APRIL • 1943

electronics

Proper maintenance conserves critical materials and minimizes need for new tubes by prolonging tube life. Method of cleaning terminals illustrated above.

For a full measure of service

Not only are men being tried on battlefronts, the equipment that they employ is being subjected to equally critical tests . . .with the lives of the men as the stakes. We at home, entrusted with war contracts, are overcoming serious raw material shortages through laboratory and production developments, making each individual tube that we produce do more than its planned job . . . and do it better.

Through a series of design refinements, Amperex engineers have developed transmitting and rectifying tubes that are being operated for longer periods of time than hitherto had been practical. These new Amperex radio and radar tubes present a dual economy . . . many more hours of uninterrupted service . . . and priceless savings of scarce materials.

AMPEREX ELECTRONIC PRODUCTS

79 WASHINGTON STREET • BROOKLYN, NEW YORK

electronics

APRIL • 1943

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330 West 42nd Street, New York, N. Y.

Director of Circulation:
Please change my address on Electronics

From .....

.....

To .....

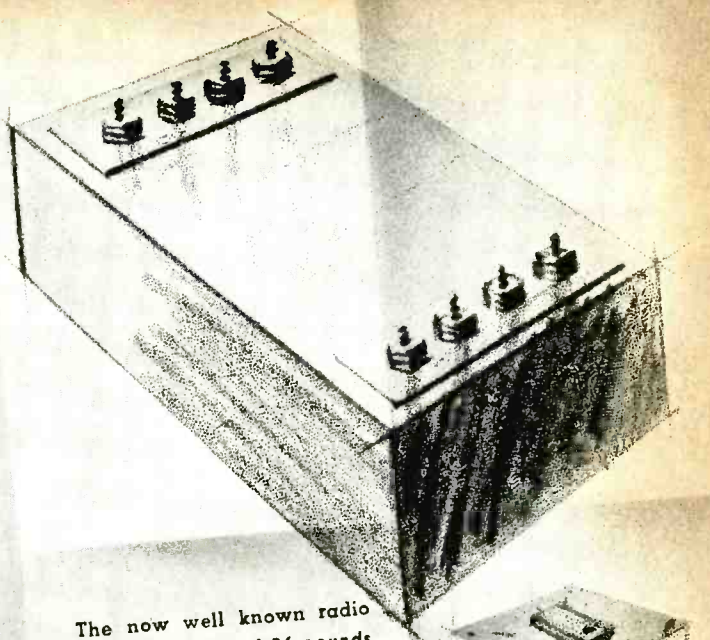
.....

Signed .....

FILTERS—
Designed for war

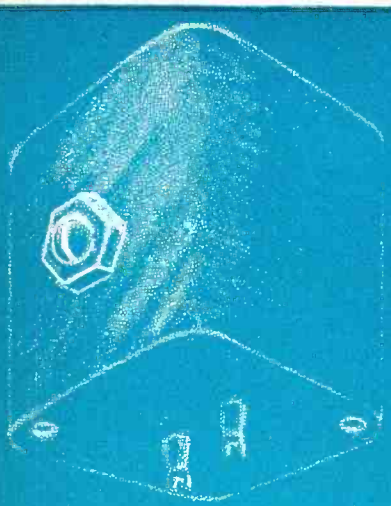
Unique characteristics of many UTC filters are the result of years of research on core materials and filter structures. We are proud of our part in the development of filters for wartime electronics. Here are a few typical elements, based on UTC design, which have led to UTC leadership in this field.

May we design a "Victory" unit to your application?

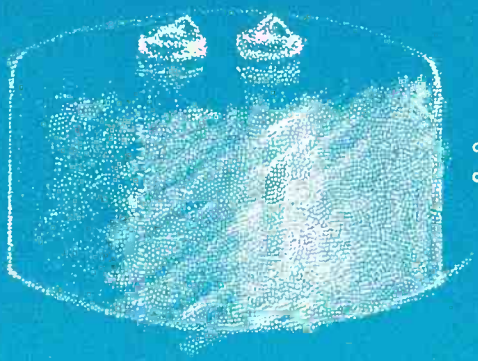


The now well known radio range filter weighed 36 pounds when it originally was submitted to us.

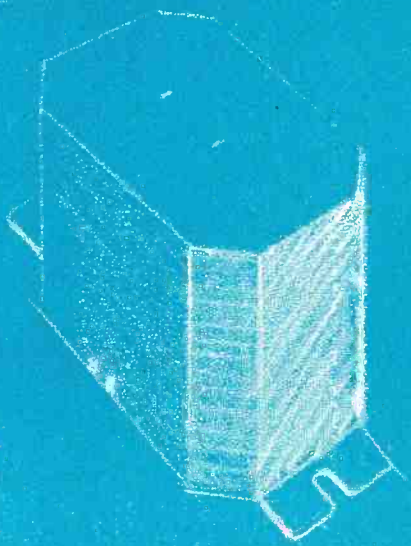
Continuous refinement by UTC has resulted in the modern radio range filter weighing only 1.6 pounds — a weight reduction of 95%.



This UTC development is a tunable inductance, adjusted in the same manner as an I.F. trimmer.



Designed for high frequencies, the Q of this coil is 300 at 20,000 cycles.



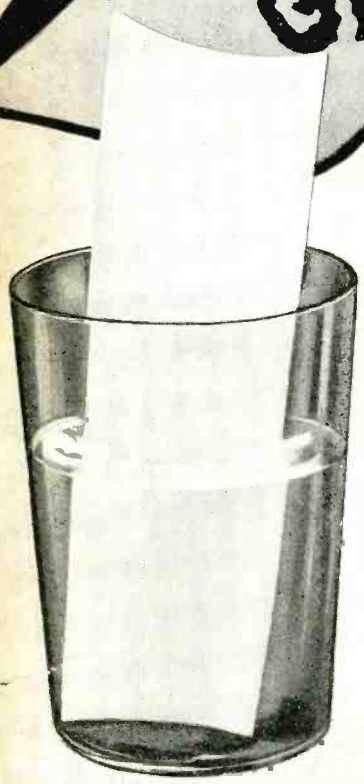
. . . For medium frequencies, the Q of this coil is 210 at 1,000 cycles.

. . . For low frequencies, the Q of this coil is 80 at 100 cycles.

UNITED TRANSFORMER CO.

150 VARICK STREET ★ NEW YORK, N. Y.

EXPORT DIVISION: 100 VARICK STREET NEW YORK, N. Y. CABLES: "ARLAB"



This new tracing cloth defies moisture stains and erasure scars

This new tracing cloth won't show perspiration stains or water marks—*holds pencil smudges and erasure scars at a minimum.* Now you can have clean tracings, in pencil or ink, free from these untidy "ghosts" that reproduce on blueprints!

For PHOENIX is ghost-proofed by a remarkable new process that defies moisture and gives you an unusually durable working surface. You can use harder pencils with this improved cloth and get sharper lines with less tendency to smudge. Even 6H lines show clearly, and reproduce sharply! Erasing does not mar the drawing surface; erased areas take pencil smoothly—and ink without feathering. Its new white color and increased transparency give you excellent drawing contrast and produce strong blueprints.

Put PHOENIX through your own drawing board test. See your K&E dealer, or write for a generous working sample and an illustrated brochure.

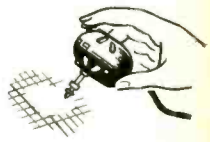
PHOENIX DEFIES MOISTURE GHOSTS . . .

Perspiration and water splashes on ordinary tracing cloth create "ghosts" which reproduce on blueprints. PHOENIX Tracing Cloth withstands actual immersion in water for fully 10 minutes at a time! *Perspiration and water marks will not stain it!*

PHOENIX LESSENS SMUDGE GHOSTS . . .

The new improved surface of PHOENIX Tracing Cloth permits you to use harder pencils (5H and 6H) and to get sharper lines with less tendency to smudge.

Result: Cleaner tracings and blueprints.



PHOENIX REDUCES ERASURE GHOSTS . . .

Ordinary tracing cloths become scarred when erased . . . erased spots produce ghosts on blueprints.

PHOENIX has a durable drawing surface that reduces working scars to a minimum.

K&E

Phoenix

REG. U.S. PAT. OFF.

TRACING CLOTH

for pencil *and* ink

EST. 1867

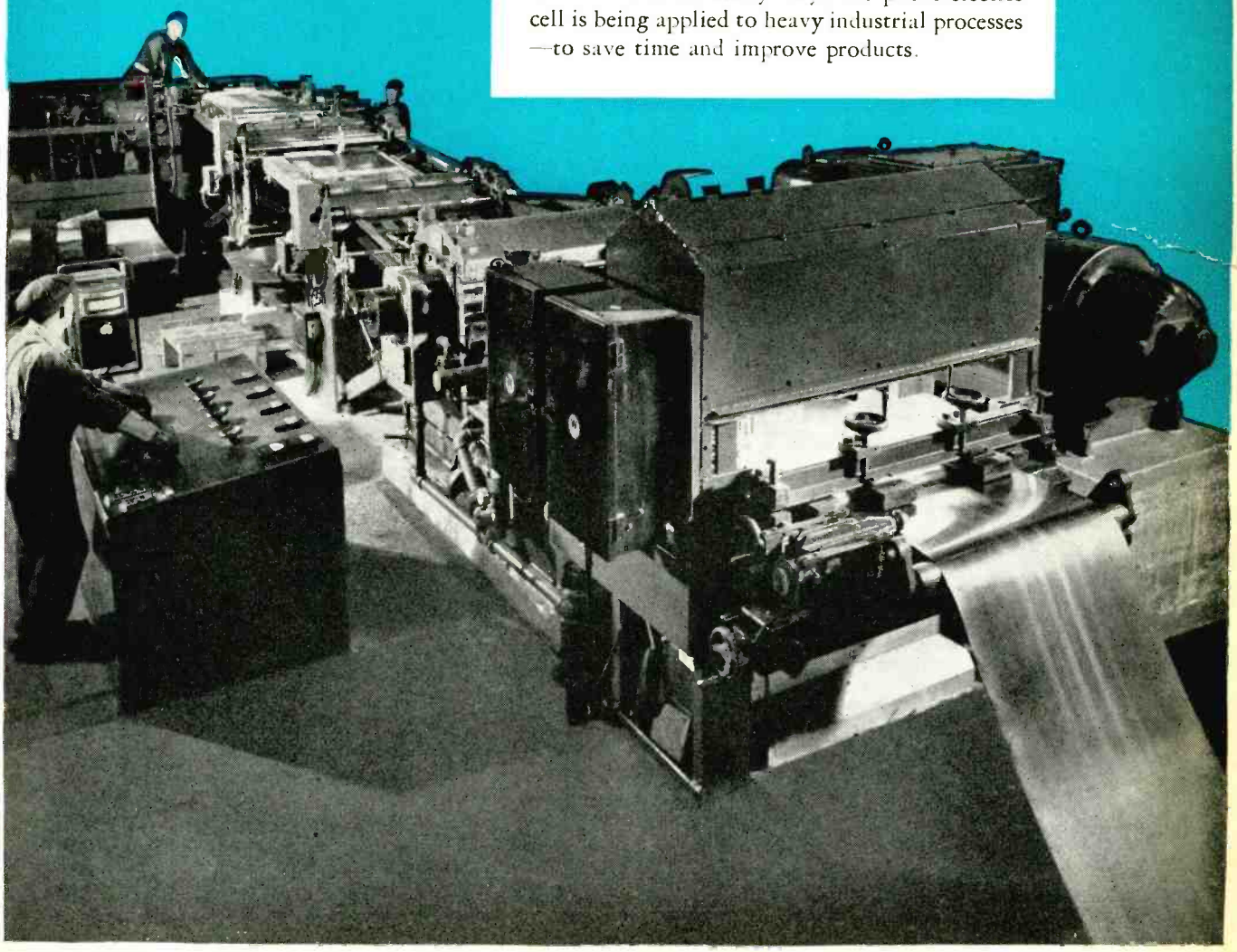
KEUFFEL & ESSER CO.

NEW YORK · HOBOKEN, N. J.

CHICAGO · ST. LOUIS · SAN FRANCISCO · LOS ANGELES

DETROIT · MONTREAL

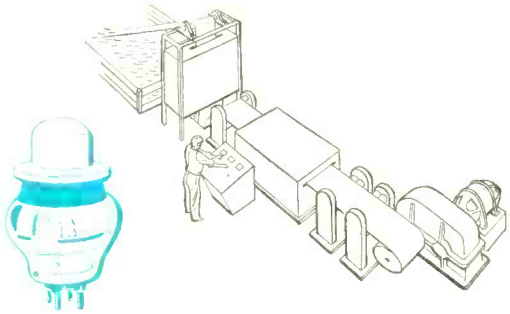
Electronics



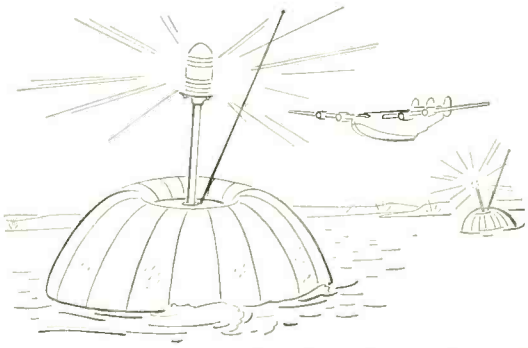
The Pinhole Detector automatically spots, classifies and marks minute holes smaller than 1/64 of an inch in tinplate racing through a shearing line at 1,000 ft. per minute. This application shows one of the many ways the photo-electric cell is being applied to heavy industrial processes —to save time and improve products.

. . at Work

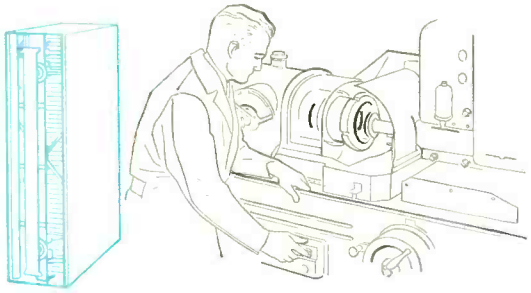
Exciting as the future of Electronics may be, it is far more than a "science of tomorrow." Electronic devices are at work *today* in practically every war industry—speeding production, improving products, cutting costs. Here are typical examples of Westinghouse "Electronics at Work."



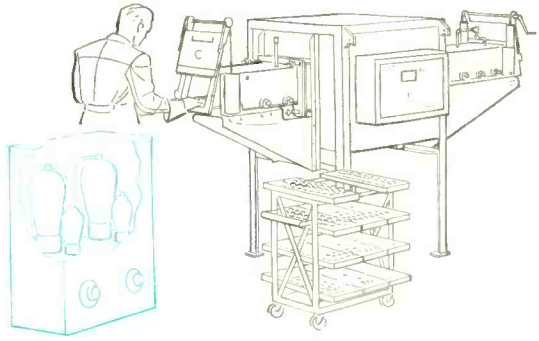
Saving Tons of Tin—Through the use of high-frequency electronic tubes, induction heating at 200,000 cycles per second is used to "flow" tin electrolytically deposited on steel strip. By this means, a coating of tin 1/30,000,000 of an inch thick becomes smooth and corrosion-resistant.



Safe Night Landings for giant clipper planes are made possible by seadrome lights controlled by electronics. An entire landing lane can be turned on by shore radio to meet the arriving plane's requirements and guide it to a safe, sure landing, even in pitch darkness.



Removing Oil Mist created by gear-grinding and thread-cutting operations is a highly important application of PRECIPITRON—the Westinghouse electric air cleaner. Electronic tubes in the Precipitron's power pack create a 12,000-volt electrostatic field, which draws oil and dust particles irresistibly to charged collector plates.



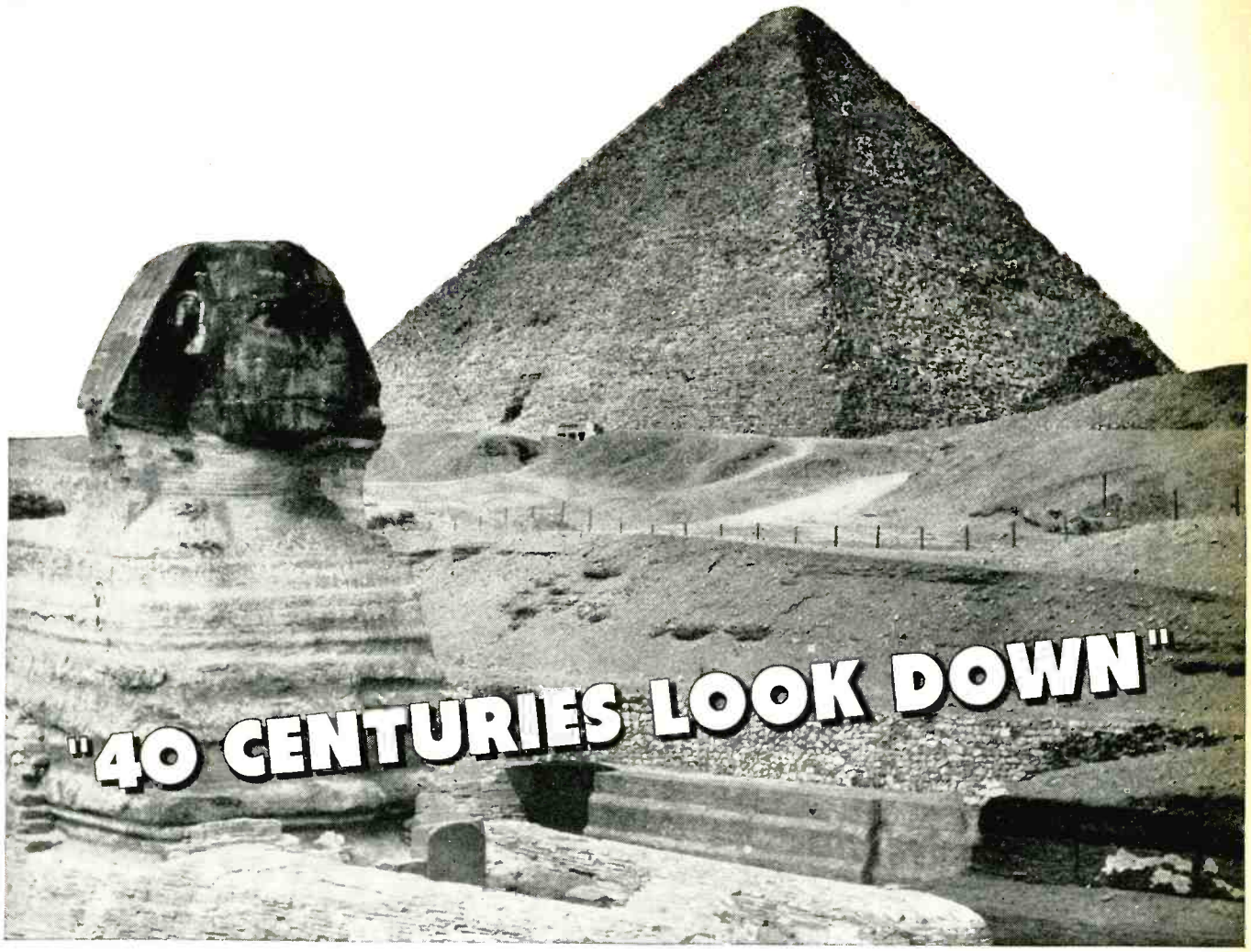
Heat-treating at 2000° C. can now be controlled more precisely than ever before possible. Thyratron tubes, actuated by the temperature recorder, react to minute variations in temperature. They control a saturable reactor, by which current entering the furnace is increased or decreased to maintain a nearly constant temperature.

J-91013-A

For further information on practical applications of Westinghouse Electronic devices, write or phone your nearest Westinghouse office, Westinghouse Electric & Manufacturing Company, East Pittsburgh, Pa.

Westinghouse ELECTRONICS

PLANTS IN 25 CITIES . . . OFFICES EVERYWHERE



Long life is the outstanding quality you require in a capacitor. And greatest guarantee of long life is the record of the past.

This record in the case of Tobe Capacitors warrants the fullest confidence . . . a record that is almost completely free of condensers that "couldn't take it".

Tobe's exacting standards mean persistent research and the constant "raising of sights" in excellence of production.

Typical example is the Tobe Oilmite Capacitor shown below. This capacitor, impregnated and filled with mineral oil, is made with meticulous care and rated with conservatism. It is doing yeoman service as a filter condenser in secret war equipment. We welcome inquiries arising from your condenser problems.

LONG LIFE ASSURED

CHARACTERISTICS OF TOBE OIL-MITE CAPACITORS

STANDARD CAPACITY TOLERANCE = 10% RATINGS: .05 mfd. to 2.0 mfd. • 600 V.D.C. • .05 mfd. to 1.0 mfd. • 1,000 V.D.C.
TEST VOLTAGE . . . Twice D. C. rating GROUND TEST . . . 2,500 Volts D. C. POWER FACTOR . . . At 1,000 cycles—.002 to .005
SHUNT RESISTANCE . . . .05 to 0.1 mfd. • 20,000 megohms • .25 to 0.5 mfd. • 12,000 megohms • 1.0 to 2.0 mfd. • 4,000 megohms

Special units can be held to 12,000 megohms per microfad depending solely on terminal construction.

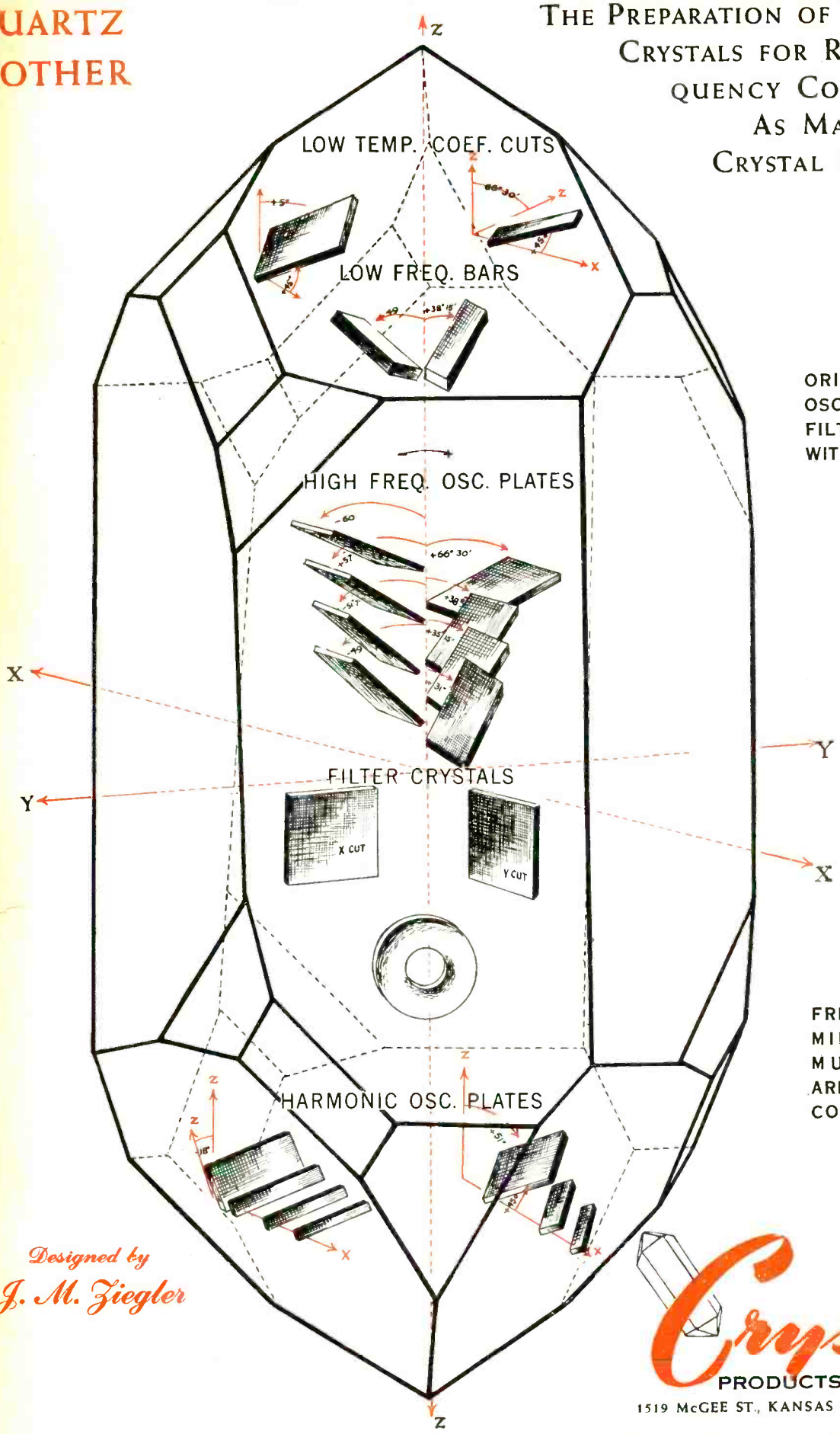
A SMALL PART IN VICTORY TODAY

TOBE DEUTSCHMANN CORP. TOBE CANTON · MASSACHUSETTS

A BIG PART IN INDUSTRY TOMORROW

QUARTZ MOTHER

THE PREPARATION OF PRECISION CRYSTALS FOR RADIO FREQUENCY CONTROL.... AS MADE BY CRYSTAL PRODUCTS



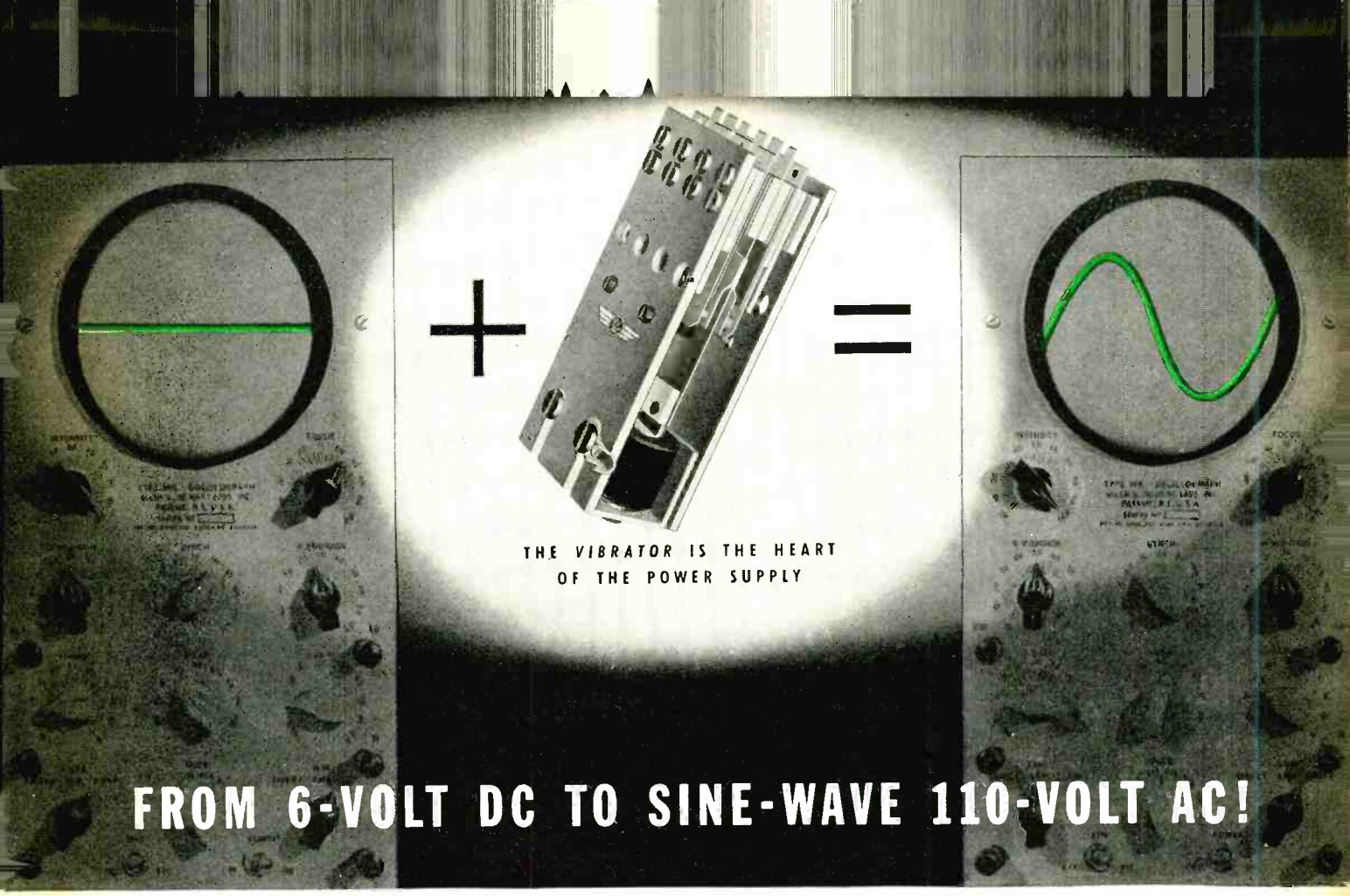
ORIENTATION OF OSCILLATOR AND FILTER CRYSTALS WITH RESPECT TO MOTHER

FREQUENCIES IN MILITARY COMMUNICATIONS ARE ACCURATELY CONTROLLED BY CRYSTALS

Designed by
J. M. Ziegler

Crystal
PRODUCTS COMPANY
1519 McGEE ST., KANSAS CITY, MISSOURI

Producers of Approved Precision Crystals for Radio Frequency Control



E·L is the Only Vibrator Converter That Can Produce This Result

All electrical engineers know that the Sine-Wave current form is more efficient than any other, particularly in the operation of motors and of test equipment.

—But, not all electrical engineers know that it is possible, with an Electronic Vibrator Power Supply, to convert DC current of almost any voltage to AC current of desired voltage and Sine-Wave form.

This is but one of an infinite number of advances which have been made by Electronic Laboratories through intensive development of the principle and technique of *vibrator type* power supplies, coupled with probably the world's most extensive research on power supply circuits. For instance: capacities up to 1,000 Watts—tremendous savings in weight—new output efficiency—close voltage regulation, to name a few.

Wherever electric current must be changed, in voltage, frequency or type—for war or peace—*E·L* Vibrator Converters will do the job more efficiently—more economically—and last longer. Electronic's engineers will be glad to work with you in meeting your current conversion needs.

Only E·L VIBRATOR POWER SUPPLIES Offer All These Advantages:

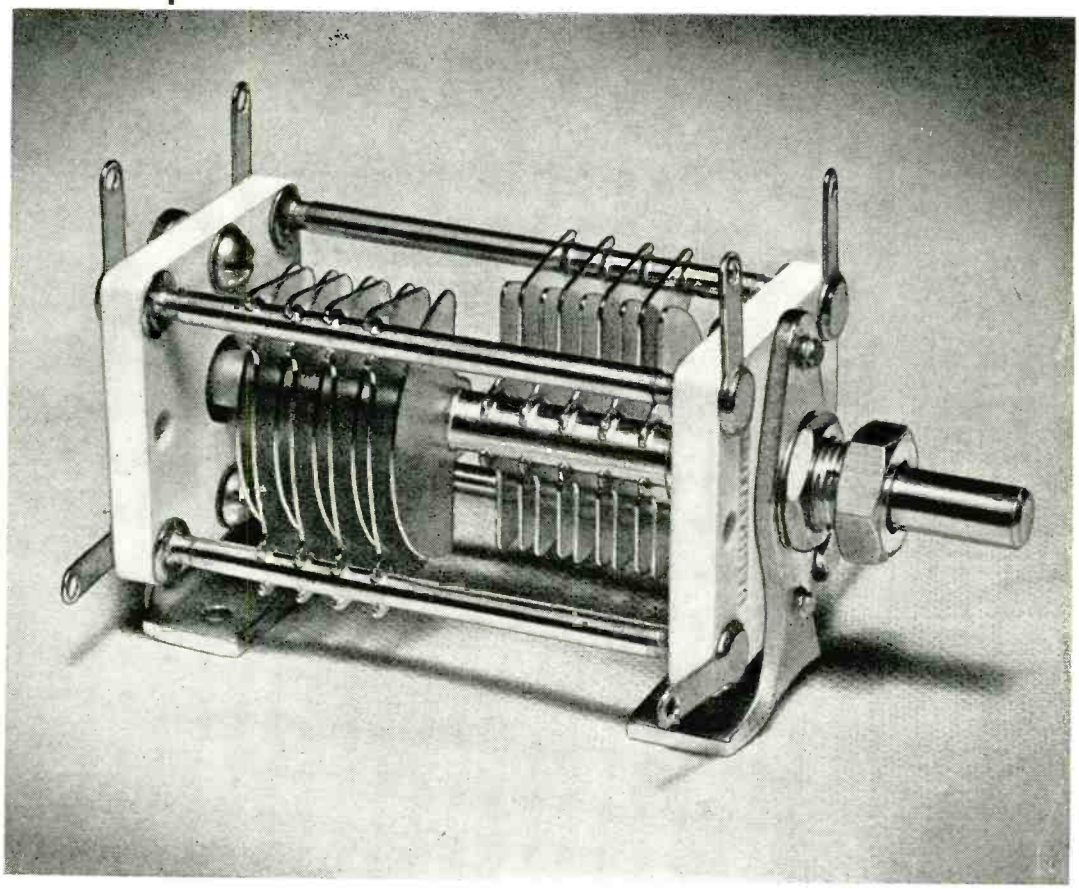
1. **CONVERSION**—DC to AC; DC to DC; AC to DC; AC to AC.
2. **CAPACITIES**—Up to 1,000 Watts.
3. **VARIABLE FREQUENCIES**—A power supply may be designed to furnish any frequency from 20 to 280 cycles, or a controlled variable output within a 5% range of the output frequency.
4. **MULTIPLE INPUTS**—For example, one E·L Power Supply, in quantity production today, operates from 6, 12, 24, 110 volts DC or 110 volts AC, and 220 volts AC, with a single stable output of 6 volts DC.
5. **MULTIPLE OUTPUTS**—Any number of output voltages may be secured from one power supply to suit individual needs.
6. **WAVE FORMS**—A vibrator power supply can be designed to provide any wave form needed for the equipment to be operated.
7. **FLEXIBLE IN SHAPE, SIZE AND WEIGHT**—The component parts of a vibrator power supply lend themselves to a variety of assembly arrangements which makes them most flexible in meeting space and weight limitations.
8. **HIGHEST EFFICIENCY**—E·L Vibrator Power Supplies provide the highest degree of efficiency available in any type power supply.
9. **COMPLETELY RELIABLE**—Use on aircraft, tanks, PT boats, "Walkie-Talkies," jeeps, peeps and other military equipment, under toughest operating conditions has demonstrated that E·L units have what it takes!
10. **MINIMUM MAINTENANCE**—There are no brushes, armatures or bearings requiring lubrication or replacement because of wear. The entire unit may be sealed against dust or moisture.

Electronic LABORATORIES, INC.

INDIANAPOLIS

E·L ELECTRICAL PRODUCTS—Vibrator Power Supplies for Communications . . . Lighting . . . Electric Motor Operation . . . Electric and Electronic Equipment on Land, Sea, or in the air.

PERMANENCE



High-stability variable condenser.

MILITARY equipment must perform continuously with a minimum of attention. Permanence of electrical and mechanical characteristics has won a high place for Hammarlund condensers.

THE HAMMARLUND MANUFACTURING CO., INC.
460 West 34th Street, New York, N. Y.

HT-4B

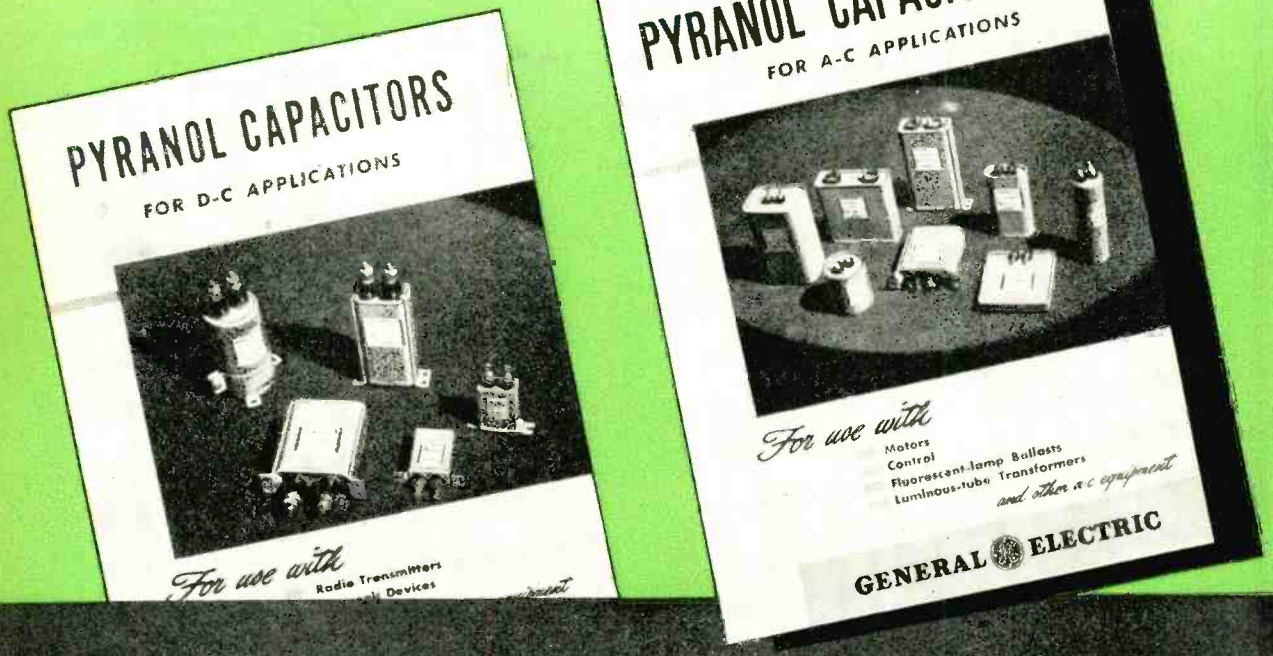
HERE is that high-powered rig you have always wanted to own . . . one that you can depend upon for peak operating efficiency. Hallicrafters have built into the HT-4B the resultant experience from years of engineering research.

Model HT-4B delivers a carrier output of 325 watts on phone and 450 watts on CW. The preamplifier supplied with the transmitter can be mounted conveniently at the operating position, controlling volume, keying and standby . . . once adjusted to any band the rig may be operated remotely.

When, once again, we are permitted to sell communications equipment for civilian use — your HT-4B will be waiting for you.

hallicrafters
CHICAGO, U. S. A.
World's largest exclusive manufacturer of short wave radio communications equipment.

YOURS FOR THE ASKING . . .



NEW, TIME-SAVING CATALOGS

on Small Pyranol Capacitors for Built-in Applications

THESE publications make it easy for you to select Pyranol* capacitors for applications such as electronic devices, communications equipment, control, motors, and transformers.

This technical information is up to the minute, easy to use. Covers all the standard types and sizes generally required—all those that have been found most desirable with respect to ratings and dimensions.

You'll find it's easy to design with G-E capacitors, because: (1) Pyranol, the treating material, makes these units small and compact—often you can reduce the size of your equipment and save critical material; (2) many of the ratings are available in cylindrical, oval, or rectangular cases; and (3) they can be operated in any position.

Get your copies of these comprehensive, time-saving publications.

**Pyranol is the G-E trade name for askarel—a synthetic, noninflammable liquid.*

VALUABLE FOR ENGINEERING, DRAFTING, OR PURCHASING DEPARTMENTS

- ★ More than 350 standard ratings to choose from
- ★ Easy-to-read, easy-to-use tables and diagrams
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- ★ Handy thumb index for quick reference

GENERAL ELECTRIC

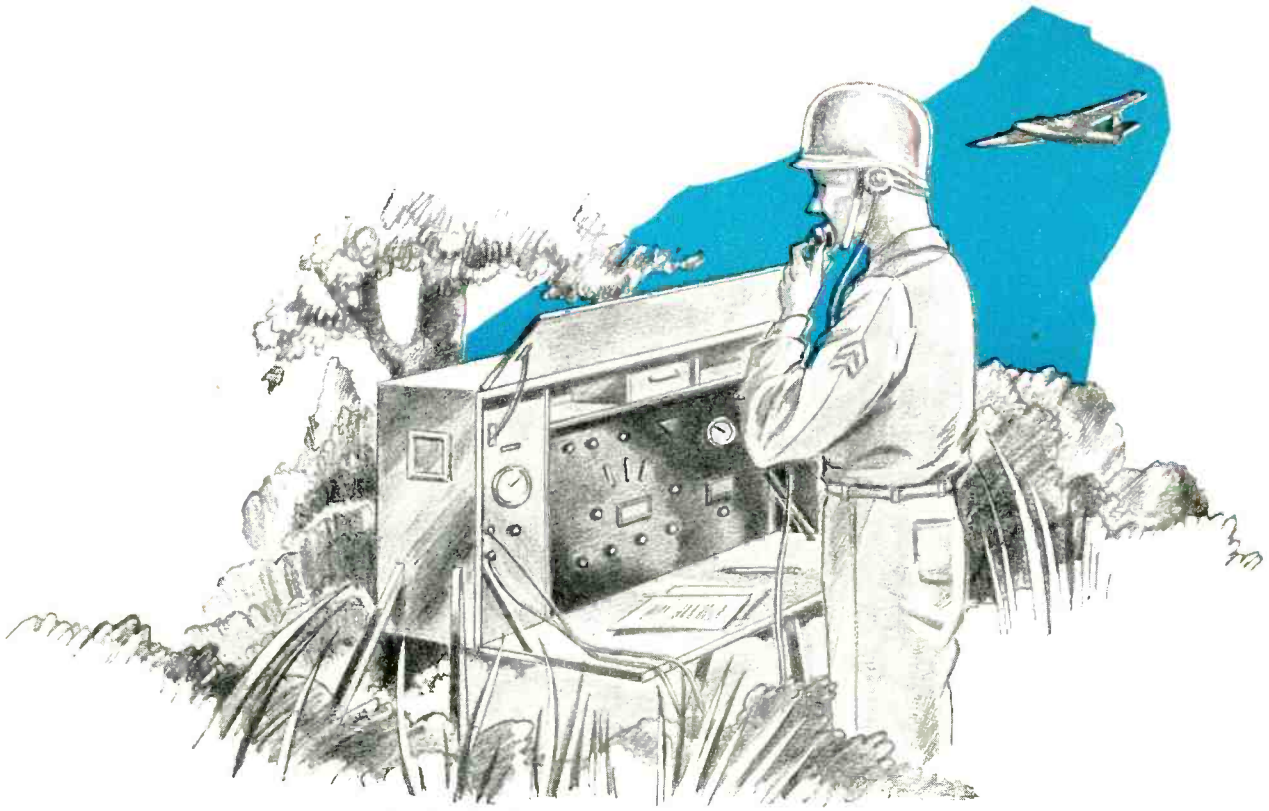
General Electric Company, Section C 407-49
Schenectady, N. Y.

Please send me complete information on small Pyranol capacitors for built-in applications.

☐ For D-c Applications (GEA-2621A)
☐ For A-c Applications (GEA-2027B)

Name.....
Company.....
Address.....
City..... State.....

5700



THE BETTER INSULATION FOR BETTER RADIOS!

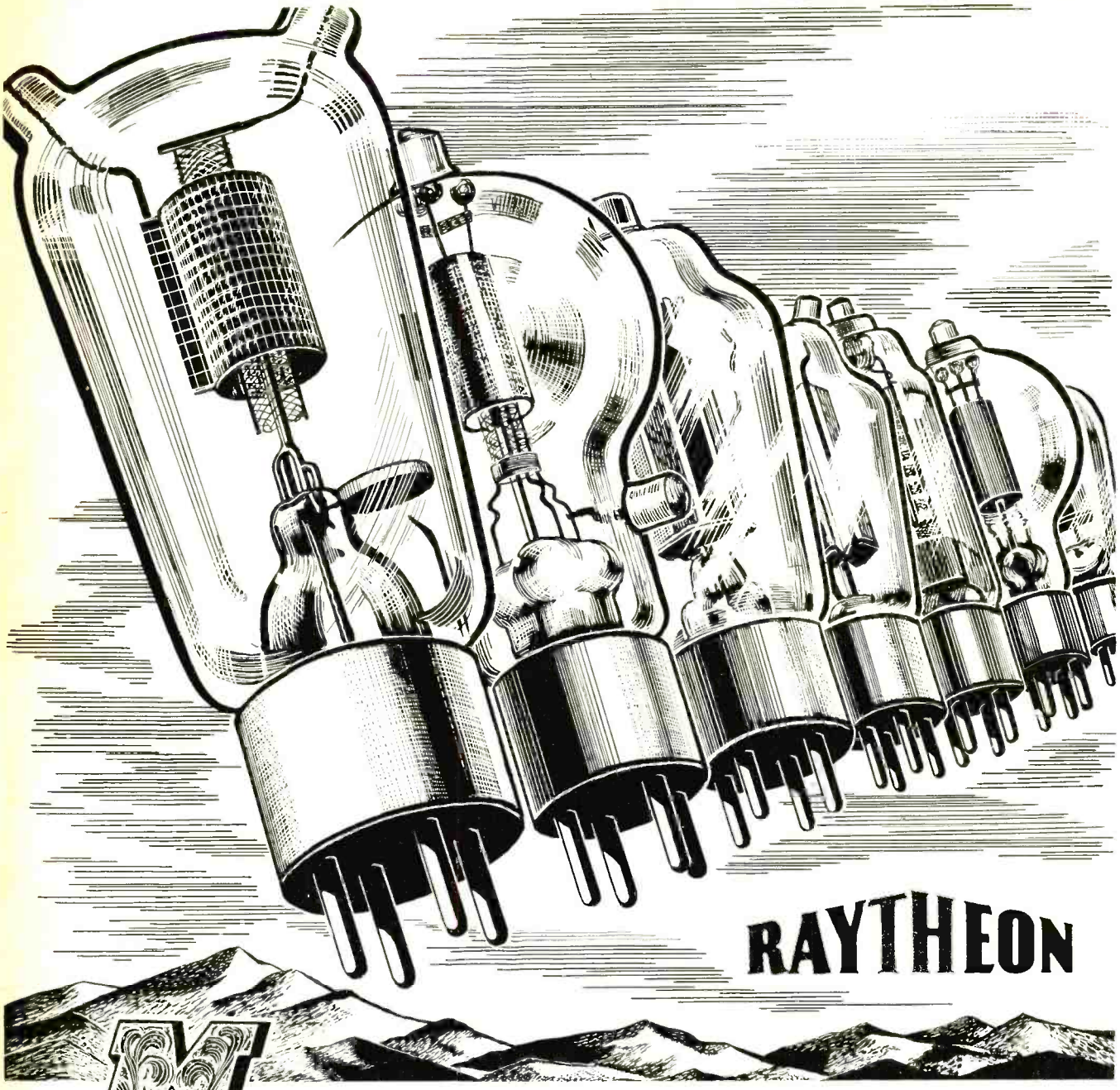
THE wartime radios that are now coming through are much better than any similar instruments that have ever been mass-produced. These better devices require better insulation—and wartime developments have enabled Formica to provide it. The new MF grades — glass mat base—are so good that they will do most of the things it was once thought necessary to use ceramics for. Yet they may be machined and worked with ordinary tools providing an adaptability that is impossible in molded forms.

For the television, radar and radio development after the war these new materials—born of new synthetic varnishes and new fibre bases—will be available for the big commercial development which is sure to follow.

ARMY E NAVY

FORMICA

THE FORMICA INSULATION COMPANY, 4661 SPRING GROVE AVE., CINCINNATI, OHIO



RAYTHEON

MILEPOSTS IN THE PROGRESS OF RESEARCH!

RAYTHEON tubes for the peacetime electronic era will incorporate all of the engineering skill gained through scientific accomplishments in wartime.

Your new RAYTHEON tubes will be adaptable to a wide scope of newly developed uses . . . with performance characteristics that have been time-tested through service in stringent military campaigns.

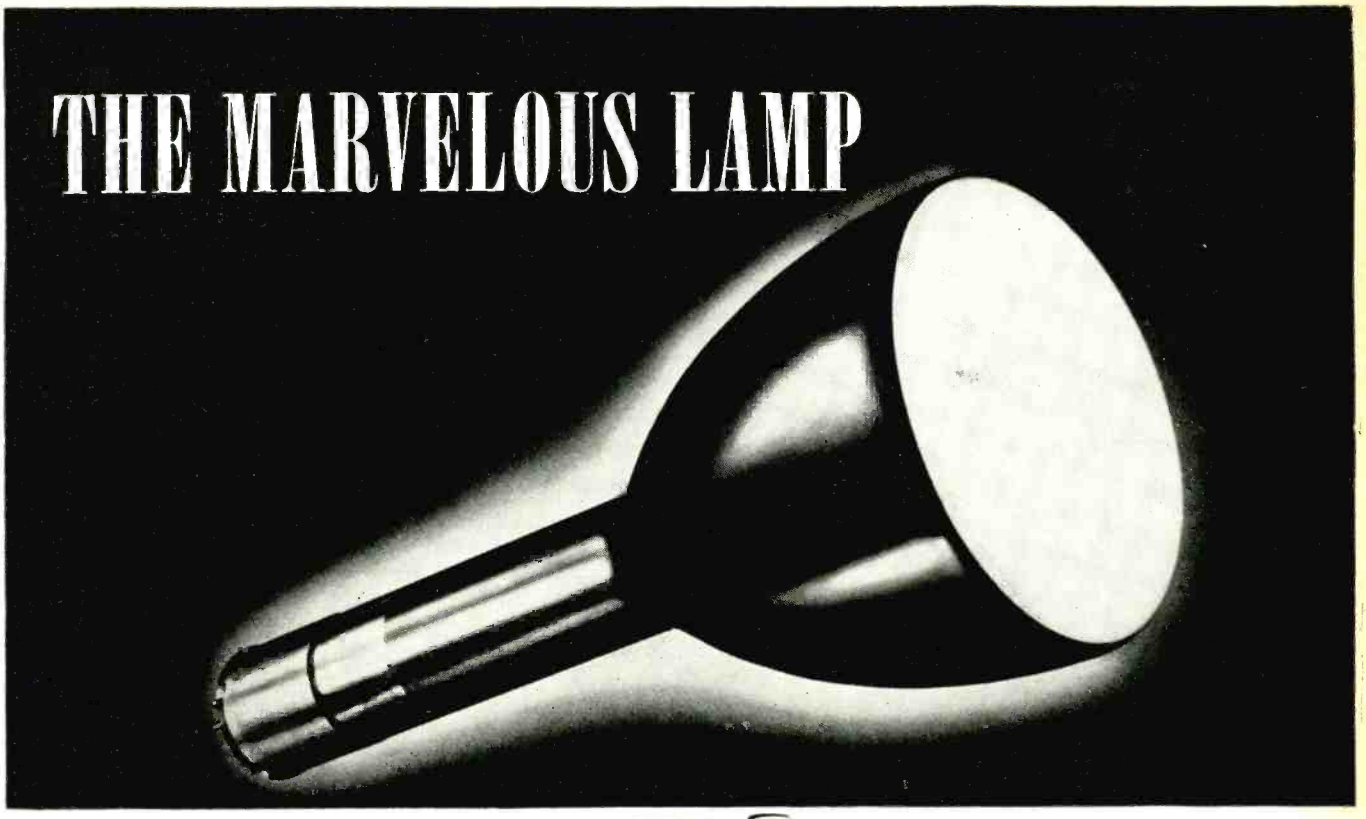
You can look to RAYTHEON leadership when you again purchase tubes . . . no matter what type of function your requirements may be . . . you will find a RAYTHEON tube designed and engineered to faithfully perform its task.

For military reasons tubes illustrated are not a new development.

Raytheon Manufacturing Company

WALTHAM AND NEWTON, MASSACHUSETTS

DEVOTED TO RESEARCH AND THE MANUFACTURE OF TUBES AND EQUIPMENT FOR THE NEW ERA OF ELECTRONICS



from Genie to Electron

● The fantasy of Aladdin's marvelous genie-commanding lamp – first conceived by the unknown author of "The Arabian Nights' Entertainments" – comes true in the cathode ray tube of today. And there are practical advantages in electrons over genii in modern life and work – in television, for example.

We go back to Aladdin's lamp, because Sylvania has specialized as a maker of marvelous lamps – and electronic tubes.

First it was the incandescent lamp.

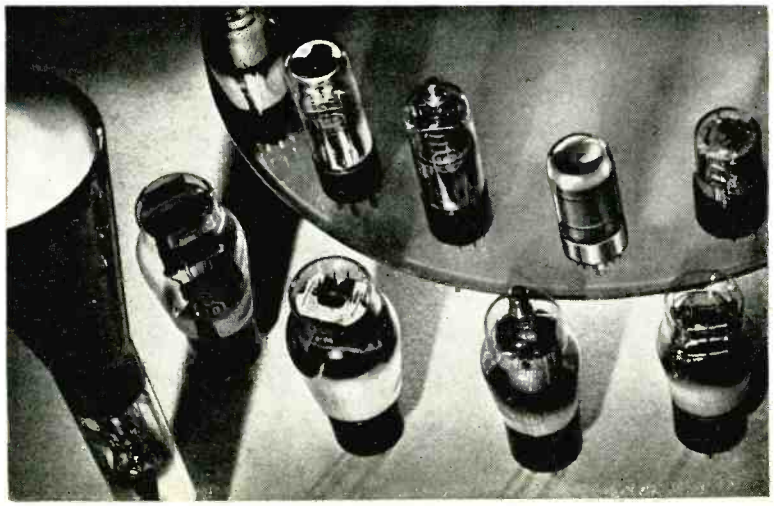
Then, in the early days of radio, we put the incandescent "Edison Effect" to work in electronic tubes.

Having attained an electronic reputation in radio research and tube manufacture, Sylvania applied this experience to the making of better artificial light as a fluorescent lamp pioneer.

In our forty years of experience, it has been a far cry from the original incandescent lamp to today's many electronic devices, which have far more possibilities than ever after a year of global war.

Today Sylvania aspires to serve the radio and electronic industries, whose wider destiny is being written in American laboratories, as a supplier of electronic tubes with hundreds of envisioned uses. Ours will be in the role of maker of these marvelous tubes – yours, their application to new products for better life and work in the peace to come.

MAKER OF ELECTRONIC TUBES FOR INDUSTRY



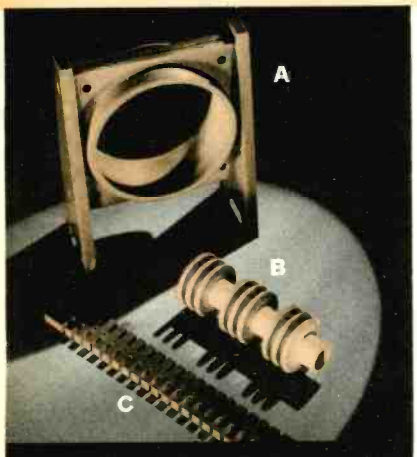
SYLVANIA

ELECTRIC PRODUCTS INC.

Emporium, Pa.

Incandescent Lamps, Fluorescent Lamps and Fixtures, Radio Tubes, Electronic Devices

Voice of the A. E. F.



A. Milled, drilled, and turned variometer stator mounting. B. Turned high-tension insulator. C. Milled and drilled spacing strip.

SECONDS after the U. S. landing in Africa, orders to troops were winging their way by portable radio. There are dozens of applications for Synthane as insulation in radio equipment of this kind. Most important use is to prevent undue loss of minute high-frequency currents.

Long before Synthane entered the armed services it was valued for its many combined properties—resistance to corrosion from solvents, acids, salts and water . . . structural strength . . . light weight (half that of aluminum) . . . hardness, excellent insulating characteristics, and ease of machining. Some day it will return again to civilian ways, with more uses, it now seems certain, than ever before. Meanwhile, keep posted on Synthane with information such as you will find on the back of this page.

SYNTHANE CORPORATION, OAKS, PENNSYLVANIA

Plan your present and future products with Synthane Technical Plastics

SHEETS • RODS • TUBES • FABRICATED PARTS **SYNTHANE** SILENT STABILIZED GEAR MATERIAL

Bakelite— laminated

Corrosion-Resisting SYNTHANE

SYNTHANE, a laminated phenolic plastic, may be more familiar to you for its physical, mechanical and electrical properties. More recently, through research and development, grades of SYNTHANE have been found of great value as corrosion-resisting materials. Parts made from SYNTHANE have successfully resisted the effects of corrosive waters and atmospheres, chemical salts and solutions, solvents, gasolines, oils, greases, and other petroleum products. The corrosion-resisting possibilities of SYNTHANE for your application may be well worth examining. Only by examination can they be accurately determined.

SYNTHANE is available in sheets, rods, and tubes, fabricated parts, and in parts made by molding the impregnated base materials.

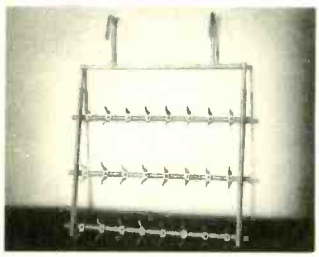
Corrosion-Resistance Factors

The corrosion resistance of any material is usually relative. The degree of corrosion resistance depends generally upon a combination of factors —the nature, concentration, and temperature of the chemical or corrosive agent, time of exposure, degree of agitation, and moisture absorption and chemical reactivity of the material itself.

For example, 10% solutions of either sulphuric acid or potassium dichromate have little effect on SYNTHANE. But if the two are mixed in the presence of organic matter, a vigorous oxidizing action occurs which will destroy any synthetic resin.

Corrosion-Resistance Economics

SYNTHANE is not immune to all corrosion conditions. Nor is any material.



Multiple-type plating rack assembled from SYNTHANE tubing

Corrosion-resisting piping and couplings made from SYNTHANE

Yet it need not be 100% corrosion-proof to be economically practical.

In many instances SYNTHANE is used—not because it is completely corrosion-proof—but because it retains its size, shape and strength and has a longer life per dollar invested than other materials, taking into consideration labor and material for the original installation and the cost of replacements.

Base Materials

Selection of the base material must be made with care since in nearly every case it is the base rather than the resin that is first affected.

Cotton cloth base is satisfactory for weak acids, weak bases and low concentrations of salts, or neutral salts in any concentration. Asbestos base is used for strong alkaline conditions or highly concentrated salt solutions which tend to hydrolyze or split into alkaline radicals. Asbestos is not recommended for acids or acid salts even in low concentrations. Glass cloth base is recommended for strong concentrations of acids or acid salts, and is excellent for those conditions. Special corrosion-resisting resins are used for corrosion-resisting SYNTHANE.

When to Use Synthane

We prefer to examine each application individually. If a previous experience does not approximate yours, laboratory and commercial tests will be made to reach a solution profitable and practical in your case.

The Effect of Chemicals

In general, any concentration and temperature up to 180° Fahr. of the salts of the following metals will not affect SYNTHANE except to produce a slight change in its color:

Aluminum	Copper	Mercury
Barium	Iron	Nickel
Bismuth	Lead	Silver
Cadmium	Magnesium	Tin
Cobalt	Manganese	Zinc

Calcium (except hypochlorite)
Potassium (except hydroxide)
Sodium (except hydroxide and hypochlorite)

Synthane Also Resists the Following Solvents:

Aliphatic hydrocarbons	Ketones at room temperature
Aromatic hydrocarbons	Alcohols, esters and ethers

Chlorinated hydrocarbons (except those which have hydrolyzed; for example, carbon tetrachloride in the presence of moisture)

Synthane Will Not Resist:

Chlorine gas, wet or dry
Sodium hypochlorite
Chlorine water
Sodium hydroxide over 2%
Potassium hydroxide over 2%
Calcium hypochlorite
Bromine and bromine water
Pyridine

SYNTHANE will resist the following acids at the concentrations noted at room temperature:

Acetic 50%	Formic conc.
Benzoic conc.	Hydrochloric 10%
Boric conc.	Hydrofluoric 20%
Phenol 10%	Lactic conc.
Chromic 45% (special resin required; intermittent exposure as in plating)	Nitric 2%
	Oleic 5%
	Oxalic conc.
	Phosphoric 10%
	Sulphuric 15%
	Sulphurous 6%

Citric conc.

Note: The addition of salts such as 20% sodium sulphate to 10% sulphuric acid is known to inhibit the effect of the acid for a long period of time.

A mixture of sodium hydroxide 10% and sodium cyanide 10% also shows this phenomenon. This concentration of sodium hydroxide alone would rapidly attack SYNTHANE.

Standards of Quality Corrosion-Resisting Synthane Sheets

GRADE	C-CR Coarse Weave Fabric Base	L-CR Fine Weave Fabric Base	AA-CR Asbestos Cloth Base	A-CR Asbestos Paper Base	GLF Glass Cloth Base
TENSILE STRENGTH (1) Lbs./Sq. In.	9,500	9,000	10,000	8,000	16,000
TRANSVERSE STRENGTH (1) Lbs./Sq. In.	20,000	20,000	20,000	16,000	20,000
COMPRESSIVE STRENGTH (1) Lbs./Sq. In.	38,000	35,000	38,000	36,000	40,000
DIELECTRIC STRENGTH (2) Volts per mil (.001") Short-Time Test	200	200	50	225	350
DIELECTRIC STRENGTH (2) Volts per mil (.001") Step-by-Step Test	120	120	30	135	250
POWER FACTOR (3) at 1,000,000 Cycles	.10	.10	.15	.10	.026
DIELECTRIC CONSTANT (3) at 1,000,000 Cycles	7.0	7.0	7.5	7.0	5.9
DIELECTRIC LOSS FACTOR (3) at 1,000,000 Cycles	.70	.70	1.12	.70	.10-.25
% WATER ABSORPTION (4)	1.7	1.4	.85	.85	1.2
ROCKWELL HARDNESS	M105	M105	M110	M110	M115

The values above represent average for standard grades.

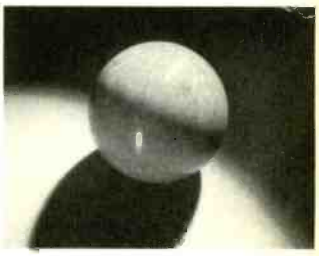
Methods Used in Testing Synthane

(1) Tests were made on $\frac{1}{8}$" thickness at room temperature, approximately 25 deg. C., following the American Society for Testing Materials Method D-229-42.

(2) Tests were made under oil on $\frac{1}{16}$" thickness, according to American Society for Testing Materials Method D-149-40T. (For grade AA-CR, $\frac{1}{8}$" thickness was used.)

(3) Tests were made on $\frac{1}{16}$" thickness at a frequency of 1,000,000 cycles, according to American Society for Testing Materials Method D-150-42T.

(4) Tests were made on pieces 3" x 1" x $\frac{1}{8}$" thick, according to the American Society for Testing Materials Method D-229-42 after immersion in water for 24 hours at approximately 25 deg. C plus or minus 2 deg. C.



SYNTHANE molded-macerated valve ball for oil well equipment

Washers and molded-macerated gears for rayon machinery

PLAN YOUR PRESENT AND FUTURE PRODUCTS WITH SYNTHANE TECHNICAL PLASTICS

SYNTHANE
Bakelite — laminated

SHEETS•RODS•TUBES•FABRICATED PARTS•SILENT STABILIZED GEAR MATERIAL

SYNTHANE CORPORATION, OAKS, PENNA.

REPRESENTATIVES IN ALL PRINCIPAL CITIES

On Time! QUICKER DELIVERY FOR STEATITE INSULATORS

Not so long ago, an order for Steatite Insulators brought a sympathetic shrug of the shoulders and a "Sorry, five to six months delivery." We did not like to tell our customers that. We did not like it because we knew how badly Steatite was needed for the war effort.

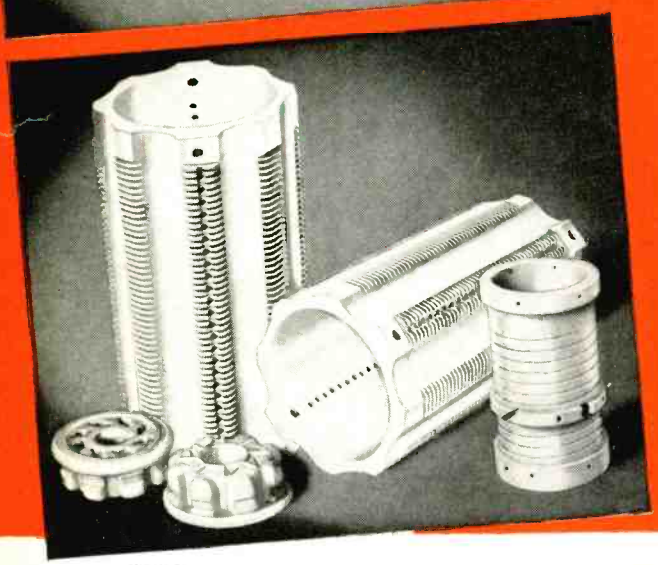
This is what we did to quicken deliveries of Steatite Insulators.

- Expanded our plant facilities.
- Enlarged our staff of engineers and technicians.
- Devised improved methods of production.

As a result, there rolls from our kilns every month increasing quantities of insulators. Gradually, but surely the backlog of orders was reduced. Now we can promise our customers deliveries on standard parts from stock in a reasonably short time.

If you have any insulator problem—whether specialized or standard — we would like a shot at it. You can rest assured that your requirements will receive prompt, individual attention.

Above . . . stock insulators such as these are now available in quantity for prompt delivery. Write for data concerning the many different types of Steatite Insulators.



Left . . . these coil forms and insulators were designed and pressed for special applications where stock insulators would not serve. They are working examples of the engineering skill available for your special insulator problem.

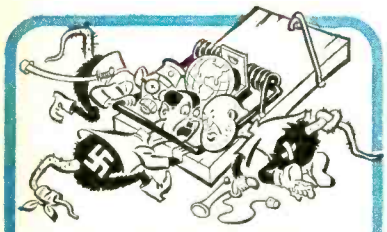
General Ceramics

GENERAL CERAMICS AND STEATITE CORPORATION — STEATITE INSULATORS

AND STEATITE CORP.

KEASBEY NEW JERSEY

Some Evening, Spring This on Yourself

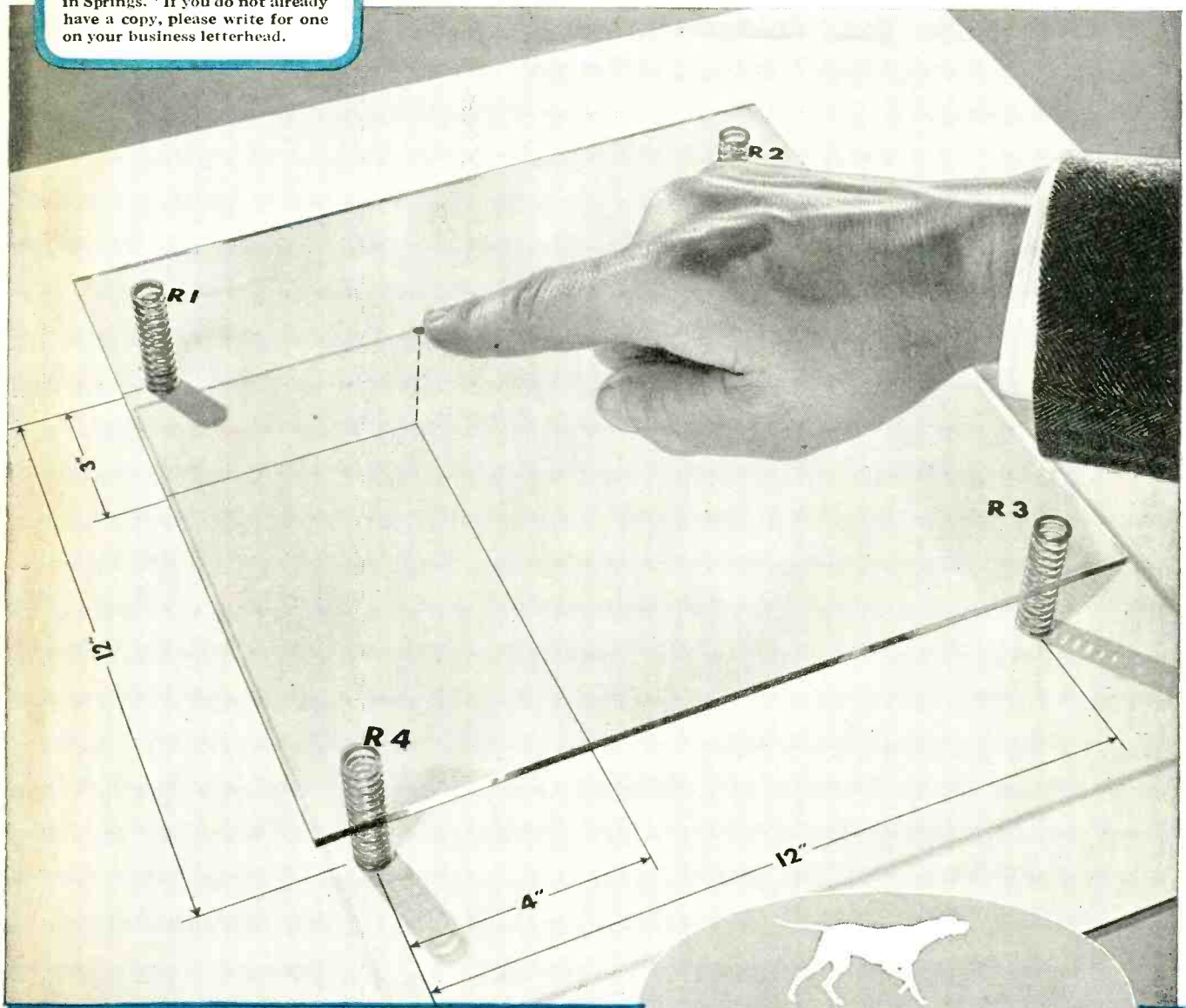


ACH, SCHPRINGTIME!

We don't make the type of spring required above, but we do design and make many another needed for war equipment to catch the Japanazis. Many important curves, charts, and formulas for developing essential springs are contained in our booklet, "Science in Springs." If you do not already have a copy, please write for one on your business letterhead.

LIKE brain-twisters? Some evening, then, when you're in the mood, take a crack at this one: Imagine a square plane supported at the corners by equal springs. Place your finger at any point on the board and press downward. For the sake of argument, assume you push with a force of ten pounds, that the springs are centered, a foot apart and the spot you have pressed upon is 3″ one way and 2″ the other way from the center. Can you figure the proportion of the load shared by each spring? The practical equivalent of the problem is found, for example, in the design of springs for applications requiring vibration or shock isolation. The answer looks deceptively easy, but it will challenge you, may even plague you. From a spring maker's viewpoint it is a problem of springs working in combination, a worthy example of our experienced knowledge that there is only ONE right spring for your job. We can produce it for you.

WHAT DO YOU NEED? . . . *A spring manufacturer with adequate capacity to do your job now? Help in designing springs as well as manufacture? If it's essential for the war, get in touch with us.*



HUNTER
Science in Springs

HUNTER PRESSED STEEL COMPANY, LANSDALE, PENNA.

"Cruiser and transport ahead . . . *LET'S TAKE 'EM!*"

Messages like these "must go through," and to make certain they do, the communication systems in our Army and Navy aircraft are as sensitive, as rugged, and as trouble-defying as advanced design and precision manufacturing methods can make them.

Producing transformers, headsets and other communications equipment for the Army and Navy Air Forces is ROLA's present responsibility to the war program. To keep abreast . . . and ahead . . . of demands, new machines have been designed, new methods devised, new tests and inspections applied. Facilities have been expanded, and production vastly increased.

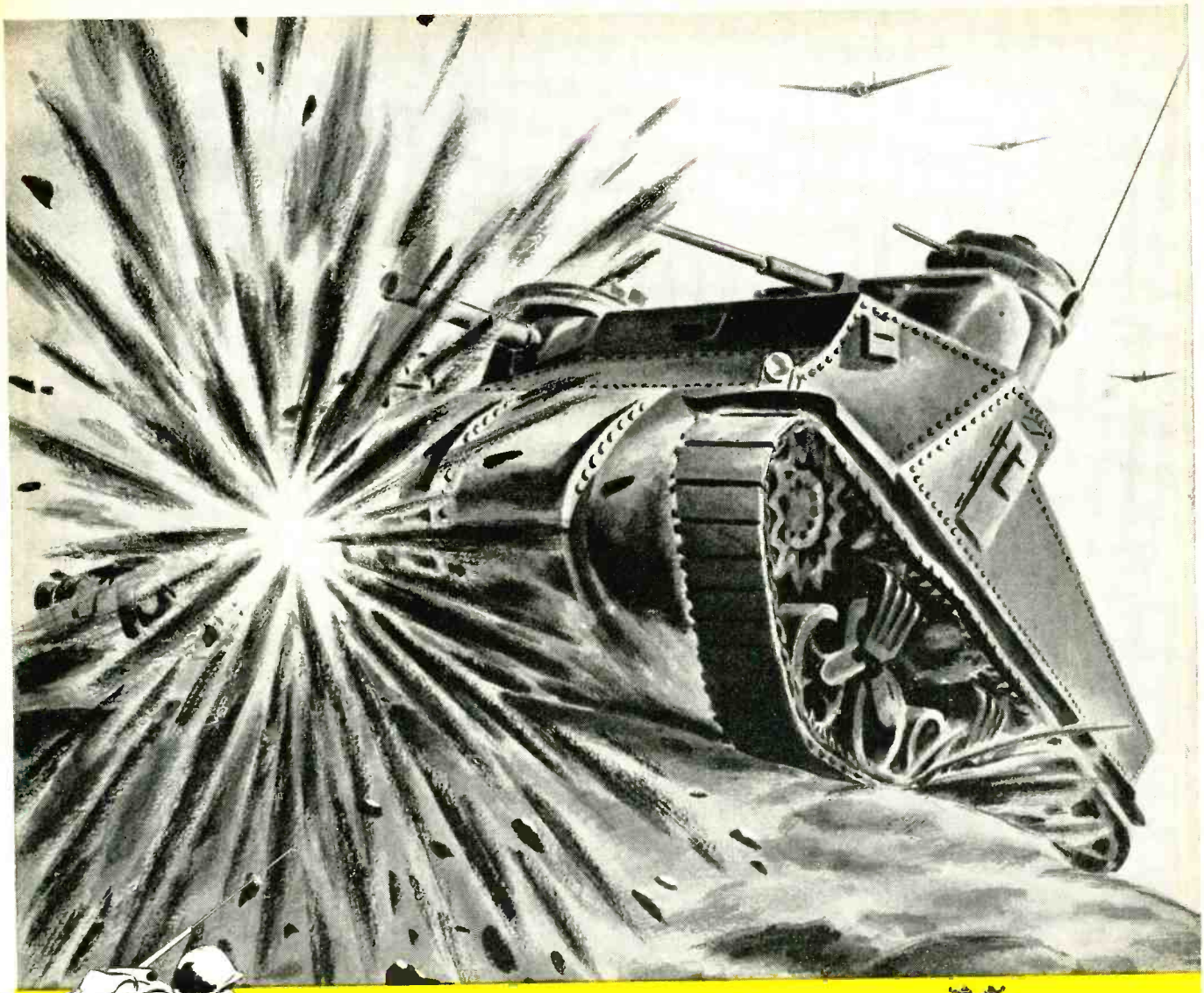
All this is important to peacetime users of ROLA equipment, for it is only logical to believe that the research and the skill and the equipment inspired by wartime necessity will find important application in the Electronic World of Tomorrow.

* * *

The "know how," gained through twenty years of leadership in the radio field, has enabled ROLA to meet . . . and exceed . . . every war demand made upon it, both as prime and as subcontractor. We have facilities available for additional contracts. If you are interested, we suggest you write us . . . or ask our representative to call. THE ROLA COMPANY, Inc., 2530 Superior Avenue, Cleveland, Ohio.

★ ROLA ★

MAKERS OF THE FINEST IN SOUND REPRODUCING AND ELECTRONIC EQUIPMENT



"that darned walkie-talkie S-S-STUTTERED"

Stutterers don't give commands in the Signal Corps. In the stress of battle you can't have a man who stammers. Neither can you have equipment that will fail at the critical moment. Not when seconds mean the difference between success or failure in battle.

With men's lives at stake, you can't afford to use anything less than the best. When a design calls for Capacitors, specify C-Ds. Thirty-three years devoted to the exclusive manufacture of capacitors is your assurance of absolute reliability. Our Engineering department will be glad to cooperate with you. Cornell-Dubilier Electric Corporation, South Plainfield, New Jersey.

DYKANOL FILTER CAPACITORS

Type TQ

The Type TQ Dykanol Filter Capacitors have been designed for low power transmitters, high power public address systems and portable power amplifiers. Several of the more important features are listed below:

Impregnated and filled with Dykanol — a non-inflammable, high dielectric impregnant of stable characteristics.

Dried, impregnated and filled under continuous vacuum.

Hermetically sealed — these Capacitors are not affected by moisture, time or temperature up to approximately 200° F.

