COMMUNICATIONS ECONDOLOGY Official trade journal of the Society of Cable Television Engineers

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May 1992

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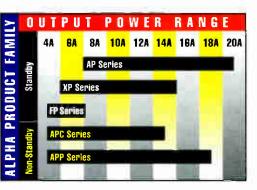
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Reader Service Number 3



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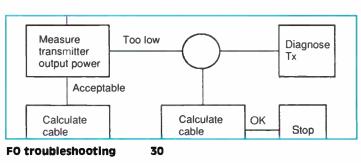
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Compression art by Geri Saye. TV photo by Bob Sullivan.

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The following highlights are from Optical Networks International's quarterly newsletter.

Optical Network

News

ONI's new architecture extends fiber's reach

ONI has developed a new fiber architecture designed to cost-effectively drive fiber deeper into cable systems. The Star-Star-Bus-500 (SSB-500) is a migratory architecture that enables operators to build cable plant today serving 500 homes per node at cost parity with FTF systems serving 2500 homes per node. The SSB-500 positions cable systems for introduction of new services with extensive interactive requirements. (Visit ONI's Booth #1614 and see related story in the May, 1992 issue of *CED*)

AT&T to stage digital compression theater

AT&T will be unveiling its NTSC digital compression system at the May NCTA show in Dallas, with a demonstration in AT&T's new digital compression theater. AT&T's digital compression system was first announced to CableLabs in a response to their RFP on digital compression. (Visit the AT&T Theater at Booth #1623.)

Alternate Access and Digital Transmission presentations at NCTA

Be sure to mark your show calendar for these important technical sessions:

Monday, May 4	3:15 p.m.	Technical Implications of Alternate Access Andy Paff, ONI
Wednesday, May 6	9:00 a.m.	Digital Transmission Fundamentals for Cable Engineers Ed Callahan, ANTEC (Carl McGrath, AT&T, co-author)

ONI demos new automated fusion splicer

ONI will be demonstrating the new Type-35SE fusion splicer from Sumitomo at the May NCTA show. This latest version of fusion splicers reduces splicing time and provides newly automated functions which ensure quality splices every time. The Type-35SE features an enhanced user interface, automatic atmospheric arc compensation, electrode monitoring and self-diagnostics.

(See a demonstration in ONI's Booth #1614)

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MAY 1992

EDITOR'S LETTER

PAC attack

ccording to a recent edition of Denver's Rocky Mountain News, the CATV industry has contributed over \$2 million to government officials during the last seven years through a vehicle known as political action committees (PACs). I hadn't given much though to the PAC process since a number of years ago when some of us in "key" positions in a corporate office were solicited to support the process. While the pressure to contribute was subtle, my decline to do so was equally subtle.

I personally do not believe in PACs, since I feel they are nothing more than an attempt to buy influence. Call me oldfashioned or even idealistic, but I think our elected representatives should be voting the will of the public, not the desires of special interests and lobbyists. Granted, some will say the cable industry's PACs are necessary to ensure that cable legislation remains generally favorable, or maintain "access" to those in Washington.

Nonsense. Since when should we have to pay to maintain access to our elected officials? As for unfavorable cable legislation (read "re-regulation"), who do we have to blame but ourselves for this one? First of all, had our rates and quality of service managed to stay in line after deregulation, we probably wouldn't have unfavorable legislation to worry about. Second, our industry was regulated for a lot longer than it has been deregulated and I seem to recall rather rapid growth during that time.

But back to PACs. Our industry's \$2 million since 1985 represents a pretty small piece of the PAC process. According to the News article, PACs contributed more than \$160 million to congressional candidates in 1990 alone. During the seven-year period mentioned in the article, telco PACs gave a little over \$9 million, and TV/radio PACs lined up with just under \$1 million.

It's interesting that the subject of PAC money should come up during an election year, especially a year that has already seen a lot of problems with the House bank scandal and other financial controversies. This whole mess has shown that money tends to drive way too much of our national policy.



"Some will say the cable industry's PACs are necessary to ensure that cable legislation remains generally favorable, or to maintain 'access' to those in Washington. Nonsense."

I haven't been too keen on our national politics for a long time. I lodged my own miniprotest years ago by not registering with any political party. My voter registration reads "unaffiliated," but yes, I do exercise my right to vote (except in election primaries, where unaffiliated voters are not allowed to vote). I'm one of those radicals who supports term limitations, too. I say, let's do away with career politicians.

For that matter, we now have the technology to put the vote on almost everything - including proposed legislation - directly in the hands of the general public. When our founding fathers created the system we have today, the public didn't have telephone, radio, television. CATV or personal computers. I get tired of the argument that we elect our officials to vote on our behalf. When was the last time your congressman asked you how he or she should vote on a particular issue? No, it's the lobbyists and special interest groups - including PACs — who determine the outcome of most legislation, not you and me.

Ronald J. Hranac Senior Technical Editor



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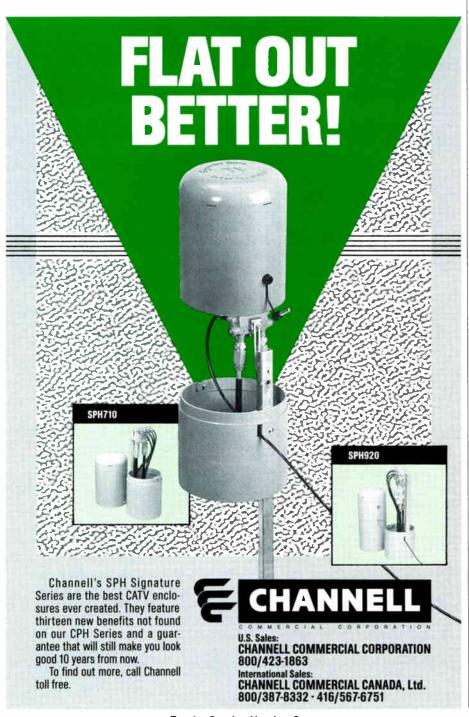
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Because of the weather extremes in Sudbury, Ontario, any kind of regular coaxial cable may last only months before some type of failure occurs. The weather, in fact, can be blamed for a 15-year history of unimaginable cable repair and replacement costs for Sudbury headquartered MSO, Northern Cable Services. It was a cable line technician's worst nightmare.

In 1984, all that changed for Northern Cable when they turned to our Quantum Reach. With an already established impressive performance record, QR promised better days ahead. And that's exactly what happened. The continuous cycle of splicing and replacement ended with the first installed section of QR.

Today, Northern Cable credits Quantum Reach with reducing their maintenance time by 75% and they tell us that their "construction guys just love it". They know that every new mile of QR installed is one less mile to worry about come next year, or the year after that, or the year after that, or the ...

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The point here is simple. If Quantum Reach will do the job for Northern Cable under the worst conditions when every other cable failed, think what it could mean for your system. We even have a comprehensive article detailing the QR installation in Sudbury. It's free for the asking. Simply contact your nearest Comm/Scope representative or call us at (800) 982-1708 or (704) 324-2200.

Comm/Scope, Inc. THE Cable in CableTV.

Comm/Scope, Inc., P.O. Box 1729, Hickory, NC 28602. Phone (800) 982-1708 or (704) 324-2200. Fax: (704) 328-3400.

Reader Service Number 10



National Show technical agenda

DALLAS — The National Cable Television Association's show is being held here from May 3-6. The following is a listing of the times and specific locations of tech sessions, seminars and meetings to be held in the convention center.

• Monday, May 4 tech sessions: "HDTV/ATV — The big picture" (12-1:15 p.m., West Ballroom A); "Optimizing fiber technology for cable" (12-1:15 p.m., West Ballroom B); "Advances in fiber technology" (1:30-2:45 p.m., West Ballroom A); "Flexible network architectures — Safeguarding cable's future" (3:15-4:30 p.m., West Ballroom A).

As well, the NCTA Engineering Committee Signal Leakage Subcommittee meeting will be held on Monday from 4:30-6 p.m. in Room N217.

• *Tuesday, May 5* tech sessions: "Digital techniques and applications audio and data" (10:30-11:45 a.m., West Ballroom A); "Improving the cable-consumer electronics interface - Issues and hardware" (12-1:30 p.m., West Ballroom A); "Real-world solutions to outage problems" (12-1:30 p.m., West Ballroom B); "Winning papers from signal security competition" (12-1:30 p.m., West Ballroom C); "Digital systems techniques and performance" (2:30-3:45 p.m., West Ballroom A); "Meet the FCC staff" (2:30-3:45 p.m., West Ballroom D); "High-speed digital transmission for CATV" (4:15-5:30 p.m., West Ballroom A).

• Wednesday, May 6 tech sessions: "Cable systems or networks — What are you building?" (9-10:15 a.m., West Ballroom A); "The new technical standards: A sharper image" (9-10:15 a.m., West Ballroom B); "Advances in conditional access and consumer electronics capability" (10:30 a.m.-12 p.m., West Ballroom A); "Headend operations" (10:30 a.m.-12 p.m., West Ballroom B).

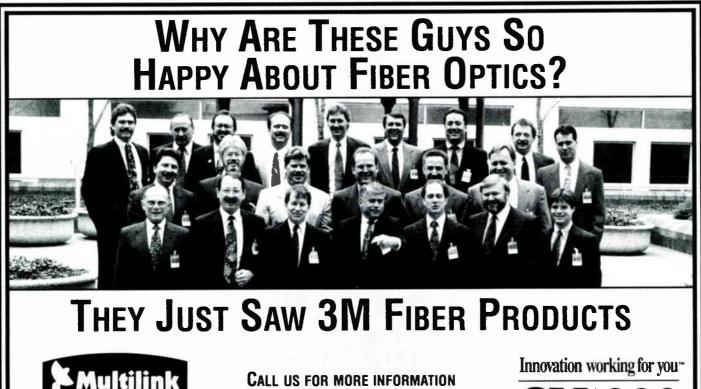
Also, two tech seminars will be held 3-4:30 p.m. on Wednesday in the Lower North Meeting Rooms: "Basic introduction to digital applications" and "Implementation of the new technical standards."

HDTV: One demoed, one being tested

WASHINGTON, D.C. — General Instrument's DigiCipher and partner Massachusetts Institute of Technology recently conducted the "world's first" alldigital transmission over-the-air and via cable for lawmakers, the FCC and the press.

At local public station WETA, a digital HDTV video recorder rolled at the transmitter site, the signal went out over normal bandwidth, and the broadcast was received, decoded and displayed on HDTV monitors located in the U.S. Capitol connected to off-air antennas and Congress' cable system. Meanwhile, District Cablevision also picked up, monitored and evaluated the transmission.

In Alexandria, Va., Zenith Electronics and AT&T's all-digital HDTV system, Digital Spectrum Compatible HDTV, is being tested at the Advanced Television Test Center. It is the third of five HDTV systems to undergo the battery of tests. →





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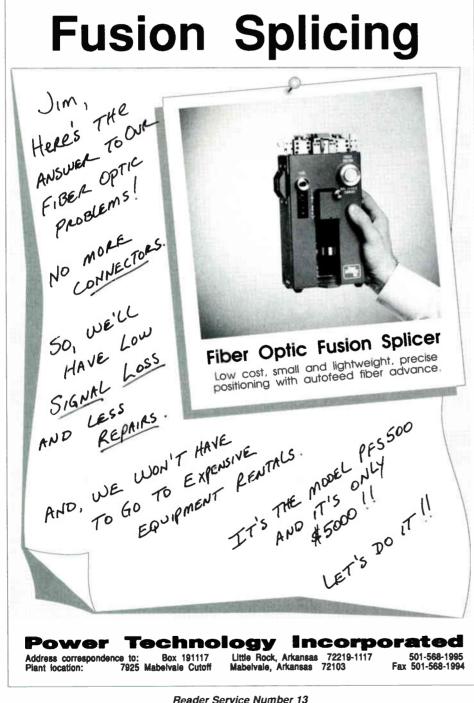
CableLabs files complaint to ATSC

WASHINGTON, D.C. — Cable Television Laboratories' general counsel filed a letter of grievance to the Advanced Television Systems Committee, which has a subgroup for creating a voluntary standard for a ghost-cancellation reference signal.

The complaint concerns the editing of the six-page report CableLabs submitted to the ATSC highlighting the Labs' view of the ghost-cancelling test procedure and test results. According to the letter, the ATSC edited Cable-Labs' submission "without the authorization of CableLabs, and in spite of its direct objection." The letter goes on to say "the editing done distorts the intent and meaning of CableLabs' report."

Galaxy V launches

LOS ANGELES — Eight days following its March 13 launch, Galaxy V, Hughes Communications' next-generation cable-dedicated satellite, was successfully deployed in geosynchronous orbit. Galaxy V's final birth is at 125° WL. As



well, Hughes' Westar V satellite was set to end service on May 1 and subsequently be retired. (For a list of the programmers set to occupy Galaxy V along with a wall chart of the latest data on U.S. C-band birds, see last month's issue of *CT*, page 45.)

In other Hughes news, the company contracted with Thomson Consumer Electronics and News Datacom to provide the transmission system, encryption system and initial consumer receiving units for its DirecTv entertainment distribution system. According to Hughes, the system will be capable of providing over 100 channels to 18-inch antennas installed at consumers' homes across the country in 1994.

TCI/McCaw do PCS trial

ASHLAND, Ore. — TCI and McCaw Cellular began a market trial of a residential microcellular service here. The trial, promoted as the Ashland Personal Telephone Service, is said to be the first in the country to sell a combined residential/local wireless service to the public.

The test is set to last six months and 200 area residents are participating. They will be able to make and receive calls to and from anywhere in the greater Ashland community.

Magnavox changes name

MANLIUS, N.Y. — Magnavox CATV Systems changed its name to Philips Broadband Networks Inc. as of April 6. The change was said to reflect "enhanced commitment from its parent company, Philips N.V." (Magnavox CATV has been a division of Philips since 1974.) The Magnavox name, however, will not become a CATV label of the past; PBN's distribution products will continue to bear the Magnavox moniker.

Pico sues over patent infringement

LAKEVIEW TERRACE, Calif. — Pico Products announced it's suing Northeast Filter Co. for breach of contract and patent infringement. Pico says Northeast's license under Pico's patent to make and sell certain encoding and positive trapping devices had been terminated for failure to pay royalties. As well, a license agreement under the same patent with Arrow Communications Labs has been terminated. Eagle Comtronics and Production Products are still authorized to use Pico's patent.

COMMUNICATIONS TECHNOLOGY

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SIECOR	-20°C to +70°C		•	•			50	144	36	24	3-4 weeks
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COMPANY X	-20°C to +80°C		•				?	?	?	?	?
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Reader Service Number 14

SCTE NEWS

Society elects new board members

EXTON, Pa. — March 28, 1992, marked the official closing of the Society of Cable Television Engineers' annual election to fill empty seats on its 1992-93 board of directors. The results of this year's election are as follows:

At-Large: Tom Elliot, Tele-Communications Inc., representing the entire United States

Region 3: Norrie Bush, Columbia Cable, representing Alaska, Idaho, Montana, Oregon and Washington

Region 4: Wayne Hall, Warner Cable, representing Oklahoma and Texas **Region 5:** Mark Wilson, Multimedia, rep-

resenting Illinois, Iowa, Kansas, Missouri and Nebraska

Region 7: Terry Bush, Trilithic Inc., representing Indiana, Michigan and Ohio Region 8: Jack Trower, WEHCO Video, representing Alabama, Arkansas, Louisiana, Mississippi and Tennessee Region 10: Mike Smith, Adelphia Cable, representing Kentucky, North Carolina, Virginia and West Virginia **Region 12:** Walt Ciciora, Ph.D., American Television & Communications, representing Connecticut, Massachusetts, Maine, New Hampshire, New York, Rhode Island and Vermont

They will join the following seven SCTE board members currently serving their 1991-1993 terms:

At-Large: Wendell Bailey, National Cable Television Association, representing the entire United States At-Large: Richard Covell, Texscan, representing the entire United States **Region 1:** Tom Elliott, Catel, representing California, Hawaii and Nevada **Region 2:** Ron Hranac, Coaxial International, representing Arizona, Colorado, New Mexico, Utah and Wyoming

Region 6: Rich Henkemeyer, Paragon Cable, representing Minnesota, North Dakota, South Dakota and Wisconsin

Region 9: Jim Farmer, Scientific-Atlanta, representing Florida, Georgia and South Carolina

Region 11: Diana Riley, Jerry Conn

Associates, representing Delaware, Maryland, New Jersey and Pennsylvania

In addition, the referendum vote proposed by the board of directors to change the titles of the Society's officers passed.

Fake ballots caught in election

EXTON, Pa. — Unfortunately, a problem was recently detected with this year's Society of Cable Television Engineers election. DLS Accounting Services, the accounting firm retained by the board since 1987 to tabulate national elections, discovered fraudulent ballots among the legitimate votes using a security process initiated several years ago by SCTE national headquarters.

After consultation with SCTE's attorney, DLS began working with paper experts at the print shop that produced the election package to carefully examine each ballot in order to purge the election of invalid votes. This separation was accurately accomplished by comparing the differences in ink density,





14 MAY 1992

COMMUNICATIONS TECHNOLOGY

Knock echoes clean out of your system!

Until now, cable operators had to fight with the positioning of their antennas and delay lines to stop echoes from impairing their customer's television reception. The VECTOR Video Echo Canceler from Philips Broadband Networks changes that by knocking out even complex echo artifacts from off-air channels quickly, economically and reliably.

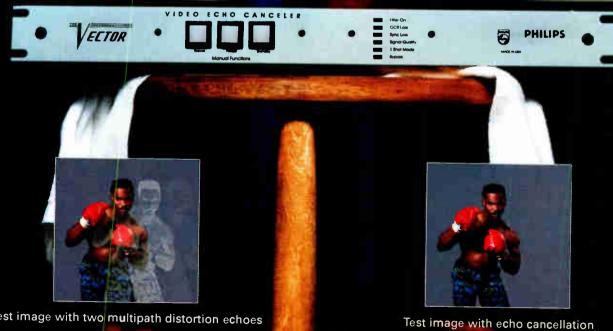
Based on a revolutionary new technology and manufactured in the USA by Philips Broadband Networks, VECTOR utilizes a unique "Ghost Cancelation Reference" (GCR) signal. Declared the clear winner and undisputed champion in recent field tests conducted by the NAB, the Philips GCR took on the challenge to clean up ghosted signals better than all contenders.

With up to seventy-five percent of TV viewers currently experiencing some degree of ghosting, VECTOR is destined to become a heavyweight champion of picture quality improvment in your headend. It operates automatically, continuously and spectacularly allowing you to provide your subscribers with much higher quality, ghost-free signals.

So, if you've been hit by customers complaining of ghosting, strike back! Ask your Philips Broadband Networks representative about our newest Technical Knock Out .

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For more information contact: Philips Broadband Networks, Inc. (formerly Magnavox CATV Systems) 100 Fairgrounds Drive, Manlius, NY 13104 Ph: (315) 682-9105, Fax: (315) 682-9006 Call 1-800-448-5171 (in NY State 1-800-522-7464)



Test image with two multipath distortion echoes

Philips Broadband Networks, Inc.





Reader Service Number 16

print quality and raw paper stock. As a result, DLS and the print shop provided SCTE's board of directors at its March 23 meeting with written testimony of their evaluation process, which resulted in a calculated accuracy exceeding 99 percent.

Upon carefully reviewing the testimony and also establishing that all individual elections were decided by differences outside this possible margin of error, the board voted to certify the election. (All candidates currently on the board abstained from the vote.) It was only then that the preliminary standings of the candidates running in the election were announced. The board then voted unanimously to conduct further investigations to identify the individual(s) responsible. It also directed the national headquarters staff to increase security measures in order to maintain the intearity of future elections.

The board then called a meeting on April 7 to discuss further action regarding the invalid ballots cast during the election. The board voted to offer amnesty from legal prosecution to the individual(s) responsible should that individual(s) come forward and contact the Society before April 27, 1992.

If the perpetrator(s) was to come

16

forward, that individual(s)'s name would not be made public by SCTE, no criminal prosecution would be initiated by the Society and the individual(s) would be dealt with in accordance with the Society's national bylaws.

The board then voted unanimously to conduct a full investigation into the election fraud if the person(s) responsible did not come forward by April 27. If the responsible individual(s) is identified as a result of the investigation, SCTE will prosecute to the fullest extent of the law and shall seek restitution for all costs of private investigators, document experts, legal counsel and other related expenses.

During the meeting, the board also created an Ad-Hoc Oversight Subcommittee comprised of both board and nonboard members to act as observers during the investigative process in order to ensure a fair and impartial investigation.

Newly elected directors will officially take their seats at the next SCTE board meeting, scheduled to be held Saturday, June 13, prior to Cable-Tec Expo '92 in San Antonio, Texas.

Technology Update '92 to be held in New York

LAKE GEORGE, N.Y. - The Society of

Cable Television Engineers, along with the New York State Commission on Cable Television, is sponsoring Technology Update '92 — the 18th annual northeast technical seminar and trade show — here from May 18-20.

Included will be a wide variety of technical sessions. Sessions are as follows:

• "How to establish in-house installer training" with Ralph Haimowitz, SCTE

• "Secrets of digital band compression" with Walt Ciciora, American Television & Communications

• "Consumer service through service call reduction" with Joe Van Loan, Cablevision Industries

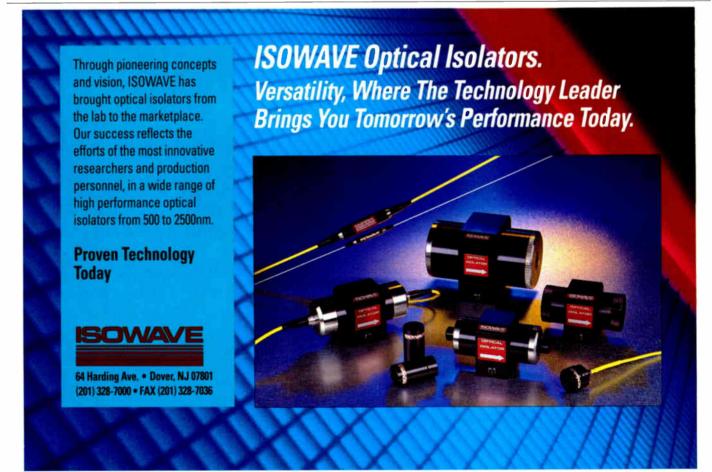
• "New technical standards" with Wendell Bailey, National Cable Television Association

• "Beyond AM fiber" with John Holobinko, American Lightwave

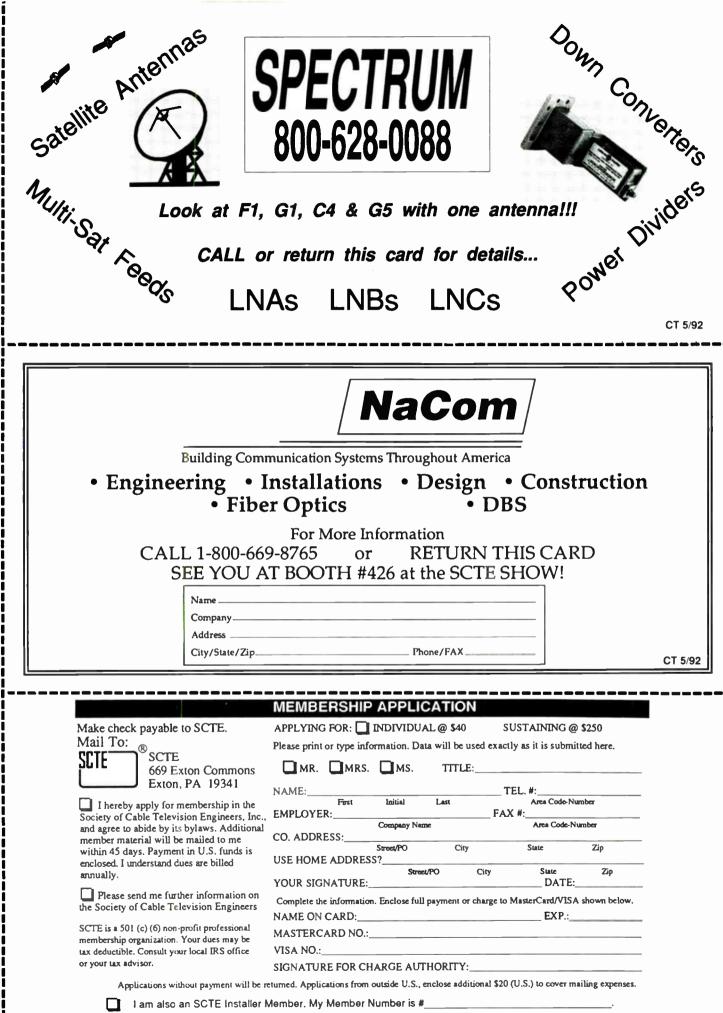
• "Overview of digital applications" with Tom Staniec, NewChannels Corp.

