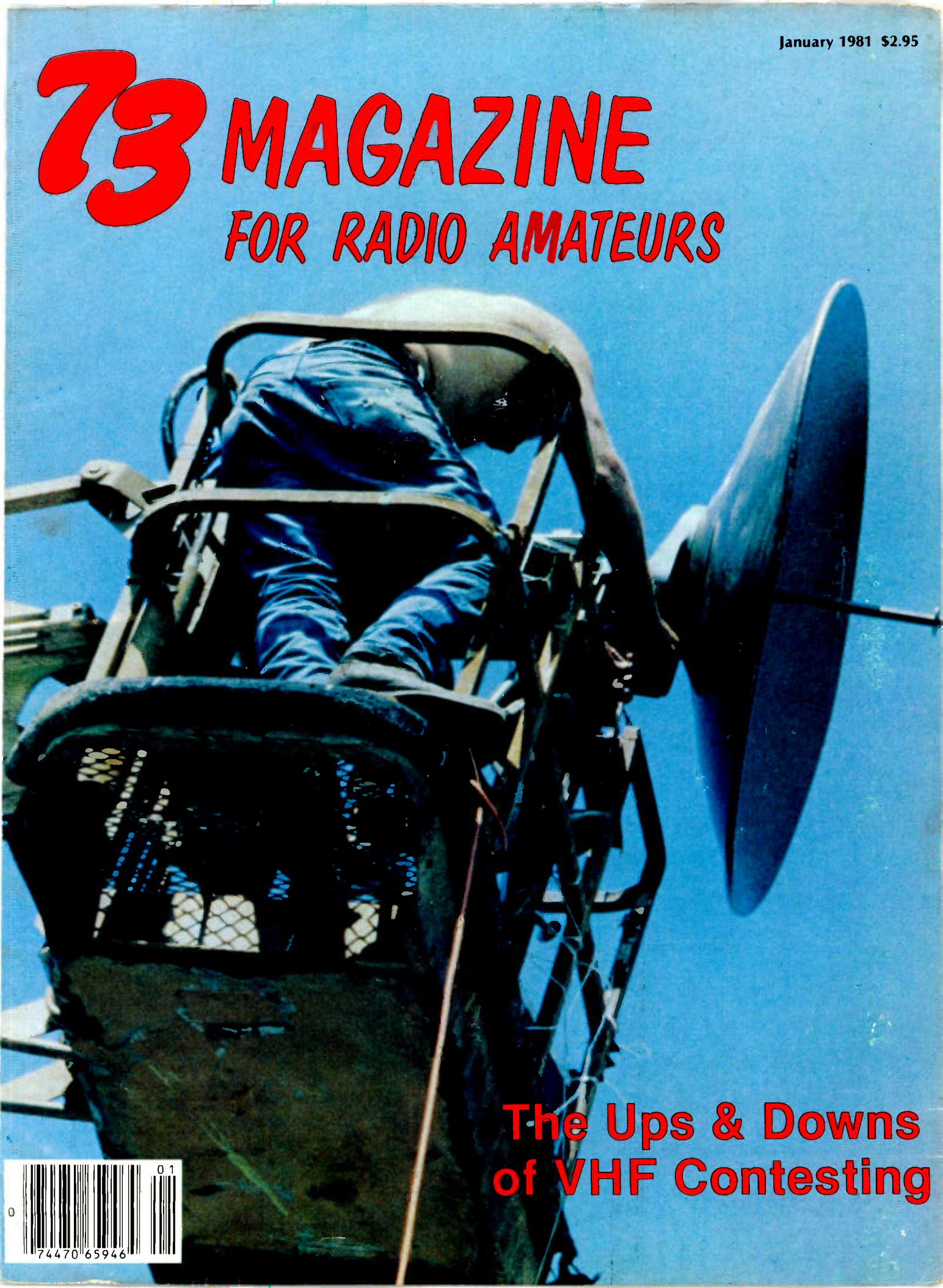
January 1981 $2.95

73 MAGAZINE
FOR RADIO AMATEURS



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- Resonant cathode pi input circuit
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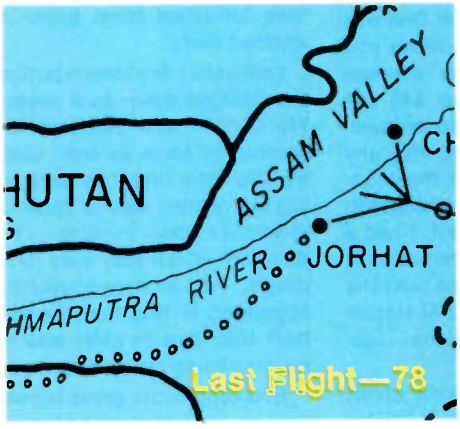

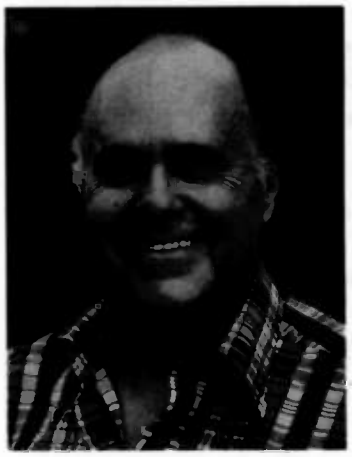

W2NSD/1
NEVER SAY DIE

editorial by Wayne Green

HAMMING IN CHINA

During the 1980 trip to Asia, I organized a group tour of China. Ten of us made a relatively short trip up into Guangzhou. Though I enjoyed the unusual visit and the fascinating things which we saw...and ate...one of the main reasons for the trip was to get the feel of the possibilities for developing some amateur radio there. Most of the people on the trip were hams and microcomputer people, so the company was enjoyable.

The Asian trip was for several reasons. It started out with a visit to a computer show in Tokyo. This was followed by visits to consumer electronic shows in Seoul, Tokyo, Taipei, and Hong Kong. In addition to my wanting to keep abreast of the state of the art in electronics in these countries, I also had a strong interest in the development of sales of our Instant Software in Asia. I'll try to write up a more comprehensive report when I get my pictures processed and get the more important developments taken care of.

Just about any DXer would give his eye teeth to sit in China and run the pileups...or even run through lists. It may take a time before this comes about, but I think I have a handle on an approach now...which is more than I've seen before. I think that it may be possible to get amateur radio opened up in China, though I don't think it is going to be either easy or soon.

A visit to China is a sobering experience. I've visited a lot of places during my life...in fact, using the ARRL country count, China was number 97 for me. That is, if you don't take away some countries which have disappeared since I visited them. I'd prefer to make those up after I get to 100, if you'll allow me the ego trip. Right after China, Sherry and I took a jetfoil boat up to Macao (CR9) for a day, racking up #98 for me, so it won't be long.

I've experienced the primitiveness of some of the African countries, the grinding poverty of India, the pervasive fear in the Communist block countries...but still I wasn't really prepared for what I found in China. Much of it was like being thrown back in time at least a hundred years.

In Guangzhou, formerly known as Canton, just a 20-minute flight from Hong Kong and a four-hour railroad trip back, it was a completely different world. The people were pleasant...and there was none of the pressure of communist politics which put tensions on visits to East Germany and other Russian-dominated countries. The people are no longer dressed identically in Mao outfits, but the heritage of using masses of people to do things instead of machinery and technology was pervasive.

The streets of Canton were almost solid with people on bicycles. As our small tour bus drove along, horn rasping out almost continually, the waves of cyclists parted to let the bus through and then closed behind it. There is little in the way of cars, but plenty of trucks...all owned by the state and used to service the communes and factories.

The black bicycles, though individually owned, were all identical except for a number on the back...and a rare colored bicycle seat. I saw no sign of any transistor radios for sale...or in use. There were a few portable radios in the department store, but they were for sale in a special section which was off limits to most Chinese and the prices were prohibitive. One was priced at over $700. When you understand that the average wage there is about $45 per month, this puts it into perspective. You have to register any radios you bring into the country...and they check them both going in and going out. I had a little Panasonic shirt-pocket AM/FM radio, so I checked the bands. They had one FM station and a couple AM stations...period.

The $700 radios were about what we would expect to sell for maybe $35 or so...and of disappointing quality. The TV sets were about $1500. A commune of several hundred people could gang together to buy these, so there is a market. I saw loudspeakers strung out around the communes so many people could hear the radio. These were in homemade wooden boxes for baffles.

But what about hamming? In a country where it is still undesirable to let most of the people even listen to the radio...or at least to anything except a single Chinese radio station, it may be some time before the government will be willing to chance letting people hear much from outside the country. Even small transistor radios would be able to tune in stations from Hong Kong, hence their lack.

On the one hand there are people in China who would like to start the country toward coming to grips with the modern world. On the other are the fears of those in power. Add to that a serious lack of educated people...a heritage of the persecutions of teachers and land owners...and you have a most difficult situation. I don't know how much of the entrepreneurial spirit is inherited, but if it is, then much of this has been bred out of the Chinese as a result of the executions when the communists took over. You might call it the survival of the unfittest.

All buildings are designed and built by the government. This means that all of them look pretty much the same...terrible. There is no reason, apparently, to make them look attractive. Our hotel was brand new...just three years old. It looked as if it were at least 75 years old inside. The rooms were adequate, but sparse and primitive by Western standards. At least they had flush toilets, which are a rarity in China. And they furnished toilet paper...another rarity.

I am not by any means putting the Chinese down as a people. We found them pleasant and anxious to show us their country. We knew that they were going out of their way to show us the most modern aspects...the things of which they were most proud...so we were doubly disappointed to find that the very best they had to offer was so disappointing by our standards.

Everyone in our group agreed that we were glad we had made the trip...that it had been an exciting experience. We also agreed that we would not be much interested in doing it again.

Despite heroic efforts by the China Travel Service to fill in every minute of our visit to China with organized activities, our group did exercise its initiative and manage to get some time to see the Canton Trade Fair...and to visit the American Consulate for a cocktail party. In addition to getting a free Pepsi (which tasted no better than the last one I had a couple of years ago), I had an opportunity to talk with the people at the consulate and get some insight on approaches toward getting amateur radio started in China.

After my experience in Jordan, I felt that if it were only possible to sit down and explain the benefits of amateur radio to the top man of the country, this would be the best approach. Trying to work up through the ranks of bureaucrats is almost certain

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TR-2400 FEATURES:

- **Large LCD digital readout**
  Readable in direct sunlight (better than LEDs). Readable in the dark (with lamp switch). Virtually no current drain (much less than LEDs) and display stays on. Rugged and dependable in hot or cold temperature ranges. Shows receive and transmit frequencies and memory channel.
- **5-kHz-step frequency selection**
  PLL synthesized keyboard channel selection system. No "5 up" switch needed. Selects from 144.000 to 147.995 MHz.
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  Single or fast continuous 5-kHz steps from 143.900 to 148.495 MHz for Amateur and MARS or CAP simplex or repeater operation.
- **10 memories**
  Retained with battery backup (only 2.0 mA). "M0" memory may be used to shift the transmit frequency any desired amount to operate on repeaters with nonstandard split frequencies.
- **Built-in autopatch DTMF (Touch-Tone®) encoder**
  Uses all 16 buttons of keyboard while transmitting.

- **Automatic memory scan**
  Checks all 10 memory channels. Programmable to lock automatically on either BUSY (signal present) or OPEN (no signal) channels.
- **Subtone switch**
  Activates subaudible tone encoder (not Kenwood-supplied).

- **Repeater or simplex operation**
  Convenient mode switch shifts transmit frequency +600 kHz or -600 kHz or to the frequency stored in "MO" memory.
- **Reverse operation**
  Push-button switch shifts receiver to transmit frequency and transmitter to receive frequency.
- **Extended operating time**
  With LCD and overall low-current circuit design. Only draws about 28 mA squelched receive and 500 mA transmit (at 1.5 W RF output), for longer operating time between charges.
- **Two lock switches**
  Prevent accidental frequency change and accidental transmission.
- **BNC antenna connector**
  Easy to connect external antenna.
- **LCD "arrow" indicators**
  Show "ON AIR," "MR" (memory recall), "BATT" (battery status), and "LAMP" switch on.
- **High-impact case and zinc die-cast frame**
  Extremely rugged with antenna counterpoise.
- **External PTT microphone and earphone connectors**
  Easily accessible on right side of transceiver.
- **Compact and lightweight**
  Only 2-13/16 inches wide, 7-9/16 inches high, and 1-7/8 inches deep. Weighs only 1.62 pounds (including antenna, battery, and hand strap).

STANDARD ACCESSORIES INCLUDED:

- Flexible rubberized antenna with BNC connector
- Heavy-duty (450-mAh) NiCd battery pack
- External-standby (PTT) plug
- AC charger
- Hand strap
- External-microphone plug
- Earphone

NOTE: *Price, specifications subject to change without notice and obligation.*

OPTIONAL ACCESSORIES:

- ST-1 base stand (shown) which provides 1.5-hour quick charge and automatic switch to trickle charge, floating charge (operate while charging), 4-pin connector for dynamic microphone, and SO-239 antenna connector
- BC-5 DC quick charger (1.5 to 2.0 hours)
- SMC-24 speaker/microphone
- LH-1 deluxe leather case (top-grain cowhide)
- PB-24 extra battery pack with charger adapter
- BH-1 belt hook

to doom any effort to failure. Bureaucrats exist by adhering to rules, and their greatest fear is making a decision or proposing some idea which is controversial and could thus reflect poorly on their record.

In this I found that the problems of dealing with China are quite different from dealing with most other countries for, despite the impressions we have been getting from our media, no one person is in charge in China. There are many factions, all jostling for more power, and the country is thus run by committee. This probably goes a long way towards explaining why they seem to be about a hundred years behind us.

Despite all these problems, I am going to start work on the situation and see what I can do to get some interest in the highest official circles. I'm available to fly over there and deal directly, should that be beneficial. Sure, I'd love to have a week or two of DXing from China, but I have too much going on these days for that, so perhaps we can work on longer range plans for getting amateur radio introduced. I know that a number of DXers will be glad to help out, should anything start to break loose. Lloyd Colvin (W6KG) and his wife Iris (W6QL) would be on a plane tomorrow if they thought it would help.

The trip to Asia was, again, fantastic and I'm sorry that more of you did not have the time to go along. Those who did had the time of their lives. I did write about it and invite all of you to make the trip...and it was certainly a bargain, with first class hotels everywhere, wonderful meals, and the excitement of a completely different world.

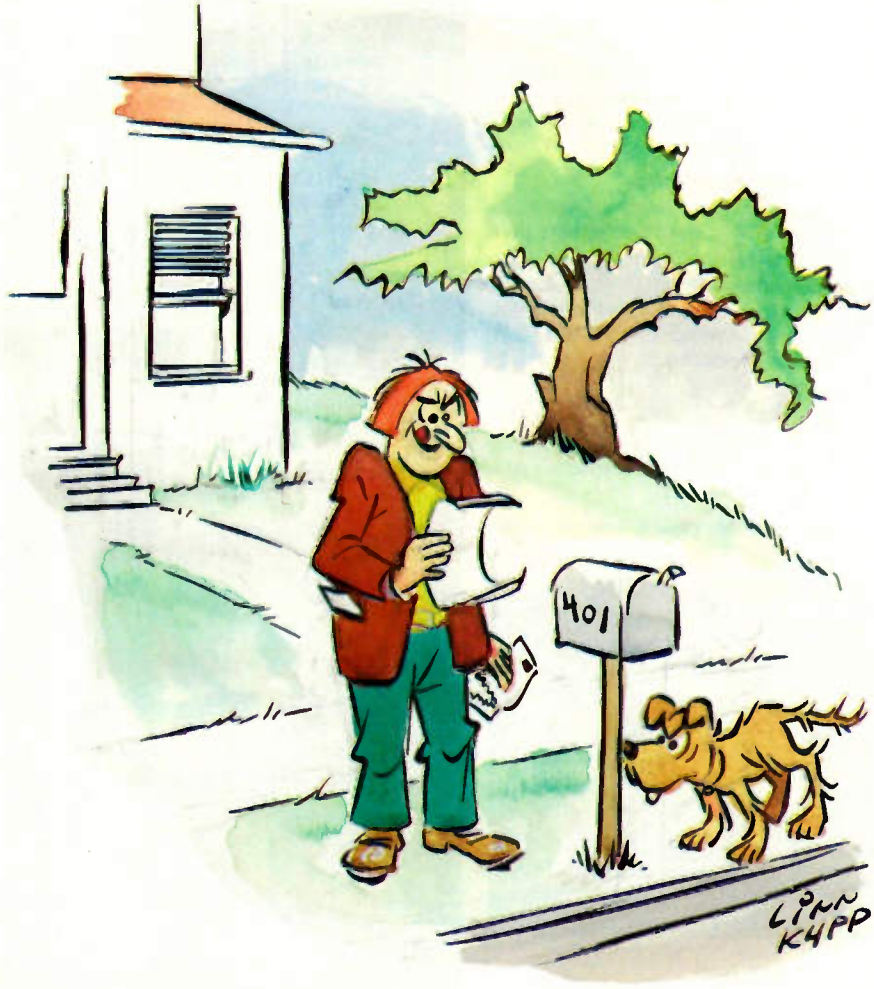
BOMBSHELL IN TAIWAN

In addition to my talk to the China Youth Association scheduled in the Grand Hotel, I was also called upon to speak briefly to several hundred members of the electronics industry on Taiwan at a business breakfast. I made all the papers with my short talk.

Without putting you through the complete text of the talk, I got their attention by saying flatly that Taiwan's electronics products, while impressive, were not by any means state of the art. I pointed out that Taiwan was in the position of having to import technology from Japan and the US and was depending entirely on being able to pro-

Continued on page 152

Well...I Can Dream, Can't I? **by Bandel Linn K4PP**



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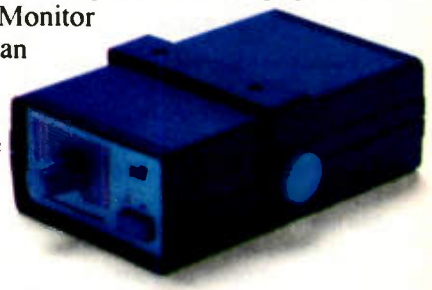

- All tones in Group A and Group B are included.
- Output level flat to within 1.5db over entire range selected.
- Separate level adjust pots and output connections for each tone Group.
- Immune to RF
- Powered by 6-30vdc, unregulated at 8 ma.
- Low impedance, low distortion, adjustable sinewave output, 5v peak-to-peak.
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- Reverse polarity protection built-in.

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71.9 XA	94.8 ZA	123.0 3Z	162.2 5B
74.4 WA	97.4 ZB	127.3 3A	167.9 6Z
77.0 XB	100.0 1Z	131.8 3B	173.8 6A
79.7 SP	103.5 1A	136.5 4Z	179.9 6B
82.5 YZ	107.2 1B	141.3 4A	186.2 7Z
85.4 YA	110.9 2Z	146.2 4B	192.8 7A
88.5 YB	114.8 2A	151.4 5Z	203.5 M1

- Frequency accuracy, ± .1 Hz maximum - 40°C to + 85°C
- Frequencies to 250 Hz available on special order
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TEST-TONES:	TOUCH-TONES:	BURST TONES:			
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2805		1800	2100	2350	

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FIGHT BACK

Have you ever heard of David Horowitz? No, David is not an amateur radio operator. David Horowitz is the host of a weekly syndicated NBC television program called *Fight Back*. David is the author of a new book of the same name, and, in my opinion, it's the best book on consumer awareness I have ever set my eyes on. Basically, it tells you how to avoid getting ripped off and what to do if you are. I won't try to review the book here, but it's more than just another consumer awareness volume. I *will* tell you the same thing I told David a few weeks ago when I happened to run into him at the NBC studios in Burbank: "That's one heck of a book!" If you ever have been ripped off or if you want to be sure it never happens to you, then read *Fight Back*.

CALIFORNIA VS. THE PAY-TV PIRATES

On October 1st, 1980, California Governor Jerry Brown signed a law into the state statute books which this author feels is one of the most irresponsible pieces of state legislation ever enacted. In fact, by the time you read this, the law may be a thing of the past, this because many people have vowed to fight it on various grounds. The law I speak of is called Section 593e of the California State Penal Code. It makes it a crime for any person "who for profit manufactures, distributes, or sells any device, plan, or part for the knowing purpose of facilitating an unauthorized interception or decoding of subscription television signals." Additionally, it provides for a jail term of up to 90 days and/or a fine of up to $2500 per count on any conviction. Not a bad law, you say? I quite agree. But not a law for California or any other state to enact.

Here, again, we see the classic example of a state trying to usurp the jurisdiction of the federal government. Unless the Communications Act has been rewritten without anyone noticing, the role of the FCC in such matters has been clearly defined for years. It is not the prerogative of California or any other state to try to usurp that which is governed by federal jurisdiction. But neither our Governor nor State Assemblyman Mel Levine, who sponsored the bill, seems to have bothered to read the Communications Act or any subsequent FCC interpretation. They never bothered to consult the findings in the Cerritos tower case in which the government stated specifically that it had jurisdiction over radio communication, and, in effect, told California to keep its nose out of the FCC's business. No, our state legislators failed to do their homework. If they had, they would not have permitted themselves to get caught in what may well become a "Catch 22" situation.

No, I am not on the side of the pay-TV pirates. I want this clear from the start. I understand the intricacies of pay-TV, the most important of which being that for subscription television programming to survive, the companies that provide such services must be assured that they will make a profit. If this assurance is destroyed because of widespread piracy of such services, then subscription television will fail, and eventually there will be nothing left to pirate. However, I do not think that the solutions now being addressed are the proper ones. Laws are only as good as the enforcement that goes with them. In the case of the California ordinance, most lawyers with whom I have consulted agree that the federal government, not the state, is the governing body, and that 593e was nothing but a lot of wasted effort.

Further, I have to question the concept of getting federal laws passed to protect subscription television. While the Commission may be good at generating rules and regulations to govern just about every eventuality occurring in the electromagnetic spectrum, their record on enforcement leaves a bit to be desired. And. . . what's to keep someone or some group from challenging such laws, the result of which is a court battle that will last years and cost us taxpayers. No, my feeling is that there is only one answer to the problem of pay-TV piracy, and that answer is technology.

The major problem, as I see it, comes from the fact that the majority of subscription television systems are just too easy to pirate. As with anything else, when the systems were developed, the cost factor of the system was one of the prime concerns to those developing it. Therefore, with but one exception, the pay-TV encoding systems of today are so simple to decode that a high-school student with only a bit of knowledge in electronics can overcome them. In fact, if you know how to read and understand a composite TV video waveform, there is no way for you not to figure out how a given subscription television system works. Once you have this knowledge, you are halfway home.

The key to combatting subscription TV piracy then becomes one of developing a pay-TV encoding system so complex as to make piracy uneconomical. In the end, it comes down to simple economics. If it's cheaper to purchase a pirate decoder than to pay the monthly subscription fee, then such decoders will become as fashionable as linear amplifiers for CB. But, should the subscription television services finally get together and, with their collective resources, develop a highly complex encoding/decoding system, one so complex as to make illegal decoders non-cost-effective items, they can ensure the longevity of subscription television in this nation.

Frankly, I suspect that the opposite will happen. I feel that most subscription-TV services are themselves such bureaucracies that they cannot see the forest for the trees. They will probably continue their court battles. They may eventually obtain the federal laws they seek to theoretically curtail the manufacture and distribution of such devices. In the long run, they will be the losers. I need only point to the 10-meter amplifier ban to make my point. The only one who tells us that the amplifier ban is a success is the FCC. You wouldn't know it by listening to 11 meters and hearing operators extol the virtues of their *new* "Super Whizbanger 10K" and such. If the subscription-TV people want a quick solution, leave it to the engineers to find it. Keep trying to change the laws, and they will only develop the same black market for decoders that now exists for CB linears.

I doubt if it will ever be possible to curtail the piracy problem completely. There will always be an individual somewhere who will figure out even the most complex of systems and find a way to beat it. Sort of like those who sit for hours trying to break the "top-secret" control codes on remote-base and repeater systems. But, they are a minority and as long as they cannot produce a cost-effective product to mass merchandise, they are no real threat to the survival of pay-TV. A few years ago, I predicted to a friend that this problem would occur. I based my assumption upon my understanding of the current pay-TV systems and human nature. Now, three years later, I find that I am correct.

Here, in California, and elsewhere, the problem with subscription TV piracy is growing, and, as I predicted then, the pay-TV people are grasping for straws in trying to solve it. Yet, the answer is in front of them. It will cut deeply into corporate earnings in the short term, but will give them long-term security. Let's see if these bigwigs of high finance are smart enough to realize this and initiate a technological change. If they're the typical bureaucrats I think them to be, I doubt if they will. In the end, you and I will pay the price, as cases are fought with our tax dollars. Even those of you who do not have subscription television will be the losers if this happens. Maybe we can at least start the ball rolling to forbid the use of our tax dollars for use in such litigation. Frankly, if the pay-TV people want protection, then they should be prepared to foot every penny it costs. If this means that it will cost their subscribers more, then so be it.

By the way, I am one of this nation's pay-TV subscribers and want to see subscription TV survive. I enjoy our HBO service and feel that it's worth the monthly service fee. If I wanted to pirate

Continued on page 149

SUPER RIG

NEW TEN-TEC

OMNI-C 9 Band Transceiver + HERCULES Solid-State KW Linear

TEN-TEC SUPER RIG IS READY. For every band, every band condition. With the latest in solid-state hf technology, the latest in features. To make communications easier, more reliable — super.

OMNI-C

The new model in this famous series. With new coverage and new features to make it better than ever!

All 9 HF Bands. From 160 through 10 meters, including the new 10, 18 and 24.5 MHz bands. Coverage you can live with—for years and years.

3-Mode, 2-Range Offset Tuning. Offset the receiver section or the transmitter section or the entire transceiver! In 2 ranges: ±500 Hz or ±4 kHz. For complete flexibility in fine tuning, a DX work, or net operations.

Seven Response Curves. Four for SSB, three for CW. With new switching to select the standard 2.4 kHz filter, optional 1.8 kHz SSB filter, 500 Hz or 250 Hz CW filters, and standard 450 and 150 Hz CW active audio filters. Up to 16 poles of i-f filtering plus audio filtering to handle any situation.

Built-In Notch Filter and Noise Blanker. Notch is variable from 200 Hz to 3.5 kHz with a depth of more than 50 dB. New noise blanker reduces ignition and line noise. Both standard equipment.

"Hang" AGC. New, smoother operation.

Super Specs. *Optimized sensitivity*—a balance between dynamic range and sensitivity (2 μV on 160 to 0.3 μV on 10 meters) *Greater dynamic range*: better than 90 dB. And a PIN diode switchable 18 dB attenuator. *200 watts input* on *all* bands! *100% duty cycle* on *all* bands for up to 20 minutes.

Super Convenient. *Built-In VOX* with 3 up-front controls. *Built-In PTT* control at front and rear jacks. *Built-In Zero-Beat* switch puts you on exact frequency. *Built-In Adjustable Sidetone* with variable pitch and level. *Adjustable ALC* for full control from low power to full output. *2-Speed Break-In*, fast or slow speeds to fit operating conditions. *Built-In Speaker* eliminates desk clutter. *Automatic Sideband Selection*—reversible.

Super Design. *All Solid-State and Broadbanded*—from the pioneer, Ten-Tec. *Modular* plug-in circuit boards. *Functional Styling* with convenient controls, full shielding, easy-to-use size (5¾"h x 14¼"w x 14"d).

Super Hercules Companion. Styled to match, plus separate receiving antenna capability, plus transceiver front panel control of linear's bandswitching (one knob does it all).

Full Accessory Line including filters, remote VFO, power supplies, keyers, microphones, speech processors, antenna tuners—all in matching color.

Model 546 OMNI-Series C.... $1289

HERCULES

Amateur Radio's first full break-in solid-state kW linear amplifier. With the reliability you'd expect from the pioneer in high-power solid-state technology—TEN-TEC.

All Solid-State. No tubes. Instead, HERCULES uses two 500-watt push-pull solid-state amplifier modules with an output combiner. Super solid.

Broadband Design. No knobs, no tuning. From the pioneer, TEN-TEC. For fast, effortless changing of bands. Super easy.

Automatic Bandswitching when used with OMNI (the OMNI bandswitch also controls HERCULES bandswitching through a motor driven stepping switch). Super convenient.

Full Break-In. HERCULES puts the conversation back into high power CW operation—you can hear between every character you send.

Full Coverage. 160 through 15 meters plus four "AUX" positions for 10-meter conversion by owner and future band additions.

Full Gallon. 1000 watts input on *all* bands, 600 watts output, typical. Built-in forced-air cooling. Driving power: 50 watts, typical. Adjustable negative ALC voltage. 100% duty cycle for SSB voice modulation; 50% duty cycle for CW/RTTY (keydown time: 5 minutes max.) Continuous carrier operation at reduced output.

Full Protection. *Six LED status indicators* continuously monitor operating conditions and shut down the amplifier whenever any one exceeds set limits (the exciter automatically bypasses the amplifier under amplifier shut-down for barefoot operation). The six parameters monitored are: 1) overdrive; 2) improper control switch setting; 3) heat sink temp.; 4) SWR; 5) overvoltage/overcurrent; 6) rf output balance. *Two meters* monitor collector current, voltage, and forward/reverse power. And a highly efficient *automatic line voltage correction* circuit (patent applied for) eliminates the need for selecting transformer taps, prevents applying too high a voltage to final amplifier devices, becomes operative under low line conditions.

Super Power Supply. Provides approximately 45 VDC @ 24 amperes, operates on 105/125 VAC or 210/250 VAC. Tape wound transformer and choke reduce weight (50 lbs.) and size (7½"h x 15¾"w x 13½"d). Separate enclosure.

Super Styling. Designed to match OMNI, the HERCULES has the same height as OMNI, plus matching bail and matching colors. The front panel is simplicity in itself with two push-button switches (power and mode) plus two knobs (meter and bandswitch), and a "black-out" monitor panel (when unit is off, meters are unobtrusive). Amplifier size is 5¾"h x 16"w x 15½"d.

Model 444, HERCULES amplifier & power supply.... $1575.

Experience SUPER RIG at your TEN-TEC dealer, or write for full details.

TEN-TEC, INC.
SEVIERVILLE, TENNESSEE 37862
EXPORT: 5715 LINCOLN AVE., CHICAGO, ILL. 60646

CONTESTS

Robert Baker WB2GFE
15 Windsor Dr.
Atco NJ 08004

HUNTING LIONS IN THE AIR CONTEST

Starts: 1200 GMT January 10
Ends: 1200 GMT January 11

The contest is sponsored by Lions Clubs International and coordinated by Lions Club Rio de Janeiro Arpoador, Brazil. Participation in the contest is open to all duly licensed radio operators, Lion and non-Lion. There are two modes—phone and CW. Participation in both modes is allowed, but points are counted separately. All amateur stations participating must operate within their licensing regulation. Separate categories will exist for single operator and radio clubs/societies. Multi-operators may participate, but each prefix must be listed dn the log.

Use all bands, 80 through 10 meters. Only one QSO with the same station on each band may be counted. Remember that phone and CW are counted separately!

EXCHANGE:

RS(T) and sequential QSO number. When contacts are made with Lions and Leos, the name of the Lions Club or Leo Club contacted should be clearly identified.

SCORING:

QSOs within the same continent count 1 point, while those between different continents count 3 points. Score 1 extra bonus point for each QSO with a member of a Lions Club or Leo Club and 5 points for a QSO with a member of the Lions Club Rio de Janeiro Arpoador. Contacts between Brazilian stations and members of the Arpoador club will count only 2 extra points.

AWARDS:

Lions Club International will present awards for single operators for first, second, and third place on both modes. The first-place winner in each mode will receive a trophy, the second-place winner will receive a medallion, and the third-place winner will receive a plaque. A trophy will be awarded to the first-place radio club on each mode. Certificates will be awarded fourth- through tenth-place winners in each mode for single operators. In addition, each log sent by participants, radio clubs, or radio societies will receive a special certificate. The contest committee will also select and award the most active Lions Club participating in the contest.

ENTRIES:

Keep a separate log for each mode. Each participant will note in the logs the callsign and information exchanged. Confirmation of contacts will be made by comparing the logs of the participants. Participants should send their logs not later than 30 days after the contest to: Contest Committee—Hunting Lions in the Air, Lions Club of Rio de Janeiro Arpoador, Rua Souza Lima #310, Apt. 802, 22081 Rio de Janeiro RJ Brazil.

2nd ANNUAL INTERNATIONAL 160-METER PHONE CONTEST
Sponsored by 73 Magazine
Starts: 0000 GMT January 17
Ends: 2400 GMT January 18

This is the second annual 160-meter contest sponsored by our magazine. The object is to work as many stations as possi-

Continued on page 155

CALENDAR

Jan 3-5	Zero District QSO Party
Jan 10-11	Hunting Lions in the Air
Jan 17-18	73's International 160-Meter Phone Contest
Jan 17-18	Michigan ARP Club CW Contest
Jan 17-18	ARRL VHF Sweepstakes
Jan 17-19	QRP SSB QSO Party
Jan 18	FRACAP Worldwide Contest
Jan 24-25	Texas QSO Party
Jan 31-Feb 8	ARRL Novice Roundup
Feb 2-3	CWSP International DX Competition
Feb 14-15	QCWA QSO Party—CW
Feb 21-22	ARRL DX Contest—CW
Mar 7-8	1981 SSTV Contest
Mar 7-8	ARRL DX Contest—Phone
Mar 14-15	QCWA QSO Party—Phone
Mar 21-22	Bermuda Contest
Mar 21-22	CARF Phone Commonwealth Contest
Aug 8-9	European DX Contest—CW
Sep 12-13	European DX Contest—Phone
Nov 14-15	European DX Contest—RTTY

AMATEUR RADIO NEWS SERVICE (ARNS)
1980 PUBLICATION CONTEST INFORMATION

Mail one copy each of any of three issuances during the period from July, 1979, through July, 1980, to:

Arny Gamson K6PXA, Chairman
ARNS Publication Contest
8034 Gentry Ave.
North Hollywood CA 91605

Papers will be reviewed by a team of three judges. Points will be awarded by each judge independently based upon the criteria discussed below. Final average totals will be adjusted up or down based upon a group reevaluation of all papers. All papers will receive an award and, based upon adjusted point value, will be judged OUTSTANDING, EXCELLENT or HONORABLE MENTION. All papers will also receive a summary critique on their favorable qualities and the judges' constructive suggestions for improvement.

Criteria for judging will include achieving the apparent goals of:

- Purpose of publication
- Interest to readers
- Imagination and attractiveness of layout
- Mast, titles, and layout
- Humor and cartoons
- Members' involvement and contribution
- Ease of readability of product

The following "housekeeping" items will be considered:

- Date and frequency of issue
- Name and address of editor and officers of sponsoring organization
- Utilization of ARNS emblem and ARNS contributions from the *Bulletin* (if member)
- Minimal effect will result from method of reproduction unless it affects the readability
- Technical articles and recruiting/training/subscriber solicitation material will be evaluated on an appropriate basis

Decision of the judges will be final. Scores/critiques of individual papers will be issued to individual entrants. Categories earned will be publicized.

There is no entry fee or membership in ARNS required. The contest is international and open to all amateur radio clubs, societies, organizations, groups, etc., issuing periodicals. Include separate recruiting, training, etc., material issued in connection with your paper.

Deadline for submissions two weeks after receipt of this publication.

INFORMATION TO BE INCLUDED WITH PUBLICATION CONTEST APPLICATION

1. Name of publication
2. Frequency of issue
3. First issue date
4. Circulation (No. sent to members/Complimentaries)
5. Club dues or subscription rate
6. Sponsoring group (if any)
7. Club mailing address
8. Editor's name, call, phone number
9. Editor's address
10. Editor's city, state, ZIP
11. Editor: How long this paper? Other papers (list and how long associated)?
12. Method of printing (offset, copier, stencil, spirit)
13. Approximate cost of printing each issue
14. Postage
15. Principal objectives of your paper
16. Items judged which you feel are *not* applicable to your paper
17. Remarks
18. Amateur Radio News Service member?

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TS 520 SE	629.95
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CW - 520 FILTER	
TOTAL	629.95

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TERRY ELIMINATOR FOR MOBILES REQUIRES MINOR

TELSTAR ENTERPRISES TR-2400 BA

DRAKE TR7

synthesized hf transceiving system

continuous coverage

0-30 MHz — continuous coverage reception no gaps no range crystals required

160-10 Meters — Amateur Band transmission, including capability for MARS, Embassy, Government, and future band expansions

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R. I. T.
INDEPENDENT RECEIVE SELECTIVITY WILL HANDLE WARC BAND EXPANSIONS

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ETO/ALPHA SOME LEFT AT OLD PRICES

BELDEN

	Part Number	MHz	dB/100 ft	dB/100 m
RG8/u Dbl. Shield	9888 56¢/ft.	50	1.2	3.9
		100	1.8	5.9
		200	2.6	8.5
		300	3.3	10.8
		400	3.8	12.5
RG8/u Foam .81VF	8214 32¢/ft.	50	1.2	3.9
		100	1.8	5.9
		200	2.6	8.5
		300	3.3	10.8
		400	3.8	12.5
RG8/u Regular .66VF	8237 28¢/ft.	100	2.0	6.6
		200	3.0	9.8
		400	4.7	15.4
		900	7.8	25.6
RG8/u Non-contaminating	8267 36¢/ft.	100	2.0	6.6
		200	3.0	9.8
		400	4.7	15.4
		900	7.8	25.6

8448 24¢/ft.

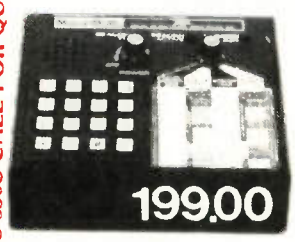
No. of Cond — 8
AWG (in mm) —
6-22 (7 · 30),
2-18 (16 · 30). (1.19)

9405 38¢/ft.

No. of Cond — 8
AWG (in mm) —
2-18 (26 · 30)
6-18 (16 · 30). (1.17)

MINI RG-8 19¢ FOOT

MEMORY KEYER BREAK-THROUGH!



The remarkable AEA Morsematic memory keyer has 35 fantastic features including two AEA designed microcomputers, up to 2,000 character memory, automatic serial number, beacon mode and automatic morse trainer mode.

NEW! CONTEST KEYER CK1 - 129.95

AEA
Brings you the Breakthrough!

TS-130S & TS-830S CALL FOR QUOTE.

LARGE BOOKSTORE - WHAT DO YOU NEED?

ALL BAND COVERAGE!
160 THROUGH 10, INCLUDING WARC
9 BANDS FULLY OPERATING

ASTRO 103
Professional Grade
HF SSB Transceiver

- 100 WATTS ALL BANDS ALL MODES
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Astro 150 A	779.00
Astro 100MXA	499.00
Mirage B23 1 watt-30 Watt amp	89.95
DSI 5600A w/Ant/Ac	185.00
Cushcraft A3 Tribander	169.00
Bird 43, Slugs	Stock
CDE Ham-4 Rotor	169.00
Ham-X	239.00
FDK Palm 2 Handie with BP/AC	149.00
Cetron, GE 572 B	34.00
GE 6146B	9.95
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Telrex TB5EM	425.00
Belden #14 8000 Stranded Antenna Wire	10¢ ft.
Telrex Monobanders	Stock
Adel Nibbling Tool	8.95
Janel QSA5	41.95
Rohn Tower 25G, 45G Sections	20% off dealer
Alliance HD73 Rotor	109.95
Amphenol Silverplate PL259	1.00
ICOM 255A 2M Synthesized	319.00
ICOM 260A 2M SSB/FM/CW	429.00
Kenwood TS180S/DFC/SSB	Call
ICOM IC2AT/TTP/NICAD	229.00
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Bearcat 220 - $299.00	300-399.00
Manual Typewriters Guarenteed to Work	$35
Mallory 205A/1000 PIV Epoxy Diode	19¢ ea.
Antique Tubes	Call

2 Guaranteed Service Techs on COLLINS KWM-2/KWM-380/S-LINE. CALL!

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HOUSTON, TEXAS 77010

AWARDS

Bill Gosney KE7C
c/o Micro-80 Inc.
S-2665 No. Busby Road
Oak Harbor WA 98277

COMPU-WARD

As publicized in over 25 individual amateur radio publications throughout the world, the COMPU-WARDs, sponsored by Micro-80 Incorporated, are available to licensed amateurs and shortwave listeners worldwide. Emphasis of these award programs is focused on the advancement of both the amateur radio and computer hobbies through demonstrated excellence in the art of computerized communications.

Stations applying for these awards may or may not have a computerized station of his/her own; however, *all stations contacted must be computerized*, meaning the contacted station must have his/her transmitter interfaced with a computer, such as the well-known TRS-80, Apple II, Commodore PET, Heathkit, Atari, etc.

To be valid, all contacts must be made on or after January 1, 1980. There are two (2) awards being offered: (1) HF bands—29.7 MHz and below; (2) VHF/UHF—50.0 MHz and above.

All contacts must be made on one or any combination of the following modes (including any modes authorized by the FCC since the release of this announcement)—RTTY, SSTV, CW, and ASCII. Crossmode communications will not be recognized for these awards.

Single-band and mixed-band endorsements will be given with each band segment (HF, VHF, UHF, etc.). Crossband operation will only be accepted for OSCAR contacts. All OSCAR contacts will be considered only for VHF/UHF accomplishments even though some of the OSCAR satellites have receive frequencies on 10 meters. Contacts via repeaters are acceptable.

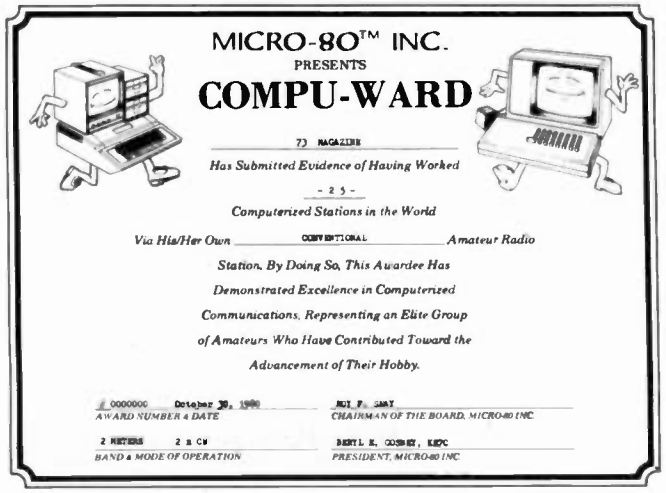
To qualify for either COMPU-WARD:

Applicants *with* a computerized station of his/her own must contact a *minimum of 15* other computerized stations on the bands and modes authorized.

Applicants *without* a computerized station of his/her own must contact a *minimum of 25* computerized stations on the bands and modes authorized.

To apply, prepare a list of contacts for each award. In prefix order, list each call worked, mode utilized, frequency or band of operation, and date and time of each contact made. *Do not send QSL cards!* Have your list of contacts and supporting QSL cards verified by two fellow amateurs or a local radio club official. The services of a notary may be sought if applicants prefer.

Forward the verified list with $4.00 for each award. Send your application to the Oak Harbor address of Micro-80 listed above. Foreign stations may substitute the awards fee by enclosing 10 IRCs for each award sought.



Last month we reviewed the very challenging Gozo Island Award and completely overlooked the very beautiful DIP-MED Award Diploma. My apologies to MARL for this obvious error.

DIP-MED AWARD

Awarded to any licensed amateur, the DIP-MED Award has no band or mode restrictions; however, single band or mode accomplishments will be recognized if requested at the time application is made.

To qualify, HF applicants must work a minimum of 15 Mediterranean countries including 9H Island of Malta. On VHF, only 5 Mediterranean countries including 9H Malta need to be confirmed.

To apply, prepare a list of claimed contacts indicating callsign, date and time in GMT, the band and mode of operation, and the country contacted. Have this list verified by at least two fellow amateurs or a local radio club official. Forward the application and $3.00 or 12 IRCs to: MARL, PO Box 575, Valletta, Island of Malta.

Mediterranean countries include: Malta, Spain, Balearic Islands, Ceuta and Melilla, France, Corsica, Morocco, Algeria, Tunisia, Monaco, Italy, Sicily, Sardinia, Greece, Cyprus, Crete, Dodecanese Isles, Gibraltar, Yugoslavia, Albania, Israel, Lebanon, Egypt, Turkey, Syrla, and Libya.

GUAM ISLAND AWARD

I am proud to announce the very latest award being offered by the Mariana Amateur Radio Club of Guam Island, known as the Guam Island Award. The requirements of the award are very straightforward. Applicants must work and confirm at least five (5) individual amateurs located on Guam Island.

There are no band or mode restrictions; applicants must have their list of contacts verified by at least two amateurs or a radio club secretary. Be sure to give the usual log book information plus the name of the operator for the contact to count.

Enclose your application and an award fee of $1.00 or 5 IRCs to: Mariana ARC of Guam, PO Box 445, Agana, Guam 96910.

ANNUAL 73 MAGAZINE AWARD ENDORSEMENTS

The end of 1980 brings to a close another eventful year of enjoyable operating. Award seekers can now tabulate their totals and make application for their annual endorsements for the *73* DX Country Club Award and the Worked All USA Award. To learn more about both of these very challenging awards and the seventeen other programs which accompany them, turn in your back issues of *73* to my Awards column for the months of September and October. The entire details of the *73 Magazine* Awards portfolio are featured there.

WABP AWARD OF BELGIUM

The UBA Awards Manager, ON5TO, has announced the very popular WABP Award Program. This award is available to licensed amateurs and SWL stations. There is no limit as to date; there are no band or mode restrictions.

To qualify for the WABP Award, the applicant must work and confirm contact with each of the nine Belgium provinces on a minimum of two amateur bands.

Once the requirements have been met, have your list of contacts verified by a radio club official. Do not send QSL cards!

Enclose your verified application and five (5) IRCs to: ON5TO, UBA Awards Program, PO Box 634, Brussels, Belgium.

Belgium provinces include: WV—West Flanders; OV—East Flanders; AN—Antwerp; LM—Limburg; LG—Liege; LX— Luxembourg; NR—Namur; HT—Hainaut; BT—Brabant.

While in Belgium, we have learned of another award incentive which should capture the interest of most DX stations, the Onion Award.

THE ONION AWARD OF BELGIUM

Licensed amateurs or SWL stations will find this award a considerable challenge. Only contacts made with the Aalst section of Belgium will count and these contacts must be established after January 1, 1975, to be valid.

Continued on page 158

ICOM IC2AT OWNERS SCANNER

Also available—scanners for

KENWOOD TR7400A, TR7600 & TR7625, TEMPO (S-1, S-1A, S-2, S5), KDK 2015R, KDK 2016A, ICOM IC22S, MIDLAND 13-510, 13-513, CLEGG FM-28, YAESU FT227R

•AED continues to expand its line of quality scanners.

•All of AED's scanners are custom designed to install completely inside of their respective rigs.

•Installation is simple. Unlike other competitive products all AED scanners are designed so that it is totally unnecessary to cut any wires inside your rig during installation.

•All P.C.B.s are silk-screened and tin plated for easier and more effective soldering.

•The kit comes complete with all parts and a detailed instruction manual including schematics.

•In the scanner OFF mode the rig operates normally. In the scanner ON mode the scanner locks on an occupied frequency, pauses for a preset time (about 5 sec.) and then resumes scanning (except 22S).

•The frequency being scanned is displayed on the digital readout (except 22S IC2AT and Tempo).

•This gives you the ability to eavesdrop all over the band without lifting a finger. When you hear something interesting, you flip the switch to the LOCK mode and the rig is ready to transmit.

SUPER SPECIAL

KIT PRICE: REG. $39.95
SPECIAL NOW $34.95
(TEMPO & IC2AT PREASSEMBLED ONLY)
PREASSEMBLED: REG. $59.95
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TRS-80/RTTY

The Crowning Touch

ROM-116

Amateur RTTY Operating System

• MODES: RTTY (ASCII or BAUDOT) • CW •

• REAL-TIME CLOCK: 24 hour clock • Automatic updating • Time display includes day, month and year.

• SPLIT-SCREEN VIDEO: 12 lines receive text • 3 lines transmit text or pre-typing a message • 1 line display, real-time clock • Status displayed continuously • Word-wrapping.

• TWO SERIAL PORTS PROVIDED: Port "A" -Interfaces to internal or external terminal unit • RS-232, TTL and 60 ma. • ASCII/BAUDOT •

Supports any 8-level serial printer or modem • Baud rate keyboard selectable • Expansion interface not required for operation of serial printer or modem.

• BUFFERS: 7.5K Main text buffer • Pre-typed messages up to 7.5K possible. • 2.5K general purpose buffer •

• AUTOMATIC CW/ID: At the start/end of each transmission • Every 10 minutes • Provision for quick break (no ID).

• TRANSMITTER CONTROL: Transmitter turns on/off automatically via software control • Provisions made for quick break.

• SOFTWARE PROVIDED: 2 RTTY Programs (Cassette/Disk version) • ASCII/BAUDOT Driver routines (permits use of "LLIST" and "LPRINT" commands from basic) • CW send/receive program.

• HARDWARE REQUIREMENTS: TRS-80 with 16K RAM • External terminal unit recommended (Flesher TU-170, ST-6 etc) • AFSK/FSK unit.

PRICE **$300** with cabinet

CROWN MicroProducts

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Marysville, Washington 98270
206-659-4279

•A Trademark of The Tandy Corp.

Preamplifiers

The famous Palomar Engineers preamplifier has been updated and packaged in an attractive new cabinet.

For the SWL there is the P-305 (9-v DC powered) and the P-308 (115-v AC powered) featuring full shortwave coverage, selection of two antennas, 20 db attenuator, 15 db gain control and on-off-bypass switch.

For transceivers, the P-310X features automatic bypass on transmit, adjustable delay for return to receive, and 350 watt transmit capability.

All models have these features:

- **Up to 20 db gain.**
- **Covers 1.8 to 54 MHz in four bands.**
- **Low noise figure.**
- **Reduces image and spurious response.**
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- **SO-239 connectors.**
- **LED pilot.**

Order direct or from your favorite dealer. Model P-305 Receiver Preamplifier for 9-v DC $77.95. Model P-308 for 115-v AC $87.95. Transceiver Preamplifier Model P-310X $107.95. Add $3 shipping/handling. Calif. residents add sales tax.

Don't wait any longer to pull out weak, rare DX.

Palomar Engineers

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Phone: [714] 747-3343

RTTY LOOP

Marc I. Leavey, M.D. WA3AJR
4006 Winlee Road
Randallstown MD 21133

Let's start off the New Year with a look back at some things we have mentioned in the past few months.

Several months ago, I reviewed the Jameco JE-610 ASCII keyboard. One of the troubles I noted was that, in spite of advertisements proclaiming the "full 128-character ASCII character set," the keyboard is unable to generate one code, $1F, as supplied, and another, underline ($5F), is omitted from the keyboard, although it can be generated with some manipulation. I related that Jameco acknowledged the problem, although no apparent fix has been offered. Well, take a look at the latest ads for the keyboard. No longer is the "full 128-character set" claimed; now the keyboard's "60 keys generate the *126* characters, upper- and lowercase ASCII set." Don't change the hardware, just the software, or something like that! Oh, well.

Also back a few months, we reviewed the iRL FSK-1000 RTTY demodulator. In it, I issued a challenge, albeit half-heartedly, to tell which button on the panel was pushed. Well, in response to the many questions, only the "170-Hz Shift" button is depressed. All others are in the "out" position. Study the picture if you don't believe me.

Now, quite some time back, extending over the many subsequent months, we have been following the progress of a firm known as Teleprinter Art, Ltd. To my knowledge, no repeat inquiries to the firm have been answered and, as of this writing date, I am forwarding a good deal of the correspondence and details received to the Postal Inspectors. I will try to keep anyone forwarding information to me informed of the progress of any investigation.

About a year ago, we passed along the saga of George Firmin WA4FSK, who wondered what weather transmissions such as

66228 05210 05315 05323 04928
66028 06525 06234 05838

mean. Now along comes a note from Robert Munro in Newport, R.I., who used a book entitled *Worldwide Marine Weather Broadcasts* to decode the above. His translation reads: 66228 = Warm front at surface, weak, and frontal characteristics decreasing. 052 N. latitude, 10 W. longitude, 053 N. longitude, 15 W. latitude, etc. 66028 = Quasi-stationary front at surface, weak, little or no change. Frontal characteristics diffused. 065 N. latitude, 25 W. longitude, etc.

Thanks to Robert for the help. He wonders if anyone has a computer program to decode this type of information. I would suggest that the data is encrypted in a rather straightforward manner and that anyone reasonably fluent in BASIC should be able to put the book's tables into a program. Ask around your area.

While we're talking about computers (slid into that one, didn't I?), George Gadbois W3FEY passes along his contribution in the form of a UART interface for the RCA VIP computer. This allows George to use his VIP, which is an 1802-based computer, on Baudot and ASCII. His straightforward design is shown in Fig. 1.

George also noted that the Red Rose Repeater Association in Lancaster, Penn., is in the center of a few two-meter RTTY repeaters. The Harrisburg machine is on 147.975/.375 and a "computer link" to Eagleville may be found on 146.235/.835. Keep up the good work, fellas!

Buzz Gorsky K8BG, of Carlisle, Penn., writes in regarding his Model 15. It seems as though a non-overline, automatic CR/LF gizmo has been added, and Buzz wants to turn it off! Of course, with such a device, intentional overlines, such as in many pictures, are impossible. Well, Buzz, there are at least three non-overline schemes I have seen used in a Model 15, and how you defeat it depends on which one or another you have. The best I can offer, sight unseen, is to look for a lever or hook that the typing basket trips as it passes the sixty-fifth space or so, roughly where the bell would ring. This usually is the actuator and has a lever which can be swung out of the way. Perhaps some of the RTTY nuts in the Red Rose Repeater Association can help you. Write them at PO Box 5029, Lancaster PA 17601.

73 does get around. A letter from John L. Webster 9Y4JW/8P6KX in Trinidad, asks about the software to put the 6800 computer on RTTY. Well, John, over the past few years several separate receiving and transmitting routines have been published in this column. Copies of these are still available at $1.00 each to cover reproduction and postage. However, these two have formed the nucleus for a bigger and far better program, a full transceive program for RTTY with a 6800. Featuring preloadable buffers, variable speeds, and a true FIFO, the program fits in less than 4K of memory. Want more? How about one key RYRY, QUICK BROWN FOX, and ID, and throw in a CW ID to boot. And how much will this wonderful program cost? Why, not a cent more than you already spend, for it shall be published soon right here in *73*! So don't let your subscription lapse; watch for this fantastic program.

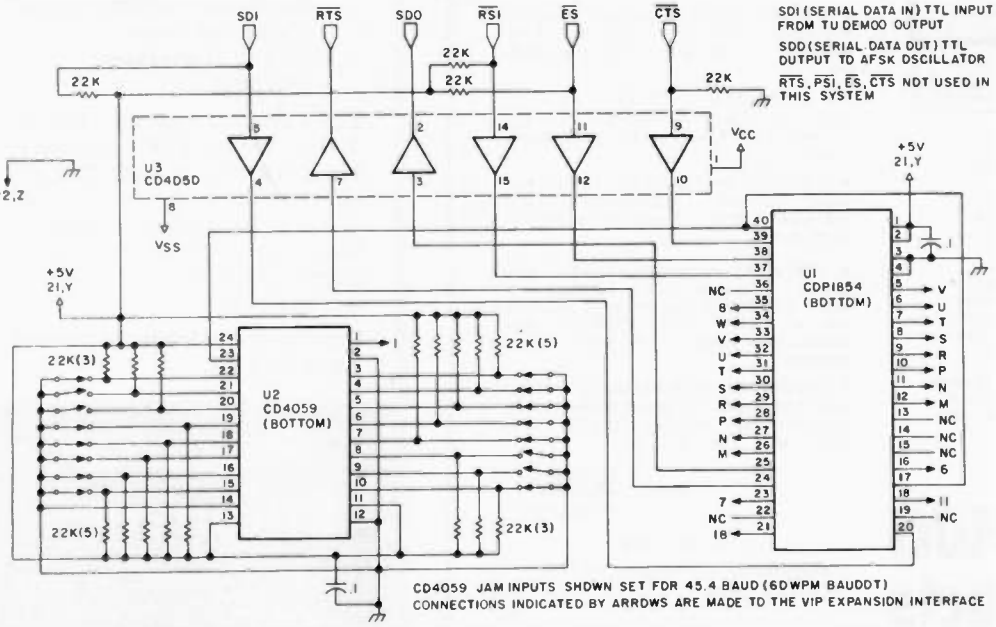

Fig. 1.

Kevin McKewen WA3LPK, a new RTTYer here in the Baltimore area, has acquired a HAL ST-5 and AK-1 setup, sans literature. He wonders if data is still available. Sure is, Kevin. HAL maintains a full spectrum of literature on all their products, and I am sure that they would be glad to help out anyone who drops them a line at HAL Communications Corp., PO Box 365, Urbana, Illinois 61801. And don't forget to mention RTTY Loop, OK?

Anyone around Rockland, Massachusetts, want to give a newcomer a hand? George Beaupre KA1CGP is putting a Model 32 on the air and is looking for suitable demodulators. This brother of the ASCII Model

Continued on page 31

A touch of Class

There are those who will only be satisfied with the finest.

For these perfectionists HAL Communications is pleased to offer the DS 3100 Automatic Send-Receive ASCII, Baudot and Morse Terminal.

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LETTERS

H 5 H, COMRADE

This letter has been started at least a half-dozen times during the past several months, only to be pushed aside by the press of some other matter and to then be restarted when triggered by something I read or heard.

This time, the "kick" was a comment of yours in *73* calling attention to the fact that the activities of the Russian Woodpecker were markedly reduced during the time WARC was in session. I suspect, for reasons that I'll try to make clear in this letter, that although your observation is quite correct, factors other than WARC may have played a significant role.

Some months back, I found it necessary to visit the Bonn-Cologne area of the Federal Republic of Germany, a locale in which there are a great number of good friends. Some are still quite active, professionally speaking; others are retired or (as am I) semi-retired.

I decided to make an unannounced call upon one of my better friends in Bad Godesberg, Herr S., who had retired from a very senior position in the Federal Ministry of Defense a few years back.

Frau S. met me at the door as casually and as graciously as though I'd never been away and then knocked the pins out from beneath me by stating quietly that my good friend Gunter had passed away only weeks earlier. She invited me in, but I'd had enough for one day.

I went over to the Weinhaus Maternas. Frankly, I've never thought too much of the place. My wife and I used to dine there from time to time until John Le Carre mentioned it in his book, *The Spy Who Came*... After that, the prices and the crowd increased while the...well, enough said!

One thing, though—if anyone were to be found anywhere in town, it would be there. Or back at the American Embassy club in Plittersdorf, and I didn't feel like driving over to the American community right then.

I was shown to an empty table and, before my eyes were fully adjusted to the light level, someone sat at the table across from me. Actually, I didn't really have to see him—the voice and accent were enough. It was Alex K. He'd been the scientific and technical attache at one of the eastern bloc embassies during most of my period there. I thought that he'd left about the same time as I. We'd met frequently at formal functions but I don't recall ever before having been with him in as private a situation as right then.

I might add that I had often teased him about defecting to our side. He has and had a great sense of humor and took the kidding in stride...I think. At any rate, he seemed to sense my mood and appeared to be really trying to cheer me up.

After a few glasses and some trivial banter about mutual acquaintances, my humor gradually restored itself, but it was clear that Alex didn't realize it. It was about then that he inquired if there was anything that he could do for me, meaning, of course, to further cheer me up. I chose deliberately to misunderstand that. And now we come to the point: I asked him why his friends didn't turn off that "damned over-the-horizon radar" and stop "screwing up" the ham bands.

The man was shocked! He looked at me in total disbelief, accusing me of once again pulling his leg. He refused to accept the statement that the Woodpecker (by the way, he found the name amusing) was really bothering US hams. He mentioned that there were many amateurs in countries much closer to the radar's transmitter site than are the Americans.

Then, as I recall it, he said something about their technology being better than ours and able to cope with simple periodic interference. Finally, he noted that the West German amateurs seemed to have reduced the problem, referring to a technical paper that he'd seen in *CQ DL*, the FRG ham magazine, sometime in the summer of 1978. (Editor's Note: Also see *Ham Radio*, June, 1980.)

Still feigning a by-then completely dispelled ill humor, I said something like, "Dammit, I'm not smart enough, personally, to engineer a blanking circuit to eliminate the pulse noise for each of my rigs! Why don't you do the whole world a favor and just turn the thing off?"

Imagine my surprise when, after a rather lengthy pause, he very quietly said that he supposed something could be done to alleviate the problem. He didn't elaborate on that statement but did go on with something in the same vein. He said that if "that" (sic) doesn't take care of things, whenever the signal is exactly on my frequency, I am to swing my antenna to beam a signal over the pole and to send "H 5 H" in Morse.

I distinctly recall his telling me that the dot frequency should be exactly 10 Hz (about 13 wpm), as it was obvious that he was suggesting synchronization with an unnamed something, such as, for example, the Woodpecker's pulse repetition frequency. He said no more on the matter, turning the conversation towards questions of my family's health and other innocuous subjects. I left Alex and Maternas' shortly thereafter.

The meeting was prior to WARC so one can't say whether it was WARC or that chance encounter that resulted in a lessening of the Woodpecker's activities. It does seem to me that the interference has been somewhat less than in the past, even since the WARC.

I, of course, will neither admit to ever sending a coded "H 5 H" in order to clear a frequency nor will I suggest that others try Alex's proposed solution because I'm not sure whether the FCC would call such a transmission illegal coding or deliberate interference. I thought, however, that it might interest everyone to know the possibilities, not to mention knowing *really* why the Woodpecker is down.

(Name withheld by request)

Many of us have found that synchronized dots sent on the Woodpecker frequency will move it. Somehow I doubt if the FCC would have any objections to such counteraction to this invader of our bands.—Wayne.

20-YEAR KUDOS

Congratulations on 20 years of *73*! And what a fabulous issue to commemorate!

You know, I have every issue of *73* here on two shelves, and I consider them to be one of my most valuable possessions.

Best luck in the next 20 years!

Ron Johnson WA5RON
Austin TX

THINK POSITIVE

Happy Anniversary! Keep it up!

E. P. Rolek K9SQG
Dayton OH

A GOOD INVESTMENT

About 20 years ago, I took a chance on a new ham magazine called *73*. I invested my life's savings (students were very poor in those days and so were magazine publishers) in one of your life subscriptions. The deal was your life or mine.

I figure that both of us have a good investment in each other. From those early days, the magazine and you have grown and become prosperous; so have I. I now am one of those "electron" engineers. Ham radio had something to do with it. I hope the next 20 years are as good for both of us.

Until I read the anniversary issue editorials, I did not know that you were a member of MENSA. So am I.

Clive Frazier K9FWF/4
Orlando FL

CONSERVING ENERGY

Don't you think it would be appropriate at this time to devote one page of *73* to ideas and concepts of conserving energy? I'm sure amateurs the world over have experimented and come up with systems. I utilize a large heat sink placed on a coal stove and blow air over it with a muffin fan. I get heated air at 90°. I am now working on a pre-heater for the fan air by building a jacket around the stove pipe and pulling the air through it.

Continued on page 158

✓Reader Service—see page 194

FUN!

John Edwards WB2IBE
78-56 86th Street
Glendale NY 11385

This month's "Fun!" offering should really set your heads spinning. Instead of concentrating on one specific operating endeavor, as in our previous quizzes, this month we'll be testing you on the entire gamut of amateur radio history, everything from spark to space communications, with lots of other interesting highlights in between. So get those thinking caps on, for this month we learn about ham history.

ELEMENT 1—CROSSWORD PUZZLE
(Illustration 1)

Across

1 One end of first transatlantic QSO
2 End of contact
8 Morse question mark
9 British tube
11 Disaster Radio Service (abbr.)
13 "Shahland" prefix
15 Upstart ham organization of 1950s (abbr.)
17 Status of 11-meter amateur band
19 Initials of government man who reopened our bands after WWI
20 Low frequency (abbr.)
23 Former deceptive ham outlet
26 WWII ham substitute (abbr.)
28 Irish prefix
29 It replaced spark (abbr.)
32 80-10 meters (abbr.)
34 Old receiver
36 Our fate
38 Caribbean QTH (abbr.)
39 Former ham manufacturer

Down

1 6-meter predecessor (2 words)
2 Old traffic post (abbr.)
3 What we get on
4 Before SOS
5 Greek prefix
6 New Novice-type call
7 Triode inventor
10 Idle ham
12 November contest (abbr.)
14 Wouff_____
16 Audio frequency (abbr.)
18 Element (abbr.)
21 FCC predecessor (abbr.)
22 Long wave (abbr.)
24 Old FCC agent (abbr.)
25 Equipment
27 ARRL appointee (abbr.)
30 QRZ?
31 FCC legal step (abbr.)
33 RACES official (abbr.)
35 Cycles_____second
36 Bad op
37 "The Old Man" (abbr.)
38 Former Novice prefix

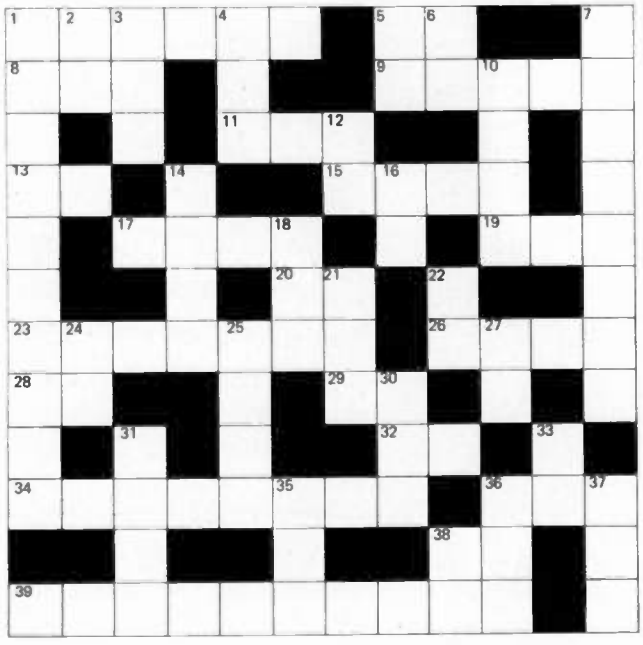


Illustration 1.

ELEMENT 2—MATCHING

Match the former ham manufacturers and distributors in Column A with their QTHs in Column B.

Column A		Column B	
1	E. F. Johnson	A	Brooklyn NY
2	RCA Electron Tubes	B	Roslyn NY
3	Gonset	C	Chicago IL
4	Lafayette Radio	D	Millington-Watchung NJ
5	Atlas Radio	E	Indianapolis IN
6	Hammarlund	F	Hicksville NY
7	Hallicrafters	G	Council Bluffs IA
8	Regency	H	New York NY, Mars Hill NC
9	Uncle Dave's Radio Shack (Fort Orange Radio)	I	Oklahoma City OK
		J	Waseca MN
10	Amperex	K	Rockford IL
11	Greenlee Tool	L	New York NY
12	Sonar Radio	M	Boston MA
13	Galaxy	N	Albany NY
14	Terminal Radio	O	Kansas City MO
15	LTV-University	P	Harrison NJ
16	RME-ElectroVoice	Q	San Francisco CA
17	Burstein-Applebee	R	Buchanan MI
18	Alltronics-Howard	S	Jamaica-Syosset NY
19	Squires-Sanders	T	Burbank-Anaheim CA
20	Sideband Engineers	U	Oceanside CA

ELEMENT 3—MULTIPLE CHOICE

1) In 1921, the "Transatlantic Tests" were held to see which amateur could first transmit a signal from America to Europe. What was so unusual about the first ham to accomplish this feat?

1) He was a pirate signing 1AAW.
2) He sent his signal on 2 meters.
3) His signal was frequency modulated.
4) He was not an American, but a Canadian.

2) Back in the 1950s, General Electric sponsored an annual award presented to an "amateur who has rendered outstanding public service." The name of this award was:

1) The Maxim Award.
2) The Baldwin Cup.
3) The Edison Award.
4) The WB2LWJ Certificate of Merit.

3) Speaking of awards, the Elser-Mathes Trophy, currently on display in Newington, will be awarded to the first amateur who accomplishes:

1) A 2-way contact with Mars.
2) WAS on a microwave band.
3) The first digital phone transmission.
4) DXCC on fast-scan television.

4) We all know that Guglielmo Marconi invented radio. But did you know that he had a brother who helped him with many of the invention's trial experiments? What was the first name of this "other" Marconi?

1) Luigi
2) Alfonso
3) Kevin
4) Luciano

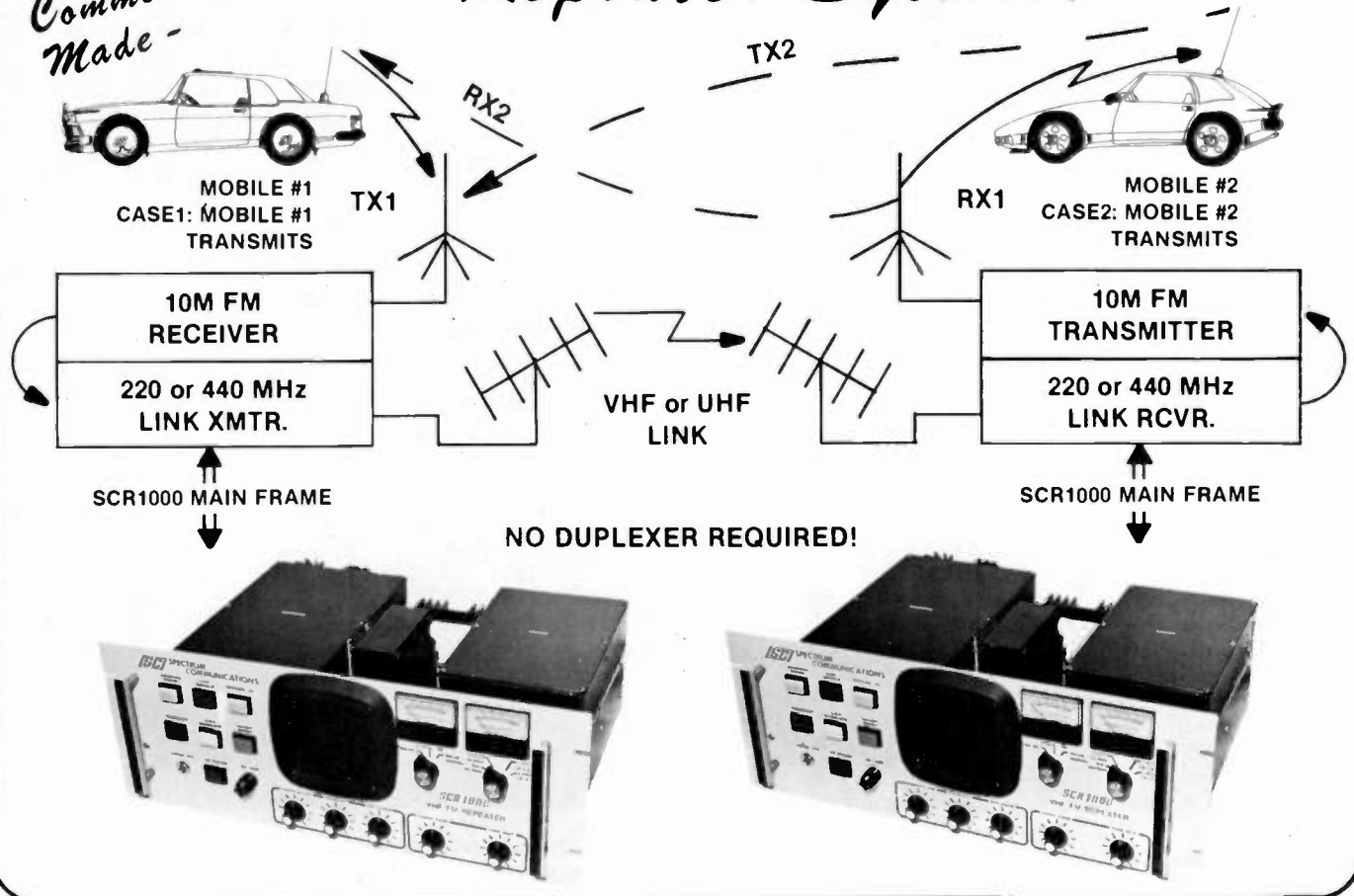
Continued on page 150

NEW

Now "In the works" at Spec Comm -

Complete 10M FM "Split Site" Repeater System!

The 1st Commercially Made -



- **JOIN THE FUN ON 10M FM!** This new phase of Amateur Radio is growing every day, and *promises to be one of the most exciting new modes of operation in years!*
- **10M FM COMBINES ALL OF THE BENEFITS OF VHF FM OPERATION WITH HF "LOW BAND" OPERATION;** i.e., the quiet, noise-free QSOs of 2M FM *except better ground wave range,* with less mobile fading and flutter due to hills and trees, etc. *Plus—occasional "Skip" contacts all over the country and around the world*. . . with all of the clarity and "solidness" of cross-town 2M FM contacts!
- **ON 10M FM,** you can use low cost, cutdown CB antennas and accessories. And, low cost 10M FM Transceivers are now available from other manufacturers.
- **ON 10M FM,** you can avoid the crowded conditions on other bands!

THE SPEC COMM 10M FM REPEATER SYSTEM IS COMPOSED OF 2—SCR1000 REPEATER/LINK UNITS. One unit includes the 10M receiver and a 10W 220 or 440 MHz link transmitter. The second unit (which should be operated a mile or more from the first) includes the 30 W 10M transmitter and a 220 or 440 MHz link receiver. Note that this system does *not* require a duplexer—which is impractical on 10M (over 8' high, and super expensive). Each of the 2 units is basically the same as our tried and proven SCR1000 Repeater which includes all of the necessary Audio and Control circuitry, plus AC Power Supply with instant Battery Switchover, CW IDer, full front panel controls and metering, etc., We can also supply 10M commercial grade vertical antennas, "Hardline" cable, cabinets, etc.

Call or write for further details on this new system which is now under development at Spectrum. Estimated price is about the same as 2—SCR1000 VHF Repeaters. ✓68

SPECTRUM COMMUNICATIONS

1055 W. Germantown Pk., Dept. S1 • Norristown PA 19401 • (215) 631-1710

✓ Reader Service—see page 194

KENWOOD
...pacesetter in amateur radio

TS-830S

"Top-notch"...VBT, notch, IF shift, wide dynamic range

The TS-830S has every conceivable operating feature built-in for 160-10 meters (including the three new bands). It combines a high dynamic range with variable bandwidth tuning (VBT), IF shift, and an IF notch filter, as well as very sharp filters in the 455-kHz second IF. Its optional VFO-230 remote digital VFO provides five memories.

TS-830S FEATURES:

- LSB, USB, and CW on 160-10 meters, including the new 10, 18, and 24-MHz bands. Receives WWV.
- Wide receiver dynamic range. Junction FETs in the balanced mixer, MOSFET RF amplifier at low level, and dual resonator for each band.
- Variable bandwidth tuning (VBT). Varies IF filter passband width.
- Notch filter (high-Q active circuit in 455-kHz second IF.
- IF shift (passband tuning).
- Built-in digital display (six digits, fluorescent tubes), analog subdial, and display hold (DH) switch.
- Noise-blanker threshold level control.
- 6146B final with RF negative feedback. Runs 220 W PEP (SSB)/180 W DC (CW) input on all bands.
- Built-in RF speech processor.
- Narrow/wide filter selection on CW.
- SSB monitor circuit to check transmitted audio quality.
- RIT (receiver incremental tuning) and XIT (transmitter incremental tuning).

OPTIONAL ACCESSORIES:

- SP-230 external speaker with selectable audio filters.
- VFO-230 external digital VFO with 20-Hz steps, five memories, digital display.
- AT-230 antenna tuner/SWR and power meter/antenna switch; 160-10 meters, including three new bands.
- YG-455C (500-Hz) and YG-455CN (250-Hz) CW filters for 455-kHz IF.
- YK-88C (500-Hz) and YK-88CN (270-Hz) CW filters for 8.83-MHz IF.

(VFOs for TS-830S, TS-130 Series, and TS-120S are compatible with all three series of transceivers.)

SP-230 TS-830S VFO-230 AT-230

TS-130S/V

"Small wonder"...processor, N/W switch, IF shift, DFC option

The compact, all solid-state HF SSB/CW mobile or fixed station TS-130 Series transceiver covers 3.5 to 29.7 MHz, including the three new bands.

TS-130 SERIES FEATURES:

- 80-10 meters, including the new 10, 18, and 24-MHz bands. Receives WWV.
- TS-130S runs 200 W PEP/160 W DC input on 80-15 meters and 160 W PEP/140 W DC on 12 and 10 meters. TS-130V runs 25 W PEP/20 W DC input on all bands.
- Built-in speech processor.
- Narrow/wide filter selection on both CW (500 Hz or 270 Hz) and SSB (1.8 kHz) with optional filters.
- Automatic selection of sideband mode (LSB on 40 meters and below, and USB on 30 meters and above). SSB REVERSE switch provided.
- Built-in digital display.
- Built-in RF attenuator.
- IF shift (passband tuning).
- Effective noise blanker.

OPTIONAL ACCESSORIES:

- PS-30 base-station power supply.
- YK-88C (500 Hz) and YK-88CN (270 Hz) CW filters.
- YK-88SN (1.8 kHz) narrow SSB filter.
- AT-130 compact antenna tuner (80-10 meters, including three new bands).
- SP-120 external speaker.
- VFO-120 remote VFO.
- MB-100 mobile mounting bracket.
- PS-20 base-station power supply for TS-130V.

Optional DFC-230 Digital Frequency Controller
Frequency control in 20-Hz steps with UP/DOWN microphone (supplied with DFC-230). Four memories and digital display. (Also operates with TS-120 and TS-830S.)

PS-30 SP-120 TS-130S VFO-120

TRIO-KENWOOD COMMUNICATIONS INC.
1111 WEST WALNUT / COMPTON, CA 90220

TS-180S with DFC

High quality...top performance, with optimum features

The top-of-the-line TS-180S all solid-state HF SSB/CW/FSK transceiver with DFC (Digital Frequency Control) provides maximum performance and efficiency for every amateur.

TS-180S FEATURES:

- All solid-state. 200 W PEP/160 W DC input on 160-15 meters, and 160 W PEP/140 W DC on 10 meters. Adaptable to three new bands.
- Dual SSB filter (optional) to improve selectivity, reduce noise, and improve RF-speech-processor operation.
- Digital Frequency Control (DFC), including four memories with digital up/down paddle-switch tuning in 20-Hz steps. Memories operate in transceiver or split modes. (Also available without DFC.)
- IF shift (passband tuning).
- Built-in digital display with differential function. Shows actual VFO frequency and difference between VFO and "M1" memory (or "hold" without DFC) frequencies.
- Selectable wide and narrow CW bandwidth.
- Tunable noise blanker.
- RF AGC.
- Automatic selection of upper and lower sideband (with SSB NORMAL/REVERSE switch).
- Dual RIT (VFO, memory/fix).

OPTIONAL ACCESSORIES:

- PS-30 base-station power supply.
- SP-180 external speaker with selectable audio filters.
- VFO-180 remote VFO.
- AT-180 antenna tuner/SWR and power meter/antenna switch.
- DF-180 digital frequency control (for TS-180S without DFC).
- YK-88C (500 Hz) and YK-88CN (270 Hz) CW filters.
- YK-88S SSB filter for dual IF filter system.

PS-30 SP-180 TS-180S VFO-180

TS-520SE

"Cents-ability" in a quality 160-10 meter SSB/CW rig

The TS-520SE is an economical, full-featured 160-10 meter transceiver, found in more ham shacks than any other rig.

TS-520SE FEATURES:

- 160-10 meters . . . and receives WWV on 15 MHz.
- 200 W PEP (SSB)/160 W DC (CW) input on all bands.
- CW WIDE/NARROW bandwidth switch for use with optional 500-Hz CW filter.
- Speech processor for extra audio punch.
- Effective noise blanker.
- 20-dB RF attenuator.
- RIT (receiver incremental tuning) control.
- Digital display with optional DG-5, showing actual operating frequency while transmitting and receiving.
- Eight-pole crystal filter for excellent selectivity.
- Built-in 25-kHz calibrator, adjustable to WWV.
- VOX and semi-break-in CW with sidetone.
- Built-in speaker.
- Solid-state, with tube driver and final.
- Amplified-type AGC circuit.
- Amplified-type ALC.
- Front-panel carrier level control.

OPTIONAL ACCESSORIES:

- SP-520 external speaker.
- DG-5 digital frequency display and 40-MHz counter.
- VFQ-520S remote VFO.
- CW-520 500-Hz CW filter.
- AT-200 antenna tuner/SWR and RF power meter/antenna switch.

SP-520 TS-520SE VFO-520S

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TR-7800

"Easy selection"...15 memories/offset recall, scan, priority, DTMF (Touch-Tone®)

Frequency selection with the TR-7800 2-meter FM mobile transceiver is easier than ever. The rig incorporates new memory developments for repeater shift, priority, and scan, and includes a built-in autopatch Touch-Tone® encoder.

TR-7800 FEATURES:

- 15 multifunction memory channels, selected with a rotary switch. M1-M13 . . . memorize frequency and offset (±600 kHz or simplex). M14 . . . memorize transmit and receive frequencies independently for nonstandard offset. M0 . . . priority channel, with simplex, ±600 kHz, or nonstandard offset.
- Internal backup for all memories, by installing four AA NiCd batteries (not Kenwood-supplied) in battery holder.
- Priority channel (memory "0") and priority alert.
- Covers 143.900-148.995 MHz, in 5-kHz or 10-kHz steps.
- Built-in autopatch DTMF (Touch-Tone®) encoder.
- Front-panel keyboard for selecting frequency, transmit offset, and autopatch encoder tones, programming memories, and controlling scan.
- Automatic scan of entire band (5-kHz or 10-kHz steps) and memories.
- Manual scan of band and memories, with UP/DOWN microphone (standard).
- Repeater REVERSE switch.
- Selectable power output. 25 W (HI)/5 W (LOW).
- LED S/RF bar meter.
- TONE switch to actuate subaudible tone module (not Kenwood-supplied).

OPTIONAL ACCESSORIES:

- KPS-7 fixed-station power supply.

SP-40

Compact, high-quality mobile speaker

- Matches all HF, VHF, and UHF radios for mobile operation.
- Only 2-11/16 inches wide by 2-1/2 inches high by 2-1/8 inches deep.
- 4-ohm input impedance.
- Handles 3 watts of audio.
- Mounting bracket with ferrite magnet. Adhesive-backed steel plate supplied for mounting virtually anywhere.

TR-8400

"Go synthesized on 440 MHz FM"... 5 memories, memory/band scan

The TR-8400 synthesized 70-cm UHF FM mobile transceiver covers 440-450 MHz in 25-kHz steps and includes five memories, automatic memory and band scan, UP/DOWN manual scan, and two VFOs.

TR-8400 FEATURES:

- Synthesized coverage of 440-450 MHz in 25-kHz steps.
- Five memories and memory backup terminal on rear panel.
- Two VFOs.
- Offset switch for ±5 MHz transmit offset and simplex operation. Fifth memory allows any other offset by memorizing receive and transmit frequencies independently.
- Automatic scan of memories and of 440-450 MHz band (in 25-kHz steps). Locks on busy channel and resumes when signal disappears. HOLD or mic PTT button cancels scan.
- Up/down manual band scan in 25-kHz steps with UP/DOWN microphone supplied with TR-8400.
- Only 5-3/4 inches wide, 2 inches high, and 7-5/8 inches deep. Weighs only 3.75 pounds.
- TONE switch to activate subtone device (not Kenwood-supplied). DTMF (Touch-Tone®) terminal on rear panel.
- Four-digit frequency display and S/RF bar meter. Other LEDs indicate BUSY, ON AIR, and REPEATER operation.
- HI/LOW (10 W/1 W) RF-output power switch.

OPTIONAL ACCESSORIES:

- KPS-7 fixed-station power supply.
- SP-40 compact mobile speaker.

Subject to FCC Approval

TRIO-KENWOOD COMMUNICATIONS INC.
1111 WEST WALNUT / COMPTON, CA 90220

TR-9000

"New 2-meter direction"...compact rig with FM/SSB/CW, scan, five memories

The TR-9000 combines the convenience of FM with long distance SSB and CW. It is extremely compact . . . perfect for mobile operation. Matching accessories are available for optimum fixed-station operation.

TR-9000 FEATURES:

- FM, USB, LSB, and CW.
- Only 6-11/16 inches wide, 2-21/32 inches high, 9-7/32 inches deep.
- Two digital VFOs, with selectable tuning steps of 100 Hz, 5 kHz, and 10 kHz.
- Digital frequency display. Five, four, or three digits, depending on selected tuning step.
- Covers 143.9000-148.9999 MHz.
- Band scan . . . automatic busy stop and free scan.
- SSB/CW search of selectable 9.9-kHz bandwidth segments.
- Five memories . . . four for simplex or ±600 kHz repeater offsets and the fifth for a non-standard offset (memorizes transmit and receive frequency independently).
- UP/DOWN microphone (standard) for manual band scan.
- Noise blanker for SSB and CW.
- RIT (receiver incremental tuning) for SSB and CW.
- RF gain control.
- CW sidetone.
- Selectable RF power outputs . . . 10 W (HI)/1 W (LO).
- Mobile mounting bracket with quick-release levers.
- LED indicators . . . ON AIR, BUSY, and VFO.

OPTIONAL ACCESSORIES:

- PS-20 fixed-station power supply.
- SP-120 fixed-station external speaker.
- BO-9 System Base . . . with power switch, SEND/RECEIVE switch (for CW), memory-backup power supply, and headphone jack.

PS-20 TR-9000 BO-9 SP-120

TR-2400

"Hand-shack"...synthesized, big LCD, scan, 10 memories, DTMF (Touch-Tone®)

CONVENIENT TOP CONTROLS

The TR-2400 has the most convenient operating features desired in a 2-meter FM hand-held transceiver.

TR-2400 FEATURES:

- Large LCD digital readout. Readable in direct sunlight (virtually no current drain) and in the dark (lamp switch). Shows receive and transmit frequencies and memory channel. "Arrow" indicators show "ON AIR," "MR" (memory recall), "BATT" (battery status), and "LAMP" switch on.
- Keyboard selection of 144.000-147.995 MHz in 5-kHz increments. No "5-UP" switch needed.
- UP/DOWN manual scan in 5-kHz steps from 143.900 to 148.495 MHz.
- 10 memories. Retained with battery backup. "M0" memory may be used to shift transmitter to any frequency for nonstandard-split repeaters.
- Built-in autopatch DTMF (Touch-Tone®) encoder, using all 16 keyboard buttons.
- Automatic memory scan.
- Repeater or simplex operation. Transmit frequency shifts ±600 kHz or to "M0" memory frequency.
- Reverse switch. Transposes receive and transmit frequencies.
- Subtone switch (tone encoder not Kenwood-supplied).
- Two lock switches to prevent accidental frequency change and accidental transmission.
- External PTT microphone and earphone connectors.
- Rubberized antenna with BNC connector, NiCd battery pack, AC charger, PTT and mic plugs, handstrap, and earphone included.
- Extended operating time with LCD and overall low-current circuit design. Only draws about 28 mA squelched receive and 500 mA transmit (at 1.5 W RF output).
- High-impact case and zinc die-cast frame.
- Compact and lightweight. Only 2-13/16 inches wide, 7-9/16 inches high, and 1-7/8 inches deep. Weighs only 1.62 pounds (including antenna, battery, and hand strap).

OPTIONAL ACCESSORIES:

- ST-1 Base Stand (provides 1.5-hour-quick, trickle, and floating charges, 4-pin microphone connector, and SO-239 antenna connector).
- BC-5 DC quick charger.
- LH-1 leather case.
- BH-1 belt hook.
- PB-24 extra NiCd battery pack.
- SMC-24 speaker/microphone.

KENWOOD
...pacesetter in amateur radio

R-1000

"Hear there and everywhere"... easy tuning, digital display

The R-1000 is an amazingly easy-to-operate, high-performance, communications receiver, covering 200 kHz to 30 MHz in 30 bands. This PLL synthesized receiver features a digital frequency display and analog dial, plus a quartz digital clock and timer.

R-1000 FEATURES:

- Covers 200 kHz to 30 MHz continuously.
- 30 bands, each 1 MHz wide.
- Five-digit frequency display with 1-kHz resolution and analog dial with precise gear dial mechanism.
- Built-in 12-hour quartz digital clock with timer to turn on radio for scheduled listening or control a recorder through remote terminal.
- Step attenuator to prevent overload.
- Three IF filters for optimum AM, SSB, CW. 12-kHz and 6-kHz (adaptable to 6-kHz and 2.7-kHz) for AM wide and narrow, and 2.7-kHz filter for high-quality SSB (USB and LSB) and CW reception.
- Effective noise blanker.
- Terminal for external tape recorder.
- Tone control.
- Built-in 4-inch speaker.
- Dimmer switch to control intensity of S-meter and other panel lights and digital display.
- Wire antenna terminals for 200 kHz to 2 MHz and 2 MHz to 30 MHz. Coax terminal for 2 MHz to 30 MHz.
- Voltage selector for 100, 120, 220, and 240 VAC. Also adaptable to operate on 13.8 VDC with optional DCK-1 kit.

OPTIONAL ACCESSORIES:

- SP-100 matching external speaker.
- HS-5 and HS-4 headphones.
- DCK-1 modification kit for 12-VDC operation.

SP-100

R-1000

HS-5

HC-10

Digital world clock with two 24-hour displays, quartz time base

The HC-10 digital world clock with dual 24-hour display shows local time and the time in 10 preprogrammed plus two programmable time zones.

HC-10 FEATURES:

- Two 24-hour displays with quartz time base. Right display shows local (or UTC) hour, minute, second, day. Left display shows month, date, world time in various cities, memory time (QSO starting time), and time difference (in hours from UTC).
- Preprogrammed time in 10 cities around the world, plus two programmable time zones.
- "TOMORROW" and "YESTERDAY" indicators.
- Memorization of present time. Can be recalled later, for logging purposes.
- High accuracy (±10 seconds/month).

DM-81

Dip meter performs many RF measurements

The DM-81 dip meter is highly accurate and features, in addition to the traditional inductive-coupling technique, capacitive coupling for measuring metal-enclosed coils and toroidal coils.

DM-81 FEATURES:

- Measuring range of 700 kHz-250 MHz in seven bands.
- Built-in storage compartment for all seven coils, capacitive probe, earphone, and ground clip lead.
- All solid-state and built-in battery.
- HC-25U and FT-243 sockets for checking crystals and marker-generator function.
- Amplitude modulation.
- FET for good sensitivity.
- Absorption frequency meter function.
- Earphone for monitoring transmitted signals.
- Capacitance probe for measuring resonant frequencies without removing coil shields, and also for measuring resonant frequencies of toroidal coils.

TRIO-KENWOOD COMMUNICATIONS INC.
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TL-922-A

Maximum legal power on 160-15 meters

The TL-922A linear amplifier provides maximum legal power on the 160-15 meter Amateur bands.

TL-922A FEATURES:

- 2000 W PEP (SSB)/1000 W DC (CW, RTTY) input power on 160, 80, 40, 20, and 15 meters, with 80 W drive.
- Excellent IMD characteristics.
- Pair of EIMAC 3-500Z high-performance transmitting tubes.
- Safety protection.
- Blower with automatic turnoff-delay circuit.
- Variable threshold level type ALC.
- Two meters, one indicating plate current, and the other indicating grid current, relative RF output, and high voltage.

SM-220

High-performance oscilloscope for various monitoring functions

The SM-220 Station Monitor provides a variety of waveform-observing capabilities, and an optional pan display.

SM-220 FEATURES:

- Monitors transmitted SSB and CW waveforms from 1.8 to 150 MHz.
- Monitors signal waveforms in receiver's IF stage.
- Functions as high-sensitivity, wide-frequency-range (up to 10 MHz) oscilloscope.
- Tests linearity of linear amplifiers (provides trapezoid pattern).
- Allows observation of RTTY tuning points (cross pattern).
- Built-in two-tone (1000-Hz and 1575-Hz) generator.
- Expandable to pan-display capability for observing the number and amplitude of stations within a switchable ±20 kHz/±100 kHz bandwidth.

OPTIONAL ACCESSORIES:

- BS-8 pan-display module for TS-180S, TS-830S, and TS-820 Series.
- BS-5 pan-display module for TS-520 Series.

SP-70 TS-600 W/VOX-3

TS-600

All-mode, all solid-state 6-meter transceiver

The TS-600 is a 6-meter, all-mode, all solid-state transceiver with VFO (and crystal-controlled) coverage of the entire band.

TS-600 FEATURES:

- SSB (20 W PEP input), FM and CW (10 W output), and AM (5 W output).
- Operates on 120/220 VAC, 50/60 Hz or 13.8 VDC.
- VFO coverage of 50-54 MHz in four bands, with two-speed dial mechanism. Favorite frequencies may be crystal-controlled.
- Effective noise blanker.
- VOX operation with VOX-3 accessory (standard).

TS-700SP 2-meter, all-mode, all solid-state transceiver is also available . . . with similar features, plus:

- Digital frequency display, with 100-Hz resolution.
- VFO coverage of 144-148 MHz in four bands.
- Simplex and repeater operation, including all repeater subbands. REVERSE switch.

OPTIONAL ACCESSORIES:

- VFO-700S remote VFO (for TS-700S/SP).
- SP-70 external speaker.

ACCESSORIES

A wide selection of optional accessories is offered for optimum operating flexibility. In addition to the optional items listed with each piece of equipment described in this catalog, the following accessories are also available:

PC-1 phone patch with hybrid circuit and VU meter for null and audio gain measurements.

MC-45 Touch-Tone® (with automatic transmit) microphone.

MC-50 dynamic dual-impedance (50 kΩ/500Ω) desk microphone.

MC-30S (500Ω) and **MC-35S** (50 kΩ) dynamic noise-canceling hand microphones.

HS-5 deluxe 8Ω headphone set.

HS-4 8Ω headphone set.

NOTE: Prices and specifications of all Trio-Kenwood products are subject to change without prior notice or obligation.

Look for the Kenwood banner.

Only the best dealers are Authorized Kenwood Dealers. If your dealer displays a Kenwood Authorized Dealer banner and plaque in his store, you will know he can provide you with the service you demand . . . of the same quality as factory service. Authorized Kenwood Dealers employ factory-trained service technicians, maintain an extensive inventory of spare parts, and have direct access to factory service information. When you deal with an Authorized Kenwood Dealer, you deal with an expert on the entire line of Kenwood Amateur Radio equipment.