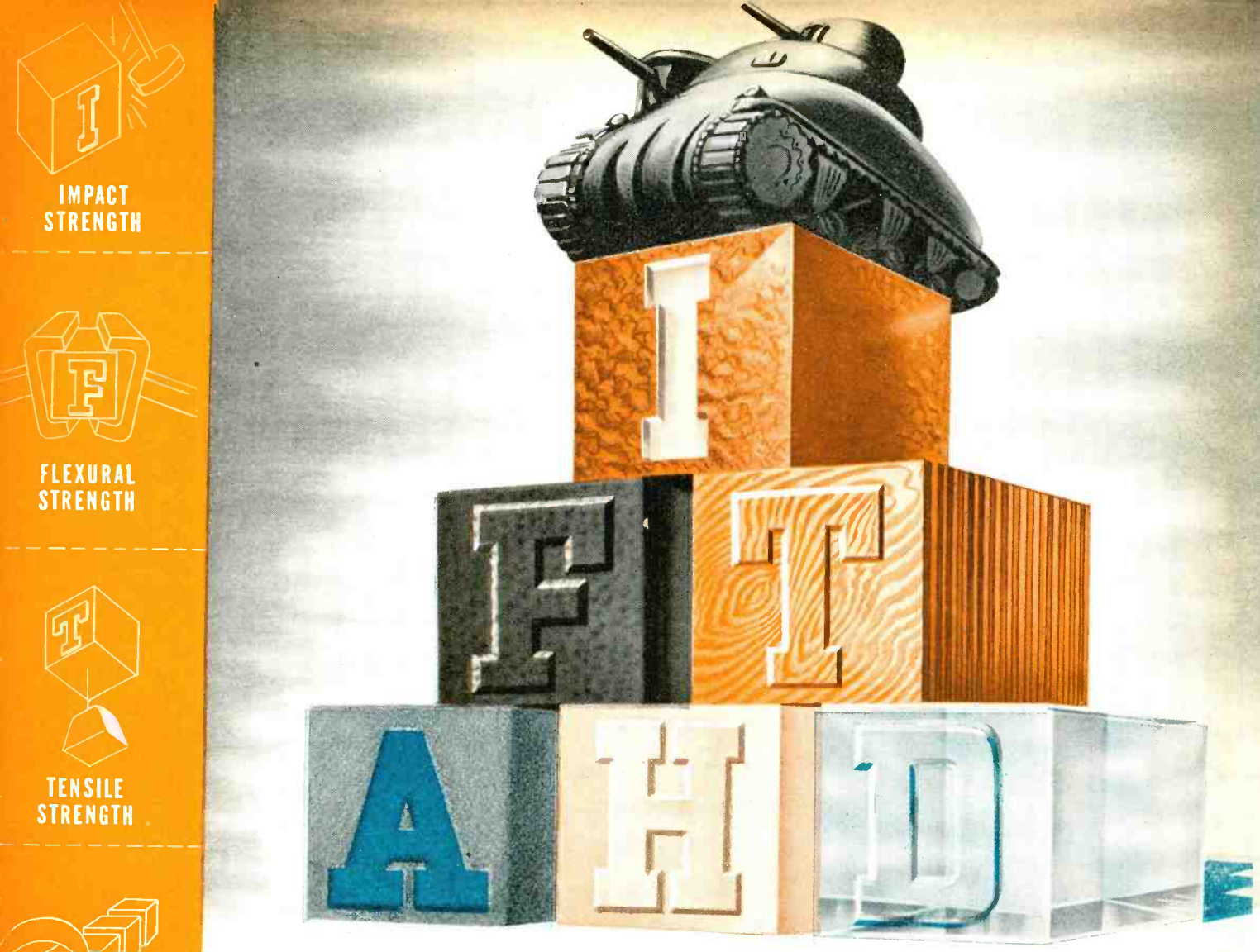
Conservatively rated — can be safely operated continuously at 10% above rated voltage.

For further details write for Catalog No. 160T.

Cornell-Dubilier capacitors

MORE IN USE TODAY THAN ANY OTHER MAKE.

MICA • DYKANOL • PAPER • WET AND DRY ELECTROLYTICS



PHYSICAL PROPERTIES OF "BAKELITE" PLASTICS

that mean Fighting Strength

THE SEVERE SERVICE under which equipment must operate today puts heavy demands on plastic materials. In many instances, plastic parts must possess not only high tensile strength, but impact resistance and hardness as well. Other parts may require high flexural strength combined with dimensional stability and wear and abrasion resistance. Thus the designer and engineer, in selecting plastics, must constantly keep in mind the correct balance of *all* these physical properties.

The problem may be the selection of a BAKELITE Plastic material possessing high impact resistance, with tensile or flexural strength requirements running a very close second. On the basis of impact resistance alone, it might seem advisable to choose a high-impact BAKELITE Phenolic Molding Material. But such a material might not meet tensile strength requirements! On the other hand, a general-purpose BAKELITE Phenolic that possesses the required tensile strength can have as little as 1/18 the shock resistance of the high-impact material! In such a case, final choice of material may lie between the two extremes.

The design of the part has a lot to do with its ultimate strength characteristics. Frequently, BAKELITE Molding Boards and Blanks are used in conjunction with general-purpose phenolic plastics to provide reinforcement around inserts, and at corners, shoulders, and other points that are subjected to severe service. Mechanical strength may also be improved by increasing wall thickness, or by making adjustments in fabricating techniques.

Apart from these physical properties, mechanical strength can also be interpreted in terms of *toughness*, particularly with flexible plastics that are not usually tested for impact resistance. *Mechanical fatigue* may also become a major problem where plastics are placed under load, or are subjected to repeated blows, or to continued flexing.

On the facing page are presented the outstanding physical properties of those BAKELITE Plastics of primary importance to war production. Later messages will deal with the chemical, electrical, and thermal properties. For more detailed information write for a copy of Booklet 7—"A Simplified Guide to BAKELITE Plastics."

BAKELITE CORPORATION, 30 E. 42nd St., New York
Unit of Union Carbide and Carbon Corporation

UCC

BAKELITE

The word "Bakelite" and the identifying products Symbol are registered trade-marks of Bakelite Corporation

PLASTICS HEADQUARTERS

Physical Properties of "Bakelite" MOLDING MATERIALS

Thermosetting General-Purpose Phenolics

These materials provide well-balanced combinations of dimensional stability and other physical properties suitable for everyday requirements. *Impact strength:* 0.26 to 0.40 foot-pounds per inch of notch (Izod). *Tensile strength:* 6,500 to 8,500 pounds per square inch. *Flexural strength:* 8,800 to 13,000 pounds per square inch.

Thermosetting Shock-Resistant Phenolics

Four types, offering a wide range of physical properties. All types are dimensionally stable, and resistant to wear and abrasion. Depending upon type, *impact strength:* from 0.46 to 5.4 foot-pounds per inch of notch (Izod); *tensile strength:* from 5,300 to 8,500 pounds per square inch; *flexural strength:* from 6,300 to 11,000 pounds per square inch.

Thermosetting Phenolic Molding Boards and Blanks

These are medium-high, impact materials that may be used in molds built for general-purpose phenolics. Can be used alone, or with other plastics to provide reinforcement at vital points. Supplied as board stock or as blanks approximating shape of finished part. Also sold in diced form suitable for automatic preforming. Depending upon type, *impact strength:* from 1.6 to 2.0 (with grain) and 0.6 to 0.9 (against grain) foot-pounds per inch of notch (Izod); *tensile strength:* from 3,000 to 11,000 pounds per square inch; *flexural strength:* from 8,400 to 25,000 pounds per square inch.

Special Phenolics

This group comprises a variety of dimensionally stable, thermosetting materials, for special requirements of heat resistance, low power factor, chemical and water resistance, low friction coefficient, opacity to X-rays, and transparency.

Thermosetting Ureas

Most color stable and hardest of all thermosetting plastics. *Impact strength:* from 0.30 to 0.36 foot-pounds per inch of notch (Izod); *tensile strength:* from 9,500 to 12,000 pounds per square inch; *flexural strength:* from 10,000 to 14,000 pounds per square inch.

Thermoplastic Cellulose Acetates

Two types—Class I, general purpose, for compression and injection molding, and Class II, heat- and water-resistant, for injection molding only. Both types noted for high impact strength, toughness, and wide color range. *Impact strength:* from 1.4 to 4.0 foot-pounds per inch of notch (Izod); *tensile strength:* from 2,500 to 9,500 pounds per square inch; *flexural strength:* from 5,000 to 15,000 pounds per square inch.

Thermoplastic Polystyrenes

Outstanding in dimensional stability, chemical resistance, and dielectric qualities. For compression as well as injection molding. Supplied as crystal-clear material, and in transparent and translucent colors. *Impact strength:* from 0.40 to 0.70 (compression-molded), 0.8 to 1.2 (injection-molded) foot-pounds per inch of notch (Izod); *tensile strength:* 5,500 to 6,500 (compression), 6,500 to 7,000 (injection) pounds per square inch; *flexural strength:* 6,500 to 7,500 (compression), 14,000 to 19,000 (injection) pounds per square inch.

Physical Properties of Laminated Plastics made with "Bakelite" LAMINATING VARNISHES

BAKELITE Laminating Varnishes are used in the production of paper-base and fabric-base laminated sheets, tubes, and rods. Laminated plastics made from these varnishes possess excellent dimensional stability, high impact, tensile, and flexural strength, and are extremely resistant to wear and abrasion. In addition, they offer an unusual combination of other properties such as high dielectric strength, resistance to corrosion, and immunity to water, brine, oil, ordinary solvents, most acids, and weak alkalies.

Physical Values

Tensile strength of standard paper-base grades ranges from 7,000 to 12,500 pounds per square inch; flexural strength (transverse), from 15,000 to 21,000 pounds per square inch; and compressive strength, from 22,000 to 36,000 pounds per square inch. For standard fabric-base grades, tensile strength ranges from 8,000 to 10,000 pounds per square inch; flexural strength (transverse), from 17,000 to 20,000 pounds per square inch; and compressive strength, from 35,000 to 38,000 pounds per square inch.

Sheets, Rods, Tubes, Special Shapes

Laminated sheet stock and gear stock is supplied by laminators and fabricators in various thicknesses and sizes. Tubing can be obtained in lengths from 36 inches, with I.D. from 3/16 of an inch to 72 inches. Larger tubing can be made for special requirements. Rods come in standard lengths up to 48 inches, and in diameters from 1/8 of an inch to 4 inches. Special shapes are made to order.

Special Types

In addition, special laminated plastics have been developed for specific mechanical requirements. Molded-laminated plastics permit the manufacture of such unusually tough and wear-resistant products as heavy-duty bearings. Rubber-laminated plastics combine the rigidity and mechanical strength of laminated plastics with the vibration-absorbing qualities of the rubber interlayer. Tough, densified-laminated woods also are made possible by impregnating wood veneers with a laminating varnish and subsequently applying heat and pressure.

Physical Properties of "Bakelite" BONDING MATERIALS

Phenolic and Urea Resin Wood Glues

For bonding plywood and other wood products. Glue line is dimensionally stable under extreme conditions of heat, cold, moisture, and impact shocks. Bonded woods are resistant to mould growth.

Resin Cements for Lamp Basing

Because of their dimensional stability when subjected to heat, BAKELITE Resin Cements are used widely to set electric light bulbs and radio tubes in their metal or plastic bases. Mechanical shock or vibration does not impair the bond.

Resin Cements for Bristle Setting

A tough, tenacious bond for bristles used in brushes of all types is provided with BAKELITE Resin Cements. The bond obtained is unaffected by constant use, or by frequent cleaning in water or solvents.

Bonding Resins for Glass and Mineral Wool

To form glass, rock, and mineral wool into easily handled, dimensionally stable insulation batts, the fibers are bonded together with BAKELITE Resins. Heat cold, and moisture do not affect bonding strength.

Bonding Resins for Abrasive Products

Abrasive grit used to form high-speed grinding and cut-off wheels is securely bonded with BAKELITE Resins. This tough, strong bond has made it possible to operate grinding wheels safely, at speeds considerably higher than with other bonds.

Resins for Brake Linings

Both woven and molded brake linings are processed with BAKELITE Resin for greater toughness, dimensional stability, and resistance to wear and heat.

Physical Properties of SURFACE COATINGS *made with "Bakelite" Resins*

BAKELITE Synthetic Resins, when formulated into protective coatings, provide such properties as durability, faster drying speed, toughness, hardness or flexibility, resistance to wear and abrasion, and resistance to water and chemicals.

Phenolic Resins

For fortifying paints, primers, varnishes, and enamels of all types. Outstanding are the para-phenyl-phenol type of resins BR-17000 and BR-254, which have established new standards of durability for government and industrial specification coatings. Numerous other BAKELITE Phenolic Resins are serving widely diversified coating requirements. Certain types are used to fortify non-phenolic coatings to improve performance.

Dispersion Resins

These resins provide coatings with an unusual combination of properties—extremely fast drying time and maximum resistance to moisture. Such coatings dry as fast as *one minute*, entirely by solvent evaporation, without need of baking treatment. Because they are non-oxidizing, they do not become brittle after long years of service. They are especially useful as primers for ferrous and non-ferrous metals, particularly aluminum and magnesium alloys.

Baking Resins

For hard, abrasion-resistant coatings for lining cans, drums, and tanks. Baked on immediately after application, they provide high resistance to heat, chemicals, and moisture. Equipment need not be dismantled nor shipped out of the plant; the coatings can he applied, *right on the job*, by means of special, portable baking apparatus.

C-9 Resins

For coatings on cloth, paper, concrete, plaster, brick, plastics, wood, and metal, these versatile resins contribute many unusual physical properties. They are noted for their adhesion and long retention of flexibility. In wet scrub tests, water-emulsion paints made with them far exceed durability required in government specifications. Baking enamels based on them do not blister or flake even when immediately plunged into cold water after long baking.

Physical Properties of "Bakelite" IMPREGNATING, SEALING, and CALENDERING MATERIALS

Calendering Resins for Cloth

Cloth calendered with BAKELITE Resins gains added toughness with little or no sacrifice in flexibility. The resins impart a high order of resistance to water, chemicals, and heat.

Resins for Wood Densifying and Stabilizing

The many important advantages of wood are supplemented by high mechanical strength and excellent resistance properties when impregnated with BAKELITE Resins. In particular, the moisture content of wood veneers can be stabilized by such treatment. Impregnated veneers can be compressed into densified wood, known as "compreg," with specific gravity up to 1.37. On parallel-grained specimens, modulus of rupture can reach 38,000 pounds per square inch (with grain), and compressive strength 25,000 pounds per square inch (with grain). "Compreg" is fire retardant, has excellent aging properties, and is resistant to sulphuric and hydrochloric acid solutions.

Sealing Solutions for Castings

Castings ordinarily rejected for porosity and small blowholes are reclaimed by forcing BAKELITE Sealing Solutions into the pores under pressure, and then baking. The sealing solution thus becomes exceedingly hard and tough, unaffected by hot or cold water, steam, oils, chemicals, or heat up to 400 deg. F.

Impregnating Varnishes for Windings

As protective coatings and insulating bonds for coils, armatures, and windings, BAKELITE Varnishes remain stable and hard despite elevated operating temperatures and high rotational speeds. Better mechanical strength is also obtained.

For the Shapes of Things to Come—

You'll want this Information

That answer to "what material?" will be as important to post-war products as it is today. For both immediate and long-range planning avail yourself now of the latest informative data on C-D's wide range of NON-metallics . . . Dilecto laminated and Celoron molded phenolic plastics, Diamond Vulcanized Fibre, Micabond, Vulcoid and Dilectene. Bulletin GF may contain the one and only answer to "What Material?" . . . Write for it today.

Continental-Diamond FIBRE COMPANY

Established 1895 . . Manufacturers of Laminated Plastics since 1911 — NEWARK • DELAWARE

Neither were planned for war

We're not raising new generations to die on battlefields; we're not designing implements for future wars. We Americans are a peace and freedom-loving lot, with an economy that is geared to the home . . . washing machines, automobiles, radio . . .

But we first must finish an unpleasant job of blasting the daylights out of those who deliberately attacked our way of life. For that purpose, we've given our men. And our men are getting the very best tools for that piece of grim business.

We thank heaven that change, progress and mass production are an integral part of a system that enabled us to redesign our products for military applications. True, our new designs were speeded by war necessity—but we like to think of these latest Electro-Voice microphones as no different from the others in our evolutionary scale.

For, as eagerly as any soldier on a fighting front, we retain a vision of returning again to our natural mode of living. We plan to build better microphones for civilian communication . . . for music . . . for laughter . . .

Electro-Voice MICROPHONES

ELECTRO-VOICE MANUFACTURING CO., INC. 1239 SOUTH BEND AVENUE, SOUTH BEND, INDIANA

Dunco Quality
INDUSTRIAL CONTROL RELAYS

Although Struthers Dunn, Inc. makes many more complicated, and therefore more "spectacular," relay types, there are none in which Dunco design and manufacturing care have proved more effective than in these Industrial Control and Power Transfer types commonly used for controlling motors, heats, lights, and for other industrial tasks.

Their success over a long period of time has been largely a matter of refinement of every detail having a bearing on performance and dependability—and topping this off with individual adjustment plus two separate inspections before shipment.

Dunco Industrial Control and Transfer Relays are made in many types and with mounting styles for almost any application.

WRITE for your copy of the Dunco Relay-Timer Catalog and Data Book. Contains details on the largest line of high-quality Relays and Timers, as well as helpful engineering information.

STRUTHERS DUNN, Inc.

1321 ARCH STREET PHILADELPHIA, PA.

LET DUNCO DISTRICT ENGINEERS IN 28 CITIES HELP SOLVE YOUR RELAY-TIMER PROBLEMS

War jobs have posed infinite production problems.

We know a lot of them that were solved with as simple a thing as a nut.

Because the solution was an Elastic Stop Nut.

For example, aircraft. Their very worth depends upon fastenings that grip sure and won't shake loose under the chatter of machine guns, the impact of cannon fire and the vibration of air combat.

Every plane streaming off America's production lines has Elastic Stop Nuts fastening important structural parts. Several millions of them go into aircraft every day.

And to our knowledge, not one has ever failed to do its job.

With two big plants running full-tilt 24 hours a day, we can't satisfy all the needs of today's one big customer.

But in the days ahead, with Elastic Stop Nuts generally available, peacetime products and their production are going to be better.

And our engineers schooled in solving the rigorous problems of war production will be at the service of manufacturers with fastening requirements.

Whenever you wish, they will be ready to share their knowledge with you and recommend the desirable Elastic Stop Nut.

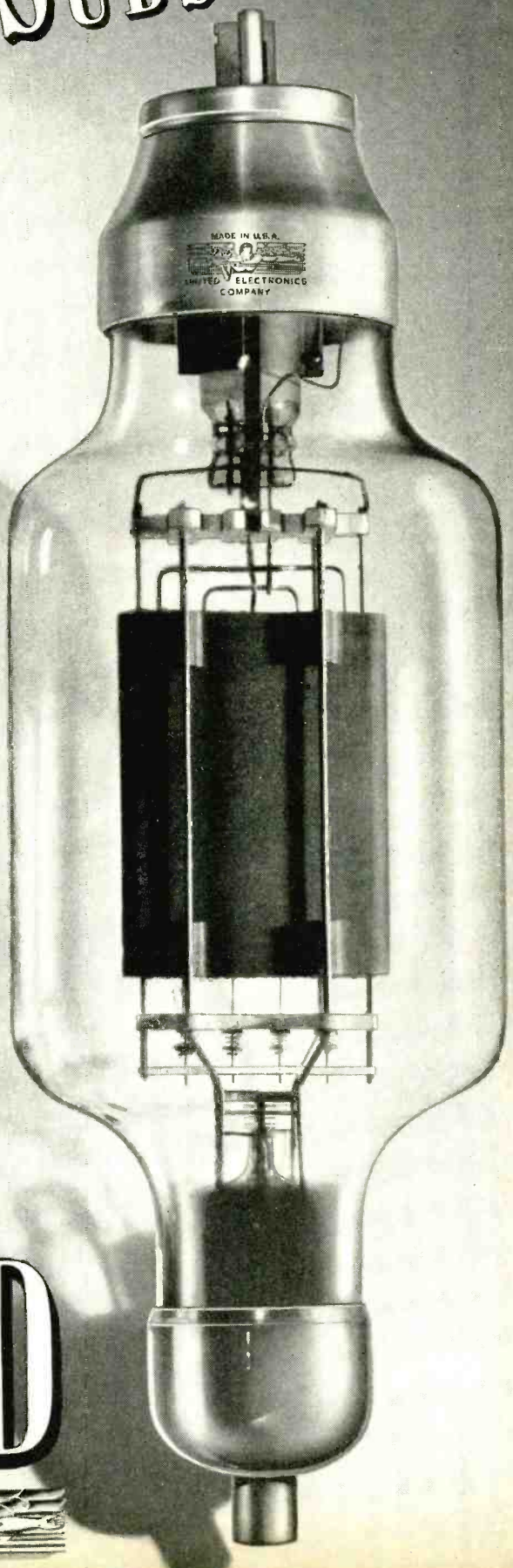
ELASTIC STOP NUTS

Lock fast to make things last

ELASTIC STOP NUT CORPORATION OF AMERICA
UNION, NEW JERSEY

ESNA TRADE MARK

SHADOW AND SUBSTANCE



In the highly specialized field of electronics, the question "Who made the tubes?" will always be a matter of vital importance. Power tubes bearing the name "United" are products of original pioneers in the miracle known today as electronics. Step by step these seasoned engineers helped evolve the principles and advance the science of fabricating transmitting tubes which hold a superb record of performance. The early pioneers at United are *still actively pioneering!* The wealth of experience which they have been privileged to accumulate under the demands of war will be available to you when "United" electronic tubes are available again on a peace-time scale for radio and industrial applications.

UNITED

ELECTRONICS COMPANY

NEWARK NEW JERSEY

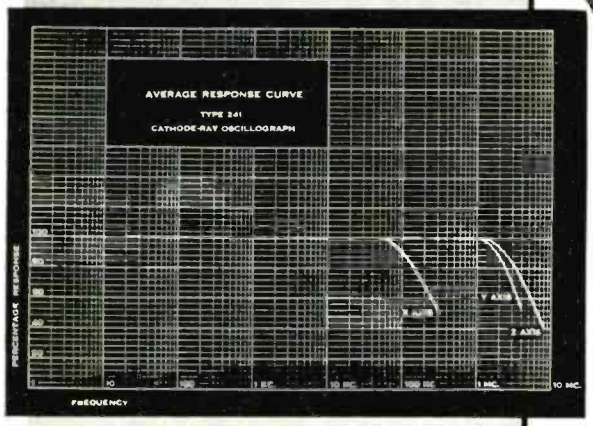
DuMONT *Oscillography*

...from A to X, Y and Z

The *new* DuMont Type 241 oscillograph is literally an enlarged version of the 3-inch Type 224 already meeting the more critical requirements of oscillograph users.

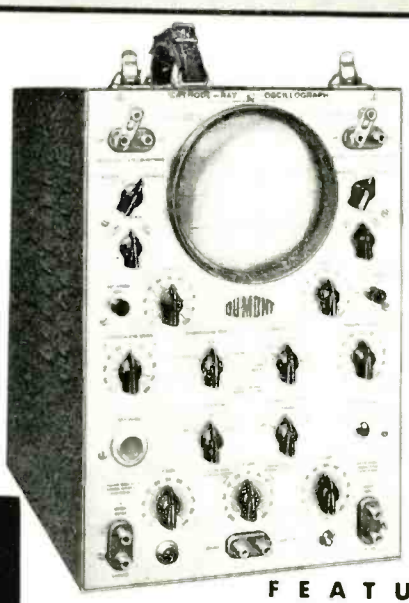
The 5-inch tube means larger oscillograms for more detailed studies. The added Z-axis amplifier for beam modulation permits use of timing signals or blanking impulses for further applications.

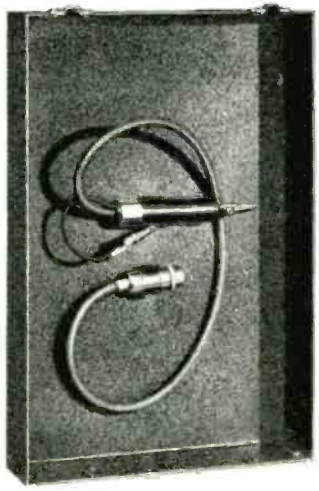
Both instruments—Type 224 (3-inch) and the new Type 241 (5-inch) set *new standards* for commercial-grade oscillographs. Wide-band Y-axis amplifiers permit study of signals of frequencies far beyond the range of usual instruments. Both have a comparably wide-band square and sinusoidal wave response. Both permit a wide choice of panel connections for extreme flexibility in applying signals to the cathode-ray tube. Both are ruggedly housed and supplied with removable front cover for added protection in transit or when not in actual use.



These two expanded-range-expanded-versatility DuMont Oscillographs, along with other DuMont types, round out an outstanding choice of instruments for your particular kind of oscillography.

Write for literature





FEATURES

DuMont Type 5JP1 intensifier-type cathode-ray tube for brilliant, easy-reading oscillograms.

Y-axis or vertical deflection response uniform from 20 c.p.s. to 2 mc. Comparable faithful square and sinusoidal wave response.

X-axis or horizontal deflection amplifier with uniform response to 100 kc.

Both amplifiers have input attenuators and distortionless gain controls.

Y-amplifier has input connection for test probe and shielded cable supplied with instrument, reducing input capacitance and eliminating usual stray pickup.

Z-axis amplifier modulates electron beam with any signal applied to input terminal post, or with return trace-blanking pulse produced by linear-time-base generator.

All high-voltage electrolytic capacitors eliminated from circuit.

17½" high; 10¾" wide; 21" deep. 65 lbs.


50 c.p.s.

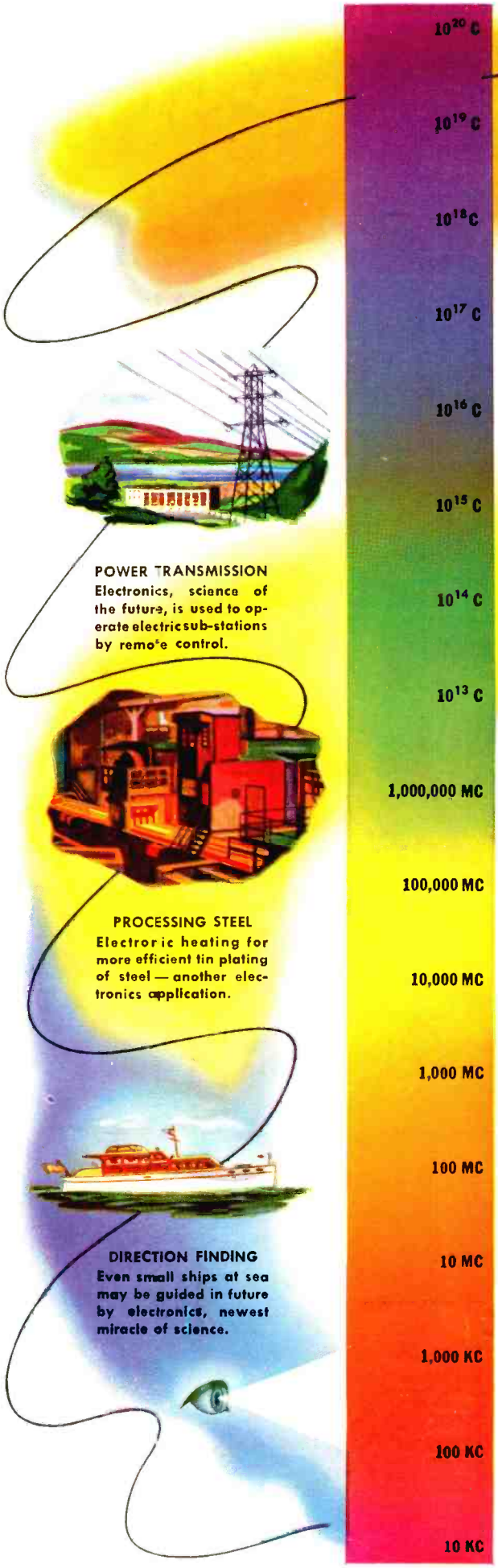

500 c.p.s.


25 KC.


100 KC.

DUMONT

ALLEN B. DU MONT LABORATORIES, Inc.
Passaic • New Jersey
Cable Address: Wespexlin, New York



THERE'S MAGIC IN ELECTRONICS. AND NEW CAREERS!

With electronics man can now see through stone and steel... detect smoke, dust and fog invisible to the eye. He can match colors and finishes... manipulate doors, furnaces, traffic—even make meat tender by means of the science of electronics.

The industrial uses for the magic of electronics appear almost endless. In the 100-1000 kilocycle range of the frequency spectrum, for example, the applications of electronics include operation of electric substations by remote control, more efficient tin plating of steel, maritime direction finding applied even to small pleasure craft.

And almost every day astounding new uses are being recorded—in transportation, food, medicine. With the dawn of peace, the range of useful electronic applications is expected to embrace almost every phase of modern living.

For the electronically-minded, there will be no limit to the opportunities when the war is won. Fascinating new careers, undreamed-of a few years ago, will be waiting—in the service of those who will produce the many electronic devices, as well as in the fields where this new science will be applied in the coming "Era of Electronics."

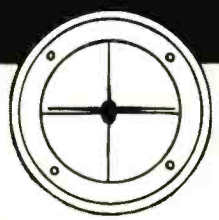
Isolantite has followed closely the development of science's newest miracle, aware of the possibilities for its commercial application at war's end. Aware, too, of the role *insulation* must play in adapting the electronic principle to new products and uses for peacetime living. The electronic world will not be delayed for want of high-grade insulating materials.

ISOLANTITE

CERAMIC INSULATORS

ISOLANTITE INC., BELLEVILLE, N. J.

"X" MARKS THE SPOT YOU CAN PUT YOUR FINGER ON *Blind!*



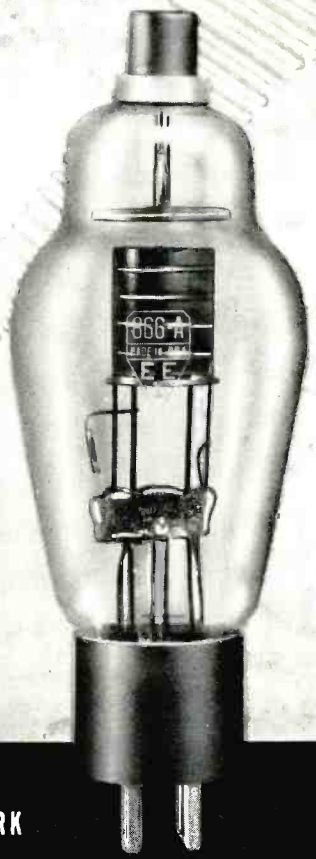
THE VITAL SIXTH SENSE IN INSTRUMENT NAVIGATION

Thanks to the tremendous strides achieved in the field of electronics, a new sixth sense takes the sting out of 'closed' weather—minimizes accidents, permits landings on schedule.

An electric device on an instrument panel registers the gliding path of the craft, vertically and horizontally, in relation to the pre-determined beam of the airport. Safe landings . . . without the pilot ever having seen the field!

The part played by ELECTRONIC ENTERPRISES power and transmitter tubes in furthering aviation progress is but one of the achievements of these highly-sensitive, precision-functioning electronic components.

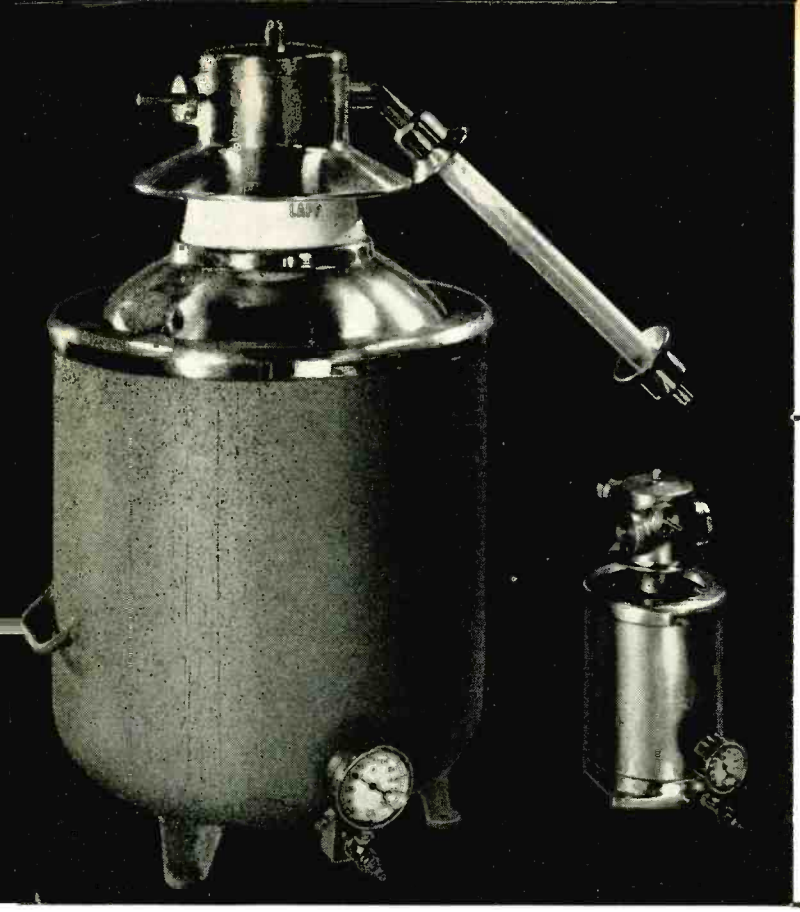
The complete engineering facilities of ELECTRONIC ENTERPRISES are available to you for collaboration on your problems. Inquiries are invited.



ELECTRONIC ENTERPRISES, INC.

ELECTRONIC e ENTERPRISES

GENERAL OFFICES: 65-67 SEVENTH AVENUE, NEWARK NEW JERSEY



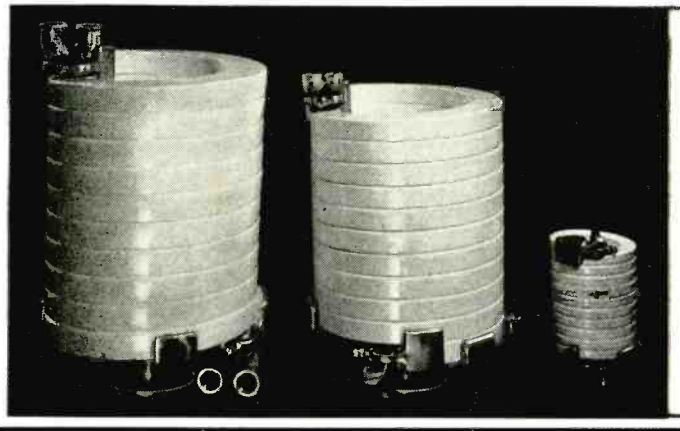
FOR HIGH-FREQUENCY POWER SOURCES

LAPP GAS-FILLED CONDENSERS

In any electronic circuit, wherever lump capacitance is needed, Lapp condensers will save space, save power and save trouble. Available for duty at almost any conceivably-useable voltage rating and capacitance, they bring to any application notable mechanical and electrical advantages: practically zero loss, smallest space requirement, non-failing, puncture-proof design, constant capacitance under temperature variations. *Shown, at left, Unit No. 25934, rated at 200 amp., 6500 volts, capacitance variable 4300 mmf. to 11000 mmf.; right, Unit No. 23722, rated at 50 amp., 7500 volts, capacitance 45 mmf. to 75 mmf.*

STANDOFF, BOWL, ENTRANCE INSULATORS

Standoff, bowl, entrance and other special-purpose insulators are available in wide range as standard Lapp catalog items. Other insulators of special design are easily produced by Lapp methods, either in porcelain or steatite. The wide choice of such insulators available from Lapp simplifies the design of high-frequency equipment. Also, Lapp is equipped for production of many special assemblies, of porcelain or steatite, and the associated metal parts.



LAPP PORCELAIN WATER COILS

For cooling of high-frequency tubes in radio transmitters and other electronic power sources, Lapp porcelain water coils have been widely used. With nothing about the porcelain to deteriorate, sludging is eliminated, and with it the need for cleaning and water changes. Porcelain pipe and fittings in any needed size are also available as catalog items. We welcome inquiry on any Lapp equipment for experimental or industrial electronic application.

Lapp

INSULATOR CO., INC.

LEROY, N. Y.

ARMY E NAVY

"We've been using Wilcox Equipment for two years—without a single interruption"

says E. H. Forsman, Supt. of Communications for Continental Air Lines

WILCOX equipment has an important part in the vital communications operations of leading airlines, and uninterrupted service is proving Wilcox dependability. The Wilcox factories have converted their entire facilities and experience to production for military needs...to help keep 'em flying until Peace is assured. But, after the war Wilcox equipment again will be available for the huge expansion in civil air transportation that is certain to come.

There MUST Be Dependable Communications

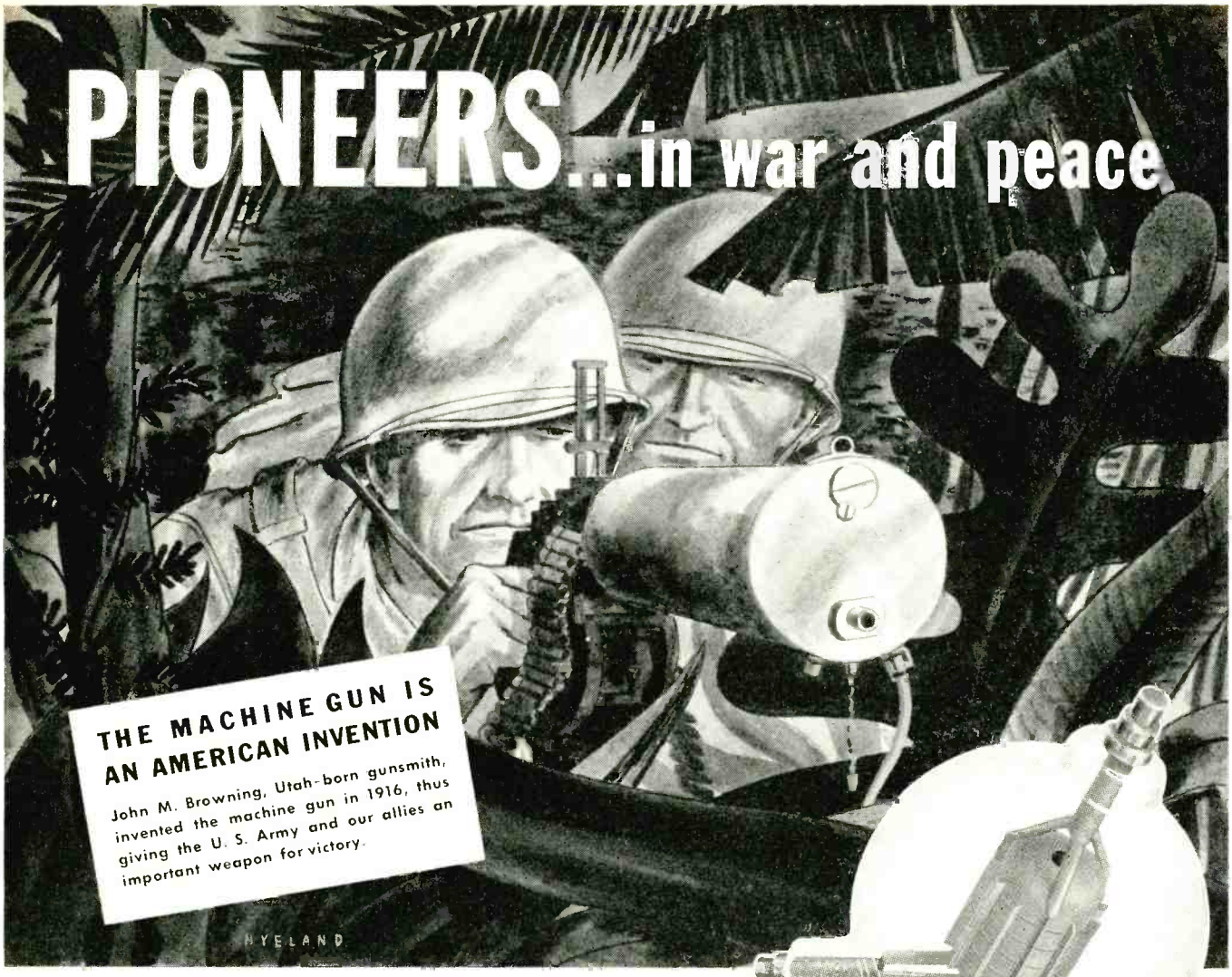
Communication Receivers
Airline Radio Equipment Aircraft Radio Transmitting Equipment

WILCOX ELECTRIC COMPANY

Quality Manufacturing of Radio Equipment

14th & Chestnut Kansas City, Mo.

Photo, courtesy Continental Air Lines



HEINTZ AND KAUFMAN ORIGINATED THE TANTALUM ELECTRON TUBE

GAMMATRON tubes exemplify the ability of Heintz and Kaufman engineers to meet difficult design problems with exceptional skill and ingenuity.

Faced with the need for tubes which can endure great physical and electrical punishment without faltering, our engineers were the first to appreciate the unique advantages of tantalum as a plate and grid material. In addition they pioneered new principles of construction which discarded all internal insulators. As a result, GAMMATRONS are inherently gas-free.

Heintz and Kaufman brought this same pioneering spirit to the UHF band. Some of the accomplishments of GAMMATRONS at high frequencies are well known, but many developments are today classed as restricted information. Until the full story can be told, keep GAMMATRONS in mind for postwar applications . . . for then as now they will help open new frontiers for electronics.

HEINTZ AND KAUFMAN, LTD.

SOUTH SAN FRANCISCO · CALIFORNIA · U. S. A.

Gammatron Tubes

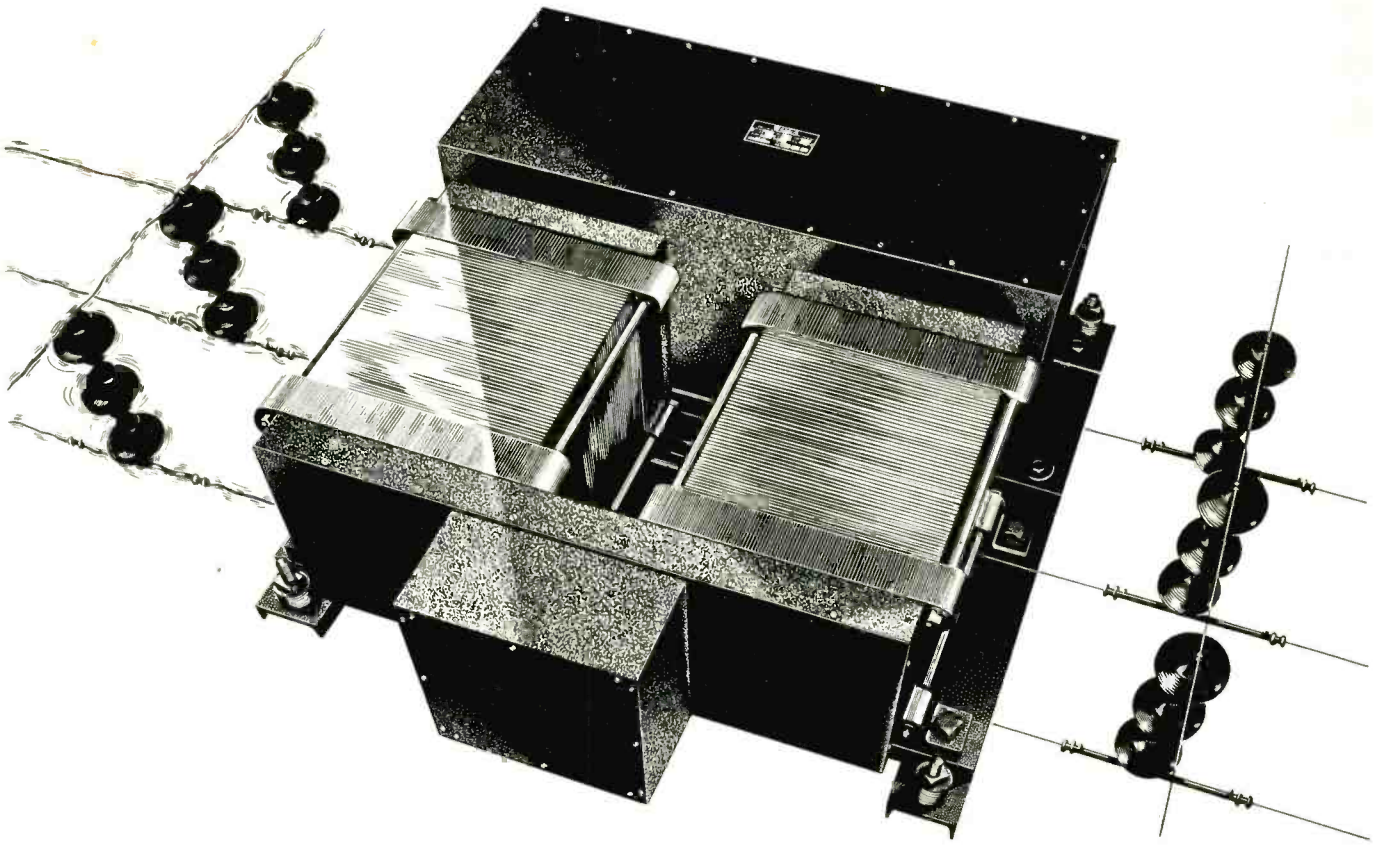
HK-1054 TRIODE

OPERATING DATA

As an RF Power Amplifier, Class C, Unmodulated.

	Typical	Maximum
Power Output	3000 Watts	—
Driving Power	140 Watts	—
DC Plate Voltage	5000 Volts	6000
DC Plate Current	750 M.A.	1000
DC Grid Voltage	-950 Volts	-2000
DC Grid Current	105 M.A.	150
Peak RF Grid Volts	1475 Volts	—
Plate Input	3750 Volts	3750
Plate Dissipation	750 Watts	750

Industry steadies its "nerves"



FACED with production schedules that have no precedent in history, American industry finds the fluctuating voltages of its over-loaded power lines wholly inadequate to meet the "deadly" precision demanded for total war.

Vital "nerve centers" of production lines are geared for precise performance when operated at specific line voltages. Any variation from these rated values, and there are many these days, may well mean lagging production schedules and a noticeable lack of uniformity in products.

Fluctuating line voltages are no problem in plants where Sola "CV's" have taken over. Even though the peaks and valleys of power consumption may cause a voltage variation of as much as ± 30%—the vital "nerve centers" of their production lines continue to operate smoothly and with unerring precision.

Day and night, without care or supervision, Sola Constant Voltage transformers maintain positive control over electrically operated instruments and machines that are indispensable to the nation's war effort. These transformers are available in standard units with capacities ranging from 15 KVA, which might be used for an entire communications system for instance, to the small 10 VA units for vacuum tubes. Special units can be built to specifications.

Note to Industrial Executives: *The problems solved by Sola "CV" transformers in other plants may have an exact counterpart in yours. Find out. Ask for bulletin DCV-74*

SOLA Constant Voltage Transformers

Transformers for: Constant Voltage • Cold Cathode Lighting • Mercury Lamps • Series Lighting • Fluorescent Lighting • X-ray Equipment • Luminous Tube Signs Oil Burner Ignition • Radio • Power • Controls • Signal Systems • Door Bells and Chimes • etc. **SOLA ELECTRIC CO., 2525 Clybourn Ave., Chicago, Ill.**

THE ROSÁN

REMOVABLE TERMINAL STUD

LOCKED IN THE MATERIAL

INSERTED FROM THE FRONT

NO SHIELDING NECESSARY

THE Rosán Removable Terminal Stud is one of the many applications of the Rosán Locking System designed into our threaded inserts and studs. The red Locking Ring in the illustration broaches its way into the material and locks the stud in place. This is the principle of the Rosán Locking System.

The introduction of this remarkable device has solved one of the most baffling problems with which engineers have been confronted. Ordinary studs or inserts will turn and loosen under vibration. The Rosán Locking System locks our studs and inserts permanently in metals, plastics, wood, or any material which can be threaded.

The Rosán *Removable* Terminal Stud is also locked in the material; but with this difference: By means of the flange above the serrated collar, the locking ring may be removed and the stud replaced. Rosán Removable Terminal Studs are put in from the front of the panel. No counterboring at the back. No shielding necessary. Effects enormous savings in material and repair time. No special taps or screws required. Standard threads throughout.

The operating principle of the Rosán Threaded Insert is shown in the illustrations below.

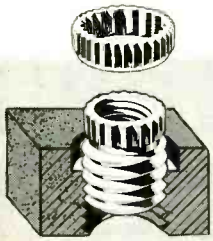
Manufacturers are invited to submit their problems to our Engineering Department. The Rosán Locking System has types of inserts and studs for every branch of industry.

BARDWELL & McALISTER, INC.

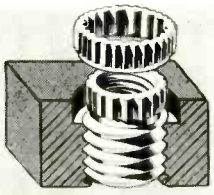
7638 Santa Monica Blvd., Hollywood, Calif.

DESIGNERS AND MANUFACTURERS

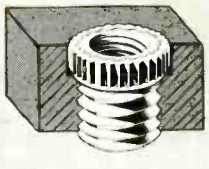
THE ROSÁN LOCKING SYSTEM



(1) Material has been drilled and tapped. Insert, minus locking ring, has been partly screwed into place.



(2) Insert in place. Top flush with surface of material. Note the counter-bored channel for the locking ring.



(3) Insert locked in place. Inner serrations engaged with teeth of collar. Outer serrations broached permanently into material.

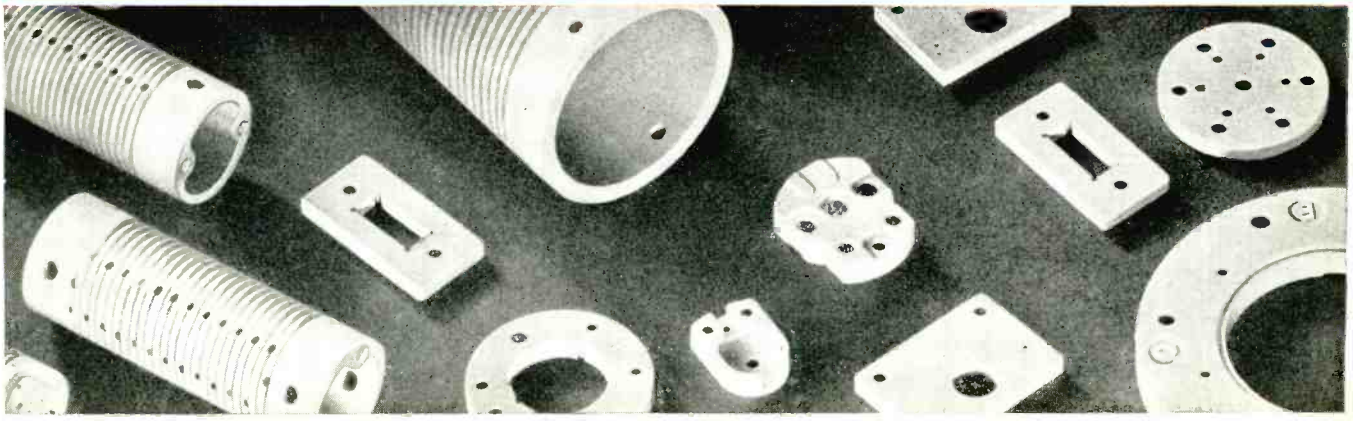
STEATITE . . .

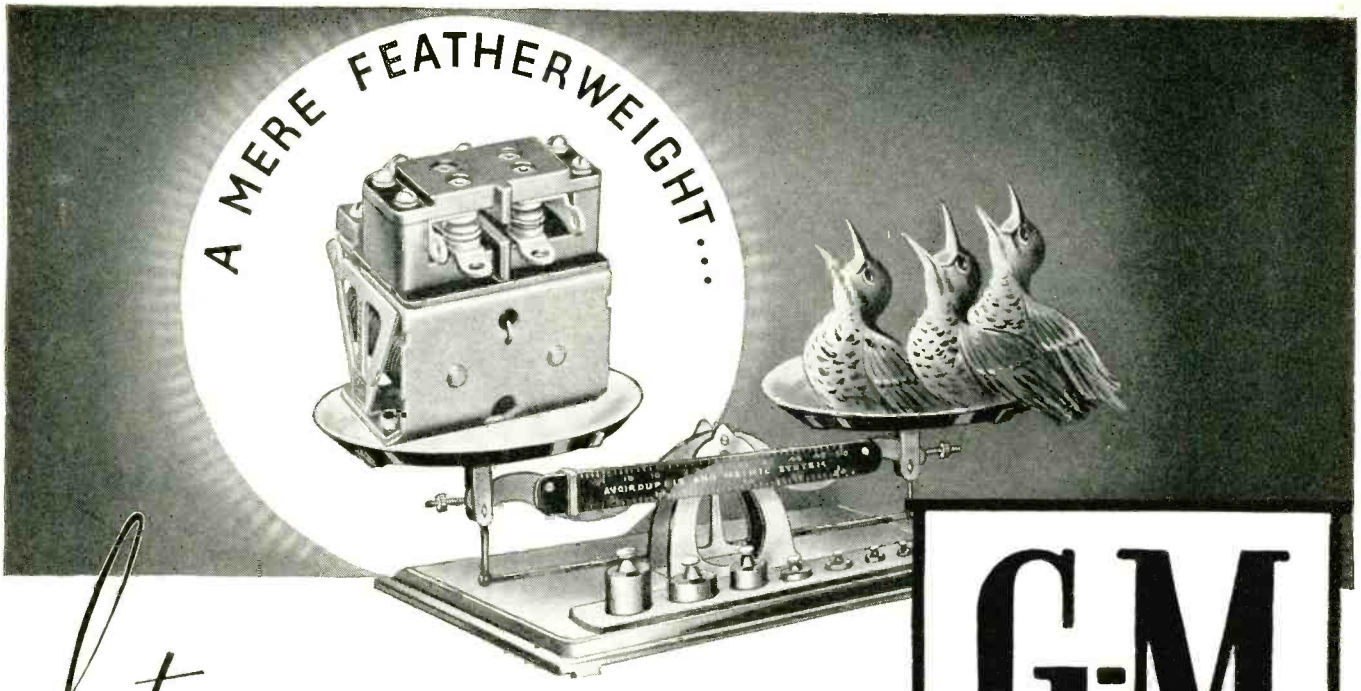
★ Centralab's Steatite plant can furnish coil forms up to 5" diameter and pressed pieces to approximately 6 inches square. Centralab's engineering, laboratory and production experience in Ceramics extends back to 1930. In addition to Steatite, Centralab also produces other types of Ceramics.* Consult our engineering dept. on your Ceramic problems.

Centralab

Division of **GLOBE-UNION INC., Milwaukee**

*Cordierite: a low thermal expansion type of ceramic. Hy Dielectric: a ceramic suitable for capacitors and special application.





but BUILT TO DO A HERCULEAN JOB

The Type 27
SUPER AIRCRAFT RELAY

G-M

Expert design . . . Small size . . . Light Weight . . . yet a powerful Aircraft Relay possessing a number of noteworthy characteristics, which can be varied over a wide range to suit the requirements of different applications.

The box frame construction gives the Type 27 Relay superior strength and sturdiness . . . yet it weighs only 5 ounces. The above illustrated relay is capable of withstanding 15g or more without a tremor . . . has a contact pressure of 60 grams (double make-double break) and a contact capacity of 20 amperes at 30 volts d.c. (100 ampere inrush). The pickup is 6.5 volts (.61 watt) at 20° C. The nominal coil voltage is 12 volts d.c. Coil wattage at 12 volts d.c. is 2.1 watts at 20° C. Temperature range is from —40 to 90° C. Size 1½ x 1⅝ x 1⅞".

Free samples of the above Type 27 Relay (SPDT double make-double break in 2 pole construction) are available to relay users if request is accompanied by a priority of AA-4 or better. Write or wire today requesting specification No. 12723.

VISITRON PHOTOTUBES

are available in quantity in numerous sizes. Made by G-M, pioneer in development and manufacture of quality phototubes.

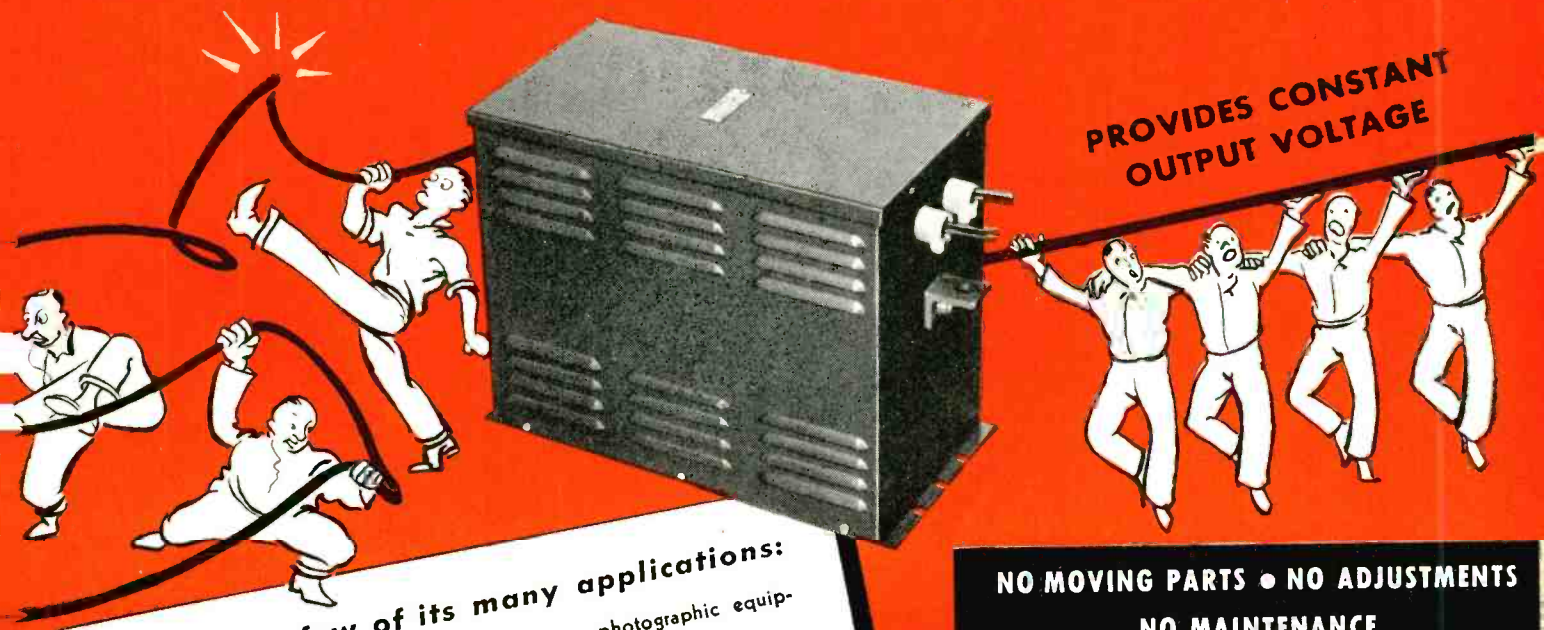
G-M LABORATORIES INC.

4313 NORTH KNOX AVENUE, CHICAGO, ILLINOIS

Buy WAR BONDS & STAMPS

G.E. ANNOUNCES A NEW VOLTAGE STABILIZER

...that is insensitive to load power factor



Here are a few of its many applications:

1 Radio transmitters
2 Radio testing equipment
3 Electronic-tube apparatus
4 Motion-picture sound equipment
5 Motion-picture projectors
6 Telephone apparatus
7 X-ray machines
8 Photo-cell equipment
9 Precision photographic equipment
10 Photometers
11 Color comparators
12 Calibration of meters, instruments, relays
13 Laboratory precision processes and testing equipment

NO MOVING PARTS • NO ADJUSTMENTS NO MAINTENANCE

HERE is a voltage stabilizer that digests variations in load or power factor, or both, and continues *unaffected* in its smooth, reliable regulation of voltage. Variations in load from no load to full load bother it not a whit. Changes in power factor from unity to 0.8 lagging leave it indifferent.

Electronic-device *manufacturers* who build it into their equipment, or offer it as an accessory, will find that it means better performance and greater salability of their products. Present *users* of electronic devices will likewise find that it can improve the performance and reliability of their equipment. This stabilizer is ideal for precision control of many laboratory processes.

If *your* problem is one of providing constant voltage for the operation of diversified electric equipment—all or much of which has fluctuating loads and power factor—solve it by installing G-E stabilizers, the only voltage stabilizer on the market that is insensitive to load power factor. Available ratings from 50 va to 5000 va. Ask our local office for Bulletin GEA-3634—the complete story. *General Electric Co., Schenectady, New York.*

Engineers, note these performance features!

WIDE LIMITS FOR INPUT VOLTAGE—95 to 130 volts—ample for all ordinary voltage conditions.

CONSTANT OUTPUT VOLTAGE—For any fixed load, ±½ per cent. For any load that varies between full load and half load, and power factor between unity and 0.8 lagging, the output voltage will not vary more than ±1½ per cent. For simultaneous variations in input voltage, load, and load power factor—with load between no load and full load, and load power factor between unity and 0.8 lagging—the output voltage will not vary more than ±2½ per cent.

QUICK RESPONSE—Stabilizing action takes place in less than three cycles.

LEADING INPUT POWER FACTOR—Approximately 20 per cent at no load, and 70 per cent at full load.

CURRENT-LIMITING FEATURE—On short circuit the output is limited to approximately 130 per cent of full load—especially valuable for electronic-tube apparatus during the filament warming-up period.

LOW HARMONIC CONTENT—Only about 6 per cent at or near full load, unity power factor. Only slight variations in harmonic content result from variations in input voltage.

SELF-PROTECTING—Will operate continuously throughout the range from open circuit to short circuit without damage.

GENERAL ELECTRIC

408-37-5205

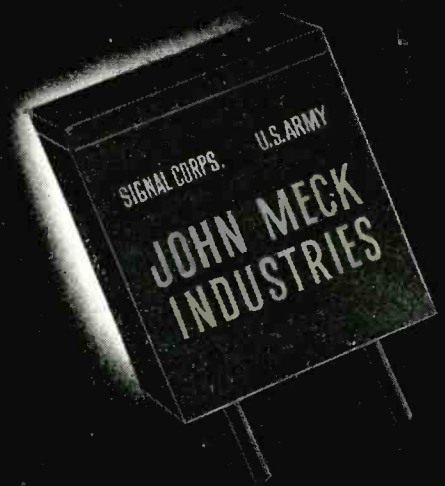
The Army-Navy "E", for Excellence in the manufacture of war equipment, now flies over six G-E plants employing 100,000 men and women.

CRYSTALS

"SHORT ORDERS" IN A HURRY

If it's a "Rush" phone us, and your order for special crystals will go into work immediately under a competent crystal engineer personally charged with the responsibility for your project.

Our full facilities, including latest electrical and optical equipment, X-ray orientation, etc.—are at your service. John Meck Crystals are "Good Will Ambassadors of the Future" to acquaint you with our Family of Activities in the field of Sound and its Projection. That's why "Short Orders in a Hurry" are welcome.



Phone **CRYSTAL SERVICE DIVISION**
PLYMOUTH THREE THREE

JOHN MECK INDUSTRIES
PLYMOUTH, INDIANA

EXCELLENCE IN MUSIC AND VOICE RECREATING INSTRUMENTS

_For lack of a Tube

The Big "B" was limping home over the water with two motors shot away. Too far gone to reach the home field. No visibility for a navigational fix.

Radio Op was trying to locate a closer field when a tube went dead. Which one? No time to test. He yanked out all the tubes. Started putting in a spare set.

But one of the tubes he jerked out was a "special selection." The replacements didn't work. The big bomber never got that bearing. And $350,000 worth of fighting ship drowned in the Pacific.

The moral? If you are a designer of radio and radio-electronic circuits for our armed forces, you can avoid the use of special selection tubes in 99 cases out of 100.

There's hardly a radio-electronic circuit today that can't be designed to function perfectly with standard tubes.

You might need two of these in place of one "special selection," but standardization makes it worthwhile.

We can and do supply "special selections" but only when authorized by the Army or Navy. Even then your special selection will interfere with the mass production and delivery of our standard tubes — and today time is the essence.

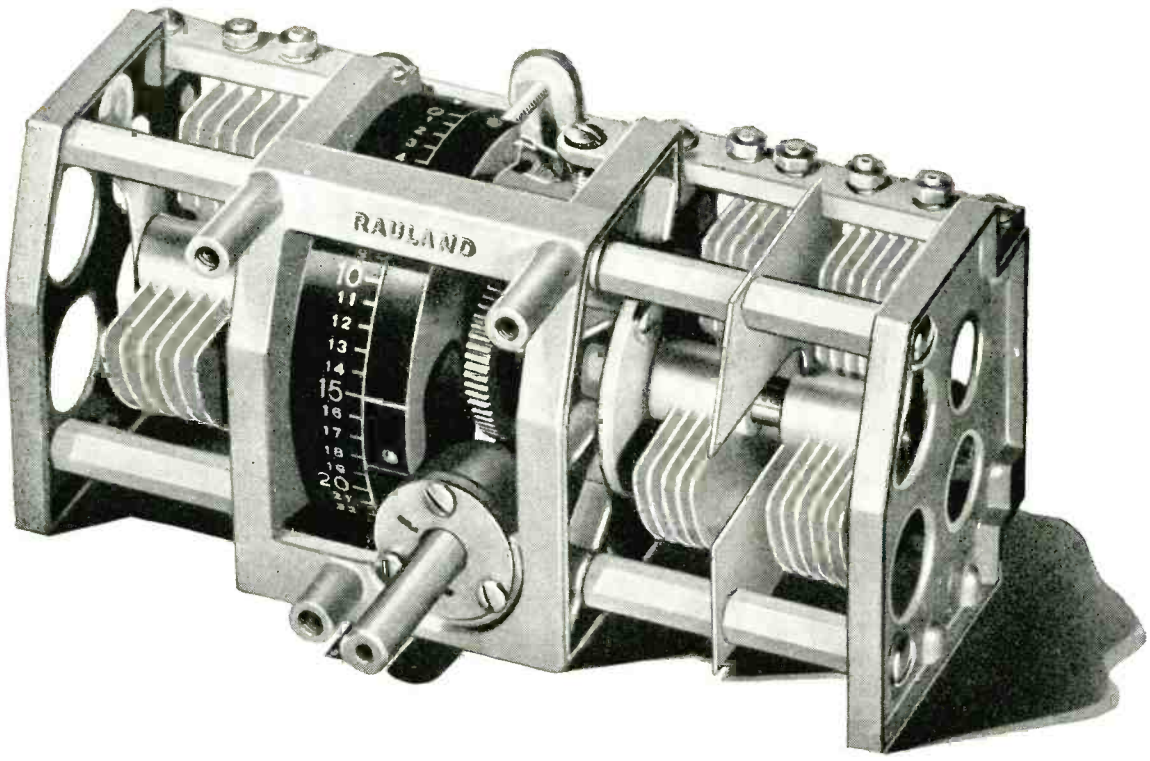
So why not first find out if the circuit you're working on now, can't be designed without the use of "special selections"? Our staff of application engineers is always ready to help you solve your design and manufacturing problems — and they can help you avoid "special selections"!

RCA

RCA RADIO TUBES

RECEIVING TUBES • POWER TUBES • CATHODE-RAY TUBES • SPECIAL-PURPOSE TUBES

RCA Victor Division, **RADIO CORPORATION OF AMERICA**, Camden, N. J.



"Condenser by Rauland"

Back of every fine instrument is a combination of wide experience, infinite skill and painstaking care. RAULAND condenser users *know* the utter dependability of these *electroneered* units; how successfully they have met and performed the most difficult tasks demanded of communications by modern warfare. They are made to "stand the gaff," having battleship toughness, yet blended with a precision accuracy that insures a fine degree of tuning. These are the things you get when you specify *"Condenser by RAULAND."*

RADIO ... SOUND ... **Rauland** ... COMMUNICATIONS

Electroneering is our business

THE RAULAND CORPORATION » » » CHICAGO, ILLINOIS

Buy War Bonds and Stamps! Rauland employees are still investing 10% of their salaries in War Bonds

ON THE JOB

Whenever our Flying Fortresses fulfill their missions for victory, AlSiMag ceramic insulators are on the job to help make the flight a success.

AlSiMag steatite insulation can be found in all vital electronic components and is selected by designers of electronic equipment for dependable service.

ARMY E NAVY

AWARDED JULY 27, 1942

AlSiMag

TRADE MARK REGISTERED U. S. PATENT OFFICE

AMERICAN LAVA CORPORATION

CHATTANOOGA, TENNESSEE

The N-Y-T Sample Dept. was established so that we may have...

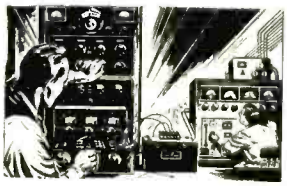
MAJOR AIR VICTORIES!

..without the world ending for Johnny Smith

An eighteen-to-one defeat for the enemy is good reading . . . it's the ratio of advantage that spells ultimate success for the United Nations. However, let's give a thought to Johnny Smith, pilot of the short-end of the score.

For the purpose of making good transformers better, to design and engineer them for more efficient and dependable functioning, the N-Y-T Sample Department was established. By intensive research and laboratory work, new developments are engineered, then made tangible components for ordnance machines and radio equipment.

Which means another day for the Johnny Smiths in our Army, Navy and Air Corps. Translated into post-war practice it will mean better living when they return.



* * *

The N-Y-T Sample Department is prepared to give immediate consideration to your special problems, and make deliveries within a matter of days. Inquiries invited.

NEW YORK TRANSFORMER CO.

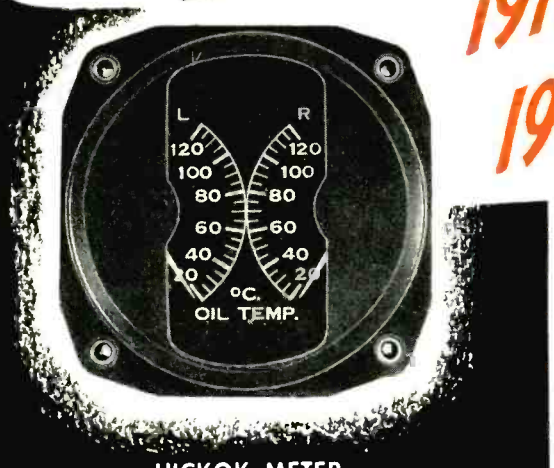
26 WAVERLY PLACE NEW YORK, N. Y.

HICKOK

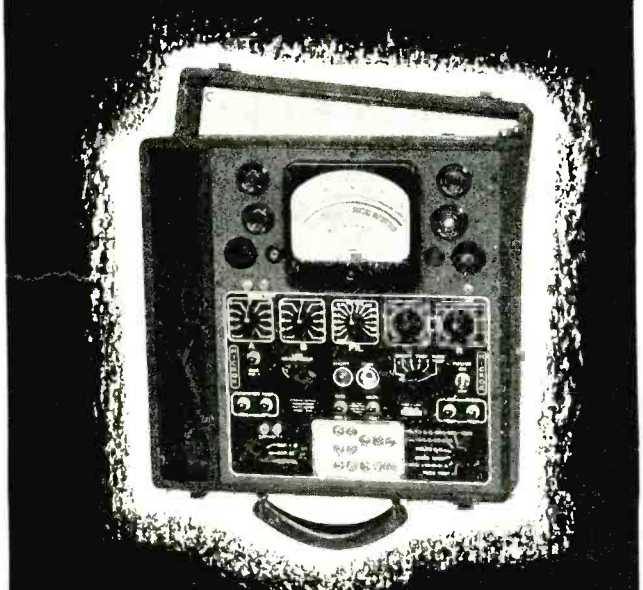
33 Years of Progress..

1910.. 1 small plant
1 employee
2 styles of meters

1943.. 2 large plants
Nearly 1000 employees
Hundreds of styles of meters
and test instruments.



HICKOK METER



HICKOK DYNAMIC MUTUAL CONDUCTANCE TUBE TESTER

• From its organization in 1910 until now The Hickok Electrical Instrument Co., has always been in the forefront of those companies who have contributed most to Electrical and Radio Instrument progress.

Quality has always predominated over quantity of production—building a reputation for highest grade instruments that is now reflected in the enormous demand for Hickok Meters for Aviation and other War Time uses. The meter illustrated is typical of these War Time Instruments.

The Hickok Dynamic Mutual Conductance Tube Tester, developed soon after the advent of the 3-element radio tube, is the standard instrument for tube testing today.

New Hickok Meters and instruments are being designed or are already in production for the use of our Armed Forces. They will be available for everyone as soon as the present emergency is over.

So keep your eye on Hickok for the newest and best in indicating meters and radio service equipment.

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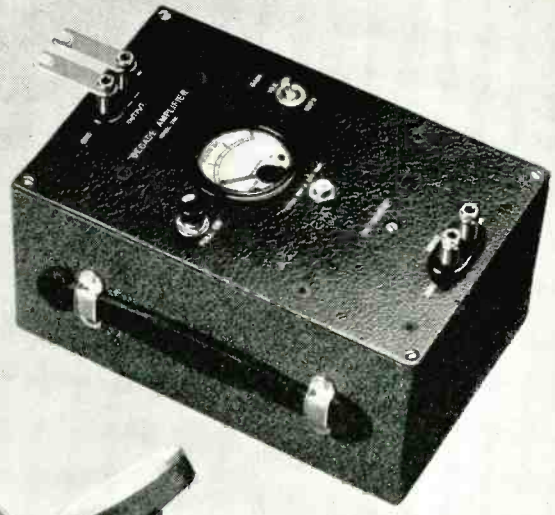
CLEVELAND, OHIO • U. S. A.

0.00002 to 10,000 VOLTS!

BALLANTINE
ELECTRONIC
AC VOLTMETER
AND ACCESSORIES

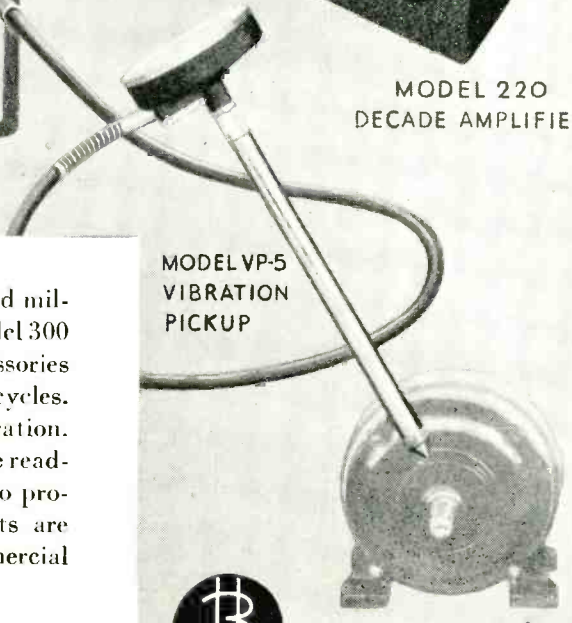
MODEL 300
ELECTRONIC
VOLTMETER



MODEL 220
DECADE AMPLIFIER

MODEL 505
ARTIFICIAL EAR

MODEL 402
MULTIPLIER



MODEL VP-5
VIBRATION
PICKUP

This enormous range of voltages—five hundred million to one—is accurately covered by our Model 300 Electronic Voltmeter and some of the accessories shown above. Frequency range 10 to 150,000 cycles. Accuracy 2% over most of the range. AC operation. Five decade ranges with logarithmic scale make readings especially easy. Uniform decibel scale also provided. Over a thousand of these instruments are giving excellent service in Government, commercial and university laboratories and factories.

Send for Bulletin 8

BALLANTINE LABORATORIES, INC.
BOONTON, NEW JERSEY, U.S.A.

FABRICATED PARTS IN MYCALEX

THE INSULATOR

FROM BLUE PRINT SPECIFICATIONS ...TO PRECISION STANDARDS

REAL assistance to manufacturers of communications, high-frequency, electrical and electronic equipment is offered by the announcement of Precision Fabricators, Inc. as a licensed producer of fabricated parts in "LDS" (Leadless) *Mycalex.*

Mycalex as a material has won wide recognition for its high dielectric strength, its low loss even at highest frequencies, its mechanical strength and its stability under pressure, high voltage, heat and humidity.

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VULCANIZED FIBRE ★ RUBBER ★ ASBESTOS AND OTHER MATERIALS

when Johnny comes marching home again

As a radio technician, Johnny is a vital part of our armed forces. He sees an amazing electronic future in the new devices developed by the urgency of war. No, he can't talk about them now, but as he uses them he dreams of electronic wonders to come.

Someday soon, Johnny and thousands like him will come marching home to take their places in their chosen field. Their vision . . . their plans . . . their energy will give us those wonders in electronics of which they dreamed.

Wherever Johnny's ambition leads him in electronics, he will find TUNG-SOL ready for the peacetime developments. TUNG-SOL tubes for transmitting, receiving and amplifying, TUNG-SOL research engineering service will be important parts of his future and the future of electronics.

TUNG-SOL
vibration-tested
RADIO TUBES

TUNG-SOL LAMP WORKS INC., NEWARK, N. J., *Sales Offices:* ATLANTA, CHICAGO, DALLAS, DENVER, DETROIT, LOS ANGELES, NEW YORK
ALSO MANUFACTURERS OF MINIATURE INCANDESCENT LAMPS, ALL-GLASS SEALED BEAM HEADLIGHT LAMPS AND THERMAL SWITCHES

NEW CORNING MULTIFORM GLASSWARE
A CHALLENGE TO ENGINEERS!

Can you name another electrical insulation product available today with so many advantages?

IT'S not only something absolutely new in glass—Pyrex brand Multiform Glassware is an exciting new improvement in electrical insulation!