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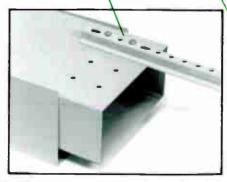
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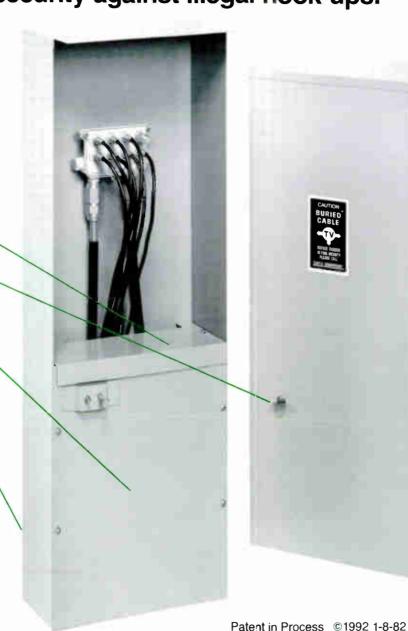
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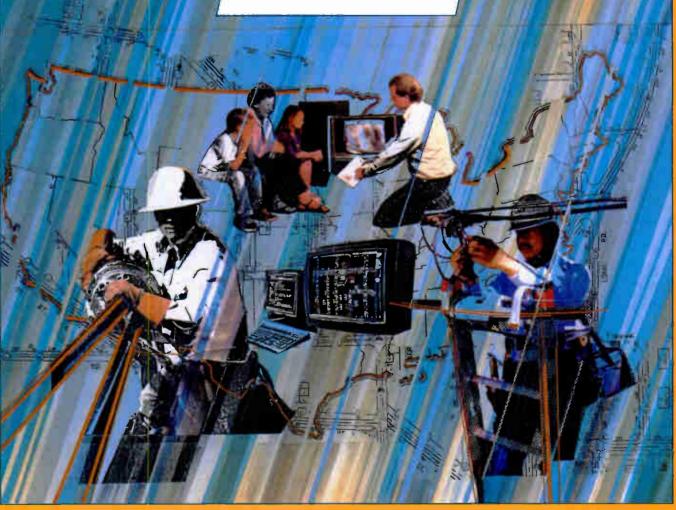




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Compression and its impact on cable

By Vito Brugliera

Vice President of Marketing & Product Planning Zenith Cable Products Division Zenith Electronics Corp.

convergence of technological and marketing forces is resulting in a dramatic change of the cable TV business. The number of programmers is steadily increasing the choices available to operators and subscribers. This expansion of choice, the growth of the videocassette rental market and the lengthened release window for films available to cable has reduced the growth of premium pay services.

As a consequence, the premium pay services are experimenting with different approaches. One of these is multiplexing, or running the same repertoire of movies on several channels. The number of movies in the library is the same. Near-video-on-demand (NVOD) pay-perview (PPV) will give subscribers more options and variety in viewing a movie. As all of this has been happening, technology has been steadily advancing. Cable plant is being extended beyond typical 350 MHz and 450 MHz bandwidths, with some systems to 1 GHz. Channel availability is being extended as programming options increase.

Transponder shortage

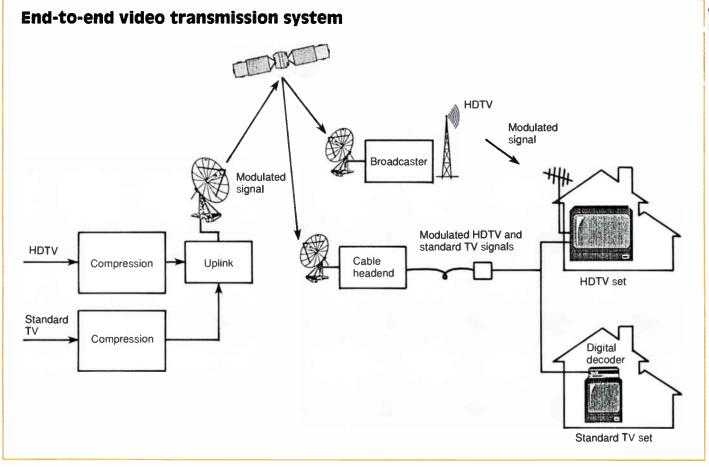
One portion of the cable distribution infrastructure has not kept pace. Satellite transmission facilities have lagged behind cable plant and programming expansion. A potential scarcity of satellite transponder capacity is developing.

Technology advances will alleviate this developing transponder shortage. The effort to develop a terrestrial high definition TV (HDTV) broadcast standard has advanced digital compression technology, making it possible to compress multiple NTSC TV programs into the 6 MHz occupied by a conventional NTSC signal. CableLabs, in conjunction with a major operator and programmer, has issued a request for proposal for satellite transmission equipment to compress satellite-delivered signals. It is anticipated that within a year, equipment will be available for compression of satellite-delivered NTSC signals.

Digital video compression technology offers an alternative to bandwidth extension of cable plants, which usually implies a plant rebuild. Digital technology requires less signal power and by operating compressed signals at the upper end of the cable plant spectrum, it will be possible to extend the viable bandwidth of the plant to regions unusable for conventional NTSC signals. As a result:

• Signal bandwidth is extended electronically.

• Compressed signals are concen-



trated at one end of the signal bandwidth.

• Conventional plant operation remains for the prior bandwidth.

• A new tier of services becomes available to subscribers.

• Only these subscribers receive decoders for decompressing signals.

• Even more bandwidth and channels are available by physically rebuilding the plant.

What we have now is a seamless expansion path for new services the additional channel capacity provides. The unanswered question is: "Is there enough business and revenue to justify the cost?" The next year will provide an answer as new services such as NVOD are tested.

This technological opportunity is not just limited to cable. Terrestrial services such as MMDS and over-the-air broadcasters also could avail themselves of the technology and, as a result of the extended channel capacity, become more viable competitors.

Another class of competition will come from direct broadcast satellite (DBS) services. The technology was originally developed for satellite transmission and all that is required is a subscriber terminal instead of a headend terminal.

4

Another catalyst for additional channel capacity will be the diffusion of HDTV services from terrestrial, satellite and cable programmers. The FCC has placed a time window within which deployment of HDTV transmission is required or the terrestrial broadcaster will lose its additional channel. Under the most stringent mustcarry scenario, cable operators will be required to carry these additional HDTV channels, thereby reducing their channel capacity for existing services.

Advantage of choice

Cable's most salient advantage from a subscriber's point of view has been choice. Compression will allow satellite services expanded channel capacity and increase options for choice. This will diminish the differentiation between cable and satellite. An effective way for cable to maintain a competitive edge is to increase channel capacity and choice of services.

Comparison of modulation approaches4-VSB16-QAM32-QAMData
Number of data levels446Theoretical relative data rate1*11.25Ruggedness

Ruggedness Functions in all existing cable plants Adds channels in bandwidth roll-off region Continuous wave interference rejection Phase-noise rejection Forward error correction Required C/N (without error protection)	Yes Yes Excellent Excellent Yes 22 dB	Yes Yes Good Good Yes 22 dB	No No Moderate Poor Yes 25 dB	No No Poor Poor Yes 28 dB	
Analog friendliness Coexistence with analog signals Composite triple beat rejection filter Signal acquisition with noise/interference Channel equalizer	Excellent Yes Excellent Yes	Good No Good Yes	Poor No Fair Yes	Poor No Fair Yes	
Cost Manufacturing complexity Cost of receiving equipment	Lowest Lowest	Low Low	Moderate Moderate	High High	

*Although, theoretically, all four-level approaches have the same relative data rate, the 4-VSB system uses a 21.5 megabit-per-second channel bit rate — greater than any announced four-level 6 MHz digital data transmission system.

The need for increased channel capacity already is evident with multiplexing by programmers. Programmers will be among the first to adopt HDTV signal formats as a competitive element in their marketing strategies. Programmers offering HDTV will not be costly to cable operators because: 1) there will be minimal capital outlays, 2) HDTV programming offers a competitive advantage, and 3) additional channel capacity is available in the roll-off portion of the cable spectrum and by using NTSC compressed signals elsewhere.

This will increase the need for additional channel capacity. As the addressable universe grows and revenues from PPV increase, additional channels will be needed for NVOD services.

Consumer friendliness

Another opportunity digital video signal compression offers the cable and consumer electronics industries is the creation of a truly user-friendly product along with a host of new services for subscribers.

NTSC signal transmissions will be with us for several decades because there are almost 170 million NTSC receivers in consumer homes and they will continue to be sold for decades. HDTV receivers will be dual receivers, capable of receiving and displaying both HDTV and NTSC signals. A settop terminal will be required to decode NTSC compressed signals for subscriber use on NTSC-only receivers.

64-QAM

8

1.5

There are two aspects to HDTV or NTSC compressed signals: transmission and compression. There are several different transmission modulation approaches for the proposed HDTV broadcast standard. The accompanying table compares various modulation techniques. It is quite conceivable, and in fact desirable, that a common transmission method be usable with both NTSC compressed and HDTV signals.

A modulation method known as 4-VSB can be used to transmit both HDTV and NTSC compressed signals. An advantage of the 4-VSB transmission system is its ruggedness. Cable plants with a marginal signal-to-noise ratio (36 dB) will have difficulty using 32/64 QAM transmission systems in the roll-off portions of their cable plant because the QAM systems are less rugged. The 4-VSB transmission system delivers digital information to the TV receiver decoder. The digital data packets can represent either a compressed HDTV signal or multiple NTSC compressed signals. The receiver will recognize which type of signal is present and convey the digital data to the HDTV decoder or a plug-in compressed NTSC decoder. This plug-in decoder would be provided by the cable oper-

(Continued on page 40)

COMMUNICATIONS TECHNOLOGY

Performance of digital modulation methods

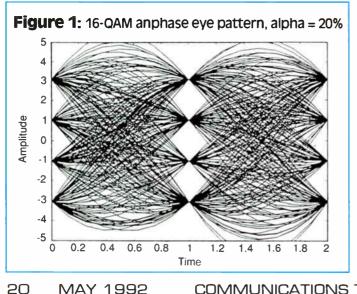
The following is used with permission of the National Cable Television Association. It is adapted from a paper that ran in the "1991 NCTA Technical Papers."

This article provides a brief overview of digital modulation techniques and the important parameters used in quantifying them, and discusses the major types of channel impairments and their effect on the signal as well as the effects of real (non-ideal) demodulator's performance. The specific modulation methods, QPSK, QPR, 16-QAM, and 4-VSB AM, modeled in this article are discussed. A description is provided of the simulation technique as well as the channel model it simulates. A model for a "typical" cable channel is discussed along with the performance variation that may be "typical" for a consumer-grade demodulator. Simulation results for this model are presented and discussed.

By Leo Montreuil Staff Engineer **And William Wall** Principal Scientist Scientific-Atlanta

ecently introduced new digital audio services and the promise of highly compressed digital video in the near future instigated this study of digital modulation methods for cable applications. Digital modulation offers many potential advantages over analog transmission such as better transmission power, more services in a given bandwidth, essentially perfect noise-free reproduction of the original source when above some threshold carrier-to-noise ratio (C/N), and unbreakable signal security. In order to utilize these potential advantages, a modulation method must be selected that provides reliable reception in a cable environment, a data rate appropriate for the service and economical demodulation in the subscriber's home.

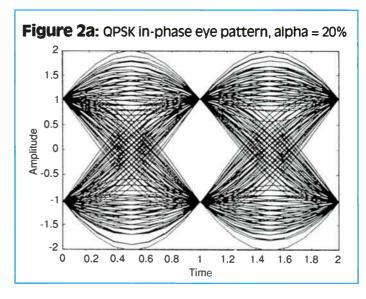
While numerous theoretical analyses of digital modula-

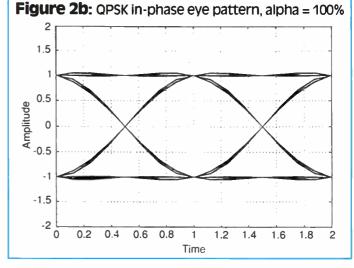


tion performance exist in the literature listed at the end of this article, a practical comparison under signal conditions typical of cable systems was not found. Further, a method for simulating specific channel conditions and measuring performance for a variety of modulation techniques with those specific channel conditions was desired. To that end, a computer simulation has been developed that accurately models digital modulation/demodulation methods in the time domain, adds a variety of controlled impairments and measures the resultant bit error rate. This simulation technique has been found to be highly accurate and greatly reduces the time to test system design changes as well as test competing modulation methods.

Methods of digital transmission

As a brief review, digital transmission is accomplished by modulating an RF carrier to a discrete value (or state)







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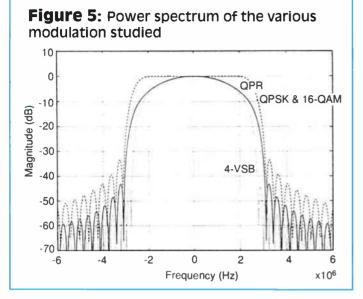
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Quadrature phase shift keying (QPSK) is a phase modulation technique that has four phase states per symbol located 90° apart. QPSK may be alternately described as a suppressed carrier AM technique where two independently AM modulated signal components in phase guadrature (90° apart) each have two amplitude states. These two components, known as the in-phase (I) and guadrature (Q) components are orthogonal and may be demodulated separately without mutual interference in the ideal case. Figure 3 on page 22 shows a phase state diagram for QPSK (alpha 20 percent) with the I axis horizontal and the Q axis vertical. The four areas of highest density are the four phase states: the remaining lines indicate the trajectories between phase states. With an alpha of 20 percent, QPSK can achieve a data rate of 10 Mbps in a 6 MHz bandwidth. The noise performance of QPSK is the best of any digital modulation technique.

By adding controlled ISI to QPSK, one can effectively generate a third level to each of the quadrature AM components such that the interpretation of that third-level depends on the estimate of the previous symbol state, creating a nine-state modulation format known as quadrature partial response (QPR). An eye diagram for one component of a QPR signal is shown in Figure 4 (page 22). QPR provides a higher bandwidth efficiency allowing a data rate of 12 Mbps in a 6 MHz channel bandwidth, with a slight

Table 1: Modulation parameters

Modulation QPSK	Data rate 10 Mbps	Transmit filter Square root raised cosine, alpha 20%	Receive filter Square root raised- cosine, alpha 20%, noise BW = 5 MHz
QPR BW,	12 Mbps	Partial response class 1	Maximally flat, 6 MHz noise BW = 6 MHz
16-QAM	20 Mbps	Square root raised cosine, alpha 20%,	Square root raised- cosine, alpha 20%, noise BW = 5 MHz
4-VSB AM	12 Mbps	Square root raised cosine, alpha 40%	Square root raised- cosine, alpha 40%, noise BW = 3 MHz

noise performance penalty.

Another modulation method is created by the encoding of two bits in four levels in each of the quadrature AM components that allows the transmission of a total of four bits per symbol. The 4x4 states gives a total of 16 states per symbol. Hence the name 16 state quadrature AM (16-QAM). Using an alpha of 20 percent, 16-QAM allows the transmission of 20 Mbps in a 6 MHz channel. Again the addition of the additional states degrades the noise performance.

Taking only the in-phase four-level AM component and transmitting it as vestigial sideband AM improves the bandwidth efficiency, allowing a data rate of 12 Mbps to be sent in a 6 MHz channel bandwidth. This technique, unlike the double sideband AM techniques, which allow reference carrier regeneration from the transmitted signal, requires the transmission of a carrier or pilot component for a reference carrier regeneration. Referred to as 4-VSB AM, the noise performance is similar to 16-QAM.

Qualitative effects of transmission impairment

There are six main processes that contribute to errors in the demodulated data: thermal noise, phase noise, ISI, timing errors, crosstalk between I and Q, and threshold errors. In most modulation methods thermal noise is gaussian and is additive to each state of a symbol. The demodulator will incorrectly estimate the modulation state if the noise caused the instantaneous received signal to be closer to another state than the actual transmitted state. The "tails" of a gaussian distribution extend far so that even at high signal-to-noise ratios (S/N) there is still a measurable error rate.

Clearly, for a given signal level, the fewer the states in a symbol, the greater the distance between states and the lower the probability of error. That is, the fewer bits per symbol, the better the noise performance. Similarly, the lower the noise bandwidth of the receive filter, the better the performance assuming that the filter causes no ISI.

Phase noise, either introduced in the transmission path by frequency converters or in the reconstructed reference carrier, degrades performance by introducing apparent thermal noise on the received symbol and by causing crosstalk between in-phase and quadrature components in a given symbol, which reduces the effective distance between states. ISI is caused by improper filtering or reflections within the transmission path causing previous symbols to interfere with the current symbol, again reducing

effective distance between symbol states ("closing the eye").

Nominally, the state estimate is made when the eye has the greatest opening, or the distance between states is the greatest. Timing errors in the clock recovery part of the demodulator cause the state estimate to be sampled either before of after the nominal time where the distance between states has been reduced, degrading the demodulator performance. Modulation techniques that use in-phase and quadrature AM components may be degraded by crosstalk between components that reduce effective distance between states. Similarly, static bias

(Continued on page 42)

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Reader Service Number 20

Using constellation analysis to diagnose digital transmission problems

By Joseph B. Waltrich Manager of Analog Programs And Marc Ryba

Data in

Senior Development Engineer Applied Media Lab, Jerrold Communications

he video waveform monitor is universally accepted as a tool for analyzing problems with analog video transmission. Impairments such as hum, field tilt, incorrect sync and/or chroma levels, undesirable transients and other problems are easily discernable. All of these impairments are observable via the waveform monitor's display of analog voltage vs. time. However, impairments to digital transmission are not easily observed on a voltage vs. time display.

Figure 2: Digital modulator block diagram

1 (2 bits)

Q (2 bits)

Symbol

generator

A/D

A/D

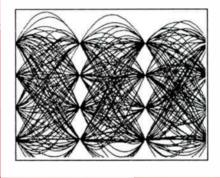
A time display of digital transmission results in an eye pattern, so called because of its resemblance to the human eye (as shown in Figure 1). All transmission impairments have the same resultant effect on this waveform. That is, they tend to "close the eye." Therefore, a more meaningful way of determining which impairments are present must be used. Constellation analysis provides such a tool.

Modulation review

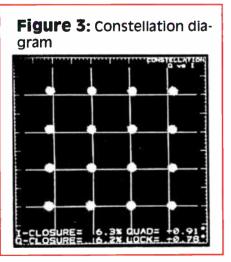
Cos (wt)

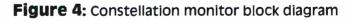
Sin (wt)

In order to understand constellation analysis, it is helpful to review the modulation process for digital transmission. A simplified block diagram of a digital modulator is shown in Figure 2. The Figure 1: 16-QAM eye diagram

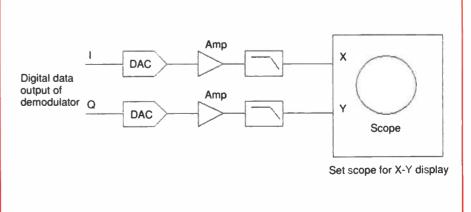


modulation scheme illustrated here is 16-QAM (16-level quadrature amplitude modulation) in which the input serial data stream is divided into groups of two bits and each two-bit group is converted to four analog levels, which are then modulated by in-phase and quadrature components of the carrier. The output of the modulator is the sum of the two modulated carriers. This gives a total of 16 possible combinations of transmitted data. If all of the possible data combinations are plotted in phase space (that is, the data on the quadrature carrier is plotted against the data on the in-phase carrier), the plot would look like that shown in Figure 3.

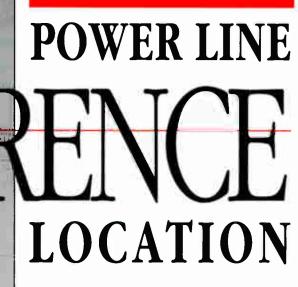




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Reader Service Number 21

Measuring the impact of fiber optics

The following article was originally prepared for the SCTE's Fiber Optics Plus '92 conference.

By Richard Rexroat

Director of Fiber-Optic Technology Tele-Communications Inc.

ithout a doubt, fiber-optic technology is one of the most significant advancements in cable TV distribution in recent years. It is a development that is going to pay immediate dividends and continue to pay dividends for many years to come.

Everyone in the industry is aware of the benefits or objectives involved in electing to install fiber optics:

• Enhance the quality of pictures delivered to subscribers.

• Increase the reliability of the distribution system.

• Decrease the cost of system maintenance.

• Provide the most cost-effective means to upgrade system bandwidth.

• Provide the most cost-effective means to rebuild systems that require complete change-out of electronics and cable.

• Provide an economical but technically superior method of consolidating multiple headends.

Yet there is even more to fiber. Optical technology has the capacity to reduce operational costs, as well as lay the foundation for a myriad of new business opportunities in the future. By installing fiber, operators are assured of having a technology in place that will fully support such services as personal communications networks, high definition TV, near-video-on-demand and alternate access.

Reducing trouble calls

When analyzing cost savings, we compared fiber-optic vs. conventional RF rebuilds and upgrades. Everyone knows that fiber optics can save money by reducing the amount of electronics in a system, eliminating expensive AML sites and consolidating headends.

However, fiber also saved money by reducing the amount of trouble calls and maintenance-related truck rolls. Overall maintenance will always decrease with fiber-optic transportation, simply because of the reduced number of active electronics used. However, maintenance for the headend, cumulative leakage index and converters are not affected. Drop-in backbone fiber installations also have little effect on maintenance.

On average, TCI systems deploying optical technology reduced trouble calls by 35 percent. Specific examples of how this was accomplished are:

• Pacifica, Calif. — The system ran fiber point-to-point from Pacifica to Millbrae. This run eliminated an 11-mile supertrunk containing 28 amplifiers. The reduced amount of electronics and elimination of related power problems accounted significantly for the reduction in trouble calls. As well, fiber optics generated a large number of calls from subscribers wanting to compliment us on the improved picture quality.

• Reno, Nev. — This system also did a point-to-point run from the earth station site to the distribution headend. From there, the system ran another fiber from the headend to an AML receiver site. By replacing the AML equipment with an optical node, subscriber calls related to AML rain fade were eliminated.

It is interesting to note that one system experienced a strange twist to fiber-optic deployment. At TCI's Bennettsville, N.C., system, average monthly trouble calls equaled 5.1 percent. Within six weeks of installing fiber, trouble calls were reduced to 2.1 percent. However, nine weeks after the installation, the trouble calls were back to 5 percent. After further investigation,

"Optical technology has the capacity to reduce operational costs, as well as lay the foundation for a myriad of new business opportunities in the future."

it was found the trouble calls were related to channels the system received off-air. Subscribers noticed that satellite channels were significantly better in quality than the off-air signals and felt fiber optics also would improve the offair signals delivered on their cable systems.

Difficult to quantify

Unfortunately, in most instances, it's difficult to obtain quantitative information concerning trouble calls and reduced maintenance. Many of the systems deploying fiber are too new for such data. This type of analysis is better performed after a full year of implementation. However, even without such information, the following conclusions can be made.

• By comparing conventional rebuild costs to fiber-optic builds, we can rebuild a system for \$2,000 to \$3,000 per mile less than a conventional RF system.

• When deploying fiber, TCI found that by reducing the number of amplifiers in cascade, it was possible to optimize the laser performance, trading distortion for noise. This is basically a confirmation of statements made three years ago when the industry first considered fiber optics.

• At this point, cost reductions related to powering cannot be determined simply because systems: 1) must be metered, 2) contain different amperage levels and 3) generally havemore power supplies, but they operate more efficiently.