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Phoenix, AZ 85015
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Ham Radio Outlet
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Van Nuys, CA 91401
(213) 988-2212

Ham Radio Outlet
2620 West La Palma
Anaheim, CA 92801
(213) 860-2040

Ham Radio Outlet
5375 Kearny Villa Road
San Diego, CA 92123
(714) 560-4900

Henry Radio, Inc.
11240 W. Olympic Blvd.
Los Angeles, CA 90064
(213) 477-6701

Henry Radio, Inc.
931 North Euclid
Anahelm, CA 92801
(213) 430-7997

Webster Radio
2602 East Ashlan
Fresno, CA 93726
(209) 224-5111

COLORADO

CW Electronics
800 Lincoln Street
Denver, CO 80202
(303) 893-5525

FLORIDA

Amateur Electronic Supply
621 Commonwealth
Orlando, FL 32803
(305) 894-3238

Amateur Radio Center
2805 N.E. Second Avenue
Miami, FL 33137
(305) 573-8383

HAWAII

Honolulu Electronics
819 Keeaumoku Street
Honolulu, HI 96814
(808) 949-5564

IDAHO

Ross Distributing
78 South State Street
Preston, ID 83263
(208) 852-0830

ILLINOIS

Erickson Communications
5456 N. Milwaukee Ave.
Chicago, IL 60630
(312) 631-5181

Klaus Radio, Inc.
8400 N. Pioneer Pkwy.
Peoria, IL 61614
(309) 691-4840

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Indianapolis, IN 46240
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Fort Wayne, IN 46815
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IOWA

HI, Incorporated
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Council Bluffs, IA 51502
1601 Avenue "D"
Council Bluffs, IA 51501
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KANSAS

Associated Radio Comm.
P.O. Box 4327
8012 Conser
Overland Park, KS 66204
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MARYLAND

Electronic Int'l Service
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Wheaton, MD 20902
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Lincoln, NB 68508
(402) 466-3733

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Electronic Module
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Hobbs, NM 88240
(505) 397-3022

NEW YORK

Adirondack Radio Supply
P.O. Box 88
185-191 West Main Street
Amsterdam, NY 12010
(518) 842-8350

Harrison Radio Corporation
20 Smith Street
Farmingdale,
Long Island, NY 11735
(516) 293-7990

Radio World*
Oneida County Airport
Terminal Building
Oriskany, NY 13424
(315) 337-0203

OHIO

Amateur Electronic Supply
28940 Euclid Avenue
Wickliffe, OH 44092
(216) 585-7388

Srepco Electronics
314 Leo Street
Dayton, Ohio 45404
(513) 224-0871

Universal Amateur Radio, Inc.
1280 Aida Drive
Reynoldsburg, OH 43068
(614) 866-4267

OKLAHOMA

Derrick Electronics
P.O. Box 457
714 West Kenosha
Broken Arrow, OK 74012
(918) 251-9923

Radio, Inc.
1000 South Main
Tulsa, OK 74119
(918) 587-9123

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G.I.S.M.O. Communications
2305 Cherry Road
Rock Hill , SC 29730
(803) 366-7157

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208 East Kemp Avenue
Watertown, SD 57201
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Amateur Radio Supply of Nashville
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Madison, TN 37115
(615) 868-4956

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1465 Wells Station Road
Memphis, TN 38108
(901) 683-9125

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Corpus Christi, TX 78404
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(713) 658-0268

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San Antonio, TX 78222
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Seattle, WA 98155
(206) 364-8300

Amateur Radio Supply Co.
6213 13th Avenue South
Seattle, WA 98108
(206) 767-3222

WISCONSIN

Amateur Electronic Supply
4828 W. Fond Du Lac Ave.
Milwaukee, WI 53216
(414) 442-4200

As of September 16, 1980, only the above are fully Authorized Trio-Kenwood Communications, Inc. dealers.

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TRIO-KENWOOD COMMUNICATIONS INC.
1111 WEST WALNUT / COMPTON, CA 90220

*Interim dealer.

LEAKY LINES

Dave Mann K2AGZ
3 Daniel Lane
Kinnelon NJ 07405

I've had a hankering for a long time to write about flea markets. And now that the season is over for this year, here in the north, anyway, I thought that I might make some observations. Like most guys who are somewhat quick on the trigger (I'm sometimes known as the quickest mike button in the east), I was going to shoot from the hip, quite convinced that I had a valid point of view. But after some discussions with several friends, I made a 180° turn. I must confess that I had not delved very deeply below the surface, and my ideas had been all wet.

The most important thing about flea markets is that if they weren't included, none of our ham conclaves could begin to draw the huge attendance they do. In fact, many convention symposiums and caucuses are relatively poorly attended, but flea markets are generally so crowded that you invariably have to elbow your way to get through the aisles. Flea markets are unquestionably the most popular attractions of all. Why should this be so?

Because the idea of something for nothing (or relatively nothing) is one of the most powerful motivations in all Creation. That's why there was a huge crowd when they first opened the Oklahoma Territory, why hordes of people flocked to Sutter's Mill and the Klondike when someone struck gold, and why department stores are thronged on Washington's Birthday. The prospect of a big bargain is almost irresistible.

Some flea markets are good, and some are not so good. It all depends upon just how well the individual makes out in his or her buying and selling. If you are on the prowl for a certain item and you happen to find it at a good price, then you are apt to conclude that it's a good flea market. But if you load a couple of tons of stuff into your pickup truck and lug it three or four hundred miles, then don't succeed in selling any of it, you might well be justified in thinking it's a lousy one. It all depends on your individual frame of reference... like anything else.

Flea markets generally depend upon word of mouth for success. If a given flea market turns out to be fruitful for a large number of people, you can bet that it will be even better attended next year. For there are enormous multitudes who look forward to these things, and they think nothing of traveling hundreds, if not thousands, of miles to attend. They go with bulging pockets, looking for good buys. Sometimes they find them. But frequently, they wind up buying stuff they never anticipated buying, and it is merely deposited on a shelf in the basement for future use and is rarely ever heard of any more.

I suppose that I have scores of HF connectors that I wouldn't be able to use if I lived to be a hundred. And God alone knows how many linear feet of shrink tubing and spaghetti, how much stranded #14 copperweld, how many meters, relays, tube sockets, rf chokes, capacitors, resistors, packets of electronic hardware, rubber grommets, nibblers, wire strippers, phone plugs and jacks, test leads, antenna traps, baluns, and other assorted "junk" I have squirreled away in my cellar! Why, I must have ten cigar boxes full of porcelain egg insulators alone!

Almost all of that stuff was bought at flea markets, and I will probably buy a lot more of it in ensuing years.

Tell me something if you can: What makes an otherwise intelligent guy go into the pot for over a dozen lapel badges? I have so many of the danged things that I can never make up my mind which one to wear. But I'll bet that the very next flea market I attend, if one of those birds is there grinding out call-sign badges, I'll buy another! I'll see one in a color I don't have or with a couple of flickering LEDs, and there'll go another couple of bucks!

Of course, the worst part is that after you bring this stuff home, you put it in a special place so that you'll be able to lay your hands on it when you have to use it, and then you can't remember where you put it. I'm still looking for a whole box full of zeners that I stashed away for safekeeping about four years ago. I've turned the place upside down and I just can't find them.

Flea markets are viewed by some people as a golden opportunity to unload what can only be described as useless junk. They don't represent it as such, of course; that would be cutting off their nose to spite their face. I wish I had a ten spot in my pocket right this minute for every piece of equipment someone intends to take to a flea market to sell, even though he is quite aware that there is something drastically wrong with it. But this fact will be concealed so that he can "sandbag" some willing sucker. Burned-out transformers, shorted components, kits assembled with wiring errors and cold solder joints, you name it. It's par for the course.

That's why everyone who goes to a flea market ought to remember to bear the old warning *caveat emptor* constantly in mind. Some sponsoring groups have had so many complaints that they have taken to displaying a large sign: "The XYZ Amateur Radio Club makes no warranties in respect to the condition of items bought or sold. All transactions are subject to the discretion of buyers, and the club is neither directly nor indirectly responsible."

But I have another thought, and I'm not at all sure I'm incorrect about it. The good Lord must have made gullible pigeons for some purpose or another, and if they are dumb enough to allow themselves to be taken, it is probably what they deserve.

The reason this postulate doesn't disturb me is that many years of observance and experience have taught me that chiselers cannot cheat anyone who is not himself looking for an opportunity to chisel. Those who believe in dealing honestly are much harder to cheat than those who wouldn't hesitate to pull something a bit shady themselves. If you tend to doubt this, just take a look at the video tapes brought to light in the Abscam mess. Who fell for the sting operation that was set up by the FBI? You don't suppose for a moment that any scrupulously honest senator or congressman would have allowed himself to be enticed into a meeting in some seedy motel room with an Arab oil sheik, do you?

So, by all means, attend flea markets. Buy and sell to your heart's content. And if it should happen that you get stung, well, there's always another one where you might find the buy of a lifetime. I once bought a Collins 32V-2 and had the strange sensation that I was being watched. I opened the rig up and there in the rf cage I found an electrocuted field mouse... his beady little black eyes were open, staring right into mine!

You never can tell what sort of a bonanza you might run into!

RTTY LOOP

from page 18

33 should go up fairly easily, with just about any modern demodulator. I would check the ads here in *73* for something that appeals to you. Anyone who has a 32 on the air might drop George a note at 32-D Martha Drive, Rockland, Massachusetts 02370.

And now, a bit of a tease. I am currently evaluating one of the "new breed" RTTY units. This thing will speak Baudot, ASCII, and Morse at any reasonable speed, convert codes, and store data on tape. Its microcomputer brain is user accessible, so new functions can be devised. One of the cutest is sending SSTV signals with no other equipment! Want a hint? It is made by a company here in the Free State, and it is advertised in *73*. Watch for the full review, as always with both the good and the bad, in next month's RTTY Loop.

OSCAR ORBITS

Courtesy of AMSAT

The OSCAR satellites are subject to atmospheric drag, of course, and the present period of intense solar activity has accentuated the problem. During this period, our sun has been expelling huge numbers of charged particles, some of which find their way into the Earth's upper atmosphere, increasing the density (and thus the drag) there. It is through this region that the OSCARs must pass. OSCAR 8, in a lower orbit than OSCAR 7, is the more seriously affected of the two.

If the drag factor is not considered when OSCAR calculations are performed, long-range orbital projections will be in error. For example, by the end of 1979, OSCAR 8 was more than 20 minutes ahead of some published schedules. The nature of orbital mechanics is such that extra drag on a satellite causes it to move into a lower orbit, resulting in a shorter orbital period. Thus, the satellite arrives above a given Earthbound location earlier than predicted.

Using data supplied to us by Dr. Thomas A. Clark W3IWI of AMSAT, the equatorial crossing tables shown here were generated with the aid of a TRS-80™ microcomputer. The tables take into account the effects of atmospheric drag and should be in error by a few seconds at most.

The listed data tells you the time and place that OSCAR 7 and OSCAR 8 cross the equator in an ascending orbit for the first time each day. To calculate successive OSCAR 7 orbits, make a list of the first orbit number and the next twelve orbits for that day. List the time of the first orbit. Each successive orbit is 115 minutes later (two hours less five minutes). The chart gives the longitude of the day's first ascending (northbound) equatorial crossing. Add 29° for each succeeding orbit. When OSCAR is ascending on the other side of the world from you, it will descend over you. To find the equatorial descending longitude, subtract 166° from the ascending longitude. To find the time OSCAR 7 passes the North Pole, add 29 minutes to the time it passes the equator. You should be able to hear OSCAR 7 when it is within 45 degrees of you. The easiest way to determine if OSCAR is above the horizon (and thus within range) at your location is to take a globe and draw a circle with a radius of 2450 miles (4000 kilometers) from your QTH. If OSCAR passes above that circle, you should be able to hear it. If it passes right overhead, you should hear it for about 24 minutes total. OSCAR 7 will pass an imaginary line drawn from San Francisco to Norfolk about 12 minutes after passing the equator. Add about a minute for each 200 miles that you live north of this line. If OSCAR passes 15° east or west of you, add another minute; at 30°, three minutes; at 45°, ten minutes. Mode A: 145.85-.95 MHz uplink, 29.4-29.5 MHz downlink, beacon at 29.502 MHz. Mode B: 432.125-.175 MHz uplink, 145.975-.925 MHz downlink, beacon at 145.972 MHz.

At press time, OSCAR 7 was scheduled to be in Mode A on odd numbered days of the year and in Mode B on even numbered days. Monday is QRP day on OSCAR 7, while Wednesdays are set aside for experiments and are not available for use.

OSCAR 8 calculations are similar to those for OSCAR 7, with some important exceptions. Instead of making 13 orbits each day, OSCAR 8 makes 14 orbits during each 24-hour period. The orbital period of OSCAR 8 is therefore somewhat shorter: 103 minutes.

To calculate successive OSCAR 8 orbits, make a list of the first orbit number (from the OSCAR 8 chart) and the next thirteen orbits for that day. List the time of the first orbit. Each successive orbit is then 103 minutes later. The chart gives the longitude of the day's first ascending equatorial crossing. Add 26° for each succeeding orbit. To find the time OSCAR 8 passes the North Pole, add 26 minutes to the time it crosses the equator. OSCAR 8 will cross the imaginary San Francisco-to-Norfolk line about 11 minutes after crossing the equator. Mode A: 145.85-.95 MHz uplink, 29.4-29.50 MHz downlink, beacon at 29.40 MHz. Mode J: 145.90-146.00 MHz uplink, 435.20-435.10 MHz downlink, beacon on 435.090 MHz.

OSCAR 8 is in Mode A on Mondays and Thursdays, Mode J on Saturdays and Sundays, and both modes simultaneously on Tuesdays and Fridays. As with OSCAR 7, Wednesdays are reserved for experiments.

OSCAR 7 ORBITAL INFORMATION FOR JANUARY

ORBIT #	DATE	TIME (GMT)	EQ. CROSSING (DEGREES WEST)
28042	1	0131:05	98.7
28054	2	0030:23	83.5
28067	3	0124:37	97.1
28079	4	0023:55	82.0
28092	5	0118:09	95.6
28104	6	0017:27	80.4
28117	7	0111:41	94.0
28129	8	0010:59	78.8
28142	9	0105:14	92.4
28154	10	0004:31	77.3
28167	11	0058:46	90.9
28180	12	0153:00	104.4
28192	13	0052:18	89.3
28205	14	0146:32	102.9
28217	15	0045:50	87.7
28230	16	0140:04	101.3
28242	17	0039:22	86.2
28255	18	0133:36	99.8
28267	19	0032:54	84.6
28280	20	0127:09	98.2
28292	21	0026:26	83.0
28305	22	0120:41	96.6
28317	23	0019:58	81.5
28330	24	0114:13	95.1
28342	25	0013:30	79.9
28355	26	0107:45	93.5
28367	27	0007:03	78.3
28380	28	0101:17	91.9
28392	29	0000:35	76.8
28405	30	0054:49	90.4
28418	31	0149:03	103.9

OSCAR 8 ORBITAL INFORMATION FOR JANUARY

ORBIT #	DATE	TIME (GMT)	EQ. CROSSING (DEGREES WEST)
14402	1	0057:44	71.6
14416	2	0102:29	72.8
14430	3	0107:13	74.0
14444	4	0111:58	75.3
14458	5	0116:43	76.5
14472	6	0121:27	77.7
14486	7	0126:12	78.9
14500	8	0130:56	80.1
14514	9	0135:40	81.3
14528	10	0140:25	82.5
14541	11	0001:57	57.9
14555	12	0006:42	59.2
14569	13	0011:26	60.4
14583	14	0016:10	61.6
14597	15	0020:54	62.8
14611	16	0025:38	64.0
14625	17	0030:23	65.2
14639	18	0035:07	66.4
14653	19	0039:51	67.6
14667	20	0044:35	68.9
14681	21	0049:19	70.1
14695	22	0054:03	71.3
14709	23	0058:46	72.5
14723	24	0103:30	73.7
14737	25	0108:14	74.9
14751	26	0112:58	76.1
14765	27	0117:42	77.3
14779	28	0122:25	78.5
14793	29	0127:09	79.8
14807	30	0131:53	81.0
14821	31	0136:36	82.2

OSCAR 7 ORBITAL INFORMATION FOR FEBRUARY

ORBIT #	DATE	TIME (GMT)	EQ. CROSSING (DEGREES WEST)
28430	1	0048:21	88.8
28443	2	0142:35	102.4
28455	3	0041:53	87.2
28468	4	0136:07	100.8
28480	5	0035:25	85.7
28493	6	0129:39	99.3
28505	7	0028:57	84.1
28518	8	0123:11	97.7
28530	9	0022:29	82.5
28543	10	0116:43	96.1
28555	11	0016:01	81.0
28568	12	0110:15	94.6
28580	13	0009:32	79.4
28593	14	0103:47	93.0
28605	15	0003:04	77.8
28618	16	0057:19	91.4
28631	17	0151:33	105.0
28643	18	0050:50	89.9
28656	19	0145:05	103.4
28668	20	0044:22	88.3
28681	21	0138:37	101.9
28693	22	0037:54	86.7
28706	23	0132:08	100.3
28718	24	0031:26	85.2
28731	25	0125:40	98.8
28743	26	0024:58	83.6
28756	27	0119:12	97.2
28768	28	0018:30	82.0

OSCAR 8 ORBITAL INFORMATION FOR FEBRUARY

ORBIT #	DATE	TIME (GMT)	EQ. CROSSING (DEGREES WEST)
14835	1	0141:20	83.4
14848	2	0002:52	58.8
14862	3	0007:35	60.0
14876	4	0012:19	61.2
14890	5	0017:02	62.4
14904	6	0021:45	63.6
14918	7	0026:29	64.8
14932	8	0031:12	66.1
14946	9	0035:55	67.3
14960	10	0040:39	68.5
14974	11	0045:22	69.7
14988	12	0050:05	70.9
15002	13	0054:48	72.1
15016	14	0059:31	73.3
15030	15	0104:14	74.5
15044	16	0108:57	75.7
15058	17	0113:40	76.9
15072	18	0118:23	78.1
15086	19	0123:06	79.3
15100	20	0127:49	80.6
15114	21	0132:32	81.8
15128	22	0137:15	83.0
15142	23	0141:57	84.2
15155	24	0003:29	59.6
15169	25	0008:11	60.8
15183	26	0012:54	62.0
15197	27	0017:36	63.2
15211	28	0022:19	64.4

✓Reader Service—see page 194

NEW PRODUCTS

HEATH CONTINUING EDUCATION OFFERS NEW ADVANCED ELECTRONICS PROGRAMS

Heath Continuing Education, a division of Heath Company, has introduced a series of three new learn-at-home electronics programs. Each program covers an advanced electronic subject.

All three programs use programmed self-instruction textbooks that present the subject matter in easy, "bite-sized" segments. They come complete with electronic parts for optional hands-on experiments.

Operational Amplifiers, EE-101, covers the fundamentals of this commonly-used integrated circuit family, including the popular Norton and BiFET designs. The Active Filters program, EE-102, covers the design, operation, and uses of active filters. It describes low-pass, high-pass, bandpass, and state-variable filters, as well as others. The Phase-Locked Loops program, EE-104, discusses the uses, designs, and operation of PLLs. Phase-locked loops are widely used in television receivers, FM receivers, CB and 2-meter transceivers, industrial telemetry circuits, and motor controls.

For further information, contact *Heath Continuing Education, Dept. 350-160, Benton Harbor MI 49022.* Reader Service number 483.

BENJAMIN MICHAEL INDUSTRIES' MODEL 173A STATION CLOCK

Benjamin Michael Industries has annnounced the introduction of the Model 173A station clock. The 173A provides the proper 24-hour military time format used by serious communications operators when logging transmissions or verifying contacts and reports. The unit allows the operator to directly read GMT and avoid the confusion created by various local time zones.

The 173A features quartz-crystal accuracy and greater than one year operation from a single penlight battery. Battery operation eliminates the need to reset the clock after power line failures and makes the unit ideal for mobile, field, and emergency power operations.

Time setting is accomplished by the use of two push-buttons and a hold switch which stops the clock operation and resets the internal seconds counter to zero for precise setting to WWV or other time standards. The unit is housed in an attractive aircraft instrument style case.

Benjamin Michael Industries' Model 173A station clock.

For further information, contact *Benjamin Michael Industries, PO Box 173, Prospect Hts. IL 60070.* Reader Service number 480.

KANTRONICS' VARIFILTER™

You can vary the frequency and the bandwidth of the Varifilter™, a new addition to Kantronics' line of products. The Varifilter can be set to maximize one signal (peaking) or to minimize an interfering signal (notching), and it works with CW (Morse), single-sideband, and AM signals. The Varifilter circuitry is designed to provide optimum results without ringing, oscillating, or instability.

The bandwidth is variable from less than 30 Hz to over 1000 Hz. The frequency range runs from less than 150 Hz to over 3000. Once it has been set, the bandwidth will remain constant regardless of changes in the frequency range setting. This feature has not been readily available in variable filters until now.

The Varifilter has its own internal power supply which is switchable from 115 V ac to 230 V ac. It is able to run from 12 to 18 V dc as well. Each unit has a tuning eye that lets the operator see when he has filtered the signal he wants to.

For further information, contact *Kantronics, Inc., 1202 E. 23rd Street, Lawrence KS 66044.*

NEW IC DISPENSERS

OK Machine and Tool Corpor-

Heath's Phase-Locked Loops program.

Kantronics' Varifilter™.

ation has introduced its new MDD series of DIP IC dispensers for MOS and CMOS as well as standard devices. The dispensers offer flexibility and convenience to such a unique degree that they are patented. Each channel easily accepts any standard IC shipping tube and can accommodate any standard IC from 2 to 64 pins on .300, .400, or .600 centers.

Adjustable guides position each IC individually for easy extraction, and simple gravity feed ensures reliable deposit of next IC into extraction position after previous IC is removed. Ruggedly made of unique conductive carbon-filled thermoplastic with steel supports, the MDD design ensures effective static dissipation (a grounding lug is included) as well as long and reliable performance. Available in 1-, 5-, and 10-channel versions, the dispensers will greatly facilitate any IC handling or PCB assembly process.

For further information, contact *OK Machine and Tool Corporation, 3455 Conner Street, Bronx NY 10475; (212)-994-6600.* Reader Service number 482.

WRAASE SC-422 SSTV SCAN CONVERTER

The SC-422 is a complete slow-to-fast and fast-to-slow scan converter. It has two full-size SSTV picture memories which can be used either independently to store two different pictures or together for improved picture definition of 256 pixels per line. Received pictures can also be stored in the two memories.

On transmission, a cursor is automatically inserted into the screen, indicating the portion of the SSTV picture being transmitted. The SC-422 allows you to display the fast scan content of the memory, for easy adjustment of the camera. SSTV picture transmission is not interrupted during adjustment of the camera and controls. A built-in SSTV output filter ensures a distortion-free sine wave output.

In the receive mode, a grey scale is inserted at the top of the picture to aid in the adjustment of brightness and contrast controls. An automatic "hold" circuit keeps the most recently received picture in memory when the SSTV input signal stops.

Continued on page 156

✓ *Reader Service—see page 194*

REVIEW

S-F MOD KITS

S-F Radio Amateur Services of Culver City, California, distributes a series of modification kits for the very popular Kenwood TS-820, and makes some pretty impressive improvement claims for them. Both the receiver and transmitter sections are addressed.

The four kits are a front end improvement, a balanced mixer improvement, a "high-power" (QRO) kit, and an rf compressor-to-clipper conversion.

Actually, the compressor-to-clipper modification is not W6TOG's work. It is produced by Magicom of Bellevue, Washington, and is included here with the others because all are related and all are available through S-F.

These kits are not inexpensive, ranging in price from $27.50 to $37.50. The total tab for all four is well over $100. Are they worth it? Can the average ham install them? Without reducing the value of the transceiver? Maybe. . . read on.

The Front-End Modification

The advertising brochure claims rather remarkable improvements in sensitivity, noise figure, and immunity to rf overload. The kit, consisting of two diodes and two transistors, retails for $34.50. The installation instructions are something less than Heathkit® quality, but with a bit of study, they are both adequate and accurate. A disclaimer in large print warns against installation by persons unfamiliar with solid-state circuitry. True, this is probably not a good first project for the beginner, but with ordinary skill and care, installation is not difficult. After all, how hard can it be to remove and install two transistors and two diodes?

Before installation, however, let's do a simple test. With the antenna input terminated to a 50-Ohm load, increase the af gain and check the noise level at the speaker. It is *loud*! With headphones, you probably won't get beyond 12 o'clock without discomfort. All of this racket is internal noise. Make a mental note of the level.

Probably the most difficult part of the installation is finding the transistors to be removed from the foil side of the rf board. The full-size photo in the TS-820 service manual was invaluable. Such a photo would be a useful addition to the installation instructions for the benefit of those who don't have the service manual. Once you find the right pads, removal and reinstallation takes only a few minutes.

The receiver realignment requires no external instruments and goes quickly once you find the right slugs to turn. Again, a photo or sketch with the instructions would be most helpful. Perhaps I'm being too fussy, but I really believe that a few photos or other pictorials might have cut installation time in half.

Does it work? Connect your 50-Ohm load to the antenna terminal, crank up the af gain, and listen to the internal noise again. Listen carefully, because there's not much noise left to hear. As for sensitivity, an improvement from 0.25 microvolts to 0.09 microvolts is claimed. I don't have the instrumentation to measure it, but there is an improvement. The original TS-820 used to run neck and neck with my SB-303 on weak-signal performance. Now, especially on 10 meters, the TS-820 hears signals that just aren't there on the SB-303.

The Balanced Mixer Mods

I was so pleased with the results of the front-end improvements that I decided to go ahead with the balanced mixer mods. This kit retails for $27.50 and consists of two more transistors and several resistors. A substantial improvement in immunity from rf overload is claimed to result. This is particularly important to me, since I live within 500 feet of another ham who runs full legal power, and I've become accustomed to the distinctive sound of my S-meter needle pounding the pin on top of the scale. We simply can't operate simultaneously on the same band.

For practical purposes, installation is just about the same as the front-end kit. The actual parts replacement takes less time than locating the parts to be removed, and, once again, a picture would be most helpful. If I had to do the job again, I surely would install both kits at once, since the rf board would have to be removed only once, and ditto the receiver realignment.

This time when you listen for internal noise, listen very, very carefully. In my installation, there is virtually none. It was so quiet I was almost afraid the radio wasn't working. On the air, weak signals just seem to pop out of an almost silent background. More recently, this advantage has been lost to a noisy power line, but certainly not through any fault of the balanced mixer mods.

I wish the rf-overload problem had gone the same route as the internal noise, but not quite so. However, the situation is very much improved. I now can hear a relatively weak signal 10-15 kHz from the local ham's transmit frequency, and this is at least as much as I expected. We still can't operate the same band at the same time, but that's because I still do the same number on his receiver that he used to do on mine.

The QRO Kit

This kit retails for $37.50, and consists of two 6293 tubes and several small components. The 6293 is a ruggedized version of the 6146 and is a direct pin-for-pin replacement. This modification consists of two separate operations. One involves raising the screen voltage, and the other changes the ALC time constant for better action.

The first part of the modification couldn't be easier. Move a wire, install two resistors, and replace the finals. A note of caution here—neutralize the new finals quickly! I turned on the radio to warm up and went to look for a non-metallic tool to make the adjustment. The new finals were so far out of neutralization that I returned just in time to see the fuse blow from all the plate current being drawn from self-oscillation. This may be an isolated case, but be careful anyway. The finals went downhill with the fuse and I thought I might have an expensive problem, but the folks at S-F solved that one by replacing the tubes at no charge. They are good people to do business with.

The ALC modifications involve finding and replacing a resistor, a diode, and a capacitor on the rf board. These components are located in a less dense section of the board than the front end and balanced mixer. Thus, the job is relatively easier, even without pictures. This is another task that could easily be worked in with the front-end and balanced mixer mods, so that only one removal of the rf board would be required.

As it came from the factory, my TS-820 delivered 100 Watts output on 160 and 80 meters, 100 Watts on 40 through 15 meters, and less than 80 Watts on 10 meters. With the QRO mod, output was increased at least 25 Watts on all bands and nearly 35 Watts on 10 meters. Still more power is available by using 220 volts ac rather than 110. This brought output to 170 Watts on 160 and 80 meters, 150 Watts on 40 through 15, and an honest 140 Watts on 10 meters. Simply changing to 220 volts ac probably would have made a noticeable improvement even without the QRO kit. Also noticeable is the much faster ALC recovery.

The Magicom

This unit is a preassembled circuit board about two inches square, which sells for $27.50. It converts the stock rf compressor to an rf clipper. While I have no reason to believe there is any connection, there is a striking similarity to the Magnum Six available a few years ago.

The Magicom board installs on the i-f board in a relatively open area near the crystal filter(s). If you have additional crystal filters installed, or have plans to do so, you may wish to consider relocating either the filters or the Magicom. Installation consists of removing two capacitors and connecting four leads from the Magicom.

The instructions warn that careful workmanship and sufficient study of the work are required. This is good advice. Parts density on the i-f board is high, and great care certainly is required. In this case, an exploded view of the foil side of the board is provided with the instructions and is worth its weight in gold. When the appropriate pads are found, installation is a snap.

Once installed, the Magicom lives up to its claims, but first a few words about my goals and expectations with respect to speech processing. I am not an

audio purist. I am a DXer. It's not nearly as important to me that the DX station enjoys the sound of my voice as it is that he can understand my call letters through a pileup. I'm perfectly willing to sacrifice tonal fidelity for penetrating intelligibility.

As it turns out, I sacrificed nothing with the Magicom. The same audiophiles who complained that my audio sounded "harsh" and "overprocessed" now report that it sounds much better. At the same time, the DXers who reported "weak" or "muffled" audio now find it to be far more penetrating.

So, is the whole thing worth it? If all your time on the air is spent rag chewing with solid-copy stations, it certainly is not. The stock TS-820 (and many other radios) will do the job very nicely without the extra expense and work. Strictly in terms of dollars per components, the price is steep. If you could identify all the components, you surely could buy them for a lot less. But remember, you're buying more than components. You're paying for many hours of someone's research and experimentation. For me, it's worth every penny.

Can the average ham install it? I think so. My technical skills are well on the low side of average. To provide a reference point, there's a local joke about the W4LVM School of (backward) Diode Installation. On the other hand, if you have difficulty recognizing a diode, maybe you should forget about it.

One distinct advantage is the absence of external signs of modification. There are no holes, nothing outboard, nothing to detract from resale value. In fact, the whole operation is easily reversible should you wish to do so. I don't ever plan to reverse it. In fact, if S-F should offer additional mods, I'll probably be one of the first in line.

For further information, contact *S-F Amateur Radio Services, 4384 Keystone Ave., Culver City CA 90230.* Reader Service number 477.

Wayne Mueller W4LVM
Roswell GA

AED SCANNERS

You have undoubtedly heard of Murphy's Law. OK, but have you heard of Orozco's postulate? I thought not! Well, simply stated, it says that the degree of dissatisfaction with one's own

rig is directly proportional to the number of visits to the local candy store. As we watch the microprocessor come of age, we realize that if a particular rig exists, then it is obsolete! Only what is on the drawing boards is state of the art. If your transceiver doesn't have two vfos, six memories, three scanning modes, and the ability to poach your morning eggs, then it just isn't up to date!

Sad, but true. You drive home, looking at your once-current mobile rig, noticing its plain face and lack of dials and lights... how could this happen so fast! You say it will only transmit and receive? How quaint...

Enter AED Electronics and their line of scanners. Don't send old Dobbin to the glue factory just yet... I purchased one of these scanner boards from a local dealer and headed home with great expectations. No creeping obsolescence for me!

Installation

On closer inspection, the board itself is not at all complicated and probably does not warrant the extra expenditure to purchase it fully assembled. Beyond that, all installation and operation instructions are both complete and easy to read. The circuit board is tailored to fit in your particular radio with no modification whatsoever. A few wiring connections to the rotary frequency-control switch and to the PLL section were all that were required. I had only to decide for myself where to put the two toggle switches that control the scanning functions. There was even a provision for older transceivers that had only the two-position power switch. About an hour later, my Midland 13-513 was ready for the time-honored smoke test. Lo and behold... no cold solders or miswired leads!

Operation

The scanner for the Midland 220 rig is very easy to operate and does its job very well indeed. There are two switches that control the operation of the microprocessor chip. The first switch either leaves the rig operating normally or puts it in the scan mode. The second one allows it to scan the MHz section selected or will stop it on the current frequency to transmit or receive. That's all there is to it. While scanning the section of the band selected, it will stop for about eight seconds on any frequency that will break the squelch, giving you time to lock it there if you wish. If you don't, it will continue its scan *ad infinitum*. On my unit, the return time to a particular frequency, barring any interruption, is about 16 seconds more than sufficient to catch the action. As warned in the instructions, you must set the frequency to zero-zero (i.e., 224.00) to have it scan normally. Yes, I tried it with a random frequency in the window, and yes, it scans... but quite erratically. So much for experimentation!

Conclusions

I feel that this unit is a particularly valuable addition to the Midland 13-513, due to the fact that fully-synthesized 220 rigs are hard to find. This scanner increases the capabilities of an already very capable radio. Frequency scanning is well suited to the 220 band because of the long periods of silence encountered when monitoring just one frequency. It lets you monitor practically the whole band and participate when and where you wish. I am finding frequencies that I never knew existed. Have you ever heard someone say, "Let's QSY to the other one," and wonder where they went? Never again. Now, let's see... how can I squeeze another vfo into this case?

For More Information

These units are available for a wide range of 2-meter and 220 transceivers, and the price range starts at $39.95. Scan rates, frequency coverage, and switch functions and configurations will vary from model to model. More information can be obtained from *AED Electronics, 750 Lucerne Rd., Suite 120, Montreal, Quebec, Canada H3R 2H6.* Reader Service number 476.

Dave Orozco WB6SMD
Coronado CA

AEA CK-1 MORSE MEMORY KEYER

For some time now, Advanced Electronic Applications, Inc., has been producing some unique and rather exciting products for the radio amateur. Whether the device be an autodialer, an antenna, or an electronic keyer, AEA's products have been injected with a healthy dose of careful research and solid engineering. The company's latest offering, the CK-1 Morse Memory Keyer, is certainly no exception. In a case just barely larger than a typical calculator, we are given a keyer with almost every feature that the dedicated or even not-so-dedicated CW operator could ask for. While it is perfectly possible to put the CK-1 on the air without ever opening the instruction book, you'll want to read and even reread the manual a few times in order to be able to take full advantage of the keyer's capabilities. Once you've figured everything out, you'll never want to part with it!

The first thing you notice about the CK-1 is its apparent simplicity. On top, there is a standard twelve-tone touchpad; it gives a reassuring tactile response to each entry, and an audio confirmation as well, through the tiny but adequate speaker which also is mounted on top. The only other control topside is the combination on-off switch/volume control. Be careful! When you turn the unit off, you erase everything you have programmed into the keyer's memories. Fortunately, AEA assures us that the keyer is designed to be left on continuously.

On the left side of the case is the only other switch on the keyer; this selects either the memory-send or the memory-load mode. On the opposite side of the keyer is a non-shorting, power-input jack.

AEA specifies the unit as requiring 12 V dc ± 3 volts, which is quite reasonable in light of the fact that everything but the side-

tone amp is powered through an on-board 7805 regulator chip. On the back side are found two jacks. One is a DIN plug for input from a keying paddle, and the other is a phono jack for keying a transmitter. As it comes from the factory, the CK-1 is set up for negative keying. If you have a transistorized rig that requires positive keying, don't panic. On the first page of the manual, AEA outlines a simple modification that will allow the keyer to work with your rig. The mod consists of soldering a jumper across a diode inside the keyer. I had the mod completed and the CK-1 happily keying my Icom 701 in five minutes; even the least technically minded among us should have no problems with this one!

Hooking up the paddles is equally simple. Some hams might prefer to see the more standard phone plug used for the paddle input, but space considerations inside the CK-1 don't permit that. Besides, the DIN plug *is* a rather neat arrangement; maybe the Europeans know something we don't!

Once everything is hooked up, the next step is to turn it on. On power-up, the CK-1 is set for 20 wpm with fully-automatic iambic operation, dot and dash memories, and standard weighting. Each of these functions can be selected or rejected individually at your whim, all by entering the proper code through the touchpad. The most eccentric operator can set up this keyer to his personal taste quickly, with the digital-entry method providing a precision and repeatability of adjustment that is impossible with the knobs found on more traditional keyers.

For now, let's assume that you are content to operate with the standard operating parameters, but find the speed a bit too fast for your taste. No problem. The CK-1 offers two methods of changing speeds. If 20 wpm is too fast, you press the " * " button once and then hold down the "7" button. What will greet your ears is a dihdahdihdahdihdah pattern, with each dihdah being a bit slower than the one which preceded it. When it reaches the speed you have in mind, you simply lift your finger off the keyboard and commence operation. If you want to speed up, you follow the same procedure,

Continued on page 157

WILSON SYSTEMS, INC. MULTIBAND ANTENNAS

WV-1A $59.95

FACTORY DIRECT

4 BAND TRAP VERTICAL (10 - 40 METERS)

No bandswitching necessary with this vertical. An excellent low cost DX antenna with an electrical quarter wavelength on each band and low angle radiation. Advanced design provides low SWR and exceptionally flat response across the full width of each band.

Featured is the Wilson large diameter High-Q traps which will maintain resonant points with varying temperatures and humidity.

Easily assembled, the WV-1A is supplied with a hot dipped galvanized base mount bracket to attach to vent pipe or to a mast driven in the ground.

NOTE: Radials are required for peak operation. (See GR-1 below)

SPECIFICATIONS

- 19′ total height
- Self supporting—no guys required
- Weight — 14 lbs.
- Input impedance: 50 Ω
- Powerhandling capability: Legal Limit
- Two High-Q traps with large diameter coils
- Low angle radiation
- Omnidirectional performance
- Taper swaged aluminum tubing
- Automatic bandswitching
- Mast bracket furnished
- SWR: 1.1:1 or less on all bands

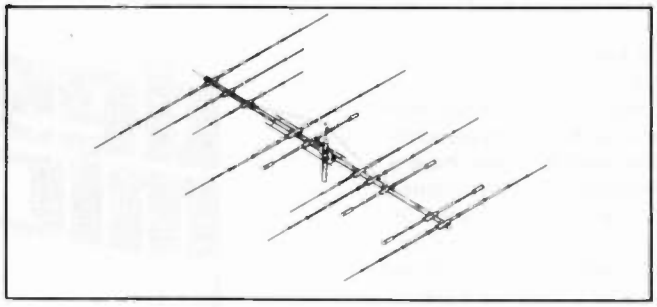
GR-1 $12.95

The GR-1 is the complete ground radial kit for the WV-1A. It consists of 150′ of 7/14 stranded aluminum wire and heavy duty egg insulators, instructions. The GR-1 will increase the efficiency of the WV-1A by providing the correct counterpoise.

33-6 MK $59.95

Now you can have the capabilities of 40-meter operation on the SYSTEM 36 and SYSTEM 33. Using the same type high quality traps, the 40-meter addition will offer 150 KHZ of bandwidth at less than 2:1 SWR. The new 33-6 MK will fit your present SY36, SY33, or SY3 and use the same single feed line. The 33-6 MK adds approximately 15′ to the driven element of your tri-bander, increasing the tuning radius by 5 to 6 feet. This addition will offer an effective rotatable dipole at the same height of your beam.

SY-40A $337.95



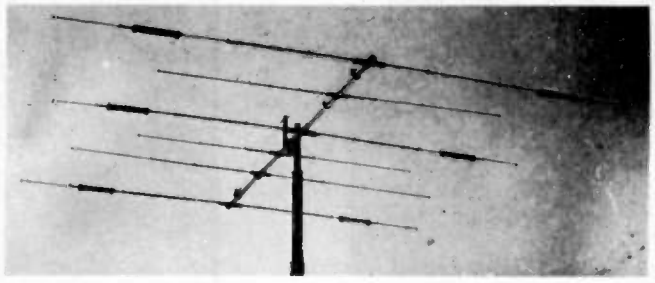
★ 3 MONOBANDERS on 1 Boom
- 4 elements on 20 mtrs FULL SIZE
- 4 elements on 15 mtrs
- 5 elements on 10 mtrs

The System 40A is the answer to the DXer who does not have space to stack monobanders yet wants the advantages they offer. Through the use of a switchable matching unit, only one feed line is required and complete coverage of both the phone and cw bands are available with only one setting.

SPECIFICATIONS

Max. Pwr. Input	Legal Limit	
VSWR @ Res.	1.2:1	
Impedance	50 ohm	
Feed Method	Balun Supplied	
Gain	10 on 15, 20; 12 on 10	
Matching Method	Split Beta	
F/B Ratio	25 db	
Boom	2″ x 26′	
Longest Element	36′	
Turning Radius	22′6″	
Surface Area	12.1 sq.ft.	
Wind Loading @ 80 mph	309 lbs.	
Assem. Weight	75 lbs.	
Shipping Weight	84 lbs.	

SY-36 $199.95

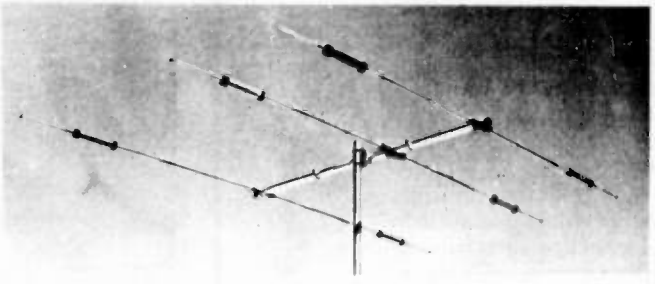


A trap loaded antenna that performs like a mono-bander! That's the characteristic of this six element three band beam. Through the use of wide spacing and interlacing of elements, the following is possible: three active elements on 20, three active elements on 15, and four active elements on 10 meters. No need to run separate coax feed lines for each band, as the bandswitching is automatically made via the High-Q Wilson traps. Designed to handle the maximum legal power, the traps are capped at each end to provide a weatherproof seal against rain and dust. The special High-Q traps are the strongest available in the industry today.

SPECIFICATIONS

Band MHz	14-21-28	
Maximum Power Input	Legal Limit	
Gain (dBd)	9 dB	
VSWR @ Resonance	1.3:1	
Impedance	50 ohm	
F/B Ratio	20 dB or better	
Boom (O.D. x Length)	2″ x 24′2½″	
Number of Elements	6	
Longest Element	29′6½″	
Turning Radius	18′6″	
Maximum Mast Diameter	2″	
Surface Area	8.6 sq. ft.	
Wind Loading @ 80 mph	215 lbs.	
Maximum Wind Survival	100 mph	
Feed Method	Coaxial Balun (Supplied)	
Assembled Weight (approx)	53 lbs.	
Shipping Weight (approx.)	62 lbs.	

SY-33 $149.95



Capable of handling the Legal Limit, the SYSTEM 33 is the finest compact tribander available to the amateur. Designed and produced by one of the world's largest antenna manufacturers, the traditional quality of workmanship and materials excels with the SYSTEM 33. New boom-to-element mount consists of two 1/8″ thick formed aluminum plates that will provide more clamping and holding strength to prevent element misalignment. Superior clamping power is obtained with the use of a rugged 1/4″ thick aluminum plate for boom to mast mounting. The use of large diameter High-Q Traps in the SYSTEM 33 makes it a high performance tri-bander and at a very economical price. A complete step-by-step illustrated instruction manual guides you to easy assembly and the lightweight antenna makes installation of the SYSTEM 33 quick and simple.

SPECIFICATIONS

Band MHz	14-21-28	
Maximum Power Input	Legal Limit	
Gain (dBd)	8 dB	
VSWR at Resonance	1.3:1	
Impedance	50 ohm	
F/B Ratio	Up to 20 db	
Boom (O.D. x Length)	2″ x 14′4″	
Number of Elements	3	
Longest Element	27′4″	
Turning Radius	15′9″	
Maximum Mast Diameter	2″ O.D.	
Surface Area	5.7 sq. ft.	
Wind Loading @ 80 mph	114 lbs.	
Assembled Weight (approx)	37 lbs.	
Shipping Weight (approx)	42 lbs.	
Direct 52 ohm feed	No Balun Required	
Maximum Wind Survival	100 mph	

ORDER FACTORY DIRECT 1-800-634-6898

Prices Effective 1-1-81 to 1-31-81

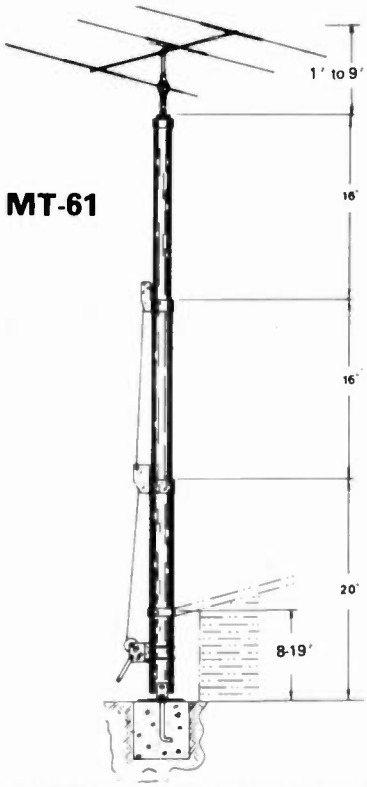
WSI WILSON SYSTEMS, INC.

4286 S. Polaris Ave., Las Vegas, Nevada 89103

Prices and specifications subject to change without notice.

WILSON SYSTEMS TOWERS

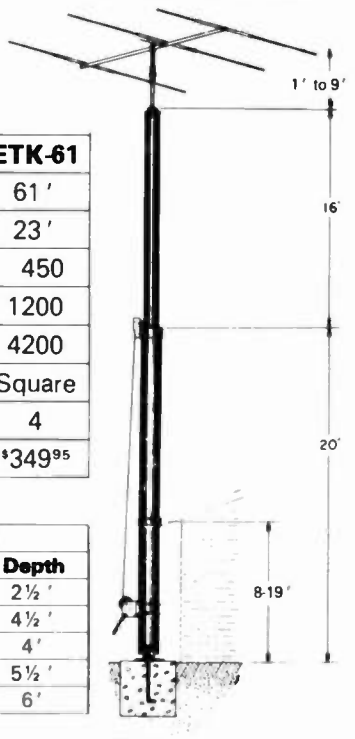
61 FT. TOWERS



MT-61

"NEW"
ECONOMICAL TOWER KIT FOR 45' & 61' TOWERS

45 FT. TOWERS



MODEL	TT-45	ETK-45	MT-61	ETK-61
Max. Height . .	45'	45'	61'	61'
Min. Height . .	22'	22'	23'	23'
Weight (lbs.). .	250	250	450	450
Winch (lbs.) . .	1200	1200	1200	1200
Cable (lbs.) . . .	4200	4200	4200	4200
Tubing	Round	Square	Round	Square
Sections	3	3	4	4
Price	$399.95	$249.95	$614.95	$349.95

Wind Loading		
Tower	Height	Sq. Ft.*
ETK-45	37	15
	45	10
TT-45B	37	18
	45	12
ETK-61	53	15
	61	10
MT-61B	53	18
	61	12
ST-77B	69	16
	77	10

* Square Footage Based on 50 MPH Wind.

BASE CHART		
Tower	Width	Depth
45'	12" x 12"	2½'
FB/RB	30" x 30"	4½'
61'	18" x 18"	4'
FB/RB	36" x 36"	5½'
77 + RB	42" x 42"	6'

The ETK towers offer the ham a chance to have a 45 or 61 ft. tower at a very economical price. The tower is shipped to you in kit form. You do the final assembly and painting. You do not have to do any welding, just bolting together the parts. We supply you with the cold galvanizing compound to put the protective coating on the tower. This is not just paint, but the full galvanizing coating that will give your tower years of service.

Using square tubing, the assembly is fast and easy. It can still be mounted against the house for a non-guyed installation. Or you may use the fixed base for away from the house and completely free-standing installation.

TT-45, MT-61, ST-77

Wilson Systems uses a high strength carbon steel tube manufactured especially for Wilson Systems. It is 25% stronger than conventional pipe or tubing. The tubing size used is: 2" & 3½"-.095; 4½" & 6"-.125; 8"-134. All tubing is hot dip galvanized. Top section is 2" O.D. for proper rotor and antenna mounting.

The TT-45B and MT-61B come complete with house bracket and hinged base plate for against-house mounting. For totally free-standing installation, use either of the tilt-over bases shown below.

The ST-77B cannot be mounted against the house and must be used with the rotating tilt-over base RB-77B shown below.

WILSON ELECTRIC WINCH

Now you can raise and lower your Wilson Tower electrically. The electric winch will replace the hand operated winch. Available for use on the TT-45, MT-61 and ST-77 towers.

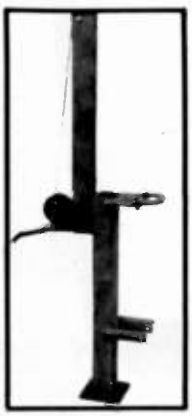
EW-45 (TT-45)
EW-61 (MT-61)
EW-77 (ST-77)
$249.95

Remote Switch. $24.95

TILT-OVER BASES FOR TOWERS

FIXED BASE

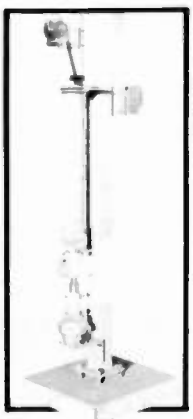
The FB Series was designed to provide an economical method of moving the tower away from the house. It will support the tower in a completely free-standing vertical position, while also having the capabilities of tilting the tower over to provide an easy access to the antenna. The rotor mounts at the top of the tower in the conventional manner, and will not rotate the complete tower.



FB-45 ... 112 lbs. ... $189.95
ETB-45 ... 112 lbs. ... $164.95
FB-61 ... 169 lbs. ... $269.95
ETB-61 ... 169 lbs. ... $244.95

ROTATING BASE

The RB Series was designed for the amateur who wants the added convenience of being able to work on the rotor from the ground position. This series of bases will give that ease plus rotate the complete tower and antenna system by the use of a heavy duty thrust bearing at the base of the tower mounting position, while still being able to tilt the tower over when desiring to make changes on the antenna system.



RB-45B ... 144 lbs. ... $259.95
RB-61B ... 229 lbs. ... $344.95
RB-77B ... 300 lbs. ... $514.95

Tilting the tower over is a one-man task with the Wilson bases. (Shown above is the RB-61B. Rotor is not included.)

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E. van der Smissen WB5ASA
PO Box 149
University of Texas Medical Branch
Galveston TX 77550

Jerry Karlovich WB5PRD
1617 Bittercreek
Garland TX 75040

Emergency Tone Alert System

During the last part of July, 1979, tropical storm Claudette hit the Galveston-Houston area, dropping from ten to forty-five (yes, forty-five) inches of rain in various parts of the region in a very short time. Although the area was well blanketed with repeaters carrying emergency information, the rapid rise of water at night caught many hams unaware; some did not know of the emergency until water started coming into their homes. At that time, there was no way of alerting the radio amateurs once they went to bed, since most of them turned off their two-meter rigs so that the routine chatter on the frequency would not keep them awake.

Claudette made it extremely clear that a method was needed to quickly and efficiently alert area amateurs that an emergency situation existed. Two additional emergencies in rapid sequence made it imperative that we act immediately.

Our need was for a simple, economical system that could be put into effect almost immediately. Discussion on the air and at the August meeting of the Tidelands Amateur Radio Society (TARS) and the University of Texas Medical Branch (Galveston)-Emergency Communications Group (UTMB-ECG) developed criteria for a device similar to the tone-alert system of the National Weather Service (NWS), a single-tone system.

A system for decoding dual tones has been used in Dallas for the past two years. Of the approximately 400 Radio Amateur Civil Emergency Service (RACES) members in Dallas, one hundred have the tone alert available. The usual response to any use of the emergency tone alert is at least 50% of the hams equipped to receive it. The local authorities are very impressed with the ability of the hams to respond to emergencies. The Dallas system is the "A-Tone Decoder" using the DTMF A tone. The tone alert is initiated by Civil Defense. Initially, the alert is on the 146.28/.88-MHz repeater, but it may go to other repeaters if the area of emergency is wider than can be covered by one repeater. The choice of the A tone for this metropolitan area was based upon the high possibility for abuse of other tones. The A tone generally is not available on the pads commonly used by hams. So far, Dallas has had no false alerts, even though some non-hams have gotten access to two-meter equipment and some hams have tried to jam the

Photo A. Completed tone alert.

transmissions.

Tarrant County (Fort Worth), near Dallas, is interested in implementing a similar system in the near future.

The decision of TARS and UTMB-ECG was to develop a tone-alert device based upon the success of Dallas, the ideas expressed by WA3ENK,[1] the WB5PRD design, and utilizing at least a four-second signal of the dual tones of the DTMF figure 9 (which most amateurs have available in a touch-tone™ or comparable pad) as the triggering signal. Use of a relay to silence the audio circuit to an external speaker until activated by the tone was considered the simplest alert device. The four-to-five-second duration of the tone in our tone alert causes a relay to close which then turns on an external speaker or alarm bell.

Twenty copies of the original WB5PRD board were ordered, and within three days the interest was so great that an additional 50 boards were ordered.

The original WB5PRD schematic was modified (but still using the original board) to fit our needs and to use the DTMF 9 tones. Local sources of parts in quantity were inadequate, so parts were ordered to provide 50 tone-alert kits. Parts were ordered from companies advertising in the several amateur radio journals. Upon checking the parts when they arrived, we found one company had shipped 30% of the parts in an inoperable condition, so these had to be replaced. By careful selection of sources, we were able to get the total cost (parts and board) down to $12.50 for each kit. (The prototype using parts bought in small quantities was built for about $18.00.) While awaiting receipt of parts, a construction and testing manual was written.

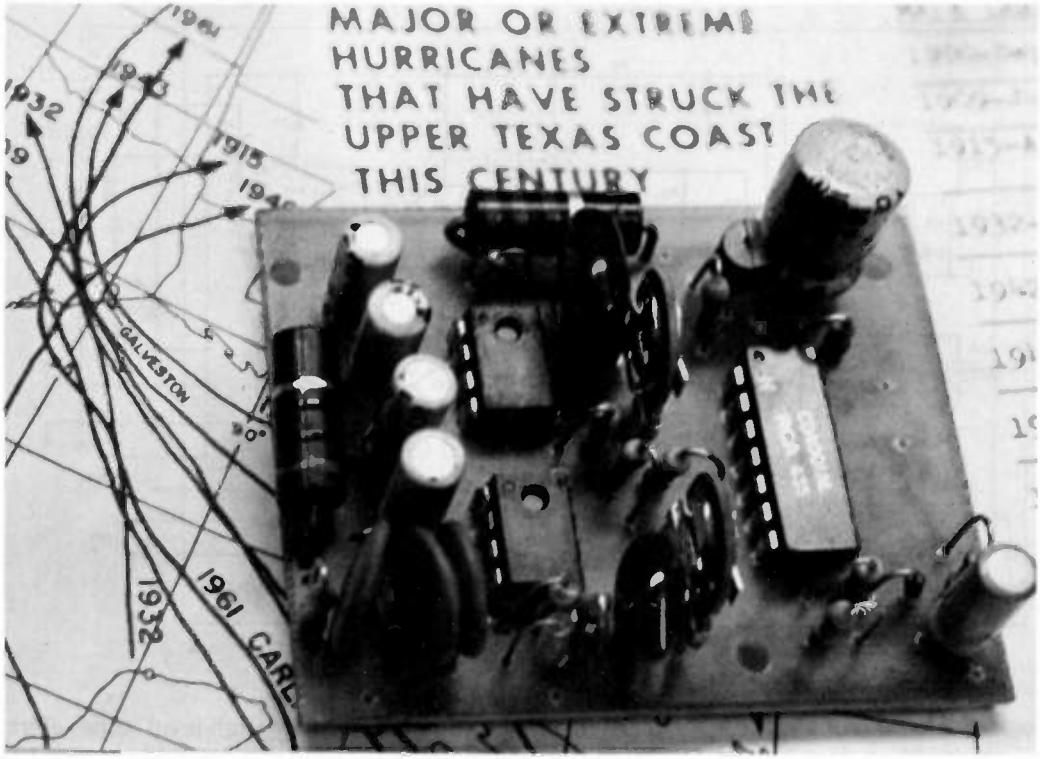

Photo B. Assembled PC board.

Word of what we were doing spread rapidly and inquiries came from other clubs and groups. Discussions concerning this system became quite active among several RACES and CD nets in Houston, Alvin, Clear Lake, and East Texas areas. Several groups asked if the device could be adapted to their special needs.

The concept of TARS and UTMB-ECG calls for the Emergency Operating Centers (EOCs) or a duly-authorized operator to initiate the 9 tone whenever the need arises to activate the net for emergencies. We also use the tone alert to call up our weekly repeater (147.75/.15 MHz) and simplex (145.53 MHz) nets.

As others have discovered, in the absence of phone-patch capability, hams must rely on tone alert.[2] It soon became apparent that two levels of alert would be needed: a low-level alert for personal emergencies such as car trouble, and a high-level alert for general emergencies such as hurricanes, floods, or explosions. A single-tone capability for low-level alerts can be added without additional circuitry, using a toggle switch to ground one decoder output. With the switch in the low position, the tone alert can be activated by a DTMF 7, 8, or 9. We recommend the use of the figure 7 for low-level alerts and reservation of the figure 9 for high-level alerts.

Generally, the amateurs leave the tone alert on low level when they are around the shack and switch to high level when they go to bed. Thus, their alert device would awaken them only for high-level general emergencies.

Several other groups are planning to use the 9 for their alerts. Thus, a number of hams are now using the tone alert with scanners monitoring these several repeaters. The scanners are being modified so that they will scan silently even if there is routine activity on the frequency, but if the 9 signal is given, the scanner will lock onto that frequency and activate the audio.

The Texas DX Society is considering using the tone alert on their repeater to alert members when rare DX is heard on the HF bands. They anticipate using a set of tones other than the 9 so that their signal will not activate scanners that are monitoring the repeaters for emergencies.

Another modification of the tone alert will be for use with weather radios to decode the 1050-Hz tone of the National Weather Service alerts and activate weather receivers not previously provided with tone alert. Since the NWS alert is only a single tone, such use will require only one decoder of the tone alert. The tone alert used for NWS cannot be used at the same time for the DTMF emergency tones.

Why were the 9 and 7 tones chosen? We thought that since 911 is used on the telephone to dial emergencies to fire and police, use of a 9 would be easy to remember as the alert sig-

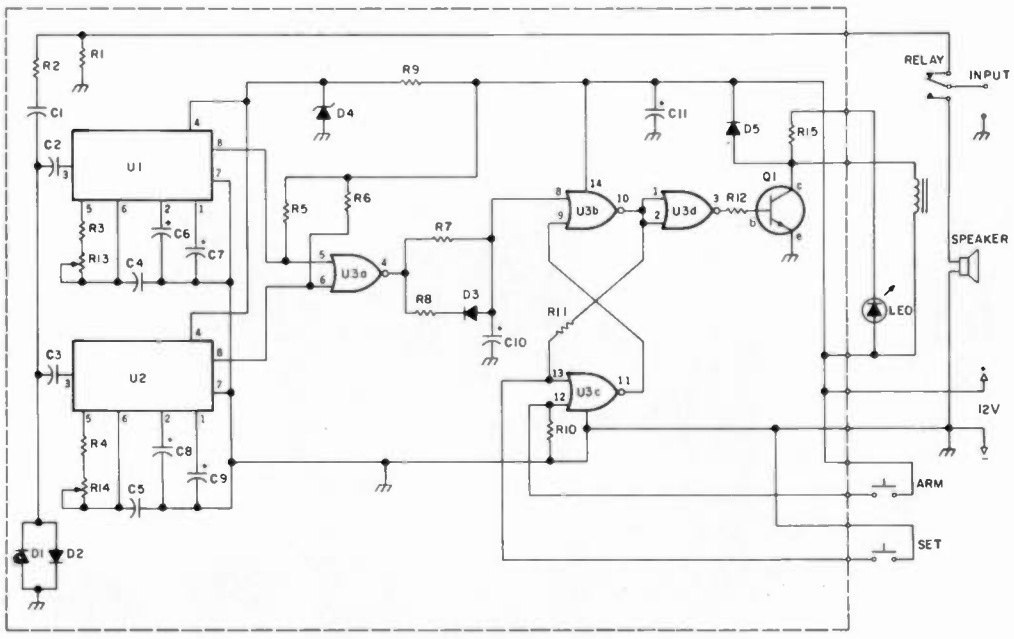

Fig. 1. Schematic diagram. (See Parts List.)

nal. The low-level alert is a good-neighbor service for individual or personal emergencies; therefore, it was considered appropriate to use the 7 or 73 for this alert tone.

Whether a large area such as the Galveston-Houston area is involved in emergencies or smaller local areas only, there is a way to alert only one or the other. If a general alert is involved, then the alerting operator goes from repeater to repeater giving the alert and announcing the emergency. If only a local area is involved, then only the repeater covering that area is alerted.

Because of the seriousness of emergencies that can occur in this region of the Gulf Coast and the potential for abuse, it was early decided to establish the following Galveston County general guidelines for use of the tone alert.

High-Level Alert

1. The tone alert will be activated only by duly-authorized operators acting on behalf of emergencies declared by Civil Defense or other official agencies, or on behalf of the repeater organization.

2. Alert will be sounded:
   a) in the event of a civil emergency;
   b) for a regularly scheduled test or drill;
   c) to call attention to bulletins of general interest during an emergency.

3. Initially, the alert will be sounded on the repeater (147.75/.15 MHz) covering the area affected by the emergency and on 145.53 MHz simplex.

4. Alert will be sounded by transmitting the digit 9 for 15 seconds. The station transmitting the tone will:
   a) identify;
   b) transmit tone for 15 seconds;
   c) call CQ or QST;
   d) state the nature of the emergency or that a test or drill is in progress;
   e) give instructions concerning action to be taken and/or frequencies to be monitored.

5. Individual testing and tune-up of the tone-alert circuit will be done on a simplex frequency other than 145.53 MHz and will not be done on repeaters. Use low power if possible when testing or tuning circuit.

6. High-level tone alert will not be used for routine personal emergencies such as flat tire, out of gas, etc.

Low-Level Alert

1. This alert may be sounded by any amateur having a personal or individual emergency for which he needs help. (It is recommended that a direct call on the repeater or simplex frequency be tried first before using the tone alert.)

2. Low-level alerts will be sounded only on the local area simplex or repeater frequency. Low-level alerts are not to be used for general alerts covering more than one repeater.

3. Alert will be sounded by transmitting the digit 7 for 15 seconds. The station transmitting the tone will:
   a) identify;
   b) transmit the 7 tone for 15 seconds;
   c) call CQ or QST;
   d) state the nature of the emergency and request the necessary assistance.

This plan has been operational since August, 1979, is gaining adherents, and the idea is spreading. Based upon our experience, we would recommend this or a similar system to other amateurs participating in emergency activities.

Circuit Description

The schematic is shown in Fig. 1. The components listed in the Parts List are standard items which are readily available. Advantages and disadvantages of the 567 PLL tone decoder have been discussed previously in the amateur literature.[3,4]

The circuit is powered from a 12-volt dc source. Zener diode D4 provides 6.2 volts dc for U1 and U2.

When the circuit is armed by bringing pin 12 of U3c to logic one briefly, audio is routed through the normally-closed contact of the relay to loading resistor R1 and to the input of the decoder circuits through R2. Germanium diodes D1 and D2 conduct at 300 mV to protect the circuit from audio overload. C2 and C3 pass the audio tones but block dc from entering U1 and U2 along with the audio signal.

U1 and U2 decode the high and low tones, respectively. R3, R13, and C4 set the center frequency of U1; R4, R14, and C5 set the center frequency of U2 (bandwidth is about 5% of the center frequency).

When a decoder locks on an incoming tone, pin 8 goes to logic zero. When both U1 and U2 are locked, pin 4 of NOR gate U3a goes to logic one. C10 then charges through R7 to provide a delay before pin 8 of U3b reaches logic one. U3d inverts the output of U3b. The sequence is now complete, the relay and LED are activated by Q1, and audio is now routed to the speaker until the circuit is again armed.

A total delay of three to four seconds is introduced between initial reception of the tone and activation of the relay to prevent false activation of the circuit.

D3 and R8 provide a discharge path for C10 when no tone is present. This prevents a buildup of charge over a period of time from intermittent false signals which might cause activation of the circuit. D5 protects Q1 from the transient voltage present when the relay is deactivated.

Momentarily closing the normally-open ARM (RESET) switch will deactivate the relay (open the audio circuit to the speaker) and will arm the decoders so that they can respond to an incoming tone signal.

Momentarily closing the normally-open SET switch will activate the relay so that audio goes to the speaker. This mode will continue until the ARM (RESET) switch is activated. (A momentary DPDT toggle switch with center off can be used in place of two separate momentary switches.)

Assembly

The circuit was assembled on a WB5PRD circuit board. (Drilled printed circuit boards are available from WB5PRD for an SASE and $4.00.) The foil side of the board is shown in Fig. 2, which is suitable for use in reproducing the board. An assembled PC board and a completed tone alert are shown in the photographs.

Parts layout is shown in Fig. 3. Assembly can be facilitated if one starts with those components at the center of the board and works outward toward the edge. Diodes, capacitors, trimpots, and quarter-Watt resistors are mounted vertically. The two one-Watt resistors are mounted horizontally. If proper care is taken as to which end of the vertically-mounted resistors is upmost, then that point of the resistor can be used as a test-point contact for testing other parts of the circuit. (See Table 1.)

The usual precautions should be observed when handling the 4001 CMOS integrated circuit. For temperature stability, C4 and C5 must be high-quality mylar™ or metallized film capacitors.

The switches and LED are installed on the front panel or speaker enclosure. The LED should be near the SET switch; the LED lights when the tone-alert unit is in the SET activation. The relay is installed off the circuit board with epoxy glue or silicone rubber. A multi-pole relay may be substituted if other devices, in addition to the speaker, are to be controlled. (Remember that when other devices such as bells or buzzers are on the relay, they will be activated when the SET switch is activated.)

The twelve-volt dc supply is connected between points marked + and − (ground). One side of the relay coil and the LED anode are connected to point K&L and the other side of the relay coil goes to K. The cathode of the LED goes to L. The ARM (RESET) switch is connected to the points marked A. The SET switch is connected to the two points marked S. Audio is connected between INPUT and ground. Points E, B, and C indicate the emitter, base, and collector of Q1.

Tune-Up

The tone alert may be adjusted for the DTMF tone 9 using either of two procedures—either a frequency counter or a voltmeter may be used. With the frequency counter method, the counter is connected to U1 at pin 5 (for a square wave) or pin 6 (for a triangle wave), and R13 is adjusted until the counter shows 1477 Hz. Take care not to load the circuit with the test equipment. Next, connect the counter to pin 5 or 6 of U2 and adjust R14 until the counter shows 852 Hz.

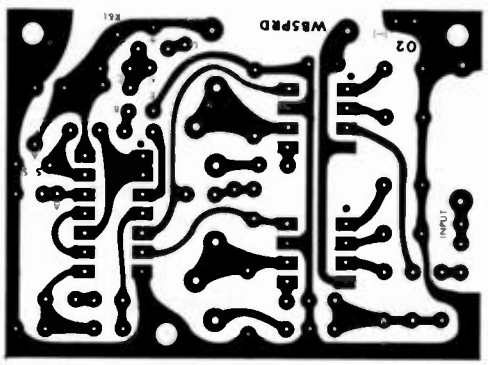

Fig. 2. PC board, foil side. This is suitable for reproducing the board for those who would like to do so.

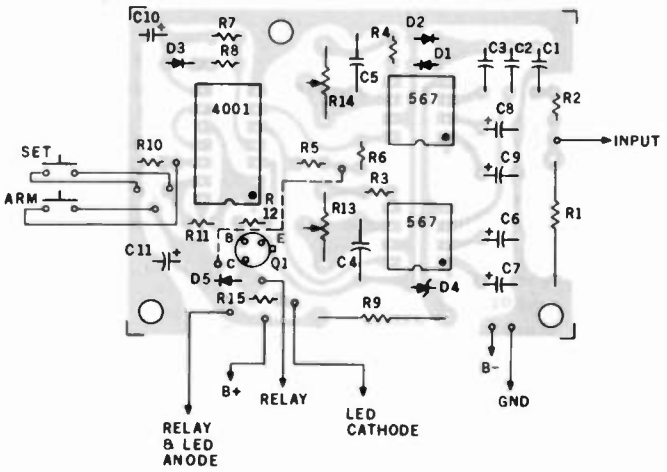

Fig. 3. Parts layout.

Alternatively, a voltmeter or logic probe may be used. Start with R13 and R14 fully counterclockwise. Apply an alert tone with the probe on pin 8 of U1 or pin 5 of U3 and slowly turn R13 clockwise. Note the position of R13 when the voltage drops and continue turning R13 clockwise until the voltage goes back up; note this point. Turn R13 counterclockwise to a point midway between the two voltage change settings. Do the same with the probe on pin 8 of U2 or pin 6 of U3 while adjusting R14.

Operation

Apply 12 volts dc to the unit. Momentarily close the SET switch; the relay should activate. Provide an audio input from the two-meter rig. The circuit will not function properly with a high noise signal or with too little audio drive. Turn the audio gain up to ensure proper drive level. The loading resistor is rated at one Watt. ARM the circuit and have another operator transmit an alert tone on a simplex frequency for fifteen seconds. The unit should activate in less than ten seconds.

Circuit Alternatives

The circuit can be tuned for tones other than the digit 9. The standard tone pairs are listed in Table 2.

Component	Connection
R3	Pin 5, U1
R4	Pin 5, U2
R5	Pin 5, U3a
R6	Pin 6, U3a
R7	Pin 8, U3b
R8	Pin 4, U3a
R11	Pin 2, U3d
R12	Pin 3, U3d

Table 1. The end of the component connected to the listed test point is placed in the up position.

Low Tone	High Tone			
	1209 Hz	1336 Hz	1477 Hz	1633 Hz
697 Hz	1	2	3	A
770 Hz	4	5	6	B
852 Hz	7	8	9	C
941 Hz	*	0	#	D

Table 2. DTMF tone pairs. Each digit or sign is composed of two tones. For example, 1 is composed of a 697-Hz tone and a 1209-Hz tone.

Low Tone (Hz)	R4 (kilohms)	High Tone (Hz)	R3 (kilohms)
697	11.0	1209	5.6
770	10.0	1336	5.6
852	8.2	1477	5.6
941	8.2	1633	3.9

Table 3. Alternate values for R3 and R4.

Pin	Set	4001 Armed	Tone Present	U1 and U2 Pin	Voltage
1	Low	High	—	4	6.2 V
2	Low	High	—	5	12.0 V (no
3	High	Low	—		alert tone)
4*	Low	Low	High		0.1 V (alert
5*	High	High	Low		tone present)
6*	High	High	Low		
7	--------Ground pin--------				
8*	Low	Low	High		
9	High	Low	—		
10	Low	High	—		
11	High	Low	—		
12**	Low	Low	—		
13	Low	High	—		
14	---------12 volt pin---------				

*These remain at the same state during SET and ARMed periods and change only during the presence of the alert tone. Do not replace the chip yet if any of these pins do not agree.
**This pin should go high while pressing the ARMed button.

Table 4. Logic and voltage chart.

The corresponding alternative values for R3 and R4 are shown in Table 3.

Most of the delay between the introduction of an alert tone and relay activation is introduced by R7 and C10. These may be adjusted to provide a longer or shorter delay.

If one wishes to have both a low level of alert and a high level of alert, this can be done by adding an SPST toggle switch so that pin 5 of U3a (or pin 8 of U1) can be grounded. With pin 5 or pin 8 grounded, only a single tone (852 Hz) will activate the unit. With the switch in the closed (grounded) position, the tone alert can be activated by the digit 7 for a low-level or personal emergency, and in the switch-open position, it will take both tones of the digit 9 to activate the unit.

Weather Watch (Alert) Modifications

Only minor changes are required on this circuit to decode the NWS 1050-Hz alert tone for weather radios that do not have this feature. U1, R3, R5, R13, C4, C6, and C7 are omitted. A jumper is placed between the foils originally intended for pins 7 and 8 of U1. R14 is adjusted for 1050 Hz at pin 5 or 6 of U2. Activation methods and time will remain the same.

Troubleshooting

Step One: Most problems with performance can be traced to bad solder joints, solder bridges, incorrect parts placement, or failure to observe polarity of diodes or capacitors. All construction steps should be retraced with this firmly in mind.

Step Two: Confirm that adequate noise-free audio is actually present at the input and that the relay will work out of the circuit. Close the SET switch to activate the relay.

Step Three: Use a VTVM or FET-VOM (at least a megohm resistance) and check the voltages listed in Table 4.

Step Four: Using a piece of hookup wire, connect one end to ground and carefully touch the other end to both pins 5 and 6 of U3 with the circuit ARMed. The relay should activate in about four seconds. If it takes as long as thirty seconds to activate the relay, check R7, R8, C10, and D3. If this fails, replace U3.

Step Five: Check U1 and U2 for proper tuning.

Step Six: Ground pin 8 of U1 and send a DTMF digit 7 signal over the audio input. If this activates the relay in 4-6 seconds, then U2 is tuned and functioning. If the relay does not activate, then replace U2 and try again.

Step Seven: Ground pin 8 of U2 and send a DTMF digit 3 signal over the audio input. If this activates the relay in 4-6 seconds, then U1 is tuned and functioning. If the relay does not activate, then replace U1 and try again. ■

Parts List

Resistors
R1—10 Ohms, 1 Watt
R2—1.5k Ohms, ¼ Watt
R3—5.6k Ohms, ¼ Watt
R4—8.2k Ohms, ¼ Watt
R5, 6, 11—27k Ohms, ¼ Watt
R7—560k Ohms, ¼ Watt
R8—1k Ohms, ¼ Watt
R9—220 Ohms, 1 Watt
R10—10k Ohms, ¼ Watt
R12—22k Ohms, ¼ Watt
R13, 14—5 kilohms, vertical trimpots
R15—1k Ohms, ¼ Watt

Capacitors
C1, 2, 3—0.1 μF ceramic disc, 25 V
C4, 5—0.1 μF mylar™, 16 V
C6, 8—1.0 μF electrolytic, 6 V
C7, 9—10.0 μF electrolytic, 6 V
C10—3.3 μF electrolytic, 16 V
C11—100 μF electrolytic, 16 V

Semiconductors
D1, 2—1N34A germanium (or equivalent)
D3—1N914 silicon (or equivalent)
D4—6.2 volt, 400 mW zener
D5—1N4001 (or equivalent)
Q1—2N2222 NPN transistor
U1, U2—567 dual inline, tone decoder
U3—4001 CMOS logic block
Keep CMOS wrapped In foil until ready to install.
LED—jumbo LED of choice

References

1. Rodney A. Kreuter WA3ENK, "Two Meter Tone Alert," *73 Magazine*, January, 1979.
2. Stan Horzepa WA1LOU, "FM/RPT—Tone Alert Standards," *QST*, December, 1979.
3. J. H. Everhart WA3UXH, "Toward A More Perfect Touch-tone Decoder," *73 Magazine*, November, 1976.
4. Rick Swenton WA1LWV, "Tone Decoder Improvements," *73 Magazine*, February, 1979.

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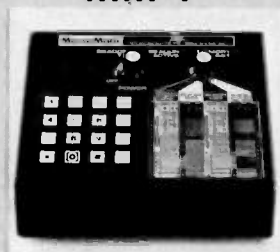				
MorseMatic™	Keyer Trainer	Morse Trainer	Contest Keyer	Morse Keyer

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Speed Range (WPM)	2-99	1-99	1-99	1-99	2-99	8-50	5-50+	?	8-50
Memory Capacity (Total Characters)	500			500		400	100/400	400	
Message Partitioning	Soft			Soft		Hard	Hard	Hard	
Automatic Contest Serial Number	Yes			Yes		No	No	No	
Selectable Dot and Dash Memory	Yes	Yes		Yes	Yes	No	No	No	No
Independent Dot & Dash (Full) Weighting	Yes	Yes	Yes	Yes	Yes	No	No	No	No
Calibrated Speed, 1 WPM Resolution	Yes	Yes	Yes	Yes	Yes	No	No	Yes	No
Calibrated Beacon Mode	Yes			No		No	No	No	
Repeat Message Mode	Yes			No		Yes	Yes	Yes	
Front Panel Variable Monitor Frequency	Yes	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes
Message Resume After Paddle Interrupt	Yes			Yes		No	No	Yes	
Semi-Automatic (Bug) Mode	Yes	Yes		Yes	Yes	No	No	No	No
Real-Time Memory Loading Mode	Yes			Yes		Yes	Yes	No	
Automatic Word Space Memory Load	Yes			Yes		No	No	Yes	
Instant Start From Memory	Yes			Yes		No	No	Yes	
Message Editing	Yes			Yes		No	No	No	
Automatic Stepped Variable Speed	No	No	No	Yes	No	No	No	No	No
2 Presettable Speeds, Instant Recall	No	No	No	Yes	No	No	No	No	No
Automatic Trainer Speed Increase	Yes	Yes	Yes						No
Five Letter or Random Word Length	Yes	Yes	Yes						No
Test Mode With Answers	Yes	Yes	Yes						No
Random Practice Mode	Yes	Yes	Yes						Yes
Standard Letters, Numbers, Punctuation	Yes	Yes	Yes						Yes
All Morse Characters	Yes	Yes	Yes						No
Advertised Price	**$199.95**	**$129.95**	**$99.95**	**$129.95**	**$79.95**	**$139.95**	**$ 99.50/ $139.50**	**$229.00**	**$129.95**

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WWV-to-80-Meter Converter

This simple and inexpensive frequency converter will place the WWV 10-MHz signal anywhere within the 80-meter band. Credit for the basic design goes to PM Electronics, a local firm that is now defunct.

Referring to the schematic in Fig. 1, L1-C2 are tuned to the WWV 10-MHz signal. This signal is coupled to the base of Q1 by L2. Oscillator Q2 operates at any selected crystal frequency between 6 and 6.5 MHz, and is coupled to the emitter of Q1 by C7. Q1 mixes the two frequencies. The L3-C5-C6 combination is tuned to the 3.5-to-4-MHz difference frequency which appears at the collector of Q1. Impedance matching to the 50-Ohm receiver antenna is provided by the C5-C6 capacitive divider.

Crystal frequency is determined by subtracting the desired 80-meter frequency from the WWV 10-MHz frequency. The 3750-to-3800-kHz range (6250-to-6200-kHz crystal) might be a good choice for minimum signal interference. The crystal may be obtained from Jan Crystals, 2400 Crystal Drive, Ft. Myers FL 33906. Specify type FT-243 holder and desired crystal frequency. This crystal will be .005% tolerance. Jan's 1980 catalog (#23) lists this crystal at $2.00 each with a 30-cent per crystal handling and first class mail charge. The FT-243 socket, part SSO-1, also may be obtained for an additional 30 cents.

The circuit board can be quickly and easily made by first positioning and securing the copper face of a 1-3/4" × 3-3/8" board under the circuit pattern in Fig. 2. Next, mark through the pattern at each hole location and then drill a #60 hole at each mark. The inductor pin and crystal socket holes may require pattern adjustment and larger holes. Also, check the lead spacing of your capacitors. The layout is for 1/4-inch spacing but room is available for the 3/8-inch variety.

Finally, carefully connect the related holes with 1/8-inch strips of art or masking tape. Place masking tape over the component side of the board to prevent acid from entering the holes. Thoroughly clean the copper surface after etching. Using this method, I easily etched and assembled a checkout board in one afternoon.

The inductors are wound on a 1/4-inch diameter slug-tuned coil form as shown in Photo A. These may be found in most junked TV sets and radios. As viewed from the base, coils L1 and L2 are wound counterclock-

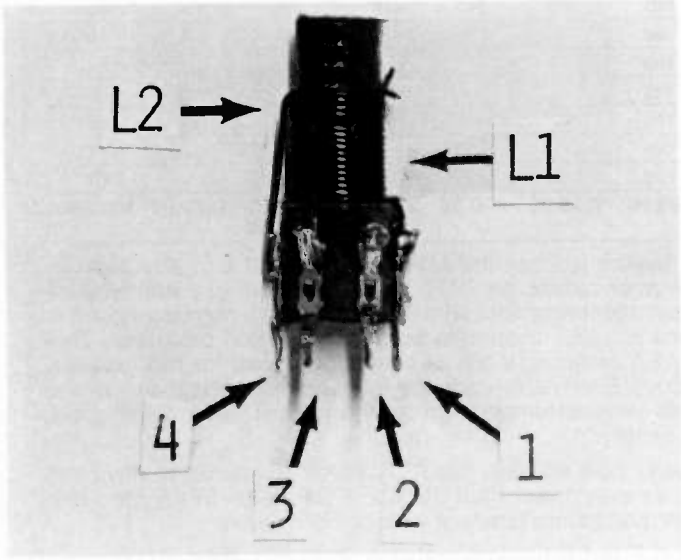

Photo A. Close-up of the L1-L2 inductor. L1 is 12 ccw turns and L2 is 4 ccw turns of #24 enameled wire. L3 is 35 cw turns of #32 enameled wire. All inductors are wound on a 1/4-inch slug-tuned coil form.

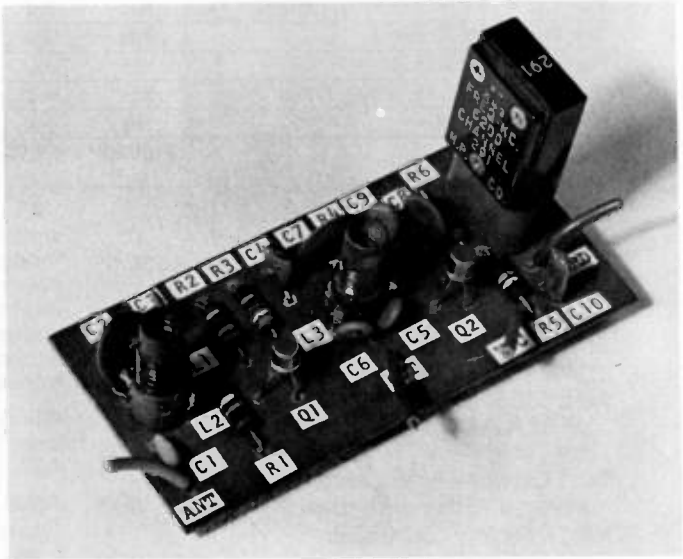

Photo B. Top view of the completed WWV-to-80-meter frequency converter.

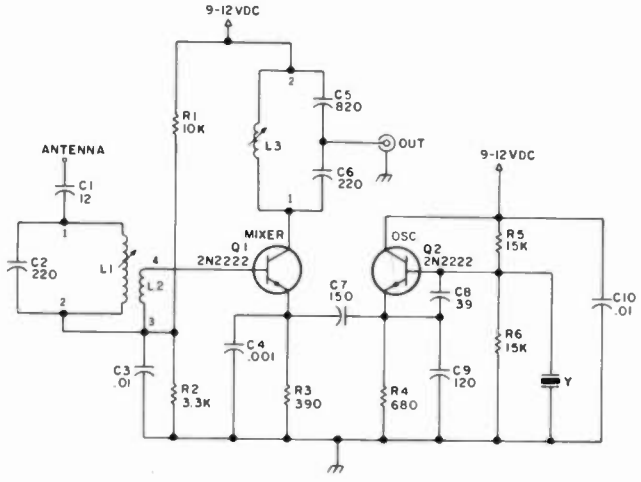

Fig. 1. Schematic diagram of the WWV converter. Resistors are 1/4 or 1/2 Watt. Capacitors C3 and C10 are Mylar™, with all others being disc ceramic.

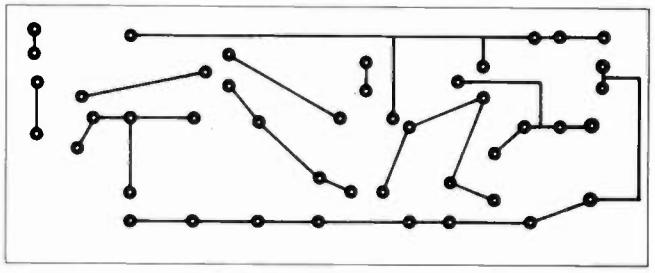

Fig. 2. Foil side of the circuit board.

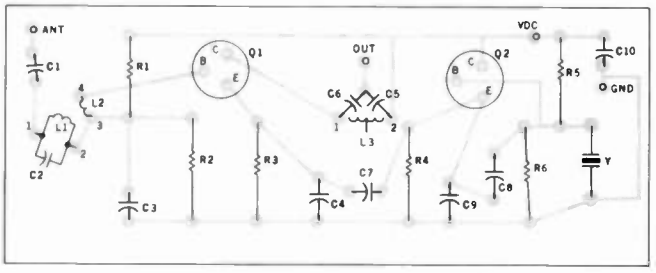

Fig. 3. Parts placement guide (foil side shown).

wise with #24 enameled wire, and L3 is wound clockwise with #32 enameled wire. All three inductors are wound with no space between turns. L2 begins at the end of L1 with no space between the end of L1 and the start of L2. Secure the coil ends with thread or tape and apply two or three coats of varnish to hold the coil in place.

Capacitors C2, C5, and C6 are soldered directly to the inductor pins. I tried several sets of transistors, both NPN and PNP types, and they all worked. Just reverse the voltage polarity for PNP types. To align, connect a short antenna and set L1 and L3 for maximum S-meter reading with a nonmetallic tool. Use shielded cable for hookup to the receiver.

My thanks to Chuck Allyn, who so kindly provided the photographs for this article. If you have a question or need parts help, an SASE will bring a prompt reply. ■

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Kankakee IL 60901

Cheap and Simple

— your basic 13.8-V, 25-A power supply

The 13.8-volt ham radio transceiver has really come of age. Many of these units are great for mobile operation, but when it comes to fixed-station use, the transceivers can really come up short—primarily because of the comparatively high current values they draw on peaks.

The two-meter FM and police-scanner industries have given us a variety of 13.8-volt, low-current power supplies which in many cases can be bought more cheaply than built. However, the seemingly rarified 13.8-volt, fifteen-Amp (or higher) power supply is not that easy to come by, which really limits the possibilities with transceivers drawing anywhere from sixteen to twenty Amperes.

Scanning the catalogs became a depressing experience for me, particularly when supporting one wife, three cats, and twelve hobbies on a pilot's salary. There are a number of excellent commercial power supplies available, but you can expect to pay an absolute minimum of $100 for low-current versions and as much as $300 for a power supply beefy enough to keep my Vibroplex Presentation dancing its way through the kilos and megas. Besides all that, my idea of a power supply is something that sits in a darkened corner, is not seen, and is purely an accessory to my equipment. $100? $200? $300? For a lousy power supply?

Occasionally, a magazine article has slipped through on the subject of 13.8-volt, high-current power supplies. Unfortunately, in many cases the authors have escaped the world of simplicity and featured components and techniques that are available easily only through NASA. Hence, I drew up a priorities list so that I could readily view my criteria for such a power supply: 1) cheap, 2) simple, 3) cheap, and above all, 4) cheap. I am one of those chicken-wire and chewing-gum types whose home-brewed projects are best characterized as "functional" and are best unseen. (At least with power supplies, anyway.)

My particular need was to supply power to an Atlas 210X. While my home station is basically a salvage yard for old boat anchors, six years or so ago I pressed the Atlas into mobile service. In fact, mobile operation is all my Atlas has ever seen. Until recently it has

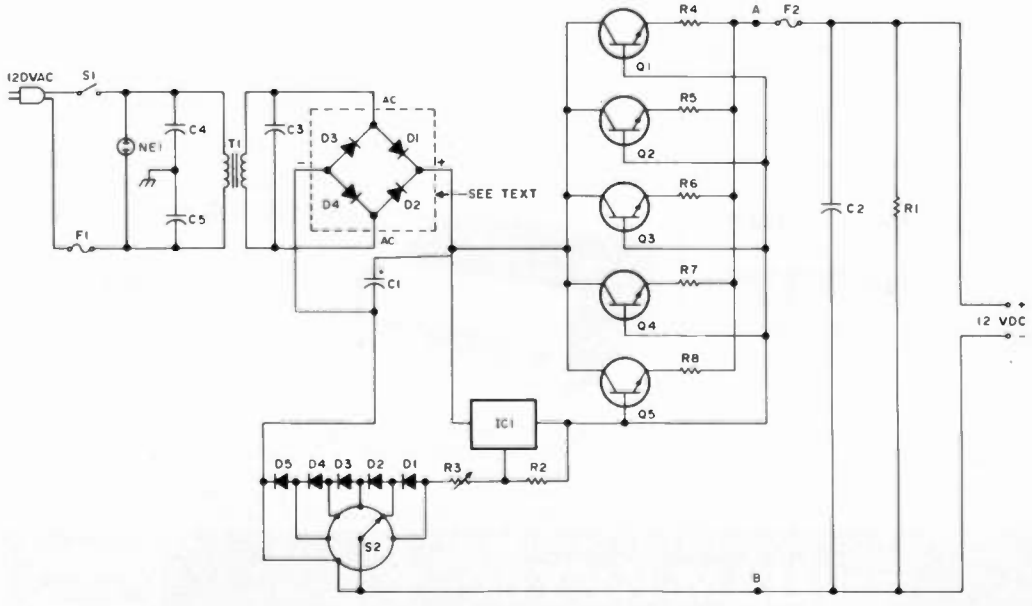

Fig. 1. Power supply schematic diagram.

never known the joy of taking a spike from the ac mains. Besides, with a dc supply, I could haul the 210X into the motel room, run coax out to the bumper mount, and dit-dah my eyeballs out.

Why not carry around a car battery and trickle charger, you ask? Too messy and cumbersome. Another option was to buy the factory-built console/power supply, but I heard rumors (only rumors) that the console/power supply left a little to be desired in the regulation department.

The Circuit

The power-supply circuit uses 2N3055 transistors. You can tailor your current capability by the number of pass transistors you use. I wanted a 25-Amp supply, so I used five 2N3055s. You can figure roughly one transistor for every 5 Amps you'll be drawing. In a 10-Amp supply, only two transistors would be used, and so on.

The 2N3055 is an NPN power device built into a TO-3 case. The 3055 is one of the more easily come by transistors and is very cheap (meeting criteria 1, 3, and 4). Because of the power these little devils are going to be dissipating, heat sinks should be employed. I used a heat sink with approximately 27 square inches of surface area with four half-inch fins, which cools nicely. Extreme heat can quickly mess up the transistor junction (not to mention a nice paint job). Before securing the transistors to the heat sink, apply some silicone thermal compound between the 3055s and the surface of the heat sink to provide a good positive heat transfer.

I have always used the rule of thumb that if you can't touch it, you can blow it. If you don't care to go heat-sink shopping, use a cooling fan. If you use a fan in addition to the heat sink, be sure the air circulates in line with the fins. Blowing air perpendicularly to the fins sets up standing waves—the aerodynamic kind—and turbulence and the cooling effect is minimal.

Transistor-mounting hardware is nice, but I didn't feel that it was necessary. I attached the transistors directly to the heat sink and then mounted the whole heat-sink assembly on a sheet of Plexiglas™ attached to four standoffs. Since the transistor case is common to the collector, I tapped a screw into one of the heat-sink fins and this became my common collector tiepoint. It is important to keep all lead lengths constant. After drilling matching holes for the base and emitter pins in the heat sink, heavy-gauge wire was soldered (carefully) to each emitter pin through a 0.25-Ohm resistor, and then a second piece of wire was attached to each base pin. I then had only to connect the rest of the circuit to either the heat sink or one of the two bus wires.

You may or may not have difficulty locating a suitable transformer capable of taking 120 V ac and squeezing it down to 17 to 24 V ac. I was lucky enough to locate an old, beat-up, ex-battery-charger transformer at a hamfest which gave me 120/17 V ac. I think you will find old battery chargers to be a good source for the transformer you will need. Remember, the transformer must be capable of carrying the current you are going to draw from your power supply. I paid $3.00 for my transformer and felt robbed; I have seen them for a dollar. Yes, you do take a risk, but remember, even if the transformer is no good, it is an excellent source of #14 AWG antenna wire (or larger)!

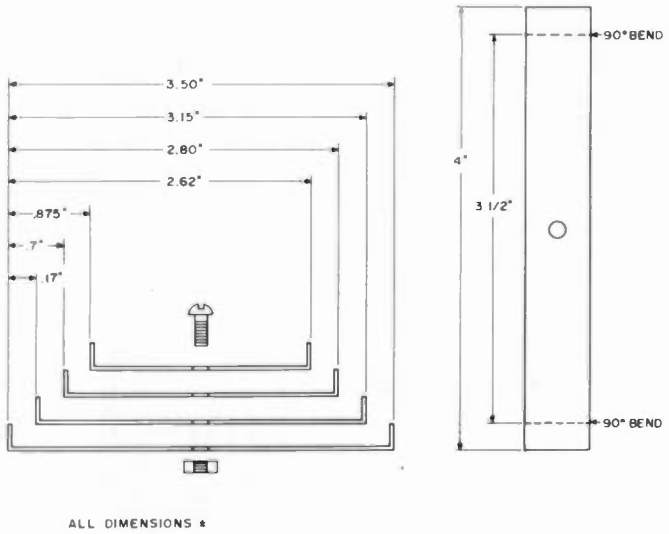

Fig. 2. Heat sink construction details.

In the rectifier circuit there are two avenues to follow. You can buy four diodes and make your bridge or you can do as I did and use one of the nifty one-inch-square epoxy bridge rectifiers. The little one-inch jobs are convenient because you don't have to mess around figuring which end is the anode and which is the cathode. Ordinarily, the epoxied bridges are simply marked AC, AC, +, and −. Can you beat that?

As always, no matter what you do for rectification, be sure your rectifier is rated for the current you will be needing. Most of the little square bridges are rated between 20 and 35 Amps. I am using a Semtech-Alpac 7905 only because I happened to have one on hand. Motorola, International Rectifier, VARO, and EDI make excellent equivalents.

Voltage regulation depends on adequate filtering and an IC known as a 7812. After much experimentation, I found that my voltage regulation (as well as hum attenuation) improved as I increased the value of filter capacitor C2. Starting out with 2000 uF, I worked my way upward to 13,000 uF. Though I now have a 37,000-uF filter capacitor in the circuit, 13,000 uF seemed to be enough. The amount of filtering achieved by going from

Parts List

C1—13,000-uF, 25-V electrolytic capacitor
C2—10-uF, 25-V electrolytic capacitor
C3—0.22-uF, 100-V tubular capacitor
C4, C5—0.01-uF, 500 V ceramic capacitor
D1-D4—25-A diodes or epoxy bridge rectifier (see text)
D1-D5—1N4004 diodes
F1—Fuse, 5 Amp
F2—Fuse, 30 Amp
Q1, Q2, Q3, Q4, Q5—2N3055 transistors
R1—120-Ohm 4-W resistor
R2—3000-Ohm, ½-W resistor
R3—500-Ohm, 1-W potentiometer
R4, R5, R6, R7, R8—0.25-Ohm, 1-W resistor
IC1—7812 voltage regulator
S1—SPST switch
S2—6-position wafer switch
T1—120/17-24-V ac power transformer (see text)
Miscellaneous: NE1 neon bulb, binding posts, line cord, 0-25-V dc voltmeter, 0-30-A ammeter, heat sinks, chassis, blower, fuseholders, and bulb socket.

13,000 to 37,000 uF is very, very slight and detectable only with a scope. Obviously one can't ignore the thought that if 13,000 uF is good, a higher value would be better, but let me caution you enthusiastic high-capacity freaks against installing 150,000-uF capacitors without limiting inrush current. I haven't experimented beyond 37,000 uF.

The 7812 voltage regulator is an IC device capable of maintaining excellent regulation as long as the input voltage falls between 14.6 and 19 volts nominally. A number of companies are producing the 7812 and it generally has some sort of prefix or suffix, but the digits remain the same.

In this circuit, the 7812 is above ground through a 200- to 500-Ohm resistor. I don't put an exact value on this because it is not that critical. Going from receive to full-output transmit on my Atlas (300 mA to peaks of 16 Amperes), the voltage drop on the power supply is 0.4 V, which ain't bad. Since I normally don't run my equipment at full bore, the drop from receive to transmit is quite small.

As was the case with the pass transistors, I mounted the 7812 on a heat sink affixed to a small piece of Plexiglas on standoffs (to simplify its isolation from the chassis). The heat sink (see Fig. 2) is made of four strips of one-inch-wide aluminum cut at varying lengths and bent up a half-inch at each end. I then placed each one "inside" a larger one until, voilà, La Heat Sink a la Cheap. To keep the strips aligned, a hole was drilled which also served to attach the 7812.

While it isn't necessary, you can build in a selectable voltage feature by connecting any number of 1N4004 diodes on a wafer-type switch. This switch goes between pin 3 of the 7812 and ground. (If this seems like a lot of hooey to you, you may disregard the above and connect pin 3 of the 7812 to ground through R3. You will see a voltage change of approximately 0.7 V with each position on the switch. With my supply, I have the capability of as much as 15 V or so, and the switch permits me to "switch down to" the proper voltage I desire (13.8 V dc).

