

SPECIAL SUPPLEMENT ULTRA HI-FI DESIGN

electronics today

SEPTEMBER 1978

INTERNATIONAL

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Windscreen Wiper
Delay Unit

Space Shuttle
Communications

Light Chaser
Project

A woman with long, wavy blonde hair is smiling and looking towards the camera. She is wearing a thin chain necklace with a white, teardrop-shaped pendant. The pendant has a small black rectangular component and the infinity symbol (∞) printed on it. The background is a solid red color.

LED Pendant

The competition don't like the sound of this at all.

For quite some time, other manufacturers have been trying to produce tape with the qualities of the Maxell UD-XL. At the same time, Maxell have been quietly perfecting an even better series.

The UD-XL I and UD-XL II tapes are designed to attain maximum performance at the ferric and chrome position on your tape deck. Whichever tape position you choose, Maxell can give you a better performance.

UD-XL I TAPE, FOR FERRIC (norm.) POSITION (120us)

UD-XL I offers an excellent sensitivity of 1 dB higher than even UD-XL. MOL performance is also 1 dB higher over the entire audio frequency spectrum. The result is a new standard in ferric tape, with wider dynamic range and less distortion than ever before.

How does the UD-XL I compare then, with ordinary low-noise tapes?

Sensitivity is higher by 2.5 dB, and MOL performance by as much as 6 dB.

Yet, for all this UD-XL I requires no special bias or equalization. Simply set your tape selector as you normally would at the ferric position – but there the comparison ends.

UD-XL II TAPE, FOR THE CHROME POSITION (70us)

UD-XL II tape is such a dramatic improvement on most other tape that can be used in this position, that comparison is really unfair.

For example, if you're familiar with conventional chromium-dioxide tape, you'll know of the associated problems of poor output uniformity – plus low maximum output level and rather high distortion.

UD-XL II tape offers you excellent MOL, sensitivity, and an output improvement of more than 2 dB over the entire frequency range.

Maxell's unique 'Epitaxial' process gives you absolute sensitivity and stability, and no drop-out problems. What's more, the shells are moulded in diamond cut dies, and made to tolerances 5 times greater than the Philips standard. And, like all Maxell tapes, UD-XL II has the 5-second cleaning leader.

In short, if you're recording in the chrome position, you can now achieve all the advantages – with none of the drawbacks.

A prospect we think you'll find very exciting – even if the competition don't.



For details on all Maxell Recording Tape write to Maxell Advisory Service, P.O. Box 49, Kensington, N.S.W. 2033

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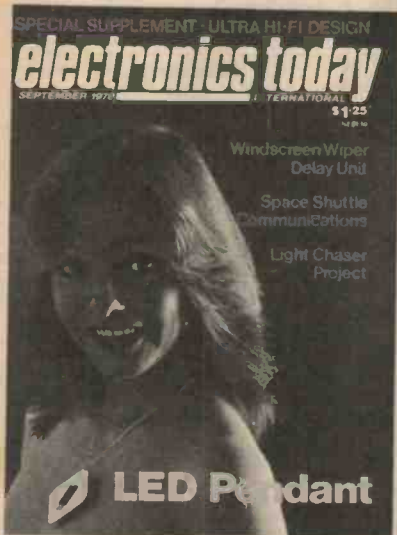
INTERNATIONAL

Editorial: Les Bell

Publisher: Collyn Rivers

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Sometimes you want lots of proximity effect.

"The Mike With Guts"

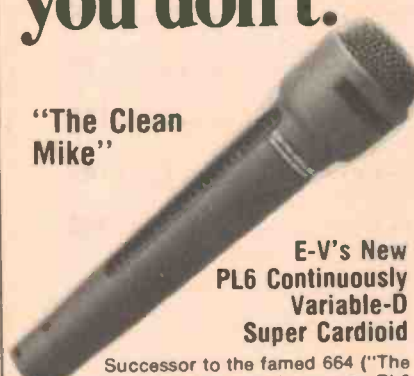


E-V's New PL91 Dynamic Cardioid

Proximity effect. It's that husky bass boost a singer gets working close to the mike. It's just one of the things our new PL91 does better than other mikes. Make a comparison test. We think you'll find that the PL91 provides greater gain before feedback than the mike you are using now — or any competitive mike. You'll also find that our sophisticated shock mounting assures superior rejection of handling noise. And it's got all the tough-as-nails ruggedness you expect from an Electro-Voice microphone.

Sometimes you don't.

"The Clean Mike"



E-V's New PL6 Continuously Variable-D Super Cardioid

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News Digest

Wind Turbine Test

The 200 kW experimental wind turbine generator at Clayton, New Mexico, has been inspected after its first six months of operation. Although the inspection revealed that most components are wearing normally, 3 small cracks and many loose rivets have been found in the blades. The NASA Lewis Research Centre, which manages the large wind turbine portion of the DOE, will conduct an inspection and analysis to determine the blades' wear and life potential.

Speak and Spell

Texas Instruments' new speech synthesizer has found a new application in teaching children commonly misspelt words. The unit asks a user to spell a word and after buttons are pressed in response, will tell the user whether or not the correct answer has been indicated.

New Oscilloscope Camera

A new, low price oscilloscope camera, the Model 7000, is now available from BWD Electronics Pty. Ltd.

The Model 7000 has been completely updated. It incorporates an improved shutter and lens, with eight speeds ranging from 1 second to 1/125 second, and aperture control from f3.5 down to f32. As well as hand-held operation, the new 7000 can be used for permanent mounting with the range of precision oscilloscope adaptors. According to BWD, this is the first time that a low priced camera has been available with a choice of mounting systems.

The new camera weighs less than 680gms and is highly portable. It produces fully developed 83 mm x



108 mm (3 1/4" x 4 1/4") quality prints with virtually no picture distortion in just 30 seconds, so it is quick and simple to check that all relevant data has been recorded. It needs no focussing, and the exposures can be accurately controlled to take account of the brightness of the display and type of CRT phosphor used. Once the initial settings have been determined, changes are seldom necessary.



For further information please contact *BWD Electronics Pty. Ltd., Miles Street, Mulgrave, Victoria, 3170* or *P.O. Box 325, Springvale, Victoria, 3171.*

BWD540 - New Data Sheet

A new comprehensive data sheet is available from BWD Electronics Pty. Ltd., which fully describes their DC-100MHz dual trace oscilloscope, the Model BWD 540.

The data sheet provides full details of the specification for the oscilloscope and illustrates details of the Line Selector Module, BWD 701, which can be fitted in conjunction with a battery pack, BWD BP3 making the whole unit a completely portable data base suitable for communications, video and computer applications.

The BWD 540 oscilloscope is claimed to combine laboratory accuracy and versatility with true field portability and is well suited to all forms of logic circuitry from DTL to ECL.

Further details from: *BWD Electronics Pty. Ltd., Miles Street, Mulgrave, Vic 3170.*

Cheap Holograms

Somewhere we've heard a rumour that the CSIRO National Measurement Lab has succeeded in producing full-colour, 3-D holograms using ordinary light bulbs. This technique eliminates the need for lasers, reducing the cost and reducing the associated safety requirements. We don't normally pass on rumours, but this one really had us baffled. Would anyone at CSIRO like to either confirm or deny it?

Melbourne Parts Supplier

A new electronics store has opened in

the North Melbourne suburb of Coburg, supplying a range of components, kits and hardware. Centrally located in the Coburg shopping centre, you can find Tasman Electronics at *12 Victoria St., Coburg, VIC.*

Holographic Memories

Research by the Plessey research labs at Towcester in England points to 'photonics' as the successor to electronics as a data storage and retrieval medium. Chemical behaviour known as photochromism offers the prospect of a dense holographic memory which can be read, written and erased like magnetic tape. Plessey hope to have a prototype by mid-1979.

Price of Progress

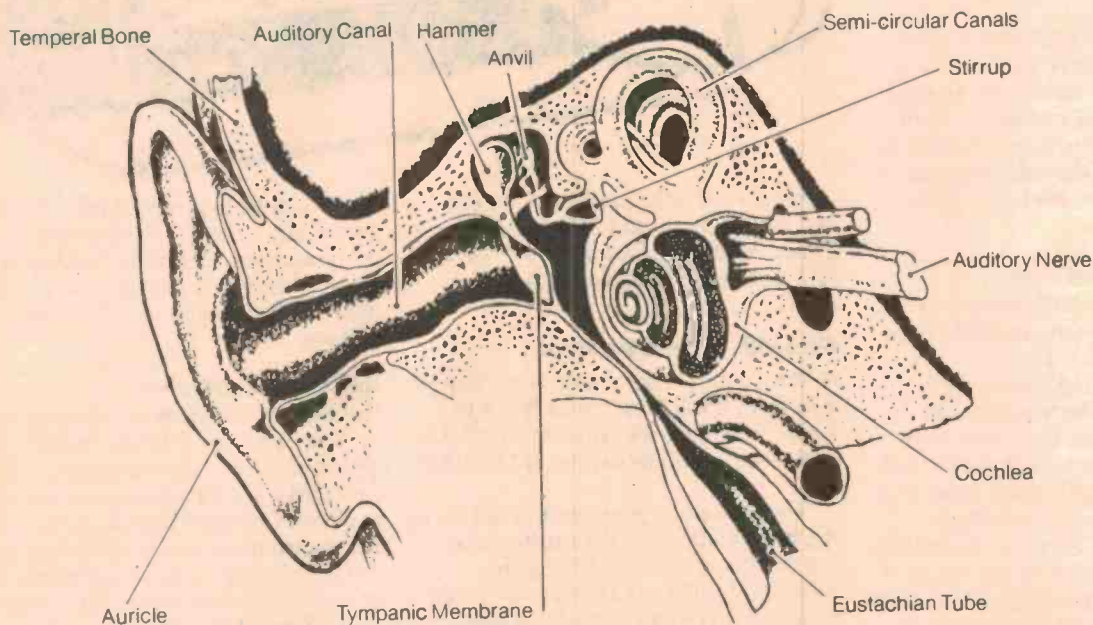
Sad tale of the month - seeking a way to make fuel to run his tractors, L. Crombie of Webster Minnesota designed a solar fuel-alcohol still made of plywood and thin plastic sheet. Trying to apply for a licence for his still, Crombie received a huge packet of materials which required that he be bonded, have an environmental study made, and once approved, would have tax and Treasury agents eyeing him up - the whole process taking about 2 years. Crombie went ahead and built his still, but then made the mistake of saying too much to the local sheriff's deputies.

No charges have been laid against Crombie yet.

Power Transistor

General Electric has developed a Darlington transistor capable of switching 400V and 350A in 1 μ s with an external drive of only 0.1 A. Key to the new device is a new copper package/heatsink design.

TO JUDGE THE QUALITY OF OUR NEW MAGNETIC CARTRIDGES WE MADE USE OF THE MOST SOPHISTICATED MEASURING EQUIPMENT AVAILABLE.



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For that reason each and every step on the way to our new line of magnetic cartridges was carefully monitored by the Ortofon "Golden Ear Panel". We believe that a good cartridge should produce perfect sound rather than convincing diagrams. And we trust you feel the same.

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New Catalogue

Electronic (Distributors), suppliers of electronic components and equipment, have just issued their 1978 Catalogue and Product Selection Guide. The catalogue lists a comprehensive range of products suitable for government and industry as well as providing quite a lot of product information to assist in the selection of the right component for specific applications.

Copies of the catalogue will be mailed free of charge by writing on a company or departmental letterhead to *Electronic (Distributors), PO Box 33, Pendle Hill, NSW, 2145.*

Low Distortion Function Generator

The New B & K Precision Model 3010 Function Generator is claimed to offer convenient use and excellent waveform accuracy at a moderate price. Frequency coverage spans 0.1 Hz to 1 MHz in six ranges, with each range providing linear 100:1 frequency control.

Push-button range and function selection provides fast, error-free operation. The stable voltage-controlled oscillator (VCO) of the 3010 is varied on each range by the front panel frequency control, or the VCO external input. A 0 to 5.5V ramp applied to the VCO external input will provide a 100:1 output frequency change. By applying such an input ramp, the 3010 can be used as a sweep generator for response measurements in audio and I-F circuits. When an audio signal is applied in place of a ramp, the 3010 will produce a direct FM output.

The 3010 features a variable DC offset control which provides up to $\pm 5\text{VDC}$ (into 600 ohm) combined with the selected audio output frequency. Engineering applications for this feature include evaluation of the effects of: DC bias on an AC circuit, an audio transformer approaching saturation and shifted operating points of a DC coupled amplifier. The DC offset function can even be used to simulate a DC power supply for the evaluation of power supply filter networks. When used in this manner, the 3010 output can be tuned to simulate the line frequency input of the "model" power supply.

For square-wave operation, the 3010 offers a fixed TTL output level and a variable amplitude output. Variable output square wave rise or fall time is 100 nanoseconds or less; TTL square wave rise/fall time is 25 nanoseconds or less. Square-wave symmetry at 100 kHz is a near-perfect 99%. In addition to response tests, the square-wave outputs are ideal for clock-pulse substitution in digital circuits.

The triangle-wave function is always useful when linearity tests are required. Small amounts of distortion indicated by non-linear changes in a waveform are easier to detect on a triangle wave than on other common waveforms. For that reason, triangle-wave linearity is a highly important specification. Again, the 3010 generates a near-perfect output by providing 99% triangle-wave linearity at 100 kHz.

As a sine-wave generator, the 3010 is conservatively rated at less than 1% distortion from 0.1 Hz to 100 kHz; less than 0.5% is typical. Above 100 kHz, harmonics are suppressed by over 30 dB at maximum output amplitude.

For further information contact Bruce McCarthy, *Parameters Pty. Ltd., 68 Alexander St., Crows Nest NSW 2065.*



Solar Panels

Soanar Electronics Pty. Ltd. is now a distributor for the Philips type BPX 47A Silicon Solar Panel. The panel consists of an array of interconnected solar cells that convert solar energy directly into usable electric power. Full sunlight is not essential for operation, as the solar cells continue to supply energy even under overcast conditions.

In optimum conditions a single solar panel will deliver 11 watts of power at 15.5 volts. Several panels can be connected together in series or parallel to provide the output required for a specific purpose.

Construction of the panel consists of

34 series-connected solar cells of 57 mm diameter moulded in transparent resin and sandwiched between two clear glass plates. An edge seal of silicon rubber framed with aluminium edging completes the assembly and prevents the ingress of dirt and moisture. Overall dimensions of the panel are 468 x 365 x 15 mm and the unit weighs a mere 2.4 kg.

The Solar panel is suitable for use under severe environmental conditions and conforms to the requirements of relevant IEC tests with respect to elevated and freezing temperatures, humidity, wind pressure, salt spray and blown sand. Thus it is ideally suited to charging batteries in boats, caravans and holiday homes or for power equipment in remote or isolated areas.

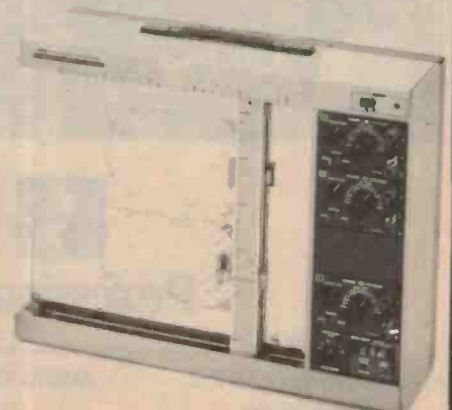
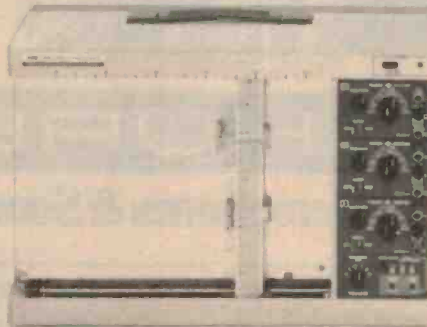
Soanar Electronics will be maintaining stocks of the BPX 47A Solar Panel at their branch and agents' stores in all states. Full technical specifications are available from *Soanar Electronics Pty. Ltd., 30 Lexton Road, BOX HILL, VIC. 3128.*


Two New X-Y Recorders

Parameters has announced the release to two new YEW X-Y Recorders Models 3036 and 3086. Both are designed for A4 size paper and the writing areas are 250 mm x 180 mm and 250 mm x 250 mm respectively.

Accuracy is maintained at $\pm 0.25\%$ and the sensitivity is 5uV/cm. Optional input ranges include 19 ranges from 5uV/cm to 5V/cm or for 13 ranges from 0.5mV/cm to 5V/cm. Both units are suitable for bench-top or rack-mounting and are supplied with disposable felt-tip pen cartridges for high quality traces. Electrostatic paper holddown and "light spot" paper alignment is incorporated.

Built-in time base is standard with 3036 and optional on model 3086. For further information contact Bruce McCarthy, *Parameters Pty. Ltd., 68 Alexander St., Crows Nest, NSW 2065.*





fact: Shure's up front with Maynard Ferguson... and backstage too!

The Performance

Maynard settles for nothing short of the finest . . . in his music, in his arrangements, in his creativity, in his road engagements, in his band. And in his microphones and sound system. That's why he insists on a Shure SM58 microphone. That's why engineer Tony Romano puts the sound together on Shure SR consoles.



The Sound

Maynard builds it from feelings, ideas, crescendos, rhythms, harmonics, and layers of raw sound.

Shure's professional SR sound equipment performs superbly even in Maynard's most demanding sets. It projects his trumpets to everyone—whatever the size or shape of the hundreds of clubs and halls he works. Take it from Maynard . . . Shure performs. That's the up-front information. And the backstage story, too! Shure . . . the Sound of the Professionals.



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News Digest

Electronic Yoghourt

Yes, electronic yoghurt! The latest home yoghurt maker released by Rolmex Electro Inc. of Quebec, Canada, uses an electronic temperature controller instead of a conventional thermostat, to hold temperature constant to within 0.5 degrees. Because of this, it is claimed the Yogourmet completes incubation of yoghurt in 4 hours, 2 or 3 times faster than most conventional home yoghurt makers.

Latest From Polaroid

Not content with making extraordinarily simple-to-use cameras with instant results, Polaroid are now going one further by offering an auto-focussing camera. The SX-70 Sonar One Step uses a very sophisticated sonar technique, bouncing sound waves off the subject to obtain correct focus in all light levels, yet will retail for around \$20 more than the standard SX70 model. The same feature will also be added to the Pronto range.

Humidity Meter

An electronic version of the wet and dry bulb psychrometer has been designed by J. de Yong of the CSIRO Div. of Chemical Technology. The instrument has two temperature sensors, one dry and the other covered with a wet sleeve, and will measure atmospheric humidity to better than 0.5%.

Dickie's Anniversary Sale

Next month, October, marks the 10th anniversary of the creation of the Dick Smith empire (or kingdom, as it was then). Accordingly, and being the nice chap he is, Dick is holding a 10th anniversary sale, with a mini-catalogue in every copy of next month's ETI. So don't miss the October ETI or you'll miss out on some bargains!

Asean Trade Fair

A number of electronic manufacturers will be among the exhibitors at the first Asean Trade Fair which is being held in Sydney at the MLC Centre from October 23 - 28. The Fair, which will involve all five Asean nations - Indonesia, Malaysia, the Philippines, Singapore and Thailand - will include displays of FM two way, long range HF/SSB and clock radios, electronic and mechanical toys, cassette recorders, burglar alarms and colour TV sets.

Television and radio components from the Tanin Industrial Company in Thailand are also scheduled for display.

The fair is for trade visitors only, although part of two days - Thursday afternoon and evening and Saturday, the last day of the exhibition - will be

open to the general public. Invitations and catalogues have been sent to the trade but more are available on request. Simply ring 20622 and ask for Dick Fletcher, Asean Trade Fair, at the Department of Trade and Resources, or call into their offices at 181 Castle-reagh Street.

PCB - Mounting Electrolytic

A new style of electrolytic capacitor that allows large capacitance values to be mounted directly onto a printed circuit board has just been introduced by Soanar Electronics Pty. Ltd.

Designated, 'Type RP' this capacitor is generally similar to the conventional can electrolytic except that the terminations consist of a three-wire configuration instead of the usual solder pins and securing lugs. Two of the wires provide the usual electrical connections of the capacitor while the third wire acts as an anchor to provide stability to the PCB mounting.

Soanar Electronics are stocking an initial range of values, at their head office, interstate branches and agents stores, comprising 2500uF in 35V, 63V and 80V DC WkG, and 5600uF in 40V DC WkG. This initial range will shortly be expanded to meet the total requirements of the local market.

Further details and technical specifications are available on application to Soanar Electronics Pty. Ltd., 30 Lexton Road, BOX HILL, VIC. 3128.



New Bankstown Store

Radcom Pty Ltd, who for the past 4½ years have specialised in the supply of military communications equipment, are opening a new component supply store at 105-109 Eldridge Rd, Bankstown. As well as a wide range of components, including the Silicon Valley range of semiconductors, the store will sell kits, test gear and instruments.

CB for UK?

A working party of the UK National Electronic Council has concluded that "A high quality form of citizens' band radio service should be introduced in the United Kingdom". The report, which was published in the May-June issue of National Electronics Review, recommends the use of either SSB or FM somewhere between 100 and 500

MHz. Curiously, the report recommends also that each sideband transceiver would have to be phase locked to the 200 kHz standard frequency transmission from Droitwich - a requirement which, to our minds, would be almost impossible on both technical and economic grounds, as the 200 kHz transmissions cannot be received satisfactorily in some parts of the country.

The report, by such a prestigious body as the NEC, allied with the mobile radio manufacturers' keen interest in CB (c.f. Philips in Australia) surely must mean that the Home Office cannot be so certain in their opposition to CB.

Teletext System Rivalry

The UK Post Office has not completely swept the field with its Teletext system, and in fact, there is now some fairly heavy political manoeuvring going on in the electronic conference chambers of Europe. The problem is the French, who with characteristic Gallic tenacity, have set about developing their own Teletext/Viewdata system, called Antiope. This is not compatible with the UK Teletext system, but has the advantage of being able to handle the seven alphabet sets required for all European languages.

Rumours are rife that Antiope will be the Teletext system used at the Moscow Olympics in 1980, and this would be a major propaganda coup for the system.

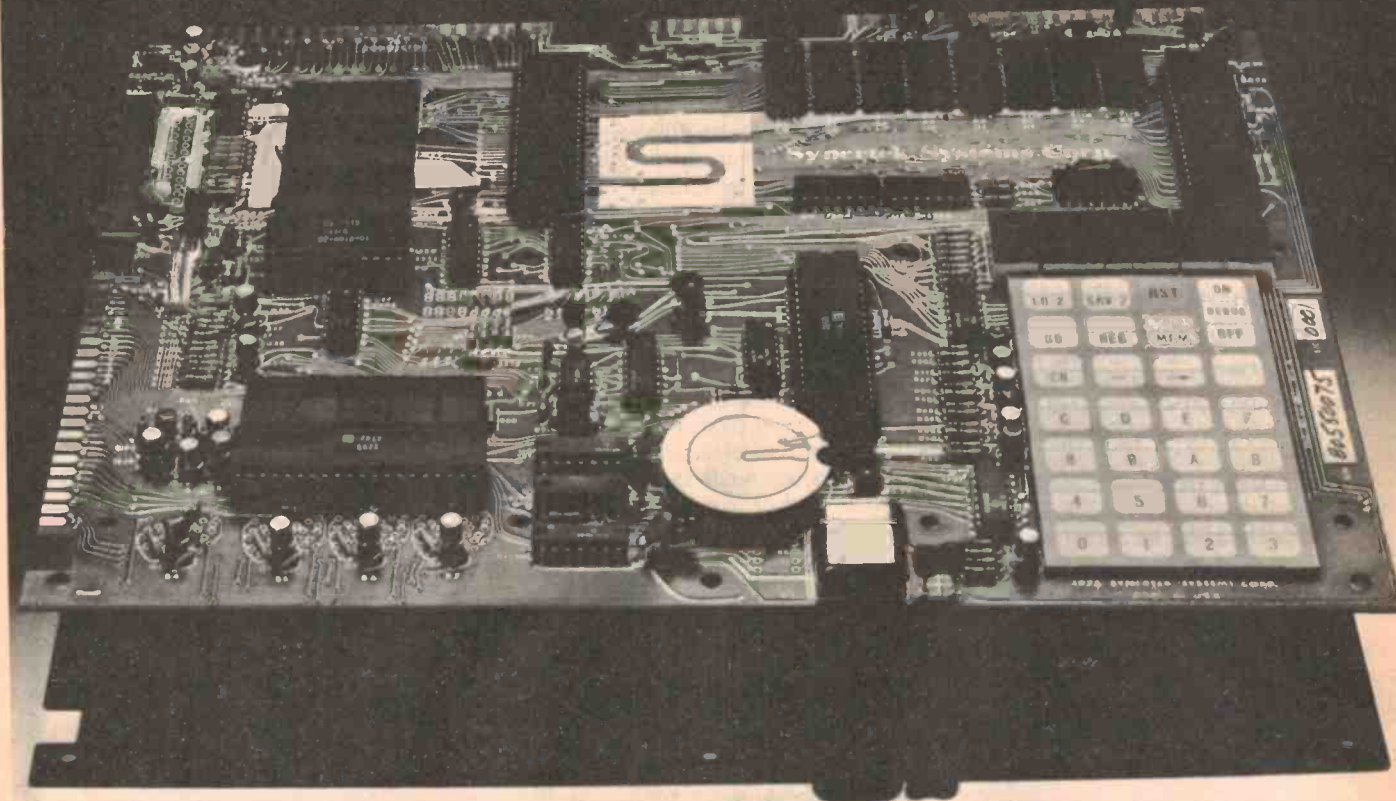
Fortunately for the UK interests, Antiope is not yet available to the French public, whereas Viewdata and Teletext equipment has been sold to West Germany, the Netherlands and Australia; although the French are trying hard to show the Germans the disadvantages of Teletext, which cannot display accents such as umlauts without modification.

Incidentally, the Viewdata service provided by the UK Post Office is now officially known as Prestel.

Computer Courses

To coincide with the recently introduced range of Central Data 2650 micro-computer systems and kits, Rod Irving Electronics have announced that they will be running microprocessor courses in September. The courses will be oriented toward the hobbyist, ranging from basic understanding of micro-processors to a general understanding of systems, followed by using and programming the Central Data 2650 system. Course Details may be obtained from Rod Irving Electronics on (03) 489 8131.

Finally. A dependable microcomputer board.



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- Microprocessor CPU's; 6502 available up to 3 MHz.
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- Asynchronous Communications Interface Adapter; 6551 available Nov. 1978.
- Mini Floppy Disc Drives; MICROPOLIS: S100 and SBC80 bus compatible. 1, 2 and 4 disc systems available.

Batteries Standard

The Standards Association of Australia has published a revised standard on Primary batteries, to supersede AS C387-1967, Dry primary cells and batteries. In this revision, only those batteries which are in common use in Australia and which are appropriate for inclusion in new designs, have been included. A battery designation system, based on the International Electrotechnical Commission system, has been specified and with the increasing use of this system, it is expected that consumers will soon see a reduction in the proliferation of different type numbers — all identifying the same battery. A further requirement in the standard is that, batteries are marked with a 'use by' date.

Design and construction requirements and performance criteria have been given in the revised standard. The tests specified are all intended to simulate, as closely as possible, several applications for which batteries are commonly used and include lighting, transistor radios, toys, calculators and watches. Copies of AS 2176 (\$7.60) may be obtained from the offices of the Association in the state capitals and Newcastle. Postage and handling 80 cents extra.

Electronics Trade Fair Tour

In conjunction with Astrid International Tours of Sydney, Mr. Steve Colman is organising a trip to visit 3 important Electronics Shows in Japan, Korea and Taiwan.

During the tour Tour members will be able to visit, if they wish, the following exhibitions and trade fairs:

Japan Electronics Show
Japan Measuring Instruments
Exhibition

Japan Analytical Instruments Show
JETRO Exhibition at Tokyo Trade
Centre

Korea Electronics Show
Korean Autumn Fair 1978
KOTRA Permanent Exhibition
Taiwan Electronics Trade Fair
Taiwan Toys and Gifts Show
CETDC Exhibition in Taipei

Mr. Colman emphasised that while members will have the assistance of the various Government Export Councils and will have the opportunity to enjoy their help and in some cases hospitality, it will be an organised Tour only as far as travel and accomodation is concerned. It will be up to the individual member to decide which exhibition he wishes to visit and ample time will be available for independent negotiations, visits to manufacturers factories, etc.

The cost saving is quite considerable over individual travel costs. Not including meals the tour will cost \$1420 or \$1590 if single room is required, subject to more than 15 acceptances.

For further particulars contact Steve Colman (02) 498-1622 who will be escorting the Group.

Schools Computer Fayre

The Computer Science Department at La Trobe University is organizing Victoria's (and in fact Australia's) first "Schools Computer Fayre". Pupils at all Victorian schools are invited to participate by submitting any work they have done which is related to computers. The Fayre will be held in October, on the La Trobe Campus.

The Fayre was conceived by Dr. Harvey Cohen as providing an opportunity for the display of computer projects, and to arouse interest in computing in Victorian schools. There will be prizes in a range of categories: these prizes have been donated by various firms concerned with computers, micro computers, and electronics.

Students are offered the following suggestions as to the sort of entries expected:

- Hardware — a microprocessor-based control system
- a general-purpose micro-computer system
- a digital logic circuitry
- Software — commercial program
- scientific program
- game-playing programs
- an original application
- Other — animated flow diagram
- essay
- carton
- model built of computer scrap, etc. etc. etc.

Prizes will be given for the best entries; details will be announced later, but there will be at least one prize in each of the levels Form 1 and 2, Forms 3 and 4, and Forms 5 and 6. Some certification will be required that the entry is the work of the person or group submitting it; an entry fee of \$1 per entry will be charged.

The Fayre will be held at the end of October at La Trobe University, and all are invited to visit it, whether or not they have submitted entries.

For further information, write to *Computer Fayre, Computer Science Department, La Trobe University, Bundoora, VIC. 3083.*

Propagation Predictions

Once again, our propagation predictions seem to be ill-fated — this month, restrictions on computing time meant that the predictions could not be got to us on time, so they have had to be omitted for this month. Our apologies, and please bear with us — normal propagation will, hopefully, be resumed next month.

Radiation Supported Mirror

Oregon University Institute of Theoretical Science are proposing a mirror to reflect VHF and UHF transmissions, which would be held aloft at an altitude of 100 km by the radiation pressure of the 10 MW erp signal it was reflecting.

ETI/Unitrex Calculator Contest

The July contest obviously stumped almost all of you, as there were only a very few correct entries. The contest, you may remember, was to use the digit 4, four times in an equation, and to do this six times over to make the equations equal all the digits from integers from 70 to 75 inclusive. John Nicholson, of Salisbury, NT, got the right answers (though several are possible): his answers are:

$$70 = 44 + 4! + \sqrt{4}$$

$$71 = \text{Antilog} \sqrt{4} - (\text{Antilog} \sqrt{4/4}) - 4$$

$$72 = 44 + 4! + 4$$

$$73 = \text{Antilog} \sqrt{4} - (\text{Antilog} \sqrt{4/4}) - \sqrt{4}$$

$$74 = 4! + 4! + 4! + \sqrt{4}$$

$$75 = \text{Antilog} \sqrt{4} - \left[\frac{\text{Antilog} 4}{\text{Antilog} \sqrt{4}} \right]$$

To those of you who only got solutions for 72 and 74, commiserations; we were finding it pretty tough going ourselves!

For this month's contest, we racked our brains to come up with a good puzzle that would be fun and challenging but found that we were better at solving the darn things than making them up! We've got a few old favourites in stock, but everyone must know the answers by now! So, this month, to make it easy for ourselves, we're running a 'Design A Contest' Contest, in which we want you to write in with ideas for brain-teasers suitable for use in the ETI/Unitrex Contest in future issues. They should be short, amusing, of reasonable difficulty and preferably of unique solution to make it easy to judge.

So this month, write your entry down, stuff it in an envelope and mail it to ETI/Unitrex Calculator Contest, Electronics Today, 15 Boundary St., Rushcutters Bay, NSW 2011. We will award a calculator for every puzzle used, and the closing date is Friday, October 6th.

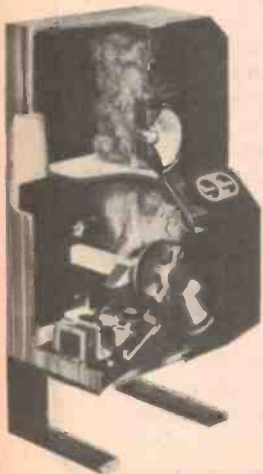
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DM7 is the first of a new loudspeaker family reflecting our computer-aided research programme. It is a compact 3 unit system employing entirely new drive units in an enclosure engineered to exceptionally high standards. Many advances have been incorporated to reveal new horizons in loudspeaker performance, making possible a standard of musical reproduction unequalled in an enclosure of this size. The DM7 gives almost perfect amplitude linearity throughout the entire audio spectrum, and produces phase-coherent sound within a broad listening area. The drive units are purpose-designed and manufactured entirely in our own factory, employing new technology in order to achieve incredibly low distortion levels — typically less than 1% THD from 30Hz to 200Hz and less than 0.5% above that frequency. Another new feature in the DM7 is a variable energy control giving four frequency weightings — different to those obtainable from the control unit — to accommodate widely varying room acoustics.

Hear the B & W DM7 — you may well agree that this is the finest small speaker in the world today. Guaranteed for 5 years.

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Shuttle communications

The successful operation of the Space Shuttle is dependent on a complex communications and navigation system. By Brian Dance.

THE SPACE SHUTTLE has been designed to carry out a very wide variety of missions, including the launching of international communications satellites, of space laboratories, etc. The Orbiter vehicle employed for the Shuttle contains complex communications systems; these systems have been carefully designed to provide all facilities required for the various missions with very little modification of the communications equipment for any particular mission.

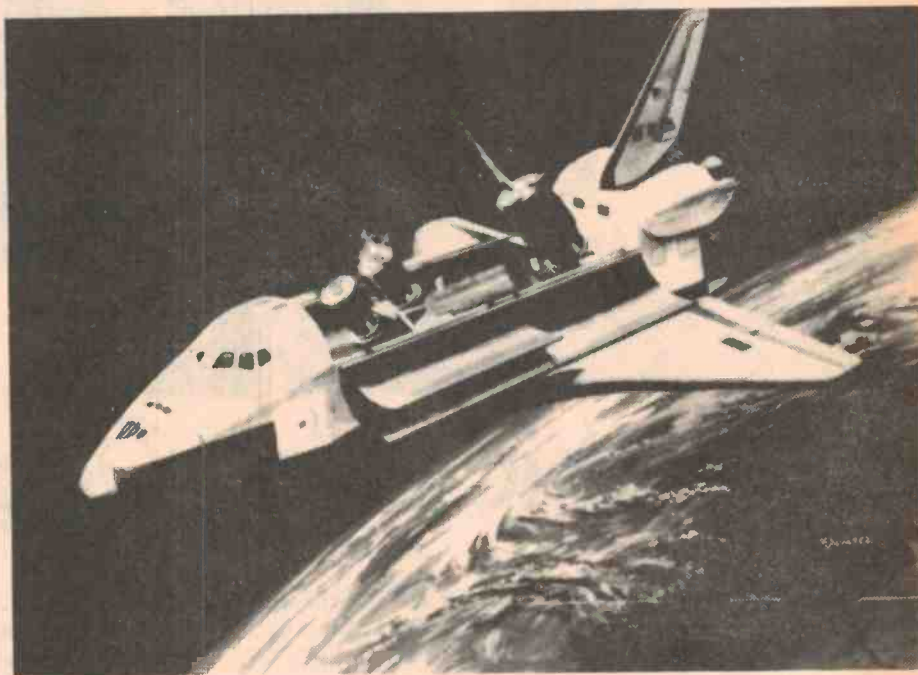
The Orbiter vehicle carries up to 23 antennae for communications with ground stations, with detached payloads launched by the Orbiter, and with the Orbiter vehicle crew when they are carrying out extra-vehicular activities. Information can be transmitted as voice or data signals using these antennae over a wide range of radio frequencies in the S-, Ku-, L-, C- and P-bands. The frequencies used for various purposes are listed on Table 1.

Ground Links

The S-band equipment in the Orbiter vehicle can communicate directly with the US ground station at White Sands, New Mexico or with other stations of the US Space Tracking and Data Network (STDN), the frequencies being somewhat over 2000 MHz. Two digitised phase-modulated links are available for this purpose, the four frequencies being shown in Table 1.

In addition, frequency modulated signals are transmitted from the Orbiter to the ground on an S-band carrier together with the frequency modulated data from the "Development Flight Instrumentation" (DFI) equipment carried aboard the Shuttle during its test flights.

During the Orbiter approach and landing phases of any mission, standard L-band TACAN units will be employed, as well as C-band radar altimeters and P-band analogue voice links for air traffic control. Voice communications for



extra-vehicular activities will also use the P-band.

Communications with the earth networks will also be available through the use of Tracking and Data Relay Satellites which will be placed in geosynchronous orbits 35 800 km above the equator over the Atlantic and Pacific oceans. The Shuttle can employ S-band frequencies for communication with one of these satellites, but Ku-band frequencies can also be employed for wide bandwidth links capable of high data rate operation (Fig. 1).

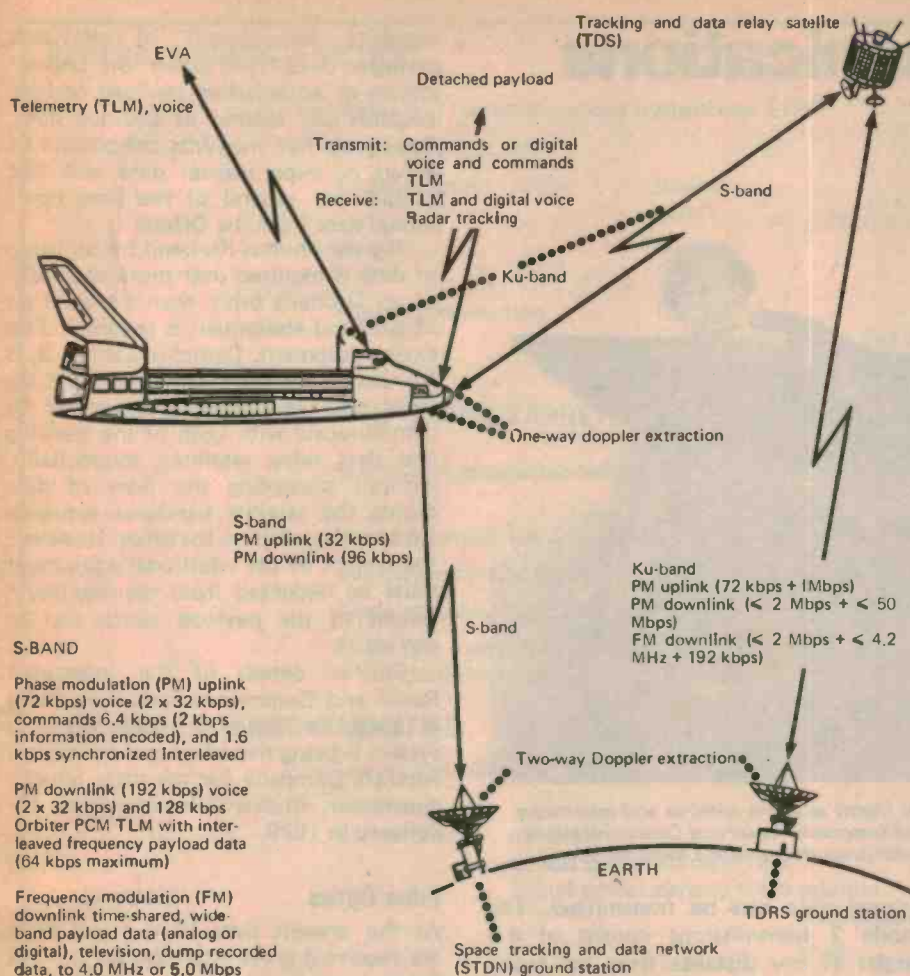
The satellites can relay signals to and from the earth using Ku-band frequencies at data rates of up to about 2 megabits/second. The advantage of using relay satellites is that one or both of the satellites will be able to "see" both the orbiting Shuttle vehicle and also a particular ground station at least 95% of the time the Shuttle is in orbit. The satellite link carries the same kind of information as the direct S-band link,

but much higher data rates are possible. The information carried will include scientific and engineering data, command signals, digital voice transmissions, video signals and performance monitoring information.

Multichannel two-way communication between the Orbiter vehicle and either attached or detached payloads is also available using S-band frequencies. However, the Orbiter rendezvous radar and the microwave scan beam landing system operate in the Ku-band.

S-band Systems

A variety of voice, command signals and telemetered data can be sent to or from the Orbiter vehicle using S-band links. Phase modulated signals beamed directly at the Orbiter vehicle from the Space Tracking and Data Network stations or relayed by means of a satellite can be transmitted at two different data rates. In the high bit rate mode, two digital voice channels at 32 kilobits



S-BAND

Phase modulation (PM) uplink (72 kbps) voice (2 x 32 kbps), commands 6.4 kbps (2 kbps information encoded), and 1.6 kbps synchronized interleaved

PM downlink (192 kbps) voice (2 x 32 kbps) and 128 kbps Orbiter PCM TLM with interleaved frequency payload data (64 kbps maximum)

Frequency modulation (FM) downlink time-shared, wide-band payload data (analog or digital), television, dump recorded data, to 4.0 MHz or 5.0 Mbps

include recorded voice, real time closed circuit television, main engine data, etc.

The Orbiter can transmit or relay a 2 kilobits per second command signal to attached or detached NASA payloads. Commands to free-flying payloads are sent at a one or two kilobaud rate by using a ternary frequency shift keyed (FSK) amplitude modulated signal. A 500 or 1000 Hz synchronisation signal is provided as the amplitude modulated signal.

Ku-band System

The Space Shuttle Orbiter vehicle will employ an integrated radar and communications Ku-band subsystem packaged in two sets of assemblies. One of these, Radar/Communications A, is carried aboard the Orbiter as standard equipment. It employs an antenna mounted on the starboard payload bay door and an electronics assembly. During the ascent of the Orbiter, the antenna is stowed in the space between the payload bay door panels and the clear volume of the payload bay.

Before the Shuttle can use the tracking and data relay satellites for communications work, it must first locate the satellites in space. When the vehicle first arrives in its orbit, the cargo bay doors are opened by the crew using a remote control system. The parabolic antenna moves into its operating position. The general location of the satellite is obtained from the Shuttle's computer and fed to the communications and radar subsystem. The

per second per channel and 8 kilobits per second of command data are interleaved into a 72 kilobits per second digital data stream.

The low bit rate consists of a single 24 kilobits per second digital voice channel together with 8 kilobits per second of command data. Transmissions via the relay satellite are convolutionally encoded.

Two bit rate modes are available for transmissions from the Orbiter directly to a ground station or via a satellite using phase modulation. The high bit rate mode accepts two digital voice channels at 32 kilobits per second per channel inter-leaved with 128 kilobits of telemetered information to form a 192 kilobits per second stream of digital information. Data from a payload can occupy up to 64 kilobits per second. When the low bit rate mode is being used, one channel of a digitised voice signal plus 64 kilobits per second of a telemetry signal can be inter-leaved for transmission.

The S-band frequency modulated signals from the Orbiter sent directly to ground can carry signals from the payload and Orbiter with a 4.5 MHz maximum bandwidth. The signals can

FUNCTION OR SYSTEM

ORBITER TRANSMIT

ORBITER RECEIVE

STDN Communication, Phase Modulation - 1	2287.5 MHz	2106.4 MHz
STDN Communication, Phase Modulation - 2	2217.5 MHz	2041.9 MHz
STDN Communication, Frequency Modulation	2250.0 MHz	None
Development Flight Instrumentation	2205.0 MHz	None
NASA Payloads	2025.0 to 2120.0 MHz	2202.5 to 2297.7 MHz
Separated payloads	1760.0 to 1843.0 MHz	2202.5 to 2297.7 MHz
Extra-vehicular activity communications	296.8 MHz	259.7 MHz
Rendezvous radar	13.679 to 13.887 GHz	13.679 to 13.887 GHz
Ku-band communications	15.0034 GHz	13.775 GHz
TACAN	1025 to 1150 MHz	962 to 1213 MHz
Air traffic control, voice	296.8 MHz	259.7 MHz
Microwave scan beam landing system	Ku-band	Ku-band

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Here's how:

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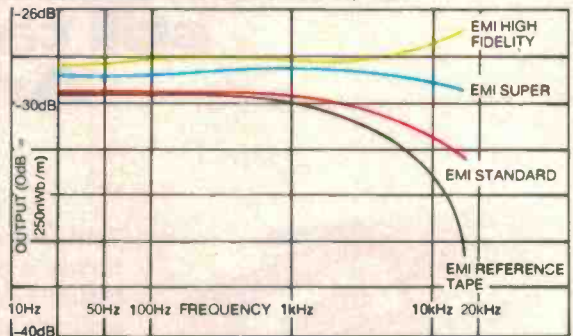
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The new EMI Cassettes produce excellent results over the whole range of available equipment. All are available in 60, 90 and 120 minute playing time.

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1. Measured using the EMI recommended 2.5dB overbias at 6.3kHz, derived from the reference batch C521V (the value of bias internationally used by the majority of domestic recorder manufacturers).
Tape speed 4.76cm/s (1 7/8 in/s)
Track width 0.6 mm
Record head gap length 2µm
Replay head gap length 2µm
Replay amplifier characteristics: 120µsec and 3180µsec
(In accordance with IEC Publication 94 Edition 3, BS1568 Part 1 and DIN 45513)
 2. The Frequency Response is obtained when the record amplifier characteristic has been adjusted to give a flat frequency response (25Hz - 15Hz) from the reference tape batch C521V of -30dB (Ref. 1*).
- *Ref 1. Relative to an RMS Flux of 250mWb/m Tape Width (25mMx1mm) at a frequency of 315Hz (in accordance with IEC Publication 94 Part 2).

TYPICAL FREQUENCY RESPONSE OF EMI CASSETTES



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SOUND

New Recorders for Metafine Tapes

IN OUR AUGUST issue we forecast that new recorders would soon become available which are suitable for the recently announced Metafine tape which is essentially based on metallic iron particles instead of the normal oxide mixture. Our forecast proved very true, since the well-known Norwegian based manufacturer Tandberg announced a whole new series of recorders in August, some of which are suitable for the new type of tape. The new recorders are not specifically designed for use with the new tapes, but can be used with all types of tape currently available and any types which are likely to become available for a long time to come. Indeed, these recorders have been specifically designed so that they will not become outdated by any normal developments in tape technology.

Tandberg is the first recorder manufacturer to announce recorders suitable for use with the new iron particle tapes, but many other manufacturers are working on the design of suitable equipment and more announcements can be expected soon. It will also be interesting to see how other tape manufacturers will respond to the new development from 3M tapes.