Multiform Glassware can be made to provide whatever qualities are required. Corning's Glass Number 790, for example, combines the properties of very low thermal expansion, resistance to high temperatures, great chemical durability, and very low dielectric losses. This glass meets all the requirements of U. S. Navy Standard RE-13A-317F, Grade G. Corning Glasses Number 7761 and Number 707, to give further examples, also have very low dielectric losses and can be used as insulation at extreme frequencies. Laboratory tests have shown that all of these glasses and others will meet the A. S. A. American War Standard on Ceramic Radio Insulating Materials, Grades L-5 and L-6.

Outstanding among the advantages of Multiform Insulators are minimum frequency drift, negligible water absorption, low loss factor, and an unusually wide range of size and shape. If insulator shortages have you worried, take this step now: clip and mail the coupon today for a free sample and complete descriptive booklet on Pyrex brand Multiform Glassware!

Multiform Insulation Products already include radio coil forms, coil form end plates and flanges, capacitor bushings, tube socket bases, rest bar insulators, antenna strain insulators, filament guides, rectifier rings, switch cups, co-axial line spacers, crystal holders, condenser spacers, mounting blocks, various beads and wafers, and many other electrical and industrial parts.

MAIL COUPON FOR FREE SAMPLE AND DATA

Pyrex Insulators
BRAND

"PYREX" is a registered trade-mark and indicates manufacture by Corning Glass Works

Corning Glass Works, Corning, N. Y.
Insulation Division, Dept. E-42

Please send me immediately, without charge, sample and descriptive booklet on new Pyrex brand Multiform Insulators.

Name .....

Company .....

Street Address .....

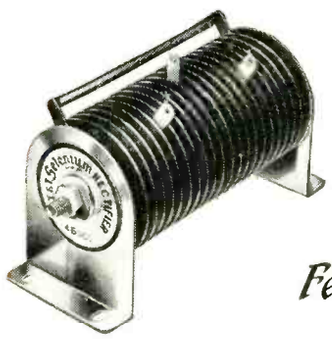
City ..... *State* .....

FIRST in Ability to "Take It" at Sea

Official U. S. Navy Photograph

Special Assembly Method — *showing single metal washer which facilitates protective coating against corrosion*

Standard Assembly Method—*showing conventional petal-shaped brass contact washer*



I. T. & T. Selenium Rectifiers "Armored" against Salt Sea and Air... as result of New Assembly Method

Another I. T. & T. First! Now – in addition to the standard assembly – I. T. & T. Selenium Rectifiers can be supplied with a *special assembly*, coated for protection against the corrosive action of salt spray, moisture and humidity.

Thus the organization which was first to introduce Selenium Rectifiers in the United States is now first to extend their many advantages to marine and other high humidity services.

Compact, light, electrically and mechanically stable – with no moving parts to wear out or cause failure – I. T. & T. Selenium Rectifiers have set a standard for the industry.

Now, on the Fifth Anniversary of their introduction, they are prepared to take on the toughest jobs that weather and war can hand them.

Consulting Engineering Service available for specific requirements. For descriptive bulletins address Department H.

SELENIUM RECTIFIER DIVISION

Federal Telephone and Radio Corporation

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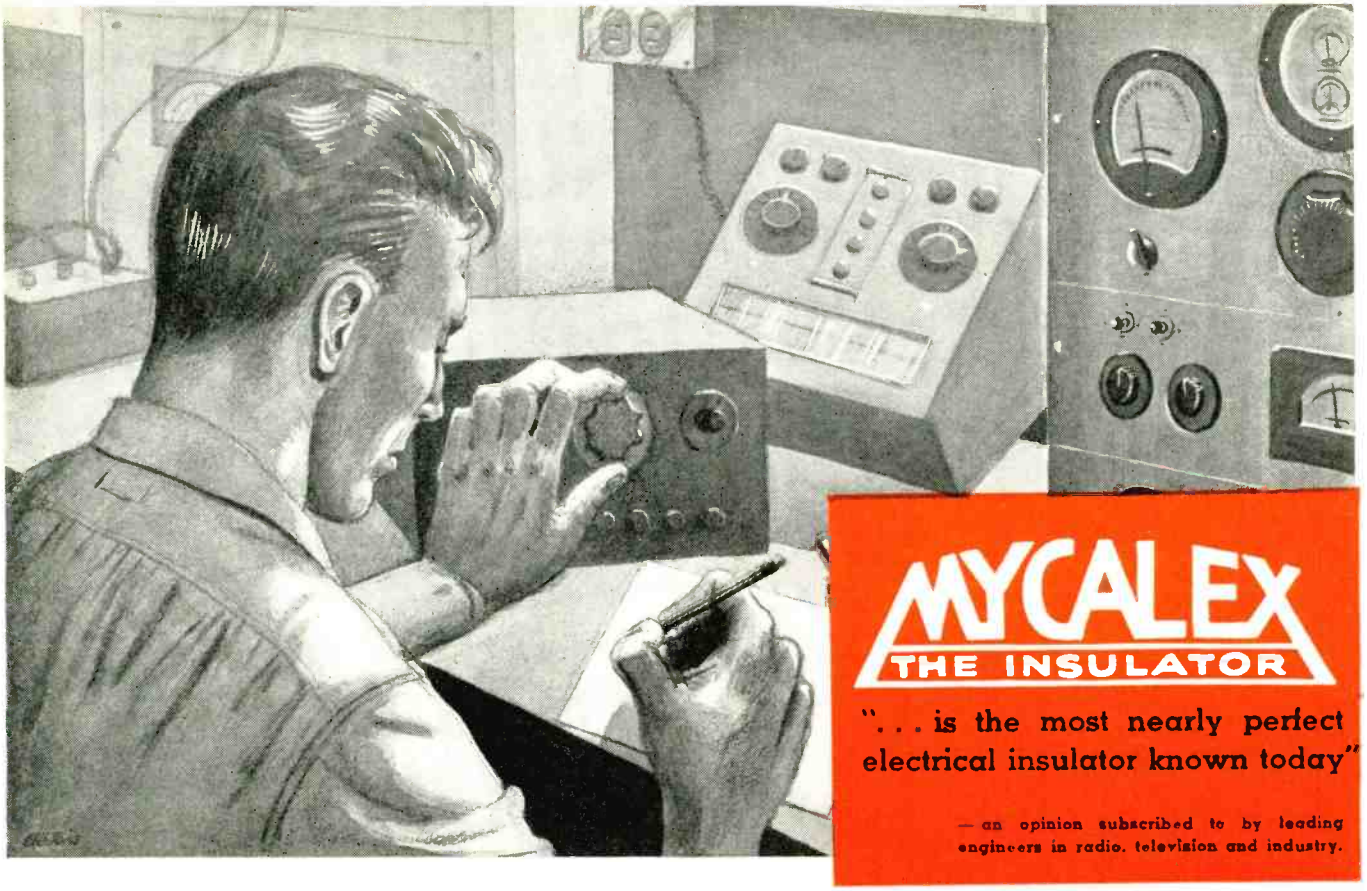


THERE IS ONLY ONE MYCALEX

MYCALEX is not the name of a class of materials. MYCALEX is the registered trade-name for low-loss insulation manufactured only by the Mycalex Corporation of America in the Western Hemisphere. MYCALEX is specified by engineers because MYCALEX is required.

More than a quarter century of extensive application here and abroad has made the name MYCALEX a familiar one in the electrical and communications industries, and we are proud of the important part this versatile insulation is playing today in the military and civil life of the United Nations. The snows of Russia, the sands of Africa, the sweating jungles of New Guinea, the mountains of China—MYCALEX is no stranger to these backgrounds. Unsolicited testimonials to the vital role being performed in the war program by MYCALEX have been given us generously by the Army and the Navy.

If your present insulation fails because of deformation at room temperature or because of failure to withstand elevated temperatures MYCALEX will solve your problem. If you must have hole diameters, hole spacings, or other dimensions with close tolerances, slots, grooves, or accurately tapped holes, combined with low loss at all frequencies, you should bear in mind that MYCALEX has been meeting these requirements for many years. If, on the other hand, dimensions and tolerances are not too critical but ability to withstand high voltages is paramount, MYCALEX is the ideal material for your purpose. The greater machinability of MYCALEX, which is leadless, gives it advantages over any other type of insulation. Our engineering service is available in all cases where the choice of the most reliable insulation is in doubt.

MYCALEX is not available, except in experimental quantities, for other than war applications.

MYCALEX
THE INSULATOR

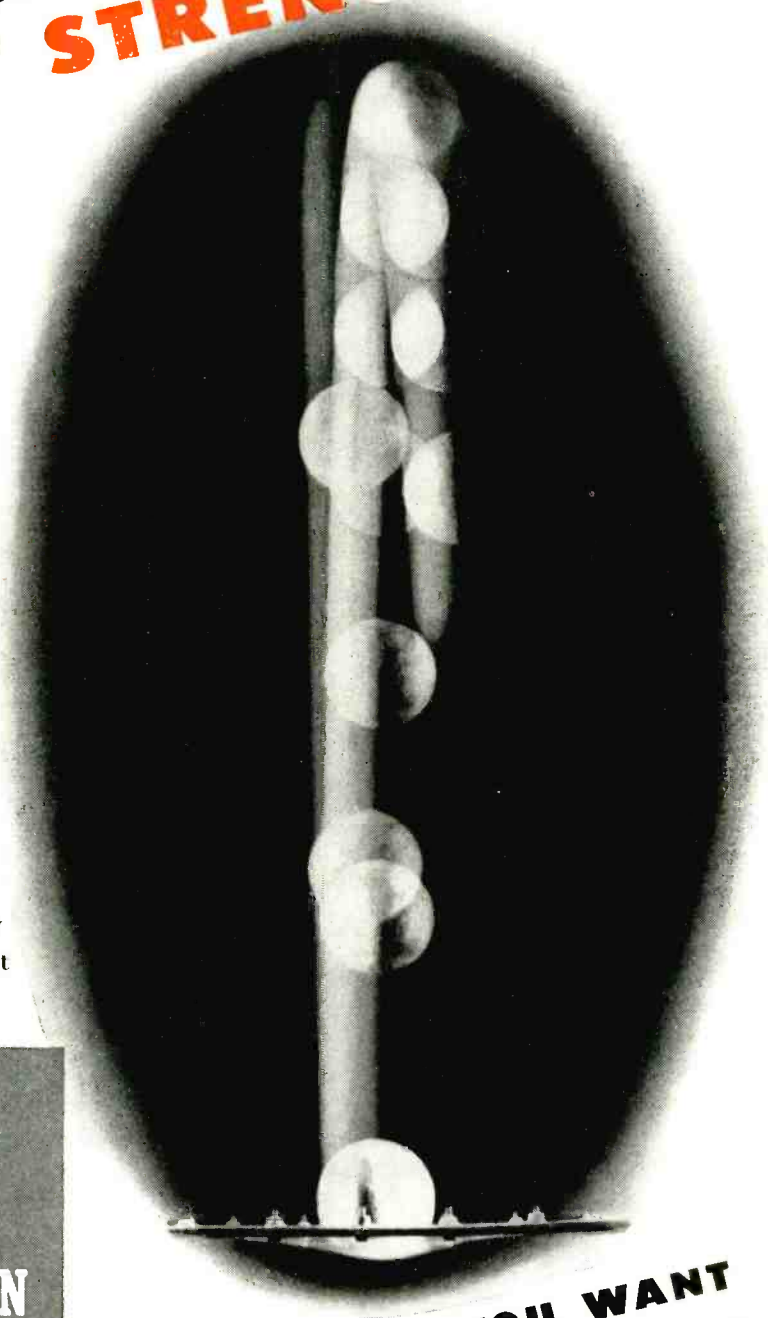
Trade Mark Reg. U. S. Pat. Off.

MYCALEX CORPORATION OF AMERICA

Exclusive Licensee under all patents of MYCALEX (PARENT) CO. Ltd.

60 CLIFTON BOULEVARD CLIFTON, NEW JERSEY

IF YOU ARE
WORKING ON A WAR APPLICATION
Start with
IMPACT STRENGTH



IN ALL forms, from sheets to molding materials, LUMARITH'S impact strength is outstanding. (Some indication of its great strength is given by this Gjon Mili repetitive flash photo, showing a 12-lb. iron ball, dropped from a height of 12 ft. on ⅛″ thick sheet of Aero-Quality LUMARITH, leaving sheet intact.)

CELANESE CELLULOID CORPORATION

The first name in plastics

Celanese Celluloid Corporation, a division of Celanese Corporation of America. 180 Madison Ave., New York City. *Representatives: Cleveland, St. Louis, Dayton, Chicago, Detroit, San Francisco, Los Angeles, Washington, D. C., Leominster, Montreal, Toronto, Ottawa.*

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CELANESE CORPORATION
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IF YOU WANT
IMPACT STRENGTH IN A PLASTIC
Start with
LUMARITH
MOLDING MATERIALS

Food—The Deciding Issue

Our food problem remains to be solved

THE first thing the Germans did when they occupied Czecho-Slovakia, Poland, Belgium, France—was to empty all warehouses. Everything went into trucks headed for Germany.

The Nazis knew that this war would be won by the army that had the most supplies and the best supply system.

The Nazis knew that supplies are as essential as guns. They knew that the most essential of all supplies is . . . food.

Being the only people on earth who can watch women and children starve, the Nazis seized upon food as their most powerful instrument for disciplining the masses. They added famine to their arsenal of conquest.

The flocks and herds of Europe are being consumed with alarming rapidity. The desperate shortage of meats and fats is growing steadily worse. Our Allies are short of certain foods that we must supply if we expect them to carry on.

And as we supply them, as our imports are curtailed, as our fighting men consume more than they do in civil life, and as we fail to increase our production rapidly enough . . . we, too, become short of certain foods.

Former President Herbert Hoover, speaking before a conference of the Governors and Representatives of twelve Mid-Western farming states in Des Moines on March 15th, sounded the warning that American agriculture, beset by Washington bungling on manpower, farm machinery and price systems, strangling production and distribution, is facing a deterioration which may bring on a national food shortage such as led to the collapse of Russia, the defeat of Germany in the first World War and the fall of France in the present war. Unless this deterioration is stopped, warns Mr. Hoover, we cannot hope to win the present conflict.

Complications of similar magnitude face the food processor and the distributor.

Never in the history of the world has man's dependence on food been so crucial. Yet it is not easy for us to grasp the full significance of the crisis. We are so accustomed to finding milk, eggs and butter on our doorsteps every morning, we are so used to filling our pantries from the shelves of our grocers and markets that we accept food as something that is due us on demand. We do not stop to think that we never are more than a few meals ahead of famine.

But this picture has changed. Now we are faced with food rationing, and every day the shelves of our food markets become more bare.

* * *

Let it be noted that the appointment of two Food Administrators has not solved the food problem. It is still with us; daily it becomes more critical. Unless it is solved, and solved quickly, the very food that ex-Food Administrator Wickard said would "win the war and write the peace" may lose the war and lose the peace.

Put very simply and clearly, the food problem amounts to this: we are trying to feed upward of 200 million people. We are trying to do it with the farms and other facilities that heretofore have been capable of feeding about 145 million people (our present population plus a 5% surplus).

Had the Government foreseen the need and planned ahead, we could have begun by 1941 the enlargement of our farm production and food processing capacity. Two irreplaceable years have been lost!

The gravity of the situation becomes apparent when we consider that 50,000 factories are required to process our foods. Food processing not only is America's biggest industry—it is one of America's most important for, without processing, most foods would perish before they could reach the consumer. The term "processing" covers the salting, drying, smoking, pickling, chilling, canning, packing and other methods of preservation that make it possible for us to eat in 1943 food that was produced in 1942. Few realize that most of the food we shall eat in 1943 was produced and processed last year, that most of the seed we plant this spring will grow food for 1944 or perhaps later.

In one important process of preservation, tin and rubber are vital materials. When the Japs captured Malaya and the Netherlands East Indies more than half of the world's tin and nearly all of its rubber fell into their hands. This forced drastic changes upon our entire food economy. The importance of tinplated steel containers, tops for glass jars and rubber gaskets is fairly obvious . . . metal food containers alone consume, every year, more than 2,700,000 tons of steel.

The aggression of Japan has snared our whole food industry in a maze of intricate packing problems. It has enforced recognition of a new principle of food technology, i.e., that the *method* of food preservation is determined by the type of container available. The tin, steel and rubber stringency compels many food processors to adopt

unfamiliar methods — methods that call for a great deal of new equipment. This, in turn, involves the use of critical materials that are so urgently needed for other war purposes.

This conversion of the food processing industry to meet these exacting restrictions has been greatly complicated by two factors that have increased its wartime burden. Indeed, it is these that provide the principal reason for civilian food rationing.

The first of these is the task of feeding our armed forces overseas. Allied ships are being sunk at an alarming rate and the loss of cargo is considerable.

The second factor gravely augments the first. Under Lend-Lease our country is undertaking to feed our Allies to the extent of approximately 60 million people.

Types of food required for Lend-Lease and the armed forces are the finest we can produce. They are the high protein foods, especially meats, cheese and milk; and the protective foods which rate high in vitamin content. Peculiarly enough, the more valuable a food is from a nutritive angle, the more specialized is the processing required to preserve it.

The food processing industry, handicapped as it is, is meeting today's challenge with resourcefulness and enthusiasm . . . despite container complications and shipping shortages.

This is the tenth of a series of editorials appearing monthly in all McGraw-Hill publications, reaching more than one and one-half million readers, and in daily newspapers in New York, Chicago and Washington, D. C. They are dedicated to the purpose of telling the part that each industry is playing in the war effort and of informing the public on the magnificent war-production accomplishments of America's industries.

It is accomplishing its Herculean task by resurrecting and modernizing a method of food preservation that is as old as mankind. Probably you have read a great deal about dehydration. You actually may have eaten dehydrated food, but right now nearly every bit of dehydrated food is earmarked for the armed forces or for Lend-Lease.

Food processing never will be as spectacular as the production of bombers or tanks. But under today's conditions, the performance of the food processor is no less important . . . no less inspiring. When we consider that dehydrated food is compressed into solid blocks with a density nearly equal to that of coal, so that almost a whole meal can be carried in a vest pocket, and that half of the shipping space is thereby saved in transportation, we begin to appreciate what the processors have contributed to meet the food problem imposed by the war.

But they have not only contributed new methods, they are achieving new highs in production. And now they are asked to do what borders on the impossible. Consider dehydrated egg powder. Normal production in pre-war years was about 3,000,000 lbs. In 1940 this was increased two and one-half times, in 1942 it was stepped up again, this time forty-fold. And in 1943 the call is for another 60 per cent boost, to make a total of 480,000,000 lbs. Dried milk powder production of 350,000,000 lbs. in 1940 must be increased to 685,000,000 lbs. in 1943.

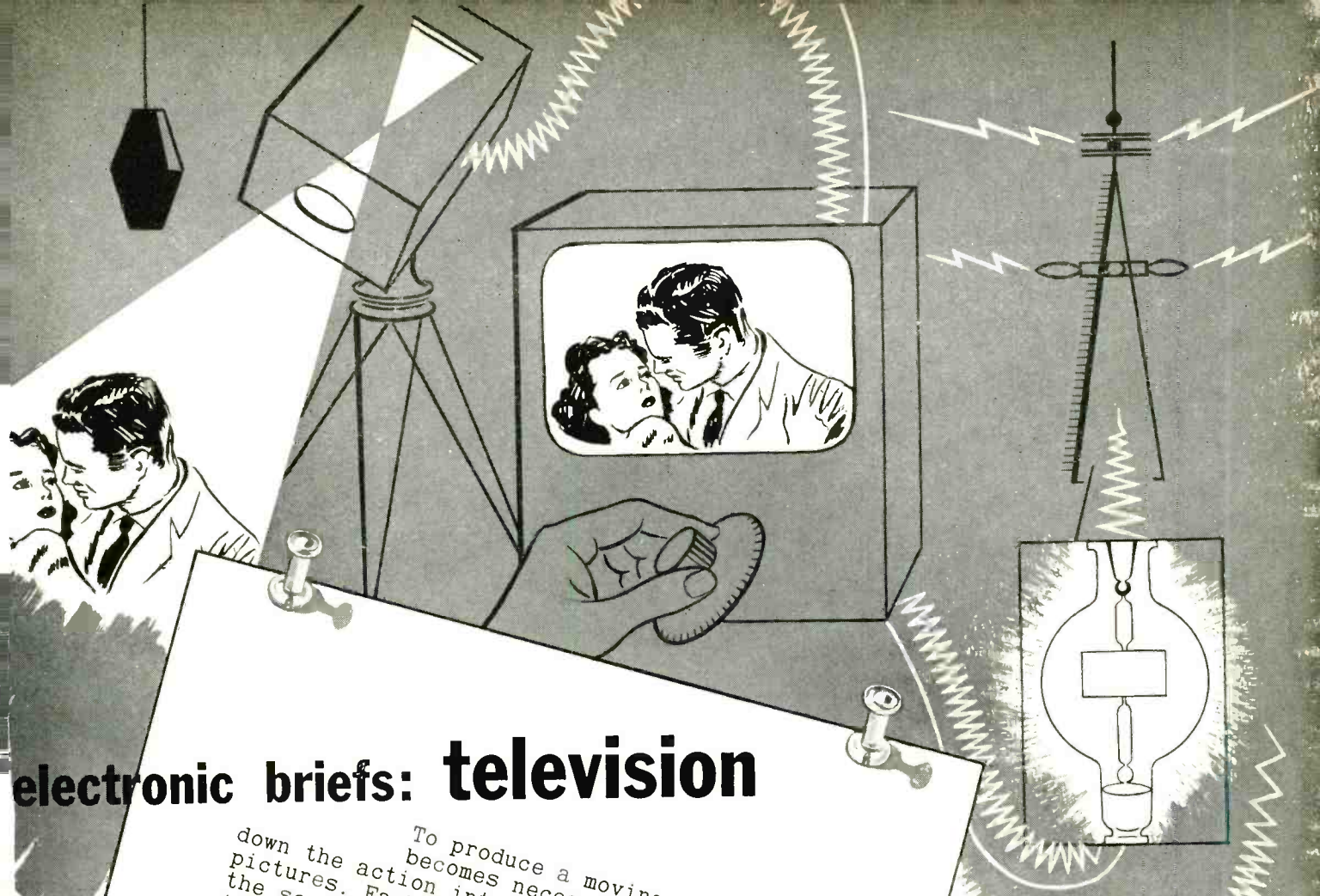
Vegetables, which were a small item to the processor before the war, now are dehydrated in enormous quantities. The vegetable dehydration industry has had to grow by leaps and bounds without benefit of the high priorities accorded to arms, ship and aircraft building. Production of dehydrated vegetables in 1942 was four times that of 1941, and 1943 calls for a sixteen-fold increase over 1942.

Total dehydrated food production in 1943 is scheduled at 1,750,000,000 lbs., dry basis . . . *all for export.* Multiply that by 10 and you have a rough approximation of the astronomical amount of raw materials that will have to be produced.

Many problems remain to be solved in the troublesome days that lie ahead. But with all his resourcefulness, man has little control over the weather. A severe drought could wipe out all of man's carefully laid plans. If we are tempted to reassure ourselves with the thought that the food situation probably is not so serious as it is painted, it will be well to remember that last year's crop increase over 1941 was due to better than average growing weather.

The war-bred food crisis that now confronts us will be met only by immediate measures to insure a food production ample to allow for adverse weather conditions. The food processing industry is capable, but has not been granted the needed help, in coping with its tasks. The food problem as a whole involves all three functions of production, processing and distribution. And if we are to master the problems that now beset us, all three of them must be coordinated under a single administrative control. "Food will win the war and write the peace". But if American food is to do that double job, we must develop a capacity for food *administration* comparable with the genius of our food industries.

President, McGraw-Hill Publishing Company, Inc.



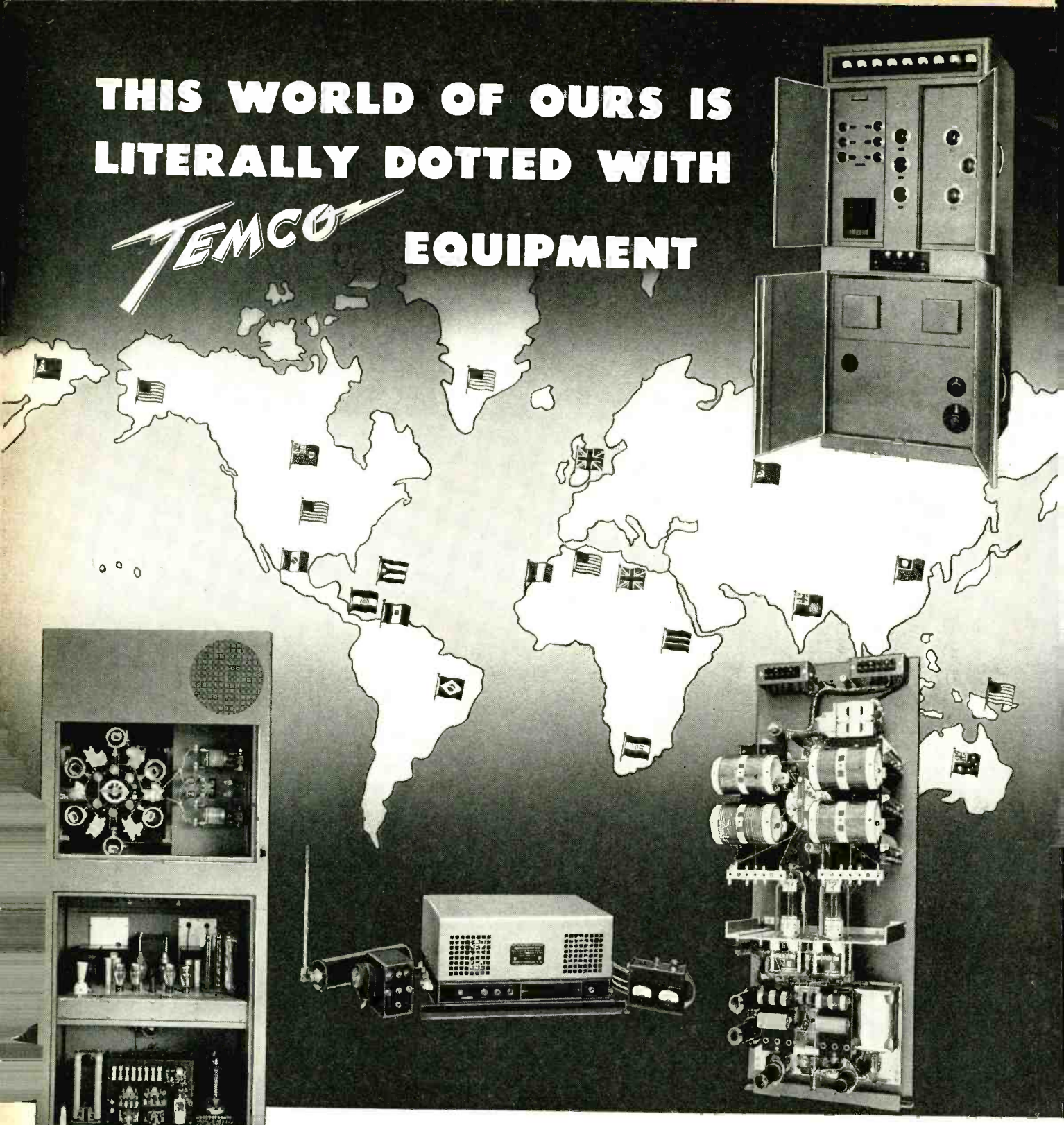
electronic briefs: television

To produce a moving picture it becomes necessary to break down the action into a series of still pictures. Each still scene is flashed on the screen individually but done so rapidly that the human eye sees a smooth action. If the motion picture projector is slowed down the action becomes jerky. Each still picture is called a frame. The conventional movie projector flashes between 24 and 30 frames per second on the screen. Television is based upon the same principle but the problems involved are much more complex.

Television, using the same basis for creating picture action as the movies, breaks down the picture or scene to be broadcast into a series of still pictures called frames. But each frame must also be broken down into approximately 200,000 tiny segments, each segment being broadcast separately and reassembled at the receiving end so rapidly that 30 frames can be flashed on the screen every second. Thus some 6,000,000 separate signals must be transmitted per second. Furthermore each of these signals starts as light, is converted into an electrical impulse, broadcast and then reconverted to light again. To make television talk, a conventional sound transmitter must be coordinated and synchronized with the picture broadcast.

As with all things in the field of electronics, vacuum tubes are what make television possible. Remember; Eimac tubes enjoy the enviable distinction of being first choice among leading electronic engineers throughout the world.

THIS WORLD OF OURS IS LITERALLY DOTTED WITH TEMCO EQUIPMENT



TEMCO

TEMCO IS NOW demonstrating its superb performance in the far flung corners of a mighty global war . . . from Alaska to Madagascar and from Greenland to China . . . for this military conflict has brought about a demand for radio equipment beyond our most far-sighted visualization. The excellence of TEMCO engineering and workmanship is reflected in these units . . . typical of the quality that will *again* be available for the broad requirements of commercial radio communication.

STANDARD AND CUSTOM-BUILT RADIO COMMUNICATION EQUIPMENT

TRANSMITTER EQUIPMENT MANUFACTURING CO., INC.
345 Hudson Street, New York, N. Y.

WASHINGTON FEEDBACK

☛ When the story of World War II is fully told, the battle of communications will furnish one of the most spectacular chapters. Even today, and despite the atmosphere of hush-hush, one cannot mistake the sense of urgency and expectation back of every phase of the government's radio and radar program.

One day, for instance, Robert P. Patterson, Under Secretary of War, tells a congressional committee that while the War Department has plenty of "inspectors" in production plants, the only "expeditors" are for plants making radio and radar equipment, thus bespeaking the urgency of speeding up those programs and their far-reaching implications.

A few days later, chief analyst of the BEW, Dr. Lyman Chalkley, reports to the American Council of Public Affairs that radar, neglected in time of peace because of the alleged lack of profit motive, is the most dramatic new weapon of this war. It was necessary to start almost from scratch to get radar from the stages of laboratory curiosity to the manufacture of practical instruments, he said.

Dr. Joseph Slepian of Westinghouse goes even further in his address before the Science Talent Institute in referring to electronics as "the fresh and expanding vista that lies before the electrical engineer of today and tomorrow."

It was against this backdrop that the major happenings of the month took place.

WPB—Shake-up in WPB and vesting of control over materials allocation and production in Vice Chairman Charles E. Wilson means more and not less tightening of control over war materials. Wilson stands ready to assume full responsibility for the assignment of orders for components (see WPB Order M-293). Drastic regulations were set up for a few items of which radio test equipment is one. Lesser controls have been imposed on the rest of the 32 items which are designated as critical, including certain types of tubes, condensers, capacitors and control instruments.

Present setup should cause no upheaval in the R and R Div. of WPB. Mr. Wilson is communications-minded; he knows the industry and its production capacity. The Division has been functioning under his direction for some time. Relations with Army and Navy are friendly and cooperative. An outstanding example is the work of the Standardization Committees under S. K. Wolfe, chief, WPB Resources Branch. When this work is finished, every component used by the Signal Corps will be included. Mr. Wolfe wants all standardization of component parts to be completed in less than a year. About $160,000 more will be needed for the job.

Resources Branch is also responsible for formation of production integrating committees in the field of resistors, electrical measuring instruments and capacitors. These committees will eventually be extended to all components; will integrate best manufacturing practices throughout each component industry. The work is a continuation of that done by the Industry Advisory and Standardization Committees.

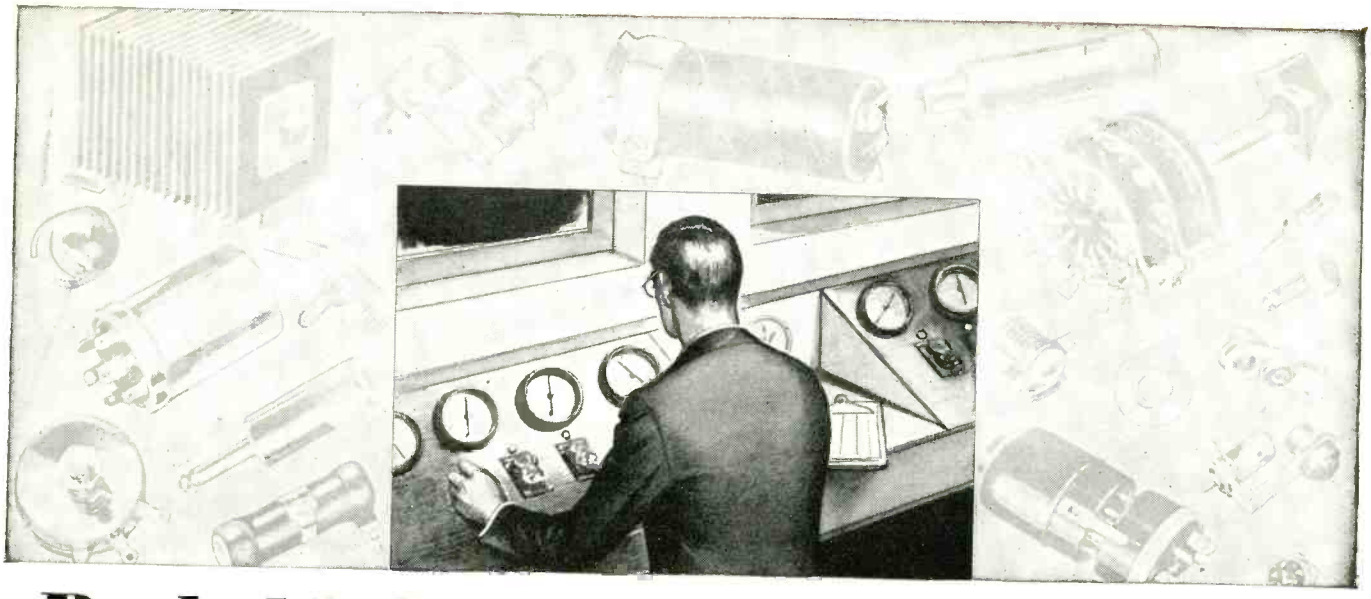
Steatite—An interesting report on Ceramic Capacitors and Steatite has just come from the Industry Advisory Committee, headed by Elmer Crane, Chief of the Component Section of WPB Radio Division. Evidently steatite is no longer a bottleneck in the production of military radio equipment. Producers are able to accept orders for delivery in from four to eight weeks vs eight months backlog last summer, because facilities constructed to meet war demands are now in operation and because phenol plastics have been substituted for steatite. There is a danger now that the pendulum will swing too far towards phenol and cause a scarcity of it instead of steatite. Producers of ceramic capacitors forecast sharp increase in output within two months because of new facilities now being completed.

Manpower — Recognizing that program objectives hinge as much if not more on adequate manpower as they do on materials and orderly scheduling, the government and industry have moved to solve this No. 1 problem. "Electronics Manpower Advisory Committee" has been organized to prepare recommendations to War Manpower Commission and other government agencies. Formed by the Radio Division of the Bureau of Ships, United States Navy; the Army and Navy Electronic Production Agency and the Radio Division of the War Production Board. Management members are: L. B. Morris, R.C.A. Mfg. Co., Inc., Chairman; J. D. Washburn, Sprague Specialities Co., and W. K. Wiggins, Western Electric Co., Chicago.

Labor members are: Harold Sharpe and James J. Conroy, United Electric, Radio and Machine Workers of America, C.I.O., and Lawson B. Wimberly, International Brotherhood of Electrical Workers, A.F.L.

At the organization meeting, attended by representatives of Armed Services and WPB, a special task committee was set up to summarize electronics manpower problem for presentation to the committee. First subject to be studied is that of absenteeism.

Additional Washington news will be found in Crosstalk and Industry in Review.



Probably Your Mallory Distributor Can Give You Help Like This—

Somewhere in the Middle West is an aircraft engine manufacturer who uses many Mallory Electronic parts in dynamometer test cells. Recently he sent us a hurry call for some Mallory phone jacks to go in the control panel of a new cell being rushed to completion. He had the right priority, too.

It was a standard jack, but as is so often the case with manufacturers immersed in war production, it was out of stock. To produce it, we would have had to start from scratch—"when, as and if!"

But we referred his request to the local Mallory distributor—who filled his needs from stock.

This is just a sample of how Mallory distributors can help. We do our level best to furnish them with adequate stocks so that essential electronic parts to fill small orders with high priorities may be handled promptly.

It will pay you to maintain a contact with your local Mallory distributor. He will give good service, furnish your purchasing department with complete information and prices; your engineering and design departments with application data; work his head off to get you those parts you need for maintenance, test equipment and pre-production models.

P. R. MALLORY & CO., Inc., INDIANAPOLIS, INDIANA

Cable Address—PELMALLO

Get acquainted with your local Mallory distributor. Or if you do not know who he is, write us and we will put him in touch with you. And, for good measure, we will send along a copy of the Mallory Catalog for ready reference.

P. R. MALLORY & CO. Inc.

MALLORY

APPROVED PRECISION PRODUCTS

CROSS TALK

► **GARCIAS** . . . At the recent AIEE-IRE meeting in New York City, Brigadier General F. E. Stoner, Director of the Army Communications Division, Signal Corps, paid a fine compliment to the many behind-the-lines communications engineers designing and producing electronic equipment for the armed services. He told of the Army major who got a medal for taking a message to Garcia in another war. "In this war," said the General, "there are thousands of soldiers carrying thousands of messages to thousands of Garcias." After the war some means must be found for letting the rest of the nation know how electronic men in the many laboratories and factories and communications systems have made possible the carrying of these messages with accuracy, speed and security.

► **MARCH 8** . . . As of this date, the President signed the bill merging Western Union and Postal Telegraph. Thus, in time, the United States will have a single integrated land-line communications system for telegraph. Chairman Fly of FCC prophesied that the merger would result in better telegraph service.

"You see," he said, "the great difficulty in having parallel lines under different management is that you can't use vacant capacities as they occur, but where the telegraph is under a single management you can fall back on whatever facilities and personnel you have that can be adapted to the particular need."

► **SYMBOLS** . . . People growing up in different and widely spaced parts of the world developed their own languages. In a smaller way, electrical engineers working in radio and in power fields have developed their own languages, much of which is moderately unintelligible to each other. A generator, for example, means only a piece of rotating equipment to a power man; although to a radio engineer it may mean a tube oscillator. Even the symbols which these two branches of electrical engineering employ in their blueprints are not alike. A zigzag line to a radio engineer is a resistor; to a power engineer it is an inductor.

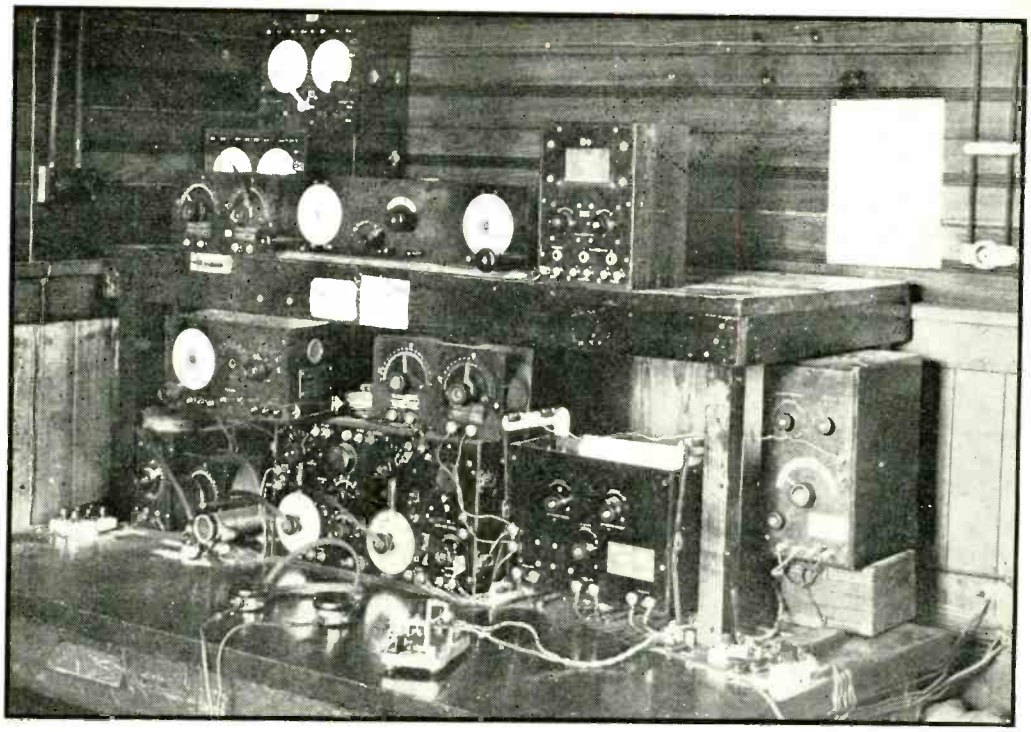
In this issue, Mr. Dudley surveys this situation, pointing out the similarities and the differences. Because of the long standing practices to which engineers have become accustomed there is little liklihood that the differences will be reduced during the war. Which proves, probably, nothing but that engineers are people like the rest of us, agreeing on big things, disagreeing on trifles.

► **AMEN** . . . On March 2, FCC announced following terminology defining the bands in the useful radio spectrum.

Frequency in KC		Mc	Designation
10 to	30		Very Low (VLF)
30 to	300		Low (LF)
300 to	3,000	3	Medium (MF)
3,000 to	30,000	30	High (HF)
30,000 to	300,000	300	Very High (VHF)
300,000 to	3,000,000	3,000	Ultra High (UHF)
3,000,000 to	30,000,000	30,000	Super High (SHF)

► **FCC** . . . Narrowly escaping starvation or at least a drastic budget cut when a move was made in the House to eradicate its 1944 fiscal year $7,609,914 appropriations from the Independent Officers Supply Bill, FCC was saved by Speaker Rayburn in his first speech in this session of Congress.

► **DREAM** . . . We woke up the other night from the damndest dream in which we were saying to someone, whose identity was lost in the shuffle, "It is the strangest thing how the manufacturers who have the best products and the swellest catalogs always get their information to you just after you have been forced, by time limitations, to order your stuff from someone else." We haven't the remotest idea what was going on in our subconscious mind to bring forth such an illuminating statement.



How far the Navy has gone with radio communication may be seen by looking over this NSF-NOF apparatus of 20 years ago. This is an early superheterodyne used for communication with planes. Old timers will recognize on the top shelf the two-stage audio amplifier (SE 1000) which amplified so well at 1000 cycles it wanted to oscillate all the time. Assigned to find out why, Hazeltine started on his way to the Neutrodyne. Lower center is the celebrated SE 1420 designed by Hazeltine

Radio and Electronics in

From the earliest days of "wireless," the United States Navy has made wide use of radio for communication. Through its own research, the Navy has made important contributions to the application of electronics to communication and to other, now secret, uses. A brief history plus details of the present Navy radio organization under the Bureau of Ships

By S. P. SASHOFF

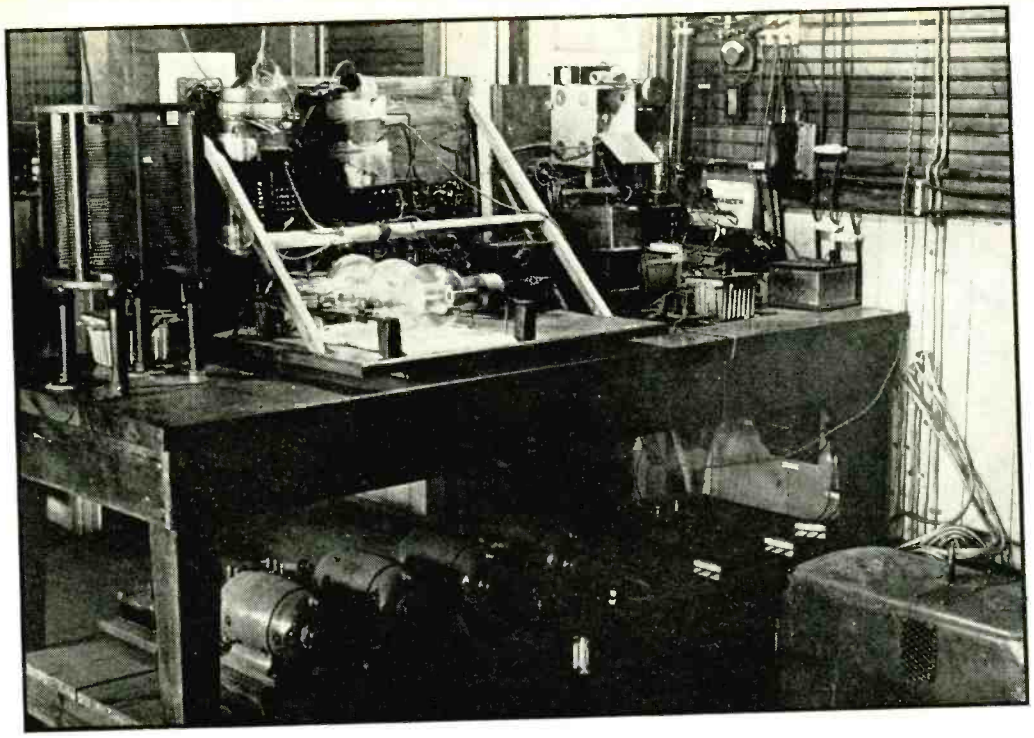
Lt. Comdr. USNR.—Officer in Charge Training and Publications Section Radio Division, Bureau of Ships

THE United States Navy has long recognized the value of electronics in the conduct of warfare. From the earliest days of the science to the present, the attempt has been made to examine and make use of every worthwhile development in the field. In many cases, the advances came from commercial companies. In others, Naval and other government laboratories and activities have made substantial contributions of their own. The result of the progressive policy of past years is that the vacuum tube is now one of the most important weapons our Navy has for winning the war.

A vast amount of coordinated effort is required to meet the present electronic needs of the fleet and air arm. Many thousand men and women, in the Navy and outside of it, are working on electronic equipment. Hundreds more are administrators, functioning solely to see that the following sequence of events occurs with efficiency and dispatch: to see that a new tool, a good war tool, is designed; that it is carefully built; that men are trained to use it; that, if it breaks, it is repaired.

The guiding agency for the Navy's present radio and electronics program is the Radio Division of the Bureau of Ships in Washington. This Division is responsible for design, procurement, installation, and maintenance of all radio equipment for use on board ship and shore, and, in cooperation with the Bureau of Aeronautics, for the design and procurement of aircraft radio equipment. The organizational chart serves to give an idea of the complex structure necessary to do the job.

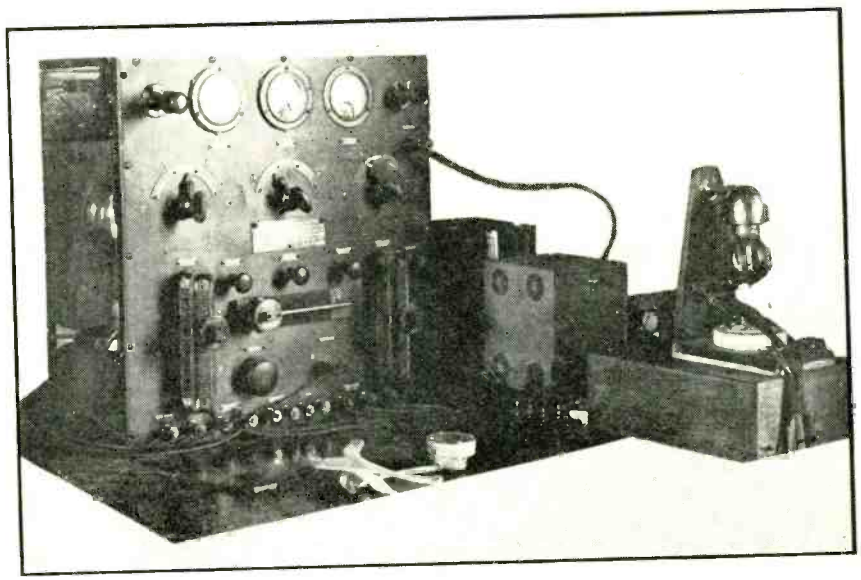
Before the last war, the only Naval use of the vacuum tube was in radio. "Electronic design" meant a new hookup to get the most from a Fleming valve or, better, an audion. Today, though electronics is no longer confined to communications, the need for a dependable fleet radio system continues. It is interesting to note, therefore, that the Navy brought many radio developments into use in this country, was for many years the biggest user of radio gear, and had many skilled radio engineers in the days of the great discoveries of deForest, Fessenden, and Armstrong.



Transmitters weren't so hot in those days either, compared to modern standards. This is rear view of NSF "table model"

An aircraft job. This is the SE 1100 tube transmitter dating back to December 1919

the Navy



The interest of the Navy in radio dates back to 1901, when a proposal was made to replace homing pigeons with wireless telegraphy. In 1902, an offer from the Marconi Company to lease equipment was turned down because the transaction involved disclosure of Naval information to a foreign concern. In 1903, a satisfactory arrangement was made with another company, and work on wireless installations began. By 1912 a number of stations were in operation, the huge Arlington transmitter had been completed and the first Naval purchase of triode vacuum tubes—audions—is recorded.

The early research work in Naval radio was undertaken by a group of Bureau of Standards personnel, headed by Dr. L. W. Austin. Two small rooms at the Washington Navy Yard were taken over, and became the radio test shop. Here trained officer and civilian assistants were assigned special problems in the design, standardization, and testing of communications equipment.

The advent of the first world war brought increased responsibility to these men and the others concerned with Naval radio. Improved equipment and new developments were urgently needed. Among the achievements to grow out of the cooperative effort of Naval and private research during this first World War were the following:

Design of radio equipment for aircraft having 100 to 500 miles range.

Invention of the directional loop antenna by Dr. F. A. Kolster of the Bureau of Standards. This device was manufactured in secrecy and used with notable success as an aid to navigation and to locate enemy stations.

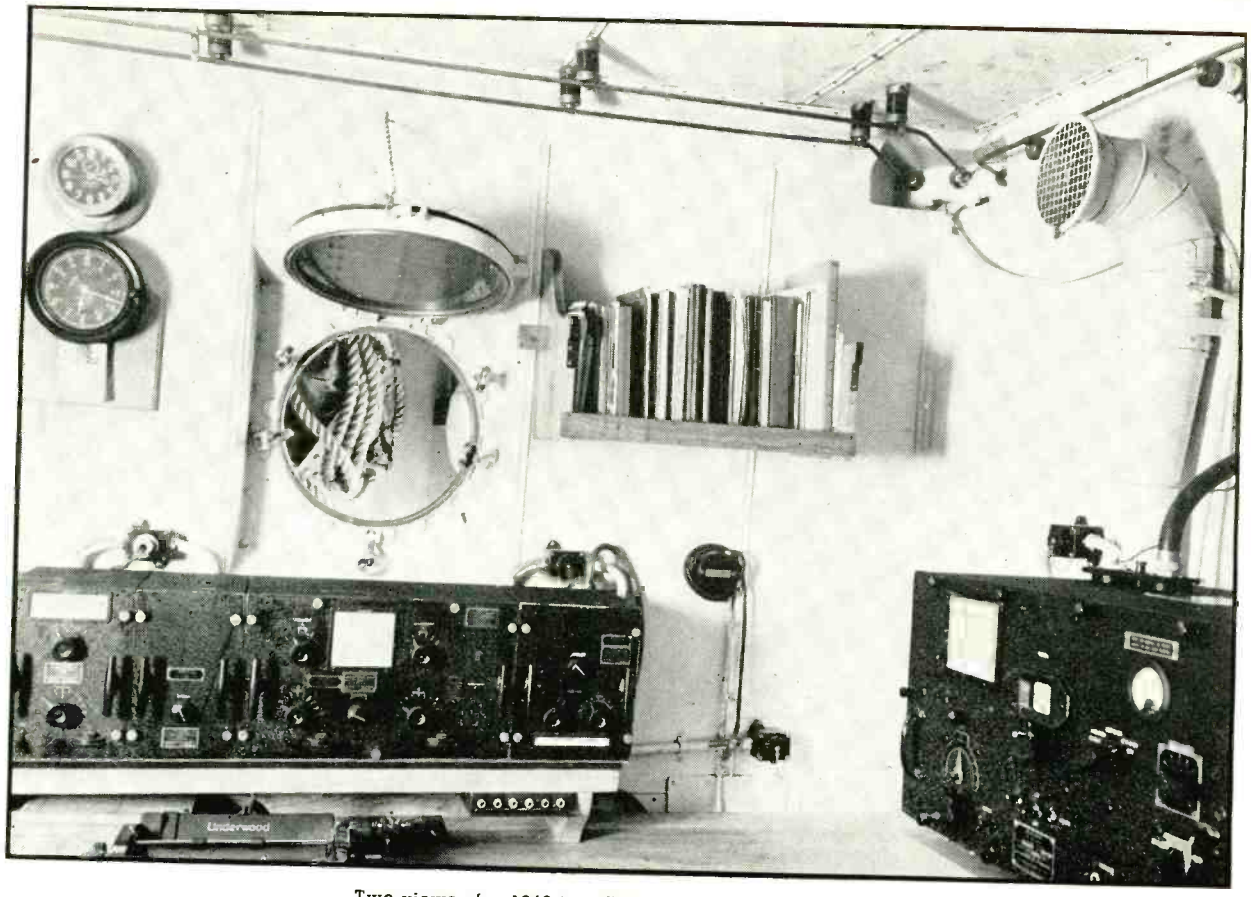
Invention of acoustic methods of detecting submarines.

Development of an audion circuit using both plate and grid tuning.

Development of radio telephone equipment. This was first used in 1916. The original equipment had a range of 30 miles, used three wavelengths, and permitted nine simultaneous conversations.

Design of apparatus for remote control of radio stations, for automatic rebroadcasting.

Investigations into tuned audio frequency amplifiers to reduce static, underground and underwater antennas, and methods of using contact detectors for measurement of small r-f currents.



Two views of a 1942 installation aboard ship. Note the individual receivers for the several bands to be covered. This clean-cut layout is in marked contrast to those of the early days

By the end of the war, Naval radio activities had increased to the point that radio materiel officers were required at practically all Navy Yards. Crystal sets had given way to crystal-audion arrangements and finally to straight vacuum tube receivers. Spark was superceded by arc and the Alexanderson alternator. The transmitting tube was coming in, accelerated by a Navy order for a half million dollars worth of 250-watt types in 1919. Progress in electronics went rapidly forward.

Naval Research Laboratory Achievements

The year 1923 was marked by the opening of the Naval Research Laboratory at Anacostia, D.C. This laboratory filled a long felt need for increased facilities to carry on developmental work in electronics and in other fields. This organization, and the two later laboratories at San Diego and New London, are responsible in large measure for the Navy's high degree of preparedness in electronic design before the outbreak of the present war.

The succesful history of these Naval laboratories has been largely due to adherence to certain basic policies. For example, the only projects undertaken are those which have a direct value to the Navy, and which are sponsored by one of the Naval bureaus. The research work is accomplished by eminent scientists from civilian life, working with technically qualified Naval personnel. The officer personnel is changed every two to four years so that men trained in the latest scientific developments may be with the fleet, and so that replacement officers may bring practical service problems back to the laboratories.

Another beneficial policy has been to enlist active cooperation from the research laboratories of universities and industrial plants throughout the country. More than seventy colleges and industries have furnished invaluable technological assistance in electronics.

A listing of a few of the achievements of the Naval Research Laboratory should prove of interest. The laboratory:

Designed and built the first high frequency and the first ultra high-frequency radio sets used by the fleet.

Developed and installed in the fleet the first multiple reception radio system permitting the operation of a large number of receivers from one small antenna.

Developed the technique of producing quartz crystals for the frequency control of radio transmitters, and designed the first crystal controlled high frequency high power transmitters in 1924.

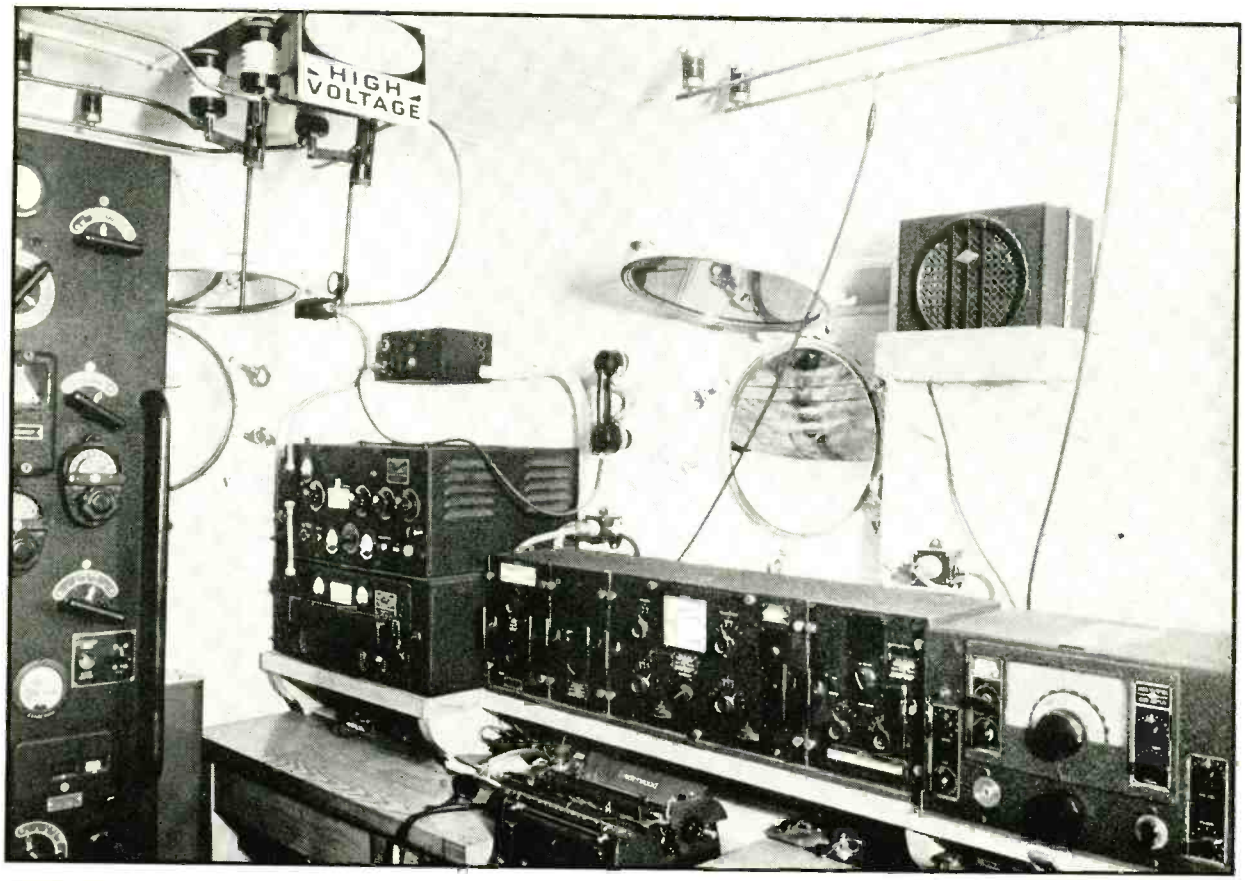
Designed special radio transmitting and receiving equipment for the U.S.S. Shenandoah. This was the first high frequency radio equipment ever used in the air.

Developed the sonic depth finder, the first successful acoustical means for measuring ocean depths from a ship under way.

Was the first to use the hull and other parts of a ship's structure for the radiation of radio energy without a conventional antenna.

Assisted in the development of direction finding units used in all types of ships.

Developed an underwater sonic de-



Spark apparatus of the last war has given way to tube transmitters, crystal detectors to highly selective and sensitive tube receivers; long waves to intermediate and short waves

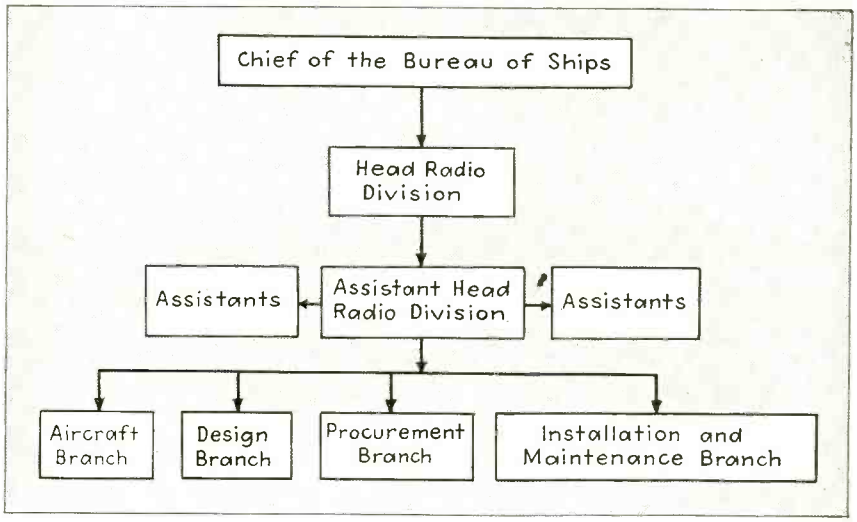
vice by use of which cruisers, destroyers, and other anti-submarine craft are enabled to detect enemy submarines at considerable distances.

Developed a system for the radio control of aircraft in flight, resulting in use of a considerable number of obsolete Naval aircraft as targets for anti-aircraft practice.

Many other research projects have been successfully completed which cannot be discussed here, for reasons of security.

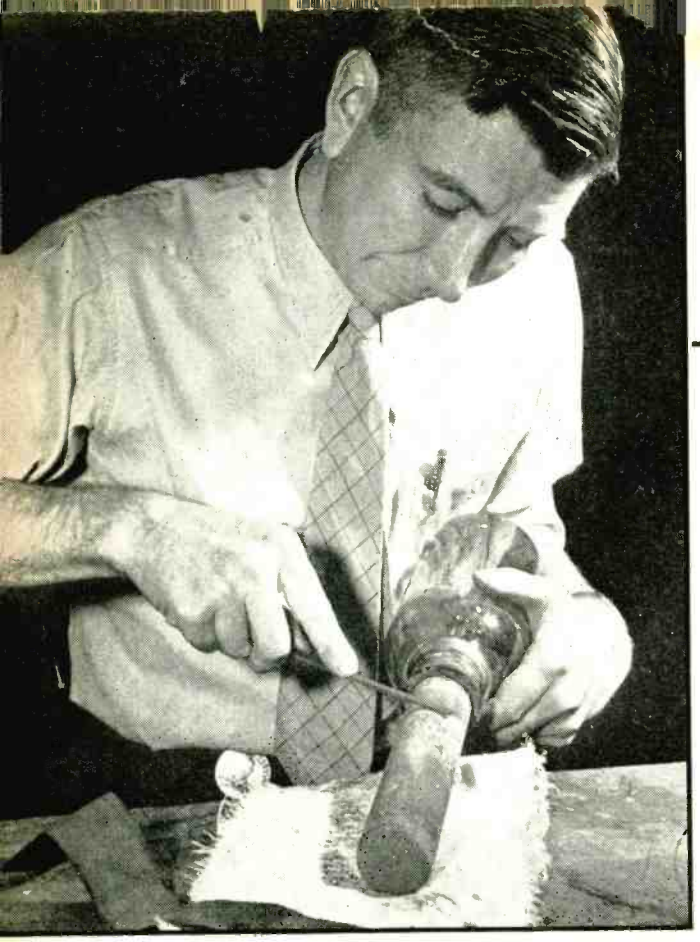
Today electronics means to the Navy—in addition to radio—underwater sound, direction finding, control of electro-mechanical systems, and a host of other non-communication services. In terms of design it means forward-looking ideas—and a good sense of what's practical. This last is important. Service conditions are tough. Temperature variations may be from −40 deg. to +85 deg. C, and humidity from low values up to 95 percent. The equipment must be built to withstand the corrosive action of salt spray, constant vibration, and the shock of gunfire. It must be built to take all the rigours of modern warfare and, if trouble develops, must be capable of speedy repair from the material on hand at distant bases.

The Navy is depending to an ever-increasing extent on radio and electronics. The coordination of intensive research, skillful engineering, and careful manufacture is making the best equipment which can be produced, available to the fleet. The men who design, build, and operate this complex equipment, contribute materially towards winning the war.



Radio and electronic matters of the U. S. Navy are handled by the Bureau of Ships. At the present time Captain Jennings B. Dow, a contributor to radio technique of long standing, is head of the radio division

RULES FOR



Carl Wirth, test operator at Westinghouse Lamp Division, demonstrates one method of removing hard water precipitates from a rectifier anode

AT this time when the electronic industry is being expanded and pushed for ever-increasing production of tubes vital to our war effort, it is imperative that every possible precaution be taken to prolong the life of our electronic devices. No longer is cost the prime incentive. It is the inability to obtain a replacement for an important tube that now induces us to make every effort to prolong its life.

The observations and experiences of the author on ways and means to prolong the life of electronic devices are given in the belief that this information can contribute to the war effort.

Electronic tubes can be divided into three general classifications, (1) Pure tungsten filament types (2) Thoriated tungsten filament types (3) Oxide coated filament and indirectly heated oxide coated cathode types.

The golden rules of the tube user should be these:

(1) Use the electronic device within its ratings.
(2) Operate the tube at the filament voltage recommended by its manufacturer. (Measure it—don't guess).
(3) Keep the tube clean at all times—contact terminals, glass bulb, and anode (if water cooled.)
(4) Supply an ample cooling medium when required.
(5) Neither apply filament voltages suddenly nor remove them suddenly except as permitted by the manufacturers' ratings.
(6) Do not apply filament and anode voltages simultaneously except as permitted by the manufacturer's ratings.
(7) Handle this device carefully, as sudden shocks will probably damage it.

The pure tungsten filament types, for example, the 207, 891, 892, 893, 895, 899A and 898, are usually designed for operation at about 2550 deg. Kelvin. At this temperature the evaporation rate of tungsten from the filament is 13.5×10^{-9} gram per square centimeter per second.* If we can reduce this temperature by only 50 deg. and yet get passable performance we can more than double (theoretically) the useful tube life as the evaporation rate is then 6.36×10^{-9} gram per cm^2 per second.

Two curves are shown in the figure. One curve shows the expected tube life expressed as a percentage. It is based on the expected life at rated filament voltage of 100 percent versus rated filament voltage expressed as a percentage. The other curve shows the expected emission versus filament voltage and again is expressed in percentages.

While pure tungsten filament tubes do have a rated voltage, we may express as a generality that "The most economical filament voltage for a pure tungsten filament tube is the lowest voltage which permits satisfactory operation." This generalization holds true within quite wide limits but it would be wise to point out the restrictions and precautions which should be observed in its application.

When used as an oscillator (class C operation) for induction heating, certain minimum power output requirements are usually necessary. To find this most economical filament voltage we may reduce the filament voltage to the point where a decided rise in either the cooling radiator temperature or cooling water temperature takes place. If the minimum requirements on power are met at this point then that filament voltage will be the most economical.

In water cooled tubes, if the filament voltage is reduced too far the formation of steam bubbles at the anode surface will probably occur and the tube may be permanently damaged or destroyed. The formation of steam bubbles may be detected by placing the end of a piece of long insulating tubing against the tube radiator and listening at the other end. (Caution—A good ground should be used on the end of the tubing next to the ear.) When steam bubbles start, the sound is quite distinctive. The formation of these bubbles may be prevented by a higher velocity water flow and by making certain that the filament voltage is not reduced too far. For radiator cooled tubes, one may observe this minimum permissible filament voltage by reducing the filament voltage slowly thus giving the radiator temperature ample time to reach an equilibrium temperature.

* Jones and Langmuir—GE Research Lab. Report No. 419.

PROLONGING TUBE LIFE

BY HAMPTON J. DAILEY

Electronics Engineer, Westinghouse Electric & Manufacturing Company, Bloomfield, N. J.

This increased anode dissipation is the result of an increased tube voltage drop during the conducting portion of the cycle, that is, during the time the grid is essentially positive with respect to the cathode. If the filament voltage is reduced too far, the tube voltage drop may become a major portion of the total applied voltage and, therefore, the power dissipated in the anode may be sufficient to melt it or heat it to the point where sufficient gas or metallic vapors would be released to permanently damage the tube.

Distortion May be Limiting Factor

For the triodes used to provide the carrier for broadcast stations, another approach is necessary to determine the correct voltage for maximum tube economy. (We may no longer use the same method as that outlined for straight oscillator service as other factors have to be considered.) The filament voltage may be reduced to the point where distortion or harmonic percentage is at the maximum permitted when maximum modulation is being used. The voltage may then be increased just beyond this point.

Let us examine the tabulations given in the table. Under the normal and light load columns for tungsten filament types, we find "100 percent" and "reduce." The 100 percent value may be considered as that filament voltage which satisfies the operating conditions as set forth in the foregoing paragraphs. For conditions of light or reduced load, the filament voltage may be reduced to the point where the same operating conditions are reached for that reduced load.

Where "hard" water is used for cooling tubes, rule 3 should be applied rigorously. With hard water a scale that is essentially lime is formed. This should be removed periodically as it reduces the tube's dissipation capabilities which in turn can cause tube destruction. This scale may be removed by the careful use of a scraper as shown in the illustration or by immersing the anode (usually copper) in a 10 to 25 percent solution of hydrochloric acid. The acid will remove the lime but does not attack the copper. The anode should then be rinsed thoroughly with tap water to remove all traces of the acid.

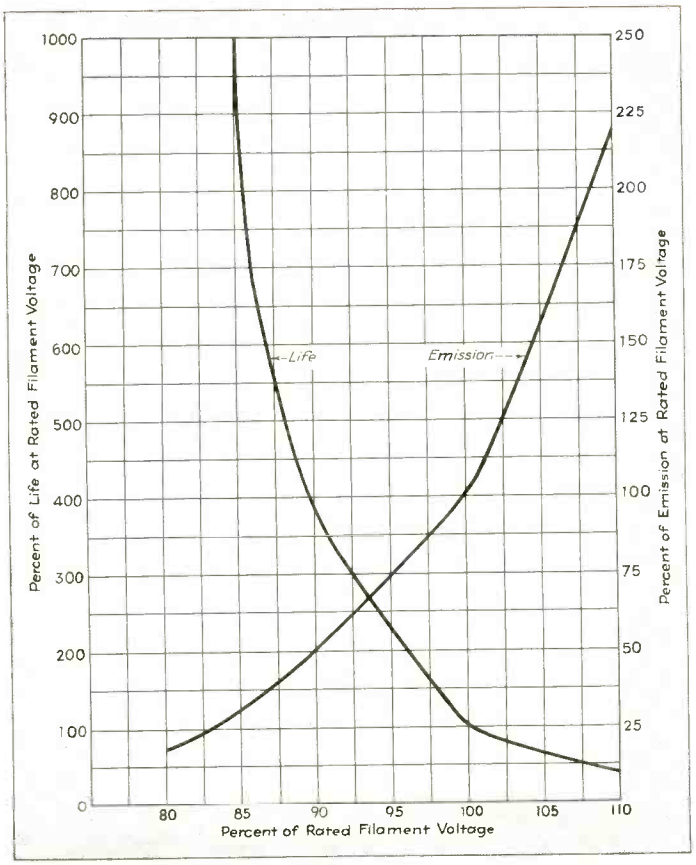
Another application of rule 3 is in keeping the tube contacts clean and particularly the filament terminals. As the filament currents are usually quite high, any dirt, lint, or oxidation presents a comparatively high resistance to the filament current with resultant heating at the contacts. This effect becomes cumulative and may permanently ruin the tube. Terminals should be kept tight at all times and occasional polishing with a very fine polishing agent is desirable. After polishing, the terminals should then be wiped with a cloth dampened with alcohol. The glass surfaces should also be cleaned periodically with an alcohol dampened cloth. This prevents the formation of sufficient dirt or lint on the glass surface which promotes tube punctures.

An insufficient flow of water can contribute to premature tube failure by permitting chronic formation of steam at the anode surface. An interlocking switch on the high pressure side of the water supply will guard against water supply failure while an interlock in the low pressure side will prevent tube damage due to foreign matter clogging up the water jacket. A similar interlock should always be used in the air stream of an air-cooled installation.

The sudden stresses which take place in the filaments and filament leads when the filament voltage is

Percentage of Rated Filament Voltage to be Used Under Operating and Stand-by Conditions to give Maximum Filament Life

Tube type by kind of filament	Operating Conditions		Recommended Stand-by Conditions				
	Normal load operation	Light load may increase life	Under 15 min.	15 min. to 2 hrs.	2 hrs. to 12 hrs.	Over 12 hrs.	Typical tube types
1. Tungsten filament in small & medium sized tubes	100	reduce	80	80	off	off	207, 891R, 892R
2. Tungsten filament in large tubes	100	reduce	80	80	80	off	895R, 899A, 898
3. Thoriated tungsten types	100	95–100	80	off	off	off	211, 803, 851
4. Oxide-coated direct heated filament (gas) (vapor)	100	100	100	100	off	off	866A, 872A
5. Oxide-coated heater cathode types (high vacuum)	100	95–100	100	80	off	off	807, 837
6. Oxide-coated heaters in large tubes (mercury vapor)	100	100	100	100	100	off	857B, 870
7. Oxide-coated quick heater types (high vacuum)	100	95–100	80	off	off	off	1619, 1624, 1616



Effect of filament voltage on life and emission from pure tungsten filament. Assumptions are that filament is operated at constant voltage throughout life; that at beginning tube operates at 2550°K with rated voltage; that life is ended when filament current has been reduced 10 percent by evaporation

applied or removed suddenly can lead to premature failure, especially in the larger size tubes. Most manufacturers limit the starting current to 150 percent of the rated current on the larger tubes and it is well to heed this limit by using a starting device. For small size tubes, the filament transformers are usually designed to limit the maximum starting currents to from 200 to 300 percent of the rated filament current.

In the table the recommended filament voltages for stand-by conditions show 80 percent. This value was selected as it reduces the tungsten evaporation to a negligible factor and at the same time reduces to a minimum the number of times the filament and its supports must undergo the stresses of the heating and cooling cycle when reducing the filament voltage to zero or starting up from zero.

Avoid Filament Stresses

For tungsten filament rectifiers we may say that the most economical filament voltage is that minimum voltage which just permits satisfactory operation. The voltage should not be set at a point which would permit line voltage fluctuations to lower the filament voltage to a point where the rectifier voltage drop would be sufficiently high to cause tube punctures.

Rules for Thoriated Tungsten Filaments

The thoriated tungsten filament types such as the types 803, 833, 211, 810, 806, 849, 860 and 861, require a different handling to obtain an increased useful life. In the table we may note that the recommended filament voltage during operation is never under 95 percent. If a thoriated tungsten filament is operated at too low a filament voltage it may lose its emission rapidly. If operated appreciably beyond its 100 percent rating, the tungsten carbide on the filament surface reduces to pure tungsten at an excessively high rate and the effective life of the tube is shortened. Rule 2 should be applied rigorously.

The tubes should be examined periodically for poor contacts either on the tube itself or its socket. The bulb should be kept clean by wiping with a cloth dampened with alcohol.

The lowest possible anode voltage should be used which will supply the required output. This is always possible when the required power output is less than the tube's maximum ratings. Maximum life will be obtained if the filament voltage is held between 95 and 100 percent of its rated voltage. A violation of this rule is sometimes accomplished unknowingly by users of short-wave diathermy equipment. The voltage fluctuations of well controlled power systems are usually within plus or minus 5 percent but the transformer taps usually provided by the manufacturers of such equipment may not be adjusted or adjustable for the line voltage of the user. Such maladjustments in addition to line voltage fluctuations can easily reduce the tube life appreciably. The users of diathermy equipment can prolong the life of their tubes by observing the rules given. Be sure the output controls are set at their minimum value before turning the equipment on or off. The output control should be advanced slowly from its minimum setting up to that adjustment for the heat required. In this way the tubes will be operating under the best conditions possible. There is a maximum output setting and beyond this point the output again goes down, but the tubes are "over coupled" to the load and thus operate inefficiently and have shorter life.

The care and operation of gaseous tubes was given by D. E. Marshall and W. W. Watrous in the January 1942 issue of ELECTRONICS and will not be covered in this paper. If we assume that all of the precautions outlined in that paper are observed, the user of gaseous tubes may further prolong the tube life by observing the recommended filament voltages given in the table.

The high vacuum oxide cathode or filamentary types, such as the 807, 837 and 1616, may be compared quite closely with the thoriated tungsten types in the care required for long life.

As mentioned before, tubes as a rule are quite rugged and will withstand a degree of abuse, but if we develop a healthy respect for their limitations and provide them with suitable working conditions within the limits of their design capabilities, we will be well repaid by a longer trouble-free life.

RECORDING UNIT
For Strain and Timing Functions

Dynamic performance of heavy machines under actual operating conditions in the field can be permanently recorded by combination of electronic and photographic equipment. Method particularly useful where shop tests cannot be made, or where unusual operating conditions occur infrequently. An important application in industrial electronics

By J. H. MEIER

Bucyrus-Erie Co., South Milwaukee, Wisc.

DYNAMIC strain measurements on machines and structures have long been recognized as an important supplement to design computations. New methods are constantly developed to make dynamic field measurement more accurate, complete, and reliable.

In cases where the designing engineer has no accurate means of estimating the forces acting on his product, it is imperative to check estimates and designs by field measurements when the unit is under actual working conditions. This is, perhaps, particularly true in the case of heavy excavating equipment where the machines are subjected to considerable impact loads and rather complicated dynamic phenomena occur. Shop tests are not possible in many cases because of the size of the machines and because proper test conditions cannot be obtained.