The value of bleeder resistor R1 across the output is not critical either, but have something there for your protection.

By varying the resistance of R3, your output voltage will vary considerably. I believe a potentiometer instead of a fixed-value resistor is a better route so that more flexibility is available for future voltage needs which now might not be considered. As in my case, if you are receiving 16.8 V from your transformer, 250 Ohms is sufficient to yield the 13.8 V dc you want.

Should you be supplying your rectifier with 16 to 18 volts and not be getting a stable 13 volts or so, check to be sure that you are not losing (dropping) all of your voltage in your rectifier diodes or epoxy bridge. Some of the epoxy bridge rectifiers are poor in the area of voltage consistency. Try a different one, even of the same manufacturer. Another place to watch for voltage losses is in your wiring. The more current you draw, the higher your voltage drops may become in your transformer, rectifier, filter capacitor, or wiring. Wire which is too small may cause substantial voltage drops. I would suggest using #14 AWG wire at least.

H-u-m-m-m-m

My first test of the power supply was disastrous. Not only was the regulation terrible, but the audio was 80% hum, 20% ham. Two things lead to the elimination of hum: First (and already covered), I placed my voltage regulator above ground on the Plexiglas support; second, I connected all of my chassis ground connections to one point.

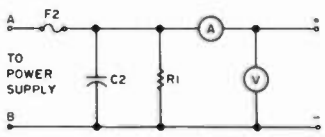

Fig. 3. Power supply metering arrangement.

As with my other homebrew endeavors, I first mounted the power supply on an open chassis. Breadboarding can save you much agony when it comes time to actually fitting the darned thing in a permanent box. Scouting around at the Dayton Hamvention, I was able to come up with a perfect cabinet (which formerly was a microvolt meter) for $1.00. When shopping for an enclosure, don't overlook old, non-working test equipment, etc.

Metering can be added easily as shown in Fig. 3. (When will the price of meters ever come down?)

The cost is going to vary depending on the state of your junk box and what kind of hamfest bargains you can locate. I spent more than I really wanted to, and that was slightly over ten dollars. You can't beat the pages of *73 Magazine* for bargains on the components used here; it was from there that I purchased all of my purchased parts.

As you build this, take your time. Do a good job. Dress all of your leads. Use red wires for + and black wires for −. Take time to consider the aesthetics of this project. Then tuck it away in a dark corner and ignore it, because it's only a stupid power supply. ■

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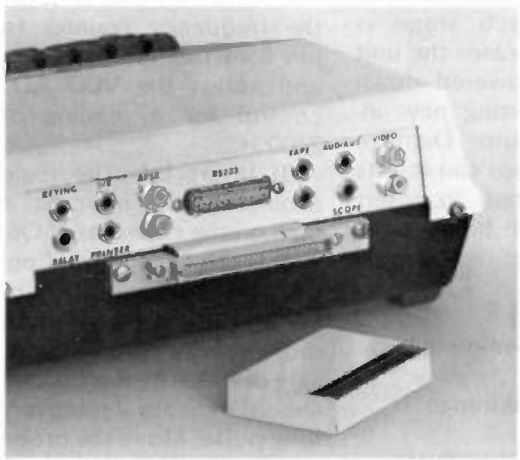

51

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Innovators in Digital Communications

Dr. Ralph E. Taggart WB8DQT
602 South Jefferson
Mason MI 48854

Direct Printing FAX

— part III: testing and operation

In this third and last part of this article, I will cover preparation, testing, and operation of the facsimile recorder.

Initial alignment will require a frequency counter, a VOM, a logic probe, and a source of video—either a live signal from the receiver, a recorded signal, or the test generator of chapter 7 in the *Weather Satellite Handbook*. In the following sequence of tests, we will gradually add ICs to the board as each stage is tested. In *all* cases the unit should be powered down prior to inserting new integrated circuits. Damage to specific chips can results if you attempt to insert them with the board powered up. Preset the controls as follows:
POWER—OFF
WHITE SET—minimum (max. CCW)
VOC ADJ—midrange
DRUM—OFF
RESET/STANDBY/PRINT—STANDBY

The following checks are associated with the particular chips added to the board as we move along. If problems are encountered at any step, you should check the board wiring around the specific chips, measure the supply voltages on the chips themselves, and try a replacement IC if it seems necessary.

1) Power up and measure the unregulated power supply voltages. You should get about 24-28 V from the LV supply and anything from 250-350 is acceptable on the HV bus. +5 and +12 volts should be obtained at the appropriate main board buses and the POWER lamp should be on.

2) Insert U3 and connect the frequency counter to pin 5 of this IC. Power up and adjust the VCO ADJ control for a reading of 2400 Hz.

3) Insert U4. The logic probe should indicate a high on the collector of Q6.

4) Insert U5 and U6. Connect the probe to pin 6 of U5 and use a test lead to momentarily ground the IC side of R21. The logic probe should indicate a relatively long pulse. Move the probe to pin 6 of U6 and again short the IC side of R21 to ground—a much shorter pulse should be indicated.

5) Insert U7. Press the PHASE switch and the PHASE ERROR lamp should come on and stay on. Use the test lead to ground the IC side of R21, and the PHASE ERROR lamp should go out.

6) Insert U8 and connect the logic probe to pin 8 of U8. With the PHASE ERROR lamp off, the probe should indicate a steady high as the IC side of R21 is grounded with the test lead. Use another clip lead to ground the transistor side of R19. Press the PHASE switch and the PHASE ERROR lamp should come on and stay on even if you ground R21. The probe should indicate a short low each time R21 is grounded. Remove the clip lead from R19—the PHASE ERROR lamp should go out the next time you ground R21 and the probe should indicate a steady logic high from that point on.

7) Insert U9, U10, U11, and U12. The following frequencies should be noted as the counter is moved to the indicated ICs:
U9 (pin 8)—2400 Hz
U10 (pin 12)—240 Hz
U11 (pin 8)—60 Hz
U12 (pin 8)—60 Hz

8) Connect the VOM across the 115-V windings of T202 and set the instrument for ac volts (120-V min.). Turn the drum switch on and advance the DRUM LEVEL control for a reading of 110-115-V ac. The drum should now be rotating away from you as you look at it from the carriage side. Momentarily pressing the MANUAL PHASE switch should cause the drum to slow slightly. It should stop if you keep the switch depressed.

9) With the drum revolving, connect the logic probe to pin 6 of U6 and a steady string of short, high pulses should be noted. If they are not present or are erratic, alter the position of the reed switch until you get a steady pulse indication. Depress and hold the PHASE switch and note the PHASE ERROR lamp. It should be on but should blink off very briefly once for each drum revolution. Release the PHASE switch and the PHASE ERROR lamp should go off at once. Turn off the DRUM switch.

10) Temporarily disconnect the TRAVERSE cable. Set the VOM to dc volts (350 min.) and connect the positive lead to the stylus probe. A reading of 240 V (±10%) should be obtained when the RESET/STANDBY/PRINT is cycled to PRINT. No voltage should be noted with the switch in the RESET or STANDBY position. Return the switch to STANDBY.

11) Connect the TRAVERSE cable and cycle the RESET/STANDBY/PRINT switch to PRINT. The carriage should begin to move away from the traverse motor. If the switch is cycled to RESET, the drive nut should begin to move back toward the traverse motor. Leave the switch in the STANDBY position and unplug the TRAVERSE cable.

12) Connect a source of video to the VIDEO INPUT jack. Unless otherwise noted, all of the following adjustments will be made during the phasing interval preceding picture transmission. This interval is a steady 2400-Hz tone, interrupted by the short phasing pulses. Insert U1 and U2.

13) Temporarily connect a speaker from the negative side of C7 to ground. Advance the WHITE SET control and you should hear an undistorted reproduction of the video signal. As the video level is increased, cycle the RESET/STANDBY/PRINT switch to PRINT and monitor the stylus voltage. (Each time you check the stylus voltage, the switch should be in the PRINT position. Keep it in STANDBY between these measurements to avoid the possibility of a shock hazard.)

14) As the WHITE SET control is advanced, the stylus voltage should gradually decrease and the meter indication should bounce up very slightly with each phasing pulse. Continue to advance the WHITE SET control and you should reach a point —between 25 and 35 volts —where the voltage will drop no lower. Retard the WHITE SET control to the point where you first reach this low-voltage threshold. If you watch the voltage during actual data transmission, it will fluctuate between the low and high voltage limits.

15) Observe the VCO LOCK lamp—it should light whenever video is applied to the input and should remain lighted throughout a frame transmission.

16) Connect the logic probe to the collector of Q6 and adjust R14 for a steady stream of logic highs during the phasing interval.

17) Turn the drum on and press the PHASE switch at the completion of the start tone. The PHASE ERROR lamp will come on and you may be able to hear a slight difference in the sound of the drum motor, indicating that it has slowed slightly. The lamp should go off sometime within about 15 seconds, depending upon the initial phase error.

At this point, all the major systems have been checked out. The last remaining step is to prepare the wire stylus and condition it. Cut one of the wires from a wire brush (one intended for use in an electric drill) and straighten it with a pair of needle-nosed pliers. The wire need not be completely straight, as some remaining curvature will assist in holding it in the stylus holder. Insert the wire into the protruding stylus tubing and trim the end so that it extends about 1/16" out of the end of the tube. Wrap a piece of fine emery paper around the drum and secure it with transparent tape. Rotate the stylus assembly such that the wire contacts the emery paper, and observe the orientation of the wire. If it is tilted slightly, it should be tilted in the direction of drum movement—that is, it should point toward the back of the drum. If it points toward the front of the drum, remove the wire and reinsert it so that it is tilted in the proper direction. Turn the drum and allow the stylus to run in contact with the rotating emery paper for a period of 30 seconds or so. The end of the wire will be quite rough initially, but you should be able to hear a considerable difference in sound as it smoothes out under the abrasive action of the paper. Remove the emery paper and prepare for the moment you have been waiting for—your first picture!

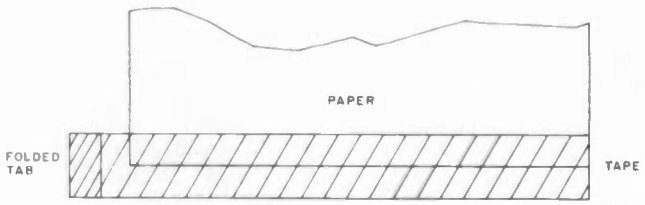

Fig. 1. Paper preparation and manipulation. The tape is placed along one edge of the paper as shown. The opposite edge is then inserted under the aluminum foil strip on the drum and the drum is rotated to wrap the paper around the drum. The edge of the paper with the tape will then completely overlap the foil strip and the tape can be smoothed down to secure the paper to the drum. Removal of the paper is accomplished by lifting the small tab at the end of the tape strip and carefully peeling the tape away from the paper surface. A strip of tape can be reused several times if handled carefully.

Operation

Three different papers have been used to date, all of which work quite well, although there are some advantages to one over the others. The preferred paper is that manufactured by Xerox® for their Telecopier™ office facsimile machines. Contact the nearest Xerox office and request reorder number 3R830. The paper is 8.5" × 11" and comes in packages of 150 and 500 sheets. The cost is lower in 500-sheet lots, and you can save still more by ordering two boxes of 500 sheets at one time.

A paper equal to the Xerox is Timefax NDK, manufactured by Fitchburg Coated Paper Products of Scranton PA. The main difficulty is getting Fitchburg to supply the paper in small lots. They have yet to prove the least bit cooperative, and the Xerox paper is much easier to obtain. If you can get the Timefax NDK, it will do an excellent job.

3M, Inc., of Minneapolis MN makes a similar paper for its line of office fax machines, and the price is in line with that of Xerox. While it will do a good job, I have found the 3M paper to be somewhat smokey in operation and it doesn't seem to yield as nice a gray scale as the Xerox paper despite the claims of the sales reps. It is quite possible that it functions best at a slightly lower maximum printing voltage, so I wouldn't say to avoid it if it is the easiest paper for you to obtain. You might try substituting a 100-V zener for D5 to bring the printing voltage down to 220-V maximum if you plan to use the 3M paper.

All of the papers come in the standard 8.5" × 11" size and must be cut down to 7" × 7" for use on the recorder. A small office paper cutter set up with wooden stops is the fastest way to cut the paper to size. With a good cutter, you can slice up to 10 sheets at a time.

Loading the Paper. The printing side of the paper is the smooth white surface —the back looks slightly mottled and is a little rougher in texture. Lay the piece of paper—printing side up—on a table and strip off a piece of transparent tape (the high-quality translucent variety is best) about 7.5" long. Fold over one end to make a little tab so that you can strip

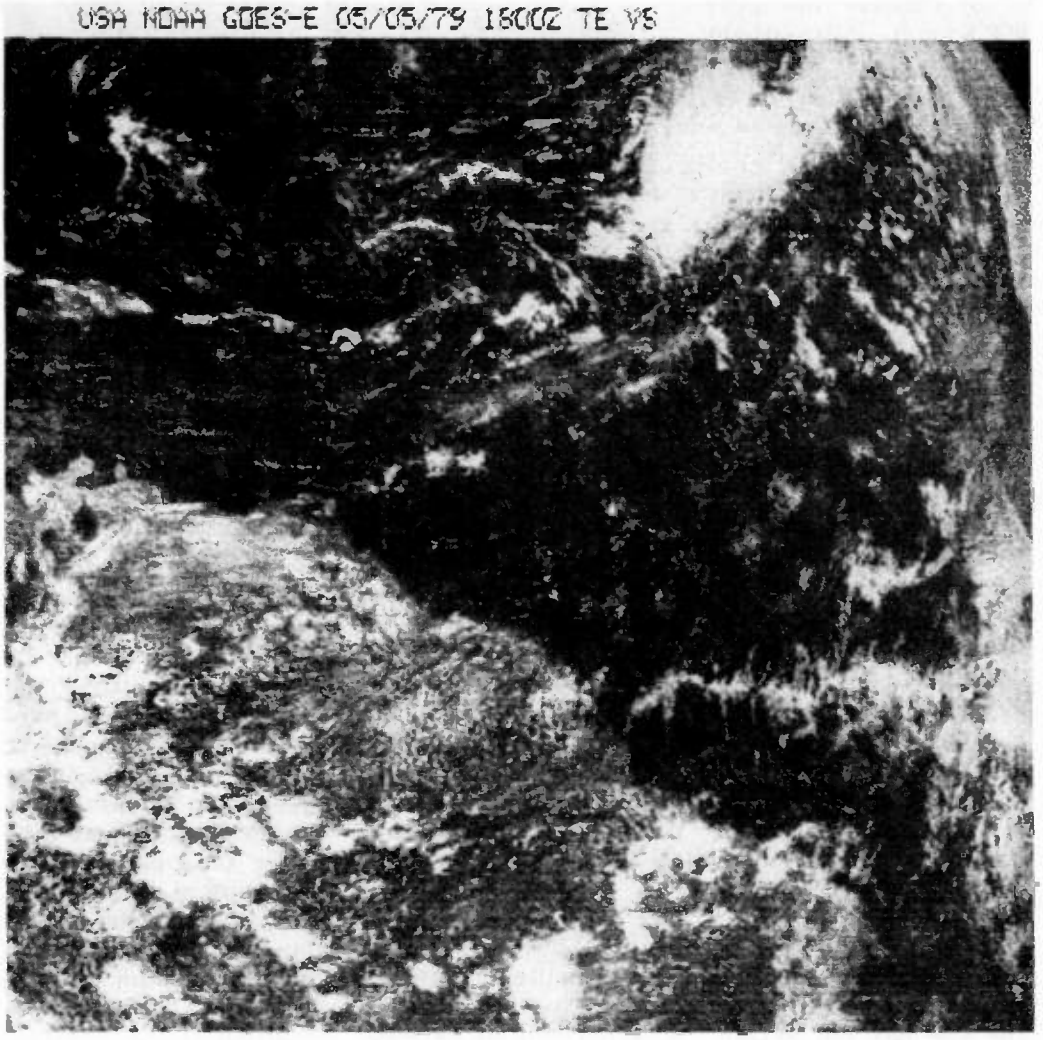

Fig. 2. An example, from a GOES E Tropical East quad, of the excellent resolution obtained with the FX-2E direct-printing recorder. These fine cloud details could be resolved with a photographic system, but extreme care in focusing the light gun would be required. The direct-printing option, because a wire stylus is used, always yields optimum resolution without the need to worry about focusing the system.

the tape off later. Lay the tape over one edge of the paper as indicated in Fig. 1.

Cycle the RESET/STANDBY/PRINT switch to RESET until the drive nut reaches the right end of the drive rod. Slide the edge of the paper opposite the tape under the folded strip of foil and, holding the paper against the drum with your fingers, rotate the drum away from you, wrapping the paper around the drum. When you get all the way around, the paper should overlap the foil strip and you can smooth down the tape to secure the paper to the drum.

Position the carriage so that the stylus rests just inside the right margin of the paper. Remove the stylus from the paper and cycle the switch to PRINT. The drive nut will move back toward the carriage. Guide the brad over the base of the carriage and cycle the switch to STANDBY when the drive nut starts to move the carriage. Rotate the stylus assembly to place the stylus back on the paper and you are ready to go.

Printing. When the GOES carrier comes on, turn on the drum. At the completion of the start tone, press the PHASE switch. Sometime within about 15 seconds of this action the PHASE ERROR lamp should go off, indicating the drum is in phase with the incoming signal. Twenty seconds after the end of the start tone, cycle the RESET/STANDBY/PRINT switch to PRINT. When the frame starts, you should be able to see the effect on the drum as the stylus moves along. When the stop tone arrives, cycle to STANDBY, stop the drum, remove the stylus, and take off your picture by carefully stripping off the strip of tape. If you put the tape carefully aside, you can use it for quite a few prints.

Optimizing. If this is your first print, it is not likely to be perfect—it probably will be too light. To optimize the WHITE SET control, start the printing during the phasing interval and carefully watch the paper as you back off the WHITE SET control. The optimum setting is where you can just see the slightest darkening of the surface at the printing stylus.

The reset procedure can be shortened somewhat by locating the proper start position for the carriage and running the drive nut up against the carriage as noted. Slide the carriage away from the nut and use india ink to mark the glass where the brad contacts it. In the future when you reset the drive nut, simply run it back to the mark you have made and then you can move the carriage up against it, knowing that the stylus is properly located.

Operation with TIROS/ NOAA or METEOR Imagery

A triggered oscilloscope is used to phase the incoming picture when the FX-2E is used to display pictures from polar-orbiting spacecraft. Connect the TRIGGER jack to the scope trigger input and the VIDEO OUT jack to the scope vertical input. What you will get is a video waveform display triggered by the fax drum. With a little experience, you will be able to recognize the position of the line sync pulses on the scope display. Set the recorder up as described and when the signal is solidly out of the noise and with the drum running, simply press the MANUAL PHASE switch in short bursts until the line sync pulse is aligned with the left edge of the scope display. At this point, the RESET/STANDBY/PRINT switch can be cycled to PRINT until the carriage reaches its limit of travel.

Alternatively, if you have built the CRT monitor of chapter 4 of the *Weather Satellite Handbook*, you can use it for phasing display. Connect the video input to the monitor in parallel with that of the fax and

lift the diode connected to point B in Figure 4.6 of the *Handbook*. Connect the TRIGGER output to this point, and the monitor display will now trigger from the fax drum. In practice, it is easiest to install an EXTERNAL TRIGGER jack to the back of the monitor, connected to the TRIGGER output of the FX-2E. An SPST toggle switch (INTERNAL/EXTERNAL TRIGGER) can then be added so that you have switch-selection of either internal or external triggering. The internal position is used for normal monitor operation or when the fax drum is not running (saving wear and tear on the horizontal deflection transistors), while the external position is used to manually display and phase the fax. To use the monitor in this fashion, you should reset the fax carriage and load paper as instructed. Start the drum, and switch the monitor to EXTERNAL TRIGGER. When the signal is out of the noise, you can start the monitor sweep and operate the MANUAL PHASE switch of the FX-2E to move the line sync pulse (either visible or IR) to the left edge of the viewing area. At that point, you can start the fax printing.

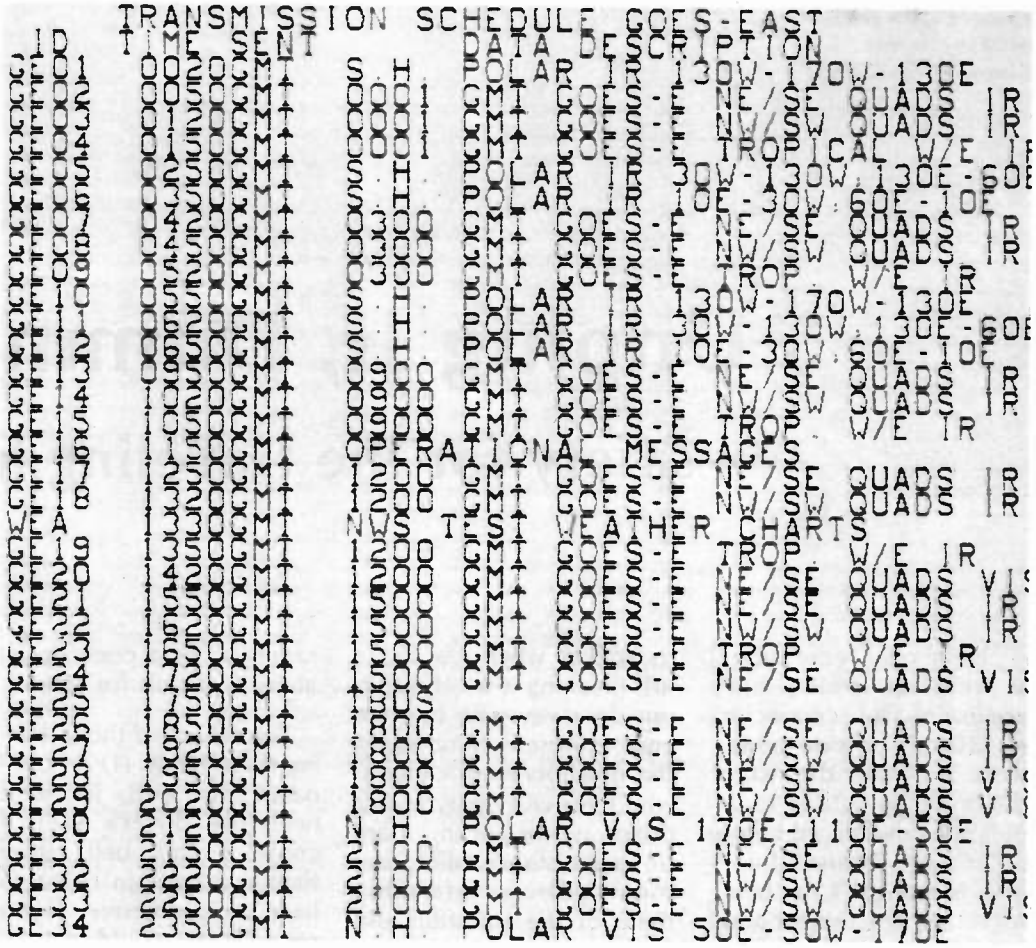

Fig. 3. Direct-printing readout of a GOES E operational message, showing the excellent printing clarity which is obtained.

Operation as a Photographic Facsimile Recorder

The only electronic changes for photofax operation include the following:

1) Delete R9, R10, D5, D6, Q2, and R11.

2) Replace R8 with a 100-Ohm pot, which will serve as a BLACK SET control.

3) Add a 15-mA meter in the switched 300-V line.

4) Connect an R1130B glow modulator tube from the collector of Q1 to the 350-V bus, with the 15-mA meter in series. Rewire S201A so that the lamp is energized (connected to the 350-V line) with the switch in the PRINT position.

5) Reverse the diodes (D1-D4) in the detector, delete R7, and replace it with a 2200-Ohm resistor connected between the base of Q1 and the +12-V bus.

Refer to either the first edition of the *Weather Satellite Handbook* or the September and October, 1975, issues of *73* for construction of the light gun and its mounting to the carriage. The phase-sensor reed switch will have to be reoriented so that it closes just as the edge of the photographic paper passes the light gun lens.

With no video input, adjust R8 (BLACK SET) for a meter reading of 15 mA with S201 in the PRINT position. Full video drive (white level) should then be applied and the WHITE SET control adjusted for a reading of about 1 mA. Resin-coated enlarging papers are recommended for printing, with Kodak Kodabrome RC being preferred (normal contrast grade). Black and white level adjustment should be altered in practice to produce good prints when the paper is processed for 2 minutes in Kodak Dektol developer. Any commercial fixer may be used, and you should consult your local photographic supplier for trays, chemicals, safelights, etc. The aluminum foil strips and ground connections will not be required on the drum and can be omitted. When used in the photofax mode, the recorder must be operated in a darkroom with suitable safelight illumination to protect unexposed paper. The paper can be cut to the required 7" × 7" in the darkroom.

Although the recorder will produce superb photographic prints, I have not operated it in the photographic mode since first setting up the direct-printing version (see Figs. 2 and 3). The fax system is certainly somewhat more complicated a project than a CRT monitor, primarily due to the mechanical aspects of the project. Once finished, however, it should give you years of trouble-free service. The prototype of the photographic facsimile version has been in operation for over two years without a single problem, and there is no reason to assume that the direct-printing version will not have the same reliability. The FX-2E system is virtually ideal in that it provides for easy operation, low operating costs, immediate availability of good-sized prints, superb resolution, and photographic image quality. ■

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Unplug It, Dummy!

—safety for the traveling ham

For those recreational vehicles which have provisions for connecting to 110-volt outside power, there is always the risk of the owner forgetting to unplug the power cord before driving off. Human frailty and Murphy's Law being what they are, this is bound to happen sooner or later.

For us, the reckoning came one time when we had our camper van parked in our driveway while we were packing for a trip. We had the cord plugged into our house power for precooling the refrigerator. Getting off later than we had hoped, we took off in a hurry. When we got to our first stop, we were horrified to find the socket from our extension cord sitting in the van power receptacle. The cord had pulled right out of its socket when we drove off, meaning it was lying in our driveway with the live ends exposed. Mindful of the neighborhood children who frequently play in our driveway, we put in a frantic long-distance call to our local police, informing them of the situation and asking them to do something about the hazard. Fortunately, no further harm came of it.

To preclude any repetition of this fiasco, I installed a cord alarm in our van. It is arranged so that a door bell rings if the ignition is turned on while the cord is plugged in. You can install such an alarm in your RV for an expenditure of about $15 for parts—less than the cost of a power cord that might be ruined by a drive-off. It does the same job as a commercial alarm that sells for $50.

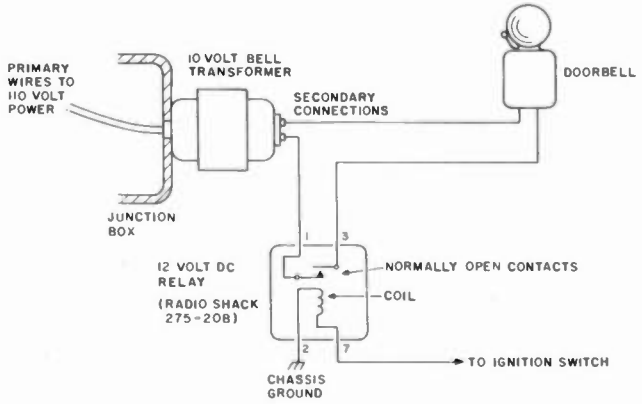

Fig. 1. Wiring diagram of the cord alarm.

You will need the following three items: (1) An ordinary door bell, installed near the driver's seat. I chose a door bell rather than a buzzer in order to have a distinctive alarm sound that would not be confused with the seat-belt warning buzzer. (2) A bell transformer of the type designed to mount in a knockout hole in a junction box. Be sure to get a 10-volt transformer rather than a 16-volt type, which is for chimes. (3) A 12-volt dc relay (Radio Shack #275-208 or equivalent).

Attach the bell transformer to an unused knockout hole in the power control center or the junction box for the outside power receptacle. (Confinement of the 110-volt wiring to the inside of such a box makes for a very safe installation.) Connect the primary wires to the 110-volt power at the point where it enters the vehicle, with no circuit breakers or other switching devices intervening so that the alarm will not fail to operate because of a breaker or switch being turned off. (Protection against short circuits in the transformer is given by the circuit breaker feeding the outlet into which the cord is plugged.)

Make a bracket for the relay socket out of sheet metal or aluminum angle and mount the relay in a convenient location. Wire up the system as shown in Fig. 1, soldering all connections to the relay socket. The transformer is connected to the bell in series with a pair of normally-open contacts on the relay. One end of the relay coil is connected to chassis ground, and the other end is connected to a circuit that is energized when the ignition is turned on. Pick a circuit that is energized only in the "ignition" position of the switch, and not the "accessory" position. For our Econoline van, a convenient connection point was the wire feeding power to the seat-belt warning system.

With these connections, turning on the ignition operates the relay and completes the circuit from the transformer to the bell so that it will ring if the transformer is powered by the cord being plugged in.

What if you remember to unplug the cord but forget to stow it? This alarm is foolproof but it is not claimed to be *damn*-foolproof! ■

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Power Plus for the Omni

— improving on Ten-Tec's power supply

The Ten-Tec Omni (#252-MO) power supply is a fine unit, but there are some improvements that can be made. I am sure competition dictates just how much a manufacturer can put into a piece of equipment, but there is no reason ham operators cannot make a few usable modifications themselves. The modifications I made were relatively simple, and I now have a better and more useful power supply.

My first modification was to install a chassis-mounted ac receptacle to be powered whenever the power switch is turned on. This provides a switched source for a cooling fan. By doing this, my cooling fan is on any time that my power supply is on and I cannot forget to turn it on (see Fig. 1).

My next undertaking was to install an overvoltage protection (crowbar) circuit. This is a must to protect expensive gear from being zapped should a pass transistor become shorted and allow excessive high voltage to reach places it should not! The crowbar circuit described in the August issue of *73 Magazine* (page 90) by K9MLD was used. (See Fig. 2). All of the components were mounted on a three-lug terminal strip with the exception of the 25-Amp SCR, which was mounted on a bracket of its own. Space is no problem. I used a 2N685 SCR which must be isolated from ground, as the stud is the positive terminal. Fuse installation is very simple. With a fuse holder mounted on the back cover of the power supply near the top edge, the red wire from the pass transistor can be cut near the center and connected to the fuse holder without disconnecting either end of the wire.

With this circuit connected to the 13.8 positive voltage line, should the SCR be gated by an overvoltage signal, the SCR will short the 13.8 positive voltage line to ground and blow the fuse, thereby positively disconnecting the output of the power supply. Should you have a variable power source available, the trimpot can be adjusted to gate the SCR at 15 V and marked at that position. After installation in the power supply, the trimpot can be turned to test for proper operation, and when testing is completed, returned to the marked (15-V) position. During checkout, the current limiter (not the fuse) was shutting down the power supply inadvertently. This apparently was being caused by rf getting on the gate of the SCR, causing the SCR to conduct. The installation of the two .01 caps corrected this problem (see Fig. 2).

There was no reason to have two 12-volt power supplies in my shack (one for my Omni and the other for other equipment such as the 2m rig), so I set out to eliminate the home-brew job and use the Ten-Tec #252MO for everything.

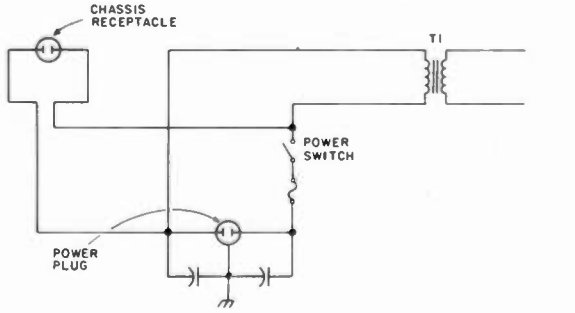

Fig. 1.

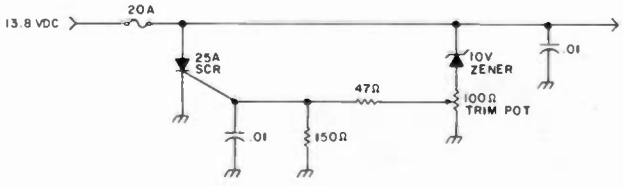

Fig. 2.

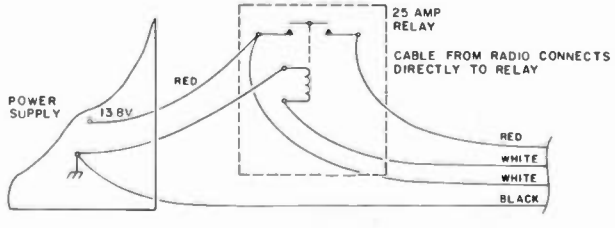

Fig. 3.

The manufacturer designed it to be turned on by the power switch on the Omni in series with the on/off switch on the front of the power supply. The power supply could not be turned on and used without the Omni being turned on as well. A simple rearrangement of the 115-V ac wiring in the power supply bypassed the switch on the radio and allowed the power supply to be turned on by the switch on the power supply only (see Fig. 1).

To control the 13.8 V dc to the Omni, a 25-Amp Potter & Brumfield #PR5DY relay was installed, as suggested in the owner's manual. The relay coil is controlled by the switch on the Omni through the two center wires of the cable between the power supply and the radio. Now my Ten-Tec power supply can be turned on without turning the Omni on (see Fig. 3).

Note: To facilitate mounting the relay, the two auxiliary phono jacks and their associated wiring were removed and discarded, and two banana plug type jacks were installed in the front panel, with wiring capable of handling the total output of the power supply. This makes 13.8 V dc readily available for anything in the shack with current limiting and overvoltage protection.

So, Ten-Tec owners, if you are of the mind to do a little improving of your equipment, the details are left to your discretion, imagination, and ingenuity. I might add that the #252M and #252MO are identical electrically, so these modifications apply to both. The peace of mind that comes from having the overvoltage protection is reward enough, not to mention the good feeling of knowing that I did it myself! 73. ■

Reader Service—see page 194

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Oddball Offsets for the KDK-2015R

— make a good rig better

Did you ever wish you could program any offset into the 2015R? If so, read on. Here is a cheap ($0-$5, depending on your junk box) modification which will do just that, without drilling any holes or installing any extra switches. The KDK has all you need and even has the correct labels on one of the switches. The offset frequency can be programmed into the memory in the normal manner, and the KDK will display transmit and receive frequencies when the PTT switch is operated. It does not interfere with the normal function of the memory scanner, either.

All of the tools that are needed to do the job are a small soldering iron, a Phillips screwdriver, dikes, and perhaps a pair of tweezers or hemostats. The only materials needed are an SPDT reed relay with a 10-V coil, two diodes, some hookup wire, and solder.

Study the diagram (Fig. 1) so that you will understand the hookup and proceed as follows:

1. Remove the four screws from the case and remove both halves.

2. Turn the rig on its back with the antenna connection facing you.

3. Locate SW8 (Fig. 2) and lift the yellow wire from tab "A". Insulate the end with spaghetti.

4. Solder a diode between the tab marked "A" and the tab marked "SIM"; observe polarity.

5. Solder a piece of hookup wire to the tab marked "A". The length of the hookup wires will depend on the make of switch you use and where you locate it. This is all of the work to be done on SW8.

6. Locate SW6 (Fig. 3) and lift the violet wire from the tab marked "COM".

7. Solder a piece of hookup wire to the violet wire and cover the splice with spaghetti.

8. Solder a piece of hookup wire to the tab marked "4". This is a tight place; be careful not to melt any wires.

9. Select the place to install the reed relay. I put mine on the rear side of the CONT-2010 board on the

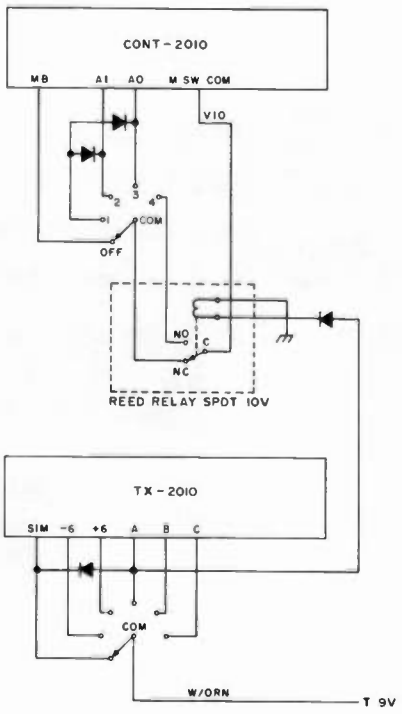

Fig. 1.

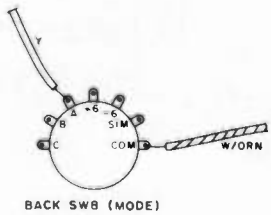

Fig. 2.

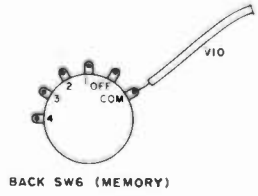

Fig. 3.

left-hand end in front of L6 and L7 on the PLL-2010 board, with the connections pointing up. It can be fixed in place with Silastic™.

10. Place a solder lug under the front-left corner screw on the PLL-2010 board.

11. Solder a piece of hookup wire to the solder lug.

12. Solder the other end of this wire to one side of the relay coil.

13. Solder a diode to the other end of the relay coil. Observe polarity.

14. Solder a wire from SW8, tab "A" (step 5) to this diode.

15. Solder the extension of the violet wire (step 7) to the common terminal of the relay.

16. Solder a piece of hookup wire to SW6, tab "COM" (step 6) and solder the other end to the NC contact of the relay.

17. Solder the wire from SW6, tab 4 (step 8) to the NO contact of the relay. This completes the modification. Be sure that none of the connections will touch the case. Check your wiring and install the case halves.

To operate, program the transmit frequency into the number 4 memory in the normal manner. Set the receive frequency on the vfo. Place the mode switch in the "A" position. Place the memory switch in the OFF position.

Now for the moment of truth. Press the mike button and, presto, the transmit frequency programmed into the number 4 memory is displayed. Release the button and the receive frequency in the vfo is displayed.

This modification works well, costs about the same as one offset crystal, takes about an hour of your time, and is fairly easy to do. Have fun! ■

↙ Reader Service—see page 194

The Strange Predicament of Walter Hann

—OE8WHK did the right thing— and suffered the consequences

Robert B. Grove WA4PYQ
Grove Enterprises, Inc.
Rt. 1, Box 156
Brasstown NC 28902

Walter Hann OE8WHK, prosecuted after rendering life-saving communications assistance.

It was a foggy Monday, August 13, 1979, when Walter Hann OE8WHK switched on his Bearcat 101 scanner. Immediately, the scanner locked onto a local police channel and Hann learned of a frantic rescue attempt being conducted in the picturesque Austrian Alps a few miles from his home.

But the communications was by no means routine. A local ham radio operator, OE8PPK, was unwittingly causing interference on a nearby amateur frequency, preventing the police from making radio contact with the rescue helicopter hovering nearby, desperately searching for the injured victim.

A small segment of Walter Hann's listening post.

Walter Hann grabbed the microphone of his two-meter Icom IC-215 and immediately called OE8PPK to urge him to QRT so that the rescue mission could proceed. The other ham dutifully complied, thanking Hann over the air for alerting him.

This initial episode was the very essence of amateur radio at its best: A ham radio operator, aware of a life-saving attempt being threatened by a communications problem, takes immediate action to solve the interference problem. Unfortunately, the story did not end there, for in Austria it is illegal to possess a radio capable of monitoring police calls.

The interfering transmissions of OE8PPK had been tape-recorded by the police for follow-up, and now they heard Walter Hann's name and callsign being announced by the involuntary intruder.

Because Hann is an employee of the Austrian government, identification came quickly. Officials rapidly made the 20-km journey from Klagenfurt to St. Veit/Glan, Hann's QTH, and there confronted his wife.

Although Hann was no longer at home, the PTT officials demanded access to the ham shack where they siezed the Bearcat and made note of all other equipment owned by Hann.

The next day Hann was summoned to Klagenfurt for a three-hour interrogation. His inquisitors wanted to know where he got the equipment, how it cleared customs, who else had such equipment, and other details about his monitoring hobby.

Since Hann is employed by the government, he was dealt with harshly. He was forced to forfeit the Bearcat receiver and pay a steep

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- Four simplex/repeater memory channels, plus receive-only memory channel.
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- Built-in 1800 Hz tone generator.
- Priority channel with search-back feature.
- Pause feature that holds, then restarts scan, on busy or clear channels.
- Digital display of last four digits of operating frequency.
- Single Control Head may be used for operation on both 440 MHz and 2 meters via optional switching box and remote cables.
- Extremely compact size, light weight.

FT-720RVH	Specifications	FT-720RU
144.00-147.99 MHz	Frequency Coverage	440.00-449.975 MHz
10 kHz	Synthesizer Steps	25 kHz
25 watts	Power Output	10 watts
32 uV for 20 dB quieting	Sensitivity	0.5 uV for 20 dB quieting
±6 kHz (—6dB) ±12 kHz (—60 dB)	Selectivity	±12 kHz (—6dB) ±24 kHz (—60 dB)

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fine. But that wasn't all. In November, two Customs investigators came to his office and conducted a lengthy hearing. How did the BC-101 get into Austria? How much did he pay? Who else owns similar equipment? How was his ham equipment brought into the country?

Hann owned a Drake R-4B, an SPR-4, and an FS-4 synthesizer, a Barlow-Wadley SCR-30, a HAL RVD-1002 RTTY demodulator, a Collins 51J3 receiver, and many other pieces of gear. The officious officials pointed out that unless Hann could produce legal proof of customs clearance, they would conclude that all the equipment had been smuggled into Austria.

Since Customs officials could not determine that Hann had used the equipment in the commission of an illegal act, he was not imprisoned. But he has been assessed heavy fees for additional duties, fined for the act of listening to a private communication, and is now awaiting additional disciplinary action because of his government position with the Austrian Finance Administration (Customs). This action will probably be both verbal and punitive, and Hann expects his salary to be cut.

Investigators then intruded into Hann's private papers, looking for evidence of illegal activities, confiscating a letter from an American collegue who offered to send him a Bearcat 250 scanner.

Post- und Telegraphendirektion für Kärnten in Klagenfurt als

Fernmelde[illegible]e I. Instanz

Zustellung zu eigenen Handen

9020 Klagenfurt, Sterneckstraße 19

(Behörde)

GZ. 24915-3/79 Klagenfurt, am 29. August 1979

An Herrn Walter HANN, Finanzbeamter,

Neubaugasse 23

9300 St.Veit a.d.Glan

Beschuldigten-Ladungsbescheid

Es wird Ihnen zur Last gelegt, in der Zeit von 2. Juni 1979 bis 13. August 1979 in St.Veit an der Glan eine Funkempfangsanlage, welche zum Empfang von nicht für die Allgemeinheit bestimmten Aussendungen geeignet ist, ohne fernmeldebehördliche Bewilligung verwahrt, errichtet und betrieben

und dadurch eine Verwaltungsübertretung nach § 26 des Fernmeldegesetzes, BGBl. Nr. 170/1949, begangen zu haben.

Gemäß § 40 Abs. 2 und § 41 des Verwaltungsstrafgesetzes werden Sie aufgefordert, unter Mitnahme dieses Ladungsbescheides und

zur Vernehmung — mündlichen Verhandlung —

am Mittwoch, den 12.9. 1979, 9.00 Uhr

bei diesem Amte, II. Stock, Zimmer Nr. 132

beim Amtstag in persönlich zu erscheinen oder einen mit der Sachlage vertrauten und schriftlich bevollmächtigten eigenberechtigten Vertreter zu entsenden. Die Vollmacht ist stempelpflichtig.

Gleichzeitig werden Sie aufgefordert, die Ihrer Verteidigung dienlichen Beweismittel mitzubringen oder diesem Amte so zeitlich anzuzeigen, daß sie zur Vernehmung herbeigeschafft werden können.

Im Falle ungerechtfertigten Ausbleibens

wird gemäß § 41 Abs. 3 des Verwaltungsstrafgesetzes das Strafverfahren ohne Ihre Anhörung durchgeführt werden.

Sie haben gemäß § 19 Abs. 3 des Allgemeinen Verwaltungsverfahrensgesetzes Ihre zwangsweise Vorführung zu gewärtigen.

Gegen diesen Bescheid ist zufolge § 19 Abs. 4 des Allgemeinen Verwaltungsverfahrensgesetzes kein Rechtsmittel zulässig.

Für den Präsidenten:

(Unterschrift)

Post- und Telegraphendirektion für Kärnten in Klagenfurt als Fernmeldebehörde I. Instanz

Formular 30 zu § 41 VStG. (Beschuldigten-Ladungsbescheid für Behörden, die zugleich Vollstreckungsbehörden sind.)

VwV. 1—2011. BMZl. 79.349-4/68. — Österreichische Staatsdruckerei. L0010959

Official summons served by the Austrian PTT.

Investigators intruded into Hann's private papers, looking for evidence of illegal activities, confiscating a letter from an American collegue who offered to send him a Bearcat 250 scanner.

In the United States, any citizen is permitted by law (Section 605, 1934 Communications Act) to monitor for his own personal interest any radio communication of any nature, just as long as he does not disclose the contents to another person or use the information for his own personal gain.

But an unsettling spectre has appeared on the horizon. A number of new interpretations, prospective amendments, and even an entire rewrite of the Communications Act threaten to undermine the American privilege of listening in.

The catalyst for these actions has been the common-carrier television industry, disturbed because of the prospect of home TV viewers picking up satellite programs direct without having to pay subscriber fees. Law enforcement agencies are also concerned about the use of scanners to evade apprehension. Several bills are now on the floor of Congress intended to limit our constitutional right to listen.

Will it be the conscientious amateur community who will protest the implementation of these restrictions on our rights? Only you can answer that question. ■

Put "the Rep" in Your Repeater

— an automatic autopatch dialer

O.C. Stafford K4ALS
3702 Holts Chapel Rd.
Greensboro NC 27401

Continuing changes and interpretations of FCC rules indicate that autopatch facilities attached to amateur repeater stations must be monitored to prevent the abuse of the autopatch.

Because of these requirements and other restrictions, numbers of clubs have discontinued the use of their autopatch facilities or else now have a very limited operation. Some clubs have disintegrated over the issue of autopatches. One solution, however, is to use a control operator to monitor the calls.

One of the big problems facing owners of repeaters equipped with autopatch is the ability to control the numbers being dialed. Another problem is that some people make calls which are not really legal or are not in the best interests of ham radio. Now you can control what gets dialed, with the Rep.

The circuit described in this article makes use of the repertory dialer chip, the MK5170, made by Mostek. The chip is a 3870 microcomputer that has been programmed to act as a repertory dialer. The pin connections diagram is shown in Fig. 1. The unit can be programmed with only approved phone numbers for later dialing.

The chip can be addressed by a touchtone™ pad in a minimum-hardware configuration. It will store up to 100 phone numbers which can be loaded and retrieved with a two-digit access code. The circuit diagram for the 100-number system is shown in Fig. 2. If a system with 24 numbers or fewer is needed, the memory circuit of Fig. 3 can be used.

I have tried to include enough hardware and logic on the board to make the circuit easier to interface with systems other than the Buffington phone patch and control system which has been described in past issues of *73 Magazine*.[2] That system will be used to show how the unit can be interfaced.

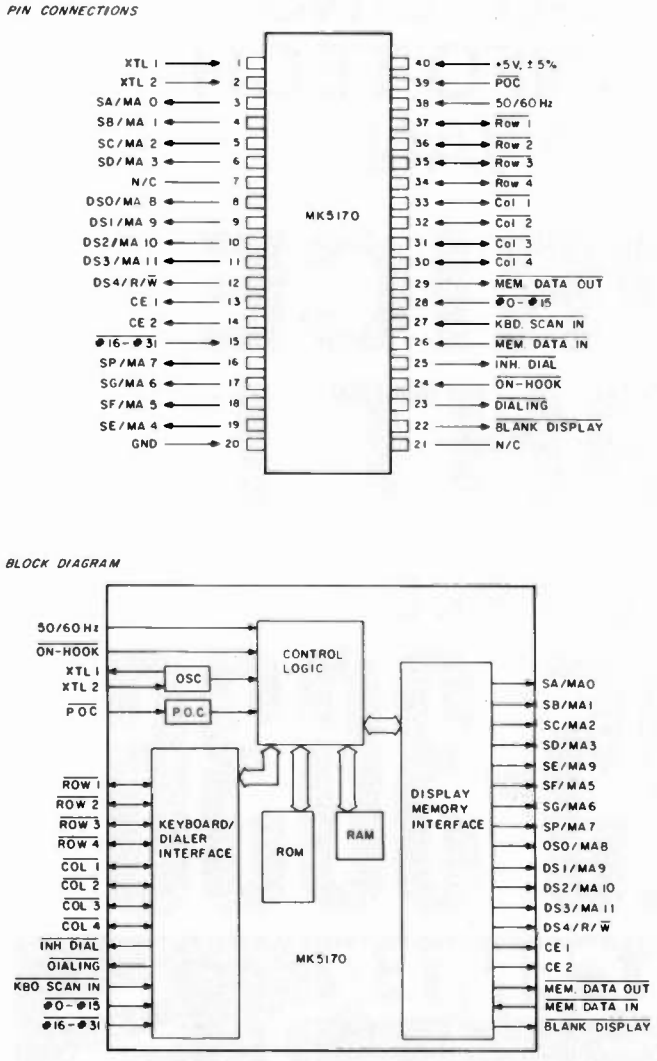


Fig. 1. Pin connections and block diagram.

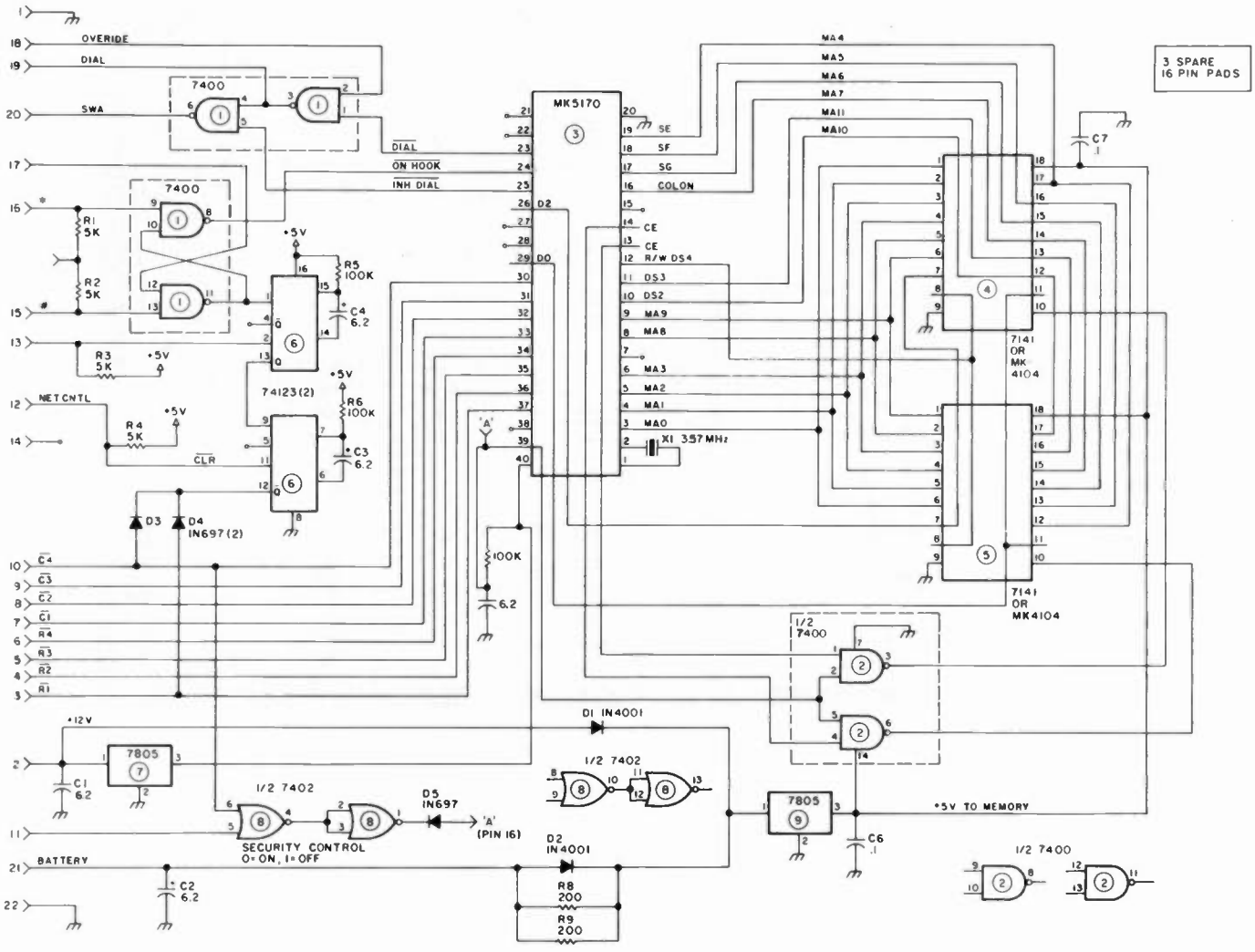


Fig. 2. Circuit diagram for the 100-number system.

There are three control pins which define the mode of operation: Pin 23 indicates that a dialing cycle is in progress by going low, pin 24 (if low) indicates that the phone is on hook, and pin 25 goes low during data entry and is used to inhibit the dialer circuit.

Fig. 4 shows how the unit is connected to the autopatch and control system described by Buffington. The unit operates in the Dial mode when accessed by a user and in the Enter mode when accessed by a control station. Fig. 5 shows the actual hardware hookup. Fig. 6 shows the switch circuit that is used to route data between the decoder, the dialer, and the Rep.

To access the Rep, the user must use the following sequence:

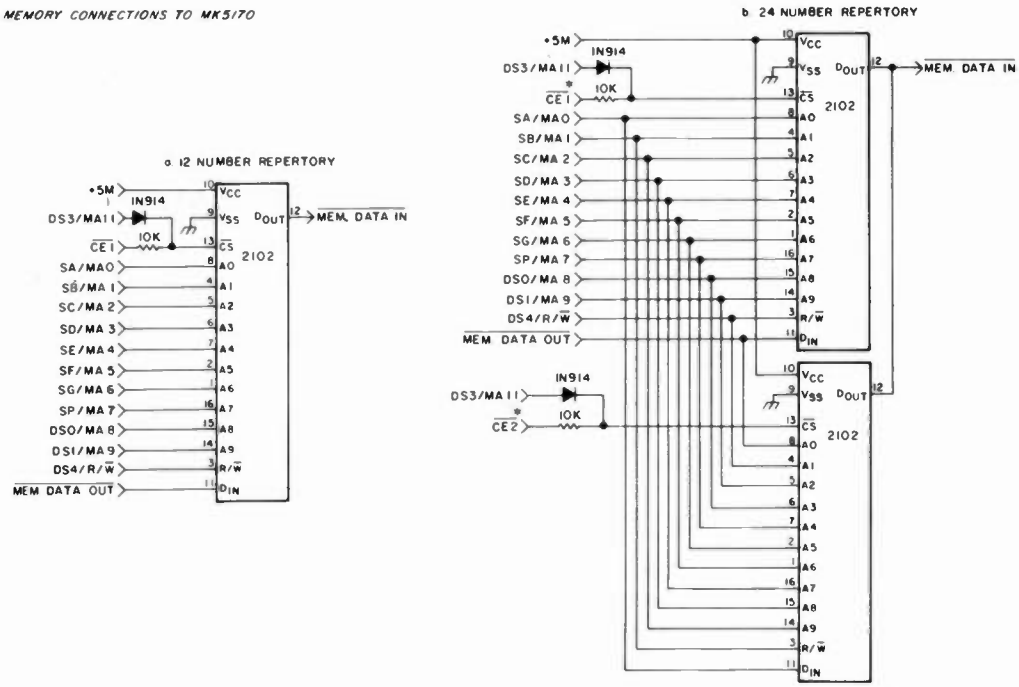
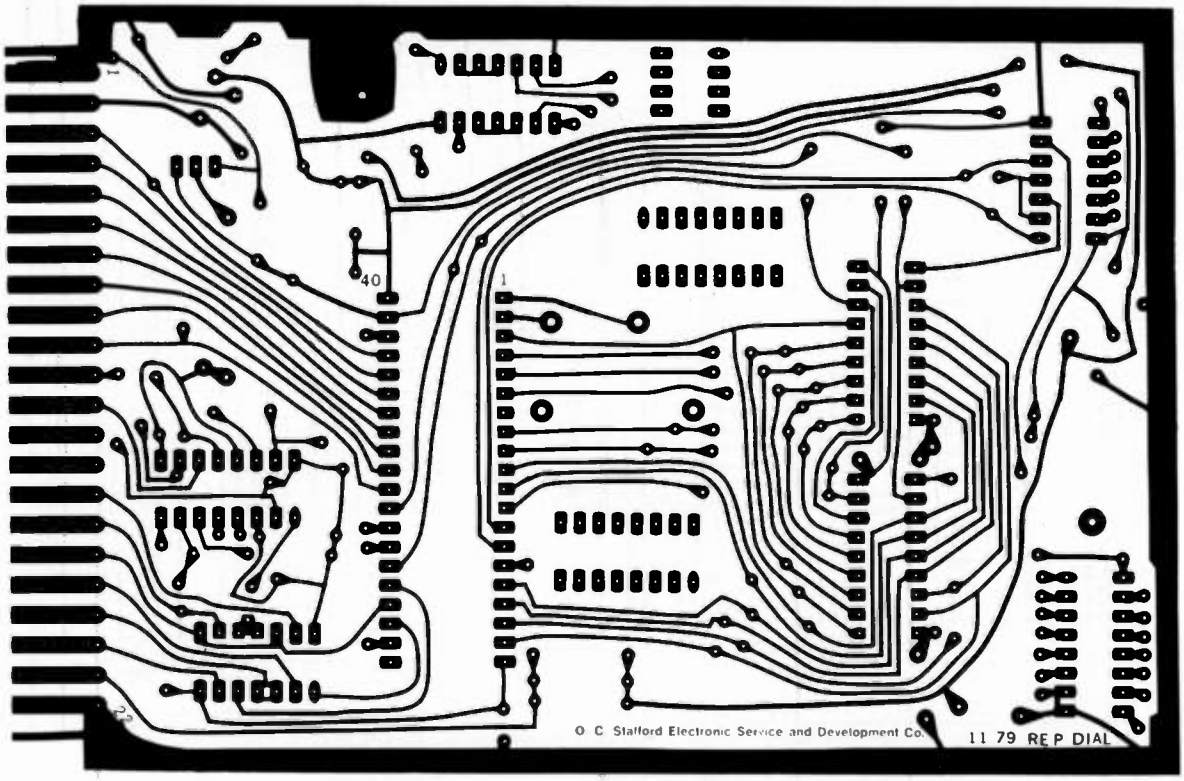
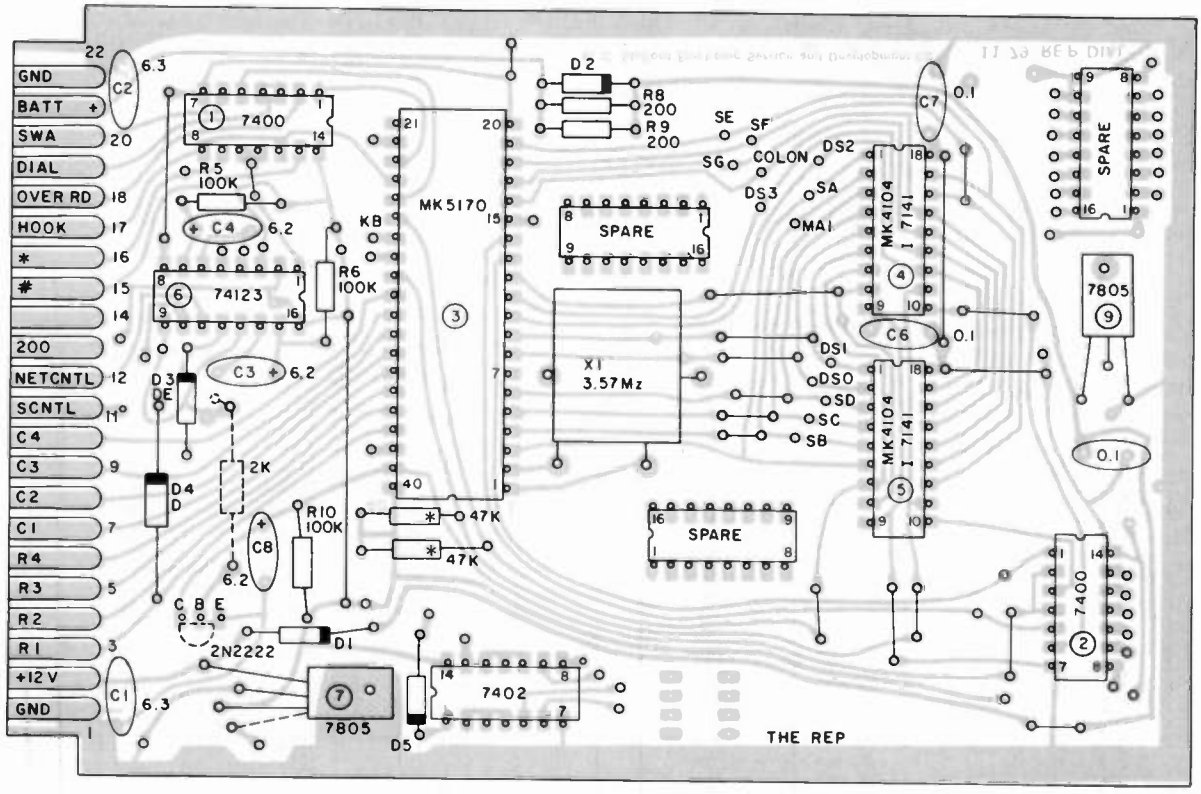


Fig. 3. Memory circuit for a 24-number (or fewer) system. It can be built on header chip and attached to the 18-pin socket.



PC board for the repertory dialer.



Component layout for repertory dialer.

1. Identify and state your intention to make a call. (This is good operating procedure any way you look at it.)

2. Enter *. This causes the demux circuit to lock out for 20 seconds, connects the dialer to the phone line, starts the three-minute timer, and readies the Rep to look for two numeric digits.

3. Wait for the dial tone, then enter the two digits.

4. The phone number associated with the two digits will be retrieved, and pin 20 will go low while pin 12 goes high, causing the decoder circuit to disconnect and the dialer to be connected to the Rep. The number is then transmitted to the dialer from the Rep. It takes 980 milliseconds for a seven-digit number to be transferred to the dialer with a 3.57-MHz clock.

5. Once the call is completed, send # to knock the patch down and reset the Rep.

The system has some built-in security. A 4×4 touchtone pad is used to access the unit for loading. The pad is shown in Fig. 7. The security function will not allow the user to get into the Enter mode when the phone is off hook. The Enter is sent when the security lock is on; the Rep simply resets. The lock and unlock sequence code should be known only to the control station, and is controlled by the demux/sequence circuit.

The demux and sequence boards are needed if the phone numbers are to be loaded from a remote location, as shown in Fig. 5.

The control station uses the sequence circuit to unlock the system for programming. Programming is accomplished using the following sequence:

1. The control station generates a # to make sure the phone is on hook.
2. Send a sequence code to latch pin 12 low and pin 11 high in order to lock out the security function.
3. Press the Enter button.
4. Key in two numeric digits for the address code of the phone number.
5. Press the Clear key to clear the area where the number will be loaded.
6. Key in the phone number.
7. Press the Store key.
8. If more numbers are to be loaded, go to step 5, or unlatch pins 12 and 11. Provision for battery back-up is provided on the board. A 9-volt nicad should be used with this circuit. When the main power fails, the chip enable lines go high. This causes a drop in current to the chip. The trickle charge circuit will not allow the nicads to overcharge.

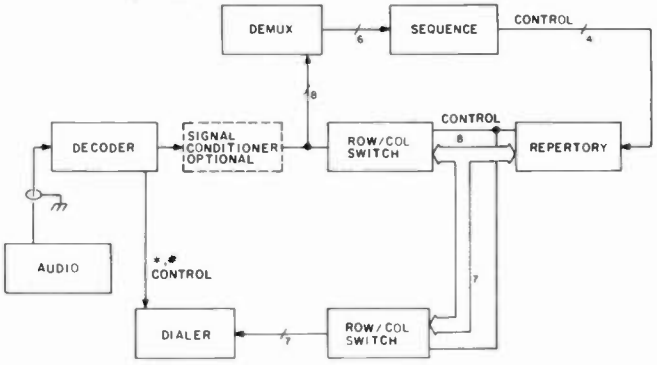


Fig. 4. Repertory connection to phone patch.

The override circuit is used to defeat the Rep and connect the decoder to the dialer for manual dialing. The control station, through a sequencer, makes pins 18 and 12 go low. The patch is brought up with *, and after the dial tone is heard, the dialing can start.

System security is achieved by locking out any column 4 signal by grounding pin 11 using a sequence circuit. If a column 4 signal is received, the Rep goes off hook and the next two digits simply cause the circuit to get a number, but not dial it, since the patch is not on and the unit is in the dial mode, so no damage can be done.

Most repeater groups

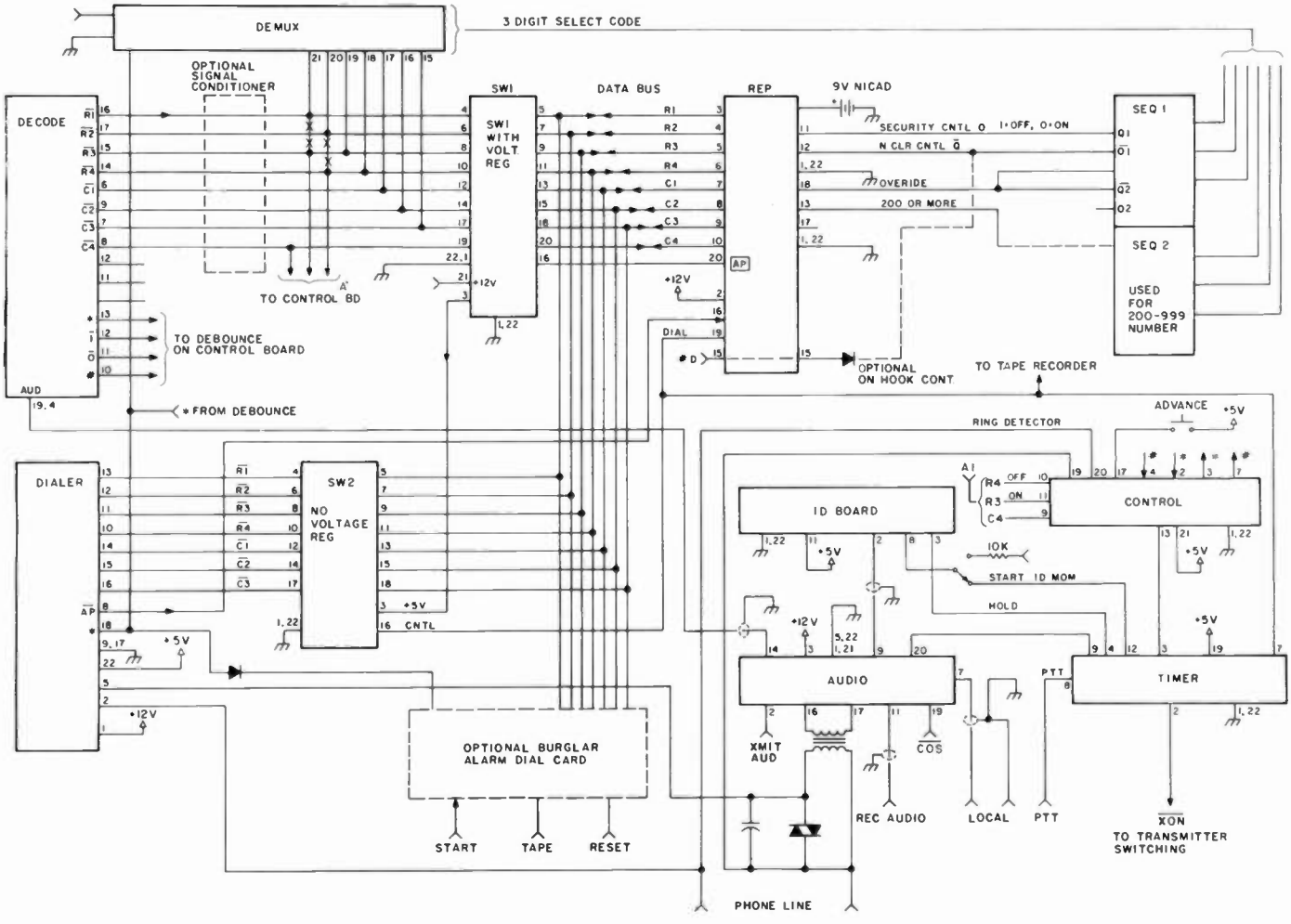
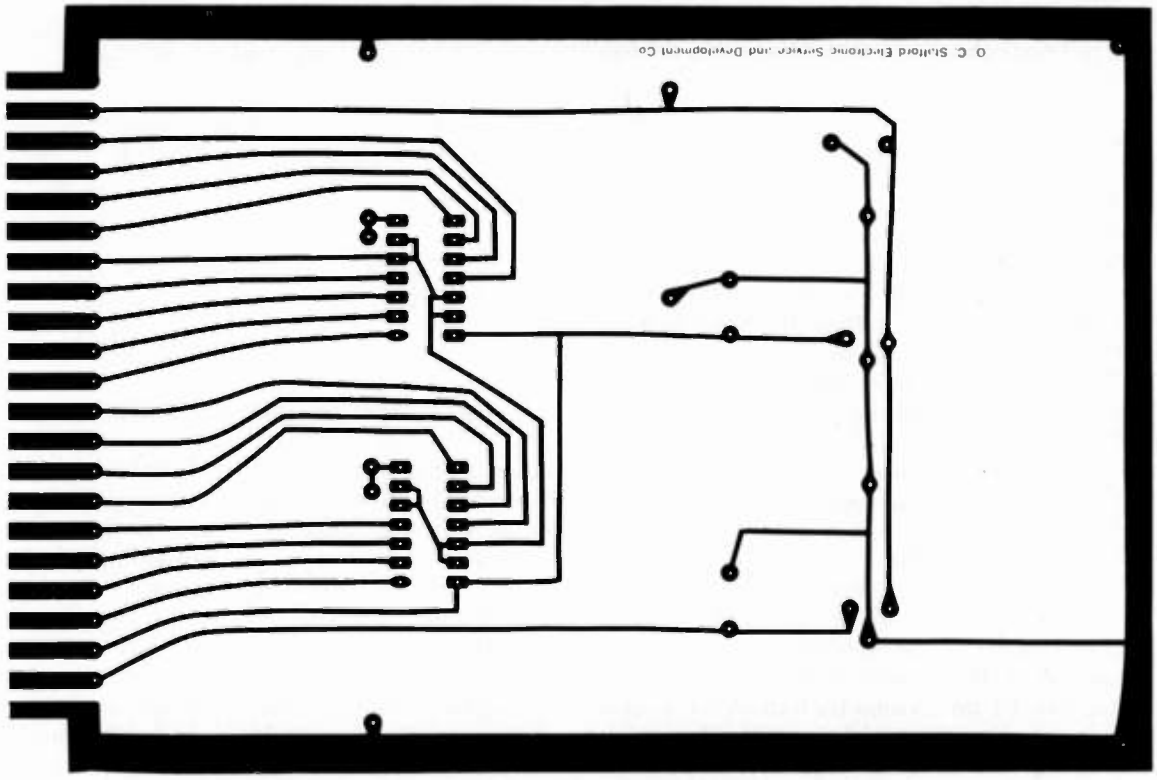
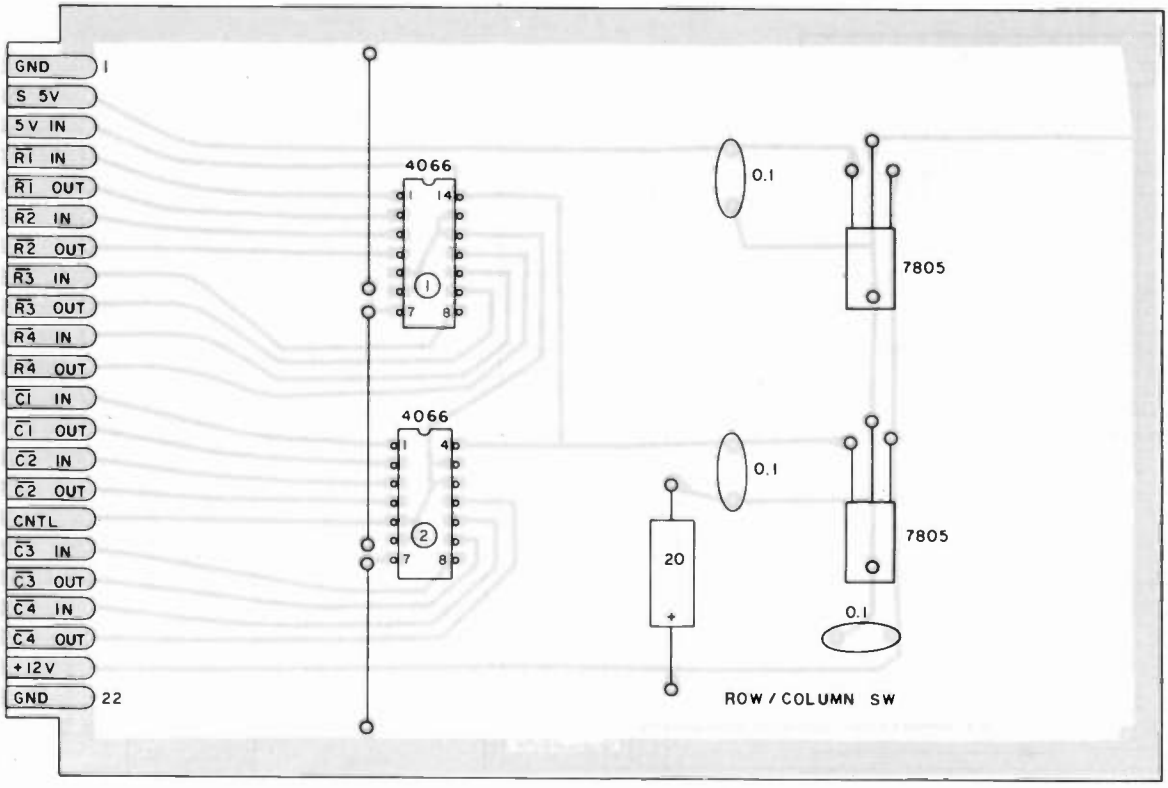


Fig. 5. Basic repeater control system with repertory dialer.



PC board for the row/column switch and regulator.



Component layout for the row/column switch and regulator board.

have fewer than 100 members. One use of the Rep could be to direct calls to special numbers for assistance. For example: If the first two digits of all the exchanges in your area are used as access codes to a common number, then that number would be reached whenever the patch is accessed. This could be helpful if a visitor tries to access the patch with a regular phone number but no access code.

What if your group has more than 100 members and everybody needs a number? No problem. The system can be expanded to select additional 100-number banks. The expansion circuit for a 200-number system is shown in Fig. 8.

To go above 100 numbers requires adding a bank-select digit. The delay gen-

Parts List

Row/Column Switch Board

Quad switches, 4066	2
Voltage regulator, 7805	1
Capacitor, 0.1-uF, tantalum	1
Card edge connector, 22-pin	1
14-pin IC socket	2

Printed circuit board: drilled $7.50, undrilled $5.80.

Rep Board

Capacitor, 6.2-uF, tantalum	5
Capacitor, 0.1-uF, tantalum	2
Resistor, 100k, 1/4 W	3
Resistor, 5.1k, 1/4 W	4
Resistor, 200k, 1/4 W	2
Voltage regulator, 7805	2
Diode, 1N4001	2
Diode, 1N697	3
Crystal, 3.57 MHz	1
Dialer, MK5170	1
Dual one-shot, 74123	1
Quad NAND gate, 7400	2
Quad NOR gate, 7402	2
RAM memory, MK4104	2
16-pin IC socket	1
14-pin IC socket	3
18-pin IC socket	2
40-pin IC socket	1
Card edge connector, 22-pin	1

The above items make up the parts kit, for $100.00. Printed circuit board: $12.50 drilled, $9.50 undrilled. Parts and boards are available from O.C. Stafford Electronic S and D Co., 427 South Benbow Road, Greensboro NC 27401, phone: (919)-274-9917.

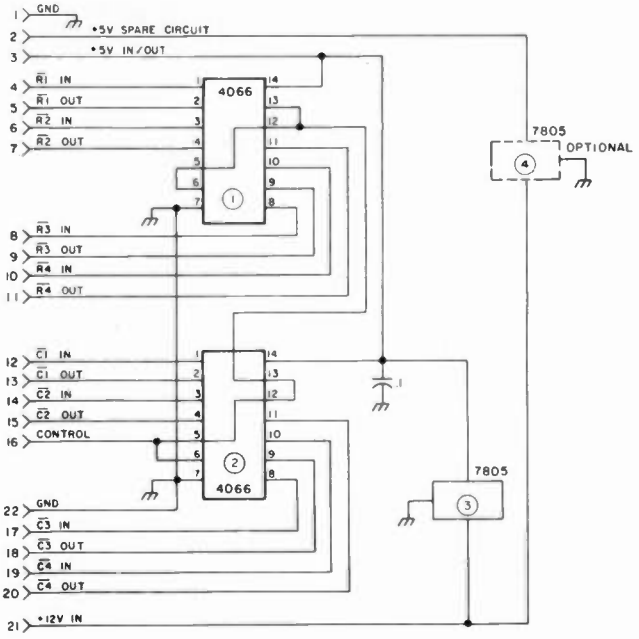


Fig. 6. Row/column switch and regulator board.

erated by the first section of IC6 is increased to 5 seconds. During this five-second interval, the bank-select digit is keyed right after the * and before the five seconds have elapsed.

The input to the row/column lines on the Rep board is not effective during this time because the MK5170 is held in a reset condition and the bank-select switch is on, allowing the digit to be decoded and clock one of the flip-flops. When the call is completed, the bank

BASIC SYSTEM KEYBOARD CONFIGURATION

1	ABC 2	DEF 3	ENTER / DIAL	ROW 1
GHI 4	JKL 5	MNO 6	STORE	ROW 2
PRS 7	TUV 8	WXY 9	INF PAUSE	ROW 3
*	OPER 0	#	CLEAR	ROW 4
COL 1	COL 2	COL 3	COL 4	

Fig. 7. Touchtone pad.

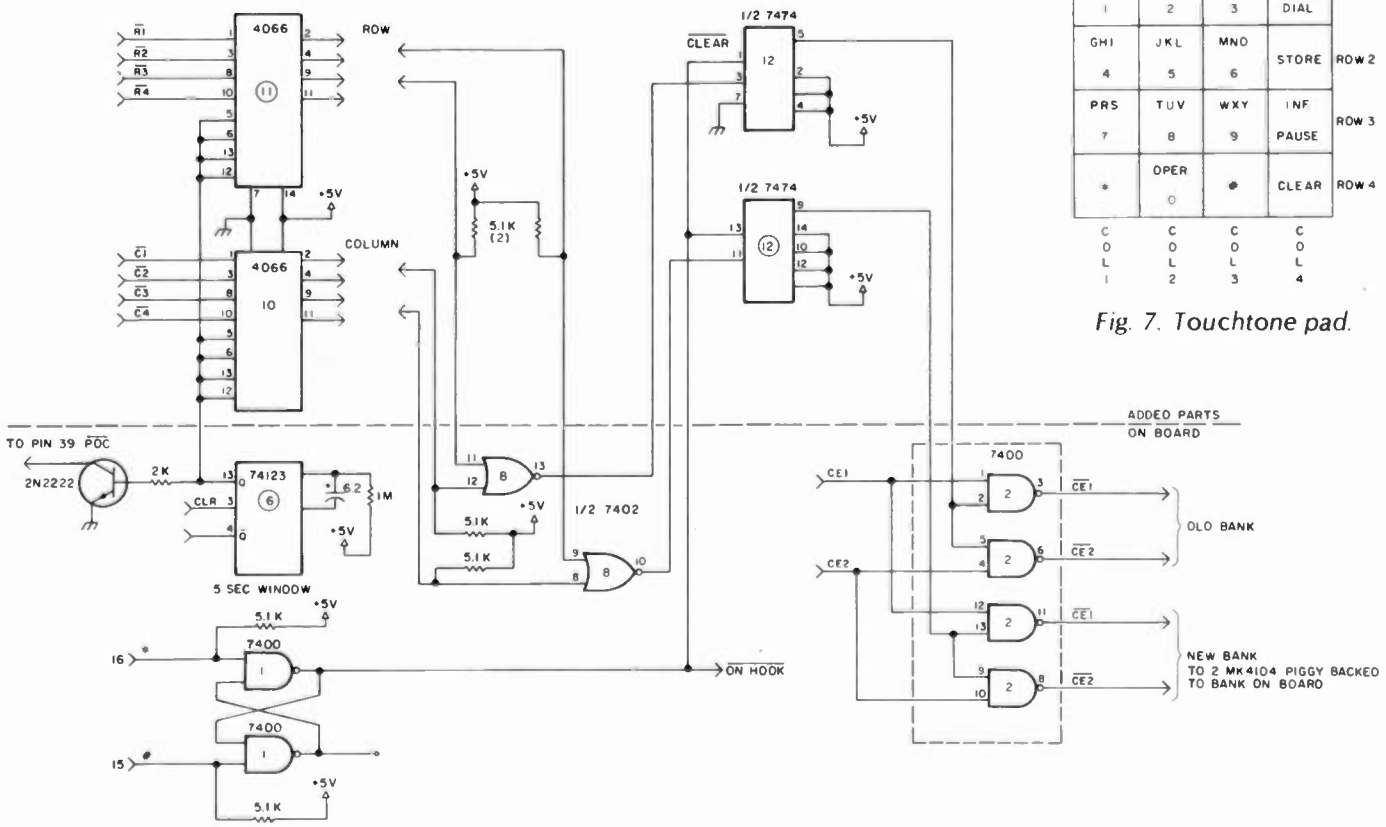


Fig. 8. Expansion circuit for a 200-number system.

flip-flops are reset through diode D6.

In loading a number, the control station pulses pin 13 to get the 5-second window for the bank select. The procedure for loading a number is then used to complete the process.

The spare IC pads on the circuit card can be used to add the 200-number system. The extra memory chips are piggybacked onto the existing chips with chip enables connected to the appropriate bank-select pins. I suggest you use wire-wrap techniques to build the addition, if you need it. Using this type of logic, the circuit can be expanded to handle 999 numbers! If you need that many, you will have to buffer the address lines and add a memory board.

The original control system used R1, R2, and C4 to control the transmitter. This function should be changed to a sequence circuit. The R1/C4 combination could cause the Rep to go into the Enter data mode.

R3 and R4 can be used in place of R1 and R2 and the operation of the Rep will not be affected.

It is hoped that the ideas presented in this circuit will help to alleviate some of the problems associated with autopatches. At the least, it can reduce the hazard of dialing while driving.

I will appreciate any and all comments on this circuit. If you have any questions about how the circuit operates and would like answers, send me a letter along with a self-addressed, stamped envelope. ■

References

1. Mostek Repertory Dialer Data Sheet.
2. *73 Magazine* for April, 1977, June, 1977, March, 1978, May, 1978, and May, 1979.

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74LS30	.55	74LS161	1.79
74LS32	.69	74LS174	1.79
74LS38	.69	74LS175	1.79
74LS42	1.49	74LS192	1.89
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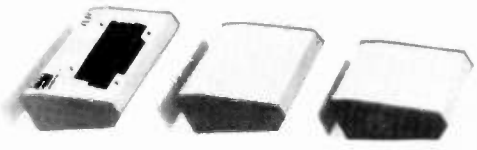
IN4004	4/.69	2N3904	2/.69
IN4007	4/.79	2N3906	2/.69
IN4148	10/.99	2N4401	2/.79
IN4733	2/.69	2N4403	2/.79
IN4734	2/.69	2N5129	2/.69
IN4735	2/.69	2N5139	2/.69
IN4742	2/.69	2N5210	2/.79
IN4744	2/.69	2N5951	2/1.29

DESK TOP ENCLOSURES



DTE-8 (Pictured)	$31.95
DTE-11 (Pictured)	34.95
DTE-14	36.95
DTE-HK (Case for JE600)	47.95
DTE-AK (Case for JE610) (Pictured)	52.95

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.47mfd@35V	2/.89	4.7mfd@50V	2/.59
1mfd@35V	2/.89	10mfd@50V	2/.69
2.2mfd@25V	2/1.09	22mfd@50V	2/.79
3.3mfd@25V	2/1.19	47mfd@50V	2/.89
4.7mfd@25V	2/1.39	100mfd@50V	.59
10mfd@25V	1.19	220mfd@50V	.69
33mfd@25V	3.95	1000mfd@25V	1.19
100V MYLAR		2200mfd@16V	1.39
.001-.01mfd	4/.79	50V CERAMIC	
.022mfd	4/.89	10pf-.022mfd	4/.59
.047mfd	4/.99	.047mfd	4/.69
.1mfd	4/1.19	.1mfd	4/.79
.22mfd	4/1.29		

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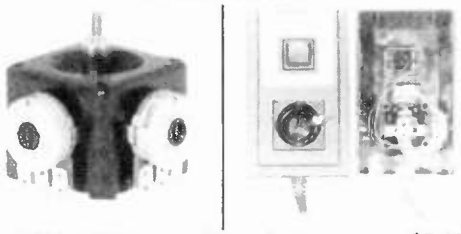
4002	.69	4044	1.39
4006	1.95	4046	2.49
4009	.89	4047	2.75
4010	.85	4049	.89
4011	.69	4050	.89
4013	.85	4051	1.95
4016	.85	4066	1.19
4017	1.49	4069	.79
4018	1.49	4070	.79
4020	2.19	4071	.79
4023	.49	4081	.69
4024	1.29	4093	1.19
4027	.89	4511	1.95

JOYSTICKS



JS-100K	100K Linear Taper Pots	$5.49
JVC-40	40K (2) Video Controller	5.95

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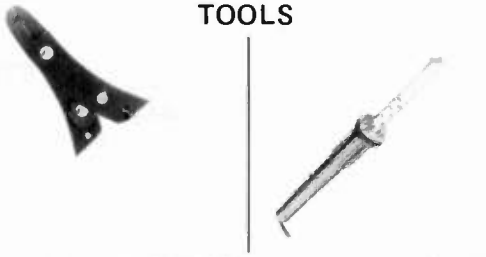
DB25S	D-Subminiature Socket	4.95
DB51226	Cover for DB25P/S	2.25
22/44SE	P.C. Edge	2.95
UG88/U	BNC Plug	2.19
UG89/U	BNC Jack	3.95
UG175/U	UHF Adapter	.59
SO239	UHF Panel Recp.	1.49
PL258	UHF Adapter	1.95
PL259	UHF Plug	1.95
UG260/U	BNC Plug	2.39
UG1094/U	BNC Bulkhead Recp.	1.49

TOOLS



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SG-30	10" 110-120V 30W Solder Iron	7.50
SG-TIP	Replacement Tip for SG-30 S. Iron	1.25

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LM308N	1.19	LM380N	1.49
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LM310N	2.69	LM555N	.69
LM311N	1.49	LM556N	1.49
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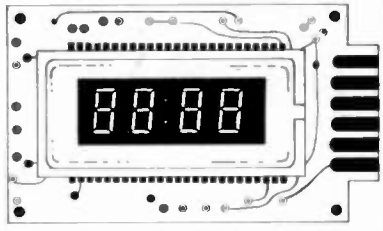

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Photo A.

One of the most irritating sources of electrical noise, characterized by sharp clicks heard through the speaker of a receiver, is contact noise. The make/break cycles of appliances, aquarium heaters, flashing Christmas tree lights, and other noisy electrical contacts can wreak havoc with radio reception.

Fortunately, there are several options which may be elected to minimize these ear-splitting distractions. Perhaps the simplest is the installation of a 0.1-uF capacitor across the contacts themselves.

Since it is often difficult to find direct access to the offending contacts, an alternate solution is found by bypassing the plug with the capacitor. Probably the simplest way to do this is by rigging a plug-in interference filter as shown in the photo.

For standard 120 lines, select a mylar™ capacitor with a 600-volt rating. Insulate the exposed capacitor leads and connect them directly to the terminal screws of any convenient plug. Insert the plug-in filter into the same outlet as used to power the offending contact device.

The bypass capacitor acts as a smoothing filter for the sharp voltage-spike transients generated by the sparking contact. While it is true that the capacitor might actually resonate an unusually long line cord to enhance the noise at some frequency, in actual practice this is extremely unlikely to happen within the passband of most receiving installations. ■

Cal Ritchey
116 Lexington Drive
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Over the Hump and into History

— the last flight of #42-107270

November 30, 1943: In a C-87 airplane (number 42-107270) somewhere over the Himalaya Mountains of Asia, radio operator Kenneth Spencer, a 19-year-old corporal from Rockville Center, Long Island, anxiously twisted the dials of his HF command sets, trying to raise one of the ground stations he knew should be down below.

In the cockpit, Lt. Robert Crozier of Waco, Texas, the pilot, and Flight Officer Harold McCallum of Quincy, Massachusetts, the co-pilot, sat straining their eyes in an attempt to see anything other than the black storm clouds at 24,000 feet.

Aft of the radio shack, Sergeant William Perram of Tulsa, Oklahoma, kept a sharp eye on his dwindling fuel supplies, while the fifth man in the plane, PFC John Huffman of Straughn, Indiana, wondered what was happening.

Though listed on the manifest as assistant engineer, Huffman didn't belong in the plane. Three days earlier, he'd made his first flight east over the Hump from Jorhat Airbase in the Assam Valley of northeast India, to Kunming, an American base 550 miles away in China. At Kunming, he'd been grounded because of a head cold and was deadheading home. He was on the manifest in order to draw special flight pay. Huffman had no access to the inter-crew phone system and relied on shouted explanations of what was happening.

What was happening was that they couldn't find their way back to Jorhat.

Earlier in the day, the C-87 (which was a modification of the B-24 bomber known as the *Liberator*, built by consolidated Aircraft Corporation of San Diego and identical to the B-24 except for the removal of machine guns, turrets, bomb-handling equipment, and related controls, and the addition of a floor in the cargo compartment and a row of windows on either side of the fuselage), had made a quiet flight from Jorhat to Kunming carrying a load of 55-gallon drums of fuel destined to be used by bombers and fighters striking at the Japanese further east and south in China and Burma. They had dropped the fuel at Kunming and been given a partial load of garden produce to go to Yunannyi, about 45 minutes west of Kunming and almost directly on the western flight plan. They had left Yunannyi at about 6 pm, anticipating a routine flight back to Jorhat.

But no flight over the Hump was ever truly routine. By the end of the war, more than 400 planes and 850 men were lost flying the 50-mile-wide corridor, which became known as Aluminum Valley because of the wrecked planes littering the mountain slopes. In clear weather, pilots navigated from one collection of wreckage to the next. In November and December, 1943, there were 38 and 28 *major* accidents, respectively, over the Hump. Between June and December 1943, 168 men were killed making the trip. Some were shot down by marauding Japanese Zeroes up out of Burma, while others were killed when their planes flew into a mountain during the unpredictable storms which sometimes had winds measured at 200 mph. Despite weather as severe as any in the world, the planes flew 24 hours a day, stopping only to change crews, load and refuel, and receive required maintenance.

In September, 1943, Colonel Thomas Hardin was given command of Hump operations; one of his first orders was that "Effective immediately, there will be no weather over the Hump." In the face of extreme icing conditions, high winds, zero visibility, and attacks by Japanese planes, the crews and their aircraft kept flying.

Although the C-87 had a range of about 3000 miles and a ceiling of about 30,000 feet with its four Pratt & Whitney 1200 horsepower engines, it was often hampered by maintenance problems. Parts came from the US via the longest supply route in military history. Temperature ranges from 100 plus degrees at sea level in the Assam Valley to below zero at altitude, coupled with high humidity on the ground, caused rapid rusting and breakdown. The communications equipment was as susceptible to trouble as any other part of the aircraft, and the HF gear was often affected by severe electrical storms over the Hump, caused when warm air from the Bay of Bengal met cold air sweep-

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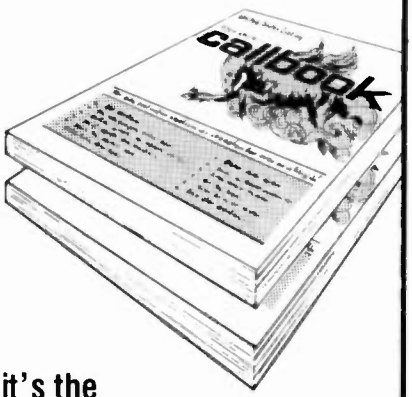

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D-20	20	33	24.95	20.95
D-15	15	22	23.95	19.95
D-10	10	16	22.95	18.95
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SD-80	80,75	90	31.95	27.95
SD-40	40	45	28.95	24.95
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PD-4010	40,20,10,15	66	33.95	29.95
PD-8040	80,40,15	130	35.95	31.95
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ing down across the steppes of north central Asia.

The plane was equipped with up-to-date specialized navigational gear, but some of it was useless because no Hump base had the counterpart equipment.

The C-87 had the same radio gear as its parent B-24, except that the C-87 had fewer interphone crew stations due to elimination of the bombardier and gunner stations on the plane. If the interphone was operating correctly, all crew stations could hear the radio compass signal, the liaison and command radios, and other crewmen.

The command radio equipment in 1943 was high-frequency type (in 1944 upgraded to UHF) and, according to the B-24 manual, was used for plane-to-plane communications, though in practice it was used for all normal traffic, air-to-air or air-to-ground, because all crew members could either receive or transmit via the command set. The command gear included two transmitters mounted on racks on the deck over the wing, along with three receivers. A modulator unit, an antenna-switching relay, a transmitter-control box, a receiver-control unit, a dynamotor, a terminal strip, and two receiver dynamotors completed the rig. The command radio, like most other equipment on the plane, operated on 24 V dc.

The two transmitters had frequency ranges between 5300-7000 kilocycles (kc) and 7000-9100 kc. The three receivers covered frequencies of 190-550 kc, 3000-6000 kc, and 6000-9100 kc.

The liaison equipment was of medium power. Its transmitter had seven removable tuning units supplied with it. The tuners could be inserted by the operator to change frequencies in flight. The tuners handled 200-500 kc, 1500-3000 kc, 3000-4500 kc, 4500-6200 kc, 6200-7700 kc, 7700-10,000 kc, and 10,000-12,500 kc. An antenna-tuning unit, a frequency meter, a receiver in frequency range from 1500-18,000 kc, a dynamotor, a transmitting key, an antenna-transfer switch, and a 200-foot trailing antenna made up the liaison unit. (According to the B-24 manual, the liaison radio could be controlled by the radio operator, pilot, or copilot. Harold McCallum, copilot of #42-107270, says the C-87 liaison gear could be controlled only by the radio operator and was not normally used because of this limitation.)

The radio compass was a 15-tube superheterodyne receiver using 24-28 V dc for operation of the relays. The radio circuits ran on 110 volts ac at 400 cycles; the 110 juice was supplied by inverters under the flight deck, which also supplied power for autosyn instruments and the interior lighting. The loop was electrically driven and could be controlled from either of two remote boxes.