Fundamentals

Let us first consider the fundamental reasons why new types of recorder are required for use with the iron particle tapes. Present recorders (when set for 'chrome' playback with a 70 microsecond equalisation) are quite suitable for replaying cassettes containing the iron particle tape and will provide an improved performance over that obtainable from conventional tapes using the same equipment.

Unfortunately our existing recording equipment will not enable us to obtain an optimum performance from the new tapes when used to record material. The new tapes require a stronger magnetic field to be applied across the recording head gap in order to record material on them satisfactorily and a stronger erasing field is also required to erase material from iron particle tapes. The bias current levels required for optimum performance are also different from those required for use with conventional tapes.

In case readers are becoming worried by now, we will mention that there is no possibility of their existing collection of tapes being unsuitable for replay on any new recorders designed for iron particle tapes. Obviously one can obtain the improved performance only from the new tapes, but one will be able to obtain the same quality of reproduction from one's older tapes as one has obtained in the past.

The new iron particle tapes will first be marketed as cassettes, since it is here that performance is most critical. However, it is expected that they will soon also be available in the reel-to-reel form, as video tapes and as tapes suitable for



computer and data storage purposes. The new tape can provide improved performance at conventional tape speeds, but it also offers the possibility of considerably lower tape speed without any deterioration in quality.

Tape differences

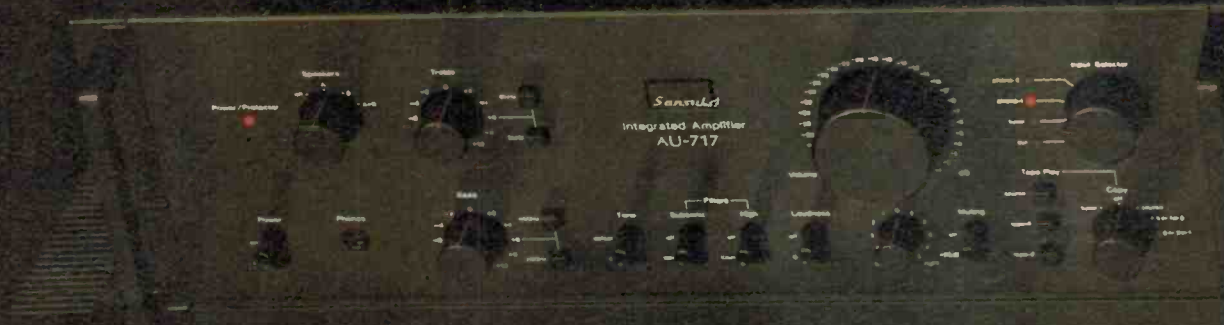
The magnetic properties of a tape are not simple, but two quantities are of vital importance in assessing the practical performance of a tape. One of these is the saturation flux density which, in everyday language, is a measure of how strongly the tape can be magnetised. It is given the symbol B_m . If one attempts to magnetise a tape above this level, severe distortion is the inevitable result. If one employs a tape with a high value of B_m , one will be able to obtain a relatively large output signal from it on replay and one may therefore expect that the signal-to-noise ratio will be improved if other factors are unchanged.

The other important property of a tape is its coercivity, H_c . This is a measure of how strong a field is required to record on the tape concerned, but it can also be employed as a measure of how well the tape retains the recorded material. A high coercivity tape will require a high signal current through the recording head, but once this signal is satisfactorily recorded, it will not easily be lost.

During the past fifteen years or so there has been a definite

Specs with a purpose!

Sansui's new amplifiers

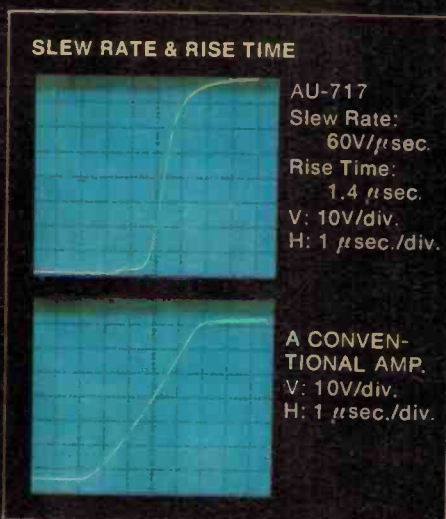


Sansui's all-new integrated amplifiers have absolutely astounding specifications. Compare them with any others in their class, and Sansui comes out far ahead. But what really makes Sansui's new amplifiers so superior is that all these great specs have a single purpose — outstanding sound quality.

Take response speed, for example. Your amplifier doesn't move, but it does respond. The more rapid its response, the cleaner and the more accurate the sound. That's why the AU-717, for example, features an advanced DC power amplifier design. Sansui's DC amplifier eliminates all capacitors in the signal path and even in NFB loop so amplification is direct without coloration and phase delay. Response is astoundingly rapid — the proof is in the ultra-high (60v/ μ sec.) slew rate and ultra-rapid rise time (1.4 μ sec).

But Sansui didn't strive for such outstanding specs just to be able to print impressive figures. On the contrary, Sansui research showed that to achieve accurate reproduction and reduce signal loss, lightning-fast response was essential.

In addition, special circuits were incorporated to achieve new levels in stamping out TIM (transient inter-modulation distortion), a type



of distortion that is now receiving high priority. Still another important benefit of Sansui's DC amplifier is the ultra-wide frequency response from zero (DC) to 200,000 Hz.

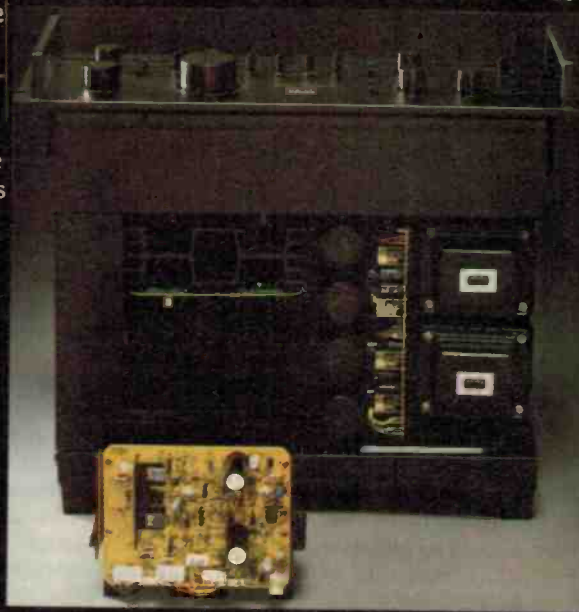
The final result is music with a purity and clarity that must be heard to be believed. All the dimensions of

complex musical sounds — the wide dynamic range, the sudden pulsive signals, the nuances of barely perceptible but critical overtones in the ultra-high frequencies — all these are now crystal clear, all are proof of Sansui's new levels in superior sound quality. Impressive power is 85 RMS watts per channel, 20 — 20k Hz, and total harmonic distortion at rated output is 0.015%. That means it can be considered non-existent as far as the human ear is concerned.

Keep in mind that though the AU-717 is special, it's not special for Sansui. Each and every amplifier on the left-hand page embodies the same Sansui commitment to outstanding sound quality. All controls have been carefully thought out and designed for their specific purposes. Sansui has no place for gadgets and gimmicks in its dedication to the ultimate in hi-fi.

The AU-517 and AU-317 also feature the same DC power amplification as the AU-717, and offer 65 and 50 RMS watts respectively. The AU-217 and AU-117 offer 30 and 20 RMS watts respectively, but are not to be under-rated. In fact, they represent exceptional values in low distortion and true hi-fi performance.

Sansui for specs with a purpose — outstanding musical quality.



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trend towards the use of tapes of higher B_m and H_c values, largely in order to obtain improved signal-to-noise ratios. The introduction of cassette recorders greatly stimulated this trend to tapes of higher B_m and H_c values, since there is no possibility of obtaining a better performance by increasing the tape speed or increasing the track width in such recorders.

At high signal frequencies the signal-to-noise ratio is determined mainly by the value of H_c , whereas at lower frequencies it is more dependent on the value of B_m . The earliest cassette tapes had H_c values of around 250 oersted, but this was gradually increased to around 350 oersted. A big breakthrough came with the chromium dioxide tapes which have H_c values of over 500 oersted, but the new Metafine iron particle tapes have an H_c of about 1000 oersted.

Similarly the saturation flux density, B_m of the new tapes is considerably higher than that of currently available tapes. Conventional tapes have a B_m value of around 0.1 to 0.15 weber/square metre, whereas the iron particle tape has a value of about 0.34 weber/square metre.

Another feature of the new iron particle tape is that the coating thickness of the magnetic film on the base material is only $3.8 \mu\text{m}$ in contrast to the more usual $5 \mu\text{m}$ of conventional cassette tapes.

Therefore one may summarise the problem by stating that the new tapes will require recording equipment which can impress a strong signal upon them and which can generate an adequate erasing field to wipe off all previously recorded material.

Actilinear Systems

Tandberg have used the name 'Actilinear' for their new recorders, since they employ *active* components in the recording process which results in greater *linearity*. In order to understand how this type of circuitry differs from that of conventional recorders, we must first consider conventional recorders and their limitations.

The recording amplifier of a conventional system contains an equalisation circuit so that the overall record/playback frequency response is flat. As shown in Fig. 1, the output of this recording amplifier is a voltage which drives a signal current through the resistor R and through the recording head. The bias oscillator also feeds a current at the bias frequency of some 90 kHz to the recording head.

It should be noted that the network connecting the recording amplifier to the head in Fig. 1 contains only a single passive component, namely the resistor R. However, the Tandberg Actilinear recording system (Fig. 2) employs a recording amplifier transconductance converter (containing active components) between the output of the recording equalisation amplifier and the recording head network.

The full circuit of a conventional passive recording system

CONVENTIONAL

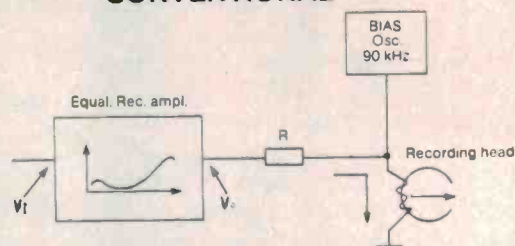


Fig. 1. A block diagram of a conventional recording system.

ACTILINEAR

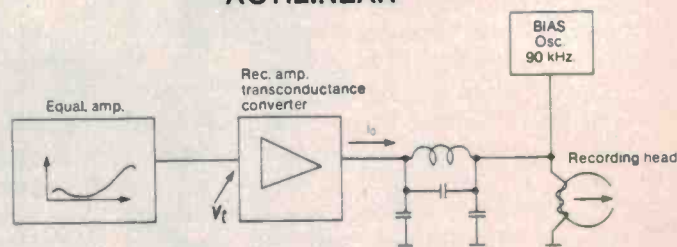


Fig. 2. A block diagram of the new Actilinear recording system.

is shown in Fig. 3 and the Tandberg Actilinear circuit in Fig. 4. In the latter circuit, the C2 and R4 network provides the correct equalisation at low frequencies, whilst equalisation at the middle and high frequencies is provided by the components L1, C1, R2 and R3. Adjustment of the trimming capacitor C_T provides a method of adjusting the system for the correct signal level for the particular type of tape in use.

The transconductance module shown within the dashed lines has two main purposes. It converts the signal voltage from the potentiometer R_5 into a signal current which is fed to the recording head to produce the signal on the tape. This stage also provides electrical buffering between the oscillator and the output of the recording amplifier so that the oscillator voltages do not enter the recording amplifier and cause interfering tones.

The transconductance module employs two transistors, Q1 and Q2 with Q2 acting as the collector load of Q1. The transistors are complementary types (that is, an npn and a pnp pair). Each transistor passes a current of about 10mA, the voltage at the junction of their collectors being about +12V under quiescent conditions. This voltage can swing from +2V to +22V when a signal is applied.

The output impedance of the transconductance module is some 5 kilohms, but as the recording head impedance is far less than this (only about 200 ohms at 5 kHz), the circuit acts as a current source. In other words, a constant voltage applied at the input produces a constant current through the recording head; this is why it is known as a transconductance module.

The capacitor C12 prevents any appreciable oscillator voltage from finding its way back into the recording amplifier. The filter circuit in the output section can reach the transistors of this module. This filter, comprising L2, C14, C15 and C16, reduces the bias oscillator voltage from its value of about 20 V at the recording head to less than 0.1 V at C13.

Apart from the better rejection of the oscillator signal, the Tandberg Actilinear system is a much better system for providing signal and bias currents to the new high coercivity iron particle tapes.

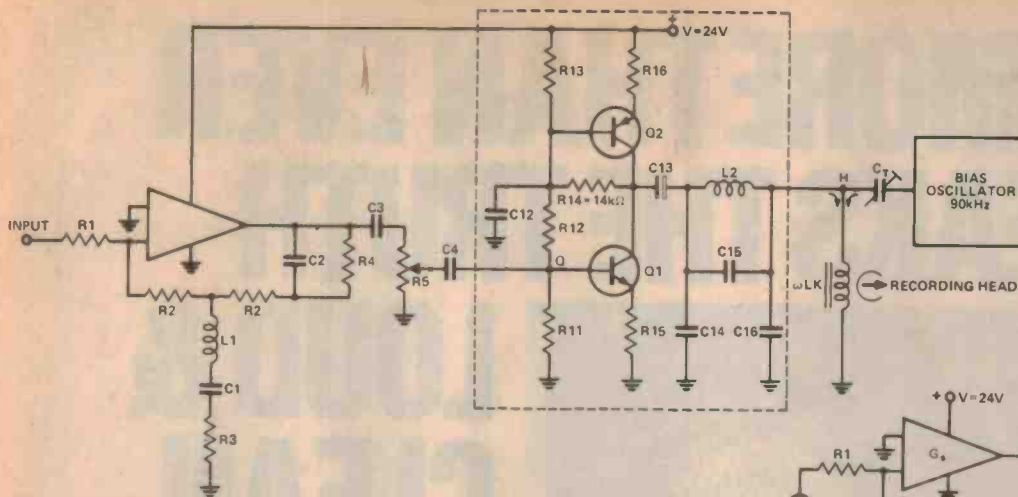


Fig. 4. The circuit of an Actilinear recording system.

Slew Rate

A further advantage of the Actilinear system is concerned with slew rate limitations. All amplifiers have a limitation on their slew rate which is the maximum rate at which their output voltage can change. If the output voltage is small, the output can follow a high frequency signal with ease, but if the output voltage is large, the output cannot change fast enough to faithfully reproduce a high frequency signal waveform.

In the circuit of Figs. 1 and 3 for a conventional system, a relatively high voltage is required from the recording amplifier to provide the necessary voltage to drive the signal frequency recording current through the resistor R. However, in the Actilinear circuit of Figs. 2 and 4, only a small voltage is required from the output of the recording amplifier to provide a signal which can be converted into an adequate current by the transconductance module. Thus slew rate distortion limitations will appear at much lower signal amplitude levels in the conventional circuits than in the Actilinear circuit; indeed, the latter is almost free from any slew rate problem.

The graph of Fig. 5 shows one of the practical benefits conferred by the new Actilinear recording technique in a reel-to-reel recorder at a tape speed of 3 3/4 inches per second (95 mm per second) using a conventional tape. It can be seen that the Actilinear system provides a larger dynamic range.

Perhaps the most important advantage of the Actilinear system is the availability of ample signal frequency recording current for the recording head so that the system can be employed with high coercivity tapes of any type, including the new Metafine Scotch type of iron particle tape.

It is claimed that the Actilinear system reduces intermodulation interference from the bias oscillator and increases the signal handling capacity by 20dB over that in a conventional system. Signal-to-noise ratio is improved because Actilinear recording provides a stronger recording at a given distortion level than conventional recording systems. In addition, the new system has more than 20dB overload reserve for recording on the highest coercivity tapes one can envisage in the coming years.

When the Actilinear recorders are employed with the new Metafine tapes, one can obtain an improvement in the signal-to-noise ratio of some 10dB; this is approximately equivalent to the improvement one can obtain through the use of Dolby circuitry. However, the Dolby system improves the signal-to-noise ratio only at the higher frequencies, whereas the use of iron particle tapes with the new Tandberg recorders is said to improve the signal-to-noise ratio by some 5dB even at the lower frequencies. In addition, no special encoders or decoders are required nor any complex circuitry. Even more impressive results can be obtained by the use of a Dolby circuit with an

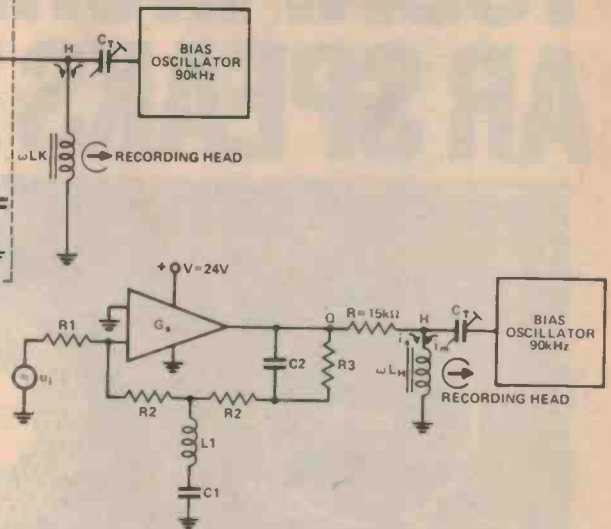


Fig. 3. A practical circuit of a conventional recording system.

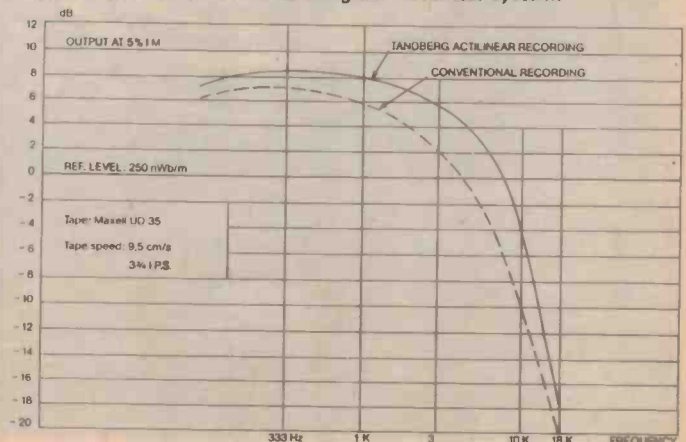
Actilinear recorder and Metafine tape. Perhaps this is the point of perfection in signal-to-noise ratio?

The new recorders

Tandberg have just introduced two recorders with their Actilinear system. The TCD 340A is a cassette deck with three heads (separate record and replay heads) and three motors. The new model resembles its predecessor, the TCD 330, and is equipped with 4 Dolby B processors, the Tandberg developed equalised peak reading meters for precise control of record and playback, multiplex filter and a pneumatically damped cassette compartment for the highest grade of cassette recording. The Anciliar system used in this recorder replaces the well-known Tandberg crossed-field heads used in their current range of recorders.

Tandberg claim that the TCD 340A has a signal processing capacity of more than 20dB above the level of any cassette tape equipment currently available. Recording head azimuth adjustment is available for the manual adjustment of the angle of the tape-to-head contact so as to assure the best possible frequency response with any of the recommended high quality cassettes. Although some recorders employ two-in-one combined record replay heads, Tandberg rejected this solution and

Fig. 5. Improvement obtained using the Actilinear system.



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SOUND

adopted completely separate heads because they felt this is the only way to eliminate bias interference and tape tracking problems associated with such combined head systems.

On the mechanical side, the TCD 340A employs a dual capstan closed loop drive system for optimum tape handling precision and stability, whilst it eliminates uneven tape speed and sudden jumps that are often caused by poor quality cassettes.

The synchronous drive motor is designed for minimum speed deviations together with minimum effect of temperature and mains voltage on the tape speed. Two separate servo-controlled DC motors take care of the wind and rewind functions.

The TCD 340A employs electronic logic control throughout. It is thought that this is ideal for rendering the equipment safe and fool-proof in normal operation and for safeguarding both the tape and the machine. An optional remote control is available which can be pre-set with a separate radio tuner for unattended record or playback operations.

The frequency response is 30Hz to 20kHz. The production specification is for 0.12% wow WRMA for recording and playback (0.08% Japanese industrial standard). Signal-to-noise ratio is better than 65dB IECA.

TD 20A Reel-to-reel

The Tandberg TD 20A is a reel-to-reel recorder using the Actilinear process which can accept 10½ inch reels of tape. Front panel bias adjustment and optional radio infra-red remote control are incorporated into this instrument. This recorder employs a 4 motor drive system, including a phase-locked brushless Hall Effect synchronous motor combined with drive belt which prevents the transmission of unwanted, mechanically induced irregularities in the tape motion.

The TD 20A is equipped with separate power supplies for the operational and for the audio functions in order to eliminate thermal component stress and to isolate the audio chain from electrical disturbances. It incorporates PROM (electronic brain) speed regulation combined with triac controlled direct drive spooling motors for proper tape tensioning and minimum mechanical wear and tear. The fourth motor engages the pinch roller/tape guidance mechanism to ensure more precise tape tracking and head-to-tape contact.

The TD 20A is available in half track and one quarter track versions. A high speed version is provided with 15 inches per second and 7½ inches per second tape speeds whilst a low speed version has 7½ and 3¼ inches per second tape speeds.

Tandberg have also just released a TCD 320 cassette recorder (without the Actilinear recording system) and four new high quality radio receivers.

SOUND BRIEFS

PCM Now

Sony USA is now distributing the first batch of its pulse-code modulated audio units – which enable the company's Betamax video-cassette recorders (or any other similar device) to be used to record and play back audio material.

The device can record 12 bits of data on each channel and is expandable to 16 bits per channel, corresponding to 1.7 million bits per second.

Sony claim a dynamic range of 85 – 95 dB – about 20 to 30 dB greater than the best present analogue techniques. Frequency response is claimed to be 0 to 20 kHz plus or minus 0.25 dB with THD of less than 0.03% across the whole range.

Price in the USA is US\$4000 which is going to limit sales for a bit but Sony are confident the system will have many professional and semi-professional applications.

Super-Recorded Cassettes

A newly formed UK company is planning to market a range of super-quality pre-recorded cassettes – claimed to be the tape equivalent of direct-cut discs.

Only the very best quality tape will be used and the recordings will be made directly from master recordings on a 'one-to-one' basis rather than by the multiple process normally used. We understand that the cassettes should sell for around £8.00 (about A\$12.80). More details hopefully next month.

Direct Control Turntable

Philips has developed a range of belt-drive turntables in which the actual turntable speed itself is sensed and used to control motor speed.

The feedback loop servo system thus compensates for external influences such as changes in tracking force, drag from 'dust bugs' etc, as well as varying mains voltage and frequency, and changes in humidity or temperature.

Philips claim that their new machines achieve the performance levels of direct-drive units without incurring what Philips claim are their disadvantages.

Tone control chip

Motorola in Geneva have developed an IC which replaces the four dual potentiometers normally required to control volume, balance, bass and treble in stereo receivers. The chip enables gain to be controlled over a range of 84 dB using dc signals from 0 – 6 volts.

At present the chip is primarily suited to car radios but a hi-fi version is currently being developed.

Japan Audio Fair

A number of readers have asked for the dates of the forthcoming All-Japan Audio Fair.

It's from October 6 through October 11 at the Tokyo International Fairgrounds in Harumi (Tokyo).

A major independent research company proved that the ADC XLM MkII incurred no perceivable record wear over the life of your records! Since then ADC's massive research programme has created a new state-of-the-art, top of the line model—the ZLM Aliptic—designed for ultimate stereo performance combined with the concept of zero record wear.

Greatly reduced tip mass

The ZLM has a tiny nude diamond with a .004" x .008" rectangular shank.

This achieves more lateral strength than the fashionable .006" square shank, plus a 10% reduction in mass.

The diamond is mounted on a new tapered stylus, which again reduces mass.

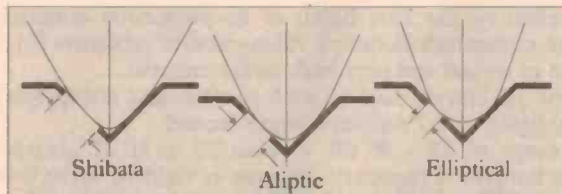
In fact, the ZLM has only half the tip mass of the famous ADC XLM MkII.

Less mass by patent

The patented ADC Induced Magnet system, where the magnet is suspended over the moving stylus arm instead of being attached to it, inherently means less mass for the record groove to move. This, coupled with major innovations in the pivot block stylus suspension (which have solved deficiencies in the old system), has resulted in greatly improved frequency response characteristics.

New low-wear ALIPTIC shape

The ZLM has a new tip shape that combines the advantages of the elliptical and Shibata shapes, while eliminating their disadvantages.



It is basically elliptical (.0003" x .0007"), but its bottom radius has been modified to extend the vertical bearing surface on the groove wall by 100%.

Large enough to greatly reduce record wear, while still small enough to prevent dirt particles being reproduced. This new shape is called ALIPTIC™.

The best polish available

We decided it was worth the extra cost to get the ultimate polish for the ZLM.

The method involves a cam action to shape and polish evenly while forming the elliptical surfaces simultaneously with the other radii. This Pathe-Marconi method is expensive, but the result makes another important contribution towards reducing record wear.

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Certain ZLMs fall within a range of $\pm 1/2$ dB 10Hz to 20kHz and ± 1 dB out to 26kHz.

These rare cartridges are called ZLM Select and are only available on special order.

The best cartridge we've ever made

The ZLM is without doubt the best cartridge we've ever made, but it's well worth taking a closer look at the new ADC XLM III which incorporates all of the reduced mass accomplishments of the ZLM, but with a tiny elliptical diamond. This also includes an individual specification.

Complementing the range, we have the new four-cartridge QLM Mk III series, incorporating our new design criteria and exciting innovations like the Diasa (diamond + sapphire) elliptical tip.

ZLM Aliptic specifications

Diamond tip	Nude Aliptic
Tracking force	1/2 to 1 1/2 gram
Frequency response	10Hz to 20kHz ± 1 dB 20kHz to 26kHz $\pm 1 1/2$ dB
Output	1.0mV per cm/sec
Output balance	1dB max. diff.
Channel separation	30dB at 1kHz/20dB at 10kHz
Inductance	580mH
Resistance	820 Ohms
Load resistance	47,000 Ohms
Load capacitance	275pF
Cartridge weight	5.75 grams
Accessories	Stylus brush, screwdriver, all mounting hardware and signed frequency response curve.

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SL1803: 18" 4" coil, 200W, Bass, 14 kg,
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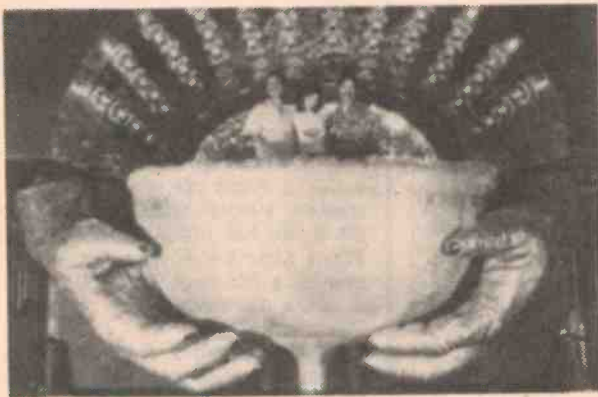
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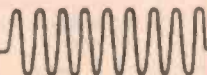
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LER 214

LED Pendant

WANTING TO IMPRESS upon one's partner that electronics is not a boring useless occupation, has inspired many an electronic engineer to build egg-timers and liquid overflow indicators, etc. for their loved ones.

However, such devices, appreciated though they may be, cannot usefully be exhibited at parties and pubs to achieve maximum admiration. An obvious solution is electronic jewellery.

Before LEDs became commonly available it was possible to build illuminated jewellery using miniature catheter bulbs. But the current drain still involved the inelegant strapping-on of bulky power supplies and concealed switches.

Nowadays, by using LEDs and CMOS 'chips', it is possible to build a piece of self-contained jewellery that doesn't even need an on/off switch.

Electronic jewellery may take virtually any form that the designer seeks — the main limitation being availability of miniature resistors which are often hard to find in this country.

The example shown was in fact built using 1/8th watt resistors obtained from the UK. IRH manufacture a range of 1/4 watt resistors which are marketed via A & R-Soanar and only minor changes are needed to the mechanical details shown to accommodate these.

The operation is as follows. Upon touching the contact plates the seven-segment LED flashes between the two sections of the design for about eight seconds and then switches off again.

The pendant is not limited to letters that the seven segment display can handle. There is nothing to stop the reader from hard-wiring LEDs into dot patterns of any desired form.

(The prototype shown here was designed to flash the initials BJ).



Project 552

Mechanical Construction

Because one of the design aims was to keep the width to a minimum a common pc board design is impracticable. Therefore the components are hard wired and we do mean *hard* wired.

The front panel is cut from 16 SWG aluminium with a window for the seven-segment display and two holes below, with sufficient clearance for the heads of 8BA cheesehead screws, filed smooth. The red perspex window and the 8BA screws are fixed to the front panel using epoxy resin. Then the front is sanded down and polished. The epoxy insulates the contacts from the aluminium and also provides mechanical anchorage.

Electronic Construction

When the front facia is finished, the electronics can be mounted with super glue or epoxy resin (having first centralised the display over the window).

Great care must be taken to prevent shorts. Tinned copper wire and PTFE sleeving to suit, was used to hard wire the circuit as in the wiring diagram. Small pieces of tin plate were stuck down with double sided sticky pads for the battery contacts.

The sticky pads serve a dual purpose. They insulate the contacts from the front panel and also provide the tension to ensure good electrical contact.

Fig. 1a is the monostable and astable multivibrator which is the basic circuit. Fig. 1b and 1c show alternative circuits for BJ and AL respectively.

HOW IT WORKS - ETI 552

The prototype was designed with the initials BJ in mind, which was very convenient as the segments b, c, d and e remain on the the monostable period and segments a, f and g flash at 1 Hz to complete the letter B (Fig. 1 a, b).

To illustrate the technique involved in obtaining different combinations of letters, a further circuit (Fig.1 c) was designed to accommodate the letters A, L. This requires a further transistor Q3 and resistors R9 and R10 to give an inverse function. This circuit will be described in detail.

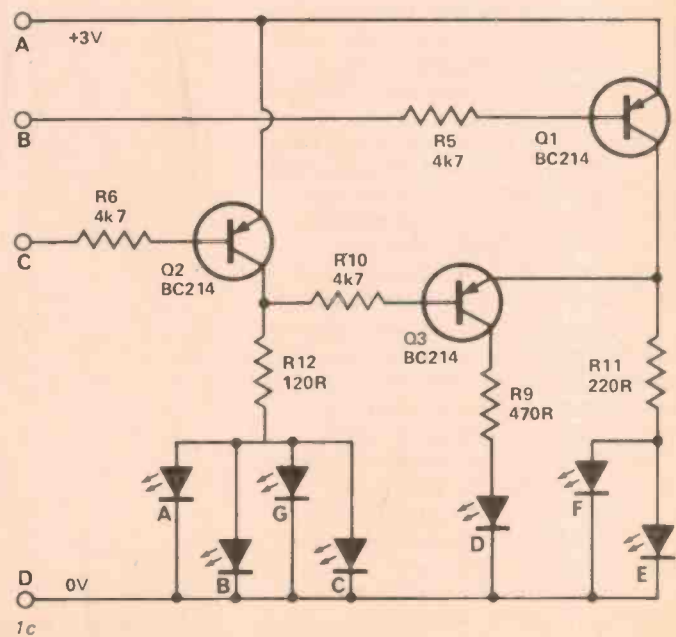
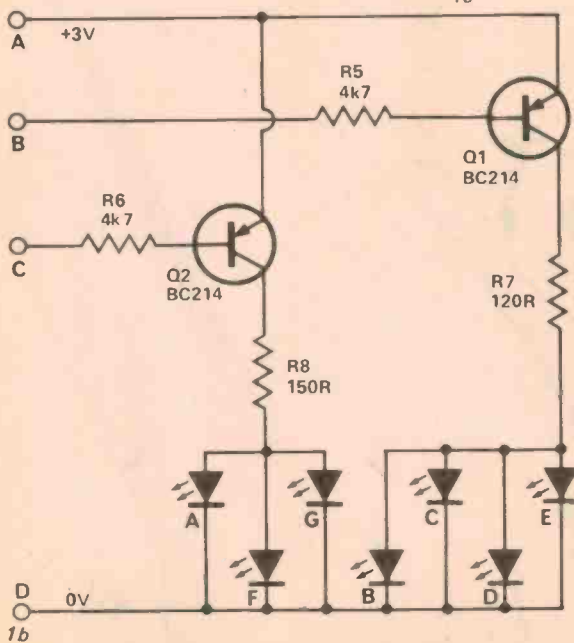
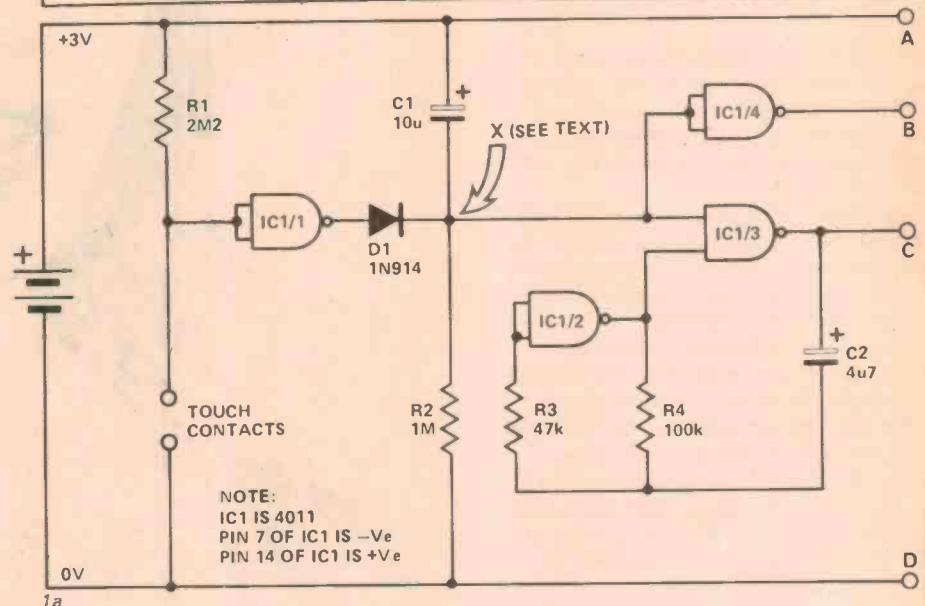
Under quiescent conditions no measurable current is drawn. When the touch plates are joined by a finger, inverter 1 discharges C1, this point X goes high for about 8 seconds, as C1 -charges down. Then, via inverter 4, Q1 turns on and lights LED segments e and f. These remain on for the monostable period.

The output from the astable (gates 2 and 3) is initially low after the beginning of the monostable period, so that Q2 is switched on. This lights segments a, b, g and c, but Q3 is switched off via Q2, so that segment d is off. Thus the letter A is formed.

When the astable changes over Q2 is switched off, turning Q3 on, and lighting segment d. Thus with segments e and f on, the letter L is lit up.

Resistors 7, 8, 11 and 12 are chosen so that all segments have the same current and thus the same intensity. In this case about 2 mA per segment forms a compromise between battery drain and visibility.

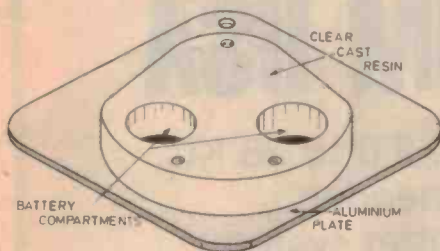
The batteries are Mallory MS76H 1.5 volt cells and in the prototype a life of two months was typical, with approx two minutes usage a day.



Finishing It Off

When all the wiring is complete the battery compartments need to be constructed. Make up two tubes of the same external diameter as the batteries from cellophane or plastic and position them on the fascia over the battery contacts, then pour quick-set epoxy around the tubes. When the epoxy has set remove the tubes and you have two battery compartments.

Make up another cellophane or plastic tube about 37 mm in diameter. Place this around the finished electronics and battery compartments and pour more clear cast over to cover everything to the depth of the battery compartments. When this has set a thin sheet of aluminium can be screwed down with counter-sunk self-tappers. (This sheet forms the common connector for the two cells).



LED Pendant as seen from rear after potting, note battery compartments.

Presentation

Having built the device, and given it to your loved one, all that remains is for you to reap your just rewards, preferably in dimly lit surroundings where the pulsating red glow will hopefully produce the desired effect!

Note

This project could have been made much smaller by using a flat pack version of the 4011 and miniature hearing aid type transistors, and 1/20th watt resistors. This would reduce the size to almost the display and battery dimensions. But by using commonly available components a respectable size has been achieved.

PARTS LIST - ETI 552

Resistors all 1/8 W 5% or smaller

R1	2M2
R2	1M
R3	47k
R4	100k
R5,6	4k7
R7	120R
R8	150R

Capacitors

C1	10 μ 6V3 tantalum
C2	4 μ 7 16V tantalum

Semiconductors

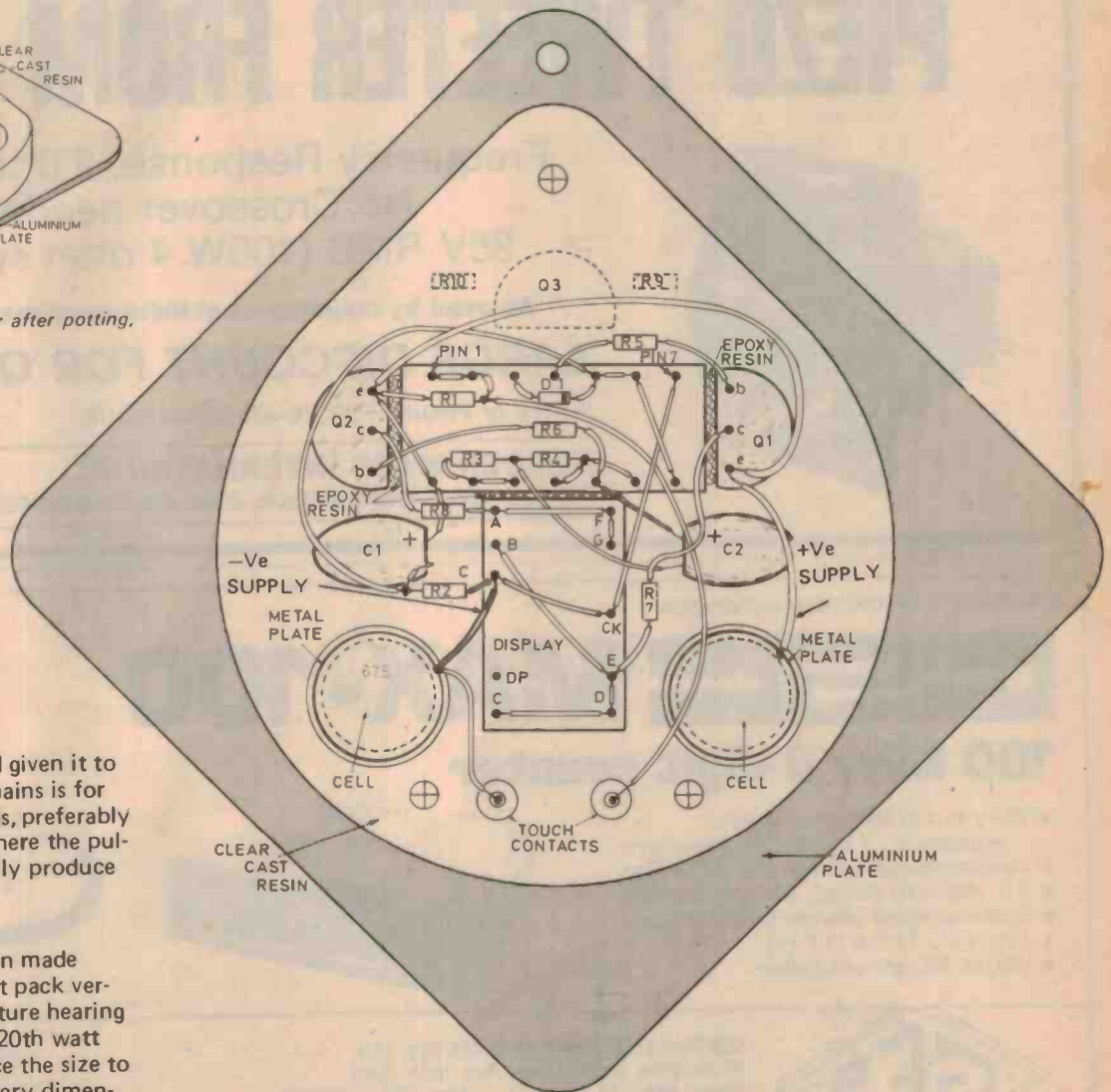
IC1	4011
D1	1N914
Q1,2	BC214
DISPLAY	7-segment common cathode type

Additional components for the circuit shown in Fig. 1(c)

R9	470R
R10	4k7
R11	220R
R12	120R
Q3	BC214

Miscellaneous

Piece aluminium 14 B&S 50 mm square, piece red perspex 21 mm x 12 mm, epoxy resin, 2 off 6 BA brass cheese-head bolts, 19 B&S tin plate, 28 B&S tinned copper wire, PTFE sleeving, 2 off Mallory MS76M cells.



Component layout, shown at twice times life size.



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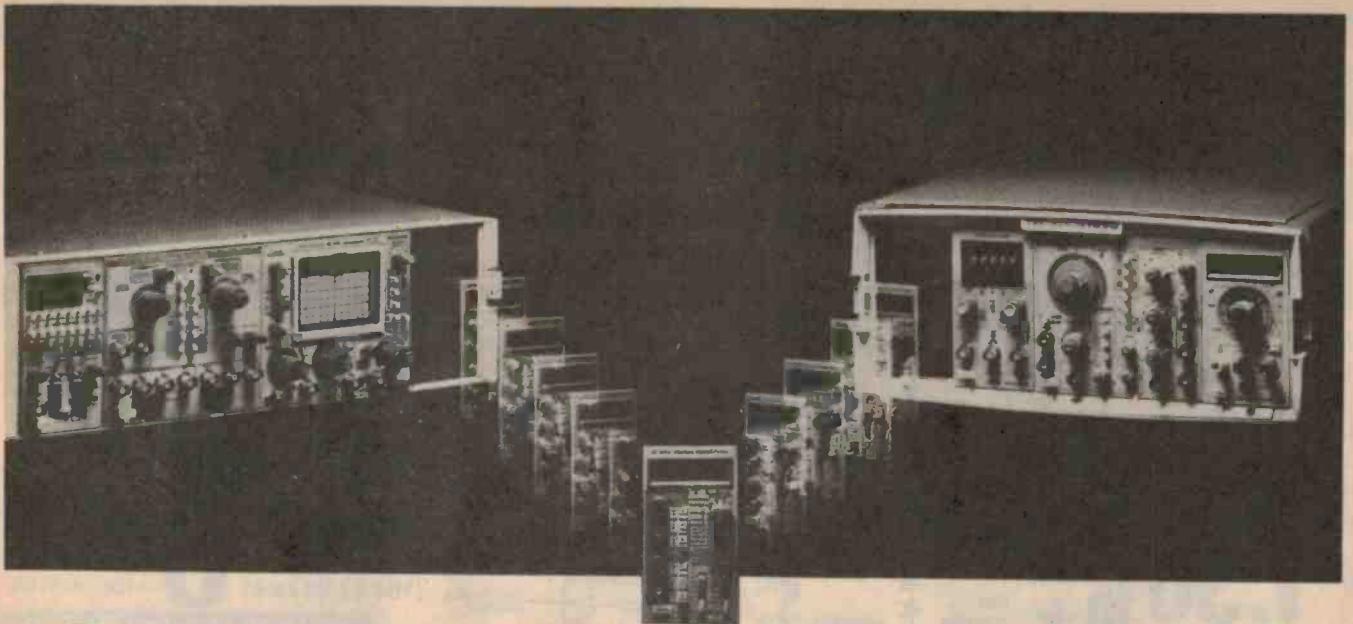


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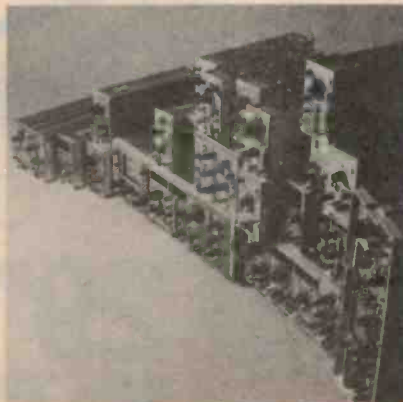
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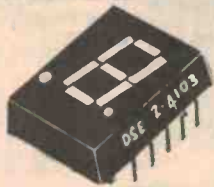
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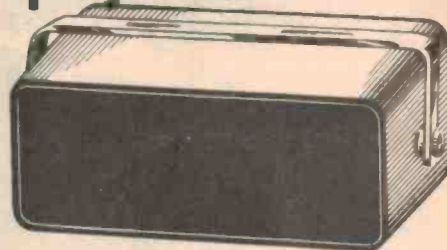
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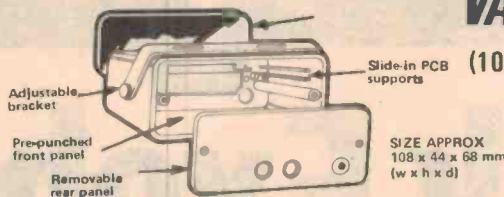
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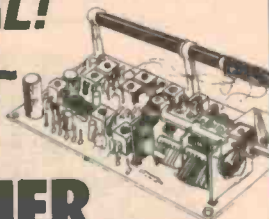
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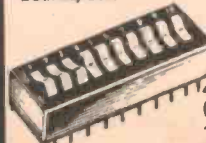
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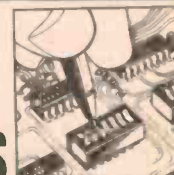


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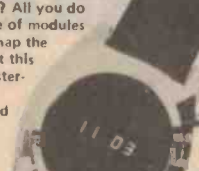
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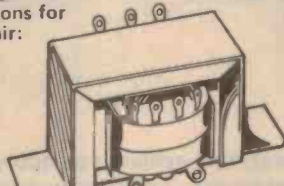
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Not produced as a special kit — all parts available ex stock:
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LT-303 7 segment display ... Cat Z-4103 .. \$1.50
All other components are normal stock lines at all of our stores.