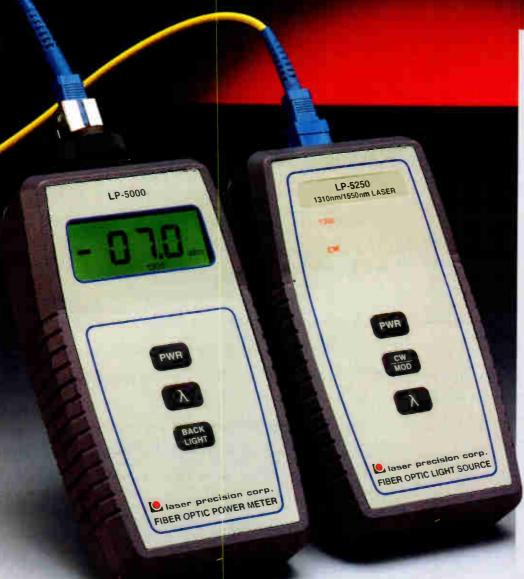
• To date, we have found 2,500 to 3,000 homes per node provide the optimum cost benefit when deploying fiber optics. In the future, it may be necessary to go down to 1,000 homes per node, or possibly even 250 homes per node. Yet, when building, TCI decided to avoid this scenario for today's systems. Instead, it has developed a migration path for new services that will allow the room to expand if necessary.

How far do we push lasers?

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Fiber troubleshooting and emergency restoration

By K. Charles Mogray Jr.

Start

Measure

received

power

Measure

transmitter

output power

Applications Engineering Manager, Comm/Scope Inc.

he process of troubleshooting a fiber-optic cable system begins by identifying the component that has failed. This is normally done by a logical process of elimination. The four major components of a fiber system are the transmitter, receiver, patch cords/pigtails/connectors and the fiber-

Acceptable

Too low

Cable troubleshooting/fault locating

Diagnose

Rx and/or

electronics

optic cable. Table 1 shows typical faults with these components and what to do about them. Using a power meter and an optical time domain reflectometer (OTDR), most failures can be quickly identified. Unfortunately, the repairs and/or replacements may not be so auick.

The flow figure (below) shows how to troubleshoot and locate faults in a fiber system. The process begins by

Diagnose

Тx

measuring the output power of the transmitting device. This is usually measured directly at the output connector/sleeve of the transmitter using an optical power meter. Received power is compared to that recorded when the equipment was installed and as specified by the equipment manufacturer.

consists of checking output power through any patch cords/sleeves installed at the transmit end of the fiber system. Patch cords, pigtails, connectors and/or sleeves may be defective or damaged and should be replaced by substitution using a unit that is known to be good. Again, assuming measured power is within installed or specified values, the next step is to go to the receive end of the fiber system and measure received power through the passive fiber cable system.

Using the same process of elimination, received power is checked with an optical power meter through the patch cords/sleeves up to the receiver. If measured power is within specification, then it is safe to assume that the problem is in the receiving equipment.

Cable problem

If the process of elimination indicates that the fiber-optic cable is the problem, then an OTDR or other test device is required to pinpoint the fault. When using an OTDR, do not confuse

The next step

(Continued on page 53)

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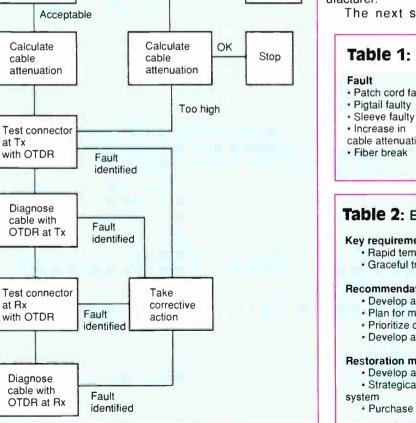


 Table 1: Typical fiber cable system faults

· Patch cord faulty

cable attenuation

Cause Dirt or damage Dirt or Damage Dirt or damage Kinked/damaged cable or splice point Kinked/damaged cable or splice point

Solution Clean or replace Clean or replace Clean or replace Re-splice or replace

Re-splice or replace

Table 2: Emergency restoration of fiber system

Key requirements:

- Rapid temporary restoration
- Graceful transition to permanent repair

Recommendations:

- Develop a plan for emergency restoration
- Plan for material, equipment and labor for emergency restoration
- Prioritize circuits for re-splicing
- · Develop a plan for permanent repair

Restoration materials and equipment:

- · Develop a list of required materials and equipment
- Strategically locate required materials and equipment throughout

Purchase (or make) an emergency restoration kit

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Find that fiber!

By Norman L. Elsasser Marketing Development Manager 3M Telecom Markets Division

t's 1995 and a technician who works for a major northeastern U.S. cable TV company is dispatched to initiate cable service for the owners of a newly constructed home in a planned residential development on the outskirts of Boston. In 1989, when the land for the subdivision was surveyed, parcelled into lots and excavated for the utility infrastructure of electric power, cable TV and telephone service to the 925 individual houses planned in the suburban development hard recessionary times fell on the area. Long before the first house was built, the property went into foreclosure.

As the recession eased and construction began to increase in the region, new houses were built in the subdivision, and then it was time to turn on utility services. Arriving at the subdivision, the technician finds a jumble of cables in the route, each containing 12 bundles of eight optical fibers. Looking for "Bundle 11, Yellow" has become a confusing task. To make matters worse, the colors have faded and it's difficult to distinguish the red fibers from the yellow.

The fiber boom

Since 1989, optical fiber has been going into service at an unprecedented rate. In many areas, fiber is being installed in new residential and commercial construction projects long before the structures are built on lot sites. Technicians are dispatched to initiate cable service months and sometimes years after the utility infrastructure is installed.

As more optical fiber cable goes into service, the ability to identify, test and maintain individual fibers has become more critical. Because optical fibers carry so much traffic, misidentification of individual fibers can result in staggering costs if service is interrupted. Complicating the picture is the fact that fiber-optic system designs have become increasingly complex.

Now, when the cable system for a new housing development is designed, for example, the optical fibers are bundled into groups within the cable, and "drops" are made at each lot. Systems are designed to go from points A to Z, with drops made along the way at points C, G, K, N and so on. Later, when construction is finished, the CATV technician returns to initiate service for the new customers.

Further, routes today may contain cables with 144 fibers — or 12 bundles of 12 color-coded fibers. So when a technician goes out into the field to activate one of the spare live fibers, he must identify which of the colored and bundled fibers is the correct one.

Critical business of identifying fibers

There are several factors that make the potential for misidentification high: the difficulty in distinguishing between light and dark fibers; a high potential for breaking fibers in the process of identification; the fact that the coloring used to code individual fibers may fade over time; and the possibility of contamination of the test equipment itself. Let's detail each of these problems:

Light vs. dark. Risks that the technician faces here include identifying the wrong fiber as dark when it may in fact be light — and could be transmitting up to 54 broadband channels. Fibers are carrying critical traffic, so it could cost many thousands of dollars if a fiber is shut down by mistake. Therefore, the need to accurately identify individual fibers is becoming increasingly critical and pervasive as the installation of optical fiber proliferates and fiber counts increase.

Accidental breakage. There is high potential for breakage or fatiguing of the fibers during the process of identification and testing because of the fragility of fiber strands. With many fiber identification test instruments, technicians use triggers or buttons to clip onto the fiber. The force applied varies among technicians — some push the trigger with more force than others — and excessive force can break or fatigue the fiber.

Fading of color. As fiber-optic cables age, the dyes used to originally colorcode individual fibers fade. Generally, the dyes begin to pale, making it difficult to distinguish between yellows and reds, and blues and greens.

Test instrument sensitivity. Another

"As usage of CATV fiber systems becomes more prevalent, it is evident that a more sensitive identifier is needed."

problem technicians encounter in trying to identify live fibers involves the optical sensitivity, or dynamic range, of the identifying equipment. Many instruments are unable to pick up low-level signals and indicate that a fiber is dark when in fact it may be operational.

Test instrument contamination and/or malfunction. The reliability of test instruments is critical in identifying optical fibers. If the test instrument is malfunctioning, or if the signal detection electronics in the unit have been contaminated with dust particulates from the atmosphere, there is high potential for misreading light fibers.

Equipment designed to overcome problems

As more and more fiber goes into service, the demand from cable companies has accelerated recently for identification and test instruments that are accurate and reliable, and technician-friendly.

Manufacturers of identification and test equipment for fiber optics seek to minimize the problems associated with fiber identification through new designs and use of software technology. Since optical fiber identification is a relatively new science, particularly in the field environment, much of the equipment developed in the late 1980s lacked certain capabilities required for accurate testing of light fibers, in the following areas:

Optical sensitivity or "dynamic range." Many of the test instruments on the market since the late 1980s contained detectors that were not sensitive enough to pick up low-level signals in a fiber.

Clipping mechanisms. Accidental breaking or fatiguing of the fiber is a major risk with equipment that contains a lever or clipping device because the

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FCC report and order: The new rules for cable TV

If buying a new copy of the "Code of Federal Regulations" is not in your budget, here's all the changes to Part 76 applicable to cable TV, taken from Appendix C of the Federal Communications Commission report and order on cable TV technical and operational requirements adopted Feb. 13, 1992 (released March 4, 1992).

Part 76 of Chapter I of Title 47 of the *Code of Federal Regulations* is amended to read as follows:

1. Section 76.5 is amended by adding paragraph (jj) to read as follows:

§ 76.5 Definitions.

* * * * *

(jj) Rural Area. A community unit with a density of less than thirty households per route mile of coaxial and/or fiber optic cable trunk and feeder line.

* * * * *

2. Section 76.305 is amended by revising paragraphs (a) and (c) to read as follows:

§ 76.305 Records to be maintained locally by cable system operators for public inspection.

(a) Records to be maintained. The operator of every cable television system having 1,000 or more subscribers shall maintain for public inspection a file containing a copy of all records which are required to be kept by § 76.205(d) (origination cablecasts by candidates for public office); § 76.221(f) (sponsorship identifications); § 76.79 (EEO records available for public inspection); § 76.601(c) (proof-of-performance test data); and § 76.601(e) (signal leakage logs and repair records).

* * * * *

(c) The records specified in paragraph (a) of this section shall be retained for the period specified in \$76.205(d), 76.221(f), 76.79, 76.601(c), and 76.601(e), respectively.

* * * * *

3. Section 76.601 is amended by revising paragraphs (a) and (b), adding paragraphs (c), (d) and (e), and by deleting the concluding note. It is to read as follows:

§ 76.601. Performance tests.

(a) The operator of each cable television system shall be responsible for insuring that each such system is designed, installed, and operated in a manner that fully complies with the provisions of this subpart. Each system operator shall be prepared to show, on request by an authorized representative of the Commission or the local franchiser, that the system does, in fact, comply with the rules.

(b) The operator of each cable television system shall maintain at its local office a current listing of the cable television channels which that system delivers to its subscribers.

(c) The operator of each cable television system shall conduct complete performance tests of that system at least twice each calendar year (at intervals not to exceed seven months), unless otherwise noted below, and shall maintain the resulting test data on file at the operator's local business office for at least five (5) years. The test data shall be made available for inspection by the Commission or the local franchiser, upon request. The performance tests shall be directed at determining the extent to which the system complies with all the technical standards set forth in § 76.605(a) and shall be as follows:

(1) For cable television systems with 1,000 or more subscribers but with 12,500 subscribers or less, proof-ofperformance tests conducted pursuant to this section shall include measurements taken at no less than six (6) widely separated points within each mechanically continuous set of cables within the cable television system. Within the cable system, one additional test point shall be added for every ad-

ditional 12,500 subscribers or fraction thereof (e.g., 7 test points if 12,501 to 25,000 subscribers; 8 test points if 25,001 to 37,500 subscribers, etc.). Such proof-of-performance test points shall be balanced to represent all geographic areas served by the cable system. Within each mechanically continuous set of cables, at least one-third of the test points shall be representative of subscriber terminals most distant from the system input in terms of cable length. The measurements may be taken at convenient monitoring points in the cable network: Provided, that data shall be included to relate the measured performance of the system as would be viewed from a nearby subscriber terminal. An identification of the instruments, including the makes, model numbers, and the most recent date of calibration, a description of the procedures utilized, and a statement of qualifications of the person performing the tests shall be set forth.

(2) Proof-of-performance tests to determine the extent to which a cable television system complies with the standards set forth in § 76.605(a)(3), (4), and (5) shall be made on each of the NTSC or similar video channels of that system. Proof-of-performance tests for all other standards in § 76.605(a) shall be made on a minimum of four (4) channels plus one additional channel for every 100 MHz, or fraction thereof, of cable distribution system upper frequency limit (e.g., 5 channels for cable television systems with a cable distribution system upper frequency limit of 101 to 216 MHz; 6 channels for cable television systems with a cable distribution system upper frequency limit of 217 to 300 MHz; 7 channels for cable television systems with a cable distribution upper frequency limit of 300 to 400 MHz, etc.). The channels selected for testing must be representative of all the channels within the cable television system.

(3) The operator of each cable television system shall conduct semi-annual proof-of-performance tests of that system, to determine the extent to which the system complies with the technical standards set forth in § 76.605(a)(4) as follows. The visual sig-

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nal level on each channel shall be measured and recorded, along with the date and time of the measurement, once every six hours (at intervals of not less than five hours or no more than seven hours after the previous measurement), to include the warmest and the coldest times, during a 24-hour period in January or February and in July or August.

(4) The operator of each cable television system shall conduct triennial proof-of-performance tests of that system to determine the extent to which the system complies with the technical standards set forth in § 76.605(a)(11), (12), and (13).

(d) Successful completion of the performance tests required by paragraph (c) of this section does not relieve the system of the obligation to comply with all pertinent technical standards at all subscriber terminals. Additional tests, repeat tests, or tests involving specified subscriber terminals may be required by the Commission or the local franchiser to secure compliance with the technical standards.

(e) The provisions of paragraphs (c) and (d) of this section shall not apply to any cable television system having fewer than 1,000 subscribers: Provided, however, that any cable television system using any frequency spectrum other than that allocated to over-the-air television and FM broadcasting (as described in § 73.603 and § 73.201) is reguired to conduct all tests, measurements and monitoring of signal leakage that are required by this subpart. A cable television system operator complying with the monitoring, logging and the leakage repair requirements of § 76.614, shall be considered to have met the requirements of this paragraph. However, the leakage log, shall be retained for five years rather than the two years prescribed in § 76.614.

* * * * *

4. Section 76.605 is amended by revising paragraphs (a) and (b), by revising Note (1), by renaming Note (2) as Note (3) and by adding a new Note (2). It is to read as follows:

§ 76.605 Technical Standards.

(a) As of [6 months and 90 days following publication in the Federal Register], unless otherwise noted, the following requirements apply to the performance of a cable television system as measured at any subscriber terminal with a matched impedance at the termination point or at the output of the modulating or processing equipment (generally the headend) of the cable television system or otherwise as noted. The requirements are applicable to each analog NTSC or similar video downstream cable television channel in the system:

(1) The cable television channels delivered to the subscriber's terminal shall be capable of being received and displayed by TV broadcast receivers used for the off-the-air reception of TV broadcast signals, as authorized under Part 73 of this chapter.

(2) The aural center frequency of the aural carrier must be 4.5 MHz ±5 kHz above the frequency of the visual carrier at the output of the modulating or processing equipment of a cable television system, and at the subscriber terminal.

(3) The visual signal level, across a terminating impedance which correctly matches the internal impedance of the cable system as viewed from the subscriber terminal, shall not be less than 1 millivolt across an internal impedance of 75 ohms (0 dBmV). Additionally, as measured at the end of a 100 foot cable drop that is connected to the subscriber tap, it shall not be less than 1.41 millivolts across an internal impedance of 75 ohms (+3 dBmV). (At other impedance values, the minimum visual signal level, as viewed from the subscriber terminal, shall be the square root of 0.0133(Z) millivolts and, as measured at the end of a 100 foot cable drop that is connected to the subscriber tap, shall be 2 times the square root of 0.00662(Z) millivolts, where Z is the appropriate impedance value.)

(4) The visual signal level on each channel shall not vary more than 8 decibels within any six-month interval which must include four tests performed in six-hour increments during a 24-hour period in July or August and a 24-hour period in January or February, and shall be maintained within:

(i) 3 decibels (dB) of the visual signal level of any visual carrier within 6 MHz nominal frequency separation;

(ii) 10 dB of the visual signal level on any other channel on a cable television system of up to 300 MHz of cable distribution system upper frequency limit, with a 1 dB increase for each additional 100 MHz of cable distribution system upper frequency limit (e.g., 11 dB for a system at 301-400 MHz; 12 dB for a system at 401-500 MHz, etc.); and

(iii) A maximum level such that signal degradation due to overload in the subscriber's receiver or terminal does not occur.

(5) The rms voltage of the aural signal shall be maintained between 10 and 17 decibels below the associated visual signal level, and shall be maintained at levels not to cause interference to the upper adjacent channel. This requirement must be met both at the subscriber terminal and at the output of the modulating and processing equipment (generally the headend).

(6) The amplitude characteristic shall be within a range of ± 2 decibels from 0.75 MHz to 5.0 MHz above the lower boundary frequency of the cable television channel, referenced to the average of the highest and lowest amplitudes within these frequency boundaries.

(7) The ratio of RF visual signal level to system noise shall be as follows:

(i) From [90 days following publication in the Federal Register to 1 year thereafter], shall not be less than 36 decibels.

(ii) From [1 year and 90 days following publication in the Federal Register to 2 years thereafter], shall not be less than 40 decibels.

(iii) As of [3 years and 90 days following publication in the Federal Register], shall not be less than 43 decibels.

(iv) For class I cable television channels, the requirements of paragraphs (a)(7)(i), (a)(7)(ii) and (a)(7)(iii) of this section are applicable only to:

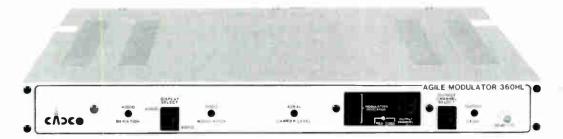
(A) Each signal which is delivered by a cable television system to subscribers within the predicted Grade B contour for that signal;

(B) Each signal which is first picked up within its predicted Grade B contour;

(C) Each signal that is first received by the cable television system by direct video feed from a TV broadcast station, a low power TV station, or a TV translator station.

(8) The ratio of visual signal level to the rms amplitude of any coherent dis**AGILE PLUS**

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turbances such as intermodulation products, second and third order distortions, or discrete-frequency interfering signals not operating on proper offset assignments shall be as follows:

(i) The ratio of visual signal level to coherent disturbances shall not be less than 51 decibels for noncoherent channel cable television systems, when measured with modulated carriers and time averaged; and

(ii) The ratio of visual signal level to coherent disturbances which are frequency-coincident with the visual carrier shall not be less than 47 decibels for coherent channel cable systems, when measured with modulated carriers and time averaged.

(9) The terminal isolation provided to each subscriber terminal:

(i) Shall not be less than 18 decibels. In lieu of periodic testing, the cable operator may use specifications provided by the manufacturer for the terminal isolation equipment to meet this standard; and

(ii) Shall be sufficient to prevent reflections caused by open-circuited or short-circuited subscriber terminals from producing visible picture impairments at any other subscriber terminal.

(10) The peak-to-peak variation in visual signal level caused by undesired low frequency disturbances (hum or repetitive transients) generated within the system, or by inadequate low frequency response, shall not exceed 3 percent of the visual signal level.

As of [3 years and 90 days following publication in the Federal Register], the following requirements apply to the performance of the cable television system as measured at the output of the modulating or processing equipment (generally the headend) of the system:

(11) The chrominance-luminance delay inequality or chroma delay, which is the change in delay time of the chrominance component of the signal relative to the luminance component after passing through the system, shall be within 170 nanoseconds.

(12) The differential gain for the color subcarrier of the television signal, which is measured as the difference in amplitude between the largest and smallest segments of the chrominance

signal (divided by the largest and expressed in percent), shall not exceed ±20%.

(13) The differential phase for the color subcarrier of the television signal which is measured as the largest phase difference in degrees between each segment of the chrominance signal and reference segment (the segment at the blanking level of 0 IRE), shall not exceed ± 10 degrees.

(14) As an exception to the general provision requiring measurements to be made at subscriber terminals, and without regard to the type of signals carried by the cable television system, signal leakage from a cable television system shall be measured in accordance with the procedures outlined in § 76.609(h) and shall be limited as follows:

Frequencies	Sig nal leakage limit (μV/m)	Distance in meters
Less than and including 54 MHz, and over 216 MHz	15	30
Over 54 up to and including 216 MHz	20	3

(b) Cable television systems distributing signals by using methods such as nonconventional coaxial cable techniques, noncoaxial copper cable techniques, specialized coaxial cable and fiber optical cable hybridization techniques or specialized compression techniques or specialized receiving devices, and which, because of their basic design, cannot comply with one or more of the technical standards set forth in paragraph (a) of this section. may be permitted to operate: Provided, that an adequate showing is made pursuant to § 76.7 which establishes that the public interest is benefited. In such instances, the Commission may prescribe special technical requirements to ensure that subscribers to such systems are provided with an equivalent level of good quality service.

Note 1: Local franchising authorities of systems serving fewer than 1,000 subscribers may adopt standards less stringent than those in § 76.605(a). Any such agreement shall be reduced to writing and be associated with the system's proof-of-performance records.

Note 2: For systems serving rural areas as defined in § 76.5, the system's local franchising authority may

adopt standards less stringent than those in §§ 76.605(a)(3), 76.605(a)(7), 76.605(a)(8), 76.605(a)(10), 76.605(a) (11), 76.605(a)(12), and 76.605(a)(13). Any such agreement shall be reduced to writing and be associated with the system's proof-of-performance records.

* * * * *

5. Section 76.606 is to be added to read as follows:

§ 76.606 Closed Captioning.

(a) The requirements for closed captioning are as follows:

(i) As of [90 days following publication in the Federal Register], the operator of each cable television system shall not take any action to remove or alter closed captioning data contained on line 21 of the vertical blanking interval; and

(ii) As of July 1, 1993, the operator of each cable television system shall deliver intact closed captioning data contained on line 21 of the vertical blanking interval, as it arrives at the headend or from another origination source, to subscriber terminals and (when so delivered to the cable system) in a format that can be recovered and displayed by decoders meeting § 15.119 of the Rules.

* * * * *

6. Section 76.607 is to be added to read as follows:

§ 76.607 Resolution of Complaints.

Cable system operators shall establish a process for resolving complaints from subscribers about the quality of the television signal delivered. These records shall be maintained for at least a one-year period and be available for inspection by the Commission and franchising authority, upon request. Subscribers shall be advised, at least once each calendar year, of the procedures for resolution of complaints by the cable system operator, including the address of the responsible officer of the local franchising authority.

NOTE: Prior to being referred to the Commission, complaints from subscribers about the quality of the television signal delivered must be re* * * * *

7. Section 76.609 is to be amended to revise paragraph (d)(2), the last sentence in paragraph (e), paragraph (g), the first sentence in paragraph (h), and paragraph (h)(2), to replace paragraph (i), and to add paragraph (j). It is to read as follows:

§ 76.609 Measurements.

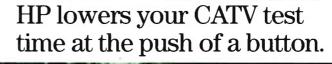
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(d)(2) By using either a multiburst generator or vertical interval test signals and either a modulator or processor at the sending end, and by using either a demodulator and either an oscilloscope display or a waveform monitor display at the subscriber terminal.

(e) * * * Alternatively, measurements made in accordance with the NCTA Recommended Practices for Measurements on Cable Television Systems, 2nd edition, November 1989, on noise measurement may be employed.

(g) The terminal isolation between any two terminals in the cable television system may be measured by applying a signal of known amplitude to one terminal and measuring the amplitude of that signal at the other terminal. The frequency of the signal should be close to the midfrequency of the channel being tested. Measurements of terminal isolation are not required when either (1) the manufacturer's specifications for subscriber tap isolation based on a representative sample of no less than 500 subscriber taps or (2) laboratory tests performed by or for the operator of a cable television system on a representative sample of no less than 50 subscriber taps, indicates that the terminal isolation standard of § 76.605(a)(9) is met. To demonstrate compliance with § 76.605(a)(9), the operator of a cable television system shall attach either such manufacturer's specifications or laboratory measurements as an exhibit to each proof-of-performance record.

(h) Measurements to determine the field strength of the signal leakage emanated by the cable television system shall be made in accordance with stan-





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(h)(2) Field strength shall be expressed in terms of the rms value of synchronizing peak for each cable television channel for which signal can be measured.

(i) For systems using cable traps and filters to control the delivery of specific channels to the subscriber terminal, measurements made to determine compliance with § 76.605(a)(5) and (6) may be performed at the location immediately prior to the trap or filter for the specific channel. The effects of these traps or filters, as certified by the system engineer or the equipment manufacturer, must be attached to each proof-of-performance record.