Marker beacon equipment operated on ultra-high-frequency signals at 75 megacycles (mc) and could receive signals from instrument landing systems (ILS), fan stations, cone-of-silence stations, and any other station equipped with horizontally-polarized 75-mc wave systems. According to McCallum, there were no ILS systems in the China-Burma-India (CBI) Theatre, although Chabua had a cone-of-silence system. Planes entering the range received either A or N signals in Morse code, depending on their relation to the range. On the correct approach, no signal was received.

There were six antennas on the B-24/C-87. The command antenna was a single wire from the top of the fuselage above the wing to the top of the left vertical stabilizer (the B-24/C-87 had a twin-tail unit), while the liaison fixed-antenna wire ran to the right vertical stabilizer. The radio compass had two antennas: a vertical whip and a loop, both mounted topside over the wing. The marker beacon antenna was under the plane between the landing gear, and the liaison trailing antenna was a single wire wound on an electrically-operated reel located in the forward compartment under the flight deck and controlled by the radio operator.

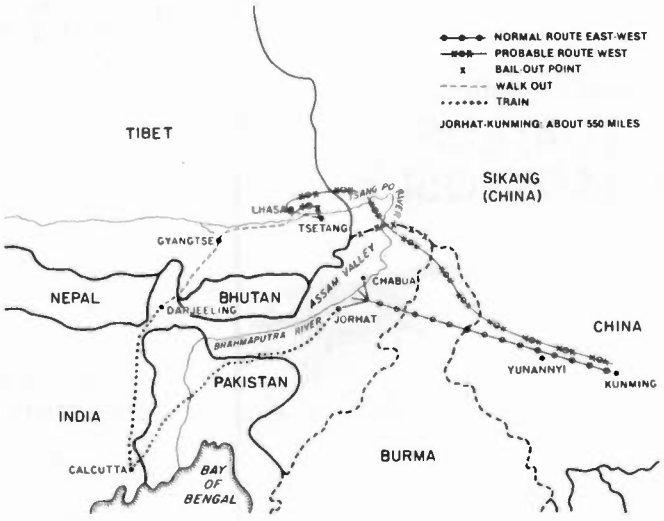

Fig. 1. Map of the area.

According to official briefing information given to crews flying out of the Assam Valley in 1943 and 1944, there were at least four ground stations in operation. Tezpur, Jorhat, Chabua, and Ridge Station were all located along the Brahmaputra River within about 200 miles. Tezpur, Jorhat, and Chabua offered ground-to-air transmission facilities on 4220 and 5588 kc (A-3 emission) or 4595 and 8200 kc (A-1 emission). A-1 was continuous wave (CW). A-2 was tone, A-3 was voice. Receiving was done on 4495 and 5588 kc (A-3) or on 4595 and 8200 kc (A-1). Ridge Station transmitted and received on 5588 kc (A-3).

Chabua and Jorhat had homing beacons of 1000-Watt power-emitting tone signals. The Jorhat tower used 1200 kc, Chabua 1070 kc. Tezpur homed the planes on 295 kc with a 1200-Watt source, while Ridge Station brought the birds in on 390 kc from 50 Watts. All bases with direction-finding equipment in the theatre operated receiving-only on 2000-8000 kc, with all three types of emission.

Since the homing facilities and the DF equipment were operated on request only, at least part of the reason for the plight of the Crozier-McCallum C-87 could have been a result of the inability of the crew to call for operation of the equipment.

Even though the plane was equipped with then-modern gear, Spencer, the radio operator, was unable to get accurate bearings. The radio equipment may not be entirely to blame, however. It is known that in 1942 one or more Japanese stations located in Burma succeeded in giving false bearings to several planes flying the Hump. Some planes and crews were lost before the deception was discovered and steps taken to counteract the problem. Weeks later, McCallum and other members of the C-87 were told that the bearings

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they received that night might also have been of Japanese origin, though it has never been proven.

In 1944, McCallum wrote an account of the flight that night:

"[After leaving Yunannyi] we flew for some time on the same heading, over an overcast and just flying ETAs (estimated time of arrival). We then changed our heading and were still climbing, finally topping it at 24,000 feet.

"When we had estimated that we were within range of our station [Jorhat], we started concentrating on our radio compasses, which began to reciprocate and were not coming in. Next came our try at the radio range, which was throwing As and Ns at us.

"We went on flying over the overcast and trying to see [ground] lights when we hit a break in the clouds.

"Just to be on the safe side, we decided to have a QDM [bearing] shot... Spencer told them to shoot a bearing and gave them a long call. They came back and told us to fly 278 degrees. This was done via Chabua and Jorhat. We decided this couldn't be right, and Spencer relayed the [Crozier's] question if it was 'reciprocal' or 'to fly.' The answer came back 'to fly.' We flew this for a while trying to get contact and see if there were any lights below. Fifteen minutes went by and another bearing was shot.

"...they gave us the same heading, 'to fly.' We told them they must be wrong...the total flying time on this heading was 40 minutes. Another bearing was shot and this time it was 'to fly' 268. And then another which was the same."

What nobody realized was that the plane had been blown off-course by winds later estimated to be from the south at about 100 mph. By the time they were given the 268 heading, they were probably many miles north of their supposed course.

Suddenly Crozier turned to McCallum. "Mac, does that look like a mountain out there?" "It sure is, and I've got one over here!" Crozier twisted the plane into a sharp bank and one of the mountain peaks flashed by, barely feet away.

Thirty-seven years later, McCallum still remembered: "If we'd had our landing gear down, we'd have left tracks in the snow."

Because of the storm, they were still flying at about 24,000 feet—far higher than normal on the route over the Hump in good weather—and those mountains had loomed higher than the plane. For the first time they realized they were really lost, and McCallum quietly tightened his parachute harness as much as possible without leaving the cockpit.

Spencer called the ground station again; the distant operator asked to have the plane's landing lights turned on. "You're over Chabua, we've sighted you, watch for a green flare," Spencer was told. (McCallum thinks the message was a harmonic with another airfield in the area; harmonics were "quite common at night with HF equipment.") Everybody who could get to a window tried to spot the flare, but instead they saw flickering lights through a break in the cloud cover.

Crozier took the plane down and circled the lights, looking for the Chabua field. It wasn't Chabua below, nor Jorhat, nor any of the other bases in the area—the men couldn't recognize anything except that they were over some city of fair size. They took the plane back to about 20,000 feet and flew for a few minutes while Crozier and McCallum talked over the situation. Fuel was becoming critically low: Planes flying the Hump were given only enough fuel to make their destination and return, with about 45 minutes extra flight time.

They were already long overdue at Jorhat, and even as they talked, Number Two engine sputtered and died. Perram was sent back to make a fuel transfer from one of the other tanks, but before he could begin, another engine coughed, smoothed out, coughed again, and quit. Crozier, as commander of the aircraft, made the decision: They would have to bail out.

Parachute jumps were especially dangerous over the Hump route even in daylight, and night jumps were even more so. In daylight, a jumper had some chance of choosing his landing spot. At night he might land in a tree or be impaled on a clump of bamboo, land in a river and drown, or simply plummet straight to the ground beneath an unopened 'chute—parachutes were just as prone to the weather problems as other equipment. Still, there was little choice for the five men. It was jump and have an even chance at survival on the ground, or stay with the plane to almost certain death.

McCallum trimmed the plane level while Crozier took the rest of the crew to the cargo compartment and prepared to jump, but not before Spencer sent out a distress call and screwed down the sending key. When McCallum left the cockpit for the last time, the altimeter read 17,500 feet, all engines were dead, and the plane was dropping rapidly—a C-87 wasn't known for its gliding ability.

In the rear, McCallum found all four men still trying to get the door off—it had opened about two feet and jammed. McCallum and Crozier wrestled it further open until it fell away from the plane. Crozier, Spencer, and probably Perram exited first (Huffman says Perram and McCallum were still aboard when he left; McCallum says the order was Crozier, Spencer, Perram, Huffman, and McCallum).

McCallum started to the door, realized Huffman didn't have his harness straps properly hooked, and went back to help. They got the harness on, though it wasn't tight enough and there was little time to adjust it. Just as Huffman snapped the final hook, the plane lurched as if going into a spin. McCallum knew that once the plane began spinning, centrifugal force might pin them inside all the way to the ground. He hustled Huffman out the door and followed immediately.

McCallum and Huffman both agree that the scene was one of urgency without panic. They also agree that the time from cockpit to bail-out was about one minute.

McCallum hit the airstream and pulled his ripcord, expecting a long ride to the ground, since the crew still thought they were somewhere over India, or perhaps Burma.

He felt the shock of the 'chute opening, and seconds later hit the ground and was knocked unconscious for an indeterminate period of time. When he came to, his watch had stopped at 10:45 p.m. It was dark, but there was enough light to see that he was sitting on the edge of a precipice.

When the sun came up the next morning, McCallum found himself on the side of a mountain, which the crew later decided was more than 16,500 feet high.

As McCallum took stock of his situation and

checked his equipment, he took the Form 58, the sheet signed by the parachute packer, from the 'chute bag—it was common for surviving jumpers to personally thank the rigger. He didn't have to wait long to do that—it was his own name at the bottom. As Assistant Parachute Officer at Jorhat, McCallum packed one 'chute a month as practice. This month, the 'chute he'd packed had been the one he jumped with.

Within an hour or two, McCallum, Crozier, and Spencer had located each other by shouting. Crozier and Spencer were together 1000 or 1500 feet lower than McCallum and perhaps a quarter of a mile away.

Huffman and Perram couldn't be seen. Huffman had landed in a hole and was dangling by his harness; he could hear the other three, but couldn't yell loudly enough to attract their attention. Despite a badly injured left arm—possibly a broken collarbone—he later managed to pull himself out of the hole, but by then, McCallum, Crozier, and Spencer were gone.

Perram had landed on the far side of the peak; during the next few days, he suffered frostbitten feet, but eventually recovered with no damage.

By the fourth day, both Huffman and Perram had been brought to Tsetang. Both men had been found by Tibetans who already knew of the presence of the other three men in Tsetang.

McCallum, who had been studying Hindustani in his free time, was able to talk to one man in the village—everyone else spoke a strange language he'd never heard before. The three Americans were unpleasantly surprised and shocked to learn they had landed in Tibet, several hundred miles to the northeast of Jorhat. There were no American bases—in fact, no Americans at all—in Tibet. The nearest American base was to the south in India, on the other side of the Himalayas.

By the evening of December 2, 1943, Crozier, McCallum, and Spencer were resting in a nearby village called Tsetang which they had found by following a mule caravan.

For two weeks the men waited in Tsetang while the village elders sent messengers back and forth to Lhasa, the capital city, for instructions on how to deal with the Americans. Tibet was a country isolated not only by physical features, but also by national policy. Almost certainly, no more than five Americans had ever visited the country, though both the British and the Chinese maintained small trade missions in Lhasa, both of which aided the flyers in their subsequent journey through Tibet.

Finally word arrived that they were to go to Lhasa, a three-day trip by horse or mule.

At Lhasa they were stoned by an angry crowd of Tibetans. The Americans couldn't understand why; up to this point, all the Tibetans had been friendly. It wasn't until they arrived at Deyki Lingka, home of Mr. and Mrs. George Sherriff of the British Trade Mission, that George Sherriff explained the problem: When the plane had circled the lights of the strange city weeks earlier, they had been over Lhasa, the Holy City of Tibetan Buddhism and the home of the Dalai Lama, the supreme God to the Tibetans. It was a mortal sin, according to the Tibetans, for anyone to place himself physically above the Dalai Lama, whose home was the Potala, a palace of 1000 rooms looming high above Lhasa. The Americans, unknowingly, had been guilty of a religious transgression.

Because of this sin, fanatical monks were agitating the Tibetan populace in Lhasa, and the Tibetan government insisted it could not be responsible for the safety of the Americans in Lhasa. After only three days in Lhasa (spent inside Deyki Lingka for safety), they were escorted to the edge of Lhasa by a crowd of Chinese officials and Mr. and Mrs. Sherriff, as well as other members of the British Mission.

On their first day in Lhasa, Reggie Fox AC4YN, an expatriate Englishman who later married a Tibetan woman, sent a radio message to China informing authorities that all five men were safe. (McCallum has the telegram received by his mother after the plane was lost, reporting him missing, and another a few weeks later after Fox's message was received.)

Fox's station, AC4YN, was a powerful one, and Fox was able to work as far as Indiana, USA, with the equipment, which probably was powered by a small hydroelectric plant on a river about eight miles from Lhasa. (In the mid-'30s, a Tibetan named Rangang, an engineer educated in England, seems to have almost single-handedly built the power plant, which may have been under contract from General Electric Corporation. Another source says the unit was diesel, but since fuel would have had to be carried in over the mountains by mule, the hydro unit seems more reasonable. There were no autos or trucks, or, in fact, wheeled vehicles of any kind, in Lhasa—except for two circa 1920 autos which no longer ran.)

On the edge of Lhasa, the Americans said good-bye to their newly-met British friends and to the Chinese, and guided by two Tibetan soldiers and a Tibetan cook who spoke some Hindustani, set out for India. On the journey, McCallum served as the group's interpreter, through the cook.

Fifty-two days after bailing out of the plane, the five men were back in Jorhat, by way of Darjeeling and Calcutta. Theirs is believed to have been the second-longest walk-out of any downed crew in World War II—the longest was 93 days.

In 1980, four of the crewmen were still living. Crozier lives in Texas; Spencer went back to Long Island. Huffman is retired and lives in the state of Washington. McCallum, who makes his living as a corporate chief pilot, lives in Pennsylvania. William Perram was killed on his first flight after returning from Tibet.

George Sherriff died at his home in Ascreavie, Scotland, in 1967. His wife, Betty, died in 1979. Reggie Fox, still in Tibet in 1948, has dropped from sight.

As for the airplane, #42-107270, she had crashed not far from Tsetang. While the men waited in Tsetang for instructions from Lhasa, they were taken out to the wreckage. The aircraft came down at the edge of the Tsangpo River, which becomes the Brahmaputra in India and flows through Jorhat.

As the men watched, hordes of Tibetans savaged the hulk of the plane for usable metal. One man tried to carry away part of the radio gear but found it too heavy to manage. He seized an axe, hacked the unit in half, and proudly carted away the pieces.

Like many another wreck further south in India or Burma, the skeleton of #42-107270 may still rest along a river bank in a distant country which few Americans have ever seen. ■

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R_X and C_X

— easy-to-build substitution boxes

I finally got tired of trying to read the ohmmeter, hold the test leads in place, and turn the potentiometer to find a resistance value that would keep my experimental circuit from going up in smoke.

What I needed was a resistor substitution box. Well, I got out some paper and a pencil and went to work. The circuit shown in Fig. 1 is the result.

By using 28 resistors and switches in the 1-2-3-3 arrangement, I now have at my fingertips—in one-Ohm steps—resistance values of 1 to 9,999,999 Ohms.

Construction of this unit is simple. The resistors are mounted across the switches' terminals. By opening a switch, *that* resistor is connected in circuit.

The switches are arranged in rows of seven across and four down (See Fig. 1). Then the resistor/switch combinations are connected in series. I used slide switches in my unit (I happened to have them on hand).

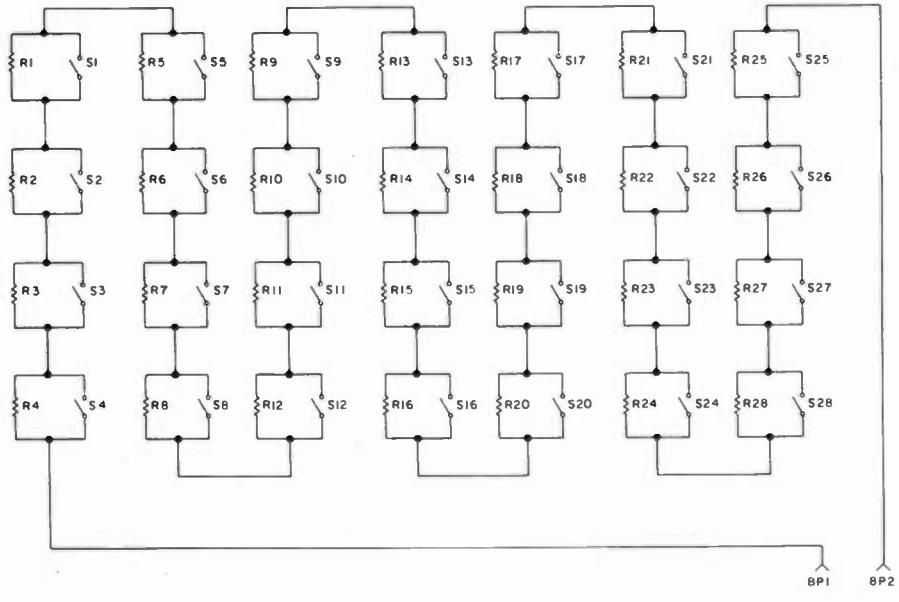

Fig. 1. Schematic for resistor substitution box.

The rectangular openings were cut out with a nibbling tool and the switches were mounted to the box panel with pop rivets.

With the use of 1% resistors, there is a possible error of ±100k (that's with all resistors in circuit for a total of 9,999,999 Ohms).

With this circuit, there is a possible monetary advantage over conventional resistance substitution boxes which usually require sixty-three resistors and seven ten-position switches to cover the same range.

A Capacitor Substitution Box

A ham shack without a capacitor substitution box?

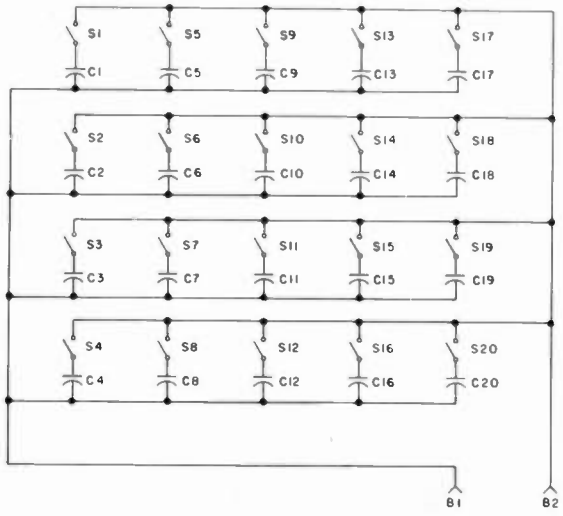

Fig. 2. Schematic for capacitor substitution box.

Resistor Substitution Box Parts List

R1	1 Ohm
R2	2 Ohm
R3-R4	3 Ohm
R5	10 Ohm
R6	20 Ohm
R7-R8	30 Ohm
R9	100 Ohm
R10	200 Ohm
R11-R12	300 Ohm
R13	1k Ohm
R14	2k Ohm
R15-R16	3k Ohm
R17	10k Ohm
R18	20k Ohm
R19-R20	30k Ohm
R21	100k Ohm
R22	200k Ohm
R23-R24	300k Ohm
R25	1 Megohm
R26	2 megohm
R27-R28	3 megohm

S1 through S28—SPST slide or toggle switches
BP1, BP2—5-way binding posts
Misc.—wire, cabinet, rub-on letters and numbers

Capacitor Substitution Box Parts List

C1	10 pF
C2	20 pF
C3	30 pF
C4	30 pF
C5	100 pF
C6	200 pF
C7	300 pF
C8	300 pF
C9	0.001 uF
C10	0.002 uF
C11	0.003 uF
C12	0.003 uF
C13	0.01 uF
C14	0.02 uF
C15	0.03 uF
C16	0.03 uF
C17	0.1 uF
C18	0.2 uF
C19	0.3 uF
C20	0.3 uF

S1 through S20—SPST switches (slide or toggle type)
B1, B2—5-way binding posts
Misc.—wire, cabinet, rub-on letters and numbers

I don't believe it. Well, I've been wrong before, so, if yours happens to be without one, build this one.

This capacitor substitution box has a range of from 10 pF to within 10 pF of 1 uF, in 10-pF steps. That amounts to 99,999 possible values. This is done with only twenty capacitors and switches. Construction of this unit is simple and straightforward. The capacitors are connected between a common line (B1) and one terminal on each switch. The other terminals on the switches are wired to B2. The switches are arranged in rows of four down and five across (Fig. 2). I used mica (5%) and polystyrene (2%) capacitors in my unit.

Of course, the tighter the tolerance on the capacitors, the more accurate the unit. ■

Don't Be Sunk by Heat Sinks

— a painless introduction to heat-transfer physics

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Application

Find the right heat sink for an LM309K voltage regulator IC. The maximum input voltage is 10 volts, the output voltage is to be held at a constant 5 volts, and the maximum current to be drawn from the supply is 1 Amp.

Step 1: Write down the formula:
$R\theta_{SA}(max) = (T_J - T_A)/P_D - R\theta_{JC} - R\theta_{CS}$.

Step 2: Calculate P_D:
$P_D = (Vin - Vout) \times I(max)$
$P_D = (10\ V - 5\ V) \times 1\ A = 5$ Watts

Step 3: Find $T_J(max)$ and derate by 50° C. The data sheet gives us a figure of 125° C for the absolute maximum operating junction temperature; derating that figure by 50° C gives us 75° C for $T_J(max)$.

Step 4: Find $T_A(max)$. The maximum ambient temperature is 25° C, 5° C above room temperature of 20° C.

Step 5: Find $R\theta_{JC}$. Keep in mind that the LM309K is an IC, not a transistor. The data sheet reveals a figure of 3.0° C/W for $R\theta_{JC}$. For transistors, Table 1 is fairly accurate, but for ICs, watch out!

Step 6: Find $R\theta_{CS}$. Since the case is ground on the LM309K used as a fixed 5-volt regulator, we will not need an insulating washer. To improve the heat transfer between the device and the heat sink, we will use some heat-sink compound. From Table 2 we obtain a value of 0.1° C/W for $R\theta_{JC}$.

Step 7: Plug the values into the formula:
$R\theta_{SA}(max) = (75° C - 25° C)/5\ W - 3.0° C/W - 0.1° C/W = 6.9° C/W$.

Step 8: Pick a suitable heat sink. Choose the next lower value for a TO-3 type case. The RCA-SK KH3423 looks suitable with a $R\theta_{SA}$ value of 5° C/W.

For years I have been resorting to B.F.I. (Brute Force and Ignorance) when designing transistor projects. Mainly, this meant using the biggest heat sink I could afford or watching my project go up in smoke. After the loss of a few precious power transistors, I set out to find out all about proper heat sinking. The principle behind picking the right heat sink is rather simple.

In this article, we will explore heat-transfer physics, interfaces, and practical heat-sink choices. First, let's look at how heat sinks work.

Theory

Heat-transfer physics is a scary-sounding phrase for something that some hams don't think they know about, although they know of something similar: basic electricity. Fig. 1 shows the analogy between thermal resistance and ohmic resistance.

In electrical circuits, whenever there is a difference of voltage between

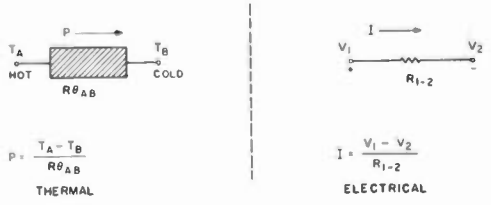

Fig. 1. The electrical analog of heat transfer.

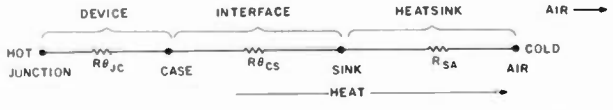

Fig. 2. The electrical analog of heat transfer from the junction of the semiconductor to ambient air ($R\theta_{JA} = R\theta_{JC} + R\theta_{CS} + R\theta_{SA}$).

two points, or nodes, current is said to flow from the more positive node to the more negative node. The amount of current that flows is inversely proportional to the resistance between the two nodes.

Similarly, in thermal circuits, whenever there is a difference of temperature between two bodies (T_A and T_H) or between two portions of one body, heat (P) is said to flow in a direction from higher to lower temperature. This heat flow is expressed in Watts. The amount of heat which flows when a given change in temperature is applied will be found to vary with what is called the thermal resistance of the material ($R\theta$). The lower the thermal resistance of the material, the greater the heat it transfers. Thermal resistance can be expressed in terms of degrees centigrade per Watt (°C/W).

Applying the Theory to Heat Sinks

In semiconductors, heat is produced at the junction of the differently-doped silicon materials. To escape the semiconductor, heat travels from the junction through the case, the interface, and the heat sink into the ambient air. The heat sink dissipates the heat into the surrounding air by means of radiation and convection. The whole system can be represented by the electrical equivalent circuit shown in Fig. 2.

The total thermal resistance from junction to air is the sum of individual thermal resistances: junction to case ($R\theta_{JC}$), case to sink ($R\theta_{CS}$), and sink to air ($R\theta_{SA}$). Applying the analogy found previously, we can say that $P_D\ (max) = [T_J(max) - T_A(max)]/R\theta_{JA}(max)$, where P_D is the maximum power dissipated by the device in Watts, T_J is the maximum junction temperature in °C, T_A is the maximum ambient temperature in °C, and $R\theta_{JA}$ is the maximum thermal resistance from junction to ambient air in °C/W. With a little algebra, we can combine the two formulas found above and get a very useful equation for finding the correct heat sink. In this equation, $R\theta_{SA}(max) = [(T_J - T_A)/P_D] - R\theta_{JC} - R\theta_{CS}$.

Although manufacturers list maximum junction temperatures of 150°-200° C, it is a good design practice to operate the device at a much lower temperature. To ensure plenty of leeway and extend the useful life of the device, use a maximum junction temperature of 50° C less than the manufacturer's listed maximum junction temperature.

There are several ways of obtaining the maximum power dissipated by the device. A simple way of calculating the power dissipated is: $P_D(max) = P_{input} \times (1 - eff)$.

Another way of calculating the power dissipated is: $P_D(max) = I(max) \times E(max)$.

In some cases, the actual power dissipated may be less than these values, but keep in mind this is a worst-case figure.

The thermal resistance from the junction to case ($R\theta_{JC}$) depends mostly on the type of case that the device is packaged in. Although it is best to obtain the value from the data sheet for the transistor or semiconductor device, Table 1 shows some typical values if the data sheet is unavailable.

The thermal resistance from case to sink ($R\theta_{CS}$) depends on a handful of factors: the type of washer used (if any), the tightness of the transistor or semiconductor device against the heat sink, and whether or not silicone thermal paste or heat-sink compound is used. Some approximate values are shown in Table 2.

It should be fairly obvious why thermal joint compound is important. These zinc oxide and silicone oil mixtures reduce the high thermal resistance of the air gap between the case and the heat sink. But be sure to use it sparingly; the paste has a large thermal resistance and it is important to keep the layer as thin as possible.

Case	$R\theta_{JC}$
TO-3	1.5
TO-5	30.0
TO-18	150.0
TO-36	0.7
TO-39	35.0
TO-66	7.0
TO-92	125.0
TO-220	4.0

Table 1. Typical values for $R\theta_{JC}$ for common case styles.

Washer	Paste	No Paste
none	0.1	0.2
beryllia	0.2	0.4
alumina	0.3	0.5
mica	0.4	0.8

Table 2. Approximate values for $R\theta_{CS}$.

A list of commonly available heat sinks and their thermal resistances ($R\theta_{SA}$) is shown in Table 3. The thermal resistance of heat sinks can be improved or lowered by improving the heat-sink-to-air interface. When the ambient air moves, it more readily accepts heat; thus, some benefits can be gained from a fan blowing across the fins of the heat sink. Also, a change in color can decrease the thermal resistance of a heat sink. A thin coat of flat black paint (such as barbecue black) sprayed over a shiny aluminum heat sink lowers the thermal resistance by about 25%. For a real application, see box.

Conclusion

Although calculations in finding the right heat sink can be much more complicated, this article was written to simplify heat transfer physics as much as possible for the amateur or radio experimenter. Hopefully, the reader will be able to pick the right heat sink for the right job with the guidelines presented here. ■

For More Information:

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135 West Magnolia Blvd.
Burbank CA 91502

Thermalloy, Inc.
PO Box 340839
Dallas TX 75234

Wakefield Engineering
60 Audubon Road
Wakefield MA 01880

Brand	Stock	$R\theta_{SA}$	Fits these cases
Calectro	J4-866	23*	TO-220
	J4-878	11	TO-3
	J4-880	2.25	(2) TO-3,TO-36,TO-66, and TO-220
Radio Shack	276-1361	2.25*	(2) TO-3,TO-36,TO-66, and TO-220
	276-1363	20*	TO-220
	276-1364	13*	TO-3
RCA-SK	KH3413	80	TO-1,TO-18,TO-72,TO-104, and TO-92
	KH3415	52	TO-5 and TO-39
	KH3417	20	TO-220
	KH3421	15	TO-66
	KH3423	5	TO-3
Thermalloy	6011	60	14 and 16 pin DIP ICs
	6087	25	40 pin DIP ICs
	6038	10	TO-220
	6017	8	TO-66
	6013	8	TO-3
	6157	0.9	Circuit board or external mounting
Wakefield Engineering	502	1.3	TO-36
	641	3.5	TO-3

*The $R\theta_{SA}$ values for these heat sinks were found experimentally by the author.

Table 3. Typical values for $R\theta_{SA}$.

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Tracker— The Ultimate OSCAR Finder

After a few weeks of "sensory overload" playing games with our new 16K Level II TRS-80 systems, both Dennis and I realized that there was a huge untapped potential inside that rather innocent-looking case. What better way to tap it than to harness the power of the computer to make our hobby a lot more fun by allowing us to operate more and calculate less?

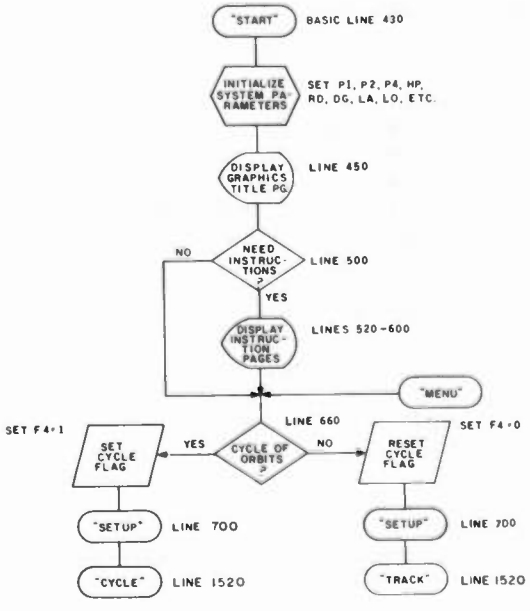
Having both cut our teeth on KIM-1™ systems, and having built them up to the degree of having BASIC programs running on them, we decided that translating some of those programs over to the TRS-80 would be a good way to familiarize ourselves with its capabilities.

The first of the translations undertaken was the program we wrote to track the OSCAR satellites. Considering that both of us are AMSAT members and OSCAR enthusiasts, it seemed like the logical thing to do. Besides, anything that we could use around the shack was bound to be more fun than another game.

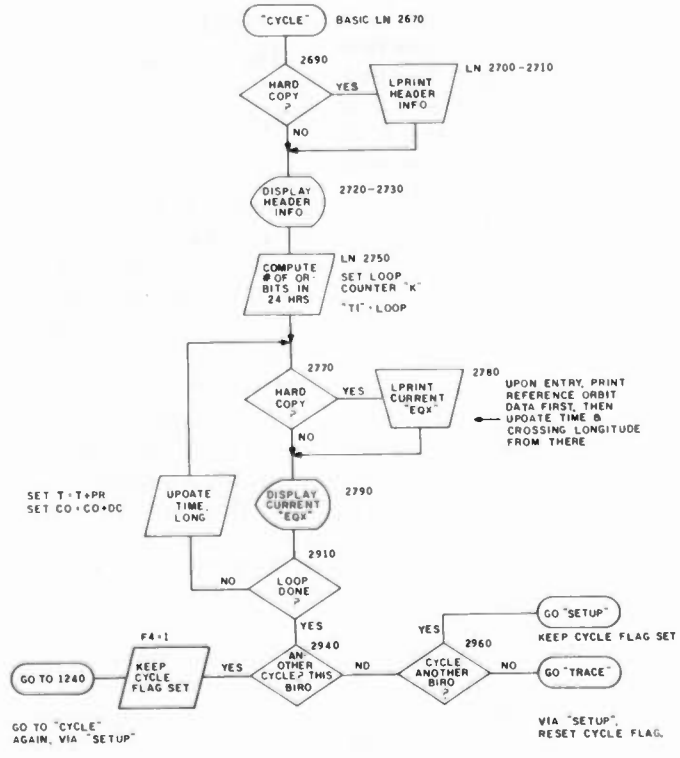
Satellite Tracker is Born

"Tracker" is the fruit of that labor. This program will allow you to use your Level II TRS-80 to track OSCAR 7 and 8 (or any satellite in a polar orbit). Using only the Reference Orbit information published monthly in *73 Magazine*, *QST*, or ARRL bulletins, Tracker will compute the orbits for the day, the time and longitude of each pass (its EQX), and azimuth and elevation data for your steerable beam arrays.

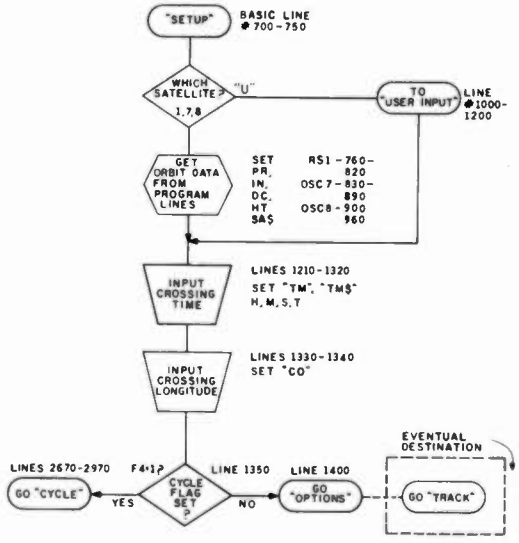
In addition, some slick features have been added that weren't in the original KIM-1 program. For instance, you may now enter a second station's latitude and longitude and Tracker will compute a "Mutual Visibility Window" indicating when the stations will have simultaneous access on any given pass (great for those DX orbits). Line printer routines for hard copy have also been added and will support non-Radio Shack printers as well as the parallel-port Cen-



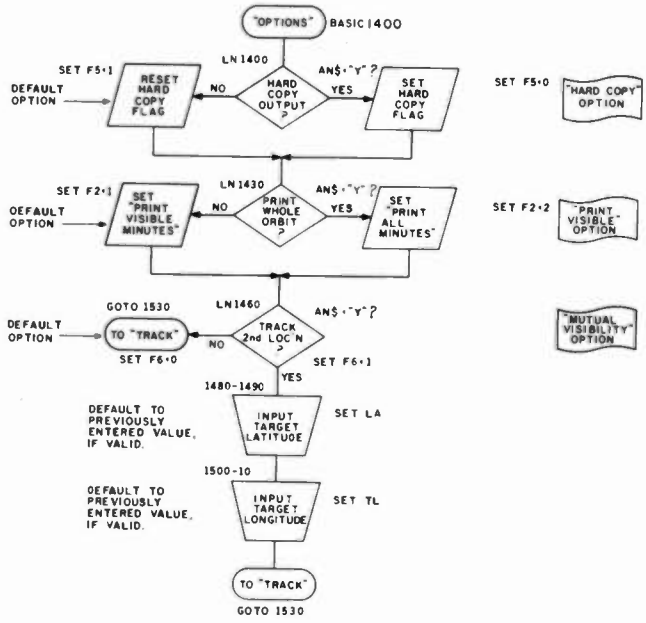
Flowchart 1. Main selection logic.



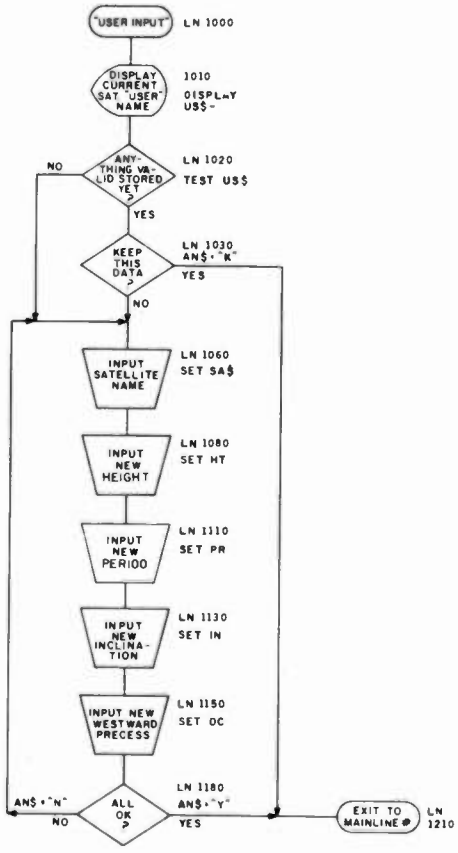
Flowchart 2. Orbit Cycle logic.



Flowchart 3. Setup logic.



Flowchart 5. Options logic.



Flowchart 4. User Input Routine logic.

```
DO YOU WANT A DAY'S CYCLE OF ORBITS (Y/N)?       Y

FOR WHICH SATELLITE?
ENTER 1 FOR RS-1; 7 FOR OSCAR 7; 8 FOR OSCAR 8
ENTER 'U' TO  ACCESS USER INPUT ROUTINE?         R

ORBITAL DATA FOR OSCAR 8 NOW AVAILABLE

FOR OSCAR 8, ENTER REFERENCE ORBIT'S:
TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)? 0035.15
LONGITUDE AT 'EQX' (DECIMAL DEGREES)?              64.5

••• SET OUTPUT OPTIONS •••

PRINT DATA ON LINE PRINTER (Y/N) 'ENTER'=NO  ?  Y

----------  HARD COPY REQUEST CONFIRMED
PRINTER OFF-LINE..CANCEL HARD COPY (Y/N)?        N

HIT 'ENTER' WHEN PRINTER READY?
```

Fig. 1(a). Typical Orbit Cycle request for OSCAR 8, requesting printout.

DAY'S ORBITS FOR OSCAR 8

REF#	TIME (UTC)	LONGITUDE AT 'EQX'
REF	00:35.15	64.5
1	02:18.28	90.3
2	04:01.41	116.1
3	05:44.54	141.9
4	07:28.07	167.7
5	09:11.21	193.5
6	10:54.34	219.3
7	12:37.47	245.2
8	14:21.0	271.0
9	16:04.13	296.8
10	17:47.27	322.6
11	19:30.40	348.4
12	21:13.53	14.2
13	22:57.06	40.0
14	00:40.19	65.8

Fig. 1(b). Printout resulting from request shown in Fig. 1(a).

tronics types. Automatic "sequential tracking" will allow you to track any number of orbits in a row from only one EQX or you may enter the specific orbits you wish to be tracked from the keyboard. Tracker has been extensively tested and should be completely crash-proof (but Murphy always can pay a surprise visit).

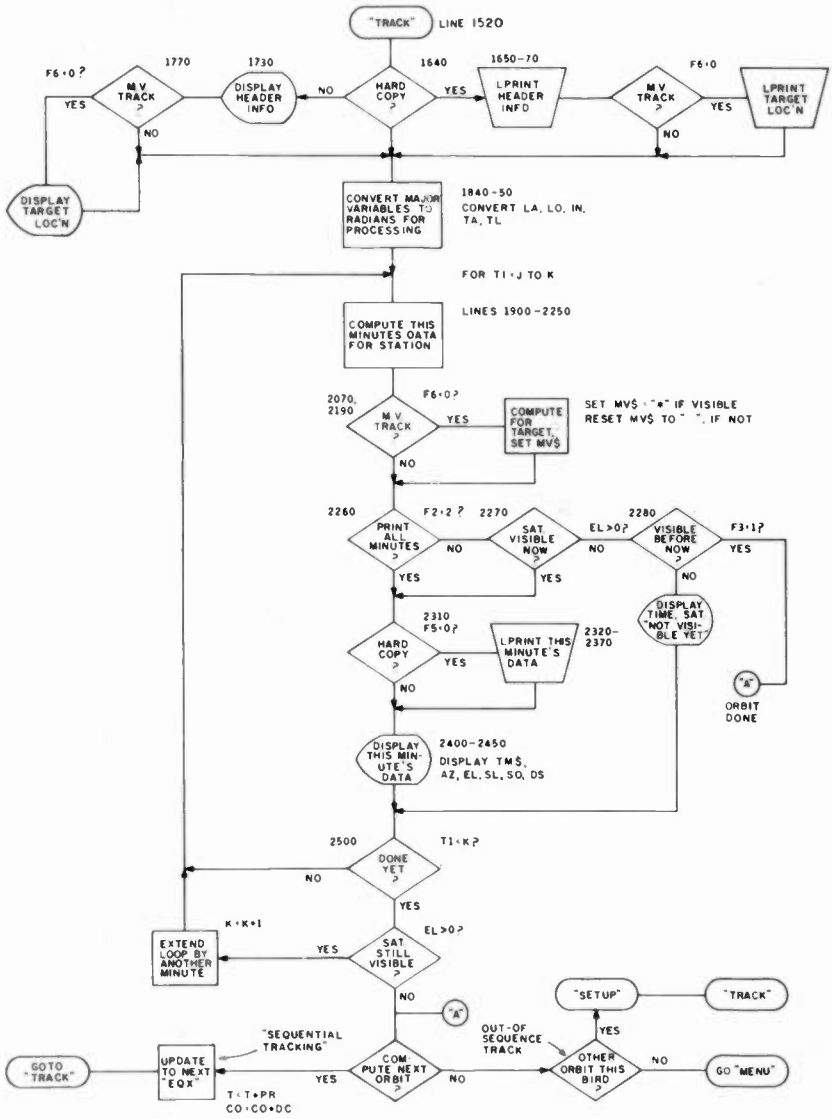
What You Need to Make It Work for You

Tracker will run on any Level II TRS-80 system, either cassette- or disk-based, having at least 16K of RAM. Hard copy is available for those of you who have a line printer, but you don't need one to run the program. Because of the length of the program (12K, more or less) and the use of Level II's built-in trig functions, Level I systems or Level II systems with less than 16K are not suitable.

For you die-hards who insist on typing in everything, the program listing is reproduced here for your convenience, but the rest of you take heart. If you feel that 12K of Level II BASIC is a bit long to type in and debug (and we agree wholeheartedly), cassette tapes are available.

Using Tracker with OSCAR

Using Tracker may look complicated at first glance, but it really isn't. Rather than enter into a detailed description of the program's execution right off, I'll just cover the major sections and how they function. Flowcharts will be



Flowchart 6. Orbit Track logic.

```
COMPUTE ANOTHER CYCLE FOR OSCAR 8 (Y/N) 'ENTER'=NO  ? N

COMPUTE A CYCLE FOR A DIFFERENT SATELLITE (Y/N) 'ENTER'=NO  ? N


WHICH SATELLITE TO TRACK?
ENTER 1 FOR RS-1; 7 FOR OSCAR 7; 8 FOR OSCAR 8
ENTER 'U' TO  ACCESS USER INPUT ROUTINE? 8


ORBITAL DATA FOR OSCAR 8 NOW AVAILABLE

TO TRACK OSCAR 8 ENTER:
TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)? 0035.15

LONGITUDE AT 'EQX' (DECIMAL DEGREES)? 64.5

LATITUDE OF YOUR STATION (DECIMAL DEGREES)? 42.375

LONGITUDE OF YOUR STATION (DECIMAL DEGREES)? 83.75

*** SET OUTPUT OPTIONS ***

PRINT DATA ON LINE PRINTER (Y/N) 'ENTER'=NO  ? N
----------  'NO HARD COPY' CONFIRMED

DO YOU WISH TO SEE THE WHOLE ORBIT (Y/N) 'ENTER'=NO  ? N
----------  'PRINT VISIBLE MINUTES ONLY'  CONFIRMED

TRACK FOR MUTUAL VISIBILITY (Y/N) 'ENTER'=NO  ? N
----------  'NO  M.V.TRACK'
```

Fig. 2. Typical Orbit Track run, tracking OSCAR 8 reference orbit from Fig. 1. Options requested are: NO HARD COPY, PRINT VISIBLE ONLY, NO M.V. TRACK.

used to assist you in understanding the logic of the program. A reference chart has been provided, listing the functions by line numbers for those of you who might want to modify it (although I really can't think of anything we have left out).

Tracker in Action

To compute and track all orbits of either of the polar OSCARs (or other polar satellites) for any given day, the only information you will need is the time and longitude (EQX) of the reference orbit for that day. This data is available in most of the monthly amateur publications and also is available from AMSAT Orbit Calendars and in daily bulletin transmissions over W1AW.

To make things easier, the main logic has been divided into two sections: Orbit Cycle Compute and Orbit Track. The functions and differences of these two routines are described in the following sections. To select Orbit Cycle or Orbit Track, Tracker will prompt:

DO YOU WANT A DAY'S CYCLE OF ORBITS (Y/N)?

A YES or Y answer will select Orbit Cycle and a NO or N will select Orbit Track routine. Flowchart 1 details the main selection logic.

Orbit Cycle

Given the EQX of a reference orbit (the first orbit after GMT midnight, generally), Orbit Cycle—which is *not* a moon bike—will compute and display the EQX data for every orbit of that satellite in the 24-hour period following the reference orbit. This data will be used later in Orbit Track, so you might want to jot down the orbits that look good to you. This routine is provided mostly as a convenience for those who need to generate a list of the day's orbit times. Flowchart 2 details the Orbit Cycle logic, and Flowchart 3 details the logic used to select a satellite for cycle or track, called Setup. Fig. 1 shows a typical Orbit Cycle printout.

Orbit Track

The Orbit Track routine is the main body of the program. Orbit Track will take EQX data entered from the keyboard by you (and probably computed by Orbit Cycle) along with orbital parameters for the satellite of interest and the location of your station and will compute and display, on a minute-by-minute basis, the visibility of the satellite. It also will produce azimuth and elevation headings from your station location, the latitude and longitude of the sub-satellite point (the point on the Earth's surface directly under the satellite), and the direct distance from you to the satellite, in kilometers.

Phew . . . Wanna try doing all that on your little four-banger and still get ready for that 6:20 pm pass while the XYL is screaming *"DINNER'S READY"* and the kids want to know when you can fix that broken bike? You get the picture!

You may make a selection from the pre-programmed satellites (OSCAR 7, OSCAR 8, or RS-1), or Tracker will accept your own orbital parameters to facilitate tracking other polar orbiting satellites, like the NOAA weather birds. This is accomplished by the "User Input Routine" (see

```
SATELLITE TRACKING DATA FOR OSCAR 8
FOR LAT: 42.375 LONG: 83.75
ORBIT BEGINS 00:35.15 (UTC), AT LONG: 64.5

TIME(UTC)      AZ        EL       S-LAT     S-LONG     DIST.(KM)

00:40.15      148.7      0.7      17.2       68.8       3441.5
00:41.15      147.3      4.5      20.6       69.8       3054.9
00:42.15      145.4      8.8      24.0       70.7       2672.7
00:43.15      142.8     14.0      27.4       71.7       2299.0
00:44.15      139.0     20.4      30.9       72.7       1940.3
00:45.15      132.9     28.5      34.3       73.8       1608.9
00:46.15      122.1     38.8      37.7       75.0       1327.0
00:47.15      100.4     50.1      41.1       76.3       1133.6
00:48.15       62.6     54.6      44.5       77.6       1078.3
00:49.15       29.2     46.8      47.9       79.1       1181.0
00:50.15       11.8     35.4      51.2       80.8       1407.1
00:51.15        2.9     25.7      54.6       82.7       1707.6
00:52.15      357.7     18.2      57.9       84.9       2049.3
00:53.15      354.4     12.3      61.2       87.5       2413.7
00:54.15      352.2      7.4      64.4       90.6       2790.8
00:55.15      350.6      3.2      67.6       94.5       3174.8
```

Fig. 3. Printout that would result from options requested in Fig. 2, had hard copy been selected.

```
SATELLITE TRACKING DATA FOR OSCAR 8
FOR LAT: 42.375 LONG: 83.75
ORBIT BEGINS 00:35.15 (UTC), AT LONG: 64.5

TIME(UTC)      AZ        EL       S-LAT     S-LONG     DIST.(KM)

00:36.15      152.1     -11.4      3.4       65.4       4090.0
00:37.15      151.4      -8.7      6.9       66.2       4605.3
00:38.15      150.7      -5.8     10.3       67.1       4218.3
00:39.15      149.8      -2.7     13.7       67.9       3829.9
00:40.15      148.7       0.7     17.2       68.8       3441.5
00:41.15      147.3       4.5     20.6       69.8       3054.9
00:42.15      145.4       8.8     24.0       70.7       2672.7
00:43.15      142.8      14.0     27.4       71.7       2299.0
00:44.15      139.0      20.4     30.9       72.7       1940.3
00:45.15      132.9      28.5     34.3       73.8       1608.9
00:46.15      122.1      38.8     37.7       75.0       1327.0
00:47.15      100.4      50.1     41.1       76.3       1133.6
00:48.15       62.6      54.6     44.5       77.6       1078.3
00:49.15       29.2      46.8     47.9       79.1       1181.0
00:50.15       11.8      35.4     51.2       80.8       1407.1
00:51.15        2.9      25.7     54.6       82.7       1707.6
00:52.15      357.7      18.2     57.9       84.9       2049.3
00:53.15      354.4      12.3     61.2       87.5       2413.7
00:54.15      352.2       7.4     64.4       90.6       2790.8
00:55.15      350.6       3.2     67.6       94.5       3174.8
00:56.15      349.4      -0.4     70.6       98.5       3562.3
00:57.15      348.5      -3.7     73.5      106.1       3951.1
00:58.15      347.8      -6.7     76.1      115.2       4339.4
00:59.15      347.3      -9.5     78.3      127.8       4726.0
01:00.15      346.8     -12.2     79.7      144.8       5110.1
01:01.15      346.5     -14.7     80.1      164.9       5490.9
01:02.15      346.3     -17.2     79.3      184.2       5867.5
01:03.15      346.1     -19.5     77.5      199.5       6239.6
01:04.15      345.9     -21.8     75.1      210.6       6606.5
01:05.15      345.8     -24.1     72.4      218.6       6967.8
01:06.15      345.8     -26.3     69.4      224.5       7322.9
01:07.15      345.7     -28.4     66.3      229.0       7671.6
01:08.15      345.7     -30.5     63.1      232.6       8013.3
01:09.15      345.8     -32.6     59.9      235.5       8347.7
01:10.15      345.8     -34.7     56.6      237.9       8674.5
01:11.15      345.9     -36.7     53.3      240.0       8993.2
01:12.15      346.0     -38.8     49.9      241.8       9303.6
01:13.15      346.2     -40.8     46.6      243.4       9605.3
01:14.15      346.3     -42.8     43.2      244.8       9898.0
01:75.15      346.5     -44.8     39.8      246.1      10181.4
01:76.15      346.7     -46.7     36.4      247.4      10455.2
01:77.15      346.9     -48.7     33.0      248.5      10719.3
01:18.15      347.1     -50.6     29.5      249.6      10973.1
01:19.15      347.4     -52.6     26.1      250.6      11216.7
01:20.15      347.7     -54.5     22.7      251.6      11449.6
01:21.15      348.0     -56.4     19.3      252.5      11671.8
01:22.15      348.4     -58.4     15.8      253.4      11882.8
01:23.15      348.8     -60.3     12.4      254.3      12082.7
01:24.15      349.2     -62.2      9.0      255.2      12271.1
01:25.15      349.7     -64.1      5.5      256.0      12447.9
01:26.15      350.3     -66.0      2.1      256.9      12612.9
```

Fig. 4. Printout for same input as Fig. 2, but selecting PRINT ALL MINUTES.

```
SATELLITE TRACKING DATA FOR OSCAR 8
FOR LAT: 42.375 LONG: 83.75
ORBIT BEGINS 00:35.15 (UTC), AT LONG: 64.5
* = WINDOW OPEN TO LAT: 45.25  LONG: 110.375

TIME(UTC)      AZ        EL       S-LAT     S-LONG     DIST.(KM)

00:40.15      148.7      0.7      17.2       68.8       3441.5
00:41.15      147.3      4.5      20.6       69.8       3054.9
00:42.15      145.4      8.8      24.0       70.7       2672.7
00:43.15      142.8     14.0      27.4       71.7       2299.0
00:44.15      139.0     20.4      30.9       72.7       1940.3
00:45.15      132.9     28.5      34.3       73.8       1608.9
00:46.15*     122.1     38.8      37.7       75.0       1327.0
00:47.15*     100.4     50.1      41.1       76.3       1133.6
00:48.15*      62.6     54.6      44.5       77.6       1078.3
00:49.15*      29.2     46.8      47.9       79.1       1181.0
00:50.15*      11.8     35.4      51.2       80.8       1407.1
00:51.15*       2.9     25.7      54.6       82.7       1707.6
00:52.15*     357.7     18.2      57.9       84.9       2049.3
00:53.15*     354.4     12.3      61.2       87.5       2413.7
00:54.15*     352.2      7.4      64.4       90.6       2790.8
00:55.15*     350.6      3.2      67.6       94.5       3174.8
```

Fig. 5. Printout for same input as Fig. 2, but tracking for a second station located at Lat 42.25, Long 110.375. Asterisks next to TIME(UTC) mean cross-communication is possible during those minutes.

```
DO YOU WANT A DAY'S CYCLE OF ORBITS (Y/N)? Y
FOR WHICH SATELLITE?
ENTER 1 FOR RS-1; 7 FOR OSCAR 7; 8 FOR OSCAR 8
ENTER 'U' TO  ACCESS USER INPUT ROUTINE? 7

ORBITAL DATA FOR OSCAR 7 NOW AVAILABLE

FOR OSCAR 7, ENTER REFERENCE ORBIT'S:
TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)? 2424.10

** INPUT ERROR **
FOR OSCAR 7, ENTER REFERENCE ORBIT'S:
TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)? 0024.65

** INPUT ERROR **
FOR OSCAR 7, ENTER REFERENCE ORBIT'S:
TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)? 0024.10
LONGITUDE AT 'EQX' (DECIMAL DEGREES)? 400

** INPUT ERROR **
LONGITUDE AT 'EQX' (DECIMAL DEGREES)? -24

** INPUT ERROR **
LONGITUDE AT 'EQX' (DECIMAL DEGREES)? 80

*** SET OUTPUT OPTIONS ***

PRINT DATA ON LINE PRINTER (Y/N) 'ENTER'=NO  ? Y
----------  HARD COPY REQUEST CONFIRMED
PRINTER OFF-LINE..CANCEL HARD COPY (Y/N)? N
HIT 'ENTER' WHEN PRINTER READY?
```

Fig. 6(a). Input run for Cycle showing error messages that alert user to incorrect entries.

```
LATITUDE OF YOUR STATION (DECIMAL DEGREES)? 400.25

** INPUT ERROR **
 LATITUDE MUST BE BETWEEN -90 & 90 DEGREES

LATITUDE OF YOUR STATION (DECIMAL DEGREES)? 40.025

LONGITUDE OF YOUR STATION (DECIMAL DEGREES)? 830.75

** INPUT ERROR **
 LONGITUDE MUST BE BETWEEN 0 & 360 DEGREES

LONGITUDE OF YOUR STATION (DECIMAL DEGREES)? 83.075

*** SET OUTPUT OPTIONS ***

PRINT DATA ON LINE PRINTER (Y/N) 'ENTER'=NO  ? Y
----------  HARD COPY REQUEST CONFIRMED
DO YOU WISH TO SEE THE WHOLE ORBIT (Y/N) 'ENTER'=NO  ? N
----------  'PRINT VISIBLE MINUTES ONLY'  CONFIRMED
TRACK FOR MUTUAL VISIBILITY (Y/N) 'ENTER'=NO  ? N
----------  'NO  M.V.TRACK'
PRINTER OFF-LINE..CANCEL HARD COPY (Y/N)? NO
HIT 'ENTER' WHEN PRINTER READY?
```

Fig. 6(b). Input run showing error messages for incorrect entry of station coördinates. Actual latitude cannot exceed 89.99 degrees, plus or minus, without causing program error. Longitude is required to be positive.

```
DO YOU WANT A DAY'S CYCLE OF ORBITS (Y/N)? N
WHICH SATELLITE TO TRACK?
ENTER 1 FOR RS-1; 7 FOR OSCAR 7; 8 FOR OSCAR 8
ENTER 'U' TO  ACCESS USER INPUT ROUTINE? U
                  ==================
                  USER INPUT ROUTINE
                  ==================

DATA NOW ON FILE FOR: ** NO CURRENT ENTRY **
PLEASE ENTER THE FOLLOWING:
NAME OF THIS SATELLITE? SAMPLE1
HEIGHT OF SATELLITE (IN KM)? 20
THAT'S PRETTY LOW...BETTER DUCK½½
HEIGHT OF SATELLITE (IN KM)? 1400
PERIOD OF SATELLITE (IN DECIMAL MINUTES)? 20
INCLINATION OF ORBIT (IN DECIMAL DEGREES)? 99.9
WESTWARD PROGRESS OF ORBIT (IN DECIMAL DEGREES)? 370.25
THAT'S VERY LARGE..ARE YOU SURE??
WESTWARD PROGRESS OF ORBIT (IN DECIMAL DEGREES)? 37.025
IS THIS DATA ALL CORRECT? N


PLEASE ENTER THE FOLLOWING:
NAME OF THIS SATELLITE? SAMPLE1
HEIGHT OF SATELLITE (IN KM)? 1400
PERIOD OF SATELLITE (IN DECIMAL MINUTES)? 200.5
INCLINATION OF ORBIT (IN DECIMAL DEGREES)? 99.9
WESTWARD PROGRESS OF ORBIT (IN DECIMAL DEGREES)? 37.025
IS THIS DATA ALL CORRECT? Y

ORBITAL DATA FOR SAMPLE1 NOW AVAILABLE

TO TRACK SAMPLE1 ENTER:
TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)? 0010.0
LONGITUDE AT 'EQX' (DECIMAL DEGREES)? 80
```

Fig. 7. "User Input Routine" entries showing error inquiries and corrections double-check at end of run. Program then continues to Track or Cycle as selected.

Program listing.

```
100 REM ************************************************
110 REM ****                                            ****
120 REM ****     SATELLITE TRACKING PROGRAM             ****
130 REM ****                                            ****
140 REM ****     COPYRIGHT (C) 1979 BY:                 ****
150 REM ****     GNOME COMPUTERWORKS,          FOR:     ****
160 REM ****     DENNIS MITCHELL, K8UR.....AND          ****
170 REM ****     BRUCE NAZARIAN, WD8DRK.....AUTHORS     ****
180 REM ****                                            ****
190 REM ****     THIS PROGRAM WILL COMPUTE ORBITS AND   ****
200 REM ****     ANTENNA AZ-EL CO-ORDINATES FOR THE     ****
210 REM ****     USER'S LOCATION. DATA FOR OSCAR 7,     ****
220 REM ****     OSCAR 8 AND RS-1 IS PRE-PROGRAMMED.    ****
230 REM ****     DATA FOR OTHER SATELLITES MAY BE       ****
240 REM ****     ENTERED BY THE USER FOR COMPUTING      ****
250 REM ****     ORBITS FOR FUTURE LAUNCHED SPACECRAFT. ****
260 REM ****                                            ****
270 REM ****     OPERATION IS EASY-- THIS PROGRAM IS    ****
280 REM ****     VERY USER-ORIENTED AND WILL TALK YOU   ****
290 REM ****     THROUGH MOST EVERY STEP NECESSARY FOR  ****
300 REM ****     SUCCESSFUL COMPUTING..                 ****
310 REM ****                                            ****
320 REM ****     FOR FURTHER INFORMATION OR CLARIFICATION ****
330 REM ****     CONTACT:                               ****
340 REM ****              BRUCE NAZARIAN, WD8DRK        ****
350 REM ****            \ GNOME COMPUTERWORKS           ****
360 REM ****              P.O.BOX 8063                  ****
370 REM ****              ANN ARBOR, MICH  48107        ****
380 REM ****              (313)  995-2398               ****
390 REM ****     16K FREE MEMORY = 2124   <VERSION 4.1>  ****
400 REM ****                                            ****
410 REM ************************************************
420 REM
430 REM          PRINT TITLE PAGE  (WITH ANIMATION)
440 REM
450 CLS
452 SS="OPENCLOSE"
455 FOR I=0TO100:PRINT@RND(1916/2),"*";:NEXT
460 FORI=1TO2:
    PRINT@400,"                ";:FORI=1TO200:NEXTI:
    PRINT@400," SATELLITE ";:FORI=1TO200:NEXTI:
    NEXTI1
470 FORI1=1TO2:
    PRINT@550,"                ";:FORI=1TO200:NEXTI:
    PRINT@550," TRACKER ";:FORI=1TO200:NEXTI:
    NEXTI1
480 PRINT@960,"AN OSCAR USER'S AID";:
    PRINT@992,"(C) 1979 GNOME COMPUTERWORKS";
490 J=846:
    FORI=0TO13:C=J-(62*I)+I:PRINT@C,SS;:
    FORI1=0TO100:NEXTI1:PRINT@C,"  ";:NEXTI
492 REM J=846:FOR I=0TO12:C=J-(62*I)+I:PRINT@C,SS;:FORI1=0TO100:NEXTI1:
PRINT@C,"  ";:NEXT I
500 FORI=0TO1000:NEXT:CLS:PRINT@512,"";
510 INPUT"DO YOU NEED INSTRUCTIONS (Y/N)";AN$
515 IF LEFT$(AN$,1)<>"Y"THEN600
520 REM          PRINT OUT INSTRUCTIONS
530 CLS:PRINT"
        THIS PROGRAM WILL ASSIST YOU IN TRACKING THE PATHS OF
SATELLITES IN CIRCULAR OR NEAR-CIRCULAR ORBITS. OSCAR 7 & 8
ARE EXAMPLES OF THIS TYPE OF SATELLITE, AND ARE THE PRIMARY
FOCUS OF THIS PROGRAM.";
540 PRINT"  HOWEVER, ANY SATELLITE IN A SUITABLE
ORBIT WHOSE PARAMETERS ARE KNOWN MAY BE TRACKED BY INSERTING
THOSE PARAMETERS INTO THE PROGRAM THROUGH THE 'USER INPUT'
ROUTINE"
550 PRINT"
        TO ACTIVATE THIS 'USER INPUT' ROUTINE, TYPE 'U' IN
RESPONSE TO THE SATELLITE MENU:

        'ENTER 1 FOR RS-1; 7 FOR OSCAR 7; 8 FOR OSCAR 8;
         ENTER 'U' FOR ACCESS TO USER INPUT ROUTINE.'"
560 PRINT@960,"(HIT 'ENTER' TO CONTINUE)";:INPUT AN$
570 CLS:PRINT"
        THE 'USER INPUT' ROUTINE WILL NOW PROMPT YOU FOR THE
NAME OF YOUR SATELLITE, AND THE VARIOUS ORBIT PARAMETERS.
WHEN ALL NECESSARY PARAMETERS HAVE BEEN INPUT, THE COMPUTER WILL THEN PROMPT
FOR A REFERENCE ORBIT."
580 PRINT"
        THE PROGRAM WILL THEN OFFER THE STANDARD OPTIONS, AND
WILL CYCLE THROUGH ITS FUNCTIONS.

        'TRACKER' WILL TALK YOU THROUGH ALL OF THE STEPS YOU
NEED TO EXECUTE FOR ANY GIVEN TRACKING  OR ORBIT COMPUTING."
590 PRINT@960,"";:INPUT"(HIT 'ENTER' WHEN READY TO BEGIN)";AN$
600 REM
610 REM          BEGIN PROGRAM RUN HERE
620 CLEAR400
630 CLS:PI=3.14159265:P2=2*PI:PY=180:IS="#####.#":CR$=CHR$(13):
    US$="** NO CURRENT ENTRY **":RD=PI/PY:DG=PY/PI:HP=PI/2:
    PD$=STRING$(18,"="):P9=.999999:N9=-.999999:P1=.000001:
    RA$=STRING$(18,"-")+"> "
640 LA=-100:LO=-1:REM FORCE ERROR MESSAGE IF NO INPUT
650 CLS:PRINT@512,"";
660 INPUT"DO YOU WANT A DAY'S CYCLE OF ORBITS (Y/N)";AN$
670 IF LEFT$(AN$,1)="Y",F4=1:GOTO700
680 IF LEFT$(AN$,1)="N",F4=0 ELSE GOTO 660
690 REM
700 IF F4=1 PRINT"FOR WHICH SATELLITE?" ELSE
    CLS:PRINT"WHICH SATELLITE TO TRACK?"
710 PRINT"ENTER 1 FOR RS-1; 7 FOR OSCAR 7; 8 FOR OSCAR 8";CR$;:
    INPUT"ENTER 'U' TO  ACCESS USER INPUT ROUTINE";AN$
720 IF AN$="1"THEN 760
730 IF AN$="7"THEN 830
740 IF AN$="8"THEN 900
750 IF AN$="U"THEN 980ELSE 700
760 REM ****  RS-1 DATA  ****
770 PR=120.389433
780 DC=30.227
790 HT=1706
800 IN=82.5556
810 SAS="RS-1"
820 GOTO 1210
830 REM ****  OSCAR 7 DATA  ****
840 PR=114.944836
850 DC=28.737620
860 HT=1460
870 IN=101.59660
880 SAS="OSCAR 7"
890 GOTO 1210
900 REM *****  OSCAR 8 DATA  ****
910 PR=103.22726
920 DC=25.807932
930 HT=906
940 IN=99.9
950 SAS="OSCAR 8"
960 GOTO 1210
970 REM
980 REM         ENTER HERE IF NOT USING AO-7,AO-8,RS-1
990 REM
1000 CLS:PRINTTAB(20)PD$;CR$;TAB(20)"USER INPUT ROUTINE";CR$;TAB(20);PD$;CR$;
1010 PRINT:PRINT"DATA NOW ON FILE FOR: ";US$
1020 IF LEFT$(US$,1)="*" THEN PRINT"PLEASE ENTER THE FOLLOWING:"      :GOTO 1060
1030 INPUT"TYPE 'K' TO KEEP, 'N' TO ENTER NEW DATA";AN$
1040 IF AN$=""THEN 1030
1050 IF LEFT$(AN$,1)="K" THEN 1210
1060 INPUT"NAME OF THIS SATELLITE";US$
1070 IF US$=""THEN 1060
1080 INPUT"HEIGHT OF SATELLITE (IN KM)";HT
1090 IF HT<=0 THEN PRINT:GOTO 1080
1100 IF HT<200PRINT"THAT'S PRETTY LOW...BETTER DUCK!!":GOTO1080
1110 INPUT"PERIOD OF SATELLITE (IN DECIMAL MINUTES)";PR
1120 IF PR<=0 THEN PRINT:GOTO 1110
1130 INPUT"INCLINATION OF ORBIT (IN DECIMAL DEGREES)";IN
1140 IF IN<=0 THEN PRINT:GOTO 1130
1150 INPUT"WESTWARD PROGRESS OF ORBIT (IN DECIMAL DEGREES)";DC
1160 IF DC<=0 THEN PRINT:GOTO 1150
1170 IFDC>=360PRINT"THAT'S VERY LARGE..ARE YOU SURE??":GOTO1150
1180 AN$="":INPUT"IS THIS DATA ALL CORRECT";AN$
1190 IF LEFT$(AN$,1)<>"Y" THEN US$="*":PRINTCR$:GOTO1020
1200 SAS=US$:CLS
1210 REM
     RESUME MAINLINE HERE
1220 TA=-91:TL=-1:REM SET TARGET ERROR VALUES
1230 PRINTCR$;"ORBITAL DATA FOR ";SA$;" NOW AVAILABLE";CR$
1240 IF F4=1 PRINT"FOR ";SA$;", ENTER REFERENCE ORBIT'S:" ELSE
     PRINT "TO TRACK ";SA$;" ENTER:"
1250 TM=-1:INPUT
     "TIME OF NORTHBOUND EQUATOR CROSSING 'EQX' (HHMM.SS)";TM
1260 IF TM>=2400 OR TM<0 THEN GOSUB3250:GOTO1240
1270 IF TM-INT(TM)>=.60 THEN GOSUB3250:GOTO1240
1280 H=FIX(TM/100):      REM H=HOURS
1290 M=FIX(TM-H*100):    REM M=MINUTES
1300 S=TM-FIX(TM) :      REM S=SECONDS
1310 T=H*60+M+(S/.6):    REM CONVERT FROM HHMM.SS TO DECIMAL
1320 ST=T:REM SAVE START TIME FOR LATER USE
1330 CO=-1:INPUT"LONGITUDE AT 'EQX' (DECIMAL DEGREES)";CO
1340 IF CO>=360 OR CO<0 THEN GOSUB3250:GOTO1330
1350 ON F4 GOTO 1400
1355 L4=-91
1360 PRINTCR$;"LATITUDE OF YOUR STATION (DECIMAL DEGREES)";:
     IF LA>-90 THEN PRINT"
<HIT 'ENTER' TO RETAIN VALUE:";LA;" >";
1365 INPUT L4:IF L4=-91 AND LA>-90 THEN L4=LA:GOTO 1375
1370 IF L4>90 OR L4<=-90 GOSUB3250:PRINT
     "<LATITUDE MUST BE BETWEEN -90 & 90 DEGREES>":GOTO 1360
1375 LA=L4:L4=-1
1380 PRINTCR$;"LONGITUDE OF YOUR STATION (DECIMAL DEGREES)";:
     IF LO>-1 PRINT"
<HIT 'ENTER' TO RETAIN VALUE: ";LO;">";
1385 INPUT L4:IF L4=-1 AND LO>-1 THEN L4=LO:GOTO 1395
1390 IF L4>=360 OR L4<0 GOSUB3250:PRINT
     "<LONGITUDE MUST BE BETWEEN 0 & 360 DEGREES>":GOTO 1380
1395 LO=L4
1400 PRINT CR$;"*** SET OUTPUT OPTIONS ***";CR$:
     AN$="":INPUT"PRINT DATA ON LINE PRINTER (Y/N)
<'ENTER'=NO> ";AN$:
     IF LEFT$(AN$,1)="Y" THEN F5=0 ELSE F5=1
1410 IF F5=0 PRINTRA$;"HARD COPY REQUEST CONFIRMED" ELSE PRINT
     RA$;"'NO HARD COPY' CONFIRMED"
1420 ON F4 GOTO 1530
1430 ANS="":INPUT"DO YOU WISH TO SEE THE WHOLE ORBIT (Y/N)
<'ENTER'=NO> ";AN$
1440 IF LEFT$(AN$,1)="Y" THEN F2=2 ELSE F2=1
1450 IF F2=1 PRINTRA$;"'PRINT VISIBLE MINUTES ONLY'  CONFIRMED" ELSEPRINTRA$;
"'PRINT ALL MINUTES' CONFIRMED"
1460 AN$="":INPUT"TRACK FOR MUTUAL VISIBILITY (Y/N)
<'ENTER'=NO> ";AN$
1470 IF LEFT$(AN$,1)<>"Y",F6=1:PRINTRA$;"'NO  M.V.TRACK'":
     GOTO 1530 ELSE F6=0
```

Flowchart 4). Once entered, these user orbit parameters will be retained during the program run until you change them. Fig. 2 shows a typical input run.

After you have selected your bird, Orbit Track will prompt for entry of the EQX data and for selection of the various options described below. (See Flowchart 5 for Options logic). After setting your option choices, the orbit track commences.

Orbit Tracking Options

In Orbit Track there are several options that may be set or reset for each orbit computed. Flowchart 6 shows Orbit Track logic. These include listing the computed data on the line printer (hard copy), suppressing the display of data for minutes when the satellite is not visible from your station location (PRINT VISIBLE MINUTES ONLY), and tracking the orbit for simultaneous access from a second station location (M.V.TRACK). Each of these options has a default mode, which the computer will select if you respond with just an ENTER after the prompt for that option. All of the options may be set or reset before each orbit tracking operation, so you won't be stuck with a selection you don't want.

In the PRINT VISIBLE MINUTES ONLY mode, Tracker will print a single line indicating the current time and (satellite name) NOT VISIBLE until the satellite comes into the range of your station location. It then will output all data normally. When it has computed that the satellite has dropped below your horizon, it will end the tracking routine for that orbit and ask if you wish to track the next orbit of the same satellite. This is the "Sequential Tracking" feature. Fig. 3 shows the abbreviated

```
1480 T4=-91:PRINT"TARGET LOCATION LATITUDE (DEC. DEGREES)";:
     IF TA>-91 PRINT"
<HIT 'ENTER' TO KEEP  VALUE:";TA;" >";
1485 INPUT T4:IF T4=-91 AND TA>-90 THEN T4=TA:GOTO 1500
1490 IF T4>=90 OR T4<=-90 THEN 1480ELSE TA=T4
1500 T4=-1:PRINT"TARGET LOCATION LONGITUDE (DEC. DEGREES)";:
     IF TL>-1 PRINT"
<HIT 'ENTER' TO KEEP VALUE:";TL;" >";
1505 INPUT T4:IF T4=-1 AND TL>-1 THEN T4=TL:GOTO 7520
1510 IF T4>=360 OR T4<0 THEN 1500 ELSE TL=T4
1520 REM
       INPUT CONTINUES HERE

1530 FORJ=0TO500:NEXT:CLS
1540 J=1:IF LA>=0 THEN K=FIX(PR/2) ELSE K=FIX(PR):
     REM SET LOOP POINTERS
1550 ON F5 GOTO 1610
1560 AN$="":IF PEEK(14312)<128 THEN1600ELSEINPUT"PRINTER OFF-LINE..CANCEL
HARD COPY (Y/N)";AN$
1570 IF LEFT$(AN$,1)="Y",F5=1:GOTO1600
1580 IF LEFT$(AN$,1)="N",F5=0:GOTO1600
1590 GOTO1560
1600 IF F5=0,INPUT"HIT 'ENTER' WHEN PRINTER READY";AN$
1610 L2=LA:O2=LO:I2=IN:L3=TA:O3=TL
1620 ON F4 GOTO 2670:REM PRINT DAY'S ORBITS
1630 GOSUB3020
1640 ON F5 GOTO 1700
1650 LPRINTTAB(10)"SATELLITE TRACKING DATA FOR ";SA$
1660 LPRINTTAB(10)"FOR LAT:";LA;"LONG:";LO
1670 LPRINTTAB(10)"ORBIT BEGINS ";TM$;" (UTC), AT LONG:";:
     LPRINTUSING"###.#";CO
1680 IF F6=0,LPRINTTAB(10)"* = WINDOW OPEN TO LAT:";TA;" LONG:";TL
1690 LPRINT" ";:LPRINT"TIME(UTC)";TAB(16)"AZ";TAB(26)"EL";TAB(35)      "S-LAT";
TAB(44)"S-LONG";TAB(54)"DIST.(KM)";CR$
1700 REM
               PRINT THE HEADER

1710 REM
1720 CLS
1730 PRINTTAB(10)"SATELLITE TRACKING DATA FOR ";SA$
1740 PRINTTAB(10)"FOR LAT:";:PRINTUSINGI$;LA;
1745 PRINT"  LONG:";:PRINTUSINGI$;LO
1750 PRINTTAB(10)"ORBIT BEGINS ";TM$;" (UTC), LONG:";
1760 PRINTUSINGI$;CO
1770 ON F6 GOTO 1790
1780 PRINTTAB(10)"* = WINDOW OPEN TO LAT:";TA;" LONG:";TL
1790 PRINTTAB(10)"<USE  'CLEAR'  KEY TO  ABORT LISTING>":
     GOSUB3240:REM PRINT HEADER LINE
1800 IF F2=1 THEN PRINT "THIS WILL TAKE A SECOND...HANG ON";CHR$(29);
1810 REM
1820 REM          CONVERT TO RADIANS
1830 'IFLA>=90THEN LA=89.99ELSE LA=LA:IF LA>=-90 THEN LA=-89.99ELSE LA=LA
1840 LA=LA*RD:LO=LO*RD:IN=IN*RD
1850 TA=TA*RD:TL=TL*RD
1860 R=6378.1*(1-(.00335*(SIN(LA)[2))):REM
1870 F=R+HT:F3=0:LC=0
1880 T=T+(J-1)
1890 :          FOR TI=J TO K
1900 REM                    SOLVE FOR SAT. LATITUDE
1910 X=SIN(P2*TI/PR)*SIN(IN):REM
1920 IF X>=1  THEN X=P9
1930 IF X<=-1 THEN X=N9
1940 IF X=0 THEN X=P1
1950 SL=ATN(X/SQR(-X*X+1)):REM ARCSIN (X)
1960 REM                    SOLVE FOR SAT. LONGITUDE
1970 Y=COS(P2*TI/PR)/COS(SL):REM
1980 IF Y>=1 THEN Y=P9
1990 IF Y<=-1 THEN Y=N9
2000 SO=-ATN(Y/SQR(-Y*Y+1))+HP:REM ARCCOS (Y)
2010 SO=SO+((TI/4)*RD)+(CO*RD):REM
2020 IF SO>=P2 THEN SO=SO-P2
2030 REM - SOLVE FOR ANGLE BETWEEN SAT,CNTR OF EARTH,OBSERVER;
2040 Z=(SIN(LA)*SIN(SL))+(COS(LA)*COS(SL)*COS(SO-LO)):REM
2050 IFZ>=1,Z=P9 ELSE IFZ<=-1,Z=N9
2060 OO=-ATN(Z/SQR(-Z*Z+1))+HP:REM ARCCOS (Z)
2070 ON F6 GOTO2110:REM MUTUAL VIS FLAG =0 FOR CALC, 1 FOR NO.
2080 ZT=(SIN(TA)*SIN(SL))+(COS(TA)*COS(SL)*COS(SO-TL)):REM
2090 IFZT>=1,ZT=P9 ELSE IF ZT<=-1,ZT=N9
2100 OT=-ATN(ZT/SQR(-ZT*ZT+1))+HP:REM ARCCOS (ZT)
2110 REM                    SOLVE FOR AZIMUTH TO SATELLITE
2120 W=(SIN(SL)-SIN(LA)*COS(OO))/(SIN(OO)*COS(LA)):REM
2130 IFW>=1,W=P9 ELSE IFW<=-1,W=N9
2140 AZ=-ATN(W/SQR(-W*W+1))+HP:REM ARCCOS (W)
2150 XX=SIN(SO-LO):IF XX>=0 THEN AZ=P2-AZ
2160 REM                    SOLVE FOR ELEVATION TO SATELLITE
2170 EL=ATN((COS(OO)-(R/F))/SIN(OO)):REM
2180 IF EL>0 THEN F3=1
2190 ON F6 GOTO 2220
2200 ET=ATN((COS(OT)-(R/F))/SIN(OT)):REM
2210 IF F3=1 AND ET>0 THEN MV$="*" ELSE MV$=" "
2220 REM                    SOLVE FOR DISTANCE TO SATELLITE
2230 DS=SQR((F*F)+(R*R)-2*F*(R*COS(OO))):REM
2240 T=T+1:GOSUB3020
2250 IF INKEY$=CHR$(31) PRINT CR$;"*** ORBIT TRACK ABORTED ***";CR$:LA=L2:LO=O2:
IN=I2:TA=L3:TL=O3:GOTO1240:REM RESTORE VALUES
2260 ON F2 GOTO 2270,2310
2270 IF EL<0 AND F3=0 THEN PRINTTM$;TAB(14)SA$;" NOT WITHIN RANGE";
CHR$(29);:GOTO 2500
2280 IF EL<0 AND F3=1 THEN IF LA>=0 THEN 2530
2290 IF EL<0 AND F3=1 AND LA<0 THEN F3=0:GOTO 2260
2300 REM
          PRINT ONE MINUTE'S DATA

2310 ON F5 GOTO 2380
2320 LPRINTTM$;MV$;
2330 LPRINTTAB(12)USINGI$;AZ*DG;
2340 LPRINTTAB(22)USINGI$;EL*DG;
2350 LPRINTTAB(33)USINGI$;SL*DG;
2360 LPRINTTAB(43)USINGI$;SO*DG;
2370 LPRINTTAB(54)USINGI$;DS
2380 REM
2390 REM
2400 PRINT TM$;MV$;
2410 PRINTTAB(12)USING I$;AZ*DG;
2420 PRINTTAB(22)USING I$;EL*DG;
2430 PRINTTAB(33)USING I$;SL*DG;
2440 PRINTTAB(43)USING I$;SO*DG;
2450 PRINTTAB(54)USING I$;DS
2460 IF F5=0 THEN 2500
2470 LC=LC+1:IF LC>=12 THEN LC=0: GOSUB 3240
2480 REM
2490 REM
2500 :          NEXT TI
2510 IFEL>=0,J=TI:K=TI+1:FORTI=JTOK:GOTO1910
2520 IF EL<0 AND F3=0,PRINT CR$;SA$;" NOT VISIBLE THIS ORBIT"
    :IF F5=0 LPRINT SA$;" NOT VISIBLE THIS ORBIT"
2530 LA=L2:LO=O2:IN=I2:TA=L3:TL=O3
2540 PRINT"COMPUTE NEXT ORBIT OF ";SA$;
2550 AN$="":INPUT AN$:IF LEFT$(AN$,1) <> "Y" THEN 2630
2560 REM
2570 REM          ADD PR TO TIME FOR NEXT ORBIT TIME
2580 REM
2590 T=INT((ST+PR)*100)/100:IF T>=1440,T=T-1440
2600 CO=CO+DC:ST=T
2610 IF CO>360 THEN CO=CO-360
2620 GOTO 1400
2630 AN$="":PRINT"ANOTHER ORBIT FOR ";SA$;:INPUTAN$
2640 IF LEFT$(AN$,1)="Y" THEN CLS:GOTO 1230
2650 GOTO 650:REM RESTART MAINLINE, SAVE LA,LO
2660 REM
2670 REM          ROUTINE TO PRINT DAY'S ORBITS
2680 REM
2690 CLS:ON F5 GOTO 2720
2700 LPRINTTAB(10);"DAY'S ORBITS FOR ";SA$;CR$
2710 LPRINT"REF+";TAB(14)"TIME (UTC)";TAB(30)
     "LONGITUDE AT 'EQX'";CR$
2720 PRINTTAB(10)"DAY'S ORBITS FOR ";SA$
2730 PRINT"REF+";TAB(14);"TIME(UTC)";
2740 PRINT TAB(30);"LONGITUDE AT EQX"
2750 K=INT(1440/PR+.5)
2760 GOSUB 3020
2770 ON F5 GOTO 2790
2780 LPRINT"REF";TAB(14);TM$;TAB(35);CO
2790 PRINT"REF";TAB(14);TM$;TAB(35);CO
2800 FOR TI=1 TO K
2810 T=INT((T+PR)*100)/100
2820 IF T>=1440 THEN T=T-1440
2830 REM 8150 CORRECTS FOR 24HR WRAP-AROUND (24HRS=1440 MINS)
2840 GOSUB 3020
2850 CO=CO+DC
2860 IF CO>360 THEN CO=CO-360
2870 ON F5 GOTO 2890
2880 LPRINTTI;TAB(14);TM$;TAB(35);:LPRINTUSING"###.#";CO
2890 PRINT TI;TAB(14);TM$;TAB(35);:PRINTUSING"###.#";CO;
2900 IF TI<>K THEN PRINT
2910 NEXT TI
2920 PRINT@244,"HIT";:PRINT@372,"'ENTER'";:PRINT@500,"WHEN";:
     PRINT@628,"READY";:INPUT AN$
2930 CLS
2940 PRINT"COMPUTE ANOTHER CYCLE FOR ";SA$;" (Y/N)
<'ENTER'=NO> ";:INPUTAN$
2950 IF LEFT$(AN$,1)="Y"THEN 1240
2960 AN$="":INPUT
     "COMPUTE A CYCLE FOR A DIFFERENT SATELLITE (Y/N)
<'ENTER'=NO> ";AN$
2970 IF  LEFT$(AN$,1)="Y"THEN 700 ELSE F4=0:GOTO700
2980 REM
2990 REM
3000 REM          SUBROUTINE TO CONVERT TIME TO STRINGS
3010 REM
3020 H=INT(T/60)
3030 M=INT(T-H*60)
3040 S=T-INT(T)
3050 S=INT(S*100+.5)/100 * .6
3060 S=INT(S*100)/100
3070 IF S>=.60 THEN M=M+1:S=0
3080 IF M>=60 THEN H=H+1:M=0
3090 IF H>=24 THEN H=0
3100 H$=STR$(H)
3110 M$=STR$(M)
3120 S$=STR$(S):IF LEN(S$)<4,S$=S$+"0"
3130 IF H=0 THEN H$="00"
3140 IF H<10 THEN H$="0"+RIGHT$(H$,1)
3150 IF H>=10 THEN H$=RIGHT$(H$,2)
3160 IF M=0 THEN M$="00"
3170 IF M<10 THEN M$="0"+RIGHT$(M$,1)
3180 IF M>=10 THEN M$=RIGHT$(M$,2)
3190 S$=MID$(S$,3,2)
3200 TM$=H$+":"+M$+"."+S$
3210 RETURN
3240 PRINT:PRINT"TIME(UTC)";TAB(16)"AZ";TAB(26)"EL";TAB(35)"S-LAT";
TAB(44)"S-LONG";TAB(54)"DIST.(KM)":RETURN
3250 PRINTCR$;"** INPUT ERROR **":RETURN
```

nature of PRINT VISIBLE, contrasted against Fig. 4 showing the same orbit printed with the PRINT ALL MINUTES option.

Selecting the PRINT ALL MINUTES option will force Tracker to print data for the entire duration of the orbit selected without regard to the visibility of the satellite. With either option, if the program cannot find *any* time during the orbit when the satellite is within range, it will indicate that the satellite is NOT VISIBLE THIS ORBIT.

The HARD COPY option is pretty self-explanatory, but a word or two about its operation will help. The TRS-80's Line Printer routine will lock out your BASIC program if you issue an LPRINT command without a printer hooked up. To prevent this from happening and to support some of the after-market printer adapters (like the TRS-232 that I used here with my Anderson-Jacobson 841 Selectronic to type this article), Tracker samples the Printer Port for a READY signal. If it senses that the printer is off-line or that there isn't one there (the two conditions look identical to the computer), it will prompt:

PRINTER OFF-LINE . .
CANCEL HARD COPY
(Y/N)? —

Answering YES will reset the HARD COPY flag and cancel all further attempts to LPRINT. Answering NO will keep the HARD COPY flag set and will attempt to LPRINT the data requested. If you have a Centronics-type printer that uses the Expansion Interface printer port, this message will remind you to turn it on and get it ready. If you have the TRS-232 or a similar adapter that uses BASIC's Printer Device Control Block as a link to its machine language driver, this little option is not

Table 1. Symbol table for Satellite Tracker.

AN$	General-purpose input string. Contains keyboard input in response to prompts.	
AZ	Antenna azimuth calculated each minute, in radians.	
CO	Crossing longitude . . . from EQX input.	
DC	Westward precess of orbit . . . used to update CO for "Sequential Tracking" function.	
DG	Conversion constant (radians * DG = Degrees).	
DS	Distance to satellite, calculated each minute, in km.	
EL	Antenna elevation calculated each minute, in radians.	
ET	Elevation seen from "Target." Used with "M. V. Track."	
F2	PRINT LENGTH FLAG	= 1 means PRINT VISIBLE MINUTES. = 2 means PRINT ALL MINUTES.
F3	VISIBLE FLAG	= 1 means bird visible once this orbit. = 0 means bird not visible this orbit.
F4	CYCLE FLAG	= 1 means ORBIT CYCLE only. = 0 means TRACK.
F5	HARD COPY FLAG	= 1 means NO HARD COPY. = 0 means HARD COPY REQUESTED.
F6	M. V. TRACK FLAG	= 1 means NO M. V. TRACKING. =0 means TRACK.
H,H$ M,M$ S,S$, TM$,T, ST	Used in time conversion routine. Time is computed in decimal, then converted to strings for printing. H = Hours. M = Minutes. S = Seconds, TM$ = Composite.	
HT	Height of satellite's orbit, in km.	
IN	Inclination of satellite's orbit.	
PR	Period of orbit.	
LA	Your station latitude in decimal degrees.	
LO	Your station longitude in decimal degrees.	
SL	Latitude of sub-satellite point.	
SO	Longitude of sub-satellite point.	
TA	Target station latitude for "M. V. Tracking."	
TL	Target station longitude for "M. V. Tracking."	
OO	Angle, Theta, between satellite, center of the Earth, and you. Used to determine position of bird.	
RD	Conversion constant (degrees * RD = radians).	
SA$	Name of satellite being tracked.	
US$	Name of "User" satellite that has been input.	
W,X,Y, Z,ZT,P, HP,P2	Are either intermediate calculations to derive one of the above, or are system variables which do not change value.	

necessary. If you don't have a printer, this little warning may save you some grief. Remember, if you do force the issue, and don't have a printer or other adapter, BASIC will lock you out of the program for good (or at least until you RESET).

Two Tracks for the Price of One

The MUTUAL VISIBILITY TRACK option is a feature that was not in the original KIM program. If you answer YES to this option, you will be prompted to input the latitude and longitude of a "Target" location. You can use this option for things like tracking a pass to see if that G3 station can hear OSCAR 8 when you can, or even to see if your buddy in North Dakota can access the same orbits as you. You will find it convenient and easy to use, and it will make working satellite DX a lot less chancy and a lot more fun. To indicate that this option is operational, the header printout will now include:

*=WINDOW OPEN TO (LAT), (LONG)

The program printout will be modified to print an asterisk (*) next to the time column for each minute when both stations have access to that satellite. See Fig. 5 for a sample printout. Tracker will retain the location of your target station and will allow you to update it or keep it the same each time you select the M.V. TRACK option. This makes it a snap to track more than one orbit for the same target.

Additional Features

Another slick feature of Tracker is sequential tracking. To eliminate repetitive data entry (and the inevitable sore fingertips), the Orbit Track routine is programmed to compute the EQX for the next orbit in normal sequence. After tracking any orbit, the computer will prompt:

COMPUTE NEXT ORBIT OF (satellite name)?

A YES answer will tell Tracker to update the EQX data to the next orbit in normal sequence and offer you the options selection for that orbit. A NO answer will bring the prompt:

ANOTHER ORBIT FOR (satellite name)?

A YES answer will retain the satellite selected but will allow you to input another EQX and track it. Use this when you wish to skip certain orbits that are of no interest to you (like when it is 5:00 am and the satellite is passing over southern Borneo, or some other exotic port-of-call). A NO answer returns you to the main menu. To fully appreciate the versatility of the options, note that Figs. 3, 4, and 5 are tracks of the same orbit, but printed with different options.

Some Niceties

During development of this program it became apparent that some tricky timing problems can occur for stations located close to the equator. These stations may experience a "wrap-over" of a visible pass from the southern to northern hemisphere, or vice versa. To eliminate this, Tracker monitors the status of any Orbit Track listing and if the satellite is still visible as it crosses the equator, Tracker will extend its computations across the equator until it loses visibility for that pass.

Slippery-Finger-Proof, Too

Tracker also monitors the values for all user entries from the keyboard and will print error messages as appropriate. You will not be allowed to make mistakes by entering a value that is too large or too small for the desired function, and you may even find Tracker questioning your input to the User routine if the parameters don't make sense. Believe me, after playing with some programs where there is no provision for error correcting, sometimes making the en-

tire output useless, using Tracker is a pleasure. Fig. 6 shows typical input error messages, and Fig. 7 shows User Input Routine error messages.

Input/Output Conventions

It should be understood that in OSCAR tracking, longitude is expressed as West only, from 0 to 360 degrees. Latitude is expressed as either +1 to +90 or −1 to −90 for North or South, respectively. Tracker printouts follow these conventions. All longitudes displayed are West. To find the correct East longitude for numbers exceeding 180 degrees, subtract 360 from the indicated West longitude. All latitudes are displayed as *positive* numbers for North and *negative* numbers for South. Your input to Tracker should follow this convention too, or you may get some very strange results.

Tracker will compute orbits for stations in either hemisphere as long as the above standards are followed in inputting station and target locations, etc. Tracks computed for southern hemisphere stations may take a while before they show output since Tracker uses a complex iterative method to compute the data for each minute of the orbit and cannot fast-forward these calculations. Since it begins each orbit calculation at the northbound equator crossing, it must compute between 40-50 minutes worth of data before it "wraps over" into the southern hemisphere. Be patient. It's still faster than a hand calculator. Just remember that the EQX data should be entered for a northbound equator crossing regardless of the hemisphere in which your station is located.

So How Does It Work?

For you programmers out there, Table 1 is a symbol table of the variables used and their significance to the program. Each of the flowcharts shows the BASIC line numbers of the program sections on that chart and where the jumps go. In addition, operations that change variables will have those variable names shown next to them, indicating changes. You should be able to use these aids to follow the program just about anywhere in its execution. If all else fails, use the TRON function of Level II BASIC to show you the line numbers as you are executing Tracker.

Some Final Notes

Dennis and I hope that you enjoy using Tracker on your TRS-80 system. The program is written in Microsoft's Level II BASIC and can be translated into other BASICs that have the trig functions with only minor syntax changes. Versions are available for the PET (yes, it will run on the 8K version) and APPLE (16K with APPLESOFT). And the updated KIM-1 version will also be available. As interest arises, we will translate Tracker into versions suitable for other micros as well.

As indicated before, cassettes for the TRS-80 (and for the PET as well) are available from GNOME Computerworks, at the address listed under our names. The price is $10.00, postpaid, and includes a user's guide that should answer any questions this article may have left unanswered. (We have other ham software goodies available, too. Please inquire.) For now, 73 from us both, and see *you on OSCAR*. ■

Bill Vergona
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North Las Vegas NV 89030

You Still Haven't Built a Logic Probe?

— try this one

Many people who get involved in home computer systems or any other form of digital electronics at one time or another run into hardware problems. If you want to fix them yourself, you need some way to look at what's going on inside the logic.

Usually, if you want to see logic levels, you might use a simple logic probe or a high-impedence FET (Field-Effect Transistor) volt ohmmeter (VOM). If you want to see a timing relationship, you need a triggered sweep oscilloscope to see the actual timing relationship of two different pulses or signals.

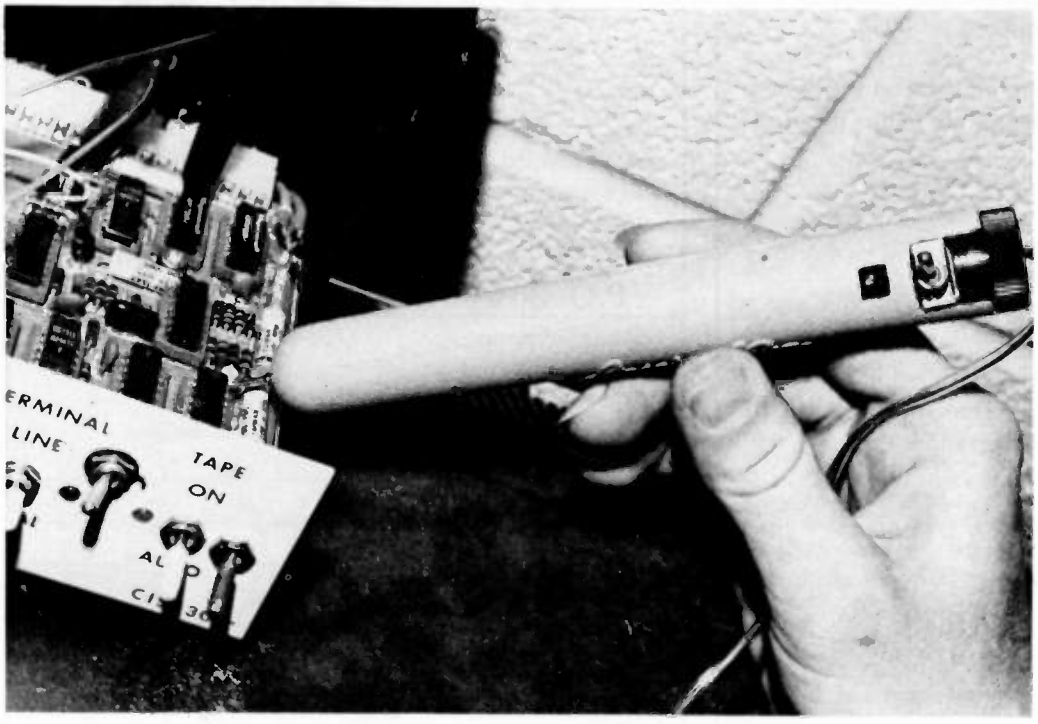
Not every home computerist can afford to buy a good scope just to look at a logic signal once in awhile, so here is a unique logic probe which can see timing relationships as well as perform the usual functions of a logic probe. It's inexpensive, with provisions for both positive and negative sync input. It can almost replace an oscilloscope in many digital applications. If you don't have an oscilloscope and can't afford one, then this logic probe is a useful substitute.