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Although we do not produce a full kit for this project, all parts are normal stock lines at all of our stores.
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Complete kit, including instructions ... Cat K-3491 .. \$49.50
SEPARATE PARTS:
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UP/DOWN PRESETTABLE COUNTER (See E.T.I. July)
Not a full kit. Special parts:
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Special PCB boards to suit the Dick Smith Z-4103 7 segment displays:
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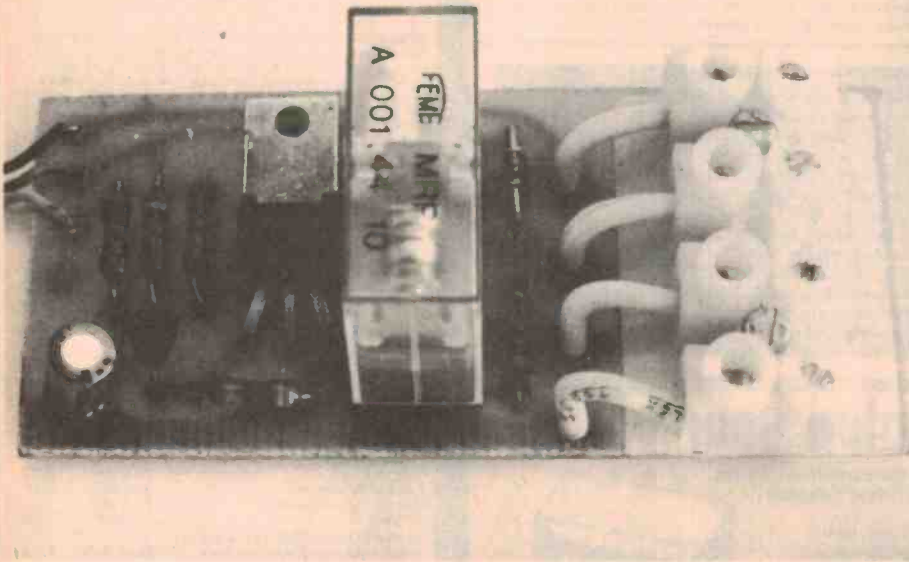
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Vari Wiper mk2

This pulsed windscreen wiping circuit can be used on cars fitted with most types of modern wiper motors.



WHEN OPERATING IN heavy rain windscreen wipers often have difficulty providing adequate visibility. However, during light rain or mist all that is necessary is an occasional sweep of the blades at intervals of a few seconds.

Turning them on and off repeatedly takes the driver's concentration off the road, and his hands off the wheel, increasing the risk of an accident. Alternatively, if the wipers are kept working all the time in such conditions the blades tend to scrape on dry glass, wearing out the rubber inserts, your nerves, and worse still, the screen itself.

The answer is obvious; have the wipers operate intermittently at a duration which can be varied to suit the conditions.

This project is an updated version of the popular ETI 301 Vari-Wiper which appeared in the May 71 edition.

Figure 1 shows the circuit of a modern wiper assembly. Dynamic

braking is achieved by applying a short across the armature, by a cam-actuated change-over switch synchronised with the wiper blades. When the wipers are switched off, the change-over switch shorts out the motor armature via the main wiper ON/OFF switch.

The circuit of fig. 2 is suitable for use with negative earth cars fitted with permanent magnet motors. Some early model cars are fitted with wound field coil motors and are not suitable for use with this circuit (more about them later).

Some types of permanent magnet wiper motors, especially those on British cars, have a fifth wire extended to the wiper switch. These motors are designed to operate independently of an earth to allow for their use on either positive or negative earth vehicles. The circuit of fig. 2 can also be used with these motors provided they are fitted to a negative earth car. However, some

more expensive imported cars have wiper motors which are reversed in the parking sequence to lower the blades below the bottom of the windscreen when not in use. The Vari-Wiper unit described cannot be used with these wipers.

Before installing the Vari-Wiper unit make sure that you have one of the types of permanent magnet wiper motors described. If necessary remove the cover of the motor and identify the wire to the centre contact of the cam-operated switch.

Normal Wiper Operation

Conventional operation of the wipers is obtained by using the vehicle wiper switch in the normal way. Figure 2 shows the sliding contacts of this switch in the correct position for each function. Note that in the off position the switch shorts lead B to lead C. In the SLOW position the short is removed and an earth is extended to B, while in the FAST position the earth is removed from B and extended to A. For single speed wipers slide contact A will be omitted.

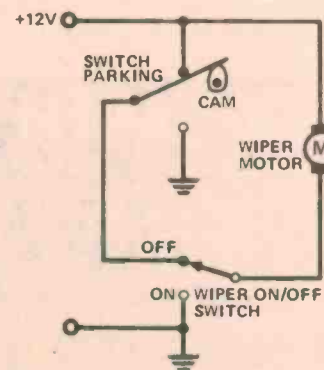


Fig. 1. Circuit of modern wiper motor assembly. Dynamic braking is achieved by applying a short across the armature.

HOW IT WORKS - ETI 319

The timing circuit is energized by operating switch SW1, which is part of switch/potentiometer RV1. This switch applies power to the unijunction/SCR circuit via the still-closed parking switch contacts.

Capacitor C1 charges via RV1 and R1, at a rate determined by the setting of RV1, until the unijunction "fires", producing a positive going pulse which triggers the SCR into conduction. Resistor R4 ensures that the SCR latches on, thus energizing relay RL1.

Relay contacts RL1 (1) now change-over, removing the short circuit from the motor armature before energizing the motor by extending an earth via the now-closed relay contacts.

As the motor gathers speed, the associated cam-actuated switch changes over, removing power from the timing circuit (causing the relay to drop out) and extending an earth to the wiper motor via wiper switch contacts B and C, the now de-energized relay contacts, and the cam-actuated switch.

The wipers continue their sweep across the screen, but on their return the cam-actuated switch cuts in just before the end of the sweep. This removes power from the wiper motor and places a short circuit across the armature.

Operation of the ETI319A unit is similar except the motor, which does not require dynamic braking, can be driven directly from the SCR, saving the cost of a relay. Note that either D1 or D2 become redundant depending on the polarity of the vehicle.

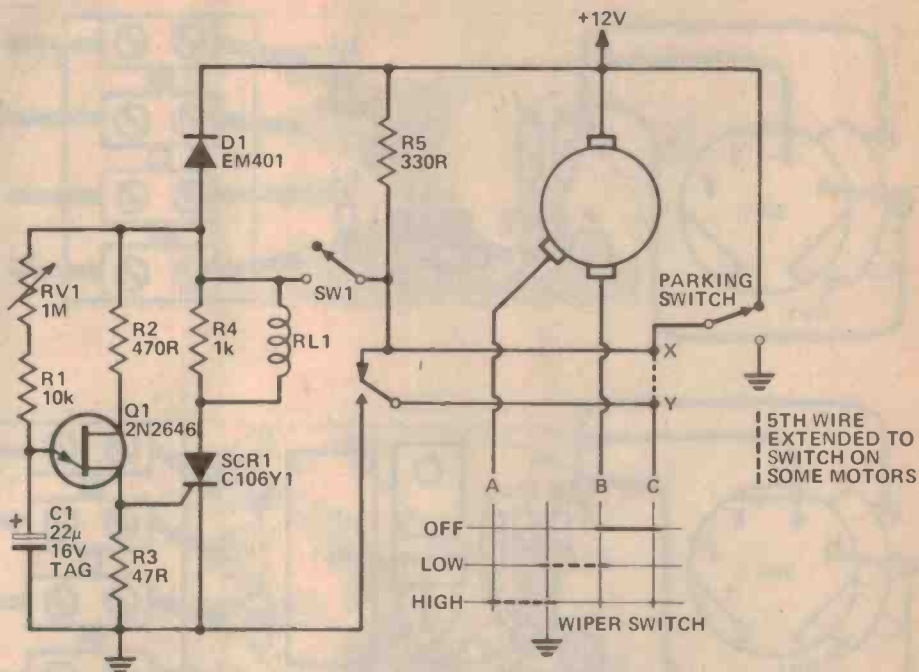


Fig. 2. The ETI319B Vari-Wiper circuit using relay output for use with permanent magnet motors.

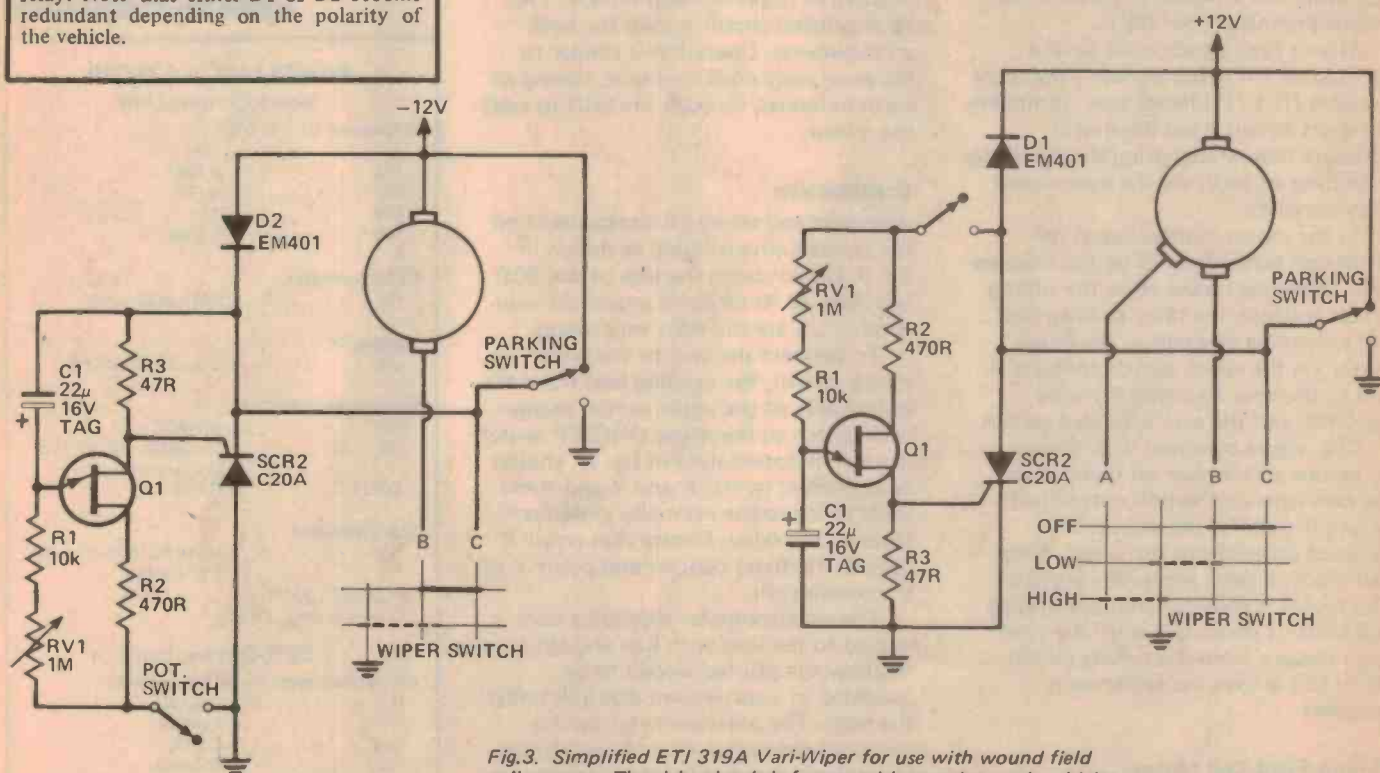


Fig. 3. Simplified ETI 319A Vari-Wiper for use with wound field coil motors. The right circuit is for use with negative earth vehicles, and the left for positive earth. Both share the same PCB.

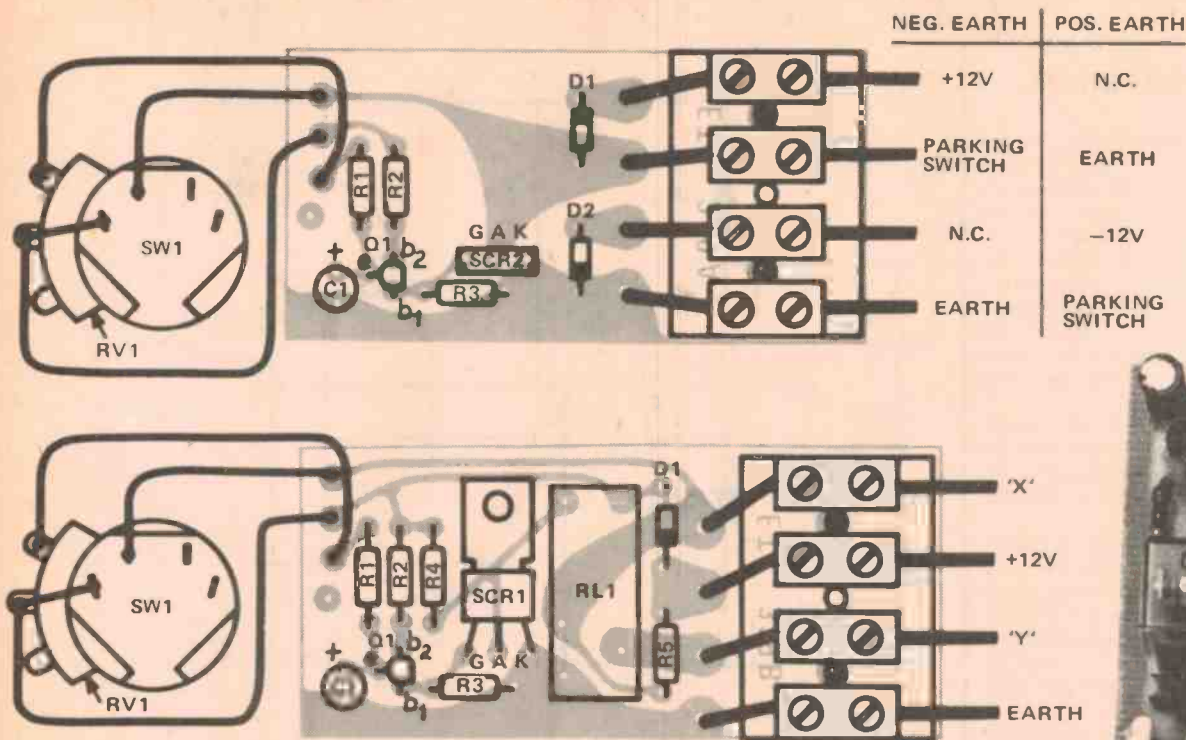


Fig. 5. Component overlays. Note that the same PCB is used for both earth polarities on the ETI 319A.

Delayed Operation

When delayed operation is required, the upper switch is left in the OFF position and the timing circuit energised by operating SW1 which is part of the switch/potentiometer RV1.

After a time which is set by the position of RV1 (0.5-25 secs.) the relay contacts RL1 (1) change over, removing the short circuit from the motor armature before energising the motor by extending an earth via the now closed relay contacts.

As the motor gathers speed the associated cam-operated switch changes over, removing power from the timing circuit (causing the relay to drop out), and extending an earth to the wiper motor via the wiper switch contacts B and C, the now de-energised relay contacts, and the cam-activated switch.

The wipers continue their sweep across the screen, but on their return the cam-operated switch cuts in just before the end of the sweep. This removes power from the wiper motor and places a short across the armature. The motor is thus dynamically braked and remains stationary until the next relay closure from the timing circuit. When this arrives the sequence is repeated.

Wound Field Coil Motors

Because wound field coil motors do not

use dynamic braking, the Vari-Wiper can be made without a relay. Figure 3 shows the simplified Vari-Wiper circuit and its connections to either a positive or negative earth vehicle. The same printed circuit is used for both arrangements. Operation is similar to the previously described unit, having an earth extended through the SCR to start the motor.

Construction

Assemble and solder all components on the printed circuit board as shown in fig. 5. Do not bend the lugs of the SCR too close to its case and ensure all semi-conductors are the right way round.

To connect the unit to the wiper motor circuit, the existing lead from the centre pole of the wiper motor change-over switch to the wiper ON/OFF switch (shown in dotted lines in fig. 2), should be broken at points X and Y and these leads taken to the normally closed contacts on the relay. Ensure that point X goes to the fixed contact and point Y to the moving one.

The potentiometer should be connected to the unit with just enough wire to allow the printed circuit to be mounted in a convenient position under the dash. The potentiometer can be mounted through a 10 mm hole drilled in the fascia panel or by attaching it to a bracket mounted in a convenient place.



PARTS LIST – ETI 319 Relay Output Unit

Resistors all 1/4W 5%	
R1	10k
R2	470R
R3	47R
R4	1k
R5	330R

Potentiometer	
RV1	1M switch pot

Capacitor	
C1	22μ 16 V electro

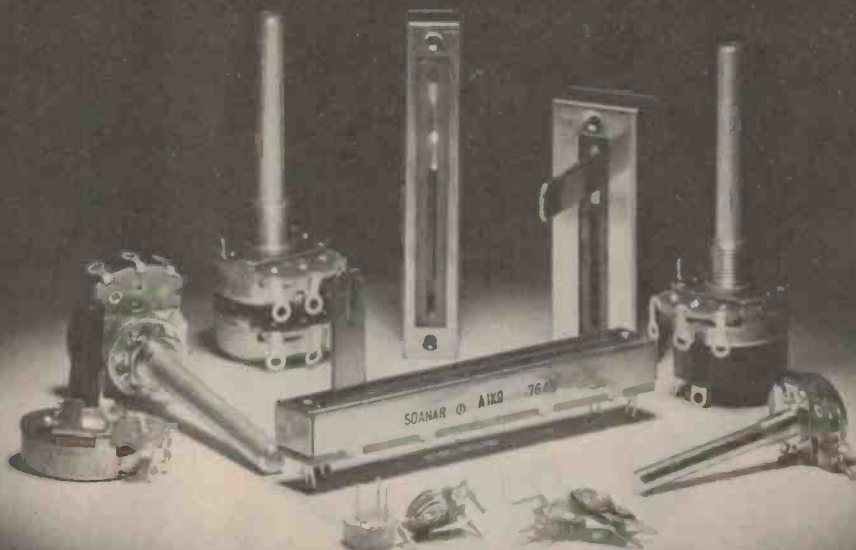
Semiconductors	
D1	EM401
Q1	2N2646 or MU10 unijunction
SCR1	C106Y1

Miscellaneous	
RL1	Mini PC heavy duty 12 V relay
PCB ETI 319B	
Nylon terminal strip	

SCR Output Unit

All components identical, except:	
R5	deleted
D1/2	EM401
SCR2	C20A
RL1	deleted
PCB ETI 319A	

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ETI 318



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The kit includes all components necessary to build the project, including a metal case which has a rectangular hole in the front for the LED display.

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Tunes all CB channels, foreign broadcasts, police, planes, trains—more. Has 10.1cm speaker, squelch on CB/VHF/UHF, dial light, tone control, automatic AC-to-battery switching, FM-AFC, 1/4" headphone jack, telescoping antennas, jack for external SW/CB/FM/VHF antenna. Requires 6 "C" batteries. With AC cord.

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- Tunes VHF-Low, VHF-HI, UHF, CB, AM, FM
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Hear CB channels, police and fire calls, trains, trucks and aircraft, plus AM/FM. Features big 10.1 cm speaker, 1/2" headphone jack, AFC on FM, dial light button, telescoping UHF and FM/CB/VHF swivel-mount antennas and external-antenna jack. AC cord. Requires 4 "C" batteries.

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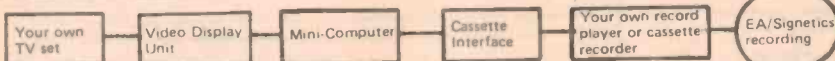
UHF type connections, screw-on lock.

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Components marked † below are required to build the system shown in this block diagram. They make a total of only \$369.20!

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AC/DC cassette recorder ideal for this system.

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LIGHT CHASER

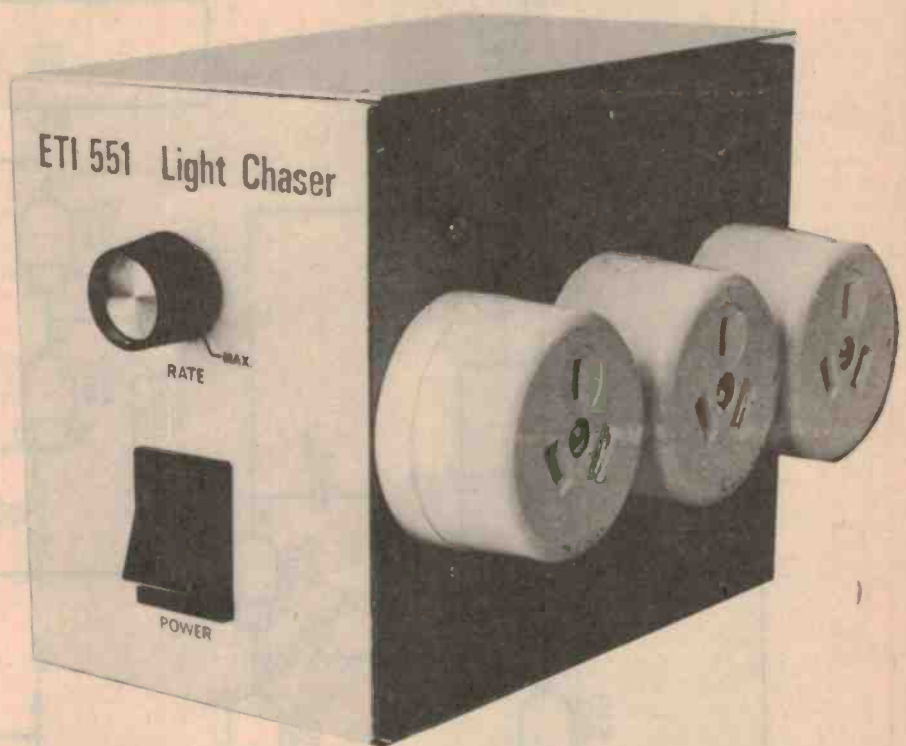
Low cost, simple design handles up to 1000 W per channel and can be expanded if required.

A LIGHT CHASER is a mechanical, or in this case, electronic, gadget which controls three or more sets of lights arranged in a chain. These are flashed on, one at a time in sequence, to create an illusion of movement. Such devices can be seen at fairgrounds, on advertising signs and in shop windows. Here is a design that is simple and cheap to build, and suitable for any of these applications.

Design Features

We have seen many designs for light chasers ranging from three relays switched sequentially by a motor and cam follower contacts to elaborate phase control circuits. We chose to steer for a happy medium retaining features like easily adjustable rate and zero crossing switching but still being simple and cheap to build.

To reduce cost, we decided against using an isolation transformer. Because of this, the *entire* circuit is at mains potential and should therefore be treated with due respect. By using a series capacitor which costs about \$1.50, we save a power transformer (\$4.50) and three pulse transformers (about \$2.00 each), resulting in a \$9 – \$10 saving.



The unit can be expanded beyond three channels if desired by moving the reset line of IC4 (pin 15) from the fourth output to the (n+1)th, where n is the desired number of channels. The sequence in which the pins on IC4 go high is 3,2,4,7,10,1,5,6,9 and 11. Therefore for a 6 channel unit pin 5 will be connected to pin 15. The output stage consisting of the NAND gate, transistors,

capacitor and triac will of course have to be duplicated for each additional channel.

The unit as described is suitable for about 1000W per channel but if additional heatsinks are used this could be raised to the 15 A limit of the triacs or, if different triacs are used (e.g. the BTW 41-400) even higher currents can be handled.

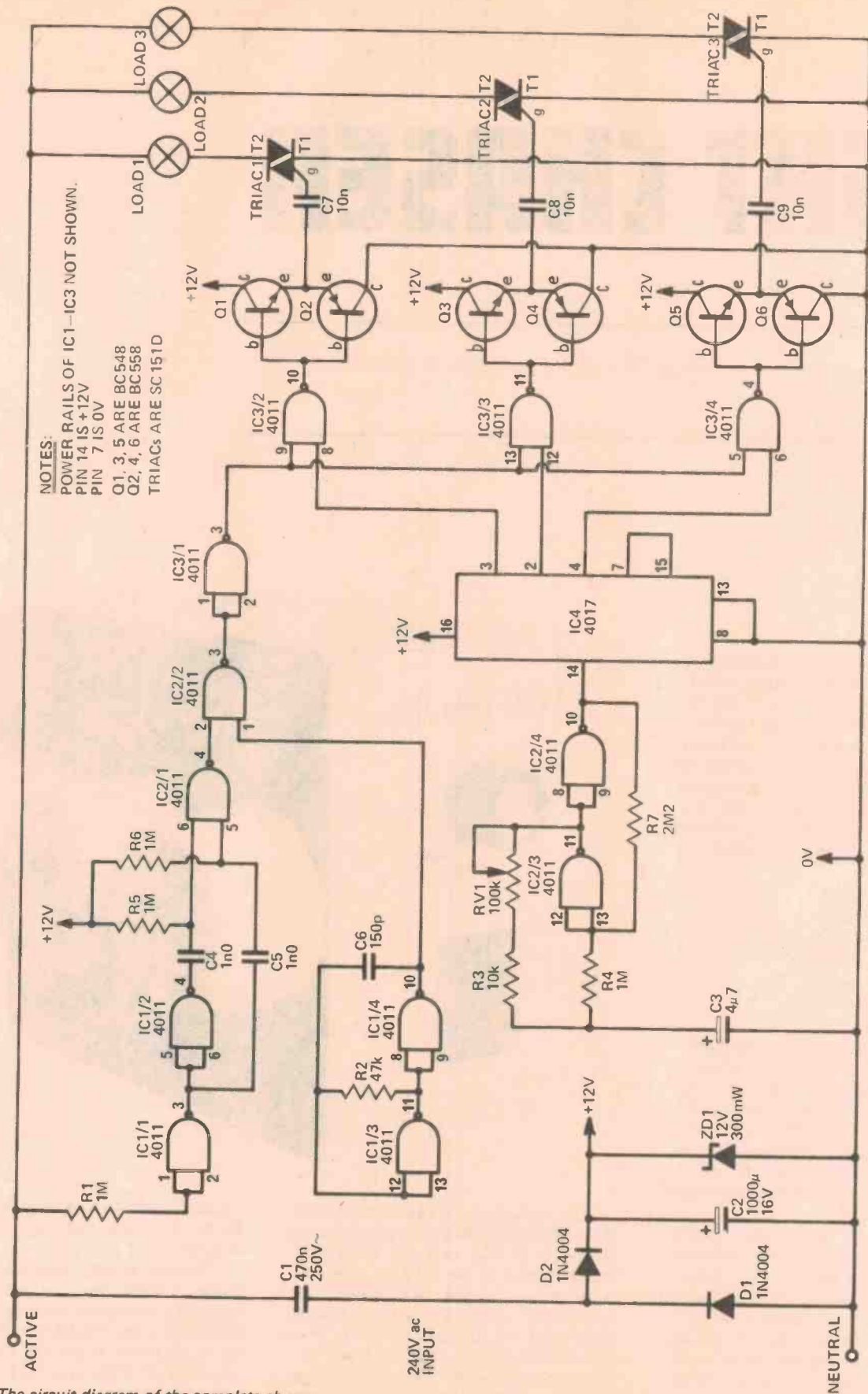


Fig. 1. The circuit diagram of the complete chaser.

HOW IT WORKS – ETI 551

A light chaser consists of three or more ac switches which are turned on, one at a time, in sequence. To make this explanation simpler, we have separated the circuit into several sections.

Power Supply

The 240 Vac is reduced to the 12 Vdc required to operate the control circuitry by the use of a series capacitor C1, the diodes D1 and D2, the smoothing capacitor C2, and is then regulated by zener diode ZD1.

Synchronization Generator

The input to IC1/1 is connected to the 240 Vac supply via the 1 M resistor R1. The value of this resistor, combined with the effects of the protection diodes inside the IC, prevent damage to the IC. The output of this device is a 50 Hz square wave which is synchronized with the mains. IC1/2 is used to invert this square wave and then the RC networks R5/C4 and R6/C5 are used to generate negative pulses on the two inputs of IC2/1 on each zero crossing of the 50 Hz signal – i.e. 100 pulses per second. The width of these pulses is about 0.6 ms.

High Frequency Oscillator

This is formed by IC1/3 and IC1/4, and runs at about 80 kHz. Its output is gated with the synchronizing pulses by IC2/2; this results in 600 μ s long bursts of 80 kHz at the start of each half cycle.

Low Frequency Oscillator

This is formed by IC2/3 and IC2/4 and its frequency is variable by RV1 from 1 Hz to 10 Hz. We have used this form of oscillator in preference to that used for the high frequency oscillator to prevent reverse biasing the tantalum capacitor.

Counter

This is IC4 which is normally a divide-by-ten counter with ten decoded outputs which go high in sequence. By connecting the fourth output back to the reset, a divide-by-three is formed. This IC is clocked by the low frequency oscillator.

Driver & Output Stages

There are three identical output stages consisting of a two input NAND gate, a two transistor buffer, a series capacitor and a triac. The function of the gate is to direct the high frequency tone bursts onto the appropriate triac gate. The counter IC4 selects the required gate.

General

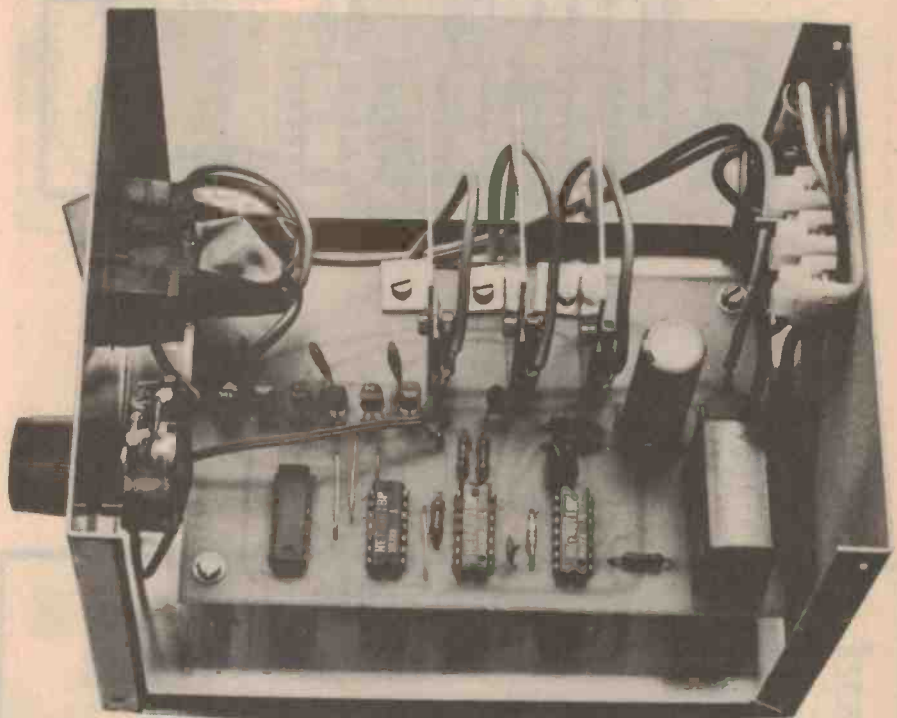
The use of a short tone burst at the start of each half cycle is intended to minimise RFI as the triac can only switch on at this point. This does, however, limit its use to incandescent loads. For use on fluorescent loads C4 and C5 can be increased to 10 n.

The fact that we have not used an isolation transformer reduces the cost, but it does mean that the complete circuit must be considered live! We did not use a fuse in the prototype, but one can be used if required in the active input lead. Ensure that the fuse used will protect the triac.

WARNING

The circuit described here does not use an isolation transformer and therefore all sections of the circuit must be considered dangerous.

If the unit does not work when switched on, disconnect the mains and then, using a separate dc power supply, apply 10 V across C2. Now add a 50 Hz ac signal of 12 – 32 V onto the normal active-neutral input. In this way the control circuitry can be safely checked up to the triacs.



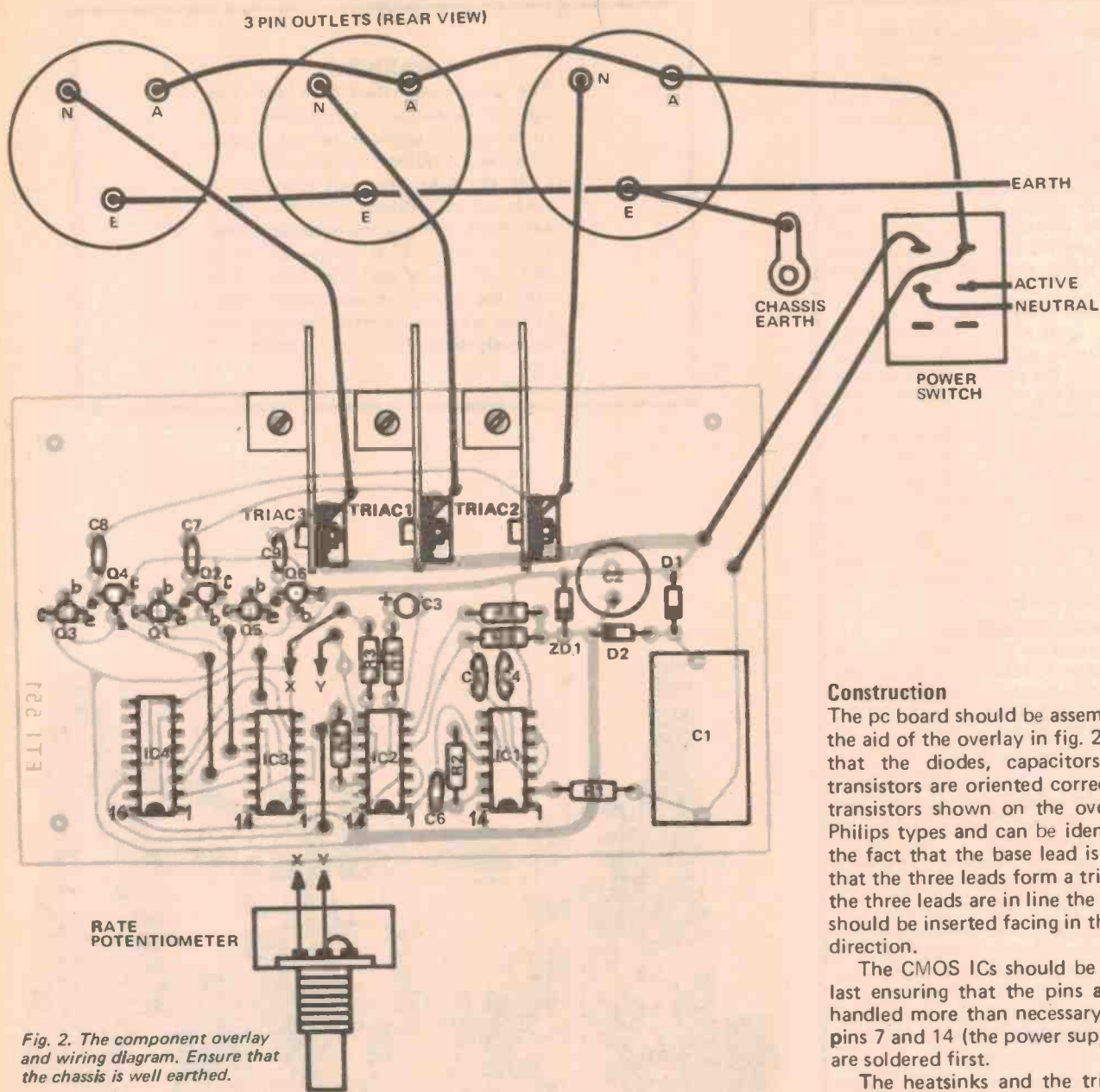


Fig. 2. The component overlay and wiring diagram. Ensure that the chassis is well earthed.

PARTS LIST - ETI 551

Resistors all 1/2W, 5%

R1 1M
 R2 47k
 R3 10k
 R4-R6 . . . 1M
 R7 2M2

Potentiometer

RV1 100k lin (trim or rotary)

Capacitors

C1 470n 250Vac (AEE type PME271M)
 C2 1000µ 16V electro
 C3 4µ7 25V tantalum
 C4, 5 1n0 polyester
 C6 150p ceramic
 C7-C9 10n polyester

Semiconductors

IC1-IC3 . . . 4011 (CMOS)
 IC4 4017 (CMOS)
 Q1, 3, 5 . . . BC548
 Q2, 4, 6 . . . BC558
 D1, 2 1N4004
 ZD1 12V, 300mW
 TRIAC 1-3 SC151D

Miscellaneous

PC board ETI 551
 Metal box to suit
 Three 3 pin power outlets
 Power switch
 3 core flex and plug

Construction

The pc board should be assembled with the aid of the overlay in fig. 2. Ensure that the diodes, capacitors and transistors are oriented correctly. The transistors shown on the overlay are Philips types and can be identified by the fact that the base lead is bent so that the three leads form a triangle. If the three leads are in line the transistors should be inserted facing in the opposite direction.

The CMOS ICs should be inserted last ensuring that the pins are not handled more than necessary and that pins 7 and 14 (the power supply rails) are soldered first.

The heatsinks and the triacs used depends on the intended load. We used about 2500 square mm of aluminum on each triac, and found this to be satisfactory for about 1000 W per channel. The tabs of the triacs are live and separate heatsinks, insulated from earth, should be used or the triacs should be insulated from the heatsink.

We mounted our prototype into a simple folded aluminium box, with an external rate potentiometer and three 3-pin sockets. If an external potentiometer is not required a trim potentiometer can be mounted on the board. To adjust this potentiometer an insulated trimming tool must be used. The unit can be wired according to fig. 2 taking care with insulation as many points are at 240 V.

Get both price and performance

Make a detailed price/performance comparison and you'll find that these DMMs come out on top. Only these models give you bench-top features like four digits and auto ranging plus the kind of price that used to be reserved for field service instruments. Not that the PM 2517 isn't ideal for field service.

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Choice of LED or LCD: so whatever your light/line requirements, there's a Philips DMM to match.

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.018	8c.18	14c	
.022	8c.22	16c	
.027	8c.27	16c	
.033	8c.33	18c	
.039	9c.39	19c	
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33 uF	9c(\$5)	10c(\$6)	11c(\$7)
47 uF	10c(\$6)	12c(\$7)	14c(\$11)
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TEMPERATURE STABILIZED LOG-EXPONENTIAL CONVERTER

This converter can be set up for either logarithmic or exponential operation and incorporates a neat heater circuit for temperature stability.

IN THE CONVENTIONAL musical scale, consecutive notes are not separated by the same frequency, but by the same ratio — the twelfth root of two. This is quite acceptable for most musical instrument manufacturers, except that in electronic music equipment it is easier to make oscillators which have an accurately linear frequency/control voltage characteristic. The keyboards of most music synthesizers give an output voltage of 1 V for each octave on the keyboard. This can easily be generated by a set of equal resistors between the contacts on each key and a voltage applied to each end (normally 5 V). However this means the oscillator is required to have an exponential frequency/control voltage response.

This is where the trouble usually starts. An exponential converter is normally used which relies for its operation on the relationship between current and voltage in a silicon diode or transistor. However unless temperature stabilisation is used the oscillator will not stay in tune for very long. With this unit the transistor used is heated to around 55°C and stabilised at this temperature, eliminating the problem of thermal drift.

In the instrumentation field a lot of functions are displayed in dBs which are a logarithmic measurement. As this unit can be connected in either exp or log modes it is useful for this purpose also.

Construction

As the unit will normally be used with some other equipment, we have not described any mechanical housing. The only difference between the assembly of this board and any other is the oven and the connections to the transistor array package. The oven is made out of two pieces of polystyrene about 55 x 35 x 12 mm. The outside of the oven should

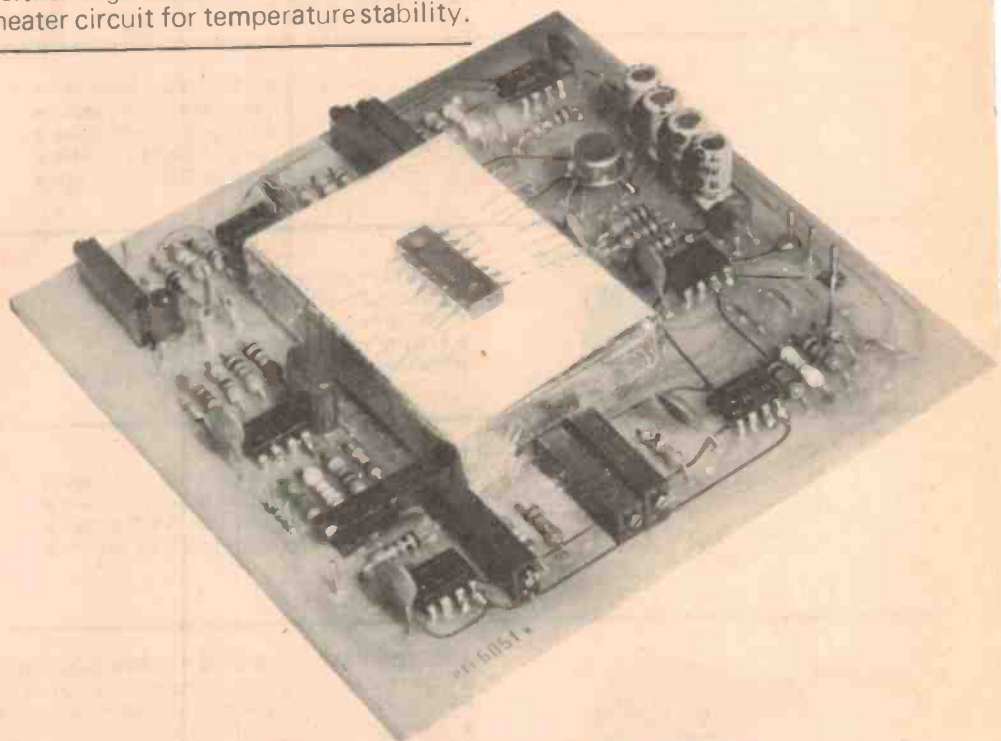


Photo showing the complete unit with the top of the oven removed to show IC5. Note that link 1 is made out of a couple of pins from an old valve socket.

be covered with aluminium foil to help reduce heat loss. The aluminium itself should be covered with a layer of adhesive tape where the leads can touch. A piece of thick paper should be used between the oven and the PCB to insulate the tracks.

The centre of the oven should be hollowed slightly to hold the IC (bend the leads out straight as shown in the photo); a hot soldering iron is the easiest method. Do not remove more than necessary. Now solder a 40 mm length of thin copper wire (a single strand of a multistrand cable is best) to each pin, then with the base of the oven in position, sit the IC in the oven and connect the leads to the appropriate

holes. If a small amount of epoxy cement is placed under the oven it will stay in position. Now fit the top of the oven and secure with a piece of adhesive tape until it has been checked out. It finally can be cemented with epoxy adhesive.

The potentiometer values chosen are a compromise between ease of adjustment and the ability to compensate different transistors. If the potentiometer does not have enough range then the series resistor will have to be varied. We have specified 2% resistors throughout to obtain a better temperature coefficient than is possible with conventional 5% resistors. It will not help to select out of normal 5% types.

SPECIFICATION – ETI 605

Transfer functions
exponential
log.

$$V_{out} = 0.15625 \times 2^{V_{in}}$$

$$V_{out} = \text{Ln}(V_{in}/0.15625) / \text{Ln} 2$$

Useful dynamic range

50dB or 8octaves

Oven temperature

approx. 55° C

Warm up time

about 2 minutes

Power supply

±10 to ±15 volts

HOW IT WORKS – ETI 605

This unit relies on the fact that the collector current of a transistor is exponentially related to the base voltage.

In the log mode the collector of the transistor is linked back to the input of IC1. In this way the collector current is proportional to the input voltage and therefore the voltage on its emitter is logarithmically related to the input voltage. This voltage is then amplified and level shifted by IC3 to give the desired output.

In the exponential mode the 10k resistor R9 is linked back to the input of IC1 and the voltage on the emitter of the transistor is proportional to the input voltage; the collector current is exponentially related to the input voltage. This current is converted to a voltage by IC3.

All this works well provided the transistor is at a constant temperature. Compensation can be made by using other junctions and thermistors, however even the self-heating effect of the transistors can affect linearity. The transistors we have used are part of a transistor array IC which has three individual NPN transistors and a differential pair. We heat the chip up by dissipating heat in the differential pair while measuring the base-emitter voltage of one of the individual transistors. IC8 is used to compare this voltage to one set by the divider R25, 26, 27 and RV7. The base-emitter voltage is normally about 0.67 V at 20° C and drops about 2.2 mV per degree above this temperature. IC8 then stabilises the chip temperature to about 35° C above the temperature at which it was initially calibrated. As it warms up the current in the transistors will fall and when hot the voltage drop across R31 will be low enough that the LED will extinguish. The transistor array is housed in a polystyrene housing to conserve heat.

VALUES OF UNMARKED COMPONENTS		
	LOG	EXPONENTIAL
R3	33k	390k
R5	∞	150k
R13	∞	100k
R15	22k	470k
R17	390k	33k
RV3E	LINK	200k
RV3L	200k	LINK
LINKS REQUIRED		
	A-B	A-D
	D-C	B-C

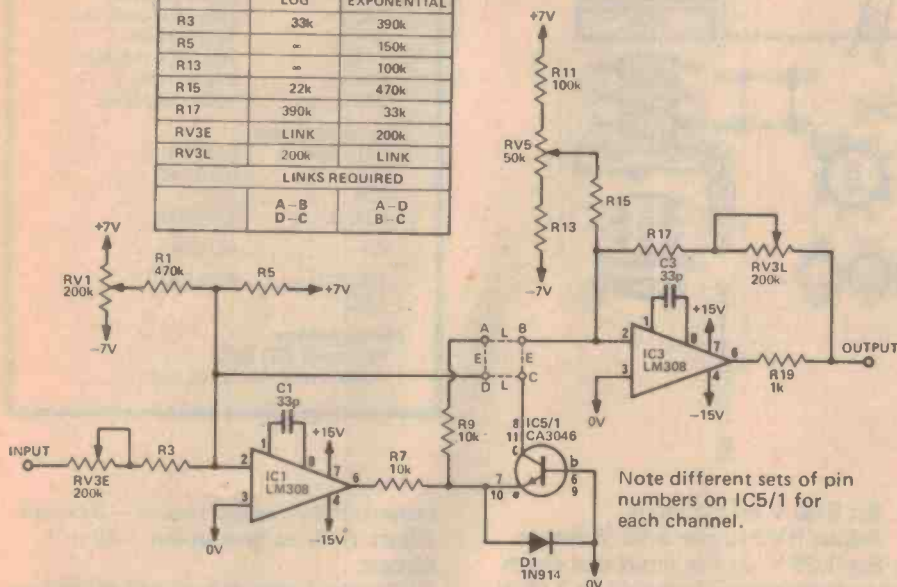


Fig. 1a. The circuit diagram of the converter section. Note that although only one channel is shown here that there are two identical units on the pcb. The component numbers used on the second channel are the missing even numbers, ie R12 is the same as R11.