The equipment described in this paper was built to record the performance of machines under actual operating conditions in the field. It lends itself, however, quite readily to laboratory use or to a direct reading instead of a recording unit.

The first requirement is the accurate measurement of strains—be it for determining stresses in structural elements or for the determination of forces by means of calibrated links.

Of almost equal importance is the measurement of instantaneous shaft speeds at the time the strains occur and the recording of the functions the machine is performing.

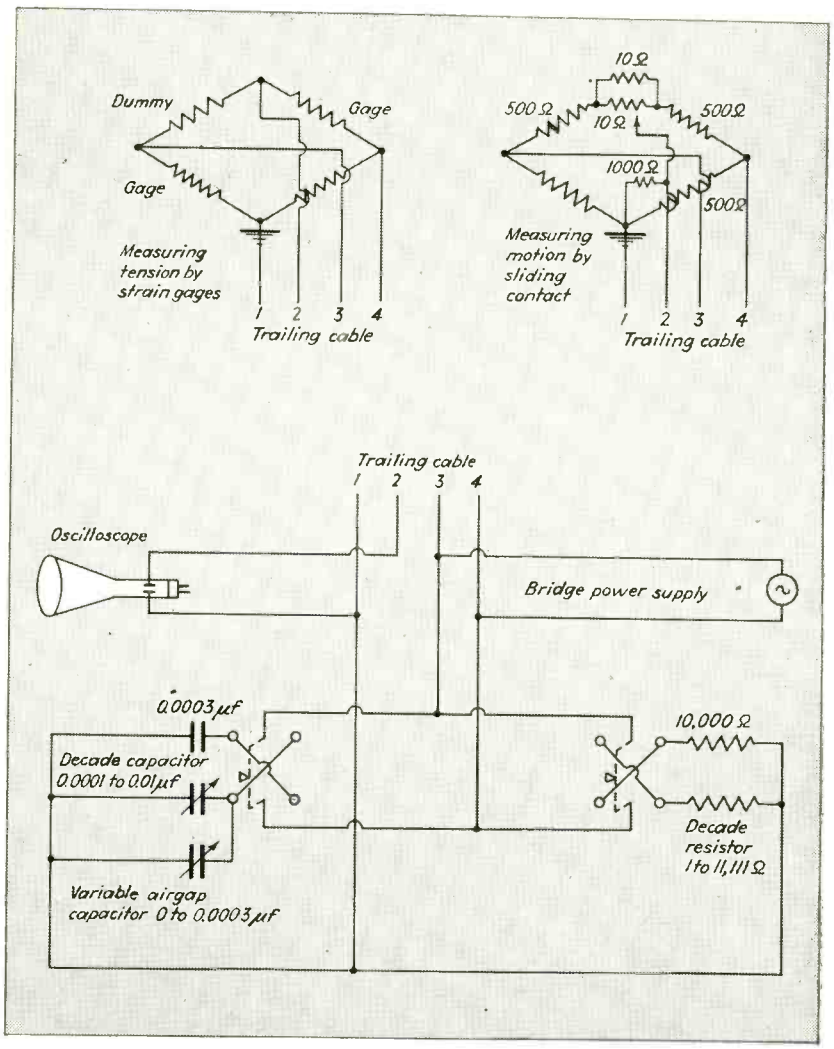


FIG. 1—Schematic wiring diagram of bridge circuits (above) and bridge control circuit (below). Bridge circuit at left is used for recording strain; that at right for recording vibration. Bridge circuits are mounted on machine under test, and connected to control circuit through shielded trailing cable

A typical example is the investigation of the behavior of a fluid drive on an excavator. Load, speed, and slip must be recorded instantly and simultaneously to make possible the analysis of the transient condition when a heavy load is suddenly applied.

Frequencies of mechanical vibrations on heavy machinery may run as high as 50 to 100 cps and impact features may require the recording

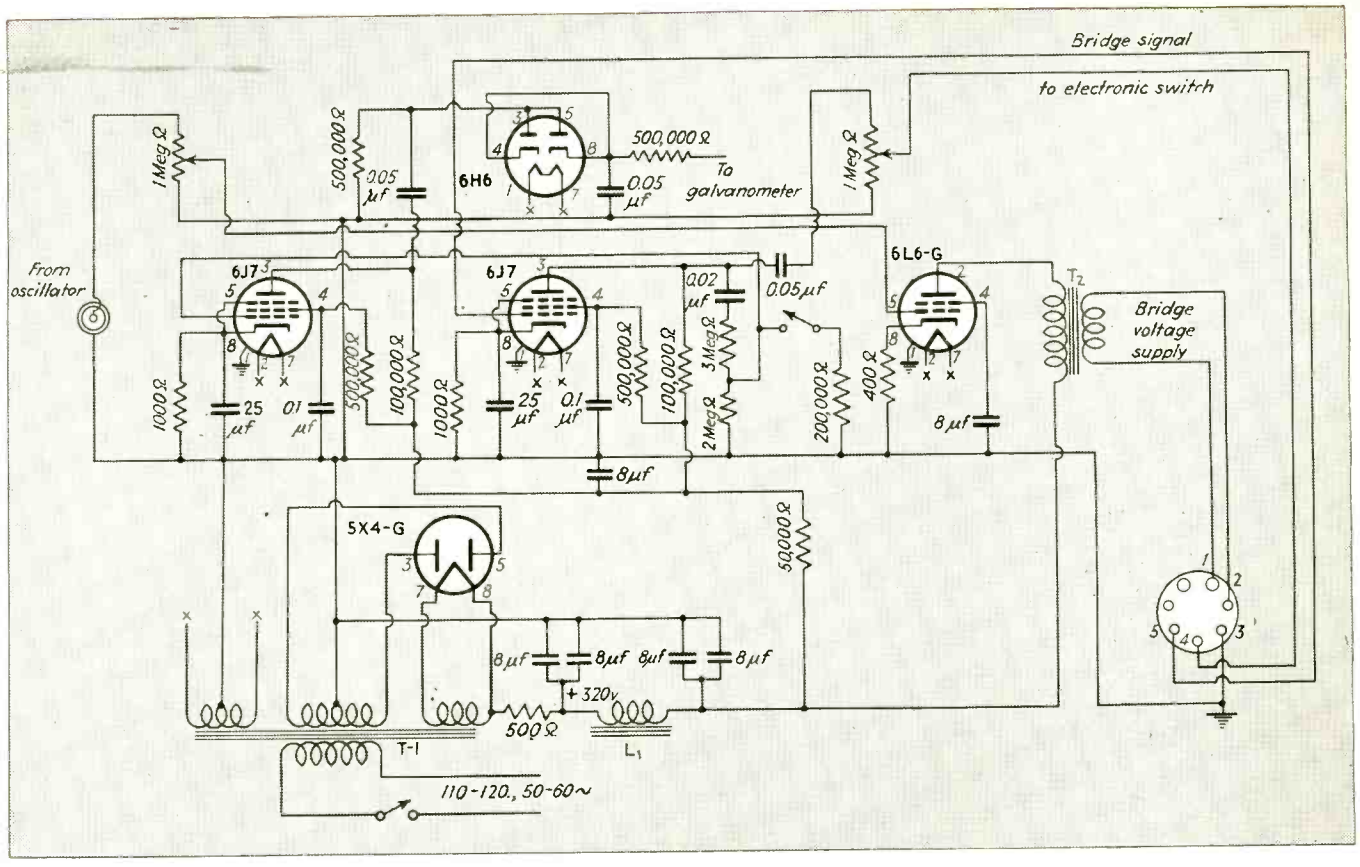


FIG. 2—Modified wiring diagram of amplifier used in strain recorder

of strains of a few thousandths of a second duration. Thus, the severe requirements with respect to speed of recording cannot be met by mechanical recorders because of their inertia distortions. Only entirely electronic equipment, in combination with photographic recording, is suited for these purposes.

Nature of Apparatus

The entire set of equipment was designed to work from a 110 volt a-c power supply. Where good voltage regulation cannot be obtained, a voltage stabilizer is employed to furnish constant voltage.

When choosing the equipment for this recording unit it was attempted to utilize standard equipment as far as possible. In many instances apparatus designed for quite a different purpose was adapted, certain changes being made when required. Although the entire set works very satisfactorily, several improvements and simplifications could be made.

Principle of Operation

Measurements of strain, as well as measurements of small motions, such as the compression of a rubber shock absorber, are made by the unbalance of a bridge circuit. The functional arrangement of the bridge network, is shown in its basic form in Fig. 1, the bridge arms being mounted at the seat of the disturbance to be measured. By means of flexible trailing cable the network is connected to the bridge control consisting of power source, detector, and final balancing circuit. In operation, the bridge network is almost completely balanced for the quiescent conditions of the equipment under test. The presence of dynamic variations of this equipment results in an unbalance which may be compensated for by adjustments of the bridge balancing control.

For the measurement of strain, two arms of the bridge are composed of SR-4 bonded metalectric strain gage resistance units.* Since these gages make use of strain sensitive resistance wire, their resistance undergoes variations when the wire is stressed. The remaining two arms are fixed resistors of such resistance as to almost completely balance the bridge. Through the use of such bridge circuits, conduction is metallic throughout, and connections can be soldered, which makes the use of these gages extremely accurate and reliable. Gages with a remarkably low temperature coefficient are available, so that change in ambient temperatures do not affect the readings.

When a small motion, like the compression of a rubber shock absorber is to be measured instead of a strain, a bridge circuit with a sliding contact actuated by the motion being analyzed, is employed in place of the strain gages.

The schematic diagrams of both types of bridge circuits are shown in Fig. 1. The bridge control circuit, which is the same for either form of bridge, is shown at the bottom of of Fig. 1. Connections between the bridge and control circuits are made with a three-conductor cable, encased in a grounded shield which serves as the fourth conductor.

Measuring Strains

The measuring equipment to be used in connection with the strain gages had to be designed for a wide range of frequency—from zero to several hundred cycles per second. As d-c amplifiers with such a frequency response combined with small zero drift are not commercially available, it was decided to use an amplitude modulation scheme with a modulation frequency from 300 to

* See Bulletin 164, Baldwin Southwark Co., Philadelphia.

3000 cps. Gages and dummies are arranged in a Wheatstone bridge and the bridge balance detector is a cathode-ray oscillograph.

The modulation frequency is furnished by a beat frequency oscillator. The 6L6 power stage of a Thordarson T30W08 amplifier is employed to supply the necessary power to the bridge. The output is adjusted for a gage current of about 0.025 ampere. In general, less than one watt is required and this power can be obtained without appreciable distortion.

Usually, two active and two dummy gages make up the bridge. The dummy gages substantially reduce temperature effects, permitting the use of higher sensitivity gages with inherently higher temperature coefficients. The four bridge arms are arranged and almost perfectly balanced near the place of strain measuring. Three leads and a shield establish the connections. Two leads feed the bridge, while one lead and the shield carry the signal. The leads thus do not form integral parts of the bridge arms and difficulties due to distributed capacity are greatly reduced. Since small changes in lead resistance do not affect the signal, plug connections can be used between bridge and control box. The shields are grounded to prevent stray pick-up. Ground is established at one point only, usually near the gages, and ground loops are avoided.

Final balancing is achieved at the control box. Resistance balancing is obtained by a large fixed resistor in shunt with one arm of the bridge and a variable resistor of similar magnitude across the adjoining arm, the common point being ground. To facilitate calibration, a decade box is employed as the variable resistor. A small fixed capacitor across one arm and a variable capacitor across the adjoining arm are provided for the phase balancing. Again ground is the common point of the two capacitors. Double throw switches are used to reverse the fixed and variable resistors and capacitors with respect to the two bridge arms.

Due to the symmetrical arrangement of the bridge and the control unit, the effect of frequency upon the balance setting is relatively small.

If only one strain function is to be recorded, the bridge signal is fed directly into a cathode-ray oscillograph. The amplitude of the resulting wave is proportional to the strain to which the gages are subjected. Linearity is very good throughout the range of measurements. For calibration purposes the resistance offset on the decade box corresponding to a certain strain is computed and the resistance at balance is changed by this amount. At high frequencies the calibration is made by shunting a dummy gage by a large fixed resistor, and computing the corresponding strain. The amplifier gain is then adjusted so that the deflection on the screen assumes the desired value. The calibration deflection is photographed before the test so that the scale on the film can be determined easily.

Direction of Strain

Where distinction between positive and negative strain is required, an initial deflection is produced by a certain resistance offset. An increase in deflection then indicates a strain of one sign and a decrease a strain of opposite sign.

Without special precautions a sensitivity can be obtained whereby a strain of 7×10^{-6} (corresponding to about 200 pounds per square inch stress in steel) causes 0.1 inch deflection on the oscillograph screen. This deflection produces a trace displacement of 0.01 inch on the film and can be detected without magnification. Tests have shown that the accuracy of recording is very high, the errors being one to two percent at the maximum loads.

If two strain functions are to be recorded simultaneously, two identical bridge sets and an electronic switch are employed. This switch connects the signals alternately with the input of the cathode-ray oscillograph. The switching frequency is chosen somewhat below one half of the modulation frequency so that at least one full wave of each strain function is recorded. A modulation frequency of 600 cps and a switching rate of 250 double reversals per second make a very good combination for average strain recordings.

The amplification following the electronic switch is limited by the permissible tailings. Therefore, the bridge signal must be amplified before reaching the electronic switch. For this purpose the second 6J7 stage of the Thordarson T30W08 amplifier is employed. This stage is available in these amplifiers, but not required for feeding the bridge. Besides the separation of the stages, some measures had to be taken to reduce the 60 cps pick-up in the 6J7 stage. The schematic diagram of the amplifier, as modified for our use, is shown in Fig. 2.

In many cases it is desirable to follow the general trends of the strains while records are being taken. For this purpose the modified first 6J7 stage of the Thordarson amplifier is used in connection with a 6H6 rectifier tube and a spotlight galvanometer. This galvanometer has fast response and while it cannot follow the peaks of short dura-

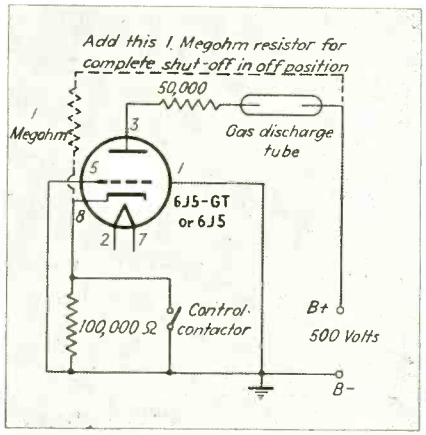


FIG. 4—Electronic relay circuit for control of gas discharge tubes. If several gas tubes are to be controlled, a 6SN7-GT tube may be used to replace two 6J5-GT tubes in the above circuit

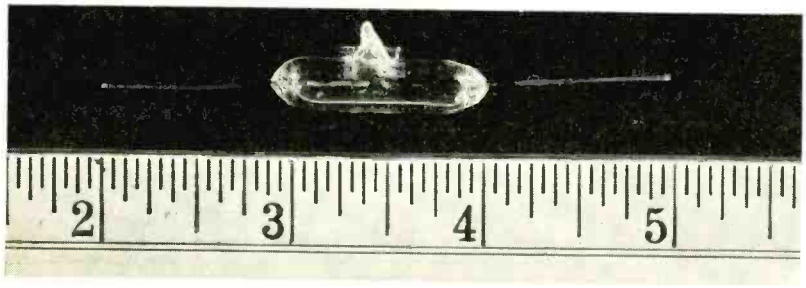


FIG. 3—Photograph of gas discharge tube used in making timing traces

tion strains, it gives the one second average very closely and thus serves as a good indicator. Any irregularity shows up immediately on the galvanometer and hence the danger of failure in test procedure is greatly reduced. Since the first 6J7 stage is used in cascade with the second, enough sensitivity is available on the galvanometer to balance the bridge. This makes it unnecessary to disturb the light shield arrangement for checks on drift.

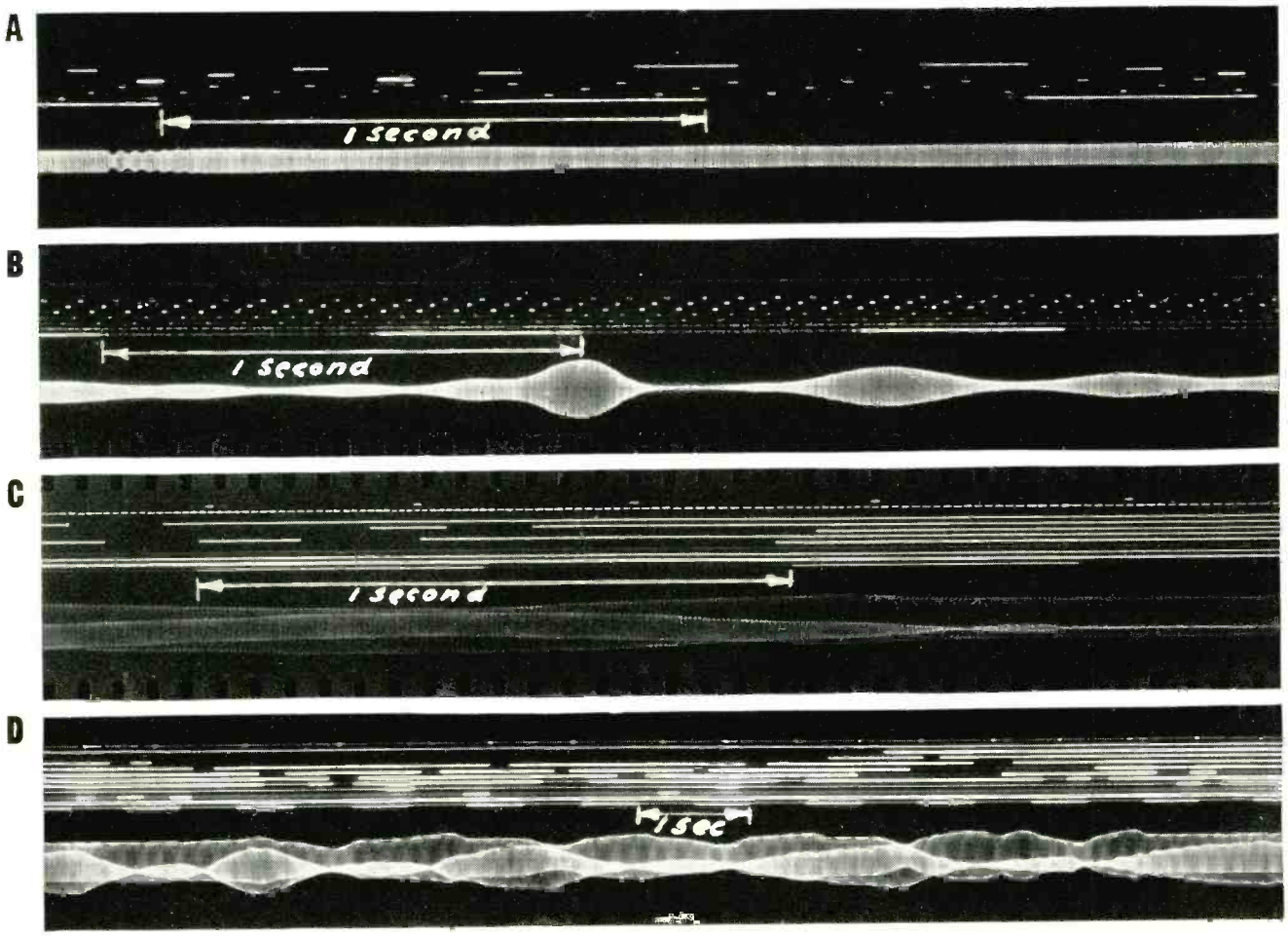
Where static or slowly varying strains are to be observed and a photographic record is not required, the galvanometer can be used to great advantage. The a-c modulation bridge supply is then replaced by some dry cell batteries. The amount of equipment is thus greatly reduced and the entire setup is independent of the 110 volt power supply.

Recording of Timing Functions

Timing functions, such as revolutions or clutch positions, are marked by the light of a special bulb. A very small gas discharge tube, which flashes instantaneously when the voltage is applied, has been developed for this purpose. A photograph of one of these tubes is shown in Fig. 3. Both, argon-mercury and neon tubes proved satisfactory. The argon-mercury type, with blue light, has a somewhat higher actinic value than the neon lamps which emit an orange colored light. Due to difficulties in keeping impurities out of mercury, bulbs containing a small amount of it have a shorter life time than those without it. In general, neon lamps are preferred, inasmuch as highly sensitive film is used anyway. The tubes can be used for well over one hundred flashes per second, thus fulfilling all practical purposes.

The tubes work from a 500 volt d-c power supply which consists of a transformer, two 816 rectifier tubes, a simple filter, and a bleeder. The light flashes are controlled by an electronic relay circuit, schematic diagram for which is shown in Fig. 4. The voltage across the contactor of this cathode bias control circuit is only 30 volts and since the current flowing is less than 10 milliamperes, the arrangement is entirely harmless and contactors stay perfectly clean. In order to ascertain flashing at low temperatures the circuit is such that the lamps maintain a small glow and intensify their emission when con-

FIG. 5—Typical strain and timing records obtained with the equipment described in this article



A Timing function provided by three lamps actuated by contacts, 120 deg. apart on same shaft. Reversal of rotation shown in top record. Vibration of rope after it falls over wrap shown in bottom strain function

B Strain function shows impact on rope due to sudden application of brake while lowering. Timing as above

C Two independent strain functions recorded simultaneously with axes displaced, each trace symmetrical about its axis. Normal film speed. Various timing functions at top

D Two independent strain functions recorded at slow film speed. Various timing function at top

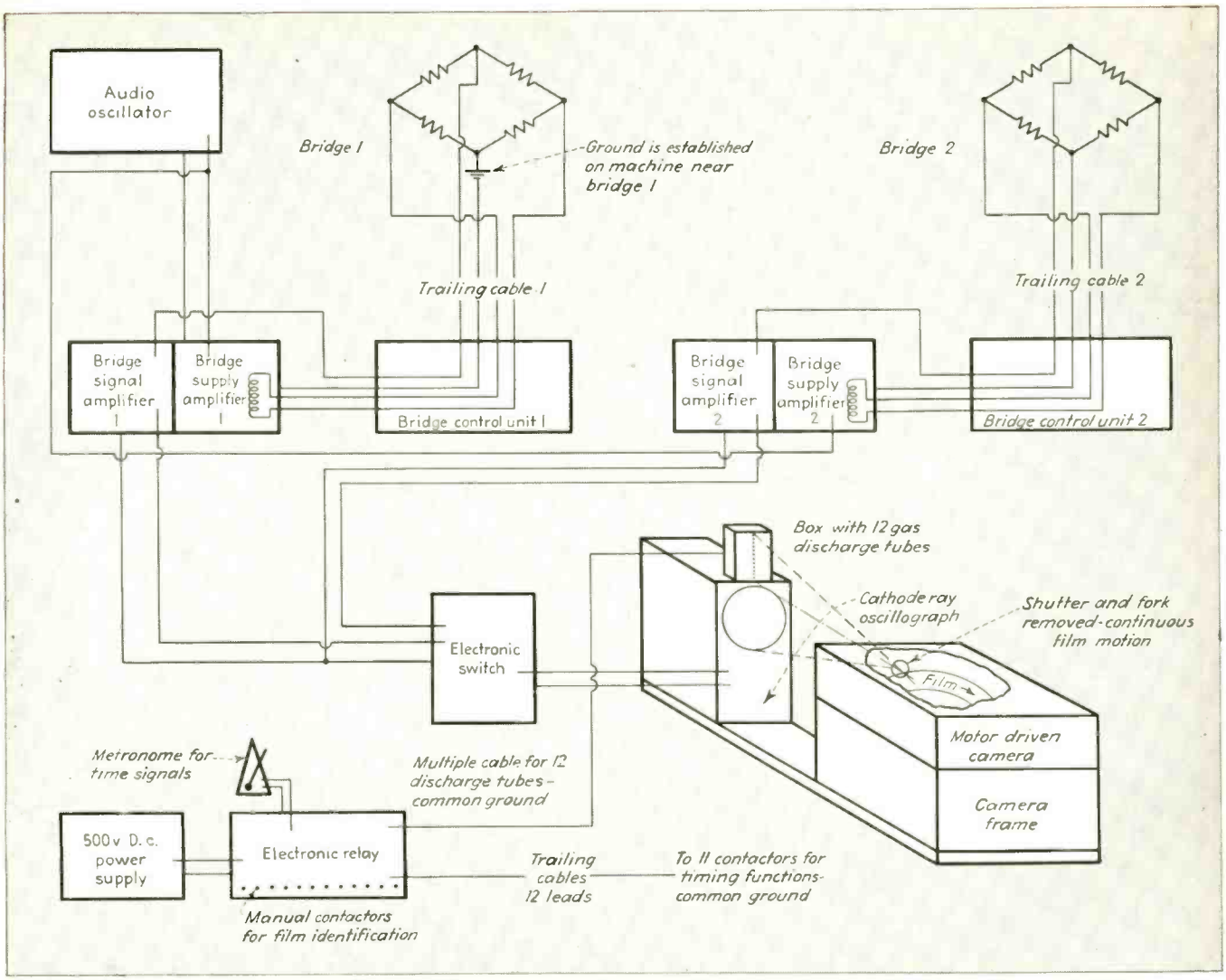


FIG. 6—Block diagram of entire equipment used in making strain and timing analyses of machinery

tact is made. The electronic relay arrangement is also provided with manual contactors so that records can be identified by means of the gas discharge tubes.

Photographing Strain and Timing Functions

For making permanent records of strain and timing functions, the traces of the cathode-ray oscilloscope and the flashes from the timing lamps are recorded simultaneously upon photographic film. The available width of the film is about equally divided between the traces made by the oscilloscope and the traces made by the flashing neon lamps. The images of the two traces due to strain measurements are obtained from alternate traces of the oscilloscope, an electronic switch being used to change from one to the other. The zero lines of the two modulated waves which are obtained in double strain recordings are displaced by only one fifth of the screen width so that even for small amplitudes, the traces from the two functions overlap. However, the two traces are easily identifiable and can be separated from one another since each trace is symmetrical about its zero or reference axis.

Twelve neon lamps of the type already described are arranged in a small box on top of the oscilloscope in such a manner that their traces may be photographed simultaneously with the trace from the oscilloscope. One lamp is used to provide timing marker signals derived from a metronome. The remaining lamps are available for recording as many as eleven various functions, and for identification.

A number of typical strain and timing traces are shown in Fig. 5.

Camera Arrangement

A professional 35-mm camera of 400 ft. film capacity is used for the recording. The shutter was removed and the driving mechanism was arranged for continuous film propelling. The camera is driven by a governor controlled variable speed motor. Usually a film speed of six inches per second is considered sufficient for recordings of heavy machinery performance. This results in an effective running time of at least twelve minutes per 400 feet of film. An $f/3.5$ lens stop proved to be of ample strength for these recording purposes. The use of Eastman Super XX film permits photographing with a relatively low intensity on the oscillograph screen which is an important factor in increasing the lifetime of the tube.

Oscillograph and camera are held in relative position by a wooden frame. A tubular shield between the oscillograph and the camera lens keeps out all outside light. Two slides are provided to facilitate ob-

(Continued on page 114)

GRAPHICAL SYMBOLS

Compilation of the graphical symbols most commonly encountered in the electronics field is presented as a war aid in interpreting schematic wiring diagrams. On the following three pages the symbols used differently in the various fields are indicated

A SCHEMATIC wiring diagram may be thought of as the technician's short-hand method of indicating the inter-relationship of the various elements of an electrical device. The various elements are indicated in the diagram by graphical symbols which, through customary use and widespread adoption became more or less standardized. When such individual symbols are properly coordinated in a schematic drawing, the diagram serves either as (1) a condensed, compact set of instructions, indicating the functional operations which must be carried out to construct the electrical device, or (2) as a record of the electrical design of equipment which has already been fabricated. The schematic diagram is somewhat akin to the musical score which indicates the voices of the various instruments, and therewith, the musical functions to be performed by each musician; the score also serves as a record for the composer. The attainment of a satisfactory result is predicated upon the assumption that the symbolic notation employed means the same thing to all concerned. Disastrous consequences may have to be faced if this condition is not fulfilled.

The development of graphical symbols for use in the various branches of electrical technology has progressed, more or less, independently in each field. While the symbols might be well suited for the particular field for which they were advanced, they are sometimes inconsistent with the symbolic notation employed in other branches. Differences in symbols could be tolerated so long as each specialized field of electrical technology was, more or less, an independent unit. The telephone engineer had little contact or interest in the generation and distribution of appreciable amounts of electric power, while the engineer in the power plant was seldom, if ever, concerned with electron tubes or communication equipment. But as each field expanded and drew upon the techniques and practices of adjacent fields, it became evident that the various groups of electrical engineers were speaking different dialects. In a few instances, they might even be said to speak in different languages, for the graphical symbols not only lacked consistency, but sometimes the same symbol was used in different branches to represent completely different circuit elements.

The need for a unified system of graphical symbols has been evident for at least a dozen years, but the technological developments under conditions of war have emphasized the existing differences. The need for uniformity and consistency becomes more acute as the various fields coalesce; it is, perhaps, most urgent in electronics, where the same type of tube may be used in the power, communication, traction, or measurement applications where not only different symbols may be used but in which the philosophy underlying the development of graphical symbols is frequently different. Lack of a unified system of symbols may be quite confusing to the engineer who must recognize that a zig-zag line represents a resistance in the communications field but an inductance in the power field.

On the following pages have been tabulated the graphical symbols most frequently encountered in the science of electronics. The list is presented as reference material to aid in determining the intended meaning of a wiring diagram where conflicting symbols must be faced. The compilation is such that where two or more symbols are commonly encountered as representing the same circuit element, the alternative sketches are indicated. Symbols for electron tubes are fairly well standardized. The only differences normally found are those minor ones indicating the manner in which a grid or filament is drawn. These discrepancies cause no confusion, and could be standardized.

In the preparation of this material, some two dozen associations and organizations most likely to be concerned were asked to indicate the standards they had established or customarily used. Replies indicated that the majority followed the graphical symbols established by the American Standards Association, the American Institute of Electrical Engineers, the Institute of Radio Engineers, and the Radio Manufacturers Association. Certain of the standards on graphical symbols are now undergoing revision and new standards may be available within the next several months. The following standards represent the graphical symbols usually employed in the electrical field:

Graphical Symbols for Electric Power and Wiring:

- American Standards Association,—Z10g2
- American Institute of Electrical Engineers Standard—17g2

Graphical Symbols for Radio

- A. S. A. Standard,—Z10g5
- Institute of Radio Engineers Standard, published in 1941
- A. I. E. E. Standard,—17g5

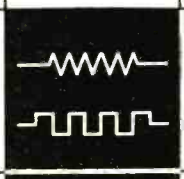
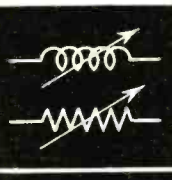
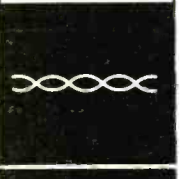
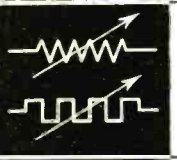
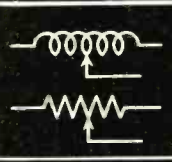
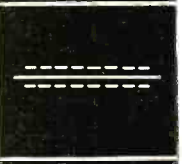
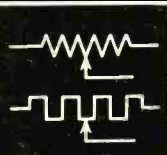
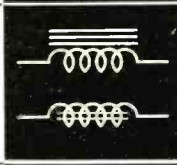
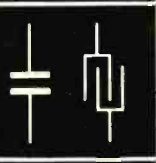
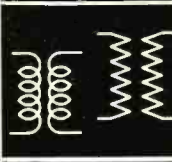
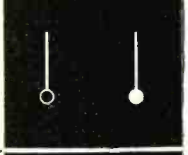
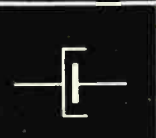
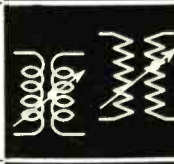
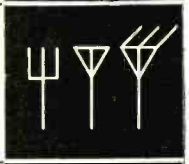
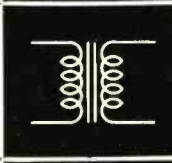
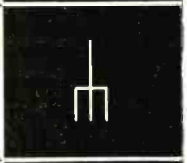
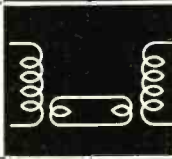
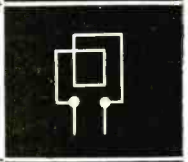
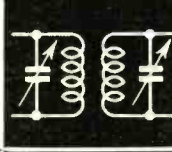
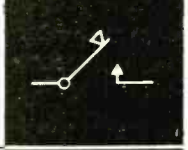
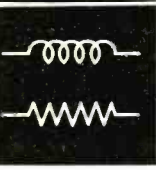
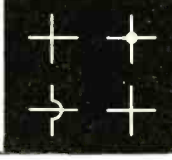
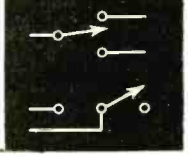
Graphical Symbols for Telephone and Telegraph Use:

- A. S. A. Standard,—Z10g6
- A. I. E. E. Standard,—17g6.

Symbols for electron tubes of the Radio Manufacturers Association.

Symbols for Metering Diagrams, Edison Electric Institute.

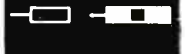
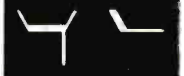
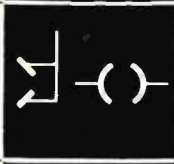
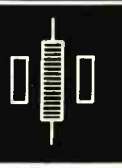
Tabulation of Common Graphical Symbols

Device	Symbol	Device	Symbol	Device	Symbol
Resistor, Fixed*		Inductor or Reactor, Variable*		Twisted Pair	
Resistor, Variable*		Inductor or Reactor, Adjustable (in steps)		Shielded Conductor	
Resistor, Adjustable (in steps)*		Inductor or Reactor, Iron Core		Coaxial Cable	
Rheostat		Inductor or Reactor, Powdered Iron Core		Shielding	
Condenser or Capacitor, Fixed**		Transformer, or Inductors, Coupled; Air Core**		Terminals	
Condenser or Capacitor, Fixed, Shielded		Transformer, or Inductors, Coupled, Air Core, Moving coil indicated**		Antenna	
Condenser or Capacitor, Variable		Transformer, Iron Core		Counterpoise	
Condenser or Capacitor, Variable, with movable plates indicated		Inductors, Link Coupled		Loop Antenna	
Condenser or Capacitor, Variable, Shielded		Tuned Air Core Transformer		Ground	
Condensers or Capacitors, Variable, Ganged		Conductors, or Connecting Wires		Key	
Inductor or Reactor*		Crossed Wires. Top symbol shows wires connected; bottom symbol indicates no connection		Switch, single-pole double throw	

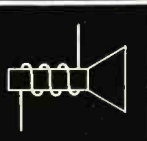
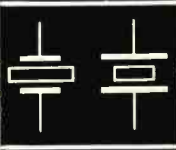
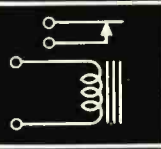
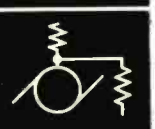
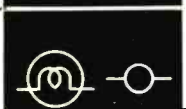
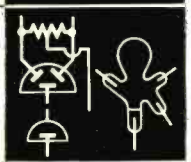
*Upper symbol preferred for radio uses; lower symbol for power applications.

**Symbol at left preferred for radio uses; symbol at right for power applications.

Tabulation of Common Graphical Symbols

Device	Symbol	Device	Symbol	Device	Symbol
Switch, Rotary		Cathode, Photoemissive		Shell, with Contact	
Switch double pole double throw		Cathode, Pool Type		Envelope, Gas Filled	
Jacks		Filament (Thermionic Cathode)		Envelope or Shell, with Shielding indicated by dotted line	
Plug		Grid		Shell or Socket with Alignment Pin Indicated	
Power Switch		Screen Grid		Basing Arrangement for Electron Tubes	
Fuse		Plate or Anode		Cathode Ray Tube	
Dry Cell, or Battery (The positive terminal is represented by the long line)		Plate or Anode		Beam Tube	
A-C Plug for Power Outlet		Target Electrodes		Microphone (Telephone Transmitter)	
A-C Receptacle		Deflecting Plates		Microphone, Single Button Carbon	
Cathode, Thermionic		Beam Forming Electrodes		Microphone, Double Button Carbon	
Cathode, Cold Discharge		Envelope or Shell (General)		Microphone, Ribbon or Velocity	

Tabulation of Common Graphical Symbols

Device	Symbol	Device	Symbol	Device	Symbol
Microphone, Piezoelectric		Frequency Meter		Thermoelement	
Telephone Headset		Power Factor Meter		X-Ray Tube	
Loud Speaker		Watt-Hour Meter		A-C Generator or Motor (Basic Symbol)	
Magnetic Loud Speaker		Graphic Instrument (Basic Symbol)		Induction Motor with Slip Ring Rotor	
Loud Speaker, Permanent Magnet		Synchroscope		Synchronous Generator or Motor with Separately Excited Field	
Loud Speaker, Electrodynamic		Piezoelectric Plate (and mounting)		Synchronous Converter	
Voltmeter		Rectifier Crystal Detector		D-C Generator or Motor (Basic Symbol)	
Galvanometer		Relay (Contact arrangement may be built up as required)		D-C Generator or Motor with Shunt and Series Field	
Ammeter		Lamp		Mercury Arc Rectifier	
Milliammeter		Arc		Delta or Pi Connection	
Wattmeter		Spark Gap (Rotary, Plain, Quenched, from left to right, respectively)		Wye or Tee Connection	
		Phonograph Pick-up			

ROCHELLE SALT CRYSTAL

An outline of experiments leading to the use of a single Rochelle salt crystal, made possible by bonding the surface of the crystal with a thin sheet of gold foil

By RAYMOND W. TIBBETTS

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Cambridge, Massachusetts.

PIERRE CURIE and his distinguished wife, Marie Sklodowska Curie, world famous co-discoverers of radium, contributed much to the science of electronics by their less known discovery of the piezo-electric effect of certain crystalline substances. Among the crystals having this property are quartz, tourmaline, and Rochelle salt. Long ago it was determined that Rochelle salt had many times the piezo-electric effect of any other crystalline material, and many ideas have been presented, and patented, in an effort to efficiently utilize this phenomenon.

Only one manufacturer has thus far succeeded in making commercially available, suitable piezo-electric units. The unit consists of two crystalline plates having foil or graphite electrodes attached on opposite sides, with the plates cemented together in opposition. The unit assembly is supported on suitable elastic pads in such a way that the saddle warping effect, caused by the mutual constraint of the opposing crystals, may be mechanically utilized for acoustic and other devices.

One system using this unit affixes a perpendicular yoke piece to each corner of a substantially square crystal unit, and supports the other two corners by elastic pads. The diaphragm or other actuating device is connected by pin means to the yoke. In another arrangement, three corners of the crystal unit are cemented to rubber pads, and the fourth corner is actuated. In still another system the crystal unit is supported along one edge and a center shaft is connected at the midpoint of the opposite edge. Due to the twisting effect of the unit when so supported a rotary oscillatory motion is imparted to the shaft, which is used to actuate a stylus, mirror, etc.

Several early attempts were made to adapt a single Rochelle salt crystal plate to a piezo-electric device. All of these gave more or less indifferent results, except for very specific applications. Most of the devices used either a whole homogeneous crystal or an assembly of them, in an effort to secure sufficient mechanical amplitude. The displacement amplitude of the crystal per se is very small even under high electrical stress. Plates of quite some thickness have been suggested but in these cases sufficiently low impedance could not be attained.

In attempting to solve these problems the author first developed a gold electrode which in effect gives to the crystal unit assembly a capacitance practically equal to the maximum theoretical capacitance of a condenser having Rochelle salt as the dielectric. This in effect reduces the internal capacitive reactance of the crystal generator to a minimum. The gold electrode is applied directly to the crystal surfaces and is in mechanical and molecular bond therewith.

It was found impractical to deposit gold by the electro-deposit or sputtering methods on Rochelle salt crystals, since the material is water soluble and dissolves in its own water of crystallization at about 132 degrees F.

It was discovered that extremely thin gold foil, in the order of 0.000004 inch thick became bonded to the wet surface of the crystal, when dried and recrystallized. It was also determined that thick gold sheet would not adhere in this manner. A patent has been granted the author for this process and the products made thereby.

Tests showed the capacitance of the gold-electroded crystals to be more than twice that for commercially available crystals of the same dimensions. This was indeed a happy discovery, for the gold deposit pro-

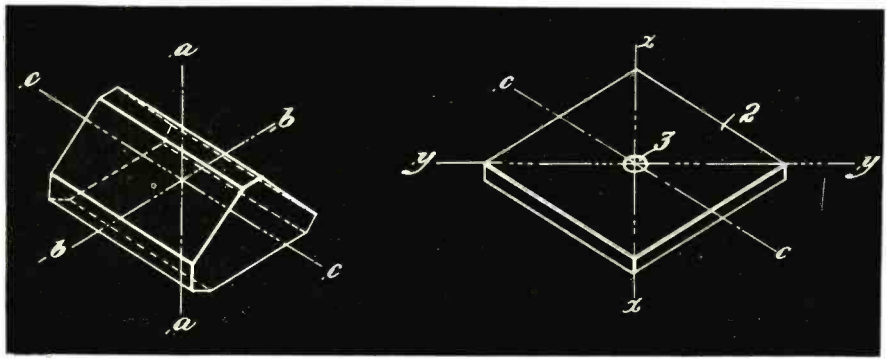


Fig. 1—Longitudinal axis, c-c, electrical axis, *a-a*, mechanical axes, *x-x and y-y*. The hole in the Rochelle salt slab provides for the connecting pin between the two toggles

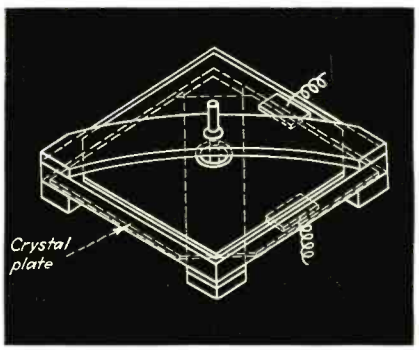
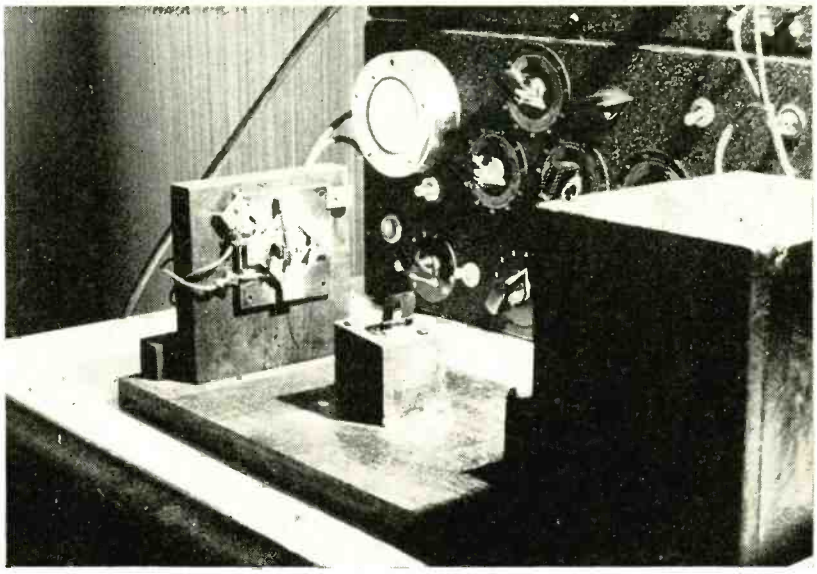


Fig. 2—The complete unit assembly, showing the bow or "toggle" arrangement with connecting pin. The crystal slab has a gold electrode on both surfaces

DEVICES OF LOW IMPEDANCE



The setup using phototube for testing response and waveform of the oscillograph unit

vided an extremely flexible electrode of low specific resistance which was impervious to atmospheric conditions and which was bonded to the surface of the crystal with sufficient adhesion for practically all acoustic applications of Rochelle salt.

The very high capacitance attained has made it possible to make acoustic devices with a relatively low impedance and with a small amount of crystalline material. For example: in one size of the "Monobar" crystal unit adapted for microphones, the single plate used is $20\times20\times\frac{1}{2}$ mm, and has an average capacitance of over 0.007 μf. From the formula $C = 0.0088\,\frac{KA}{d}$, where K is the dielectric constant, A the area in square centimeters and d the thickness of the plate in cm, the value of K will be found to be about 10,000. Capacitance measurements were made at 1000 cps. This high capacity is of extreme importance in a high fidelity acoustic device which must faithfully reproduce very low frequencies or which must have a very long cable.

Means of Utilizing Crystal Deformation

To adapt to best advantage the properties of the gold electroded crystal, a new mechanical system has been developed. This system is based on two general principles: first, the adaptation of bow or spring toggle members as mechanical multiplying devices for the small oscillations of the crystal per se, and second, a frame-like structure within which the crystal slab is cemented, and on the corner portions of which the toggle members are secured.

Since the mechanical axes x-x and y-y of the crystal plate form a 45-deg. angle with the longitudinal axes c-c of the mother crystal, as shown in Fig. 1, the oscillations of the crystal and frame cause a simultaneous bending of the opposed toggles, as these may be secured on opposite sides of the frame and oriented at 90 deg. to each other. This is due to the fact that the crystal under electrical stress contracts along one diagonal and simultaneously expands along the other diagonal. It will be seen therefore that when the two bows or toggles are interconnected by a pin member, a greatly enlarged version of the crystal and frame oscillations will be obtained. The converse is of course also true—when the pin is mechanically actuated, a greatly increased force with a reduced amplitude will be transmitted to the frame and crystal member. A much greater electrostatic potential will be obtained from the crystal devices than from the crystal itself if actuated by the original force applied to the pin.

Many arrangements and combinations are possible with this new development. For example, when it is desirable to secure a very low impedance or large mechanical output as would be necessary for a loud speaker or a direct-writing pen oscil-

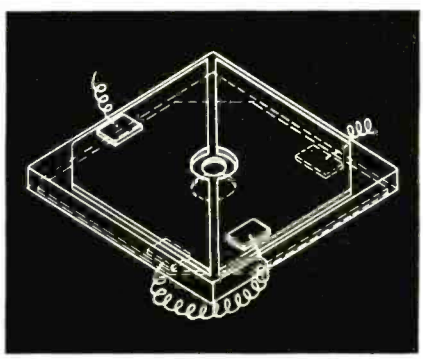


Fig. 3—Arrangement of the electrodes for greater voltage output. Two electrodes are provided on each side of the crystal plate and leads are connected in series

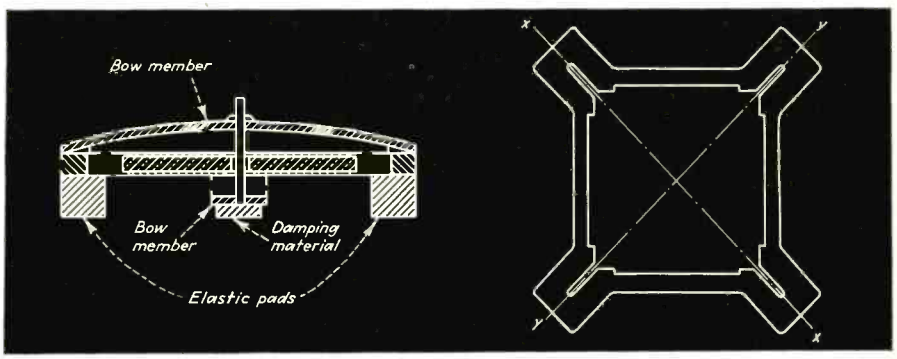
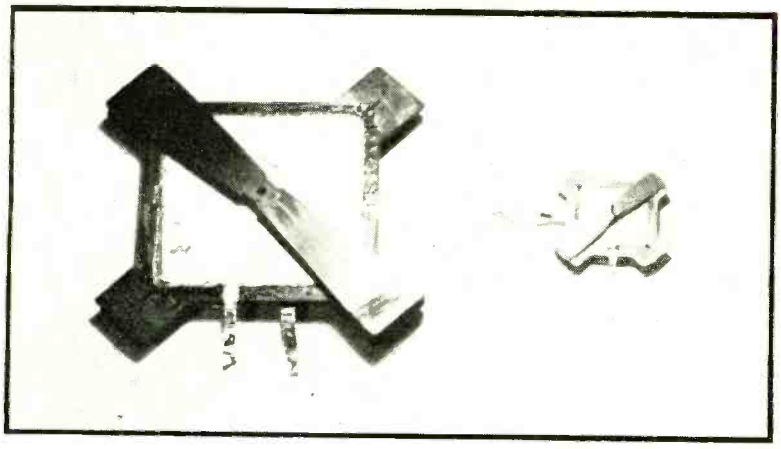


Fig. 4—Cross-sectional view of the framed type of Monobar unit, and a plan view of the frame. The bow members are cemented to the wing portions of the frame



The small unit has a 20 mm x 20 mm crystal suitable for most microphone applications, such as earphones, etc. The large unit has a 57 mm x 57 mm crystal and is particularly suitable for low-frequency devices where low impedance and high power are necessary considerations

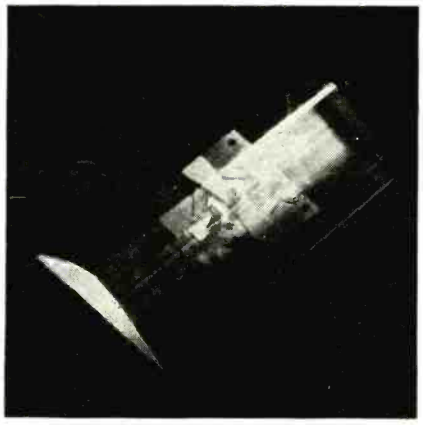
lograph, multiple crystal plates may be assembled within the frame structure with their major surfaces parallel, with the leads so connected that all the plates act in unison and in the same directions.

Perhaps one of the most important features is the frame member, which by virtue of its shape and nature adapts itself to the mechanical displacements of the crystal. Under electrical stress the crystal tends to become diamond shaped, to which the frame conforms. By virtue of the frame assembly it is almost impossible to break the crystal, either by mechanical or by electrical shock. So rugged is the unit that a very sensitive microphone or ear piece may be thrown on the floor without in any way damaging the crystal unit. Voltages up to the limit of the dielectric strength of the crystal material have been applied without harm. This lies in the fact that the bows or toggles do the bending while the frame supports the crystal.

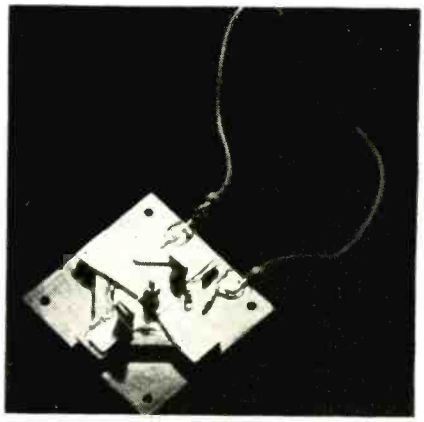
One of the outstanding important characteristics of the Monobar type of piezo unit is the fact that cathode-ray oscillograph studies indicate the remarkable freedom from harmonic distortion on sine wave input enjoyed by Monobar microphones. While this type of distortion has not been emphasized very much, most of the emphasis being given to frequency distortion, it is recognized that harmonic distortion undoubtedly plays a most significant part in the thing we call "quality" in acoustic equipment.

It seems to the writer that there are now greater possibilities for the crystal loud speaker, especially for small, portable radio sets. Already a very satisfactory 5-inch speaker has been developed which uses no critical war materials for its fabrication. The crystal unit weighs less than one ounce, a very desirable feature for portable radios and possibly for certain war communication equipment. To date the power capabilities of the speaker, over one watt, do not equal the dynamic type. It is expected, however, that this will be increased appreciably.

The crystal speaker should make it possible to eliminate the output transformer, using instead resistance capacity coupling. There will be some loss of course, but this should not be a serious matter in those cases requiring extreme lightness and compactness. The development of a power tube having the proper output characteristics would help greatly in this matter.



Composite photo of Rochelle salt crystal and the Monobar ocillograph unit



The Monobar unit as used in an oscillograph. Size is 2⅛ by 2⅛ by ⅝ inches

The new unit is adaptable to practically all conventional acoustic equipment in which Rochelle salt crystals are used and apparatus of a special nature in which the frequency characteristics must conform to certain specifications. By varying the toggle structure and the crystal capacity together with resonant cavities of specified structure, almost any required response may be had.

Standard Monobar microphones use the bow and frame unit and are highly damped. This damping cuts down the output voltage but provides a straight-line response and eliminates most of the handling noise. Microphones for special purposes such as hearing aid units may have an output of about −36 db. These are damped only by the cartridge chamber itself.

Where it is necessary to obtain maximum output, the crystal is multiple-electroded and connected in series. This is accomplished simply by dividing the single plate electrodes and connecting the alternate opposed electrodes in series. By this method a gain of about 6 db can be obtained without phase shift or harmonic distortion, since the single crystal is the only element involved and the distribution of mechanical and electrical forces is uniform through its mass.

The very high capacity of the crystal makes possible a rising characteristic toward the low end of the spectrum, and by using more flexible toggle elements the highs are greatly attenuated while the output of the low frequencies is actually increased.

(*Continued on page* 116)

Adjustment of DIRECTIONAL ANTENNAS

A method of measuring resistance and reactance values at radio frequencies with an ordinary 3-inch cathode-ray oscilloscope while full power is being fed to the broadcast antenna. Width and height measurements of an elliptical pattern give the required constants

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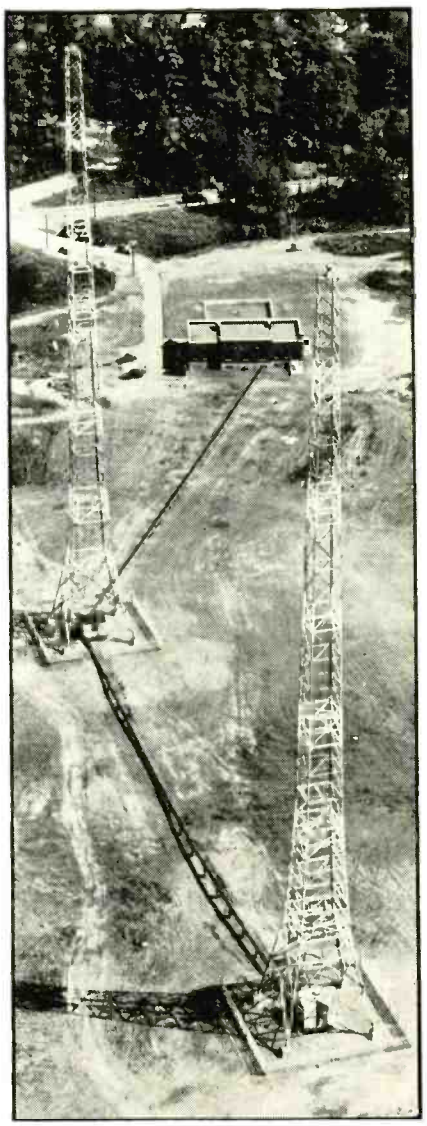

This two-tower directional antenna system of station WEAF in Port Washington, Long Island has been adjusted by the cathode-ray method described in this article. Two oscilloscopes were used, one in each under-the-tower tuning house

IN the alignment of directional antennas there arise two types of problems. The first is that of securing the proper phase relations and amplitude relations between the various antenna currents. The second is that of tuning each antenna to match its transmission line, so no standing waves exist on the line.

The methods of arriving at proper phasing and current ratios are as varied as the number of engineers engaged in tuning directional antennas. It is not proposed to discuss this subject here, but instead to deal with the second part of the problem. Specifically, this involves determining the resistance and reactance which each transmission line sees at its antenna. The engineer wants to know if the line is "working" into too high or too low resistance, how much reactance is present and whether this reactance is inductive or capacitive.

In some cases, particularly with antennas less than about 120 degrees high, it is possible to calculate the line termination networks with reasonable accuracy by a combination of ordinary measurements and proper application of circuit theory. With high antennas having distorted current distribution, or with a combination of high and low antennas, accurate calculations are not possible. It has heretofore been necessary in these cases to obtain final circuit adjustment by what almost becomes a trial and error method.

It must be noted that it is impossible to measure, by normal methods, the impedance of an antenna as a working part of a directional system. The measurement must necessarily be made without disturbing the system, under the condition of partial or full power. It is in this manner that the cathode-ray tube measurements to be described are made.

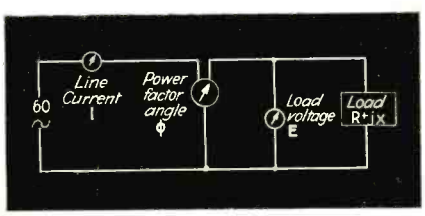

FIG. 1—Standard method of measuring the resistance and reactance of a load at power frequencies, using ordinary meters

Method Used in 60-cycle Circuits

In 60-cycle single-phase power circuits the load impedance can be found with meters measuring volts, amperes and power factor, connected as shown in Fig. 1. In brief, one current flowing in the power factor meter is proportional to the phase and magnitude of the load current, and the other current is proportional to the phase and magnitude of the load voltage. The resultant action of the fields of these two currents upon a vane produces a displacement of the vane. A pointer attached to the vane indicates directly the phase angle between load current and voltage.

With E, I and the phase angle ϕ known, the resistance R and X are obtained from the following basic formulas:

$$R = \frac{E}{I}\cos\phi \qquad X = \frac{E}{I}\sin\phi$$

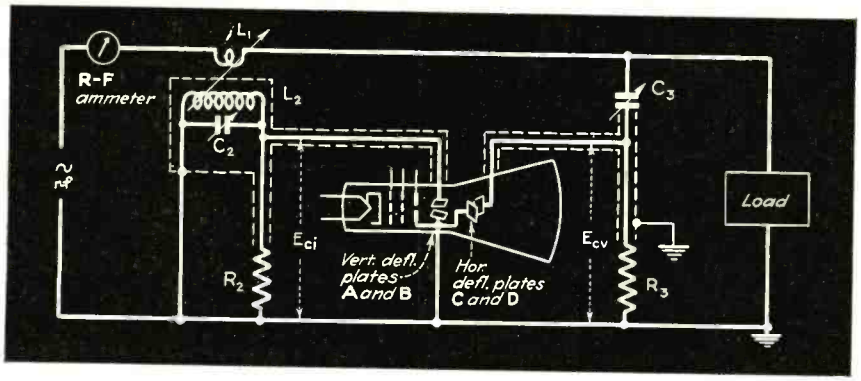

FIG. 2—Circuit for measuring the resistance and reactance of a load at radio frequencies under operating conditions. The cathode-ray tube may be part of an ordinary three-inch cathode-ray oscilloscope

Cathode-ray Tube Method

In the r-f version of the procedure for determining load impedance, a cathode-ray tube is substituted for the voltmeter, ammeter, and power factor meter, as shown in Fig. 2. In this case it is simpler to use voltages instead of currents. A cathode-ray tube with electrostatic deflecting plates is chosen. A voltage proportional to the amplitude and phase of the load voltage is taken from voltage divider C_3R_3 and applied to horizontal deflecting plates C and D. A voltage proportional to the amplitude and phase of the line current is secured from a well-shielded transformer L_1L_2 and applied to vertical deflecting plates A and B.

Initially, the voltages applied to the two sets of deflecting plates are adjusted so that when the load is a pure resistance of known value the pattern on the tube is a circle of convenient size. Any other load then gives an ellipse, the orientation and dimensions of which permit calculation of the load constants.

Condenser C_3 permits reducing the r-f voltage applied to the horizontal deflecting plates, and at the same time serves with R_3 to provide approximately 90-deg. phase shift. The voltage due to line current is adjusted by varying the coupling between the primary and secondary of the transformer. It has been found in practice that no coil is necessary in the primary, since sufficient deflection generally can be obtained by coupling to the bus feeding the terminating equipment.

Analysis of Circuit Relations

It can be shown that when secondary circuit L_2C_2 is tuned to resonance, the following relation based on the simplified equivalent circuit in Fig. 3 will provide a sufficiently close approximation to actual conditions:

$$E_{ci} = E'_{ci} = -jI_2X_2 = I_0X_{12}X'_2/R_1 \quad (1)$$

Here E_{ci} is the voltage on the cathode-ray tube due to the load current I_0. This means the cathode-ray tube voltage E_{ci} is in phase with the load current.

The load voltage part of the circuit is as shown in Fig. 4. In this case,

$$E_{cv} = E_0R_3\left[\frac{R_3}{R^2_3 + X^2_c} + j\frac{X_c}{R^2_3 + X^2_c}\right] = E_0R_3K\angle\theta \quad (2)$$

where E_{cv} is the voltage on the cathode-ray tube due to the load voltage, and

$$\theta = \tan^{-1}(X_c/R_3)$$

In Fig. 5 is a vector representation of the cathode-ray tube voltages resulting from the load current and load voltage when the load is a pure resistance. A circular pattern is obtained on the cathode-ray tube screen when capacity C_2 in Fig. 2 is adjusted until voltage vector E_{ci} takes the position designated as E''_{ci}. This adjustment is necessary for calibration because E_{cv} is not fully 90 deg. ahead of load voltage E_0 (R_3C_3 does not provide a full 90-deg. shift in phase). Adjusting C_2 makes the vertical deflecting plate voltage E''_{ci} lag E_{cv} by 90 deg., and adjusting the coupling between L_1 and L_2 makes these voltages equal.

Analysis of The Cathode-ray Pattern

It is well known that if equal voltages 90 deg. out of phase are applied to a cathode-ray tube the pattern will be a circle. If the voltages are unequal but 90 deg. out of phase the pattern will be an ellipse with its major axis on either the x or y axis, depending upon which set of deflection plates has the larger voltage. If the phasing is other than 90 deg., the major axis of the ellipse will assume an intermediate position somewhere between 0 and 90 deg. with respect to the x axis.

An example of a general pattern is shown in Fig. 6. It is obtained with voltage E_{ci} (that due to the current) acting on the vertical deflecting plates, and voltage E_{cv} (that due to the load voltage) acting on the horizontal deflecting plates, as is shown in Fig. 2. The center of the ellipse is at 0. The ellipse intercepts the x axis at points separated by distance A_1. The total deflection along the x axis is A and the total deflection along the y axis is B. It can be shown that when this pattern is obtained from a given load under the operating conditions described above, the impedance of the load is

$$Z = \frac{R\,A_1}{B} \pm j\,R\frac{A}{B}\sqrt{1 - \left(\frac{A_1}{B}\right)^2} \quad (3)$$

Here, R is the load resistance which gives a circular pattern. The first term of this equation is the resistance of the load under operating conditions, and the second term is similarly the reactance of the load.

It will be noted that the reactive term has a plus or minus sign. If the cathode-ray tube connections are

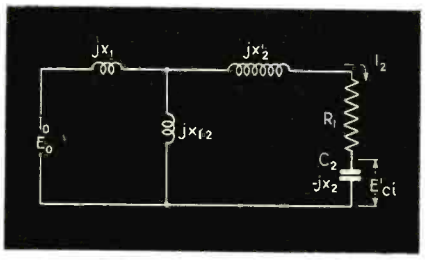

FIG. 3—Equivalent circuit for the current section of the cathode-ray measuring circuit. The voltage drop across the condenser depends on the load current value

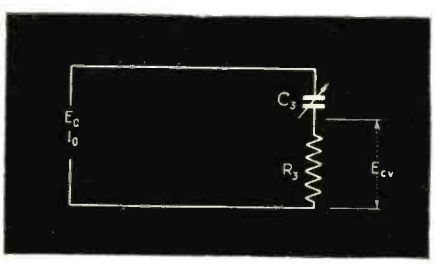

FIG. 4—Equivalent circuit for voltage section is identical to the actual circuit since it is simply an r-f voltage divider connected across the load

so made that with a capacitive load the major axis of the ellipse is in the first and third quadrants, the sign of the reactive term is negative. It will be assumed that this is the case in the following examples. It will also be assumed that R is equal to 75 ohms. Patterns for four different types of loads, with resulting resistance and reactance values based on these assumptions, appear in Fig. 7.

The Practical Application

In a normal application the tuning equipment which matches an antenna to its transmission line corresponds to the load shown in Fig. 2. The simplest method of adjusting L_2C_2 and C_3 involves starting with any one antenna and tuning its matching equipment so that it presents a resistive load R of the correct value for proper termination of the transmission line. This antenna only is then fed from the transmitter with approximately the same power it will carry when it is a part of the directional system. The condenser C_3 is now varied until about half of full-scale deflection is obtained on the screen of the cathode-ray tube. Next, C_2 is adjusted so that the major axis of the ellipse is along either the x or y axis, depending upon the relative voltages. Finally, the coupling between L_1 and L_2 is adjusted so that a circular pattern is obtained. This constitutes the calibration of the equipment. If similar equipment is used at all the radiators, the same procedure is followed at each.

All radiators are now fed together, and the three measurements indicated in Fig. 6 are made on the elliptical pattern of each antenna. From this data, the resistance and reactance of each antenna are calculated as previously explained.

Coil L_2 should be well shielded electrostatically, so it is excited only by the intended field due to line current. Likewise, C_3 and its associated connections should not be subject to extraneous electrostatic fields. In order to assure this result, it is preferable to use coaxial leads for all connections shown with shielding in Fig. 2.

Resistors R_2 and R_3 in Fig. 2 are of arbitrary value. When these resistors are 200 ohms each, the power consumed by the measuring equipment is of the order of 25 watts. This is ordinarily low enough so that the equipment may be removed without any noticeable effect on the directional system. The values of R_2 and R_3 may be increased considerably in order to reduce power consumption.

Some types of cathode-ray oscilloscopes may have to be modified by the installation of r-f jacks on the sides of the unit, to permit short leads directly to the deflecting plates (internal amplifiers in the oscilloscope are not used.) Special provisions may also have to be made for the spot-centering voltages.

Where a cross-ruled scale is not provided with the oscilloscope, transparent graph paper will prove satisfactory and may be fastened to the face of the tube. This permits reading dimensional values directly without a ruler; units of measurement are unimportant so long as all three values are in the same units.

The true r-f power being fed to the antenna or load may readily be determined in this cathode-ray method if an r-f ammeter is inserted in the circuit, as shown in Fig. 2. Multiplying the resistive component of the load impedance by the square of the current reading gives the power.

In this application the degree of accuracy required is not very great. Consequently, such sources of inaccuracy as non-linear deflection or observational errors in reading the values of A, A_1 and B are not of a serious magnitude. A three-inch tube has been found to be satisfactory, but it is entirely feasible to obtain greater accuracy if needed.

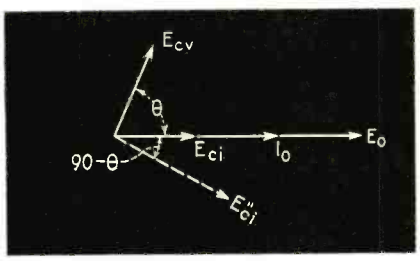

FIG. 5—The circular pattern required for calibration is obtained by detuning L_2-C_2 until the deflecting plate voltages are equal and 90 degrees out of phase

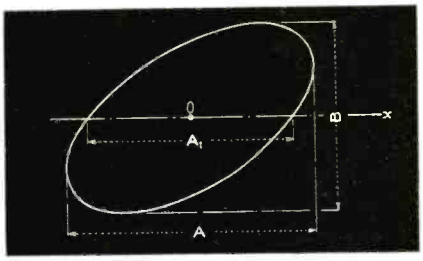

FIG. 6—Typical pattern. Resistance and reactance values are found by measuring lengths A, A_1 and B and substituting the results in equation 3

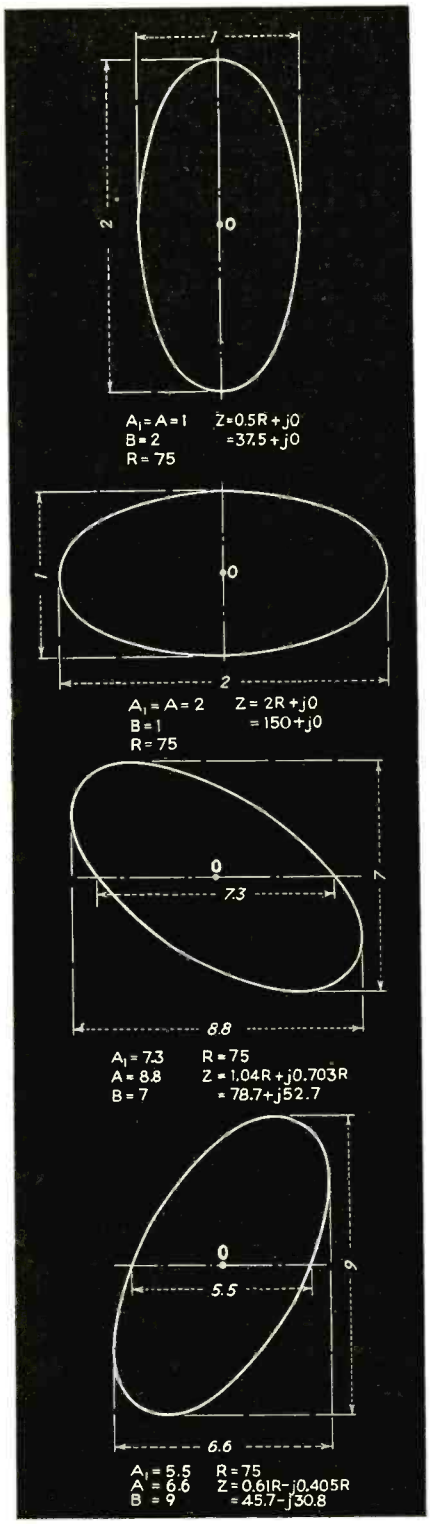

FIG. 7—Examples of cathode-ray patterns and corresponding r-f impedance values

Analysis of

FULL WAVE RECTIFIER

An engineering analysis of the behavior of the full wave, single phase rectifier with choke input is given, together with means of determining critical inductance permitting continuous flow of current. Measurements confirm accuracy of theoretical procedure

THE single phase full-wave rectifier, in which is used the so-called "choke input" type of filter, has become popular since the introduction of small capacity mercury vapor tubes. Despite its wide use today, the design is still based to a great extent upon experimental methods. A more exact analysis of the performance of this type of circuit, which is not so tedious as to discourage its use, should help in the understanding of its applications, and permit its characteristics to be more accurately predetermined. Principle emphasis has been placed on the derivation and discussion of the equation for the filter input current, from which expressions for the d-c voltage and current output are determined under two general types of operation. A simple but accurate expression for the critical choke inductance is also presented.

The specific type of circuit treated in this analysis is shown in Fig. 1. Two basically different types of operation of this circuit may occur. One, where the current through the inductance is continuous, termed "non-cut-off operation", and the other, where the current through the inductance is zero during a period in each half cycle, termed "cut-off operation".

To keep the solution in as simple and usable form as possible certain basic assumptions are made. These are: (1) The circuit parameters are assumed constant and independent of current magnitude. (2) The winding resistance and leakage reactance of the input transformer are assumed to be negligibly small. (3) The anode-to-cathode voltage drop in the rectifier tube is considered to be constant during the current conduction period. (4) Steady state operation of the rectifier unit is assumed.

The circuit parameters are actually constant with the exception of the inductance of the (iron core) filter choke. This inductance is a function of the current which the choke carries. However, for non-cut-off operation in which the load current is not too small (greater than 25 percent of full load) the inductance of the filter smoothing choke may be considered constant without serious error. For cut-off operation, only those filters which use air-core inductors are capable of simple solution. Analytical treatment of this circuit, on the supposition that the choke inductance is a function of the current, presents a problem whose solution is extremely complicated.

The other assumptions are those which may be made in low power rectifier circuits without serious error.

The following symbols are used throughout the paper.

E_m = Peak value of one half the transformer secondary voltage
E_s = Tube voltage drop during conduction (assumed constant)
e = Instantaneous voltage across input to filter
i_1 = Instantaneous current through filter choke
R_1 = Resistance of filter choke
R_2 = Equivalent load resistance
L = Inductance of filter choke
C = Capacitance of filter condenser
E_{dc} = d-c value of output voltage
I_{dc} = average value of load current
T = complete period of rectifier operation = $1/2f$
f = frequency of a-c supply
$p = d/dt$ = differential operator
$Y \angle \mu$ = vector value of admittance of the filter (and load) looking into its input terminals

TABLE I—CIRCUIT PARAMETERS REQUIRED FOR CRITICAL CUT-OFF OPERATION

No.	Peak Voltage	Voltage Drop Across Tube	Capacitance of Filter	Load Resistance	Critical Inductance
	E_m (Volts)	E_s (Volts)	C (Microfarads)	$R_1 + R_2$ (Ohms)	L_c (Henries)
1	368	13	4.0	11,000	10.5
2	281	13	8.0	11,000	11.0
3	141	13	12.0	9,900	12.0

TABLE II—PERCENT DEVIATION OF ACTUAL CRITICAL INDUCTANCE FROM VALUES CALCULATED BY VARIOUS METHODS

No.	THEORETICAL VALUE OF CRITICAL INDUCTANCE CALCULATED FROM: Eq. (9)	Eq. (9a)	$L_c = R_i/1130$*	$L_c = R_i/1000$†
1	+ 2.0	+4.75	− 7.1	+ 4.8
2	− 3.6	+2.72	−11.4	0.0
3	−11.7	−6.25	−26.7	−17.5

* Dellenbaugh and Quimby, Smoothing Chokes, *QST*, 1932.
† Terman, "Radio Engineering," McGraw-Hill Book Co.

By L. C. TILLOTSON*
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With Choke Input

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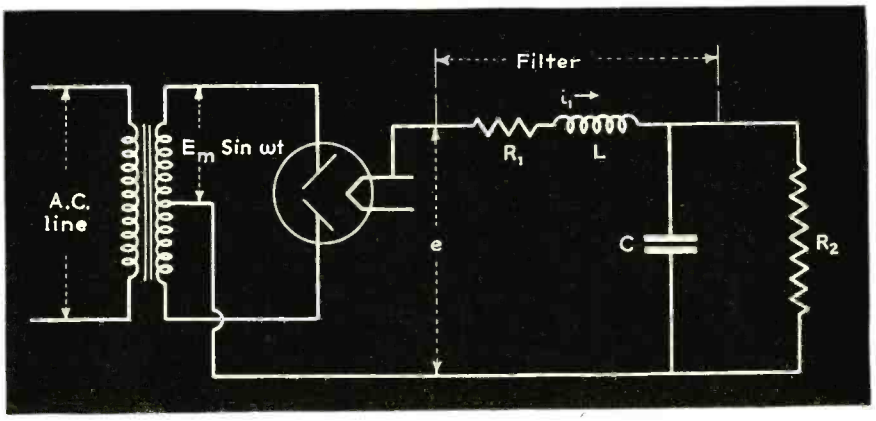

Fig. 1—Schematic wiring diagram of single phase, full wave rectifier circuit with simple choke input filter, and load resistance, R_2

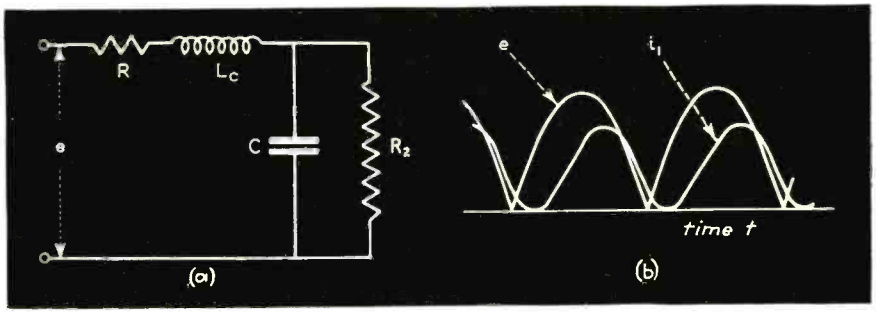

Fig. 2—Equivalent circuit of rectifier filter and load (a), with the resulting voltage and current waveforms (b). The flow of current can be made continuous if the inductance of the choke equals or exceeds the critical value, L_c. Means of calculating the critical inductance are given in the article

General Solution of Current Equation

Considering the circuit of Fig. 1, the current through the choke may be expressed as

$$i_1 = e/Z(p) \qquad (1)$$

where $Z(p)$ is the generalized impedances of the filter and load, looking into the filter input terminals. Thus

$$Z(p) = R_1 + Lp + \frac{R_2/Cp}{R_2 + (1/Cp)} \qquad (2)$$

During the period when the upper half of the tube is conducting, the instantaneous voltage across the filter input is

$$e = E_m \sin \omega t - E_o \qquad (3)$$

Substituting the values of e and $Z(p)$ into Eq. (1) results in a differential equation, the solution of which (see Appendix I) can be expressed in the form

$$i_1 = YE_m \sin(\omega t + \mu) + \epsilon^{-\alpha t}[A_o \cos \psi t + C_o \sin \psi t] + I_c \qquad (4)$$

where

$$Y = \left[\frac{1+R_2^2C^2\omega^2}{(R_1+R_2-R_2LC\omega^2)^2+(R_1R_2C+L)^2\omega^2}\right];$$

$$\mu = \left\{\tan^{-1}(R_2C\omega) - \tan^{-1}\left(\frac{R_1R_2C\omega + L\omega}{R_1+R_2-R_2LC\omega^2}\right)\right\};$$

$$\psi = \sqrt{\beta - \alpha^2} \quad ; \quad \beta = \frac{R_1+R_2}{LCR_2}$$

$$\alpha = \frac{R_1R_2 + L}{2LCR_2} \quad ; \quad I_c = \frac{-E_o}{R_1 + R_2}$$

In this expression A_o and C_o are arbitrary constants which must be evaluated from a knowledge of the circuit behaviour. If θ_1 is defined as the time angle at which current conduction starts at one anode, and θ_2 as the time angle at which it ceases, then Eq. (4) is valid only within this period. Where non cut-off operation occurs, $\theta_1 = 0$, and $\theta_2 = \pi$.

