, type LZ. Used. Excellent.....$49.50

MARK 16 RADAR FREQ METER & SIG GEN
CW-60ABQ-1, type LZ, 2700-3333 MC. Used. Excellent $59.00

SIGNAL GENERATOR MOD-78B
Made by measurements corp. Calibrated from 1-100,000 microvolts. 2 bands 25-50 MC & 190-230 Mc. 400cy or 82cy modulation. Has built in vacuum tube voltmeter for calibration. 110VAC 60 cy input. Used $42.00

PHANTOM TARGET RF-4A/AP
Used for checking operation & alignment of SCR-717A, 717B, 720A, 720B radar. Brand new w/inst. book $14.50

725A MAGNETRON
W/magnet & shield $7.95

2J22 MAGNETRON
W/magnet, connector, shield & wave guide fittings & plumbing assy for connection to mixer, local OSC & ant. $9.95

2J21 MAGNETRON
W/magnet & shield $8.95

2K28 CLYSTRON
W/cavity socket & fittings..... $8.95

WL-417A CLYSTRON
W-cavity, mounting bracket, socket & fittings. $12.95

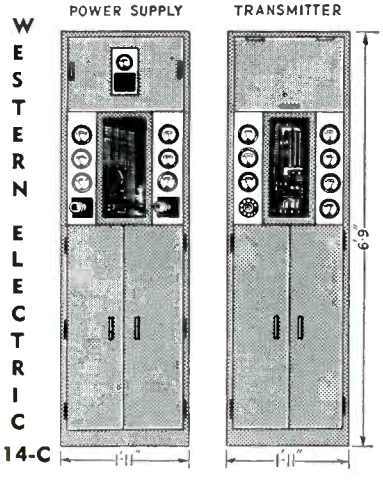
3 CENTIMETER DUPLEXER, MIXER, DETECTOR & OSC ASSY
Includes 2-723A/B LOC, OSC, 2-724B duplexers, IN23 mixer with connector to IF strip. Has ANT & magnatron flanges $18.95

3 CENTIMETER DUPLEXER, MIXER, DETECTOR & OSC ASSY
Includes 2-723 clystrons, 2-724B duplexers, IN23 mixer & 2-6AC7 ..... $16.95
Above magnetrons, clystrons & assy's have been removed from spare equipment. All are in excellent cond. & filaments checked.

Send 30% with order or full price and save COD charge. All shipments will be made via railway express unless other instructions given. All prices subject to change without notice and all merchandise subject to prior sale. Quantity price available.

RADIO V & H ELECTRONICS

2033 WEST VENICE BLVD. *Write for New Catalog* **LOS ANGELES 6, CALIF.**



- Freq range 2 to 18 MC.
- Power Output: 800 w. A1, 400 w. A2 A3.
- Telephone dial 10-channel selector.
- Input: 220/3/60.

This equipment is packed in 8 cases and includes 2 cases of spares. Export crated, F.O.B. N.Y.C. subject to prior sale.

AIRCRAFT RADIO INDUSTRIES, INC.
101 Dixwell Ave., New Haven, Conn.

SPECIAL OFFERING

RG 18/U COAXIAL CABLE
Braided armor overall, otherwise same as RG 17/U. 52 ohms OD .920 efficient solid dielectric cable. A REAL BARGAIN 40¢ per foot. Other coaxial cables. Write for price information and availability.
MARLAN CORPORATION Dept. E.
162 N. Clinton St. Chicago, Illinois

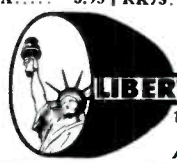
UNUSUAL PRICES

PERFECT JAN. & STANDARD MAKE TUBES

Minimum order $10.00. Add postage or tubes will be sent by Express Collect.