At work and at home I use my Synchronized Logic Probe to identify most logic problems easier and faster than with a scope. Many times it's too much trouble to pull out the scope, so I use this probe instead. My probe also has features missing in an oscilloscope. Did you ever try to see an 18-ns pulse on a scope when it only happens about once every 5 or 10 seconds? With a scope, such a pulse is invisible, but using a probe which stretches the pulse enables it to be seen.

This logic probe will display a P for approximately 0.75 seconds every time a pulse occurs. It also displays standard logic levels like L for a low (false), H for a high (true), and an F for a float (open). Not only that, you can synchronize it to one signal and see if another signal happens at the leading or trailing edge of the sync input. One of the nicest points about this logic probe is that you can build it for about seven dollars.

How does this work? See the schematic, Fig. 1, and the timing diagram, Fig. 2. Under all conditions, segments E and F are always enabled via the +5-volt power bus forming the left-hand vertical bar of P, L, H, or F. The first condition discussed will be the static or no-signal condition.

At this time, the probe tip



The completed Synchronized Logic Probe in action. Custom case is a cigar tube.

is connected to neither a ground nor a true value. Pin 1 of IC1A is floating (true in TTL) and pin 2 is connected to a true (Vcc) through S1 and J1 (Sync input), giving a false output of IC1A. Pin 13 of IC1D is at ground potential through R6, and pin 12 of IC1D is also true through S1 and J1, so the output of pin 11 is true. The false output of IC1A is applied to both inputs of IC1B, making its output true.

This true is applied to one input, pin 9, of IC1C. The other input, pin 10, also is true from the output of IC1D, so now IC1C has an output which is false. This false is applied to input pin 12 of IC2D. The other input is tied to the $\overline{Q}$ output of the one-shot, IC4, which is statically true. The output of IC2D is logic true, which causes segment A of the display to be lit. To complete an F, we need to light segment G and make sure segments B, C, and D are off.

Pin 9 of IC2C is true from the output of IC1D and pin 10 of IC2C is true from the one-shot, making its output false and thus keeping segment B off. Pin 3 of inverter IC3B is true from IC1, making its output false, which, when applied to IC2B, makes its output true.

This output is inverted again through IC3C and makes segment C false, thus keeping its segment off. Pin 1 of IC2A is false from IC1A, making its output true and lighting segment G; this output is also inverted by IC3D, keeping segment D off. Thus, segments A, E, F, and G are lit while B, C, and D are off, giving a display of F (float).

Now that we have seen the float condition and the basic operation, I am going to explain the logic true or high condition. When a logic true is present at the probe tip, it is applied to pin 1 of IC1A, making its output false. This false output is applied to both inputs of IC1B, making its output true, which is then applied to pin 9 of IC1C.

The probe tip input is also applied to pin 13 of IC1D, making its output false and this being the other input to IC1C, thus makes its output true. This true which is applied to one input of IC2D along with a true on the other input from the $\overline{Q}$ output of the one-shot makes the output of IC2D false, which turns segment A off. Pin 9 of IC2C is false from IC1D, making its output true and lighting segment B. Pin 4 of IC2B is true from the inverted output of IC1D, making the output of IC2B false, which is inverted by IC3E, lighting segment C. Pin 1 of IC2A is false from the output of IC1A making the output of IC2A true, which is used to light segment G and is also inverted by IC3D which keeps segment D off. Now we have segments B, C, and G lit, while segments A and D are off. Remember that segments E and F are always on and thus the display of H for a static true.

As for the low condition, all segment outputs are opposite except for segment A, which remains off. Pin 1 of IC1A goes false, making its output true. This is inverted by IC1B, so a false is applied to pin 9 of IC1C along with a true from the output of IC1D. This makes the output of IC1C true. This is then applied to pin 12 of IC2D, along with a true from the $\overline{Q}$ output of IC4, which makes the IC2D output false. This keeps segment A off.

A note about the low condition: When you first apply the probe tip to a logic false signal, the changing state of IC1A through IC3A triggers the one-shot, making the $\overline{Q}$ output false. This, in turn, enables segments A, B, and G regardless of the other inputs and also disables segments C and D, thus displaying a P for approximately .75 seconds before going to an L display. This can be viewed as a self-checking way to see if

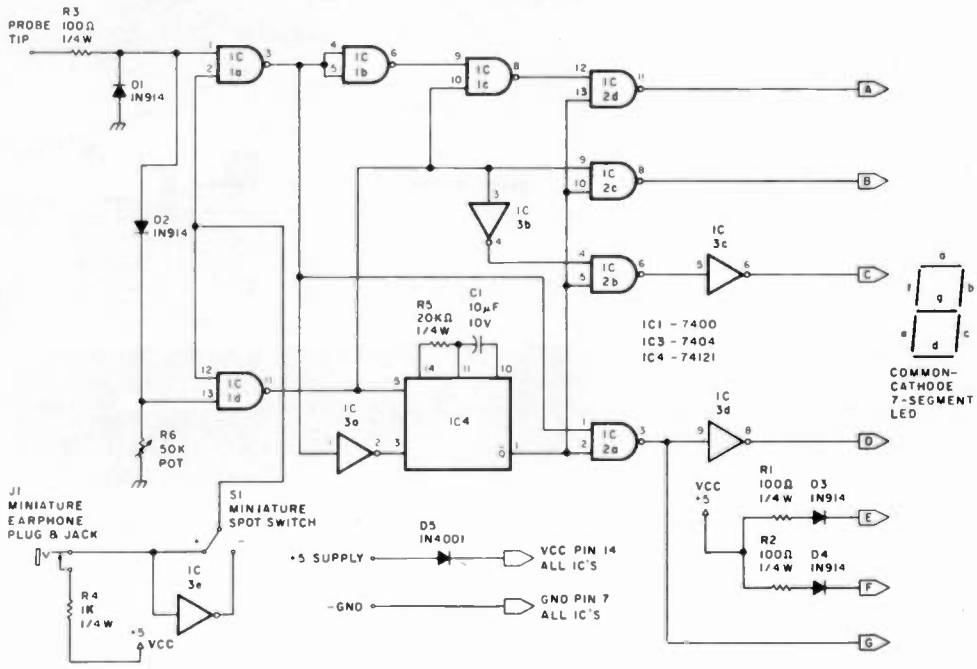


Fig. 1. Schematic diagram of the Synchronized Logic Probe.

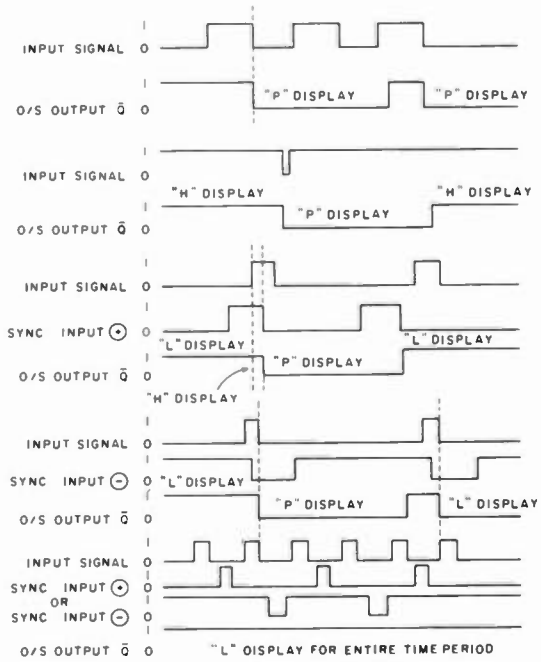
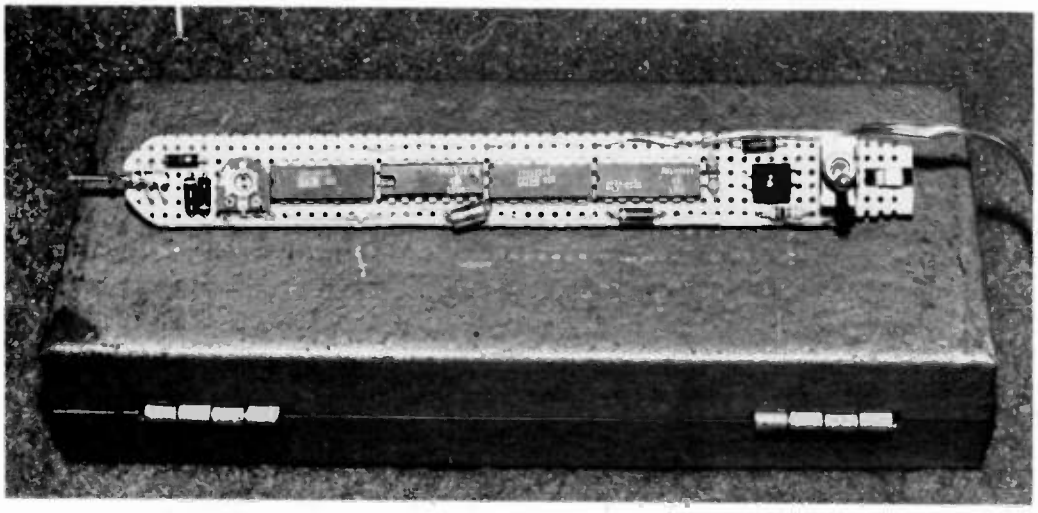


Fig. 2. Timing diagram for logic probe.



Components are mounted on 0.1" perfboard shaped to fit inside cigar tube.

the pulse circuit is working. Whenever there is a high-to-low transition at the input of IC1A, the one-shot will be triggered and a P will be displayed until a constant state is reached. This covers the generation of the H, L, P, and F display conditions. Note that the length of the P display can be changed by varying R5 and/or C1.

This brings us to the operation of the sync input. Under normal conditions (not using sync), switch S1 is kept in the positive (+) position, thus applying a logic true to one input of IC1A and IC1D. When the sync-pulse input is used, the logic true is disconnected from the switch input and replaced by the sync-input signal.

First the positive sync input will be discussed. When using the positive sync input, this means that we are looking for a signal at the probe tip which is either occurring at the leading edge (low-to-high transition) of the sync pulse or during the true state of the sync pulse. When the sync pulse is true, it is applied through the switch and enables the inputs to both IC1A and IC1D. If the signal you are looking for at the probe tip becomes true at the same time or during the time of the sync pulse, a P will be displayed, indicating that the logic true was present. This is accomplished by the changing states of IC1A and IC1D which trigger the one-shot, IC4. If the signal you are looking for was not true during the sync pulse time, an L will be displayed and remain.

When using the negative sync input, this means that you are looking for a signal at the trailing edge of a sync pulse or during the time that the sync is false. The first thing to do is to move the switch (S1) to the negative position. When the sync pulse goes low at its trailing edge, it is applied to pin 11 of IC3E, making its output true and thus enabling IC1A and IC1D. If the input signal goes true during that time, the pulse circuit is triggered and a P is displayed, indicating that the pulse was there at that time. When you are not using a sync input, switch S1 must be kept in a positive position or the normal probe functions will not work correctly. Also, when the sync input is used and the probe tip is floating, a P will display if the sync input is active.

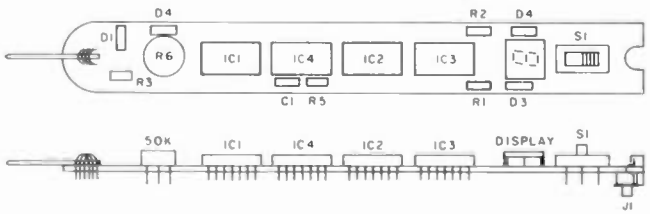


Fig. 3. Synchronized Logic Probe component mounting.

Construction

Fig. 3 and the photos show the complete circuit of the Synchronized Logic Probe, but there are a few things that might prove to be helpful. The prototype of this probe was built using 0.1" perfboard which was cut and shaped to fit inside a cigar tube prior to mounting any of the components. Wire buses were used for the +5-volt and ground connections for the chips and other components. As shown in Fig. 3, you should mount the display, switch, and sync jack on the end of the board first, and make any necessary cutouts on the tube housing and board. Make sure that switch S1 is easily accessible and sticks up through an opening in the tube.

There is only one adjustment on the probe—the 50k variable resistor used to establish the F state. When you get the probe assembled, connect it to your power supply and note that there is a legible display (L, H, or F). You should adjust the potentiometer until an F is displayed with no connection to the probe tip. Once this is obtained, you will notice that there is a range of adjustment before the display changes from an F to an L or H. This adjusts the sensitivity of the probe tip to a logic high or low.

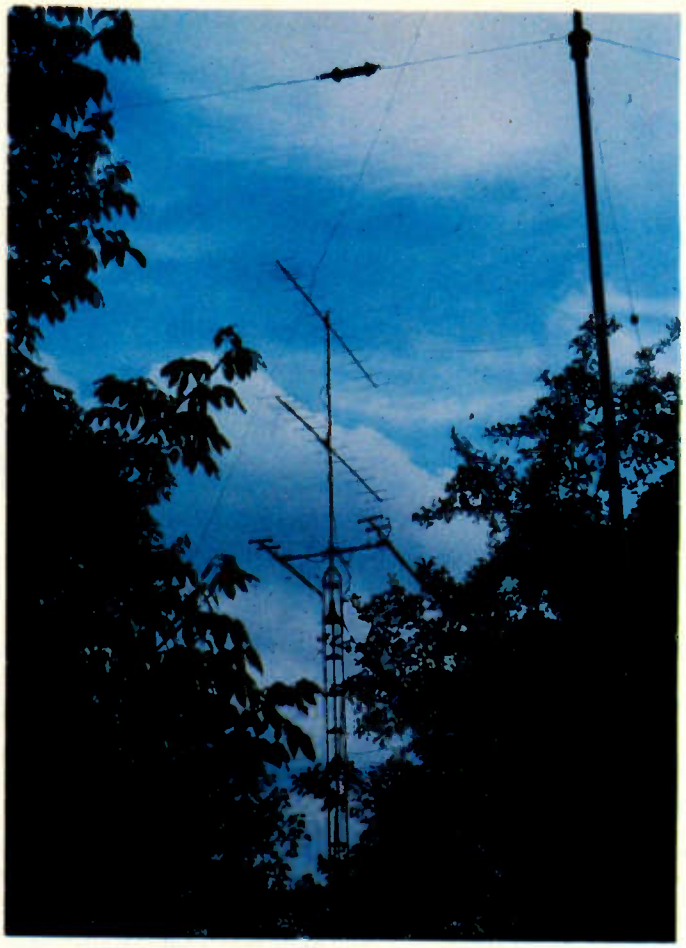
Upon completion, touch the probe tip to the +5-volt side and then to the ground side of the power supply that you are using. The probe should display an H when touched to the +5 volts. A P should be displayed for approximately .75 seconds when first touched to ground, before going to an L display. If a P is not displayed when the probe tip is first touched to ground, the pulse circuit is not functioning correctly. As long as the other displays are correct, then the problem should be in the one-shot (IC4). Check the external capacitor and resistor connections to the chip. If the other displays do not work correctly, then you will have to troubleshoot the entire circuit.

A neat trick for troubleshooting can be used if you have a display with a decimal point: Connect a piece of wire approximately 10 inches long through a 100-Ohm resistor to the decimal point and use it for a simple probe. If you touch the wire to a logic high, the decimal point will light, and if it is a low the decimal point will stay off. The 100-Ohm resistor in series with the wire is to prevent burning up the decimal point.

I used this basic logic probe when troubleshooting the more sophisticated, Synchronized Logic Probe. This, along with the circuit operation and schematics provided, should give you everything you need to build and troubleshoot the Synchronized Logic Probe. Good luck! ■

Microwave operation from Pack Monadnock means excellent range and great views of the New Hampshire countryside for the W1FC crew.

Up, up, and away. The cherry picker is pressed into service so that the microwave signals can clear the trees easily in all directions.



Visitors to Miller State Park shook their heads in disbelief as they saw erected arrays like this one for two meters.

had been molded into a comprehensive organization dedicated to winning the June VHF QSO Party. Each band was under the direction of a manager who oversaw the installation and then the operation. Other experts handled the liaison with park officials, telephone and power companies, and the very essential food tent.

The 1980 June contest was the Barnstormers' first effort involving a cherry picker snorkel truck. Arrays for 2 meters, 220, and 432 went up in minutes on 20- and 30-foot towers guyed to nearby rocks with packing twine. The cherry picker, borrowed from a Boston area firm for the weekend, was just one example of how the W1FC gang makes the most of available resources.

By 1978, the W1FC contesters had developed excellent stations and operating techniques for the frequencies below 2 gigahertz. In 1979, a year of hard work paid off when they were able to operate on 2.3, 3.4, 5.7, and 10 GHz. One setup remained on Pack Monadnock while others were sent traveling to nearby states so that five sections could be worked on each of the new bands. The efforts paid off. The score was a record one that outdistanced the nearest competitor by more than 20,000 points.

A rules change made the 1980 contest even more challenging. This year they needed five complete microwave stations, each capable of operating on four bands. The collection of gear required was probably the largest amount of amateur microwave equipment ever assembled in this country. Once again, the resources and skills of the Barnstormers prevailed.

At the last-minute strategy session, there was talk of setting another record—one that nobody could break. The friendly euphoria of setting up was gone. The mood grew serious. "Keep your stations transmitting all the time, always turning the antennas!" The operators on the populated six- and two-meter bands were expected to keep the rate up. Suddenly, the pep talk was over and it was time to begin.

The spirit of W1FC was expressed by one operator who gazed proudly at a remote 1296 rig which he had helped to build. He said that last year they made 19 contacts on 1296 and that this year the goal was 25. I noticed that he had a six-pack in hand as he headed for the shack (which was someone's van the rest of the year). It would be a long night of calling, hoping, and thinking about what could be done for 1981.

Conclusion

On the low bands, cynics abound. They claim amateur radio is dead. It is said that we are guilty of being appliance operators, that the gentlemen's camaraderie is long gone, and even that the fun has left ham radio. Visit or talk to a VHF contester; he or she will tell you a far different story. ■

Sell 'Em with Slides

— A/V shows can fire club enthusiasm

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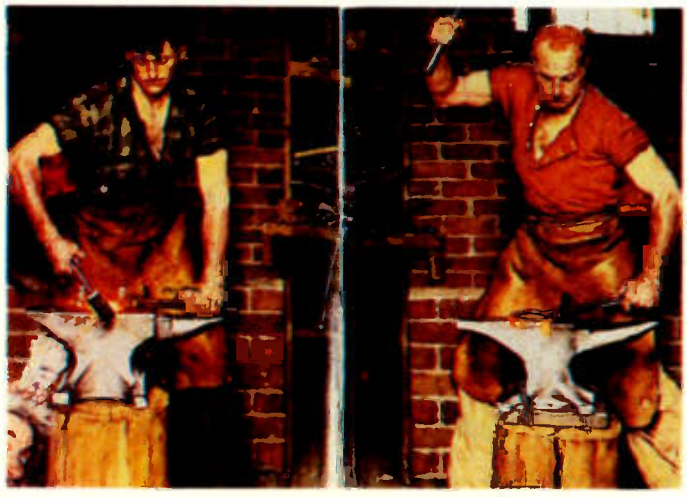
St. Joseph MI 49085

"Let's put on our thinking caps and produce one hamfest that will really draw a crowd."

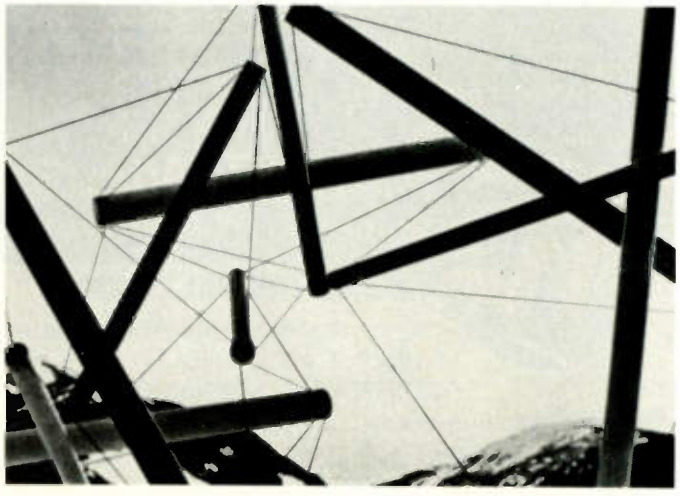
When I was named chairman of the Blossomland Amateur Radio Association's 1980 hamfest, I had some new ideas. To make sure they would be accepted, to thwart the potential wet-blanket-thrower every group seems to have, and to light a fire of enthusiasm under our club, I decided to promote our hamfest with a big kickoff.

For background, let me explain that the hamfest the year before had been held in an unheated county fair exhibition hall on a cold October Sunday. More than a few of us went home with the sniffles. That, plus the fact that I wanted to produce a little more than a flea market, prompted me to look for a new and better site for our 1980 function.

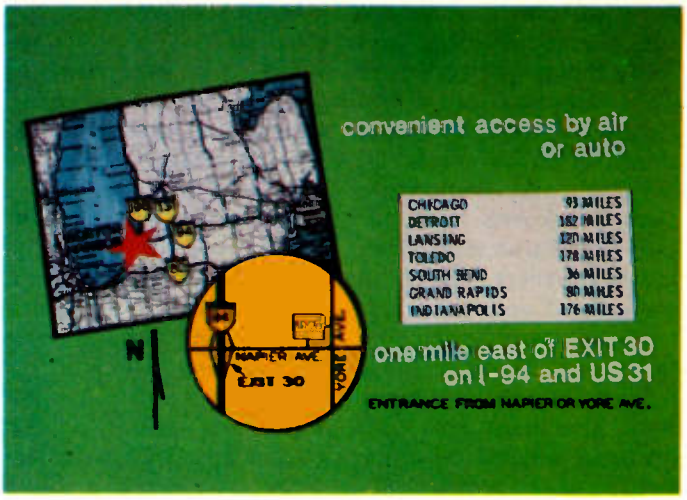
The logical site, in my estimation, was Lake Michigan College's new Community Center near Benton



"How about a brass-pounder's contest?"



"Let's let the club experts give a lecture on antenna design."



"It's conveniently located to Chicago, South Bend, and Kalamazoo . . ."

"The place we should hold our 1980 Blossomland ARA Hamfest is the beautiful new Lake Michigan College Community Center."

"That's the plan for the 1980 Blossomland Blast—the biggest and best hamfest yet in southwestern Michigan!"

Harbor, Michigan. Not only did it offer us the chance to double our floor space, have heat or air conditioning as needed, and have separate areas for tech sessions, movies, and flea market, but also its location just one mile off exit 30 of I-94 was more convenient than last year's.

I checked with the College. Would the Community Center be available for Sunday, October 5, the traditional day for the Blossomland Fest? A sigh of relief—Linda Castle, the director of the Center, said the date was still available. Next crucial question: How much would it cost? Just as I had suspected—about double what we had spent the previous year. That would require a little selling job to the club members.

First, I gathered a nucleus of club members I knew would support me, and we arranged for a tour of the Community Center to make sure it would meet our needs. On February 18, Jon WA0TAQ, Matt WA3LOP, Craig WB8VKA, Al W8LRM, and I were given a tour by Mrs. Castle. Fantastic! The center had more than twice the space of our previous site; plenty of electrical outlets; handy access for our dealers and distributors to unload and load large quantities of ham gear; a catering service to provide food; and our choice of one, two, or three beautifully carpeted lecture rooms in addition to the flea market area. They even had 2,500 paved parking spaces.

So far, so good. Now to prepare a presentation for the next club meeting to forestall any negative ideas . . . and to generate enthusiasm for our 1980 hamfest.

I decided an A/V (audio/video) show with lively music and a script supported by slides would sell the idea to the club. First I wrote the script, beginning with the negative aspects of our previous site, moving on to possible plans for a bigger hamfest with technical sessions, and then presenting the Lake Michigan College facility as the perfect setting for our 1980 "Blossomland Blast," as I decided to call it.

Once I had written and rewritten the script, I jotted down some notes on possible slides to illustrate my points. Armed with script and a list of pictures, I took off down Washington Avenue to the Lincoln Township Library. I made a beeline to the photography section and selected a dozen or so books of photographic art pictures. I set up camp at a table and flipped through each book, page by page. When I spotted a picture I thought would illustrate a point (sometimes humorous, sometimes not), I would put that book aside. Within two hours I had the pictures I wanted and checked the books out.

I was spared the task of shooting the slides myself. We're privileged to have a professional photographer in our club, whose studio shoots the ham gear pictures for the Heathkit® catalog. Jim KA8GIX volunteered to make the slides for me and did a super job.

Naturally, not all the slides I needed were to be found in books. I wanted supporting proof that our club could afford the higher rent. First, I did a survey of hamfest ads for amateur magazines. I discovered that our 1979 ticket prices had been way below average. If we raised prices just to the average and maintained attendance, we would be able to cover our expenses. And with a little added promotion, we would be able to show enough profit to keep our repeater rig going for another year, which was the original intent of the hamfest.

I made up some charts, a rough sketch of the Community Center's floor plan, and a map showing access. Another club member, Floyd K8ZLO, arranged to have some beautiful graph-

ics done, and those also became slides.

When I got the slides, I put them in the projector and started a tape. The music I had selected for background music was Billy Joel's "Root Beer Rag," a very lively instrumental that I knew would generate enthusiasm. Then I ran through the slides and script, timing them to the music, changing slide sequence here and there, until I had the time down pat.

I practiced a number of times before the meeting to make sure I knew when to hit the slide changes (wishing I had the bucks to have it pulse-controlled). On meeting night, our club president, Larry W5VUF, arranged for me to have the last spot on the business agenda so that I could talk to potential volunteers for hamfest duty while we broke for refreshments.

My spot came, the lights went out, and I launched into a short, snappy six-minute presentation with the script I had memorized, the music, and the slides.

When the lights came on, there was a fair round of applause. Co-chairman Jon WA0TAQ and I passed out a prepared sheet to each member. On it I had written up a sample program for our planned hamfest—an ARRL movie (if I could get it), a slide-show tour of the Heathkit factory (if I could shoot it), an XYL program, lectures, and demonstrations by experts from our club or the area. At the bottom of the sheet I had typed out a list of requests—typing help, volunteers to take posters and flyers to other fests, volunteers to make signs, give ideas, etc. I put my name and address at the bottom of the sheet.

The enthusiasm was great. If there had been any wet blankets waiting to be tossed because of the high rent (or who knows what), they weren't in evidence when the membership voted to expend the necessary funds to hold our October 5 Blossomland Blast at Lake Michigan College. It was unanimous.

I enjoyed the slide show so much that I've since done another on our club's first transmitter hunt, using the folksong "The Fox" for background music. I'm going to do another on our Field Day activities for another club meeting. Slide shows are fun to do, and they can add a new dimension to your club's meetings. ■

Slide	Narration
Churchill holding up two fingers in Victory sign	In the past, the Blossomland Amateur Radio Association has held *two* hamfests each year.
Modern art skeleton	They were pretty bare-bones affairs—basically flea markets where everybody came...
Modern art junk pile	to look at everybody else's used gear, kick the tires, and then go home.
Crowd of 1910 kids	This year let's really draw a crowd to our Blossomland Hamfest...
Kid with weird hat	let's put on our thinking caps and produce one hamfest that will...
Large crowd with motorcycle cops	really draw a crowd.
Girl watching puppet show	Let's really put on a show...
Man with huge 5¢ sign	and give ticket buyers their money's worth!
Squiggly art work	We could give demonstrations on slow-scan TV.
Old-timer at typewriter	Or show people how RTTY works.
Two blacksmiths	How about a brass-pounder's contest?
Boat and flooded sign	Hutch WB8WLS could give a presentation on emergency operations...
1920's rig	Neil WD8MAW, would you like to head a program on contest operations?
Rube Goldberg contraption	We could have a slide and sound tour of the Heathkit factory.
Modern art spider web	Let's let the club experts give a lecture on antenna design.
1910 school kids	We'll send our ticket buyers home a little wiser than they came, with a program like this.
"Etc." cartoon	Those are just a few ideas. With the talent we have in this club, there's even more that we can do.
Packed football stadium	A hamfest like this will draw a crowd, so we'll need a place to put them.
Nutty tractor driver	The place I'm thinking of has plenty of free, paved parking—2,500 spaces, in fact!
Men with electronic gizmo	It's a place that will attract a lot of dealers and distributors to display their wares.
Kid with hamburger stuffed in mouth	The place I have in mind even has a food catering service...
Crazy sheriff	and its own security force.
Map with distances	It's conveniently located to Chicago, South Bend, and Kalamazoo.
Lake Michigan College Community Center	The place we should hold our 1980 Blossomland ARA Hamfest is the beautiful new Lake Michigan College Community Center.
Floor plan	14,400 square feet of space, more than double what we have had in the past—with separate areas for movies and lectures. All the space we need to put on a first-class hamfest!
Baby crying	Now you're asking, "How much is this going to cost?"
Less-than-$650 slide	Including tables, chairs, setup and security, less than $650. But you're asking, "Where will we get the money?" Take a look at this...
Chart—1979 hamfests	a survey of 1979 hamfests shows that our ticket prices were well below average.
Chart—1979 sales, projected sales	Last year we brought in $1,266.00 in ticket and flea market sales. If we have the same attendance in 1980 and raise our prices to the average (and that's only the 1979 average), we'll bring in $1,817, more than enough to meet the increased expenses. Of course, if we put on a great fest and promote it, we could double attendance.
Chart—promotion	How can we promote our hamfest? First, with a mailing to last year's ticket buyers; second, a mailing especially for clubs; third, ham magazine ads, press releases, and photos to area newspapers; next, television and radio talk shows. What about a QSO party to promote our fest? Later I'll be giving you flyers to send out with your QSL cards. We'll have flyers to give dealers who will be attending. Finally, you'll receive mike-side fact sheets you can use to promote our hamfest when you make a contact.
Club's Bumblebee with Blossomland Blast logo	That's the plan for the 1980 Blossomland Blast—the biggest and best hamfest yet in southwestern Michigan! See you on Sunday, October 5.
KA8GIX slide	I'd like to give special thanks to Jim KA8GIX for the photography...
K8ZLO	and to Floyd K8ZLO who provided the graphics.

The Power Waster

— adjustable electronic load for power supply testing

John Roos K6IQL
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Thousand Oaks CA 91360

Testing of bench power supplies, batteries, voltage regulators, or current limiters often requires application of an adjustable load to the circuit. After years of connecting haywire combinations of resistors together to test various power supplies, I determined that a really high-power adjustable electronic load would be a welcome addition to my test equipment. In short order the Power Waster was created, and during some three years it has proven most useful.

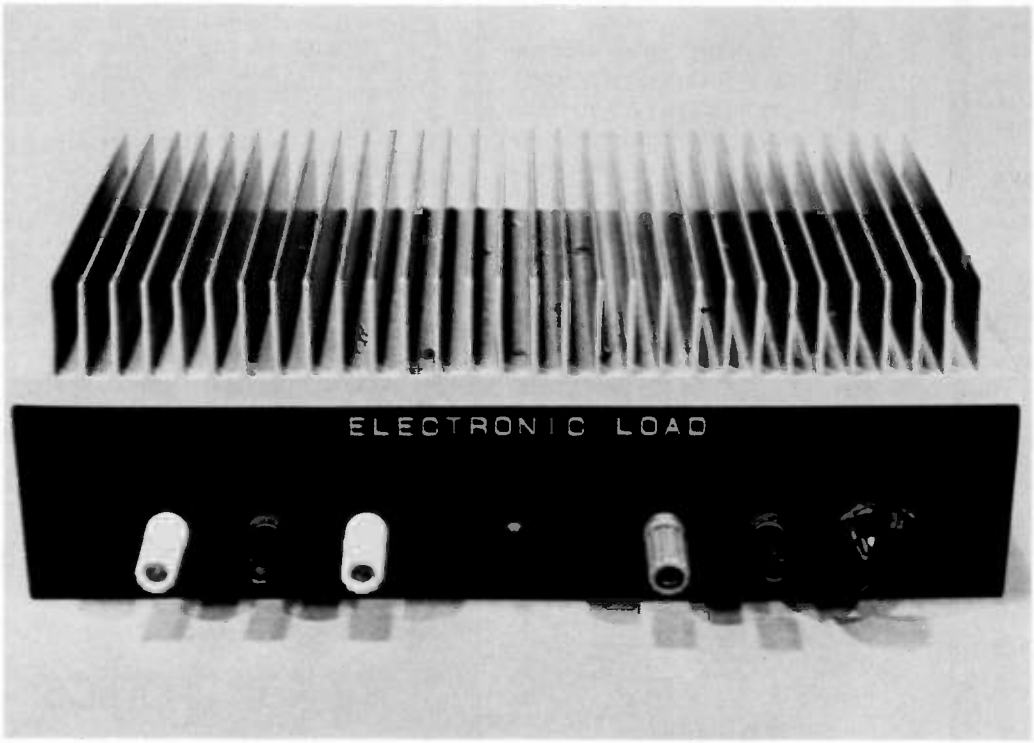

Photo A. The Power Waster. This electronic load is adjustable from 0 to 10 A and can dissipate up to 300 Watts. The unit is built upon a piece of heat-sink extrusion and has both reverse polarity and thermal overload protection.

The load described in this article will handle the majority of amateur radio and microprocessor power supply tests. In addition, it has a number of other uses, such as constant-current battery charging.

Current drawn by the load is adjustable from 0 to 10 Amperes. Input voltages up to 30 volts are permitted at full current; that's 300 Watts dissipation! Heat sinking of the pass transistors is sufficient to permit 300-Watt operation for about ten minutes, at which point a thermal protection switch shuts the current off.

At 100 Watts dissipation the heat sink is adequate for indefinite operation. By directing a small blower at the heat sink, I have run the load at 300 Watts for hours without difficulty.

Since I desired essentially self-contained operation, I included a small supply in the unit to bias the load transistors. Current is controlled by means of a front panel pot, and reverse polarity protection is included. A front-panel LED indicates operation of thermal shutdown circuitry. I took advantage of extra heat sink area to add two 8-Ohm, 50-Watt resistors. These are used for testing audio amplifiers or to increase the dissipation capability of the Power Waster circuit.

Circuit Operation

The simplified schematics in Fig. 1 are useful in understanding how the circuit operates. Commercial load boxes use current sensing and feedback to set the load current. My approach is simpler and uses the constant-current collector load-line characteristic of all bipolar transistors.

Fig. 1 shows the basic idea. The base of Q1 is biased at several volts from voltage source V1. The collector supply (V2) is greater than V1 by at least 1 volt. The voltage at the emitter of Q1 is one diode drop (0.7 V) below the base voltage, and the circuit is essentially an emitter follower. Emitter current is set by dividing the emitter voltage by R1. As R1 is decreased, the emitter current increases.

The collector current for any transistor is simply alpha (the common-base current gain) times the emitter current. As alpha is essentially equal to 1 for any modern transistor, we see that setting the emitter current also sets the collector current. And this is the point; the collector current is determined only by the emitter current. Collector voltage has almost no effect on the collector current, provided the transistor is kept from saturation or breakdown. Saturation occurs if the collector voltage becomes less than the base voltage. Breakdown will occur if any excessive voltage is applied.

The constant-current collector load line is a useful property. If the voltage across R1 is small compared to the collector supply, a lot of power can be controlled and will be quite independent of the collector supply voltage. If a relatively low base-bias voltage is used, most of the power will be dissipated in the transistor and relatively little in R1.

As useful as this circuit is, there are some disadvantages. The main problem is that R1 must be a variable resistor capable of handling the entire load current. In a practical circuit, this becomes a 0.2-Ohm pot rated for 10 Amperes, which is an expensive item.

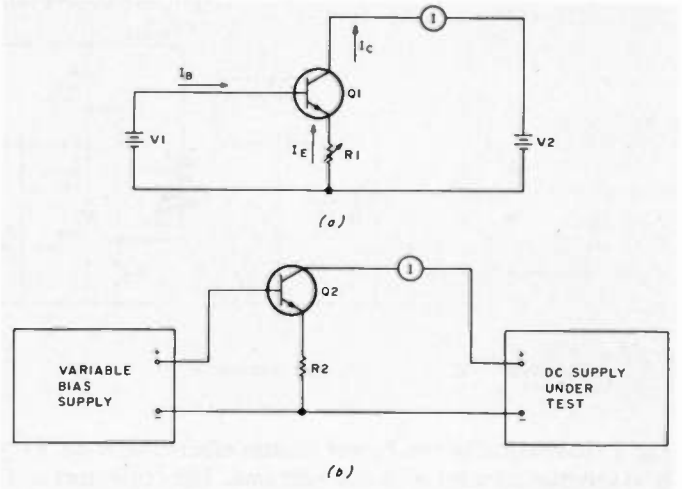

Fig. 1. Constant-current bias circuits. (a) A transistor with fixed base voltage. Collector current is set by emitter resistor. (b) Basic circuit of the electronic load. Emitter resistor is fixed, and both emitter and collector current are controlled with base-bias supply voltage.

By arranging the circuit as indicated in Fig. 1(b), things become a bit easier. Resistor R2 is a fixed high-power resistor. The base supply is made variable. Since the circuit is essentially an emitter follower, the emitter voltage follows the base voltage. Increasing the base bias increases the emitter voltage and the emitter current through R2. This increases the collector current to the desired value.

Within limitations, the collector current is set solely by the base-bias voltage and the value of R2. These limitations are: The collector supply must be at least one volt more than the max-

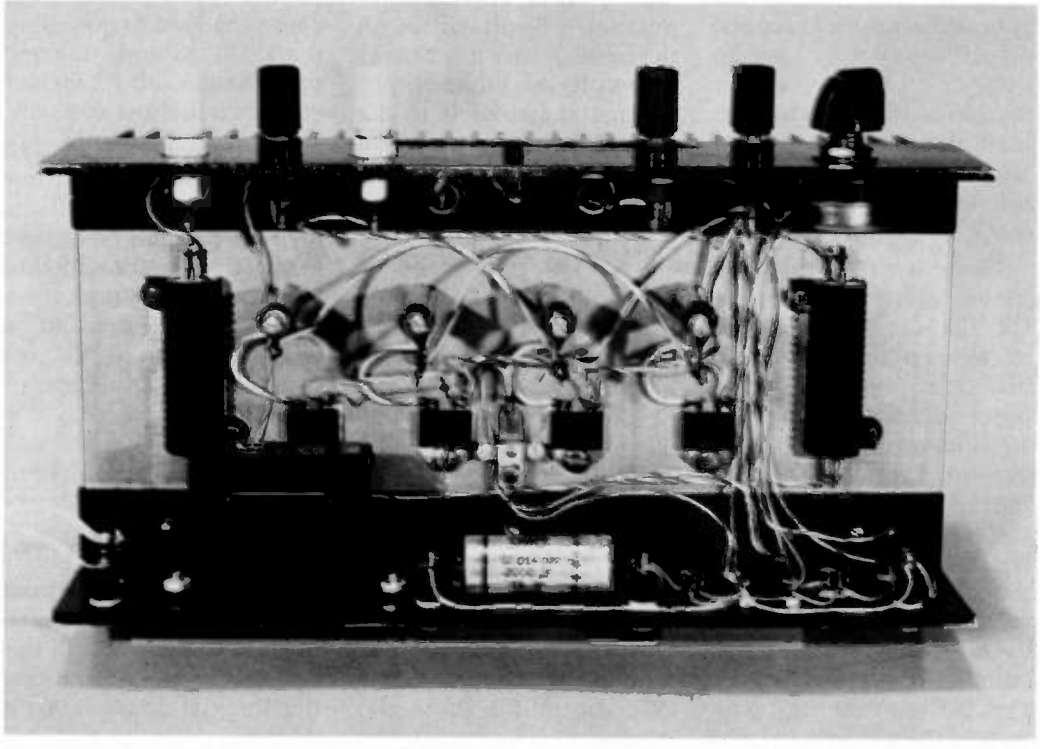

Photo B. Interior view of the Power Waster. Four TIP 35C load transistors are mounted to the heat sink. The thermal switch is located between the two center transistors. A U-shaped chassis is formed from the heat sink and two pieces of aluminum angle stock.

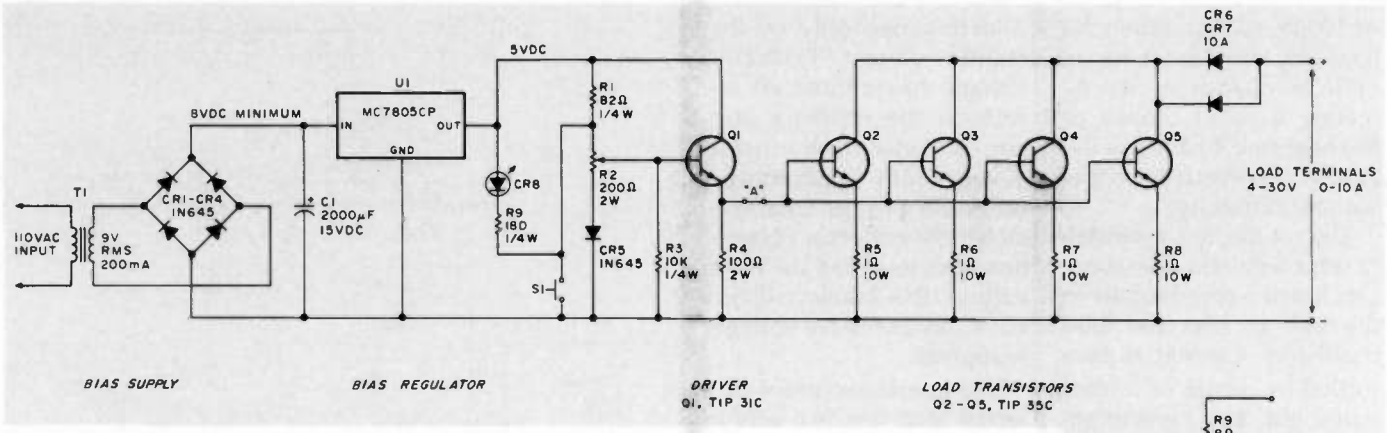

Fig. 2. Schematic of the Power Waster electronic load. S1 is a 75° C NO thermal switch. S1 is in thermal contact with the heat sink. The collectors of Q2-Q5 are connected directly to the sink. LED CR8 indicates thermal shutdown. Jumper at point A is opened in test.

imum base-bias voltage, and must be less than the transistor breakdown voltage for the current drawn.

In addition, it is assumed that the base-bias supply is capable of supplying increasing current to the transistor base as the collector current increases. The base current will be the transistor collector current divided by beta, the common emitter current gain. Beta will vary from 10-50 for practical power transistors.

To convert these ideas into the final design, I had only to add a base-bias supply, circuit overload, reverse polarity protection, and to increase the number of load transistors to handle the required power. The result is shown in the schematic diagram.

Power is dissipated in the pass element (consisting of Q2, Q3, Q4, and Q5 connected in parallel). Four TIP 35C transistors are used in order to safely handle the 10-Ampere maximum load current. Each pass transistor has a 1-Ohm resistor in the emitter which corresponds to R2 of Fig. 1. In addition to setting the collector current for a given base voltage, these resistors also equalize the load distribution between the four pass transistors and help to keep the load current constant as the transistor temperature increases.

Variable base voltage for the load transistors is obtained from emitter follower Q1 which operates from a 5-volt regulated supply. This circuit consists of transformer T1, the bridge rectifier (CR1-CR4), C1, and an MC7805CP three-terminal regulator chip (U1).

The base of emitter follower Q1 is connected to a variable voltage divider consisting of R1, the pot (R2), and diode CR5. R1 and CR5 limit the driver base voltage range to approximately 0.8 to 4 volts. An additional 0.8-volt offset in the base-emitter junction of Q1 results in a driver output voltage range of 0 to 3.2 volts. Restricting the drive voltage to 3.2 V sets the maximum current the load will draw to 10 A. CR5 was included to compensate for the change in the base-to-emitter threshold voltage of Q1 as the temperature changes. In use, this simple bias supply has proven completely adequate. There is very little drift in load current as the temperature increases.

Some additional features are worthy of mention. Diodes CR6 and CR7 provide reverse polarity protection. A thermal switch (S1) shorts the base-bias supply and turns the current off if the heat-sink temperature becomes excessive. An over-temperature shutdown is indicated by illumination of the LED (CR8).

R4 provides a return path to the transistor emitters for collector-to-base leakage current. This assures that they will actually turn off when the base-bias voltage is removed. R3 is there for safety in case the wiper of R2 opens. This is the usual method of failure for pots. Inclusion of R3 assures a path from base to emitter for the collector-to-base leakage current of Q1. In its absence, failure of R2 could cause the load to pull more than 10 A and damage something. With R3 included, the circuit just shuts off.

A series-connected pair of 8-Ohm, 50-Watt resistors is also mounted on the heat sink of the electronic load. These are provided to increase the dissipation capability of the unit and, in addition, are handy for testing audio amplifiers.

Power Rating

While the nominal input capability of the Power Waster is 10 A at up to 30 V, it may be operated at higher voltages if the proper conditions for safe operation are understood. In this section, I will explain how the nominal power rating is derived.

All high-power transistors have a "safe area" of operation, in which no damage will occur. Fig. 3 is a safe-area curve for a single TIP 35C. This is a plot of maximum-permitted collector current as a function of collector voltage. Operation at any point in the region below and to the left of the curve will not damage the transistor. Combinations of voltage and current above and to the right of the curve will certainly destroy the transistor.

It is interesting that the power dissipation capability is not constant. At a Vce of 5 V, a current of 25 A is permitted. That's 125 Watts. But if the voltage is increased to 50 volts, only 1 Ampere is allowed, providing a dissipation capability of only 50 Watts! The successful designer of high-power transistor circuits stares long and hard at the safe area curves before picking a final configuration!

When I designed the Power Waster, I tried to be conservative so that it could really take abuse without failure. Thus, four TIP 35C transistors were used. In Fig. 4, the composite safe-area curve for the four devices in parallel is shown. This is Curve B. Curve A indicates the "rated" operating envelope for the Power Waster. Only at the 10 A and 30 V point does the "rating" curve approach the safe-area curve.

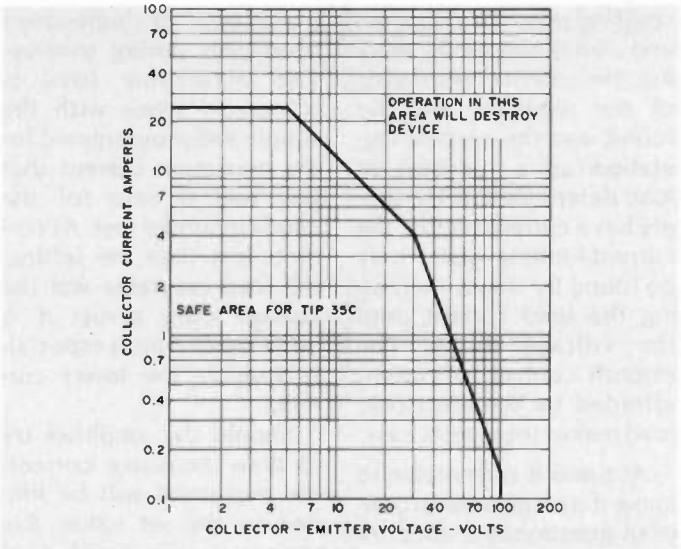

Fig. 3. Safe-area curve for TIP 35C. Safe operation is limited to the area below and to the left of the curve. Operation beyond the safe area will destroy the transistor.

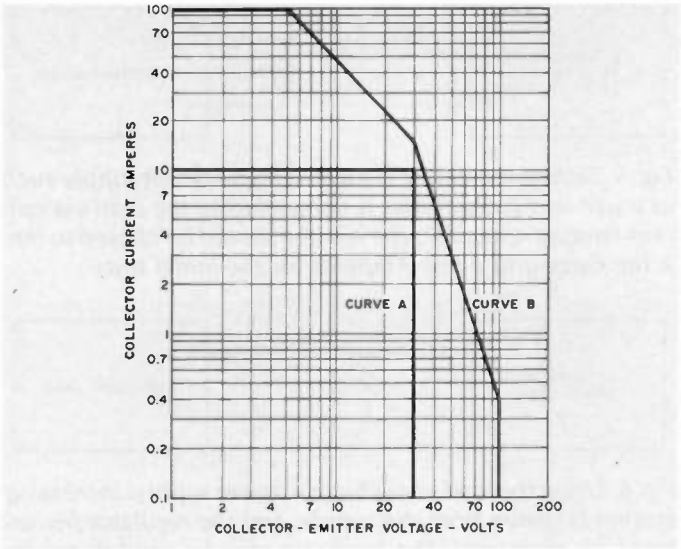

Fig. 4. Operating areas for the electronic load: Curve A indicates the rated operating area for the load. Curve B shows the composite safe area of the four TIP 35C transistors used as the load element. The rated operating area (Curve A) is well inside of the safe area.

At all other combinations of current and voltage, the power dissipation is comfortably inside of curve B.

This conservative design assures that the unit will never fail as long as the 10 A and 30 V maximums are observed.

Construction

Construction of the electronic load can take almost any form because of the non-critical nature of the circuit. In most cases, the shape of the heat sink will determine the final configuration. In order to dissipate 300 Watts, a sink having a thermal resistance of 0.1° C per Watt is required. This is a truly massive piece of metal. I elected to depend upon thermal inertia to permit short tests of up to ten minutes duration and to let the thermal cutout act if things got too hot. Continuous operation is obtained by directing a small blower at the heat sink.

I used a 5" × 11" piece of heat-sink extrusion having 32 one-inch-high fins as a chassis. To this I fastened a pair of 0.75" × 2" pieces of angle to form a U-shaped chassis with the fins on top. All parts are mounted on the underside of the extrusion, and the front and rear panels are formed by the pieces of angle. Vertical fins are more efficient, of course, but since a cooling fan is required to obtain the full power rating, this arrangement is quite convenient.

Parts located on the front panel include the three binding posts for the 8-Ohm resistors (R9 and R10). These are at the left end of the panel. Next is the LED over-temperature indicator. Adjacent to the LED are the input terminals for the electronic load. The load current adjustment pot, R2, is on the extreme right end of the panel.

Mounted directly to the underside of the heat sink are the two 8-Ohm resistors, the four emitter resistors for the load transistors, and transistors Q2 through Q5. The thermal switch (S1) is located in the center of the sink. Two reverse-polarity protection diodes (CR6 and CR7) are also mounted directly onto the heat sink near the center of the front panel. All parts are mounted to the sink by threaded holes tapped directly into the extrusion. The cathode ends of CR6 and CR7 are connected to the sink via threaded mounting holes. In the same way, the collectors of Q2-Q5 are screwed directly to the sink. Thus, the connection from the polarity protection diodes to the transistor collectors is via the heat sink itself. Fastening the transistors to the sink without insulating wafers puts the entire chassis at the potential of the positive supply input.

Normally, I would have insulated the transistor collectors from the sink but there is a good reason for not doing so. The thermal impedance of the transistor junction to case is 1° C per Watt. Most insulating wafers have a thermal resistance of at least 0.5° C per Watt. If a wafer were used, the resistances are summed to yield a thermal resistance of 1.5° C per Watt. The junction temperature would rise by fifty percent! Instead, I elected to have the positive supply input on the sink and to exercise caution in using the unit. The low voltages involved certainly pose no shock hazard.

On the rear panel are located: the power transformer, bridge rectifier, filter capacitor, 5-volt regulator, and the driver transistor (Q1). The transformer is located at the left end of the rear panel. The filter capacitor is in the center of the panel as is the bridge rectifier, which is hidden by the capacitor in the photograph. Adjacent to the filter capacitor is the 5-V regulator and the driver circuit components. U1 and Q1 are both fastened to the rear panel for cooling. All small parts such as resistors, capacitors, and diodes are mounted with push-in Teflon terminals. Threaded standoffs are used for the larger components.

Not everyone who wishes to build this circuit will be able to find a heat sink similar to the one I used. One approach is to use four smaller sinks and to mount a load transistor on each. A suitable configuation would use four Wakefield Engineering type NC-423 heat sinks. Individually, these units have a thermal resistance of 0.8° C per Watt so the resistance of the combination would be 0.2° C per Watt. Such an arrangement would permit inputs of about 150 Watts without forced-air cooling.

Testing

A few simple tests prior to using the load will prevent damage to it, or to the circuit being tested. First, break the circuit between

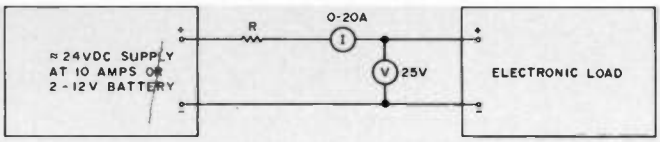

Fig. 5. Testing the Power Waster. A high-current supply such as a pair of 12-V batteries is connected to the load via current-limiting resistor R. The resistor should be chosen to limit the current to a few Amperes for the initial tests.

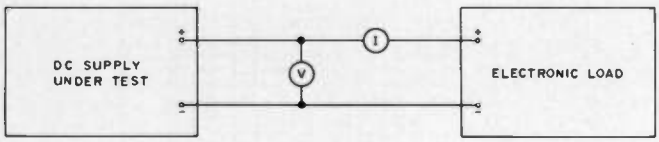

Fig. 6. Using the load to evaluate a power supply. Increasing current is drawn from the supply, and the regulator performance is measured. The load also may be used to ensure proper current-limiter operation.

the driver transistor (Q1) and the load transistors (Q2 through Q5), at point A in Fig. 2. Apply 110 V ac to the power transformer and verify that the voltage is variable from about 0 to 3.5 V as R2 is rotated. Zero volts should occur at the extreme counterclockwise position of R2. This is the zero current setting.

Reconnect the circuit at point A. Then arrange a high-current test setup similar to Fig. 5. Resistor R is chosen to limit the current to 3 or 4 A under short-circuit conditions. Two automobile headlamps in series may be used for this resistor. Set the current control pot (R2) at minimum (CCW position) and turn on the supply and the bias supply in the Power Waster.

Increase the current setting until 2 A is drawn by the load. Measure the voltage drop across R5 through R8 and assure yourself that the voltages are about equal. About 0.5 V should appear across each resistor for a 2-A load. If no voltage appears, then the associated transistor is not drawing any current.

Next, advance the current control. The load current should increase smoothly until the voltage at the load input terminals drops well below 5 V. At this point the load transistors will saturate and the current will be set by resistor R.

The next step is to test the current-limiting feature to verify that the load current is limited to about 10 A. Reduce R in value so that for the supply voltage present under load, about 15 A may be drawn. Again increase the load current from zero with R2. The load should current limit at 9 to 11 A if the same parts values were used.

If all of the above tests were successful, the electronic load is ready for use.

Applications

My purpose in building the electronic load was to enable rapid test of power-supply circuits. The 10-A and 30-V input capability will suffice for almost the entire range of solid-state supplies found in amateur equipment. After I built the load, a number of other applications surfaced. Some of these are worthy of mention.

The performance of a voltage regulator is easily plotted by using the load, connected as indicated by Fig. 6. The regulator is connected to the load via an ammeter. A voltmeter is connected across the output of the supply. By increasing the load current and noting the meter reading, the internal resistance of the regulator may be found, and the percent regulation as a function of load determined. If the supply has a current limiter, the current-limiting point may be found by slowly increasing the load current until the voltage drops. The smooth control of current afforded by the electronic load makes these tests easy.

At times it is desirable to know if a surplus transformer of questionable ancestry can meet a given requirement. Of particular concern is the "overhead" voltage requirement. This is the input voltage required to maintain a regulator in operation (at full load) subtracted from the output voltage.

Typical three-terminal regulators require a 3-volt overhead to function properly. If all circuit parameters are known, it is easy to determine if a certain transformer, rectifier, and filter capacitor will work. If junkbox parts are used, the calculation is often difficult or impossible. It takes only a few minutes to connect up the unregulated supply parts and apply the expected load current using the Power Waster. The unregulated voltage and ripple may be measured, and the suitability of the components determined.

Battery charging is another application. All batteries must be charged from a current source so the charging current is held constant as the battery terminal voltage increases. To use the load as a battery charger, simply connect it in series with a source having a voltage at least 4 V greater than the full-charge voltage of the battery. Then place the combination in series with the battery and dial up the desired charging current.

One final application is protection of high-power transistors during tune-up. The electronic load is placed in series with the supply and programmed for the maximum current that you feel is safe for the amplifier under test. At currents less than the setting, the load saturates and the voltage drop across it is quite small. This is especially true at the lower currents.

Should the amplifier try to draw excessive current, the maximum will be limited to the set value. Response is very rapid. Current limiting occurs in about a microsecond and in the case, is much faster than a normal power-supply current limiter. So effective is this method of protection that I have built it into several solid-state transmitters.

Conclusion

Electronic loads are common in professional labs where power supplies are developed. Many are built from scratch, but also they are sold by commercial test equipment manufacturers. Such devices permit evaluation of supplies prior to connecting them to their intended (and often very expensive) loads.

In writing this article, I have attempted to describe the application and operation of a little-known but very useful piece of test equipment. While my Power Waster is certainly austere as compared with the professional units, it will definitely do the job. The basic design could be modified to include meters and an internal cooling fan. If this were done, the complete unit could be packaged in a well-ventilated box where the heat sinks would be better protected from accidental contact.

I welcome comments or questions from anyone wishing to either duplicate or modify the circuit. ■

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QRZ Sunshine

— building solar-powered repeaters

Photo A. AARC repeater. Photovoltaic array is visible on the left side of the shack at the base of the tower.

A totally solar-powered repeater recently went on the air in Maryland. On March 15, 1980, the Anne Arundel Radio Club (AARC) switched from 110 V ac to sunshine to power a new 220-MHz repeater recently installed at the AARC site in Davidsonville, Maryland, near Annapolis. This unique microprocessor-controlled repeater will itself be the topic of a forthcoming article, as soon as its builders get around to writing it up.

The Site

The repeater is located at an abandoned Nike missile site which was provided to AARC by the local Davidsonville Family Recreation Center. A ready-made clubhouse and a 10m-high structure (former radar pedestal) at one of the highest points in the area offer an ideal location for this active and public-service-oriented amateur radio club. A 3m × 3m repeater shack was built atop the pedestal and a 40m antenna tower was added. At the present time, the club operates both a 2-meter repeater (147.105/147.705) and the 220-MHz repeater (223.88/222.28) and is planning to install a 430-MHz ATV repeater in the near future.

The repeaters offer reliable and convenient communications within the Washington, Baltimore, Annapolis, and central Chesapeake Bay area. Many of the club members are avid boaters, and during the boating season maintain a weekend weather net which also provides real-time information to the National Weather Service about the rapidly changing weather conditions on the Bay.

Photovoltaics

Photovoltaic (PV) panels, which convert sunlight into electricity, were provided by the Department of Energy in response to a request from the AARC in December, 1979. The panels were shipped to the club on loan from the Jet Propulsion Lab in Pasadena, California, in late February, 1980. (Who says government can't react quickly?) The PVs were part of a DoE research-and-development program to improve PV technology and reduce production costs.

The PV array consists of 14 individual panels, made by Sensor Technology Corp., each about .3m × .6m × .03m, attached to a 1.3m × 2.3m frame made of pressure-treated lumber. The frame is fastened directly to the south side of the repeater shack at a 53° angle (from the horizontal) which will optimize electric generation during the winter. Each panel is rated about 18 V at 0.55 A, and with the panels connected in parallel, the array was expected to produce about 18 V at 8 A (at noon on a sunny day).

Output voltage for this particular panel is somewhat temperature-sensitive, but at a constant temperature, it is fairly independent of current draw up to the rated current, whereafter it falls very rapidly to a maximum short-circuit value of 0.62 A per panel. A check of our 14-panel array showed a maximum short-circuit current of 8.7 A. Even on a very cloudy day, the array produces about 0.5 A, which is more than adequate to provide the repeater's standby current draw of around 300 mA.

The 14-panel array is expected to produce almost 400 Watt-hours during an average December day, while in June it should be almost twice that amount. The array converts only about 6 percent of the sunlight falling on it into electric energy (actually the individual cells are about 10-percent efficient, but there is considerable open area between each cell in the panel). This should be sufficient power to run the repeater without auxiliary power, year-round, hopefully for the next 10 years, the panel service-life design goal.

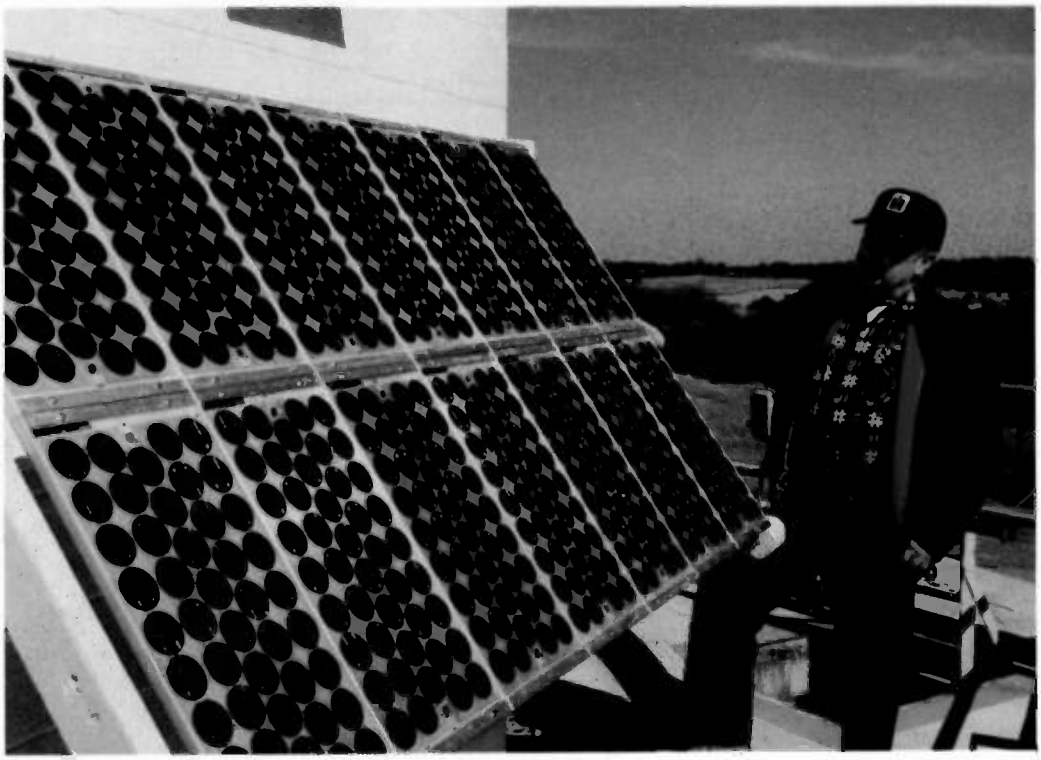

Photo B. Photovoltaic array. Frank Troutman WB3CLF helped install the array on the side of the shack.

Power Conditioning and Storage

Since the repeater requires 12 V dc around-the-clock, and the array produces 18 to 25+ V dc for only part of the 24-hour cycle, some sort of power-conditioning and energy-storage system is needed. A simple system was designed to provide high reliability and efficiency at a low cost. It consists of a 16 V (13-cell, 20-Ah) primary nicad battery storage module, charged directly by the PV array through an overcharge protector. A 12-volt (60-Ah) secondary-storage auto battery is diode-isolated from, and trickle-charged by, the nicad battery.

A clock attached to the transmitter measured an average daily transmit time of about two hours. At a transmit current of 3 A, the average daily transmit power is 6 Ah, and at the .3 A standby level, another 7 Ah is consumed. Thus, the total average daily power consumption is around 13 Ah at 12 V dc (156 Wh/day). While the array output of 400 Wh would appear to be more than sufficient to power the repeater, there are major energy losses built into the system which must be taken into account.

Batteries are less than 100-percent efficient, and the trickle-charge circuit dissipates an appreciable amount of energy. If we assume an average battery efficiency of 80 percent and a trickle-charge rate of 700 mA, we end up with only about 170 Wh being delivered to the repeater, which just slightly exceeds its anticipated demand of 156 Wh/day. It must be remembered that this was calculated for the worst part of the year (December), and in any event, the fully-charged 12-V battery should have enough capacity to run the repeater for at least four consecutive cloudy days.

During the design and testing of the power-conditioning and storage equipment, it was found that current and comprehensive technical information on lead-acid and nicad batteries was very difficult to obtain. Building a battery-charging circuit may appear at first to be a simple task. But to build one that does not damage the battery, seriously degrade its performance, or doom it to an early death is not really as straightforward as one might expect.

An excellent handbook has just become available on this topic entitled *Handbook for Battery Storage in Photovoltaic Power Systems*, February, 1980. The 120-page handbook was prepared for the Department of Energy by Bechtel National, Inc., and contains a wealth of engineering data on most types of rechargeable batteries. It includes a section on advanced batteries now under development primarily for electric vehicle applications. The handbook is well-referenced and includes an extensive listing of battery manufacturers, suppliers, and developers. A limited number of copies are available at $9.95 (including handling and postage) from: Moonraker East, Publications Department, Box 117, Riva MD 21140.

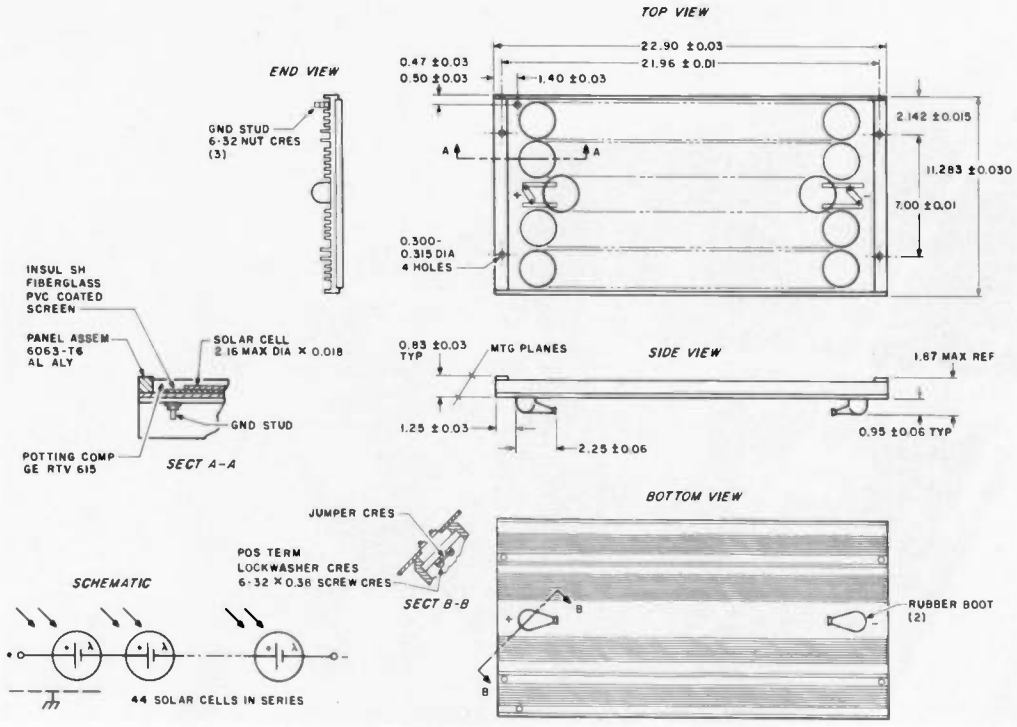

Fig. 1. Diagrams of PV module.

Design Considerations

A simple constant-voltage charging circuit was considered, which would have eliminated the need for the 16-V nicad battery by connecting the PV array directly to the 12-V auto battery through a regulator. While the overall efficiency might have been slightly better, the design was rejected for several reasons:

1) The lead-acid auto battery would discharge continuously at night due to the power demands of the repeater, with the terminal voltage falling to about 11.5 V by dawn. The PV array would then start to charge the battery with currents rapidly increasing to almost 9 Amps and, as the battery attained full charge, its terminal voltage would climb to about 15 V. This wide swing in supply voltage was not considered conducive to stable repeater operation, or to extended battery life.

2) Nicad batteries are much better suited for repeated charge/discharge cycling and are far more resistant to damage from overcharging.

3) The two-battery circuit provides an almost constant supply voltage to the repeater by continuously trickle-charging the lead-acid battery around the clock, not just when the sun is out.

4) The two-battery circuit design appears to be much more fail-safe in that a regulator failure would not cook the lead-acid battery, as it could in the simple circuit. Component failure in the two-battery circuit likely would result in a decrease in repeater performance noticeable over a period of days, allowing time to correct the problem rather than resulting in a sudden complete repeater failure.

This last consideration is an important factor in the operation of our repeaters, since routine inspection of the system is limited by the requirement that someone must climb the 10m structure, and thus periods of unattended operation of a month or more are expected. But this is all just theory and we should know much more about the reliability of our solar-powered repeater in a year or so.

PVs: Current Technology and Future Potential

The principle of the photovoltaic effect was discovered by Edmond Becquerel back in 1893, but useful energy conversion devices have been available only for the last 25 years. An early PV application was in photographic exposure meters. The first breakthrough in PV cell manufacture for electric power generation was made by researchers working at Bell Laboratories in 1954. Subsequently, high-reliability single-crystal silicon PVs were used as an energy source for U.S. and Russian space vehicles thoughout the 1960s. A few terrestrial PV devices were marketed on a trial basis as early as 1959 using silicon cells rejected by the space program as not meeting NASA's high-reliability requirements, but the first PVs designed specifically for terrestrial use were not produced until 1973. Thus, we are dealing with a very new product only recently available in the marketplace, and it is probable that PV applications will grow rapidly in the coming years, especially if anticipated tenfold PV cost reductions can be achieved.

Photovoltaic cells have much in common with transistors and utilize semiconductor technology to convert light into electricity. They consist of a junction of semiconducting material formed by one of three methods: (1) adding impurities (dopants) to one side of a pure material (homojunction); (2) joining two dissimilar semiconductor materials (heterojunction); (3) joining a semiconductor to a metal (Schottky junction).

The combination of materials creates a potential difference across the junction, with the materials on each side of the barrier having different electrical characteristics. One side has excess negative charges and is called n-material, while the other side has excess positive charges and is called p-material. Absorption of light in the semiconductor energizes the negative and positive charges and creates an electrical current when the absorbed energy is greater than the material's energy bandgap.

Fundamental restrictions of quantum physics limit the portion of the sun's spectrum which can be utilized by solar cells and the efficiencies which are achievable. Thus, each different cell design has a unique performance characteristic across the spectrum of sunlight from ultraviolet to infrared. Light with energy below the material's bandgap is insufficient to generate a current; light with energy above the bandgap produces energy equal to the bandgap, with excess energy resulting in heat which must be dis-

sipated. The direct-current electricity that is produced is collected by a contact grid imprinted on the surface of the cell.

The capability to control the energy bandgap and the electrical characteristics of the materials on each side of the barrier is fundamental to the science and art of photovoltaic cell design. Particularly for terrestrial photovoltaics, the technical problem is to construct and control these sophisticated material characteristics in a mass-production process.

Manufacturing of the cell, or a module (panel) of cells, is complete when anti-reflection coatings and protective encapsulants are applied. Single-layer anti-reflection coatings can reduce average reflective losses from 40 percent to as little as 10 percent, and double-layer coatings can further reduce reflective losses to about three percent. Glass, plastic, or silicone encapsulants seal the panel of cells against environmental elements and are a key factor in determining the useful life of the cells. The output of a terrestrial solar cell in peak Watts (Wp) depends on the daily insolation in each location.

On a clear day, the sun's energy reaches the Earth at a rate of about one kilowatt per square meter. This is equivalent to the energy contained in a gallon of gasoline for every 10 minutes the sun shines on an area the size of a tennis court. Even with the low efficiency of today's solar cells (say, 10%), 60 square meters of cells with adequate storage under optimum conditions can provide the needs of an average single-family residence (6 kWp, 700 kWh per month). Unfortunately, such an installation would be far too expensive for an average homeowner. For example, at a PV module price of $10/Wp, the cost would amount to $60,000 just for the PVs, and the installation, energy storage, and power conditioning equipment would be extra.

That is precisely why the Department of Energy is spending over a billion dollars on a 10-year program to develop the technology and production techniques needed to reduce the cost of PVs to $.50-$1.00/Wp by 1986. By then, utility electric rates will be considerably higher and PVs should be able to compete on a sound economic basis. But what are DoE's chances of pulling this off, you might ask? Of course, no one really knows, but DoE is fairly confident that the price goal can be achieved. So much is happening in the PV field (advances in competing cell materials such as silicon, cadmium sulfide, gallium arsenide, encapsulation improvements, better and lower-cost manufacturing techniques being developed) that it is just too early to attempt to select the best technology/manufacturing mix. The next few years may bring several major breakthroughs in PV material technology providing lower-cost cells and in developing cells with much higher efficiencies.

One particularly promising avenue of PV research involves the use of lenses or reflectors to concentrate the light striking the PVs. Concentrations equivalent to many thousands of suns have been tried with very encouraging results. A recent breakthrough was achieved with one type which is called a thermophotovoltaic cell, which reached an efficiency of 26 percent. This particular device utilizes concentrating mirrors to focus the light on a spectral converter which absorbs the full spectrum of sunlight, then reradiates the energy at specific wavelengths which match the optimum operating bandgap of the cell. Ultimately, 30- to 50-percent efficiencies are expected.

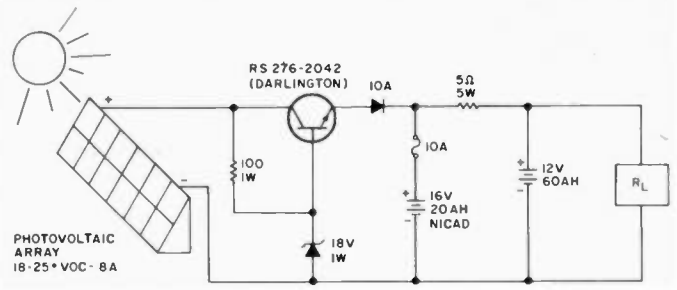

Fig. 2. Power conditioning and storage circuit.

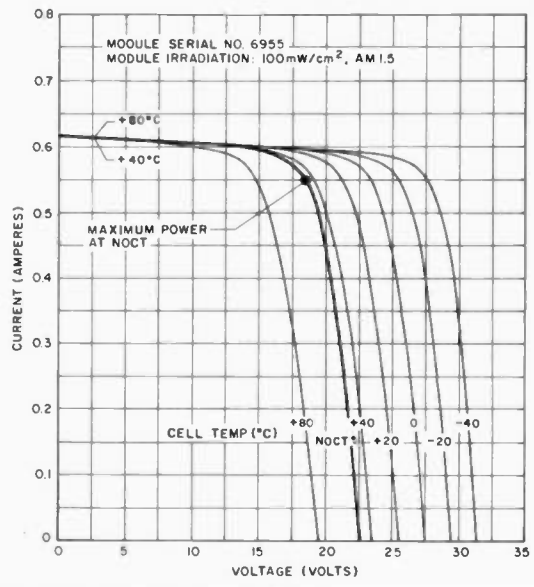

Fig. 3. Specifications of photovoltaic array.

Much of the R-&-D effort on concentrating PVs has been privately supported, and it is still too early to tell just how much of a competitor they will be to flat-plate non-concentrating options. But the overall trend is plain; the immense potential of PVs is no longer just theoretical, and the question now appears to be one more appropriately stated in terms of how long will it take PVs to capture a significant market share.

Photovoltaics and Repeaters

The use of PVs to power amateur repeaters provides us with new opportunities to locate our repeaters at sites which offer better coverage, but which otherwise may not be usable because of a lack of electricity. PVs with battery storage also provide a much greater degree of communications reliability during local emergencies accompanied by commercial power outages (as is often the case). Although many repeater clubs are equipped with auxiliary generators, it is often not easy to find a member who is willing (or able) to hurry over to the repeater site in the middle of a flood or blizzard, start up the generator, and keep it running during an extended power outage.

At the present time, high cost is one of the major problems hindering use of PVs by amateurs. Eventually, prices will come down, but it will take a number of

years, and in the meantime our repeaters will remain dependent on external power. This is a situation where a little creative groundwork could be of great service to amateur radio. Here's how: The Congress is very anxious to accelerate the commercialization of PVs and for the past few years has appropriated millions of dollars over and above agency requests with the intent of stimulating PV manufacture and use. But it is not always easy for the administration to effectively utilize all of the funds; hence, most deserving PV projects have been welcomed with open arms.

Amateur radio spokesmen could approach the newly-created Federal Emergency Management Administration with a proposal to solar-power a number of repeaters throughout the country, to strengthen the nation's emergency preparedness. The Federal Emergency Management Administration, in cooperation with the Department of Energy, might provide the PVs at no cost to repeater clubs as part of the PV accelerated commercialization program. The whole program could be coordinated at the user end by the ARRL.

The federal cost of a program to solar-power 1000 repeaters based on today's PV prices and a collector system similar to ours would be less than $5 million. This is a pretty small part of a billion-dollar PV program budget, and not only that, the real benefit the nation would gain from such a program would far outweigh its very modest cost. So how about it, ARRL, is anybody there in Newington listening? ■

Transmitter Tune-Up for Blind Hams

— an audible indicator for power out

James D. Burney WA4LBX
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Florence AL 35630

Blind hams have used a variety of devices to tune their transmitters, with the conversion of visual indications to audio tones being the most common approach. A blind friend, W5KUY, recently asked me to build a coupler to insert in his coax to sample the rf voltage. This voltage would be used to drive a voltage-to-frequency converter. After looking at his converter with its three transistors and two transformers, I decided to build a more up-to-date version to go with the new coupler.

The audible tuning aid described in this article operates on the assumption that maximum power trans-

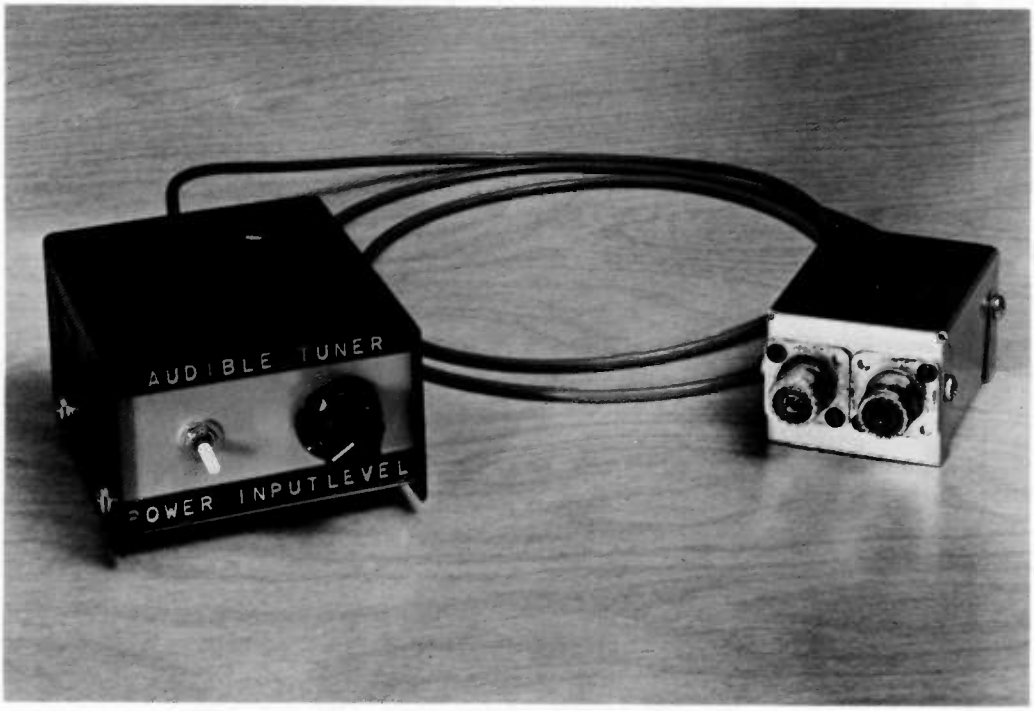

Photo A. Complete audible tuning aid.

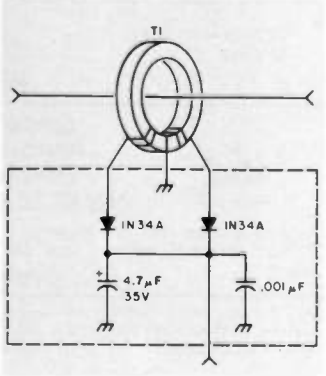

Fig. 1. Rf coupler. T1=60 bifilar turns #30 enameled wire, center-tapped, on an Amidon T-68-2 toroidal core (see text).

fer from the transmitter to the antenna will occur when the transmitter is properly tuned. Rf power is sampled by inserting a coupler similar to the ones found in wattmeters into the feedline following the transmitter or linear amplifier, if one is used. The coupler is connected by a length of shielded microphone cable to a voltage-to-frequency converter constructed around a 555 timer IC.

The circuit for the rf coupler is shown in Fig. 1. It is built in a 2-3/4" × 2-1/8" × 1-5/8" minibox. Two SO-239s are mounted next to each other in the small end of the box (Photo B). A two-inch length of center conductor and inner insulation from a piece of RG-8/U is prepared by removing a half inch of insulation from each end and bending the bare wire at right angles on each end, so that it fits into the center contacts of the SO-239s.

The rf transformer is wound on an Amidon T-68-2 core. To make the transformer, take two lengths of #30 enameled wire, each five feet long, and twist them together with about five turns per inch. Wind 60 turns of this twisted pair on the core. You will find that 30 turns will fill the core when the turns are evenly spaced. When these turns are on, continue winding the remaining 30 turns over the first layer until all 60 turns are in place. Trim the ends to about three inches and untwist them back to the core.

Scrape the insulation off of all four ends to within an inch of the core and locate the start and finish ends of each wire with an ohmmeter. Twist the start end of one wire and the finish end of the other together to form a center tap. Slip the toroid over the wire from the RG-8/U that you previously prepared; it should be a snug fit. You now have an rf transformer with the center wire constituting the primary and the secondary consisting of 120 turns, center-tapped.

Mount a three-lug terminal strip in the center of the large side of the box and an RCA phono jack and ground lug set in the end opposite the SO-239s. Solder the center wire of the transformer to the center terminals of the SO-239s. The center tap of the secondary is soldered to the center ground lug of the terminal strip, and the ends of the secondary are wrapped around the two insulated lugs.

A 1N34A diode is connected from each end of the secondary to the center terminal of the RCA jack, with the cathode band of each diode positioned toward the RCA jack. A 4.7-uF 35-volt electrolytic or tantalum capacitor and a .001 disc capacitor are also connected from the center of the jack to its ground lug, and all joints are soldered. This completes the coupler, and the other half of the minibox can be attached.

The voltage-to-frequency converter is housed in a utility box measuring 3-1/4" × 2-3/16" × 4". Fig. 2 shows the circuit of the converter. Voltages between 1.7 and 9 volts applied to pin 5 of the 555 timer IC cause the oscillation frequency to vary. With the values given, the frequency of oscillation will be about 10 kHz with less than 1.7 volts applied to pin 5. As the voltage is increased above 1.7 volts, the frequency of oscillation will decrease in a linear fashion until the voltage reaches 9 volts, at which point oscillation will stop.

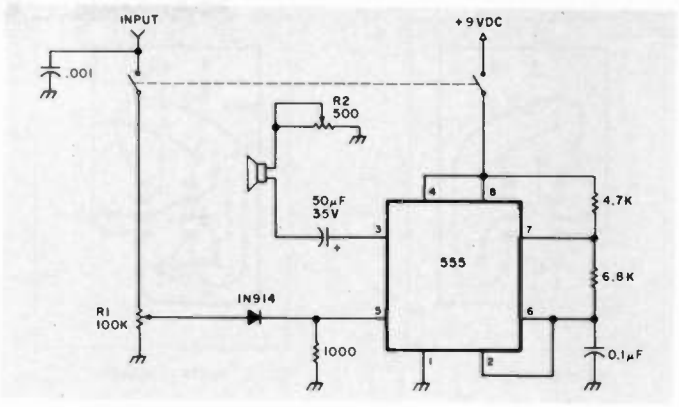

Fig. 2. Voltage-to-frequency converter schematic.

Potentiometer R1 controls the voltage reaching pin 5. When R1 is adjusted to place maximum resistance between the wiper and ground, approximately 20 Watts of output power from the transmitter will begin to lower the audio tone from the converter, and 100 Watts will lower it to about 1 kHz. If higher power is used, adjustment of R1 will set the tone to a usable frequency.

All parts for the converter are mounted on a printed circuit board with the exception of R1, R2, the power switch, and the speaker. An etching pattern for the circuit board is shown in Fig. 3. Although I used a panel-mounted potentiometer for R2 (the volume control), a printed circuit type can be used with only a

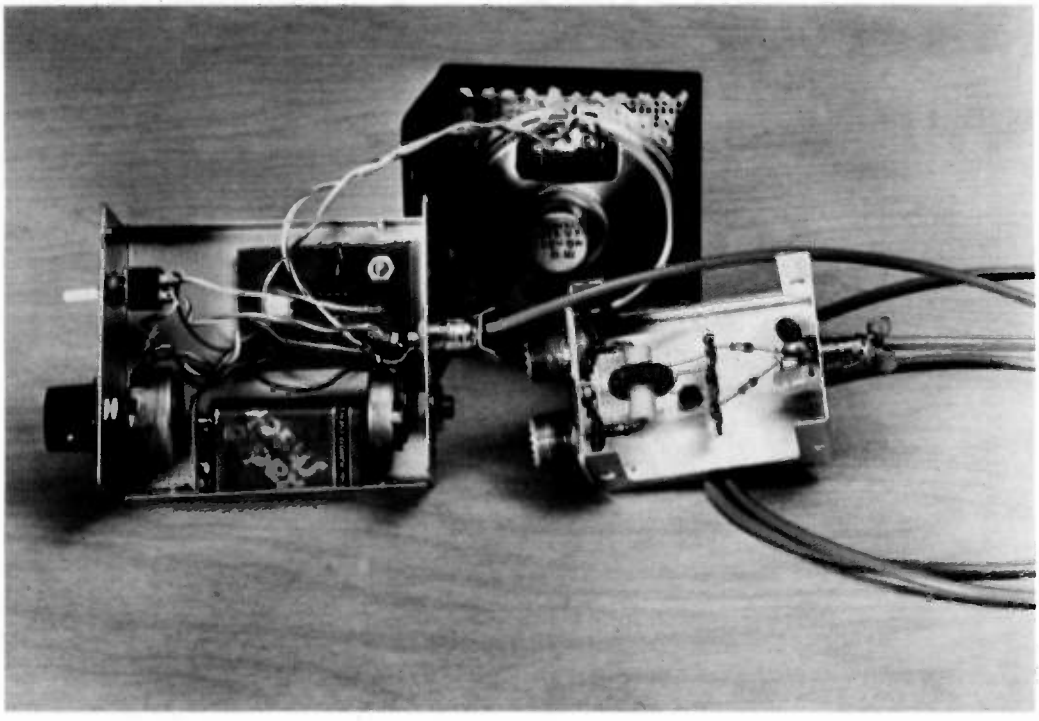
Photo B. Assembly details. Voltage-to-frequency converter is on left, rf coupler is on right.

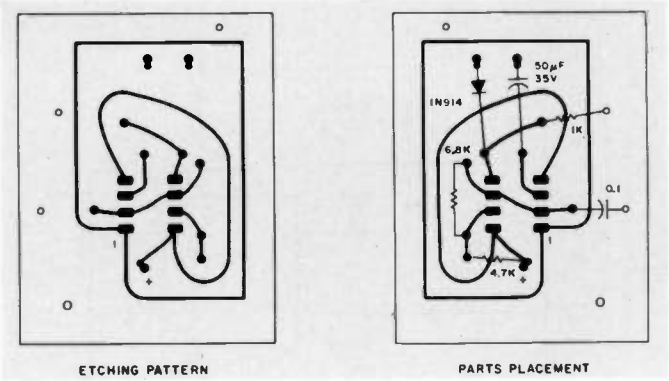

Fig. 3. PCB layout and parts placement.

minor modification to the circuit board. Input voltage from the coupler is through an RCA phono jack on the rear wall of the enclosure along with R2.

The DPDT switch shown is necessary to remove voltage from pin 5 of the IC when the converter is not in use. I failed to remove the input voltage while breadboarding the circuit, and the IC got very hot in a hurry. The resistors are all 1/4 Watt. C1 is mylar™ and C2 is either electrolytic or tantalum.

Since I did not want any bolt heads showing on the outside of the cover, I mounted the speaker by fastening it with hot-melt glue. I cut a 2" diameter hole in the cabinet top with a wing cutter in my electric drill. Next, I glued a piece of perforated aluminum to the inside of the cabinet, painted it, and then glued the speaker to the underside of the cabinet top.

I mounted the circuit board by removing the screw from the left rear foot of the cabinet and drilling out the hole to clear a 6-32 bolt. I then reattached the foot with a 1-inch-long 6-32 bolt and nut. I ran another nut about halfway down the bolt, put the circuit board on the bolt, and tightened a third nut on top of the board. Be sure to scrape the paint away from around the inside of all mounting holes to ensure good electrical contact. The battery is fastened down by making a loop of masking tape with the sticky side out and pressing it between the battery and the bottom of the cabinet.

As with any construction project today, finding the parts is a major part of the job. Most of the parts are available at Radio Shack, and I have added a parts list with Radio Shack part numbers where available to aid in locating the parts.

Operation of the audible tuning aid is very simple. Just insert the coupler in the antenna feedline and connect it to the converter with a shielded cable to prevent rf pickup. The coupler is non-directional, so either SO-239 may be connected to the transmitter input.

When the power switch is turned on, a high-pitched tone will be heard from the speaker. Adjust R2 for minimum usable volume to preserve battery life. Apply transmitter power and tune the transmitter for the lowest tone pitch from the tuning aid. For power levels up to 100 Watts or so, R1 should be set to minimum resistance between the input and pin 5 of the IC. If the tone stops during the tuning procedure, advance R1 until a high-pitched tone is reestablished. When further tuning of the transmitter results in no further lowering of the tone frequency, the transmitter is tuned for maximum output and is ready for use.

I hope this tuning aid will help amateurs with visual limitations to enjoy their hobby more. Other uses of the voltage-to-frequency converter can be made (such as audible voltmeters and other test instruments) with changes in the input circuitry. I would be interested in hearing of such uses which others find for the converter. ■

Parts List

Component	Radio Shack Part Number
50-uF, 35-volt capacitor	272-1027
0.1-uF dipped mylar™ capacitor	272-1069
0.001-uF disc ceramic capacitor	272-126
4.7-uF 35-volt capacitor	272-1012
100k-Ohm potentiometer	271-092
1000-Ohm, 1/4-Watt resistor	271-023
4700-Ohm, 1/4-Watt resistor	271-030
6800-Ohm, 1/4-Watt resistor	271-032
1N34A diodes	276-1123
1N914 diode	276-1122
555 IC	276-1723
DPDT switch	275-614
Battery clip	270-325
2-1/2" speaker	40-247
SO-239	278-201
RCA phono jacks	274-346
Minibox	270-235
Utility box	270-251

The T-68-2 toroid core is available from Amidon Associates, 12033 Otsego Street, North Hollywood CA 91607. Radio Shack does not stock a 500-Ohm panel-mount potentiometer. If the circuit board is modified for a PC-mount pot, part number 271-226 may be obtained from Radio Shack.

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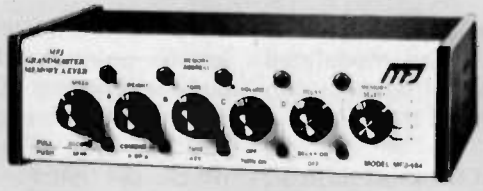

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Installing Subaudible Tone Encoders

— do it right

Today's communication channels are becoming more crowded every day, and with the increasing amount of intermod and other interference, amateur repeater systems are incorporating tone-access systems to help solve these problems. Probably the most common use of tone-control signaling in FM two-way radio is the continuous-tone-controlled squelch system (CTCSS). This consists of a low-level subaudible tone, typically below 250 Hz, being modulated on the radio frequency carrier of an FM transmitter.

One of the most difficult aspects of connecting CTCSS equipment to a radio is locating the proper injection point for the subaudible encoder. Depending on the encoder used and the type of radio in which the encoder is installed, this procedure can be relatively easy or it can produce many hours of frustration. This article will describe some of the problems of installing a subaudible encoder and will guide you to the successful installation of these units.

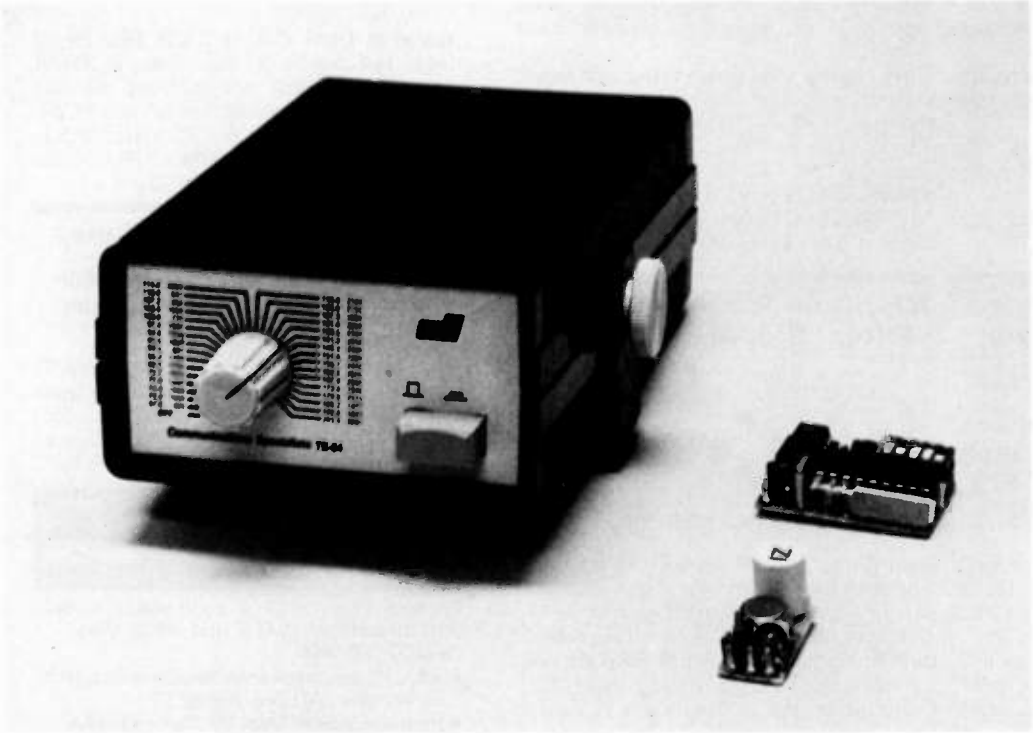

Photo A. This is an example of the types of subaudible encoders available with low-impedance outputs. Moving clockwise from the top is the TE-64 universal encoder, capable of encoding all 32 CTCSS tones via a front-panel switch. Next is the model SS-32 programmable encoder which can be programmed without the use of a frequency counter. Third is the model ME-3 microminiature encoder which uses field-replaceable, plug-in frequency-determining elements. All units are manufactured by Communications Specialists in Orange, California.