Since the rectifier is a full-wave type, a complete period of its operation, T, is half a line voltage cycle.

DC Value of Load Current

The d-c component of the load current is equal to the average value of the current, i_1, through the filter inductance, and may be expressed as

$$I_{dc} = 2f \int_{\theta_1/\omega}^{\theta_2/\omega} i_1 dt$$

Substituting for i_1 and integrating gives

$$I_{dc} = \frac{YE_m}{\pi}\left[A_1 - A_2\right] + \frac{2fC_o}{\alpha^2+\psi^2}\left[S_1(\alpha B_1 + \psi C_1) - S_2(\alpha B_2 + \psi C_2)\right] + \frac{I_c}{\pi}(\theta_2 - \theta_1) + \frac{2fA_o}{\alpha^2+\psi^2}\left[S_2(\psi B_2 - \alpha C_2) + S_1(\alpha C_1 - \psi B_1)\right] \qquad (5)$$

where

$$A_1 = \cos(\theta_1 + \mu) \qquad A_2 = \cos(\theta_2 + \mu)$$
$$S_1 = \epsilon^{-\alpha\theta_1/\omega} \qquad S_2 = \epsilon^{-\alpha\theta_2/\omega}$$
$$B_1 = \sin\psi\,\frac{\theta_1}{\omega} \qquad B_2 = \sin\psi\,\frac{\theta_2}{\omega}$$
$$C_1 = \cos\psi\,\frac{\theta_1}{\omega} \qquad C_2 = \cos\psi\,\frac{\theta_2}{\omega}$$

The d-c value of the voltage is of course the product of the d-c current and load resistance R_2.

Harmonic Content of Output Voltage

The filter is inserted between the rectifier and the load to smooth out the pulsations in the output voltage and current. The degree to which it accomplishes this objective is a measure of the filter's excellence. To determine ripple content it is necessary to first calculate the harmonic components of the choke current. The current i_1 can be expressed as a

TABLE III—CORRELATION BETWEEN CALCULATED AND EXPERIMENTAL BEHAVIOR OF FULL WAVE RECTIFIER*

Circuit Factor	Calculated Value	Experimentally Observed Value	Deviation in Percent
Output voltage, E_{dc}	178 volts	182 volts	2.3
Load current, I_{dc}	0.248 amp.	0.250 amp.	2.0
120 cps component of i_1	0.0174 amp.	0.0176 amp.	1.2
240 cps component of i_1	0.00212 amp.	0.00218 amp.	2.8
Percent of 120 cps component of output voltage	3.96	3.91	1.3
Percent of 240 cps component of output voltage	0.26	0.28	7.1

* Tabulation determined for the following conditions: $E_m = 324$ volts; $E_o = 12.7$ volts; $L = 8.24$ henries; $C = 4.23$ μf; $R = 53$ ohms; $R_2 = 728$ ohms; and $\omega = 2\pi f = 377$ radians

Fourier series involving a d-c component, and cosine and sine terms of the harmonic components, the coefficients of these terms for the nth harmonic being evaluated from the expressions

$$I_n = 4f \int_{\theta_1/\omega}^{\theta_2/\omega} i_1 \cos 2n\,\omega t\, dt \qquad (6)$$

$$I_n' = 4f \int_{\theta_1/\omega}^{\theta_2/\omega} i_1 \sin 2n\,\omega t\, dt \qquad (7)$$

The resulting equations for I_n and I'_n are given in Appendix II. Expressed in literal form, these equations seem rather long and involved. However, using numerical values, their evaluation is not especially tedious. The amplitude of the nth harmonic of the output voltage across the load can be calculated from the equation

$$E_n = Z_n \sqrt{I_n^2 + I'^2_n} \qquad (8)$$

where Z_n is the combined impedance of R_2 and C_2 in parallel for the nth harmonic.

Critical Inductance

Whether the current through the choke flows continuously or intermittently depends primarily upon the relative values of the choke inductance L, the capacitance C, and the load resistance R_2. The limiting value of the inductance above which cut-off does not occur is defined here as the critical inductance and symbolized by the term L_c.

When the inductance of the circuit shown in Fig. 2a has been adjusted to its critical value, the current through the choke has a waveform corresponding to the curve marked i_1 in Fig. 2b. The minimum value of the current just reaches zero, characterising the border line condition between cut-off and non-cut-off operation. If it be assumed that this current is comprised of only a d-c and a second harmonic component, and that R_1 and R_2, in comparison to the filter circuit reactance, have negligible effect in determining the magnitude of the second harmonic then the value of the critical inductance can be expressed as

$$L_c = \frac{1}{\omega}\left[\frac{2(R_1 + R_2)}{3K} + \frac{1}{4C\omega}\right] \qquad (9)$$

where $K = \left[2 - \frac{\pi E_o}{E_m}\right]$

L_c is the minimum value of the choke inductance which, for given values of R_1, R_2, C, and E_o/E_m will cause the current flow through the choke to be continuous. For values of L less than this value the current flow is intermittent. The derivation of the above equation is given in Appendix III.

Neglecting the higher harmonic components of current in arriving at Eq. (9) leads to only small error in final result.[1] For practical filter circuits the critical value of inductance is considerably on the inductive side of resonance (X_L is at least 10 times X_c). Consequently components of current higher than the second harmonic are of relatively small magnitude. Furthermore, the ratio of $2L_c\omega/R_1$ equals 30 or more, and at the critical point the ratio of $2R_2C\omega$ is about 20. Therefore little error is made in considering reactances only in evaluating the second harmonic component.

[1] If the effect of the fourth harmonic along with the second is considered Eq. (9) becomes

$$L_c = \frac{1}{\omega}\left[\frac{0.711\,(R_1 + R_2)}{K} + \frac{1}{4C\omega}\right] \qquad (9a)$$

To indicate the percentage error likely to incur in the use of Eq. (9) and (9a), experimental results on several representative circuits are presented. Table I gives the values of the circuit parameters determined by direct test, necessary to produce the critical condition between cut-off and non-cut-off operation.

Table II gives the percent deviation of calculated values of L_c from those obtained experimentally.

Non-Cut-Off Operation

An oscillogram of the current through the filter choke when non-cut-off operation prevails is shown in Fig. 3. Under these circumstances the constants of integration in Eq. (4) are evaluated from the boundary conditions at $\omega t = 0$ and $\omega t = \pi$. Assuming balanced anode voltages and steady state operation of the circuit, those are

$$(i_1)_0 = (i_1)_\pi$$

$$\left(\frac{di_1}{dt}\right)_0 = \left(\frac{di_1}{dt}\right)_\pi$$

Applying these conditions to Eq. (4) yields the following expressions for A_o and C_o

$$A_o = \frac{D_1(\psi K_1 + \alpha K_2) - D_2 K_2}{K_1(\psi K_1 + \alpha K_2) - K_2(\psi K_2 - \alpha K_1)} \qquad (10)$$

and

$$C_o = \frac{D_2 K_1 - D_1(\psi K_2 - \alpha K_1)}{K_1(\psi K_1 + \alpha K_2) - K_2(\psi K_2 - \alpha K_1)} \qquad (11)$$

where

$$K_1 = 1 - \epsilon^{-\alpha/2f} \cos \psi/2f$$
$$K_2 = -\epsilon^{-\alpha/2f} \sin \psi/2f$$
$$D_1 = -2YE_m \sin \mu$$
$$D_2 = -2YE_m \cos \mu$$

Where the current through the filter choke is continuous it is evident that the d-c component can be expressed directly as

$$I_{dc} = \frac{(2/\pi)\,E_m - E_o}{R_1 + R_2} \qquad (12)$$

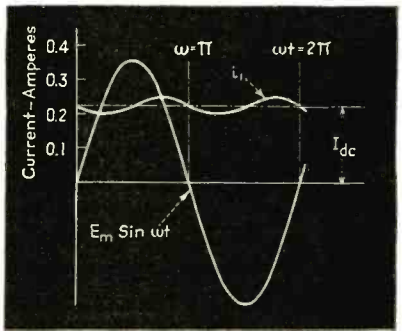

Fig. 3—Applied voltage and rectifier current flowing through filter choke for condition of continuous current flow for non-cut-off operation

the d-c voltage output being merely $I_{dc}R_2$.

The general Fourier series for the choke current is given in Appendix II. Where $\theta_1 = 0$ and $\theta_2 = \pi$, a certain amount of simplification in the coefficients of the sine and cosine terms results, and therefore these expressions are repeated in Appendix IV for reference. Knowing the coefficients, the amplitude of any harmonic of the output voltage can be determined by Eq. (8).

Table III gives comparative results on a rectifier circuit in which $E_m = 324$ volts; $E_o = 12.7$ volts; $L = 8.24$ henrys; $C = 4.23$ μf; $R = 53$ ohms; $R_2 = 728$ ohms, and $\omega = 2\pi f = 377$. The general current equation which is valid from $\omega t = 0$ to $\omega t = \pi$ is

$$i_1 = 0.117 \sin (377t - 82.5) + \epsilon^{-165.3t}[0.375 \cos 58.4t + 0.535 \sin 58.4t] - 0.016 \text{ amperes}$$

Cut-Off Operation

If the circuit parameters have values such that the current flows through the filter in pulses, the arbitrary constants in the general current equation, and the limits of the period of conduction $\omega t = \theta_1$ and $\omega t = \theta_2$ are not so easily determined. Equation (4) is applicable in the cut-off case but it must be restricted by imposing conditions which arise due to fundamental properties of the circuit. At the point of firing, the rising transformer voltage must be equal to the decaying voltage across the filter input since the voltage across the choke is zero at this instant. Therefore at $\omega t = \theta_1$ the following conditions must hold

No. 1 $\quad (i_1)_{\theta_1} = 0$

No. 2 $\quad \left(\frac{di_1}{dt}\right)_{\theta_1} = 0$

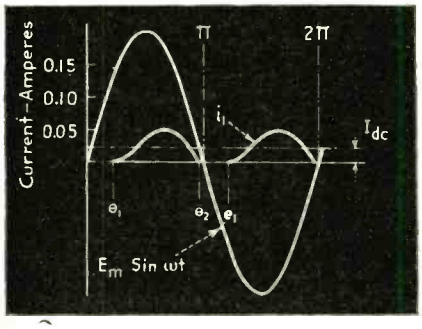

Fig. 4—Waveforms of applied voltage and rectified current output through filter choke for cut-off operation or discontinuous flow of current through choke

TABLE IV—CORRELATION BETWEEN CALCULATED AND EXPERIMENTAL BEHAVIOR OF FULL WAVE RECTIFIER*

Circuit Factor	Calculated Value	Experimentally Observed Value	Deviation in Percent
Output voltage, E_{dc}	195 volts	198.2 volts	1.65
Load current, I_{dc}	0.0250 amp.	0.0254 amp.	1.6
120 cps component of i_1	0.0296 amp.	0.0308 amp.	3.9
240 cps component of i_1	0.00493 amp.	0.00467 amp.	5.45
Percent of 120 cps component of output voltage	5.02	5.15	2.6
Percent of 240 cps component f output voltage	0.42	0.39	7.7

* Tabulation determined for the following conditions: $E_m = 324$ volts; $E_o = 12.7$ volts; $L = 4.0$ henries (air core); $C = 4.0$ μf; $R_1 = 900$ ohms; $R_2 = 7800$ ohms; $\omega = 2\pi f = 377$ radians.

No. 3 $\quad E_m \sin \theta_1 - E_o = V' \epsilon^{-\frac{\pi - \theta_2 + \theta_1}{R_2 C \omega}}$

where V' is the voltage across the filter condenser at the instant of cut-off i.e.: $\omega t = \theta_2$. At this latter point two other conditions are true. Namely:

No. 4 $\quad (i_1)_{\theta_2} = 0$

No. 5 $\quad E_m \sin \theta_2 - E_o = V' + L\left(\frac{di_1}{dt}\right)_{\theta_2}$

Condition 4 is in reality a definition of the angle of cut-off. At this point the voltage across the inductance is not zero even though the current is zero.

It is possible to set up four simultaneous equations involving the unknowns A_o, C_o θ_1, and θ_2 from the above conditions. However, an explicit solution for any one of these terms is not possible. Consequently trial and error methods must be employed. By applying the first two boundary conditions to Eq. (4) the constants A_o and C_o are evaluated in terms of θ_1 and the known circuit parameters. Applying condition No. 4 to Eq. (4) and substituting in these values of A_o and C_o yields an equation involving the two unknown angles θ_1 and θ_2. From conditions 3 and 5 a second equation in terms of θ_1 and θ_2 may be evolved. These two equations can be solved only by assuming values of one angle and calculating the other in a trial and error process. Appendix V gives a more detailed discussion of the manner in which this may be carried out.

Once the values of θ_1 and θ_2 are determined the integration constants A_o and C_o can be easily calculated, and thence the d-c load current and the harmonic content in the output voltage by Eq. (5), (6), (7) and (8).

Table IV gives comparative results in a rectifier circuit having the following constants. $E_m = 324$ volts; $E_o = 12.7$ volts; $L = 4.0$ henrys (air core); $C = 4.0$ μf; $R_1 = 900$ ohms; $R_2 = 7800$ ohms, $\omega = 2\pi f = 377$.

By solution $\theta_1 = 42.1$ deg.; $\theta_2 = 175$ deg.; $A_o = 0.232$; $C_o = -0.480$

The current equation applicable from $\omega t = \theta_1$ to $\omega t = \theta_2$ is

$$i_1 = 0.255 \sin (377t - 41.6°) + \epsilon^{-129t}[0.232 \cos 232t - 0.480 \sin 232t] - 1.46\ (10^{-3}) \text{ amperes}$$

Figure (4) illustrates current waveform for this particular circuit.

Appendix I

Substituting in the values of e and $Z(p)$ into Eq. (1) gives the differential equation

$$i_1[(LCR_2)\,p^2 + (R_1R_2C + L)\,p + (R_1 + R_2)] = (1 + R_2^2C^2\omega^2)^{1/2}[E_m \sin(\omega t + \phi) - E_o]$$

The complete solution of above equation consists of two parts. The solution of the homogeneous equation plus the particular integrals due to the presence of the two voltage functions $E_m \sin(\omega t + \Phi)$ and $-E_o$. Let i_a be the solution of the homogeneous equation, i_b and i_c the particular integrals due to the two voltage functions.

The homogeneous equation is

$$i_a[(LCR_2)p^2 + (R_1R_2C + L)p + (R_1 + R_2)] = 0 \quad (13)$$

which has roots $p_1 = -\alpha + \sqrt{\alpha^2 - \beta}$ and $p_2 = -\alpha - \sqrt{\alpha^2 - \beta}$. In all practical filter circuits $\beta > \alpha^2$, hence the roots are complex and may be written as

$$p_1 = -\alpha + j\psi; \quad \text{and} \quad p_2 = -\alpha - j\psi;$$

where α, β and ψ are constants whose values in terms of the circuit parameters are previously given in the paper. The solution of Eq. (13) is

$$i_a = A_1\epsilon^{p_1 t}, + A_2\epsilon^{p_2 t} \quad (2A$$

where A_1 and A_2 are arbitrary complex constants. Since p_1 and p_2 are complex conjugate roots, Eq. (2a) may be converted into the form

$$i_a = \epsilon^{-\alpha t}[A_o \cos \psi t + C_o \sin \psi t] \quad (14)$$

(*Continued on page* 120)

Walkie-Talkies at War

DEFENSE—An officer, watching the movements of a simulated enemy force from a strategic Iceland height, reports to the headquarters command via radiophone operated by an aide

LANDING—Ashore on a hostile coast, watchers may conceal themselves and observe defensive or offensive activities, reporting such preparations via ultrahigh-frequency radio to their own ships or aircraft

Photos by U. S. Army Signal Corps

OBSERVATION—Here a reconnaissance party, high on a hilltop somewhere in the south Pacific, spies out the land ahead. The man in the background reports by means of a walkie-talkie to the main body of troops, safely under cover at the rear

GUNFIRE—The crew in the background blasts away with its 75-mm fieldpiece, receiving range corrections via the foreground pack set from a spotter located at a point from which the effect of the shells may be seen

Performance of SELF BIASED MODULATED AMPLIFIERS

A procedure is given for determining the dynamic characteristics and optimum performance of self biased modulated amplifiers. The manner in which polarizing voltages vary during tube operation is determined as a function of bias resistor and its location in circuit. Improved linearity of circuit operation and reduced peak driving power are shown by this analysis

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IN AN EFFORT to solve the power tube problems arising from the various classes and conditions of service which the power tube may be called upon to meet, it is helpful to have within reach as many methods of analysis as possible to make available the operating or dynamic characteristics of the power tube. From the operating characteristics may be determined the correct values of the potentials and circuit constants necessary to meet the special conditions and limitations of the problems.

The dynamic characteristics of power tubes may, of course, be obtained by testing the tube directly at the frequency at which it will be required to operate. Special methods[1-4] have been developed for testing the tube at line frequencies, and these methods are more exact and more flexible than the high frequency methods. Other methods for obtaining the dynamic characteristics of the tube, which are often more convenient, are those involving various calculation techniques. Some of these are based on analytical approximations to the static characteristic curves of the tube and others on simplifying assumptions in regard to the wave shape of the current pulses.[5-12] Others involve graphical integrations of the current waveform which may be obtained from the characteristic curves of the tube. Of these methods of calculation some are very accurate but laborious, while others are inaccurate although rapid. A method of calculation described by Chaffee[13] which employs the static characteristics of the tube is exact enough for engineering purposes and is, at the same time, reasonably rapid.

In the above methods of calculation it is not possible to obtain the dynamic characteristics of plate modulated amplifiers with resistance bias except by cut and try methods. In a critical analysis such technique may be exceedingly time consuming. It is the purpose of this paper to present a method which is straightforward in approach and which may be extended to other types of resistance bias operation of electron tubes. Results obtained by this method throw some light on the manner of operation of resistance biased class C plate modulated amplifiers.

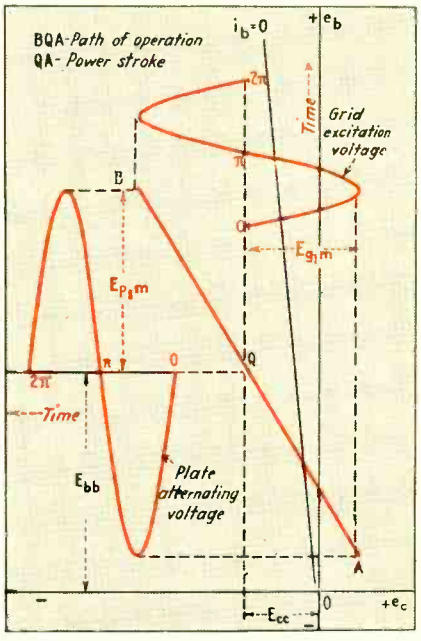


FIG. 1—Static curves in e_b-e_c plane showing quiescent point, Q, path of operation, A-B, and power stroke, Q-A

The method of calculation to be described here requires that the complete static characteristics of the tube be available. These may sometimes be obtained from the manufacturer or by special techniques described elsewhere.[14, 15]

To clarify the treatment which is to follow, it will be well to have clearly in mind what is meant by the "path of operation" and the "power stroke" as these terms are applied in class C operation of power tubes. On the e_b-e_c diagram, the path of operation represents the locus of the instantaneous values of the plate and grid voltages during a complete cycle. If these voltages are sinusoidal and 180 deg. out of phase, the path of operation is a straight line having a negative slope, and centered at the quiescent point, *Q*, as shown in Fig. 1. The end points for

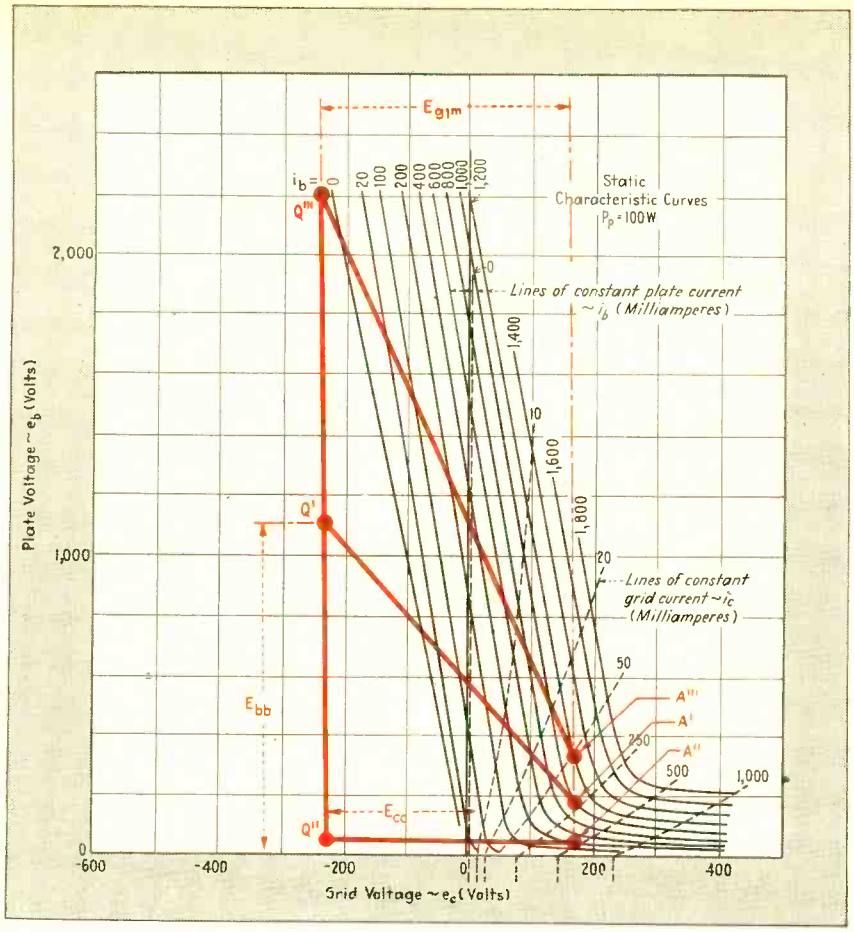


FIG 2.—Constant plate current and constant grid current curves (dotted) of tube whose performance as self-biased plate-modulated amplifier is to be determined. For plate modulated tube with constant bias, the plate operating point varies between Q'' and Q'''. Only the power stroke of the path of operation is shown

the path of operation are shown as A and B. In the analysis in this article, we are concerned only with that part of the path of operation between Q and A, called the power stroke, since it is only during this part of the path that plate and grid currents flow.

Plate Modulated Tube with Fixed Bias

As an introduction to this method let us first consider the conditions that exist in the case where fixed bias is employed in the modulated amplifier. The required characteristics of the power tube, plotted on the e_b-e_c diagram are shown in Fig. 2. Under "carrier" conditions, with no modulation voltage applied, the quiescent point established by the application of the polarizing potentials to the tube is located arbitrarily at Q'. During the modulation cycle, when generator bias or battery bias is employed, this Q point is constrained to move vertically up and down as the amplitude of the plate polarizing potential is being changed at an audio rate. The limiting excursions of Q are Q''' and Q'' when 100 percent modulation is employed. The calculation of the dynamic characteristics under this condition of operation is straightforward. It is necessary to determine only the end point, A, of the path of operation for any given position of the point Q on the line joining Q''' and Q''. When this information about the position of A is available, the shape of the plate or grid current pulse that exists for this path is known. By the application of any of the harmonic analysis techniques referred to previously, the average or fundamental components of the current pulses may be calculated. The determination of A for any position of Q during the modulation cycle follows from the selection of the grid excitation and the equivalent resistance of the tank circuit. The selection of the grid excitation fixes A in the horizontal direction. The vertical position of A may be found by first assuming three or four possible vertical positions as indicated by A_1, A_2, A_3 and A_4, as in Fig. 3, for different values of fundamental voltage across the plate tank. For each assumed position of A we may calculate the fundamental plate current, I_{p1m}, by the use of an appropriate harmonic analysis. This may be plotted as a function of E_{p1m}, as indicated in the lower part of Fig. 3. On the I_{b1m}-E_{p1m} diagram, lines of constant equivalent resistance of the tank circuit $(R_b)\omega = L/RC = E_{p1m}/I_{p1m}$ will appear as straight lines. In Fig. 3 is shown the line corresponding to the particular value of $(R_b)\omega = K_1$ chosen for this calculation. The intersection of this line with the curve through the various A points gives the vertical coordinate of the end point, A' of the path of operation for the particular plate load and Q' point chosen, as indicated in Fig. 2. By repeating this procedure, the fundamental and average currents in both plate and grid circuit may be calculated by this method for different positions of Q and the value of A may be determined for each value of Q consistent with the requirements of the grid excitation and equivalent plate resistance. Knowing the fundamental and average currents for any Q and A points, the power output, driving

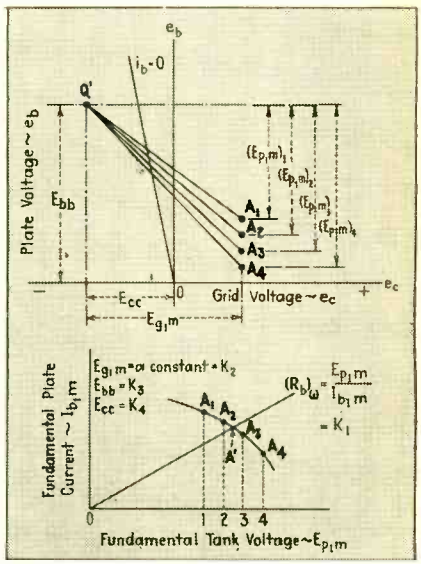


FIG. 3—For specified plate polarizing voltage, grid bias, and grid excitation voltage, the end point of the operating path, A', is determined by selecting several arbitrary end points, A_1 to A_4, (above). These points are plotted on the I_{p1m}-E_{p1m} plane and a smooth curve drawn through them. The intersection of this curve with the load line, $(R_b)_\omega$ determines the desired end point, A'

power, plate efficiency and other so called dependent variables of the modulating system may be calculated. Hence, the dynamic characteristics may be determined.

Complications of Resistance Bias

When resistance bias is employed the problem is far more complicated, for the path followed by Q during the modulation cycle is no longer known. This is because the average grid current which determines the bias is a function of the position of both Q and A. Since Q is not known, A cannot be determined. For example, if at a given carrier condition (zero modulation) we introduce a resistance of such a value as to replace the generator and supply the same bias as it does, operating conditions at this point will be identical with those obtained with the generator. But if the plate potential is increased or decreased, the movement of the Q point is dependent upon the way the grid current will vary, consistent with the limitations imposed upon the tank circuit equivalent resistance and the excitation. Further, if the bias is supplied by inserting a resistance in the cathode lead, the movement of Q will depend on the variation of the average plate current in addition to the above. Obviously, the path followed by Q will be a complex function of at least four independent variables, E_{bb}, E_{cc}, E_{g1m} and $(R_b)\omega$, and in the case where the bias, or part of the bias, is furnished by plate current, by five independent variables, the fifth variable being the bias resistor.

The problem then is to determine the locus which the Q point takes during the excursion of the plate voltage in the modulation cycle. Once this locus is determined for the particular grid excitation, equivalent plate resistance, and biasing resistance that are chosen and fixed for this calculation, the position of A could be determined for any Q point along this path in a manner similar to that outlined above. However, in order to find the path which Q follows in the case of resistance biasing, it is necessary first to find the coordinates of A for any likely position of Q during the modulation cycle. The positions that A is likely to take can certainly be restricted to that portion of the e_b-e_c plane to the right of the $e_c = 0$ axis and above the $e_b = 0$ axis, in Fig. 3. When these coordinates of A are found, the problem is greatly simplified, as will be shown.

Now, for any position of Q on the e_b-e_c plane, (Fig. 2) the horizontal coordinate of A is fixed by the choice of the grid excitation voltage. The vertical coordinate of A can be determined for any given equivalent plate resistance in the following manner. First we select an arbitrary position for Q for a given value of plate polarizing potential E_{bb}, and a specified value of the grid polarizing potential, E_{cc}, the value of the

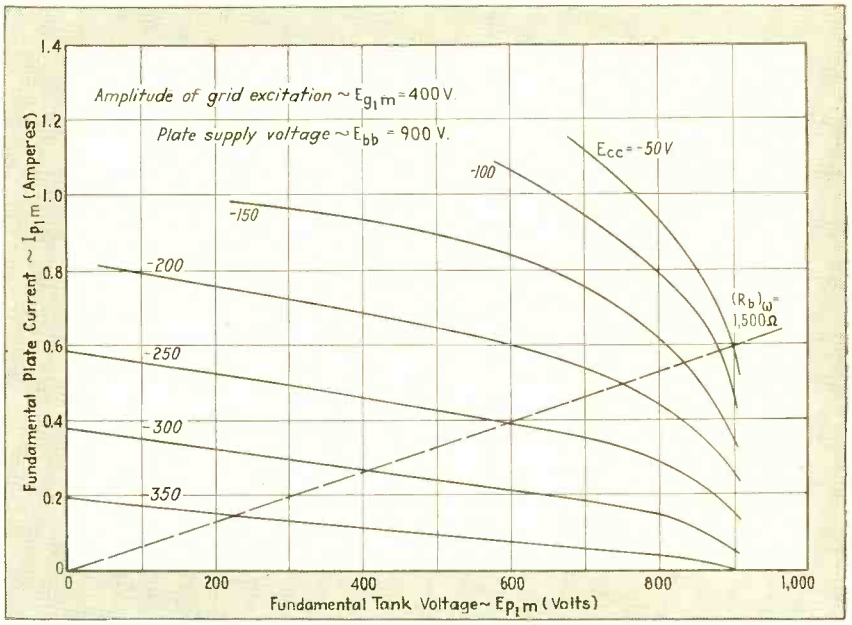
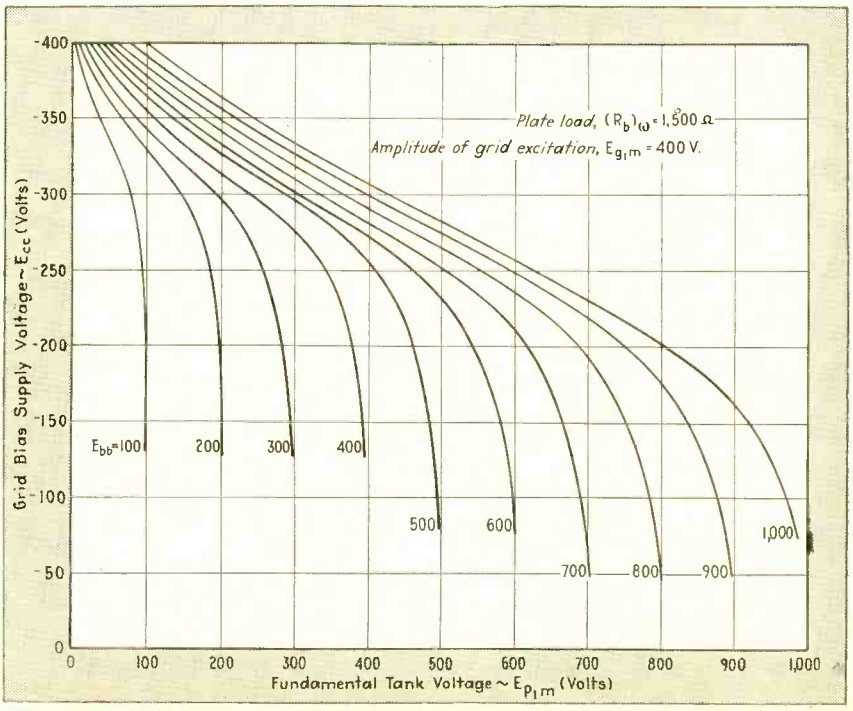


FIG. 4—Graphical plot of end points of the path of operation. Each curve, for different value of grid bias, is determined in the same manner as the curve in the lower half of Fig. 2. The intersection of the plate load line with the family of curves permits the determination of data for one curve of those shown in Fig. 4. Several such diagrams are required, each for the same grid excitation but for different values of plate voltage

FIG. 5.—For constant plate load and grid excitation, this family of curves (each one of which is derived from a family like those of Fig. 3) shows the relation between grid bias and alternating voltage across the tank circuit



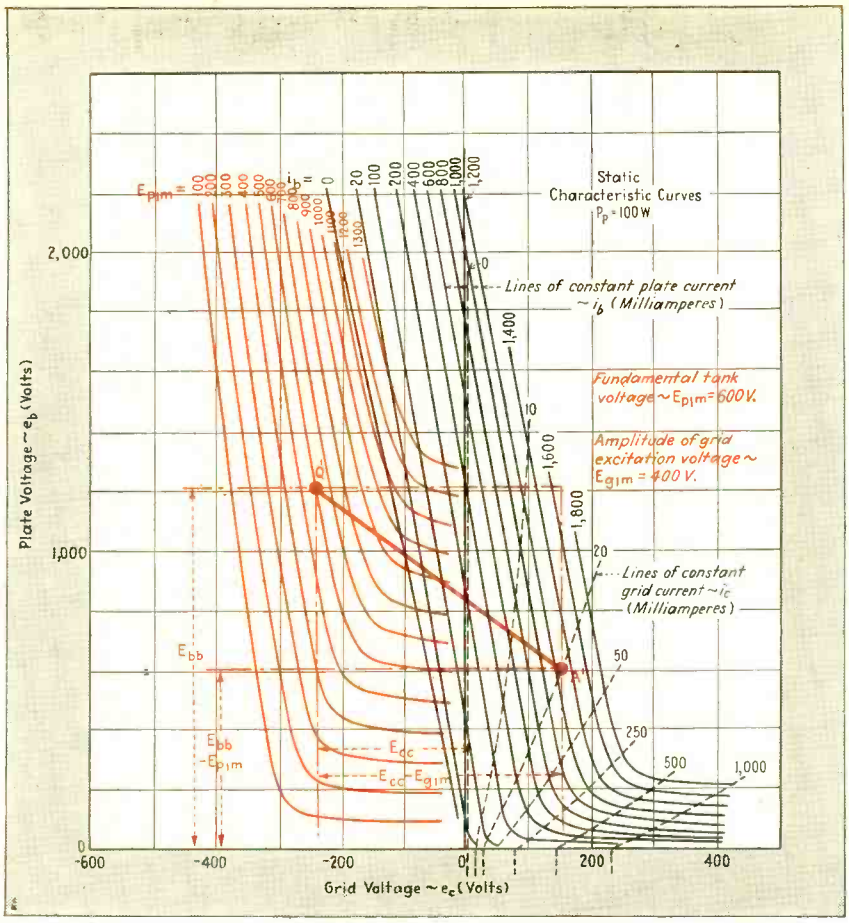
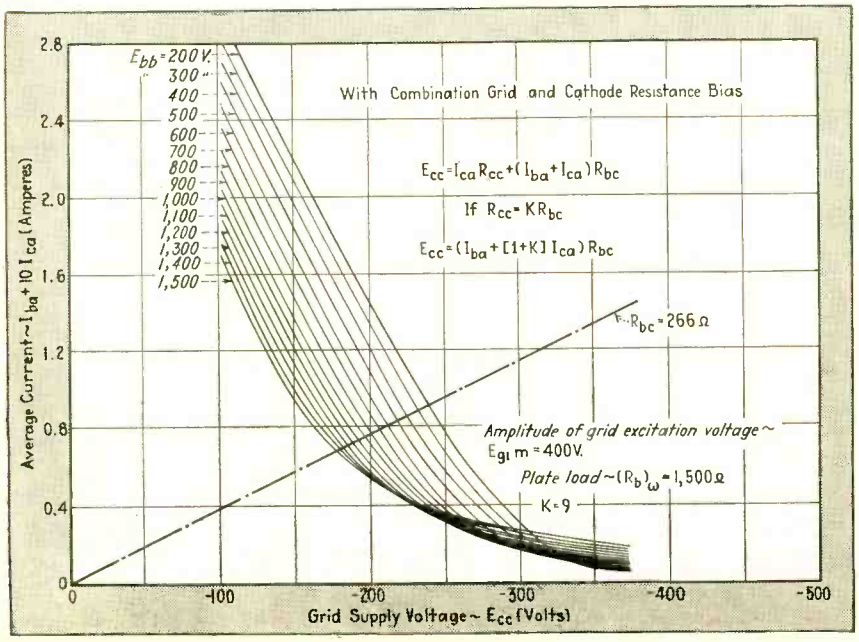


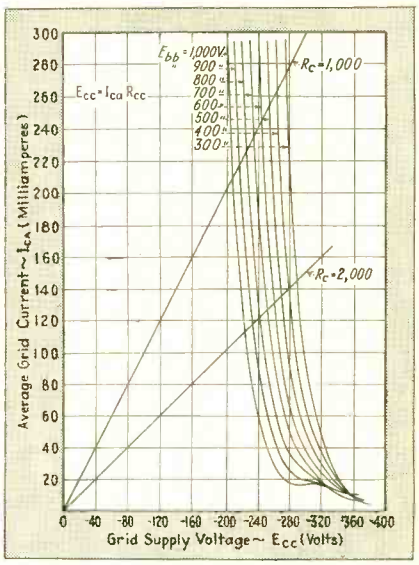
FIG. 6.—Curves of Fig. 4, replotted on the e_b-e_c *plane* (in red) and super-imposed on the original constant current curves of Fig. 1. The composite set of curves enables the end point *A'* to be determined for any *Q'* point, for the grid excitation voltage, constant grid bias, and plate load, $(R_b)_\omega$, assumed for this calculation

FIG. 7—Family of curves, for different values of plate polarizing voltage, plotted on grid voltage- average grid current characteristics. From this diagram on which grid resistance R_g, appears on a straight line, the paths followed by Q in the e_b-e_c plane can be determined

FIG. 8—Family of plate polarizing voltages for combined grid and cathode resistance bias. In this diagram, it has been assumed that $R_{cc} = 9R_{bc}$



grid excitation, E_{g1m}, remaining fixed. For this *Q*-point we may calculate the fundamental plate current amplitude as a function of the fundamental voltage across the plate tank circuit in a manner similar to that employed in the case of generator bias. For the tube whose characteristics are shown in Fig. 2, and for operating voltages E_{bb} = 900 v., E_{cc} = —50 v., the curve obtained is that labeled E_{cc} = —50 volts in Fig. 4. Other curves like this may be obtained by holding the plate polarizing potential E_{bb} fixed at 900 volts and increasing the grid polarizing potential E_{cc} negatively in steps of 50 volts. These curves take the form of the famliy of curves



shown in Fig. 4. Lines of constant plate resistance may now be drawn on this diagram. For example, the dashed line, Fig. 4, represents a constant equivalent resistance $(R_b)\omega$ = 1500 ohms. Diagrams similar to this one are obtained for a number of values of plate polarizing potential, and on each the same line of constant equivalent plate resistance is drawn.

For various values of plate voltage the intersection of the lines of constant grid voltage, E_{cc} with the line of constant plate resistance $(R_b)\omega$ may be plotted on a diagram having the coordinates of Fig. 5. These curves of Fig. 5 may, in turn, be transferred to the e_b-e_c plane. When this is done they take the form indicated by the red curves in Fig. 6. Actually Fig. 5 is only an intermediate diagram which is convenient to

FIG. 9—Characteristic paths of the Q point for various methods of bias. Curve *A* is for cathode resistance bias, and is the least desirable type of resistance bias. Curve *B* is for constant grid voltage bias. Curve *C*, which represents the most desirable type of resistance bias, is for the bias resistance in the grid circuit

use in order to obtain the material represented on Fig. 6.

Tube Operation for Fixed Bias, Plate Modulated Conditions

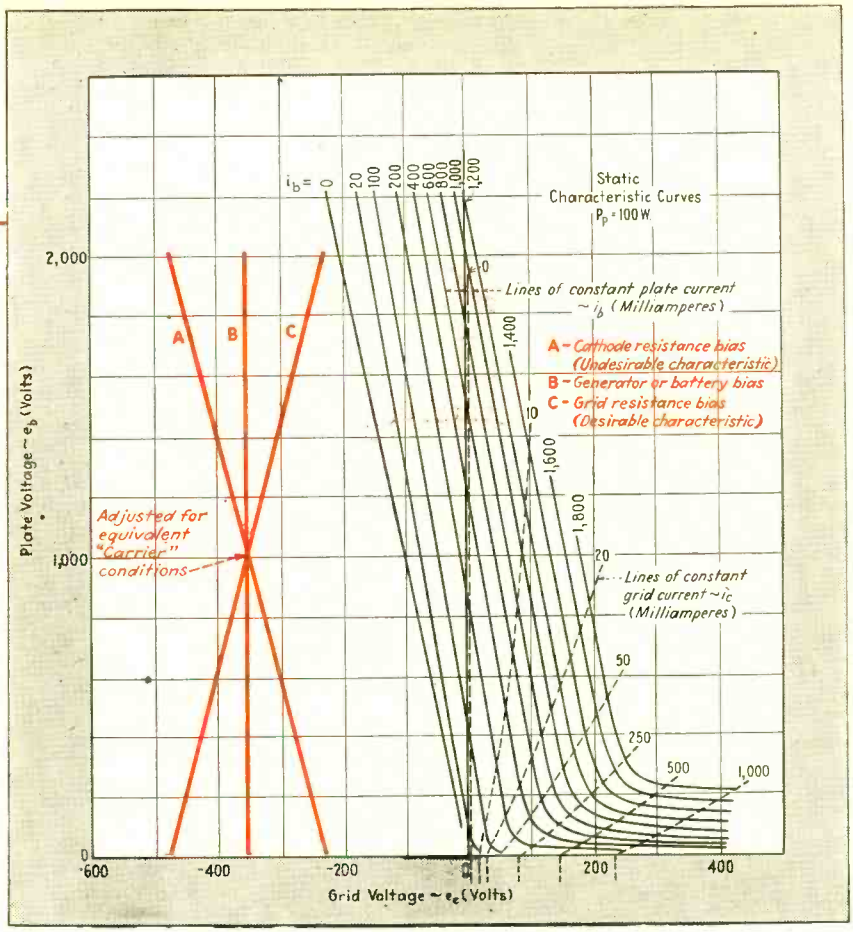
When the family of curves of Fig. 6 representing lines of constant E_{p1m}, have been obtained and plotted on the e_b-e_c diagram, the problem is almost solved. It is convenient to draw the family of curves, E_{p1m} = constant, on transparent or translucent paper rather than to plot them directly on the e_b-e_c diagram so that they may be superimposed on the curves of Fig. 2, as shown in Fig. 6, the superimposed curves being indicated in red. From the superimposed curves we know the value of E_{p1m} that must be used for any arbitrarily chosen Q point. For any Q-point in the region to the left of $e_c = 0$ and above $e_b = 0$, both horizontal and vertical coordinates of A are now determined, since the assumed grid excitation gives the horizontal distance of A from the Q point while the value of E_{p1m} on which the Q point falls as read from the red curves gives the vertical distance.

An example will help clarify the procedure. The derived curves (red) are superimposed on the constant current static curves (black). A point Q' is arbitrarily selected at E_{bb} = 1200 volts and E_{cc} = −250 volts. This Q' point cuts the derived curves at E_{p1m} = 600 volts, and the excitation voltage was taken as E_{g1m} = 400 volts. Then, with Q' as the starting point, the coordinates of A' are $e_b = E_{bb} - E_{p1m} = 1200 - 600 = 600$ volts, and $e_c = E_{cc} = E_{g1m} = -250 + 400 = +150$ volts.

Effect of Resistance Bias

We have not yet taken into account the effect of resistance bias, which is

(*Continued on page* 128)



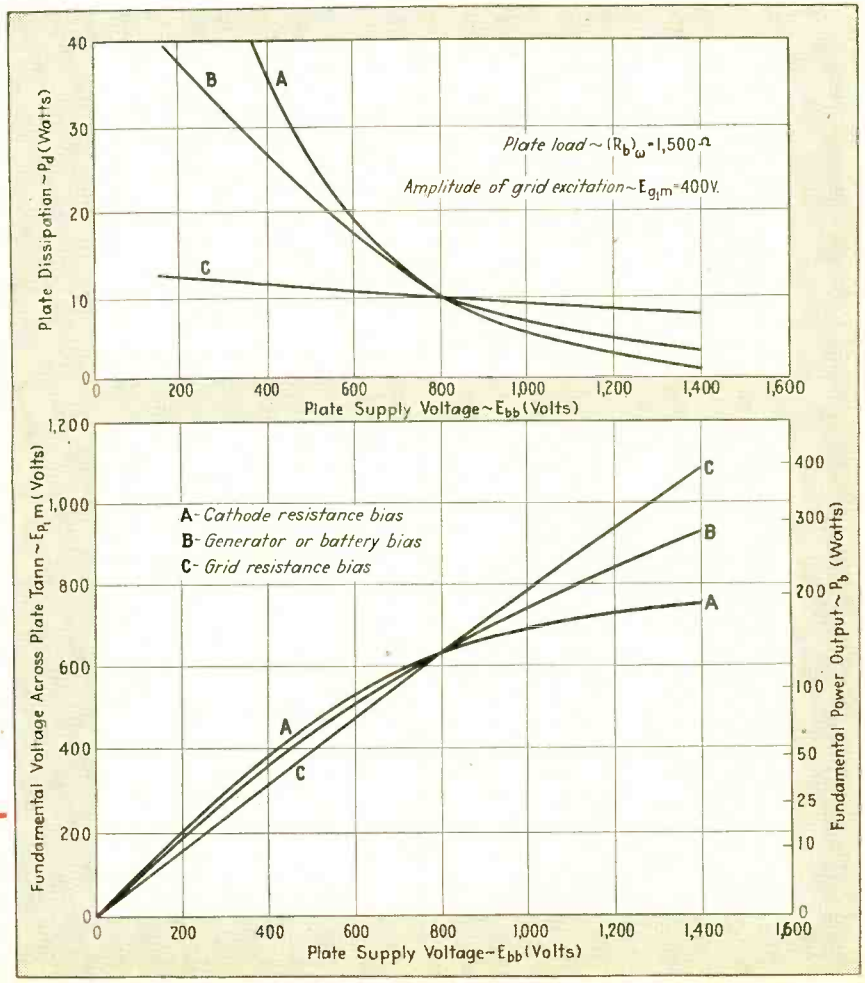


FIG. 10—Dynamic characteristics for plate modulated amplifier, for three types of biasing conditions. Most desirable characteristic is that for which power output is linearly proportional to d.c. plate voltage, and maximum driving power is a minimum

Electronic Regulators

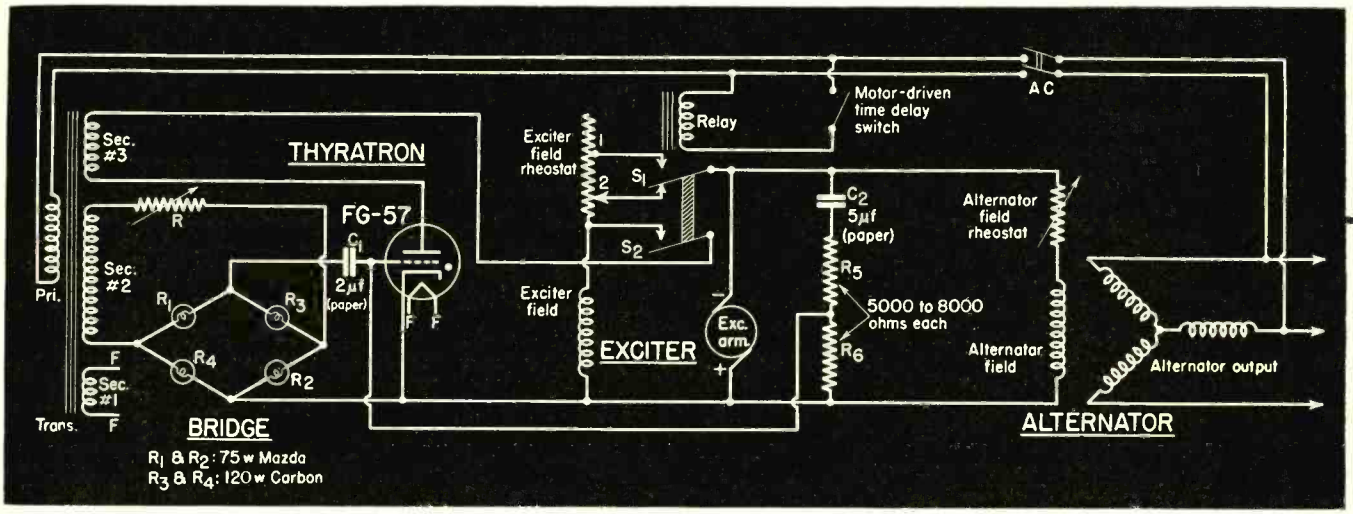


FIG 1—Circuit diagram of an electronic voltage regulator using a single thyratron and a lamp bridge. The thyratron carries only that fraction of the exciter field current which is required for effective control of the a-c generator output voltage

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NUMEROUS electronic regulators for small and medium-size a-c generators have been described in the literature of both physics and electrical engineering. These have either consisted of a large number of tubes with rather complicated circuits, or else have not utilized to the fullest extent the advantage of the electronic regulator over mechanical regulators. This advantage lies chiefly in the rapid response of the electronic regulator.

Several years ago the writer developed a simple single-tube electronic regulator which has the advantages of simplicity and rapid response as well as stability, and may be assembled from standard parts. This regulator is described in the first part of this paper.

Later developments indicated changes and improvements which made possible an even cheaper regulator for small generators. This second regulator is described in the second part of this paper.

Single-Tube Regulator

Referring to the complete circuit diagram in Fig. 1, the machine at the right is an ordinary three-phase a-c generator (it could just as well be a single-phase or two-phase a-c generator) with a d-c exciter connected to furnish the excitation for the alternator field. The a-c generator is provided with a field rheostat (which is usually not necessary in practice), and the d-c exciter is provided with a field rheostat. This much of the diagram constitutes the ordinary commercial set-up for any a-c generator.

The heart of this electronic control circuit is an FG-57 grid-controlled mercury vapor rectifier tube (thyratron) with a negative grid control characteristic. It secures power from a transformer whose primary is connected directly to the output of the a-c generator. Secondary No. 1 of this transformer supplies the proper voltage for heating the filament which requires 4.5 amps at 5 volts.

The bridge circuit consists of two 115-volt, 75-watt Mazda lamps (R_1 and R_2) and two 115-volt, 120-watt carbon-filament lamps (R_3 and R_4). Secondary No. 2 supplies this bridge circuit with a voltage of approximately 120 volts. An adjustable resistor R is provided in this circuit so the applied voltage may be adjusted within limits. The output of this bridge circuit is applied to the grid-cathode path of the thyratron through 2-μf paper condenser C_1. Secondary No. 3 supplies plate voltage for the tube. The output of the tube is fed to the exciter field through relay contacts S_2.

Relay contacts S_1 are used to change the exciter field rheostat from position 2 to position 1. The relay itself is operated by a motor-driven time delay mechanism which allows the thyratron approximately five minutes to warm up before it is called on to function as a regulator.

The circuit $C_2R_5R_6$ serves to prevent the tube and machine from surging or hunting while in operation. By proper proportioning of these three values the action is smooth and rapid. Condenser C_2 is usually 4 to 5 μf, while R_5 and R_6 are 5000 to 8000 ohms each. Resistor R_6 must be adjusted to the time constant of the exciter and alternator fields. Reducing the resistance of R_6 reduces the sensitivity of the regulator, hence this resistor should be set at the highest value which will give stable operation.

Description of Operation

When the a-c generator and exciter are started up by their prime mover, the regulator is not operative immediately. Contacts S_2 are open, and contacts S_1 are in position 2.

for A-C Generators

Two simple circuits are given. In the first, a single large thyratron handles only the portion of exciter field current needed for control purposes. In the second circuit, for small a-c generators, a thyratron and two 866's furnish all exciter field current

Control of voltage is accomplished manually by means of the exciter field rheostat. The voltage is adjusted to the desired value by hand as load is applied during the first five minutes. A motor-driven time delay switch starts up immediately. After the five-minute delay, during which time the filament is heated, the delay switch energizes the relay. Contacts S_2 then complete the plate circuit of the thyratron and contacts S_1 change from rheostat position 1 to 2. The S_1 contacts are so designed that the circuit is made at 1 before it is broken at 2.

The regulator is now in operation and has full control of the voltage. When the machine is shut down, the time delay relay automatically resets itself, opening S_2 and throwing S_1 from position 1 to position 2.

The reason for using S_1 to change the rheostat from position 2 to 1 when the tube is placed in operation is as follows: The exciter rheostat is initially adjusted to maintain the proper alternating voltage with the thyratron inoperative and S_1 in position 2. When S_2 is closed, the tube is inoperative at the load for which the exciter rheostat was set during the warm-up period. If some load were dropped from the alternator, the voltage would rise above normal. Additional resistance is introduced by S_1 so that even at no load the voltage will not be too high when the electronic regulator is operating. Best results are usually obtained by a resistance between positions 1 and 2 of at least twice the exciter field resistance, with the optimum value depending on the constants of the machine.

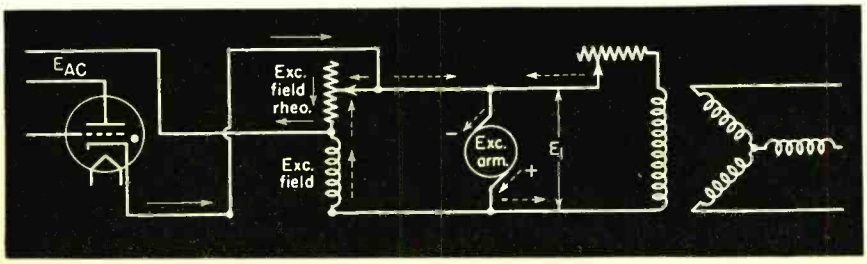
The control of the voltage is accomplished as follows: If the voltage drops below a value determined by the setting of rheostat R in the circuit of secondary No. 2, bridge $RR_2R_3R_4$ unbalances in such a direction as to make the grid of the thyratron less negative. The thyratron then becomes operative, rectifying the a-c supply from secondary No. 3 and feeding this rectified pulsating direct current through the exciter field in the same direction as the regular field current flows. The net excitation of the field thereby increases, causing the voltage of the exciter to rise. The current in the alternator field therefore increases and the alternating output voltage rises.

Parenthetically, it should be explained that part of the output of the tube probably flows through the exciter field rheostat and exciter armature, thus reducing the voltage drop in the rheostat. The net result is to raise the exciter field current.

The rising alternating voltage acts through the transformer to make the grid more negative, stoping conduction of the tube. This in turn allows the voltage of the exciter, and thus of the alternator, to decrease until the tube again becomes operative.

To prevent the circuit from surging or hunting, resistors R_5 and R_6 and condenser C_2 are connected across the exciter output as shown.

FIG. 2—Method of connecting a thyratron across the field rheostat for voltage control purposes. The necessity for a grid bias battery is one drawback of this previously-used arrangement



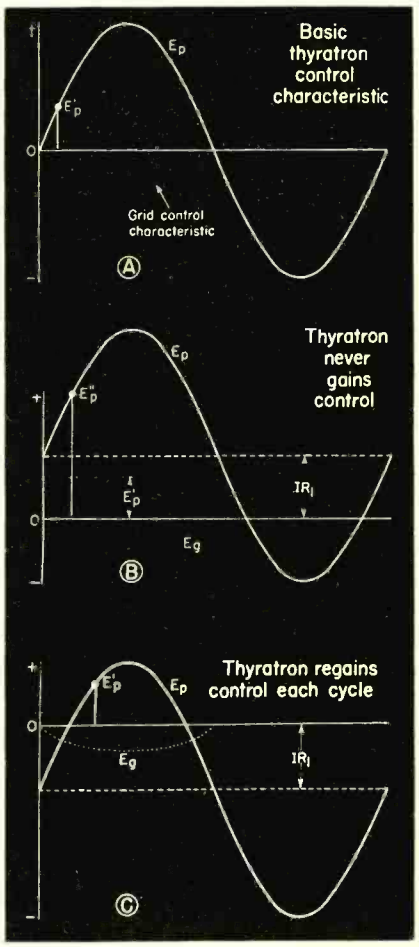


FIG. 3—Diagrams illustrating why a grid bias battery is required in the circuit of Fig. 2 in order for the thyratron grid to regain control each cycle

When the exciter voltage rises, a charging current flows through this circuit. The momentary voltage drop across R is in such a direction as to bias the grid of the tube negatively with respect to the cathode, which tends to make the tube inoperative. This action prevents the system from setting up sustained oscillations, called hunting or surging. Resistance R_6 also acts as a grid leak from the grid to the cathode.

By properly proportioning the values of R_5, R_6, and C_2 the action can be made so smooth and rapid that no change is detected in the alternating voltage when the load is constant. The recovery of the voltage when full load is suddenly applied to the a-c machine is quicker than with other conventional regulators, since it does not depend entirely on the time constants of the alternator and exciter fields. When more voltage is required, the exciter field is energized almost instantly by the output of the tube.

Other Electronic Regulator Circuits

In some previous electronic regulators the output of the tube was connected across the field of the exciter so as to reduce the excitation at light loads. When the load came on and the alternating voltage dropped, the tube was blocked and the excitation rose according to the time constants of the exciter and alternator fields. This arrangement had the disadvantage of requiring maximum tube current at light loads, and also was slow in response to sudden increases in load.

Another method of connection which has been previously used is that shown in Fig. 2, where the tube is connected in parallel with the field rheostat. Such a circuit required the use of a grid bias battery to allow the grid to remain in control at all times.

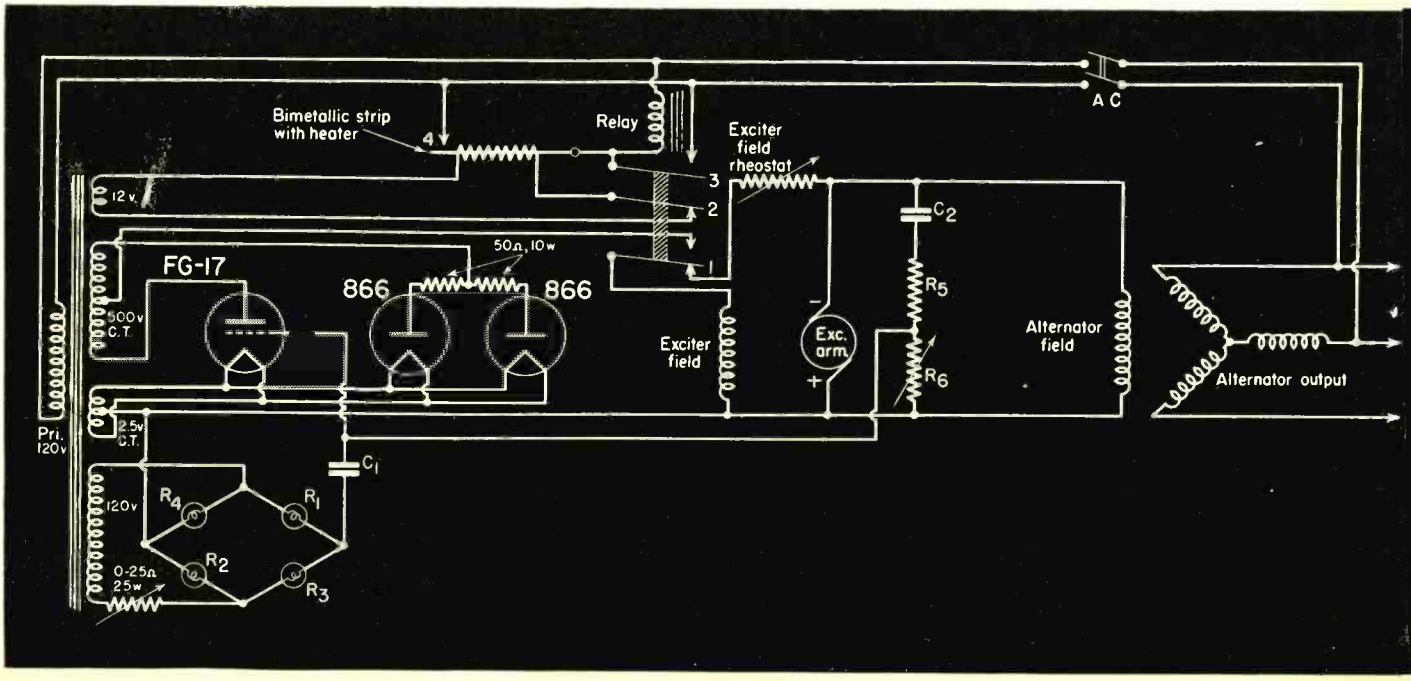
In order to show why this was necessary, we will consider the relative directions of current flow in the tube, exciter, and rheostat. In Fig. 2, the dotted arrows indicate current flow in the circuit due to the exciter voltage E_1, and the solid arrows indicate current flow due to the tube output. It is seen that the tube current flows through the field rheostat in a direction opposite that of the generator current, thus decreasing the voltage across the field rheostat and increasing the total current in the field. The rheostat voltage drop is in the same direction as that half-cycle of the alternating voltage which causes the tube to fire, and the two direct voltages add. The resulting actions are portrayed by the diagrams in Fig. 3.

In Fig. 3A is the well-known control characteristic of the thyratron. The tube will start to fire at any time during the cycle that the grid voltage is more positive than the dotted grid characteristic curve, and once started it continues to conduct until the plate voltage E_p is reduced to zero. The critical plate voltage required to cause the tube to fire with no grid voltage is E'_p.

Figure 3B shows the voltage drop of the rheostat (IR_1) added to E_p. The actual grid control voltage obtained from the bridge circuit of Fig. 1 is shown by dotted curve E_g. If the voltage drop is greater than the critical plate voltage E'_p, the tube conducts during the entire positive half-cycle and the grid voltage can never gain control. It then becomes necessary to add a grid bias battery to the grid circuit, to prevent the tube from firing until a new value of critical voltage E''_p is reached. This battery arrangement is unsatisfactory for two reasons: 1. The grid bias battery is likely to go dead without warning, thus allowing the tube to conduct all the time and raise the voltage to a value which would destroy connected loads; 2. The voltage drop increases with increase of excitation, so unless the bias voltage is carefully adjusted, the voltage drop with heavy loads and large exciters may rise high enough to overcome the grid bias and allow the tube to operate without control.

If now the output of the tube is connected directly across the exciter field, as is done in the new circuit in Fig. 1, the voltage drop across the field opposes the half-cycle of the alternating plate voltage which

FIG. 4—Alternative electronic voltage regulator circuit which has proved satisfactory in applications where the maximum exciter field current does not exceed 1 amp



causes the tube to fire, as shown in Fig. 3C. The critical plate voltage E'_p always occurs after the grid voltage increases negatively, no grid bias battery is required, and the entire circuit is always stable.

Other Features of New Regulator

With the regulator shown in Fig. 1, the excitation is aided by the tube when the load comes on, thus raising the voltage more rapidly. Also, the tube is only fully conducting during short periods of very heavy loads. Under normal loads it rectifies only a small portion of the time, which results in increased tube life. Some of the required current for the exciter field comes normally from the exciter armature itself, and hence the tube can be much smaller than if it supplied all the field current. No special field winding is required; any standard exciter will work with this arrangement.

The development work on this regulator was done on two different 5-kva, 3-phase, 230-volt alternators, one a sine-wave alternator and the other a salient-pole machine having a very pronounced 19th harmonic due to slot ripple. These machines were driven by 7.5-hp d-c compound motors. As a performance test, each alternator was driven at rated speed at no load, and one and one-half times full balanced 3-phase load at 100 percent power factor was thrown on the machine. Beyond the momentary dip due to the lag of the machine fields, no change in voltage could be determined on the 300-volt scale of a Weston a-c voltmeter even though the speed of the driving motor decreased about 15 percent.

The same result was obtained with 70 percent power factor balanced load. With single-phase loading the voltage on the regulated phase was constant, although of course the three-phase voltage was unbalanced.

The time delay consists of a clock mechanism manufactured by Hansen Manufacturing Co., and may be obtained on special order with the minute hand making one revolution in five minutes. A small cam placed on this shaft acts on one blade of the relay, closing the contacts. This energizes the relay coil, closing S_2 and changing S_1 from contact 2 to contact 1 and thus putting the regulator in operation. The motor on the clock mechanism is still energized as long as the cam touches the blade, so it runs until the cam is free. The motor then stops, and is ready for another cycle of operation.

Simplified Regulator for Small Generators

Where the maximum field current of the exciter does not exceed 1 amp, the circuit shown in Fig. 4 is just as satisfactory as the previous one, and the cost of the parts is less. Several regulators of this design have been in commercial use over a year on 40-kva, 1200-rpm machines.

The same voltage-sensitive bridge described for the first regulator is used. The plate supply is a center-tapped 500-volt winding which serves a full-wave rectifier circuit feeding the exciter field directly. The response is slightly more rapid than that of the previous regulator, but the adjustment of anti-hunting circuit $R_5R_6C_2$ is more critical. For this reason R_6 is a 1000-ohm fixed resistor in series with a 5000-ohm variable wire-wound resistor which can be adjusted readily to eliminate hunting. Reducing this resistance reduces the sensitivity of the regulator, hence the maximum value which gives stable operation should be used.

The rectifiers are two 866/866A tubes operated in parallel for one half of the cycle, and an FG-17 thyratron for the other half-cycle. As is commonly known, if one half of the cycle of a rectifier feeding an inductance is controlled, the current during the other half of the cycle will necessarily be the same, due to the inductance. Thus only one grid-controlled tube is needed.

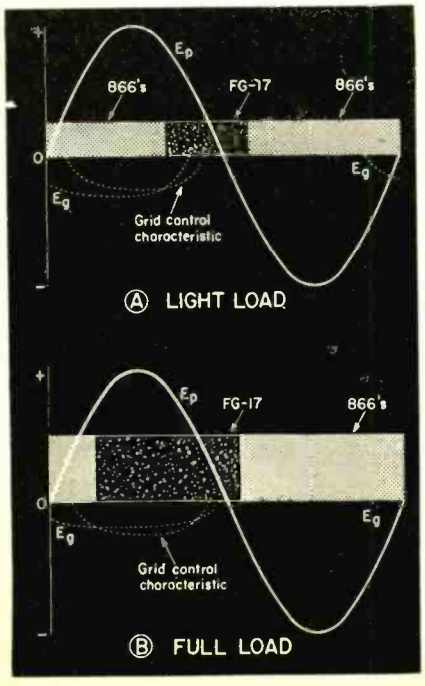
Two 866 tubes are used in parallel because they normally carry the greatest part of the current, with the grid-controlled tube operating over a very small portion of the cycle. To make these two 866 tubes divide the current equally, a 50-ohm, 10-watt fixed resistor is connected in series with each plate as shown in Fig. 4.

Figure 5A shows the division of load between the grid-controlled tube and the 866 tubes for light load conditions, while Fig. 5B shows the changed conditions for heavy load. The 866 tubes continue to conduct until the applied voltage E_g on the grid of the control tube becomes less negative than the grid control characteristic, even though these tubes may be conducting in the range where the applied voltage is in the wrong direction. This action is due to the inductance of the exciter field. The grid-control tube cuts off as soon as the applied voltage on the 866 tubes is sufficient to equal the internal tube drop, at which time the pair of tubes again takes over. Voltage E_p is the applied plate voltage for the grid-controlled tube; the plate voltage for the 866 tubes will be inverted, since it is obtained from another half of the transformer secondary.

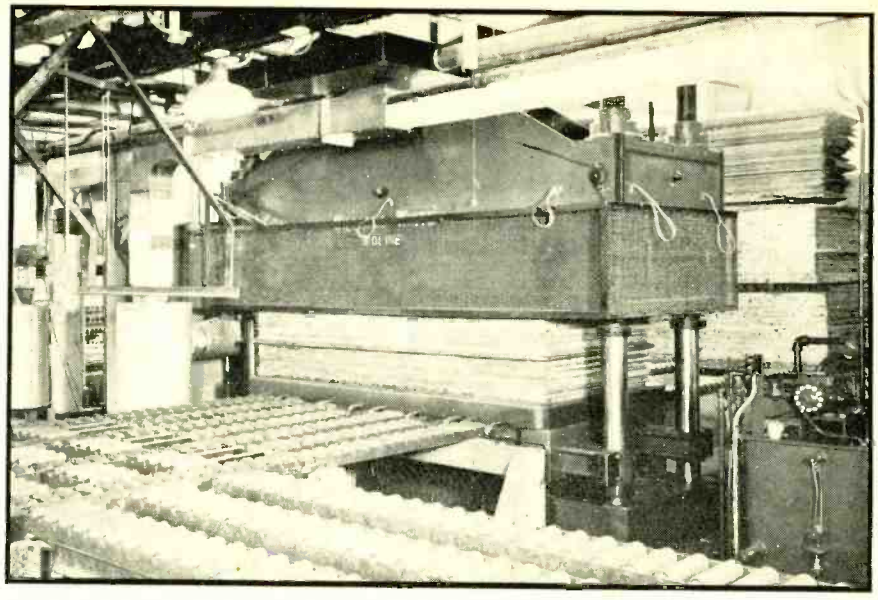
Since these tubes reach operating filament temperature in 15 to 20 seconds, the time delay device is considerably simplified. A 20-second delay thermal strip which operates on 12 volts is used.

The field rheostat is set by hand to give rated voltage when the machine is brought up to normal speed. At the end of the 20-second time delay interval, contact 4 on the thermal delay closes, energizing the relay coil. Relay contact 1 then connects the exciter field to the regulator. Relay contact 3 closes, providing a holding circuit which keeps the relay energized. Relay contact 2 opens, breaking the circuit through the heater on the thermal delay and allowing this heater to cool down in readiness for another cycle of operation.

FIG. 5—The shaded portions indicate the division of load between the two halves of the rectifier circuit of Fig. 4 under different loads



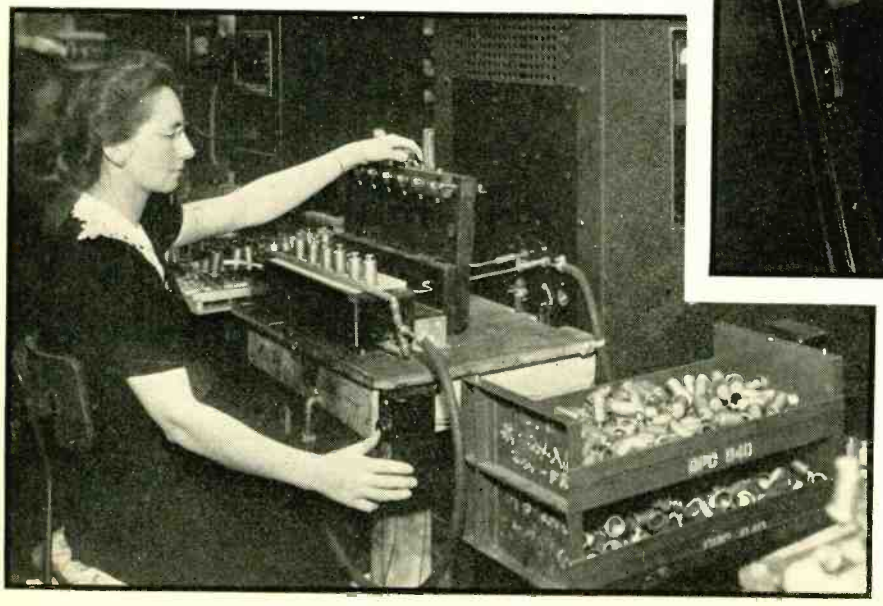
TRANSFORMERS—By wrapping short lengths of solder around terminals and then heating all of them at once by means of power induced from a single-turn coil RCA avoids the necessity for applying a soldering iron to each individual terminal



WOOD—Fir veneer bonding is quickly set in this press, bundles 12 inches thick being placed each side of a center electrode. Girdler Corporation high-frequency equipment raises the temperature of the stacks to 160 deg. F in less than five minutes

High-Frequency HEATING

CRYSTALS—Here high frequency heat takes the place of gas heat in a G-E plant, soldering a protective shell to a base without overheating a frequency control unit mounted inside



CRANKSHAFTS — This Ohio Crankshaft Company machine, powered by Westinghouse generators, hardens bearings in four seconds by inducing current into them from a collar constituting a single-turn coil. Distortion of the shaft is minimized as resulting heat is closely confined to the bearings

CHART FOR
Equivalent Series and Parallel Circuits

Semi-circle diagram permits rapid conversion of series values of an impedance to the equivalent of an impedance composed of parallel elements, and vice versa. Chart may be applied over wide range of impedance values.

BY R. TOOMBS

British Broadcasting Corp.
London, England

IN dealing with circuits containing resistance and reactance, the need often arises for a quick and easy method of converting the series values of an impedance to the equivalent parallel values. The possibility of a graphical process appeared most useful and the semicircle diagram has been devised as a graphical method of meeting these requirements. This, of course, conforms to a general type of circle diagram which is already quite familiar.

Any point on this diagram represents an impedance whose series resistance and reactance are indicated by its rectangular coordinates, while the equivalent parallel components are given by the values where the corresponding circular coordinates cut the resistance and reactance axes, remote from the origin.

For finding the equivalent series components of an impedance expressed as parallel quantities, the resistance and reactance circles corresponding to the parallel values are followed round to their point of intersection. The rectangular coordinates of this point indicate the equivalent series components of the impedance. As the chart is symmetrical about the diagonal $X_1 = R_1$, either axis may be used for resistance as long as the other axis is used for reactance.

Values at which the circles would meet their respective axes have been marked against some of the circles. The range of the diagram may be increased by applying a common multiplication factor to the scales of both axes and the figures marked on the circles.

The chart is particularly useful in the design of networks for matching two circuits of different impedances. Where a resistance load of R_A is to be built out to match a circuit of higher resistance R_B without any power loss, this can be done by adding a series reactance j_sX_A and then shunting the combination by a parallel reactance j_pX_B of opposite sign. The resistance circle corresponding to the value of R_B is followed until it cuts the rectangular resistance ordinate of the value of R_A. The other rectangular and circular ordinates of this point immediately give the respective values of the series and parallel reactances, j_sX_A and j_pX_B, which are required to effect the matching. These, of course, must be of opposite sign.

Examples: (1) To find the equivalent parallel components of an impedance expressed as 19 ohms resistance in series with 9 ohms positive reactance. The impedance point on the chart is determined by the rectangular coordinates from 19 on the horizonal (resistance) axis and 9 on the vertical (reactance) axis. The circles which intersect at this point would cut these two axes respectively at 23.25 and 49. Therefore, a resistance of 23.25 ohms shunted by a reactance of 49 ohms is equivalent to the given impedance expressed as a resistance of 19 ohms in series with a reactance of 9 ohms.