Magnetron		701A	6.00	394A	3.95	705A	1.25
2J26	$18.00	715A	6.00	885	1.45	719A	14.95
2J27	18.00	715B	9.00	**Rectifier**		866A	1.50
2J31	18.00	5D21	29.95	2X2	$.45	872A	2.50
2J32	18.00	**Thyratron**		2X2A	.75	869B	29.95
2J40	54.00	C1B	$3.95	371B	1.25	1616	1.95
2J49	36.00	3C23	3.95	5R4GY	1.25	8020	2.95
2J50	45.00	3C31	3.95	RK72	1.25	**Power**	
2J61	45.00	393A	3.95	RK73	1.75	2C40	1.80
2J62	45.00					2C44	.75
714AY	4.00					350B	2.40
725A	15.00					368AS	1.80
730A	12.00					388A	1.80
Klystron							
2K25	$24.95						
2K28	19.95						
707A	9.95						
707B	9.95						
Pulse							
527	8.95						

446A	1.80	1624	.69
450TH	19.95	1625	.25
WL468	8.95	8012A	1.95
703A	1.80	8025	3.95
802	4.25	**Acorn**	
803	5.25	1A3	$.29
807	1.35	954	.45
813	6.95	955	.45
814	2.95	956	.45
832A	3.95	957	.35
845	3.25	958A	.45
849	29.95	959	.55
851	19.95	9001	.55
		9002	.35
		9003	.45
		9004	.45
		9006	.35
		C. R. Tubes	
		5BP1	2.75
		5BP4	4.75



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NEW and Used — Brakes — Shears
Forming Rolls — Folders — Punches — Di-Acro, Pexto, Niagara & Whitney Equipment.
R. D. BROOKS CO., INC.
Han. 5226
361 Atlantic Ave., Boston, Mass.

Reactor, Filter: 10 H, 0.7 ADC; 45 ohms	$1.00
Transf; 10,000 cyc; Pri 100; Sec 600 & 1.25	1.00
Variometer, ceramic; 1500-1800 KC; split stator & Rotor	1.75
Drop Lines, WE; Standard relay & Drop for Tele Sw Bds	.38
Dee Rings; Steel, joint-weld; for 1" belting; per 1000	1.75
Vibrator; 19 cyc; 12 V. 4-prong plug-in; tele work	.09
Vibrator; Non-syn; 24 V. Sp. plug-in socket req. #VB-11A	.10
Vibrator; Syn; 12 V. Stand. 7-prong, 1½" dia; Oak V-6485	.11
Bell ringers, MC-131; NEW, for field tele EE-8, 9A, etc	.35

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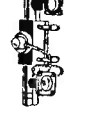



1.25 CENTIMETER

"K" BAND DIRECTIONAL COUPLER CU104/APS-34 20 DB.....$49.50 ea.
"K" BAND FEEDBACK TO PARABOLA HORN, with pressurized window.....$30.00
MITRED ELBOW cover to cover.....$4.00
TR/ATR SECTION choke to cover.....$4.00
FLEXIBLE SECTION 1" choke to choke...$5.00
ADAPTER, rd. cover to sq. cover.....$5.00
MITRED ELBOW and S sections choke to cover $4.50
WAVE GUIDE ½ x ¼ per ft.....$1.00
K BAND CIRCULAR FLANGES.....50¢

10 CENTIMETER

WAVEGUIDE TO ⅞" RIGID COAX "DOORKNOB" ADAPTER. CHOKE FLANGE. SILVER PLATED, BROAD BAND. $49.50 EACH
WAVEGUIDE DIRECTIONAL COUPLER. 27 db. Navy type CABV-47AAN, with 4 in. slotted section.....$42.50
SQ. FLANGE to rd choke adapter, 18 in. long OA 1½ in. x 3 in. guide, type "N" output and sampling probe.....$32.00
"S" BAND CRYSTAL MOUNT, gold plated, with 2 type "N" connectors.....$12.50
PICKUP LOOP, Type "N" Output.....$2.75
TR BOX Pick-up Loop.....$1.25
POWER SPLITTER: 726 Klystron input, dual "N" output.....$5.00
MAGNETRON TO WAVEGUIDE coupler with 721-A duplexer cavity, gold plated.....$27.50
10 CM WAVEGUIDE SWITCHING UNIT, switches 1 input to any of 3 outputs. Standard 1½" x 3" guide with square flanges. Complete with 115 vac or dc arranged switching motor. Mfg. Raytheon. CRP 24AAS. New and complete.$150.00
10 CM END-FIRE ARRAY POLYRODS..$1.75 ea.
"S" BAND Mixer Assembly, with crystal mount, pick-up loop, tunable output.....$3.00
721-A TR CAVITY WITH TUBE. Complete with tuning plungers.....$12.50
10 CM. McNALLY CAVITY Type SG.....$3.50
WAVEGUIDE SECTION, MC 445A, rt. angle bend. 5½" ft. OA. 8" slotted section.....$21.00
10 CM OSC. PICKUP LOOP, with male Homedell output.....$2.00
10 CM DIPOLE WITH REFLECTOR in lucite ball, with type "N" or Sperry fitting.....$4.50
10 CM FEEDBACK DIPOLE ANTENNA, in lucite ball, for use with parabola ⅞" Rigid Coax Input.....$8.00
PHASE SHIFTER. 10 CM WAVEGUIDE. WE TYPE ES-683816. E PLANE TO H PLANE MATCHING SLUGS.....$95.00
721A TR cavities. Heavy silver plated...$2.00 ea.
10 cm. horn and rotating joint assembly, gold plated.....$65.00 ea.
10 cm. right angle bend "E" or "H" plane, less flanges.....$17.50 ea