Proper connection of a subaudible encoder is very important. If the correct connection point is not found, the result can cause serious system problems. These problems include an excessive buzz on the carrier; loss of microphone audio, loss of transmit power, and intermittent or unreliable operation.

The key to locating the proper tone-injection point involves looking at two areas. First, how universal is the encoder? Is it capable of driving a low impedance load? Second, does the transmitter have a phase modulator or an FM modulator? Are you using a synthesized transceiver? These are just a few of the questions which are important to the proper installation of

the encoder.

Fig. 1 shows a block diagram of a typical phase-modulated transmitter. Most transmitters using individual crystals for each transmit frequency are of the phase-modulated type. The output of the subaudible encoder is typically connected in or just prior to the modulator stage in the transmitter. If the transmitter has a subaudible tone connection point, this point should be used. Do not confuse this connection with another common point often referred to as *tone input*. This is normally used for touchtone™ pads or audible encoders, and is not satisfactory for subaudible connections. This is primarily because this point is usually located in the microphone amplifier section of the transmitter (more on this later).

A radio manufacturer's connecting point is often to the center of the deviation control (sometimes called the IDC control), to the input of the final audio driver, or directly to the varactor modulator diodes. Should the transmitter not have provisions for tone injection, one or all of these connection points should be tested, and the one that provides the best results with minimum distortion and a minimum amount of voice intermoding should be used. This connection point varies with each different model radio, and you must determine which provides the best results.

In some cases, amateur transceivers are not designed to interface readily with tone-coded squelch systems, and injection of the subaudible tone sometimes can be very difficult. In these cases, when using a phase modulator, a varactor assembly can be used. The varactor changes ac voltage into changing capacitance which truly FM modulates the transmitter.

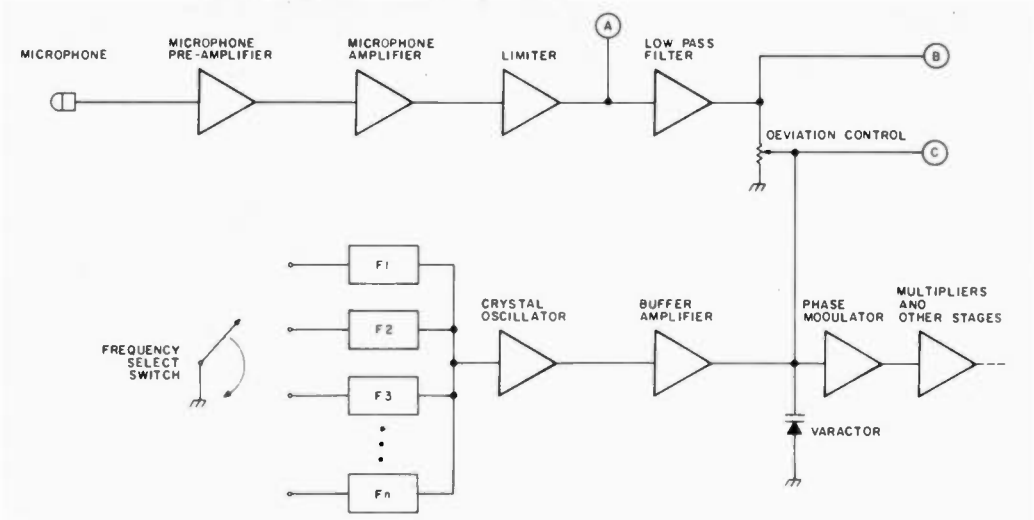

Fig. 1. Partial block diagram of a phase-modulated transmitter. The points labeled A, B, and C are typical connection points for the subaudible encoder. These points are located after the audio-shaping circuitry which would cause tone distortion.

No intermoding or distortion of the voice will be noted with this method, as compared to some injection points in the phase modulators.

Fig. 2 shows a typical varactor assembly, where the collector-base junction of a low-frequency NPN silicon transistor is used as the varactor diode. Various values of coupling capacitors are shown for different frequency ranges of the transmitter; a higher value of capacitance will increase the deviation level. However, if the capacitance is too high, it may be difficult to set the transmitter on frequency. It should be noted that when the varactor assembly is connected to the oscillator circuit, the oscillator frequency will probably shift slightly and require retuning. This method is used quite often in tube-type transmitters and in a few solid-state units, as well. This method also can be used if other connection points prove unsuccessful.

Another common type of transmitter that is now extremely popular is the synthesized transceiver (Fig. 3). This type of radio often uses a frequency modulator whereby a varactor, as described before, is used to vary the frequency of the

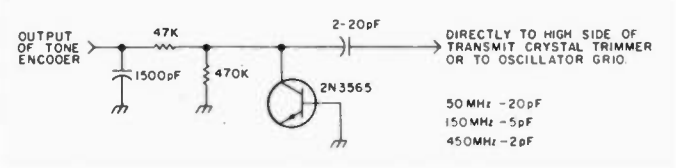

Fig. 2. Schematic of a typical varactor assembly. The collector-base junction of an NPN transistor is used as the varactor. The output of the assembly is connected to the high side of the transmit crystal trimmer. In a tube-type transmitter, the output is often connected to the grid of the oscillator tube. The value of the coupling capacitor changes, depending on the frequency range used. The values shown are approximate and may require adjustment to obtain the proper deviation level.

crystal oscillator. In some transceivers, the varactor is used to change the frequency of a voltage-controlled oscillator (vco). This type of modulator interfaces quite well with subaudible encoders.

The frequency-modulated transmitter is very similar to the phase-modulated transmitter up to the low-pass filter section. The FM modulator is identified quite easily, as the audio is fed into the varactor, which is often part of the crystal oscillator. The tone-injection point for a frequency-modulated transmitter is found in a similar manner as with the phase-modulated transmitter.

When connecting power to the encoder, be sure to use switched power that is active only during transmit. This voltage can be taken right from the transmitter circuit board or a push-to-talk relay coil. Switched power should be used for two reasons. First, the encoder will draw current only during transmit since it is not used during receive operation. Second, the crystal oscillator, which is frequency modulated during transmit, is often the same oscillator which is used during receive operation. If the encoder is not disabled during receive, a buzz will probably be heard through the speaker as the encoder continues to modulate the receiver oscillator.

If you have an encoder that has a low-impedance output, insufficient level output should never be a problem. However, if the tone connection point is a high-impedance load such as a 100k deviation control,

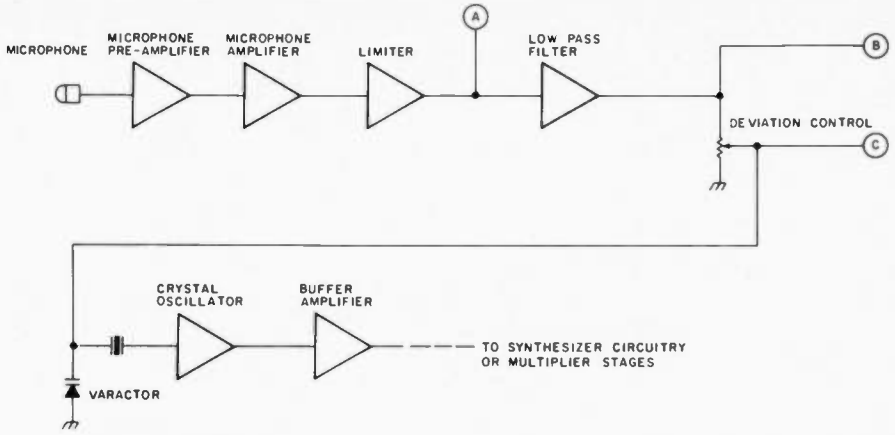

Fig. 3. Partial block diagram of a frequency-modulated transmitter. Although these transmitters are generally a lot easier to interface, some synthesized transmitters using FM modulators can be difficult.

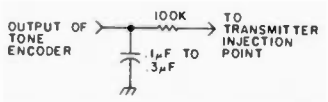

Fig. 4. Tone output filter.

then a series isolation resistor will be required so as not to load down the normal voice modulation. This resistor value must be determined experimentally, but a 100k resistor would be a good starting point. This value could change from 10k to 1 megohm, depending on the radio used. It is best to use an encoder with a low-impedance output (less then 10k). This is more easily adaptable to various types of transmitters, since the encoder often is required to drive into a low-impedance load. If the tone deviation cannot be set up to the proper level, it is possible that the encoder is not supplying a sufficient output level. This would be the case when using an encoder with a high-impedance output to drive a low-impedance load. If this happens, another connecting point must be located which is at a higher impedance level.

Do not connect the encoder tone to the microphone input or the microphone preamplifier as this invariably causes excessive tone distortion due to the frequency response of the transmitter's speech amplifier. The speech amplifier has a typical response of 300 Hz to 3000 Hz and does not permit the fundamental tone to be transmitted. This is the usual cause of a distorted tone output as monitored through a speaker or with a deviation scope. If the purity of the encoder output is in question, look at the output of the encoder with an oscilloscope.

If tone distortion continues to be a problem, then a capacitor can be placed on the tone output to provide additional filtering when required (see Fig. 4). This is not noticeable in phase modulators, since the frequency response can be quite poor at the low end of the audio range. If a deviation scope is used, the scope trace will not be a pure sine wave and will sound like a buzz. The additional filtering will cure the problem. If a deviation scope is not available, then another receiver on the transmitter's frequency can be used. Using this method, an oscilloscope can be connected to the discriminator output in the receiver, and a clean sine wave should appear when transmitting.

Another area which should be given special attention is rf interference. This is most common when installing encoders into hand-held portable transceivers. Although the encoders tested were not susceptible to being affected by rf, care should be taken when installing the units near the transmitter circuitry. In most cases of rf interference causing loss of audio or loud buzzing oscillations, it has been found that the rf is coupled into the connecting leads of the encoder and then fed back into the transmitter itself. This causes the bias conditions and other tuned circuits to become unstable, producing oscillations and distortion. But, under these conditions, it should be noted that the encoder is still working properly. The solution to this is to keep all leads as short as possible and install one or more bypass capacitors on the radio's circuit board where the encoder leads are connected. Also, relocating the encoder or rerouting the connecting leads through another part of the radio should correct the interference caused by the stray rf.

One final problem which is common when connecting tone-coded squelch equipment is setting the encoder to the proper deviation level. Unless you have access to a communications monitor with a deviation scope (not a deviation meter!), setting the proper level can be very difficult. If the proper injection point is not found, you could be encoding a highly-distorted tone which would have to be set at a very high level in order to open the associated decoder. If you are encoding a clean sine wave, then follow this procedure for setting the level:

1) Turn the level adjustment all the way down so that you have zero output and move to a repeater requiring tone access.

2) Next, turn the level up just a little bit and key your transmitter.

3) Did your transmitter key up the repeater? If not, repeat step 2 and continue to increase the level until the repeater keys up reliably.

4) Now increase the level just a little bit more, and you are finished. This little extra level will help you in marginal signal areas, and will operate the decoder more reliably.

5) Button up the radio, and you are on your way.

If you happen to have access to a deviation scope, then the proper deviation level of the subaudible tone should be set from 0.5 kHz to 1.0 kHz peak-to-peak. This is the standard range for this setting. However, it is best to keep the deviation as low as is practical within this range as long as reliable operating is maintained.

It should be clear that installing a subaudible encoder to a transmitter is not an easy job. There are many variables to contend with and each one of them can cause a multitude of problems. But, with practice and experience and, of course, a little patience, excellent system operation can be attained.

I would like to thank the various manufacturers of tone equipment for providing the test equipment and information required for this article. I would also like to thank them for the use of their new line of encoder products which were used for testing and evaluation. ■

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Four-Band Mobile Antenna

— looks like a weird hat rack

Do you ever find yourself cruising down the highway working forty meters and wishing you could switch to twenty, fifteen, or ten without having to stop to change resonators? You can! I experimented with this contraption in 1960 and have been using it ever since. There is even a commercial version that came out a couple of years ago.

Any set of three resonators may be used but I prefer the 40-20-10 combination since you also get a 15-meter fallout from it. When I first started using it with an old Galaxy V, I installed a remotely-operated super-tuner gizmo in the trunk, but later found that with patient stinger adjustments on the three resonators, the tuner was not really needed. I am presently using an Atlas 210 for mobile, and the broadbanded rigs are supersensitive to swr over 1.5:1. I have worked many foreign countries with this rig with good signal reports.

The strap that holds the resonators must be of sufficient strength to prevent the angles of the forward and aft resonators from changing. Changing this angle affects the resonant frequency. The strap I happened to start out with was about one inch wide and 3¼ inches long. A hole large enough to accommodate the threaded extension on the mast is drilled in the center. (I happened to have had all Hustler equipment so that is what I have used since.) The other holes on each end are large enough to hold non-corrosive bolts that will screw into the bottoms of the other resonators. The strap is bent as shown with each end dropped at forty-five degrees. The assembly is attached to the mast and held in place by the center resonator, and the time-consuming tuning is started.

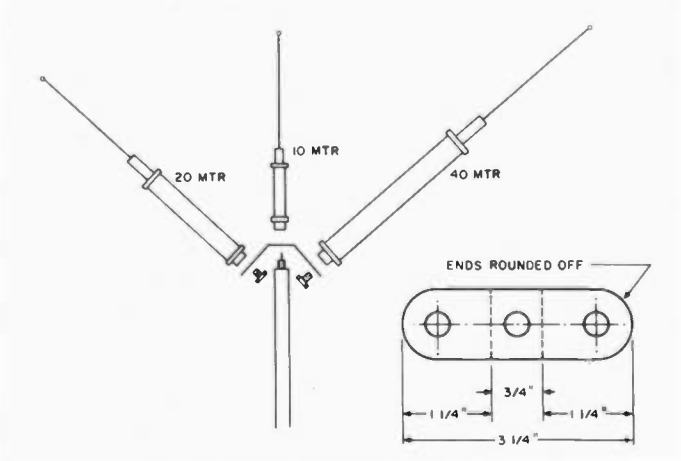

Fig. 1. Four-band mobile antenna construction details.

Begin with the lowest frequency resonator, adjusting to the lowest swr, then proceed to the next higher and then the last. The resonators interact, and this procedure must be repeated several times until the swr no longer can be improved. I have 1.1 at 7.260 and 1.35 at 7.225 and 7.295. On twenty meters, the swr is less than 1.35 across the band and even better on ten. The swr does peak up to 1.5 on fifteen meters. I use the ten-meter resonator to hold the strap to the mast with the twenty-meter resonator in front and the forty-meter aft. This streamlines the assembly in the direction of travel and reduces wind resistance. Also, with the larger resonator aft, it tends to stabilize the assembly at normal highway speeds.

I have found that the majority of the noise associated with mobile reception can be eliminated by using the copper braid out of RG-8 coax as grounding straps and grounding the car hood and trunk lid to the frame of the car. In addition, the exhaust should be grounded in at least two places, one in front of the muffler and one aft. Be sure to scrape the rust off to bare metal when attaching the grounding straps. The braid can be cut to the desired length, the ends shaped to hold a bolt, and then heavily soldered to make a good connection.

Several of my ham friends around the country have built this antenna system over the years and have enjoyed it. I would be pleased to hear from anyone who tries it and of any ideas for improvement. ■

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Computers and HF

— a discussion of alternatives

Microcomputers are becoming increasingly popular, and they can be used to give us faster and more reliable communications on the amateur bands. But what is the best way to use them? If the FCC offered us a choice of several emission types and transmission speeds for computer communications today, which should we choose? It would be good for us to start now to consider the character of the ham bands we have to communicate over and the nature and potential of the computer links that we want to set up so that later we can go to the FCC with proposals and justifications for what we want.

This article will present my thoughts on how an optimum scheme for computer-to-computer communications on the HF amateur bands should be designed. For purposes of this discussion, whether or not these techniques are authorized under the current FCC rules is immaterial; we can work on the rules after we decide what we want.

Advantages

Why, in the first place, do we *need* a special emission type for use in computer-to-computer communications? Current practice for those with microcomputers running in their ham shacks is to program the computer to emulate a TTY machine. This allows communications with other amateurs using TTY machines, but we can do much better.

Computers will allow us to communicate at much higher speeds than TTY machines. This will reduce the time required for transmission of large data files and also allow retransmission of data that was garbled by fading or QRM without incurring unacceptable overall transmission times in the process.

Computers will allow us to implement error-detecting and error-correcting codes in the transmission of our data. This means that the receiving computer will be able to determine whether or not it has received a particular data block error-free and request retransmission of portions if some were garbled. This is a fantastic step forward compared to current RTTY operation.

By combining the use of computers with frequency-shift keying (FSK) and error-detecting codes, we can obtain another advantage—diversity operation. The receiving computer can detect independently both the mark and space signals. Since these two signals are separated in frequency, the overall system gains immunity to fading of one channel with respect to the other ("selective fading") and also to narrowband QRM such as CW signals which might be obliterating one of the two tone frequencies at any given time.

Uses

There are several immediate uses for interconnected microcomputers on the amateur bands. First, in emergency communications, links with computers supporting them could handle formal message traffic error-free and at much higher rates than either CW, phone, or RTTY operation can today. This could reduce the typical logjam of message traffic out of disaster areas.

Second, the transfer of image data (TV pictures or

computer graphics) from one amateur to another could be done much better using microcomputers and digital techniques than by the current slow-scan TV system. This is because the images could be digitized and sent over the link using error-detection coding. By retransmitting portions of the image that were received garbled, display of a perfect image could be ensured.

Third, people will want to exchange computer programs. This will require a high-speed communications link between computers, with a means to detect and retransmit garbled data, since programs can tolerate no errors.

Now let's discuss an inter-computer communications scheme that is intended to be optimum for amateur use on the HF bands.

Emission

One of the most important characteristics of the HF amateur bands is the typical presence of fading and interference. For operation under these conditions, a frequency-shift keying approach is best. Since it is desirable to keep the signal bandwidth as narrow as possible, use of the present standard FSK shifts of 170 and 425 Hz is recommended. Use of 170-Hz shift would minimize one's bandwidth, at the expense of reduced advantage from diversity operation (the wider the mark-space frequency separation, the better the diversity receiver will work).

On the other hand, on a band that is not too crowded, 425-Hz shift can be used and the system will be closer to being immune to narrowband interference. (A shift of 850 Hz would offer even more diversity advantage and also allow a faster signaling speed, but I am not recommending it due to the greater bandwidth required.)

Speeds

Once the frequency shifts are chosen, the maximum signaling speed is set also. This occurs because the significant sidebands produced around each tone frequency must be separated enough to allow reliable detection at the receiver. Analysis shows that we should be able to use a pulse width as short as 7.84 milliseconds (ms) with 170-Hz shift and still allow adequate separation between the mark and space sidebands. With 425 Hz, a minimum pulse width of 3.14 ms should be usable. Both these schemes would require good quality detection filters at the receiver. And in both cases, the system could be slowed down from this maximum rate when band conditions are bad so that added interference immunity could be gained from the longer pulse times.

If we assume use of an asynchronous 8-bit ASCII code, the 7.84-ms pulse width yields a speed of 12 characters per second (cps) and the 3.14-ms width yields 30 cps. Overall emitted bandwidth of the 170-Hz shifted signal at 12 cps would be about 340 Hz, and that of the 425-Hz shifted signal at 30 cps would be about 850 Hz.

Coding

While the Baudot code presently in use for RTTY is most efficient for sending text messages (it requires only a 5-bit code), the 8-bit ASCII code set (with its capability to send special characters and represent full 8-bit computer words) is superior when transmission of all sorts of data is considered. The only penalty in the use of ASCII will be that pure text messages will require slightly longer transmission times than if Baudot coding had been used.

I recommend that we use asynchronous ASCII coding for our inter-computer communications because the design of the receiving hardware and software is simpler. Also, the timing accuracy requirements of the sending and receiving computers are greatly reduced compared to those required with synchronous codes (no start or stop pulses). The code will use a 1-unit start pulse, 8 bits of data, and a 1.5-unit stop pulse—similar to present RTTY coding.

We can take a tremendous step and obtain error-free reception of data by employing error-detecting or error-correcting codes in our scheme. These are special methods of coding the basic ASCII characters of a message so that the receiving computer can determine, after it has received the full message, whether there were any errors in it. If there were, it can request a retransmission of portions of the message from the sending computer. The sending computer can retransmit data blocks that were garbled in transmission whenever necessary until the receiving computer has received the entire message correctly. (There is a catch, of course, in that as more transmission errors occur, data blocks must be retransmitted more often, and the longer it then takes to receive the entire message error-free.)

Since we can expect a lot of interference on the ham bands, it is best to break up the data we are sending into small blocks containing perhaps 16 or 32 characters each. A typical transmission might contain 20 or 30 blocks, and only garbled *blocks* would need to be repeated, not the entire transmission. (This is known as "block coding.")

Diversity

As mentioned earlier, the use of FSK with block coding and error-detecting or error-correcting codes will in turn allow the use of diversity receivers. After detecting both the mark and space signals complete with error-detecting information, the receiving computer can request retransmission of garbled blocks. Since the receiving computer need receive only one of the two signals without garble to receive a complete block, the system is now much more nearly immune to narrowband QRM and selective fading.

What Now?

The hardware and software needed to implement all of these ideas has not yet been completed, but it is under development. Much experimentation will still be required, even within the framework of ideas presented here, to determine which of the several possible schemes is really optimum for use on the HF bands for computer linking. The most experimentation will probably be required in determining which of the many available error-detection and error-correction schemes we want to use. I am starting to work along these lines and would like very much to hear from others interested in participating in this development effort.

The ideas presented here are intended to be a starting point for discussion and experimentation within the amateur community, with the eventual goal being an optimum agreed-to standard for inter-computer communications on the HF bands. Let's give this topic some thought and ensure that the eventual FCC rules authorize us to use state-of-the-art techniques for linking our personal computers. ■

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Ned Novice and his Capacitance Meter

— you, too, can build one

Ned Novice visited Mike Cord (the boy electronics wizard) the other day with a perplexing problem pertaining to plastic parts. Ned asked, "Mike, what are these?" and set a box of parts on the workbench.

Mike replied, as he pawed through the box of parts, "They seem to be capacitors with no markings as to value."

"Do you know a way to determine the value of these parts?" asked Ned quizzically.

"First of all," Mike replied, "let's get back to basics."

The Capacitor Defined

"My father's physics book should be of help. Hmm . . . Ah, yes, here it is . . . Q=CV. This says that the charge on a capacitor in coulombs is equal to the capacitance in farads multiplied by the voltage."

"How can that relationship be of use to me?" interjected Ned.

"Quite easy," replied Mike. "If we charge up a capacitor to a known voltage and measure the coulombs, we will have it."

Ned thought for a few moments before retorting: "But I have never heard of a *coulomb* meter!"

Mike grinned and searched through his junk box for a few moments before coming up with a 0 to 100 microammeter. "With this we will measure your capacitors."

"You *do* have a coulomb meter, then," said Ned, hopefully.

Mike replied, "Look at it this way, Ned. The definition of the Ampere is one coulomb per second, so what we will do is measure the current."

Mike wrote the cryptic formula: I=Qf=CVf. "We will charge and discharge the capacitor at a frequency. The measurement of picofarads will be indicated by microamps," he stated in a firm voice, with the confidence one would expect only from a more mature individual.

The Circuit Designed

"Now for specific values," said Mike as he studied over the scratch pad for a moment. He wrote down: V=4.5 volts, I=100 microamperes, C=100 picofarads full scale.

"Therefore, f=I/CV=222 kHz!" exclaimed Mike as he turned off his calculator. "And to change ranges all you have to do is change frequency. Thus, 100 pF=222 kHz, 1000 pF=22.2 kHz, .01 uF=2.22 kHz, .1 uF=222 Hz, and 1 uF=22.2 Hz."

Just then Mike's father entered the ham lab and asked what fun the boys were into today. Mike related all that had happened and asked his dad if he had any suggestions.

"So far, so good, Mike.

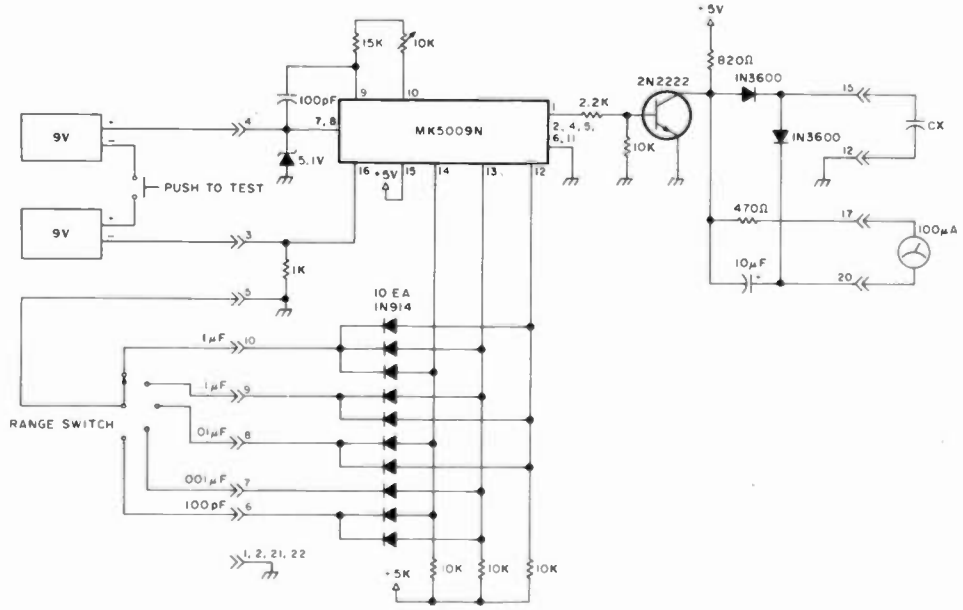

Fig. 1. Capacitor meter schematic.

Parts List

9-V transistor battery	2
Battery jacks	2
Push-to-test switch, SPST	1
Zener diode, 5.1 V, ½-Watt	1
Rotary switch, 5-position	1
Diode, 1N914, 1N697, etc.	10
Diode, 1N3600, 1N198, etc.	2
IC, Mostek MK5009	1
Transistor 2N2222	1
Resistors:	
15, ¼-W, 5%	1
1k, ¼-W, 5%	1
2.2k, ¼-W, 5%	1
470, ¼-W, 5%	1
820, ¼-W, 5%	1
10k, ¼-W, 5%	4
TO5 pot, 10k	1
Meter, 100 dc uA full-scale	1
Capacitors:	
100-pF dipped mica	1
10-uF tantalum, 10 V	1

Circuit board is available from O. C. Stafford Electronics, 427 S. Benbow Road, Greensboro NC 27401.

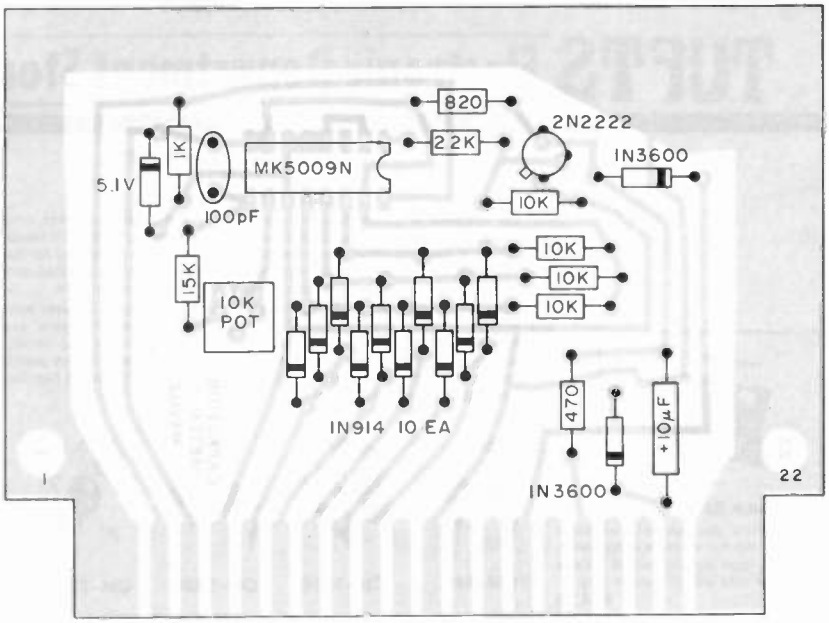

Fig. 2. Capacitor meter parts layout.

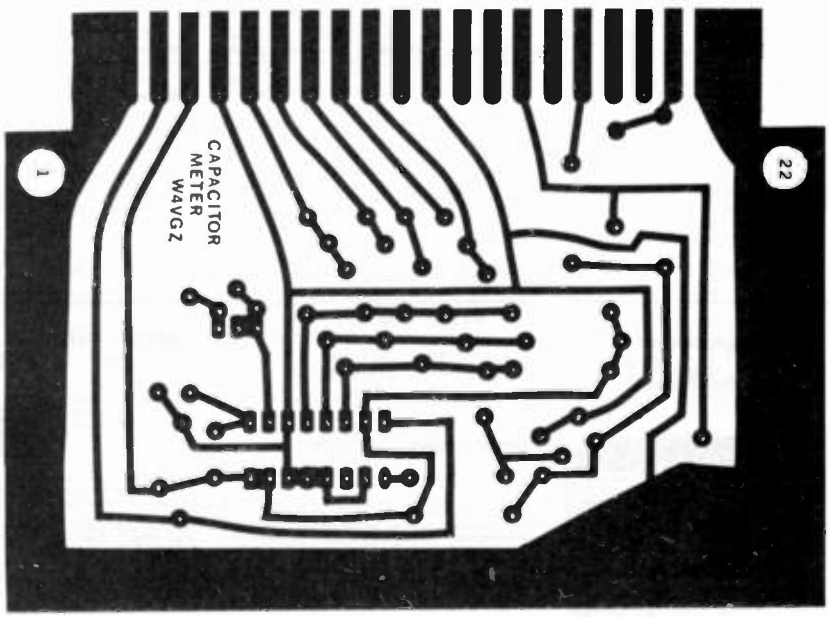

Fig. 3. PC board.

However, I do have a suggestion. Mostek has an integrated circuit that will do all you want in generating a 5-decade range of signals. This chip has an oscillator implemented as well." Dad then reached for the Mostek data book from a crowded bookshelf and drew the schematic shown in Fig. 1.

The Project Built

The next evening, Dad came into the ham lab with a grin and threw a large envelope on the bench. "I had a few spare minutes at work today, so I laid out a PC board for your capacitor meter, and here is the photomaster."

"Golly, Dad!" exclaimed Mike, "I was going to build it on perfboard, but this is so much better."

Ned was already putting the negative over a pre-sensitized PC board blank and exposing the resist with the photoflood lamp. Mike reached over and turned on the crock pot that contained the ammonium persulfate etchant. A half-hour later, the boys were stuffing the board with parts. Luckily, the local industrial parts distributor had the MK5009 in stock, and Dad had had the foresight to pick one up on the way home.

"What are all these diodes for?" asked Mike.

Dad signed off from his 20-meter QSO. "The decade selection is made by 4 binary-coded lines to the MK5009. I weighed the cost of a BCD thumbwheel switch against the cost of the diodes, considering that we have many rotary switches in the junk box. At 20 for a dollar, the diodes won," explained Dad.

While Dad was explaining, Ned had been soldering wires, and he called from the workbench area, "It works! I tried a .001-uF capacitor and trimmed the oscillator for full scale. Then I measured a 470 pF and the meter was *exactly* on calibration!"

By the next evening, the circuitry was mounted in a nice looking box purchased from the local hobby electronics store. Dry transfer labels were used to mark switch positions, and Ned was busy identifying his unknown capacitors.

"Mike, I have noticed that the meter reads 3 or 4 picofarads on the most sensitive scale, with no connection to the output terminals. This must be distributed capacitance and leakage effects, right?"

"Yes," replied Mike. "Dad explained it to me just that way after you left last evening."

"Mike, what do we do if we have a really large electrolytic to measure?"

"Hmm . . ." said Mike, as he reached for the physics book. ■

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PROFESSIONAL HEADPHONES & HEADSETS

BOOM MIC HEADSETS

TELEX®

For the ultimate in communications convenience and efficiency select a boom mic headset. Long-time favorites of professional communications, boom mic headsets allow more personal mobility while always keeping the mic properly positioned for fast, precise voice transmission. Boom microphones are completely adjustable to allow perfect positioning. And, boom headsets leave both hands free to perform other tasks.

All modes are supplied with "close talking" microphones to limit ambient noise pick-up and provide superior intelligibility. Each model as a convenient, inline push-to-talk switch, which can be wired for either push-to-talk relay control or mic circuit interrupt for voice operated transmitters. The switch may be used as a momentary push-button or it can be locked in the down position. All models have tough, flexible, 8 foot cords which are stripped and tinned, unterminated.

C-610 C-1210 C-1320

Headphone Jack Box

Ham Clubs, field day contest operation. No more jury rigs for multiple headphones. Six ¼" phone jacks with individual volume controls, 4 foot cord with ¼" phone plug.

$14.30

CM-610 CM-1210 CM-1320 CM-1320-S PC-100 HTC-2 HMC-2 HTC-91

MODEL	C-610	SWL-610	C-1210	C-1320	CM-610	CM-1210	CM-1320	CM-1320S	PC-100	HTC-2	HMC-2	HFC-91
Headphone Sensitivity Ref 0002 Dynes/cm² @ 1mW input, 1kHz	103dB SPL ±5dB	103dB SPL ±5dB	103dB SPL ±3dB	105dB SPL ±5dB	103dB SPL ±5dB	103dB SPL ±3dB	105dB SPL ±5dB	105dB SPL ±dB				
Headphone Impedance	3.2 20 ohms	2000 ohms	3.2 20 ohms	3.2 20 ohms	3.2 20 ohms	3.2 20 ohms	3.2 20 ohms	3.2 20 ohms	8 200 ohms	3.2 20 ohms	3.2 20 ohms	3.2 20 ohms
Microphone Frequency Response					50 8000 Hz	50 8000 Hz	50 8000 Hz	50 8000 Hz	50 1200 Hz	100 3000 Hz	100 3000 Hz	100 3000 Hz
Microphone Impedance					High	High	High	High	Low	Low	Low	Low
Microphone Sensitivity Below 1 volt/microbar at 1 kHz					51 dB ±5 dB	51 dB ±5 dB	51 dB ±5 dB	51 dB ±5 dB				
PRICE:	$10.45	$12.25	$29.70	$41.80	$47.20	$62.75	$75.25	$59.95	$16.95	$24.50	$15.50	$9.90

THOMSON-CSF NPC ELECTRONICS

MODEL	PRICE	MODEL	PRICE
12V4	$19.95	104R	$ 59.95
102	26.95	108RA	89.95
107	36.95	108RM	99.95
103R	42.95	109R	159.95

MODEL 109R $159.95

NPC 25 Amp Regulated Power Supply 4 Way Protected Output Voltage and Current Meters.

Extra heavy duty unit quietly converts 115 volts AC to 13.6 volts DC - 200 millivolts, 10 amps continuous, 25 amps max. All solid state. Features dual current overload, overvoltage and thermal protection. Ideally suited for operating mobile Ham radio and linear amplifier in your home or office. Excellent bench power supply for testing and servicing of mobile communications equipment.

	TYPICAL	MAXIMUM
Output Voltage	13.8 2VDC	13.6 3VDC
Line/Load Regulation	50 mV	100 mV
Ripple/Noise	5 mV RMS	10 mV RMS
Transient Response	20 uSec	
Current Continuous	10 Amp	
Current Limit	20 Amp	
Overvoltage Protection	14.5 V	15 V
Thermal Overload	180 F	

Case 4¾" (H) × 9" (W) × 8½" (D) Shipping Weight 15 lbs.

MODEL 107 $36.95

NPC 4 Amp Power Supply, 6 Amp Max Solid State Overload Protected

Functions silently in converting 115 volts AC to 12 volts DC 4 amps continuous, 6 amps max. Enables anyone to enjoy CB radio, car 8-track cartridge, cassette player or car radio in a home or office.

Continuous Current (Full Load)	4 Amp
Output Voltage (No Load)	18 V max
Output Voltage (Full Load)	12 V min
Filtering Capacitor	10,000 uF
Ripple (Full Load)	5 V RMS
Short Circuit Protection	Thermal Breaker

Case 3" (H) × 4¾" (W) × 5¾" (D) Shipping Weight 5 lbs.

MODEL 12V4 $19.95

NPC 1.75 Amp Power Supply 3 Amp Max

Functions silently in converting 115 volts AC to 12 volts DC. Ideally suited for most applications including 8-track stereo, burglar alarm, car radio and cassette tape player within power rating.

Continuous Current (Full Load)	1.75 Amp
Output Voltage (No Load)	16 V max
Output Voltage (Full Load)	12 V min
Filtering Capacitor	5,000 uF
Ripple (Full Load)	4 V RMS
Short Circuit Protection	Thermal Breaker

Case 3" (H) × 4" (W) × 5" (D) Shipping Weight 3 lbs.

MODEL 108RM $99.95

NPC 12 Amp Regulated Power Supply Solid State 3 Way Protected Current Meter

This heavy duty unit quietly converts 115 volts AC to 13.6 volts DC - 200 millivolts, 8 amps continuous, 12 amps max. All solid state. Features dual current overload and overvoltage protection. Ideally suited for operating mobile Ham radio 2 meter AM/FM/SSB trans. centers in your home or office. Can also be used to trickle charge 12 volt car batteries.

	TYPICAL	MAXIMUM
Output Voltage	13.6 2VDC	13.6 3VDC
Line/Load Regulation	20 mV	50 mV
Ripple/Noise	2 mV RMS	5 mV RMS
Transient Response	20 uSec	
Current Continuous	8 Amp	
Current Limit	12 Amp	
Current Foldback	2.5 Amp	
Overvoltage Protection	14.5 V	15 V

Case 4" (H) × 7" (W) × 5" (D) Shipping Weight 9.5 lbs.

ALSO AVAILABLE AS MODEL 108RA WITHOUT METER AND OVERVOLTAGE PROTECTION

MODEL 104R $59.95

NPC 6 Amp Power Supply Regulated Solid State, Dual Overload Protection.

Converts 115 volts AC to 13.6 volts DC - 200 millivolts. Handles 4 amps continuous and 6 amps max. Ideally suited for applications where excellent DC stability is important such as CB transmission, small Ham radio transmitter and high quality eight track car stereos. Can be used to trickle charge 12 volt car batteries.

	MAXIMUM	TYPICAL
Output Voltage	13.6 2 VDC	13.6 3 VDC
Line/Load Regulation	20 mV	50 mV
Ripple/Noise	2 mV RMS	5 mV RMS
Transient Response	20 uSec	
Current Continuous	4 Amp	
Current Limit	6 Amp	
Current Foldback	2 Amp	

Case 3" (H) × 5" (W) × 6" (D) Shipping Weight 6 lbs.

MODEL 103R $42.95

NPC 4 Amp Regulated Power Supply, Solid State, Dual Overload Protection.

Converts 115 volts AC to 13.6 volts DC - 200 millivolts. Handles 2.5 amps continuous and 4 amps max. Ideally suited for applications where no hum and DC stability are important such as CB transmission, small Ham radio transmitter, and high quality eight track car stereos. Can also be used to trickle charge 12 volt car batteries.

	TYPICAL	MAXIMUM
Output Voltage	13.6 2 VDC	13.6 3 VDC
Line/Load Regulation	20 mV	50 mV
Ripple/Noise	2 mV RMS	5 mV RMS
Transient Response	20 uSec	
Current Continuous	2.5 Amp	
Current Limit	4 Amp	
Current Foldback	1 Amp	

Case 3" (H) × 4" (W) × 5" (D) Shipping Weight 4 lbs.

MODEL 102 $26.95

NPC 2.5 Amp Power Supply, 4 Amp Max. Solid State, Overload Protected

Functions silently in converting 115 volts AC to 12 volts DC 2.5 amps continuous, 4 amps max. Enables anyone to enjoy CB radio, car 8-track cartridge, cassette tape player or car radio in a home or office.

Continuous Current (Full Load)	2.5 Amp
Output Voltage (No Load)	16 V max
Output Voltage (Full Load)	12 V min
Filtering Capacitor	5,000 uF
Ripple (Full Load)	6 V RMS
Short Circuit Protection	Thermal Breaker

Case 3" (H) × 4½" (W) × 5½" (D) Shipping Weight 4 lbs.

Unarco-Rohn

COMPLETE 25G TOWER PACKAGES

50' Guyed Tower: Includes top section, 4 regular sections, base plate, rotor plate, 50' guy wire, 2 guy assemblies with torque bars, 3 concrete guy anchors and other miscellaneous hardware.

REGULAR PRICE $698.00
SALE PRICE 499.00
SAVE $199.00

50' Bracketed Tower: Includes top section, 4 regular sections, base plate, rotor plate and universal house bracket.

REGULAR PRICE $430.00
SALE PRICE 299.00
SAVE $131.00

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$299.00

BEARCAT 220

Aircraft, Marine, Public Service. The 220 adds features and advanced sophistication.

- Aircraft and Marine – press button to search entire Aircraft Band, another for Marine
- 7 Bands – Low, High, UHF, UHF-T, 2m amateur and 75 CM Ham – plus the Aircraft Band
- 20 Channels – scan up to 20 frequencies or either of two banks of 10 channels each
- Automatic Search – Selective Scan Delay – Automatic Lock-Out – Patented Track Tuning – Manual Scan Control – Single Antenna
- Priority – automatically samples designated channel every two seconds
- AC/DC operation

BEARCAT 300 **$429.95**

Service Search

Over 2100 pre-programmed frequencies.

- 11 Service Search categories arrange stored frequencies into "interest" groups – Police, Fire, Marine, HAM, Emergency, Telephone, Government, Forestry, Industrial, Transportation and Aircraft.
- 50 Channels/5 bands
- 7 Bands (Low & High VHF, UHF, and UHF-T, AM Aircraft, 2m & 75 CM Amateur)
- Non-volatile memory; AC/DC
- Automatic Search with Hold & Resume functions
- Patented Selective Scan Delay
- Vacuum Fluorescent Decimal-Display with Dimmer Control
- Speed Control
- Quartz Clock
- Patented Track Tuning
- Direct Channel Access
- Automatic Squelch

Bearcat®

NEW!

$149.95

BEARCAT® FOUR-SIX THIN SCAN™

More bands, more channels – more scanning capabilities than other Hand-Helds.

- 4 Bands (Low, High, UHF and UHF-T)
- 6 Channels – more monitoring capacity
- "Rubber Ducky" Antenna
- Belt Clip frees hands while monitoring
- 8 channels per second scan speed
- Automatic or manual scanning
- Individual channel lock-outs
- Portable – weighs only 12 ounces
- Battery operated (6 Vdc)

$199.95

BEARCAT 210

The one that pioneered synthesized scanning – and unlocks new channels of communication.

- No crystals to buy – full 6-band coverage.
- Keyboard programming makes frequency selection as easy as punching a push-button telephone.
- Decimal display and exclusive rolling zeros to show what's being programmed and monitored.
- Automatic search for finding new frequencies.

Cobra®

PUNCHES THROUGH *LOUD* and *CLEAR*

Only $179.00

Cobra 29GTL Recognized Industry Standard

Cobra's most popular CB mobile—the "Truckers choice" • Delta tune • "DynaMike" • Antenna warning indicator • Illuminated S/RF/SWR meter • Switchable automatic noise limiting and noise blanking

Cobra 78X Dollar Saver

Only $89.95

Talk to the best of them with this economy-sized, economy-priced CB • Large illuminated tuning dial • Sensitive squelch control • Full range volume control • PA jack • Legal maximum output of four watts

Only $124.95

Cobra 25GTL Full Feature Compact

You'll know your voice is out there being heard: • "DynaMike" • LED channel display with brightness control • LED transmit/receive indicator • PA/external speaker jacks • RF gain control

Only $96.00

Cobra 21GTL Command Performance/"Mini" Size

Has all the beef to punch through loud and clear • Digital LED channel display • "DynaMike" • Switchable automatic noise limiting • Illuminated S/RF Meter and much more

The Cobra 140GTL mobile gives you maximum distance with 12 full watts of power, plus quieter communications and 120 channels (80 on side-band). A perfect match for the Cobra 142GTL!

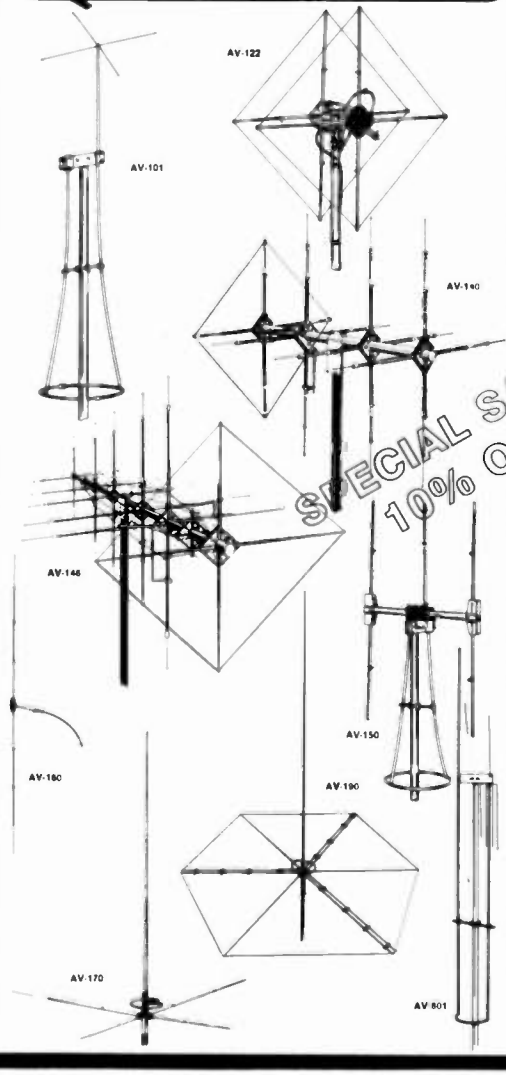
Only $249.95

Only $359.95

Cobra 142GTL CB Base Station

The COBRA 142GTL SSB/AM Base Station is for CB-ers who want extra distance, full 12 watts of power, quieter communications due to elimination of AM "clutter," and 120 channels — 80 of them on sideband.

avanti® antennas base stations



CB Antennas

AV-101 ASTRO PLANE™ — Patented performance. Best value available today in an omni directional base antenna. **$47.95**

AV-122 PDL II™ — Patented design dual polarity antenna with orbital gamma match. Light weight and long range communication in a beam antenna. Five elements on each polarity. **$199.95**

AV-140 MOONRAKER® — America's most popular and most imitated CB antenna design in a dual polarity beam. Includes cast aluminum hubs, stainless steel tip wires and many other Avanti quality features. **$515.95**

AV-146 MOONRAKER® — King of CB antennas. All the quality features of Avanti Moonraker 4 plus the exclusive 4-way boom support that protects against structural failures common to competitor's super big beam antennas. **$99.95**

AV-150 ASTRO BEAM™ — Big power in a small package. Unprecedented 40 dB front-to-back ratio for a three element vertical beam.

AV-160 RAMROD™ — The versatile all purpose antenna • CB • low or high band Business radio • short wave listening • monitor • TV-FM • civil defense • amateur • aircraft • marine • experimenting • a no nonsense full 1/2 wave antenna that is fully adjustable from 25 to 175 MHz (adjustment chart provided). **$29.95**

AV-170 SIGMA II™ — Second generation 5/8 wave with incredibly low S.W.R., 5.14 dBi gain. New static arrestor system. Easy installation. New H.D. mounting tube. Aircraft quality aluminum. New low price. **$89.95**

AV-190 SATURN™ — New scientific breakthrough. Now vertical and horizontal polarity in an omni directional antenna. Strong, long distance power in a unique dual polarity design. Unsurpassed omni power gain and SWR characteristics. Static arrestor system for clearest possible communications in all weather conditions. Easy assembly — aero space light, high strength construction tested to withstand years of wind and weather. Switchbox included. **$199.95**

Tri-Band Monitor Antenna

AV-801 ASTRO SCAN™ — A patented Tri-band base monitor design with no compromises. Unmatched gain over the whole tri-band range from 25 MHz to 512 MHz, including the new "T" band. Aerospace light construction of aircraft quality aluminum and stainless steel is well balanced on the mast to withstand years of severe wind and weather. **$34.95**

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OMNI
TEN-TEC, INC.

OMNI-Series C.

OMNI moves boldly forward to meet the new decade. With new features, new conveniences, new techniques, and new band coverage. Full amatuer band coverage from 160 through 10 meters. With its new hf capability, OMNI-C covers all six of the present hf bands and all three of the new hf bands. Crystals are supplied for seven bands (crystals for 18 and 24.5 MHz bands will be available when the bands are ready). New built-in noise blanker is standard equipment in the OMNI-C. A new design with a 2-pole monolithic crystal filter to handle the big signals with ease, to make impossible locations usable. New "Hang" AGC for smoother operation, less abrupt action.

Model 255 — Deluxe Power Supply/ Speaker Combination.

Includes the electronics of Model 280 power supply plus a built-in 3" x 5" front facing speaker.

NOVICE SPECIAL

570

Century 21 (570)
Novice Exclusive

Purchase your Century 21 570 from us and have up to one year to apply the full purchase price towards a Ten-Tec model of your choice when you upgrade your station.

MODEL 243 — Remote VFO

A duplicate of the OMNI VFO, Model 243 VFO, is housed in a matching enclosure and provides 6 modes of dual frequency operation. LEDs indicate selection of any of six modes of operation. OMNI transmit and receive, REMOTE transmit and receive, OMNI transmit—REMOTE receive, REMOTE transmit—OMNI receive, OMNI transmit—both receive, or REMOTE transmit—both receive. Full break-in is retained in all modes. Frequency range and accuracy is the same as OMNI.

In addition to the remote VFO capability, Model 243 also has a 4-position crystal oscillator for fixed frequency operation. Out-of-band crystal frequencies (with some limitations) may be used as well as any n-band amateur frequencies.

Model 243 comes with connecting cable, less crystals. Power is obtained from the OMNI system. Semiconductors: 9 transistors, 5 diodes, 6 LEDs. SIZE: HWD 5½ x 8½ x 8. Wt.: 3 lbs.

DELTA — Transceiver

DELTA is the name of a great new TEN-TEC transceiver. All 9 HF bands. First new rig since WARC, 160m through 10, including the new 10, 18 and 24.5 MHz bands! With everything incorporated except the plug-in crystals for 18 and 24.5 MHz segments (available when bands open to amateurs). No receiver front end or final amplifier adjustments. From the pioneer in broadband design. 200 Watts input on *all* bands including 10m (with 50 ohm load). High SWR does not automatically limit output to a few watts. With a proven, conservatively rated final amplifier whose solid-state output devices are fully warranted the first year and pro-rata warranted for an additional *five* years. Has all the options you could want. Model 289 Noise Blanker, Model 282 200 Hz CW Filter, Model 285 500 Hz CW Filter, Model 283 Remove VFO, Model 287 Mobile Mount, Model 280 18A Power Supply with over-current and over-voltage protection. Other matching accessories include Model 645 Dual Paddle Keyer, Model 670 Single Paddle Keyer, Model 247 Antenna Tuner, Model 234/214 Speech Processor and Mircophone, Models 215P and 215PC Ceramic Microphones, Model 252MO Power Supply.

MODEL 280 — Dual Primary Power Supply

Ideal for powering the DELTA or OMNI transceivers on either 115 or 230 VAC, 50-60 Hz. Easy to chagne for either primary voltage. Regulated output, over-voltage and over-current protected, and can be switched from transceiver or power supply Styled to match DELTA and OMNI colors.

MODEL 210 — Power Supply

Delivers up to 15 watts, sufficient for the 515. 117 VAC, 50-60 Hz input, 13 VDC, ±0.5 V, 1.2 A. output. Solid-state. Finish matches 515.

MODEL 206A — Pulsed Crystal Calibrator

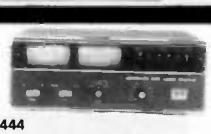
Companion to the 515, but useful with any receiving system. 25 and 100 kHz fundamental with harmonics into the VHF region. Pulsed output for easy identification. Powered by the 515 or any 9-12 VDC source. Finish matches the 515.

MODEL 208A — CW Filter/Variable Notch Filter.

CW filter has 3-position bandwidth switch, 450, 300, or 150 Hz, centered at 750 Hz; "off" position removes filter from circuit. Variable notch filter is effective over range of 200 Hz to 3.5 kHz with a depth down to 50 dB or more. Together these filters offer superb defense against unwanted signals, allow operation under most adverse conditions.

MODEL 670 — Single Paddle Electronic Keyer

Uses transistor switching and is powered through the OMNI system. Speed 6-50 wpm. Self-completing characters. Preset weighting for optimum articulation in the most used speed range (dit length increased approx. 10% at 20 wpm).



HERCULES 444
All Solid-State KW Linear Amplifier

No tubes, no tuning, full coverage: 160-15m, bands switched from OMNI panel or linear, instant break-in. 1000 Watts input, all bands. 600 Watts output, typical. Forced air cooling, automatic line voltage correction, automatic exciter by-pass, black-out meter panel, 6 status monitors with LEDs. Two meters — collecter current and voltage — forward and reverse power. Negative ALC voltage, adjustable. Built-in control power supply. Tape wound transformer and choke in, separate power supply. 117/230 VAC. Styles to match OMNI.

MODEL 247 — Antenna Tuner.

Matches 50 ohm unbalanced output of OMNI to variety of balanced or unbalanced antenna impedances. Universal Transmatch circuit. 46-tap inductor allows vernier adjustment. 200 watts intermittant, 100 watts continuous.

MODEL 217 — 500 Hz 8-Pole Crystal Ladder CW Filter

MODEL 218 — 1.8 kHz 8-Pole Crystal Ladder SSB Filter.

MODEL 219 — 250 Hz 6-Pole Crystal Ladder CW Filter.

MODELS 215P and 215PC — Microphones

Ceramic types for hand held or desk top operation. Include cable, 3-circuit plug, PTT switch, and separate desk stand. Offer optimum articulation, free of power peaks, impervious to temperature and humidity changes. High impedance; 200-4000 Hz response; -50 dB level; die cast zinc and Cycolac; 8½"h; 4' cable, single conductor shielded, two conductors unshielded. 3-circuit phone plug included. 215P has 4' regular cable; 215PC has 4' coiled cable.

Argonaut 515 — QRP Transceiver

Totally solid state, full band coverage: 3.5, 7, 14, 21, and 28 MHz (optional crystals for 29-30 MHz). 10m band now in four 500 kHz segments for greater bandspread. Improved receiver sensitivity: 0.35uV for 10 dB S+N/N, max. Four-pole 9 MHz crystal filter, 2.4 kHz Bandwidth, 1.7 shape factor. New heterodyne VFO with new permeability tuned oscillator for new frequency calibration accuracy. Direct frequency readout with new dial pointer zero-set. WWV receive at 10 and 15 MHz. Offset receiver tuning with new LED indicator. Receiver resonate control. New design no-tune broadband final amplifier. New LED rf output indicator flashes on 2 Watt voice peaks. PTT.

MODEL 645 Dual Paddle Electronic Keyer

The 645 keyer uses transistor switching and is powered by the transceiver. Adjustable magnetic paddle return. Paddle force 5-50 gms. Speed 6-50 wpm. Weighting ratio 50-150% of classical dit length. Self completing characters. Dit and dah memories with defeat switches. Torque drive paddles with 4 ball bearing pivots. Powered through the OMNI system.

MODELS 214/234 — Speech Processor and Microphone

Extends operating range of ssb transmitters under adverse and low propagation conditions. Converts audio signal into ssb signal, clips and processes it through 4-pole monolithic filter for greater average envelope power and converts signal back into audio. Adjustable levels of processing and output plus disable switch and passband adjustment. Powered through the OMNI system or by calculator type plug-in AC adapter which supplies 12 VDC @ 75 mA. Model 214 Electret Microphone is designed specifically to be used with Model 234 Processor.

MODEL	DESCRIPTION	PRICE
	ACCESSORIES	
206A	Crystal Calibrator	$ 34.50
208A	Notch/CW Filter for Model 515	39.00
212	Crystal, for Model 515, 29.0-29.5 MHz	5.00
213	Crystal, for Model 515, 29.5-30.0 MHz	5.00
214	Electret Microphone for Model 234	39.00
215P	Microphone, Ceramic with plug	29.50
215PC	Microphone, Ceramic with plug and coil cord	34.50
217	500 Hz 8 Pole Ladder Filter, for Models 545/546	55.00
218	1.8 kHz 8 Pole Ladder Filter, for Models 545/546	55.00
219	250 Hz 6 Pole Ladder Filter, for Models 545/546	50.00
234	Speech Processor	124.00
243	Remote VFO, for Models 545/546	139.00
247	Antenna Tuner	69.00
248	Noise Blanker, for Models 545/546	49.00
273	Crystal, for Model 570, 28.5-29.0	5.00
276	Crystal Calibrator, for Model 570	29.00
277	Antenna Tuner/SWR Bridge, for Model 570	85.00
282	250 Hz 6 Pole Ladder Filter, for Model 580	50.00
283	Remote VFO, for Model 580	179.00
285	500 Hz 6 Pole Ladder Filter, for Model 580	45.00
287	Mobile Mount, for Model 580	TBA
289	Noise Blanker, for Model 580	$ 39.00
	POWER SUPPLIES	
210	117 VAC, 13 VDC, 1A	$ 34.00
210/E	Same as Model 210, but 115/230 VAC	39.00
255	Deluxe, 117 VAC, 13.5 VDC, 18 A with 3" x 5" speaker	169.00
280	117/230 VAC, 13.5 VDC, 18 A	139.00
	LINEAR AMPLIFIERS	
444	Hercules, 1 kW with 115/230 VAC Power Supply	$1575.00
	TRANSCEIVERS	
515	Argonaut, 5W, SSB/CW, 3.5-30MHz	$ 429.00
545	OMNI-A, Analog, Series B, SSB/CW, 1.8-30 MHz	949.00
546	OMNI-D, Digital, Series C, SSB/CW, 1.8-30 MHz	1189.00
570	Century/21, 70 W. CW, 3.5-29 MHz	349.00
580	DELTA, 200 W. SSB/CW, 1.8-30 MHz	849.00
	KEYERS	
645	Ultramatic, Dual Paddle	$ 85.00
670	Single Paddle Keyer	34.50

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PALOMAR ENGINEERS

$299.95

ANTENNA TUNER

Here is a new tuner that puts more power into your antenna, works from 160m-10m, handles full legal power and then some, and works with coax, single wire and balanced lines. And it lets you tune up without going on the air.

All tuners lose some rf power, mostly in the inductance coil and the balun core. To avoid this we switched from No. 12 wire for the main inductor to ¼" copper tubing. It can carry ten times the rf current. And we've moved the balun from the output, where it almost never sees its design impedance, to the input where it always does. Thus more power to your antenna.

The biggest problem with tuners is getting them tuned up. With three knobs to tune on your tranceiver and three on the tuner and ten seconds to do it (see the warning in your transceiver manual) that's 1½ seconds per knob. We have a better way; a built-in 50 Ohm noise bridge that lets you set the tuner controls without transmitting. And a switch that lets you tune your transmitter into a dummy load. So you can do the whole tuneup without going on the air. Saves that final; cuts QRM.

TEMPO

TEMPO
the first in synthesized portables gives you the broadest choice at the lowest price

PRICE LIST	
Tempo S-5	$299.00
Tempo S-5 with touch tone pad	339.00
12 Button touch tone pad (not installed)	39.00
16 Button touch tone pad (not installed)	48.00
Tone burst generator	29.95
CTCSS sub-audible tone control	29.95
Rubber flex antenna	8.00
Leather holster	16.00
Cigarette lighter plug mobile charging unit	6.00
Matching 30 watt output 13.8 VDC power amplifier (S30)	89.00
Matching 80 watt output power amplifier (S80)	149.00
Tempo S-2	349.00
Tempo S-2 with touch tone pad	399.00
Tempo S-1	259.00
Tempo S-1 with touch tone pad	289.00

. . . the new S-5

- The only synthesized hand-held offering 5 watts output. (Switchable for 1 or 5 watt operation)
- The same dependability as the time proven S-1. Circuitry that has been proven in more than a million hours of operation.
- Heavy duty battery pack.
- Telescoping whip antenna.
- Ni-cad battery pack, charger.
- External microphone capability.

If you're not on 220 this is the perfect way to get started. With the addition of the S-25 (25W output) or S-75 (75W output) Tempo solid state amplifier it becomes a powerful mobile or base station. If you have a 220 MHz rig, the S-2 will add tremendous versatility. Its low price includes an external microphone capability, heavy duty ni-cad battery pack, charger, and telescoping whip antenna.

the Tempo S-2

Tempo is first again. This time with a superior quality synthesized 220 MHz hand-held transceiver. With an S-2 in your car or pocket you can use 220 MHz repeaters throughout the U.S. It offers all the advanced engineering, premium quality components and exciting features of the S-1. The S-2 offers 1000 channels in an extremely lightweight but rugged case.

Tempo S-1

- The first and most thoroughly field tested hand-held synthesized radio available. 800 channels in the palm of your hand.
- Simple to operate. (You don't need a degree in computer programming).
- Heavy duty battery pack allows more operating time between charges.
- External microphone capability.

R-X NOISE BRIDGE $55.00

- Learn the truth about your antenna.
- Find its reasonant frequency.
- Find R and X off-resonance.
- Broadband 1-100 MHz.
- Simple to use. — Self contained.

VLF CONVERTER $59.95

- New device opens up the world of VLF radio.
- Converts VLF to 80 meters. For use with any shortwave receiver covering 3.5 - 4 MHz.
- Advanced design for simple operation, high performance.
- Gives reception of the 1750 meter band.
- Also covers navigation radiobeacons, WWVB, ship-to-shore, and LF broadcast band.

LOOP ANTENNA
Loop Amplifier $67.50
Plug-in loops $47.50 ea.

- Plug-in loops available for:
  1600-5000 KHz (160/80 meter amateur bands)
  550-1600 KHz (Broadcast Band)
  150-550 KHz (VLF, 1750 meter band)
  40-150 KHz (WWVB, Loran)
  10-40 KHz (Omega)
- Nulls out interference

IC KEYER $117.50

- Sends Manual, Semi-Automatic, Full Automatic, Dot Memory, Dash Memory, Squeeze and Iambic.
- More Features than any other keyer. Built-in sidetone, speaker, speed and volume controls.
- Fully Adjustable contact spacing and paddle tension. The perfect paddle touch will Amaze you.
- Battery Operated. Heavy shielded die-cast metal case. 3-lb. steel base.
- By the World's oldest manufacturer of electronic keys.

FREQUENCY STANDARD $42.50

- 100, 50, 25, 10 and 5 Khz. Markers selectable by panel switch.
- Crystal controlled. A true secondary frequency standard.
- Square Wave Signal. Rich harmonics usable from 5 kHz to 50 MHz.
- Sharp Clear Output. Exclusive circuit suppresses unwanted markers.
- Battery Operated. No line cord. Self contained battery.

RF TRANSFORMER $42.50

- Full 2000 watt CW (5 Kw PEP).
- Matches 32, 28, 22, 18, 12, 8, 5 ohm antennas.
- For all verticals and mobile whip antennas.
- Smaller size. Higher efficiency.
- RF ferrite toroid core.

500 W. RF TRANSFORMER $35.00

- Full 500 watt CW capability. No time limit.
- Convenient switch selection of impedance taps.
- Small size. High efficiency.
- RF ferrite toroid core.

CW FILTER $39.95

- Steep skirts. No ringing.
- Simulated-stereo technique filters QRM, improves copyability of CW signals.
- 80 Hz bandwidth.
- Eight pole IC filter.

ALL BANDS PREAMPLIFIER $89.50

- Tunes 1.8 to 54 MHz. Covers ALL amateur bands 160 to 6 meters. ALL shortwave broadcast bands.
- For receivers AND transceivers.
- Up to 20 db gain.
- Peps up that tired receiver.
- Reduces image and spurious response.

BEAM BALUN $47.50

- 3 Kw CW, 6 Kw PEP input power.
- U bolt for 2" boom.
- 1.7 - 30 MHz.
- 1:1 or 4:1 ratio available.
- All stainless steel hardware.

MODEL 2K BALUN $42.50

- 3 Kw CW, 6 Kw PEP input power.
- Replaces center insulator.
- 1.7 - 30 MHz.
- 1:1 or 4:1 ratio available.

MODEL 1K BALUN $22.50

- 1.5 Kw CW, 3 Kw PEP input power.
- Replaces center insulator.
- 1.7 - 30 MHz.
- 1:1 or 4:1 ratio available.

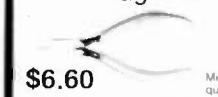
PALOMAR ENGINEERS

P.O. Box 27, Medford, Massachusetts, 02155 = TEL. 1-617-391-3200

TUFTS Electronic Department Store™ TUFTS

Tools, Parts, Accessories

Diagonal Pliers



$6.60 — ·54CG — Midget 4" size for close quarter work

$7.13 — ·55CG — 5" Plier for most cutting needs

$8.87 — ·64CG — 4" long, for fast clean, easy tip cutting of fine wires in close quarters

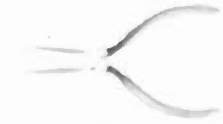
$7.48 — ·66CG — 6" all-purpose diagonal plier

$7.33 — ·67CG — 7" diagonal pliers for heavy duty cutting

Needle-Nose Pliers

$8.37 — ·56CG — 6" size. Long, slim serrated jaws permit entry inaccessible to regular long nose plier

$8.27 — ·57CG — 5½" size with fine serrated jaws and coil spring for firm gripping and looping of wire



Long-Nose Pliers

$6.85 — ·41CG — Midget 4" pliers serrated jaws without side cutters

$7.92 — ·51CG — 6" long-nose pliers with side cutters

$6.37 — ·52CG — 6" long-nose pliers without side cutters

Xcelite®

XST-5 — Super-Tru Tip (phillips type) Screwdriver Set

Contains 5 pieces — all Phillips

$13.97

SDS-44 — Square Blade Screwdriver Set

$14.76

Contains 5 Square Blade Screwdrivers for slotted screws. Catalog Nos. S-141, S-3164, S-144, S-5166, S-388

Adjustable Wrenches

Xcelite's exclusive thin-pattern design permits access where regular adjustables will not fit. Rugged construction, chrome-plated, polished heads, with quick one-hand adjustment and Cushion-Grip (CG).

·44CG — 4" length, ½" opening — $6.38
·46CG — 6" length, ¾" opening — $6.45
·48CG — 8" length, 1" opening — $7.28

Wire Strippers & Cutters

With Cushion Grip Handles

·100-X $2.63

Has adjustable screw stop for different wire sizes, and cushion grips. Cuts and strips both solid and stranded wire cleanly, neatly. Hardened with ground blades.

·101-S $3.32

Specifications same as 100, except with spring-equipped self-opening handles.

·103-S $4.12

Has unique cam stop adjustment for different wire sizes. Cam adjustment stays put, won't move, even with screw loose. Fine for industrial use.

104CG Wire Stripper and Cutter

$10.08

Cutter, stripper and crimper for all types and sizes of wire, with a wide-size-range bolt cutter. Features scissor action-up front wire cutting and wire stripping, bolt cutters, cushion grips, plier nose, hardened pivot joint bushing and crimp stations.

Quality Coaxial Cable for All Applications

- LOW LOSS CABLE • NON TARNISHING CONNECTORS
- FACTORY ASSEMBLED, TESTED FOR 100% RELIABILITY

RG58/U Type

PART NUMBER	DESCRIPTION	APPLICATIONS
581-58018 * $3.20	18" length with UHF CB plugs on both ends	Used as patch cords for mobile & base station SWR & power meters, antenna switches and SWR matchers.
581-583 * $3.70	3' length with UHF CB plugs on both ends	
581-585L * $4.10	5' length with UHF CB plug & spade lugs	Used to connect mobile CB sets to trunk, mirror, gutter or bumper mount antennas using spade lug terminations to the antenna.
581-5812L * $4.10	12' length with UHF CB plug & spade lugs	
581-5820L * $4.99	20' length with UHF CB plug & spade lugs	
581-5812 * $4.99	12' length with UHF CB plugs on both ends	Used to connect mobile CB sets to trunk, mirror, gutter or bumper mount antennas requiring a UHF CB plug termination to the antenna.
581-5820-259 $5.49 *	20' length with UHF CB plugs on both ends	
581-5850-420 $7.25	50' length with UHF CB plugs on both ends	Used where smaller diameter cable is required and signal loss is not critical.
581-5875-420 $9.29	75' length with UHF CB plugs on both ends	
581-58100-420 $10.99	100' length with UHF CB plugs on both ends	

RG 58/U Type

RG 8/U Low Loss Type

RG8/U Low Loss Type

PART NUMBER	DESCRIPTION	APPLICATIONS
581-83 * $4.10	3' lengths with UHF CB plugs on both ends	Used as patch cords for mobile and base station SWR and power meters, antenna switches & SWR matchers.
581-820 $8.50	20' length with UHF CB plugs on both ends	Used to connect mobile or base stations with antennas requiring a UHF CB plug termination at the antenna.
581-850-420 $14.99	50' length with UHF CB plugs on both ends	Used to connect base station CB sets with base antennas. Where loss is critical, these cables will out perform RG 58/U cables of the same length.
581-875-420 $22.50	75' length with UHF CB plugs on both ends	
581-8100-420 $26.50	100' length with UHF CB plugs on both ends	

LAB QUALITY CABLES

BNC Test Voltage

1500 vac; Frequency: 0-4 GHZ; Impedance: 50 Ohms nominal; Cable Retention Force: 60 lbs. minimum (RG-58C/U)

UHF Test Voltage

1500 vac; Frequency: 0-500 MHz; Impedance: Non Constant; Cable Retention Force: 60 lbs. minimum (RG-58C/U)

50 ohm UHF Plug to UHF Plug

No. 651	3 feet	$ 6.52
No. 652	5 feet	$ 7.05
No. 653	10 feet	$ 8.34

50 ohm BNC Plug to UHF Plug

No. 657	1 foot	$ 7.20
No. 658	3 feet	$ 7.72
No. 656	5 feet	$ 8.24

50 ohm BNC Plug to BNC Plug

No. 668	3 feet	$ 8.91
No. 662	5 feet	$ 9.43
No. 666	10 feet	$10.73

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Panasonic

$179.00

Panasonic RF-2200

International Band

Eight-band worldwide shortwave radio. AC or battery power. Includes AM, FM and six shortwave bands. Combination 2-stage selectivity and AFC switch. RF gain control. Separate bass, treble, and volume controls. FM/SW telescoping antennas. Four "D" batteries, AC power cord, and earphone included.

$239.00

Command Series RF-2600

Six-band portable shortwave radio with all-band, five-digit fluorescent frequency display. SW frequencies from 3.9–28 MHz. FM/AM radio. Battery/signal strength meter. AFC on FM. RF gain control. 4" dynamic speaker. Comes with AC power cord, shoulder belt and earphone. Operates on 6 "D" batteries (not included).

$249.00

Command Series RF-2900

Portable 5-band shortwave radio. Five-digit fluorescent display. SW from 3.2 to 30 MHz. RF gain control. BFO pitch control. Comes with AC power cord, shoulder belt, dial hood and earphone. Operates on 6 "D" batteries (not included).

$399.00

Command Series RF-4900

Ten-band communications receiver with 5-digit, all-band fluorescent display. SW from 1.6 to 30 MHz. FM and AM frequencies. FET RF amplifier. BFO pitch control. RF gain control. Comes with earphone, AC power cord and headphone converter. Operates on 8 "D" batteries (not included).

Kantronics

Our smart machine reads sloppy copy.

NEW! INCLUDES 24-hour UTC Clock
110 and 300 baud ASCII, & tuning eye!

Kantronics **Field Day®** $399.00

If someone tells you they offer the same features we do, check them out with the list below.

- Morse copying ability
- 3 to 80 WPM Morse range
- Computer programs for improving sloppy Morse
- Radioteletype copying ability – 60, 67.75 and 100 WPM Baudot
- ASCII radioteletype ability – 110 and 300 WPM baud
- Copies any shift of RTTY
- 24-hour UTC clock available in any mode
- Entire unit contained in one package
- Automatic code-speed tracking
- Full 10-character, large-size display
- Displays code speed
- Tuning eye for faster tuning
- Full year limited warranty
- Internal speaker
- Requires no TV set for use
- Advanced demodulator circuits
- Internal 200 Hz bandwidth filter
- All leters, numbers and punctuation plus special Morse characters and 5 special RTTY characters

DRAKE

See back cover for specials!

$1449.00

Drake R-7 / DR-7

Synthesized, General Coverage Receiver

- Fully synthesized with a permeability tuned oscillator (PTO) for smooth, continuous tuning.
- Covers complete range 0-30 MHz. Both digital and analog readout.
- Special low distortion "synchro-phase" AM detector provides superior international shortwave broadcast reception.
- Tunable IF notch filter effectively reduces heterodyne interference from nearby stations.
- Multi-function antenna selector/50 Ohm splitter is switch-selected from the front panel. Provides simultaneous dual receive with the TR-7, making possible the reception of two different frequencies at the same time.
- Built-in power supply operates from 100, 120, 200, 140 Vac, 50/60 Hz, or nominal 13.8 Vdc.
- Much more!

See back cover for specials!

YAESU

FRG-7000 $599.00

Digital Display Communications Receiver with CPU Digital Clock and Timer

- 0.25 Thru 29.9 MHz Coverage with 1 kHz Readout

Computer technology and convenience features are brought together in the FRG-7000, a digital-display general coverage receiver for the discriminating SWL. The digital clock and timer, controlled by a CPU (Central Processing Unit) chip, will read out both local and GMT time, and will control peripheral station equipment such as a tape recorder.

FRG-7 $299.00

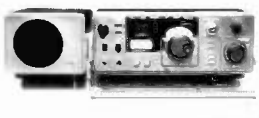
General Coverage Receiver

- 0.5-29.9 MHz Coverage with 10 kHz Readout

The FRG-7 is a precision-built all-purpose communications receiver, featuring all solid state construction for long life and high performance. Utilizing the Wadley Loop drift cancellation system, in conjunction with a triple conversion superheterodyne circuit, the FRG-7 boasts high sensitivity along with excellent stability

KENWOOD

...pacesetter in amateur radio



$499.00

Kenwood R-1000

The R-1000 is a highly advanced communications receiver. Up-conversion, PLL circuitry and other new technology provide optimum sensitivity, selectivity, and stability from 200 kHz to 30 MHz. Featuring easy-to-operate single-knob tuning and digital frequency display, it's perfect for listening to shortwave, medium-wave, and long-wave bands. Even SSB signals are received perfectly. Included is a quartz digital clock and timer.

R-1000 FEATURES:

- Continuous frequency coverage from 200 kHz to 30 MHz.
- 30 bands, each 1 MHz wide.
- Five-digit frequency display and illuminated analog dial.
- Quartz digital clock and ON/OFF timer.
- Multi-modes . . . AM (wide and narrow), SSB (USB and LSB), and CW.
- Three IF filters . . . 2.7 kHz for SSB and CW, 6.0 kHz for AM narrow, and 12 kHz for AM wide.
- Effective noise blanker, built-in speaker, three antenna terminals, rf step attenuator, tone control, recording terminal.
- Remote terminal, for access to timer relay ON/OFF circuit and muting circuit.
- SSB sensitivity of 0.5 μV from 2 to 30 MHz.
- More than 60 dB IF image ratio.
- More than 70 dB IF rejection.

P.O. Box 27, Medford, Massachusetts, 02155 = TEL. 1-617-391-3200

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FINCO STINGER VHF/UHF Antennas

On this page Tufts brings you . . .
Finco Stinger *Hitachi*
Ham-Key *Alliance*

$62.95

10 meter

STINGER A 10-4 DESCRIPTION

The model Stinger A 10-4 is a wide spaced, full size, high gain four element 10 meter monobander designed for optimum DX performance. Utilizing the exclusive Stinger Series square boom construction, the A 10-4 is light enough to be easily stacked for an additional 3 dB gain yet strong enough to withstand the most adverse weather conditions. The highly efficient gamma match system easily withstands 2,000 watts P.E.P. of power and maintains a relatively low V.S.W.R. across the entire 10 meter amateur band.

SPECIFICATIONS – A 10-4

ELECTRICAL–		MECHANICAL–	
Forward Gain	10dB	Boom Length	16 ft.
Front-to-Back Ratio	25dB	Longest Element	18.2 ft.
V.S.W.R. (at resonance)	1.1:1	Turning Radius	7.4 ft.
Half Power Beam Width	55°	Maximum Surface Area	4.4 sq. ft.
Bandwidth	28 to 30 MHz	Wind Load at 80 MPH	116 lbs.
Impedance	50 Ohms	Weight	12.5 lbs.
Matching System	Adjustable Gamma		

$46.50

6 meter

STINGER A 6-5 DESCRIPTION

The model Stinger A6-5 is a highly directional 6 meter five element beam specifically designed for maximum forward gain with a "no compromise" front to back ratio. The elements are constructed of high tensile strength seamless, aluminum tubing plus the exclusive Stinger square boom and bracket assemblies. For maximum power transfer and low V.S.W.R., a carefully designed gamma matching assembly capable of withstanding 2,000 watts P.E.P. is incorporated. Wide element spacing assures optimum DX performance and good operating efficiency across the entire 50 to 54 MHz 6 meter band. The square boom allows optional vertical mounting for accessing 6 meter repeaters.

SPECIFICATIONS – A 6-5

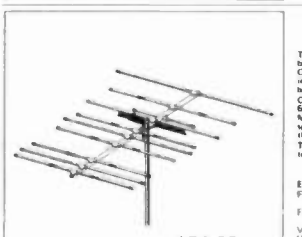
ELECTRICAL–		MECHANICAL–	
Forward Gain	11dB	Boom Length	13 ft.
Front-to-Back Ratio	25dB	Longest Element	10 ft.
V.S.W.R. (at resonance)	1.1:1	Turning Radius	8.3 ft.
Half Power Beam Width	52°	Maximum Surface Area	3.23 sq. ft.
Bandwidth	50 to 54 MHz	Wind Load at 80 MPH	40.2 lbs.
Impedance	50 ohms	Weight	11.5 lbs.
Matching System	Adjustable Gamma		

STINGER A 6-3 DESCRIPTION

The model Stinger A 6-3 is a 3-element high gain 6 meter beam similar to the A 6-5 but expressly designed for the casual 6 meter enthusiast. The A 6-3 finds excellent application for portable use as it disassembles into a very compact package. Due to the units light weight and minimal surface area, it is also ideal for double stacked and quad stacked arrays. The model Stinger A 6-3 is rated at 2,000 watts P.E.P. and incorporates gamma matching and high tensile strength aluminum elements.

SPECIFICATIONS – A 6-3

ELECTRICAL–		MECHANICAL–	
Forward Gain		Boom Length	6.0 ft.
Front-to-Back Ratio		Longest Element	10 ft.
V.S.W.R. (at resonance)		Turning Radius	5.4 ft.
Half Power Beam Width		Maximum Surface Area	1.75 sq. ft.
Bandwidth		Wind Load at 80 MPH	17.8 lbs.
Impedance		Weight	7 lbs.
Matching System			



$74.95

6 and 2 meter

STINGER A 62 DESCRIPTION

The model Stinger A 62 is a truly remarkable combination 6 and 2 meter beam designed for optimum performance on both bands yet only requiring ONE transmission line. This is accomplished through the use of exclusive phasing elements to accomplish dual band operation with no sacrifice to either band – NO SWITCHING REQUIRED!

On 2 meters, the A 62 has 8 collinear elements – equivalent to three 1/2 λ 6 element yagis stacked side by side – thus giving outstanding performance. Maximum forward gain is assured on 6 meters through the use of four wide spaced elements. The heavy duty Stinger construction is used throughout so that the antenna will withstand 100 mph plus wind loads.

The A 62 is ideal for mounting on the same mast as your tri-bander or other antenna thus easily opening up the world of 6 and 2 meter VHF communication.

SPECIFICATIONS – A 62

ELECTRICAL–		MECHANICAL–	
Forward Gain	6 meters 9.5dB 2 meters 12.0dB	Boom Length	10.1 ft.
		Longest Element	10 ft.
Front-to-Back Ratio	6 meters 19dB 2 meters 22dB	Turning Radius	6.7 ft.
		Maximum Surface Area	4.48 sq. ft.
V.S.W.R. (6 & 2 meters)	1.1:1	Wind Load at 80 MPH	43 lbs.
Half Power Beam Width	40° to 55°	Weight	13.8 lbs.
Bandwidth	6 meters 50 to 54 MHz 2 meters 144 to 148 MHz		
Impedance	50 ohms		
Matching System	Adjustable Gamma		

2 meter

STINGER A 2-10 DESCRIPTION

The model Stinger A 2-10 is a high performance wide spaced ten element 2 meter yagi designed for the serious VHF operator. Utilizing the Stinger construction features, the A 2-10 is almost indestructable no matter what weather conditions are encountered. Complete coverage of the 2 meter band and low V.S.W.R. is assured through the use of non-linear spaced elements thus also achieving maximum forward gain. Power rating – 2,000 watts P.E.P.

The A 2-10 can be mounted for vertical polarization, there by making the antenna quite useful in repeater accessing, or mounted for horizontal polarization for station to station VHF DX work. Additional bays of the A 2-10 can be easily stacked for even greater gain and front to back ratio.

SPECIFICATIONS – A 2-10

ELECTRICAL–		MECHANICAL–	
Forward Gain	13.8dB	Boom Length	10 ft.
Front to Back Ratio	25dB	Longest Element	42 in.
V.S.W.R. (at resonance)	1.1:1	Turning Radius	71 in.
Half Power Beam Width	40°	Maximum Surface Area	2.36 sq. ft.
Bandwidth	144 to 148 MHz	Wind Load at 80 MPH	76.2 lbs.
Impedance	50 Ohms	Weight	9.8 lbs.
Matching System	Adjustable Gamma		

$44.95

STINGER A 2-5 DESCRIPTION

The model Stinger A 2-5 is a five element high gain antenna similar to the A 2-10 but having physically less of a profile. The A 2-5 finds excellent application as a portable antenna as it disassembles into a very compact package. Like the A 2-10, the antenna can be mounted for vertical or horizontal polarization for repeater or general coverage work. Constructed of the Stinger heavy duty materials, the A 2-5 is ideal for locations encountering adverse weather conditions. Power rating 2,000 watts P.E.P.

SPECIFICATIONS – A 2-5

ELECTRICAL–		MECHANICAL–	
Forward Gain	9.5dB	Boom Length	5.5 ft.
Front to Back Ratio	22dB	Longest Element	41 in.
V.S.W.R. (at resonance)	1.1:1	Turning Radius	42 in.
Half Power Beam Width	60°	Maximum Surface Area	1.23 sq. ft.
Bandwidth	144 to 148 MHz	Wind Load at 80 MPH	12.3 lbs.
Impedance	50 Ohms	Weight	6.5 lbs.
Matching System	Adjustable Gamma		

$27.95

STINGER A 2+2 DESCRIPTION

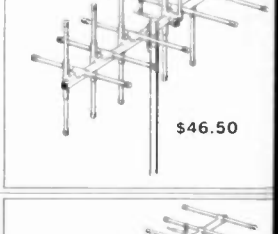
The model Stinger A 2+2 is a ten element, dual polarization 2 meter antenna designed for OSCAR communications or where switching from horizontal to vertical polarization is required. The A 2+2 can even be phased to operate on both horizontal and vertical polarization at the same time. This is not only ideal for OSCAR work but gives your station versatility for ground communications.

Wide spaced element spacing gives the A 2+2 superior gain, however, since it is a ten element beam in one given plane, the half power beam width does not make satellite tracking difficult because of its sharp directivity. The dual gamma match assemblies provide for a very low V.S.W.R. and will withstand 2,000 watts P.E.P.

The Stinger construction features make the A 2+2 extremely heavy duty. Provisions are made for mounting the antenna at the end of the boom – for azimuth control – or at the middle of the boom for normal applications.

SPECIFICATIONS – A 2+2

ELECTRICAL–		MECHANICAL–	
Forward Gain	9.5dB	Boom Length	6 ft.
Circular Gain	10.5dB	Longest Element	41 in.
Front to Back Ratio	22dB	Turning Radius End Mount	5.5 ft.
Half Power Beam Width		Center Mount	3.4 ft.
Horizontal Polarization E Plane 52° H Plane	58°	Maximum Surface Area	1.81 sq. ft.
Vertical Polarization E Plane 58° H Plane	52°	Wind Load at 80 MPH	13.4 lbs.
Circular Polarization E Plane 52° H Plane	52°	Weight	11 lbs.
Bandwidth	144 to 148 MHz		
Impedance	50 Ohms		
Matching System	Adjustable Gamma		



$46.50

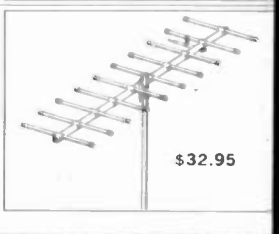
1 1/4 meter

STINGER A 1 1/4 – DESCRIPTION

The model Stinger A 1 1/4 is a ten element 1 1/4 meter (220 MHz) high performance yagi designed for all 220 MHz communication needs. Designed to be mounted in either the vertical or horizontal plane, the A 1 1/4 is adaptable for OSCAR, repeater, or general communication work. Incorporating the Stinger heavy duty elements, boom and boom to mast assemblies, the antenna easily withstands 120 mph wind loads under 1/4" ice conditions. A low loss gamma matching system assures a low V.S.W.R. and is power rated at 1,000 watts.

SPECIFICATIONS – A 1 1/4

ELECTRICAL–		MECHANICAL–	
Forward Gain	13.8dB	Boom Length	8 ft.
Front to Back Ratio	25dB	Longest Element	28 in.
V.S.W.R. (at resonance)	1.2:1	Turning Radius	4.3 ft.
Half Power Beam Width	40°	Maximum Surface Area	1.32 sq. ft.
Bandwidth	220 to 226 MHz	Wind Load at 80 MPH	17.8 lbs.
Impedance	50 Ohms	Weight	8 lbs.
Matching System	Adjustable Gamma		



$32.95

slinky

SLINKY! $43.95 Kit A LOT of antenna in a LITTLE space New Slinky® dipole* with helical loading radiates a good signal at 1/10 wavelength long!

This electrically small 80/75, 40 & 20 meter antenna operates at any length from 24 to 70 ft. ● no extra balun or transmatch needed ● portable – erects & stores in minutes ● small enough to fit in attic or apt. ● full legal power ● low SWR over complete 80/75, 40 & 20 meter bands ● much lower atmospheric noise pick-up than a vertical & needs no radials ● kit incl. a pr. of specially-made 4" dia. by 4" long coils, containing 335 ft. of radiating conductor, balun, 50 ft. RG58/U coax, PL259 connector, nylon rope & manual.

HAM-KEY™

Model HK-3M

$19.95

* Deluxe straight key
* Anti-tip bracket, Can't tip
* Heavy base No need to attach to desk
* Navy type knob
* Smooth action

CC 3P shielded cable & plug for HK 3M $7.49
Add $.50 Shipping & Handling
Model AT B anti-tip bracket only to convert any HK 3 to HK-3M $2.99

Model HK-4

$44.95

* Combination HK 1 & HK 3 on same base
* Straight key may be used conventionally or as a switch to trigger a memory.

CC 1/3P Shielded cable with plugs for HK 4 $5.99.

RADIO TELEGRAPH SENDING DEVICES

Model HK-1

$29.95

* Dual lever squeeze paddle
* For use with all electronic keyers
* Heavy base with non-slip rubber feet
* Paddles reversible for wide or close finger spacing

CC 1P shielded cable & plug for HK 1 $3.75

Model HK 2, same as HK 1 but less base for incorporation in your own keyer $19.95

Model HK-5A Electronic Keyer

$69.95

* Iambic circuit for squeeze keying
* Self completing dots & dashes
* Dot & dash memory
* Built in sidetone
* Battery operated with provisions for external power
* Uses Curtis 8044 keyer chip
* Grid block or direct keying
* Speed, volume, tone & weight controls on front panel
* Use with HK 1 or HK 4

DATONG

$219.95

MODEL FL1

Frequency – Agile Audio Filter

The Datong Frequency-Agile Audio Filter is intended primarily for post-detector signal filtering in RF and LF communications receivers for SSB and CW. It offers an unusually versatile combination of benefits to the user including:

For the SSB operator:

- Fast automatic suppression of interfering heterodyne whistles in the range 280-3000 Hz by a unique search-lock-and-track notch filter. The tracking notch can be left in circuit with no audible effect until a whistle appears in which case the whistle will 'disappear' within typically one second.
- A continuously adjustable audio 'window' or a variable-width notch to improve reception in the presense of other off-tune SSB, RTTY or SSTV signals.

For the CW operator:

- Continuously variable center-frequency (280-3000 Hz) and bandwidth (25-1000 Hz) for perfect matching of receiver passband to changing band conditions, sending speeds, and personal preference.
- Flat-topped, steep-skirted response shape for optimum ease of tuning combined with excellent noise rejection.
- Linear tuning law with bandwidth independent of frequency and gain independent of bandwidth for natural 'feel'.

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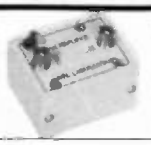
JANEL LABORATORIES



CLASSIC 2 METER PREAMP

This widely used 2 meter preamp is probably the most sensitive available today. One model provides a uniformly low noise figure across the full band. Equally applicable for DX, AM, SSB, FM and OSCAR. 18 dB gain, 2 dB noise figure, 12 vdc power (5mA). BNC connectors. Aluminum box is 1⅝x2⅛x2⅛.
Model 144PB 144-148MHz

MODEL	DESCRIPTION	PRICE
	PREAMPS	
30PB	28-30 MHz (BNC)	$ 21.95
50PB	50-52 MHz (BNC)	21.95
53PB	52-54 MHz (BNC)	21.95
137PB	135-139 MHz (BNC)	21.95
144PB	144-148 MHz (BNC)	21.95
PM-1	2m Preamp Module (Solder Terminals)	16.95
QSA 5	144-148 MHz for Transceivers (SO-239)	41.95
QSA 6	50-52 MHz (SO-239)	43.95
220PB	220-225 MHz (BNC)	21.95
432PA	420-450 MHz (BNC) 3.5 dB maximum NF	33.00
432PC	420-450 MHz (BNC) 2.0 dB maximum NF	54.95
432PE	1.0 dB typical NF	90.00
PB	Any single frequency between 30 and 50, or 148-174 MHz (BNC)	27.00
	CONVERTERS	
144CF	144-146 MHz IN, 28-30 MHz OUT (BNC)	$ 79.95
	2nd crystal for 144CF (146-148 IN, 28-30 OUT)	12.00
432CF	432-434 MHz IN, 28-30 MHz OUT (BNC)	79.95
	2nd crystal for 432CF (434-436 IN, 28-30 OUT)	10.00
	(Also available with 434-436 MHz IN and 28-30 MHz OUT, (Oscar 8, Mode J)	79.95
	OSCILLATORS	
01-A	Precision, Specify 4 or 10 MHz	$ 79.95
D1-A	10 to 1 Digital Divider	11.95
D8-A	Eight, 10 to 1 Dividers	27.95
	USEFUL ACCESSORIES	
17013	BNC to BNC, 36" RG-58C/U Cable	$ 6.00
17010	BNC to UHF, 36" RG-58C/U Cable	6.00
17014	BNC to RCA Phono, 36" RG-58C/U Cable	6.00
03005	Adaptor, BNC Plug to UHF Jack	4.00
03006	BNC Connector, UG-88/U for RG-58 size cable	1.25
	MISCELLANEOUS	
ISOLINE	Antenna Isolator, 144-174 MHz (SO-239)	$ 14.95
432FA	Cavity Filter, .5 dB loss	105.00
432FA.2	Cavity Filter, .2 dB maximum loss	115.00

For 6 Meter Transceivers

QSA5 PREAMP
For Transceivers

The QSA 5 preamp is a high performance, low noise preamp for improving the receiving sensitivity of 2 Meter transceivers. This preamp features easy installation with no modification to the transceiver required. This preamp can be used with virtually all 2 meter transceivers and on all modes — FM, SSB, CW or AM. Relays in the QSA 5 automatically bypass the preamp when transmit power is sensed. A LED indicator shows the status of the QSA 5. A front panel switch allows the preamp to be bypassed while receiving. The low noise figure of the QSA 5 provides for exceptional sensitivity. The gain has been set to optimize the performance with 2 meter transceivers.

Model PM-1

PREAMP MODULE

This low noise preamp is designed to be easily incorporated into new or existing 2 meter equipment. Solder pins are provided for mounting to a PC board or for connection to wire or coax. Uses low noise JANEL MOSFET circuitry. Each unit is fully tested for gain and noise figure. Quantity prices are available for OEM's.

UHF PREAMPS

Model 432PA 420-450MHz

Low Cost All Around Favorite

This two stage amplifier provides high sensitivity across the full 420 to 450 MHz band. A low 3.5 dB noise figure makes this preamp ideal for most amateur applications. Can be used for all modes. 17dB gain, 12vdc power (10mA). BNC connectors (50 ohms), aluminum box 1⅝x4x2⅛.

Model 432PC 420-450MHz

Extremely Sensitive

This preamp provides a low noise figure required for demanding applications. A premium state-of-the-art transistor is used to provide extremely high sensitivity. Two stages, 20 dB gain, 2 dB maximum noise figure (1.7 dB typical), 12 volt dc power BNC connectors.

6 METER PREAMP

Ideal for DX

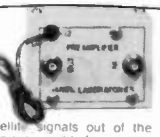
This low noise preamp significantly improves the sensitivity of most 6 meter receivers. Available in two frequency versions to cover DX and FM portions of the band. 18 dB gain, 2 dB noise figure, 12 vdc power, BNC connectors.
Model 50PB 50-52MHz. Model 53PB 52-54MHz.

For 6 Meter Transceivers

All of the features of our popular QSA-5 but for 6 meters. Fully compatable with transceivers running 30 watts or less. All mode use. Noise Figure 2dB. Gain 15dB. VSWR (transmit) 1.2. Available for 50-52 or 52-54MHz (specify when ordering). UHF connectors. **Model QSA-6.**

10 METER PREAMP

Oscar Special



Ideal for pulling weak satellite signals out of the noise. This preamp has been responsible for producing many "impossible" OSCAR QSO's. 18 dB gain, 2 dB noise figure. 12vdc power (5mA). BNC connectors. Aluminum box is 1⅝x2⅛x2⅛.
Model 30 PB 28-30MHz.

220 MHz

A Low Noise Preamp

1¼ Meters-Covers full 220-225 MHz range with 15 dB gain, 3 dB noise figure, 12 volt power and BNC connectors. **Model 220PB.**

Our Finest UHF Preamp—1.0 dB NF

This outstanding 432 MHz preamp provides the lowest practical noise figure. The finest transistors available today are combined with the ultimate in construction and alignment. Single stage. Gain 15dB (min) Noise Figure 1.2dB (max including measurement uncertainty), 0.8 to 1.0dB typical. Bandwidth 100 MHz, 12 volts at about 7 mA. Type N connectors. Size 1⅝x3x1⅝ inches. Center Frequency 400 to 512 MHz (specify when ordering). **Model 432PE.**

DAIWA

$65.95

$20.95

Coaxial Switches
2 Position/Model CS-201
4 Position/Model CS-401

RF-440 $135.95

RF Speech Processor
Models RF-400

Increases talk power with splatter free operation. RF clipping assures low distortion. **Simply install between microphone and transmitter.**
Talk Power: Better than 6 dB.
Frequency Response: 300-3000 Hz at 12 dB down.
Distortion: Less than 3% at 1 kHz, 20 dB clipping.

SWR & Power Meters
Models CN-720, CN-620 and CN-630

Professionally engineered cavity construction.
Power Rating: 2.5kW PEP, 1kW CW
Impedance: 50 Ohms
Connectors: SO-239
Insertion Loss: Less than 2 dB
VSWR: 1:1.2
Maximum Frequency: 500 MHz
Isolation: Better than 50 dB at 300 MHz; better than 45 dB at 450 MHz; adjacent terminal.
Unused Terminals grounded.