(j) Measurements made to determine the differential gain, differential phase and the chrominance-luminance delay inequality (chroma delay) shall be made in accordance with the NCTA Recommended Practices for Measurements on Cable Television Systems, 2nd edition, November 1989, on these parameters. **CT**

COMMUNICATIONS TECHNOLOGY

Impact of fiber optics

(Continued from page 28)

another question posed was: How far can a laser be pushed in today's environment — without getting in trouble?

By experimenting, it was possible to take a single fiber with 62 channels 19.9 miles with modulated specs of 55 dB C/N, 65 dB CTB and 65 dB CSO at the fiber node. (The lasers used are Optical Networks International's Laser Link II.) From there, a second laser was used to feed a cascade of four amplifiers, resulting in overall continuous wave performance specifications of 49 dB C/N, 53 dB CTB and 53 dB CSO at the subscriber tap. Using this cascaded laser design, TCI systems are able to go a distance of 40 miles from the headend.

An important question is: How reliable is such a design? For the past year, the Puerto Rico system has been closely monitored to judge the operational impact of such a design. After a year in operation, the system's 19.5mile run, with the original transmitter

Compression impact

(Continued from page 19)

ator, who would control the conditional access parameters.

The TV receiver provides signal access (tuning) and display. Subscriber access and control to premium services is provided by the plug-in decoder, which would decrypt the digital signal and decode the compressed signal. Since all of this happens inside the receiver, the customer benefits because all of the features of the receiver are retained. The cable operator gains not only from having a more satisfied customer but also from minimizing capital outlay - a relatively inexpensive add-on decoder module vs. a less user-friendly addressable set-top terminal. The decoder would not require a tuner or other redundant circuitry. In addition, power and cabinet costs are reduced.

The accompanying figure (page 18) displays a system that allows the subscriber to receive conventional NTSC, HDTV and digitally compressed NTSC. In addition, various levels of premium services are supported. The subscriber with the HDTV receiver has the added benefit of not requiring a set-top terminal, thereby enjoying all the features of his TV receiver.

and receiver, has not required a single readjustment. To ensure reliability, proofs are preformed every 30 days to monitor system performance.

Future considerations

It's no secret that TCI is currently doing a near-video-on-demand test with AT&T and US West. Neither is it a secret that TCI also is testing personal communications networks with McCaw Cellular in Oregon (see "News," page 12). Neither test involves experimentation with new technology, but both will yield important information on marketability of new service.

As we wait for the data to come in, engineers are faced with another question: How do operators design today's systems to meet existing requirements while still being flexible enough to meet tomorrow's business needs?

Take a look at some systems currently putting in 90 fibers. Is it really necessary to install this much capacity? The overall transmission capacity of fiber is unbelievable.

TCI's policy is to install four fibers at the node. But what if this is an insufficient number? What if the future requires six fibers at the node? The need today is to concentrate on maximizing the existing capacity of a single fiber. If this is done, it doesn't matter whether there are four, six or eight fibers at the node. If fiber is used to its fullest capacity, 90 fibers may be a bit much and there will always be a significant amount of fiber at the node.

Of course, no one is advocating only a single fiber at the node. There are already companies interested in leasing available dark fibers from cable systems — an interest with real implications in today's market. Rather, the message is simply that the industry has not researched the technology well enough to fully use a single fiber's capacity. And because technology will change quickly, it's possible that a single fiber could be used for more than one service.

Using digital technology

Another thought when considering future business is the operational impact of digital delivery on an analog cable system. For years now, the industry has been deploying fiber optics in an effort to reduce operational and maintenance costs. Rebuilds and upgrades using fiber optics have reduced capital expenditures, while im-

proving picture quality. But now, digital transmission will pose new challenges.

No one realized digital could be problematic in a broadband environment. Although operators have been subjected to countless discussions of digital transmission's benefits, no one has discussed the real-world impact of a digital overlay on an analog system beyond just the technological impact.

Let's look at what the industry has done. Everyone has worked to reduce operating costs. Profit margins are up, systems are operating as cost-effectively as possible and the number of operational personnel has been minimized.

Now that the industry is at this point, maintenance and operations will increase 25 to 50 percent when digital transmission is deployed. Systems will have to run tighter and better to offer high-quality services. Subscribers who pay \$10,000 for an HDTV receiver will expect to receive the highest resolution possible.

This is an issue that must be addressed when contemplating the use of digital delivery. To date, both CableLabs and AT&T are testing the effects of a digital overlay on an analog system. The results of these tests are critical to cable TV operators. It's important to know and understand exactly how this technology will impact cable TV systems.

Summary

Fiber optics is definitely the most significant advancement in cable TV distribution in recent years. It not only pays immediate dividends, it is the foundation for future technologies. It has been demonstrated again and again that fiber reduces trouble calls — in TCI's case, by 35 percent.

But there are other issues to consider as the industry moves forward. It is necessary to focus on such issues as fully utilizing the existing capacity of a single fiber, as well as realizing the full impact of digital on today's cable systems.

Ten years ago, the industry viewed life as complicated when it came to providing quality entertainment services. With the diversity of new opportunities available today, it's going to get more complicated. Operators need to fully explore each technology and its operational impact if the cable TV industry is to stay on the leading edge. **CT**

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Modulation methods

(Continued from page 24)

errors in either phase or amplitude that offset the decision threshold of some symbol states relative to their nominal position will degrade the noise performance of the demodulator.

Simulation program and channel model

To evaluate the effects of the channel and the filter distortion on various modulation types, a simulation program was written in MATLAB language. (MATLAB is an interactive program for numerical linear algebra, matrix computation and signal processing.) The simulation was done using the complex baseband representation of the bandpass modulated signal, meaning a carrier frequency of 0 Hz. The complex baseband representation permits us to sample the time waveform of the studied modulation at a better rate than what would be necessary if we were using a high carrier frequency. This is done without losing generality and keeping the same properties as a band-limited signal modulating a high frequency carrier. All the parameters of the simulation are normalized to the symbol rate and the filter bandwidths are specified as a ratio of the symbol rate instead of hertz.

The modulator block is an information source that, in the program, is composed of multiple pseudo random binary sequence (PRBS) generators and two digital-to-analog converters (D/A) — one in-phase and one in-quadrature. The simulation being numerical, frames of 4,096 complex samples are formed by the sampling of 512 symbols with eight samples per symbol.



The filters and the channel in the system are modeled as finite impulse response digital filters and the coefficients for these filters are real for symmetric filters or complex for asymmetric filters. The filtering is done in the time domain if both the input signal and the filter coefficients are real by convolving the signal with the filter coefficients. If the signal or the filter coefficients are complex, the filtering is done in the frequency domain by using a 512 point fast fourier transform (FFT) and the overlap-and-add method for processing long records, instead of doing two or four convolutions in the time domain. The program also generates all the conventional filter responses plus raisedcosine², square root raised-cosine, partial response and various channel distortions. The group-delay of the designed filters can be specified independently of the magnitude response enabling us to simulate any type of filter technologies like SAW filters, digital filters or LC filters.

After the signal is passed through the filters and the channel, the signal is demodulated synchronously. In a complex baseband signal, the carrier frequency is zero but the phase of the received signal is unknown and is function of the delay between the modulator and the demodulator. The demodulator extracts the I and Q components along two orthogonal axis offset in phase relative to the modulator phase reference in order to minimize the cross-correlation between I and Q components. The demodulated samples are then resampled by the symbol clock. If the sampling instant falls between demodulated samples, the values at that sampling instant are then estimated by linear interpolation that gives accurate results for a sampling rate to symbol rate of eight or more.

The bit error rate (BER) measurement is based on the quasi-analytical (QA)³ instead of the direct Monte-Carlo simulation. For linear systems this technique permits accurate measurements of low BERs without excessive computation. In the QA technique, also referred to as the hybrid simulation, a simulation is done without the addition of noise and with a source data pattern long enough to obtain all the possible combinations of ISI.

A histogram of the clock sampled data is then built, the noise is added analytically to the bins of the histogram, and the average symbol error rate is calculated. To convert the average symbol error rate to BER vs. energy per bits normalized (Eb/No), we need to calibrate our system by measurements of the signal power in the channel, the receiver noise bandwidth and the number of bits per symbol.

Quantitative effects of transmission impairments

We considered the following impairments to a digital signal and divided them in two categories:

- 1) Hardware imperfections:
- Quadrature error
- Phase error
- Symbol timing error

2) Channel distortion are as follows:

- Linear slope across passband
- Sinusoidal ripple across passband

The quadrature error is the deviation from orthogonality of the transmitter or the receiver, the symbol timing error is the deviation from the optimal sampling instant. These two errors

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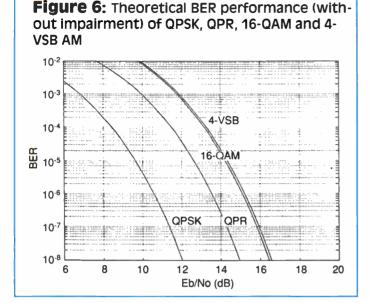
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are usually due to initial adjustment error or drift caused by components aging or temperature change. The phase error is an indirect measurement of the system sensitivity to phase noise. If the component of the phase noise is a sinusoidal waveform with a frequency less than the symbol rate, the BER degradation due to the untracked RMS phase noise give similar results to the same static phase error in the recovered carrier relative to the optimal carrier phase. This result was verified by simulating both degradations as well as by comparing our data with the results of Tranter, et al.⁴ To simulate the channel distortions encountered in a cable plant, we designed two linear phase filters, a linear slope filter and a ripple filter.⁵ The slope is defined as the number of decibel variation in a 6 MHz bandwidth. The ripple error is generated by a three tap FIR filter. This filter simulates three path propagation and can simulate the effect of reflection due to mismatch and the triple transit in SAW filters.

The bit rate and the filters for each modulation method in the simulation are selected to have a null-to-null bandwidth of 6 MHz using sharp filters that are today's state-ofthe-art. The resultant RF spectrum for each of the modulation methods simulated is shown in Figure 5 on page 34. The bit rate and filters used are shown in Table 1 (page 34).

Theoretical performance for each of these modulation methods is shown in Figure 6. Examining these results would suggest that while QPSK is the most robust, there is not much difference among the rest. These results do not take into account the relative sensitivities to distortions and demodulator imperfections.

Results for a "typical" cable channel

Elsewhere in the literature cited at the end of this article¹ results are presented showing the BER degradation of the four modulation types studied in the presence of a single non-optimal condition. In an actual system all forms of degradation will be present in varying degrees simultaneously. The results of each impairment do not linearly contribute to the total system performance degradation, thus it is necessary to model the system with all impairments included. In an attempt to understand the performance of these modulation methods in a "typical" cable environment,



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Table 3: Comparison of "typical" cable performance at 10⁻⁶ BER

Modulation type QPSK	Eb/No (dB) 12.2	Rate/BW (dB) 3.8	C/N* (dB) 16	Degradation (dB) 1.6
QPR	16.2	4.6	20.8	2.7
16-QAM	25.2	6.8	32	10.1
4-VSB AM	26.1	3 .8	29.9	10.9

* Note: Equivalent C/N in 4.2 MHz noise bandwidth video channel

erances in manufacturing would be required than for QPSK or QPR. QPR on the other hand, appears to be an attractive alternative to QPSK, providing 20 percent greater data rate with a relatively small penalty in C/N and very little additional complexity in implementation.

Conclusion

Four digital modulation techniques have been studied (QPSK, QPR, 4-VSB AM, and 16-QAM). They are capable of providing data rates between 10 and 20 Mbps in a 6 MHz bandwidth and are suitable for transmission of digital audio or compressed digital video. A time domain simulation program has been written that allows accurate simulation of the entire modulation-transmission-demodulation process and calculates error performance. The simulation allows imperfect filters, timing errors, quadrature errors, phase noise and bias errors to be included explicitly.

The results suggest that QPSK and QPR are significantly more rugged than 4-VSB AM or 16-QAM. QPR offers 20 percent greater bandwidth than QPSK with only a minor increase in signal power. Since 4-VSB AM does not offer any advantages over QPR and is much less rugged, it does not appear to be an attractive alternative. If the higher data rate offered by 16-QAM is essential, a significantly more complex demodulator would be required to provide acceptable performance, and then only

СТ

with an 11 dB higher signal than QPR.

References

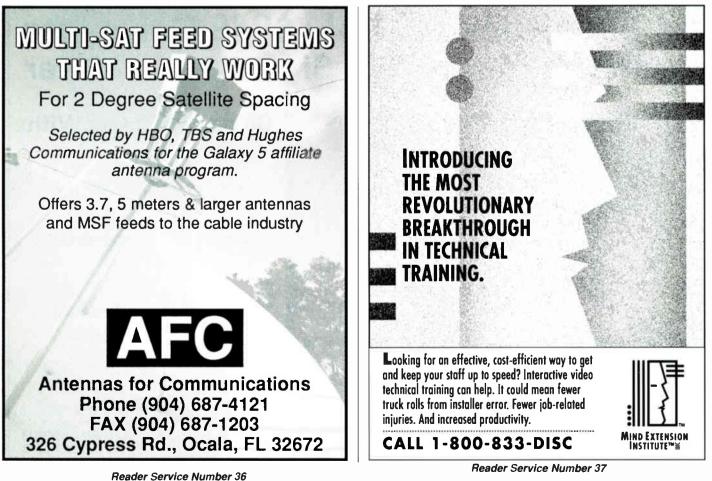
¹ John D. Oetting, "A Comparison of Modulation Techniques for Digital Radio," *IEEE Transactions on Communications*, Vol. COM-27, No. 12, December 1979.

² Kamilo Feher, *Advanced Digital Communications, Systems and Signal Processing Techniques*, Prentice-Hall, 1987.

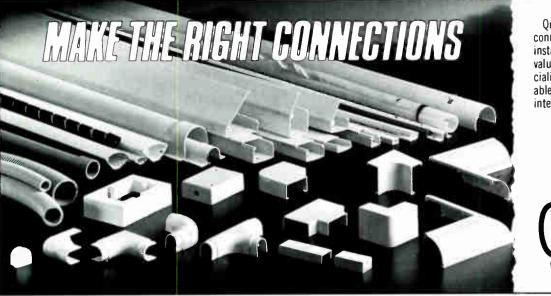
³ Michael J. Jeruchim, "Techniques for Estimating the Bit Error Rate in the Simulation of Digital Communications Systems," *IEEE Journal on Selected Areas in Communications*, Vol. SAC-2, No. 1, January 1984, p. 153-170.

⁴ Walter R. Braun, et al., "CLASS: A Comprehensive Satellite Link Simulation Package," *IEEE Journal on Selected Areas in Communications*, Vol. SAC-2, No. 1, January 1984, p. 129-137.

⁵ William H. Trantor, et al., "Simulation of Communications Systems Using Personal Computers," *IEEE Journal on Selected Areas in Communications*, Vol. SAC-6, No. 1, January 1988, p. 13-23.



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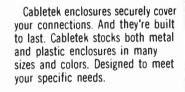
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Constellation analysis

(Continued from page 26)

This is actually a vector diagram where the transmitted signal is the vector sum of the data on the in-phase and quadrature carriers (hereafter called I and Q data). Expressed mathematically, the transmitted data is:

X(t) = I(t) + Q(t)

Where:

X(t) = transmitted data at time t I(t) = I data at time t Q(t) = Q data at time t

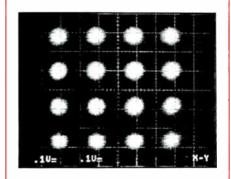
Since it is not necessary to show anything but the tips of the vectors, the resulting constellation diagram is always shown as a group of points.

Demodulation process

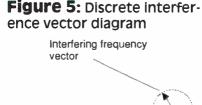
The demodulation process is the reverse of the modulation process. The signal is multiplied by in-phase and quadrature components of the carrier to recover the I and Q components. The four-level I and Q signals are then converted to digital form and recombined to generate a serial data output. In the absence of channel impairments, the output signal is, presumably, identical to the modulator input data.

Although 16-QAM is shown here as an example, other modulation schemes may be used. Among these are 64-QAM, in which three bits are converted to eight levels per phase, and 256-QAM, for which four bits are used to generate 16 levels per phase. Since the choice of modulation format is a topic unto itself, further discussion of constellation diagrams will be confined to 16-QAM. Transmission impairments affect all forms of quadrature amplitude modulation in the same manner.

Figure 7: Constellation impaired by random noise



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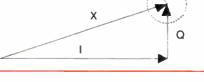
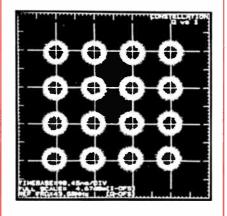


Figure 6: Discrete interference constellation



The only difference is one of degree.

The hardware implementation of a constellation analyzer is rather simple and is shown in Figure 4 on page 26. The demodulated I and Q data are applied to two inputs of an oscilloscope (that has X-Y display capability) to obtain the constellation. The primary purpose of constellation analysis is to provide a visual check of what impairments are present in the transmission channel. When the constellation analyzer is used in conjunction with a bit error rate tester, impairments can be quantified as well as identified.

Constellation analysis is useful for determining the effect of the following impairments:

- Discrete frequency interference
- Random noise
- Reflections
- Phase noise

A vector diagram illustrating the effect of discrete frequency interference is shown in Figure 5. The interfering carrier is a vector that is added to each point in the constellation. Since the phase of the carrier continuously varies with respect to the signal, the points appear as circles. The radius of the circles is proportional to the level of the interfering carrier. Expressed mathematically, the equation for the received single becomes:

$$X(t) = I(t) + Q(t) + f(t)$$
 (2)

Where the vector f(t) is the interfering frequency whose phase $\phi(t)$ varies with time.

An actual constellation with discrete frequency interference is shown in Figure 6.

Since random noise has a broadband spectrum, when noise is added to the signal, the effect is that of adding multiple vectors with varying amplitudes and phase. This results in a "smearing" of each point in the constellation as shown in Figure 7. The amount of point spreading is proportional to the carrier-to-noise ratio (C/N). A detailed discussion of the effect of noise on digital transmission may be found in Lee and Messerschmitt's *Digital Communication* (Kluwer Academic Publishers, 1988).

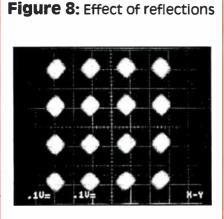
The effect of reflections on digital transmission depends on the number of echoes, their respective delays and their phase relative to the demodulating carrier. For a single reflection, the received signal may be expressed as:

$r(t) = I(t)cos(w_ct) + K^*I(t-\tau)cos$	s[w _c (t-τ)]+
$Q(t)sin(w_ct) + K^*Q(t-\tau)sin[w_c(t-\tau)]$	

Where:

$$\begin{split} &\mathsf{K} = \text{attenuation of reflected signal (K< 1)} \\ &\tau = \text{delay of reflected signal} \\ &\mathsf{W}_c = \text{carrier frequency} \\ &\mathsf{I}(t{\text{-}}\tau) = \text{amplitude of I signal at time t-}\tau \\ &\mathsf{Q}(t{\text{-}}\tau) = \text{amplitude of Q signal at time t-}\tau \\ &\mathsf{Demodulation and filtering of the re-} \end{split}$$

Demodulation and filtering of the received signal is mathematically equivalent to multiplying the I component by cos





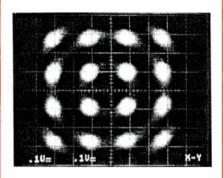
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Figure 9: Effect of phase noise



(w_t) and the Q component by sin(w_t) and throwing out the double frequency terms. The resultant equations are:

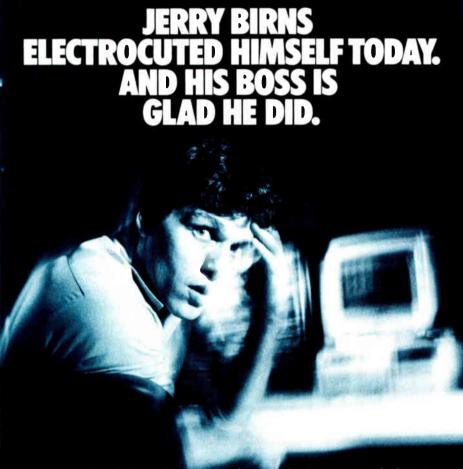
$$\begin{aligned} r_{Q}(t) &= Q(t) + K[Q(t - \tau) cos(w_{c}\tau) - \\ I(t - \tau) sin(w_{c}\tau)] \end{aligned}$$

Where:

 $r_{i}(t) = demodulated I component$ $r_{o}(t) =$ demodulated Q component

If the preceding equations are plotted

(5)



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in vector form for all possible values of I and Q, the result is a miniature replica of the entire constellation about each point in the original constellation. The size of the replicated constellation is equal to K times the size of the original constellation and the replicated constellation is rotated by an angle $w_c \tau$ relative to the original constellation. (If $w_c \tau$ is close to 45°, the constellation has the so-called "16 of diamonds" look as in Figure 8 on page 50.)

Multiple reflections occurring at various levels and delays will result in a number of superimposed replicas of the original constellation, producing a pattern that looks similar to that generated by random noise. However, if one echo is dominant, as is frequently the case in cable systems, the pattern will still have a square or diamond-shaped configuration.

Phase noise is largely a function of the stability of the local oscillator in either the modulator or the demodulator (usually the demodulator). When the receiver demodulates with a carrier having excessive phase jitter, the received constellation will oscillate about its center as shown in Figure 9. If the demodulating frequency is incorrect, the result will be a continuously rotating constellation.

At this point, it would be worthwhile to consider the implications of constellation analysis for cable transmission of digital signals. In a cable environment, noise is not generally a problem. Most systems have C/N levels in the neighborhood of 48 dB or better and, even if the digital signal is transmitted at reduced power, errors would not occur until the C/N becomes less than about 22 dB. Reflections, on the other hand, tend to cause errors in digital transmission at levels that are not noticeable on analog signals.

In particular, unterminated drops on the distribution system and unterminated cables in the customer's home can cause significant problems. This condition is typical of all drops terminated by a cableready receiver or a VCR. Phase noise would generally indicate a converter phase-locked loop malfunction.

The net result of all transmission channel impairments is to generate bit errors. Although all digital transmission systems proposed to date will contain powerful error correction schemes, error correction shouldn't be regarded as a cure-all for system problems. System impairments will still need to be found and corrected. Just as the video waveform monitor has been a useful tool for detection of analog transmission impairments, constellation analysis will provide a tool for detection of digital transmission problems. СТ

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Table 3: Emergency cablerestoration alternatives

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4) Verify end-to-end continuity utilizing
 OTDR or light source and power meter
 5) Make transition to permanent repair

as soon as possible

Cable cut with no slack

1) Locate damage point with OTDR

2) Install new cable

3) Splice in new piece of cable with temporary mechanical splices

4) Verify end-to-end continuity utilizing OTDR as soon as possible

5) Make transition to permanent repair as soon as possible

Note: Downtime can be further reduced by the use of an emergency restoration kit.

FO troubleshooting

(Continued from page 30)

resolution with accuracy.

Many times management becomes frustrated with what appears to be an inability of the technician to pinpoint the break. There are many variables that must be considered in order to effectively locate a break in fiber cable. For this reason, documentation and training is critical with fiber systems.

Unfortunately, an extrinsic reason is the usual cause of fiber problems. The normal result is a total failure of random fibers within the cable sheath. The failure is normally of the catastrophic type. Extrinsic reasons include rodents, lightning, ground faults, gunshots, freezing water in conduits, vandalism,

Table 4: Typical emergencyrestoration kit

- 1) Restoration splice trays
- 2) Two pre-drilled splice closures
- 3) Approximately 150 feet fiber cable
- 4) Temporary mechanical splice parts (twice count of active fibers)
- 5) Two complete tool kits consisting of:
 - a) Alcohol packs
 - b) Gel-off packs
 - c) 88 vinyl tape
 - d) Miller stripping tool
 - e) Book of numbers
 - f) Kim wipes

g) Diagonal side cutting pliers h) Pliers

- i) Wrenches
- j) Cable sheath knife
- k) Ty-raps
- I) Snips
- m) Precision cleaving tool

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excavation, damaged poles (especially from auto accidents) and failures at splice points caused by poor craftsmanship. Improper closure assembly and/or poor storage of the fiber or cable within the closure assembly or hand hole also can result in failures.

Restoration

Once the cause of system failure has been determined, measures must be taken to restore the cable system. Standard procedures for restoration should be established by the CATV operator. Tables 2 (page 30) and 3 out-

COMMUNICATIONS TECHNOLOGY

line emergency restoration procedures and alternatives. In many cases, the operator will need to work with the local utility operator to restore service. It is important to have an agreement with the owner of the utility pole line as to priorities of restoration in the case of downed poles. Additionally, the availability (or lack thereof) of "slack" cable will usually dictate your course of action in the field.