⅞" RIGID COAX—¼" I.C.

⅞" **RIGID COAX.** Bead Supported.....$1.20
SHORT RIGHT ANGLE BEND.....$2.50
Rotating joint, with deck mounting.....$15.00
RIGID COAX, slotted section CU-60/AP.....$5.00
"S" BAND "Y" JUNCTION. SQ. FLANGES $65.00
10 cm. waveguide to ⅞" rigid coax doormknob transition, 21" high with 8" slotted section $52.50 ea
10 cm. flexible section 4 feet long.....$42.50 ea.
10 CM. FLANGES, UG65/U.....$8.50
UG65/U 10 CM. FLANGE.....$8.50
ADAPTER 1½ x 3 TO 1" x 2". SQ. 10 CM FLANGE TO SQ 5 CM CHOKE.....$57.50
KLYSTRON MOUNT W/TUNABLE MATCHING OUTPUT TO TYPE "N" CONNECTOR. SOCKET & TUBE CLAMP INCLUDED..$12.50

⅞" RIGID COAX—⅜" I.C.

⅞" **RIGID COAX ROTARY JOINT.** PRESSURIZED. SPERRY #810613. GOLD PLATED $27.50
Dipole assembly. Part of SCR 584.....$25.00 ea.
Rotary joint. Part of SCR-584.....$35.00 ea.
RIGHT ANGLE BEND, with flexible coax output pick-up loop.....$8.00
SHORT RIGHT ANGLE bend, with pressurizing nipple.....$3.00
RIGID COAX to flex coax connector.....$3.50
STUB-SUPPORTED RIGID COAX, gold plated 5' lengths. Per length.....$5.00
RT. ANGLES for above.....$2.50
RT. ANGLE BEND 15" L. OA.....$3.50
FLEXIBLE SECTION. 15" L. Male to female $4.25
MAGNETRON COUPLING to ⅞" rigid coax, with TR pickup loop, gold plated.....$7.50
FLEX COAX SECT. Approx. 30 ft.....$16.50

MISCELLANEOUS

Type "N" patching cord UG11/U female to UG9/U using RG5/U cable 12" long.....$2.25 ea
AN/TPS-1B flanged nipple and insert assembly for rotary coupling.....$3.75 ea
Pulse connector Navy type 49579.....$1.50 ea.
Transmission line pressure gauge. 2" 15 lbs $1.85 ea
Pulse cable assembly Western Electric type D163262. 10 feet long.....$4.50 ea.
Holmdell Jack Western Electric #BO-12962-1 D.B. #J-102X.....$3.75 ea.
Adapter type "N" RG8/U to RG17/U or 18/U cable.....$4.50 ea.
ADAPTER TYPE "N" TO RG-17/U CONNECTOR......$5.50
F-29/SPR-2 HIGH PASS FILTER P/O AN/APR-5AX. TYPE "N" CONNECTORS.....$12.50
Magnetron coupling to ⅝ rigid coax.....$5.00 ea.
Hand pumps for pressurizing transmission line with humidity indicator.....$12.50 ea.

MARINE RADAR

SO-1 AND SO-8 RADAR SETS, Complete, in Used but Excellent Condition. 10 CM Surface Search using 2J26 or 2J27 Magnetron, 707B Mixer. PPI Indicator. Input 115VDC. Used on Merchant Ships throughout the world. FCC Approved. Guaranteed. $1250.00.