(2) To match an antenna of 19 ohms resistance and 142 ohms series reactance to a 100 ohm transmission line. For convenience of operation on the chart, half the above values are considered, and an impedance of $9.5 - j_s71$ converted to a pure resistance of 50 ohms. This is also a case where it is advantageous to use the vertical axis for resistance and the horizontal axis for reactance. The rectangular ordinate from 9.5 on the vertical axis cuts the 50 resistance circle (i.e. which would meet the vertical axis at 50) at the point whose other rectangular and circular ordinates meet the horizontal axis at 19.62 and 24.25 respectively. Thus we have

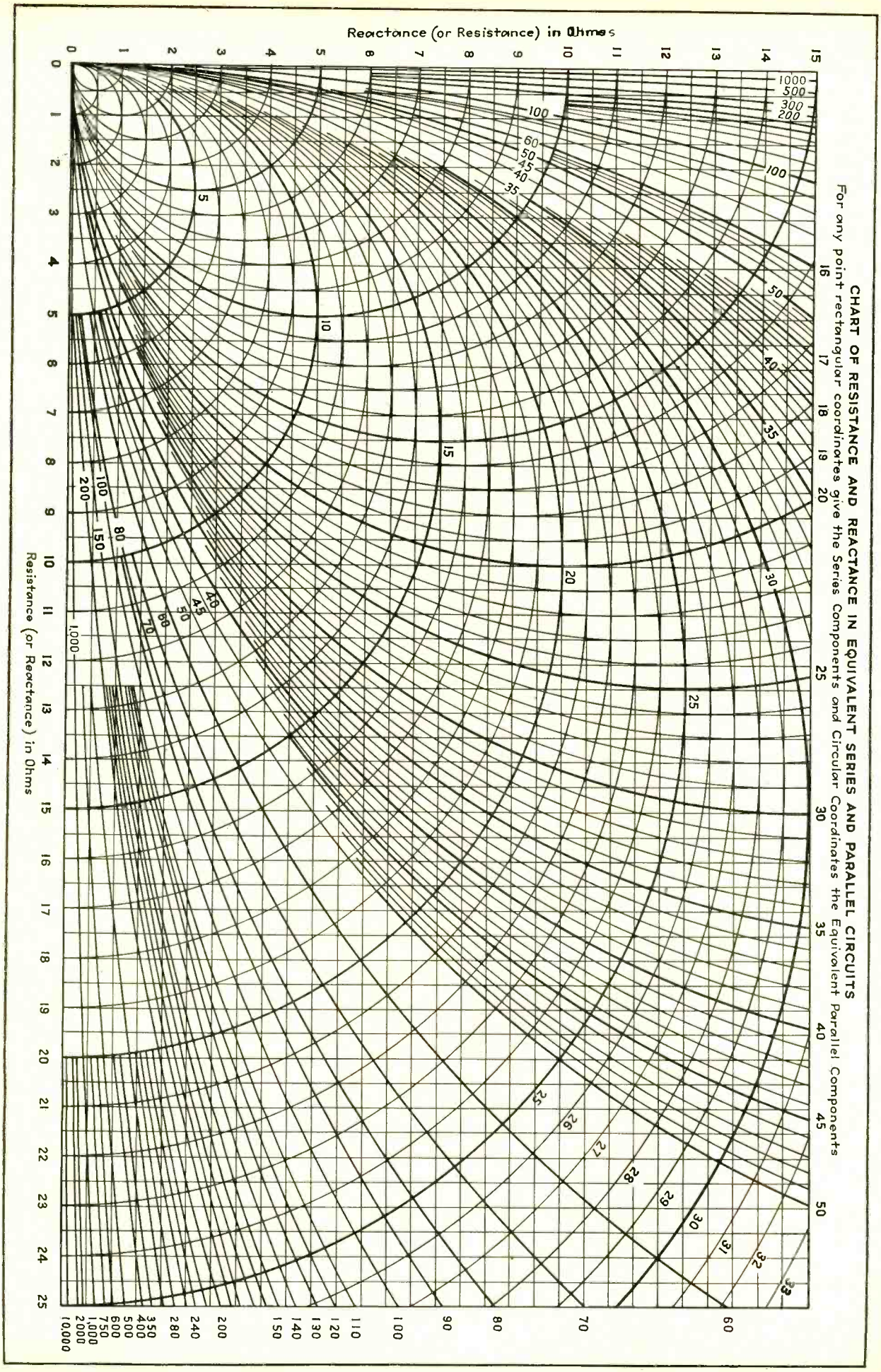
$9.5 \pm j_s\ 19.62 = 50 \pm j_p\ 24.25$

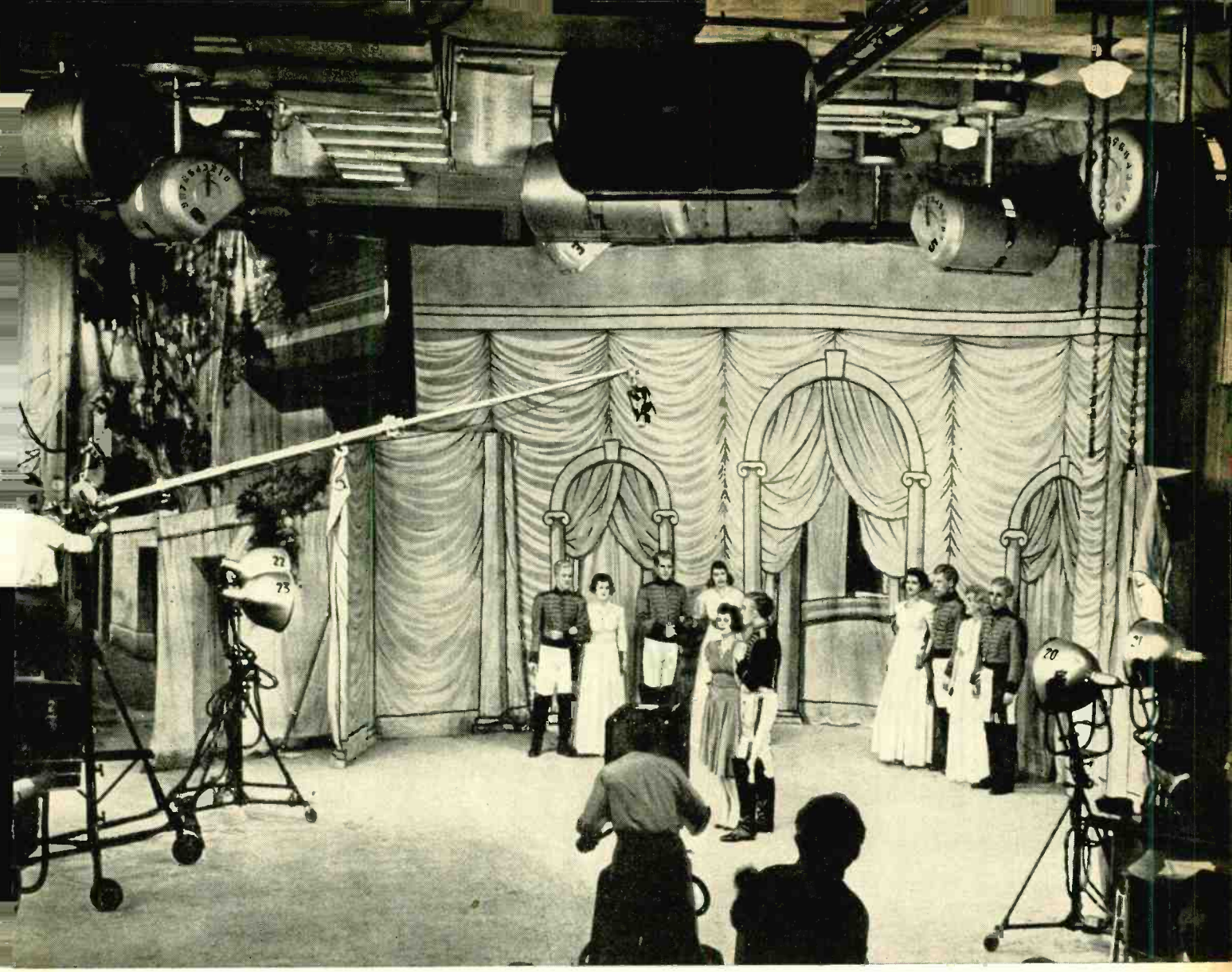
and multiplying by 2

$19 \pm j_s\ 39.24 = 100 \pm j_p\ 48.5$

Therefore, if the antenna reactance of $-j142$ ohms is reduced to $-j_s39.24$ ohms by the addition of a series coil having a reactance of 102.8 ohms, the circuit will be equivalent to 100 ohms resistance in parallel with a negative reactance of 48.5 ohms. This reactance is then tuned out by a shunt coil of + 48.5 ohms reactance thus leaving the equivalent pure resistance of 100 ohms to match the feeder.

If the added series coil had a reactance of 181.24 ohms (i.e. 142 + 39.24) the effective series reactance of this, together with the antenna, would be $+j_s39.24$ ohms. The equivalent parallel reactance would also be positive and would have to be tuned out by a shunt condenser of 48.5 ohms reactance to leave the same pure resistance of 100 ohms.





Bright but cool lights now simplify live-talent programming at G-E Television Station WRGB

Studio lighting bright as daylight . . . and cool

An Example of General Electric's Complete Service to Radio and Television Broadcasters

Once television actors had to work under hot studio lights that brought beads of perspiration through make-up, wilted costumes, caused discomfort, hindered good production.

Today at General Electric's proving-ground Television Station WRGB, Schenectady, made-up faces stay cool, costumes don't wilt. Excessive studio air conditioning is no longer necessary. For the handicap of high heat from studio lights is on its way to being completely licked by G-E developed, mercury-filled capillary lamps. They give illumination of daylight intensity with less than half the heat of the noonday sun. Water-cooled, and three to a unit, they have a light efficiency more than double — and heat output one-tenth — that of incandescent lamps. And one control panel aims a dozen of them, noiselessly, independently, anywhere in the studio.

These lamps that give cool studio lighting are another example of the bold research that will enable G-E electronics engineers to build improved cathode-ray scanning and picture tubes, cameras, transmitters, and other equipment for post-war television.

All this so that television may more quickly find its proper place in the peace-time scheme of things as a vital medium of public entertainment and education. . . . *Electronics Department, General Electric, Schenectady, New York.*

Tune in on Frazier Hunt and the News every Tuesday, Thursday, Saturday evenings over C.B.S. On Sunday night listen to the "Hour of Charm" over N.B.C. See newspapers for time and station.

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TUBES AT WORK

Simple Test Set For Mercury Vapor Rectifiers

By M. J. WEINER

THE USUAL DIFFICULTIES encountered with mercury vapor rectifiers can be held to a minimum if certain operating conditions are maintained. In properly designed equipment the tube temperatures are held within certain prescribed limits to avoid arc-backs. The internal tube drop, however, is a function of the filament emission and load current, and increases with the age of the tube.

Since there has been no readily available measuring equipment to check the filament emission of mercury vapor tubes, it was decided to build one in as simple a form as possible to permit routine tube tests. The test set to be described gives an indication of the tube performance by measuring the tube drop when passing rated current. The parts required are simple and few in number.

The basic circuit is shown in Fig. 1. Being a half-wave rectifier circuit with resistance load, the average voltage drop across the tube and resistor is

$$(E_T + E_{DC})\ \text{av.} = E_{max}/2\pi \int_0^{\pi} \sin \omega t\, d\omega t = 0.318\, E_{max}$$

The a-c voltmeter reads the effective value E, however, so the maximum (peak) applied voltage is

$$E_{max} = 1.414\, E$$

Substituting:

$$(E_T + E_{DC})\ \text{av.} = 0.45\, E$$

$$E_T = 0.45\, E - E_{DC}$$

For the initial calibration procedure, place a new tube in the proper socket for a preliminary warm-up period, with the plate supply off. Next, apply plate voltage and increase it until the d-c ammeter indicates the rated load current for the particular tube under test. This is 1.25 amp for a type 872 tube, and 0.5 amp for a type 866 tube. Read the d-c voltmeter connected across the resistor to get the value of E_{DC}. Read the a-c voltmeter to get the r.m.s applied voltage E. Now, subtract E_{DC} from 0.45 E to get the average tube drop E_T. Repeat for each other type of tube to be tested and record all values. (If it is desired to rate the tube in terms of peak values, multiply this result by π.)

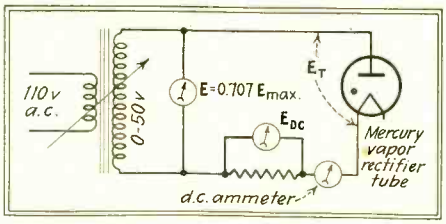


Fig. 1—Basic circuit arrangement for testing a mercury vapor rectifier tube

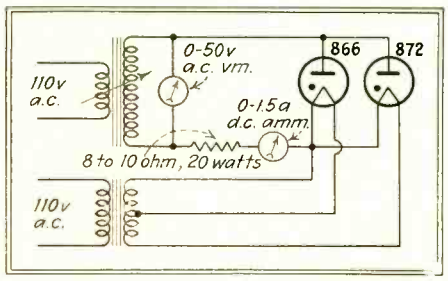


Fig. 2—Schematic circuit diagram of a simple test set for mercury vapor rectifiers. Additional sockets can be provided for other types of tubes if desired

A calibration chart can now be made up, showing the drop across the resistor at rated load current for each type of tube to be tested. The d-c voltmeter across the resistor may then be removed and this chart can be used to find the value of E_{DC} for the tube being tested.

If the tube drop E_T as measured for an old tube exceeds the drop in a new tube by 5 to 10 volts, erratic operation of the rectifier equipment will follow and the tube should be taken out of service. It may still give many hours of useful service, however, in lower-powered equipment, where the load requirements are less.

The complete schematic circuit of the test set is shown in Fig. 2. The filament voltage at each tube socket must be the exact value required for the tube under test.

The tube to be tested is placed in the correct socket and allowed to warm up with plate supply off. Plate voltage is then adjusted until the ammeter reads rated load current for the tube, and the a-c voltmeter is read to get E. Reference to the calibration chart gives E_{DC} for the rated load current, and this subtracted from 0.45 E gives the average tube drop E_T.

The equipment is calibrated in terms of the readings obtained with a new tube because the input voltage required for rated load current will vary according to the position of the d-c return lead with respect to the filament winding. For example, connecting the d-c return to the filament center-tap will not give a value of input voltage which is the means of the values obtained by connecting this lead to either side of the filament.

The variable voltage is obtained from a UTC Varitran, but the same result can of course be obtained with a fixed transformer using a primary rheostat.

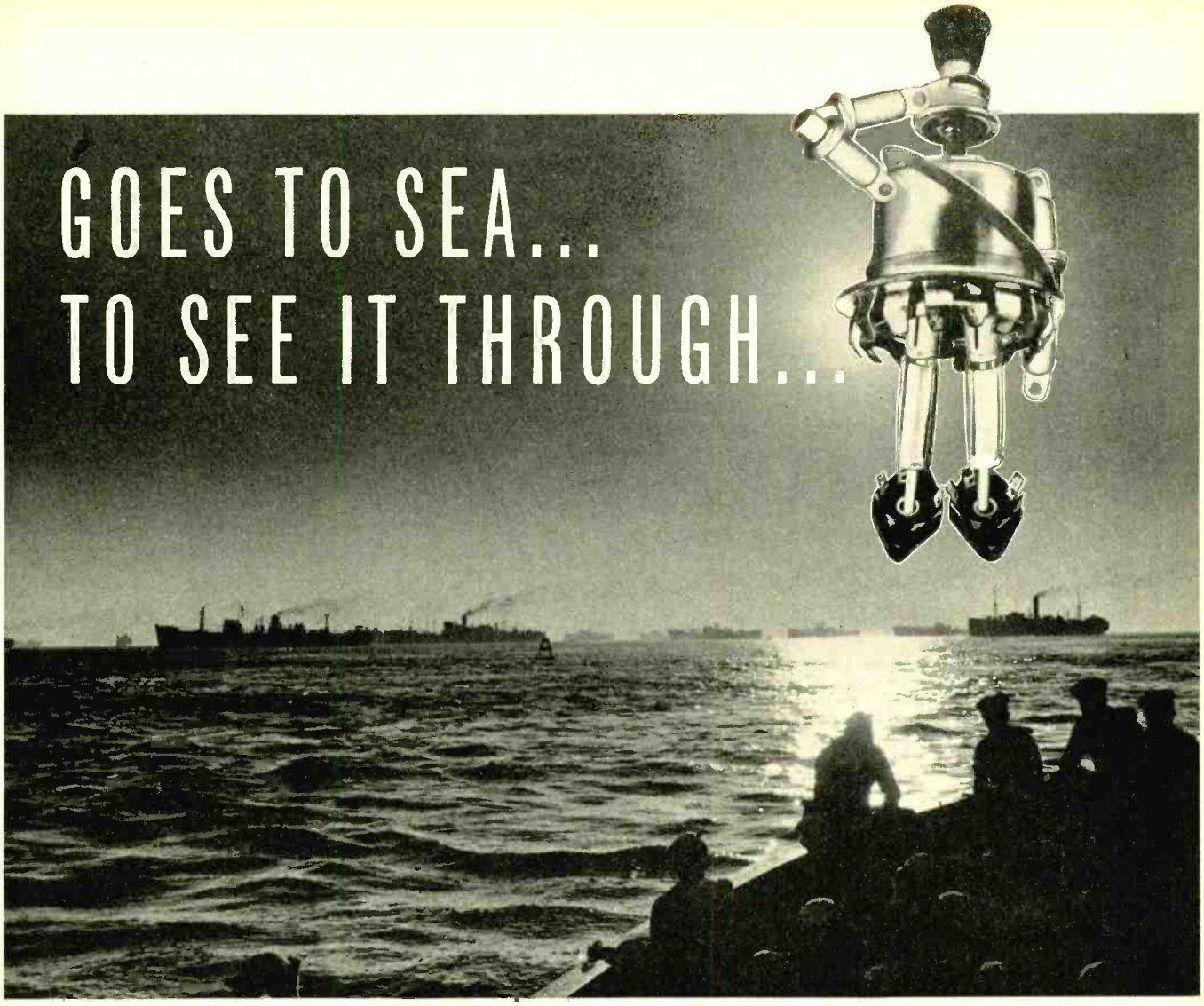
Photoelectric Manometer

By W. E. GILSON, M.D.

THE PHOTOELECTRIC membrane manometer described in the article "Applications of Electronics to Physiology" on pages 86–89 of the Jan. 1943 issue of ELECTRONICS provided a means for making an accurate record of pressure changes in the cardiovascular systems of animals such as dogs and turtles. It has since become desirable to reduce both the size and weight of the manometer.

The resulting improved manometer is shown in Fig. 1. The lens forms an image of the exciter lamp filament directly above the rubber diaphragm, with the lower part of

(Continued on page 140)



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Recording Unit for Strain and Timing Functions

(Continued from page 83)

serving of oscillograph screen and lamp box and for focusing the camera.

A diagram of the complete equipment is shown in Fig. 6. The various units are set up at some distance from the machine under observation so that the machine can perform undisturbed and the recording equipment is not affected by too severe vibrations. Five hundred feet of trailing cable is available for each bridge circuit and for the gas discharge lamps. This makes it possible to take recordings from very large machines and from moving units like tractors and scrapers when they are under actual operating conditions.

Remote Control Actuator

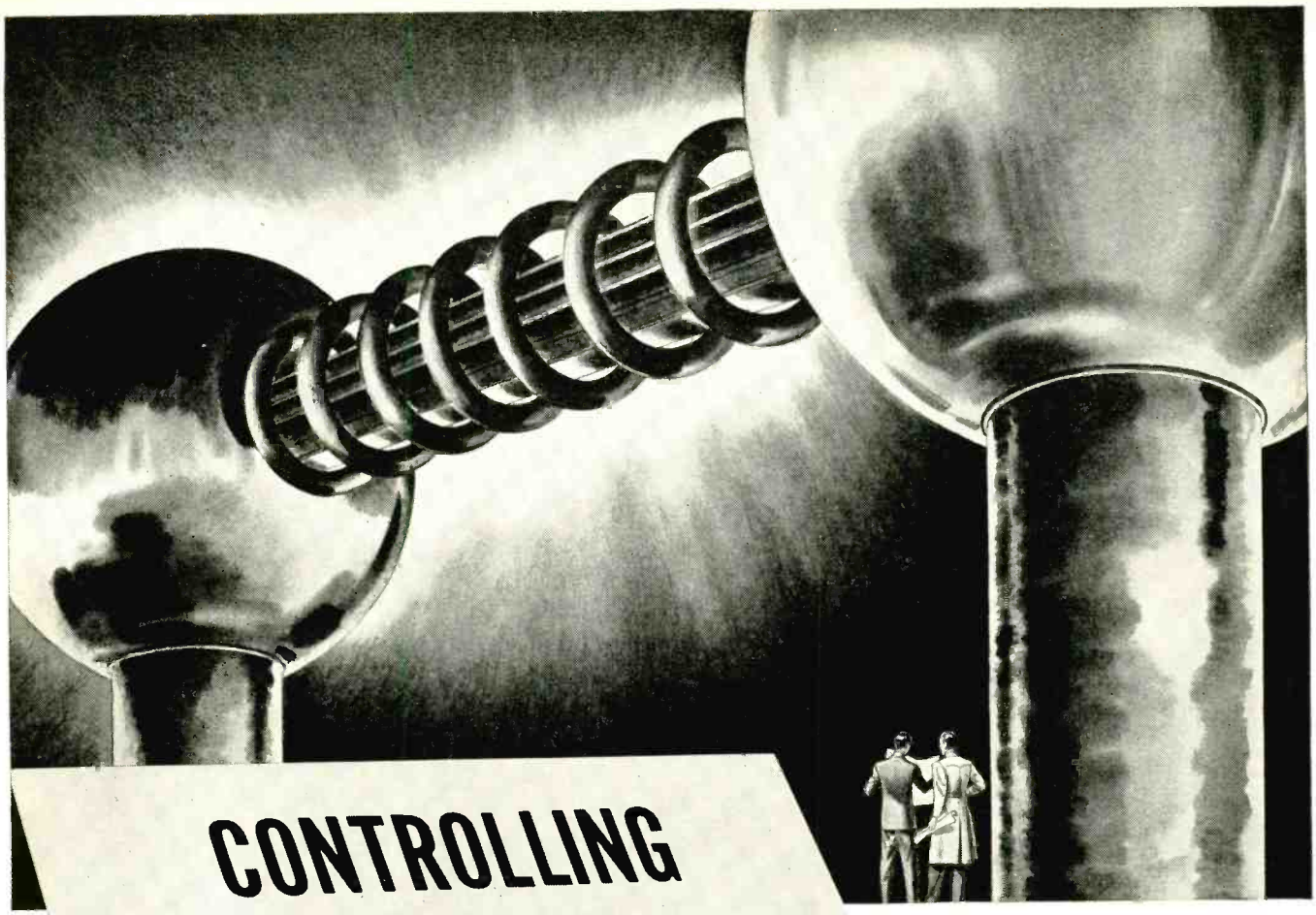
Recording is started and stopped by a six volt remote control system. It actuates the camera motor, the power supply for the discharge tubes, and a double pole relay which throws the electron beam on and off the screen of the cathode ray tube. All amplifiers are on all the time to keep filament temperature even and to make recording possible at the instant the machine under observation performs as desired. Yet, no film is wasted and the fluorescent screen of the cathode-ray tube is afforded maximum protection.

Acknowledgement

The interest of Dr. Arnold Peterson of Boston in this recording unit was greatly appreciated. He has suggested the scheme for the electronic relay and recommended changes for adapting the Thordarson amplifier for these special purposes.

The Aladdin Neon Sign Company of Milwaukee deserves thanks for cooperating in the development of the gas discharge tube.

Mr. Harry Halinton of the Electronics Sales Company of Milwaukee (now Chicago) has been very helpful in the selection and the procurement of standard equipment.



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Electron beam tube of atom-smasher.

In the vast new province of Nuclear Physics the atom-smashing "Big Guns"—the Van de Graaff generators, the cyclotrons and betatrons—are carrying on a campaign of *creative* destruction.

Manned by an army of collaborating specialists, this massive and complex artillery has already achieved spectacular results in the medical, chemical and biological fields and in scientific developments which must remain secret for the duration. The "smashing" of atoms has released new energies, created new atoms.

Despite the tremendous force required to produce high-speed electrons, protons and ions, the controls and measuring devices perform with amazing accuracy.

IRC is proud to have contributed to the development of resistor units, both Wire Wound and Metallized—of fixed and variable types—used in the measuring instruments. And IRC engineers have produced special resistors used to stabilize corona and other disturbing phenomena in atom-smashers.

If you are confronted with a problem involving resistance devices, we invite your inquiry. Our engineering staff, specialists in the design of all types of resistors, can be depended upon for impartial counsel.

PREFERRED FOR PERFORMANCE
IRC
FIXED & VARIABLE RESISTORS

INTERNATIONAL RESISTANCE COMPANY

403 N. BROAD ST., PHILADELPHIA

Rochell Salt Crystal Devices

(Continued from page 90)

One unit of this type had an output of —27 db at 5 cps.

Of particular interest is a newly developed mirror oscilloscope. This instrument is very compact and weighs less than one ounce. The unit uses a framed crystal and a novel multiplying system attached to the toggle elements in such a way that effective damping is obtained without loading the device. The high velocity elements are so small and light that virtually no inertia effects are apparent. The units developed to date have a maximum amplitude at 12-inch beam distance of approximately one-half inch, and a substantially uniform response to 5000 cps.

The photograph shows the set-up used to determine the characteristics of the oscilloscope. A conventional phototube having its output fed to the high-gain amplifier of the cathode-ray oscilloscope provides the means to determine the response and waveform characteristics of the crystal oscilloscope. Both modulated and sine-wave inputs to the crystal are provided by the beat-frequency oscillator and an audio amplifier.

Applications to Medicine

In the author's practice of osteopathic medicine he has considered the possibilities of using sound transmission and sound reflection in medical diagnosis. The several types of amplifying and recording apparatus now provided for diagnosis are confined to stethoscopic work.

During tests of the Monobar microphone in stethoscopic investigations, it was noted that the very large low frequency response of the crystal unit rendered the normal thoracic and abdominal sounds extremely clear and distinct. Further work indicated that various types of partial intestinal obstructions could be detected. Investigations also indicated that types of pneumonic consolidations and thoracic cavity complications can be detected and diagnosed. These procedures can be carried out at the bedside with a portable instrument, and if a permanent record of the findings are desirable, they can be made.

The author has made only a be-

one style case...

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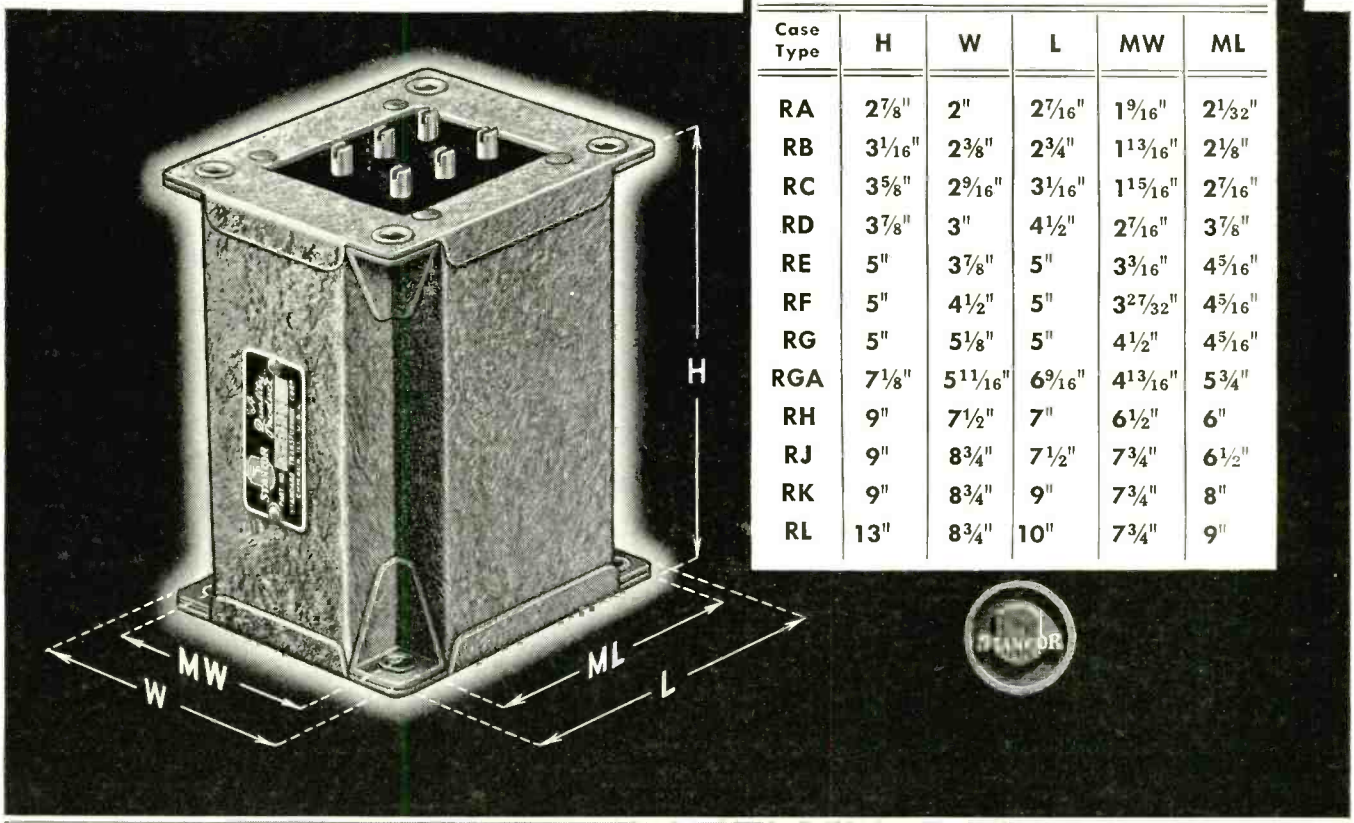

DIMENSIONS
Professional Series Transformers

Case Type	H	W	L	MW	ML
RA	2 7/8"	2"	2 7/16"	1 9/16"	2 1/32"
RB	3 1/16"	2 3/8"	2 3/4"	1 13/16"	2 1/8"
RC	3 5/8"	2 9/16"	3 1/16"	1 15/16"	2 7/16"
RD	3 7/8"	3"	4 1/2"	2 7/16"	3 7/8"
RE	5"	3 7/8"	5"	3 3/16"	4 5/16"
RF	5"	4 1/2"	5"	3 27/32"	4 5/16"
RG	5"	5 1/8"	5"	4 1/2"	4 5/16"
RGA	7 1/8"	5 11/16"	6 9/16"	4 13/16"	5 3/4"
RH	9"	7 1/2"	7"	6 1/2"	6"
RJ	9"	8 3/4"	7 1/2"	7 3/4"	6 1/2"
RK	9"	8 3/4"	9"	7 3/4"	8"
RL	13"	8 3/4"	10"	7 3/4"	9"

STANCOR

ginning in what appears to be a new approach to the diagnosis of a number of diseases and their complications. Work by another investigator covers a new approach to the diagnosis of disease by the interpretation of pulse wave propagation along an artery. This worker has used two pressure-operated crystal microphones at two points along the course of the artery, feeding the output of the two microphones into suitable recording apparatus.

It is perhaps not too much to say that by the recording of contractions of the various portions of the human body, and by sound transmission and reflections technique, using piezo-electric sound generation and detecting devices, we may be led to a better understanding of certain diseases and their earlier and surer diagnosis and treatment.

Altogether the Monobar developments present a promising picture. The known applications of the new piezo-electric device together with its potential possibilities in new fields, and its many basic points of superiority over other systems, lead us to believe that we really "have something".

• • •

SOUND EFFECTS TECHNICIANS

The National Broadcasting Company in Hollywood is training women as sound effects technicians to replace the men who have been called into the Armed forces. Harry Saz is shown explaining the technique of manipulating coconut shells in such a manner that they sound like horses walking, trotting or galloping

Full Wave Rectifier

(Continued from page 97)

where A_o and C_o are arbitrary real constants. The particular integral due to the voltage function $E_m \sin(\omega t + \Phi)$ is readily obtained from the equation

$$i_b = \frac{(1 + R_2^2C^2\omega^2)^{1/2} \quad E_m \sin(\omega t + \phi)}{(LcR_2)\,p^2 + (R_1R_2C + L)\,p + (R_1 + R_2)}$$

by letting $p = j\omega$. This yields the result

$$i_b = YE_m \sin(\omega t + \mu) \qquad (15)$$

where Y and μ are given in the body of the paper. The second particular integral is determined from the equation

$$i_c = \frac{-E_o}{(LcR_2)p^2 + (R_1R_2C + L)p + (R_1 + R_2)}$$

by letting $p = 0$. This gives

$$i_c = \frac{-E_o}{R_1 + R_2} = I_c \qquad (16)$$

whence the complete solution of the current is

$$i = YE_m \sin(\omega t + \mu) + \epsilon^{-\alpha t}[A_o \cos \psi t + C_o \sin \psi t] + I_c \qquad (4)$$

Appendix II

The current i_1 can be expressed by the Fourier series:

$$x_t = I_{dc} + I_1 \cos\left(\frac{2\pi}{T}\right)t + I_2 \cos 2\left(\frac{2\pi}{T}\right)t + \ldots I_n \cos n\left(\frac{2\pi}{T}\right)t + I'_1 \sin\left(\frac{2\pi}{T}\right)t + I'_2 \sin 2\left(\frac{2\pi}{T}\right)t + \ldots I'_n \sin n\left(\frac{2\pi}{T}\right)t \qquad (17)$$

The value I_n and I'_n resulting from integration of Eq. (6) and (7), and which express the coefficient of the cosine and sine terms in the above equation are as follows:

$$\begin{aligned} I_n = {} & 4fYE_m\{\cos\mu[A'_1 + A_1 - A'_2 - A_2] \\ & + \sin\mu[B'_2 + B_2 - B'_1 - B_1]\} \\ & + \frac{2fA_o}{\alpha^2 + K^2}\Big\{S_2[-\alpha C_2 + KD_2] \\ & - S_1[-\alpha C_1 + K_1D_1]\Big\} \\ & + \frac{2fA_o}{\alpha^2 + K_1^2}\Big\{S_2[-\alpha C'_2 + K_1D'_2] \\ & - S_1[-\alpha C'_1 + K_1D'_1]\Big\} \\ & + \frac{2fC_o}{\alpha^2 + K^2}\Big\{S_2[-\alpha D_2 - KC_2] \\ & + S_1[\alpha D_1 + KC_1]\Big\} \\ & + \frac{2fC_o}{\alpha^2 + K^2_1}\Big\{S_2[-\alpha D'_2 - K_1C'_2] \\ & + S_1[\alpha D'_1 + K_1C'_1]\Big\} \qquad (18) \end{aligned}$$

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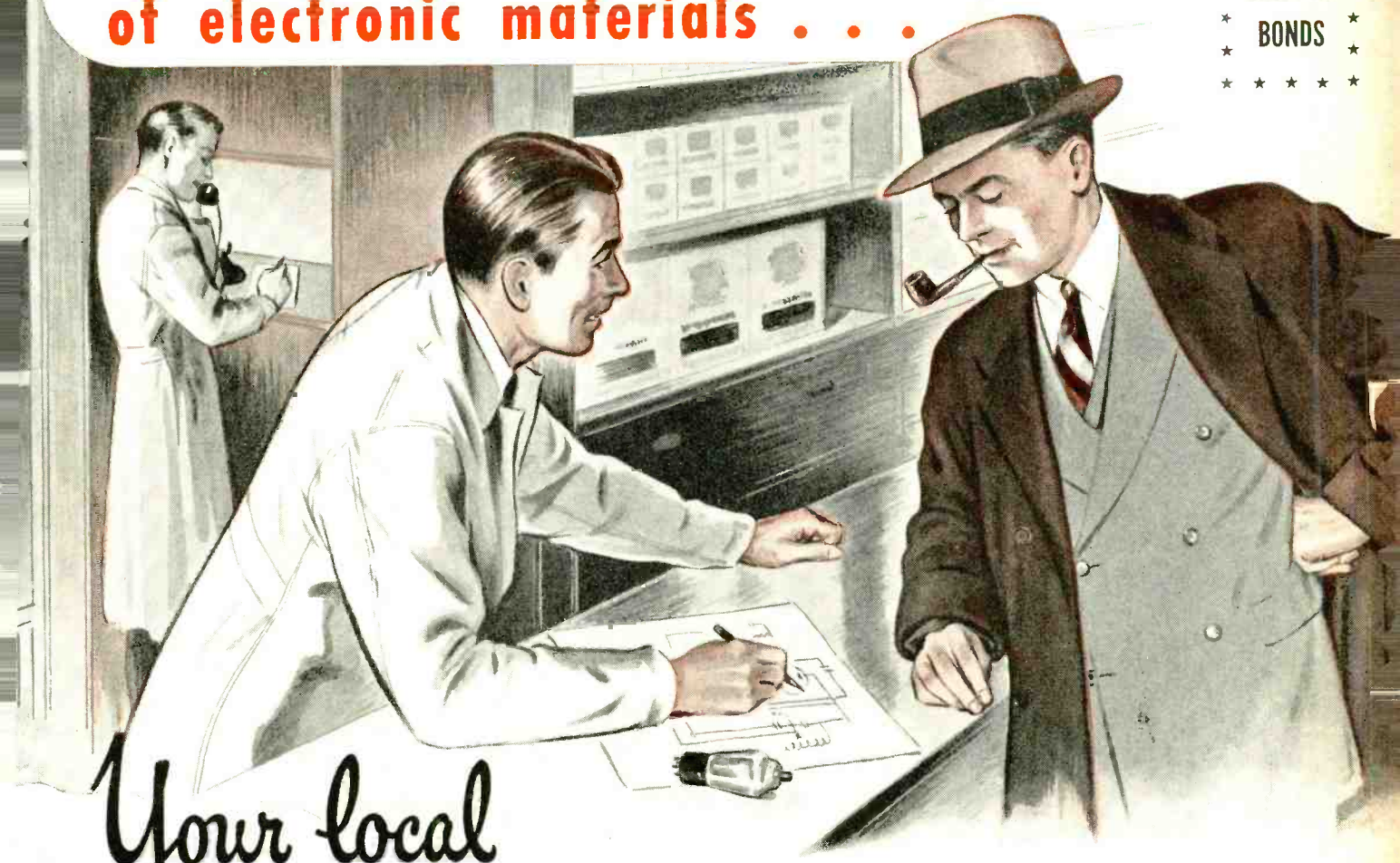

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He may have just what you need in stock for immediate delivery upon receipt of a suitable priority. If he doesn't, he is well equipped to get it for you as fast as circumstances permit—and to render an intelligent, personalized expediting service all along the line.

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AN ADVERTISEMENT OF THE RCA TUBE AND EQUIPMENT DIVISION IN THE INTEREST OF GREATER SERVICE AND EFFICIENCY IN PRIORITY-COVERED WAR MATERIALS BUYING

$$
\begin{aligned}
I'_n = {} & 4fYE_m\{\cos\mu[B'_2 - B_2 - B'_1 + B_1] \\
& + \sin\mu[A'_2 - A_2 + A_1 - A'_1]\} \\
& + \frac{2fA_o}{\alpha^2 + K^2}\Big\{S_2[-\alpha D_2 - KC_2] \\
& - S_1[-\alpha D_1 - KC_1]\Big\} \\
& + \frac{2fA_o}{\alpha^2 + K_1^2}\Big\{S_2[\alpha D'_2 + K_1C'_2] \\
& - S_1[\alpha D_1' + K_1C_1']\Big\} \\
& + \frac{2fC_o}{\alpha^2 + K_1^2}\Big\{S_2[-\alpha C'_2 + K_1D'_2] \\
& - S_1[-\alpha C_1' + K_1D_1']\Big\} \\
& + \frac{2fC_o}{\alpha^2 + K^2}\Big\{S_2[-\alpha C_2 + KD_2] \\
& - S_1[-\alpha C_1 + KD_1]\Big\} \qquad (19)
\end{aligned}
$$

where

$$A_1 = \frac{\cos(1+2n)\theta_1}{2(1+2n)\omega};$$

$$A_1' = \frac{\cos(1-2n)\theta_1}{2(1-2n)\omega};$$

$$A_2 = \frac{\cos(1+2n)\theta_2}{2(1+2n)\omega};$$

$$A'_2 = \frac{\cos(1-2n)\theta_2}{2(1-2n)\omega};$$

$$B_1 = \frac{\sin(1+2n)\theta_1}{2(1+2n)\omega_1};$$

$$B_1' = \frac{\sin(1-2n)\theta_i}{2(1-2n)\omega_1};$$

$$B_2 = \frac{\sin(1+2n)\theta_2}{2(1+2n)\omega_2};$$

$$B_2' = \frac{\sin(1-2n)\theta_2}{2(1-2n)\omega_2};$$

$$C_1 = \cos(\psi + 2n\omega)\frac{\theta_1}{\omega};$$

$$C_1' = \cos(\psi - 2n\omega)\frac{\theta_1}{\omega};$$

$$C_2 = \cos(\psi + 2n\omega)\frac{\theta_2}{\omega};$$

$$C'_2 = \cos(\psi - 2n\omega)\frac{\theta_2}{\omega};$$

$$D_1 = \sin(\psi + 2n\omega)\frac{\theta_1}{\omega};$$

$$D'_1 = \sin(\psi - 2n\omega)\frac{\theta_1}{\omega};$$

$$D_2 = \sin(\psi + 2n\omega)\frac{\theta_2}{\omega};$$

$$D'_2 = \sin(\psi - 2n\omega)\frac{\theta_2}{\omega};$$

$$S_1 = \epsilon^{-\frac{\alpha\theta_1}{\omega}}$$

$$S_2 = \epsilon^{-\frac{\alpha\theta_2}{\omega}}$$

$$K = (\psi + 2n\omega)$$

$$K_1 = (\psi - 2n\omega)$$

Appendix III

Referring to Fig. 2b, the voltage e across the filter input terminals can be expressed as the Fourier series

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$$e = \frac{E_m}{\pi}\left[1 - \frac{2}{3}\cos 2\omega t - \frac{2}{15}\cos 4\omega t - \frac{2}{35}\cos 6\omega t \ldots\right] - E_o \quad (20)$$

Considering only the components of current due to the dc and second harmonic of the voltage e, the current through the choke can be expressed as

$$i = \left[\frac{2/\pi E_m - E_o}{R_1 + R_2}\right] + \left[\frac{4\,E_m}{3\pi\,(X_L - X_c)}\right]\cos 2\,\omega t + \quad (21)$$

where X_L and X_c are the reactances of the filter choke and condenser to the second harmonic. If the current wave just grazes the zero axis at some point in its period T, then the d-c and peak value of the a-c component must be equal. Equating these two terms given in Eq. (21) and solving for the critical inductance gives

$$L_c = \frac{1}{\omega}\left[\frac{2\,(R_1 + R_2)}{3\,K} + \frac{1}{4\,C\omega}\right] \quad (22)$$

where

$$K = \left(2 - \frac{\pi\,E_c}{E_m}\right)$$

Appendix IV

For non cut-off operation where $\theta_1 = 0$ and $\theta_2 = \pi$ the value of I_n and I'_n evaluated by Eq. (6) and Eq. (7) are:

$$I_n = 4fYE_m\left\{\cos\mu\,[A'_1 + A_1 - A'_2 - A_2]\right\} + \frac{2fA_o}{\alpha^2 + K_1^2}\left\{S_2[-\alpha C'_2 + K_1 D'_2] + \alpha\right\} + \frac{2fA_o}{\alpha^2 + K^2}\left\{S_2[-\alpha C_2 + KD_2] + \alpha\right\} + \frac{2fC_o}{\alpha^2 + K^2}\left\{S_2[-\alpha D_2 - KC_2] + K\right\} + \frac{2fC_o}{\alpha^2 + K_1^2}\left\{S_2[-\alpha D'_2 - K_1 C'_2] + K_1\right\}$$

$$I_n{}' = -4fYE_m \sin\mu[-A'_2 + A_2 + A'_1 - A_1] + \frac{2fA_o}{\alpha^2 + K^2}\left\{S_2[-\alpha D_2 - KC_2] + K\right\} + \frac{2fA_o}{\alpha^2 + K_1^2}\left\{S_2[\alpha D'_2 + K_1 C'_2] - K_1\right\} + \frac{2fC_o}{\alpha^2 + K_1^2}\left\{S_2[-\alpha C'_2 - K_1 D'_2] + \alpha\right\} + \frac{2fC_o}{\alpha^2 + K^2}\left\{S_2[-\alpha D'_2 - K_1 C'_2] + \alpha\right\} \quad (24)$$

where

$$A_1 = \frac{1}{2(1 + 2n)\,\omega}\,;$$

$$C_2 = \cos\left(\frac{\psi + 2n\omega}{2f}\right);$$

$$K = (\psi + 2n\omega)$$

$$A'_1 = \frac{1}{2(1 - 2n)\omega}\,;$$

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$$K_1 = (\psi - 2n\omega)$$

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$$D_2 = \sin\left(\frac{\psi + 2n\omega}{2f}\right);$$

$$S_2 = \epsilon^{-\frac{a}{2f}}$$

$$A'_1 = \frac{-1}{2(1-2n)\omega};$$

$$D'_1 = \sin\left(\frac{\psi - 2n\omega}{2f}\right);$$

Appendix V

Applying the first two boundary conditions to Eq. (4) results in the following two equations for i_1 and di_1/dt at $\omega t = \theta_1$

$$i_1 = 0 = YE_m \sin(\theta_1 + \mu) + I_e + \epsilon^{-\frac{\alpha\theta_1}{\omega}}\left[A_o \cos\frac{\psi\theta_1}{\omega} + C_o \sin\frac{\psi\theta_1}{\omega}\right] \quad (25)$$

$$\frac{di_1}{dt} = 0 = Y\omega E_m \cos(\theta_1 + \mu) + \epsilon^{-\frac{\alpha\theta_1}{\omega}}\left[(C_o\psi - \alpha A_o)\cos\frac{\psi\theta_1}{\omega} - (A_o\psi + \alpha C_o)\sin\frac{\psi\theta_1}{\omega}\right] \quad (26)$$

Solving for A_o and C_o

$$A_o = \frac{D_1(\psi S_2 - \alpha S_1) - D_2 S_1}{S_2(\psi S_2 - \alpha S_1) + S_1(\alpha S_2 + \psi S_1)} \quad (27)$$

$$C_o = \frac{D_2 S_2 + D_1(\alpha S_2 + \psi S_1)}{S_2(\psi S_2 - \alpha S_1) + S_1(\alpha S_2 + \psi S_1)} \quad (28)$$

where

$$S_1 = \epsilon^{-\frac{\alpha\theta_1}{\omega}} \sin\frac{\psi\theta_1}{\omega};$$

$$D_1 = I_e - YE_m \sin(\theta_1 + \mu)$$

$$S_2 = \epsilon^{-\frac{\alpha\theta_1}{\omega}} \cos\frac{\psi\theta_1}{\omega};$$

$$D_2 = -Y\omega E_m \cos(\theta + \mu)$$

Imposing condition 4 to Eq. (4) gives

$$0 = YE_m \sin(\theta_2 + \mu) + I_e + \epsilon^{-\frac{\alpha\theta_2}{\omega}}\left[A_o \cos\frac{\psi\theta_2}{\omega} + C_o \sin\frac{\psi\theta_2}{\omega}\right] \quad (29)$$

The value of the (di_1/dt) at $\omega t = \theta_2$ is given by Eq. (26) except that θ_1 is replaced by θ_2. This is not equal to zero for $\omega t = \theta_2$.

The procedure in solving for θ_1 and θ_2 is as follows. A value of θ_1 is assumed and A_o and C_o are calculated. On the basis of these values, θ_2 is calculated by Eq. (29). A check on the accuracy of the assumed value of θ_1 is condition 3, namely that

$$E_m \sin\theta_1 - E_o = V^1 \epsilon^{-\frac{\pi - \theta_2 + \theta_1}{R_2 C\omega}} \quad (30)$$

where

$$V^1 = E_m \sin\theta_2 - E_o - L'\left(\frac{di}{dt}\right)_{\theta_2}$$

f the right-hand side of Eq. (30) is less than the left-hand side, the assumed value of θ_1 is too large, and vice versa.

Self Biased Amplifiers

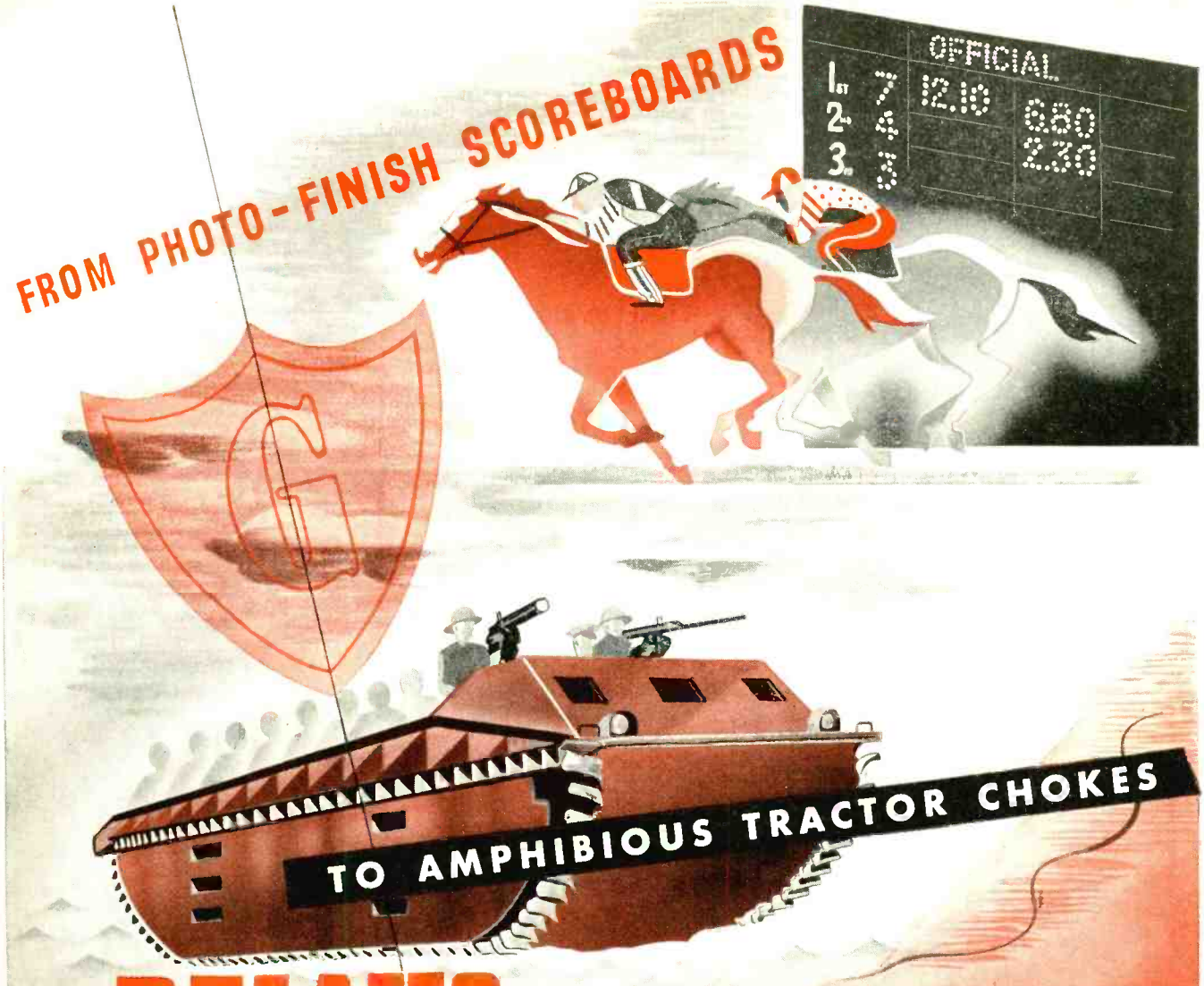
(Continued from page 103)

the final step in the analysis. The value of the bias voltage will depend upon the value of the bias resistor and its location in the circuit. It will also depend upon the average grid current in the case of grid bias or upon the average cathode current in the case of cathode bias. For triodes, the cathode current is the sum of the grid and plate currents. Accordingly, the next step in the analysis is to determine the average value of the grid bias voltage for the possible methods of resistance bias. To determine this bias voltage, we must first determine the average current, flowing through the bias resistance. If it is entirely in the grid circuit we are interested in determining only the grid current whereas if it is in the cathode circuit, both grid and plate current must be known.

To determine the average currents we use paths of operation such as the one mapped out between Q' and A', Fig. 6. We may select the Q points for these paths at regular intervals in the region defined by the red curves of Fig. 6. In the present calculation these points were selected at the intersection of lines drawn at 50 volt intervals through the grid axis and 100 volt intervals through the plate axis. The paths of operation for each of these Q points were drawn in accordance with the previous discussion. After the paths have been determined, the calculation of the current follows. This calculation is greatly facilitated through the use of a plastic calculating device described in an earlier article.[16] After obtaining the average currents they may be plotted as a function of the grid polarizing voltage for constant values of the plate polarizing potential. These polarizing voltages correspond, of course, to the coordinates of Q for which a given current calculation was made.

Bias Resistance in the Grid Circuit

When the bias resistance is in the grid circuit, it is only necessary to calculate, for the various paths of operation chosen, the average grid current I_{ca}. This is plotted as a func-



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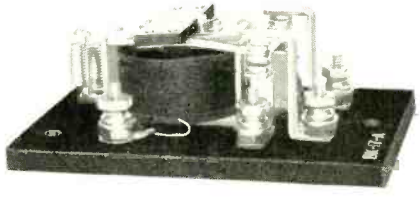

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tion of E_{cc} on Fig. 7, for various values of plate polarizing potential E_{bb}. From this figure we can determine the locus followed by Q on the e_b-e_c diagram for any given grid biasing resistance in the following way. Since the bias resistance is entirely in the grid circuit, the grid polarizing potential is given by

$$E_{cc} = I_{ca} R_{cc}$$

where R_{cc} is the grid resistance. This equation, when plotted on the I_{ca}—E_{cc} diagram, appears as a straight line passing through the origin, having a slope equal to $1/R_{cc}$. Two such lines corresponding to two values of R_{cc} are shown on Fig. 7. The intersections of one of these lines with the lines of constant plate voltage determines the grid polarizing potentials which must be developed across R_{cc} for the given grid excitation voltage, and equivalent plate resistance $(R_b)\omega$ which were chosen and fixed for this calculation. These intersections may be plotted on the e_b-e_c plane, and thus determine the locus of the Q point during the modulation cycle for this value of grid resistance. When this locus has been obtained, the calculation of the complete dynamic characteristics may proceed directly. A number of Q points are selected, evenly spaced, along this locus. For each of these Q points the coordinates of the A points are defined. The horizontal distance from Q to A is given by the grid excitation, the vertical distance from Q down to A is given by the red curves of Fig. 6. Thus the paths of operation for any Q on the locus are obtained. For these paths the average grid current, average plate current, fundamental grid current, and fundamental plate current may be calculated using the plastic device referred to above. Knowing these currents together with E_{bb}, E_{cc}, E_{g1m}, E_{p1m}, and R_{cc}, the power relations in the modulator may be calculated from the relations:

Driving power, $P_d = \frac{1}{2} I_{g1m} E_{g1m}$

Power input, $P_B = I_{ba} E_{bb}$

Power output. $P_b = \frac{1}{2} I_{p1m} E_{p1m}$

Power delivered to grid resistor, $P_{rcc} = I^2_{ca} R_{cc} = I_{ca} E_{cc}$

Grid dissipation, $P_g = P_d - I_{ca} E_{cc}$

Plate dissipation, $P_p = P_B - P_b$

Determination of these quantities for each of the Q points selected along the locus gives the complete dynamic characteristics of the modulator. Other characteristics may be

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obtained by selecting a different value of R_{cc}, and a family of dynamic characterists showing the effect of a variation of this parameter may be calculated.

Bias Resistance in both the Plate and Grid Circuits Cathode Bias

When the bias resistance is in both the plate and grid circuits, it is necessary to calculate both the average grid current I_{ca} and the average plate current I_{ba} for the various paths of operation. The sum of these currents $(I_{ba} + I_{ca})$ may then be plotted as a function of E_{co} for the various values of E_{bb} selected. Lines of constant cathode resistance $R_{bc} = E_{cc}/(I_{ba} + I_{ca})$ may be drawn on this diagram and will appear as straight lines. The intersection of any one of these straight lines with the lines of constant plate voltage E_{bb} will determine the coordinates of the path followed by Q during the modulation cycle, on the e_b-e_c diagram. When this locus of Q is found for the desired cathode resistance, the remaining problem of obtaining the dynamic characteristics for the modulator is again, straight-forward. With any point on this path as a Q point, the coordinates of the end point for the path of operation passing through this Q are known as in the preceding case. That is, the horizontal coordinate of A is given by the grid excitation, as measured from Q, and the vertical coordinate of A is given by the red curve passing through this Q. This vertical coordinate will be given in terms of the maximum fundamental plate voltage, E_{p1m}, of course, and thus will represent the vertical distance in volts below Q to the point A. Hence we may calculate for the path joining this Q and A the fundamental plate and grid currents from which may be determined, together with the average plate and grid current which we already know, all the dependent variables associated with this condition of operation. By repeating this process for other selected Q points along this locus, the complete dynamic characteristics of the modulator are determined. These dynamic characteristics apply, of course, only for the specific cathode resistance chosen. Families of characteristics may be obtained by choosing other values of cathode resistance, as in the case discussed pre-

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viously. The power relations in the modulator are slightly modified by the cathode resistor. The quantities P_d, P_b, P_B, and P_g are the same but the other relations are

Power delivered to cathode resistor,
$$P_{bc} = (I_{ba} - I_{ca})^2 R_{bc}$$
Plate dissipation,
$$P_p = P_B - P_b - I_{ba}^2 R_{bc}$$

Bias Resistance partly in the Grid and partly in the Plate Circuits

If the biasing resistance is partly in the cathode circuit and partly in the grid circuit, the calculation is somewhat more involved. For now we are concerned with two resistances R_{cc} and R_{bc} instead of only one. Here the grid polarizing voltage is given by

$$E_{cc} = I_{ca} R_{cc} + (I_{ba} + I_{ca}) R_{bc}$$

Let us set

$$R_{cc} = k R_{bc}$$

where k is a positive constant greater than zero. Then

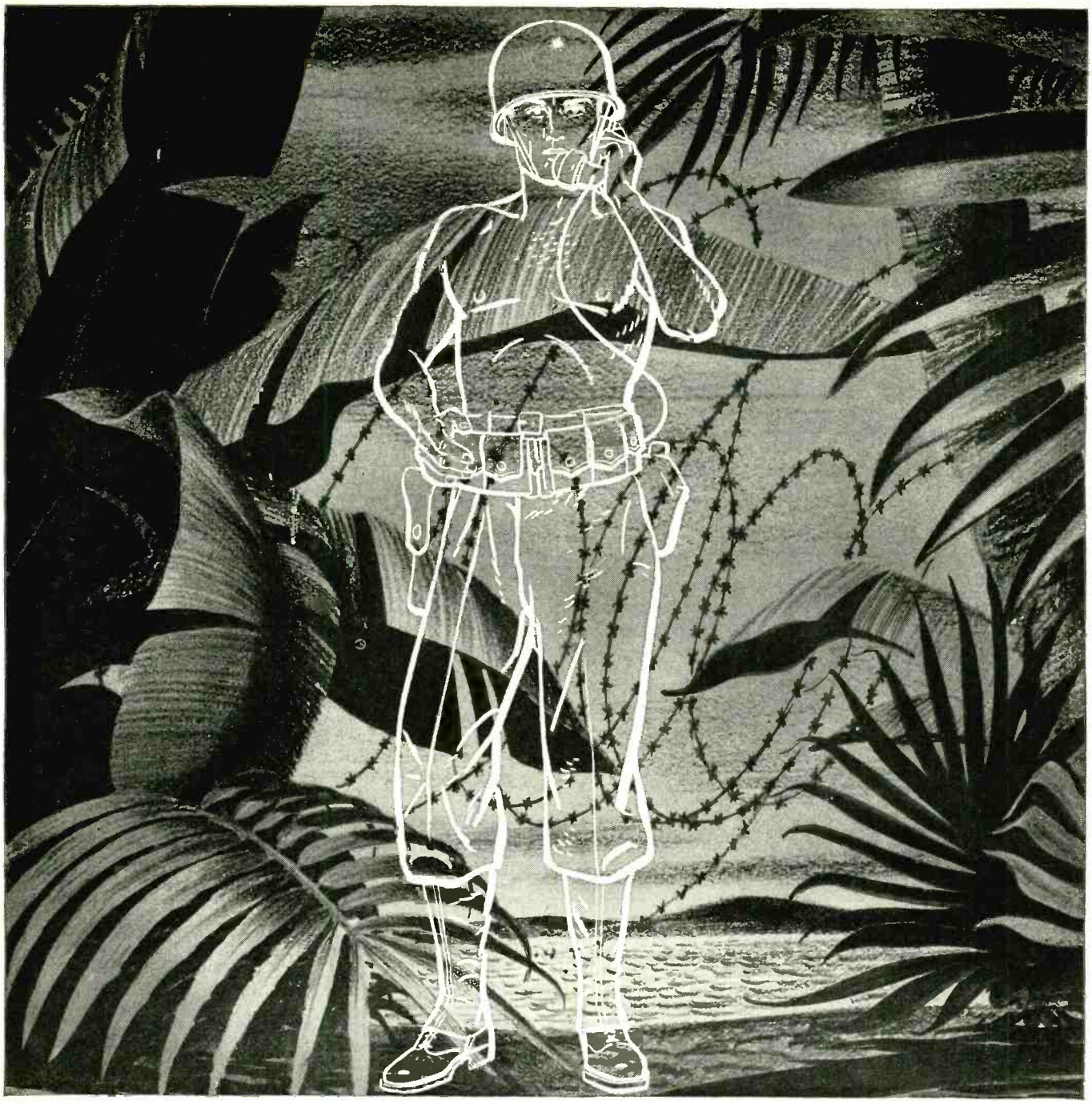
$$E_{cc} = \left\{ I_{ba} + (1 + k) I_{ca} \right\} R_{bc}$$

and the polarizing grid voltage is again expressed in terms of only one resistor. It is, therefore, evident that if $I_{ba} + (1 + k) I_{ca}$ is plotted as a function of E_{cc} we will be able to determine the path followed by Q in a manner similar to that used in the case of grid bias alone or plate bias alone. An example of this plot when $k = 9$ is shown in Fig. 8. The intersections of line $R_{bc} = 266$ ohms with the lines of constant E_{bb} give the values of E_{cc} which will determine the locus of the Q point under this condition of operation. Families of characteristics may be obtained for various values of k. The power relations under this condition of operation are also modified slightly from those forms as given under grid bias operation. The quantities P_d, P_b, and P_B remain the same, but the other relations are

Power delivered to grid resistor,
$$P_{cc} = I_{ca}^2 R_{cc}$$
Power delivered to cathode resistor,
$$P_{bc} = (I_{ca} + I_{ba})^2 R_{bc}$$
Plate dissipation,
$$P_p = P_B - P_b I_{ba}^2 R_{bc}$$
Grid dissipation,
$$P_g = P_d - I_{ca}^2 R_{cc} - I_{ca}^2 R_{bc}$$

Part Generators and Part Resistance Bias

In the case of part battery and part resistance bias the lines for constant resistance may be drawn on



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any of these average current versus grid voltage diagrams depending on the location of the bias resistance. The procedure is to draw the lines of constant biasing resistance through the zero current axis at the value of E_{cc} corresponding to the battery voltage. The intersection of this line with the lines of constant plate voltage determine the path, as in the previous cases.

Characteristics of Various Bias Methods

Since the locus of Q can be found for any combination of self biasing or battery and resistance biasing combination, a complete solution of the problem is at hand. The effect on this locus of different conditions of service are shown in Fig. 9. This illustrates the paths followed by the Q point on the e_b-e_c plane during the modulation cycle for three different types of biasing. Curve A is for cathode bias alone, curve B is for battery bias alone, and curve C is for grid resistance bias alone. The system is here adjusted for equivalent carrier conditions in order to make the comparison of the different types of biasing more effective. Curve C, which is shown below to be the most desirable, may be obtained by part battery and part grid resistance bias, or part cathode resistance and part grid resistance bias.

The effect on the dynamic modulation characteristics for these three paths is indicated in Fig. 10. We can see that the path C is by far the most desirable, since it improves the linearity of the modulation process, increases the power output, and reduces the driving power. Further, the driving power is less peaked, while the change in efficiency is but slightly effected. Hence, it is desirable to use grid resistance bias entirely. For tube protection, however, it is sometimes desirable to use a certain amount of generator or cathode resistance bias. Path A, for the case of cathode bias alone, gives most unfavorable results, reducing the linearity while, at the same time, increasing the grid driving power and reducing the power output and efficiency. However, it is found that by using an amount of cathode bias sufficient to protect the tube, and the remaining bias supplied by the grid current alone, it is possible to approximate the condition indicated in C with only a slight sacrifice in efficiency. Or if part battery bias and

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The Charles Parker Co., Meriden, Conn.
Parker-Kalon Corp., New York, N. Y.
Pawtucket Screw Co., Pawtucket, R. I.
Russell Burdsall & Ward Bolt & Nut Co., Port Chester, N. Y.
Reading Screw Co., Norristown, Pa.
Pheoll Manufacturing Co., Chicago, Ill.
Scovill Manufacturing Co., Waterville, Conn.
Shakeproof Inc., Chicago, Ill.
The Southington Hardware Mfg. Co., Southington, Conn.
Whitney Screw Corp., Nashua, N. H.

part grid resistance bias are used, these conditions may be approximated more easily. Complete dynamic characteristics for every condition of operation are, therefore, made available.

While the graphical method developed by Dr. Sarbacher may require graphical constructions which are too tedious for use by the operating engineer, nevertheless, a way has been shown by which the performance of self-biased, plate-modulated amplifiers can be accurately determined. It is to be hoped that the derived curves of Fig. 6 can be made available by tube manufacturers for those tubes most likely to be used as plate-modulated self-biased amplifiers.

Acknowledgments

I wish to express my appreciation to Professor E. L. Chaffee for suggesting the problem and to Professor R. P. Siskind and Mr. Beverly Dudley for most helpful criticisms and suggestions in the preparation of the text. I was aided in the calculation by my students and friends Messrs. R. K. Beach, G. G. Carne, W. R. Faust, R. E. Glass, R. M. Soria and H. J. Woll, who also contributed in the calculation of other allied problems and to whom assistance is most gratefully acknowledged.

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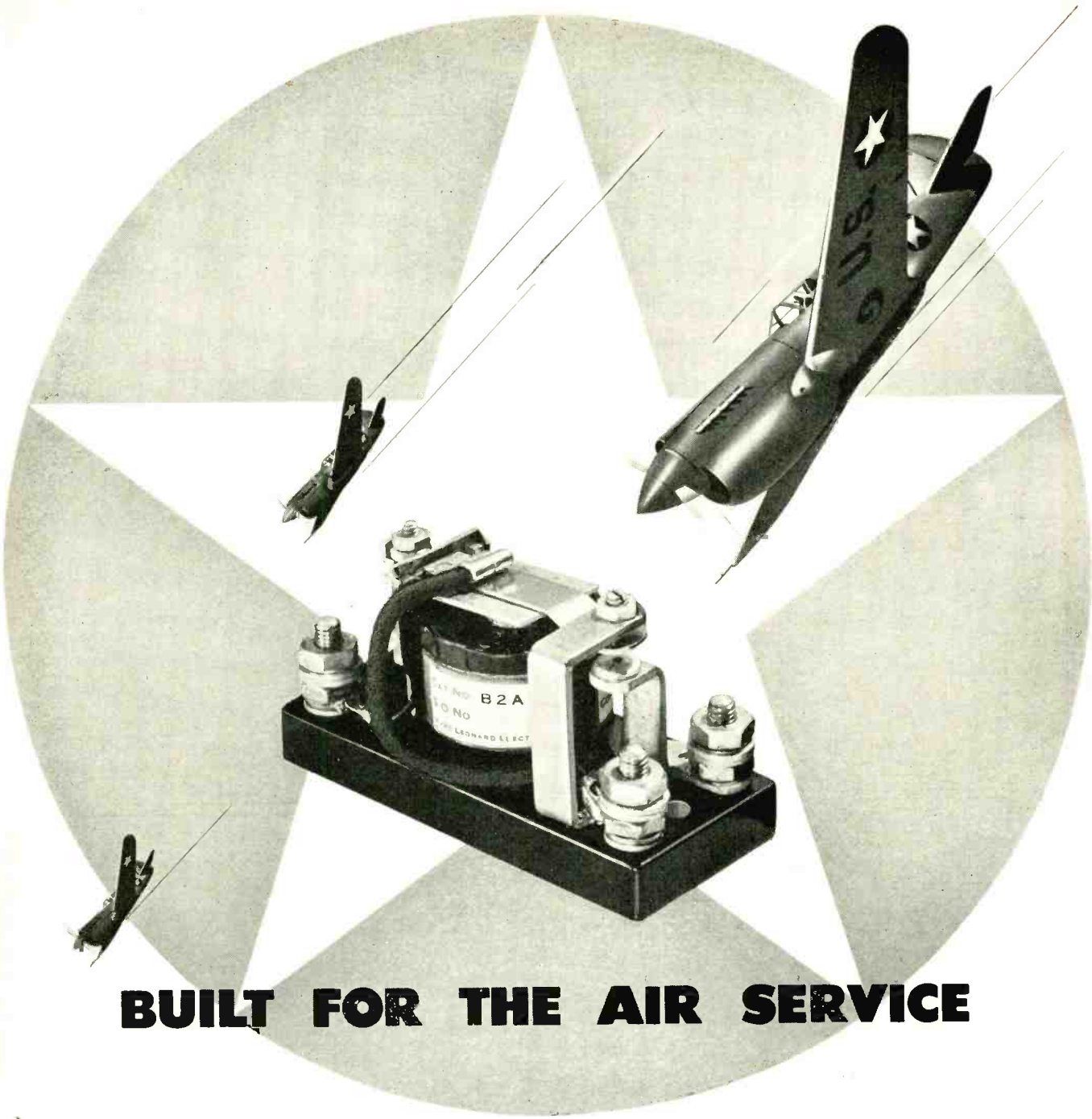

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(*Continued from page* 112)

the image falling on a small shutter of black paper attached to the diaphragm. That portion of the light beam which gets past this shutter spreads to form a diffuse spot covering practically the entire cathode area of the type CE 20 photocell.

An increase in the pressure being measured forces the diaphragm upward, moving the shutter further into the light beam and thereby darkening the spot on the photocell cathode in an approximately uniform

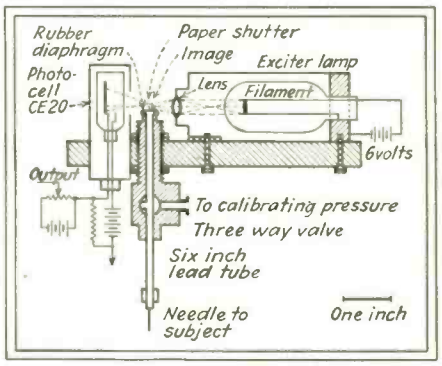

Fig. 1—Circuit and mechanical arrangement of the improved photoelectric manometer developed by Dr. W. E. Gilson for converting small variations in pressure into corresponding electrical values which can be observed on an oscilloscope screen

Fig. 2—Record of calibration, showing the linearity obtained. The pressure was decreased from 150 mm of mercury to 0 mm in 25-mm steps

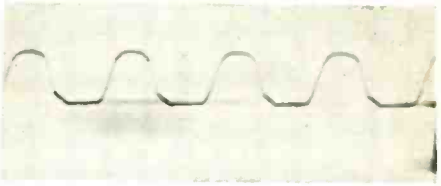

Fig. 3—Oscillogram showing the intraventricular pressure in a dog as detected by the improved electronic manometer

manner. Any nonlinearity due to nonuniform sensitivity of the cathode is thus eliminated, giving a linear calibration record as shown in Fig. 2. A comparatively large output is obtained, and is fed into a cathode-ray oscilloscope of the type described on page 22 of the Dec. 1941 issue of ELECTRONICS. This oscilloscope is now being manufactured in improved form by Clough-Brengle Co., Chicago. An example of the resulting record is shown in Fig. 3.

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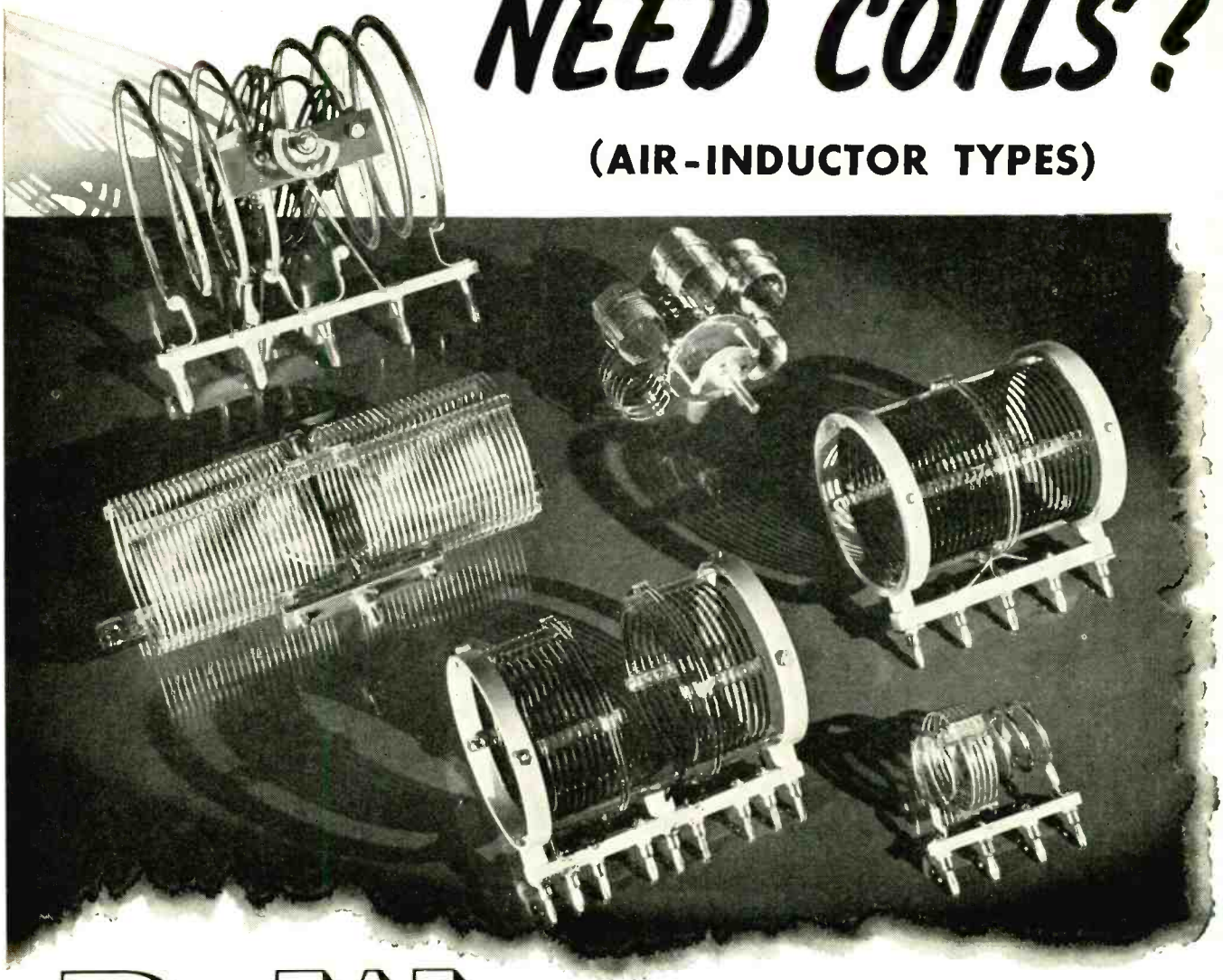

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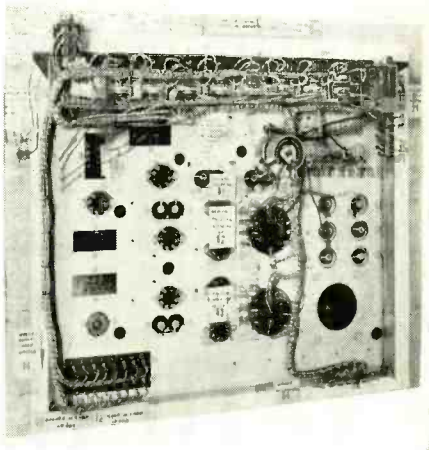
Navy Buoy Uses 45-Volt Fluorescent Lamp

A FLUORESCENT LAMP which operates at a voltage of only 45 volts is now being used by the U. S. Navy on doughnut-shaped rubber buoys which mark seaplane landing lanes at night, according to Westinghouse engineers. The low-voltage lamp eliminates the insulation difficulties which had been experienced in salty ocean atmosphere when 3000-volt luminous tubing was used.

• • •

Large Photos Teach Assembly of Intricate Amplifiers

INEXPERIENCED WOMEN are being successfully taught to assemble and wire large amplifiers at the Sound-Scriber Corp., New Haven, Conn., by means of large photographs on which parts and wires involved in only one series of operations are mounted. One giant chassis photograph (19 x 22 inches) mounted on heavy cardboard is used for each of the six consecutive steps in the complete assembly and wiring of an amplifier. Holes are drilled in each photo as required to hold only the parts actually involved in a particular step, and each operation involved in that step is numbered in correct sequence. Explanatory notes are placed alongside the numbers when necessary.



Example of a photo instruction board which shows the parts and wires involved in one sequence of operations for building an intricate amplifier. The tube sockets, T pads and filter condenser terminals are in the original photograph, while the wiring and other parts which cast shadows are mounted on the photograph

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"THE PLACE OF QUALITY AND ECONOMY"

Side Shifts of Paper Corrected in Roll-Winding Machine

PHOTOELECTRIC SIDE REGISTER controls which insure true rewinding of paper rolls at high speeds are now available as commercial units for rewinding machinery in paper mills, for web-operated printing presses, for slitting equipment, and for other types of paper machinery operating from the roll. Crosswise register can be maintained with a high degree of accuracy even though the original roll is telescoped or unevenly wound. With roll-slitting machines trim waste can be avoided by rewinding into rolls having straight ends.

The control system consists essentially of three sections: (1) The scanning head, which converts sidewise shifts of the moving paper or web into electrical impulses, (2) The amplifying system, which rectifies and amplifies the output of the scanning head to provide a suitable register current for operation of the side-shift motor, (3) The side-shifting mechanism, containing a motor, levers and screws which shift the paper and scanning rolls the correct amount in the correct direction to keep the paper running true. These three sections are identified in Fig. 1, which shows a complete installation.

Photoelectric side register controls as manufactured by Cameron Machine Co., Brooklyn, N. Y. employ two distinct types of scanning heads and amplifying sections, but all have same side-shifting mechanism.

Scanning Head

The General Electric scanning system, illustrated in Fig. 2, contains a

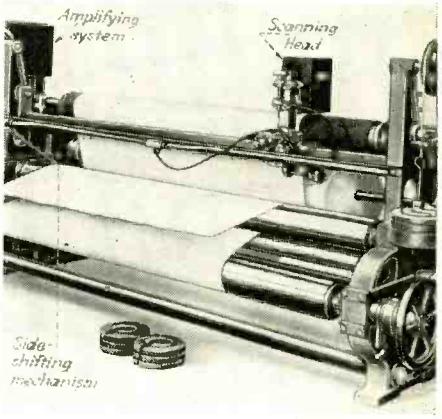


Fig. 1—Cameron photoelectric side register control installed in a web press, with the three basic sections of the control system identified

light source which projects a small spot of light onto the edge of the web of paper, in such a way that the web bisects the circle of light when running true. The light reflected from the paper is focussed onto a phototube by a collecting lens. No light is reflected from that part of the spot which falls on the dark rubber idler roll (scanning roll) over which the web passes. Sidewise shifting of the web changes the amount of light falling on the phototube, correspondingly changing its output current.