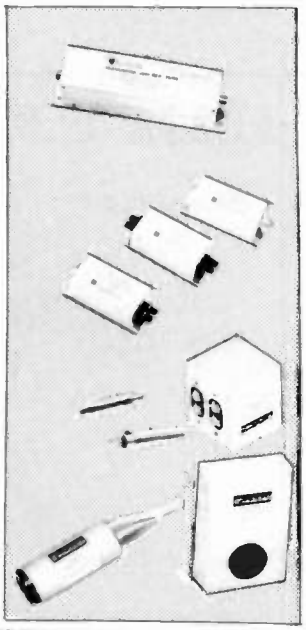
CN-720 $166.95

CN-720 and CN-620
Frequency Range: 1.8-150 MHz
SWR Detection Sensitivity: 5W min.
Power: 3 Ranges (Forward, 20/200/100W) (Reflected, 4/40/200W)

$140.50

CN-620

Interference Filters from J. W. Miller



Low Pass Filters

Eliminate or greatly reduce interference to TV receivers by radio amateur stations when installed in antenna lines of those transmitters. Input and output impedance 50 ohms. Insertion loss .3 dB max.; VWSR 1.2:1. Attenuation greater than 75 dB above 41 MHz.
C-511-T: 25 W AM 50 W PEP SSB. $19.50
C-514-T: 1000 W AM 2000 W PEP SSB. $26.80

High Pass Filters

When installed in the antenna, eliminate or greatly reduce front end overload interference to TV or FM receivers caused by amateur radio transmitters and other high frequency radio services. Filter attenuates signals below 40 MHz by a power factor greater than 1,000,000:1. Impedance C-513-T 1: 75/300 ohm C-513-T2: 75/75 ohm; C-513-T3: 300/300 ohm $10.18 $10.18

Audio Interference Filters

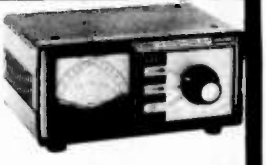
Eliminate interference caused in your audio equipment by radio amateur transmitters and other radio services. C-505-R installs in the input lines of audio equipment. Consists of 1 pair. C-506-R installs in speaker lines. Unit will take care of stereo speaker system. $5.07 $6.67

AC Power Line Filters

Eliminate or reduce interference to radio amateur receivers, TV's and radios, and prevent radio signals from entering power line.
C-508-L: 3 section LC filter, 3 A max. $ 8.33
C-509-L: 5 section LC filter (for more severe interference), 5 A max. $18.35

CN-630
Frequency Range: 140-450 MHz
Power: 2 Ranges (Forward 20/200W) (Reflected 4/40W)

CN-630 $139.00



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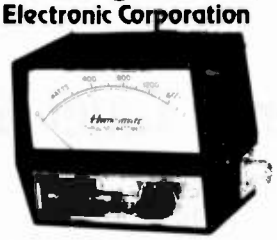
BIRD Electronic Corporation

$99 VHF model 4362 (140-180 MHz)
$99 HF model 4360 (18- 30 MHz)



The 4360, 4362 HAM-MATE Directional Wattmeters are insertion type instruments for measuring forward or reflected power in 50-ohm coaxial transmission lines. They are direct descendants of the model 43 THRULINE® Wattmeter — the professional standard of the industry—and will accurately measure RF power flow under any load condition. Each wattmeter is made up of a precisely machined section of 50-ohm line, a rotatable sensing element and meter calibrated in watts, all mounted in a high-impact plastic housing. It is this type of solid construction and the directional THRULINE coupling circuit, without toroids, that account for the superiority of the HAM-MATE Wattmeters.

the indispensable BIRD 43 THRULINE WATTMETER

Power Range	Frequency Bands (MHz) 2-30	25-60	100-250	200-500	400-1000
5 watts	—	5A	5C	5D	5E
10 watts	—	10A	10C	10D	10E
25 watts	—	25A	25C	25D	25E
50 watts	50M	50A	50C	50D	50E
100 watts	100M	100A	100C	100D	100E
250 watts	250M	250A	250C	250D	250E
500 watts	500M	500A	500C	500D	500E
1000 watts	1000M	1000A	1000C	1000D	1000E
2500 watts	2500M				
5000 watts	5000M				

MODEL 43

Elements (Table 1) 2-30 MHz	$135.00
Elements (Table 1) 25-1000 MHz	50.00
Carrying case for Model 43 & 6 elements	42.00
Carrying case for 12 elements	28.00
	17.00

READ RF WATTS DIRECTLY! (Specify Type N or SO239 connectors) 0.45 — 2300 MHz, 1-10,000 Watts ±5%, low insertion VSWR — 1.05. Unequalled economy and flexibility. Buy only the element(s) covering your present frequency and power needs, add extra ranges later if your requirements expand.

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Amphenol's BNC connectors are small, lightweight, weatherproof connectors with bayonet action for quick disconnect applications.
Shells, coupling rings and male contacts are accurately machined from brass. Springs are made of beryllium copper. All parts in turn are ASTRO-plate(R) to give you connectors that can take constant handling, high temperatures and resist abrasion.

BNC BULKHEAD RECEPTACLE 31-221-385 UG-1094 Mates with any BNC plug. Receptacle can be mounted into panels up to 104" thick. $1.25


UG-1094

BNC (M) TO UHF (F) ADAPTER 309-2900-385 UG 255 Adapts any BNC jack to any UHF plug. $3.63


UG-255

DOUBLE MATE ADAPTER 83-877-385 Both coupling rings are free turning. Connects 2 female components. $2.72


83-877-385

JACK ADPATER $1.95 575-102-385 Adapts 83-1SP-385 to Motorola type auto antenna jack or pin jack.

PANEL RECEPTACLE 83-1R-385 SO239 Mounts with 4 fasteners in 21/32" diameter hole. $1.17


575-102-385

PANEL RECEPTACLE


SO239

BNC(F) TO UHF (M) ADAPTER 31-028-385 UG-273 Adapts any BNC plug to any UHF jack. $2.39


UG-273

PUSH-ON 83-5SP-385 Features an unthreaded, springy shell to push fit on female connectors. $2.27


83-5SP-385

LIGHTNING ARRESTOR 575-105-385 Eliminates static build-up from antenna. Protects your valuable equipment against lightning damage. $4.80


575-105-385

BNC PLUG 31-002-385 UG-88 Commonly used for communications antenna lead cables. For RG 55/U & RG 58/U cables. $1.59


UG-88

BNC STRAIGHT ADAPTER 31-219-385 UG-914 1 9/32" long, allows length of cables to be joined. Mates with BNC plugs. $2.12


UG-914

BNC PANEL RECEPTACLE 31-003-385 UG-290 Mounts with 4 fasteners in 29/64" diameter hole. $1.74


UG-290

83-878-385 SO239SH Mounts in single 21/32" diameter hole. Knurled lock nuts prevent turning. $1.59


SO239SH

BNC ANGLE ADAPTER 31-009-385 UG-306 Adapts any BNC plug for right angle use. $4.23


UG-306

BNC TEE ADAPTER 31-008-385 UG-274 Adapts 2 BNC plugs to 31-003-385 or other female BNC type receptable. $4.56


UG-274

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First is the Fox XK. It reads all bands and tucks away on the visor.

Our remote (RW) unit is "out-of-sight" when installed. Out-of-sight in performance, too.

And now there's Superfox!
The first remote, superheterodyne radar warning system. Superfox has 10 times the sensitivity capability of any conventional radar detector. It is ideal for custom installations.

PRICE LIST

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60	**Fox XK** All band detector w/self contained aural/visual alarm	$109.00
60-2	**Fox XK (RW)** All band detector w/remote control, waterproof	$139.00
60-3	**Super Fox** Super-Heterodyne remote radar warning system	$279.95

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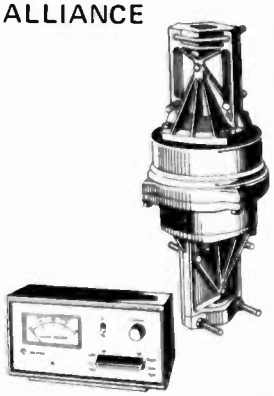
Single and dual trace, 15 and 30 MHz. All four high sensitivity Hitachi oscilloscopes are built to demanding Hitachi quality standards and are backed by a 2-year warranty. They're able to measure signals as low as 1mV/division (with X5 vertical magnifier). It's a specification you won't find on any other 15 or 30 MHz scope. Plus: Z-axis modulation, trace rotation, front panel X-Y operation for all four scope models, and X10 sweep magnification. And, both 30 MHz oscilloscopes offer internal signal delay lines. For ease of operation, functionally-related controls are grouped into three blocks on the color coded front panel.

- V-302 30 MHz Dual Trace $850.50
- V-301 30 MHz Single Trace $670.50
- V-152 15 MHz Dual Trace $625.25
- V-151 15 MHz Single Trace $490.50

ALLIANCE



$119.95

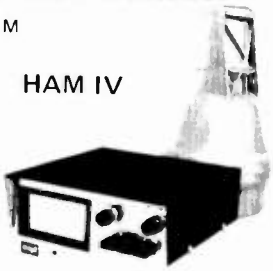
HD-73 HEAVY-DUTY ROTATOR
with exclusive Dual-Speed Control!

For antennas up to 10.7 sq. ft. of wind load area. Mast support bracket design permits easy centering and offers a positive drive no-slip option. Automatic brake action cushions stops to reduce inertia stresses. Unique control unit features DUAL-SPEED rotation with one five-position switch. SPECIFICATIONS: Max. wind load bending moment — 10,000 in.-lbs. (side-thrust overturning); Starting torque — 400 in.-lbs.; Hardened steel drive gears; Bearings — 100-3/8" diameter (hardened); Meter — D'Arsonval, taut band (back-lighted). There's much, much more.

CDE Two NEW Rotors from Cornell-Dubilier

TAIL TWISTER™

HAM IV



- For the New Super Communications Antennas
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- New Steel Ring Gear
- New Metal Pinion Gear
- New Motor Prebrake
- New Super Wedge Brake
- New L.E.D. Control Box
- Safe 26 Volt Operation

Designed for the newest of the king-size communications antennas, the TAIL TWISTER™ is the ultimate in antenna rotational devices. The TAIL TWISTER™ starts with a deluxe control box featuring snap action controls for brake and directional controls; L.E.D. indicators signal rotation and brake operation, while the illuminated meter provides direction readout. This new control box couples to the newest bell rotor. Using the time tested bell rotor principle, the TAIL TWISTER™ is a brand new design with thickwall castings and six bolt assembly. A brand new motor with prebrake action brings the antenna system to an easy stop, while the massive square front brake wedge locks the assembly in place. A new stainless steel spur gear system provides final drive into a new steel ring gear for total reliability. Triple race, 138 ball bearing assembly carries dead weight and maintains horizontal stability.
An optional heavy duty lower mast adaptor is available for lighter loads with mast mounting.
Price: $249.00

The HAM IV sets new levels of performance. Snap action switched wedge brake and rotational controls brings pinpoint accuracy to large directional arrays popular in communications. A new motor provides pre-brake action to assist in slowing down rotational mass, and the new thicker wedge brake offers far stronger lock-in phase action. To take full advantage of this new design, the HAM III is designed for in-tower mounting. A new optional heavy duty lower mast adaptor is available when the HAM III is to be mast mounted with smaller arrays. A stainless steel spur gear system multiplies the torque into the dual race 98 ball bearing support assembly assuring years of trouble free performance. **Price: $169.00**

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BANDPASS-REJECT DUPLEXER
DPLA-144 FOR 144-174 MHz
Also available for 54, 220, 450 MHz.

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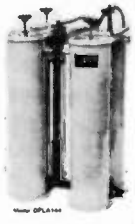
WACOM



These Band Pass Band Reject Circuit duplexers include the use of an exclusive circuit developed for WACOM, which provides superior suppression of spurious sideband noise between and adjacent to the duplex frequencies. When used with a high Q filter, the Band Pass-Band Reject Circuit provides frequency response curves with bandpass cavity characteristics at the frequency to be passed and band-reject cavity characteristics at the frequency to be attenuated.

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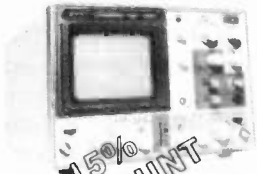


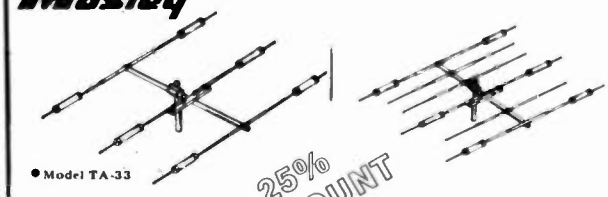
15% DISCOUNT

HITACHI OSCILLOSCOPES

Single and dual trace 15 and 30 MHz. All four high sensitivity Hitachi oscilloscopes are built to demanding Hitachi quality standards and are backed by a 2-year warranty. They're able to measure signals as low as 1mV/division (with X5 vertical magnifier). It's a specification you won't find on any other 15 or 30 MHz scope. Plus: Z-axis modulation, trace rotation, front panel X-Y operation for all four scope models, and X10 sweep magnification. And, both 30 MHz oscilloscopes offer internal signal delay lines.

- V-302 30 MHz Dual Trace $850.50
- V-301 30 MHz Single Trace $670.50
- V-152 15 MHz Dual Trace $625.25
- V-151 15 MHz Single Trace $490.50

Mosley



● Model TA-33

25% DISCOUNT

- AK-60 mast plate adapter — $14.50
- Model MPK-3, 7500 Watts AM/CW and 2000 Watts P.E.P. SSB — $67.75
- Model TA-36, 6 elements — $392.75
- Model CL-36, 6 elements — $392.75
- Model CL-203, 3 elements — $290.00
- Model TA-40 KR — 40 meter conversion kit — $119.50

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Forest Hills NY 11375

Daze of Whine and Noises

— intoxicating information about alternators

One of the puzzling problems that crop up in our VHF FM equipment is the sudden appearance of alternator whine. It is usually the first comment you receive if you have it on your signal. As befits the individualistic aspect of the hobby, there are many myths pertaining to its elimination which I shall attempt to dispel, after which I will suggest some ways of eliminating it. First, however, we should understand the reason for its being, and learn where to look for its source. The charging system in your car is the cause; the reason we have the charging system is to keep the source of all of your car's electrical power at its proper potential; the source being the car battery.

Fig. 1 diagrams the charging system for late-model GM cars. Note that the alternator is a 3-phase full-wave bridge with an output shown in Fig. 2. It is the dc component of the pulsating output voltage of the alternator that charges the battery. Since the output of the alternator will vary with engine speed — anywhere from slow idle of about 600 rpm to several thousand rpm — a regulator is added to ensure an almost constant charging voltage to the battery. This constant voltage is perhaps one to one-and-one-half volts higher than the 12.5-volt battery. Note that the battery is 12.5 volts, not the 12 volts often assumed.

Photos courtesy of Ford Motor Co.

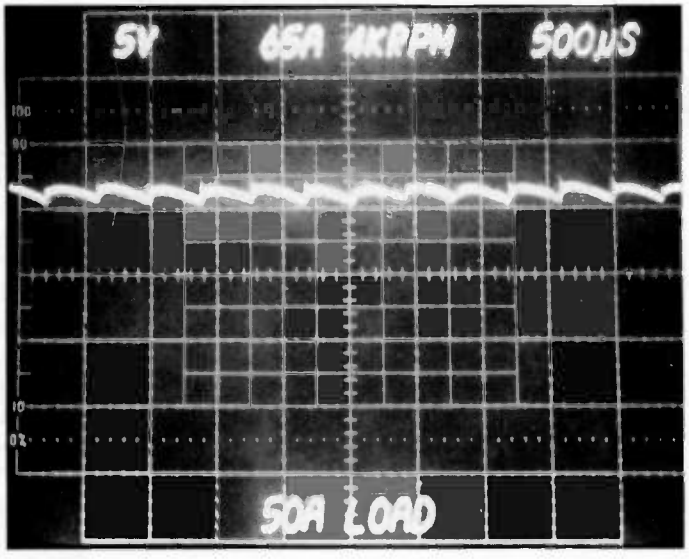

Photo A. Alternator output under actual load condition.

At one time, it was possible to adjust the charging voltage and current. My late-model car is permanently adjusted. The regulator module is mounted inside the alternator. Granted, it is a solid-state assembly, but if the permanent adjustment becomes temporary, the regulator must be replaced in its entirety. A very positive aspect of these new-fangled solid-state regulators is that there are no longer any arcing contacts involved. The older regulators had (at least) one set of contacts (voltage-adjust) opening and closing all the time the engine was running. The spurious radiation from these beauties was stultifying!

Alternator whine is the squeal mixed in with your audio that the receiving stations hear when you transmit. It varies in frequency in proportion to engine speed. The root cause of alternator whine is related to diode switching and the chopping action of the regulator. Rather than the ideal waveform shown in Fig. 2, the output of an alternator is the square wave shown in Photo A — a photo of alternator output under actual load conditions. All the scope-trace photos used a setting of 5 v/cm on the vertical axis and 500-μs timebase for the horizontal sweep.

Square waves contain many harmonics extending well into the VHF range, and since automotive designers may not be aware of the fact that we amateurs are installing VHF equipment in our cars, they don't spend too much time properly routing wiring. Nor do they spend time or additional parts trying to clean up the garbage you will see on a 12-V (sic) bus in the car, should you happen to put a scope on the Vcc line to your radio. They design in only what they have to for general usage. The fact that cars are becoming physically smaller compounds the felony. All wires, by necessity, are closer together.

In most cases, spurious radiation in the audio frequency range gets into your rig via what automotive engineers call backway point of entry. This means

through the "A" lead to your rig. The result of this is the modulation of your signal with an unwanted audio signal, represented by the squeal, in addition to the desired modulation from the microphone. I would hazard a guess that the reason that the whine manifests itself more on the transmitted signal, as opposed to receiver audio, is related to total gain in each audio circuit and the number of stages (discrete and/or IC) in the chain. I have experienced whine in a receiver, but not in its transmitter in one instance, and vice versa in another.

The spurious audio is generated by the unique nature of the alternator system. Its frequency is related to alternator rpm times a constant, K, where K equals the number of poles times the number of phases times the diode rectification factor, all divided by 60 (the conversion of rpm to Hz).

For Ford cars, which use a six-pole alternator, K = 0.6; for GM cars, which use a seven-pole alternator, K = 0.7. With an engine speed of 600 rpm, the alternator rotates at approximately 2400 rpm, since there is about a four-times multiplication factor between the engine pulley and the alternator pulley. The spurious is therefore about 1440 Hz (0.6 × 2400) for Fords—right in the middle of the audio range.

All FM gear uses audio wave-shaping in the receiver audio system not only to de-emphasize, but also to limit bandwidth. Audio is usually cut off above three kHz. Any spurious audio is also reduced in amplitude; therefore, when a radio is transmitting alternator whine, you will usually hear it only at low speeds of travel or at idle speeds. The whine may still be there, but your radio's audio system cuts it off or reduces it by a substantial amount. As a point of information, you can, with a little mathematical manipulation, ascertain that when you rev up your Ford engine above 1300 rpm, a ham, listening for your whine, will no longer hear it. All of this presupposes that your charging system is in perfect working order.

Photos B and C show the results of a failure in one of the rectifier diodes in an alternator. Photo B shows a shorted diode; Photo C, an open diode. Note first that the average output voltage drops just a little but, more importantly, that the waveform is more distorted. Without getting into a Fourier analysis, it follows

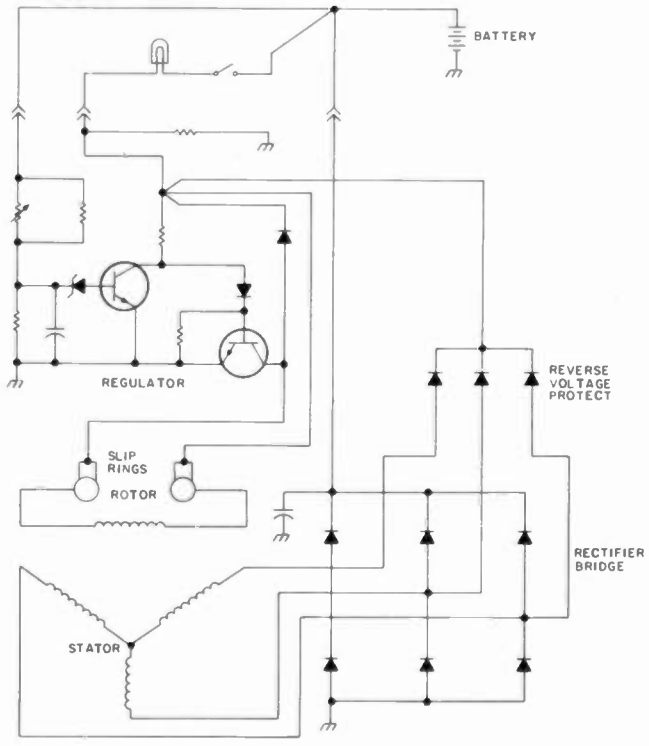

Fig. 1. The charging system for late-model GM cars.

that more spurious harmonics will be generated along with more spurs in the audio range. This will affect the "purity" of the whine you transmit. Get the hint? If your whine suddenly changes its characteristics, check your alternator diodes! Hopefully, you will have removed this annoying signal from the air long before any diodes break down.

Much has been said, but little written regarding ways to reduce the spurious transmission of whine. The most effective way that I have found, borne out by automotive people I've contacted, is to insert a properly rated choke in series with the "A" line to your radio. A value of about 20 mH worked for me. The most flagrant error made is to attempt to use a standard CB-type choke. These things are rated at only 2 Amperes. Most amateur equipment draws up-

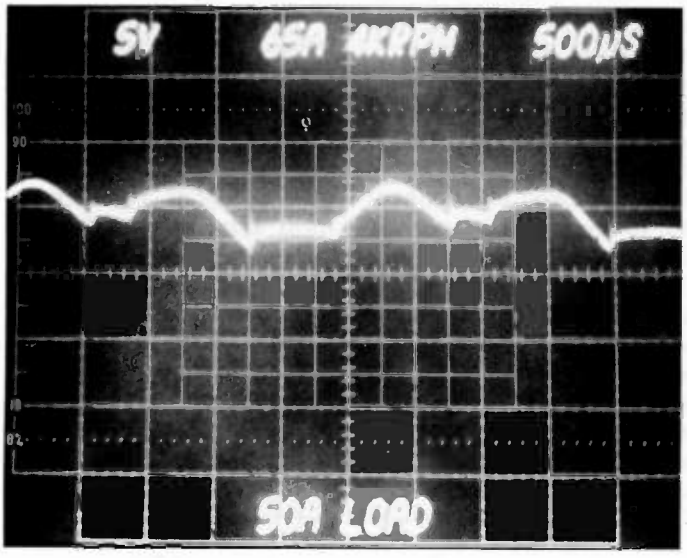

Photo B. Result of shorted diode in an alternator.

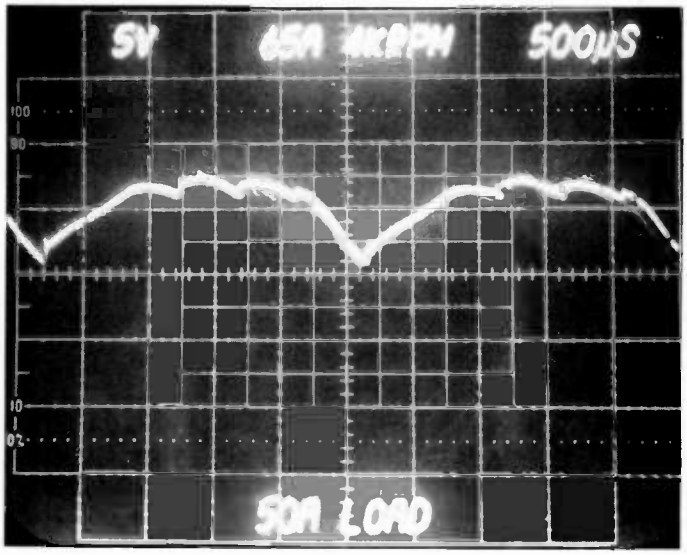

Photo C. Result of open diode in an alternator.

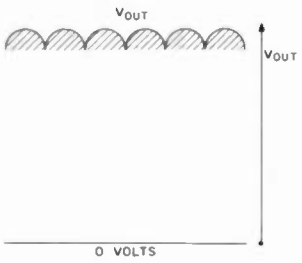

Fig. 2. Three-phase full-wave bridge output.

wards of three Amperes. This amount of current flowing through a choke rated at 2 Amps would saturate the iron core, rendering it useless. There are some 5-A CB chokes available, as well as high-current chokes used with high-power auto stereo systems.

Make sure that there is, in fact, some iron in the choke you buy. I built one on a toroidal core which had strip-iron as its base—not ferrite. Since it involved winding about 100 turns of #16 wire through the toroid, I don't recommend it—unless, of course, your hands are really calloused. I don't find that adding electrolytics across the power line is as effective as a good 0.1-to-0.5-uF capacitor. Among others, Sprague makes an excellent line of feedthrough capacitors (48P series). These should be connected in series with the battery output terminal of the alternator after you check that the capacitor case is truly grounded to the alternator case. Be sure to get a capacitor with an adequate current rating. Remember, the environment under the hood of a car is severe insofar as temperature is concerned.

For years I've been hearing that the only way to eliminate whine is to run the Vcc feed directly to the battery. One problem with this approach is that the batteries in the new cars have terminals that do not lend themselves to adding external connections. The other problem with this approach is that running long lengths of unshielded wires in the engine compartment can cause more problems than using existing wiring.

If you happen to run this new wiring in close proximity to the car wires that are radiating, you're making the job tougher to correct. Your connections should be made with at least #16 wire if there is any appreciable run length. In case you're interested in using coaxial cable for your power connections, be advised that the inner conductor of RG-8 approximates a #12 wire, RG-58 has a #19, RG-59 a #22, and a good "mini 8," a #16 wire.

Bring an AM radio close to your car wiring in the engine compartment, and note the presence or absence of whine. Don't worry too much about the other noises you hear. What you are listening to is the snap, crackle, and pop of the primary and secondary of the ignition system, the myriad solenoids and valves that are now added to the engine for pollution control. The saving grace in all this is that all of the aforementioned snap, crackle, and pop is in the form of amplitude modulation. Our VHF equipment, being frequency modulated, is pretty much immune to these spurious AM radiations. Generally, only whine is the problem.

In view of the number of models of autos on the road, it is obviously impossible to list specific fixes for whine. In general, make sure that you are making good grounds in your installation. If you are connecting your ground to a factory-installed ground, be sure the latter is a *zero resistance* connection to the battery. Arm yourself beforehand with a roll of bonding braid (Belden 8663, 8669, or equal) and literally bond your car together—electrically. You can use the same braid to shield long runs of wire by snaking the wire through the expanded braid and then grounding one or both ends of the braid.

Move some of the wires in the engine compartment away from each other to see if the induced spurs are reduced. Be careful in this operation. The SAE (Society of Automotive Engineers) has had much experience (75 years) in routing wires to prevent them from being wrapped around fans, belts, and other moving parts guaranteed to rip a harness from your car. I cannot stress too strongly the need for good grounding, and one area you should be sure to check is the antenna-to-radio ground connection if you use a magnetic-mount antenna. Remember, the base of this antenna is not grounded—it is insulated from car ground by the paint on the car, rubber gasket, or other nonconducting base material. If you use a gutter-clip mount or a trunk mount, be sure that the mounting screw(s) break through the paint and make zero-resistance contact with the body of the car. These points should be checked regularly to ensure that no oxidation or corrosion sets in to take your antenna off ground.

In my previous car, I used an extra Faston connector in the fuse block as my source of power with a choke in series with my Vcc line. But with the purchase of a new car, I found, much to my chagrin, that GM (at least) changed this connector to a special one, not yet available to the public. Temporarily, I used the cigarette lighter to power my rig with the same choke in the line. According to current myth, this is supposed to be a no-no, but I've had no complaints with that setup. I have since made a direct connection to an unused connector in the fuse block, because the cigarette lighter connection was sloppy and I wanted—or at least my wife wanted—a neater installation. This also provided me with the advantage of ignition-key control of power.

Speaking of cigarette lighters, I have been told that some new cars have reverse polarity. Be sure to check for this, because if you don't have reverse-voltage protection in your rig, you may well cause serious (and expensive) damage to your equipment. When your car is delivered with a factory-installed radio, the manufacturer usually installs a bypass capacitor—probably at the fuse block. After all, they have to have some justification for the prices charged for radios. You might consider tapping the lead that goes to your AM/FM radio for a source of power. This is easily accomplished by three-way pressure taps available in auto supply stores.

In an older car, I once was advised that I had whine where I didn't have it before and that the cause was a "weak" battery; that the internal resistance of the battery was increasing and causing whine. Well, it may have been true that the internal resistance of the battery was increasing with age, but putting in a new battery—which I hastened to do—did nothing to eliminate alternator whine!

Now, after a great deal of time expended in communicating with people at both General Motors and Ford—all of whom have been most cooperative—I have come to the conclusion that eliminating alternator whine must be done at the source—that is, at the alternator. Capacitive bypassing plus a suitable choke in series with the power feed to your radio (at the radio), in addition to good grounding practice should alleviate, if not eliminate, most whine problems. ■

LOOKING WEST

from page 12

this service, I have the knowledge to do so. Why don't I? Simply because I want to see pay-TV flourish. I feel that it has a lot to offer in quality of entertainment and consider the monthly service fee to be the same as money given to support public broadcasting. I am, however, very critical of the subscription-TV services themselves because I feel that the piracy problem is one that they have indirectly generated, and, therefore, it's one that they must solve without government intervention.

SIX METERS: A NEW YEAR'S RESOLUTION

The mail has something to say, and I am delighted with what it says. Amateurs who had put their six-meter gear in the attic or garage are taking it out and putting it back into operation. Others tell me of next-to-nothing purchases that they're making at flea markets. They're gobbling up old Heath Sixer's for 10 bucks or less, and grabbing Gonset Communicators for a song, and Clegg 99ers, radios that for years had been a collector's item, are being put back into service. People are coming back to good old six meters and having fun to boot. Many call it a return to the good old days of ham radio. No, it's not a mass exodus from other bands. In fact, it's not a mass anything—not yet. But movements take time to gain momentum and repopulating six meters will not be an overnight affair.

With the exception of one letter from a VRAC chap, all correspondence received has been highly positive. Some did question the wisdom of a return of activity to six in light of possible severe TVI, but in most cases, those writing said they would chance such a move if some good low-pass filters could be found. Many stated that the low-pass filters marketed may claim a 52-MHz cut-off but that they do not seem to be very effective. True, most are not very effective, as years of six-meter operation have shown me firsthand but, back in the early 60s, there was a very effective low-pass filter. The next time you hit a swap meet, keep your eyes open for a dull-gray aluminum box with the name "Gavin" marked on it. If you can find one of these beauties, you can literally tune away most TVI caused by six-meter transmitters operating below 52 MHz.

As I remember it, the Gavin six-meter filter had 6 sections with a tuning capacitor for each section brought out to the front panel. As I remember it, you first tuned it for maximum forward power and then re-tuned it for minimum TVI. . . and it worked. My buddy, Larry Levy WA2INM, had one of them, and it's the only filter he ever condescended to use on his home-brew six-meter masterpiece.

Larry's transmitter was a 6U8 driving a 6146 with an outboard pair of 1625s as class B modulators. The transmitter was not shielded in any way, shape, or form and completely took out the low VHF band on a TV in the next room. When Gavin came out with their filter, *73* gave it to Larry for evaluation. Reluctantly, Larry installed a coax connector on his transmitter and put the filter in-line. (ed note: Until that time, WA2INM's transmitter had no connectors in the rf circuitry. The only break in the coax came at the antenna changeover relay—an antique itself.) A "tune-for-minimum-scream" technique was employed wherein Larry tuned and waited for the screams of anguish from the other room to subside. Amazingly, in short order they did.

Later on, I borrowed the same filter from Larry and tried it at my place with the same results. In my case, the filter had an even harder job since my 6BQ6 final amplifier tube was also a doubler rich in harmonic content, and the transmitter had a link-coupled output. (ed note: I did use coax connectors and my transmitter was in a shielded enclosure.) The Gavin filter completely eliminated every trace of TVI on both the RCA set in the living room and the old DuMont upon which the entire station sat.

I do not know what ever happened to the manufacturer of this device. For a while they were involved in the consumer-TV antenna business, but seem to have now dropped from sight. Maybe one of you out there knows where they are, or perhaps how to contact someone from that company in relation to obtaining the specifications for their six-meter filter. If we were able to obtain such specifications, along with the necessary clearance to publish the data, I would be happy to do so. The Gavin filter worked; I can attest to this from firsthand experience. I also have the inimitable "INM" to back me up in this one.

Another important matter discussed in the received mail was that of converting older AM equipment to FM. I have personally converted only three radio types to FM service. They were the Lafayette HE-45 series, the Gonset Communicator II, and, believe it or not, one Heath Sixer. The Sixer was the easiest, since the superregenerative detector was broad as a barn door to start with, permitting marginal FM reception as it stands. It's only necessary to FM the transmit oscillator stage using the existing internal modulator, while rerouting the final amplifier B+ supply around the modulation transformer and directly to unmodulated B+.

I should warn you that the early HW-32s that used 50-MHz overtone crystals were extremely unstable, and conversion to 8-MHz crystals is a necessity. This means adding another tube on a sub-chassis as an electron-coupled oscillator, and converting the original oscillator to a doubler stage. Again, those of you with a good library of older *73 Magazines* are in good luck here, since Larry Levy and others wrote countless articles on how to modify a Sixer. The later HW-32As used an 8-MHz oscillator, so here it's just a simple rewire job. But, the Sixer receiver on FM? Well, if you must, but remember that they were barely marginal on AM.

The easiest FM conversions are to the Gonset Communicators. Here, there are two ways to go. If you have a matching Communicator vfo, you need only to plug in a mike and preamp. Or you can again rewire the existing transmit oscillator and screen-grid modulate it. Transmitter conversions in general are usually a matter of rerouting existing wiring. Receiver mods run the gamut from "use as they are and slope detect" to "crystal control and quad-detector installation." Here, the choice is yours.

With equipment costs as low as they are for old six-meter gear, we can afford to experiment to our hearts' content—kind of like the experimentation with 10-meter gear salvaged from the 11-meter CB service. The 11-to-10 and what is starting to happen on six meters are similar. The idea of getting back to low-cost basics. As my friend Bob Heil K9EID says in his new book about 10-meter FM, it's "putting the ham back into amateur radio." In fact, I am in the process of reading Bob's new book at this moment, and may have a review for you next month.

I guess the greatest joy I am getting out of all of this is the stir I seemed to have generated among the 10½-meter illegals. I am very proud to tell you that I have become a thorn in their side, and consider being hated by that crowd a position of honor in our society. The other evening I sat glued to my Realistic DX-160 as one of them read what he termed a "*73 Magazine* exposé" to his cronies, and then listened as this group of fanatics discussed ways to get even. Obviously, we amateurs are not the only ones who read *73*.

For those of you who may wonder if my divulging of what I have overheard is legal, well, Section 605 does not offer any form of protection to those who operate illegally, out-of-band, and unlicensed. And I do not worry about them either. Like those who harass two meters and other bands, their bark is greater than their bite. Remember, I am also a persona non grata among certain segments of the Los Angeles two-meter community, and consider this also something to be proud of. When I took to writing this column, I did not intend for it to become a popularity contest. I believe in calling things as I see them, and if certain elements of our society don't like it, such is life.

I'm not out to win any popularity contest, be it with the ARRL or anyone else. But, it's also the

same reason that I have waited a long time in some cases to report on some items, such as cases involving malicious interference. I have no intention of "trying cases in print." It's for the courts to make the legal decisions—we report. I know this is a bone of contention with some readers, but here in this nation, a person is considered innocent until proven otherwise. With the slow movement of the bureaucratic system, coupled with normal magazine lead time, it's sometimes months before you read something here that might appear in other news services sooner, though in far less detail.

But we are getting off the subject. The main thing I want to report is that people are coming to six meters little by little. They're discovering a whole new world in amateur radio. A world seemingly untouched by time. A place where they can still experiment, rag-chew, and enjoy a hobby, and do so with practically no monetary outlay. Eventually those who supply equipment for our service will catch on and start promoting new goodies, but in the meantime we can still sit back and enjoy what amateur radio is really all about. Six meters may be the band that time forgot, but, in retrospect, this may have been a blessing in disguise.

WESTLINK UPDATE DEPARTMENT

Another question that is often asked of me is why I continue to produce a weekly amateur radio newscast when there is no way to subsidize it. Actually, I am not the only one who subsidizes it, there are two of us. For the most part, the funding to keep the Westlink Amateur Radio News alive comes from Bill Orenstein KH6IAF and me. Currently, it costs us close to $500 each month, a cost that we share. And we cannot use Westlink as a tax deduction since it's not a charity, business, or any known category of business operation. It's simply the "free service" that its founder, Jim Hendershot WA6VQP, meant it to be and we intend to keep it that way. Every now and then we do receive a small donation but after doing the math out a few weeks ago, the results show that Bill and I fund over 97% of the operational costs.

Unlike other similar services, we do not solicit financial support and only accept that which is offered with no strings attached. It's this concept of total autonomy that has kept us from soliciting support from any organized group, including the ARRL. It has also kept us from asking funding from the amateur manufacturers and publishers. One cannot be autonomous if one accepts the open support of industry or anyone else. So, we just continue as best we can. It's not ego. It may have been in the beginning, but spending 10 hours a week in producing a 10-minute newscast can become an ego buster really quickly. Yet, instead of falling apart, we are growing! And I think I know the reason.

Unlike anything else in amateur radio, save one's own private station, Westlink is the only entity of its type. First, it costs the amateur nothing but a phone call to get news about his hobby service, and another phone call by him may put him into the position of providing an important story to his peers. These days, better than half of our news stories are those which are phoned to us. True, the 10-minute time constraint of our format makes it impossible to use every story we receive, but, nonetheless, the input from the amateur community itself coupled with other standard news sources is what makes it really work. It adds up to about 10 hours each week, 52 weeks a year. We take no holidays.

The reason for bringing this all up at this time is to tell you about the latest expansion of the Westlink news service: A second automated number located in the Dayton, Ohio, area is intended to provide bulletin stations and visually handicapped amateurs in the eastern and central time zones with a more economic method of obtaining the weekly newscast. The people sponsoring the new automated newsfeed are the same people who put on the nation's largest amateur radio convention each year. I speak of the Dayton Amateur Radio Association and its current President, Vic Stauder WA2KOO/8.

The whole idea started over a late snack during the 1980 Hamvention and became a reality in late September of 1980 when the Dayton newsfeed went into full-time operation. Both the Los Angeles (213)-465-5550 and the Dayton (513)-275-9991 numbers carry the same information produced in the Los Angeles Westlink facilities. The new service was inaugurated with newscast number 156, the start of the 4th year of Westlink operation. Another change made was to make the dial-in numbers public. We realize that there will be some who may abuse the service as a result of this change, but we also feel that it is far more important to have the service available to all who may need it with as little effort in obtaining it as is possible.

So, to those who ask why people like Bill Orenstein, Alan Kaul W6RCL, Jim Davis KA6IUH, Lenore Jensen W6NAZ, Burt Hicks WB6MQV, and others far too numerous to mention devote their time and effort to something that has no monetary reward, I can only tell you that we do it because we love the Amateur Service, and if nothing else, it's our way of paying back a bit of the debt we each owe amateur radio for the many hours of enjoyment we have obtained from it.

Personally, I know that Westlink, this column, and everything else I do in the name of amateur radio will never begin to repay the debt I owe the hobby, a debt that goes back many years when it was my fellow hams who carried me through one of the worst times in my life.

FUN!

from page 22

5) Believe it or not, Hiram Percy Maxim wrote an autoblographical book about his experiences as a youngster, called *A Genius in the Family*. Later, it was adapted as a motion picture and retitled. What was the name of this movie, and who played HPM's parents?

1) "That Gang of Mine"—Leo Gorcey and Joyce Bryant.
2) "Black Like Me"—James Whitmore and Judy Canova.
3) "You for Me"—Peter Lawford and Jane Greer.
4) "So Goes My Love"—Don Ameche and Myrna Loy.

ELEMENT 4—TRUE-FALSE

		True	False
1)	The original Novice license restricted its holders to QSOs of ten minutes or less, and limited conversations to discussions of signal reports, names, QTHs, weather, and rigs.		
2)	A technical editor of *QST* once electrocuted himself.		
3)	Nikola Tesla, father of practical ac power, was deathly afraid of round objects (such as baseballs and pearls) and spent many years trying to invent a device that would photograph a person's thoughts from his retina.		
4)	SSB was originally called SSSC.		
5)	The first "W" calls were issued in 1929.		
6)	Before 1950, you only had to confirm 80 countries to become a DXCC member.		
7)	Major Edwin H. Armstrong, inventor of FM radio, committed suicide by leaping fom a 13th story window. He was despondent over the fact that commer-		

cial interests were using his invention without paying due compensation. ____ ____

8) ARRL Headquarters has two club stations, W1AW and W1INF. ____ ____

9) Before 1940, the continental code for a "period" was .. .. .., not today's . - . - . -. ____ ____

10) During the "atom scare" of the late 1950s, the FCC required amateurs to monitor a broadcast station while operating in case of an enemy attack. ____ ____

11) Louis Daguerre invented the resistor. ____ ____

12) The average spark transmitter used up to 18 tubes. ____ ____

13) The US Post Office issued an amateur radio commemorative stamp in 1952. ____ ____

14) In 1957, ARRL membership cost only $5.00. ____ ____

15) First marketed in 1946, Collins' KWM-1 was the world's first fully transistorized transceiver. ____ ____

Five Questions About Marconi

16) Marconi had only one eye. ____ ____

17) Marconi won a Nobel Prize for inventing radio. ____ ____

18) Marconi was a Fascist. ____ ____

19) Marconi was half-Irish. ____ ____

20) Marconi held the amateur callsign I2CC. ____ ____

ELEMENT 5—SCRAMBLED WORDS

Unscramble these names of men who made Amateur Radio possible.

zerht	atwt	soomli
atvlo	xlwemla	yfaaard
miteteszn	plopred	pamree
mroinac		

THE ANSWERS

Element 1:
See illustration 1A.

Element 2:
1-J, 2-P, 3-T, 4-S, 5-U, 6-H, 7-C, 8-E, 9-N, 10-F, 11-K, 12-A, 13-G, 14-L, 15-I, 16-R, 17-O, 18-M, 19-D, 20-Q.

Element 3:

1-1 Sort of makes you think that ham radio hasn't really come all that far in the past 60 years, doesn't it?

2-3 Named after GE's founder, this award was tossed on the scrap heap when the company ceased selling its products to amateurs.

3-1 DX clubs and foundations, prepare your spaceships!

4-2 But friends just called him Al.

5-4 I'll bet you wonder where I dig up this info. Never mind. Just let me know the next time it appears on the *Late Show.* Perhaps the ARRL should spring some loot for a print of this classic. Bet it would be a great draw at hamfests and conventions.

Element 4:

1 False—But it sounds like a typical Soviet QSO.

2 True—Ross Hull's last experiment in 1938 involved touching the high-voltage cage on an experimental TV.

3 True—He also thought you could beam electricity from satellites in orbit around the Earth. A "crazy" idea that may actually come true in the future.

4 True—"Single-sideband, suppressed carrier" was the original name.

5 True—Before then, things were pretty confusing when you had a 2XYZ in 40 different countries.

6 False—Eighty countries isn't a "century," is it?

7 True—Typical American "success" story.

8 True—It was abuses like this that led the FCC to eliminate all new club callsigns.

9 True—And the exclamation point was - - . . - - until the change.

10 True—It was hard trying to keep the music from going out over the air.

11 False—He invented photography.

12 False—Spark transmitters didn't use tubes, silly!

13 False—1964.

14 False—It was only $4.00.

15 False—That would have been a neat trick, considering that the transistor wasn't even invented until a few years later.

16 True—He lost his right eye, in 1910, in an auto accident.

17 True—A prize which he shared with radio's "co-inventor," Karl F. Braun. By the way, the unknown Braun was so amazed that he was chosen for the honor, he actually apologized to Marconi at the awards ceremony.

18 True—Politically naive, he was an early supporter of Mussolini's Blackshirts.

19 True—His mother was born in Ireland. Marconi's first wife was also Irish.

20 False—Marconi was never a licensed amateur.

Element 5:
(Reading from left to right) Hertz, Marconi, Loomis, Volta, Watt, Faraday, Steinmetz, Maxwell, Ampere, Doppler.

SCORING

Element 1:
Twenty points for the complete puzzle, or ½ point for each question correctly answered.

Element 2:
One point for each manufacturer/distributor you matched to its QTH.

Element 3:
Four points for each correct answer.

Element 4:
One point for each correct answer.

Element 5:
Two points for each name successfully unscrambled.

0-20 points—Novice school dropout
21-40 points—Vacuum resident
41-60 points—RCC member
61-80 points—Good memory
81-100 + points—Ham historian

Illustration 1A.

W2NSD/1
NEVER SAY DIE
editorial by Wayne Green

from page 8

duce already invented and developed products more cheaply than other countries.

Further, I said that I felt that this was a perilous long-term course. Only by the development of their own electronic engineers and technicians will they be able to compete with Japan in technology. I then quoted the figures on hams in Japan. . . 500,000 active, and the US with perhaps 200,000 active. I further said that the technologies of all countries of the world are surprisingly proportional to their ham populations. Taiwan could hardly expect to compete with these other countries when it has but one single licensed radio amateur.

I told them that you get people interested in technical careers when they are teenagers and that these are the people who have always made the technology breakthroughs. Recognizing the security problem which is almost paranoic in Taiwan, I mentioned that amateur radio had been introduced in the country of Jordan right in the middle of their civil war and that no security problems had been encountered.

The Taiwan businessmen came up after the talk to thank me for it and say how much they appreciated me speaking out like that. One American was furious with me. . . a representative of the Electronic Industries Association (EIA) who felt that we should try to keep technology in the US and not encourage other countries to compete.

Two of the newspaper reporters present wanted copies of my talk to publish, so Sherry typed it up for them from her recording of my impromptu remarks. They also sent photographers to take pictures of me to go with the articles. Whether this will have any long-range effect or not remains to be seen.

To show that Japan is decidedly ahead of us in the development of electronics products, all I have to do is open my gadget bag which I cart around. Out comes a Sony TCS-300 stereo recorder, a Sony 400 micro-recorder, a Sharp Talking Clock, A Casio musical calculator or two. . . things like that. On my wrist is a Casio C-80 calculator watch which has replaced the Rolex I wore for many years. Sherry usually has her Sharp computer and cassette Interface in her bag, along with her Sony recorder for program and data storage. This is the same unit Radio Shack is importing and selling as their TRS-80PC. With about twice the number of active hams in Japan, is it any wonder they are so far ahead of us in electronics technology?

My recent visit to Kenwood in Tokyo did not brighten my view of the prospects for American firms. I've seen nothing here to compare with the Kenwood development lab. . . and with the Yaesu lab which I visited last year. These labs are packed with hams, all having a ball designing next year's ham rigs.

JAPAN AND REPEATER JAMMING

Since repeaters are not yet permitted in Japan, what is the connection I'm trying to make? This one is a bit far afield, but perhaps you'll come with me and see some parallels. By the way, with regard to repeaters in Japan, the benefits of repeaters in other countries have not been entirely lost on the Japanese. . . it's just that their version of the FCC moves far more slowly than ours, though you may think that impossible.

Having recently wandered the streets of several Asian countries, often at night, and never once having to fear that I would be in trouble, I have been wondering about this. Why is it that women can walk alone at night in Tokyo with no worries? Why is it that I have no problems when I walk in even the seemingly worst parts of Hong Kong at night? Yet, there are many areas of New York City which are not even safe during the daytime?

One of the reasons why I deserted New York almost 20 years ago had to do with the deterioration of life there. Nowadays, when I do have to visit the city on business or for a show, I can feel the fear which grips New Yorkers as they plod through the subway stations or walk the streets. . . even the well-lighted streets. . . at night.

Another indication of the wide difference between the Asian cities and our U.S. cities is evidenced in the graffiti. This is just one clear evidence of resentment which is not well hidden. . . the growing hate of the government by the people. This manifests itself in incessant vandalism, where anything which can be destroyed usually is. You don't see this in Japan, Hong Kong, Taiwan, and Singapore.

Milton Friedman put his finger on this in a recent *Newsweek* column. . . and I think he is right. This vandalism and the growing crime are results of the frustrations people are having with government. The recent election results certainly showed that the frustration level is high. It makes sense to me.

Having recently read the William Simon paperback, *A Time For Truth*, an expose of the gradual encroachment upon us by our government. . . and having felt the helpless frustration of being in the clutches of that government myself. . . I am beginning to understand what has happened to our country. . . and to much of Europe, which has been going along with the same political tide. In the Asian countries which I have visited, the governments for the most part are not interfering with business and with the people. . . certainly not to the extent which we have developed.

Having been around since before these great changes started, back in the 30s, I've seen personally the enormous change which we have undergone in our country. . . and been frustrated by it. Much of this has been in reaction to the panic and depression of the 30s, yet we know now that that was brought about primarily by the actions of our government and was not a failure of business at all. Friedman, in his TV series, *A Time To Choose*, made this clear.

Hong Kong and Singapore are shining examples of what can result when the government does not try to shackle business and dominate the people. Both are centers of great industrial growth and wealth. Indeed, you see more Mercedes cars per block in these countries than anywhere else in the world I've visited. Yet this wealth is not gained from taking advantage of workers, who also are enjoying a level of living which is attracting people from all over the world.

One wonders what would happen to the spirit of our country if the government stopped trying to manage the economy and business. . . a sort of small-scale copy of the Russian management system, which has failed so monstrously. It does seem likely that our oil problems would be resolved in a free market. . . that businesses could save billions a year if they could stop having to fill out forms for the government. I know that even in a business as small as mine, we are spending an estimated $75,000 a year just in filling out forms for the government. . . gathering information that we have no need for ourselves and sending it in. That may not seem like much, but that's almost a dollar per subscriber for *73*.

It may be that Reagan will be able, as none before him has, to start cutting down on the government proliferation. Will they be able to get rid of the HEW? Of the ICC? OSHA? The Energy Department. . . and so on? And will that eventually bring about happier people and less crime? My end question. . . I wonder, if we are able to make these changes, if it will result in a spirit in our country which will still the jamming of repeaters, the cursing on the bands, and the general unhappiness which is being demonstrated on our ham bands?

We really don't have to just learn from our past, when we did not have the government bureaucrats all over us and things were happier. . . we can learn from the lessons of those few countries where there is freedom and they do show the same spirit I saw here when I was young. . . and which I think we can regain.

The people in Japan are happy and their subways clean. There is not one hint of the graffiti which covers every car and station in the New York subway system. In describing what I saw in a public toilet in the leading restaurant in Canton, China, I

was moved to compare it with the filth and smells of a toilet in a New York subway...only worse, if such is imaginable. Japan, though close to China, has nothing like that.

Several of the people on our visit to China described the frequent serving of tea as the Chinese water torture...since the use of any bathroom but that in our hotel was almost impossible for the women...and the tourist service kept us away from the hotel from early morning till very late at night.

OOPS, WE GOOFED AGAIN?

A few years ago, I ran an article in *73* by a chap who told about discovering the principle of the transistor back in the 1930s...the only problem was that he didn't recognize what he had discovered. Thus amateur radio managed to miss out on one of the most startling discoveries of history. Win a few, lose a few.

Some recent events lead me to wonder if we may not have managed to miss the boat again, though this time there is still an opportunity to pick up the marbles and claim ourselves winners.

Thirty years ago, when amateur radio was in a period of very rapid development using ideas left over from the War and catching up for the time lost from 1941-1945 when we were off the air, we saw the beginnings of VHF repeaters, the first single sideband rigs, and a brief experimentation with double sideband. But, let me explain some recent events so you'll see what I'm talking about.

My success in recording business meetings and symposiums with a miniature Sony TCM-600 cassette recorder was such that when the need arose for a second recorder for this purpose, nothing else was even considered. It is small, light, and amazingly sensitive, putting similarly sized recorders of other brands to shame. Fortunately for me ...and possibly for you...the local Sony dealer was out of TCM-600s when I wanted one.

A few days later, I saw an ad in *The New Yorker* for a Sony TCS-300, a miniature stereo cassette recorder. Having enjoyed the phenomenal reproduction of the Sony Walkman stereo cassette player, the idea of being able to make stereo recordings with something not much larger than the player was attractive. And the ad pointed out that a stereo recording of a meeting made it possible to sort out the various voices talking with ease, while a mono recorder mixed them all together. Definitely a plus.

Despite the full-page ads for the new recorder, Sony had no TCS-300 recorders available when I called. Okay, I'd be in Tokyo in a few days and I'd get one there. Sure enough, I checked with the Sony store in Tokyo and was able to get a 300 immediately. Further, the price was $130 instead of the U.S. price of $220—a plus. I'd brought along my Walkman Sony and some music tapes, so I checked them out on the 300 and found it as fantastic on music as the Walkman...though a bit more bulky to carry.

As a side note, the Sony Walkman has been such a hit worldwide that I saw imitations of it at all of the consumer electronic shows...in Tokyo, Seoul, Taipei, and Hong Kong. They all seemed to be good buys and less expensive than the Sony. Once you hear one of these tiny stereo cassette players, you almost have to have one. I use one while I walk, to make the time pass better on plane trips, and even while skiing.

On the Asian trip, I began to use the 300 to make recordings during some of the dinners. When I checked the recordings, I was surprised to find that I could indeed hear what everyone around the table was saying, despite the high level of din from surrounding tables. Most Chinese meals call for ten people to a table, so there are two to five simultaneous conversations going on. With the stereo I could "tune in" with my mind and listen to any of them.

This brought to mind a letter to the editor in one of the ham magazines back in the early 50s. It had to do with using the General Electric Signal Splitter, with one earphone connected to the upper sideband output and the other to the lower sideband. The letter reported that using this system it was possible to tune in one double sideband signal and hear it much more clearly than with ordinary monophonic reception. I tried the idea at the time and found that the writer was right—the result was a very easy to copy phone signal which could be heard clearly through considerable interference.

The next idea came quickly ...what would happen if we were to use stereo microphones on our double sideband transmitter and separate channels into stereo earphones for reception? I suspect that the result would be much the same as listening to the individuals around the table amid the babble in the background...something which completely ruins monophonic recordings.

Would it be possible to use stereo DSB on the ham bands? With such a system, would it be possible for us to operate with stations every few Hertz up and down the band? I suspect that this might well be so. We know that monophonic double sideband signals with a synchronous detector can give good results with very narrow channel spacing. Using the human brain for the filter we should be able to get even better operation since no filter has ever even come close to the ability of the brain to do this kind of work.

The ball is in your court. There is the idea...now it is up to you to do the experimentation and development. Will it be possible for phone stations to operate at a density of perhaps 50 times that presently possible using single sideband...and with far less interference? I suspect this may be true. If it is, we may have another amateur radio breakthrough in communications techniques. You may be sure that I'm interested in getting articles for *73* on your experimental work ...and the results.

As I've written recently, the possibilities for DSB seem greater than those for SSB and one is led to wonder what might have happened in history if General Electric had supported John Costas and his DSB work as well as Art Collins did single sideband. Amateurs who were active on the DX bands in the 50s remember the many experimental flights of SAC planes with Collins sideband gear aboard. I remember Mort Kahn W2KR and Don Merten W2UOL (also K2AAA) and their efforts to promote SSB for Collins. I don't know how much they got out of their work, but I know Mort would be unlikely to work that hard for much less than millions. Since billions were at stake, a few million would have been a small investment.

It thus turns out that Kahn has had a substantial impact on amateur radio...and the world, for that matter. He originally owned Tempco, a firm making transmitters, but which he sold to Otis Elevator. Kahn retired to his yacht with several million dollars from the sale, as I understand the story. The SSB coup did not hurt his fortunes and I think got him interested in taking over the ARRL, which he did almost singlehandedly during the early 60s.

I've already reported on how Kahn managed to get elected to the ARRL and how he quickly took over running the organization. I've also covered how he engineered the move toward a return to the Class A and B licensing which stopped U.S. ham growth for over ten years and set up Japan to surpass us in technology in the 1980s.

If DSB/stereo turns out to be as efficient a communications medium as it appears, we may find that Kahn, by masterminding the sales pitch for Art Collins on SSB, did it to us again.

HORIZONS' FALL

Ham Radio Horizons, which was started in early 1977... about the same time that I started *Kilobaud MICROCOMPUTING*...and reached its peak about a year later when we had a fair number of new hams in need of the simplified articles they presented, finally threw in the towel. With the number of ad pages shrinking constantly, the magazine was losing money every month. A last-ditch effort to rescue it by changing it from a Novice magazine into another *Ham Radio* was doomed to failure.

Ham Radio itself seems to be going the same route, with the average number of ad pages dropping off. In 1977 they had 66 pages average...in 1978 there were 65 pages. By 1979 it was down to 54 pages. This year the average is down to under 35 pages of ads per month! That's obviously a catastrophe.

Part of this has been due to the competition with *73*, where most authors are aware of the better payment they get for articles in the larger circulation magazine, thus bringing the best articles first to *73*. Part has been due to the drop in interest in amateur radio in general... reflected in a particular drop in esoteric, high-technology articles. Part has been due to the

troubles between the top management of the magazine, now resolved with the death of Jim Fisk, which was reflected in the magazine content. Part was the result of the gathering depression on everyone at the publication over the failure of *Horizons* and the panic over the failure of *Ham Rádio* to cope with the changing market.

These are generally hard days for the starting of new magazines. Much of the economy is hurting. Even computer magazines have been more characterized by failure than success. We've seen *Microtrek* and *ROM* give it a big try, only to fail. We've seen *Personal Computing* magazine stagger alone, losing money for several years before throwing in the towel and giving up (it's now in the hands of Hayden Publishing, who is going to have a try at it). One of the worst debacles in the computer field has been the *Byte* offspring, *onComputing*... a total disaster. Despite incredible investments in circulation ads, the magazine has brought little more than laughs to the industry.

Our *MICROCOMPUTING* and *80-MICROCOMPUTING* magazines showed that it was not the market, only the understanding of the market that was responsible for the success or failure of a magazine. *80-MICROCOMPUTING* has been one of the most successful high-technology publications in the history of publishing.

Frankly, though the failure of *Horizons* came as no surprise, we were really expecting *CQ* to go down for the final count first. Cowan ran it into the ground before turning it over to the new crew. Despite major efforts at bringing it back to life, neither circulation nor advertising has seemed to really respond. The pages of ads have dropped from 40 average in 1979 to 36 in 1980. With the ham market continuing to drop off, the going is getting tougher for all ham magazines... and the weaker can be expected to go under. Even *QST* has been dropping... from 107 pages average in 1979 to 95 in 1980. *73* dropped a little, about 2½ pages average, running now about even with *QST*.

What will 1981 bring? Unless amateurs are able to get the hobby going again, there are going to be fewer magazines... and fewer sources of information.

THE NEW ENGLAND CONVENTION

Though I was in Tokyo at the time of the show, some spies have reported on the Boxborough ARRL convention. It appears that a fair crowd turned out for Saturday, but it was virtually deserted on Sunday. There is considerable difference of opinion on the actual number of attendees, with exhibitors putting it at around 3,500 and management at 4,500 or so. Judging from the response at the *73* booth, even the 3,500 figure is generous.

There were only two dealers at the show exhibiting... Tufts and Harrison Radio. Harrison, which seems to be in trouble these days, had little merchandise, but was promising shipment. With all but one of their stores closed and a lot of rumors flying, it was good to see that there was some life left. Tufts, which had piles of equipment available, racked up record sales for a convention.

The *73* booth kept active all through the convention, but some of the other magazines folded up early due to inactivity. *CQ* apparently has yet to win over many amateurs with their "new" format... which looks amazingly like the one which sunk it for Cowan. *HR* and *HRH*, with the loss of Fisk, seem to have lost direction and the resulting boredom with the publications was evident at the convention.

The hit of the show was a new slow-scan system from KW Control Systems. This new system provided virtually 500-line resolution pictures and had just about everything you could ask. Kenwood was there with their new equipment and that certainly got the blood going. Ditto the new Icom gear. Yaesu seems to have lost enthusiasm and was not present... nor was Den-Tron. There are rumors of a change in management at Den-Tron, with emphasis on non-ham equipment.

The Avanti and Kantronics booths were packed all through the show, as was the Optoelectronics booth. The convention was definitely worthwhile for the attendees... and for the exhibitors... no matter the actual attendance numbers.

RADAR DETECTOR PRECEDENT

The state of Connecticut was recently backed down by the courts and prohibited from confiscating radar detectors. Since this decision came from the Appeals Court, it will act as a precedent for other courts. The court also affirmed the right to a jury trial for radar detector defendants, which should further discourage that state from harassing detector users.

I WANT *YOU*!

With most magazines, your responsibility as a reader ends once you have subscribed or bought a single copy. This is not true with *73*. When you decide to read *73*, you are committing yourself to much more. I expect you to do your part toward making the magazine interesting and to accept some responsibility for this.

For instance, one of the reasons you enjoy *73* is because we have the newest in state-of-the-art articles. In fact, many professionals write to say that they are able to find out far more about new ideas by reading *73* than by reading the dry papers in the professional journals. You can help with this by keeping your eyes open for any friend who has done something or built something which we all should know about. For some reason, those who do the most brilliant work are usually least interested in doing the paperwork, so they need to have you lean on them.

You should be aware of one other factor: The more readers we have, the more advertisers we will have... and the more pages of articles we will be able to publish. So see that everyone in your ham club knows about *73*, spread the word at work, and help us to grow.

You can help me get information, too. Though I breeze through some 200 magazines a month, with several thousand out there I don't see, it is very likely that I am missing a lot of things which I should know about. So, if you run into something which you think might be of interest to me, please cut it out or make a copy and send it so I can read it. I'm interested in many things... anything on hamming, radar detectors, UFOs, Jordan, getting the US going again, microcomputers, etc.

Each month I read *Car and Driver* magazine with envy... noting their many interesting editorials. I do wish that more readers with interesting ideas and experiences would write in. With the color we are able to use in the magazine these days, we can do a much better job on DXpedition reports. So keep those cards and letters coming.

HAM HELP

I wish to convert a Lafayette model HB-740 CB rig to 10 meters. I need a schematic for this rig since Lafayette has gone out of business. Any hints or suggestions for converting the HB-740 to 10 meters will be greatly appreciated. I'll be glad to pay all costs.

Chris Van Veen N1AUD
440 Main Street
Concord MA 01742

I am in need of an ac power supply for a Collins KWM-2A.

H. F. Schnur
115 Intercept Ave.
N. Charleston SC 29405

I have a James Thomas HCV-3KB-1 keyboard for SSTV. I would like to hear from anyone who knows of a successful way to superimpose lettering over other video SSTV pictures generated by the Robot 400 scan converter. I'm also looking for any information on the RTTY and CW add-on boards for the HCV-3KB-1.

Any and all information and/or ideas would be greatly appreciated and passed on to other James Thomas owners. Thank you.

Michael Larson WD0EZK
RR2, Box 57
Jewell IA 50130
(515)-539-4345 (collect)

CONTESTS

from page 14

ble on 160-meter phone in a maximum of 30 hours allowable contest time. Multi-operator stations may operate the entire 48-hour contest period. Entry categories include single- and multi-operator, both with single transmitter on phone only.

EXCHANGE:

Stations within the Continental USA and Canada transmit RS report and state or province. All others transmit RS report and DX country.

SCORING:

All valid two-way contacts score 5 points per QSO. A station may be worked only once for contest credit! Multipliers are as follows: 1 multiplier point for each of the Continental US states (48 max.); 1 multiplier point for each of the Canadian provinces (13 max.); 3 multiplier points for each DX country outside the Continental US and Canada.

The final score is the total QSO points times the total multiplier points.

DX WINDOW:

Stations are expected to observe the DX window from 1.825 to 1.830 MHz as mutually agreed by Top Band operators. Stations in the US and Canada are asked not to transmit in this 5-kHz segment of the band.

AWARDS:

Contest awards will be issued in each award category in each of the Continental US states, each Canadian province, and each DX country.

DISQUALIFICATIONS:

Disqualifications may result if contestant omits any required entry forms, operates in excess of legal power authorized for his given area, manipulates operating times to achieve a score advantage, or fails to omit duplicate contacts which reduce the overall score more than 2%.

ENTRIES:

Each entry must include log sheet, dupe sheet for 100 or more contacts, a contest summary sheet, and a multiplier checklist. All entries must be postmarked no later than February 21st. To request contest forms or submit your entry, write: Dan Murphy WA2GZB, PO Box 195, Andover NJ 07821 USA. Please include an SASE!

FREEZE YOUR ARCTIC OFF EXPEDITION

Starts: 2000 GMT January 17
Ends: 1500 GMT January 18

The Ford Tin Lizzy Club's North Metro Chapter will endure their third expedition out on the frozen wastes of Lake Saint Clair. Operating frequencies will be 7275, 21380, 146.52, 146.55, and 146.58, as propagation allows. One station will always be active on 7275! The callsign is AD8R/8 and, as usual, a handsome certificate will be awarded to all contacts. QSL to Box 545, Sterling Heights MI 48078. No SASE is needed!

MICHIGAN QRP CLUB CW CONTEST

Starts: 1500 GMT January 17
Ends: 1500 GMT January 18

This is a CW-only allband (160-10 meters) QRP contest in conjunction with the dates of the AGCW-DL QRP contest. This contest is open to all amateurs and all are eligible for the awards. Each station will be competing within own state, province, or country in the three categories listed: (1) one Watt or less of output power; (2) five Watts or less of output power; (3) over five Watts of output power. A station may be worked only once per band for point credit.

EXCHANGE:

RST, QSO number, and power output.

SCORING:

Each contact is worth one point.

AWARDS:

Certificates awarded to the highest-scoring station in each state, province, and country.

ENTRIES:

Log information must include full log data, name, address, equipment used, and power output. Logs must be received by the contest manager no later than 6 weeks after the end of the contest. US and Canadian entries please include an SASE. All others please include one IRC for contest results. Send all logs to: Contest Manager, Michigan QRP Club, 281 Crescent Drive, Portland MI 48875.

QRP ARCI JANUARY SSB PARTY

Starts: 2000 GMT January 17
Ends: 0200 GMT January 19

The contest is open to all amateurs and all are eligible for the awards. Stations may be worked once per band for QSO and multiplier credits. No repeater contacts are allowed. VHF/UHF contacts must be direct.

EXCHANGE:

Members—RS, state/province/country, and QRP number. Non-members—RS, state/province/country, and power input.

SCORING:

Each member QSO counts 3 points. Non-member QSOs are 2 points, and stations other than W/VE count 4 points each. Multipliers are as follows: more than 100 Watts input— x 1; 25.1-100 Watts input— x 1.5; 5.1-25 Watts input— x 2; 1.1-5 Watts input— x 3; less than 1 Watt input— x 5.

Final score is total QSO points times total number of states/provinces/countries per band times the power multiplier. Any bonus points are then added to the final score. Stations powered by solar or wind power can add 300 bonus points. Stations powered by other emergency-type power (batteries, generator, etc.) can add 100 bonus points.

FREQUENCIES:

SSB—1810, 3985, 7285, 14285, 21385, 28885, 50385.

AWARDS:

Certificates to the highest-scoring station in each state, province, or country with more than two entries.

LOGS & ENTRIES:

Send full log data, including full name, address, and bands used, plus equipment, antennas, power used, and method used for determining bonus points. Members should include their QRP number on the summary sheet with the scoring. Entrants desiring results sheet and scores, please enclose a business-size envelope with sufficient return postage. Logs must be received by March 25th to qualify. Logs arriving after this date will be used as check logs. Finally, in case of disputes with scoring, the decision of the contest chairman shall be irrevocable. Send all logs and data to: QRP ARCI Contest Chairman, Edwin R. Lappi WD4LOO, 203 Lynn Drive, Carrboro NC 27510.

FRACAP WORLDWIDE CONTEST

Starts: 0000 GMT January 18
Ends: 2400 GMT January 18

Use all bands, 10 through 160 meters, on SSB only. Operating categories include single-operator, one band, and all bands.

EXCHANGE:

RS report plus a three-figure contact number starting with 001.

SCORING:

Stations in FRACAP: Each contact with another FRACAP country counts 3 points; others count 1 point.

Stations in the rest of the world: Each contact with a FRACAP country counts 5 points; others count 1 point.

The multiplier is the total number of FRACAP countries plus all call areas in the 6 FRACAP countries worked. Final score is then the total QSO points times the sum of the multipliers.

AWARDS:

Certificates to all stations with at least 20 contacts with FRACAP countries. Plaque for the first-place station in each FRACAP country in each category, and for the winner outside FRACAP. Other awards according to participation.

ENTRIES:

Entries must be postmarked no later than February 28th and addressed to: PO Box 2412, San Jose, Costa Rica, C.A. For additional information, write to the same QTH.

TEXAS QSO PARTY

Starts: 0000 GMT January 24
Ends: 2400 GMT January 25

Sponsored by the West Texas Amateur Radio Club of Odessa TX. Use all bands and modes.

Each station may be worked on each band and each mode. Mobiles may be worked again upon each county change.

EXCHANGE:

QSO number (beginning with 001) and state, province, country, or Texas county.

FREQUENCIES:

Novice—3710, 7110, 21110, 28110.

Phone—3940, 7260, 14280, 21370, 28600.

CW—3575, 7055, 14070, 21070, 28090.

SCORING:

All non-Texas stations score points as follows: Phone contact with fixed station in TX = 1 point; CW contact with fixed station in TX = 2 points; phone contact with mobile station in TX = 5 points; CW contact with mobile station in TX = 7 points. Multiply by the number of Texas counties worked (254 max).

All Texas stations score 1 point per contact on phone, 2 points on CW regardless of fixed or mobile. Multiply by the number of state, countries, and Canadian provinces worked.

AWARDS:

Plaques to top scores: US, US Novice, DX, Canada, Texas fixed, Texas mobile, Texas Novice. Certificates to top score in each state, country, and province. Special awards as activity dictates.

ENTRIES:

All logs must be received by March 15th. Mail entries to: Tom Horton K5IID, 2708 Halifax, Odessa TX 79762.

SNOWFLAKE MADNESS

The Michigan Technological University Amateur Radio Club and the Copper Country Radio Amateur Association announce a radio celebration of our Winter Carnival festivities in the northernmost part of Michigan's Upper Peninsula.

Tech's Winter Carnival is probably the most spectacular winter festival in America with fantastic snow sculptures, dog-sled races, lots of skiing, and other festive events.


HOUGHTON, MICHIGAN

Certificate No. ####

WINTER CARNIVAL

_____ of Radio Station SAMPLE has sucessfully made contact with a member of the Michigan Technological University Amateur Radio Club or the Copper Country Radio Amateur Association during our Radio Celebration of Winter Carnival.

sponsored by the Copper Country Chamber of Commerce

Date

Awards Manager

In association with the Copper Country Chamber of Commerce, we are issuing a certificate to all amateurs who make contact with any ham in the Copper Country between 0000Z February 2 and 0000Z February 9. Only one contact is required for the certificate.

Suggested frequencies are: 3.705, 3.975, 7.085, 7.105, 7.285, 14.085, 14.305, 21.085, 21.185, 21.385, 28.185, and 28.685. On CW, listen for "CQ Winter Carnival."

Send your QSL along with two 15¢ stamps (for postage and handling) to: Debbie Nietzke WD8JPX, 2005D Woodmar Dr., Houghton MI 49931.

NEW PRODUCTS

from page 35

The SC-422 is housed in a 12- × 4- × 7-inch aluminum cabinet. The US distributor for the SC-422 is *KW Control Systems, Inc., Box 114C, RD#4 South Plank Road, Middletown NY 10940.* Reader Service number 479.

1750-METER TRANSMITTER

Palomar Engineers has announced a new transmitter kit for the 160-190-kHz experimenters' band. Operation at one Watt input power and with a 50-foot maximum antenna length is permitted by the FCC with no license required.

The transmitter is in two parts. The main transmitter assembly and wiring (including winding the Litz wire coils) is factory-completed. Wiring of the kit takes about an hour with simple tools. Complete assembly and operating instructions are supplied. The transmitter is for CW operation but easily can be AM-modulated if desired. For further information, contact *Palomar Engineers, Box 455, Escondido CA 92025.*

NEW NLS TOUCH TEST 20 DMM

Futuristic touch controls and a multitude of test functions are featured in Non-Linear Systems' new Touch Test 20 digital multimeter.

The 3½-digit Touch Test 20 measures 10 parameters and 20 functions and includes 44 ranges. Test parameters include ac and dc volts, ac and dc current, resistance, capacitance, temperature, continuity, conductance, and diode test. The package size is a small 2.9 inches high by 6.4 inches wide by 8 inches deep. Weight is less than 3 pounds. Touch Test 20 may be purchased as a line powered unit or (optionally) comes equipped with rechargeable batteries for battery or line operation.

Accessories included with the instrument are OSHA-style test leads, a temperature probe,

Palomar Engineers' 1750m transmitter.

and a component test adapter for radial lead components.

An optional leather carrying case allows the Touch Test 20 to be operated while worn around the neck or on the belt, providing hands-free operation.

For further information, contact *Non-Linear Systems, Inc., PO Box N, Del Mar CA 92014; (714)-755-1134.* Reader Service number 481.

NLS's Touch Test 20.

REVIEW

from page 39

only this time you hold down the "6" button. When you think about it, this is pretty much the same way that a traditional keyer is adjusted, except that AEA has taken out the knob-twiddling.

If variable speed doesn't suit your taste, the CK-1 offers two preset speeds as well. You simply press the " * " button twice, and then press the "8". Following that, you enter the exact speed you desire. If that happens to be, say, 15 wpm, you press the "1" and then the "5". Presto! You're now operating at exactly 15 wpm. And just in case there is another CW fan in the family, you can preset another speed in the same manner, this time using the "9" key instead of the "8". Either memory can then be recalled. In either the variable mode or the preset, you can select speeds from 2 wpm all the way up to 99 wpm.

Well, so far we've discussed a lot of interesting features, but nothing of exceptional interest. Don't worry, it gets better! When AEA called this a memory keyer, they weren't joking. The CK-1 has a total capacity of about 500 characters, and this capacity is soft-partitioned, allowing you to divide the memories into up to ten messages of any length as long as the total does not exceed the storage capacity. If you want to put 400 characters in memory location "1" and 50 characters each in memory locations "2" and "3", it's perfectly possible. 50 characters in each of the ten memories? Fine. There aren't too many keyers that offer this flexibility. No matter how you juggle those memories, five hundred characters is a lot of memory. Get out your calculator and figure out how long it would take to send that at your usual speed, and you'll see what I mean. You'll have a blast loading it up with all the name, QTH, rig, and antenna information you can think of—and there still will be room for more!

"Aha," you say. "How hard is it to load?" Loading the memories couldn't be easier. Select the memory-load mode with the switch on the side of the keyer, push any button "1" through "0" to select a memory location, and start sending. This loading mode has automatic character- and word-space loading. If you pause for a normal word space or longer between characters, it will insert a normal word space in the memory and no more, so you can sit and think about what you are going to say next without filling up your memory with empty space. This provides a distinct advantage over most keyers that limit you to a real-time method of loading memory.

Admittedly, it sometimes is useful to be able to load in real time. For instance, if you are going to make a sally into the Novice bands, you may want to send at about 18 wpm but space your characters and words out so that actually you are sending at 10 wpm. Surprise! The CK-1 can do this, too. Just remember that like any real-time loading keyer, it then will eat up your available memory a lot quicker than if you send with "correct" spacing.

As you contemplate filling up that vast memory with seamless CW, the awful specter of *mistakes* rears its ugly head. Don't fret; the CK-1 has full editing capability, so when you err, you won't have to start all over again. If you get completely fed up with a particular message, it is a simple matter to erase the whole thing. You just press the memory location number (say "2") and the " * ". Whatever was in location "2" is gone forever. Naturally, if you shut the keyer off completely, *everything* goes. It is more blessed to leave the CK-1 on all the time than to reload its memories every time you operate.

By now, all the CW contesters are jumping up and down and yelling, "But does it do serial numbers?" Suffice it to say that the CK-1 will send and automatically increment any numbers between 01 and 9999, starting with the number of your choice. If you work more than 9999 stations in any single contest, you are either cheating or hallucinating.

There are a lot more things that the CK-1 can do, but I think I'll leave you to discover them on your own. All in all, I have only one complaint regarding the CK-1, and this involves the audio confirmation it gives you on each entry. I think this is a wonderful idea, but for various reasons I prefer to use the sidetone in the transceiver rather than the sidetone in the keyer. When you turn down the sidetone on the keyer, you lose the audio confirmation feature. Perhaps AEA could provide the option of having audio confirmation without the sidetone. This is, or course, a very small complaint, particularly in light of the fact that the CK-1 provides an excellent tactile response to each entry.

A commonly asked question is, "How do you remember which buttons to push?" I must confess that I was a little worried about this at first, but after about an hour with the thing I found myself handling the touchpad automatically. It's as though the keyer becomes an extension of your mind, and you suddenly realize that you are making it do what you want it to, without even thinking about it. I can't tell you exactly why, but the touchpad entry is much easier to handle than the knobs and switches on more traditional keyers. If you do forget how to make the keyer perform a particular function, you can simply refer to the clear and straightforward chart that AEA provides on the back of the instruction book.

Perhaps the most amazing thing about the CK-1 is its price. At the time of this writing, the list price is $129.95. A memory keyer with the features of the CK-1 can be a very useful tool for the CW operator; at the price, a lot of hams will be able to afford one. The CK-1 may well become the standard against which all other keyers are measured.

For further information, contact *Advanced Electronic Applications, Inc., PO Box 2160, Bldg. O & P, 2006-196th SW, Lynwood WA 98036; (206)-775-7373/524-7374.*

Paul Grupp KA1LR
73 Staff

KRECO MODEL CO2A COAXIAL ANTENNA

When hams decide to put up a base station antenna for two meters, thoughts often turn to the ubiquitous quarter-wave ground plane. The usual approach is to mangle some coat hangers and solder the results to an SO-239 chassis-mount connector. This might be the cheapest solution, but it is not necessarily the best. This configuration has a relatively high angle of radiation and is not what could be referred to as a neighbor-pleasing design. Worse, the antenna-to-coax connection is exposed to nature; if your area receives a lot of precipitation, all you can do is buy lots of plastic tape and hope for the best.

The Kreco coaxial antenna makes up for all these deficiencies, and more. As suggested by its name, this antenna uses the coaxial method of achieving a ground plane. Instead of radials, a sleeve or skirt made of aluminum is connected to the shield of your 50-Ohm coax. The sleeve fits over the support pipe, and attaches to the antenna with a reassuringly large number of hefty sheet metal screws.

All this provides several advantages over the mangled-coat-hanger approach. The angle of radiation is lowered somewhat, and the coax feedline is effectively decoupled from the antenna, allowing your transmitter's power to be put to work where it will do the most good. Best of all, since the sleeve completely covers the coax connection, you don't have to worry about water getting into your expensive coax. Finally, the whole thing screws securely onto a 3/4-inch threaded pipe. If the pipe is well supported, the Kreco antenna will survive anything short of a tornado.

So how does it work? Very well indeed. Kreco makes no claims for spectacular gain; what they offer is good basic performance in a sleek package that can be put up and left up for years and never require attention. I'll never mangle another coat hanger again!

For further information, contact *Herb Kreckman Company, Cresco PA 18326.* Reader Service number 478.

Paul Grupp KA1LR
73 Staff

LETTERS

from page 20

I'm sure that hams could come up with some pretty good ideas.

Mike Desharnais WA1IPD
Somersworth NH

IT'S YOUR FAULT

Some observations: *73 Magazine* is the only ham radio magazine that I have subscribed to since 1963. Before then, I was an ardent supporter of *QST*, but when they got whole-hawg behind this incentive licensing and helped snatch away privileges I had earned fair and square and enjoyed for ten years, then the hell with them. They couldn't *pay* me to become an ARRL member—now or ever!

I don't go out of my way to bad-mouth the ARRL, but I don't hesitate to voice my own opinions on the air when asked, either. My philosophy has always been "the first time they do it to you is their fault, but if you go back for more and they do it to you again, then it's *your* fault!"

If anyone can show me where the incentive licensing change of 1968 helped amateur radio more than it devastated it, then I'll be the first to back-paddle, but first I'll need a satisfactory answer to why today—twelve years afterward—one must tune and search across the Advanced- and Extra-class portions of the bands, especially 40 and 75 meters, to find a QSO in progress while the General part is overflowing with nets and, yes, Advanced- and Extra-class hams, all bitching about the QRM!

Oh, I know the theory behind incentive licensing—everyone does. But it hasn't really worked out, has it? The way I see it, about all it accomplished was to crowd all the activity into the upper ends of the phone bands and leave the lower ends sparsely used. And this in present-day overcrowded bands! Well, there! That's off my chest. Oh, I don't expect it to do a bit of good, but it helps to relieve the pressure inside. Thanks for listening.

Bill Skipper K0ARG
Greeley CO

THANK YOU, DICK

I have enjoyed your magazine for several years but best of all was the article on Dick Bash. It gave me the idea to upgrade to Advanced, so I sat down and ordered the "Bash cheat sheet."

I want to tell you that the Final Exam is not something to "just memorize." I followed his advice and read the guide over 10 times, but, when I came to a question that I didn't understand, I would look it up in other books.

By the time I had finished the guide, I had read many articles pertaining to electronics. When I did go to the FCC to take the test, I actually knew much more than when I started the Bash system. I also found one question in the FCC test that was exactly as Bash stated it would be. But, I knew enough to pass with flying colors.

Thanks to Dick Bash and the Final Exam, I got the shot in my arm to get off my duff and study enough to pass one more exam. Now I am looking forward to sending for the *Final Exam* for Extra and trying to upgrade for the final time.

Thank you, Mr. Bash, for not giving me anything except the incentive to learn something.

Leo Mercer N0AHH
Albert Lea MN

AWARDS

from page 16

There are no band or mode restrictions; however, I am told if the applicant wishes to be recognized for single band or mode accomplishments, the preference should be stated when making application.

The Onion Award is issued on a point basis. Stations in Belgium need to total 10 points for the award; Europeans need 5 points; other DX stations must accumulate a total of 3 points. These points are earned as follows: one (1) point for a contact with an amateur located in the Aalst section of Belgium and two (2) points for a club station within Aalst.

To apply, have your list verified by two amateurs or a local radio club official. Enclose your confirmed list with 10 IRCs and send to: Onion Award Manager, Beulens Annemie, Ravenakkerstraat 52, 9390 Moorsel, Aalst, Belgium.

Stations which qualify for points are: ON1CH, ON1JA, ON1MC, ON1MV, ON1MW, ON4JT, ON4MS, ON4NJ, ON5HZ, ON5KC, ON5NM, ON5QT, ON5SU, ON5VP, ON5VW, ON6AZ, ON6BA, ON6BN, ON6BP, ON6CW, ON6EE, ON6ED, ON6EJ, ON6HW, ON6HX, ON6IR, ON6NN, ON6NV, ON6OX, ON6PZ, ON6RK, ON6SM, ON6VW, ON6WA, ON6WS, ON6YZ.

WAC YL AWARD

The Young Ladies Radio League issues the Worked All Continent Young Ladies Award to any licensed amateur who can meet the requirements of their program.

Two-way communications must be established with Young Lady amateurs in each of the six continents of the world: North America, South America, Europe, Asia, Africa, and Oceania. The applicant may utilize any band or mode of operation; however, crossband contacts will not be valid. There is no date limitation.

While all contacts with the six continents must have been made with duly licensed women operators, your contacts must have been made from the same QTH or community not to exceed a 25-mile radius.

To apply, applicant must prepare a list of contacts and also submit QSL cards or written proof of each contact along with the application.

While there is no charge for the award, applicants are requested to forward sufficient postage to cover first class return of your QSL cards. The YL Radio League assumes no responsibility for damaged or lost cards.

Forward your applications to the Award Custodian: Miriam Blackburn W3UUG, Box 2, Ingomar PA 15127.

While on the subject of YL awards, the YL Radio League also sponsors a Worked All States effort as well.

WORKED ALL STATES—YL

If you thought for one minute that the Worked All USA Award was fairly simple, try your luck at working each state with a YL contact! Not so easy, is it?

The Young Ladies Radio League makes available the WAS-YL Award to any licensed amateur who can establish two-way contact with a YL in each of the 50 US states.

While there are no date, band, or mode restrictions, you can request single band or mode recognition at the time application is made.

To qualify, all contacts must have been made within 25 miles of your QTH and any call you possess may be used to make contact with the 50 state YLs.

To apply, place your contacts in order by state beginning with Alabama and working alphabetically through your list. Include QSL cards or other forms of written confirmation for each contact claimed.

Forward your QSL cards, your application, and the list of claimed contacts to: Stella McPherson WA4WPN, 2029 Elbow Road, Chesapeake VA 23320. Be sure to include sufficient postage for first class mail return of your QSL cards. While there is no award fee, the League will not assume responsibility for the loss or damage of your cards.

WORKED ALL TRANSKEI

Early this week I received a very nice letter from Len S8AAT and he told of the very popular

Transkei Amateur Radio League Award now being offered.

The Transkei Amateur Radio League has formally announced the Worked All Transkei Award which is made available to licensed amateurs throughout the world.

To qualify for the award, stations within Zone 38 must log a total of 4 Transkei (S8 prefix) stations since October 26, 1976. Stations outside of Zone 38 need only log two stations in Transkei.

There are no restrictions on bands or modes and even cross-band contacts are permitted. Stations wishing to be recognized for single band or mode achievements may request recognition at the time application is made.

To apply for this award, prepare a list of claimed contacts and have it verified by at least two fellow amateurs or a local radio club official. Forward this list and an award fee of $1.00 or 10 IRCs to: The Transkei Amateur Radio League, PO Box 750, UMTATA, Republic of Transkei, South African Coast.

DIPLOMA DOS CONCELHOS PORTUGUESES

Sponsored by Associacao de Radioamadores Portugueses, this Portuguese County Award is available to licensed amateurs of the world under the following rules and conditions.

First of all, the DCP (Diploma of Portuguese Counties) is issued in four (4) classes: Class A—fixed HF; Class B—HF mobile; Class C—fixed VHF; Class D—VHF mobile. According to the number of Portuguese counties confirmed, the applicant may achieve one of the following grades of award: Grade I—75 counties; Grade II—125 counties; Grade III—175 counties; Grade IV—200 counties; Grade V—255 counties; Grade VI—250 counties; Grade VII—the maximum of 274 counties.

When making application for the DCP Award, the applicant is advised first to obtain the special awards booklet available from WB9RLY, who is the Canadian and US associate of the Amateur Radio Club of Portugal. This booklet will be extremely helpful to the applicant in establishing county locations and for finally submitting his or her application.

Do not send QSL cards! Have your list of confirmed contacts verified by at least two fellow amateurs or a local radio club secretary. Forward your application and an award fee of $2.50 or 7 IRCs to: ARP, PO Box 2145, 4021 Porto Codex, Portugal.

RCCI DX AWARD

This week I was very happy to hear from my dear friend Professor Giulio Nardona, the President of the Radio Club Ciechi d'Italia. Giulio and his fellow amateurs are particularly proud of the following two awards.

The Radio Club of Blind Radio Amateurs of Italy has organized a new award entitled the RCCI DX Award. Starting from December 25, 1975, this award is open to all radio amateurs who can accumulate a total of 350 points as prescribed by the rules of the award.

Increments of 400, 500, and 600 points are earned with the delivery of blue, silver, and gold cockades to be fixed to the basic RCCI Award. In addition, every year prizes will be given to the first three amateurs better classified according to the points totaled during that year. Applicants scoring 600 points in the maximum of 10 years will be listed in the Honor Roll and will become Honorary Members of RCCI and will become "Jolly Stations" for this award.

To determine points, each country listed on the DXCC list of 1975 will have a value of one (1) point if worked on 15 and/or 20 meters. For contacts on 10, 40, or 80 meters, two points may be credited. A country may be worked only once on a band and contact with a Jolly Station may earn you 15 points; however, a Jolly Station may only be worked once.

Do not send QSL cards! Prepare a list of contacts, including date and time worked in GMT, band and mode of operation, and the points claimed for each contact. Have this list verified by at least two amateurs.

I0LL, the chairman of RCCI (Italian Radio Club for Blind Operators), in his shack. He is showing some of the instruments specifically manufactured by RCCI for blind amateurs.

Forward your application and an award fee of $4.00 or 10 IRCs to: RCCI Awards, I8KUT, PO Box 2011, 80100 Napoli, Italy, Europe.

The following stations earn the applicant 15 points: I0LL, I0PNK, I0SUQ, I0WFI, I0WHY, I1KJ, I3ANE, I4LDY, I8DOE, I8FTV, I8KUT, I8NMM, I8SRP, I8YRK, I0OGT, IT9VQC, and GM4ELV.

WORKED ITALIAN PREFIX AWARD

In remembrance of Pietro Spriano I0KA, founder and first President of the Radio Club of Blind Radio Amateurs of Italy, the organization has organized the Worked All Italian Prefix Award which becomes available to amateurs worldwide.

To qualify, all contacts must have been made on or after June 5, 1977. Contacts must be made with the following Italian prefixes: I1 through I0, IS0, IT9, one of the special ARI stations (IZ0ARI or I3ARI as examples), or one of the special memorial stations such as II4FGM or IY4FGM.

As with the RCCI Award, do not send QSL cards. GCR apply. Forward your application and an award fee of $4.00 or 10 IRCs to: I8KUT, PO Box 2011, 80100 Napoli, Italy, Europe.

Congratulations to Vernon G. Dameron, Jr. K1DRN of Bedford MA. He was the winner of a lifetime subscription to *73 Magazine* at the New England Division Convention, October 4 and 5, at Boxboro MA.

HAM HELP

I would like to obtain the service or instruction manual for a Wavetek VCG (generator), model 155. I will gladly pay a reasonable amount for a copy or the manual itself.

Arthur Hagopian W6LGQ
34 Laurel Ave.
Petaluma CA 94952

I need a copy of assembly instructions for a Hy-Gain tri-band beam, circa 1960. Commonly called the eggbeater because of the 23" loops on each end of the three elements, it has four open coils on each element and an 18' boom. I will pay for a copy.

Leslie Hogg WB8NVJ
28423 Kendallwood Dr.
Farmington Hills MI 48018

I am in need of operating manuals and schematics for the following test equipment: H-P model 520 high-speed decade scaler and model 500BR frequency meter and Sweep-Systems, Inc., model 950 oscilloscope. I will buy or reproduce and return and pay shipping costs. Thank you.

Stan Boler WD9BBV
116 S. Washington
Knightstown IN 46148

I need a manual for an AN/USM 106 video voltmeter made by Ballantine. I will pay postage and copying costs and prefer to copy here and return.

John Weber K4JW
102 Southgate Blvd.
Melbourne FL 32901

SOCIAL EVENTS

Listings in this column are provided free of charge on a space-available basis. The following information should be included in every announcement: sponsor, event, date, time, place, city, state, admission charge (if any), features, talk-in frequencies, and the name of whom to contact for further information. Announcements must be received two months prior to the month in which the event takes place. They should be sent directly to Editorial Offices, 73 Magazine, Pine Street, Peterborough NH 03458, Attn: Social Events.

SOUTH BEND IN
JAN 4

A hamfest swap & shop will be held on Sunday, January 4, 1981, at New Century Center, across from St. Joseph Bank building, US 33 north, South Bend IN. Tables are $3.00 each. There is a half acre of carpeted floor in the same building as the industrial history museum. Talk-in on 146.52/.52, .04/.64, .34/.94 and 147.99/.39, .93/.33, .78/.18, .69/.09.

OAK PARK MI
JAN 11

The Oak Park ARC will hold its annual indoor Swap & Shop on January 11, 1981, at the Oak Park High School, Oak Park Boulevard (9½ miles west of Coolidge Highway), Oak Park MI. Doors will be open from 8:00 am to 3:00 pm and admission is $2.00 per person. Features will include an ARRL table, a door prize, a YLRL table, food, refreshments, and free parking. Talk-in on 146.04/.64 and 146.52. For more information, send an SASE to Rob Numerick, 23737 Couzens, Hazel Park MI 48030, or call (313)-398-3189.

CHESTERFIELD VA
JAN 11

The Richmond Amateur Telecommunications Society will hold Frostfest 1981 on Sunday, January 11, 1981, at the Chesterfield County Fairgrounds, Chesterfield VA, from 8:00 am to 4:00 pm. New and large facilities include spacious aisles, and plenty of on-site parking, with charter buses welcome. Admission is $3.00 for each four-foot-long flea market table, and $2.00 for each tailgating vehicle. Features will include commercial exhibitors, a flea market, an auction, and prizes consisting of a color TV, a Bird Wattmeter with slug, a digital VOM, and many more. Talk-in on 146.34/.94 and 146.28/.88. For further information, contact the Richmond Amateur Telecommunications Society, PO Box 1070, Richmond VA 23208.

ARLINGTON HEIGHTS IL
JAN 25

The Wheaton Community Radio Amateurs' hamfest will be held on January 25, 1981, at the Arlington Park Race Track EXOP Center, Arlington Heights IL. Doors open at 8:00 am. Tickets are $2.00 in advance and $3.00 at the door. There will be 300 free flea market tables available, plus 100 commercial booths and clear paved parking. Prizes will be awarded. Talk-in on 146.94 and 146.01/.61. For advance tickets, send an SASE to WCRA, PO Box QSL, Wheaton IL 60187. For information, call (312)-766-1684 or (312)-629-3296.

MIAMI FL
FEB 7-8

The 21st annual Tropical Hamboree and 1981 ARRL Florida State Convention will be held on February 7-8, 1981, at the Flagler Dog Track, Miami FL. Registration is $3.00 in advance and $4.00 at the door. Swap tables are an additional $12.00 for both days, $7.00 for Saturday only, and $6.00 for Sunday only. Events will include tech talks and forums, over 100 exhibit booths, 400 swap tables, ladies' programs, group meetings, and many awards. There will be free overnight RV parking for self-contained units at the site (advance registration is recommended). Special gatherings are planned for QCWA/OOTC/SOWP and DXers. For further information and special hotel rates, write Dade Radio Club, PO Box 350045 Riverside Station, Miami FL 33135.

MANSFIELD OH
FEB 15

The Mansfield midwinter hamfest auction will be held on February 15, 1981, at the Richland County Fairgrounds, Mansfield OH. Doors will open to the public at 8:00 am. Tickets are $1.50 in advance and $2.00 at the door. Features will include prizes, an auction, and a flea market, all in a large heated building. Talk-in on 146.34/.94. For additional information, advance tickets, and/or tables, send an SASE to Harry Frietchen K8HF, 120 Homewood Road, Mansfield OH 44906, or phone (419)-529-2801.

LIVONIA MI
FEB 22

The Livonia Amateur Radio Club will hold its 11th annual LARC Swap 'n Shop on Sunday, February 22, 1981, from 8:00 am to 4:00 pm, at Churchill High School, Livonia MI. There will be plenty of tables available. Other features include door prizes, refreshments, and free parking. Talk-in on 146.52. For further information, send an SASBE (4" x 9") to Neil Coffin WA8GWL, c/o Livonia Amateur Radio Club, PO Box 2111, Livonia MI 48150.