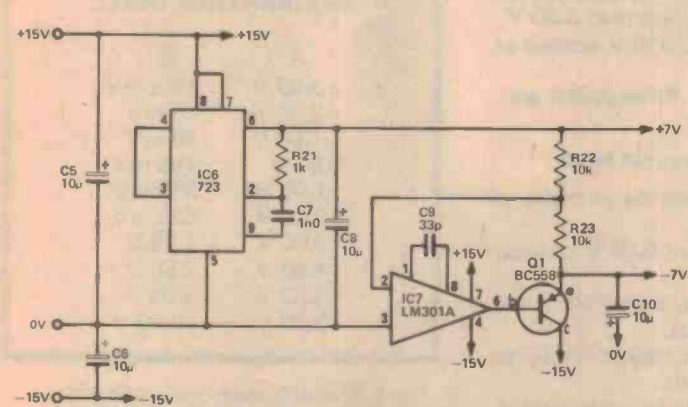


Fig. 1b. The power supply section which supplies the stable ±7 volts needed for the bias and adjustment controls.

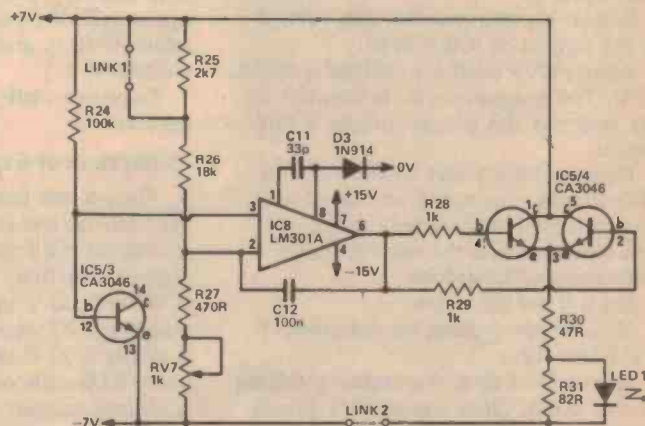


Fig. 1c. The oven circuitry.

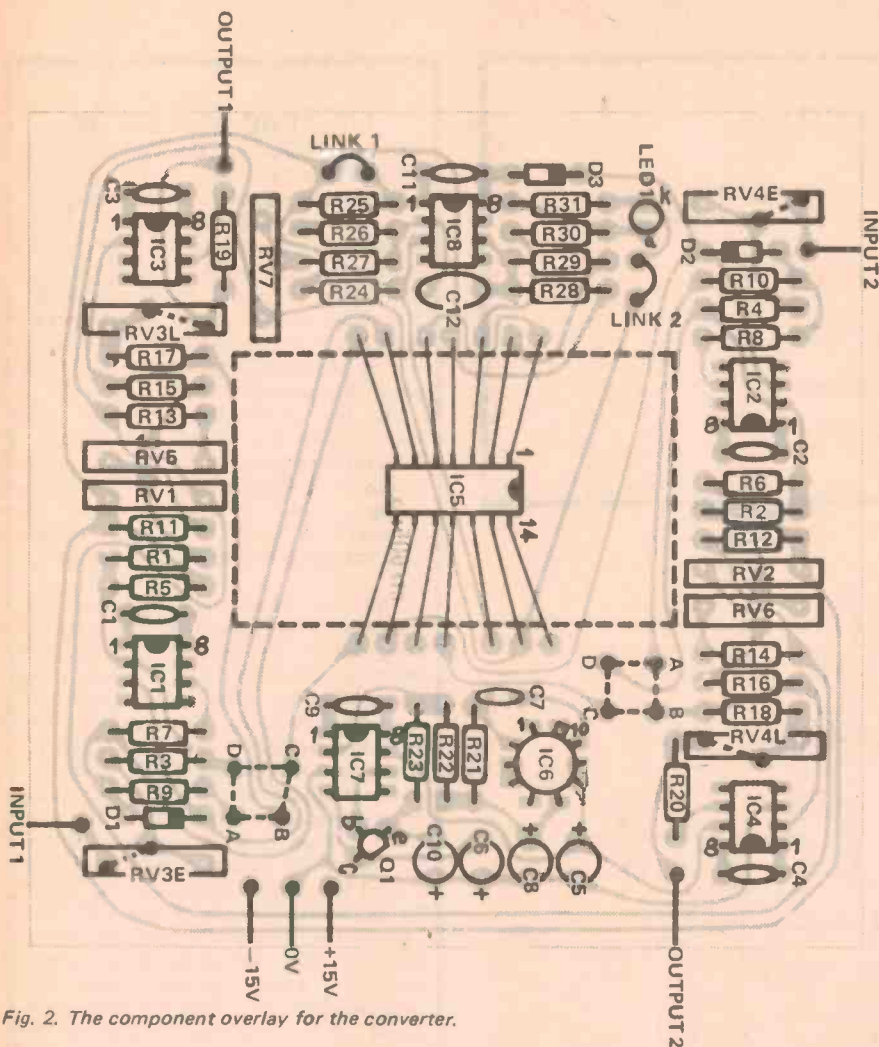


Fig. 2. The component overlay for the converter.

Calibration

The equipment needed comprises an accurate digital voltmeter and a variable power supply with a fine voltage control. The +7 V rail can be used for this with a multi-turn potentiometer.

Oven Control

1. Before switching on, remove link 2 and fit link 1.
2. Switch on and monitor the voltage on the output of IC8 (pin 6).
3. Adjust RV7 until the voltage is about -5 V. The potentiometer is sensitive in this area but the actual voltage is not critical.

4. Remove link 1 and fit link 2. The LED should now come on for about two minutes before slowly going out. This indicates that the oven is stable.

Calibration of Log Mode

1. Set 0 V on the input.
2. Monitor the voltage on the junction of R7 and R9.
3. Adjust RV1 to give a negative voltage on this point. Now adjust RV1 slowly until the voltage just switches positive.
4. Set 0.15625 V on the input.
5. Adjust RV5 to give 0 V output.

6. Set 5.00 V on the input.
7. Adjust RV3 to give 5.00 V output.
8. Set 1.25 V on the input and check the output voltage. It should be 3.00 V. If it is higher go back to step 4 except adjust RV5 to give -0.010 V and use RV1 to bring it back to zero. Continue with step 6, 7 and 8. If the output voltage at 1.25 V input is less than 3.00 V adjust RV5 to give +0.010 V instead of -0.010 V.

Continue until all three points are correct.

Calibration of Exponential Mode

1. Place a link between the junction of R7 and R9, and 0 V.
2. Adjust RV5 to give 0.00 V output. Remove the link.
3. With 0.00 V input, adjust RV1 to give 0.15625 V output.
4. With 5.00 V input, adjust RV3E to give +5.00 volts output.
5. Check output voltage with 3.00 V input. It should be 1.25 V.
6. If high repeat steps 1 - 5 except adjust RV5 to give about +10 mV

PARTS LIST - ETI 605

Resistors all 2%, 5W
 R1, 2 470k
 R3-R6 see table 1
 R7-R10 10k
 R11, 12 100k
 R13-R18 see text
 R19-R21 1k
 R22, 23 10k
 R24 100k
 R25 2k7
 R26 18k
 R27 470R
 R28, 29 1k
 R30 47R
 R31 82R

Potentiometers
 RV1-RV4 200k multturn trim
 RV5, 6 50k multturn trim
 RV7 1k multturn trim

Capacitors
 C1-C4 33p ceramic
 C5, 6 10µ 25V electro
 C7 1n0 polyester
 C8 10µ 25V electro
 C9 33p ceramic
 C10 10µ 25V electro
 C11 33p ceramic
 C12 100n polyester

Semiconductors
 IC1-IC4 LM308
 IC5 CA3046
 IC6 723
 IC7, 8 LM301A
 Q1 BC558
 D1-D3 1N914
 LED

Miscellaneous
 PC board ETI 605
 Polystyrene foam for oven

- output. If low, repeat steps 1 - 5 except adjust RV5 to give about -10 mV output.
7. Continue adjustment until all readings are correct.

CALIBRATION TABLE	
A	B
-3.00 V	19.5 mV
-2.00 V	39 mV
-1.00 V	78 mV
0.00 V	156 mV
+1.00 V	312 mV
+2.00 V	625 mV
+3.00 V	1.25 V
+4.00 V	2.50 V
+5.00 V	5.00 V
+6.00 V	10.00 V

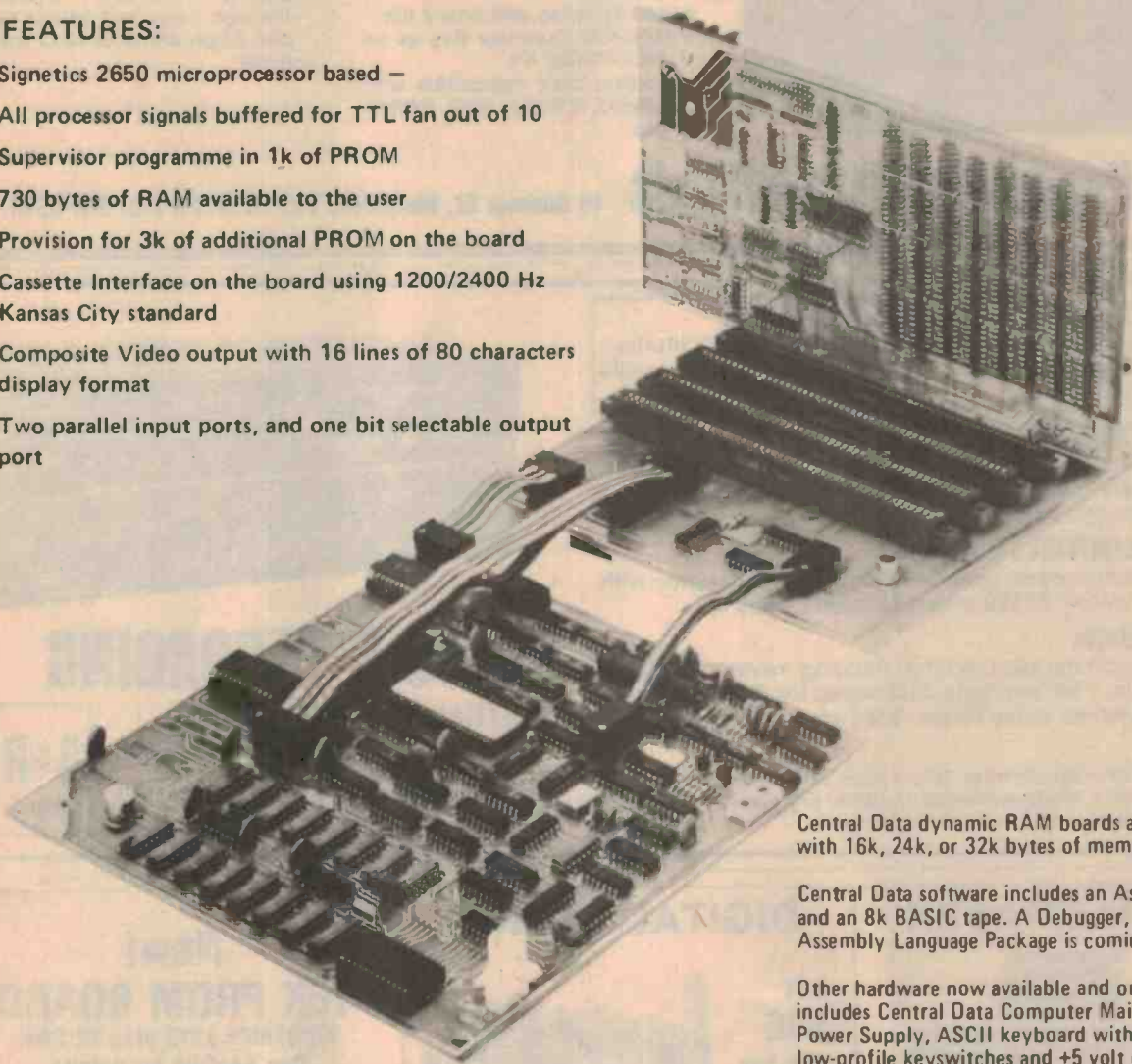
Fig. 3. This table shows the relationship between the input and output. In the exponential mode A is the input with B the output while in the log mode B is the input and A the output.

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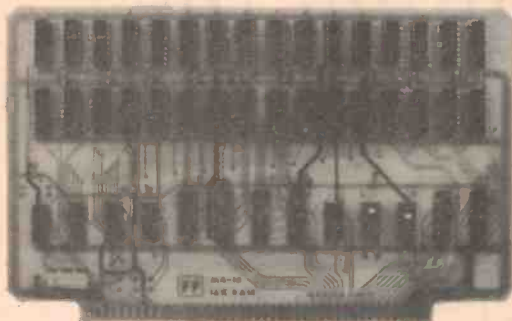
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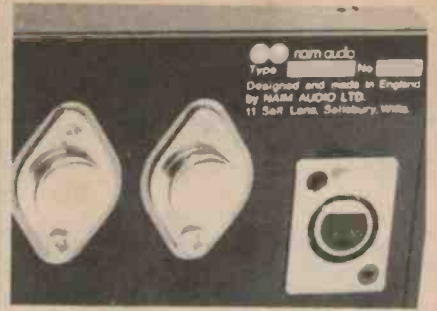
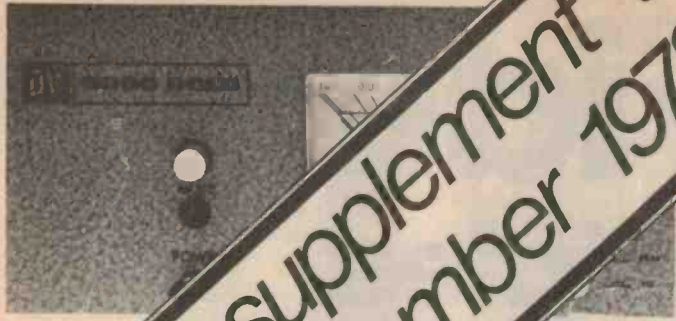
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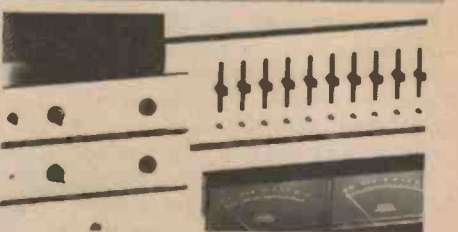
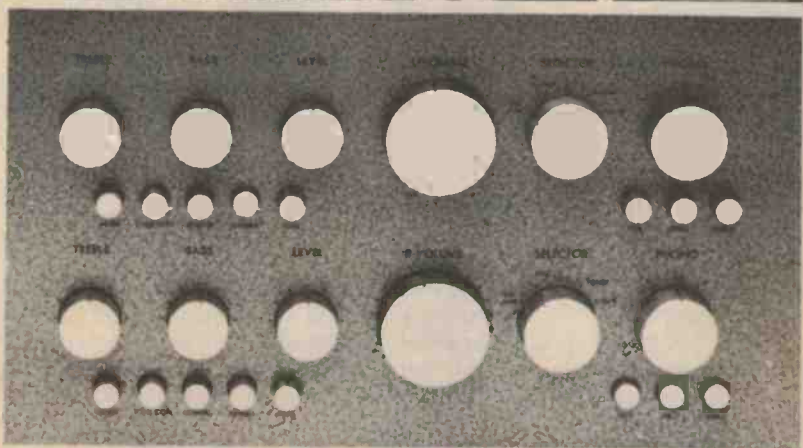
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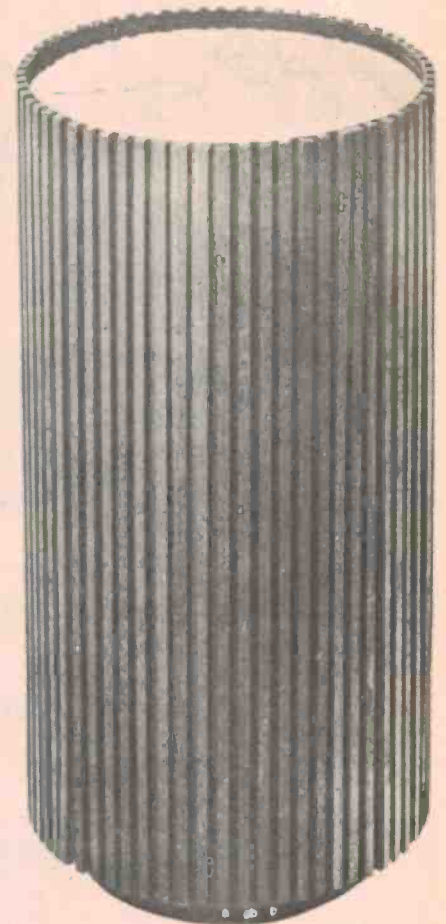
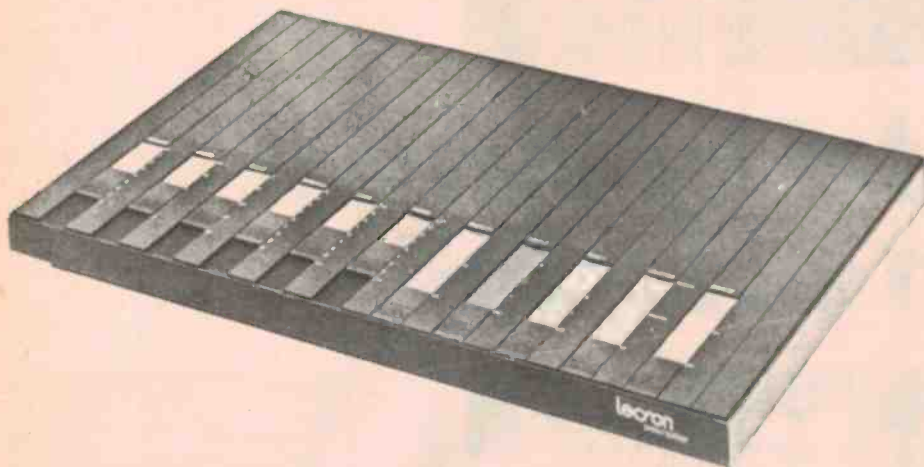


Ultra-Fidelity Amplifiers -design principles



Ultra-Fidelity -design principles

Audio amplifier design has come a long way since the introduction of semiconductors into hi-fi. Stan Curtis, who has been responsible for such excellent examples of the art as the Cambridge Audio and the Lecson, explains here the black arts of ultra hi-fi design.



CAREFUL listening tests have shown that while an amplifier that measures badly is *unlikely* to sound good one that measures well *cannot* be guaranteed to sound good. Thus it is apparent that the traditional measurements of power distortion and frequency response need supplementing by new and more powerful laboratory tests. Such tests should more closely relate to the conditions prevailing when the amplifier is driving realistic loads and using music signals rather than sine-waves, which of course represent only one special case.

Balancing Act

The first such test was popularised by Peter Walker of Quad. It is a simple nulling system which attempts to cancel the input and output signals of an amplifier. With full cancellation whatever remains must be distortion, i.e. signals added to or subtracted from the original. The ideal or perfect amplifier will produce no residual at the output of the nulling circuit.

In practical terms the balancing of this circuit is very difficult if a significant degree of accuracy is required. Thermal drifts can aggravate the problem and generally it is

difficult to set up for more than one amplifier type as usually the whole phase-balance network needs to be recalculated and readjusted each time. However this simple circuit is useful for showing just how often amplifiers are clipping the signal in the course of a piece of music and how frequently some amplifiers slew-rate limit the signal.

However, with such high current capability it is essential that the amplifiers have speaker muting to prevent switch-on "thumps" (or more accurately, earthquakes) and dc offset protection to protect the loudspeakers from the effects of 20 amps of pure dc!

Offsetting Long Tails!

Dc offset has been a major problem with many dc coupled amplifiers (i.e. those having no output capacitor). The offset voltage measured across the output terminals should not be any more than ± 50 mV. Once this voltage starts to rise the loudspeaker is subjected to a dc bias which moves the coil out of the central position. This in turn causes the coil to heat up and the power-handling capability of the loudspeaker to be restricted.

Eventually (and often sooner) the loudspeaker will blow.

Amplifiers

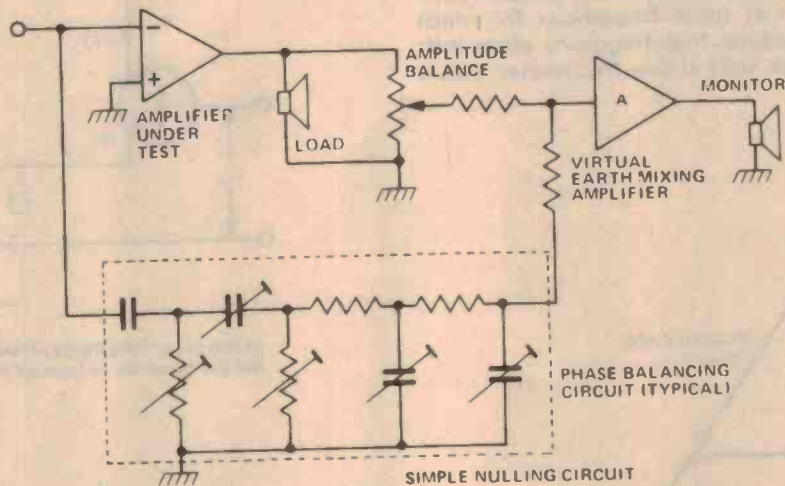
Many amplifiers have an offset voltage that is acceptable when the amplifier is first switched on but which starts to increase as the amplifier heats up. Such amplifiers are subject to thermal drift and this drift is normally due to a component mismatch in the circuit. The conventional amplifier, with a long-tailed pair at the input, is "theoretically" free of thermal drift as these will be automatically compensated for by the DC feedback.

However, this is on the assumption that the first two transistors (or FETs), forming the long-tailed pair, are perfectly matched.

The input offset voltage (upon which the output offset voltage is dependent) is related to the base-emitter voltage V_{BE} of each transistor.

$$\text{e.g. } V_{OS} = V_{BE1} - V_{BE2}$$

This difference can be made almost insignificant by using



Block diagram of the Peter Walker balancing test.

a dual-transistor or a monolithic integrated-circuit differential stage where matching is provided by the simultaneous adjacent fabrication of the two transistors. With discrete transistors, however, a close match is unlikely.

Similarly unbalanced output loading or mismatch of the collector resistors also increases the offset voltage. These mismatches also worsen the linearity (and hence the distortion) of this stage. Thus well designed amplifiers usually use 1% tolerance resistors in these positions and adopt balanced circuitry throughout.

The offset voltage is considerably reduced by the applic-

ation of local dc feedback that occurs when emitter resistors are fitted. In this case;

$$V_{OS} = V_{BE1} - V_{BE2} + I_{E1} R_{e1} - I_{E2} R_{e2}$$

and so by adjusting the balance between R_{e1} and R_{e2} with a trimpot a balance can be achieved.

Emitter Resistance

Note that $R_e = R_E + r_e$ is the total external emitter resistance and r_e is the transistor dynamic emitter resistance. Thus it can be seen that in the earlier typical example of a stage without emitter resistors, an imbalance of r_e and r_e will cause a worsening of the offset voltage. More importantly it can reduce the common mode rejection of the stage.

Of course the presence of emitter resistors also lowers the ac gain of the stage. For reasons to be discussed later this is not such a bad thing. This gain can be recovered by using bypass capacitors.

Clip-on Off Set

Another situation where abnormal dc offset voltages occur is following a clipping overload. When many amplifiers are driven into clipping, the dc voltage of output rises towards one of the HT lines and then when the signal comes out of clipping the amplifier takes a finite time (often several seconds) to recover with the output dc voltage often oscillating between a positive and negative voltage before finally settling back to its nominal zero. Of course, when the amplifier is driven into clipping the normal negative feedback system ceases to control the amplifier.

Ultra-Fidelity Amplifiers -design principles

Thus the dc instability is indicative of poor low frequency stability in the amplifier. Some of the worst (but not all) amplifiers in this respect, have separate ac and dc feedback loops and so have big electrolytic capacitors (decoupling the ac loop) which take time to charge and discharge.

The old Cambridge P100 amplifier had this problem and the effect on the reproduction of a loud bass note can be imagined. Regrettably many amplifiers still suffer from this problem.

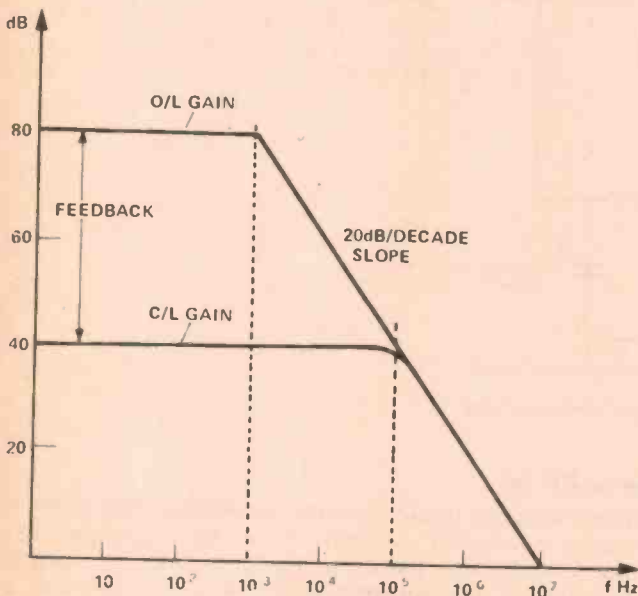
Quite often some amplifiers go unstable without their owners becoming aware of the problem. Sometimes the oscillation may be moderate in level and at a very high frequency; the only symptom being that the amplifier seems to run hotter and next-door's electric drill causes more TV interference than before!

Compensation Phase

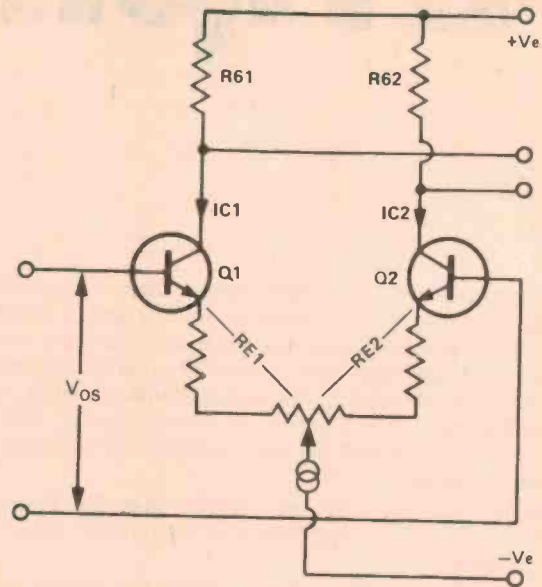
To know why some amplifiers are potentially unstable it is necessary to understand the principles of phase compensation. Much of the low distortion characteristics of amplifiers is achieved through negative feedback. If the phase shift around the feedback loop reaches 360 at any frequency at which the loop gain (i.e. the overall amplifier gain) is unity the result is a self-sustaining oscillation at that frequency.

The phase-inversion to provide negative feedback produces a stabilizing 180 (eg. "out of phase") phase shift, but an additional 180 can be developed in the amplifier.

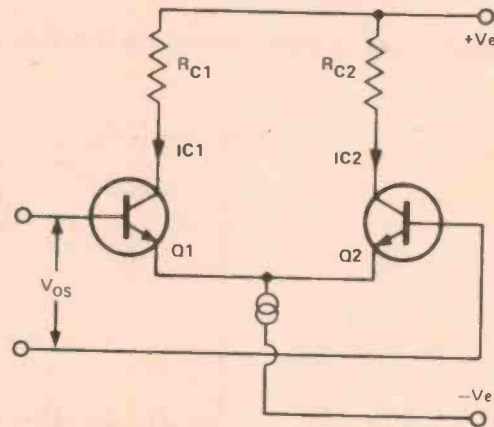
The phase shift developed through an amplifier is the combined phase shift of its several stages, and it usually develops 180 at higher frequencies. To ensure frequency stability under feedback conditions, phase compensation reduces the amplifier gain at those frequencies for which phase shift is high and it reduces high frequency phase shift by accepting a greater phase shift at low frequencies. This is



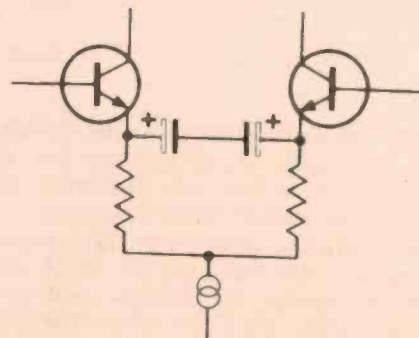
In the case shown in the diagram (unconditional stability) the open-loop response of the amplifier is stabilised by rolling it off at a slow 20 dB/decade slope with a single pole at 1 kHz. This amplifier would be stable with any amount of resistive feedback. However it will be seen that at higher audio frequencies the amount of feedback available reduces and so the distortion of the amplifier will increase. For this reason many amplifiers are of the "marginally stable" type.



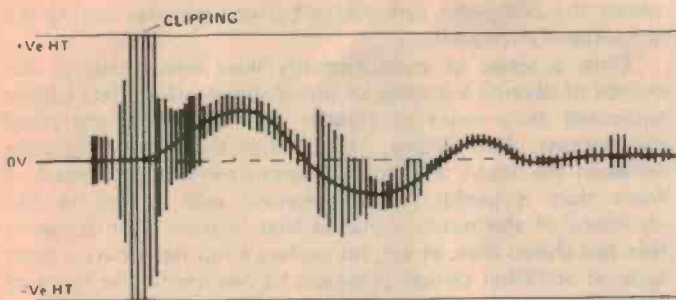
Differential pair with variable emitter resistances balanced by variation of the potentiometer.



In this circuit the input offset voltage is related to the base-emitter voltage of this transistor.



Recovering lost gain by use of bypass capacitors across the emitter resistances.



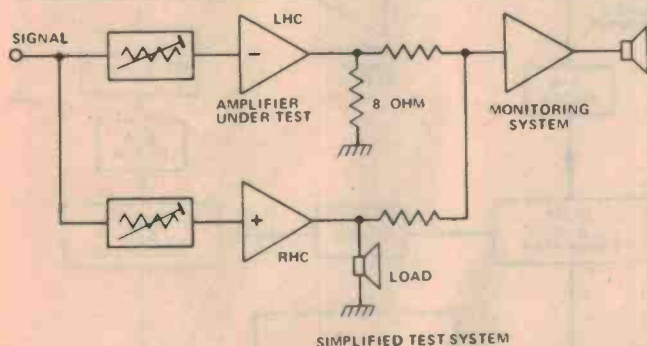
Effect of a sine wave of varying amplitude as signal upon the dc offset voltage at the output.

accomplished by adding response poles and zeros in the form of resistor-capacitor networks (real or inherent in the transistors) in the amplifier circuitry.

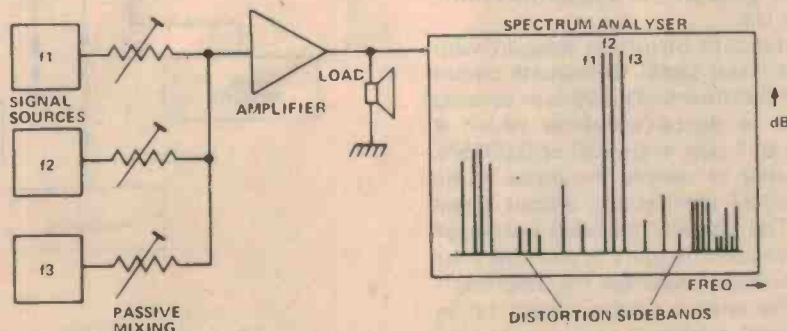
Equally important, to the owner of an expensive pair of loudspeakers, is the problem of high-frequency instability. These days very few high quality amplifiers are so unstable that they break into oscillation. However, quite a few respected units are on the edge of instability and so can potentially become unstable following a shift in operating conditions or of output loading.

Sum Theory

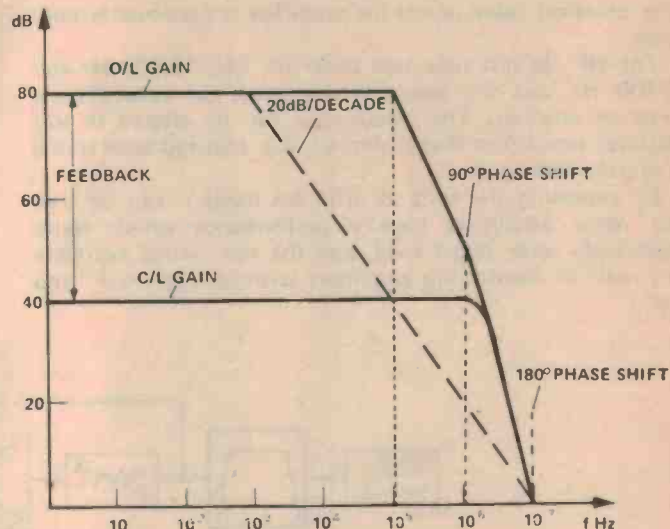
The author used another technique at Cambridge to investigate the changes in amplifier performance that are dependent upon the loudspeaker load. The two channels of a stereo amplifier are driven in mono but one channel is converted to become non-inverting. The outputs of both



Using one channel as an inverting amplifier to monitor distortion produced by the design.



Intermodulation distortion testing using three frequencies.



In this case the amplifier has a fast roll-off which allows an improved closed loop performance at higher frequencies but without careful compensation they are not stable under all conditions of feedback. Once the phase shift reaches 180° the amplifier will become unstable so it can be seen that our example is only marginally stable.

channels are summed and the resulting signal is monitored. Theoretically both channels should transmit the signal in the same way and (for a given circuit design) any distortion, time aberrations etc. should be the same for both channels. It is often quite possible to balance the two channels (driving 8 ohm resistive loads) so that the residual is inaudible. However when one 8 ohm load is replaced by a real "live" loudspeaker the residual betrays problems caused by the new load. In a refined form the test works well and reveals two interesting things;

- i) the two channels of average amplifiers are rarely identical
- ii) some amplifiers work better in the inverting mode than in the non-inverting.

IM High

The conventional IM test uses an LF (50 Hz) and an HF (7 kHz) tone in a 4 to 1 ratio and then measures the sum-total of the sideband (e.g. distortion) components. This is of

Ultra-Fidelity Amplifiers -design principles

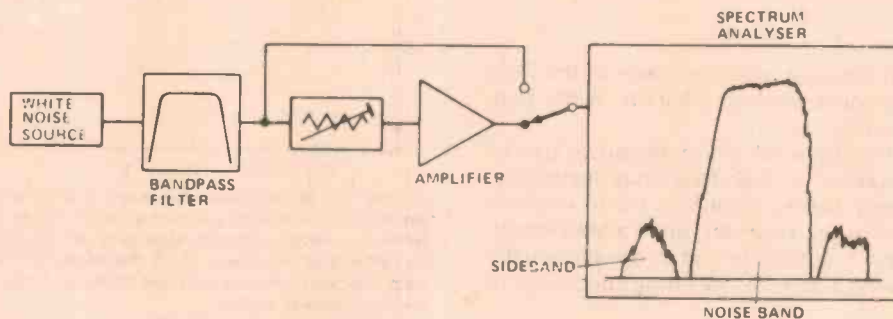
little practical value unless the amplifier is particularly non-linear.

The HF IM test uses two tones of, say, 15 000 Hz and 15 100 Hz and the resulting side-bands are viewed on a spectrum analyser. The frequencies can be altered to suit whatever simulation that is desired, e.g. two sopranos trying to sing the same note.

By repeating the tests at different levels it can be seen that many amplifiers have a performance which varies appreciably with signal level, and the test results correlate very well in identifying amplifiers with an aggressive "top end".

which the computer can use to correct the data during the subsequent error analysis.

Once a series of measurements have been made in the course of playing a passage of music the resultant data can be subjected to a series of Fourier and coherence analytical calculations. Put simply, this means that any difference between the input and output signals can be described in a form that is useful to the engineer and related to the structure of the music signal at that instant. Unfortunately this test shows that, as yet, no perfect amplifier exists — each type of amplifier circuit produces its own particular types of "transient error".



SIMPLIFIED VERSION OF NOISE BAND TEST

Noiseband testing with a spectrum analyser, the sidebands produced by the amp are clearly visible.

Dynamically Noisy

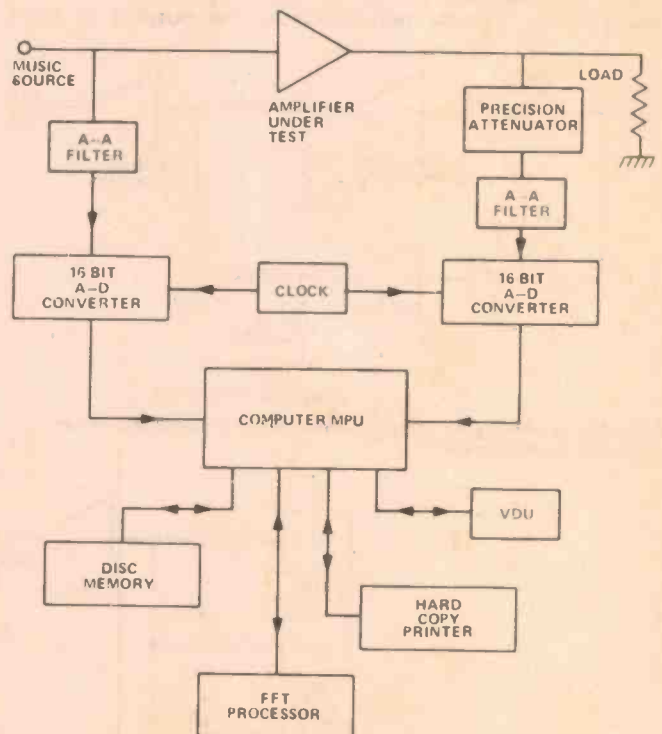
The second test is similar but attempts to measure the amplifiers' performance under more varying "dynamic" conditions. A white noise source has a harmonic and amplitude structure which is variable and random and thus provides a better simulation of a music signal than does a sine-wave. The noise signal is passed through a bandpass filter to define its frequency response. The bandwidth and centre-frequency can be altered to suit the investigation as can the overall operating level. The output of the amplifier is fed to a spectrum analyser where the out of band components can be studied. Again this test is very useful for studying the effects of different loudspeaker loads but more significantly for subjecting the amplifier to random momentary "clipping" overloads.

A Channel and A Log

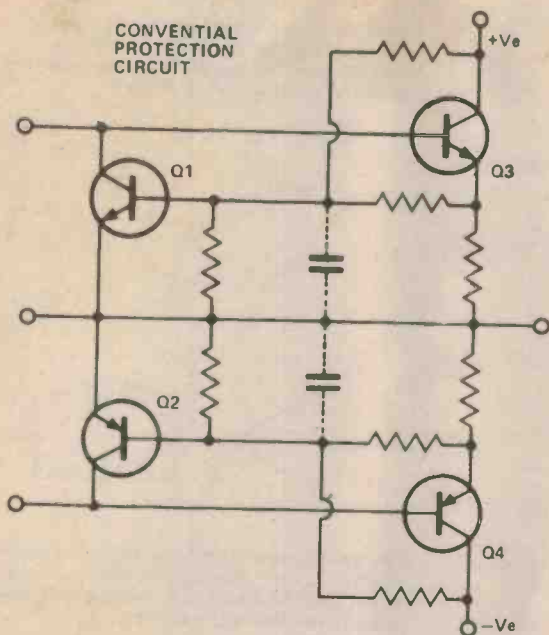
Possibly the most complex type of testing in use is a form of input and output signal comparison used by Analog Engineering Associates of the USA and, in a simplified form, by Mission Electronics in the UK.

AEA have developed a transient distortion measurement system that uses a music as a test signal to evaluate circuit performance under dynamic conditions. This system consists of a dual channel analogue to digital converter which is designed to have a resolution of 1 part in 65,536 or 0.0015%.

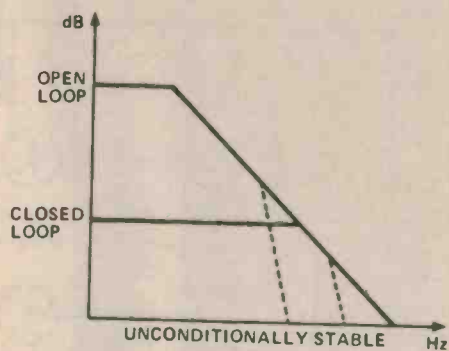
One channel of this is used to sample the input music signal whilst the second channel samples the output signal via a precision attenuator. The digitally encoded output of the converters is fed to a computer memory system for later analysis. Instead of trying to compensate for the amplifier's phase and frequency response with a passive circuit (as in the earlier simple nulling circuit) a frequency sweep is made through the amplifier to generate a "transfer function"



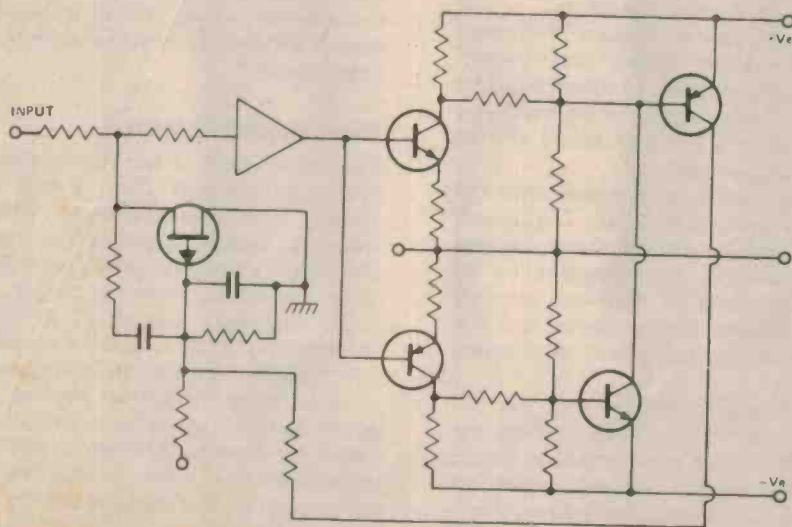
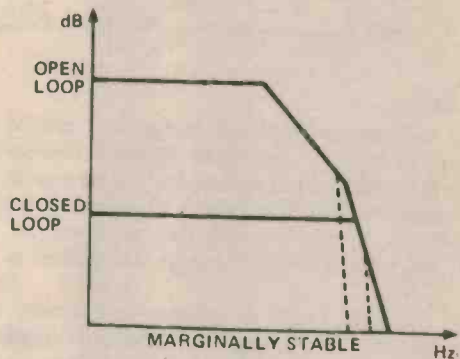
Analog Engineering's transient intermodulation distortion measurement system, used in Britain by Mission Electronics.



A study of the circuit of a conventional V-I protection circuit will show that as the protection transistors turn on they become a 'non-linear resistor' across the bases of output transistors Q3 and Q4 and as such create unpleasant distortion. One solution tried by some companies was to slug the bases of Q1 and Q2 with a capacitor to provide a time delay to prevent the protection operating except during a sustained short-circuit.

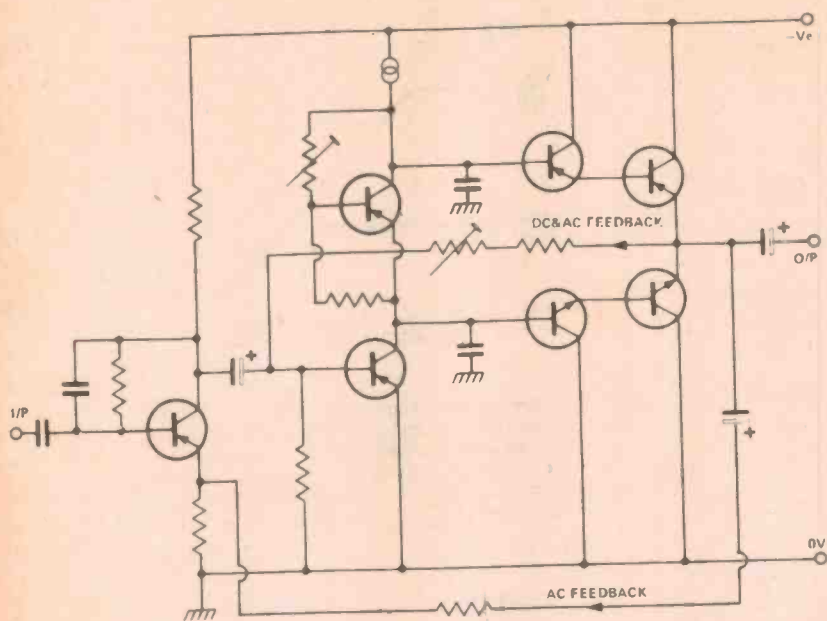


Above: Effect of adding an extra pole at the output of an unconditionally stable amplifier, such as might be added by a complex cross-over network. Below: Same condition applied to marginally stable type. Phase shift now borders on 180° , i.e. oscillation.



In this protection circuit the FET starts to turn-on when full-power is delivered into a 2 ohm load. The main advantage over a conventional protection circuit is that the limiting is "soft" (i.e. very gradual) and thus audibly acceptable and secondly that the distortion is much lower - and still only about 0.1% at limiting.

Ultra-Fidelity Amplifiers -design principles



Circuit diagram showing a typical circuit which would prove to be prone to dc instability when in use. Note that separate paths exist for ac and dc feedback.

Out of The Rut

A few years ago power-amplifier design had settled into a satisfying rut. In the UK the Quad 303 and the Cambridge P-Series had achieved very satisfactory performance figures and they were generally considered to be good amplifiers. In the USA the Crown DC300 has achieved an almost theoretically perfect specification and was hailed as "State of the Art".

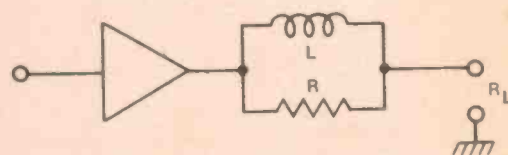
However, the first crack to appear was caused by new loudspeaker designs. Some had very demanding impedance curves which in some cases presented a two ohm load to the amplifier. Such a low value of load (almost a short circuit to some minds!) operated protection circuits in many amplifiers, limiting the current to protect the output transistors.

The operation of these caused a very unpleasant "clipping" sound in some cases and even stranger "clicks" and "bangs" in others. Thus alerted it became apparent to some designers that conventional protection circuits were turning partly-on quite frequently in the course of a piece of music and so giving a sort of premature clipping action.

Without any doubt the best results are achieved when the output stage is devoid of any protection at all. The output stage should be designed to deliver all the current a load demands without limiting. Consider the reproduction of a bass drum. If the amplifier starts to limit the start of the "thump" the sound pressure will collapse and the bass-drum will appear to have no body and thus sound unrealistic.

The output-stage should ideally be able to sink the full energy of the power-supply until its regulation causes the current to limit progressively. So in a good amplifier design the output-stage and the power-supply must be designed as a single item and not as separate circuits. Several amplifiers are designed like this. The Lecson AP3 Mk II, the BGW models 500 and 750, and the Mission Power Amplifier. The Lecson AP3/11 can, for instance, deliver nearly 20 amps to the load before the mains fuse blows and the BGW model 750 even more.

If the amplifier now has to drive a capacitive load eg.



Ever wondered what this circuit in the output of an amplifier is for? Wonder no more — it's to aid the output stage in handling a capacitive loading by partially cancelling the effect.

electrostatic speakers, or complex crossover networks; another pole is added at the output.