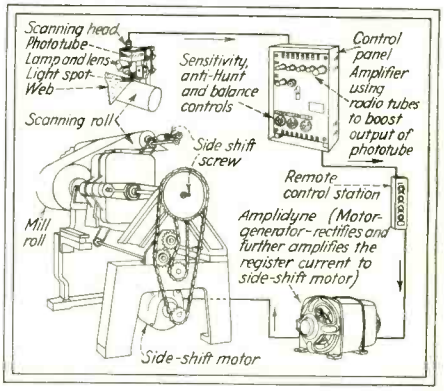


Fig. 2—Photoelectric side register control using G-E scanning and amplifying units. The control panel contains an ordinary audio amplifier as used in radio, along with necessary sensitivity, balancing and anti-hunting controls

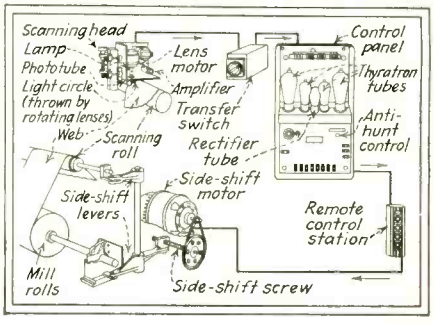
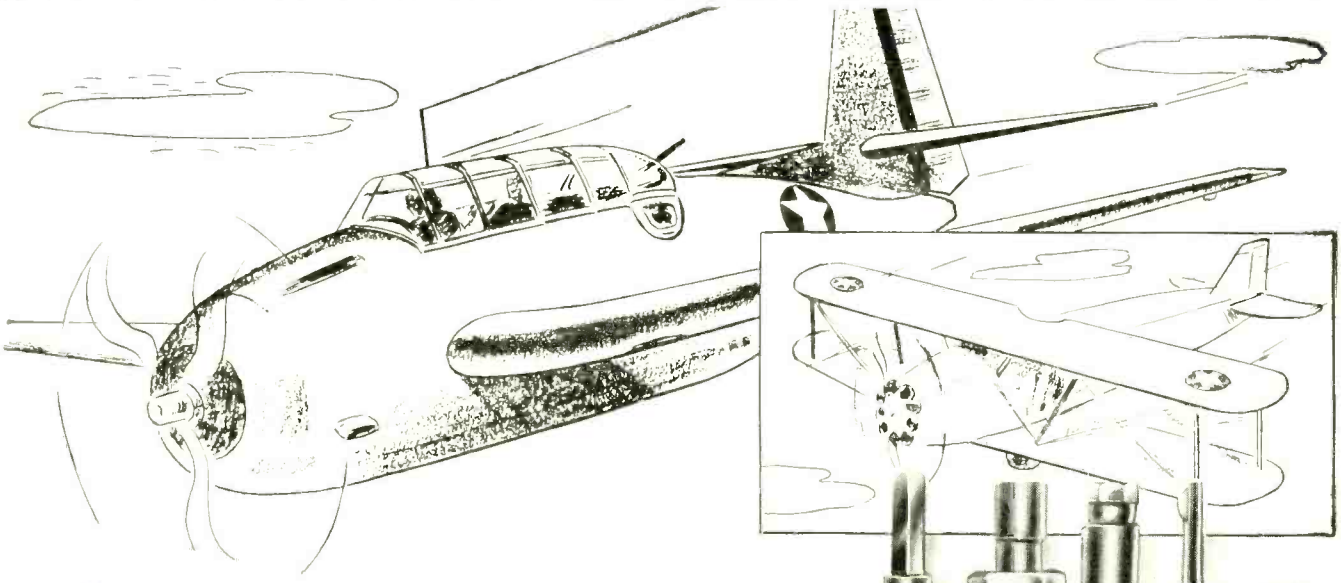


Fig. 3—Equivalent register control system using Westinghouse rotary-lens type scanning unit and thyratron amplifier. This diagram clearly shows the screw-and-lever mechanism used for shifting the rolls sideways

The Westinghouse scanning system, illustrated in Fig. 3, employs a light source and a fixed-focus rotary lens driven by a small electric motor to produce concentric circles of light on the edge of the web. The light reflected from the web is picked up by a phototube, and the output of the phototube is fed through an amplifier stage built into the scanning head.

IT'S SMART TO SIMPLIFY...



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Amplifying System

The General Electric amplifying system uses standard radio receiving tubes to boost the phototube output initially, with this unit feeding into an Amplidyne motor-generator set which rectifies and further amplifies the register current.

In the Westinghouse amplifying system, all amplification is performed by thyratron tubes, which feed the side-shift motor directly.

Side-Shifting Mechanism

The type of mechanism used to correct unevenness in a roll depends upon the size and nature of the machine, but in general consists of a side-shift motor capable of rotating a desired amount in either direction in response to the demands of the scanning head and amplifying system, and a side-shift screw which shifts the printing and scanning rolls either directly or through a lever system.

One requirement for accurate side registry control is constant web tension, which is obtained mechanically in Cameron roll-handling equipment. Under this condition, full correction can be made in a sidewise direction at the rate of 25 inches per minute. Register may be taken either from the right or left edge of the web, or from a printed line having a minimum width of $\frac{1}{8}$ inch anywhere throughout the width of the web.

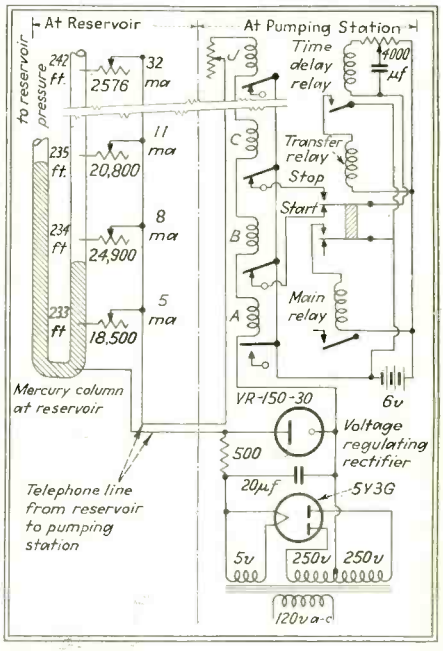
• • •

Pumps Controlled Automatically Over Phone Line to Reservoir

AUTOMATIC STARTING and stopping of four groups of water pumps in accordance with changes in reservoir water level is provided in the municipal water system of Kalamazoo, Mich. by a system of remote relays connected through a three-mile telephone line to a mercury column and rheostat arrangement at the reservoir. The controls, described in *Water Works Engineering*, were developed by Earl E. Norman, Supt. of Public Utilities of Kalamazoo, to maintain the reservoir level automatically within one foot of any predetermined depth.

In a vault alongside the reservoir

is a mercury U-tube balanced against the head of water in the reservoir. Ten plain wire electrodes are inserted in the atmospheric side of this glass tube as indicated in the diagram, at positions such that movement of the mercury column from one electrode to the next corresponds to a change of one foot in the water level. The electrodes connect through rheostats to one of the telephone wires running to the central pumping station three miles away. An additional electrode contacts the mercury at the bottom of the column at all times, and connects to the other telephone wire. Since each of the ten rheostats is set at a different ohmic value, each one-foot change in water level places a different resistance value across the reservoir end of the telephone line.



Essential features of the automatic control system used to maintain a desired level of water in the main reservoir at Kalamazoo, Michigan. The electronic voltage-regulating rectifier shown below the relays provides the constant d-c voltage required for the series arrangement of relays

At the central pumping station twelve sensitive relays are connected in series with a voltage source and a rheostat across the telephone line running to the reservoir. Ten of these relays correspond to the ten electrodes in the mercury column at the reservoir, and are adjusted so that each one-foot rise in reservoir level closes one additional relay. Thus, a current of 5 ma flows over the telephone line when the column

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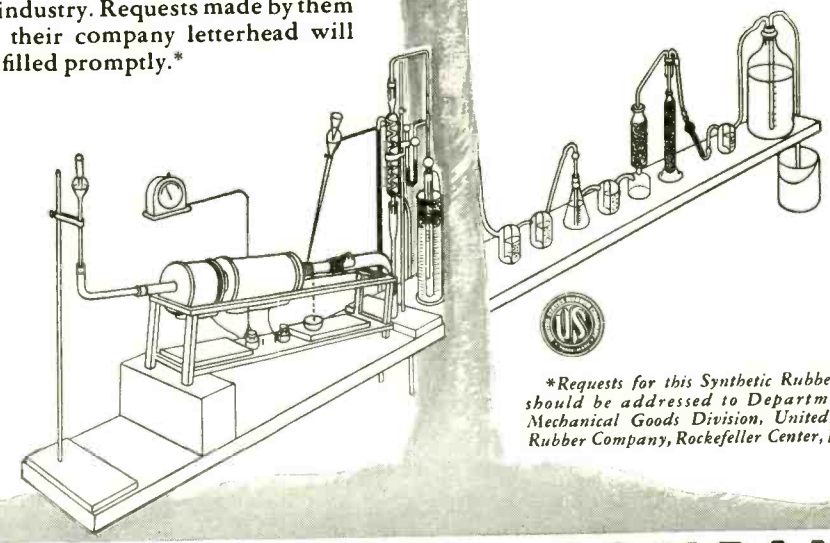

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rises to the first electrode, corresponding to a water elevation of 233 ft., and relay *A* is adjusted to pull up at this current. Line current increases to 8 ma when the water level rises one foot, and relay *B* pulls up at 8 ma. Each additional electrode circuit in parallel with the reservoir end of the phone line increases the current three ma, so that the 32-ma current for the highest electrode pulls up relay *J*. The two additional relays are for protection, one closing if the telephone line becomes shorted and the other acting if the telephone line breaks and opens the circuit.

A voltage-regulating rectifier circuit fed by a constant-voltage transformer (not shown in the diagram) provides a voltage source for the relays which remains constant within one volt even though the power line voltage drops as low as 55 volts or rises to 130 volts.

The system uses four sets of pumps, each controlled by a group of three relays—a time delay relay, a transfer relay and the main motor-starting relay. One group of these relays is shown in the diagram. The group can be connected between any two of the relays *A* to *J* by an arrangement of telephone-type switches, numbered according to the water levels they represent.

When the reservoir is full, 32 ma flows over the telephone line and relays *A* to *J* are all closed. With a relay group connected to relays *C* and *B* as in the diagram nothing will happen until the water drops to the level which makes relay *B* drop out. This closes the circuit to the time delay relay, which it closes after a delay of about ten seconds produced by the condenser and potentiometer in its circuit. Closing of the time delay relay energizes the transfer relay, which transfers control of the time delay relay from relay *B* to relay *C* and at the some time energizes the main relay controlling the motor-starting mechanism. When the reservoir level has risen one foot, relay *C* opens and disconnects the time delay relay. After a few seconds delay it drops out, causing the other two relays also to drop out and shut down the pumps. The time delay relay prevents chattering of the main relay contacts if the mercury tends to quiver at one of the electrodes in the U-shaped tube.

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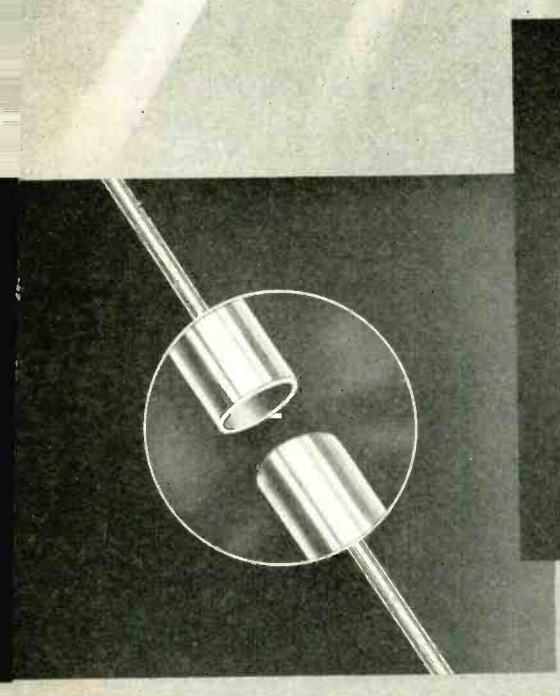

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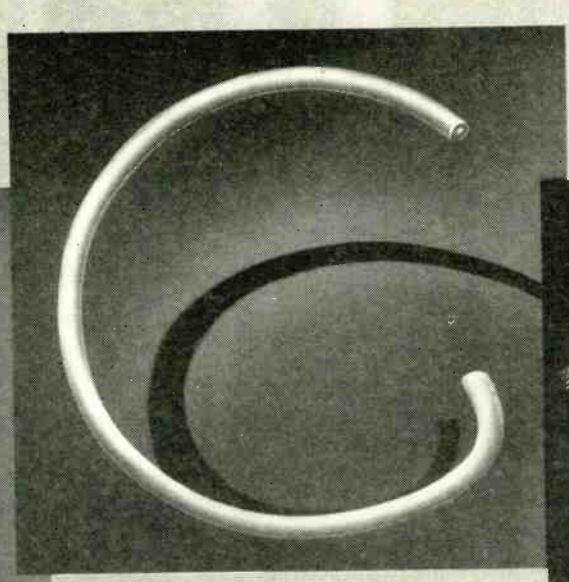

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THE ELECTRON ART

Chemical Analysis With A Cathode-ray Oscilloscope

NEWLY-DEVELOPED MEANS for producing current-voltage curves of chemical solutions instantly on the screen of a cathode-ray oscilloscope have brought the polarographic method of chemical analysis within the field of commercial electronics. Speedy identification of as many as half a dozen different substances in a dilute solution is now possible simply by watching the patterns appearing on the oscilloscope screen, once the apparatus has been calibrated with known solutions.

A paper by Tudor S. G. Jones in the Feb. 1943 issue of *Electronic Engineering* (a British publication) gives a comprehensive survey of polarographic methods of analysis. Early history, fundamental explanations, principles underlying each advance in laboratory technique, and the new oscillographic techniques are fully presented.

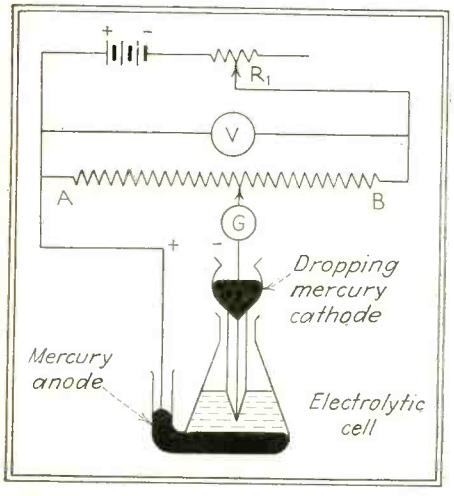

Fig. 1—Basic circuit for polarographic analysis

Basically, the method involves placing the solution to be analyzed in a container or cell having two electrodes. The smaller electrode is usually a capillary tube from which tiny drops of mercury issue every 2 to 4 seconds. The larger electrode is

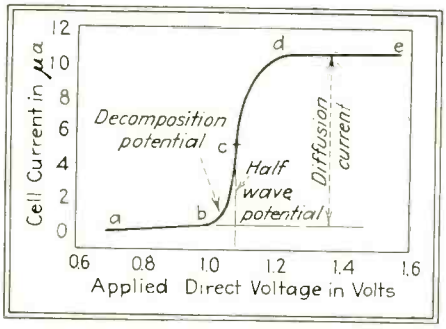

Fig. 2—Example of a current-voltage curve obtained with a polarograph

a pool of mercury in the bottom of the cell. The technique is based upon interpretation of the current-voltage curve obtained for the solution when a direct voltage is applied to the electrodes and gradually increased. Both the nature and the concentration of the substances present can be determined from the resulting curves.

As originally developed about 20 years by Jaroslav Heyrovsky[1] of the Charles University of Prague, the method required tedious manual plotting of the current-voltage curves, and perhaps for this reason received little attention. Nevertheless, it constituted a significant advance in analytical technique, providing a new tool for routine analysis and solving abstract problems immune to conventional methods.

The basic circuit is given in Fig. 1. The direct voltage is applied to the cell by calibrated potentiometer *AB*, and the current through the cell is measured by galvanometer *G*. When the voltage between the electrodes is increased from zero, the current will increase somewhat in the manner shown by the curve in Fig. 2. From *a* to *b* the current is small and increases but slowly with increases in voltage. At point *b*, the decomposition potential, the current suddenly starts to increase. Eventually, however, the current reaches a limiting value and follows an almost horizontal curve *d-e* which is parallel to the residual-current portion *a-b*. The paper explains the limiting current in terms of the diffusion of ions in the immediate vicinity of the dropping electrode.

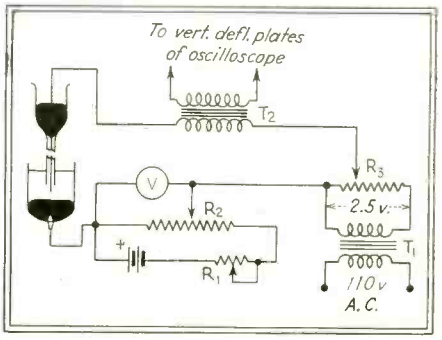

Fig. 3—Polarograph circuit arrangement permitting use of a cathode-ray oscilloscope for identification of ions in a solution

When several different electrolytes are present in the solution, the current-voltage curve will have a number of steps, each similar to that shown in Fig. 2. The decomposition potentials of the several electrolytes will determine the widths of the steps, and the concentrations will determine the heights.

Curves for different concentrations of any given electrolyte are symmetrical about a value of applied voltage at which half the limiting current is flowing. This voltage is known as the half-wave potential, is independent of the concentration and is characteristic of the electrolyte. A determination of the half-wave potential is therefore sufficient to identify an ion, and a determination of the limiting current value gives its concentration.

The development by Heyrovsky and Shikata[2] of an instrument called the polarograph, which automatically recorded in a few minutes the current-voltage curve for a solution, made polarography of practical use.

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In this instrument an electric motor simultaneously drives the moving arm of the potentiometer and a drum covered with photographic paper, while a miror galvanometer with its light source traces the desired curve on the paper. The method has since been modified to permit use of an automatic ink-writing recorder in place of a photographic recorder.

An early attempt to apply the cathode-ray oscilloscope to polarography is that of Matheson and Nichols,[3] who eventually were able to secure recurrent traces resembling a Heyrovsky polarogram. Their method involved synchronizing a rotating switch with the rate at which the mercury was dropping, this sometimes being quite difficult.

The latest oscilloscope application is based on an entirely new principle of detecting and measuring polarographic waves. When a small alternating voltage is superimposed on the direct voltage during polarographic analysis, the waveform of the resulting current will be the same as that of the applied alternating voltage whenever the current-voltage curve is linear, as at half-wave potential *c* and flat portions *a-b* and *d-e* in Fig. 2. At curved portions *b-c* and *c-d* the distortion will be marked.

Muller, Garman, Droz and Petras based their cathode-ray oscilloscope circuit in Fig. 3 on this principle. The direct potential is applied to the cell by potentiometer R_2 and is measured by voltmeter V. The alternating potential is upplied by transformer T_1 and potentiometer R_3. The resulting cell current is applied to the vertical deflecting plates of an oscilloscope through step-up transformer T_2, while the horizontal plates are driven by the usual internal synchronized sweep circuit.

The applied direct voltage is varied until the oscilloscope screen shows a trace having the same form as that of the alternating applied voltage (sinusoidal). The half-wave potential is then read on the voltmeter, making due allowance for direct voltage drops in R_3 and the primary of T_2. The entire pattern disappears as the mercury drop falls, but the interruption is only momentary.

The foregoing circuit arrangement was used with a slight modification by the Dutch workers Boeke and van Suchtelen[5]. By applying the

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alternating potential to the horizontal plates in place of the usual sweep circuit voltage, they secured the traces shown in Fig. 4 as the applied direct voltage was successively increased in steps. Trace *a* is symmetrical, indicating that the voltage is lower than the decomposition potential. Trace *b* is unsymmetrical, corresponding to region *b-c* in Fig. 2. Trace *c* is symmetrical and indicates that the half-wave potential has been reached. Traces *d* and *e* show the effect of changing the direct voltage 0.2 volts higher and lower respectively than that for *c*.

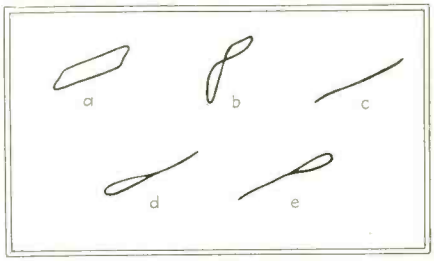

Fig. 4—Traces obtained on an oscilloscope as the direct voltage is increased in steps. The potentiometer is adjusted until the pattern at *c* is obtained, and the direct voltage giving this pattern is then the characteristic half-wave potential of one substance in the solution. Complex solutions containing as many as six different substances may be analyzed in a few minutes by this method

Interest in polarographic methods has lately been stimulated by publication of a comprehensive monograph by Kolthoff and Lingane[6], two of the leading workers in this field.

In conclusion, the author points out that the polarograph is finding many uses in industry, especially in metallurgy and in the control of proceses where even minute traces of metallic contamination are to be avoided. Recent work has been done on the determination of organically bound arsenic used in the treatment of disease, and other applications to biological chemistry are anticipated. The method also makes it possible for the first time to distinguish between tervalent and pentavalent compounds.

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(2) Heyrovsky, J. and Shikata, M., *Rec. trav. chim.*, 44, 496, 1925.
(3) Matheson, L. A. and Nichols, N., *Trans. Am. Electrochemical Soc.*, 73, 193, 1938.
(4) Muller, R. H., Garman, R. L., Droz, M. E. and Petras, J. *Ind. Eng. Chem., Anal. Ed.*, 10, 339, 1938.
(5) Boeke, J. and van Suchtelen, H., *Philips Tech. Rev.*, 4, 213, 1939.
(6) Kolthoff, I. M. and Lingane, J. J., *Polarography*. Interscience Publishers, Inc., New York, 1941. (This monograph contains numerous additional references.)

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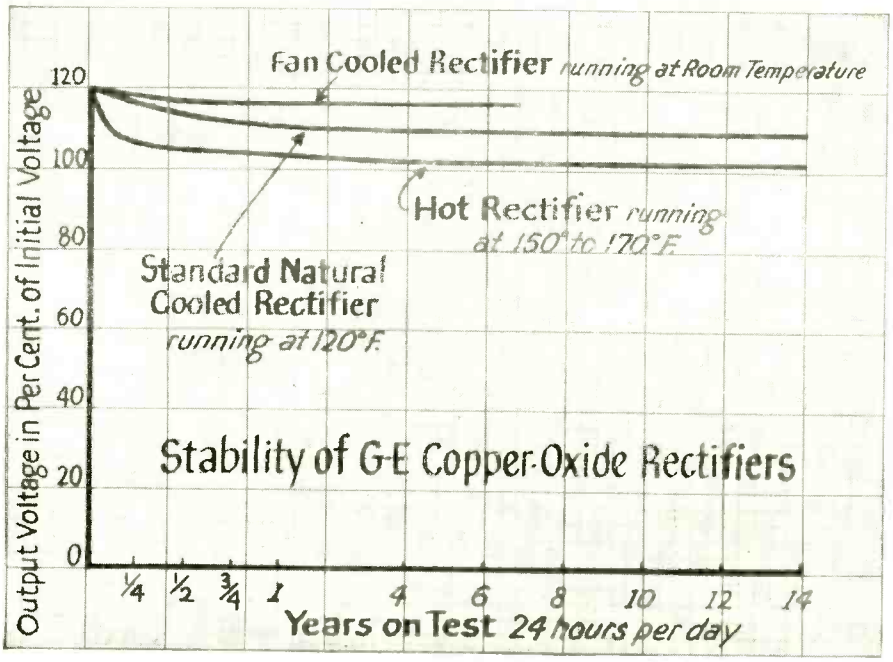

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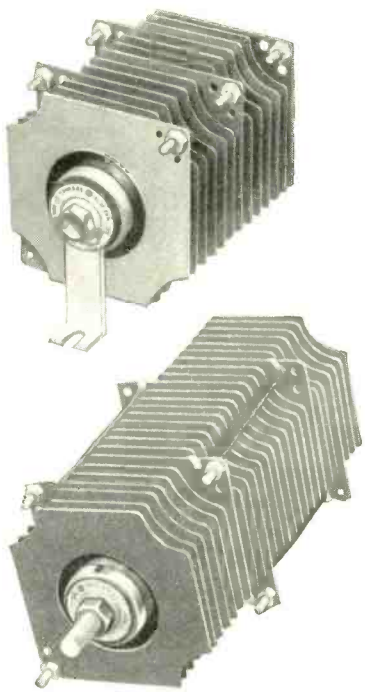

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GENERAL ELECTRIC

Combining of Phase-Shifted Rectified Sine Waves

THE RESULTS OBTAINED by combining rectified sine waves in various phase relations are described in a 54-page report by J. T. Tykociner and L. R. Bloom in University of Illinois Engineering Experiment Station bulletin No. 339 (Urbana, Illinois; price 60 cents). The properties of waveforms obtained by subtraction or addition of two phase-shifted rectified

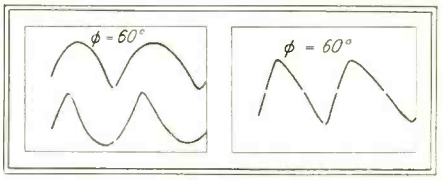

Fig. 1—When rectified pulses differing in phase by 60 deg. are subtracted, the saw-tooth waveform shown at the right is obtained. The greater the phase difference, the sharper the saw-tooth pattern

sine waves are investigated graphically and analytically for various phase angles, and a number of oscillograms are reproduced. One example, in which rectified waves shifted by 60 deg. are subtracted, is shown in Fig. 1. Methods of producing phase-shifted rectified sine waves in various frequency ranges are covered and circuits are given. The waveforms obtained by combining rectified pulses with full sine waves are also considered.

• • •

Electromechanical Calculator for Directional Antennas

RADIATION PATTERNS of a directional antenna array can be drawn with ease for any desired elevation angle by an electromechanical calculator described by Carl E. Smith and Edward L. Gove in the February 1943 issue of *Electrical Engineering*. Once the desired antenna parameters have been set up, the machine draws the field-intensity curve for the desired conditions on polar coordinate paper and indicates the rms value for drawing a circle of the equivalent non-directional pattern. The directional arrays may have any number of antennas. If desired, the pattern can be viewed on an oscilloscope screen, and parameters adjusted until a particular desired pattern is obtained. The whole hemisphere of an array can be explored in a relatively short time, eliminating laborious computations, and the total power radiated by the array can be determined.

Magnetostriction Made Visible

RAPID MEASUREMENTS of magnetostriction effects in transformer core samples can now be made to a fraction of a millionth of an inch as a routine semi-production procedure, according to Stephen C. Leonard writing in the November 1942 issue of the *General Electric Review*. His article points out that designers of induction apparatus are becoming increasingly aware of possible relations between magnetostriction in core materials and audible sounds such as the hum of a transformer core or a refrigerator motor. The problems involved in developing a satisfactory equipment for routine testing are analyzed, and a successful visual method utilizing a pair of optical flats as the indicating device is described.

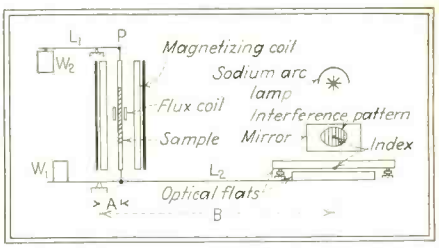

Fig. 1—Schematic diagram of the optical-mechanical system which is capable of magnifying movements due to magnetostriction 500,000 times with an accuracy of 12 percent or better

The arrangement of the optical system is shown in Fig. 1. The sample under test is mounted between lever arms L_1 and L_2 in such a way that any change in the length of the sample will change the spacing between the two optical flats. Sodium light projected normal to the flats produces an interference pattern dependent upon the spacing between the flats. Any change in the spacing can thus be measured directly in terms of the wavelength of sodium light by counting the number of interference lines which appear to pass the reference index mark as the sample is magnetized.

A movement of one light and one dark band across the reference index represents a change in spacing equal to one-half wavelength of sodium length, or 11.6 millionths of an inch. By making the lever-arm ratio (B/A) equal to 11.6 to 1, a direct-reading scale of magnetostriction is obtained in which each division (consisting of one dark and one light line) is equal to a millionth of

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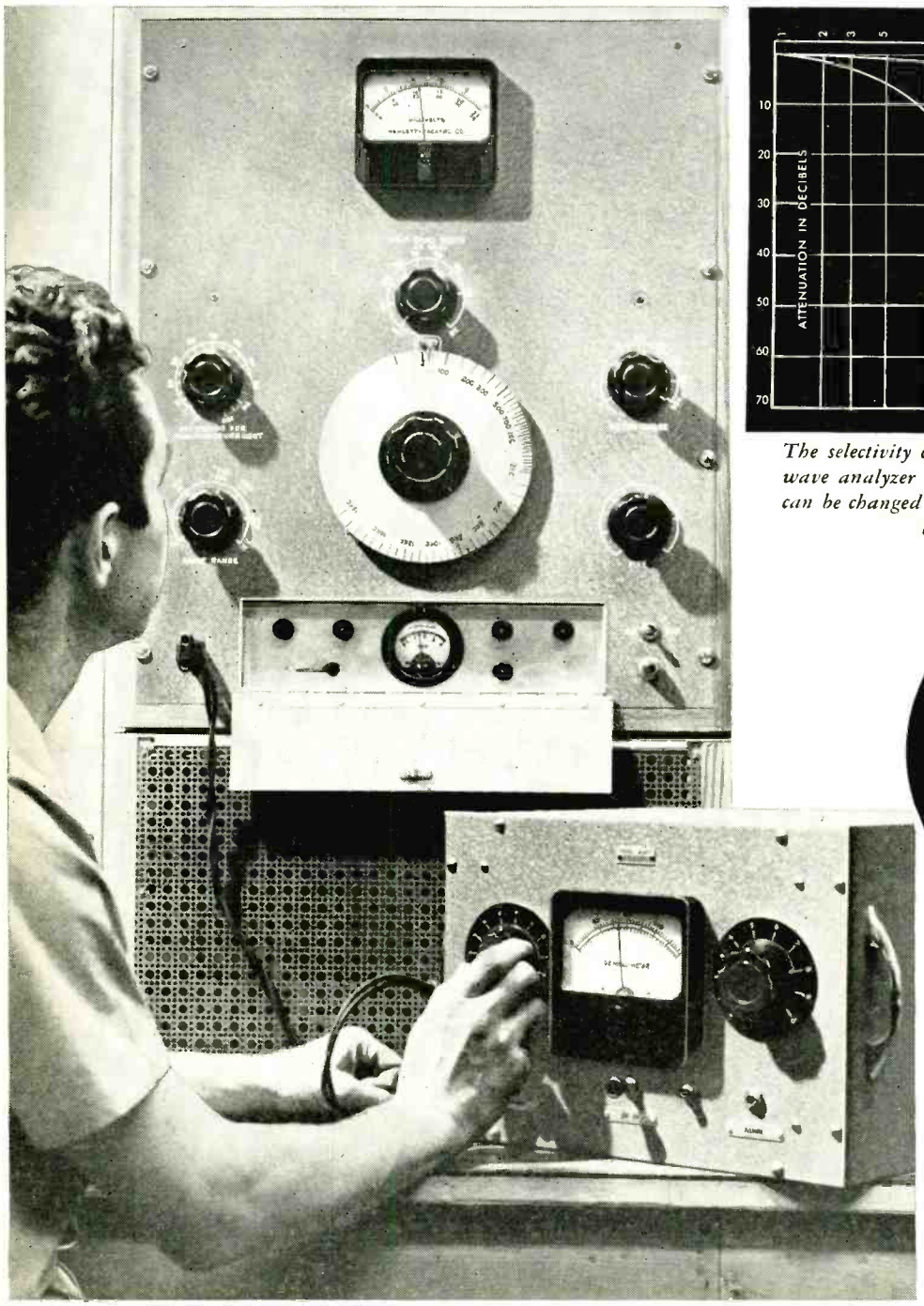
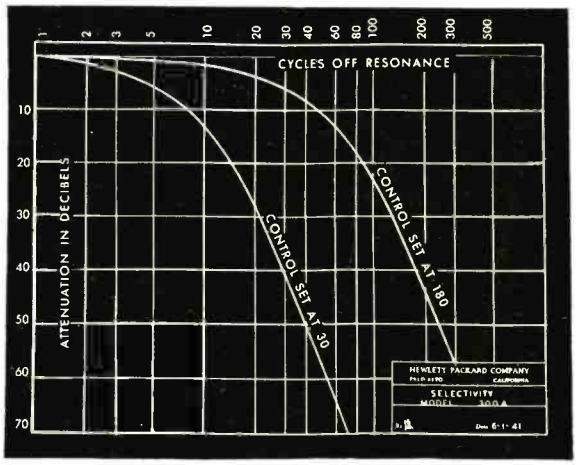
The overall voltage accuracy is ± 5%, the input impedance is 200,000 ohms, the voltage regulated power supply operates from 110 volts 60 cycles. Here is an instrument designed throughout for ease of operation and for accuracy which will be maintained over long periods of time. Write for further particulars. A 24-page catalog of *-hp-* instruments contains much valuable information relative to electronic measurement devices. A copy of this fully illustrated catalog will be sent you upon request. No obligation, of course, but mail your request early for the edition is limited.





The selectivity characteristic of the Model 300A wave analyzer is shown above. The band width can be changed to any value between these curves by a turn of a knob

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an inch. Furthermore, by slightly changing the tilt between the two optical flats, the interference bands can be spread out so that each division covers a distance of half an inch in the mirror mounted above the flats. This is equivalent to an overall magnification of 500,000 times for changes in the length of the sample.

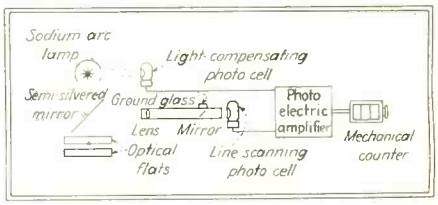

Fig. 2—Photoelectric arrangement for counting moving interference lines. Each number indicated on the mechanical counter represents a change in length of a millionth of an inch

The major portion of the article deals with methods of eliminating temperature effects, adjusting techniques, simultaneous measurements of flux density, and a consideration of practical problems involved in making factory tests. From one to four samples per hour can be tested by a trained operator, depending upon the amount of data desired.

In tests requiring the counting of a large number of moving lines, the interference pattern can be projected optically onto a photoelectric cell connected to a sensitive amplifier and a mechanical counter, as shown in Fig. 2.

• • •

Method of Predicting A-F Harmonic Distortion

A RELIABLE and essentially practical method of estimating the amount of harmonic distortion produced by an a-f transformer from transformer design data, operating conditions and the characteristics of the core material is described in a paper by Norman Partridge entitled "An Introduction to the Study of Harmonic Distortion in Audio Frequency Transformers" in a summer 1942 issue of the *Journal of the British Institution of Radio Engineers.* The author believes this to be the first recognized procedure for predicting harmonic distortion with accuracy. The same subject is treated more formally and at greater length in a series of articles in the British publication *Wireless Engineer.*

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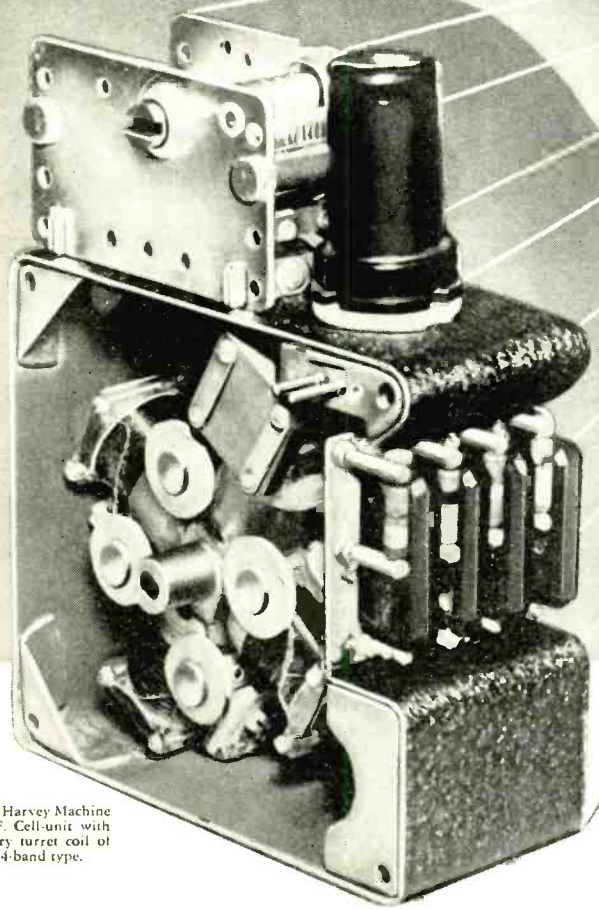

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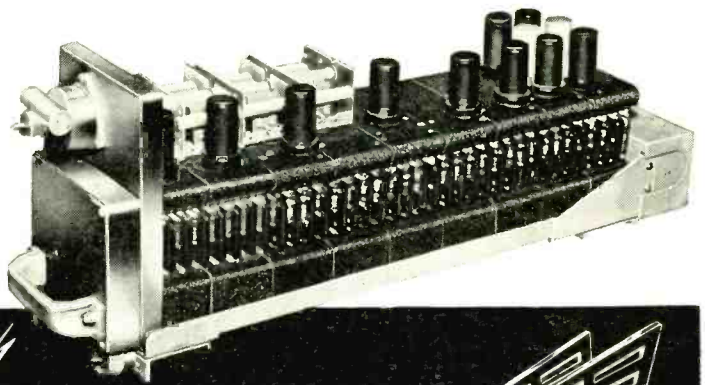

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A DISC WITH NINE equally-spaced radial lines can be used in connection with a Strobotron or other modern stroboscopic lamp connected to a 60-cycle a-c line for determination of speeds of rotation between 400 and 7200 rpm. Accuracy is only slightly less than that at which the power line frequency itself is maintained, both for fixed points at which stationary patterns are observed and for intermediate speeds at which the rate of precession or recession of a moving pattern must be considered. The entire speed-measuring procedure is described in detail in an article by D.A. MacInnes entitle "The Use of Stroboscopic Patterns in the Determination of Speeds of Rotation" in the January 1943 isue of *Review of Scientific Instruments.*

Speeds at which stationary patterns are observed when using a 60-cycle source can be determined by the formula: rpm $= 3600m/n$, in which n is the number of radial lines visible in the pattern and m is the "multiplicity," all values of m being excluded which make m and n have a common factor for a given condition. Thus, a three-line pattern can mean 1200, 2400, 4800 or 6000 rpm, but not 3600 rpm because that gives a single-line pattern.

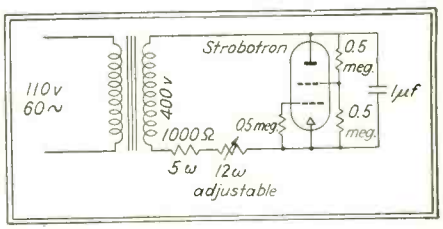
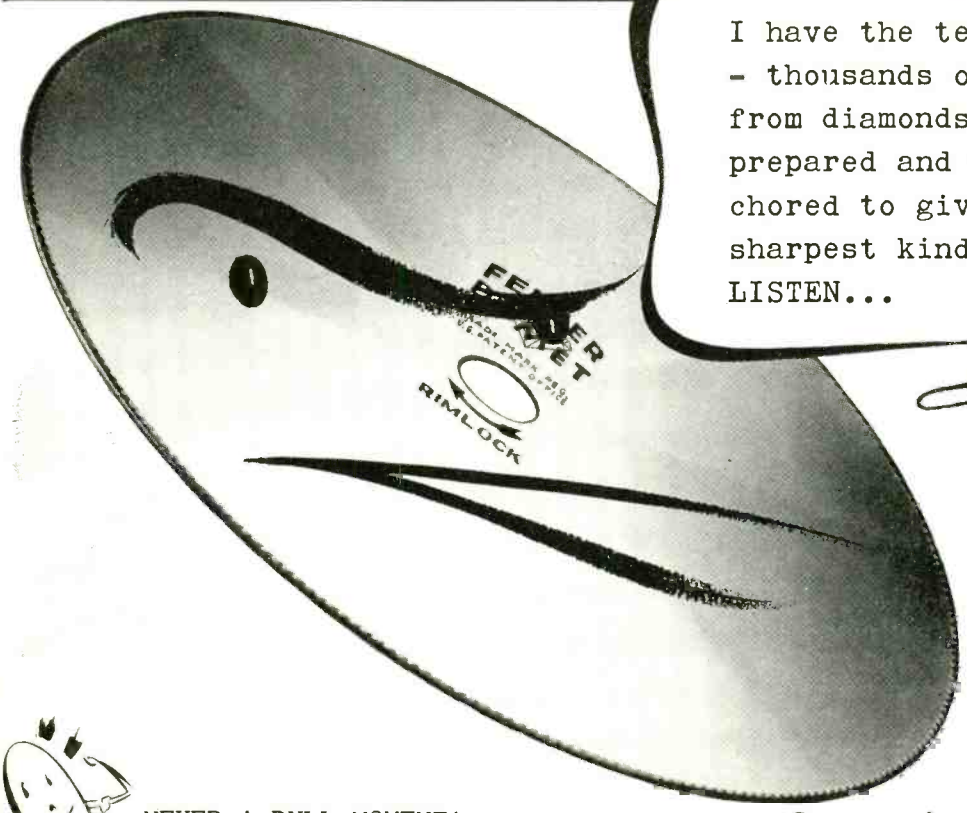


Fig. 1—This simple circuit produces 3600 flashes of intense light per second

To utilize this method, it is necessary to know the approximate speed. This can be determined with an inexpensive speed indicator or other means, or by noting the sequence of patterns observed as speed is changed and comparing with a table based on the foregoing speed formula. Intermediate speeds are determined by the fact that all of the patterns rotate at a rate dependent only upon the difference between the actual speed and the speed at which the pattern is stationary. Thus, if a five-line pattern with a stationary speed of 1440 rpm is turning ten times per minute in the direction of

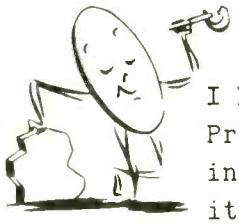
I PUT TEETH

behind any man's quartz program

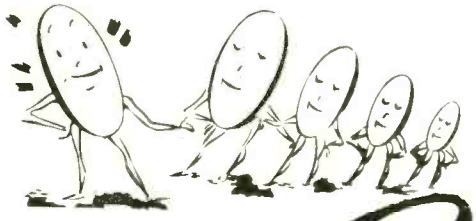


I have the teeth, too - thousands of them - made from diamonds specially prepared and anchored to give me the sharpest kind of a bite. LISTEN...

NEVER A DULL MOMENT!
Stamina? When I leave the factory I'm really in condition – hand straightened, they call it – nicely broken in and waiting for a chance to mow through that quartz. Guess I keep going because I hang on to my teeth and have plenty of 'em to start with.



I HOLD 'EM ON THE NOSE, TOO. Precision's the word! I get in the groove and stick to it. No wavering, no runout, but perfectly smooth, parallel cuts morning til night.



HOW BIG AM I?
Heck, my brothers and I vary from 4" to 24" in diameter. There's a 3" baby in the family, too!

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rotation, the actual speed is 1450 rpm.

A simple circuit for operating a stroboscopic lamp at the line frequency is given in Fig. 1. A standard broadcast receiver replacement transformer having a secondary voltage of about 400 volts is used. The tube is a General Radio Strobotron tube.

• • •

Diodes as Frequency Changers

THE MATHEMATICS INVOLVED in using a diode as a frequency-changer for reception of very short wavelengths is covered in two papers appearing in the January 1943 issue of *Wireless Engineer*. This type of converter is often used with the local oscillator set to a sub-multiple of what it would normally be for superheterodyne reception. A number of theoretical conclusions are presented, some confirmed by measurements at frequencies up to 600 megacycles. The conversion factor is greater than 90 percent for oscillator voltages in excess of 2 or 3 volts, and is essentially independent of the oscillator voltage. With a suitable d-c load resistance, the diode current is of sharply impulsive character, and the local oscillator may be set at half, third or even a fourth of the signal frequency plus or minus the beat frequency with little loss of conversion ratio. Performance formulas are deduced from an equivalent circuit consisting of a pi network of resistances.

• • •

Electronic Coil-Turns Counter

A CIRCUIT CAPABLE OF counting the number of turns in a coil to an accuracy of 1 turn in 500, on coils up to 4½ inches long with minimum inside diameter of ⅜ inch and with up to 111,000 turns, is given in the November 1942 issue of *Electronic Engineering*. The apparatus was developed by the Metropolitan-Vickers Electrical Co. of Great Britain and is sufficiently automatic for routine work. The coil to be tested is placed on an iron core along with a tapped standard coil, and connected in opposition to the standard coil. Decade-type selector switches are then adjusted for zero galvanometer deflection, indicating that both standard and test coils have the same numbers of turns. The decade switches then indicate directly the number of turns in the unknown coil.

Equipment for Combat

TO see in the dark and to see at a greater distance ...to push back the clouds and fogs of ignorance has been since the beginning of time one of man's greatest aspirations.

Spurred by war, the scientific laboratories of the nation are making tremendous strides toward meeting this aspiration.

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AIEE Bibliography Available on Automatic Power Stations

SUPPLEMENTING earlier bibliographies on the subject, the publication "Bibliography on Automatic Stations, 1930–1941" is now obtainable from AIEE headquarters, 33 W. 39th St., New York City at 25 cents for AIEE members (50 cents to nonmembers). Entries are arranged alphabetically by years in eight sections: General; supervisory and remote control; telemeter and telemetry; automatic and remote-controlled switches and switchgear; automatic boiler and combustion control; automatic hydroelectric plants; automatic substations.

• • •

Concentricity Tester for Enamel Film on Wire

AN ELECTRONIC CIRCUIT which makes it possible to measure the thickness or concentricity of enamel insulation on a sample of magnet wire in about one minute is described by Elmer F. Hansen in the Nov. 1942 issue of *General Electric Review*. The sample of wire is inserted in a turning chuck and placed over two brass plates mounted end to end in the same plane. An insulating block applies pressure to hold the wire flat against the plates. This gives two capacitances in series between the brass plates; the copper wire is the common conductor and each brass plate serves as a conductor, with the film of enamel acting as the principal dielectric for each capacitance. This series connection eliminates the necessity for scraping off insulation.

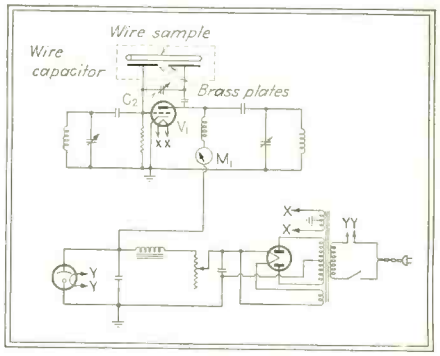


Fig. 1—Basic electronic circuit for measuring the thickness of enamel insulation on wire at production speeds

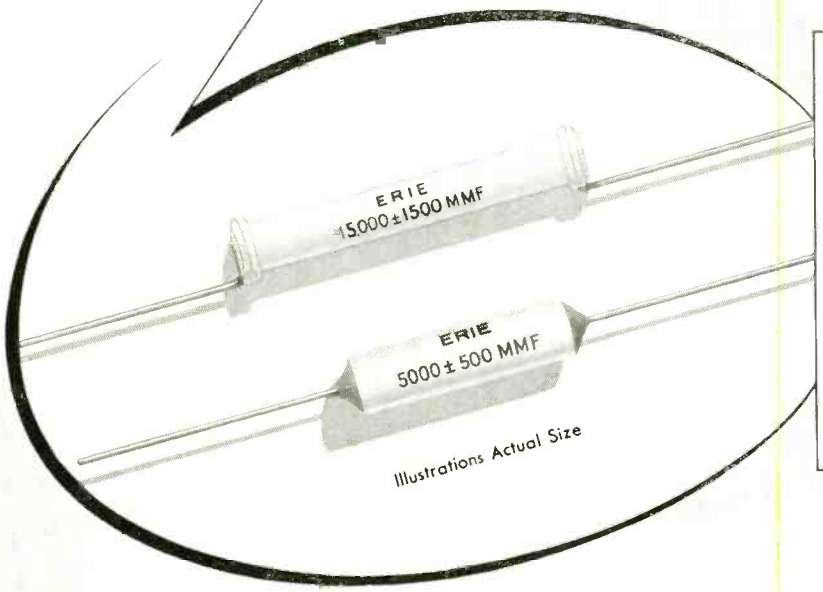
Changes in film thickness change the capacitance over a range of 5 $\mu\mu$f to 7 $\mu\mu$f for an average wire samples with varying degrees of concentric-

NOW!

Erie "Hi-K" Ceramicons

REG. U. S. PAT. OFF.

IN CAPACITIES UP TO 16,000 MMF



Capacity Range: Maximum capacity, insulated style 5,600 MMF; Non-insulated, 16,000 MMF. Minimum tolerance, ± 10%.

Working Voltage: 500 volts D.C. up to 60° C. Flash test 1,000 volts D.C.

Maximum Power Factor: 2.5% at 25°C.

Initial Leakage Resistance: Over 5,000 megohms at 1,000 volts D.C. at 25° C.

COMPACT, HIGH CAPACITY, CERAMIC CONDENSERS

ERIE is now in production on a group of new "Hi-K" Ceramicons in capacities up to 16,000 MMF. Behind these units are nearly 7 years of experience in producing silvered-ceramic condensers and over 1½ years of research and development of these high dielectric ceramic units.

Present Erie "Hi-K" Ceramicons have a dielectric constant (K) of 1050 at 25°C, and are available in the capacity range listed above. Insulated units are encased in a sealed ceramic sleeve. Non-insulated units have an extremely hard white protective coating.

The announcement of Erie "Hi-K" Ceramicons has been purposely withheld until they were developed to a point where they would successfully fulfill present day requirements. These units have very high and changing temperature coefficient and are recommended for use as by-pass or blocking condensers where high stability and high leakage resistance is not essential. The ratings of these capacitors, shown in the above panel, are conservative and are indicative of their operating performance.

Interested engineers are invited to write for samples to test in their laboratory.

ERIE RESISTOR CORP., ERIE, PA. LONDON, ENGLAND · TORONTO, CANADA.

ity. This change is measured by connecting the brass plates to the grid and plate circuits respectively of an oscillator, as shown in Fig. 1. An increase in film thickness causes a decrease in the connected grid-plate capacitance and an inversely proportionate increase in the d-c plate current of the oscillator. The deflection of the plate current milliammeter M_1 was found by test to be a linear function of film thickness.

A calibration in terms of the ratio of maximum to minimum film thickness was found more suitable for production testing because it remains accurate regardless of normal changes in circuit parameters with age, and is also independent of slight changes in oscillator frequency. In making a test, the wire sample is rotated to get minimum meter deflection, and sensitivity control C_2 is varied until a reading of 1.0 is obtained. The wire is then rotated for maximum deflection, and the ratio of maximum to minimum film thickness is read directly on the meter. The results are accurate to within about 5 percent.

• • •

MINE DETECTOR

This compact case and earphones is a British mine detector used by skillful and courageous engineers who sweep the desert before advancing troops. When the device detects a mine, certain sounds reach the earphones worn by "sappers" who then go about the task of unearthing the deadly mine and rendering it harmless. This detector played a big part in Britain's conquest of Egypt

WITH OUR FEET ON THE GROUND

. . . and our eyes to the future

Today, with our feet firmly planted on the ground, we are producing vital electrical and electronic instruments to help win this war. But we also believe that the time to plan for tomorrow is today. That is why our engineering laboratories are working continuously, developing and designing instruments that will not only keep abreast of war-accelerated radio demands, but will also meet the requirements of industry after the war.

★ ★ ★ ★

Illustrated are a few of the R.C.P. instruments now available. Others are described in catalog material available on request. If you do not find among these the instrument for your specific needs, our engineers will be glad to cooperate in solving your instrumentation problem.

SIGNAL GENERATOR
MODEL 703

A sturdy test oscillator with a range from 95 Kc to 100 Mc. Fundamental frequencies in 5 bands variable from 95 Kc to 25 Mc. Has self contained 400 cycle modulation source.

VOLT-OHM-MILLIAMMETER
MODEL 423

A multitester with a meter movement of 2,500 ohms per volt. Has a uniform A.C.-D.C. voltmeter sensitivity of 1,000 ohms per volt. Voltmeter range to 1,000 volts. All multipliers individually matched to 1%. Suppressor type copper oxide rectifier used on A.C. readings.

VACUUM TUBE VOLTMETER
MODEL 666

Essentially a peak voltmeter for accurate measurements over the entire a.f. range. Ranges are 0-3-6-30-150 volts, with meter movement of 0-200 microamperes. Uniform input resistance of 16 megohms for all ranges.

ELECTRONIC
VOLT-OHM-CAPACITY METER
MODEL 662

A true vacuum tube voltmeter for A.C. and D.C., combining sensitivity, flexibility and utility. Six range D.C. and 7 range A.C. voltmeter to 6,000 volts. Sensitivity 16 megohms on low and 160 megohms on high ranges. Ohmmeter range: .1 ohm to 1,000 megohms. Capacitymeter range from .00005 to 2,000 mfd. All measurements are direct reading.

ULTRA-SENSITIVE MULTITESTER
MODEL 461

A multitester with a sensitivity of 20,000 ohms per volt on all D.C. measurements. Uses a wide scale meter with a movement of 50 microamperes. Readings as low as 1 microampere on 100 microampere scale. Six range A.C.-D.C. voltmeter to 5,000 volts.

RADIO CITY PRODUCTS COMPANY, INC.

127 WEST 26th STREET — NEW YORK CITY

MANUFACTURERS OF PRECISION ELECTRONIC LIMIT BRIDGES—VACUUM TUBE VOLTMETERS — VOLT-OHM-MILLIAMMETERS — SIGNAL GENERATORS — ANALYZER UNITS — TUBE TESTERS — MULTI-TESTERS — OSCILLOSCOPES — AND SPECIAL INSTRUMENTS BUILT TO SPECIFICATIONS.

NEWS OF THE INDUSTRY

New Signal Corps radio sets; latest FM log; replacement tubes and parts for civilian sets; technical employment information from the FCC, Navy and industry; data on new tubes; radio industry personnel and business news; how electronics aids in solving heat-transfer problems; new television station; CBC uses relay transmitters in western Canada

Navy Commissions Still Given

OFFICERS TRAINED in electrical engineering are needed by the Navy for work on ultrahigh-frequency electronic apparatus. Men with electrical engineering degrees and experience, or men who have majored in physics, mathematics or other fields dealing with a-c circuits and electronics are technically qualified for commissions. Those accepted as officers are given a three-month Navy u-h-f course either at Harvard or at Bowdoin College, followed by a three-month lab course at MIT. Qualified engineers are urged to apply for a commission at the nearest office of Naval Officer Procurement.

New Shortwave Station at Rio

WITH EQUIPMENT BUILT and installed by RCA Victor Division, a new 50,000-watt shortwave station is on the air at Rio de Janeiro, Brazil. Known as Radio National, it broadcasts nightly to North America on 26.5 meters.

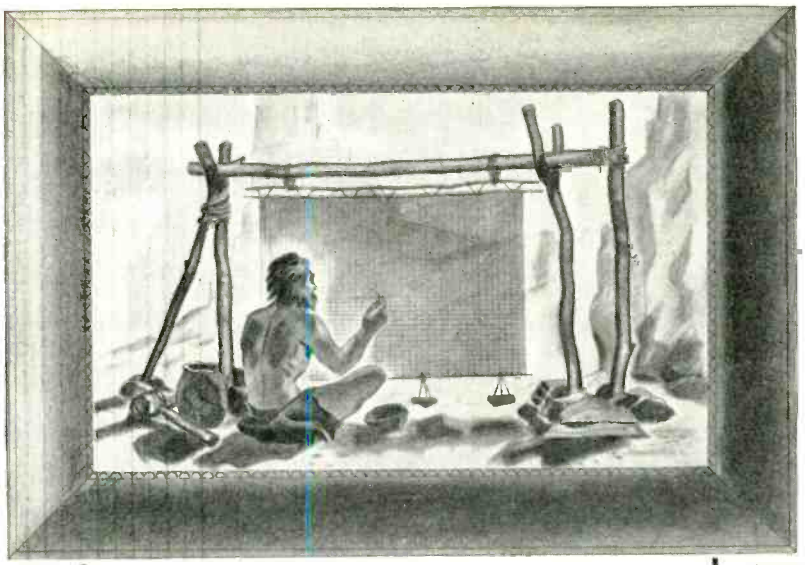
Vital War Jobs Await Retired Skilled Workers

INABILITY OF WAR plants to locate specialists for key jobs has held up employment of many thousands of war workers, according to case histories in the files of the War Manpower Commission. In one case, lack of skilled men prevented the hiring of 3000 workers, and in dozens of other cases vital military orders were held up because of critical shortages of machinists and machine operators.

This situation prompted WMC to begin a nationwide campaign through the U. S. Employment Service, aimed at bringing into the war effort as many as possible of the skilled workers who are in retirement or in a non-essential job. One of the 25 skills specifically chosen for this campaign is that of radio chassis assembler.

An example of the type of worker desired is Mrs. D. A. Ausmus, who twenty years ago worked as laboratory assistant in the original radio department of G-E's research lab. Marriage brought retirement to the

Above: Photograph taken 20 years ago, showing Mrs. Ausmus (then Miss Doris Evans) running tests on radio equipment in the General Electric radio research lab Below: Mrs. Ausmus at her workbench in the G-E general engineering lab today, carrying out experimental work again after almost 20 years as a housewife



WE GLORIFY AN ANCIENT ART

As We Further Develop the Age of Cloth

The Stone Age and other ages which have marked progress in man's advancement have come and gone. A few persist. Through all ages one alone holds its dominant position. Cloth is of all time, from the earliest to the present. Into the future we see it projected as the structure of many modifications serving many new uses — alone, or in combination with plastics, colors, printings, and finishes. We, at Holliston Mills, continue to pioneer in the development of cloth specialties — cloth finishes, modified and adapted to specific uses.

RESEARCH AND DEVELOPMENT — cloth has a permanent structure combining light weight with strength and flexibility. On or within this structure filling, coating and processing fits cloth for many uses. *Consider cloth — consult HOLLISTON.* In general, THE HOLLISTON MILLS can take any type of print cloth, sheeting, drill, twill, duck, in widths from 30" to 80", and can dye; coat with every type of coating, in any color desired; can stiffen fabrics to meet any required pliability, hand, bond, weight of coating, tensile strength, Elmendorf tear strength, for any industrial use.

BOOKBINDING FABRICS

(a) Waterproof, full coated, impregnated, linens and vellums; pyroxylin and other synthetic resin coatings and lacquer finishes; embossed, plain, super finished, contrast printing.

(b) Starch filled, coated, impregnated, mottled, linen and vellum; plain or embossed, special glazed and matte finishes; natural, rough and smooth finishes.

SHADE CLOTH

(a) Pyroxylin or resin impregnated waterproof, meeting Government specifications; all weights, widths and colors; print cloths, sheetings and ducks.

(b) Starch filled, water color, and Halland type shades; machine oil, oil tints, oil filled opaques; fast dyed duck shades; light-proof and translucent.

PHOTO CLOTH

Photo Mounting cloth (self adhesive), single and double adhesive.

REINFORCING FABRICS

All types of waterproof and starch-filled reinforcing fabrics and industrial cambrics, for books, file folders, file pockets, box stays; to be combined, gummed and plain. Various weights from the thinnest print cloth to the heaviest drills and twills.

SIGN, LABEL & TAG CLOTHS

Waterproof and starch filled. Designed for any purpose, for hand lettering, letterpress printing, offset printing. We can design a surface that will take any ink or meet any inking problem.

RUBBER SEPARATOR CLOTHS

Starch filled glazed sheetings and base treated starched fabrics for waterproof separator cloths.

INSULATING CLOTH BASE

Base treated and stiffened fabrics for insulating cloths; all weights, widths and thicknesses.

TRACING & BLUE PRINT CLOTHS

White and blue ink or pencil cloth; map cloth; blue print cloth, thin and regular, all widths.

LINING FABRICS

Shae and drapery linings; starch filled, special filled, mercerized and shreiner finishes; straight backfilled finish; high lustre finish, all colars and widths.

COATED AND IMPREGNATED FABRICS

All widths and colors; synthetic resin, nitro cellulose, thermo plastic and thermo setting coatings; mildew proofing; fire, weather and water resistant finishes; gas impermeable finishes, etc., far war and industrial purposes.

BOOK CLOTHS Holliston cloths for bookbinding are world famous and the line includes a great variety of colors and finishes. Starch filled, Pyroxylin filled or coated. Special embossings. Any book or catalog bound in cloth is bound to be kept. Consider cloth binding for your business literature. Costs but a little more than paper. For attention and retention value cloth binding stands alone. Lesser bindings discount content value. Write for samples of Holliston Bindings. Make your new catalog a cloth bound book.

THE HOLLISTON MILLS, INC.

CONVERTING CLOTHS TO GREATER USE FIELDS

NORWOOD, MASSACHUSETTS

Sales Agents in Principal Cities

duties of a housewife. When her husband, Col. Delbert Ausmus, was reported as missing on Corregidor and was presumed to be captured, she offered her services once again to General Electric. Mrs. Ausmus is now using her scientific experience in carrying out experimental work on new measuring devices.

In order that workers responding to this campaign can be referred to specific jobs without delay, WMC urges holders of war contracts to make their skilled worker requirements known immediately to the nearest local U. S. Employment Service office.

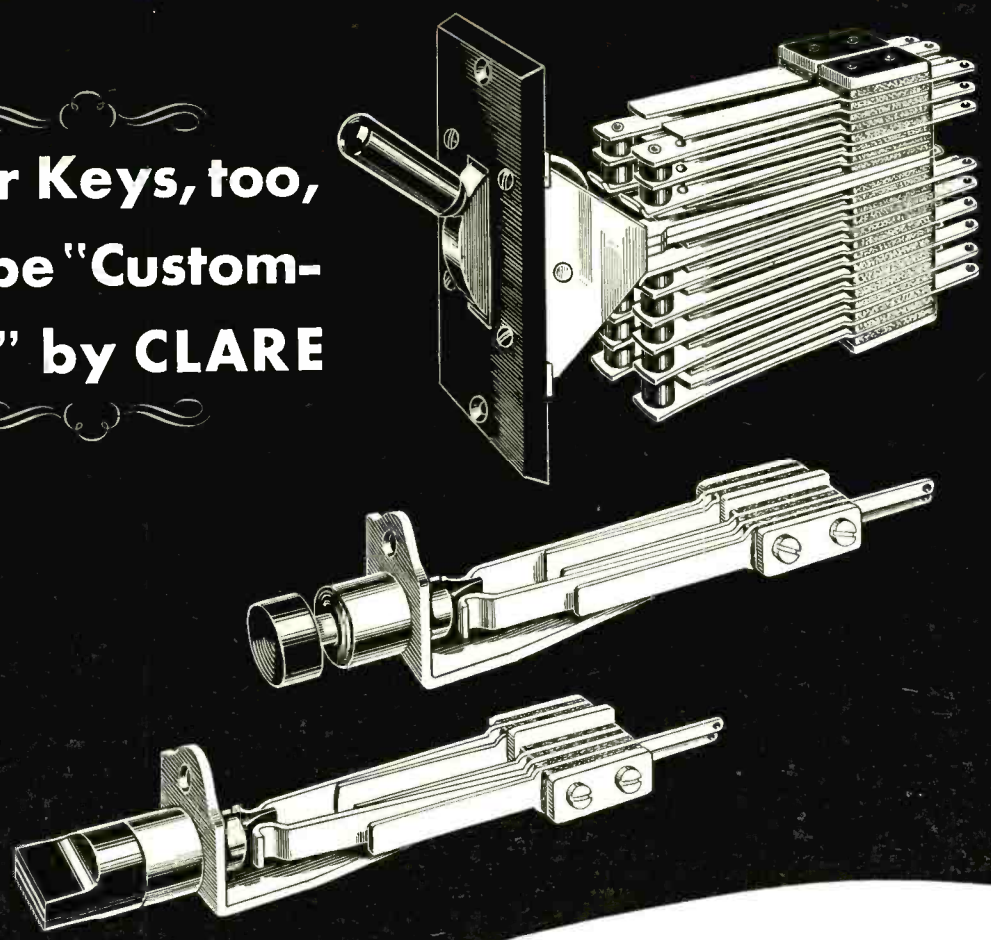
Separation Process Found For Tin-Tungsten Ores

GREAT AMOUNTS of almost pure tin and tungsten are being recovered from otherwise worthless tailings and complex tinny wolfram ores with a long-sought separation process developed by the Foote Mineral Co. of Philadelphia in cooperation with Brazilian mine operators. Although details are a military secret, the general treatment involves rolling and crushing the mixed ore, then passing it through a series of machines which break the physical bond holding particles of tin and tungsten together. The ores can then be separated and the impurities removed. The entire process recovers 97 percent of the tin and tungsten.

RCA Will Pay Girls to Study Electronics at Purdue

FROM 80 TO 100 GIRLS between the ages of 18 and 22 will be selected from RCA plants and from colleges and universities to take a special electronic training course at Purdue University as employees in training. Those chosen will be paid a salary in addition to all university expenses, and will live on the Purdue campus. The curriculum provides for two terms of 22 weeks each, with classes starting around May 1. Basic requirements are two years of college study with satisfactory grades, some competence in mathematics, good health, and an interest in technical radio work. Those completing the training will be qualified for immediate assignment on test and quality control work on RCA electronic, sound, and radio equipment.

Lever Keys, too, Can be "Custom-Built" by CLARE



. . . and so, too, can Push and Turn Keys

The Lever Key illustrated is another example of Clare "custom-building" to meet requirements. Its frame is designed to hold all parts together by their interlocking shapes, then welded to make virtually a "one solid piece frame," to provide maximum rigidity.

The cam assembly is also unique because at the time of manufacture, or at any future time, stops may be provided, added or removed to change the key from locking to non-locking or vice versa. Or it may be changed from one-way to two-way, or vice versa.

The same careful design and construction are typical of the Push Key and Turn Key also illustrated above.

In every feature of design, these keys possess all the construction and design features which make Clare Relays outstanding in performance. Some of these features are listed at the right. Our engineers will be glad to "custom-build" keys to fit your requirements. Write us regarding them. Ask for the Clare catalog and data book. C. P. Clare and Company, 4719 Sunnyside Ave., Chicago, Ill. Sales engineers in all principal cities. Cable Address: "CLARELAY."

● Contact springs are made of nickel silver to exacting specifications.

● Flat or hemispherical contacts of either rare metals or special alloys are "over all" welded to contact springs by a special process which makes them an integral part of the springs, thereby reducing contact resistance to a minimum and providing for rapid heat dissipation.

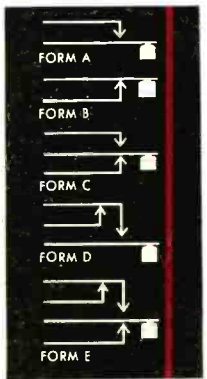
● Contacts available and their current ratings are as follows:

Contact Ratings: 110 Volt, 60 Cycle, A. C. Non-Inductive

Code No. 1	1 Amp. 50 Watts
Code No. 2	2 Amp. 125 Watts
Code No. 4	3 Amp. 150 Watts
Code No. 5	4 Amp. 175 Watts
Code No. 7	4 Amp. 175 Watts

● Insulation between springs and between springs and frame may be either single, double or special. Single insulation will stand a 500 volt a.c. test, double insulation a 1000 volt a.c. test, and special insulation a 1500 volt a.c. test. These spring insulators are made from special heat-treated Bakelite that permits punching without cracks or checks and possesses minimum cold flow and low moisture absorption properties.

● Contact forms may consist of any one of the five forms shown below, or of any combination of those forms.



● The Lever Key may incorporate as many as 40 springs, whereas the maximum number of springs that may be had on the Push and Turn Keys is 20.

● Spring bushings of Bakelite are designed under a special secret process providing long wearing features.

● The Lever Key handle is made of catalin, in either polished black, red or white. Push Key buttons and Turn Key knobs are of Bakelite, in black only.

● The Lever Key escutcheon is made of Bakelite and is held to the key frame by four oval head No. 3-48 screws; keys may be furnished with or without escutcheon, depending upon the type of mounting to be used.

C L A R E R E L A Y S

"Custom-Built" Multiple Contact Relays for Electrical, Electronic and Industrial Use

FM Log Has Over 50 Stations

FM BROADCASTING enters 1943 with 36 stations throughout the country operating from 6 to 24 hours a day on a regular commercial basis, nine other stations operating with experimental transmitters, and at least seven more operating as noncommercial educational stations.

Call letters of regular f-m stations contain numbers from 31 to 99 which represent the last two figures of the frequency assignment in the f-m band covering 43.1 Mc to 49.9 Mc. The first letter indicates whether the station is east (W) or west (K) of the Mississippi river, just as for regular broadcast stations, and the last letters are the initials of the location whenever possible. Thus, W65H is in Hartford, Conn., and has an assigned frequency of 46.5 Mc. Experimental stations have call letters similar to those of radio amateurs.

COMMERCIAL FM STATIONS

W45BR	Baton Rouge, La.
W49BN	Binghamton, N. Y.
W43B	Boston, Mass.
W67B	Boston, Mass.
W51C	Chicago, Ill.
W59C	Chicago, Ill.
W67C	Chicago, Ill.
W75C	Chicago, Ill.
W41MM	Clingman's Peak, N.C.
W45CM	Columbus, Ohio
W45D	Detroit, Mich.
W49D	Detroit, Mich.
W45V	Evansville, Ind.
W49FW	Fort Wayne, Ind.
W53H	Hartford, Conn.
W65H	Hartford, Conn.
K49KC	Kansas City, Mo.
K45LA	Los Angeles, Calif.
W55M	Milwaukee, Wis.
W39B	Mount Washington, N.H.
W47NV	Nashville, Tenn.
W47NY	New York City
W63NY	New York City
W67NY	New York City
W71NY	New York City
W75NY	New York City
W49PH	Philadelphia, Pa.
W53PH	Philadelphia, Pa.
W57PH	Philadelphia, Pa.
W69PH	Philadelphia, Pa.
W73PH	Philadelphia, Pa.
W47P	Pittsburgh, Pa.
W75P	Pittsburgh, Pa.
W51R	Rochester, N. Y.
W47A	Schenectady, N. Y.
W85A	Schenectady, N. Y.

EXPERIMENTAL FM STATIONS

W1XTG	Worcester, Mass. 43.4 mc
W1XSN	Springfield, Mass. 42.6 mc
W2XMN	Alpine, N. J. 42.8 mc
W2XQR	New York City 45.9 mc
W2XWG	New York City 45.1 mc
W3XO	Washington, D.C. 43.2 mc
W8XAD	Rochester, N.Y. 42.6 mc
W9XER	Kansas City, Mo. 46.5 mc
W9XYH	Superior, Wis. 43.0 mc

EDUCATIONAL FM STATIONS

KALW	San Francisco Schools
KSDS	San Diego Schools
WBEZ	Chicago Public Schools
WBOE	Cleveland Board of Education
WIUC	University of Illinoiis
WMBE	Memphis Public Schools
WNYE	New York City Board of Education

WBOE is broadcasting eight full hours each school day. Westinghouse's W67B in Boston is now run entirely by women. Eleven Connecticut cities are getting two-way f-m police systems developed by G.-E.

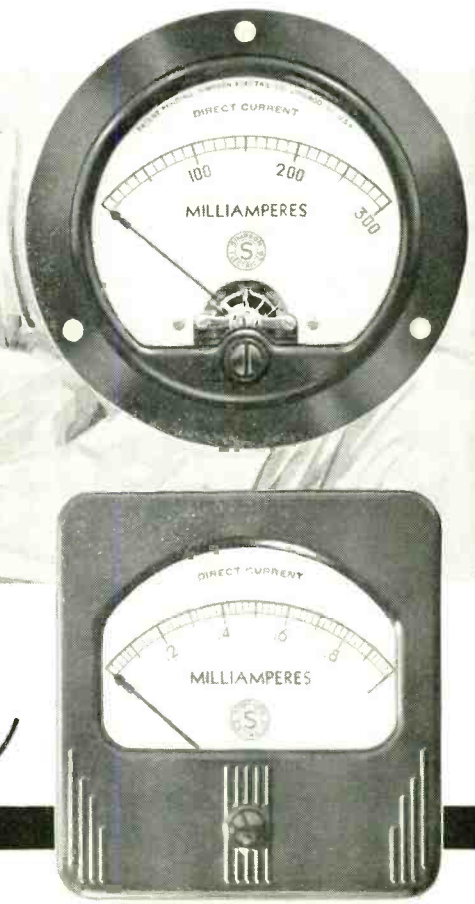
A BIG STEP FORWARD

EVERY TIME our fighting men win a new beach head . . . every time an enemy plane falls from the sky . . . every time the sun sets on a war-torn world . . . America is that much closer to Victory.

No man can know how many days there are between us and peace. We can only do our best to make those days as few as possible.

Hard work is what it takes — good old-fashioned hard work, and sweat, to save us blood and tears. Here at Simpson we hold this as a sacred trust — to send ever more and better Simpson Instruments into battle, and to make each working hour a big step forward toward America's inevitable Victory.

SIMPSON ELECTRIC CO.
5200-5218 Kinzie Street, Chicago, Illinois



Simpson

INSTRUMENTS THAT STAY ACCURATE

Buy War Bonds and Stamps for Victory

FCC Announces New Position as Radio Intercept Officer

INTERCEPTION OF RADIO messages to insure compliance with radio silence orders of the Army Air Force is one of the duties connected with the newly announced FCC position of Radio Intercept Officer. Other duties involve maintaining a continuous watch on distress channels and carrying out monitoring assignments related to the war effort.

No written tests are required, and the only age qualification is that the applicant must have reached 18. Positions are available throughout the United States. Qualifications for the $2600 grade are either a full four-year college course in electrical engineering or physics, four years of technical experience in radio, or a time-equivalent combination of education and experience. For the $2000-a-year grade, less education and experience are required. Ability to send and receive code is essential for both grades. Overtime pay for eight additional hours a week increases the above salary figures about 21 percent. Application forms can be obtained from most post offices or from Civil Service offices.

Infrared Rays Dehydrate Food

THE USE OF INFRARED radiation in a vacuum chamber to dehydrate completely cooked dishes like soups, puddings and pork-and-beans is the subject of U. S. patent No. 2,308,601, issued to J. G. W. Gentele of Stockholm. The infrared rays maintain the food at a temperature above the boiling point of water until the greater part of the contained moisture is driven out.

Heat-Transfer Problems Solved With Roomful of R-C Networks

ALMOST ANY PRACTICAL PROBLEM in heat flow can be duplicated electrically by Dr. Victor Paschkis on the Heat and Mass Flow Analyzer which he developed at Columbia University in New York City. The results are read on meters or recorder charts without the usual expenses for building sample structures and running long heat tests. The procedure, first proposed in Holland by C. L. Beuken, is based upon the similarity between

the flow of electricity in a resistance-capacitance circuit and the transient heat flow through walls or other structures. Temperature corresponds to voltage, and heat flow per unit time corresponds to current.

In utilizing this analogy, the structure to be studied is considered to be cut into a number of sections, over 100 sections being possible with the present apparatus. For each section, the capacitance corresponding to the thermal capacity and the resistance commensurate with the thermal conductivity are computed. The resulting electrical values are then set up in the apparatus, and a direct voltage is applied. If the temperature applied to the structure varies under actual conditions, the applied voltage is likewise varied during the test.

Current flowing through the entire circuit along resistive paths corresponds to transmitted heat, and current flowing into capacitors corresponds to heat being stored within the structure during the initial unsteady state.

Voltage values during the test run are measured at carefully selected points with specially-developed electronic voltmeters drawing practically no current, and these values are interpreted in terms of temperature. Two electronic recorders are used to provide continuous records on charts of voltages at four selected points which may be of particular interest.

By appropriate choice of electrical values, the time of a heat cycle can be condensed or stretched as desired. Thus, a heat cycle of 24 hours in a furnace can be condensed to last only 15 minutes in the model, or a fractional-second cycle during welding operations can be stretched to several minutes. Cooling conditions are studied by applying a voltage for a definite time, then removing the voltage and measuring voltage drops across circuit resistors as the capacitors discharge.

Description of Apparatus

The apparatus has 15 condenser sections and 115 resistors sections filling three walls of the room with sufficient resistors, capacitors and plug-board connections to duplicate electrically one section of the heat - transfer structure being

studied. It is possible to secure in each bank a capacity anywhere between 0.1 and 152 μf in steps of 0.1 μf. All condensers have an accuracy of 1 percent or better, and a leakage resistance higher than 15,000 megohms per microfarad. Selector switches and jacks provide resistance values ranging from 100 ohms to 1,111,000 ohms for each section. Thirty-six buses run at the tops of the sections, to simplify connecting instruments to sections. The arrangement is such as to permit changing the values during an experiment to duplicate changes in thermal conductivity and thermal capacity with temperature. A motor-driven sequence timer has been constructed to imitate complex processes requiring considerable switching.