DAVENPORT IA
MAR 1

The Davenport Radio Amateur Club will hold its tenth annual hamfest on March 1, 1981, from 8:00 am to 4:00 pm at the Davenport Masonic Temple, Highway 61 (Brady Street) and 7th Street, Davenport IA. Tickets are $2.00 in advance, $3.00 at the door. Tables are $4.00 each with a $2.00 additional charge for an electrical hookup (limited number). Features will include over $2,000 worth of major prizes. Hotel discounts and refreshments will be available. There will be a pre-hamfest Saturday night banquet with Paul Graver, midwest ARRL SCM, as guest speaker. Banquet tickets are $8.00 and reservations must be paid by February 18, 1981. Talk-in on 146.28/.88, W0BXR. For advance tickets, dinner, and table reservations, write Dave Johannsen WB0FBP, 2131 Myrtle, Davenport IA 52804.

STERLING IL
MAR 8

The Sterling-Rock Falls Amateur Radio Society will hold its 21st annual hamfest on Sunday, March 8, 1981, at the Sterling High School field house, 1608 4th Avenue, Sterling IL. Advance tickets are $2.00 and tickets at the door are $2.50. A large indoor flea market will be restricted to radio and electronic items only. Tables are available for $5.00 for commercial and $3.00 for others. Plenty of free parking will be available, including an area to accommodate campers and mobile trailers. Many prizes will be given away, including a first prize of a minicomputer. Doors open at 7:30 am. Featured will be a movie, "The World of Amateur Radio," to be shown throughout the day, bargains, good food, and plenty of close-by activities for XYLs and kids. Talk-in on .52 and WR9AER .25/.85. For advance tickets and tables, write Sue Peters KA9GNR, 511 8th Avenue, Sterling IL 61081. Make checks payable to Sterling-Rock Falls Amateur Radio Society and enclose an SASE.

CORRECTIONS

In "Single-Tone Paging for Wilson HTs," December, 1980, pp. 112-114, several errors managed to creep in, not the least of which was the author's old callsign. Fred's call *is* W4CK.

On page 112, zener D2 in Fig. 1 should be a 1N751A. This change should be reflected in the parts list on page 114, too. Also, on page 113, column 1, at the beginning of the bottom paragraph, the opening line should read "There is no *dis*advantage in. . ."

An improvement over the insulation technique described on page 114, column 2, lines 19 through 25, would be to use non-conducting styrofoam cut to the shape of the PCB.

Finally, at the bottom of the parts list, time and inflation have had their effect. Microsizer Co. (at the same address) now offers the kit for $17.95 and the PCB alone for $4.50.

Gene Smarte WB6TOV
News Editor

HAM HELP

I am in need of a Galaxy III schematic and owner's manual. I will pay for original or copy. Thank you.

Phillip R. Lofton WA4NVE
349 Quinn Rd.
Collierville TN 38017

I am in need of the manual(s) for two Gonset, Inc., FM 150-175-MHz radios. One is a model 960A, series (G40033), while the other lacks a model number but is stamped with the series (G40019). The two are identical but for power supplies and number of channels.

I would, of course, be willing to pay for any costs involved in obtaining the paperwork for these radios.

Zak Hargraves, KA0EGW
550 East 30th Street
Durango CO 81301

I came across a few schematics the other day and started to destroy them and then I thought that someone might want them.

I have schematics available for the following: HT-33-B linear amplifier, Globe DSB-100 Sidebander, Heathkit® V-2 VTVM, typical Command Set transmitter, with power-plug connections for "BC" series, modification of Heath HP-10 for use with Collins KWM series, and the popular Command Receiver.

These are free for the asking—an SASE would be appreciated, however.

Reid Martin W4BP
Rt. #3 Box 250
Tavares FL 32778

I need very badly a noise blanker for a Drake TR-4C. The unit Drake made for this rig was numbered 34-PNB. I would like to buy an original unit or obtain photocopies of printed information pertaining to it (schematics, photos, etc.). I will pay a reasonable price for either or both, and, of course, all shipping costs.

If you have a 34-PNB that you are willing to sell, or have information (or know where I can get either), please drop me a note at the address given below. Please state condition of unit, nature of information, and a price (please exclude shipping costs from this figure). Your time and attention is greatly appreciated.

Keith Inman, President
Bucknell Amateur Radio Club
Box C-281
Bucknell University
Lewisburg PA 17837

✓Reader Service—see page 194

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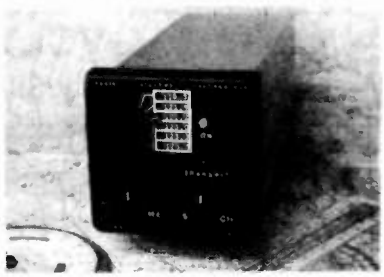

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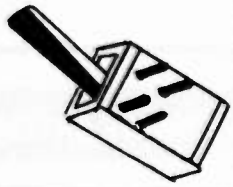

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2N3294	1.15	2N5944	8.92	MMT74	1.17
2N3301	1.04	2N5945	12.38	MMT2857	2.63
2N3302	1.05	2N5946	14.69	MRF245	33.30
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Manufacture & Model	Description	Price
AIL		
124A	200 to 2500MHZ Wide Range Power Oscillator	$ 300.00
390A-3	Microwave Diode Test Set	25.00
AILTECH		
473A	Swept RF Power Source 225 to 400MHZ	500.00
ALTO		
34A1	FM TV Receiver 220MHZ	200.00
B&K		
161	Transistor Tester	75.00
607	Tube Tester	100.00
Ballantine		
303-06	AC Voltmeter	100.00
355	Digital Voltmeter AC/DC	75.00
6130A	Time Mark Generator	350.00
Bell & Howell		
2970	Color Video TV Camera with Monitor	300.00
Bird		
67C	RF Wattmeter 0 to 2.5KW at 30 to 500MHZ	200.00
TS-118A/AP	RF Wattmeter 2 to 500W at 20 to 1400MHZ	150.00
CY-1764/UPM	RF Wattmeter	
Birtcher		
10-AC	Hybrid Parameter Plug In For Model 70	50.00
10-C	Transistor Leakage Plug In For Model 70	50.00
10-E	Test Plug In For Model 70	50.00
70	Transistor Test Set For Above Plug In,s	175.00
Boonton		
63M	Inductance Bridge	500.00
71AR	Capacitance Inductance Bridge	600.00
71D	Capacitance Inductance Refrence	200.00
74CS8	Capacitance Bridge	600.00
91CA	RF Voltmeter 300uV/3V at 10Hz/600MHZ	300.00
91H	RF Voltmeter 100uV/300V at 20Hz/1.2GHZ	350.00
95AR	DC Microvolt/Picoammeter 10uV/1000V , 1pA/1A	200.00
Boonton/Hewlett Packard		
190A	Q Meter 20 to 260MHZ	500.00
207H	Univerter 100KHZ to 55MHZ	100.00
230A	Power Amplifier 10 to 500MHZ 4.5watts	500.00
230B	Power Amplifier Later Version of 230A	900.00
240A	Sweep Generator 4.5 to 120MHZ	200.00
250A	R X Meter .5 to 500MHZ	1500.00
260A	Q Meter 50KHZ to 50MHZ	500.00
280A	Q Meter 200 to 600MHZ	500.00
Clevite Brush		
13/4214-00	Log Amplifier	75.00
Cohu		
204AR	Galvenometer	75.00
Chromally/Military		
ACR/TS-20	Radio Test Set	100.00
Dana		
5500/130	Digital Voltmeter	150.00
5740	Digital Voltmeter	150.00
5800	Digital Ratiometer/Multimeter	200.00
Dymec/Hewlett Packard		
2650A	Oscillator Synchronizer	100.00
Dynamic		
504	Multimeter DC Micromiltimeter	100.00
E.H.LAB		
120D	Pulse Generator 100HZ to 20MHZ	200.00
E.I.P.		
101A	Spectrum Analyzer Plug In and Power Supply 700MHZ to (15.4GHZ)	1500.00
Electronic Service		
710A	Crystal Impedance Meter	300.00
Empire/Singer		
NF105	Noise & Field Intensity Meter	400.00
TA/NF105	150KHZ to 30MHZ Mod.M126 For NF105	200.00
TX/NF105	14KHZ to 150KHZ Mod.M126 For NF105	200.00
T1/NF105	20MHZ to 200MHZ Mod.M126 For NF105	200.00
T2/NF105	200MHZ to 400MHZ Mod.M126 For NF105	200.00
T3/NF105	400MHZ to 1000MHZ Mod.M126 For NF105	200.00
TA/NF105	150KHZ to 30MHZ For NF105	200.00
T2/MM120	50MHZ to 1000MHZ	200.00
T2/NF112	2000MHZ to 4000MHZ For NF112	200.00
T3/NF112	3900MHZ to 7200MHZ For NF112	200.00
Fairchild		
74-03	Time Base Plug In For 700 Series Scopes	150.00
76-01A	Single Input Vertical Amplifier For 700 Series Scopes	75.00
757	Oscilloscope	200.00
FEL	Microwave Synchronizer	300.00

Reader Service—see page 194

F.L.Mosley/Hewlett Packard		
3S	X Y Recorder .5mv to 10v	225.00
60D	Logarithmic Converter	100.00
Fluke		
80E	High Voltage Divider	250.00
102	VAW Meter	150.00
710A	Impedance Meter Bridge	250.00
845AB	DC Null Detector/High Impedance Voltmeter	250.00
853A	Differential Meter	250.00
871A	DC Differential Voltmeter	250.00
General Microwave		
454AR	Microwave Power Meter	100.00
General Radio		
546C	Audio Frequency Microvolter	25.00
631D	Strobe	50.00
670F	Compensated Decade Resistor	50.00
740B	Capacitance Test Bridge	75.00
1203A	Power Supply	40.00
1203B	Power Supply	60.00
1208B	Oscillator 65 to 500MHZ	75.00
1211C	Oscillator .5 to 50MHZ	100.00
1212A	Null Detector	50.00
1214AS2	Unit Oscillator	50.00
1214D	Unit Oscillator	50.00
1215B	Unit Oscillator 50 to 250MHZ	100.00
1215C	Unit Oscillator 50 to 250MHZ	200.00
1216A	1F Amplifier	75.00
1217B	Unit Pulse Generator	50.00
1231P3	Tune Circuit	15.00
1269A	Power Supply	100.00
1363	Unit Oscillator 50 to 500MHZ	300.00
1382	Noise Generator	275.00
1390B	Noise Generator	200.00
1391B	Pulse,Sweep,Time Delay Generator With 1391P2 Power Supply	450.00
1604B	Comparison Bridge	125.00
1617A	Capacitance Bridge	500.00
1652A	Resistance Limmit Bridge	100.00
W50HM	Variac	200.00
Gertsch		
SB-4C-4R	Synchro Bridge	50.00
ST-100	Transformer	15.00
Heathkit		
IO-4560	Oscillscope	75.00
Hewlett Packard/F.L.Mosley		
2DR2	X Y Recorder .1 to 20v	350.00
Hewlett Packard		
AC-60K	Barretter Matching Transformer	15.00
196A	Scope Camera	200.00
214A	Pulse Generator 10HZ to 1MHZ	650.00
216A	Pulse Generator to 100MHZ	650.00
350D	Attenuator Set	100.00
354A	Attenuator	250.00
400DR	VTVM 10HZ to 4MHZ	50.00
403A	AC Transistor Voltmeter	150.00
410B	VTVM	125.00
411AR	RF Millivoltmeter	250.00
413AR	DC Null Voltmeter	100.00
415B	VSWR Meter	50.00
416A	Ratio Meter	100.00
417A	VHF Detector 10 to 500MHZ	125.00
425A	DC Microvolt/Ammeter	250.00
428A	Clip ON DC Ammeter	275.00
430C	Microwave Power Meter DC to 10GHZ 10mw.	100.00
431B	Microwave Power Meter 10MHZ to 40GHZ 10uw to 10mw	200.00
431C	Microwave Power Meter 10MHZ to 40GHZ 10uw to 10mw	350.00
434A	Caloimetric Power Meter DC to 12.4GHZ 10watts	450.00
457A	AC DC Converter	75.00
500BR	Frequency Meter	100.00
508A	Motor	25.00
1105A	Pulse Generator	50.00
1111A	AC Current Amplifier	75.00
1510A	Electromyograph Plug In	250.00
1752A	High Gain Vertical Plug In For 175A Scope	50.00
1780A	Auxiliary Plug In For 175A Scope	25.00
2470A	Amplifier	100.00
2772A	Power Supply	100.00
3301A	Auxiliary Plug In	25.00
3310A	Function Generator	500.00
3406A	Broadband Sampling Voltmeter 10KHZ to 1.2GHZ	750.00

Hewlett Packard		
3430A	Digital Voltmeter	150.00
3434A	Comparator	250.00
3441A	Range Selector For 3439A/ 3440A	75.00
3442A	Plug In For 3439A Automatic Range Selector & 3440A	50.00
3443A	High Gaun Auto Range Plug In For 3439A/3440A	200.00
3445A	AC DC Range Plug In For 3439A/3440A	175.00
3446A	AC DC Remote Plug In For 3439A/3440A	150.00
3450A	Digital Voltmeter	750.00
4260A	Universal Bridge	900.00
4910F	Open Fault Locator	250.00
5252A	Prescaler For 5245L/5246L to 350MHZ	250.00
5260A	Frequency Divider to 12.4 GHZ	1000.00
5327B	Timer Counter DVM to 512MHZ	1000.00
5383A	520MHZ Frequehcy Counter	300.00
5480A	with a 5486A and a 5485A , Memory Display, Control , and a Two Channel Input	3500.00
8005B	Pulse Generator	750.00
8007A	Pulse Generator	750.00
8402A	Calibrator For 431A and 431B	250.00
8601A	Generator/Sweeper	1200.00
8802A	Medium Gain Amplifier	100.00
10405	Vertical Response Tester	100.00
10407B	Plug In Extender	100.00
10411A	Horizontal Gain Calibrator	100.00
H03-353A	Attenuator Set	100.00
Hickok		
CA-4	Compactron Adapter For Tube Tester	150.00
DP100	DC Plug In	25.00
Hughes/Cobilt		
TCB-440/PE-100	Die Bonder (Like New)	1000.00
ITT/Standard Telephones and Cables Ltd.		
74834SG	Distortion Measuring Equipment	100.00
Kay		
110A	Mega Sweep	100.00
570A	Rada Pulse Sr. 10 to 80MHZ	100.00
990A	Utilator 4.5 to 220MHZ	100.00
Keithley		
200B	DC VTVM	50.00
250	Static Meter	300.00
416	Pico Ampmeter	100.00
600A	Electrometer	200.00
Keltec		
XR630-100	TWT Amplifier 8 to 12.4GHZ at 100watts 40dB Gain	5000.00
Krohn Hite		
310ABR	Band Pass Filter 20CPS to 200KC	100.00
350A	Ultra Low Frequency Rejection Filter .02HZ to 2KHZ	100.00
360AR	Rejection Filter 20CPS to 200KC	100.00
Leeds & Northrup		
Spectray 90	Temp. Detector	100.00
8686	Millivolt Potentiometer	250.00
Meguro		
MSG2282A	Signal Generator	500.00
Military		
AN/URM90	Impedance Bridge	150.00
SG-103/URM25F	H F Signal Generator 10KHZ to 50MHZ	250.00
ME180B/USM116B	RF Viltmeter Multimeter	100.00
TV-7DU	Tube Tester	125.00
Millivac		
828A	RF Microvoltmeter Solid State (NO PROBE)	100.00
Nelson Ross		
PSA-023	Spectrum Analyzer OKC to 500KC	300.00
PSA-034	Spectrum Analyzer 1KC to 2MHZ	300.00
NLS		
FM-7	Frequency Counter	100.00
MS-215	Scope	200.00
SC-5	Prescaler	150.00
North Atlantic		
RB-503C/S-1177	Ratio Box	75.00
VM-204	Phase Angle Voltmeter	100.00
Singer		
MF-5	Spectrum Analyzer with a UR-3 and a VR-4 1KHZ to 27.5MHZ	1200.00
Philco/Sierra		
470A-500	High Power Signal Generator 200 to 500MHZ 50watts	1100.00
Polarad		
SD-1	Multi Pulse Spectrum Analyzer	75.00
1001M4	Modulator	150.00

Reader Service—see page 194

Polarad		
1107	Signal Generator 3.8 to 8.2GHZ	$ 500.00
1108	Signal Generator 6.95 to 11GHZ	500.00
1108M4	Signal Generator 7 to 11GHZ	500.00
1206	Signal Generator 1.95 to 4.2GHZ	500.00
PRD		
680/X670	Calorimetric Power Meter with Dry Calorimeter 8.2 to 14.4 GHZ	300.00
Radio Ometer Copenhaggen		
SMG-1	Stereo Generator	500.00
Ramcor		
1200	Densiometer	250.00
RCA		
WV-98C	Senior Volt Ohmyst	75.00
RFL		
107A	Magnet Charger	500.00
541A	10KC to 1100KC Crystal Impedance Meter	400.00
541C	2.5KC to 1100KC Crystal Impedance Meter	500.00
942A-8/HB7778	Magnet Charger with Transformer	1000.00
Rohde & Schwarz		
KRT	Capacitance Meter	500.00
SLRD	UHF Power Signal Generator 275 to 2750MHZ 20watts	1000.00
Sencor		
CA122B	Color Circuit Analyzer	200.00
Siemens		
3D3325	Selective Voltmeter	250.00
Spectra		
UBD 1/2°	Photo Research Spotmeter	1500.00
Stoddart		
NM-10A	RFI Meter 10 to 250KHZ	200.00
NM-40A	RFI Meter 30HZ to 15KHZ	300.00
Teca Corp		
CH-3	Variable Pulse Generator & Chronavie Meter	150.00
Tele Signal Corp		
320	Test & Meter Unit	100.00
Telonic		
SM2000	Sweeper	300.00
Tektronix		
B	Wideband High Gain Plug In	35.00
CA	Dual Trace Plug In	100.00
D	High Gain Differential	25.00
H	Wideband High Gain DC	50.00
K	Fast Rise DC	35.00
M	Four Trace	200.00
N	Sampling	200.00
Q	Transducer & Strain Gage	200.00
R	Transistor Risetime	75.00
TU-2	Test Load	35.00
W	High Gain Differential Comparator	100.00
1A2	Dual Trace	200.00
1A5	Differential Comparator Amplifier	250.00
1S1	Sampling Unit with 350ps Risetime DC to 1GHZ	300.00
2A61	AC Differential	75.00
2A63	Differential	75.00
2B67	Time Base Single Sweep	200.00
3A75	Wideband DC	75.00
3S3	Dual Trace Sampling DC to 1GHZ	250.00
3S76	Dual Trace Samplins DC to 875MHZ	200.00
3T4	Programmable Sampling Sweep	300.00
3T77	Sampling Sweep	200.00
3T77A	Sampling Sweep	250.00
4S1/4S2/4S3/5T1/661	Sampling Scope with Dual Trace Sampling Units (3) and Timing Unit.	1000.00
7A15AN-11	Vertical Amplifier DC to 80MHZ	450.00
10A1	Differential Amplifier	250.00
10A2A	Dual Trace	250.00
RM15	Oscilloscope Same as 515 15MHZ	200.00
RM31A	Oscilloscope Same as 531A with Dual Trace Plug In 15MHZ	300.00
RM35A	Oscilloscope Same as 535A with Dual Trace Plug In 15MHZ	300.00
RM41A	Oscilloscope Same as 541A with Dual Trace Plug In 30MHZ	350.00
50	Amplifier	50.00
51	Sweep	50.00
53A	Wideband DC Plug In	20.00
53B	Wideband High Gain	25.00
53/54B	Wideband High Gain	30.00
53/54C	Dual Trace	75.00
53/54D	High Gain Differential	20.00
53/54K	Fast Rise DC	45.00
63	Differential	65.00
81	Plug In Adapter For 581/A & 585/A	65.00

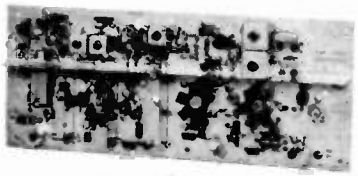
TEKTRONIX		
81A	Adapter For 581/A & 585/A	$ 90.00
84	Test Unit	75.00
107	Square Wave Generator	50.00
RM122	Preamplifier	50.00
123	AC Coupled Preamplifier	20.00
131	Current Probe Amplifier	75.00
240	Control Unit	150.00
280	Trigger Countdown Unit	75.00
RM503	Oscilloscope 450KHZ	200.00
535	Oscilloscope with Dual Trace Plug In 15MHZ	325.00
535A	Oscilloscope with Dual Trace Plug In 15MHZ	375.00
543	Oscilloscope with Dual Trace Plug In 33MHZ	350.00
543A	Oscilloscope with Dual Trace Plug In 33MHZ	400.00
545A	Oscilloscope with Dual Trace Plug In 3DMHZ	450.DO
555	Dual Beam Oscilloscope with Dual Trace Plug In 33MHZ	500.00
561	Oscilloscope 1DMHZ	100.00
RM561	Oscilloscope 10MHZ Same as 561	100.00
RM561A	Oscilloscope 10MHZ Same as 561A	175.00
561B	Oscilloscope 10MHZ	250.00
564	Split Screen Storage Oscilloscope	45D.DO
RM565	Oscilloscope Same as 565 Dual Beam 10MHZ	650.00
581	Oscilloscope with 81 Adapter and Dual Trace Plug In	550.00
601	Storage Display	250.00
611	Storage Display	1000.DO
1791	NC Program Verfier	1500.00
067-0513-00	Calibration Fixture	100.00
067-0591-00	Calibration Fixture	100.00
067-508	Calibration Fixture	100.00
TIC		
T-10A	DME Pulse Generator	200.00
T-10M	DME Speed Indicator Adapter	200.00
Teradyne		
ACT1	Analogical Circuit Tester with Boards	500.00
Texscan		
HS-85	Sweep Generator 400 to 1000MHZ	250.00
VS-73	Sweep Generator 400 to 450MHZ	100.00
Theta		
SSB-11E	System Error Bridge	75.00
Wandel u Goltermann		
LDE2 & LDS2	Measurins Set For Group Delay Attenuation and Receiver and Attenuation Generator	Make Offer
Weinschel Eng.		
BA5	Attenuation Calibrator	100.00
675	Thermistor Mount	100.00
935N	Thermistor Mount	10D.00
Western Reserve		
RFI RF-204U	RFI Receiver	200.00
Wiltron		
321/322/326/327/640G50	Phase & Amplitude Indicator with Local Oscillator 2.5 to 100MHZ , Time Delay Unit , High Resolution Time Delay Unit , Modulation Unit	750.00
640G50	Sweep Generator to 500MHZ	750.00
LATE ADD ON,s		
Textron		
N160	X Y Recorder	200.00

All Prices Are In US Dollars.
All Equipment Shipped Airfreight or UPS FOB Phoenix , Arizona
All Equipment Working Unless Other Wise Stated.60 Day Warranty On All Equipment.
We Do Not Take P.O.,s Unless COD , or Check With Order.
Manuals Not Included But Some In Stock At A Small Charge.

These Low Cost SSB TRANSMITTING CONVERTERS

Let you use inexpensive recycled 10M or 2M SSB exciters on UHF & VHF!

- Linear Converters for SSB, CW, FM, etc.
- A fraction of the price of other units; no need to spend $300 – $400!
- Use with any exciter; works with input levels as low as 1 mW.
- Use low power tap on exciter or simple resistor attenuator pad (instructions included).
- Link osc with RX converter for transceive.



XV4 UHF KIT — ONLY $99.95

28-30 MHz in, 435-437 MHz out; 1W p.e.p. on ssb, up to 1½W on CW or FM. Has second oscillator for other ranges. Atten. supplied for 1 to 500 mW input, use external attenuator for higher levels.

Extra crystal for 432-434 MHz range $5.95
XV4 Wired and tested $149.95

XV2 VHF KIT - ONLY $69.95

2W p.e.p. output with as little as 1mW input. Use simple external attenuator. Many freq. ranges available.

MODEL	INPUT (MHz)	OUTPUT (MHz)
XV2-1	28-30	50-52
XV2-2	28-30	220-222
XV2-4	28-30	144-146
XV2-5	28-29 (27-27.4 CB)	145-146 (144-144.4)
XV2-7	144-146	50-52

XV2 Wired and tested $109.95

XV28 2M ADAPTER KIT - $24.95

Converts any 2M exciter to provide the 10M signal required to drive above 220 or 435 MHz units.

NEW! COMPLETE TRANSMITTING CONVERTER AND PA IN ATTRACTIVE CABINET

Far less than the cost of many 10W units!

Now, the popular Hamtronics® Transmitting Converters and heavy duty Linear Power Amplifiers are available as complete units in attractive, shielded cabinets with BNC receptacles for exciter and antenna connections. Perfect setup for versatile terrestial and OSCAR operations! Just right for phase 3! You save $30 when you buy complete unit with cabinet under cost of individual items. Run 40-45 Watts on VHF or 30-40 Watts on UHF with one integrated unit! Call for more details.

MODEL	KIT	WIRED and TESTED
XV2/LPA2-45/Cabt (6M or 2M)	$199.95	$299.95
XV4/LPA4-30/Cabt (for UHF)	$229.95	$349.95

Easy to Build FET RECEIVING CONVERTERS

Let you receive OSCAR and other exciting VHF and UHF signals on your present HF or 2M receiver

- NEW LOW-NOISE DESIGN
- ATTRACTIVE WOODGRAIN CASE
- Less than 2dB noise figure, 20dB gain

MODEL	RF RANGE	OUTPUT RANGE
CA28	28-32 MHz	144-148 MHz
CA50	50-52	28-30
CA50-2	50-54	144-148
CA144	144-146	28-30
CA145	145-147–or–144-144.4	28-30 27-27.4 (CB)
CA146	146-148	28-30
CA220	220-222	28-30
CA220-2	220-224	144-148
CA110	Any 2MHz of Aircraft Band	26-28 or 28-30
CA432-2	432-434	28-30
CA432-5	435-437	28-30
CA432-4	432-436	144-148

Easily modified for other rf and if ranges.

STYLE	VHF	UHF
Kit less case	$34.95	$49.95
Kit with case	$39.95	$54.95
Wired/Tested in case	$54.95	$64.95

Professional Quality VHF/UHF FM/CW EXCITERS

- Fully shielded designs
- Double tuned circuits for spurious suppression
- Easy to align with built-in test aids

T50-50	6-chan, 6M, 2W Kit	$44.95
T50-150	6-chan, 2M, 2W Kit	$44.95
T50-220	6-chan, 220 MHz, 2W Kit	$44.95
T450	1-chan, 450 MHz, ¾W Kit	$44.95

See our Complete Line of VHF & UHF Linear PA's

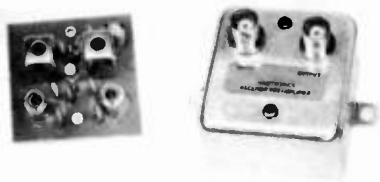
- Use as linear or class C PA
- For use with SSB Xmtg Converters, FM Exciters, etc.

LPA2-15	6M, 2M, 220; 15 to 20W	$59.95
LPA2-30	6M, 2m; 25 to 30W	$89.95
LPA2-40	220 MHz; 30 to 40W	$119.95
LPA2-45	6M, 2M; 40 to 45W	$119.95
LPA4-10	430MHz; 10 to 14W	$79.95
LPA4-30	430MHz; 30-40W	$119.95

See catalog for complete specifications

FAMOUS HAMTRONICS PREAMPS

Let you hear the weak ones too!
Great for OSCAR, SSB, FM, ATV. Over 14,000 in use throughout the world on all types of receivers.



- NEW LOW-NOISE DESIGN
- Less than 2 dB noise figure, 20 dB gain
- Case only 2 inches square
- Specify operating frequency when ordering

MODEL P-30 VHF PREAMP, available in many versions to cover bands 18-300 MHz.

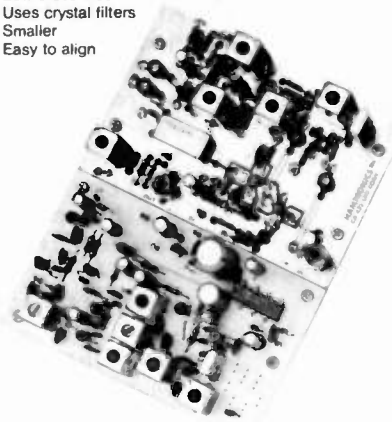
MODEL P432 UHF PREAMP, available in versions to cover bands 300-650 MHz.

STYLE	VHF	UHF
Kit less case	$12.95	$18.95
Kit with case	$18.95	$26.95
Wired/Tested in Case	$27.95	$32.95

NEW VHF/UHF FM RCVRS

Offer Unprecedented Range of Selectivity Options

- New generation
- More sensitive
- More selective
- Low cross mod
- Uses crystal filters
- Smaller
- Easy to align



R75A* VHF Kit for monitor or weather sattelite service. Uses wide L-C filter. -60dB at ± 30 kHz. $69.95

R75B* VHF Kit for normal nbfm service. Equivalent to most transceivers. -60dB at ± 17 kHz, -80dB at ± 25 kHz... $74.95

R75C* VHF Kit for repeater service or high rf density area. -60dB at ±14kHz, -80dB ±22kHz, -100dB ±30kHz.... $84.95

R75D* VHF Kit for split channel operation or repeater in high density area. Uses 8-pole crystal filter. -60dB at ±9 kHz, -100dB at ± 15 kHz. The ultimate receiver!... $99.95

* Specify band: 10M, 6M, 2M, or 220 MHz. May also be used for adjacent commercial bands. Use 2M version for 137 MHz WX satellites.

R450( ) UHF FM Receiver Kits, similar to R75, but for UHF band. New low-noise front end. Add $10 to above prices. (Add selectivity letter to model number as on R75.)

A14 5 Channel Adapter for Receivers. $9.95

NEW R110 VHF AM RCVR

AM monitor receiver kit similar to R75A, but AM. Available for 10-11M, 6M, 2M, 220 MHz, and 110-130 MHz aircraft band $74.95. (Also available in UHF version.)

IT'S EASY TO ORDER!

- Write or phone 716-392-9430
(Electronic answering service evenings & weekends)
- Use Credit Card, UPS COD, Check, Money Order
- Add $2.00 shipping & handling per order

✓33

Call or Write to get
FREE CATALOG
With Complete Details
(Send 4 IRC's for overseas mailing)

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✓ Reader Service—see page 194

SEMICONDUCTORS SURPLUS

2822 North 32nd Street, #1 • Phoenix, Arizona 85008 • Phone 602-956-9423

MEMORY

	Description	Price
2708	1K x 8 Eprom	$ 5.00
2716/2516	2K x 8 5V single supply	9.99
2114/9114	1K x 4 Static	5.00
4027	4K x 1 Dynamic Ram	2.99
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CRYSTAL FILTERS
TYCO 001-19880 Same as 2194F
10.7 MHz narrow band
3 dB bandwidth 15 KHz min.
20 dB bandwidth 60 KHz min.
40 dB bandwidth 150 KHz min.
Ultimate 50 dB insertion loss 1 dB max.
Ripple 1 dB max. Ct. 0+/-5 pf 3600 Ohms
$3.99 each

MRF454, same as MRF458 12.5 VDC, 3-30 MHz
80 Watts output, 12 dB gain $17.95 each

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MRF472
12.5 VDC, 27 MHz
4 Watts output, 10 dB gain
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for PCB Boards
5 mix for $5.00

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SFD 455D	455 KHz	$2.00
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YOUR CHOICE $12.99 each

J310 N-CHANNEL J-FET 450 MHz
Good for VHF/UHF Amplifier, Oscillator and Mixers 3/$1.00

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26 VDC Coil SPDT #360-11892-13
100 Watts Good up to 18 GHz
$19.99 each

78M05 Same as 7805 but only ½ Amp @ 5 VDC 49¢ each or 10/$3.00

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39¢ each or 10/$3.00

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230 VAC @ .78 Amps
Will also work on 115 VAC
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NEW & USED BCD SWITCHES
3 switch with end plates
New $8.99
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Minimum shipping by UPS is $2.35 with insurance. Please allow extra shipping charges for heavy or long items.

All parts returned due to customer error will be subject to a 15% restock charge.

If we are out of an item ordered, we will try to replace it with an equal or better part unless you specify not to, or we will back order the item, or refund your money.

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Red	6/$1.00
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NEW G.E. OPTO COUPLERS 4N26
69¢ each or 10/$5.00

MICRO-MINI WATCH CRYSTALS
32.768 Hz $3.00 each

NEW 2 inch ROUND SPEAKERS
100 Ohm coil 99¢ each

PLASTIC TO-3 SOCKETS 4/$1.00

NO ORDERS UNDER $10

INTRODUCING SONY'S NEW DIGITAL DIRECT ACCESS RECEIVER!

A Whole New Breed Of Radio

Innovative design. Advanced technology. Digital key-touch tuning. The ICF-2001. It's a whole new breed of radio. A receiver that supplants the conventional multi-band concept, receiving a wide amplitude-modulated frequency range–shortwave, mediumwave and most longwave broadcasts. Plus FM, SSB and CW. Even more important, the 2001 replaces the ordinary tuning knob and dial with a direct-access tuning keyboard and a Liquid Crystal Display (LCD) for digital frequency readout. Which make the unit as easy to use as a pocket calculator. Instant, direct-access tuning modes and six memory-station presets assure maximum ease of use. And the quartz-crystal, frequency-synthesized circuitry behind them assures outstanding reception. Reception of local broadcasts and exciting news, music, sports, entertainment and information from around the world. You'll get the inside, local news stories from foreign countries ... exclusive coverage of world sports events ... plus everything from informal "ham" to marine communications. All at your fingertips.

Key-Touch Tuning

To tune a station manually, you simply punch in the station frequency numerals on the direct-access, digital tuning keyboard. Press the "Execute" key and the command is entered, the station is received and LCD readout confirms tuning. If you punch in an incorrect frequency by mistake, the ICF-2001 tells you to "Try Again" by flashing those words on the display. The instant, fingertip tuning provides total accuracy and convenience. And the LCD digital frequency display confirms the exact, drift-free signal reception.

Automatic Scanning

In auto-scan mode, the tuner can be set for continuous scanning of a given frequency range, which you set by means of upper and lower limit keys designated "L_1" and "L_2." You may want to scan an entire frequency range. For instance, the 76 to 108 MHz FM spectrum. If you want scanning to stop at any strong signal–one that reads "4" or "5" on the LED signal-strength indicator– switch on "Scan Auto Stop." For continuous scanning, leave the switch off, and just press the "Start/Stop" key to listen to a station or resume scanning.

Manual Tuning

Like the auto-scanning mode, manual tuning is useful for quick signal searching when you don't know particular station frequencies within a given range. You simply press the "Up" or "Down" key, and the tuner does the searching for you. And if you press the "Fast" key at the same time, the scanning rate increases for especially rapid station location. When you hear a broadcast you want to receive, just release the keys for instant reception, presssing the "Up" or "Down" key again if necessary for exact tuning.

Memory Presets

After you've tuned a station using punch-in, key-touch tuning or either scanning mode, you can enter it in the 2001's memory for instant, one-touch preset reception. Which means no retuning hard-to-find foreign broadcasts. Plus instant access to your favorite local stations for music and news. Six preset buttons allow up to six stations–in any wave range–to be memorized. And there's LCD digital readout of the memory buttons being used on each band. What's more, the upper and lower limit keys can be used as memory presets when they're not being used for scanning, allowing a total of eight frequencies to be memorized for instant, one-touch reception.

Frequency Synthesis

The 2001's direct-access tuning and outstanding reception quality are made possible by the unit's all-band quartz-crystal, PLL frequency synthesis. Instead of the conventional analog tuning system, with its variable tuning capacitor, the 2001 incorporates an LSI and a quartz-crystal reference oscillator. Which means that the local-oscillator frequencies used in superheterodyning are locked to the "synthesized" quartz reference frequencies. The result is the utmost in tuning stability, without a trace of tuning drift. In addition, dual-conversion superheterodyning for AM assures exceptionally clean, clear reception across the entire 150-to-29,999kHz spectrum.

Features

- FM/AM/SSB/CW/wide spectrum coverage
- Dual-conversion superheterodyne circuitry of AM assures high sensitivity and interference rejection
- Quartz-crystal, phase-locked-loop frequency synthesis for all bands assures the utmost tuning stability, without a trace of tuning drift
- Direct-access, digital tuning keyboard and LCD digital frequency readout for quick, key-touch station selection–maximum accuracy and ease of use
- Manual tuning and automatic scanning for effortless signal searching, easy DXing
- 6-station presets, plus 2 auxiliary presets, for instant reception of memorized stations on any band–plus LCD memory indication.
- 5-step LED signal-strength indicator
- Local/Normal/DX sensitivity selector for AM
- SSB/CW compensator for low-distortion reception
- Telescopic antenna, plus external antenna included
- 4" speaker for full, rich sound
- Slide-bar bass and treble controls
- Sleep timer–with LCD readout–can be set in 10-minute increments for up to 90 minutes of play before automatic radio shut-off

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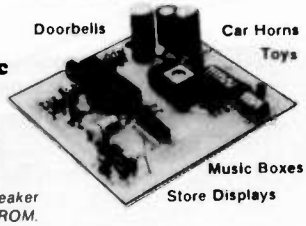


New! **The Super Music Maker**
REVISION 2
$24.95
(Basic Kit)
Does not include speaker switches or 2708 ROM.

Now you can play hundreds of songs using the Bullet Super Music Maker. The unit features a single factory programmed microprocessor IC that comes with 20 pre-programmed short tunes. By adding the additional PROMS (2708's) the system can be expanded to play up to 1000 notes per PROM. Just think . . . a compact electronic instrument that will play dozens, hundreds or even thousands of selections of music. The kit comes with all electronic components (less the PROM), and a drilled, plated and screened PC Board which measures 4" x 4¾". The 7 watt amplifier section is on the same PC board and drives an 8 ohm speaker (not included), from a whisper to ear splitting volume. Since the unit works on 12 VDC or 12 VAC*, vehicle or portable operation is possible. What do you get for $24.95? Everything but a speaker, transformer, case, switches, and PROM. Additional 2708 albums containing popular tunes are available for $15.00 each or you can program your own PROMS using information provided with the kit instructions. Lists of available PROM albums are available on request. *(Note: Unit plays electronic music one note at a time, It is not possible to play chords or a melody with harmony simultaneously.)*

- ★ Envelope control gives decay to notes.
- ★ "Next tune" feature allows sequential playing of all songs.
- ★ On board inverter allows single voltage (+12) operation.

OPTIONAL ACCESSORIES

DIP Switches One 8 pos., One 5 pos. **2.00/Set**
(Can be directly soldered to PC Bd. to access tunes)

Rotary Switches Two 5 position **2.00/Set**
(For remote wiring to PC Bd. to access tunes)

Attractive Black Plastic Case **6.50**

Wallplug Transformer **3.00**
(For operation on 117VAC house voltage)

Super Value Power Transformer

Well made, open frame transformer with mounting ears. Build a +5 and ±12 supply with inexpensive parts. Free schematics of several designs. Primary 117VAC. SEC #1 15VAC @ .5A SEC #2 15 VAC @ .5A SEC #3 8VAC @ 2.5A. **$2.95**

ORDER: BET-0005

7 Watt Audio Amp Kit $5.95

SMALL, SINGLE, HYBRID IC AND COMPONENTS FIT ON A 2" x 3" PC BOARD (INCLUDED). RUNS ON 12 VDC. GREAT FOR ANY PROJECT THAT NEEDS AN INEXPENSIVE AMP. LESS THAN 3% THD @ 5 WATTS. COMPATIBLE WITH SE-01 SOUND KIT.

Overvoltage Protection Kit $6.95

Protect your expensive equipment from overvoltage conditions. Every computer should have one! Works with any fused DC power source from 10 to 20 volts up to 25 amps.

AY3-8910 PROGRAMMABLE SOUND GENERATOR

The AY3-8910 is a 40 pin LSI chip with three oscillators, three amplitude controls, programmable noise generator, three mixers, an envelope generator, and three D/A converters that are controlled by 8 BIT WORDS. No external pots or caps required. This chip hooked to an 8 bit microprocessor chip or Buss (8080, Z80, 6800 etc.) can be software controlled to produce almost any sound. It will play three note chords, make bangs, whistles, sirens, gunshots, explosions, bleets, whines, or grunts. In addition, it has provisions to control its own memory chips with two IO ports. The chip requires +5V @ 75ma and a standard TTL clock oscillator. A truly incredible circuit.

12.95 W/Basic Spec Sheet (4 pages)
60 page manual with S-100 interface instructions and several programming examples, **$3.00 extra**

ZULU II CLOCK KIT X-RATED!

WITH CALENDAR AND NOX™ CIRCUIT

X-TRA VALUE: All the components and high quality plated G-10 PC Boards are provided.
X-TRA CARE IN DESIGN: Easy Assembly! Large open layout.
X-CELLENCE IN IDEAS: 5 years of designed products for the amateur radio market.
X-CELLENCE IN INSTRUCTIONS: Clear step-by-step instructions with quality illustrations and schematic.
X-TRA FEATURES: There has never been a clock kit with so many features — at any price!

- Unit operates on either **12 VAC** or **12 VDC**.
- On board **QUARTZ XTAL TIMEBASE** or 60Hz AC line freq. can be used.
- Automatic **BATTERY BACKUP***
- Reads true **24 HOUR TIME** and **31 DAY CALENDAR**.
- **Unique NOX™ CIRCUIT activates readouts with a handclap followed by the date for 4 seconds. Or they can be turned on constantly.**
- When used mobile readouts blank whe ignition is off.
- Special **NOISE SUPPRESSION** and battery reversal circuits.
- Bright 1/2" LED's show hours, minute and seconds.

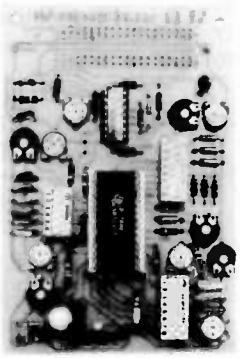
19.95
LESS CASE

ACCESSORIES

Custom High Impact Molded Case with Ruby Lens. Available in Blue or Tan.
$6.50

117 VAC to 12 VAC Transformer.
$1.35

*9V Battery Not Included



Sound Effects Kit 18.50

The **SE-01 Sound Effects Kit** is a complete kit, all you need to build a programmable sound effects machine except a battery and speaker. Our kit is designed to really ring out the **TI 76477** Sound Chip. Only the SE-01 provides you with additional circuitry that includes a **PULSE GENERATOR, MUX OSCILLATOR and COMPARITOR** to make more complex sounds a snap. We help you in building the kit with a clear, easy-to-follow construction manual and we show you how to easily program the unit. Other dealers will sell you the chip or a "kit" of parts but you are on your own to do the most difficult part...make neat sounds! Within a short time after you build the SE-01 you can easily create **Gunshots, Explosions, Space Sounds, Steam Trains** and much more. We think the Bullet SE-01 is the best deal on the market but don't ask us. — ask the **15,000** happy SE-01 owners!

Complete Kit With Quality Plated PC Board **$18.50**
(Less battery & speaker)

AUTO/VAN CLOCK KIT 16.95

- 12 Hr. Format
- 6 Digit ½" LED Readouts
- Quartz XTAL Timebase
- Alarm & Snooze Options
- Noise Filtering
- Easy Assembly • 12 VDC
- 4 5/8" x 3" x 1 1/2"
- All Parts!

ULTRASONIC RELAY KIT

Invisible Beam Works Like A Photo Electric Eye. **COMPLETE KIT**. All Parts & PC Board. Use Up To 25 Ft. Apart.
$21.50

Optional entry delay and Alarm Timeout Circuit will source or sink up to 200 MA DC.
$3.95

PARTS

LM3046	(CA3046) Xistor Array	.75
RCA 40430	400V 6A TRIAC TO-66	.75
LM567	Tone Decoder	.99
CD4046	PLL CMOS	.99
LM3302	Quad Comparator	.89
2SC 1849	High Freq. NPN TO-92	6/1.00
MPS A 20	NPN General Purpose	8/1.00
TL490	Bar/Graph Driver w/specs	2.50
7812	12V 1A Regulator	.99
7805	5V 1A Regulator	.99
78M05	5V ½A Reg. TO-5 (Hse #)	.60
LM3911	Temp. Transducer w/specs	1.10
555	Timer IC	.49
2N6028	P.U.T. w/specs	.50
IL-1	Opto Isolator w/specs	.60
LM380	2W Audio IC w/specs	.50
LM377	Dual LM380 w/specs	1.09
TIP-30	PNP Power TO-220	3/1.00
SCR	Sensitive Gate 200V 4A	7/1.00
SCR	Sensitive Gate 600V 4A RCA	3/1.00
GE ST-2 DIAC	Trigger diode for triacs in AC phase control operation	.29

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Perfect for power transistors, or 309 and 340K series voltage regulators.

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THE PERFECT TRANSFORMER

117VAC primary. 12VAC secondary @ 200ma Great for all your CMOS, or low power TTL projects. PC board mount. *ORDER:*
99¢ ea. 3/$2.50 *XFMR 03*
Size: 1.5" W x 1.25" D x 1.25" H

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Most popular transistor for power supplies, audio amps, switching, etc.
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9 DIGITS 600 MHz $129.95 WIRED

PRICES
CT-90 wired, 1 year warranty $129.95
CT-90 Kit, 90 day parts warranty 109.95
AC-1 AC adapter 3.95
BP-1 Nicad pack - AC Adapter/Charger 12.95
OV-1, Micro-power Oven time base 49.95
External time base input 14.95

The CT-90 is the most versatile, feature packed counter available for less than $300.00! Advanced design features include; three selectable gate times, nine digits, gate indicator and a unique display hold function which holds the displayed count after the input signal is removed! Also, a 10mHz TCXO time base is used which enables easy zero beat callbration checks against WWV. Optionally; an internal nicad battery pack, external time base input and Micro-power high stability crystal oven time base are available. The CT-90, performance you can count on!

SPECIFICATIONS:

Range:	20 Hz to 600 MHz
Sensitivity:	Less than 10 MV to 150 MHz Less than 50 MV to 500 MHz
Resolution:	0.1 Hz (10 MHz range) 1.0 Hz (60 MHz range) 10.0 Hz (600 MHz range)
Display:	9 digits 0.4" LED
Time base:	Standard-10.000 mHz, 1.0 ppm 20-40°C Optional Micro-power oven-0.1 ppm 20-40°C
Power:	8-15 VAC @ 250 ma

7 DIGITS 525 MHz $99.95 WIRED

SPECIFICATIONS:

Range:	20 Hz to 525 MHz
Sensitivity:	Less than 50 MV to 150 MHz Less than 150 MV to 500 MHz
Resolution:	1.0 Hz (5 MHz range) 10.0 Hz (50 MHz range) 100.0 Hz (500 MHz range)
Display:	7 digits 0.4" LED
Time base:	1.0 ppm TCXO 20-40°C
Power:	12 VAC @ 250 ma

The CT-70 breaks the price barrier on lab quality frequency counters. Deluxe features such as: three frequency ranges - each with pre-amplification, dual selectable gate times, and gate activity indication make measurements a snap. The wide frequency range enables you to accurately measure signals from audio thru UHF with 1.0 ppm accuracy - that's .0001%! The CT-70 is the answer to all your measurement needs, in the field, lab or ham shack.

PRICES:

CT-70 wired, 1 year warranty	$99.95
CT-70 Kit, 90 day parts warranty	84.95
AC-1 AC adapter	3.95
BP-1 Nicad pack + AC adapter/charger	12.95

7 DIGITS 500 MHz $79.95 WIRED

PRICES:

MINI-100 wired, 1 year warranty	$79.95
MINI-100 Kit, 90 day part warranty	59.95
AC-Z Ac adapter for MINI-100	3.95
BP-Z Nicad pack and AC adapter/charger	12.95

Here's a handy, general purpose counter that provides most counter functions at an unbelievable price. The MINI-100 doesn't have the full frequency range or input impedance qualities found in higher price units, but for basic RF signal measurements, it can't be beat! Accurate measurements can be made from 1 MHz all the way up to 500 MHz with excellent sensitivity throughout the range, and the two gate times let you select the resolution desired. Add the nicad pack option and the MINI-100 makes an ideal addition to your tool box for "in-the-field" frequency checks and repairs.

SPECIFICATIONS:

Range:	1 MHz to 500 MHz
Sensitivity:	Less than 25 MV
Resolution:	100 Hz (slow gate) 1.0 KHz (fast gate)
Display:	7 digits, 0.4" LED
Time base:	2.0 ppm 20-40°C
Power:	5 VDC @ 200 ma

8 DIGITS 600 MHz $159.95 WIRED

NEW READ RECEIVER FREQUENCY

SPECIFICATIONS:

Range:	20 Hz to 600 MHz
Sensitivity:	Less than 25 mv to 150 MHz Less than 150 mv to 600 MHz
Resolution:	1.0 Hz (60 MHz range) 10.0 Hz (600 MHz range)
Display:	8 digits 0.4" LED
Time base:	2.0 ppm 20-40°C
Power:	110 VAC or 12 VDC

The CT-50 is a versatile lab bench counter that will measure up to 600 MHz with 8 digit precision. And, one of its best features is the Receive Frequency Adapter, which turns the CT-50 into a digital readout for any receiver. The adapter is easily programmed for any receiver and a simple connection to the receiver's VFO is all that is required for use. Adding the receiver adapter in no way limits the operation of the CT-50, the adapter can be conveniently switched on or off. The CT-50, a counter that can work double-duty!

PRICES:

CT-50 wired, 1 year warranty	$159.95
CT-50 Kit, 90 day parts warranty	119.95
RA-1, receiver adapter kit	14.95
RA-1 wired and pre-programmed (send copy of receiver schematic)	29.95

DIGITAL MULTIMETER $99.95 WIRED

PRICES:

DM-700 wired, 1 year warranty	$99.95
DM-700 Kit, 90 day parts warranty	79.95
AC-1, AC adaptor	3.95
BP-3, Nicad pack +AC adapter/charger	19.95
MP-1, Probe kit	2.95

The DM-700 offers professional quality performance at a hobbyist price. Features include; 26 different ranges and 5 functions, all arranged in a convenient, easy to use format. Measurements are displayed on a large 3½ digit, ½ inch LED readout with automatic decimal placement, automatic polarity, overrange indication and overload protection up to 1250 volts on all ranges, making it virtually goof-proof! The DM-700 looks great, a handsome, jet black, rugged ABS case with convenient retractable tilt bail makes it an ideal addition to any shop.

SPECIFICATIONS:

DC/AC volts:	100uV to 1 KV, 5 ranges
DC/AC current	0.1 uA to 2.0 Amps, 5 ranges
Resistance:	0.1 ohms to 20 Megohms, 6 ranges
Input impedance:	10 Megohms, DC/AC volts
Accuracy:	0.1% basic DC volts
Power:	4 'C' cells

AUDIO SCALER

For high resolution audio measurements, multiplies UP in frequency.

- Great for PL tones
- Multiplies by 10 or 100
- 0.01 Hz resolution!

$29.95 Kit $39.95 Wired

ACCESSORIES

Telescopic whip antenna - BNC plug	$ 7.95
High impedance probe, light loading	15.95
Low pass probe, for audio measurements	15.95
Direct probe, general purpose usage	12.95
Tilt bail, for CT 70, 90, MINI-100	3.95
Color burst calibration unit, calibrates counter against color TV signal	14.95

COUNTER PREAMP

For measuring extremely weak signals from 10 to 1,000 MHz. Small size, powered by plug transformer-included.

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✓ Reader Service—see page 194

Save on Scanners!
NEW Rebates!

Communications Electronics,™ the world's largest distributor of radio scanners, celebrates Christmas early with big savings on *Bearcat* synthesized scanners. Electra Company, the manufacturers of *Bearcat* brand scanners is offering consumer rebates on their fantastic line of crystalless scanners purchased between September 15 and November 15, 1980.

We give you excellent service because CE distributes more scanners worldwide than *anyone* else. Our warehouse facilities are equipped to process thousands of scanner orders every week. We also export scanners to over 300 countries and military installations. Most items are **in stock** for **quick shipment**. Do your Christmas scanner shopping early and **order today** from CE!

Bearcat®† 300

The Ultimate Synthesized Scanner!
List price $519.95/**CE price $329.00/$20.00 rebate**
Your final cost is a low $309.00
4-Band, 50 Channel • Service Search • No-crystal scanner • AM Aircraft and Public Service bands. • Priority Channel • AC/DC
Bands: 32-50, 118-136 AM, 144-174, 421-512 MHz.
The new *Bearcat* 300 is the most advanced automatic scanning radio that has ever been offered to the public. The *Bearcat* 300 uses a bright green fluorescent digital display, so it's ideal for mobile applications. The *Bearcat* 300 now has these added features: Service Search, Display Intensity Control, Hold Search and Resume Search keys, Separate Band keys to permit lock-in/lock-out of any band for more efficient service search.

Bearcat® 250

List price $419.95/**CE price $259.00/$20.00 rebate**
Your final cost is a low $239.00
50 Channels • Crystalless • Searches Stores • Recalls • Digital clock • AC/DC Priority Channel • 3-Band • Count Feature.
Frequency range 32-50, 146-174, 420-512 MHz.
The *Bearcat* 250 performs any scanning function you could possibly want. With push button ease you can program up to 50 channels for automatic monitoring. Overseas customers should order the *Bearcat* **250FB** at $349.00 each. This model is like a *Bearcat* 250, but designed for international operation with 220 V AC/12 V DC power supply and 66-88 MHz low band coverage instead of 32-50 MHz.

Bearcat® 220

List price $419.95/**CE price $259.00/$20.00 rebate**
Your final cost is a low $239.00
Aircraft and public service monitor. *Frequency range 32-50, 118-136 AM, 144-174, 420-512 MHz.*
The *Bearcat* 220 is one scanner which can monitor all public service bands plus the exciting AM aircraft band channels. Up to twenty frequencies may be scanned at the same time. Overseas customers should order the *Bearcat* **220FB** at $349.00 each. This model is like a *Bearcat* 220, but designed for international operation with 220 V AC/12 V DC power supply and 66-88 MHz low band coverage instead of 32-50 MHz.

NEW! Bearcat® 210XL

List price $319.95/**CE price $209.00/$20.00 rebate**
Your final cost is a low $189.00
18 Channels • 3 Bands • Crystalless • AC/DC
Frequency range: 32-50, 144-174, 421-512 MHz.
The *Bearcat* 210XL scanning radio is the second generation scanner that replaces the popular *Bearcat* 210 and 211. It has almost twice the scanning capacity of the *Bearcat* 210 with 18 channels plus dual scanning speeds and a bright green fluorescent display.

NEW! 50-Channel Bearcat 300

FREE Bearcat® Rebate Offer

Get a coupon good for a $20 rebate when you purchase a *Bearcat* 300, 250, 220 or 210XL. $10 rebate on models 211, 210 and 160. To get your rebate, mail this coupon with your original dated sales receipt and the *Bearcat* model number from the carton to Electra. You'll receive your rebate in four to six weeks. Offer valid only on purchases made betwen September 15, 1980 and November 15, 1980. All requests must be postmarked by November 29, 1980. Limit of one rebate per household. Coupon must accompany all rebate requests and may not be reproduced. Offer good only in the U.S.A. Void where taxed or prohibited by law. Resellers, companies, clubs and organizations–both profit and non-profit–are not eligible for rebates. Employees of Electra Company, their advertising agencies, distributors and retailers of *Bearcat* Scanners are also not eligible for rebates. Please be sure to send in the correct amount for your scanner. Pay the listed **CE** price in this ad. *Do not* deduct the rebate amount since your rebate will be sent directly to you from Electra. Orders received with insufficient payments will not be processed and will be returned.

NEW! Bearcat® 160

List price $279.95/**CE price $189.00/$10.00 rebate**
Your final cost is a low $179.00
16 Channels • 3 Bands • AC only • Priority Dual Scan Speeds • Direct Channel Access
Frequency range: 32-50, 144-174, 440-512 MHz.
The *Bearcat* 160 presents a new dimension in scanning form and function. The keyboard is smooth. No buttons to punch. No knobs to turn. Instead, finger-tip pads provide control of *all* scanning operations, including On/Off, Volume and Squelch. Green easy to read fluorescent display.

NEW! Bearcat® 5/800 MHz

The world's first 800 MHz. scanner!
This is a new model. Shipments will begin in December, 1980.
List price $179.95/**CE price $129.00**
8 Crystal Channels • 4 Bands • AC only
Frequency range: 33-50, 144-174, 440-512, 806-870 MHz.
The *Bearcat* 5/800 MHz is the only scanner on the market today that offers coverage of the 800 MHz. public service band and the other public service bands. Individual channel lockout. Scan Delay. Manual Scan.

Bearcat® 5

List price $129.95/**CE price $89.00**
8 Crystal Channels • 3 Bands • AC only
Frequency range: 33-50, 146-174, 450-508 MHz.
The *Bearcat* 5 is a value-packed crystal scanner built for the scanning professional — at a price the first-time buyer can afford. Individual lockout switches.

Bearcat® Four-Six ThinScan™

List price $179.95/**CE price $114.00**
Frequency range: 33-47, 152-164, 450-508 MHz.
The Incredible, new *Bearcat* Four-Six Thin Scan™ is like having an information center in your pocket. This three band, 6 channel crystal controlled scanner has patented Track Tuning on UHF. Scan Delay and Channel Lockout. Measures 2¾ x 6¼ x 1". Includes rubber ducky antenna. Order crystals for each channel. Made in Japan.

NEW! Fanon Slimline 6-HLU

List price $169.95/**CE price $109.00**
Low cost 6-channel, 3-band scanner!
The new *Fanon* Slimline 6-HLU gives you six channels of crystal controlled excitement. Unique Automatic Peak Tuning Circuit adjusts the receiver front end for maximum sensitivity across the entire UHF band. Individual channel lockout switches. Frequency range 30-50, 146-175 and 450-512 MHz. Size 2¾ x6¼ x 1." Includes rubber ducky antenna. Order crystal certificates for each channel. Made in Japan.

NEW! Fanon Slimline 6-HL

List price $149.95/**CE price $99.00**
6-Channel performance at 4-channel cost!
Frequency range: 30-50, 146-175 MHz.
If you *don't* need the UHF band, get this model and save money. Same high performance and features as the model HLU without the UHF band. Order crystal certificates for each channel. Made in Japan.

FANON SCANNER ACCESSORIES

CHB-6 AC Adapter/Battery Charger	$15.00
CAT-6 Carrying case for Fanon w/Belt Clip	$15.00
AUC-3 Auto lighter adaptor/Battery Charger	$15.00

OTHER SCANNER ACCESSORIES

SP50 AC Adapter	$8.00
SP51 Battery Charger	$8.00
SP58 Carrying Case for *Bearcat* 4-6 ThinScan™	$12.00
FB-E Frequency Directory for Eastern U.S.A.	$12.00
FB-W Frequency Directory for Western U.S.A.	$12.00
FFD Federal Frequency Directory for U.S.A.	$12.00
B-4 1.2 V AAA Ni-Cad's for ThinScan™ and Fanon	$9.00
A-135cc Crystal certificate	$3.00

Add $3.00 shipping for all accessories ordered at the same time.

INCREASED PERFORMANCE ANTENNAS

If you want the utmost in performance from your scanner, it is essential that you use an external antenna. We have six base and mobile antennas specifically designed for receiving all bands. Order **#A60** is a magnet mount mobile antenna. Order **#A61** is a gutter clip mobile antenna. Order **#A62** is a trunk-lip mobile antenna. Order **#A63** is a ¾ inch hole mount. Order **#A64** is a ⅜ inch snap-in mount, and **#A70** is an all band base station antenna. All antennas are $30.00 and $3.00 for UPS shipping in the continental United States.

TEST ANY SCANNER

Test any scanner purchased from **Communications Electronics™** for 31 days before you decide to keep it. If for any reason you are not completely satisfied, return it in original condition with all parts in 31 days, for a prompt refund (less shipping/handling charges and rebate credits).

NEW! Regency®‡ M400

List price $379.95/**CE price $259.00**
30 Channel • Synthesized • Service Search Digital clock • Digital timer • M100 styling Search/Store • Priority Channel • AC/DC
Frequency range: 30-50, 144-174, 440-512 MHz.
The new *Regency* M400 is a compact programmable FM monitor receiver for use at home or on the road.

OTHER REGENCY‡ SCANNERS

Touch K100	$199.00
Touch M100	$199.00

NEW! Telephone Products

Electra's cordless *Freedom Phone* does everything an ordinary phone does and more. Because it is cordless, you can take it anywhere, inside or outside—on the patio, by the pool, in the garage, in the workshop...even next door at the neighbor's.

Model **FF-500** has pushbutton dialing. Rechargeable ni-cad batteries included. Battery low light. Secure feature. Telescopic antenna. Your cost is $179.00. Model **FF-1500** has the same features as the FF-500 but also includes a charger/cradle that allows the phone's handset to be recharged away from the base station. Your cost for this cordless phone is $199.00. The model **FF-3000** has all the standard features (except charger/cradle) plus interchangeable telescopic and rubber ducky antenna. Redial feature. Belt clip. Carrying case. Greater range. Your cost is $229.00.

World Scanner Association™

The WORLD SCANNER ASSOCIATION is sponsored as a public service by **Communications Electronics.™** When you join, you'll receive a one-year membership and our quarterly newsletter with scanner news and features. You'll also get a wallet I.D. card, an Official WSA Membership Certificate, and more. FREE classified ads for members so you can contact other scanner owners when you want to sell or buy a scanner. FREE membership in the WSA Buyer's Co-op. Your Co-op membership will allow you to get special discounts on scanners and scanner related products. Since the WSA Buyer's Co-op gives you group purchasing power, you can easily pay for your membership dues the first time you make a Co-op purchase. To join, send $12.00 ($20.00 outside U.S.A.) for your membership materials.

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To ***get the fastest delivery from CE*** of any scanner, send or phone your order directly to our Scanner Distribution Center™ Be sure to calculate your price using the **CE** prices in this ad. Michigan residents please add 4% sales tax. Written purchase orders are accepted from approved government agencies and most well rated firms at a 10% surcharge for net 30 billing. All sales are subject to availability. All sales on accessories are final. Prices, terms and specifications are subject to change without notice. Out of stock items will be placed on backorder automatically unless **CE** is instructed differently. Most products that we sell have a manufacturer's warranty. Free copies of warranties on these products are available prior to purchase by writing to CE. International orders are invited with a $20.00 surcharge for special handling in addition to shipping charges. All shipments are F.O.B. Ann Arbor, Michigan. No COD's please. Non-certified and foreign checks require five weeks bank clearance.

Mail orders to: **Communications Electronics,™** Box 1002, Ann Arbor, Michigan 48106 U.S.A. Add $6.00 per scanner or phone product for U.P.S. *ground* shipping, or $12.00 for faster U.P.S. *air* shipping to some locations. If you have a Master Charge or Visa card, you may call anytime and place a credit card order. **Order toll free** in the U.S.A. 800-521-4414. If you are outside the U.S. or in Michigan, dial 313-994-4444. **Dealer inquiries invited.** All order lines at **Communications Electronics™** are staffed 24 hours.

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SN7416N	.29	SN7491N	.59	SN74176N	.79
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SN7421N	.29	SN7494N	.69	SN74180N	.79
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SN7426N	.29	SN74100N	1.49	SN74185N	2.49
SN7427N	.25	SN74107N	.35	SN74190N	1.25
SN7429N	.39	SN74109N	.39	SN74191N	1.25
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SN7438N	.40	SN74123N	.59	SN74195N	.69
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SN7454N	.20	SN74152N	.69	SN74367N	.69
SN7459A	.25	SN74153N	.79	SN74368N	.69
SN7460N	.20	SN74154N	1.25	SN74390N	1.49
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74LS01	.29			74LS193	1.15
74LS02	.29	74LS92	.75	74LS194	1.15
74LS03	.29	74LS93	.75	74LS195	1.15
74LS04	.35	74LS95	.99	74LS197	1.19
74LS05	.35	74LS96	1.15	74LS221	1.19
74LS08	.29	74LS107	.45	74LS240	1.95
74LS09	.35	74LS109	.45	74LS241	1.95
74LS10	.29	74LS112	.45	74LS242	1.95
74LS11	.75	74LS113	.49	74LS243	1.95
74LS12	.35	74LS114	.49	74LS244	1.95
74LS13	.59	74LS122	.89	74LS245	2.95
74LS14	.99	74LS123	1.25	74LS247	1.19
74LS15	.35	74LS125	.89	74LS248	1.19
74LS20	.29	74LS126	.55	74LS249	1.19
74LS21	.35	74LS132	.99	74LS251	1.49
74LS22	.35	74LS133	.89	74LS253	.99
74LS26	.35	74LS136	.49	74LS257	.89
74LS27	.35	74LS138	.89	74LS258	.99
74LS28	.35	74LS139	.89	74LS260	.69
74LS30	.29	74LS151	.89	74LS266	.69
74LS32	.35	74LS153	.89	74LS273	1.95
74LS33	.59	74LS154	1.75	74LS279	.75
74LS37	.45	74LS155	1.19	74LS283	1.09
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74LS48	1.15	74LS161	1.15	74LS353	1.29
74LS49	1.15	74LS162	1.15	74LS365	.75
74LS51	.29	74LS163	1.15	74LS366	.75
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74LS55	.29	74LS165	1.25	74LS368	.75
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74LS76	.45	74LS173	1.39	74LS386	.69
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74LS83	.89	74LS175	.99	74LS399	2.49
74LS85	1.25	74LS181	2.95	74LS670	2.49
74LS86	.45	74LS190	1.25	81LS95	1.95
74LS90	.59	74LS191	1.25	81LS97	1.95

74S

74S00	.50			74S244	3.25
74S02	.50			74S251	1.45
74S03	.50	74S133	.55	74S253	1.45
74S04	.56	74S134	.69	74S257	1.35
74S05	.56	74S135	1.19	74S258	1.35
74S08	.50	74S136	1.75	74S260	.79
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CA3046N	1.30	CA3081N	2.00	CA3140H	1.25
CA3059N	3.25	CA3082N	2.00	CA3160H	1.25
CA3060N	3.25	CA3083N	1.60	CA3401N	.59
CA3080H	1.25	CA3086N	.85	CA3600N	3.50

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CD4001	.39			CD4093	.99
CD4002	.39			CD4098	2.49
CD4006	1.19			CD4506	.75
CD4007	.25	CD4041	1.49	CD4507	.99
CD4009	.49	CD4042	.99	CD4508	3.95
CD4010	.49	CD4043	.89	CD4510	1.39
CD4011	.39	CD4044	.89	CD4511	1.29
CD4012	.25	CD4046	1.79	CD4514	3.95
CD4013	.49	CD4047	2.50	CD4515	2.95
CD4014	1.39	CD4048	1.35	CD4516	1.49
CD4015	1.19	CD4049	.49	CD4518	1.79
CD4016	.59	CD4050	.69	CD4519	.89
CD4017	1.19	CD4051	1.19	CD4520	1.29
CD4018	.99	CD4052	1.19	CD4526	1.79
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CD4020	1.19	CD4056	2.95	CD4529	1.95
CD4021	1.39	CD4059	9.95	CD4543	2.79
CD4022	1.19	CD4060	1.49	CD4562	11.95
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CD4025	.23	CD4069	.45	CD4723	1.95
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JE608 PROGRAMMER

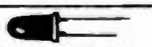
2708 EPROM PROGRAMMER

- 3 separate Display Registers: 8 LED's for Hex Key entries, 10 LED's (2" 2") for Address Register and 8 LED's for Data Memory Register. The Data Memory Register displays the content of the RAMs from the EPROM Chip.
- Development of microprocessor systems by means of a ribbon cable from the programmer panel test socket to the EPROM socket on the microprocessor board.
- Rapid checking verification of programmed data changes.
- User may move data from a master to RAM's or write into RAM's with keyboard entries.
- Allows manual stepping manipulation (up and down) at any address location.
- Stand alone EPROM Programmer consisting of: A 19 key Hexadecimal Keyboard assembly, Programmer Board assembly with 4 power supplies and a LED/Test Socket Panel Board assembly. The Test Socket is zero force insertion type. Power requirements: 115VAC, 60Hz, 6W.
- Compact desk top enclosure. Color coordinated designer's case with light tan panels and molded end pieces in mocha brown. Size: 3⅛"H x 11"W x 8⅛"D. Weight: 5 lbs.

The JE608 EPROM Programmer is a completely self contained unit which is independent of computer control and requires no additional systems for its operations. The EPROM can be programmed from the Hexadecimal Keyboard or from a pre-programmed EPROM. The JE608 Programmer can emulate a programmed EPROM by the use of its internal RAM circuits. This will allow the user to test or pretest a program, for a system, prior to programming a chip. Any changes in the program can be entered directly into the memory circuits with the Hexadecimal Keyboard so that rewriting the entire program will not be necessary. The JE608 Programmer contains a Programmer/Board with 25 IC's and including power supplies of −5V, +5V, +12V and +26V. The Hexadecimal Keyboard and LED/Test Socket Panel Board are separate assemblies within the system.

JE608K KIT **$399.95**
JE608A Assembled and tested **$499.95**

DISCRETE LEDS

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XC556C	.200"	clear	4/$1	XC209Y	.125"	yellow	4/$1	XC111C	.190"	clear	4/$1
XC22R	.200"	red	5/$1	XC526R	.185"	red	5/$1				
XC22G	.200"	green	4/$1	XC526G	.185"	green	4/$1				
XC22Y	.200"	yellow	4/$1	XC526Y	.185"	yellow	4/$1				
MV10B	.170"	red	4/$1	XC526C	.185"	clear	4/$1				

INFRA-RED LED
¼" x ¼" x 1/16" flat
IRL — 5/$1

DISPLAY LEDS

C.A. — Common Anode | C.C. — Common Cathode

Type	Polarity	Ht	Price	Type	Polarity	Ht	Price
MAN 1	C.A.—red	.270	2.95	DL741	C.A.—red	.600	1.25
MAN 2	5x7 D.M.—red	.300	4.95	DL746	C.A.—red ± 1	.630	1.49
MAN 3	C.C.—red	.125	.25	DL747	C.A.—red	.600	1.49
MAN 52	C.A.—green	.300	1.25	DL750	C.C.—red	.600	1.49
MAN 54	C.C.—green	.300	1.25	DL33B	C.C.—red	.110	.35
MAN 71	C.A.—red	.300	.75	FND358	C.C. ± 1	.357	.99
MAN 72	C.A.—red	.300	.75	FND359	C.C.	.357	.75
MAN 74	C.C.—red	.300	1.25	FND503	C.C. (FND500)	.500	.99
MAN 82	C.A.—yellow	.300	.49	FND507	C.A. (FND510)	.500	.99
MAN 84	C.C.—yellow	.300	.99	HDSP-3401	C.A.—red	.800	1.50
MAN 3620	C.A.—orange	.300	.49	HDSP-3403	C.C.—red	.800	1.50
MAN 3630	C.A.—orange ± 1	.300	.99	5082-7613	C.C., R.H.D.—red	.300	1.25
MAN 3640	C.C.—orange	.300	.99	5082-7620	C.A., L.H.D.—yel.	.300	1.25
MAN 4610	C.A.—orange	.400	.99	5082-7623	C.C., R.H.D.—yel.	.300	1.25
MAN 6610	C.A.—orange—DD	.560	.99	5082-7730	C.A., L.H.D.—red	.300	.99
MAN 6630	C.A.—orange ± 1	.560	.99	5082-7731	C.A., R.H.D.—red	.300	1.25
MAN 6640	C.C.—orange—DD	.560	.99	5082-7750	C.A., L.H.D.—red	.430	1.75
MAN 6650	C.C.—orange ± 1	.560	.99	5082-7751	C.A., R.H.D.—red	.430	1.25
MAN 6660	C.A.—orange	.560	.99	5082-7760	C.C., R.H.D.—red	.430	1.75
MAN 6710	C.A.—red—DD	.560	.99	5082-7300	4x7 sgl. dig. RHD	.600	22.00
MAN 6750	C.C.—red ± 1	.560	.99	5082-7302	4x7 sgl. dig. LHD	.600	22.00
MAN 6780	C.C.—red	.560	.99	5082-7304	Overnge. char. (±1)	.600	19.95
DL704	C.C.—red	.300	1.25	4N28	Photo Xsistor Opto-Isol.		.99
DL707	C.A.—red	.300	1.25	LIT-1	Photo Xsistor Opto-Isol.		.69
DL728	C.C.—red	.500	1.49	MOC3010	Optically Isol. Triac Driver		1.25

POTENTIOMETERS

$2.95 each
2 Watt @ 70°C ± 10%
7/8" Slotted Shaft
Linear Taper
Meets Mil-R 94

Part No.		
CMU 1021	RV4NAY SD - 102A	1K
CMU 5021	RV4NAY SD - 502A	5K
CMU 1031	RV4NAY SD - 103A	10K
CMU 2531	RV4NAY SD - 253A	25K
CMU 5031	RV4NAY SD - 503A	50K
CMU 1041	RV4NAY SD - 104A	100K
CMU 1052	RV4NAY SD - 105A	1Meg

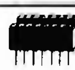
$1.35 each
3/4 Watt @ 70°C
15 turn pot. Linear taper. Printed circuit mount.

Part No.	Part No.	Part No.
830P-50ohm	830P-5K	830P-100K
830P-100ohm	830P-10K	830P-200K
830P-500ohm	830P-20K	830P-500K
830P-1K	830P-50K	830P-1Meg
830P-2K		

LOW PROFILE (TIN) SOCKETS

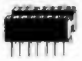
	1-24	25-49	50-100
8 pin LP	.17	.16	.15
14 pin LP	.20	.19	.18
16 pin LP	.22	.21	.20
18 pin LP	.29	.28	.27
20 pin LP	.34	.32	.30
22 pin LP	.37	.36	.35
24 pin LP	.38	.37	.36
28 pin LP	.45	.44	.43
36 pin LP	.60	.59	.58
40 pin LP	.63	.62	.61

SOLDERTAIL STANDARD (TIN)



	1-24	25-49	50-100
14 pin ST	.27	.25	.24
16 pin ST	.30	.27	.25
18 pin ST	.35	.32	.30
24 pin ST	.49	.45	.42
28 pin ST	.99	.90	.81
36 pin ST	1.39	1.26	1.15
40 pin ST	1.59	1.45	1.30

SOLDERTAIL (GOLD) STANDARD



	1-24	25-49	50-100
8 pin SG	.39	.35	.31
14 pin SG	.49	.45	.41
16 pin SG	.54	.49	.44
18 pin SG	.59	.53	.48
24 pin SG	.79	.75	.69
28 pin SG	1.10	1.00	.90
36 pin SG	1.65	1.40	1.26
40 pin SG	1.75	1.59	1.45

WIRE WRAP SOCKETS (GOLD) LEVEL #3

	1-24	25-49	50-100
8 pin WW	.59	.54	.49
10 pin WW	.69	.63	.58
14 pin WW	.79	.73	.67
16 pin WW	.85	.77	.70
18 pin WW	.99	.90	.81
20 pin WW	1.19	1.08	.99
22 pin WW	1.49	1.35	1.23
24 pin WW	1.39	1.26	1.14
28 pin WW	1.69	1.53	1.38
36 pin WW	2.19	1.99	1.79
40 pin WW	2.29	2.09	1.89

1/4 WATT RESISTOR ASSORTMENTS – 5%

ASST. 1	5 ea.	10 Ohm 12 Ohm 15 Ohm 18 Ohm 22 Ohm 27 Ohm 33 Ohm 39 Ohm 47 Ohm 56 Ohm	50 pcs.	$1.95
ASST. 2	5 ea.	68 Ohm 82 Ohm 100 Ohm 120 Ohm 150 Ohm 180 Ohm 220 Ohm 270 Ohm 330 Ohm 390 Ohm	50 pcs.	$1.95
ASST. 3	5 ea.	470 Ohm 560 Ohm 680 Ohm 820 Ohm 1K 1.2K 1.5K 1.8K 2.2K 2.7K	50 pcs.	$1.95
ASST. 4	5 ea.	3.3K 3.9K 4.7K 5.6K 6.8K 8.2K 10K 12K 15K 18K	50 pcs.	$1.95
ASST. 5	5 ea.	22K 27K 33K 39K 47K 56K 68K 82K 100K 120K	50 pcs.	$1.95
ASST. 6	5 ea.	150K 180K 220K 270K 330K 390K 470K 560K 680K 820K	50 pcs.	$1.95
ASST. 7	5 ea.	1M 1.2M 1.5M 1.8M 2.2M 2.7M 3.3M 3.9M 4.7M 5.6M	50 pcs.	$1.95
ASST. 8R		Includes Resistor Assts. 1-7 (350 pcs.)		$10.95 ea.

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INTERSIL

Part No.	Function	Price
7045IPI	CMOS Precision Timer	14.95
7045EV/Kit*	Stopwatch Chip, XTL	22.95
7106CPL	3½ Digit A/D (LCD Drive)	16.95
7106EV/Kit*	IC, Circuit Board, Display	34.95
7107CPL	3½ Digit A/D (LED Drive)	15.95
7107EV/Kit*	IC, Circuit Board, Display	28.95
7116CPL	3½ Digit A/D LCD Dis. HLD.	18.95
7117CPL	3½ Digit A/D LED Dis. HLD.	17.95
7201IDR	Low Battery Volt Indicator	2.25
7205IPG	CMOS LED Stopwatch/Timer	12.95
7205EV/Kit*	Stopwatch Chip, XTL	19.95
7206CJPE	Tone Generator	5.15
7206CEV/Kit*	Tone Generator Chip, XTL	9.95
7207AIPD	Oscillator Controller	6.50
7207AEV/Kit*	Freq. Counter Chip, XTL	11.10
7208IPI	Seven Decade Counter	17.95
7209IPA	Clock Generator	3.95
7215IPG	4 Func. CMOS Stopwatch CKT	13.95
7215EV/Kit*	4 Func. Stopwatch Chip, XTL	19.95
7216AIJI	8-Digit Univ. Counter C.A.	32.00
7216CIJI	8-Digit Freq. Counter C.A.	26.95
7216DIPI	8-Digit Freq. Counter C.C.	21.95
7217IJI	4-Digit LED Up/Down Counter	12.95
7218CIJI	8-Digit Univ. LED Drive	10.95
7224IPL	LCD 4½ Digit Up Counter DRI	11.25
7226AIJL	8-Digit Univ. Counter	31.95
7226AEV/Kit*	5 Function Counter Chip, XTL	74.95
7240IJE	CMOS Bin Prog. Timer/Counter	4.95
7242IJA	CMOS Divide-by-256 RC Timer	2.05
7250IJE	CMOS BCD Prog. Timer/Counter	6.00
7260IJE	CMOS BCD Prog. Timer/Counter	5.25
7555IPA	CMOS 555 Timer (8 pin)	1.45
7556IPD	CMOS 556 Timer (14 pin)	2.20
7611BCPA	CMOS Op Amp Comparator 5MV	2.25
7612BCPA	CMOS Op Amp Ext. Cmvr. 5MV	2.95
7621BCPA	CMOS Dual Op Amp Comp. 5MV	3.95
7631CCPE	CMOS Tri Op Amp Comp. 10MV	5.35
7641CCPD	CMOS Quad Op Amp Comp. 10MV	7.50
7642CCPD	CMOS Quad Op Amp Comp. 10MV	7.50
7660CPA	Voltage Converter	2.95
8069CCQ	50ppm Band—GAP Volt Ref. Diode	2.50
8211CPA	Volt Ref/Indicator	2.50
8212CPA	Volt Ref/Indicator	2.50

* INTERSIL'S EVALUATION KITS

74C

74C00	.39			74C195	1.59
74C02	.39			74C221	1.95
74C04	.39			74C240	2.25
74C08	.39	74C106	.75	74C244	2.25
74C10	.39	74C107	1.89	74C373	2.49
74C14	.75	74C151	2.95	74C374	2.59
74C20	.39	74C154	3.95	74C901	.89
74C30	.39	74C157	2.25	74C903	1.15
74C42	1.39	74C160	1.69	74C911	10.95
74C48	1.95	74C161	1.60	74C912	10.95
74C73	.79	74C162	1.49	74C915	1.69
74C74	.79	74C163	1.69	74C917	10.95
74C85	1.95	74C164	1.59	74C922	5.49
74C86	.99	74C173	1.39	74C923	5.75
74C89	6.95	74C174	1.39	74C925	7.50
74C90	1.29	74C175	1.39	74C926	7.50
74C93	1.29	74C192	1.69	80C95	.79
74C95	1.59	74C193	1.69	80C97	.79

LINEAR

LH0002CN	6.85			NE570N	4.95
LM10CLH	4.50			LM702H	.79
LM11CLH	4.75			LM703CN	.89
LH0070-OH	6.05	LM340T-5	1.25	LM709N	.29
TL071CP	.79	LM340T-12	1.25	LM710N	.79
TL072CP	1.39	LM340T-15	1.25	LM711N	.79
TL074CN	2.49	LM341P-5	.75	LM723N	.69
LH0082CD	35.80	LM341P-12	.75	LM733N	1.00
TL082CP	1.19	LM341P-15	.75	LM739N	1.19
TL084CN	2.19	LM342P-5	.69	LM741CN	.35
LH0094CD	36.80	LM342P-12	.69	MC1741SCG	3.00
LM300H	.99	LM342P-15	.69	LM747N	.79
LM301CN	.35	LM348N	1.25	LM748N	.59
LM302H	1.95	LM350K	5.75	LM1014N	2.75
LM304H	1.95	LF351N	.60	LM1310N	1.95
LM305H	.99	LF353N	1.00	LM1458CN	.59
LM307CN	.45	LF355N	1.10	LM1488N	1.25
LM308CN	1.00	LF356N	1.10	LM1489N	1.25
LM309H	1.95	LM358N	1.00	LM1496N	1.95
LM309K	1.25	LM359N	1.79	LM1556V	1.75
LM310CN	1.75	LM370N	4.49	LM1800N	2.95
LM311H	.90	LM373N	3.25	LM1877N-9	3.25
LM312H	2.49	LM377N	2.95	LM1889N	3.20
LM317MP	1.15	LM380N	1.25	LM1896N	1.75
LM317T	1.75	LM381N	1.95	LM2002T	1.49
LM317K	3.95	LM382N	1.79	LM2877P	2.05
LM318CN	1.95	LM384N	1.95	LM2878P	2.25
LM319N	1.95	LM386N-3	1.29	LM2896P-1	2.25
LM320K-5	1.35	LM387N	1.45	LM3189N	2.95
LM320K-12	1.35	LM389N	1.35	LM3900N	.69
LM320K-15	1.35	LM392N	.69	LM3905CN	1.25
LM320T-5	1.25	LF398N	4.00	LM3909N	1.15
LM320T-12	1.25	LM399H	5.00	LM3914N	3.95
LM320T-15	1.25	TL494CN	4.49	LM3915N	3.95
LM323K-5	5.95	TL496CP	1.75	LM3916N	3.95
LM324N	.99	NE510A	6.00	RC4136N	1.25
LM329DZ	.65	NE529A	4.95	RC4151NB	3.95
LM331N	3.95	NE531H	3.95	RC4194TK	5.95
LM334Z	1.30	NE536H	6.00	RC4195TK	5.49
LM335Z	1.40	NE540H	6.00	KB4428	4.25
LM336Z	1.75	NE544N	4.95	KB4429	5.95
LM337T	1.95	NE550A	1.30	LM4500A	3.25
LM337MP	1.15	NE555V	.39	ICL8038B	4.95
LM338K	6.95	LM556N	.99	LM13080N	1.29
LM339N	.99	NE564N	3.95	LM13600N	1.49
LM340K-5	1.35	LM565N	1.25	75138N	1.95
LM340K-12	1.35	LM566CN	1.95	75450N	.89
LM340K-15	1.35	LM567V	1.25	75451CN	.39

CAPACITOR CORNER

50 VOLT CERAMIC DISC CAPACITORS

Value	1-9	10-99	100+	Value	1-9	10-99	100+
10 pf	.08	.06	.05	.001µF	.08	.06	.05
22 pf	.08	.06	.05	.0047µF	.08	.06	.05
47 pf	.06	.06	.05	.01µF	.08	.06	.05
100 pf	.08	.06	.05	.022µF	.09	.07	.06
220 pf	.08	.06	.05	.047µF	.09	.07	.06
470 pf	.08	.06	.05	.1µF	.15	.12	.10

100 VOLT MYLAR FILM CAPACITORS

.001mf	.12	.10	.07	.022mf	.13	.11	.08
.0022mf	.12	.10	.07	.047mf	.21	.17	.13
.0047mf	.12	.10	.07	.1mf	.27	.23	.17
.01mf	.12	.10	.07	.22mf	.33	.27	.22

+20% DIPPED TANTALUMS (Solid) CAPACITORS

.1/35V	.39	.34	.29	1.5/35V	.41	.37	.29
.15/35V	.39	.34	.29	2.2/35V	.51	.45	.34
.22/35V	.39	.34	.29	3.3/25V	.53	.47	.37
.33/35V	.39	.34	.29	4.7/25V	.63	.56	.45
.47/35V	.39	.34	.29	6.8/25V	.79	.69	.55
.68/35V	.39	.34	.29	15/25V	1.39	1.25	.95
1.0/35V	.39	.34	.29	22/6V	.79	.69	.55

MINI. ALUMINUM ELECTROLYTIC CAPACITORS

Axial Lead				Radial Lead			
.47/50V	.16	.14	.10	.47/25V	.15	.13	.12
1.0/50V	.19	.16	.12	.47/50V	.16	.14	.13
3.3/50V	.17	.15	.11	1.0/16V	.15	.13	.12
4.7/25V	.18	.15	.11	1.0/25V	.16	.14	.13
10/25V	.18	.15	.11	1.0/50V	.17	.15	.14
10/50V	.19	.16	.12	4.7/16V	.15	.13	.12
22/25V	.19	.16	.12	4.7/25V	.16	.14	.13
22/50V	.24	.20	.18	4.7/50V	.17	.15	.14
47/25V	.25	.21	.19	10/16V	.15	.13	.12
47/50V	.29	.25	.23	10/25V	.16	.14	.13
100/25V	.28	.24	.22	10/50V	.17	.15	.14
100/50V	.41	.37	.34	47/50V	.25	.21	.19
220/25V	.39	.34	.33	100/16V	.21	.17	.14
220/50V	.49	.45	.41	100/25V	.25	.23	.21
470/25V	.54	.49	.45	100/50V	.37	.34	.31
1000/16V	.79	.69	.61	220/16V	.25	.21	.19
2200/16V	.89	.79	.69	470/25V	.35	.31	.27

Reader Service—see page 194

38

fact: ARMCHAIR COPY begins here!

NEW!

The NEW Model 444D For: High/Low Impedance SSB/FM

The Model 444D incorporates all the tried-and-proven features that made Shure's Model 444 the recognized "standard" fixed-station microphone among serious amateurs. The 444D retains the Shure-designed, super-rugged CONTROLLED MAGNETIC® microphone element that lets you come across with "armchair copy"! Its unmatched performance characteristics include a tailored response for maximum voice intelligibility, PLUS...

DUAL IMPEDANCE—(150 ohms) Low & High. Impedance selector switch located on bottom of base.

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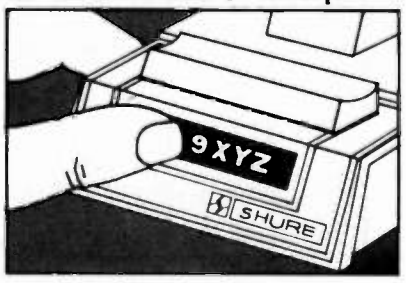
IMPROVED CONTROL BAR—Shure Million-Cycle push-to-talk (PTT) improved fingertip action actuates microphone and an external relay or control circuit.

VOX/NORMAL SWITCH—Defeats PTT switch, for VOX equipment requiring continuously "on" microphone. Located conveniently on bottom of base.

PROFESSIONAL BLACK FINISH—Sturdy, high impact ARMO-DUR® base and microphone case is metalized for RF shielding. It is comfortable to the touch in any temperature or humidity, and will not rust or deteriorate.

CONVENIENT INSTALLATION—The coiled cable leads and push-to-talk switch are arranged to permit immediate hookup to transmitters with either isolated or grounded switching.

FREE! Personalized call letter nameplate



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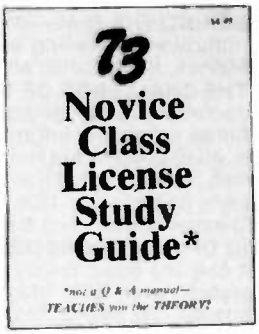

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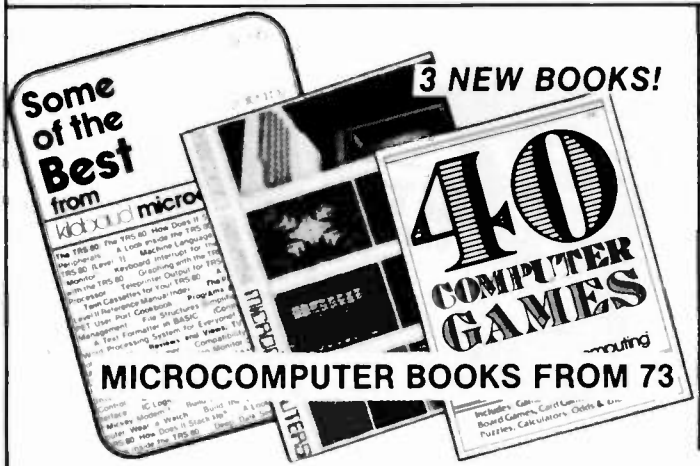

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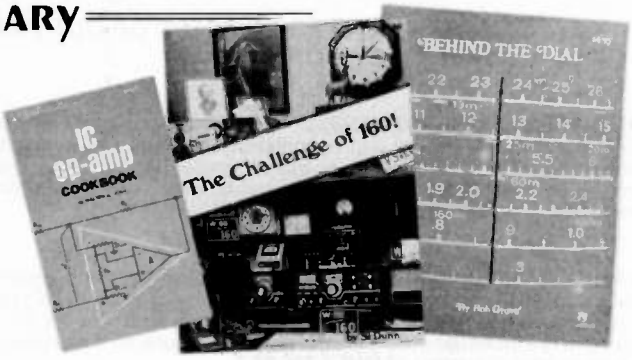

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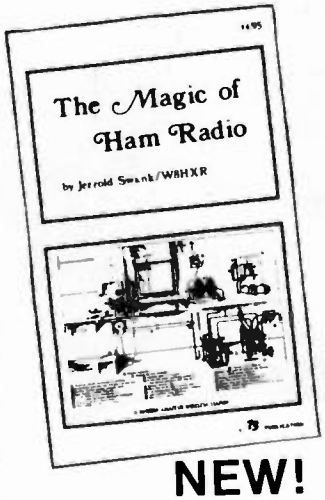

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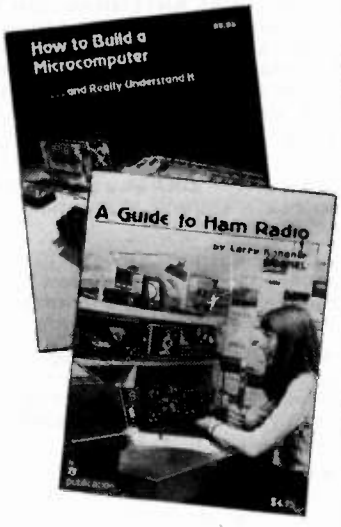

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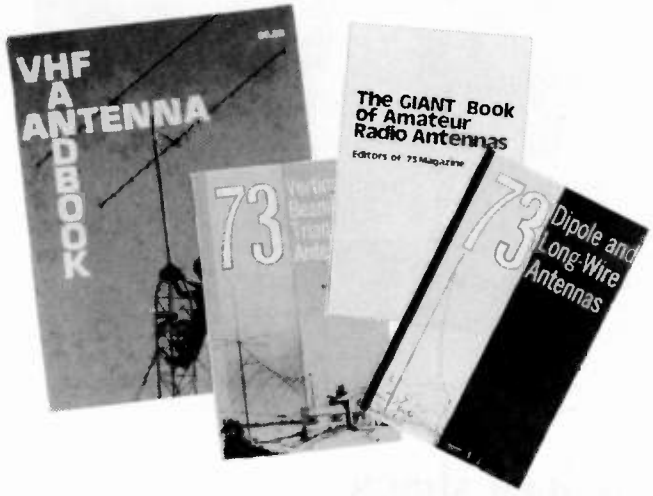

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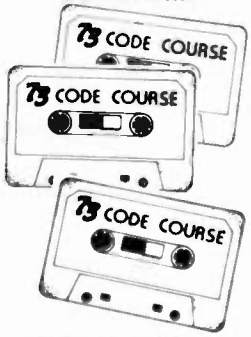

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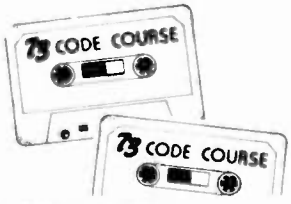

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ARGENTINA	14	14	7	7	7	7	14	21	21A	21A	21A	21
AUSTRALIA	21	14	7B	7B	7B	7B	14	21	21	21A	21A	21A
CANAL ZONE	14A	14	7	7	7	7	14	21	21A	21A	21A	21
ENGLAND	7	7	7	7	7	7	14	21	21A	21	14	14
HAWAII	21A	14	7B	7	7	7	7	7B	14	21	21A	21A
INDIA	7	7	7B	7B	7B	7B	14	14A	14	7B	7B	7B
JAPAN	14A	14	7B	7B	7B	7	7	7	7B	7B	7B	14
MEXICO	14A	14	7	7	7	7	7	14	21A	21A	21A	21
PHILIPPINES	21	14	7B	7B	7B	7B	7B	7	7	7	7B	14
PUERTO RICO	14	7	7	7	7	7	14	21	21A	21A	21	14A
SOUTH AFRICA	14	7	7	7B	7B	14	14A	21A	21A	21A	21	21
U.S.S.R.	7	7	7	7	7	7B	14	21A	14A	7B	7B	7
WEST COAST	21A	14	7	7	7	7	7	14	21	21A	21A	21A

CENTRAL UNITED STATES TO:

ALASKA	21	14	7	7	7	7	7	7	14	14A	21A	21A
ARGENTINA	21	14	7A	7	7	7	14	21	21A	21A	21A	21
AUSTRALIA	21	14A	14	7B	7B	7B	7B	7B	14A	21	21A	21A
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PHILIPPINES	21A	14	7B	7B	7B	7B	7B	7	7	7	7B	14
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MEXICO	21	14	7A	7	7	7	7	14	14A	21A	21A	21A
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U.S.S.R.	7B	7	7	7	7	7B	7B	7B	14A	7B	7B	7B
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A = Next higher frequency may also be useful
B = Difficult circuit this period
F = Fair G = Good P = Poor
SF = Chance of solar flares

january

sun	mon	tue	wed	thu	fri	sat
				1 F	2 G	3 G
4 G	5 G	6 G	7 G	8 G	9 G	10 G
11 G	12 F/SF	13 P	14 F	15 G	16 G	17 G
18 F	19 G	20 G	21 G	22 F	23 F	24 F
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391	Butternut Electronics	107
13	Clegg	59
89	Clutterfree Modular Consoles	81, 113
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382	Comm. Concepts, Inc	164
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31	Hal-Tronix	63, 74
30	The Ham-Key Co	49
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375	Herb Kreckman Co	164
478	Herb Kreckman Co	157
47	MFJ Enterprises	124, 125
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385	MELCO Enterprises	81
44	Macrotronics	103
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318	National Comm. Group Co	74
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482	OK Machine & Tool	34
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381	Radio Systems Tech., Inc	165
397	Radio World	33
62	Ramsey Electronics	178, 185
394	s a electronics	161
65	S-F Amateur Radio Services	38
477	S-F Amateur Radio Services	36
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376	SMP	164
64	Semiconductors Surplus	180-182
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52	57	62	67	72	177	182	187	192	197	302	307	312	317	322	427	432	437	442	447
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103	108	113	118	123	228	233	238	243	248	353	358	363	368	373	478	483	488	493	498
104	109	114	119	124	229	234	239	244	249	354	359	364	369	374	479	484	489	494	499
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