Restoration can range from simply transferring system operation from one

(Continued on page 68)

MAY 1992 53

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CABLE-TEC EXPO '91	THE BUSTGEN ENTITLE CITY IN THE WORLD SCTE
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Phone #: (Date :	Signature:

Find that fiber!

(Continued from page 32)

rate of force applied by the technician is not controlled.

Self-testing and diagnostics. Contamination, especially in the outdoor elements, is a distinct problem with any test set that does not contain some type of self-testing and diagnostic program that ensures that the equipment itself is operating properly, and that the signal detector device is free of contamination.

Minimizing misidentification

As usage of CATV fiber systems becomes more prevalent, it is evident that a more sensitive identifier is needed. Such a fiber identifier would eliminate the potential for failure of technicians to identify light fibers and contain several features to help alleviate the most common reasons for misidentification. The following are among them:

• A signal level sensitivity of 50 dBm to pick up low-level signals on a live fiber, especially in trunking systems.

• Tone detection capability of 1 kHz and 2 kHz and transmission direction indicators.

• The capability to operate over 1,310 nm to 1,550 nm with low insertion loss at 1,300 nm and 1,500 nm.

Since the rate of force applied to fibers during the identification process can vary from technician to technician, a bidirectional mechanical damping device that automatically controls the rate and amount of force applied to the fiber would be built in.

To ensure that the unit operates properly during each use and is free of contaminants that could distort readings, some sort of self-testing procedure is required in the software before and after each fiber insertion. These self-tests should check the optical channel in which the fiber is inserted.

To minimize confusion for the technician, the identifier operation should be kept as simple and straightforward as possible. Pertinent messages — such as indicators for low batteries, signal direction and no signal detection should be displayed on an LED panel to simplify the identification process for technicians. The identifier should be lightweight and portable and built for the rugged and harsh field environment with weather-protected, self-contained operation. It should operate on a standard, readily available 9-volt battery.

RiserBond TDRs are the best way to save you TIME and MONEY when locating faults or measuring cable. It's that simple. Rugged, Compact and Lightweight Automatic Distance and Return Loss Readings High Precision Accuracy (+/-.01%) Built-in Printer and **Rechargeable NiCad** Batteries Standard Waveform Storage and Comparison Standard





As more and more optical fiber goes into service, the need to accurately identify and test individual fibers within systems is escalating. Fibers are carrying so much video — one fiber can carry 54 broadband channels — that it can cost many thousands of dollars if a fiber is shut down in error.

Model 1220

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Summary

The complexity of fiber-optic systems has increased. Now, in order to maximize the transmission capability of fiber-optic technology, cable companies are designing elaborate infrastructures with multiple hubs and routes containing up to 144 individual fibers.

While much of the identification and test equipment developed in the late 1980s helped cable technicians in their work identifying and testing fiber, there were still some shortcomings that led to misidentification. As the science of optical fiber identification and testing advances, new features are being designed into test equipment that help technicians overcome many of the critical factors involved in identifying and analyzing optical fibers. **CT**

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COMMUNICATIONS TECHNOLOGY

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Jerry Neal Senior Software Engineer Pioneer Communications of America Cable Systems Division

When Pioneer developed the Pioneer LaserDisc Universal System (PLUS), our goal was to simplify operations and increase revenue for the cable operator. We know that system automation and increased customer programming selection are both good economic moves. So, we created PLUS to provide

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REVOLUTIONIZING TELEVISION AUTOMATION

Real-Time Control Solutions for Small Systems

By John Gerstenberg Systems Engineer

Situation

Small cable systems are looking for a cost-effective and integrated approach to real-time automated control of a host of different devices, including VCR's, audio/video switchers, IF/RF switchers, satellite receivers, and more.

Objective

Provide a capable, yet low-cost clock controller that is modular in design, for use in a variety of control applications.

Solutions

For less than \$1000, cable operators can buy the Li'l Ben, a basic seven-day clock controller with eight programmable outputs, capable of controlling up to 400 events. (Other optional configurations cost a little more.)

The Li'l Ben[™] Clock Controller from Channelmatic is designed as an allpurpose clock for small cable systems, which means it does just about anything, but costs next to nothing.

Many Configuration Options

This versatile, microcomputer-controlled device can be configured in many different ways, simply by adding custom control modules internally, or by controlling the same modules in an external chassis. In its basic form (LCC-1A), the Li'l Ben has eight opencollector, FET "pull to ground" outputs, through which it performs direct VCR control, A/V switching, or virtually any custom control in real-time.

A slightly different version of the Li'l Ben (LCC-2A) uses Single-Pole, Double-Throw relays. As illustrated in Figure 1, the LCC-2A is used to control an external channel modulator with a built-in A/B switch, to select one of two program sources for that channel.

The LCC-3A has a 2x1 stereo audiofollow-video switcher actually built-in, for switching between any two A/V sources, such as VCR's, networks, or character generators. Two of the control outputs are internally wired to control the audio/video switching, leaving six FET outputs to control other external devices. Incorporating the switcher in the Li'l Ben saves the operator money and valuable rack space.

The LCC-5A was developed to work in conjunction with sequential ad insertion systems to provide limited fixedposition insertion capability, as shown in Figure 2. By automatically rewinding the VCR to the beginning of its tape at a scheduled time, the Li'l Ben allows the ad insertion system to recue the VCR to the first commercial on the tape. Unique software logic enables the LCC-5A to monitor the on-air line from the ad insertion controller, and rewind the VCR only when a commercial is not actively being inserted.

Ease of Operation

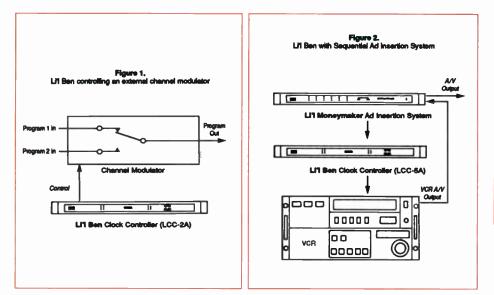
Programming the Li'l Ben is as easy as setting a digital wristwatch. Instructions are keyed in with a four-button keypad. A four-digit multiplexed LED display guides the user through the various modes of operation, and also displays output circuit status.

Custom Solutions

The real-time control applications discussed here are only a few of the typical uses for the versatile Li'l Ben Clock Controller. In combination with Channelmatic's extensive line of 3000-Series function modules, the possibilities of low-cost, real-time automated control are limited only by your imagination.

Channelmatic designs, manufactures and installs complete automation systems that improve operating efficiency and on-air signal quality. With a complete line of over 200 modular units and A/V accessories, we can enhance your system with virtually any feature you could want or need.

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Table of Contents Power awareness The safety importance of hot gloves and voltage meters and how to use them. By Pam Nobles of Jones Intercable. Bucket trucks -Part 4 Wrapping up his series, Pat Bartol of Mobile Lifts describes the dos and don'ts of safe operation. Ves

Courtesy of Mind Extension Institute, General Safety interactive video

Figure 1: High-voltage gloves (with protector gloves and inner liners)

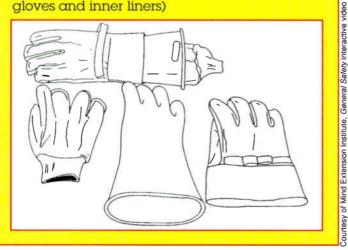
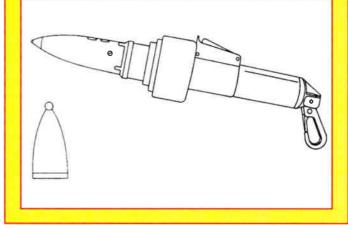


Figure 2: Voltage detector



Power awareness: Hot gloves and voltage detectors

Based upon careful interpretation of the "Code of Federal Regulations Title 29" Part 1910.268, it is the position of this author that all associates who climb poles or work where there is danger of contact with power need to be is-

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Computer Utilities (800) 541-8825 (501) 741-1616 See us in Dallas at booth 1137. sued high-voltage gloves and voltage detectors.

This article will review the thought process behind this decision, outline recommendations for when and how to use high-voltage gloves and voltage detectors, and touch upon training and follow-up guidelines.

By Pam Nobles

Senior Staff Engineer/Technical Training Jones Intercable Inc.

High-voltage gloves and voltage detectors have been a source of controversy and confusion in cable TV systems for years. This primarily is due to the diverse interpretation of the codes and the fact that there are no direct regulations for CATV in the codes. In addition, issuing high-voltage gloves and detectors opens up a "can of worms" involving inspection and testing of the equipment, training of the associates, and follow-up on both.

Many managers don't want to deal with these issues — especially, since the misuse of such equipment may cause injury or death. Unfortunately, not using this protective equipment at all could cause the same result.

Quite frankly, discussions on highvoltage gloves and voltage detectors at times can become very emotional! Different system offices of the same company are quite often divided in their interpretations of *if* or *when* this protective gear should be used.

Thought process behind decision

Guidelines for when high-voltage gloves and voltage testers should be used are found in the "Telecommunications" section of *CFR Title 29*, Part 1910.268. The individual paragraphs that refer to our topic have been reproduced in this article for your reference. (See accompanying table on page 66.) It is important for you to secure an entire copy of this code for your own reference.

The first test a lineman makes is to determine if the pole is climbable. When climbing a joint-use or light fixture pole, a visual check is made of condition and rake of the pole, and whether or not the metal power conduit, exposed vertical power ground wires, or street light fixtures are bonded to the communications strand or cable sheath. If grounding cannot be determined visually, the code states that these items shall be tested for voltage. The code continues in (ii): "If no hazardous voltage is shown by the voltage test, a temporary bond shall be placed between such street light fixture, exposed vertical power grounding conductor, or metallic power conduit and the communications cable strand."

In (5), we learn how to attach and remove temporary bonds: "When attaching grounds (bonds), the first attachment shall be made to the protective ground. When removing bonds, the connection to the line or equipment shall be removed first. Insulating



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gloves shall be worn during these operations."

In addition, we learned in (4) there are specific requirements that deal with "suitable protective grounding" that the communications cable sheath or shield must meet:

"(A) Bonded to an underground or buried cable that is connected to a central office ground, or

(B) Bonded to an underground metallic piping system, or

(C) Bonded to a power system multigrounded neutral or grounded neutral of a power secondary system that has at least three services connected."

After the lineman has completed all these visual checks, if he can't be completely sure the line is bonded, testing for voltage and wearing high-voltage gloves is necessary.

Gloves use

High-voltage or rubber-insulated safety gloves (Figure 1 on page 60) are worn to prevent injury in the event of an accidental encounter with electricity. It is very important to note that wearing hot gloves does not mean you can intentionally grab a hot wire. Good work practices and safe procedures will pro-

"Wearing hot gloves does not mean you can intentionally grab a hot wire."

tect you from electricity. In all cases, avoid hot wires and energized surfaces.

For use in CATV, 10,000 volt gloves are recommended. Always wear rubber-insulated safety gloves when:

• There is a possibility of contacting electrical power,

• Placing and removing temporary and permanent electrical bonds,

• Installing a ground rod, and/or

• When using a voltage detector.

American Standard Test and Measurement (ASTM) Designation F 496-85 — Standards on Electrical Protective Equipment for Workers, provides the specification for the in-service care of insulating gloves. The following guidelines have been extracted from this standard.

Inspections and tests

The field care and inspection of electrical insulating gloves, performed by the individual, is an important requirement in providing protection from electric shock. Defective or suspected defective gloves shall not be used.

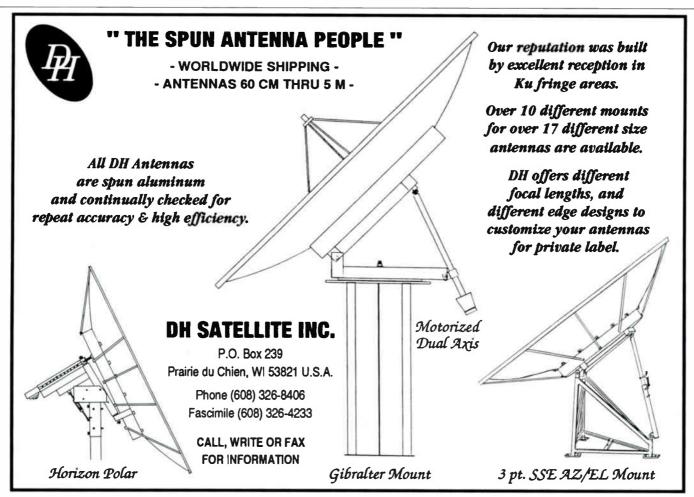
Insulating gloves shall be visually inspected by the wearer for defects when initially received, and before and after each use. Gloves shall be air-tested before use each day and at other times if there is cause to suspect any damage. They shall be inspected over the entire surface and shall be rolled gently between the hands to expose defects and imbedded materials.

Insulating gloves shall be given an air-test by rolling the cuff tightly toward the palm in such a manner that air is entrapped inside the glove, or by using a mechanical inflator. When using the latter, care shall be taken to avoid over-inflation. The glove shall be examined for punctures and other defects. Puncture detection may be enhanced by listening for escaping air or holding the gloves against the worker's cheek to feel for escaping air.

A visual inspection of gloves shall be made in the field monthly by a designated person to determine that such equipment is being maintained in a satisfactory condition by the tech.

Follow this inspection sequence:

1) Visually check return for test



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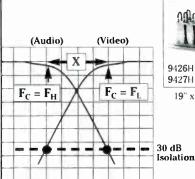
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Model	L	ow	High	Isolation	Functional Use
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3329-57*	0	45.75	60 - 300	45 dB	Sub-band/VHF
3329-51.5(25)	0	- 48	54 - 450	25 dB	Sub-band/VHF
3329-51.5(40)*	0	- 48	54 - 450	40 dB	Sub-band/VHF
3329-38	5	- 33	54 - 500	25 dB	Sub/low VHF
3329-98	5	- 88	108 - 300	25 dB	Low VHF/Mid-band
3329-130	5	- 110	170 - 450	30 dB	Low/high VHF
3329-M/S	5	- 174	216 - 420	30 dB	Mid-band/Super-band
3329-375	54	- 300	470 - 890	25 dB	UHF/VHF

Baseplate dimensions: 21/4" x 61/8"

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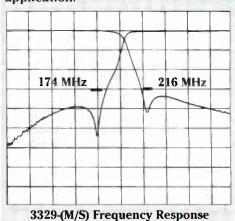


21/4" x 6" x 1'



(MHz) (dB) Cut-Off Loss dB (ns) Option RL Delay Cut-Off Type Type <u>F_H</u> <u>F</u>L X > 8 Low Pass Adjacent 9426L-(F_H) 54 - 300 < 3 1.5 ≈ 50ns Low Pass 9426H-(FH) 300 - 550 < 3 1.5 > 8 = 50ns Adjacent 54 - 300< 3 High Pass Adjacent 9427L-(FL) 1.5 > 8 ≈ 50ns -High Pass Adjacent 9427H-(F1) 300 - 550 < 3 1.5 > 8 ≈ 50ns 54 - 300 < 3 Splitter Semi adjacent 9428-F_H/FL < 3 7.5 > 12 ≈ 20ns *Splitter Adjacent 9429-FH/FL 54 - 300< 5 < 5 1.5 > 12 ≈ 50ns *PRODUCT UNDER DEVELOPMENT Customer to specify FL, FH or FH/FL

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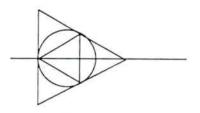
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date. If out of date do not use and return for test.

2) Pull vigorously between fingers looking for cracks and inner liner, normally a contrasting color, showing through.

3) Look for signs of abrasions or deterioration on the palms, back of the thumb side and little finger side.

 Turn the glove inside out and repeat the stretch test.

5) Turn the glove right side out.

6) Squeeze the fingers of the glove together and let go quickly. Live rubber will return to normal.

7) Fill the glove with air by revolving the glove around the edge of the gauntlet axis, rolling it toward the palm and fingers.

If insulating gloves fail any of these tests, do not use.

In addition to the daily and monthly inspections done at the system, highvoltage gloves should be checked with voltage every nine months. According to ASTM Designation F 496-85, since the telecommunications industry utilizes insulating gloves as precautionary protection against unintentional contact with energized conductors, the maximum interval between issue and retest is nine months. CFR Title 29 Part 1910.268 indicates 12 months for new gloves. Gloves can be voltage tested by your local power company or by a testing lab for their ability to insulate against voltage. Tests should be identified as indicated under record keeping.

The following are more tips for keeping gloves in good working order:

1) Storage — Gloves shall be stored in a location as cool, dark and dry as possible, free from damaging substances, vapors and fumes, and away from electrical discharges and sunlight. Gloves shall be stored in their natural shape, with fingers up, so debris does not fall in the gloves. Gloves may be kept inside of protectors or in a bag, box or container that is designed for and used exclusively for them. Gloves shall not be stored folded, creased, inside out, compressed, or in any manner that will cause stretching or compression. Hang the storage bag in a protected location that visible to tech.

2) *Care* — Gloves shall be wiped clean of any oil, grease or other damaging substances as soon as practicable. Gloves should be rinsed as necessary to remove perspiration. Excess water should be shaken out and then the gloves should be air-dried. Never patch or repair rubber-insulated gloves in any way.

Carelessness causes the following glove damages:

• Snags (caused by not wearing protective leather gloves over the hot gloves)

• Ozone (caused by storage near ozone-producing equipment)

• Chemical attack (swelling caused by oils and petroleum compounds)

• Sun checking (caused by prolonged exposure to sunlight)

• Cracking (caused by prolonged folding of gloves — the strain on the rubber at the folded point is equal to stretching the glove to twice its length)

3) Protector gloves — The protector gloves shall meet Specification F 696 and shall be worn over insulating gloves to prevent mechanical damage. ASTM Specification F 696 describes the type and thickness of the leather for the gloves as well as the material for the cuffs. The protector glove shall be sized and shaped so that the insulating glove shall not be deformed from its natural shape.

The minimum distance between the top of the cuff of the protector glove and the rolled top of the cuff of the in-



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CFR Title 29, Telecommunications, Ch. XVII (7/1/91 Edition)

(m) Grounding for employee protectionpole lines

(1) Power conductors. Electric power conductors and equipment shall be considered as energized unless the employee can visually determine that they are bonded to one of the grounds listed in paragraph (m)(4) of this section.

(2) Nonworking open wire. Nonworking open wire communications lines shall be bonded to one of the grounds listed in paragraph (m)(4) of this section.

(3) Vertical power conduit, power ground wires and street light fixtures.

(i) Metal power conduit on joint-use poles, exposed vertical power ground wires, and street light fixtures which are below communications attachments or less than 20 inches above these attachments, shall be tested for voltage unless the employee can visually determine that they are bonded to the communications suspension strand or cable sheath.

(*ii*) If no hazardous voltage is shown by the voltage test, a temporary bond shall be placed between such street light fixture, exposed vertical power grounding conductor, or metallic power conduit and the communications cable strand. Temporary bonds used for this purpose shall have sufficient conductivity to carry at least 500 amperes for a period of one second without fusing.

(4) Suitable protective grounding. Acceptable grounds for protective grounding are as follows:

sulating glove shall be not less than 1 inch for a Class 1 glove.

Protector gloves that have been used for any other purpose shall not be used to protect insulating gloves. Supplying protectors with bright color gantlets may guard against this problem, since an inspector can see the gloves in use from a distance. Protector gloves shall not be used if they have holes, tears or other defects that affect their ability to give mechanical protection to the insulating gloves. Keep protector gloves as free as possible from oils, greases, chemicals and other materials that may injure the insulating gloves. If contaminated, do not use unless they have been thoroughly cleansed of the contaminating substance. The inner surface of the protector gloves should be inspected for sharp or pointed objects. This inspection should be made as often as the rubber gloves are inspected.

Cloth gloves may be worn inside of insulating gloves for warmth in cold weather and to absorb perspiration in hot weather.

Gloves with any of the following defects shall not be used and shall be re(i) A vertical ground wire that has been tested, found safe and is connected to a power system multigrounded neutral or the grounded neutral of a power secondary system where there are at least three services connected;

(ii) Communications cable sheath or shield and its supporting strand where the sheath or shield is:

(A) Bonded to an underground or buried cable which is connected to a central office ground, or

(B) Bonded to a underground metallic piping system, or

(Č) Bonded to a power system multigrounded neutral or grounded neutral of a power secondary system which has at least three services connected;

(5) Attaching and removing temporary bonds. When attaching grounds (bonds) m, the first attachment shall be made to the protective ground. When removing bonds, the connection to the line or equipment shall be removed first. Insulating gloves shall be worn during these operations.

(n) Overhead lines.

(1) Handling suspension strand.

(i) The employer shall insure that when handling cable suspension strand which is being installed on poles carrying exposed energized power conductors, employees shall wear insulating gloves and shall avoid body contact with the strand until after it has been tensioned, dead-ended and permanently grounded.

turned to an electrical testing facility for inspection and electrical retest:

- Holes, tears, punctures or cuts;
- Ozone cutting or ozone checking;
- Imbedded foreign objects;

• Texture changes (swelling, softening, hardening, becoming sticky or inelastic); and/or

 Other defects that damage the insulating properties.

Gloves that have been rejected and are not suitable for electrical service shall be defaced, cut or otherwise marked and identified to indicate that they are not to be used for electrical service.

Record keeping and marking

Gloves shall be marked to identify the type, class and size. The test procedures of the electrical test facility shall specify the test voltage for each class of glove to be tested or a record shall be kept of the voltage used in the test. A date specified as test or retest shall be either recorded or provided by marking or affixing a label to the glove. The marking or labeling method and material shall not adversely affect the electrical or physical characteristics of the glove or sleeve or conflict with the manufacturer's original marking or labeling. Employees should inform their supervisor if inspection date is past due.

Voltage detector use

The voltage detector (Figure 2 on page 60) is included in this discussion since its purpose is similar to that of high-voltage gloves — that is, to prevent injury in the event of an accidental encounter with electricity. In addition, high-voltage gloves must be worn during most applications of the voltage tester. Much of the information in this section has been summarized from the C-9970 Voltage Detector Handbook. Since voltage detectors vary, it is important to understand the theory and operation of the particular test set your company uses.

The voltage detector is a high-voltage detection device. It is intended for use in testing various conductive objects such as power ground wires, street light fixtures, mobile homes, metal frameworks, metal conduit, pedestals, newly driven ground rods, homes covered with metallic siding, electrical machinery and similar items that a tech may contact.

The C-9970 voltage detector uses electronics and high-voltage mechanical design to indicate the presence of dangerously high AC and DC voltages. The voltage detector does this by comparing the voltage difference between the user's body and the object being tested to an internal (to the voltage detector) safety reference. If the voltage difference exceeds this reference, the voltage detector will indicate danger by way of a flashing red LED.

The capacitance between the handle of the voltage detector and the user's hand is part of the measuring circuit and can affect the sensitivity of the voltage detector. Thus the final test using the voltage detector must be done with the bare hand holding the test set. However, the voltage tester should first be used while wearing high-voltage gloves.

Electrical testing is required on the followina:

· Whenever there is reason to suspect damage to any utility;

· Uninsulated vertical grounds, electrical power guys, and conduits;

Street light fixtures (ungrounded);

Metal-sided buildings, mobile

homes and trailers, aluminum siding;

Joint-use pedestals;

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FO troubleshooting

(Continued from page 53)

fiber to another to a complete replacement of a segment of cable. Table 4 (page 53) shows what you should have in your emergency restoration kit. Normally, temporary mechanical splices are installed to expedite the restoration of service. Develop and practice emergency restoration procedures. After service is restored, permanent repairs via a "hot cut" can be made. The speed of the restoration of service is essential in order to keep customers satisfied.

Conclusions

Develop and practice an emergency restoration plan before a problem occurs. Know where the necessary records, equipment, materials and personnel may be found to make the temporary repairs. Use a logical process of elimination to determine the failure. After determining which of the components has failed, quickly effect the repairs. The most important thing about emergency restoration is to restore service as quickly as possible using temporary repairs that permit a graceful transition to a permanent repair. **CT**

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• Foreign plant in our work space, including telephone, down guys, etc.; and/or

• Ceiling grids.