The applied d-c voltage is obtained from a 110-volt a-c power pack providing a constant output voltage at any desired value from 286 volts down to zero. An electronic constant-current source is used when it is necessary to duplicate the condition of constant heat input with varying input temperature.

The facilities of the Heat and Mass Flow Analyzer at Columbia University are available to manufacturers for technical investigations on heat flow in solid materials, however complex the shape and however irregular the heating cycle. Dr. Paschkis is in charge of the technical and scientific work of the laboratory, and Prof. C. F. Kayan, as Executive Secretary, is responsible for its administration.

Investigations already carried out with th eapparatus include studies of thermal phenomena in the wheel and brakeshoe of an express train locomotive during emergency braking, temperature distribution and heat losses in intermittently operated furnace walls, summer cooling load and heat absorption of building walls under solar radiation, heat loss in intermittently heated steam pipe insulation cooling rates in arc welding, and permissible loading of intermittently operated underground cables.

Standards are Released for Home Radio Parts

SIMPLIFIED STANDARDS for "War Model" home radio replacement parts have been prepared by the

American Standards Association in cooperation with OPA and WPB, and production of these parts is scheduled by manufacturers to start in April. The parts will be covered by price ceilings, will be constructed according to ASA performance and quality standards requiring minimum use of strategic materials, and will carry no private brand names. A special symbol consisting of the letter V above the Morse Code V inside a circle will appear on all parts.

The list of replacement parts constitutes a radical reduction from the thousands of different types of each item made before the war. The ASA list contains but nine paper capacitors ranging from 0.00025 to 0.25 μf, all with a d-c working voltage of 600 volts. Dry electrolytic capacitors are reduced to seven single units and two dual units, in various voltage ratings. There are eleven volume control values, six power transformers, two chokes, two interstage audio transformers, one driver audio transformer, and three output audio transformers.

Detailed data on "War Model" parts is given in the following three American War Standard bulletins: C16.8–1943—Simplified List of Home Radio Replacement Parts; C16.6–1943—Fixed Paper-Dielectric Capacitors (manufacturing specifications for home receiver replacement types); C16.7–1943—Dry Electrolytic Capacitors (manufacturing specifications). These are available at 20 cents each from American Standards Association, 29 West 39th St., New York City.

New Signal Corps Radio Sets

A COMBINATION WEATHER AND RADIO station no larger than a steamer trunk is one of many Signal Corps radio developments shown to newsmen at Fort Monmouth recently by Major General Dawson Olmstead, Chief Signal Officer. The unit can be buried on a hostile shore where weather observers could not stay, and will transmit reports every few hours on temperature, humidity and barometric pressure. Batteries provide two to three months of operation.

A combination transmitter-receiver weighing only 5½ pounds with batteries is now being furnished to parachutists by the Signal Corps so they can talk to each other while descending or after landing.

Another new Signal Corps radio set is designed to be attached to a parachute for the purpose of bringing aid to aircraft personnel in distress. It weighs 23 pounds, is powered by a hand-cranked generator, and is modulated by a code SOS signal recorded on a disc inside. The unit is sealed to the distress frequency to which all receiving stations with direction finders will listen the instant an airplane is reported as missing. Operation of the set requires no knowledge of radio code or theory. The normal coverage is 25 miles, but the signals can be received 500 miles away on favorable nights.

Duplication of Telephones In Philadelphia To Be Ended

TENTATIVE FCC APPROVAL of absorption of properties of the Keystone Telephone System by the Bell Telephone Co. of Pa. and the New Jersey Bell Telephone Co. paves the way for elimination of the last major competitive telephone installation in the United States. The Keystone system operates approximately 50,000 stations and 14 exchanges in Philadelphia and surrounding counties, and approximately 5000 stations in southern New Jersey.

Keystone service has been popular with Philadelphia business concerns because of special rate schedules which permitted unlimited service without message charges. The existence of two telephone systems in the same community made it necessary for many firms to have duplicate telephone service, however.

It is estimated that the merger will release for war use about 1500 tons of copper, 47 tons of zinc, 8 tons of tin and 2.5 tons of aluminum, salvaged from Keystone's underground cable system in Philadelphia and other duplicated facilities.

Telephone Inquiry Service Is Set Up in Washington

TO ELIMINATE CONFUSION and delays when businessmen seek information in Washington on war production problems, WPB has set up a Telephone Inquiry Service. The telephone number is REpublic 7500, Extension 73011, Washington, D. C. Competently trained specialists will answer the questions or refer the caller to the proper WPB official.

New Television Station Begins in Hollywood

EXPERIMENTAL OPERATION by television station W6XYZ in Hollywood began recently under the direction of Klaus Landsberg. The station uses 100 watts on television channel No. 4 (79.25 Mc) for video, and 200 watts on 83.75 Mc for the audio carrier.

W6XYZ is owned and operated by Television Productions Inc., a subsidiary of Paramount Pictures Inc. DuMont cameras and transmitting equipment are being used with several custom-built units and a special experimental antenna system.

To conserve equipment, only two programs weekly are planned at present. These programs will be confined almost entirely to Civilian Defense activities. Civilian defense workers assembled in Hollywood police stations and some 200 television-equipped homes will receive instruction via television.

WPB Orders 11,000,000 Tubes for Civilian Receivers

A PROGRAM CALLING for the manufacture of eleven million radio tubes in 114 different types by July 1 of this year for home radio receivers is now under way, according to a WPB announcement. The seven tube manufacturers cooperating in the program are: Hytron Corp., Ken-Rad Tube & Lamp Corp., National Union Radio Corp., Raytheon Production Corp., RCA Victor Division, Sylvania Electric Products and Tung-Sol Lamp Works. No manufacturer's names will appear on the tubes.

CBC Uses Relay Transmitters

ISOLATED REGIONS in western Canada are being provided with radio service by means of 20-watt relay transmitters connected to railway telegraph repeater stations. Six such low-power transmitters are in operation in British Columbia, and plans are under way to extend the service to all isolated communities on the 3000-mile network system of the Canadian Broadcasting Corporation. CBC field engineers found that the railway telegraph circuits acted as carriers for r-f signals, providing adequate radio reception within a radius of over 15 miles from the relay transmitter.

Radio Business News

ELECTRONIC CORPORATION OF AMERICA is the new name of the Transformer Corporation of America. Offices and plant have been moved to 45 West 18th St., New York City.

THE SCOPHONY CORPORATION OF AMERICA, with offices at 527 Fifth Ave., New York City, has been formed by Television Productions Inc., a subsidiary of Paramount Pictures, Inc., and General Precision Equipment Corp. The new enterprise controls the western hemisphere rights for the supersonic system of television developed by the British Scophony company in 14 years of research. Arthur Levey, president and general manager, announces that his new firm will soon make available in this country a large-screen television projection system which is easily adaptable to color.

ADDITIONAL PLANT FACILITIES for Ken-Rad Tube and Lamp Corp. will be constructed in Indiana and Kentucky under a $1,300,000 Defense Plant Corp. contract.

BUDD INDUCTION HEATING, INC. announces that its new plant in Detroit, Mich. is now at full production, filling war orders for vital induction heating equipment.

FOLLOWING COMPLETION of a program of plant expansion providing additional facilities for electronic research, Hazeltine Service Corporation changed its name to Hazeltine Electronics Corp.

THE G-E RADIO, Television and Electronics Department will henceforth be known simply as the Electronics Department.

RADIO AND DETECTION equipment production for military and civilian use—chiefly military—exceeded $1,200,000,000 in 1942 according to WPB Chairman Donald M. Nelson. This was more than three times the volume of 1941.

EMBY PRODUCTS CO., INC. announces a change in name to Selenium Corp. of America. The firm manufactures Emby photoelectric cells, selenium rectifiers and other electronic products, and is located at 1800 West Pico Blvd., Los Angeles.

ACRO ELECTRIC CO., manufacturers of Acro snap switches, has moved into a new plant at 1305 Superior Ave. in Cleveland. Manufacturing facilities and space have been enlarged 300 percent for increased production.

INTERNAL REVENUE TAX collections for radio sets, parts, phonographs, manufactured in Jan. 1943 amounted to only $186,688, as compared with $2,650,829 for Jan. 1942. Interstate communication revenue for the same periods remained essentially the same, but taxes for local telephone service jumped almost a million dollars, from $4,280,926 in Jan. 1942 to $5,033,317 this January.

Data on New Tubes

2C21 High-vacuum heater-type twin triode with small 7-pin base 7BH and ST-12 glass envelope. $E_f = 6.3$ v; $I_f = 0.6$ amp; max $E_b = 250$ v; max power = 2.1 w; $I_b = 8.3$ ma; $r_p = 7600$ ohms; $r_L = 20{,}000$ ohms; $E_c = -16.5$ v; $\mu = 10.4$; $g_m = 1375$.

3B23 High-vacuum heater-type full-wave rectifier with 4-pin medium bayonet base 4AN and S-19 glass envelope. $E_f = 2.5$ v; $I_f = 8$ amp; max a-c $E_b = 1250$ v per plate; $E_{inv} = 3500$ v; max d-c $I_b = 0.2$ amp; $I_{peak} = 0.6$ amp per plate.

6SH7GT High-vacuum heater-type r-f pentode with 8-pin octal base 8BK and glass envelope. Single-ended, with sharp cut-off. $E_f = 6.3$ v; $I_f = 0.3$ amp; max $E_b = 300$ v; max power = 3 w; $g_m = 4900$; $r_p = 0.9$ meg.

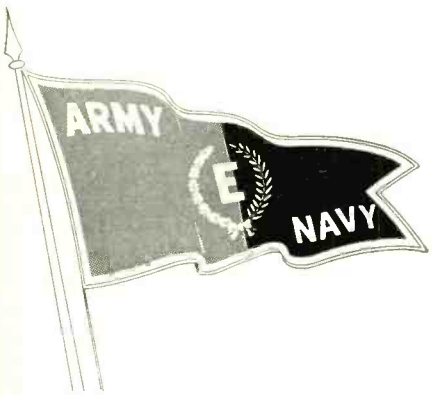
1005 Gaseous ionic-heated-cathode full-wave rectifier with 8-pin octal base 5AQ and MT-8 metal envelope. For starting, $E_f = 11.0$ v and $I_f = 0.125$ amp; continuous, $E_f = 4.0$ or 6.3 v and $I_f = 0.08$ or 0.1 amp. Max peak voltage per anode = 225 v; max peak inverse voltage = 450 v; average tube voltage drop = 20 v; max d-c anode current = 70 ma.

8020 High-vacuum filament-type half-wave rectifier with 4-pin medium bayonet base 4P and T-18 glass envelope. $E_f = 5$ v; $I_f = 6$ amp; $E_{inv} = 40{,}000$ v; average $I_b = 100$ ma; $I_{peak} = 750$ ma.

0B3/VR90 Gas-filled cold-cathode regulator tube, now assigned a regular RMA number. Double branding is employed in view of long usage of the older designation VR-90-30. The

operating voltage drop across the tube is 80 to 100 volts (design center value is 90 volts).

0D3/VR150 Gas-filled cold-cathode regulator tube, now assigned a regular RMA number. The operating voltage drop across the tube is 145 to 160 volts (design center value is 150 volts).



COLONIAL RADIO CO.
Buffalo, N. Y.

CORNING GLASS WORKS
Corning, N. Y.

ELECTRONIC LARORATORIES, INC.
Indianapolis, Ind.

FARNSWORTH TELEVISION & RADIO CORP.
Marion, Ind.

FORMICA INSULATION CO.
Cincinnati, Ohio

C. O. JELLIFF MFG. CORP.
Southport, Conn.

P. R. MALLORY & CO., INC.
Indianapolis, Ind.

REPUBLIC STEEL CORP.
Cleveland, Ohio.

SOLAR MFG. CORP.
Bayonne, N. J. and West New York, N. J.

SPRAGUE SPECIALTIES CO.
North Adams, Mass.

WINCHARGER CORP.
Two plants
Sioux City, Iowa

Personnel

Dr. Joseph Slepian, associate director of research at Westinghouse, has been selected by the AIEE to receive the 1942 Lamme Medal. The award is for "contributions to the

development of circuit-interrupting and current-rectifying apparatus."

I. R. Baker, one of radio's best-liked pioneers, died suddenly of a cerebral hemorrhage on Feb. 19 while at his office at RCA Mfg. Co. in Camden. From 1929 to the outbreak of the war he had been head of broadcast transmitter sales at the Camden plant, and since then had been devoting most of his time to research in applying high-frequency radio current to speed up war production.

T. A. Willard, storage battery inventor and former president of the Willard Storage Battery Co., died Feb. 3 at his home in Beverly Hills, Calif. at the age of 80. After more than 30 years spent in inventing devices for storage batteries, for which 65 patents were awarded, he retired from business and devoted his time to a study of Mayan culture and to frequent trips of exploration to Yucatan. His four books on Mayan culture have made him an authority on the subject.

William Fay and Fred C. Young, vice-president in charge of broadcasting and vice-president in charge of engineering respectively, are among the newly-elected directors of Stromberg-Carlson Tel. Mfg. Co.

Dr. W. R. G. Baker, G-E vice-president, outlined the future of electronics in a talk before a recent New York section meeting of the American Marketing Association. He cautioned against expecting f-m and television sets to sell for $9.95 after the war, and pointed out that it will take time to apply war-acquired knowledge to peacetime practice.

G-E vice-president Dr. W. R. G. Baker (center), who warned against expecting an overnight flood of new products after the war, is shown here with AMA radio group chairman George H. Allen (left) and Dr. H. S. Hettinger of OWI in Washington, other speakers at the American Marketing Association meeting

W. C. White, engineer in charge of the G-E Electronics Laboratory at Schenectady, has been named a member of the IRE board of directors. He has played a leading part in all G-E radio tube developments, and from 1929 to 1941 was in charge of the Vacuum Tube Engineering Department.

Dr. L. Grant Hector has joined National Union as Director of Engineering, and will direct all electronic tube research and engineering activities for laboratories and

manufacturing plants of the company in Newark, N. J. and Lansdale, Pa. Previously he had been engaged in electronic development work for the Office of Scientific Research and Development.

S. Caplan, after nine years as research chemist with Harvel Research Corp., has become research manager and acting technical director of Irvington Varnish and Insulator Co. of Irvington, N. J. He succeeds C. F. Hanson, who has been appointed chief consulting engineer and will be responsible for expediting technical work on war production.

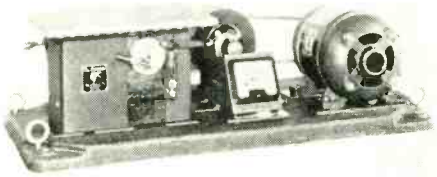
Radio and Radar Advisory Committee, under the direction of WPB radio and radar officer Ray Ellis, now includes the following members from industry: Max Balcom of Sylvania, M. Cohen of F. W. Sickles Co., W. P. Hilliard of Bendix Radio, W. F. Hosford of Western Electric Mfg. Co., E. E. Lewis of RCA, Percy L. Schonen of Hamilton Radio, and Al Wells of Wells-Gardner Co.

NEW PRODUCTS

Month after month, manufacturers develop new materials, new components, new measuring equipment; issue new technical bulletins, new catalogs. Each month descriptions of these new items will be found here

Variation Fatigue Test Equipment

MODEL 25 VIBRATION fatigue testing machine was designed for heavier vibration fatigue testing equipment. Its table load capacity is 25 lbs. and its horizontal table movement frequency range (adjustable) is rated 10 to 60 cps. Table area is 12x15 inches. Total displacement (adjustable) is 0 to 0.125 inches. Maximum acceleration is approximately 14 g. The machine is mounted on a sturdy cast iron base measuring 19x38 inches. Base mounting hole dimensions are 16x25 inches. The table top over all height is 11 inches from the bottom of the base, and provides adequate clearance above the machine to permit handling of parts larger than the table dimensions. Total net weight of the machine is 365 lbs. It is powered by a 1-hp, 220-volt, a-c motor. No keys or wrenches are needed to make an accurate adjustment of amplitude. Rugged Timken and SFK bearing are used in the machine. The manufacturer states that the machine runs cool, will operate unattended for hours, and will not spill oil. An accurate electric tachometer is provided for frequency readings, and the machine is guaranteed for one year against defective material and workmanship.



All American Tool & Mfg. Co., 1014 Fullerton Ave., Chicago, Ill.

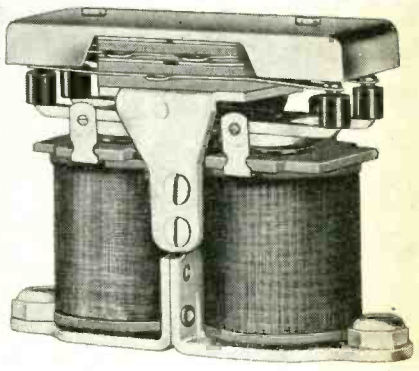
Kilovoltmeter

SPECIFICATIONS of No. 760 kilovoltmeter include a low current consumption (not more than 1 ma); all multiplier units are an integral part of the self-contained instrument; three ranges are 5, 10 and 20 kv; plus or minus 2 percent accuracy at full scale; and sensitivity of movement, 1000 ohms per volt.

The instrument is rugged and portable and is obtainable from Shallcross Mfg. Co., Collingdale, Pa.

Double Armature Relay

THIS RELAY is a double action interlocking control unit with balanced armature control. It is ruggedly built to withstand vibration and sudden shocks of mobile applications, and can be custom built to fit into designs where light weight and small size are essential. It is available in various contact arrangements or with Micro switches (in place of spring pile-ups). Capacities are rated up to 5 amps, 110 volts a.c. Coil resistance is 10,000 ohms. Contact tact forms or assemblies have up to 12 springs on each side.



Cook Electric Co., Chicago, Ill.

SURE..

PREFERENCE RATINGS DRIVE US NUTS TOO

What with rating requirements and priorities, aspirin has become an important part of our office equipment. But we swallow them cheerfully and tackle our extra work with enthusiasm, for, in spite of the headaches, we've developed a *better* Audiodisc, we're filling more orders than ever before in our history — and Audiodiscs are actively helping the war effort. Naturally, we realize too that these priority restrictions are essential. Audiodiscs do contain some critical materials. Proper control enables us to get these materials and thus maintain the superior quality and dependability found only in Audiodiscs. Recently the preference rating procedure on recording blanks and cutting points has been greatly simplified. So help us speed up your deliveries by sending in your preference rating extensions with your orders. Thanks a lot!

This war may be bringing us headaches, but there is a lot of satisfaction in knowing that Audiodiscs are doing their part for Victory . . . bringing messages and music to boys at the front and training camps . . . reaching millions of our allies and friends in Axis-conquered countries . . . presenting the truth to thousands who listen even in enemy countries . . . recording important speeches and up-to-the-minute news . . . transmitting messages and instructions in war plants . . . releasing wires for wartime communications, and performing many other highly important roles on both the home and fighting fronts.

Whatever your particular application, Audiodiscs will serve you with the same characteristic dependability, under the most exacting conditions, that wins for them universal acclaim, wherever they go on a turntable. Audiodiscs are readily available through a coast-to-coast network of distributors. Call your nearest one — or wire us for complete information today. Audio Devices, Inc., 1600 Broadway, New York City.

AN IMPROVEMENT—NOT A SUBSTITUTE THANKS TO PRIORITIES

With no more aluminum available, Audio's recording engineers, stepped in and developed the superior 4-hole, glass base Audiodisc which contains all features essential to high-fidelity recording—superior coating formula and process—flawlessly smooth, non-deteriorating surface — improved tracking — controlled thread action — reduced static—longer playback life—thin, flexible glass base with correct strength-to-weight ratio—center hole and all three drive-pin holes in non-chipping fibre insert (patented) — complete interchangeability with pre-war aluminum-base types — safe, dustproof packing cases — special reshipping cartons.

THERE'S AN AUDIODISC *designed and priced* FOR YOUR SPECIFIC NEEDS

audiodiscs

— they speak for themselves

RED LABEL · YELLOW LABEL · MASTER REFERENCE RECORDING AUDIODISCS

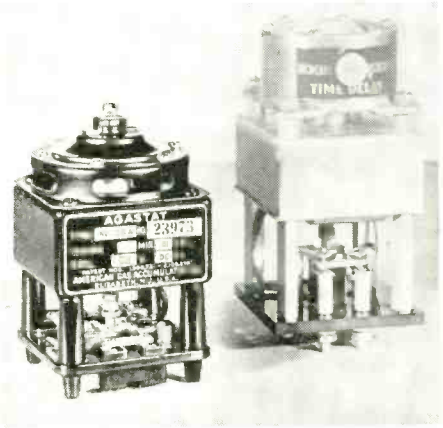
Voltage Regulator

A NEW TYPE VOLTAGE regulator controls the voltage delivered to a vibrator used for airplane service, by the use of an automatic thermal switch which automatically turns on any auxiliary circuit ten seconds after the vibrator is started. (Similar regulators can be designed to control the current and voltage applied to any load, providing the total wattage consumed by the regulator itself is not more than 40 watts.) With a battery variation of 20 to 30 volts (50 percent), the voltage on the vibrator is kept between 6.0 and 6.3 volts (5 percent) variation. With a 10 percent change in current through the regulator, the voltage drop increases 200 percent.

Amperite Co., 561 Broadway, New York, N. Y.

Time Delay Relay

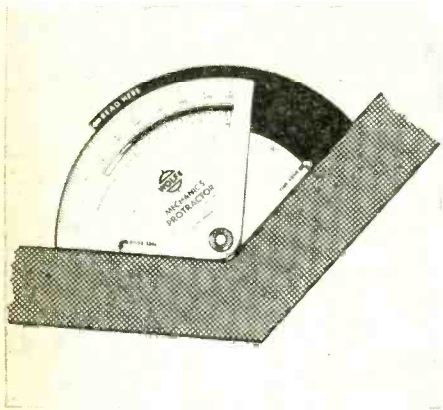
IN THE RE-DESIGN of Agastat (an electro-pneumatic time delay relay for making or breaking electrical circuits at pre-determined intervals) the basic design and principle of operation were adhered to, but the newer model weighs 1 lb and 6 ozs less than its predecessor (actual weight being 1 lb and 6 oz) and it is only 4 inches high in comparison to the older model's 5 inch height. Another difference is in the housing and component parts which are made of substitute materials, although heavy brass is used in the operating mechanism. A simple screw adjustment permits a delay ranging from a fraction of a second to several minutes. The relay is unaffected by heat, cold or variations in operating voltage, temperature or humidity.



American Gas Accumulator Co., Elizabeth, N. J.

Mechanic's Protractor

ESPECIALLY DESIGNED for the man on the job is a mechanic's protractor which gives readings for outside angles (such as angles of bend or deflection), or inside (inclusive) angles, or inches-per-foot against degrees up to 24 inches-per-foot (63 deg.–26 inches). All of the above mentioned readings can be taken with one setting. The more difficult angles can be measured by using a bevel in conjunction with the protractor. The calibrations are located at the extreme of the radius, assuring accurate, clear reading to a fraction of a degree. The protractor is printed in red on ⅛ inch-thick phenol-resin laminated birch. It is light and durable and is unaffected by grease or water. Prices are $1.00 for one protractor, 90¢ each for two, 85¢ each for three, and 80¢ each for twelve or more, to be remitted when ordering, from the Interstate Sales Co., 1123 Broadway, New York, N. Y.



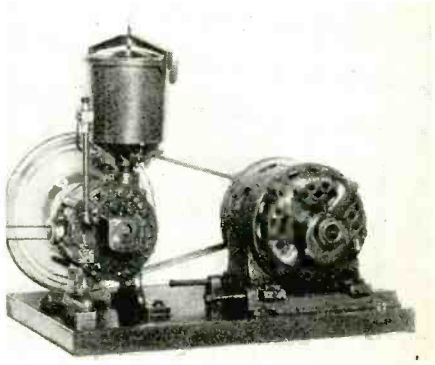
Pilot Light Assembly

JEWEL LIGHT assembly, No. 675 Type, has a one-inch jewel and is designed for horizontal mounting on panels measuring up to one-half inch thick. Its outstanding features are heavy-duty construction, and double contact candelabra bayonet socket which is housed in a thick black Bakelite base. Any double contact, candelabra-sized bayonet base lamp with C7, G6, S6, or T4½ bulb-size can be used. The assembly is available in jewels of smooth, colorless frosted-back glass—with a removable color disc or a diamond-cut (faceted) colored glass. A bezel, which holds the jewel permits easy removal of lamp from panel front.

Drake Mfg. Co., 1731 West Hubbard St., Chicago, Ill.

Vacuum-Creating Outfit

A UNIT WHICH produces and maintains vacuum or pressure needed to test delicate instruments, such as directional gyros, artificial horizon instruments, altimeters, etc., is a motor-driven rotary pumping unit



which is furnished with full automatic controls and automatic lubrication. The vacuum or pressure may be adjusted to any degree desired. The machine is slow-running and quiet in operation.

Lieman Bros., Inc., Christie St., Newark, N. J.

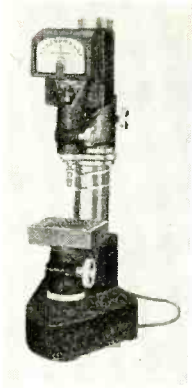
Throat Microphone

FOR USE IN AIRCRAFT, submarines, military tanks, defense plants and other noisy places, this is an improved throat microphone which is placed around the neck, over the larynx. Words spoken by the wearer are picked up and may be amplified and transmitted through a PA system. No surrounding noise is transmitted through the microphone. Any standard amplifier designed to use a crystal or other high impedance microphone may be used with the microphone. The microphone is constructed on the inductor-dynamic principle, and is rugged and compact (weighs 2 ounces). It is leather covered and equipped with an adjustable neck strap.

Miles Reproducer Co., Inc., 812 Broadway, New York, N. Y.

Electronic Armament Gauge

AN ELECTRONIC GAUGE capable of indicating differences as small as 0.00002 inch in metal objects up to eight inches in diameter or length is announced by Televiso Products, Inc., 6533 No. Olmsted Ave., Chicago. Indications appear on a four-inch meter scale having ranges of



plus or minus 0-0.0005, 0-0.005, and 0-0.05 inches. Ranges are changed by means of a selector switch. In use, a standard work piece is placed under the feeler point and the instrument is adjusted to give a zero reading (at mid-scale). Deviations of production pieces from standard can then be read directly on the scale by unskilled operators as fast as parts can be placed under the feeler point. The instrument is known as the Model 11 Micrometron, and is available on priority only.

Phenolic Plastics

PHENOLIC MOLDING material, BM-13017, is designed especially for the production of aircraft and automotive ignition parts. The material is natural colored and is suitable for extrusion molding around inserts.

Type BM-16034 phenolic molding plastic was developed for long flow extrusion work. It may also be used for transfer molding.

Physical and electrical molded properties are available from the manufacturer, Bakelite Corp., 30 East 42nd St., New York, N. Y.

Screw-On Type Wire-Nuts

NO RUBBER, tin or lead are used in these "Wire-Nuts" (solderless, tapeless wire connectors) which consist of a cone-shaped spiral spring insert which is imbedded in a molded insulation. The nuts utilize insulation which will not melt and is puncture-proof at 10,000 volts. Five sizes are available for making all combination of wires from 2 No. 18 to 3 No. 10, solid or stranded. The nuts are approved by Underwriters' Laboratories, and Factory Mutual Laboratories.

Ideal Commutator Dresser Co., Sycamore, Ill.

Voltage Stabilizer

THIS INSTRUMENT provides a constant output of 115 volts from circuits varying between 95 and 130 volts. It is insensitive to load power factor, and is not affected by variations in load from no load to full load, or by changes in power factor from unity to 0.8 lagging. Completely self-protecting, it will operate continuously throughout the range from open circuit to short circuit without damage. Ratings from 50 volt amps to 5000 volt amps are available. The new stabliizer can be applied wherever close voltage regulation is needed, such as in radio transmitters, electron tube apparatus, motion-picture sound equipment and projectors, x-ray machines, etc.

Publication GEA-3634 which describes the stabilizer in detail is available from General Electric Co., Schenectady, N. Y.

Tube Stud Connector

A NEW TUBE STUD connector (called Hystud) has been developed for use in joining flexible leads to filament studs of large electronic tubes. It is

an indent-type of connector and is compact. The connector is assembled to the stud by means of a knurled thumb screw.

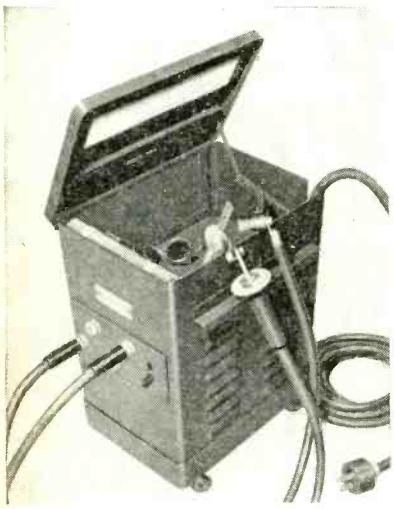
Burndy Engineering Co., Inc., 459 East 133rd St., New York, N. Y.

Modern War Sound Effects

AUTHENTIC SOUNDS of warfare such as the sound of Spitfires, Messerschmitts, and other modern fighters and bombers in various flight maneuvers, dogfights, dives, and ground battles with tanks, falling bombs, machine-gunning, etc., are available on Super-Sound Effect records. These sound effects are pressed on Victrolac. A catalog supplement giving descriptions of other effects may be obtained from Standard Radio, 45 West 45th St., New York, N. Y.

Fuse-Bond Process

MACHINE COMPONENTS and similar metal parts may be prepared for metallizing electrically by a new process called "Fuse-Bond". It is claimed that this process affords an adequate bond on the hardest surfaces, and it also simplifies preparation of narrow edges, flat areas, and cylindrical parts having keyways and other interruptions in their surfaces. Available with this process is a unit (Type C is illustrated) which operates on any 110 or 220 volt, single phase power line. The equipment fuses a rough deposit of electrode metal onto a surface to be metallized.



The Unit is compact, and is contained in a cabinet measuring 24 inches high. It weighs, complete, 170 lbs. All cables and attachments fit into a bin in the top of the cabinet. The unit is mounted on casters and can be wheeled right to the job with ease. A complete instruction manual provides all operating data. The manufacturer states unskilled labor can operate the unit efficiently within an hour or so.

Further information on the process and its equipment contained in Bulletin 44, is obtainable from the manufacturer, Metallizing Engineering Co., Inc., Long Island City, N. Y.

Instrument Washer

AN INSTRUMENT WASHER which is electric and portable is available for washing and cleaning aircraft, tank, automobile and navigation instruments, as well as indicating and control units, carburetors, gear trains, mechanism. It may also be used for production cleaning of small parts

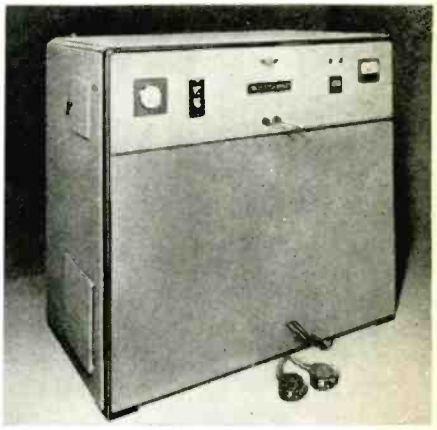
such as screws, small electrical units, distributor and relay parts, and other odd and complicated shapes of various materials. The material which is to be cleaned is put into any one of the four to six separate trays. The trays (which serve to keep disassembled parts together) remain stationary while a cleansing liquid circulates through the washer. Any of the trays may be removed without stopping or disturbing the other work in the machine. The compartments may be lifted out to accommodate larger parts which may have to be cleaned. A drain well is contained at the bottom of the machine for dirt elimination.

The machine measures 26 inches high x 18 inches in diameter. The weight is 50 lbs.

Naxon Utilities Corp., 2101 Walnut Street, Chicago, Ill., are the manufacturers.

Induction Heating Units

NEW INDUCTION heating units for surface hardening, brazing, soldering, and other heating applications requiring localized heat are available in sizes of 16 kw and 32 kw. Each machine is a completely enclosed unit readily adaptable for low cost hardening and heating of many parts which are manufactured in small lots, or they can be incorporated into any production line. The

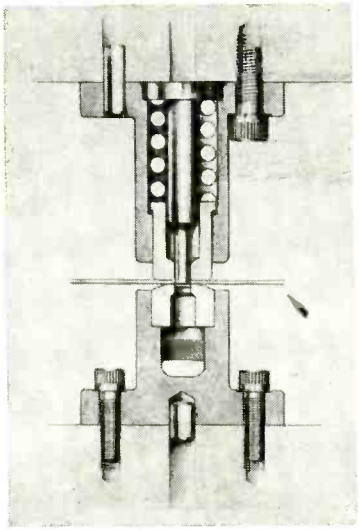


machines are easy to operate and in changing from one job to another, the operator simply changes the work-holding fixture and heating coil and resets the heating cycles to meet the new requirements. The entire heating operation is automatic. Bulletin 2-1-42-5M describes the units in more detail. Quenched spark gaps are used.

Van Norman Machine Tool Co., Springfield, Mass.

Hole Punching Units

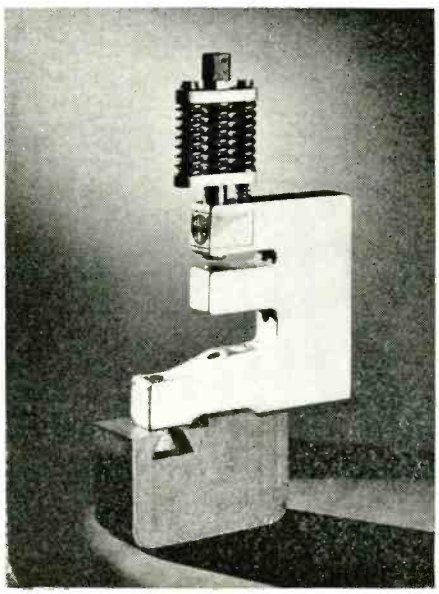
WALES CD UNITS are sets of punch units for use in conventional die sets. The punch half of the unit contains a punch with a pilot, a holder, a stripping spring, and a guide. The die half of this set consists of a holder with a slug clearance chute, and a die. Each unit is self-contained and may be independently mounted to either the punch or the



die shoe. Broken or dulled parts may be changed easily without breaking down the entire die set. Punch and die alignment is automatically assured through the use of a pilot pin which is centered on the punch or die.

These units may be used in either punch presses or press brakes to punch holes from ⅛ to 1¼ inches diameter in metal which measures up to 11 gage.

ANOTHER UNIT is the flexible Type E unit designed for punching a ser-

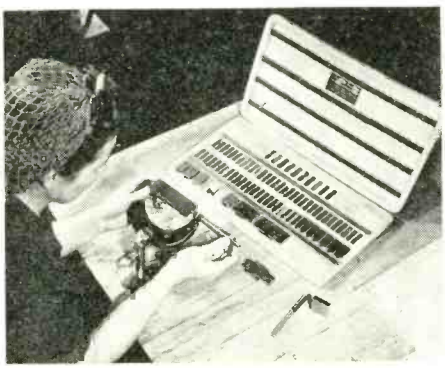


ies of holes in extruded shapes on press brake. Nothing is attached to the press. Each unit is made up of punch, die, holder, stripping spring and guide. The punch and die are held in perfect alignment. A line-up of units may be set up to punch over 200 holes at the same time on a rail.

The Strippit Corp., 345 Payne Ave., North Tonawanda, N. Y.

Gage Blocks

DOALL MASTER GAGE Blocks are available in a standard set (Set 400) and consist of 81 blocks. The 81 individual blocks range in length from 0.050 inches to 4.00 inches. These precision gage blocks are produced in "AA" grade (accuracy 0.000002 inch), "A" grade (accuracy 0.000004 inch), and "B" grade (accuracy 0.000008 inch). Each gage block in addition to being accurate in length, has its measuring surface lapped to a flatness of less than the quarter wavelength of light, and is produced with a mirror finish. These two factors enable the blocks to be wrung together in combination, enabling the user to secure practically any dimensions in steps of 0.00001 inches from 0.1000 inches to 12.00 inches.



The illustration shows Doall gage blocks in a mahogany case supplied with the gages. The inspector is checking a 4 inch micrometer. The manufacturer states that precision optical measuring instruments are used to check the accuracy of gage blocks produced, and this equipment is also available to users for rechecking their gage blocks after they have been in use. The used gage blocks sent in will be recalibrated and gages that have been worn beyond tolerance of the original set are replaced to maintain the required standards of accuracy.

Savage Tool Company, Savage, Minn.

Stamping Equipment

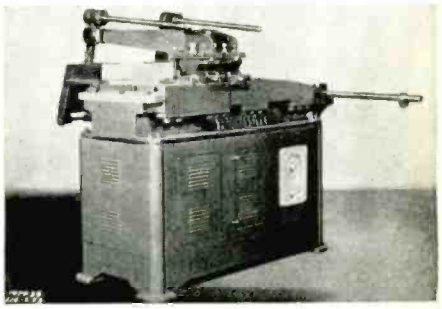
TWO PRODUCTS AVAILABLE from The Acromark Co. (323 Morrell St. Elizabeth, N. J.) includes a foot-operated stamping machine and a holder for stamping with steel type.

NO. 1-F FOOT-OPERATED name plate and parts stamping machine is a pedal-operated unit which allows an operator's hands to be free for feeding. This pedal feature is available in Models 1, 5 and 7 which may be used to mark steel, brass, bronze, zinc, tin, fibre, celluloid and plastics. The size and height of the machine permit installation in a production line where the machine may be needed. Thickness adjustment ranges from zero to $\frac{3}{4}$ inch. Standard die sizes range from $\frac{1}{8}$ inches to $\frac{3}{16}$ inch in size. Each machine comes with a marking head (any specified size), with a full alphabet and set of figures and punctuation marks.

For marking multiple characters that change, the Heavy Duty Hercules holder is available for stamping with steel type. A holding clip allows type to be quickly changed by thumb pressure on the top of the clip as shown by the illustration. The type used is a heavily built shoulder style type. The holder is made from heavy tool steel bar stock and is available in larger sizes.

Standardized Flash-Welders

THE FIRST OF A SERIES of standardized flash-welders, recently announced, further expands the manufacturer's line of products which

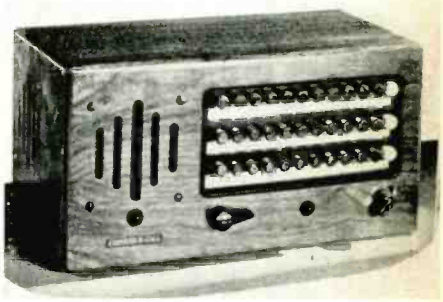


now includes all forms of resistance welding equipment from guns and fixtures to seam, projection, rocker arm and pedestal type welders, etc.

Progressive Welder Co., 3100 Outer Drive, Detroit, Mich.

Inter-communicating System

"CONVERS-O-CALL" is the name of an intercommunicating system which is available for ten to thirty stations. It is designed as an all-in-one master system to facilitate fac-



tory and office inter-communications. The system is easy to install and to operate and may be utilized, if necessary, for music transmission to employees.

Fred E. Garner Co., 53 E. Ohio Street, Chicago, Ill.

Liquid Coating Prevents Adhesion of Welding Spatter

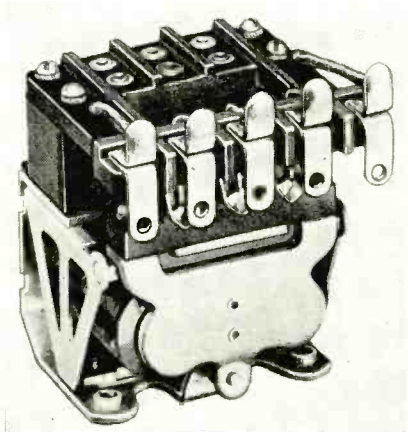
A LIQUID COATING called "No-Spat" resists rust, will not freeze, and may be used over the full welding range of amperage and voltage. Adhesion of welding spatter is prevented when the coating is brushed over the seam and area where weld spatter may fall. After welding the spatter may

be wiped away and no chipping or grinding is necessary. Two other features claimed for the coating is that it fuzes with the molten and maintains maximum tensile strength by floating off impurities and preventing porosity, and that it stabilizes the arc and thus minimizes rod spatter and saves rod metal. Another application suggested by the manufacturer is that of coating the jig to prevent spatter from throwing the production job out of alignment.

The Midland Paint & Varnish Co., Cleveland, Ohio.

Relay

DEVELOPED FOR AIRCRAFT as well as other uses, 3PDT Type 27 relay, No. 12814, measures 2 x 1⅞ x 2⅛ inches and weighs 5 ounces. Its characteristics are as follows: Acceleration, 15 g plus; nominal coil voltage, 12 volts, d-c; pick-up, 6.5 volts (0.92 watt) at 20 deg. C.; coil wattage at 12 volts d-c is 3.2 watts; contact

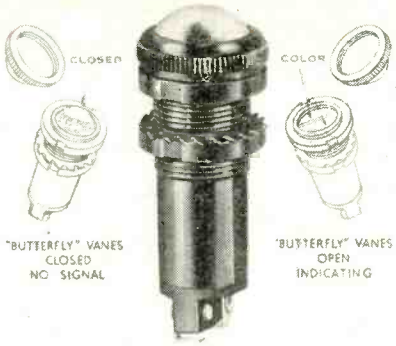


pressure, 60 grams; contact capacity, 10 amps at 30 volts, d-c; and temperature rise 32 deg. C., at 12 volts, d-c. Free samples of this relay may be had if requests designate specification number 12814 and if accompanied by a priority rating of AA-4 or better.

G-M Laboratories, 4326 N. Knox Ave., Chicago, Ill.

Signal Indicator

"SIGNALETTE" is the name of a new signal indicator for use in aircraft or wherever a signal light is used. It is designated as No. 1534. Indication is entirely by reflected light and radio activity. Indications are made in sunlight or daylight, black-light

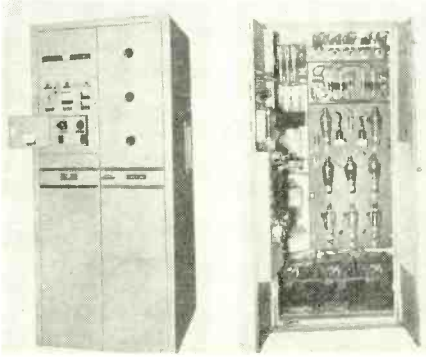


or no light. It is available with red, amber, green or white butterfly vanes. The overall length is $2\frac{5}{32}$ inches and is available for mounting on panels up to $\frac{3}{8}$ inch thickness. The gadget may be interchanged with signal indicator (AC 42B3529) now used in aircraft. The indicator is protected against shattering by the use of a transparent plastic cap which withstands shock or explosion and which permits free penetration by ultraviolet rays.

Littlefuse, Inc., 4757 Ravenswood Ave., Chicago, Ill.

Electronic Control for Resistance Welding of Aluminum

ONE OF THE FEATURES of this welding control is its simple construction which facilitates thorough inspection and servicing. The control utilizes the energy-storage principle, and provides very high currents and short welding time. The control consists of a charging circuit, a discharge circuit, control station, Pyranol capacitors, and sequence control. All this equipment is mounted in one cabinet-type enclosure with full-length front doors and removable rear covers. The enclosure is ventilated by filtered air which creates a positive pressure within the cabinet and minimizes the infiltration of dust and dirt. The main



anode transformer and tubes are air-cooled. The charge and discharge tube circuits are mounted on a single base that can be swung out readily for servicing. The control station may be removed from the cabinet and attached to a welding machine at any remote point.

General Electric Co., Schenectady, N. Y.

Literature

Radio Servicing and Buying Guide. A pocket-sized manual, written by Major J. G. Tustison, U. S. Army Signal Corps, describes practical methods for serving electronic and radio devices. This manual includes color code information on resistors, speaker lead and plug connections and a conversion table of fractional inches to decimal and millimeter equivalents. The price of this manual is ten cents, requests on firm letterheads from engineers maintenance and serviceman will be sent free.

A 1943 Buying Guide covering radio and electronic materials and parts includes detailed listings of transformers, resistors, condensers, rheostats, relays, switches, rectifiers, electronic tubes, tools, wire and cable, batteries, sockets, generators, power supplies, converters and other types of equipment in this field. One section is devoted to sound equipment and accessories and another section contains a technical book section on radio, electronics and electricity.

Both the radio servicing manual and buying guide may be obtained from Allied Radio Corp., 833 W. Jackson Blvd., Chicago, Ill.

Solders. In a 6-page folder substitute solders, regular solder and the solving of solder problems is described. A lead-tin fusion graph is included. Among solders described are fusible alloy, or low melting point solder; wire solder, for automatic processes and special operations; ribbon solder, for the sweating of parts; foil, for joining two flat surfaces; acid and rosin cored solders; drop solder and special solders. Alpha Metal Rolling Mills, Inc., 363 Hudson St., Brooklyn, N. Y.

Electrical Connectors. This AN Electrical Connector bulletin contains general information and tabular matter which meets Army and Navy specifications. The following types of AN connectors are shown: AN3100, wall mounting unit; AN3102, box mounting unit; AN3106, straight connector; AN3108, angle 90 deg. connector; AND10066, integral mounting and special plugs adaptable to points of high vibration. 167 insert arrangements with wire data are included. There are also pages on junction shells, AN cable clamps, dust caps, dummy or stowage receptacles and cannon bonding ring. The Cannon catalog condensed supplements are included in a separate section. Copies from Dept. U, Cannon Electric Development Co., 3209 Humboldt St., Los Angeles, Calif.

Pilot Light Assemblies. The pilot light assemblies for marine, aircraft, Signal Corps and industrial applications illustrated in this 8-page catalog are standard items made by this company. A complete range of the various types and sizes are covered; included also are dimensional diagrams and prices. Special assemblies are designed and built for specific requirements. Gothard Mfg. Co., Springfield, Ill.

Transformers. Bulletin 159 lists standard specifications and mounting means of audio, driver, interstage and microphone input transformers and reactors for aircraft equipment and transmitter transformers and reactors for mobile equipment. Specifications covering each unit are included. Bulletin 159 available from Acme Electric and Mfg. Co., Cuba, N. Y.

Blind Rivets. A handbook which tells how to save time on difficult riveting jobs. The book tells how rivets are used for airframe construction, field repair and airframe salvage. Methods of specifying rivets, grip length, handling and storing rivets, preparation and drilling material, operation and care of riveting guns, gun accessories and interchangeable pulling heads are given in the handbook. Charts on material thickness and standard rivet sizes are also included. Copies from Dept. 29, Cherry Rivet Co., Los Angeles, Calif.

Backtalk

This department is operated as an open forum where our readers may discuss problems of the electronic industry or comment on articles which ELECTRONICS has published

Stroudsburg, Pa.

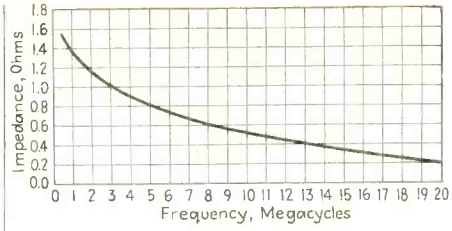
Condensers at R.F.

WHY DOES AN electrolytic condenser have a relatively high impedance to r.f.?

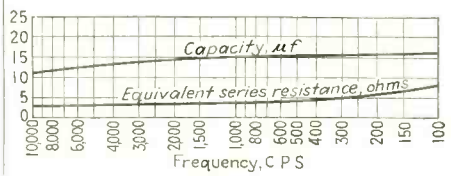
✦ An electrolytic capacitor has a relatively high value of impedance at r.f. because at these frequencies it no longer functions as an electrolytic capacitor. Furthermore, the impedance at r.f. is not a function of definite values of capacitative reactance and resistance but rather the impedance of a somewhat complex network containing inductively reactive elements as well as capacitative reactance and resistance.

In the basic construction of an electrolytic capacitor, one conductive surface is metallic and the other conductive surface is an electrolyte. The electrolyte has appreciable resistance and as conduction through such an electrolytic path is by ionization, the resistivity of such a path is subject to considerable change under varying conditions of both frequency and temperature. Under conditions of extremely low temperatures the mobility of the ions is greatly reduced with resultant large increase in resistivity. Also, at high frequencies, the relatively large mass of an ion is too great to permit the requisite speed of movement through the electrolyte path to provide proper conductivity. In other words, the specific resistivity of the electrolyte increases with increase in frequency, until a condition is reached where the electrolyte becomes substantially non-conductive and begins to function as a dielectric.

During this transition there has been an increase in the equivalent series resistance of the electrolytic capacitor structure with proportional increase in power factor and impedance. At the point, however, where the electrolyte becomes effective as a dielectric medium, the normally operative dielectric (the anodic film of aluminum oxide) no longer is effective in determining the capacitance of the structure. Under these new conditions the structure now becomes a purely electrostatic device and the cathode foil, normally employed to only make contact with the electrolyte, becomes the other conduc-



Radio frequency characteristics, dry electrolytic condensers, etched anodes



Audio frequency characteristics of dry, etched anode electrolytic condensers

tive surface of the electrostatic structure. This electrostatic structure now consists of: two metallic conducting surfaces separated by two dielectric mediums in series, namely; the aluminum oxide film and the now non-conductive electrolyte. The effective capacity is now determined by the geometry of the structure if other factors do not have to be taken into consideration.

At the higher frequencies, the foil surfaces represent appreciable values of inductive reactance. Also, the now non-conductive electrolyte represents a polar-molecular dielectric structure of extremely poor dielectric properties. These two conditions prevent the capacitative reactance of this electrostatic structure from closely following the requirement that X_c equal $\frac{1}{2\pi fC}$, with the result that a given electrolytic capacitor structure does not appreciably change impedance with change in frequency. The graph of impedance vs frequency illustrates this characteristic.

In almost all filter and by-pass circuit applications, the dry electrolytic capacitor has a sufficiently low value of r-f impedance to meet circuit stability requirements but should the occasion arise where such is not the case then the electrolytic capacitor must be shunted with a mica dielectric or other type of capacitor which will provide the requisite low impedance path.

Circuit instability is frequently encountered in very high gain amplifiers where the r-f impedance of an electrolytic capacitor represents an impedance common to all parts of the circuit and thereby provides sufficient coupling from output to input to cause effective feedback. The correction for this condition has already been mentioned.

Similar conditions of common impedance coupling also sometimes result where three or more capacity sections are concentrically wound with a common cathode foil member in the electrolytic capacitor. In such cases of multiple capacitor structures, the com-

mon cathode foil itself is the source of common impedance coupling. The corrective measure in such instances is to employ separate electrolytic capacitor sections.

PAUL MCK. DEELEY

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Feedback

IN DERIVING a formula for the improvement in signal-to-noise ratio when negative feedback is applied to an amplifier, it appears that a serious error in logic has been made and as a result the formula generally stated in all the standard texts is entirely erroneous, even though mathematically it may be correct.

The fact is, and mathematical analysis shows, that the application of negative feedback to an amplifier reduces the output signal voltage and the noise, *but it reduces the signal more than it reduces the noise,* and the ratio of the resulting output signal to the resulting noise is *less than without negative feedback.*

The statement that the signal-to-noise ratio in an amplifier is better with negative feedback than it is without it, for the same output voltage, is true but ridiculous. It is exactly the same as saying that the signal-to-noise ratio in an amplifier is improved by increasing the signal, which statement is also true, and equally ridiculous.

In effect, the standard derivation depends upon the comparison of two different amplifiers having two different amplification constants. The output of the amplifier having the greater amplification constant is then reduced by applying negative feedback until the output of both amplifiers is the same for a given input. Now, if a noise voltage is introduced into both ampilfiers near the output, it can be shown that the signal-to-noise ratio is better for the amplifier with feedback.

But! Had the output of the amplifier having the greater amplification constant been reduced the same amount by merely putting an attenuator across it, the signal-to-noise ratio would have been still better!

The mathematical demonstration of the above is quite simple and it shows that signal-to-noise ratio is impaired by negative feedback in the proportion,

Signal-to-noise ratio with feedback—
Signal-to-noise ratio without feedback $= (a_o/a_f)\,(1/1\text{-}BM)$

where:—

A is the amplification constant of the whole amplifier.

a_o is the amplification constant of the portion of the amplifier included between the point at which noise is introduced and the output.

a_f is the gain, with feedback, of the same portion of the amplifier.

B is the feedback propagation constant (usually assumed a negative quantity, numerically, for negative feedback).

F. S. MACKLEM
Research Enterprises Limited
Leaside, Ontario

Radio Parts for Schools

WITH REFERENCE to an item in "Cross-Talk" of the Nov. 1942 issue regarding radio parts desired by schools I would like to offer a suggestion.

This project of supplying representative equipment to the schools would definitely be a war contribution. As you point out, it is desirable not to sidetrack new material nor rely on priorities if possible.

I would suggest that this problem be turned over to the "ham" organizations to carry on. I am not a member of that order myself, but had planned to carry on some development work and do have a number of radio items stored away for the duration that could well be put to use now as you point out. Many of the ham fraternities must also be in the same condition. Therefore, why not call on the radio, amateur organization.

Could there be a more fertile source of miscellaneous and representative radio parts and equipment? Equipment that can be turned over without priorities or red tape and certainly at nominal cost.

S. SOLOMON

Directional Drainage Relay

MR. HAROLD P. HELLER'S letter in ELECTRONICS September 1942 issue refers to an error in the application of the directional drainage relay, the article on this subject being previously abstracted in the June and March 1942 issues of ELECTRONICS.

I would like to point out that this material was abstracted from the complete article appearing in the *Proceedings of the Pacific Coast Gas Association* (Vol. 30, pp. 163–165) and that the theory advanced in the original article is correctly stated. The authors did not make or edit the abstracts in question, and, therefore, are not responsible for the error which has occurred in stating the direction of current flow. Underground pipes which are electrically positive to rails or to other underground structures will experience a current flow from pipe to rails or to the other structures and, ordinarily, an accelerated corrosion rate. On the other hand, if the pipe system is sufficiently negative to the surrounding medium, current will be accumulated by the pipe system and corrosion will be mitigated.

Mr. Heller states that the application of the directional relay does not constitute cathodic protection. I cannot be in complete agreement with this statement in a practical sense. By the use of the relay a lower resistance path is provided for the return of stray currents to the negative rails, therefore the current pick-up on the pipe system may be increased. Increased cathodic protection will then ensue to areas of negative pipe potentials just as if an additional source of outside power had been provided. Now if the potentials reverse on the pipe system on account of train or street-car movements, the

area of positive potential may now be negative, and the relay blocks the reverse current flow causing the current to be accumulated via the soil paths. Another relay at the newly positive area will then operate to provide the metallic return path.

It will be noted that more than one relay must be used ordinarily to take advantage of the shifting negative areas. In practice certain areas are found to be predominantly positive for considerable periods, and these locations are then taken as the drainage cable locations. If the pipe potentials merely increase or decrease without change of direction, fixed drainage cables may be installed and the relays eliminated. This is not always the case however.

It is quite possible that, by a properly arranged system of relays and drainage points, cathodic protection can be achieved on a system over a large percentage of the time without the use of additional current sources other than the local electric railway system. However, as Mr. Heller mentions, additional forced drainage using separate ground beds and separate current sources is in many cases desirable inasmuch as railway currents may be insufficient to provide complete protection against corrosion at all times. This presents a problem in economics and engineering which is separate from the problem of controlled pipe system drainage. The latter involves controlling stray soil currents such that (1) they may become less detrimental, and that (2) they may become actually beneficial under certain conditions.

RAY M. WAINWRIGHT,
Engineer

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Toledo, Ohio

Medical Electronics

CERTAIN PHYSICIANS are using electronic machines in an attempt to diagnose diseases. Their contention is that such a machine measures vitality of organs and tissues. The operating physician places an electrode on the leg and another on some other part of the body. With one hand he turns switch after switch. The other hand is used to rub a diaphragm which looks like cellophane.

Is such a machine more or less accurate in diagnosis? If so, what does it actually measure?

C.A.S.
Van Nuys, Calif.

✦ The machine described is undoubtedly effective only in transferring money from the pocket of the patient to the pocket of the quack operating it. I am quite sure that the machine could not effectively differentiate between a live patient and a dead one, although the quacks use some machines which are of value to the physician trained in their use, such as x-ray.

The machine is probably a dummy, in other words is composed of meters

and dials without function, but may have thermocouples and other devices which will produce a reading which differs on different parts of the body. This reading would be equally meaningless. The business of rubbing the cellophane diaphragm speaks quite eloquently of charlatanism.

The only practical application of recording potentials of the voluntary muscles was described by Jacobson in the Review of Scientific Instruments in the last 3 or 4 years. This or a similar device, would be applicable only where there is a definite disease affecting the muscles, such as infantile paralysis or myasthenia gravis or spasticity, and then it is largely of theoretical interest.

The only electronic devices which can be used safely by the layman for treatment are the ultraviolet generators and hearing aids.

W.E.G.

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Wave Analysis Schedules

SINCE THE SCHEDULES published by Col. Denman in September 1942 ELECTRONICS furnish tools of permanent value for the engineer, they should be free from errors. After hearing from Mr. Corrington (a reader of ELECTRONICS) who has found errors in the article as published, I have found it necessary to rederive the analysis schedules from the beginning. This has been a tedious and time-consuming job, but it is finished and I am ready to report.

The errors, noted below are of three sources: those occurring in typesetting and printing; two errors made by me in redrawing the schedules to fit them into the publication space available; errors which are in Col. Denman's original article. Mr. Corrington's findings are correct at every point, and I think his services in this connection should be publicly noted. He must have done a lot of work on the schedules.

The list of errata follows.

FREDERICK W. GROVER,
Schenectady, N.Y.

Page 44, column 2, in the equation. For y_1, read y.

Page 45, *36 Ordinate Schedule:*

In second row of ordinates y_{36}, y_{35}, y_{34} . . ., y_{36} should be omitted.

At bottom of page, for θ_{10}, read $\theta_{10} = \Sigma_0 + \Sigma_2 + \Sigma_4 + \Sigma_6 + \Sigma_8$.

Page 46, first column:

In equation for d_2 for $+(A_7+A_{17})$, read (A_1-A_{17}).

Page 46, second column:

Line 2, check for d_8, for $-(A_{11}+A_{25})$, read $(A_{11}+A_{25})$.

Second line of check for d_{18}, for $(A_{13}-A_{23})$, read $(A_{13}-A_{23})$.

Fifth line of the check for S_0 should read $(B_{12}+B_{24}) + (B_{13}+B_{23}) + (B_{14}+B_{22}) + (B_{15}+B_{21}) + (B_{16}+B_{20})$.

Sixth line of check for S_1, for (B_1-B_{25}) sin 35°, read $(B_{11}-B_{25})$ sin 35°.

72 Point Schedule, page 46:

Bottom of the page. $\mu_1 = \Delta_1 - \Delta_3 - \Delta_5 + \Delta_7 + \Delta_9 - \Delta_{11} - \Delta_{13} + \Delta_{15} + \Delta_{17}$.

For $\alpha_1 = R_1 - (R_5 - R_7)$, read $\alpha_1 = R_1 - (R_5 + R_7)$.

For $\alpha_2 = R_2 - (R_4 - R_8)$, read $\alpha_2 = R_2 - (R_4 + R_8)$.

For $\gamma_2 = \sigma_1 - \sigma_6 + \sigma_{10} - \sigma_{14} + \sigma_{18}$, read $\gamma_2 = \sigma_2 - \sigma_6 + \sigma_{10} - \sigma_{14} + \sigma_{18}$.

Page 47:

Column for A_{17} and A_{19} in the line for sin 80°, the symbol is not clear. It should read $-\sigma_{16}$.

Table for Cosine Terms:

Column for B_7 and B_{20}, line for $\alpha = 30°$. For $-\Delta_{12}$, read Δ_{12}.

Column for B_8 and B_{28}, line for $\alpha = 50°$. For $-T_8 T_1$, read $T_8 T_1$

Column for B_8 and B_{28}, line for $\alpha = 70°$, for $T_4 T_5$, read $-T_4 - T_5$.

Column for B_{11} and B_{25}, line for $\alpha = 20°$, for Δ_2, read Δ_2.

Column for B_{11} and B_{25}, line for $\alpha = 55°$, for Δ_{17}, read $-\Delta_{17}$.

Column for B_{13} and B_{23}, line for 15°, symbol is correct, but not very clear. Read $-\Delta_{15}$.

Column for B_{13} and B_{23}, line for $\alpha = 45°$, for Δ_9, read $-\Delta_9$.

Editor's Note.—Colonel Denman was killed in active service in November 1941.

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BLIND RADIO OPERATOR

Leo Sadowsky of New York has overcome his physical handicaps to become an amateur radio operator, licensed by the FCC. He was born deaf, and never learned to speak, was blinded by an accident when two years of age. He showed an interest in radio and was encouraged by instructors at the N. Y. Institute for the Education of the Blind. He learned to distinguish radio signals by means of a buzzer, feeling the vibrations through his hands. He is now a licensed ham

NEW BOOKS

Mathematics of Modern Engineering

BY ERNEST G. KELLER. *John Wiley and Sons, New York, 1942, Volume II (mathematical engineering), 309 pages. Price $4.00.*

WRITTEN IN THE INTEREST of the Advanced Course in Engineering of the General Electric Company this second volume follows by six years the first which was written jointly with R. E. Doherty. Volume II is relatively independent of Volume I and may be read by itself.

The book is divided into three nearly equal length chapters. The first treats the classical methods for setting up the differential equations for studying the dynamics of complicated mechanical systems such as the suspension system of an electric locomotive. The approach is to start with energies and then use Hamilton's principle to derive Lagrange's equations or to use Lagrange's equations directly.

The second chapter is divided into two parts, the first containing an introduction to matric algebra and tensor analysis, and the second an introduction to the use of these techniques in the formulation of the electromechanical differential equations for rotating electrical machines. The final chapter is concerned principally with methods for solving nonlinear and variable-coefficient linear differential equations analytic in a parameter. Such equations arise in difficult electrical and mechanical problems. A fairly extensive treatment of elliptic and hyperelliptic functions is included.

As this survey of the contents indicates, except for the introductory material in the first part of Chapter 2, the book was not intended for and is not suited to the needs of the beginner. It is essentially written for engineering graduates who are interested in formulating and solving mathematically difficult mechanical and electrical problems associated with lumped-parameter, i.e. discrete physical systems. Volume III, which is yet to appear, will deal with continuous systems.

For Volume II it is presupposed that the reader will be thoroughly familiar with the usual undergraduate mathematics through ordinary differential equations. Volume I,

which assumes a knowledge of calculus, would be appropriate toward the end of such a preparation.

Unfortunately the first printing is full of misprints which even occur in important equations such as (42) on page 44. The necessary corrections are not obvious in some cases. More serious than these are a number of careless and erroneous statements on important points. An indication of the type and distribution of these is as follows.

Chapter 1 is carelessly done in places. For example, the last part of the statement of Rayleigh's Principle on page 87 is vague and misleading if not incorrect.

Chapter 2 is definitely below the level of the other chapters at many points. The following samples will illustrate this. A large number of unsubstantiated claims regarding the contributions of G. Kron and their power, form the introduction to this chapter. The type of coordinate transformation considered, Eq. (13), page 114, is not well defined. The historical remark on page 132 is incorrect. The credit should go to a 1919 paper by Professor Rosebrugh of the University of Toronto. The generalization postulates are too vague to be significant. In obtaining the equations of a stationary network the transformation from branch to loop currents is trivial and unnecessary. These equations may be written down at once in the ordinary way by using the network diagram labeled with loop currents. Consequently matrix transformations are not required for setting up the equations. The network chosen for the main illustrative example, Fig. 2.13, page 143 (also Fig. 2.15, page 148), is found on redrawing to be the trivial five-leaf clover.

Chapter 3 is rather carefully written and is to be recommended to those who wish to solve difficult non-linear and variable-coefficient linear equations of the types which arise in electric control circuits employing iron-core inductors, in the theory of frequency modulation, in the theory of super-regeneration, and in non-linear vacuum tube problems. The book does not mention the last three applications, but stresses applications to electrical rotating machinery.

In general, numerous interesting examples illustrate the text, and

many practice problems, with hints for solving the more difficult ones, are placed at the ends of sections. A valuable set of well classified references appears at the end of each chapter.

In brief then, although Volume II cannot be uniformly recommended, its good features constitute a valuable contribution to the literature of advanced mathematical engineering.

—J.L.B.

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A-C Calculation Chart

By R. LORENZEN, *John F. Rider, Publisher, New York. (166 pages, price $7.50.)*

THE CHARTS CONTAINED in this volume have been prepared primarly for increasing speed and minimizing the amount of labor required in making certain types of calculations of alternating current circuits. All except two of the 146 plates make use of the reactance-frequency-inductance-capacitance type of chart originally prepared by the Bell Telephone Laboratories and available as a standard graph sheet from the Keuffel & Esser Company. This type of chart contains four logarithmically ruled scales; values of reactance and frequency being plotted as the ordinates and abscissa, respectively, while another set of logarithmically ruled scales at a 45 deg. angle contain values of inductance and capacitance. Any point on such a graph serves to correlate four factors: X, f, L and C.

In the introduction and also in the explanation of the use of the chart, the author makes a contribution in outlining the history, theory, and development of this type of chart. Several pages are devoted to the use of the charts in convenient form, and illustrating the use of the charts in conditions which are not always realized. Another contribution which has been made is in the inclusion of a number of charts with inverted scales so that values of susceptance rather than reactance are plotted as the ordinates, with the necessary inversion in the logarithmic scales of inductance and capacitance. Two charts at the end of the book deal with Q and phase angle, the latter of which is a double scale device similar to two scales of a slide rule.

In all, there are seventy-two separate charts of frequency against reactance, and seventy-two charts of admittance plotted against reactance. In each case supplementary

scales are printed at the bottom of the sheet giving the relationship between any number and its square root, as well as the reciprocal relationships between ohms and mhos. Each chart is well printed in green and red and is 6¾ in. square. This scale size is sufficiently large so that results of engineering precision may be easily achieved. Each of the individual charts is devoted to one decade (a 10 to 1 ratio) of reactance and frequency, and the multiplicity of charts is required to accommodate the wide range of reactance and frequency encountered. In effect, all the information of 144 charts could be placed on two charts, with the exception of the location of the appropriate decimal point. It appears to this reviewer that a single chart with appropriate notation for the location of the decimal point would be as quick to use as 144 separate charts. It would also appear that the price of $7.50, while a fair price for a book of this size and type of construction, is somewhat high for the convenience of locating a decimal point. Nevertheless, those who have occasion to make frequent use of such calculations of the type for which the book is intended, may not show this point of view. Certainly the charts cover a very wide range of circuit parameters. Conductance from 0.1 micromho to 100 mhos (corresponding to a range of from 0.01 ohms to 10 megohms) may be found on the chart. The frequency range extends from 10 cps to 1,000 megacycles.—B.D.

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Principles of Aeronautical Radio Engineering

BY P. C. SANDRETTO. *McGraw-Hill Book Co., Inc., New York, N. Y. 414 pages. Price $3.50.*

PRIOR TO HIS ENTRY into the Army, Major (now Lieutenant Colonel) Sandretto served as Superintendent of the Communications Laboratory of United Air Lines, and his work in aircraft radio extends over many years. It is not surprising therefore that he has written, in this reviewer's opinion, the best book yet to appear on the engineering applications of radio to flying. The book is well-written and well-arranged; it is complete; the author knows what he is talking about; and it keeps close to the engineering realities of

the subject. It is a thoroughly readable book. All of which is fortunate because in this war, as never before, engineers must assimilate quickly what has gone before in engineering radio equipment for aircraft.

The book begins with a chapter on the evident need of radio in aircraft, and then launches into detailed treatments of the low-frequency radio range ("A-N") beacon, (with comments on its shortcomings as well as its capabilities), the u-h-f radio range beacon, aircraft loop direction finders, marker beacons, the various forms of instrument landing developed prior to the war, the absolute altimeter, ground (Adcock) direction finding, medium and ultra-high frequency radio communication. Treated also is that neglected subject, airplane power systems. The concluding chapter treats the system-engineering aspect of aeronautic radio, which is so often neglected by the equipment designer.

Unlike most other books on the subject, this volume does not take a self-consciously elementary approach. It assumes that the reader already has a basic understanding of radio technique and confines itself to the application of this technique to the aircraft problem. Mathematics is used, where needed, but simply so. The author has added to his own authority, by submitting each chapter to a specialist, such as Andrew Alford, Lt. Col. R. R. Brunner, W. E. Jackson, F. C. McMullen, Harry Diamond, Charles R. Burroughs, and A. F. Trumbull, names which are well known in and out of aircraft radio circles.

The book treats all the subjects which military exigencies permit. It is to be hoped that, when censorship is lifted and the behind-the-scenes developments in this field become publishable, the author will not delay in preparing a second, enlarged edition.—D.G.F.

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Frequency Modulation

By AUGUST HUND. *McGraw-Hill Book Co., Inc., New York, N. Y. 375 pages. Price $4.00.*

THE READER HAS A RIGHT to expect, on the basis of his previous work, that any book by August Hunt should be sound and comprehensive,

(*Continued on page* 224)

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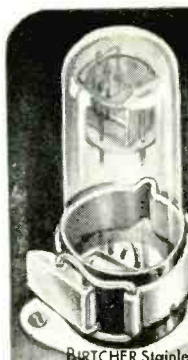

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useful for obtaining a basic understanding as well as for reference. "Frequency Modulation" is no exception. It is the first thoroughly sound treatment of the subject on the level of the designing engineer. It is not an easy book to read, partly because the concepts on FM are not easy in themselves, and partly because of the author's style. But, hard or easy, it is a book which should be read by every engineer who aspires to a basic understanding of the art and who despairs, as this reviewer does, of obtaining such understanding from periodical publications.

The author wisely adopts the policy of introducing the mathematics of the subject hind-end-to. The analyses of Lord Rayleigh, van der Pol, and Carson are presented in the first chapter as the familiar series of Bessel functions. The derivation of the series is confined to an Appendix, where it rightly belongs. This appendix should not be neglected by the reader. It will serve to disabuse anyone of the idea that the derivation is a simple and logical tracing of cause and effect. It is an adventure in mathematical compromise and judicious simplifying assumptions. It proves what many have already guessed: that the sideband theory of FM is truly abstruse, a delight to the mathematical physicist, but something less than delightful to the practicing radio engineer.

The end result, the Bessel series, is a powerful engineering tool (leading directly to the "zero" method of checking deviation, for example). The author makes immediate use of the series as an engineering tool in the first 25 pages of the book, and it is never completely out of sight for the remaining 325 pages of the text. This does not indicate that the approach is theoretical only. Over 100 pages are given to practical applications, with detailed discussions of transmitters, (which, praise be, are actually identified with the manufacturers' names) receivers and antennas.

The first chapter, which constitutes nearly half of the book, treats the fundamental relationships from the standpoint of the Bessel series, and painstakingly compares amplitude-, phase-, and frequency-modulated waves. A great many numerical examples and basic numerical con-

Index to Advertisers

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SEARCHLIGHT SECTION

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stants in this section help the reader to link the theory with familiar practice. Every available approach is taken: the series, tables of sideband distributions, vector diagrams. This chapter is truly the work of a scholar and a gentleman. It is worth a solid month of midnight oil.

The second chapter, on auxiliary apparatus, discusses circuits for transmitting (the Armstrong modulator, reactance modulators and center-frequency stabilizers) and receiving (r-f and i-f amplifiers, limiters and frequency detectors). The universally-used Seeley discriminator is given a thorough going over. Frequency pre-emphasis and de-emphasis networks are discussed and typical examples (with circuit constants!) are given. The remaining chapters are devoted to practical embodiments of the circuits in commercial and laboratory equipment.

This book is an exceptionally complete treatment of a most important specialized branch of radio engineering. Its current appearance is fortunate, since it permits engineers to catch up on the subject, while the industry marks time pending the end of the War.—D.G.F.

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A.S.T.M. Standards and Data on Electrical-Heating and Resistance Alloys

By A.S.T.M. COMMITTEE B-4, *American Society for Testing Materials, 260 S. Broad St., Philadelphia, 1942. 160 pages, with heavy paper cover. Price $1.50.*

TWENTY-THREE SPECIFICATIONS AND TESTS of interest to radio and electronic engineers are here combined with four pertinent technical papers in a single convenient volume. A large portion of the book covers materials used in the manufacture of radio tubes and lamps, such as nickel and nickel-alloy wire and ribbon, mica stampings, grid wires, electrode support wires, strip and sheet metals for tube electrodes, and sleeves and tubing for cathodes. Methods of test and specifications are given for alloy resistance wires, alloy wires used for electric heaters, electric-furnace alloys, heat-resisting alloys, and thermostat metals. The papers cover a contact-testing machine, surge tests on contact materials, design of devices using thermostat metal, and methods of testing thermocouples and thermocouple materials.—J.M.

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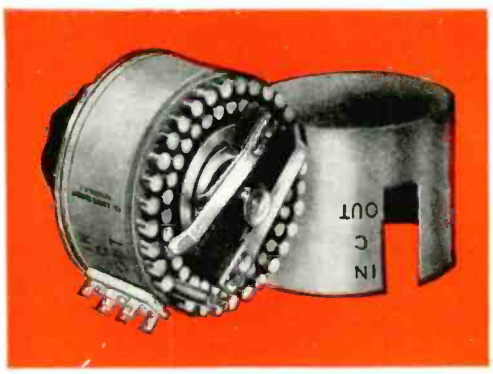

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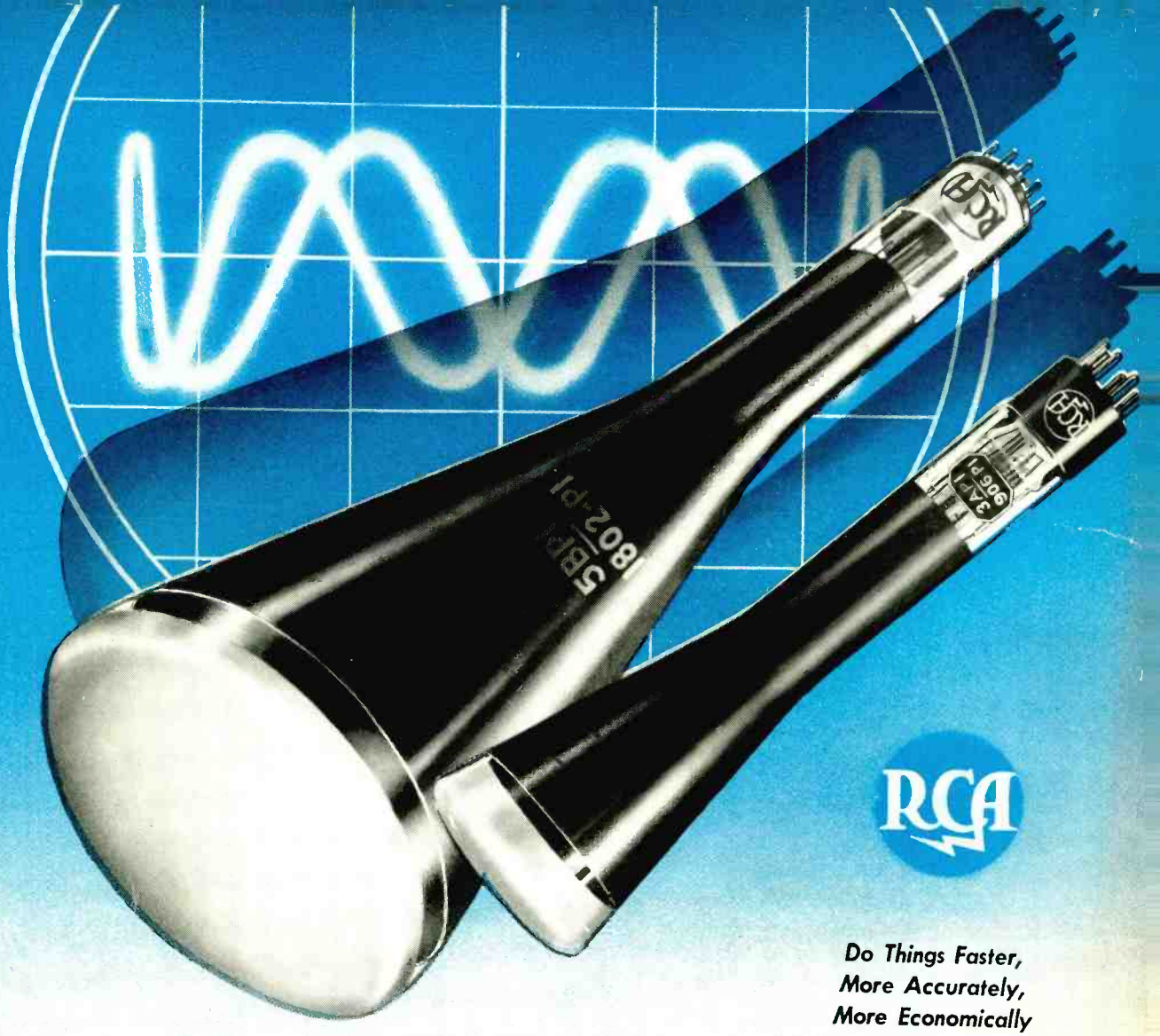

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