In the case of the unconditionally stable amplifier the only ill-effect will be some "ringing" in the closed loop step response — but in the case of the marginally stable amplifier it may go completely unstable. The most popular "belt and braces" solution to this problem is to fit a resistor-inductor network at the output to "cancel-out" the effect of the capacitive loading.

It is interesting to note that some marginally stable amplifiers omit those components as most speaker cables have sufficient resistance and inductance. However, some of the new "Super-Cables" (Litz and Lucas, etc) have a very low resistance and almost no inductance but some capacitance — and their use with certain amplifiers has caused instability, with the amplifier (or speakers) eventually blowing-up!

Which Parameters Matter?

For many years it has been usual to specify and compare amplifiers through their ability to handle a continuous (steady state) sine-wave signal. Thus such a signal is used to measure power-output, frequency response, harmonic distortion, crosstalk, input overload capability, intermodulation distortion, damping factor, and gain! Unfortunately many engineers and Hi Fi pundits still believe that such information is ALL that is necessary to quantify an amplifier's performance and to compare it with others. Not so!

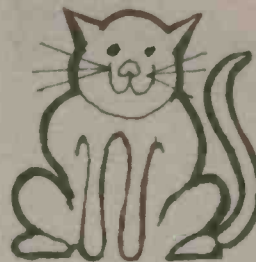
Steady-state sine-wave testing can tell only part of the story and can often be misleading. Music contains complex wave forms with a spectral content of greater than eight octaves and dynamic ranges of up to 100 dB. Yet such complexity is readily understood by the human brain which, in mastering the subtleties of spoken language, has evolved the ability of extraordinary auditory sensory perception. The music signal, as with all audio signals, can be considered in terms of two variable qualities — the frequency domain, and the time domain.

The frequency domain has monopolised engineers' thought

Continued on p.73...

H=2

CAT spells



DAREO

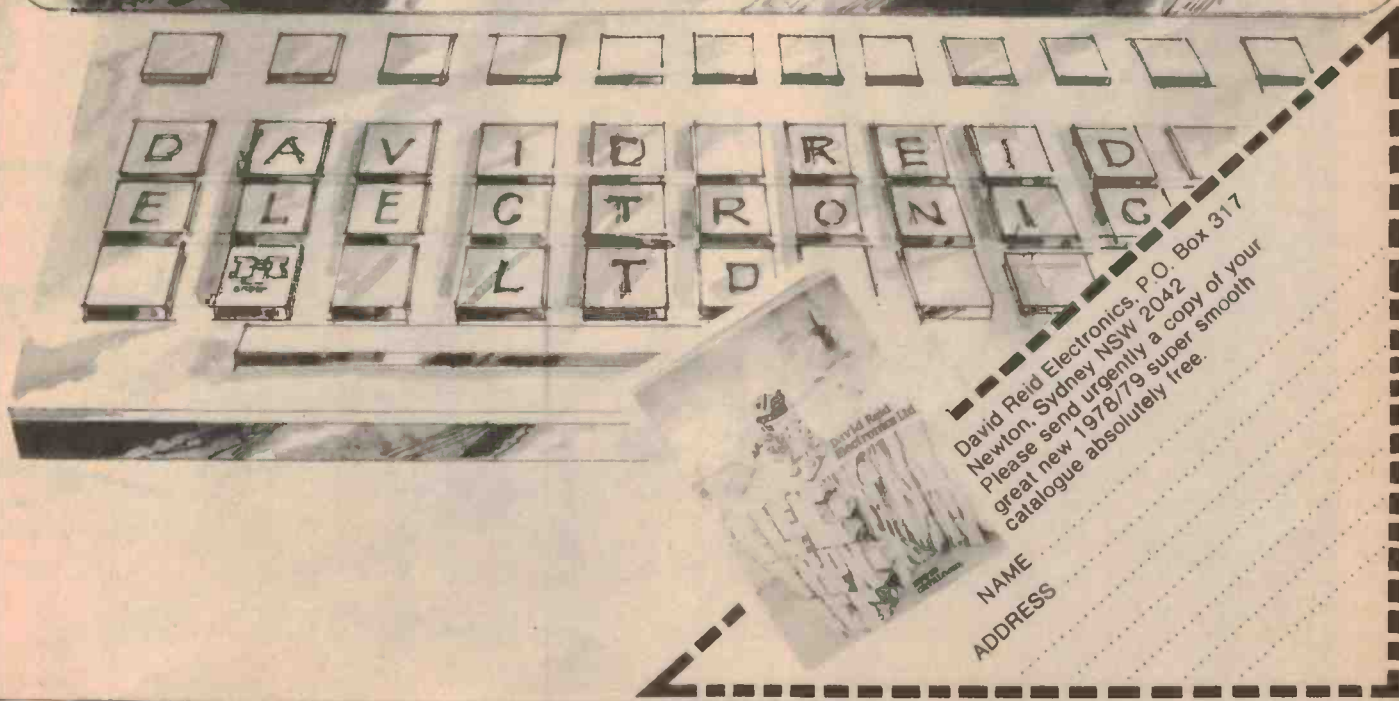
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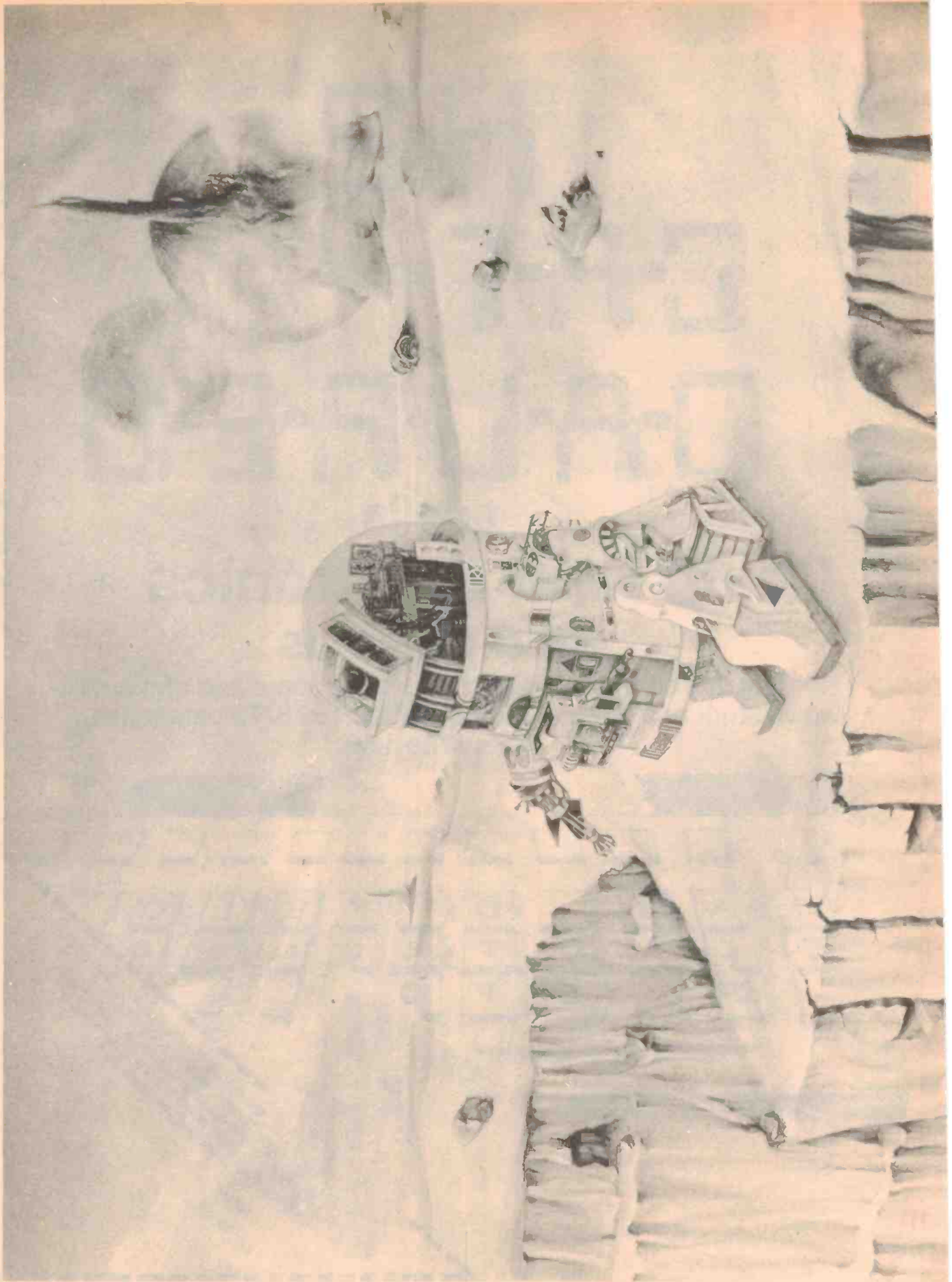
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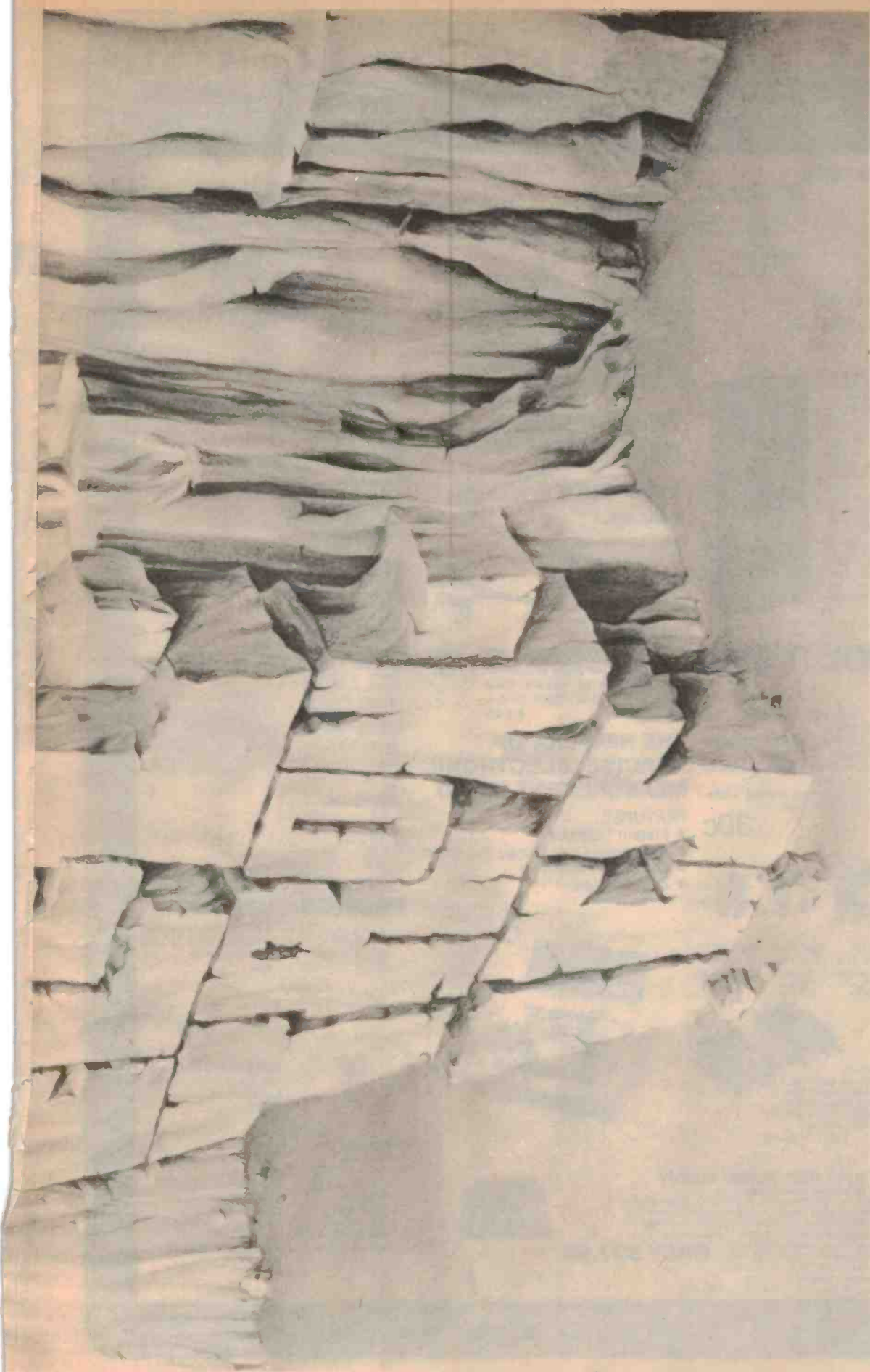
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for so long — even the most complex music signal can be represented by a Fourier analysis.

This mathematical equation lists separately each frequency making up the signal, (together with its phase and amplitude). However, a Fourier analysis is only complete in the case of simple waveforms, with more complex waveforms it becomes only a convenient approximation.

To make a Fourier analysis of a signal the components of that signal have to be analysed over a period of time such that complete cycles of the lowest frequency can occur. Thus we take consideration of the time domain.

Where steady-state signals are concerned the time domain is not normally considered, as the signal is of a continuous unchanging nature between any two periods. If the "time window", during which the signal is Fourier analysed, is reduced progressively it becomes apparent that an accurate spectral analysis becomes less possible. It can then be seen that the important characteristics of the signal are amplitude and rate of change. In other words its envelope.

What Do We Want?

What is required is the amplification of an audio waveform in such a way that the ear can detect no degradation.

Let us consider ways in which such degradation can occur. The waveform envelope can be distorted by amplitude changes of any component or by changes in the phase relationship of the component harmonics.

Experimental work has established that changes in the relative amplitudes of the harmonic structure of the waveform are readily detectable.

Other work has shown that the qualitative characteristics of a complex sound depend upon the phase relationships of the component harmonics. It would seem that as a phase difference must be interpreted as a time delay between the component parts of the signal, then a sufficient phase shift in a system must eventually become audible as these component parts are moved in respect to each other in time. In practice large phase shifts are very audible and indeed telephone lines are often phase and delay corrected to render speech intelligible. However, establishing an acceptable degree of phase shift is extremely difficult.

Following the arrival of "linear phase" loudspeakers great controversy has raged over whether phase shifts affect sound quality. A study of the experimental work performed to date shows that

1. It seems to be very difficult to replicate someone else's experiment.
2. It seems, on balance, that where recurrent waveforms (steady state) such as sine-waves (and instruments producing a "continuous" although decaying tone) are concerned; then quite large phase shifts, between the extremes of the frequency band, have no identifiable effect on sound quality. However, a phase non-linearity on the leading edge of a true transient appears to be audibly more perceptible, particularly on speech and percussive sounds.

Bandwidth and TID

Transient signals cause many problems of which phase linearity is but one. Other problems include; instability and ringing, clipping, slew-rate limiting, and transient inter-modulation distortion.

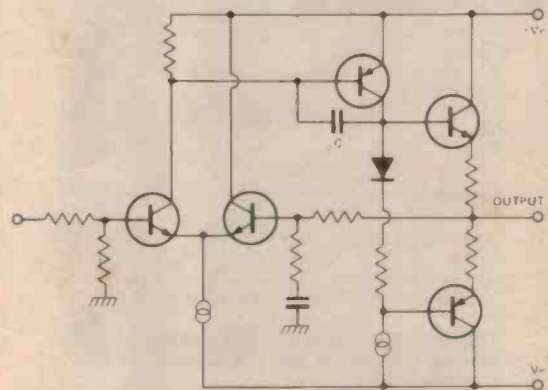
Transient intermodulation distortion (TID or TIM) is much in vogue but is often misunderstood. TID most

commonly occurs when an amplifier, with overall negative feedback over several stages, is driven by a large enough signal whose frequency (or equivalent rise time) is above the open loop bandwidth of that amplifier.

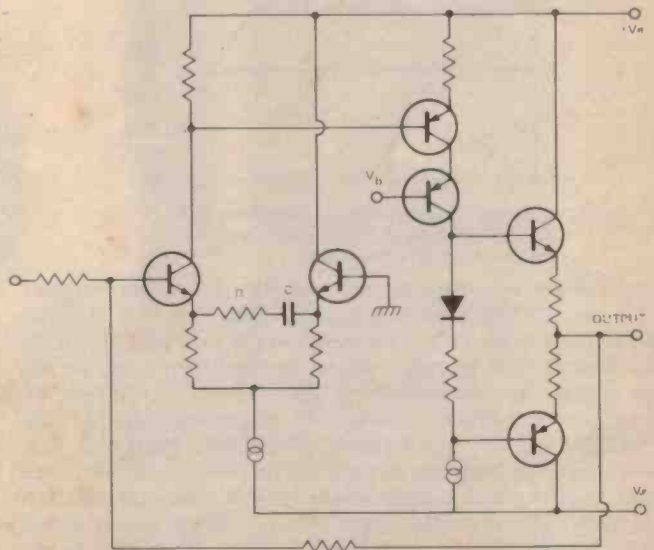
Because the feedback loop is fed from the output of the amplifier, there is no effective feedback until signal current flows at the output, i.e. during the open-loop rise time of the amplifier.

Very large signals occurring in the intermediate stages of the amplifier cause those stages to distort or even to clip. With some amplifiers this clipping can cause the stage to latch-up for a time until the operating conditions stabilise. Thus not only is the leading edge of the signal severely distorted — in some cases it is removed completely.

TID is therefore a form of overloading that is dependent upon both amplitude and time. It is audibly (but at a higher signal level) similar to cross-over distortion, as both effects cause phase and amplitude modulation of the signal due to momentary change in gain. (Remember that at the cross-over point zero, there is no current flow in the output stage and hence no feedback current and so the amplifier is momentarily open-loop.)



Circuit diagram of a typical amplifier circuit which employs lag compensation techniques — provided by C.



Lead compensation: components R and C provide the time constant.

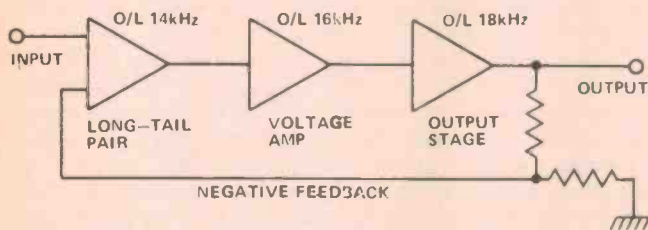
Ultra-Fidelity Amplifiers - design principles

Making Big Bands

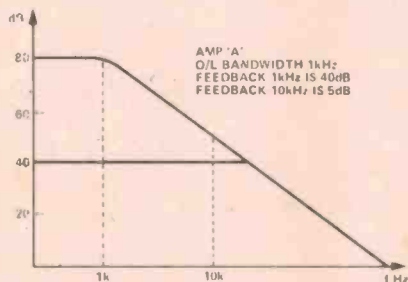
TID can be avoided by designing an amplifier whose open-loop bandwidth is greater than the highest frequency of the input signal. The maximum bandwidth can then be defined at the input by a passive RC filter. Thus if we decide upon a maximum signal bandwidth of 20 kHz then our filter will limit the signal waveform rise-time to $T = 0.35$.

$$T = \frac{0.35}{20 \text{ kHz}}$$

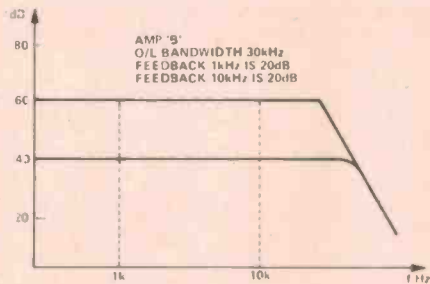
i.e. 17.5 μ s.



Third method of avoiding TID. Each stage in the design has a wider bandwidth than the preceding one.



This amplifier design has a limited open loop bandwidth and the THD will rise with frequency.



Contrast this with the graph above. The bandwidth here is much wider, resulting in a more linear THD response.

Our amplifier's open-loop bandwidth should be designed to be, say, 23 kHz, giving it an open-loop rise-time of 15 μ s and freedom from TID. If however, in the interests of a good specification, and possibly better reproduction, we decide upon a close-loop bandwidth of 100 kHz (i.e. a rise time of 3.5 μ s) then our amplifier will need an open-loop bandwidth of greater than 100 kHz to maintain freedom from TID. In a power amplifier such performance is not easy to obtain. Fast power transistors are notoriously easy to blow-up and are expensive. The common form of lag compensation (used where the open-loop bandwidth is restricted) has to be replaced by lead compensation:—

Another technique is an extension of the first in that the

preceding stage of the power-amplifier is designed to have a lower open-loop band width than the next.

Important or Not?

Many people now consider that TID is unimportant or even that it doesn't exist. This is partly because it is very difficult to measure and only readily visible (in the laboratory) in the "clipping" state. To reach this stage with most amplifiers (but not TID-free designs) there is a requirement for either fast rise-time or higher signal levels or both, — conditions that are unlikely to occur in practice. However, a large degree of non-linearity and hence bad intermodulation will still occur with more realisable input signals. Although this cannot be measured yet (how do you measure say, 5% IM over a period of 5 milliseconds?) it can be predicted mathematically and, just as important, heard. Amplifiers free of TID have a very "open" quality with accuracy of depth.

An amplifier designed with a wide open-loop bandwidth, for low TID, often has other more tangible benefits. The high frequency THD is usually no higher than at the mid-point; in stark contrast to more traditional designs. This is because gain is still available at high frequencies for negative feedback. Such amplifiers also usually have much higher slew-rate.

Slew

Slew-rate defines the speed with which the amplifier can deliver output voltage to the load. For example, if an amplifier has a maximum output of 100 volts p/p and a rise-time of 100 μ s, then the amplifier, if it were perfect, should have an output of about 80 volts after 10 μ s in response to a suitable square wave input. In other words the output voltage would have risen at the rate of 8 V/ μ s. However, amplifiers do not generally respond to large changes as fast as their small signal characteristics predict, for circuit and transistor capacitances can be charged only as fast as their driving circuits allow.

In its simplest form the slew-rate of an amplifier defines how fast the output voltage can change for large signal conditions, and it is normally quoted in volts per micro second. The maximum slew-rate of an amplifier is usually limited by the slowest stage in its circuit.

That stage will have an operating current T (as set in the design) and a capacitance C (usually a frequency compensation capacitor)

$$\text{Slew-Rate} = \frac{T}{C}$$

Thus if a transistor stage has a standing current of 100 μ A and is compensated by a 43 pF capacitor then its slew-rate will be

$$\frac{100}{33}$$

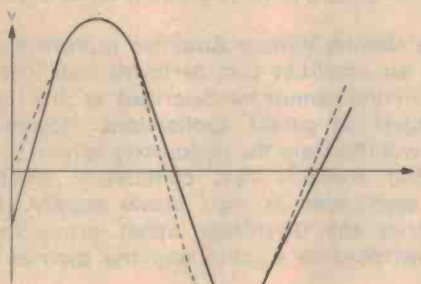
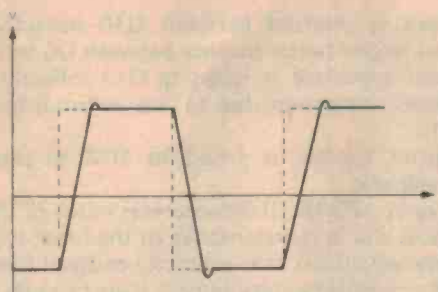
i.e. 3 V/ μ s

Depending upon the design some circuits have a different slew-rate depending upon whether their output is negative-going or positive-going. Slew limiting also defines the full-power bandwidth; a figure more commonly quoted by manufacturers.

$$f_p = \frac{SR}{2\pi E_{op}} \quad E_{op} = \text{peak output swing in volts}$$

f_p = Full power bandwidth in hertz.

Thus in a 100 watt (into 8 ohms) amplifier having full-power bandwidth of 20 kHz the required minimum slew-



The effects of slew-rate on a signal passing through an amplifier prone to this fault. Top: a squarewave, note the slight overshoot. Below that, a sinewave. In both cases the dotted line represents the input.

rate would be about $5 \text{ V}/\mu\text{s}$. This is, however, the absolute minimum figure and experience suggests that such an amplifier would have a hard, gritty high-frequency sound. Such an amplifier should have a slew-rate greater than $20 \text{ V}/\mu\text{s}$ to be certain of avoiding the increase in distortion caused by the gradual onset of slew-limiting.

Unfortunately the higher the power output of the amplifier the greater the required slew-rate as more volts swing at the output in the same period of time and so as our 100 W amp needs $20 \text{ V}/\mu\text{s}$ an otherwise identical 50 W amp needs $14 \text{ V}/\mu\text{s}$ and a 20 W amp needs only $9 \text{ V}/\mu\text{s}$. But these forms of distortion tend to give subtle audible effects compared to the most common amplifier problem — that of clipping.

Clipping

Clipping occurs when an amplifier is overloaded by high level signal peaks. Such peaks occur frequently in much music material and so the manner in which the amplifier clips determines its audibility. A soft, clipping effect where the distortion rises gradually (typical of valve amplifier circuits) is audibly preferable to the hard clipping typical of transistor circuits.

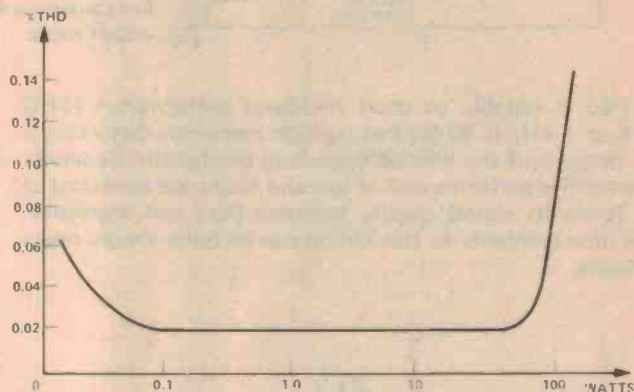
Worse still, some amplifiers tend to suffer saturation effects on clipping and take a time to recover; thus artificially extending the length of time the signal is clipped. The use of overall negative feedback to reduce distortion unfortunately makes things worse. Overall feedback effectively linearises the clipping — the distortion changes from 0.01% (say) to 10%, and quite suddenly too.

Design Procedure

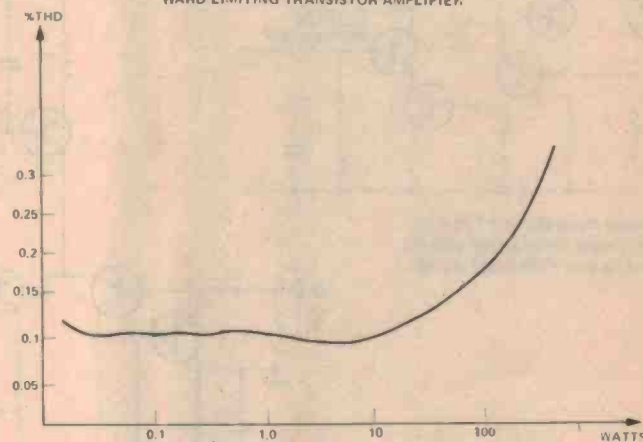
We have covered just a few of the requirements a designer must consider when working upon the design of power-amplifiers. There are many more to be considered to even

rough out a design specification before the circuit hardware is considered. The following sequence is mandatory:

1. What parameters are important to prevent audible degradation of the signal?
2. Detail a performance specification that meets the requirements of (1).
3. Decide upon the circuit technology necessary; Bipolar; MOSFET; Valve; Class A; Class B; Switching; etc; etc.
4. Undertake a development programme to produce a prototype.



HARD LIMITING TRANSISTOR AMPLIFIER



SOFT LIMITING VALVE AMPLIFIER

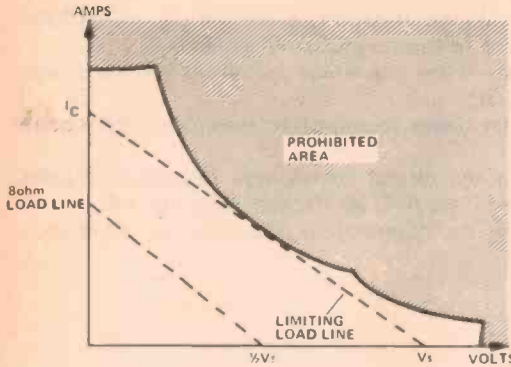
A comparison of the limiting characteristics — in general — of both transistor and valve amplifier types. There is a body of opinion which holds these curves to be the whole truth as to why valve amplifiers are preferred by many musicians.

At this point the designer has to accept that it's a real world and that his performance specification cannot be achieved in a way that is acceptable to accountants, salesmen, customers, customer's wives or whoever else is around. Trade-offs are necessary and much of the "art" is in deciding which defects and degradations are more acceptable than others.

As an illustration of the changes in design approach over the years we will briefly illustrate three designs for which the author has been responsible:

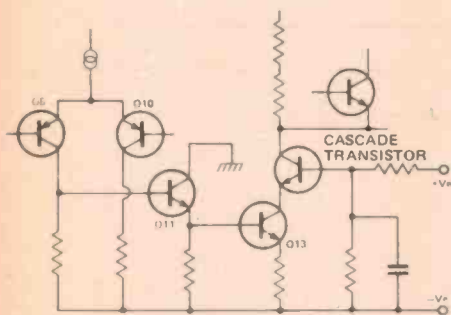
1. Cambridge Audio P60 (P80)
2. Lecson AP3 Mk II
3. Mission Electronics Voltage Amplifier

Ultra-Fidelity Amplifiers -design principles



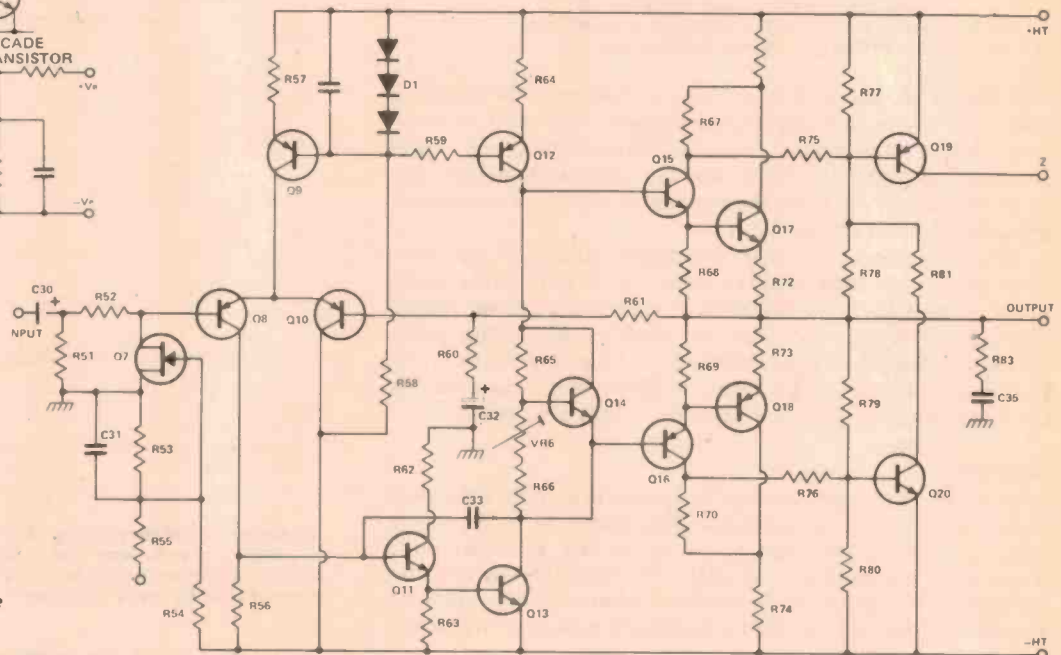
Illustrating the load line conditions for output stages.

The P60 is capable of good mid-band performance (THD 0.01% at 1 kHz is 30 W) but its high frequency distortion is poor because of the limited open-loop bandwidth. Generally this amplifier performs well at low and moderate levels but at high levels its sound quality becomes hard and aggressive. Some improvements to this circuit can be quite simply made as follows:



Showing how some of the improvements mentioned can be added to the P60 basic design.

Full circuit diagram of the Cambridge P60 power amplifier design.



HOW IT WORKS—Cambridge P60

The P60 power amplifier is of a conventional design but with care being taken to optimise each stage. Q8 and Q10 form a long-tailed pair with Q9 as their emitter current source. Q8 and Q10 must be very closely matched for minimum DC offset and for maximum common-mode rejection to avoid H. T. ripple appearing at the output. The next stage is the Q13 voltage amplifier which is loaded by a current source (Q12) instead of the more common "bootstrapped" resistors. Note that Q13 is buffered

from the long-tail pair by an emitter follower (Q11) to prevent any loading of that stage worsening the distortion characteristics.

Capacitor C33 gives lag compensation which defines the dominant pole of the amplifiers. The open-loop bandwidth is quite high (for this type of circuit) at 12 kHz but none the less this amplifier is prone to TID effects. The protection circuit is very unusual in that the output is limited by an FET (Q7), Q19 and Q20 each form conven-

tional V-I summing circuits which monitor the loading on the output stage.

If either Q19 or Q20 turns-on, the gate of the FET Q7 (normally biased-off by R54 to the negative HT) is biased positive and it starts to turn-on. It then acts as a potential divider with R52 and thus attenuates the audio signal. This protection only turns on at the equivalent of 50 W into 2 Ohms load and when it turns on it only adds moderate distortion (0.2% typically) as distinct from clipping.

1. A resistor is inserted between Q10 collector and the negative rail to give better balance between Q8 and Q10.
2. A cascade transistor is fitted to Q13 collector to reduce "early effect" distortion due to the collector-base capacitance of Q13.
3. An emitter resistor is fitted to Q13 to provide local negative feedback.

The Lecson AP3 Mk II incorporates much of the thinking in this article and is representative of the latest types of high performance amplifiers. It is a directly-coupled Class B design using a fully complementary output stage of series connected transistors and gives a power output of around 150 watts per channel.

The New Mission Voltage Amplifier represents an attempt to produce an amplifier that performs well irrespective of load. The circuits cannot be described at this stage as they are the subject of patent applications. However, a brief description will illustrate the philosophy behind the design.

The casing contains two completely separate mono amplifiers, each with its own power supply. A separate module carries the dc-voltage offset protection circuits; the delay switched-on circuits; and the thermal protection

circuits. Particular attention has been paid in the design to achieving:

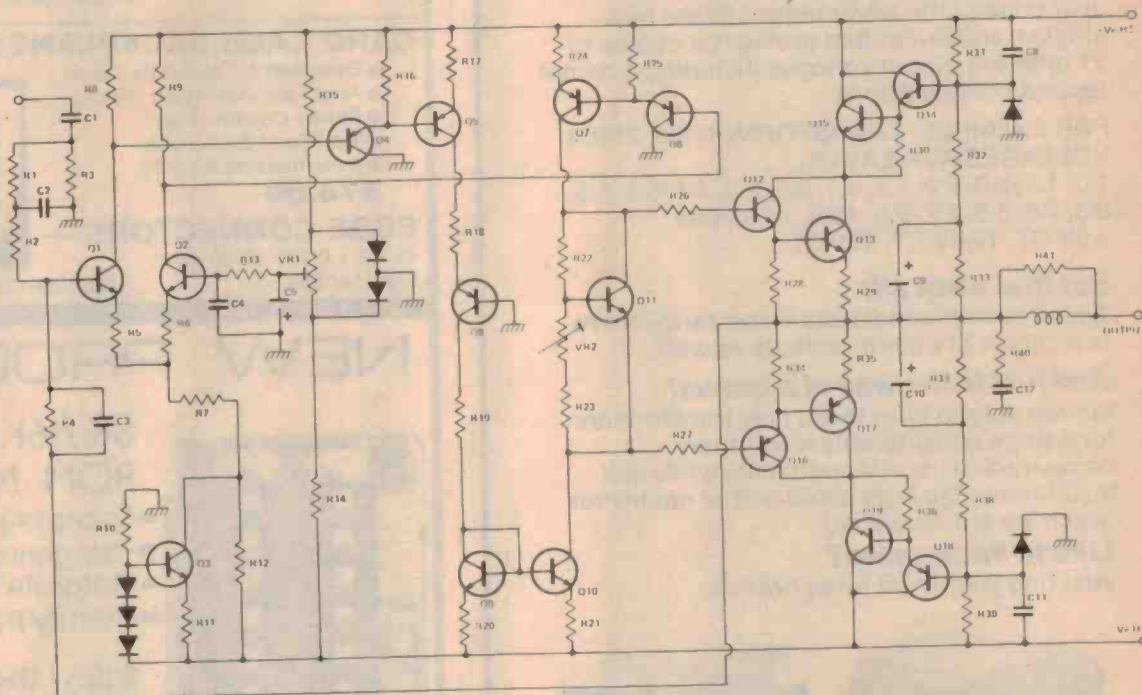
1. Low distortion with a very low order of overall feedback
2. Wide open-loop bandwidth with an excellent slewing rate
3. Minimum time and phase distortion
4. A high transient power capability with virtual freedom from clipping effects.

The output stages have a very high current capability but have no protection circuits, the output transistors being designed to sink the full energy of the power-supply into the load. A patented form of voltage feed to this stage gives the amplifier a short term power delivery capability of about 600 watts (compared to the rated 150 watts 8 ohms). This represents a 6 dB increase in power availability over the rated figure. The voltage amplifying stages are designed to clip softly and this combined with the low-overall feedback gives overload characteristics similar to those of an equivalent valve amplifier.

Conclusion

This feature has discussed just some aspects of modern audio amplifier design. At present much attention is still given to whether an amplifier is designed around bipolar transistors, FETs, valves, or switching transistors. However designers are beginning to appreciate that the major stumbling block is not designing a circuit using any of these technologies but in deciding upon what is the performance specification required *that will give faithful reproduction of the sound source*. Until this problem is solved there will continue to be an element of uncertainty in amplifier design.

The Mission Amplifier referred to in this article is due for release very soon now, and we will be taking a closer and more detailed look at this design — results as soon as possible in ETI.



Full circuit diagram for the Lecson AP3 power amplifier design, producing around 150W.

HOW IT WORKS—Lecson AP3

Transistors Q1 and Q2 form a long-tailed pair differential amplifier with Q3 as the emitter current source. Local feedback is applied in the form of emitter resistors R5 and R6. The base of Q2, instead of being grounded, is connected to a potential divider RV1 which permits the DC offset at the output to be set to zero. The input signal to Q1 is passed through a low-pass filter (R1, C2) which sets the bandwidth to 22 kHz (i.e. below the open loop bandwidth for no TID effects). The bi-phase outputs of the long-tail pair feed a second differential amplifier Q5 and Q7. Transistor Q5 has a constant current load (Q8) whilst the other is terminated by a current mirror (Q9 and Q10). Transistor Q10 will always deliver the same current as transistor Q9 hence the term "Current Mirror" and the excellent symmetry and balance this stage achieves. Functionally, however, Q10 can be considered as an active load whilst Q7 is a voltage amplifier from whose collector the drive to the output stage is taken. Note that Q5 and Q7 both have local emitter feedback (R17, R24) and that both are buffered from the long-tail pair (Q4 and Q6 emitter followers).

Transistors Q12, Q13, Q16 and Q17 each form conventional Darlington emitter follower stages. Each stage is series connected to a further power transistor (Q14, Q15 and Q18, Q19 respectively) which is permanently biased ON. Their emitter potentials are determined by the ratio of the base potential dividers. This ratio was chosen such that Q13 and Q15 each has half the supply rail across them.

The whole amplifier is in the inverting mode with overall shunt feedback through R4 and C3.

This amplifier is quite fast having an open-loop bandwidth of about 27 kHz. The circuit is stable without the usual compensation capacitors within the loop. THD is low being typically (at 100 W into 8 Ohms) 0.004% at 1 kHz and 0.02% at 10 kHz. The HF distortion can be further improved by selection of transistor Q7 for a device with a low collector-base capacitance.

No conventional protection circuits are used as extremely high power transistors are fitted and these can survive a short-circuit condition in the time taken for the power supply to shut down.

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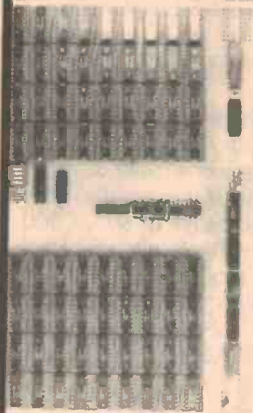
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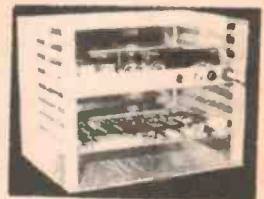
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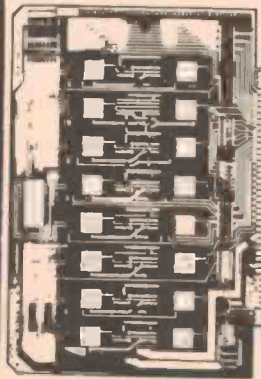
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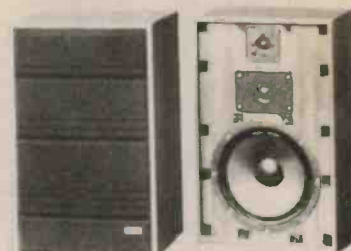
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74C193.....2.25	

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301.....40	
307.....65	
308.....1.35	
311.....85	
324.....1.35	
339.....90	
349.....2.25	
356.....1.65	
380.....2.00	
381.....2.00	
382.....2.00	
386.....1.95	
555.....35	
556.....85	
565.....1.95	
566.....2.50	
567.....2.65	
709.....75	
723(VR).....55	
741.....35	
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309.....2.25	
317.....3.50	
323.....8.25	
325.....2.60	
723.....55	
7805.....1.30	
7806.....1.30	
7808.....1.30	
7812.....1.30	
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DISPLAYS— the state of the art

Dramatic developments are currently underway in both analogue and digital displays — ETI's special correspondent Associate Professor Peter Sydenham describes the present state of the art.

DURING the past few years digital displays have often been specified for applications where their analogue equivalents would have been more suitable. Now though, common sense is beginning to prevail. Analogue displays are gradually regaining ground as it becomes clear that they are more suitable for trend and other dynamic observations. Nevertheless many of today's analogue displays use digital techniques internally.

Rotating pointers, bar-graphs and similar analogue visual effects are now being developed for use in the automotive industry. Large-scale production prototype systems are already undergoing trials in cars. From this area of development it is logical to expect these new forms of analogue display to find their way into other applications. Now that most of the development has been completed the costs should be low. The consequence is that they will be introduced very rapidly into general use.

CHOICE OF DISPLAY

Choosing a display can be quite a task because many options exist.

Factors of key importance relate to the appearance of the display as seen by the user, reliability, ease of servicing, and power consumption.

Of particular importance is the 'price to use'. This can greatly exceed the cost price because of the costs of power supply, mounting, wiring, and possible connectors. It is also important that at least two sources of supply are available.

Another factor to consider is the special characteristics of a display. Each has some good and some bad characteristics. For example a liquid crystal display is fine where ambient light exists but needs auxiliary illumination in low light conditions. LED's on the other hand are best seen in the dark — they need to be very bright to be seen in full sunlight.

It is also important to assess if the device is really fully developed. Many

new products reach the marketplace before they have been fully tested. Today a new solid-state product can be realised and marketed in a matter of a year but it is not possible to test it for the whole of that time. The tens of thousands of hours life that may be postulated by the manufacturer is often merely conjecture. Liquid crystal displays were one example. No user wants to be part of a test programme . . . especially if he's paying for the privilege. New is not necessarily best!

The main display contenders are currently LED's, gas discharge tubes, cathode ray tubes, liquid crystals, and the fast-emerging electroluminescent panels.

The time-honoured filament lamps continue and need no further comment except to say that they are being replaced in small power displays by the more up-to-date devices.

LEDS

LED's emerged first as single element light sources of rather low brightness and in red only. Today they are available in brighter forms and of many different optical styles providing diffusing effects, wider angles of viewing and generally greater utility. Present day technology can provide 50 um square elements of which 300-600 may be integrated into a matrix. Such LEDs are available with light output sufficient for aircraft instrumentation

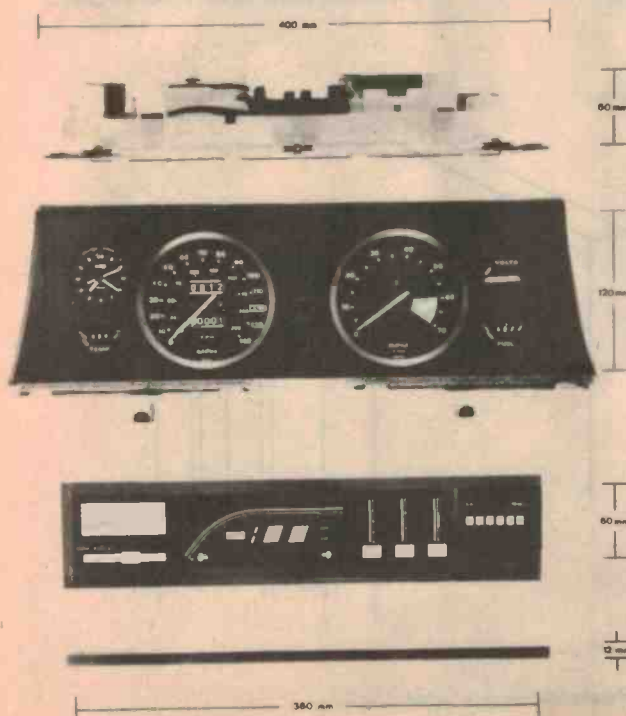


Fig. 1 (left). The conventional mechanical instrument panel (upper) contains 430 parts and is much bigger than the 35-part electroluminescent solid-state display (lower).

Fig. 2. Comparison of the display technologies now in vogue.

		Optimum Number of Bits
Tungsten Filaments		1 - 20
Light Emitting Diodes	LED	1 - 30
Cathode Ray Tubes	CRT	10K - 250K
Gas Discharge (Plasma Panels)		30 - 5K
AC or DC Electroluminescence	DCEL	30 - 3K
Liquid Crystal Display	LCD	5 - 200
Electrochromic (liquid or solid)		5 - 200
Electrophoretic		5 - 200
Vacuum Fluorescent	VAC.FL.	10 - 100

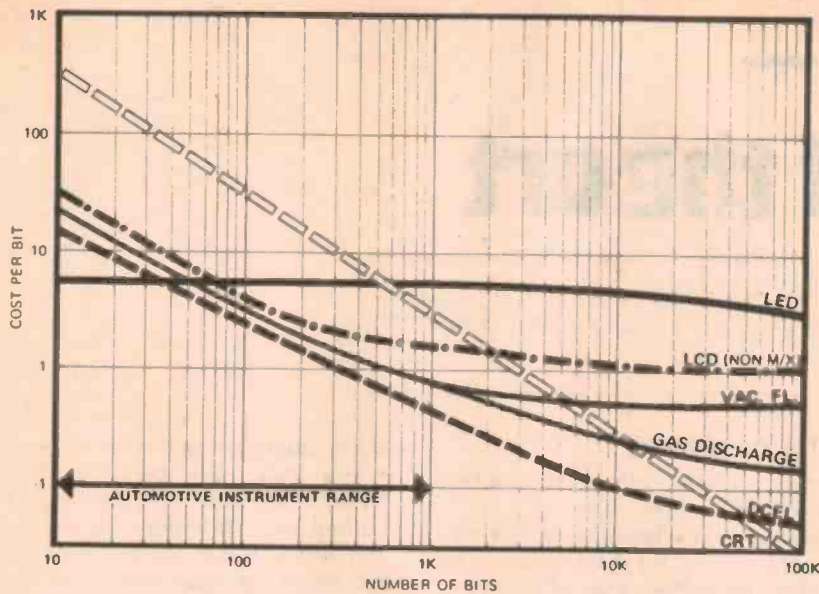


Fig. 3. Comparison of the cost per bit of the various display options.