Inspection and testing

Before using the voltage detector, perform all inspections outlined by the manufacturer. To use, grasp the detector by the handle and depress the trigger with the thumb. A red flashing LED indicates a dangerous voltage; green indicates voltage is not present. After determining the area is safe for work, a temporary bond is placed as a precaution should a fault develop once work is underway.

The voltage detector must be visually inspected and tested:

- When received,
- · Before each use (self-test),

• At least once a month (maintain a record), and

· Annually with appropriate test set.

Underground plant

Mobile homes, trailers, metal-sheath buildings, ground rods and electrical machinery all present a potential electrical hazard and always require testing. Test the siding and frame or both frames in the case of double-wide mobile homes before starting work. If a voltage is detected on these objects, the property owner should be notified for corrective action according to the your company's procedures. Do not contact the potential hazard until all hazardous voltage has been removed and the voltage detector indicates a safe condition.

When a pedestal closure used in joint-buried plant has been damaged or disturbed or a trouble condition involving power is suspected, any power company work should be performed first. After the power company has completed its work, the pedestal should be tested with the voltage detector before any bodily contact is made. Work should not be done on the plant until the power company has completed repairs. Additional precautions should be exercised during construction or in storm repair situations. Be sure you understand the operation of the voltage tester as well as your company's procedures before proceeding in such situations.

Aerial

Examine the pole for potential electrical hazards such as a vertical power ground wire, vertical metallic power

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conduit, street light fixture, power company primary disconnect hardware, or other foreign metal objects. Metal power conduit on joint-use poles, exposed vertical power ground wires and street light fixtures that are below communications attachments (or less than 20 inches above these attachments) shall be tested for voltage unless the employee can visually determine that they are bonded to the communications suspension strand or cable sheath. Also, observe the pole and adjacent spans for such hazards as improper clearance from power conductors or equipment, dangling power wires, inadequate clearance on poleto-pole guys from power wires or energized attachment, etc. If none of these are present, the pole may be climbed providing no other hazard is evident.

If a vertical power conduit or other power company hardware extends to the base of the pole, make a voltage test before climbing or working on the pole.

If the ground wire is broken, test the portion going up the pole unless the break exists above the cable space. Do not attempt to test a broken ground wire or fixture in the power company's space (40 inches or more above highest cable attachment). If a vertical power ground wire is present, make a voltage test of the wire before climbing or working on the pole.

If the voltage tester does not indicate a hazardous voltage, poles carrying vertical power ground wires may be climbed. Care should be exercised to avoid simultaneous contact between power ground wires and cable or guys since a small voltage may be present. This is recommended to avoid the possibility of a surprise shock, which might cause a fall from the pole.

In general, the tech should avoid unsecured objects, dangling wires, etc., which would tend to move if probed. Do not contact supply wires going to the fixture. If a temporary bond cannot be attached effectively, wear high-voltage gloves.

To test for potential electrical hazards follow these steps:

1) Make pre-use test,

2) Put on insulating gloves,

3) Depress switch and approach the object to be tested,

4) If the LED does not flash, do another test without insulating gloves,

5) If the red LED does not flash, the object is not energized, and

6) If the red LED flashes, move away. Notify your supervisor and identify the hazard for the public and other employees.

Voltage detector temporary bond

The temporary bond is used to temporarily ground a fixture, conduit or bare vertical ground wire that has been tested for and found to be free from a voltage potential while working aloft. Should a fault develop, the temporary bond will provide a direct path to ground for the foreign potential. The insulation on the bond may overheat and smoke, which should alert the lineman to descend the pole.

While using insulating gloves, attach the bond in the following manner: Attach the small clip of the temporary bond to the cable suspension strand in such a manner that it will not be in the way of work operations. Then attach the large clip of the bond wire to the fixture, conduit or bare vertical ground wire. Do not bond to a support bracket of multiple line wire or the suspension strand of isolated cable. Never attach to any street light wires or terminals to which the wires are attached or to a fixture that causes the red LED to flash.

The insulating gloves may be removed only after the temporary bond is in place, and then only if other protec-



tion requirements permit. Leave the temporary bond in place until all work operations have been completed at this pole for the day.

If the bond starts smoking, put on insulating gloves and descend the pole immediately. Do not make any contact with the bond, the fixture or its wiring.

Upon completion of work operations on a pole, remove the temporary bond as follows:

1) Put on insulating gloves,

2) Remove the clip from the fixture, metallic conduit or bare vertical ground wire, then

Remove the other clip that was attached to the strand. If a spark is detected when removing the bond, descend the pole immediately.

Particular care must be taken when working near traffic light wiring or other wiring that may become energized momentarily. Voltage tests made during one part of a cycle may not be valid during another part.

To use the temporary bond,

1) Wear insulating gloves.

2) Connect the small clamp of the bond to a known ground source first,

3) Connect the large clamp of the bond to the fixture last.

4) Leave the temporary bond in place until all work operations have been completed.

5) While wearing insulating gloves. remove the large clamp from the fixture first, and then

6) Remove the small clamp from the ground last.

If the bond smokes:

1) Leave the bond in place and move away and do not touch,

2) Identify hazard for the public and other employees and do not leave hazard unguarded,

3) Notify your supervisor immediately, and

4) See that the responsible company owner is notified of the hazard.

Training and follow-up

Since the improper use of hot gloves could result in death, a properly developed training program, adequately implemented and monitored, is critical.

One of the most difficult tasks may be addressing the need for a change of attitude regarding hot gloves and ensuring support from management in each system. This involves backing from management — we need to make sure this is not taken lightly.

Once your company's guidelines have been established and you have secured agreement from management. your training program can be developed. It is important that your training be geared specifically for your company.

Decide in advance what type of disciplinary action should be taken if guidelines are not followed. Use an employee sign-off sheet to aid you in training and inspection. Once begun, ongoing training and monitoring is critical.

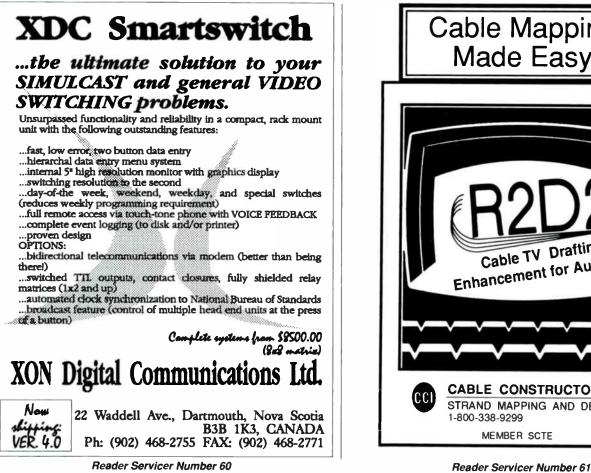
Be sure to read the codes before deciding your position on high-voltage gloves and voltage detectors. Also, discuss your plan for with your company's safety director before implementation of their use. BTB

References

1) CFR Title 29, Part 1910.268, "Telecommunications."

2) ASTM Standards on Electrical Protective Equipment for Workers, Seventh Edition 1988, ASTM Designation: F 496-85 and ASTM Designation: F 696-85.

3) C-9970 Voltage Detector Handbook. US West Communications Safety Assurance System.



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The bucket truck: A versatile tool (Part 4)

This is the fourth and last in a series of articles on bucket trucks and will cover "dos" and "don'ts." Part 1 (February 1991) explored their uses and benefits, Part 2 (March 1991) discussed maintenance and routine service, while Part 3 (July 1991) outlined equipment and accessories.

By Pat Bartol

Technical Representative, Mobile Lifts Inc.

The long open stretch of rural road shimmered in the late afternoon heat. Barely a tree in sight on the pole line for a good mile and a half and for the construction crew that spelled out dollar bills. There would be nothing to slow down or hinder lashing up a .750inch trunk cable and a .500-inch feeder with it at maximum speed. When being paid by the foot, speed is essential in order to make good bucks. "Bonus time. Let 'er rip."

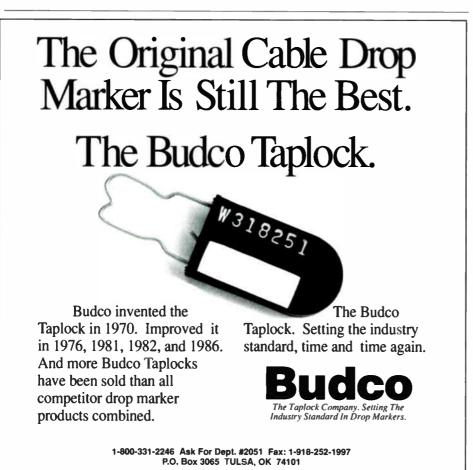
Well look at that would you! What the heck is Mike doing? Mike had just

passed the lashing machine to the other side of the pole, made his loops and secured the lashing wire to the clamp and after placing the snap hooks from the pulling rope to the lashing machine so that the ground hands could pull the lasher, he is now bringing the bucket all the way down again to be moved to the next pole.

Neil Knowsitall

"Hey! Hey Mike, whatcha doin' man? C'mon dude, stay up there and I'll drive the truck to the next pole. You just hold on to the lasher rope and pull the machine from up there and we'll save some time and make more footage today." That of course was from Neil Knowsitall. He's the old hand on the crew who has been around a year or two now including a project down Texas or Arizona way (or so he says). It was something like a 10-mile extension — a real big project.

Neil knows a lot of shortcuts like not wasting too much time on rollers, "One



to a span is plenty," says Neil. Neil also tells a story of the time he and one helper put up 5,000 feet of strand all by themselves including several corners. As Neil says, "Well shoot, it got a little tricky when we couldn't see the strand after the first bend or the #!&@*# trailer either. We just kept pulling off with the bucket truck until the strand tension got a little tight. That's when we went back to check the (ha ha ha) trailer and there it was (heh heh) halfway up the #%!&@# pole. Oh Geez, was that ever funny. The strand snagged on the reel and bound tight and pulled the whole #@%!*# shebang right up the pole." What he doesn't mention is that at the same time about three or four rural route mail boxes were now around 18 feet in the air as well.

I suppose you might be wondering about now what all this has to do with bucket trucks. Well, I'm getting to that. You see, what was happening here is that the guys who knew better were allowing themselves to be influenced by a guy who should have known better. The issue is simple. In order to speed things up, make better time or more money, sometimes people have a tendency to shortcut, which is not really shortcutting but more like gambling. They take a chance on the durability of equipment beyond the manufacturer's design specifications betting on the safety margins inherent in that equipment to allow them to get away with some very dumb things. They don't consider that someone could get hurt or that equipment could be abusively damaged, which could necessitate expensive repairs or long down time far beyond the small amount of time or money saved.

Don't risk it

The gears, hinge pins, bolts, mounts and hydraulics are designed in most cases to function with lifting a certain amount of weight, usually 300 pounds maximum, to a certain height at a certain angle and speed. This 300-pound maximum weight is generally regarded as a 180- to 200-pound man with his tools and test equipment or line equipment, such as a lashing machine. In the case of pulling the

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Cable & Satellite TV Guide P.O. Box 101-391 Taipei, Taiwan Tel: 886-2-506-3335 Fax: 886-2-507-2375 or The Cable Television Association 186, Chung Yang Road, # 7F Nankang District Taipei, Taiwan Tel: 886-2-788-5773 Fax: 886-2-788-5774 lashing machine from the bucket as previously mentioned, the stresses exerted on these components from a fully extended boom (even if only trying to overcome a 100- or 200-pound lateral resistance) is tremendous. It is similar to a large lever prying away at the gear teeth and other parts. Of course the manufacturers purposely over-design in the interest of safety and durability. However, knowledge of this fact should not entice us to stretch the rules from time to time.

The previously mentioned semi-hypothetical story does happen often enough to get concerned about. We have all witnessed it from one time or another. Another common abuse of the lift is using it as a crane to lift heavy objects. I once observed a construction crew lifting a fully assembled 5-meter dish into position on its mount. I'm not sure of the weight of the antenna but I would guess it would have to have been 700-900 pounds and believe me, I held my breath until that thing was bolted into position. I couldn't believe that the bucket and boom would tolerate such abuse without serious damage and also possible injury to the men guiding the antenna. But it did however and I felt at the time that the "big engineer in the sky" had been overlooking that job.

More don'ts

The following are some abuses of equipment and safety rules in the use of bucket trucks. These are definitely "don'ts."

1) Do not allow two people in the bucket at the same time. This usually happens when someone wants to demonstrate something or point something out to another person. Aside from the possibility of excess weight, there simply isn't enough room for two people to work simultaneously.

2) Do not get into a bucket with climbing hooks on and attempt to step out of the bucket onto a pole, roof, tree or some other object.

3) Do not work from the bucket without a safety belt that is properly attached to the belt ring.

4) Do not stand on top of the bucket lip to reach an object beyond the normal reach from the bucket. (This one is surely a widow maker!)

5) Do not get outside of the bucket enclosure for any reason while it is elevated.

6) Do not permit anyone to operate a mobile lift without proper instruction

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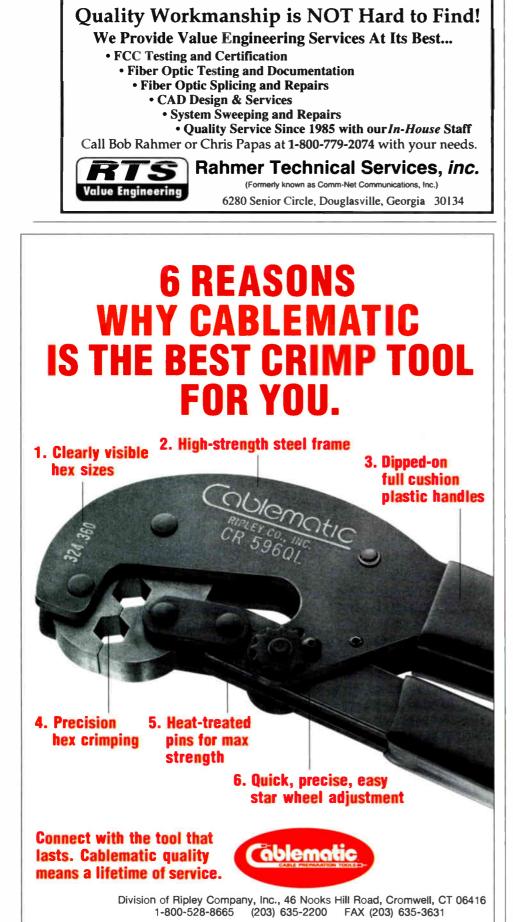
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in the use of the bucket movement controls.

7) Do not continue operation of a mobile lift knowing something is malfunctioning such as leaking hydraulic seals, cracked pins, cracked bucket enclosure, poor stabilizer, etc.

8) Do not operate a lift without a micro-lock and/or wheel chocks in place.

9) Do not use the lift as a crane or in situations where high lateral forces are brought to bear, such as pulling cable or a lashing machine with the bucket.

10) Do not engage in horseplay with your lift such as leaping from the bucket to a pole or tree, standing on the bucket rim, driving down the road with the bucket ascended, etc.

11) Do not subject the bucket and lift arm to unnecessary heavy stresses by pushing through heavy foliage and tree limbs.

The dos

As important as it is to heed the "don'ts," it is equally important to adhere to the "dos" to ensure safe dependable operation of your mobile lift. Some important "dos" are as follows:

1) Do routinely and regularly perform the maintenance functions required such as greasing, checking hydraulic hoses, oil, pumps and electrical systems and switches. Keep a dated record and logs both for in the office and in the vehicle.

2) Do make needed repairs a priority. Do not put off even minor items for another day because it could result in an injury or costly repair later.

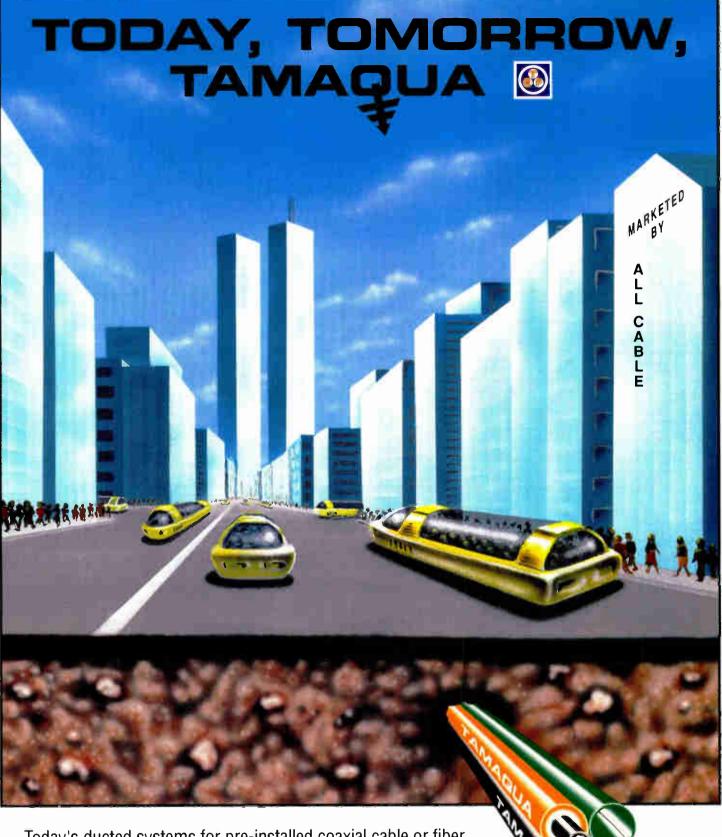
3) Do operate the lift within the rated weight capacity.

4) Do use your lift intelligently and within the range of tasks for which it was designed.

For a long lift life and trouble-free operation of your mobile lift a little common sense is mostly what is required. The lift itself is surely built to perform beyond its stated specifications and the professional maintenance programs will find and correct potential problems before they become major repairs.

Perhaps the two most important tips to good safe bucket truck operation are: Keep that "loose nut" behind the bucket controls well secured and the most important grease to be applied is the "elbow grease" to perform the simple checks that should become routine and second nature to a good lift operator. **BTB**

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DINOSAURS CLUB

Early CATV: Falling tools, shotguns, snakes

By Len Ecker

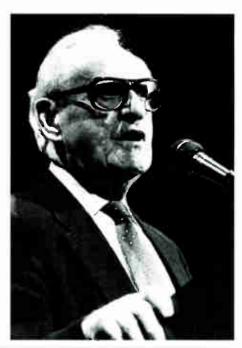
There is so much new and exciting in the world of cable today — fiber optics, digital compression, high definition TV (HDTV) — that it makes an old-timer like me wish I could roll back the years and be young again.

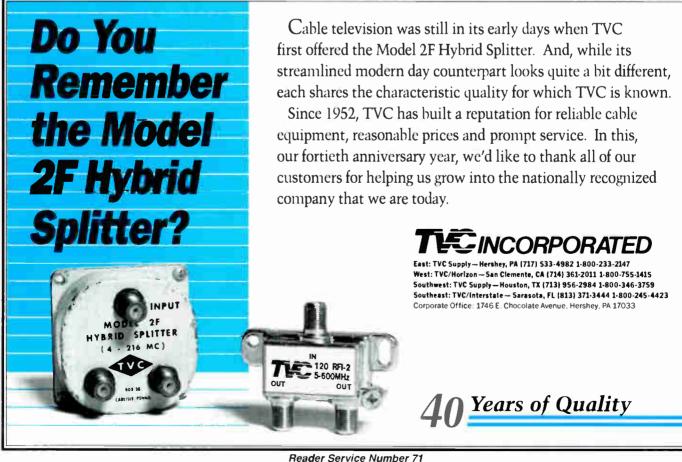
Unfortunately, I can only look back at what was. As I do, I have to wonder how we ever got this cable TV business going when we knew so little. I realize now that nothing in my days at Georgia Tech prepared me for what was to consume 40 years of my life.

My first encounter with cable really wasn't cable at all. I heard about a community in Pennsylvania where an enterprising appliance dealer had picked up some TV signals on a local hill and delivered them into town to help sell TV sets. He'd never heard of coaxial cable, so he used what was available — twin lead. The town center was the county seat — court house, offices and jail and to avoid running the wire around the block he took a direct route: in a window on one side and out on the other.

An "accidental" career

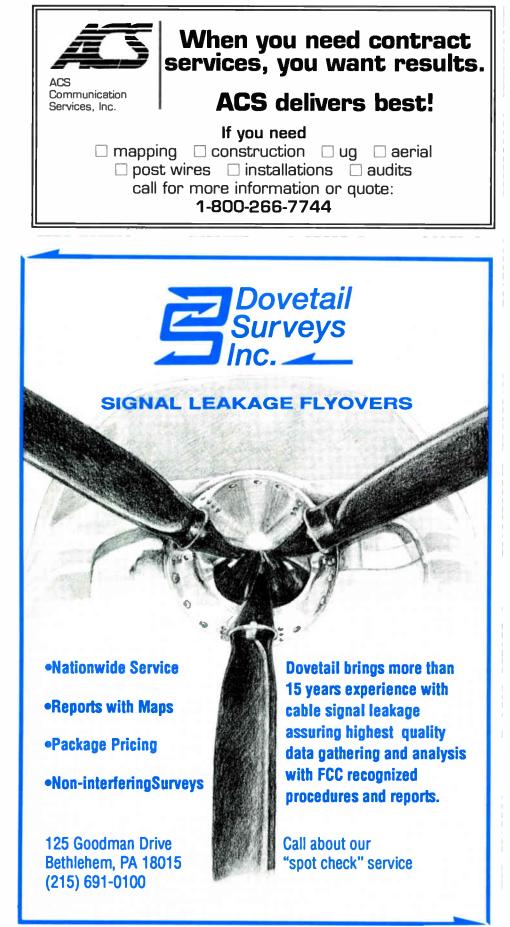
Since I found this interesting, I thought I might like to get involved in this endeavor as a sideline. It looked easy, and the extra money would come in handy for my young family. So I spent a cold winter night on a hill in central Pennsylvania watching a picture that appeared on a TV set. Since I didn't know where it originated, I had to wait for station identification. Finally, I learned the signal was coming from Dallas. Soon after, it disappeared. →





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Since I'd never heard of ducting or temperature inversion, I was at a loss to explain what had happened. Somehow, though, I knew that this signal would never be the basis of a system, and I gave up on the ideal of pursuing this new enterprise. Thus, it was only by accident that I finally became involved in what would be cable TV.

My wife, on a visit to her hometown, met with a neighbor whose husband was seeking an engineer for a new venture. He hired me, and I found myself building a cable system in South Williamsport, Pa.

Those early days were long and hectic. The local mountains provided a way to pick up TV pictures from Philadelphia, which, by those standards of the day, were usable. Since boxing and wrestling were the major TV events, we knew we had a good picture when you could tell the black trunks from the white ones.

Perils on the mountain

Those days on that mountain were an experience I would not want to repeat. To get the best possible reception, we built an H-frame tower so all the antennas might be at the top. A local TV repairman helped in the construction process and turned out to be more a menace than a help. Any time he was on the tower, tools rained down from every pocket. Who'd ever heard of hard hats?

That first winter ice was a major problem. When it rained in town, it invariably turned to ice on the mountain. We soon learned that a shotgun and buckshot would clean the ice off the tower without damage, and we could climb up.

The headend shack was just that, a plywood shanty with cinder block steps. Those steps were to play a dramatic role in my life on the mountain.

These Pennsylvania mountains were well-populated with rattlesnakes and water moccasins. One Sunday I escaped to the mountain to watch a football game. I hadn't bothered to put on the normal knee-high boots I always wore at the antenna site. As I left to go home, I stepped out and bang! — a rattlesnake was sunning himself on the top step. Being a snake, he immediately challenged my right to share the choice position with him. I still have fang marks on my ankle, which, though they've faded over the years, are still faintly visible.

That mountain was loaded with

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wildlife. Besides the snakes there were deer, bears, wildcats, wild turkeys and all sorts of small game. That made hunting season a reign of terror. I conceded the mountain to the hunters for two weeks and waited with bated breath for it to end. If the picture remained on, I heaved a sign of relief. Upon returning to the mountain I always found insulators shot away and bullet holes in the shack. And, if that were the extent of the damage, I felt fortunate.

Having completed the mountain-top site, it became necessary to get the signals off the mountain. Following the road into town was an 18-mile trip. The only other way down was a straight line from the shack to the closest highway - a mere 7,000 feet. With state permission we built a pole line, sliding them down from the top. We learned how fast a pole can move when one of them broke loose and careened down the slope until it finally wedged between two trees and broke in half-quite a feat for a 45-foot class 1 pole.