TEST EQUIPMENT

TS-L17/GP 10 CM WAVEMETER TEST SET. Mfg. "Sperry". 2400-3400 MC. Micrometer Adj. Coaxial Cavity. Freq. Meas by absorption or transmission method. Mounts Crystal Current Meter & Calib. Chart.....$145.00
VSWR AMPLIFIER TS-12/AP. Unit 1 3 stages of Amplif. and Diode Rectifier w/direct VSWR. reading on meter. 115 volts 60 cyc. AC operation w/Inst. BK and CCT diag. New..$235.00
SLOTTED LINE PROBE and Matched Termination Incld'g Accessories TS-12/AP Unit 2 incl. UG81/U, CG92/U, CG91/U, CG89/U, UG79/U, CG87/U, MX158/U, CG-88/U, CG90/U, UG80/U plus Tools. New.....$135.00
COMPLETE TS-12/AP UNITS 1 AND 2..$350.00
10 CM ECHO BOX CABV 14ABA-1 of OBU-3. 2890 MC to 3170 MCS, direct reading micrometer head. Ring prediction scale plus 9% to minus 9%. Type "N" input. Resonance indicator meter. New and Comp. w/access. Box and 10 CM Directional Coupler.....$350.00
3 CM RECEIVER. SO-3. Complete with W.G. Mixer Assy (723 A/B) Reg. Fil. Power Supply, 6 Stages IF (6AC7).....$99.50
10 cm. horn assembly consisting of two 5" dishes with dipoles feeding single type "N" output. Includes UG28/U type "N" "T" junction and type "N" pickup probe. Mfg. Bernard Rice. RGH/U cable. New.....$15.50 ea.
10 cm. cavity type wavemeters 6" deep 6¼" in diameter. Coax. output. Silver plated.$64.50 ea.
10 cm. echo box. Part of SF-1 Radar with 115 volt DC tuning motor Sub Sig 1118A..$47.50 ea.
TS33AP WAVEMETER, MICROMETER ADJ. TYPE "N" FITTINGS.....$125.00
"X" Band test set TS45A. APM-3 using 723 AB Oscillator. Input 115 volts single phase 60 to 800 cycles. 0 to 35 DB attenuator in used, fair condition.....$110.00 ea.
TS-268/U crystal test set for checking 1N21, 1N21A, 1N21B, 1N23, 1N23A, 1N23B crystals. New.....$39.50 ea.
THERMISTOR BRIDGE: Power meter 1-203-A. 10 cm. mfg. W.E. Complete with meter, interpolation chart, portable carrying case....$72.50
W. E. I 138. Signal generator, 2700 to 2900 Mc. range. Lighthouse tube oscillator with attenuator & output meter. 115 VAC input, reg. Pwr. supply. With circuit diagram.....$50.00
3 cm. Wavemeter: 9200 to 11,000 mc. transmission type with square flanges.....$15.00
3 cm. stabilizer cavity, transmission type...$20.00

MAGNETRONS

Tube	Frq. Range	Pk. Pwr. Out	Price
2J31	2820-2860 mc.	265 KW.	$25.00
2J21-A	9345-9405 mc.	50 KW.	$25.00
2J22	3267-3333 mc.	265 KW.	$25.00
2J26	2992-3019 mc.	275 KW.	$25.00
2J27	2965-2992 mc.	275 KW.	$25.00
2J32	2780-2820 mc.	285 KW.	$25.00
2J37			$45.00
2J38 Pkg.	3249-3263 mc.	5 KW.	$35.00
2J39 Pkg.	3267-3333 mc.	87 KW.	$35.00
2J40	9305-9325 mc.	10 KW.	$65.00
2J49	9000-9160 mc.	58 KW	$85.00
2J34			$55.00
2J61	3000-3100 mc.	35 KW.	$65.00
2J62	2914-3010 mc.	35 KW.	$65.00
3J31	24,000 mc.	50 KW.	$55.00
5J30			$39.50
714AY			$25.00
718DY			$25.00
720BY	2800 mc.	1000 KW.	$50.00
720CY			$50.00
725-A	9345-9405 mc.	50 KW.	$25.00
730-A	9345-9405 mc.	50 KW.	$25.00
728	AY, BY, CY, DY, EY, FY, GY		$50.00
700	A, B, C, D		$50.00
706	AY, BY, DY, EY, FY, GY		$50.00

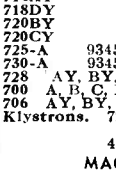
Klystrons. 723A/B $12.50: 707B W/Cavity 417A $25.00 2K41 $65.00

MAGNETRON MAGNETS

Gauss	Pole Diam.	Spacing	Price
4850	¾ in.	⅝ in.	$12.50
5200	21/32 in.	¾ in.	$17.50
1300	1⅝ in.	1 5/16 in.	$12.50
1860	1⅝ in.	1¼ in.	$14.50

Electromagnets for magnetrons.....$24.50 ea.