(10^5 Lux) and can be made to full MIL specifications including operation over a temperature range of -55°C to 125°C .

They are available in colours ranging from red (the most common and cheapest) through yellow, green, orange and violet. Blue LEDs have been made but appear to lack a large enough market to enable them to be produced at a commercially attractive price.

The reliability of LED's is variously claimed to be from 10^4 to 10^9 hours. There is a suggestion (based on evidence from large-scale users) that price wars have tempted makers to reduce reliability. Reject rates as high as 20% are said to be experienced by some buyers.

LED's are fast operating: typical rise times are 10 - 50 ns. They are offered in pcb packages, in larger metal packages suitable for sealing and in more-expensive-still ceramic packages.

The ready ease with which they can be assembled into lines, circles, matrices and other graphical forms enables them to be used in analogue displays.

LED's are not necessarily the best choice for all displays. Figure 2 compares various displays on the basis of the optimum number of bits for each alternative. It can be seen that LEDs are restricted to applications where the type of display requires only a small number of bits. Electroluminescent panels (discussed below) are more suitable where the application calls for the use of many bits.

Another factor is the cost per bit to manufacture. Figure 3 compares this variable for the various types of displays. The LED does not compare well for applications requiring over 100 bits. On this basis the CRT is way ahead. As yet

it is not even remotely matched by any solid-state technique. The CRT's main drawback is that it is bulky and fragile compared with most other types of display.

GAS DISCHARGE TUBES

Gas discharge tubes were the first displays that could reasonably be regarded as versatile. Many older readers will recollect the Dekatron counter tubes of the 1950's in which 'dots' moved circumferentially in a scale of ten. A later development incorporated grids placed behind one another in a single glass envelope in what was generally called the Nixie tube. Their main dis-

advantage for use with solid-state circuits was their need for a 170 volt supply.

With the introduction of solid-state displays it might be thought that gas discharge tubes would have been supplanted. This has not happened so far. Indeed indications are that they will be used for a considerable time yet. Their brightness and large size are still strong advantages.

Gas discharge tubes are made in many forms. These include low profile, alpha-numeric, bar-graph, special purpose graphical displays, and still in the research and development stage, are phase addressed matrix co-planar units which use thick film manufacturing techniques.

It is possible to construct gas-discharge cells so that a particular cell is set to strike and erase at different discrete voltage levels. Thus, increasing the voltage level to a line of adjacent cells will produce a bar-graph effect. Once struck, the cells latch on exhibiting a bistable storage characteristic.

Cross-bar arrangements of grids (as shown in Fig 4) enable 'dot' discharges to be established at the junction of any two selected bars. Thick-film replication methods are used to manufacture the units.

The colour of discharge tubes can be finely tuned to just about any wavelength. This is done by adding an appropriate phosphor to the cell during manufacture. White and blue remain difficult to produce.

A phase-addressed technique has been developed to reduce the number of leads otherwise needed to connect all matrix positions to external circuits.

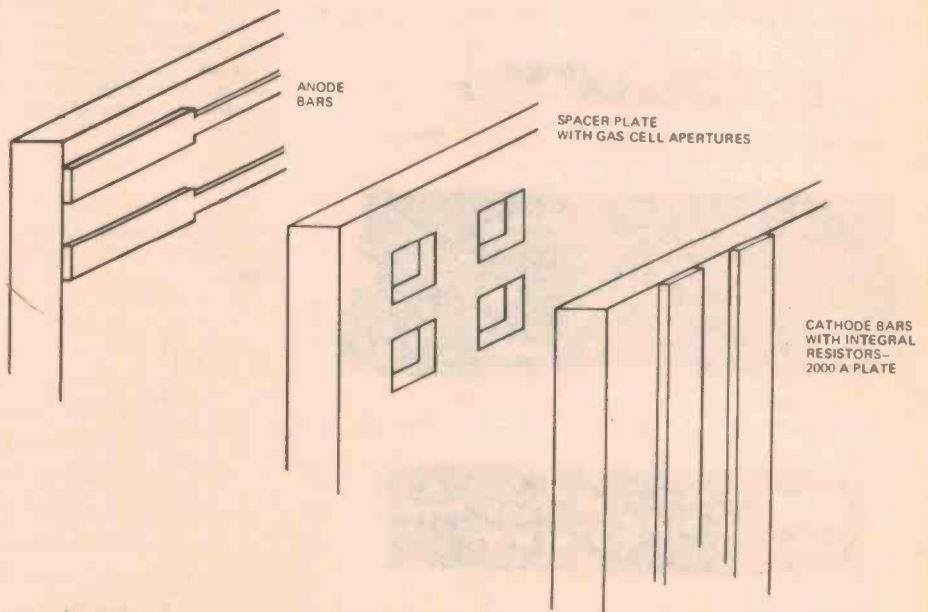


Fig. 4. Construction of dot-matrix gas-discharge display unit.

Gas discharge tubes are still, and will remain, a strong contender in the choice of a display. Figure 2 illustrates this well.

CATHODE RAY TUBES

A CRT screen of good quality and having a good linear scanning system can accommodate a display of 1000 by 1000 elements. The full range of colours is available as well as an intensity scale having perhaps 200 levels. Cost per element is very low but size and fragility go against the CRT in many applications. Eventually, as matrix manufacturing methods become more developed, the CRT's thin flat digital equivalent will become a serious rival. At present (1978) though the CRT has no rivals for displays requiring large numbers of bits.

LIQUID CRYSTAL DISPLAYS

In many ways LCD's got off to a start less worthy than they deserved. Reliability was variable: many failed rapidly whilst others did very well. Failure of an individual display within a batch could vary from almost immediate through to years.

The second generation of LCD's has shown itself to be very much better if made by more controlled procedures and with better materials. Figures such as 90 000 hours to reach a 2% cumulative failure have been claimed for twisted-nematic LCD displays.

A key factor has been the realisation that a non-zero dc cell level rapidly degraded the cell. That restriction was originally controlled by the use of ac bias but now zero level dc working has been devised.

Initial commercial incentive came from watch manufacturers, but now researchers are seeking ways of building much larger panels — 150 mm square for example. Such large sizes pose manufacturing problems for the glass enclosing the LCD material must be flat to within a mere 10 μ m.

Manufacturing methods are constantly being improved. The glass front

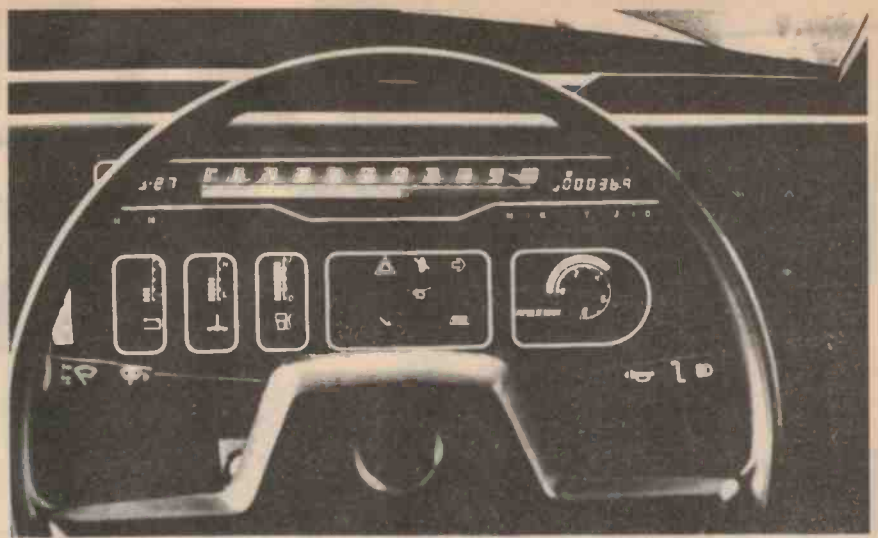


Fig. 6. On-vehicle electroluminescent display dash panel (Smiths Industries).

seal has been greatly changed . . . that was a cause of many premature failures. Purer LCD material and improved stability with temperature and humidity have also improved.

Matrix units are being investigated but, as with all such units, connecting problems remain. Some LCD's currently being released have shift registers integrated onto the display. This trend may become common practice, for the user does not wish to connect any more than the minimum of leads from the drive circuits to the display.

In general LCD manufacturers suggest that their products are best suited for applications requiring a portable display. The current LCD's are certainly much better than the first generation and their low power consumption gives them a firm place in the display range.

ELECTROLUMINESCENT DISPLAY PANELS

Electroluminescent devices are basically just a layer of special paint between two pieces of glass.

Two basic groups exist . . . ac working (called acel) and dc working (called dcel). Each uses zinc sulphide, manganese-doped phosphors which radiate a yellow-orange light at 585 nm wavelength. The ac cells operate in a capacitive mode, the dc units in a resistive mode. Figure 5 shows the schematic of a dcel unit.

Manufacturing processes are mainly vacuum deposition using photolithographic procedures for masking. This method offers great prospects for the future. The British Post Office for example is considering 1250 character displays for phone call costing. Smiths Industries have vehicle instrument panels in pilot scale production. (Figure 6 shows a recent panel of this type).

As always, addressing the display is a problem. Multiplexing methods have been used to reduce lead counts from 257 (for a 256 unit) down to only 32. The displays can be used in a continuous mode or they can be pulsed. Pulse durations of around 0.5% duty cycle are typical using 5 — 15 micro-second pulses.

Around 120 volts is needed to drive the display present day units require 50 mW per character. A prototype unit using CMOS circuitry consumes only two watts for a 480 character display.

This information was compiled from lectures delivered at an Institution of Electrical Engineers day meeting held in London in January 1978. No full Proceedings were published but the five speakers would be able to provide further information if contacted. Details can be obtained from the Conference Secretary, IEE, Savoy Place, London. Smiths Industries kindly provided most of the illustrations used here.

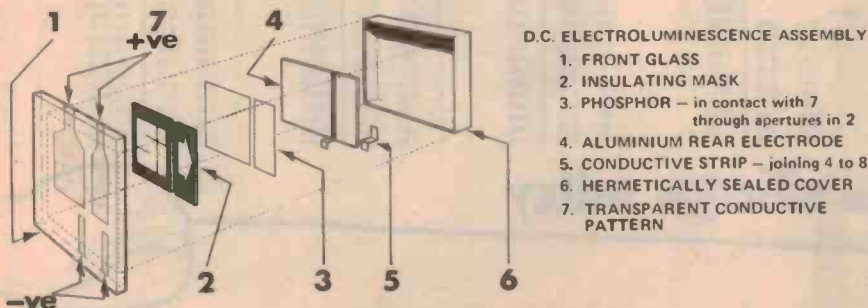


Fig. 5. Schematic of a dcel electroluminescent display panel.

STOP PRESS

- 741 — OP AMPS
- 555 — TIMERS
- 4001 — CMOS
- 4011 — CMOS
- 1N914 — DIODES
- 7805P — REGULATORS
- C106Y1 — SCRS
- LM382 — PREAMP

- 5 for 1.50
- 5 for 1.50
- 5 for 1.00
- 5 for 1.00
- 20 for 1.00
- 2 for 2.00
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MDA3502	1	3.04	0.69
MDA3504	1	3.46	0.67

DIODES			
Type	Qty	Price	* Tax
1N218	1	0.00	0.68
1N238	1	3.00	0.58
1N914	15	1.20	0.24
1N4001	15	1.00	0.20
1N4004	18	2.00	0.24
1N4007	5	1.20	0.24
1N4148	15	1.20	0.24
1N5401	2	0.80	0.16
A140	3	0.84	0.17
MR754	1	1.00	0.20

ZENER DIODES			
Type	Qty	Price	* Tax
5Watt 3.3V	4	0.92	0.18
8Watt 5%	1	1.00	0.20

Voltage			
Watt	5 Watt	5 Watt	
3.3	1N745A	1N5333B	
3.6	1N747A	1N5333B	
3.9	1N748A	1N5338B	
4.3	1N749A	1N5338B	
4.7	1N750A	1N5337B	
5.1	1N751A	1N5338B	
5.6	1N752A	1N5338B	
6.2	1N753A	1N5341B	
6.7	1N754A	1N5342B	
7.2	1N755A	1N5344B	
7.8	1N756A	1N5348B	
8.4	1N757A	1N5348B	
9.1	1N758A	1N5347B	
10	1N5348B	1N5348B	
12	1N759A	1N5349B	
13	1N9648	1N5350B	
15	1N9658	1N5352B	
16	1N9668	1N5353B	
18	1N9678	1N5355B	
20	1N9688	1N5357B	
22	1N9698	1N5358B	
24	1N9708	1N5359B	
27	1N9718	1N5361B	
30	1N9728	1N5363B	
33	1N9738	1N5365B	
36	BZX	1N5365B	
39	BZX	1N5366B	
43	BZX	1N5367B	
47	BZX	1N5368B	
51	BZX	1N5369B	
56	BZX	1N5370B	
62	BZX	1N5372B	
68	BZX	1N5373B	

Type			
Type	Qty	Price	* Tax
2N2222A	2	0.80	0.16
2N2646	1	0.82	0.16
2N2907A	2	1.10	0.22
2N3053	2	1.10	0.22
2N3054	1	0.75	0.15
2N3055	1	0.99	0.20
2N3442	1	1.40	0.28
2N3644	3	1.05	0.21

TRANSISTORS			
Type	Qty	Price	* Tax
2N3789	1	2.20	0.43
2N3856	1	1.09	0.21
2N4121	3	0.80	0.16
2N4220A	2	0.90	0.18
2N4236	1	1.73	0.34
2N4250	3	0.80	0.18
MP54258	2	0.96	0.19
2N4351	1	2.85	0.55
2N4352	1	2.70	0.52
2N4360	2	1.08	0.21
2N4427	1	1.24	0.24
2N44870	1	0.79	0.16
2N44871	1	0.75	0.15
2N5191	1	0.98	0.19
2N5194	1	1.00	0.21
2N5458	2	0.80	0.18
2N5459	2	1.00	0.20
2N5461	2	1.34	0.26
2N5484	2	1.00	0.20
2N5485	2	1.02	0.20
2N5486	2	1.00	0.20
2N6027	2	0.88	0.17
2N6425	1	1.80	0.35
2N6958	1	1.55	0.30
3N	1	1.45	0.28
JN210	1	1.45	0.28
AC126	1	0.75	0.15
AC128	1	0.75	0.15
AD149	1	1.34	0.26
AD161	1	1.44	0.28
AD182	1	1.50	0.29
AF126	1	0.75	0.15
AF127	1	0.75	0.15
BC107	3	1.05	0.21
BC108	3	1.05	0.21

BC109	3	1.05	0.21
BC177	3	1.05	0.21
BC178	3	1.05	0.21
BC179	3	1.08	0.21
BC237	3	0.90	0.18
BC238	3	0.90	0.18
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BC282	3	0.90	0.18
BC283	3	0.90	0.18
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BC296	3	0.90	0.18
BC297	3	0.90	0.18
BC298	3	0.90	0.18
BC299	3	0.90	0.18
BC300	3	0.90	0.18

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7807P	1	1.20	0.13
7808P	1	1.20	0.13
7809P	1	1.20	0.13
7810P	1	1.20	0.13
7811P	1	1.20	0.13
7812P	1	1.20	0.13
7813P	1	1.20	0.13
7814P	1	1.20	0.13
7815P	1	1.20	0.13
7816P	1	1.20	0.13
7817P	1	1.20	0.13
7818P	1	1.20	0.13
7819P	1	1.20	0.13
7820P	1	1.20	0.13
7821P	1	1.20	0.13
7822P	1	1.20	0.13
7823P	1	1.20	0.13
7824P	1	1.20	0.13
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7827P	1	1.20	0.13
7828P	1	1.20	0.13
7829P	1	1.20	0.13
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7831P	1	1.20	0.13
7832P	1	1.20	0.13
7833P	1	1.20	0.13
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7843P	1	1.20	0.13
7844P	1	1.20	0.13
7845P	1	1.20	0.13
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7860P	1	1.20	0.13
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7863P	1	1.20	0.13
7864P	1	1.20	0.13
7865P	1	1.20	0.13
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74LS240	1	2.10	0.22	74LS323	1	2.20	0.23	74LS395	1	2.20	0.23
74LS241	1	2.10	0.22	74LS324	1	1.46	0.18	74LS396	1	1.92	0.20
74LS242	1	2.89	0.29	74LS325	1	4.15	0.47	74LS398	1	3.80	0.41
74LS243	1	2.89	0.29	74LS326	1	4.18	0.47	74LS399	1	2.85	0.30
74LS244	1	2.69	0.29	74LS327	1	4.18	0.47	74LS424	1	7.20	0.76
74LS245	1	2.20	0.23	74LS348	1	2.20	0.23	74LS445	1	2.25	0.24
74LS247	1	2.20	0.23	74LS352	1	2.50	0.27	74LS447	1	1.65	0.18
74LS248	1	2.20	0.23	74LS353	1	2.50	0.27	74LS490	1	3.35	0.35
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74LS251	1	1.80	0.16	74LS363	1	2.50	0.27	74LS669	1	1.25	0.13
74LS252	1	1.80	0.16	74LS365	1	1.04	0.11				
74LS257	1	1.80	0.16	74LS366	1	1.04	0.11				
74LS258	1	1.80	0.16	74LS367	1	1.04	0.11				
74LS259	1	1.80	0.16	74LS368	1	1.04	0.11				
74LS261	1	3.84	0.37	74LS373	1	2.50	0.27				
74LS266	1	0.75	0.08	74LS374	1	2.50	0.27				
74LS276	1	0.20	0.05	74LS375	1	0.80	0.10				
74LS275	1	1.25	0.13	74LS377	1	3.12	0.33				
74LS279	1	1.25	0.13	74LS378	1	1.55	0.18				
74LS280	1	2.85	0.30								

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CA-18S-WW	1	0.90	0.10
CA-22S-WW	1	1.20	0.13
CA-24S-WW	1	1.30	0.14
CA-28S-WW	1	1.82	0.19
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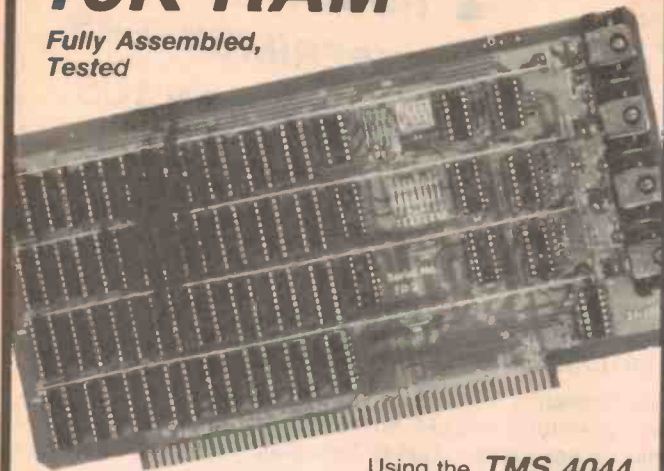
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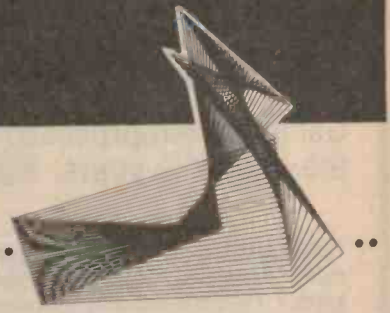
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ETI's COMPUTER SECTION



MEMO

Appledisk

Now available from Computerland, 55 Clarence Street, Sydney, is the Disk II floppy disk subsystem for the Apple II personal computer. The Disk II comprises a Shugart minifloppy in a heavy duty steel case with an intelligent interface card which plugs into the Apple II, and offers 116 Kbytes of soft-sectored storage. The Disk II Operating System supports both ROM Applesoft and Apple Integer BASIC, and has a comprehensive selection of commands. Computerland say they had samples of the disk within one week of its release in the States, so Australia is obviously catching up with the US in personal computing technology.

Amongst other new products from Computerland is a new multi-user multi-tasking disk operating system which is claimed to be machine independent and compatible with hard disks. According to Rudi Hoess of Computerland, the system also offers ISAM multi-keying file support and communications in the IBM 2780 mode. Incidentally, Computerland, which started in the States, celebrates its 2nd birthday shortly with a giant party stretching right across the US and Pacific from Boston to Sydney. 50,000 guests are expected to attend at the many Computerland stores.

Print Out Cutback

Our S100 Printer Project this month 'just grew and grew' until it reached the stage where it wouldn't fit in the space we'd allowed for it. Rather than chop it into two parts, we've had to cut back the Print Out section this month — but the magazine still contains the same amount of computer articles, so don't feel too cheated!

TACS

TACS is an acronym for Tasmanian Amateur Computer Society, which is now up and running in Hobart. The

Secretary, Clive Myers, dropped us a line to tell us TACS meets regularly, on the first and third Tuesdays of the month, in the Computer Studies Area of the Rosny Matriculation College, at 7.30 p.m. So drop in and swell the numbers of the TACS-men (?), or if you want, phone Clive on 65 2252 after 6.30 p.m.

16K RAM Card

Pennywise Peripherals' new 16K x 8 bit static RAM card is designed for those who are after a quality compact memory system which uses the latest technology.

The PCB is 247.5 x 152.5 mm and has plated through holes with a solder resistant coating. The edge connector is for the Motorola Exorcisor bus (43 way x 2 double sided 0.156" pitch) as used by the popular MEK6800D2 KIT. However, the read/write control logic is jumper selectable for a variety of schemes other than the M6800, such as 8080/85, 2650, SC/MP.

The 2114 1K x 4 bit static RAM used is an industry standard and probably the most popular latest generation 4K static RAM. It is produced by a variety of manufacturers including Intel, Texas Instruments,

Motorola, Synertek and Signetics. It requires only a single +5 volt supply.

The 16K bytes on the memory card are divided into two 8K blocks each of which is switch selectable to any 8K area within 64K. All bus signals are buffered with low powered schottky TTL and the bi-directional data bus is driven by tri-state buffers. Further information from *Pennywise Peripherals, 19 Suemar Street, Mulgrave, Vic, 3168.*

IREE Microprocessor Group

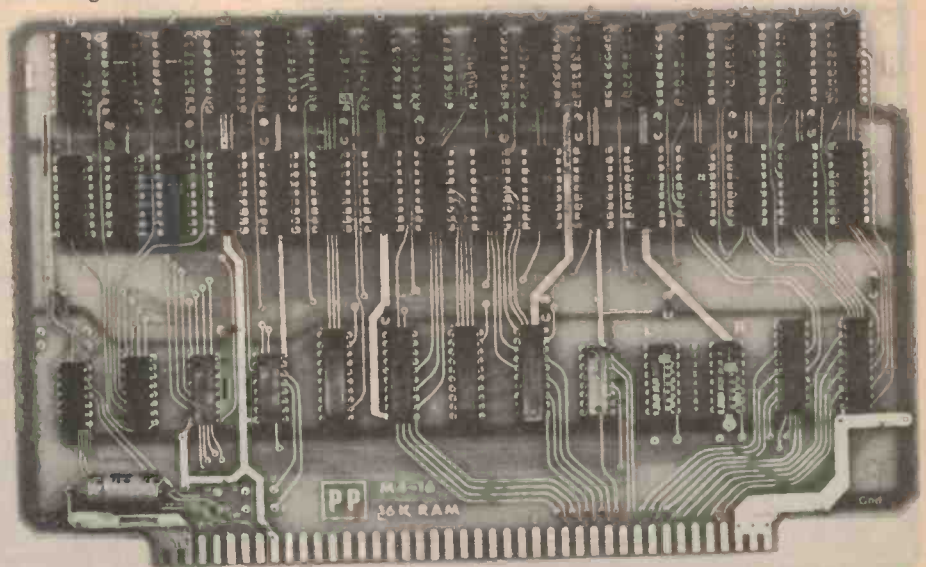
At a recent well attended meeting, over 130 people formed the I.R.E.E. Sydney Microprocessor Group.

The aim of the Group is to foster greater knowledge of microprocessors and to improve the link between the programming and hardware fields.

Non members of the I.R.E.E. will be welcome to become members of this new Group.

Further information can be obtained from: *The Hon. Secretary, Dr. Barry Madden, School of Chemical Technology, University of New South Wales, P.O. Box 1, KENSINGTON, NSW, 2033.*

The other office bearers are S. Wolkowicz (Chairman) and D. Skellern (Treasurer).



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- a 2650 microprocessor
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A. 2650 Computer Board System Assembled	\$356.40
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KITS

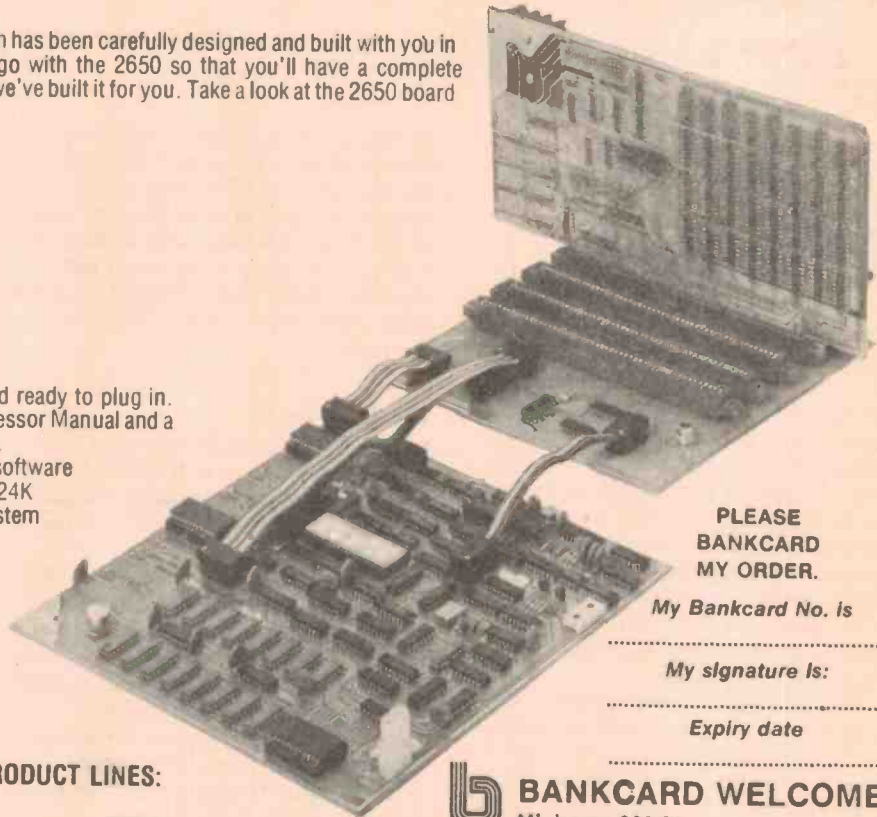
A. 2650 Computer Board System	248.00
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A. Editor/Assembler	30.00
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Shop 499, High Street, Northcote. Vic. 3070. Ph (03) 489-8131. Open Mon-Thurs 8 am — 5.30 pm, Fri 8 am — 7 pm. Sat 9 am — 1 pm. Mail Orders: PO Box 135, Northcote. Vic. 3070.
Send SAE for free condensed catalogue.

S100 PRINTER

Our most ambitious project yet for the computer hobbyist — low cost hard copy!

WHILE THE COST of the large-scale integrated electronics built into computers has dropped, that of the mechanical peripheral devices has not followed this trend. Most printers cost several hundreds, if not thousands, of dollars, so when Philips showed us a new mechanism which costs around \$70 we were more than interested.

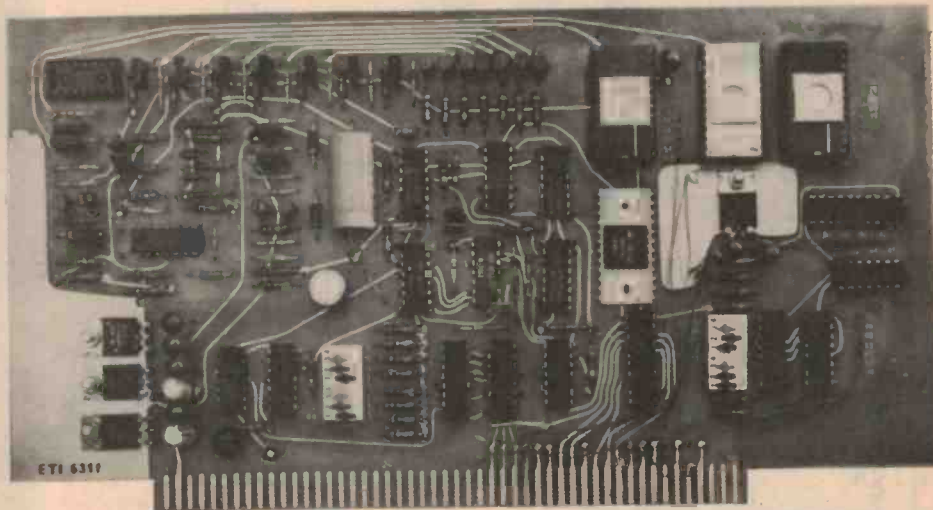
You rarely get something for nothing and this printer is no exception — it cannot do everything more sophisticated types can. It uses a 60 mm wide paper which allows 32 characters per line, and the paper is a special metallized type. However it is still a very useful printer, especially for the hobbyist who doesn't have a grand to spare.

Design Features

As we seem to have standardised on the S100 bus this was the obvious choice for mechanical construction and electrical interfacing. Philips do offer an interface for the printer; however it requires the computer to be dedicated to it during the print cycle. The computer has to present and hold each character in sequence as requested by the printer. This involves a fairly lengthy program (124 steps for the MEK6800D2) as well as tying up the processor.

We therefore chose a different approach using a dedicated memory on the interface to store the characters which can be entered at any speed (up to approximately 5 μ s apart) until either 128 characters (the limit of the memory) or a carriage return has been transmitted. At this point the print cycle starts and no further action is required from the processor. We initially tested the unit using only a keyboard, entering data manually with the carriage return initiating printing.

Text continued on page 96.



SPECIFICATION — ETI 641

Print format	7 x 5 dot matrix
Number of different characters	127
Number of characters per line	32
Printing speed	2 lines per second
Character height	2.4 mm
Interface format	S100 bus compatible
Data entry time	5 μ s per character
Character storage capability	128
Power supply	+16 V @ 100mA
motor stopped	+8 V @ 350mA
	-16 V @ 80mA
motor running	+16 V @ 200mA
	+8 V @ 350mA
	-16 V @ 180mA
Printer mechanism	EUY-10E023LE (Philips)
Paper	EUY-SUB006

Project 641

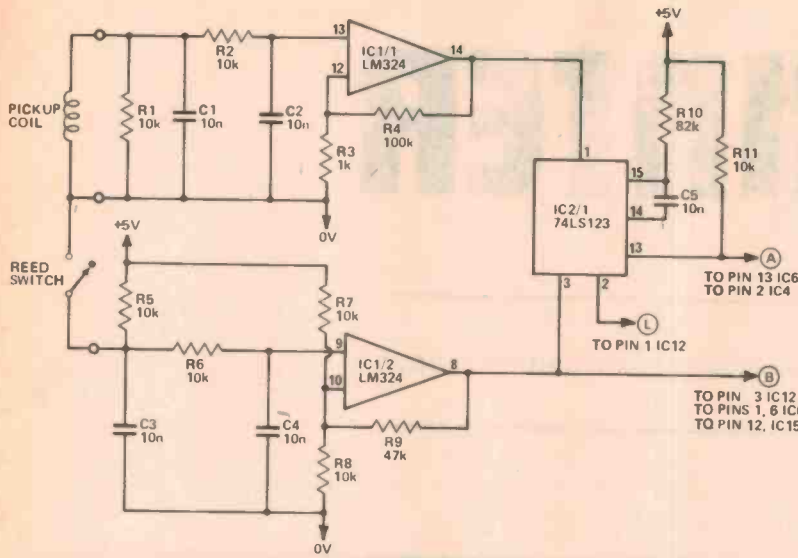


Fig. 1a. The circuit diagram of the pickup coil and reed switch buffer.

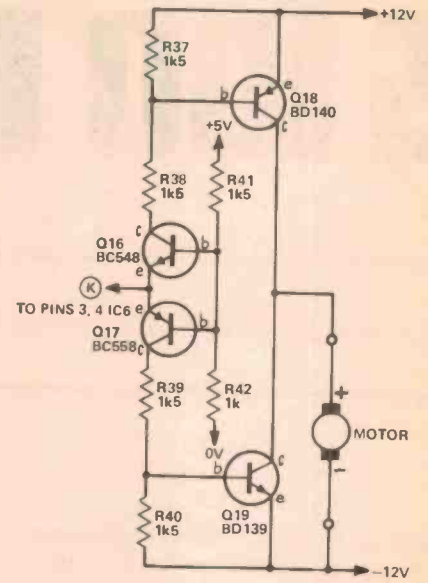


Fig. 1d. The motor drive interface.

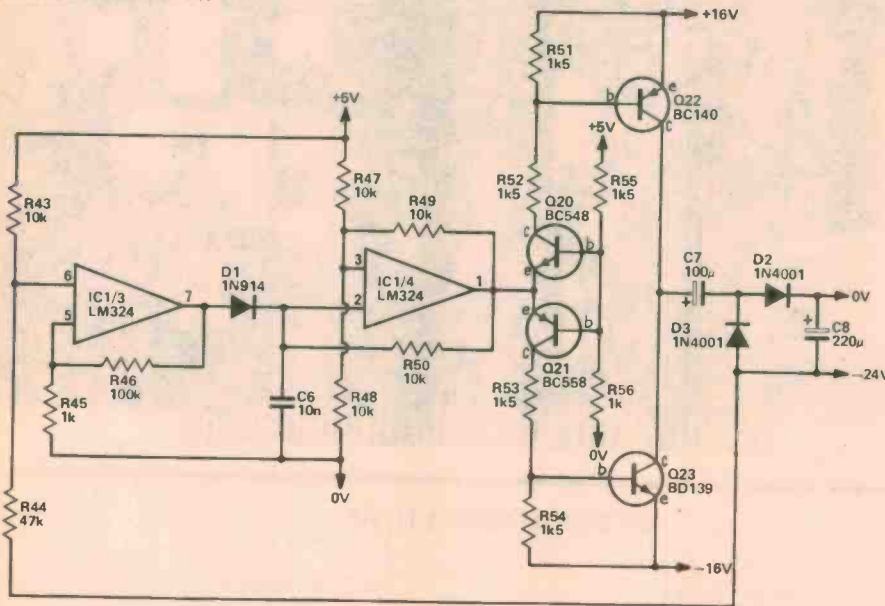


Fig. 1b. The -24 volt power supply.

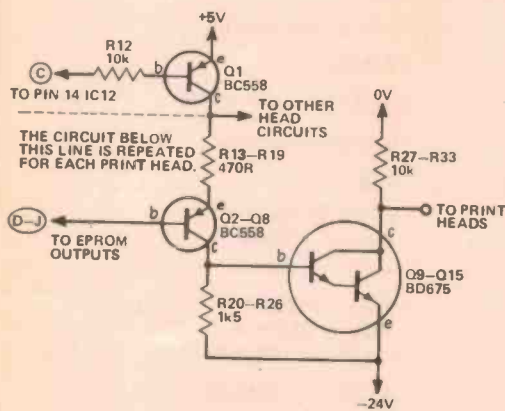


Fig. 1c. The circuit of the head drive. Although only one channel is shown there are 7 identical circuits.

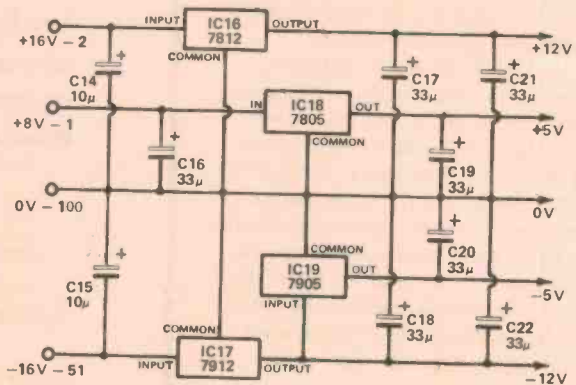


Fig. 1e. The main power supply.

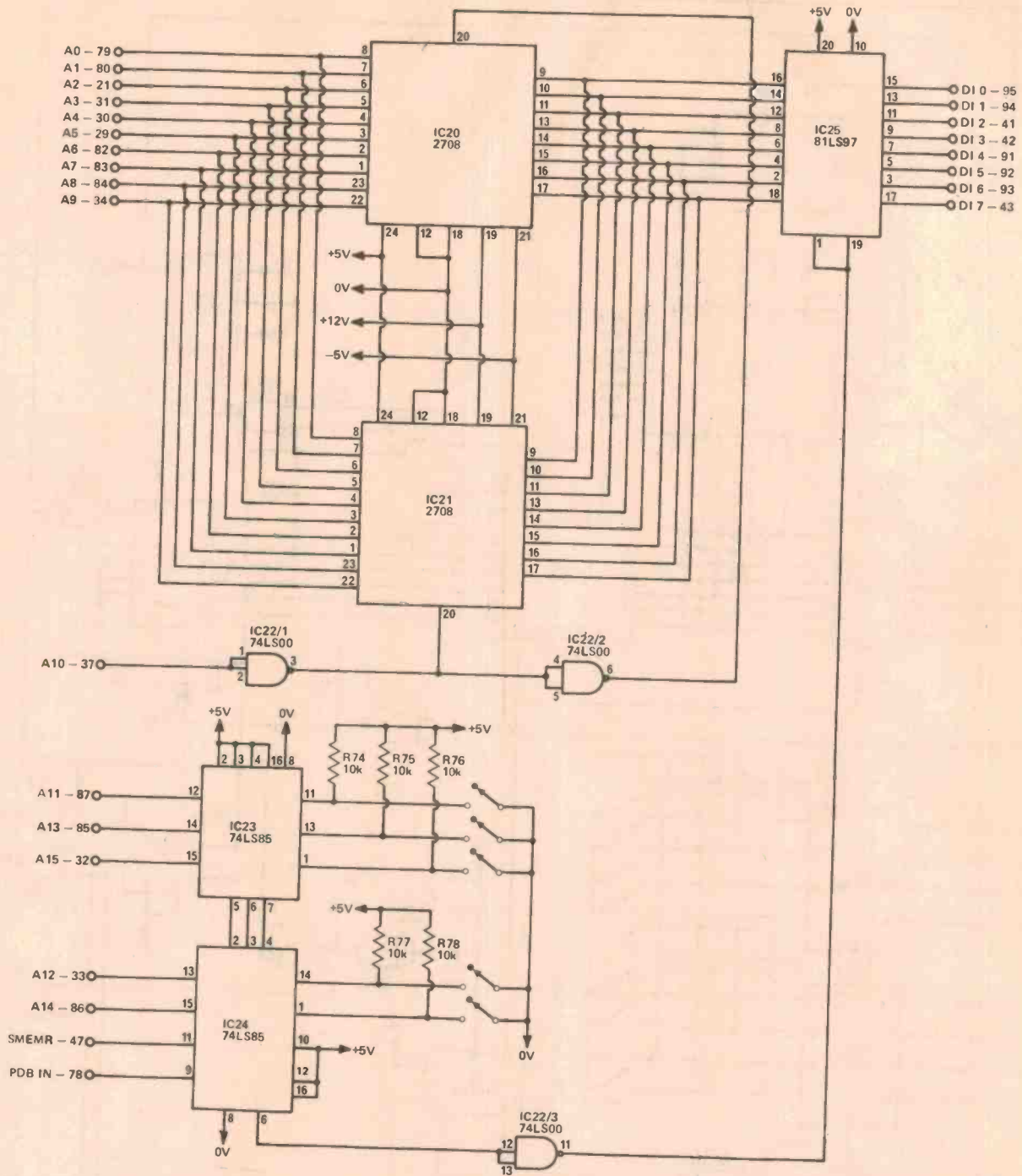


Fig. 1g. The circuit of the auxiliary memory which can be used to store some of your software.

Pre-programmed EPROMs containing the standard character set listed in this article are available from Romtech Pty Ltd, P.O. Box 446, Campbelltown 2560 for \$15.00 including sales tax + \$2.00 for postage and packing.

The printed circuit board patterns for this project were too large to fit in the magazine, so, as for the ETI 640 VDU, they will be available from us on receipt of a large stamped self-addressed envelope. The address to write to is Printer PCBs, Electronics Today, 15 Boundary Street, Rushcutters Bay, NSW 2011.

HOW IT WORKS — ETI 641

Before starting an explanation of the electronics we will give a description of the printer used. It has a 24 Vdc motor which drives both the paper feed and the head drive. The head is simply a set of seven fine contacts arranged in a vertical line and is moved across the paper from left to right. The 'paper' is metallized with a thin coating of aluminium, and by applying a voltage pulse between one of the head contacts and the paper the metallization is burnt off at that point. By applying pulses to each of the seven heads in the correct sequence as the head moves across the paper characters and words can be formed in a 5 x 7 dot matrix. The pulse required is -24 V for 240 - 480 μ s with a peak current of around 3 A per head.

At the end of the left to right scan of the head it returns quickly to the left while advancing the paper feed. The head is lifted off the paper on the return pass.

Also in the printer mechanism is a toothed wheel and pickup coil which gives an ac output of about 1 V which is used to synchronise the printing, and a reed switch which closes on the left to right passage of the print head. This is used to indicate the start of the line when printing.

The Electronics

The circuit is designed to operate on the S100 bus, and a proportion of the electronics forms an interface to the bus. The principle of operation of the unit is to present the data representing the first character to an I/O port along with the S100 timing signals to tell the printer circuitry to accept the character, and then repeat this process for up to 128 characters. No characters are printed until 128 characters have been output to the printer or until it recognises a carriage return. Printing starts immediately either of these events occurs and during printing a busy signal is available on the I/O port as no data can be entered while printing is in progress.

The S100 bus has available +8 V and ± 16 V unregulated dc supplies, and from these we derive, using three-terminal regulators, both positive and negative 5 V and 12 V supplies. Also required for the printer is -24 V, and we derive this from the ± 16 V supply using a diode pump type circuit. This consists of IC1/4 which is connected as a square wave oscillator running at 400 Hz. Its output drives the transistor buffer stage Q22 - Q25 the output of which is a square wave of 32 V p-p. The capacitors C7 and C8, and the diodes D2 and D3 rectify this to give a

negative voltage which if not limited would reach -30 V. However IC1/3 acts as a comparator and when the voltage on pin 6 drops below 0 V, which represents a voltage of -23.5 V, its output will go high, disabling IC1/4. This effectively regulates the -24 V supply.

Before we can print any data we must first store it. The data is presented to IC7 on the Data Out lines, then if the address presented to IC9 and IC10 is correct along with pin 10 (IC2) being high and a high pulse on pin 3 (IC14), the monostable IC2/2 is triggered. This produces a 500 ns wide pulse which enables the three-state buffer IC7, allowing the data to be written into the RAM IC8. At the end of this pulse, a second monostable (IC11/3) is triggered (about 5 μ s) and during this time the contents of the EPROM are examined. If the character just written into the RAM is not a carriage return, pin 9 of that IC (IC9) will remain high. At the end of this 5 μ s period, the address counter IC13 is incremented. The next character can now be entered.

If a carriage return is entered pin 9 of IC5 will go low during this 5 μ s wide pulse. This forces pin 10 of IC11 high resetting the address counter IC13 and clocking the flipflop IC12/2. If a carriage return is not detected but the 128th character has been entered pin 13 of IC13 will go low and this, via C9, will cause a positive pulse on the output of IC11/1 as well as causing the flipflop IC12/2 to be toggled.

Toggling this flipflop the first time causes pin 15 to go high and 14 low. This disables the monostable via IC14/2, and starts the motor. This is controlled by Q16 - Q19; if point K is low Q16 and Q18 will turn on hard applying 24 V to the motor. When point K goes high, Q17 and Q19 will turn on, shorting out the motor and stopping it quickly.

Also reset by the carriage return is IC12/1, and a '0' will be applied to pins 1 and 2 of IC3 which holds IC4 reset. Once the motor starts, pulses are generated by the pickup coil. The output of the coil is filtered by R1,2 and C1,2 to remove any high frequency interference and is then buffered by IC1/1 which is connected as a schmitt trigger. The output of IC1/1 is used to clock the monostable IC2/1 which generates the 350 μ s wide pulse used for printing.

The reed switch is also filtered by R5,6 and C3,4 to remove contact bounce and noise, before being buffered by IC1/2 which is also connected as a schmitt

trigger. The output of this IC is high from the start of the printing line until the start of the head return.

Once the print stroke has commenced the closing of the reed switch toggles the flipflop IC12/1, allowing IC4 to be clocked. IC4 then scans the 3 least significant address lines of IC5; on each successive clock pulse the EPROM is interrogated for 350 μ s. The outputs from the EPROM are used to drive the print head circuitry.

After seven clock pulses IC3/2 detects this and resets IC4 back to zero so forming a divide by seven circuit. This pulse also clocks the RAM address counter IC13 to the next step. In this way, the RAM tells the EPROM what character it wants.