Life on the mountain was a neverending experience. One day, while working with a technician assigned to me, we were carrying a ladder for some midspan splicing when I heard a distinctive danger signal --- a rattle. I didn't say anything to my partner, and just kept walking. Only after we'd passed out of danger did I stop and point to the bed of rattlers we'd just walked through. You know, it's funny. It was weeks before he'd go up on the mountain with me again.

I learned many things they don't teach in college up on that mountain. For instance, all sorts of animals think PVC, the cable jacket, is a salt lick. They were constantly chewing on the cable. The larger animals, meanwhile, used the poles to scratch themselves so after a while the splinters made the poles poor risks for climbing.

When the day finally arrived that we could see actual TV pictures at the bottom of the hill, I heaved a sigh of relief to be off that mountain. Little did I realize the tough job was yet to come, but, that's another story. СТ

Len Ecker started in the cable industry in 1950 with a five-channel broadband system in Williamsport, Pa. In 1956 he went to work for Jerrold and in 1966 became the engineering advisor to the marketing group. Later he was heavily involved in Jerrold training seminars. Today he owns his own consulting company, The Len Ecker Corp.

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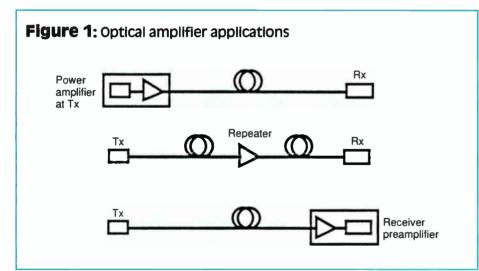
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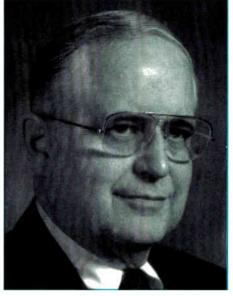


By Lawrence W. Lockwood President, TeleResources East Coast Correspondent

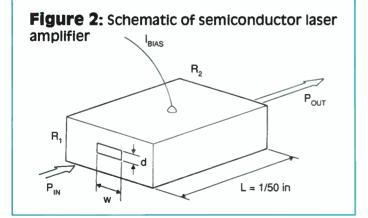
y last column on optical amplifiers was in January 1990. With the speed of developments in this field that corresponds to the ice age, erbium-doped fiber amplifiers have improved and been deployed in the field for applications at 1,550 nm and there have been striking advances in the development of a 1,310 nm fiberoptic amplifier. Production of a satisfactory 1,310 nm fiber amplifier would be of enormous significance to CATV since the installed fiber in CATV (and in general elsewhere) is almost exclusively 1,310 nm — not 1,550 nm.

Currently there are two generic types of optical amplifiers, the semiconductor optical amplifier (SOA) and the erbium-doped fiber optical amplifier (EDFA). Their applications in optical transmission are shown in Figure 1. Using one at the transmitter increases the output level of the optical signal. This is a handy method of

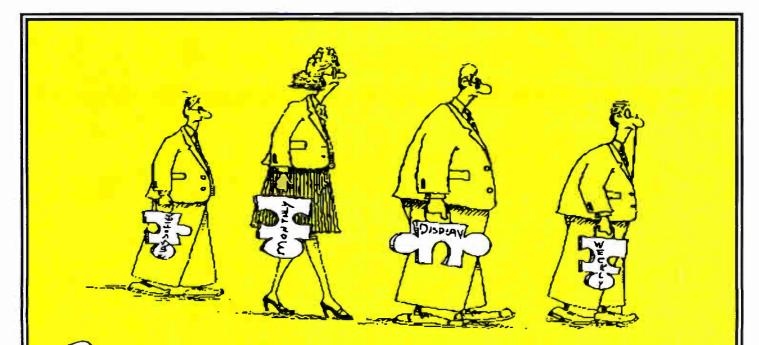




"It looks as if praseodymium-doped fluoride fiber amplifiers will, with further development, come close to meeting the gain and power requirements of an ideal amplifier."







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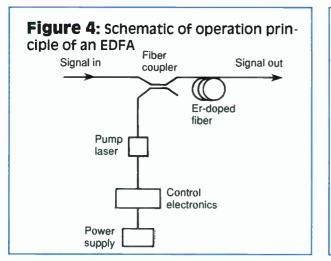


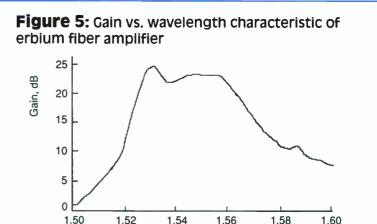
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Signal wavelength, µm

providing sufficient signal levels (power budget) to permit subsequent splitting and branching of the transmission path. Use in mid span permits a longer total path and using one at the receiver permits the use of a signal whose level has decreased to an otherwise unacceptable amount.

Semiconductor optical amplifiers

The SOA uses the same basic construction as the conventional Fabry-Perot semiconductor laser. As shown in Figure 2 on page 86, a typi-

cal SOA has a 500 µm (1/50 in) long buried heterostructure, which is the active region (wxd) that the optical signal enters, traverses the 500 µm and exits amplified. Antireflection coatings (R, and R₂) are applied to the laser facets leaving a residual reflectivity of less than 0.5 percent (in a conventional Fabry-Perot laser the reflectivity is approximately 30 percent). The effect of the greatly reduced reflectivity is to significantly increase the lasing threshold of the device. This means that the operating current and the accompanying optical gain may be increased without the amplifier lasing.

The SOAs are interesting because they can be made in different forms so that they can amplify at 1,550 nm or at 1,310 nm. However, the available performance of SOAs has not promised imminent deployment in fiber-optic systems because they are highly non-linear in operation and also semiconductor gain is highly dependent on the polarization state of the optical input signal, which varies greatly in the output of typical fiber feeding the signal into the amplifier.

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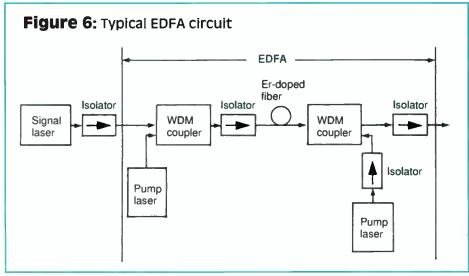
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Correction can be achieved by active monitoring and control of the SOA gain but this adds to the complexity of the optical amplifier. This problem does not exist in fiber-optic amplifiers because the amplification occurs in the doped fiber, which is circularly symmetric and thus insensitive to signal polarization. Compared to EDFAs, the higher noise figures, poorer high-power linearity of SOAs restrict their usefulness in AM analog video transmission but are satisfactory for FM.

The photograph of an SOA (Figure 3 on page 86) shows the heart of an amplifier, the semiconductor package (placed in front of the SOA). This SOA is made by British Telecom and DuPont (BT&D). BT&D has done a great deal of the research and development in the field of optical amplifiers, both SOAs and EDFAs.

Optical amplifiers for 1,550 nm

Figure 4 shows schematically the configuration of a pumped fiber to illustrate the basics of operation of an EDFA. Pump power (usually at either 980 nm or 1,480 nm) is absorbed by the erbium in the length of doped fiber (which is a short 10 to 20 me-



ters in length) creating stored excited state electronic energy. Signal photons then stimulate electronic-to-optical power conversion at the signal wavelength. When input signals are at the 0 dBm level that is typical of signal lasers, the efficiency with which pump photons are converted to signal photons can exceed 80 percent, resulting in output powers greater than 15 dBm. While the fiber provides a gain medium when pumped, when unpumped the fiber becomes very lossy at the signal wavelengths (1,550 nm region). This loss is about 5 to 6 dB per meter of Er-doped fiber, so the total absorption for a typical device may be as high 80 dB. However, in the 1,310 nm region the absorption is very low (in either the pumped or unpumped state), with absorption losses of less than 0.005 dB/m at 1.2 μ m wavelength. The gain vs. wavelength characteristic of erbium fibers is shown in Figure 5.

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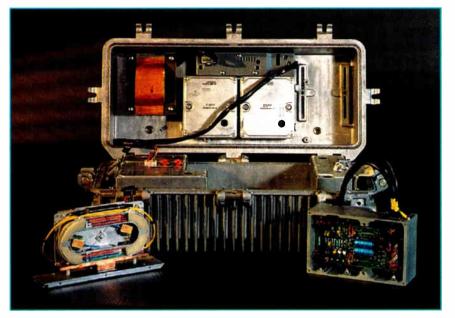


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Figure 7: Optical amplifier (left) and power supply (right) modules, with Jerrold SX amplifier housing specifications



Specifications

Environmental/mechanical Ambient temperature range Power consumption Housing Strand-mount Rack-mount **Optical connectors**

-40° to +60° C 30 watts

SX amplifier 3.5 in (h) x 19 in (w) FC-APC

Operating/performance Pump wavelength Input power Saturated output power Noise figure CSO/CTB distortion

1,480 and 980 nm -6 dBm to +4 dBm, typical 15 dBm, typical 4 dB, typical 70 dBc

There are three possible arrangements for pumping the amplifier. The pump can be fed in at the input of the amplifier (Figure 4 on page 88) so it travels in the same direction as the signal (a propagating pump) or it can be fed in at the output of the amplifier so that it travels in the opposite direction to the signal (counter-propagating pump) or the amplifier can be pumped at input and output (dual or bidirectional pumping). It may seem intuitively wrong to amplify using a pumping beam travelling against the signal, but after all the sole function of the pumping beam is to excite the erbium ions so that they can provide the signal amplification and it doesn't matter in which direction that exciting beam comes from. The gain of the amplifier is not affected by pumping configuration. Figure 6 on page 89 shows a typical EDFA circuit.

A joint development program between Jerrold and BT&D produced an EDFA that is packaged in a standard Jerrold housing. The amplifier has a gain of approximately 15 dB. Its current price is \$30,000. (See Figure 7.)

At a recent meeting of the Optical Society of America (OSA), interesting

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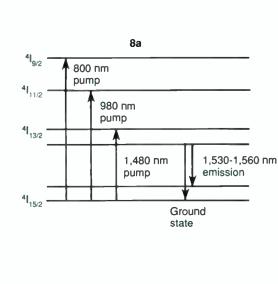
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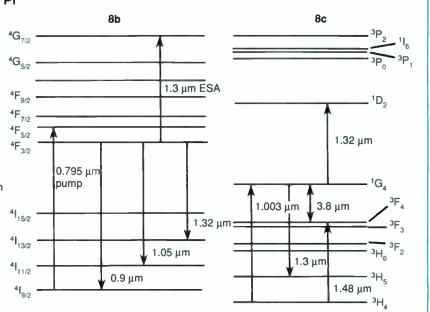
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Figure 8: Energy levels of Er, Nd and Pr

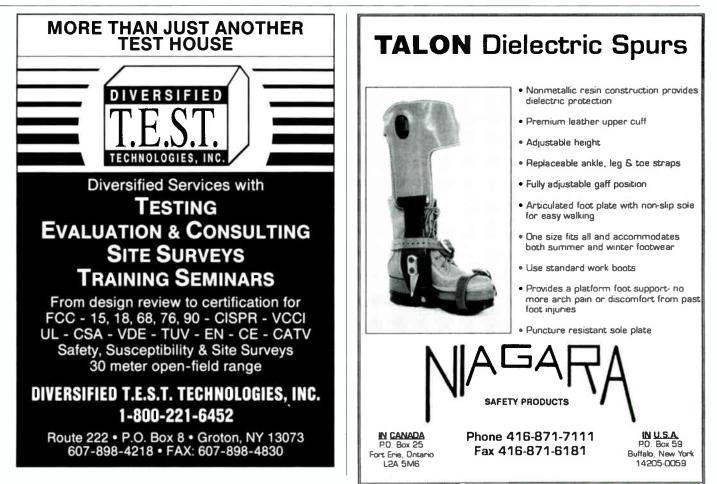




work with fiber amplification was reported. Distributed amplifiers, made by lightly doping the fiber and pumping its entire length, promise a "lossless" fiber. Analysis coupled with experimental results indicates that with erbium concentrations of about 1 ppm and 70 mW pump lasers spaced at 30 km (19 mi) intervals, a lossless fiber can be achieved. One group demonstrated a lossless fiber length of 14 km at a signal of -10 dBm, and another showed that a lossless 19x19 star coupler can be made using 19 amplifier fibers and a single 980 nm pump.

Optical fiber amplifiers for 1,310 nm

But how to get a fiber amplifier for 1,310 nm since erbium, the amplifying dopant, will amplify at 1,550 nm only? In the January 1992 issue of *Optics & Photonics News* (a publication of the Optical Society of Ameri-



Comparison of optical amplifier properties

Net gain Output power Bandwidth Center wavelength Pump Noise figure Status

**BT

SOA 20 dB +3 dBm 45 nm ≅ 7,900/5,600 GHz 1,300 or 1,500 nm Electrical

Electrical 8-10 dB Commercially available EDFA 35 dB +15 dBm 45 nm ≅ 5,600 GHz

1,500 nm 980 or 1,480 nm 3-4 dB NDFA 7 dB +14 dBm 30 nm ≅ 5,300 GHz PRFA 32 dB (reported)* +20 dBm (reported)** 25 nm (predicted) ≅ 4,400 GHz

 1,300 nm
 1,300 nm

 795 nm
 1,010 nm

 3-4 dB
 3-4 dB (expected)

 Experimental but PRFA is promising

ca), M. Brierly of BT Labs presented a most interesting report on the current status of development work in the 1,310 nm amplifier field.¹ (British Telecom, BT, is the British part of BT&D.) In this report he sets out an ideal specification for a 1,310 nm amplifier:

"Ideal specification: An ideal optical amplifier for 1.3 µm will be capable of high gain, greater that 30 dB (100 times) between the incoming and outgoing fiber. It will amplify signals at least from 1.28-1.31 µm wavelength, and preferably shorter and longer, simultaneously and with the same gain at all wavelengths. It will operate bidirectionally with minimum extra noise added to the signal. It will not be sensitive to signal polarization. It will not have any interference between signals with the gainbandwidth (crosstalk), and will operate on both analog and digital signals from kbit/s to multi-Gbit/s. It would be very linear over a wide range of input levels and capable of high output power operation under saturated conditions. It should be reliable and self contained, i.e., should not depend on physically large pump lasers, and should be power efficient. These are very difficult specifications to meet, but the EDFA comes close in all but wavelength — hence the reason for researching a 1.3 µm alternative."

A good deal of experimentation has been conducted with doping another rare earth element, neodymium, but these have only so far produced an amplifier with 10 dB gain at 1,345 nm for only 50 mW pump power. This amplifier departs from the ideal specification in that the gain is low and is also at too long a wavelength.

A further, and currently the most promising, option is the praseodymi-

um-doped amplifier - praseodymium being yet another of the rare earth elements. S. Davey, a BT scientist, first observed fluorescence at 1.3 µm in praseodymium-doped ZBLAN glass in 1989 and suggested that amplification might be possible. (ZBLAN is a heavy-metal fluoride glass.) The fiber doped with Pr is ZBLAN glass rather than silica. The year 1991 seems to have been "the year of the praseodymium-doped fiber amplifier," with many publications appearing, each with better results than the last. However, none of the results come close to being "ideal" in one major respect, i.e., power efficiency. The pumping wavelengths for Pr are 1,007-1,017 nm and at this time such pumping lasers are not commercially available.

However, Y. Miyajima of NTT in a recent report to the OSA announced work at NTT that achieved a 38.2 dB





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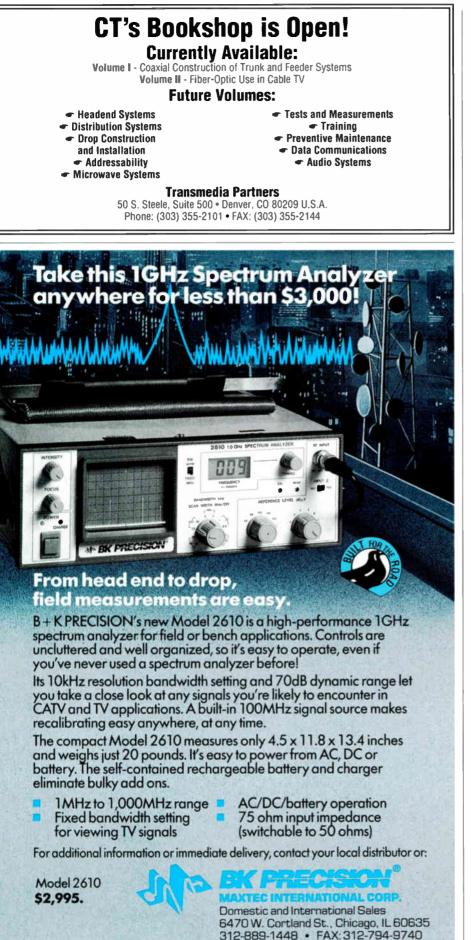
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July	May 15	IBC (International Broadcasting Convention) Amsterdam, The Netherlands	December	October 15	The Western Cable Show Anaheim, California, USA
			*Exhibition	dates, locations	s and distributions are subject to
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signal change, equivalent to about 32 dB of true amplifier gain in the fiber used. More significant perhaps is the fact that the pump power to achieve this gain was only 300 mW, and that usable amplifier gains were obtained from only 100 mW of pump power.

So, it looks as if praseodymiumdoped fluoride fiber amplifiers will, with further development, come close to meeting the gain and power requirements of an ideal amplifier. But what about the other requirements? NTT researchers report a saturated output power of 8 mW in their high gain fiber, but BT Labs report 100 mW in a less power efficient fiber, which certainly satisfies the output power requirements. The noise figure (the degradation in signal-to-noise ratio) of the BT device was estimated to be less than 6 dB, and could be lower. For those interested in the quantum energy levels involved in Er, Nd and Pr, they are shown in Figures 8a, 8b and 8c respectively on page 91.

The accompanying table on page 92 shows typical operating parameters for all the optical amplifiers discussed.

Conclusions

Is Pr the ideal 1.310 nm amplifier? The answer is obviously "no, not yet," but the praseodymium-doped fluoride fiber amplifier comes far closer than any other. It has the inherent linearity, low crosstalk and polarization insensitivity of other fiber amplifiers and fits the bill in terms of gain, output power and noise requirements. Perhaps the suspect area is in the efficiency (0.2 dB/mW compared to 11 dB/mW for the EDFA), and pump source availability. However, it is less than one year since the first report of gain in this system. and with developmental work progressing apace we might be surprised sooner rather than later. СТ

References

¹ "Progress On Optical Fiber Amplifiers for 1.3 μm," M. Brierly, *Optics & Photonics News*, January 1992.

² Fiber Optics Communications Handbook, Technical Staff of CSELT, Edited by F. Tosco, Tab, 1990.

³ "Optical Amplifiers Make Their Move", J. Mellis, *Lasers & Optronics*, August 1991.

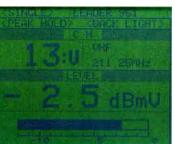
⁴ BT&D specifications.

⁵ Jerrold specifications.

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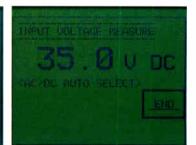
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Reader Service Number 98

MAY 1992 COMMUNICATIONS TECHNOLOGY

AD INDEX

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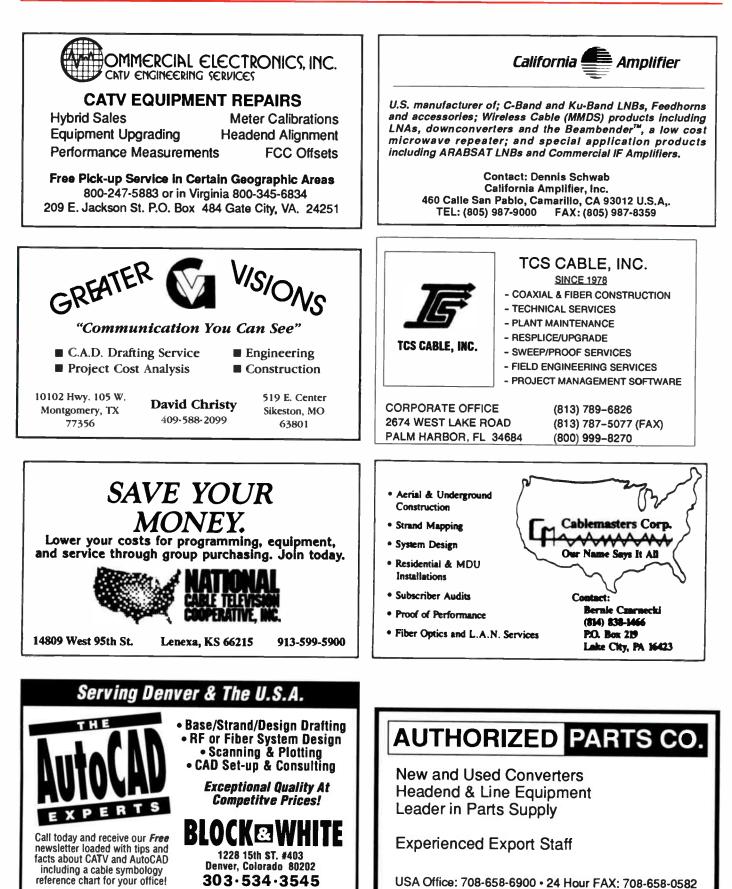
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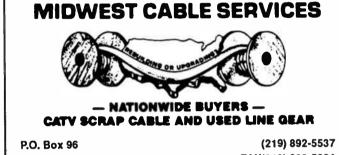
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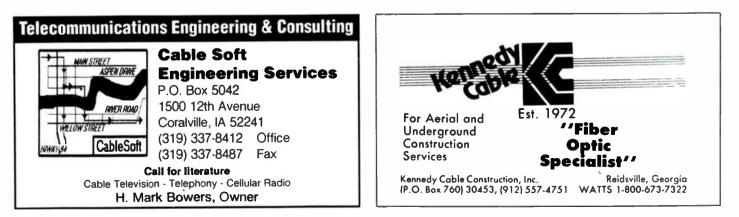
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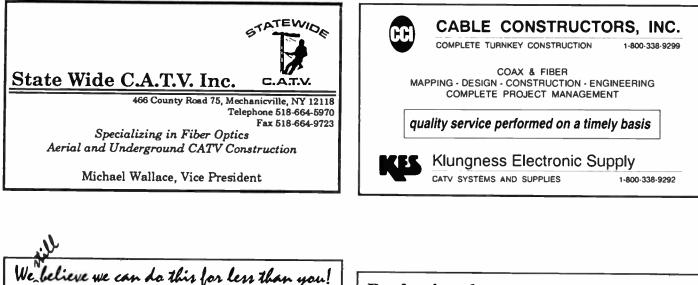
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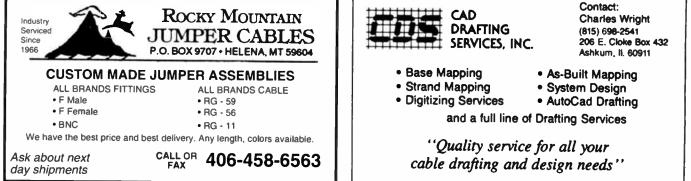
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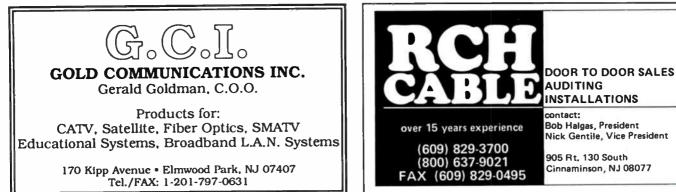


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CITY OF MORGANTON

Marketing Coordinator for new cable television system, city of Morganton, NC. A progressive southern community of approximately 15,000 cit-zens. Recent election held voted for municipal construction and ownership. Position to be filled during construction of system. Duties will involve marketing cable tv, developing and implementing advertising and promotional materials. Will super-vise a small staff of customer service employees. Will provide liaison with programming, community access and civic programming committee. Skills: public speaking, marketing, writing, and develop-ing materials. Should be computer literate, Prefer college degree in marketing or related field and experience. Excellent benefits. Call Personnel Director (a application and information conclusion) Director for application and information package at 1-704-438-5255, or write and send resume to: Personnel Director, P.O. Drawer 430, Morganton, NC 28655. Closing date: May 8, 1992. Equal Opportunity Employer. FAX: (704) 438-5264.