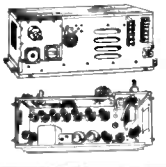
MICROWAVE ANTENNAS



SO-3 RADAR 3 CM. SURFACE SEARCH ANTENNA. Complete with 24 VDC Drive Motor, Selsyn, Gear Mechanisms, "X" Band Slotted "Peel" Reflector. Less Plumbing.....$135.00
As Shown
APS-15 Antennas. New....$99.50
AN MPG-1 Antenna. Rotary feed type high speed scanner antenna assembly, including horn parabolic reflector. Less internal mechanisms. 10 deg. sector scan. Approx. 12'L x 4'W x 3'H. Unused. (Gov't Cost—$4500.00).....$250.00
APS-4 3 cm. antenna. Complete. 14½ dish. Cutler feed dipole directional coupler, all standard 1" x ½" waveguide. Drive motor and gear mechanisms for horizontal and vertical scan. New, complete.....$5.00
AN/TPS3. Parabolic dish type reflector approx. 10' diam. Extremely lightweight construction. New in 3 carrying cases.....$89.50
RELAY SYSTEM PARABOLIC REFLECTORS: approx. range: 2000 to 6000 mc. Dimensions: 4¼' x 3' rectangle, now.....$85.00
TDY "JAM" RADAR ROTATING ANTENNA, 10 cm. 30 deg. beam. 115 v.a.c. drive. New..$100.00

R. F. EQUIPMENT

LHTR. LIGHTHOUSE ASSEMBLY. Part of RT-39/APG-5 & APG-15. Receiver and Transmitter Lighthouse Cavities with assoc. Tr Cavity and Type N CPLG. To Rcvr. Uses 2C40, 2C43, 1B27. Tuneable APX 2400-2700 MCS. Silver plated $49.50
Receiver transmitter Rt-39A/APG-5 10 cm. gun laying RF package using 2C40 and 2C43, new $150.00 ea.
APS-2 10CM RF HEAD COMPLETE WITH HARD TUBE (715B) Pulser, 714 Magnetron 417A Mixer all ⅞" rigid coax, incl. rcvr. front end $210.00
Beacon lighthouse cavity 10 cm with miniature 28 volt DC FM motor. Mfg. Bernard Rice.$47.50 ea.
T-128/APN-19 10 cm. radar Beacon transmitter package, used, less tubes.....$59.50 ea.
SO-3 "X" banc 3 cm RF package, new complete, including receiver unit as illustrated on Page 337, Volume 23 RAD LAB Series....$375.00 ea.
Pro-amplifier cavities type "M" 7410590GL to use 446A lighthouse tube. Completely tunable, Heavy silver plated construction.....$37.50 ea.
RT32/APS 6A RF HEAD, Compl. with 725A Magnetron magnet pulse xfmr. TRA-ATR. 723 A/B local osc. and beacon mount, pre amplifier. Used but exc. cond.....$97.50
AN/APS-15A "X" Band compl. RF head and modulator, incl. 725-A magnetron and magnet, two 723A/B klystrons (local osc. & beacon), 1B24, TR, rcvr-ampl. duplexer, HV supply, blower, pulse xtmr. Peak Pwr Out: 45 KW apx. Input: 115, 400 cy. Modulator pulse duration .5 to 2 micro-sec. apx. 13 KV Pk Pulse. Compl with all tubes incl. 715-B, 829B, RKR 73, two 72's. Compl. pkg, new.....$210.00
APS-15B. Complete pkg. as above, less modulator $150.00
"S" BAND AN/APS-2. Complete RF head and modulator, including magnetron and magnet, 417-A mixer, TR, receiver, duplexer, blower, etc., and complete pulser. With tubes, used, fair condition.....$75.00
10 CM, RF Package. Consists of: SO Xmtr.-receiver using 2J27 magnetron oscillator, 250 KW peak input. 707-B receiver-mixer.....$150.00