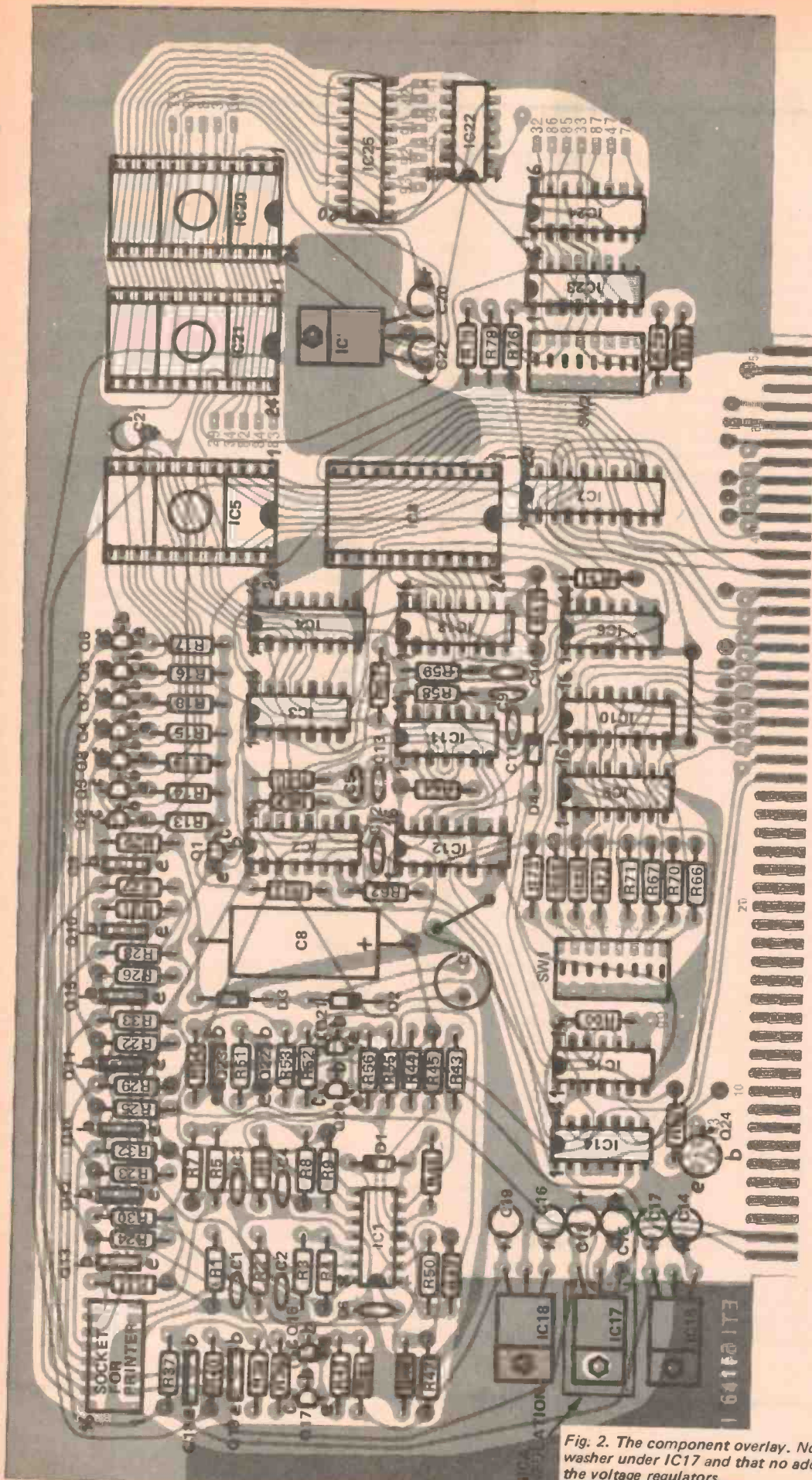
If a carriage return is detected the outputs of IC11/1 and IC11/2 will both go high, resetting IC12/1 preventing any further clocking of IC4. It also resets IC13 and clocks IC12/2 back to its original state where pin 14 is high and pin 15 low.

This allows data to be again entered, but as the reed switch is still closed the motor will continue to run due to the action of IC6/2,3 until the reed opens. If more than 32 characters were entered before the carriage return, after the first 32 characters have been printed pin 11 of IC13 will go low and the mono formed by C10/R59 causes IC12/1 to be reset, stopping IC4 from being clocked. IC12/2 however is not affected and the motor will continue to run, even after the reed switch opens. The printer then starts a second print stroke and the re-closing of the reed switch clocks IC12/1 allowing printing to continue.

The print head requires a negative 24 V pulse of 240 - 480 μ s width with a peak current of about 3 A (for only 10 μ s) while the metallization is evaporated. The drive consists of seven identical circuits each with an interface transistor and a drive darlington transistor. One additional transistor is used (Q1) to disable the print head while the EPROM is active during the write mode.

The carriage return detection is performed by the EPROM as part of its programming. As there are only seven heads but eight bits in the memory, the least significant bit is always programmed as '1' except for the carriage return character. While the CR character Ψ is programmed in the EPROM it cannot be accessed on this printer.

The auxiliary EPROMs use a standard address decoding and buffering circuit and do not require explanation.



CONNECTIONS

- Header
Pin No.
- 1 Head common
 - 2 Motor -Ve
 - 3 Motor +Ve
 - 6 Coil-reed common
 - 7 Pickup coil
 - 8 Reed switch
 - 10 Head 5
 - 11 Head 4
 - 12 Head 6
 - 13 Head 3
 - 14 Head 7
 - 15 Head 2
 - 16 Head 1

- Printer
Pin No.
- 1 Reed switch
 - 2 Pickup coil
 - 3 Coil-reed common
 - 4 Motor +Ve
 - 5 Motor -Ve
 - 6 Head common
 - 7 NC
 - 8 Head 1
 - 9 Head 2
 - 10 Head 3
 - 11 Head 4
 - 12 Head 5
 - 13 Head 6
 - 14 Head 7
 - 15 NC

Fig. 2. The component overlay. Note that there must be an insulating washer under IC17 and that no additional heat sinks are needed on the voltage regulators.

PARTS LIST - ETI 641

Resistors all 1/4W, 5%

R1,2	10k
R3	1k
R4	100k
R5-R8	10k
R9	47k
R10	82k
R11,12	10k
R13-R19	470R
R20-R26	1k5
R27-R33	10k
R34-R36	numbers not used
R37-R41	1k5
R42	1k
R43	10k
R44	47k
R45	1k
R46	100k
R47-R50	10k
R51-R55	1k5
R56	1k
R57	10k
R58,59	100k
R60	1k
R61	100k
R62	10k
R63	1k
R64	100k
R65	1k

R66-R73	10k
* R74-R78	10k

Capacitors

C1-C6	10n polyester
C7	100µ 25V electro
C8	220µ 35V electro
C9-C13	100p ceramic
C14,15	10µ 25V electro
C16-C22	33µ 16V tantalum

Semiconductors

IC1	LM324 quad op-amp
IC2	74LS123 dual mono
IC3	4023 three input NAND
IC4	4520 dual ÷ 16
IC5	2708 8K EPROM
IC6	4001 two input NOR
IC7	81LS97 octal buffer
IC8	6810 128x8 RAM
IC9,10	74LS85 comparator
IC11	4011 two input NAND
IC12	4027 dual JK flipflop
IC13	4520 dual ÷ 16
IC14	74LS10 three input NAND
IC15	74LS02 two input NOR
IC16	7812 positive 12V reg.
IC17	7912 negative 12V reg.
IC18	7805 positive 5V reg.

IC19	7905 negative 5V reg.
* IC20,21	2708 8K EPROM
* IC22	74LS00 two input NAND
* IC23,24	74LS85 comparator
* IC25	81LS97 octal buffer

Q1-Q8	BC558
Q9-Q15	BD675
Q16	BC548
Q17	BC558
Q18	BD140
Q19	BD139
Q20	BC548
Q21	BC558
Q22	BD140
Q23	BD139
Q24	2N3643
D1	1N914
D2,3	1N4001
D4	1N914

Miscellaneous
 PC board ETI 641
 Mosaic printer EUY-10E023LE
 Four 24 pin sockets
 One 16 pin socket and header
 Two 8 pole DIP switches
 One 15 pin 0.156 inch edge connector
 * These components are not required if the additional memory is not needed.

Construction

As this is an economical printer, it was decided that the expense of a through-hole plated pcb was not warranted. This means that a lot of components are soldered on both sides of the board preventing the use of sockets except for the EPROMs and the 6810 RAM.

The board can be assembled with the aid of the overlay in fig. 2. If the additional EPROMs are not required these ICs and the associated components can be deleted. None of the components in this area are used as feedthroughs for the printer electronics. In the printer circuitry there are two links in the 0 V rail and three more leading to the edge connector. If the additional EPROMs are used all the address and data lines are linked to the edge connector as it was not possible (without a plated-through board) to use copper tracks. We used thin enamelled wire of the type where the enamel will melt on soldering for all these links. The numbers on the pcb next to these points indicate the pins on the edge connector to which they are to be linked. Note that the connector is numbered 1 - 50 on the component side and 51 - 100 on the copper side.

Connection to the printer is made via a 16 pin IC socket using a piece of ribbon cable and a 16 pin DIP header.

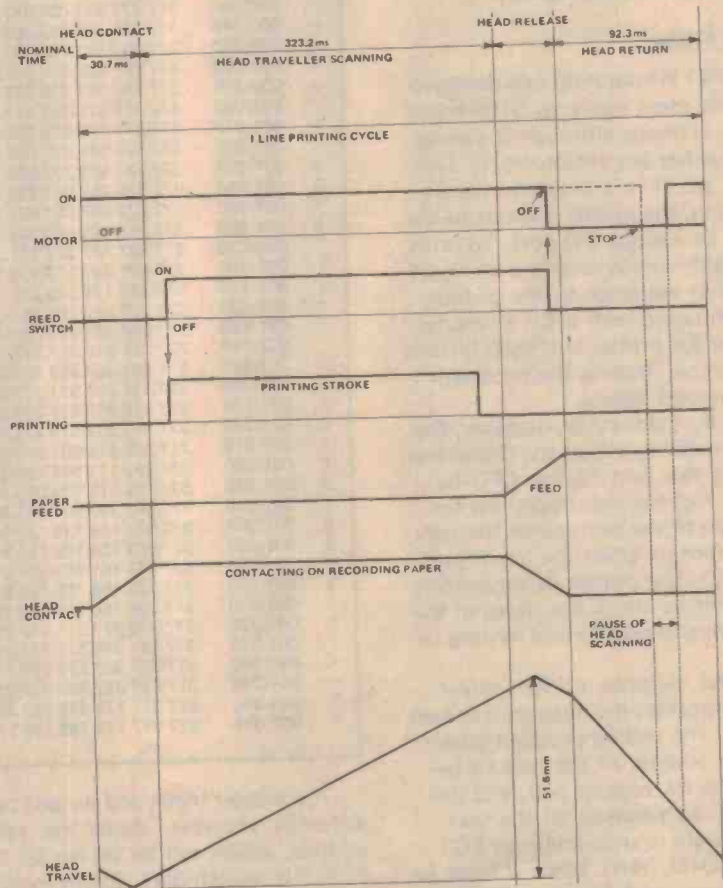


Fig. 3. The timing chart for the printer.

This method simplifies the software required and only ties up the processor long enough for it to output data at its own rate.

As we had some space left over on the card we decided to make provision for two additional 2708 EPROMs and their associated decoding/buffering. These are completely independent of the printer logic and can be used to store any software the user wishes. We do use another 2708 as the character generator as we were unable to find a suitable commercial device at a reasonable price. As this EPROM has 1024 locations, using eight bytes per character, we can have 128 characters. We therefore chose the full upper and lower case font with some Greek and mathematical symbols thrown in for good measure. As we are limited to a 5 x 7 dot matrix character some of the lower case characters are a bit strange (the ones with tails normally below the line) but are still quite legible.

Using the Printer

The ET1 641 Printer has been designed to interface most easily to S100-based computer systems, although it can be used with other bus structures, or even no bus at all. If it is plugged into an S100 system, the printer appears to the system to be a single I/O port. To print, the processor simply writes a string of characters in sequence to the output port, terminating with a CR character, whereupon the printer will itself initiate the print cycle, freeing the processor from any housekeeping.

During the print cycle, however, the printer is unable to accept any characters, and signals this fact to the CPU by pulling bit 7 of the input port low for the duration of the print cycle (though this only appears when the input port is addressed). The printer driver routine should therefore check the status of the printer from this port before writing to it.

A general purpose printer driver which incorporates this feature is shown in Table 2. The calling program passes the starting address of the text to be output in the HL register pair, and the routine will then output all the text from there until it encounters an EOT character (004Q, 04H). When it finds an EOT, the routine substitutes a CR and outputs it to the printer to start the print cycle.

Table 1

α	000:000	377 363 355 355 363 355 377 377	@	002:000	377 203 175 105 125 207 377 377
β	000:010	377 377 201 155 155 223 377 377	A	002:010	377 201 167 157 157 201 377 377
γ	000:020	377 163 155 201 277 177 377 377	B	002:020	377 001 155 155 155 223 377 377
δ	000:030	377 223 155 155 163 377 377 377	C	002:030	377 203 175 175 175 273 377 377
ε	000:040	377 377 343 325 325 377 377 377	D	002:040	377 001 175 175 175 203 377 377
θ	000:050	377 203 155 155 155 203 377 377	E	002:050	377 001 155 155 155 175 377 377
ι	000:060	377 377 343 375 373 377 377 377	F	002:060	377 001 157 157 157 177 377 377
λ	000:070	377 335 353 367 373 375 377 377	G	002:070	377 203 175 175 155 141 377 377
μ	000:100	377 377 201 367 367 217 377 377	H	002:100	377 001 357 357 357 001 377 377
ν	000:110	377 337 301 373 367 317 377 377	I	002:110	377 377 175 001 175 377 377 377
π	000:120	377 357 301 337 301 337 377 377	J	002:120	377 373 175 175 003 177 377 377
Σ	000:130	377 175 071 105 155 175 377 377	K	002:130	377 001 357 327 273 175 377 377
Φ	000:140	377 347 333 001 333 347 377 377	L	002:140	377 001 375 375 375 375 377 377
ψ	000:150	376 316 366 000 366 316 376 376	M	002:150	377 001 277 317 277 001 377 377
ω	000:160	377 363 355 373 355 363 377 377	N	002:160	377 001 337 357 367 001 377 377
Ω	000:170	377 315 261 277 261 315 377 377	O	002:170	377 203 175 175 175 203 377 377
ο	000:200	377 377 363 355 355 363 377 377	P	002:200	377 001 157 157 157 237 377 377
ο	000:210	377 377 377 355 371 375 377 377	Q	002:210	377 203 175 165 173 205 377 377
α	000:220	377 377 365 331 325 355 377 377	R	002:220	377 001 157 147 153 235 377 377
α	000:230	377 377 333 335 325 353 377 377	S	002:230	377 235 155 155 155 163 377 377
α	000:240	377 377 237 157 157 237 377 377	T	002:240	377 177 177 001 177 177 377 377
α	000:250	377 377 267 147 127 267 377 377	U	002:250	377 003 375 375 375 003 377 377
α	000:260	377 333 333 213 333 333 377 377	V	002:260	377 007 373 375 373 007 377 377
α	000:270	377 357 357 253 357 357 377 377	W	002:270	377 003 375 343 375 003 377 377
α	000:300	377 267 157 267 333 267 377 377	X	002:300	377 071 327 357 327 071 377 377
α	000:310	377 367 373 001 177 177 377 377	Y	002:310	377 077 337 341 337 077 377 377
α	000:320	377 373 375 203 177 277 377 377	Z	002:320	377 171 165 155 135 075 377 377
α	000:330	377 377 377 001 377 377 377 377	[002:330	377 377 001 175 175 377 377 377
α	000:340	377 357 307 253 357 357 377 377	\	002:340	377 277 337 357 367 373 377 377
α	000:350	377 357 357 253 307 357 377 377]	002:350	377 377 175 175 001 377 377 377
α	000:360	377 357 337 203 337 357 377 377	^	002:360	377 337 277 177 277 337 377 377
α	000:370	377 357 367 203 367 357 377 377	-	002:370	377 375 375 375 375 375 377 377
α	001:000	377 377 377 377 377 377 377 377	`	003:000	377 377 177 277 375 377 377 377
α	001:010	377 377 377 015 377 377 377 377	a	003:010	377 373 325 325 325 341 377 377
α	001:020	377 377 037 377 037 377 377 377	b	003:020	377 001 355 355 355 363 377 377
α	001:030	377 327 001 327 001 327 377 377	c	003:030	377 377 343 335 335 335 377 377
α	001:040	377 333 253 001 253 267 377 377	d	003:040	377 363 355 355 355 001 377 377
α	001:050	377 073 067 357 331 271 377 377	e	003:050	377 377 343 325 325 347 377 377
α	001:060	377 363 215 145 233 366 377 377	f	003:060	377 377 357 201 157 277 377 377
α	001:070	377 377 337 277 177 377 377 377	g	003:070	377 377 357 327 325 343 377 377
α	001:100	377 377 307 273 175 377 377 377	h	003:100	377 377 001 357 357 361 377 377
α	001:110	377 377 175 273 307 377 377 377	i	003:110	377 377 355 241 375 377 377 377
α	001:120	377 327 357 203 357 327 377 377	j	003:120	377 377 377 375 243 377 377 377
α	001:130	377 357 357 203 357 357 377 377	k	003:130	377 377 001 367 353 335 377 377
α	001:140	377 377 375 363 377 377 377 377	l	003:140	377 377 175 001 375 377 377 377
α	001:150	377 357 357 357 357 357 377 377	m	003:150	377 341 337 347 337 341 377 377
α	001:160	377 377 377 371 377 377 377 377	n	003:160	377 377 341 337 337 341 377 377
α	001:170	377 373 367 357 337 277 377 377	o	003:170	377 377 343 335 335 343 377 377
α	001:200	377 377 203 175 175 203 377 377	p	003:200	377 377 301 327 327 357 377 377
α	001:210	377 377 275 001 375 377 377 377	q	003:210	377 357 327 327 301 375 377 377
α	001:220	377 275 171 165 155 235 377 377	r	003:220	377 377 301 357 337 337 377 377
α	001:230	377 173 175 135 055 163 377 377	s	003:230	377 357 325 325 325 373 377 377
α	001:240	377 347 327 267 001 367 377 377	t	003:240	377 377 337 203 335 377 377 377
α	001:250	377 033 135 135 135 143 377 377	u	003:250	377 303 375 375 301 375 377 377
α	001:260	377 303 255 155 155 363 377 377	v	003:260	377 307 373 375 373 307 377 377
α	001:270	377 177 161 157 137 077 377 377	w	003:270	377 303 375 363 375 303 377 377
α	001:300	377 223 155 155 155 223 377 377	x	003:300	377 335 353 367 353 335 377 377
α	001:310	377 237 155 155 153 207 377 377	y	003:310	377 377 317 367 365 303 377 377
α	001:320	377 377 377 311 377 377 377 377	z	003:320	377 335 331 325 315 335 377 377
α	001:330	377 377 375 311 377 377 377 377	⌋	003:330	377 357 357 223 175 175 377 377
α	001:340	377 357 327 273 175 377 377 377	⌋	003:340	377 377 377 021 377 377 377 377
α	001:350	377 327 327 327 327 327 377 377	⌋	003:350	377 175 175 223 357 357 377 377
α	001:360	377 377 175 273 327 357 377 377	⌋	003:360	377 357 337 357 357 357 377 377
α	001:370	377 277 177 145 137 277 377 377	⌋	003:370	377 125 253 125 253 125 377 377

The printer input and output ports, although separate, share the same address, which can be set up on the 8-bit DIL switch SW1. In our example, the printer is set up for I/O address 031Q (19H). Although, the routine given is assembled at 001:000Q (0100H),

it can easily be reassembled to any other address. Be sure when trying out the program, to initialise the Stack Pointer, as otherwise, the routine will return to 377:377Q and 'gallop off into the wide blue yonder', possibly self-destructing for good measure.

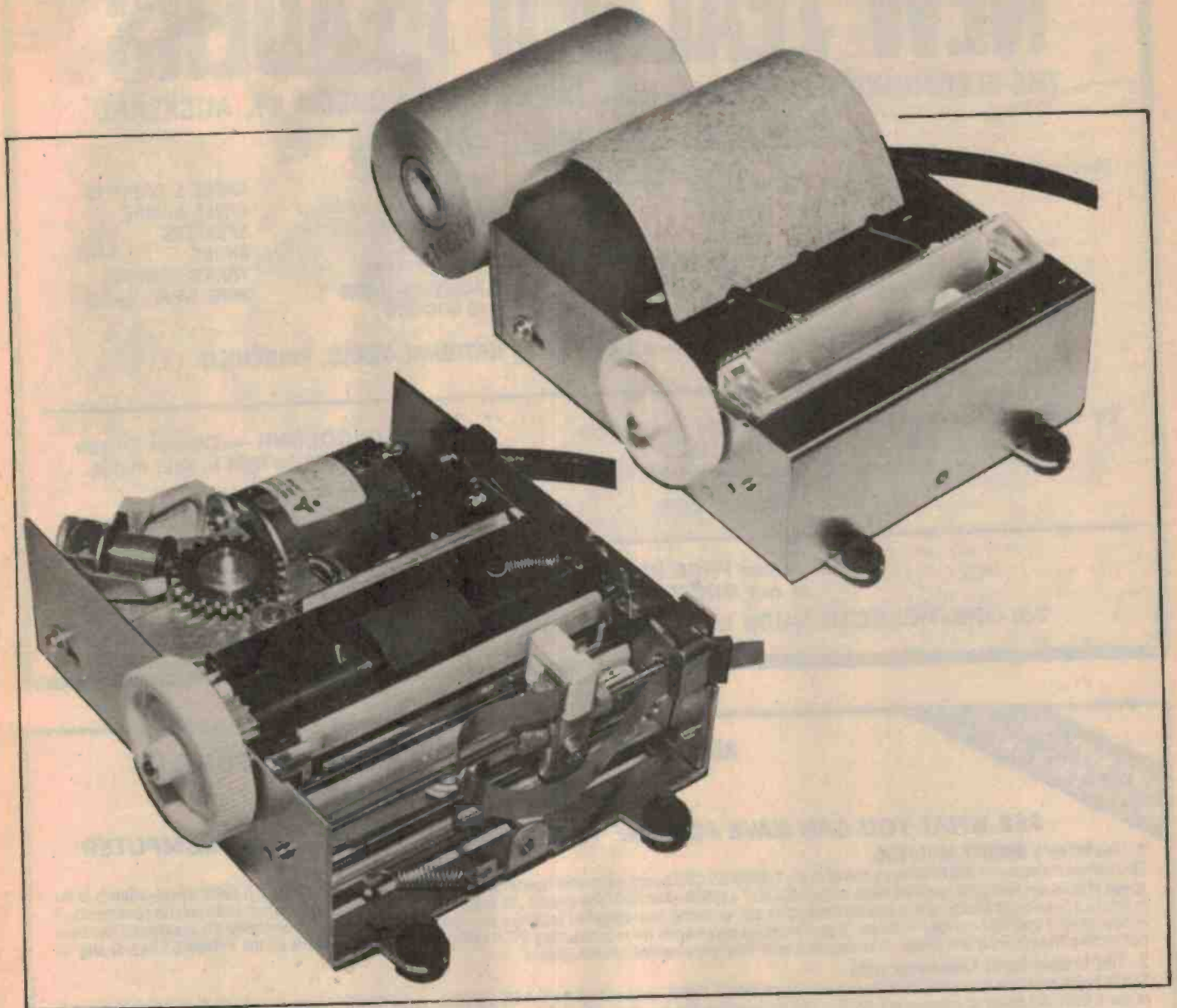


Table 2

Address	Op Code	Op 2	Op 3	Label	Instruction	Comment
001:000	333	031		PRINT	IN	PRINTER
001:002	376	177			CPI	177Q
001:004	312	000	001		JZ	PRINT
001:007	176				MOV	A,M
001:010	043				INX	H
001:011	376	004			CPI	004Q
001:013	312	023	001		JZ	END
001:016	323	031			OUT	PRINTER
001:020	303	000	001		JMP	PRINT
001:023	076	015		END	MVI	A,015Q
001:025	323	031			OUT	PRINTER
001:027	311				RET	
						CHECK STATUS BIT 7 ZERO? LOOP IF YES FETCH CHAR NEXT CHAR EOT? END IF YES OUTPUT CHAR ROUND AGAIN LOAD CR PRINT CR BACK TO CALLING ROUTINE

This general-purpose printer driver routine will output a character string until it comes to an EOT character, when it will output a CR to begin the print cycle. Beware if reassembling this program that your assembler can differentiate between the labels PRINT and PRINTER — it may be wise to choose alternative labels.

Another common trick used to indicate the end of message text is to set the most significant bit of the last character — as this is 7-bit ASCII it will not affect the printer or the CPU. However, the printer driver should recognise this and insert a CR, otherwise nothing will be printed.

The two EPROM sockets are addressed as a contiguous 2 K block of memory — they cannot be split apart. Consequently only 5 bits of address information have to be set on SW2 — one more bit selects which 2708 is addressed, and the final 10 bits are decoded inside the 2708's.

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4008	.75	7406	.25	7483	.75	74192	.75	74L02	.20	74S194	1.05
4009	.35	7407	.55	7485	.55	74193	.85	74L03	.25	74S257 (8123)	1.05
4010	.35	7408	.15	7486	.25	74194	.95	74L04	.30		
4011	.20	7409	.15	7489	1.05	74195	.95	74L10	.20	74LS00	.20
4012	.20	7410	.15	7490	.45	74196	.95	74L20	.35	74LS01	.20
4013	.40	7411	.25	7491	.70	74197	.95	74L30	.45	74LS02	.20
4014	.75	7412	.25	7492	.45	74198	1.45	74L47	1.95	74LS04	.20
4015	.75	7413	.25	7493	.35	74221	1.00	74L51	.45	74LS05	.25
4016	.35	7414	.75	7494	.75	74367	.75	74L55	.65	74LS08	.25
4017	.75	7416	.25	7495	.60			74L72	.45	74LS09	.25
4018	.75	7417	.40	7496	.80	75108A	.35	74L73	.40	74LS10	.25
4019	.35	7420	.15	74100	1.15	75491	.50	74L74	.45	74LS11	.25
4020	.85	7426	.25	74107	.25	75492	.50	74L75	.55	74LS20	.20
4021	.75	7427	.25	74121	.35			74L93	.55	74LS21	.25
4022	.75	7430	.15	74122	.55			74L123	.85	74LS22	.25
4023	.20	7432	.20	74123	.35	74H00	.15			74LS32	.25
4024	.75	7437	.20	74125	.45	74H01	.20	74S00	.35	74LS37	.25
4025	.20	7438	.20	74126	.35	74H04	.20	74S02	.35	74LS38	.35
4026	1.95	7440	.20	74132	.75	74H05	.20	74S03	.25	74LS40	.30
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4028	.75	7442	.45	74150	.85	74H10	.35	74S05	.35	74LS51	.35
4030	.35	7443	.45	74151	.65	74H11	.25	74S08	.35	74LS74	.35
4033	1.50	7444	.45	74153	.75	74H15	.45	74S10	.35	74LS86	.35
4034	2.45	7445	.65	74154	.95	74H20	.25	74S11	.35	74LS90	.55
4035	.75	7446	.70	74156	.70	74H21	.25	74S20	.25	74LS93	.55
4040	.75	7447	.70	74157	.65	74H22	.40	74S40	.20	74LS107	.40
4041	.69	7448	.50	74161	.55	74H30	.20	74S50	.20	74LS123	1.00
4042	.65	7450	.25	74163	.85	74H40	.25	74S51	.25	74LS151	.75
4043	.50	7451	.25	74164	.60	74H50	.25	74S64	.15	74LS153	.75
4044	.65	7453	.20	74165	1.10	74H51	.25	74S74	.35	74LS157	.75
4046	1.25	7454	.25	74166	1.25	74H52	.15	74S112	.60	74LS164	1.00
4049	.45	7460	.40	74175	.80	74H53J	.25	74S114	.65	74LS193	.95
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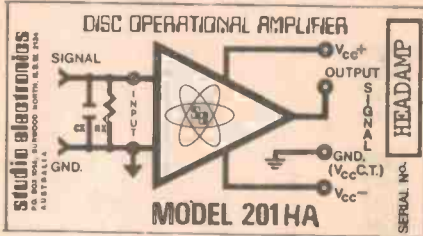
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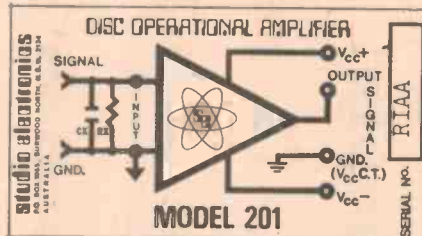
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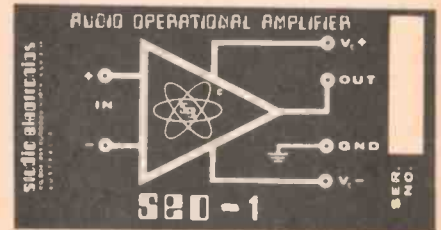
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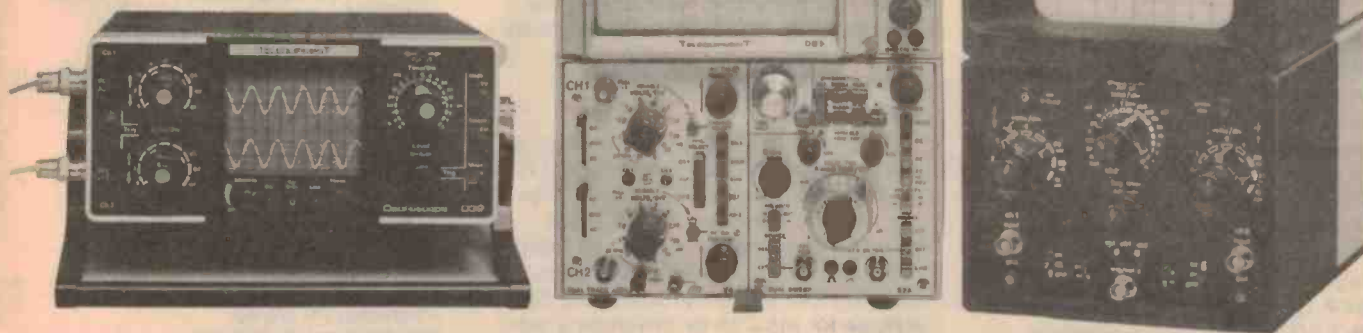
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TK11

DIGITAL ELECTRONICS

BY EXPERIMENT part 7

Continuing our series on TTL digital logic — this month decade counters.

THE 7490 DECADE COUNTER is a single-chip counter containing four flip-flops and various gates, which are arranged so that frequency division and decimal counting can be carried out. To make the counter more versatile, one flip-flop is separately connected so that it can be independently used as a scale-of-two counter, and the remaining three flip-flops are gates so that they act as a scale-of-five. The two sections of the counter can be connected together in different ways, either as a divide-by-ten circuit, or as a decimal counter with BCD outputs.

Twos Into Tens

BCD — meaning Binary-Coded-Decimal — is a form of binary code which is particularly useful if decimal numbers have to be displayed. In a BCD count, each figure of a decimal number is represented by its binary equivalent, so that the number 85 (decimal) becomes 1000 0101, binary 8 and binary 5. Although more convenient, because each BCD counter can then drive a display unit, this form is longer than a pure binary number (binary 85 = 1010101, only seven figures), and BCD numbers are not so simple to add and subtract as pure binary numbers.

BCD in Practice

Connect the power supplies to the 7490 with pin 10 to earth and pin 5 to +5 V. Pins 2 and 7 should also be earthed for most of the experimental work in this section, although we may use pin 2 later for resetting to zero. Now connect LEDs and their limiting resistors, using the spare pads on the board, to Qa on pin 12 and Qd on pin 11. Connect the clock pulse from the slow oscillator to input A (pin 14) and by watching the clock LED and the LED connected to pin 12 (Qa), note the action of this section of the counter.

Switch off, transfer the clock pulse input to input B on pin 1, and switch on again, watching the clock LED and the Qd LED on pin 11. Note that the counter will operate only if the

reset pins, each pair being inputs to an AND gate which operates the reset. Pins 2 and 3 are the reset to zero pins, and earthing either of them enables the counter. If both are allowed to float to logic 1, or are taken to logic 1, the counter resets to zero. Pins 6 and 7 also act through an AND gate, but with both high the reset is to BCD 9 (1001) rather than to zero.

To use the 7490 as a frequency divider (Fig. 2), we connect Qd (pin 11) to INa (pin 14) and take the clock pulse to INb (pin 1). The output will appear at Qa, on pin 12, and the state of this output is monitored by an LED already. Connect up the clock pulse from the slow oscillator on the board, and by counting pulses, confirm that the correct division ratio is being obtained.

For a BCD count, the connections must be changed around (Fig. 3). We now need LED indicators on the Qb (pin 9) and Qc (pin 8) outputs as well as on Qa (pin 12) and Qd (pin 11), and the cross-connections are different, with Qa connected to input B and the clock input taken to input A on pin 14. Label the LEDs as A, B, C, and D, and switch on, noting the values at each stage of the count. Use a de-bounced switch as a clock supply if the oscillator is too fast to follow. Note that in the circuit of Fig. 3 a reset switch has been used; because we are using push-to-make switches, an inverter must be used as shown.

Because the 7490 is on a single chip it may be more convenient to adapt it for counts of less than 10, rather than use separate flip-flops. This is made easier by the arrangement of the reset lines, connected through AND gates. Ignoring the reset-to-nine pins, we can arrange for pin 2 to be driven by a gate whose output must be zero during the count, rising to 1 at the end of the count. Pin 3 must be kept high, or the count will not be interrupted.

Try the circuit of Fig. 4 — can you work out what the count figure will be? Connect up and try the circuit out.

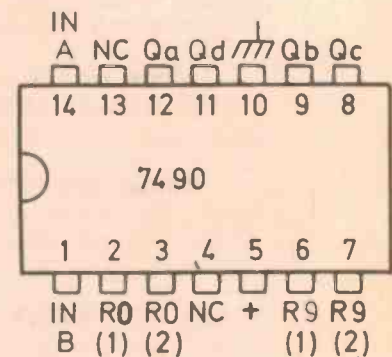


Fig 1. Pinout of 7490 Decade counter.

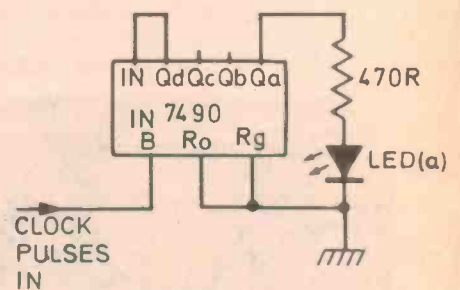


Fig 2. Connections for frequency division by ten — note that the symbol does not show the true pin positions.

Displays

Though several other forms of display exist, the most convenient type for use with TTL circuits is the seven-segment LED display. The type used for this board, the Jumbo DL747 is one of the largest displays of this type available at the time of writing, and has been selected from the point of view of easy reading at a distance. If any other type is substituted, care will have to be taken with the pin connections, since there are several pinout standards for this type of display.

As the name suggests, the seven-segment display consists of seven LEDs made in one chip in the arrangement of a figure-of-eight, as shown in Fig. 5. The letters allocated to the strips are also shown (fortunately these are standardised).

Looking at the arrangement of the segments, we can draw up a table of the segments that will have to be activated (ON) for each number we want to display. Fig. 6 shows such a table for the numbers 0 to 9, and also some of the other characters which can be obtained. We now have to translate this ON/OFF table into terms of logic 1 and 0.

The next step depends on the type of display that is being used — common cathode or common anode. As the name suggests, the common cathode display has all of the LED cathodes connected together to logic 0, and each anode must be taken to logic 1 to be illuminated. To prevent excessive current flowing — because the normal forward voltage across the LED is less than the +5 V of the logic circuits — we must wire a limiting resistor in the connection to each anode. We cannot use one single resistor in the cathode lead, as this would cause the brightness of the display to alter according to the number of segments lit.

The other possibility is to connect the anodes of the LEDs together and take the cathodes out to separate pins. In this common-anode type of display, the segments will be lit when their respective cathodes are at logic zero, and once again limiting resistors must be used between each cathode and the TTL driving stage.

The type of display specified for this board is a common anode type, with several of the pins on the display connected to the common anode. Only one of these pins need be connected to the 5V line.

Decoders

To obtain a decimal readout from the BCD output of the 7490 counter, a decoder stage, is needed with the truth table shown in Fig. 7.

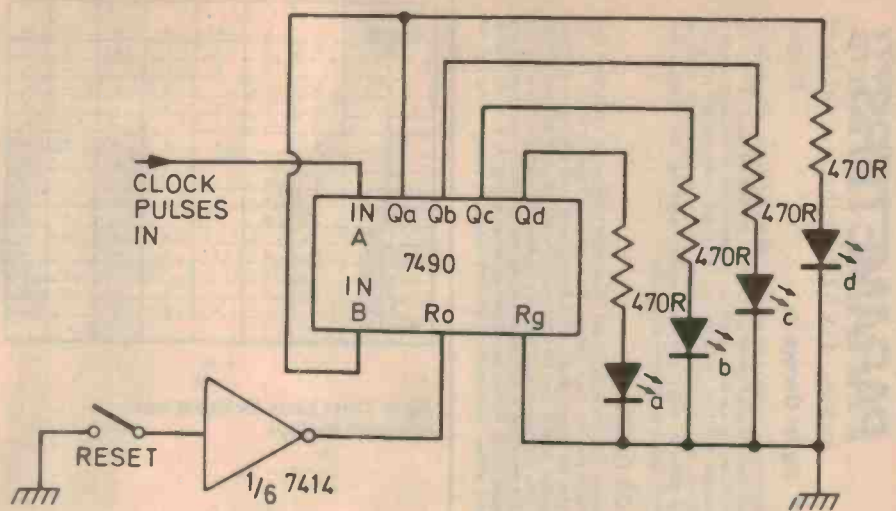


Fig 3. Connections for BCD counting, with reset switch. The reset pin must be kept at logic zero for counting, and taken to logic 1 for reset, so that an inverter must be used along with the push-button switch.

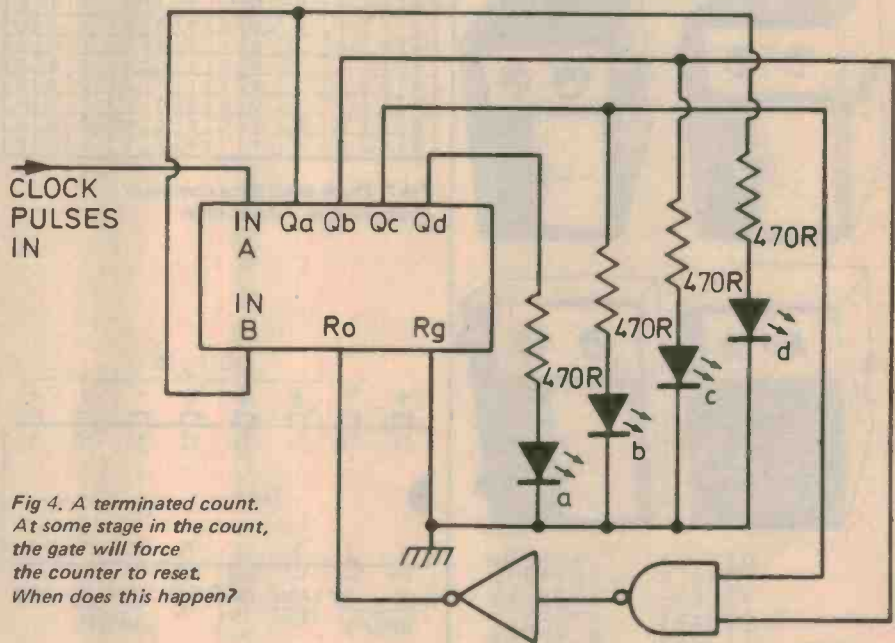
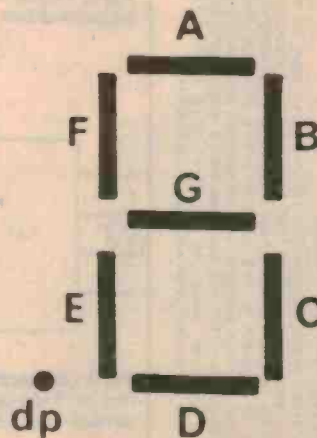


Fig 4. A terminated count. At some stage in the count, the gate will force the counter to reset. When does this happen?



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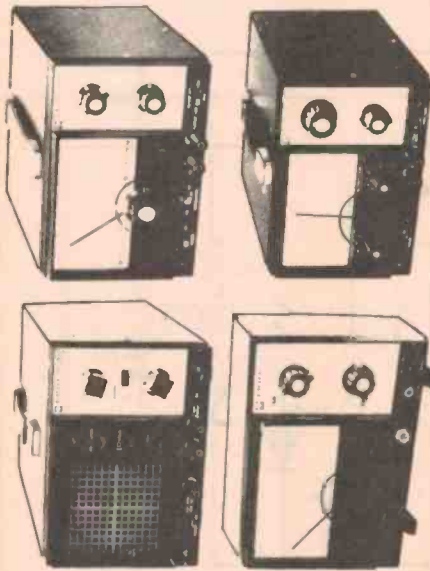
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- An external sync. input connector allows output frequency to synchronize with more accurate external signal
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Number/Character	a	b	c	d	e	f	g
0	x	x	x	x	x	x	x
1	-	x	x	x	-	-	-
2	x	x	x	-	x	-	x
3	x	x	x	x	-	-	x
4	-	x	x	-	-	x	x
5	-	-	x	x	-	x	x
6	x	x	x	x	x	x	x
7	x	x	x	-	x	-	-
8	x	x	x	x	x	x	x
9	x	x	x	-	-	x	x
(10)	x	-	-	x	x	-	-
(11)	x	x	x	x	-	-	-
(12)	-	x	-	-	-	x	x
(13)	x	x	-	x	-	-	-
(14)	-	-	x	x	x	x	x
Blank (15)	-	-	-	-	-	-	-

x - lit
- - unit

Fig 6 Truth table for figure and character displays.

	A	B	C	D	a	b	c	d	e	f	g
0	0	0	0	0	0	0	0	0	0	0	1
1	1	0	0	0	1	0	0	1	1	1	1
2	0	1	0	0	0	0	1	0	0	1	0
3	1	1	0	0	0	0	0	0	1	1	0
4	0	0	1	0	1	0	0	1	1	0	0
5	1	0	1	0	0	1	0	0	1	0	0
6	0	1	1	0	1	1	0	0	0	0	0
7	1	1	1	0	0	0	0	1	1	1	1
8	0	0	0	1	0	0	0	0	0	0	0
9	1	0	0	1	0	0	0	1	1	0	0

Fig 7 Truth table for a common-anode display, figures only.

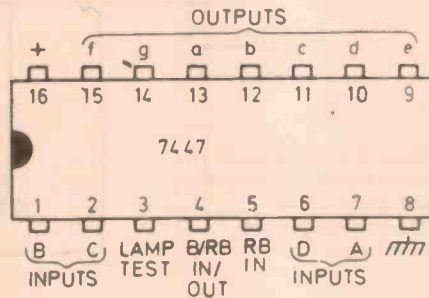


Fig 8. Pinout of the 7447 BCD to 7-segment decoder-driver.

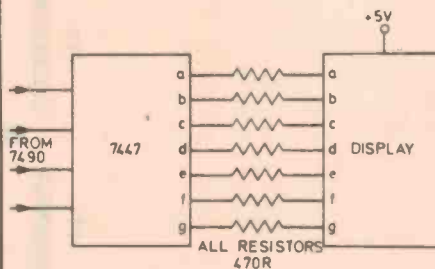


Fig 9. Connection of the 7447 to the display - not that the arrangement on the board is as neat as the drawing would suggest!

The type used here is the 7447 BCD-to-seven segment decoder/driver, which has output stages of transistor collectors with no loads. In this way, the combination of LED and limiting resistor acts as load for the collectors of the output transistors in the 7447.

Care should be taken that the outputs of a 7447 are never connected directly to the +5 V line, as excessive currents could flow if the decoder were operated.

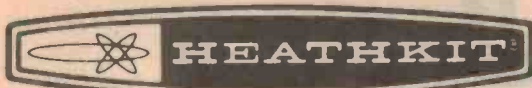
In use, the segment output pins of the 7447 are connected through the limiting resistors to the segment pins of the display. The values of the limiting resistors used will determine the brightness of the display. For the 7447 display we can use 150 R resistors, but 470R resistors have been specified on our board to ensure long life and to cut down current consumption. If other displays are used, 470R should also be suitable - in general the small displays need less current, and so larger values of limiting resistors should be used than with larger displays. If a common cathode display, such as the MAN-3 types, had been used, the 7448 decoder would have been needed.

Now connect up the display and the decoder on your board, noting the connection diagram of Fig. 9. In the prototype boards, the very small resistors used for limiting could be passed under the body of the display, so avoiding long paths around it. The +5 V supply is taken to pin 16 of the 7447, and earth is taken to pin 8. The outputs of the 7447, all on the side facing the display, and marked on the circuit diagram with small letters, are taken through the 470R limiters to the correspondingly lettered pins of the display. The inputs indicated by the capital letters A, B, C and D on pins 1, 2, 7 and 6 of the 7447 are for the BCD input from a 7490 and should be connected to the appropriate Q outputs from the 7490 counter.

Testing and Blanking

Note that pin 3 of the 7447 is labelled "lamp test". Taking this pin to logic 0 illuminates all segments of the display irrespective of what stage the count has reached, and is a useful check on the operation of the display. For example, an operator can check that a steady display of 8 is not just 3 with two segments faulty.

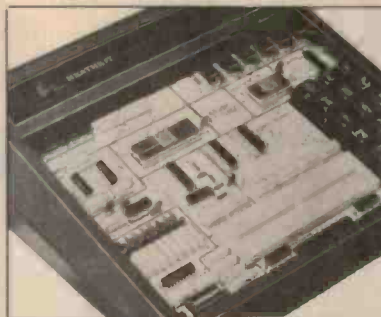
Pins 4 and 5 on the 7447 are for blanking, used mainly when the display is one of a set, to suppress zeros occurring before the first significant figures and after the last one. When pin 4 is low, the display is blanked out, though counting is unaffected.



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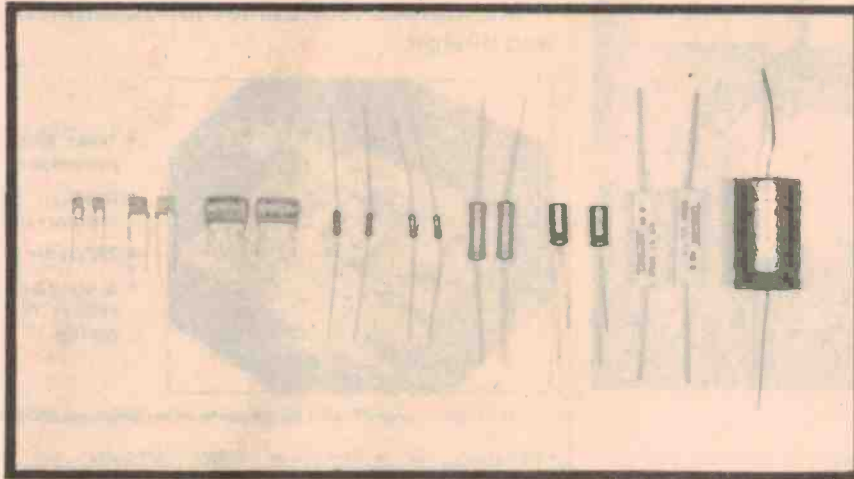
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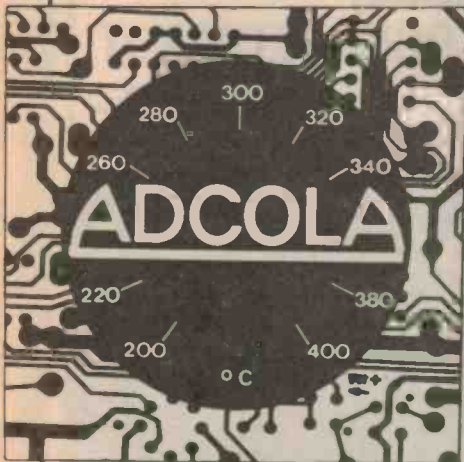
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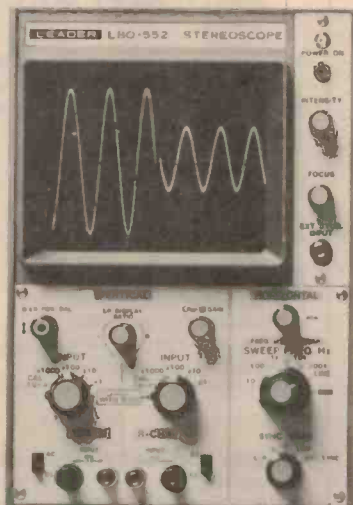
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CB COMMUNICATIONS

FCC propose 900 MHz PC band.