CATV MANAGER: City of Morganton, NC. New municipal system in progressive southern com-munity of approximately 15,000 citizens. Recent election held voted for municipal construction and ownership. Position to be filled at beginning of construction of system with approximately 100 miles, 5000 subscribers. Position will oversee construction, when completed will manage sys-tem. Successful applicant will be self starter, highly motivated with strong electronic background as well as headend experience. Knowledge and experience with fiber optics is major plus. Supervisory experience important. Five plus. Supervisory experience important. Five years cable operations experience with some management experience desired. Excellent ben-efits. Call Personnel Director for application and information package at 1-704-438-5255, or write at P.O. Drawer 430, Morganton, NC., 28655. Closing date: May 8, 1992. Equal Opportunity Employer. FAX: (704) 438-5264.

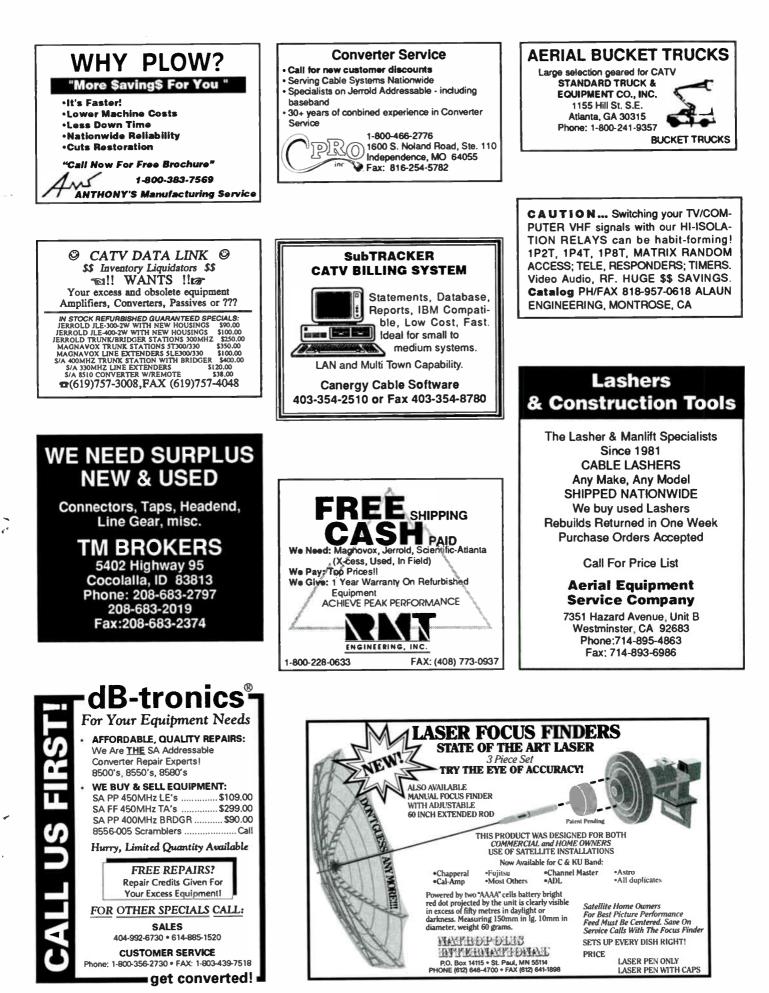
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Equipment





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December 1991 BPA Publisher's Statement.

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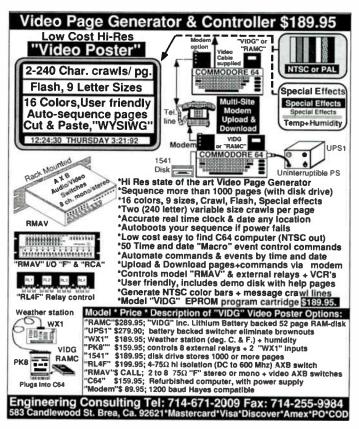
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PRODUCT NEWS



Fiber storage

Optical Networks International introduced its FiberLoop fiber-optic storage unit designed to accommodate extra lengths of fiber along aerial support strand. The product is said to permit establishment of installation practices concerning the storage of extra fiber and ensures installers do not violate the minimum bend radius of fiber.

The units can be attached at any location along the support strand and at splice locations to store and protect the fiber bend radius of extra lengths of fiber. At splice closures, the Fiber-Loops store the additional fiber needed to reach a splice vehicle. The design allows the units to be stacked for multiple cable applications and the products can be installed inside a headend equipment building to accommodate arrangement of equipment racks. In this case, the units can be mounted on the ceiling or equipment rack. Four design configurations are available. The Model FOSS-1 is used for single cable loop AT&T fiber with four to 48 fiber counts (10-inch bend diameter). The Model FOSS-2 is used for a dual cable loop AT&T fiber with four to 48 fiber counts (10-inch bend diameter). For larger fiber counts, the Model FOSS-100 was designed to handle AT&T fiber with 49 to 96 fiber counts and Siecor's armored cables of two to 60 fiber counts (Siecor fiber requires a 12inch bend diameter). The Model FOSS-200 is used for AT&T fiber with greater than 96 fiber counts (16-inch bend diameter). This model also can be used for Siecor's armored fiber with 61 to 120 fiber counts (16-inch bend diameter).

Reader service #204

TDR

Riser-Bond Instruments introduced its Model 1220 time domain reflec-

tometer. The unit has long-range readability to 65,000 feet (19,500 m) and high precision accuracy (± 0.01 percent). It also has an exclusive automatic cursor placement feature, waveform storage/comparison, and a multilevel/function noise filter.

It can be used for troubleshooting aerial and underground cables as well as cables in conduits and behind finished walls. As well, the unit can be used for measuring cables on-the-reel and during new cable installations. Other uses include testing cables for shipping damage, cable shortages, cable usage and inventory management. The instrument is portable, weighing under 10 pounds.

Reader service #203

Light source

The LP-5100 series of LED light sources was introduced by Laser Precision Corp. The products are handheld, modulated LED light sources designed for field use. They operate at both continuous wave and modulated modes (270 Hz and 2 kHz). Single wavelength models are available at 850 nm and 1.300 nm wavelengths. Dual wavelength sources are available in 850/1,300 nm and 1,300/1,550 nm models. LP-5100 series light sources can operate up to 10 hours on fully recharged NiCad batteries. They also can be powered using the AC charger/adapter included with each source or run on alkaline batteries.

Applications include attenuation measurements using the CW mode, splicing, connectorization, end-to-end testing of installed links, and fiber identification using the modulated modes. Each model comes with an operator's manual, AC charger/adapter and a soft pack carrying case.

Reader service #202

Compatible set-tops

Scientific-Atlanta announced its Model 8600 addressable set-top terminals can now be used in certain Zenith and Jerrold scrambling systems. By being compatible with other scrambling systems, the unit can be installed without requiring the dual carrying of scrambled services.

In addition to compatibility, the unit has self-revealing menus and prompts

in simple English. On-screen features (including channel name and number, time and mute) are said to upgrade older TV sets. Ordering and confirmation of pay-per-view (PPV) events appear on-screen and automatic onscreen notices remind subscribers when the PPV event is about to start. Other menu-driven on-screen features available when using the product include VCR programming up to eight events over 14 days, preselected favorite channels, parental control, sleep timer, on-screen volume control and large display with up to 240 characters per screen for messaging and up to 16 pages per message. Video baseband and RF sync suppression scrambling techniques provide more than 100 different modes of scrambling. Operators can reserve maximum levels of random video and sync inversion for the most valuable premium and PPV programming.

Reader service #189



Fiber microscope

Noyes Fiber Systems introduced the Model OFS 300 fiber-optic inspection microscope. It offers 200x precision optics for viewing polished fiber connectors or cleaved fiber ends. It uses the company's universal adapter mount to interface all commonly available fiber connectors to the instrument,

The product features backlighting and battery operation or AC adapter input. It also has a tripod mount for laboratory use.

Reader service #198

Sweep system

New from Avatron is a low-level sweep system including the Model AT60G sweep reference test generator and a Model AT60R sweep/spectrum analyzer. The microprocessor-controlled system uses the company's patented low-level sweep technology

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that allows true continuous sweeping with real-time display.

The sweep/analyzer can be programmed to facilitate manual measurements, make decisions, perform calculations, interact with the operator and is fully compatible with the company's Model CR/CT4000 sweep systems. A built-in frequency counter provides the capability to measure modulated video and audio carriers as well as 4.5 MHz intercarrier spacing. Microprocessor power adds storage capabilities for up to 64 control settings and 100 documented measurements recorded in non-volatile memory for later viewing, printing or transferring to a personal computer. The technician sees things as they happen using continuous noninterfering sweep without loss of resolution. A RS-232C communication port is included for data transfer and remote system monitoring capabilities. Reader service #197

Digital tuners

Jerrold announced its DCR-3000 tuners will have aesthetic changes so Digital Cable Radio subscribers can enjoy an enhanced look that is said to blend seamlessly with home entertainment systems. According to the company, the tuners' dimensions have been maintained. The company also reported that future models will incorporate a six-pin Molex connector digital output port for interfacing with digital tape machines.

Reader service #196



Spectrum analyzer

The new Model FSM spectrum analyzer from Rohde & Schwarz has >100 dB intermodulation-free dynamic range and a low-noise floor that is typically -142 dBm (6 Hz BW) at 26 GHz, according to the company. Signals of interest can be captured without the introduction of spurious frequency components over the full 100 Hz to 26.5 GHz range.

Accuracy and low phase noise are attained through fundamental mixing using an integrated diplexer, six-stage tracking filter and mixer together with a spectrally pure synthesizer. The company says the quasi-continuous, variable resolution bandwidth and dynamic, multivariable correction techniques facilitate fast sweeps with flat frequency response. AM and FM demodulators with calibrated outputs provide full modulation analyzer capability. The product can make manual and automatic test routine measurements. Results are viewed on a high-resolution color monitor with grids, test curves, parameters and markers. The onscreen display range is 110 dB. Reader service #195



BERT system

The Model 110/210 gigabit bit error rate test (BERT) system was intro-



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duced by Broadband Communications Products. It is said to be ideal for testing digital communications links and components at rates from 10 Mb/s to over 1.1 Gb/S. The Model 110 data sequence generator and the Model 210 error detector make up the system. Each unit is 5x12x12 inches and weighs 15 pounds.

Three selectable PN sequence lengths of 2⁷-1, 2¹⁵-1 and 2²²-1 are provided. Clock-to-data phasing can be adjusted in 200 ps steps within a 1.2 ns range in both the generator and detector. Both single error insertion and constant 10⁻³ bit error insertion are available for system verification. Four error calculations are made continuously and include total errors, error rate, percent error-free intervals and errored intervals. The detector has a GPIB interface for data acquisition and control. **Reader service #194**

Oscillator

Piezo Crystal Co. announced the availability of its Model 2900082 oscillator. It uses the company's SC cut crystals. The frequency range is from 4 to 15 MHz.

Typical phase noise at 10 MHz is -110 dBc/Hz at 10 Hz, -140 dBc/Hz at

100 Hz, -160 dBc/Hz at 1 kHz, and -165 dBc/Hz at 10 kHz. The aging rate at time of shipment is 5×10^{-10} /day. Frequency stability is $\pm1\times10^{-8}$ over a temperature range of -40° to 70° C. Vibrational sensitivity is 1×10^{-9} /g. **Reader service #191**



Cable locators

The Path Finder 8840 and Path Finder 8850 portable locators are new from Rycom Instruments. They are designed to identify buried cable or pipe. Features of the products include ABS plastic construction, a one-piece receiver design with built-in probe, a peak/null meter with audio tone and an automatic transmitter load matching.

The units are powered by alkaline batteries. Both models have low frequency conductive coupling. The Model 8850 has the capability of high frequency inductive coupling and an optional flexi-coupler.

Reader service #193



FO talk set

Meson Design & Development's DB-118 LANTALK fiber-optic talk set uses a single fiber and can be operated with its headset or through a built-in mike and speaker. It can be voice-operated or used in a push-to-talk (PTT) mode. Combined with the firm's JU-414 bare fiber adapter, the talk set can be used from the onset of an installation. **Reader service #192**

State State St



May

12: SCTE Cascade Range Chapter seminar. Contact Cynthia Stokes, (503) 230-2099.

12: SCTE Desert Chapter, BCT/E and Installer exams to be administered. Contact Chris Middleton, (619) 340-1312, ext. 258.

12: SCTE New York City Chapter seminar, fiber measurement, Time Warner, Flushing, N.Y. Contact Rich Fevola, (516) 678-7200.

12-13: SCTE Ohio Valley Chapter seminar, BCT/E Category II, "Video and audio signals and systems," and Smart House, Cincinnati (12th) and Cleveland (13th). Contact Jon Ludi, (513) 435-2092.

12-13: SCTE West Virginia Mountaineer Meeting Group seminar, OSHA and safety, Ramada Inn, Charleston, W.V. (12th) and Holiday Inn, Clarksburg, W.V. (13th). Contact Joe Jarrell, (304) 522-8226.

12-14: Magnavox CATV mobile training seminar, San Francisco. Contact Patricia Morgenstern, (800) 448-5171 or (800) 522-7464 (in New York state).

13: SCTE Cascade Range Chapter, BCT/E exams to be administered in all categories, Paragon Cable, Portland, Ore. Contact Cynthia Stokes, (503) 230-2099.

13: SCTE Florida Chapter, BCT/E exams to be administered in all categories at the technician level, Continental Cablevision, Pompano Beach, Fla. Contact Pat Skerry, (904) 735-1571.

13: SCTE Great Plains Chapter seminar, coax/fiber upgrades, fiber-to-the-feeder and future applications, Crown Court Quality Inn, Bellevue, Neb. Contact Jennifer Hays, (402) 333-6484.

13: SCTE Oklahoma Chapter seminar. Contact Arturo Amaton, (405) 353-2250.

13: SCTE Magnolia Meeting Group seminar, compression technology and coaxial cable characteristics, Ramada Inn Coliseum, Jackson, Miss. Contact Steven Christopher, (601) 992-0445. 14: SCTE Mid-South Chapter seminar, digital compression, Howard Johnson's, Senatobia, Miss. Contact Scott Young, (901) 365-

1770, ext. 4150. 14: SCTE Penn-Ohio Chapter seminar, safety, Sheraton Hotel, Warrendale, Pa. Contact Bernie Czarnecki, (814) 838-1466.

14: SCTE Satellite Tele-Seminar Program, earth station site planning. To air from 2 to 3 p.m. ET on Transponder 6 of Galaxy I. Contact SCTE, (215) 363-6888.

14: SCTE Wheat State Chapter, BCT/E exams to be administered in all categories, Red Coach Inn, Wichita, Kan. Contact Mark Wilson, (316) 262-4270.

14: NCTI seminar, highway safety, Denver. Contact (303) 761-8554.

16: SCTE Golden Gate Chapter, BCT/E exams to be administered, Viacom, Pleasanton, Calif. Contact Michael Gorin, (510) 534-3364.

16: SCTE Cactus Chapter seminar, CLI and broadband test equipment. Contact Harold Mackey (602) 358-5860, ext. 135.

17-18: SCTE Old Dominion Chapter seminar, Holiday Inn, Richmond, Va. Contact Margaret Davison, (703) 248-3400.

18: SCTE North Country Chapter, Installer exams to be administered, Sheraton Midway, St. Paul, Minn. Contact Bill Davis, (612) 646-8755.

18-20: New York State Commission on Cable Television and SCTE TechPlanning ahead June 14-17: SCTE Cable-Tec Expo '92, San Antonio, Texas. Contact (215) 363-6888. Sept. 8-10: Eastern Cable Show, Atlanta. Contact (404) 252-2454. Sept. 15-17: Great Lakes Cable Expo, Cleveland. Contact (517) 482-9350. Oct. 13-14: Atlantic Cable

Show, Atlantic City, N.J. Contact (609) 848-1000. Dec. 2-4: Western Cable Show, Anaheim, Calif. Contact (415) 428-2225.

nology Update '92 (18th annual northeast technical seminar and trade show), Roaring Brook Ranch, Lake George, N.Y. Contact Al Richards, (518) 474-1324.

18-21: Siecor seminar, fiber installation, splicing, maintenance and restoration for CATV, Siecor Training Facility, Hickory, N.C. Contact (800) SIECOR 1, ext. 5539.

18-22: ONI Fiberworks '92 seminar, ONI Training and Product Development Center, Englewood, Colo. Contact Ray Reynard, (800) FIBER ME.

18-22: Hughes seminar, AML microwave equipment for local signal distribution. Contact (310) 517-5633.

19: SCTE Chattahoochee Chapter seminar, satellite communications, Perimeter North Inn, Atlanta. Contact Hugh McCarley, (404) 843-5517.

19: SCTE Southeast Texas Chapter seminar, fiber-optic design and maintenance, Warner Cable office, Houston. Contact Rosa Rosas, (409) 646-5227.

20: SCTE Bluegrass Chapter seminar, BCT/E Category VII, "Engineering management and professionalism." Contact Liz Robinson, (606) 299-6288. 20: SCTE Central California Chapter, seminar, BCT/E Category II, "Video and audio signals and systems." Contact Jim Robinson, (209) 835-4037.

20: SCTE Dixie Chapter seminar. Contact Scott Peden, (904) 968-6959.

20: SCTE Gateway Chapter seminar, basics of fiber optics, fiber system design, fiber splice enclosures and fiber test equipment, Joe Hannon's Restaurant, Maryland Heights, Mo. Contact Chris Kramer, (314) 949-9223.

20: SCTE Greater Chicago Chapter seminar, construction. Contact Bill Whicher, (708) 362-6110.
20: SCTE Michiana Chapter seminar, Turner's Ameri-

can, South Bend, Ind. Contact Russ Stickney, (219) 259-8015. 20: SCTE Mount Rainier

Chapter seminar. Contact Sally Kinsman, (206) 938-8787.

20: SCTE Piedmont Chapter seminar, BCTE Category V, "Data networking and architecture," PCNs, telco bypass and office-to-headend data ties, Charlotte, N.C. Contact Tod Dean, (919) 757-0279.

21: SCTE New Jersey Chapter vendor fair (tentative). Contact Jim Miller, (201) 446-3612.

21: SCTE Heart of America Chapter seminar, fiber technology. Contact Don Gall, (816) 942-3715.

26-28: Magnavox CATV mobile training seminar, San Francisco. Contact Patricia Morgenstern, (800) 448-5171 or (800) 522-7464 (in New York state).

27: SCTE Southern California Chapter seminar, safety and risk management. Contact Tom Colegrove, (805) 251-8054.

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PRESIDENT'S MESSAGE

remembers the Alamo!

By Wendell Woody

SCTF.

President, Society of Cable Television Engineers

On't be overrun for lack of adequate technology ... "Remember the Alamo!" Maintain your communications link for all the new emerging technologies ... "Remember the Alamo!" Training for survival ... "Remember the Alamo!" SCTE Cable-Tec Expo '92 ... "Remember the Alamo!"

CATV industry technical leaders, engineers and technicians are all massing in great force to move on the Alamo in June. Thereupon, they will attend this year's SCTE Engineering Conference at the San Antonio Convention Center in Texas.

The conference will open with a dynamic panel on digital compression exploring expanding channel capacity while enhancing video and audio quality. Then all the great technical "generals" from Washington D. C., will address CATV technical compliance and how Federal Communications Commission reregulation will impact your system operations and maintenance practices.

With the industry focus on customer service, a panel of delegates from state cable commissions will expound on how our industry is meeting the subscriber expectations. For a better today and a look into the future the panel session titled, "Current events in cable TV technology: Fiber optics, HDTV, PCN and outage reduction" will be most inspiring.

Expo workshops

Once again, there will be six workshop periods and 10 workshops to choose from in planning your schedule. This year's workshop subject materials are all new, exciting and most timely. Here they are for your review: "Assessing your system's picture quality"; "BCT/E certification - An overview of technical certification and related category examinations"; "The best of Fiber Optics Plus '92"; "Customer Service ----Doing the job right the first time"; "EBS and the cable industry"; "How will the new NEC, NESC and OSHA regulations impact your system?"; "One-onone with the FCC"; "Outage reduction techniques"; "Primary testing under technical reregulation"; and "Secondary testing under technical reregulation."

Pre-meetings

Arrive early! On Friday, June 12, the National Cable Television Association Engineering Committee will meet from 9 a.m. to 6 p.m. On Saturday, June 13, NCTA will sponsor a seminar on "Reregulation of Technical Standards." It is scheduled from 9 a.m. to 5 p.m. Both meetings will be at the convention center. Pre-registration for the seminar is mandatory and seating is limited to the first 300 applicants. Call the NCTA at (202) 775-3639 for more information.

Post-meetings

Stav late! On Wednesday morning, June 17, four of the SCTE engineering subcommittees will meet. In-Home Cabling (wiring) and Emergency Broadcast System (EBS) subcommittees' meetings are scheduled from 7:30 to 9:30 a.m. Interface Practices and Cumulative Leakage Index (CLI) subcommittees' meetings are scheduled from 9:30 to 11:30 a.m. You will be able to attend portions of all four or two of them in their entirety. Make sure your travel schedule will accommodate your attendance at these meetings. BCT/E and Installer Certification testing also will be conducted on Wednesday morning from 8:30 a.m. to 12 p.m.

National Cable-Tec Games

The second National Cable-Tec Games will be featured during Expo Evening. The Games are a competition among CATV system personnel centering around technical tasks and knowledge. After each event, points are awarded by the judges for each contestant based on speed, accuracy and performance parameters. First, second and third place Olympic-style individual medals are presented to the winner of each event. The event is supported by a national SCTE subcommittee (chaired by Ron Wolfe of ATC Training Center in Denver). He can be reached there at (303) 753-9711 for more details.

Welcome new directors

Re-elected to seats on the national SCTE board were: Tom Elliot, TCI (atlarge); Jack Trower, WEHCO Video (Region 8); Mike Smith, Adelphia Cable (Region 10); and Walt Ciciora, ATC (Region 12). New board directors to be seated at our June meeting in San Antonio are: Norrie Bush, Columbia Cable (Region 3); Wayne Hall, Warner Cable (Region 4); Mark Wilson, Multimedia (Region 5); and Terry Bush, Trilithic (Region 7). Join me in welcoming these new directors aboard. Congratulations to all election winners.

Meeting the members

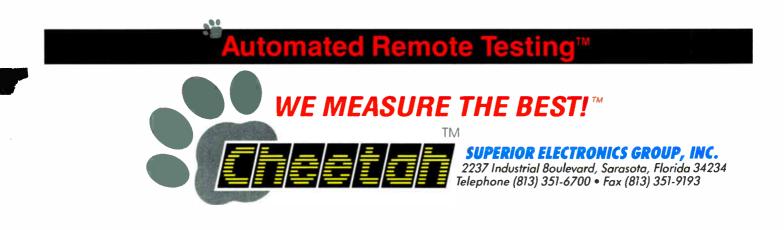
"The state of the industry" was the program title for a recent Greater Chicago Chapter meeting. The guest speakers were: The Honorable Dennis Hastert, U.S. Representative, Illinois; Gary Maher, president, Illinois Cable Television Association; Russell Monie, FCC regional director, Chicago; Chris Scott, general manager, Jones Intercable; and I represented the SCTE as president. Chapter officers supporting the program were: Bill Cohn, Kevin Walker, Bill Whicher, Nick Theroux, Bob Runchy, John Grothendick, Wes Schick, Jason Shreeram, Joe Thomas, Brian Hurd, Bob Hill and John Fedorky.

The SCTE was pleased to develop and conduct the technical program for this year's North Central Cable Show. We had technical panels, an OSHA safety session, BCT/E testing and followed with a two-day "Technology for Technicians" seminar by SCTE's Ralph Haimowitz. We certainly appreciated the assistance and support from the officers of the SCTE North Country Chapter: Bill Davis, Kelly Booth, Lanny Sparks, Matt Haviland, Jimmy Schulz, Scott Gunderson, Scott Melter, Wes Schick and SCTE Region 6 Director Rich Henkemeyer.

SCTE meetings and functions were most successful at both the Texas Cable Show and the L'ARK Show in New Orleans. We acknowledge the excellent membership support from Lee Anderson, Darrell Eichelberger and Jim Wood from the Ark-La-Tex Chapter; Terry Blackwell, Mark Webb and national Director Les Read from the North Central Texas Chapter; Rosa Rosas and Tom Rowan from the Southeast Texas Chapter; Charles Thibodeaux, Leroy Naguin, and Kevin Smith from the Miss/Lou Chapter; and Bob Griffith from the new Ozark Mountain Meeting Group. СТ



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See us at the NCTA Show, Booth #1614. Reader Service Number 97