3 CM RECEIVER

SO-3. Complete With W.G. Mixer Assy (723 A/B) Reg. Fil. Power Supply, 6 Stages IF (6AC7).....$99.50

3 CENTIMETER (STD. 1" x ½" GUIDE, UNLESS OTHERWISE SPECIFIED)

3 cm. 180° bend with pressurizing nipple.$4.00 ea.
3 cm. 90° bend. 14" long 90° twist with pressurizing nipple.....$4.00 ea.
3 cm. "S" curve 18" long.....$5.50 ea.
3 cm, "S" curve 6" long.....$3.50 ea.
3 cm. right angle bends. "E" plane 18" long cover to cover.....$6.50 ea.
3 cm. Cutler feed dipole. 11" from parabola mount to feed back.....$8.50 ea.
3 cm. directional coupler. One way waveguide output.....$15.00 ea.
Tr ATR section for mounting 1B24 with 721A ATR cavity. Iris coupling flange. Choke to choke.....$12.50 ea.
APS-31 mixer section for mounting two 2K25's Beacon reference cavity 1B24 TR tube. New and complete with attenuating slugs.....$42.50 ea.
DUPLEXER SECTION for 1B24.....$10.00
CIRCULAR CHOKE FLANGES, solid brass. .55
SQ. FLANGES, FLAT BRASS.....ea. .55
APS-10 TR/ATR DUPLEXER section with additional iris flange.....$10.00
FLEX. WAVEGUIDE.....$4.00/Ft.
TRANSITION 1 x ½ to 1¼ x ⅝, 14 in. L..$8.00
"X" BAND PREAMPLIFIER, consisting of 2-723 A/B local oscillator-beacon feeding waveguide and TR/ATR Duplexer sect, incl. 60 mc IF amp.....$67.50
Random Lengths wavegd, 6" to 18" Lg...$1.10 Ft.
WAVEGUIDE RUN, 1¼" x ½" **guide,** consisting of 4 ft. section with Rt. angle bend on one end 2" 45 deg. bend other end.....$8.00
WAVEGUIDE RUN, 1¼" x ½" **guide,** consisting of 4 ft. long.....$10.00
"X" BAND PRESSURIZING gauge section w/15-lbs. gauge & Pressurizing Nipple.....$18.50
45 DEG. TWIST 6" Long.....$10.00
12" SECTION 45 deg twist 90 deg. bend.....$6.00
11" STRAIGHT WAVEGUIDE section choke to cover. Special heavy Construction, silver plated $4.50
15 DEG BEND 10" choke to cover.....$4.50
5 FT SECTIONS choke to cover. Silver Plated.....$14.50
18" FLEXIBLE SECTION.....$17.50
"E" and "H" PLANE BENDS.....$12.50
BULKHEAD FEED THRU.....$15.00
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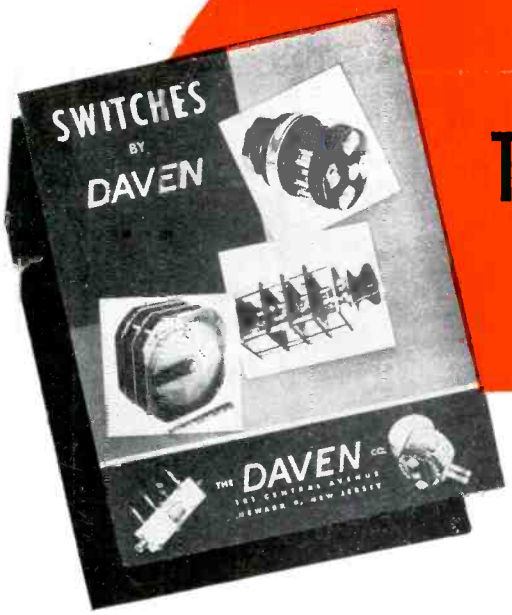
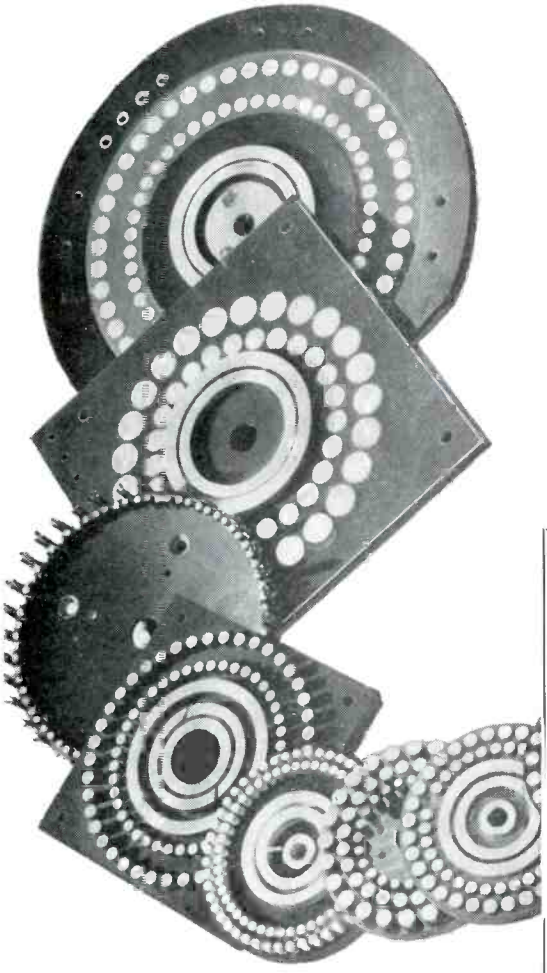
. . . FOR THOSE TOUGH "Switching" PROBLEMS TRY DAVEN!