The FCC is considering establishing a new Personal Communications (PC) band in the United States around the 900 MHz region.

The proposed band would be at least 10 MHz wide and could be divided into 400 FM channels at 25 kHz spacing. If and when established, it would not replace the existing US 27 MHz CB band but would operate in addition to that service.

A legal conversion?

Johnson's Viking 352D 23 channel side-band rig was a very popular set in its heyday. If you own one and omitted/forgot/didn't bother to get it licensed before January 31 this year did you know that you could get a fully type approved 18 channel conversion done by Mike Skovron Agencies. And only \$35 too! That not only makes you legal — but you can resell the rig later too!

If you actually managed to license your 352D, and you want to go to 18 channels — remember you get two channels not on the 23 channel rigs, then you can have an 18 channel switch fitted for a mere \$25.

The type-approved conversion must be done by the *Mike Skovron Agencies* crew at 5 Curlewis St, Bondi Junction NSW (phone 30-4334). You'll get a rig to match the specs of the 4740-18 and a proper type-approval label pop-riveted on the back! Do it, and feel good.

Amazing! Fact! Shock release — draft RB14!

The long-awaited draft RB14 was finally released for (more or less) public consumption around 21 July. The NCRA has a few weeks preview and have already submitted a 'commentary' — more a rebuff really.

There are quite a few improvements over the first RB14 (still 'in force', even though it's not worth a pinch of goatsh). There are also a few things that won't curry much favour around the traps included in the draft. CB Australia's June issue front-page story foreshadowed most of the major changes.

However, while the P & T draftees have removed the original restrictions on antenna heights etc they have introduced a new 'rule' that disallows the use of antennas having more gain than a half-wave dipole. This is not going to be well received by a large body of Cbers and the CB industry alike. Instantly, such antennas as 5/8 groundplane base

antennas, the UHF 'gain' mobile antennas and the UHF collinear base antennas (6 dB omni-gain), are all 'not on mate'!

Good grief, any 27 MHz antenna offering 'substantial' real gain — like 10 dBi — is almost impossible to fit in the standard suburban real estate and restricting UHF users to nothing bigger than a 30 cm dipole antenna is ludicrous! If excessive TVI is feared, then it's not going to come from the use of 'gain' antennas. Linears and 'garbage' rigs are the trouble makers.

Among the concessions included in the draft are: up to five transceivers allowed per licensee; other persons (limited to family, employees and club associates) allowed to operate a licensee's rig; dedication of channels five on HF and UHF for emergency calling and traveller's assistance; no antenna height restrictions other than State — local government or Department of Transport requirements; no more '32 km rule' — which allows skip working within the geographical boundaries of Australia; introduction of 'notice of violation' system etc.

The full text of the new RB14 appears in the August issue of CB Australia.

Classy Wattmeter

In their 'classic' tradition, CPI present the WM7000 wattmeter — a comprehensive transmission performance test instrument. The WM7000 will read peak

or average power on three scales: 20, 200 and 1000 watts as well as VSWR over the frequency range from 1.8 to 30 MHz. It features a 30 dB coupler and a large, easy to read meter face.

For more information, contact *Communications Power Inc*, at P.O. Box 246, Double Bay 2028 or phone (02) 36-3703.

A Hi-fi CB Rig?

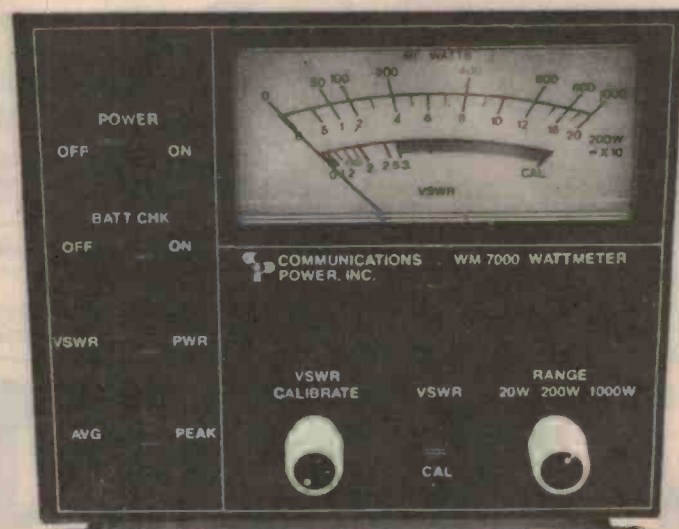
You might think their timing is wrong, you might wonder what the hell they're doing getting into the CB market, but Pioneer are determined that they have a winner with their first CB rig.

Called the GT-202, Pioneer's latest equipment release is an AM-only mobile rig specifically designed for under-dash mounting and features a unique slide-lock, theft-preventing mounting bracket.

Styling of the GT-202 follows on from Pioneer's long expertise in other consumer electronics markets — hi-fi and tape recorders ect. It is undoubtedly the smallest rig on the market at present as it measures a fine 150 mm wide by 50 mm high by 198 mm deep.

Technically it features a PLL frequency synthesizer, LED digital readout and a proper noise blanker — unusual on AM-only rigs. A dimmer push-button is provided to dim the LED display and S/R/F meter light for night time use.

The GT-202 will be available through Pioneer stores throughout Australia and selected retailers later.



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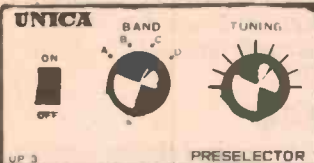
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TV502S 2m transverter	\$290.00
TR3200 70cm fm portable transceiver	\$229.00

6146B for Uniden, Kenwood, Yaesu	\$13.00
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VALVES



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RINGO RANGER



AMATEUR COMMUNICATIONS

Reyco antenna traps

Scalar Industries have recently been appointed sole Australian distributors for the Reyco range of multibrand trap antenna coils.

Designated type KW40, the coils are rated at 2 kW PEP (min.), weigh only about 180 grams and measure a compact 46 mm diameter by 140 mm long. They are encased in a waterproof coating for protection from the effects of the weather.

Construction of the coils is such that high Q values are achieved using aluminium wire wound on a threaded polystyrene former with an integral resonating capacitor.

A multi-band dipole can be readily constructed using the KW40 trap coils; complete details are available from *Scalar Industries, 18 Shelley Ave, Kilsyth Vic., 3137, (03) 725-9677*. They also have agencies in Sydney and Brisbane.

Combination counter/generator

An unusual test bench instrument was recently brought to our attention by GFS Electronics Imports. This is a combination frequency counter and RF signal generator manufactured by Mizuho. Designated DX555D, this compact little instrument features a generator coverage from 400 kHz to 30 MHz and a five-digit (switchable to seven digits) LED readout frequency counter that will read up to 220 MHz.

It measures only 160 x 58 x 215 mm and operates from the 240 Vac mains. For further information, contact *GFS Electronics Imports at 15 McKeon Rd, Mitcham, Vic, (03) 873-3939*.



Daiwa Coax Relays

Vicom have recently released a range of coaxial antenna changeover relays from the Japanese Daiwa Corporation.

Two models are available for different powers and frequency ranges. The first is rated at 100 W PEP and covers 1.8 MHz through 170 MHz; the second being rated at 200 W PEP covers from 1.8 to 450 MHz. Both feature extremely low insertion loss, 50 ohm impedance across the frequency range and operation from 10 – 15 volts DC.

For further information contact *Vicom P/L, 68 Eastern Rd, South Melbourne 3205, (03) 699-6700*.



Wadley-loop receiver from Standard

Standard Radio Company of Japan have produced a general coverage receiver using the now-common Wadley-loop technique for the front end, providing coverage from 500 kHz to 30 MHz in 1 MHz-wide bands.

Designated the type C-6500, it provides a dial readout down to 5 kHz and will resolve AM, SSB and CW signals. It may be operated from an internal battery supply (which requires eight cells), a 12 Vdc external supply, or the ac mains.

A large illuminated S-meter is featured on the receiver's front panel and an internal speaker is included. The C-6500 is currently available for around \$300 from *GFS Electronic Imports of 15 McKeon Rd, Mitcham Vic, (03) 873-3939*.

The 5A/0 battle

Most readers will be aware of the amateur fraternity's opposition to the allocation of channels 5A and 0 for 'special broadcasting' purposes and the proliferation of ch. 5A stations being proposed, particularly a high powered station for Mt Dundas in Victoria.

Committees under the auspices of the state Divisions of the WIA have been formed in all states, but a special technical committee was formed in Victoria to draft a submission for presentation to the Minister for Post and Telecommunications, Mr Tony Staley.

Mr Staley requested the submission be presented directly to him, with a copy to the P & T Department, early in August. However, it is likely that we will have to wait until after the budget session of Parliament before we'll hear any news.

Keep your fingers crossed.

US Antenna case won

John L. Schroeder, a Californian amateur accused of committing a criminal misdemeanour by violating a local zoning ordinance which restricted the height of radio and television antennas, has won a three-year long court battle against the California State courts, who were pressing for this conviction.

The California Supreme Court refused to review the case indicating that State courts do not have jurisdiction over radio interference cases. The Supreme Court decision means that the US Federal Government, through the FCC, has complete jurisdiction over "radio transmission, including assignment of frequencies and interference phenomena, and therefore State courts do not have jurisdiction to consider interference cases."

John Schroeder, who had the support of the Personal Communications Foundation in his battle through the courts, had claimed that the ordinance which limited antenna heights also violated the US Constitution.

The PCF backed him on this, saying that operation of an amateur radio station was clearly an exercise of freedom of speech! However, none of the courts petitioned, including the Supreme Court, agreed with this. They did say that had the ordinance restricted antenna heights only for interference reasons it would have been invalid, but that there were other justifications for restricting height, including safety and aesthetic considerations.

Two precedents have emerged from this case: Only the US Federal Government has the right to deal with such matters as TVI and frequency assignments; and restrictions imposed by State and local government authorities can only be imposed for other than radio interference reasons.



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PS Did you know Kenwood are to release a new solid state 30W PEP HF Mobile Transceiver with full 10M coverage, digital display and noise blander in OCTOBER — watch for further details.

SWL COMMUNICATIONS

Compiled by Peter Bunn,
on behalf of the Australian Radio DX Club (ARDXC).

The Australian Radio DX Club is a non-profit body with headquarters in Melbourne. For further information on shortwave radio, and on the activities of the ARDXC, please write to the General Secretary, PO Box 67, Highett, Vic. 3190, enclosing a 30c. stamp for return postage.

BBC Far Eastern Relay Station On The Move

The BBC is currently in the process of transferring its Far Eastern Relay transmitters from Tebrau in penninsular Malaysia to a site at Kranji in nearby Singapore. Adrian Peterson, Director of Adventist World Radio in Asia, recently paid a visit to the new Kranji shortwave relay base, and provides the following report:

Kranji is located on the northern edge of the island of Singapore, just 14 miles from the older station at Tebrau. When Kranji becomes fully operational, the Tebrau station will be phased out.

The BBC estate at Kranji contains just 4 acres, but into this compact area the construction engineers have erected a comprehensive antenna system and a large two story transmitter building. This building is constructed on cement piles because of swampy location. There are 17 self-supporting masts from which are strung 18 antennas. These antennas are slewable and reversible and are of various designs, some being unique to BBC broadcasting. They are intended for coverage of the BBC's several target areas in Asia.

Inside the main transmitter building is the transmitter hall, and the switching room for programmes. Four transmitters, each of 250 kilowatts, have been installed at Kranji, and two of these are currently operational. When the station is fully commissioned, there will be 4 transmitters of 250 kilowatts and 4 of 100 kilowatts, all of these transmitters having been originally located at the old site at Tebrau. Two of the older units of 100 kilowatts located at Tebrau will not be transferred to Kranji.

At present, off-air programs for the BBC Far Eastern Relay Station are received at Pongol on the south-west edge of Singapore island. The receiving antenna is actually located in the edge of the sea. Programs are sent by microwave link to Tebrau, where they are split for Kranji on shortwave and for Tanglin (on the edge of Singapore city) for FM broadcasting.



The first two shortwave transmitters at Kranji were switched into regular service on February 1st 1978. The transfer of transmitters from Tebrau is expected to be completed by late 1979, when the Malaysian relay site is expected to leave the air.

Many test broadcasts have been made from BBC Kranji, and these have been either test tones or broadcasts of the regular World Service or Asian language programs as carried by BBC Tebrau. Frequencies used have all been channels allocated to the Tebrau transmitters.

The schedule for the Kranji transmitters is not available, however their schedule up until September 3 was as follows: 6010 kHz 2200-2315, 6050 kHz 1215-1645, 6080 kHz 2315-0045, 6195 kHz 0900-1830, 7180 kHz 2200-0045 and 0930-1830, 9725 kHz 0930-1245, 11710 kHz 0015-0045, 11865 kHz 2200-2230.

DX On The Air

Radio station HCJB in Quito, Ecuador, has a weekly program for shortwave enthusiasts known as "DX Party Line" heard between 0900 and 0930 each Thursday. A new feature of the program is "South Pacific Report" presented once a month by Robert Hanner of the Australian Radio DX Club. Robert will feature comment and discussions of recent DXing activity and developments in Australia and the Pacific region. The next South Pacific Report is expected to be aired on DX Party Line of either Thursday September 21 or 28. Frequencies to tune to are: 11900, 9745 to 6130 kHz.

The Australian Radio DX Club now presents a "Pacific DX Report" over the

DX session heard on the Sri Lanka Broadcasting Corporation in Colombo. Aired monthly, this is also hosted by Robert Hanner, and the first segment went to air on September 4 during "Radio Monitors International" heard on Mondays at 1115 on frequencies of 11835, 15120 and 17850 kHz. Best reception in Australia is on 11835 kHz.

Latin American Round-up

The Colombian station, La Vox de la Selva at Florencia, which operates on 6170 kHz, gives excellent reception between 0700 and 1000 when operating to a 24 hour schedule. This station is one of the Caracol network stations, and many Caracol announcements may be heard during programming.

Radio Minería, at La Oroya, is a seldom heard Peruvian station which is currently audible on 6145 kHz, with popular songs noted between 1120 and 1200. The station usually identifies itself after each musical selection. Programmes are of course all in Spanish.

Further to our summary of Brazilian stations last issue, one Brazilian outlet giving unusually good reception at present is Radio Continental at Rio de Janeiro on 6195 kHz. Sign-on time for Radio Continental is generally 0900, and the station remains audible until 1000.

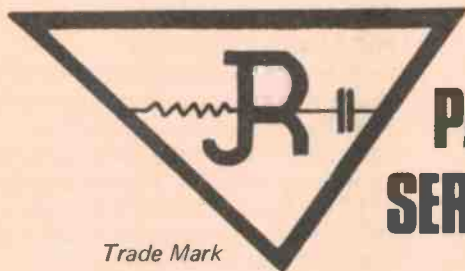
All times are given in Greenwich Mean Time (GMT) and you should add 10 hours to calculate Australian Eastern Standard Time.

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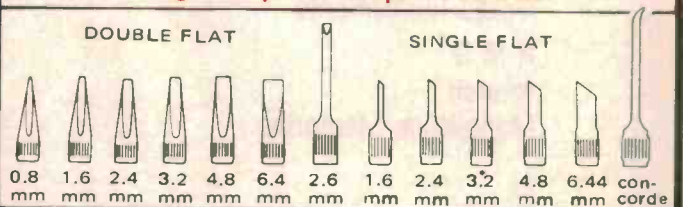
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We get many enquiries from readers wanting to know where they can get kits for the projects we publish. The list below indicates the suppliers we know about and the kits they do.

Any companies who want to be included in this list should phone LES BELL on 33-4282.

Key to companies:

- A** Applied Technology Pty. Ltd. 109-111 Hunter St, Hornsby. 2077. NSW.
- C** Amateur Communications Advancements, PO Box 57, Rozelle, NSW.
- D** Dick Smith Pty. Ltd. of Crows Nest, NSW. (see Ads. for address).
- E** All Electric Components (formerly ED & E Sales), 118 Lonsdale Street, Melbourne, Victoria, 3000.
- J** Jaycar Pty. Ltd. 405 Sussex St., Sydney 2000.
- L** Delsound Pty. 1 Wickham Terrace. Queensland.
- M** Mode Electronics. PO Box 365, Mascot 2020.
- N** Nebula Electronics Pty. Ltd. 15 - 19 Boundary St., Rushcutters Bay 2011. NSW.
- P** Pre-Pac Electronics. 718 Parramatta Rd., Croydon NSW 2132.
- T** Townsville Electronics Centre. 281E Charters Towers Rd, Rising Sun Arcade, Hermit Park. 4812

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ETI 048	Buzz Board	DS
ETI 061	Simple Amplifier	DATS
ETI 062	Simple Amplifier Tuner	DSE
ETI 063	Electronic Bongo's	DS
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ETI 065	Electronic Siren	DS
ETI 066	Temperature Alarm	ADTSE
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ETI 113	7-Input Thermocouple Meter	P,E
ETI 116	Impedance Meter	ES
ETI 117	Digital Voltmeter	E,AS
ETI 118	Simple Frequency Counter	E,AS
ETI 119	5V Switching Regulator supply	ETS
ETI 120	Logic Probe	L,ES
ETI 121	Logic Pulser	L,ES
ETI 122	Logic Tester	ES
ETI 123	CMOS Tester	ES
ETI 124	Tone Burst Generator	ES
ETI 128	Audio Millivoltmeter	L,ES
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ETI 133	Phase Meter	E
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ETI 220	Siren	ET
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ETI 236	Code Practice Oscillator	E
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ETI 313	Car Alarm	E,DT
ETI 316	Transistor Assisted Ignition	E
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ETI 406	One Transistor Receiver	T
ETI 408	Spring Reverb. Unit	E
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ETI 413	x 200 Watt Bridge Amp	SE
ETI 414	Master Mixer	E,J
ETI 416	25 Watt Amplifier	E
ETI 417	Amp Overload Indicator	E
ETI 419	Guitar Amp Pre-Amp	P,E,DT
ETI 420	Four-channel Amplifier	LE
ETI 420E	SQ Decoder	E
ETI 422	International Stereo Amp	SL,D
ETI 422B	Booster Amp	E
ETI 422	50 Watt Power Module	E
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ETI 425	Integrated Audio System	E
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ETI 429	Simple Stereo Amplifier	E
ETI 433	Active Crossover	J
ETI 435	Crossover Amp	J
ETI 438	Audio Level Meter	L,ES
ETI 440	Simple 25 Watt Amp	LE
ETI 441	Audio Noise Generator	L,ES
ETI 443	Compressor-Expander	E,J
ETI 444	Five Watt Stereo Preamp	ES
ETI 445	Preamp	J,E,D
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ETI 582	House Alarm	E
ETI 583	Gas Alarm	ME
ETI 586	Shutter Speed Timer	E

ELECTRONIC MUSIC

ETI 601	4600 Synthesiser	J
ETI 601	3600 Synthesiser	J
ETI 602	Mini Organ	E,A,D
ETI 604	Accentuated Beat Metronome	E

COMPUTER PROJECTS

ETI 630	Hex Display	AE
ETI 631	VDU Keyboard Encoder	AE
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ETI 633	VDU Sync Generator	AE

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ETI 702	Radar Intruder Alarm	DE
ETI 703	Antenna Matching Unit	E
ETI 704	Crosshatch/Dot Generator	L,A,D,ES
ETI 706	Marker Generator	ES
ETI 707	Modern Solid State Converters	C,E
ETI 708	Active Antenna	E
ETI 709	RF Attenuator	E
ETI 710	2 metre Booster	C,E
ETI 711B	Single Relay Remote Control	AE
ETI 711C	Double Relay Remote Control	AE
ETI 711R	Receiver	AE
ETI 711AR	Remote Control Transmitter	AE
ETI 711DR	Remote Control Decoder	AE
ETI 712	CB Power Supply	E
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ELECTRONIC GAMES

ETI 804	Selecta-Game	O,A,DS
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PCB's

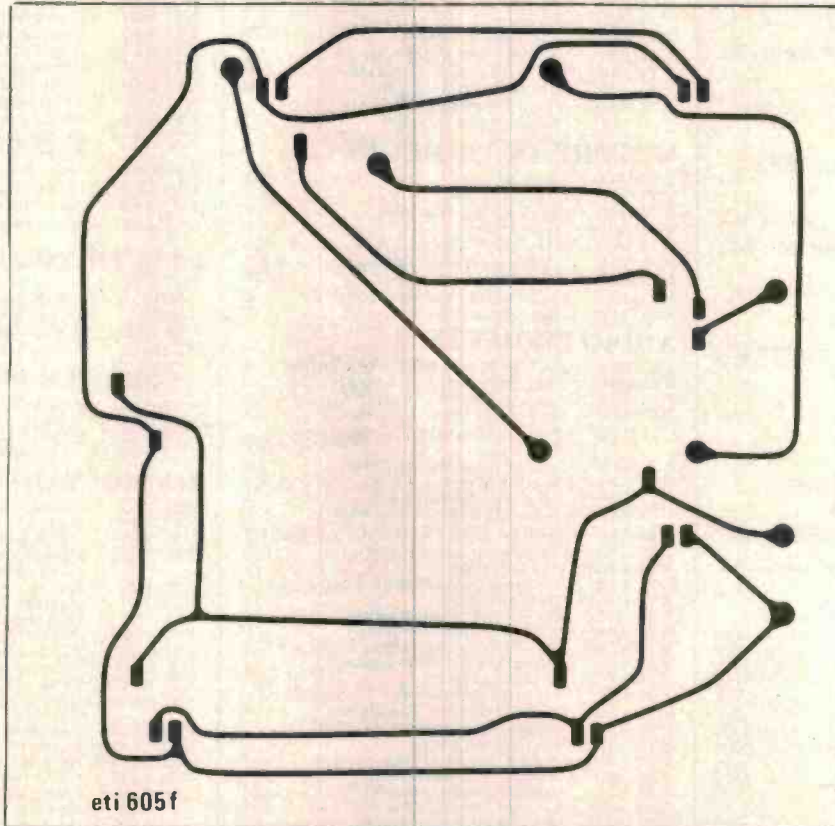
Using ETI PCB Artwork

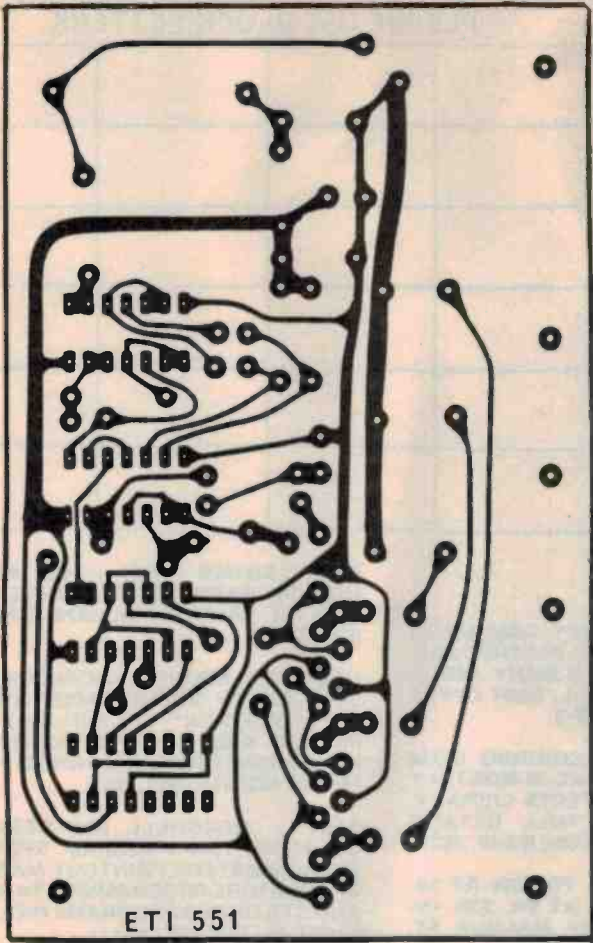
This method can be used to make negatives of ETI artwork from October 1977 on, provided the reverse of the page is printed in blue. The film used is Scotchcal 8007 which is UV sensitive and can be used under normal subdued light.

Cut a piece of film a little larger than the PC board and expose it to UV light through the magazine page. The non emulsion side should be in contact with the page. This surface can be detected by picking the film up by one corner - it will curl towards the emulsion side. Exposures of about 20 minutes are normally necessary.

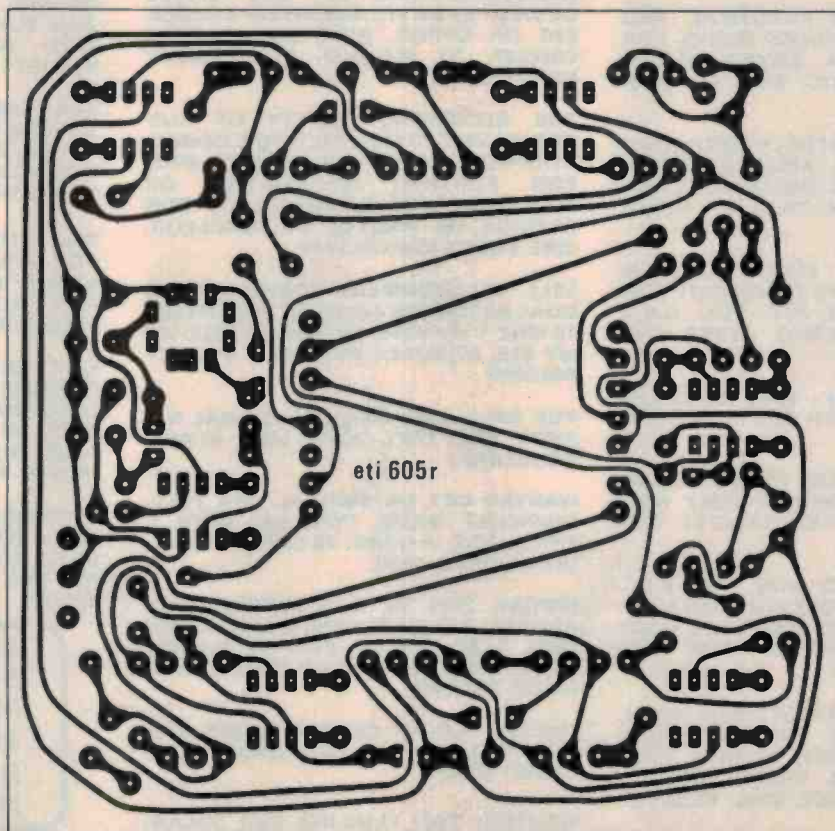
The film can now be developed by placing it emulsion side up on a table, pouring some Scotchcal 8500 developer on the surface and rubbing it with a clean tissue.

Further information on Scotchcal and PCB manufacture can be found in the September and December 1977 issues of ETI. Please note also, that occasionally pressure on space may unfortunately prohibit the printing of blue type behind all PCB's, in which case the reader must resort to more conventional photographic techniques for PCB manufacture.





The printed circuit board for the ETI 641 S100 Printer is a double sided, 125 x 250 mm (approx) board, and is too big to reproduce here. However, printed circuit board drawings for the ETI 641 are available from us on receipt of a large, stamped, self-addressed envelope. Write to: *ETI 641 PCB, Electronics Today International, 15 Boundary Street, Rushcutters Bay, NSW 2011.*



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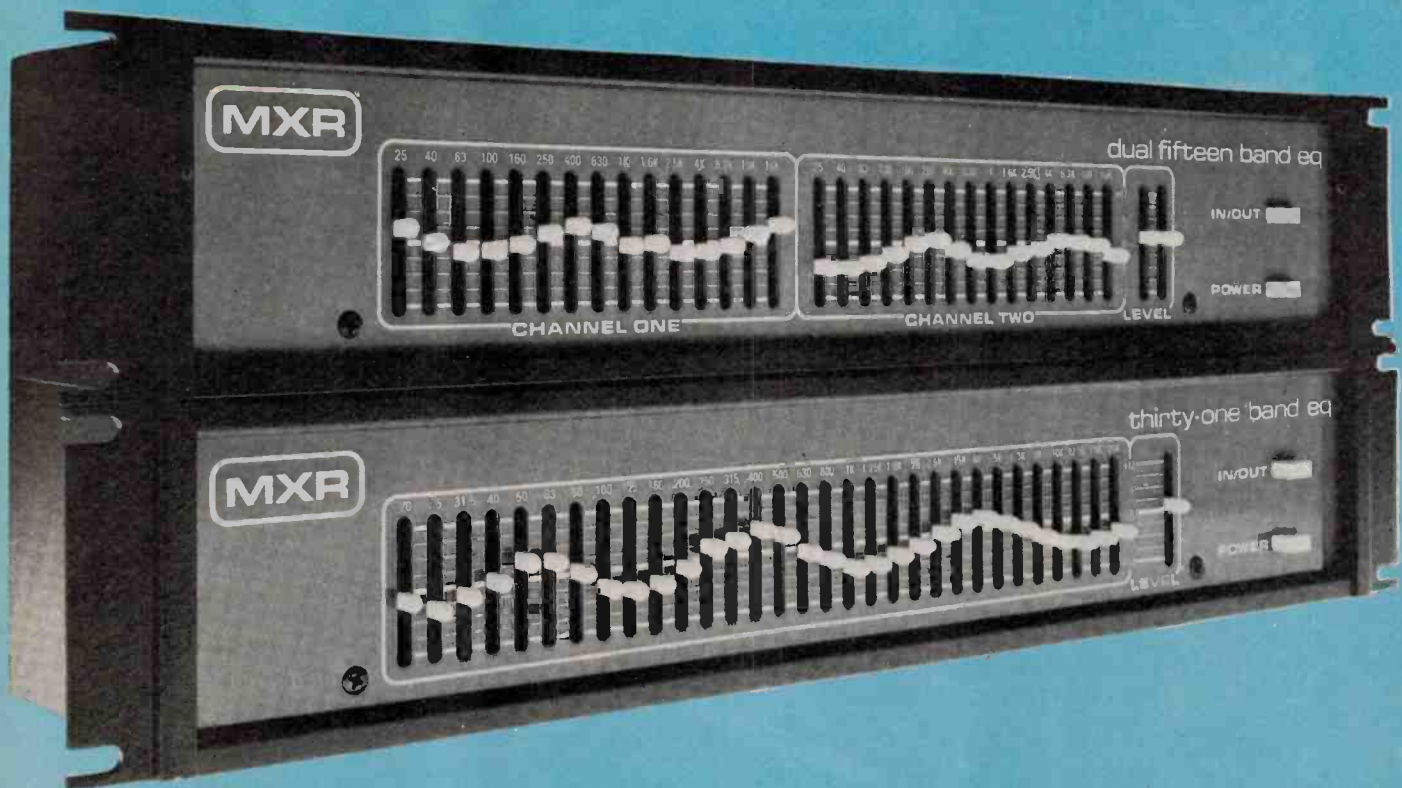
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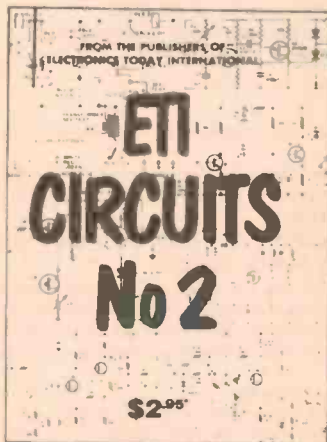


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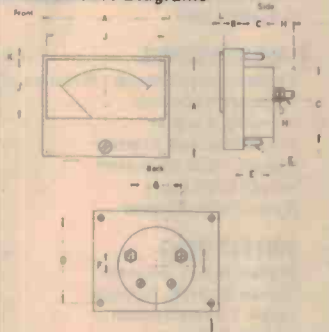
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Dimensional Diagrams



MODEL	VT-1	VT-2	VT-3	VT-4
A	86	78	56	46
A1	78	66	51	44
J1	50	42	31	26
C1	69	55.5	46	37.5
C	24	25	24.5	23.5
B	14	12	10.7	10.5
E1	13	13	10	10
E	3	3	3	2.3
H1	5	5	4	4
H	4	4	3	3
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BOOK REVIEWS



Electronics (2nd Edition), Sparkes, Hutchinson & Co, 1978, \$5.80.

Originally published in 1972 as *Electronics for Schools*, this volume forms a course in the fundamentals of electronics for 11 to 14 year old schoolchildren. The first eight chapters introduce the theory of electronics by means of practical experiments using cheap, easily available components.

The material in the book is covered at a fairly fast pace, although the difficulty level is not high - progress is smooth, with no gigantic 'leaps' in level. Chapter 2 introduces semiconductors, Chapter 3 covers 'controlling the transistor', Chapter 4 is about inverters, and Chapter 5 discusses other switching circuits. This material concerns only dc operation of the circuits, but Chapter 6 onwards more on to ac theory and amplifier circuitry.

The treatment is thoroughly non-mathematical, obviously a qualitative rather than quantitative approach to circuit operation. Once the student has a 'feel' for the operation of various components and circuits, Chapter 10 gives designs for 14 projects which may be attempted.

The book is well thought out and will provide a firm basis for further experiment. Our review copy was supplied by McGill's Authorised Newsagency of 187-193 Elizabeth Street, Melbourne, 3000.

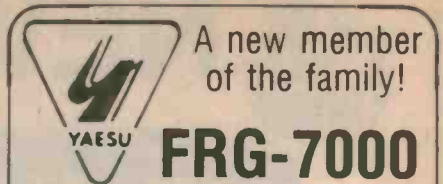


Programmable Calculators - Business Applications, Aronofsky, Frame and Greynolds, Jr, McGraw-Hill, 1978, \$9.85.

In reviewing a book like this, as an engineer it is difficult to put oneself into the position of a businessman who is new to the potential of programmable pocket calculators (PPC's). Most engineers have been using PPC's for some time now and are both numerate and logical enough to handle them with ease. Unfortunately, the impression one gets from this book is that businessmen are not so fortunate.

The bulk of the book deals with the programming features and logic of the TI-58 and -59 calculators in great depth - information that is of dubious value to the owner of one of these calculators since it is all explained in the handbook, and is of little interest to those who don't own one. However, the approach taken is to use examples of a business, rather than a scientific, nature. The examples are not very complex, but cover the calculation of uneven cash flows and elementary sensitivity analysis.

As a refresher course for a businessman who hasn't done any mathematics since his school days, the book would undoubtedly be of benefit, but we would suggest that any TI-58 or -59 owning reader of ETI is probably at a much more advanced level than this book. Our review copy was supplied by McGill's Authorised Newsagency of 187-193 Elizabeth Street, Melbourne, 3000.



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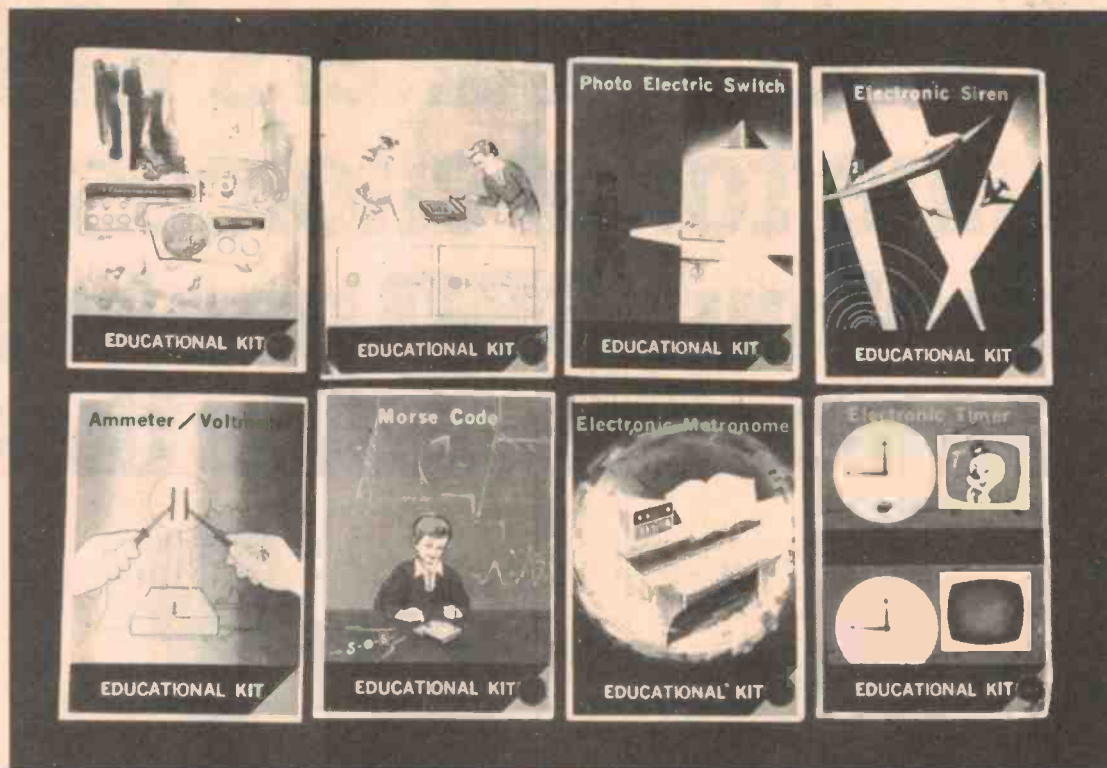


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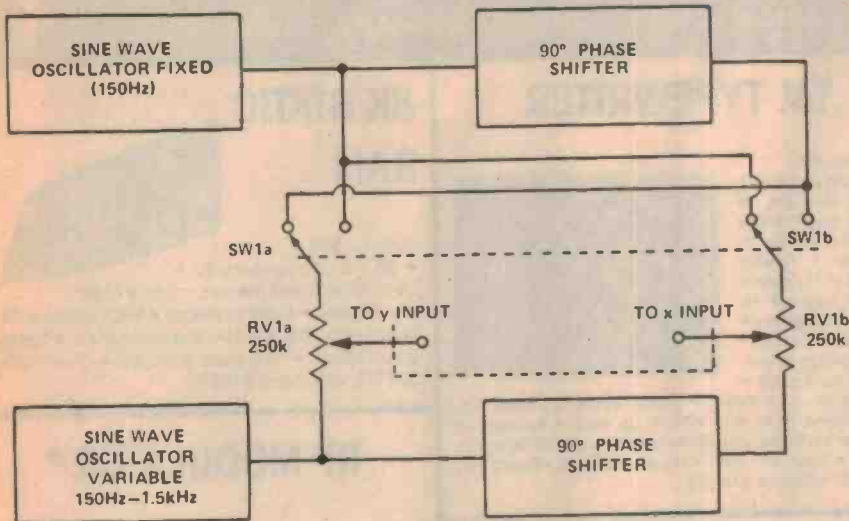


Fig. 1. Block diagram of the 'Spirograph'.

Electronic 'Spirograph'

The circuit will generate 'Spirograph' patterns on a conventional oscilloscope. The circuit consists of two sinewave generators followed by allpass filters which we use to phase shift the input signals by 90°. Applying a sinewave to the y input gives a circular trace. If a second set of sin and cos signals are mixed in, a 'Spirograph' pattern is obtained. A block diagram of the system is shown in Fig. 1.

RV1 is a balance control which varies the contribution of each oscillator to the pattern without affecting the size, so that once set up there is no need to re-adjust the gain controls on the oscilloscope. This type of control can only be used if the oscillators have a low impedance output.

SW1 is a reversing switch which has the effect of turning the pattern inside out.

An existing sinewave oscillator can of course be used and the 50 Hz mains could be employed (attenuated to about 2 V RMS from a low voltage transformer secondary) as the fixed oscillator. However flickering is a problem with lower frequencies (complex patterns requiring four or more cycles to complete will flicker at about 10 Hz using the mains frequency as an oscillator. I found 150 Hz to be a good compromise (higher frequencies require more critical tuning).

The allpass filter is recommended for phase splitting as it has a unity gain for all frequencies and settings of RV5.

First connect the y input of the scope to the output of an oscillator and adjust RV2 until a two volt RMS sine-wave is obtained, repeat for second

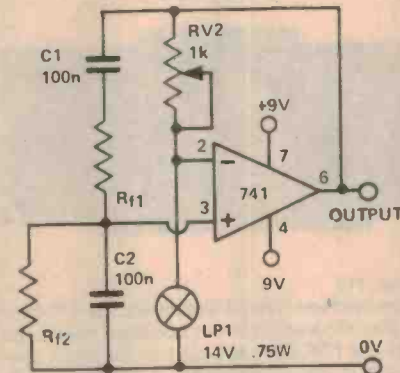


Fig. 2(a). Suitable oscillator for the 'Spirograph'.

oscillator. Then connect up the x and y inputs as shown in Fig. 1, turn the balance control to one end so as to look at the output of the fixed oscillator then adjust the 100 k pot until a circle

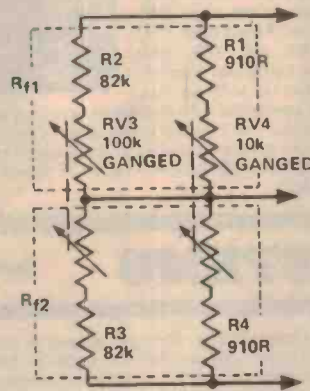
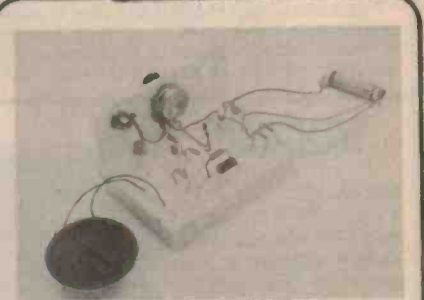


Fig. 2(b). Arrangement to give fine control of the frequency of the oscillator shown in Fig. 2(a). For 150 Hz fixed frequency use $Rf1 = Rf2 = 10 k$.

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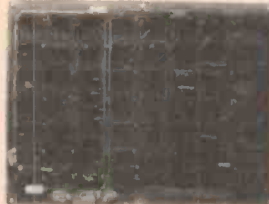
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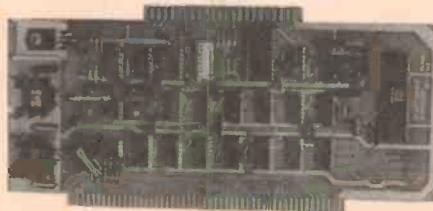
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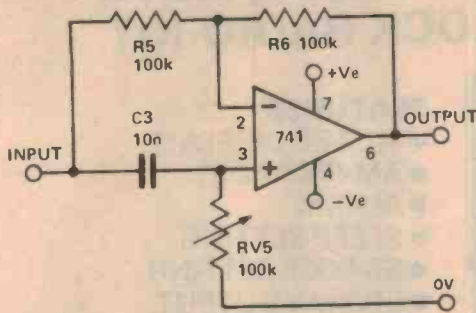


Fig. 3. Phase shifter circuit for use in the 'Spirograph' circuit.

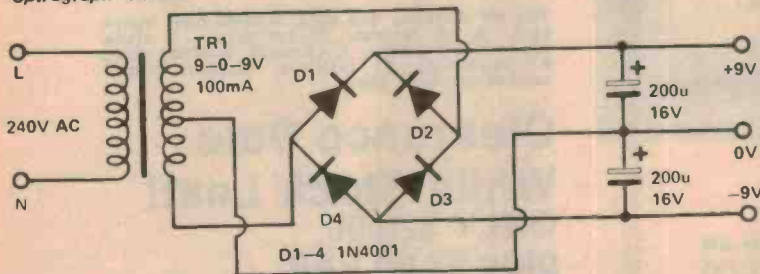
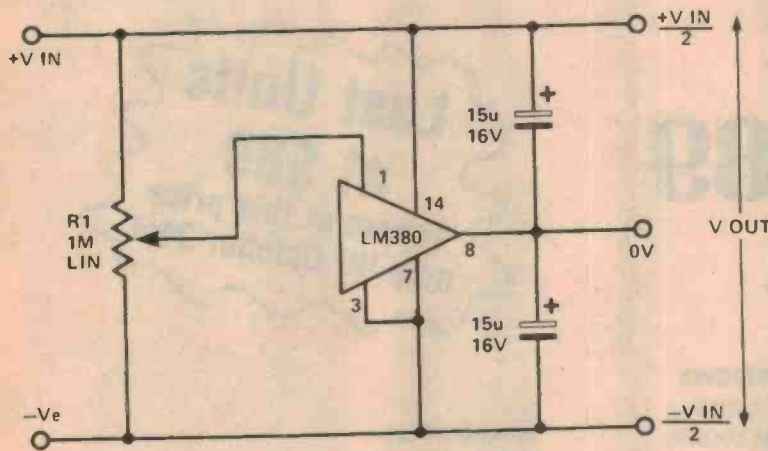


Fig. 4. PSU for 'Spirograph'.

is obtained (with suitable x and y gains). Now put the balance control in the middle and adjust the frequency controls until a stable pattern is produced. SW1 and RV1 the balance control can be used to alter the nature

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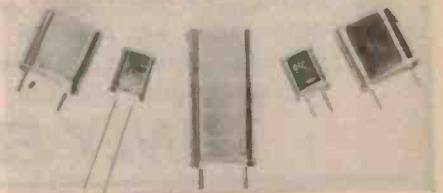
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Secretary: Charles O'Leary
 Publisher: Collyn Rivers

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Art Director: Sheila Tonic
 Assembly: Bill Crump/Simon Bracken
 Production Manager: Bob Izzard
 Subscriptions & Circulation: John Oxenford
 Project Design: Nebula Electronics
 Acoustical Consultants: Louis A. Challis & Assoc.

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Tokyo: Genzo Uchida, Bancho Media Service, 15 Sanyocho, Shintoku-Ku, Tokyo 160.

London: Electronics Today International, 25-27 Oxford St, London, W1R 1RF. Tel: 01-434-1781/2.

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Electronics Today International is published by Modern Magazines (Holdings) Ltd, 15 Boundary St., Rushcutters Bay, NSW 2011. It is printed (in 1978) by Wilke & Co., Browns Rd, Clayton, Victoria and distributed by Australian Consolidated Press.

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