Write for your copy of our new Switch Bulletin

Whether you use switches for industrial applications, communications or laboratory work, a Daven-constructed unit will give maximum performance. Many years of engineering experience and skilled workmanship have been combined to make a truly superior switch.

Daven switches are the rotary selector type—outstanding in design and capable of withstanding the most critical tests. They are preferred by engineers who want the best.



Some outstanding features are—

- **Low and uniform contact resistance.**
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- **High resistance to leakage.**
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- **Depth of unit not increased by addition of detent.**

A full line of standard switches are available. Listed below are a few of the popular types.

Type	Operation	Maximum No. of Positions (per pole)	Maximum Poles per Deck	Deck Diameter
C1A	Make before break	31	1	1 3/4"
C2B	Break before make	15	1	1 3/4"
C7A	Make before break	11	2	1 3/4"
C8A	Break before make	5	2	1 3/4"
D1A	Make before break	47	1	2 1/4"
D7A	Make before break	14	4	2 1/4"
D9A	Make before break	9	5	2 1/4"
D10B	Break before make	5	5	2 1/4"
E3A	Make before break	47	2	2 3/4"
E4B	Break before make	23	2	2 3/4"
E7A	Make before break	23	4	2 3/4"
E8B	Break before make	12	4	2 3/4"
F1A	Make before break	60	1	3"

ven has a standard switch for your special requirements.
r engineers will be glad to offer suggestions on *your* problems.

ıd your detailed information to Dept. E-1

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A new milestone in television progress

... the RCA 16-inch metal-cone television kinescope

• The RCA-16AP4—a 16-inch, directly viewed metal-cone kinescope—is RCA's newest contribution to the television industry. It is the outgrowth of a perfected process of sealing glass to large areas of metal.

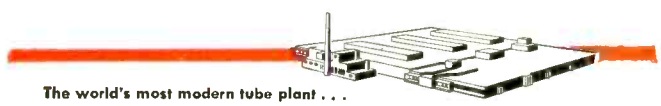
Use of the metal cone reduces weight substantially below that of a similar all-glass tube and provides greatly increased strength.

Other features of the 16AP4 include high picture brightness, good contrast even under high ambient light conditions, a high-quality face plate, and large useful screen area in relation to face area.

The RCA-16AP4 meets the growing demand for a picture size midway between that of the popular directly viewed RCA-10BP4 and the larger, projected picture provided by the RCA-5TP4.

The 16AP4 is currently being produced in quantity at the RCA Lancaster plant. Ground has been broken for a new large plant in Marion, Indiana, the entire production of which will be centered on the 16-inch metal tube.

RCA Application Engineers are ready to cooperate with you in applying the 16AP4 and associated components to your specific designs. For further information write RCA, Commercial Engineering, Section 42GR, Harrison, New Jersey.



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